Transportation Land Development Environmental Services



54 Tuttle Place Middletown, Connecticut 06457 860 632-1500 FAX 860 632-7879

Memorandum

To: Nicole Dentamaro

Environmental/GIS Analyst

Date: March 10, 2008

Project No.: 40999.16

From: Dean Gustafson

Professional Soil Scientist

Re: Proposed Optasite Facility 497A Wickham Road

Glastonbury, Connecticut

Vanasse Hangen Brustlin, Inc. (VHB) has completed a determination of NEPA compliance for listed category item 7, significant change in surface features (e.g., wetland fill, etc.) for the following Site.

Project Site:

State: Connecticut County: Hartford

Address: Wickham Road, Glastonbury

Latitude/Longitude Coordinates: N41°42'04.0" W72°33'50.5"

Size of Property: ±12.15 acres

Watershed: Hubbard Brook (basin # 4007)

The proposed Optasite communications facility and associated infrastructure (e.g., access drive, utilities, etc.) are located on the west side of a 12.15± acre property. A forested wetland system consisting of an unnamed, shallow perennial watercourse and associated bordering wetlands transects the property from south to north. Wetlands were identified and delineated by Kleinfelder, as detailed in the attached June 25, 2007 delineation report. The watercourse receives inputs from associated bordering hillside seeps as well as runoff from Route 2. Evidence of road runoff and stormwater inputs are apparent in the presence of alluvial (road) sand deposits on terraces above the eroded stream channel. The proposed access road would enter the property in the northeast corner, south of an existing driveway. The access road would generally follow the east and south property boundary lines, within a narrow forested strip adjacent to cleared areas, before entering the forested portion of the lot east of the riparian corridor. The access road would cross the watercourse (a 10± foot wide channel) and associated bordering wetlands for a distance of approximately 52 linear feet, before entering the facility compound located in uplands west of the riparian corridor.

The proposed wetland/watercourse crossing in support of Optasite's development includes placement of fill material to create a stable road base and placement of a 6-foot by 6-foot box culvert for the stream crossing. Improvements to the wetland crossing will result in permanent wetland fill of 2,852± square feet (SF) as reported by Clough Harbour & Associated LLP and shown on Sheet Number D01, Culvert Details (see attached).

Date: March 10, 2008 Project No.: 40999.16

Under NEPA compliance with respect to wetland/waterway impacts, in order to determine if a proposed project results in a "significant environmental effect" and as a result an Environmental Assessment (EA) would need to be prepared, a project is evaluated against the Corps' minimal impact threshold criteria to "Waters of the U.S." (e.g., wetlands, waterways, etc.). Generally, if a project is determined to satisfy the requirements of a Category 1 project (minimal impact and eligible without screening by reviewing agencies) under the Department of the Army Programmatic General Permit (PGP) State of Connecticut (effective May 311, 2006, expiration date May 31, 2011) it is not considered to result in a significant environmental effect and a Finding of No Significant Impact (FONSI) could be issued for the NEPA listed category item 7. In order to support this conclusion, a careful review of the PGP criteria for Category 1 is necessary.

For the proposed wetland/watercourse crossing improvements, the following criteria are required in order to be eligible under Category 1 of the PGP (refer to the PGP for further details).

Unconfined in-stream work, including construction, installation or removal of cofferdam structures or placement of fill, is limited to the period July 1 through September 30 except in instances where a specific written exception has been issued by the CT DEP.

Less than 5,000 SF of Inland Waters, Waterway and/or Wetland Fill and Secondary Impacts. Fill impacts include all temporary and permanent fill and excavation discharges resulting from a single and complete project, see #5 of General Requirements. Secondary impacts include but are not limited include to impacts to inland waters, waterways or wetlands drained, dredged, flooded, cleared or degraded resulting from a single and complete project. (See 40 CFR 230.11 (g) and (h))

Driveway/Roadway Crossings. The following are required for driveway/roadway crossings constructed on brooks, streams, rivers and their tributaries. These provisions do not apply to crossings of drainage ditches or waters with no definable channel.

Driveway or Roadway crossings using a culvert provided:

- \triangleright the tributary watershed to the culvert is ≤ 1.0 sq. mile (640 acres),
- > the culvert gradient (slope) is no steeper than the streambed gradient immediately upstream or downstream of the culvert,
- \succ for a crossing constructed using a pipe culvert, the inverts are set such that \geq 25% of the pipe or 12", whichever is less, is set below the streambed elevation,
- > the culvert is backfilled with natural substrate material matching upstream and downstream streambed substrate.
- > the structure does not otherwise impede the passage of fish and other aquatic organisms, and
- > the structure allows for continuous flow of the 50-year frequency storm flows.

The proposed wetland/watercourse crossing design carefully considered these requirements (a.k.a., natural stream crossing design standards) in order to be compliant with a Category 1 determination. First, the wetland fill required to improve the existing wetland/watercourse crossing total 2,850 SF, less than the 5,000 SF trigger. Also, the tributary watershed to the existing culvert is approximately 48.7 acres, well below the 640 acre limit; refer to attached Hydrologic & Hydraulic Assessment report prepared by Clough Harbour & Associates LLP, dated November 21, 2007. In addition, the 6-foot by 6-foot box culvert will have a gradient no steeper than the existing upstream or downstream gradients and will be set 12 inches below the streambed elevation and backfilled with natural streambed substrate. The culvert proposed will not impede fish or aquatic organism movement and allow for unimpeded flow of the 50-year design storm.

As a result of careful adherence to the Corps' natural stream crossing design standards, the proposed wetland/watercourse impacts associated with Optasite's development are considered eligible under Category 1 of the PGP and therefore a Finding of No Significant Impact for NEPA listed category item 7 is provided.

Date: March 10, 2008 Project No.: 40999.16

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Attachments

- ➤ Wetland & Watercourse Delineation Report, Kleinfelder, June 25, 2007
- Sheet No. D01 Culvert Details, Clough Harbour & Associates LLP, 06/15/07
- Hydrologic & Hydraulic Assessment, Clough Harbour & Associates LLP, November 21, 2007

KLEINFELDER

June 25, 2007

Mr. Paul Lusitani Clough Harbour & Associates, LLP. 2139 Silas Deane Highway Suite 212 Rocky Hill, CT 06067-2336

RE: Wetland & Watercourse Delineation Report 618 Neipsic Road a.k.a. 497a Wickham Rd

Glastonbury, Connecticut

Dear Mr. Lusitani:

Kleinfelder East, Inc. (Kleinfelder) completed an on-site investigation to determine the presence or absence of wetlands and/or watercourses on the above referenced property (618 Neipsic Road a.k.a. 497a Wickham Rd, Glastonbury, CT), as requested and authorized. This investigation involved a wetland/watercourse delineation that was completed by a qualified staff soil scientist and conducted in accordance with the principles and practices noted in the United States Department of Agriculture (USDA) Soil Survey Manual (1993). The soil classification system of the National Cooperative Soil Survey was used in this investigation to identify the soil map units present on the project site.

INVESTIGATION

The project site was investigated on June 5, 2007, with a temperature in the mid-70s under partly sunny conditions. Soil types are identified by observing soil morphology (soil texture, color, structure, etc.). To observe the morphology of the soils, numerous test pits and/or hand borings (generally to a depth of at least two feet) are completed. Wetland and watercourse boundaries were identified with flags and hung from vegetation. These flags are labeled "Wetland Delineation", numbered consecutively, and generally spaced a maximum of approximately 50 feet apart. It is important to note that flagged wetland and watercourse boundaries are subject to change until verified by local, state, or federal regulatory agencies.

REGULATORY INFORMATION

Wetlands and watercourses are regulated by both state and federal law each with different definitions and regulatory requirements. Accordingly, the State may regulate waters that fall outside of federal jurisdiction; however, where federal jurisdiction exists concurrent State jurisdiction is almost always present.

State Regulation

Wetland determinations are based on the presence of poorly drained, very poorly drained, alluvial, or floodplain soils and submerged land. Watercourses are defined as "rivers, streams, brooks, waterways, lakes, ponds, marshes, swamps, bogs and all other bodies of water, natural or artificial, vernal or intermittent, public or private, which are contained within, flow through or border upon the state or any portion thereof." Intermittent watercourse determinations are made based on the presence of a defined permanent channel and bank, and two of the following characteristics: (1) evidence of scour or deposits of recent alluvium or detritus, (2) the presence of standing or flowing water for a duration longer than a

particular storm incident, and (3) the presence of hydrophytic vegetation. (See Inland Wetlands and Watercourses Act §22a-38 CGS.)

Federal Regulation

The United States Army Corps of Engineers (ACOE) regulate "Waters of the Untied States" under Section 404 of the Clean Water Act, which includes adjacent/tributary wetlands and watercourses. The New England Region of the ACOE has issued guidance documents discussing how wetlands and/or watercourses can be as much as 500 or more feet from regulated Waters of the U.S. and still be regulated if the Corps finds scientific indicators (e.g. ecological/biological/hydrological) that provide connections to the jurisdictions wetland. This guidance distance has been developed by the Corps New England Region based on research suggesting home range and migratory distances of 54 palustrine/riparian (wetland and watercourse) reptiles, amphibians and mammals. Discontinuities between jurisdictional Waters of the U.S. and neighboring wetlands can cause isolation of those wetlands or watercourse, which in turn can eliminate federal jurisdiction. The Corps use a three (3) parameter approach to wetland delineation that includes soils, hydrology and vegetation. It is necessary to successfully observe all three in order for the area to be considered a federal wetland in addition to it being "adjacent" to Waters of the U.S. Disturbed and atypical conditions allow for some modification of this requirement and invoke professional judgment.

Generally, in accordance with the Connecticut Programmatic General Permit (PGP), the Corps requires a permit application for activities of one (1) acre or greater affecting federal jurisdictional wetland areas or if special wetlands occur (these are defined in the PGP document).

WETLAND AND WATERCOURSE SITE DESCRIPTION

Wetland classifications used to identify the type of wetland(s) occurring on the project site are based on guidance from the U.S. Fish and Wildlife Service (USFWS) (Cowardin et.al. 1979). These are further qualified with the Hydrogeomorphic Method of wetland classification (Brinson, 1993). Photographs of the wetland/watercourse and upland habitats are attached.

The on-site wetland that was delineated consisted of a lacustrine unconsolidated bottom and emergent wetland system (USFWS class: LUB1C and LEM2E) which is seasonally flooded. Surrounding this system was a palustrine forested - emergent wetland system (USFWS class: PFO1 and PEM1) that was associated with the stream. These wetlands were delineated using sequentially numbered flags 1-17 (open end), 50 (open end) – 118 (open end), and 150 (open end) – 175. This wetland area is situated along an unnamed stream which receives overland flow form both the surrounding uplands and runoff from State Route 2, which borders the wetland to south. Water flows in a generally southern direction and ends in a small pond at the northern end of the property associated with Hubbard Brook. The wetland system on-site consists of the immediate edges of the stream, as well as, other seasonally saturated areas surrounding the stream where water ponds during high flow events. In general, the majority of the stream has 1 to 2 inches of water, with the outside edges of turning the channel containing as much as 6 inches. The water which falls on the surrounding uplands during a rain event tends to flow directly into the stream, as well as, flatter areas with the uplands surrounding the stream. Vegetation in these areas is thick and consists mostly of facultative and wetter species.

TABLE 1: Predominate Vegetation within and adjacent to the wetlands (Common (Scientific) names)

TREES & SAPLINGS

Green ash (Fraxinus pennsylvanica)

Pin oak (Quercus palustris)

Red maple (Acer rubrum)

Red oak (Quercus rubra)

Sweet birch (Betula lenta)

White pine (Pinus strobus)

Atlantic White Cedar (Chamaecyparis thyoides)

Yellow birch (Betula alleghaniensis)

SHRUBS

Rosebay Rhododendron (Rhododendron maximum)

HERBS/VINES

Slender blue iris (Iris prismatica)

Cinnamon fern (Osmunda cinnamomea)

Sensitive fern (Onoclea sensibilis)

Skunk cabbage (Symplocarpus foetidus)

Virginia creeper (Parthenocissus quinquefolia)

*Denotes State non-native invasive species

SOIL MAP TYPES

A brief description of each soil map unit identified on the project site is presented below including information from the Untied States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) soil descriptions. Further information on these and other soils, please refer to the internet site at http://soils.usda.gov/technical/classification/osd/index.html). The soil survey map and soil identification pages for the project site are attached.

Upland Soils

Manchester (MgB) gravelly sandy loam, 3 to 45 percent slopes

The Manchester series consists of very deep, excessively drained soils formed in sandy and gravelly glacial outwash and stratified drift. They are nearly level to steep soils on outwash plains, terraces, kames, deltas and eskers. Slope ranges from 0 to 45 percent, approximately 3% on site. The soils formed in sandy and gravelly glaciofluvial materials and stratified drift derived mainly from a red sedimentary rocks and basalt. Diagnostic horizons in this pedon include an Ochric epipedon from 0 to 9 inches, a sandy-skeletal particle-size control section from 10 to 40 inches and no diagnostic subsoil.

Hartford sandy loam, 0 to 3 percent slopes

The Hartford series consists of very deep, somewhat excessively drained soils formed in sandy glacial outwash. They are nearly level to strongly sloping soils on plains and terraces. Slope ranges from 0 to 8 percent. Saturated hydraulic conductivity is high in the surface layer and subsoil and high or very high in the substratum. Diagnostic horizons in this pedon include an ochric epipedon from 0 to 8 inches (Ap horizon), and a cambic horizon in the zone from 8 to 26 inches (Bw1 and Bw2 horizons).

Wetland Soils

Saco (108) silt loam

Saco soils are nearly level soils on flood plains, along rivers and streams. They are in depressed areas. Slope ranges from 0 to 2 percent. The soils formed in recent silty alluvium derived mostly from granite, gneiss, schist, shale and sandstone. In places water is ponded on the surface from late fall through early

spring. Permeability is moderate in the silty layers and rapid or very rapid in the underlying sandy materials. These soils flood in the spring and after periods of heavy rainfall.

REFERENCES

- 1. Brinson, M.M. 1993. A Hydrogeomorphic Classification for Wetlands. Tech. Rpt.WRP-DE-4, U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.
- 2. Cowardin, L.M., V. Carter, F.C. Golet, E.T. LaRoe. 1979. Classification of Wetland and Deepwater Habitats of the Untied States. US Government Printing Office. Washington D.C. GPO 024-010-00524-6.103 pp.

CLOSING

Thank for the opportunity to work with you on this project. Please contact me at (860) 683-4200 if you have any questions or require additional assistance.

Very truly yours,

Kleinfelder East, Inc.

2007.07.02 20:24:43 -04'00'

Paul Wheeler

Project Wetland Scientist

Date: 2007.07.02 20:24:12 -04'00'

Jeffrey R. Shamas, CE, SS, PWS Natural Resources Program Manager

Attachments

Photographs

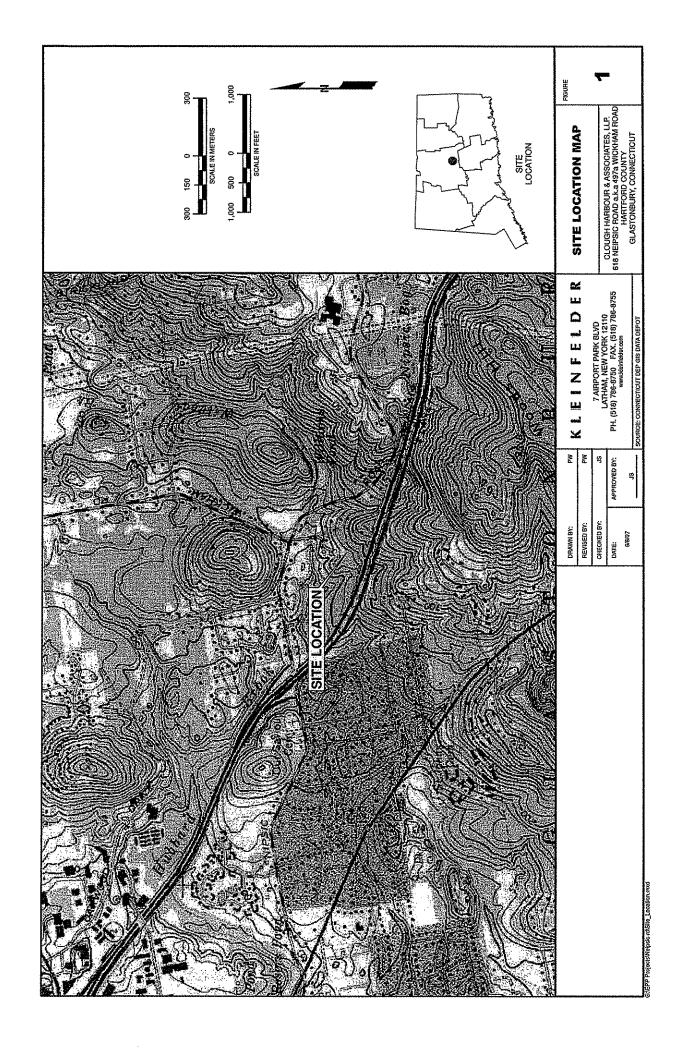


Cover types within Wetland Area

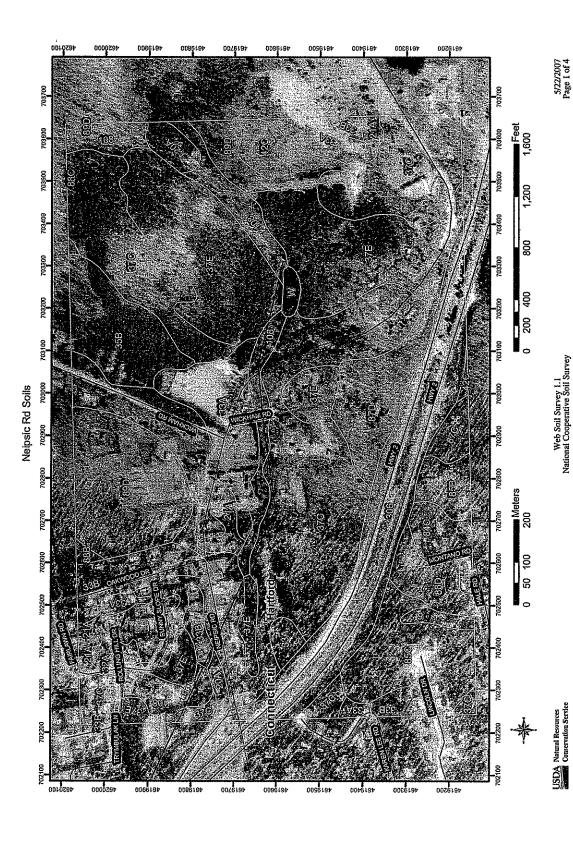


Stream and a portion of the associated wetland within the project Site

Site Location Map



Soil Survey Map and Associated Information



SOIL SURVEY OF STATE OF CONNECTICUT

Perennial Water Wet Spot

Web Soil Survey 1.1 National Cooperative Soil Survey

5/22/2007 Page 2 of 4

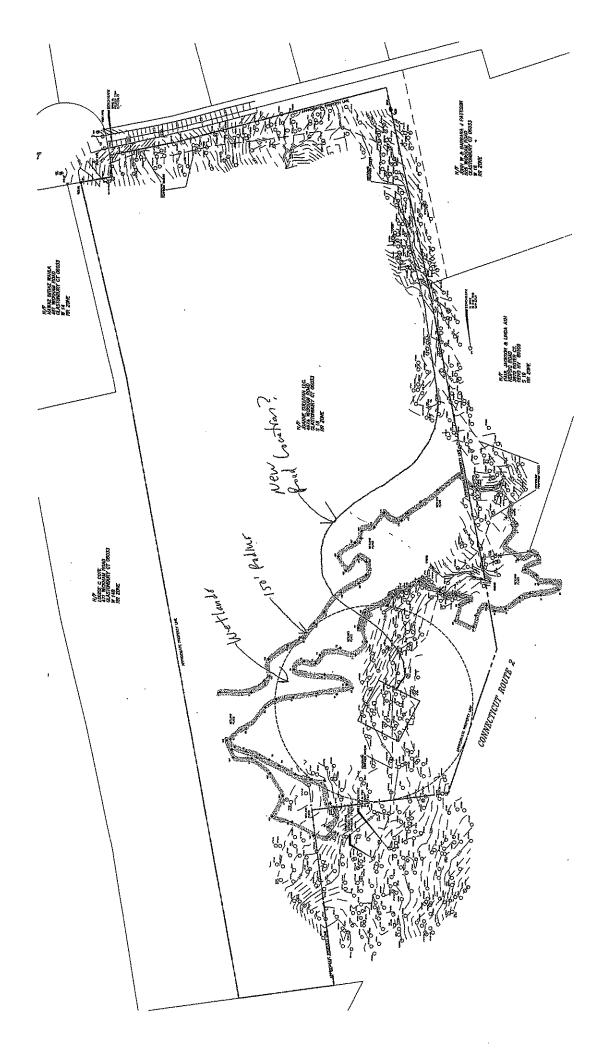
Map Unit Legend Summary

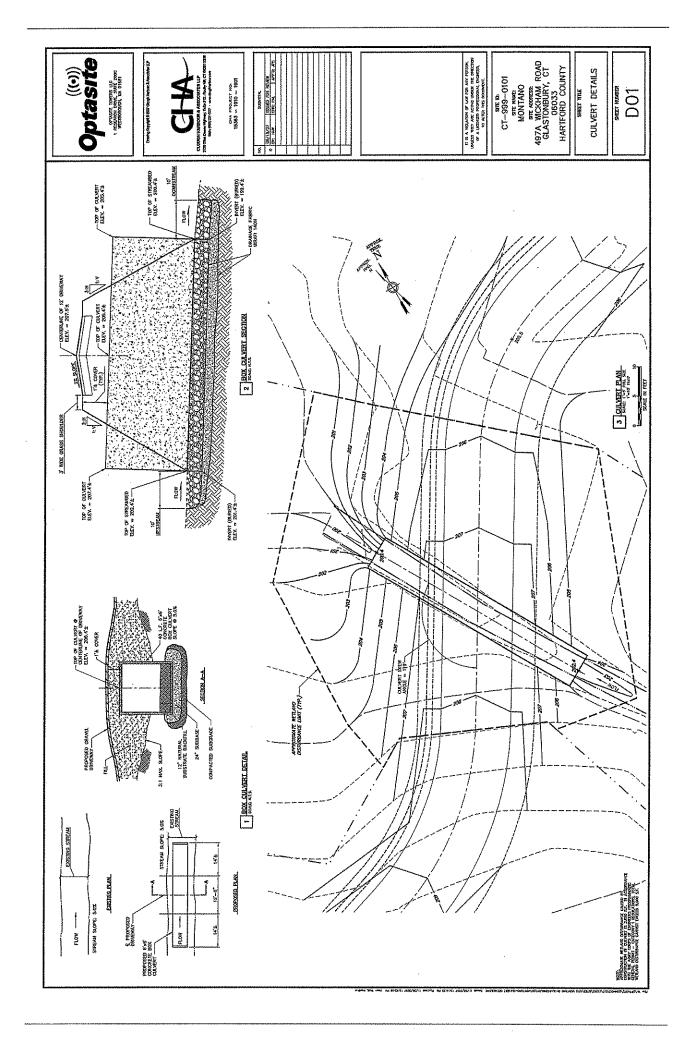
State of Connecticut

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI		
6	Wilbraham and Menlo soils, extremely stony	1.3	04		
20A	Ellington silt loam, 0 to 5 percent slopes	3.5	1.1		
2 1A	Ninigret and Tisbury soils, 0 to 5 percent slopes	3.7	1.1		
32A	Haven and Enfield soils, 0 to 3 percent slopes	1.8	0.5		
33A	Hartford sandy loam, 0 to 3 percent slopes	17.6	5.4		
33B	Hartford sandy loam, 3 to 8 percent slopes	11.9	3.7		
35B	Penwood loamy sand, 3 to 8 percent slopes	12.2	3.8		
37C	Manchester gravelly sandy loam, 3 to 15 percent slopes	105.4	32.4		
47E	Manchester gravelly sandy loam, 15 to 45 percent slopes	52.7	16/2		
42C :	Ludlow silt loam, 2 to 15 percent slopes, extremely stony	3.2	1.0		
84C	Paxton and Montauk fine sandy loams, 8 to 15 percent slopes	4.7	14		
85B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes, very stony	3.8	1.2		
85C	Paxton and Montauk fine sandy loams, 8 to 15 percent slopes, very stony	13:7	4.2		
86D	Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony	5.2	1.6		
87C	Wethersfield loam, 8 to 15 percent slopes	2.4	0.7		
87D	Wethersfield loam, 15 to 25 percent slopes	10.7	3.3		
88B	Wethersfield loam, 3 to 8 percent slopes, very stony	0.5	0.2		
88C	Wethersfield loam, 8 to 15 percent slopes, very stony	0.1	0.0		
89D	Wethersfield loam, 15 to 35 percent slopes, extremely stony	25.6	7.9		
108	Saco silt loam	16.4	5.0		

State of Connecticut

Map Unit Symb	ol Map Unit Name	Acres in AOI	Percent of AOI
306	Udorthents-Urban land	complex 28.3	8.7
1. No. of the State of the Stat			
W	Water	1.0	0.3







November 21, 2007

Mr. Keith Coppins Optasite Towers LLC 1 Research Drive, Suite 200C Westborough, MA 01581

RE: Hydrologic & Hydraulic Assessment @ Montano Cell Site - 497A Wickham Road, Town of Glastonbury, Hartford County, Connecticut; CHA Project 15363-1010

Mr. Coppins:

Clough Harbour & Associates LLP (CHA) has completed the hydrologic and hydraulic evaluations for the above mentioned roadway crossing. The purpose of this letter report is to: (1) quantify the design flow rates for the contributing watershed; (2) evaluate the existing hydraulic conditions; and (3) specify the hydraulic opening (culvert size) of the proposed structure that is necessary to meet the Category 1 design standards of the U.S. Army Corps of Engineers Programmatic General Permit for Connecticut.

HYDROLOGIC EVALUATION

The culvert crossing under the roadway at 497A Wickham Road conveys an unnamed and unclassified tributary of Hubbard Brook (Class B/A waterway). The drainage area upstream of the crossing is approximately 48.7 acres (0.076 mi²) (See Watershed Map). Aerial photos of the watershed show that it is primarily composed of forested and residential area, and is intersected by State Route 2. The USGS Glastonbury Quadrangle Map indicates that the predominant landform is moderately to steeply sloped hills, with elevations ranging from 500± ft along the northeastern watershed boundary to 200± ft at the upstream face of the proposed culvert location.

In order to evaluate the potential impacts associated with the development of the site, existing and proposed condition hydrographs were generated using a type III rainfall distribution. Rainfall amounts were referenced from Appendix B of the Connecticut Department of Transportation Drainage Manual dated October 2000. The 24-hour rainfall amounts for the 2-, 5-, 10-, 50-, and 100-year design storms in Hartford County are 3.2-, 4.1-, 4.7-, 6.2-, and 6.9-inches, respectively.

Runoff curve numbers and times of concentration were computed using standard NRCS TR-55 methodology. Additionally, peak stormwater flows and hydrographs for the existing and post development conditions were computed using the Haestad Method's Pondpack Hydrology Program (Version 10.0).

The results of the hydrologic analysis are presented in Table 1 below and detailed calculations are included in the technical appendix.

Peak Discharges (ft /sec) Design Point Watershed Drainage Location Атеа Area (acres) 5-year 2-vear 10-vear 50-year 100-year DA-1A 4.92 1.0 2.5 3.8 7.5 9.4 Montano Cell DA-1B 3.50 **4.1** 5.9 7.1 10.2 11.6 Site at 497A DA-1C 40.28 16.3 31.6 43.0 74.7 90.6 Wickham Road Totals: 48.7 21.4 39.7 53.3 91.2 110.0

Table 1 - Summary of Design Flows

HYDRAULIC EVALUATION

Basis of Design

In accordance with the engineering guidelines established by the Category 1 Requirements of the U.S. Army Corps of Engineers, driveway/roadway crossings constructed on brooks, streams, rivers and their tributaries must be designed to allow for continuous flow of the 50-year frequency storm flows. For a crossing constructed using a single box culvert, the inverts must be set a minimum of 12 inches below the streambed elevation and the culvert slope must also be no steeper than the streambed gradient immediately upstream or downstream of the culvert. The hydraulic performance of a culvert is commonly expressed as a ratio of depth of water measured from the invert of the culvert to the diameter or rise of the culvert (HW/D). As such, ConnDOT requirements specify that a HW/D ratio less than or equal to 1.5 must be used as a design standard for the culvert design.



Design Methodology

The roadway crossing for the Montano Cell Site at 497A Wickham Road was analyzed using Haestad Methods CulvertMaster Computer Software (Version 3.1). This program was used to compute the headwater elevation at the culvert, evaluating both inlet and outlet control equations. The required geometry and channel slope necessary for the hydraulic evaluation was based on a combination of record information and data obtained from a recent site visit. In addition, the results of the hydraulic analysis were based on the assumption of unobstructed flow through the culvert section.

HYDRAULIC RESULTS

Proposed Condition

Several shape and size options were investigated in order to maximize the hydraulic opening of the proposed culvert while minimizing the impact and cost. The most favorable solution is to use a 6' x 6' concrete box culvert. The results of the hydraulic analysis for the box culvert chosen are summarized in Table 2 below and indicate that the proposed culvert will convey the 50-year design storm with a HW/D ratio of 0.83.

Table 2 - Summary of the Proposed Condition Hydraulic Analysis @ Montano Cell Site

Hydraulic Design Parameters	Storm Event Recurrence Interval				
	50-year	100-year			
HW/D ratio	0.83	0.85			
Freeboard (ft)	1.0	0.9			
Outlet Velocity (ft/sec)	12.5	12.6			

RECOMMENDATIONS

Based on the hydraulic analysis, the proposed concrete box culvert has excess conveyance capacity during the 50-year design storm event. The proposed culvert will provide 36 ft² of cross-sectional opening (6ft² of which



November 21, 2007

Montano Cell Site - Hydrologic & Hydraulic Evaluation

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will be submerged below the streambed) and will convey the 50-year design storm with a HW/D ratio of 0.83. Additionally, discharge velocities in the downstream channel will remain essentially unchanged from the existing to the proposed condition. In summary, the results of the analysis indicate that the proposed culvert design meets the Category 1 hydraulic design guidelines established by the U.S. Army Corps of Engineers, as well as requirement set forth by the Connecticut Department of Transportation.

We trust that this letter report meets your needs. However, should you have any questions or concerns, please feel free to contact our office.

Sincerely,

CLOUGH HARBOUR & ASSOCIATES LLP

Peter L. Lilholt, Jr., P.E.

Associate



Job File: W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\OPT. Rain Dir: W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\

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Project Date: 11/12/2007 Project Engineer: KZD Project Title: Existing Conditions Project Comments: Optasite Project Glastonbury, CT

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DA-1C To Cales	2.08
**************************************	****
DA-1A Runoff CN-Area	3.01
DA-1B Runoff CN-Area	3.02
DA-1C Runoff CN-Area	3.03

Type.... Master Network Summary

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Name.... Watershed

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MASTER DESIGN STORM SUMMARY

Network Storm Collection: Glastonbury

Return Event	Total Depth in	Rainfall Type	RNF ID
2	3.2000	Synthetic Curve	TypeIII 24hr
5	4.1000	Synthetic Curve	TypeIII 24hr
10	4.7000	Synthetic Curve	TypeIII 24hr
50	6.2000	Synthetic Curve	TypeIII 24hr
100	6.9000	Synthetic Curve	TypeIII 24hr

MASTER NETWORK SUMMARY SCS Unit Hydrograph Method

(*Node=Outfall; +Node=Diversion;)
(Trun= HYG Truncation: Blank=None; L=Left; R=Rt; LR=Left&Rt)

		Return	HYG Vol	Qpeak	Qpeak	Max WSEL	Max Bond Stores
Node ID	Type	Event	ac-ft	hrs	cfs	ft ft	Pond Storage ac-ft
CULVERT IN	JCT	2	2.307	 12.3500	16.30		
CULVERT IN	JCT	5	4.052	12.3500	31.59		
CULVERT IN	JCT	10	5.363	12.3500	42.96		
CULVERT IN	JCT	50	9.005	12.3000	74.70		
CULVERT_IN	JCT	100	10.836	12.3000	90.60		
CULVERT_OUT	JCT	2	3.009	12.4500	21.38		
CULVERTOUT	JCT	5	5,152	12.4500	39.65	•	
CULVERT OUT	JCT	10	6.754	12.4000	53.30		
CULVERTOUT	JCT	50	11.186	12.4000	91.20		
CULVERT_OUT	JCT	100	13.409	12.4000	110.01		
DA-1A	AREA	2	.167	12.3500	1.00		
DA-1A	AREA	5	.333	12.3000	2.53		
DA-1A	AREA	10	.463	12.3000	3.78		
DA-1A	AREA	50	.842	12.2500	7.46		
DA-1A	AREA	100	1.038	12.2500	9.37		

Type.... Master Network Summary

Page 1.02

Name.... Watershed

MASTER NETWORK SUMMARY SCS Unit Hydrograph Method

(*Node=Outfall; +Node=Diversion;) (Trun= HYG Truncation: Blank=None; L=Left; R=Rt; LR=Left&Rt)

Node ID	Туре	Return Event	HYG Vol ac-ft	Trun	Qpeak hrs	Qpeak cfs	Max WSEL ft	Max Pond Storage ac-ft
DA-1B	AREA	2	.534		12.3500	4.14		
DA-1B	AREA	2 5	.768		12.3500	5.93		
DA-1B	AREA	10	.929		12.3500	7.14		
DA-1B	AREA	50	1.340		12.3500	10.18		
DA-1B	AREA	100	1.535		12.3500	11.59		
DA-1C	AREA	2	2.307		12.3500	16.30		
DA-1C	AREA	2 5	4.052		12.3500	31.59		
DA-1C	AREA	10	5.363		12.3500	42.96		
DA-1C	AREA	50	9.005		12.3000	74.70		
DA-1C	AREA	100	10.836		12.3000	90.60		
*DESIGN POINT	JCT	2	3.009		12.5000	21.38		
*DESIGN POINT	JCT	5	5.152		12.5000	39.65		
*DESIGN POINT	JCT	10	6.754		12.4500	53.30		
*DESIGN POINT	JCT	50	11.186		12.4500	91.20		
*DESIGN POINT	JCT	100	13.409		12.4500	110.01		
MID_CULVERT	JCT	2	2.841		12.4000	20.42		
MID_CULVERT	JCT	5	4.820		12.4000	37.46		
MID_CULVERT	JCT		6.291		12.4000	50.02		
	JCT	50	10.344		12.3500	84.88		
MID_CULVERT	JCT	100	12.371		12.3500	102.19		

Name.... DA-1A

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

TIME OF CONCENTRATION CALCULATOR

Segment #1: Tc: TR-55 Sheet

Mannings n .4000 Hydraulic Length 150.00 ft 2yr, 24hr P 3.2000 in Slope .067000 ft/ft

Avg. Velocity .14 ft/sec

Segment #1 Time: .3052 hrs

Segment #2: Tc: TR-55 Shallow

Hydraulic Length 180.00 ft .028000 ft/ft Slope

Unpaved

Avg.Velocity 2.70 ft/sec

Segment #2 Time: .0185 hrs

________ Total Tc: .3237 hrs ________________

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Type.... Tc Calcs Page 2.02
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Name.... DA-1A

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```

Tc Equations used...

Tc = (.007 * ((n * Lf) **0.8)) / ((P**.5) * (Sf**.4))

Where: Tc = Time of concentration, hrs

n = Mannings n
Lf = Flow length, ft

P = 2yr, 24hr Rain depth, inches

Sf = Slope, %

Unpaved surface:

V = 16.1345 * (Sf**0.5)

Paved surface:

V = 20.3282 * (Sf**0.5)

Tc = (Lf / V) / (3600sec/hr)

Where: V = Velocity, ft/sec

Sf = Slope, ft/ft

Tc = Time of concentration, hrs

Lf = Flow length, ft

Name.... DA-1B

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

TIME OF CONCENTRATION CALCULATOR

Segment #1: Tc: TR-55 Sheet

Mannings n .4000 Hydraulic Length 150.00 ft 2yr, 24hr P 3.2000 in Slope .030000 ft/ft

Avg.Velocity .10 ft/sec

Segment #1 Time: .4209 hrs

Segment #2: Tc: TR-55 Shallow

Hydraulic Length 710.00 ft .080000 ft/ft Slope

Unpaved

Avg. Velocity 4.56 ft/sec

Segment #2 Time: .0432 hrs

Segment #3: Tc: TR-55 Channel

FIOW Area .9500 sq.ft
Wetted Perimeter 4.50 ft
Hydraulic Radius .21 ft
Slope Slope .070000 ft/ft Mannings n .0150 Mannings n .0150 Hydraulic Length 50.00 ft

Avg.Velocity 9.32 ft/sec

Segment #3 Time: .0015 hrs

Name.... DA-1B

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

Segment #4: Tc: TR-55 Channel

2.8000 sq.ft
Wetted Perimeter 11.70 ft
Hydraulic Radius .24 ft
Slope Slope .033000 ft/ft
Mannings n .0600
Hydraulic Length 100.00 ft

Avg. Velocity 1.74 ft/sec

Segment #4 Time: .0160 hrs

Segment #5: Tc: TR-55 Channel

Flow Area 2.7000 sq.ft
Wetted Perimeter
Hydraulic Radius .43 ft
Slope .033000 ft/ft
Mannings n
Hydraulic T Hydraulic Length 100.00 ft

Avg.Velocity 2.56 ft/sec

Segment #5 Time: .0108 hrs

Segment #6: Tc: TR-55 Channel

2.1000 sq.ft Flow Area Wetted Perimeter 5.10 ft
Hydraulic Radius .41 ft Hydraulic Radius .41 ft
Slope .033000 ft/ft
Mannings n .0600 Hydraulic Length 100.00 ft

Avg. Velocity 2.50 ft/sec

Segment #6 Time: .0111 hrs

Name.... DA-1B

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

Segment #7: Tc: TR-55 Channel

1.7000 sq.ft Flow Area Wetted Perimeter 4.20 ft Hydraulic Radius .40 ft Slope .033000 ft/ft Mannings n .0600 Mannings n .0600 Hydraulic Length 50.00 ft

Avg.Velocity 2.47 ft/sec

Segment #7 Time: .0056 hrs

Segment #8: Tc: TR-55 Channel

Flow Area 15.9000 sq.ft Wetted Perimeter 1.50 ft 10.00 ft 510pe .005000 ft/ft Mannings n .0240 Hydraulic Radius 10.60 ft Hydraulic Length 95.00 ft

Avg. Velocity 21.18 ft/sec

Segment #8 Time: .0012 hrs

Total Tc: .5104 hrs

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Type.... Tc Calcs
Name.... DA-1B
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Lf = Flow length, ft

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

Page 2.06

```
Tc Equations used...
Tc = (.007 * ((n * Lf)**0.8)) / ((P**.5) * (Sf**.4))
   Where: Tc = Time of concentration, hrs
         n = Mannings n
         Lf = Flow length, ft
         P = 2yr, 24hr Rain depth, inches
         Sf = Slope, %
Unpaved surface:
   V = 16.1345 * (Sf**0.5)
   Paved surface:
   V = 20.3282 * (Sf**0.5)
   Tc = (Lf / V) / (3600sec/hr)
   Where: V = Velocity, ft/sec
         Sf = Slope, ft/ft
         Tc = Time of concentration, hrs
```

```
Type.... Tc Calcs
```

Name... DA-1B

Page 2.07

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

www SCS Channel Flow www.commons.commons.commons.commons.commons.commons.com

V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n

Tc = (Lf / V) / (3600sec/hr)

Where: R = Hydraulic radius

Aq = Flow area, sq.ft.

Wp = Wetted perimeter, ft

V = Velocity, ft/sec

Sf = Slope, ft/ft

n = Mannings n

Tc = Time of concentration, hrs

Lf = Flow length, ft

Name.... DA-1C

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

TIME OF CONCENTRATION CALCULATOR

Segment #1: Tc: TR-55 Sheet

Mannings n .4000 Hydraulic Length 150.00 ft 2yr, 24hr P 3.2000 in Slope .100000 ft/ft

Avg. Velocity .16 ft/sec

Segment #1 Time: .2600 hrs

Segment #2: Tc: TR-55 Shallow

Hydraulic Length 130.00 ft .080000 ft/ft Slope

Unpaved

Avg.Velocity 4.56 ft/sec

Segment #2 Time: .0079 hrs

Segment #3: Tc: TR-55 Shallow

Hydraulic Length 270.00 ft Slope .190000 ft/ft Unpaved

Avg. Velocity 7.03 ft/sec

Segment #3 Time: .0107 hrs

Name.... DA-1C

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

Segment #4: Tc: TR-55 Shallow

Hydraulic Length 463.00 ft Slope .060000 ft/ft

Unpaved

Avg.Velocity 3.95 ft/sec

Segment #4 Time: .0325 hrs

Segment #5: Tc: TR-55 Channel

15.9000 sq.ft Flow Area Wetted Perimeter 1.50 ft Hydraulic Radius 10.60 ft Hydraulic Radius 10.60 ft Slope .005000 ft/ft Mannings n .0240 Hydraulic Length 200.00 ft

Avg. Velocity 21.18 ft/sec

Segment #5 Time: .0026 hrs

Segment #6: Tc: TR-55 Channel

.9500 sq.ft Flow Area Wetted Perimeter 4.50 ft
Hydraulic Radius .21 ft
Slope .070000 ft/ft
Mannings n .0150 Hydraulic Length 50.00 ft

Avg. Velocity 9.32 ft/sec

Segment #6 Time: .0015 hrs

Page 2.10 Type.... Tc Calcs

Name.... DA-1C

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

Segment #7: Tc: TR-55 Channel

Flow Area 2.8000 sq.ft Wetted Perimeter 11.70 ft
Hydraulic Radius .24 ft
Slope .033000 ft/ft
Mannings n .0600 Hydraulic Length 100.00 ft

Avg.Velocity 1.74 ft/sec

Segment #7 Time: .0160 hrs

Segment #8: Tc: TR-55 Channel

Flow Area 2.7000 sq.ft
Wetted Perimeter 6.30 ft
Hydraulic Radius .43 ft
Slope .033000 ft/ft
Mannings n .0600 Mannings n .0600 Hydraulic Length 100.00 ft

Avg.Velocity 2.56 ft/sec

Segment #8 Time: .0108 hrs _____

Segment #9: Tc: TR-55 Channel

Flow Area 2.1000 sq.ft
Wetted Perimeter
Hydraulic Radius
Slope .033000 ft/ft
Mannings n .0600 Hydraulic Length 100.00 ft

Avg.Velocity 2.50 ft/sec

Segment #9 Time: .0111 hrs Type.... Tc Calcs Page 2.11

Name.... DA-1C

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

Segment #10: Tc: TR-55 Channel

rlow Area 1.7000 sq.ft
Wetted Perimeter
Hydraulic Radius
Slope .033000 ft/ft
Mannings n .0600
Hydraulic Jorgan Mannings n .0600 Hydraulic Length 50.00 ft

Avg. Velocity 2.47 ft/sec

Segment #10 Time: .0056 hrs

Segment #11: Tc: TR-55 Shallow

Hydraulic Length 1253.00 ft 310pe .100000 ft/ft Unpaved

Avg. Velocity 5.10 ft/sec

Segment #11 Time: .0682 hrs

> Total Tc: .4271 hrs that that sale bull tool date from left take abot lock abot from both abou and both arm mad both some some some

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Type.... Tc Calcs
                                                                                                                                                                                                                                        Page 2.12
Name.... DA-1C
\label{thm:connecticut} File.... \verb|W:\Optasite|Connecticut|15363|Sites|1010| Montano B-Glastonbury|Misc|Pondpack|Optable | Connecticut| | C
   Tc Equations used...
    Tc = (.007 * ((n * Lf) **0.8)) / ((P**.5) * (Sf**.4))
                       Where: Tc = Time of concentration, hrs
                                                      n = Mannings n
                                                      Lf = Flow length, ft
                                                       P = 2yr, 24hr Rain depth, inches
                                                       Sf = Slope, %
    Unpaved surface:
                       V = 16.1345 * (Sf**0.5)
                       Paved surface:
                       V = 20.3282 * (Sf**0.5)
                        Tc = (Lf / V) / (3600sec/hr)
                        Where: V = Velocity, ft/sec
```

Sf = Slope, ft/ft

Lf = Flow length, ft

Tc = Time of concentration, hrs

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Page 2.13
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Type.... Tc Calcs
Name.... DA-1C

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

R = Aq / WpV = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n

Tc = (Lf / V) / (3600sec/hr)

Where: R = Hydraulic radius

Aq = Flow area, sq.ft.
Wp = Wetted perimeter, ft
V = Velocity, ft/sec

Sf = Slope, ft/ft n = Mannings n

Tc = Time of concentration, hrs

Lf = Flow length, ft

Type.... Runoff CN-Area Page 3.01

Name... DA-1A

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

RUNOFF CURVE NUMBER DATA

··

Soil/Surface Description	CN	Area acres	Impervious Adjustment %C %UC	Adjusted CN
Impervious	98	1.427	No. 200 NO. 200 400	98.00
HSG D - Woods	77	.839		77,00
HSG B - Woods	55	,358		55.00
HSG A - Woods	30	2.296		30.00
COMPOSITE AREA & WEIGHTED CN>		4.920		59.56 (60)

Type Runoff CN-Area Name DA-1B		Page 3.02	
File W:\Optasite\Connecticut\3	5363\Sites\1010 Montand	o B-Glastonbury\Misc\Pondpack\Op	pta
RUNOFF CURVE NUMBER DATA			
Soil/Surface Description	Imper Area Adjust CN acres %C	vious tment Adjusted %UC CN 	

Name... DA-1C

File.... W:\Optasite\Connecticut\15363\Sites\1010 Montano B-Glastonbury\Misc\Pondpack\Opta

RUNOFF CURVE NUMBER DATA

~~~~~			CN
98	-515		98.00
82	5.930		82.00
72	6.155		72.00
77	3.095		77.00
70	8.824		70.00
65	.177		65.00
58	.039		58.00
55	15.549		55.00
	40.285		67.14 (67)
	82 72 77 70 65 58 55	82 5.930 72 6.155 77 3.095 70 8.824 65 .177 58 .039 55 15.549	82 5.930 72 6.155 77 3.095 70 8.824 65 .177 58 .039 55 15.549

Appendix A A-1

Index of Starting Page Numbers for ID Names

---- D ----DA-1A... 2.01, 3.01 DA-1B... 2.03, 3.02 DA-1C... 2.08, 3.03

----- W -----Watershed... 1.01

S/N: 39YXYWGXW886 Bentley PondPack (10.00.025.00) 10:56 AM

## **Culvert Calculator Report** Worksheet-50 Year

Solve For: Discharge

Culvert Summary					
Allowable HW Elevation	206.40	ft	Headwater Depth/Height 0.80		
Computed Headwater Elev-	ε 206,40	ft	Discharge 108.20		cfs
Inlet Control HW Elev.	206.02	ft	Tailwater Elevation	202.64	ft
Outlet Control HW Elev.	206.40	ft	Control Type E	Entrance Control	
Grades					
Upstream Invert	202.40	ft	Downstream Invert	201.40	ft
Length	40.00	ft	Constructed Slope	0.025000	ft/ft
Hydraulic Profile					
Profile	\$2		Depth, Downstream	1.44	ft
Slope Type	Steep		Normal Depth	1.14	ft
Flow Regime	Supercritical		Critical Depth	2.16	ft
Velocity Downstream	12.53	ft∕s	Critical Slope	0.003927	ft/ft
Section					
Section Shape	Вох		Mannings Coefficient	0.013	
Section Material	Concrete		Span	6.00	ft
Section Size	6 x 5 ft		Rise	5.00	ft
Number Sections	1				
Outlet Control Properties					
Outlet Control HW Elev.	206.40	ft	Upstream Velocity Head	1.08	ft
Ke	0.70		Entrance Loss	0.76	ft
Inlet Control Properties		****			
Inlet Control HW Elev.	206.02	ft	Flow Control	Unsubmerged	
Inlet Type 0° w	ingwall flares		Area Full	30.0	ft²
K	0.06100		HDS 5 Chart	8	
M	0.75000		HDS 5 Scale	3	
С	0.04230		Equation Form	1	
Y	0.82000				

## Culvert Calculator Report Worksheet-100 Year

## Solve For: Discharge

<del></del>					
Culvert Summary					
Allowable HW Elevation	206.50	ft	Headwater Depth/Heigh	t 0.82	
Computed Headwater Elev	e 206.50	ft	Discharge	112.29	cfs
inlet Control HW Elev.	206.11	ft	Tallwater Elevation	202.85	ft
Outlet Control HW Elev.	206.50	ft	Control Type E	Entrance Control	
Grades					
Upstream Invert	202,40	ft	Downstream Invert	201.40	ft
Length	40.00	ft	Constructed Slope	0.025000	ft/ft
Hydraulic Profile					
Profile	\$2	****	Depth, Downstream	1.48	ft
Slope Type	Steep		Normal Depth	1.16	ft
Flow Regime	Supercritical		Critical Depth	2.22	ft
Velocity Downstream	12.63	ft/s	Critical Slope	0.003949	ft/ft
Section					
Section Shape	Box		Mannings Coefficient	0.013	
Section Material	Concrete		Span	6.00	ft
Section Size	6 x 5 ft		Rise	5.00	ft
Number Sections	1				
Outlet Control Properties					
Outlet Control HW Elev.	206.50	ft	Upstream Velocity Head	1.11	ft
Ke	0.70		Entrance Loss	0.78	ft
Inlet Control Properties					
Inlet Control HW Elev.	206.11	ft	Flow Control	Unsubmerged	·····
Inlet Type 0° w	ingwall flares		Area Full	30.0	ft²
K	0.06100		HDS 5 Chart	8	
M	0.75000		HDS 5 Scale	3	
C	0.04230		Equation Form	1	
Υ	0.82000				

