



STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square
New Britain, Connecticut 06051
Phone: (860) 827-2935
Fax: (860) 827-2950

April 7, 1999

Peter van Wilgen
SNET Mobility Inc.
500 Enterprise Drive
Rocky Hill, CT 06067-3900

RE: **TS-SCLP-003-990317** - Springwich Cellular Limited Partnership request for an order to approve tower sharing at an existing telecommunications facility located off 20 Seles Road in Ashford, Connecticut.

Dear Mr. van Wilgen:

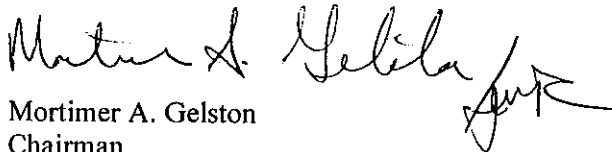
At a public meeting held April 6, 1999, the Connecticut Siting Council (Council) ruled that the shared use of this existing tower site is technically, legally, environmentally, and economically feasible and meets public safety concerns, and therefore, in compliance with General Statutes § 16-50aa, the Council has ordered the shared use of this facility to avoid the unnecessary proliferation of tower structures.

This facility has been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequency now used on this tower. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

This decision applies only to this request for tower sharing and is not applicable to any other request or construction.

The proposed shared use is to be implemented as specified in your letter dated March 17, 1999, and additional information provided on April 16, 1999. Please notify the Council when all work is complete.

Very truly yours,


Mortimer A. Gelston
Chairman

MAG/RKE/kj

c: Honorable John M. Zulick, First Selectman, Town of Ashford



RECEIVED

MAR 17 1999

March 17, 1999

CONNECTICUT
SITING COUNCIL

SNET Mobility, Inc.
500 Enterprise Drive
Rocky Hill, Connecticut 06067-3900
Phone: (860) 513-7730
Fax: (860) 513-7614

Peter W. van Wilgen
Director - Real Estate Operations

Mr. Mortimer A. Gelston, Chairman
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051

**RE: Springwich Cellular Limited Partnership—Ashford Cellular
Communication Site**

Dear Chairman Gelston:

Springwich Cellular Limited Partnership (SCLP) plans to install cellular antennas and a related equipment building at the tower facility owned by Mr. Raymond Baker of Ashford, Connecticut, and managed by Cordless Data Transfer, Inc. of Marlborough, Connecticut. Please accept this letter as notice of intent, pursuant to R.C.S.A. Section 16-50aa, of the placement of associated equipment on an existing non-facility tower pursuant to R.C.S.A. Section 16-50aa. In further compliance with R.C.S.A. Section 16-50j-73, a copy of this letter is being sent to the First Selectman of Ashford.

The existing non-facility tower is a 180' guyed tower located at 20 Seles Road, Ashford, Connecticut. NEXTEL Communications is presently located on this tower, and SCLP plans to install up to twelve panel-type cellular antennas on the tower. SCLP will also install a single story, approximately 12'x26' equipment building, which will contain radio transmission equipment.

The addition of SCLP's antennas and equipment to the tower site does not constitute a substantial environmental affect since such additions do not cause a significant change or alteration in the physical and environmental characteristics of the site (see attached site plan). Rather, the planned changes to the existing non-facility tower falls squarely within those activities explicitly provided for in R.C.S.A. Section 16-50aa.

First, the height of the existing tower will be unaffected. Twelve antennas, ALP Model 11011N, will be mounted four per sector on a triangular platform to be attached to the tower. The center of radiation will be 160' AGL and the top of the antennas will be 162' high. The tower will not require any structural modification to support the proposed attachments.

Second, the proposed addition will not extend the site boundaries. The proposed equipment building will be located next to the tower on a parcel of land of approximately 312 square feet in size, which will be leased to SCLP (see attached site plan).

Third, the proposed addition will not increase the noise levels at the existing facility by six decibels or more.

Fourth, operation of the additional antennas will not increase the total radio frequency electromagnetic radiation power density, measured at the tower base, to a level at or above the ANSI standard. The following table summarizes the power densities at the site from the various sources on the tower (including proposed herein) in relation to the standard.

FREQUENCY	POWER DENSITY	HEIGHT	ANSI/IEEE STANDARD LIMITS (mW/cm2)	% OF MPE
NEXTEL 851	0.0228	175'	0.5673	4.02
SCLP 880-894	0.0290	160'	0.5867	4.95
TOTAL	N/A		N/A	8.97

As the table demonstrates, SCLP's proposed antennas would contribute 4.95% of the ANSI standard for the cellular frequency range, bringing the site total to 8.97% of the standard as calculated for a mixed frequency site.

Finally, SCLP will obtain the necessary municipal approvals and permits for the project once Connecticut Siting Council approval has been received, as the Town of Ashford requires proof of CSC approval before any permits will be issued.

SCLP submits that the proposed additions would not cause a significant change or alteration in the physical and environmental characteristics of the site and comply with R.C.S.A. Section 16-50aa. For the foregoing reasons, SCLP therefore requests a determination that the placement of the antennas and equipment on the existing non-facility tower site does not constitute a substantial environmental effect under R.C.S.A. Section 16-50aa, and that the requested tower sharing be approved.

Thank you for your consideration.

Sincerely,

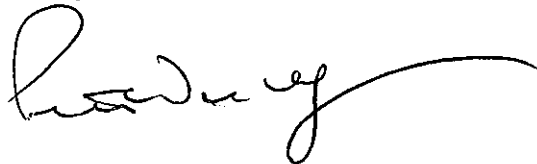


EXHIBIT A
The Site

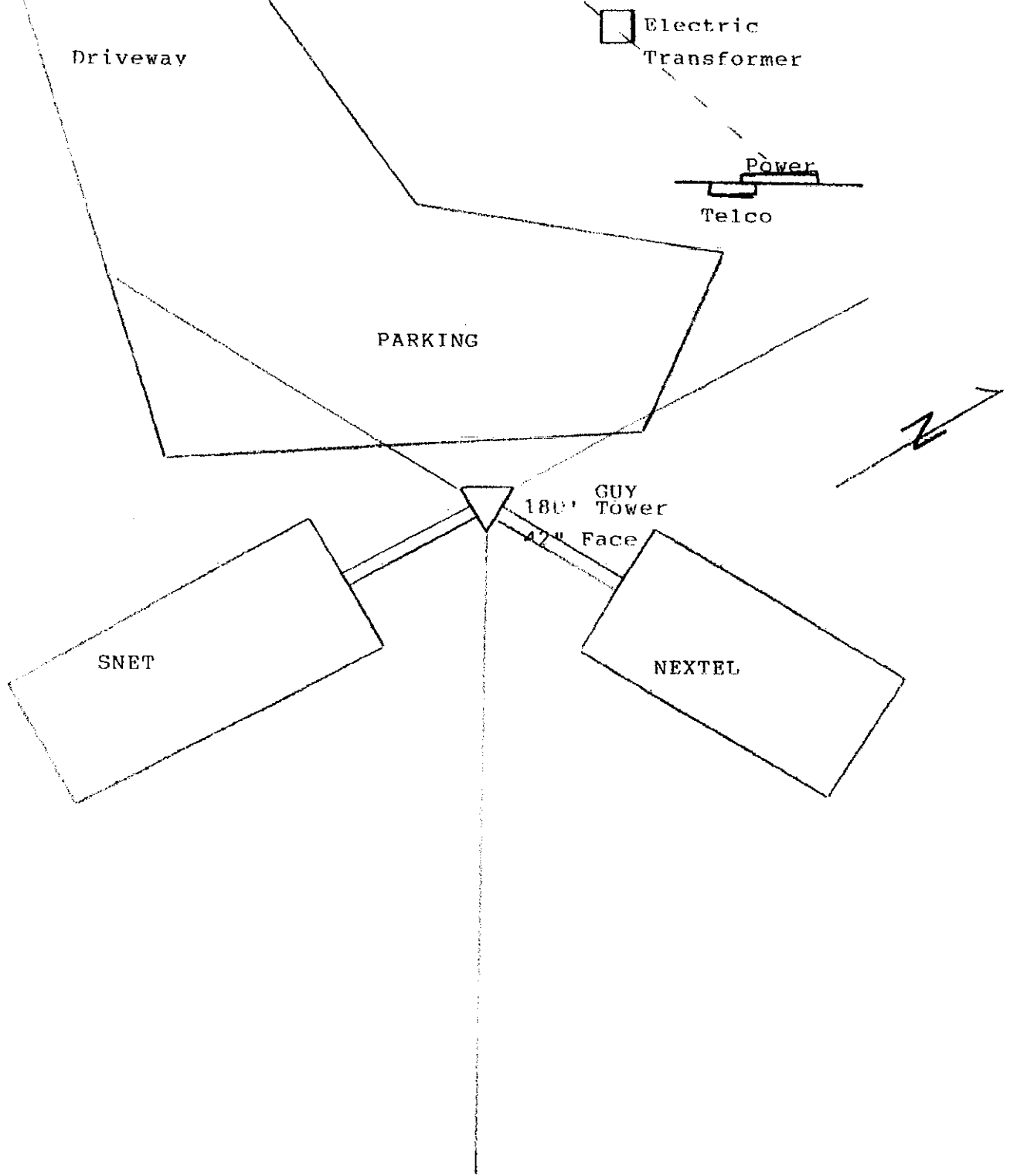
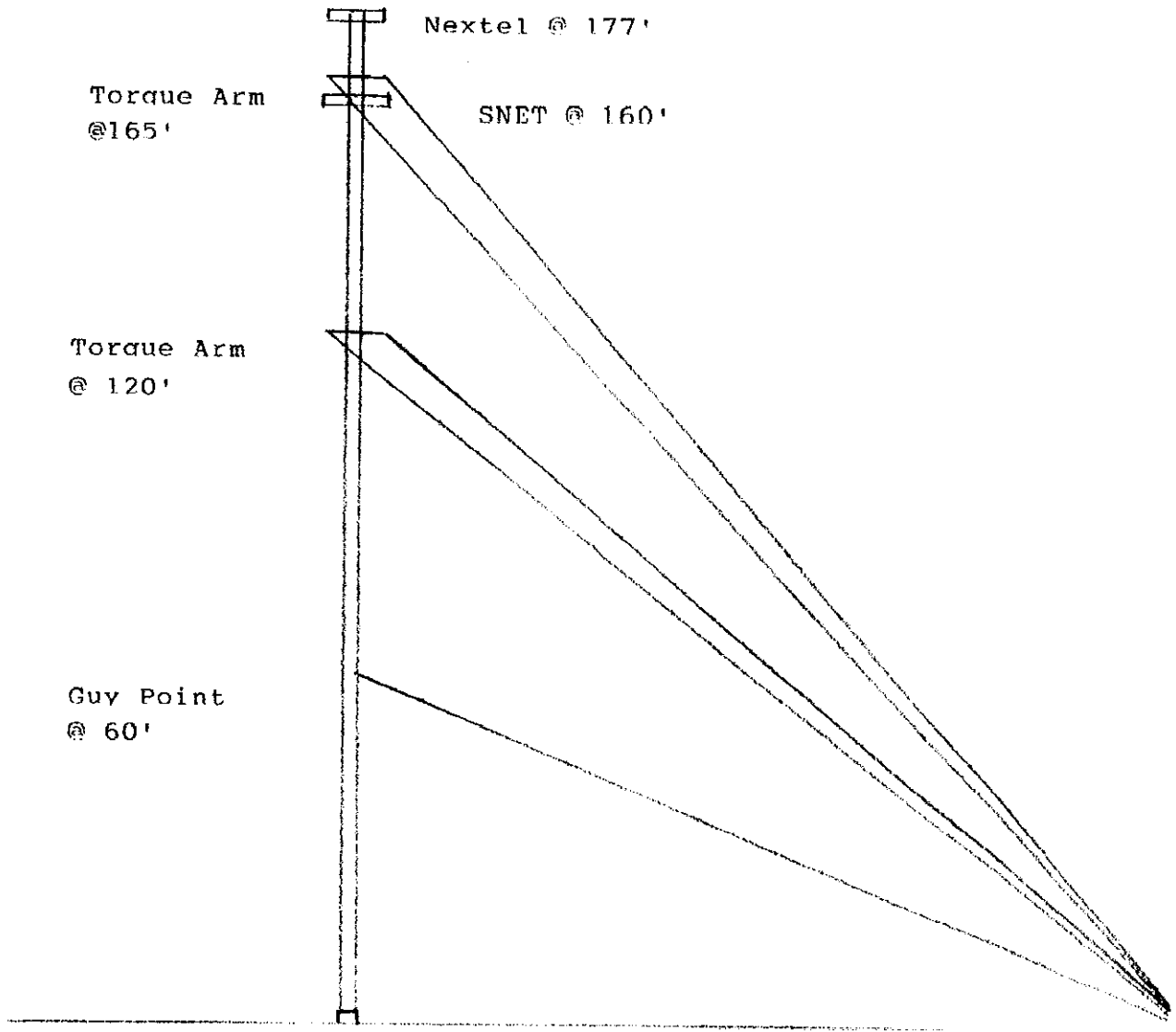


EXHIBIT B
Antennae Placement





SNET Mobility, Inc.
500 Enterprise Drive
Rocky Hill, Connecticut 06067-3900
Phone: (860) 513-7730
Fax: (860) 513-7614

March 17, 1999

Peter W. van Wilgen
Director - Real Estate Operations

Mr. John M. Zulick, First Selectman
Town of Ashford
25 Pompey Hollow Road
Ashford, Connecticut 06278

Dear First Selectman Zulick:

Springwich Cellular Limited Partnership (SCLP) plans to install antennas and associated equipment at the existing tower facility owned by Mr. Raymond Baker of Ashford, Connecticut and managed by Cordless Data Transfer of Marlborough, Connecticut. As required by Section 16-50j-73 of the Regulations of Connecticut State Agencies (R.C.S.A.), please accept this letter and the attached letter to the Connecticut Siting Council dated March 16, 1999, describing SCLP's planned use of this tower facility.

The attached letter fully describes SCLP's proposal. However, if you have any questions or require any further information on our plans or the Siting Council's procedures, please call me at (860) 513-7730 or Mr. Joel Rinebold, Executive Director, Connecticut Siting Council at (860) 827-2935.

Sincerely,

A handwritten signature in black ink, appearing to read "Peter W. van Wilgen". The signature is fluid and cursive, with a long horizontal stroke extending to the right.

Enclosure



STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square
New Britain, Connecticut 06051
Phone: (860) 827-2935
Fax: (860) 827-2950

March 19, 1999

Honorable John M. Zulick
First Selectman
Town of Ashford
Knowlton Memorial Town Hall
Route 44, 25 Pompey Hollow Road
Ashford, CT 06278

RE: TS-SCLP-003-990317 - Springwich Cellular Limited Partnership request for an order to approve tower sharing at an existing telecommunications facility located off 20 Seles Road in Ashford, Connecticut.

Dear Mr. Zulick:

On March 17, 1999, the Connecticut Siting Council (Council) received a request from Springwich Cellular Limited Partnership for an order to approve tower sharing at an existing telecommunications facility located off 20 Seles Road in Ashford, Connecticut, pursuant to Connecticut General Statutes § 16-50aa.

The Council will consider this item at the next meeting tentatively scheduled for Tuesday, April 6, 1999, at 1:30 p.m., in Hearing Room Two, Ten Franklin Square, New Britain, Connecticut.

Please call me or inform the Council if you have any questions or comments regarding this modification of an existing facility.

Thank you for your cooperation and consideration.

Very truly yours,

A handwritten signature in black ink, appearing to read "Joel M. Rinebold", written over a circular stamp.

Joel M. Rinebold
Executive Director

JMR/jlh

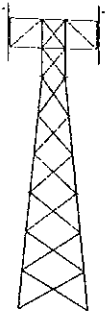
Enclosure: Notice of Intent



FRED A. NUDD CORPORATION

1743 ROUTE 104, BOX 577
ONTARIO, NY 14519
(315) 524-2531 FAX (315) 524-4249

www.nuddtowers.com



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APR - 6 1999

CONNECTICUT
SITING COUNCIL

Design of 180'
Guyed Tower

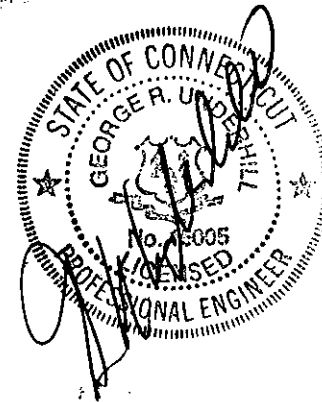
MODEL #: G42WPAR

PROJECT #: 6111

LOCATION: Ashford, CT

for

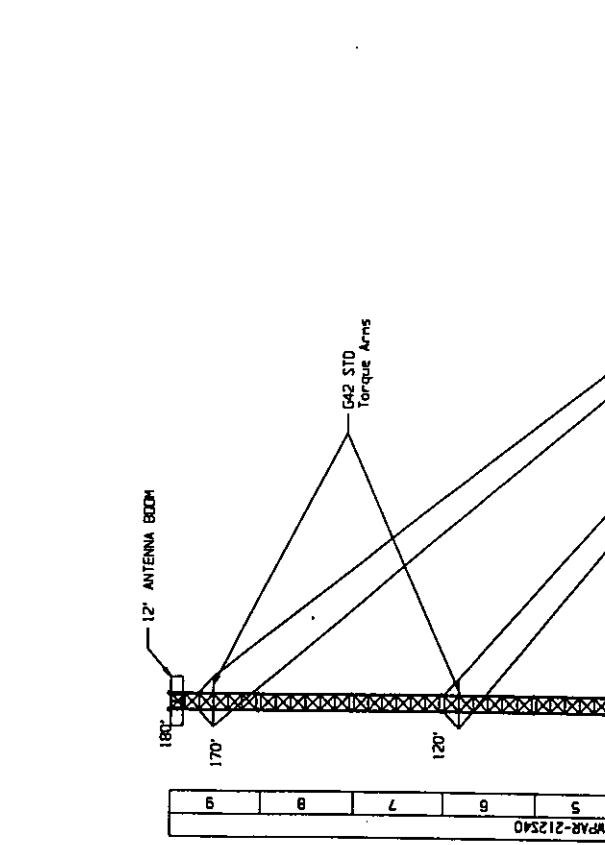
CDT
17 Ridgewood Drive
Marlborough, CT 06447



June, 1998

tower was designed to resist 85 mph wind speed with
 total ice per AWS/EA/TIA 222-F recommended standard.
 In case load condition is wind with ice with load reduction.
 Allowable steel stresses per AISC ASD 9th Edition
 Allowable concrete stresses per ACI 318-88.

MATERIAL SPECIFICATIONS
 Tower Legs: ASTM A36 Modified, $F_y > 55$ ksi. See Section Schedule.
 Guy Anchors: ASTM A36 Modified, $F_y > 48$ ksi
 All other steel: ASTM A36 Modified, $F_y > 50$ ksi
 Guy Cable: Extra High Strength Grade
 Hardware: A325 Hot Dipped Galvanized Bolts with
 Washers and Nuts
 Galvanizing: ASTM A152

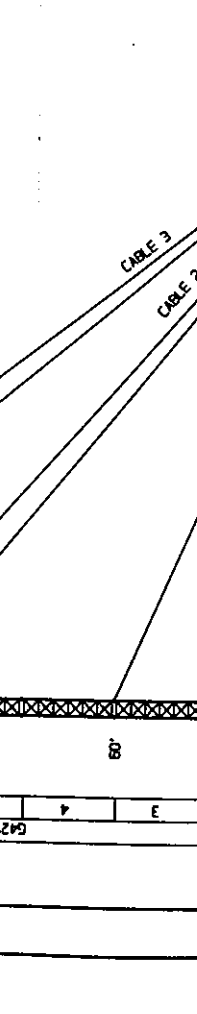


1	2	3	4	5	6	7	8	9
G42WPAR-212540								

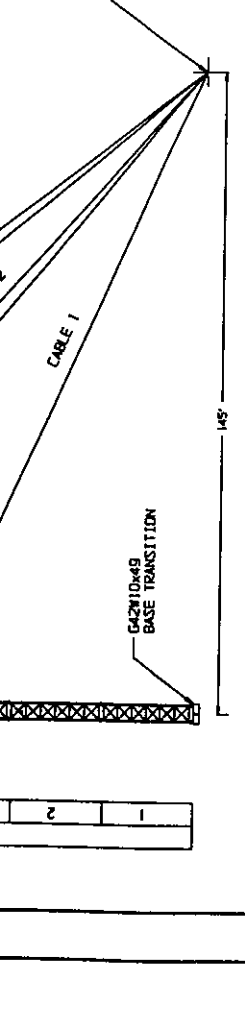
TOWER LOADING CONDITIONS

QTY	Antenna	Elevation	Windload	Deadload
3	12' Cellular Boom	178	285	170
9	Sinclair SRL 411CER130	180	392	80
10	FD 10017	180	104	25
3	12' Cellular Boom	170	281	170
9	ALP 9212	170	124	27
3	12' Cellular Boom	160	276	170
9	Sinclair SRL 411CER130	160	380	80
3	12' Cellular Boom	150	271	170
9	ALP 9212	150	119	27
1	6" HP Dish	140	837	814
1	6" HP Dish	130	819	814
1	6" HP Dish	120	801	814
1	G42 Torque Arm	170	537	262
1	G42 Torque Arm	120	486	262

QTY	Type	Elevation	Start	Stop	Windload	Deadload	#/ft
19	LF7-50A 1-5/8"	170	170	180	5.90	0.90	0.90
9	LF7-50A 1-5/8"	170	170	180	0.90	0.90	0.90
9	LF7-50A 1-5/8"	0	150	180	0.00	0.00	0.00
9	LF7-50A 1-5/8"	0	140	180	0.00	0.00	0.00
9	LF7-50A 1-5/8"	0	130	180	0.00	0.00	0.00
9	LF7-50A 1-5/8"	0	120	180	0.00	0.00	0.00
1	Tower Span 1	0	50	155.00	0.00	0.00	0.00
1	Tower Span 2	60	120	207.10	53.28	53.28	53.28
1	Tower Span 3	120	170	237.10	53.28	53.28	53.28
1	Tower Span 4	170	180	45.98	53.28	53.28	53.28



NOTE: Install cable hardware per manufacturer's specifications.



INSTALLATION NOTES

1. Installation of tower must be performed by a qualified tower erector.
2. Install sections with section number on the bottom, and climbing device is aligned.
3. Install safety climb, lights, cable attachments per manufacturer's recommendations.
4. Do not use more than 100' of assembled tower sections.
5. Do not use sharp edge of adapter plates against face of tower.
6. Plumb and tension tower and cables as erected.
7. *T1 = Initial tension of cable.

G42 Section Heights: 785/685 +/-
 Top Frame: 1000 +/-

SECTION DESIGNATION:
 G42WPAR-212555 = 2-1/2" (212), (S)Sch. 40/16H)Sch. 80, (55)ksi strength
 96-47-xx = Year-(47) ksi strength-xx

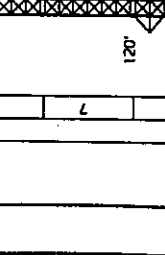
GUY CABLE SCHEDULE

CABLE	QTY/TYPE	Length	T _i	Turnbuckle	Prestorm	Thimble	Endsive Spleet
Cable 3	2 @ 5/8x7 EHS	228'	4240W	J-J	5/8" BG	3/4"	BS268 3/4"
Cable 2	2 @ 9/16x7 EHS	189'	3500W	J-J	9/16" BG	3/4"	BS267 3/4"
Cable 1	1 @ 9/16x7 EHS	157'	3500W	J-J	9/16" BG	3/4"	BS267 3/4"

NOTE: Cable lengths assume anchors at elevation 0'.
 Cable lengths and anchor layout must compensate for site topography.

NOTE: Any deviation from the proposed design antenna loading will require a tower analysis for verification of structural integrity.

Initial Installation:
 Tower: Full Height



FRED A. NUDD CORPORATION
 Route 104-Ontario, New York 14519-524-253

DATE: 6/19/98
 DRAWN BY: EES
 CHECKED BY: [Signature]
 PROJECT NO: 98-6111-1

180' G42WPAR TOWER

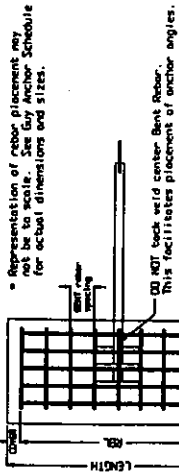
CON: Ashford, CT

This guy anchor foundation conforms to ANSI/EIA 222-E recommended standard.

DIMENSION INHER GUY ANCHOR

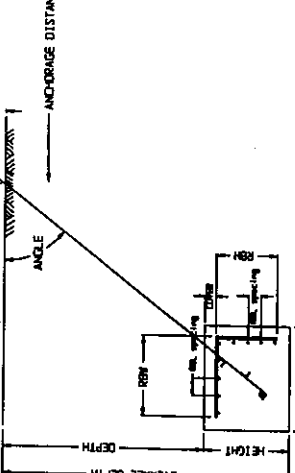
Bar Dimensions:	1.75" x 1.75" x 11.75"	12x1 pcs
Design Loads:	48.1 kip	
Horizontal:	56.0 kip	
Vertical:	74.4 kip	
Safety Factor:	2.37	
Anchor Distance:	145 ft	
Length:	11'-6"	
Width:	5'-0"	
Depth:	8'-0"	
Overall Depth:	8'-0"	
Dimension "A":	7'-0"	
Angle:	12'-6"	
Rebar Size:	4"	
Rebar Spacing:	12"	
Rebar Quantity:	12x1 pcs	
Concrete Volume:	3.47 cu yds	
Total Concrete:	14.1 cu yds	

NOTE: *Install the extra one long rebar inside the bottom angle of the guy anchor.
 *Field tie the 2 extra bent rebar.
 *Rebar #1's for one anchor only.



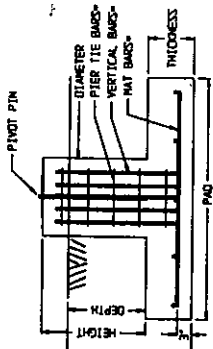
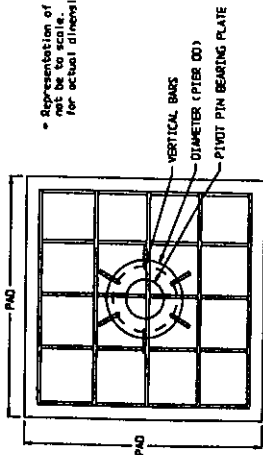
* Representation of rebar placement may not be to scale. See Guy Anchor Schedule for actual dimensions and sizes.

DD NOT lock weld center Bent Rebar. This facilitates placement of anchor angles.



GUY ANCHOR PLAN AND ELEVATION VIEWS

* Representation of rebar placement may not be to scale. See Rebar Specifications for actual dimensions and sizes.



PIER & PIER PLAN & ELEVATION VIEW

PIER SPECIFICATIONS
 Diameter: 2'-0"
 Height: 5'-0"
 Thickness: 4'-0"
 Overall Depth: 1'-6"
 Overall Height: 4'-3"
 Vertical Ties: 4.08" dia. x 9' bent leg.
 V. Bar Spacing: 10-F5 bars, 54" dia., 13.50" spacing.
 Pad Bars: 5 bars crossed each way.

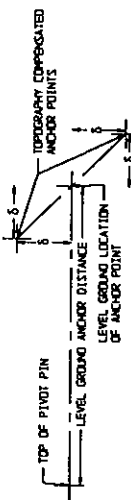
DESIGN LOADS
 Volume: 2.0 cu. yd.
 Tension: 71 k ip
 Shear: 3.600 k ip

CONCRETE SPECIFICATIONS

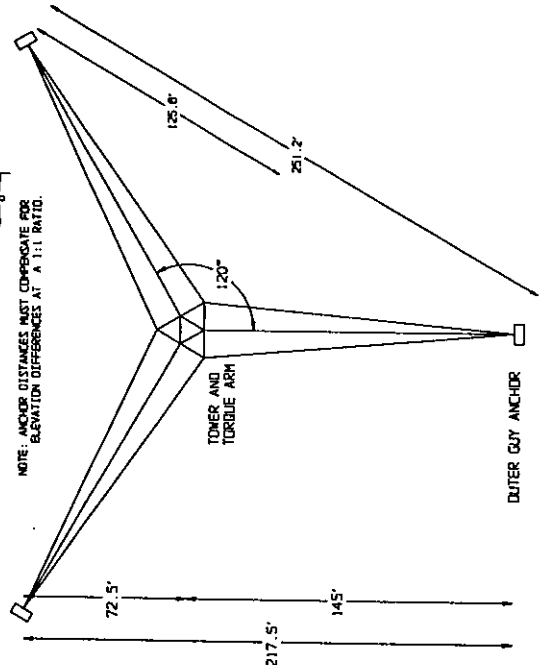
- Concrete shall have a minimum compressive strength of at least 3000 psi at 28 days. The concrete shall be placed and cured in accordance with the specifications for concrete. Concrete installation shall meet ACI 318-88 installation requirements for reinforced concrete.
- All concrete shall be placed against undisturbed soil free of water and all foreign objects and materials.
- Reinforcing bars shall be ASTM A-615 Grade 60 deformed bars.
- Welding of bars shall be in accordance with AWS D1.1 Structural Welding Code for Reinforcing Steel.
- Structural weld splices on bars must be inspected by a Fred A. Nudd engineer.
- Chapman all sharp corners of exposed concrete.

SOIL SPECIFICATIONS

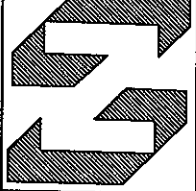
- Per customer specification soil is assumed to be EIA normal soil.
- All foundations shall be free of free water and shall be placed on a firm, stable, and well-drained subgrade. Backfill shall be in place. If not possible, special pouring procedures must be followed.
- Soils are not to be considered as normal soil. See EIA 7.2.2.
- Backfill shall be compacted to 100% of the in place dry weight.
- Backfill shall be free of organic material, accumulation of water around foundations or anchors.



NOTE: ANCHOR DISTANCES MUST COMPENSATE FOR ELEVATION DIFFERENCES AT A 1:1.1 RATIO.



TOWER PLOT PLAN AND ANCHOR LAYOUT



FRED A. NUDD CORPORATION
 Route 104-Dunbar, N.Y. New York 14519-315/524-2531
 SCALE: N/S
 DATE: 6/19/98
 EES
 FOUNDATION DETAILS
 COT
 Ashford, CT
 98-6111-2

06-19-1998
 13:58:33
 CDT
 Ashford, CT
 6111

Guy Cable Data	ft, lb				Wind	Total	Cable
	Elev	Horiz	Length	Angle	Length	Length	Type
Cable 3 :	170	145	224	49.70	1189	1345	EHS
Cable 2 :	120	145	189	39.84	938	1133	EHS
Cable 1 :	60	145	157	22.81	339	472	EHS

Cable Loads	-lb					
	Shear	Download	Cable Load	Cable Size	%Loaded	
Cable 3 :	19864	27050	35465	2 - 5/8x7	83.64	
Cable 2 :	16975	16356	25529	2 - 9/16x7	72.94	
Cable 1 :	11618	5644	14555	1 - 9/16x7	83.17	

Cable Safety Factor: 2
 Shear at 0': 3618 lb
 Shear on Guy Anchors: 351 lb

Accumulated Down Loads	
Elevation	Down load (lb)
170.0	30327
145.0	34819
120.0	55328
90.0	58569
60.0	66695
30.0	68905
0.0	71116

Guy Anchor Reactions

Vertical Reaction: 49050 lbs
 Horizontal Reaction: 55953 lbs
 Resultant: 74408 lbs
 Angle: 41.23 Degrees

Tower Plot Dimensions

A= 217.5 ft
 B= 145 ft
 C= 72.5 ft
 D= 251.2 ft
 E= 125.58 ft

MOMENT DISTRIBUTION OUTPUT - E

Beam Configuration:

4 Spans		3 Beams					
SPAN	FEMB	FEMT	VB	VT	dfB	dfT	
1	-46500	46500	4650	4650	1.0000	0.5000	
2	-62130	62130	6213	7499	0.5000	0.4545	
3	-76519	95503	8689	13450	0.5455	1.0000	
4	-52946	0	6923	0	0.0000	0.0000	

10 Iterations

SPAN #	DISTRIBUTED MOMENTS (ft-lb)			SHEARS (lb)		REACTIONS (lb)
	MOM B	MOM T	VB	VT		
1	0	61869	3618	5681		3618
2	-61870	78413	5937	7775		11618
3	-78414	52945	9198	12940		16974
4	-52946	0	6923	0		19863
						0

Tower Loads

Point Loads

No.	QTY	Antenna	Elevation	Windload	Deadload
1	3	12' Cellular Boom	178	285	170
2	9	Sinclair SRL 411C9R130	178	392	80
3	10	PD 10017	180	104	25
4	3	12' Cellular Boom	170	281	170
5	9	ALP 9212	170	124	27
6	3	12' Cellular Boom	160	276	170
7	9	Sinclair SRL 411C9R130	160	380	80
8	3	12' Cellular Boom	150	271	170
9	9	ALP 9212	150	119	27
10	1	6' MHP Dish	140	837	814
11	1	6' MHP Dish	130	819	814
12	1	6' MHP Dish	120	801	814
13	1	G42 Torque Arm	170	537	262
14	1	G42 Torque Arm	120	486	262

Uniform Loads

No.	QTY	Type	Start	Stop	Windload	Deadload
1	19	LDF7-50A 1-5/8"	170	180	5.50	0.90
2	9	LDF7-50A 1-5/8"	170	170	0.00	0.90
3	9	LDF7-50A 1-5/8"	0	160	0.00	0.90
4	9	LDF7-50A 1-5/8"	0	150	0.00	0.90
5	1	LDF7-50A 1-5/8"	0	140	0.00	0.90
6	1	LDF7-50A 1-5/8"	0	130	0.00	0.90
7	1	LDF7-50A 1-5/8"	0	120	0.00	0.90
8	1	Tower Span 1	0	60	155.00	54.78
9	1	Tower Span 2	60	120	207.10	53.28
10	1	Tower Span 3	120	170	237.10	53.28
11	1	Tower Span 4	170	180	45.96	53.28

$i := 0, \text{step}.. M_{\text{last}(\langle 0 \rangle)}, 0$

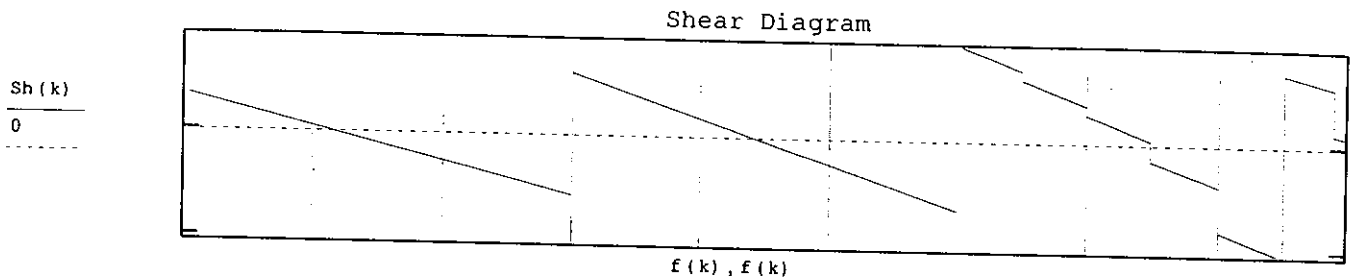
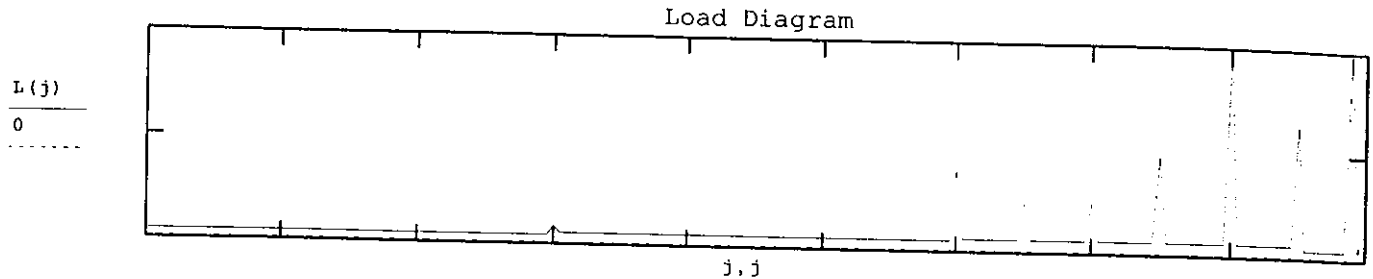
$j := 0, 1.. L_{\text{last}(\langle 0 \rangle)}, 0$

Maximum_Download := 117720

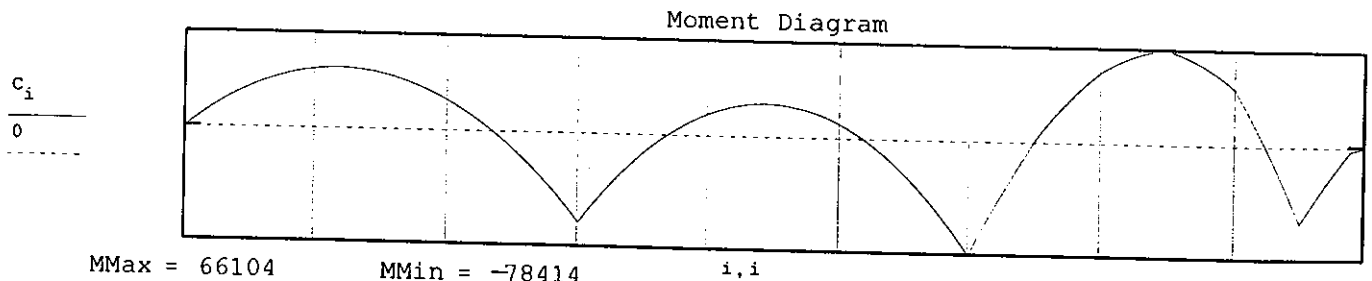
Maximum_Load = 4531.6

Lmax := Maximum_Load

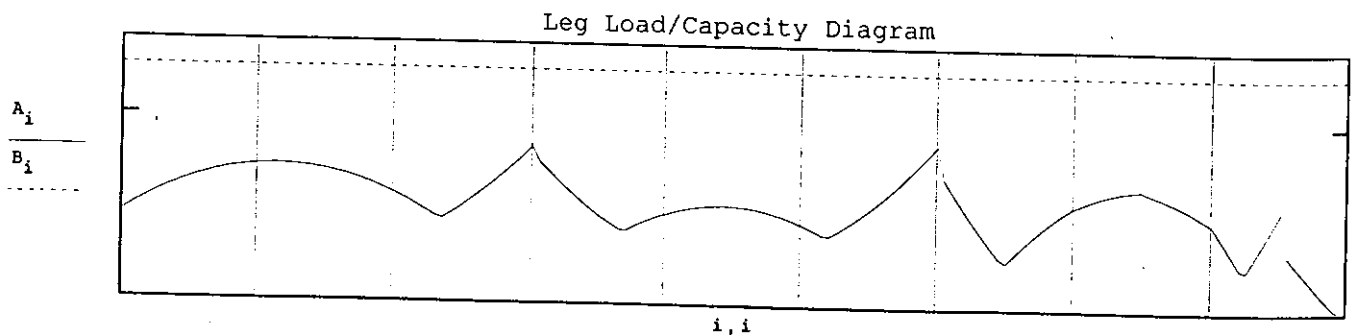
Top := 180 ft High



SMax = 9198.8 SMin = -10448.4



MMax = 66104 MMin = -78414



A_i = Leg Load
 B_i = Leg Capacity
 C_i = Moment

Elevation = 120
 Moment = -78414

Leg_Load = 44671
 Leg_Capacity = 63828

Percent_Loaded₁ = 70%

Check Girts at Guy Pulls:

Tensile capacity of (1) L1.75x1.75x1/4:

$$\text{Area} := [1.75^2 - (1.75 - .25)^2 - .375 \cdot .25] \cdot \text{in}^2$$

$$\text{Capacity} := .6 \cdot F_{y_{\text{girt}}} \cdot \frac{4}{3} \cdot \text{Area} \cdot 1 \text{ bars}$$

Maximum Single cable shear is 11618 lb, resolved into each brace.

$$\text{Percent_Loaded}_2 := \frac{11618 \cdot \text{lb} \cdot \cos(30 \cdot \text{deg})}{2 \cdot \text{girt} \cdot \text{Capacity}}$$

Steel Properties:

$$E := 29 \cdot 10^6 \cdot \text{psi}$$

$$F_{y_{\text{girt}}} := 45000 \cdot \text{psi}$$

$$F_{y_{\text{diag}}} := 45000 \cdot \text{psi}$$

$$\text{Capacity} = 25875 \cdot \text{lb} \cdot \text{f}$$

$$\text{Percent_Loaded}_2 = 25.9\%$$

Check compression capacity of girts against maximum shear:

$$l := (42 - 2.875) \cdot \text{in} \quad \text{Area} := [1.5^2 - (1.5 - .1875)^2] \cdot \text{in}^2$$

$$r := .293 \cdot \text{in} \quad \text{L1.5x1.5x.1875"} \quad \text{Area} = 0.527 \cdot \text{in}^2$$

$$K := .70 \quad \text{All welded}$$

$$klr := \frac{K \cdot l}{r}$$

$$C_c := \sqrt{\frac{2 \cdot \pi^2 \cdot E}{F_{y_{\text{girt}}}}}$$

$$klr = 93.5$$

$$C_c = 112.8$$

$$F_a := \frac{\left[1 - \frac{\left(\frac{klr}{C_c} \right)^2}{2} \right] \cdot F_{y_{\text{girt}}}}{\frac{5}{3} + \frac{3}{8} \frac{klr}{C_c} - \frac{\left(\frac{klr}{2 \cdot C_c} \right)^3}} \cdot (klr < C_c) + \frac{12 \cdot \pi^2 \cdot E}{23 \cdot klr^2} \cdot (klr \geq C_c)$$

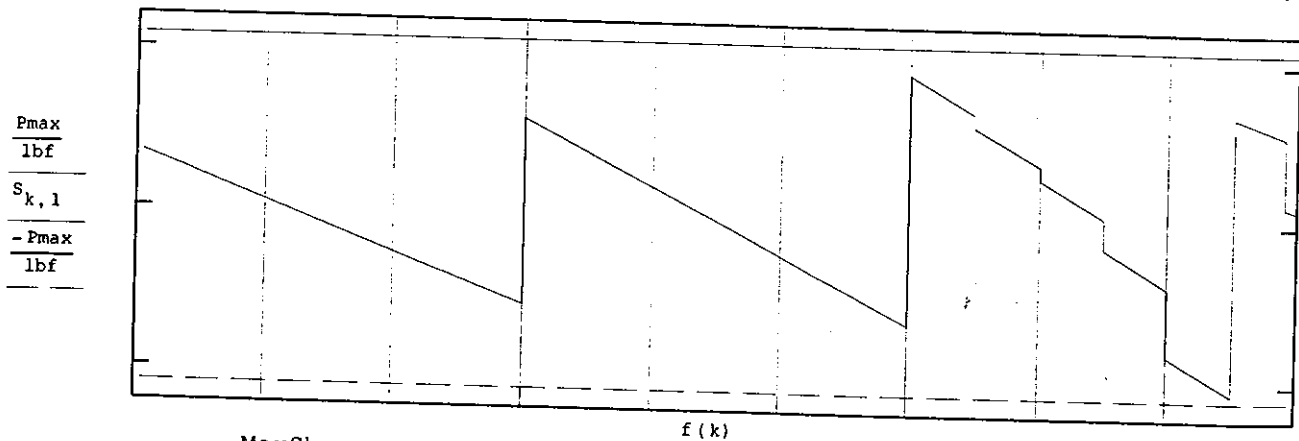
$$F_a = 15499.2 \cdot \text{psi}$$

Maximum allowable compression load:

$$P_{\text{max}} := F_a \cdot \frac{4}{3} \cdot \text{Area}$$

$$P_{\text{max}} = 10897.9 \cdot \text{lb} \cdot \text{f}$$

$$\text{MaxShear} = 10448.4$$



$$\text{Percent_Loaded}_3 := \frac{\text{MaxShear}}{P_{\text{max}}} \cdot \text{lb} \cdot \text{f}$$

$$\text{Percent_Loaded}_3 = 95.9\%$$

Check tension capacity of diagonals:

$$S(k) := \frac{Sh(k)}{2 \cdot \text{braces} \cdot \cos(45 \cdot \text{deg})}$$

$$P_{\max} := \frac{\pi}{4} \cdot \left(\frac{5}{8} \cdot \text{in}\right)^2 \cdot .6 \cdot F_{Y_{\text{diag}}} \cdot \frac{4}{3}$$

$$P_{\max} = 11044.7 \cdot \text{lbf}$$

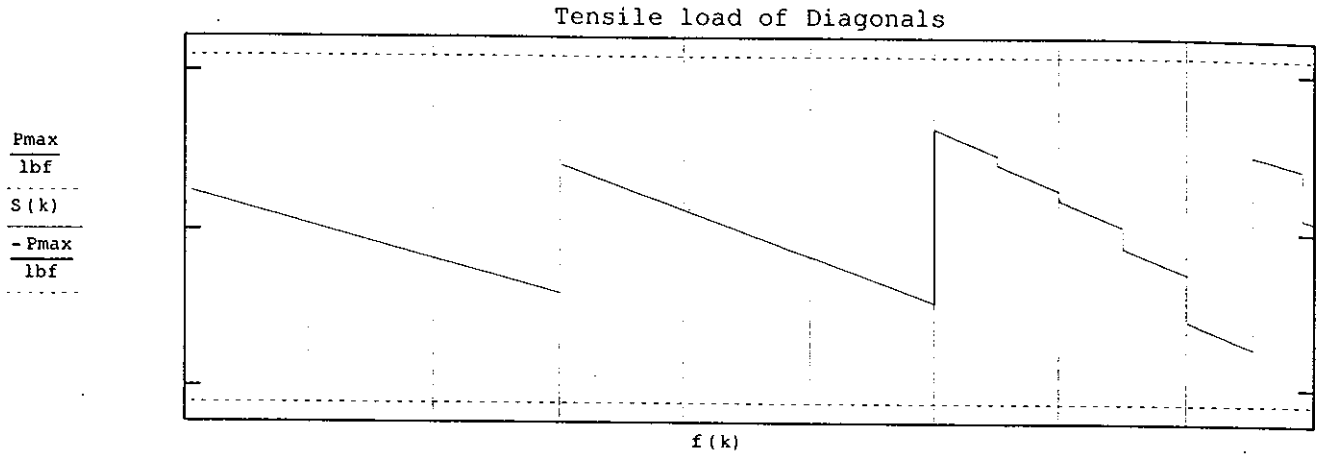
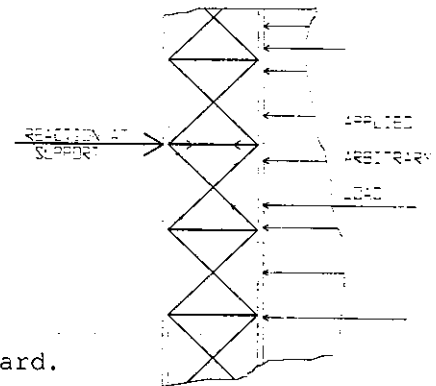


Diagram of force resolution:



Bracing:

Use 5/8" diagonals throughout tower,
Use L1.75x1.75x1/4 at gypulls,

L1.5x1.5x.1875" everywhere else.

Legs: 2-1/2" pipe

All allowable stresses per
American Institute of Steel Construction 9th edition and
Electronics Industry Association 222-E recommended standard.

REACTIONS:

Vertical 49.1 kips
 Horizontal 56.0 kips
 Resultant 74.4 kips
 Hor. Angle 41.2 °
 Submerged? 0 No
 Water Depth: 0 ft

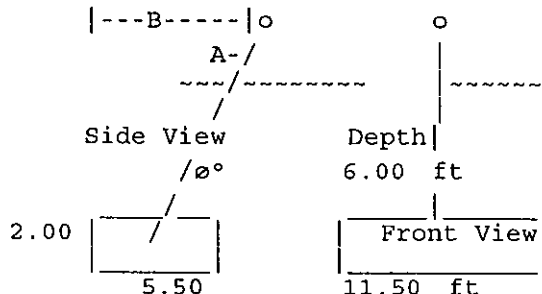
Soil Wt: 100.0 lb/ft³
 Soil Gs: 2.65
 Subm Soil Wt 62.3 lb/ft³
 H.Bearing 400.0 psf/ft
 Rebar Fy: 60.0 ksi
 Conc. Wt: 150.0 lb/ft³
 Conc f`c: 4.0 ksi

CONCRETE WEIGHT:

Block Volume 4.7 cu yds
 Block Wt 19.0 kips

SOIL FRUSTUM WEIGHT:

Frustum: 30 °
 Block: 38.0 kips
 Edges: 35.3 kips
 Corners: 9.6 kips
 Total Wt: 82.9 kips
 Excavation: 506 cuft



HORIZONTAL CAPACITY: EIA 7.1.2

Load @ 7 ft
 Load: 64400 lb

Check anchor shaft embedment? OK

GUY ANCHOR ROD:

Resultant 74.41 kips
 Hole QTY 6 holes
 # of rods 1
 Fy 48000 psi

Design Loads: 49.05 Uplift 55.95 kips
 Capacity:* 56.62 Horizontal 64.40 kips
 % Loaded: 87% 87% OK
 * EIA 7.2.4
 Concrete Volume: 14.1 cu yds

Min. Area 1.938 in²/bar
 Min. Dia. 1.571 in
 Act. Area 2.405 in²/bar
 Act. Dia. 1.75 in, 80.6% Loaded
 Anchor ID: GA6-115-15

ANCHOR ROD LENGTH:

Minimum: 13.38 ft
 Maximum: 15.17 ft
 Recommend: 14.00 ft
 Actual: 15 ft

BLOCK REINFORCEMENT:

Cover: 6 in
 Vertical Horizontal
 Factored Loads: 63.8 72.7 kips EIA 3.1.13
 Factored Moment: 1222.2 1394.2 kip-inch
 Minimum As: 1.526 0.518 in² ACI 10.5.1
 Minimum Qty: 8 3 Bar #:
 Actual Qty: 9 3 4
 Actual As: 1.767 0.589 in² OK

ANCHOR DIMENSIONS:

Length - 11'- 6"
 Width - 5'- 6"
 Height - 2'- 0"
 Depth - 6'- 0"
 OADepth- 8'- 0"
 Dim. A: 7'- 0"
 Dim. B: 12'- 6"
 ø: 41°

REBAR DIMENSIONS:

RBL: 121"
 RBH: 12"
 RBW: 56"
 Bent OAL: 68"
 QTY Long: 13 Bars ea
 QTY Bent: 14 Bars ea
 Rebar Wt. 157 lb ea

MASTER CHECK: OK

SQUARE FOOTING AND PIER DESIGN

Customer: CDT
 Project: Ashford, CT
 6/19/98 2:02 PM

Dead Load 0.0 kips
 Live Load 75 kips

G42W10x49 Base Transition ID

ASSUMED DIMENSIONS:

Width	5.50 ft	OK	f'c:	3000	psi
Thickness	1.50 ft		Fy:	60000	psi
Pier OD	2.00 ft		Soil:	4000	psf bearing capacity
Sqr Pier	0				
Rnd Pier	1		Pier Area:	452	inch ²
Depth	3.00 ft		Ht. above Grade	12	inches
Cover	6	inches			
Bar #	4	0.5			
Eff. Depth	11.750	inches			

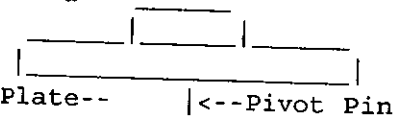
CALCULATIONS: Minimum Width: 4.330 ft
 Ultimate Load: 108.8 kips ACI 9.2.2
 Net Load: 3598 psf (factored)

CHECK SHEAR

Two Way Action: Assumes $\beta_c=1$	One Way Action Load Area:	4.240 ft ²
Vu: 83753 lbs	Vu:	15253 lbs
Vc: 245756 lbs	Vc:	72209 lbs
34.08%	<= OK =>	21.12%

LOAD TRANSFER

Pier Capacity/Pu ACI 15.8
 @ Pad/Pier interfac 742% OK - Dowels not required.
 Pivot Pin Bearing Stress: ACI 10.15.1
 Minimum Area 30 inch²
 Minimum plate OD 6.23 inch \emptyset , 5.52" ea. side square
 Distance "d" to edge 0.5 inch -> d
 Minimum Plate Thickness: 0.2846 inch

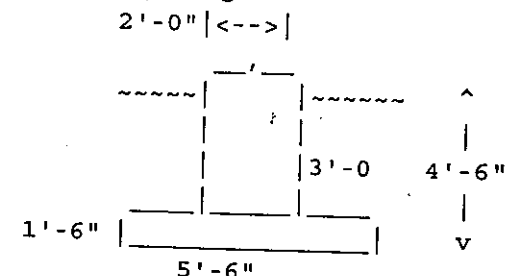


MINIMUM PIER REINFORCING ACI 15.8.2.1, 7.10.5

.5% Req.	2.262 inch ²	Steel Area:
8 Bars of # 5	2.454 inch ²	OK
Bar Lngth: 55.5 inch		
Pier Tie bar #: 4	10" tie bar spacing	

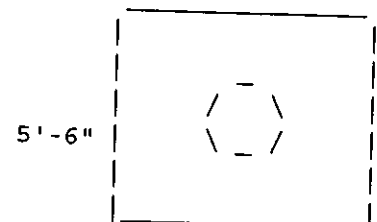
PAD BENDING MOMENT REINFORCEMENT

Mu: 30300 ft-lbs	
Ratio: 0.000997	ACI 10.5.1
Steel: 0.773 inch ²	
Bar #: 5	
Req'd QTY: 3	
Act'l QTY: 5	OK
Act. Stl: 1.534 inch ²	
Act. d: 11.500 inches	



Moment? OK
 Ldb: 11.25 inches OK

Mat Bars: Concrete:
 10 @ 13.50" spacing 2.0 cuyd
 85 lb 8220.0 lb



MASTER CHECK: OK

TRIANGULAR TOWER SECTION DATA

Client: CDT

=====

Project: Eastford, CT

Guyed Tower Section

6/19/98 2:03 PM

Wind Angle 0,60,90 90 °

Span: 1

Elevation of Foundation: 1 ft Elev@Top 40 feet

Wind Speed 85 mph Elev@Base 20 feet

Gh 1.12 EIA 2.3.4 Tower Ht. 180 feet

Wind Pres. 20.7 psf EIA 2.3.3 Top Face 42 inches 3.50

Radial Ice 0.5 inch Bot Face 42 inches 3.50

EIA 2.3.15 Wind/Ice Reductn? Yes Taper 0 in./sect.

ANSI/EIA Overstress Factor: Yes Ave Face 42 inches

Length 240 inches

LEGS OD,L1 ID,L2 wall FL.to BR 6 inches

2.5" Sch40 2.875 2.469 0.203 # Panel 6 panels

DIAGONALS Panel 38.00 inches

5/8" Rod 0.625 0.000 0.313 Br/Panel 2 |x|

HORIZONTALS Br Lngth 54.54 inches

L1.5x1.5x3 1.500 1.500 0.188 # Horiz 7 7

Density 0.283 lb/in^3

Dbl Angle Gap: 0 in Bracing Type: 1 |x|

Galvanizing? Yes

WaveGuide hole reduction? Yes SECTION GEOMETRY > 1508 in^4

Section Ixx,Iyy > 1508 in^4

ITEM DL WL Face Vert. Angle 0.000 °

Ladder: 10 10 Leg Angle in face 0.000 °

Misc. 68 0 Leg/Axis Angle 0.000 °

Total lbf: 78 10 Brace Angle 42.138 °

SECTION 1 WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

Ag: 11010 Total Weig 759 336 lbs

Af: 411 Df: 0.850

Ar: 3197 Rr: 0.625 K 1.00

SR(e): 0.328 Dr: 1.000 Legs: KL/r 40.1 OK

Cf: 2.225 Fy 55000 psi

EIA 3.1.1, Cc 102.0

Area: 16.30 ft^2 AISC E2 Fa 37457 psi

Shear: 574 28.7 lbf,lbf/ Max.Compresn.Force 63828 lbs

CnMoment: 5736 ft-lbf

Deadload: 1096 54.8 lbf,lbf/ft K 0.70

Solid Area Windloads: Diagonals: KL/r 119.1 OK

Shear: 3100 155.0 lbf,lbf/ft Fy 36000 psi

Cc 126.1

inches^2 feet^2 EIA 3.1.1 Fa 13882 psi

Ae 0° 2408.5 16.73 Max.Compresn.Force 4259 lbs

Ae 45° 2890.2 20.07 Max.Tension.Force* 8836 lbs

Ae 60° 2326.3 16.16 *Verify Net Section on member.

Ae 90° 2346.9 16.30 K 0.7

Horizontals: KL/r 93.4 OK

Cc 126.1

Span Length 60 ft EIA 3.1.1 Fa 18401 psi

pan Capacity 63137 lbf/leg Max.Compresn.Force 8194 lbs

TRIANGULAR TOWER SECTION DATA

Client: CDT

=====

Project: Eastford, CT

Guyed Tower Section

6/19/98 2:03 PM

Wind Angle 0,60,90 90 °

Span: 2

Elevation of Foundation: 1 ft

Elev@Top 100 feet

Wind Speed 85 mph

Elev@Base 80 feet

Gh 1.12 EIA 2.3.4

Tower Ht. 180 feet

Wind Pres. 27.7 psf EIA 2.3.3

Top Face 42 inches 3.50

Radial Ice 0.5 inch

Bot Face 42 inches 3.50

EIA 2.3.15 Wind/Ice Reductn? Yes

Taper 0 in./sect.

ANSI/EIA Overstress Factor: Yes

Ave Face 42 inches

Length 240 inches

LEGS OD,L1 ID,L2 wall

FL.to BR 6 inches

2.5" Sch40 2.875 2.469 0.203

Panel 6 panels

DIAGONALS

Panel 38.00 inches

5/8" Rod 0.625 0.000 0.313

Br/Panel 2 |x|

HORIZONTALS

Br Lngth 54.54 inches

L1.5x1.5x3 1.500 1.500 0.188

Horiz 7 7

Density 0.283 lb/in^3

Dbl Angle Gap: 0 in

Bracing Type: 1 |x|

Galvanizing? Yes

WaveGuide hole reduction? Yes

SECTION GEOMETRY » 1508 in^4

Section Ixx,Iyy » 1508 in^4

ITEM DL WL

Face Vert. Angle 0.000 °

Ladder: 10 10

Leg Angle in face 0.000 °

Misc. 38 0

Leg/Axis Angle 0.000 °

Total lbf: 48 10

Brace Angle 42.138 °

SECTION 2 WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs.	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

Ag:	11010		Total Weig	729	336 lbs
Af:	411	Df: 0.850			
Ar:	3197	Rr: 0.625		K	1.00
SR(e):	0.328	Dr: 1.000	Legs:	KL/r	40.1 OK
Cf:	2.225			Fy	55000 psi

Area:	16.30	ft²	EIA 3.1.1,	Cc	102.0
Shear:	763	38.2 lbf,lbf/	AISC E2	Fa	37457 psi
CnMoment:	7631	ft-lbf	Max.Compresn.Force		63828 lbs
Deadload:	1066	53.3 lbf,lbf/ft		K	0.70
Solid Area Windloads:			Diagonals :	KL/r	119.1 OK
Shear:	4142	207.1 lbf,lbf/ft		Fy	36000 psi

	inches²	feet²	EIA 3.1.1	Fa	psi
Ae 0°	2408.5	16.73	Max.Compresn.Force		4259 lbs
Ae 45°	2890.2	20.07	Max.Tension.Force*		8836 lbs
Ae 60°	2326.3	16.16	*Verify Net Section on member.		
Ae 90°	2346.9	16.30		K	0.7

Horizontals:	KL/r	93.4 OK
	Cc	126.1
EIA 3.1.1	Fa	18401 psi
Max.Compresn.Force		8194 lbs

Span Length 60 ft
pan Capacity 63137 lbf/leg

TRIANGULAR TOWER SECTION DATA

Client: CDT

=====

Project: Eastford, CT

Guyed Tower Section

6/19/98 2:03 PM

Wind Angle 0,60,90 90 °

Span: 3

Elevation of Foundation: 1 ft Elev@Top

155 feet

Wind Speed 85 mph

Elev@Base 135 feet

Gh 1.12 EIA 2.3.4

Tower Ht. 180 feet

Wind Pres. 31.7 psf EIA 2.3.3

Top Face 42 inches 3.50

Radial Ice 0.5 inch

Bot Face 42 inches 3.50

EIA 2.3.15 Wind/Ice Reductn? Yes

Taper 0 in./sect.

ANSI/EIA Overstress Factor: Yes

Ave Face 42 inches

Length 240 inches

LEGS OD,L1 ID,L2 wall

FL.to BR 6 inches

2.5" Sch40 2.875 2.469 0.203

Panel 6 panels

DIAGONALS

Panel 38.00 inches

5/8" Rod 0.625 0.000 0.313

Br/Panel 2 |x|

HORIZONTALS

Br Lngth 54.54 inches

L1.5x1.5x3 1.500 1.500 0.188

Horiz 7 7

Density 0.283 lb/in^3

Dbl Angle Gap: 0 in

Bracing Type: 1 |x|

Galvanizing? Yes

WaveGuide hole reduction? Yes

SECTION GEOMETRY » 1508 in^4

Section Ixx,Iyy » 1508 in^4

ITEM DL WL

Face Vert. Angle 0.000 °

Ladder: 10 10

Leg Angle in face 0.000 °

Misc. 38 0

Leg/Axis Angle 0.000 °

Total lbf: 48 10

Brace Angle 42.138 °

SECTION 3 WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

 Ag: 11010 Total Weig 729 336 lbs

Af: 411 Df: 0.850

Ar: 3197 Rr: 0.625

SR(e): 0.328 Dr: 1.000

Cf: 2.225

Legs: K 1.00

KL/r 40.1 OK

Fy 55000 psi

EIA 3.1.1, Cc 102.0

AISC E2 Fa 37457 psi

Max.Compresn.Force 63828 lbs

?

K 0.70

Diagonals : KL/r 119.1 OK

Fy 36000 psi

Cc 126.1

EIA 3.1.1 Fa 13882 psi

Max.Compresn.Force 4259 lbs

Max.Tension.Force* 8836 lbs

*Verify Net Section on member.

K 0.7

Horizontals: KL/r 93.4 OK

Cc 126.1

EIA 3.1.1 Fa 18401 psi

Max.Compresn.Force 8194 lbs

Span Length 50 ft
 pan Capacity 65715 lbf/leg

	inches ²	feet ²
Ae 0°	2408.5	16.73
Ae 45°	2890.2	20.07
Ae 60°	2326.3	16.16
Ae 90°	2346.9	16.30

Area: 16.30 ft²
 Shear: 872 43.6 lbf,lbf/
 CnMoment: 8720 ft-lbf
 Deadload: 1066 53.3 lbf,lbf/ft

Solid Area Windloads:
 Shear: 4741 237.1 lbf,lbf/ft

TRIANGULAR TOWER SECTION DATA

=====

Guyed Tower Section

Wind Angle 0,60,90 90 °
 Elevation of Foundation: 1 ft
 Wind Speed 85 mph
 Gh 1.12 EIA 2.3.4
 Wind Pres. 33.4 psf EIA 2.3.3
 Radial Ice 0.5 inch
 EIA 2.3.15 Wind/Ice Reductn? Yes
 ANSI/EIA Overstress Factor: Yes

Client: CDT
 Project: Eastford, CT
 6/19/98 2:03 PM
 Span: 4
 Elev@Top 185 feet
 Elev@Base 165 feet
 Tower Ht. 180 feet
 Top Face 42 inches 3.50
 Bot Face 42 inches 3.50
 Taper 0 in./sect.
 Ave Face 42 inches
 Length 240 inches
 FL.to BR 6 inches
 # Panel 6 panels
 Panel 38.00 inches
 Br/Panel 2 |x|
 Br Lngth 54.54 inches
 # Horiz 7 7
 Density 0.283 lb/in^3
 Bracing Type: 1 |x|

LEGS OD,L1 ID,L2 wall
 2.5" Sch40 2.875 2.469 0.203
 DIAGONALS
 5/8" Rod 0.625 0.000 0.313
 HORIZONTALS
 L1.5x1.5x3 1.500 1.500 0.188

Dbl Angle Gap: 0 in
 Galvanizing? Yes
 WaveGuide hole reduction? Yes

ITEM DL WL
 Ladder: 10 10
 Misc. 38 0
 Total lbf: 48 10

SECTION GEOMETRY » 1508 in^4
 Section Ixx,Iyy » 1508 in^4
 Face Vert. Angle 0.000 °
 Leg Angle in face 0.000 °
 Leg/Axis Angle 0.000 °
 Brace Angle 42.138 °

SECTION 4 WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

 Total Weig 729 336 lbs

Ag:	11010			
Af:	411	Df: 0.850		
Ar:	3197	Rr: 0.625	K	1.00
SR(e):	0.328	Dr: 1.000	Legs:	KL/r 40.1 OK
Cf:	2.225		Fy	55000 psi
Area:	16.30	ft^2	EIA 3.1.1, Cc	102.0
Shear:	919	46.0 lbf,lbf/ft	AISC E2 Fa	37457 psi
CnMoment:	9193	ft-lbf	Max.Compresn.Force	63828 lbs
Deadload:	1066	53.3 lbf,lbf/ft	K	0.70
Solid Area Windloads:			Diagonals :	KL/r 119.1 OK
Shear:	5001	250.1 lbf,lbf/ft	Fy	36000 psi
			Cc	126.1
	inches^2	feet^2	EIA 3.1.1 Fa	13882 psi
Ae 0°	2408.5	16.73	Max.Compresn.Force	4259 lbs
Ae 45°	2890.2	20.07	Max.Tension.Force*	8836 lbs
Ae 60°	2326.3	16.16	*Verify Net Section on member.	
Ae 90°	2346.9	16.30	K	0.7
Span Length	20	ft	Horizontals: KL/r	93.4 OK
pan Capacity	72067	lbf/leg	Cc	126.1
			EIA 3.1.1 Fa	18401 psi
			Max.Compresn.Force	8194 lbs

Elevation	Moment	Accum. Download	Resolved Legload	Panel / Span Capacity		% Loaded
0	0	71116	23705	63828	63137	37.5
1	3541	71042	24849	63828	63137	39.3
2	6928	70968	25942	63828	63137	41.0
3	10159	70895	26983	63828	63137	42.7
4	13235	70821	27974	63828	63137	44.2
5	16157	70747	28913	63828	63137	45.7
6	18923	70674	29801	63828	63137	47.1
7	21534	70600	30638	63828	63137	48.4
8	23991	70526	31424	63828	63137	49.6
9	26292	70453	32158	63828	63137	50.8
10	28438	70379	32842	63828	63137	51.9
11	30430	70305	33474	63828	63137	52.8
12	32266	70232	34056	63828	63137	53.8
13	33948	70158	34586	63828	63137	54.6
14	35474	70084	35065	63828	63137	55.3
15	36845	70011	35493	63828	63137	56.0
16	38062	69937	35869	63828	63137	56.6
17	39123	69863	36195	63828	63137	57.1
18	40029	69790	36469	63828	63137	57.5
19	40781	69716	36693	63828	63137	57.9
20	41377	69642	36865	63828	63137	58.2
21	41818	69568	36986	63828	63137	58.3
22	42105	69495	37056	63828	63137	58.5
23	42236	69421	37075	63828	63137	58.5
24	42212	69347	37042	63828	63137	58.4
25	42034	69274	36959	63828	63137	58.3
26	41700	69200	36824	63828	63137	58.1
27	41211	69126	36638	63828	63137	57.8
28	40568	69053	36401	63828	63137	57.4
29	39769	68979	36113	63828	63137	57.0
30	38815	68905	35774	63828	63137	56.4
31	37707	68832	35384	63828	63137	55.8
32	36443	68758	34942	63828	63137	55.1
33	35024	68684	34450	63828	63137	54.4
34	33451	68611	33906	63828	63137	53.5
35	31722	68537	33311	63828	63137	52.6
36	29839	68463	32665	63828	63137	51.6
37	27800	68390	31968	63828	63137	50.5
38	25606	68316	31220	63828	63137	49.3
39	23258	68242	30420	63828	63137	48.1
40	20754	68169	29570	63828	63137	46.7
41	18095	68095	28668	63828	63137	45.3
42	15282	68021	27715	63828	63137	43.8
43	12313	67947	26711	63828	63137	42.2
44	9189	67874	25656	63828	63137	40.6
45	5911	67800	24550	63828	63137	38.9
46	2477	67726	23393	63828	63137	37.0
47	-1112	67653	22918	63828	63137	36.3
48	-4855	67579	24128	63828	63137	38.2
49	-8754	67505	25390	63828	63137	40.2

Elevation	Moment	Accum. Download	Resolved Legload	Panel / Span Capacity		% Loaded
100	9941	57847	22562	63828	63137	35.7
101	7491	57775	21730	63828	63137	34.4
102	4834	57703	20829	63828	63137	33.0
103	1969	57631	19860	63828	63137	31.4
104	-1103	57558	19550	63828	63137	31.0
105	-4381	57486	20608	63828	63137	32.6
106	-7867	57414	21733	63828	63137	34.4
107	-11560	57342	22928	63828	63137	36.2
108	-15460	57270	24190	63828	63137	38.2
109	-19567	57198	25521	63828	63137	40.3
110	-23881	57125	26921	63828	63137	42.5
111	-28403	57053	28388	63828	63137	44.8
112	-33131	56981	29924	63828	63137	47.2
113	-38066	56909	31528	63828	63137	49.7
114	-43209	56837	33201	63828	63137	52.3
115	-48559	56764	34942	63828	63137	55.1
116	-54115	56692	36751	63828	63137	57.9
117	-59879	56620	38628	63828	63137	60.8
118	-65850	56548	40574	63828	63137	63.9
119	-72028	56476	42588	63828	63137	67.0
120	-78414	56404	44671	63828	63137	70.3
121	-69333	38140	35587	63828	65715	55.2
122	-60490	38068	32646	63828	65715	50.6
123	-51884	37997	29783	63828	65715	46.1
124	-43515	37926	26998	63828	65715	41.7
125	-35383	37855	24292	63828	65715	37.5
126	-27488	37783	21663	63828	65715	33.4
127	-19831	37712	19113	63828	65715	29.4
128	-12410	37641	16641	63828	65715	25.5
129	-5227	37569	14248	63828	65715	21.8
130	1720	37498	13067	63828	65715	19.9
131	7610	36614	14715	63828	65715	22.5
132	13263	36543	16557	63828	65715	25.4
133	18679	36473	18320	63828	65715	28.2
134	23857	36403	20005	63828	65715	30.8
135	28799	36332	21612	63828	65715	33.3
136	33504	36262	23141	63828	65715	35.7
137	37971	36192	24591	63828	65715	38.0
138	42201	36121	25963	63828	65715	40.1
139	46195	36051	27257	63828	65715	42.2
140	49951	35980	28473	63828	65715	44.1
141	52633	35097	29063	63828	65715	45.0
142	55078	35027	29847	63828	65715	46.2
143	57286	34958	30552	63828	65715	47.3
144	59257	34888	31179	63828	65715	48.3
145	60991	34819	31728	63828	65715	49.2
146	62488	34750	32199	63828	65715	49.9
147	63748	34680	32591	63828	65715	50.5
148	64770	34611	32906	63828	65715	51.0
149	65556	34541	33142	63828	65715	51.4

Elevation	Moment	Accum. Download	Resolved Legload	Panel / Span Capacity		% Loaded
150	66104	34472	33299	63828	65715	51.7
151	64529	33657	32508	63828	65715	50.4
152	62717	33596	31890	63828	65715	49.5
153	60667	33534	31193	63828	65715	48.4
154	58381	33473	30418	63828	65715	47.2
155	55857	33412	29565	63828	65715	45.8
156	53097	33350	28634	63828	65715	44.4
157	50099	33289	27625	63828	65715	42.8
158	46864	33228	26537	63828	65715	41.1
159	43392	33166	25371	63828	65715	39.3
160	39683	33105	24127	63828	65715	37.3
161	31487	31822	20995	63828	65715	32.4
162	23054	31768	18195	63828	65715	28.0
163	14384	31715	15317	63828	65715	23.5
164	5477	31662	12361	63828	65715	18.9
165	-3668	31608	11746	63828	65715	17.9
166	-13049	31555	14823	63828	65715	22.8
167	-22668	31502	17979	63828	65715	27.7
168	-32523	31449	21213	63828	65715	32.8
169	-42616	31395	24525	63828	65715	38.0
170	-52946	31342	27915	63828	65715	43.3
171	-46098	2113	15913	63828	72067	24.8
172	-39401	2043	13680	63828	72067	21.3
173	-32854	1973	11496	63828	72067	17.9
174	-26457	1902	9363	63828	72067	14.6
175	-20211	1832	7279	63828	72067	11.3
176	-14115	1762	5244	63828	72067	8.1
177	-8170	1691	3259	63828	72067	5.0
178	-2376	1621	1324	63828	72067	2.0
179	-1113	320	474	63828	72067	0.7
180	0	250	83	63828	72067	0.1

Input File:E

Tower Data File

Associated Data Files

E.out

E.mom

E.mcn

ID

CDT

Ashford, CT

6111

th face wind ice vo int az

180 42 85 0 1 1 0

Beam Configuration

HBHBHBHC

Guy Data

3

2 170 145 1

2 120 145 1

1 60 145 1

Section Inertia

4

0 60 7.270259E-02

60 120 7.270259E-02

120 170 7.270259E-02

170 180 7.270259E-02

Leg Capacity

3

0 120 63828.3 63136.79

120 170 63828.3 65715.18

170 180 63828.3 72067.23

Point Loads

14

3 12' Cellular Boom , 178 284.82 170

9 Sinclair SRL 411C9R130 , 178 391.8543 80

10 PD 10017 , 180 103.7366 25

3 12' Cellular Boom , 170 281.1024 170

9 ALP 9212 , 170 123.5418 27

3 12' Cellular Boom , 160 276.2752 170

9 Sinclair SRL 411C9R130 , 160 380.0984 80

3 12' Cellular Boom , 150 271.2275 170

9 ALP 9212 , 150 119.2019 27

1 6' MHP Dish , 140 836.7584 814

1 6' MHP Dish , 130 819.2274 814

1 6' MHP Dish , 120 800.7048 814

1 G42 Torque Arm , 170 537.1382 262

1 G42 Torque Arm , 120 486.258 262

Uniform Loads

11

19 LDF7-50A 1-5/8" , 170 180 5.5 .9

9 LDF7-50A 1-5/8" , 170 170 0 .9

9 LDF7-50A 1-5/8" , 0 160 0 .9

9 LDF7-50A 1-5/8" , 0 150 0 .9

1 LDF7-50A 1-5/8" , 0 140 0 .9
1 LDF7-50A 1-5/8" , 0 130 0 .9
1 LDF7-50A 1-5/8" , 0 120 0 .9
1 Tower Span 1 , 0 60 155 54.78
1 Tower Span 2 , 60 120 207.1 53.28
1 Tower Span 3 , 120 170 237.1 53.28
1 Tower Span 4 , 170 180 45.96 53.28
End