



STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: siting.council@ct.gov

www.ct.gov/csc

VIA ELECTRONIC MAIL

November 4, 2019

Jake Shappy
Transcend Wireless
10 Industrial Avenue, Suite 3
Mahwah, NJ 07430

RE: **TS-SPRINT-077-191001** – Sprint Spectrum L.P. (“Sprint”) request for an order to approve tower sharing at an existing telecommunications facility located at 250 Olcott Street, Manchester, Connecticut.

Dear Mr. Shappy:

The Connecticut Siting Council (Council) is in receipt of your correspondence of October 30, 2019 submitted in response to the Council’s October 9, 2019 notification of an incomplete request for tower sharing with regard to the above-referenced matter.

The submission renders the request for tower sharing complete and the Council will process the request in accordance with the Federal Communications Commission 60-day timeframe.

Thank you for your attention and cooperation.

Sincerely,

Melanie A. Bachman
Executive Director

MAB/IN/emr



Robidoux, Evan

From: jshappy@transcendwireless.com
Sent: Wednesday, October 30, 2019 9:09 AM
To: Robidoux, Evan
Cc: CSC-DL Siting Council
Subject: RE: Council Incomplete Letter for TS-SPRINT-077-191001 (250 Olcott Street, Manchester, Connecticut)
Attachments: ts-sprint-077-191001_incompleteltr_OlcottSt.pdf; 18116.00 - CT03XC067 Mount Analysis Rev 0_19.10.29.pdf; 18116.00 - CT03XC067 - Structural Analysis Rev2 19.10.11.pdf

Evan,

Please see attached soft copies of the mount analysis and revised structural analysis for your review for this exempt mod. The hard copies will be sent to you as soon as they are received from the A&E.

Jake Shappy
10 Industrial Ave, Suite 3
Mahwah, NJ 07430
Cell: 845-553-3330
jshappy@transcendwireless.com

From: Robidoux, Evan <Evan.Robidoux@ct.gov>
Sent: Thursday, October 10, 2019 10:22 AM
To: 'jshappy@transcendwireless.com' <jshappy@transcendwireless.com>
Cc: CSC-DL Siting Council <Siting.Council@ct.gov>
Subject: Council Incomplete Letter for TS-SPRINT-077-191001 (250 Olcott Street, Manchester, Connecticut)

Please see the attached correspondence.

Evan Robidoux
Clerk Typist
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Structural Analysis Report

Antenna Mount Analysis

Sprint Site Ref: CT03XC067

*20 Olcott Street
Manchester, CT*

Centek Project No. 18116.00

Date: October 29, 2019

Max Stress Ratio = 75.4%

Prepared for:

*Transcend Wireless
10 Industrial Ave, Suite 3
Mahwah, NJ 07430*

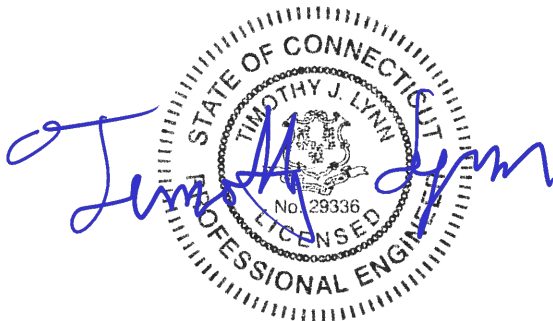


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- RF DATA SHEET, DATED 07/24/2018
- EQUIPMENT CUT SHEETS

October 29, 2019

Mr. Jake Shappy
Transcend Wireless
10 Industrial Ave
Mahwah, NJ 07430

Re: *Structural Letter ~ Antenna Mount*
Sprint – Site Ref: CT03XC067
20 Olcott Street
Manchester, CT 06040

Centek Project No. 18116.00

Dear Mr. Shappy,

Centek Engineering, Inc. has reviewed the Sprint antenna installation at the above referenced site. The purpose of the review is to determine the structural adequacy of the proposed mounts, consisting of three (3) 12-ft V-Frames (SitePro P/N: VFA12-HD-SPT), to support the equipment configuration. The review considered the effects of wind load, dead load and ice load in accordance with the 2018 Connecticut State Building Code (CTBC) including ASCE 7-10 and ANSI/TIA-222-G *Structural Standards for Steel Antenna Towers and Supporting Structures*.

The loads considered in this analysis consist of the following:

- Sprint:
V-Frames: Three (3) Commscope NNVV-65B-R4 panel antennas, three (3) Nokia AAHC panel antennas, three (3) 1900MHz 4X45W RRHs and six (6) 800MHz 2X50W RRHs mounted on three (3) 12-ft frames with a RAD center elevation of +/-135-ft AGL.

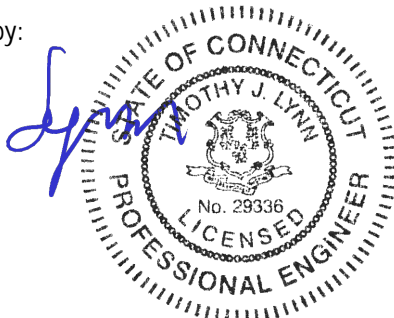
The antenna mount was analyzed per the requirements of the 2015 International Building Code as modified by the 2018 Connecticut State Building Code considering a nominal design wind speed of 97 mph for Manchester as required in Appendix N of the 2018 Connecticut State Building Code.

Based on our review of the installation, it is our opinion that the subject antenna mount has sufficient capacity to support the aforementioned antenna configuration. If there are any questions regarding this matter, please feel free to call.

Respectfully Submitted by:



Timothy J. Lynn, PE
Structural Engineer



Prepared by:



Fernando J. Palacios
Engineer

CEN TEK Engineering, Inc.
Structural Analysis – Mount Analysis
T-Mobile Site Ref. ~ CT03XC067
Manchester, CT
October 29, 2019

Section 2 - Calculations

Development of Design Heights, Exposure Coefficients, and Velocity Pressures Per TIA-222-G

Wind Speeds

Basic Wind Speed	V := 97	mph	(User Input - 2018 CSBC Appendix N)
Basic Wind Speed with Ice	V _i := 50	mph	(User Input per Annex B of TIA-222-G)

Input

Structure Type =	Structure_Type := Lattice	(User Input)
Structure Category =	SC := 11	(User Input)
Exposure Category =	Exp := C	(User Input)
Structure Height =	h := 180	ft (User Input)
Height to Center of Antennas =	Z _{Sprint} := 135	ft (User Input)
Radial Ice Thickness =	t _i := 1.00	in (User Input per Annex B of TIA-222-G)
Radial Ice Density =	l _d := 56.00	pcf (User Input)
Topographic Factor =	K _{zt} := 1.0	(User Input)
	K _a := 1.0	(User Input)
Gust Response Factor =	G _H = 0.85	(User Input)

Output

Wind Direction Probability Factor =	$K_d := \begin{cases} \text{if Structure_Type = Pole} & 0.95 \\ \text{if Structure_Type = Lattice} & 0.85 \end{cases} = 0.85$	(Per Table 2-2 of TIA-222-G)
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Importance Factors =	$I_{Wind} := \begin{cases} \text{if SC = 1} & 0.87 \\ \text{if SC = 2} & 1.00 \\ \text{if SC = 3} & 1.15 \end{cases} = 1$	(Per Table 2-3 of TIA-222-G)
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$K_{iz} := \left(\frac{Z_{Sprint}}{33} \right)^{0.1} = 1.151$	$I_{Wind_w_Ice} := \begin{cases} \text{if SC = 1} & 0 \\ \text{if SC = 2} & 1.00 \\ \text{if SC = 3} & 1.00 \end{cases} = 1$
	$I_{ice} := \begin{cases} \text{if SC = 1} & 0 \\ \text{if SC = 2} & 1.00 \\ \text{if SC = 3} & 1.25 \end{cases} = 1$

Velocity Pressure Coefficient Antennas =	$t_{iz} := 2.0 \cdot t_i \cdot I_{ice} \cdot K_{iz} \cdot K_{zt}^{0.35} = 2.303$
	$K_{Z_{Sprint}} := 2.01 \cdot \left(\frac{Z_{Sprint}}{z_g} \right)^\alpha = 1.348$

Velocity Pressure w/o Ice Antennas = $q_{Z_{Sprint}} := 0.00256 \cdot K_d \cdot K_{Z_{Sprint}} \cdot V^2 \cdot I_{Wind} = 27 \text{ psf}$

Velocity Pressure with Ice Antennas = $q_{Z_{ice.Sprint}} := 0.00256 \cdot K_d \cdot K_{Z_{Sprint}} \cdot V_i^2 \cdot I_{Wind} = 7 \text{ psf}$

Development of Wind & Ice Load on Antennas

Antenna Data:

Antenna Model =	Commscope NNVV-65B-R4	
Antenna Shape =	Flat	(User Input)
Antenna Height =	$L_{ant} := 72$	in (User Input)
Antenna Width =	$W_{ant} := 19.6$	in (User Input)
Antenna Thickness =	$T_{ant} := 7.8$	in (User Input)
Antenna Weight =	$WT_{ant} := 77.4$	lbs (User Input)
Number of Antennas =	$N_{ant} := 1$	(User Input)
Antenna Aspect Ratio =	$Ar_{ant} := \frac{L_{ant}}{W_{ant}} = 3.7$	
Antenna Force Coefficient =	$Ca_{ant} = 1.25$	

Wind Load (without ice)

Surface Area for One Antenna = $SA_{antF} := \frac{L_{ant} \cdot W_{ant}}{144} = 9.8$ sf

Total Antenna Wind Force Front = $F_{ant} := q_{z_{sprint}} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{antF} = 288$ lbs

Surface Area for One Antenna = $SA_{antS} := \frac{L_{ant} \cdot T_{ant}}{144} = 3.9$ sf

Total Antenna Wind Force Side = $F_{ant} := q_{z_{sprint}} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{antS} = 115$ lbs

Wind Load (with ice)

Surface Area for One Antenna w/ Ice = $SA_{ICEantF} := \frac{(L_{ant} + 2 \cdot t_{iz}) \cdot (W_{ant} + 2 \cdot t_{iz})}{144} = 12.9$ sf

Total Antenna Wind Force w/ Ice Front = $F_{ant} := q_{z_{ice, sprint}} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{ICEantF} = 101$ lbs

Surface Area for One Antenna w/ Ice = $SA_{ICEantS} := \frac{(L_{ant} + 2 \cdot t_{iz}) \cdot (T_{ant} + 2 \cdot t_{iz})}{144} = 6.6$ sf

Total Antenna Wind Force w/ Ice Side = $F_{ant} := q_{z_{ice, sprint}} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{ICEantS} = 52$ lbs

Gravity Load (without ice)

Weight of All Antennas = $WT_{ant} \cdot N_{ant} = 77$ lbs

Gravity Loads (ice only)

Volume of Each Antenna = $V_{ant} := L_{ant} \cdot W_{ant} \cdot T_{ant} = 1 \cdot 10^4$ cu in

Volume of Ice on Each Antenna = $V_{ice} := (L_{ant} + 2 \cdot t_{iz}) \cdot (W_{ant} + 2 \cdot t_{iz}) \cdot (T_{ant} + 2 \cdot t_{iz}) - V_{ant} = 1 \cdot 10^4$

Weight of Ice on Each Antenna = $W_{ICEant} := \frac{V_{ice}}{1728} \cdot \rho = 389$ lbs

Weight of Ice on All Antennas = $W_{ICEant} \cdot N_{ant} = 389$ lbs

Development of Wind & Ice Load on Antennas

Antenna Data:

Antenna Model =	Nokia AAHC	
Antenna Shape =	Flat	(User Input)
Antenna Height =	$L_{ant} := 25.6$	in (User Input)
Antenna Width =	$W_{ant} := 19.7$	in (User Input)
Antenna Thickness =	$T_{ant} := 9.6$	in (User Input)
Antenna Weight =	$WT_{ant} := 103.6$	lbs (User Input)
Number of Antennas =	$N_{ant} := 1$	(User Input)
Antenna Aspect Ratio =	$AR_{ant} := \frac{L_{ant}}{W_{ant}} = 1.3$	(User Input)
Antenna Force Coefficient =	$Ca_{ant} = 1.2$	

Wind Load (without ice)

Surface Area for One Antenna = $SA_{antF} := \frac{L_{ant} \cdot W_{ant}}{144} = 3.5$ sf

Total Antenna Wind Force Front = $F_{ant} := qZ_{Sprint} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{antF} = 99$ lbs

Surface Area for One Antenna = $SA_{antS} := \frac{L_{ant} \cdot T_{ant}}{144} = 1.7$ sf

Total Antenna Wind Force Side = $F_{ant} := qZ_{Sprint} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{antS} = 48$ lbs

Wind Load (with ice)

Surface Area for One Antenna w/ Ice = $SA_{ICEantF} := \frac{(L_{ant} + 2 \cdot t_{iz}) \cdot (W_{ant} + 2 \cdot t_{iz})}{144} = 5.1$ sf

Total Antenna Wind Force w/ Ice Front = $F_{ant} := qZ_{ice.Sprint} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{ICEantF} = 38$ lbs

Surface Area for One Antenna w/ Ice = $SA_{ICEantS} := \frac{(L_{ant} + 2 \cdot t_{iz}) \cdot (T_{ant} + 2 \cdot t_{iz})}{144} = 3$ sf

Total Antenna Wind Force w/ Ice Side = $F_{ant} := qZ_{ice.Sprint} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{ICEantS} = 22$ lbs

Gravity Load (without ice)

Weight of All Antennas = $WT_{ant} \cdot N_{ant} = 104$ lbs

Gravity Loads (ice only)

Volume of Each Antenna = $V_{ant} := L_{ant} \cdot W_{ant} \cdot T_{ant} = 4841$ cu in

Volume of Ice on Each Antenna = $V_{ice} := (L_{ant} + 2 \cdot t_{iz}) \cdot (W_{ant} + 2 \cdot t_{iz}) \cdot (T_{ant} + 2 \cdot t_{iz}) - V_{ant} = 5587$

Weight of Ice on Each Antenna = $W_{ICEant} := \frac{V_{ice}}{1728} \cdot 1d = 181$ lbs

Weight of Ice on All Antennas = $W_{ICEant} \cdot N_{ant} = 181$ lbs

Development of Wind & Ice Load on RRUS's

RRUS Data:

RRUS Model =	RRUS-2x50-800	
RRUS Shape =	Flat	(User Input)
RRUS Height =	$L_{RRUS} := 16$	in (User Input)
RRUS Width =	$W_{RRUS} := 13$	in (User Input)
RRUS Thickness =	$T_{RRUS} := 10$	in (User Input)
RRUS Weight =	$WT_{RRUS} := 69.1$	lbs (User Input)
Number of RRUS's =	$N_{RRUS} := 1$	
RRUS Aspect Ratio =	$A_{RRUS} := \frac{L_{RRUS}}{W_{RRUS}} = 1.2$	
RRUS Force Coefficient =	$Ca_{RRUS} = 1.2$	

Wind Load (without ice)

Surface Area for One RRUS = $SA_{RRUSF} := \frac{L_{RRUS} \cdot W_{RRUS}}{144} = 1.4$ sf

Total RRUS Wind Force = $F_{RRUS} := q_{z_{Sprint}} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{RRUSF} = 41$ lbs

Surface Area for One RRUS = $SA_{RRUSU} := \frac{L_{RRUS} \cdot T_{RRUS}}{144} = 1.1$ sf

Total RRUS Wind Force = $F_{RRUS} := q_{z_{Sprint}} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{RRUSU} = 31$ lbs

Wind Load (with ice)

Surface Area for One RRUS w/ Ice = $SA_{ICERRUSF} := \frac{(L_{RRUS} + 2 \cdot t_{iz}) \cdot (W_{RRUS} + 2 \cdot t_{iz})}{144} = 2.5$ sf

Total RRUS Wind Force w/ Ice = $F_{IRRUS} := q_{z_{ice.Sprint}} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{ICERRUSF} = 19$ lbs

Surface Area for One RRUS w/ Ice = $SA_{ICERRUSU} := \frac{(L_{RRUS} + 2 \cdot t_{iz}) \cdot (T_{RRUS} + 2 \cdot t_{iz})}{144} = 2.1$ sf

Total RRUS Wind Force w/ Ice = $F_{IRRUS} := q_{z_{ice.Sprint}} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{ICERRUSU} = 16$ lbs

Gravity Load (without ice)

Weight of All RRUSs = $WT_{RRUS} \cdot N_{RRUS} = 69$ lbs

Gravity Loads (ice only)

Volume of Each RRUS = $V_{RRUS} := L_{RRUS} \cdot W_{RRUS} \cdot T_{RRUS} = 2080$ cu in

Volume of Ice on Each RRUS = $V_{ice} := (L_{RRUS} + 2 \cdot t_{iz}) \cdot (W_{RRUS} + 2 \cdot t_{iz}) \cdot (T_{RRUS} + 2 \cdot t_{iz}) - V_{RRUS} = 3218$ cu in

Weight of Ice on Each RRUS = $W_{ICERRUS} := \frac{V_{ice}}{1728} \cdot \rho_d = 104$ lbs

Weight of Ice on All RRUSs = $W_{ICERRUS} \cdot N_{RRUS} = 104$ lbs

Development of Wind & Ice Load on RRUS's

RRUS Data:

RRUS Model =	RRUS-4X45-1900	
RRUS Shape =	Flat	(User Input)
RRUS Height =	$L_{RRUS} := 25$	in (User Input)
RRUS Width =	$W_{RRUS} := 12$	in (User Input)
RRUS Thickness =	$T_{RRUS} := 12$	in (User Input)
RRUS Weight =	$WT_{RRUS} := 69.5$	lbs (User Input)
Number of RRUS's =	$N_{RRUS} := 1$	
RRUS Aspect Ratio =	$A_{RRUS} := \frac{L_{RRUS}}{W_{RRUS}} = 2.1$	
RRUS Force Coefficient =	$Ca_{RRUS} = 1.2$	

Wind Load (without ice)

Surface Area for One RRUS = $SA_{RRUSF} := \frac{L_{RRUS} \cdot W_{RRUS}}{144} = 2.1$ sf

Total RRUS Wind Force = $F_{RRUS} := q_{Z_{Sprint}} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{RRUSF} = 59$ lbs

Surface Area for One RRUS = $SA_{RRUS} := \frac{L_{RRUS} \cdot T_{RRUS}}{144} = 2.1$ sf

Total RRUS Wind Force = $F_{RRUS} := q_{Z_{Sprint}} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{RRUS} = 59$ lbs

Wind Load (with ice)

Surface Area for One RRUS w/ Ice = $SA_{ICERRUSF} := \frac{(L_{RRUS} + 2 \cdot t_{iz}) \cdot (W_{RRUS} + 2 \cdot t_{iz})}{144} = 3.4$ sf

Total RRUS Wind Force w/ Ice = $F_{IRRUS} := q_{Z_{Ice.Sprint}} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{ICERRUSF} = 26$ lbs

Surface Area for One RRUS w/ Ice = $SA_{ICERRUS} := \frac{(L_{RRUS} + 2 \cdot t_{iz}) \cdot (T_{RRUS} + 2 \cdot t_{iz})}{144} = 3.4$ sf

Total RRUS Wind Force w/ Ice = $F_{IRRUS} := q_{Z_{Ice.Sprint}} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{ICERRUS} = 26$ lbs

Gravity Load (without ice)

Weight of All RRUSs = $WT_{RRUS} \cdot N_{RRUS} = 70$ lbs

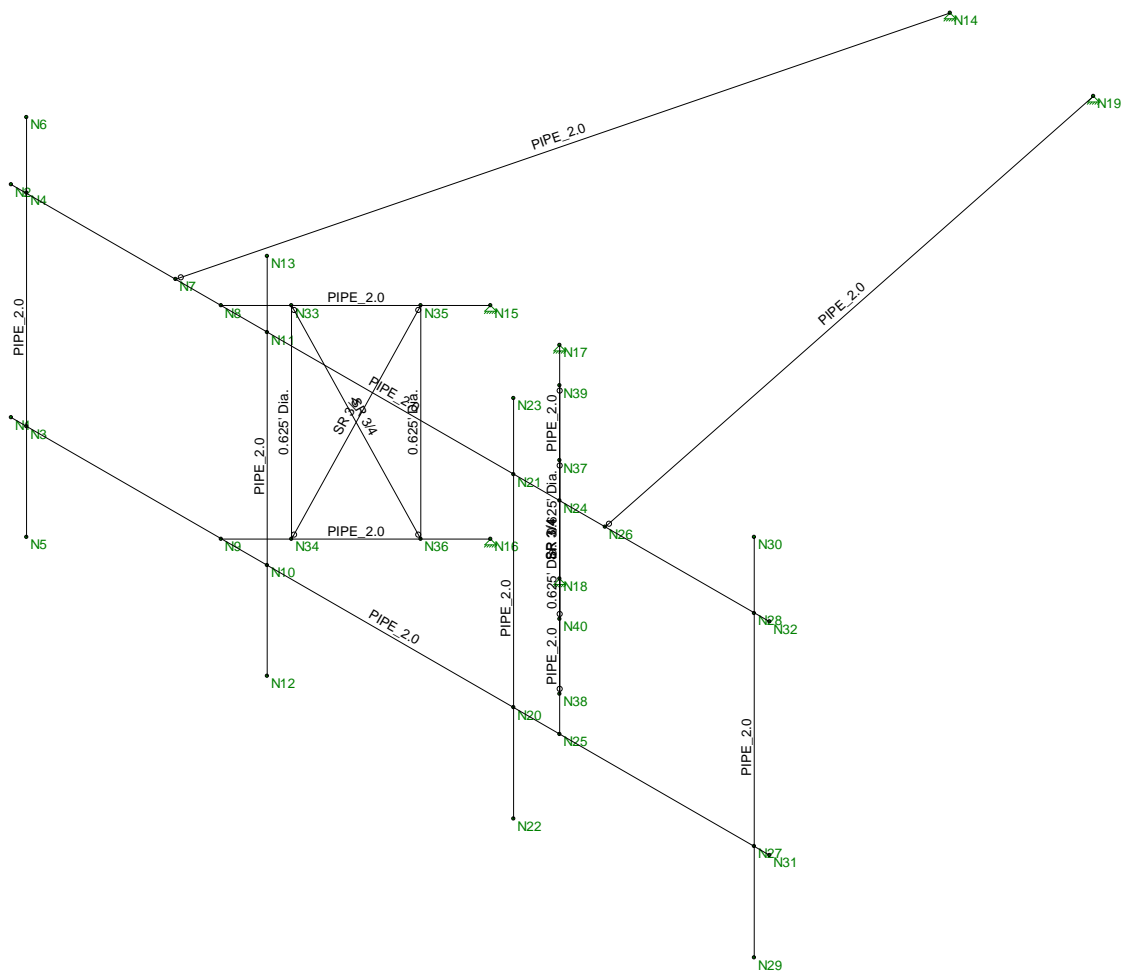
Gravity Loads (ice only)

Volume of Each RRUS = $V_{RRUS} := L_{RRUS} \cdot W_{RRUS} \cdot T_{RRUS} = 3600$ cu in

Volume of Ice on Each RRUS = $V_{Ice} := (L_{RRUS} + 2 \cdot t_{iz}) \cdot (W_{RRUS} + 2 \cdot t_{iz}) \cdot (T_{RRUS} + 2 \cdot t_{iz}) - V_{RRUS} = 4563$ cu in

Weight of Ice on Each RRUS = $W_{ICERRUS} := \frac{V_{Ice}}{1728} \cdot \rho_d = 148$ lbs

$W_{ICERRUS} \cdot N_{RRUS} = 148$



Envelope Only Solution

Centek
FJP
18116.00

CT03XC067 - Mount
Member Framing

SK - 1
Oct 29, 2019 at 10:22 AM
Antenna Mount.r3d

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GD	ɒGD	FĚĚ Ę Ī H	HĚHHHH	ĚĚĚ	€
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HH	ɒHH	Ī Ě Ī Ī Ī Ī	HĚHHHH	ĚĚĪ Ī Ī Ī F	€
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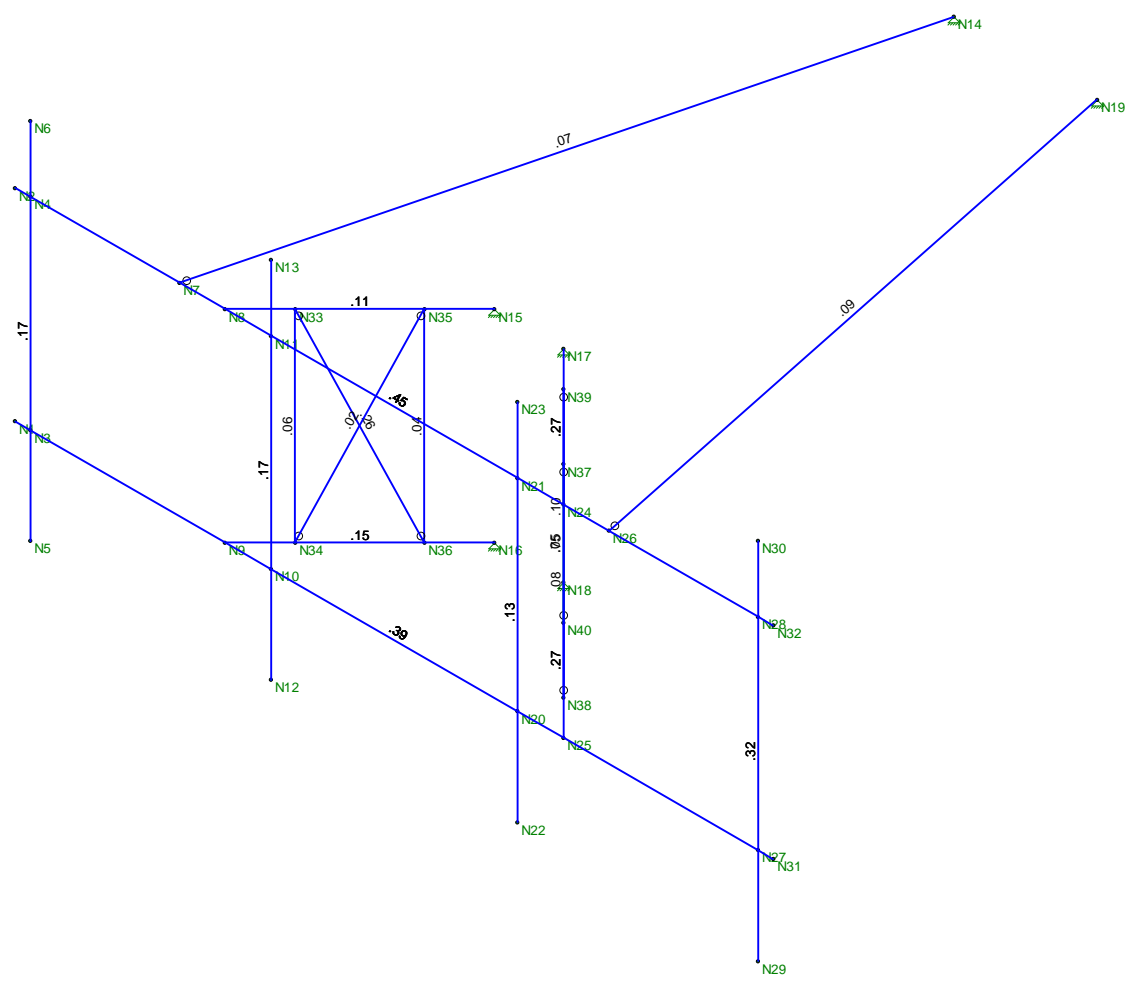
R ā c Šsaa^]	Y'Åcá	Y'Åcá	Z'Åcá	Y'ÅJ[cĀ Ě Ğ cāā	Y'ÅJ[cĀ Ě Ğ cāā	Z'ÅJ[cĀ Ě Ğ cāā
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Member Code Checks Displayed (Enveloped)
Envelope Only Solution

Centek	CT03XC067 - Mount Member Unity Check	SK - 2
FJP		Oct 29, 2019 at 10:22 AM
18116.00		Antenna Mount.r3d

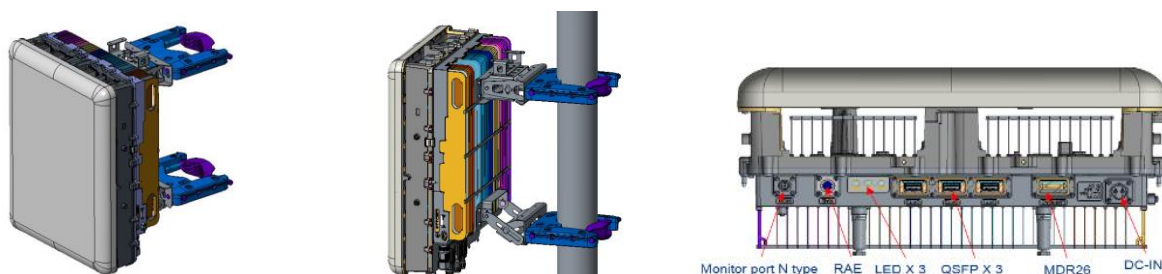
Site Data	Region: Northeast	Market:	Northern CT	Revision 2.7	Rev Date: 23-July-2018
	Cascade ID		CT03XC067	BTS OEM: ALU	RFDS Type: Preliminary
	Augment Import Code:	Augment: Relocation		Structure Type:	Tower
	Address: 250 South Olcott Street, Manchester CT 06040 Latitude: 41.77000352 Longitude: -72.55834028	Sprint Eng. Name: Bill Hastings Manager Name: Jonathan Hull		Bill.M.Hastings@sprint.com Jonathan.B.Hull@sprint.com	Eng. Phone: 978-590-9700 Manager Phone: 617-233-2920
	Detailed RFDS Description:	RFE:		RFE Phone:	
	Tower Relocation	Filter Analysis Complete:	Border Analysis Complete:	Channel Plan Complete:	
		Alpha	Beta	Gamma	
1900	1900MHz_Azimuth	0	120	240	
	1900MHz_No_of_Antennas	1	1	1	
	1900MHz_RADCenter(ft)	135	135	135	
	1900MHz_Antenna Make	CommScope	CommScope	CommScope	
	1900MHz_Antenna Model	NNVV-65B-R4	NNVV-65B-R4	NNVV-65B-R4	
	1900MHz_Horizontal_Beamwidth	68	68	68	
	1900MHz_Vertical_Beamwidth	5.1	5.1	5.1	
	1900MHz_Antenna Dimensions (ft) & Weight (lbs)	72 x 19.6 x 7.8 77.4 (lbs)	72 x 19.6 x 7.8 77.4 (lbs)	72 x 19.6 x 7.8 77.4 (lbs)	
	1900MHz_AntennaGain(dBi)	18.8	18.8	18.8	
	1900MHz_E_Tilt	0	0		
	1900MHz_M_Tilt	0	0		
	1900_Effective_Tilt	0	0		
	1900MHz_Carrier_Forecast_Year_2017				
	1900MHz_RRH Manufacturer	ALU	ALU		
	1900MHz_RRH Model	RRH 1900 4X45 65MHz	RRH 1900 4X45 65MHz	RRH 1900 4X45 65MHz	
	1900MHz_RRH Count	1	1	1	
	1900MHz_RRH Specs	25 x 11.1 x 11.4 (60 lbs)	25 x 11.1 x 11.4 (60 lbs)	25 x 11.1 x 11.4 (60 lbs)	
	1900MHz_RRH Location	Top of the Pole/Tower	Top of the Pole/Tower	Top of the Pole/Tower	
	1900MHz Combiner Model	No Combiner Required	No Combiner Required	No Combiner Required	
	1900MHz Power Split Ratio (Main/Split)				
	1900MHz Splitter Manufacturer				
	1900MHz Splitter Model	No Splitter Required	No Splitter Required	No Splitter Required	
1900MHz Number of Splitters	0	0	0		
1900MHz_Top_Jumper #1_Length (RRH or Combiner-to-Antenna for TT or Main Coax to Antenna for Ground Mount, ft)	8	8	8		
1900MHz_Top_Jumper #1_Cable_Model (RRH or Combiner-to-Antenna for TT or Main Coax to Antenna for Ground Mount)	LCF12-50J	LCF12-50J	LCF12-50J		

	1900MHz_Top_Jumper #2_Length (RRH to Combiner for TT if applicable, ft)			
	1900MHz_Top_Jumper #2_Cable_Model (RRH to Combiner for TT if applicable)			
	1900MHz_Main_Cable_Length (ft)	135	135	135
	1900MHz_Main_Cable_Model	HB114-1-08U4-M5F	HB114-1-08U4-M5F	HB114-1-08U4-M5F
	1900MHz_Bottom_Jumper #1_Length (Ground based RRH to Combiner OR-Main Coax, ft)			
	1900MHz_Bottom_Jumper #1_Cable_Model (Ground based RRH to Combiner-OR-Main Coax)			
	1900MHz_Bottom_Jumper #2_Length (Ground based-Combiner to Main Coax, ft)			
	1900MHz_Bottom_Jumper #2_Cable_Model (Ground based-Combiner to Main Coax)			
800	800MHz_Azimuth	0	120	240
	800MHz_No_of_Antennas	1	1	1
	800MHz_RADCenter(ft)	135	135	135
	800MHz_AntennaMake	NA	NA	NA
	800MHz_AntennaModel	Antenna assigned on a different band	Antenna assigned on a different band	Antenna assigned on a different band
	800MHz_Horizontal_Beamwidth	NA	NA	NA
	800MHz_Vertical_Beamwidth	NA	NA	NA
	800MHz_Antenna Dimensions (ft) & Weight (lbs)	NA NA	NA NA	NA NA
	800MHz_AntennaGain (dBi)	NA	NA	NA
	800MHz_E_Tilt	0	0	0
	800MHz_M_Tilt	0	0	0
	800 MHz_Effective Tilt (degrees)	0	0	0
	800MHz_RRH Manufacturer	ALU	ALU	ALU
	800_Combiner_Model	No Combiner Required	No Combiner Required	No Combiner Required
	800MHz_RRH Model	RRH 800 MHz 2x50W	RRH 800 MHz 2x50W	RRH 800 MHz 2x50W
	800MHz_RRH Specs	15.8 x 13.0 x 14.0 (64 lbs)	15.8 x 13.0 x 14.0 (64 lbs)	15.8 x 13.0 x 14.0 (64 lbs)
	800MHz_RRH Count	2	2	2
	800MHz_RRH Location	Top of the Pole/Tower	Top of the Pole/Tower	Top of the Pole/Tower
	800MHz BILT Border Filter	na	na	na
	800MHz Splitter Manufacturer			
	800MHz Splitter Model			
	800MHz Number of Splitters	0	0	0
	800_Top_Jumper #1_Length (RRH to Antenna for TT or Main Coax to Antenna for GM)	8	8	8
800_Top_Jumper_Cable_Model (RRH to Antenna for TT or Main Coax to Antenna for GM)	LCF12-50J	LCF12-50J	LCF12-50J	

	800MHz_Main_Coax_Cable_Length (ft)	NA	NA	NA
	800MHz_Main_Coax_Cable_Model	NA	NA	NA
	800_Bottom_Jumper #1_Length (Ground based RRH to Main Coax)			
	800_Bottom_Jumper #1_Cable_Model (Ground based RRH to Main Coax)			
2500	2500MHz_Azimuth	0	120	240
	2500MHz_No_of_Antennas	1	1	1
	2500MHz_RADCenter(ft)	135	135	135
	2500MHz_AntennaMake	Nokia	Nokia	Nokia
	2500MHz_AntennaModel	AAHC (Nokia Massive MIMO RRU/Antenna Standard)	AAHC (Nokia Massive MIMO RRU/Antenna Standard)	AAHC (Nokia Massive MIMO RRU/Antenna Standard)
	2500MHz_Horizontal_Beamwidth	65	65	65
	2500MHz_Vertical_Beamwidth			
	2500MHz_AntennaHeight (ft)	25.6 x 19.7 x 9.64 103.7 (lbs)	25.6 x 19.7 x 9.64 103.7 (lbs)	25.6 x 19.7 x 9.64 103.7 (lbs)
	2500MHz_AntennaGain (dBi)			
	2500MHz_E_Tilt	0	0	0
	2500MHz_M_Tilt	0	0	0
	2500 MHz_Effective Tilt (degrees)	0	0	0
	2500MHz_RRH Manufacturer			
	2500_Combiner_Model	No Combiner Required	No Combiner Required	No Combiner Required
	2500MHz_RRH Model			
	2500MHz_RRH Count			
	2500MHz_RRH Location			
	2500MHz Power Split Ratio (Main/Split)			
	2500MHz Splitter Manufacturer			
	2500MHz Splitter Model			
	2500MHz Number of Splitters	0	0	0
	2500_Top_Jumper #1_Length (RRH to Antenna for TT or Main Coax to Antenna for GM)	8	8	8
	2500_Top_Jumper_Cable_Model (RRH to Antenna for TT or Main Coax to Antenna for GM)	LCF12-50J	LCF12-50J	LCF12-50J
	2500MHz_Main_Cable_Length (ft)	135		
	2500MHz_Main_Cable_Model	HB114-08U3M12-xxxF		
	2500_Bottom_Jumper #1_Length (Ground based RRH to Main Coax)			
	2500_Bottom_Jumper #1_Cable_Model (Ground based RRH to Main Coax)			
	Has_Split			
	Plumbing Scenario			

Comments	Date Updated			
	Update Description			
	Site Type			
	Comments			
	This RFDS is Deployment View			

TD LTE 2.5G Massive MIMO Adaptive Antenna (MAA) – AAHC



Category	Description	Unit	AAHC
Spectrum	3GPP Band		B41
	Operating frequency	MHz	2496-2690
RF characteristic	Number of TX/RX paths	#	64T64R
	Instantaneous Bandwidth IBW	MHz	194
	Occupied Bandwidth OBW	MHz	60
	Total Output power	W	120
	EIRP	dBm	74.8
	TX OBUE in B41 for sum of all 64 pipes at 1MHz offset	dBm/MHz	-13 sum of all ports
Power	Emission at IPWireless 2558-2568MHz	dBm/MHz	-57 sum of all ports
	Emission at NEXTRADAR at 2704-3000MHz	dBm/MHz	-27 sum of all ports
	Power inputs		2 pin, and with APPB/APPC
Interface	Supply Voltage / Voltage Range	V	-48V DC voltage (-40.5V~ -57V)
	Typical Power Consumption	W	75% duty cycle, 1400W for LTE
	Optical Interface		3x QSFP (4 x 9.8G CPRI each)
	RAE Interface		Circle connector, AISG-ES-RAE v2.1.0
Antenna Specifications	LMI interface		MDR26
	Monitor interface		N_Female
	Antenna array		8x8x2
	Element Polarization	H/V or ± 45	± 45
	Gain [Broadcast 65 HBW]	dBi	15.2
	Horizontal BW [Broadcast] (@ -3dB)	Degrees	65
	Vertical BW [Broadcast] (@ -3dB)	Degrees	9
	Mechanical Downtilt Range	Degrees	± 5
	Electrical Downtilt Range	Degrees	± 10
	Cross Polar Isolation [Element]	dB	19
	Front-to-Back Ratio [Broadcast] (@ 180° ±15° cone)	dB	25
	Element Spacing	λ (mm)	horizontal 57.5, Vertical 80
	Upper Side Lobe Suppression (1st USLS) [Broadcast]	dB	16
	Cross Polar Discrimination [Broadcast] (@ -3dB)	dB	10
	Traffic (Service) Beam Azimuthal Pan	Degrees	± 55
	Traffic (Service) Beam Elevational Tilt	Degrees	± 10
	Azimuth Beamwidth Squint (@ Boresight)	Degrees	configurable
Broadcast Tracking @ ±60°	dB	2	
Mechanical Specifications	Dimensions (LxWxD)	mm (in)	651x501x245 mm (25.6x19.7x9.6 in)
	Weight	kg (lb)	47Kg (103.6lb)
	Max Wind Speed	kmh/mph	200kmh (125 mph)
	Wind Load Front/Side/Rear @ 150kmh	N(lbF)	349 /168/130 N (78.5 / 37.8 /29.2 lbF)
	Radom Material		PC
	Radom Color		Cold Gray
	Mounting Kit	mm (in)	FPKA/FPKB/FPKC
	Operational Temperature Range	C(F)	-40 ~ 55@ -40 ~ 131(F)
	Ingress protection class		IP65
	Installation options		Pole, Wall
Surge protection	kA	20	

NNW-65B-R4

8-port sector antenna, 4x 698–896 and 4x 1695–2690 MHz, 65° HPBW, 4x RET



- Uses the 4.3-10 connector which is 40 percent smaller than the 7-16 DIN connector
- Supports re-configurable antenna sharing capability enabling control of the internal RET system using up to two separate RET compatible OEM radios
- All internal RET actuators are connected in “Cascaded MRET” configuration

Electrical Specifications

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2180	2300–2500	2500–2690
Gain, dBi	14.5	14.9	16.8	17.2	17.5	18.1	17.8
Beamwidth, Horizontal, degrees	66	64	60	60	62	59	64
Beamwidth, Vertical, degrees	11.7	10.4	7.3	6.8	6.4	5.4	5.1
Beam Tilt, degrees	2–14	2–14	2–12	2–12	2–12	2–12	2–12
USLS (First Lobe), dB	16	18	14	16	15	16	18
Front-to-Back Ratio at 180°, dB	31	34	38	38	37	33	30
Isolation, dB	25	25	25	25	25	25	25
Isolation, Intersystem, dB	25	25	25	25	25	25	25
VSWR Return Loss, dB	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0
PIM, 3rd Order, 2 x 20 W, dBc	-150	-150	-150	-150	-150	-150	-150
Input Power per Port at 50°C, maximum, watts	300	300	250	250	250	200	200
Polarization	±45°	±45°	±45°	±45°	±45°	±45°	±45°
Impedance	50 ohm	50 ohm	50 ohm	50 ohm	50 ohm	50 ohm	50 ohm

Electrical Specifications, BASTA*

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2180	2300–2500	2500–2690
Gain by all Beam Tilts, average, dBi	14.1	14.6	16.5	16.9	17.0	17.6	17.3
Gain by all Beam Tilts Tolerance, dB	±0.5	±0.5	±0.7	±0.4	±0.5	±0.6	±0.7
	2 ° 14.2	2 ° 14.7	2 ° 16.6	2 ° 16.8	2 ° 16.9	2 ° 17.5	2 ° 16.9
Gain by Beam Tilt, average, dBi	8 ° 14.2	8 ° 14.7	7 ° 16.7	7 ° 17.1	7 ° 17.2	7 ° 17.9	7 ° 17.5
	14 ° 13.9	14 ° 14.2	12 ° 16.2	12 ° 16.7	12 ° 16.7	12 ° 17.3	12 ° 17.0
Beamwidth, Horizontal Tolerance, degrees	±3.9	±3.9	±5.7	±2.7	±3.1	±7.9	±8
Beamwidth, Vertical Tolerance, degrees	±0.9	±0.8	±0.7	±0.5	±0.6	±0.4	±0.2
USLS, beampeak to 20° above beampeak, dB	16	18	14	15	14	14	14
Front-to-Back Total Power at 180° ± 30°, dB	20	20	31	31	28	28	26
CPR at Boresight, dB	21	20	18	18	19	19	20
CPR at Sector, dB	8	6	8	8	7	8	5

* CommScope® supports NGMN recommendations on Base Station Antenna Standards (BASTA). To learn more about the benefits of BASTA, [download the whitepaper Time to Raise the Bar on BSAs.](#)

Array Layout

NNV-65BR4

RF Connector Quantity, high band	4
RF Connector Interface	4.3-10 Female
Grounding Type	RF connector inner conductor and body grounded to reflector and mounting bracket
Radiator Material	Low loss circuit board
Radome Material	Fiberglass, UV resistant
Reflector Material	Aluminum
RF Connector Location	Bottom
Wind Loading, frontal	685.0 N @ 150 km/h 154.0 lbf @ 150 km/h
Wind Loading, lateral	232.0 N @ 150 km/h 52.2 lbf @ 150 km/h
Wind Loading, maximum	889.0 N @ 150 km/h 199.9 lbf @ 150 km/h
Wind Speed, maximum	241 km/h 150 mph

Dimensions

Length	1828.0 mm 72.0 in
Width	498.0 mm 19.6 in
Depth	197.0 mm 7.8 in
Net Weight, without mounting kit	35.1 kg 77.4 lb

Remote Electrical Tilt (RET) Information

Input Voltage	10–30 Vdc
Internal RET	High band (2) Low band (2)
Power Consumption, idle state, maximum	1 W
Power Consumption, normal conditions, maximum	8 W
Protocol	3GPP/AISG 2.0 (Multi-RET)
RET Hardware	CommRET v2
RET Interface	8-pin DIN Female 8-pin DIN Male
RET Interface, quantity	1 female 1 male

Packed Dimensions

Length	2010.0 mm 79.1 in
Width	608.0 mm 23.9 in
Depth	352.0 mm 13.9 in
Shipping Weight	49.0 kg 108.0 lb

Regulatory Compliance/Certifications

Agency	Classification
RoHS 2011/65/EU	Compliant by Exemption
China RoHS SJ/T 11364-2006	Above Maximum Concentration Value (MCV)
ISO 9001:2008	Designed, manufactured and/or distributed under this quality management system



Structural Analysis Report

180-ft Self-Supporting Lattice Tower

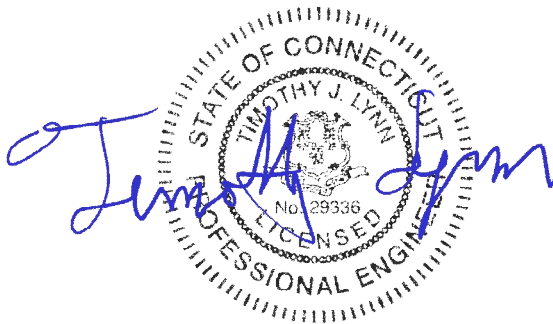
Proposed Sprint Antenna Installation

Sprint Site Ref: CT03XC067

*250 Olcott Street
Manchester, CT*

CEN TEK Project No. 18116.00

~~*Date: August 13, 2018*~~
Rev 2: October 11, 2019



Prepared for:
*Transcend Wireless
10 Industrial Ave, Suite 3
Mahwah, NJ 07430*

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Introduction

The purpose of this report is to summarize the results of the non-linear, P- Δ structural analysis of the antenna installation proposed by Sprint on the self-supporting lattice tower located in Manchester, Connecticut.

The host tower is a 180-ft, nine-section, three legged, self-supporting tapered lattice tower originally designed and manufactured by Sabre Industries report no. 408277, dated May 9, 2018. The tower geometry, structure member sizes and the foundation system information were obtained from the aforementioned design documents.

Antenna and appurtenance information were obtained from the tower design documents and a Sprint RF sheet.

The existing tower consists of nine (9) tapered steel pipe leg sections conforming to ASTM A500-50. Diagonal lateral support bracing consists of steel angle sections conforming to ASTM A572-50. The vertical tower sections are connected by bolted flange plates while the pipe legs and bracing are connected by bolted and welded gusset connections. The width of the tower face is 7-ft at the top and 23-ft at the base.

Antenna and Appurtenance Summary

- Eversource:
Appurtenance: One (1) dB Spectra DS9A09F36D-N antenna, one (1) 24' x 6" Omni antenna, one (1) Kreco CO-41A antenna and one (1) TTA leg mounted to the top of the tower.
Conduit: Four (4) 1-5/8" \varnothing , one (1) 1/2" \varnothing and one (1) 7/8" \varnothing coax cable.
- Eversource :
Appurtenance: Three (3) 8-ft \varnothing microwave dishes pipe mounted with a RAD center elevation of 175-ft above existing grade.
Conduit: Six (6) E65 cables.
- Eversource :
Appurtenance: One (1) 8-ft \varnothing microwave dish pipe mounted with a RAD center elevation of 164-ft above existing grade.
Conduit: Two (2) E65 cables.
- Eversource:
Appurtenance: One (1) Comprod 531-70HD antenna and one (1) Sinclair SD212 antenna mounted one a 6-ft sidearm with an elevation of 158-ft above existing grade.
Conduit: Two (2) 7/8" \varnothing coax cables.
- Eversource:
Appurtenance: One (1) 24' x 6" Omni antenna mounted one a 6-ft sidearm with an elevation of 156-ft above existing grade.
Conduit: Two (2) 7/8" \varnothing coax cables

- **FUTURE CARRIER (Reserved):**
Antennas: Twelve (12) 8' panel antennas, twelve (12) RRHs and three (3) distribution boxes mounted on three (3) 14-ft V-Frames with a RAD center elevation of 125-ft above existing grade.
Coax Cables: Twenty-One (21) 1-5/8"Ø cables running on a face of the existing tower as specified in Section 3 of this report.
- **FUTURE CARRIER (Reserved):**
Antennas: Twelve (12) 8' panel antennas, twelve (12) RRHs and three (3) distribution boxes mounted on three (3) 14-ft V-Frames with a RAD center elevation of 115-ft above existing grade.
Coax Cables: Twenty-One (21) 1-5/8"Ø cables running on a face of the existing tower as specified in Section 3 of this report.
- **FUTURE CARRIER (Reserved):**
Antennas: Twelve (12) 8' panel antennas, twelve (12) RRHs and three (3) distribution boxes mounted on three (3) 14-ft V-Frames with a RAD center elevation of 105-ft above existing grade.
Coax Cables: Twenty-One (21) 1-5/8"Ø cables running on a face of the existing tower as specified in Section 3 of this report.
- **SPRINT (Proposed):**
Antennas: **Three (3) Commscope NNVV-65B-R4 panel antennas, three (3) Nokia AAHC panel antennas, three (3) 1900MHz 4X45W RRHs and six (6) 800MHz 2X50W RRHs mounted on three (3) 14-ft V-Frames with a RAD center elevation of 135-ft above existing grade.**
Coax Cables: **Four (4) 1-1/4"Ø Hybriflex cable running on a face of the existing tower as specified in Section 3 of this report.**

Primary Assumptions Used in the Analysis

- The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- The tower carries the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- Tower is properly installed and maintained.
- Tower is in plumb condition.
- Tower loading for antennas and mounts as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original tower design documents.
- All members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.
- All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.

Analysis

The existing tower was analyzed using a comprehensive computer program entitled tnxTower. The program analyzes the tower, considering the worst case loading condition. The tower is considered as loaded by concentric forces along the tower, and the model assumes that the tower members are subjected to bending, axial, and shear forces.

The existing tower was analyzed for the controlling basic wind speed (3-second gust) with no ice and the applicable wind and ice combination to determine stresses in members as per guidelines of TIA-222-G-2005 entitled “Structural Standard for Antenna Support Structures and Antennas”, the American Institute of Steel Construction (AISC) and the Manual of Steel Construction; Load and Resistance Factor Design (LRFD).

The controlling wind speed is determined by evaluating the local available wind speed data as provided in Appendix N of the CSBC¹ and the wind speed data available in the TIA-222-G-2005 Standard.

Tower Loading

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA-222-G-2005, gravity loads of the tower structure and its components, and the application of 1.00” radial ice on the tower structure and its components.

Basic Wind Speed:	Hartford County; $v = 90-105$ mph (3-second gust) [Annex B of TIA-222-G-2005]
	Manchester; $v = 105$ mph (Nominal – Structure Class III) [Appendix N of the 2018 CT Building Code]
Load Cases:	<u>Load Case 1</u> ; 105 mph wind speed w/ no ice plus gravity load – used in calculation of tower stresses and rotation. [Appendix N of the 2018 CT Building Code]
	<u>Load Case 2</u> ; 50 mph wind speed w/ 1.00” radial ice plus gravity load – used in calculation of tower stresses. [Annex B of TIA-222-G-2005]
	<u>Load Case 3</u> ; 105 mph wind speed used in calculation of tower deflection.

¹ The 2015 International Building Code as amended by the 2018 Connecticut State Building Code (CSBC).

Tower Capacity

- Calculated stresses were found to be within allowable limits. This tower was found to be at **99.8%** of its total capacity.

Tower Section	Elevation	Stress Ratio (percentage of capacity)	Result
Leg (T8)	20'-0"-40'-0"	81.6%	PASS
Diagonal (9)	0'-0"-20'-0"	99.8%	PASS

- The tower combined deflection is **0.4408 degrees**.

Deflection Criteria	Proposed (degrees)
Sway (Tilt)	0.4303
Twist	0.0957
Combined	0.4408

| *Note 1: Tower deflection calculated utilizing the service wind load combination and max wind speed.*

Foundation and Anchors

The existing foundation consists of three (3) 4'-0" diameter x 4'-9" long piers on one (1) 34'-0" square x 1'-9" thick concrete mat. The foundation properties and sub-grade conditions used in the analysis of the existing foundation were obtained from the aforementioned original design documents. Tower legs are connected to the foundation by means of (6) 1-1/2"Ø, ASTM F1554-105 anchor bolts per leg, embedded into the concrete foundation structure.

- The tower base maximum corner reactions developed from the governing Load Case 2 were used in the verification of the foundation and its anchors:

Vector	Proposed Reactions
Compression	491 kips
Uplift	443 kips
Shear	59 kips
Total Shear	99 kips
Overturning Moment	9429 kip-ft

- The foundation was found to be within allowable limits.

Foundation	Design Limit	TIA-222-G Section 9.4 FS ⁽¹⁾	Proposed Loading (FS) ⁽¹⁾	Result
Reinf. Conc. Pad and Piers	Uplift	1.0	1.44	PASS

Note 1: FS denotes Factor of Safety

- The anchor bolts were found to be within allowable limits.

Tower Component	Design Limit	Stress Ratio (percentage of capacity)	Result
Anchor Bolts	Tension	57.6%	PASS

Conclusion

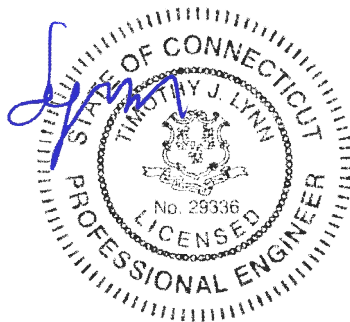
This analysis shows that the subject tower **is adequate** to support the proposed modified antenna configuration.

The analysis is based, in part, on the information provided to this office by Sprint. If the existing conditions are different than the information in this report, Centek Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:

Timothy J. Lynn, PE
 Structural Engineer



*Standard Conditions for Furnishing of
Professional Engineering Services on
Existing Structures*

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of Centek Engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to Centek Engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an uncorroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the “as new” condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. Centek Engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM

tnxTower, is an integrated structural analysis and design software package for Designed specifically for the telecommunications industry, tnxTower, formerly ERITower, automates much of the tower analysis and design required by the TIA/EIA 222 Standard.

tnxTower Features:

- tnxTower can analyze and design 3- and 4-sided guyed towers, 3- and 4-sided self-supporting towers and either round or tapered ground mounted poles with or without guys.
- The program analyzes towers using the TIA-222-G (2005) standard or any of the previous TIA/EIA standards back to RS-222 (1959). Steel design is checked using the AISC ASD 9th Edition or the AISC LRFD specifications.
- Linear and non-linear (P-delta) analyses can be used in determining displacements and forces in the structure. Wind pressures and forces are automatically calculated.
- Extensive graphics plots include material take-off, shear-moment, leg compression, displacement, twist, feed line, guy anchor and stress plots.
- tnxTower contains unique features such as True Cable behavior, hog rod take-up, foundation stiffness and much more.

DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
DS9A09F36D-N (Eversource)	189.4	AAHC (Sprint - Proposed)	135
24' x 6" Omni (Eversource)	189	(4) RRUS-11 (Future Carrier)	125
CO-41A (Eversource)	187	(4) RRUS-11 (Future Carrier)	125
Tower Top Amplifier (Eversource)	180	(3) RC2DC-3315-PF-48 (Future Carrier)	125
8' Dish (Eversource)	175	14' V-Boom (Future Carrier)	125
8' Dish (Eversource)	175	14' V-Boom (Future Carrier)	125
8' Dish (Eversource)	175	14' V-Boom (Future Carrier)	125
8' Dish (Eversource)	164	(4) 8' x1' Panel (Future Carrier)	125
531-70HD (Eversource)	158	(4) 8' x1' Panel (Future Carrier)	125
SD212 (Eversource)	158	(4) 8' x1' Panel (Future Carrier)	125
ROHN 6-ft Side Arm (Eversource)	158	(4) RRUS-11 (Future Carrier)	125
24' x 6" Omni (Eversource)	156	(4) RRUS-11 (Future Carrier)	115
ROHN 6-ft Side Arm (Eversource)	153	(4) RRUS-11 (Future Carrier)	115
ROHN 3-ft Side Arm (Eversource)	144.4	(3) RC2DC-3315-PF-48 (Future Carrier)	115
NNVV-65B-R4 (Sprint - Proposed)	135	14' V-Boom (Future Carrier)	115
AAHC (Sprint - Proposed)	135	14' V-Boom (Future Carrier)	115
FD-RRH 2x50 800 (Sprint - Proposed)	135	14' V-Boom (Future Carrier)	115
FD-RRH 2x50 800 (Sprint - Proposed)	135	(4) 8' x1' Panel (Future Carrier)	115
FD-RRH 2x50 800 (Sprint - Proposed)	135	(4) 8' x1' Panel (Future Carrier)	115
FD-RRH 4x45 1900 (Sprint - Proposed)	135	(4) 8' x1' Panel (Future Carrier)	115
FD-RRH 4x45 1900 (Sprint - Proposed)	135	(4) RRUS-11 (Future Carrier)	115
FD-RRH 4x45 1900 (Sprint - Proposed)	135	(4) RRUS-11 (Future Carrier)	105
FD-RRH 2x50 800 (Sprint - Proposed)	135	(4) RRUS-11 (Future Carrier)	105
FD-RRH 2x50 800 (Sprint - Proposed)	135	(3) RC2DC-3315-PF-48 (Future Carrier)	105
FD-RRH 2x50 800 (Sprint - Proposed)	135	14' V-Boom (Future Carrier)	105
14' V-Boom (Sprint - Proposed)	135	14' V-Boom (Future Carrier)	105
14' V-Boom (Sprint - Proposed)	135	(4) 8' x1' Panel (Future Carrier)	105
14' V-Boom (Sprint - Proposed)	135	(4) 8' x1' Panel (Future Carrier)	105
NNVV-65B-R4 (Sprint - Proposed)	135	(4) 8' x1' Panel (Future Carrier)	105
AAHC (Sprint - Proposed)	135	(4) 8' x1' Panel (Future Carrier)	105
NNVV-65B-R4 (Sprint - Proposed)	135	(4) RRUS-11 (Future Carrier)	105

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A500-50	50 ksi	62 ksi	A572-50	50 ksi	65 ksi

TOWER DESIGN NOTES

1. Tower designed for Exposure C to the TIA-222-G Standard.
2. Tower designed for a 97 mph basic wind in accordance with the TIA-222-G Standard.
3. Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 97 mph wind.
5. Tower Structure Class III.
6. Topographic Category 1 with Crest Height of 0.00 ft
7. TOWER RATING: 99.8%

ALL REACTIONS ARE FACTORED

MAX. CORNER REACTIONS AT BASE:

DOWN: 491 K
SHEAR: 59 K

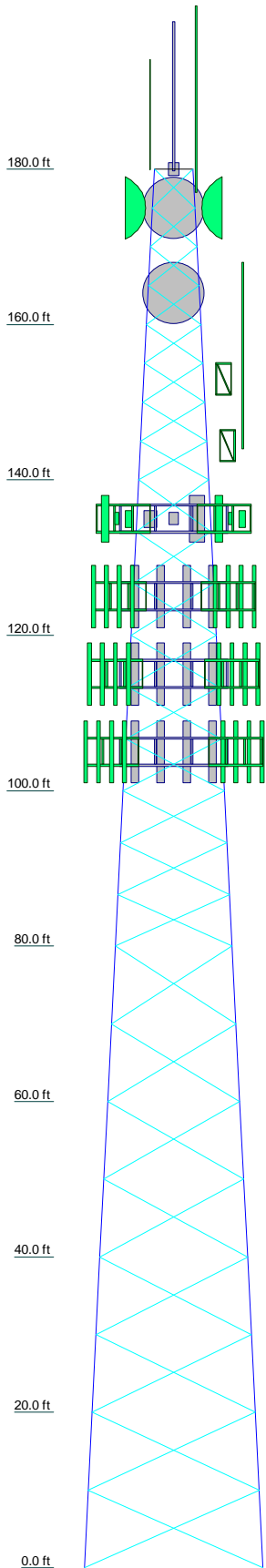
UPLIFT: -443 K
SHEAR: 55 K

AXIAL 245 K
SHEAR 26 K
MOMENT 2673 kip-ft

TORQUE 10 kip-ft
50 mph WIND - 1.0000 in ICE

AXIAL 55 K
SHEAR 99 K
MOMENT 9429 kip-ft

TORQUE 38 kip-ft
REACTIONS - 97 mph WIND

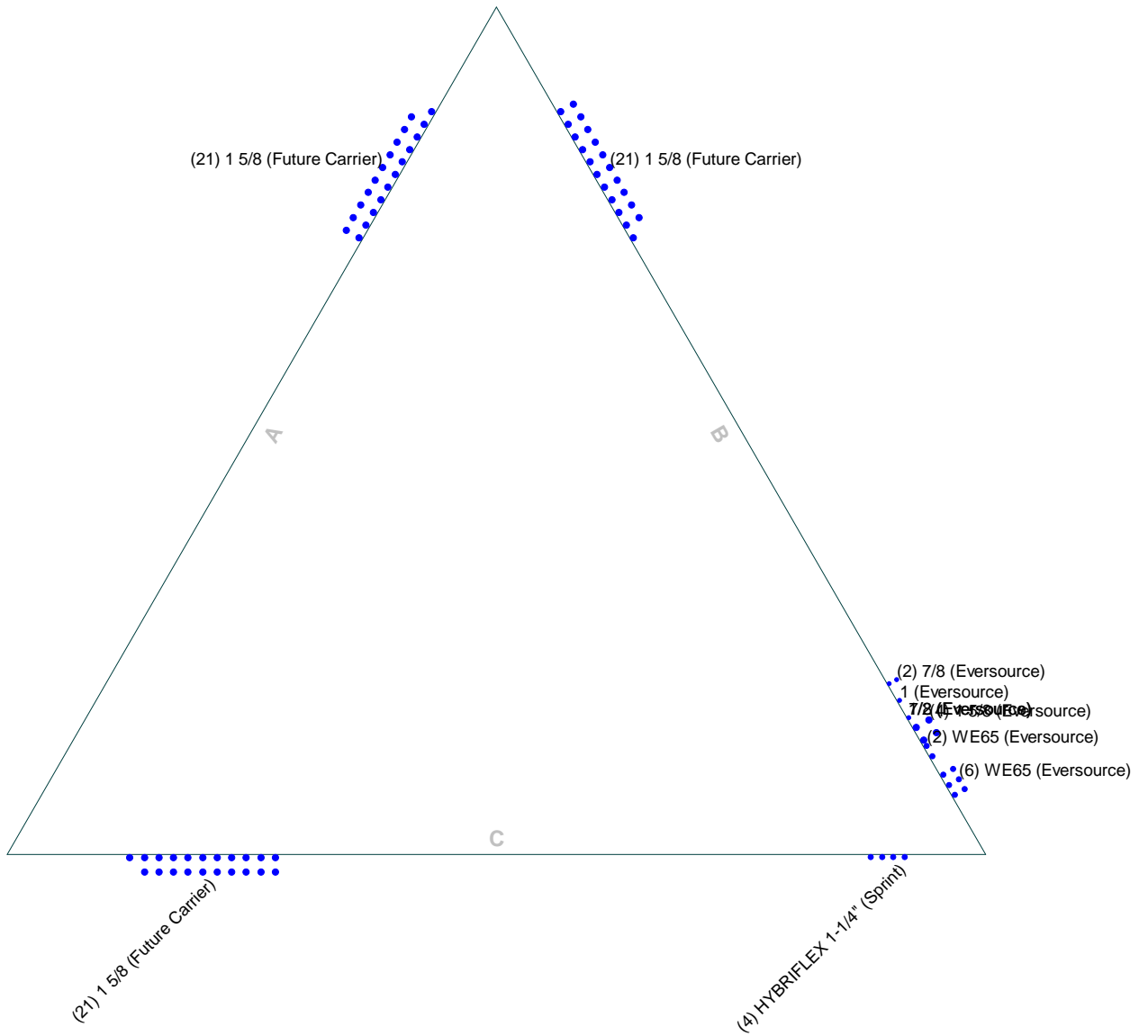


Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11	T12	T13	T14	T15	T16	T17	T18	T19	T20	T21	T22	T23	
Legs	P2.5x2.76	P3x.3		P5.0x.5	A500-50		P8x.5		P10x.5															
Leg Grade																								
Diagonals	L2x2x1/8	L2x2x3/16	L2 1/2x2 1/2x1/4		L3 1/2x3x1/4	L4x3 1/2x5/16	L4x3 1/2x3/8	L4x4x3/8	L5x5x5/16															
Diagonal Grade																								
Top Girts	L2x2x1/8																							
Face Width (ft)	5	7	9	11	13	15	17	19	21	23														
# Panels @ (ft)	8 @ 5	1.2	2.5	2.9	3.1	4.3	4.9	5.2	6.3															
Weight (K)	0.8																							

Centek Engineering Inc.			Job: 18116.00 - CT03XC067
63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587			Project: 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT
Client: Sprint	Drawn by: T.JL	App'd:	
Code: TIA-222-G	Date: 01/03/19	Scale: NTS	
Path:	Dwg No: E-1		

Feed Line Plan

— Round
 — Flat
 — App In Face
 — App Out Face

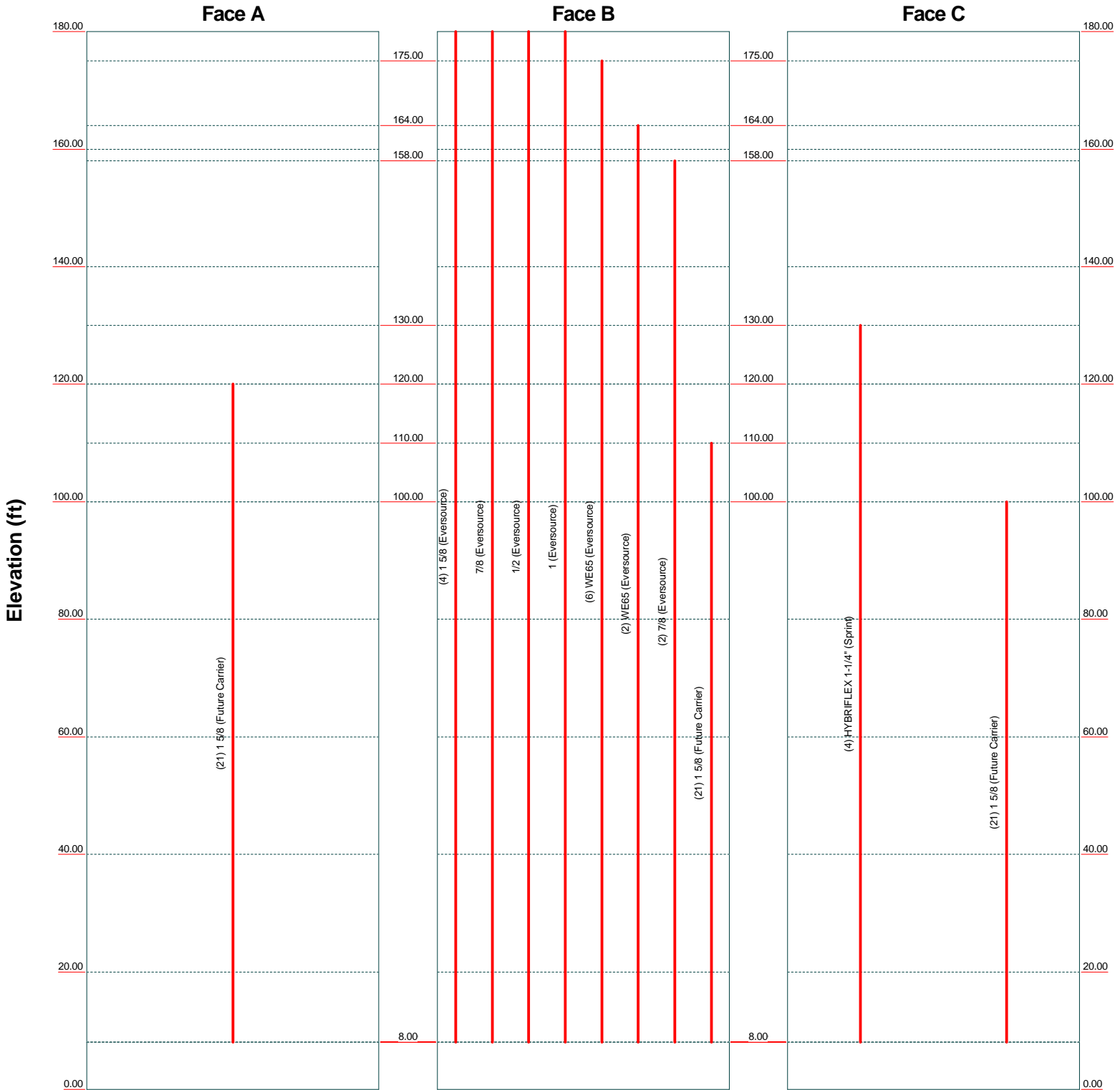


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Project: 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Client: Sprint	Drawn by: T.JL
Code: TIA-222-G	Date: 01/03/19	App'd:
Path:	Scale: NTS	Dwg No. E-7
J:\jobs\1811600\1811600_180ft Sabre Lattice Tower\Drawings\Rev 1\1811600_Self-supporting Lattice.dwg		

Feed Line Distribution Chart

0' - 180'

— Round
 — Flat
 — App In Face
 — App Out Face
 — Truss Leg



Centek Engineering Inc.		
63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587		
Job: 18116.00 - CT03XC067	Project: 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Client: Sprint
Code: TIA-222-G	Date: 01/03/19	App'd: _____
Path: <small>3:\jobs\1811600\1800_W04_Structural\Backup Documents\Rev (1)E29 Files\180 Self-supporting Lattice.cad</small>	Scale: NTS	Dwg No: E-7

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 18116.00 - CT03XC067	Page 1 of 34
	Project 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Date 13:56:50 01/03/19
	Client Sprint	Designed by TJJ

Tower Input Data

The main tower is a 3x free standing tower with an overall height of 180.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 5.00 ft at the top and 23.00 ft at the base.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Basic wind speed of 97 mph.

Structure Class III.

Exposure Category C.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 97 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

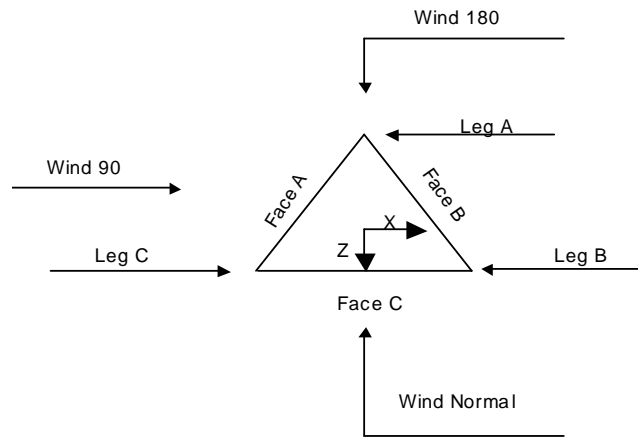
Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs	Distribute Leg Loads As Uniform	Use ASCE 10 X-Brace Ly Rules
Consider Moments - Horizontals	Assume Legs Pinned	√ Calculate Redundant Bracing Forces
Consider Moments - Diagonals	√ Assume Rigid Index Plate	Ignore Redundant Members in FEA
Use Moment Magnification	√ Use Clear Spans For Wind Area	SR Leg Bolts Resist Compression
√ Use Code Stress Ratios	√ Use Clear Spans For KL/r	√ All Leg Panels Have Same Allowable
√ Use Code Safety Factors - Guys	Retension Guys To Initial Tension	Offset Girt At Foundation
Escalate Ice	Bypass Mast Stability Checks	√ Consider Feed Line Torque
Always Use Max Kz	√ Use Azimuth Dish Coefficients	Include Angle Block Shear Check
Use Special Wind Profile	√ Project Wind Area of Appurt.	Use TIA-222-G Bracing Resist. Exemption
√ Include Bolts In Member Capacity	Autocalc Torque Arm Areas	Use TIA-222-G Tension Splice Exemption
Leg Bolts Are At Top Of Section	Add IBC .6D+W Combination	Poles
√ Secondary Horizontal Braces Leg	√ Sort Capacity Reports By Component	Include Shear-Torsion Interaction
Use Diamond Inner Bracing (4 Sided)	Triangulate Diamond Inner Bracing	Always Use Sub-Critical Flow
SR Members Have Cut Ends	Treat Feed Line Bundles As Cylinder	Use Top Mounted Sockets
SR Members Are Concentric		

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 18116.00 - CT03XC067	Page 2 of 34
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Triangular Tower

Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	<i>ft</i>			<i>ft</i>		<i>ft</i>
T1	180.00-160.00			5.00	1	20.00
T2	160.00-140.00			7.00	1	20.00
T3	140.00-120.00			9.00	1	20.00
T4	120.00-100.00			11.00	1	20.00
T5	100.00-80.00			13.00	1	20.00
T6	80.00-60.00			15.00	1	20.00
T7	60.00-40.00			17.00	1	20.00
T8	40.00-20.00			19.00	1	20.00
T9	20.00-0.00			21.00	1	20.00

Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	<i>ft</i>	<i>ft</i>				<i>in</i>	<i>in</i>
T1	180.00-160.00	5.00	X Brace	No	Yes	0.0000	0.0000
T2	160.00-140.00	5.00	X Brace	No	No	0.0000	0.0000
T3	140.00-120.00	6.67	X Brace	No	No	0.0000	0.0000
T4	120.00-100.00	6.67	X Brace	No	No	0.0000	0.0000
T5	100.00-80.00	6.67	X Brace	No	No	0.0000	0.0000
T6	80.00-60.00	10.00	X Brace	No	No	0.0000	0.0000

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	Client	Sprint		Designed by	TJL

Tower Section	Tower Elevation ft	Diagonal Spacing ft	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset in	Bottom Girt Offset in
T7	60.00-40.00	10.00	X Brace	No	No	0.0000	0.0000
T8	40.00-20.00	10.00	X Brace	No	No	0.0000	0.0000
T9	20.00-0.00	10.00	X Brace	No	No	0.0000	0.0000

Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 180.00-160.00	Pipe	P2.5x.276	A500-50 (50 ksi)	Single Angle	L2x2x1/8	A572-50 (50 ksi)
T2 160.00-140.00	Pipe	P3x.3	A500-50 (50 ksi)	Single Angle	L2x2x3/16	A572-50 (50 ksi)
T3 140.00-120.00	Pipe	P5x0.5	A500-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x1/4	A572-50 (50 ksi)
T4 120.00-100.00	Pipe	P5x0.5	A500-50 (50 ksi)	Single Angle	L3 1/2x3x1/4	A572-50 (50 ksi)
T5 100.00-80.00	Pipe	P5x0.5	A500-50 (50 ksi)	Single Angle	L3 1/2x3x1/4	A572-50 (50 ksi)
T6 80.00-60.00	Pipe	P8x.5	A500-50 (50 ksi)	Single Angle	L4x3 1/2x5/16	A572-50 (50 ksi)
T7 60.00-40.00	Pipe	P8x.5	A500-50 (50 ksi)	Single Angle	L4x3 1/2x3/8	A572-50 (50 ksi)
T8 40.00-20.00	Pipe	P8x.5	A500-50 (50 ksi)	Single Angle	L4x4x3/8	A572-50 (50 ksi)
T9 20.00-0.00	Pipe	P10x.5	A500-50 (50 ksi)	Single Angle	L5x5x5/16	A572-50 (50 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 180.00-160.00	Equal Angle	L2x2x1/8	A36 (36 ksi)	Solid Round		A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Gusset Area (per face) ft ²	Gusset Thickness in	Gusset Grade	Adjust. Factor A _f	Adjust. Factor A _r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
180.00-160.00 T1	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
160.00-140.00 T2	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000

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Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A_f	Adjust. Factor A_r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
ft	ft ²	in							
T3 140.00-120.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T4 120.00-100.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T5 100.00-80.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T6 80.00-60.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T7 60.00-40.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T8 40.00-20.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T9 20.00-0.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000

Tower Section Geometry (cont'd)

Tower Elevation	Calc K Single Angles	Calc K Solid Rounds	Legs	K Factors ¹						
				X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
				X Y	X Y	X Y	X Y	X Y	X Y	X Y
T1 180.00-160.00	Yes	Yes	1	1	1	1	1	1	1	1
T2 160.00-140.00	Yes	Yes	1	1	1	1	1	1	1	1
T3 140.00-120.00	Yes	Yes	1	1	1	1	1	1	1	1
T4 120.00-100.00	Yes	Yes	1	1	1	1	1	1	1	1
T5 100.00-80.00	Yes	Yes	1	1	1	1	1	1	1	1
T6 80.00-60.00	Yes	Yes	1	1	1	1	1	1	1	1
T7 60.00-40.00	Yes	Yes	1	1	1	1	1	1	1	1
T8 40.00-20.00	Yes	Yes	1	1	1	1	1	1	1	1
T9 20.00-0.00	Yes	Yes	1	1	1	1	1	1	1	1

¹Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

Tower Section Geometry (cont'd)

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	Client	Sprint		Designed by	TJL

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 180.00-160.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 160.00-140.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 140.00-120.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 120.00-100.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T5 100.00-80.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T6 80.00-60.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T7 60.00-40.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T8 40.00-20.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T9 20.00-0.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1 180.00-160.00	Flange	0.7500	0	0.6250	1	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T2 160.00-140.00	Flange	0.7500	0	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T3 140.00-120.00	Flange	0.7500	0	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T4 120.00-100.00	Flange	1.5000	0	0.7500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T5 100.00-80.00	Flange	1.5000	0	0.7500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T6 80.00-60.00	Flange	1.5000	0	0.7500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T7 60.00-40.00	Flange	1.5000	0	0.7500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T8 40.00-20.00	Flange	1.5000	0	0.7500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T9 20.00-0.00	Flange	1.5000	6	0.7500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		F1554-105		A325X		A325N		A325N		A325N		A325N		A325N	

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	# Per Row	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
1 5/8 (Eversource)	B	No	Ar (CaAa)	180.00 - 8.00	0.0000	0.36	4	2	1.9800	1.9800		1.04

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Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
7/8 (Eversource)	B	No	Ar (CaAa)	180.00 - 8.00	0.0000	0.34	1	1	1.1100	1.1100		0.54
1/2 (Eversource)	B	No	Ar (CaAa)	180.00 - 8.00	0.0000	0.34	1	1	0.5800	0.5800		0.25
1 (Eversource)	B	No	Ar (CaAa)	180.00 - 8.00	0.0000	0.32	1	1	1.2500	1.2500		0.58
WE65 (Eversource)	B	No	Ar (CaAa)	175.00 - 8.00	0.0000	0.42	6	3	1.5836	1.5836		0.53
WE65 (Eversource)	B	No	Ar (CaAa)	164.00 - 8.00	0.0000	0.38	2	2	1.5836	1.5836		0.53
7/8 (Eversource)	B	No	Ar (CaAa)	158.00 - 8.00	0.0000	0.3	2	1	1.1100	1.1100		0.54
HYBRIFLEX 1-1/4" (Sprint)	C	No	Ar (CaAa)	130.00 - 8.00	0.0000	-0.4	4	4	1.5400	1.5400		1.30
1 5/8 (Future Carrier)	A	No	Ar (CaAa)	120.00 - 8.00	0.0000	0.3	21	11	1.9800	1.9800		1.04
1 5/8 (Future Carrier)	B	No	Ar (CaAa)	110.00 - 8.00	0.0000	-0.3	21	11	1.9800	1.9800		1.04
1 5/8 (Future Carrier)	C	No	Ar (CaAa)	100.00 - 8.00	0.0000	0.3	21	11	1.9800	1.9800		1.04

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
T1	180.00-160.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	37.239	0.000	0.16
		C	0.000	0.000	0.000	0.000	0.00
T2	160.00-140.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	51.053	0.000	0.21
		C	0.000	0.000	0.000	0.000	0.00
T3	140.00-120.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	51.497	0.000	0.22
		C	0.000	0.000	6.160	0.000	0.05
T4	120.00-100.00	A	0.000	0.000	83.160	0.000	0.44
		B	0.000	0.000	93.077	0.000	0.44
		C	0.000	0.000	12.320	0.000	0.10
T5	100.00-80.00	A	0.000	0.000	83.160	0.000	0.44
		B	0.000	0.000	134.657	0.000	0.65
		C	0.000	0.000	95.480	0.000	0.54
T6	80.00-60.00	A	0.000	0.000	83.160	0.000	0.44
		B	0.000	0.000	134.657	0.000	0.65
		C	0.000	0.000	95.480	0.000	0.54
T7	60.00-40.00	A	0.000	0.000	83.160	0.000	0.44
		B	0.000	0.000	134.657	0.000	0.65
		C	0.000	0.000	95.480	0.000	0.54
T8	40.00-20.00	A	0.000	0.000	83.160	0.000	0.44
		B	0.000	0.000	134.657	0.000	0.65
		C	0.000	0.000	95.480	0.000	0.54
T9	20.00-0.00	A	0.000	0.000	49.896	0.000	0.26
		B	0.000	0.000	80.794	0.000	0.39

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Tower Section	Tower Elevation ft	Face	A_R ft ²	A_F ft ²	C_{AA} In Face ft ²	C_{AA} Out Face ft ²	Weight K
		C	0.000	0.000	57.288	0.000	0.32

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A_R ft ²	A_F ft ²	C_{AA} In Face ft ²	C_{AA} Out Face ft ²	Weight K
T1	180.00-160.00	A	2.945	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	122.241	0.000	2.72
		C		0.000	0.000	0.000	0.000	0.00
T2	160.00-140.00	A	2.909	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	183.751	0.000	3.87
		C		0.000	0.000	0.000	0.000	0.00
T3	140.00-120.00	A	2.867	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	184.965	0.000	3.86
		C		0.000	0.000	22.557	0.000	0.45
T4	120.00-100.00	A	2.820	0.000	0.000	121.547	0.000	3.94
		B		0.000	0.000	243.836	0.000	5.75
		C		0.000	0.000	44.802	0.000	0.88
T5	100.00-80.00	A	2.764	0.000	0.000	121.209	0.000	3.90
		B		0.000	0.000	302.028	0.000	7.58
		C		0.000	0.000	165.642	0.000	4.76
T6	80.00-60.00	A	2.695	0.000	0.000	120.794	0.000	3.84
		B		0.000	0.000	298.868	0.000	7.41
		C		0.000	0.000	164.777	0.000	4.68
T7	60.00-40.00	A	2.606	0.000	0.000	120.257	0.000	3.76
		B		0.000	0.000	294.761	0.000	7.19
		C		0.000	0.000	163.655	0.000	4.57
T8	40.00-20.00	A	2.476	0.000	0.000	119.476	0.000	3.65
		B		0.000	0.000	288.788	0.000	6.88
		C		0.000	0.000	162.025	0.000	4.42
T9	20.00-0.00	A	2.219	0.000	0.000	70.759	0.000	2.06
		B		0.000	0.000	166.165	0.000	3.77
		C		0.000	0.000	95.283	0.000	2.48

Feed Line Center of Pressure

Section	Elevation ft	CP_x in	CP_z in	CP_x Ice in	CP_z Ice in
T1	180.00-160.00	5.0894	1.8428	2.5391	0.8865
T2	160.00-140.00	6.9381	2.5952	4.0233	1.3833
T3	140.00-120.00	7.8683	3.2783	5.1931	2.0047
T4	120.00-100.00	3.5018	-5.9550	3.4434	-2.9211
T5	100.00-80.00	0.3520	-3.4771	1.4120	-1.8168
T6	80.00-60.00	0.3828	-3.8635	1.5850	-2.1003
T7	60.00-40.00	0.4199	-4.3111	1.7278	-2.3776
T8	40.00-20.00	0.4562	-4.7498	1.8425	-2.6789
T9	20.00-0.00	0.4009	-4.2139	1.5620	-2.5424

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Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K _a No Ice	K _a Ice
T1	1	1 5/8	160.00 - 180.00	0.6000	0.4660
T1	2	7/8	160.00 - 180.00	0.6000	0.4660
T1	3	1/2	160.00 - 180.00	0.6000	0.4660
T1	4	1	160.00 - 180.00	0.6000	0.4660
T1	5	WE65	160.00 - 175.00	0.6000	0.4660
T1	6	WE65	160.00 - 164.00	0.6000	0.4660
T2	1	1 5/8	140.00 - 160.00	0.6000	0.5525
T2	2	7/8	140.00 - 160.00	0.6000	0.5525
T2	3	1/2	140.00 - 160.00	0.6000	0.5525
T2	4	1	140.00 - 160.00	0.6000	0.5525
T2	5	WE65	140.00 - 160.00	0.6000	0.5525
T2	6	WE65	140.00 - 160.00	0.6000	0.5525
T2	7	7/8	140.00 - 158.00	0.6000	0.5525
T3	1	1 5/8	120.00 - 140.00	0.6000	0.6000
T3	2	7/8	120.00 - 140.00	0.6000	0.6000
T3	3	1/2	120.00 - 140.00	0.6000	0.6000
T3	4	1	120.00 - 140.00	0.6000	0.6000
T3	5	WE65	120.00 - 140.00	0.6000	0.6000
T3	6	WE65	120.00 - 140.00	0.6000	0.6000
T3	7	7/8	120.00 - 140.00	0.6000	0.6000
T3	9	HYBRIFLEX 1-1/4"	120.00 - 130.00	0.6000	0.6000
T4	1	1 5/8	100.00 - 120.00	0.6000	0.6000
T4	2	7/8	100.00 - 120.00	0.6000	0.6000
T4	3	1/2	100.00 - 120.00	0.6000	0.6000
T4	4	1	100.00 - 120.00	0.6000	0.6000
T4	5	WE65	100.00 - 120.00	0.6000	0.6000
T4	6	WE65	100.00 - 120.00	0.6000	0.6000
T4	7	7/8	100.00 - 120.00	0.6000	0.6000
T4	9	HYBRIFLEX 1-1/4"	100.00 -	0.6000	0.6000

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Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K _a No Ice	K _a Ice
			120.00		
T4	10	1 5/8	100.00 - 120.00	0.6000	0.6000
T4	11	1 5/8	100.00 - 110.00	0.6000	0.6000
T5	1	1 5/8	80.00 - 100.00	0.6000	0.6000
T5	2	7/8	80.00 - 100.00	0.6000	0.6000
T5	3	1/2	80.00 - 100.00	0.6000	0.6000
T5	4	1	80.00 - 100.00	0.6000	0.6000
T5	5	WE65	80.00 - 100.00	0.6000	0.6000
T5	6	WE65	80.00 - 100.00	0.6000	0.6000
T5	7	7/8	80.00 - 100.00	0.6000	0.6000
T5	9	HYBRIFLEX 1-1/4"	80.00 - 100.00	0.6000	0.6000
T5	10	1 5/8	80.00 - 100.00	0.6000	0.6000
T5	11	1 5/8	80.00 - 100.00	0.6000	0.6000
T5	12	1 5/8	80.00 - 100.00	0.6000	0.6000
T6	1	1 5/8	60.00 - 80.00	0.6000	0.6000
T6	2	7/8	60.00 - 80.00	0.6000	0.6000
T6	3	1/2	60.00 - 80.00	0.6000	0.6000
T6	4	1	60.00 - 80.00	0.6000	0.6000
T6	5	WE65	60.00 - 80.00	0.6000	0.6000
T6	6	WE65	60.00 - 80.00	0.6000	0.6000
T6	7	7/8	60.00 - 80.00	0.6000	0.6000
T6	9	HYBRIFLEX 1-1/4"	60.00 - 80.00	0.6000	0.6000
T6	10	1 5/8	60.00 - 80.00	0.6000	0.6000
T6	11	1 5/8	60.00 - 80.00	0.6000	0.6000
T6	12	1 5/8	60.00 - 80.00	0.6000	0.6000
T7	1	1 5/8	40.00 - 60.00	0.6000	0.6000
T7	2	7/8	40.00 - 60.00	0.6000	0.6000
T7	3	1/2	40.00 - 60.00	0.6000	0.6000
T7	4	1	40.00 - 60.00	0.6000	0.6000
T7	5	WE65	40.00 - 60.00	0.6000	0.6000
T7	6	WE65	40.00 - 60.00	0.6000	0.6000
T7	7	7/8	40.00 - 60.00	0.6000	0.6000
T7	9	HYBRIFLEX 1-1/4"	40.00 - 60.00	0.6000	0.6000
T7	10	1 5/8	40.00 - 60.00	0.6000	0.6000
T7	11	1 5/8	40.00 - 60.00	0.6000	0.6000
T7	12	1 5/8	40.00 - 60.00	0.6000	0.6000
T8	1	1 5/8	20.00 - 40.00	0.6000	0.6000
T8	2	7/8	20.00 - 40.00	0.6000	0.6000
T8	3	1/2	20.00 - 40.00	0.6000	0.6000
T8	4	1	20.00 - 40.00	0.6000	0.6000
T8	5	WE65	20.00 - 40.00	0.6000	0.6000
T8	6	WE65	20.00 - 40.00	0.6000	0.6000
T8	7	7/8	20.00 - 40.00	0.6000	0.6000
T8	9	HYBRIFLEX 1-1/4"	20.00 - 40.00	0.6000	0.6000
T8	10	1 5/8	20.00 - 40.00	0.6000	0.6000
T8	11	1 5/8	20.00 - 40.00	0.6000	0.6000
T8	12	1 5/8	20.00 - 40.00	0.6000	0.6000
T9	1	1 5/8	8.00 - 20.00	0.6000	0.6000
T9	2	7/8	8.00 - 20.00	0.6000	0.6000
T9	3	1/2	8.00 - 20.00	0.6000	0.6000
T9	4	1	8.00 - 20.00	0.6000	0.6000
T9	5	WE65	8.00 - 20.00	0.6000	0.6000
T9	6	WE65	8.00 - 20.00	0.6000	0.6000
T9	7	7/8	8.00 - 20.00	0.6000	0.6000
T9	9	HYBRIFLEX 1-1/4"	8.00 - 20.00	0.6000	0.6000
T9	10	1 5/8	8.00 - 20.00	0.6000	0.6000
T9	11	1 5/8	8.00 - 20.00	0.6000	0.6000
T9	12	1 5/8	8.00 - 20.00	0.6000	0.6000

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Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	CAAA Front	CAAA Side	Weight
			Horz Lateral	Vert					
			ft	ft	°	ft	ft ²	ft ²	K
DS9A09F36D-N (Eversource)	A	From Leg	1.00	0.0000	189.40	No Ice	5.78	5.78	0.05
			0.00			1/2" Ice	7.73	7.73	0.09
			0.00			1" Ice	9.71	9.71	0.15
24' x 6" Omni (Eversource)	B	From Leg	1.00	0.0000	189.00	No Ice	7.36	7.36	0.10
			0.00			1/2" Ice	16.86	16.86	0.20
			0.00			1" Ice	19.33	19.33	0.31
CO-41A (Eversource)	C	From Leg	1.00	0.0000	187.00	No Ice	2.27	2.27	0.01
			0.00			1/2" Ice	3.71	3.71	0.03
			0.00			1" Ice	5.16	5.16	0.06
Tower Top Amplifier (Eversource)	A	From Leg	1.00	0.0000	180.00	No Ice	2.67	1.03	0.04
			0.00			1/2" Ice	2.87	1.17	0.06
			0.00			1" Ice	3.08	1.32	0.08
531-70HD (Eversource)	A	From Leg	6.00	0.0000	158.00	No Ice	6.00	6.00	0.04
			0.00			1/2" Ice	6.90	6.90	0.05
			0.00			1" Ice	7.80	7.80	0.06
SD212 (Eversource)	A	From Leg	6.00	0.0000	158.00	No Ice	2.14	2.14	0.03
			0.00			1/2" Ice	3.71	3.71	0.06
			0.00			1" Ice	5.28	5.28	0.08
ROHN 6-ft Side Arm (Eversource)	A	From Leg	3.00	0.0000	158.00	No Ice	6.68	6.68	0.08
			0.00			1/2" Ice	10.00	10.00	0.10
			0.00			1" Ice	13.32	13.32	0.13
24' x 6" Omni (Eversource)	B	From Leg	6.00	0.0000	156.00	No Ice	7.52	7.52	0.10
			0.00			1/2" Ice	16.86	16.86	0.20
			0.00			1" Ice	19.33	19.33	0.31
ROHN 6-ft Side Arm (Eversource)	B	From Leg	3.00	0.0000	153.00	No Ice	6.68	6.68	0.08
			0.00			1/2" Ice	10.00	10.00	0.10
			0.00			1" Ice	13.32	13.32	0.13
ROHN 3-ft Side Arm (Eversource)	B	From Leg	3.00	0.0000	144.40	No Ice	3.10	3.10	0.07
			0.00			1/2" Ice	5.00	5.00	0.10
			0.00			1" Ice	6.90	6.90	0.13
NNVV-65B-R4 (Sprint - Proposed)	A	From Leg	3.00	0.0000	135.00	No Ice	14.61	9.17	0.11
			3.00			1/2" Ice	15.13	9.63	0.21
			0.00			1" Ice	15.65	10.11	0.32
AAHC (Sprint - Proposed)	A	From Leg	3.00	0.0000	135.00	No Ice	4.20	2.06	0.10
			-3.00			1/2" Ice	4.46	2.25	0.14
			0.00			1" Ice	4.72	2.45	0.17
NNVV-65B-R4 (Sprint - Proposed)	B	From Leg	3.00	0.0000	135.00	No Ice	14.61	9.17	0.11
			3.00			1/2" Ice	15.13	9.63	0.21
			0.00			1" Ice	15.65	10.11	0.32
AAHC (Sprint - Proposed)	B	From Leg	3.00	0.0000	135.00	No Ice	4.20	2.06	0.10
			-3.00			1/2" Ice	4.46	2.25	0.14
			0.00			1" Ice	4.72	2.45	0.17
NNVV-65B-R4 (Sprint - Proposed)	C	From Leg	3.00	0.0000	135.00	No Ice	14.61	9.17	0.11
			3.00			1/2" Ice	15.13	9.63	0.21
			0.00			1" Ice	15.65	10.11	0.32
AAHC (Sprint - Proposed)	C	From Leg	3.00	0.0000	135.00	No Ice	4.20	2.06	0.10
			-3.00			1/2" Ice	4.46	2.25	0.14
			0.00			1" Ice	4.72	2.45	0.17
FD-RRH 2x50 800	A	From Leg	3.00	0.0000	135.00	No Ice	0.00	1.93	0.06

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Client						Designed by		
Sprint						TJL		

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Lateral					
			ft	ft	°	ft	ft ²	ft ²	K
(Sprint - Proposed)			0.00			1/2" Ice	0.00	2.11	0.09
			0.00			1" Ice	0.00	2.29	0.11
FD-RRH 2x50 800	B	From Leg	3.00		0.0000	No Ice	0.00	1.93	0.06
(Sprint - Proposed)			0.00			1/2" Ice	0.00	2.11	0.09
			0.00			1" Ice	0.00	2.29	0.11
FD-RRH 2x50 800	C	From Leg	3.00		0.0000	No Ice	0.00	1.93	0.06
(Sprint - Proposed)			0.00			1/2" Ice	0.00	2.11	0.09
			0.00			1" Ice	0.00	2.29	0.11
FD-RRH 4x45 1900	A	From Leg	3.00		0.0000	No Ice	0.00	2.38	0.06
(Sprint - Proposed)			0.00			1/2" Ice	0.00	2.59	0.08
			0.00			1" Ice	0.00	2.80	0.11
FD-RRH 4x45 1900	B	From Leg	3.00		0.0000	No Ice	0.00	2.38	0.06
(Sprint - Proposed)			0.00			1/2" Ice	0.00	2.59	0.08
			0.00			1" Ice	0.00	2.80	0.11
FD-RRH 4x45 1900	C	From Leg	3.00		0.0000	No Ice	0.00	2.38	0.06
(Sprint - Proposed)			0.00			1/2" Ice	0.00	2.59	0.08
			0.00			1" Ice	0.00	2.80	0.11
FD-RRH 2x50 800	A	From Leg	3.00		0.0000	No Ice	2.06	1.93	0.06
(Sprint - Proposed)			0.00			1/2" Ice	2.24	2.11	0.09
			0.00			1" Ice	2.43	2.29	0.11
FD-RRH 2x50 800	B	From Leg	3.00		0.0000	No Ice	2.06	1.93	0.06
(Sprint - Proposed)			0.00			1/2" Ice	2.24	2.11	0.09
			0.00			1" Ice	2.43	2.29	0.11
FD-RRH 2x50 800	C	From Leg	3.00		0.0000	No Ice	2.06	1.93	0.06
(Sprint - Proposed)			0.00			1/2" Ice	2.24	2.11	0.09
			0.00			1" Ice	2.43	2.29	0.11
14' V-Boom	A	From Leg	2.00		0.0000	No Ice	13.00	13.00	0.04
(Sprint - Proposed)			0.00			1/2" Ice	15.00	15.00	0.06
			0.00			1" Ice	17.00	17.00	0.07
14' V-Boom	B	From Leg	2.00		0.0000	No Ice	13.00	13.00	0.04
(Sprint - Proposed)			0.00			1/2" Ice	15.00	15.00	0.06
			0.00			1" Ice	17.00	17.00	0.07
14' V-Boom	C	From Leg	2.00		0.0000	No Ice	13.00	13.00	0.04
(Sprint - Proposed)			0.00			1/2" Ice	15.00	15.00	0.06
			0.00			1" Ice	17.00	17.00	0.07
(4) 8' x1' Panel	A	From Leg	3.00		0.0000	No Ice	11.47	6.80	0.03
(Future Carrier)			0.00			1/2" Ice	12.08	7.38	0.09
			0.00			1" Ice	12.71	7.98	0.16
(4) 8' x1' Panel	B	From Leg	3.00		0.0000	No Ice	11.47	6.80	0.03
(Future Carrier)			0.00			1/2" Ice	12.08	7.38	0.09
			0.00			1" Ice	12.71	7.98	0.16
(4) 8' x1' Panel	C	From Leg	3.00		0.0000	No Ice	11.47	6.80	0.03
(Future Carrier)			0.00			1/2" Ice	12.08	7.38	0.09
			0.00			1" Ice	12.71	7.98	0.16
(4) RRUS-11	A	From Leg	3.00		0.0000	No Ice	0.00	1.07	0.05
(Future Carrier)			0.00			1/2" Ice	0.00	1.21	0.07
			0.00			1" Ice	0.00	1.36	0.09
(4) RRUS-11	B	From Leg	3.00		0.0000	No Ice	0.00	1.07	0.05
(Future Carrier)			0.00			1/2" Ice	0.00	1.21	0.07
			0.00			1" Ice	0.00	1.36	0.09
(4) RRUS-11	C	From Leg	3.00		0.0000	No Ice	0.00	1.07	0.05
(Future Carrier)			0.00			1/2" Ice	0.00	1.21	0.07
			0.00			1" Ice	0.00	1.36	0.09
(3) RC2DC-3315-PF-48	A	From Leg	3.00		0.0000	No Ice	0.00	1.96	0.03
(Future Carrier)			0.00			1/2" Ice	0.00	2.15	0.05
			0.00			1" Ice	0.00	2.35	0.08
14' V-Boom	A	From Leg	2.00		0.0000	No Ice	13.00	13.00	0.04

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	Project		180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT					Date		13:56:50 01/03/19
	Client		Sprint					Designed by		TJL

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight	
			Horz	Lateral						Vert
(Future Carrier)			0.00						0.06	
			0.00			1/2" Ice	15.00	15.00	0.07	
14' V-Boom	B	From Leg	2.00		0.0000	125.00	No Ice	13.00	13.00	0.04
(Future Carrier)			0.00				1/2" Ice	15.00	15.00	0.06
			0.00				1" Ice	17.00	17.00	0.07
14' V-Boom	C	From Leg	2.00		0.0000	125.00	No Ice	13.00	13.00	0.04
(Future Carrier)			0.00				1/2" Ice	15.00	15.00	0.06
			0.00				1" Ice	17.00	17.00	0.07
(4) 8' x1' Panel	A	From Leg	3.00		0.0000	115.00	No Ice	11.47	6.80	0.03
(Future Carrier)			0.00				1/2" Ice	12.08	7.38	0.09
			0.00				1" Ice	12.71	7.98	0.16
(4) 8' x1' Panel	B	From Leg	3.00		0.0000	115.00	No Ice	11.47	6.80	0.03
(Future Carrier)			0.00				1/2" Ice	12.08	7.38	0.09
			0.00				1" Ice	12.71	7.98	0.16
(4) 8' x1' Panel	C	From Leg	3.00		0.0000	115.00	No Ice	11.47	6.80	0.03
(Future Carrier)			0.00				1/2" Ice	12.08	7.38	0.09
			0.00				1" Ice	12.71	7.98	0.16
(4) RRUS-11	A	From Leg	3.00		0.0000	115.00	No Ice	0.00	1.07	0.05
(Future Carrier)			0.00				1/2" Ice	0.00	1.21	0.07
			0.00				1" Ice	0.00	1.36	0.09
(4) RRUS-11	B	From Leg	3.00		0.0000	115.00	No Ice	0.00	1.07	0.05
(Future Carrier)			0.00				1/2" Ice	0.00	1.21	0.07
			0.00				1" Ice	0.00	1.36	0.09
(4) RRUS-11	C	From Leg	3.00		0.0000	115.00	No Ice	0.00	1.07	0.05
(Future Carrier)			0.00				1/2" Ice	0.00	1.21	0.07
			0.00				1" Ice	0.00	1.36	0.09
(3) RC2DC-3315-PF-48	A	From Leg	3.00		0.0000	115.00	No Ice	0.00	1.96	0.03
(Future Carrier)			0.00				1/2" Ice	0.00	2.15	0.05
			0.00				1" Ice	0.00	2.35	0.08
14' V-Boom	A	From Leg	2.00		0.0000	115.00	No Ice	13.00	13.00	0.04
(Future Carrier)			0.00				1/2" Ice	15.00	15.00	0.06
			0.00				1" Ice	17.00	17.00	0.07
14' V-Boom	B	From Leg	2.00		0.0000	115.00	No Ice	13.00	13.00	0.04
(Future Carrier)			0.00				1/2" Ice	15.00	15.00	0.06
			0.00				1" Ice	17.00	17.00	0.07
14' V-Boom	C	From Leg	2.00		0.0000	115.00	No Ice	13.00	13.00	0.04
(Future Carrier)			0.00				1/2" Ice	15.00	15.00	0.06
			0.00				1" Ice	17.00	17.00	0.07
(4) 8' x1' Panel	A	From Leg	3.00		0.0000	105.00	No Ice	11.47	6.80	0.03
(Future Carrier)			0.00				1/2" Ice	12.08	7.38	0.09
			0.00				1" Ice	12.71	7.98	0.16
(4) 8' x1' Panel	B	From Leg	3.00		0.0000	105.00	No Ice	11.47	6.80	0.03
(Future Carrier)			0.00				1/2" Ice	12.08	7.38	0.09
			0.00				1" Ice	12.71	7.98	0.16
(4) 8' x1' Panel	C	From Leg	3.00		0.0000	105.00	No Ice	11.47	6.80	0.03
(Future Carrier)			0.00				1/2" Ice	12.08	7.38	0.09
			0.00				1" Ice	12.71	7.98	0.16
(4) RRUS-11	A	From Leg	3.00		0.0000	105.00	No Ice	0.00	1.07	0.05
(Future Carrier)			0.00				1/2" Ice	0.00	1.21	0.07
			0.00				1" Ice	0.00	1.36	0.09
(4) RRUS-11	B	From Leg	3.00		0.0000	105.00	No Ice	0.00	1.07	0.05
(Future Carrier)			0.00				1/2" Ice	0.00	1.21	0.07
			0.00				1" Ice	0.00	1.36	0.09
(4) RRUS-11	C	From Leg	3.00		0.0000	105.00	No Ice	0.00	1.07	0.05
(Future Carrier)			0.00				1/2" Ice	0.00	1.21	0.07
			0.00				1" Ice	0.00	1.36	0.09
(3) RC2DC-3315-PF-48	A	From Leg	3.00		0.0000	105.00	No Ice	0.00	1.96	0.03

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	Project 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Date 13:56:50 01/03/19
	Client Sprint	Designed by TJL

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz Lateral	Vert					
			ft	ft	°	ft	ft ²	ft ²	K
(Future Carrier)			0.00	0.00		1/2" Ice	0.00	2.15	0.05
14' V-Boom	A	From Leg	2.00	0.0000	105.00	No Ice	13.00	13.00	0.04
(Future Carrier)			0.00	0.00		1/2" Ice	15.00	15.00	0.06
14' V-Boom	B	From Leg	2.00	0.0000	105.00	No Ice	13.00	13.00	0.04
(Future Carrier)			0.00	0.00		1/2" Ice	15.00	15.00	0.06
14' V-Boom	C	From Leg	2.00	0.0000	105.00	No Ice	13.00	13.00	0.04
(Future Carrier)			0.00	0.00		1/2" Ice	15.00	15.00	0.06
			0.00	0.00		1" Ice	17.00	17.00	0.07

Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight
				Horz Lateral	Vert						
			ft	ft	°	°	ft	ft	ft ²	K	
8' Dish	A	Paraboloid w/o Radome	From Leg	1.00	0.0000	175.00	8.00	No Ice	50.27	0.10	
(Eversource)				0.00	0.00			1/2" Ice	51.32	0.26	
				0.00	0.00			1" Ice	52.37	0.49	
8' Dish	B	Paraboloid w/o Radome	From Leg	1.00	0.0000	175.00	8.00	No Ice	50.27	0.10	
(Eversource)				0.00	0.00			1/2" Ice	51.32	0.26	
				0.00	0.00			1" Ice	52.37	0.49	
8' Dish	C	Paraboloid w/o Radome	From Leg	1.00	0.0000	175.00	8.00	No Ice	50.27	0.10	
(Eversource)				0.00	0.00			1/2" Ice	51.32	0.26	
				0.00	0.00			1" Ice	52.37	0.49	
8' Dish	A	Paraboloid w/o Radome	From Leg	1.00	0.0000	164.00	8.00	No Ice	50.27	0.10	
(Eversource)				0.00	0.00			1/2" Ice	51.32	0.26	
				0.00	0.00			1" Ice	52.37	0.49	

Tower Pressures - No Ice

$G_H = 0.850$

Section Elevation	z	K _Z	q _z	A _G	F a c e	A _F	A _R	A _{leg}	Leg %	C _{AA} In Face	C _{AA} Out Face
ft	ft		psf	ft ²	e	ft ²	ft ²	ft ²		ft ²	ft ²
T1	170.00	1.415	33	124.798	A	10.802	9.599	9.599	47.05	0.000	0.000
180.00-160.00					B	10.802	9.599		47.05	37.239	0.000
					C	10.802	9.599		47.05	0.000	0.000
T2	150.00	1.378	32	165.841	A	12.137	11.686	11.686	49.05	0.000	0.000
160.00-140.00					B	12.137	11.686		49.05	51.053	0.000
					C	12.137	11.686		49.05	0.000	0.000
T3	130.00	1.337	31	209.283	A	14.377	18.574	18.574	56.37	0.000	0.000

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	Client Sprint	Designed by TJL

Section Elevation ft	z ft	K _Z	q _z psf	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _{AA} In Face ft ²	C _{AA} Out Face ft ²
140.00-120.00					B	14.377	18.574		56.37	51.497	0.000
					C	14.377	18.574		56.37	6.160	0.000
T4 120.00-100.00	110.00	1.291	30	249.283	A	23.101	18.574	18.574	44.57	83.160	0.000
					B	23.101	18.574		44.57	93.077	0.000
					C	23.101	18.574		44.57	12.320	0.000
T5 100.00-80.00	90.00	1.238	29	289.283	A	26.242	18.574	18.574	41.45	83.160	0.000
					B	26.242	18.574		41.45	134.657	0.000
					C	26.242	18.574		41.45	95.480	0.000
T6 80.00-60.00	70.00	1.174	28	334.393	A	24.133	28.798	28.798	54.41	83.160	0.000
					B	24.133	28.798		54.41	134.657	0.000
					C	24.133	28.798		54.41	95.480	0.000
T7 60.00-40.00	50.00	1.094	26	374.393	A	26.363	28.798	28.798	52.21	83.160	0.000
					B	26.363	28.798		52.21	134.657	0.000
					C	26.363	28.798		52.21	95.480	0.000
T8 40.00-20.00	30.00	0.982	23	414.393	A	28.747	28.798	28.798	50.04	83.160	0.000
					B	28.747	28.798		50.04	134.657	0.000
					C	28.747	28.798		50.04	95.480	0.000
T9 20.00-0.00	10.00	0.85	20	457.939	A	38.722	35.893	35.893	48.10	49.896	0.000
					B	38.722	35.893		48.10	80.794	0.000
					C	38.722	35.893		48.10	57.288	0.000

Tower Pressure - With Ice

$G_H = 0.850$

Section Elevation ft	z ft	K _Z	q _z psf	t _z in	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _{AA} In Face ft ²	C _{AA} Out Face ft ²
T1 180.00-160.00	170.00	1.415	8	2.9453	134.628	A	10.802	61.083	29.268	40.71	0.000	0.000
						B	10.802	61.083		40.71	122.241	0.000
						C	10.802	61.083		40.71	0.000	0.000
T2 160.00-140.00	150.00	1.378	7	2.9087	175.548	A	12.137	66.414	31.110	39.60	0.000	0.000
						B	12.137	66.414		39.60	183.751	0.000
						C	12.137	66.414		39.60	0.000	0.000
T3 140.00-120.00	130.00	1.337	7	2.8674	218.853	A	14.377	70.700	37.722	44.34	0.000	0.000
						B	14.377	70.700		44.34	184.965	0.000
						C	14.377	70.700		44.34	22.557	0.000
T4 120.00-100.00	110.00	1.291	7	2.8199	258.695	A	23.101	74.629	37.405	38.27	121.547	0.000
						B	23.101	74.629		38.27	243.836	0.000
						C	23.101	74.629		38.27	44.802	0.000
T5 100.00-80.00	90.00	1.238	7	2.7638	298.508	A	26.242	78.476	37.030	35.36	121.209	0.000
						B	26.242	78.476		35.36	302.028	0.000
						C	26.242	78.476		35.36	165.642	0.000
T6 80.00-60.00	70.00	1.174	6	2.6952	343.388	A	24.133	79.319	46.796	45.23	120.794	0.000
						B	24.133	79.319		45.23	298.868	0.000
						C	24.133	79.319		45.23	164.777	0.000
T7 60.00-40.00	50.00	1.094	6	2.6061	383.091	A	26.363	80.553	46.201	43.21	120.257	0.000
						B	26.363	80.553		43.21	294.761	0.000
						C	26.363	80.553		43.21	163.655	0.000
T8 40.00-20.00	30.00	0.982	5	2.4763	422.658	A	28.747	80.926	45.334	41.34	119.476	0.000
						B	28.747	80.926		41.34	288.788	0.000
						C	28.747	80.926		41.34	162.025	0.000
T9 20.00-0.00	10.00	0.85	5	2.2186	465.344	A	38.722	85.073	50.709	40.96	70.759	0.000
						B	38.722	85.073		40.96	166.165	0.000
						C	38.722	85.073		40.96	95.283	0.000

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	Project 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Date 13:56:50 01/03/19
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Tower Pressure - Service

$G_H = 0.850$

Section Elevation ft	z ft	K_Z	q_z psf	A_G ft ²	F a c e	A_F ft ²	A_R ft ²	A_{leg} ft ²	Leg %	C_{AA} In Face ft ²	C_{AA} Out Face ft ²
T1 180.00-160.00	170.00	1.415	29	124.798	A	10.802	9.599	9.599	47.05	0.000	0.000
					B	10.802	9.599	47.05	37.239	0.000	
					C	10.802	9.599	47.05	0.000	0.000	
T2 160.00-140.00	150.00	1.378	28	165.841	A	12.137	11.686	11.686	49.05	0.000	0.000
					B	12.137	11.686	49.05	51.053	0.000	
					C	12.137	11.686	49.05	0.000	0.000	
T3 140.00-120.00	130.00	1.337	27	209.283	A	14.377	18.574	18.574	56.37	0.000	0.000
					B	14.377	18.574	56.37	51.497	0.000	
					C	14.377	18.574	56.37	6.160	0.000	
T4 120.00-100.00	110.00	1.291	26	249.283	A	23.101	18.574	18.574	44.57	83.160	0.000
					B	23.101	18.574	44.57	93.077	0.000	
					C	23.101	18.574	44.57	12.320	0.000	
T5 100.00-80.00	90.00	1.238	25	289.283	A	26.242	18.574	18.574	41.45	83.160	0.000
					B	26.242	18.574	41.45	134.657	0.000	
					C	26.242	18.574	41.45	95.480	0.000	
T6 80.00-60.00	70.00	1.174	24	334.393	A	24.133	28.798	28.798	54.41	83.160	0.000
					B	24.133	28.798	54.41	134.657	0.000	
					C	24.133	28.798	54.41	95.480	0.000	
T7 60.00-40.00	50.00	1.094	22	374.393	A	26.363	28.798	28.798	52.21	83.160	0.000
					B	26.363	28.798	52.21	134.657	0.000	
					C	26.363	28.798	52.21	95.480	0.000	
T8 40.00-20.00	30.00	0.982	20	414.393	A	28.747	28.798	28.798	50.04	83.160	0.000
					B	28.747	28.798	50.04	134.657	0.000	
					C	28.747	28.798	50.04	95.480	0.000	
T9 20.00-0.00	10.00	0.85	17	457.939	A	38.722	35.893	35.893	48.10	49.896	0.000
					B	38.722	35.893	48.10	80.794	0.000	
					C	38.722	35.893	48.10	57.288	0.000	

Tower Forces - No Ice - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C_F	q_z psf	D_F	D_R	A_E ft ²	F K	w plf	Ctrl. Face
T1 180.00-160.00	0.16	0.79	A	0.163	2.723	33	1	1	16.265	1.89	94.35	C
			B	0.163	2.723	1	1	16.265				
			C	0.163	2.723	1	1	16.265				
T2 160.00-140.00	0.21	1.17	A	0.144	2.795	32	1	1	18.562	2.28	113.81	C
			B	0.144	2.795	1	1	18.562				
			C	0.144	2.795	1	1	18.562				
T3 140.00-120.00	0.27	2.50	A	0.157	2.744	31	1	1	22.921	2.61	130.49	C
			B	0.157	2.744	1	1	22.921				
			C	0.157	2.744	1	1	22.921				
T4 120.00-100.00	0.98	2.94	A	0.167	2.709	30	1	1	31.802	5.15	257.52	C
			B	0.167	2.709	1	1	31.802				
			C	0.167	2.709	1	1	31.802				
T5 100.00-80.00	1.63	3.11	A	0.155	2.753	29	1	1	34.948	7.04	352.04	C
			B	0.155	2.753	1	1	34.948				
			C	0.155	2.753	1	1	34.948				

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	Client Sprint	Designed by TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T6 80.00-60.00	1.63	4.34	C	0.155	2.753	28	1	1	34.948	6.76	337.79	C
			A	0.158	2.741		1	1	36.314			
			B	0.158	2.741		1	1	36.314			
T7 60.00-40.00	1.63	4.86	C	0.158	2.741	26	1	1	36.314	6.45	322.58	C
			A	0.147	2.781		1	1	38.382			
			B	0.147	2.781		1	1	38.382			
T8 40.00-20.00	1.63	5.22	C	0.147	2.781	23	1	1	38.382	5.94	297.14	C
			A	0.139	2.813		1	1	40.644			
			B	0.139	2.813		1	1	40.644			
T9 20.00-0.00	0.98	6.28	C	0.139	2.813	20	1	1	40.644	4.42	221.05	C
			A	0.163	2.724		1	1	53.991			
			B	0.163	2.724		1	1	53.991			
Sum Weight:	9.13	31.22	C	0.163	2.724		1	1	53.991	42.54		
								OTM	3219.69 kip-ft			

Tower Forces - No Ice - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 180.00-160.00	0.16	0.79	A	0.163	2.723	33	0.8	1	14.104	1.72	86.02	C
			B	0.163	2.723		0.8	1	14.104			
			C	0.163	2.723		0.8	1	14.104			
T2 160.00-140.00	0.21	1.17	A	0.144	2.795	32	0.8	1	16.135	2.09	104.45	C
			B	0.144	2.795		0.8	1	16.135			
			C	0.144	2.795		0.8	1	16.135			
T3 140.00-120.00	0.27	2.50	A	0.157	2.744	31	0.8	1	20.046	2.40	119.93	C
			B	0.157	2.744		0.8	1	20.046			
			C	0.157	2.744		0.8	1	20.046			
T4 120.00-100.00	0.98	2.94	A	0.167	2.709	30	0.8	1	27.182	4.83	241.34	C
			B	0.167	2.709		0.8	1	27.182			
			C	0.167	2.709		0.8	1	27.182			
T5 100.00-80.00	1.63	3.11	A	0.155	2.753	29	0.8	1	29.700	6.68	334.14	C
			B	0.155	2.753		0.8	1	29.700			
			C	0.155	2.753		0.8	1	29.700			
T6 80.00-60.00	1.63	4.34	A	0.158	2.741	28	0.8	1	31.487	6.45	322.25	C
			B	0.158	2.741		0.8	1	31.487			
			C	0.158	2.741		0.8	1	31.487			
T7 60.00-40.00	1.63	4.86	A	0.147	2.781	26	0.8	1	33.109	6.13	306.53	C
			B	0.147	2.781		0.8	1	33.109			
			C	0.147	2.781		0.8	1	33.109			
T8 40.00-20.00	1.63	5.22	A	0.139	2.813	23	0.8	1	34.894	5.62	281.24	C
			B	0.139	2.813		0.8	1	34.894			
			C	0.139	2.813		0.8	1	34.894			
T9 20.00-0.00	0.98	6.28	A	0.163	2.724	20	0.8	1	46.246	4.06	203.10	C
			B	0.163	2.724		0.8	1	46.246			
			C	0.163	2.724		0.8	1	46.246			
Sum Weight:	9.13	31.22	C					OTM	3017.09 kip-ft	39.98		

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	Project 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Date 13:56:50 01/03/19
	Client Sprint	Designed by TJL

Tower Forces - No Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 180.00-160.00	0.16	0.79	A	0.163	2.723	33	0.85	1	14.644	1.76	88.10	C
			B	0.163	2.723		0.85	1	14.644			
			C	0.163	2.723		0.85	1	14.644			
T2 160.00-140.00	0.21	1.17	A	0.144	2.795	32	0.85	1	16.742	2.14	106.79	C
			B	0.144	2.795		0.85	1	16.742			
			C	0.144	2.795		0.85	1	16.742			
T3 140.00-120.00	0.27	2.50	A	0.157	2.744	31	0.85	1	20.765	2.45	122.57	C
			B	0.157	2.744		0.85	1	20.765			
			C	0.157	2.744		0.85	1	20.765			
T4 120.00-100.00	0.98	2.94	A	0.167	2.709	30	0.85	1	28.337	4.91	245.38	C
			B	0.167	2.709		0.85	1	28.337			
			C	0.167	2.709		0.85	1	28.337			
T5 100.00-80.00	1.63	3.11	A	0.155	2.753	29	0.85	1	31.012	6.77	338.62	C
			B	0.155	2.753		0.85	1	31.012			
			C	0.155	2.753		0.85	1	31.012			
T6 80.00-60.00	1.63	4.34	A	0.158	2.741	28	0.85	1	32.694	6.52	326.14	C
			B	0.158	2.741		0.85	1	32.694			
			C	0.158	2.741		0.85	1	32.694			
T7 60.00-40.00	1.63	4.86	A	0.147	2.781	26	0.85	1	34.427	6.21	310.55	C
			B	0.147	2.781		0.85	1	34.427			
			C	0.147	2.781		0.85	1	34.427			
T8 40.00-20.00	1.63	5.22	A	0.139	2.813	23	0.85	1	36.332	5.70	285.22	C
			B	0.139	2.813		0.85	1	36.332			
			C	0.139	2.813		0.85	1	36.332			
T9 20.00-0.00	0.98	6.28	A	0.163	2.724	20	0.85	1	48.183	4.15	207.59	C
			B	0.163	2.724		0.85	1	48.183			
			C	0.163	2.724		0.85	1	48.183			
Sum Weight:	9.13	31.22						OTM	3067.74 kip-ft	40.62		

Tower Forces - With Ice - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 180.00-160.00	2.72	6.26	A	0.534	1.86	8	1	1	53.799	1.03	51.38	C
			B	0.534	1.86		1	1	53.799			
			C	0.534	1.86		1	1	53.799			
T2 160.00-140.00	3.87	7.16	A	0.447	1.978	7	1	1	55.841	1.35	67.55	C
			B	0.447	1.978		1	1	55.841			
			C	0.447	1.978		1	1	55.841			
T3 140.00-120.00	4.30	9.13	A	0.389	2.087	7	1	1	59.019	1.53	76.59	C
			B	0.389	2.087		1	1	59.019			
			C	0.389	2.087		1	1	59.019			
T4 120.00-100.00	10.57	11.00	A	0.378	2.11	7	1	1	69.887	2.35	117.49	C
			B	0.378	2.11		1	1	69.887			
			C	0.378	2.11		1	1	69.887			
T5	16.23	11.75	A	0.351	2.17	7	1	1	74.612	2.95	147.45	C

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	Project 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Date 13:56:50 01/03/19
	Client Sprint	Designed by TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
100.00-80.00			B	0.351	2.17		1	1	74.612			
			C	0.351	2.17		1	1	74.612			
T6 80.00-60.00	15.92	12.56	A	0.301	2.293	6	1	1	71.671	2.80	139.79	C
			B	0.301	2.293		1	1	71.671			
			C	0.301	2.293		1	1	71.671			
T7 60.00-40.00	15.53	13.24	A	0.279	2.353	6	1	1	74.106	2.64	131.90	C
			B	0.279	2.353		1	1	74.106			
			C	0.279	2.353		1	1	74.106			
T8 40.00-20.00	14.96	13.84	A	0.259	2.409	5	1	1	76.281	2.39	119.44	C
			B	0.259	2.409		1	1	76.281			
			C	0.259	2.409		1	1	76.281			
T9 20.00-0.00	8.31	15.70	A	0.266	2.39	5	1	1	88.839	1.62	80.90	C
			B	0.266	2.39		1	1	88.839			
			C	0.266	2.39		1	1	88.839			
Sum Weight:	92.41	100.64						OTM	1515.79 kip-ft	18.65		

Tower Forces - With Ice - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 180.00-160.00	2.72	6.26	A	0.534	1.86	8	0.8	1	51.638	1.00	50.06	C
			B	0.534	1.86		0.8	1	51.638			
			C	0.534	1.86		0.8	1	51.638			
T2 160.00-140.00	3.87	7.16	A	0.447	1.978	7	0.8	1	53.413	1.32	66.02	C
			B	0.447	1.978		0.8	1	53.413			
			C	0.447	1.978		0.8	1	53.413			
T3 140.00-120.00	4.30	9.13	A	0.389	2.087	7	0.8	1	56.144	1.49	74.73	C
			B	0.389	2.087		0.8	1	56.144			
			C	0.389	2.087		0.8	1	56.144			
T4 120.00-100.00	10.57	11.00	A	0.378	2.11	7	0.8	1	65.267	2.29	114.58	C
			B	0.378	2.11		0.8	1	65.267			
			C	0.378	2.11		0.8	1	65.267			
T5 100.00-80.00	16.23	11.75	A	0.351	2.17	7	0.8	1	69.363	2.88	144.19	C
			B	0.351	2.17		0.8	1	69.363			
			C	0.351	2.17		0.8	1	69.363			
T6 80.00-60.00	15.92	12.56	A	0.301	2.293	6	0.8	1	66.844	2.74	136.78	C
			B	0.301	2.293		0.8	1	66.844			
			C	0.301	2.293		0.8	1	66.844			
T7 60.00-40.00	15.53	13.24	A	0.279	2.353	6	0.8	1	68.834	2.58	128.76	C
			B	0.279	2.353		0.8	1	68.834			
			C	0.279	2.353		0.8	1	68.834			
T8 40.00-20.00	14.96	13.84	A	0.259	2.409	5	0.8	1	70.532	2.33	116.30	C
			B	0.259	2.409		0.8	1	70.532			
			C	0.259	2.409		0.8	1	70.532			
T9 20.00-0.00	8.31	15.70	A	0.266	2.39	5	0.8	1	81.095	1.55	77.26	C
			B	0.266	2.39		0.8	1	81.095			
			C	0.266	2.39		0.8	1	81.095			
Sum Weight:	92.41	100.64						OTM	1479.68 kip-ft	18.17		

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	Project 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Date 13:56:50 01/03/19
	Client Sprint	Designed by TJL

Tower Forces - With Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 180.00-160.00	2.72	6.26	A	0.534	1.86	8	0.85	1	52.179	1.01	50.39	C
			B	0.534	1.86		0.85		52.179			
			C	0.534	1.86		0.85		52.179			
T2 160.00-140.00	3.87	7.16	A	0.447	1.978	7	0.85	1	54.020	1.33	66.40	C
			B	0.447	1.978		0.85		54.020			
			C	0.447	1.978		0.85		54.020			
T3 140.00-120.00	4.30	9.13	A	0.389	2.087	7	0.85	1	56.863	1.50	75.20	C
			B	0.389	2.087		0.85		56.863			
			C	0.389	2.087		0.85		56.863			
T4 120.00-100.00	10.57	11.00	A	0.378	2.11	7	0.85	1	66.422	2.31	115.31	C
			B	0.378	2.11		0.85		66.422			
			C	0.378	2.11		0.85		66.422			
T5 100.00-80.00	16.23	11.75	A	0.351	2.17	7	0.85	1	70.675	2.90	145.00	C
			B	0.351	2.17		0.85		70.675			
			C	0.351	2.17		0.85		70.675			
T6 80.00-60.00	15.92	12.56	A	0.301	2.293	6	0.85	1	68.051	2.75	137.53	C
			B	0.301	2.293		0.85		68.051			
			C	0.301	2.293		0.85		68.051			
T7 60.00-40.00	15.53	13.24	A	0.279	2.353	6	0.85	1	70.152	2.59	129.55	C
			B	0.279	2.353		0.85		70.152			
			C	0.279	2.353		0.85		70.152			
T8 40.00-20.00	14.96	13.84	A	0.259	2.409	5	0.85	1	71.969	2.34	117.09	C
			B	0.259	2.409		0.85		71.969			
			C	0.259	2.409		0.85		71.969			
T9 20.00-0.00	8.31	15.70	A	0.266	2.39	5	0.85	1	83.031	1.56	78.17	C
			B	0.266	2.39		0.85		83.031			
			C	0.266	2.39		0.85		83.031			
Sum Weight:	92.41	100.64						OTM	1488.71 kip-ft	18.29		

Tower Forces - Service - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 180.00-160.00	0.16	0.79	A	0.163	2.723	29	1	1	16.265	1.64	82.04	C
			B	0.163	2.723		1		16.265			
			C	0.163	2.723		1		16.265			
T2 160.00-140.00	0.21	1.17	A	0.144	2.795	28	1	1	18.562	1.98	98.97	C
			B	0.144	2.795		1		18.562			
			C	0.144	2.795		1		18.562			
T3 140.00-120.00	0.27	2.50	A	0.157	2.744	27	1	1	22.921	2.27	113.47	C
			B	0.157	2.744		1		22.921			
			C	0.157	2.744		1		22.921			
T4 120.00-100.00	0.98	2.94	A	0.167	2.709	26	1	1	31.802	4.48	223.93	C
			B	0.167	2.709		1		31.802			
			C	0.167	2.709		1		31.802			
T5	1.63	3.11	A	0.155	2.753	25	1	1	34.948	6.12	306.12	C

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	Project	180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Date	13:56:50 01/03/19
	Client	Sprint	Designed by	TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
100.00-80.00			B	0.155	2.753		1	1	34.948			
			C	0.155	2.753		1	1	34.948			
T6	1.63	4.34	A	0.158	2.741	24	1	1	36.314	5.87	293.73	C
80.00-60.00			B	0.158	2.741		1	1	36.314			
			C	0.158	2.741		1	1	36.314			
T7	1.63	4.86	A	0.147	2.781	22	1	1	38.382	5.61	280.51	C
60.00-40.00			B	0.147	2.781		1	1	38.382			
			C	0.147	2.781		1	1	38.382			
T8	1.63	5.22	A	0.139	2.813	20	1	1	40.644	5.17	258.38	C
40.00-20.00			B	0.139	2.813		1	1	40.644			
			C	0.139	2.813		1	1	40.644			
T9 20.00-0.00	0.98	6.28	A	0.163	2.724	17	1	1	53.991	3.84	192.22	C
			B	0.163	2.724		1	1	53.991			
			C	0.163	2.724		1	1	53.991			
Sum Weight:	9.13	31.22						OTM	2799.73 kip-ft	36.99		

Tower Forces - Service - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1	0.16	0.79	A	0.163	2.723	29	0.8	1	14.104	1.50	74.80	C
180.00-160.00			B	0.163	2.723		0.8	1	14.104			
			C	0.163	2.723		0.8	1	14.104			
T2	0.21	1.17	A	0.144	2.795	28	0.8	1	16.135	1.82	90.83	C
160.00-140.00			B	0.144	2.795		0.8	1	16.135			
			C	0.144	2.795		0.8	1	16.135			
T3	0.27	2.50	A	0.157	2.744	27	0.8	1	20.046	2.09	104.28	C
140.00-120.00			B	0.157	2.744		0.8	1	20.046			
			C	0.157	2.744		0.8	1	20.046			
T4	0.98	2.94	A	0.167	2.709	26	0.8	1	27.182	4.20	209.86	C
120.00-100.00			B	0.167	2.709		0.8	1	27.182			
			C	0.167	2.709		0.8	1	27.182			
T5	1.63	3.11	A	0.155	2.753	25	0.8	1	29.700	5.81	290.56	C
100.00-80.00			B	0.155	2.753		0.8	1	29.700			
			C	0.155	2.753		0.8	1	29.700			
T6	1.63	4.34	A	0.158	2.741	24	0.8	1	31.487	5.60	280.22	C
80.00-60.00			B	0.158	2.741		0.8	1	31.487			
			C	0.158	2.741		0.8	1	31.487			
T7	1.63	4.86	A	0.147	2.781	22	0.8	1	33.109	5.33	266.55	C
60.00-40.00			B	0.147	2.781		0.8	1	33.109			
			C	0.147	2.781		0.8	1	33.109			
T8	1.63	5.22	A	0.139	2.813	20	0.8	1	34.894	4.89	244.56	C
40.00-20.00			B	0.139	2.813		0.8	1	34.894			
			C	0.139	2.813		0.8	1	34.894			
T9 20.00-0.00	0.98	6.28	A	0.163	2.724	17	0.8	1	46.246	3.53	176.61	C
			B	0.163	2.724		0.8	1	46.246			
			C	0.163	2.724		0.8	1	46.246			
Sum Weight:	9.13	31.22						OTM	2623.56 kip-ft	34.77		

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	Project 180-ft Sabre Lattice Tower - 250 Olcott St., Manchester, CT	Date 13:56:50 01/03/19
	Client Sprint	Designed by TJL

Tower Forces - Service - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 180.00-160.00	0.16	0.79	A	0.163	2.723	29	0.85	1	14.644	1.53	76.61	C
			B	0.163	2.723		0.85	1	14.644			
			C	0.163	2.723		0.85	1	14.644			
T2 160.00-140.00	0.21	1.17	A	0.144	2.795	28	0.85	1	16.742	1.86	92.86	C
			B	0.144	2.795		0.85	1	16.742			
			C	0.144	2.795		0.85	1	16.742			
T3 140.00-120.00	0.27	2.50	A	0.157	2.744	27	0.85	1	20.765	2.13	106.58	C
			B	0.157	2.744		0.85	1	20.765			
			C	0.157	2.744		0.85	1	20.765			
T4 120.00-100.00	0.98	2.94	A	0.167	2.709	26	0.85	1	28.337	4.27	213.38	C
			B	0.167	2.709		0.85	1	28.337			
			C	0.167	2.709		0.85	1	28.337			
T5 100.00-80.00	1.63	3.11	A	0.155	2.753	25	0.85	1	31.012	5.89	294.45	C
			B	0.155	2.753		0.85	1	31.012			
			C	0.155	2.753		0.85	1	31.012			
T6 80.00-60.00	1.63	4.34	A	0.158	2.741	24	0.85	1	32.694	5.67	283.60	C
			B	0.158	2.741		0.85	1	32.694			
			C	0.158	2.741		0.85	1	32.694			
T7 60.00-40.00	1.63	4.86	A	0.147	2.781	22	0.85	1	34.427	5.40	270.04	C
			B	0.147	2.781		0.85	1	34.427			
			C	0.147	2.781		0.85	1	34.427			
T8 40.00-20.00	1.63	5.22	A	0.139	2.813	20	0.85	1	36.332	4.96	248.01	C
			B	0.139	2.813		0.85	1	36.332			
			C	0.139	2.813		0.85	1	36.332			
T9 20.00-0.00	0.98	6.28	A	0.163	2.724	17	0.85	1	48.183	3.61	180.51	C
			B	0.163	2.724		0.85	1	48.183			
			C	0.163	2.724		0.85	1	48.183			
Sum Weight:	9.13	31.22						OTM	2667.60 kip-ft	35.32		

Force Totals

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, M _x kip-ft	Sum of Overturning Moments, M _z kip-ft	Sum of Torques kip-ft
Leg Weight	17.08					
Bracing Weight	14.14					
Total Member Self-Weight	31.22					
Total Weight	46.20			-17.85	-6.55	
Wind 0 deg - No Ice		0.00	-61.49	-5874.57	-6.55	10.49
Wind 30 deg - No Ice		30.29	-50.12	-4703.11	-2937.86	-2.64
Wind 60 deg - No Ice		50.27	-29.14	-2788.11	-4756.70	-13.75
Wind 90 deg - No Ice		58.06	-1.12	-213.02	-5434.45	-20.83
Wind 120 deg - No Ice		52.58	32.33	3170.31	-4952.53	-20.47
Wind 150 deg - No Ice		27.79	52.33	5040.91	-2506.76	-15.62
Wind 180 deg - No Ice		0.00	59.18	5670.21	-6.55	-10.02
Wind 210 deg - No Ice		-27.79	52.33	5040.91	2493.65	-1.94
Wind 240 deg - No Ice		-52.58	32.33	3170.31	4939.43	9.98

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Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, M _x kip-ft	Sum of Overturning Moments, M _z kip-ft	Sum of Torques kip-ft
Wind 270 deg - No Ice		-58.06	-1.12	-213.02	5421.34	20.83
Wind 300 deg - No Ice		-50.27	-29.14	-2788.11	4743.60	23.77
Wind 330 deg - No Ice		-30.29	-50.12	-4703.11	2924.76	20.19
Member Ice	69.42					
Total Weight Ice	235.96			-119.87	-130.41	
Wind 0 deg - Ice		0.00	-25.96	-2638.15	-130.41	7.37
Wind 30 deg - Ice		12.86	-21.80	-2212.51	-1387.49	3.27
Wind 60 deg - Ice		21.75	-12.66	-1346.53	-2228.03	-1.42
Wind 90 deg - Ice		25.07	-0.28	-169.43	-2534.20	-5.60
Wind 120 deg - Ice		22.18	13.38	1205.19	-2264.48	-7.76
Wind 150 deg - Ice		12.22	22.36	2067.57	-1278.04	-8.21
Wind 180 deg - Ice		0.00	25.54	2370.90	-130.41	-7.27
Wind 210 deg - Ice		-12.22	22.36	2067.57	1017.23	-4.43
Wind 240 deg - Ice		-22.18	13.38	1205.19	2003.67	0.40
Wind 270 deg - Ice		-25.07	-0.28	-169.43	2273.39	5.60
Wind 300 deg - Ice		-21.75	-12.66	-1346.53	1967.21	8.69
Wind 330 deg - Ice		-12.86	-21.80	-2212.51	1126.68	9.37
Total Weight	46.20			-17.85	-6.55	
Wind 0 deg - Service		0.00	-53.47	-5096.21	-2.19	9.12
Wind 30 deg - Service		26.34	-43.59	-4077.55	-2551.16	-2.29
Wind 60 deg - Service		43.72	-25.34	-2412.33	-4132.76	-11.96
Wind 90 deg - Service		50.49	-0.97	-173.13	-4722.10	-18.11
Wind 120 deg - Service		45.73	28.11	2768.90	-4303.04	-17.80
Wind 150 deg - Service		24.16	45.50	4395.51	-2176.28	-13.58
Wind 180 deg - Service		0.00	51.46	4942.73	-2.19	-8.71
Wind 210 deg - Service		-24.16	45.50	4395.51	2171.90	-1.68
Wind 240 deg - Service		-45.73	28.11	2768.90	4298.66	8.68
Wind 270 deg - Service		-50.49	-0.97	-173.13	4717.72	18.11
Wind 300 deg - Service		-43.72	-25.34	-2412.33	4128.38	20.67
Wind 330 deg - Service		-26.34	-43.59	-4077.55	2546.78	17.56

Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice

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Comb. No.	Description
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T1	180 - 160	Leg	Max Tension	15	21.00	-0.45	0.01
			Max. Compression	2	-23.72	0.31	-0.03
			Max. Mx	10	11.51	0.59	-0.02
			Max. My	16	-4.83	0.13	-0.65
			Max. Vy	3	2.44	0.06	-0.01
		Diagonal	Max. Vx	2	-2.05	-0.03	0.14
			Max Tension	10	4.37	0.00	0.00
			Max. Compression	10	-4.36	0.00	0.00
			Max. Mx	29	0.56	0.04	0.01
			Max. My	10	-3.79	-0.00	0.01
		Top Girt	Max. Vy	29	0.05	0.04	0.01
			Max. Vx	10	-0.00	0.00	0.00
			Max Tension	15	0.65	0.00	0.00
			Max. Compression	18	-0.70	0.00	0.00
			Max. Mx	29	-0.01	-0.07	0.00
T2	160 - 140	Leg	Max. My	27	-0.02	0.00	0.00
			Max. Vy	29	0.06	0.00	0.00
			Max. Vx	27	0.00	0.00	0.00
			Max Tension	15	57.24	-0.07	0.01
			Max. Compression	2	-60.71	0.39	-0.06
			Max. Mx	14	30.52	-0.39	0.03
			Max. My	23	-15.40	0.14	-0.57
			Max. Vy	14	-0.24	-0.39	0.03
			Max. Vx	8	0.51	0.00	0.54

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft			
T3	140 - 120	Diagonal	Max Tension	24	5.47	0.00	0.00			
			Max. Compression	10	-5.54	0.00	0.00			
			Max. Mx	29	0.94	0.07	-0.01			
			Max. My	27	-0.04	0.06	-0.01			
			Max. Vy	29	0.07	0.07	-0.01			
			Max. Vx	27	0.00	0.00	0.00			
		Leg	Max Tension	15	91.57	-0.84	0.02			
			Max. Compression	2	-98.61	1.61	-0.05			
			Max. Mx	11	-97.47	1.65	0.12			
			Max. My	8	-13.39	0.02	1.66			
			Max. Vy	22	-1.32	-0.83	-0.02			
			Max. Vx	8	1.37	0.01	0.82			
			Diagonal	Max Tension	24	8.61	0.00	0.00		
				Max. Compression	24	-8.66	0.00	0.00		
Max. Mx	29	1.66		0.12	0.02					
Max. My	27	0.09		0.11	-0.02					
Max. Vy	29	0.09		0.12	0.02					
Max. Vx	27	-0.01		0.00	0.00					
T4	120 - 100	Leg	Max Tension	15	141.69	-1.10	0.02			
			Max. Compression	2	-154.67	0.97	-0.01			
			Max. Mx	11	-113.34	1.65	0.12			
			Max. My	8	-14.25	0.02	1.66			
			Max. Vy	22	-1.40	-1.08	-0.06			
			Max. Vx	8	1.48	0.02	1.04			
		Diagonal	Max Tension	24	13.47	0.00	0.00			
			Max. Compression	24	-13.55	0.00	0.00			
			Max. Mx	31	2.63	0.20	0.02			
			Max. My	27	0.21	0.17	-0.03			
			Max. Vy	29	0.13	0.19	0.02			
			Max. Vx	27	-0.01	0.00	0.00			
			T5	100 - 80	Leg	Max Tension	15	202.10	-0.40	-0.01
						Max. Compression	2	-220.47	1.53	-0.06
Max. Mx	10	-220.34				1.54	0.19			
Max. My	8	-21.22				0.06	1.47			
Max. Vy	19	-0.26				1.54	-0.13			
Max. Vx	8	-0.28				0.06	1.47			
Diagonal	Max Tension	24			15.12	0.00	0.00			
	Max. Compression	24			-15.32	0.00	0.00			
	Max. Mx	31			3.33	0.24	0.03			
	Max. My	27			0.36	0.22	-0.03			
	Max. Vy	29			0.15	0.24	0.03			
	Max. Vx	27			-0.01	0.00	0.00			
	T6	80 - 60			Leg	Max Tension	15	257.02	-1.56	-0.01
						Max. Compression	10	-281.08	2.33	0.18
Max. Mx			10	-281.08		2.33	0.18			
Max. My			12	-33.99		0.08	-1.82			
Max. Vy			19	-0.24		2.32	-0.15			
Max. Vx			8	-0.21		0.01	1.74			
Diagonal			Max Tension	24	18.09	0.00	0.00			
			Max. Compression	24	-18.32	0.00	0.00			
			Max. Mx	29	3.60	0.38	0.05			
			Max. My	27	0.41	0.33	-0.05			
			Max. Vy	29	0.19	0.38	0.05			
			Max. Vx	27	-0.01	0.00	0.00			
			T7	60 - 40	Leg	Max Tension	15	316.28	-1.67	-0.00
						Max. Compression	10	-347.29	2.39	0.14
Max. Mx	10	-347.29				2.39	0.14			
Max. My	12	-37.99				0.04	-1.95			
Max. Vy	33	0.30				-2.01	0.04			
Max. Vx	8	0.21				-0.02	1.91			
Diagonal	Max Tension	24			19.40	0.00	0.00			

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T8	40 - 20	Leg	Max. Compression	24	-19.69	0.00	0.00
			Max. Mx	29	4.10	0.46	0.06
			Max. My	27	0.08	0.44	-0.06
			Max. Vy	29	0.21	0.46	-0.06
			Max. Vx	27	-0.01	0.00	0.00
			Max Tension	15	374.13	-1.63	0.00
			Max. Compression	10	-412.48	3.03	0.09
		Diagonal	Max. Mx	29	41.09	-5.40	0.01
			Max. My	12	-41.85	-0.03	-2.52
			Max. Vy	33	0.81	-5.38	0.03
			Max. Vx	8	0.29	-0.08	2.46
			Max Tension	24	20.50	0.00	0.00
			Max. Compression	24	-20.87	0.00	0.00
			Max. Mx	29	2.87	0.54	0.07
T9	20 - 0	Leg	Max. Mx	37	-5.15	0.47	-0.07
			Max. Vy	29	0.24	0.52	-0.06
			Max. Vx	37	-0.01	0.00	0.00
			Max Tension	15	429.25	-3.31	0.00
			Max. Compression	10	-475.37	-0.00	-0.00
			Max. Mx	27	-196.37	8.50	0.10
			Max. My	12	-45.58	-0.03	-6.18
		Diagonal	Max. Vy	33	-1.27	-5.38	0.03
			Max. Vx	8	0.75	-0.12	5.97
			Max Tension	12	21.48	0.00	0.00
			Max. Compression	24	-21.83	0.00	0.00
			Max. Mx	29	0.88	0.77	0.08
			Max. My	37	-8.11	0.70	-0.09
			Max. Vy	29	0.27	0.77	0.08
Max. Vx	37	0.01	0.00	0.00			

Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg C	Max. Vert	18	490.63	51.29	-30.10
	Max. H _x	18	490.63	51.29	-30.10
	Max. H _z	7	-429.15	-46.31	27.36
	Min. Vert	7	-429.15	-46.31	27.36
	Min. H _x	7	-429.15	-46.31	27.36
	Min. H _z	18	490.63	51.29	-30.10
Leg B	Max. Vert	10	491.32	-51.09	-30.47
	Max. H _x	23	-428.63	46.09	27.71
	Max. H _z	23	-428.63	46.09	27.71
	Min. Vert	23	-428.63	46.09	27.71
	Min. H _x	10	491.32	-51.09	-30.47
	Min. H _z	10	491.32	-51.09	-30.47
Leg A	Max. Vert	2	490.93	0.42	59.30
	Max. H _x	21	30.38	8.20	2.34
	Max. H _z	2	490.93	0.42	59.30
	Min. Vert	15	-442.90	-0.41	-54.91
	Min. H _x	9	30.38	-8.19	2.34
	Min. H _z	15	-442.90	-0.41	-54.91

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Tower Mast Reaction Summary

Load Combination	Vertical	Shear _x	Shear _z	Overturning Moment, M _x	Overturning Moment, M _z	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	46.20	0.00	0.00	-17.85	-6.55	0.00
1.2 Dead+1.6 Wind 0 deg - No Ice	55.44	-0.00	-98.39	-9410.46	-7.96	16.86
0.9 Dead+1.6 Wind 0 deg - No Ice	41.58	0.00	-98.39	-9400.47	-5.98	16.84
1.2 Dead+1.6 Wind 30 deg - No Ice	55.44	48.46	-80.20	-7532.29	-4707.21	-4.20
0.9 Dead+1.6 Wind 30 deg - No Ice	41.58	48.46	-80.20	-7523.27	-4702.90	-4.20
1.2 Dead+1.6 Wind 60 deg - No Ice	55.44	80.44	-46.62	-4462.53	-7622.82	-22.05
0.9 Dead+1.6 Wind 60 deg - No Ice	41.58	80.44	-46.62	-4454.98	-7617.12	-22.03
1.2 Dead+1.6 Wind 90 deg - No Ice	55.44	92.89	-1.79	-334.61	-8709.23	-33.43
0.9 Dead+1.6 Wind 90 deg - No Ice	41.58	92.89	-1.79	-329.03	-8703.01	-33.40
1.2 Dead+1.6 Wind 120 deg - No Ice	55.44	84.13	51.73	5089.64	-7936.79	-32.89
0.9 Dead+1.6 Wind 120 deg - No Ice	41.58	84.13	51.73	5092.46	-7930.96	-32.87
1.2 Dead+1.6 Wind 150 deg - No Ice	55.44	44.46	83.72	8088.42	-4015.79	-25.11
0.9 Dead+1.6 Wind 150 deg - No Ice	41.58	44.46	83.72	8089.77	-4011.92	-25.08
1.2 Dead+1.6 Wind 180 deg - No Ice	55.44	-0.00	94.68	9097.25	-7.97	-16.11
0.9 Dead+1.6 Wind 180 deg - No Ice	41.58	-0.00	94.68	9098.12	-5.99	-16.09
1.2 Dead+1.6 Wind 210 deg - No Ice	55.44	-44.46	83.72	8088.47	3999.89	-3.12
0.9 Dead+1.6 Wind 210 deg - No Ice	41.58	-44.46	83.72	8089.82	3999.98	-3.11
1.2 Dead+1.6 Wind 240 deg - No Ice	55.44	-84.13	51.73	5089.70	7920.98	16.04
0.9 Dead+1.6 Wind 240 deg - No Ice	41.58	-84.13	51.73	5092.51	7919.09	16.02
1.2 Dead+1.6 Wind 270 deg - No Ice	55.44	-92.89	-1.79	-334.63	8693.46	33.44
0.9 Dead+1.6 Wind 270 deg - No Ice	41.58	-92.89	-1.79	-329.05	8691.19	33.41
1.2 Dead+1.6 Wind 300 deg - No Ice	55.44	-80.44	-46.62	-4462.61	7607.02	38.15
0.9 Dead+1.6 Wind 300 deg - No Ice	41.58	-80.44	-46.62	-4455.06	7605.27	38.12
1.2 Dead+1.6 Wind 330 deg - No Ice	55.44	-48.46	-80.20	-7532.37	4691.35	32.41
0.9 Dead+1.6 Wind 330 deg - No Ice	41.58	-48.46	-80.20	-7523.35	4690.99	32.38
1.2 Dead+1.0 Ice+1.0 Temp	245.20	-0.00	0.00	-124.60	-133.67	-0.00
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	245.20	-0.00	-25.96	-2669.53	-133.70	7.65
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	245.20	12.86	-21.80	-2239.18	-1404.12	3.41
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	245.20	21.75	-12.66	-1364.24	-2253.36	-1.42
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	245.20	25.07	-0.28	-174.90	-2562.63	-5.75

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Load Combination	Vertical K	Shear _x K	Shear _z K	Overturning Moment, M _x kip-ft	Overturning Moment, M _z kip-ft	Torque kip-ft
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	245.20	22.18	13.38	1214.61	-2290.18	-8.06
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	245.20	12.22	22.36	2086.02	-1293.16	-8.54
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	245.20	-0.00	25.54	2392.50	-133.74	-7.56
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	245.20	-12.22	22.36	2086.01	1025.70	-4.60
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	245.20	-22.18	13.38	1214.59	2022.74	0.38
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	245.20	-25.07	-0.28	-174.95	2295.21	5.77
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	245.20	-21.75	-12.66	-1364.29	1985.94	8.96
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp	245.20	-12.86	-21.80	-2239.22	1136.72	9.69
Dead+Wind 0 deg - Service	46.20	0.00	-53.47	-5119.00	-6.59	9.15
Dead+Wind 30 deg - Service	46.20	26.34	-43.59	-4098.58	-2559.73	-2.32
Dead+Wind 60 deg - Service	46.20	43.72	-25.34	-2430.73	-4143.82	-11.98
Dead+Wind 90 deg - Service	46.20	50.49	-0.97	-187.97	-4734.09	-18.13
Dead+Wind 120 deg - Service	46.20	45.73	28.11	2759.04	-4314.42	-17.87
Dead+Wind 150 deg - Service	46.20	24.16	45.50	4388.27	-2184.10	-13.66
Dead+Wind 180 deg - Service	46.20	0.00	51.46	4936.38	-6.59	-8.75
Dead+Wind 210 deg - Service	46.20	-24.16	45.50	4388.29	2170.92	-1.67
Dead+Wind 240 deg - Service	46.20	-45.73	28.11	2759.05	4301.26	8.71
Dead+Wind 270 deg - Service	46.20	-50.49	-0.97	-187.98	4720.95	18.13
Dead+Wind 300 deg - Service	46.20	-43.72	-25.34	-2430.76	4130.68	20.72
Dead+Wind 330 deg - Service	46.20	-26.34	-43.59	-4098.61	2546.58	17.63

Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-46.20	0.00	0.00	46.20	0.00	0.000%
2	0.00	-55.44	-98.39	0.00	55.44	98.39	0.000%
3	0.00	-41.58	-98.39	-0.00	41.58	98.39	0.000%
4	48.46	-55.44	-80.20	-48.46	55.44	80.20	0.000%
5	48.46	-41.58	-80.20	-48.46	41.58	80.20	0.000%
6	80.44	-55.44	-46.62	-80.44	55.44	46.62	0.000%
7	80.44	-41.58	-46.62	-80.44	41.58	46.62	0.000%
8	92.89	-55.44	-1.79	-92.89	55.44	1.79	0.000%
9	92.89	-41.58	-1.79	-92.89	41.58	1.79	0.000%
10	84.13	-55.44	51.73	-84.13	55.44	-51.73	0.000%
11	84.13	-41.58	51.73	-84.13	41.58	-51.73	0.000%
12	44.46	-55.44	83.72	-44.46	55.44	-83.72	0.000%
13	44.46	-41.58	83.72	-44.46	41.58	-83.72	0.000%
14	0.00	-55.44	94.68	0.00	55.44	-94.68	0.000%
15	0.00	-41.58	94.68	0.00	41.58	-94.68	0.000%
16	-44.46	-55.44	83.72	44.46	55.44	-83.72	0.000%
17	-44.46	-41.58	83.72	44.46	41.58	-83.72	0.000%
18	-84.13	-55.44	51.73	84.13	55.44	-51.73	0.000%
19	-84.13	-41.58	51.73	84.13	41.58	-51.73	0.000%
20	-92.89	-55.44	-1.79	92.89	55.44	1.79	0.000%
21	-92.89	-41.58	-1.79	92.89	41.58	1.79	0.000%
22	-80.44	-55.44	-46.62	80.44	55.44	46.62	0.000%
23	-80.44	-41.58	-46.62	80.44	41.58	46.62	0.000%
24	-48.46	-55.44	-80.20	48.46	55.44	80.20	0.000%

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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
25	-48.46	-41.58	-80.20	48.46	41.58	80.20	0.000%
26	0.00	-245.20	0.00	0.00	245.20	-0.00	0.000%
27	0.00	-245.20	-25.96	0.00	245.20	25.96	0.000%
28	12.86	-245.20	-21.80	-12.86	245.20	21.80	0.000%
29	21.75	-245.20	-12.66	-21.75	245.20	12.66	0.000%
30	25.07	-245.20	-0.28	-25.07	245.20	0.28	0.000%
31	22.18	-245.20	13.38	-22.18	245.20	-13.38	0.000%
32	12.22	-245.20	22.36	-12.22	245.20	-22.36	0.000%
33	0.00	-245.20	25.54	0.00	245.20	-25.54	0.000%
34	-12.22	-245.20	22.36	12.22	245.20	-22.36	0.000%
35	-22.18	-245.20	13.38	22.18	245.20	-13.38	0.000%
36	-25.07	-245.20	-0.28	25.07	245.20	0.28	0.000%
37	-21.75	-245.20	-12.66	21.75	245.20	12.66	0.000%
38	-12.86	-245.20	-21.80	12.86	245.20	21.80	0.000%
39	0.00	-46.20	-53.47	-0.00	46.20	53.47	0.000%
40	26.34	-46.20	-43.59	-26.34	46.20	43.59	0.000%
41	43.72	-46.20	-25.34	-43.72	46.20	25.34	0.000%
42	50.49	-46.20	-0.97	-50.49	46.20	0.97	0.000%
43	45.73	-46.20	28.11	-45.73	46.20	-28.11	0.000%
44	24.16	-46.20	45.50	-24.16	46.20	-45.50	0.000%
45	0.00	-46.20	51.46	0.00	46.20	-51.46	0.000%
46	-24.16	-46.20	45.50	24.16	46.20	-45.50	0.000%
47	-45.73	-46.20	28.11	45.73	46.20	-28.11	0.000%
48	-50.49	-46.20	-0.97	50.49	46.20	0.97	0.000%
49	-43.72	-46.20	-25.34	43.72	46.20	25.34	0.000%
50	-26.34	-46.20	-43.59	26.34	46.20	43.59	0.000%

Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00000001
3	Yes	4	0.00000001	0.00000001
4	Yes	4	0.00000001	0.00000001
5	Yes	4	0.00000001	0.00000001
6	Yes	4	0.00000001	0.00000001
7	Yes	4	0.00000001	0.00000001
8	Yes	4	0.00000001	0.00000001
9	Yes	4	0.00000001	0.00000001
10	Yes	4	0.00000001	0.00000054
11	Yes	4	0.00000001	0.00000001
12	Yes	4	0.00000001	0.00000001
13	Yes	4	0.00000001	0.00000001
14	Yes	4	0.00000001	0.00000001
15	Yes	4	0.00000001	0.00000001
16	Yes	4	0.00000001	0.00000001
17	Yes	4	0.00000001	0.00000001
18	Yes	4	0.00000001	0.00000001
19	Yes	4	0.00000001	0.00000001
20	Yes	4	0.00000001	0.00000001
21	Yes	4	0.00000001	0.00000001
22	Yes	4	0.00000001	0.00000001
23	Yes	4	0.00000001	0.00000001
24	Yes	4	0.00000001	0.00000001
25	Yes	4	0.00000001	0.00000001

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26	Yes	4	0.00000001	0.00000001
27	Yes	4	0.00000001	0.00000240
28	Yes	4	0.00000001	0.00000244
29	Yes	4	0.00000001	0.00000247
30	Yes	4	0.00000001	0.00000241
31	Yes	4	0.00000001	0.00000240
32	Yes	4	0.00000001	0.00000238
33	Yes	4	0.00000001	0.00000238
34	Yes	4	0.00000001	0.00000227
35	Yes	4	0.00000001	0.00000231
36	Yes	4	0.00000001	0.00000218
37	Yes	4	0.00000001	0.00000230
38	Yes	4	0.00000001	0.00000234
39	Yes	4	0.00000001	0.00000001
40	Yes	4	0.00000001	0.00000001
41	Yes	4	0.00000001	0.00000001
42	Yes	4	0.00000001	0.00000001
43	Yes	4	0.00000001	0.00000001
44	Yes	4	0.00000001	0.00000001
45	Yes	4	0.00000001	0.00000001
46	Yes	4	0.00000001	0.00000001
47	Yes	4	0.00000001	0.00000001
48	Yes	4	0.00000001	0.00000001
49	Yes	4	0.00000001	0.00000001
50	Yes	4	0.00000001	0.00000001

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 160	9.095	43	0.4303	0.0957
T2	160 - 140	7.265	43	0.4049	0.0835
T3	140 - 120	5.630	43	0.3378	0.0503
T4	120 - 100	4.233	43	0.3017	0.0367
T5	100 - 80	2.989	43	0.2539	0.0265
T6	80 - 60	1.941	43	0.1932	0.0165
T7	60 - 40	1.146	43	0.1488	0.0110
T8	40 - 20	0.552	43	0.0989	0.0068
T9	20 - 0	0.173	43	0.0448	0.0032

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
189.40	DS9A09F36D-N	43	9.095	0.4303	0.0957	84831
189.00	24' x 6" Omni	43	9.095	0.4303	0.0957	84831
187.00	CO-41A	43	9.095	0.4303	0.0957	84831
180.00	Tower Top Amplifier	43	9.095	0.4303	0.0957	84831
175.00	8' Dish	43	8.629	0.4271	0.0943	84831
164.00	8' Dish	43	7.620	0.4139	0.0880	26519
158.00	531-70HD	43	7.091	0.3992	0.0807	20968
156.00	24' x 6" Omni	43	6.919	0.3929	0.0776	20447
153.00	ROHN 6-ft Side Arm	43	6.665	0.3826	0.0724	19903
144.40	ROHN 3-ft Side Arm	43	5.968	0.3515	0.0570	18351

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Elevation	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
135.00	NNVV-65B-R4	43	5.261	0.3259	0.0449	20641
125.00	(4) 8' x1' Panel	43	4.565	0.3095	0.0388	31370
115.00	(4) 8' x1' Panel	43	3.908	0.2923	0.0344	35797
105.00	(4) 8' x1' Panel	43	3.284	0.2682	0.0293	27355

Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 160	16.733	10	0.7911	0.1763
T2	160 - 140	13.369	10	0.7445	0.1538
T3	140 - 120	10.361	10	0.6213	0.0927
T4	120 - 100	7.790	10	0.5552	0.0676
T5	100 - 80	5.501	10	0.4673	0.0489
T6	80 - 60	3.574	10	0.3557	0.0304
T7	60 - 40	2.109	10	0.2739	0.0203
T8	40 - 20	1.016	10	0.1820	0.0125
T9	20 - 0	0.318	10	0.0826	0.0059

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
189.40	DS9A09F36D-N	10	16.733	0.7911	0.1763	46266
189.00	24' x 6" Omni	10	16.733	0.7911	0.1763	46266
187.00	CO-41A	10	16.733	0.7911	0.1763	46266
180.00	Tower Top Amplifier	10	16.733	0.7911	0.1763	46266
175.00	8' Dish	10	15.876	0.7853	0.1737	46266
164.00	8' Dish	10	14.022	0.7610	0.1620	14463
158.00	531-70HD	10	13.048	0.7341	0.1486	11431
156.00	24' x 6" Omni	10	12.732	0.7226	0.1429	11143
153.00	ROHN 6-ft Side Arm	10	12.265	0.7037	0.1334	10841
144.40	ROHN 3-ft Side Arm	10	10.983	0.6466	0.1050	10006
135.00	NNVV-65B-R4	10	9.683	0.5995	0.0826	11253
125.00	(4) 8' x1' Panel	10	8.402	0.5695	0.0714	17094
115.00	(4) 8' x1' Panel	10	7.192	0.5378	0.0634	19480
105.00	(4) 8' x1' Panel	10	6.045	0.4936	0.0540	14896

Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
T1	180	Diagonal	A325X	0.6250	1	4.37	9.75	0.449 ✓	1	Member Bearing

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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
		Top Girt	A325X	0.6250	1	0.65	5.22	0.124 ✓	1	Member Bearing
T2	160	Diagonal	A325X	0.6250	1	5.54	14.63	0.379 ✓	1	Member Bearing
T3	140	Diagonal	A325X	0.6250	1	8.66	15.19	0.570 ✓	1	Bolt Shear
T4	120	Diagonal	A325X	0.7500	1	13.47	19.99	0.674 ✓	1	Member Bearing
T5	100	Diagonal	A325X	0.7500	1	15.12	19.99	0.757 ✓	1	Member Bearing
T6	80	Diagonal	A325X	0.7500	1	18.32	21.87	0.838 ✓	1	Bolt Shear
T7	60	Diagonal	A325X	0.7500	1	19.69	21.87	0.900 ✓	1	Bolt Shear
T8	40	Diagonal	A325X	0.7500	1	20.87	21.87	0.954 ✓	1	Bolt Shear
T9	20	Leg	F1554-10 5	1.5000	6	71.54	124.25	0.576 ✓	1	Bolt Tension
		Diagonal	A325X	0.7500	1	21.83	21.87	0.998 ✓	1	Bolt Shear

Compression Checks

Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio P _u / φP _n
T1	180 - 160	P2.5x.276	20.03	5.01	65.0 K=1.00	2.2535	-23.72	74.43	0.319 ¹ ✓
T2	160 - 140	P3x.3	20.03	5.01	52.9 K=1.00	3.0159	-60.71	110.61	0.549 ¹ ✓
T3	140 - 120	P5x0.5	20.03	6.68	44.5 K=1.00	7.9529	-98.61	309.54	0.319 ¹ ✓
T4	120 - 100	P5x0.5	20.03	6.68	44.5 K=1.00	7.9529	-154.67	309.54	0.500 ¹ ✓
T5	100 - 80	P5x0.5	20.03	6.68	44.5 K=1.00	7.9529	-220.47	309.54	0.712 ¹ ✓
T6	80 - 60	P8x.5	20.03	10.02	41.8 K=1.00	12.7627	-281.08	505.56	0.556 ¹ ✓
T7	60 - 40	P8x.5	20.03	10.02	41.8 K=1.00	12.7627	-347.29	505.56	0.687 ¹ ✓
T8	40 - 20	P8x.5	20.03	10.02	41.8 K=1.00	12.7627	-412.48	505.56	0.816 ¹ ✓
T9	20 - 0	P10x.5	20.03	10.02	33.1 K=1.00	16.1007	-475.37	668.66	0.711 ¹ ✓

¹ P_u / φP_n controls

Diagonal Design Data (Compression)

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160	L2x2x1/8	8.40	4.04	122.0 K=1.00	0.4844	-4.36	7.34	0.594 ¹ ✓
T2	160 - 140	L2x2x3/16	10.08	4.85	147.7 K=1.00	0.7150	-5.42	7.41	0.732 ¹ ✓
T3	140 - 120	L2 1/2x2 1/2x1/4	12.58	6.05	147.8 K=1.00	1.1900	-8.66	12.31	0.704 ¹ ✓
T4	120 - 100	L3 1/2x3x1/4	14.32	6.92	131.6 K=1.00	1.5600	-13.55	20.36	0.666 ¹ ✓
T5	100 - 80	L3 1/2x3x1/4	16.11	7.82	148.7 K=1.00	1.5600	-15.32	15.94	0.961 ¹ ✓
T6	80 - 60	L4x3 1/2x5/16	19.30	9.35	153.8 K=1.00	2.2500	-18.32	21.50	0.852 ¹ ✓
T7	60 - 40	L4x3 1/2x3/8	21.03	10.22	168.8 K=1.00	2.6700	-19.69	21.18	0.930 ¹ ✓
T8	40 - 20	L4x4x3/8	22.81	11.12	169.3 K=1.00	2.8600	-20.87	22.54	0.926 ¹ ✓
T9	20 - 0	L5x5x5/16	24.62	11.93	144.0 K=1.00	3.0300	-21.83	33.01	0.661 ¹ ✓

¹ P_u / φP_n controls

Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160	L2x2x1/8	5.00	4.52	136.5 K=1.00	0.4844	-0.70	5.88	0.120 ¹ ✓

¹ P_u / φP_n controls

Tension Checks

Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160	P2.5x.276	20.03	5.01	65.0	2.2535	21.00	101.41	0.207 ¹ ✓
T2	160 - 140	P3x.3	20.03	5.01	52.9	3.0159	57.24	135.72	0.422 ¹ ✓
T3	140 - 120	P5x0.5	20.03	6.68	44.5	7.9529	91.57	357.88	0.256 ¹ ✓

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	Client Sprint	Designed by TJL

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T4	120 - 100	P5x0.5	20.03	6.68	44.5	7.9529	141.69	357.88	0.396 ¹
T5	100 - 80	P5x0.5	20.03	6.68	44.5	7.9529	202.10	357.88	0.565 ¹
T6	80 - 60	P8x.5	20.03	10.02	41.8	12.7627	257.02	574.32	0.448 ¹
T7	60 - 40	P8x.5	20.03	10.02	41.8	12.7627	316.28	574.32	0.551 ¹
T8	40 - 20	P8x.5	20.03	10.02	41.8	12.7627	374.13	574.32	0.651 ¹
T9	20 - 0	P10x.5	20.03	10.02	33.1	16.1007	429.25	724.53	0.592 ¹

¹ P_u / φP_n controls

Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160	L2x2x1/8	8.40	4.04	80.6	0.2930	4.37	14.28	0.306 ¹
T2	160 - 140	L2x2x3/16	9.22	4.43	89.3	0.4308	5.47	21.00	0.261 ¹
T3	140 - 120	L2 1/2x2 1/2x1/4	12.58	6.05	97.0	0.7519	8.61	36.65	0.235 ¹
T4	120 - 100	L3 1/2x3x1/4	14.32	6.92	93.1	1.0059	13.47	49.04	0.275 ¹
T5	100 - 80	L3 1/2x3x1/4	16.11	7.82	105.0	1.0059	15.12	49.04	0.308 ¹
T6	80 - 60	L4x3 1/2x5/16	19.30	9.35	107.3	1.4824	18.09	72.27	0.250 ¹
T7	60 - 40	L4x3 1/2x3/8	21.03	10.22	118.6	1.7564	19.40	85.62	0.227 ¹
T8	40 - 20	L4x4x3/8	22.81	11.12	110.1	1.8989	20.50	92.57	0.221 ¹
T9	20 - 0	L5x5x5/16	24.62	11.93	92.4	2.0674	21.48	100.79	0.213 ¹

¹ P_u / φP_n controls

Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160	L2x2x1/8	5.00	4.52	91.2	0.2930	0.65	12.74	0.051 ¹

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	Client Sprint	Designed by TJJ

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
									✓

¹ P_u / φP_n controls

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	φP _{allow} K	% Capacity	Pass Fail
T1	180 - 160	Leg	P2.5x.276	3	-23.72	74.43	31.9	Pass
T2	160 - 140	Leg	P3x.3	33	-60.71	110.61	54.9	Pass
T3	140 - 120	Leg	P5x0.5	60	-98.61	309.54	31.9	Pass
T4	120 - 100	Leg	P5x0.5	81	-154.67	309.54	50.0	Pass
T5	100 - 80	Leg	P5x0.5	102	-220.47	309.54	71.2	Pass
T6	80 - 60	Leg	P8x.5	122	-281.08	505.56	55.6	Pass
T7	60 - 40	Leg	P8x.5	137	-347.29	505.56	68.7	Pass
T8	40 - 20	Leg	P8x.5	152	-412.48	505.56	81.6	Pass
T9	20 - 0	Leg	P10x.5	167	-475.37	668.66	71.1	Pass
T1	180 - 160	Diagonal	L2x2x1/8	9	-4.36	7.34	59.4	Pass
T2	160 - 140	Diagonal	L2x2x3/16	37	-5.42	7.41	73.2	Pass
T3	140 - 120	Diagonal	L2 1/2x2 1/2x1/4	64	-8.66	12.31	70.4	Pass
T4	120 - 100	Diagonal	L3 1/2x3x1/4	85	-13.55	20.36	66.6	Pass
							67.4 (b)	
T5	100 - 80	Diagonal	L3 1/2x3x1/4	106	-15.32	15.94	96.1	Pass
T6	80 - 60	Diagonal	L4x3 1/2x5/16	127	-18.32	21.50	85.2	Pass
T7	60 - 40	Diagonal	L4x3 1/2x3/8	142	-19.69	21.18	93.0	Pass
T8	40 - 20	Diagonal	L4x4x3/8	157	-20.87	22.54	92.6	Pass
							95.4 (b)	
T9	20 - 0	Diagonal	L5x5x5/16	172	-21.83	33.01	66.1	Pass
							99.8 (b)	
T1	180 - 160	Top Girt	L2x2x1/8	5	-0.70	5.88	12.0	Pass
							12.4 (b)	
							Summary	
						Leg (T8)	81.6	Pass
						Diagonal (T9)	99.8	Pass
						Top Girt (T1)	12.4	Pass
						Bolt Checks	99.8	Pass
						RATING =	99.8	Pass

Pier and Mat Foundation Analysis:

Input Data:

Tower Data

Overturing Moment =	OM := 9429-ft-kips	(User Input from tnxTower)
Shear Force =	$S_t := 99$ -kip	(User Input from tnxTower)
Axial Force =	$WT_t := 55$ -kip	(User Input from tnxTower)
Max Compression Force =	$C_t := 491$ -kip	(User Input from tnxTower)
Max Uplift Force =	$U_t := 443$ -kip	(User Input from tnxTower)
Tower Height =	$H_t := 180$ -ft	(User Input)
Tower Width =	$W_t := 23$ -ft	(User Input)
Tower Position on Foundation (1=offset, 2=centered) =	Pos _t := 1	(User Input)

Footing Data:

Overall Depth of Footing =	$D_f := 6.0$ -ft	(User Input)
Length of Pier =	$L_p := 4.75$ -ft	(User Input)
Extension of Pier Above Grade =	$L_{pag} := 0.5$ -ft	(User Input)
Diameter of Pier =	$d_p := 4.0$ -ft	(User Input)
Thickness of Footing =	$T_f := 1.75$ -ft	(User Input)
Width of Footing =	$W_f := 34.0$ -ft	(User Input)

Material Properties:

Concrete Compressive Strength =	$f_c := 4500$ -psi	(User Input)
Steel Reinforcement Yield Strength =	$f_y := 60000$ -psi	(User Input)
Internal Friction Angle of Soil =	$\Phi_s := 30$ -deg	(User Input)
Allowable Soil Bearing Capacity =	$q_s := 8000$ -psf	(User Input)
Unit Weight of Soil =	$\gamma_{soil} := 125$ -pcf	(User Input)
Unit Weight of Concrete =	$\gamma_{conc} := 150$ -pcf	(User Input)
Foundation Bouyancy =	Bouyancy := 0	(User Input) (Yes=1 / No=0)
Depth to Neglect =	n := 0-ft	(User Input)
Cohesion of Clay Type Soil =	c := 0-ksf	(User Input) (Use 0 for Sandy Soil)
Seismic Zone Factor =	Z := 2	(User Input) (UBC-1997 Fig 23-2)
Coefficient of Friction Between Concrete =	$\mu := 0.45$	(User Input)

Pier Reinforcement:

Bar Size =	$BS_{\text{pier}} := 8$	(User Input)	
Bar Diameter =	$d_{\text{bpier}} := 1.0\text{-in}$	(User Input)	
Number of Bars =	$NB_{\text{pier}} := 20$	(User Input)	
Clear Cover of Reinforcement =	$Cvr_{\text{pier}} := 3\text{-in}$	(User Input)	
Reinforcement Location Factor =	$\alpha_{\text{pier}} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Coating Factor =	$\beta_{\text{pier}} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Concrete Strength Factor =	$\lambda_{\text{pier}} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Reinforcement Size Factor =	$\gamma_{\text{pier}} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Diameter of Tie =	$d_{\text{Tie}} := 4\text{-in}$	(User Input)	

Pad Reinforcement:

Bar Size =	$BS_{\text{top}} := 10$	(User Input)	(Top of Pad)
Bar Diameter =	$d_{\text{btop}} := 1.27\text{-in}$	(User Input)	(Top of Pad)
Number of Bars =	$NB_{\text{top}} := 67$	(User Input)	(Top of Pad)
Bar Size =	$BS_{\text{bot}} := 10$	(User Input)	(Bottom of Pad)
Bar Diameter =	$d_{\text{bbot}} := 1.27\text{-in}$	(User Input)	(Bottom of Pad)
Number of Bars =	$NB_{\text{bot}} := 67$	(User Input)	(Bottom of Pad)
Clear Cover of Reinforcement =	$Cvr_{\text{pad}} := 3.0\text{-in}$	(User Input)	
Reinforcement Location Factor =	$\alpha_{\text{pad}} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Coating Factor =	$\beta_{\text{pad}} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Concrete Strength Factor =	$\lambda_{\text{pad}} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Reinforcement Size Factor =	$\gamma_{\text{pad}} := 1.0$	(User Input)	(ACI-2008 12.2.4)

Calculated Factors:

Pier Reinforcement Bar Area =	$A_{\text{bpier}} := \frac{\pi \cdot d_{\text{bpier}}^2}{4} = 0.785 \cdot \text{in}^2$
Pad Top Reinforcement Bar Area =	$A_{\text{btop}} := \frac{\pi \cdot d_{\text{btop}}^2}{4} = 1.267 \cdot \text{in}^2$
Pad Bottom Reinforcement Bar Area =	$A_{\text{bbot}} := \frac{\pi \cdot d_{\text{bbot}}^2}{4} = 1.267 \cdot \text{in}^2$
Coefficient of Lateral Soil Pressure =	$K_p := \frac{1 + \sin(\Phi_s)}{1 - \sin(\Phi_s)} = 3$
Load Factor =	$LF := 1$

Stability of Footing:

Adjusted Concrete Unit Weight =

$$\gamma_c := \text{if}(\text{Bouyancy} = 1, \gamma_{\text{conc}} - 62.4\text{pcf}, \gamma_{\text{conc}}) = 150\text{-pcf}$$

Adjusted Soil Unit Weight =

$$\gamma_s := \text{if}(\text{Bouyancy} = 1, \gamma_{\text{soil}} - 62.4\text{pcf}, \gamma_{\text{soil}}) = 125\text{-pcf}$$

Passive Pressure =

$$P_{pn} := K_p \cdot \gamma_s \cdot n + c \cdot 2 \cdot \sqrt{K_p} = 0\text{-ksf}$$

$$P_{pt} := K_p \cdot \gamma_s \cdot (D_f - T_f) + c \cdot 2 \cdot \sqrt{K_p} = 1.594\text{-ksf}$$

$$P_{top} := \text{if}[n < (D_f - T_f), P_{pt}, P_{pn}] = 1.594\text{-ksf}$$

$$P_{bot} := K_p \cdot \gamma_s \cdot D_f + c \cdot 2 \cdot \sqrt{K_p} = 2.25\text{-ksf}$$

$$P_{ave} := \frac{P_{top} + P_{bot}}{2} = 1.922\text{-ksf}$$

$$T_p := \text{if}[n < (D_f - T_f), T_f, (D_f - n)] = 1.75\text{-ft}$$

$$A_p := W_f \cdot T_p = 59.5\text{-ft}^2$$

Ultimate Shear =

$$S_u := P_{ave} \cdot A_p = 114.352\text{-kip}$$

Weight of Concrete =

$$WT_c := \left[(W_f^2 \cdot T_f) + (3) \cdot \left(\frac{d_p^2 \cdot \pi}{4} \cdot L_p \right) \right] \cdot \gamma_c = 330.311\text{-kip}$$

Weight of Soil Above Footing =

$$WT_{s1} := \left[W_f^2 - (3) \cdot \left(\frac{d_p^2 \cdot \pi}{4} \right) \right] \cdot (L_p - L_{pag} - n) \cdot \gamma_s = 594.1\text{-kip}$$

Weight of Soil Wedge at Back Face =

$$WT_{s2} := \left[\frac{(D_f - n)^2 \cdot \tan(\Phi_s)}{2} \cdot W_f \right] \cdot \gamma_s = 44.167\text{-kip}$$

Foundation has undercut toe per Fred A. Nudd dwg 96-4992-1

Tower Offset =

$$X_{t1} := \left[\frac{W_f}{2} - \frac{(W_t \cdot \cos(30\text{-deg}))}{2} \right] \quad X_{t2} := \frac{W_f}{2} - \frac{(W_t \cdot \cos(30\text{-deg}))}{3}$$

$$X_t := \text{if}(\text{Pos}_t = 1, X_{t1}, X_{t2}) = 7.041$$

$$X_{off1} := \frac{W_f}{2} - \left[\frac{(W_t \cdot \cos(30\text{-deg}))}{3} + X_t \right] = 3.32 \quad X_{off2} := 0$$

$$X_{off} := \text{if}(\text{Pos}_t = 1, X_{off1}, X_{off2}) \quad X_{off} = 3.32\text{-ft}$$

Total Weight = $WT_{tot} := 0.9WT_c + 0.75WT_{s1} = 742.9\text{-kip}$

Resisting Moment = $M_r := (WT_{tot}) \cdot \frac{W_f}{2} + 0.9WT_t \cdot \left(\frac{W_f}{2} - X_{off} \right) + 0.75 \left(S_u \cdot \frac{T_p}{3} \right) + 0.75WT_{s2} \cdot \left[W_f + \frac{(D_f - n) \cdot \tan(\Phi_s)}{3} \right] = 14520\text{-kip-ft}$

Overturning Moment = $M_{ot} := OM + S_t \cdot (L_p + T_f) = 10072.5\text{-kip-ft}$ Foundation has undercut toe per Fred A. Nudd dwg 96-4992-1

Factor of Safety Actual = $FS := \frac{M_r}{M_{ot}} = 1.44$

Factor of Safety Required = $FS_{req} := 1$ OverTurning_Moment_Check := if(FS ≥ FS_{req}, "Okay", "No Good")

OverTurning_Moment_Check = "Okay"

Shear Capacity in Pier:

Shear Resistance of Pier =
$$S_p := \frac{P_{ave} \cdot A_p + \mu \cdot W_{T_{tot}}}{FS_{req}} = 448.635 \text{ kips}$$

Shear_Check := if($S_p > S_t$, "Okay", "No Good")

Shear_Check = "Okay"

Bearing Pressure Caused by Footing:

Total Load =
$$Load_{tot} := W_{T_c} + W_{T_{s1}} + W_{T_t} = 979 \text{ kip}$$

Area of the Mat =
$$A_{mat} := W_f^2 = 1.156 \times 10^3$$

Section Modulus of Mat =
$$S := \frac{W_f^3}{6} = 6550.67 \cdot ft^3$$

Maximum Pressure in Mat =
$$P_{max} := \frac{Load_{tot}}{A_{mat}} + \frac{M_{ot}}{S} = 2.385 \text{ ksf}$$

Max_Pressure_Check := if($P_{max} < 0.75q_s$, "Okay", "No Good")

Max_Pressure_Check = "Okay"

Minimum Pressure in Mat =
$$P_{min} := \frac{Load_{tot}}{A_{mat}} - \frac{M_{ot}}{S} = -0.69 \text{ ksf}$$

Min_Pressure_Check := if($(P_{min} \geq 0) \cdot (P_{min} < 0.75q_s)$, "Okay", "No Good")

Min_Pressure_Check = "No Good"

Distance to Resultant of Pressure Distribution =
$$X_p := \frac{P_{max}}{P_{max} - P_{min}} \cdot \frac{1}{3} = 8.789$$

Distance to Kern =
$$X_k := \frac{W_f}{6} = 5.667$$
 Since Resultant Force is Not in Kern, Area to which Pressure is Applied Must be Reduced.

Eccentricity =
$$e := \frac{M_{ot}}{Load_{tot}} = 10.284$$

Adjusted Soil Pressure =
$$P_a := \frac{2 \cdot Load_{tot}}{3 \cdot W_f \left(\frac{W_f}{2} - e \right)} = 2.86 \text{ ksf}$$

$q_{adj} := \text{if}(P_{min} < 0, P_a \cdot P_{max}) = 2.86 \text{ ksf}$

Pressure_Check := if($q_{adj} < 0.75q_s$, "Okay", "No Good")

Pressure_Check = "Okay"

Concrete Bearing Capacity:

Strength Reduction Factor = $\Phi_c := 0.65$ (ACI-2008 9.3.2.2)

Bearing Strength Between Pier and Pad = $P_b := \Phi_c \cdot 0.85 \cdot f_c \cdot \frac{\pi \cdot d_p^2}{4} = 4.499 \times 10^3 \text{ kips}$ (ACI-2008 10.14)

Bearing_Check := if($P_b > LF \cdot C_t$, "Okay", "No Good")

Bearing_Check = "Okay"

Shear Strength of Concrete:

Beam Shear: (Critical section located at a distance d from the face of Pier) (ACI 11.3.1.1)

$\Phi_c := 0.85$ (ACI 9.3.2.5)

$d := T_f - C_{vrpad} - d_{bot} = 16.73 \text{ in}$

$FL := LF \cdot \frac{C_t}{W_f^2} = 0.425 \text{ ksf}$

$V_{req} := FL \cdot (X_t - .5 \cdot d_p - d) \cdot W_f = 52.66 \text{ kips}$

$V_{Avail} := \Phi_c \cdot 2 \cdot \sqrt{f_c \cdot \text{psi}} \cdot W_f \cdot d = 778 \text{ kip}$ (ACI-2008 11.2.1.1)

Beam_Shear_Check := if($V_{req} < V_{Avail}$, "Okay", "No Good")

Beam_Shear_Check = "Okay"

Punching Shear: (Critical Section Located at a distance of d/2 from the face of pier) (ACI 11.11.1.2)

Critical Perimeter of Punching Shear = $b_o := (d_p + d) \cdot \pi = 16.9$

Area Included Inside Perimeter = $A_{bo} := \frac{\pi \cdot (d_p + d)^2}{4} = 22.9$

Required Shear Strength = $V_{req} := FL \cdot (W_f^2 - A_{bo}) = 481 \text{ kips}$

Available Shear Strength = $V_{Avail} := \Phi_c \cdot 4 \cdot \sqrt{f_c \cdot \text{psi}} \cdot b_o \cdot d = 776 \text{ kip}$ (ACI-2008 11.11.2.1)

Punching_Shear_Check := if($V_{req} < V_{Avail}$, "Okay", "No Good")

Punching_Shear_Check = "Okay"

Steel Reinforcement in Pad:

Required Reinforcement for Bending:

Strength Reduction Factor = $\phi_m := .90$ (ACI-2008 9.3.2.1)

Maximum Moment in Pad = $M_{max} := 5340 \cdot \text{kip}\cdot\text{ft}$ (User Input)

Design Moment = $M_n := \frac{LF \cdot M_{max}}{\phi_m} = 5.933 \times 10^3 \cdot \text{kips}\cdot\text{ft}$

$$\beta := \begin{cases} 0.85 & \text{if } 2500 \cdot \text{psi} \leq f_c \leq 4000 \cdot \text{psi} \\ 0.65 & \text{if } f_c > 8000 \cdot \text{psi} \\ \left[\left[0.85 - \left[\frac{\left(\frac{f_c}{\text{psi}} - 4000 \right)}{1000} \right] \cdot 0.5 \right] \right] & \text{otherwise} \end{cases} = 0.6$$

(ACI-2008 10.2.7.3)

$b_{eff} := W_t \cdot \cos(30 \cdot \text{deg}) + d_p = 287.023 \cdot \text{in}$

$A_s := \frac{M_n}{(f_y \cdot d)} = 70.93 \cdot \text{in}^2$

$a := \frac{A_s \cdot f_y}{\beta \cdot f_c \cdot b_{eff}} = 5.492 \cdot \text{in}$

$A_s := \frac{M_n}{f_y \cdot \left(d - \frac{a}{2} \right)} = 84.858 \cdot \text{in}^2$

$\rho := \frac{A_s}{b_{eff} \cdot d} = 0.21206 \cdot \text{in}$

Required Reinforcement for Temperature and Shrinkage:

$$\rho_{sh} := \begin{cases} .0018 & \text{if } f_y \geq 60000 \text{ psi} \\ .0020 & \text{otherwise} \end{cases} = 0.0018 \quad (\text{ACI-2008 7.12.2.1})$$

Check Bottom Bars:

$$A_s := \text{if} \left(\rho \geq \rho_{sh}, A_s, \rho_{sh} \cdot \frac{b_{eff}}{2} \cdot d \right) = 84.9 \text{ in}^2$$

$$A_{s_{prov}} := A_{bbot} \cdot NB_{bot} = 84.9 \text{ in}^2$$

$$\text{Pad_Reinforcement_Bot} := \text{if}(A_{s_{prov}} > A_s, \text{"Okay"}, \text{"No Good"})$$

Pad_Reinforcement_Bot = "Okay"

Check top Bars:

$$A_s := \text{if} \left(\rho \geq \rho_{sh}, A_s, \rho_{sh} \cdot \frac{b_{eff}}{2} \cdot d \right) = 84.9 \text{ in}^2$$

$$A_{s_{prov}} := A_{btop} \cdot NB_{top} = 84.9 \text{ in}^2$$

$$\text{Pad_Reinforcement_Top} := \text{if}(A_{s_{prov}} > A_s, \text{"Okay"}, \text{"No Good"})$$

Pad_Reinforcement_Top = "Okay"

Development Length Pad Reinforcement:

Bar Spacing =

$$B_{sPad} := \frac{W_f - 2 \cdot C_{vr_{pad}} - NB_{bot} \cdot d_{bbot}}{NB_{bot} - 1} = 4.8 \text{ in}$$

Spacing or Cover Dimension =

$$c := \text{if} \left(C_{vr_{pad}} < \frac{B_{sPad}}{2}, C_{vr_{pad}}, \frac{B_{sPad}}{2} \right) = 2.401 \text{ in}$$

Transverse Reinforcement Index =

$$k_{tr} := 0 \quad (\text{ACI-2008 12.2.3})$$

$$L_{dbt} := \frac{3 \cdot f_y \cdot \alpha_{pad} \cdot \beta_{pad} \cdot \gamma_{pad} \cdot \lambda_{pad}}{40 \cdot \sqrt{f_c \cdot \text{psi}} \cdot \frac{c + k_{tr}}{d_{bbot}}} \cdot d_{bbot} = 45.1 \text{ in}$$

Minimum Development Length =

$$L_{dbmin} := 12 \text{ in} \quad (\text{ACI-2008 12.2.1})$$

$$L_{dbtCheck} := \text{if}(L_{dbt} \geq L_{dbmin}, \text{"Use L.dbt"}, \text{"Use L.dbmin"}) = \text{"Use L.dbt"}$$

Available Length in Pad =

$$L_{Pad} := \frac{W_f}{2} - \frac{W_t}{2} - C_{vr_{pad}} = 63 \text{ in}$$

$$L_{pad_Check} := \text{if}(L_{Pad} > L_{dbt}, \text{"Okay"}, \text{"No Good"})$$

Lpad_Check = "Okay"

Steel Reinforcement in Pier:

Area of Pier = $A_p := \frac{\pi \cdot d_p^2}{4} = 1809.56 \cdot \text{in}^2$

$A_{smin} := 0.01 \cdot 0.5 \cdot A_p = 9.05 \cdot \text{in}^2$ (ACI-2008 10.8.4 & 10.9.1)

$A_{sprov} := N_{B_{pier}} \cdot A_{b_{pier}} = 15.71 \cdot \text{in}^2$

Steel_Area_Check := if($A_{sprov} > A_{smin}$, "Okay", "No Good")

Steel_Area_Check = "Okay"

Bar Spacing In Pier = $B_{sPier} := \frac{d_p \cdot \pi}{N_{B_{pier}}} - d_{b_{pier}} = 6.54 \cdot \text{in}$

Diameter of Reinforcement Cage = $Diam_{cage} := d_p - 2 \cdot C_{vr_{pier}} = 42 \cdot \text{in}$

Maximum Moment in Pier = $M_p := S_t(L_p) \cdot LF = 5643 \cdot \text{in} \cdot \text{kips}$

Pier Check evaluated from outside program and results are listed below;

$(D \ N \ n \ P_u \ M_{xu}) := \left(d_p^{12} \ N_{B_{pier}} \ B_{S_{pier}} \ \frac{C_t \cdot 1.333}{\text{kips}} \ \frac{M_p}{\text{in} \cdot \text{kips}} \right)$

$(D \ N \ n \ P_u \ M_{xu}) = (48 \ 20 \ 8 \ 654.503 \ 5.643 \times 10^3)$

$(\phi P_n \ \phi M_{xn} \ f_{sp} \ \rho) := (0 \ 0 \ 0 \ 0)$

$(\phi P_n \ \phi M_{xn} \ f_{sp} \ \rho) := \phi P'_n (D, N, n, P_u, M_{xu})^T$

$(\phi P_n \ \phi M_{xn} \ f_{sp} \ \rho) = (2.356 \times 10^3 \ 2.031 \times 10^4 \ -38.05 \ 8.731 \times 10^{-3})$

Axial_Load_Check := if($\phi P_n \geq P_u$, "Okay", "No Good")

Axial_Load_Check = "Okay"

Bending_Check := if($\phi M_{xn} \geq M_{xu}$, "Okay", "No Good")

Bending_Check = "Okay"

Development Length Pier Reinforcement:

Available Length in Foundation:

$$L_{\text{pier}} := L_p - C_{\text{vr}}_{\text{pier}} = 54 \cdot \text{in}$$

$$L_{\text{pad}} := T_f - C_{\text{vr}}_{\text{pad}} = 18 \cdot \text{in}$$

Tension:

(ACI-2008 12.2.3)

Spacing or Cover Dimension =

$$c := \text{if} \left(C_{\text{vr}}_{\text{pier}} < \frac{B_{\text{sPier}}}{2}, C_{\text{vr}}_{\text{pier}}, \frac{B_{\text{sPier}}}{2} \right) = 3 \cdot \text{in}$$

Transverse Reinforcement =

$$k_{\text{tr}} := 0$$

(ACI-2008 12.2.3)

$$L_{\text{dbt}} := \frac{3 \cdot f_y \cdot \alpha_{\text{pier}} \cdot \beta_{\text{pier}} \cdot \gamma_{\text{pier}} \cdot \lambda_{\text{pier}}}{40 \cdot \sqrt{f_c \cdot \text{psi}} \cdot \left(\frac{c + k_{\text{tr}}}{d_{\text{bpier}}} \right)} \cdot d_{\text{bpier}} = 22.36 \cdot \text{in}$$

Minimum Development Length =

$$L_{\text{dh}} := \frac{1200 \cdot d_{\text{bpier}}}{\sqrt{\frac{f_c}{\text{psi}}}} \cdot .7 = 12.522 \cdot \text{in} \quad (\text{ACI 12.2.1})$$

Pier reinforcement bars are standard 90 degree hooks and therefore development in the pad is computed as follows:

$$L_{\text{db}} := \max(L_{\text{dbt}}, L_{\text{dbmin}}) = 22.361 \cdot \text{in}$$

$$L_{\text{tension_Check}} := \text{if}(L_{\text{pier}} + L_{\text{pad}} > L_{\text{db}}, \text{"Okay"}, \text{"No Good"})$$

$$L_{\text{tension_Check}} = \text{"Okay"}$$

Compression:

(ACI-2008 12.3.2)

$$L_{\text{dbc1}} := \frac{.02 \cdot d_{\text{bpier}} \cdot f_y}{\sqrt{f_c \cdot \text{psi}}} = 17.889 \cdot \text{in}$$

$$L_{\text{dbmin}} := 0.0003 \cdot \frac{\text{in}^2}{l_b} \cdot (d_{\text{bpier}} \cdot f_y) = 18 \cdot \text{in}$$

$$L_{\text{dbc}} := \text{if}(L_{\text{dbc1}} \geq L_{\text{dbmin}}, L_{\text{dbc1}}, L_{\text{dbmin}}) = 18 \cdot \text{in}$$

$$L_{\text{compression_Check}} := \text{if}(L_{\text{pier}} + L_{\text{pad}} > L_{\text{dbc}}, \text{"Okay"}, \text{"No Good"})$$

$$L_{\text{compression_Check}} = \text{"Okay"}$$

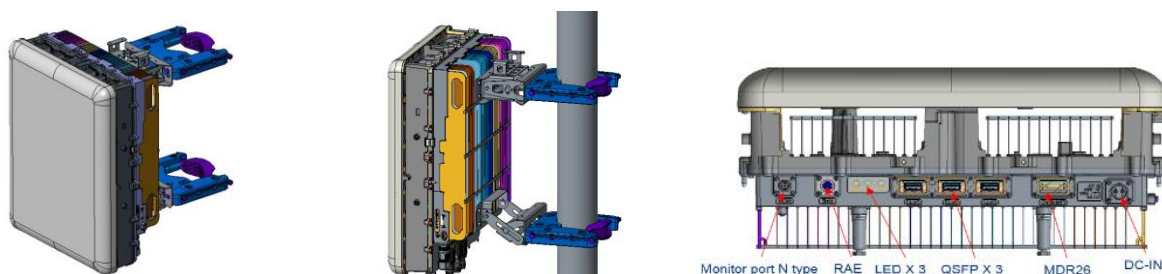
Site Data	Region: Northeast	Market:	Northern CT	Revision 2.7	Rev Date: 23-July-2018
	Cascade ID		CT03XC067	BTS OEM: ALU	RFDS Type: Preliminary
	Augment Import Code:	Augment: Relocation		Structure Type:	Tower
	Address: 250 South Olcott Street, Manchester CT 06040 Latitude: 41.77000352 Longitude: -72.55834028	Sprint Eng. Name: Bill Hastings Manager Name: Jonathan Hull		Bill.M.Hastings@sprint.com Jonathan.B.Hull@sprint.com	Eng. Phone: 978-590-9700 Manager Phone: 617-233-2920
	Detailed RFDS Description:	RFE:			RFE Phone:
	Tower Relocation	Filter Analysis Complete:	Border Analysis Complete:		Channel Plan Complete:
		Alpha	Beta		Gamma
1900	1900MHz_Azimuth	0	120		240
	1900MHz_No_of_Antennas	1	1		1
	1900MHz_RADCenter(ft)	135	135		135
	1900MHz_Antenna Make	CommScope	CommScope		CommScope
	1900MHz_Antenna Model	NNVV-65B-R4	NNVV-65B-R4		NNVV-65B-R4
	1900MHz_Horizontal_Beamwidth	68	68		68
	1900MHz_Vertical_Beamwidth	5.1	5.1		5.1
	1900MHz_Antenna Dimensions (ft) & Weight (lbs)	72 x 19.6 x 7.8 77.4 (lbs)	72 x 19.6 x 7.8 77.4 (lbs)		72 x 19.6 x 7.8 77.4 (lbs)
	1900MHz_AntennaGain(dBi)	18.8	18.8		18.8
	1900MHz_E_Tilt	0	0		
	1900MHz_M_Tilt	0	0		
	1900_Effective_Tilt	0	0		
	1900MHz_Carrier_Forecast_Year_2017				
	1900MHz_RRH Manufacturer	ALU	ALU		
	1900MHz_RRH Model	RRH 1900 4X45 65MHz	RRH 1900 4X45 65MHz		RRH 1900 4X45 65MHz
	1900MHz_RRH Count	1	1		1
	1900MHz_RRH Specs	25 x 11.1 x 11.4 (60 lbs)	25 x 11.1 x 11.4 (60 lbs)		25 x 11.1 x 11.4 (60 lbs)
	1900MHz_RRH Location	Top of the Pole/Tower	Top of the Pole/Tower		Top of the Pole/Tower
	1900MHz Combiner Model	No Combiner Required	No Combiner Required		No Combiner Required
	1900MHz Power Split Ratio (Main/Split)				
1900MHz Splitter Manufacturer					
1900MHz Splitter Model	No Splitter Required	No Splitter Required		No Splitter Required	
1900MHz Number of Splitters	0	0		0	
1900MHz_Top_Jumper #1_Length (RRH or Combiner-to-Antenna for TT or Main Coax to Antenna for Ground Mount, ft)	8	8		8	
1900MHz_Top_Jumper #1_Cable_Model (RRH or Combiner-to-Antenna for TT or Main Coax to Antenna for Ground Mount)	LCF12-50J	LCF12-50J		LCF12-50J	

	1900MHz_Top_Jumper #2_Length (RRH to Combiner for TT if applicable, ft)			
	1900MHz_Top_Jumper #2_Cable_Model (RRH to Combiner for TT if applicable)			
	1900MHz_Main_Cable_Length (ft)	135	135	135
	1900MHz_Main_Cable_Model	HB114-1-08U4-M5F	HB114-1-08U4-M5F	HB114-1-08U4-M5F
	1900MHz_Bottom_Jumper #1_Length (Ground based RRH to Combiner OR-Main Coax, ft)			
	1900MHz_Bottom_Jumper #1_Cable_Model (Ground based RRH to Combiner-OR-Main Coax)			
	1900MHz_Bottom_Jumper #2_Length (Ground based-Combiner to Main Coax, ft)			
	1900MHz_Bottom_Jumper #2_Cable_Model (Ground based-Combiner to Main Coax)			
800	800MHz_Azimuth	0	120	240
	800MHz_No_of_Antennas	1	1	1
	800MHz_RADCenter(ft)	135	135	135
	800MHz_AntennaMake	NA	NA	NA
	800MHz_AntennaModel	Antenna assigned on a different band	Antenna assigned on a different band	Antenna assigned on a different band
	800MHz_Horizontal_Beamwidth	NA	NA	NA
	800MHz_Vertical_Beamwidth	NA	NA	NA
	800MHz_Antenna Dimensions (ft) & Weight (lbs)	NA NA	NA NA	NA NA
	800MHz_AntennaGain (dBi)	NA	NA	NA
	800MHz_E_Tilt	0	0	0
	800MHz_M_Tilt	0	0	0
	800 MHz_Effective Tilt (degrees)	0	0	0
	800MHz_RRH Manufacturer	ALU	ALU	ALU
	800_Combiner_Model	No Combiner Required	No Combiner Required	No Combiner Required
	800MHz_RRH Model	RRH 800 MHz 2x50W	RRH 800 MHz 2x50W	RRH 800 MHz 2x50W
	800MHz_RRH Specs	15.8 x 13.0 x 14.0 (64 lbs)	15.8 x 13.0 x 14.0 (64 lbs)	15.8 x 13.0 x 14.0 (64 lbs)
	800MHz_RRH Count	2	2	2
	800MHz_RRH Location	Top of the Pole/Tower	Top of the Pole/Tower	Top of the Pole/Tower
	800MHz BILT Border Filter	na	na	na
	800MHz Splitter Manufacturer			
	800MHz Splitter Model			
	800MHz Number of Splitters	0	0	0
	800_Top_Jumper #1_Length (RRH to Antenna for TT or Main Coax to Antenna for GM)	8	8	8
800_Top_Jumper #1_Cable_Model (RRH to Antenna for TT or Main Coax to Antenna for GM)	LCF12-50J	LCF12-50J	LCF12-50J	

	800MHz_Main_Coax_Cable_Length (ft)	NA	NA	NA
	800MHz_Main_Coax_Cable_Model	NA	NA	NA
	800_Bottom_Jumper #1_Length (Ground based RRH to Main Coax)			
	800_Bottom_Jumper #1_Cable_Model (Ground based RRH to Main Coax)			
2500	2500MHz_Azimuth	0	120	240
	2500MHz_No_of_Antennas	1	1	1
	2500MHz_RADCenter(ft)	135	135	135
	2500MHz_AntennaMake	Nokia	Nokia	Nokia
	2500MHz_AntennaModel	AAHC (Nokia Massive MIMO RRU/Antenna Standard)	AAHC (Nokia Massive MIMO RRU/Antenna Standard)	AAHC (Nokia Massive MIMO RRU/Antenna Standard)
	2500MHz_Horizontal_Beamwidth	65	65	65
	2500MHz_Vertical_Beamwidth			
	2500MHz_AntennaHeight (ft)	25.6 x 19.7 x 9.64 103.7 (lbs)	25.6 x 19.7 x 9.64 103.7 (lbs)	25.6 x 19.7 x 9.64 103.7 (lbs)
	2500MHz_AntennaGain (dBi)			
	2500MHz_E_Tilt	0	0	0
	2500MHz_M_Tilt	0	0	0
	2500 MHz_Effective Tilt (degrees)	0	0	0
	2500MHz_RRH Manufacturer			
	2500_Combiner_Model	No Combiner Required	No Combiner Required	No Combiner Required
	2500MHz_RRH Model			
	2500MHz_RRH Count			
	2500MHz_RRH Location			
	2500MHz Power Split Ratio (Main/Split)			
	2500MHz Splitter Manufacturer			
	2500MHz Splitter Model			
	2500MHz Number of Splitters	0	0	0
	2500_Top_Jumper #1_Length (RRH to Antenna for TT or Main Coax to Antenna for GM)	8	8	8
	2500_Top_Jumper_Cable_Model (RRH to Antenna for TT or Main Coax to Antenna for GM)	LCF12-50J	LCF12-50J	LCF12-50J
	2500MHz_Main_Cable_Length (ft)	135		
	2500MHz_Main_Cable_Model	HB114-08U3M12-xxxF		
	2500_Bottom_Jumper #1_Length (Ground based RRH to Main Coax)			
	2500_Bottom_Jumper #1_Cable_Model (Ground based RRH to Main Coax)			
	Has_Split			
	Plumbing Scenario			

Comments	Date Updated			
	Update Description			
	Site Type			
	Comments			
	This RFDS is Deployment View			

TD LTE 2.5G Massive MIMO Adaptive Antenna (MAA) – AAHC



Category	Description	Unit	AAHC
Spectrum	3GPP Band		B41
	Operating frequency	MHz	2496-2690
RF characteristic	Number of TX/RX paths	#	64T64R
	Instantaneous Bandwidth IBW	MHz	194
	Occupied Bandwidth OBW	MHz	60
	Total Output power	W	120
	EIRP	dBm	74.8
Power	TX OBUE in B41 for sum of all 64 pipes at 1MHz offset	dBm/MHz	-13 sum of all ports
	Emission at IPWireless 2558-2568MHz	dBm/MHz	-57 sum of all ports
	Emission at NEXTRADAR at 2704-3000MHz	dBm/MHz	-27 sum of all ports
Interface	Power inputs		2 pin, and with APPB/APPC
	Supply Voltage / Voltage Range	V	-48V DC voltage (-40.5V~ -57V)
	Typical Power Consumption	W	75% duty cycle, 1400W for LTE
	Optical Interface		3x QSFP (4 x 9.8G CPRI each)
Antenna Specifications	RAE Interface		Circle connector, AISG-ES-RAE v2.1.0
	LMI interface		MDR26
	Monitor interface		N_Female
	Antenna array		8x8x2
Mechanical Specifications	Element Polarization	H/V or ± 45	± 45
	Gain [Broadcast 65 HBW]	dBi	15.2
	Horizontal BW [Broadcast] (@ -3dB)	Degrees	65
	Vertical BW [Broadcast] (@ -3dB)	Degrees	9
	Mechanical Downtilt Range	Degrees	± 5
	Electrical Downtilt Range	Degrees	± 10
	Cross Polar Isolation [Element]	dB	19
	Front-to-Back Ratio [Broadcast] (@ $180^\circ \pm 15^\circ$ cone)	dB	25
	Element Spacing	λ (mm)	horizontal 57.5, Vertical 80
	Upper Side Lobe Suppression (1st USLS) [Broadcast]	dB	16
	Cross Polar Discrimination [Broadcast] (@ -3dB)	dB	10
	Traffic (Service) Beam Azimuthal Pan	Degrees	± 55
	Traffic (Service) Beam Elevational Tilt	Degrees	± 10
	Azimuth Beamwidth Squint (@ Boresight)	Degrees	configurable
	Broadcast Tracking @ $\pm 60^\circ$	dB	2
Mechanical Specifications	Dimensions (LxWxD)	mm (in)	651x501x245 mm (25.6x19.7x9.6 in)
	Weight	kg (lb)	47Kg (103.6lb)
	Max Wind Speed	kmh/mph	200kmh (125 mph)
	Wind Load Front/Side/Rear @ 150kmh	N(lbF)	349 /168/130 N (78.5 / 37.8 /29.2 lbF)
	Radom Material		PC
	Radom Color		Cold Gray
	Mounting Kit	mm (in)	FPKA/FPKB/FPKC
	Operational Temperature Range	C(F)	-40 ~ 55 $^\circ$ C (-40 ~ 131 $^\circ$ F)
	Ingress protection class		IP65
	Installation options		Pole, Wall
Mechanical Specifications	Surge protection	kA	20

NNW-65B-R4

8-port sector antenna, 4x 698–896 and 4x 1695–2690 MHz, 65° HPBW, 4x RET



- Uses the 4.3-10 connector which is 40 percent smaller than the 7-16 DIN connector
- Supports re-configurable antenna sharing capability enabling control of the internal RET system using up to two separate RET compatible OEM radios
- All internal RET actuators are connected in “Cascaded MRET” configuration

Electrical Specifications

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2180	2300–2500	2500–2690
Gain, dBi	14.5	14.9	16.8	17.2	17.5	18.1	17.8
Beamwidth, Horizontal, degrees	66	64	60	60	62	59	64
Beamwidth, Vertical, degrees	11.7	10.4	7.3	6.8	6.4	5.4	5.1
Beam Tilt, degrees	2–14	2–14	2–12	2–12	2–12	2–12	2–12
USLS (First Lobe), dB	16	18	14	16	15	16	18
Front-to-Back Ratio at 180°, dB	31	34	38	38	37	33	30
Isolation, dB	25	25	25	25	25	25	25
Isolation, Intersystem, dB	25	25	25	25	25	25	25
VSWR Return Loss, dB	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0
PIM, 3rd Order, 2 x 20 W, dBc	-150	-150	-150	-150	-150	-150	-150
Input Power per Port at 50°C, maximum, watts	300	300	250	250	250	200	200
Polarization	±45°	±45°	±45°	±45°	±45°	±45°	±45°
Impedance	50 ohm	50 ohm	50 ohm	50 ohm	50 ohm	50 ohm	50 ohm

Electrical Specifications, BASTA*

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2180	2300–2500	2500–2690
Gain by all Beam Tilts, average, dBi	14.1	14.6	16.5	16.9	17.0	17.6	17.3
Gain by all Beam Tilts Tolerance, dB	±0.5	±0.5	±0.7	±0.4	±0.5	±0.6	±0.7
	2 ° 14.2	2 ° 14.7	2 ° 16.6	2 ° 16.8	2 ° 16.9	2 ° 17.5	2 ° 16.9
Gain by Beam Tilt, average, dBi	8 ° 14.2	8 ° 14.7	7 ° 16.7	7 ° 17.1	7 ° 17.2	7 ° 17.9	7 ° 17.5
	14 ° 13.9	14 ° 14.2	12 ° 16.2	12 ° 16.7	12 ° 16.7	12 ° 17.3	12 ° 17.0
Beamwidth, Horizontal Tolerance, degrees	±3.9	±3.9	±5.7	±2.7	±3.1	±7.9	±8
Beamwidth, Vertical Tolerance, degrees	±0.9	±0.8	±0.7	±0.5	±0.6	±0.4	±0.2
USLS, beampeak to 20° above beampeak, dB	16	18	14	15	14	14	14
Front-to-Back Total Power at 180° ± 30°, dB	20	20	31	31	28	28	26
CPR at Boresight, dB	21	20	18	18	19	19	20
CPR at Sector, dB	8	6	8	8	7	8	5

* CommScope® supports NGMN recommendations on Base Station Antenna Standards (BASTA). To learn more about the benefits of BASTA, [download the whitepaper Time to Raise the Bar on BSAs.](#)

Array Layout

NNV-65BR4

RF Connector Quantity, high band	4
RF Connector Interface	4.3-10 Female
Grounding Type	RF connector inner conductor and body grounded to reflector and mounting bracket
Radiator Material	Low loss circuit board
Radome Material	Fiberglass, UV resistant
Reflector Material	Aluminum
RF Connector Location	Bottom
Wind Loading, frontal	685.0 N @ 150 km/h 154.0 lbf @ 150 km/h
Wind Loading, lateral	232.0 N @ 150 km/h 52.2 lbf @ 150 km/h
Wind Loading, maximum	889.0 N @ 150 km/h 199.9 lbf @ 150 km/h
Wind Speed, maximum	241 km/h 150 mph

Dimensions

Length	1828.0 mm 72.0 in
Width	498.0 mm 19.6 in
Depth	197.0 mm 7.8 in
Net Weight, without mounting kit	35.1 kg 77.4 lb

Remote Electrical Tilt (RET) Information

Input Voltage	10–30 Vdc
Internal RET	High band (2) Low band (2)
Power Consumption, idle state, maximum	1 W
Power Consumption, normal conditions, maximum	8 W
Protocol	3GPP/AISG 2.0 (Multi-RET)
RET Hardware	CommRET v2
RET Interface	8-pin DIN Female 8-pin DIN Male
RET Interface, quantity	1 female 1 male

Packed Dimensions

Length	2010.0 mm 79.1 in
Width	608.0 mm 23.9 in
Depth	352.0 mm 13.9 in
Shipping Weight	49.0 kg 108.0 lb

Regulatory Compliance/Certifications

Agency	Classification
RoHS 2011/65/EU	Compliant by Exemption
China RoHS SJ/T 11364-2006	Above Maximum Concentration Value (MCV)
ISO 9001:2008	Designed, manufactured and/or distributed under this quality management system

