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Kristen Motel
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October 28, 2019

VIA EMAIL AND FEDERAL EXPRESS

Members of the Connecticut Siting Council
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051

Re: Development and Management Plan (“D&M Plan”)
Connecticut Siting Council Docket No. 485
Certificate of Environmental Compatibility and Public Need for the
Construction, Maintenance and Operation (“Certificate”) of a
Telecommunications Facility at
1542 Boston Post Road, Westbrook, Connecticut

Dear Members of the Siting Council:

On behalf of Message Center Management, Inc. (“MCM”), and in furtherance of the captioned Certificate, please accept for review and Council approval this Development Management Plan (“D&M Plan”) filing for the captioned Facility as approved in Docket No. 485.

Tower, Compound & Other Equipment

Enclosed are an original and fifteen (15) sets of 11” x 17” D&M Plan drawings prepared by All Points Technology Corporation (APT) revised through October 21, 2019 being filed in accordance with the Siting Council’s (“Council”) Decision and Order dated August 15, 2019 (“Decision and Order”). Two full sized sets of the D&M Plan drawings are also enclosed.

As per order number 1 of the Council’s Decision and Order, the D&M Plan incorporates a 130’ monopole tower with an overall facility height of 136’ 8” to the top of the whip antenna for the Old Saybrook Police Department. The monopole design and the D&M Plan incorporate the antennas and specifications for Celco Partnership d/b/a Verizon Wireless, AT&T, T-Mobil and the Old Saybrook Police Department. Included in the D&M plans, enclosed in Attachment 1, are the final site plans including specifications for the tower, tower foundation, antennas, modifications to the existing equipment compound, radio equipment, utilities and access road.

Of note, the D&M Plan also includes construction sequencing and site preparations, drainage, and erosion and sedimentation control measures consistent with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control as amended. Sheet L-1 of the D&M Plan drawings details a landscaping plan, including an evergreen tree planting plan. Sheet C-1 of the



D&M Plan drawings outlines construction sequencing, including proposed hours and days of the week for construction activities and a schedule for removal of the existing temporary tower.

As per condition 2 of the Council's Decision and Order the tower incorporates a yield point to ensure the setback radius remains within the boundaries of the subject property. This is described in detail in the October 17, 2019 letter from Habib Azouri, P.E. and structural analysis completed by ROHN Products LLC, included in Attachment 3.

Please also find enclosed a geotechnical report, prepared by Nobis Engineering, Inc. and dated March 18, 2017, included in Attachment 2. Details of the antennas and equipment to be installed on the tower by Verizon (Attachment 4), AT&T (Attachment 5) and T-Mobile (Attachment 6) are also provided. Please note that no additional backup emergency power generator is proposed at this time.

Required Notifications

In accordance with RCSA Section 16-50j-75, a copy of this filing is being provided to The Connecticut Water Company, as the property owner of record and the service list.

In accordance with the provisions of RCSA Section 16-50j-77, MCM hereby notifies the Council of its intention to begin site work immediately after Council approval of the D&M Plan. Construction of the tower and other site improvements will commence upon issuance of a local building permit. The supervisor for all construction related matters on this project is supervisor for all construction related matters on this project is Robert Stanford. Mr. Stanford is located at MCM's office in Hartford, Connecticut and can be reached by telephone at (860) 614-9929.

We respectfully request that this matter be included on the Council's next available agenda for review and approval.

Thank you for your consideration of the enclosed.

Very truly yours,

A handwritten signature in blue ink, appearing to read 'Kristen Motel', is written over a light blue horizontal line.

Kristen Motel

Enclosures

cc: Connecticut Water Company
Virginia King, MCM
Robert Stanford, MCM
Matthew Bandle, MCM
All-Points Technology Corporation
Christopher B. Fisher, Esq.
Anthony Befera, Verizon Wireless
Noel Bishop, First Selectman



CERTIFICATE OF SERVICE

I hereby certify that on this day, an original and 15 copies of the foregoing was sent electronically and by overnight delivery to the Connecticut Siting Council with copy to:

Facility Site Owner:

The Connecticut Water Company
93 West Main Street
Clinton, CT 06413

Town of Westbrook First Selectman:

Noel Bishop, First Selectman
866 Boston Post Road
Town of Westbrook
Westbrook, CT 06489

Anthony Befera
Cellco Partnership d/b/a Verizon
Wireless
20 Alexander Drive
Wallingford, CT 06492

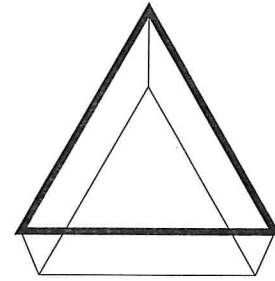
Virginia King
MCM Holdings, LLC
40 Woodland Street
Hartford, CT 06105

Dated: October 28, 2019



Kristen Motel, Esq.

1



MCM HOLDINGS, LLC

40 WOODLAND STREET
HARTFORD, CT 06105

OFFICE: (888) 973-7483

WIRELESS SERVICES FACILITY

WESTBROOK H2O TANK
1542 BOSTON POST ROAD
WESTBROOK, CT 06498

MCM HOLDINGS, LLC
P.O. BOX 320361
HARTFORD, CT 06132
OFFICE: (888) 973-7483

ALL-POINTS
TECHNOLOGY CORPORATION

3 SADDLEBROOK DRIVE PHONE: (860)-663-1697
KILLINGWORTH, CT 06419 FAX: (860)-663-0935
WWW.ALLPOINTSTECH.COM

DEVELOPMENT & MANAGEMENT PLANS		
NO	DATE	REVISION
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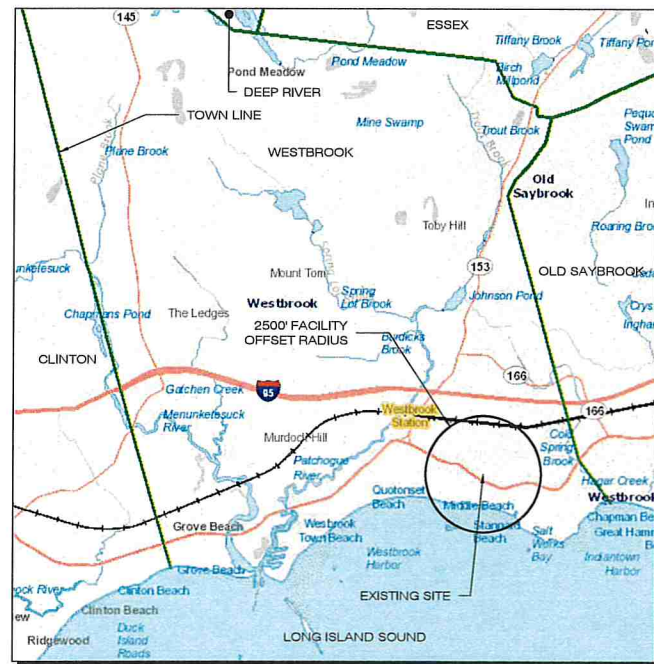


DESIGN PROFESSIONALS OF RECORD
 PROF: ROBERT C. BURNS P.E.
 COMP: ALL-POINTS TECHNOLOGY CORPORATION, P.C.
 ADD: 3 SADDLEBROOK DRIVE
 KILLINGWORTH, CT 06419
 OWNER: THE CONNECTICUT WATER COMPANY
 ADDRESS: 93 WEST MAIN STREET
 CLINTON, CONNECTICUT 06413

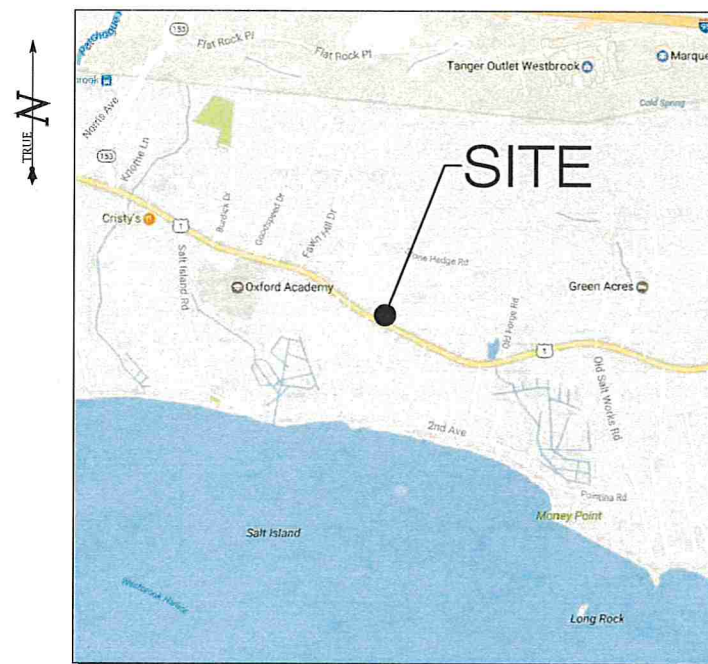
MCM SITE
 WESTBROOK H2O TANK
 SITE 1542 BOSTON POST ROAD
 ADDRESS: WESTBROOK, CT 06498
 APT FILING NUMBER: CT524120
 DATE: 10/08/19
 DRAWN BY: CSH
 CHECKED BY: RCB

SHEET TITLE:
TITLE SHEET & INDEX

SHEET NUMBER:
T-1



MUNICIPAL NOTIFICATION LIMIT MAP
 SCALE: 1" = 4000'-0"



VICINITY MAP
 SCALE: 1" = 1000'-0"

SITE INFORMATION

SITE TYPE: PROPOSED 130' AGL MONOPOLE
 SCOPE OF WORK: PROPOSED RF EQUIPMENT ON PROPOSED 130' AGL MONOPOLE TO CONNECT TO EXISTING GROUND EQUIPMENT WITHIN AN EXISTING FENCED COMPOUND.
 SITE NAME: WESTBROOK H2O TANK
 SITE ADDRESS: 1542 BOSTON POST ROAD
 WESTBROOK, CT 06498
 ZONING JURISDICTION: CONNECTICUT SITING COUNCIL
 COUNTY: MIDDLESEX
 ASSESSOR'S TAX ID#: MAP: 182, LOT: 007
 ZONING DISTRICT: NEIGHBORHOOD COMMERCIAL DISTRICT (NCD)
 LATITUDE: 41° 16' 54.9197" N
 LONGITUDE: 72° 26' 14.9183" W
 GROUND ELEVATION: 48± AMSL
 PROPERTY OWNER: THE CONNECTICUT WATER COMPANY
 93 WEST MAIN STREET
 CLINTON, CONNECTICUT 06413
 LEGAL: CUDDY & FEDER, LLP
 445 HAMILTON AVENUE
 14TH FLOOR
 WHITE PLAINS, NY 10601
 APPLICANT: MCM HOLDINGS, LLC
 40 WOODLAND STREET
 HARTFORD, CT 06105
 SITE ENGINEER: ALL-POINTS TECHNOLOGY CORP., P.C.
 3 SADDLEBROOK DRIVE
 KILLINGWORTH, CT 06419
 (860) 663-1697 x206

LIST OF DRAWINGS

- T-1 TITLE SHEET & INDEX
- 1 OF 1 TOPOGRAPHIC SURVEY
- R-1 ABUTTERS MAP
- SP-1 PARTIAL SITE PLAN
- A-1 COMPOUND PLAN & TOWER ELEVATION
- C-1 SITE DETAILS
- C-2 VERIZON ANTENNA PLAN & DETAILS
- C-3 AT&T ANTENNA PLAN & DETAILS
- C-4 T-MOBILE ANTENNA PLAN & DETAILS
- L-1 LANDSCAPING PLAN
- N-1 ENVIRONMENTAL NOTES
- N-2 NOTES & SPECIFICATIONS

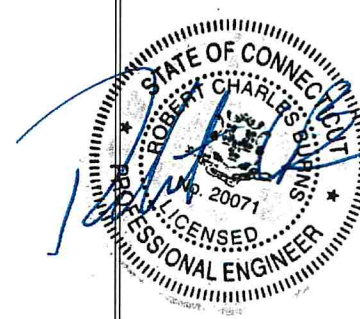
MCM HOLDINGS, LLC
 P.O. BOX 320361
 HARTFORD, CT 06132
 OFFICE: (888) 973-7483

ALL-POINTS
 TECHNOLOGY CORPORATION

3 SADDLEBROOK DRIVE PHONE: (860)-663-1697
 KILLINGWORTH, CT 06419 FAX: (860)-663-0935
 WWW.ALLPOINTSTECH.COM

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 KILLINGWORTH, CT 06419

OWNER: THE CONNECTICUT WATER COMPANY
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 CLINTON, CONNECTICUT 06413

**MCM SITE
 WESTBROOK H2O TANK**

SITE 1542 BOSTON POST ROAD
 ADDRESS: WESTBROOK, CT 06498

APT FILING NUMBER: CT524120

DRAWN BY: CSH

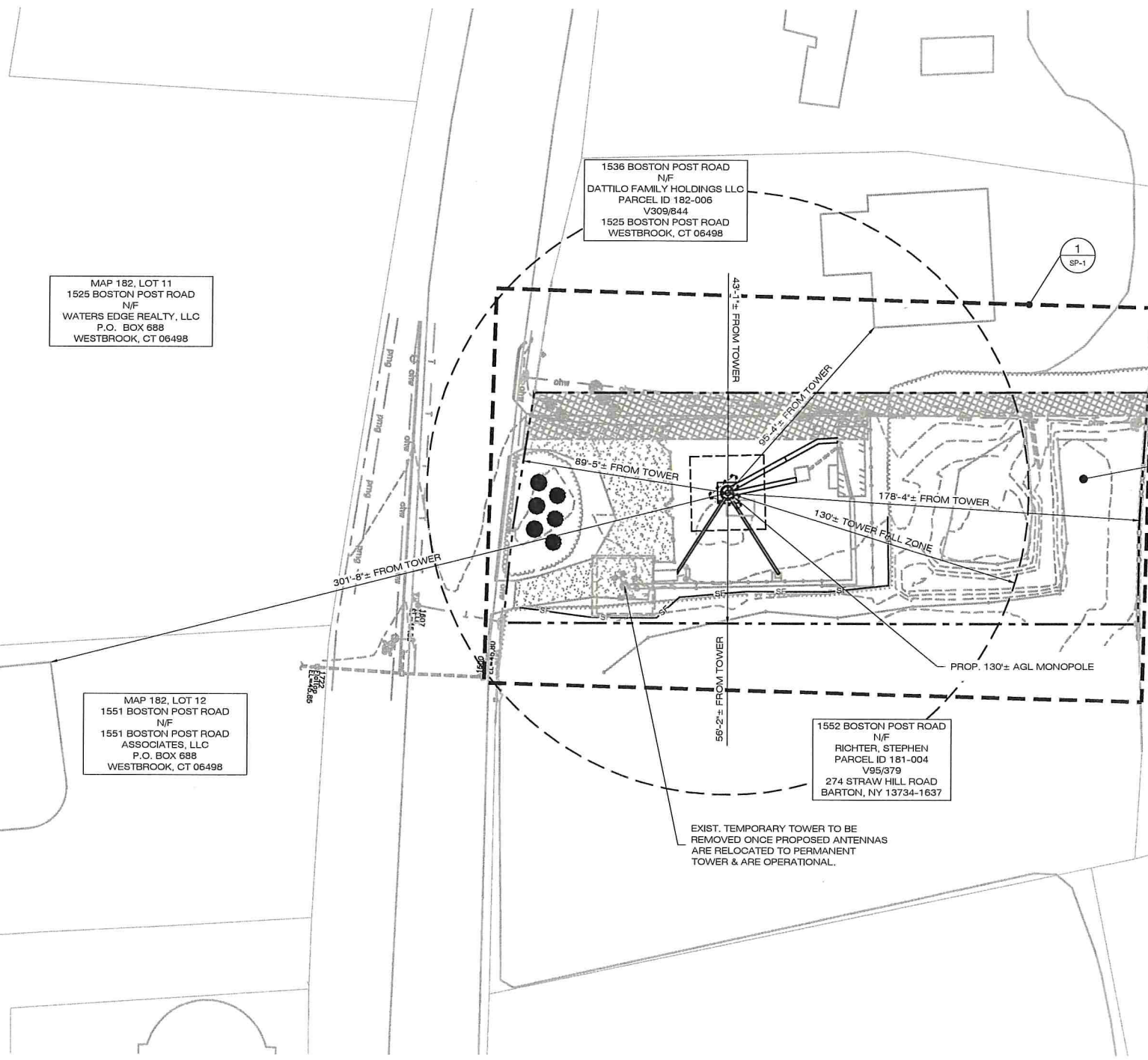
DATE: 10/08/19 CHECKED BY: RCB

SHEET TITLE:

**ABUTTERS
 MAP**

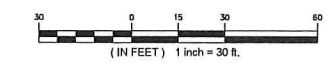
SHEET NUMBER:

R-1



EXIST. TEMPORARY TOWER TO BE REMOVED ONCE PROPOSED ANTENNAS ARE RELOCATED TO PERMANENT TOWER & ARE OPERATIONAL.

1 ABUTTERS MAP
 SCALE: 1" = 30'-0"



SITE AREAS & VOLUMES OF EARTHWORK

SITING WORK ENTAILS APPROXIMATELY 0 CY OF FILL. THE PROPOSED WORK WILL ONLY CONSIST OF THE NEW FOUNDATION ASSOCIATED WITH THE PROPOSED MONOPOLE. THE EXISTING WATERTANK AND FOOTINGS WILL BE REMOVED AND THE SITE WILL BE BACKFILLED TO EXISTING ELEVATIONS.

COMPOUND AREA SLOPES:
 EXISTING - 0.5%-3%
 PROPOSED - 0.5%-3%

TOTAL AREA OF DISTURBANCE = 4,300± SF

STORMWATER VELOCITY:
 PRIOR TO GROUND COVER < 3.0 FT/SEC
 FOLLOWING GROUND COVER < 3.0 FT/SEC

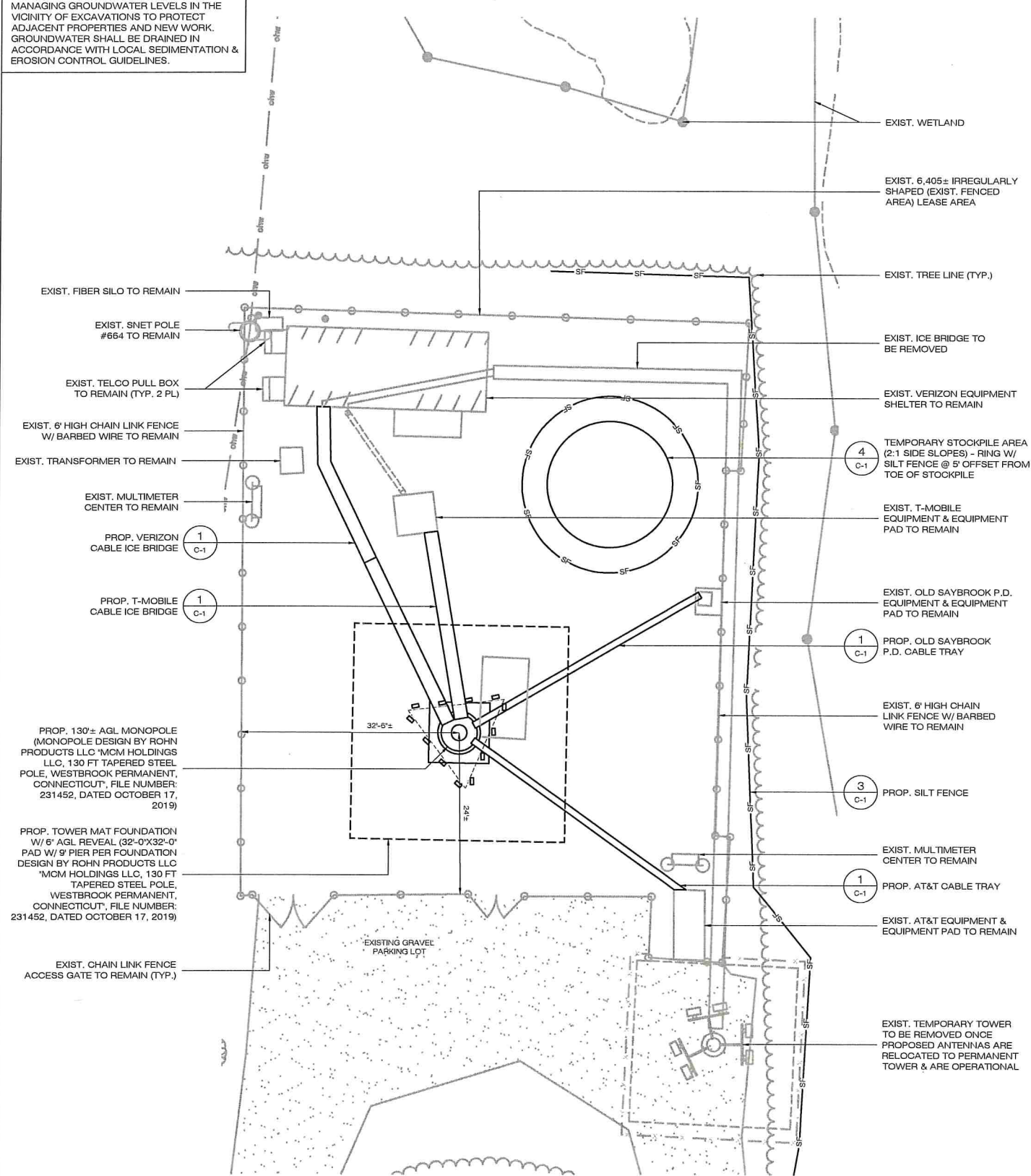
STORMWATER VOLUME:
 PROPOSED IMPERVIOUS AREA = N/A
 WATER QUALITY STD VOLUME (1") = N/A
 STORAGE VOLUME (6" DEPTH, 40% VOIDS) = N/A

GROUND COVER TO BE ESTABLISHED AS FOLLOWS (U.O.N):
 - WHITE CLOVER @ 0.20#/- SF
 - TALL FESCUE @ 0.45#/- SF
 - RYEGRASS @ 0.10#/- SF

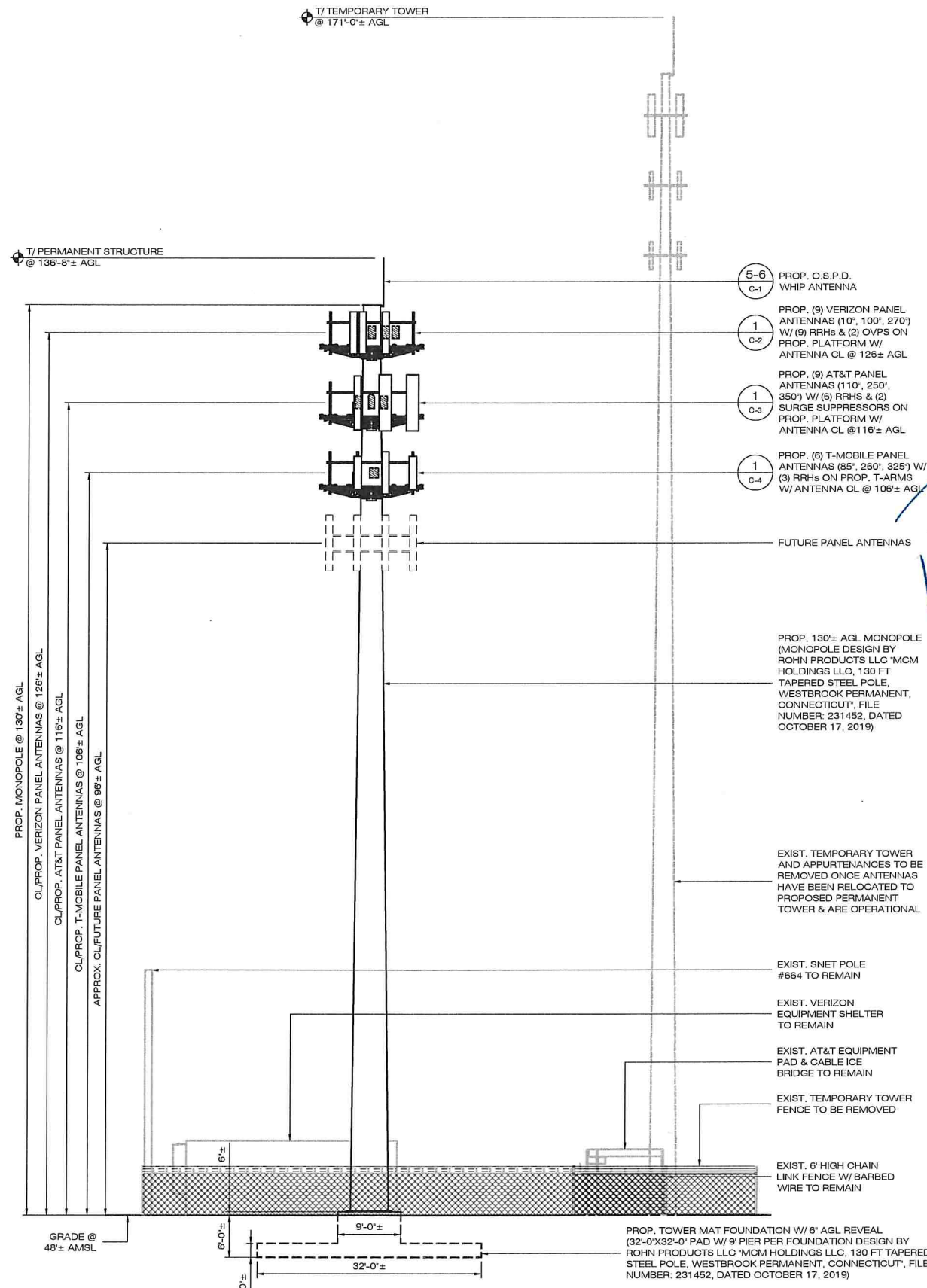
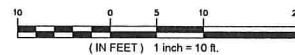
BASE MAPPING FOR SHEETS R-1, SP-1 & A-1 FROM:

1. TOPOGRAPHIC SURVEY OF 1542 BOSTON POST ROAD (AKA ROUTE #1), WESTBROOK, CONNECTICUT, PREPARED FOR CONNECTICUT WATER, PREPARED BY GESICK & ASSOCIATES, P.C., SURVEYORS/MAPPERS/PLANNERS, 19 CEDAR ISLAND AVE., CLINTON, CONNECTICUT 06413, OFFICE: (860) 669-7799 FAX: (860) 669-5833, WWW.GESICKSURVEYORS.COM.
2. BASE MAPPING SUPPLEMENTED W/ FIELD MEASUREMENTS TAKEN BY ALL-POINTS TECHNOLOGY CORP. ON 04-21-2017.

THE CONTRACTOR IS RESPONSIBLE FOR MANAGING GROUNDWATER LEVELS IN THE VICINITY OF EXCAVATIONS TO PROTECT ADJACENT PROPERTIES AND NEW WORK. GROUNDWATER SHALL BE DRAINED IN ACCORDANCE WITH LOCAL SEDIMENTATION & EROSION CONTROL GUIDELINES.



1 COMPOUND PLAN
A-1 SCALE: 1" = 10'-0"



2 SOUTH ELEVATION
A-1 SCALE: 1" = 10'-0"



MCM HOLDINGS, LLC
P.O. BOX 320361
HARTFORD, CT 06132
OFFICE: (888) 973-7483

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3 SADDLEBROOK DRIVE PHONE: (860)-663-1697
KILLINGWORTH, CT 06419 FAX: (860)-663-0935
WWW.ALLPOINTSTECH.COM

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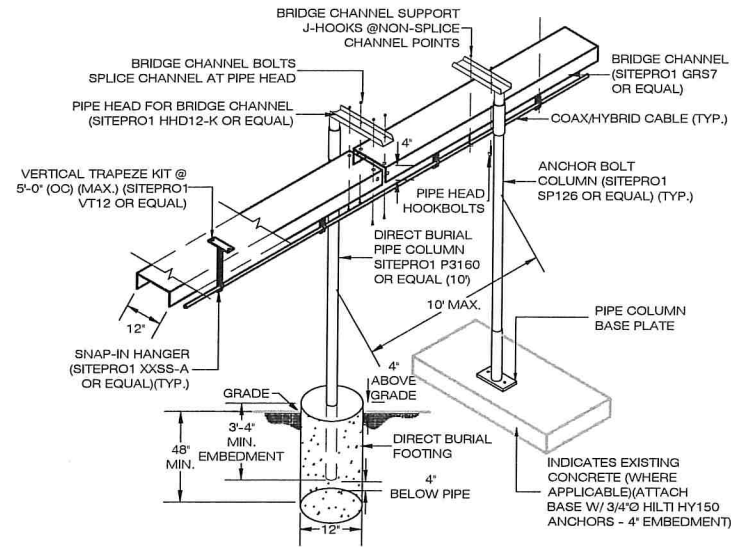


DESIGN PROFESSIONALS OF RECORD
 PROF: ROBERT C. BURNS P.E.
 COMP: ALL-POINTS TECHNOLOGY CORPORATION, P.C.
 ADD: 3 SADDLEBROOK DRIVE KILLINGWORTH, CT 06419
 OWNER: THE CONNECTICUT WATER COMPANY
 ADDRESS: 93 WEST MAIN STREET CLINTON, CONNECTICUT 06413

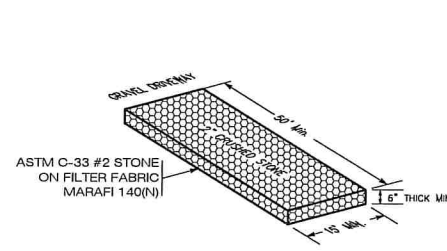
MCM SITE WESTBROOK H2O TANK
 SITE 1542 BOSTON POST ROAD
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 APT FILING NUMBER: CT524120
 DATE: 10/08/19
 DRAWN BY: CSH
 CHECKED BY: RCB

SHEET TITLE:
COMPOUND PLAN & TOWER ELEVATION

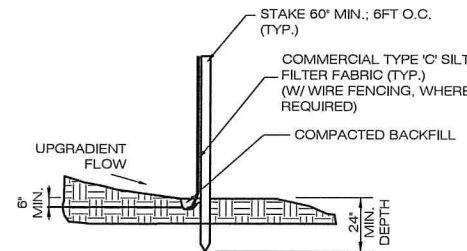
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A-1



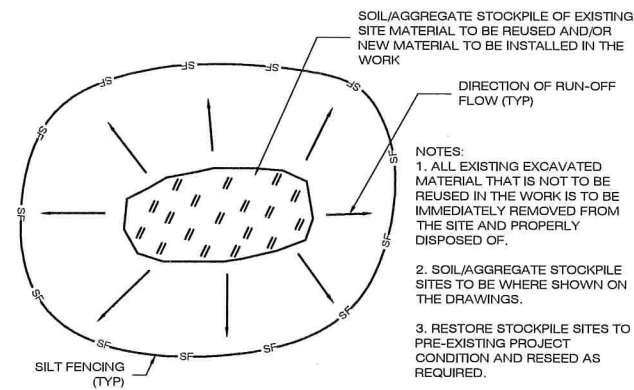
1 CABLE BRIDGE & COAX HANGER DETAIL
SCALE : N.T.S.



2 (CE) CONSTRUCTION ENTRANCE DETAIL
SCALE : N.T.S.



3 GEOTEXTILE SILT FENCE DETAIL
SCALE : N.T.S.



4 TEMPORARY STOCKPILE DETAIL
SCALE : N.T.S.

Fiberglass Omnidirectional Antennas

PCTEL Heavy Duty Fiberglass Base Station Omnidirectional Antennas

The BOA omnidirectional base station antennas consist of a linear array, encapsulated in a heavy duty fiberglass radome with a thick walled 6061-T6 aluminum mounting base for reliable long term use. This rugged design allows the antennas to withstand harsh environments and is ideal for Industrial Wireless and SCADA applications. The BOA series is DC grounded and is UPS shippable.

- Features**
- UV Stable Light Gray Fiberglass Radome
 - Hard-Coat Anodized Mounting Base
 - Galvanized Mounting Hardware
 - Removable Drain Plug for Upright or Inverted Mounting

Antenna Electrical Specifications

Model	Frequency Range	Nominal Gain	Return Loss	SWR	E-Plane Beamwidth
BOA4357	430-470 MHz	7 dBi/5 dBd	12 dB	< 1.7	20°
BOA9025	902-928MHz	5.1 dBi/3 dBd	> 14 dB	< 1.5	25°
BOA9028	902-928MHz	8.1 dBi/6 dBd	> 14 dB	< 1.5	13°
BOA90211	902-928MHz	11.1 dBi/9 dBd	> 14 dB	< 1.5	6°

Mechanical Specifications

Model	Weight	Height	Bending Moment at Rated Wind	Lateral Thrust at Rated Wind	Equivalent Flat Plate Area
BOA4357	7.0 lbs	81"	250 ft-lbs	45 lbs	1.125 ft²
BOA9025	5.0 lbs	55"	106 ft-lbs	29 lbs	0.77 ft²
BOA9028	6.0 lbs	68"	178 ft-lbs	38 lbs	0.95 ft²
BOA90211	10.0 lbs	122"	685 ft-lbs	74 lbs	1.7 ft²

Technical Data

Maximum Power:	250 watts
Nominal Impedance:	50 ohms
Radome Material:	Pultruded fiberglass
ESD Protection:	DC grounded
Rated Wind:	125 mph
Termination:	N female bulkhead
Mounting Hardware:	BWC1005 (included)

©2010 PCTEL, Inc. Product specifications are subject to change without notice.

PCTEL, Inc.

WEB: www.antenna.com

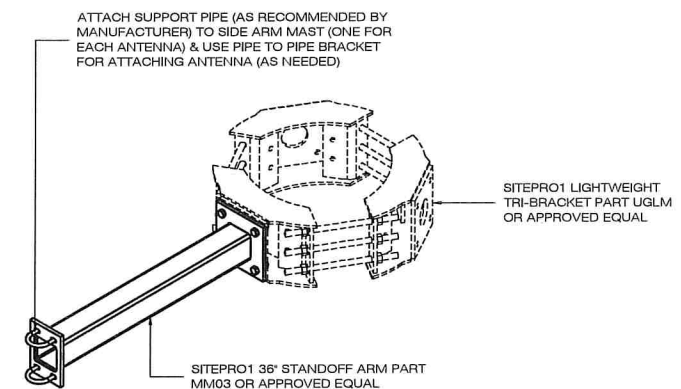
5 MUNICIPAL OMNI ANTENNA
SCALE : N.T.S.

CONSTRUCTION SEQUENCING

CONTRACTOR TO FOLLOW THE FOLLOWING CONSTRUCTION PHASING AS CLOSELY AS POSSIBLE:

1. MOBILIZATION: BRING MATERIAL AND EQUIPMENT TO SITE. ALL CONSTRUCTION TRAFFIC AND ACTIVITIES MUST RESIDE INSIDE ACCESS PATH DELINEATED, WITHIN STAGING AND STOCKPILE AREA, OR WITHIN AREA WHERE PROPOSED WORK IS BEING COMPLETED. THE CONTRACTOR IS TO PROTECT WETLANDS FROM DISTURBANCE AT ALL TIMES AND NO CONSTRUCTION ACTIVITIES OR DUMPING SHALL OCCUR IN THE WETLANDS. HOURS OF CONSTRUCTION ARE 8 AM - 6 PM, MONDAY - SATURDAY.
2. THE CONTRACTOR SHALL HOST AND ATTEND AN ENVIRONMENTAL EDUCATION SESSION AT THE PRE-CONSTRUCTION MEETING (SEE NOTES ON DRAWING N-1).
3. INSTALL TEMPORARY EROSION AND SEDIMENTATION CONTROL AND ISOLATION BARRIERS.
4. INSTALL CONSTRUCTION ENTRANCE.
5. EXCAVATE FOR TOWER FOUNDATION.
6. INSTALL BURIED GROUND RINGS, GROUND RODS & GROUND LEADS.
7. BACKFILL TOWER FOUNDATION.
8. ERECT MONOPOLE.
9. INSTALL TELECOMMUNICATIONS EQUIPMENT ON TOWER & CONNECT TO EXIST. EQUIPMENT AREAS.
10. CONNECT GROUNDING LEADS AND LIGHTENING PROTECTION.
11. REMOVE TEMPORARY TOWER.
12. FINAL GRADE AROUND COMPOUND.
13. LOAM AND SEED DISTURBED AREAS OUTSIDE COMPOUND, AS REQUIRED.
14. REMOVE TEMPORARY EROSION & SEDIMENTATION CONTROL BARRIER AFTER SEEDED AREAS HAVE ESTABLISHED VEGETATION.
15. FINAL CLEANUP AND EQUIPMENT TESTING.

THE ESTIMATED TIME FOR COMPLETION OF THE WORK IS APPROXIMATELY FOUR (4) WEEKS. THE EXACT PROCESS MAY VARY DEPENDING ON THE CONTRACTORS' AND SUBCONTRACTORS AVAILABILITY TO COMPLETE WORK AND WEATHER DELAYS.



NOTE: CONTRACTOR TO COORDINATE WITH ANTENNA MANUFACTURERS FOR PROPER ANTENNA MOUNTING PROCEDURES.

6 3' SIDEARM ANTENNA MOUNT
SCALE : N.T.S.

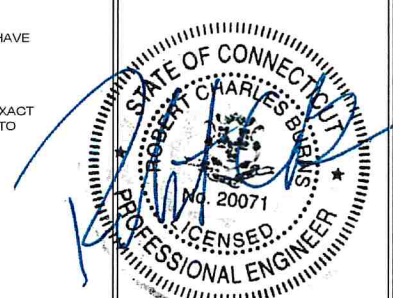
MCM HOLDINGS, LLC
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DESIGN PROFESSIONALS OF RECORD

PROF: ROBERT C. BURNS P.E.
COMP: ALL-POINTS TECHNOLOGY CORPORATION, P.C.
ADD: 3 SADDLEBROOK DRIVE
KILLINGWORTH, CT 06419

OWNER: THE CONNECTICUT WATER COMPANY
ADDRESS: 93 WEST MAIN STREET
CLINTON, CONNECTICUT 06413

MCM SITE WESTBROOK H2O TANK

SITE 1542 BOSTON POST ROAD
ADDRESS: WESTBROOK, CT 06498

APT FILING NUMBER: CT524120

DRAWN BY: CSH
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SHEET TITLE:

SITE DETAILS

SHEET NUMBER:

C-1

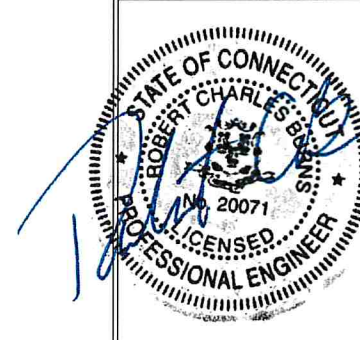
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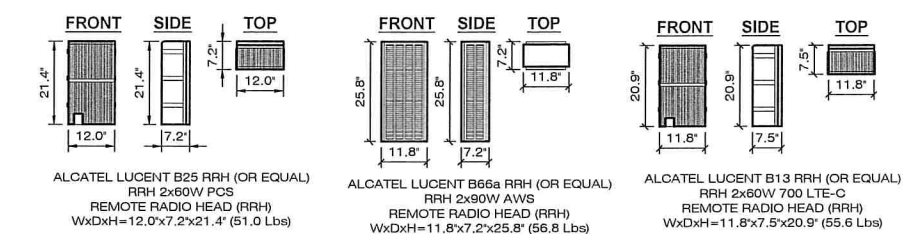
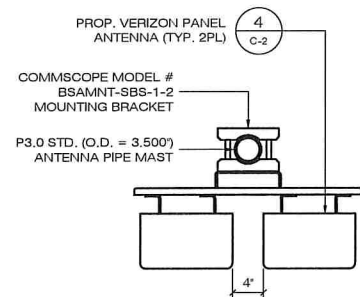
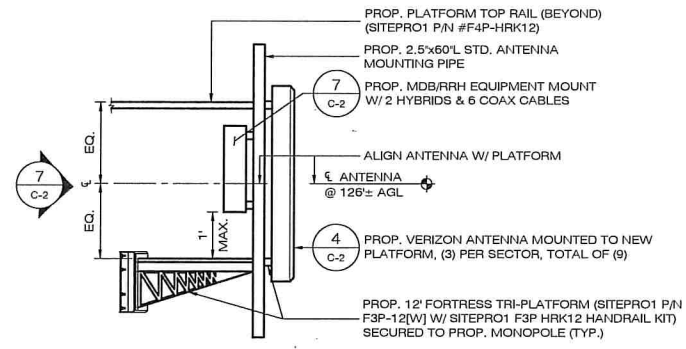
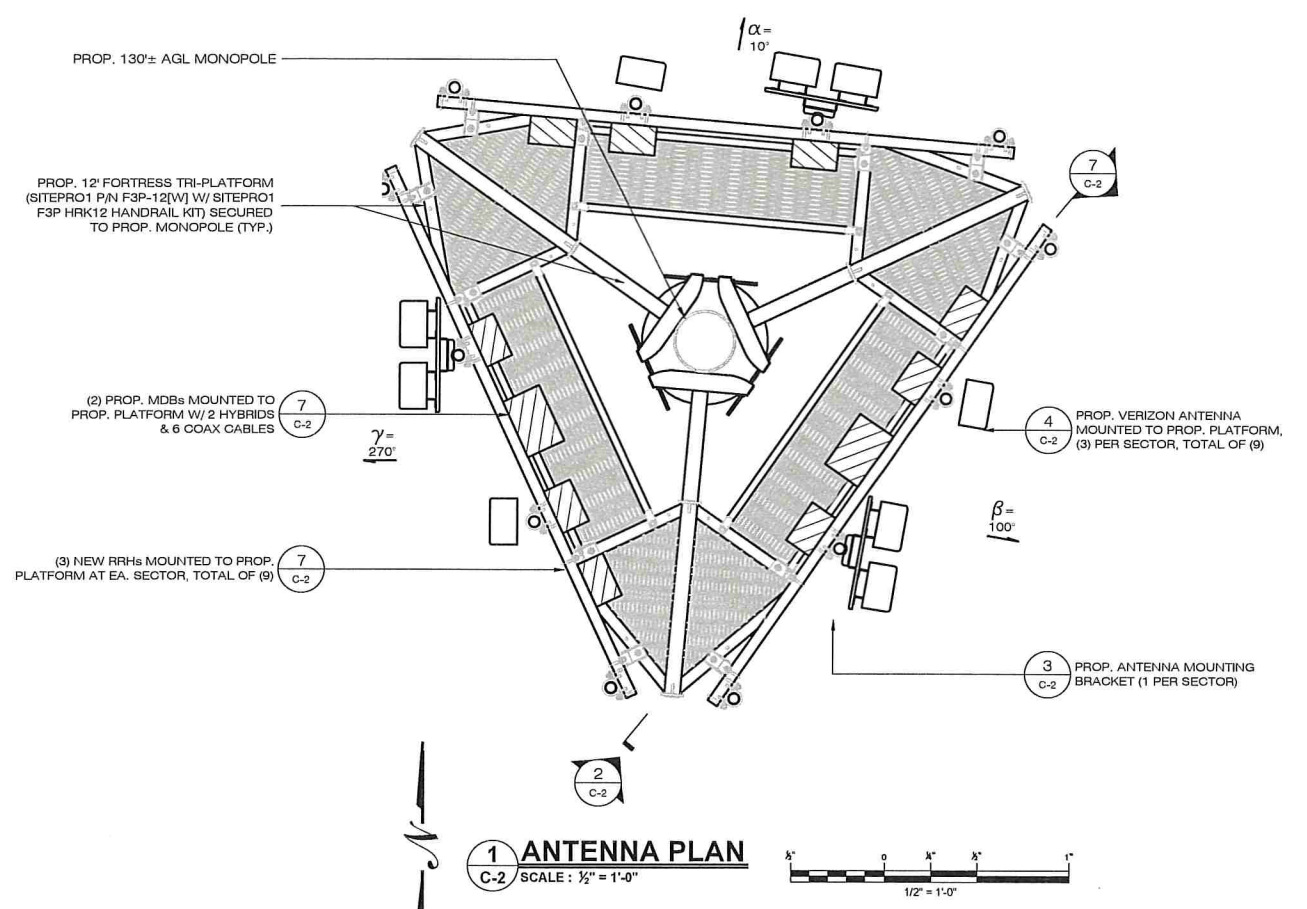
DATE: 10/08/19 CHECKED BY: RCB

SHEET TITLE:

VERIZON ANTENNA PLAN & DETAILS

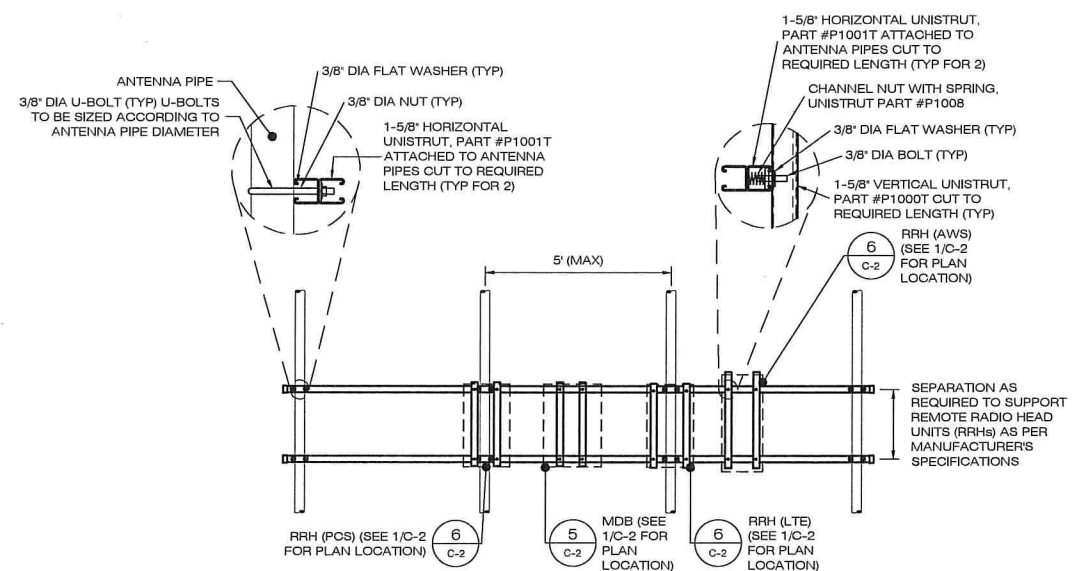
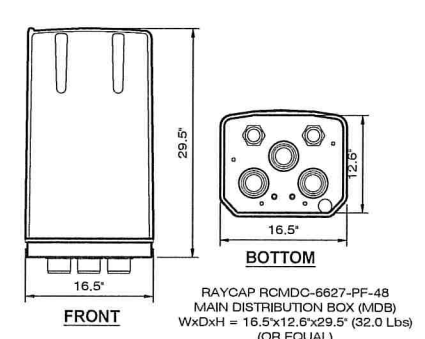
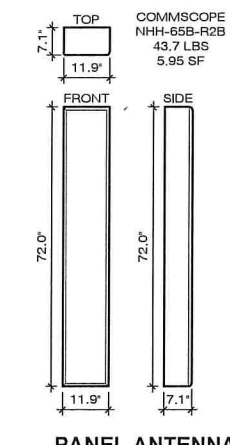
SHEET NUMBER:

C-2



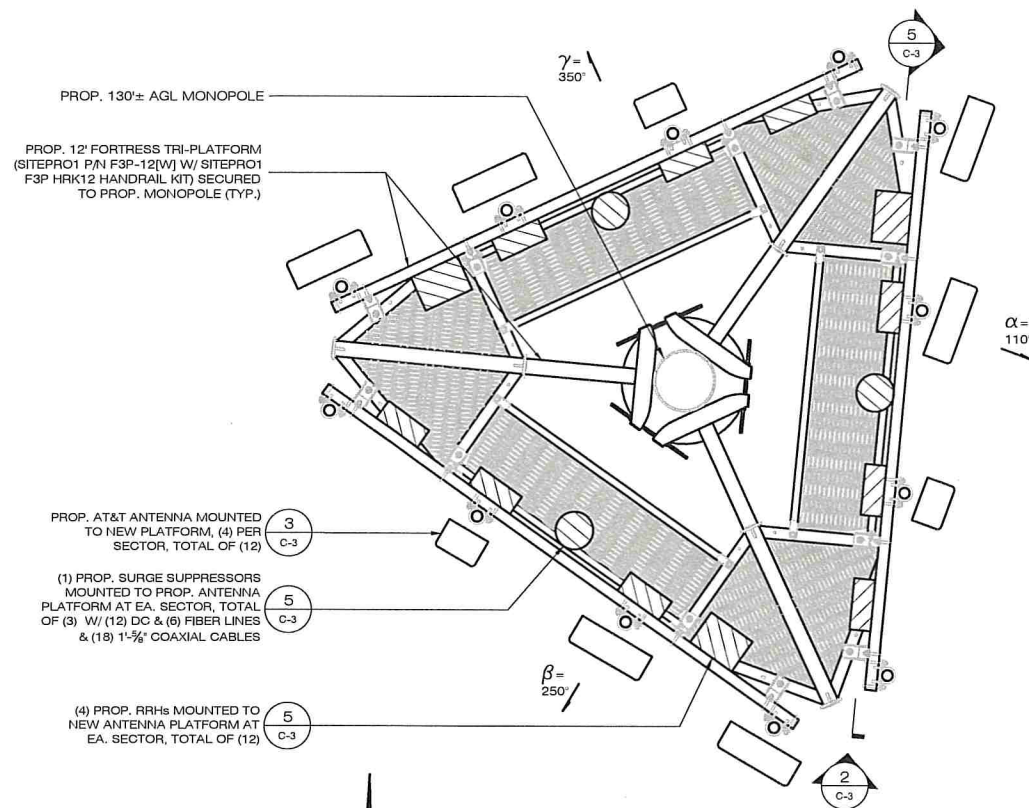
- NOTES:**
- DIMENSIONS SUBJECT TO CHANGE BASED UPON AVAILABILITY AT TIME OF CONSTRUCTION.
 - MANUFACTURER'S RECOMMENDED RRH CLEARANCES: FRONT: 36"; SIDES: 12"; BOTTOM: 24".
 - SFPs ARE PROTOCOL SPECIFIC. THE CONNECTIONS BETWEEN RRHS AND BBUS ARE CPRI CONNECTIONS, AND REQUIRE CPRI SFP (ON BOTH ENDS). THE CONNECTIONS BETWEEN BBUS AND 7705 ARE ETHERNET AND REQUIRE ETHERNET SFP (ON BOTH ENDS).

NOTE:
1) RRH=REMOTE RADIO HEAD
2) MDB=MAIN DISTRIBUTION BOX

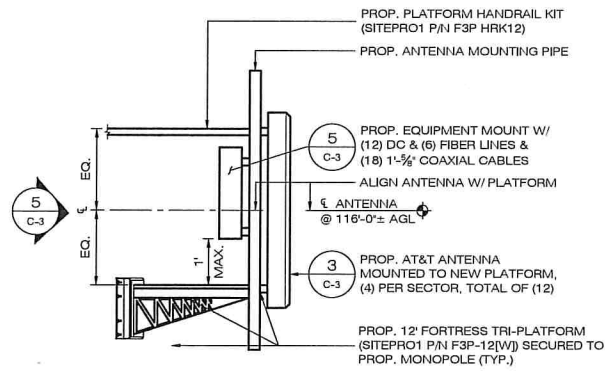


- NOTES:**
- ALL EXPOSED UNISTRUT ENDS TO BE CAPPED WITH UNISTRUT CAP (MODEL #P2860-10)
 - ONLY 1-5/8" UNISTRUT TO BE USED FOR RACK CONSTRUCTION.
 - EXTEND UNISTRUT AS NEEDED BASED ON LENGTH OF ANTENNA SECTOR. DO NOT CANTILEVER UNISTRUT FOR MORE THAN 24" BEYOND ANTENNA MAST.

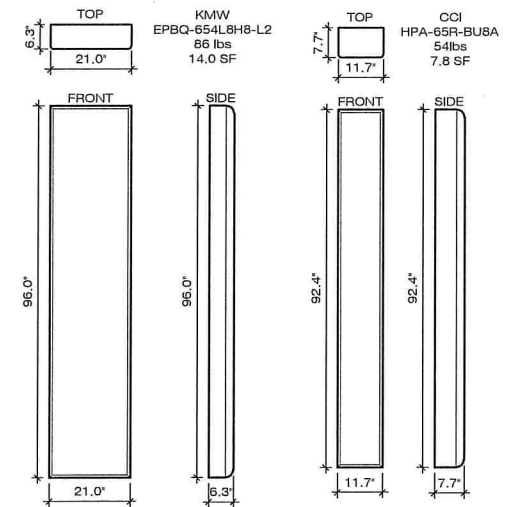
7 MDB/RRH EQUIPMENT ANTENNA MOUNT
SCALE: 1/2" = 1'-0"



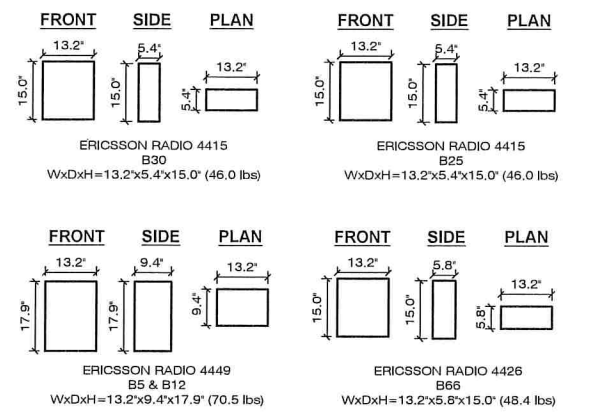
1 ANTENNA PLAN
C-3 SCALE: 1/2" = 1'-0"



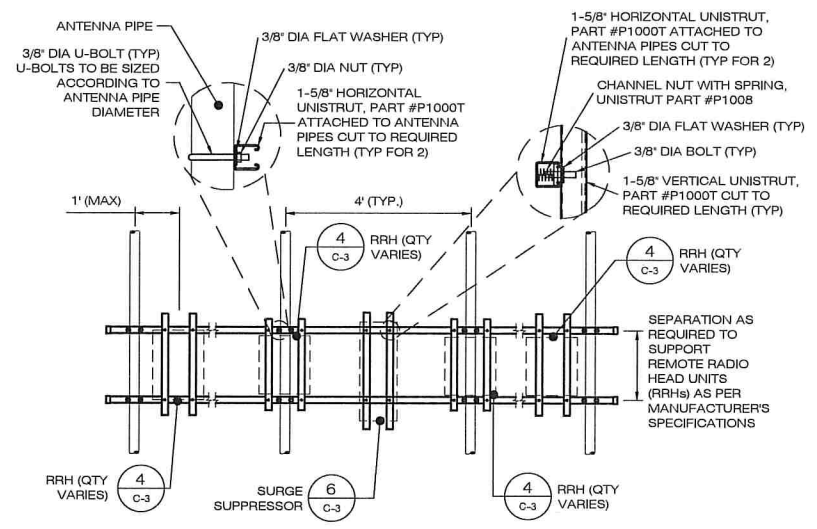
2 ANTENNA MOUNTING DETAIL
C-3 SCALE: 1/2" = 1'-0"



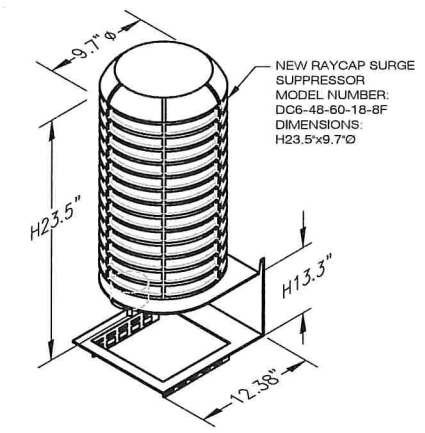
3 ANTENNA DETAIL
C-3 SCALE: 1/2" = 1'-0"



4 RRH EQUIPMENT
C-3 SCALE: 1/2" = 1'-0"



5 EQUIPMENT ANTENNA MOUNT
C-3 SCALE: 1/2" = 1'-0"



6 TYPICAL SURGE SUPPRESSOR
C-3 SCALE: N.T.S.

NOTES:
1. DIMENSIONS SUBJECT TO CHANGE BASED UPON AVAILABILITY AT TIME OF CONSTRUCTION.
2. MANUFACTURER'S RECOMMENDED RRH CLEARANCES: FRONT: 36"; SIDES: 12"; BOTTOM: 24"
3. SFPs ARE PROTOCOL SPECIFIC. THE CONNECTIONS BETWEEN RRHs AND BBUs ARE CPRI CONNECTIONS, AND REQUIRE CPRI SFP (ON BOTH ENDS). THE CONNECTIONS BETWEEN BBUs AND 7705 ARE ETHERNET AND REQUIRE ETHERNET SFP (ON BOTH ENDS).

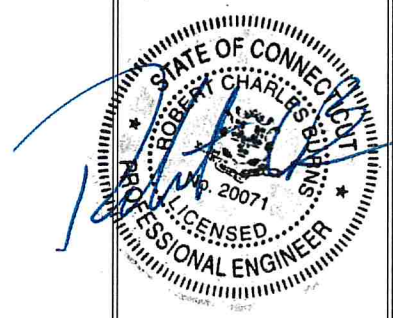
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4. FOR SPANS GREATER THAN 5'-0" USE UNISTRUT PART #P1001T.

RAYCAP DC6-48-60-18-8F SURGE SUPPRESSOR
HxDia. = 23.5"x9.7"
(20.0 lbs W/O MOUNTING BRACKET)
(OR EQUAL)
COLOR: GRAY
NOTE: MOUNT PER MANUFACTURER'S SPECIFICATIONS.

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HARTFORD, CT 06132
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KILLINGWORTH, CT 06419 FAX: (860)-663-0935
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COMP: ALL-POINTS TECHNOLOGY CORPORATION, P.C.
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KILLINGWORTH, CT 06419
OWNER: THE CONNECTICUT WATER COMPANY
ADDRESS: 93 WEST MAIN STREET
CLINTON, CONNECTICUT 06413

MCM SITE
WESTBROOK H2O TANK
SITE 1542 BOSTON POST ROAD
ADDRESS: WESTBROOK, CT 06498
APT FILING NUMBER: CT524120
DRAWN BY: CSH
DATE: 10/08/19 CHECKED BY: RCB

SHEET TITLE:
AT&T ANTENNA PLAN & DETAILS

SHEET NUMBER:
C-3

DEVELOPMENT & MANAGEMENT PLANS	
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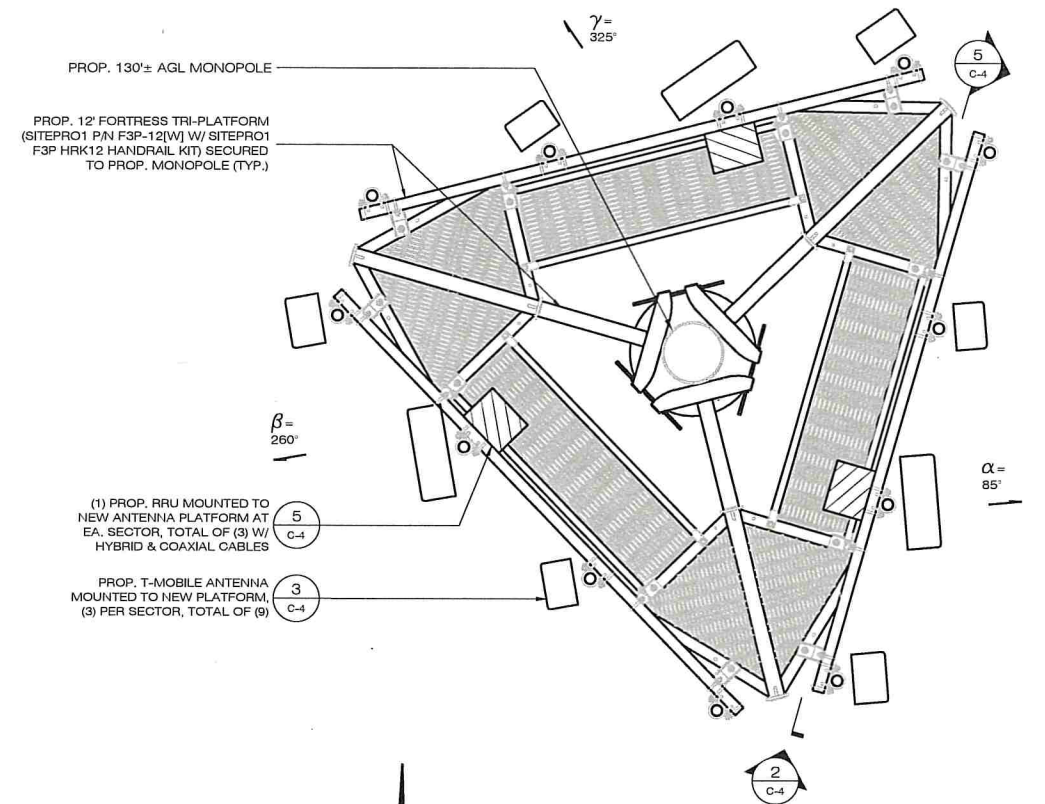
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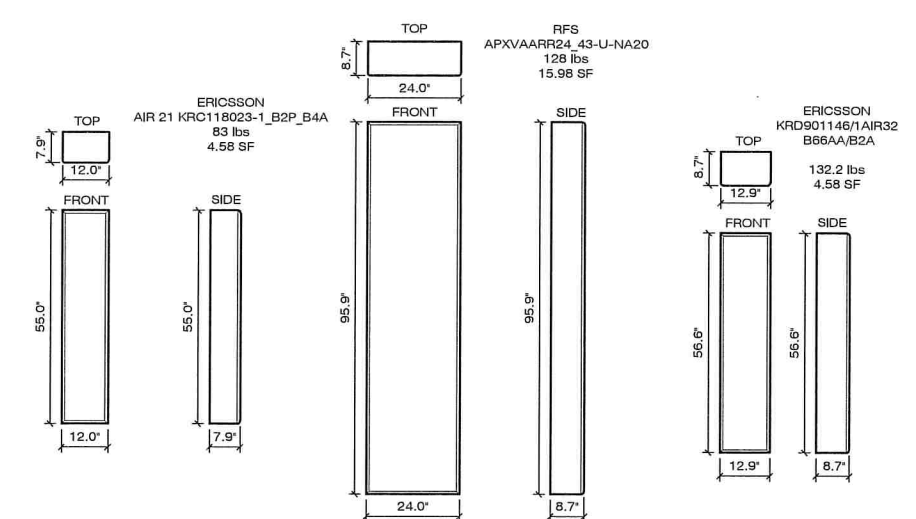
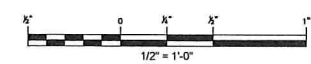
**T-MOBILE ANTENNA
PLAN & DETAILS**

SHEET NUMBER:

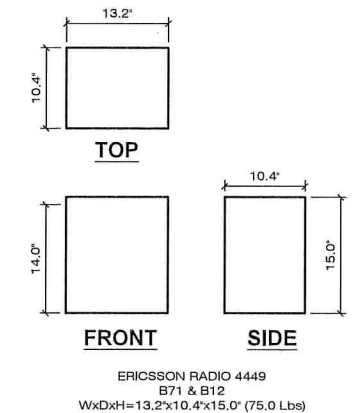
C-4



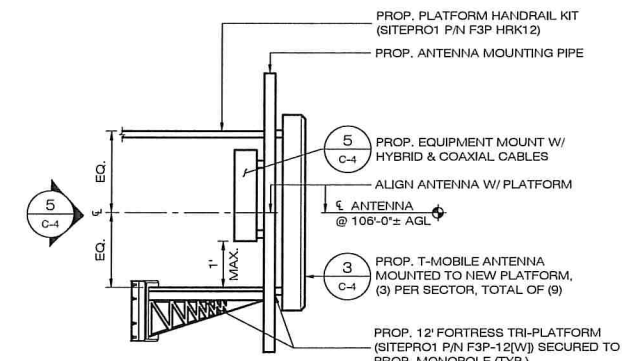
1 ANTENNA PLAN
C-4 SCALE: 1/2" = 1'-0"



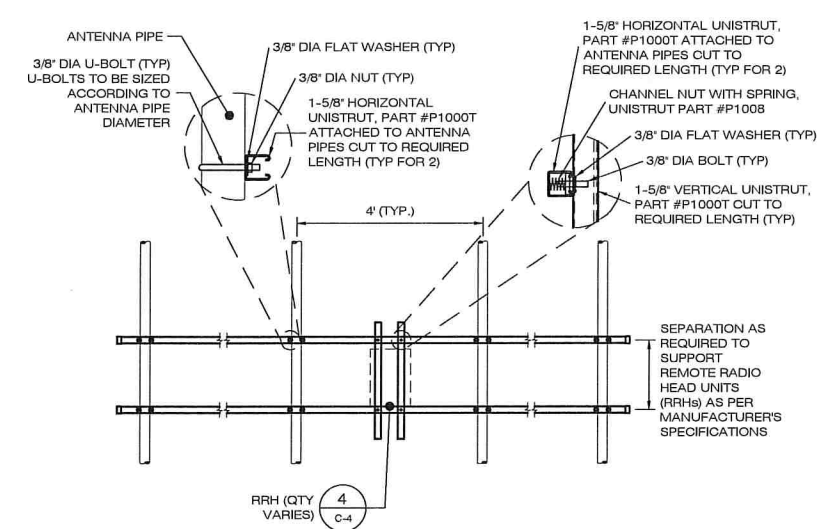
PANEL ANTENNAS
3 ANTENNA DETAIL
C-4 SCALE: 1/2" = 1'-0"



4 RRU EQUIPMENT
C-4 SCALE: 1" = 1'-0"



2 ANTENNA MOUNTING DETAIL
C-4 SCALE: 1/2" = 1'-0"



- NOTES:**
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5 EQUIPMENT ANTENNA MOUNT
C-4 SCALE: 1/2" = 1'-0"

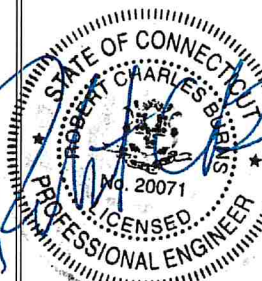
MCM HOLDINGS, LLC
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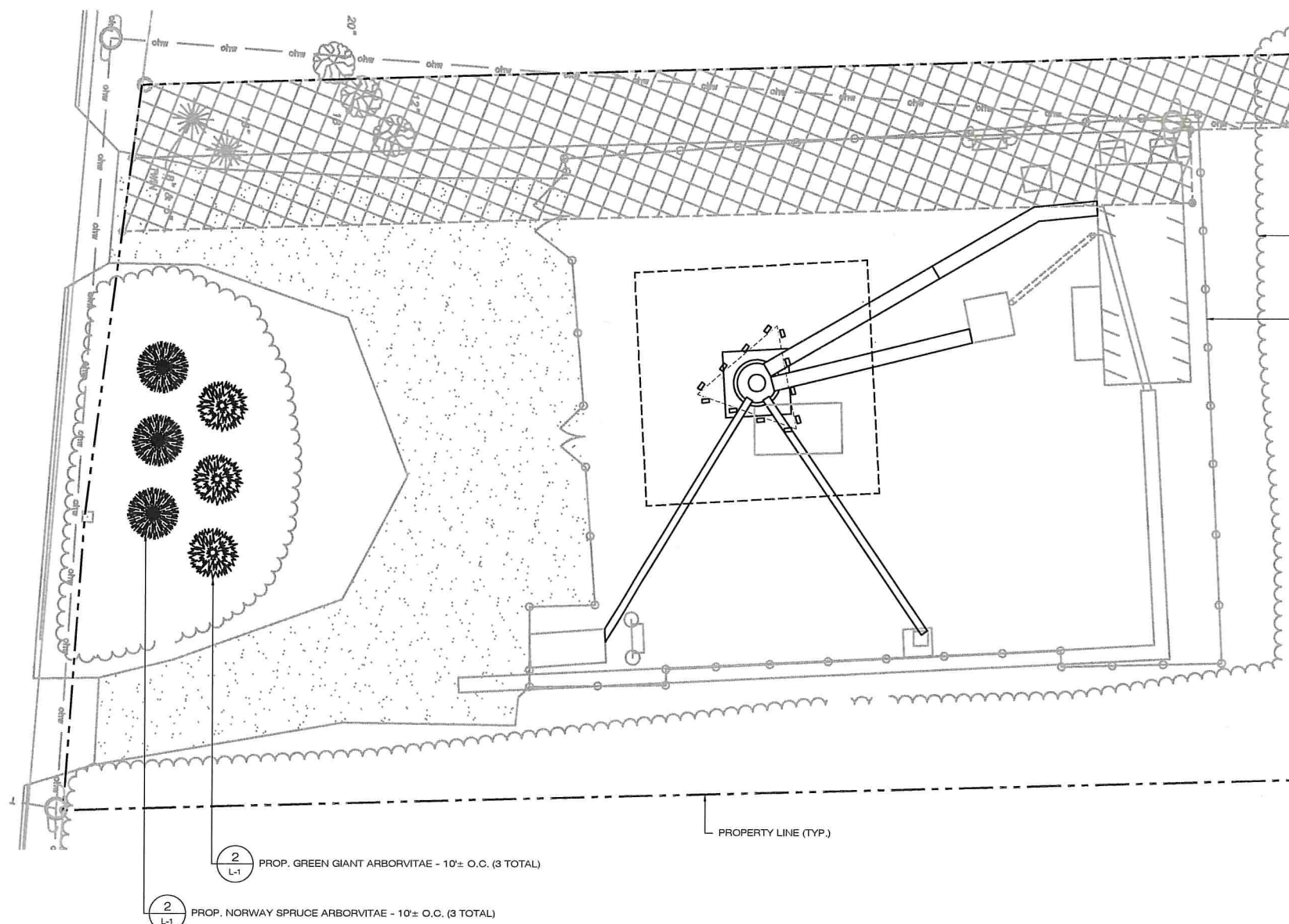
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LANDSCAPING PLAN

SHEET NUMBER:

L-1

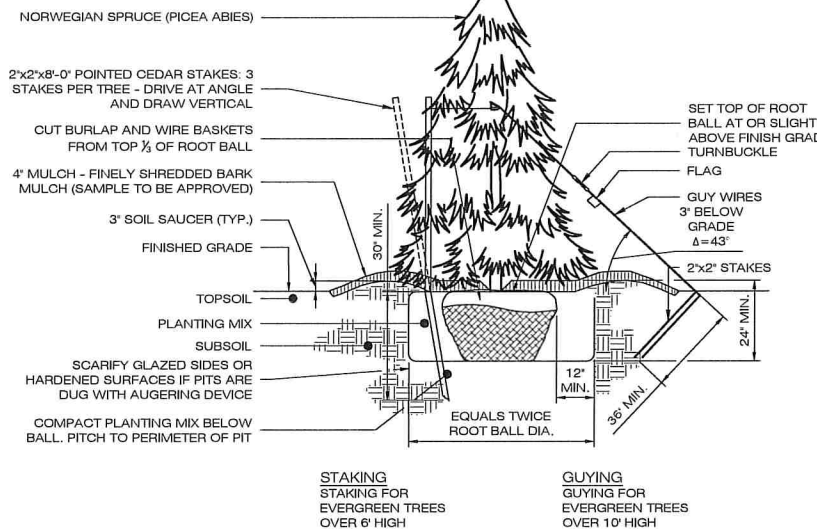
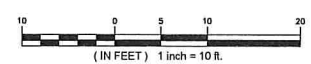


2 L-1 PROP. GREEN GIANT ARBORVITAE - 10± O.C. (3 TOTAL)

2 L-1 PROP. NORWAY SPRUCE ARBORVITAE - 10± O.C. (3 TOTAL)



1 LANDSCAPING PLAN
SCALE: 1" = 10'-0"



2 EVERGREEN TREE PLANTING
SCALE: N.T.S.

ENVIRONMENTAL NOTES

WETLAND PROTECTION PROGRAM

PORTIONS OF THE PROPOSED MCM HOLDINGS, LLC ("MCM") WESTBROOK CT H2O TANK FACILITY'S COMPOUND ARE LOCATED IN CLOSE PROXIMITY (±10 FEET) TO A WETLAND AREA. AS A RESULT, THE FOLLOWING PROTECTIVE MEASURES SHALL BE FOLLOWED TO HELP AVOID DEGRADATION OF THE NEARBY WETLAND SYSTEM.

IT IS OF THE UTMOST IMPORTANCE THAT THE CONTRACTOR COMPLIES WITH THE REQUIREMENT FOR THE INSTALLATION OF WETLAND PROTECTIVE MEASURES AND THE EDUCATION OF ITS EMPLOYEES AND SUBCONTRACTORS PERFORMING WORK ON THE PROJECT SITE. THIS PROTECTION PROGRAM SHALL BE IMPLEMENTED REGARDLESS OF TIME OF YEAR THE CONSTRUCTION ACTIVITIES OCCUR. ALL-POINTS TECHNOLOGY CORPORATION, P.C. ("APT") WILL SERVE AS THE ENVIRONMENTAL MONITOR FOR THIS PROJECT TO ENSURE THAT WETLAND PROTECTION MEASURES ARE IMPLEMENTED PROPERLY. THE CONTRACTOR SHALL CONTACT DEAN GUSTAFSON, SENIOR ENVIRONMENTAL SCIENTIST AT APT, AT LEAST 5 BUSINESS DAYS PRIOR TO THE PRE-CONSTRUCTION MEETING. MR. GUSTAFSON CAN BE REACHED BY PHONE AT (860) 663-1697 EXT. 201 OR VIA EMAIL AT DGUSTAFSON@ALLPOINTSTECH.COM.

THE WETLAND PROTECTION PROGRAM CONSISTS OF SEVERAL COMPONENTS: USE OF APPROPRIATE EROSION CONTROL MEASURES TO CONTROL AND CONTAIN EROSION WHILE AVOIDING/MINIMIZING WILDLIFE ENTANGLEMENT; PERIODIC INSPECTION AND MAINTENANCE OF ISOLATION STRUCTURES AND EROSION CONTROL MEASURES; EDUCATION OF ALL CONTRACTORS AND SUB-CONTRACTORS PRIOR TO INITIATION OF WORK ON THE SITE; PROTECTIVE MEASURES; AND, REPORTING.

1. CONTRACTOR EDUCATION

- A. PRIOR TO WORK ON SITE, THE CONTRACTOR SHALL ATTEND AN EDUCATIONAL SESSION AT THE PRE-CONSTRUCTION MEETING WITH THE ENVIRONMENTAL MONITOR. THIS ORIENTATION AND EDUCATIONAL SESSION WILL CONSIST OF AN INTRODUCTORY MEETING WITH THE ENVIRONMENTAL MONITOR TO UNDERSTAND THE ENVIRONMENTALLY SENSITIVE NATURE OF THE DEVELOPMENT SITE AND THE NEED TO FOLLOW THESE WETLAND PROTECTION PLAN MEASURES.
- B. THE CONTRACTOR WILL BE PROVIDED WITH CELL PHONE AND EMAIL CONTACTS FOR THE ENVIRONMENTAL MONITOR TO IMMEDIATELY REPORT ANY RELEASES OF SEDIMENT INTO NEARBY WETLANDS.

2. EROSION AND SEDIMENTATION CONTROLS

- A. THE EXTENT OF THE BARRIER FENCING WILL BE AS SHOWN ON THE SITE PLANS. THE CONTRACTOR SHALL HAVE ADDITIONAL BARRIER FENCING SHOULD FIELD CONDITIONS WARRANT EXTENDING THE FENCING AS DIRECTED BY THE ENVIRONMENTAL MONITOR.
- B. PLASTIC NETTING USED IN A VARIETY OF EROSION CONTROL PRODUCTS (I.E., EROSION CONTROL BLANKETS, FIBER ROLLS (WATTLES), REINFORCED SILT FENCE) HAS BEEN FOUND TO ENTANGLE WILDLIFE, INCLUDING REPTILES, AMPHIBIANS, BIRDS AND SMALL MAMMALS. NO PERMANENT EROSION CONTROL PRODUCTS OR REINFORCED SILT FENCE WILL BE USED ON THE MCM PROJECT. TEMPORARY EROSION CONTROL PRODUCTS THAT WILL BE EXPOSED AT THE GROUND SURFACE REPRESENT A POTENTIAL FOR WILDLIFE ENTANGLEMENT WILL USE EITHER EROSION CONTROL BLANKETS AND FIBER ROLLS COMPOSED OF PROCESSED FIBERS MECHANICALLY BOUND TOGETHER TO FORM A CONTINUOUS MATRIX (NETLESS) OR NETTING WITH A MESH SIZE <1/8" SUCH AS THAT TYPICALLY USED IN COMPOST FILTER SOCKS TO AVOID/MINIMIZE WILDLIFE ENTANGLEMENT.
- C. INSTALLATION OF CONVENTIONAL SILT FENCING SHALL BE PERFORMED BY THE CONTRACTOR PRIOR TO ANY EARTHWORK. THE ENVIRONMENTAL MONITOR WILL INSPECT THE WORK ZONE AREA FOLLOWING BARRIER INSTALLATION TO ENSURE EROSION CONTROLS ARE PROPERLY INSTALLED.
- D. THE FENCING WILL CONSIST OF NON-REINFORCED CONVENTIONAL EROSION CONTROL WOVEN FABRIC, INSTALLED APPROXIMATELY SIX INCHES BELOW SURFACE GRADE AND STAKED AT SEVEN TO TEN-FOOT INTERVALS USING FOUR-FOOT OAK STAKES OR APPROVED EQUIVALENT.
- E. IN ADDITION TO REQUIRED DAILY INSPECTION BY THE CONTRACTOR, THE FENCING WILL BE INSPECTED BY THE CONTRACTOR FOR TEARS OR BREECHEES IN THE FABRIC FOLLOWING INSTALLATION AND FOLLOWING STORM EVENTS THAT PRODUCE A DISCHARGE. INSPECTIONS WILL BE CONDUCTED PERIODICALLY BY THE ENVIRONMENTAL MONITOR THROUGHOUT THE COURSE OF THE CONSTRUCTION PROJECT.
- F. ALL SILT FENCING AND OTHER EROSION CONTROL DEVICES SHALL BE REMOVED WITHIN 30 DAYS OF COMPLETION OF WORK AND PERMANENT STABILIZATION OF SITE SOILS SO THAT POSSIBLE REPTILE AND AMPHIBIAN MOVEMENT BETWEEN UPLANDS AND WETLANDS IS NOT RESTRICTED. IF FIBER ROLLS/WATTLES, STRAW BALES, OR OTHER NATURAL MATERIAL EROSION CONTROL PRODUCTS ARE USED, SUCH DEVICES WILL NOT BE LEFT IN PLACE TO BIODEGRADE AND SHALL BE PROMPTLY REMOVED AFTER SOILS ARE STABLE SO AS NOT TO CREATE A BARRIER TO MIGRATING WILDLIFE. SEED FROM SEEDING OF SOILS SHALL NOT BE SPREAD OVER FIBER ROLLS/WATTLES AS IT MAKES THEM HARDER TO REMOVE ONCE SOILS ARE STABILIZED BY VEGETATION.

3. PETROLEUM MATERIALS STORAGE AND SPILL PREVENTION

- A. CERTAIN PRECAUTIONS ARE NECESSARY TO STORE PETROLEUM MATERIALS, REFUEL AND CONTAIN AND PROPERLY CLEAN UP ANY INADVERTENT FUEL OR PETROLEUM (I.E., OIL, HYDRAULIC FLUID, ETC.) SPILL DUE TO THE PROJECT'S LOCATION IN PROXIMITY TO SENSITIVE WETLANDS.
- B. A SPILL CONTAINMENT KIT CONSISTING OF A SUFFICIENT SUPPLY OF ABSORBENT PADS AND ABSORBENT MATERIAL SHALL BE MAINTAINED BY THE CONTRACTOR AT THE CONSTRUCTION SITE THROUGHOUT THE DURATION OF THE PROJECT. IN ADDITION, A WASTE DRUM SHALL BE KEPT ON SITE BY THE CONTRACTOR TO CONTAIN ANY USED ABSORBENT PADS/MATERIAL FOR PROPER AND TIMELY DISPOSAL OFF SITE IN ACCORDANCE WITH APPLICABLE LOCAL, STATE AND FEDERAL LAWS.
- C. THE FOLLOWING PETROLEUM AND HAZARDOUS MATERIALS STORAGE AND REFUELING RESTRICTIONS AND SPILL RESPONSE PROCEDURES WILL BE ADHERED TO BY THE CONTRACTOR.
 - I. PETROLEUM AND HAZARDOUS MATERIALS STORAGE AND REFUELING
 - a. REFUELING OF VEHICLES OR MACHINERY SHALL OCCUR A MINIMUM OF 100 FEET FROM WETLANDS OR WATERCOURSES AND SHALL TAKE PLACE ON AN IMPERVIOUS PAD WITH SECONDARY CONTAINMENT DESIGNED TO CONTAIN FUELS.
 - b. ANY FUEL OR HAZARDOUS MATERIALS THAT MUST BE KEPT ON SITE SHALL BE STORED ON AN IMPERVIOUS SURFACE UTILIZING SECONDARY CONTAINMENT A MINIMUM OF 100 FEET FROM WETLANDS OR WATERCOURSES.
 - II. INITIAL SPILL RESPONSE PROCEDURES
 - a. STOP OPERATIONS AND SHUT OFF EQUIPMENT.
 - b. REMOVE ANY SOURCES OF SPARK OR FLAME.
 - c. CONTAIN THE SOURCE OF THE SPILL.
 - d. DETERMINE THE APPROXIMATE VOLUME OF THE SPILL.
 - e. IDENTIFY THE LOCATION OF NATURAL FLOW PATHS TO PREVENT THE RELEASE OF THE SPILL TO SENSITIVE NEARBY WATERWAYS OR WETLANDS.
 - f. ENSURE THAT FELLOW WORKERS ARE NOTIFIED OF THE SPILL.
 - III. SPILL CLEAN UP & CONTAINMENT
 - a. OBTAIN SPILL RESPONSE MATERIALS FROM THE ON-SITE SPILL RESPONSE KIT. PLACE ABSORBENT MATERIALS DIRECTLY ON THE RELEASE AREA.
 - b. LIMIT THE SPREAD OF THE SPILL BY PLACING ABSORBENT MATERIALS AROUND THE PERIMETER OF THE SPILL.
 - c. ISOLATE AND ELIMINATE THE SPILL SOURCE.
 - d. CONTACT THE APPROPRIATE LOCAL, STATE AND/OR FEDERAL AGENCIES, AS NECESSARY.
 - e. CONTACT A DISPOSAL COMPANY TO PROPERLY DISPOSE OF CONTAMINATED MATERIALS IN ACCORDANCE WITH ALL LOCAL, STATE AND FEDERAL REGULATIONS.
 - IV. REPORTING
 - a. CONTRACTOR SHALL COMPLETE AN INCIDENT REPORT.
 - b. CONTRACTOR SHALL SUBMIT A COMPLETED INCIDENT REPORT TO APPROPRIATE LOCAL, STATE AND/OR FEDERAL AGENCIES, AS NECESSARY.
4. HERBICIDE AND PESTICIDE RESTRICTIONS
 - A. THE USE OF HERBICIDES AND PESTICIDES AT THE PROPOSED WIRELESS TELECOMMUNICATIONS FACILITY SHALL BE AVOIDED WHEN POSSIBLE. IN THE EVENT HERBICIDES AND/OR PESTICIDES ARE REQUIRED AT THE PROPOSED FACILITY, THEIR USE WILL BE USED IN ACCORDANCE WITH INTEGRATED PEST MANAGEMENT ("IPM") PRINCIPLES WITH PARTICULAR ATTENTION TO MINIMIZE APPLICATIONS WITHIN 100 FEET OF WETLAND OR WATERCOURSE RESOURCES. NO APPLICATIONS OF HERBICIDES OR PESTICIDES ARE ALLOWED WITHIN ACTUAL WETLAND OR WATERCOURSE RESOURCES.
6. REPORTING
 - A. INSPECTION REPORTS (BRIEF NARRATIVE AND APPLICABLE PHOTOS) WILL BE PREPARED BY THE ENVIRONMENTAL MONITOR DOCUMENTING EACH INSPECTION AND SUBMITTED TO MCM FOR COMPLIANCE VERIFICATION. ANY NON-COMPLIANCE OBSERVATIONS OF EROSION CONTROL MEASURES OR EVIDENCE OF EROSION OR SEDIMENT RELEASE WILL BE IMMEDIATELY REPORTED TO THE CONTRACTOR AND MCM'S CONSTRUCTION MANAGER AND INCLUDED IN THE REPORTS.
 - B. ANY INCIDENTS OF SEDIMENT RELEASE INTO WETLAND RESOURCE AREAS SHALL BE REPORTED WITHIN 24 HOURS BY MCM TO THE TOWN OF WESTBROOK INLAND WETLAND AGENT.
 - C. ANY OBSERVATIONS OF RARE SPECIES WILL BE REPORTED TO THE CONNECTICUT DEPARTMENT OF ENERGY & ENVIRONMENTAL PROTECTION NATURAL DIVERSITY DATA BASE.
 - D. FOLLOWING COMPLETION OF THE PROJECT, A SUMMARY REPORT WILL BE PREPARED BY THE ENVIRONMENTAL MONITOR DOCUMENTING COMPLIANCE WITH THE WETLAND PROTECTION PLAN AND SUBMITTED TO MCM FOR SUBMISSION TO THE CONNECTICUT SITING COUNCIL.



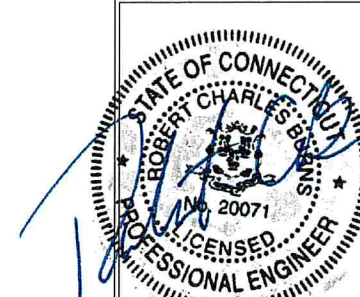
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DESIGN PROFESSIONALS OF RECORD

PROF: ROBERT C. BURNS P.E.
COMP: ALL-POINTS TECHNOLOGY CORPORATION, P.C.
ADD: 3 SADDLEBROOK DRIVE
KILLINGWORTH, CT 06419

OWNER: THE CONNECTICUT WATER COMPANY
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MCM SITE WESTBROOK H2O TANK

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SHEET TITLE:
ENVIRONMENTAL NOTES

SHEET NUMBER:
N-1

2

Geotechnical Engineering Report

**Proposed Telecommunications Towers: Westbrook H2O
1542 Boston Post Road
Westbrook, Connecticut**

FOR

**All-Points Technology Corporation, P.C.
3 Saddlebrook Drive
Killingworth, CT 06419**

BY

**NOBIS ENGINEERING, INC.
122 CHURCH STREET
NAUGATUCK, CT 06770**

(203) 409-1292
www.nobiseng.com

**Nobis Project No. 92790.00
MARCH 18, 2017**



Engineering a Sustainable Future

March 18, 2017
File No. 92790.00

All-Points Technology Corporation, P.C.
Mr. Scott M. Chasse, P.E.
3 Saddlebrook Drive
Killingworth, CT 06419

Re: Transmittal of Geotechnical Engineering Report
Proposed Telecommunications Towers: Westbrook H2O
1542 Boston Post Road, Westbrook, Connecticut

Dear Scott:

This report provides the results of Nobis Engineering Inc.'s (Nobis') geotechnical engineering review for the proposed telecommunications towers to be located at 1592 Boston Post Road in Westbrook, Connecticut. Our services were performed in general accordance with our January 8, 2017, *Geotechnical Engineering Services Proposal*. This report provides geotechnical recommendations for earthwork and foundation design for the proposed permanent and temporary tower. The results of our field exploration program and geotechnical analyses are provided herein.

We appreciate the opportunity to work with you. Please call if you have any questions.

Sincerely,

NOBIS ENGINEERING, INC.

A handwritten signature in blue ink, appearing to read "Raymond P. Janeiro".

Raymond P. Janeiro, PE
Project Manager

A handwritten signature in blue ink, appearing to read "Scott M. Carter".

Scott M. Carter, PE
Reviewer



Engineering a Sustainable Future

TABLE OF CONTENTS

GEOTECHNICAL ENGINEERING REPORT
PROPOSED TELECOMMUNICATIONS TOWERS: WESTBROOK H2O
1542 BOSTON POST ROAD
WESTBROOK, CONNECTICUT

NOBIS FILE NO. 92790.00

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- A Figures
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C Limitations



1.0 INTRODUCTION

Nobis Engineering, Inc. (Nobis) prepared this geotechnical engineering report for the two proposed telecommunications towers located at 1542 Boston Post Road in Westbrook, Connecticut ("Site") for All-Points Technology Corporation, P.C. ("Client"). A Site Locus Plan is included as **Figure 1 – Appendix A**.

Existing conditions and proposed features relating to Site development are generally based on the Client's provided drawings (*Westbrook H2O, 1542 Boston Post Road, Westbrook, CT, sheets LE-1 through LE-3A, prepared by All-Points Technology Corp., dated 12/22/2016*). Elevations referenced herein reference the NAVD88 datum. This report is subject to the limitations presented in **Appendix C**.

2.0 SITE AND PROJECT DESCRIPTIONS

2.1 Existing Site Conditions

The Site generally consists of an existing water tank currently mounted with telecommunications equipment. The Site is owned by the Connecticut Water Company and it is their intention to demolish the water tank. This will require temporary relocation of the existing telecommunications equipment until a permanent tower can be constructed within the footprint of the tank.

The Site is bordered by the Boston Post Road (U.S. Route 1) to the south and various commercial parcels to the east, north and west. Existing site grades appear to be relatively level in the area of existing Site improvements at about El. 47± according to the referenced drawings. Existing site conditions consist of an unpaved parking area and fenced compound around the existing tank and equipment shelters.

2.2 Proposed Construction

The project will initially consist of constructing a 165-foot temporary monopole tower supported on a 24-foot by 24-foot ballasted frame. Once the equipment is relocated and the water tank is demolished, a permanent 130-foot monopole tower will be constructed within the former tank footprint. Minor adjustments to the existing chain link fence at the perimeter of the compound will be required to accommodate the proposed improvements. It is our understanding that the existing equipment shelters will remain.



The estimated vertical load of the permanent tower is assumed to be about 30 kips, and the ballast lot for the temporary tower is proposed at 150 kips. It's anticipated that nominal cuts and fills on the order of 1-foot or less are anticipated to achieve design grade and that no significant slopes will be required. Refer to the Exploration Location Plan (**Figure 2 – Appendix A**) for additional proposed development details.

3.0 SUBSURFACE CONDITIONS

3.1 Geologic Information

We reviewed available subsurface/geological information in the vicinity of the project area (*Surficial Geologic Map of the Essex Quadrangle, Connecticut, Richard Flint, 1972* and *Bedrock Geology of the Essex Quadrangle, Lawrence Lundgren, Jr., 1964*).

The surficial material within the area of the proposed telecommunications compound is mapped as glacial till consisting of a variable mixture of gravel, sand, silt, and clay that is intermixed with cobbles and boulders. The underlying bedrock is classified as light- to dark-gray, medium-grained plagioclase-quartz gneiss (Monson Formation).

3.2 Subsurface Exploration Program

The subsurface exploration program coordinated and logged by Nobis included the observation of two test borings (NB-1 and NB-2) and three test probes (NP-1 through NP-3). The test borings and probes were completed on March 8 and 9, 2017, by New England Boring Contractors, Inc. of Derry, New Hampshire. Test borings were completed to assess in-situ soil conditions, and, if encountered, groundwater and bedrock conditions at the Site. The explorations were field located using taped measurements referencing existing site features. The approximate, as-drilled exploration locations are depicted on the attached **Figure 2, Exploration Location Plan**.

The explorations were completed using an Acker Soil Scout ATV-mounted drill rig utilizing drive and wash drilling methods to advance the test borings to a depth of approximately 36 feet (El. 11.5) below ground surface (bgs) at NB-1, and approximately 26 feet bgs (El. 21) at NB-2. Upon encountering equipment refusal at NB-1, at a depth of approximately 31 feet bgs, a rock core sample was obtained to aid in bedrock confirmation and evaluating the type and quality of bedrock. The core samples were drilled using a five foot, double-barrel, NQ-size core barrel. The



core times were recorded every foot of core length and rock quality was determined using visual classification.

The test probes were advanced using a series of 2-inch outside diameter split-spoon samplers to a depth of 6 feet bgs. The objective of the probes was to assess fill thickness, relative density, and soil consistency within the area of the proposed temporary tower.

Soil samples were obtained in the explorations by split-spoon sampling procedures in general accordance with ASTM D-1586. The split-spoon sampling procedure utilizes a standard 2-inch O.D. split-barrel sampler that is driven into the bottom of the boring with a 140-pound hammer falling a distance of 30 inches. The number of blows required to advance the sampler the middle 12-inches of a typical 24-inch penetration is recorded as the Standard Penetration Resistance Value (N). The blows are indicated on the boring log at their depth of occurrence and provide an indication of the relative consistency of the material.

3.3 Generalized Subsurface Profile

Excluding the presence of fill, the explorations were generally consistent with published geologic mapping. A silt stratum was also encountered at the northern limits of the existing compound (near an area of flagged wetlands). The generalized subsurface profile in the area of the proposed telecommunications compound, as inferred from the subsurface exploration data, is summarized as follows:

- Fill: Loose to medium dense, dark brown, silty SAND with gravel, containing very few organic fibers and wood debris (SM)
 - 1.5 to 5.5 feet thick (to about Elev. 45.5 to 42); over
- Silt (encountered in NP-1 and NP-3): Loose, black, SILT with sand, containing very few organic fibers (ML)
 - 0.5 to 1.5 feet thick (to about Elev. 44 to 43.5); over
- Glacial Till: Dense to very dense, brown, silty SAND with gravel (SM)
 - 14.5 to 16.5 feet thick (to about Elev. 28.5 to 25.5); over
- Decomposed Rock: Very dense, gray-white, well-graded SAND with gravel (SW)
 - 14 feet thick in NB-1 (to about Elev. 11.5). A core barrel was advanced within the Decomposed Rock stratum in NB-1. Bedrock was classified as soft, extremely weathered, white/gray Gneiss. The core recovery and rock quality designation (RQD), was 20% and 0%, respectively, indicating a very poor rock mass quality.



Visual classifications of soil and rock, and conditions encountered at each exploration location can be found in the provided boring and test probes logs, included as **Appendix B**.

3.4 Groundwater

Groundwater levels were measured in the boreholes at the times and under the conditions stated on the logs. Water was encountered at about 5 feet bgs (NB-1) during drilling at the permanent tower location. Water was encountered at about 4 feet bgs during probing at the temporary tower location. Groundwater could not be determined at NB-2, since drive and wash drilling methods introduced water to the borehole prior to encountering the groundwater table.

Groundwater observations were measured at the time of drilling and may not be indicative of stabilized groundwater elevation. Additionally, the drilling method utilized introduces water to the borehole which may result in an elevated groundwater measurement. Groundwater levels will vary due to seasonal factors, temperature, precipitation, construction activity and other conditions which may be different from the time of the exploration program. Therefore, groundwater levels during construction or at other times in the life of the structure may be higher or lower than the levels indicated on the boring logs. The possibility of groundwater level fluctuations should be considered when developing the design and construction plans for the project.

3.5 Soil Resistivity Testing

On February 24 and March 1, 2017, Nobis field personnel conducted in-situ soil resistivity testing in accordance with accepted engineering practices using the Wenner electrode configuration. Electrodes were spaced at 5, 10, 20, 30 and 40 feet, where possible. Two sets of two approximately perpendicular resistivity lines were completed in the general vicinity of the proposed tower location. The approximate locations and orientations of the resistivity lines are shown on the attached **Figure 2**. The results of the resistivity tests are as follows:

<u>Electrode Spacing (ft)</u>	<u>Resistivity (ohm-cm)</u>			
	<u>Line 1</u>	<u>Line 2</u>	<u>Line 3</u>	<u>Line 4</u>
5	68,940	27,768	60,323	42,130
10	22,980	5,745	30,640	32,555
20	3,830	3,830	19,150	11,490
30	5,745	5,745	11,490	11,490
40	7,660	-*	7,660	-*

*The proximity of the property lines did not allow completion of this spacing interval.



Field resistivity results may be influenced by boulders, concrete, foundations, and underground utilities within the test area. Resistivity results will also fluctuate depending on the degree of compaction, moisture content, constituent solubility, and temperature. Field resistivity values may also vary depending upon season, precipitation, and other conditions that may differ from those at the time of testing.

4.0 GEOTECHNICAL DESIGN AND CONSTRUCTION RECOMMENDATIONS

4.1 Geotechnical Evaluation

Based on the results of our subsurface investigation, it is our opinion the proposed 130-foot permanent steel monopole telecommunications tower may be supported on a monolithic mat or a pier-and-pad foundation bearing on the glacial till, or compacted Structural Fill or Crushed Stone (see *Section 4.5 Materials and Compaction*) placed over a prepared glacial till subgrade. Alternatively, the permanent telecommunications tower may be supported on a drilled shaft foundation extending into competent glacial till and weathered bedrock.

We understand the proposed 165-foot temporary tower will be supported on a 24-feet by 24-feet ballasted frame foundation. Referenced drawings indicated the foundation system will bear at finish grade at approximately El 47 and not have embedment. We recommend that the ballasted frame foundation bear on compacted Structural Fill or Crushed Stone placed over glacial till. Design recommendations and construction considerations for the recommended foundation systems are presented in the following sections.

4.2 Seismic Design Recommendations

Based on the density/consistency of the soils encountered in the explorations, it is our opinion that Site soils are not considered susceptible to liquefaction. Seismic forces on foundations should be designed in accordance with the Connecticut State Building Code. We recommend using the following seismic design values based on the 2016 Connecticut State Building Code:

- Site Class: C;
- MCE Spectral Response Accelerations: $S_s = 0.167g$ and $S_1 = 0.059g$;
- Site Coefficients: $F_a = 1.2$ and $F_v = 1.7$; and
- Seismic Design Parameters: $S_{MS} = 0.200$ and $S_{M1} = 0.100$; $S_{DS} = 0.134$ and $S_{D1} = 0.067$.



4.3 Permanent Tower Foundation Design Recommendations

4.3.1 Shallow Foundation (Mat/Pad) Alternative

The proposed permanent monopole communications tower may be supported on a mat or pad-and-pier foundation bearing on proof-rolled glacial till, or compacted Structural Fill or Crushed Stone placed on above a proof-rolled glacial till subgrade. Crushed stone, if used, should be separated from soil subgrades, excavation sidewalls and backfill using a geotextile separation fabric such as Mirafi 140N, or equivalent.

Nobis recommends a maximum net allowable bearing pressure of 6 kips per square foot (ksf). Foundations should be embedded a minimum of 42 inches below final grades for frost protection. The total settlement is anticipated to be less than 1 inch and differential settlement to be less than 0.5 inches. Foundation settlement will depend on the variations within the subsurface soil profile, the structural loading conditions, the embedment depth of the foundation, the thickness of compacted fill, and the quality of earthwork operations.

We recommend an ultimate passive pressure coefficient (Kp) of 3.0. Calculated passive pressures should be reduced by a minimum factor of safety of 3, to reflect the amount of movement required to mobilize the passive resistance. We also recommend an ultimate coefficient of sliding friction of 0.5. A factor of safety of at least 1.5 should be applied to calculated sliding resistance.

To summarize, we recommend the following static design parameters:

Description	Value
Maximum Net Allowable Bearing Pressure	6 kips per square foot
Minimum Foundation Width	Isolated Spread Footing/Mat Foundation: 2 feet
Minimum Embedment Below Finished Grade	42 inches
Estimated Total Settlement	<1 inch
Estimated Differential Settlement	<½ inch
Total Soil Unit Weight	130 pounds per cubic foot
Ultimate Passive Pressure Coefficient, Kp	3.0
Ultimate Coefficient of Sliding Friction	0.5



Uplift resistance for the tower foundation may be computed as the sum of the weight of the foundation element and the weight of the soil overlying the foundation.

4.3.2 Shallow Foundation (Mat/Pad) Construction Recommendations

The proposed mat/pad foundation and associated equipment areas should be cleared of existing structures and vegetation and grubbed; and existing cobbles, boulders, and any identifiable compressible or deleterious materials should be removed. Existing fill (including re-worked parent materials), and other unsuitable materials (e.g., silt deposit), must be removed from beneath footing zones of influence to the top of firm, natural glacial till prior to construction. Over-excavation below foundations should include the zone of influence, defined as the area beneath 1 horizontal to 1 vertical (1H:1V) lines extending downward and outward from footing edges. Footings shall bear on a prepared subgrade of firm natural glacial till, or compacted Structural Fill or Crushed Stone (over firm natural soil). Refer to *Section 4.5 Materials and Compaction* for material placement recommendations.

The proposed project area is partially occupied with the existing water tank and associated underground utilities. The existing water tank will be demolished prior to construction of the permanent communications tower. Existing foundation elements and underground utilities should be removed where they conflict with the planned development. Areas disturbed during removal of foundations and utilities should be undercut and the excavations should be backfilled in systematic, compacted lifts. Fill materials and compaction efforts should be consistent with the intended future use.

Excavations for foundation subgrades are anticipated to consist of native glacial till containing varying amounts of silt that will be easily disturbed when wet. Earthwork should be performed in dry conditions so that disturbance to foundation subgrades is limited. During earthwork, the Contractor should be responsible for protecting subgrades from the elements and maintaining the soils in a suitable state until completion of the project. Backfill should not be placed over a subgrade with standing water or that is frozen. Standing water, if present, should be removed and any soft and yielding soil should be removed prior to backfill placement. Excavations to subgrade levels should be performed using a smooth-edged bucket to minimize possible disturbance to the in-place subgrade soils.



Soil subgrades should be proof-rolled under the observation of a qualified Geotechnical Engineer with at least four (4) passes of a smooth-drum vibratory roller (minimum 8,000 pounds, minimum centrifugal force of 12,500 pounds) or, where approved by the geotechnical engineer, a vibratory plate compactor with a minimum of 2,500 pounds of centrifugal force. Any soft or loose zones identified during proof-rolling should be excavated and replaced with compacted Structural Fill, as necessary, and as required by the Geotechnical Engineer. It is imperative that subgrade preparations occur under the observation of the Geotechnical Engineer, as applying vibratory energy to a well-prepared natural, glacial till subgrade may cause disturbance and create soft and loose zones.

4.3.3 Deep Foundation (Drilled Shaft) Alternative

We recommend the following static design parameters for a drilled shaft foundation alternative:

Description	Value
Maximum Net Allowable Bearing Capacity Glacial Till Decomposed Rock	6 kips per square foot (ksf) 8 ksf
<u>Ultimate Side Friction Values²</u> Glacial Till Decomposed Rock	20 pounds per square inch (psi) 25 psi
<u>Coefficient of Lateral Subgrade Reaction³</u> Glacial Till Decomposed Rock	80 (z/D) kips per cubic foot (kcf) 90 (z/D) kcf
<u>Angle of Internal Friction</u> Glacial Till Decomposed Rock	36 38
<u>Total Soil Unit Weight</u> Glacial Till Decomposed Rock	135 pounds per cubic foot (pcf) 140 (pcf)
Minimum Drilled Shaft Diameter	Diameter of Monopole Base
Allowable Deflection at Top of Shaft	0.5 inch
<ol style="list-style-type: none"> 1. The allowable end bearing capacity also assumes that loose, disturbed material has been removed from the base of the shaft. 2. Contribution to shaft capacity from soil above a depth of 4 feet should be ignored. The uplift capacity should be based on the dead weight of the shaft and side resistance provided by the glacial till and decomposed rock. It's assumed that applied loading will not have a significant Poissons-effect on the shaft. 3. z represents the depth below ground surface (feet) and D is the diameter of the foundation element (feet). 	



We anticipate that the design length of the shaft will be primarily dependent on the embedment/lateral capacity required to resist live loading. The base of the drilled shaft should be at least 15 feet below ground surface. The drilled shaft will be subject to tension loads and therefore should have reinforcing steel that extend through the entire length of the shaft.

4.3.4 Deep Foundation (Drilled Shaft) Construction Recommendations

Technical specifications should be prepared by the specialty Contractor that require detailed material and construction submittals and proof of experience in drilled shaft installation. The drilling method or combination of methods selected by the contractor should be submitted for review by the geotechnical engineer, prior to mobilization of drilling equipment.

A section of temporary casing may be required to reduce the likelihood of caving of the side walls of the shaft hole. Concrete should be placed by directing the concrete down the center of the shaft to reduce the likelihood of hitting the reinforcing steel and segregating. Groundwater, if encountered in the shaft, should be removed prior to placing concrete; alternatively, concrete may be placed by tremie methods.

4.4 Temporary Tower Foundation Design Recommendations

4.4.1 Ballasted Frame Alternative

Based on anticipated loading and the conditions encountered during our subsurface investigation, it is our opinion that the proposed ballasted frame foundation system cannot derive support on the encountered silt stratum located beneath the existing fill. The variable presence and thickness of the soft, compressible silt stratum would result in unpredictable, differential settlements within the ballasted frame area. Support should instead be derived from a minimum 12-inch layer of compacted structural fill placed above natural, glacial till as described in *Section 4.3.2 Shallow Foundation (Mat/Pad) Construction Recommendations*. This will require replacing existing soil within the foundation zone of influence [defined as the area beneath 1 horizontal to 1 vertical (1H:1V) lines extending downward and outward from the foundation edge] with compacted nonfrost-susceptible structural fill, which will also reduce the potential for frost action. A non-woven geotextile, such as Mirafi 140N, or equivalent, is recommended over stable, prepared subgrade and beneath the Structural Fill.



We recommend a maximum net allowable bearing pressure of 5 kips per square foot (ksf) for the 24-foot by 24-foot foundation. This allowable bearing capacity is based on the complete removal/replacement of existing fill and silt below the ballasted frame foundation. Deeper excavation may be required if exposed subgrades have an appreciable amount of organic content or appear unsuitable for bearing. Nobis should be retained to evaluate exposed subgrade conditions prior to placing fill.

We recommend an ultimate coefficient of sliding friction of 0.5. A factor of safety of at least 1.5 should be applied to the sliding resistance.

The total settlement is anticipated to be less than 1 inch and differential settlement to be less than 0.5 inch. Based on the granular nature of bearing materials, much of the settlement is anticipated to occur as load is applied. Foundation settlement will depend on the variations within the subsurface soil profile, the structural loading conditions, frost susceptibility of subgrade soils, the embedment depth of the foundation, the thickness of compacted fill, and the quality of earthwork operations.

4.5 Materials and Compaction

Recommended earthwork materials are as follows:

Structural Fill is to be used beneath footings, and other areas as appropriate, or as directed by the Geotechnical Engineer or his/her representative. The material shall consist of hard, inert, durable particles of stone and coarse sand. It shall be free from ice and snow, roots, surface coatings, sod, loam, clay, rubbish, and other deleterious or organic matter, and shall conform to the following gradation requirements:

Sieve Size	Percent Passing by Weight
3-inch	100
½-inch	50-85
No. 4	40-75
No. 50	8-28
No. 200	0-10*



*To be considered nonfrost-susceptible, structural fill should have a maximum of 3 percent of particles by weight smaller than 0.02mm in effective diameter.

Crushed Stone shall consist of either angular fragments of crushed rock or durable crushed gravel stone, be reasonably free of loam, clay, or other deleterious or organic matter, and shall conform to the following gradation requirements:

Sieve Size	Percent Passing by Weight
¾-inch	100
½-inch	10-50
⅝-inch	0-20
No. 4	0-5

Nonfrost-Susceptible Material shall consist of granular fill or crushed stone containing less than 3 percent smaller than 0.02 mm.

Structural Fill and Crushed Stone should be placed in loose lifts not exceeding 8 inches in depth, and compacted to at least 95 percent of its maximum dry density, and within 2% of optimum moisture content, as determined by ASTM D1557, Method C (Modified Proctor).

4.6 Additional Construction Considerations

Based on information obtained from the subsurface exploration program, groundwater may be encountered during construction. We anticipate that water can be managed with conventional sump pumps and trenches in the excavations; however, the contractor should review the plans and borings and make his/her own interpretation of the means and methods needed to control water during construction. Stormwater runoff should not be permitted to accumulate on/within exposed subgrades and the runoff should be directed away from the exposed subgrade areas.

Where space permits and as needed, temporary slopes no steeper than 1.5H:1V appear to be appropriate. Excavation geometry should conform to OSHA excavation regulations contained in 29 CFR Part 1926. Temporary earth support is not anticipated for the excavations. If needed, temporary earth support systems should be designed by a Professional Engineer registered in the State of Connecticut.



We recommend that Nobis be provided the opportunity to review the final design plans and specifications to ensure that the recommendations of this report have been incorporated as intended. We further recommend that Nobis observe excavation to subgrade levels, subgrade preparation, and fill placement and compaction. This is recommended to evaluate and document the bearing material for the foundation subgrades. We also recommend that Nobis be retained to monitor the construction of the drilled shaft, if selected as the foundation alternative. The geotechnical engineer in the field should observe the work for compliance with the recommendations in this report, identify changes in subsurface conditions from those observed in the explorations should they become apparent, and assist in the development of design changes should subsurface conditions differ from those anticipated prior to the start of construction.

5.0 CLOSURE

This report is subject to the Limitations, included as **Appendix C**.

APPENDIX A – Figures



4492790.00 - Westbrook H2O Call Tower, Westbrook, CT (CAD) 1642 Boston Post Road, Westbrook, CT Call Tower.dwg 3/2/2017 9:44 AM



USGS TOPOGRAPHIC MAP

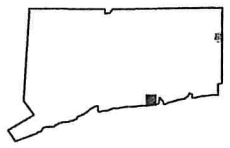
7.5 MINUTE QUADRANGLE: ESSEX, CT
1977

APPROX. SCALE IN FEET



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Client-Focused, Employee-Owned



QUADRANGLE LOCATION

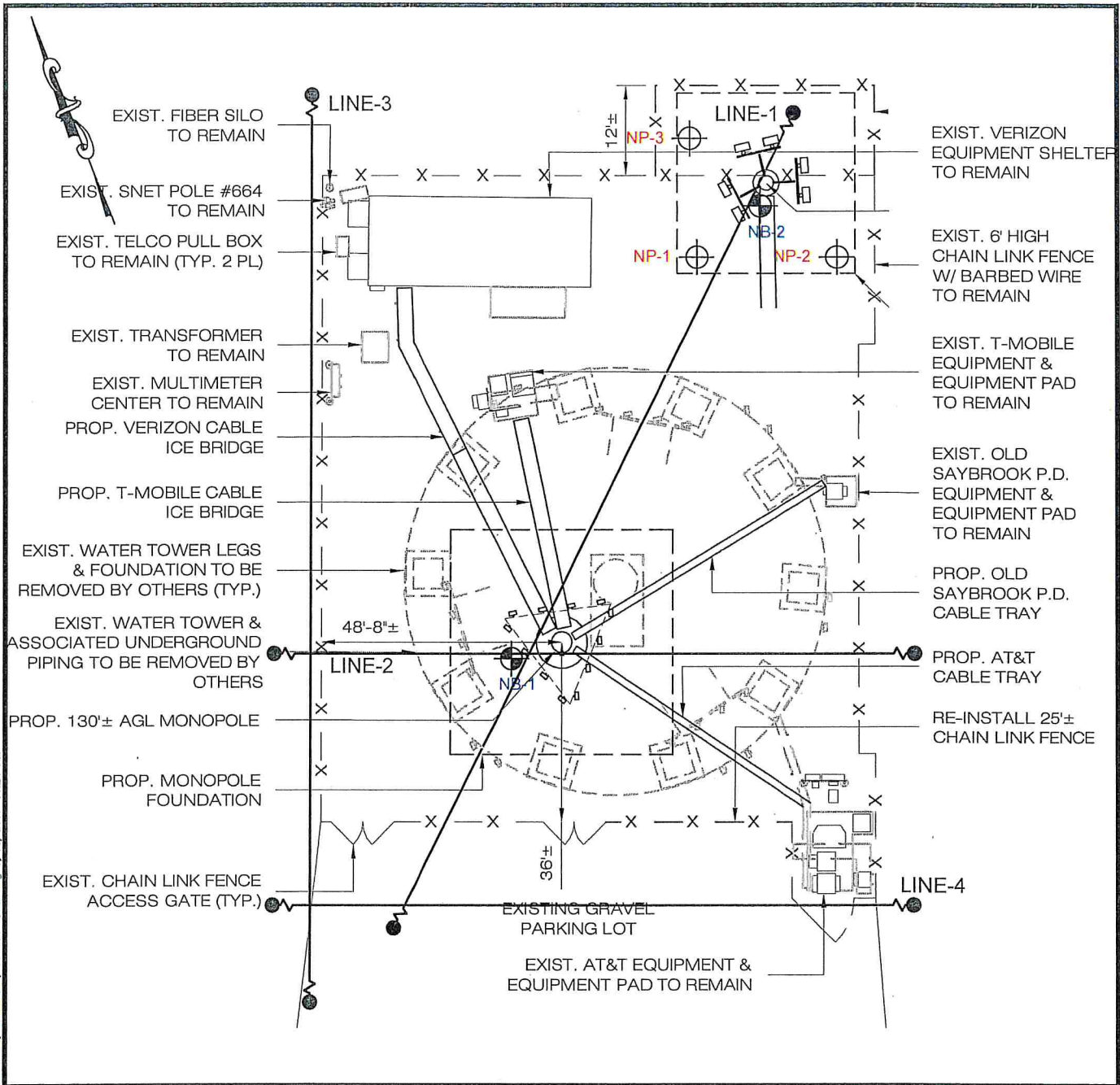
FIGURE 1

LOCUS PLAN
WESTBROOK H2O
1542 BOSTON POST ROAD
WESTBROOK, CT 06498

PROJECT NO. 92790.00

DATE: MARCH 2017

1524 BOSTON POST ROAD, WESTBROOK, CT 06790
 3/10/2017 11:24 AM
 92790.00 - Westbrook H2O Cell Tower, Westbrook, CT



NOTES:

1. THE BASE PLAN WAS DEVELOPED FROM FIGURE ENTITLED, "COMPOUND PLAN," PREPARED BY ALL-POINTS TECHNOLOGY ENGINEERING CORPORATION, P.C., REVISION DATED DECEMBER 22, 2016.
2. TEST BORINGS AND PROBES WERE DRILLED BY NEW ENGLAND BORING CONTRACTORS OF GLASTONBURY, CONNECTICUT, AND OBSERVED BY NOBIS ON MARCH 8, 2017.
3. RESISTIVITY TESTING WAS PERFORMED ON FEBRUARY 24 2017 AND MARCH 1, 2017 BY NOBIS FIELD STAFF.
4. THE APPROXIMATE LOCATIONS OF THE TEST BORINGS, TEST PROBES, AND RESISTIVITY TESTS WERE TAPED FROM EXISTING SITE FEATURES. THE LOCATIONS SHOULD BE CONSIDERED ACCURATE ONLY TO THE DEGREE IMPLIED BY THE METHOD USED.

LEGEND:

- NP-1 TEST PROBE LOCATION
- NB-1 TEST BORING LOCATION
- RESISTIVITY TEST LOCATION (TYP.)

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 Client-Focused, Employee-Owned

APPROX. SCALE IN FEET

DRAWN BY: JDV
 CHECKED BY: RPJ

FIGURE 2

EXPLORATION LOCATION PLAN
WESTBROCK H2O
1542 BOSTON POST ROAD
WESTBROCK, CONNECTICUT 06498

PROJECT NO. 92790.00	DATE: MARCH 2017
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APPENDIX B – Exploration Logs

BOREHOLE LOG - NOBIS GINT DATA TEMPLATE OCT 7 2011.GDT - 3/17/17 12:38 - J192790.00 - WESTBROOK H2O CELL TOWER, WESTBROOK, CT; GTECHNICAL/EXPLORATIONS/BOREHOLE LOGS/GINT/192790.00 - 1542 BOSTON POST RD WESTBROOK, CT DRILLINGS



Engineering a Sustainable Future

BORING LOG

Project: Westbrook H2O Towers

Location: 1542 Boston Post Rd, Westbrook, CT

Nobis Project No.: 92790.00

Boring No.: NB-1

Boring Location: See Boring Location Plan

Checked by: R. Janeiro

Date Start: March 8, 2017

Date Finish: March 8, 2017

Contractor: New England Boring Contractors

Driller: Bub Thompson

Nobis Rep.: R. Janeiro

Rig Type / Model: ATV/ Acker Soil Scout

Hammer Type: Donut Hammer

Hammer Hoist: Rope & Cathead

Ground Surface Elev.: (+/-) 47.5

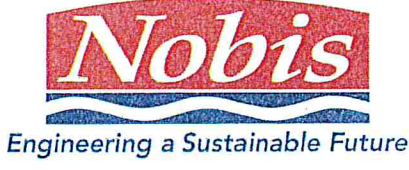
Datum: NAVD 88

Type	Drilling Method	Sampler	Groundwater Observations					
			Date	Time	Depth Below Ground (ft.)	Depth of Casing (ft.)	Depth to Bottom of Hole (ft.)	Stabilization Time
	Flush Joint Casing	Split-Spoon	03/08/17	10:05	5	N/A	N/A	Wet Sample
Size ID (in.)	4	1-3/8						
Advancement	Standard Rotary	140-lb Hammer						




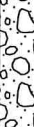
Depth (ft.)	SAMPLE INFORMATION					REC % / RQD %	Drilling Rate (min/ft)	Ground Water	LITHOLOGY	SAMPLE DESCRIPTION AND REMARKS (Classification System: Modified Burmister)	NOTES
	Type & No.	Rec (in.)	Depth (ft.)	Blows/6 in.	Stratum Elev. / Depth (ft.)						
1	S-1	13	0-2	3				FILL	S-1 (4"): Dark Brown, TOPSOIL.		
2				4					S-1 (9"): Loose, brown, fine to coarse SAND and SILT, trace fine Gravel, very few organic fibers.		
3	S-2	18	2-4	2					S-2: Loose, brown, SILT and fine to medium SAND, trace fine Gravel, very few organic fibers. moist.		
4				3					S-3 (11"): Loose to medium dense, brown, fine to coarse SAND and SILT, trace fine Gravel, very few decomposed wood fragments. wet.		
5	S-3	14	4-6	2					S-3 (3"): Loose to medium dense, orange brown, fine to coarse SAND, little Silt. wet.		
6				3							
7				3							
8				3							
9				3							
10	S-4	8	9-9.8	30					TILL	S-4: Very dense (refusal), brown, fine to coarse SAND, trace Silt, few weathered rock fragments, with a piece of weathered rock in sample tip.	
11				50/3"							
12											
13											
14											
15	S-5	19	14-15.8	50				S-5: Very dense (refusal), brown, fine to coarse SAND and GRAVEL, little Silt, few weathered rock fragments.			
16				52							
17				55							
18				50/4"							
19											
20	S-6	8	19-19.8	42				S-6: Very dense (refusal), brown, fine to coarse SAND, little fine Gravel, little Silt.			
21				50/4"							
22											
23											
24											
25	S-7	4	24-24.3	100/4"				DECOMPOSED ROCK	S-7: Very dense (refusal), gray/ orange/ white, fine to coarse SAND and GRAVEL, trace Silt.		
26											
27											
28											
29											
30	S-8	2	29-29.2	50/2"					S-8: Very dense (refusal), gray-white, fine to coarse GRAVEL and SAND, trace Silt.		
31											
32	C-1	12	31-36		20/0	2			C-1: Very Poor Quality, Soft, Extremely Weathered, gray-white, coarse grained, GNEISS.		
33						2					
34						3					
35						2					
36						2					
37									Boring terminated at 36 feet.		
38											
39											
40											

Soil	Percentage	Non-Soil	NOTES:
trace	5 - 10	very few	1) Rig chatter observed from 17 to 31 feet below grade (fbg). 2) Driller notes increased drilling resistance at 22 fbg.
little	10 - 20	few	
some	20 - 35	several	
and	35 - 50	numerous	

BOREHOLE LOG - NOBIS GINT DATA TEMPLATE OCT 7 2011.GDT - 3/17/17 12:39 - J192790.00 - WESTBROOK H2O CELL TOWER, WESTBROOK, CT; GEOTECHNICAL EXPLORATION; BORING LOGS; GINT 192790.00 - 1542 BOSTON POST RD WESTBROOK, CT DRILLINGS

	BORING LOG	Boring No.: <u>NP-1</u>
	Project: <u>Westbrook H2O Towers</u>	Boring Location: <u>See Boring Location Plan</u>
Location: <u>1542 Boston Post Rd, Westbrook, CT</u>	Nobis Project No.: <u>92790.00</u>	Checked by: <u>R. Janeiro</u>
Contractor: <u>New England Boring Contractors</u>	Rig Type / Model: <u>ATV/ Acker Soil Scout</u>	Date Start: <u>March 8, 2017</u>
Driller: <u>Bub Thompson</u>	Hammer Type: <u>Donut Hammer</u>	Date Finish: <u>March 8, 2017</u>
Nobis Rep.: <u>R. Janeiro</u>	Hammer Hoist: <u>Rope & Cathead</u>	Ground Surface Elev.: <u>(+/-) 46.5</u>
		Datum: <u>NAVD 88</u>

Type	Drilling Method	Sampler	Groundwater Observations					
			Date	Time	Depth Below Ground (ft.)	Depth of Casing (ft.)	Depth to Bottom of Hole (ft.)	Stabilization Time
	N/A	Split-Spoon	03/08/17	00:00	3	NP-1	N/A	Wet Sample
Size ID (in.)	N/A	1-3/8						
Advancement	N/A	140-lb Hammer						

Depth (ft.)	SAMPLE INFORMATION				Ground Water	LITHOLOGY		SAMPLE DESCRIPTION AND REMARKS (Classification System: Modified Burmister)	NOTES
	Type & No.	Rec (in.)	Depth (ft.)	Blows/ 6 in.		Graphic	Stratum Elev. / Depth (ft.)		
1	S-1	17	0-2	2		 FILL	S-1 (4"): Loose, dark brown, TOPSOIL, with few stone process fragments.		
									S-1 (13"): Loose, dark brown, fine to coarse SAND and SILT, trace fine Gravel, very few organic fibers. moist.
2				2					S-2 (10"): Loose, brown, fine to coarse SAND, some fine Gravel, some Silt, very few organic fibers. moist.
3	S-2	18	2-4	2		 SILT			S-2 (4"): Loose, black, SILT, little fine Sand, very few organic fibers. moist.
4				2					S-2 (4"): Loose, brown, fine to coarse SAND and SILT, trace fine Gravel. wet.
5				6					
6	S-3	19	4-6	18	 TILL		S-3: Medium dense to dense, brown, fine to coarse SAND, some Silt, trace fine Gravel. wet.		
7				16					
8				14					
9				15					
10									
11									
12									
13									
14									
15									
16									
17									
18									
19									
20									

Soil	Percentage	Non-Soil	NOTES:
trace	5 - 10	very few	
little	10 - 20	few	
some	20 - 35	several	
and	35 - 50	numerous	

BOREHOLE LOG - NOBIS GINT DATA TEMPLATE OCT 7 2011.GDT - 3/7/17 12:39 - J.192790.00 - WESTBROOK H2O CELL TOWER, WESTBROOK, CT.GEOTECHNICAL EXPLORATIONS.BORING LOGS.GINT.192790.00 - 1542 BOSTON POST RD WESTBROOK, CT.DRILLINGS



BORING LOG

Project: Westbrook H2O Towers
 Location: 1542 Boston Post Rd, Westbrook, CT
 Nobis Project No.: 92790.00

Boring No.: NP-2
 Boring Location: See Boring Location Plan
 Checked by: R. Janeiro
 Date Start: March 8, 2017
 Date Finish: March 8, 2017

Contractor: New England Boring Contractors
 Driller: Bub Thompson
 Nobis Rep.: R. Janeiro

Rig Type / Model: ATV/ Acker Soil Scout
 Hammer Type: Donut Hammer
 Hammer Hoist: Rope & Cathead

Ground Surface Elev.: (+/-) 46.5
 Datum: NAVD 88

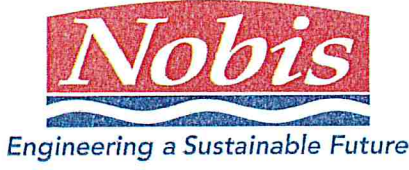
Type	Drilling Method	Sampler	Groundwater Observations					
			Date	Time	Depth Below Ground (ft.)	Depth to Bottom of Hole (ft.)	Stabilization Time	
	N/A	Split-Spoon	03/08/17	00:00	4	NP-2	N/A	Wet Sample
Size ID (in.)	N/A	1-3/8						
Advancement	N/A	140-lb Hammer						

Depth (ft.)	SAMPLE INFORMATION				Ground Water	LITHOLOGY	SAMPLE DESCRIPTION AND REMARKS (Classification System: Modified Burmister)	NOTES
	Type & No.	Rec (in.)	Depth (ft.)	Blows/ 6 in.				
1	S-1	12	0-2	3	 FILL	S-1 (3"): Very loose, dark brown, TOPSOIL, with few stone process fragments. S-1 (9"): Very loose, dark brown, fine to coarse SAND and SILT, little fine Gravel, very few organic fibers. moist.		
				2				
				2				
				3				
2	S-2	14	2-4	9	 FILL	S-2 (10"): Loose, dark brown, fine to coarse SAND and SILT, little fine Gravel, very few organic fibers and decomposed wood fragments. moist. S-2 (4"): Loose, olive, fine to medium SAND and SILT, (mottled), very few organic fibers. moist.		
				4				
				2				
3				2	 TILL	S-3: Dense, brown, fine to coarse SAND, some fine to coarse Gravel, little Silt. wet.		
				3				
4				8	 TILL	40.5 / 6.0 Boring terminated at 6 feet.		
5								
23								
24								
6				24				
7								
8								
9								
10								
11								
12								
13								
14								
15								
16								
17								
18								
19								
20								

Soil	Percentage	Non-Soil
trace	5 - 10	very few
little	10 - 20	few
some	20 - 35	several
and	35 - 50	numerous

NOTES:

BOREHOLE LOG - NOBIS GINT DATA TEMPLATE OCT 7 2011.GDT - 3/17/17 12:39 - J:\92790.00 - WESTBROOK H2O CELL TOWER, WESTBROOK, CT\GEO\TECH\EXPLORATIONS\BORING LOGS\GINT\92790.00 - 1542 BOSTON POST RD WESTBROOK, CT DRILLINGS

	BORING LOG		Boring No.: <u>NP-3</u>
	Project: <u>Westbrook H2O Towers</u>		Boring Location: <u>See Boring Location Plan</u>
	Location: <u>1542 Boston Post Rd, Westbrook, CT</u>		Checked by: <u>R. Janeiro</u>
	Nobis Project No.: <u>92790.00</u>		Date Start: <u>March 8, 2017</u> Date Finish: <u>March 8, 2017</u>
Contractor: <u>New England Boring Contractors</u>	Rig Type / Model: <u>ATV/ Acker Soil Scout</u>	Ground Surface Elev.: <u>(+/-) 47</u>	
Driller: <u>Bub Thompson</u>	Hammer Type: <u>Donut Hammer</u>	Datum: <u>NAVD 88</u>	
Nobis Rep.: <u>R. Janeiro</u>	Hammer Hoist: <u>Rope & Cathead</u>		

Type	Drilling Method	Sampler	Groundwater Observations					
			Date	Time	Depth Below Ground (ft.)	Depth of Casing (ft.)	Depth to Bottom of Hole (ft.)	Stabilization Time
	N/A	Split-Spoon	03/08/17	00:00	4	NP-3	N/A	Wet Sample
Size ID (in.)	N/A	1-3/8						
Advancement	N/A	140-lb Hammer						

Depth (ft.)	SAMPLE INFORMATION				Ground Water	LITHOLOGY		SAMPLE DESCRIPTION AND REMARKS (Classification System: Modified Burmister)	NOTES
	Type & No.	Rec (in.)	Depth (ft.)	Blows/ 6 in.		Graphic	Stratum Elev. / Depth (ft.)		
1	S-1	16	0-2	2	▼	[Cross-hatch pattern]	FILL	S-1 (3"): Loose, dark brown, TOPSOIL, very few organic fibers.	
				2				S-1 (7"): Loose, brown, fine to coarse SAND, some fine to coarse Gravel, some Silt, very few organic fibers. moist.	
				3				S-1 (6"): Loose, black, SILT, little fine to medium Sand, few organic fibers. moist.	
2	S-2	7	2-4	3	▼	[Vertical lines pattern]	SILT	S-2: Medium dense, black, SILT, some fine to coarse Sand, very few organic fibers.	
				4					
3				15	▼	[Vertical lines pattern]			
				27					
4	S-3	14	4-6	42	▼	[Circular pattern]	TILL	S-3: Very dense, brown, fine to coarse SAND, some Silt, little fine to coarse Gravel, with a piece of fractured coarse gravel at top of sample.	
				27					
5				24					
6				24			41.0 / 6.0	Boring terminated at 6 feet.	
7									
8									
9									
10									
11									
12									
13									
14									
15									
16									
17									
18									
19									
20									

Soil	Percentage	Non-Soil	NOTES:
trace	5 - 10	very few	
little	10 - 20	few	
some	20 - 35	several	
and	35 - 50	numerous	

APPENDIX C – Limitations

GEOTECHNICAL LIMITATIONS

Explorations and Subsurface Conditions

1. The analyses and design recommendations submitted in this report are based in part upon the data obtained from subsurface explorations. The nature and extent of variations between these explorations may not become evident until construction. If variations then appear evident, it will be necessary to reevaluate the recommendations of this report.

In preparing this report, Nobis relied on certain information provided by the Client and other parties referenced therein which were made available to Nobis at the time of our evaluation. Nobis did not attempt to independently verify the accuracy or completeness of all information reviewed or received during the course of this evaluation.

2. The generalized soil profile described in the text is intended to convey trends in subsurface conditions. The boundaries between strata are approximate and idealized and have been developed by interpretations of widely spaced explorations and samples; actual soil transitions are probably more erratic. For specific information, refer to the exploration logs.

3. Water level readings have been made in the explorations at times and under conditions stated on the logs. These data have been reviewed and interpretations have been made in the text of this report. However, it must be noted that fluctuations in the level of the groundwater may occur due to variations in rainfall, temperature, and other factors occurring since the time measurements were made. The water table encountered in the course of the work may differ from that indicated in the Report.

Recommendations for foundation drainage, waterproofing, and moisture control address the conventional geotechnical engineering aspects of seepage control. These recommendations may not preclude an environment that allows the infestation of mold or other biological pollutants.

4. Nobis' geotechnical services did not include an assessment of the presence of oil or hazardous materials at the property. Consequently, we did not consider the potential impacts (if any) that contaminants in soil or groundwater may have on construction activities, or the use of structures on the property.

Additional Services

5. Nobis recommends that we be retained to provide services during future site observations, design, implementation activities, construction and/or property development/redevelopment. This will allow us the opportunity to: i) observe conditions and compliance with our recommendations, design concepts and/or opinions; ii) allow for changes in the event that conditions are other than anticipated; iii) provide modifications to our design recommendations; and iv) assess the consequences of changes in technologies and/or regulations.

Use of Report

6. Nobis prepared this report on behalf of, and for the exclusive use of our Client for the stated purpose(s) and location(s) identified in our proposal and/or report. Use of this report, in whole or in part, at other locations, or for other purposes, may lead to inappropriate conclusions; and we do not accept any responsibility for the consequences of such use(s). Reliance by any party not expressly identified in the agreement, for any use, without our prior written permission, shall be at that party's sole risk, and without any liability to Nobis.

This report is for design purposes only and is not sufficient to prepare an accurate construction bid. Contractors wishing a copy of the report may secure it with the understanding that its scope is limited to design considerations only.

7. Nobis' findings and conclusions are based on the work conducted as part of the scope of work set forth in our proposal and/or report, and reflect our professional judgment. These findings and conclusions must be considered not as scientific or engineering certainties, but rather as our professional opinions considering the limited data gathered during the course of our work. If conditions other than those described in this report are found at the subject location(s), or the project design has been altered in any way, Nobis shall be so notified and afforded the opportunity to revise the report, as appropriate, to reflect the unanticipated changed conditions.

8. Nobis' services were performed using the degree of skill and care ordinarily exercised by qualified professionals performing the same type of services, at the same time, under similar conditions, at the same or a similar property. No warranty, expressed or implied, is made.

Compliance with Codes and Regulations

9. Nobis used reasonable care in identifying and interpreting applicable codes and regulations. These codes and regulations are subject to various, and possibly contradictory, interpretations. Compliance with codes and regulations by other parties is beyond our control.

Opinion of Cost

10. This report may contain or be based on comparative cost opinions for the purpose of evaluating alternative foundation schemes. These opinions may also involve approximate quantity evaluations. It should be noted that quantity estimates may not be accurate enough for construction bids. In addition, since we are not professional estimators of labor and materials cost, the evaluation of construction costs should be considered as approximate guidelines and could vary significantly from actual costs. Nobis does not guarantee the accuracy of our cost opinions as compared to contractor's bids for construction costs.

END OF LIMITATIONS

3



1 Fairholm Avenue
Peoria, IL 61603 USA
Phone 309-566-3000
FAX 309-566-3079

October 17, 2019

MCM Holdings LLC
Attn: Virginia King
40 Woodland Street
Hartford, CT. 06105

Reference: 130' Future 150' Tapered Steel Pole
Westbrook Permanent, Middlesex County, CT.

File Number: 231452

<u>Copies</u>	<u>Drawing Number</u>	<u>Description</u>
1	231452-01-D1R5	Design Drawing Sealed for the State of Connecticut
1	231452-01-F1R5	Foundation
1		Sealed Letter

Email Only: vking@mcmgmt.com

Sincerely,

JD Long

crp



1 Fairholm Avenue
Peoria, IL 61603 USA
Phone: (309)-566-3000
Fax: (309)-566-3079

DATE: OCTOBER 17, 2019

PURCHASER: MCM HOLDINGS LLC

PROJECT: 130 FT TAPERED STEEL POLE
WESTBROOK PERMANENT, CONNECTICUT

FILE NUMBER: 231452

DRAWINGS: 231452-01-D1 R5, 231452-01-F1 R5

I CERTIFY THAT THE REFERENCED DRAWINGS WERE PREPARED UNDER MY SUPERVISION IN ACCORDANCE WITH THE DESIGN AND LOADING CRITERIA SPECIFIED BY THE PURCHASER AND THAT I AM A REGISTERED PROFESSIONAL ENGINEER UNDER THE LAWS OF THE STATE OF CONNECTICUT.

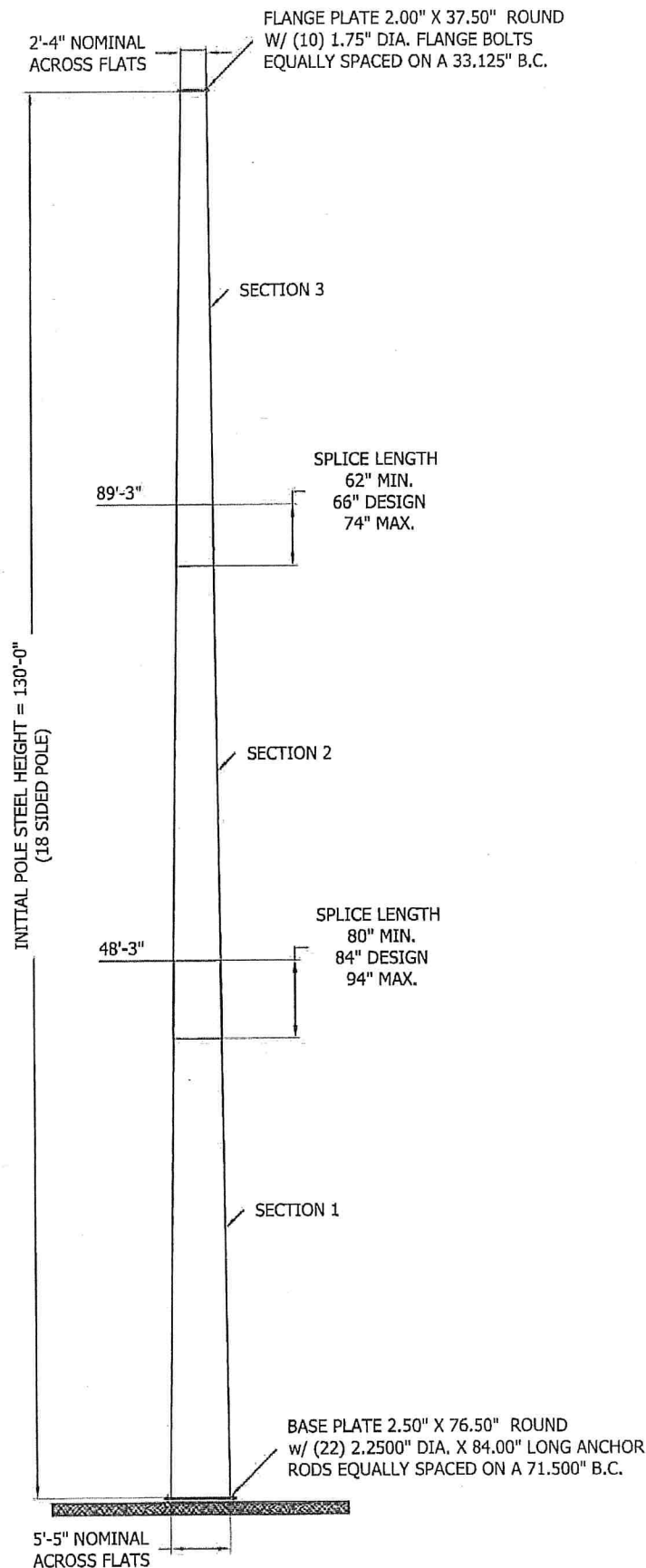
CERTIFIED BY: _____

[Handwritten signature]

DATE: _____

10/17/19





POLE DESIGN LOADING		
DESIGN WIND LOAD PER ANSI/TIA-222-G & 2018 CONNECTICUT STATE BUILDING CODE USING THE FOLLOWING DESIGN CRITERIA: ASCE 7-10 FACTORED WIND SPEED (NO ICE): 135 MPH BASIC WIND SPEED (WITH ICE): 50 MPH PER ASCE 7-10 DESIGN ICE THICKNESS: 0.75" PER ASCE 7-10 EXPOSURE CATEGORY: D STRUCTURE CLASSIFICATION: II TOPOGRAPHIC CATEGORY: 1 EARTHQUAKE SPECTRAL RESPONSE ACCELERATION, S_s : 0.167, S_1 : 0.059		
DESIGN PER ANSI/TIA-222-H & 2018 CONNECTICUT STATE BUILDING CODE: RISK CATEGORY: II BASIC WIND SPEED (NO ICE): 135 MPH PER ASCE 7-16 BASIC WIND SPEED (W/ ICE): 50 MPH PER ASCE 7-16 DESIGN ICE THICKNESS: 1.0 INCHES PER ASCE 7-16 EXPOSURE CATEGORY: D TOPOGRAPHIC METHOD: 1, CATEGORY 1 GROUND ELEVATION, Z_g : 47 FT SEISMIC DESIGN PARAMETERS, S_s : 0.167, S_1 : 0.059, T_1 : 6, SITE CLASS: C THIS STRUCTURE HAS BEEN DESIGNED TO SUPPORT THE FOLLOWING LOADS:		
ELEVATION (FT)	ANTENNA TYPE	LINE SIZE (NOM)
TOP	LIGHTNING ROD	-
150 [FUTURE]	(1) OMNI [6 SQFT MAX EPA]	(1) 1-5/8"
146 [FUTURE]	(12) 8 FT PANELS, (6) RRU'S, & (3) RAYCAPS ON A LP PLATFORM	(3) 1-5/8"
136 [FUTURE]	(12) 8 FT PANELS, (6) RRU'S, & (3) RAYCAPS ON A LP PLATFORM	(3) 1-5/8"
130	(1) PCTEL 430-470	(1) 7/8"
126	(9) NHH-65B-R2B, (3) UHBA, (3) UHFA, (3) UHIE, & (2) RAYCAPS ON LP PLATFORM	(9) 1-5/8"
116	(6) EPBQ-654L8H8-L2, (3) HPA-65R-BU8A (1) 4426 B66, (1) 4415 B30, (1) 4449 B5/B12, (1) 4415 B25, (1) 4478 B14, (1) RRU'S E2, & (3) RAYCAPS ON A LP PLATFORM	(8) 3/4"
106	(3) AIR32 KRD901146-1 B66A, (3) APXVAARR24-43-U-NA20, & (3) 4449 B12/B71 ON A LP PLATFORM	(3) 1-5/8"
96 (FUTURE)	(12) 8 FT PANELS, (6) RRU'S, & (3) RAYCAPS ON A LP PLATFORM	(3) 1-5/8"

MAXIMUM ADJUSTED FACTORED REACTIONS	
DOWNLOAD =	140.7 KIPS
SHEAR =	84.8 KIPS
O.T.M. =	9230.4 FT-KIPS

GENERAL NOTES:

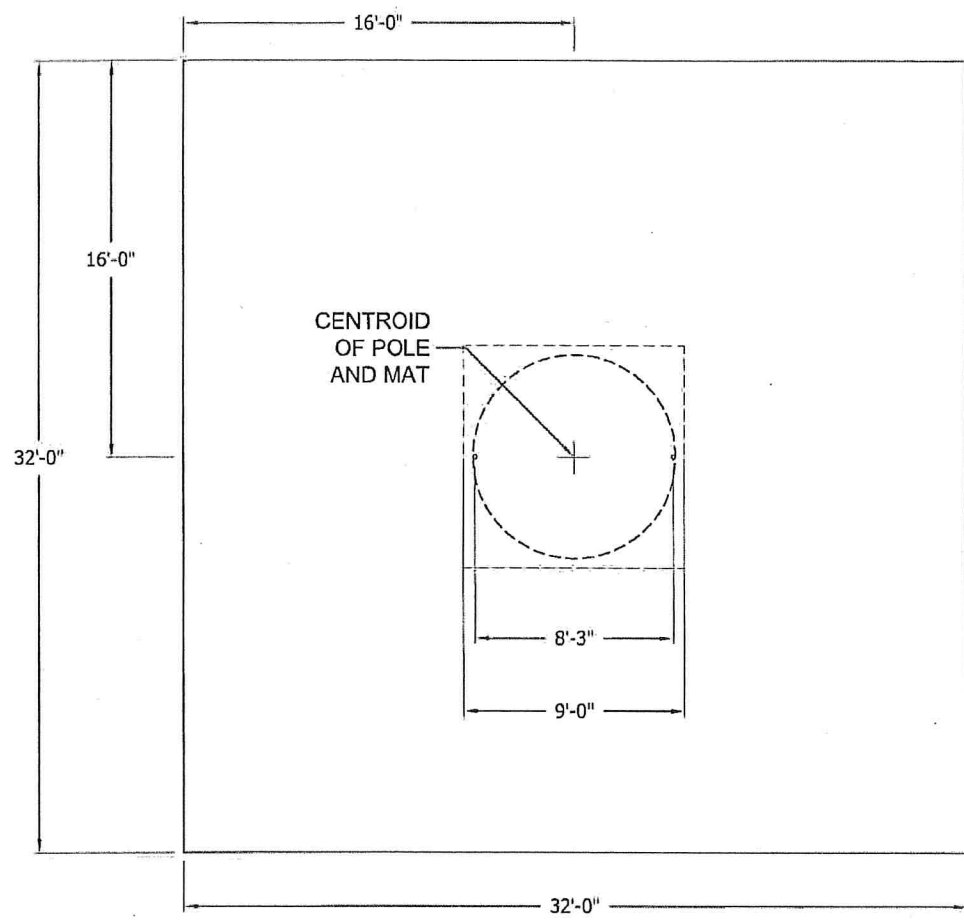
- ROHN PRODUCTS POLE DESIGNS CONFORM TO ANSI/TIA-222-G/H UNLESS OTHERWISE SPECIFIED UNDER POLE DESIGN LOADING.
- THE DESIGN LOADING CRITERIA INDICATED HAS BEEN PROVIDED TO ROHN. THE DESIGN LOADING CRITERIA HAS BEEN ASSUMED TO BE BASED ON SITE-SPECIFIC DATA IN ACCORDANCE WITH ANSI/TIA-222-G/H AND MUST BE VERIFIED BY OTHERS PRIOR TO INSTALLATION.
- ANTENNAS AND LINES LISTED IN POLE DESIGN LOADING TABLE ARE PROVIDED BY OTHERS UNLESS OTHERWISE SPECIFIED.
- STEP BOLTS AND SAFETY CLIMB SYSTEM ARE PROVIDED AS A CLIMBING FACILITY FOR THE INSTALLATION OF THE STRUCTURE.
- POLE MEMBER DESIGN DOES NOT INCLUDE STRESSES DUE TO ERECTION SINCE ERECTION EQUIPMENT AND CONDITIONS ARE UNKNOWN. DESIGN ASSUMES COMPETENT AND QUALIFIED PERSONNEL WILL ERECT THE POLE.
- WORK SHALL BE IN ACCORDANCE WITH ANSI/TIA-222-G/H, "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND ANTENNA SUPPORTING STRUCTURES".
- FIELD CONNECTIONS SHALL BE BOLTED. NO FIELD WELDS SHALL BE ALLOWED.
- STRUCTURAL BOLTS SHALL CONFORM TO GRADE A325 PER ASTM F3125, EXCEPT WHERE NOTED.
- A NUT LOCKING DEVICE SHALL BE PROVIDED FOR ALL STRUCTURAL BOLTS ON THE POLE.
- STRUCTURAL STEEL AND CONNECTION BOLTS SHALL BE HOT-DIPPED GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ANSI/TIA-222-G/H.
- ALL HIGH STRENGTH BOLTS ARE TO BE TIGHTENED TO A "SNUG TIGHT" CONDITION AS DEFINED IN THE RCSC "SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS". NO OTHER MINIMUM BOLT TENSION OR TORQUE VALUES ARE REQUIRED.
- PURCHASER SHALL VERIFY THE INSTALLATION IS IN CONFORMANCE WITH LOCAL, STATE, AND FEDERAL REQUIREMENTS FOR OBSTRUCTION MARKING AND LIGHTING.
- TOLERANCE ON POLE STEEL HEIGHT IS EQUAL TO PLUS 1% OR MINUS 1/2%.
- DESIGN ASSUMES THAT, AS A MINIMUM, MAINTENANCE AND INSPECTION WILL BE PERFORMED OVER THE LIFE OF THE STRUCTURE IN ACCORDANCE WITH ANSI/TIA-222-G/H.
- DESIGN ASSUMES LEVEL GRADE AT POLE SITE.
- FOUNDATIONS SHALL BE DESIGNED TO SUPPORT THE REACTIONS SHOWN FOR THE CONDITIONS EXISTING AT THE SITE.
- DESIGN ASSUMES ALL TRANSMISSION LINES ARE ROUTED INTERNALLY.
- POLE SHAFT CONFORMS TO ASTM A572 GR 65. POLE BASE PLATE AND TOP PLATE STEEL CONFORMS TO ASTM A572 GR 50. POLE ANCHOR BOLTS CONFORM TO ASTM A615 GR 75.
- POLE DESIGN INCLUDES A FUTURE 20 FT EXTENSION TO 150 FT WITH FUTURE ANTENNA LOADING AND LINES.
- POLE DESIGN INCLUDES CONSIDERATION OF A CONTAINED FALL RADIUS EQUAL TO 43 FEET BY PROVIDING STRONGER SECTIONS THAN REQUIRED BY ANALYSIS IN THE LOWER PORTION OF THE POLE.

SECTION	LENGTH (FT)	DIAMETER		WALL THICK (IN)	Fy (KSI)	WEIGHT (KIPS)
		BOT	TOP			
3	46.29	41.53	28.00	0.3125	65.0	5.7
2	48.00	53.78	39.06	0.6250	65.0	15.8
1	48.21	65.00	50.22	0.7500	65.0	23.6

FOR POLYGONAL POLES, DIAMETER IS MEASURED ACROSS FLATS.

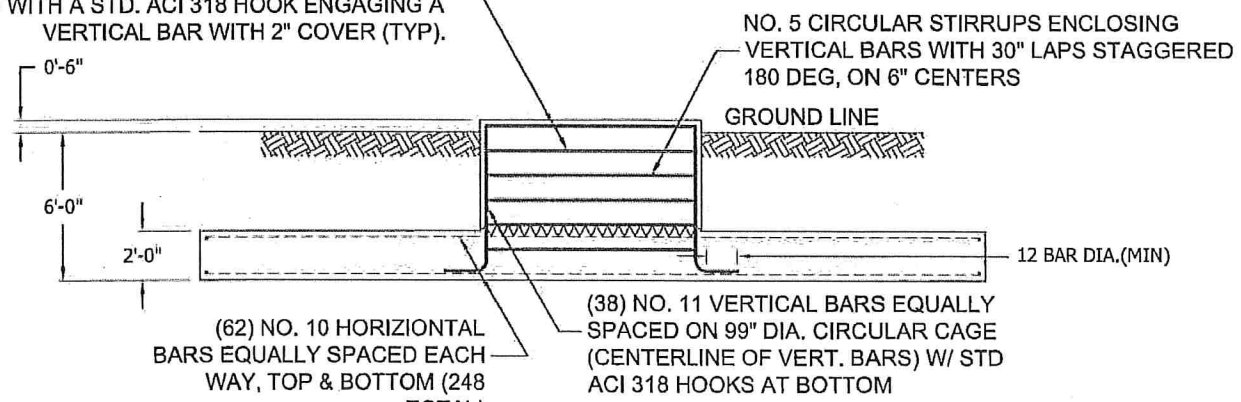
NOTE: TABULATED WEIGHTS ARE APPROXIMATE. REFER TO ASSEMBLY DRAWING FOR FINAL WEIGHTS. ALL WEIGHTS SHALL BE VERIFIED PRIOR TO LIFTING.

FILE NO. 231452				
REVISIONS				
REV.	DESCRIPTION	DWN	CHK	APP
5	ADDED 43 FT FALL RADIUS; REVISED POLE DESIGN DATE: 10/15/2019	SWG	HA	HA
 PO BOX 5999 PEORIA, IL 61601-5999 TOLL FREE 800-727-ROHN <small>THIS DRAWING IS THE PROPERTY OF ROHN. IT IS NOT TO BE REPRODUCED, COPIED OR TRACED IN WHOLE OR IN PART WITHOUT OUR WRITTEN CONSENT.</small> MCM HOLDINGS LLC DESIGN PROFILE 130' TAPERED STEEL POLE WESTBROOK PERMANENT, CT				
DWN:	AS	CHK'D:	HA	DATE: 8/30/2019
ENG'R:	HA	SHEET #: 1 OF 1		
PRJ. ENG'R:	AS	PRJ. MANG'R:		
DRAWING NO:	231452-01-D1			REV: 5



PLAN VIEW

(2) NO. 5 CIRCULAR STIRRUPS ENCLOSING VERTICAL BARS @ 2-1/2" C-C W/ 180 DEG. STAGGERED 6" MIN LAPS TERMINATED AT EACH END WITH A STD. ACI 318 HOOK ENGAGING A VERTICAL BAR WITH 2" COVER (TYP).



ELEVATION VIEW

FACTORED REACTIONS

O.T.M. =	9,230.4 FT-K
DOWNLOAD =	140.7 KIPS
SHEAR =	84.8 KIPS

CONCRETE VOLUME

SQUARE PIER	13.5 CU.YDS
PAD	75.9 CU.YDS
TOTAL	89.4 CU.YDS

GENERAL NOTES

- FOUNDATION DESIGN HAS BEEN DEVELOPED IN ACCORDANCE WITH GENERALLY ACCEPTED PROFESSIONAL ENGINEERING PRINCIPLES AND PRACTICES WITHIN THE LIMITS OF THE SUBSURFACE DATA PROVIDED. FOUNDATION DESIGN MODIFICATIONS MAY BE REQUIRED IN THE EVENT THE FOLLOWING DESIGN PARAMETERS ARE NOT APPLICABLE FOR THE SUBSURFACE CONDITIONS ENCOUNTERED.
 - ULTIMATE SOIL BEARING PRESSURE AT 6 FT DEPTH = 12,000 PSF.
 - GROUND WATER TABLE IS AT 4.0 FT BELOW GRADE.
 - MAXIMUM FROST PENETRATION DEPTH LESS THAN FOUNDATION DEPTH.
- WORK SHALL BE IN ACCORDANCE WITH THE PROJECT CONSTRUCTION DOCUMENTS, LOCAL CODES, SAFETY REGULATIONS AND UNLESS OTHERWISE NOTED, THE LATEST REVISION OF ACI 318, "BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE". PROCEDURES FOR THE PROTECTION OF EXCAVATIONS, EXISTING CONSTRUCTION AND UTILITIES SHALL BE ESTABLISHED PRIOR TO FOUNDATION INSTALLATION.
- CONCRETE MATERIALS SHALL CONFORM TO THE APPROPRIATE STATE REQUIREMENTS FOR EXPOSED STRUCTURAL CONCRETE.
- PROPORTIONS OF CONCRETE MATERIALS SHALL BE SUITABLE FOR THE INSTALLATION METHOD UTILIZED AND SHALL RESULT IN DURABLE CONCRETE FOR RESISTANCE TO LOCAL ANTICIPATED AGGRESSIVE ACTIONS. THE DURABILITY REQUIREMENTS OF ACI 318 SHALL BE SATISFIED BASED ON THE CONDITIONS EXPECTED AT THE SITE. AS A MINIMUM, CONCRETE SHALL DEVELOP A MINIMUM COMPRESSIVE STRENGTH OF 4,500 PSI IN 28 DAYS.
- MAXIMUM SIZE OF AGGREGATE SHALL NOT EXCEED SIZE SUITABLE FOR INSTALLATION METHOD UTILIZED OR 3/4 CLEAR DISTANCE BEHIND OR BETWEEN REINFORCING. WORKABILITY AND METHODS OF CONSOLIDATION SUCH AS VIBRATING SHALL BE UTILIZED TO PREVENT HONEYCOMBS OR VOIDS.
- REINFORCEMENT SHALL BE DEFORMED AND CONFORM TO THE REQUIREMENTS OF ASTM A615 GRADE 60 UNLESS OTHERWISE NOTED. SPLICES IN REINFORCEMENT SHALL NOT BE ALLOWED UNLESS OTHERWISE INDICATED.
- WELDING IS PROHIBITED ON REINFORCING STEEL AND EMBEDMENTS.
- MINIMUM CONCRETE COVER FOR REINFORCEMENT SHALL BE 3 INCHES UNLESS OTHERWISE NOTED. APPROVED SPACERS SHALL BE USED TO INSURE A 3 INCH MINIMUM COVER ON REINFORCEMENT.
- CONCRETE COVER FROM TOP OF FOUNDATION TO ENDS OF VERTICAL REINFORCEMENT SHALL NOT EXCEED 3 INCHES NOR BE LESS THAN 2 INCHES.
- FOUNDATION DESIGN ASSUMES STRUCTURAL BACKFILL TO BE COMPACTED IN 8 INCH MAXIMUM LAYERS TO 95% OF MAXIMUM DRY DENSITY AT OPTIMUM MOISTURE CONTENT IN ACCORDANCE WITH ASTM D1557. ADDITIONALLY, STRUCTURAL BACKFILL MUST HAVE A MINIMUM COMPACTED UNIT WEIGHT OF 110 POUNDS PER CUBIC FOOT.
- FOUNDATION DESIGN HAS BEEN BASED ON GEOTECHNICAL REPORT NO. 92790.00 DATED 3/18/2017 BY NOBIS ENGINEERING, INC.
- FOUNDATION DEPTH INDICATED IS BASED ON THE GRADE LINE DESCRIBED IN THE REFERENCED GEOTECHNICAL REPORT. FOUNDATION MODIFICATION MAY BE REQUIRED IN THE EVENT CUT OR FILL OPERATIONS HAVE TAKEN PLACE SUBSEQUENT TO THE GEOTECHNICAL INVESTIGATION.
- FOUNDATION DESIGN ASSUMES THE RECOMMENDATIONS IN THE REFERENCED GEOTECHNICAL REPORT CONCERNING VERIFICATION OF SUBSURFACE CONDITIONS ARE IMPLEMENTED PRIOR TO PLACEMENT OF CONCRETE.
- FOUNDATION INSTALLATION SHALL BE SUPERVISED BY PERSONNEL KNOWLEDGEABLE AND EXPERIENCED WITH THE PROPOSED FOUNDATION TYPE. CONSTRUCTION SHALL BE IN ACCORDANCE WITH GENERALLY ACCEPTED INSTALLATION PRACTICES.
- ALL CONSTRUCTION AND SAFETY EQUIPMENT AND TEMPORARY SUPPORTS REQUIRED FOR CONSTRUCTION SHALL BE DETERMINED, FURNISHED AND INSTALL BY THE CONTRACTOR BASED ON THE MEANS AND METHODS CHOSEN BY THE CONTRACTOR. ALL CONSTRUCTION ACTIVITIES SHALL BE PERFORMED BY COMPETENT, QUALIFIED AND TRAINED PERSONNEL.
- FOUNDATION DESIGN ASSUMES INSTALLATION PROCEDURES WILL INCORPORATE THE PROCEDURES RECOMMENDED IN THE REFERENCED GEOTECHNICAL REPORT.
- FOUNDATION DESIGN ASSUMES FIELD INSPECTIONS WILL BE PERFORMED TO VERIFY THAT CONSTRUCTION MATERIALS, INSTALLATION METHODS AND ASSUMED DESIGN PARAMETERS ARE ACCEPTABLE BASED ON CONDITIONS EXISTING AT THE SITE.
- FOR FOUNDATION AND ANCHOR TOLERANCES SEE ANCHOR ROD LAYOUT DRAWING.
- LOOSE MATERIAL SHALL BE REMOVED FROM BOTTOM OF EXCAVATION PRIOR TO CONCRETE PLACEMENT. SIDES OF EXCAVATION SHALL BE ROUGH AND FREE OF LOOSE CUTTINGS.
- CONCRETE SHALL BE PLACED IN A MANNER THAT WILL PREVENT SEGREGATION OF CONCRETE MATERIALS, INFILTRATION OF WATER OR SOIL AND OTHER OCCURRENCES WHICH MAY DECREASE THE STRENGTH OR DURABILITY OF THE FOUNDATION.
- CONCRETE PREFERABLY SHALL BE PLACED AGAINST UNDISTURBED SOIL. WHEN FORMS ARE NECESSARY, THEY SHALL BE REMOVED PRIOR TO PLACING STRUCTURAL BACKFILL.
- CONSTRUCTION JOINTS, IF REQUIRED AT THE BASE OF THE PIERS, SHALL BE INTENTIONALLY ROUGHENED TO A FULL AMPLITUDE OF 1/4 INCH. FOUNDATION DESIGN ASSUMES NO OTHER CONSTRUCTION JOINTS.
- TOP OF FOUNDATION SHALL BE SLOPED TO DRAIN WITH A FLOATED FINISH.
- EXPOSED EDGES OF CONCRETE SHALL BE CHAMFERED 3/4" X 3/4" MINIMUM.

NOTE: SEE STRUCTURE ASSEMBLY DRAWING FOR FOUNDATION LAYOUT AND ANCHORAGE EMBEDMENT DRAWING NUMBER.

FILE NO. 231452					
REVISIONS					
REV	DESCRIPTION	DWN	CHK	APP	
5	POLE REVISED TO MEET FALL RADIUS REQ.	SWG	HA	HA	
DATE: 10/17/2019					
<p>ROHN PRODUCTS LLC</p> <p>PO BOX 5999 PEORIA, IL 61601-5999 TOLL FREE 800-727-ROHN</p> <p>THIS DRAWING IS THE PROPERTY OF ROHN. IT IS NOT TO BE REPRODUCED, COPIED OR TRACED IN WHOLE OR IN PART WITHOUT OUR WRITTEN CONSENT.</p> <p>MCM HOLDINGS LLC MAT W/RAISED PIER FOUNDATION DESIGN WESTBROOK PERMANENT, CT</p>					
DWN:	AS	CHK'D:	HA	DATE:	8/30/2019
ENG'R:	HA	SHEET #:		1 OF 1	
PRJ. ENG'R:	AS	PRJ. MANG'R:			
DRAWING NO:				REV:	
231452-01-F1				5	



1 Fairholm Avenue
Peoria, IL 61603 USA
Phone 309-566-3000
FAX 309-566-3079
Toll Free 800-727-ROHN

October 17, 2019

MCM Holdings
40 Woodland St
Hartford, CT 06105

Attn: Virginia King

Reference: 130' Tapered Steel Pole
Site Name: Westbrook Permanent
Middlesex County, CT
File # 231452

Dear Ms. King

The referenced pole is designed to meet the specified loading requirements in accordance with ANSI/TIA-222-G & H for a 135 MPH ASCE 7-16 Factored wind speed with no ice and a 50 MPH 3-second gust wind speed with 1.0 inch radial ice, Structure Class: II; Exposure Category: D and Topographic Category: 1.

It is our understanding that the design of the referenced pole requires consideration of a contained fall radius in the event that a catastrophic wind speed would result in collapse. Although the pole is not designed to fail, stronger sections than required by analysis is provided in the lower sections of the pole. This will result in an increased safety factor in the lower sections. This design enables the pole to fail through a combination of bending and buckling in the upper portion of the pole under a catastrophic wind loading. Failure in this manner will result in the upper portion of the pole folding over the lower portion, resulting in a fall radius no greater than **43** ft. The failure mode will theoretically be a local buckling failure involving a crippling of the pole wall on one side of the pole as opposed to the pole shearing off or completely breaking off and hitting the ground.

Please contact us at your convenience should you have further questions concerning the safety of pole structures or other aspects of pole design.

Sincerely,



Habib Azouri, P.E.
Engineering Manager

cc: JD Long





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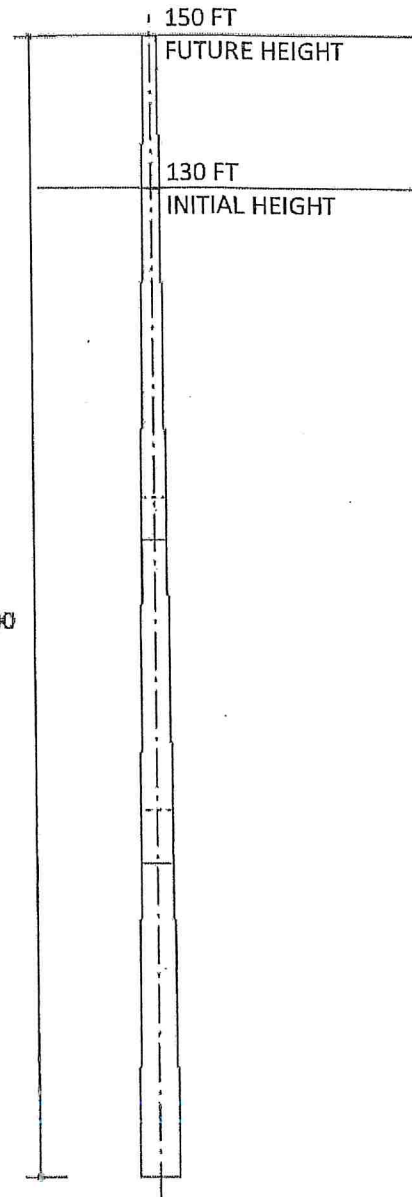
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File: W:\Jobs\2019\231452\231452 REV H R5.out
 Contract: 231452
 Project: 130 FT OF 150 FT TSP
 Date and Time: 10/17/2019 9:46:26 AM

Revision: 4
 Site: WESTBROOK PERMANENT- CT
 Engineer: AS *HA*

DESIGN SPECIFICATION

Sct	Length (ft)	Overlap (ft)	Top Dia (in)	Bot Dia (in)	Thick. (in)
4	20.00	0.00	22.00	28.00	0.2500 (FUTURE)
3	46.29	0.00	28.00	41.84	0.3125
2	48.00	5.50	39.57	53.93	0.6250
1	48.21	7.00	50.58	65.00	0.7500



MAXIMUM BASE REACTIONS

		<u>ADJUSTED REACTIONS</u>
Download (Kips)	124.1	140.7
Shear (Kips)	74.8	84.8
Moment (Kipsft)	8140.3	9230.4



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 Contract: 231452
 Project: 130 FT OF 150 FT TSP
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Revision: 4
 Site: WESTBROOK PERMANENT- CT
 Engineer: AS

Section A: PROJECT DATA

Project Title: 130 FT OF 150 FT TSP
 Customer Name: MCM HOLDINGS LLC
 Site: WESTBROOK PERMANENT- CT
 Contract No.: 231452
 Revision: 4
 Engineer: AS
 Date: Oct 17 2019
 Time: 09:46:07 AM

Design Standard: ANSI/TIA-222-H-2017

GENERAL DESIGN CONDITIONS

Start wind direction: 0.00 (Deg)
 End wind direction: 315.00 (Deg)
 Increment wind direction: 45.00 (Deg)
 Elevation above ground: 0.00 (ft)
 Gust Response Factor Gh: 1.10
 Structure class: II
 Exposure category: D
 Topographic category: 1
 Material Density: 490.1 (lbs/ft^3)
 Young's Modulus: 29000.0 (ksi)
 Poisson Ratio: 0.30
 Weight Multiplier: 1.06

WIND ONLY CONDITIONS:

Basic Wind Speed (No Ice): 135.00 (mph)
 Directionality Factor Kd: 0.95
 Importance Factor I: 1.00
 Wind Load Factor: 1.00
 Dead Load Factor: 1.20

WIND AND ICE CONDITIONS:

Basic Wind Speed (With Ice): 50.00 (mph)
 Directionality Factor Kd: 0.95
 Wind Load Importance Factor Iw: 1.00
 Ice Thickness Importance Factor Ii: 1.00
 Ice Thickness: 1.00 (in)
 Ice Density: 56.19 (lbs/ft^3)
 Wind Load Factor: 1.00
 Dead Load Factor: 1.20
 Ice Load Factor: 1.00

WIND ONLY SERVICEABILITY CONDITIONS:

Serviceability Wind Speed: 60.00 (mph)
 Directionality Factor Kd: 0.85
 Importance Factor I: 1.00
 Wind Load Factor: 1.00
 Dead Load Factor: 1.00

EARTHQUAKE CONDITIONS:

Site class definition: C
 Spectral response acceleration Ss: 0.167
 Spectral response acceleration S1: 0.059
 Acceleration-based site coefficient Fa: 1.300
 Velocity-based site coefficient Fv: 1.500
 Design spectral response acceleration Sds: 0.145
 Design spectral response acceleration Sd1: 0.059
 Seismic analysis method: 1
 Fundamental frequency of structure f1: 0.578



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Contract: 231452
Project: 130 FT OF 150 FT TSP
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Revision: 4
Site: WESTBROOK PERMANENT- CT
Engineer: AS

Total seismic shear Vs (Kips) : 2.12
Analysis performed using: TowerSoft Finite Element Analysis Program



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 Engineer: AS

Section B: STRUCTURE GEOMETRY

Total Height (ft)	Bottom Diameter (in)	Top Diameter (in)
150.00	65.00	22.00

Sect. No	Length (ft)	Overlap (ft)	Bot Dia. (in)	Top Dia. (in)	Thick. (in)	Sides	Joint Type	Yield Stress (ksi)	Mass (lbs)	Calculated Taper (in/ft)	Corner Radius (in)
4	20.00	0.00	28.00	22.00	0.2500	18-sided	Flange	65.0	1416.8	0.30000	1.88
3	46.29	0.00	41.84	28.00	0.3125	18-sided	Telescopic	65.0	5731.9	0.29904	1.88
2	48.00	5.50	53.93	39.57	0.6250	18-sided	Telescopic	65.0	15842.8	0.29904	2.50
1	48.21	7.00	65.00	50.58	0.7500	18-sided	Flange	65.0	23613.9	0.29904	2.50

Total Mass: 46605.4



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 Site: WESTBROOK PERMANENT- CT
 Engineer: AS

Section D: TRANSMISSION LINE DATA

Transmission Lines Position

No.	Bot El (ft)	Top El (ft)	Desc.	Radius (ft)	Az.	Orient.	No.	Shielded	Shielded Lines	Antenna
1	0.00	150.00	3/8" CABLE	3.00	0.00	0.00	1	No	0	
2	0.00	150.00	LDF7P-50A	0.00	0.00	0.00	1	Yes	1	
3	0.00	146.00	LDF7P-50A	0.00	0.00	0.00	3	Yes	3	
4	0.00	136.00	LDF7P-50A	0.00	0.00	0.00	3	Yes	3	
5	0.00	130.00	LDF5P-50A	0.00	0.00	0.00	1	Yes	1	
6	0.00	126.00	LDF7P-50A	0.00	0.00	0.00	9	Yes	9	
7	0.00	116.00	LDF5P-50A	0.00	0.00	0.00	8	Yes	8	
8	0.00	106.00	LDF7P-50A	0.00	0.00	0.00	3	Yes	3	
9	0.00	96.00	LDF7P-50A	0.00	0.00	0.00	3	Yes	3	

Transmission Lines Details

No.	Desc.	Width (in)	Depth (in)	Unit Mass (lb/ft)
1	3/8" CABLE	0.38	0.38	1.00
2	LDF7P-50A	2.01	2.01	0.92
3	LDF7P-50A	2.01	2.01	0.92
4	LDF7P-50A	2.01	2.01	0.92
5	LDF5P-50A	1.10	1.10	0.33
6	LDF7P-50A	2.01	2.01	0.92
7	LDF5P-50A	1.10	1.10	0.33
8	LDF7P-50A	2.01	2.01	0.92
9	LDF7P-50A	2.01	2.01	0.92

Utilization of the cross-section for TX Lines: 7.24%



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 Engineer: AS

Section F: POINT LOAD DATA

Structure Azimuth from North:0.00

POINT LOADS

No.	Description	Elev. (ft)	Radius (ft)	Azim. (Deg)	Orient. (Deg)	Vertical Offset (ft)	Tx Line	Comments
1	LIGHTNING ROD	150.00	0.00	0.0	0.0	0.00		
2	(1) OMNI [6 SQFT]	150.00	0.00	0.0	0.0	0.00		
3	CARRIER	146.00	1.00	0.0	0.0	0.00		
4	CARRIER	136.00	1.00	120.0	120.0	0.00		
5	(1) 430-470	130.00	1.00	0.0	0.0	0.00		
6	CARRIER	126.00	1.00	240.0	240.0	0.00		
7	CARRIER	116.00	1.00	0.0	0.0	0.00		
8	CARRIER	106.00	1.00	120.0	120.0	0.00		
9	CARRIER	96.00	1.00	240.0	240.0	0.00		

POINT LOADS WIND AREAS AND WEIGHTS

No.	Description	Frontal Bare Area (ft^2)	Lateral Bare Area (ft^2)	Frontal Iced Area (ft^2)	Lateral Iced Area (ft^2)	Weight Bare (Kips)	Weight Iced (Kips)	Gh
1	LIGHTNING ROD	1.00	1.00	2.00	2.00	0.10	0.20	1.10
2	(1) OMNI [6 SQFT]	6.00	6.00	12.00	12.00	0.10	0.20	1.10
3	CARRIER	138.00	138.00	206.50	206.50	3.60	8.90	1.10
4	CARRIER	138.00	138.00	206.50	206.50	3.60	8.90	1.10
5	(1) 430-470	1.50	1.50	3.00	3.00	0.05	0.10	1.10
6	CARRIER	97.00	97.00	154.00	154.00	3.35	8.60	1.10
7	CARRIER	132.50	132.50	193.50	193.50	3.30	7.65	1.10
8	CARRIER	83.00	83.00	131.50	131.50	3.30	7.70	1.10
9	CARRIER	138.00	138.00	206.50	206.50	3.60	8.90	1.10



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Section H: STRUCTURE DISPLACEMENT DATA
 Load Combination Wind Only - Serviceability

Elev. (ft)	Maximum displacements					
	N-S Disp (in)	W-E Disp (in)	Vert. Disp (in)	N-S Rot (deg)	W-E Rot (deg)	Twist Rot (deg)
150.00	-16.5	16.6	-0.1	1.06	1.06	0.01
146.67	-15.8	15.8	-0.1	1.06	1.06	0.01
143.33	-15.1	15.1	-0.1	1.06	1.06	0.01
140.00	14.3	14.3	-0.1	1.05	1.05	0.01
136.67	13.6	13.6	-0.1	1.04	1.04	0.01
133.33	12.9	12.9	-0.1	1.03	1.02	-0.01
130.00	12.2	12.2	-0.1	1.01	1.00	0.00
121.84	10.5	10.5	-0.1	0.95	0.95	0.00
113.68	8.9	8.9	-0.1	0.89	0.88	0.00
105.53	7.5	7.5	0.0	0.80	-0.80	0.00
97.37	6.2	-6.2	0.0	0.71	-0.71	0.00
89.21	5.1	-5.1	0.0	-0.61	-0.61	0.00
83.71	4.4	-4.4	0.0	-0.54	-0.54	0.00
76.61	3.6	-3.6	0.0	-0.49	-0.49	0.00
69.51	3.0	-2.9	0.0	-0.43	-0.43	0.00
62.41	2.3	-2.3	0.0	-0.38	-0.38	0.00
55.31	1.8	-1.8	0.0	-0.33	-0.33	0.00
48.21	1.4	-1.4	0.0	-0.28	-0.28	0.00
41.21	1.0	-1.0	0.0	-0.23	-0.23	0.00
34.34	0.7	-0.7	0.0	-0.19	-0.19	0.00
27.47	0.4	-0.4	0.0	-0.15	-0.15	0.00
20.61	0.2	-0.2	0.0	-0.11	-0.11	0.00
13.74	0.1	-0.1	0.0	-0.07	-0.07	0.00
6.87	0.0	0.0	0.0	-0.04	-0.04	0.00
0.00	0.0	0.0	0.0	0.00	0.00	0.00



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 Engineer: AS

Section K: POLE OUTPUT LOAD DATA

Load Combination	Max Envelope			
Wind Direction	Maximum			
Elev. (ft)	Axial Ld. (kips)	Shear Ld. (kips)	Torque (kipsft)	Bend Mom. (kipsft)
150.00	0.63	0.71	0.00	0.00
146.67	0.63	0.71	0.00	2.36
146.67	8.68	9.56	8.52	8.37
143.33	8.68	9.56	8.52	37.38
143.33	11.01	12.04	10.65	38.22
140.00	11.01	12.04	10.65	78.35
140.00	11.44	12.39	10.64	78.33
136.67	11.44	12.39	10.64	119.24
136.67	19.55	21.17	9.70	118.87
133.33	19.55	21.17	9.69	189.46
133.33	21.94	23.65	10.24	189.67
130.00	21.94	23.65	10.23	268.52
130.00	27.75	28.20	6.67	266.51
121.84	27.75	28.20	6.66	495.15
121.84	36.21	35.59	5.13	494.01
113.68	36.21	35.59	5.12	783.66
113.68	44.35	43.95	11.35	786.17
105.53	44.35	43.95	11.36	1143.96
105.53	54.07	50.74	11.64	1144.19
97.37	54.07	50.74	11.64	1555.56
97.37	64.06	59.90	4.36	1552.70
89.21	64.06	59.90	4.37	2040.53
89.21	67.44	62.36	3.55	2040.83
83.71	67.44	62.36	3.55	2383.55
83.71	70.76	63.26	3.54	2383.70
76.61	70.76	63.26	3.55	2830.74
76.61	75.01	64.34	3.54	2830.90
69.51	75.01	64.34	3.55	3285.63
69.51	78.42	65.39	3.54	3285.77
62.41	78.42	65.39	3.54	3750.09
62.41	81.98	66.44	3.54	3750.21
55.31	81.98	66.44	3.54	4219.90
55.31	85.68	67.49	3.54	4220.00
48.21	85.68	67.49	3.54	4699.43
48.21	89.49	68.53	3.54	4699.52
41.21	89.49	68.53	3.54	5177.48
41.21	95.56	69.59	3.54	5177.55
34.34	95.56	69.59	3.54	5653.85
34.34	101.99	70.60	3.54	5653.91
27.47	101.99	70.60	3.54	6139.62
27.47	106.67	71.56	3.54	6139.66
20.61	106.67	71.56	3.54	6629.71
20.61	111.49	72.47	3.54	6629.74
13.74	111.49	72.47	3.54	7126.22
13.74	116.45	73.36	3.54	7126.23
6.87	116.45	73.36	3.54	7631.37
6.87	121.54	74.24	3.54	7631.30
0.00	121.54	74.24	3.54	8140.29
Base	124.10	74.82	3.54	8140.30



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Revision: 4
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 Engineer: AS

Section I: STRENGTH ASSESSMENT DATA

Load Combination	Max Envelope				
Wind Direction	Maximum				
Elev. (ft)	Axial Ld. (kips)	Axial Cap (kips)	Moment (kipsft)	Mom. Cap (kipsft)	Assess.
150.00	0.63	1282.19	0.00	571.60	0.000
146.67	0.63	1341.14	2.36	625.68	0.002
146.67	8.68	1341.14	8.37	625.68	0.020
143.33	8.68	1400.09	37.38	682.19	0.029
143.33	11.01	1400.09	38.22	682.19	0.060
140.00	11.01	1459.04	78.35	741.16	0.110
140.00	11.44	1459.04	78.33	741.16	0.110
136.67	11.44	1511.26	119.24	799.01	0.153
136.67	19.55	1511.26	118.87	799.01	0.157
133.33	19.55	1554.11	189.46	853.87	0.230
133.33	21.94	1554.11	189.67	853.87	0.231
130.00	21.94	1595.77	268.52	909.83	0.304
130.00	27.75	2040.26	266.51	1158.08	0.239
121.84	27.75	2220.03	495.15	1372.36	0.369
121.84	36.21	2220.03	494.01	1372.36	0.371
113.68	36.21	2381.85	783.66	1592.82	0.502
113.68	44.35	2381.85	786.17	1592.82	0.507
105.53	44.35	2509.68	1143.97	1805.20	0.646
105.53	54.07	2509.68	1144.19	1805.20	0.650
97.37	54.07	2630.46	1555.56	2025.08	0.783
97.37	64.06	2630.46	1552.70	2025.08	0.786
89.21	64.06	2744.19	2040.53	2251.40	0.924
89.21	67.44	2744.19	2040.83	2251.40	0.926
83.71	70.76	5982.43	2383.70	4958.82	0.488
76.61	70.76	6295.34	2830.74	5495.14	0.522
76.61	75.01	6295.34	2830.90	5495.14	0.523
69.51	75.01	6608.25	3285.63	6059.01	0.550
69.51	78.42	6608.25	3285.78	6059.01	0.550
62.41	78.42	6921.16	3750.09	6650.41	0.571
62.41	81.98	6921.16	3750.21	6650.41	0.572
55.31	81.98	7234.07	4219.90	7269.37	0.588
55.31	85.68	7234.07	4220.01	7269.37	0.589
48.21	85.68	7546.98	4699.43	7915.86	0.602
48.21	89.49	7546.98	4699.52	7915.86	0.602
41.21	95.56	9183.40	5177.55	9746.40	0.539
34.34	95.56	9546.64	5653.85	10538.21	0.544
34.34	101.99	9546.64	5653.91	10538.21	0.544
27.47	101.99	9909.88	6139.62	11360.95	0.548
27.47	106.67	9909.88	6139.66	11360.95	0.548
20.61	106.67	10273.12	6629.71	12214.62	0.550
20.61	111.49	10273.12	6629.74	12214.62	0.551
13.74	111.49	10636.35	7126.22	13099.22	0.552
13.74	116.45	10636.35	7126.23	13099.22	0.552
6.87	116.45	10999.59	7631.37	14014.74	0.552
6.87	121.54	10999.59	7631.30	14014.74	0.553
0.00	121.54	11362.83	8140.29	14961.21	0.552



TSTower - v 5.8.5 Tower Analysis Program
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Manufactured by
 Licensed to: ROHN Products LLC
 Peoria, IL

File: W:\Jobs\2019\231452\231452 REV H R5.out
 Contract: 231452
 Project: 130 FT OF 150 FT TSP
 Date and Time: 10/17/2019 9:46:26 AM

Revision: 4
 Site: WESTEROCK PERMANENT- CT
 Engineer: AS

Section M: SECTION PROPERTIES DATA

Elev. (ft)	Diam. (in)	Width (in)	Thick. (in)	W/t	Area (in^2)	S (in^3)
150.0	22.0	3.4	0.250	13.5	17.3	92.32
146.7	23.0	3.6	0.250	14.2	18.1	101.06
146.7	23.0	3.6	0.250	14.2	18.1	101.06
143.3	24.0	3.7	0.250	14.9	18.8	110.19
143.3	24.0	3.7	0.250	14.9	18.8	110.19
140.0	25.0	3.9	0.250	15.6	19.6	119.71
140.0	25.0	3.9	0.250	15.6	19.6	119.71
136.7	26.0	4.1	0.250	16.3	20.4	129.63
136.7	26.0	4.1	0.250	16.3	20.4	129.63
133.3	27.0	4.3	0.250	17.0	21.2	139.94
133.3	27.0	4.3	0.250	17.0	21.2	139.94
130.0	28.0	4.4	0.250	17.7	22.0	150.65
130.0	28.0	4.3	0.313	13.8	27.5	187.05
121.8	30.4	4.7	0.313	15.2	29.9	221.66
121.8	30.4	4.7	0.313	15.2	29.9	221.66
113.7	32.9	5.2	0.313	16.6	32.3	259.21
113.7	32.9	5.2	0.313	16.6	32.3	259.21
105.5	35.3	5.6	0.313	17.9	34.7	299.69
105.5	35.3	5.6	0.313	17.9	34.7	299.69
97.4	37.8	6.0	0.313	19.3	37.1	343.11
97.4	37.8	6.0	0.313	19.3	37.1	343.11
89.2	40.2	6.5	0.313	20.7	39.6	389.47
89.2	40.2	6.5	0.313	20.7	39.6	389.47
83.7	41.8	6.8	0.313	21.6	41.2	422.38
83.7	41.2	6.0	0.625	9.6	80.5	800.94
76.6	43.3	6.4	0.625	10.2	84.7	887.56
76.6	43.3	6.4	0.625	10.2	84.7	887.56
69.5	45.5	6.8	0.625	10.8	88.9	978.64
69.5	45.5	6.8	0.625	10.8	88.9	978.64
62.4	47.6	7.1	0.625	11.4	93.2	1074.16
62.4	47.6	7.1	0.625	11.4	93.2	1074.16
55.3	49.7	7.5	0.625	12.0	97.4	1174.13
55.3	49.7	7.5	0.625	12.0	97.4	1174.13
48.2	51.8	7.9	0.625	12.6	101.6	1278.55
48.2	51.8	7.9	0.625	12.6	101.6	1278.55
41.2	53.9	8.3	0.625	13.2	105.7	1385.86
41.2	52.7	7.8	0.750	10.4	123.6	1574.22
34.3	54.7	8.2	0.750	10.9	128.5	1702.11
34.3	54.7	8.2	0.750	10.9	128.5	1702.11
27.5	56.8	8.5	0.750	11.4	133.4	1835.00
27.5	56.8	8.5	0.750	11.4	133.4	1835.00
20.6	58.8	8.9	0.750	11.8	138.3	1972.88
20.6	58.8	8.9	0.750	11.8	138.3	1972.88
13.7	60.9	9.2	0.750	12.3	143.2	2115.76
13.7	60.9	9.2	0.750	12.3	143.2	2115.76
6.9	62.9	9.6	0.750	12.8	148.1	2263.63
6.9	62.9	9.6	0.750	12.8	148.1	2263.63
0.0	65.0	10.0	0.750	13.3	152.9	2416.50

Note: w/t values marked with * (asterisk) indicate width to thickness exceeding maximum allowable values by standards.

Customer: MCM HOLDINGS LLC
 Project: 130 FT OF 150 FT TSP
 Site: WESTBROOK PERMANENT- CT
 Engr. File: 231452 *RS*
 Build Code: ANSI/TIA-222-G-2005



Mat Foundation

ver.2.2.14

Design Parameters

RS

Description	Load Case					
	1	2	3	4	5	Service
Total Moment, ft-kips	9,230.36	9,178.26	2,084.96	245.51	243.32	1,436.15
Total Shear, kips	84.84	84.81	19.32	2.12	2.12	13.22
Total Tower Wt, kips	96.23	72.14	140.72	87.05	61.71	70.84
Max. Uplift, kips	N/A	N/A	N/A	N/A	N/A	N/A
Shear, kips	N/A	N/A	N/A	N/A	N/A	N/A
Max Download, kips	N/A	N/A	N/A	N/A	N/A	N/A
Shear	N/A	N/A	N/A	N/A	N/A	N/A
Soil L.F.	1.20	0.90	1.20	1.20	0.90	1.00
Concrete L.F.	1.20	0.90	1.20	1.20	0.90	1.00

Foundation	
Ht. AGL, ft	0.50
Depth, ft	6.00
Pole	
Butt OD, ft	5.42
Offset, in	.00
Soil	
Blow Count	N/A
Inplace Unit Wt, pcf	110.00
Submerged Unit Wt, pcf	47.60
Friction Angle, ϕ , deg.	30.00
Cohesion, ksf	N/A
Uplift Angle, deg.	30.00
Water Depth, ft	4.00
Ult Bearing Capacity, ksf	12.00

Mat	
Thickness, ft	2.00
Width, ft	32.00
EA, in	23.00
Batter, in/ft	0.00

Pier	
Height, ft	4.50
Diameter, ft	9.00
No. Piers	1
Shape	Square

Anchor Bolts	
Diameter, in	2.2500
No.	22
Length, in	84.00
Bolt Circle, in	71.50
Projection, in	13.00

Pocket	
Diameter, in	N/A
Thickness, ft	N/A

Concrete	
28 Day Strength, ksi	4.50
Dry Unit Wt, pcf	150.00
Wet Unit Wt, pcf	88.00

Rebar Fy	
Vertical, ksi	60.00
Circular, ksi	60.00
Horizontal, ksi	60.00

Results

ϕM_N - Parallel Axis 10,126.51 ft-kips
 ϕM_N - Diagonal Axis 11,147.33 ft-kips
 Moment - Interaction Ratio 0.961
 ϕV_N - Lateral Load 174.26 kips
 Lateral Load - Interaction Ratio 0.487

Final Mat Dimension : 32.00 x 32.00 x 2.00 ft. thick w/ (1) 9.00 ft. Square Pier

Final Pocket Dimension : Pockets not required

Total Volume of Concrete : 89.4 yd³

Designed By: AS
 Date: 17 Oct, 19 @ 10:54 AM

Checked By: *HA*
 Date: *10/17/19*

Customer: MCM HOLDINGS LLC
 Project: 130 FT OF 150 FT TSP
 Site: WESTBROOK PERMANENT- CT
 Engr. File: 231452
 Build Code: ANSI/TIA-222-G-2005



Mat Foundation

ver.2.2.14

OTM Capacity

Controlling Load Case: 2 [Wind w/Min. Dead Load]
 Foundation Width = 32.00 ft
 $M_U = 9,729.5$ ft-kips

	ϕM_N , ft-kips	x, ft	N	σ_{IR}
Parallel	10,126.5	3.200	0.100	8.97
Diagonal	11,147.3	10.119	0.224	8.97

$\phi M_N = 10,126.51$ ft-kips IRatio = 0.961
 $\phi V_N = 174.26$ kips IRatio = 0.487

Mat Design

$\gamma_c = 102.67$ pcf

Exterior Slab	x, ft	N	σ_R , ksf	P_s , kips	P_{su} , kips	Moment, ft-kips/ft		Shear, kips/ft	
						DownLoad Side	Uplift Side	DownLoad Side	Uplift Side
Parallel	4.271	0.133	5.04	25.31	0.00	164.74	57.88	20.41	9.28
Diagonal	13.145	0.290	3.98	25.31	0.00	104.23	34.24	22.54	7.39

Punching Shear	Download			Uplift			Description
	Interior	Edge	Corner	Interior	Edge	Corner	
b_{in} , ft	42.33	N/A	N/A	N/A	N/A	N/A	2-Way Shear
V_{su} , psi	129.06	N/A	N/A	N/A	N/A	N/A	
ϕV_c , psi	199.34	N/A	N/A	N/A	N/A	N/A	
IR	0.65	N/A	N/A	N/A	N/A	N/A	
$0.5 * M_{ult}$, ft-kips	2,883.6			N/A			Moment transfer to slab
B_e , ft	15.0			N/A			
M_{in} , ft-kips/ft	192.2			N/A			
Edge Distances: a = 16.00 ft. b = 16.00 ft. c = 16.00 ft.							

Summary	Max. Value	Utilization
Slab Moment, ft-kips/ft	192.24	0.987
Slab Shear, kips/ft	22.54	0.867
Punching Shear, psi	129.06	0.647
Soil Bearing Required, σ_{UR} , ksf	6.71	0.559

Mat Reinforcement	
Min. Steel Area (Strength)	2.415 in ² /ft.
Min. Steel Area (Temperature)	.259 in ² /ft.
Steel Strain Actual	0.010
Minimum Steel Strain Required	0.005

62 - #10 Horizontal bars equally spaced @6.20 in., each way, top and bottom, total of 248, $A_s = 2.454$ in²/ft

Designed By: AS
 Date: 17 Oct,19 @ 10:54 AM

Checked By: HA
 Date: 10/17/19

Customer: MCM HOLDINGS LLC
Project: 130 FT OF 150 FT TSP
Site: WESTBROOK PERMANENT- CT
Engr. File: 231452
Build Code: ANSI/TIA-222-G-2005



Mat Foundation

ver.2.2.14

Pier Design

Controlling Load Case: 1 [Wind w/Max. Dead Load]

C = 96.23 kips	Vc = 84.84 kips	Mc = 9,612.14 ft-kips
T = .00 kips	Vt = .00 kips	Mt = .00 ft-kips
Fy = 60.00 ksi	Fyt = 60.00 ksi	L.F. = 1.00
H = 108.00 in.	Ds = 99.00 in.	F'c = 4.50 ksi
U = 1.00	Irs = Square	

*** NOTE: Pier cross section is Square ***

SUMMARY OF ANALYSIS

Minimum area of steel required	= 58.320 in ²	(Rhomin = 0.0050)
Area of steel provided.	= 59.335 in ²	(Rhoactual = 0.0051)
Maximum steel area limit	= 732.872 in ²	(Rhomax = 0.0628)

(38) #11 Vertical Bars equally spaced w/ #5 Circular Ties @ 6" on center.

CIRCULAR TIE DATA

$V_u < 0.85 * V_c / 2$, shear reinforcement is not required

Use maximum tie spacing specified in ACI 318,
Section 7.10.5 for compression reinforcement.

DEVELOPMENT LENGTH MODIFIERS FOR BAR DEVELOPMENT

Modifier for tension development = 0.859

Modifier for compression development = 0.505

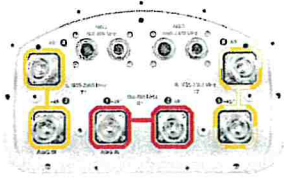
REQUIRED Ld = MODIFIER * BASIC Ld * ACI 318 MODIFIERS, (12 in. min.)

Designed By: AS
Date: 17 Oct,19 @ 10:54 AM

Checked By: HA
Date: 10/17/19

4

NHH-65B-R2B



6-port sector antenna, 2x 698–896 and 4x 1695–2360 MHz, 65° HPBW, 2x RET. Both high bands share the same electrical tilt.

- Interleaved dipole technology providing for attractive, low wind load mechanical package
- Internal SBT on low and high band allow remote RET control from the radio over the RF jumper cable
- Separate RS-485 RET input/output for low and high band
- One RET for low band and one RET for both high bands to ensure same tilt level for 4x Rx or 4x MIMO

Electrical Specifications

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2200	2300–2360
Gain, dBi	14.9	15.0	17.7	17.9	18.4	18.7
Beamwidth, Horizontal, degrees	65	60	71	69	64	57
Beamwidth, Vertical, degrees	12.4	11.2	5.7	5.2	4.9	4.6
Beam Tilt, degrees	0–14	0–14	0–7	0–7	0–7	0–7
USLS (First Lobe), dB	13	14	18	18	19	18
Front-to-Back Ratio at 180°, dB	30	29	31	30	29	31
Isolation, Cross Polarization, dB	25	25	25	25	25	25
Isolation, Inter-band, dB	30	30	30	30	30	30
VSWR Return Loss, dB	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0
PIM, 3rd Order, 2 x 20 W, dBc	-153	-153	-153	-153	-153	-153
Input Power per Port at 50°C, maximum, watts	300	300	300	300	300	300
Polarization	±45°	±45°	±45°	±45°	±45°	±45°
Impedance	50 ohm	50 ohm	50 ohm	50 ohm	50 ohm	50 ohm

Electrical Specifications, BASTA*

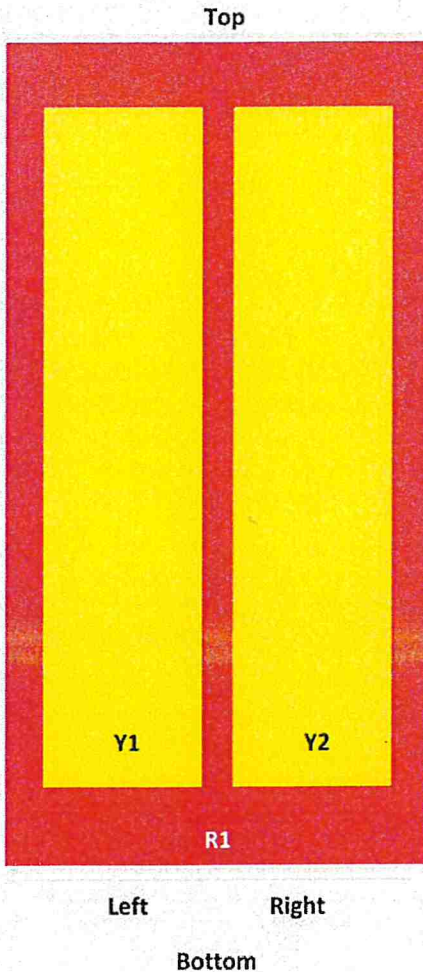
Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2200	2300–2360
Gain by all Beam Tilts, average, dBi	14.5	14.5	17.3	17.7	18.1	18.5
Gain by all Beam Tilts Tolerance, dB	±0.6	±1.1	±0.4	±0.4	±0.5	±0.3
Gain by Beam Tilt, average, dBi	0° 14.4 7° 14.6 14° 14.3	0° 14.7 7° 14.7 14° 14.1	0° 17.2 4° 17.3 7° 17.3	0° 17.6 4° 17.7 7° 17.7	0° 18.0 4° 18.2 7° 18.1	0° 18.3 4° 18.5 7° 18.6
Beamwidth, Horizontal Tolerance, degrees	±2	±2.1	±3	±4.1	±6.5	±2.9
Beamwidth, Vertical Tolerance, degrees	±0.7	±0.7	±0.3	±0.2	±0.3	±0.2
USLS, beampeak to 20° above beampeak, dB	13	14	16	16	17	15
Front-to-Back Total Power-at 180° ± 30°, dB	23	22	27	27	25	25
CPR at Boresight, dB	22	21	23	23	22	19
CPR at Sector, dB	10	7	16	13	11	4

* CommScope® supports NGMN recommendations on Base Station Antenna Standards (BASTA). To learn more about the benefits of BASTA, [download the whitepaper Time to Raise the Bar on BSAs](#).

Array Layout

NHH-65B-R2B

NHH



Array	Freq (MHz)	Conns	RET (SRET)	AISG RET UID
R1	698-896	1-2	1	ANXXXXXXXXXXXXXXXXX1
Y1	1695-2360	3-4	2	ANXXXXXXXXXXXXXXXXX2
Y2	1695-2360	5-6		

View from the front of the antenna
 (Sizes of colored boxes are not true depictions of array sizes)

General Specifications

Operating Frequency Band

1695 – 2360 MHz | 698 – 896 MHz

Antenna Type

Sector

NHH-65B-R2B

Band	Multiband
Performance Note	Outdoor usage Wind loading figures are validated by wind tunnel measurements described in white paper WP-112534-EN
Total Input Power, maximum	600 W @ 50 °C

Mechanical Specifications

RF Connector Quantity, total	6
RF Connector Quantity, low band	2
RF Connector Quantity, high band	4
RF Connector Interface	7-16 DIN Female
Color	Light gray
Grounding Type	RF connector body grounded to reflector and mounting bracket
Radiator Material	Low loss circuit board
Radome Material	Fiberglass, UV resistant
Reflector Material	Aluminum
RF Connector Location	Bottom
Wind Loading, frontal	278.0 N @ 150 km/h 63.6 lbf @ 150 km/h
Wind Loading, lateral	230.0 N @ 150 km/h 51.7 lbf @ 150 km/h
Wind Loading, maximum	120.7 lbf @ 150 km/h 537.0 N @ 150 km/h
Effective Projected Area (EPA), frontal	0.26 m ² 2.80 ft ²
Effective Projected Area (EPA), lateral	0.22 m ² 2.37 ft ²
Wind Speed, maximum	241 km/h 150 mph

Dimensions

Length	1828.0 mm 72.0 in
Width	301.0 mm 11.9 in
Depth	180.0 mm 7.1 in
Net Weight, without mounting kit	19.8 kg 43.7 lb

Remote Electrical Tilt (RET) Information

Input Voltage	10–30 Vdc
Internal Bias Tee	Port 1 Port 3
Internal RET	High band (1) Low band (1)
Power Consumption, idle state, maximum	2 W
Power Consumption, normal conditions, maximum	13 W
Protocol	3GPP/AISG 2.0 (Single RET)
RET Interface	8-pin DIN Female 8-pin DIN Male
RET Interface, quantity	2 female 2 male

NHH-65B-R2B

Packed Dimensions

Length	1952.0 mm 76.9 in
Width	409.0 mm 16.1 in
Depth	299.0 mm 11.8 in
Shipping Weight	32.3 kg 71.2 lb

Regulatory Compliance/Certifications

Agency

RoHS 2011/65/EU

ISO 9001:2015

China RoHS SJ/T 11364-2014

Classification

Compliant by Exemption

Designed, manufactured and/or distributed under this quality management system

Above Maximum Concentration Value (MCV)



Included Products

BSAMNT-3 — Wide Profile Antenna Downtilt Mounting Kit for 2.4 - 4.5 in (60 - 115 mm) OD round members. Kit contains one scissor top bracket set and one bottom bracket set.

* Footnotes

Performance Note

Severe environmental conditions may degrade optimum performance

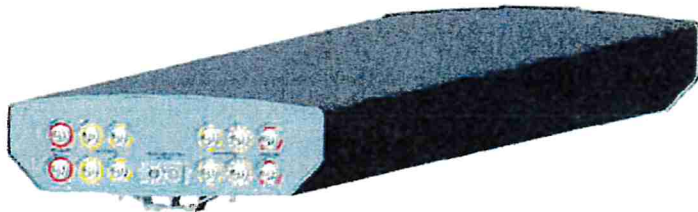
5

EPBQ-654L8H8-L2

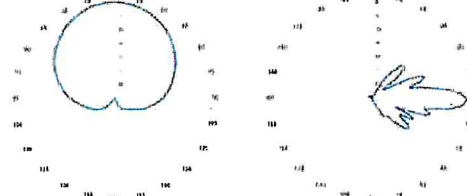
12-Port Multi-Band Antenna / 8' / 65°
 698 ~ 894MHz XX-pol., H67 V9.3 , ET:2~12°
 1695 ~ 2400MHz, XXXX-pol., H61 / V8.1 , ET: 2~12

Electrical Specification

Frequency(MHz)	698~806	806~894	1695~1850	1850~1910	1910~2180	2300~2400
Impedance(Ω)	50	50	50	50	50	50
Polarization	$\pm 45^\circ$	$\pm 45^\circ$	$\pm 45^\circ$	$\pm 45^\circ$	$\pm 45^\circ$	$\pm 45^\circ$
Gain(dBi)	15.9	16.2	16.9	17.3	17.7	17.8
Beam width	Horizontal	67°	66°	61°	60°	60°
	Vertical	9.3°	8.7°	8.1°	7.8°	7.4°
VSWR	$\leq 1.5:1$	$\leq 1.5:1$	$\leq 1.5:1$	$\leq 1.5:1$	$\leq 1.5:1$	$\leq 1.5:1$
Front-to-Back Ratio(dB)	>25	>25	>25	>25	>25	>25
Electrical Down tilt	2° ~ 12°	2° ~ 12°	2° ~ 12°	2° ~ 12°	2° ~ 12°	2° ~ 12°
Isolation Ports(dB)	≥ 25	≥ 25	≥ 25	≥ 25	≥ 25	≥ 25
Isolation Frequency(dB)	≥ 30	≥ 30	≥ 30	≥ 30	≥ 30	≥ 30
Cross Pole Discrimination	7 dB @ $\pm 60^\circ$	7 dB @ $\pm 60^\circ$	7 dB @ $\pm 60^\circ$	7 dB @ $\pm 60^\circ$	7 dB @ $\pm 60^\circ$	7 dB @ $\pm 60^\circ$
	15.0 dB @ 0°	15.0 dB @ 0°	15.0 dB @ 0°	15.0 dB @ 0°	15.0 dB @ 0°	15.0 dB @ 0°
Side Lobe Suppression (Up to 10° from Boresight)	> 16dB	> 16dB	> 16dB	> 16dB	> 16dB	> 16dB
PIM (2x20w, dBc)	≤ -150	≤ -150	≤ -150	≤ -150	≤ -150	≤ -150
Input Power(W)	400	400	300	300	300	300



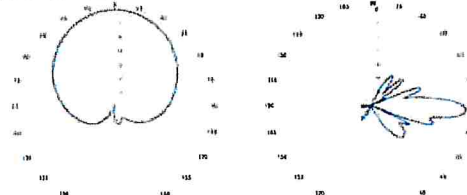
<698~806MHz>



Horizontal Pattern

Vertical Pattern (2°)

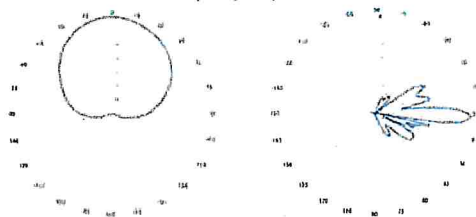
<806~894MHz>



Horizontal Pattern

Vertical Pattern (2°)

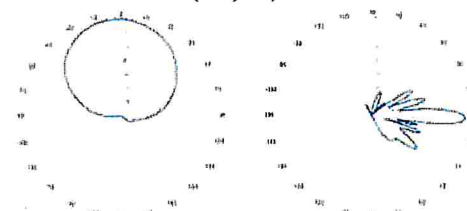
<1695~2400MHz (Y1,Y2)>



Horizontal Pattern

Vertical Pattern (2°)

<1695~2400MHz (Y3,Y4)>

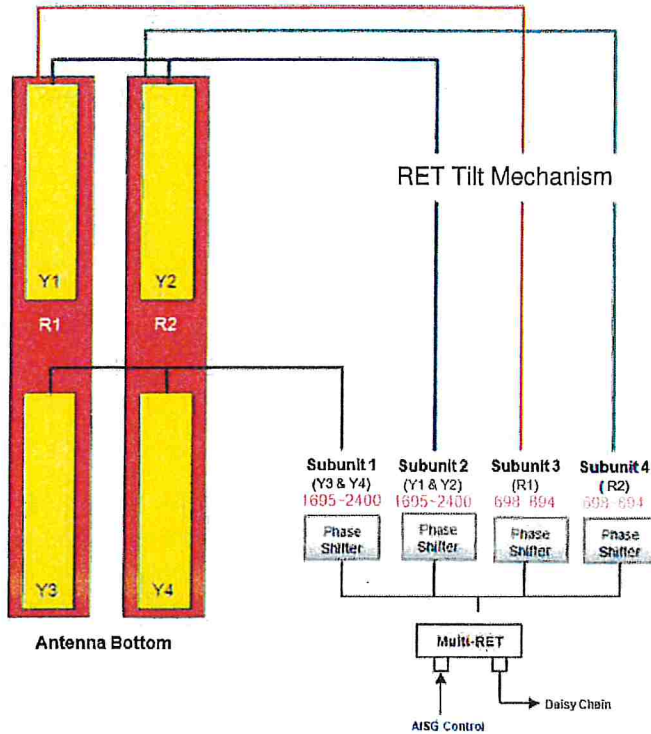


Horizontal Pattern

Vertical Pattern (2°)

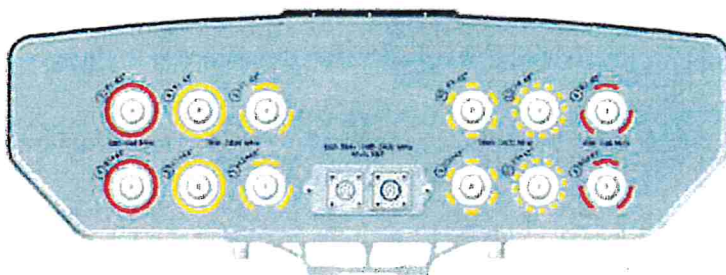
EPBQ-654L8H8-L2

12-Port Multi-Band Antenna / 8' / 65"
 698 ~ 894MHz, XX-pol., H67 / V9.3, ET:2-12
 1695 ~ 2400MHz, XXXX-pol., H61 / V8.1', ET: 2-12



Mechanical Specification

Dimension (WxDxH)	21.0x6.3x96.0 inches (533x160x2438 mm)
Weight (Without clamp)	86.0lbs (39.0kg)
Connector	12 x 4.3-10 (Female), Long Neck 4 x 698-894 8 x 1695-2400MHz
Max Wind Speed	150 mph
WindLoad (@100 mph)	1994N, 598N, 1994N (Front, Side, Rear)



Correlation Table

Frequency range	Array	Connector
698-894 MHz	R1	4.3-10 Female
698-894 MHz	R2	4.3-10 Female
1695-2400 MHz	Y1	4.3-10 Female
1695-2400 MHz	Y2	4.3-10 Female
1695-2400 MHz	Y3	4.3-10 Female
1695-2400 MHz	Y4	4.3-10 Female

***Note**

- Gain can vary and the values stated are typical
- Environmental Compliance: IP 65 for Radome & IP 67 for Connectors
- RET Motor Configuration: Field Replaceable RET Electronic Control Module RET Motor is internal to antenna & not field replaceable
- Compliant with AISG: AISG2.0
- Accessory: Standard Mounting Kit is included (Mechanical Down Tilt, KCLDM1B30000 is sold separately)



HexPort Multi-Band Antenna

HPA-65R-BUU-H8

- Eight foot (2.4 m), six port antenna with a 65° azimuth beamwidth covering 698-894 MHz and 1710-2360 MHz
- Four high band and two low band ports including the WCS band in a single antenna
- Sharp elevation beamwidth aides in network planning
- Optimal elevation sidelobe performance
- Enhanced array spacing ensures optimal MIMO performance
- Exceeds minimum PIM performance requirements
- Multi-network solution in one radome with six ports
- Reduces tower load and increases space for tower mounted remote radio heads
- Multi-band design improves site radio resource management
- Field replaceable, integrated AISG 2.0 compliant Remote Electrical Tilt (RET) system with independent tilt control for each paired port

Overview

The CCI HexPort multi-band array is a six port antenna with full Wireless Communication Service (WCS) band coverage. With four high band ports covering 1710-2360 MHz and two low band ports covering 698-894 MHz, this eight foot (2.4 m) CCI HexPort provides the capability to deploy 4x4 Multiple-input Multiple-output (MIMO) in the high band. The HexPort allows separate tilt control for each pair of ports enabling maximum flexibility in network deployment.

CCI has engineered its antennas using new and innovative design techniques to provide optimal sidelobe performance, sharp elevation beams, and high front to back ratio.

Multiple technologies can now be connected to a single antenna, reducing tower load, lease expense, deployment time and installation cost.

CCI antennas are designed and produced to ISO 9001:2008 certification standards for reliability and quality in our state-of-the-art manufacturing facilities.

Applications

- 4x4 MIMO for the high band and 2x2 MIMO for the low band
- Increase capacity without adding antennas
- Deploy WCS band without increasing antenna count
- Cosite current, and next-generation basestation technologies on the same antenna



HexPort Multi-Band Antenna

HPA-65R-BUU-H8

SPECIFICATIONS

Electrical

Ports	2 x Low Band Ports for 698-894 MHz			4 x High Band Ports for 1710-2360 MHz		
Frequency Range	698-806 MHz	824-894 MHz	1850-1990 MHz	1710-1780/2110-2180 MHz	2305-2360 MHz	
Gain	15.3 dBi	16.2 dBi	17.1 dBi	16.3 dBi	17.4 dBi	17.7 dBi
Azimuth Beamwidth (-3dB)	65°	61°	62°	68°	64°	60°
Elevation Beamwidth (-3dB)	10.1°	8.4°	5.6°	6.2°	5.0°	4.5°
Electrical Downtilt	2° to 10°	2° to 10°	0° to 8°	0° to 8°	0° to 8°	0° to 8°
Elevation Sidelobes (1st Upper)	< -17 dB	< -17 dB	< -19 dB	< -18 dB	< -18 dB	< -17 dB
Front-to-Back Ratio @180°	> 29 dB	> 28 dB	> 35 dB	> 35 dB	> 35 dB	> 35 dB
Front-to-Back Ratio over ± 20°	> 28 dB	> 27 dB	> 28 dB	> 27 dB	> 28 dB	> 28 dB
Cross-Polar Discrimination (at Peak)	> 24 dB	> 20 dB	> 25 dB	> 25 dB	> 25 dB	> 25 dB
Cross-Polar Discrimination (at ± 60°)	> 16 dB	> 14 dB	> 18 dB	> 18 dB	> 18 dB	> 18 dB
Cross-Polar Port-to-Port Isolation	> 25 dB	> 25 dB	> 25 dB	> 25 dB	> 25 dB	> 25 dB
Voltage Standing Wave Ratio (VSWR)	< 1.5:1	< 1.5:1	< 1.5:1	< 1.5:1	< 1.5:1	< 1.5:1
Passive Intermodulation (2x20W)	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc
Input Power Continuous Wave (CW)	500 watts	500 watts	300 watts	300 watts	300 watts	300 watts
Polarization	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°
Input Impedance	50 ohms	50 ohms	50 ohms	50 ohms	50 ohms	50 ohms
Lightning Protection	DC Ground	DC Ground	DC Ground	DC Ground	DC Ground	DC Ground

Mechanical

Dimensions (LxWxD)	92.8x14.4x7.3 in (2358x366x185 mm)
Survival Wind Speed	> 150 mph (> 241 kph)
Front Wind Load	327 lbs (1455 N) @ 100 mph (161 kph)
Side Wind Load	191 lbs (849 N) @ 100 mph (161 kph)
Equivalent Flat Plate Area	12.8 ft ² (1.2 m ²)
Weight *	53.0 lbs (24.1 kg)
RET System Weight	5.0 lbs (2.3 kg)
Connector	6 x 7-16 DIN female long neck
Mounting Pole	2 to 5 in (5 to 12 cm)

* Weight excludes mounting and RET



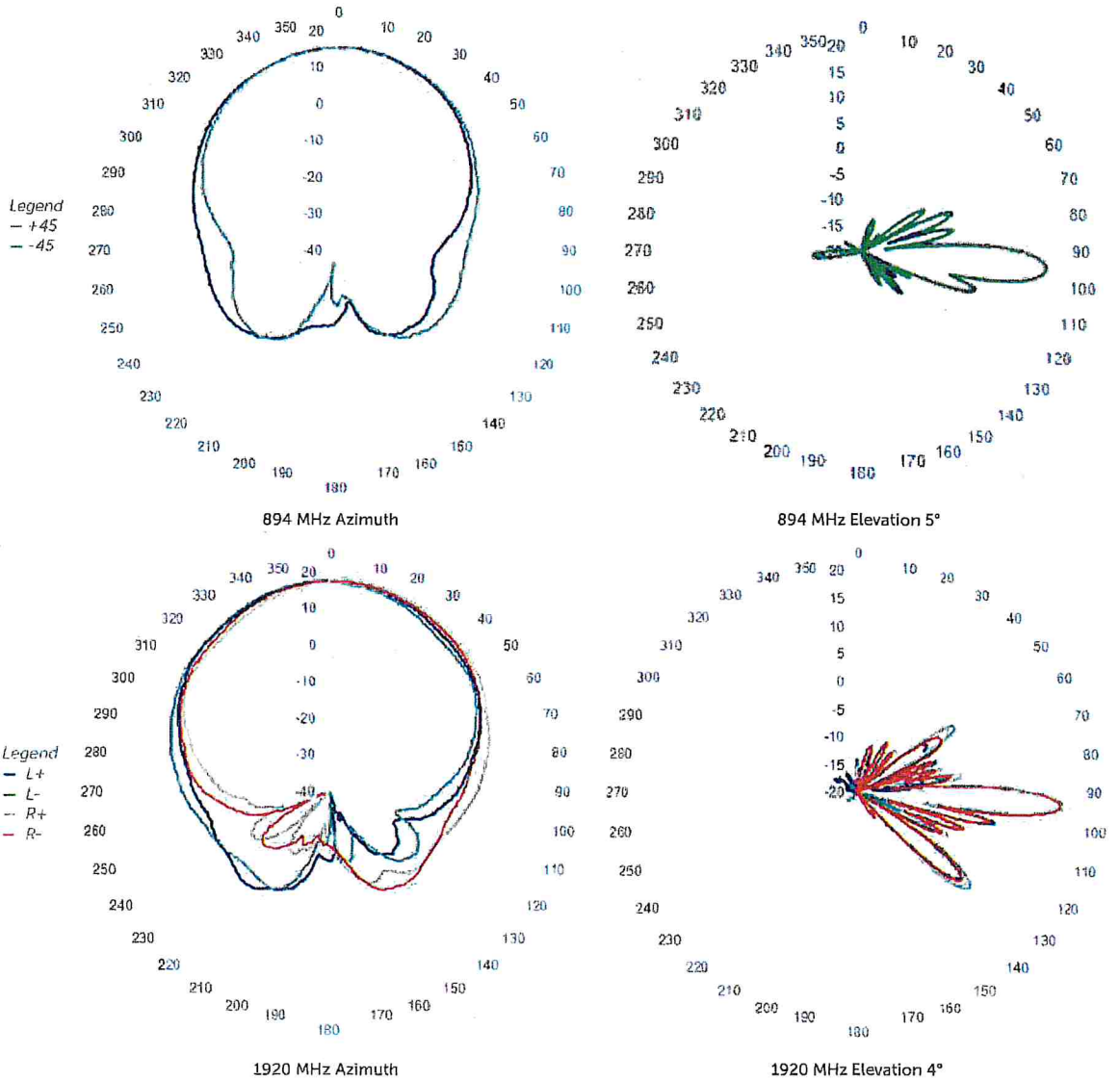
HexPort Multi-Band Antenna

HPA-65R-BUU-H8

SPECIFICATIONS

Typical Antenna Patterns

For detailed information on additional antenna patterns, contact customer support at support@cciproducts.com





ORDERING

HexPort Multi-Band Antenna

HPA-65R-BUU-H8

Parts & Accessories

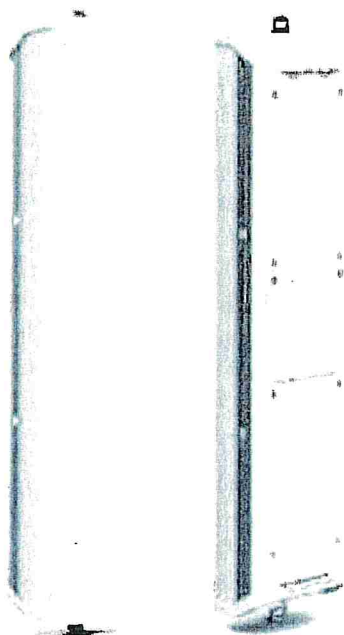
- HPA-65R-BUU-H8 Eight foot (2.4 m) HexPort antenna with 65° azimuth beamwidth and 3 factory installed BSA-RET200 RET actuators
- HPA-65R-BUU-H8-K Antenna kit with 3 factory installed RET actuators and MBK-01 mounting bracket
 - MBK-01 Mounting bracket kit (top and bottom) with 0° to 10° mechanical tilt adjustment
 - TM-01 Optional triple mount mast bracket for mounting up to three 65° antennas on a pole (or mast).
- BSA-RET200 Remote electrical tilt actuator
- HPA-CBK-AG-RRU HexPort antenna to RRU AISG cable kit
- HPA-CBK-RA-AG-RRU HexPort antenna to RRU AISG right angle cable kit

6



AIR-32 B4A/B2P & B2A/B66AA

ERICSSON ANTENNA INTEGRATED RADIO AIR-32



Radio		
	Single Band (B4a/B2p)	Dual Band (B2a/B66Aa)
Band 2 (1850-1910 / 1930-1990 MHz)	Passive frequency band	Active frequency band
Band 4 (1710-1755 / 2110-2155 MHz)	Active frequency band	Subset of Band 66A (AWS 1+3)
Band 66A (1710-1780 / 2110-2180 MHz)	N/A	Active frequency band
PA Output Power	4 x 30W	2 x (4 x 30) W
Downlink EIRP in bore-sight direction for each active band	4 x 62.5 dBmi	4 x 62.5 dBmi
Instantaneous bandwidth	45 MHz (W, L)	B2: 40 MHz (W, L) B2: 20 MHz (G) B66A: 70 MHz (W, L)
Capacity (single standard per unit)	6 GSM 6 WCDMA 2 x 20 MHz LTE	6 GSM (B2 only) 6 WCDMA per Active frequency band 2 x 20 MHz LTE per band
Multi-RAT capability	WCDMA and LTE on both PAs	WCDMA and GSM on both PAs (B2 only) WCDMA and LTE on both PAs (B2 and B4) GSM and LTE (B2 only)

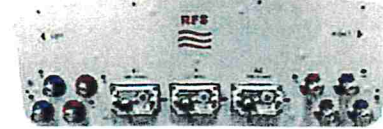
Interfaces		
Optical CPRI	2 x 10 Gbps	2 x 10 Gbps per Active frequency band
DC Power	-48 VDC 3-wire or 2-wire	-48 VDC 3-wire or 2-wire (separate input for both radios)
AC power (Optional)	PSU-AC 08	PSU-AC 08
Passive antenna	4 RF connectors (7/16 female)	N/A
Environmental		
Operating Temperature Range	-40 to +55 °C	-40 to +55 °C
Solar Radiation	≤ 1,120 W/m ²	≤ 1,120 W/m ²
Relative Humidity	5 to 100%	5 to 100%
Absolute Humidity	0.26 to 40 g/m ³	0.26 to 40 g/m ³
Maximum temperature change	1.0°C/min	1.0°C/min
Antenna		
Electrical Tilt	2° – 12° (B4)	2° – 12° (B66A)
	2° – 12° (B2)	2° – 12° (B2)
Bore-sight antenna gain	18 dBi (B4)	18 dBi (B66A)
	17.5 dBi (B2)	17.5 dBi (B2)
Nominal beam-width, azimuth	65° (B4)	65° (B66A)
	63° (B2)	63° (B2)
Nominal beam-width, elevation	6° (B4)	6° (B66A)
	6° (B2)	6° (B2)
Mechanical		
Weight	48 Kg (105.8 lbs)	60 Kg (132.2 lbs)
Dimensions (H x W x D)	1439 x 327 x 220 mm	1439 x 327 x 220 mm
	(56.6" x 12.9" x 8.7")	(56.6" x 12.9" x 8.7")
Wind load at 42 m/s (150 km/h)		
Front / Lateral / Rear	640N / 300N / 660N	640N / 300N / 660N



Dual Slant Polarized Quad Band (8 Port) Antenna, 617-746/617-746/1695-2200/1695-2200MHz, 65deg, 15/15/18/18dBi, 2.4m (8ft), VET, RET, 0-12°/0-12°/2-12°/2-12°

FEATURES / BENEFITS

This antenna provides a 8 Port multi-band flexible platform for advanced use for flexible use in deployment scenarios for encompassing 600MHz, 700MHz, AWS & PCS applications.



- ➔ 24 Inch Width For Easier Zoning
- ➔ Field Replaceable (Integrated) AISG RET platform for reduced environmental exposure and long lasting quality
- ➔ Superior elevation pattern performance across the entire electrical down tilt range
- ➔ Includes three AISG RET motors - Includes 0.5m AISG jumper for optional daisy chain of two high band RET motors for one single AISG point of high band tilt control.
- ➔ Low band arrays driven by a single RET motor

Technical Features

LOW BAND LEFT ARRAY (617-746 MHZ) [R1]

Frequency Band	MHz	617-698	698-746
Gain Over All Tilts	dBi	15.1 +/- .3	15.5 +/- .3
Horizontal Beamwidth @3dB	Deg	65 +/- 4	62 +/- 2
Vertical Beamwidth @3dB	Deg	11.4 +/- .7	10.4 +/- .5
Electrical Downtilt Range	Deg	0-12	0-12
Upper Side Lobe Suppression 0 to +20	dB	19	20
Front-to-Back, at +/-30°, Copolar	dB	25	24
Cross Polar Discrimination (XPD) @ Boresight	dB	19	19
Cross Polar Discrimination (XPD) @ +/-60	dB	5	3
3rd Order PIM 2 x 43dBm	dBc		-153
VSWR	-	1.5:1	1.5:1
Cross Polar Isolation	dB	25	25
Maximum Effective Power per Port	Watt	250	250

LOW BAND RIGHT ARRAY (617-746 MHZ) [R2]

Frequency Band	MHz	617-698	698-746
Gain Over All Tilts	dBi	14.8 +/- .2	15.1 +/- .2
Horizontal Beamwidth @3dB	Deg	65 +/- 4	62 +/- 2
Vertical Beamwidth @3dB	Deg	11.4 +/- .8	10.3 +/- .5
Electrical Downtilt Range	Deg	0-12	0-12
Upper Side Lobe Suppression 0 to +20	dB	19	20
Front-to-Back, at +/-30°, Copolar	dB	25	23
Cross Polar Discrimination (XPD) @ Boresight	dB	19	19
Cross Polar Discrimination (XPD) @ +/-60	dB	5	3
3rd Order PIM 2 x 43dBm	dBc		-153
VSWR	-	1.5:1	1.5:1
Cross Polar Isolation	dB	25	25
Maximum Effective Power per Port	Watt	250	250



Dual Slant Polarized Quad Band (8 Port) Antenna, 617-746/617-746/1695-2200/1695-2200MHz, 65deg, 15/15/18/18dBi, 2.4m (8ft), VET, RET, 0-12°/0-12°/2-12°/2-12°

HIGH BAND LEFT ARRAY (1695-2200 MHZ) [B1]

Frequency Band	MHz	1695-1880	1850-1990	1920-2200
Gain Over All Tilts	dBi	17.3 +/- .7	17.8 +/- .4	18.5 +/- .1
Horizontal Beamwidth @3dB	Deg	66 +/- 7	59 +/- 4	59 +/- 6
Vertical Beamwidth @3dB	Deg	5.3 +/- .4	4.7 +/- .4	4.3 +/- .3
Electrical Downtilt Range	Deg	2-12	2-12	2-12
Upper Side Lobe Suppression 0 to +20	dB	15	15	15
Front-to-Back, at +/-30°, Copolar	dB	25	25	25
Cross Polar Discrimination (XPD) @ Boresight	dB	19	17	16
Cross Polar Discrimination (XPD) @ +/-60	dB	4	6	4
3rd Order PIM 2 x 43dBm	dBc	-153	-153	-153
VSWR	-	1.5:1	1.5:1	1.5:1
Cross Polar Isolation	dB	25	25	25
Maximum Effective Power per Port	Watt	250	250	250

HIGH BAND RIGHT ARRAY (1695-2200 MHZ) [B2]

Frequency Band	MHz	1695-1880	1850-1990	1920-2200
Gain Over All Tilts	dBi	17.1 +/- .7	17.8 +/- .4	18.5 +/- .1
Horizontal Beamwidth @3dB	Deg	66 +/- 7	59 +/- 4	59 +/- 5
Vertical Beamwidth @3dB	Deg	5.2 +/- .4	4.7 +/- .4	4.3 +/- .3
Electrical Downtilt Range	Deg	2-12	2-12	2-12
Upper Side Lobe Suppression 0 to +20	dB	15	15	15
Front-to-Back, at +/-30°, Copolar	dB	25	24	25
Cross Polar Discrimination (XPD) @ Boresight	dB	20	17	16
Cross Polar Discrimination (XPD) @ +/-60	dB	4	6	5
3rd Order PIM 2 x 43dBm	dBc	-153	-153	-153
VSWR	-	1.5:1	1.5:1	1.5:1
Cross Polar Isolation	dB	25	25	25
Maximum Effective Power per Port	Watt	250	250	250

PRODUCT DATASHEET

APXVAARR24_43-U-NA20

RADIO FREQUENCY SYSTEMS

The Clear Choice



Dual Slant Polarized Quad Band (8 Port) Antenna, 617-746/617-746/1695-2200/1695-2200MHz, 65deg, 15/15/18/18dBi, 2.4m (8ft), VET, RET, 0-12°/0-12°/2-12°/2-12°

ELECTRICAL SPECIFICATIONS

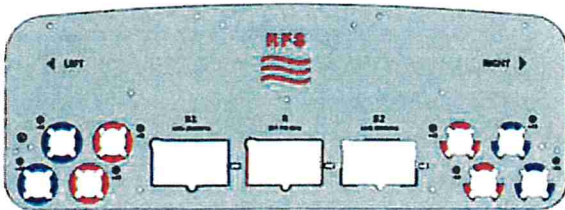
Impedance	Ohm	50.0
Polarization	Deg	±45°

MECHANICAL SPECIFICATIONS

Dimensions - H x W x D	mm (in)	2436 x 609 x 222 (95.9 x 24 x 8.7)
Weight (Antenna Only)	kg (lb)	58 (128)
Weight (Mounting Hardware only)	kg (lb)	11.5 (25.3)
Shipping Weight	kg (lb)	80 (176)
Connector type		8 x 4.3-10 female at bottom + 6 AISG connectors (3 male, 3 female)
Adjustment mechanism		Integrated RET solution AISG compliant (Field Replaceable) + Manual Override + External Tilt Indicator
Mounting Hardware		Galvanized steel
Material		
Radome Material / Color		Fiber Glass / Light Grey RAL7035

TESTING AND ENVIRONMENTAL

Temperature Range	°C (°F)	-40 to 60 (-40 to 140)
Lightning protection		IEC 61000-4-5
Survival/Rated Wind Velocity	km/h	241 (150)
Environmental		ETSI 300-019-2-4 Class 4,1E



617	617
X	X
X	X
1695	1695
X	X
X	X
X	X
2200	2200
2-12°	2-12°
X	X
X	X
746	746
0-12°	0-12°

ORDERING INFORMATION

Order No.	Configuration	Mounting Hardware	Mounting pipe Diameter	Shipping Weight
APXVAARR24_43-U-NA20	Field Replace RET included (3)	APM40-5E Beam tilt kit (included)	60-120mm	80 Kg

APXVAARR24_43-U-NA20

REV: D

REV DATE: July 3, 2018

www.rfsworld.com



Dual Slant Polarized Quad Band (8 Port) Antenna, 617-746/617-746/1695-2200/1695-2200MHz, 65deg, 15/15/18/18dBi, 2.4m (8ft), VET, RET, 0-12°/0-12°/2-12°/2-12°

External Document Links

APM40_Series_Installation_Instructions
Manual_Overdrive_Instructions
Global RFS Website

Notes

All electrical parameters are compliant with BASTA NGMN 9.6 requirements.

Available Configurations

APXVAARR24_43-U-NA20 -- External ACU is included -- shipping weight 80kg.

For additional mounting information please click "External Document Links".

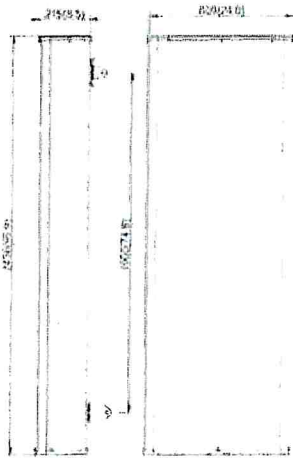
This data is provisional and subject to changes

External Link Reference

Global RFS Website

<http://www.rfsworld.com>

Dimensions: mm (in)



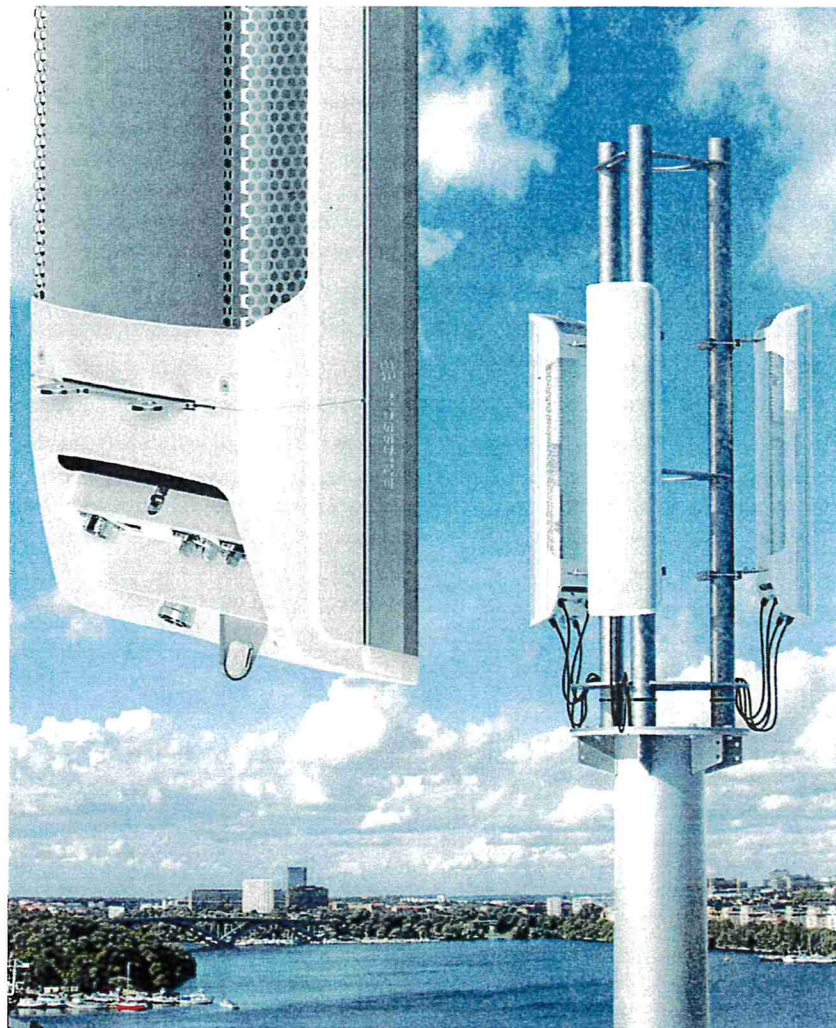
For more information
of the antenna, please visit
the website: www.rfsworld.com

AIR 21, 1.3 M B4A B2P

The Antenna-Integrated Radio (AIR) is a single tower-mounted unit that can replace the antenna/s and radio for one sector. There is no need for additional electronics such as ASC and a RET Actuator and control. A passive antenna function for an extra band is optional. (The option has to be specified when ordering, retrofit is not possible).

The height and width are the same as for a passive antenna with similar characteristics. The depth is increased to house the radios' electronics. Digital Units (DUs) from Ericsson's RBS 6000 family provide the baseband function and support GSM, WCDMA and LTE.

One or two DUs, depending on capacity and the standards to be supported, are needed for a three-sector site with AIR units.



The AIR is especially suited for state of the art mobile broadband base stations utilizing advanced MIMO techniques. Less tower-mounted equipment is required and the unit's attractive appearance enables it to blend in well with other existing equipment. The same applies to sites with multiple access technologies on different frequency bands.

With AIR, it is only necessary to swap antennas in order to add new 3G/4G technology on-site or at a new site. The AIR also saves power compared to traditional RBSs.

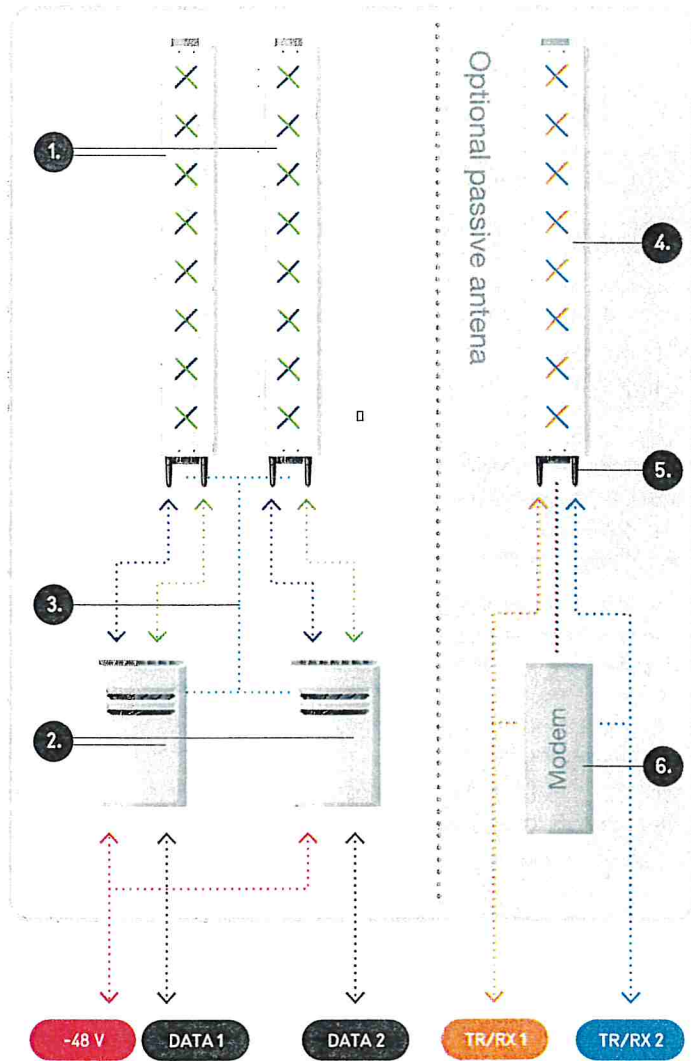
Functionality for the AIR unit

The figure to the right shows an example of the hardware that a single AIR unit can replace. The function of the AIR unit is the same, but the implementation is different.

The AIR unit's active band has two radios (2) connected to a pair of cross-polarized antenna arrays (1). Remote electrical tilt (3) is included. Air supports 2 TX for the down-link and 4 RX for the up-link.

The passive antenna function on the frequency band not used by the AIR unit's active part is optional. The passive function includes an antenna array (4) and a RET motor (5) with a modem to control it (6).

The tilts for the active part and the passive part are controlled independently, but each band has the same tilt for both arrays and for both polarizations.



Example of hardware that a single AIR unit can replace

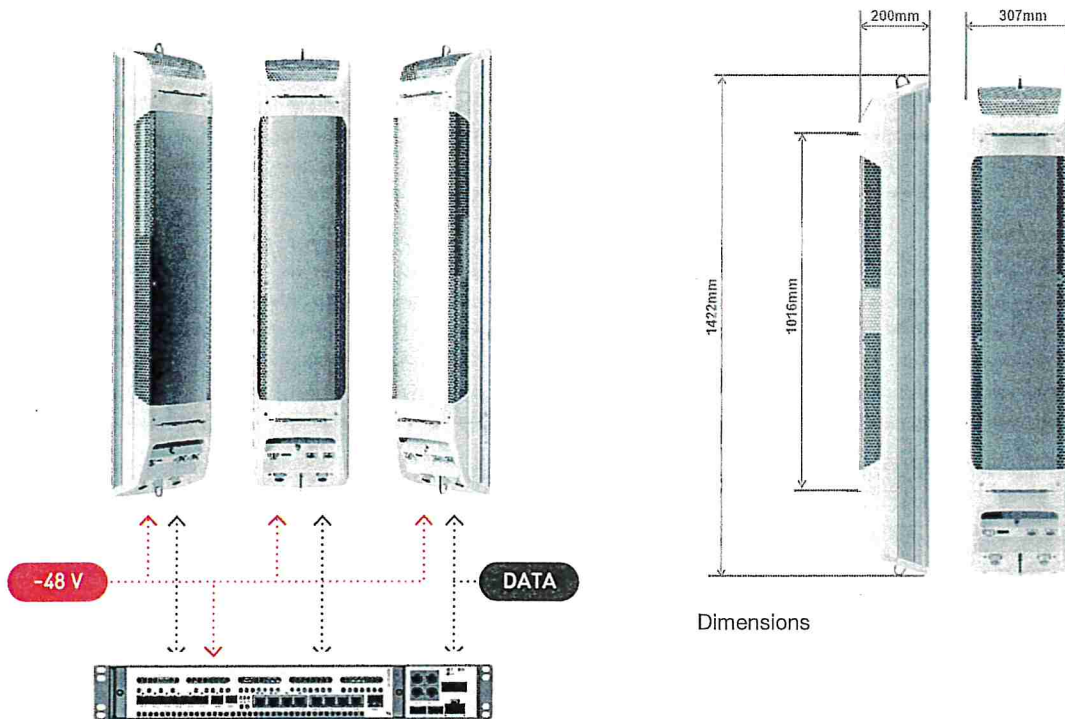
Configuration Example

Figure below shows a typical configuration with WCDMA with 2 x 2 MIMO for Band 4.

One AIR unit is deployed in each sector.

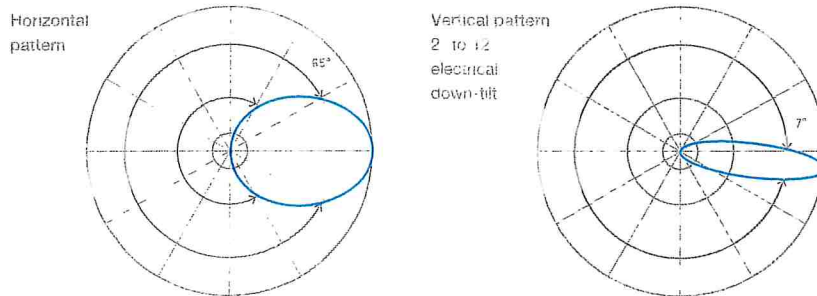
A common base band unit with a DUW inside provides base band processing and back-haul.

The AIR units can be specified with passive antennas for Band 2.



Three sector configuration example: RBS 6601 with three AIR units

Antenna Characteristics.



TECHNICAL SPECIFICATIONS AIR 21, 1.3M, B4A B2P

RADIO

Active frequency band:	Band 4 (1710-1755 / 2110-2155 MHz)
Passive frequency band (optional):	Band 2 (1850-1910 / 1930-1990 MHz)
Downlink EIRP in bore-sight direction for the active band:	2 x 62,5 dBm
Uplink sensitivity:	TBD*
Remote electrical tilt:	-2° to -12°, independently controlled per frequency band
MIMO:	2 x 2 for DL 4 RX branches to be used for diversity/ beam-steering /MIMO
Instantaneous bandwidth:	20 MHz
Capacity (single standard per sector):	Up to 4 carriers WCDMA with 2 x 2 DL MIMO Up to 20 MHz LTE with 2 x 2 DL MIMO
Multi-RAT capability:	Single standard or two simultaneous standards (Capacity above is reduced for multi-RAT)
Bore-sight antenna gain for passive antenna option:	17.5 dBi
Nominal beam-width, azimuth:	65°
Nominal beam-width, elevation:	7°
Additional antenna parameters:	See Antenna characteristics, page 3

MECHANICAL SPECIFICATION

Weight (excl. mounting brackets):	37, kg for active only 41 kg for active and passive
Size (H x W x D)	1422 mm x 307 mm x 200 mm
Wind load:	580 N / 300 N / 720 N (frontal/lateral/rear-side) @ 42 m/s wind speed

INTERFACES

AIR – DU:	DATA 1, Data 2: CPRI links (SFP modules with LC socket + flanges that match protective cover TYCO C20611458)
Power:	- 48V DC (TYCO/Ericsson RPT 447 04)
Passive antenna (option):	TX/RX 1, TX/RX 2: RF connectors (7-16 female)

SUPPORTING BASE-BAND

RBS 6601:	One or two units depending on configuration.
-----------	----------------------------------------------

* 1 dB better than best-in-class RRU connected to same size best-in-class antenna

** Other base-band configurations are available