

July 13, 2015

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Re: **Petition No. 1121 – Cellco Partnership d/b/a Verizon Wireless Petition for Declaratory Ruling that No Certificate of Environmental Compatibility and Public Need is Required for the Proposed Replacement of and Modification to an Existing Telecommunications Facility at 353 Pumpkin Hill Road, Ashford, Connecticut**

Dear Ms. Bachman:

In accordance with the requirements of the Council's January 8, 2015 approval of the above-referenced Petition, enclosed please find the original and two (2) copies of the following information:

1. Design drawings for the proposed telecommunications facility at 353 Pumpkin Hill Road. Please note that the required wetland restoration and monitoring plan details are included on Plan Sheet C-1.2. Also note that the tower setback radius of 240 feet is noted on Plan Sheet C-1.1.
2. Tower and foundation design materials for the 240-foot self-supporting lattice tower stamped by William Heiden III, Professional Engineer licensed in the State of Connecticut.

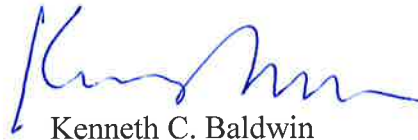
Currently, Cellco anticipates that construction of the new tower at 353 Pumpkin Hill Road will commence on or about September 1, 2015. In accordance with the Council's approval, further notification will be provided upon completion of site improvements and the removal of the existing guyed lattice tower. Once finalized, we will also provide the Council

Melanie A. Bachman
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with information regarding the FAA's determination with respect to the type of lighting required on this facility prior to operation.

If you have any questions or need any additional information please contact me.

Sincerely,

A handwritten signature in blue ink, appearing to read "Kenneth C. Baldwin".

Kenneth C. Baldwin

KCB/kmd
Enclosures
Copy to:

Anthony Befera
Brian Paul
Jim Smith

Cellco Partnership

d.b.a. verizon wireless

WIRELESS COMMUNICATIONS FACILITY

ASHFORD RELO., CT

353 PUMPKIN HILL ROAD

ASHFORD, CT 06278

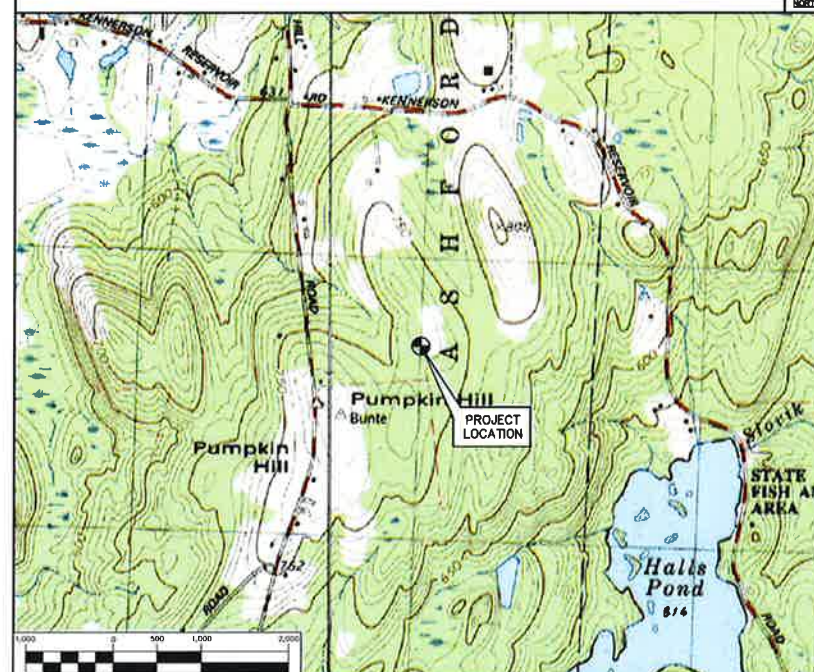
GENERAL NOTES

1. ALL WORK SHALL BE IN ACCORDANCE WITH THE 2003 INTERNATIONAL BUILDING CODE AS MODIFIED BY THE 2005 CONNECTICUT SUPPLEMENT AND 2009 AMENDMENTS, INCLUDING THE TIA/EIA-222 REVISION "F" "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND SUPPORTING STRUCTURES." 2005 CONNECTICUT FIRE SAFETY CODE AND 2009 AMENDMENTS, NATIONAL ELECTRICAL CODE AND LOCAL CODES.
2. THE COMPOUND, TOWER, PRIMARY GROUND RING, ELECTRICAL SERVICE TO THE METER BANK AND TELEPHONE SERVICE TO THE DEMARCATION POINT ARE PROVIDED BY SITE OWNER. AS BUILT FIELD CONDITIONS REGARDING THESE ITEMS SHALL BE CONFIRMED BY THE CONTRACTOR. SHOULD ANY FIELD CONDITIONS PRECLUDE COMPLIANCE WITH THE DRAWINGS, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ENGINEER AND SHALL NOT PROCEED WITH ANY AFFECTED WORK.
3. CONTRACTOR SHALL REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUBCONTRACTORS AND ALL RELATED PARTIES. THE SUBCONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
4. CONTRACTOR SHALL PROVIDE A COMPLETE BUILD-OUT WITH ALL FINISHES, STRUCTURAL, MECHANICAL, AND ELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON THE DRAWINGS OR IN THE WRITTEN SPECIFICATIONS.
5. CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OVER THE WORK.
6. CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION, PLUMBING, ELECTRICAL AND HVAC. PERMITS SHALL BE PAID FOR BY THE RESPECTIVE SUBCONTRACTORS.
7. CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS AND SPECIFICATIONS ON SITE AT ALL TIMES AND INSURE DISTRIBUTION OF NEW DRAWINGS TO SUBCONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE. ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. THE CONTRACTOR SHALL FURNISH AN "AS-BUILT" SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
8. LOCATION OF EQUIPMENT, AND WORK SUPPLIED BY OTHERS THAT IS DIAGRAMMATICALLY INDICATED ON THE DRAWINGS SHALL BE DETERMINED BY THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE LOCATIONS AND DIMENSIONS SUBJECT TO STRUCTURAL CONDITIONS AND WORK OF THE SUBCONTRACTORS.
9. THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURES AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY. MAINTAIN EXISTING BUILDING'S/PROPERTY'S OPERATIONS, COORDINATE WORK WITH BUILDING/PROPERTY OWNER.
10. DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
11. ALL UTILITY WORK SHALL BE IN ACCORDANCE WITH LOCAL UTILITY COMPANY REQUIREMENTS AND SPECIFICATIONS.
12. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUBCONTRACTORS FOR ANY CONDITION PER MFR.'S RECOMMENDATIONS. CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR CONSTRUCTION MANAGER.
13. ANY AND ALL ERRORS, DISCREPANCIES, AND "MISSED" ITEMS ARE TO BE BROUGHT TO THE ATTENTION OF THE VERIZON WIRELESS CONSTRUCTION MANAGER DURING THE BIDDING PROCESS BY THE CONTRACTOR. ALL THESE ITEMS ARE TO BE INCLUDED IN THE BID. NO "EXTRA" WILL BE ALLOWED FOR MISSED ITEMS.
14. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON-SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
15. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE CONSTRUCTION MANAGER FOR REVIEW.
16. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES, AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA.
17. COORDINATION, LAYOUT, FURNISHING AND INSTALLATION OF CONDUIT AND ALL APPURTENANCES REQUIRED FOR PROPER INSTALLATION OF ELECTRICAL AND TELECOMMUNICATION SERVICE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR.
18. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
19. THE CONTRACTOR SHALL CONTACT "CALL BEFORE YOU DIG" AT LEAST 48 HOURS PRIOR TO ANY EXCAVATIONS AT 1-800-922-4455. ALL UTILITIES SHALL BE IDENTIFIED AND CLEARLY MARKED PRIOR TO ANY EXCAVATION WORK. CONTRACTOR SHALL MAINTAIN AND PROTECT MARKED UTILITIES THROUGHOUT PROJECT COMPLETION.
20. CONTRACTOR SHALL COMPLY WITH OWNERS ENVIRONMENTAL ENGINEER ON ALL METHODS AND PROVISIONS FOR ALL EXCAVATION ACTIVITIES INCLUDING SOIL DISPOSAL. ALL BACKFILL MATERIALS TO BE PROVIDED BY THE CONTRACTOR.

SITE DIRECTIONS

| | | | |
|--|--|------------|--------------------------------------|
| FROM: | 99 EAST RIVER DRIVE EAST HARTFORD, CT | TO: | 353 PUMPKIN HILL ROAD ASHFORD, CT |
| 1. HEAD EAST ON E RIVER DR | | | 253 FT. |
| 2. TURN LEFT ONTO THE CT-2 E RAMP TO NORWICH | | | 0.2 MI. |
| 3. MERGE ONTO I-84 E | | | 20.7 MI. |
| 4. TAKE EXIT 69 FOR CONNECTICUT 74 TOWARDS U.S. 44/WILLINGTON/PUTNAM | | | 0.3 MI. |
| 5. TURN RIGHT ONTO CT-74 E | | | 7.5 MI. |
| 6. TURN LEFT ONTO US-44 E | | | 3.1 MI. |
| 7. TURN RIGHT ONTO PUMPKIN HILL DRIVE, DESTINATION WILL BE ON THE LEFT | | | 1.7 MI. |

VICINITY MAP



PROJECT SUMMARY

- THE GENERAL SCOPE OF WORK CONSISTS OF THE FOLLOWING:
1. THE INSTALLATION OF A ±240' TALL SELF-SUPPORTING LATTICE TOWER TO REPLACE AN EXISTING ±300' TALL GUYED TOWER TO BE REMOVED.
 2. A TOTAL OF TWELVE (12) VERIZON WIRELESS DIRECTIONAL PANEL ANTENNAS ARE TO BE MOUNTED AT A CENTERLINE ELEVATION OF 240'-0"± AGL ON THE 240'-0"± REPLACEMENT LATTICE TOWER.
 3. EXISTING POWER AND TELCO UTILITIES AT THE SITE TO BE UPGRADED/CONSOLIDATED WITH A SINGLE MULTI-METER UTILITY BACKBOARD TO BE LOCATED ADJACENT TO THE EXISTING FENCED COMPOUND. EXISTING CARRIER UTILITIES TO BE BACKFED FROM THE MULTI-METER UTILITY BACKBOARD LOCATION.

PROJECT INFORMATION

| | |
|---|--|
| SITE NAME: | ASHFORD RELO., CT |
| SITE ADDRESS: | 353 PUMPKIN HILL ROAD ASHFORD, CT 06278 |
| LESSEE/TENANT: | CELLCO PARTNERSHIP d.b.a. VERIZON WIRELESS 99 EAST RIVER DRIVE EAST HARTFORD, CT 06108 |
| CONTACT PERSON: | BRIAN PAUL (CONSTRUCTION MANAGER) VERIZON WIRELESS (860) 305-8446 |
| PROPOSED REPLACEMENT TOWER COORDINATES: | LONGITUDE 72°-07'-17.777" LATITUDE 41°-50'-52.136" GROUND ELEVATION: 760.8'± A.M.S.L. COORDINATES AND GROUND ELEVATION ARE BASED ON FAA 1-A SURVEY CERTIFICATION AS PREPARED FOR VERIZON WIRELESS, BY MARTINEZ COUCH AND ASSOCIATES DATED SEPTEMBER 05, 2014, REVISED MARCH 25, 2015. |

SHEET INDEX

| SHT. NO. | DESCRIPTION | REV. |
|----------|--|------|
| T-1 | TITLE SHEET | 0 |
| N-1 | SITE AND FOUNDATION SPECIFICATIONS | 0 |
| C-1.0 | SITE LOCATION PLAN | 0 |
| C-1.1 | PARTIAL SITE PLAN | 0 |
| C-1.2 | WETLAND RESTORATION PLAN, DETAILS AND NOTES | 0 |
| C-2 | COMPOUND PLAN, ELEVATION & ANTENNA MOUNTING CONFIG. | 0 |
| C-3 | SITE CONSTRUCTION, S&E CONTROL NOTES & DETAILS | 0 |
| C-4 | EQUIPMENT SHELTER PLANS AND DETAILS | 0 |
| C-5 | SHELTER FOUNDATION PLAN, DETAILS, ELEVATIONS AND NOTES | 0 |
| M-1 | MECH. NOTES, SYMBOLS, DETAILS & SCHEDULES | 0 |
| M-2 | MECHANICAL PLAND & NOTES | 0 |
| M-3 | MECHANICAL SPECIFICATIONS | 0 |
| E-1 | ELECTRICAL LEGEND AND NOTES | 0 |
| E-2 | SITE UTILITY PLAN | 0 |
| E-3 | RISER DIAGRAM AND NOTES | 0 |
| E-4 | SCHEMATIC DIAGRAM AND NOTES | 0 |
| E-5 | GROUNDING PLAN AND NOTES | 0 |
| E-6 | ELECTRICAL PART PLANS AND NOTES | 0 |
| E-7 | CABLETRAY DETAILS | 0 |
| E-8 | DETAILS | 0 |
| E-9 | DETAILS | 0 |
| E-10 | DETAILS | 0 |
| E-11 | DETAILS | 0 |
| E-12 | SPECIFICATIONS | 0 |

| | |
|-------------------|-----------|
| DATE: | 05/11/15 |
| SCALE: | AS NOTED |
| JOB NO. | 14124.000 |
| TITLE SHEET | |
| T-1 | |
| Sheet No. 1 of 24 | |

ISSUED FOR CONSTRUCTION
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DRAWN BY
CHKD BY
DATE
REV.

PROFESSIONAL ENGINEER SEAL
CENTEK engineering
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652 North Broad Road
Branford, CT 06405
www.CentekEng.com

Verizon Wireless
WIRELESS COMMUNICATIONS FACILITY
ASHFORD RELO., CT
353 PUMPKIN HILL ROAD
ASHFORD, CT 06278

SITE AND FOUNDATION SPECIFICATIONS

DESIGN BASIS

GOVERNING CODE: 2003 INTERNATIONAL BUILDING CODE (IBC) AS MODIFIED BY THE 2005 CONNECTICUT STATE BUILDING CODE AND 2009 AMENDMENTS.

1. DESIGN CRITERIA:

- * **BASIC WIND SPEED:**
WINDHAM COUNTY; V=85 MPH (FASTEST MILE) [SECTION 16 OF TIA/EIA-222-F-1996]
WINDHAM COUNTY; V=110 MPH (3 SECOND GUST) [ANNEX B OF TIA-222-G]
ASHFORD; V=100 MPH (FASTEST MILE)
EQUIVALENT TO V=80 MPH (3 SECOND GUST) [APPENDIX K OF 2005 CT BUILDING CODE SUPPLEMENT]
- LOAD CASES USED:**
LOAD CASE 1: 110 MPH WIND SPEED W/ NO ICE PLUS GRAVITY LOAD (CLASS III STRUCTURE TYPE, EXPOSURE CATEGORY C) [ANNEX B OF TIA-222-G-2005]
LOAD CASE 2: 50 MPH WIND SPEED W/ 1.00" RADIAL ICE PLUS GRAVITY LOAD (CLASS III STRUCTURE TYPE, EXPOSURE CATEGORY C) [ANNEX B OF TIA-222-G-2005]
LOAD CASE 3: 80 MPH WIND SPEED W/ 0.50" RADIAL ICE PLUS GRAVITY LOAD [SECTION 16 OF TIA/EIA-222-F-1996]
- * **SEISMIC LOAD (DOES NOT CONTROL):** [SECTION 1614.5 OF 2005 CT STATE BUILDING CODE]

SPECIAL INSPECTIONS

- SPECIAL INSPECTIONS ARE TO BE PROVIDED BY AN APPROVED AGENCY HIRED BY VERIZON WIRELESS. REFER TO THE STATEMENT OF SPECIAL INSPECTIONS PREPARED BY CENTEK ENGINEERING, INC. DATED 07.09.15.

GENERAL NOTES

- IF ANY FIELD CONDITIONS EXIST WHICH PRECLUDE COMPLIANCE WITH THE DRAWINGS, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ENGINEER AND SHALL PROCEED WITH AFFECTED WORK AFTER CONFLICT IS SATISFACTORILY RESOLVED.
- DIMENSIONS AND DETAILS SHALL BE CHECKED AGAINST THE PRE MANUFACTURED EQUIPMENT BUILDING SHOP DRAWINGS.
- THE CONTRACTOR SHALL VERIFY AND COORDINATE THE SIZE AND LOCATION OF ALL OPENINGS, SLEEVES AND ANCHOR BOLTS AS REQUIRED BY ALL TRADES.
- REFER TO DRAWING T1 FOR ADDITIONAL NOTES AND REQUIREMENTS.

SITE NOTES

- THE CONTRACTOR SHALL CALL UTILITIES PRIOR TO THE START OF CONSTRUCTION.
- ACTIVE EXISTING UTILITIES, WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES. THE ENGINEER SHALL BE NOTIFIED IMMEDIATELY, PRIOR TO PROCEEDING, SHOULD ANY UNCOVERED EXISTING UTILITY PRECLUDE COMPLETION OF THE WORK IN ACCORDANCE WITH THE CONTRACT DOCUMENTS.
- ALL RUBBISH, STUMPS, DEBRIS, STICKS, STONES AND OTHER REFUSE SHALL BE REMOVED OFF SITE AND BE LEGALLY DISPOSED, AT NO ADDITIONAL COST.
- THE SITE SHALL BE GRADED TO CAUSE SURFACE WATER TO FLOW AWAY FROM THE EQUIPMENT AND TOWER AREAS.
- NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OR EMBANKMENT.
- THE SUBGRADE SHALL BE COMPACTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE APPLICATION.
- THE AREAS OF THE COMPOUND DISTURBED BY THE WORK SHALL BE RETURNED TO THEIR ORIGINAL CONDITION.
- CONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES, SHALL BE IN CONFORMANCE WITH THE LOCAL GUIDELINES FOR EROSION AND SEDIMENT CONTROL.
- IF ANY FIELD CONDITIONS EXIST WHICH PRECLUDE COMPLIANCE WITH THE DRAWINGS, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ENGINEER AND SHALL PROCEED WITH AFFECTED WORK AFTER CONFLICT IS SATISFACTORILY RESOLVED.
- DIMENSIONS AND DETAILS SHALL BE CHECKED AGAINST THE PRE MANUFACTURED EQUIPMENT BUILDING SHOP DRAWINGS.

EARTHWORK NOTES

- COMPACTED GRAVEL FILL SHALL BE FURNISHED AND PLACED AS A FOUNDATION FOR STRUCTURES, WHERE SHOWN ON THE CONTRACT DRAWINGS OR DIRECTED BY THE ENGINEER.
- CRUSHED STONE FILL SHALL BE PLACED IN 12" MAX. LIFTS AND CONSOLIDATED USING A HAND OPERATED VIBRATORY PLATE COMPACTOR WITH A MINIMUM OF 2 PASSES OF COMPACTOR PER LIFT.
- COMPACTED GRAVEL FILL TO BE WELL GRADED BANK RUN GRAVEL MEETING THE FOLLOWING GRADATION REQUIREMENTS:

| SIEVE DESIGNATION | % PASSING |
|-------------------|-----------|
| 1 1/2" | 100 |
| No. 4 | 40-70 |
| No. 100 | 5-20 |
| No. 200 | 4-8 |
- CRUSHED STONE TO BE UNIFORMLY GRADED, CLEAN, HARD PROCESS AGGREGATE MEETING THE FOLLOWING GRADATION REQUIREMENTS:

| SIEVE DESIGNATION | % PASSING |
|-------------------|-----------|
| 1" | 100 |
| 3/4" | 90-100 |
| 1/2" | 0-15 |
| 3/8" | 0-5 |
- SELECT BACKFILL FOR FOUNDATION WALLS SHALL BE FREE OF ORGANIC MATERIAL, TOPSOIL, DEBRIS AND BOULDERS LARGER THAN 6".
- GRAVEL AND GRANULAR FILL SHALL BE INSTALLED IN 8" MAX. LIFTS. COMPACTED TO 95% MIN. AT MAX. DRY DENSITY.
- NON WOVEN GEOTEXTILE FOR SEPARATION PURPOSES SHALL BE MIRAFI 140N, OR ENGINEER APPROVED EQUAL.

CONCRETE CONSTRUCTION

- CONCRETE CONSTRUCTION SHALL CONFORM TO THE FOLLOWING STANDARDS:
ACI 211 - STANDARD PRACTICE FOR SELECTING PROPORTIONS FOR NORMAL AND HEAVYWEIGHT CONCRETE.
ACI 301 - SPECIFICATIONS FOR STRUCTURAL CONCRETE FOR BUILDINGS.
ACI 302 - GUIDE FOR CONCRETE FLOOR AND SLAB CONSTRUCTION
ACI 304 - RECOMMENDED PRACTICE FOR MEASURING, MIXING, TRANSPORTING, AND PLACING CONCRETE.
ACI 306.1 STANDARD SPECIFICATION FOR COLD WEATHER CONCRETING
ACI 318 - BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE.
- CONCRETE SHALL DEVELOP COMPRESSIVE STRENGTH IN 28 DAYS AS FOLLOWS:
SLABS ON GRADE 4,000 PSI
ALL OTHER CONCRETE 3,000 PSI
- REINFORCING STEEL SHALL BE 60,000 PSI YIELD STRENGTH.
- WELDED WIRE FABRIC SHALL CONFORM TO ASTM- A-185.
- ALL DETAILING, FABRICATION, AND ERECTION OF REINFORCING BARS, UNLESS OTHERWISE NOTED, MUST FOLLOW THE LATEST ACI CODE AND LATEST ACI "MANUAL OF STANDARD PRACTICE FOR DETAILING REINFORCED CONCRETE STRUCTURES".
- CONCRETE COVER OVER REINFORCING SHALL CONFORM TO THE FOLLOWING, UNLESS OTHERWISE SHOWN:
SURFACES EXPOSED TO THE WEATHER 1-1/2 INCHES
FORMED SURFACES EXPOSED TO EARTH 1-1/2 INCHES
BOTTOM OF FOOTINGS 3 INCHES
SURFACES NOT EXPOSED TO EARTH OR WEATHER 1-1/2 INCHES
- NO STEEL WIRE, METAL FORM TIES, OR ANY OTHER METAL SHALL REMAIN WITHIN THE REQUIRED COVER OF ANY CONCRETE SURFACE.
- ALL REINFORCEMENT SHALL BE CONTINUOUS UNLESS OTHERWISE NOTED. SPLICES SHALL BE WELL STAGGERED. ADDITIONAL BARS AND SPECIAL BENDING DETAILS ARE REQUIRED AT INTERSECTING WALLS AND AT JOINTS. SUCH DETAILS SHALL COMPLY WITH ACI 318 RECOMMENDATIONS UNLESS OTHERWISE SHOWN.
- NO TACK WELDING OF REINFORCING WILL BE PERMITTED.
- NO CALCIUM CHLORIDE OR ADMIXTURES CONTAINING MORE THAN 1 % CHLORIDE BY WEIGHT OF ADMIXTURE SHALL BE USED IN THE CONCRETE.
- UNLESS OTHERWISE NOTED, ALL LAP SPLICES SHALL BE 48 BAR DIAMETERS.
- SHEAR KEYS (2" X 4"), SEPARATING CONCRETE POURS, SHALL BE PROVIDED IN ALL CONCRETE WALLS AND BETWEEN FOOTINGS AND WALLS.
- AT ALL OPENINGS IN CONCRETE WALLS AND SUSPENDED SLABS, UNLESS OTHERWISE DETAILED, PROVIDE THE FOLLOWING ADDITIONAL REINFORCING:
1 - #4 EACH FACE AT EACH SIDE OF OPENING. EXTEND 2'-0" BEYOND OPENING.
1 - #4 X 4'-0" LONG EACH FACE DIAGONALLY AT EACH CORNER.
- INSPECTION AND TESTING OF CONCRETE WORK SHALL BE PERFORMED BY AN INDEPENDENT TESTING LABORATORY, PAID BY THE OWNER, AND APPROVED BY THE ARCHITECT. THE INSPECTOR SHALL OBSERVE CONDITION OF SOILS AND FORMWORK BEFORE FOOTINGS ARE PLACED, SIZE, SPACING AND LOCATION OF REINFORCEMENT, AND PLACEMENT OF CONCRETE.
- THE TESTING COMPANY SHALL ALSO OBTAIN A MINIMUM OF THREE (3) COMPRESSIVE STRENGTH TEST SPECIMENS FOR EACH CONCRETE MIX DESIGN. ONE SPECIMEN TESTED AT 7 DAYS, ONE AT 28 DAYS, AND ONE HELD IN RESERVE FOR FUTURE TESTING, IF NEEDED.
- FOUR COPIES OF ALL INSPECTION TEST REPORTS SHALL BE SUBMITTED TO THE ARCHITECT WITHIN TEN (10) WORKING DAYS OF THE DATE OF INSPECTION.

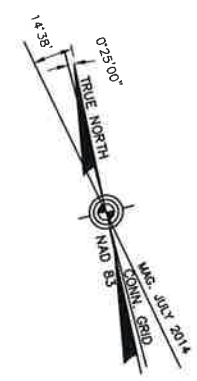
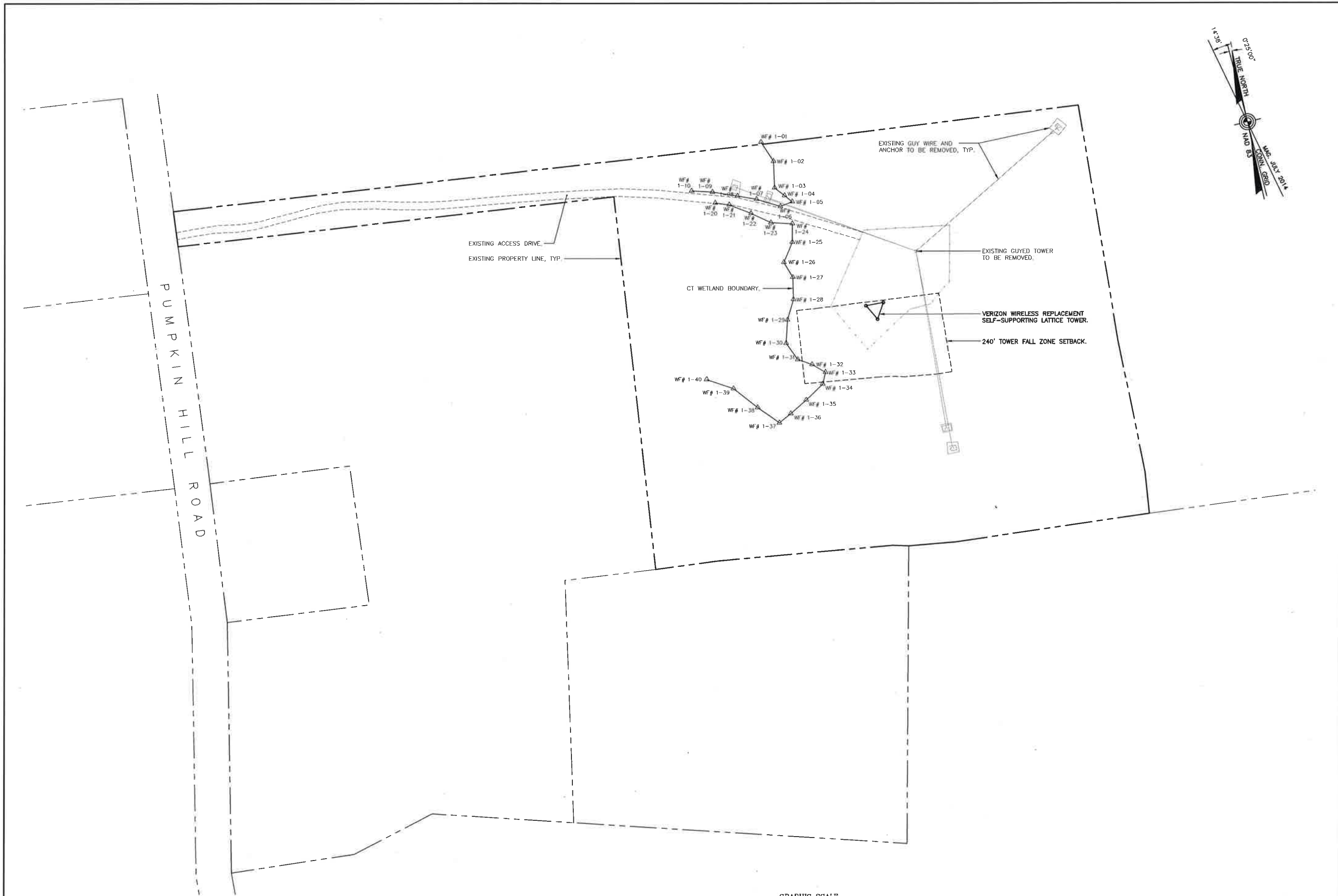
SLAB ON GRADE CONSTRUCTION

- PLACE AND COMPACT GRAVEL FILL IN LAYERS NOT TO EXCEED 10" BEFORE COMPACTION. DETERMINE MAXIMUM DRY DENSITY IN ACCORDANCE WITH ASTM D1557 AND MAKE ONE (1) FIELD DENSITY TEST IN ACCORDANCE WITH ASTM D2167 FOR EACH 50 CUBIC YARDS OF COMPACTED FILL, BUT NOT LESS THAN ONE (1) PER LAYER, TO ENSURE COMPACTION TO 95% OF MAXIMUM DRY DENSITY.
- SAW CUT CONTROL JOINTS 1/8" WIDE AND TO A DEPTH EQUAL TO 1/4 OF THE SLAB THICKNESS. CONSTRUCTION JOINTS AS REQUIRED SHALL BE KEYPED AND LOCATED AT CONTROL JOINT INTERVALS. ALL CONTROL JOINTS SHALL BE FILLED WITH EUCO EPOXY #600 EPOXY JOINT FILLER AS MANUFACTURED BY EUCO CHEMICAL CO. OR APPROVED EQUAL.
- SAW CUT CONTROL JOINTS AT 20'-0" ON CENTER MAXIMUM WITHIN 12 HOURS OF CONCRETE PLACEMENT.
- SLABS ON GRADE FINISHES: STEEL TROWEL FINISH AS DEFINED IN ACI 301. CURE SLAB WITH SONNEBORN KURE-N-SEAL WB OR APPROVED EQUAL, APPLIED AS RECOMMENDED BY MANUFACTURER.
- CONSTRUCTION JOINT SPACING IN FOUNDATION WALLS SHALL NOT EXCEED 40 FEET NOR 20 FEET FROM ANY CORNER. JOINTS SHALL BE KEYPED AND HORIZONTAL BARS SHALL EXTEND THRU JOINT AND BE 48 BAR DIAMETER SPLICED.
- IN REINFORCED CONCRETE WALLS AND FOOTINGS, PROVIDE CORNER DOWELS OF THE SAME SIZE AND AT THE SAME SPACING AS HORIZONTAL REINFORCING. DOWELS SHALL HAVE A 48 BAR DIAMETER SPLICE WITH HORIZONTAL REINFORCING EACH DIRECTION.
- WHERE FOOTINGS ARE IN CLOSE PROXIMITY TO SUBSURFACE PIPING, TOP OF FOOTING SHALL BE LOWERED TO PROVIDE A MINIMUM OF 8" BELOW INVERT ELEVATION OF PIPING.
- CONCRETE PIERS (IF PROVIDED): PLACE CONCRETE PIERS AND WALLS TOGETHER, SET PIER STEEL AND EXTEND WALL STEEL THROUGH PIER VERTICAL BARS. PROVIDE DOWELS WITH STANDARD HOOK FROM FOOTINGS AT ALL PIERS. SIZE AND QUANTITY OF DOWELS TO MATCH VERTICAL PIER REINFORCING.
- PROVIDE CORROSION RESISTANT ACCESSORIES IN ALL EXPOSED CONCRETE.
- RUB ALL EXPOSED CONCRETE SURFACES SMOOTH AND FINISH WITH CEMENT GROUT.
- PROVIDE AIR ENTRAINMENT IN ALL EXTERIOR CONCRETE AS WELL AS GARAGE AND PORCH SLABS THAT WILL BE EXPOSED TO DEICING SALTS.

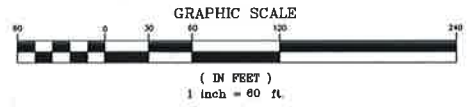
STRUCTURAL LUMBER CONSTRUCTION

- STRUCTURAL LUMBER USED FOR JOISTS, RAFTERS AND COLUMNS SHALL BE NO. 2 GRADE DOUGLAS FIR AND SHALL HAVE NOT LESS THAN THE FOLLOWING ALLOWABLE UNIT STRESSES, BEFORE ADJUSTMENT FOR DURATION FACTORS, BASED ON 1997 NDS SPECIFICATION:
EXTREME FIBER IN BENDING Fb 875 PSI
HORIZONTAL SHEAR Fv 95 PSI
TENSION PARALLEL TO GRAIN Ft = 575 PSI
COMPRESSION PERPENDICULAR TO GRAIN Fc 525 PSI
COMPRESSION PARALLEL TO GRAIN Fc = 1,350 PSI
MODULUS OF ELASTICITY E = 1,600,000 PSI
- LIGHT FRAMING LUMBER USED FOR STUDS, PARTITIONS, AND MISCELLANEOUS FRAMING SHALL NOT BE LESS THAN STANDARD GRADE AND SHALL HAVE THE FOLLOWING MINIMUM ALLOWABLE UNIT STRESSES:
EXTREME FIBER IN BENDING Fb 675 PSI
TENSION PARALLEL TO GRAIN Ft = 450 PSI
COMPRESSION PARALLEL TO GRAIN Fc 850 PSI
MODULUS OF ELASTICITY E = 1,400,000 PSI
- MOISTURE CONTENT OF ALL FRAMING LUMBER WHEN DELIVERED TO THE PROJECT SITE SHALL NOT EXCEED 19%.
- EXCEPT WHERE STRICTER PROVISIONS ARE INDICATED, 2003 INTERNATIONAL RESIDENTIAL CODE SHALL GOVERN ALL WOOD CONSTRUCTION INCLUDING, BUT NOT LIMITED TO: MATERIALS, FASTENERS (TYPE, SIZE, SPACING, EMBEDMENT), SHOP AND FIELD FABRICATION, CONNECTIONS, AND INSTALLATION.
- NOT USED
- NAIL PENETRATION INTO WALL STUDS AND CORNER POSTS SHALL BE AT LEAST 1 3/4 INCHES.
- PROVIDE AND INSTALL TIMBER POSTS (6x6 OR BUILT UP 2x6 MEMBERS) AT ALL EXTERIOR CORNERS AND ANCHOR TO FOUNDATION WALLS, AND BETWEEN EACH FRAMING LEVEL TO RESIST UPLIFT FORCES. PROVIDE AND INSTALL SIMPSON HDU5-SDS2.5 (HOLD DOWN) ANCHORS WITH SSTB24 ANCHOR RODS OR EQUIVALENT SHALL BE ATTACHED TO FLOOR JOISTS AND INSTALL HDU2-SDS2.5 ANCHORS WITH SSTB16 ANCHOR RODS AND POSTS EACH SIDE OF DOOR OPENINGS GREATER THAN 4'-0" IN EXTERIOR WALLS.
- HORIZONTAL (SLOPED) DIAPHRAGMS: THE FLOOR AND ROOF ARE DESIGNED AS DIAPHRAGMS TO RESIST LATERAL LOADS. FLOOR SHEATHING SHALL BE 3/4" INCH THICK APA RATED STURDI-FLOOR TONGUE AND GROOVE PLYWOOD. FLOOR SHEATHING SHALL BE ATTACHED TO FLOOR JOISTS WITH CONSTRUCTION ADHESIVE AND 8D NAILS. ROOF SHEATHING SHALL BE 5/8" INCH THICK CDX PLYWOOD. ROOF SHEATHING SHALL BE ATTACHED TO RAFTERS WITH 8D NAILS.
MAXIMUM NAIL SPACING OF FLOOR AND ROOF SHEATHING SHALL BE 6" O.C. ALONG ALL EDGES. ALL EDGES SHALL BE SUPPORTED WITH SOLID BLOCKING. FIELD NAILING SHALL BE 12" O.C. NAIL PENETRATION INTO SUPPORTING MEMBER SHALL BE AT LEAST 1-1/2 INCHES.
- ALL DOUBLE TOP PLATES, RIM JOISTS, AND HEADERS IN EXTERIOR WALLS ARE USED AS DIAPHRAGM CHORD MEMBERS. SPLICES IN DOUBLE TOP PLATES SHALL BE STAGGERED AND METAL STRAPS PROVIDED TO CONNECT RIM JOISTS WITH HEADER AND LINTEL BEAMS.
- FRAMING ANCHORS AND RELATED CONNECTION HARDWARE SHALL BE FABRICATED BY SIMPSON STRONG-TIE COMPANY, INC., OR EQUAL. SUCH PRODUCTS SHALL BE PROPERLY INSTALLED WITH THE TYPE AND NUMBER OF FASTENERS SPECIFIED BY THE MANUFACTURER FOR THE INTENDED USE.
JOIST AND BEAM HANGERS AND OTHER FRAMING ANCHORS SHALL BE SIZED FOR REACTIONS SHOWN ON THE DRAWINGS UNLESS A SPECIFIC HANGER OR FRAMING ANCHOR IS INDICATED. SUBMIT SHOP DRAWINGS INDICATING PROPOSED HANGER SIZE AND TYPE.
CONNECTION HARDWARE AND FASTENERS SHALL BE GALVANIZED OR STAINLESS STEEL. FRAMING ANCHORS AND FASTENERS THAT ARE NOT EXPOSED TO THE WEATHER SHALL BE G80 GALVANIZED. FRAMING ANCHORS AND FASTENERS THAT ARE EXPOSED TO THE WEATHER SHALL BE STAINLESS STEEL.
- ALL STRUCTURAL WOOD MEMBERS SHALL BE PROPERLY FIELD FABRICATED TO REQUIRED LENGTHS AND SPACING. PROVIDE SUITABLE CONNECTIONS, BEARING LENGTHS, STIFFENERS, BRIDGING, HEADERS, AND OTHER SPECIAL FRAMING AS INDICATED OR REQUIRED BY BUILDING CODE FOR COMPLETE INSTALLATION. ADDITIONAL JOISTS ARE REQUIRED AT FRAMED OPENINGS, AT CONCENTRATED LOADS, AND DIRECTLY BELOW PARTITIONS THAT ARE PARALLEL WITH JOISTS.
- ALL FRAMING (ROOF, FLOORS, WALLS) SHALL BE PROPERLY ANCHORED TO EACH OTHER AND TO CONCRETE FOUNDATIONS AGAINST UPLIFT BY ADEQUATELY SPLICED AND NAILED ROOF AND WALL SHEATHING, BY METAL STRAPS, HURRICANE ANCHORS, OR SIMILAR CONNECTION HARDWARE.
- PROVIDE HEAVY HEX NUTS AND WASHERS AT ALL ANCHOR BOLTS AND AT WOOD FRAME CONNECTIONS TO AVOID CRUSHING WOOD FIBERS.
- PRESSURE TREATED LUMBER SHALL BE USED FOR FOUNDATION SILLS AND FOR ALL LUMBER EXPOSED TO THE WEATHER AND IN DIRECT CONTACT WITH CONCRETE OR MASONRY FOUNDATIONS.
- PROVIDE SOLID BLOCKING BETWEEN ADJACENT FLOOR JOISTS AND ROOF RAFTERS, AT ALL SUPPORTS AND TOP FLANGE HANGERS, TO PREVENT MEMBER ROTATION. ALLOW SUFFICIENT CLEARANCE FOR CROSS VENTILATION AT ROOF.
- PROVIDE SOLID BLOCKING AND/OR MINIMUM 1"x3" DIAGONAL BRIDGING AT 7 FEET ON CENTER MAXIMUM AT ALL WOOD FRAMING. IF SOLID BLOCKING IS USED, IT SHALL EXTEND THE FULL DEPTH OF THE MEMBER IT IS LATERALLY SUPPORTING, UNLESS OTHERWISE NOTED.
- EXTERIOR WALLS AND INTERIOR LOAD-BEARING WALLS SHALL BE FRAMED WITH 2x6 STUDS SPACED AT 16 INCHES ON CENTER AND SHALL HAVE DOUBLE TOP PLATES. INTERIOR NON-LOAD-BEARING PARTITIONS SHALL BE FRAMED WITH 2x4 STUDS SPACED AT 16 INCHES ON CENTER. UNLESS OTHERWISE INDICATED, BEARING WALLS AND PARTITIONS THAT ARE PARALLEL WITH FLOOR JOISTS SHALL BE FULLY SUPPORTED BY DOUBLE JOISTS. INSTALL SOLID FULL-DEPTH BLOCKING BETWEEN JOISTS DIRECTLY BELOW BEARING WALLS AND PARTITIONS THAT ARE PERPENDICULAR WITH FLOOR JOISTS.

| | | | | | | | |
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| | | | | | | | |
| DATE: 05/11/15 | SCALE: AS NOTED | JOB NO. 14124.000 | SITE AND FOUNDATION SPECIFICATIONS | | | | |
| <div style="display: flex; justify-content: space-between; align-items: center;"> <div style="text-align: center;"> <p>Verizon Wireless WIRELESS COMMUNICATIONS FACILITY</p> </div> <div style="text-align: center;"> <p>ASHFORD RELO., CT 355 PUMPKIN HILL ROAD ASHFORD, CT 06278</p> </div> </div> | | | | | | | |
| <div style="display: flex; justify-content: space-between; align-items: center;"> <div style="text-align: center;"> <p>CENTEK Engineering General Contractor</p> <p>(203) 486-0360 (203) 486-8597 Fax 852 North Main Street Branford, CT 06406</p> <p>www.CentekEng.com</p> </div> <div style="text-align: center;"> <p>Calico Partnership d.b.a. Verizon Wireless</p> </div> </div> | | | | | | | |
| <p style="font-size: 2em; font-weight: bold;">N-1</p> <p>Sheet No. 2 of 24</p> | | | | | | | |



1 SITE LOCATION PLAN
 C-1.0 SCALE: 1" = 60'



| REV. | DATE | HR | DRWN BY | ISSUED FOR CONSTRUCTION | DESCRIPTION |
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| 0 | 07/09/15 | | | | |



Calico Partnership
 d.b.a. Verizon Wireless

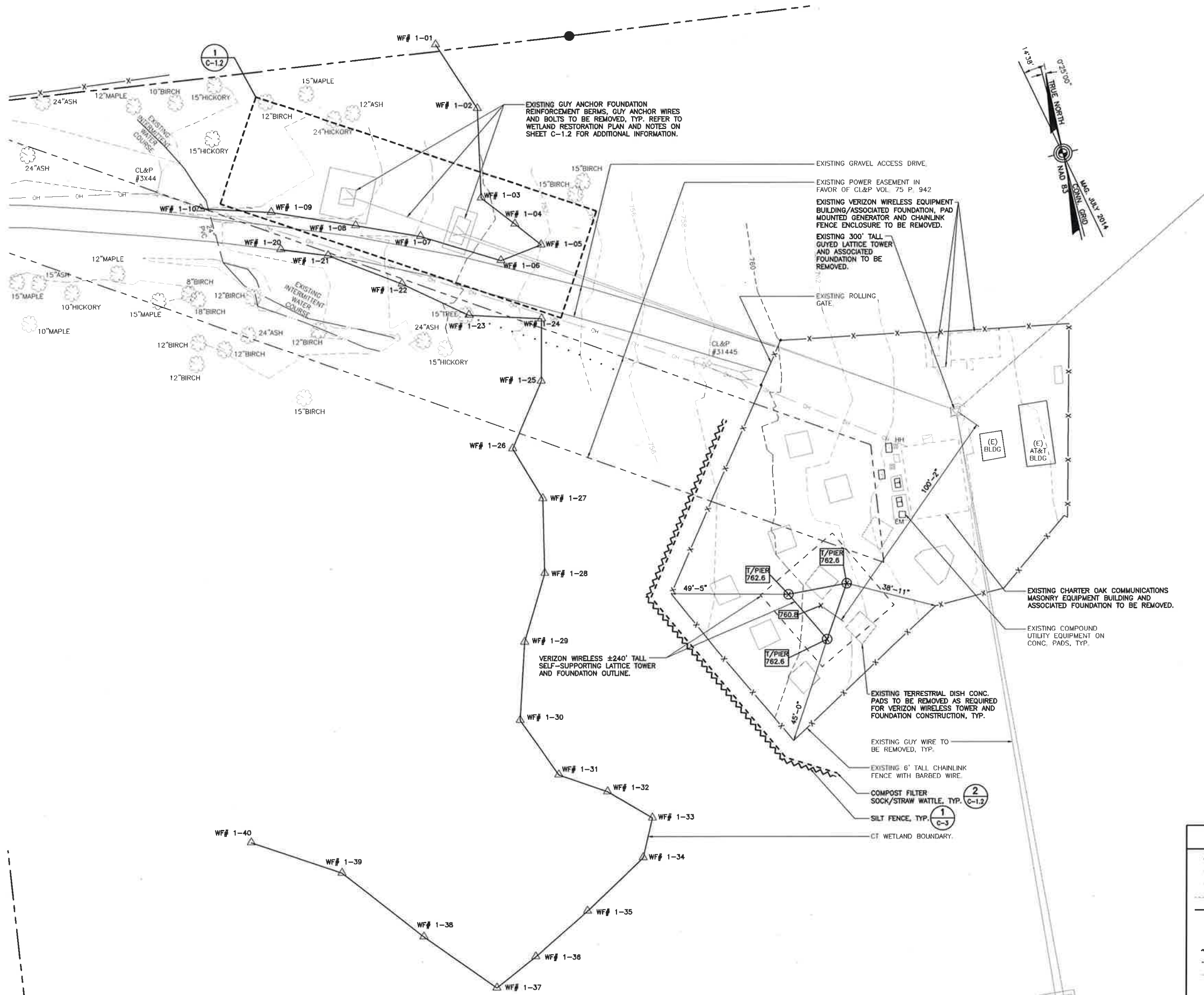
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 630 Ashford Road
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ASHFORD RELO., CT
 353 PUMPKIN HILL ROAD
 ASHFORD, CT 06278

DATE: 05/11/15
 SCALE: AS NOTED
 JOB NO. 14124.000

SITE LOCATION PLAN

C-1.0
 Sheet No. 3 of 24



SYMBOLS LEGEND

| | |
|---------|----------------------------------|
| --- | EXISTING PROPERTY LINE |
| - - - - | EXISTING EASEMENT |
| --- | EXISTING ACCESS DRIVE |
| | CONTOUR LINE |
| --- | GRADING LINE |
| ○ | UTILITY POLE |
| ○ | EXISTING DECIDUOUS TREE |
| ~~~~~ | SILTATION FENCE |
| --- | COMPOST FILTER SOCK/STRAW WATTLE |
| --- | EXISTING FENCE LINE |
| X | SPOT ELEVATION (PROPOSED) |

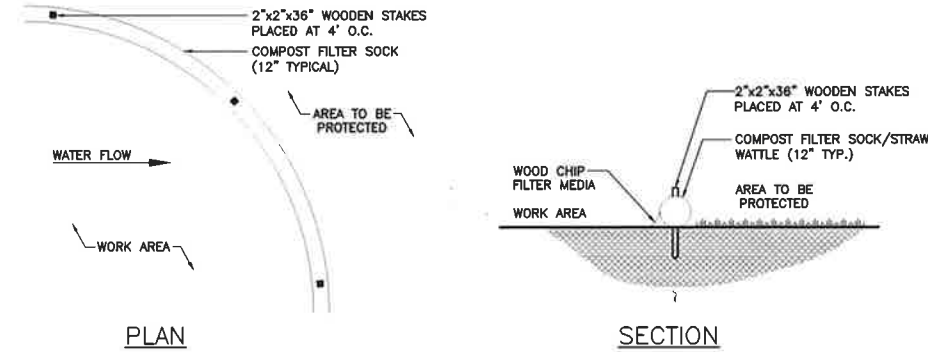
1 PARTIAL SITE PLAN
 (IN FEET)
 SCALE: 1"=20'
 GRAPHIC SCALE
 1 inch = 20 ft.

| | |
|--|---|
| PROFESSIONAL ENGINEER, SEAL | DATE: 05/11/15 |
| | SCALE: AS NOTED |
| Calico Partnership d.b.a. Verizon Wireless | JOB NO. 14124.000 |
| CENTEK engineering Centek on Solutions 2031 488-0580 Fax: 2031 488-1587 2031 488-1587 Branford, CT 06405 www.CentekEng.com | Verizon Wireless WIRELESS COMMUNICATIONS FACILITY ASHFORD RELO., CT 353 PUMPKIN HILL ROAD ASHFORD, CT 06278 |
| REG. 0 REV. 07/09/15 DATE DRAWN BY CHYD BT HMR ISSUED FOR CONSTRUCTION DESCRIPTION | C-1.1 Sheet No. 4 of 24 |

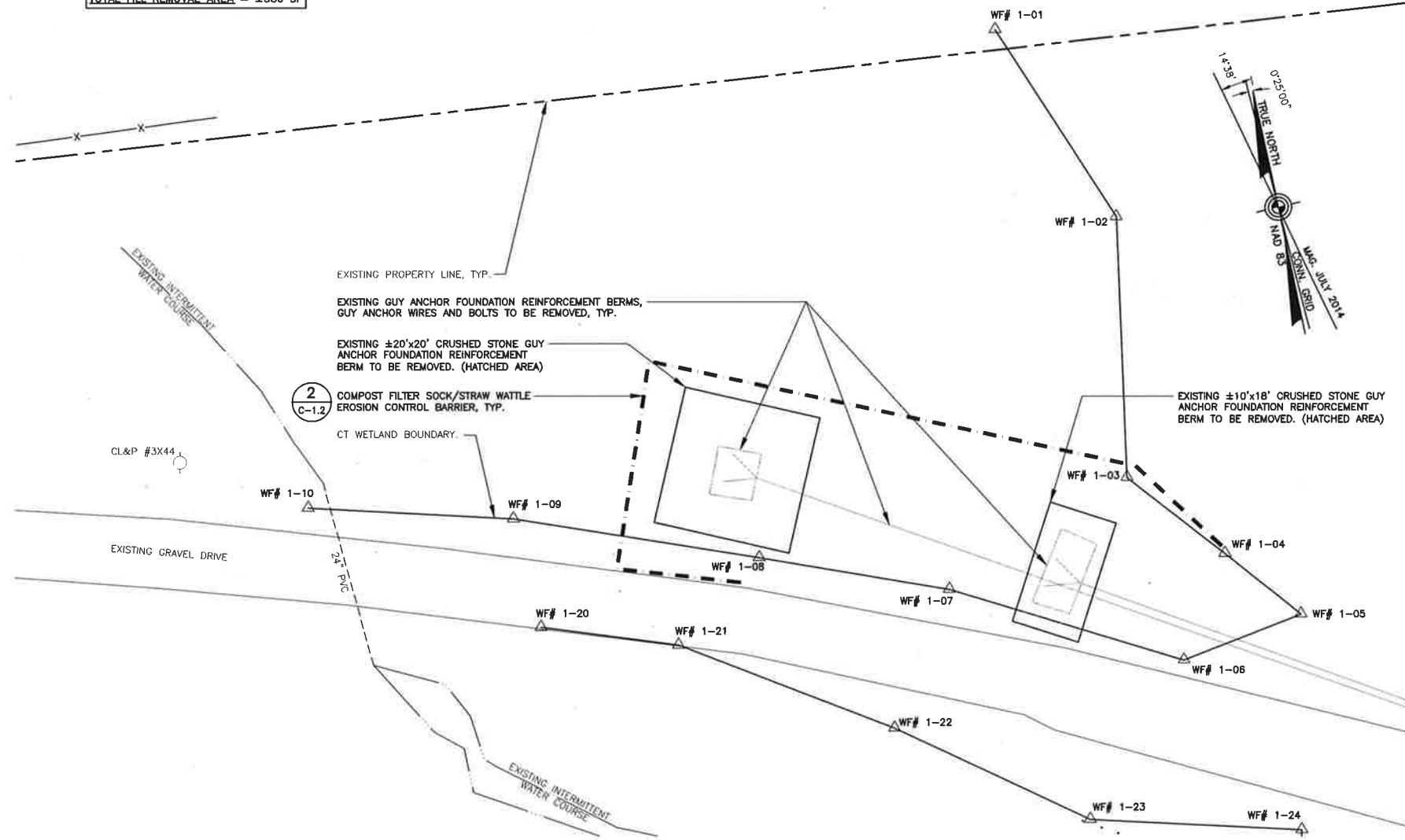
| WETLAND RESTORATION PLANTING SCHEDULE | | | | |
|---------------------------------------|---------------------|--------------------|-------|----------|
| QUANTITY | SCIENTIFIC NAME | COMMON NAME | SIZE | SPACING |
| TREES | | | | |
| 5 | ACER RUBRUM | RED MAPLE | 4'-6" | 10' O.C. |
| SHRUBS | | | | |
| 5 | CORNUS AMOMUM | SILKY DOGWOOD | 3'-4" | 5' O.C. |
| 5 | VIBURNUM DENTATUM | NORTHERN ARROWWOOD | 3'-4" | 5' O.C. |
| 5 | SALIX DISCOLOR | PUSSYWILLOW | 3'-4" | 5' O.C. |
| 5 | SAMBUCUS CANADENSIS | COMMON ELDERBERRY | 3'-4" | 5' O.C. |

- NOTES:**
- WETLAND RESTORATION AREA WILL BE SOWN WITH A NATIVE NEW ENGLAND WETLAND SEED MIX (NEW ENGLAND WETLAND PLANTS, INC., OR EQUIVALENT). THIS SEED MIX PROVIDES A PERMANENT COVER OF GRASSES, FORBS AND WILDFLOWERS TO PROVIDE BOTH GOOD EROSION CONTROL AND WILDLIFE HABITAT VALUE.
 - PLANTINGS TO BE PLACED IN HATCHED AREAS SHOWN BELOW FOLLOWING REMOVAL OF EXISTING GUY ANCHOR FOUNDATION REINFORCEMENT BERMS, GUY ANCHOR WIRES AND BOLTS.

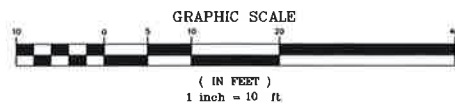
TOTAL FILL REMOVAL AREA = ±580 SF



2 TYP. COMPOST FILTER SOCK/ STRAW WATTLE DETAIL
C-1.2 NOT TO SCALE



1 WETLAND RESTORATION PLAN
C-1.2 SCALE: 1"=10'



WETLAND RESTORATION AREA NOTES

- THE WETLAND RESTORATION AREA WILL RESTORE 580± SQUARE FEET OF PREVIOUSLY FILLED WETLAND WITH REMOVAL OF TWO CRUSHED STONE GUY ANCHOR FOUNDATION REINFORCEMENT BERMS FROM BOTH THE INNER AND OUTER GUY ANCHORS FROM GUY ANCHOR BLOCK A. WETLAND RESTORATION WORK WILL BE PERFORMED DURING DEMOLITION OF THE EXISTING 300-FOOT GUYED LATTICE TOWER. THIS WETLAND AREA WILL BE RESTORED PER THE FOLLOWING:
- AN APT WETLAND SCIENTIST WILL OBSERVE ALL PHASES OF THE WETLAND RESTORATION PROJECT INCLUDING REMOVAL OF FILL MATERIAL, EXPOSURE OF UNDERLYING NATIVE WETLAND TOPSOIL, GRADING AND PLANTING TO MONITOR AND OVERSEE IMPLEMENTATION OF THE WETLAND RESTORATION PLAN. THE CONTRACTOR WILL NOTIFY APT A MINIMUM OF SEVEN (7) BUSINESS DAYS PRIOR TO THE START OF WETLAND RESTORATION ACTIVITIES TO SCHEDULE A PRE-CONSTRUCTION MEETING ON SITE AND FOR ANY SUBSEQUENT PHASES OF THE WETLAND RESTORATION PLAN.
 - PRIOR TO ANY EARTHWORK, A STRAW WATTLE EROSION CONTROL BARRIER WILL BE INSTALLED ALONG THE NORTH, EAST AND WEST SIDES OF THE PROPOSED WETLAND RESTORATION AREA TO PROTECT NEARBY WETLANDS.
 - CONSTRUCTION OF THE WETLAND RESTORATION AREA WILL ONLY OCCUR FROM THE SOUTH SIDE (EXISTING GRAVEL ACCESS DRIVE) TO MINIMIZE DISTURBANCE TO ADJOINING WETLAND AREAS.
 - THE CONTRACTOR WILL USE SWAMP MATS/TIMBER MATS AS NECESSARY TO PROVIDE A STABLE WORK SURFACE DURING REMOVAL OF GRAVEL FILL MATERIAL THAT OVERLIES BURIED WETLAND TOPSOIL.
 - AS THE WETLAND RESTORATION AREA CONSISTS OF FILL MATERIAL OVERLYING ORIGINAL WETLAND SOILS, EXCAVATION WILL CONSIST OF REMOVAL OF FILL MATERIAL UNTIL THE UNDERLYING NATIVE WETLAND SOIL IS EXPOSED. MINOR MODIFICATIONS TO THIS GRADING PLAN MAY BE MADE IN THE FIELD BY THE WETLAND SCIENTIST IN RESPONSE TO ACTUAL SOIL CONDITIONS. THE SUPERVISING WETLAND SCIENTIST WILL INSPECT THE SUB-GRADE OF THE WETLAND RESTORATION AREA TO ENSURE THAT THE PROPER HYDROLOGY HAS BEEN ESTABLISHED.
 - IF ADDITIONAL WETLAND TOPSOIL IS NEEDED TO SUPPLEMENT THE UNDERLYING NATIVE WETLAND TOPSOIL, IT SHALL CONSIST OF PREPARED WEED-FREE TOPSOIL MADE UP OF A 1:1 MIXTURE (OR EQUAL VOLUMES) OF ORGANIC AND MINERAL MATERIALS THAT CONTAINS AT LEAST 12 PERCENT ORGANIC CARBON CONTENT BY WEIGHT. CLEAN COMPOSTED LEAF MOLD OR COMMERCIALY AVAILABLE COMPOST FREE OF WEEDS OR INVASIVE SPECIES IS THE PREFERRED AMENDMENT TO ACHIEVE THIS STANDARD, THOUGH OTHER MATERIALS MAY BE USED IF APPROVED BY THE WETLAND SCIENTIST.
 - GUY ANCHOR RODS WILL BE REMOVED BY EXCAVATING A MINIMUM OF ONE (1) FOOT BELOW GROUND SURFACE AROUND THE ANCHOR ROD AND CUTTING OFF THE ROD. GUY ANCHOR FOUNDATIONS WILL REMAIN IN PLACE.
 - THESE SOILS WILL THEN BE GRADED TO ACHIEVE A SLIGHT HUMMOCK/HOLLOW MICROTOPOGRAPHY, SIMILAR TO THAT OF A NATURAL WETLAND SUBSTRATE. THE CONTRACTOR SHALL ENSURE THAT PROPER SOIL COMPACTION LEVELS (LOOSE TO FRIABLE) ARE MAINTAINED AND APPROPRIATE CORRECTION MEASURES (E.G. ROTOTILLING) MAY BE NECESSARY.
 - WETLAND RESTORATION AREA PLANTINGS SHALL TAKE PLACE ONCE THE ABOVE LISTED TASKS HAVE BEEN COMPLETED. THE WETLAND RESTORATION AREA WILL BE PLANTED WITH NATIVE TREES, SHRUBS AND HERBACEOUS SPECIES AS NOTED IN THE PLANTING SCHEDULE AND UNDER SOWN WITH A NATIVE NEW ENGLAND WETLAND SEED MIX (NEW ENGLAND WETLAND PLANTS, INC., OR EQUIVALENT) AFTER THE GRADING IS COMPLETED AT THE MANUFACTURER'S RECOMMENDED SEEDING RATE. SOIL CONDITIONING ACTIVITIES, INCLUDING RAKING, WILL BE COMBINED WITH THE SEED APPLICATION PROCESS.
 - THE SUPERVISING WETLAND SCIENTIST SHALL INSPECT THE PLANTING STOCK SPECIMENS FOR HEALTH, PEST, AND SUITABLE FOR USE WITHIN THE WETLAND RESTORATION AREA. UNSUITABLE SPECIMENS WILL BE REJECTED AND REPLACED WITH SUITABLE SPECIMENS. ANY PLANTING SUBSTITUTIONS MUST BE APPROVED BY THE WETLAND SCIENTIST. ALL WOODY PLANT STOCK SHALL BE CONTAINER-GROWN OR BURLAP BALLED. PLANTING WITHIN THE WETLAND RESTORATION AREA WILL CONFORM TO THESE PLANS OR WILL BE COMPLETED IN ACCORDANCE WITH DIRECTIONS PROVIDED IN THE FIELD BY THE SUPERVISING WETLAND SCIENTIST. ONLY PLANT MATERIALS NATIVE AND INDIGENOUS TO CONNECTICUT SHALL BE USED. INVASIVE PLANT SPECIES WILL NOT BE USED IN THE WETLAND RESTORATION AREA.
 - ALL PLANT MATERIALS INSTALLED SHALL MEET OR EXCEED THE SPECIFICATIONS OF THE "AMERICAN STANDARDS FOR NURSERY STOCK" BY THE AMERICAN ASSOCIATION OF NURSERYMEN. ALL PLANT MATERIALS SHALL BE GUARANTEED BY THE CONTRACTOR FOR ONE YEAR FOLLOWING DATE OF PLANTING. NO CULTIVARS OF THE NATIVE PLANTS IDENTIFIED IN THE PLANTING SCHEDULE SHALL BE USED.
 - THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE CAREFUL INSTALLATION, MAINTENANCE (INCLUDING WATERING), AND ESTABLISHMENT OF THE PLANT MATERIAL IN THE WETLAND RESTORATION AREA. A MAINTENANCE SCHEDULE FOR IRRIGATION AND PRUNING (AS NECESSARY) WILL BE ESTABLISHED BY THE CONTRACTOR.
 - ALL PLANTINGS TO BE SPACED GENERALLY AS NOTED ON THE PLANTING SCHEDULE WITH ASSISTANCE FROM THE WETLAND SCIENTIST TO SIMULATE NATURAL GROWTH PATTERNS.
 - AN ISOLATED PATCH OF COMMON REED (PHRAGMITES AUSTRALIS), AN AGGRESSIVE INVASIVE PLANT SPECIES, IS LOCATED ADJACENT TO THE WETLAND RESTORATION AREA. THIS AREA WILL BE TREATED AS FOLLOWS: IN LATE JUNE, COMMON REED WILL BE CUT TO THE GROUND; IN SEPTEMBER, COMMON REED WILL BE TREATED WITH GLYPHOSATE HERBICIDE RODEO®, OR APPROVED EQUIVALENT, USING AN HERBICIDE DIPPED GLOVE SWIPING TECHNIQUE TO AVOID IMPACT TO NATIVE PLANTS.
 - HERBICIDE APPLICATION WILL ADHERE TO THE FOLLOWING: ALL FEDERAL, STATE AND LOCAL REGULATIONS REGARDING HERBICIDE USE, APPLICATOR PERMIT AND POSTING REQUIREMENTS SHALL BE FOLLOWED; ALL HERBICIDE APPLICATION SHALL BE PERFORMED BY A STATE LICENSED INDIVIDUAL; CERTIFICATIONS, LICENSES AND PERMITS SHALL BE PROVIDED TO THE SUPERVISING WETLAND SCIENTIST PRIOR TO THE START OF WORK; ALL HERBICIDES SHALL BE MIXED WITH A DYE APPROVED BY U.S. EPA FOR USE AS AN HERBICIDE ADJUVANTS, SUCH AS TURFMARK® DYE OR EQUIVALENT; ONLY NONIONIC SURFACTANTS SHALL BE ADDED TO THE SPECIFIED HERBICIDE.
 - FALLEN LOGS, BRANCHES, STUMPS AND OTHER NATURAL DEBRIS, EXCLUDING INVASIVE PLANTS, WILL BE RELOCATED TO THE ENHANCEMENT AREA TO PROVIDE BENEFICIAL HABITAT FEATURES FOR WILDLIFE. THIS WILL INCLUDE DOWNED AND UNCOVERED MATERIAL THAT IS ACQUIRED DURING GRADING ACTIVITIES AND WILL BE DISTRIBUTED TO COVER NO MORE THAN 5 PERCENT OF THE WETLAND RESTORATION AREA'S SURFACE. THE NATURAL DEBRIS SHOULD BE OF VARYING SIZES AND IN VARYING DEGREES OF DECOMPOSITION.
 - THE EROSION CONTROL BARRIERS WILL BE DISASSEMBLED AND PROPERLY DISPOSED OF NO LATER THAN 30 DAYS FOLLOWING PERMANENT STABILIZATION OF EXPOSED SOILS BY THE PLANTED MATERIALS. SEDIMENT COLLECTED BY THESE DEVICES WILL BE REMOVED AND DISPOSED OF IN A MANNER THAT PREVENTS EROSION AND TRANSPORT TO A WATERWAY OR WETLAND. IF MINOR GRADING IS REQUIRED IN THIS ZONE TO PROVIDE SURFACE HYDROLOGIC CONNECTION BETWEEN THE AREAS, IT WILL BE DONE BY HAND AND STABILIZED WITH MULCH.

POST-CONSTRUCTION MONITORING REQUIREMENTS

- IN ACCORDANCE WITH THE CONNECTICUT SITING COUNCIL'S PETITION NO. 1121 DECISION, ISSUED DECEMBER 29, 2014, THE WETLAND RESTORATION AREA SHALL BE MONITORED BY THE PROJECT WETLAND MONITOR DURING CONSTRUCTION AND FOR A PERIOD OF AT LEAST THREE AND UP TO FIVE GROWING SEASONS FOLLOWING CONSTRUCTION.
- THE PROJECT WETLAND MONITOR WITH EXPERIENCE IN WETLAND RESTORATION WILL PERFORM POST CONSTRUCTION MONITORING OF THE WETLAND RESTORATION AREA. DEAN GUSTAFSON, SENIOR WETLAND SCIENTIST AT ALL-POINTS TECHNOLOGY CORPORATION, P.C. (APT) WILL SERVE AS THE PROJECT WETLAND MONITOR FOR THIS PROJECT TO ENSURE COMPLIANCE WITH THE CONNECTICUT SITING COUNCIL'S DECISION FOR RESTORATION OF THE WETLAND AREA. MR. GUSTAFSON CAN BE REACHED BY PHONE AT (860) 663-1697 EXT. 201 OR VIA EMAIL AT DGUSTAFSON@ALLPOINTSTECH.COM.
- POST CONSTRUCTION INSPECTIONS OF THE WETLAND RESTORATION AREA WILL BE PERFORMED BY THE PROJECT WETLAND MONITOR TWICE EACH YEAR: LATE SPRING/EARLY SUMMER AND LATE SUMMER/EARLY FALL FOR A PERIOD OF AT LEAST THREE (3) YEARS AND UP TO FIVE (5) YEARS IF NECESSARY. THE WETLAND RESTORATION AREA WILL BE INSPECTED GENERALLY IN ACCORDANCE WITH THE CORPS' MITIGATION GUIDANCE TO ASSESS THE GENERAL HEALTH OF PLANTINGS, SOIL STABILIZATION AND PRESENCE OF INVASIVE PLANTS. INVASIVE PLANTS WILL INCLUDE SUCH SPECIES AS NOTED IN APPENDIX D OF THE CORPS' MITIGATION GUIDANCE WITH A PARTICULAR FOCUS ON COMMON REED (PHRAGMITES AUSTRALIS) WHICH CURRENTLY DOMINATES THE WETLAND RESTORATION AREA. SHOULD THE WETLAND RESTORATION AREA NOT SATISFY THE THREE SUCCESS STANDARDS IDENTIFIED BELOW AFTER THE THIRD YEAR, MONITORING SHALL CONTINUE TO A FOURTH, AND POSSIBLY A FIFTH, YEAR UNTIL SUCCESS STANDARDS HAVE BEEN ATTAINED.
- MONITORING REPORTS GENERALLY FOLLOWING THE CORPS' MITIGATION GUIDANCE FORMAT WILL BE SUBMITTED BY THE PROJECT WETLAND MONITOR TO THE CONNECTICUT SITING COUNCIL NO LATER THAN DECEMBER 15 OF EACH YEAR. THE REPORTS WILL PROVIDE DETAILS ON THE THREE SUCCESS STANDARDS DESCRIBED BELOW. IF THERE ARE PROBLEMS THAT NEED TO BE ADDRESSED AND IF THE MEASURES TO CORRECT THEM REQUIRE PRIOR APPROVAL FROM THE CONNECTICUT SITING COUNCIL, VERIZON WIRELESS WILL CONTACT THE COUNCIL AS SOON AS THE NEED FOR CORRECTIVE ACTION IS DISCOVERED.
- THE WETLAND RESTORATION AREA WILL BE ASSESSED USING THREE SUCCESS STANDARDS, DESCRIBED AS FOLLOWS:
 - AT LEAST 80% OF THE AERIAL SURFACE OF THE WETLAND RESTORATION AREA SHALL BE ESTABLISHED WITH NATIVE HYDROPHYTES
 - CONTROL OF NON-NATIVE SPECIES WITH LESS THAN 10% TOTAL AERIAL COVERAGE BY END OF MONITORING PERIOD
 - ALL SLOPES AND SOILS WITHIN AND ADJACENT TO THE EXTENDED DETENTION SHALLOW WETLAND BASINS ARE PERMANENTLY STABILIZED WITH VEGETATION AND ANY EROSION CONTROL BARRIERS REMOVED NO LATER THAN THE END OF THE THIRD GROWING SEASON.
- WETLAND RESTORATION AS SET FORTH HEREIN WILL NOT BE CONSIDERED FULFILLED UNTIL MITIGATION SUCCESS HAS BEEN DEMONSTRATED THROUGH ATTAINMENT OF THE THREE (3) SUCCESS STANDARDS AND WRITTEN VERIFICATION FROM THE CONNECTICUT SITING COUNCIL HAS BEEN RECEIVED.

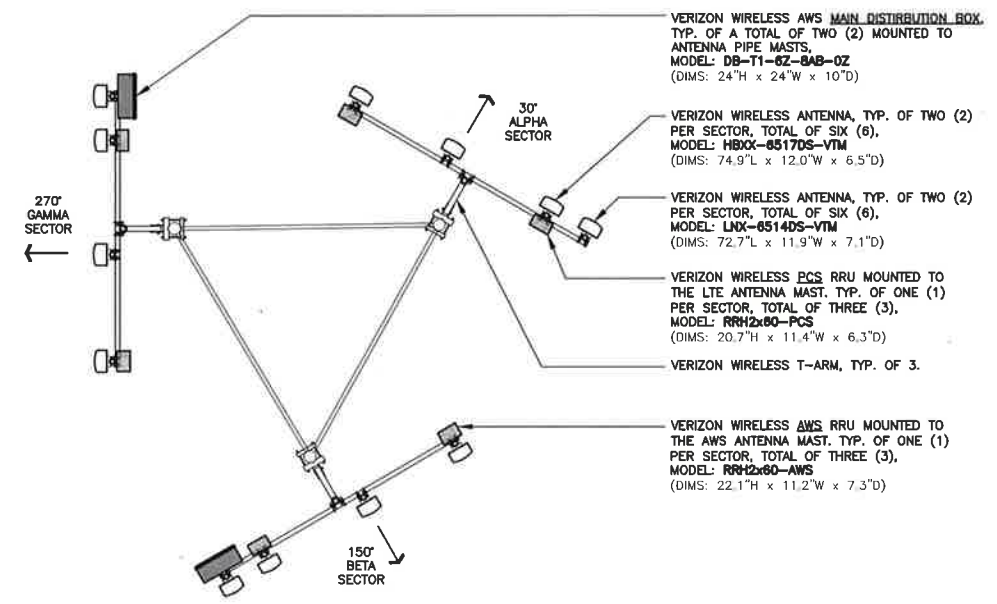
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| SCALE: | AS NOTED |
| JOB NO.: | 14124.000 |
| WETLAND RESTORATION PLAN, DETAILS AND NOTES | |
| C-1.2 | |
| Sheet No. 5 of 24 | |

Verizon Wireless
WIRELESS COMMUNICATIONS FACILITY
ASHFORD RELO, CT
353 PUMPKIN HILL ROAD
ASHFORD, CT 06278

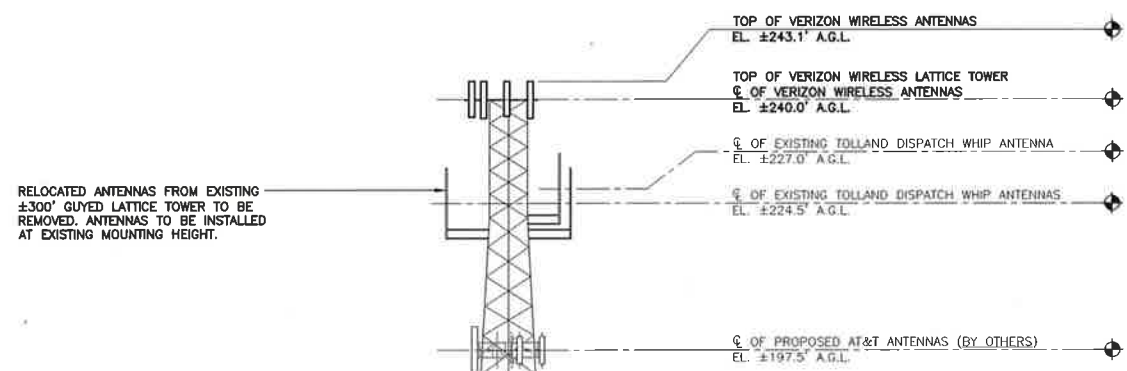
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CONNECTION STATE OF CONNECTICUT
No. 14124
DATE: 07/09/15
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ISSUED FOR CONSTRUCTION

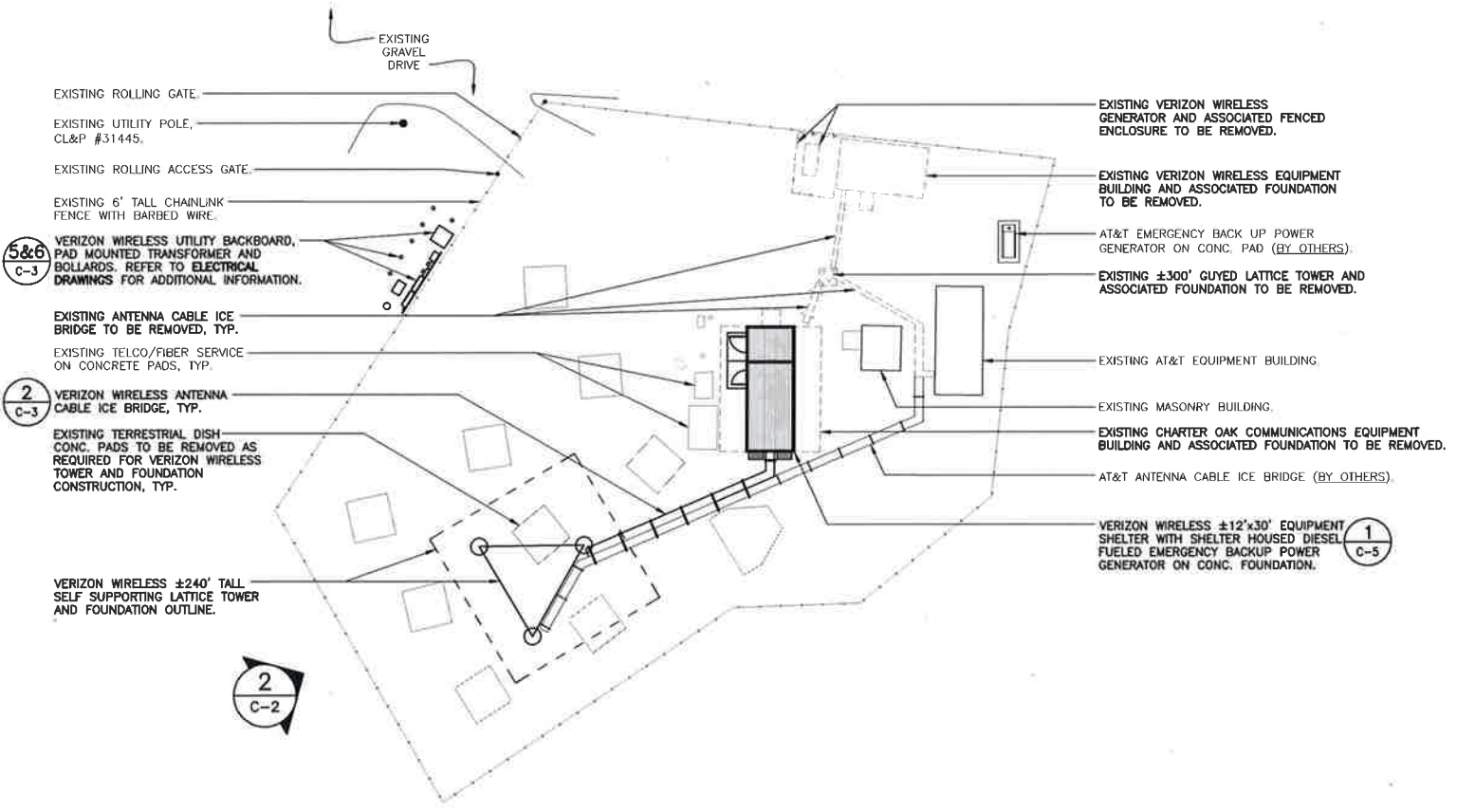


3
C-2 VERIZON WIRELESS ANTENNA MOUNTING CONFIGURATION
SCALE: 1/4" = 1'-0"

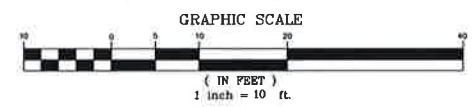


TOWER AND GEOTECH NOTES:

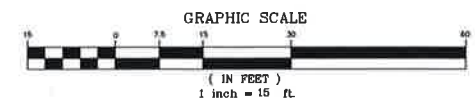
- 240' TALL SELF-SUPPORTING LATTICE TOWER STRUCTURE DESIGNED AND MANUFACTURED BY VALMONT STRUCTURES.
- REFER TO STRUCTURAL DESIGN ANALYSIS OF TOWER AND TOWER FOUNDATION AS PREPARED BY VALMONT STRUCTURES. DATED 06/02/15 (REV. 1) PROJECT NUMBER: 284859.
- REFER TO GEOTECHNICAL ENGINEERING REPORT AS PREPARED BY TERRACON CONSULTANTS, INC., DATED FEBRUARY 23, 2015. TERRACON JOB NO. J2155118.
- FAA OBSTRUCTION LIGHTING SYSTEM SHALL BE INSTALLED ON VERIZON WIRELESS SELF-SUPPORTING LATTICE TOWER. REFER TO ELECTRICAL DRAWINGS FOR ADDITIONAL INFORMATION.



1
C-2 COMPOUND PLAN
SCALE: 1" = 10'



2
C-2 SOUTHWEST TOWER ELEVATION-PROPOSED
SCALE: 1" = 15'



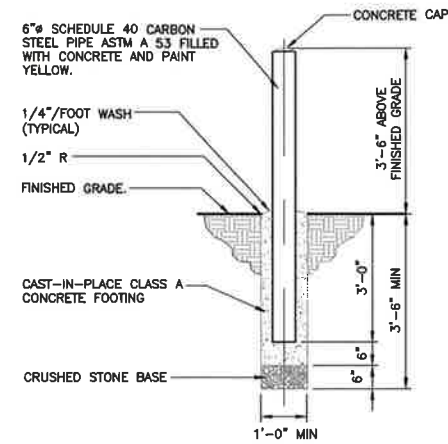
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| DATE: | 05/11/15 |
| SCALE: | AS NOTED |
| JOB NO. | 14124.000 |
| COMPOUND PLAN, ELEVATION AND ANTENNA MOUNTING CONFIGURATION | |
| C-2 | |
| Sheet No. 6 of 24 | |

VERIZON WIRELESS
WIRELESS COMMUNICATIONS FACILITY
ASHFORD RELO., CT
353 PUMPKIN HILL ROAD
ASHFORD, CT 06278

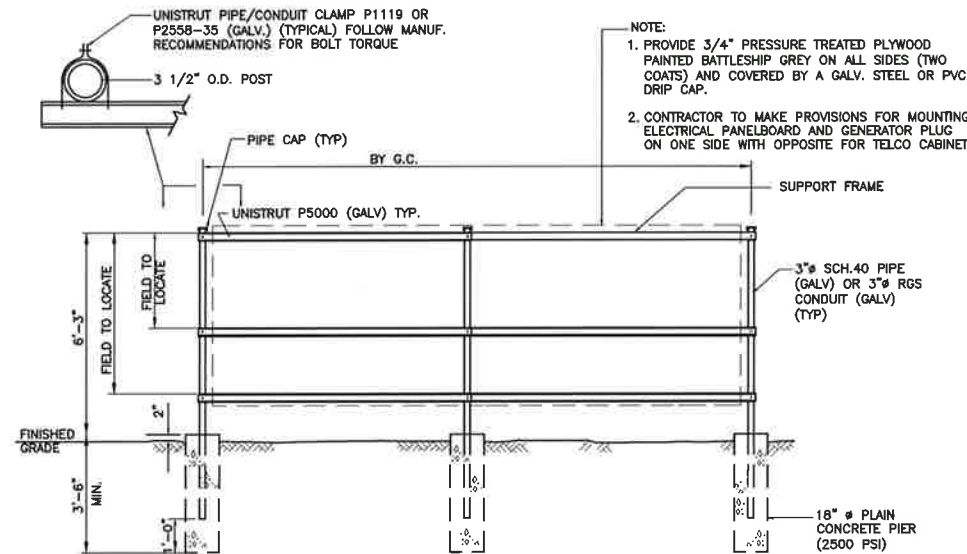
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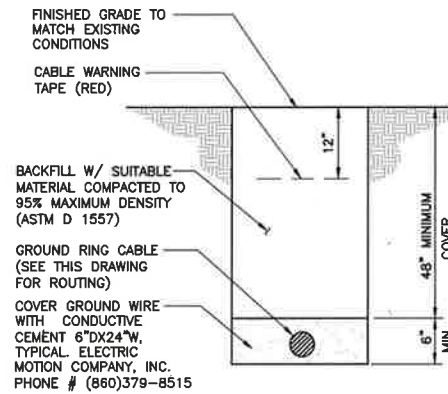
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203 486-0087 Fax
203 486-0087
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www.CentekEng.com



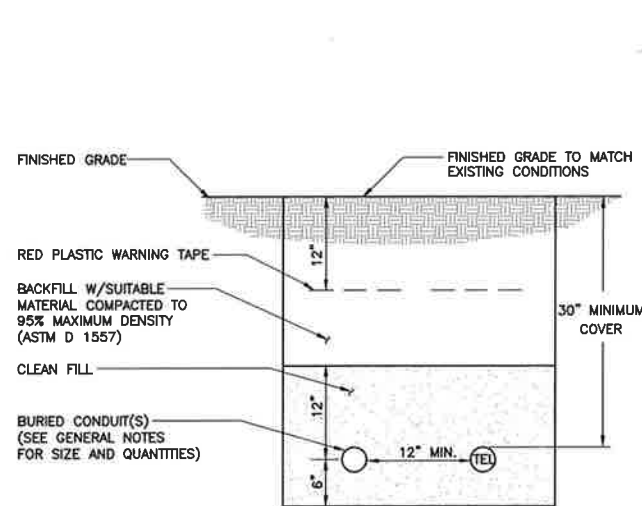
6 BOLLARD DETAIL
C-3 NOT TO SCALE



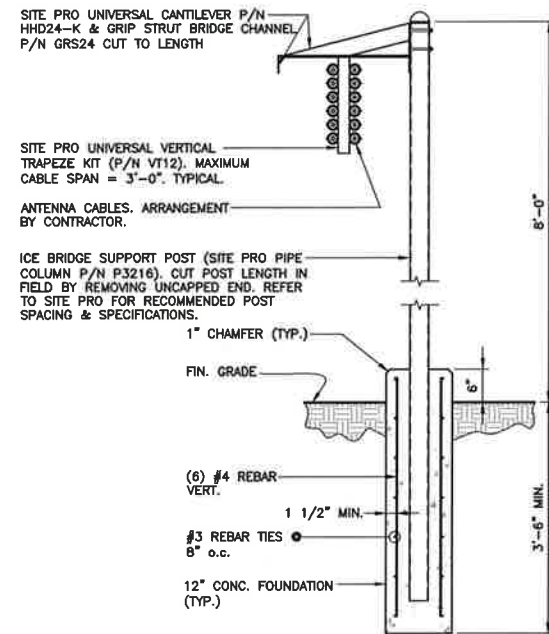
5 UTILITY SUPPORT FRAME (TYP)
C-3 NOT TO SCALE



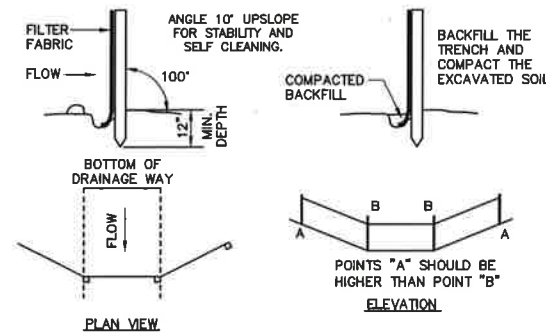
4 TYPICAL BURIAL GROUND CABLE DETAIL
C-3 NOT TO SCALE



3 TYPICAL ELECTRICAL/TEL TRENCH DETAIL
C-3 NOT TO SCALE



2 ICE BRIDGE DETAIL
C-3 NOT TO SCALE



1 PLACEMENT AND CONSTRUCTION OF SILTATION FENCE
C-3 NOT TO SCALE

GENERAL CONSTRUCTION / PRE-CONSTRUCTION NOTES

1. PRIOR TO COMMENCEMENT OF ANY CONSTRUCTION ACTIVITIES, A MANDATORY ON-SITE PRE-CONSTRUCTION MEETING SHALL BE CONDUCTED WITH THE VERIZON WIRELESS CONSTRUCTION MANAGER, CONTRACTOR'S CONSTRUCTION MANAGER, THE PROJECT EROSION AND SEDIMENTATION CONTROL/ENVIRONMENTAL MONITOR AND THE ENGINEER OF RECORD.

GENERAL CONSTRUCTION SEQUENCE

THIS IS A GENERAL CONSTRUCTION SEQUENCE OUTLINE SOME ITEMS OF WHICH MAY NOT APPLY TO PARTICULAR SITES.

- CUT AND STUMP AREAS OF PROPOSED CONSTRUCTION.
- INSTALL TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES AS REQUIRED.
- REMOVE AND STOCKPILE TOPSOIL. STOCKPILE SHALL BE SEED TO PREVENT EROSION.
- CONSTRUCT CLOSED DRAINAGE SYSTEM. PRECEPT CULVERT INLETS AND CATCH BASINS WITH SEDIMENTATION BARRIERS.
- CONSTRUCT ROADWAYS AND PERFORM SITE GRADING, PLACING HAY BALES AND SILTATION FENCES AS REQUIRED TO CONTROL SOIL EROSION.
- INSTALL UNDERGROUND UTILITIES.
- BEGIN TEMPORARY AND PERMANENT SEEDING AND MULCHING. ALL CUT AND FILL SLOPES SHALL BE SEED OR MULCHED IMMEDIATELY AFTER THEIR CONSTRUCTION. NO AREA SHALL BE LEFT UNSTABILIZED FOR A TIME PERIOD OF MORE THAN 30 DAYS.
- DAILY, OR AS REQUIRED, CONSTRUCT, INSPECT, AND IF NECESSARY, RECONSTRUCT TEMPORARY BERMS, DRAINS, DITCHES, SILT FENCES AND SEDIMENT TRAPS INCLUDING MULCHING AND SEEDING.
- BEGIN EXCAVATION FOR AND CONSTRUCTION OF TOWERS AND PLATFORMS.
- FINISH PAVING ALL ROADWAYS, DRIVES, AND PARKING AREAS.
- COMPLETE PERMANENT SEEDING AND LANDSCAPING.
- NO FLOW SHALL BE DIVERTED TO ANY WETLANDS UNTIL A HEALTHY STAND OF GRASS HAS BEEN ESTABLISHED IN REGARDED AREAS.
- AFTER GRASS HAS BEEN FULLY GERMINATED IN ALL SEEDER AREAS, REMOVE ALL TEMPORARY EROSION CONTROL MEASURES.

SOIL EROSION AND SEDIMENT CONTROL SEQUENCE

- ALL SOIL EROSION AND SEDIMENT CONTROL MEASURES, SUCH AS CONSTRUCTION ENTRANCE / ANTI TRACKING PAD, SILTATION FENCE, AND SILTATION FENCE / HAY BALE SHALL BE IN PLACE PRIOR TO ANY GRADING ACTIVITY. INSTALLATION OF PROPOSED STRUCTURES OR UTILITIES. MEASURES SHALL BE LEFT IN PLACE AND MAINTAINED UNTIL CONSTRUCTION IS COMPLETED AND/OR AREA IS STABILIZED.
- THE ENTRANCE TO THE PROJECT SITE IS TO BE PROTECTED BY STONE ANTI TRACKING PAD OF ASTM C-33, SIZE NO. 2 OR 3, OR D.O.T. 2" CRUSHED GRAVEL. THE STONE ANTI TRACKING PAD IS TO BE MAINTAINED AT ALL TIMES DURING THE CONSTRUCTION PERIOD.
- LAND DISTURBANCE WILL BE KEPT TO A MINIMUM AND RESTABILIZATIONS WILL BE SCHEDULED AS SOON AS PRACTICAL.
- ALL SOIL EROSION AND SEDIMENT CONTROL WORK SHALL BE DONE IN STRICT ACCORDANCE WITH THE CONNECTICUT GUIDELINES FOR EROSION AND SEDIMENT CONTROL INCLUDING THE LATEST DATE FROM THE COUNCIL ON SOIL AND WATER CONSERVATION.
- ANY ADDITIONAL EROSION/SEDIMENTATION CONTROL DEEMED NECESSARY BY TOWN STAFF DURING CONSTRUCTION, SHALL BE INSTALLED BY THE DEVELOPER. IN ADDITION, THE DEVELOPER SHALL BE RESPONSIBLE FOR THE REPAIR/REPLACEMENT/MAINTENANCE OF ALL EROSION CONTROL MEASURES UNTIL ALL DISTURBED AREAS ARE STABILIZED TO THE SATISFACTION OF THE TOWN STAFF.
- IN ALL AREAS, REMOVAL OF TREES, BUSHES AND OTHER VEGETATION AS WELL AS DISTURBANCE OF THE SOIL IS TO BE KEPT TO AN ABSOLUTE MINIMUM WHILE ALLOWING PROPER DEVELOPMENT OF THE SITE. DURING CONSTRUCTION, EXPOSE AS SMALL AN AREA OF SOIL AS POSSIBLE FOR AS SHORT A TIME AS POSSIBLE.
- SILTATION FENCE SHALL BE PLACED AS INDICATED BEFORE A CUT SLOPE HAS BEEN CREATED. SEDIMENT DEPOSITS SHOULD BE PERIODICALLY REMOVED FROM THE UPSTREAM SIDES OF SILTATION FENCE. THIS MATERIAL IS TO BE SPREAD AND STABILIZED IN AREAS NOT SUBJECT TO EROSION, OR TO BE USED IN AREAS WHICH ARE NOT TO BE PAVED OR BUILT ON. SILTATION FENCE IS TO BE REPLACED AS NECESSARY TO PROVIDE PROPER FILTERING ACTION. THE FENCE IS TO REMAIN IN PLACE AND BE MAINTAINED TO INSURE EFFICIENT SILTATION CONTROL UNTIL ALL AREAS ABOVE THE EROSION CHECKS ARE STABILIZED AND VEGETATION HAS BEEN ESTABLISHED.
- SWALE DISCHARGE AREA WILL BE PROTECTED WITH RIP RAP SPLASH PAD/ ENERGY DISSIPATER.
- ALL FILL AREAS SHALL BE COMPACTED SUFFICIENTLY FOR THEIR INTENDED PURPOSE AND AS REQUIRED TO REDUCE SLIPPING, EROSION OR EXCESS SATURATION.
- THE SOIL SHALL NOT BE PLACED WHILE IN A FROZEN OR MUDDY CONDITION, WHEN THE SUBGRADE IS EXCESSIVELY WET, OR IN A CONDITION THAT MAY OTHERWISE BE DETRIMENTAL TO PROPER GRADING OR PROPOSED SODDING OR SEEDING.
- AFTER CONSTRUCTION IS COMPLETE AND GROUND IS STABLE, REMOVE SILTS IN THE RIP RAP ENERGY DISSIPATERS. REMOVE OTHER EROSION AND SEDIMENT DEVICES.

CONSTRUCTION SPECIFICATIONS - SILT FENCE

- THE GEOTEXTILE FABRIC SHALL MEET THE DESIGN CRITERIA FOR SILT FENCES.
- THE FABRIC SHALL BE EMBEDDED A MINIMUM OF 8 INCHES INTO THE GROUND AND THE SOIL COMPACTED OVER THE EMBEDDED FABRIC.
- WOVEN WIRE FENCE SHALL BE FASTENED SECURELY TO THE FENCE POSTS WITH WIRE TIES OR STAPLES.
- FILTER CLOTH SHALL BE FASTENED SECURELY TO THE WOVEN WIRE FENCE WITH TIES SPACED EVERY 24 INCHES AT THE TOP, MID-SECTION AND BOTTOM.
- WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER, THEY SHALL BE OVERLAPPED BY 6 INCHES, FOLDED, AND STAPLED.
- FENCE POSTS SHALL BE A MINIMUM OF 36 INCHES LONG AND DRIVEN A MINIMUM OF 16 INCHES INTO THE GROUND. WOOD POSTS SHALL BE OF SOUND QUALITY HARDWOOD AND SHALL HAVE A MINIMUM CROSS SECTIONAL AREA OF 3.0 SQUARE INCHES.
- MAINTENANCE SHALL BE PERFORMED AS NEEDED TO PREVENT BUILD UP IN THE SILT FENCE DUE TO DEPOSITION OF SEDIMENT.

MAINTENANCE - SILT FENCE

- SILT FENCES SHALL BE INSPECTED IMMEDIATELY AFTER EACH RAINFALL AND AT LEAST DAILY DURING PROLONGED RAINFALL. ANY REPAIRS THAT ARE REQUIRED SHALL BE MADE IMMEDIATELY.
- IF THE FABRIC ON A SILT FENCE SHOULD DECOMPOSE OR BECOME INEFFECTIVE DURING THE EXPECTED LIFE OF THE FENCE, THE FABRIC SHALL BE REPLACED PROMPTLY.
- SEDIMENT SHOULD BE INSPECTED AFTER EVERY STORM EVENT. THE DEPOSITS SHOULD BE REMOVED WHEN THEY REACHED APPROXIMATELY ONE-HALF THE HEIGHT OF THE BARRIER.
- SEDIMENT DEPOSITS THAT ARE REMOVED OR LEFT IN PLACE AFTER THE FABRIC HAS BEEN REMOVED SHALL BE GRADED TO CONFORM WITH THE EXISTING TOPOGRAPHY AND VEGETATED.

PROFESSIONAL ENGINEER SEAL

DATE: 05/11/15
SCALE: AS NOTED
JOB NO. 14124.000

Verizon Wireless
WIRELESS COMMUNICATIONS FACILITY

ASHFORD RELO, CT
353 PUMPKIN HILL ROAD
ASHFORD, CT 06278

SITE CONSTRUCTION, S&E CONTROL NOTES & DETAILS

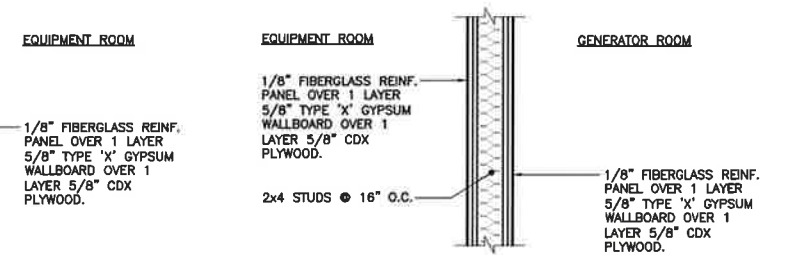
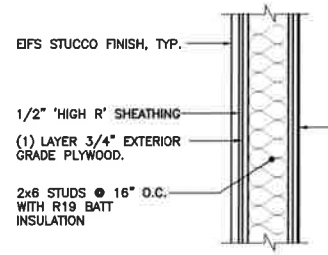
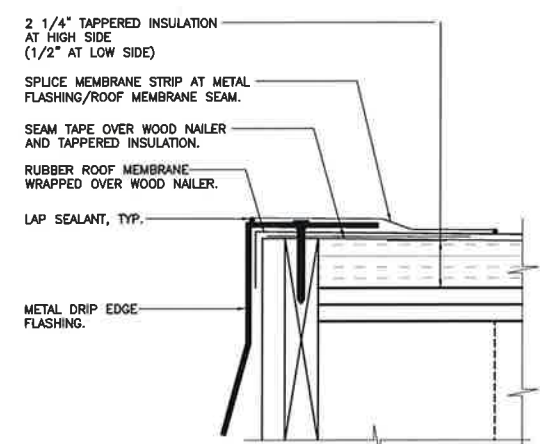
C-3
Sheet No. 7 of 24

- BUILDING FRAMING MATERIALS:**
- SILLS, BUCKS, BLOCKING, CURBING AT ROOF PENETRATIONS AND NAILERS FOR USE IN CONJUNCTION WITH WOOD CONSTRUCTION AND WHERE EXPOSED TO DAMPNESS: ANY SPECIES OF STRUCTURAL LUMBER, CONSTRUCTION GRADE, PRESSURE TREATED, MEETING THE REQUIREMENTS OF FEDERAL SPECIFICATION TT-W-571.
 - HEADERS, BEAMS, POSTS, AND OTHER STRUCTURAL SUPPORT MEMBERS: DOUGLAS FIR-LARCH NO. 2 GRADE OR BETTER (MIN Fb=1200 PSI).
 - STUDS, PLATES, AND OTHER LIGHT FRAMING IF USED: HEM-FIR NO. 2 GRADE OR BETTER (MIN. Fb= 1100 PSI).
 - BLOCKING, NAILERS, AND OTHER NON-STRUCTURAL USES: ANY SPECIES OF STRUCTURAL LUMBER, CONSTRUCTION GRADE OR BETTER.
 - SHEATHING PLYWOOD: C-C EXT-APA GROUP 1 WITH EXTERIOR GLUE, NO THINNER THAN 5/8".
 - BUILDING AIR INFILTRATION WRAP: 15 LB. ASPHALT-SATURATED FELT, ASTM D226, OR TYVEK.

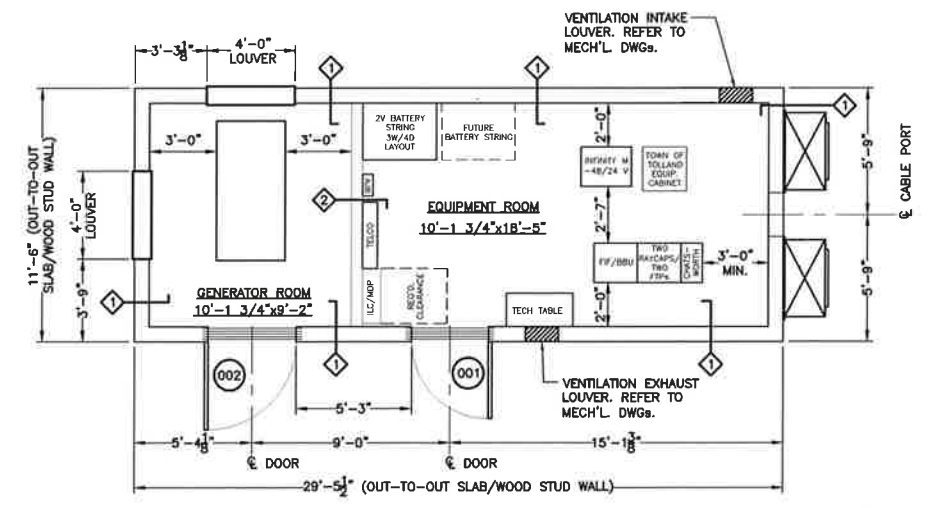
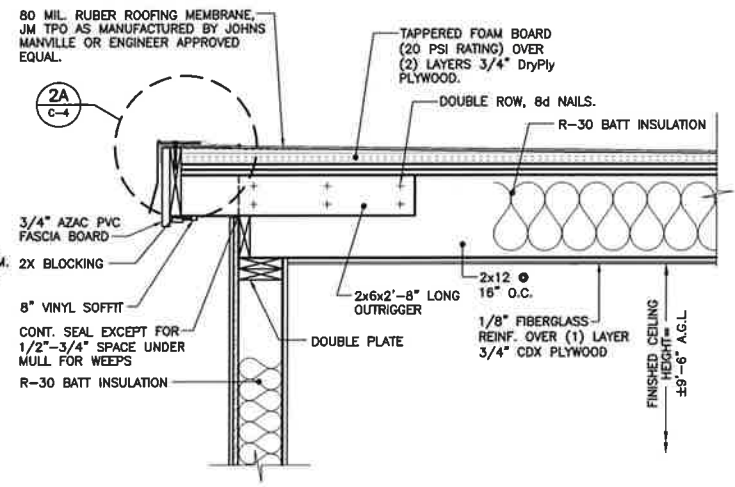
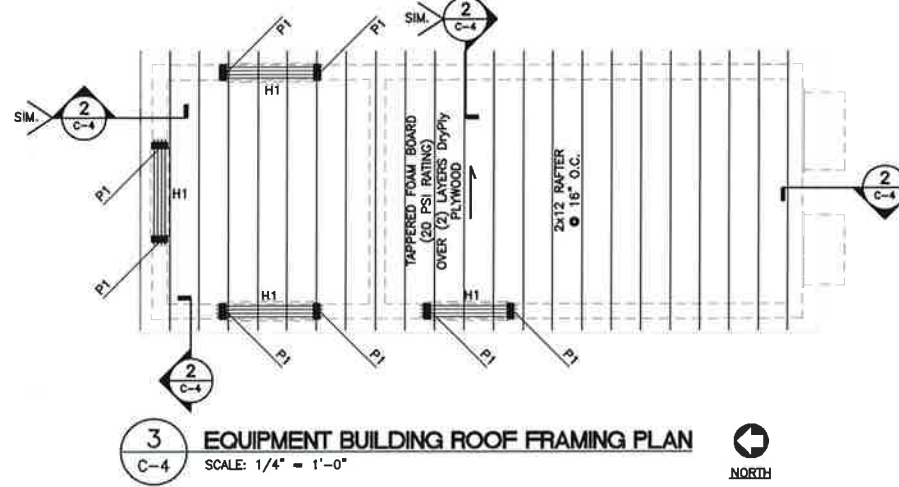
| INTERIOR FINISH SCHEDULE | | | | |
|---------------------------------|---|---------------|---|--|
| ROOM NAME | FLOORING | BASEBOARD | WALLS | CEILING |
| VERIZON EQUIPMENT ROOM | VCT OVER CONCRETE FLOOR SLAB SURFACE | 4" VINYL BASE | 1/8" FIBERGLASS REINF. PANEL OVER 1 LAYER 5/8" GWB OVER 1 LAYER 5/8" PLYWOOD <i>(PLYWOOD TELCO BOARD TO BE PAINTED "GRAY")</i> | 1/8" FIBERGLASS REINF. PANEL OVER 1 LAYER 5/8" GWB OVER 1 LAYER 3/4" PLYWOOD |
| VERIZON WIRELESS GENERATOR ROOM | MARSEAL 400 FLOOR LINING SYSTEM AS MANUFACTURED BY MRC, INC. PREPARE FLOOR AND COAT IN STRICT ACCORDANCE WITH MANUFACTURER'S REQUIREMENTS. RETURN COATING A MINIMUM 8" ON ALL ADJOINING GENERATOR ROOM WALLS. | N/A | 1/8" FIBERGLASS REINF. PANEL OVER 1 LAYER 5/8" GWB OVER 1 LAYER 5/8" PLYWOOD | 1/8" FIBERGLASS REINF. PANEL OVER 1 LAYER 5/8" GWB OVER 1 LAYER 3/4" PLYWOOD |

| EXTERIOR FINISH SCHEDULE | | |
|--|---|--|
| SIDING | TRIM | ROOFING |
| EIPS STUCCO FINISH COLOR: TO BE COORDINATED WITH CONSTRUCTION MANAGER AND BUILDING OWNER. | SOFFIT: ROYAL BUILDING PRODUCTS: ROYAL SOFFIT, TRADITIONAL SOFFIT, DOUBLE 4, 0.42 GAUGE EXTERIOR MOLDING AND TRIM: APEX ULTRIX SIDING COMPONENTS. COORDINATE WITH SPECIFIED SIDING. COLOR: TO BE COORDINATED WITH CONSTRUCTION MANAGER AND BUILDING OWNER. | 80 MIL. RUBBER ROOFING MEMBRANE. SEE DETAIL 2/C-4. COLOR: TO BE COORDINATED WITH CONSTRUCTION MANAGER AND BUILDING OWNER. |

| DOOR SCHEDULE | | | | | | | |
|---------------|------|------------------|---------------------|--|--------|-------|---------------|
| DOOR NO. | QTY. | DESCRIPTION | MANUF. | MODEL | HEIGHT | WIDTH | FINISH |
| 001 | 1 | FRAME | DE LA FONTAINE | SPLIT FRAME OPTION J7 (90 MIN. RATING) | 7'-0" | 3'-6" | PRIMED |
| | 1 | DOOR | DE LA FONTAINE | SERIES PA | 7'-0" | 3'-6" | PRIMED |
| | 1.5 | PAIR BUTT HINGES | HAGER | BB1199 4.5x4.5 NRP - STAINLESS STEEL | - | - | 32D |
| | 1 | LOCKSET | PDQ | GT 115 PHL SFC | - | - | 26D |
| | 1 | CYLINDER | BEST ACCESS SYSTEMS | 2 INTERCHANGEABLE | - | - | - |
| | 1 | DOOR CLOSER | HAGER | 5200 MLT | - | - | 686 |
| | 1 | THRESHOLD | HAGER | 412S | - | 3'-6" | MIL |
| | 1 | AUTO DOOR BOTTOM | HAGER | 747S | - | 3'-6" | MIL |
| | 1 | WEATHERSTRIP SET | HAGER | 870S | - | - | MIL |
| | 1 | LATCH PROTECTION | DON-JO | LP 211 SL | - | - | SILVER COATED |
| 002 | 1 | FRAME | DE LA FONTAINE | SPLIT FRAME OPTION J7 (90 MIN. RATING) | 7'-0" | 4'-0" | PRIMED |
| | 1 | DOOR | DE LA FONTAINE | SERIES PA | 7'-0" | 4'-0" | PRIMED |
| | 1.5 | PAIR BUTT HINGES | HAGER | BB1199 4.5x4.5 NRP - STAINLESS STEEL | - | - | 32D |
| | 1 | LOCKSET | PDQ | GT 115 PHL SFC | - | - | 26D |
| | 1 | CYLINDER | BEST ACCESS SYSTEMS | 2 INTERCHANGEABLE | - | - | - |
| | 1 | DOOR CLOSER | HAGER | 5200 MLT | - | - | 686 |
| | 1 | THRESHOLD | HAGER | 412S | - | 4'-0" | MIL |
| | 1 | AUTO DOOR BOTTOM | HAGER | 747S | - | 4'-0" | MIL |
| | 1 | WEATHERSTRIP SET | HAGER | 870S | - | - | MIL |
| | 1 | LATCH PROTECTION | DON-JO | LP 211 SL | - | - | SILVER COATED |



- ROOF FRAMING PLAN NOTES:**
- H1 = (3) 2x8 D.F. #2 HEADER
 - P1 = (2) 2x6 D.F. #2 JACK STUDS
 - INDICATES SLOPE OF TAPERED FOAM BOARD.
 - REFER TO SHEET N-1 FOR STRUCTURAL LUMBER REQUIREMENTS AND ADDITIONAL INFORMATION.



PROFESSIONAL ENGINEER SEAL
 STATE OF CONNECTICUT
 REGISTERED PROFESSIONAL ENGINEER
 No. 10000
 DATE: 07/09/15
 DRAWN BY: CHYD BY
 ISSUED FOR CONSTRUCTION DESCRIPTION

Cellco Partnership
 d.b.a. Verizon Wireless

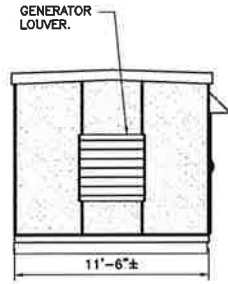
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Verizon Wireless
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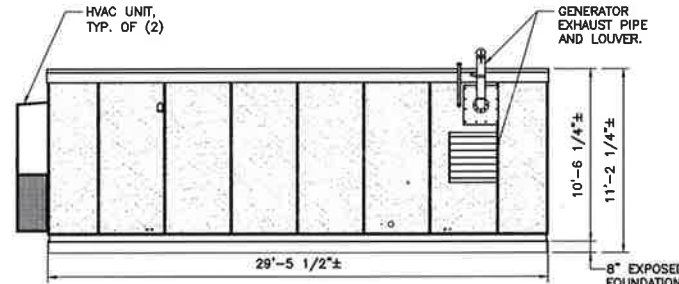
DATE: 05/11/15
 SCALE: AS NOTED
 JOB NO. 14124.000

EQUIPMENT SHELTER PLANS AND DETAILS

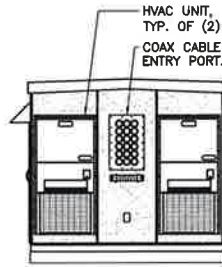
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 Sheet No. 8 of 24



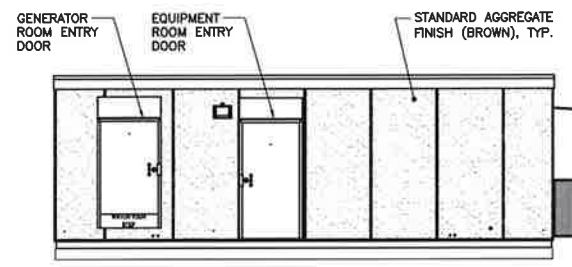
6 NORTHERN SHELTER ELEVATION
C-5 SCALE: 3/16" = 1'-0"



7 EASTERN SHELTER ELEVATION
C-5 SCALE: 3/16" = 1'-0"



8 SOUTHERN SHELTER ELEVATION
C-5 SCALE: 3/16" = 1'-0"



9 WESTERN SHELTER ELEVATION
C-5 SCALE: 3/16" = 1'-0"

FOUNDATION NOTES:

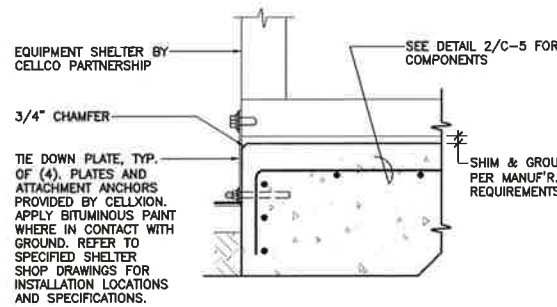
- IF ANY FIELD CONDITIONS EXIST WHICH PRECLUDE COMPLIANCE WITH THE DRAWINGS, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ENGINEER AND SHALL NOT PROCEED WITH ANY AFFECTED WORK.
- DIMENSIONS AND DETAILS SHALL BE CHECKED AGAINST THE PRE MANUFACTURED EQUIPMENT BUILDING SHOP DRAWINGS.
- THE CONTRACTOR SHALL VERIFY AND COORDINATE THE SIZE AND LOCATION OF ALL OPENINGS, SLEEVES AND ANCHOR BOLTS AS REQUIRED BY ALL TRADES.

COMPACTED GRAVEL FILL:

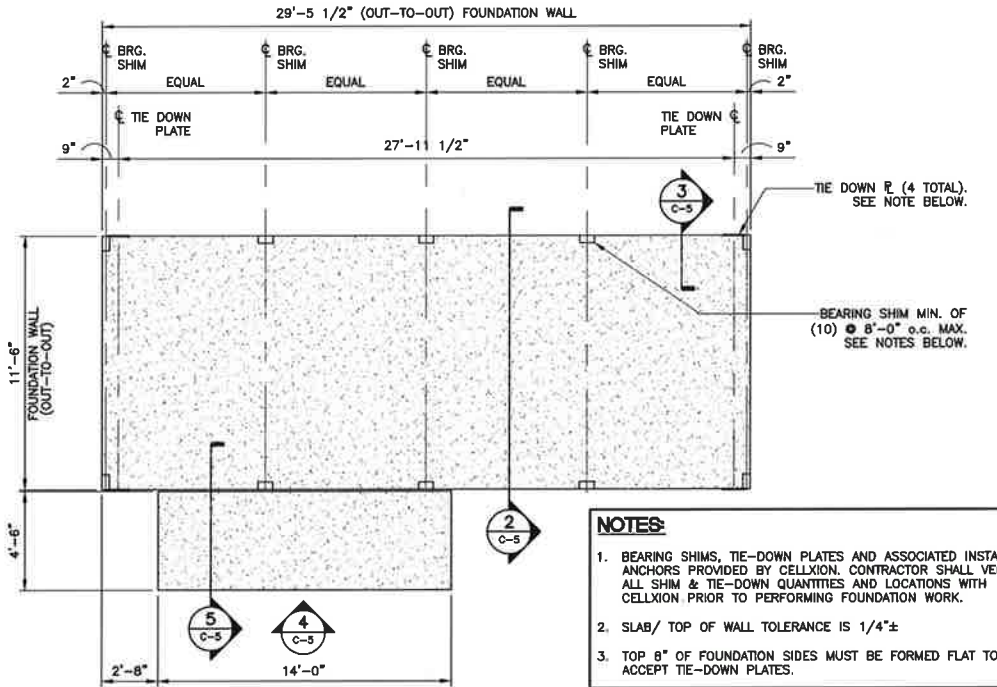
- COMPACTED GRAVEL FILL SHALL BE FURNISHED AND PLACED AS A FOUNDATION FOR STRUCTURES, WHERE SHOWN ON THE CONTRACT DRAWINGS OR DIRECTED BY THE ENGINEER.
- GRAVEL SHALL CONFORM TO THE REQUIREMENTS OF ARTICLE M.02.02 OF THE CONNECTICUT D.O.T. STANDARD SPECIFICATIONS. ADMIXTURES AND SURFACE PROTECTIVE MATERIALS USED TO PREVENT THE GRAVEL FROM FREEZING MUST MEET THE APPROVAL OF THE ENGINEER. THE LARGEST STONE SIZE SHALL BE 3-1/2 INCHES.
- SAMPLES OF THE MATERIAL TO BE USED SHALL BE DELIVERED TO THE JOB SITE 5 DAYS PRIOR TO ITS INTENDED USE SO IT MAY BE TESTED FOR APPROVAL.
- AFTER ALL EXCAVATION HAS BEEN COMPLETED, GRAVEL SHALL BE DEPOSITED IN LAYERS NOT EXCEEDING EIGHT (8) INCHES IN DEPTH OVER THE AREAS. IN EXCEPTIONAL CASES, THE ENGINEER MAY PERMIT THE FIRST LAYER TO BE THICKER THAN EIGHT (8) INCHES. EACH LAYER SHALL BE LEVELED OFF BY SUITABLE EQUIPMENT. THE ENTIRE AREA OF EACH LAYER SHALL BE COMPACTED BY USE OF APPROVED VIBRATORY, PNEUMATIC-TIRED OR TREAD-TYPE COMPACTION EQUIPMENT. COMPACTION SHALL BE CONTINUED UNTIL THE DRY DENSITY OVER THE ENTIRE AREA OF EACH LAYER IS NOT LESS THAN 95 PERCENT OF THE MAXIMUM DRY DENSITY ACHIEVED BY AASHTO T-99 METHOD C. THE MOISTURE CONTENT OF THE GRAVEL SHALL NOT VARY BY MORE THAN 3% FROM ITS OPTIMUM MOISTURE CONTENT. NO SUBSEQUENT LAYERS SHALL BE DEPOSITED UNTIL THE SPECIFIED COMPACTION IS ACHIEVED FOR THE PREVIOUS LAYER. IF NECESSARY TO OBTAIN THE REQUIRED COMPACTION, WATER SHALL BE ADDED AND GENTLE PUDDLING PERFORMED IF AUTHORIZED. COMPACTED GRAVEL FILL SHALL BE PREVENTED FROM FREEZING BY USE OF APPROVED ADMIXTURES OR BY USE OF APPROVED PROTECTIVE MATERIALS ON THE SURFACE, OR BOTH.

CONCRETE AND REINFORCING STEEL NOTES:

- ALL CONCRETE WORK SHALL BE IN ACCORDANCE WITH THE ACI 301, ACI 318.
- ALL CONCRETE SHALL BE NORMAL WEIGHT, 6% AIR ENTRAINED WITH A MAXIMUM SLUMP OF 4". AND SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH OF 3,000 PSI AT 28 DAYS, UNLESS NOTED OTHERWISE ON THE DRAWINGS.
- REINFORCING STEEL SHALL CONFORM TO ASTM A615, GRADE 60, DEFORMED BARS. WELDED WIRE FABRIC SHALL CONFORM TO ASTM A185 WELDED STEEL WIRE FABRIC. SPLICES SHALL BE CLASS "B" AND ALL HOOKS SHALL BE STANDARD UNLESS OTHERWISE INDICATED.
- THE FOLLOWING MINIMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCING STEEL UNLESS OTHERWISE NOTED ON THE DRAWINGS:
 CONCRETE CAST AGAINST EARTH.....3 IN.
 CONCRETE EXPOSED TO EARTH OR WEATHER:
 #6 AND LARGER.....2 IN.
 #5 AND SMALLER & WWF.....1 1/2 IN.
 CONCRETE NOT EXPOSED TO EARTH OR WEATHER OR NOT CAST AGAINST THE GROUND:
 SLAB AND WALL.....3/4 IN.
 BEAMS AND COLUMNS.....1 1/2 IN.
- ALL EXPOSED EDGES OF CONCRETE TO RECEIVE A 3/4" CHAMFER IN ACCORDANCE WITH ACI 301 SECTION 4.2.4.
- CONCRETE EQUIPMENT PAD TO RECEIVE A BRUSHED FINISH.
- INSTALLATION OF CONCRETE EXPANSION/WEDGE ANCHOR, SHALL BE PER MANUFACTURER'S WRITTEN RECOMMENDED PROCEDURE. THE ANCHOR BOLT, DOWEL OR ROD SHALL CONFORM TO MANUFACTURER'S RECOMMENDATION FOR EMBEDMENT DEPTH OR AS SHOWN ON THE DRAWINGS. NO REBAR SHALL BE CUT DURING DRILLING WITHOUT PRIOR REVIEW BY THE ENGINEER.

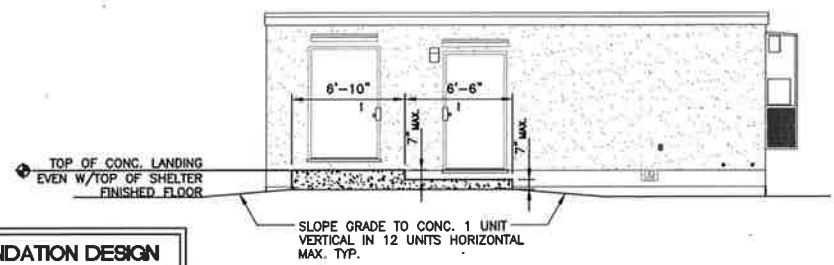


3 BUILDING TIE DOWN
C-5 SCALE: 1"=1'-0"



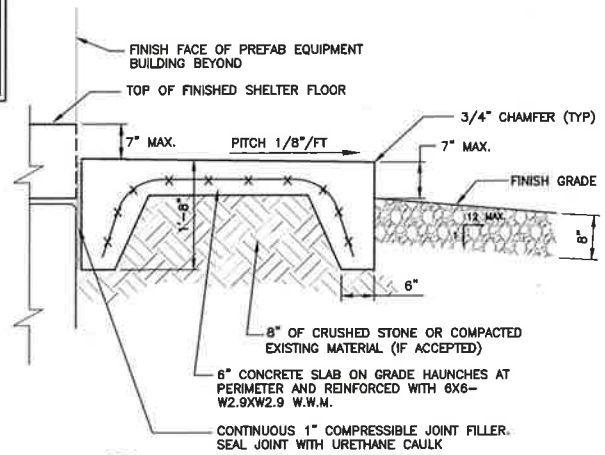
1 FOUNDATION PLAN
C-5 SCALE: 1/4"=1'-0"

- NOTES:**
- BEARING SHIMS, TIE-DOWN PLATES AND ASSOCIATED INSTALLATION ANCHORS PROVIDED BY CELLXION. CONTRACTOR SHALL VERIFY ALL SHIM & TIE-DOWN QUANTITIES AND LOCATIONS WITH CELLXION PRIOR TO PERFORMING FOUNDATION WORK.
 - SLAB/ TOP OF WALL TOLERANCE IS 1/4"±
 - TOP 8" OF FOUNDATION SIDES MUST BE FORMED FLAT TO ACCEPT TIE-DOWN PLATES.

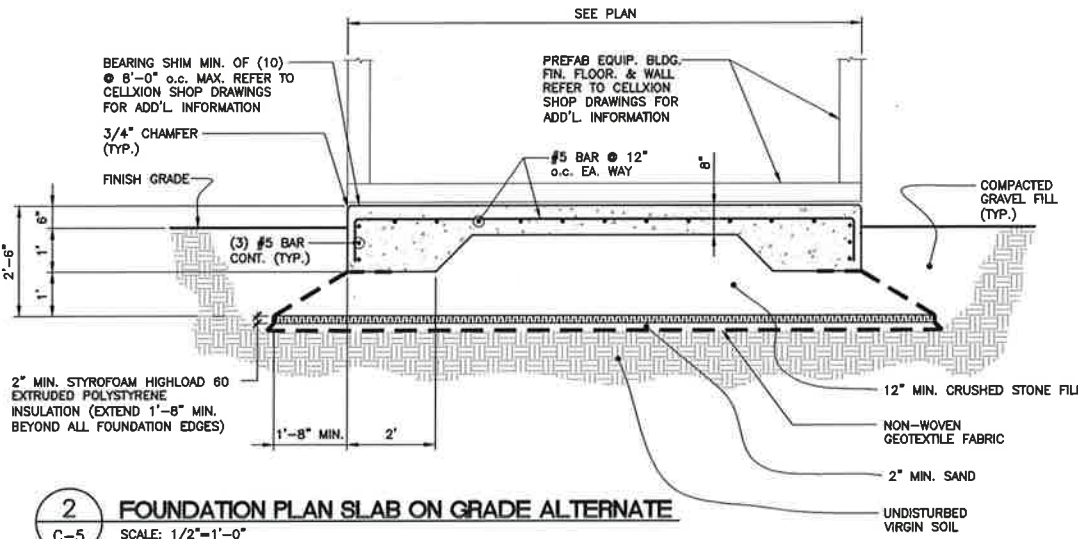


4 ENTRY STOOP DETAIL - ELEVATION
C-5 SCALE: 3/16"=1'-0"

SLAB ON GRADE FOUNDATION DESIGN CONFORMS TO THE REQUIREMENTS OF THE 2003 INTERNATIONAL BUILDING CODE AS MODIFIED BY THE 2005 CONNECTICUT STATE BUILDING CODE SUPPLEMENT SECTION 1805.21 'FROST PROTECTION' AND SE/ASCE STANDARD 32-01 SECTION 7.1 'SLAB ON GRADE CONSTRUCTION'.



5 ENTRY STOOP DETAIL - SECTION
C-5 SCALE: 3/16"=1'-0"



2 FOUNDATION PLAN SLAB ON GRADE ALTERNATE
C-5 SCALE: 1/2"=1'-0"

PROFESSIONAL ENGINEER SEAL

DATE: 07/09/15
HMR
DRAWN BY: CHY'D
ISSUED FOR CONSTRUCTION

Cellco Partnership
d.b.a. Verizon Wireless

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Centek Solutions
2003 486-098 E. 4th St.
652 North Branch Road
Branford, CT 06405
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Verizon Wireless
WIRELESS COMMUNICATIONS FACILITY

ASHFORD RELO, CT

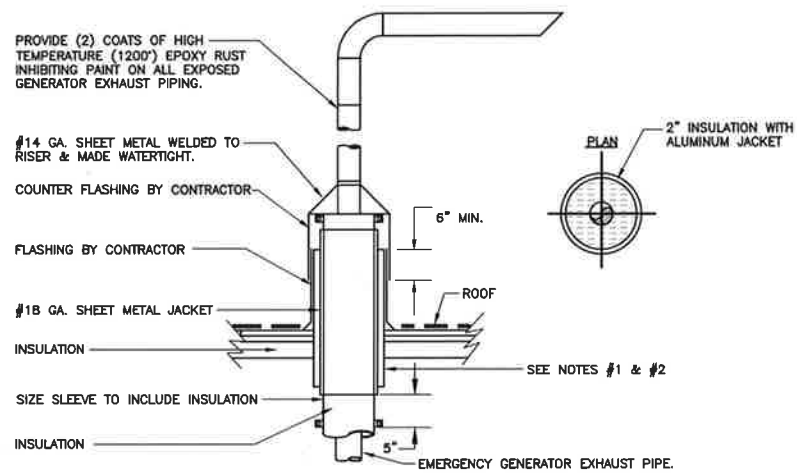
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ASHFORD, CT 06278

DATE: 05/11/19
SCALE: AS NOTED
JOB NO. 14124.000

SHELTER FOUND. PLAN, DETAILS, ELEVATIONS AND NOTES

C-5

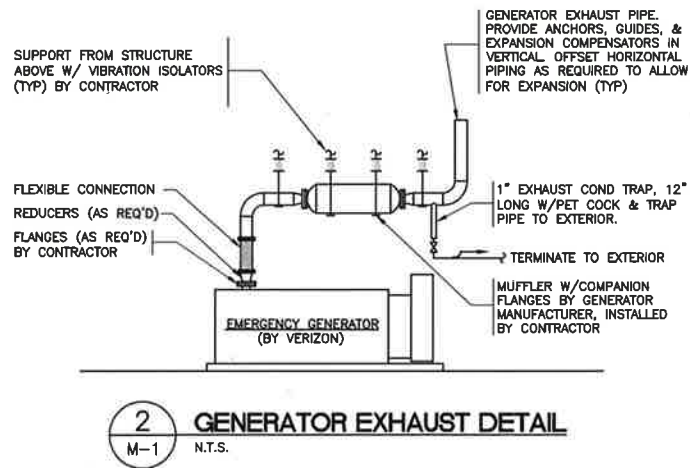
Sheet No. 9 of 24



NOTES:

1. PACK ANNULAR OPENING IN SLEEVE W/FIRE RETARDANT ROPE.
2. RING PLATE WELDED TO SLEEVE AND FASTENED TO ROOF.
3. STACK SHALL BE LOCATED MIN. 30'-0" FROM ANY AIR INTAKE OR OPERABLE WINDOW

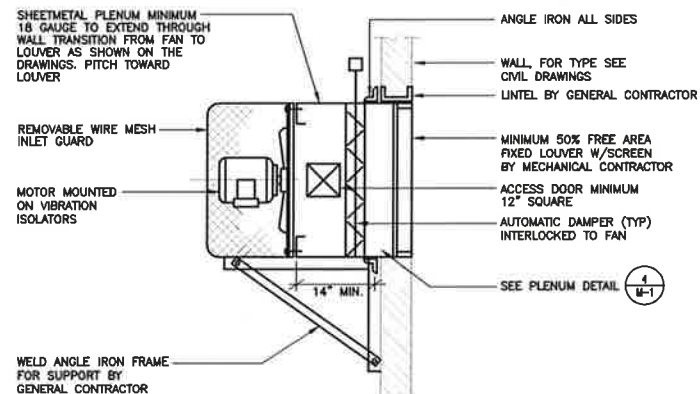
1 GENERATOR STACK DETAIL
M-1 N.T.S.



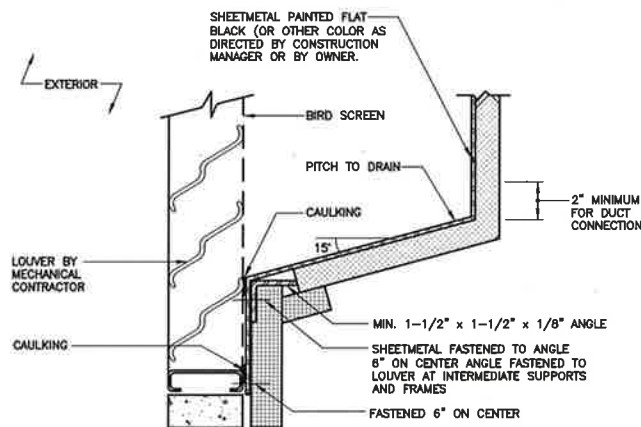
2 GENERATOR EXHAUST DETAIL
M-1 N.T.S.

| HVAC DUCTWORK SYMBOLS | |
|-----------------------|---------------------------------------|
| | DOUBLE LINE DUCTWORK |
| | FLEXIBLE DUCTWORK |
| | RECTANGULAR RETURN/EXHAUST DUCT RISER |
| | RECTANGULAR SUPPLY AIR GRILLE |
| | RECTANGULAR RETURN AIR GRILLE |
| | REVERSE ACTING THERMOSTAT |
| | THERMOSTAT |
| | HYDROGEN DETECTOR |
| | EXHAUST FAN |
| | LOUVER |
| | MOTORIZED AUTOMATIC DAMPER |
| | LOCAL ALARM LIGHT |

| ABBREVIATIONS | |
|------------------------------|-----------------------------|
| AFF ABOVE FINISHED FLOOR | AHU AIR HANDLING UNIT |
| BTU BRITISH THERMAL UNIT | MBH BTU PER HOUR (THOUSAND) |
| CFM CUBIC FEET PER MINUTE | T THERMOSTAT |
| EAT ENTERING AIR TEMPERATURE | TYP TYPICAL |
| EF-# EXHAUST FAN | V VOLTS |
| ESP EXTERNAL STATIC PRESSURE | VEL VELOCITY |
| FPM FEET PER MINUTE | W WATT |
| HP HORSEPOWER | DB DRY BULB |
| KW KILOWATTS | WB WET BULB |
| LAT LEAVING AIR TEMPERATURE | CP CONTROL PANEL |
| PH PHASE | L-# LOUVER |
| MIN. MINIMUM | FC FLEX CONNECTION |
| GA GAUGE | WC WATER COLUMN |
| COND CONDENSATE | NOM NOMINAL |
| REQ'D REQUIRED | PD PRESSURE DROP |
| N.T.S. NOT TO SCALE | IN INCH |
| HP HORSEPOWER | SF SQUARE FEET |
| | FT FOOT |



3 PROPELLER FAN (EXHAUST)
M-1 N.T.S.



NOTES:
SUPPORT PLENUM FROM FLOOR OR STRUCTURE ABOVE W/GALVANIZED STEEL ANGLES AND CHANNELS.

4 PLENUM LOUVER CONNECTION
M-1 N.T.S.

| FAN SCHEDULE | | | | | | | |
|--------------|-----------|----------------|-----|-----------|-----------------------|------------|---------|
| SYMBOL | MAKE | MODEL NUMBER | CFM | ESP IN/WG | MOTOR DATA HP-VOLT-PH | DRIVE TYPE | REMARKS |
| EF-1 | GREENHECK | SE1-12-432-E-1 | 383 | .25 | 1/20-120-1 | DIRECT | ALL |

REMARKS:
1. PROVIDE SERVICE SWITCH.
2. PROVIDE MOTORIZED DAMPER.
3. POWER FED FROM INVERTOR CONNECTED TO EMERGENCY BATTERIES. COORDINATE WITH ELECTRICAL CONTRACTOR.
4. PROVIDE WALL MOUNT HOUSING, FAN GUARD, GRAVITY BACKDRAFT DAMPER.
5. COORDINATE SIZE WITH WALL OPENING.
6. COORDINATE LOCATION WITH OTHER TRADES

| LOUVER SCHEDULE | | | | | | | | | |
|-----------------|-----------|--------------|------|-----------------|--------------|---------------|----------------|-----------|---------|
| SYMBOL | MAKE | MODEL NUMBER | CFM | VELOCITY FT/MIN | FREE AREA SF | NOM. WIDTH IN | NOM. HEIGHT IN | PD IN. WG | REMARKS |
| L-1,2 | GREENHECK | ESD-603 | 383 | 472 | .81 | 18 | 18 | .04 | ALL |
| L-3 | GREENHECK | ESD-603 | 2460 | 378 | 7.8 | 48 | 48 | .05 | ALL |
| L-4 | GREENHECK | ESD-603 | 2460 | 378 | 7.8 | 48 | 48 | .05 | ALL |

REMARKS:
1. PROVIDE WITH BIRD SCREEN.
2. PROVIDE WITH EXTENDED SILL.
3. PROVIDE WITH BAKED ENAMEL FINISH. COLOR TO MATCH EXISTING BUILDING AND APPROVED BY OWNER.
4. COORDINATE ALL LOUVER SIZES IN FIELD PRIOR TO ORDERING OR INSTALLATION.

ISSUED FOR CONSTRUCTION
DRAWN BY CHK/D BY
DATE
REV.

PROFESSIONAL ENGINEER SEAL
VERIZON WIRELESS
d.b.a. VERIZON WIRELESS

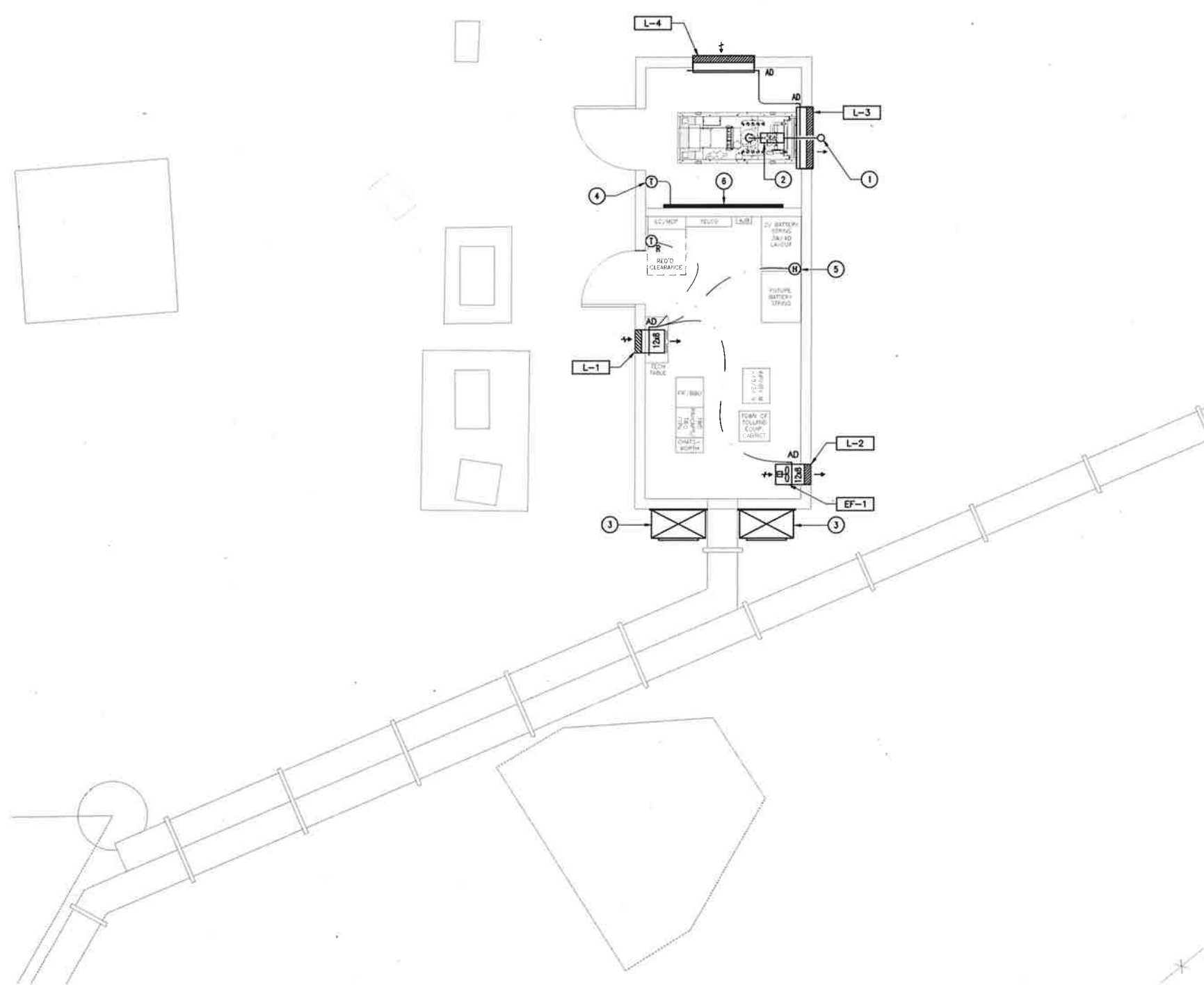
CEN TEK engineering
Center of Solution
203-488-0580
203-488-0587 Fax
80 Hartford, CT 06183
www.CentekEng.com

Verizon Wireless
WIRELESS COMMUNICATIONS FACILITY
ASHFORD RELO., CT
353 PUMPKIN HILL ROAD
ASHFORD, CT 06278

DATE: 05/11/15
SCALE: AS NOTED
JOB NO. 14124.000

MECH. NOTES
SYMBOLS, DETAILS
& SCHEDULES

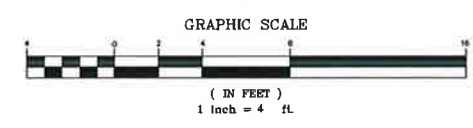
M-1
Sheet No. 10 of 24



HVAC WORK NOTES

- ① 2" SCHEDULE 40 EXHAUST PIPE THROUGH WALL AND UP. EXTEND EXHAUST PIPE 2'-0" VERTICALLY ABOVE STRUCTURE OR FIXED OBJECTS WITHIN 10'-0" HORIZONTAL OF PIPE. VERIFY IN FIELD.
- ② EMERGENCY GENERATOR MUFFLER FURNISHED BY VERIZON AND INSTALLED BY CONTRACTOR. PROVIDE ALL REQUIRED HANGERS, VIBRATION ISOLATORS, RODS, SUPPLEMENTARY STEEL, ETC. TO HOUSE GENERATOR MUFFLER. INSTALL PER MANUFACTURER'S RECOMMENDATIONS. REFER TO DETAILS 1/M-1 AND 2/M-1.
- ③ 5 TON WALL MOUNT AIR CONDITIONER EQUAL TO BARD MODEL W51A1. PROVIDE WITH 5KW HEAT, ECONOMIZER, LOW AMBIENT CONTROL, AND LEAD/LAG CONTROLLER WITH INTEGRAL THERMOSTAT.
- ④ REVERSE ACTING THERMOSTAT INTERLOCKED WITH EF-1.
- ⑤ PROVIDE HYDROGEN DETECTOR AND INTERLOCK WITH EF-1. INTERNAL RELAY SHALL ACTIVATE EXHAUST FAN WHEN HYDROGEN LEVEL IN SPACE REACHES 1% BY VOLUME (ADJUSTABLE).
- ⑥ HYDRONIC ELECTRIC HEATER EQUAL TO DAYTON 3UG29, 511B BTUH, 240V/1PH, 1500 WATTS, 7.2 AMPS. PROVIDE WITH REMOTE THERMOSTAT.

1 MECHANICAL - GENERATOR / EQUIPMENT ROOM PLAN
 M-2 SCALE: 1/4"=1'-0"



| | | | | | |
|--|--|--|---|---|---|
| | | | | | |
| | | | <p>ASHFORD RELO., CT WIRELESS COMMUNICATIONS FACILITY 353 PUMPKIN HILL ROAD ASHFORD, CT 06278</p> | <p>DATE: 05/11/15 SCALE: AS NOTED JOB NO. 14124.000</p> | <p>MECHANICAL PLAN & NOTES</p> |
| <p>07/09/15 KHS DATE DRAWN BY CHK'D BY REV.</p> | | | | | |
| <p>ISSUED FOR CONSTRUCTION DESCRIPTION</p> | | | | | |
| <p>0</p> | | | | | |
| <p>14124.000</p> | | | | | |
| <p>M-2</p> | | | | | |
| <p>Sheet No. 11 of 24</p> | | | | | |

MECHANICAL SPECIFICATIONS

SCOPE

THE WORK TO BE DONE UNDER THIS DIVISION OF THE SPECIFICATIONS INCLUDE THE FURNISHING OF ALL EQUIPMENT, SUPPLIES, LABOR, SUPERVISION AND ALL MATERIALS NOT SPECIFICALLY MENTIONED, READY FOR USE. PLUMBING, SPRINKLER, HEATING, VENTILATION, AIR CONDITIONING EQUIPMENT AND ASSOCIATED ITEMS AND ALL TEMPERATURE CONTROL OR EMS COMPONENTS. IT IS THE INTENTION OF THE SPECIFICATIONS AND DRAWINGS TO CALL FOR FINISHED WORK, TESTED AND READY FOR OPERATION.

IT IS THE INTENT THAT ALL MECHANICAL WORK AND MATERIALS NECESSARY TO COMPLETE THE ENTIRE PROJECT IN ACCORDANCE WITH THE CONTRACT PLANS AND SPECIFICATIONS, WHERE SPECIFICALLY MENTIONED HERE OR NOT, SHALL BE FURNISHED. ALL WORK AND MATERIALS NECESSARY TO FULFILL THIS INTENT SHALL BE SUPPLIED UNDER THE MECHANICAL SPECIFICATIONS WITHOUT ADDITIONAL COST TO THE OWNER.

CODES, RULES, PERMITS AND FEES

THIS CONTRACTOR SHALL GIVE ALL NECESSARY NOTICES, OBTAIN ALL PERMITS AND PAY ALL STATE AND LOCAL TAXES, FEES AND OTHER COSTS IN CONNECTION WITH HIS WORK; FILE ALL NECESSARY PLANS, PREPARE ALL DOCUMENTS AND OBTAIN ALL NECESSARY APPROVALS OF ALL STATE AND LOCAL DEPARTMENTS HAVING JURISDICTION; OBTAIN ALL REQUIRED CERTIFICATES OF INSPECTION FOR HIS WORK AND DELIVERY OF SAME TO THE OWNER BEFORE REQUEST FOR ACCEPTANCE AND FINAL PAYMENT FOR THE WORK.

THIS CONTRACTOR SHALL INCLUDE IN THE WORK, WITHOUT EXTRA COST TO THE OWNER, ANY LABOR, MATERIALS, SERVICES, APPARATUS, DRAWINGS (IN ADDITION TO CONTRACT DRAWINGS AND DOCUMENTS), IN ORDER TO COMPLY WITH ALL APPLICABLE LAWS, ORDINANCES, RULES AND REGULATIONS WHETHER OR NOT SHOWN ON THE DRAWINGS AND/OR SPECIFIED.

THIS CONTRACTOR SHALL PERFORM AND FILE ALL TESTS IN ACCORDANCE WITH CURRENT REGULATIONS OF THE STATE AND LOCAL AUTHORITIES. HE SHALL FURNISH AND INSTALL SIGNS REQUIRED BY THE STATE AND LOCAL AUTHORITIES.

ALL MATERIALS FURNISHED AND ALL WORK INSTALLED SHALL COMPLY WITH THE RULES AND RECOMMENDATIONS OF THE NATIONAL BOARD OF FIRE UNDERWRITERS, WITH ALL REQUIREMENTS OF LOCAL UTILITIES COMPANIES, WITH THE RECOMMENDATIONS OF THE FIRE INSURANCE RATING ORGANIZATION HAVING JURISDICTION.

REGULATIONS

ALL WORK SHALL BE DONE IN STRICT ACCORDANCE WITH STATE BUILDING CODE, IBC 2003, STATE FIRE SAFETY CODE, A.D.A., U.L., NEMA, O.S.H.A., NATIONAL PLUMBING CODE AND NFPA, WITH ALL REQUIREMENTS OF ALL GOVERNMENTAL DEPARTMENTS HAVING JURISDICTION, REQUIREMENTS OF THE ABOVE SHALL TAKE PRECEDENCE OVER PLANS AND SPECIFICATIONS.

GUARANTEE AND SERVICE

THE CONTRACTOR SHALL GUARANTEE ALL MATERIALS AND WORKMANSHIP FOR A PERIOD OF ONE YEAR FROM THE DATE OF ACCEPTANCE OF THE INSTALLATION. IN ADDITION, THE CONTRACTOR SHALL PROVIDE, FREE OF CHARGE, ONE YEAR'S MAINTENANCE GUARANTEE OF MAINTAINED SERVICE AND ADJUSTMENT OF ALL EQUIPMENT IN THIS CONTRACT.

DRAWINGS AND INTENT

DRAWINGS ARE INTENDED AS WORKING DRAWINGS FOR GENERAL LAYOUT OF THE VARIOUS ITEMS OF EQUIPMENT. HOWEVER, LAYOUT OF EQUIPMENT, ACCESSORIES, SPECIALTIES, AND PIPING SYSTEMS ARE DIAGRAMMATIC UNLESS SPECIFICALLY DIMENSIONED, AND DO NOT NECESSARILY INDICATE EVERY REQUIRED PIPE, VALVE, FITTINGS, TRAP, ELBOW, TRANSITION, OFFSETS, JUNCTION OR PULLBOX, OR SIMILAR ITEMS REQUIRED FOR A COMPLETE INSTALLATION.

WORK NOT INCLUDED

ALL ELECTRICAL WORK, CUTTING AND PATCHING, PIERS, LINTELS, ALL CONCRETE WORK AND ALL PAINTING.

THIS CONTRACTOR SHALL FURNISH THE GENERAL CONTRACTOR WITH THE SIZES AND LOCATIONS OF CHASES AND OPENINGS WHICH OCCUR IN WALLS, PARTITIONS, FLOORS, ETC., REQUIRED FOR THE INSTALLATION OF THE WORK CALLED FOR UNDER THIS CONTRACT, WILL BE DONE BY THE GENERAL CONTRACTOR, EXCEPT CUTTING REQUIRED FOR THE INSTALLATION OF HANGERS.

MEASUREMENTS

ALL MEASUREMENTS TAKEN AT THE BUILDING SHALL TAKE PRECEDENCE OVER SCALE DIMENSIONS. EVERY PART OF THE PLANS SHALL BE FITTED TO THE ACTUAL CONDITIONS AT THE BUILDING. IF IN CONFLICT WITH SCALE DIMENSIONS, CONTACT CONSTRUCTION MANAGER & ENGINEER FOR CLARIFICATION.

INTERRUPTION OF EXISTING SERVICES

PRIOR TO PERFORMING WORK REQUIRING INTERRUPTION OF EXISTING SERVICES, THE CONTRACTOR SHALL SECURE FROM THE OWNER, APPROVAL OF THE PROPOSED OPERATION. (72 HOURS IN ADVANCE WHENEVER POSSIBLE).

WORK SHALL BE ARRANGED FOR CONTINUOUS PERFORMANCE WHENEVER POSSIBLE. THE CONTRACTOR SHALL PROVIDE ALL NECESSARY LABOR, INCLUDING OVERTIME, IF REQUIRED, TO ASSURE THAT EXISTING OPERATING SERVICES WILL BE SHUT DOWN ONLY DURING THE TIME ACTUALLY REQUIRED TO MAKE NECESSARY CONNECTIONS.

PROTECTION OF FIXTURES, MATERIALS AND EQUIPMENT

CLOSE PIPE OPENINGS WITH CAPS OR PLUGS DURING INSTALLATION. TIGHTLY COVER AND PROTECT FIXTURES AND EQUIPMENT AGAINST DIRT, WATER AND CHEMICAL OR MECHANICAL INJURY. AT COMPLETION OF ALL WORK, FIXTURES, EXPOSED MATERIALS AND EQUIPMENT SHALL BE THOROUGHLY CLEANED.

DEMOLITION

CONTRACTOR SHALL FURNISH ALL LABOR, MATERIALS, EQUIPMENT, ETC., REQUIRED TO COMPLETE ALL DEMOLITION WORK NECESSARY FOR THE FULL COMPLETION OF THIS CONTRACT. PROTECT ALL PARTS AND EQUIPMENT THAT ARE TO REMAIN. ASSUME FULL RESPONSIBILITY FOR DAMAGE.

ALL ITEMS BEING REMOVED SHALL REMAIN THE PROPERTY OF THE OWNER UNLESS OTHERWISE INDICATED BY THE OWNER. EQUIPMENT AND DEVICES THE OWNER DOES NOT WISH TO RETAIN SHALL BECOME THE PROPERTY OF THIS CONTRACTOR AND REMOVED FROM THE SITE. ALL MATERIAL CHOSEN TO BE RETAINED BY THE OWNER SHALL BE DELIVERED BY THE CONTRACTOR TO SUCH POINT AS DESIGNATED BY THE OWNER.

EXAMINATION OF PREMISES - SPECIAL NOTE

NO CONSIDERATION OR ALLOWANCE WILL BE GRANTED FOR FAILURE TO VISIT SITE, OR FOR ANY ALLEGED MISUNDERSTANDING OF MATERIALS TO BE FURNISHED, OR WORK TO BE DONE; IT BEING THAT TENDER OF PROPOSAL INDICATED WITH IT AGREEMENT TO ITEMS AND CONDITIONS REFERRED TO HEREIN OR INDICATED ON AFOREMENTIONED DRAWINGS.

SCAFFOLDING, RIGGING AND HOISTING

UNLESS OTHERWISE SPECIFIED, CONTRACTOR SHALL FURNISH ALL SCAFFOLDING, RIGGING, HOISTING AND SERVICES NECESSARY FOR ERECTION AND DELIVERY INTO THE PREMISES OF ANY EQUIPMENT AND APPARATUS FURNISHED. REMOVE SAME FROM THE PREMISES WHEN NO LONGER REQUIRED.

HOUSEKEEPING

THIS CONTRACTOR SHALL BE RESPONSIBLE FOR KEEPING STOCK OF MATERIALS AND EQUIPMENT STORED ON PREMISES IN A NEAT AND ORDERLY MANNER AND, AT ALL TIMES, KEEP THE PREMISES FREE FROM ACCUMULATION OF WASTE MATERIAL OR RUBBISH CAUSED BY HIS EMPLOYEES AT WORK. HE SHALL REMOVE HIS RUBBISH AND SURPLUS MATERIALS FROM THE JOB SITE AND SHALL LEAVE THE PREMISES AND HIS WORK IN A CLEAN AND PERFECT CONDITION.

QUIET OPERATION

ALL WORK SHALL OPERATE UNDER ALL CONDITIONS OF LOAD WITHOUT ANY SOUND OR VIBRATION WHICH IS OBJECTIONABLE IN THE OPINION OF THE CONSTRUCTION MANAGER. IN CASE OF MOVING MACHINERY, SOUND OR VIBRATION NOTICEABLE OUTSIDE OF ROOM IN WHICH IT IS INSTALLED, OR ANNOYING INSIDE ITS OWN ROOM, WILL BE CONSIDERED OBJECTIONABLE BY THE CONSTRUCTION MANAGER AND SHALL BE REMEDIED IN APPROVED MANNER BY CONTRACTOR AT HIS EXPENSE.

SHOP DRAWINGS

PRIOR TO DELIVERY TO JOB SITE, BUT SUFFICIENTLY IN ADVANCE OF REQUIREMENTS NECESSARY TO ALLOW CONSTRUCTION MANAGER AMPLE TIME FOR REVIEW, CONTRACTOR SHALL SUBMIT FOR APPROVAL, SEVEN (7) COPIES EACH OF SHOP DRAWINGS OF ALL EQUIPMENT. ALSO, SHEET METAL FABRICATION DRAWINGS DRAWN TO A SCALE OF 1/4" TO THE FOOT OR LARGER.

ADJACENT TENANTS

WORK IN ADJACENT OCCUPIED TENANT SPACES SHALL NOT BE SCHEDULED DURING NORMAL WORK HOURS.

EQUIPMENT DEVIATION

THE PLANS AND/OR SPECIFICATIONS INDICATE THE NAME, MODEL NUMBER OR TYPE OF EQUIPMENT OR MATERIALS SPECIFIED. SHOULD THE BIDDER DESIRE TO USE EQUIPMENT OR MATERIALS OR A MAKE OTHER THAN THOSE SPECIFIED OR SHOWN, HE SHALL ATTACH A RIDER TO THE BID FORM LISTING THE DEDUCTIONS AND/OR ADDITIONS TO HIS BASE BID, TOGETHER WITH THE MANUFACTURER'S NAME AND MODEL NUMBERS OF THE EQUIPMENT OR MATERIALS HE PROPOSED TO FURNISH AS "SUBSTITUTES". IF NO SUBSTITUTE INFORMATION IS FURNISHED, IT WILL BE EXPRESSLY UNDERSTOOD THAT ALL EQUIPMENT AND MATERIALS NAMED WILL BE FURNISHED IN FULL ACCORDANCE WITH THE PLANS AND/OR SPECIFICATIONS.

CORE DRILLING/WATERPROOFING

ALL CORE DRILLING REQUIRED SHALL BE DONE BY GENERAL CONTRACTOR. ALL ROOF PENETRATIONS, FLASHING AND WATER PROOFING SHALL BE DONE BY GENERAL CONTRACTOR. WORK SHALL BE PERFORMED BY AN APPLICATOR CERTIFIED BY THE EXISTING ROOF SYSTEM MANUFACTURER.

RECORD DRAWINGS

CONTRACTOR SHALL KEEP ACCURATE RECORD OF ALL DEVIATIONS IN WORK AS ACTUALLY INSTALLED FROM WORK INDICATED PAYING PARTICULAR ATTENTION TO DIMENSIONING OUTSIDE UNDERGROUND UTILITY LINES, THEIR OFFSETS AND VALUES.

OWNER'S INSTRUCTIONS AND SYSTEM OPERATION

AT THE TIME OF THE JOB'S ACCEPTANCE BY OWNER, CONTRACTOR SHALL FURNISH ONE COMPLETE SET OF APPROVED CERTIFIED DRAWINGS TO THE OWNER. IN ADDITION, CONTRACTOR SHALL FURNISH MAINTENANCE AND OPERATING INSTRUCTIONS FOR ALL EQUIPMENT. THESE INSTRUCTIONS SHALL BE WRITTEN IN LAYMAN'S LANGUAGE AND SHALL BE INSERTED IN VINYL-COVERED THREE-RING LOOSE LEAF BINDER. THIS INFORMATION IN BINDER SHALL BE FIRST SENT TO AND APPROVED BY THE CONSTRUCTION MANAGER BEFORE TURNING OVER TO OWNER.

SEISMIC RESTRAINTS

SEISMIC RESTRAINTS DESIGNED AND CONSTRUCTED FOR LATERAL FORCES IN ANY DIRECTION SHALL BE PROVIDED FOR ALL MECHANICAL EQUIPMENT AND PIPING IN ACCORDANCE WITH THE STATE BUILDING CODE. SUBMIT SEISMIC RESTRAINT DESIGN AND CALCULATIONS STAMPED BY A CONNECTICUT LICENSED STRUCTURAL ENGINEER.

TESTS

THE CONTRACTOR SHALL, AT HIS OWN EXPENSE, DURING THE PROGRESS OF THE WORK OR UPON ITS COMPLETION AS ORDERED, MAKE SUCH TESTS OF HIS WORK AS ARE HEREIN SPECIFIED OR AS ARE REQUIRED BY AND IN THE PRESENCE OF THE BUILDING INSPECTOR. IF SO DIRECTED, TESTS SHALL BE MADE OF SECTIONS FOR THE WORK SO AS NOT TO DELAY THE WORK OR OTHER TRADES.

THE CONTRACTOR SHALL PROVIDE ALL APPARATUS, TEMPORARY WORK OR ANY OTHER REQUIREMENTS NECESSARY FOR SUCH TESTS. HE SHALL TAKE ALL DUE PRECAUTIONS TO PREVENT DAMAGE TO THE BUILDING OR ITS CONTENTS THAT MAY BE INCURRED BY SUCH TESTS AS HE WILL BE REQUIRED TO REPAIR AND MAKE GOOD, AT HIS OWN EXPENSE, ANY DAMAGE CAUSED.

ANY DEFECTS OR DEFICIENCIES DISCOVERED AS A RESULT OF TESTS SHALL BE IMMEDIATELY REPAIRED AND TESTS SHALL BE REPEATED UNTIL THE TEST REQUIREMENTS ARE FULLY COMPLIED WITH.

TESTS SHALL BE PERFORMED IN THE PRESENCE OF AND TO THE SATISFACTION OF THE ENGINEER, AND LOCAL DEPARTMENT REPRESENTATIVES.

THE CONTRACTOR SHALL NOTIFY THE ARCHITECT TWO DAYS IN ADVANCE OF RUNNING TESTS TO ALLOW THEIR REPRESENTATIVE TO BE PRESENT TO WITNESS TESTS. NOTIFICATION TO BE IN WRITING.

HANGER AND SUPPORTING

HANGING AND SUPPORTING - PIPING SHALL NOT BE SUPPORTED BY OTHER PIPING, BUT SHALL BE SUPPORTED WITH COPPER PIPE HANGERS SUITABLE FOR THE SIZE OF PIPE AND PROPER STRENGTH AND QUALITY AT PROPER INTERVALS SO THAT PIPING CANNOT BE MOVED ACCIDENTALLY FROM THE INSTALLED POSITION. REFER TO DETAIL SHEET.

SEQUENCE OF OPERATION

PROVIDE ALL CONTROLS, LOW VOLTAGE CONTROL WIRING AND ACCESSORIES NECESSARY TO ACCOMPLISH THE SEQUENCE OF OPERATION AS INDICATED BELOW. POWER WIRING SHALL BE PROVIDED IN ACCORDANCE WITH ELECTRICAL SPECIFICATIONS. COORDINATE WITH ELECTRICAL CONTRACTOR.

EF-1 EXHAUST FAN


EXHAUST FAN SHALL BE ACTIVATED BY HYDROGEN DETECTOR AND REVERSE ACTING T-STAT.

INTERLOCK AUTOMATIC INTAKE AND EXHAUST DAMPERS WITH EXHAUST FAN MOTOR.


REVERSE ACTING THERMOSTAT SHALL ENERGIZE EXHAUST FAN AT A PRESET TEMPERATURE OF 78°F (ADJUSTABLE).

EXHAUST FAN SHALL BE INTERLOCKED WITH HYDROGEN DETECTOR. HYDROGEN DETECTOR RELAY SHALL ACTIVATE EXHAUST FAN WHEN HYDROGEN LEVEL REACHES 1% BY VOLUME.

| | |
|----------------------------|-------------------------|
| PROFESSIONAL ENGINEER SEAL | ISSUED FOR CONSTRUCTION |
| DATE | 07/09/15 |
| SCALE | AS NOTED |
| JOB NO. | 14124.000 |
| MECHANICAL SPECIFICATIONS | |
| M-3 | |
| Sheet No. 12 of 24 | |



Calico Partnership
d.b.a. Verizon Wireless



Centek on Submittal

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Verizon Wireless
WIRELESS COMMUNICATIONS FACILITY

ASHFORD RELO, CT

353 PUMPKIN HILL ROAD
ASHFORD, CT 06278

| LIGHT FIXTURE SCHEDULE | | | | |
|------------------------|---|---|--------------------------------------|----------|
| TYPE | MANUFACTURER CATALOG/MODEL No. | DESCRIPTION | LAMP | MOUNTING |
| A | DAY-BRITE #OWL-470L-840-UNIV | 9" WIDE, SURFACE MOUNTED LED LIGHT FIXTURE WITH ACRYLIC PRISMATIC DIFFUSER, 4000K COLOR, UNIVERSAL VOLTAGE | 73W LED | CEILING |
| B | LUMARK #LDWPFCA120EDPE | EXTERIOR CUTOFF LED LUMINAIRE, DIE-CAST ALUMINUM HOUSING, BRONZE FINISH, IMPACT RESISTANT TEMPERED GLASS LENS, BUILT-IN PHOTO CONTROL | 40W LED | WALL |
| E | SURE-LITES #CC3-NC-WH-SD | EMERGENCY LIGHT UNIT WITH 90 MINUTE NICKEL CADMIUM BATTERY & SELF-DIAGNOSTIC TESTING FEATURE | (2) 5.4W PAR36 | WALL |
| E1 | SURE-LITES #CC5-NC-WHSD WITH SURE-LITES #6T6DWHH REMOTE HEADS | EMERGENCY LIGHT UNIT WITH REMOTE WEATHERPROOF HEADS AND 90 MINUTE NICKEL CADMIUM BATTERY & SELF-DIAGNOSTIC TESTING FEATURE | (2) 5.4W PAR36 (2) 6 WATT HALOGEN | WALL |

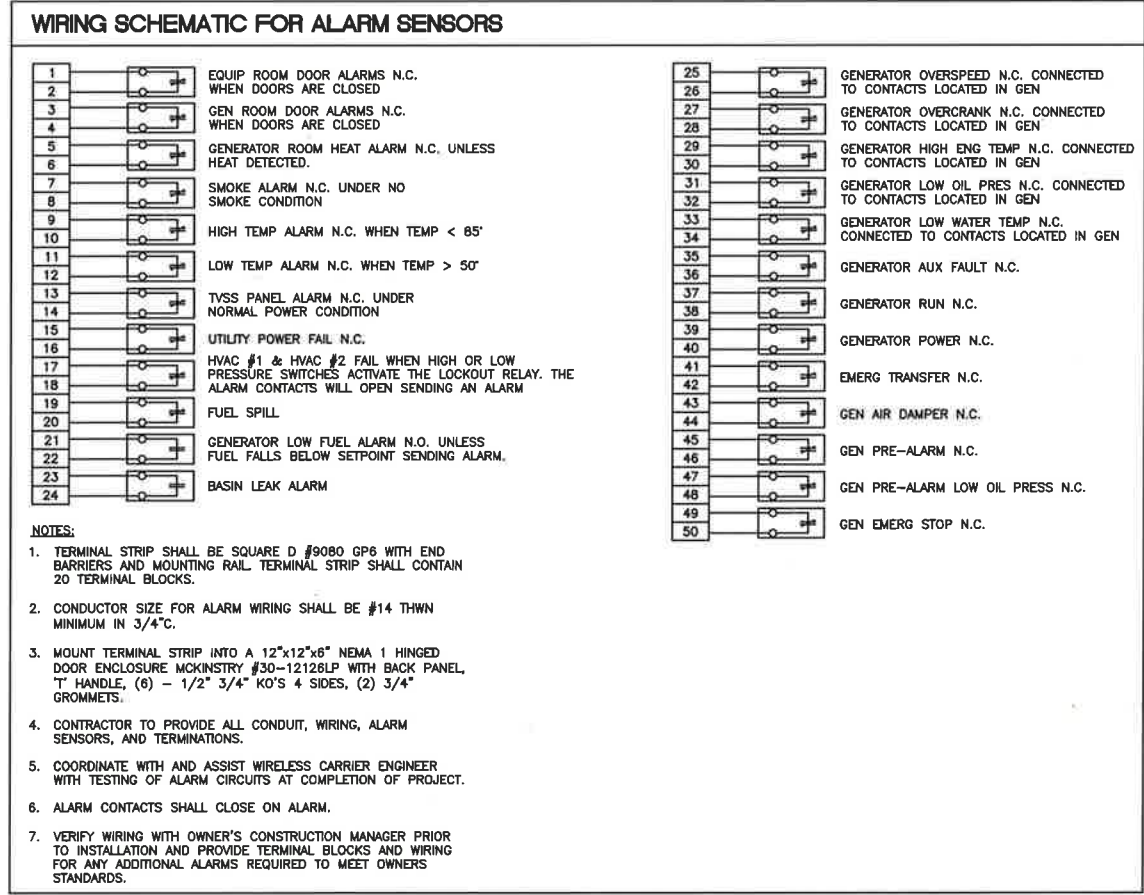
NOTES:
 1. PROVIDE ALL THE NECESSARY ACCESSORIES AS REQUIRED TO MOUNT LIGHTING FIXTURES TO CEILING STRUCTURE AS REQUIRED.
 2. EXTERIOR LIGHT SHALL BE CONNECTED TO 4HR TIMER SWITCH.

| ELECTRICAL ABBREVIATIONS | |
|--------------------------|---|
| ABBREVIATION | DESCRIPTION |
| AFF | ABOVE FINISHED FLOOR |
| AIC | AMPERE INTERRUPTING CAPACITY |
| AWG | AMERICAN WIRE GAGE |
| C | CONDUIT |
| EGR | EXTERIOR GROUND RING |
| ETR | EXISTING TO REMAIN |
| G - GRD | GROUND |
| GFCI | GROUND FAULT CIRCUIT INTERRUPTER |
| IGR | INTERIOR GROUND RING MOUNTED 9'-0" ABOVE FINISHED FLOOR |
| KWH | KILO-WATT-HOUR |
| MCCB | MOLDED CASE CIRCUIT BREAKER |
| MDP | MAIN DISTRIBUTION PANEL |
| NC | NORMALLY CLOSED |
| OC | ON CENTER |
| SA | SURGE ARRESTOR |
| VM | VOLTAGE MONITOR |
| WP | WEATHERPROOF |
| ER | EXISTING TO REMAIN |
| RR | REMOVE AND RELOCATE |
| RE | RELOCATED EXISTING |

| VOLTAGE: | | PHASE: | | WIRE: | | PANEL NO. | | MDP | |
|------------------|--|------------------|--|--------------|--|-----------|--|----------------|--|
| 120/240 | | 1 | | 3 | | | | | |
| MAIN BUS: | | AMPS: | | A FRAME: | | A TRIP: | | LOC: | |
| 200 | | 200 | | 200 | | 200 | | EQUIPMENT ROOM | |
| TOTAL WATTS, L1: | | TOTAL WATTS, L2: | | TOTAL WATTS: | | | | | |
| 38,900 | | 38,240 | | 77,140 | | | | | |
| MOUNTING: | | SURFACE | | | | | | | |

NOTES:
 A) PANEL SHALL BE GENERAL INTEGRATE LOAD CENTER, 200A, 120/240V, SINGLE-PHASE, DOUBLE TVSS.
 B) BRANCH CIRCUIT BREAKER AND CONDUCTOR SIZE BASED ON SPECIFIC EQUIPMENT. CONFIRM ELECTRICAL REQUIREMENTS PRIOR TO INSTALLATION. COORDINATE WITH MECHANICAL CONTRACTOR AND USE HACR BREAKERS FOR HVAC.
 C) ALL BRANCH CIRCUITS SHALL BE ROUTED IN 4" X 4" WIREWAY TO THE FULLEST EXTENT POSSIBLE. CONNECTIONS FROM WIREWAY TO EQUIPMENT AND DEVICES SHALL BE IN GALVANIZED RIGID METAL CONDUIT INDICATED IN SCHEDULE BELOW.
 D) INCREASE CONDUIT & CONDUCTOR SIZES AS REQUIRED TO MAINTAIN A MAXIMUM VOLTAGE DROP OF 2%, AND AS REQUIRED FOR AMBIENT TEMPERATURE CORRECTION, WHERE ROUTED ACROSS ROOFS.

| DIRECTORY | WIRE & CONDUIT | WATTS LOAD | | CKT. | AMPS | L1 | L2 | Y | AMPS | CKT. | WATTS LOAD | | WIRE & CONDUIT | DIRECTORY |
|-----------------------|------------------------|------------|-------|------|-------|----|----|---|------|------|------------|-------|------------------------|---------------------|
| | | L1 | L2 | | | | | | | | L1 | L2 | | |
| HVAC-1 | 1 1/4" C, 3 #4, #6 GND | 5,520 | | 1 | 60/2P | | | | | 2 | 5,520 | | 1 1/4" C, 3 #4, #6 GND | HVAC-2 |
| SPARE | | | 5,520 | 3 | | | | | | 4 | | 5,520 | | SPARE |
| SPARE | | | | 5 | 20 | | | | | 6 | | | | SPARE |
| SPARE | | | | 7 | 20 | | | | | 8 | | | | SPARE |
| SPARE | | | | 9 | 20 | | | | | 10 | 1,200 | | 3/4" C, 2 #12, #12GND | RECEPTACLES |
| EXHAUST FAN | 3/4" C, 2 #12, #12GND | 400 | | 11 | 20 | | | | | 12 | 600 | | 3/4" C, 2 #12, #12GND | EXT REC, COND. PUMP |
| BATTERY CHARGE/RECEPT | 3/4" C, 2 #12, #12GND | 800 | | 13 | 20 | | | | | 14 | 1,500 | | 3/4" C, 2 #12, #12GND | BLOCK HEATER |
| LIGHTING | 3/4" C, 2 #12, #12GND | | 1,000 | 15 | 20 | | | | | 16 | 2,200 | | 3/4" C, 2 #10, #10GND | RECTIFIER #6 |
| RECTIFIER #1 | 3/4" C, 2 #10, #10GND | 2,200 | | 17 | 30/2P | | | | | 18 | 2,200 | | 3/4" C, 2 #10, #10GND | RECTIFIER #7 |
| RECTIFIER #2 | 3/4" C, 2 #10, #10GND | 2,200 | | 19 | 30/2P | | | | | 22 | 2,200 | | 3/4" C, 2 #10, #10GND | RECTIFIER #8 |
| RECTIFIER #3 | 3/4" C, 2 #10, #10GND | 2,200 | | 23 | 30/2P | | | | | 24 | 2,200 | | 3/4" C, 2 #10, #10GND | RECTIFIER #9 |
| RECTIFIER #4 | 3/4" C, 2 #10, #10GND | 2,200 | | 25 | 30/2P | | | | | 28 | 2,200 | | 3/4" C, 2 #10, #10GND | RECTIFIER #10 |
| RECTIFIER #5 | 3/4" C, 2 #10, #10GND | 2,200 | | 27 | 30/2P | | | | | 29 | 2,200 | | 3/4" C, 2 #10, #10GND | RECTIFIER #11 |
| SPARE | | | | 29 | 20 | | | | | 30 | 2,200 | | 3/4" C, 2 #12, #12GND | FAA TOWER LIGHTS |
| SPARE | | | | 31 | 20 | | | | | 32 | 2,200 | | 3/4" C, 2 #12, #12GND | RECEPT - TOWN EQUIP |
| SPARE | | | | 33 | 20 | | | | | 34 | 2,200 | | | |
| SPARE | | | | 35 | 20 | | | | | 38 | 2,200 | | | |
| SPARE | | | | 37 | 20 | | | | | 40 | 1,000 | | | |
| SPARE | | | | 39 | 20 | | | | | 42 | 360 | | | |
| SPARE | | | | 41 | 20 | | | | | | | | | |



| ELECTRICAL LEGEND | |
|-------------------|---|
| SYMBOL | DESCRIPTION |
| | FLUORESCENT LIGHTING FIXTURE |
| | EMERGENCY LIGHTING FIXTURE |
| | DISCONNECT SWITCH |
| | FUSED DISCONNECT SWITCH |
| | HOMERUN, PANELBOARD AND CIRCUIT # AS INDICATED |
| | BRANCH CIRCUIT CONDUIT AND CONDUCTORS |
| | SWITCHED BRANCH CIRCUIT CONDUIT AND CONDUCTORS |
| | MAIN DISTRIBUTION PANEL |
| | ALARM JUNCTION BOX |
| | DUPLEX RECEPTACLE |
| | QUADPLEX RECEPTACLE |
| | DUPLEX RECEPTACLE WITH GFCI AND WEATHER PROOF COVER LISTED 'WHILE-IN-USE' |
| | HIGH TEMPERATURE SENSOR |
| | LOW TEMPERATURE SENSOR |
| | THERMOSTAT (PROVIDED BY DIVISION 15, INSTALLED BY DIVISION 15) |
| | HIGH HUMIDISTAT (PROVIDED BY DIVISION 15, INSTALLED BY DIVISION 15) |
| | SMOKE DETECTOR WITH N.C. AUXILIARY CONTACTS FOR FACP INTERFACE |
| | DOOR ALARM CONTACT |
| | KWH SUBMETERING AS SPECIFIED |
| | TELEPHONE OUTLET, RJ-11/45 MODULAR JACK (MOUNTED 54" AFF) |
| | EXOTHERMIC WELD CONNECTION |
| | NON METALLIC 3" STANDOFF FASTENER |
| | EXOTHERMIC WELD 'T' OF THRU' CONDUCTOR AND TAP CONDUCTOR, 'CADWELD TYPE TA' |
| | EXOTHERMIC WELD TYPE 'TA' |
| | NEW EXTERIOR GROUND RING |
| | GROUND BAR AT WAVE PORT |
| | 5/8" DIAMETER x 10'-0" COPPER GROUND ROD |
| | 5/8" DIAMETER x 10'-0" COPPER GROUND ROD WITH ACCESS |
| | AUDIO/VISUAL ALARM |
| | 12 HR TIMER SWITCH. (MOUNTED 54" AFF) |
| | EXIT SIGN WITH DUALHEAD EMERGENCY LIGHT |
| | EMERGENCY LIGHT REMOTE HEAD |
| | MOTION SENSOR CONTROLLED LIGHT |
| | GROUND WELL |
| | HEAT DETECTOR WITH N.C. AUXILIARY CONTACTS FOR FACP INTERFACE |
| | HYDROGEN DETECTOR WITH N.C. AUXILIARY CONTACTS FOR FACP INTERFACE |
| | INTERSECT 200A CAM-LOCK GENERATOR CONNECTOR, WITH DEUTSCH CONNECTOR |
| | GROUND BAR |
| | TELCO CONDUIT |
| | ELECTRICAL CONDUIT |
| | GROUND CONDUIT |
| | FIRE ALARM CONDUIT |

PROFESSIONAL ENGINEER SEAL

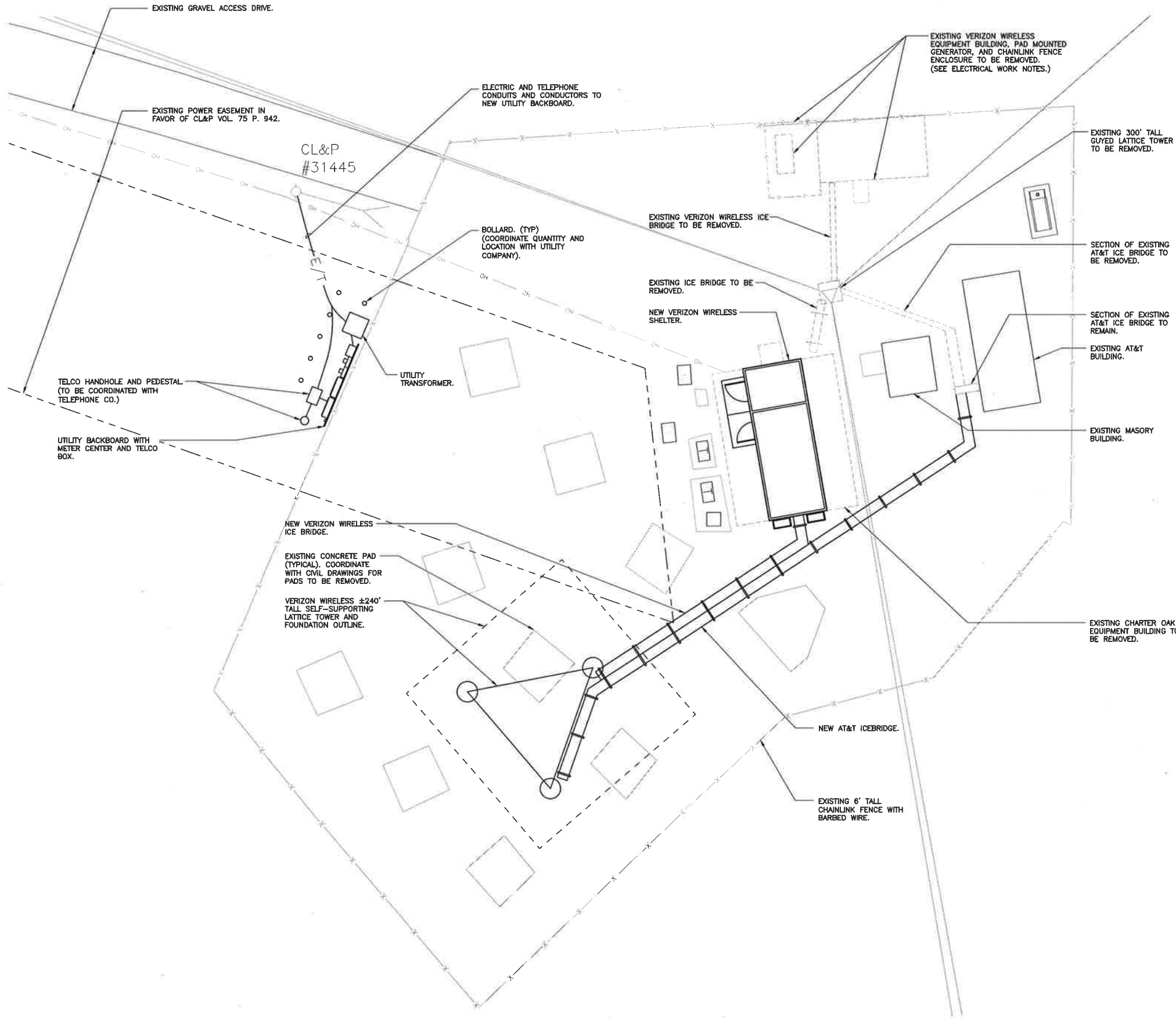
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 SCALE: AS NOTED
 JOB NO. 14124.000

ELECTRICAL LEGEND AND NOTES

Verizon Wireless
 WIRELESS COMMUNICATIONS FACILITY

ASHFORD RELO., CT
 353 PUMPKIN HILL ROAD
 ASHFORD, CT 06278

Sheet No. 13 of 24



- GENERAL NOTES:**
- REFER TO CIVIL DRAWINGS FOR ACTUAL LOCATIONS OF STRUCTURES ON SITE.
 - COORDINATION, LAYOUT AND FURNISHING OF CONDUIT, CABLE AND ALL APPURTENANCES REQUIRED FOR PROPER INSTALLATION OF ELECTRICAL/TELECOMMUNICATIONS SERVICES SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR.
 - ALL UTILITY WORK SHALL BE IN ACCORDANCE WITH LOCAL UTILITY COMPANY, AND OWNERS REQUIREMENTS AND SPECIFICATIONS.
 - PROVIDE CADWELD CONNECTION STYLES: THROUGH (CABLE TO CABLE) TYPE "TA" (CABLE TO SURFACE) TYPE "LA" OR "VS" (PIPE) (CABLE TO ROD) TYPE "GT" OR "NC" (CABLE TO CABLE) TYPE "SS"
 - ALL REFERENCES TO THE NEC WITHIN THESE PLANS SHALL ALSO INCLUDE THE MEC.
 - PRIOR TO REMOVAL OF TOWER, ICE BRIDGE, FENCE AND OTHER EQUIPMENT, DISCONNECT ALL ASSOCIATED GROUNDING CONNECTIONS.
 - EXISTING GROUND RING, RODS, AND OTHER ELEMENTS OF GROUNDING ELECTRODE SYSTEM SHALL REMAIN UNDISTURBED TO THE GREATEST EXTENT POSSIBLE UNLESS OTHERWISE NOTED. ANY DAMAGE SHALL BE RESTORED. ANY ELEMENTS IN CONFLICT WITH NEW CONSTRUCTION SHALL BE RELOCATED ACCORDING TO GROUNDING PLAN LAYOUT AND PROPERLY BONDED.
 - ANY EXISTING UNDERGROUND UTILITY CONDUITS LOCATED WITHIN PROXIMITY OF THE REPLACEMENT TOWER SHALL BE RELOCATED OUT OF THE NEW TOWER CONSTRUCTION AREA. COORDINATE RELOCATIONS AND OUTAGES WITH ALL AFFECTED PARTIES AND PROVIDE TEMPORARY POWER AS REQUIRED.

- ELECTRICAL WORK NOTES:**
- INSTALL GROUNDING FOR VERIZON WIRELESS AS SHOWN IN THE PLANS AND DETAILS.
 - INSTALL GROUNDING FOR ANTENNA SYSTEM ELEMENTS BELONGING TO TENANTS RELOCATED FROM FORMER TOWER. COORDINATE WITH EACH TENANT AND INSTALL ALL GROUNDING ELEMENTS ACCORDING TO THE DETAILS AND SPECIFICATIONS PROVIDED BY EACH RESPECTIVE ENTITY. (FOR BIDDING PURPOSES ASSUME SAME REQUIREMENTS AS FOR VERIZON WIRELESS).
 - INSTALL ICE BRIDGE GROUNDING FOR ALL NEW ICE BRIDGE SECTIONS AS SHOWN IN THE PLANS AND DETAILS.
 - INSTALL ALL OTHER GROUNDING AS SHOWN IN THE PLANS AND DETAILS.
 - COORDINATE WITH CIVIL DRAWINGS FOR SEQUENCE OF CONSTRUCTION AND SCOPE OF WORK FOR ENTITIES OTHER THAN VERIZON WIRELESS.
 - RELOCATE TOWN RADIO EQUIPMENT AND ANTENNA SYSTEM FROM EXISTING VERIZON WIRELESS SHELTER PRIOR TO DECOMMISSIONING OR REMOVING TOWER. COORDINATE SCOPE OF WORK AND REQUIREMENTS WITH CONSTRUCTION MANAGER.
 - RELOCATE ALL EXISTING 120/240V, SINGLE PHASE UTILITY SERVICE METERS AND DISCONNECTS TO NEW METER CENTER. COORDINATE ALL WORK WITH UTILITY COMPANY AND EACH AFFECTED PARTY.

- ELECTRICAL DEMOLITION NOTES:**
- REMOVE ALL CABLES, CONDUCTORS, LIGHTNING PROTECTION, SURGE PROTECTORS, GROUND BARS, AND OTHER ELECTRICAL DEVICES FROM EXISTING TOWER AND GUY WIRES.
 - DISCONNECTED GROUND LEADS CONNECTED TO GROUND RING SHALL BE CUT BACK BELOW GRADE TO A LOCATION JUST BEFORE THE BOND TO THE GROUND RING. THE GROUND RING AND ASSOCIATED EXOTHERMICALLY WELDED BONDS SHALL NOT BE DISTURBED.
 - ANY DAMAGE TO EXISTING GROUNDING SYSTEMS NOT SCHEDULED FOR REMOVAL, SHALL BE REPAIRED AND RESTORED TO ORIGINAL CONDITION.



| | | |
|--|-----------|----------|
| ISSUED FOR CONSTRUCTION | DATE | 07/09/15 |
| DRAWN BY | DATE | |
| REV. | DATE | |
| | | |
| Calico Partnership d.b.a. Verizon Wireless | | |
| CENTEK Engineering, Inc. Centered on Solutions 6031 486 0259 6031 486 9897 Fax 652 North Branford Road Branford, CT 06405 www.CentekEng.com | | |
| Verizon Wireless WIRELESS COMMUNICATIONS FACILITY ASHFORD RELO., CT 353 PLUMKIN HILL ROAD ASHFORD, CT 06278 | | |
| DATE: | 05/11/15 | |
| SCALE: | AS NOTED | |
| JOB NO. | 14124.000 | |
| SITE UTILITY PLAN | | |
| E-2 Sheet No. 14 of 24 | | |

RISER NOTES

- ① EXISTING UTILITY POLE TO BE USED. REFER TO SITE SURVEY AND UTILITY PLAN.
- ② 3" CONDUIT FOR PRIMARY ELECTRIC CONDUCTORS. CONDUCTORS PROVIDED BY UTILITY COMPANY FROM UTILITY POLE TO TRANSFORMER. PROVIDE ALL COUPLINGS, ADAPTERS, SWEEPS, AND ASSOCIATED HARDWARE. MATERIAL SHALL BE PER UTILITY COMPANY SPECIFICATIONS.
- ③ TRANSFORMER PROVIDED BY UTILITY COMPANY. TRANSFORMER VAULT, HOUSING, AND GROUND GRID BY ELECTRICAL CONTRACTOR, PER UTILITY COMPANY SPECIFICATIONS.
- ④ PROVIDE TRANSFORMER GROUNDING PER NEC AND UTILITY COMPANY SPECIFICATIONS.
- ⑤ TWO SETS OF: (3) 600 KCMIL, (1) 1/0 AWG GROUND, 4°C.
- ⑥ TWO 4" CONDUITS WITH PULL ROPES FOR TELEPHONE COMPANY CONDUCTORS. CONDUCTORS PROVIDED BY TELEPHONE COMPANY FROM UTILITY POLE TO UTILITY BOARD. PROVIDE ALL COUPLINGS, ADAPTERS, SWEEPS, AND ASSOCIATED HARDWARE. MATERIAL SHALL BE PER TELEPHONE COMPANY SPECIFICATIONS.
- ⑦ PROVIDE CONDUIT WITH PULL ROPE BETWEEN HANDHOLE AND PEDESTAL. EXPECT TWO 4" CONDUITS, BUT FINAL SIZE AND QUANTITY PER TELEPHONE COMPANY.
- ⑧ TELEPHONE AND ELECTRIC SPICE BOXES. MUST BE TRAFFIC RATED. QUANTITY AND LOCATION PER UTILITY COMPANY SPECIFICATIONS. EXPECT MAXIMUM OF ONE PER UTILITY. INSTALL ONLY IF REQUIRED BY UTILITY COMPANIES.
- ⑨ TELEPHONE COMPANY HANDHOLE. INSTALL PER TELEPHONE COMPANY SPECIFICATIONS.
- ⑩ TELEPHONE COMPANY PEDESTAL. INSTALL PER TELEPHONE COMPANY SPECIFICATIONS.
- ⑪ UTILITY BACKBOARD. REFER TO CIVIL DRAWINGS.
- ⑫ TWO 3'x4'x1" NEMA-3R TELEPHONE ENCLOSURES INSTALLED NEXT TO EACH OTHER ON UTILITY BACKBOARD. MAINTAIN APPROXIMATELY 1" SEPARATION BETWEEN AND INSTALL A SECTION OF 4" CONDUIT CONNECTING BOTH BOXES.
- ⑬ PROVIDE DOUBLE DUPLEX, GFI RECEPTACLE IN WEATHERPROOF ENCLOSURE INSIDE OF TELEPHONE ENCLOSURE. CONNECT TO DEDICATED 20A/1P CIRCUIT IN VERIZON WIRELESS ELECTRIC PANEL IN SHELTER.
- ⑭ PROVIDE GROUND BAR AS REQUIRED BY TELEPHONE COMPANY.
- ⑮ #2 AWG GROUNDING CONDUCTOR IN 3/4" PVC CONDUIT, UNLESS OTHERWISE SPECIFIED BY TELEPHONE COMPANY. BOND TO GROUNDING TRIAD.
- ⑯ 800A, 240/120V, 1P, 65 KAIC RATED, NEMA-3R, MAIN CIRCUIT BREAKER MODULE WITH 800A/2P MAIN CIRCUIT BREAKER. (SQUARE-D: EZM1800CBU OR APPROVED EQUIVALENT.) MUST BE UTILITY COMPANY APPROVED.
- ⑰ TWO 3-GANG MULTI-METER BRANCH DEVICES WITH 240V, 1P, 3W, 225A RATED METER SOCKETS. (SQUARE-D: EZML13225 OR APPROVED EQUIVALENT). MUST BE UTILITY COMPANY APPROVED.
- ⑱ UTILITY COMPANY APPROVED METER FOR VERIZON WIRELESS IN AVAILABLE SOCKET. PROVIDE LABEL STATING "VERIZON WIRELESS" ALSO PROVIDE LABEL INDICATING TYPE AND LOCATION OF GENERATOR PER NEC REQUIREMENTS.
- ⑲ 200A/2P MAIN CIRCUIT BREAKER IN AVAILABLE POSITION CORRESPONDING TO METER FOR VERIZON WIRELESS. PROVIDE LABELS INDICATING "VERIZON WIRELESS", AS WELL AS TYPE AND LOCATION OF ONSITE GENERATOR PER NEC.
- ⑳ 3/0 AWG GROUNDING ELECTRODE CONDUCTOR IN 3/4" PVC CONDUIT BONDED TO GROUNDING TRIAD LOCATED AT UTILITY BACKBOARD. GROUNDING TRIAD SHALL BE BONDED TO COMPOUND GROUND RING WITH #2 AWG SOLID TINNED BARE COPPER WIRE.
- ㉑ (3) # 3/0 AWG, (1) # 6 AWG GROUND, 2-1/2°C. FROM METER TO NORMAL POWER LUGS IN INTEGRATED LOAD CENTER IN EQUIPMENT ROOM.
- ㉒ (2) # 12 AWG, #12 AWG GROUND, 3/4°C. FROM DEDICATED 20A/1P CIRCUIT BREAKER IN VERIZON WIRELESS POWER PANEL TO RECEPTACLE IN TELCO BOXES.
- ㉓ EXPANSION COUPLING, TYPICAL.
- ㉔ (2) 4" PVC CONDUITS FOR TELEPHONE SERVICE. PROVIDE TELEPHONE CABLES AS REQUIRED BY TELEPHONE COMPANY AND OWNER. ONE CONDUIT SHALL REMAIN AS OWNERS SPARE, AND SHALL BE CAPPED AND LABELED AT BOTH ENDS. INSTALL PULL ROPE IN SPARE CONDUIT.
- ㉕ VERIZON WIRELESS EQUIPMENT SHELTER. AFTER COMPLETION OF INSTALLATION, REMOVE EXISTING VERIZON WIRELESS SHELTER AND GENERATOR AND RETURN TO VERIZON WIRELESS. COORDINATE DECOMMISSIONING WITH VERIZON CONSTRUCTION MANAGER.
- ㉖ EXTEND TO EMERGENCY LUGS FOR IN INTEGRATED LOAD CENTER/ATS IN EQUIPMENT ROOM.
- ㉗ INTEGRATED LOAD CENTER "MDP". REFER TO PANEL SCHEDULE FOR SPECIFICATIONS.
- ㉘ 1" CONDUIT AND CONDUCTORS FOR GENERATOR CONTROL WIRING.
- ㉙ (3) #3/0 AWG, (1) #6 AWG GROUND, 2" CONDUIT.
- ㉚ 150A, 240V, 2P CIRCUIT BREAKER ON GENERATOR OUTPUT.
- ㉛ GENERATOR BATTERY CHARGER. PROVIDE DEDICATED 20A, 120V CIRCUIT FROM PANEL MDP.
- ㉜ GENERATOR BLOCK HEATER. PROVIDE DEDICATED 20A, 120V CIRCUIT FROM PANEL MDP.
- ㉝ 30 KW, 120/240V, SINGLE PHASE, DIESEL FUELED GENERATOR.
- ㉞ GENERATOR GROUND PER NEC.
- ㉟ REMOTE GENERATOR SHUT OFF SWITCH IN BREAK GLASS ENCLOSURE MOUNTED TO THE EXTERIOR OF THE SHELTER IN LOCATION APPROVED BY LOCAL FIRE MARSHAL. INSTALL ALL REQUIRED SIGNAGE.
- ㊱ 3/4" CONDUIT AND CONDUCTORS REQUIRED FOR PROPER OPERATION OF EMERGENCY GENERATOR SHUT OFF SWITCH.
- ㊲ NEW TOWER. (REFER TOP CIVIL DRAWINGS FOR ADDITIONAL INFORMATION.)
- ㊳ PHOTOCELL FOR FAA LIGHTING SYSTEM CONTROL. SEE FAA LIGHTING NOTES THIS SHEET.
- ㊴ FAA LIGHTING SYSTEM CONTROLLER ENCLOSURE. PROVIDE DEDICATED 120V, 20A CIRCUIT FROM PANEL MDP. SEE FAA LIGHTING NOTES THIS SHEET.
- ㊵ DUAL RED & WHITE L-884/L-885 MEDIUM INTENSITY LED TOP MOUNTED AVIATION OBSTRUCTION FLASH HEAD. SEE FAA LIGHTING NOTES THIS SHEET.
- ㊶ L-81 LED MARKER LIGHT - TYPICAL OF THREE (ONE PER TOWER LEG). SEE FAA LIGHTING NOTES THIS SHEET.
- ㊷ CONDUITS AND CONDUCTORS FOR RELOCATED SERVICES. ALL STANDALONE METERS SHALL BE RELOCATED TO NEW METER CENTER WITH NEW CONDUITS, CONDUCTORS, METERS, DISCONNECT BREAKERS, AND LABELS. ALL EXISTING STANDALONE SERVICE EQUIPMENT SHALL BE REMOVED PRIOR TO CUTOVER. COORDINATE ALL CUTOVER WORK WITH UTILITY COMPANY AND EACH AFFECTED PARTY. PROVIDE TEMPORARY POWER AS REQUIRED TO MINIMIZE DOWN TIME. COORDINATE OUTAGES WITH EACH AFFECTED PARTY. PRE-INSTALL AND ALL EQUIPMENT AND CONDUCTORS PRIOR TO DISCONNECTION OF EXISTING SERVICES.
- ㊸ PROVIDE DEDICATED 20A, 1P CIRCUIT AND DUPLEX RECEPTACLE FOR TOWN RADIO EQUIPMENT. PROVIDE LABEL INDICATING RECEPTACLE IS FOR TOWN USE ONLY. COORDINATE LOCATION AND QUANTITY OF DUPLEX RECEPTACLES WITH CONSTRUCTION MANAGER.

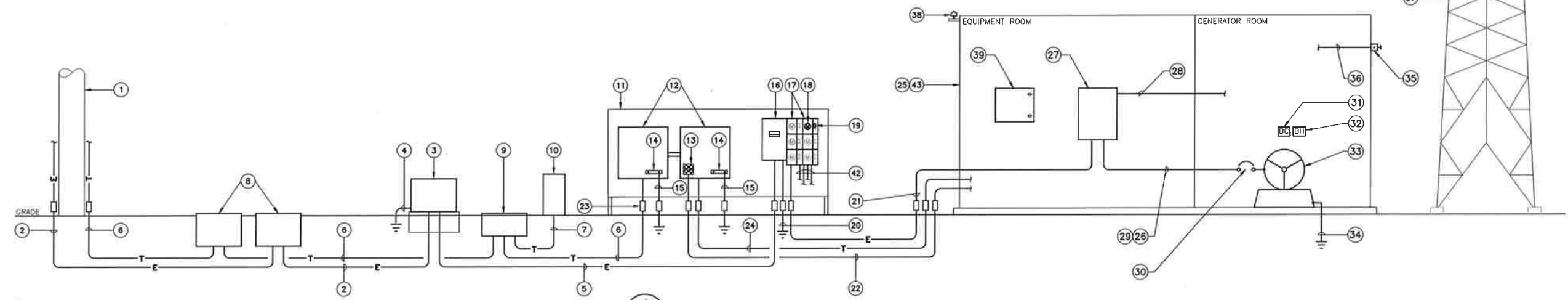
GENERAL NOTES

- 1. CONDUCTOR SIZES SHALL NOT BE REDUCED OR SUBSTITUTED WITHOUT ENGINEERS APPROVAL.
- 2. UNLESS OTHERWISE NOTED ALL CONDUCTORS AND CONDUCTOR TERMINATIONS SHALL BE RATED FOR MINIMUM 75 DEGREE C CONTINUOUS OPERATION.
- 3. COORDINATE WITH OWNER FOR ALL SHUTDOWNS.
- 4. COORDINATE ALL CONDUIT ROUTING IN THE FIELD WITH LANDLORD, CONSTRUCTION MANAGER, AND UTILITY COMPANIES.
- 5. RESTORE ALL DISTURBED AREAS TO PRE-CONSTRUCTION CONDITION.
- 6. ALL WORK SHALL BE IN ACCORDANCE WITH NEC REQUIREMENTS.
- 7. COORDINATE LOCATION AND MOUNTING REQUIREMENTS FOR ALL ELECTRICAL EQUIPMENT.
- 8. ALL CONDUITS SHALL HAVE EXPANSION COUPLINGS WHERE EXTENDING ABOVE GRADE.
- 9. ALL UTILITY SUPPLY CONDUITS, CONDUCTORS AND ASSOCIATED EQUIPMENT MUST BE LOCATED WITHIN THE LIMITS OF ASSOCIATED UTILITY EASEMENT. COORDINATE WITH OWNER FOR ALL EASEMENT DOCUMENTATION.
- 10. REFER TO SITE UTILITY PLAN.
- 11. TELEPHONE EQUIPMENT SHOWN APPROXIMATE. COORDINATE WITH TELEPHONE UTILITY COMPANY AND PROVIDE ALL SPECIFIED EQUIPMENT.
- 12. COORDINATE SERVICE EQUIPMENT INTERRUPTING RATING WITH AVAILABLE FAULT CURRENT FROM UTILITY COMPANY. EQUIPMENT SHALL NOT BE RATED LESS THAN 65 KAIC.
- 13. ALL TELEPHONE AND ELECTRIC UTILITY WORK MUST BE COORDINATED WITH UTILITY COMPANY, AND ALL EQUIPMENT MUST BE UTILITY COMPANY APPROVED. CONTRACTOR SHALL PROVIDE ALL ELEMENTS NOT PROVIDED BY UTILITY COMPANIES.
- 14. COORDINATE WITH CIVIL AND STRUCTURAL DRAWINGS FOR EXTERIOR WALL PENETRATION DETAILS. CONTRACTOR IS RESPONSIBLE FOR ENSURING ALL PENETRATIONS ARE THOROUGHLY WATERPROOF.
- 15. COORDINATE OUTAGES WITH ALL AFFECTED PARTIES, AND PROVIDE TEMPORARY POWER AS REQUIRED.

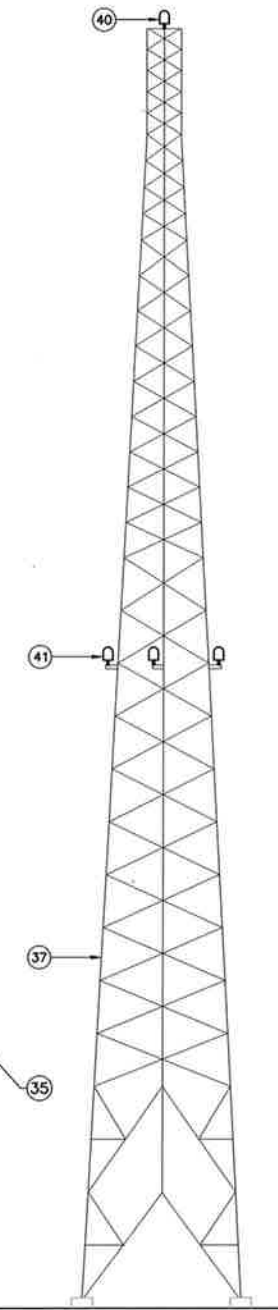
FAA LIGHTING NOTES

- 1. PROVIDE AND INSTALL AN FAA OBSTRUCTION LIGHTING SYSTEM WHICH SHALL BE A FLASH TECHNOLOGY MEDIUM INTENSITY DUAL LED VANGUARD-II FTS-370d SERIES LIGHTING SYSTEM CONSISTING OF A TOP MOUNTED L-864/L-865 DUAL RED/WHITE FLASHING LED BEACON, CONTROLLER WITH DRY CONTACTS FOR MONITORING, PHOTOCELL WITH PIGTAIL, AND (3) RED LED L-810 MARKER LIGHTS. PROVIDE CONNECTION CABLES FOR TOP BEACON AND MARKER LIGHTS. REFERENCE FLASH TECHNOLOGY QUOTATION # 2044695. FIELD VERIFY LENGTH OF CONNECTION CABLES AND PHOTOCELL PIGTAIL PRIOR TO ORDERING AND CONFIRM LIGHTING KIT WILL BE PROVIDED WITH ADEQUATE CABLE LENGTHS.
- 2. INSTALL CONTROLLER IN OWNER APPROVED LOCATION IN AVAILABLE SPACE ON WALL INSIDE VERIZON WIRELESS EQUIPMENT SHELTER.
- 3. PROVIDE DEDICATED 120V, 20A, 1P CIRCUIT FROM OWNER'S DISTRIBUTION PANEL IN SHELTER. PROVIDE ALL WIRING, CONDUIT, CIRCUIT BREAKER, MOUNTING, AND ASSOCIATED ACCESSORIES AND HARDWARE.
- 4. PROVIDE TOP OF TOWER BEACON MOUNT UNLESS PROVIDED BY TOWER MANUFACTURER.
- 5. INSTALL LIGHTING SYSTEM PER MANUFACTURERS SPECIFICATIONS.
- 6. INSTALLATION SHALL COMPLY WITH CURRENT FAA AERONAUTICAL STUDY FOR THIS TOWER. STUDY TO BE PROVIDED BY OWNER.
- 7. INSTALL ONE RED MARKER LIGHT ON EACH LEG OF TOWER IN LOCATION ON OUTER PERIMETER OF TOWER WITH UNOBSTRUCTED VIEW. INSTALL AT 125' HEIGHT ABOVE GRADE. ADJUST HEIGHT AS REQUIRED TO AVOID OBSTRUCTIONS.
- 8. INSTALL PHOTOCELL ON EXTERIOR OF SHELTER WITH UNOBSTRUCTED VIEW OF NORTHERN SKY.
- 9. PROVIDE ALL REQUIRED MOUNTING BRACKETS FOR BEACON, MARKER LIGHTS, PHOTOCELL, AND CONTROLLER.
- 10. PROVIDE ALL HARDWARE FOR ANCHORING AND SUPPORTING CABLES ON TOWER, ICE BRIDGE, AND IN SHELTER.
- 11. PROVIDE WIRING FOR INTERCONNECTION OF CONTROLLER ALARM CONTACTS TO OWNER'S ALARM PANEL IN SHELTER.
- 12. PROVIDE SYSTEM GROUNDING CONNECTIONS AS REQUIRED BY MANUFACTURER.

VERIFY ALL SHELTER DIMENSIONS, EQUIPMENT DIMENSIONS, EQUIPMENT LOCATIONS AND UTILITY OPENINGS WITH BUILDING SHOP DRAWINGS PRIOR TO COMMENCEMENT OF WORK.



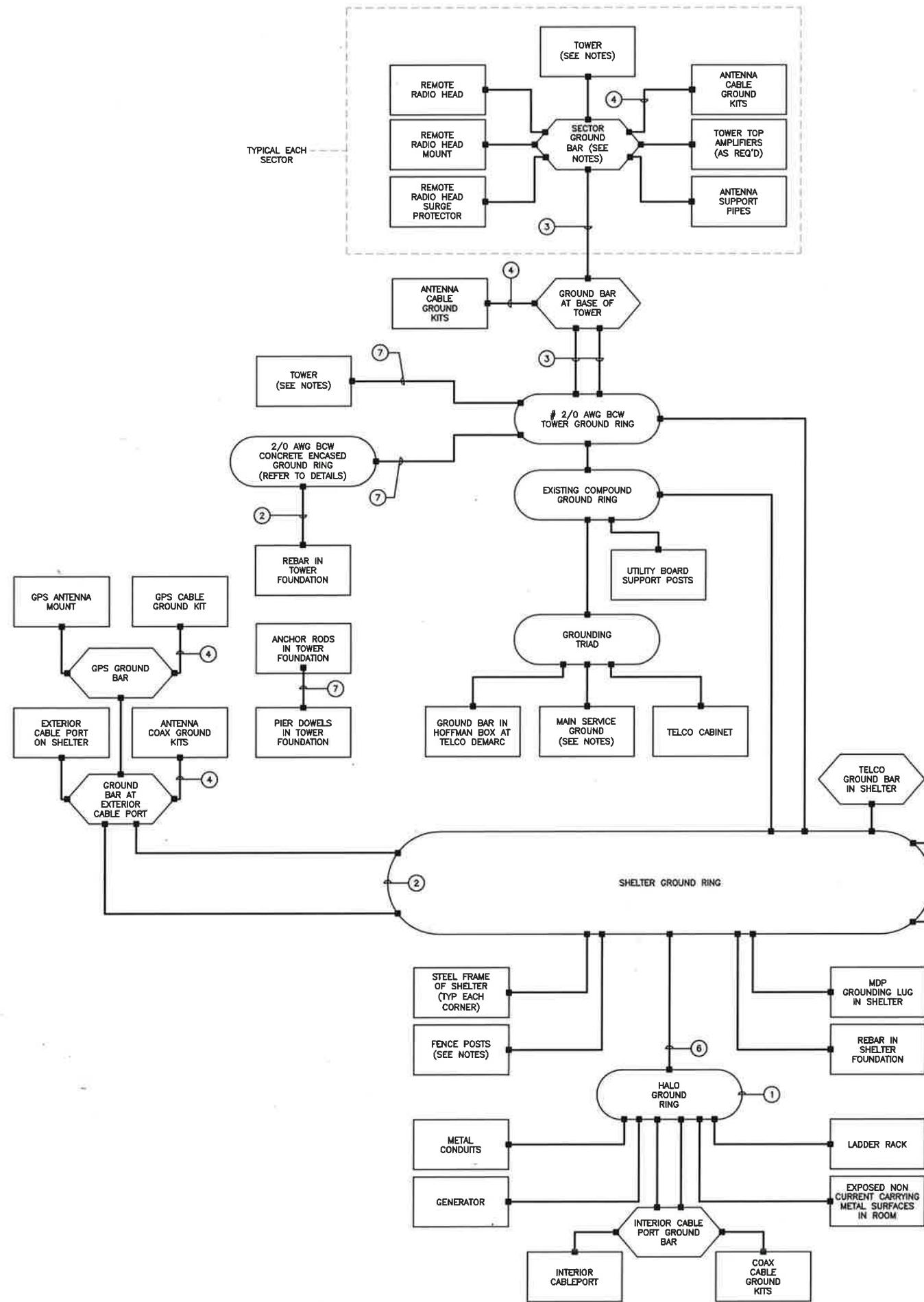
1 RISER DIAGRAM
E-3 NOT TO SCALE



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 SCALE: AS NOTED
 JOB NO. 14124.000
 RISER DIAGRAM AND NOTES
E-3
 Sheet No. 15 of 24



GROUNDING SCHEMATIC NOTES

- ① #2 AWG GREEN INSULATED.
 - ② BOND WITH LISTED MECHANICAL CONNECTION.
 - ③ #2/0 GREEN INSULATED.
 - ④ #6 AWG.
 - ⑤ REFER TO RISER DIAGRAM FOR SPECIFICATIONS.
 - ⑥ BOND ALL HALO GROUND RING TAILS TO GROUND RING. COORDINATE LOCATION AND QUANTITY WITH EQUIPMENT ROOM/SHELTER DRAWINGS.
 - ⑦ FOUR #2/0 GREEN INSULATED.
 - ⑧ BOND FAA LIGHTING SYSTEM TO GROUND PER MFG SPECIFICATIONS.
 - ⑨ REFER TO ELECTRICAL WORK NOTES ON SHEET E-2.
- GENERAL NOTES:**
1. ALL SURGE SUPPRESSION EQUIPMENT SHALL BE BONDED TO GROUND PER MANUFACTURER'S SPECIFICATIONS.
 2. GROUND CONDUCTORS SHOWN SHALL BE #2 AWG SOLID TINNED BCW UNLESS OTHERWISE NOTED OR REQUIRED BY CODE.
 3. BOND CABLE TRAY AND ICE BRIDGE SECTIONS TOGETHER WITH #6 AWG STRANDED GREEN INSULATED JUMPERS.
 4. ALL SECTOR GROUND BARS SHALL BE BONDED TOGETHER WITH #2 AWG SOLID TINNED BCW.
 5. BOND ALL EQUIPMENT CABINETS AND BATTERY CABINETS TO GROUND PER MANUFACTURER'S SPECIFICATIONS.
 6. ALL BONDS TO TOWER SHALL BE MADE IN STRICT ACCORDANCE WITH SPECIFICATIONS OF TOWER MANUFACTURER OR STRUCTURAL ENGINEER.
 7. REFER TO GROUNDING PLAN FOR LOCATION OF GROUNDING DEVICES.
 8. REFER TO ALL ELECTRICAL AND GROUNDING DETAILS.
 9. COORDINATE ALL TOWER MOUNTED EQUIPMENT WITH OWNER.
 10. ALL TOWER MOUNTED AMPLIFIERS AND ASSOCIATED EQUIPMENT SHALL BE BONDED TO THE SECTOR GROUND BAR PER MANUFACTURER'S SPECIFICATIONS.
 11. ALL FENCE POSTS WITHIN 6' OF EQUIPMENT SHELTER SHALL BE BONDED TO GROUND RING.
 12. ALL GROUNDING SHALL BE IN ACCORDANCE WITH NEC AND OWNER'S REQUIREMENTS.
 13. ALL EXPOSED METAL OBJECTS IN SHELTER SHALL BE BONDED TO THE HALO GROUND WITHIN THAT ROOM.
 14. BOND GENERATOR TO GROUND PER NEC AND MANUFACTURERS SPECIFICATIONS.
 15. REFER TO RISER DIAGRAM FOR SPECIFICATIONS OF SERVICE GROUND AND TRANSFORMER GROUND.
 16. COORDINATE WITH TOWER INSTALLATION DRAWINGS AND SPECIFICATIONS FOR ADDITIONAL TOWER MFG GROUNDING, BONDING AND LIGHTNING PROTECTION REQUIREMENTS.

CELLULAR GROUNDING NOTES

OBJECTIVE
 PROVIDE A CELLULAR GROUNDING SYSTEM WITH MAXIMUM ALTERNATING CURRENT RESISTANCE OF 5 OHMS BETWEEN ANY POINT ON THE GROUNDING SYSTEM AND REFERENCE GROUND. PROVIDE EXTERIOR GROUNDING SCHEME WITH OWNER'S ENGINEER APPROVAL AS REQUIRED TO ACHIEVE DESIRED MAXIMUM AC RESISTANCE TO GROUND.

TESTING
 CONTRACTOR TO PROVIDE AN INDEPENDENT TESTING CONTRACTOR TO DETERMINE THE GROUNDING SYSTEM RESISTANCE BY USE OF THE THREE POINT TEST AND AN AEMC MODEL 4500, OR APPROVED EQUAL. TEST TO BE PERFORMED PRIOR TO CONNECTION OF POWER SUPPLY TO THE CELL SITE AND CONNECTION OF THE GROUNDING SYSTEM TO THE WATER MAIN OR AC SUPPLY AS APPLICABLE.

CONDUCTOR USED FOR CELLULAR GROUNDING SYSTEM
 EGR - #2 AWG ANNEALED SOLID TINNED BARE COPPER
 IGR - #2 AWG ANNEALED STRANDED (7 STRAND) THW GREEN COLORED INSULATION
 INTER-BUS EXTENSION (FROM IGR TO EGR) - SEE DETAILS
 EXTERNAL BOND CONNECTIONS TO EGR - #2 ANNEALED SOLID TINNED BARE COPPER
 INTERIOR BOND CONNECTIONS TO IGR - #6 ANNEALED STRANDED (7 STRAND) THW GREEN COLORED INSULATION

MINIMUM BENDING RADIUS
 IGR #2 : 1'-0" NOMINAL AND 8" MINIMUM
 EGR #2 : 2'-0" NOMINAL AND 8" MINIMUM
 CELLULAR GROUNDING CONDUCTOR SHALL BE AS STRAIGHT AS POSSIBLE WITH MINIMUM 6" BENDING RADIUS.

FASTENER FOR CELLULAR GROUNDING CONDUCTOR
 USE NON-METALLIC FASTENER AND STANDOFF 'CLIC' (AVAIL FROM NEFCO 203-289-0285) TO SURFACE SUPPORT CONDUCTOR 3" AWAY FROM SURFACES.
 SPACING OF FASTENERS: 2'-0" O.C. OUTSIDE BUILDING
 3'-0" O.C. INSIDE BUILDING

GROUNDING ELECTRODE
 GROUNDING ELECTRODE SHALL BE 5/8" DIA. x 10'-0" L. COPPER CLAD STEEL ROD. ADJUST LOCATION OF GROUNDING ELECTRODE IF SOIL CONDITION IS NOT CONDUCTIVE (GRAVEL, SANDY SOIL, ROCKS). SPACE GROUNDING ELECTRODES 20'-0" APART (SPACING MAY BE REDUCED WHERE REQUIRED TO ACCOMMODATE FIELD CONDITIONS BUT SHALL NOT BE LESS THAN 10'-0"). ELECTRODES SHALL BE DRIVEN ONLY WITH PROPER DRIVER SLEEVE TO PREVENT MUSHROOMING TOP OF ROD. WHEN ROCK BOTTOM IS ENCOUNTERED, THE ELECTRODE SHALL BE DRIVEN AT AN OBLIQUE ANGLE NOT TO EXCEED 45° FROM THE VERTICAL AWAY FROM STRUCTURES. TOP OF GROUNDING ELECTRODE SHALL BE MIN. 3'-6" BELOW FINISH GRADE.

CONNECTIONS ABOVE GRADE (MECHANICAL)
 COMPRESSION LUG CONNECTOR - 15 TON COMPRESSION, 2 HOLE, LONG BARREL, ELECTRO TINNED PLATED, HIGH CONDUCTIVITY, COPPER 600V RATED. USE 1/4" Ø BOLT, 3/4" SPACING LUGS TO BOND OBJECTS FROM THE IGR. (CONNECTOR SHALL BE BURNDY HYLUG SERIES OR EQUAL.)
 EXOTHERMIC WELD LUG CONNECTOR - 2 HOLE, OFFSET, ELECTRO TINNED PLATED, HIGH CONDUCTIVITY, COPPER 600V. USE 1/2" Ø BOLT, 1-3/4" SPACING LUGS. CONNECTOR SHALL BE CADWELD CONNECTION STYLE (CABLE TO SURFACE) TYPE LA, LUG SIZE 1/8 x 1. EXOTHERMIC WELD TO LUG AS REQUIRED.
 C-TAP COMPRESSION CONNECTOR - HIGH CONDUCTIVITY COPPER FOR MAIN TO BRANCH LINE TAPPING. (CONNECTOR SHALL BE BURNDY HYTAP SERIES OR EQUAL.)

MECHANICAL CONNECTIONS
 USE MATCHING MANUFACTURER TOOL AND DIE FOR COMPRESSION CONNECTION.
 APPLY ANTI-OXIDANT CONDUCTIVITY ENHANCER COMPOUND ON SURFACES THAT ARE COMPRESSED.
 SURFACES INTENDED TO BE CONNECTED WITH MECHANICAL CONNECTORS SHALL BE BARE METAL TO BARE METAL PRIME AND PAINT OVER BONDED AREA TO PREVENT CORROSION.




WHEN BONDING #2 TO #2
 EXTERIOR OF BUILDING - USE EXOTHERMIC WELD CONNECTION
 INTERIOR OF BUILDING - USE COMPRESSION CONNECTION ON STRANDED CONDUCTORS ONLY.
 - USE EXOTHERMIC WELD CONNECTION ON SOLID CONDUCTOR.

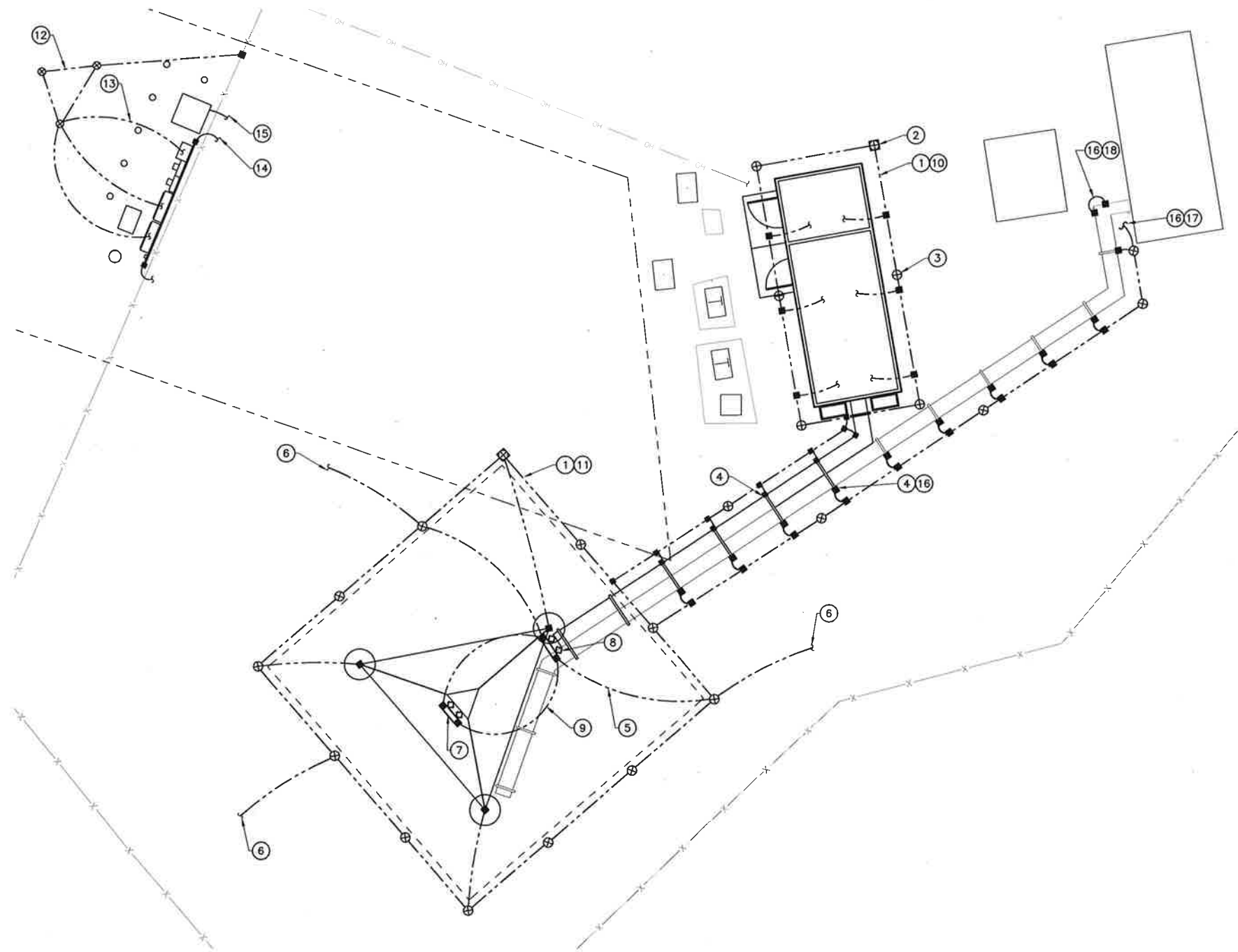
WHEN BONDING #2 TO FENCE POST
 USE EXOTHERMIC WELD 'CADWELD TYPE VS' CONNECTION TO FENCE POST STEEL SURFACE. TEST WELD FOR POSSIBLE BURN THRU. PATCH WELDED AREA WITH GALVANIZED COATING AS REQUIRED FOR PROPER WELDED PERMANENT BOND. REFER TO MANUFACTURER'S REQUIREMENTS FOR DETAILS.

GROUNDING SYSTEM INTERCONNECTION
 BOND THE EGR DOWN CONDUCTORS, AND/OR BURIED GROUND RING TO ANY METALLIC OBJECT OR EXISTING GROUNDING SYSTEM WITHIN 6'.

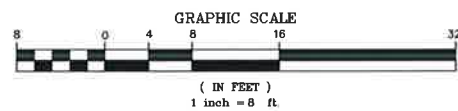
WHEN BONDING #2 TO TOWER GROUND PLATE
 TOWER GROUND PLATE SHALL BE 6" x 8" x 1/4" COPPER AND BE MADE AVAILABLE TO TOWER CONTRACTOR TO BE INSTALLED DURING TOWER CONSTRUCTION. USE EXOTHERMIC WELD 'CADWELD TYPE HS' TO TOWER GROUND PLATE TEST WELD FOR POSSIBLE BURN THRU. COORDINATE THE SIZE OF THE MOUNTING HOLE WITH TOWER CONTRACTOR.

METALLIC CONDUITS
 BOND ALL STEEL CONDUITS TO PANELS AT POINT OF CONTACT WITH APPROVED GROUNDING BUSHING.

| | |
|--|--|
|  | ISSUED FOR CONSTRUCTION DRAWN BY: CRY'D BY DATE: 07/09/15 RESY. |
|  |  |
|  | Ashford ReLo, CT 353 PUMPKIN HILL ROAD ASHFORD, CT 06278 (203) 498-0360 (203) 498-0367 Fax 852 Northford Road Northford, CT 06446 www.CentekEng.com |
| Verizon Wireless WIRELESS COMMUNICATIONS FACILITY ASHFORD RELO, CT 353 PUMPKIN HILL ROAD ASHFORD, CT 06278 | |
| DATE: 05/11/15 SCALE: AS NOTED JOB NO. 14124.000 | |
| SCHEMATIC DIAGRAM AND NOTES | |
| E-4 Sheet No. 16 of 24 | |



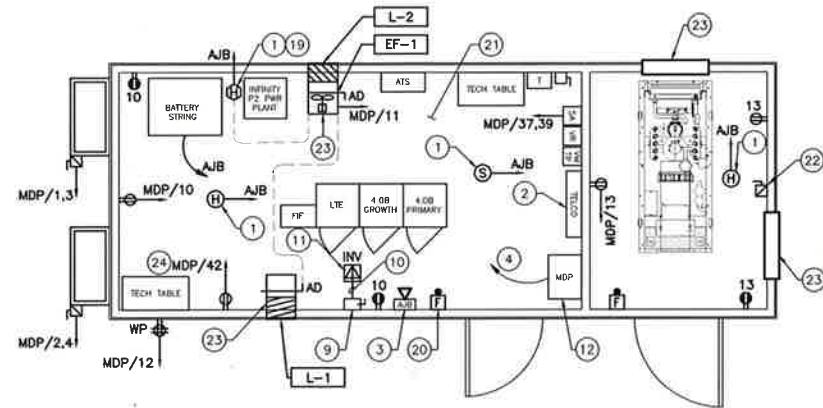
1 COMPOUND GROUNDING PLAN
E-5 SCALE: 1/8" = 1'-0"



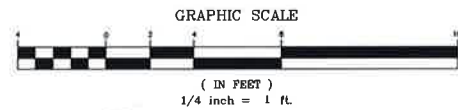
GROUNDING PLAN NOTES

- ① PROVIDE COMPLETE GROUNDING SYSTEM TESTING (INCLUDING NEW AND EXISTING) PER SPECIFICATIONS.
- ② GROUNDING ROD WITH ACCESS (TYP.) PER DETAILS.
- ③ GROUNDING ROD (TYP.) PER DETAILS.
- ④ ICE BRIDGE POST AND COVER. BOND EACH SECTION AND SUPPORT TO GROUND RING PER DETAILS.
- ⑤ BOND GROUND BAR TO NEW TOWER GROUND RING (TYP OF 2). CONTRACTOR TO VERIFY LOCATION IN FIELD.
- ⑥ BOND TO EXISTING COMPOUND GROUND RING.
- ⑦ UPPER TOWER MOUNTED GROUND BAR PER DETAILS.
- ⑧ LOWER TOWER MOUNTED GROUND BAR PER DETAILS.
- ⑨ BOND UPPER TOWER MOUNTED GROUND BAR TO LOWER TOWER MOUNTED GROUND BAR (2 GROUND LEADS) PER DETAILS.
- ⑩ #2 AWG SOLID TINNED BARE COPPER WIRE GROUND RING. TYPICAL, UNLESS OTHERWISE NOTED.
- ⑪ #2/0 TOWER GROUND RING. (COORDINATE WITH TOWER FOUNDATION)
- ⑫ GROUNDING TRIAD. BOND TO GROUND RING.
- ⑬ 4/0 AWG. MAIN SERVICE GROUNDING ELECTRODE CONDUCTOR.
- ⑭ BOND NEW UTILITY BACKBOARD TO EXISTING GROUND RING.
- ⑮ PROVIDE TRANSFORMER GROUNDING PER UTILITY COMPANY SPECIFICATIONS.
- ⑯ SHOWN FOR REFERENCE ONLY. COORDINATE WITH ICE BRIDGE USER AND PROVIDE ANY ADDITIONAL GROUNDING TO MEET THEIR SPECIFICATIONS.
- ⑰ CONNECT NEW ICE BRIDGE GROUNDING TO EXISTING ICE BRIDGE GROUNDING.
- ⑱ BOND NEW ICE BRIDGE TO EXISTING.

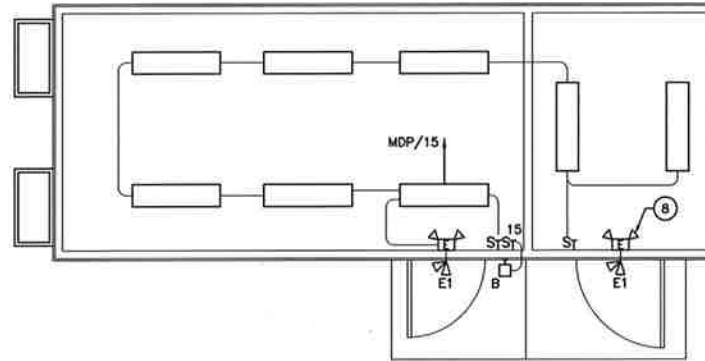
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| | | | | | | | |
| ASHFORD RELO., CT WIRELESS COMMUNICATIONS FACILITY 353 PUMPKIN HILL ROAD ASHFORD, CT 06278 | | | | | | | |
| DATE: 05/11/15 | | SCALE: AS NOTED | | JOB NO. 14124.000 | | GROUNDING PLAN AND NOTES | |
| E-5 | | | | | | | |
| Sheet No. 17 of 24 | | | | | | | |



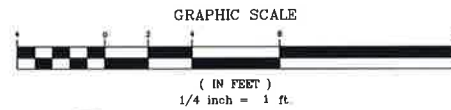
NOTE:
ROOM LAYOUT AND EQUIPMENT ARRANGEMENT ARE SHOWN TYPICAL. REFER TO CIVIL DRAWINGS FOR EXACT ROOM LAYOUT. ADJUST EQUIPMENT LOCATIONS AS REQUIRED FOR BEST FIT, CODE COMPLIANCE, AND TO AVOID OBSTRUCTIONS. FINAL EQUIPMENT LAYOUT MUST BE VERIFIED AND APPROVED BY WIRELESS CARRIER'S CONSTRUCTION MANAGER PRIOR TO INSTALLATION.



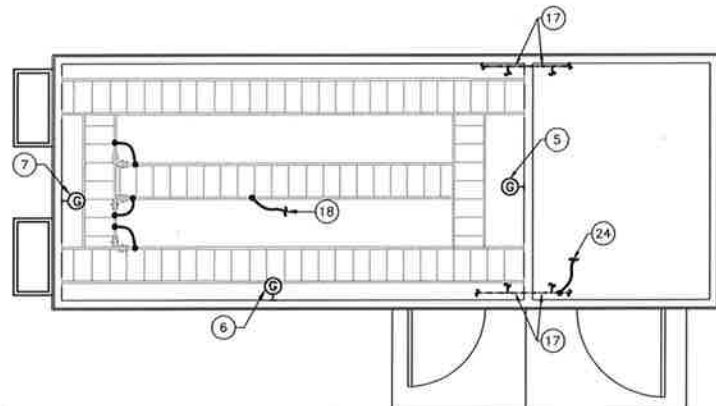
1 POWER PLAN
E-6 SCALE: 1/4" = 1'-0"



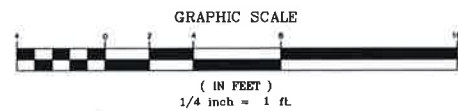
NOTE:
ROOM LAYOUT AND EQUIPMENT ARRANGEMENT ARE SHOWN TYPICAL. REFER TO CIVIL DRAWINGS FOR EXACT ROOM LAYOUT. ADJUST EQUIPMENT LOCATIONS AS REQUIRED FOR BEST FIT, CODE COMPLIANCE, AND TO AVOID OBSTRUCTIONS. FINAL EQUIPMENT LAYOUT MUST BE VERIFIED AND APPROVED BY WIRELESS CARRIER'S CONSTRUCTION MANAGER PRIOR TO INSTALLATION.



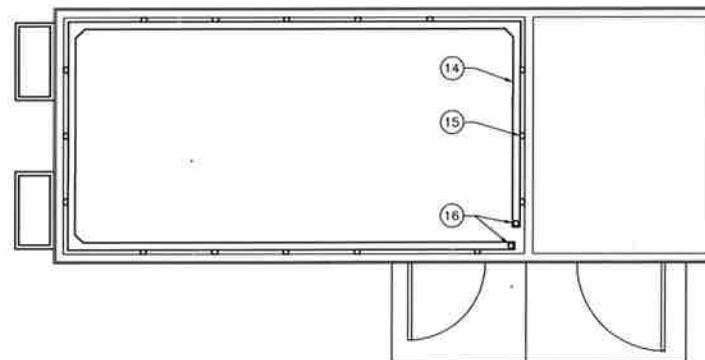
2 LIGHTING PLAN
E-6 SCALE: 1/4" = 1'-0"



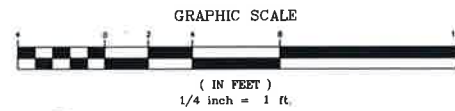
NOTE:
ROOM LAYOUT AND EQUIPMENT ARRANGEMENT ARE SHOWN TYPICAL. REFER TO CIVIL DRAWINGS FOR EXACT ROOM LAYOUT. ADJUST EQUIPMENT LOCATIONS AS REQUIRED FOR BEST FIT, CODE COMPLIANCE, AND TO AVOID OBSTRUCTIONS. FINAL EQUIPMENT LAYOUT MUST BE VERIFIED AND APPROVED BY WIRELESS CARRIER'S CONSTRUCTION MANAGER PRIOR TO INSTALLATION.



3 CABLE TRAY GROUNDING PLAN
E-6 SCALE: 1/4" = 1'-0"



NOTE:
ROOM LAYOUT AND EQUIPMENT ARRANGEMENT ARE SHOWN TYPICAL. REFER TO CIVIL DRAWINGS FOR EXACT ROOM LAYOUT. ADJUST EQUIPMENT LOCATIONS AS REQUIRED FOR BEST FIT, CODE COMPLIANCE, AND TO AVOID OBSTRUCTIONS. FINAL EQUIPMENT LAYOUT MUST BE VERIFIED AND APPROVED BY WIRELESS CARRIER'S CONSTRUCTION MANAGER PRIOR TO INSTALLATION.



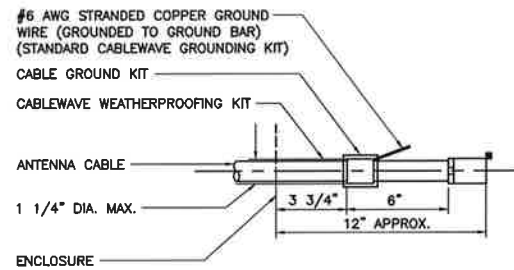
4 WIREWAY LAYOUT PLAN
E-6 SCALE: 1/4" = 1'-0"

ELECTRICAL WORK NOTES

- 1 ALL SMOKE, HEAT AND HYDROGEN DETECTORS SHALL BE OPERATE AT 48 VDC AND BE POWERED FROM THE 48 VDC POWER PLANT WITHIN THE EQUIPMENT ROOM. DO NOT MOUNT ABOVE CABLE TRAY.
- 2 TELEPHONE BACKBOARD AREA.
- 3 ALARM JUNCTION BOX.
- 4 PROVIDE CONDUCTORS FROM PANELBOARD MDP ROUTED THROUGH THE PERIMETER WIREWAY FOR RECTIFIER BRANCH CIRCUITS. PROVIDE 20' OF ADDITIONAL WIRING IN 1" FLEXIBLE METAL CONDUIT FOR FINAL TERMINATION BY OWNER.
- 5 TELCO GROUND BAR. (COORDINATE LOCATION WITH WIRELESS CARRIER'S CONSTRUCTION MANAGER.)
- 6 MAIN GROUND BAR. (COORDINATE LOCATION WITH WIRELESS CARRIER'S CONSTRUCTION MANAGER.)
- 7 GROUND BAR AT CABLE PORT. (COORDINATE LOCATION WITH WIRELESS CARRIER'S CONSTRUCTION MANAGER.)
- 8 CONNECT EMERGENCY LIGHT BRANCH CIRCUIT WIRING TO LINE SIDE OF LIGHTING CIRCUIT.
- 9 TO POWER BOARD (2) #8 AWG WHIP CABLE.
- 10 BATTERY DISCONNECT.
- 11 2400 WATT INVERTER (24VDC/120VAC) MANUFACTURED BY TRIPP-LITE MODEL #PV2400FC OR APPROVED EQUAL (TELCO, CARDS AND EXHAUST FAN).
- 12 INTEGRATED LOAD CENTER "MDP". REFER TO PANEL SCHEDULE.
- 13 VERIFY ELECTRICAL REQUIREMENT WITH AHU MANUFACTURER AND MECHANICAL DRAWINGS.
- 14 4" x 4" TYPE 1 CONTINUOUS SCREW COVER WIREWAY MOUNTED ALONG PERIMETER OF ROOM AGAINST CEILING.
- 15 SUPPORT BRACKET/SPACER (TYPICAL) (INSTALL AS REQUIRED).
- 16 (2) 3" CONDUITS CONNECTED TO PANELBOARD, MDP FROM WIREWAYS.
- 17 INSTALL HALO GROUND NEAR CEILING ALONG PERIMETER OF ROOM. INSTALL PER VERIZON WIRELESS SPECIFICATIONS AND THE DETAILS ON THESE PLANS.
- 18 BOND TO MAIN GROUND BAR.
- 19 HYDROGEN DETECTOR TO INTERFACE WITH EXHAUST FAN CONTROLS. REFER TO MECHANICAL PLANS.
- 20 AUDIO VISUAL FIRE ALARM DEVICE SHALL BE TIED DIRECTLY TO HOST BUILDING FIRE ALARM SYSTEM. THIS SHALL BE INDEPENDENT OF THE DEVICES ASSOCIATED WITH FM-200 SYSTEM.
- 21 PROVIDE 20A CIRCUIT AND WIRING REQUIRED FOR FM-200 SYSTEM. SEE FIRE PROTECTION DRAWING FOR MORE INFORMATION.
- 22 PRIOR TO START OF CONSTRUCTION ALL EXISTING ELECTRICAL EQUIPMENT DEVICES, CONDUIT, RACEWAY, LIGHTING CONTROLS, FIRE ALARM, J-BOXES, ETC. SHALL BE REMOVED AND RELOCATED OUTSIDE OF THE EQUIPMENT ROOM AREA. NEW LOCATIONS SHALL BE COORDINATED WITH BUILDING OWNER. ANY DEVICE REMOVED BUT NOT RELOCATED SHALL BE RETURNED TO BUILDING OWNER.
- 23 COORDINATE WITH MECHANICAL PLANS FOR CONTROL REQUIREMENTS OF EXHAUST FAN AND INTAKE LOUVER.
- 24 RECEPTACLE FOR TOWN EQUIPMENT COORDINATE LOCATION WITH CONSTRUCTION MANAGER. REFER TO RISER DIAGRAM FOR ADDITIONAL INFORMATION.

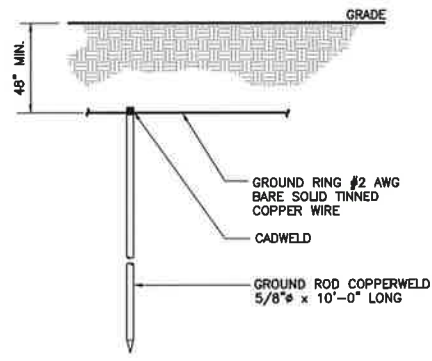
- GENERAL NOTES:**
1. REFER TO PANEL SCHEDULE FOR ADDITIONAL INFORMATION.
 2. INSTALL ALL ALARM WIRING FOR PROPER OPERATION. COORDINATE ALL REQUIREMENTS WITH WIRELESS CARRIER'S CONSTRUCTION MANAGER.
 3. COORDINATE ALL CONDUITS AND CEILING MOUNTED DEVICES WITH STRUCTURAL OBSTRUCTIONS.

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| | | | ASHFORD RELO., CT WIRELESS COMMUNICATIONS FACILITY 353 PUMPKIN HILL ROAD ASHFORD, CT 06278 | | DATE: 05/11/15 SCALE: AS NOTED JOB NO. 14124.000 | E-6 Sheet No. 18 of 24 | ISSUED FOR CONSTRUCTION DRAWN BY: CHFD DATE: 07/09/15 |



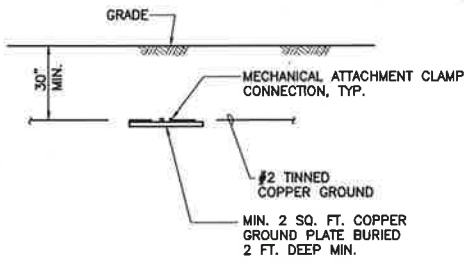
NOTE:
1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO GROUND BAR.

1 ANTENNA CABLE GROUNDING DETAIL
E-8 NOT TO SCALE



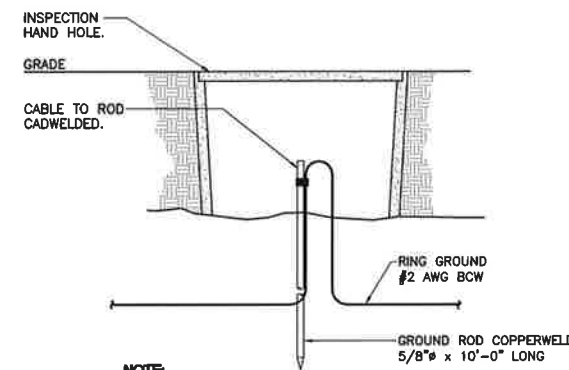
NOTE:
1. USE GROUND PLATE DETAIL IF 10 FT. GROUND ROD DEPTH CANNOT BE ACHIEVED DUE TO LEDGE CONDITION OR IF EXISTING TOWER FOUNDATION IS ENCOUNTERED.

2 GROUND ROD DETAIL
E-8 NOT TO SCALE



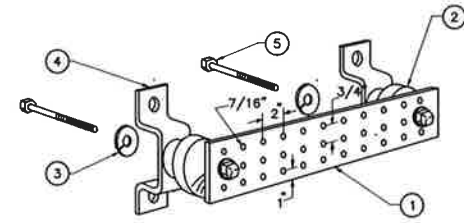
NOTE:
1. GROUND PLATE DETAIL TO BE USED ONLY IF 10 FT. GROUND ROD DEPTH CANNOT BE ACHIEVED DUE TO LEDGE CONDITION OR IF EXISTING TOWER FOUNDATION IS ENCOUNTERED.

2A GROUND PLATE DETAIL
E-8 NOT TO SCALE



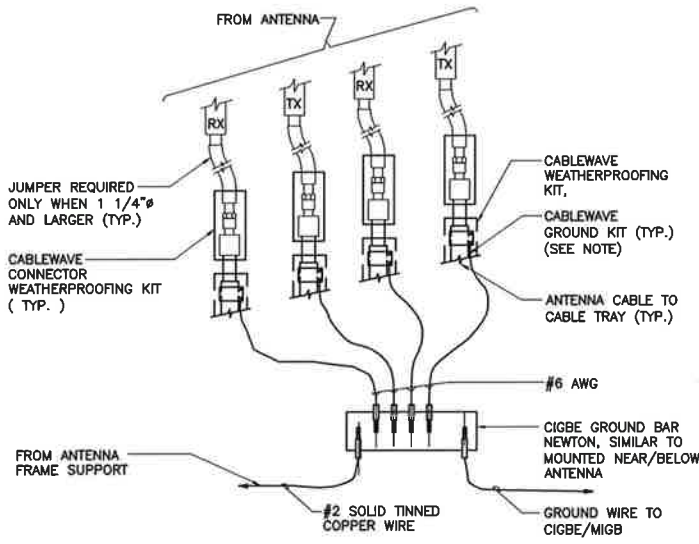
NOTE:
1. INSPECTION HAND HOLE MAY BE CONCRETE OR PVC AND SHALL BE A MINIMUM OF 12\"/>

3 GROUND ROD WITH ACCESS DETAIL
E-8 NOT TO SCALE



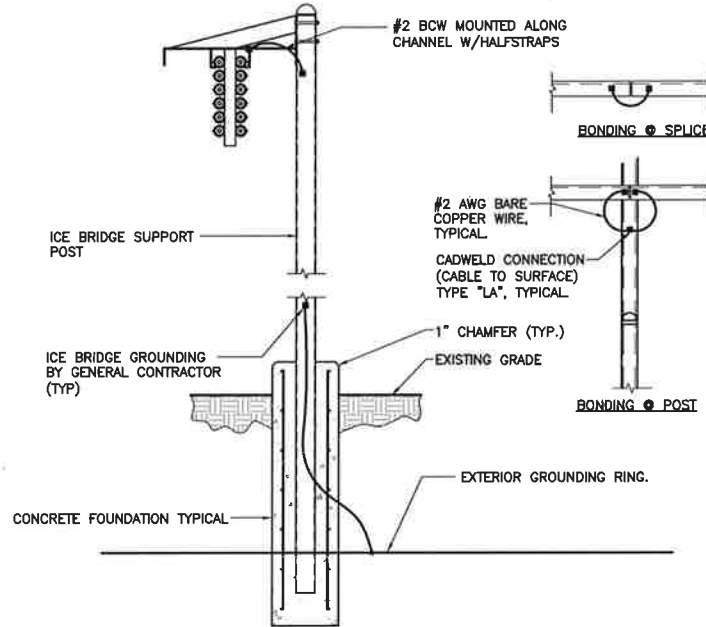
NOTES
① TINNED COPPER GROUND BAR, 1/4\"/>

4 GROUND BAR DETAIL
E-8 NOT TO SCALE

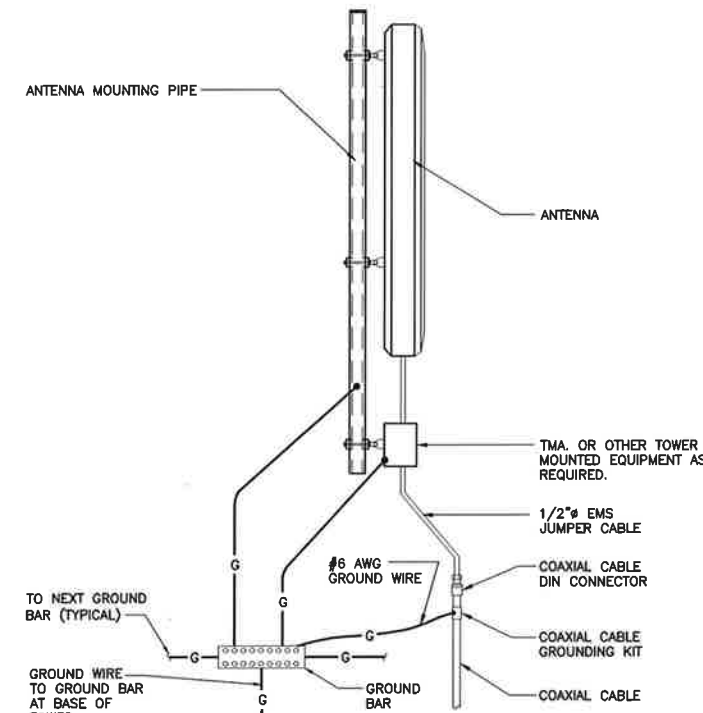


NOTE:
1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

5 CONNECTION OF GROUND WIRES TO GROUND BAR
E-8 NOT TO SCALE

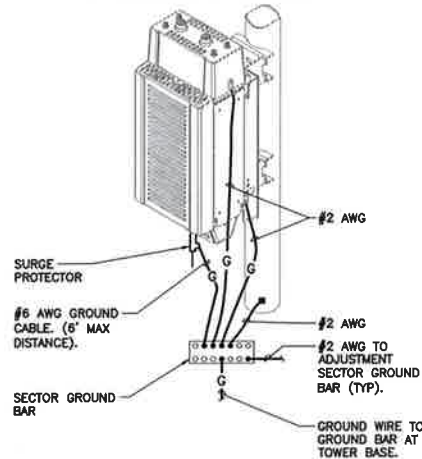


6 ICE BRIDGE BONDING DETAIL
E-8 NOT TO SCALE

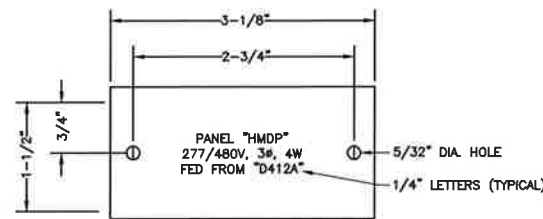


7 TYPICAL ANTENNA GROUNDING DETAIL
E-8 NOT TO SCALE

EACH RRH CABINET SHALL BE GROUNDED IN THE FOLLOWING MANNER:
1. AT TOP OF THE CABINET
2. AT RIGHT SIDE OF THE CABINET.



8 RRH POLE MOUNT GROUNDING
E-8 NOT TO SCALE



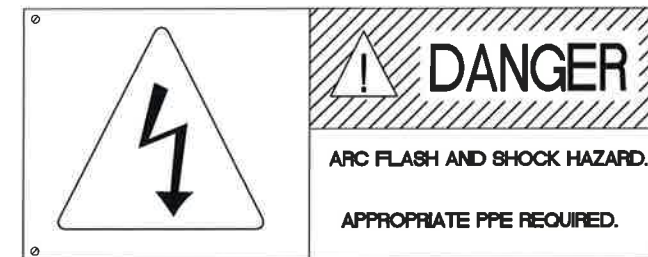
NOTES:
1. REFER TO SPECIFICATIONS FOR ADDITIONAL NAMEPLATE REQUIREMENTS.
2. NAMEPLATE TO BE 1/16\"/>

9 DETAIL OF TYPICAL NAMEPLATE
E-8 NOT TO SCALE



NOTES:
1. REFER TO SPECIFICATIONS FOR ADDITIONAL NAMEPLATE REQUIREMENTS.
2. PROVIDE WARNING LABEL ON ALL SERVICE EQUIPMENT IN ACCORDANCE WITH 2011 NEC 110.24.

10 DETAIL OF TYPICAL FAULT CURRENT SIGN
E-8 NOT TO SCALE



NOTES:
1. REFER TO SPECIFICATIONS FOR ADDITIONAL NAMEPLATE REQUIREMENTS.
2. PROVIDE WARNING LABEL ON ALL SWITCHBOARDS, DISTRIBUTION PANELS, PANELBOARDS IN ACCORDANCE WITH 2005 NEC 110.16.

11 DETAIL OF TYPICAL FLASH PROTECTION WARNING SIGN
E-8 NOT TO SCALE

| REV. | DATE | BY | DESCRIPTION |
|------|----------|------|-------------------------|
| 0 | 07/09/15 | J.B. | DRAWN BY C&D BY |
| | | | ISSUED FOR CONSTRUCTION |



Cellco Partnership
d.b.a. verizon wireless

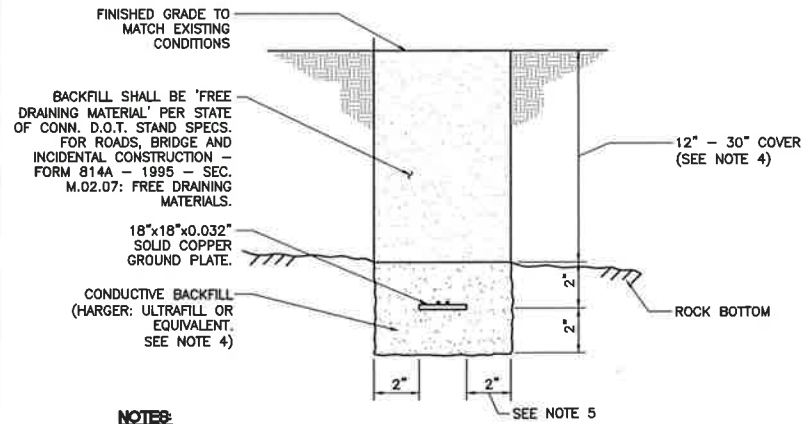
CENtek Engineering
Centers on Solutions
203-498-0380
203-498-0397 Fax
352 North Main Road
Bridford, CT 06808
www.CentekEng.com

Verizon Wireless
WIRELESS COMMUNICATIONS FACILITY
ASHFORD RELO, CT
353 PUMPKIN HILL ROAD
ASHFORD, CT 06278

DATE: 05/11/15
SCALE: AS NOTED
JOB NO. 14124.000

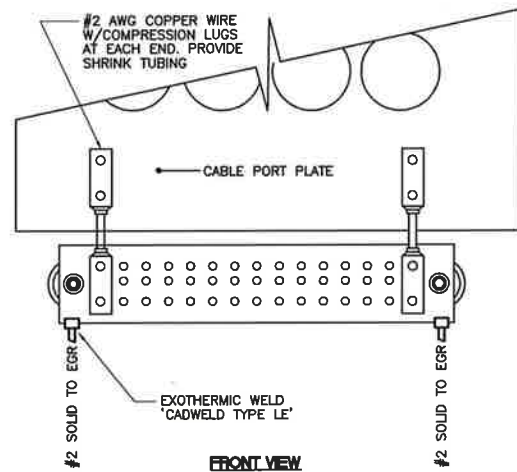
DETAILS

E-8

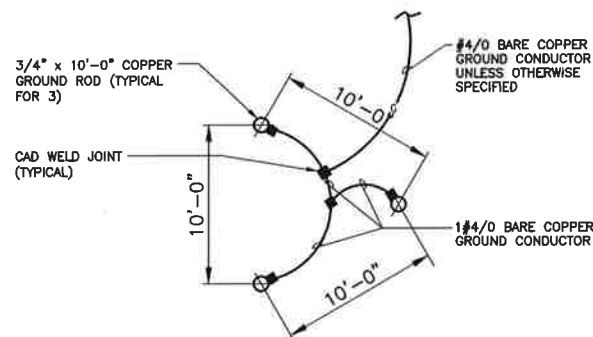


- NOTES:**
- ENGINEER SHALL INSPECT PLACEMENT OF EGR CONDUCTOR PRIOR TO BACKFILLING.
 - MAINTAIN MIN. 2'-0" LINEAR CLEARANCE BETWEEN BACKFILL AND THE FOLLOWING: FOUNDATION, UNDERGROUND PIPING/CONDUIT, UNDERGROUND SERVICES. IN THE CLEARANCE AREAS, USE EARTH BACKFILL INSTEAD.
 - EXERCISE HANDLING AND USE PRECAUTION OF BACKFILL MATERIAL PER MFR'S REQUIREMENTS.
 - FOR LOCATIONS WHERE ROCK BOTTOM DEPTH IS LESS THAN 12" CONDUCTIVE CONCRETE SHALL BE USED INSTEAD OF CONDUCTIVE BACKFILL.
 - PROVIDE MIN 2" CLEARANCE ON ALL SIDES OF GROUND PLATE.

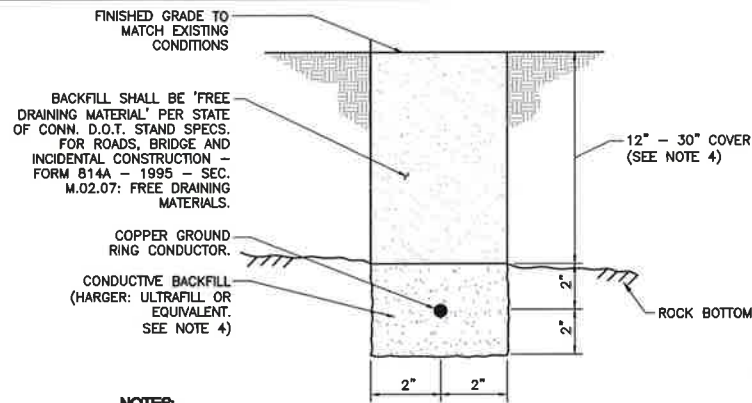
6 GROUND PLATE TRENCH/BACKFILL DETAIL (SHALLOW TOPSOIL)
E-9 NOT TO SCALE



4 CABLEPORT GROUND BAR LUG CONNECTION
E-9 NOT TO SCALE

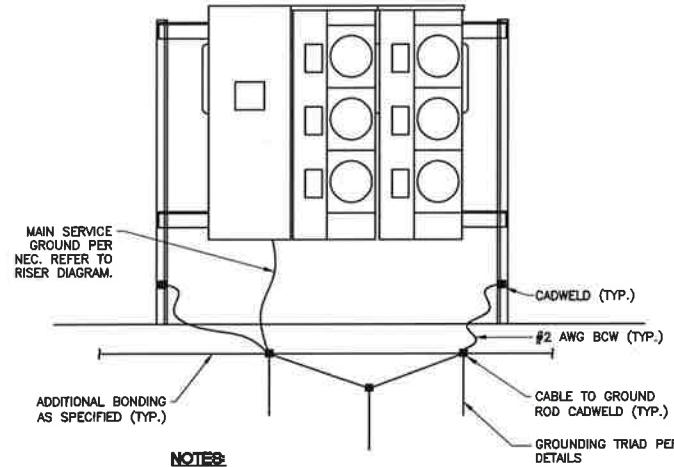


5 GROUND TRIAD DETAIL
E-9 NOT TO SCALE



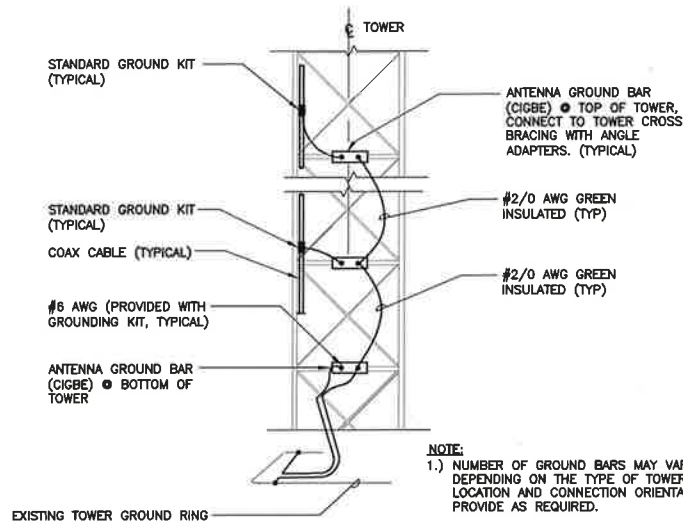
- NOTES:**
- ENGINEER SHALL INSPECT PLACEMENT OF EGR CONDUCTOR PRIOR TO BACKFILLING.
 - MAINTAIN MIN. 2'-0" LINEAR CLEARANCE BETWEEN BACKFILL AND THE FOLLOWING: FOUNDATION, UNDERGROUND PIPING/CONDUIT, UNDERGROUND SERVICES. IN THE CLEARANCE AREAS, USE EARTH BACKFILL INSTEAD.
 - EXERCISE HANDLING AND USE PRECAUTION OF BACKFILL MATERIAL PER MFR'S REQUIREMENTS.
 - FOR LOCATIONS WHERE ROCK BOTTOM DEPTH IS LESS THAN 12" CONDUCTIVE CONCRETE SHALL BE USED INSTEAD OF CONDUCTIVE BACKFILL.

2 EGR TRENCH/BACKFILL DETAIL (SHALLOW TOPSOIL)
E-9 NOT TO SCALE



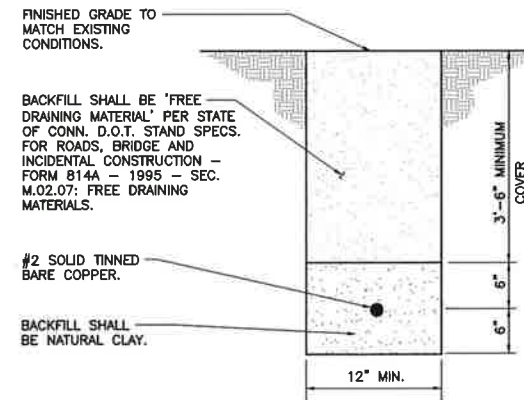
- NOTES:**
- THE #2 AWG, BCW, FROM THE GROUND RING SHALL BE CADWELDED TO EACH POST, ABOVE GRADE.

2 UTILITY FRAME GROUNDING DETAIL
E-6 NOT TO SCALE



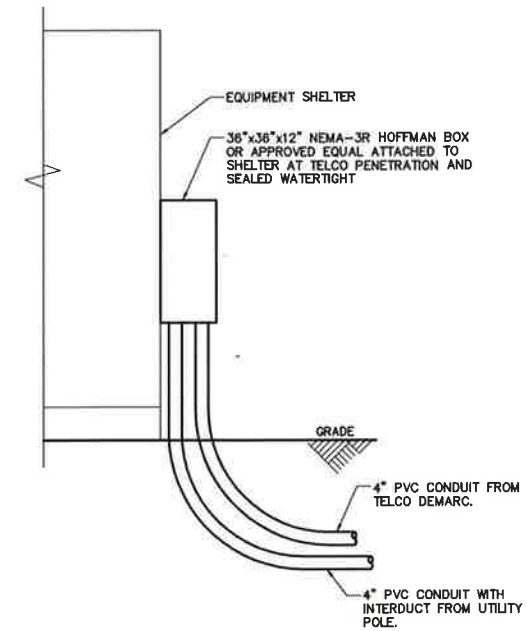
- NOTE:**
- NUMBER OF GROUND BARS MAY VARY DEPENDING ON THE TYPE OF TOWER, LOCATION AND CONNECTION ORIENTATION. PROVIDE AS REQUIRED.

7 ANTENNA CABLE GROUNDING - LATTICE TOWER
E-9 NOT TO SCALE



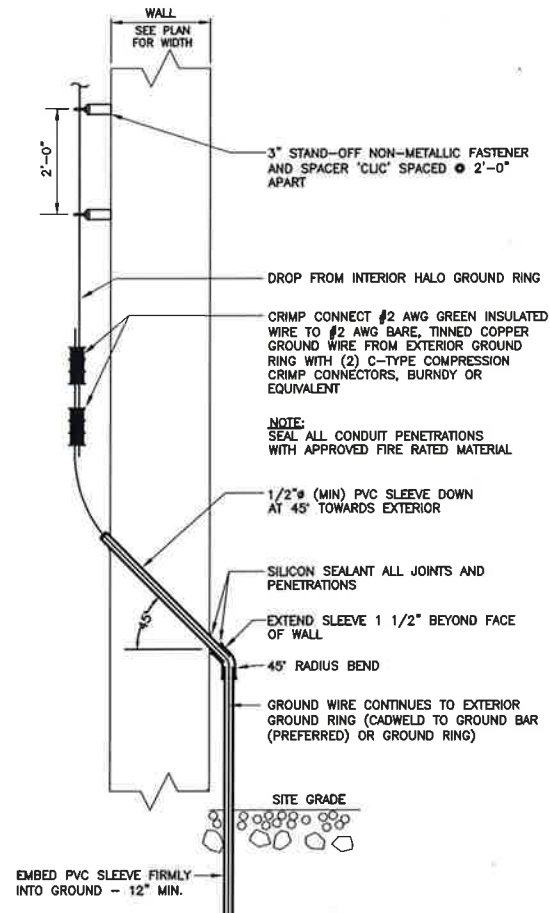
- NOTES:**
- ENGINEER SHALL INSPECT PLACEMENT OF EGR CONDUCTOR PRIOR TO BACKFILLING.
 - MAINTAIN MIN. 2'-0" LINEAR CLEARANCE BETWEEN NATURAL CLAY BACKFILL AND THE FOLLOWING: FOUNDATION, UNDERGROUND PIPING/CONDUIT, UNDERGROUND SERVICES. IN THE CLEARANCE AREAS, USE EARTH BACKFILL INSTEAD.
 - EXERCISE HANDLING AND USE PRECAUTION OF BACKFILL MATERIAL PER MFR'S REQUIREMENTS.

3 EGR TRENCH/BACKFILL DETAIL
E-9 NOT TO SCALE



- NOTES:**
- CONTRACTOR RESPONSIBLE FOR INSTALLATION OF CONDUITS, PULL ROPES, AND SUPPORT ASSEMBLY.
 - COORDINATE EXACT LOCATION AND CONDUIT SIZE WITH TELEPHONE COMPANY.

8 HOFFMAN BOX DETAIL
E-9 NOT TO SCALE



9 CELLULAR GROUNDING CONDUCTOR SECURED ON WALL
E-12 N.T.S.

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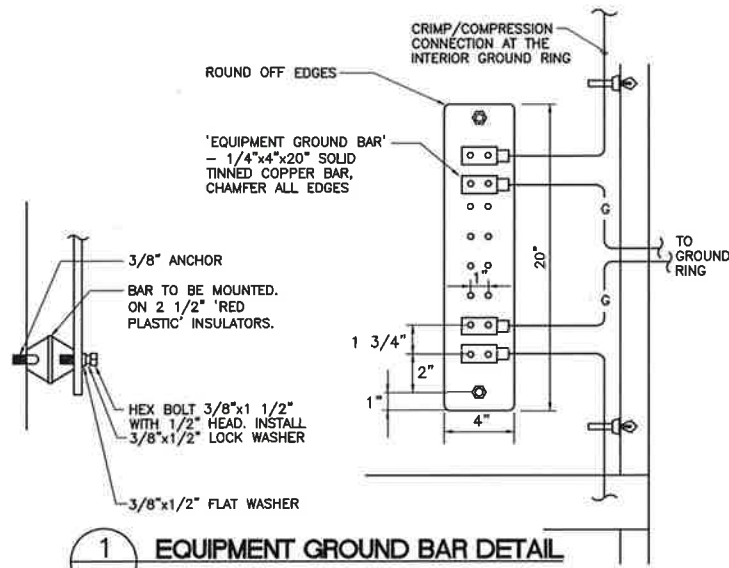
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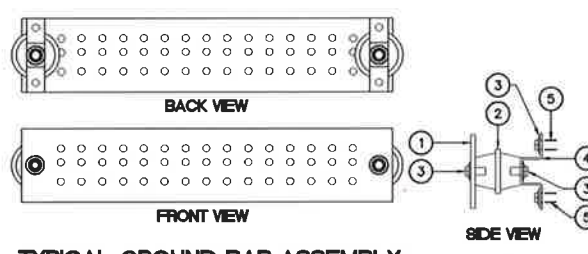
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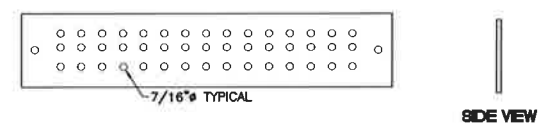
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1 EQUIPMENT GROUND BAR DETAIL
E-10 NOT TO SCALE

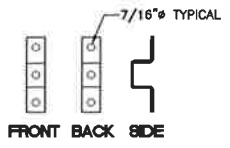


TYPICAL GROUND BAR ASSEMBLY



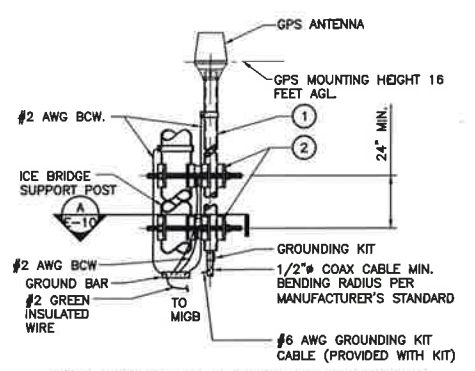
TYPICAL GROUND BAR - DIMENSIONS

- NOTES**
- HIGH CONDUCTIVITY TINNED COPPER BAR 1'-8" x 4" x 1/4" D.
 - RED COLORED STANDOFF INSULATOR PLASTIC #1872-1A.
 - STAINLESS STEEL TRUSS SPANNER MACHINE SCREWS, SPLIT LOCKWASHER AND FLAT WASHER.
 - 1" x 1/8" STAINLESS STEEL TYPE 304 BRACKET.
 - STAINLESS STEEL TYPE 304 HARDWARE - 3/8" EXPANSION BOLT FOR CONCRETE.



BRACKET FOR GROUND BAR-DIMENSIONS

3 MASTER/EQUIPMENT GROUND BAR DETAILS
E-10 NOT TO SCALE



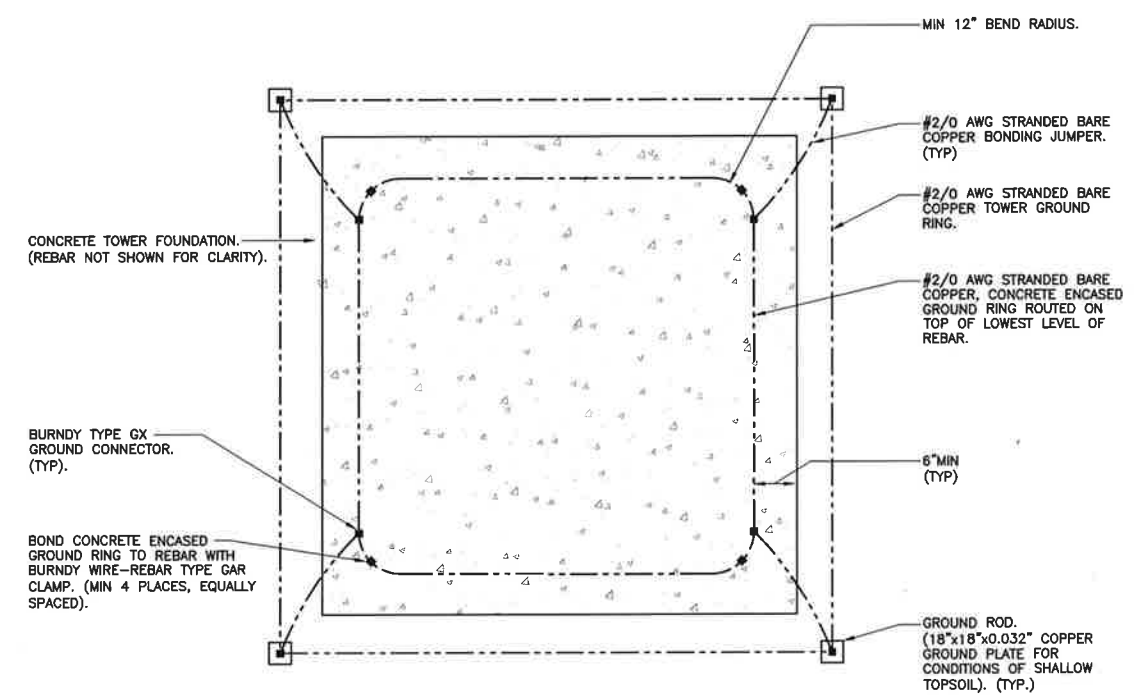
GPS ANTENNA MOUNTING BRACKET

BILL OF MATERIALS

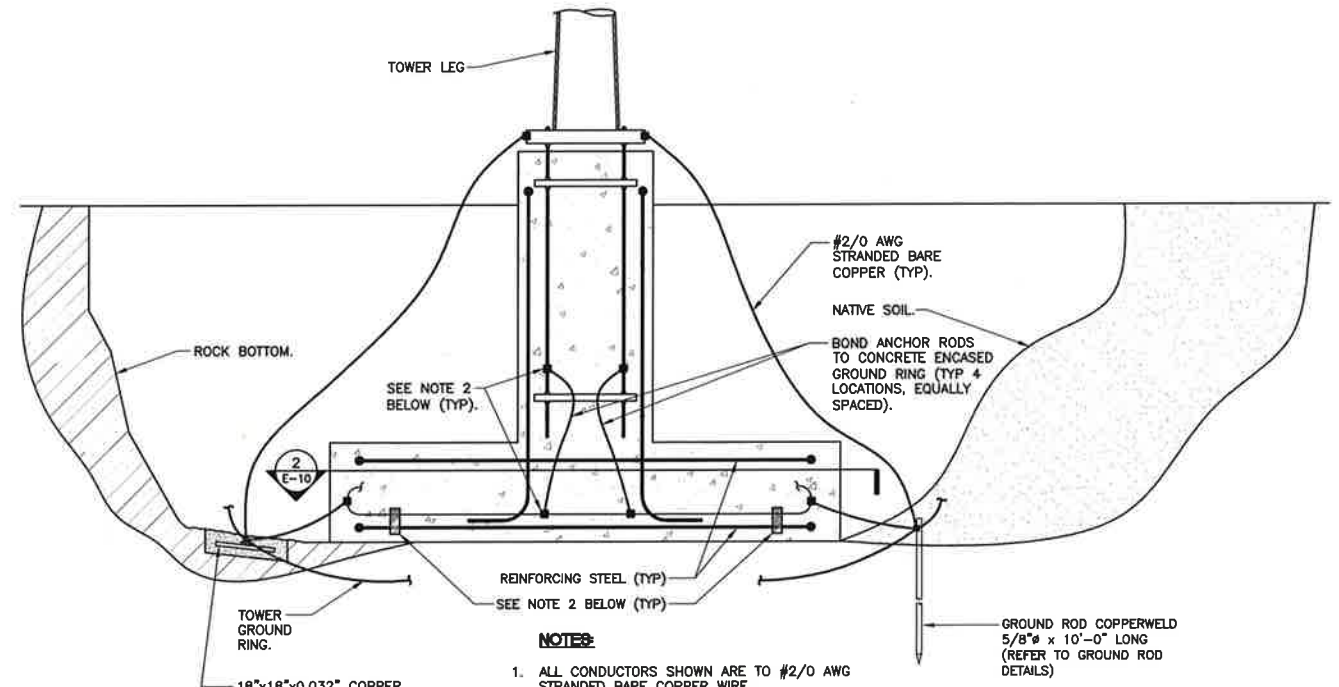
| ITEM | DESCRIPTION | QUANTITY |
|------|---|----------|
| 1 | 2-1/2" SCH. 40 x 8'-0" LG. MAX SS OR GALV. PIPE | 1 |
| 2 | UNIVERSAL CLAMP SET. | 2 |

4 GPS GROUNDING/MOUNTING BRACKET DETAIL
E-10 NOT TO SCALE

- NOTES**
- THE ELEVATION AND LOCATION OF THE GPS ANTENNA SHALL BE IN ACCORDANCE WITH THE FINAL RF REPORT.
 - THE GPS ANTENNA MOUNT IS DESIGNED TO FASTEN TO A STANDARD 2-1/2" DIAMETER, SCHEDULE 40, GALVANIZED STEEL OR STAINLESS STEEL PIPE. THE PIPE MUST NOT BE THREADED AT THE ANTENNA MOUNT END. THE PIPE SHALL BE CUT TO THE REQUIRED LENGTH (MINIMUM OF 24 INCHES) USING A HAND OR ROTARY PIPE CUTTER TO ASSURE A SMOOTH AND PERPENDICULAR CUT. A HACK SAW SHALL NOT BE USED. THE CUT PIPE END SHALL BE DEBURRED AND SMOOTH IN ORDER TO SEAL AGAINST THE NEOPRENE GASKET ATTACHED TO THE ANTENNA MOUNT.



2 CONCRETE ENCASED GROUND RING PLAN VIEW
E-10 NOT TO SCALE



- NOTES**
- ALL CONDUCTORS SHOWN ARE TO #2/0 AWG STRANDED BARE COPPER WIRE.
 - COPPER CONDUCTORS SHALL BE BONDED TO REINFORCING STEEL INSTALLED ON TOP OF LOWEST LAYER OF REBAR AND AT EACH CORNER USING BURNDY TYPE GAR WIRE-REBAR CLAMPS.
 - REFER TO ALL OTHER GROUNDING DETAILS FOR ADDITIONAL INFORMATION.
 - DESIGN IS BASED ON BARE STEEL REBAR FASTENED TOGETHER WITH THE USUAL STEEL TIE WIRES. CONTACT ENGINEER IF CONDITIONS VARY.

5 TOWER FOUNDATION GROUNDING DETAIL
E-10 NOT TO SCALE

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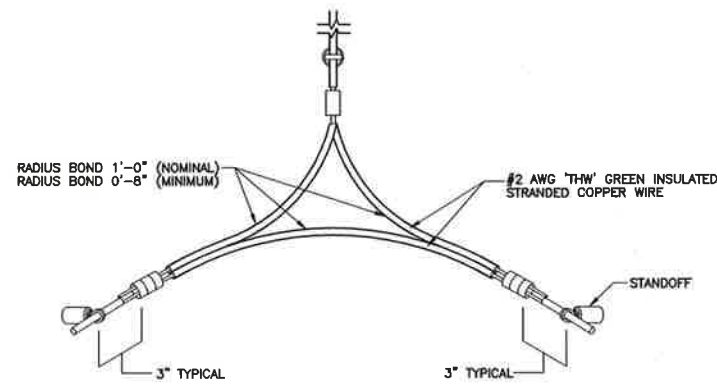
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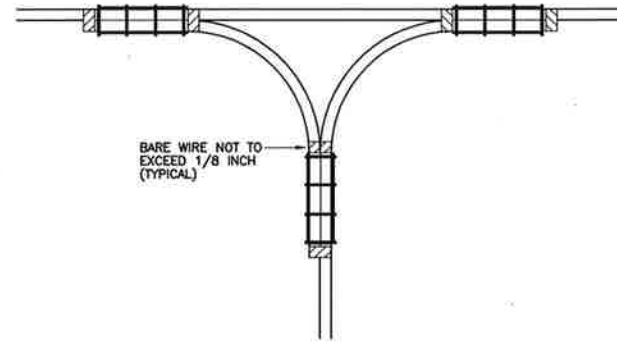
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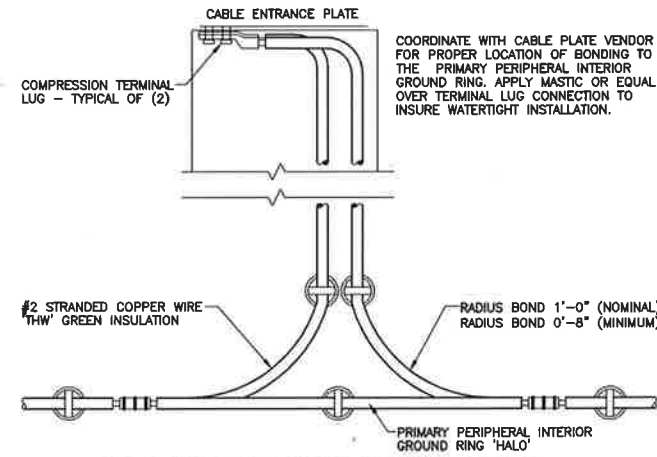
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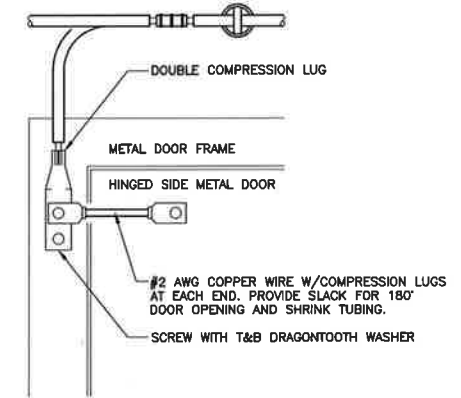
1 ISOMETRIC VIEW OF VERTICAL NONDIRECTIONAL SPLICE FOR CORNER INSTALLATION
E-11 N.T.S.



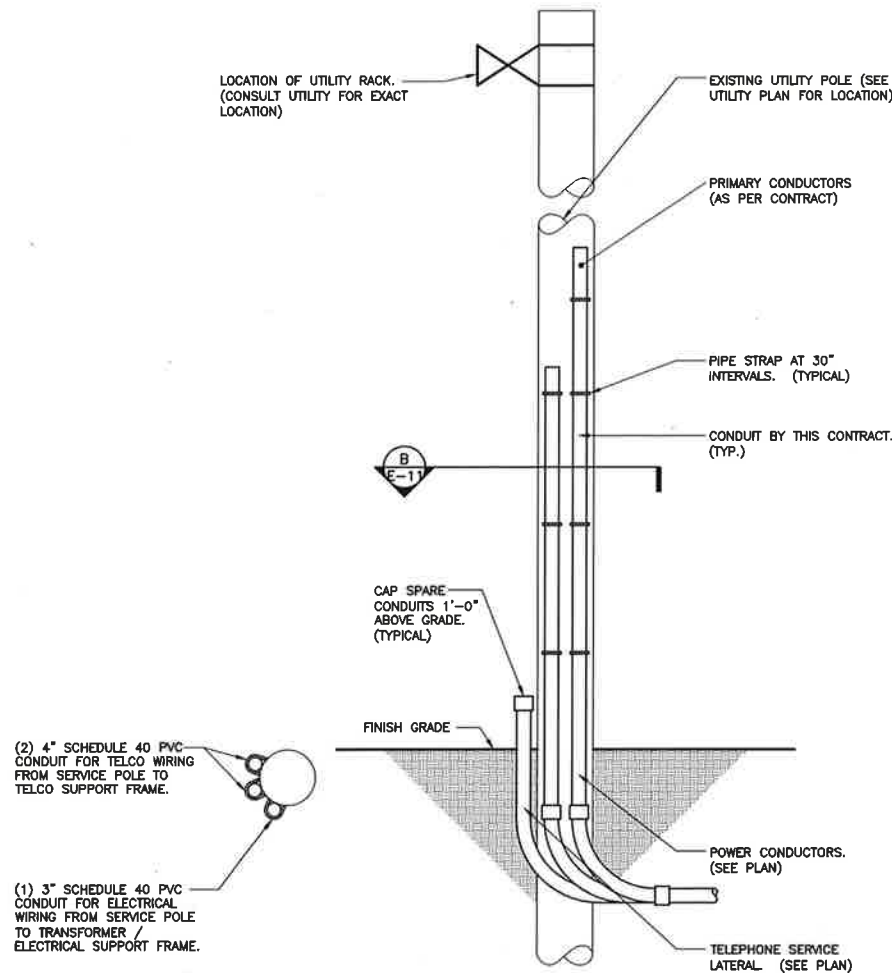
2 HORIZONTAL NONDIRECTIONAL SPLICE
E-11 N.T.S.



3 BONDING CABLE ENTRANCE PLATE TO PRIMARY PERIPHERAL INTERIOR GROUND RING
E-11 N.T.S.



4 BONDING METAL DOOR FRAME AND DOOR TO INTERIOR GROUNDING RING
E-11 N.T.S.



B DETAIL
E-11 NOT TO SCALE

5 INCOMING SERVICE POLE RISER
E-11 NOT TO SCALE

SERVICE RISER NOTES:

1. THE LOCATION SHOWN FOR THE CONNECTION TO UTILITIES, AND INCOMING POWER AND TELEPHONE SERVICES IS FOR CONCEPT ONLY. THE CONTRACTOR SHALL COORDINATE THE ACTUAL LOCATION WITH LOCAL TELEPHONE COMPANY, THE OWNER AND LOCAL ELECTRIC UTILITY COMPANY.
2. CONTRACTOR IS RESPONSIBLE FOR MAKING ARRANGEMENTS WITH LOCAL UTILITY COMPANY AND LOCAL TELEPHONE COMPANY FOR A TIMELY INSTALLATION OF THE INCOMING POWER AND TELEPHONE SERVICE. CONTRACTOR WILL OBTAIN AN ELECTRIC SERVICE ORDER (ESO) FOR THE SITE FROM LOCAL UTILITY COMPANY AND LOCAL TELEPHONE COMPANY PRIOR TO CONSTRUCTION.
3. THE INCOMING ELECTRIC SERVICE WILL BE INSPECTED BY THE AUTHORITY HAVING JURISDICTION AND A CERTIFICATE OF SUCH INSPECTION SHALL BE FURNISHED TO THE OWNER AND A COPY FORWARDED TO LOCAL UTILITY COMPANY.
4. FOR INCOMING UNDERGROUND TELEPHONE SERVICE, THE CONTRACTOR SHALL INSTALL CONDUIT AND PULL WIRES BETWEEN THE RISER POLE AND THE TELCO SERVICE CABINET. THE CONTRACTOR SHALL PROVIDE PRE CAST PULL-BOXES INCLUSIVE OF THE PRE CAST COVERS OF THE TYPE AND AS REQUIRED BY LOCAL TELEPHONE COMPANY THE MAXIMUM DISTANCE BETWEEN PULL-BOXES CAN NOT EXCEED 750' (CONTRACTOR TO CONFIRM WITH LOCAL UTILITY). AT THE PROPOSED RISER POLE EXTEND THE TELEPHONE CONDUIT UP THE POLE APPROXIMATELY 8' AND SEAL.
5. THE CONTRACTOR SHALL COORDINATE THE METER REQUIREMENTS WITH LOCAL UTILITY COMPANY.
6. THE INCOMING ELECTRICAL SERVICE SHALL BE INSTALLED IN CONFORMANCE WITH LOCAL UTILITY COMPANY STANDARDS (LATEST EDITION).
7. THIS SITE MAY CONTAIN CRITICAL UNDERGROUND ELECTRIC AND TELEPHONE SERVICES IN THE VICINITY OF THE NEW UNDERGROUND SERVICE AND THE EQUIPMENT SUPPORTS. THE CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO AVOID DISRUPTION OF THESE EXISTING FACILITIES. THE CONTRACTOR SHALL ALSO CONTACT LOCAL UTILITY COMPANY AND LOCAL TELEPHONE COMPANY AND ALL THE APPROPRIATE AGENCIES PRIOR TO EXCAVATION AT THIS SITE.

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ELECTRICAL SPECIFICATIONS

SECTION 16010

1.01. SCOPE OF WORK

- A. WORK SHALL INCLUDE ALL LABOR, EQUIPMENT AND SERVICES REQUIRED TO COMPLETE (MAKE READY FOR OPERATION) ALL THE ELECTRICAL WORK INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING:
 - 1. INSTALL TRANSFORMER AND NEW 5-GANG MULTI METER CENTER, 800A, 240/120V, 1P, 3 WIRE ELECTRIC SERVICE WITH REVENUE METER AND 200A MAIN CIRCUIT BREAKER FOR OWNER AND ASSOCIATED DISTRIBUTION EQUIPMENT. (AS REQUIRED BY UTILITY CO.) SCOPE TO ALSO INCLUDE:
 - a. RELOCATION OF ALL EXISTING ELECTRIC SERVICE METERS TO NEW METER CENTER, INCLUDING ALL CONDUITS, CONDUCTORS, DISCONNECTS, JUNCTION BOXES AND ACCESSORIES.
 - b. REMOVAL OF ABANDONED SERVICE EQUIPMENT, CONDUIT, AND CONDUCTORS AFTER COMPLETION OF EACH RELOCATION.
 - c. PROVIDE TEMPORARY POWER DURING CUTOVER AS REQUIRED.
 - d. COORDINATE OUTAGES AND SERVICE RELOCATIONS WITH EACH AFFECTED PARTY.
 - 2. NEW SITE TELEPHONE SERVICE AS SPECIFIED BY TELEPHONE COMPANY.
 - 3. GENERATOR/TRANSFER SWITCH.
 - 4. FEEDERS AND BRANCH CIRCUIT WIRING TO PANELS, RECEPTACLES, EQUIPMENT, LIGHTING FIXTURES, ETC. AS INDICATED OR NOTED ON PLANS.
 - 5. POWER AND TEMPERATURE CONTROL WIRING FOR HVAC EQUIPMENT.
 - a. FURNISH AND INSTALL ALL POWER WIRING FOR ALL HEATING, VENTILATING, AIR CONDITIONING, MOTORS AND DEVICES, AND FIRE PROTECTION EQUIPMENT INDICATED ON THE PLANS OR CALLED FOR IN THIS SPECIFICATION, EITHER ELECTRICAL OR MECHANICAL INCLUDING ALL CONTROL WIRING. ALL MAGNETIC STARTERS SHALL BE FURNISHED UNDER DIVISION 15 AND HAVE INSTALLED THEREIN A PROPER OVERLOAD HEATER FOR EACH MOTOR.
 - b. ALL WIRING, BOTH POWER AND CONTROL, FOR SUCH ITEMS AS UNIT HEATERS, EXHAUST FANS, ETC., NOT SPECIFICALLY CALLED FOR IN THE TEMPERATURE CONTROL SPECIFICATIONS, SHALL BE WIRED UNDER DIVISION 16.
 - c. ALL CONTROLS WHICH ARE TO BE WIRED BY THIS CONTRACTOR SHALL BE DELIVERED TO HIM BY THE CONTRACTOR/VENDOR FURNISHING THEM.
 - 6. CELLULAR SITE ALARMS, ASSOCIATED WIRING AND DEVICES.
 - 7. CELLULAR GROUNDING SYSTEMS, CONSISTING OF ANTENNA GROUNDING, INTERIOR GROUNDING RING, GROUND BARS, ETC.
 - 8. FURNISH AND INSTALL 3/4" PLYWOOD BACKBOARD OF SIZE INDICATED ON DRAWINGS FOR MOUNTING OF POWER/SERVICE EQUIPMENT AND TELEPHONE/ALARM EQUIPMENT. BACKBOARDS SHALL BE PAINTED WITH TWO (2) COATS OF SEMI-GLOSS GRAY FIRE RETARDANT PAINT.
 - 9. FIELD MEASURE EXISTING ELECTRICAL SERVICES TO CONFIRM AVAILABLE EXISTING POWER.
 - 10. COORDINATE ALL WORK SHOWN, ON THESE PLANS WITH LOCAL UTILITY COMPANIES.
 - 11. REMOVAL OF EXISTING GUYED TOWER AND ALL ASSOCIATED GROUNDING ELEMENTS, AS SPECIFIED IN THE PLANS.
- B. LOCAL UTILITY COMPANIES SHALL PROVIDE THE FOLLOWING:
 - 1. TELEPHONE CABLES.
 - 2. SHUTDOWN OF SERVICE (COORDINATE WITH OWNER).
- C. CONTRACTOR SHALL CONFER WITH LOCAL UTILITY COMPANIES TO ASCERTAIN THE LIMITS OF THEIR WORK AND SHALL INCLUDE IN BID ANY CHARGES OR FEES MADE BY THE UTILITY COMPANIES FOR THEIR PORTION OF THE WORK AND SHALL PROVIDE AND INSTALL ALL ITEMS REQUIRED, BUT NOT PROVIDED BY UTILITY COMPANY.
- D. ELECTRICAL CONTRACTOR SHALL COORDINATE ELECTRICAL INSTALLATION WITH ELECTRIC UTILITY CO. PRIOR TO INSTALLATION.
- E. CONTRACTOR SHALL COORDINATE WITH TELEPHONE UTILITY COMPANY FOR LOCATION OF TELEPHONE SERVICE AND TO DETERMINE ANY REQUIRED EQUIPMENT TO BE INSTALLED BY CONTRACTOR.

1.02. GENERAL REQUIREMENTS

- A. THE ENTIRE ELECTRICAL INSTALLATION SHALL BE MADE IN STRICT ACCORDANCE WITH ALL LOCAL STATE AND NATIONAL CODES AND REGULATIONS WHICH MAY APPLY AND NOTHING IN THE DRAWINGS OR SPECIFICATIONS SHALL BE INTERPRETED AS AN INFRINGEMENT OF SUCH CODES OR REGULATIONS.
- B. THE ELECTRICAL CONTRACTOR IS TO BE RESPONSIBLE FOR THE COMPLETE INSTALLATION AND COORDINATION OF THE ENTIRE ELECTRICAL SERVICE. ALL ACTIVITIES TO BE COORDINATED THROUGH OWNERS REPRESENTATIVE, DESIGN ENGINEER AND OTHER AUTHORITIES HAVING JURISDICTION OF TRADES.
- C. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND PAY ALL FEES THAT MAY BE REQUIRED FOR THE ELECTRICAL WORK AND FOR SCHEDULING OF ALL INSPECTIONS THAT MAY BE REQUIRED BY THE LOCAL AUTHORITY.
- D. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATION WITH THE BUILDING OWNER FOR NEW AND/OR DEMOLITION WORK INVOLVED.
- E. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATION WITH LOCAL TELEPHONE COMPANY THAT MAY BE REQUIRED FOR THE INSTALLATION OF TELEPHONE SERVICE TO THE PROPOSED CELLULAR SITE.
- F. NO MATERIAL OTHER THAN THAT CONTAINED IN THE "LATEST LIST OF ELECTRICAL FITTINGS" APPROVED BY THE UNDERWRITERS' LABORATORIES, SHALL BE USED IN ANY PART OF THE WORK. ALL MATERIAL FOR WHICH LABEL SERVICE HAS BEEN ESTABLISHED SHALL BEAR THE U.L. LABEL.
- G. THE CONTRACTOR SHALL GUARANTEE ALL NEW WORK FOR A PERIOD OF ONE YEAR FROM THE ACCEPTANCE DATE BY THE OWNER. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING WARRANTIES FROM ALL EQUIPMENT MANUFACTURERS FOR SUBMISSION TO THE OWNER.

- H. DRAWINGS INDICATE GENERAL ARRANGEMENT OF WORK INCLUDED IN CONTRACT. CONTRACTOR SHALL, WITHOUT EXTRA CHARGE, MAKE MODIFICATIONS TO THE LAYOUT OF THE WORK TO PREVENT CONFLICT WITH WORK OF OTHER TRADES AND FOR THE PROPER INSTALLATION OF WORK. CHECK ALL DRAWINGS AND VISIT JOB SITE TO VERIFY SPACE AND TYPE OF EXISTING CONDITIONS IN WHICH WORK WILL BE DONE, PRIOR TO SUBMITTAL OF BID.
- I. THE ELECTRICAL CONTRACTOR SHALL SUPPLY THREE (3) COMPLETE SETS OF APPROVED DRAWINGS, ENGINEERING DATA SHEETS, MAINTENANCE AND OPERATING INSTRUCTION MANUALS FOR ALL SYSTEMS AND THEIR RESPECTIVE EQUIPMENT. THESE MANUALS SHALL BE INSERTED IN VINYL COVERED 3-RING BINDERS AND TURNED OVER TO OWNER'S REPRESENTATIVE ONE (1) WEEK PRIOR TO FINAL PUNCH LIST.
- J. ALL WORK SHALL BE INSTALLED IN A NEAT AND WORKMAN LIKE MANNER AND WILL BE SUBJECT TO THE APPROVAL OF THE OWNER'S REPRESENTATIVE.
- K. ALL EQUIPMENT AND MATERIALS TO BE INSTALLED SHALL BE NEW, UNLESS OTHERWISE NOTED.
- L. BEFORE FINAL PAYMENT, THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF PRINTS (AS-BUILTS), LEGIBLY MARKED IN RED PENCIL TO SHOW ALL CHANGES FROM THE ORIGINAL PLANS.
- M. PROVIDE TEMPORARY POWER AND LIGHTING IN WORK AREAS AS REQUIRED.
- N. SHOP DRAWINGS:
 - 1. CONTRACTOR SHALL SUBMIT SIX (6) COPIES OF SHOP DRAWINGS ON ALL EQUIPMENT AND MATERIALS PROPOSED FOR USE ON THIS PROJECT, GIVING ALL DETAILS, WHICH INCLUDE DIMENSIONS, CAPACITIES, ETC.
 - 2. CONTRACTOR SHALL SUBMIT SIX (6) COPIES OF ALL TEST REPORTS CALLED FOR IN THE SPECIFICATIONS AND DRAWINGS.
- O. ENTIRE ELECTRICAL INSTALLATION SHALL BE IN ACCORDANCE WITH OWNER'S SPECIFICATIONS, AND REQUIREMENTS OF ALL LOCAL AUTHORITIES HAVING JURISDICTION. IT IS THE CONTRACTOR'S RESPONSIBILITY TO COORDINATE WITH APPROPRIATE INDIVIDUALS TO OBTAIN ALL SUCH SPECIFICATIONS AND REQUIREMENTS. NOTHING CONTAINED IN, OR OMITTED FROM, THESE DOCUMENTS SHALL RELIEVE CONTRACTOR FROM THIS OBLIGATION.

SECTION 16111

1.01. CONDUIT

- A. MINIMUM CONDUIT SIZE FOR BRANCH CIRCUITS, LOW VOLTAGE CONTROL AND ALARM CIRCUITS SHALL BE 3/4". ALL CONDUIT RUNS LOCATED WITHIN THE OWNER'S EQUIPMENT ROOM SHALL ORIGINATE FROM THE WIREWAY AND RUN VERTICALLY TO ITS DESTINATION. NO BENDS WILL BE ACCEPTED. CONDUITS SHALL BE PROPERLY FASTENED TO THE WALLS AND CEILINGS AS REQUIRED BY THE N.E.C.
- B. CONDUIT MATERIAL SHALL BE AS FOLLOWS:
 - 1. ELECTRIC METALLIC TUBING (EMT) - BRANCH CIRCUITS INSIDE WIRELESS ROOM
 - 2. GALVANIZED RIGID CONDUIT (GRC) - FEEDERS AND CIRCUITS EXPOSED TO EXTERIOR & UNDERGROUND.
 - 3. LIQUID TIGHT FLEXIBLE METAL CONDUIT - FOR SHORT LENGTHS (MAX. 3'-0") WIRING TO VIBRATING EQUIPMENT (HVAC UNITS, MOTORS, ETC.) IN WET LOCATIONS.
 - 4. FLEXIBLE METAL CONDUIT - FOR SHORT LENGTHS (MAX. 3'-0") WIRING TO VIBRATING EQUIPMENT IN DRY LOCATIONS.
 - 5. PVC CONDUIT - WHERE SHOWN ON GROUNDING DETAILS.

SECTION 16113

1.01. WIREWAYS

- A. THE 4" x 4" WIREWAY LOCATED IN THE OWNER'S EQUIPMENT ROOM SHALL BE INSTALLED ALONG THE TOP OF THE INTERIOR WALL AND SHALL HAVE ONE VERTICAL DROP CONNECTED TO PANELBOARD. MANUFACTURER SHALL BE HOFFMAN ENGINEERING COMPANY OR APPROVED EQUAL.

SECTION 16114

1.01. CABLE TRAY

- A. CABLE TRAY SHALL BE SOLID SIDE BAR, 18" WIDE (NEWTON INSTRUMENT COMPANY, INC.). TRAY SHALL BE INSTALLED AS SHOWN ON CONTRACT DOCUMENTS.
- B. CROSSWISE RUNS SHALL BE COORDINATED WITH THE SPECIFIC EQUIPMENT THE TRAY SHALL SERVE.
- C. ALL PROTRUDING CABLE TRAY SUPPORT RODS SHALL BE FILED SMOOTH WITH NO SHARP EDGES. ALL SUPPORT RODS SHALL BE CAD-PLATED FOR RUST RESISTANCE AND A MINIMUM 1/2" DIAMETER.

SECTION 16123

1.01. CONDUCTORS

- A. ALL CONDUCTORS SHALL BE TYPE THWN (INT. APPLICATION) AND XHHW (EXT. APPLICATION), 75 DEGREE C, 600 VOLT INSULATION, SOFT ANNEALED STRANDED COPPER. #10 AWG AND SMALLER SHALL BE SPLICED USING ACCEPTABLE SOLDERLESS PRESSURE CONNECTORS. #8 AWG AND LARGER SHALL BE SPLICED USING COMPRESSION SPLIT-BOLT TYPE CONNECTORS. #12 AWG SHALL BE THE MINIMUM SIZE CONDUCTOR FOR LINE VOLTAGE BRANCH CIRCUITS. REFER TO PANEL SCHEDULE FOR BRANCH CIRCUIT CONDUCTOR SIZE(S). CONDUCTORS SHALL BE COLOR CODED FOR CONSISTENT PHASE IDENTIFICATION:

| | | |
|------|------------------|--------------------------|
| LINE | 120/208/240V | 277/480V |
| A | BLACK | BROWN |
| B | RED | ORANGE |
| C | BLUE | YELLOW |
| N | CONTINUOUS WHITE | GREY |
| G | CONTINUOUS GREEN | GREEN WITH YELLOW STRIPE |
- B. MINIMUM BENDING RADIUS FOR CONDUCTORS SHALL BE 12 TIMES THE LARGEST DIAMETER OF BRANCH CIRCUIT CONDUCTOR.

SECTION 16130

1.01. BOXES

- A. FURNISH AND INSTALL OUTLET BOXES FOR ALL DEVICES, SWITCHES, RECEPTACLES, ETC.. BOXES TO BE ZINC COATED STEEL.
- B. FURNISH AND INSTALL PULL BOXES IN MAIN FEEDERS RUNS WHERE REQUIRED. PULL BOXES SHALL BE GALVANIZED STEEL WITH SCREW REMOVABLE COVERS, SIZE AND QUANTITY AS REQUIRED. PROVIDE WEATHERPROOF CONSTRUCTION IN WET LOCATIONS.

SECTION 16140

1.01. WIRING DEVICES

- A. THE FOLLOWING LIST IS PROVIDED TO CONVEY THE QUALITY AND RATING OF WIRING DEVICES WHICH ARE TO BE INSTALLED. A COMPLETE LIST OF ALL DEVICES MUST BE SUBMITTED BEFORE INSTALLATION FOR APPROVAL.
 - 1. 15 MINUTE TIMER SWITCH - INTERMATIC #FF15M (INTERIOR LIGHTS)
 - 2. DUPLEX RECEPTACLE - P&S #2095 (GFC) SPECIFICATION GRADE
 - 3. SINGLE POLE SWITCH - P&S #CSB20AC2 (20A-120V HARD USE) SPECIFICATION GRADE
 - 4. DUPLEX RECEPTACLE - P&S #5382 (20A-120V HARD USE) SPECIFICATION GRADE
- B. PLATES - ALL PLATES USED SHALL BE CORROSION RESISTANT TYPE 304 STAINLESS STEEL. PLATES SHALL BE FROM SAME MANUFACTURER AS SWITCHES AND RECEPTACLES. PROVIDE WEATHERPROOF HOUSING FOR DEVICES LOCATED IN WET LOCATIONS.
- C. OTHER MANUFACTURERS OF THE SWITCHES, RECEPTACLES AND PLATES MAY BE SUBMITTED FOR APPROVAL BY THE ENGINEER.

SECTION 16170

1.01. DISCONNECT SWITCHES

- A. FUSIBLE AND NON-FUSIBLE, 600V, HEAVY DUTY DISCONNECT SWITCHES SHALL BE AS MANUFACTURED BY SQUARE "D". PROVIDE FUSES AS CALLED FOR ON THE CONTRACT DRAWINGS. AMPERE RATING SHALL BE CONSISTENT WITH LOAD BEING SERVED. DISCONNECT SWITCH COVER SHALL BE MECHANICALLY INTERLOCKED TO PREVENT COVER FROM OPENING WHEN THE SWITCH IS IN THE "ON" POSITION. EXTERIOR APPLICATIONS SHALL BE NEMA 3R CONSTRUCTION WITH PADLOCK FEATURE.

SECTION 16190

1.01. SEISMIC RESTRAINT

- A. ALL DEVICES SHALL BE INSTALLED IN ACCORDANCE WITH ZONE 2 SEISMIC REQUIREMENTS.

SECTION 16195

1.01. LABELING AND IDENTIFICATION NOMENCLATURE FOR ELECTRICAL EQUIPMENT

- A. CONTRACTOR SHALL FURNISH AND INSTALL NON-METALLIC ENGRAVED BACK-LIT NAMEPLATES ON ALL PANELS AND MAJOR ITEMS OF ELECTRICAL EQUIPMENT.
- B. LETTERS TO BE WHITE ON BLACK BACKGROUND WITH LETTERS 1-1/2 INCH HIGH WITH 1/4 INCH MARGIN.
- C. IDENTIFICATION NOMENCLATURE SHALL BE IN ACCORDANCE WITH OWNER'S STANDARDS.
- D. PROVIDE NAMEPLATE FOR PORTABLE ENGINE/GENERATOR CONNECTION SHOWING VOLTAGE KVA/KW RATING, # PHASE, AND # OF WIRES. PLATE TO BE PLASTIC ENGRAVED, RED WITH WHITE LETTERS.
- E. ALL RECEPTACLES, SWITCHES, DISCONNECT SWITCHES, ETC. SHALL BE LABELED WITH THE CORRECT BRANCH CIRCUIT NUMBER SERVED BY MEANS OF PERMANENT PRESSES TYPE BLACK 1/4" TRANSFER LETTERING. (FOR EXAMPLE: "MDP-5", ETC.).
- F. PROVIDE A NAMEPLATE AT THE SERVICE EQUIPMENT INDICATING THE TYPE AND LOCATION OF THE ON SITE GENERATOR.

SECTION 16450

1.01. GROUNDING

- A. ALL NON-CURRENT CARRYING PARTS OF THE ELECTRICAL AND TELEPHONE CONDUIT SYSTEMS SHALL BE MECHANICALLY AND ELECTRICALLY CONNECTED TO PROVIDE AN INDEPENDENT RETURN PATH TO THE EQUIPMENT GROUNDING SOURCES.
- B. GROUNDING SYSTEM WILL BE IN ACCORDANCE WITH THE LATEST ACCEPTABLE EDITION OF THE NATIONAL ELECTRICAL CODE AND REQUIREMENTS PER LOCAL INSPECTOR HAVING JURISDICTION.
- C. GROUNDING OF PANELBOARDS:
 - 1. PANELBOARD SHALL BE GROUNDED BY TERMINATING THE PANELBOARD FEEDER'S EQUIPMENT GROUND CONDUCTOR TO THE EQUIPMENT GROUND BAR KIT(S) LUGGED TO THE CABINET. ENSURE THAT THE SURFACE BETWEEN THE KIT AND CABINET ARE BARE METAL TO BARE METAL. PRIME AND PAINT OVER TO PREVENT CORROSION.
 - 2. CONDUIT(S) TERMINATING INTO THE PANELBOARD SHALL HAVE GROUNDING TYPE BUSHINGS. THE BUSHINGS SHALL BE BONDED TOGETHER WITH BARE #10 AWG COPPER CONDUCTOR WHICH IN TURN IS TERMINATED INTO THE PANELBOARD'S EQUIPMENT GROUND BAR KIT(S).
- D. EQUIPMENT GROUNDING CONDUCTOR:
 - 1. EACH EQUIPMENT GROUND CONDUCTOR SHALL BE SIZED IN ACCORDANCE WITH THE N.E.C. ARTICLE 250-122.
 - 2. THE MINIMUM SIZE OF EQUIPMENT GROUND CONDUCTOR SHALL BE #12 AWG COPPER.
 - 3. REFER TO PANEL SCHEDULE "BRANCH CIRCUIT" DATA FOR EQUIPMENT GROUND CONDUCTOR SIZE FOR EACH BRANCH CIRCUIT.
 - 4. EACH FEEDER OR BRANCH CIRCUIT SHALL HAVE EQUIPMENT GROUND CONDUCTOR(S) INSTALLED IN THE SAME RACEWAY(S).
- E. CELLULAR GROUNDING SYSTEM:

CONTRACTOR SHALL PROVIDE A CELLULAR GROUNDING SYSTEM WITH THE MAXIMUM AC RESISTANCE TO GROUND OF 5 OHM BETWEEN ANY POINT ON THE GROUNDING SYSTEM AS MEASURED BY 3-POINT GROUNDING TEST. (REFER TO SECTION 16960).

PROVIDE THE CELLULAR GROUNDING SYSTEM AS SPECIFIED ON DRAWINGS, INCLUDING, BUT NOT LIMITED TO:

 - GROUND BARS
 - INTERIOR GROUND RING
 - EXTERIOR GROUNDING (WHERE REQUIRED DUE TO MEASURED AC RESISTANCE GREATER THAN SPECIFIED).
 - ANTENNA GROUND CONNECTIONS AND PLATES.
- F. CONTRACTOR, AFTER COMPLETION OF THE COMPLETE GROUNDING SYSTEM BUT PRIOR TO CONCEALMENT/BURIAL OF SAME, SHALL NOTIFY OWNER'S WIRELESS PROJECT ENGINEER WHO WILL HAVE A DESIGN ENGINEER VISIT SITE AND MAKE A VISUAL INSPECTION OF THE GROUNDING GRID AND CONNECTIONS OF THE SYSTEM.
- G. ALL EQUIPMENT SHALL BE BONDED TO GROUND AS REQUIRED BY N.E.C., MFG. SPECIFICATIONS, AND OWNER'S SPECIFICATIONS.

SECTION 16470

1.01. DISTRIBUTION EQUIPMENT

- A. REFER TO CONTRACT DRAWINGS FOR DETAILS AND SCHEDULES.

SECTION 16477

1.01. FUSES

- A. FUSES SHALL BE NONRENEWABLE TYPE AS MANUFACTURED BY "BUSSMAN" OR APPROVED EQUAL FUSES RATED TO 1/10 AMPERE UP TO 600 AMPERES SHALL BE EQUIVALENT TO BUSSMAN TYPE LPN-RK (250V) UL CLASS RK1, LOW PEAK, DUAL ELEMENT, TIME-DELAY FUSES. FUSES SHALL HAVE SEPARATE SHORT CIRCUIT AND OVERLOAD ELEMENTS AND HAVE AN INTERRUPTING RATING OF 200 KAIC. UPON COMPLETION OF WORK, PROVIDE ONE SPARE SET OF FUSES FOR EACH TYPE INSTALLED.

SECTION 16500

1.01. LIGHTING FIXTURES

- A. REFER TO LIGHT FIXTURE SCHEDULE FOR REQUIREMENTS.

SECTION 16620

(SUPPLIED BY OWNER, INSTALLED BY CONTRACTOR)

1.01. GENERATOR SET

- A. REFER TO CONTRACT DRAWINGS FOR DETAILS AND SCHEDULES.

SECTION 16700

1.01. BUILDING ALARMS (SIGNAL COMMUNICATIONS)

- A. ALARM BOX SHALL BE 12" W x 12" H x 6" D NEMA 1 ENCLOSURE, MCKINSTRY #30-1216LP WITH ACCESSORIES:
 - "T" HANDLE LATCH KIT
 - 14 GAUGE STEEL PANEL, PAINTED WHITE ENAMEL
 - (6) 1/2"-3/4" K.OS ON EACH SIDE/TOP/BOTTOM WALLS
 - (2) 3/4" RUBBER GROMMETS AS SLEEVES
 - PROVIDE WIRING SCHEMATIC IN REMOVABLE PLASTIC COVER, TAPED TO BACK SIDE OF HINGED DOOR.
- B. ALARM SENSORS' RELAY SHALL BE NORMALLY CLOSED. UPON ALARM CONDITION, THE RELAY SHALL REVERSE STATE TO OPEN. CONFIRM INSTALLATION AND LOCATION REQUIREMENTS FOR BUILDING'S ALARM SENSORS.

ALARM SENSORS SHALL BE:

 - FIRE ALARM CONTROL PANEL: FROM C CONTACT RELAY.
 - DOOR CONTACT SENSOR (SENTRUL #1085T): SPDT MAGNETIC FORM C CONTACT - OPEN/CLOSE LOOP, MAX 1" GAP.
 - LOW TEMPERATURE SENSOR (HONEYWELL #T631C1103): SPDT AIR SWITCH CONTROLLER COILED COPPER TUBE IN NEMA 1 ENCLOSURE, SET AT 50 DEGREES F., MOUNT LAMINATED, BACK-LIT NAMEPLATE WITH LEGIBLE DESCRIPTION "LOW TEMP 50 DEGREE F" BELOW SENSOR.
 - HIGH TEMPERATURE SENSOR (HONEYWELL #T631C1103): SPDT AIR SWITCH CONTROLLER - COILED COPPER TUBE IN NEMA 1 ENCLOSURE, SET AT 80 DEGREES F., MOUNT LAMINATED, BACK-LIT NAMEPLATE WITH LEGIBLE DESCRIPTION "HI TEMP 80 DEGREES F" BELOW SENSOR.
- C. CONFIRM REQUIREMENTS FOR ALL BUILDING ALARM SENSORS INSTALLATION, AND LOCATION OF EACH SENSOR. ALARM WIRING SHALL BE ROUTED TO ALARM BOX AND SPADE CONNECTED TO RESPECTIVE TERMINAL BLOCK. EACH PAIR OF ALARM WIRING SHALL BE PERMANENTLY AND UNIQUELY TAGGED AT EACH TERMINAL STRIP LOCATION AND AT SPlice/JUNCTION/BOXES/WIRING TROUGH.
- D. REFER TO "WIRING SCHEMATIC FOR ALARM SENSORS" ON DRAWINGS.

SECTION 16960

1.01. TESTS BY INDEPENDENT ELECTRICAL TESTING FIRM

- A. CONTRACTOR SHALL RETAIN THE SERVICES OF A LOCAL INDEPENDENT ELECTRICAL TESTING FIRM (WITH MINIMUM 5 YEARS COMMERCIAL EXPERIENCE IN THE ELECTRICAL TESTING INDUSTRY) AS SPECIFIED BY OWNER TO PERFORM:
 - TEST 1: THERMAL OVERLOAD AND MAGNETIC TRIP TEST, AND CABLE INSULATION TEST FOR ALL CIRCUIT BREAKERS RATED 100 AMPS OR GREATER.
 - TEST 2: RESISTANCE TO GROUND TEST ON THE CELLULAR GROUNDING SYSTEM.
 - B. THE TESTING FIRM SHALL INCLUDE THE FOLLOWING INFORMATION WITH THE REPORT:
 - TESTING PROCEDURE INCLUDING THE MAKE AND MODEL OF TEST EQUIPMENT.
 - CERTIFICATION OF TESTING EQUIPMENT CALIBRATION WITHIN SIX (6) MONTHS OF DATE OF TESTING. INCLUDE CERTIFICATION LAB ADDRESS AND TELEPHONE NUMBER.
 - GRAPHICAL DESCRIPTION OF TESTING METHOD ACTUALLY IMPLEMENTED.
 - C. THESE TESTS SHALL BE PERFORMED IN THE PRESENCE AND TO THE SATISFACTION OF OWNER'S CONSTRUCTION REPRESENTATIVE. TESTING DATA SHALL BE INITIALED AND DATED BY THE CONSTRUCTION REPRESENTATIVE AND INCLUDED WITH THE WRITTEN REPORT/ANALYSIS.
 - D. THE CONTRACTOR SHALL FORWARD SIX (6) COPIES OF THE INDEPENDENT ELECTRICAL TESTING FIRM'S REPORT/ANALYSIS TO ENGINEER A MINIMUM OF TEN (10) WORKING DAYS PRIOR TO THE JOB TURNOVER.
 - E. CONTRACTOR TO PROVIDE A MINIMUM OF ONE (1) WEEK NOTICE TO OWNER AND ENGINEER FOR ALL TESTS REQUIRING WITNESING.
- SECTION 16961**
- 1.01. TESTS BY CONTRACTOR**
- A. ALL TESTS AS REQUIRED UPON COMPLETION OF WORK, SHALL BE MADE BY THIS CONTRACTOR. THESE SHALL BE CONTINUITY AND INSULATION TESTS; TEST TO DETERMINE THE QUALITY OF MATERIALS, ETC. AND SHALL BE MADE IN ACCORDANCE WITH N.E.C. RECOMMENDATIONS. ALL FEEDERS AND BRANCH CIRCUIT WIRING (EXCEPT CLASS 2 SIGNAL CIRCUITS) MUST BE TESTED FREE FROM SHORT CIRCUIT AND GROUND FAULT CONDITIONS AT 500V IN A REASONABLY DRY AMBIENT OF APPROXIMATELY 70 DEGREES F.
 - B. CONTRACTOR SHALL PERFORM LOAD PHASE BALANCING TESTS. CIRCUITS SHALL BE SO CONNECTED TO THE PANELBOARDS SUCH THAT THE NEW LOAD IS DISTRIBUTED AS EQUALLY AS POSSIBLE BETWEEN EACH LOAD AND NEUTRAL. 10% SHALL BE CONSIDERED AS A REASONABLE AND ACCEPTABLE ALLOWANCE. BRANCH CIRCUITS SHALL BE BALANCED ON THEIR OWN PANELBOARDS; FEEDER LOADS SHALL, IN TURN, BE BALANCED ON THE SERVICE EQUIPMENT. REASONABLE LOAD TEST SHALL BE ARRANGED TO VERIFY LOAD BALANCE IF REQUESTED BY THE ENGINEER.
 - C. ALL TESTS, UPON REQUEST, SHALL BE REPEATED IN THE PRESENCE OF OWNER'S REPRESENTATIVE. ALL TESTS SHALL BE DOCUMENTED AND TURNED OVER TO OWNER. OWNER SHALL HAVE THE AUTHORITY TO STOP ANY OF THE WORK NOT BEING PROPERLY INSTALLED. ALL SUCH DETECTED WORK SHALL BE REPAIRED OR REPLACED AT NO ADDITIONAL EXPENSE TO THE OWNER AND THE TESTS SHALL BE REPEATED.

PROFESSIONAL ENGINEER, S.E.

Verizon Wireless
WIRELESS COMMUNICATIONS FACILITY

ASHFORD RELO., CT

353 PUMPKIN HILL ROAD
ASHFORD, CT 06278

DATE: 05/11/15
SCALE: AS NOTED
JOB NO. 14124.000

SPECIFICATIONS

E-12

Sheet No. 24 of 24

ISSUED FOR CONSTRUCTION
DRAWN BY: CAY'D BY
DATE: 07/09/15
REV.

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Calico Partnership
d.b.a. Verizon Wireless

Unit Base Foundation



STRUCTURES

Version = 4.0

| |
|--------------------------|
| Client: Verizon Wireless |
| File: A-284859 |
| Location: Ashford, CT |
| Model: V-25.0 x 240' |

Tower Reactions:

Shear: $S_w := 71 \cdot \text{kips}$
 Moment: $M := 9309 \cdot \text{ft} \cdot \text{kips}$
 Compression: $C_w := 476 \cdot \text{kips}$
 Uplift: $U := 338 \cdot \text{kips}$
 Weight: $W_t := 49 \cdot \text{kips}$

Height := 240 ft

- Soil parameters per soil report
 by: "Terracon, Dated 02/23/15, Project#J2155118"

- Concrete design conforms to the following:

- * Building Code Requirements for Reinforced Concrete (ACI 318-02)
- * 2003 International Building Code (IBC)
- * Structural Standards for Steel Antenna Towers TIA/EIA-222-F-1996



Soil Properties:

Soil strengths: $B_c := 5.0 \cdot \text{ksf}$ (Allowable bearing capacity)
 $\phi := 0 \cdot \text{deg}$ (Internal angle of friction)
 $C_w := 0 \cdot \text{ksf}$ (Undrained shear strength)
 $P_p := 0 \cdot \text{kcf}$ (Ultimate Passive Pressure)
 Soil unit weight: $\gamma := .125 \cdot \text{kcf}$
 Friction Coeff.: $\mu := 0.5$ (Concrete/Soil)

Foundation Dimensions:

Depth: $D := 6.5 \cdot \text{ft}$
 Depth to neglect: $n := 5.5 \cdot \text{ft}$
 Thickness: $T_w := 1.75 \cdot \text{ft}$
 Pier diameter: $d := 3.5 \cdot \text{ft}$
 Tower width: $W' := 25 \cdot \text{ft}$
 Ext. above grade: $E := 0.5 \cdot \text{ft}$
 Clear Cover: $cc := 3.0 \cdot \text{in}$

Soil Compaction Specifications:

Lift Thickness: $LT := 8 \cdot \text{in}$
 Compaction Percent: $CP := 98\%$
 Proctor Test:
 Enter: 698 = ASTM D698 ASTM := 698
 1557 = ASTM D1557

Material Properties:

Concrete Strength: $f'c := 4500 \text{ psi}$
 Concrete unit weight: $\delta\chi := 0.150 \cdot \text{kcf}$
 Rebar yield strength: $f_y := 60000 \cdot \text{psi}$
 Seismic zone (0,1,2,3 or 4): $Z := 2$
 (UBC Fig. 23-2)
 Is tower centroid offset from foundation centroid? (no=0, yes=1) $os := 1$

Initial Width: $W_w := \left[\frac{2 \cdot M \cdot 1.5}{T \cdot (\delta\chi - \gamma) + D \cdot \gamma} \right]^{\frac{1}{3}}$ $W = 31.95 \text{ ft}$ Try: $W_w := 33.0 \cdot \text{ft}$

Concrete volume := $(W^2 \cdot T) + 3 \cdot (D - T + E) \cdot \left(\frac{\pi}{4} \cdot d^2 \right)$ volume = $76.2 \cdot \text{yd}^3$

Concrete weight: $W_c := (\text{volume}) \cdot \delta\chi$ $W_c = 308.6 \cdot \text{kips}$

Soil weight (above footing): $W_s := \left[W^2 \cdot (D - T) - 3 \cdot (D - T + E) \cdot \left(\frac{\pi}{4} \cdot d^2 \right) \right] \cdot \gamma$ $W_s = 627.7 \cdot \text{kips}$

Total weight: $P := W_c + W_s + W_t$ $P = 985.2 \cdot \text{kips}$

EIA/TIA-222 Load Factor [EIA - 3.1.13]

$$LF := \text{if} \left[\text{Height} \leq 700, 1.3, \text{if} \left[\text{Height} \geq 1200, 1.7, 1.3 + \left(\frac{\text{Height} - 700}{1200 - 700} \right) \cdot 0.4 \right] \right] \quad LF = 1.3$$

Passive Pressure:

Passive pressure coeff.: $K_p := \text{if} \left(P_p > 0 \text{ kcf}, 0, \tan \left(45 \cdot \text{deg} + \frac{\phi}{2} \right)^2 \right)$ $K_p = 1.00$

Passive pressure: $P_{pn} := K_p \cdot \gamma \cdot n + 2 \cdot c \cdot \sqrt{K_p}$ $P_{pn} = 0.687 \cdot \text{ksf}$

$P_{pt} := K_p \cdot \gamma \cdot (D - T) + 2 \cdot c \cdot \sqrt{K_p}$ $P_{pt} = 0.594 \cdot \text{ksf}$

$P_{ptop} := \text{if} (n < D - T, P_{pt}, P_{pn})$ $P_{ptop} = 0.687 \cdot \text{ksf}$

$P_{pb} := K_p \cdot \gamma \cdot D + 2 \cdot c \cdot \sqrt{K_p}$ $P_{pb} = 0.812 \cdot \text{ksf}$

$P_{pp} := \frac{P_{ptop} + P_{pb}}{2}$ $P_p = 0.75 \cdot \text{ksf}$

Shear area: $T_{pp} := \text{if} (n < D - T, T, D - n)$ $T_{pp} = 1 \text{ ft}$

$A_{pp} := W \cdot T_{pp}$ $A_{pp} = 33 \text{ ft}^2$

Shear Capacity: (factor of safety: FS := 2.0)

$S_{\text{actual}} := \frac{(P_p \cdot A_{pp}) + \mu \cdot P}{FS}$ $S_{\text{actual}} = 258.69 \cdot \text{kips}$ $> S = 71.00 \cdot \text{kips}$ CHECK = "OK"

Moment resisting at toe: (assume soil is perfectly rigid)

Weight of soil wedge (back face): $W_{sw} := \frac{D \cdot (D \cdot \tan(\phi))}{2} \cdot W \cdot \gamma$ $W_{sw} = 0 \cdot \text{kips}$

Distance from leg to edge of concrete: $O := \text{if} \left(o_s = 0, \frac{W}{2} - \frac{1}{3} \cdot 0.866 \cdot W', \frac{W - 0.866 \cdot W'}{2} \right)$ $O = 5.675 \text{ ft}$

Additional offset of tower weight: $O_a := \frac{W}{2} - \left(\frac{1}{3} \cdot 0.866 \cdot W' + O \right)$ $O_a = 3.608 \text{ ft}$

Resisting moment: $M_{rwt} := (W_c + W_s) \cdot \frac{W}{2} + W_t \cdot \left(\frac{W}{2} - O_a \right)$ $M_{rwt} = 16079.73 \cdot \text{ft} \cdot \text{kips}$

$M_{rp} := (P_p \cdot A_{pp}) \cdot \frac{T_{pp}}{3}$ $M_{rp} = 8.25 \cdot \text{ft} \cdot \text{kips}$

$M_{rsw} := W_{sw} \cdot \left(W + D \cdot \frac{\tan(\phi)}{3} \right)$ $M_{rsw} = 0 \cdot \text{ft} \cdot \text{kips}$

Total resisting moment: $M_{rt} := M_{rwt} + M_{rp} + M_{rsw}$ $M_{rt} = 16087.98 \cdot \text{ft} \cdot \text{kips}$

Overturning moment: $M_o := M + S \cdot (D + E)$ $M_o = 9806 \cdot \text{ft} \cdot \text{kips}$

Factor of safety: $FS := \frac{M_{rt}}{M_o}$ $FS = 1.64$ $> FS_{\text{required}} = 1.50$

CHECK = "OK"

Compression exerted by foundation:

Area of mat: $Area := W^2$ Area = 1089 ft²

Section modulus: $SM := \frac{W^3}{6}$ SM = 5989.5 ft³

Pressure exerted: $P_{pos} := \frac{P}{Area} + \frac{M_o}{SM}$ P_{pos} = 2.54 · ksf < B_c = 5.00 · ksf

$P_{neg} := \frac{P}{Area} - \frac{M_o}{SM}$ P_{neg} = -0.732 · ksf < 0 ksf

Note = "The stress resultant is NOT within the kern. Bearing area has been adjusted below."

Load eccentricity: $e_{\frac{M_o}{P}} := \frac{M_o}{P}$ e = 9.953 ft $P_{adj} := \frac{2 \cdot P}{3 \cdot W \cdot \left(\frac{W}{2} - e\right)}$ P_{adj} = 3.04 · ksf

Adjusted applied pressure: $q_a := if(P_{neg} \geq 0 \cdot ksf, P_{pos}, P_{adj})$
 (assume symmetric condition controls) q_a = 3.04 · ksf < B_c = 5.00 · ksf CHECK = "OK"

Column compression capacity: (ACI 10.15)

Compression reaction: $\phi_{\frac{M_o}{P}} := 0.65$ (ACI 9.3.2.2)

$P_c := \phi \cdot 0.85 \cdot f'_c \cdot \text{psi} \cdot \left(\frac{d^2}{4} \cdot \pi\right)$ P_c = 3444.56 · kips > LF · C = 618.80 · kips CHECK = "OK"

Concrete shear strength:

One way beam action at d from column face: (ACI 11.3.1.1)

Effective depth: $d_c := T - cc - 0.5 \cdot \text{in}$ d_c = 17.5 · in

Factored load intensity: $q_s := LF \cdot \frac{C}{W^2}$ q_s = 0.568 · ksf
(ACI 9.2.1)

Required shear: $V_n := \frac{q_s \cdot \left(0 - \frac{1}{2} \cdot d - d_c\right) \cdot W}{\phi}$ V_n = 61.672 · kips
($\phi_{\frac{M_o}{P}} := 0.75$ - ACI 9.3.2.3)

Available shear: $V_c := 2.0 \cdot \sqrt{f'_c} \cdot \text{psi} \cdot W \cdot d_c$ V_c = 929.757 · kips
(ACI 11.3.1.1)

$V_c = 929.76 \cdot \text{kips} > V_n = 61.67 \cdot \text{kips}$ CHECK = "OK"

Two way action at d/2 from column face: (ACI 11.12.2.1)

Perimeter: $P_o := (d + d_c) \cdot \pi$ P_o = 15.577 ft

Required shear: $V_n := q_s \cdot \frac{W^2 - (d + d_c)^2 \cdot \frac{\pi}{4}}{\phi}$ V_n = 810.437 · kips
($\phi_{\frac{M_o}{P}} := 0.75$ - ACI 9.3.2.3)

Available shear: $V_c := 4.0 \cdot \sqrt{f'_c} \cdot \text{psi} \cdot d_c \cdot P_o$ V_c = 877.751 · kips
(ACI 11.12.2.1)

$V_c = 877.75 \cdot \text{kips} > V_n = 810.44 \cdot \text{kips}$ CHECK = "OK"

Pier reinforcement:

Cross sectional area of pier: $A_c := d^2 \cdot \frac{\pi}{4}$ $A_c = 1385.442 \cdot \text{in}^2$

Minimum area of steel: Percent (min) := if (Z > 2, 1.0%, 0.50 · 1.0%)
 (ACI 10.8.4 & 10.9.1) $A_{stmin} := A_c \cdot (\text{Percent (min)})$ $A_{stmin} = 6.927 \cdot \text{in}^2$

Bending and tension requirements:

Bar Size: $s_c := 9$ Area: $A_{bc} := \text{area}_{s_c}$ $A_{bc} = 1.00 \cdot \text{in}^2$

Quantity: $m_c := 19$ Diameter: $d_{bc} := \text{dia}_{s_c}$ $d_{bc} = 1.128 \cdot \text{in}$

Total area of steel: $A_{st} := m_c \cdot A_{bc}$
 $A_{st} = 19.00 \cdot \text{in}^2 > A_{stmin} = 6.93 \cdot \text{in}^2$ CHECK = "OK"

Treat the circular cage of reinforcement as an equivalent hollow circle (pipe). Set the outer diameter of the pipe to the diameter of the cage (d_o) and solve for the inner diameter (d_i) using the area of a pipe (A) equation.

Cage diameter: $d_o := d - 2 \cdot cc$ $d_o = 3.00 \text{ ft}$

Given $A_{st} = \frac{\pi \cdot (d_o^2 - d_i^2)}{4}$ $d_i := \text{Find}(d_i)$ $d_i = 2.972 \text{ ft}$

$A = \frac{\pi \cdot (d_o^2 - d_i^2)}{4}$ $A = 19 \cdot \text{in}^2 = A_{st} = 19 \cdot \text{in}^2$

Section Modulus: $SM = \pi \cdot \frac{d_o^4 - d_i^4}{32 \cdot d_o}$ $SM = 169.404 \cdot \text{in}^3$

Combined Stress: $\sigma := \frac{U}{A_{st}} + \frac{0.5 \cdot S \cdot (D - T + E)}{SM}$
 $\sigma = 30.99 \cdot \text{ksi} < (f_y \cdot 0.60) = 36 \cdot \text{ksi}$ CHECK = "OK"

Bar separation: $B_s := \frac{d_o \cdot \pi}{m_c} - d_{bc}$ $B_s = 4.82 \cdot \text{in}$ CHECK = "OK"

Reinforcement Development length:

Tension: (ACI 12.2.3 & 12.2.4)

$\alpha := 1.0$ $\alpha = 1$

$\beta := 1.0$ $\beta = 1$

$\gamma := \text{if}(s_c > 6, 1.0, 0.8)$ $\gamma = 1$

$\lambda := 1.0$ $\lambda = 1$

$k := 0 \cdot \text{in}$ $k = 0 \cdot \text{in}$

$c_w := \min\left(\frac{B_s}{2} + d_{bc}, cc + \frac{d_{bc}}{2}\right)$ $c = 3.54 \cdot \text{in}$

$c' := \min\left(2.5, \frac{c + k}{d_{bc}}\right)$ $c' = 2.5$

$L_{dt} := \frac{3 \cdot f_y}{40 \cdot \sqrt{f'c \cdot \text{psi}}} \cdot \frac{\alpha \cdot \beta \cdot \gamma \cdot \lambda}{c'} \cdot d_{bc}$ $L_{dt} = 30.267 \cdot \text{in}$

Reinforcement Development length: - (continued)

Minimum development length: (ACI 12.2.1)

$$L_{dtw} := \text{if}(L_{dt} < 12 \cdot \text{in}, 12 \cdot \text{in}, L_{dt}) \quad L_{dt} = 30.267 \cdot \text{in}$$

Compression: (ACI 12.3.2)

$$L_{db} := 0.02 \cdot d_{bc} \cdot \frac{f_y}{\sqrt{f'c \cdot \text{psi}}} \quad L_{dbw} := L_{db} \cdot \frac{\sigma}{(f_y \cdot 0.60)} \quad L_{db} = 17.371 \cdot \text{in}$$

$$L_{dmin} := 0.0003 \cdot d_{bc} \cdot \frac{f_y}{\text{psi}} \quad L_{dminw} := L_{db} \cdot \frac{\sigma}{(f_y \cdot 0.60)} \quad L_{dmin} = 14.954 \cdot \text{in}$$

$$L_{dc} := \max(8 \cdot \text{in}, L_{dmin}, L_{db}) \quad L_{dc} = 17.371 \cdot \text{in}$$

Length available in pier: $L_{pier} := (D + E) - T - cc$

Tension: $L_{pier} = 60.00 \cdot \text{in} > L_{dt} = 30.27 \cdot \text{in}$

Compression: $L_{pier} = 60.00 \cdot \text{in} > L_{dc} = 17.37 \cdot \text{in}$

CHECK = "OK"

CHECK = "OK"

Length available in pad: $L_{pad} := T - cc$

Tension: $L_{pad} = 18.00 \cdot \text{in} > L_{dt} = 30.27 \cdot \text{in}$

Compression: $L_{pad} = 18.00 \cdot \text{in} > L_{dc} = 17.37 \cdot \text{in}$

CHECK = "HOOK REQUIRED"

CHECK = "OK"

Rebar Hook Design:

Basic development length:
(ACI 12.5.2 & 12.5.3)

$$\alpha := \text{if}[(cc \geq 2.5 \cdot \text{in}) \cdot (s_c \leq 11), 0.7, 1] \quad \alpha = 0.7$$

$$\beta := 1.0 \quad \beta = 1$$

$$\lambda := 1.0 \quad \lambda = 1$$

$$L_{dh} := 0.02 \cdot \alpha \cdot \beta \cdot \lambda \cdot \frac{f_y}{\sqrt{f'c \cdot \text{psi}}} \cdot d_{bc} \quad L_{dh} = 14.125 \cdot \text{in}$$

Minimum development length: (ACI 12.5.1)

$$L_{dhw} := \max(8 \cdot d_{bc}, 6 \cdot \text{in}, L_{dh}) \quad L_{dh} = 14.125 \cdot \text{in}$$

Length available in pad: $L_{pad} = 18.00 \cdot \text{in} > L_{dh} = 14.12 \cdot \text{in}$

CHECK = "OK"

Hook extension length: (ACI 7.1.2)

$$l_{hex} := 12 \cdot d_{bc} \quad l_{hex} = 13.536 \cdot \text{in}$$

Length available in pad: $L_{havail} := \frac{W'}{2} - \frac{d}{2} - cc - \text{if}(s_c < 9, 3, 4) \cdot d_{bc}$

$$L_{havail} = 121.49 \cdot \text{in} > l_{hex} = 13.54 \cdot \text{in}$$

CHECK = "OK"

Pad reinforcement: Required Bending Capacity: ($\phi_w = 0.90$ - ACI 9.3.2.1)

MDSolids Geometry Input: (Case 1)

Total Beam Length:

$$B_{L1} := W$$

$$B_{L1} = 33 \text{ ft}$$

Location of Left Support:

$$S_{L1} := 0$$

$$S_{L1} = 5.68 \text{ ft}$$

Location of Right Support:

$$S_{R1} := W - 0$$

$$S_{R1} = 27.32 \text{ ft}$$

MDSolids Geometry Input: (Case 2)

Total Beam Length:

$$B_{L2} := W$$

$$B_{L2} = 33 \text{ ft}$$

Location of Left Support:

$$S_{L2} := (W - W') \cdot 0.5$$

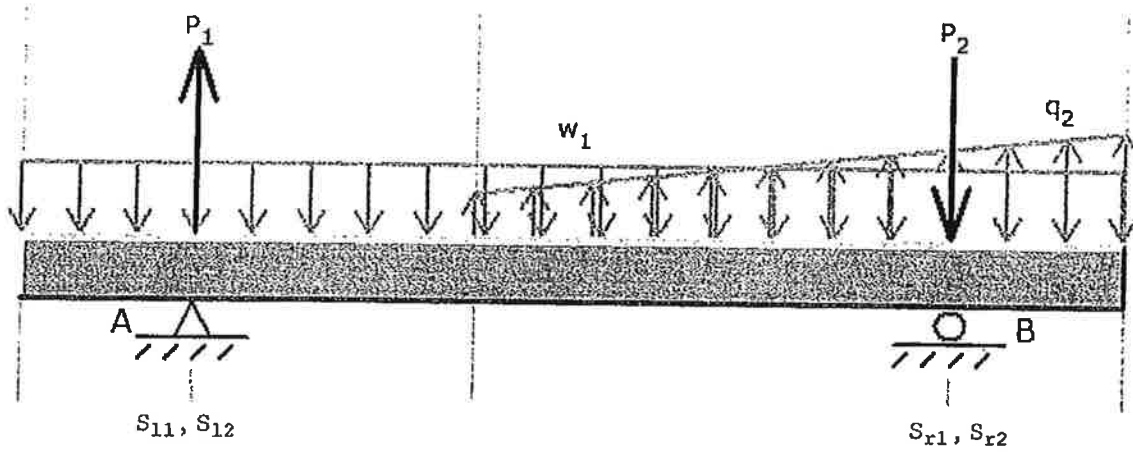
$$S_{L2} = 4 \text{ ft}$$

Location of Right Support:

$$S_{R2} := S_{L2} + W'$$

$$S_{R2} = 29 \text{ ft}$$

Pad Reinforcement: - (continued)



MDSolids Load Input (Case 1 & Case 2)

Uplift: $P_1 := U$ $P_1 = 338 \text{ kips}$

Compression $P_2 := C$ $P_2 = 476 \text{ kips}$

Weight of overburden: $w_1 := \frac{(W_c + W_s)}{W}$ $w_1 = 28.37 \text{ klf}$
 (Distributed)

Applied over the beam starting at 0' and ending at $W = 33 \text{ ft}$

Distributed Soil Pressure: $q_{2L} := 0$ $q_{2R} := q_a \cdot W$ $q_{2R} = 100.82 \text{ klf}$
 (Linearly Increasing)

This linearly increasing load is applied from $e = 9.95 \text{ ft}$ to $W = 33 \text{ ft}$

MDSolids Design Results: (Case 1)

MDSolids Design Results: (Case 2)

Max. Moment: $M_{max1} := 1030 \text{ ft} \cdot \text{kips}$

Max. Moment: $M_{max2} := 530 \text{ ft} \cdot \text{kips}$

Maximum Moment: $M_{max} := \max(M_{max1}, M_{max2})$ $M_{max} = 1030 \text{ ft} \cdot \text{kips}$

Maximum Moment w/ACI Strength Reduction Factor and EIA/TIA Load Increase Factor:

$M_n := \frac{LF}{\phi} \cdot M_{max}$ $M_n = 1487.778 \text{ ft} \cdot \text{kips}$

$\beta_w := \text{if} \left[f'c \leq 4000, 0.85, \text{if} \left[f'c \geq 8000, 0.65, 0.85 - \left(\frac{f'c - 4000}{1000} \right) \cdot 0.05 \right] \right]$ $\beta = 0.825$
(ACI 10.2.7.3)

Effective Beam Width: $W_e := W' \cdot 0.866 + d$ $W_e = 25.15 \text{ ft}$

Required Steel: $A_{st} := \frac{M_n}{0.9 \cdot f_y \cdot d_c}$ $A_{st} = 18.892 \text{ in}^2$

$a := \frac{A_{st} \cdot f_y}{\beta \cdot f'c \cdot \text{psi} \cdot W_e}$ $a = 1.012 \text{ in}$

$A_{st} := \frac{M_n}{f_y \cdot \left(d_c - \frac{a}{2} \right)}$ $A_{st} = 17.509 \text{ in}^2$

$\rho := \frac{A_{st}}{W_e \cdot T}$ $\rho = 0.0028$

Pad Reinforcement: - (continued)

Temperature & shrinkage $\rho_{sh} := \text{if}(f_y \geq 60000 \cdot \text{psi}, 0.0018, 0.0020)$ $\rho_{sh} = 0.0018$
 (ACI 7.12.2.1):

$$A_{st} := \text{if}\left(\rho \geq \frac{\rho_{sh}}{2}, A_{st}, \rho_{sh} \cdot W_e \cdot \frac{T}{2}\right)$$
 $A_{st} = 17.509 \cdot \text{in}^2$

Bars required in pad both ways: (width: $W = 33 \text{ ft}$)

Bar Size: $s_p := 8$ Area: $A_{bp} := \text{area}_{s_p}$ $A_{bp} = 0.79 \cdot \text{in}^2$
 Diameter: $d_{bp} := \text{dia}_{s_p}$ $d_{bp} = 1.000 \cdot \text{in}$

Quantity: $m_{pad} := \frac{A_{st}}{A_{bp}} \cdot \left(\frac{W}{W_e}\right)$ $m_{pad} = 29.08$ Use: $m_p := 49$

Bar separation: $B_s := \left(\frac{W - 2 \cdot cc - d_{bp}}{m_p - 1}\right) - d_{bp}$ $B_s = 7.10 \cdot \text{in}$ CHECK = "OK"

Development length of Pad Reinforcement: (ACI 12.2.3 & 12.2.4)

$$\alpha := \text{if}[T > 12 \cdot \text{in} + 2 \cdot (cc + d_{bp}), 1.3, 1.0] \quad \alpha = 1.3$$

$$\beta := 1.0 \quad \beta = 1$$

$$\gamma := \text{if}(s_p > 6, 1.0, 0.8) \quad \gamma = 1$$

$$\lambda := 1.0 \quad \lambda = 1$$

$$k := 0 \cdot \text{in} \quad k = 0 \cdot \text{in}$$

$$c := \min\left(\frac{B_s}{2} + d_{bp}, cc + \frac{d_{bp}}{2}\right) \quad c = 3.5 \cdot \text{in}$$

$$c' := \min\left(2.5, \frac{c + k}{d_{bp}}\right) \quad c' = 2.5$$

$$L_d := \frac{3 \cdot f_y}{40 \cdot \sqrt{f'_c \cdot \text{psi}}} \cdot \frac{\alpha \cdot \beta \cdot \gamma \cdot \lambda}{c'} \cdot d_{bp} \quad L_d = 34.883 \cdot \text{in}$$

Minimum development length: (ACI 12.2.1)

$$L_{dt} := \text{if}(L_{dt} < 12 \cdot \text{in}, 12 \cdot \text{in}, L_d) \quad L_d = 34.883 \cdot \text{in}$$

Length available in pad: $L_{pad} := \frac{W}{2} - \frac{W'}{2} - cc$

$$L_{pad} = 45.0 \cdot \text{in} > L_d = 34.9 \cdot \text{in} \quad \text{CHECK} = \text{"OK"}$$

Width required to ensure space for column hooks in pad:

$$w_{req} := \left(\frac{W'}{2} + \frac{d}{2} + \text{if}(s_c < 9, 16, 17) \cdot d_{bc}\right) \cdot 2$$

$$W = 33.0 \text{ ft} > w_{req} = 31.7 \cdot \text{ft} \quad \text{CHECK} = \text{"OK"}$$

Determination of Tie size and spacing requirements for columns: (ACI 7.10.5)

Minimum tie bar size: $d_{tie\min} := \text{if}(s_c \leq 10, 3, 4)$ $d_{tie\min} = 3$ Use: $d_{tie} := 4$

Factor based on seismic zone: (ACI 21.3.3.2) $z := \text{if}(Z < 2, 1, 0.5)$ $z = 0.5$

$s_{lim1} := 16 \cdot d_{bc} \cdot z$ $s_{lim1} = 9.024 \cdot \text{in}$

$s_{lim2} := 48 \cdot \frac{d_{tie}}{8} \cdot \text{in} \cdot z$ $s_{lim2} = 12 \cdot \text{in}$

$s_{lim3} := D \cdot z^2$ $s_{lim3} = 19.5 \cdot \text{in}$

$s_{lim4} := \text{if}(z > 0.5, 18.0, 12.0) \cdot \text{in}$ $s_{lim4} = 12 \cdot \text{in}$

Maximum tie spacing: $s_{tie} := \min(s_{lim1}, s_{lim2}, s_{lim3}, s_{lim4})$ $s_{tie} = 9.024 \cdot \text{in}$

Number of ties required: $n_t := \frac{D - T + E}{s_{tie}} + 2$ $n_t = 9.0$ Use: $n_{tie} := 10$

CHECK = "OK"

Foundation Design Summary

Soil Parameters: Soil parameters per soil report
by = "Terracon, Dated 02/23/15, Project#J2155118"

Allowable Soil Bearing Pressure: $B_c = 5.00 \cdot \text{ksf}$

Allowable Passive Pressure = $0.063 \cdot \text{kcf}$

Dimensions: Base Width: $W = 33.00 \text{ ft}$
Depth below grade: $D = 6.50 \text{ ft}$
Extension above grade: $E = 6 \cdot \text{in}$
Pier Diameter: $d = 3.50 \text{ ft}$
Pad Thickness: $T = 1.75 \text{ ft}$
Concrete Volume: $\text{volume} = 76.2 \cdot \text{yd}^3$

Note = "CENTROID OF THE TOWER IS OFFSET FROM THE CENTROID OF THE FOUNDATION."
(ADDITIONAL ECCENTRIC LOAD WILL BE INDUCED IF THE TOWER IS OFFSET)

| Reinforcement: | <u>Quantity</u> | <u>Size</u> | |
|-----------------------|-----------------|---------------|--|
| Pad: | $m_p = 49$ | $s_p = 8$ | equally spaced, both ways, top & bottom |
| Pier: | $m_c = 19$ | $s_c = 9$ | equally spaced on $d_o = 3 \text{ ft}$ cage |
| Ties: | $n_{tie} = 10$ | $d_{tie} = 4$ | per UBC spacing & standard overlap requirements |

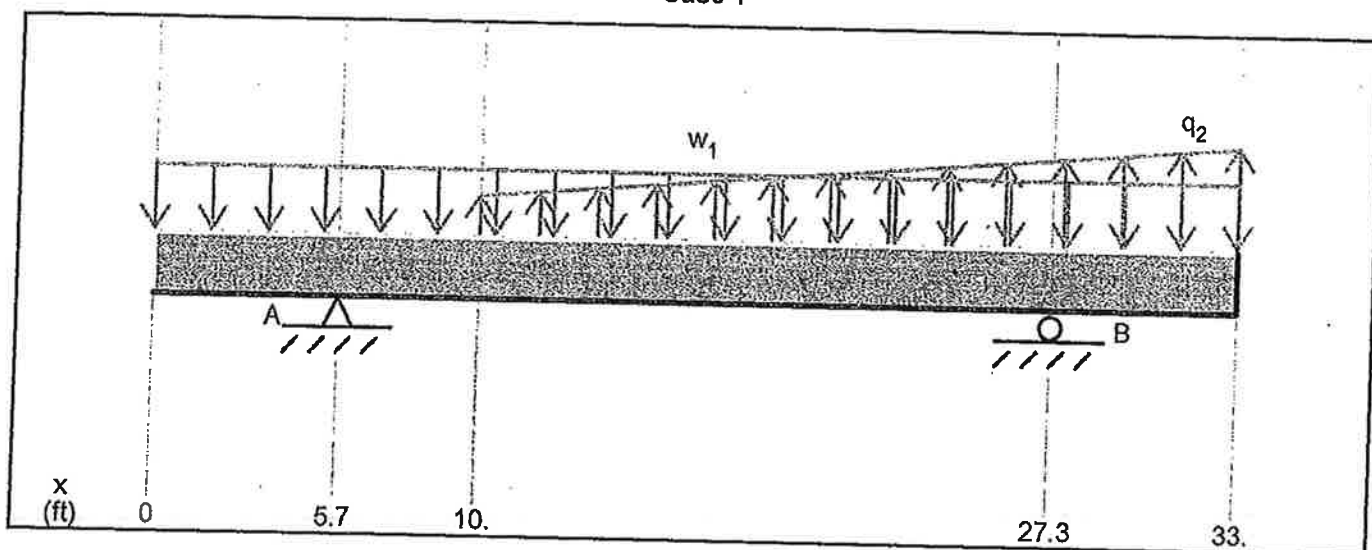
Use standees to support the top rebar above the bottom rebar in the mat.
Concrete clear cover: $cc = 3 \cdot \text{in}$

Material strengths: Concrete strength: $f'_c = 4500 \text{ psi}$
Rebar yield strength: $f_y = 60 \cdot \text{ksi}$

Compaction Notes: ALL FILL SHOULD BE PLACED IN LOOSE LEVEL LIFTS OF NO MORE THAN
 $LT = 8 \cdot \text{in}$ THICK. FILL MATERIALS SHOULD BE CLEAN AND FREE OF ORGANIC
AND FROZEN MATERIALS OR ANY OTHER DELETERIOUS MATERIALS. COMPACT FILL
TO $CP = 98 \cdot \%$ OF MAXIMUM DRY DENSITY IN ACCORDANCE WITH
ASTM = "D698 STANDARD PROCTOR TEST."

Additional Notes: None

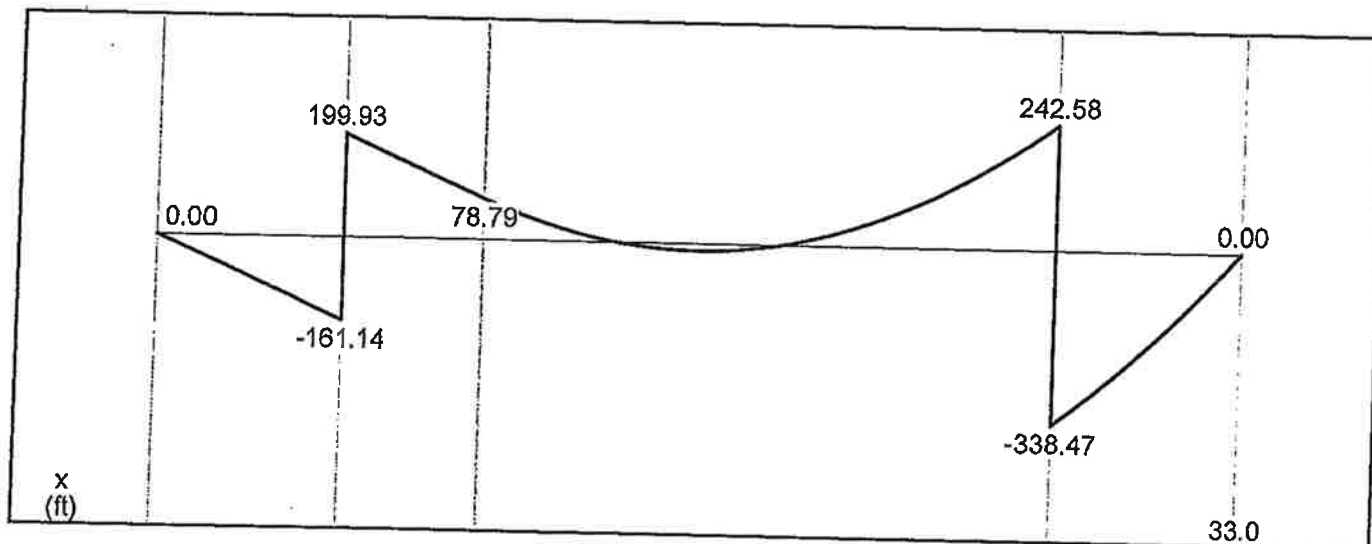
Case 1



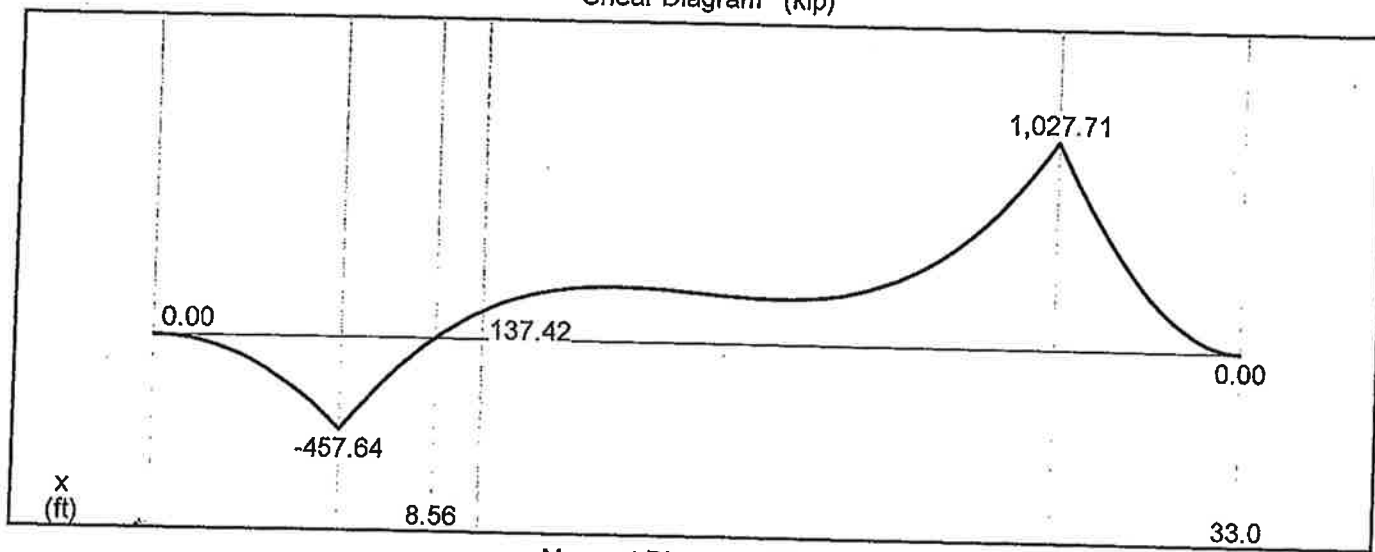
Load Diagram

$w_1 = 28.37$ kip/ft (down)
 $q_2 = 0.0$ to 100.32 kip/ft (up)

$A_y = 361.07$ kip (up)
 $B_y = 581.05$ kip (down)

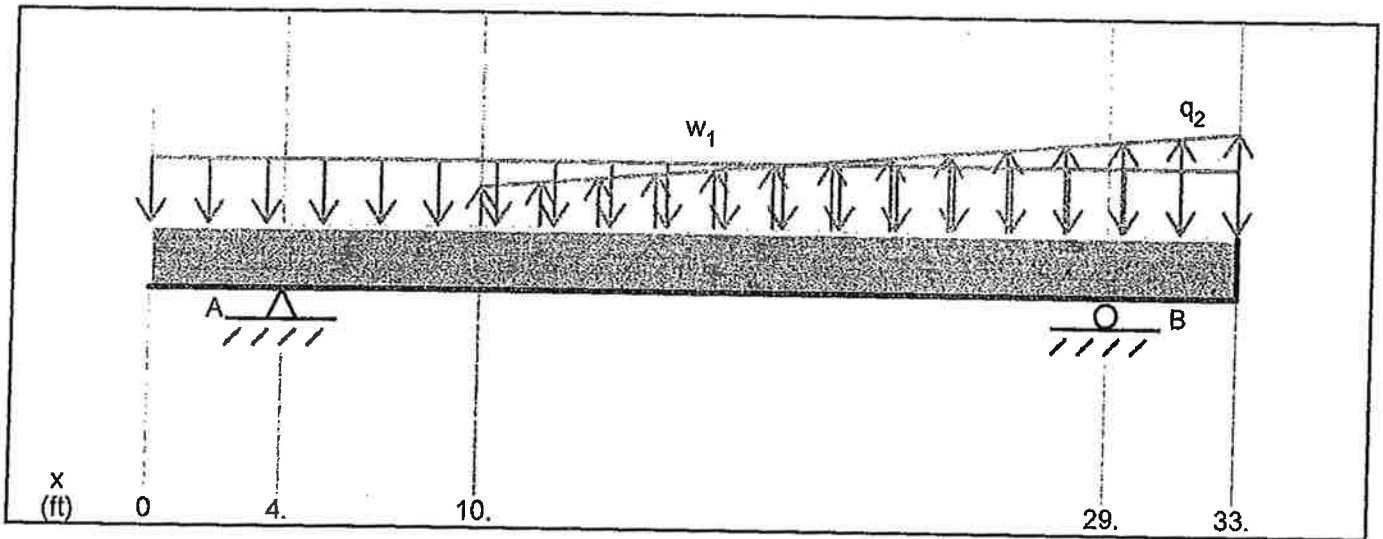


Shear Diagram (kip)



Moment Diagram (kip-ft)

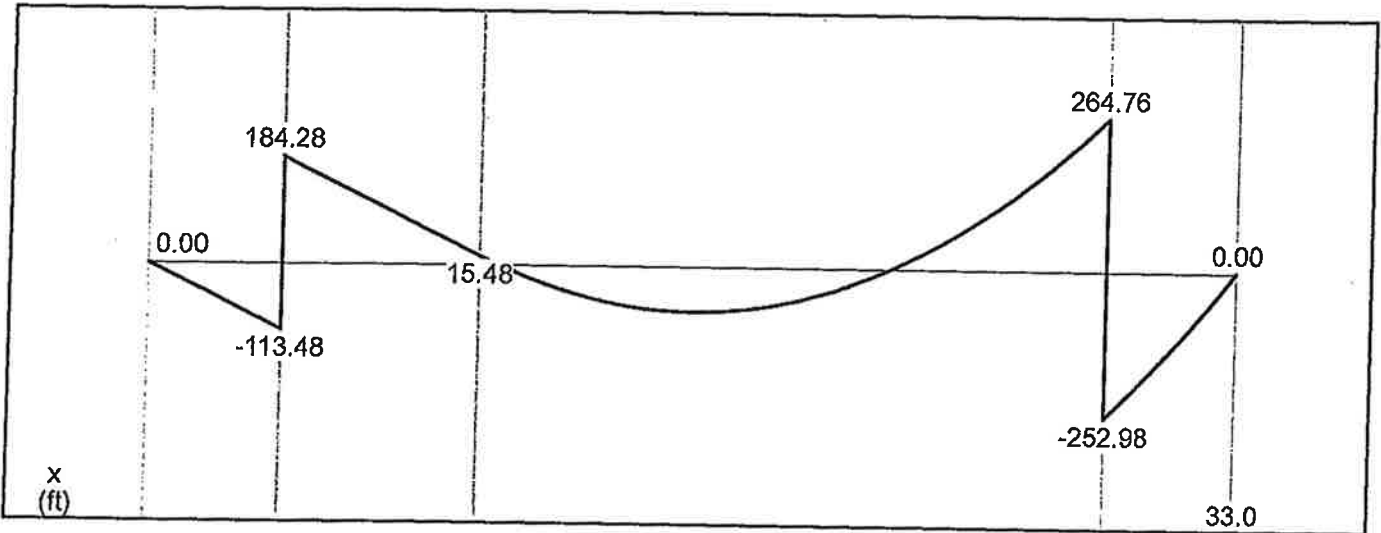
Case 2



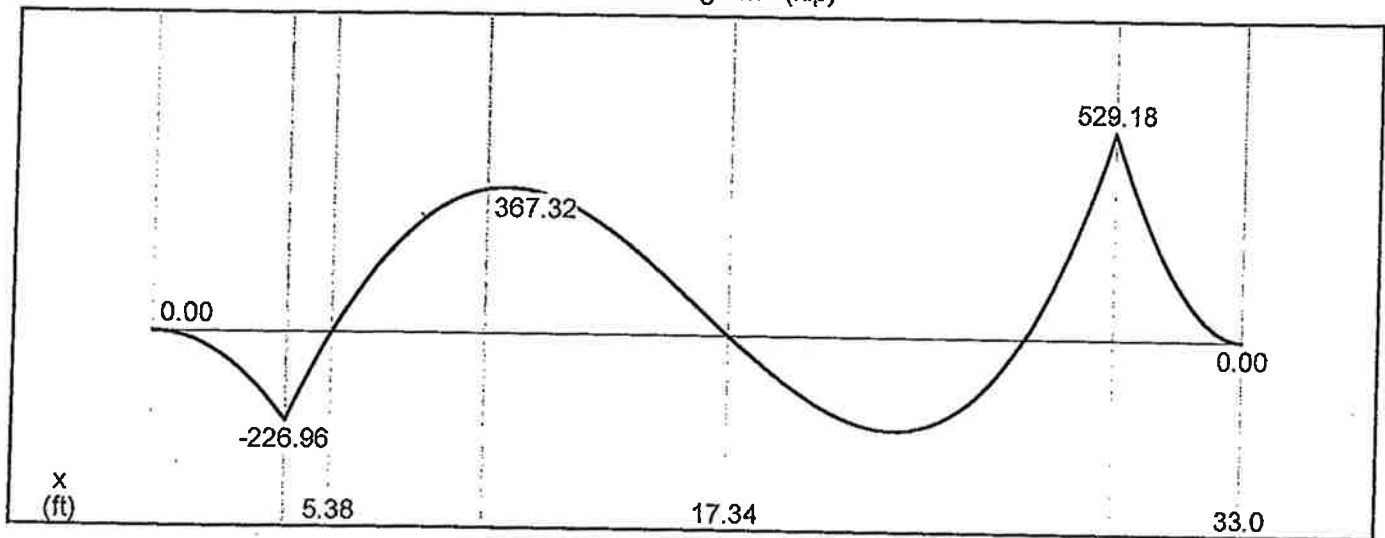
Load Diagram

$w_1 = 28.37$ kip/ft (down)
 $q_2 = 0.0$ to 100.32 kip/ft (up)

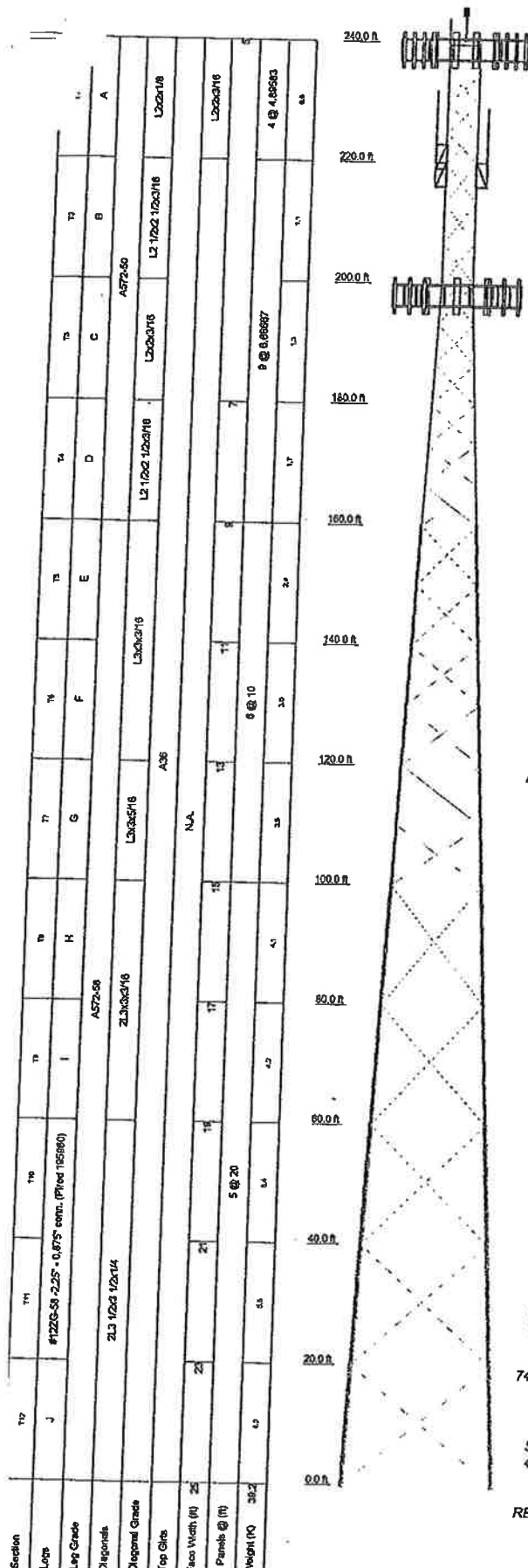
$A_y = 297.76$ kip (up)
 $B_y = 517.74$ kip (down)



Shear Diagram (kip)



Moment Diagram (kip-ft)



DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
|--|-----------|------------------------------------|-----------|
| Beacon | 240 | 24" Standoff | 210 |
| Beacon Extender (4) E03062 | 240 | WHSP (2.88" X 12) | 218 |
| 1/2" x 4" lighting rod | 240 | 24" Standoff | 218 |
| (2) HBXX-6517DS-VTM | 240 | (2) 7770.00 | 198 |
| (2) HBXX-6517DS-VTM | 240 | (2) 7770.00 | 198 |
| (2) 2" x 84" Sch. 40 | 240 | (2) 2" x 96" Sch. 40 | 198 |
| (2) 2" x 84" Sch. 40 | 240 | (2) 2" x 96" Sch. 40 | 198 |
| (2) 2" x 84" Sch. 40 | 240 | (2) 2" x 96" Sch. 40 | 198 |
| (2) LNX-6514DS-VTM | 240 | AM-X-CD-17-65-00T-RET | 198 |
| (2) LNX-6514DS-VTM | 240 | AM-X-CD-17-65-00T-RET | 198 |
| (2) LNX-6514DS-VTM | 240 | AM-X-CD-17-65-00T-RET | 198 |
| (2) 2" x 84" Sch. 40 | 240 | 2" x 96" Sch. 40 | 198 |
| (2) 2" x 84" Sch. 40 | 240 | 2" x 96" Sch. 40 | 198 |
| (2) 2" x 84" Sch. 40 | 240 | 2" x 96" Sch. 40 | 198 |
| Alcatel-Lucent RRH2X50-AV5 | 240 | (2) Powertech LGP2140X TMA-DD-1900 | 198 |
| Alcatel-Lucent RRH2X50-AV5 | 240 | (2) Powertech LGP2140X TMA-DD-1900 | 198 |
| Alcatel-Lucent RRH2X50-AV5 | 240 | (2) Powertech LGP2140X TMA-DD-1900 | 198 |
| Alcatel-Lucent RRH2X50-PCS | 240 | (2) Powertech LGP21903 | 198 |
| Alcatel-Lucent RRH2X50-PCS | 240 | (2) Powertech LGP21903 | 198 |
| Alcatel-Lucent RRH2X50-PCS | 240 | (2) Powertech LGP21903 | 198 |
| DB-T1-62-8AB-02 Assumed (20.07' x 11.22' x 7.2') | 240 | (2) Powertech 7020.00 DualBand RET | 198 |
| DB-T1-62-8AB-02 Assumed (20.07' x 11.22' x 7.2') | 240 | (2) Powertech 7020.00 DualBand RET | 198 |
| DB-T1-62-8AB-02 Assumed (20.07' x 11.22' x 7.2') | 240 | (2) Powertech 7020.00 DualBand RET | 198 |
| 12 V Frame | 240 | (2) BRUS11 (20" X 17" X 7') | 198 |
| 12 V Frame | 240 | (2) BRUS11 (20" X 17" X 7') | 198 |
| 12 V Frame | 240 | (2) BRUS11 (20" X 17" X 7') | 198 |
| WHSP (2.88" X 12) | 221 | Polyphaser (12"x12"x8') | 198 |
| 24" Standoff | 221 | 12 V Frame | 198 |
| WHSP (2.88" X 12) | 218 | 12 V Frame | 198 |

SYMBOL LIST

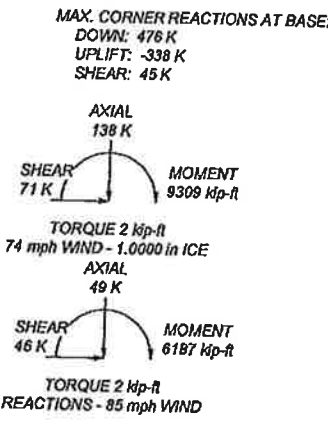
| MARK | SIZE | MARK | SIZE |
|------|---|------|--|
| A | P-2.50" - 0.75" conn-20" -C (Prod 226160) | F | #122G-58 - 1.75" - 1.00" conn-TR1 (Prod 195213) |
| B | P-4.00" - 0.75" conn-20" -C-Trans-69-49 (Prod 226184) | G | #122G-58 - 1.75" - 1.00" conn (Prod 195217) |
| C | P-6.00" - 0.75" conn-Trans-20" -C (Prod 226200) | H | #122G-58 - 2.00" - 0.875" conn-TR3 (Prod 195637) |
| D | P-6.00" - 0.75" conn-Trans-20" -C (Prod 229377) | I | #122G-58 - 2.00" - 0.875" conn (Prod 195639) |
| E | #122G-58 - 1.50" - 1.00" conn (Prod 194651) | J | #122G-58 - 2.50" - 0.875" conn-TR4 (Prod 195962) |

MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |
|---------|--------|--------|---------|--------|--------|
| A572-50 | 50 ksi | 65 ksi | A572-58 | 58 ksi | 75 ksi |
| A36 | 36 ksi | 58 ksi | | | |

TOWER DESIGN NOTES

1. Tower is located in Windham County, Connecticut.
2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 74 mph basic wind with 1.00 in ice.
4. Deflections are based upon a 60 mph wind.
5. TOWER RATING: 99.2%

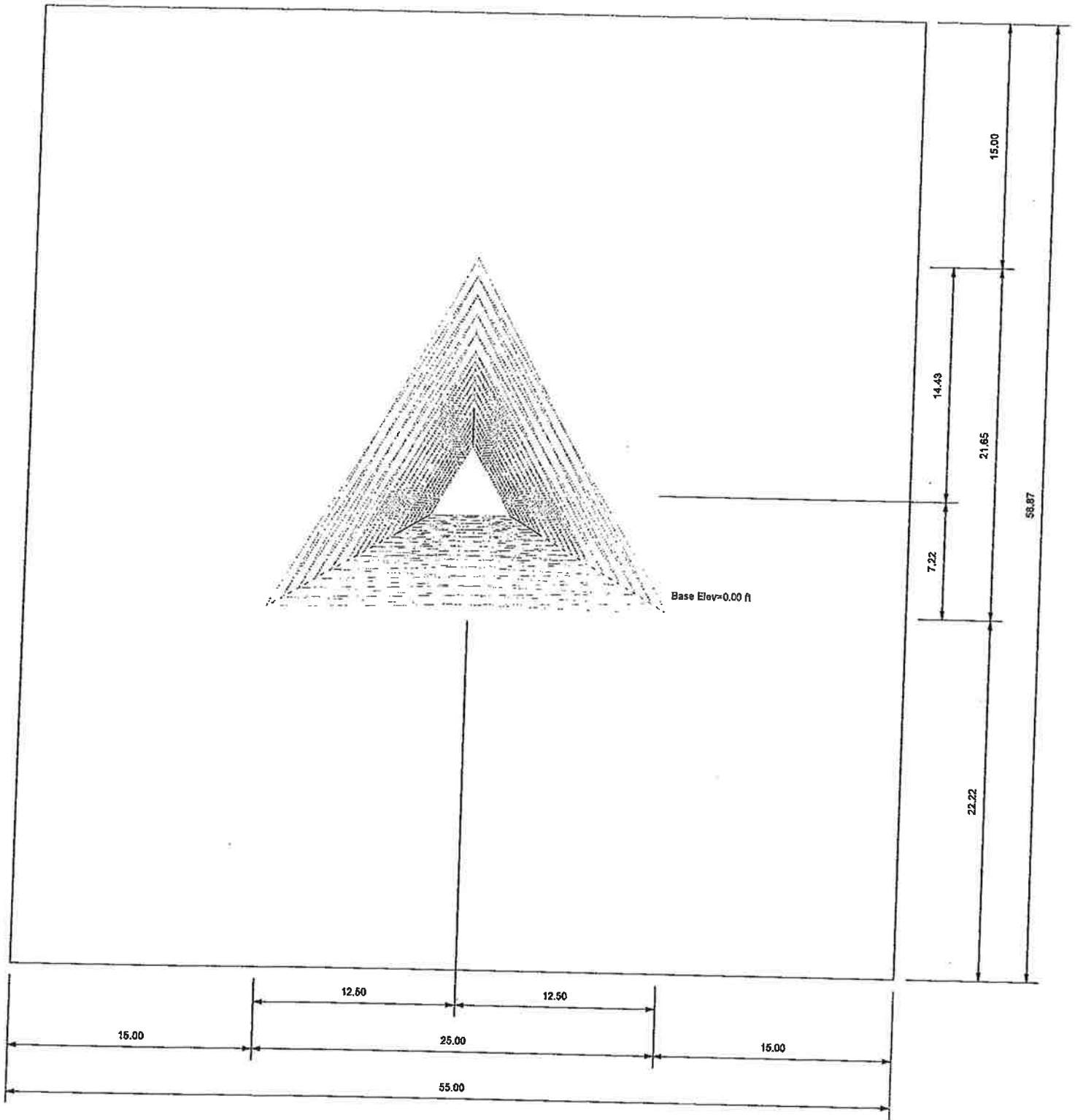



APR 01 2015

valmont 1545 Pidco Dr. Plymouth, IN
 STRUCUTURES
 Valmont Industries, Inc. - Specialty Structures Group Phone: (574) 938-4221 FAX: (574) 938-8458

Job: 284859
 Project: V-25 x 240' - Ashford, CT
 Client: Verizon Wireless Drawn by: JAK App'd: [Signature]
 Code: TIA/EIA-222-F Date: 03/30/15 Scale: NTS
 Pch: [Signature] Dwg No: E-1

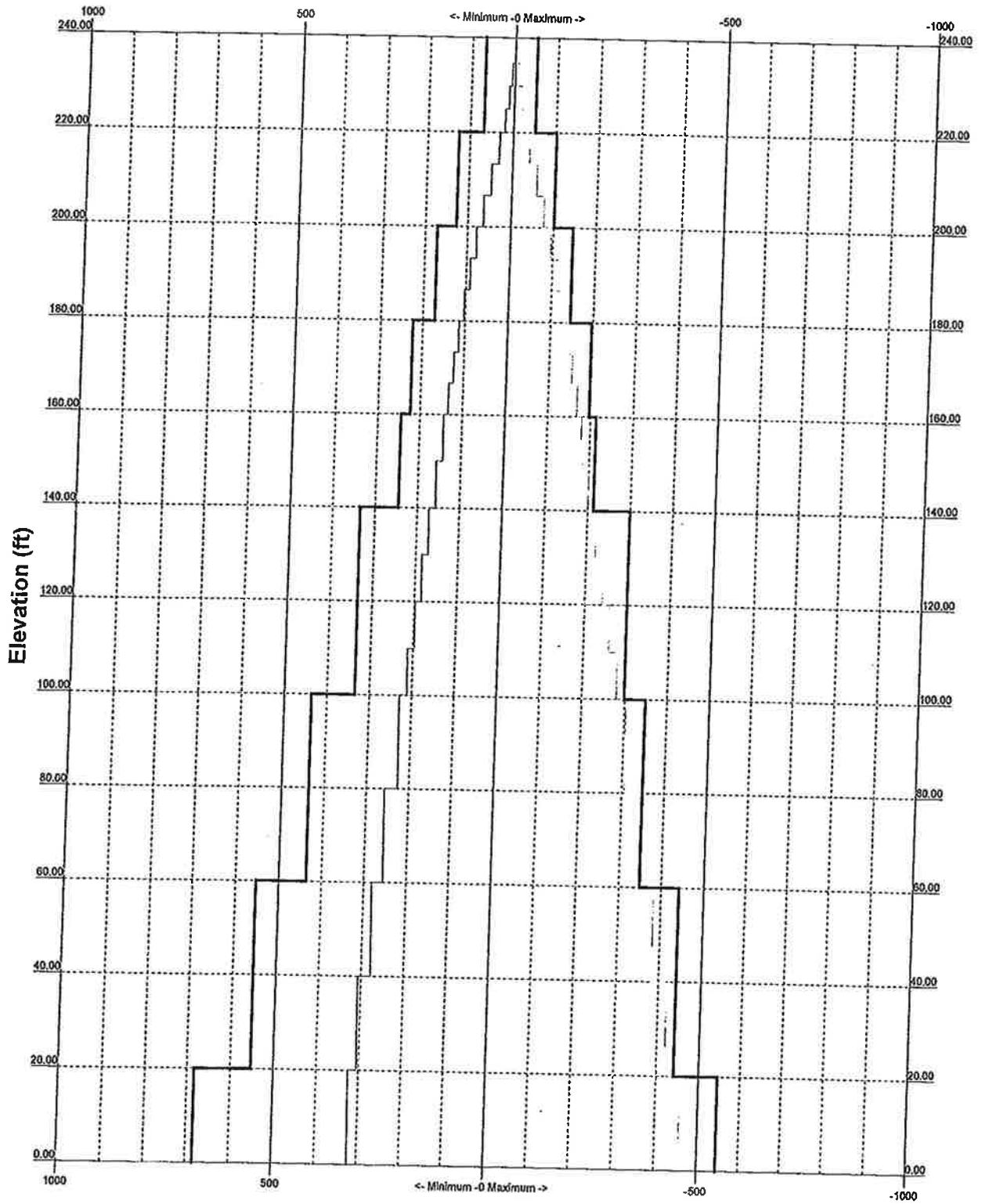
Plot Plan
Total Area - 0.07 Acres



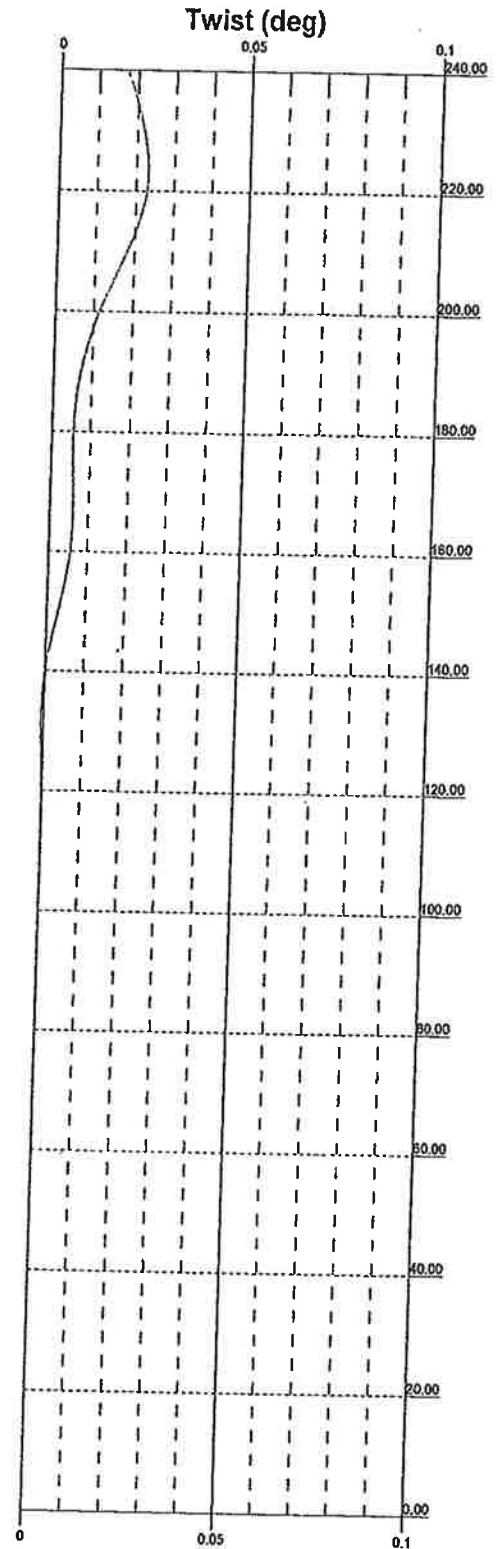
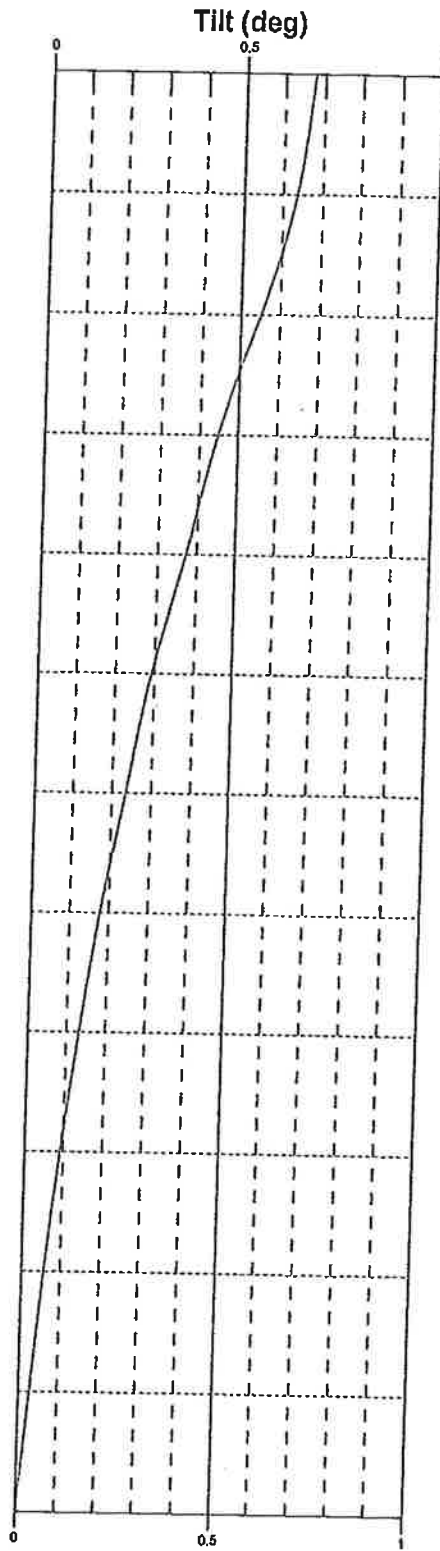
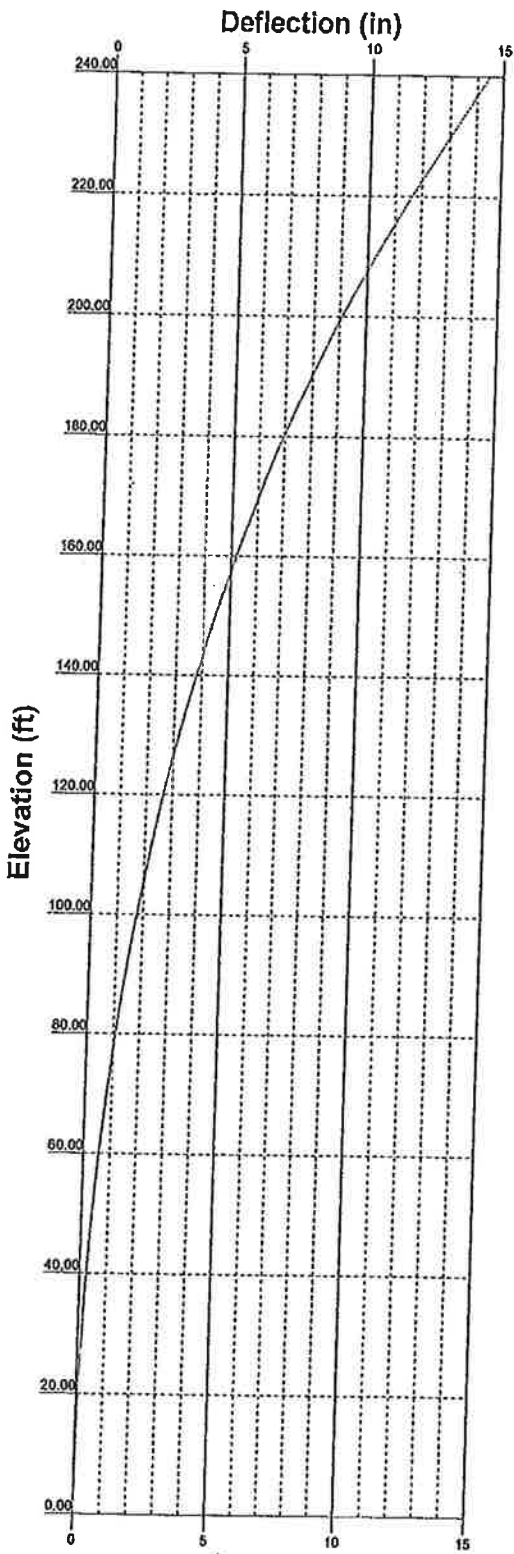
| | | | |
|---|-----------------------|----------------------------|---|
|  STRUCTURES Valmont Industries, Inc. - Specialty Structures Group | 1545 Pldco Dr. | | Job: 284859 |
| | Plymouth, IN | | Project: V-25 x 240' - Ashford, CT |
| | Phone: (574) 936-4221 | Drawn by: JAK | App'd: |
| | FAX: (574) 936-6458 | Code: TIAVEIA-222-F | Date: 03/30/15 |
| | | Path: | Scale: NTS |
| | | | Dwg No. E-2 |

TIA/EIA-222-F - 85 mph/74 mph 1.000 in Ice

Leg Capacity ——— Leg Compression (K)



| | | | | |
|---|--|------------------------------------|----------------|------------|
|  | | Job: 284859 | | |
| | | Project: V-26 x 240' - Ashford, CT | | |
| 1545 Pidco Dr. Plymouth, IN | | Client: Verizon Wireless | Drawn by: JAK | App'd: |
| Valmont Industries, Inc. - Specialty Structures Group | | Code: TIA/EIA-222-F | Date: 03/30/15 | Scale: NTS |
| Phone: (574) 936-4221 FAX: (574) 936-6458 | | Path: | Dwg No. E-3 | |



| | | | |
|---|---|------------|-------------|
|  | 1545 Pidco Dr. Plymouth, IN | | |
| | Valmont Industries, Inc. - Specialty Structures Group Phone: (574) 936-4221 FAX: (574) 936-6458 | | |
| Job: 284859 | Project: V-25 x 240' - Ashford, CT | | |
| Client: Verizon Wireless | Drawn by: JAK | App'd: | |
| Code: TIA/EIA-222-F | Date: 03/30/15 | Scale: NTS | |
| Path: | | | Dwg No. E-5 |

reeamline Distribution Chart

0' - 240'

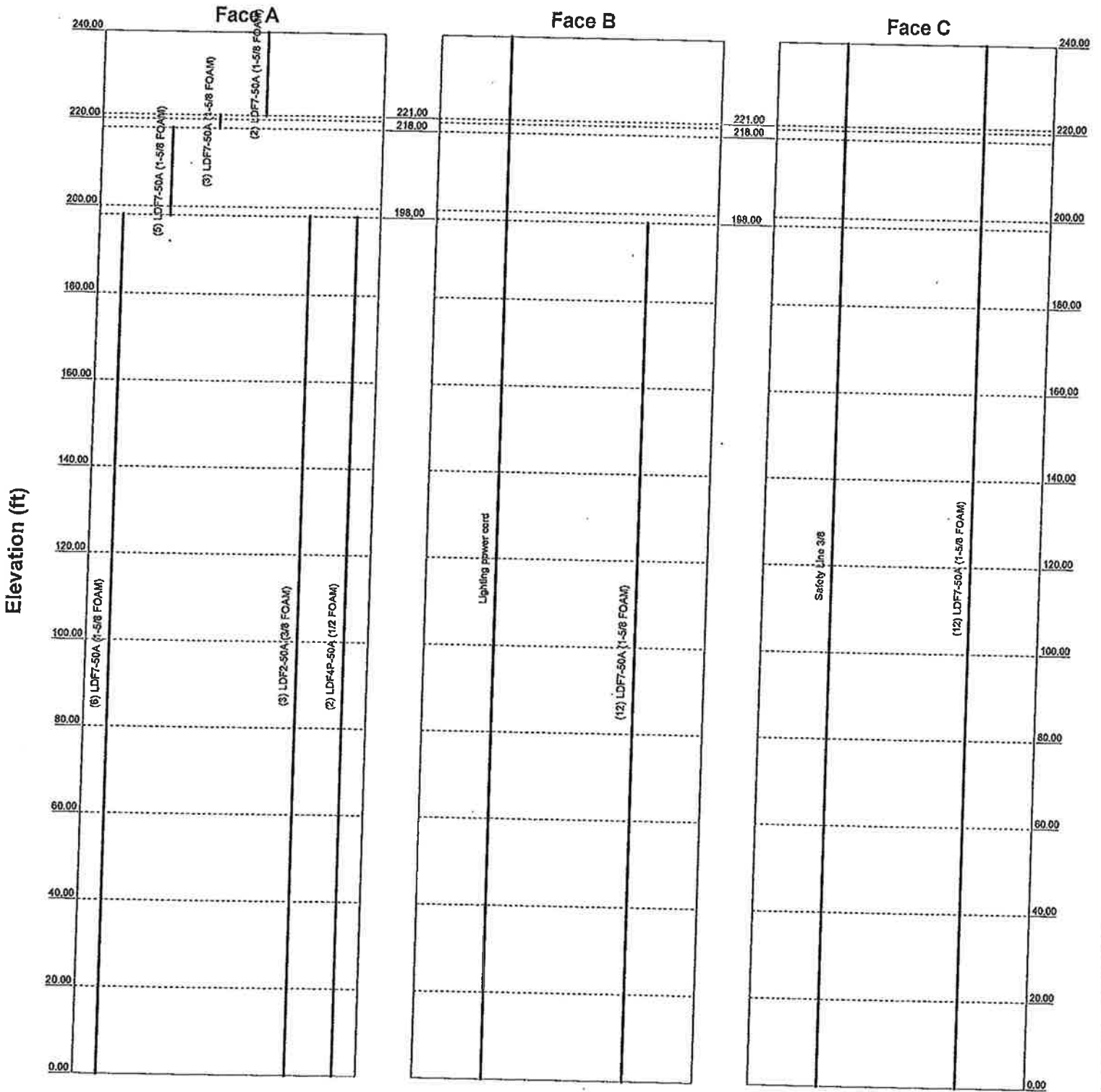
Round _____

Flat _____

App In Face _____

App Out Face _____

Truss Leg _____



| | | | |
|--|-----------------------|--------------------------------|--|
| valmont  | | 1545 Pidco Dr. Plymouth, IN | |
| STRUCTURES | | Phone: (574) 936-4221 | |
| Valmont Industries, Inc. - Specialty Structures Group | | FAX: (574) 936-6458 | |
| Job: 284859 | | | |
| Project: V-25 x 240' - Ashford, CT | | | |
| Client: Verizon Wireless | Drawn by: JAK | App'd: | |
| Code: TIA/EIA-222-F | Date: 03/30/15 | Scale: NTS | |
| Path: | | Dwg No. E-7 | |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 1518 Piko Dr. Plymouth, IN Phone: (317) 938-6221 FAX: (317) 938-6418 | Job | 284859 | Page | 5 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 1518 Piko Dr. Plymouth, IN Phone: (317) 938-6221 FAX: (317) 938-6418 | Job | 284859 | Page | 6 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |

| Tower Elevation # | Calc K Single Angle | Calc K Solid Round | K Factor | | | | | | Date | HORIZ. | Sec. HORIZ. | Tower Base |
|----------------------|------------------------------|-----------------------------|----------|---------------------|---------------------|----------------------|-----------|-------------|------|--------|----------------|---------------|
| | | | Legs | X Brace Diags | X Brace Diags | X Single Diags | X Date | X HORIZ. | | | | |
| T10 63.00-100.00 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | |
| T11 100.00-120.00 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | |
| T12 200.00-210.00 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | |

Tower Section Geometry (cont'd)

| Tower Elevation # | Trans-Leg Used As Leg Members | | | | Trans-Leg Used As Tower Members | | | |
|----------------------|-------------------------------|-------------------------|-------------------------|-------------------------|---------------------------------|-------------------------|-------------------------|-------------------------|
| | Leg Feeds | X Brace Diagonals | X Brace Diagonals | X Brace Diagonals | Leg Feeds | X Brace Diagonals | X Brace Diagonals | X Brace Diagonals |
| T1 150.00-180.00 | 1 | 0.5 | 0.7 | 1 | 1 | 0.5 | 0.7 | |
| T6 140.05-120.00 | 1 | 0.5 | 0.7 | 1 | 0.5 | 0.7 | | |
| T7 120.00-100.00 | 1 | 0.5 | 0.7 | 1 | 0.5 | 0.7 | | |
| T8 100.00-80.00 | 1 | 0.5 | 0.7 | 1 | 0.5 | 0.7 | | |
| T9 100.00-60.00 | 1 | 0.5 | 0.7 | 1 | 0.5 | 0.7 | | |
| T10 63.00-45.00 | 1 | 0.5 | 0.7 | 1 | 0.5 | 0.7 | | |
| T11 45.00-30.00 | 1 | 0.5 | 0.7 | 1 | 0.5 | 0.7 | | |
| T12 20.00-0.00 | 1 | 0.5 | 0.7 | 1 | 0.5 | 0.7 | | |

Tower Section Geometry (cont'd)

| Tower Elevation # | Leg | Diagonal | | Top Girt | | Bottom Girt | | Mid Girt | | Long Horizontal | | Short Horizontal | |
|----------------------|--------|-------------------------|--------|-------------------------|--------|-------------------------|--------|-------------------------|--------|-------------------------|--------|-------------------------|--------|
| | | Net Wt/Deflect in | U | Net Wt/Deflect in | U | Net Wt/Deflect in | U | Net Wt/Deflect in | U | Net Wt/Deflect in | U | Net Wt/Deflect in | U |
| T1 210.00-220.00 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 |
| T2 200.00-200.00 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 |
| T3 200.00-180.00 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 1518 Piko Dr. Plymouth, IN Phone: (317) 938-6221 FAX: (317) 938-6418 | Job | 284859 | Page | 7 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 1518 Piko Dr. Plymouth, IN Phone: (317) 938-6221 FAX: (317) 938-6418 | Job | 284859 | Page | 8 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |

Tower Section Geometry (cont'd)

| Tower Elevation # | Leg Connection Type | Leg | Diagonal | | Top Girt | | Bottom Girt | | Mid Girt | | Long Horizontal | | Short Horizontal | |
|----------------------|---------------------------|-------|----------------|-----|----------------|-----|----------------|-----|----------------|-----|-----------------|-----|------------------|-----|
| | | | Bot Size in | No. | Bot Size in | No. | Bot Size in | No. | Bot Size in | No. | Bot Size in | No. | Bot Size in | No. |
| T1 240.00-220.00 | Flange | A325N | 0.7500 | 1 | 0.7500 | 1 | 1.0000 | 0 | 1.0000 | 0 | 1.0000 | 0 | 1.0000 | 0 |
| T2 220.00-200.00 | Flange | A325N | 0.7500 | 1 | 0.7500 | 1 | 1.0000 | 0 | 1.0000 | 0 | 1.0000 | 0 | 1.0000 | 0 |
| T3 200.00-180.00 | Flange | A325N | 0.7500 | 1 | 0.7500 | 1 | 1.0000 | 0 | 1.0000 | 0 | 1.0000 | 0 | 1.0000 | 0 |

Feed Line/Linear Appurtenances - Entored As Round Or Flat

| Description | Face or Shield | Compensator Type | Flare Type | Total Number | Number Per Row | Clear Spacing | Width or Formosa | Weight |
|---------------------|----------------------|---------------------|---------------|-----------------|-------------------|------------------|------------------------|--------|
| 3-Cell Line Mt | Yes | Ar (CDA) | 240.00-0.00 | 1 | 1 | 0.7500 | 0.2500 | 0.15 |
| LD7F-55A (1-5) FOAM | Yes | Ar (CDA) | 240.00-0.00 | 12 | 12 | 1.9000 | 1.9000 | 0.11 |
| LD7F-55A (1-5) FOAM | Yes | Ar (CDA) | 198.00-0.00 | 12 | 12 | 1.9000 | 1.9000 | 0.12 |
| LD7F-55A (1-5) FOAM | Yes | Ar (CDA) | 210.00-198.00 | 3 | 3 | 1.9000 | 1.9000 | 0.12 |
| LD7F-55A (1-5) FOAM | Yes | Ar (CDA) | 221.00-210.00 | 3 | 3 | 1.9000 | 1.9000 | 0.11 |
| LD7F-55A (1-5) FOAM | Yes | Ar (CDA) | 240.00-228.00 | 2 | 2 | 1.9000 | 1.9000 | 0.12 |
| LD7F-55A (12) FOAM | Yes | Ar (CDA) | 198.00-0.00 | 3 | 3 | 0.4000 | 0.4000 | 0.11 |
| LD7F-55A (12) FOAM | Yes | Ar (CDA) | 198.00-0.00 | 2 | 2 | 0.5000 | 0.5000 | 0.15 |

Feed Line/Linear Appurtenances Section Areas

| Tower Section | Tower Elevation # | Face or Leg | As | | C/A In Face | | C/A Out Face | | Weight |
|---------------|-------------------|-------------|--------|-------|-------------|-------|--------------|------|--------|
| | | | As | As | As | As | As | As | |
| T1 | 240.00-220.00 | A | 6.513 | 0.000 | 0.000 | 0.000 | 0.000 | 0.21 | |
| | | B | 0.000 | 0.000 | 1.740 | 0.000 | 0.000 | 0.20 | |
| | | C | 39.800 | 0.000 | 0.000 | 0.000 | 0.000 | 0.20 | |
| T2 | 220.00-200.00 | A | 19.810 | 0.000 | 0.000 | 0.000 | 0.000 | 0.11 | |
| | | B | 0.000 | 0.000 | 1.740 | 0.000 | 0.000 | 0.20 | |
| | | C | 39.800 | 0.000 | 0.000 | 0.000 | 0.000 | 0.20 | |

Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower Section | Tower Elevation # | Face or Leg | As | | C/A In Face | | C/A Out Face | | Weight |
|---------------|-------------------|-------------|-------|--------|-------------|-------|--------------|------|--------|
| | | | As | As | As | As | As | As | |
| T1 | 240.00-220.00 | A | 1.000 | 6.633 | 6.950 | 0.000 | 0.000 | 0.21 | |
| | | B | 0.000 | 0.000 | 2.740 | 0.000 | 0.000 | 0.21 | |
| | | C | 6.633 | 72.600 | 4.750 | 0.000 | 0.000 | 0.53 | |
| T2 | 220.00-200.00 | A | 1.000 | 6.633 | 20.000 | 0.000 | 0.000 | 0.21 | |
| | | B | 0.000 | 0.000 | 2.740 | 0.000 | 0.000 | 0.21 | |
| | | C | 6.633 | 72.600 | 4.750 | 0.000 | 0.000 | 0.53 | |

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Job: 284859
Project: V-25 x 240' - Ashford, CT
Client: Verizon Wireless

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| Tower Section | Tower Elevation | Face or Leg | Use Thickness | A _p | A _s | C ₁ A ₁ In Foot | C ₁ A ₂ Out Foot | Weight |
|---------------|-----------------|-------------|---------------|----------------|----------------|---------------------------------------|--|--------|
| T6 | 140.00-150.00 | A | 1.000 | 15.013 | 11.613 | 0.000 | 0.000 | 0.85 |
| | | B | 1.000 | 6.433 | 72.600 | 5.740 | 0.000 | 1.40 |
| | | C | 1.000 | 6.433 | 72.600 | 4.750 | 0.000 | 1.39 |
| T7 | 170.00-190.00 | A | 1.000 | 13.613 | 18.613 | 0.000 | 0.000 | 0.85 |
| | | B | 1.000 | 6.433 | 72.600 | 5.740 | 0.000 | 1.40 |
| | | C | 1.000 | 6.433 | 72.600 | 4.750 | 0.000 | 1.39 |
| T8 | 100.00-80.00 | A | 1.000 | 13.613 | 18.613 | 0.000 | 0.000 | 0.85 |
| | | B | 1.000 | 6.433 | 72.600 | 5.740 | 0.000 | 1.40 |
| | | C | 1.000 | 6.433 | 72.600 | 4.750 | 0.000 | 1.39 |
| T9 | 90.00-60.00 | A | 1.000 | 15.013 | 11.613 | 0.000 | 0.000 | 0.85 |
| | | B | 1.000 | 6.433 | 72.600 | 5.740 | 0.000 | 1.40 |
| | | C | 1.000 | 6.433 | 72.600 | 4.750 | 0.000 | 1.39 |
| T10 | 60.00-40.00 | A | 1.000 | 15.013 | 11.613 | 0.000 | 0.000 | 0.85 |
| | | B | 1.000 | 6.433 | 72.600 | 5.740 | 0.000 | 1.40 |
| | | C | 1.000 | 6.433 | 72.600 | 4.750 | 0.000 | 1.39 |
| T11 | 60.00-20.00 | A | 1.000 | 15.013 | 11.613 | 0.000 | 0.000 | 0.85 |
| | | B | 1.000 | 6.433 | 72.600 | 5.740 | 0.000 | 1.40 |
| | | C | 1.000 | 6.433 | 72.600 | 4.750 | 0.000 | 1.39 |
| T12 | 20.00-0.00 | A | 1.000 | 15.013 | 11.613 | 0.000 | 0.000 | 0.85 |
| | | B | 1.000 | 6.433 | 72.600 | 5.740 | 0.000 | 1.40 |
| | | C | 1.000 | 6.433 | 72.600 | 4.750 | 0.000 | 1.39 |

| Section | Elevation | Face | A _p | A _s | A _t | A _r | Weight |
|---------|-------------|------|----------------|----------------|----------------|----------------|--------|
| T11 | 40.00-20.00 | A | 0.000 | 1.196 | 0.950 | 2.093 | 0.00 |
| | | B | 0.000 | 1.092 | 1.618 | 1.311 | 0.00 |
| | | C | 0.000 | 1.374 | 1.313 | 1.279 | 0.00 |
| T12 | 20.00-0.00 | A | 0.000 | 1.192 | 0.950 | 2.093 | 0.00 |
| | | B | 0.000 | 1.092 | 1.618 | 1.311 | 0.00 |
| | | C | 0.000 | 1.374 | 1.313 | 1.279 | 0.00 |

Feed Line Shielding

| Section | Elevation | Face | A _p | A _s | A _t | A _r | Weight |
|---------|---------------|------|----------------|----------------|----------------|----------------|--------|
| T1 | 140.00-220.00 | A | 0.000 | 1.379 | 0.418 | 1.379 | 0.00 |
| | | B | 0.000 | 0.418 | 0.147 | 0.418 | 0.00 |
| | | C | 0.000 | 1.841 | 4.411 | 1.841 | 0.00 |
| T2 | 220.00-200.00 | A | 0.000 | 2.643 | 1.619 | 2.643 | 0.00 |
| | | B | 0.000 | 0.939 | 0.131 | 0.939 | 0.00 |
| | | C | 0.000 | 6.933 | 4.190 | 6.933 | 0.00 |
| T3 | 200.00-190.00 | A | 0.000 | 1.840 | 1.374 | 1.840 | 0.00 |
| | | B | 0.000 | 2.717 | 2.717 | 2.717 | 0.00 |
| | | C | 0.000 | 0.231 | 3.623 | 0.231 | 0.00 |
| T4 | 183.00-193.00 | A | 0.000 | 3.613 | 1.945 | 3.613 | 0.00 |
| | | B | 0.000 | 1.411 | 3.241 | 1.411 | 0.00 |
| | | C | 0.000 | 5.427 | 3.285 | 5.427 | 0.00 |
| T5 | 180.00-143.00 | A | 0.000 | 2.937 | 1.796 | 2.937 | 0.00 |
| | | B | 0.000 | 1.964 | 2.937 | 1.964 | 0.00 |
| | | C | 0.000 | 3.927 | 3.414 | 3.927 | 0.00 |
| T6 | 140.00-130.00 | A | 0.000 | 2.307 | 1.370 | 2.307 | 0.00 |
| | | B | 0.000 | 3.648 | 2.874 | 3.648 | 0.00 |
| | | C | 0.000 | 3.413 | 2.678 | 3.413 | 0.00 |
| T7 | 120.00-109.00 | A | 0.000 | 2.177 | 1.112 | 2.177 | 0.00 |
| | | B | 0.000 | 3.640 | 2.324 | 3.640 | 0.00 |
| | | C | 0.000 | 2.319 | 2.894 | 2.319 | 0.00 |
| T8 | 100.00-93.00 | A | 0.000 | 2.317 | 0.954 | 2.317 | 0.00 |
| | | B | 0.000 | 2.241 | 1.642 | 2.241 | 0.00 |
| | | C | 0.000 | 2.319 | 1.650 | 2.319 | 0.00 |
| T9 | 80.00-69.00 | A | 0.000 | 1.323 | 1.323 | 1.323 | 0.00 |
| | | B | 0.000 | 2.699 | 1.374 | 2.699 | 0.00 |
| | | C | 0.000 | 2.029 | 1.203 | 2.029 | 0.00 |
| T10 | 60.00-40.00 | A | 0.000 | 1.282 | 0.994 | 1.282 | 0.00 |
| | | B | 0.000 | 1.510 | 1.631 | 1.510 | 0.00 |
| | | C | 0.000 | 1.560 | 1.631 | 1.560 | 0.00 |

Discrete Tower Loads

| Description | Face or Leg | Offset Type | Offset Horiz Dist | Offset Vertical Dist | Assumed Adjustment | Elevation | C ₁ A ₁ Foot | C ₁ A ₂ Side | Height |
|---------------------------|-------------|-------------|-------------------|----------------------|--------------------|-----------|------------------------------------|------------------------------------|--------|
| Basem | A | From Leg | 0.00 | 0.000 | 240.00 | No Ice | 3.40 | 3.40 | 0.07 |
| | | | 0.00 | 0.000 | 240.00 | 1/2" Ice | 2.47 | 2.47 | 0.19 |
| | | | 0.00 | 0.000 | 240.00 | 1" Ice | 2.56 | 2.56 | 0.12 |
| | | | 0.00 | 0.000 | 240.00 | No Ice | 1.11 | 1.11 | 0.03 |
| Basem Extension (4) 89562 | A | From Leg | 0.00 | 0.000 | 240.00 | No Ice | 1.33 | 1.33 | 0.04 |
| | | | 0.00 | 0.000 | 240.00 | 1/2" Ice | 1.34 | 1.34 | 0.01 |
| | | | 0.00 | 0.000 | 240.00 | 1" Ice | 0.20 | 0.20 | 0.01 |
| | | | 0.00 | 0.000 | 240.00 | No Ice | 0.60 | 0.60 | 0.02 |
| (1) HANN-5117DS-VTM | C | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 0.89 | 0.89 | 0.02 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 0.92 | 0.92 | 0.02 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 1.11 | 1.11 | 0.09 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 2.41 | 2.41 | 0.35 |
| (2) HANN-5117DS-VTM | B | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 4.32 | 4.32 | 0.04 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 7.11 | 7.11 | 0.47 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 7.41 | 7.41 | 0.35 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 4.32 | 4.32 | 0.04 |
| (3) HANN-5117DS-VTM | A | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 4.32 | 4.32 | 0.04 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 7.11 | 7.11 | 0.47 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 7.41 | 7.41 | 0.35 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 4.32 | 4.32 | 0.04 |
| (7) 2' x 8" Sch. 40 | C | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 0.18 | 0.18 | 0.03 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 0.28 | 0.28 | 0.04 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 0.32 | 0.32 | 0.05 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 0.11 | 0.11 | 0.02 |
| (7) 2' x 8" Sch. 40 | B | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 0.11 | 0.11 | 0.02 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 0.28 | 0.28 | 0.04 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 0.32 | 0.32 | 0.05 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 0.11 | 0.11 | 0.02 |
| (7) 2' x 8" Sch. 40 | A | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 0.11 | 0.11 | 0.02 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 0.28 | 0.28 | 0.04 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 0.32 | 0.32 | 0.05 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 0.11 | 0.11 | 0.02 |
| (7) 2" x 4" Sch. 40 | C | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 0.32 | 0.32 | 0.04 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 0.42 | 0.42 | 0.06 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 0.54 | 0.54 | 0.09 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 0.32 | 0.32 | 0.04 |
| (7) 2" x 4" Sch. 40 | B | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 0.32 | 0.32 | 0.04 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 0.42 | 0.42 | 0.06 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 0.54 | 0.54 | 0.09 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 0.32 | 0.32 | 0.04 |
| (7) 2" x 4" Sch. 40 | A | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 0.32 | 0.32 | 0.04 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 0.42 | 0.42 | 0.06 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 0.54 | 0.54 | 0.09 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 0.32 | 0.32 | 0.04 |

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Date: 15:16:37 03/30/15
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| Description | Face or Leg | Offset Type | Offset Horiz Dist | Offset Vertical Dist | Assumed Adjustment | Elevation | C ₁ A ₁ Foot | C ₁ A ₂ Side | Height |
|----------------------------|-------------|-------------|-------------------|----------------------|--------------------|-----------|------------------------------------|------------------------------------|--------|
| (7) 2' x 4" Sch. 40 | A | From Leg | -1.25 | 0.000 | 240.00 | 1" Ice | 6.43 | 2.19 | 6.66 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 0.22 | 1.33 | 0.03 |
| | | | 0.00 | 0.000 | 240.00 | 1/2" Ice | 0.32 | 1.19 | 0.04 |
| | | | 0.00 | 0.000 | 240.00 | 1" Ice | 0.42 | 2.19 | 0.06 |
| Alcatel-Lucent RRUHS50-AWS | C | From Leg | 0.00 | 0.000 | 240.00 | No Ice | 2.48 | 3.60 | 0.06 |
| | | | 0.00 | 0.000 | 240.00 | 1/2" Ice | 2.16 | 2.71 | 0.01 |
| | | | 0.00 | 0.000 | 240.00 | 1" Ice | 3.04 | 1.90 | 0.10 |
| | | | 0.00 | 0.000 | 240.00 | No Ice | 2.48 | 1.60 | 0.06 |
| Alcatel-Lucent RRUHS50-AWS | A | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 2.16 | 1.75 | 0.01 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 2.48 | 1.60 | 0.06 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 3.04 | 1.90 | 0.10 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 2.48 | 1.60 | 0.06 |
| Alcatel-Lucent RRUHS50-PCS | C | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 2.48 | 1.60 | 0.06 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 2.16 | 1.75 | 0.01 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 3.04 | 1.90 | 0.10 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 2.48 | 1.60 | 0.06 |
| Alcatel-Lucent RRUHS50-PCS | B | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 2.48 | 1.60 | 0.06 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 2.16 | 1.75 | 0.01 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 3.04 | 1.90 | 0.10 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 2.48 | 1.60 | 0.06 |
| Alcatel-Lucent RRUHS50-PCS | A | From Leg | 3.00 | 0.000 | 240.00 | No Ice | 2.48 | 1.60 | 0.06 |
| | | | 3.00 | 0.000 | 240.00 | 1/2" Ice | 2.16 | 1.75 | 0.01 |
| | | | 3.00 | 0.000 | 240.00 | 1" Ice | 3.04 | 1.90 | 0.10 |
| | | | 3.00 | 0.000 | 240.00 | No Ice | 2.48 | 1.60 | 0.06 |
| DB-T1-62-4AB-02 | C | From Leg | -1 | | | | | | |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| luxTower 1343 Piko Dr. Plymouth, NY Phone: (716) 936-6337 FAX: (716) 936-6418 | Job | 284859 | Page | 13 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| luxTower 1343 Piko Dr. Plymouth, NY Phone: (716) 936-6337 FAX: (716) 936-6418 | Job | 284859 | Page | 14 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Description | Face of Leg | Offset Type | Offset from Lateral | Actual Adjustment | Flange | C/W | C/W | Height |
|------------------------------|-------------|-------------|---------------------|-------------------|--------|--------|------|--------|
| | | | P | P | P | P | K | |
| (D) Tower Section 200.00 | A | From Leg | 0.00 | 0.0000 | 198.00 | 1" Ice | 0.39 | 0.19 |
| Dashed H&T | | | 0.00 | | 198.00 | No Ice | 0.38 | 0.28 |
| (D) R&US 11 (20' X 12' X 7') | C | From Leg | 3.00 | 0.0000 | 198.00 | 1" Ice | 0.39 | 0.15 |
| | | | 0.00 | | 198.00 | No Ice | 0.37 | 0.25 |
| (D) R&US 11 (20' X 12' X 7') | B | From Leg | 3.00 | 0.0000 | 198.00 | 1" Ice | 0.39 | 0.15 |
| | | | 0.00 | | 198.00 | No Ice | 0.37 | 0.25 |
| (D) R&US 11 (20' X 12' X 7') | A | From Leg | 3.00 | 0.0000 | 198.00 | 1" Ice | 0.39 | 0.15 |
| | | | 0.00 | | 198.00 | No Ice | 0.37 | 0.25 |
| Polystyrene (12%) [F&T] | C | From Leg | 3.00 | 0.0000 | 198.00 | 1" Ice | 0.39 | 0.15 |
| | | | 0.00 | | 198.00 | No Ice | 0.37 | 0.25 |
| 12' V Frame | C | From Leg | 0.00 | 0.0000 | 198.00 | 1" Ice | 1.45 | 1.01 |
| | | | 0.00 | | 198.00 | No Ice | 0.91 | 0.31 |
| 12' V Frame | B | From Leg | 0.00 | 0.0000 | 198.00 | 1" Ice | 1.45 | 1.01 |
| | | | 0.00 | | 198.00 | No Ice | 0.91 | 0.31 |
| 12' V Frame | A | From Leg | 0.00 | 0.0000 | 198.00 | 1" Ice | 1.45 | 1.01 |
| | | | 0.00 | | 198.00 | No Ice | 0.91 | 0.31 |

Truss-Leg Properties

| Section Designation | Area | Arm | Self Weight | Ice Weight | Equiv. Diameter | Equiv. Diameter | Leg Area |
|--|-----------------|-----------|-------------|------------|-----------------|-----------------|-----------------|
| | in ² | ft | lb/ft | lb | in | ft | in ² |
| *1220-11-1.50'-1.00' ecca (Frod 191651) | 2019.3166 | 5328.6451 | 0.82 | 1.37 | 6.5953 | 18.1118 | 5.5314 |
| *1220-11-1.75'-1.00' ecca (Frod 191651) | 2035.9952 | 5328.6451 | 0.79 | 1.43 | 7.0693 | 18.5357 | 7.2118 |
| *1220-11-1.75'-1.00' ecca (Frod 191651) | 2035.9652 | 5328.6451 | 0.79 | 1.43 | 7.0693 | 18.5357 | 7.2118 |
| *1220-11-2.00'-0.812' ecca (Frod 191651) | 2339.7677 | 5449.2451 | 1.00 | 1.44 | 8.1242 | 18.9210 | 8.4248 |
| *1220-11-2.00'-0.812' ecca (Frod 191651) | 2339.7677 | 5449.2451 | 1.00 | 1.44 | 8.1242 | 18.9210 | 8.4248 |
| *1220-11-2.25'-0.812' ecca (Frod 191651) | 2491.7141 | 5521.2451 | 1.17 | 1.47 | 8.5962 | 19.3110 | 11.9282 |

| Section Designation | Area | Arm | Self Weight | Ice Weight | Equiv. Diameter | Equiv. Diameter | Leg Area |
|---------------------|-----------------|-----------|-------------|------------|-----------------|-----------------|-----------------|
| | in ² | ft | lb/ft | lb | in | ft | in ² |
| 199990 | 2491.7141 | 5521.2451 | 1.17 | 1.47 | 8.5962 | 19.3110 | 11.9282 |
| 199991 | 2491.7141 | 5521.2451 | 1.17 | 1.47 | 8.5962 | 19.3110 | 11.9282 |

Tower Pressures - No Ice

$G_w = 1.07$

| Section Elevation | z | K _t | z | K _d | F | F | F | F | Log | C _{sa} | C _{st} |
|-------------------|--------|----------------|----|----------------|---|--------|--------|--------|-------|-----------------|-----------------|
| | ft | | ft | | # | # | # | # | N | In | Out |
| 240.00-320.00 | 280.00 | 1.741 | 33 | 104.792 | A | 2.855 | 16.376 | 9.383 | 35.58 | 0.000 | 0.000 |
| | | | | | B | 4.455 | 9.993 | 31.27 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 4.654 | 49.183 | 12.85 | 0.750 | 0.000 | 0.000 |
| 220.00-240.00 | 230.00 | 1.697 | 31 | 107.500 | A | 2.311 | 30.840 | 15.000 | 10.82 | 0.000 | 0.000 |
| | | | | | B | 3.810 | 18.000 | 35.07 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 4.773 | 14.600 | 25.37 | 0.750 | 0.000 | 0.000 |
| 200.00-180.00 | 190.00 | 1.649 | 30 | 129.283 | A | 3.595 | 41.514 | 18.574 | 18.13 | 0.000 | 0.000 |
| | | | | | B | 4.812 | 34.214 | 21.45 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 4.677 | 58.174 | 28.37 | 0.750 | 0.000 | 0.000 |
| 180.00-160.00 | 170.00 | 1.597 | 30 | 171.653 | A | 9.399 | 65.206 | 22.100 | 30.77 | 0.000 | 0.000 |
| | | | | | B | 8.813 | 41.730 | 32.89 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 10.620 | 41.720 | 39.37 | 0.750 | 0.000 | 0.000 |
| 160.00-140.00 | 150.00 | 1.541 | 29 | 222.528 | A | 16.607 | 45.406 | 23.206 | 40.17 | 0.000 | 0.000 |
| | | | | | B | 9.409 | 63.906 | 32.23 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 9.455 | 63.906 | 32.20 | 0.750 | 0.000 | 0.000 |
| 140.00-120.00 | 130.00 | 1.48 | 27 | 282.943 | A | 12.137 | 47.704 | 22.604 | 38.40 | 0.000 | 0.000 |
| | | | | | B | 11.633 | 63.204 | 31.29 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 11.100 | 63.204 | 31.76 | 0.750 | 0.000 | 0.000 |
| 120.00-100.00 | 110.00 | 1.411 | 25 | 352.919 | A | 13.791 | 47.704 | 22.604 | 38.31 | 0.000 | 0.000 |
| | | | | | B | 12.749 | 63.204 | 31.69 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 12.799 | 63.204 | 31.66 | 0.750 | 0.000 | 0.000 |
| 100.00-80.00 | 90.00 | 1.332 | 23 | 443.352 | A | 10.922 | 51.282 | 21.126 | 43.64 | 0.000 | 0.000 |
| | | | | | B | 10.423 | 64.786 | 32.14 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 10.366 | 64.786 | 32.22 | 0.750 | 0.000 | 0.000 |
| 80.00-60.00 | 70.00 | 1.24 | 21 | 581.362 | A | 11.613 | 51.282 | 21.126 | 43.64 | 0.000 | 0.000 |
| | | | | | B | 10.890 | 66.726 | 34.91 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 11.011 | 66.726 | 34.89 | 0.750 | 0.000 | 0.000 |
| 60.00-40.00 | 50.00 | 1.126 | 21 | 823.783 | A | 14.811 | 51.282 | 21.702 | 47.72 | 0.000 | 0.000 |
| | | | | | B | 13.643 | 68.302 | 35.01 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 13.716 | 68.302 | 34.99 | 0.750 | 0.000 | 0.000 |
| 40.00-20.00 | 30.00 | 1 | 18 | 1113.780 | A | 18.010 | 48.302 | 20.702 | 42.18 | 0.000 | 0.000 |
| | | | | | B | 14.430 | 64.302 | 34.45 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 14.430 | 64.302 | 34.45 | 0.750 | 0.000 | 0.000 |
| 20.00-0.00 | 10.00 | 1 | 18 | 304.197 | A | 18.146 | 34.403 | 35.333 | 42.98 | 0.000 | 0.000 |
| | | | | | B | 13.862 | 49.933 | 31.49 | 1.740 | 0.000 | 0.000 |
| | | | | | C | 13.862 | 49.933 | 31.49 | 0.750 | 0.000 | 0.000 |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| luxTower 1343 Piko Dr. Plymouth, NY Phone: (716) 936-6337 FAX: (716) 936-6418 | Job | 284859 | Page | 15 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| luxTower 1343 Piko Dr. Plymouth, NY Phone: (716) 936-6337 FAX: (716) 936-6418 | Job | 284859 | Page | 16 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

Tower Pressure - With Ice

$G_w = 2.03$

| Section Elevation | z | K _t | z | K _d | F | F | F | F | Log | C _{sa} | C _{st} |
|-------------------|--------|----------------|----|----------------|---|--------|--------|--------|-------|-----------------|-----------------|
| | ft | | ft | | # | # | # | # | N | In | Out |
| 240.00-320.00 | 280.00 | 1.741 | 33 | 104.792 | A | 14.130 | 31.619 | 18.350 | 36.10 | 0.000 | 0.000 |
| | | | | | B | 16.666 | 24.316 | 50.18 | 5.740 | 0.000 | 0.000 |
| | | | | | C | 24.697 | 32.811 | 16.81 | 4.750 | 0.000 | 0.000 |
| 220.00-240.00 | 230.00 | 1.697 | 31 | 110.473 | A | 30.757 | 32.819 | 21.617 | 34.99 | 0.000 | 0.000 |
| | | | | | B | 4.457 | 78.437 | 16.72 | 4.750 | 0.000 | 0.000 |
| | | | | | C | 24.699 | 24.316 | 21.30 | 3.740 | 0.000 | 0.000 |
| 200.00-180.00 | 190.00 | 1.649 | 30 | 138.711 | A | 48.699 | 43.319 | 25.257 | 30.06 | 0.000 | 0.000 |
| | | | | | B | 41.892 | 33.313 | 25.14 | 5.740 | 0.000 | 0.000 |
| | | | | | C | 31.611 | 31.303 | 22.33 | 4.750 | 0.000 | 0.000 |
| 180.00-160.00 | 170.00 | 1.597 | 30 | 171.653 | A | 45.662 | 49.304 | 28.701 | 45.00 | 0.000 | 0.000 |
| | | | | | B | 71.109 | 39.319 | 24.29 | 5.740 | 0.000 | 0.000 |
| | | | | | C | 59.977 | 39.303 | 24.70 | 4.750 | 0.000 | 0.000 |
| 160.00-140.00 | 150.00 | 1.541 | 29 | 222.528 | A | 46.156 | 41.291 | 30.315 | 45.00 | 0.000 | 0.000 |
| | | | | | B | 78.954 | 31.317 | 49.31 | 5.740 | 0.000 | 0.000 |
| | | | | | C | 66.200 | 32.316 | 46.80 | 4.750 | 0.000 | 0.000 |
| 140.00-120.00 | 130.00 | 1.48 | 27 | 282.943 | A | 79.032 | 21.626 | 49.326 | 47.50 | 0.000 | 0.000 |
| | | | | | B | 43.200 | 33.316 | 46.80 | 0.000 | 0.000 | 0.000 |
| | | | | | C | 83.844 | 21.626 | 39.02 | 3.740 | 0.000 | 0.000 |
| 120.00-100.00 | 110.00 | 1.411 | 25 | 352.919 | A | 39.908 | 39.660 | 39.909 | 43.53 | 0.000 | 0.000 |
| | | | | | B | 59.046 | 44.975 | 41.716 | 43.85 | 0.000 | 0.000 |
| | | | | | C | 82.771 | 39.114 | 39.12 | 4.750 | 0.000 | 0.000 |
| 100.00-80.00 | 90.00 | 1.332 | 23 | 443.352 | A | 32.733 | 25.124 | 38.178 | 42.00 | 0.000 | 0.000 |
| | | | | | B | 47.824 | 14.722 | 47.825 | 0.000 | 0.000 | 0.000 |
| | | | | | C | 41.133 | 24.689 | 40.33 | 3.740 | 0.000 | 0.000 |
| 80.00-60.00 | 70.00 | 1.24 | 21 | 581.362 | A | 51.161 | 25.120 | 43.152 | 47.50 | 0.000 | 0.000 |
| | | | | | B | 48.562 | 85.278 | 63.176 | 42.00 | 0.000 | 0.000 |
| | | | | | C | 81.977 | 26.511 | 39.98 | 3.740 | 0.000 | 0.000 |
| 60.00-40.00 | 50.00 | 1.126 | | | | | | | | | |

| | | |
|---|------------------------------------|-------------------------|
| inxTower | Job: 284859 | Page: 17 of 107 |
| 1345 Piko Dr. Plymouth, IN Phone: (117) 936-6231 FAX: (117) 936-6438 | Project: V-25 x 240' - Ashford, CT | Date: 16:15:37 03/30/16 |
| | Client: Verizon Wireless | Designed by: JAK |

| | | |
|---|------------------------------------|-------------------------|
| inxTower | Job: 284859 | Page: 18 of 107 |
| 1345 Piko Dr. Plymouth, IN Phone: (117) 936-6231 FAX: (117) 936-6438 | Project: V-25 x 240' - Ashford, CT | Date: 16:15:37 03/30/16 |
| | Client: Verizon Wireless | Designed by: JAK |

| Section Elevation | Add Weight | Self Weight | F | a | Cy | Ra | Dy | Dz | A | F | v | Cat. Face |
|-------------------|------------|-------------|---|-------|-------|-------|----|----|--------|---------|--------|-----------|
| # | K | K | f | e | | | | | # | K | # | |
| 121.00-109.00 | | | B | 0.231 | 2.435 | 0.602 | 1 | 1 | 50.501 | | | |
| | | | A | 0.231 | 2.435 | 0.602 | 1 | 1 | 50.501 | | | |
| 100.00-82.00 | 0.51 | 4.10 | B | 0.181 | 2.661 | 0.519 | 1 | 1 | 43.885 | 3.00 | 174.30 | |
| | | | A | 0.224 | 2.517 | 0.296 | 1 | 1 | 45.991 | | | |
| | | | C | 0.221 | 2.517 | 0.295 | 1 | 1 | 50.912 | | | |
| T9 | 0.51 | 4.16 | A | 0.161 | 2.771 | 0.514 | 1 | 1 | 41.514 | 1.36 | 187.99 | C |
| 81.00-63.00 | | | B | 0.209 | 2.197 | 0.591 | 1 | 1 | 36.412 | | | |
| | | | C | 0.203 | 2.387 | 0.591 | 1 | 1 | 54.444 | | | |
| T10 | 0.51 | 3.43 | A | 0.159 | 2.74 | 0.515 | 1 | 1 | 41.155 | 3.50 | 161.92 | C |
| 63.00-49.00 | | | B | 0.193 | 2.418 | 0.519 | 1 | 1 | 39.511 | | | |
| | | | C | 0.194 | 2.418 | 0.519 | 1 | 1 | 51.925 | | | |
| T11 | 0.51 | 3.53 | A | 0.147 | 2.781 | 0.521 | 1 | 1 | 34.993 | 3.82 | 111.16 | C |
| 49.00-20.00 | | | B | 0.179 | 2.669 | 0.515 | 1 | 1 | 34.618 | | | |
| | | | C | 0.179 | 2.669 | 0.515 | 1 | 1 | 47.716 | | | |
| T12 | 0.51 | 4.24 | A | 0.169 | 2.701 | 0.515 | 1 | 1 | 41.341 | 3.16 | 157.83 | C |
| 20.00-0.00 | | | B | 0.17 | 2.701 | 0.515 | 1 | 1 | 54.420 | | | |
| | | | C | 0.17 | 2.701 | 0.515 | 1 | 1 | 41.737 | | | |
| Sum Weight | 5.00 | 39.18 | | | | | | | OTH | 4187.57 | 36.94 | |

| Section Elevation | Add Weight | Self Weight | F | a | Cy | Ra | Dy | Dz | A | F | v | Cat. Face |
|-------------------|------------|-------------|---|-------|-------|-------|-----|----|--------|------|--------|-----------|
| # | K | K | f | e | | | | | # | K | # | |
| 100.00-22.00 | 0.51 | 3.33 | A | 0.147 | 2.784 | 0.511 | 0.8 | 1 | 42.935 | 2.50 | 143.22 | C |
| | | | B | 0.179 | 2.669 | 0.516 | 0.8 | 1 | 51.793 | | | |
| | | | C | 0.179 | 2.669 | 0.516 | 0.8 | 1 | 51.793 | | | |
| T12 | 0.51 | 6.24 | A | 0.11 | 2.809 | 0.51 | 0.8 | 1 | 44.411 | 2.59 | 149.28 | C |
| 20.00-0.00 | | | B | 0.169 | 2.701 | 0.515 | 0.8 | 1 | 53.287 | | | |
| | | | C | 0.17 | 2.701 | 0.515 | 0.8 | 1 | 40.359 | | | |
| Sum Weight | 5.00 | 39.14 | | | | | | | OTH | | 37.40 | |

Tower Forces - No Ice - Wind 90 To Face

Tower Forces - No Ice - Wind 60 To Face

| Section Elevation | Add Weight | Self Weight | F | a | Cy | Ra | Dy | Dz | A | F | v | Cat. Face |
|-------------------|------------|-------------|---|-------|-------|-------|------|----|--------|---------|--------|-----------|
| # | K | K | f | e | | | | | # | K | # | |
| 210.00-220.00 | 0.21 | 0.65 | A | 0.311 | 2.496 | 0.597 | 0.8 | 1 | 16.479 | 3.66 | 172.18 | C |
| | | | B | 0.172 | 2.693 | 0.515 | 0.8 | 1 | 12.331 | | | |
| | | | C | 0.212 | 1.883 | 0.204 | 0.8 | 1 | 34.189 | | | |
| T2 | 0.28 | 1.10 | A | 0.315 | 2.16 | 0.634 | 0.85 | 1 | 21.874 | 2.87 | 143.35 | C |
| 220.00-200.00 | | | B | 0.221 | 2.526 | 0.555 | 0.8 | 1 | 15.970 | | | |
| | | | C | 0.512 | 1.841 | 0.276 | 0.8 | 1 | 43.422 | | | |
| T3 | 0.49 | 1.21 | A | 0.27 | 1.927 | 0.64 | 0.8 | 1 | 31.529 | 2.91 | 148.69 | C |
| 200.00-180.00 | | | B | 0.457 | 1.962 | 0.477 | 0.8 | 1 | 40.519 | | | |
| | | | C | 0.465 | 1.919 | 0.479 | 0.8 | 1 | 43.882 | | | |
| T4 | 0.51 | 1.70 | A | 0.325 | 2.231 | 0.624 | 0.8 | 1 | 35.534 | 3.21 | 160.38 | C |
| 180.00-160.00 | | | B | 0.400 | 2.049 | 0.615 | 0.8 | 1 | 45.722 | | | |
| | | | C | 0.408 | 2.018 | 0.613 | 0.8 | 1 | 45.884 | | | |
| T5 | 0.51 | 2.40 | A | 0.240 | 2.426 | 0.605 | 0.8 | 1 | 37.155 | 3.26 | 167.96 | C |
| 160.00-140.00 | | | B | 0.325 | 2.232 | 0.624 | 0.8 | 1 | 45.720 | | | |
| | | | C | 0.325 | 2.232 | 0.624 | 0.8 | 1 | 46.720 | | | |
| T6 | 0.51 | 2.01 | A | 0.221 | 2.556 | 0.596 | 0.8 | 1 | 33.178 | 3.43 | 171.33 | C |
| 140.00-120.00 | | | B | 0.242 | 2.344 | 0.611 | 0.8 | 1 | 47.429 | | | |
| | | | C | 0.242 | 2.344 | 0.611 | 0.8 | 1 | 47.426 | | | |
| T7 | 0.51 | 3.53 | A | 0.203 | 2.816 | 0.591 | 0.8 | 1 | 42.226 | 3.45 | 172.61 | C |
| 120.00-100.00 | | | B | 0.281 | 2.495 | 0.602 | 0.8 | 1 | 41.251 | | | |
| | | | C | 0.281 | 2.495 | 0.602 | 0.8 | 1 | 48.294 | | | |
| T8 | 0.51 | 4.10 | A | 0.161 | 2.661 | 0.519 | 0.8 | 1 | 18.650 | 3.33 | 187.37 | C |
| 100.00-80.00 | | | B | 0.224 | 2.517 | 0.296 | 0.8 | 1 | 47.819 | | | |
| | | | C | 0.224 | 2.517 | 0.296 | 0.8 | 1 | 47.819 | | | |
| T9 | 0.51 | 4.16 | A | 0.169 | 2.701 | 0.515 | 0.8 | 1 | 41.341 | 3.23 | 182.59 | C |
| 80.00-60.00 | | | B | 0.203 | 2.317 | 0.591 | 0.8 | 1 | 41.763 | | | |
| | | | C | 0.203 | 2.317 | 0.591 | 0.8 | 1 | 41.763 | | | |
| T10 | 0.51 | 3.43 | A | 0.159 | 2.74 | 0.515 | 0.8 | 1 | 41.792 | 3.17 | 178.74 | C |
| 60.00-40.00 | | | B | 0.193 | 2.418 | 0.519 | 0.8 | 1 | 39.511 | | | |
| | | | C | 0.194 | 2.418 | 0.519 | 0.8 | 1 | 51.925 | | | |
| T11 | 0.51 | 3.53 | A | 0.147 | 2.781 | 0.521 | 0.8 | 1 | 34.993 | 2.90 | 143.20 | C |
| 40.00-20.00 | | | B | 0.179 | 2.669 | 0.515 | 0.8 | 1 | 52.679 | | | |
| | | | C | 0.179 | 2.669 | 0.515 | 0.8 | 1 | 54.990 | | | |
| T12 | 0.51 | 4.24 | A | 0.169 | 2.701 | 0.515 | 0.8 | 1 | 41.341 | 2.63 | 133.42 | C |
| 20.00-0.00 | | | B | 0.17 | 2.701 | 0.515 | 0.8 | 1 | 41.341 | | | |
| | | | C | 0.17 | 2.701 | 0.515 | 0.8 | 1 | 41.341 | | | |
| Sum Weight | 5.00 | 39.18 | | | | | | | OTH | 4177.32 | 31.70 | |

| Section Elevation | Add Weight | Self Weight | F | a | Cy | Ra | Dy | Dz | A | F | v | Cat. Face |
|-------------------|------------|-------------|---|-------|-------|-------|------|----|--------|------|--------|-----------|
| # | K | K | f | e | | | | | # | K | # | |
| 240.00-220.00 | 0.21 | 0.65 | A | 0.311 | 2.496 | 0.597 | 0.85 | 1 | 16.479 | 3.66 | 172.18 | C |
| | | | B | 0.172 | 2.693 | 0.515 | 0.85 | 1 | 12.331 | | | |
| | | | C | 0.212 | 1.883 | 0.204 | 0.85 | 1 | 34.189 | | | |
| T2 | 0.28 | 1.10 | A | 0.315 | 2.16 | 0.634 | 0.85 | 1 | 21.874 | 2.87 | 143.35 | C |
| 220.00-200.00 | | | B | 0.221 | 2.526 | 0.555 | 0.85 | 1 | 15.970 | | | |
| | | | C | 0.512 | 1.841 | 0.276 | 0.85 | 1 | 43.422 | | | |
| T3 | 0.49 | 1.21 | A | 0.27 | 1.927 | 0.64 | 0.85 | 1 | 31.529 | 2.91 | 148.69 | C |
| 200.00-180.00 | | | B | 0.457 | 1.962 | 0.477 | 0.85 | 1 | 40.519 | | | |
| | | | C | 0.465 | 1.919 | 0.477 | 0.85 | 1 | 43.882 | | | |
| T4 | 0.51 | 1.70 | A | 0.325 | 2.231 | 0.624 | 0.85 | 1 | 35.534 | 3.21 | 160.38 | C |
| 180.00-160.00 | | | B | 0.400 | 2.049 | 0.615 | 0.85 | 1 | 45.722 | | | |
| | | | C | 0.408 | 2.018 | 0.613 | 0.85 | 1 | 45.884 | | | |
| T5 | 0.51 | 2.40 | A | 0.240 | 2.426 | 0.605 | 0.85 | 1 | 37.155 | 3.26 | 167.96 | C |
| 160.00-140.00 | | | B | 0.325 | 2.232 | 0.624 | 0.85 | 1 | 45.720 | | | |
| | | | C | 0.325 | 2.232 | 0.624 | 0.85 | 1 | 46.720 | | | |
| T6 | 0.51 | 2.01 | A | 0.221 | 2.556 | 0.596 | 0.85 | 1 | 33.178 | 3.43 | 171.33 | C |
| 140.00-120.00 | | | B | 0.242 | 2.344 | 0.611 | 0.85 | 1 | 47.429 | | | |
| | | | C | 0.242 | 2.344 | 0.611 | 0.85 | 1 | 47.426 | | | |
| T7 | 0.51 | 3.53 | A | 0.203 | 2.816 | 0.591 | 0.85 | 1 | 42.226 | 3.45 | 172.61 | C |
| 120.00-100.00 | | | B | 0.281 | 2.495 | 0.602 | 0.85 | 1 | 41.251 | | | |
| | | | C | 0.281 | 2.495 | 0.602 | 0.85 | 1 | 48.294 | | | |
| T8 | 0.51 | 4.10 | A | 0.161 | 2.661 | 0.519 | 0.85 | 1 | 34.993 | 3.23 | 182.59 | C |
| 100.00-80.00 | | | B | 0.224 | 2.517 | 0.296 | 0.85 | 1 | 47.819 | | | |
| | | | C | 0.224 | 2.517 | 0.296 | 0.85 | 1 | 47.819 | | | |
| T9 | 0.51 | 4.16 | A | 0.169 | 2.701 | 0.515 | 0.85 | 1 | 41.341 | 3.17 | 178.74 | C |
| 80.00-60.00 | | | B | 0.203 | 2.317 | 0.591 | 0.85 | 1 | 39.511 | | | |
| | | | C | 0.203 | 2.317 | 0.591 | 0.85 | 1 | 51.925 | | | |
| T10 | 0.51 | 3.43 | A | 0.159 | 2.74 | 0.515 | 0.85 | 1 | 41.792 | 2.90 | 143.20 | C |
| 60.00-40.00 | | | B | 0.193 | 2.418 | 0.519 | 0.85 | 1 | 39.511 | | | |
| | | | C | 0.194 | 2.418 | 0.519 | 0.85 | 1 | 51.925 | | | |
| T11 | 0.51 | 3.53 | A | 0.147 | 2.781 | 0.521 | 0.85 | 1 | 34.993 | 2.63 | 133.42 | C |
| 40.00-20.00 | | | B | 0.179 | 2.669 | 0.515 | 0.85 | 1 | 41.341 | | | |

| Section Elevation | ADD Height | Sqy Height | F # | a | Cy | Rz | Dz | Dz | Az | F | w | Out Face |
|-------------------|------------|------------|-----|-------|-------|-------|------|----|---------|------|--------|----------|
| T1 | 3.60 | 9.02 | A | 0.512 | 2.811 | 0.243 | 0.85 | 1 | 123.468 | 5.23 | 241.48 | C |
| T2 | 3.60 | 9.70 | A | 0.511 | 1.811 | 0.243 | 0.85 | 1 | 123.326 | 5.02 | 251.10 | C |
| T3 | 3.60 | 9.82 | A | 0.512 | 1.811 | 0.243 | 0.85 | 1 | 123.004 | 4.84 | 241.70 | C |
| T4 | 3.60 | 11.47 | A | 0.512 | 2.047 | 0.243 | 0.85 | 1 | 119.310 | 4.59 | 229.66 | C |
| T5 | 3.60 | 11.61 | A | 0.512 | 2.047 | 0.243 | 0.85 | 1 | 119.294 | 4.21 | 210.54 | C |
| T6 | 3.60 | 12.87 | A | 0.512 | 2.227 | 0.243 | 0.85 | 1 | 122.001 | 4.31 | 213.57 | C |
| Sum Weight | 38.45 | 89.30 | | | | | | | | | | |

Tower Forces - Service - Wind Normal To Face

| Section Elevation | ADD Height | Sqy Height | F # | a | Cy | Rz | Dz | Dz | Az | F | w | Out Face |
|-------------------|------------|------------|-----|-------|-------|-------|----|----|--------|------|-------|----------|
| T1 | 0.21 | 0.43 | A | 0.331 | 2.204 | 0.597 | 1 | 1 | 12.629 | 1.33 | 67.33 | C |
| T2 | 0.28 | 1.10 | A | 0.331 | 1.889 | 0.704 | 1 | 1 | 32.070 | 1.49 | 72.56 | C |
| T3 | 0.49 | 1.28 | A | 0.331 | 2.204 | 0.597 | 1 | 1 | 17.735 | 1.48 | 74.08 | C |
| T4 | 0.51 | 1.70 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 32.323 | 1.65 | 82.60 | C |
| T5 | 0.51 | 2.43 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 41.425 | 1.74 | 87.61 | C |
| T6 | 0.51 | 3.01 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 48.715 | 1.79 | 89.33 | C |
| T7 | 0.51 | 3.53 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 50.707 | 1.81 | 90.47 | C |
| T8 | 0.51 | 4.10 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 49.908 | 1.74 | 88.85 | C |
| T9 | 0.51 | 4.16 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 45.214 | 1.67 | 83.70 | C |
| T10 | 0.51 | 4.43 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 45.135 | 1.64 | 82.18 | C |
| Sum Weight | 3.60 | 37.18 | | | | | | | | | | |

Tower Forces - Service - Wind 90 To Face

| Section Elevation | ADD Height | Sqy Height | F # | a | Cy | Rz | Dz | Dz | Az | F | w | Out Face |
|-------------------|------------|------------|-----|-------|-------|-------|----|----|--------|------|-------|----------|
| T1 | 0.21 | 0.43 | A | 0.331 | 2.456 | 0.597 | 1 | 1 | 18.449 | 1.33 | 66.21 | C |
| T2 | 0.28 | 1.15 | A | 0.331 | 1.845 | 0.704 | 1 | 1 | 54.803 | 1.43 | 74.03 | C |
| T3 | 0.49 | 1.28 | A | 0.331 | 2.204 | 0.597 | 1 | 1 | 17.735 | 1.48 | 72.56 | C |
| T4 | 0.51 | 1.70 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 32.323 | 1.61 | 83.58 | C |
| T5 | 0.51 | 2.43 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 41.290 | 1.69 | 85.31 | C |
| T6 | 0.51 | 3.01 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 47.209 | 1.73 | 85.44 | C |
| T7 | 0.51 | 3.53 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 48.788 | 1.74 | 83.32 | C |
| T8 | 0.51 | 4.10 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 48.924 | 1.61 | 83.23 | C |
| T9 | 0.51 | 4.16 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 44.829 | 1.62 | 81.01 | C |
| T10 | 0.51 | 4.43 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 44.792 | 1.58 | 79.10 | C |
| T11 | 0.51 | 5.53 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 42.995 | 1.45 | 72.33 | C |
| T12 | 0.51 | 6.24 | A | 0.331 | 2.231 | 0.624 | 1 | 1 | 45.205 | 1.51 | 75.45 | C |
| Sum Weight | 3.60 | 38.18 | | | | | | | | | | |

Mast Vectors - No Ice

| Section No | Section Elevation | Wind Direction | F | Fy | Fz | OTD _x | OTD _y | OTD _z |
|------------|-------------------|----------------|------|-------|-------|------------------|------------------|------------------|
| T1 | 240.00-220.00 | Wind Normal | 2.70 | 0.00 | -3.30 | -491.56 | 0.00 | 0.00 |
| | 0 | Wind 90 | 2.66 | 2.33 | -3.30 | -339.37 | -505.43 | 0.00 |
| | 45 | Wind 90 | 2.66 | 2.33 | -3.30 | -338.81 | -505.00 | 0.00 |
| | 90 | Wind 90 | 2.66 | 2.41 | 0.00 | -511.24 | 0.00 | |
| | 135 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |

| Section Elevation | ADD Height | Sqy Height | F # | a | Cy | Rz | Dz | Dz | Az | F | w | Out Face |
|-------------------|------------|------------|-----|-------|-------|-------|----|----|--------|------|-------|----------|
| T1 | 0.51 | 5.53 | A | 0.199 | 2.618 | 0.230 | 1 | 1 | 35.911 | 1.11 | 73.32 | C |
| T2 | 0.51 | 6.34 | A | 0.147 | 2.774 | 0.230 | 1 | 1 | 34.658 | 1.57 | 78.64 | C |
| T3 | 0.51 | 7.15 | A | 0.179 | 2.679 | 0.230 | 1 | 1 | 34.658 | 1.57 | 78.64 | C |
| T4 | 0.51 | 8.00 | A | 0.179 | 2.679 | 0.230 | 1 | 1 | 34.658 | 1.57 | 78.64 | C |
| T5 | 0.51 | 9.00 | A | 0.147 | 2.679 | 0.230 | 1 | 1 | 34.658 | 1.57 | 78.64 | C |
| Sum Weight | 5.60 | 38.18 | | | | | | | | | | |

Tower Forces - Service - Wind 60 To Face

| Section Elevation | ADD Height | Sqy Height | F # | a | Cy | Rz | Dz | Dz | Az | F | w | Out Face |
|-------------------|------------|------------|-----|-------|-------|-------|----|----|--------|------|-------|----------|
| T1 | 0.21 | 0.43 | A | 0.231 | 2.490 | 0.597 | 1 | 1 | 18.026 | 1.33 | 65.84 | C |
| T2 | 0.28 | 1.10 | A | 0.231 | 1.815 | 0.704 | 1 | 1 | 38.180 | 1.43 | 74.03 | C |
| T3 | 0.49 | 1.28 | A | 0.231 | 2.204 | 0.597 | 1 | 1 | 17.735 | 1.48 | 72.56 | C |
| T4 | 0.51 | 1.70 | A | 0.231 | 2.231 | 0.624 | 1 | 1 | 32.323 | 1.61 | 83.58 | C |
| T5 | 0.51 | 2.43 | A | 0.231 | 2.231 | 0.624 | 1 | 1 | 41.290 | 1.69 | 85.31 | C |
| T6 | 0.51 | 3.01 | A | 0.231 | 2.231 | 0.624 | 1 | 1 | 47.209 | 1.73 | 85.44 | C |
| T7 | 0.51 | 3.53 | A | 0.231 | 2.231 | 0.624 | 1 | 1 | 48.788 | 1.74 | 83.32 | C |
| T8 | 0.51 | 4.10 | A | 0.231 | 2.231 | 0.624 | 1 | 1 | 48.924 | 1.61 | 83.23 | C |
| T9 | 0.51 | 4.16 | A | 0.231 | 2.231 | 0.624 | 1 | 1 | 44.829 | 1.62 | 81.01 | C |
| T10 | 0.51 | 4.43 | A | 0.231 | 2.231 | 0.624 | 1 | 1 | 44.792 | 1.58 | 79.10 | C |
| T11 | 0.51 | 5.53 | A | 0.199 | 2.618 | 0.230 | 1 | 1 | 35.911 | 1.11 | 73.32 | C |
| T12 | 0.51 | 6.34 | A | 0.147 | 2.774 | 0.230 | 1 | 1 | 34.658 | 1.57 | 78.64 | C |
| Sum Weight | 5.60 | 37.18 | | | | | | | | | | |

| Section No | Section Elevation | Wind Direction | F | Fy | Fz | OTD _x | OTD _y | OTD _z |
|------------|-------------------|----------------|------|-------|-------|------------------|------------------|------------------|
| T1 | 220.00-200.00 | Wind 90 | 2.66 | 1.33 | -3.30 | -320.33 | -515.43 | 0.00 |
| | 180 | Wind 60 | 2.64 | 0.00 | -3.30 | -527.81 | 0.00 | |
| | 150 | Wind 90 | 2.66 | -1.33 | -3.30 | -329.37 | -529.43 | 0.00 |
| | 120 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| | 90 | Wind 90 | 2.66 | -2.66 | 0.00 | -511.24 | 0.00 | |
| | 60 | Wind 60 | 2.66 | -2.33 | -3.30 | -339.37 | -505.43 | 0.00 |
| | 30 | Wind 90 | 2.66 | -2.33 | -3.30 | -338.81 | -505.00 | 0.00 |
| | 0 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| T2 | 200.00-180.00 | Wind 90 | 2.66 | 1.33 | -3.30 | -320.33 | -515.43 | 0.00 |
| | 180 | Wind 60 | 2.64 | 0.00 | -3.30 | -527.81 | 0.00 | |
| | 150 | Wind 90 | 2.66 | -1.33 | -3.30 | -329.37 | -529.43 | 0.00 |
| | 120 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| | 90 | Wind 90 | 2.66 | -2.66 | 0.00 | -511.24 | 0.00 | |
| | 60 | Wind 60 | 2.66 | -2.33 | -3.30 | -339.37 | -505.43 | 0.00 |
| | 30 | Wind 90 | 2.66 | -2.33 | -3.30 | -338.81 | -505.00 | 0.00 |
| | 0 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| T3 | 200.00-160.00 | Wind 90 | 2.66 | 1.33 | -3.30 | -320.33 | -515.43 | 0.00 |
| | 180 | Wind 60 | 2.64 | 0.00 | -3.30 | -527.81 | 0.00 | |
| | 150 | Wind 90 | 2.66 | -1.33 | -3.30 | -329.37 | -529.43 | 0.00 |
| | 120 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| | 90 | Wind 90 | 2.66 | -2.66 | 0.00 | -511.24 | 0.00 | |
| | 60 | Wind 60 | 2.66 | -2.33 | -3.30 | -339.37 | -505.43 | 0.00 |
| | 30 | Wind 90 | 2.66 | -2.33 | -3.30 | -338.81 | -505.00 | 0.00 |
| | 0 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| T4 | 180.00-160.00 | Wind 90 | 2.66 | 1.33 | -3.30 | -320.33 | -515.43 | 0.00 |
| | 180 | Wind 60 | 2.64 | 0.00 | -3.30 | -527.81 | 0.00 | |
| | 150 | Wind 90 | 2.66 | -1.33 | -3.30 | -329.37 | -529.43 | 0.00 |
| | 120 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| | 90 | Wind 90 | 2.66 | -2.66 | 0.00 | -511.24 | 0.00 | |
| | 60 | Wind 60 | 2.66 | -2.33 | -3.30 | -339.37 | -505.43 | 0.00 |
| | 30 | Wind 90 | 2.66 | -2.33 | -3.30 | -338.81 | -505.00 | 0.00 |
| | 0 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| T5 | 160.00-140.00 | Wind 90 | 2.66 | 1.33 | -3.30 | -320.33 | -515.43 | 0.00 |
| | 180 | Wind 60 | 2.64 | 0.00 | -3.30 | -527.81 | 0.00 | |
| | 150 | Wind 90 | 2.66 | -1.33 | -3.30 | -329.37 | -529.43 | 0.00 |
| | 120 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| | 90 | Wind 90 | 2.66 | -2.66 | 0.00 | -511.24 | 0.00 | |
| | 60 | Wind 60 | 2.66 | -2.33 | -3.30 | -339.37 | -505.43 | 0.00 |
| | 30 | Wind 90 | 2.66 | -2.33 | -3.30 | -338.81 | -505.00 | 0.00 |
| | 0 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| T6 | 140.00-120.00 | Wind 90 | 2.66 | 1.33 | -3.30 | -320.33 | -515.43 | 0.00 |
| | 180 | Wind 60 | 2.64 | 0.00 | -3.30 | -527.81 | 0.00 | |
| | 150 | Wind 90 | 2.66 | -1.33 | -3.30 | -329.37 | -529.43 | 0.00 |
| | 120 | Wind Normal | 2.70 | -2.34 | 1.35 | -310.71 | -334.29 | 0.00 |
| | 90 | Wind 90 | 2.66 | -2.66 | 0.00 | -511.24 | 0.00 | |
| | 60 | Wind 60 | 2.66 | -2.33 | -3.30 | -339.37 | -505.43 | |

inxTower

Job: 284859 Page: 25 of 107

Project: V-25 x 240 - Ashford, CT Date: 15:15:37 03/30/15

Client: Verizon Wireless Designed by: JAK

1345 Fiske Dr.
 Plymouth, IN
 Phone: (317) 936-6221
 FAX: (317) 936-6218

inxTower

Job: 284859 Page: 26 of 107

Project: V-25 x 240 - Ashford, CT Date: 15:15:37 03/30/15

Client: Verizon Wireless Designed by: JAK

1345 Fiske Dr.
 Plymouth, IN
 Phone: (317) 936-6221
 FAX: (317) 936-6218

| Section No. | Section Elevation R | Wind Attach # | Directionality | F | | | OMs | | | Torque | |
|-------------|---------------------|---------------|----------------|-------------|----------------|----------------|-----------------|-----------------|-----------------|--------|------|
| | | | | K | K _x | K _y | OM _x | OM _y | OM _z | | |
| T7 | 120.00-100.00 | Wind 60 | 3-41 | 8.00 | 3.40 | 443.94 | 0.00 | 0.00 | | | |
| | | | 3-47 | -1.11 | 0.00 | 39.03 | 235.33 | 0.00 | | | |
| | | | 3-59 | -3.11 | 1.79 | 30.18 | 135.33 | 0.00 | | | |
| | | Wind 90 | 3-47 | -3.47 | 0.00 | 0.00 | 451.66 | 0.00 | 0.00 | | |
| | | | 3-43 | -2.97 | -1.77 | -222.94 | 386.23 | 0.00 | 0.00 | | |
| | | | 3-47 | -1.11 | 0.00 | -39.03 | 235.33 | 0.00 | 0.00 | | |
| | | T8 | 160.00-83.00 | Wind Normal | 3-43 | 0.00 | -3.47 | -399.43 | 0.00 | 0.00 | |
| | | | | | 3.50 | 1.75 | -3.03 | -313.15 | -192.23 | 0.00 | |
| | | | | | 3-45 | 8.00 | -1.73 | -183.87 | -328.83 | 0.00 | |
| | | | | Wind 90 | 3-45 | 8.00 | 0.00 | 0.00 | 384.66 | 0.00 | 0.00 |
| | | | | | 3-50 | -1.73 | 3.03 | 333.13 | -192.23 | 0.00 | 0.00 |
| | | | | | 3-45 | 8.00 | 1.41 | 379.24 | 8.00 | 0.00 | 0.00 |
| T9 | 83.00-60.00 | | | Wind 90 | 3-50 | -1.73 | 3.03 | 333.13 | 192.23 | 0.00 | |
| | | | | | 3-50 | -1.73 | 3.03 | 333.13 | 192.23 | 0.00 | |
| | | | | | 3-43 | -1.14 | 1.82 | 159.73 | 134.50 | 0.00 | 0.00 |
| | | | | Wind Normal | 3-50 | -3.50 | 0.00 | 0.00 | 384.66 | 0.00 | 0.00 |
| | | | | | 3-43 | -3.09 | -1.73 | -171.11 | 299.11 | 0.00 | 0.00 |
| | | | | | 3-50 | -1.73 | -3.03 | -333.13 | 192.23 | 0.00 | 0.00 |
| | | T10 | 60.00-40.00 | Wind Normal | 3-43 | 0.00 | -3.47 | -399.43 | 0.00 | 0.00 | |
| | | | | | 3.23 | 1.69 | -3.53 | -313.71 | 0.00 | 0.00 | |
| | | | | | 3-23 | 1.69 | -3.53 | -219.49 | -132.13 | 0.00 | 0.00 |
| | | | | Wind 90 | 3-23 | 1.69 | 0.00 | 0.00 | 404.26 | 0.00 | 0.00 |
| | | | | | 3-23 | 1.69 | 0.00 | 0.00 | 404.26 | 0.00 | 0.00 |
| | | | | | 3-23 | 1.69 | 0.00 | 0.00 | 404.26 | 0.00 | 0.00 |
| T11 | 40.00-20.00 | | | Wind Normal | 3-23 | 1.69 | 0.00 | 0.00 | 404.26 | 0.00 | 0.00 |
| | | | | | 3-23 | 1.69 | 0.00 | 0.00 | 404.26 | 0.00 | 0.00 |
| | | | | | 3-23 | 1.69 | 0.00 | 0.00 | 404.26 | 0.00 | 0.00 |
| | | | | Wind 90 | 3-23 | 1.69 | 0.00 | 0.00 | 404.26 | 0.00 | 0.00 |
| | | | | | 3-23 | 1.69 | 0.00 | 0.00 | 404.26 | 0.00 | 0.00 |
| | | | | | 3-23 | 1.69 | 0.00 | 0.00 | 404.26 | 0.00 | 0.00 |

| Section No. | Section Elevation R | Wind Attach # | Directionality | F | | | OMs | | | Torque | |
|-------------|---------------------|---------------|----------------|-------------|----------------|----------------|-----------------|-----------------|-----------------|--------|------|
| | | | | K | K _x | K _y | OM _x | OM _y | OM _z | | |
| T12 | 20.00-0.00 | Wind 60 | 3-30 | 2.90 | -1.40 | 1.33 | 54.55 | -13.55 | 0.00 | | |
| | | | 2-40 | 3.01 | -2.42 | 1.31 | 49.33 | -16.33 | 0.00 | | |
| | | | 2-50 | 2.90 | -2.90 | 0.00 | 0.00 | 81.13 | 0.00 | | |
| | | Wind 90 | 2-40 | -2.42 | -1.41 | -1.43 | -42.99 | 74.43 | 0.00 | | |
| | | | 2-50 | -2.90 | -1.41 | -1.51 | -35.43 | -81.56 | 0.00 | | |
| | | | 2-40 | -2.42 | -1.41 | -1.51 | -35.43 | -81.56 | 0.00 | | |
| | | T13 | 20.00-0.00 | Wind Normal | 3-10 | 0.00 | -3.16 | -1.11 | -21.21 | 0.00 | 0.00 |
| | | | | | 3-20 | 1.63 | 1.31 | -2.42 | -26.23 | -13.14 | 0.00 |
| | | | | | 3-30 | 2.90 | 2.90 | -1.49 | -14.53 | -23.83 | 0.00 |
| | | | | Wind 90 | 3-30 | 2.90 | 0.00 | 0.00 | 332.29 | 0.00 | 0.00 |
| | | | | | 3-30 | 2.90 | 0.00 | 0.00 | 332.29 | 0.00 | 0.00 |
| | | | | | 3-30 | 2.90 | 0.00 | 0.00 | 332.29 | 0.00 | 0.00 |

Mast Totals - No Ice

| Wind Attach # | F | K | OM _x | OM _y | Torque |
|---------------|--------|--------|-----------------|-----------------|--------|
| 0 | 0.00 | -18.34 | -117.57 | 0.00 | 0.00 |
| 30 | 18.99 | -32.72 | -219.14 | -323.18 | 0.00 |
| 60 | 72.39 | -11.20 | -715.95 | -393.87 | 0.00 |
| 90 | 37.70 | 0.00 | -215.97 | -393.87 | 0.00 |
| 120 | 33.72 | 18.47 | -202.21 | -392.97 | 0.00 |
| 150 | 18.81 | 52.72 | -373.14 | -225.16 | 0.00 |
| 180 | 0.00 | 47.62 | -423.95 | 0.00 | 0.00 |
| 210 | -18.89 | 32.72 | -373.14 | 225.16 | 0.00 |
| 240 | -33.72 | 18.47 | -202.21 | 372.95 | 0.00 |
| 270 | -37.70 | 0.00 | -215.97 | 393.87 | 0.00 |
| 300 | -37.33 | -18.20 | -228.58 | 119.87 | 0.00 |
| 330 | -18.92 | -32.72 | -219.14 | 225.18 | 0.00 |

Mast Vectors - With Ice

| Section No. | Section Elevation R | Wind Attach # | Directionality | F | | | OMs | | | Torque | |
|-------------|---------------------|---------------|----------------|-------------|----------------|----------------|-----------------|-----------------|-----------------|---------|----------|
| | | | | K | K _x | K _y | OM _x | OM _y | OM _z | | |
| T1 | 243.00-233.00 | Wind Normal | 3-09 | 0.00 | -5.09 | -1170.93 | 0.00 | 0.00 | | | |
| | | | 3-18 | 4.54 | 2.27 | -904.63 | -121.84 | 0.00 | | | |
| | | | 3-27 | 4.54 | 3.77 | -2.11 | -500.76 | -487.93 | 0.00 | | |
| | | Wind 90 | 3-27 | 4.54 | 4.54 | 0.00 | 0.00 | -1523.88 | 0.00 | | |
| | | | 3-27 | 4.54 | 4.54 | 0.00 | 0.00 | 0.00 | -1523.88 | | |
| | | | 3-27 | 4.54 | 4.54 | 0.00 | 0.00 | 0.00 | -1523.88 | | |
| | | T2 | 220.00-200.00 | Wind Normal | 3-09 | 0.00 | -5.09 | -1170.93 | 0.00 | 0.00 | |
| | | | | | 3-18 | 4.54 | 2.27 | -904.63 | -121.84 | 0.00 | |
| | | | | | 3-27 | 4.54 | 3.77 | -2.11 | -500.76 | -487.93 | 0.00 |
| | | | | Wind 90 | 3-27 | 4.54 | 4.54 | 0.00 | 0.00 | 0.00 | -1523.88 |
| | | | | | 3-27 | 4.54 | 4.54 | 0.00 | 0.00 | 0.00 | -1523.88 |
| | | | | | 3-27 | 4.54 | 4.54 | 0.00 | 0.00 | 0.00 | -1523.88 |

inxTower

Job: 284859 Page: 27 of 107

Project: V-25 x 240 - Ashford, CT Date: 15:15:37 03/30/15

Client: Verizon Wireless Designed by: JAK

1345 Fiske Dr.
 Plymouth, IN
 Phone: (317) 936-6221
 FAX: (317) 936-6218

inxTower

Job: 284859 Page: 28 of 107

Project: V-25 x 240 - Ashford, CT Date: 15:15:37 03/30/15

Client: Verizon Wireless Designed by: JAK

1345 Fiske Dr.
 Plymouth, IN
 Phone: (317) 936-6221
 FAX: (317) 936-6218

| Section No. | Section Elevation R | Wind Attach # | Directionality | F | | | OMs | | | Torque | |
|-------------|---------------------|---------------|----------------|-------------|----------------|----------------|-----------------|-----------------|-----------------|--------|------|
| | | | | K | K _x | K _y | OM _x | OM _y | OM _z | | |
| T2 | 220.00-200.00 | Wind 90 | 4-34 | -2.27 | -3.53 | -504.03 | 531.94 | 0.00 | | | |
| | | | 4-39 | 0.00 | -5.39 | -1113.44 | 0.00 | 0.00 | | | |
| | | | 4-34 | 1.81 | -1.19 | -410.56 | -503.23 | 0.00 | | | |
| | | Wind Normal | 4-34 | 4.81 | 0.00 | 0.00 | -1033.83 | 0.00 | 0.00 | | |
| | | | 4-39 | 2.69 | 1.69 | 55.77 | -979.95 | 0.00 | 0.00 | | |
| | | | 4-34 | 2.42 | 4.19 | 379.96 | -979.95 | 0.00 | 0.00 | | |
| | | T3 | 200.00-180.00 | Wind Normal | 4-34 | 0.00 | -4.81 | -493.81 | 0.00 | 0.00 | |
| | | | | | 4-39 | -2.42 | -4.19 | -379.96 | -502.33 | 0.00 | |
| | | | | | 4-34 | 2.42 | 4.19 | 379.96 | -502.33 | 0.00 | |
| | | | | Wind 90 | 4-34 | 4.81 | 0.00 | 0.00 | -1033.83 | 0.00 | 0.00 |
| | | | | | 4-39 | 2.69 | 1.69 | 55.77 | -979.95 | 0.00 | 0.00 |
| | | | | | 4-34 | 2.42 | 4.19 | 379.96 | -979.95 | 0.00 | 0.00 |

| Section No. | Section Elevation R | Wind Attach # | Directionality | F | | | OMs | | | Torque | |
|-------------|---------------------|---------------|----------------|-------------|----------------|----------------|-----------------|-----------------|-----------------|--------|------|
| | | | | K | K _x | K _y | OM _x | OM _y | OM _z | | |
| T7 | 120.00-100.00 | Wind Normal | 3-10 | 0.00 | -3.16 | -1.11 | -21.21 | 0.00 | 0.00 | | |
| | | | 3-20 | 1.63 | 1.31 | -2.42 | -26.23 | -13.14 | 0.00 | | |
| | | | 3-30 | 2.90 | 2.90 | -1.49 | -14.53 | -23.83 | 0.00 | | |
| | | Wind 90 | 3-30 | 2.90 | 0.00 | 0.00 | 332.29 | 0.00 | 0.00 | | |
| | | | 3-30 | 2.90 | 0.00 | 0.00 | 332.29 | 0.00 | 0.00 | | |
| | | | 3-30 | 2.90 | 0.00 | 0.00 | 332.29 | 0.00 | 0.00 | | |
| | | T8 | 160.00-83.00 | Wind Normal | 3-10 | 0.00 | -3.16 | -1.11 | -21.21 | 0.00 | 0.00 |
| | | | | | 3-20 | 1.63 | 1.31 | -2.42 | -26.23 | -13.14 | 0.00 |
| | | | | | 3-30 | 2.90 | 2.90 | -1.49 | -14.53 | -23.83 | 0.00 |
| | | | | Wind 90 | 3-30 | 2.90 | 0.00 | 0.00 | 332.29 | 0.00 | 0.00 |
| | | | | | 3-30 | 2.90 | 0.00 | 0.00 | 332.29 | 0.00 | 0.00 |
| | | | | | 3-30 | 2.90 | 0.00 | 0.00 | 332.29 | 0.00 | 0.00 |

| | | | | | |
|---|--|---------|---------------------------|-------------|-------------------|
| tnxTower | | Job | 284859 | Page | 28 of 107 |
| 1343 Peko Dr. Plymouth, IN Phone: (317) 935-0211 FAX: (317) 935-0638 | | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/15 |
| | | Client | Verizon Wireless | Designed by | JAK |

| Section No. | Section Elevation β | Wind Acreage α | Directionality | F | K | V _F | V _K | V _{V_F} | ODM _F | ODM _K | Torque |
|-------------|---------------------------|-----------------------|----------------|------|------|----------------|----------------|----------------------------|------------------|------------------|--------|
| 55 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 60 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 65 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 70 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 75 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 80 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 85 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 90 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 95 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 100 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 105 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 110 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 115 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 120 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 125 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 130 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 135 | Wind 90 | 0 | 0 | 1.31 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |

Mast Totals - With Ice

| Wind Acreage α | F | K | V _F | V _K | V _{V_F} | ODM _F | ODM _K | Torque |
|-----------------------|--------|---|----------------|----------------|----------------------------|------------------|------------------|--------|
| 0 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 30 | 28.67 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 60 | 41.69 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 90 | 37.31 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 120 | 34.81 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 150 | 28.67 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 180 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 210 | -28.67 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 240 | -44.41 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 270 | -37.31 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 300 | -17.59 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 330 | -28.67 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |

Mast Vectors - Service

| Section No. | Section Elevation β | Wind Acreage α | Directionality | F | K | V _F | V _K | V _{V_F} | ODM _F | ODM _K | Torque |
|-------------|---------------------------|-----------------------|----------------|------|------|----------------|----------------|----------------------------|------------------|------------------|--------|
| 11 | 249.05-320.00 | 0 | Wind Normal | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 20 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 30 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 40 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 50 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 60 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 70 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 80 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 90 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 100 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 110 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 120 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 130 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 140 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 150 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 160 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 170 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 180 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 190 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 200 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 210 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 220 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 230 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 240 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 250 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 260 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 270 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 280 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 290 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 300 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 310 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 320 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |
| 330 | Wind 90 | 0 | 0 | 1.31 | 0.00 | -0.31 | -0.09 | 0.00 | -0.00 | 0.00 | 0.00 |

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|---|--|---------|---------------------------|-------------|-------------------|
| tnxTower | | Job | 284859 | Page | 30 of 107 |
| 1343 Peko Dr. Plymouth, IN Phone: (317) 935-0211 FAX: (317) 935-0638 | | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/15 |
| | | Client | Verizon Wireless | Designed by | JAK |

| Section No. | Section Elevation β | Wind Acreage α | Directionality | F | K | V _F | V _K | V _{V_F} | ODM _F | ODM _K | Torque |
|-------------|---------------------------|-----------------------|----------------|------|------|----------------|----------------|----------------------------|------------------|------------------|--------|
| 130 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 140 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 150 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 160 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 170 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 180 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 190 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 200 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 210 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 220 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 230 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 240 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 250 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 260 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 270 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 280 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 290 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 300 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 310 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 320 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 330 | Wind 90 | 0 | 0 | 1.41 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |

| | | | | | |
|---|--|---------|---------------------------|-------------|-------------------|
| tnxTower | | Job | 284859 | Page | 31 of 107 |
| 1343 Peko Dr. Plymouth, IN Phone: (317) 935-0211 FAX: (317) 935-0638 | | Project | V-25 x 240' - Ashford, CT | Date | 16:16:37 03/30/15 |
| | | Client | Verizon Wireless | Designed by | JAK |

| Section No. | Section Elevation β | Wind Acreage α | Directionality | F | K | V _F | V _K | V _{V_F} | ODM _F | ODM _K | Torque |
|-------------|---------------------------|-----------------------|----------------|------|------|----------------|----------------|----------------------------|------------------|------------------|--------|
| 180 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 190 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 200 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 210 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 220 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 230 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 240 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 250 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 260 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 270 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 280 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 290 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 300 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 310 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 320 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 330 | Wind 90 | 0 | 0 | 1.39 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |

| | | | | | |
|---|--|---------|---------------------------|-------------|-------------------|
| tnxTower | | Job | 284859 | Page | 32 of 107 |
| 1343 Peko Dr. Plymouth, IN Phone: (317) 935-0211 FAX: (317) 935-0638 | | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/15 |
| | | Client | Verizon Wireless | Designed by | JAK |

| Section No. | Section Elevation β | Wind Acreage α | Directionality | F | K | V _F | V _K | V _{V_F} | ODM _F | ODM _K | Torque |
|-------------|---------------------------|-----------------------|----------------|------|------|----------------|----------------|----------------------------|------------------|------------------|--------|
| 210 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 220 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 230 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 240 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 250 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 260 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 270 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 280 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 290 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 300 | Wind 90 | 0 | 0 | 1.51 | 0.00 | 0 | 0 | | | | |

Wind Load Analysis Table (Section 11.3.1) - From Leg C

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.31 | 0.31 | 0.31 | 7.79 | -4.11 | 1.21 |
| 30 | 0.00 | 0.31 | 0.31 | 6.43 | -56.64 | 1.81 |
| 60 | 0.21 | 0.27 | 0.31 | 8.78 | 15.83 | 1.58 |
| 90 | 0.41 | 0.00 | 0.31 | 8.80 | 83.91 | 0.91 |
| 120 | 0.41 | 0.16 | 0.31 | 15.65 | 192.90 | -0.91 |
| 150 | 0.27 | 0.27 | 0.31 | -27.33 | 89.97 | -1.51 |
| 180 | 0.00 | 0.31 | 0.31 | -43.93 | 37.43 | -1.81 |

Wind Load Analysis Table (Section 11.3.1) - From Leg B

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.23 | 0.23 | 0.23 | -13.33 | 16.63 | 1.33 |
| 30 | 0.23 | 0.27 | 0.23 | -29.59 | -37.43 | 1.81 |
| 60 | 0.41 | 0.16 | 0.23 | -7.73 | -82.07 | 1.58 |
| 90 | 0.41 | 0.00 | 0.23 | 36.23 | -97.33 | 0.91 |
| 120 | 0.41 | 0.16 | 0.23 | 83.90 | -65.81 | -0.91 |
| 150 | 0.27 | 0.27 | 0.23 | 83.78 | -16.41 | -1.51 |
| 180 | 0.00 | 0.23 | 0.23 | 63.31 | 16.64 | -1.81 |
| 210 | 0.23 | 0.23 | 0.23 | 27.78 | 83.11 | -1.51 |
| 240 | 0.41 | 0.16 | 0.23 | -16.30 | 107.13 | -0.91 |
| 270 | 0.41 | 0.00 | 0.23 | -55.73 | 96.60 | 0.91 |
| 300 | 0.27 | 0.27 | 0.23 | -32.34 | 63.09 | 1.51 |
| 330 | 0.00 | 0.23 | 0.23 | -43.93 | 37.43 | 1.81 |

Wind Load Analysis Table (Section 11.3.1) - From Leg A

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.41 | 0.00 | 0.00 | -4.47 | -112.45 | 0.00 |
| 30 | 0.41 | 0.16 | 0.00 | -97.43 | -37.43 | -0.91 |
| 60 | 0.27 | 0.27 | 0.00 | -56.64 | -64.11 | -1.58 |
| 90 | 0.00 | 0.31 | 0.00 | -4.46 | -74.87 | -1.81 |
| 120 | 0.27 | 0.27 | 0.00 | 35.34 | -64.11 | -1.58 |
| 150 | 0.41 | 0.16 | 0.00 | 96.54 | -37.43 | -0.91 |
| 180 | 0.41 | 0.00 | 0.00 | 112.45 | 0.00 | 0.00 |
| 210 | 0.27 | 0.27 | 0.00 | 66.54 | 37.43 | 0.91 |
| 240 | 0.41 | 0.16 | 0.00 | 35.34 | 64.11 | 1.58 |
| 270 | 0.41 | 0.00 | 0.00 | -4.46 | 74.87 | 1.81 |
| 300 | 0.27 | 0.27 | 0.00 | -56.64 | 64.11 | 1.58 |
| 330 | 0.41 | 0.16 | 0.00 | -97.43 | 37.43 | 0.91 |

Wind Load Analysis Table (Section 11.3.1) - From Leg C

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.31 | 0.31 | 0.31 | -6.64 | -17.83 | 0.91 |
| 30 | 0.00 | 0.31 | 0.31 | -11.37 | 3.08 | -0.91 |
| 60 | 0.21 | 0.27 | 0.31 | -1.96 | -3.08 | 0.00 |
| 90 | 0.41 | 0.00 | 0.31 | 1.96 | -8.31 | 0.91 |
| 120 | 0.41 | 0.16 | 0.31 | 15.21 | -11.37 | 0.00 |
| 150 | 0.27 | 0.27 | 0.31 | 18.82 | -11.37 | 0.00 |
| 180 | 0.00 | 0.31 | 0.31 | 18.82 | -7.55 | 0.91 |

Wind Load Analysis Table (Section 11.3.1) - From Leg C

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 210 | 0.01 | 0.01 | 0.01 | 0.01 | 11.67 | -2.56 |
| 240 | 0.01 | 0.01 | 0.01 | 0.01 | 2.07 | 3.51 |
| 270 | 0.01 | 0.01 | 0.01 | -0.01 | -1.64 | 1.81 |
| 300 | 0.01 | 0.01 | 0.01 | -0.01 | -15.99 | -0.49 |
| 330 | 0.01 | 0.01 | 0.01 | -0.01 | -19.21 | -0.54 |

Wind Load Analysis Table (Section 11.3.1) - From Leg B

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.01 | 0.01 | 0.01 | -0.01 | -17.19 | -1.47 |
| 30 | 0.01 | 0.01 | 0.01 | -0.01 | -18.21 | -1.65 |
| 60 | 0.01 | 0.01 | 0.01 | -0.01 | -15.99 | -1.78 |
| 90 | 0.01 | 0.01 | 0.01 | -0.01 | -4.65 | -1.83 |
| 120 | 0.01 | 0.01 | 0.01 | 0.01 | 2.07 | -3.51 |
| 150 | 0.01 | 0.01 | 0.01 | 0.01 | 11.67 | 2.56 |
| 180 | 0.01 | 0.01 | 0.01 | 0.01 | 18.20 | 7.85 |
| 210 | 0.01 | 0.01 | 0.01 | 0.01 | 18.20 | 11.13 |
| 240 | 0.01 | 0.01 | 0.01 | 0.01 | 14.21 | 11.99 |
| 270 | 0.01 | 0.01 | 0.01 | 0.01 | 8.34 | 13.11 |
| 300 | 0.01 | 0.01 | 0.01 | -0.01 | -1.79 | 13.00 |
| 330 | 0.01 | 0.01 | 0.01 | -0.01 | -11.37 | -3.01 |

Wind Load Analysis Table (Section 11.3.1) - From Leg A

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.01 | 0.01 | 0.01 | -0.01 | -4.13 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | -0.01 | -3.41 | -0.24 |
| 60 | 0.01 | 0.01 | 0.01 | -0.01 | -2.33 | -0.70 |
| 90 | 0.01 | 0.01 | 0.01 | 0.01 | -0.20 | -0.49 |
| 120 | 0.01 | 0.01 | 0.01 | 0.01 | 1.41 | -0.70 |
| 150 | 0.01 | 0.01 | 0.01 | 0.01 | 3.07 | -1.13 |
| 180 | 0.01 | 0.01 | 0.01 | 0.01 | 3.51 | 0.00 |
| 210 | 0.01 | 0.01 | 0.01 | 0.01 | 3.51 | 0.00 |
| 240 | 0.01 | 0.01 | 0.01 | 0.01 | 3.51 | 0.00 |
| 270 | 0.01 | 0.01 | 0.01 | 0.01 | 1.41 | 11.39 |
| 300 | 0.01 | 0.01 | 0.01 | -0.01 | -0.20 | 10.73 |
| 330 | 0.01 | 0.01 | 0.01 | -0.01 | -2.33 | 16.33 |

Wind Load Analysis Table (Section 11.3.1) - From Leg C

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.01 | 0.01 | 0.01 | 0.01 | -15.83 | -3.73 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | -15.74 | -4.17 |
| 60 | 0.01 | 0.01 | 0.01 | 0.01 | -11.31 | -4.20 |
| 90 | 0.01 | 0.01 | 0.01 | 0.01 | -3.83 | -4.17 |
| 120 | 0.01 | 0.01 | 0.01 | 0.01 | 4.70 | -4.17 |
| 150 | 0.01 | 0.01 | 0.01 | 0.01 | 16.31 | -4.20 |
| 180 | 0.01 | 0.01 | 0.01 | 0.01 | 32.00 | -4.17 |
| 210 | 0.01 | 0.01 | 0.01 | 0.01 | 16.31 | -4.20 |
| 240 | 0.01 | 0.01 | 0.01 | 0.01 | 14.00 | -4.17 |
| 270 | 0.01 | 0.01 | 0.01 | 0.01 | 11.84 | -4.17 |
| 300 | 0.01 | 0.01 | 0.01 | 0.01 | 4.11 | -4.17 |

Wind Load Analysis Table (Section 11.3.1) - From Leg C

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 300 | 0.63 | 0.63 | 0.63 | -3.39 | 18.11 | -0.29 |
| 330 | 0.00 | 0.66 | 0.63 | -11.73 | 7.15 | -0.34 |

Wind Load Analysis Table (Section 11.3.1) - From Leg B

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.03 | 0.03 | 0.03 | -15.33 | 3.73 | 0.20 |
| 30 | 0.00 | 0.06 | 0.03 | -11.73 | -7.15 | 0.24 |
| 60 | 0.03 | 0.03 | 0.03 | 3.39 | -18.11 | 0.26 |
| 90 | 0.03 | 0.03 | 0.03 | 4.17 | -20.96 | 0.17 |
| 120 | 0.03 | 0.03 | 0.03 | 11.64 | -20.96 | 0.00 |
| 150 | 0.03 | 0.03 | 0.03 | 16.07 | -14.00 | -0.17 |
| 180 | 0.03 | 0.03 | 0.03 | 15.31 | -4.20 | -0.29 |
| 210 | 0.00 | 0.06 | 0.03 | 12.64 | 6.39 | -0.34 |
| 240 | 0.03 | 0.03 | 0.03 | 4.17 | 13.82 | -0.29 |
| 270 | 0.03 | 0.03 | 0.03 | -3.39 | 20.40 | -0.17 |
| 300 | 0.03 | 0.03 | 0.03 | -11.33 | 19.83 | 0.00 |
| 330 | 0.03 | 0.03 | 0.03 | -19.21 | 13.83 | 0.17 |

Wind Load Analysis Table (Section 11.3.1) - From Leg A

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.10 | 0.00 | 0.00 | -10.10 | -33.31 | 0.00 |
| 30 | 0.03 | 0.03 | 0.03 | -20.33 | -4.11 | -0.11 |
| 60 | 0.03 | 0.03 | 0.03 | -11.82 | -11.00 | -0.29 |
| 90 | 0.00 | 0.06 | 0.03 | -3.39 | -13.71 | -0.34 |
| 120 | 0.03 | 0.03 | 0.03 | 11.73 | -11.00 | -0.29 |
| 150 | 0.03 | 0.03 | 0.03 | 19.29 | -4.87 | -0.11 |
| 180 | 0.03 | 0.00 | 0.00 | 32.67 | 0.00 | 0.00 |
| 210 | 0.03 | 0.03 | 0.03 | 19.29 | 6.87 | 0.17 |
| 240 | 0.03 | 0.03 | 0.03 | 11.11 | 11.99 | 0.26 |
| 270 | 0.00 | 0.06 | 0.03 | 3.39 | 13.74 | 0.34 |
| 300 | 0.03 | 0.03 | 0.03 | -11.82 | 11.99 | 0.26 |
| 330 | 0.03 | 0.03 | 0.03 | -20.33 | 6.87 | 0.17 |

Wind Load Analysis Table (Section 11.3.1) - From Leg C

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.03 | 0.03 | 0.03 | -0.07 | -15.99 | -3.73 |
| 30 | 0.01 | 0.03 | 0.06 | -0.07 | -15.74 | -4.17 |
| 60 | 0.10 | 0.00 | 0.03 | -0.25 | -11.33 | -4.20 |
| 90 | 0.03 | 0.03 | 0.03 | -0.01 | -3.83 | -4.17 |
| 120 | 0.03 | 0.03 | 0.03 | 0.03 | 4.70 | -4.17 |
| 150 | 0.03 | 0.03 | 0.03 | 0.03 | 16.31 | -4.20 |
| 180 | 0.03 | 0.03 | 0.03 | 0.03 | 32.00 | -4.17 |
| 210 | 0.03 | 0.03 | 0.03 | 0.03 | 16.31 | -4.20 |
| 240 | 0.03 | 0.03 | 0.03 | 0.03 | 14.00 | -4.17 |
| 270 | 0.03 | 0.03 | 0.03 | 0.03 | 11.84 | -4.17 |
| 300 | 0.03 | 0.03 | 0.03 | 0.03 | 4.11 | -4.17 |

Wind Load Analysis Table (Section 11.3.1) - From Leg B

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.03 | 0.03 | 0.03 | -0.07 | -15.99 | -3.73 |
| 30 | 0.01 | 0.03 | 0.06 | 0.03 | -15.74 | -4.17 |
| 60 | 0.03 | 0.03 | 0.03 | -0.01 | -11.33 | -4.20 |
| 90 | 0.03 | 0.03 | 0.03 | 0.03 | -3.83 | -4.17 |
| 120 | 0.10 | 0.00 | 0.03 | 0.03 | 4.70 | -4.17 |
| 150 | 0.03 | 0.03 | 0.03 | 0.03 | 16.31 | -4.20 |
| 180 | 0.03 | 0.03 | 0.03 | 0.03 | 32.00 | -4.17 |
| 210 | 0.03 | 0.03 | 0.03 | 0.03 | 16.31 | -4.20 |
| 240 | 0.03 | 0.03 | 0.03 | 0.03 | 14.00 | -4.17 |
| 270 | 0.03 | 0.03 | 0.03 | 0.03 | 11.84 | -4.17 |
| 300 | 0.03 | 0.03 | 0.03 | 0.03 | 4.11 | -4.17 |

Wind Load Analysis Table (Section 11.3.1) - From Leg A

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| K | K | K | K | hp-ft | hp-ft | hp-ft |
| 0 | 0.10 | 0.00 | 0.00 | -10.10 | -33.31 | 0.00 |
| 30 | 0.03 | 0.03 | 0.03 | -20.33 | -4.11 | -0.11 |
| 60 | 0.03 | 0.03 | 0.03 | -11.82 | -11.00 | -0.29 |
| 90 | 0.00 | 0.06 | 0.03 | -3.39 | -13.71 | -0.34 |
| 120 | 0.03 | 0.03 | 0.03 | 11.73 | -11.00 | -0.29 |
| 150 | 0.03 | 0.03 | 0.03 | 19.29 | -4.87 | -0.11 |
| 180 | 0.03 | 0.00 | 0.00 | 32.67 | 0.00 | 0.00 |
| 210 | 0.03 | 0.03 | 0.03 | 19.29 | 6.87 | 0.17 |
| 240 | 0.03 | 0.03 | 0.03 | 11.11 | 11.99 | 0.26 |
| 270 | 0.00 | 0.06 | 0.03 | 3.39 | 13.74 | 0.34 |
| 300 | 0.03 | 0.03 | 0.03 | -11.82 | 11.99 | 0.26 |
| 330 | 0.03 | 0.03 | 0.03 | -20.33 | 6.87 | 0.17 |

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Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 100-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

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Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 240-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

Table with 11 columns: Wind Attach #, Fx, Fy, Fz, ODMx, ODMy, ODMz, Torque. Rows 0-330.

| | | | | |
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| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
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|--|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Peko Dr. Plymouth, IN Phone: (317) 936-4331 FAX: (317) 936-6438 | Job | 284859 | Page | 46 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Wind Annex # | Pressure (1) - From Let C | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.61 | 0.69 | -0.03 | -0.09 | -0.09 | -17.01 | -4.44 | -4.51 |
| 35 | 0.63 | 0.63 | 0.03 | -0.07 | -0.07 | -13.43 | -3.77 | -3.81 |
| 60 | 0.66 | 0.66 | 0.00 | -0.03 | -0.03 | -10.20 | -3.10 | -3.14 |
| 90 | 0.68 | 0.68 | 0.01 | 0.01 | 0.01 | -7.31 | -2.26 | -2.30 |
| 120 | 0.68 | 0.68 | 0.01 | 0.01 | 0.01 | -5.20 | -1.61 | -1.65 |
| 150 | 0.68 | 0.68 | 0.01 | 0.01 | 0.01 | -3.50 | -1.12 | -1.16 |
| 180 | 0.68 | 0.68 | 0.01 | 0.01 | 0.01 | -2.50 | -0.80 | -0.84 |
| 210 | 0.68 | 0.68 | 0.01 | 0.01 | 0.01 | -1.80 | -0.48 | -0.52 |
| 240 | 0.68 | 0.68 | 0.01 | 0.01 | 0.01 | -1.30 | -0.34 | -0.38 |
| 270 | 0.68 | 0.68 | 0.01 | 0.01 | 0.01 | -1.00 | -0.26 | -0.28 |
| 300 | 0.68 | 0.68 | 0.01 | 0.01 | 0.01 | -0.80 | -0.21 | -0.23 |
| 330 | 0.68 | 0.68 | 0.01 | 0.01 | 0.01 | -0.70 | -0.19 | -0.21 |

| Wind Annex # | Pressure (1) - From Let C | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.31 | 0.60 | -0.01 | -0.11 | -0.11 | -10.34 | -2.61 | -2.65 |
| 35 | 0.27 | 0.60 | 0.01 | -0.08 | -0.08 | -7.80 | -2.00 | -2.04 |
| 60 | 0.31 | 0.60 | 0.01 | -0.05 | -0.05 | -5.70 | -1.47 | -1.51 |
| 90 | 0.31 | 0.60 | 0.01 | 0.01 | 0.01 | -4.10 | -1.06 | -1.10 |
| 120 | 0.31 | 0.60 | 0.01 | 0.01 | 0.01 | -2.90 | -0.74 | -0.78 |
| 150 | 0.31 | 0.60 | 0.01 | 0.01 | 0.01 | -2.10 | -0.54 | -0.58 |
| 180 | 0.31 | 0.60 | 0.01 | 0.01 | 0.01 | -1.50 | -0.39 | -0.43 |
| 210 | 0.31 | 0.60 | 0.01 | 0.01 | 0.01 | -1.10 | -0.28 | -0.32 |
| 240 | 0.31 | 0.60 | 0.01 | 0.01 | 0.01 | -0.80 | -0.21 | -0.23 |
| 270 | 0.31 | 0.60 | 0.01 | 0.01 | 0.01 | -0.60 | -0.16 | -0.18 |
| 300 | 0.31 | 0.60 | 0.01 | 0.01 | 0.01 | -0.50 | -0.13 | -0.15 |
| 330 | 0.31 | 0.60 | 0.01 | 0.01 | 0.01 | -0.40 | -0.10 | -0.12 |

| Wind Annex # | Pressure (2) - From Let B | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.60 | 0.16 | -0.03 | -0.32 | -0.32 | -12.33 | -3.11 | -3.15 |
| 35 | 0.60 | 0.16 | 0.00 | -0.24 | -0.24 | -9.10 | -2.31 | -2.35 |
| 60 | 0.60 | 0.16 | 0.00 | -0.18 | -0.18 | -6.60 | -1.67 | -1.71 |
| 90 | 0.60 | 0.16 | 0.00 | -0.12 | -0.12 | -4.70 | -1.21 | -1.25 |
| 120 | 0.60 | 0.16 | 0.00 | -0.09 | -0.09 | -3.40 | -0.87 | -0.91 |
| 150 | 0.60 | 0.16 | 0.00 | -0.07 | -0.07 | -2.50 | -0.64 | -0.68 |
| 180 | 0.60 | 0.16 | 0.00 | -0.05 | -0.05 | -1.80 | -0.46 | -0.50 |
| 210 | 0.60 | 0.16 | 0.00 | -0.04 | -0.04 | -1.30 | -0.34 | -0.38 |
| 240 | 0.60 | 0.16 | 0.00 | -0.03 | -0.03 | -1.00 | -0.26 | -0.28 |
| 270 | 0.60 | 0.16 | 0.00 | -0.02 | -0.02 | -0.70 | -0.19 | -0.21 |
| 300 | 0.60 | 0.16 | 0.00 | -0.01 | -0.01 | -0.50 | -0.13 | -0.15 |
| 330 | 0.60 | 0.16 | 0.00 | -0.01 | -0.01 | -0.40 | -0.10 | -0.12 |

| Wind Annex # | Pressure (2) - From Let B | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.31 | 0.16 | -0.03 | -0.32 | -0.32 | -10.34 | -2.61 | -2.65 |
| 35 | 0.27 | 0.16 | 0.00 | -0.24 | -0.24 | -7.80 | -2.00 | -2.04 |
| 60 | 0.31 | 0.16 | 0.00 | -0.18 | -0.18 | -5.70 | -1.47 | -1.51 |
| 90 | 0.31 | 0.16 | 0.00 | -0.12 | -0.12 | -4.10 | -1.06 | -1.10 |
| 120 | 0.31 | 0.16 | 0.00 | -0.09 | -0.09 | -2.90 | -0.74 | -0.78 |
| 150 | 0.31 | 0.16 | 0.00 | -0.07 | -0.07 | -2.10 | -0.54 | -0.58 |
| 180 | 0.31 | 0.16 | 0.00 | -0.05 | -0.05 | -1.50 | -0.39 | -0.43 |
| 210 | 0.31 | 0.16 | 0.00 | -0.04 | -0.04 | -1.10 | -0.28 | -0.32 |
| 240 | 0.31 | 0.16 | 0.00 | -0.03 | -0.03 | -0.80 | -0.21 | -0.23 |
| 270 | 0.31 | 0.16 | 0.00 | -0.02 | -0.02 | -0.60 | -0.16 | -0.18 |
| 300 | 0.31 | 0.16 | 0.00 | -0.01 | -0.01 | -0.50 | -0.13 | -0.15 |
| 330 | 0.31 | 0.16 | 0.00 | -0.01 | -0.01 | -0.40 | -0.10 | -0.12 |

| Wind Annex # | Pressure (3) - From Let A | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.00 | 0.00 | -0.05 | -11.23 | -11.23 | 0.00 | 0.00 | 0.00 |
| 35 | 0.01 | 0.01 | -0.01 | -8.81 | -8.81 | -0.11 | -0.11 | -0.11 |
| 60 | 0.01 | 0.01 | 0.01 | -6.60 | -6.60 | -0.17 | -0.17 | -0.17 |
| 90 | 0.01 | 0.01 | 0.01 | -4.70 | -4.70 | -0.24 | -0.24 | -0.24 |
| 120 | 0.01 | 0.01 | 0.01 | -3.40 | -3.40 | -0.31 | -0.31 | -0.31 |
| 150 | 0.01 | 0.01 | 0.01 | -2.50 | -2.50 | -0.38 | -0.38 | -0.38 |
| 180 | 0.01 | 0.01 | 0.01 | -1.80 | -1.80 | -0.46 | -0.46 | -0.46 |
| 210 | 0.01 | 0.01 | 0.01 | -1.30 | -1.30 | -0.54 | -0.54 | -0.54 |
| 240 | 0.01 | 0.01 | 0.01 | -1.00 | -1.00 | -0.62 | -0.62 | -0.62 |
| 270 | 0.01 | 0.01 | 0.01 | -0.70 | -0.70 | -0.70 | -0.70 | -0.70 |
| 300 | 0.01 | 0.01 | 0.01 | -0.50 | -0.50 | -0.78 | -0.78 | -0.78 |
| 330 | 0.01 | 0.01 | 0.01 | -0.40 | -0.40 | -0.86 | -0.86 | -0.86 |

| Wind Annex # | Pressure (3) - From Let A | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.31 | 0.00 | -0.00 | -0.31 | -0.31 | -12.33 | -3.11 | -3.15 |
| 35 | 0.27 | 0.00 | 0.00 | -0.27 | -0.27 | -9.10 | -2.31 | -2.35 |
| 60 | 0.31 | 0.00 | 0.00 | -0.24 | -0.24 | -6.60 | -1.67 | -1.71 |
| 90 | 0.31 | 0.00 | 0.00 | -0.18 | -0.18 | -4.70 | -1.21 | -1.25 |
| 120 | 0.31 | 0.00 | 0.00 | -0.12 | -0.12 | -3.40 | -0.87 | -0.91 |
| 150 | 0.31 | 0.00 | 0.00 | -0.09 | -0.09 | -2.50 | -0.64 | -0.68 |
| 180 | 0.31 | 0.00 | 0.00 | -0.07 | -0.07 | -1.80 | -0.46 | -0.50 |
| 210 | 0.31 | 0.00 | 0.00 | -0.05 | -0.05 | -1.30 | -0.34 | -0.38 |
| 240 | 0.31 | 0.00 | 0.00 | -0.04 | -0.04 | -1.00 | -0.26 | -0.28 |
| 270 | 0.31 | 0.00 | 0.00 | -0.03 | -0.03 | -0.70 | -0.19 | -0.21 |
| 300 | 0.31 | 0.00 | 0.00 | -0.02 | -0.02 | -0.50 | -0.13 | -0.15 |
| 330 | 0.31 | 0.00 | 0.00 | -0.01 | -0.01 | -0.40 | -0.10 | -0.12 |

| Wind Annex # | Pressure (4) - From Let C | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.13 | 0.11 | 0.03 | -0.27 | -0.27 | -12.33 | -3.11 | -3.15 |
| 35 | 0.27 | 0.09 | 0.14 | -0.21 | -0.21 | -9.10 | -2.31 | -2.35 |

| Wind Annex # | Pressure (4) - From Let C | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.00 | 0.04 | -0.03 | -0.04 | -0.04 | -7.79 | -2.00 | -2.04 |
| 35 | 0.00 | 0.03 | -0.01 | -0.03 | -0.03 | -5.70 | -1.47 | -1.51 |
| 60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -4.10 | -1.06 | -1.10 |
| 90 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | -2.90 | -0.74 | -0.78 |
| 120 | 0.00 | 0.04 | 0.03 | 0.04 | 0.04 | -2.10 | -0.54 | -0.58 |

| | | | | |
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|--|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Peko Dr. Plymouth, IN Phone: (317) 936-4331 FAX: (317) 936-6438 | Job | 284859 | Page | 48 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Wind Annex # | Pressure (1) - From Let C | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 150 | 0.60 | 0.03 | 0.03 | 0.04 | 0.04 | 3.93 | -1.97 | 0.31 |
| 180 | 0.60 | 0.04 | 0.03 | 0.04 | 0.04 | 2.76 | -1.38 | 0.17 |
| 210 | 0.60 | 0.03 | 0.01 | 0.01 | 0.01 | 4.31 | -2.16 | 0.36 |
| 240 | 0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 6.10 | -3.10 | 0.00 |
| 270 | 0.60 | 0.01 | -0.01 | -0.01 | -0.01 | -4.31 | 2.16 | -0.36 |
| 300 | 0.60 | 0.04 | -0.02 | -0.04 | -0.04 | -2.59 | 4.31 | -0.23 |
| 330 | 0.60 | 0.01 | -0.01 | -0.01 | -0.01 | -4.70 | 2.76 | -0.31 |

| Wind Annex # | Pressure (1) - From Let C | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 210 | 0.60 | 0.00 | 0.00 | -0.05 | -0.05 | 3.93 | -1.97 | 0.00 |
| 270 | 0.60 | 0.01 | 0.00 | -0.01 | -0.01 | 6.10 | -3.10 | -0.00 |
| 300 | 0.60 | 0.02 | -0.01 | -0.02 | -0.02 | 4.31 | 2.16 | -0.36 |
| 330 | 0.60 | 0.02 | -0.01 | -0.02 | -0.02 | -2.59 | 2.16 | -0.31 |

| Wind Annex # | Pressure (2) - From Let B | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.60 | 0.03 | 0.03 | -0.04 | -0.04 | -3.53 | -4.51 | 0.37 |
| 35 | 0.60 | 0.05 | 0.03 | -0.04 | -0.04 | -2.73 | -3.27 | 0.31 |
| 60 | 0.60 | 0.00 | 0.00 | -0.02 | -0.02 | -1.50 | -1.90 | 0.00 |
| 90 | 0.60 | 0.03 | 0.01 | -0.02 | -0.02 | -1.34 | -1.71 | 0.10 |
| 120 | 0.60 | 0.00 | 0.00 | 0.00 | 0.00 | -0.80 | -1.06 | 0.00 |
| 150 | 0.60 | 0.03 | -0.01 | 0.01 | 0.01 | 2.41 | -1.18 | -0.10 |
| 180 | 0.60 | 0.04 | -0.02 | 0.04 | 0.04 | 1.76 | -4.21 | -0.31 |
| 210 | 0.60 | 0.05 | -0.03 | 0.04 | 0.04 | 4.21 | -3.71 | -0.27 |
| 240 | 0.60 | 0.04 | -0.02 | 0.04 | 0.04 | 2.41 | -1.18 | -0.10 |
| 270 | 0.60 | 0.03 | -0.01 | 0.01 | 0.01 | 4.21 | -3.71 | -0.27 |
| 300 | 0.60 | 0.00 | 0.00 | 0.00 | 0.00 | -0.15 | 0.65 | 0.00 |
| 330 | 0.60 | 0.03 | 0.01 | -0.02 | -0.02 | -4.34 | -2.71 | 0.11 |

| Wind Annex # | Pressure (2) - From Let B | | | | | ODM _z hp-ft | ODM _z hp-ft | Torque hp-ft |
|--------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|---------------------------|-----------------|
| | F _x K | F _y K | F _x K | F _y K | F _z K | | | |
| 5 | 0.60 | 0.03 | 0.03 | -0.03 | -0.03 | -3.53 | -4.51 | 0.37 |
| 35 | 0.60 | 0.05 | 0.03 | -0.04 | -0.04 | -2.73 | -3.27 | 0.31 |
| 60 | 0.60 | 0.00 | 0.00 | 0.00 | 0.00 | -0.80 | -1.06 | 0.00 |
| 90 | 0.60 | 0.03 | 0.01 | -0.02 | -0.02 | -1.34 | -1.71 | 0.10 |
| 120 | 0.60 | 0.00 | 0.00 | 0.00 | | | | |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Palco Dr. Plymouth, NJ Phone: (770) 936-4231 FAX: (770) 936-4144 | Job | 284859 | Page | 49 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

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|---|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Palco Dr. Plymouth, NJ Phone: (770) 936-4231 FAX: (770) 936-4144 | Job | 284859 | Page | 50 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.00 | 0.01 | -0.00 | -1.43 | 0.01 | -0.01 |
| 30 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 60 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 90 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 120 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 150 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 180 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 210 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 240 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 270 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 300 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |
| 330 | 0.00 | 0.01 | -0.01 | -1.43 | 0.01 | -0.01 |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 30 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 60 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 90 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 120 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 150 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 180 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 210 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 240 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 270 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 300 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |
| 330 | 0.01 | 0.01 | -0.01 | -1.43 | 0.01 | 0.01 |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 30 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 60 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 90 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 120 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 150 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 180 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 210 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 240 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 270 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 300 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |
| 330 | 0.01 | 0.00 | -0.01 | -2.56 | 0.00 | 0.00 |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 30 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 60 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 90 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 120 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 150 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 180 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 210 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 240 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 270 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 300 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |
| 330 | 0.01 | 0.00 | -0.01 | -1.79 | -1.12 | -0.03 |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 30 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 60 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 90 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 120 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 150 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 180 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 210 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 240 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 270 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 300 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |
| 330 | 0.01 | 0.00 | -0.01 | -1.72 | 1.12 | 0.01 |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 30 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 60 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 90 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 120 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 150 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 180 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 210 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 240 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 270 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 300 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |
| 330 | 0.01 | 0.00 | -0.01 | -3.70 | 0.00 | 0.00 |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 30 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 60 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 90 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 120 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 150 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 180 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 210 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 240 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 270 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 300 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |
| 330 | 0.01 | 0.00 | -0.01 | -1.81 | -1.11 | -0.03 |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 30 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 60 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 90 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 120 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 150 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 180 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 210 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 240 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 270 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 300 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |
| 330 | 0.01 | 0.00 | -0.01 | -1.81 | 1.11 | 0.03 |

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|---|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Palco Dr. Plymouth, NJ Phone: (770) 936-4231 FAX: (770) 936-4144 | Job | 284859 | Page | 51 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

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|---|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Palco Dr. Plymouth, NJ Phone: (770) 936-4231 FAX: (770) 936-4144 | Job | 284859 | Page | 52 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.04 | -0.01 | -1.43 | -19.23 | 0.33 |
| 30 | 0.11 | 0.01 | 0.01 | 1.09 | -25.60 | 0.19 |
| 60 | 0.09 | 0.00 | 0.01 | 11.96 | -25.95 | 0.00 |
| 90 | 0.11 | 0.01 | 0.01 | 18.83 | -25.23 | -0.19 |
| 120 | 0.01 | 0.04 | -0.01 | 17.41 | -4.22 | -0.33 |
| 150 | 0.00 | 0.04 | -0.01 | 11.93 | 5.81 | -0.33 |
| 180 | 0.01 | 0.04 | -0.01 | 2.25 | 18.11 | -0.33 |
| 210 | 0.11 | 0.01 | 0.01 | -1.43 | 25.56 | -0.19 |
| 240 | 0.09 | 0.00 | 0.01 | -11.96 | 25.95 | 0.00 |
| 270 | 0.11 | 0.01 | 0.01 | -18.83 | 25.23 | 0.19 |
| 300 | 0.01 | 0.04 | -0.01 | -17.41 | 4.22 | 0.33 |
| 330 | 0.01 | 0.04 | -0.01 | -11.93 | -5.81 | 0.33 |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.00 | 0.01 | 0.04 | 0.00 | 14.37 | 0.47 |
| 30 | 0.11 | 0.07 | 0.01 | 0.11 | 24.20 | 0.41 |
| 60 | 0.20 | 0.04 | 0.01 | 0.16 | 27.79 | 0.24 |
| 90 | 0.21 | 0.01 | 0.00 | 0.20 | 24.16 | 0.00 |
| 120 | 0.20 | 0.01 | 0.00 | 0.00 | 14.30 | -0.24 |
| 150 | 0.17 | 0.07 | -0.01 | 0.01 | 0.81 | -0.41 |
| 180 | 0.00 | 0.01 | 0.04 | -0.01 | -12.60 | -0.47 |

| Wind Azimuth | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.11 | 0.00 | -0.01 | -3.11 | 0.00 | 0.20 |
| 30 | 0.11 | 0.01 | -0.01 | -3.11 | -0.27 | -0.19 |
| 60 | 0.09 | 0.00 | -0.01 | -15.56 | -11.09 | -0.33 |
| 90 | 0.00 | 0.00 | 0.00 | -4.00 | -11.70 | -0.30 |
| 120 | 0.01 | 0.00 | 0.01 | 14.65 | -11.83 | -0.33 |
| 150 | 0.11 | 0.01 | 0.01 | 25.83 | -6.37 | -0.19 |
| 180 | 0.11 | 0.00 | 0.00 | 29.90 | 0.00 | 0.00 |
| 210 | 0.11 | 0.01 | -0.01 | 0.11 | 25.83 | 6.37 |
| 240 | 0.09 | 0.00 | 0.01 | 14.65 | 11.83 | 0.33 |
| 270 | 0.01 | 0.00 | -0.01 | -15.56 | 11.09 | 0.33 |
| 300 | 0.01 | 0.00 | -0.01 | -15.56 | -11.09 | 0.33 |
| 330 | 0.11 | 0.01 | -0.01 | -3.11 | -0.27 | 0.19 |

| Wind Azimuth | F _x | F |
|--------------|----------------|---|
|--------------|----------------|---|

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|---|---------|---------------------------|-------------|-------------------|
| inxTower 1143 Pikes Dr. Plymouth, IN Phone: (317) 936-4311 Fax: (317) 936-6438 | Job | 284859 | Page | 81 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|------|------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.12 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.03 | 0.03 | 0.03 | -0.07 | -17.50 | -6.13 | -6.13 | 0.03 |
| 60 | 0.04 | 0.04 | 0.04 | 0.04 | -0.24 | -10.26 | -10.26 | -2.26 | 0.04 |
| 90 | 0.00 | 0.01 | 0.01 | 0.00 | -0.01 | -0.41 | -13.23 | -8.35 | 0.01 |
| 120 | 0.04 | 0.04 | 0.04 | 0.04 | -0.24 | -9.13 | -18.29 | -6.29 | 0.04 |
| 150 | 0.07 | 0.03 | 0.03 | 0.07 | -0.07 | -16.29 | -6.12 | -6.12 | 0.07 |
| 180 | 0.01 | 0.00 | 0.00 | 0.01 | -0.01 | -11.99 | 0.00 | 0.00 | 0.01 |
| 210 | 0.07 | 0.03 | 0.03 | 0.07 | -0.07 | -16.29 | 6.13 | 6.13 | 0.07 |
| 240 | 0.04 | 0.04 | 0.04 | 0.04 | -0.24 | -9.13 | 18.29 | 6.29 | 0.04 |
| 270 | 0.00 | 0.01 | 0.01 | 0.00 | -0.01 | -0.41 | 13.23 | 8.35 | 0.01 |
| 300 | 0.04 | 0.04 | 0.04 | 0.04 | -0.24 | -10.26 | 10.26 | 2.26 | 0.04 |
| 330 | 0.01 | 0.03 | 0.03 | 0.01 | -0.07 | -17.50 | 6.13 | 6.13 | 0.01 |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|------|------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.01 | 0.03 | 0.03 | 0.01 | -0.04 | -10.49 | -1.81 | -3.20 | 0.01 |
| 30 | 0.01 | 0.03 | 0.03 | 0.03 | -0.04 | -10.69 | -7.24 | 9.60 | 0.01 |
| 60 | 0.03 | 0.03 | 0.03 | 0.03 | -0.03 | -8.85 | -11.87 | 9.60 | 0.03 |
| 90 | 0.01 | 0.03 | 0.03 | 0.05 | -0.05 | -1.30 | -12.62 | 8.12 | 0.01 |
| 120 | 0.03 | 0.03 | 0.03 | 0.03 | -0.03 | -3.83 | -9.89 | 9.30 | 0.03 |
| 150 | 0.06 | 0.04 | 0.04 | 0.03 | -0.03 | -3.50 | -4.41 | 6.24 | 0.06 |
| 180 | 0.01 | 0.03 | 0.03 | 0.01 | -0.04 | -10.92 | 2.31 | 2.31 | 0.01 |
| 210 | 0.03 | 0.03 | 0.03 | 0.03 | -0.03 | -10.48 | 8.34 | 8.34 | 0.03 |
| 240 | 0.06 | 0.04 | 0.04 | 0.03 | -0.03 | -2.21 | 12.61 | 0.00 | 0.06 |
| 270 | 0.01 | 0.03 | 0.03 | 0.01 | -0.04 | -2.19 | 13.36 | -1.02 | 0.01 |
| 300 | 0.03 | 0.03 | 0.03 | 0.03 | -0.03 | -3.42 | 10.83 | -0.20 | 0.03 |
| 330 | 0.01 | 0.03 | 0.03 | 0.01 | -0.04 | -10.92 | 5.16 | -5.16 | 0.01 |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|------|------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -10.30 | 1.81 | 0.20 | 0.01 |
| 30 | 0.01 | 0.01 | 0.01 | 0.02 | -0.02 | -3.42 | -5.16 | 8.24 | 0.01 |
| 60 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -10.92 | -10.92 | 2.20 | 0.01 |
| 90 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 2.19 | -13.36 | 0.12 | 0.01 |
| 120 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 7.24 | -12.61 | 0.00 | 0.01 |
| 150 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 10.48 | -8.34 | -0.12 | 0.01 |
| 180 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 10.92 | -2.31 | -0.20 | 0.01 |
| 210 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 1.50 | -4.41 | -0.24 | 0.01 |
| 240 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 3.83 | -9.89 | 0.00 | 0.01 |
| 270 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -1.75 | 12.61 | -0.12 | 0.01 |
| 300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -8.85 | 11.87 | 0.00 | 0.01 |
| 330 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -10.92 | 7.24 | 0.12 | 0.01 |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|------|------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.17 | 0.14 | 0.21 | 0.21 | -0.21 | -50.83 | -13.37 | -6.91 | 0.17 |
| 30 | 0.29 | 0.09 | 0.11 | 0.21 | -0.21 | -51.74 | -46.81 | -0.33 | 0.29 |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1143 Pikes Dr. Plymouth, IN Phone: (317) 936-4311 Fax: (317) 936-6438 | Job | 284859 | Page | 63 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|-------|-------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 150 | 0.00 | 0.18 | 0.03 | 0.14 | 0.14 | 31.55 | -17.45 | 0.14 | 0.00 |
| 180 | 0.03 | 0.14 | 0.00 | 0.14 | 0.14 | 36.31 | 0.14 | 0.14 | 0.03 |
| 210 | 0.14 | 0.03 | -0.03 | 0.14 | 0.14 | 31.55 | 18.44 | 0.14 | 0.14 |
| 240 | 0.14 | 0.03 | -0.14 | 0.03 | 0.14 | 18.29 | 31.66 | 0.00 | 0.14 |
| 270 | 0.14 | 0.03 | -0.14 | -0.03 | 0.00 | 8.24 | 36.55 | -0.39 | 0.14 |
| 300 | 0.03 | 0.14 | -0.14 | -0.03 | -0.01 | -17.81 | 31.66 | -0.47 | 0.03 |
| 330 | 0.00 | 0.18 | -0.03 | -0.14 | -0.14 | -31.05 | 18.44 | -0.71 | 0.00 |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|-------|-------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.01 | 0.01 | -0.01 | -0.01 | -0.01 | -11.11 | 5.73 | -2.31 | 0.01 |
| 30 | 0.01 | 0.01 | -0.01 | -0.01 | -0.01 | -10.31 | 0.51 | -1.19 | 0.01 |
| 60 | 0.01 | 0.00 | 0.01 | -0.01 | -0.01 | -2.78 | -1.79 | 0.00 | 0.01 |
| 90 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 5.63 | -4.74 | 0.00 | 0.01 |
| 120 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 12.55 | -10.29 | 0.00 | 0.01 |
| 150 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 15.14 | -6.02 | 0.01 | 0.01 |
| 180 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 10.64 | -6.06 | 0.01 | 0.01 |
| 210 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 15.44 | -2.28 | 0.01 | 0.01 |
| 240 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 3.01 | 3.21 | 0.00 | 0.01 |
| 270 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -3.31 | 9.19 | 0.16 | 0.01 |
| 300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -12.29 | 10.74 | -2.21 | 0.01 |
| 330 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -15.81 | 9.71 | -0.31 | 0.01 |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|------|------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.01 | 0.14 | 0.00 | 0.14 | -0.14 | -33.29 | 0.33 | -0.67 | 0.01 |
| 30 | 0.14 | 0.01 | 0.01 | 0.14 | -0.14 | -35.31 | -37.31 | -0.35 | 0.14 |
| 60 | 0.14 | 0.01 | 0.01 | 0.01 | -0.01 | -17.54 | -35.37 | 0.00 | 0.14 |
| 90 | 0.14 | 0.01 | 0.01 | 0.00 | 0.00 | 0.22 | -35.13 | 0.35 | 0.14 |
| 120 | 0.01 | 0.14 | 0.14 | 0.01 | 0.01 | 37.97 | -35.37 | 0.61 | 0.01 |
| 150 | 0.00 | 0.14 | 0.14 | 0.01 | 0.01 | 32.97 | -17.31 | 0.31 | 0.00 |
| 180 | 0.01 | 0.14 | 0.00 | 0.14 | 0.14 | 15.13 | 0.31 | 0.01 | 0.01 |
| 210 | 0.01 | 0.14 | 0.01 | 0.14 | 0.14 | 30.97 | 18.13 | 0.00 | 0.01 |
| 240 | 0.01 | 0.14 | 0.01 | 0.14 | 0.01 | 17.97 | 31.13 | 0.33 | 0.01 |
| 270 | 0.01 | 0.14 | 0.01 | 0.14 | 0.01 | 8.22 | 31.89 | -0.93 | 0.01 |
| 300 | 0.01 | 0.14 | 0.01 | 0.14 | -0.01 | -17.54 | 31.13 | -0.67 | 0.01 |
| 330 | 0.01 | 0.14 | 0.01 | 0.14 | -0.01 | -33.29 | 18.13 | -0.77 | 0.01 |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|-------|-------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.01 | 0.01 | -0.01 | -0.01 | -0.01 | -10.92 | 3.83 | -0.21 | 0.01 |
| 30 | 0.02 | 0.01 | -0.01 | -0.01 | -0.01 | -10.29 | 0.50 | -1.19 | 0.02 |
| 60 | 0.02 | 0.01 | 0.01 | -0.01 | -0.01 | -2.71 | -1.70 | 0.00 | 0.02 |
| 90 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 | 3.54 | -4.81 | 0.00 | 0.02 |
| 120 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 | 12.33 | -10.19 | 0.00 | 0.02 |
| 150 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 | 13.81 | -4.66 | 0.01 | 0.02 |
| 180 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 | 15.11 | -1.11 | 0.01 | 0.02 |
| 210 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 | 16.87 | 0.60 | 0.01 | 0.02 |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1143 Pikes Dr. Plymouth, IN Phone: (317) 936-4311 Fax: (317) 936-6438 | Job | 284859 | Page | 62 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|------|------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.34 | 0.00 | 0.00 | 0.30 | -0.17 | -31.59 | -66.81 | 0.00 | 0.34 |
| 30 | 0.29 | 0.09 | 0.11 | 0.30 | -0.27 | -14.69 | -41.23 | -6.03 | 0.29 |
| 60 | 0.17 | 0.11 | 0.11 | 0.29 | -0.29 | -12.56 | -35.67 | -0.01 | 0.17 |
| 90 | 0.00 | 0.34 | 0.29 | 0.11 | 0.11 | 31.59 | -18.71 | 1.89 | 0.00 |
| 120 | 0.17 | 0.11 | 0.11 | 0.17 | 0.17 | 33.61 | 18.81 | 0.01 | 0.17 |
| 150 | 0.29 | 0.09 | 0.09 | 0.17 | 0.17 | 34.81 | 32.19 | 0.59 | 0.29 |
| 180 | 0.34 | 0.00 | 0.00 | 0.34 | 0.34 | 41.66 | 72.11 | 0.26 | 0.34 |
| 210 | 0.29 | 0.09 | 0.09 | 0.29 | 0.29 | 17.75 | 72.31 | -0.51 | 0.29 |
| 240 | 0.17 | 0.11 | 0.11 | 0.29 | -0.29 | -10.49 | 35.93 | -0.81 | 0.17 |
| 270 | 0.00 | 0.34 | 0.29 | 0.11 | -0.11 | -31.59 | 74.63 | -1.81 | 0.00 |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|------|-------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.33 | 0.14 | 0.09 | -0.07 | -0.23 | -53.81 | 13.31 | 0.01 | 0.33 |
| 30 | 0.00 | 0.11 | 0.09 | -0.16 | -0.16 | -33.31 | -24.01 | -1.61 | 0.00 |
| 60 | 0.11 | 0.09 | 0.09 | -0.09 | -0.09 | -19.40 | -39.89 | -0.81 | 0.11 |
| 90 | 0.29 | 0.09 | 0.09 | 0.30 | 0.17 | 41.61 | -72.11 | 0.00 | 0.29 |
| 120 | 0.11 | 0.09 | 0.09 | 0.17 | 0.17 | 34.81 | -12.35 | -0.51 | 0.11 |
| 150 | 0.11 | 0.09 | 0.09 | 0.11 | 0.11 | 31.61 | -18.81 | -0.81 | 0.11 |
| 180 | 0.11 | 0.09 | 0.09 | 0.11 | 0.11 | 31.59 | 18.74 | -0.01 | 0.11 |
| 210 | 0.11 | 0.09 | 0.09 | 0.11 | 0.11 | 31.56 | 53.82 | -0.91 | 0.11 |
| 240 | 0.11 | 0.09 | 0.09 | 0.11 | 0.11 | -14.69 | 61.23 | -0.51 | 0.11 |
| 270 | 0.11 | 0.09 | 0.09 | 0.11 | 0.11 | -31.59 | 66.11 | 0.00 | 0.11 |
| 300 | 0.11 | 0.09 | 0.09 | 0.11 | 0.11 | -31.74 | 48.84 | 0.31 | 0.11 |

| Wind Azimuth | Fx | | Fy | | Fz | | ODG _x | ODG _y | Torque |
|--------------|------|------|------|------|-------|--------|------------------|------------------|--------|
| | K | E | K | E | K | E | | | |
| 0 | 0.34 | 0.00 | 0.00 | 0.34 | -0.17 | -41.33 | 0.00 | 0.00 | 0.34 |
| 30 | 0.29 | 0.09 | 0.09 | 0.29 | -0.29 | -17.97 | -41.23 | -6.03 | 0.29 |
| 60 | 0.17 | 0.11 | 0.11 | | | | | | |

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|---|---------------------------|-------------------|
| inxTower 1543 Palko Dr. Plainville, CT Phone: (878) 938-6321 Fax: (878) 938-6458 | Job 284859 | Page 65 of 107 |
| Project V-25 x 240' - Ashford, CT | Date 15:15:37 03/30/15 | |
| Client Verizon Wireless | Designed by JAK | |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.02 | 0.06 | 0.11 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.03 | 0.12 | 0.17 | 0.04 | -0.04 | -4.02 | 34.20 |
| 90 | 0.04 | 0.17 | 0.22 | 0.05 | 0.05 | 9.84 | -44.28 |
| 120 | 0.05 | 0.22 | 0.28 | 0.12 | 0.12 | 23.24 | -43.71 |
| 150 | 0.07 | 0.27 | 0.33 | 0.19 | 0.19 | 34.01 | -31.01 |
| 180 | 0.11 | 0.33 | 0.41 | 0.28 | 0.28 | 53.88 | -10.30 |
| 210 | 0.14 | 0.41 | 0.50 | 0.41 | 0.41 | 74.71 | 12.90 |
| 240 | 0.17 | 0.50 | 0.60 | 0.59 | 0.59 | 97.56 | 22.51 |
| 270 | 0.21 | 0.60 | 0.71 | 0.84 | 0.84 | 122.43 | 28.81 |
| 300 | 0.25 | 0.71 | 0.84 | 1.17 | 1.17 | 149.34 | 31.81 |
| 330 | 0.29 | 0.84 | 1.00 | 1.61 | 1.61 | 178.29 | 35.01 |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.02 | 0.06 | 0.11 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.03 | 0.12 | 0.17 | 0.04 | -0.04 | -4.02 | 34.20 |
| 90 | 0.04 | 0.17 | 0.22 | 0.05 | 0.05 | 9.84 | -44.28 |
| 120 | 0.05 | 0.22 | 0.28 | 0.12 | 0.12 | 23.24 | -43.71 |
| 150 | 0.07 | 0.27 | 0.33 | 0.19 | 0.19 | 34.01 | -31.01 |
| 180 | 0.11 | 0.33 | 0.41 | 0.28 | 0.28 | 53.88 | -10.30 |
| 210 | 0.14 | 0.41 | 0.50 | 0.41 | 0.41 | 74.71 | 12.90 |
| 240 | 0.17 | 0.50 | 0.60 | 0.59 | 0.59 | 97.56 | 22.51 |
| 270 | 0.21 | 0.60 | 0.71 | 0.84 | 0.84 | 122.43 | 28.81 |
| 300 | 0.25 | 0.71 | 0.84 | 1.17 | 1.17 | 149.34 | 31.81 |
| 330 | 0.29 | 0.84 | 1.00 | 1.61 | 1.61 | 178.29 | 35.01 |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.02 | 0.06 | 0.11 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.03 | 0.12 | 0.17 | 0.04 | -0.04 | -4.02 | 34.20 |
| 90 | 0.04 | 0.17 | 0.22 | 0.05 | 0.05 | 9.84 | -44.28 |
| 120 | 0.05 | 0.22 | 0.28 | 0.12 | 0.12 | 23.24 | -43.71 |
| 150 | 0.07 | 0.27 | 0.33 | 0.19 | 0.19 | 34.01 | -31.01 |
| 180 | 0.11 | 0.33 | 0.41 | 0.28 | 0.28 | 53.88 | -10.30 |
| 210 | 0.14 | 0.41 | 0.50 | 0.41 | 0.41 | 74.71 | 12.90 |
| 240 | 0.17 | 0.50 | 0.60 | 0.59 | 0.59 | 97.56 | 22.51 |
| 270 | 0.21 | 0.60 | 0.71 | 0.84 | 0.84 | 122.43 | 28.81 |
| 300 | 0.25 | 0.71 | 0.84 | 1.17 | 1.17 | 149.34 | 31.81 |
| 330 | 0.29 | 0.84 | 1.00 | 1.61 | 1.61 | 178.29 | 35.01 |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.02 | 0.06 | 0.11 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.03 | 0.12 | 0.17 | 0.04 | -0.04 | -4.02 | 34.20 |
| 90 | 0.04 | 0.17 | 0.22 | 0.05 | 0.05 | 9.84 | -44.28 |
| 120 | 0.05 | 0.22 | 0.28 | 0.12 | 0.12 | 23.24 | -43.71 |
| 150 | 0.07 | 0.27 | 0.33 | 0.19 | 0.19 | 34.01 | -31.01 |
| 180 | 0.11 | 0.33 | 0.41 | 0.28 | 0.28 | 53.88 | -10.30 |
| 210 | 0.14 | 0.41 | 0.50 | 0.41 | 0.41 | 74.71 | 12.90 |
| 240 | 0.17 | 0.50 | 0.60 | 0.59 | 0.59 | 97.56 | 22.51 |
| 270 | 0.21 | 0.60 | 0.71 | 0.84 | 0.84 | 122.43 | 28.81 |
| 300 | 0.25 | 0.71 | 0.84 | 1.17 | 1.17 | 149.34 | 31.81 |
| 330 | 0.29 | 0.84 | 1.00 | 1.61 | 1.61 | 178.29 | 35.01 |

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|---|---------------------------|-------------------|
| inxTower 1543 Palko Dr. Plainville, CT Phone: (878) 938-6321 Fax: (878) 938-6458 | Job 284859 | Page 66 of 107 |
| Project V-25 x 240' - Ashford, CT | Date 15:15:37 03/30/15 | |
| Client Verizon Wireless | Designed by JAK | |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.04 | 0.13 | 0.22 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.07 | 0.22 | 0.33 | 0.12 | 0.17 | -12.85 | 34.20 |
| 90 | 0.11 | 0.33 | 0.44 | 0.19 | 0.25 | -22.92 | 34.20 |
| 120 | 0.16 | 0.44 | 0.56 | 0.28 | 0.36 | -12.85 | 34.20 |
| 150 | 0.22 | 0.56 | 0.69 | 0.41 | 0.50 | 12.90 | 34.20 |
| 180 | 0.29 | 0.69 | 0.84 | 0.59 | 0.69 | 22.51 | 34.20 |
| 210 | 0.36 | 0.84 | 1.00 | 0.84 | 0.84 | 28.81 | 34.20 |
| 240 | 0.44 | 1.00 | 1.17 | 1.17 | 1.17 | 31.81 | 34.20 |
| 270 | 0.52 | 1.17 | 1.35 | 1.50 | 1.50 | 35.01 | 34.20 |
| 300 | 0.60 | 1.35 | 1.54 | 1.83 | 1.83 | 38.21 | 34.20 |
| 330 | 0.69 | 1.54 | 1.73 | 2.16 | 2.16 | 41.41 | 34.20 |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.04 | 0.13 | 0.22 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.07 | 0.22 | 0.33 | 0.12 | 0.17 | -12.85 | 34.20 |
| 90 | 0.11 | 0.33 | 0.44 | 0.19 | 0.25 | -22.92 | 34.20 |
| 120 | 0.16 | 0.44 | 0.56 | 0.28 | 0.36 | -12.85 | 34.20 |
| 150 | 0.22 | 0.56 | 0.69 | 0.41 | 0.50 | 12.90 | 34.20 |
| 180 | 0.29 | 0.69 | 0.84 | 0.59 | 0.69 | 22.51 | 34.20 |
| 210 | 0.36 | 0.84 | 1.00 | 0.84 | 0.84 | 28.81 | 34.20 |
| 240 | 0.44 | 1.00 | 1.17 | 1.17 | 1.17 | 31.81 | 34.20 |
| 270 | 0.52 | 1.17 | 1.35 | 1.50 | 1.50 | 35.01 | 34.20 |
| 300 | 0.60 | 1.35 | 1.54 | 1.83 | 1.83 | 38.21 | 34.20 |
| 330 | 0.69 | 1.54 | 1.73 | 2.16 | 2.16 | 41.41 | 34.20 |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.04 | 0.13 | 0.22 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.07 | 0.22 | 0.33 | 0.12 | 0.17 | -12.85 | 34.20 |
| 90 | 0.11 | 0.33 | 0.44 | 0.19 | 0.25 | -22.92 | 34.20 |
| 120 | 0.16 | 0.44 | 0.56 | 0.28 | 0.36 | -12.85 | 34.20 |
| 150 | 0.22 | 0.56 | 0.69 | 0.41 | 0.50 | 12.90 | 34.20 |
| 180 | 0.29 | 0.69 | 0.84 | 0.59 | 0.69 | 22.51 | 34.20 |
| 210 | 0.36 | 0.84 | 1.00 | 0.84 | 0.84 | 28.81 | 34.20 |
| 240 | 0.44 | 1.00 | 1.17 | 1.17 | 1.17 | 31.81 | 34.20 |
| 270 | 0.52 | 1.17 | 1.35 | 1.50 | 1.50 | 35.01 | 34.20 |
| 300 | 0.60 | 1.35 | 1.54 | 1.83 | 1.83 | 38.21 | 34.20 |
| 330 | 0.69 | 1.54 | 1.73 | 2.16 | 2.16 | 41.41 | 34.20 |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.04 | 0.13 | 0.22 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.07 | 0.22 | 0.33 | 0.12 | 0.17 | -12.85 | 34.20 |
| 90 | 0.11 | 0.33 | 0.44 | 0.19 | 0.25 | -22.92 | 34.20 |
| 120 | 0.16 | 0.44 | 0.56 | 0.28 | 0.36 | -12.85 | 34.20 |
| 150 | 0.22 | 0.56 | 0.69 | 0.41 | 0.50 | 12.90 | 34.20 |
| 180 | 0.29 | 0.69 | 0.84 | 0.59 | 0.69 | 22.51 | 34.20 |
| 210 | 0.36 | 0.84 | 1.00 | 0.84 | 0.84 | 28.81 | 34.20 |
| 240 | 0.44 | 1.00 | 1.17 | 1.17 | 1.17 | 31.81 | 34.20 |
| 270 | 0.52 | 1.17 | 1.35 | 1.50 | 1.50 | 35.01 | 34.20 |
| 300 | 0.60 | 1.35 | 1.54 | 1.83 | 1.83 | 38.21 | 34.20 |
| 330 | 0.69 | 1.54 | 1.73 | 2.16 | 2.16 | 41.41 | 34.20 |

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|---|---------------------------|-------------------|
| inxTower 1543 Palko Dr. Plainville, CT Phone: (878) 938-6321 Fax: (878) 938-6458 | Job 284859 | Page 67 of 107 |
| Project V-25 x 240' - Ashford, CT | Date 15:15:37 03/30/15 | |
| Client Verizon Wireless | Designed by JAK | |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.04 | 0.13 | 0.22 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.07 | 0.22 | 0.33 | 0.12 | 0.17 | -12.85 | 34.20 |
| 90 | 0.11 | 0.33 | 0.44 | 0.19 | 0.25 | -22.92 | 34.20 |
| 120 | 0.16 | 0.44 | 0.56 | 0.28 | 0.36 | -12.85 | 34.20 |
| 150 | 0.22 | 0.56 | 0.69 | 0.41 | 0.50 | 12.90 | 34.20 |
| 180 | 0.29 | 0.69 | 0.84 | 0.59 | 0.69 | 22.51 | 34.20 |
| 210 | 0.36 | 0.84 | 1.00 | 0.84 | 0.84 | 28.81 | 34.20 |
| 240 | 0.44 | 1.00 | 1.17 | 1.17 | 1.17 | 31.81 | 34.20 |
| 270 | 0.52 | 1.17 | 1.35 | 1.50 | 1.50 | 35.01 | 34.20 |
| 300 | 0.60 | 1.35 | 1.54 | 1.83 | 1.83 | 38.21 | 34.20 |
| 330 | 0.69 | 1.54 | 1.73 | 2.16 | 2.16 | 41.41 | 34.20 |

| Wind Azimuth * | F _x | F _y | F _z | OTM _x | OTM _y | OTM _z | Torque |
|----------------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30 | 0.04 | 0.13 | 0.22 | 0.07 | 0.12 | -33.64 | 18.0 |
| 60 | 0.07 | 0.22 | 0.33 | 0.12 | 0.17 | -12.85 | 34.20 |
| 90 | 0.11 | 0.33 | 0.44 | 0.19 | 0.25 | -22.92 | 34.20 |
| 120 | 0.16 | 0.44 | 0.56 | 0.28 | 0.36 | -12.85 | 34.20 |
| 150 | 0.22 | 0.56 | 0.69 | 0.41 | 0.50 | 12.90 | 34.20 |
| 180 | 0.29 | 0.69 | 0.84 | 0.59 | 0.69 | 22.51 | 34.20 |
| 210 | 0.36 | 0.84 | 1.00 | 0.84 | 0.84 | 28.81 | 34.20 |
| 240 | 0.44 | 1.00 | 1.17 | 1.17 | 1.17 | 31.81 | 34.20 |
| 270 | 0.52 | 1.17 | 1.35 | 1.50 | 1.50 | 35.01 | 34.20 |
| 300 | 0.60 | | | | | | |

| Wind Speed | F _x | F _y | F _z | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|------------|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| ft/s | K | K | K | K | K | K | ft-lb | ft-lb | ft-lb |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -0.73 | 6.13 | -0.11 |
| 60 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | -1.46 | 12.26 | -0.22 |
| 90 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | -2.19 | 18.39 | -0.33 |
| 120 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | -2.92 | 24.52 | -0.44 |
| 150 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | -3.65 | 30.65 | -0.55 |
| 180 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | -4.38 | 36.78 | -0.66 |
| 210 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | -5.11 | 42.91 | -0.77 |
| 240 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | -5.84 | 49.04 | -0.88 |
| 270 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | -6.57 | 55.17 | -0.99 |
| 300 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | -7.30 | 61.30 | -1.10 |
| 330 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | -8.03 | 67.43 | -1.21 |

| Wind Speed | F _x | F _y | F _z | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|------------|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| ft/s | K | K | K | K | K | K | ft-lb | ft-lb | ft-lb |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -0.73 | 6.13 | -0.11 |
| 60 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | -1.46 | 12.26 | -0.22 |
| 90 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | -2.19 | 18.39 | -0.33 |
| 120 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | -2.92 | 24.52 | -0.44 |
| 150 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | -3.65 | 30.65 | -0.55 |
| 180 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | -4.38 | 36.78 | -0.66 |
| 210 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | -5.11 | 42.91 | -0.77 |
| 240 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | -5.84 | 49.04 | -0.88 |
| 270 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | -6.57 | 55.17 | -0.99 |
| 300 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | -7.30 | 61.30 | -1.10 |
| 330 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | -8.03 | 67.43 | -1.21 |

| Wind Speed | F _x | F _y | F _z | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|------------|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| ft/s | K | K | K | K | K | K | ft-lb | ft-lb | ft-lb |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -11.13 | 0.00 | 0.00 |
| 60 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | -22.26 | -2.13 | -0.66 |
| 90 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | -33.39 | -4.26 | -1.32 |
| 120 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | -44.52 | -6.39 | -1.98 |
| 150 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | -55.65 | -8.52 | -2.64 |
| 180 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | -66.78 | -10.65 | -3.30 |
| 210 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | -77.91 | -12.78 | -3.96 |
| 240 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | -89.04 | -14.91 | -4.62 |
| 270 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | -100.17 | -17.04 | -5.28 |
| 300 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | -111.30 | -19.17 | -5.94 |
| 330 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | -122.43 | -21.30 | -6.60 |

| Wind Speed | F _x | F _y | F _z | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|------------|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| ft/s | K | K | K | K | K | K | ft-lb | ft-lb | ft-lb |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -0.01 | -0.01 |
| 60 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | -0.02 | -0.02 | -0.02 |
| 90 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | -0.03 | -0.03 | -0.03 |
| 120 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | -0.04 | -0.04 | -0.04 |
| 150 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | -0.05 | -0.05 | -0.05 |
| 180 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | -0.06 | -0.06 | -0.06 |
| 210 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | -0.07 | -0.07 | -0.07 |
| 240 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | -0.08 | -0.08 | -0.08 |
| 270 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | -0.09 | -0.09 | -0.09 |
| 300 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | -0.10 | -0.10 | -0.10 |
| 330 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | -0.11 | -0.11 | -0.11 |

| Wind Speed | F _x | F _y | F _z | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|------------|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| ft/s | K | K | K | K | K | K | ft-lb | ft-lb | ft-lb |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -2.27 | -4.19 | -0.64 |
| 60 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | -4.54 | -8.38 | -1.28 |
| 90 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | -6.81 | -12.57 | -1.92 |
| 120 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | -9.08 | -16.76 | -2.56 |
| 150 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | -11.35 | -20.95 | -3.20 |
| 180 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | -13.62 | -25.14 | -3.84 |
| 210 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | -15.89 | -29.33 | -4.48 |
| 240 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | -18.16 | -33.52 | -5.12 |
| 270 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | -20.43 | -37.71 | -5.76 |
| 300 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | -22.70 | -41.90 | -6.40 |
| 330 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | -24.97 | -46.09 | -7.04 |

| Wind Speed | F _x | F _y | F _z | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|------------|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| ft/s | K | K | K | K | K | K | ft-lb | ft-lb | ft-lb |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -0.01 | -0.01 |
| 60 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | -0.02 | -0.02 | -0.02 |
| 90 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | -0.03 | -0.03 | -0.03 |
| 120 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | -0.04 | -0.04 | -0.04 |
| 150 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | -0.05 | -0.05 | -0.05 |
| 180 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | -0.06 | -0.06 | -0.06 |
| 210 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | -0.07 | -0.07 | -0.07 |
| 240 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | -0.08 | -0.08 | -0.08 |
| 270 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | -0.09 | -0.09 | -0.09 |
| 300 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | -0.10 | -0.10 | -0.10 |
| 330 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | -0.11 | -0.11 | -0.11 |

| Wind Speed | F _x | F _y | F _z | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|------------|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| ft/s | K | K | K | K | K | K | ft-lb | ft-lb | ft-lb |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -2.27 | -4.19 | -0.64 |
| 60 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | -4.54 | -8.38 | -1.28 |
| 90 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | -6.81 | -12.57 | -1.92 |
| 120 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | -9.08 | -16.76 | -2.56 |
| 150 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | -11.35 | -20.95 | -3.20 |
| 180 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | -13.62 | -25.14 | -3.84 |
| 210 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | -15.89 | -29.33 | -4.48 |
| 240 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | -18.16 | -33.52 | -5.12 |
| 270 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | -20.43 | -37.71 | -5.76 |
| 300 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | -22.70 | -41.90 | -6.40 |
| 330 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | -24.97 | -46.09 | -7.04 |

| Wind Speed | F _x | F _y | F _z | F _x | F _y | F _z | OTM _x | OTM _y | Torque |
|------------|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| ft/s | K | K | K | K | K | K | ft-lb | ft-lb | ft-lb |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -2.10 | 0.97 | 0.04 |
| 60 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | -4.20 | 1.94 | 0.08 |
| 90 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 | -6.30 | 2.91 | 0.12 |
| 120 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 | -8.40 | 3.88 | 0.16 |
| 150 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | -10.50 | 4.85 | 0.20 |
| 180 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | -12.60 | 5.82 | 0.24 |
| 210 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | -14.70 | 6.79 | 0.28 |
| 240 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | -16.80 | 7.76 | 0.32 |
| 270 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | -18.90 | 8.73 | 0.36 |
| 300 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | -21.00 | 9.70 | 0.40 |
| 330 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | -23.10 | 10.67 | 0.44 |

| Wind Speed | F _x | F _y | F _z | F _x | F _y |
|------------|----------------|----------------|----------------|----------------|----------------|
|------------|----------------|----------------|----------------|----------------|----------------|

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 1343 Pico Dr. Plymouth, IN Phone: (317) 836-4311 FAX: (317) 936-6438 | Job | 284859 | Page | 73 of 107 |
| | Project | V-26 x 240' - Ashford, CT | Date | 18:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Wind Azimuth | 12" V Frame - Erection 111 - From Leg 4 | | | | | | ODM ₄ | ODM ₆ | Torque |
|--------------|---|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| | F _x | F _y | F _z | F ₄ | F ₅ | F ₆ | | | |
| 0 | 0.21 | 0.00 | 0.00 | 0.21 | 0.00 | 0.00 | 41.43 | -11.43 | -0.31 |
| 30 | 0.11 | 0.19 | 0.00 | 0.11 | 0.19 | 0.00 | 32.24 | -11.46 | -0.11 |
| 60 | 0.00 | 0.39 | 0.00 | 0.00 | 0.39 | 0.00 | 20.69 | 14.11 | -0.00 |
| 90 | 0.00 | 0.00 | 0.42 | 0.00 | 0.00 | 0.42 | 11.02 | 19.11 | -0.11 |
| 120 | 0.11 | 0.19 | 0.00 | -0.11 | -0.19 | 0.00 | -11.19 | 19.02 | -0.11 |
| 150 | 0.21 | 0.00 | 0.00 | -0.21 | 0.00 | 0.00 | -32.24 | 14.11 | 0.00 |
| 180 | 0.21 | 0.00 | 0.00 | -0.21 | 0.00 | 0.00 | -41.43 | -11.43 | 0.31 |

| Wind Azimuth | 12" V Frame - Erection 111 - From Leg 4 | | | | | | ODM ₄ | ODM ₆ | Torque |
|--------------|---|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| | F _x | F _y | F _z | F ₄ | F ₅ | F ₆ | | | |
| 0 | 0.32 | 0.00 | 0.00 | 0.32 | 0.00 | 0.00 | 56.21 | 0.00 | 0.00 |
| 30 | 0.21 | 0.19 | 0.00 | 0.21 | 0.19 | 0.00 | 37.74 | -11.81 | -0.11 |
| 60 | 0.11 | 0.39 | 0.00 | 0.11 | 0.39 | 0.00 | 20.11 | -11.81 | -0.11 |
| 90 | 0.00 | 0.42 | 0.00 | 0.00 | 0.42 | 0.00 | 11.02 | -11.81 | -0.11 |
| 120 | 0.11 | 0.39 | 0.00 | -0.11 | -0.39 | 0.00 | -20.11 | -11.81 | -0.11 |
| 150 | 0.21 | 0.19 | 0.00 | -0.21 | -0.19 | 0.00 | -37.74 | -11.81 | -0.11 |
| 180 | 0.32 | 0.00 | 0.00 | -0.32 | 0.00 | 0.00 | -56.21 | 0.00 | 0.00 |

Discrete Appurtenance Totals - With Ice

| Wind Azimuth | Discrete Appurtenance Totals - With Ice | | | | | | ODM ₄ | ODM ₆ | Torque |
|--------------|---|----------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| | F _x | F _y | F _z | F ₄ | F ₅ | F ₆ | | | |
| 0 | -0.02 | -7.31 | 0.00 | -119.15 | 5.69 | -1.13 | 0.00 | 0.00 | 0.00 |
| 30 | 3.61 | -6.23 | 0.00 | -138.48 | 7.77 | -0.17 | 0.00 | 0.00 | 0.00 |
| 60 | 6.26 | -3.61 | 0.00 | -131.81 | 0.81 | 0.81 | 0.00 | 0.00 | 0.00 |
| 90 | 7.21 | 0.00 | 0.00 | -104.16 | 1.83 | 0.00 | 0.00 | 0.00 | 0.00 |
| 120 | 6.26 | 3.61 | 0.00 | -114.29 | 1.83 | 0.00 | 0.00 | 0.00 | 0.00 |
| 150 | 3.61 | 6.26 | 0.00 | -104.16 | 1.83 | 0.00 | 0.00 | 0.00 | 0.00 |
| 180 | 0.00 | 7.21 | 0.00 | -119.15 | 5.69 | 1.13 | 0.00 | 0.00 | 0.00 |
| 210 | -3.61 | 6.26 | 0.00 | -104.16 | 1.83 | 0.00 | 0.00 | 0.00 | 0.00 |
| 240 | -6.26 | 3.61 | 0.00 | -138.48 | 7.77 | -0.17 | 0.00 | 0.00 | 0.00 |
| 270 | -7.21 | 0.00 | 0.00 | -104.16 | 1.83 | 0.00 | 0.00 | 0.00 | 0.00 |
| 300 | -6.26 | -3.61 | 0.00 | -131.81 | 0.81 | 0.81 | 0.00 | 0.00 | 0.00 |
| 330 | -3.61 | -6.26 | 0.00 | -138.48 | 7.77 | -0.17 | 0.00 | 0.00 | 0.00 |

Discrete Appurtenance Pressures - Service

| Description | Aiming Azimuth | Weight | Offset _x | Offset _y | z | K _z | φ | Calc Front R ² | Calc Side R ² |
|---------------------|----------------|--------|---------------------|---------------------|--------|----------------|----|---------------------------|--------------------------|
| Screen | 0.0000 | 0.07 | 0.00 | -2.87 | 244.29 | 1.772 | 15 | 2.40 | 2.80 |
| Screen Extender (4) | 0.0000 | 0.81 | 0.00 | -2.87 | 303.21 | 1.717 | 15 | 1.11 | 1.11 |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 1343 Pico Dr. Plymouth, IN Phone: (317) 836-4311 FAX: (317) 936-6438 | Job | 284859 | Page | 74 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Description | Aiming Azimuth | Weight | | Offset | | z | K _z | φ | Calc Front R ² | Calc Side R ² |
|-------------|----------------|--------|-------|--------|--------|-------|----------------|------|---------------------------|--------------------------|
| | | K | R | R | R | | | | | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 120.0000 | 0.30 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 120.0000 | 0.30 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | -5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 0.0000 | 0.30 | 0.00 | 5.10 | 238.75 | 1.700 | 15 | 6.91 | 2.31 | |
| 12" V Frame | 240.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 240.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | -5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12" V Frame | 0.0000 | 0.00 | 5.10 | 2.91 | 238.75 | 1.700 | 15 | 1.81 | 1.33 | |
| 12 | | | | | | | | | | |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Palco Dr. Plymouth, NY Phone: (516) 935-4311 FAX: (516) 935-6438 | Job | 284859 | Page | 77 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Palco Dr. Plymouth, NY Phone: (516) 935-4311 FAX: (516) 935-6438 | Job | 284859 | Page | 78 of 107 |
| | Project | V-26 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.21 | 0.00 | 0.00 | -0.21 | 0.00 | 0.00 |
| 30 | 0.21 | 0.07 | -0.07 | -0.21 | -0.07 | -0.44 |
| 60 | 0.21 | 0.13 | -0.13 | -0.21 | -0.13 | -0.78 |
| 90 | 0.21 | 0.15 | -0.15 | -0.21 | -0.15 | -0.91 |
| 120 | 0.21 | 0.13 | -0.13 | -0.21 | -0.13 | -0.78 |
| 150 | 0.21 | 0.07 | -0.07 | -0.21 | -0.07 | -0.44 |
| 180 | 0.21 | 0.00 | 0.00 | -0.21 | 0.00 | -0.00 |
| 210 | 0.21 | 0.07 | -0.07 | -0.21 | 0.07 | 0.44 |
| 240 | 0.21 | 0.13 | -0.13 | -0.21 | 0.13 | 0.78 |
| 270 | 0.21 | 0.15 | -0.15 | -0.21 | 0.15 | 0.91 |
| 300 | 0.21 | 0.13 | -0.13 | -0.21 | 0.13 | 0.78 |
| 330 | 0.21 | 0.07 | -0.07 | -0.21 | 0.07 | 0.44 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.00 | 0.00 | 0.00 | -0.00 | 0.00 | 0.00 |
| 30 | 0.00 | 0.04 | 0.04 | -0.00 | -0.04 | -0.21 |
| 60 | 0.00 | 0.07 | 0.07 | -0.00 | -0.07 | -0.44 |
| 90 | 0.00 | 0.10 | 0.10 | -0.00 | -0.10 | -0.67 |
| 120 | 0.00 | 0.07 | 0.07 | -0.00 | -0.07 | -0.44 |
| 150 | 0.00 | 0.04 | 0.04 | -0.00 | -0.04 | -0.21 |
| 180 | 0.00 | 0.00 | 0.00 | -0.00 | 0.00 | 0.00 |
| 210 | 0.00 | 0.04 | 0.04 | -0.00 | 0.04 | 0.21 |
| 240 | 0.00 | 0.07 | 0.07 | -0.00 | 0.07 | 0.44 |
| 270 | 0.00 | 0.10 | 0.10 | -0.00 | 0.10 | 0.67 |
| 300 | 0.00 | 0.07 | 0.07 | -0.00 | 0.07 | 0.44 |
| 330 | 0.00 | 0.04 | 0.04 | -0.00 | 0.04 | 0.21 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.00 | 0.04 | -0.04 | -0.04 | 0.00 | -0.21 |
| 30 | 0.00 | 0.07 | -0.07 | -0.04 | -0.04 | -0.44 |
| 60 | 0.00 | 0.10 | -0.10 | -0.04 | -0.07 | -0.67 |
| 90 | 0.00 | 0.13 | -0.13 | -0.04 | -0.10 | -0.91 |
| 120 | 0.00 | 0.10 | -0.10 | -0.04 | -0.07 | -0.67 |
| 150 | 0.00 | 0.07 | -0.07 | -0.04 | -0.04 | -0.44 |
| 180 | 0.00 | 0.04 | -0.04 | -0.04 | 0.00 | -0.21 |
| 210 | 0.00 | 0.04 | -0.04 | -0.04 | 0.04 | 0.21 |
| 240 | 0.00 | 0.07 | -0.07 | -0.04 | 0.07 | 0.44 |
| 270 | 0.00 | 0.10 | -0.10 | -0.04 | 0.10 | 0.67 |
| 300 | 0.00 | 0.07 | -0.07 | -0.04 | 0.07 | 0.44 |
| 330 | 0.00 | 0.04 | -0.04 | -0.04 | 0.04 | 0.21 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.13 | 0.13 | 0.00 | -0.13 | 0.00 | 0.00 |
| 30 | 0.13 | 0.23 | 0.00 | -0.13 | -0.23 | -0.44 |
| 60 | 0.13 | 0.33 | 0.00 | -0.13 | -0.33 | -0.67 |
| 90 | 0.13 | 0.33 | 0.00 | -0.13 | -0.33 | -0.67 |
| 120 | 0.13 | 0.23 | 0.00 | -0.13 | -0.23 | -0.44 |
| 150 | 0.13 | 0.13 | 0.00 | -0.13 | -0.13 | -0.21 |
| 180 | 0.13 | 0.00 | 0.00 | -0.13 | 0.00 | 0.00 |
| 210 | 0.13 | 0.13 | 0.00 | -0.13 | 0.13 | 0.21 |
| 240 | 0.13 | 0.23 | 0.00 | -0.13 | 0.23 | 0.44 |
| 270 | 0.13 | 0.33 | 0.00 | -0.13 | 0.33 | 0.67 |
| 300 | 0.13 | 0.33 | 0.00 | -0.13 | 0.33 | 0.67 |
| 330 | 0.13 | 0.23 | 0.00 | -0.13 | 0.23 | 0.44 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.20 | 0.00 | 0.00 | -0.20 | 0.00 | 0.00 |
| 30 | 0.20 | 0.06 | -0.06 | -0.20 | -0.06 | -0.40 |
| 60 | 0.20 | 0.11 | -0.11 | -0.20 | -0.11 | -0.70 |
| 90 | 0.20 | 0.13 | -0.13 | -0.20 | -0.13 | -0.80 |
| 120 | 0.20 | 0.11 | -0.11 | -0.20 | -0.11 | -0.70 |
| 150 | 0.20 | 0.06 | -0.06 | -0.20 | -0.06 | -0.40 |
| 180 | 0.20 | 0.00 | 0.00 | -0.20 | 0.00 | 0.00 |
| 210 | 0.20 | 0.06 | -0.06 | -0.20 | 0.06 | 0.40 |
| 240 | 0.20 | 0.11 | -0.11 | -0.20 | 0.11 | 0.70 |
| 270 | 0.20 | 0.13 | -0.13 | -0.20 | 0.13 | 0.80 |
| 300 | 0.20 | 0.11 | -0.11 | -0.20 | 0.11 | 0.70 |
| 330 | 0.20 | 0.06 | -0.06 | -0.20 | 0.06 | 0.40 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.17 | 0.17 | 0.00 | -0.17 | 0.00 | 0.00 |
| 30 | 0.17 | 0.27 | 0.00 | -0.17 | -0.27 | -0.40 |
| 60 | 0.17 | 0.37 | 0.00 | -0.17 | -0.37 | -0.60 |
| 90 | 0.17 | 0.37 | 0.00 | -0.17 | -0.37 | -0.60 |
| 120 | 0.17 | 0.27 | 0.00 | -0.17 | -0.27 | -0.40 |
| 150 | 0.17 | 0.17 | 0.00 | -0.17 | -0.17 | -0.20 |
| 180 | 0.17 | 0.00 | 0.00 | -0.17 | 0.00 | 0.00 |
| 210 | 0.17 | 0.17 | 0.00 | -0.17 | 0.17 | 0.20 |
| 240 | 0.17 | 0.27 | 0.00 | -0.17 | 0.27 | 0.40 |
| 270 | 0.17 | 0.37 | 0.00 | -0.17 | 0.37 | 0.60 |
| 300 | 0.17 | 0.37 | 0.00 | -0.17 | 0.37 | 0.60 |
| 330 | 0.17 | 0.27 | 0.00 | -0.17 | 0.27 | 0.40 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.00 | 0.00 | -0.01 | 0.00 | 0.00 |
| 30 | 0.01 | 0.02 | -0.02 | -0.01 | -0.02 | -0.10 |
| 60 | 0.01 | 0.04 | -0.04 | -0.01 | -0.04 | -0.20 |
| 90 | 0.01 | 0.05 | -0.05 | -0.01 | -0.05 | -0.25 |
| 120 | 0.01 | 0.04 | -0.04 | -0.01 | -0.04 | -0.20 |
| 150 | 0.01 | 0.02 | -0.02 | -0.01 | -0.02 | -0.10 |
| 180 | 0.01 | 0.00 | 0.00 | -0.01 | 0.00 | 0.00 |
| 210 | 0.01 | 0.02 | -0.02 | -0.01 | 0.02 | 0.10 |
| 240 | 0.01 | 0.04 | -0.04 | -0.01 | 0.04 | 0.20 |
| 270 | 0.01 | 0.05 | -0.05 | -0.01 | 0.05 | 0.25 |
| 300 | 0.01 | 0.04 | -0.04 | -0.01 | 0.04 | 0.20 |
| 330 | 0.01 | 0.02 | -0.02 | -0.01 | 0.02 | 0.10 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.23 | 0.00 | 0.00 | -0.23 | 0.00 | 0.00 |
| 30 | 0.23 | 0.08 | -0.08 | -0.23 | -0.08 | -0.40 |
| 60 | 0.23 | 0.15 | -0.15 | -0.23 | -0.15 | -0.70 |
| 90 | 0.23 | 0.17 | -0.17 | -0.23 | -0.17 | -0.80 |
| 120 | 0.23 | 0.15 | -0.15 | -0.23 | -0.15 | -0.70 |
| 150 | 0.23 | 0.08 | -0.08 | -0.23 | -0.08 | -0.40 |
| 180 | 0.23 | 0.00 | 0.00 | -0.23 | 0.00 | 0.00 |
| 210 | 0.23 | 0.08 | -0.08 | -0.23 | 0.08 | 0.40 |
| 240 | 0.23 | 0.15 | -0.15 | -0.23 | 0.15 | 0.70 |
| 270 | 0.23 | 0.17 | -0.17 | -0.23 | 0.17 | 0.80 |
| 300 | 0.23 | 0.15 | -0.15 | -0.23 | 0.15 | 0.70 |
| 330 | 0.23 | 0.08 | -0.08 | -0.23 | 0.08 | 0.40 |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Palco Dr. Plymouth, NY Phone: (516) 935-4311 FAX: (516) 935-6438 | Job | 284859 | Page | 79 of 107 |
| | Project | V-26 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1141 Palco Dr. Plymouth, NY Phone: (516) 935-4311 FAX: (516) 935-6438 | Job | 284859 | Page | 80 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 150 | 0.20 | 0.04 | -0.04 | -0.20 | 0.04 | 0.20 |
| 180 | 0.20 | 0.00 | 0.00 | -0.20 | 0.00 | 0.00 |
| 210 | 0.20 | 0.04 | -0.04 | -0.20 | -0.04 | -0.20 |
| 240 | 0.20 | 0.11 | -0.11 | -0.20 | -0.11 | -0.40 |
| 270 | 0.20 | 0.15 | -0.15 | -0.20 | -0.15 | -0.50 |
| 300 | 0.20 | 0.11 | -0.11 | -0.20 | -0.11 | -0.40 |
| 330 | 0.20 | 0.04 | -0.04 | -0.20 | -0.04 | -0.20 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 240 | 0.00 | 0.01 | -0.01 | 0.00 | 0.01 | 0.01 |
| 270 | 0.00 | 0.02 | -0.02 | 0.00 | 0.02 | 0.02 |
| 300 | 0.00 | 0.01 | -0.01 | 0.00 | 0.01 | 0.01 |
| 330 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.00 | 0.04 | -0.04 | -0.04 | 0.00 | -0.20 |
| 30 | 0.01 | 0.07 | -0.07 | -0.04 | -0.04 | -0.40 |
| 60 | 0.01 | 0.10 | -0.10 | -0.04 | -0.07 | -0.60 |
| 90 | 0.01 | 0.12 | -0.12 | -0.04 | -0.10 | -0.80 |
| 120 | 0.00 | 0.10 | -0.10 | -0.04 | -0.07 | -0.60 |
| 150 | 0.00 | 0.04 | -0.04 | -0.04 | -0.04 | -0.40 |
| 180 | 0.00 | 0.00 | 0.00 | -0.04 | 0.00 | 0.00 |
| 210 | 0.00 | 0.04 | -0.04 | -0.04 | 0.04 | 0.40 |
| 240 | 0.01 | 0.07 | -0.07 | -0.04 | 0.07 | 0.60 |
| 270 | 0.01 | 0.10 | -0.10 | -0.04 | 0.10 | 0.80 |
| 300 | 0.00 | 0.10 | -0.10 | -0.04 | 0.10 | 0.80 |
| 330 | 0.00 | 0.04 | -0.04 | -0.04 | 0.04 | 0.40 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.00 | 0.01 | -0.01 | -0.01 | 0.00 | -0.01 |
| 30 | 0.00 | 0.02 | -0.02 | -0.01 | -0.02 | -0.02 |
| 60 | 0.00 | 0.03 | -0.03 | -0.01 | -0.03 | -0.03 |
| 90 | 0.00 | 0.04 | -0.04 | -0.01 | -0.04 | -0.04 |
| 120 | 0.00 | 0.03 | -0.03 | -0.01 | -0.03 | -0.03 |
| 150 | 0.00 | 0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| 180 | 0.00 | 0.00 | 0.00 | -0.01 | 0.00 | 0.00 |
| 210 | 0.00 | 0.01 | -0.01 | -0.01 | 0.01 | 0.01 |
| 240 | 0.00 | 0.02 | -0.02 | -0.01 | 0.02 | 0.02 |
| 270 | 0.00 | 0.03 | -0.03 | -0.01 | 0.03 | 0.03 |
| 300 | 0.00 | 0.04 | -0.04 | -0.01 | 0.04 | 0.04 |
| 330 | 0.00 | 0.03 | -0.03 | -0.01 | 0.03 | 0.03 |

| Wind Azimuth | F _x | F _y | F _z | O _{DMx} | O _{DMy} | Torque |
|--------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.00 | 0.04 | -0.04 | -0.04 | 0.00 | -0.20 |
| 30 | 0.00 | 0.07 | -0.07 | -0.04 | -0.04 | -0.40 |
| 60 | 0.00 | 0.10 | -0.10 | -0.04 | -0.07 | -0.60 |
| 90 | 0.00 | 0.12 | -0.12 | -0.04 | -0.10 | -0.80 |
| 120 | 0.00 | 0.10 | -0.10 | -0.04 | -0.07 | -0.60 |
| 150 | 0.00 | 0.04 | -0.04 | -0.04 | -0.04 | -0.40 |
| 180 | 0.00 | 0.00 | 0.00 | -0.04 | 0.00 | 0.00 |
| 210 | 0.00 | 0.04 | -0.04 | -0.04 | 0.04 | 0.40 |
| 240 | 0.00 | 0.07 | -0.07 | -0.04 | 0.07 | 0.60 |
| 270 | 0.00 | 0.10 | -0.10 | -0.04 | 0.10 | 0.80 |
| 300 | 0.00 | 0.10 | -0.10 | -0.04 | 0.10 | 0.80 |
| 330 | 0.00 | 0.04 | -0.04 | -0.04 | 0.04 | 0.40 |

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| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 330 | 0.04 | 0.01 | -0.01 | -0.04 | 2.20 | -10.21 | 3.21 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.01 | 0.01 | 0.01 | -0.03 | -7.14 | -1.78 | -0.19 |
| 30 | 0.04 | 0.01 | 0.01 | -0.03 | -7.26 | -4.62 | -0.21 |
| 60 | 0.05 | 0.01 | 0.01 | -0.04 | -7.37 | -7.44 | -0.20 |
| 90 | 0.04 | 0.01 | 0.01 | -0.04 | -7.48 | -10.21 | -0.21 |
| 120 | 0.02 | 0.02 | 0.03 | -0.01 | -7.59 | -12.94 | -0.19 |
| 150 | 0.00 | 0.03 | 0.02 | 0.02 | -7.69 | -15.61 | -0.17 |
| 180 | 0.01 | 0.03 | 0.03 | 0.03 | -7.78 | -18.24 | -0.15 |
| 210 | 0.04 | 0.01 | 0.03 | 0.03 | -7.88 | -20.83 | -0.13 |
| 240 | 0.05 | 0.01 | 0.04 | 0.02 | -7.97 | -23.38 | -0.11 |
| 270 | 0.04 | 0.01 | 0.04 | 0.01 | -8.06 | -25.89 | -0.09 |
| 300 | 0.02 | 0.02 | 0.03 | -0.01 | -8.15 | -28.36 | -0.07 |
| 330 | 0.00 | 0.03 | 0.02 | -0.02 | -8.24 | -30.78 | -0.05 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.02 | 0.02 | -0.01 | -0.03 | -7.14 | 1.32 | 0.15 |
| 30 | 0.02 | 0.03 | 0.01 | -0.02 | -7.27 | 1.32 | 0.17 |
| 60 | 0.03 | 0.02 | 0.03 | -0.01 | -7.39 | 1.32 | 0.19 |
| 90 | 0.04 | 0.01 | 0.04 | 0.01 | -7.50 | 1.32 | 0.21 |
| 120 | 0.05 | 0.01 | 0.04 | 0.02 | -7.61 | 1.32 | 0.22 |
| 150 | 0.05 | 0.01 | 0.03 | 0.03 | -7.72 | 1.32 | 0.23 |
| 180 | 0.04 | 0.02 | 0.03 | 0.03 | -7.83 | 1.32 | 0.24 |
| 210 | 0.03 | 0.03 | 0.03 | 0.03 | -7.94 | 1.32 | 0.25 |
| 240 | 0.02 | 0.04 | 0.02 | 0.03 | -8.05 | 1.32 | 0.26 |
| 270 | 0.01 | 0.04 | 0.01 | 0.04 | -8.16 | 1.32 | 0.27 |
| 300 | 0.00 | 0.04 | 0.00 | 0.04 | -8.27 | 1.32 | 0.28 |
| 330 | 0.01 | 0.03 | -0.01 | -0.03 | -8.38 | 1.32 | 0.29 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.03 | 0.00 | 0.00 | -0.03 | -11.78 | 0.00 | 0.00 |
| 30 | 0.04 | 0.01 | 0.01 | -0.04 | -11.84 | -3.42 | -0.04 |
| 60 | 0.05 | 0.01 | 0.02 | -0.02 | -11.90 | -6.81 | -0.08 |
| 90 | 0.05 | 0.01 | 0.03 | 0.00 | -11.96 | -10.21 | -0.12 |
| 120 | 0.04 | 0.02 | 0.03 | 0.02 | -12.02 | -13.59 | -0.16 |
| 150 | 0.02 | 0.03 | 0.02 | 0.03 | -12.08 | -16.96 | -0.20 |
| 180 | 0.01 | 0.04 | 0.01 | 0.04 | -12.14 | -20.33 | -0.24 |
| 210 | 0.01 | 0.04 | 0.01 | 0.04 | -12.20 | -23.70 | -0.28 |
| 240 | 0.02 | 0.03 | 0.02 | 0.03 | -12.26 | -27.07 | -0.32 |
| 270 | 0.03 | 0.02 | 0.03 | 0.02 | -12.32 | -30.44 | -0.36 |
| 300 | 0.04 | 0.01 | 0.04 | 0.01 | -12.38 | -33.81 | -0.40 |
| 330 | 0.04 | 0.01 | 0.04 | 0.01 | -12.44 | -37.18 | -0.44 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 60 | 0.05 | 0.04 | 0.07 | -0.00 | 0.14 | -14.50 | 0.21 |
| 90 | 0.11 | 0.02 | 0.10 | 0.04 | 0.31 | -24.10 | 0.11 |
| 120 | 0.12 | 0.02 | 0.11 | 0.06 | 0.55 | -21.60 | 0.00 |
| 150 | 0.11 | 0.02 | 0.11 | 0.07 | 0.79 | -11.17 | -0.12 |
| 180 | 0.05 | 0.04 | 0.04 | 0.05 | 1.03 | -10.01 | -0.21 |
| 210 | 0.01 | 0.04 | -0.03 | 0.04 | 1.42 | -8.43 | -0.24 |
| 240 | 0.06 | 0.04 | 0.07 | 0.00 | 1.81 | -13.51 | -0.21 |
| 270 | 0.11 | 0.03 | -0.10 | -0.04 | -1.43 | -23.09 | -0.11 |
| 300 | 0.12 | 0.00 | -0.11 | -0.04 | -1.82 | -24.65 | 0.00 |
| 330 | 0.11 | 0.03 | -0.09 | -0.07 | -2.21 | -18.16 | 0.12 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.12 | 0.00 | 0.00 | -0.13 | -31.25 | 0.00 | 0.00 |
| 30 | 0.11 | 0.02 | 0.02 | -0.11 | -27.29 | -4.93 | -0.11 |
| 60 | 0.06 | 0.04 | 0.04 | -0.05 | -16.49 | -8.31 | -0.21 |
| 90 | 0.00 | 0.04 | 0.04 | 0.00 | -1.74 | -9.87 | -0.24 |
| 120 | 0.05 | 0.04 | 0.04 | 0.05 | 13.41 | -4.35 | -0.21 |
| 150 | 0.11 | 0.02 | 0.02 | 0.11 | 23.81 | -4.93 | -0.12 |
| 180 | 0.13 | 0.00 | 0.00 | 0.13 | 27.79 | 0.00 | 0.00 |
| 210 | 0.11 | 0.02 | -0.07 | 0.11 | 23.81 | 4.93 | 0.12 |
| 240 | 0.06 | 0.04 | -0.04 | 0.05 | 13.41 | 8.31 | 0.21 |
| 270 | 0.00 | 0.04 | -0.04 | 0.00 | -1.74 | 9.87 | 0.24 |
| 300 | 0.06 | 0.04 | -0.04 | -0.05 | -16.49 | 16.49 | 0.21 |
| 330 | 0.11 | 0.02 | -0.02 | -0.11 | -27.29 | 27.29 | 0.12 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.03 | 0.03 | 0.00 | -0.06 | -14.33 | 0.11 | -0.27 |
| 30 | 0.05 | 0.02 | 0.03 | -0.05 | -12.45 | -7.67 | -0.11 |
| 60 | 0.06 | 0.02 | 0.03 | -0.03 | -7.33 | -15.34 | 0.00 |
| 90 | 0.05 | 0.03 | 0.04 | 0.00 | 0.00 | -14.27 | 0.11 |
| 120 | 0.02 | 0.05 | 0.03 | 0.03 | 7.27 | -12.34 | 0.27 |
| 150 | 0.00 | 0.05 | 0.03 | 0.05 | 11.54 | -7.97 | 0.31 |
| 180 | 0.03 | 0.05 | 0.00 | 0.06 | 14.47 | 0.11 | 0.27 |
| 210 | 0.01 | 0.05 | -0.03 | 0.05 | 12.34 | 7.27 | 0.11 |
| 240 | 0.00 | 0.05 | -0.05 | 0.03 | 7.27 | 11.60 | 0.06 |
| 270 | 0.06 | 0.02 | -0.04 | 0.00 | -7.97 | 14.33 | 0.31 |
| 300 | 0.03 | 0.03 | -0.03 | -0.03 | -7.33 | 11.60 | -0.27 |
| 330 | 0.00 | 0.05 | -0.03 | -0.05 | -11.60 | -7.27 | -0.31 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.00 | 0.01 | 0.01 | -0.01 | -2.11 | 0.31 | -0.11 |
| 30 | 0.01 | 0.02 | 0.00 | -0.01 | -1.70 | 1.04 | -0.08 |
| 60 | 0.01 | 0.00 | 0.01 | -0.00 | -1.00 | -1.33 | 0.00 |
| 90 | 0.01 | 0.02 | 0.01 | 0.01 | 2.99 | -3.70 | 0.21 |
| 120 | 0.00 | 0.02 | 0.01 | 0.01 | 4.11 | -4.66 | 0.31 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.02 | 0.01 | 0.01 | -0.03 | -5.77 | -1.01 | -0.11 |
| 30 | 0.02 | 0.02 | 0.02 | -0.02 | -5.65 | -4.05 | -0.08 |
| 60 | 0.01 | 0.03 | 0.00 | 0.03 | -5.39 | -7.10 | 0.00 |
| 90 | 0.01 | 0.03 | 0.01 | -0.01 | -5.10 | -10.15 | 0.06 |
| 120 | 0.02 | 0.02 | 0.02 | 0.01 | 2.61 | -5.31 | 0.11 |
| 150 | 0.00 | 0.03 | 0.01 | 0.02 | 4.62 | -2.39 | 0.13 |
| 180 | 0.01 | 0.02 | 0.01 | 0.02 | 6.62 | -1.42 | 0.11 |
| 210 | 0.02 | 0.01 | 0.02 | 0.02 | 5.53 | 4.91 | 0.05 |
| 240 | 0.03 | 0.00 | -0.02 | 0.02 | 4.12 | 7.14 | 0.00 |
| 270 | 0.05 | 0.01 | -0.03 | 0.01 | 1.34 | 7.51 | -0.02 |
| 300 | 0.03 | 0.02 | -0.02 | -0.01 | -1.19 | 5.92 | -0.11 |
| 330 | 0.00 | 0.03 | -0.01 | -0.02 | -4.29 | 2.10 | -0.13 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.02 | 0.02 | -0.01 | -0.02 | -5.77 | 1.01 | 0.11 |
| 30 | 0.02 | 0.03 | 0.01 | -0.02 | -5.77 | 1.01 | 0.11 |
| 60 | 0.03 | 0.02 | 0.03 | -0.01 | -5.77 | 1.01 | 0.11 |
| 90 | 0.04 | 0.01 | 0.04 | 0.01 | -5.77 | 1.01 | 0.11 |
| 120 | 0.05 | 0.01 | 0.04 | 0.02 | -5.77 | 1.01 | 0.11 |
| 150 | 0.05 | 0.01 | 0.03 | 0.03 | -5.77 | 1.01 | 0.11 |
| 180 | 0.04 | 0.02 | 0.03 | 0.03 | -5.77 | 1.01 | 0.11 |
| 210 | 0.03 | 0.03 | 0.03 | 0.03 | -5.77 | 1.01 | 0.11 |
| 240 | 0.02 | 0.04 | 0.02 | 0.03 | -5.77 | 1.01 | 0.11 |
| 270 | 0.01 | 0.04 | 0.01 | 0.04 | -5.77 | 1.01 | 0.11 |
| 300 | 0.00 | 0.04 | 0.00 | 0.04 | -5.77 | 1.01 | 0.11 |
| 330 | 0.01 | 0.03 | -0.01 | -0.02 | -5.77 | 1.01 | 0.11 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.04 | 0.01 | 0.01 | -0.04 | -13.91 | 1.00 | 0.21 |
| 30 | 0.11 | 0.02 | 0.02 | -0.01 | -11.13 | -11.16 | -0.12 |
| 60 | 0.12 | 0.02 | 0.02 | 0.02 | -13.91 | -24.05 | -0.12 |
| 90 | 0.11 | 0.02 | 0.03 | 0.00 | -13.91 | -24.05 | -0.12 |
| 120 | 0.05 | 0.03 | 0.03 | 0.04 | -13.91 | -24.05 | -0.12 |
| 150 | 0.00 | 0.04 | 0.02 | 0.04 | -13.91 | -24.05 | -0.12 |
| 180 | 0.00 | 0.04 | 0.02 | 0.04 | -13.91 | -24.05 | -0.12 |
| 210 | 0.05 | 0.03 | 0.03 | 0.04 | -13.91 | -24.05 | -0.12 |
| 240 | 0.11 | 0.02 | 0.02 | 0.01 | -13.91 | -24.05 | -0.12 |
| 270 | 0.11 | 0.02 | 0.02 | -0.01 | -13.91 | -24.05 | -0.12 |
| 300 | 0.05 | 0.03 | 0.03 | -0.04 | -13.91 | -24.05 | -0.12 |
| 330 | 0.00 | 0.04 | -0.02 | -0.04 | -13.91 | -24.05 | -0.12 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.04 | 0.01 | 0.01 | -0.04 | -13.91 | 1.00 | 0.21 |
| 30 | 0.00 | 0.04 | 0.02 | -0.04 | -13.91 | -4.41 | 0.21 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 150 | 0.00 | 0.04 | 0.02 | 0.03 | 7.33 | -4.34 | 0.15 |
| 180 | 0.00 | 0.03 | 0.01 | 0.03 | 7.33 | -2.81 | 0.11 |
| 210 | 0.01 | 0.02 | -0.01 | 0.02 | 4.31 | -6.34 | 0.09 |
| 240 | 0.01 | 0.00 | -0.01 | 0.00 | 1.11 | -1.00 | 0.00 |
| 270 | 0.01 | 0.02 | -0.01 | -0.01 | -2.11 | 3.90 | 0.00 |
| 300 | 0.03 | 0.01 | -0.02 | -0.03 | -6.63 | 4.31 | -0.14 |
| 330 | 0.00 | 0.04 | -0.02 | -0.03 | -7.63 | 4.31 | -0.15 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.03 | 0.03 | 0.00 | -0.04 | -14.53 | 0.11 | -0.33 |
| 30 | 0.05 | 0.02 | 0.03 | -0.03 | -12.18 | -6.95 | -0.13 |
| 60 | 0.06 | 0.02 | 0.03 | -0.01 | -7.00 | -12.18 | 0.00 |
| 90 | 0.02 | 0.03 | 0.04 | 0.00 | 0.00 | -14.53 | 0.11 |
| 120 | 0.00 | 0.05 | 0.02 | 0.03 | 7.12 | -13.13 | 0.22 |
| 150 | 0.01 | 0.05 | 0.03 | 0.05 | 12.33 | -8.95 | 0.31 |
| 180 | 0.03 | 0.05 | 0.00 | 0.06 | 12.33 | -2.70 | 0.27 |
| 210 | 0.05 | 0.03 | 0.03 | 0.05 | 12.33 | 7.20 | 0.15 |
| 240 | 0.06 | 0.02 | 0.03 | 0.01 | 7.12 | 13.13 | 0.00 |
| 270 | 0.03 | 0.03 | -0.04 | 0.00 | 0.00 | 14.24 | -0.13 |
| 300 | 0.02 | 0.03 | -0.03 | -0.01 | -6.95 | 12.33 | -0.27 |
| 330 | 0.00 | 0.05 | -0.01 | -0.05 | -12.18 | 7.00 | -0.33 |

| Wind Azimuth | F _x | F _y | V _x | V _y | OTM _x | OTM _y | Torque |
|--------------|----------------|----------------|----------------|----------------|------------------|------------------|--------|
| 0 | 0.00 | 0.02 | 0.01 | -0.02 | -0.81 | 2. | |

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Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 330, 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

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Client: Verizon Wireless Designed by: JAK

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 330, 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120, 150, 180, 210, 240, 270, 300, 330.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120.

Table with 10 columns: Wind Azimuth, Fx, Fy, Fz, ODMx, ODMy, Torque. Rows for wind azimuths 0, 30, 60, 90, 120.

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| tnxTower 1545 Pulos Dr. Plymouth, IN Phone: (770) 936-4731 FAX: (770) 936-6438 | Job | 284859 | Page | 89 of 107 |
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| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Pressure 11000-1100-1100 - Element 1H - From Layer 1 | | | | | | | | | | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| Wind Azimuth | F _x | F _y | F _z | V _x | V _y | V _z | ODM _x | ODM _y | ODM _z | Torque |
| ° | K | K | K | K | K | K | hp-ft | hp-ft | hp-ft | hp-ft |
| 150 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 | -0.11 | -2.55 | -0.01 | -0.01 |
| 180 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -2.55 | 0.00 | 0.00 |
| 210 | 0.01 | 0.01 | -0.01 | 0.00 | 0.00 | -0.11 | -2.55 | -0.01 | 0.01 | 0.01 |
| 240 | 0.01 | 0.02 | -0.01 | 0.00 | 0.00 | -0.11 | -2.55 | -0.01 | 0.01 | 0.01 |
| 270 | 0.01 | 0.02 | 0.01 | 0.00 | 0.00 | -0.11 | -2.55 | -0.01 | 0.01 | 0.01 |
| 300 | 0.01 | 0.02 | 0.02 | 0.00 | 0.00 | -0.11 | -2.55 | -0.01 | 0.01 | 0.01 |
| 330 | 0.01 | 0.02 | 0.01 | 0.00 | 0.00 | -0.11 | -2.55 | -0.01 | 0.01 | 0.01 |

| Pressure 11000-1100-1100 - Element 1H - From Layer 2 | | | | | | | | | | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| Wind Azimuth | F _x | F _y | F _z | V _x | V _y | V _z | ODM _x | ODM _y | ODM _z | Torque |
| ° | K | K | K | K | K | K | hp-ft | hp-ft | hp-ft | hp-ft |
| 0 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -0.11 | -1.71 | -1.41 | -0.01 | -0.01 |
| 30 | 0.01 | 0.01 | 0.00 | 0.01 | -0.01 | -0.11 | -1.67 | -1.41 | -0.01 | -0.01 |
| 60 | 0.01 | 0.00 | 0.00 | 0.01 | -0.01 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 90 | 0.01 | 0.00 | 0.00 | 0.01 | -0.01 | -0.11 | -1.67 | -1.41 | 0.00 | 0.00 |
| 120 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 150 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 180 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 210 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 240 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 270 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 300 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 330 | 0.01 | 0.01 | 0.00 | 0.01 | -0.01 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |

| Pressure 11000-1100-1100 - Element 1H - From Layer 3 | | | | | | | | | | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| Wind Azimuth | F _x | F _y | F _z | V _x | V _y | V _z | ODM _x | ODM _y | ODM _z | Torque |
| ° | K | K | K | K | K | K | hp-ft | hp-ft | hp-ft | hp-ft |
| 0 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.00 | 0.01 | -0.01 | -0.11 | -1.67 | -1.41 | 0.00 | 0.00 |
| 60 | 0.01 | 0.00 | 0.00 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 90 | 0.01 | 0.00 | 0.00 | 0.01 | 0.00 | -0.11 | -1.67 | -1.41 | 0.00 | 0.00 |
| 120 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 150 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 180 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 210 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 240 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 270 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 300 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |
| 330 | 0.01 | 0.01 | 0.00 | 0.01 | -0.01 | -0.11 | -1.71 | -1.41 | 0.00 | 0.00 |

| Pressure 11000-1100-1100 - Element 1H - From Layer 4 | | | | | | | | | | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| Wind Azimuth | F _x | F _y | F _z | V _x | V _y | V _z | ODM _x | ODM _y | ODM _z | Torque |
| ° | K | K | K | K | K | K | hp-ft | hp-ft | hp-ft | hp-ft |
| 0 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.00 | 0.00 | -0.01 | -0.11 | -0.00 | -0.00 | -0.01 | -0.01 |
| 60 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 90 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 120 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 150 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 180 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 210 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 240 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 270 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 300 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 330 | 0.01 | 0.01 | 0.00 | 0.01 | -0.01 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| tnxTower 1545 Pulos Dr. Plymouth, IN Phone: (770) 936-4731 FAX: (770) 936-6438 | Job | 284859 | Page | 91 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Pressure 11000-1100-1100 - Element 1H - From Layer 5 | | | | | | | | | | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| Wind Azimuth | F _x | F _y | F _z | V _x | V _y | V _z | ODM _x | ODM _y | ODM _z | Torque |
| ° | K | K | K | K | K | K | hp-ft | hp-ft | hp-ft | hp-ft |
| 330 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |

| Pressure 11000-1100-1100 - Element 1H - From Layer 6 | | | | | | | | | | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| Wind Azimuth | F _x | F _y | F _z | V _x | V _y | V _z | ODM _x | ODM _y | ODM _z | Torque |
| ° | K | K | K | K | K | K | hp-ft | hp-ft | hp-ft | hp-ft |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.11 | 0.11 | -0.01 | -0.01 |
| 30 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.11 | 0.11 | -0.01 | -0.01 |
| 60 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 90 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 120 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 150 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 180 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 210 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 240 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 270 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 300 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 330 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |

| Pressure 11000-1100-1100 - Element 1H - From Layer 7 | | | | | | | | | | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| Wind Azimuth | F _x | F _y | F _z | V _x | V _y | V _z | ODM _x | ODM _y | ODM _z | Torque |
| ° | K | K | K | K | K | K | hp-ft | hp-ft | hp-ft | hp-ft |
| 0 | 0.00 | 0.00 | 0.00 | -0.00 | -0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 30 | 0.00 | 0.00 | 0.00 | -0.00 | -0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 120 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 150 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 180 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 210 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 240 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 270 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |
| 330 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.11 | 0.11 | 0.00 | 0.00 |

| Pressure 11000-1100-1100 - Element 1H - From Layer 8 | | | | | | | | | | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| Wind Azimuth | F _x | F _y | F _z | V _x | V _y | V _z | ODM _x | ODM _y | ODM _z | Torque |
| ° | K | K | K | K | K | K | hp-ft | hp-ft | hp-ft | hp-ft |
| 0 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.00 | -0.00 | -0.01 | -0.01 |
| 60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 120 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 180 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 210 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 240 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 270 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |
| 330 | 0.01 | 0.00 | 0.00 | 0.00 | -0.01 | -0.11 | -0.00 | -0.00 | -0.00 | -0.00 |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| tnxTower 1545 Pulos Dr. Plymouth, IN Phone: (770) 936-4731 FAX: (770) 936-6438 | Job | 284859 | Page | 90 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Pressure 11000-1100-1100 - Element 1H - From Layer 9 | | | | | | | | | | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|------------------|------------------|------------------|--------|
| Wind Azimuth | F _x | F _y | F _z | V _x | V _y | V _z | ODM _x | ODM _y | ODM _z | Torque |
| ° | K | K | K | K | K | K | hp-ft | hp-ft | hp-ft | hp-ft |
| 240 | 0.01 | 0.01 | 0.01 | -0.01 | -0.01 | -0.11 | 0.11 | 0.11 | 0.00 | 0.00 |
| 270 | 0.01 | 0.01 | 0.01 | -0.01 | -0.01 | -0.11 | 0.11 | 0.11 | 0.00 | 0.00 |
| 300 | 0.01 | 0.01 | 0.01 | -0.01 | -0.01 | -0.11 | 0.11 | 0.11 | 0.00 | 0.00 |
| 330 | 0.01 | 0.01 | 0.01 | -0.01 | -0.01 | -0.11 | 0.11 | 0.11 | 0.00 | 0.00 |

| Pressure 11000-1100-1100 - Element 1H - From Layer 10 | | | | | | | | | | |
|---|----------------|--|--|--|--|--|--|--|--|--|
| Wind Azimuth | F _x | | | | | | | | | |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 150 Falso Dr. Plymouth, CT Phone: (770) 836-4311 FAX: (770) 836-6438 | Job | 284859 | Page | 93 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 150 Falso Dr. Plymouth, CT Phone: (770) 836-4311 FAX: (770) 836-6438 | Job | 284859 | Page | 94 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| Wind Azimuth # | F _x | | F _y | | ODL | | ODR | | Torque lb-ft |
|-------------------|----------------|------|----------------|------|-------|-------|-------|------|-----------------|
| | K | K | K | K | lb-ft | lb-ft | lb-ft | | |
| 0 | 0.01 | 0.01 | 0.01 | 0.01 | -1.91 | -3.31 | -3.31 | 0.00 | 0.00 |
| 30 | 0.01 | 0.01 | 0.01 | 0.01 | -4.09 | -1.51 | -1.51 | 0.00 | 0.00 |
| 60 | 0.01 | 0.01 | 0.01 | 0.01 | 1.10 | -2.71 | -2.71 | 0.00 | 0.00 |
| 90 | 0.00 | 0.01 | 0.01 | 0.01 | 2.41 | -1.10 | -1.10 | 0.00 | 0.00 |
| 120 | 0.01 | 0.01 | 0.01 | 0.01 | 3.11 | 0.71 | 0.71 | 0.00 | 0.00 |
| 150 | 0.01 | 0.01 | 0.01 | 0.01 | 3.00 | 2.50 | 2.50 | 0.00 | 0.00 |
| 180 | 0.02 | 0.01 | 0.01 | 0.01 | 2.10 | 3.64 | 3.64 | 0.00 | 0.00 |
| 210 | 0.02 | 0.01 | 0.01 | 0.01 | 0.67 | 3.83 | 3.83 | 0.00 | 0.00 |
| 240 | 0.02 | 0.01 | 0.01 | 0.01 | -0.92 | 3.06 | 3.06 | 0.00 | 0.00 |
| 270 | 0.02 | 0.01 | 0.01 | 0.01 | -0.91 | -0.92 | -0.92 | 0.00 | 0.00 |
| 300 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | -2.73 | -2.73 | 0.00 | 0.00 |
| 330 | 0.00 | 0.01 | 0.01 | 0.01 | -0.01 | -1.51 | -1.51 | 0.00 | 0.00 |

| Wind Azimuth # | F _x | | F _y | | ODL | | ODR | | Torque lb-ft |
|-------------------|----------------|------|----------------|------|-------|-------|-------|-------|-----------------|
| | K | K | K | K | lb-ft | lb-ft | lb-ft | | |
| 150 | 0.10 | 0.01 | 0.01 | 0.01 | 1.83 | 18.37 | 18.37 | -3.81 | -0.11 |
| 180 | 0.12 | 0.00 | 0.00 | 0.01 | 3.11 | 21.45 | 21.45 | -3.81 | -0.11 |
| 210 | 0.10 | 0.01 | 0.01 | 0.01 | 1.83 | 18.37 | 18.37 | -3.81 | -0.11 |
| 240 | 0.00 | 0.01 | 0.01 | 0.01 | 0.00 | 1.83 | 18.37 | -3.81 | -0.11 |
| 270 | 0.00 | 0.01 | 0.01 | 0.01 | 0.00 | 1.83 | 18.37 | -3.81 | -0.11 |
| 300 | 0.00 | 0.01 | 0.01 | 0.01 | 0.00 | 1.83 | 18.37 | -3.81 | -0.11 |
| 330 | 0.10 | 0.01 | 0.01 | 0.01 | 1.83 | 18.37 | 18.37 | -3.81 | -0.11 |

| Wind Azimuth # | F _x | | F _y | | ODL | | ODR | | Torque lb-ft |
|-------------------|----------------|------|----------------|------|--------|--------|--------|-------|-----------------|
| | K | K | K | K | lb-ft | lb-ft | lb-ft | | |
| 0 | 0.04 | 0.01 | 0.01 | 0.01 | -10.79 | -5.13 | -5.13 | -0.30 | 0.20 |
| 30 | 0.10 | 0.01 | 0.01 | 0.01 | -12.32 | -17.92 | -17.92 | -0.12 | 0.12 |
| 60 | 0.12 | 0.01 | 0.01 | 0.01 | -10.71 | -18.53 | -18.53 | 0.12 | 0.12 |
| 90 | 0.10 | 0.01 | 0.01 | 0.01 | -5.80 | -17.80 | -17.80 | 0.12 | 0.12 |
| 120 | 0.08 | 0.01 | 0.01 | 0.01 | 0.60 | -11.87 | -11.87 | 0.20 | 0.20 |
| 150 | 0.04 | 0.01 | 0.01 | 0.01 | 7.81 | -2.24 | -2.24 | 0.20 | 0.20 |
| 180 | 0.04 | 0.01 | 0.01 | 0.01 | 0.60 | 12.50 | 12.50 | 0.20 | 0.20 |
| 210 | 0.10 | 0.01 | 0.01 | 0.01 | 6.27 | 14.29 | 14.29 | 0.11 | 0.11 |
| 240 | 0.12 | 0.01 | 0.01 | 0.01 | 0.60 | 12.47 | 12.47 | 0.00 | 0.00 |
| 270 | 0.10 | 0.01 | 0.01 | 0.01 | -0.91 | 12.47 | 12.47 | -0.12 | -0.12 |
| 300 | 0.08 | 0.01 | 0.01 | 0.01 | -0.00 | 8.11 | 8.11 | -0.20 | -0.20 |
| 330 | 0.04 | 0.01 | 0.01 | 0.01 | -0.01 | -3.31 | -3.31 | -0.21 | -0.21 |

Discrete Appurtenance Totals - Service

| Wind Azimuth # | F _x | | F _y | | ODL | | ODR | | Torque lb-ft |
|-------------------|----------------|-------|----------------|---------|-------|-------|-------|-------|-----------------|
| | K | K | K | K | lb-ft | lb-ft | lb-ft | | |
| 0 | -0.01 | -3.59 | -796.95 | 3.77 | -0.41 | -0.41 | -0.41 | -0.41 | -0.41 |
| 30 | 1.79 | -1.11 | -618.55 | -372.91 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 |
| 60 | 3.04 | -1.79 | -596.12 | -418.20 | 0.34 | 0.34 | 0.34 | 0.34 | 0.34 |
| 90 | 3.54 | 0.01 | 2.70 | -797.17 | 0.61 | 0.61 | 0.61 | 0.61 | 0.61 |
| 120 | 3.00 | 1.80 | 801.17 | -439.65 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| 150 | 1.80 | 3.12 | 922.11 | -392.61 | 0.48 | 0.48 | 0.48 | 0.48 | 0.48 |
| 180 | 0.61 | 3.50 | 797.13 | -45.04 | 0.75 | 0.75 | 0.75 | 0.75 | 0.75 |
| 210 | -1.77 | 3.11 | 629.87 | -393.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 240 | -1.79 | 1.79 | 392.10 | -444.12 | -0.35 | -0.35 | -0.35 | -0.35 | -0.35 |
| 270 | -0.55 | -0.61 | -81.20 | 791.23 | -0.69 | -0.69 | -0.69 | -0.69 | -0.69 |
| 300 | -3.09 | -1.80 | -600.30 | 656.44 | -0.44 | -0.44 | -0.44 | -0.44 | -0.44 |
| 330 | -1.79 | -3.12 | -491.30 | -387.87 | -0.76 | -0.76 | -0.76 | -0.76 | -0.76 |

| Wind Azimuth # | F _x | | F _y | | ODL | | ODR | | Torque lb-ft |
|-------------------|----------------|------|----------------|------|--------|--------|--------|-------|-----------------|
| | K | K | K | K | lb-ft | lb-ft | lb-ft | | |
| 0 | 0.04 | 0.01 | 0.01 | 0.01 | -10.79 | -5.13 | -5.13 | -0.30 | 0.20 |
| 30 | 0.10 | 0.01 | 0.01 | 0.01 | -12.32 | -17.92 | -17.92 | -0.12 | 0.12 |
| 60 | 0.12 | 0.01 | 0.01 | 0.01 | -10.71 | -18.53 | -18.53 | 0.12 | 0.12 |
| 90 | 0.10 | 0.01 | 0.01 | 0.01 | -5.80 | -17.80 | -17.80 | 0.12 | 0.12 |
| 120 | 0.08 | 0.01 | 0.01 | 0.01 | 0.60 | -11.87 | -11.87 | 0.20 | 0.20 |
| 150 | 0.04 | 0.01 | 0.01 | 0.01 | 7.81 | -2.24 | -2.24 | 0.20 | 0.20 |
| 180 | 0.04 | 0.01 | 0.01 | 0.01 | 0.60 | 12.50 | 12.50 | 0.20 | 0.20 |
| 210 | 0.10 | 0.01 | 0.01 | 0.01 | 6.27 | 14.29 | 14.29 | 0.11 | 0.11 |
| 240 | 0.12 | 0.01 | 0.01 | 0.01 | 0.60 | 12.47 | 12.47 | 0.00 | 0.00 |
| 270 | 0.10 | 0.01 | 0.01 | 0.01 | -0.91 | 12.47 | 12.47 | -0.12 | -0.12 |
| 300 | 0.08 | 0.01 | 0.01 | 0.01 | -0.00 | 8.11 | 8.11 | -0.20 | -0.20 |
| 330 | 0.04 | 0.01 | 0.01 | 0.01 | -0.01 | -3.31 | -3.31 | -0.21 | -0.21 |

Force Totals

| Load Case | Vertical Forces K | Sum of Forces | | Sum of Overturning Moments | | Sum of Torques | |
|--------------------------|----------------------|---------------|--------|----------------------------|----------|----------------|-------|
| | | X | Z | lb-ft | lb-ft | lb-ft | lb-ft |
| Leg Weight | 14.01 | | | | | | |
| Base Weight | 12.71 | | | | | | |
| Total Member Self-Weight | 26.72 | | | | | | |
| Wind 0 deg - No Ice | 0.01 | -4.11 | -4.11 | -418.45 | -5.14 | -0.57 | -0.11 |
| Wind 30 deg - No Ice | 22.41 | -18.06 | -18.06 | -3156.17 | -32.24 | -0.11 | -0.11 |
| Wind 60 deg - No Ice | 18.57 | -12.29 | -12.29 | -3312.59 | -31.67 | 0.71 | 0.71 |
| Wind 90 deg - No Ice | 14.59 | 0.01 | 0.01 | -6319.07 | 1.31 | 1.31 | 1.31 |
| Wind 120 deg - No Ice | 33.31 | 31.29 | 31.29 | -3026.47 | 1.69 | 1.69 | 1.69 |
| Wind 150 deg - No Ice | 33.49 | 31.59 | 31.59 | -3214.69 | -0.91 | 1.59 | 1.59 |
| Wind 180 deg - No Ice | 0.01 | 44.41 | 44.41 | -6034.69 | -4.31 | 0.97 | 0.97 |
| Wind 210 deg - No Ice | -12.41 | 31.56 | 31.56 | -3312.14 | -3426.07 | -0.21 | -0.21 |
| Wind 240 deg - No Ice | -19.50 | 23.09 | 23.09 | -3026.29 | -3345.33 | -0.71 | -0.71 |
| Wind 270 deg - No Ice | -14.59 | -0.01 | -0.01 | -4.21 | -6059.99 | -1.48 | -1.48 |
| Wind 300 deg - No Ice | -13.30 | -33.32 | -33.32 | -3026.74 | 3228.17 | -1.48 | -1.48 |
| Wind 330 deg - No Ice | -11.81 | -31.89 | -31.89 | -3165.99 | 3342.31 | -1.91 | -1.91 |
| Total Weight | 50.17 | | | | | | |
| Total Weight Ice | 118.41 | | | | | | |
| Wind 0 deg - Ice | | -4.01 | -4.01 | -9319.32 | 5.49 | -1.11 | -1.11 |

| Wind Azimuth # | F _x | | F _y | | ODL | | ODR | | Torque lb-ft |
|-------------------|----------------|------|----------------|------|--------|-------|-------|-------|-----------------|
| | K | K | K | K | lb-ft | lb-ft | lb-ft | | |
| 0 | 0.12 | 0.00 | 0.00 | 0.00 | -24.99 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30 | 0.10 | 0.01 | 0.01 | 0.01 | -21.86 | -3.41 | -3.41 | -0.11 | -0.11 |
| 60 | 0.06 | 0.01 | 0.01 | 0.01 | -13.31 | -6.72 | -6.72 | -0.20 | -0.20 |
| 90 | 0.00 | 0.01 | 0.01 | 0.01 | -3.71 | -7.31 | -7.31 | -0.21 | -0.21 |
| 120 | 0.04 | 0.01 | 0.01 | 0.01 | 9.82 | -4.71 | -4.71 | -0.20 | -0.20 |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 150 Falso Dr. Plymouth, CT Phone: (770) 836-4311 FAX: (770) 836-6438 | Job | 284859 | Page | 95 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 150 Falso Dr. Plymouth, CT Phone: (770) 836-4311 FAX: (770) 836-6438 | Job | 284859 | Page | 96 of 107 |
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| Load Case | Vertical Forces K | Sum of Forces | | Sum of Overturning Moments | | Sum of Torques | |
|------------------------|----------------------|---------------|--------|----------------------------|-----------|----------------|-------|
| | | X | Z | lb-ft | lb-ft | lb-ft | lb-ft |
| Wind 30 deg - Ice | 33.30 | -15.41 | -15.41 | -7420.27 | -4274.39 | -0.17 | -0.17 |
| Wind 60 deg - Ice | 54.30 | -31.34 | -31.34 | -11314.01 | -7196.32 | 0.81 | 0.81 |
| Wind 90 deg - Ice | 64.01 | 0.01 | 0.01 | -4579.84 | -4579.84 | 1.61 | 1.61 |
| Wind 120 deg - Ice | 61.10 | 35.32 | 35.32 | -4659.84 | -4022.35 | 2.00 | 2.00 |
| Wind 150 deg - Ice | 33.23 | 56.09 | 56.09 | -7672.14 | -4214.46 | 1.82 | 1.82 |
| Wind 180 deg - Ice | 0.01 | 63.72 | 63.72 | -1174.44 | -5.63 | 1.11 | 1.11 |
| Wind 210 deg - Ice | -32.30 | 55.01 | 55.01 | -7432.60 | -4294.48 | 0.17 | 0.17 |
| Wind 240 deg - Ice | -61.69 | 33.21 | 33.21 | -4522.09 | -8306.45 | -0.81 | -0.81 |
| Wind 270 deg - Ice | -44.01 | -0.01 | -0.01 | -3.31 | -1181.11 | -0.21 | -0.21 |
| Wind 300 deg - Ice | -54.27 | -31.32 | -31.32 | -41659.92 | -7925.56 | -2.00 | -2.00 |
| Wind 330 deg - Ice | -32.31 | -44.01 | -44.01 | -7424.34 | -4284.34 | -1.11 | -1.11 |
| Total Weight | 0.01 | | | 0.41 | | | |
| Wind 0 deg - Service | | -11.10 | -11.10 | -3214.80 | 2.77 | -0.11 | -0.11 |
| Wind 30 deg - Service | 31.19 | -18.41 | -18.41 | -13071.81 | -13071.81 | -0.07 | -0.07 |
| Wind 60 deg - Service | 19.22 | -11.11 | -11.11 | -1500.84 | -2196.57 | 0.36 | 0.36 |
| Wind 90 deg - Service | 22.10 | 0.01 | 0.01 | -3018.84 | -3018.84 | 0.69 | 0.69 |
| Wind 120 deg - Service | 10.19 | 11.11 | 11.11 | -1544.09 | -2657.39 | 0.84 | 0.84 |
| Wind 150 deg - Service | 13.20 | 19.42 | 19.42 | -2522.04 | -3711.25 | 0.26 | 0.26 |
| Wind 180 deg - Service | 0.01 | 32.23 | 32.23 | -3097.11 | -1.91 | 0.48 | 0.48 |
| Wind 210 deg - Service | -11.10 | 19.41 | 19.41 | -2616.09 | -1551.01 | -0.31 | -0.31 |
| Wind 240 deg - Service | -19.41 | 11.49 | 11.49 | -1840.01 | -2663.70 | -0.81 | -0.81 |
| Wind 270 deg - Service | -22.39 | -0.01 | -0.01 | -1.92 | -3199.47 | -0.69 | -0.69 |
| Wind 300 deg - Service | -19.42 | -11.11 | -11.11 | -1304.84 | -2199.77 | 0.84 | 0.84 |
| Wind 330 deg - Service | -11.20 | -19.42 | -19.42 | -3011.11 | -1512.01 | -0.26 | -0.26 |

| Conc. No. | Description | Force | Major Axis Moment | Minor Axis Moment |
|-----------|-----------------------------|-------|-------------------|-------------------|
| | | K | lb-ft | lb-ft |
| 28 | Dead+Wind 30 deg - Service | 19.54 | 0.24 | 0.11 |
| 29 | Dead+Wind 60 deg - Service | 25 | 0.34 | -0.18 |
| 30 | Dead+Wind 90 deg - Service | 15 | 0.01 | 0.00 |
| 31 | Dead+Wind 120 deg - Service | 21 | 0.57 | 0.21 |
| 32 | Dead+Wind 150 deg - Service | 19 | 0.85 | -0.54 |
| 33 | Dead+Wind 180 deg - Service | 1 | 1.33 | -0.55 |
| 34 | Dead+Wind 210 deg - Service | 2 | -1.31 | 0.00 |
| 35 | Dead+Wind 240 deg - Service | | | |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| tnxTower 1141 Park Dr. Plymouth, IN Phone: (317) 935-4331 FAX: (317) 935-6438 | Job | 284859 | Page | 97 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
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| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| tnxTower 1141 Park Dr. Plymouth, IN Phone: (317) 935-4331 FAX: (317) 935-6438 | Job | 284859 | Page | 98 of 107 |
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| | Client | Verizon Wireless | Designed by | JAK |
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| Section No | Elevation # | Component Type | Condition | Gen. Load Comb. | Force | Major Axis Moment | Minor Axis Moment | | | |
|------------|------------------|----------------|------------------|-----------------|----------|-------------------|-------------------|--------|------|------|
| T5 | 160 - 140 | Diagonal | Max. Mt | 13 | -113.37 | 1.73 | 0.00 | | | |
| | | | Max. Vy | 20 | -10.00 | -0.09 | -0.91 | | | |
| | | | Max. Vy | 20 | 6.66 | -0.09 | -0.91 | | | |
| | | | Max. Vy | 19 | 3.92 | 0.00 | 0.00 | | | |
| | | | Max. Vy | 19 | -0.69 | 0.00 | 0.00 | | | |
| | | Leg | Max. Mt | 15 | -4.50 | 0.00 | 0.01 | | | |
| | | | Max. Vy | 24 | -4.71 | -0.03 | 0.01 | | | |
| | | | Max. Vy | 15 | -0.83 | 0.00 | 0.01 | | | |
| | | | Max. Vy | 24 | -0.00 | 0.00 | 0.00 | | | |
| | | | Max. Tension | 21 | 151.03 | -2.31 | 0.03 | | | |
| | | | Max. Compression | 15 | -200.84 | 9.87 | 0.02 | | | |
| | | | Max. Mt | 15 | -200.84 | 9.80 | 0.03 | | | |
| | | | Max. Vy | 20 | -1.27 | -0.23 | -0.94 | | | |
| | | | Max. Vy | 13 | -1.46 | 0.72 | 0.03 | | | |
| | | | Max. Vy | 20 | 1.22 | -0.23 | -0.94 | | | |
| T6 | 140 - 120 | Diagonal | Max. Tension | 11 | 635 | 0.00 | 0.00 | | | |
| | | | Max. Compression | 11 | -4.86 | 0.00 | 0.00 | | | |
| | | | Max. Mt | 19 | 4.16 | 0.17 | -0.61 | | | |
| | | | Max. Vy | 24 | -0.87 | -0.06 | 0.03 | | | |
| | | | Max. Vy | 19 | -0.65 | 0.17 | -0.61 | | | |
| | | Leg | Max. Tension | 21 | 185.40 | -2.78 | 0.02 | | | |
| | | | Max. Compression | 15 | -239.94 | 6.91 | 0.03 | | | |
| | | | Max. Mt | 19 | -22.03 | 9.52 | 0.01 | | | |
| | | | Max. Vy | 20 | -17.41 | -0.35 | -0.71 | | | |
| | | | Max. Vy | 15 | -1.19 | 0.33 | 0.01 | | | |
| | | | Max. Vy | 26 | -0.98 | -0.36 | 1.77 | | | |
| | | | Max. Tension | 18 | 7.00 | 0.00 | 0.00 | | | |
| | | | Max. Compression | 18 | -7.03 | 0.00 | 0.00 | | | |
| | | | Max. Mt | 15 | 6.45 | 0.13 | -0.61 | | | |
| | | | Max. Vy | 20 | 6.55 | 0.11 | -0.61 | | | |
| T7 | 120 - 100 | Diagonal | Max. Tension | 15 | 229.70 | -0.11 | 0.03 | | | |
| | | | Max. Vy | 20 | 0.00 | 0.00 | 0.00 | | | |
| | | | Max. Tension | 21 | 212.84 | -2.75 | 0.02 | | | |
| | | | Max. Compression | 15 | -280.23 | 11.76 | 0.01 | | | |
| | | | Max. Mt | 22 | -31.71 | 0.33 | -0.05 | | | |
| | | Leg | Max. Vy | 18 | -1.30 | 11.76 | 0.01 | | | |
| | | | Max. Vy | 20 | 1.83 | 0.53 | 0.66 | | | |
| | | | Max. Tension | 19 | 7.97 | 0.00 | 0.00 | | | |
| | | | Max. Compression | 19 | -4.42 | 0.00 | 0.00 | | | |
| | | | Max. Mt | 19 | 6.60 | 0.19 | -0.01 | | | |
| | | | Max. Vy | 24 | -7.11 | 0.00 | 0.02 | | | |
| | | | Max. Vy | 15 | -0.06 | 0.19 | -0.61 | | | |
| | | | Max. Vy | 24 | -0.00 | 0.00 | 0.00 | | | |
| | | | Max. Tension | 21 | 229.70 | -0.11 | 0.03 | | | |
| | | | Max. Compression | 15 | -353.14 | 15.03 | 0.02 | | | |
| T8 | 100 - 80 | Diagonal | Max. Mt | 21 | 227.36 | -16.38 | -0.83 | | | |
| | | | Max. Vy | 20 | -33.19 | -1.65 | -12.48 | | | |
| | | | Max. Vy | 17 | 1.47 | 16.69 | -0.02 | | | |
| | | | Max. Vy | 26 | -4.37 | -1.65 | 12.48 | | | |
| | | | Max. Tension | 18 | 11.24 | 0.00 | 0.00 | | | |
| | | Leg | Max. Compression | 19 | -12.30 | 0.00 | 0.00 | | | |
| | | | Max. Mt | 21 | 10.33 | -0.20 | 0.01 | | | |
| | | | Max. Vy | 24 | -11.34 | -0.66 | -0.07 | | | |
| | | | Max. Vy | 21 | -0.69 | -0.29 | 0.01 | | | |
| | | | Max. Vy | 24 | 0.01 | 0.00 | 0.00 | | | |
| | | | Max. Tension | 21 | 251.19 | 0.96 | 0.03 | | | |
| | | | Max. Compression | 15 | -346.22 | 16.61 | 0.03 | | | |
| | | | Max. Mt | 18 | -346.22 | 16.61 | 0.03 | | | |
| | | | T9 | 80 - 60 | Diagonal | Max. Tension | 18 | 11.24 | 0.00 | 0.00 |
| | | | | | | Max. Compression | 19 | -12.30 | 0.00 | 0.00 |
| Max. Mt | 21 | 10.33 | | | | -0.20 | 0.01 | | | |
| Max. Vy | 24 | -11.34 | | | | -0.66 | -0.07 | | | |
| Max. Vy | 21 | -0.69 | | | | -0.29 | 0.01 | | | |
| Leg | Max. Tension | 21 | | | 251.19 | 0.96 | 0.03 | | | |
| | Max. Compression | 15 | | | -346.22 | 16.61 | 0.03 | | | |
| | Max. Mt | 18 | | | -346.22 | 16.61 | 0.03 | | | |
| | | | | | | | | | | |

| Section No | Elevation # | Component Type | Condition | Gen. Load Comb. | Force | Major Axis Moment | Minor Axis Moment |
|------------|-------------|----------------|------------------|-----------------|---------|-------------------|-------------------|
| T10 | 60 - 40 | Diagonal | Max. Mt | 24 | -20.00 | 2.61 | 9.82 |
| | | | Max. Vy | 15 | -3.87 | 19.63 | 0.03 |
| | | | Max. Vy | 26 | -0.37 | 2.82 | 9.82 |
| | | | Max. Tension | 18 | 11.49 | 0.00 | 0.00 |
| | | | Max. Compression | 18 | -12.77 | 0.00 | 0.00 |
| | | Leg | Max. Mt | 19 | 10.93 | -0.33 | 0.06 |
| | | | Max. Vy | 20 | 11.18 | -0.31 | 0.06 |
| | | | Max. Vy | 21 | -0.10 | -0.33 | 0.06 |
| | | | Max. Vy | 20 | -0.81 | 0.00 | 0.00 |
| | | | Max. Tension | 21 | 215.37 | 5.37 | 0.02 |
| | | | Max. Compression | 15 | -314.10 | 12.81 | 0.03 |
| | | | Max. Mt | 21 | 278.82 | -18.11 | -0.02 |
| | | | Max. Vy | 20 | -35.27 | -3.52 | -6.39 |
| | | | Max. Vy | 17 | 1.33 | -18.16 | -0.01 |
| | | | Max. Vy | 26 | -0.99 | -3.11 | 6.39 |
| T11 | 40 - 20 | Diagonal | Max. Tension | 18 | 11.24 | 0.00 | 0.00 |
| | | | Max. Compression | 19 | -12.16 | 0.00 | 0.00 |
| | | | Max. Mt | 15 | 11.10 | -0.40 | 0.01 |
| | | | Max. Vy | 20 | 12.41 | -0.43 | 0.07 |
| | | | Max. Vy | 21 | -0.14 | -0.47 | 0.07 |
| | | Leg | Max. Tension | 21 | 207.52 | -3.36 | 0.02 |
| | | | Max. Compression | 15 | -212.00 | 17.31 | 0.01 |
| | | | Max. Mt | 15 | -41.00 | 12.71 | 0.01 |
| | | | Max. Vy | 20 | -38.31 | 3.97 | -13.58 |
| | | | Max. Vy | 15 | -1.72 | 12.71 | 0.01 |
| | | | Max. Vy | 26 | -1.35 | 5.91 | 15.50 |
| | | | Max. Tension | 18 | 11.24 | 0.00 | 0.00 |
| | | | Max. Compression | 18 | -13.43 | 0.00 | 0.00 |
| | | | Max. Mt | 21 | 8.46 | -0.61 | -0.04 |
| | | | Max. Vy | 24 | -12.89 | -0.27 | -0.29 |
| T12 | 20 - 0 | Diagonal | Max. Tension | 21 | 333.51 | 5.99 | 0.03 |
| | | | Max. Compression | 15 | -458.61 | 17.43 | 0.01 |
| | | | Max. Mt | 15 | -18.61 | 7.65 | 0.01 |
| | | | Max. Vy | 24 | -0.39 | 1.91 | -18.21 |
| | | | Max. Vy | 17 | 1.18 | -6.90 | -0.01 |
| | | Leg | Max. Tension | 21 | 333.51 | 5.99 | 0.03 |
| | | | Max. Compression | 15 | -458.61 | 17.43 | 0.01 |
| | | | Max. Mt | 15 | -18.61 | 7.65 | 0.01 |
| | | | Max. Vy | 24 | -0.39 | 1.91 | -18.21 |
| | | | Max. Vy | 17 | 1.18 | -6.90 | -0.01 |
| | | | Max. Tension | 18 | 11.24 | 0.00 | 0.00 |
| | | | Max. Compression | 19 | -13.43 | 0.00 | 0.00 |
| | | | Max. Mt | 15 | 11.10 | -0.40 | 0.01 |
| | | | Max. Vy | 20 | 12.41 | -0.43 | 0.07 |
| | | | Max. Vy | 20 | -0.16 | -0.43 | 0.18 |
| Max. Vy | 20 | -0.81 | 0.00 | 0.00 | | | |

Maximum Reactions

| Location | Condition | Gen. Load Comb. | Vertical X | Horizontal X | Horizontal Z |
|----------|-----------|-----------------|------------|--------------|--------------|
| Leg C | Max. Vert | 23 | 475.56 | 38.93 | -22.45 |
| | Max. Hx | 22 | -475.56 | 38.93 | -22.45 |
| | Max. Vy | 17 | -337.73 | -32.16 | 18.54 |
| | Min. Vert | 17 | -337.73 | -32.16 | 18.54 |
| | Min. Hx | 17 | -337.73 | -32.16 | 18.54 |
| | Min. Hx | 23 | 475.56 | 38.93 | -22.45 |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
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| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

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|--|---------|---------------------------|-------------|-------------------|
| tnxTower 1141 Park Dr. Plymouth, IN Phone: (317) 935-4331 FAX: (317) 935-6438 | Job | 284859 | Page | 100 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 15:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |
| | | | | |

| Location | Condition | Gen. Load Comb. | Vertical X | Horizontal X | Horizontal Z |
|----------|-----------|-----------------|------------|--------------|--------------|
| Leg B | Max. Vert | 19 | 475.45 | -31.98 | -25.44 |
| | Max. Hx | 25 | -338.17 | 32.19 | 18.33 |
| | Max. Vy | 25 | -338.17 | 32.19 | 18.33 |
| | Min. Vert | 19 | -338.17 | -31.98 | -25.44 |
| Leg A | Max. Hx | 19 | 475.45 | -31.98 | -25.44 |
| | Max. Vy | 15 | 676.08 | -0.03 | 64.98 |
| | Max. Hx | 25 | -338.17 | 32.19 | 18.33 |
| | Max. Vy | 15 | 476.67 | -0.03 | 64.91 |
| | Min. Vert | 21 | -338.49 | -0.03 | 1.40 |
| | Min. Hx | 18 | -338.49 | -0.03 | 1.40 |

Tower Mast Reaction Summary

| Load Combination | Vertical | Shear | Shear | Overturning Moment | Overturning Moment | Temp |
|-----------------------------|----------|--------|--------|--------------------|--------------------|-------|
| | K | K | K | kip-ft | kip-ft | in-lb |
| Dead Only | 43.20 | 0.00 | 0.00 | 0.44 | 0.41 | 0.00 |
| Dead Wind 0 deg - No Ice | 49.20 | -0.02 | -0.02 | 4182.49 | 5.14 | -0.97 |
| Dead Wind 30 deg - No Ice | 49.20 | 22.45 | -33.96 | -3328.24 | -0.15 | -0.15 |
| Dead Wind 60 deg - No Ice | 49.20 | 38.17 | -22.29 | -2015.59 | -0.71 | -0.71 |
| Dead Wind 90 deg - No Ice | 49.20 | 44.93 | 0.00 | 3.16 | -6959.08 | 1.38 |
| Dead Wind 120 deg - No Ice | 49.20 | 33.92 | 23.09 | 3095.41 | -3349.43 | 1.63 |
| Dead Wind 150 deg - No Ice | 49.20 | 22.45 | 31.88 | 5791.87 | -3031.72 | 1.33 |
| Dead Wind 180 deg - No Ice | 43.20 | 0.02 | 0.02 | 44.61 | 604.07 | -0.31 |
| Dead Wind 210 deg - No Ice | 49.20 | -0.43 | 21.96 | 3357.15 | 3036.07 | 0.13 |
| Dead Wind 240 deg - No Ice | 49.20 | -33.99 | 33.96 | 3099.30 | 3345.24 | -0.71 |
| Dead Wind 270 deg - No Ice | 49.20 | -44.93 | -0.00 | -1.28 | 6099.81 | -1.31 |
| Dead Wind 300 deg - No Ice | 49.20 | -33.99 | -22.32 | -3720.77 | 3217.18 | -1.48 |
| Dead Wind 330 deg - No Ice | 49.20 | -22.45 | -33.98 | -1841.00 | 3324.25 | -1.53 |
| Dead Ice Temp | 118.41 | -6.00 | 0.00 | 1.17 | 0.04 | 0.00 |
| Dead Wind 0 deg Ice Temp | 118.41 | -69.21 | -79.49 | -8324.34 | 5.49 | -1.11 |
| Dead Wind 30 deg Ice Temp | 118.41 | 33.20 | -56.81 | -7920.28 | -2274.60 | -0.17 |
| Dead Wind 60 deg Ice Temp | 118.41 | 54.25 | -34.34 | -4133.06 | -7196.14 | 0.35 |
| Dead Wind 90 deg Ice Temp | 118.41 | 61.01 | 0.00 | 5.71 | -6158.00 | 1.65 |
| Dead Wind 120 deg Ice Temp | 118.41 | 41.10 | 33.32 | 4539.55 | -3032.33 | 2.00 |
| Dead Wind 150 deg Ice Temp | 118.41 | 33.33 | 56.82 | 7222.16 | -7882.46 | 1.82 |
| Dead Wind 180 deg Ice Temp | 118.41 | 0.02 | 61.72 | 9727.49 | -3.40 | 1.15 |
| Dead Wind 210 deg Ice Temp | 118.41 | -33.20 | 36.61 | 7222.61 | 4776.18 | 0.77 |
| Dead Wind 240 deg Ice Temp | 118.41 | -61.08 | 35.29 | 4852.09 | 8026.66 | -0.33 |
| Dead Wind 270 deg Ice Temp | 118.41 | -64.83 | -0.02 | -3.32 | 8359.89 | -1.63 |
| Dead Wind 300 deg Ice Temp | 118.41 | -34.27 | -31.38 | -1818.99 | -2052.57 | -2.00 |
| Dead Wind 330 deg Ice Temp | 118.41 | -22.45 | -66.03 | -7242.92 | -4294.35 | -1.12 |
| Dead Wind 0 deg - Service | 49.20 | -0.01 | -22.99 | -3392.31 | 2.77 | -0.41 |
| Dead Wind 30 deg - Service | 49.20 | 11.19 | -18.41 | -7418.83 | -1502.18 | -0.07 |
| Dead Wind 60 deg - Service | 49.20 | 22.29 | -11.21 | -2995.59 | 0.26 | 0.26 |
| Dead Wind 90 deg - Service | 49.20 | 22.19 | 0.00 | 2.79 | -3516.85 | 0.59 |
| Dead Wind 120 deg - Service | 49.20 | 19.89 | 11.31 | 1344.10 | -2655.23 | 0.81 |
| Dead Wind 150 deg - Service | 49.20 | 11.20 | 18.43 | 2622.55 | -1511.23 | 0.74 |
| Dead Wind 180 deg - Service | 49.20 | 0.81 | 22.32 | 3097.12 | -1.84 | 0.44 |
| Dead Wind 210 deg - Service | 49.20 | -11 | | | | |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
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| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |

| Section No. | Elevation | Area | Deflection | Gov. Load Comp. | Tilt | Tors |
|-------------|-----------|-------|------------|-----------------|--------|------|
| T1 | 100-83 | 1.713 | 27 | 0.1369 | 0.0059 | |
| T2 | 83-60 | 1.684 | 27 | 0.1318 | 0.0065 | |
| T10 | 83-40 | 0.561 | 27 | 0.0220 | 0.0021 | |
| T11 | 40-20 | 0.269 | 27 | 0.0159 | 0.0021 | |
| T12 | 20-0 | 0.611 | 27 | 0.0253 | 0.0021 | |

Critical Deflections and Radius of Curvature - Service Wind

| Elevation | Appearance | Gov. Load Comp. | Deflection | Tilt | Tors | Radius of Curvature |
|-----------|-------------------|-----------------|------------|--------|--------|---------------------|
| 240.00 | Boxed | 27 | 14.468 | 0.0776 | 0.0000 | 41113 |
| 221.00 | W/OP (2.11' x 12) | 27 | 11.772 | 0.6609 | 0.0204 | 16318 |
| 218.00 | W/OP (2.11' x 12) | 27 | 11.293 | 0.4310 | 0.0023 | 14815 |
| 198.00 | (2) 2720.60 | 27 | 8.553 | 0.5311 | 0.0211 | 16133 |

Maximum Tower Deflections - Design Wind

| Section No. | Elevation | Area | Gov. Load Comp. | Tilt | Tors |
|-------------|-----------|--------|-----------------|--------|--------|
| T1 | 240-220 | 41.008 | 15 | 1.9015 | 0.0011 |
| T2 | 220-200 | 34.648 | 15 | 1.8128 | 0.0406 |
| T3 | 200-180 | 28.781 | 15 | 1.5781 | 0.0310 |
| T4 | 180-160 | 25.604 | 15 | 1.3565 | 0.0181 |
| T5 | 160-140 | 11.695 | 15 | 1.0180 | 0.0087 |
| T6 | 140-120 | 11.326 | 15 | 0.8907 | 0.0024 |
| T7 | 120-100 | 3.715 | 15 | 0.6984 | 0.0012 |
| T8 | 100-83 | 5.339 | 15 | 0.5275 | 0.0012 |
| T9 | 83-60 | 3.270 | 15 | 0.4011 | 0.0011 |
| T10 | 60-40 | 1.315 | 15 | 0.2760 | 0.0007 |
| T11 | 40-20 | 0.218 | 15 | 0.1772 | 0.0004 |
| T12 | 20-0 | 0.177 | 15 | 0.0779 | 0.0002 |

Critical Deflections and Radius of Curvature - Design Wind

| Elevation | Appearance | Gov. Load Comp. | Deflection | Tilt | Tors | Radius of Curvature |
|-----------|-------------------|-----------------|------------|--------|--------|---------------------|
| 240.00 | Boxed | 15 | 48.006 | 1.9000 | 0.0091 | 27117 |
| 221.00 | W/OP (2.11' x 12) | 15 | 34.433 | 1.8186 | 0.0500 | 7220 |
| 218.00 | W/OP (2.11' x 12) | 15 | 31.278 | 1.7019 | 0.0415 | 4368 |
| 198.00 | (2) 2720.60 | 15 | 24.693 | 1.5502 | 0.0700 | 3381 |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1145 Palco Dr. Plymouth, NY Phone: (517) 936-4331 FAX: (517) 936-4338 | Job | 284859 | Page | 103 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |

| Section No. | Elevation | Sec | L | L _a | K1* | F _a | A | Actual P | Allow. P _a | Ratio |
|-------------|-----------|--|-------|----------------|------|----------------|---------|----------|-----------------------|-------|
| T1 | 240-220 | P-2.50' - 0.75' conn-20' C (Prod 225180) | 20.00 | 4.90 | 62.0 | 32.571 | 1.7040 | -28.63 | 31.12 | 0.920 |
| T2 | 220-200 | P-4.00' - 0.75' conn-20' C-Truss 48-48 (Prod 325181) | 20.00 | 4.67 | 53.8 | 21.877 | 1.7141 | -76.59 | 75.79 | 1.011 |
| T3 | 200-180 | P-3.00' - 0.75' conn-18' conn-20' C (Prod 225200) | 20.00 | 6.61 | 41.7 | 25.451 | 4.2099 | -126.82 | 109.44 | 1.139 |
| T4 | 180-160 | P-4.00' - 0.75' conn-48D-Truss-20' C (Prod 325177) | 20.00 | 6.41 | 33.7 | 26.422 | 3.5813 | -162.57 | 147.47 | 1.335 |
| T5 | 160-140 | #1220-11 - 1.50' - 1.00' conn. (Prod 194051) | 20.00 | 10.03 | 35.7 | 38.221 | 3.3014 | -200.84 | 160.28 | 1.354 |
| T6 | 140-120 | #1220-11 - 1.75' - 1.00' conn. TR-4 (Prod 192113) | 20.00 | 10.02 | 36.6 | 31.058 | 7.2151 | -239.94 | 224.19 | 1.070 |
| T7 | 120-100 | #1220-11 - 1.75' - 1.00' conn. (Prod 192117) | 20.00 | 10.03 | 36.6 | 31.069 | 7.2119 | -280.03 | 224.19 | 1.260 |
| T8 | 100-80 | #1220-11 - 2.00' - 0.8175' conn. TR-3 (Prod 194617) | 20.00 | 20.63 | 42.3 | 32.775 | 9.4248 | -205.14 | 262.71 | 1.166 |
| T9 | 83-60 | #1220-11 - 2.00' - 0.8175' conn. (Prod 194619) | 20.00 | 20.63 | 42.8 | 21.775 | 9.4248 | -346.32 | 261.77 | 1.315 |
| T10 | 60-40 | #1220-11 - 2.25' - 0.8175' conn. (Prod 194620) | 20.00 | 20.63 | 48.8 | 27.748 | 11.9282 | -384.10 | 331.45 | 1.159 |
| T11 | 40-20 | #1220-11 - 2.25' - 0.8175' conn. (Prod 194625) | 20.00 | 20.63 | 41.8 | 22.781 | 11.9381 | -431.00 | 331.86 | 1.276 |
| T12 | 20-0 | #1220-11 - 2.50' - 0.8175' conn. TR-4 (Prod 192948) | 20.00 | 20.63 | 47.7 | 22.303 | 14.7282 | -458.03 | 359.43 | 1.120 |

Truss-Leg Diagonal Data

| Section No. | Elevation | Diagonal Sec | L | L _a | K1* | F _a | A | Actual P | Allow. P _a | Ratio |
|-------------|-----------|--------------|------|----------------|--------|----------------|------|----------|-----------------------|-------|
| T3 | 160-140 | 0.3 | 1.43 | 95.3 | 11.573 | 0.1963 | 1.34 | 3.03 | 0.475 | 0.634 |
| T6 | 140-120 | 0.3 | 1.40 | 94.4 | 13.679 | 0.1963 | 1.39 | 3.11 | 0.417 | 0.417 |
| T7 | 120-100 | 0.3 | 1.40 | 94.4 | 13.679 | 0.1963 | 1.39 | 3.11 | 0.417 | 0.417 |
| T8 | 100-80 | 0.5 | 1.39 | 93.2 | 13.816 | 0.1963 | 1.47 | 3.15 | 0.310 | 0.310 |
| T9 | 80-60 | 0.5 | 1.39 | 93.2 | 13.816 | 0.1963 | 2.87 | 3.15 | 0.633 | 0.633 |
| T10 | 60-40 | 0.3 | 1.38 | 92.4 | 13.917 | 0.1963 | 1.75 | 3.17 | 0.511 | 0.511 |
| T11 | 40-20 | 0.3 | 1.38 | 92.4 | 13.917 | 0.1963 | 1.72 | 3.17 | 0.510 | 0.510 |
| T12 | 20-0 | 0.3 | 1.36 | 91.6 | 14.013 | 0.1963 | 1.34 | 3.19 | 0.421 | 0.421 |

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1145 Palco Dr. Plymouth, NY Phone: (517) 936-4331 FAX: (517) 936-4338 | Job | 284859 | Page | 102 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |

Bolt Design Data

| Section No. | Elevation | Component Type | Bolt Grade | Bolt Size | Number of Bolts | Maximum Load per Bolt | Allowable Load | Ratio | Allowable Ratio | Crane |
|-------------|-----------|----------------|------------|-----------|-----------------|-----------------------|----------------|-------|-----------------|-------|
| T1 | 240 | Leg | A325N | 0.7500 | 4 | 4.81 | 19.44 | 0.238 | ✓ | 1.333 |
| | | Diagonal | A325N | 0.7500 | 1 | 3.70 | 4.44 | 0.833 | ✓ | 1.333 |
| | | Top Girt | A325N | 0.7500 | 1 | 0.92 | 5.03 | 0.184 | ✓ | 1.333 |
| T2 | 220 | Leg | A325N | 0.7500 | 6 | 10.28 | 19.44 | 0.514 | ✓ | 1.333 |
| | | Diagonal | A325N | 0.7500 | 1 | 7.21 | 8.02 | 0.900 | ✓ | 1.333 |
| T3 | 200 | Leg | A325N | 0.7500 | 8 | 12.82 | 19.44 | 0.660 | ✓ | 1.333 |
| | | Diagonal | A325N | 0.7500 | 1 | 5.48 | 6.66 | 0.823 | ✓ | 1.333 |
| T4 | 180 | Leg | A325N | 1.0000 | 6 | 22.39 | 34.56 | 0.648 | ✓ | 1.333 |
| | | Diagonal | A325N | 0.7500 | 1 | 3.32 | 1.02 | 0.665 | ✓ | 1.333 |
| T5 | 160 | Leg | A325N | 1.0000 | 6 | 26.83 | 34.56 | 0.732 | ✓ | 1.333 |
| | | Diagonal | A325N | 1.0000 | 1 | 6.85 | 7.77 | 0.811 | ✓ | 1.333 |
| T6 | 140 | Leg | A325N | 1.2500 | 6 | 30.90 | 58.99 | 0.512 | ✓ | 1.333 |
| | | Diagonal | A325N | 1.0000 | 1 | 7.00 | 7.77 | 0.901 | ✓ | 1.333 |
| T7 | 120 | Leg | A325N | 1.2500 | 8 | 33.47 | 31.99 | 0.957 | ✓ | 1.333 |
| | | Diagonal | A325N | 1.0000 | 1 | 7.97 | 12.53 | 0.615 | ✓ | 1.333 |
| T8 | 100 | Leg | A325N | 1.0000 | 12 | 19.14 | 34.56 | 0.554 | ✓ | 1.333 |
| | | Diagonal | A325N | 0.7500 | 1 | 11.24 | 16.31 | 0.689 | ✓ | 1.333 |
| T9 | 80 | Leg | A325N | 1.0000 | 12 | 21.32 | 34.56 | 0.623 | ✓ | 1.333 |
| | | Diagonal | A325N | 0.7500 | 1 | 11.49 | 16.31 | 0.704 | ✓ | 1.333 |
| T10 | 60 | Leg | A325N | 1.0000 | 12 | 23.28 | 34.56 | 0.677 | ✓ | 1.333 |
| | | Diagonal | A325N | 0.7500 | 1 | 12.74 | 25.26 | 0.505 | ✓ | 1.333 |
| T11 | 40 | Leg | A325N | 1.0000 | 12 | 25.63 | 34.56 | 0.742 | ✓ | 1.333 |
| | | Diagonal | A325N | 0.7500 | 1 | 18.40 | 28.24 | 0.652 | ✓ | 1.333 |
| T12 | 20 | Leg | F1554-10 | 1.2500 | 12 | 27.13 | 50.67 | 0.536 | ✓ | 1.333 |
| | | Diagonal | A325N | 0.7500 | 1 | 14.31 | 25.26 | 0.577 | ✓ | 1.333 |

Compression Checks

Leg Design Data (Compression)

| | | | | |
|---|---------|---------------------------|-------------|-------------------|
| inxTower 1145 Palco Dr. Plymouth, NY Phone: (517) 936-4331 FAX: (517) 936-4338 | Job | 284859 | Page | 104 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:15:37 03/30/16 |
| | Client | Verizon Wireless | Designed by | JAK |

Diagonal Design Data (Compression)

| Section No. | Elevation | Sec | L | L _a | K1* | F _a | A | Actual P | Allow. P _a | Ratio |
|-------------|-----------|-------------------|-------|----------------|-------|----------------|-------|----------|-----------------------|-------|
| T1 | 240-220 | L3x3x1/2 | 2.32 | 2.72 | 91.8 | 13.713 | 0.614 | -2.53 | 6.61 | 0.311 |
| T2 | 220-200 | L3 1/2x2 1/2x3/16 | 7.17 | 7.52 | 91.8 | 13.994 | 0.900 | -7.84 | 12.62 | 0.613 |
| T3 | 200-180 | L2x3x3/16 | 8.13 | 8.07 | 91.8 | 12.8 | 0.917 | 0.719 | -5.21 | 6.29 |
| T4 | 180-160 | L2 1/2x2 1/2x3/16 | 9.04 | 4.54 | 112.0 | 13.320 | 0.920 | -1.69 | 11.23 | 0.511 |
| T5 | 160-140 | L3x3x3/16 | 12.65 | 6.43 | 129.5 | 8.901 | 1.090 | -4.86 | 5.70 | 0.707 |
| T6 | 140-120 | L3x3x3/16 | 14.19 | 7.14 | 148.2 | 7.226 | 1.090 | -7.83 | 7.89 | 0.893 |
| T7 | 120-100 | L3x3x3/16 | 14.87 | 7.52 | 152.3 | 6.362 | 1.700 | -8.43 | 11.32 | 0.743 |
| T8 | 100-80 | 2L3x3x3/16 | 21.79 | 12.45 | 159.1 | 4.899 | 2.100 | -12.73 | 15.86 | 0.990 |
| T9 | 80-60 | 2L3x3x3/16 | 23.03 | 13.97 | 165.4 | 3.939 | 2.180 | -12.77 | 11.76 | 1.044 |
| T10 | 60-40 | 2L3 1/2x3 1/2x1/4 | 26.26 | 16.61 | 150.1 | 4.029 | 3.370 | -12.16 | 22.31 | 0.544 |
| T11 | 40-20 | 2L3 1/2x3 1/2x1/4 | 27.77 | 14.33 | 157.3 | 4.017 | 3.370 | -15.43 | 20.31 | 0.661 |
| T12 | 20-0 | 2L3 1/2x3 1/2x1/4 | 29.25 | 15.04 | 164.4 | 3.431 | 3.370 | -13.43 | 18.43 | 0.729 |

Top Girt Design Data (Compression)

| Section No. | Elevation | Sec | L | L _a | K1* | F _a | A | Actual P | Allow. P _a | Ratio |
|-------------|-----------|-----------|------|----------------|-------|----------------|--------|----------|-----------------------|-------|
| T1 | 240-220 | L2x2x3/16 | 5.00 | 4.47 | 136.3 | 1.091 | 0.7150 | -6.83 | 5.31 | 0.111 |

Tension Checks

Leg Design Data (Tension)

| Section No. | Elevation | Sec | L | L _a | K1* | F _a | A | Actual P | Allow. P _a | Ratio |
|-------------|-----------|--|-------|----------------|------|----------------|--------|----------|-----------------------|-------|
| T1 | 240-220 | P-3.30' - 0.75' conn-20' C (Prod 225180) | 20.00 | 4.90 | 62.0 | 32.500 | 1.7040 | 19.24 | 51.12 | 0.311 |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 1343 Potosi Dr. Plymouth, VT Phone: (878) 856-4311 FAX: (878) 856-6458 | Job | 284859 | Page | 105 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| Section No. | Elevation | Size | L | L _u | K ₁ | F _a | A | Actual P | Allow. P | Ratio |
|-------------|-----------|--|-------|----------------|----------------|----------------|-----------------|----------|----------|----------------------|
| ft | ft | ft | ft | ft | ksi | ksi | in ² | k | k | P/P _{allow} |
| T2 | 220-200 | P-400 ⁺ -0.31 ⁺ conn-20 ⁺ -C-Deck-43-43-(Prod 221141) | 20.00 | 6.67 | 31.0 | 30.000 | 3.3141 | 51.45 | 51.23 | 0.658 |
| T3 | 200-180 | P-400 ⁺ -0.31 ⁺ conn-Trans-20 ⁺ -C-(Prod 221141) | 20.01 | 6.68 | 31.7 | 30.000 | 4.2999 | 102.99 | 120.00 | 0.795 |
| T4 | 180-160 | P-400 ⁺ -0.31 ⁺ conn-42B0-Trans-20 ⁺ -C-(Prod 221141) | 20.03 | 6.68 | 31.7 | 30.000 | 3.5115 | 134.31 | 107.44 | 0.802 |
| T5 | 160-140 | #1220-18-1.50 ⁺ -1.00 ⁺ conn-(Prod 195951) | 20.03 | 10.02 | 33.7 | 34.800 | 5.3014 | 151.08 | 114.67 | 0.527 |
| T6 | 140-120 | #1220-18-1.75 ⁺ -1.00 ⁺ conn-TR14-(Prod 195951) | 20.03 | 10.02 | 30.6 | 34.800 | 7.2158 | 165.40 | 251.12 | 0.738 |
| T7 | 120-100 | #1220-18-1.75 ⁺ -1.00 ⁺ conn-(Prod 195951) | 20.03 | 10.02 | 26.6 | 34.800 | 7.2158 | 212.84 | 251.12 | 0.848 |
| T8 | 100-80 | #1220-18-2.00 ⁺ -0.813 ⁺ conn-TR3-(Prod 195951) | 20.03 | 20.03 | 48.8 | 34.800 | 9.4248 | 229.71 | 327.98 | 0.700 |
| T9 | 80-60 | #1220-18-2.00 ⁺ -0.813 ⁺ conn-(Prod 195951) | 20.03 | 20.03 | 48.8 | 34.800 | 9.4241 | 251.10 | 327.98 | 0.787 |
| T10 | 60-40 | #1220-18-2.25 ⁺ -0.813 ⁺ conn-(Prod 195951) | 20.03 | 20.03 | 48.8 | 34.800 | 11.9283 | 280.37 | 415.10 | 0.678 |
| T11 | 40-20 | #1220-18-2.25 ⁺ -0.813 ⁺ conn-(Prod 195951) | 20.03 | 20.03 | 48.8 | 34.800 | 11.9282 | 301.52 | 415.10 | 0.741 |
| T12 | 20-0 | #1220-18-2.50 ⁺ -0.813 ⁺ conn-TR4-(Prod 195951) | 20.03 | 20.03 | 48.7 | 34.800 | 14.7252 | 325.55 | 513.47 | 0.633 |

Truss-Leg Diagonal Data

| Section No. | Elevation | Diagonal Size | L | K ₁ | F _a | A | Actual P | Allow. P | Ratio |
|-------------|-----------|---------------|------|----------------|----------------|-----------------|----------|----------|----------------------|
| ft | ft | ft | ft | ksi | ksi | in ² | k | k | P/P _{allow} |
| T3 | 180-140 | 0.5 | 1.42 | 99.2 | 11.573 | 0.1993 | 1.48 | 3.01 | 0.475 |
| T6 | 140-120 | 0.5 | 1.40 | 94.4 | 13.679 | 0.1963 | 1.19 | 3.11 | 0.384 |
| T7 | 120-100 | 0.5 | 1.40 | 94.4 | 13.679 | 0.1963 | 1.20 | 3.11 | 0.417 |
| T8 | 100-80 | 0.5 | 1.39 | 93.2 | 13.816 | 0.1963 | 1.67 | 3.15 | 0.520 |
| T9 | 80-60 | 0.5 | 1.39 | 93.2 | 13.816 | 0.1963 | 2.07 | 3.15 | 0.651 |
| T10 | 60-40 | 0.5 | 1.31 | 92.4 | 13.917 | 0.1963 | 1.75 | 3.17 | 0.551 |
| T11 | 40-20 | 0.5 | 1.38 | 92.4 | 15.813 | 0.1963 | 1.72 | 3.17 | 0.542 |
| T12 | 20-0 | 0.5 | 1.36 | 91.6 | 14.615 | 0.1993 | 1.34 | 3.19 | 0.413 |

| | | | | |
|--|---------|---------------------------|-------------|-------------------|
| inxTower 1343 Potosi Dr. Plymouth, VT Phone: (878) 856-4311 FAX: (878) 856-6458 | Job | 284859 | Page | 107 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

| Section No. | Elevation | Component Type | Size | Critical Element | P | U ² /P _{allow} | N Capacity | Pass/Fail | | |
|-------------|-----------|----------------|---|------------------|---------|------------------------------------|------------|---------------|------|------|
| T5 | 160-140 | Leg | #1220-18-1.50 ⁺ -1.00 ⁺ conn-(Prod 195951) | 95 | -100.81 | 210.07 | 94.0 | Pass | | |
| T6 | 140-120 | Leg | #1220-18-1.75 ⁺ -1.00 ⁺ conn-TR14-(Prod 195951) | 111 | -239.94 | 299.84 | 84.3 | Pass | | |
| T7 | 120-100 | Leg | #1220-18-1.75 ⁺ -1.00 ⁺ conn-(Prod 195951) | 126 | -240.02 | 298.84 | 93.7 | Pass | | |
| T8 | 100-80 | Leg | #1220-18-2.00 ⁺ -0.813 ⁺ conn-TR3-(Prod 195951) | 141 | -305.14 | 348.54 | 97.4 | Pass | | |
| T9 | 80-60 | Leg | #1220-18-2.00 ⁺ -0.813 ⁺ conn-(Prod 195951) | 150 | -346.22 | 348.94 | 99.2 | Pass | | |
| T10 | 60-40 | Leg | #1220-18-2.25 ⁺ -0.813 ⁺ conn-(Prod 195951) | 159 | -384.10 | 441.84 | 85.9 | Pass | | |
| T11 | 40-20 | Leg | #1220-18-2.25 ⁺ -0.813 ⁺ conn-(Prod 195951) | 163 | -421.00 | 441.84 | 93.3 | Pass | | |
| T12 | 20-0 | Leg | #1220-18-2.50 ⁺ -0.813 ⁺ conn-TR4-(Prod 195951) | 177 | -451.62 | 545.79 | 14.0 | Pass | | |
| T2 | 220-200 | Diagonal | L2x2x1/8 | 11 | -3.53 | 8.88 | 39.9 | Pass | | |
| T3 | 200-180 | Diagonal | L2 1/2x2 1/2x3/16 | 35 | -7.84 | 16.83 | 46.6 | Pass | | |
| T4 | 180-160 | Diagonal | L2x2x3/16 | 56 | -5.24 | 9.26 | 67.5 (6) | Pass | | |
| T5 | 160-140 | Diagonal | L2 1/2x2 1/2x3/16 | 81 | -5.69 | 13.61 | 81.0 (6) | Pass | | |
| T6 | 140-120 | Diagonal | L3x3x3/16 | 98 | -6.84 | 12.97 | 93.1 (6) | Pass | | |
| T7 | 120-100 | Diagonal | L3x3x3/16 | 113 | -7.03 | 10.30 | 64.1 (5) | Pass | | |
| T8 | 100-80 | Diagonal | L3x3x3/16 | 134 | -8.42 | 15.09 | 55.3 | Pass | | |
| T9 | 80-60 | Diagonal | L3x3x3/16 | 143 | -12.71 | 17.34 | 74.3 | Pass | | |
| T10 | 60-40 | Diagonal | L3x3x3/16 | 152 | -12.27 | 13.07 | 78.3 | Pass | | |
| T11 | 40-20 | Diagonal | L3 1/2x3 1/2x1/4 | 161 | -12.16 | 26.82 | 40.8 | Pass | | |
| T12 | 20-0 | Diagonal | L3 1/2x3 1/2x1/4 | 170 | -13.45 | 27.07 | 49.6 | Pass | | |
| T13 | 20-0 | Diagonal | L3 1/2x3 1/2x1/4 | 179 | -13.40 | 24.25 | 34.7 | Pass | | |
| T2 | 220-200 | Top Girt | L2x2x3/16 | 5 | -8.15 | 7.81 | 12.1 (3) | Pass | | |
| Summary | | | | | | | | | | |
| | | | | | | | | Leg (TP) | 99.2 | Pass |
| | | | | | | | | Diagonal (TP) | 78.3 | Pass |
| | | | | | | | | Top Girt (TP) | 13.1 | Pass |
| | | | | | | | | (TI) | 67.6 | Pass |
| | | | | | | | | Brk Checks | 99.2 | Pass |
| | | | | | | | | RATING = | 99.2 | Pass |

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|--|---------|---------------------------|-------------|-------------------|
| inxTower 1343 Potosi Dr. Plymouth, VT Phone: (878) 856-4311 FAX: (878) 856-6458 | Job | 284859 | Page | 106 of 107 |
| | Project | V-25 x 240' - Ashford, CT | Date | 16:16:37 03/30/15 |
| | Client | Verizon Wireless | Designed by | JAK |

Diagonal Design Data (Tension)

| Section No. | Elevation | Size | L | L _u | K ₁ | F _a | A | Actual P | Allow. P | Ratio |
|-------------|-----------|-------------------|-------|----------------|----------------|----------------|-----------------|----------|----------|----------------------|
| ft | ft | ft | ft | ft | ksi | ksi | in ² | k | k | P/P _{allow} |
| T2 | 220-200 | L2x2x1/8 | 5.12 | 2.72 | 35.8 | 28.000 | 0.2113 | 3.70 | 8.16 | 0.453 |
| T3 | 200-180 | L2x2x3/16 | 7.66 | 3.85 | 38.4 | 28.000 | 0.4132 | 3.41 | 13.98 | 0.418 |
| T4 | 180-160 | L2 1/2x2 1/2x3/16 | 9.60 | 4.50 | 36.9 | 28.000 | 0.5355 | 5.82 | 15.03 | 0.391 |
| T5 | 160-140 | L3x3x3/16 | 12.61 | 6.40 | 34.7 | 28.000 | 0.6389 | 6.48 | 19.12 | 0.338 |
| T6 | 140-120 | L3x3x3/16 | 14.10 | 7.14 | 33.7 | 28.000 | 0.6593 | 7.00 | 19.12 | 0.356 |
| T7 | 120-100 | L3x3x3/16 | 15.67 | 7.91 | 30.5 | 28.000 | 1.0713 | 7.97 | 31.07 | 0.256 |
| T8 | 100-80 | L3x3x3/16 | 23.79 | 12.43 | 36.5 | 28.000 | 1.3337 | 11.24 | 39.26 | 0.335 |
| T9 | 80-60 | L3x3x3/16 | 25.61 | 13.81 | 36.8 | 28.000 | 1.3337 | 11.49 | 39.26 | 0.283 |
| T10 | 60-40 | L3 1/2x3 1/2x1/4 | 26.36 | 13.45 | 32.1 | 28.000 | 2.1953 | 12.74 | 62.53 | 0.204 |
| T11 | 40-20 | L3 1/2x3 1/2x1/4 | 27.77 | 14.53 | 35.0 | 28.000 | 2.1540 | 11.23 | 62.53 | 0.183 |
| T12 | 20-0 | L3 1/2x3 1/2x1/4 | 29.23 | 15.04 | 30.000 | 2.1543 | 14.58 | 62.53 | 0.233 | |

Top Girt Design Data (Tension)

| Section No. | Elevation | Size | L | L _u | K ₁ | F _a | A | Actual P | Allow. P | Ratio |
|-------------|-----------|-----------|------|----------------|----------------|----------------|-----------------|----------|----------|----------------------|
| ft | ft | ft | ft | ft | ksi | ksi | in ² | k | k | P/P _{allow} |
| T2 | 220-220 | L2x2x3/16 | 5.00 | 4.47 | 92.4 | 28.000 | 0.4132 | 0.92 | 11.98 | 0.077 |

Section Capacity Table

| Section No. | Elevation | Component Type | Size | Critical Element | P | U ² /P _{allow} | N Capacity | Pass/Fail |
|-------------|-----------|----------------|---|------------------|---------|------------------------------------|------------|-----------|
| T1 | 240-220 | Leg | P-250 ⁺ -0.75 ⁺ conn-20 ⁺ -C-(Prod 216160) | 1 | -25.43 | 50.82 | 32.1 | Pass |
| T2 | 220-200 | Leg | P-400 ⁺ -0.31 ⁺ conn-20 ⁺ -C-Trans-43-43-(Prod 221141) | 31 | -76.50 | 101.02 | 21.8 | Pass |
| T3 | 200-180 | Leg | P-400 ⁺ -0.31 ⁺ conn-Trans-20 ⁺ -C-(Prod 221141) | 32 | -126.82 | 145.88 | 86.9 | Pass |
| T4 | 180-160 | Leg | P-400 ⁺ -0.31 ⁺ conn-42B0-Trans-20 ⁺ -C-(Prod 221141) | 35 | -167.57 | 196.38 | 65.2 | Pass |

FOUNDATION NOTES

- 1 THE ON-SITE GEOTECHNICAL ENGINEER SHALL CONFIRM THAT THE INSITU SOIL STRENGTHS MEET OR EXCEED THOSE PARAMETERS GIVEN IN THE SOIL REPORT.
- 2 GRADE THE SITE TO DRAIN AWAY FROM FOUNDATION.
- 3 A SUMP PUMP OR OTHER DEWATERING SYSTEM MAY BE REQUIRED TO LOWER THE WATER TABLE TO FACILITATE THE INSTALLATION OF THE FOUNDATION.
- 4 ANY SOFT OR UNSTABLE SUBGRADE SOILS DETECTED DURING THE EXCAVATION SHOULD BE REMOVED AND REPLACED WITH COMPACTED FILL AS PER THE SPECIFICATIONS PROVIDED IN THE GEOTECHNICAL REPORT REFERENCED ABOVE (SEE SECTION 4.3.1.2).

UNIT BASE FOUNDATION (Load Case 2)

Verizon
Ashford, CT

V- 25.0 240
A- 284859

V.2.1

| Reactions | stress ratio | 100.0% | mark up: | 0.0% |
|--------------------------------|------------------|--------|------------------|------|
| Shear, S: | 84.00 kips | x 1 = | 84.00 kips | |
| Moment, M: | 11251.00 ft-kips | x 1 = | 11251.00 ft-kips | |
| Compression / leg, C: | 530.00 kips | x 1 = | 530.00 kips | |
| Uplift / leg, U: | 473.00 kips | x 1 = | 473.00 kips | |
| Tower weight, W _c : | 59.00 kips | = | 59.00 kips | |

Soil per: Terracon, Dated 02/23/15, Project#J2155118

Ultimate bearing: 10.000 ksf
Ultimate Pp: 0.125 kcf

Load Case 2 = 0.9*D + 1.0*Dg + 1.6*Wo

Physical Parameters:

| | | | | |
|------------------|--|------------------|--------|------|
| Concrete volume: | $V = T * W^2 + 3 * (d^2 / 4 * \pi) * (D + E - T)$ | V = | 76.2 | cy |
| Concrete weight: | $W_c = V * \delta$ | W _c = | 308.6 | kips |
| Soil weight: | $W_s = (D - T) * (W^2 - 3 * (d^2 / 4 * \pi)) * \gamma$ | W _s = | 628.5 | kips |
| Total weight: | $P = W_c + W_s + W_t$ | P = | 997.05 | kips |

Passive Pressure:

| | | | | |
|-----------------|--|-----------------------|---------|-----------------|
| Pp coefficient: | $K_p = \text{TAN}(45 + \phi / 2)^2$ | K _p = | 1.000 | |
| | $P_{pn} = K_p * \gamma * N + 2 * C_o * \sqrt{(K_p)}$ | P _{pn} = | 0.813 | ksf |
| | $P_{pt} = K_p * \gamma * (D - T) + 2 * C_o * \sqrt{(K_p)}$ | P _{pt} = | 0.594 | ksf |
| | $P_{pb} = K_p * \gamma * D + 2 * C_o * \sqrt{(K_p)}$ | P _{pb} = | 0.813 | ksf |
| | $P_{ptop} = \text{IF}(N < (D - T), P_{pt}, P_{pn})$ | P _{ptop} = | 0.8 | ksf |
| | $P_{pb} = (P_{ptop} + P_{pb}) / 2$ | P _{pb} ' = | 0.813 | ksf |
| Shear area: | $T_{pp} = 0$ | T _{pp} = | 0.0 | ft |
| | $A_{pp} = T_{pp} * W$ | A _{pp} = | 0.00 | ft ² |
| Shear Capacity: | $S_{actual} = (P_{pb}' * A_{pp} + \mu * P) * \phi_r$ | S _{actual} = | 149.557 | kips |
| $\phi_r = 0.75$ | | | | |

| | | | | |
|-------|-----------------------------------|----|----------------|----|
| Check | S _{actual} = 149.56 kips | >= | S = 84.00 kips | OK |
|-------|-----------------------------------|----|----------------|----|

Overturning Moment Resistance at Toe:

| | | | | |
|--------------------------|--|--------------------|----------|---------|
| Wt of soil wedge: | $W_{sw} = D * (D * \text{TAN}(\phi)) / 2 * W * \gamma$ | W _{sw} = | 0.0 | kips |
| Dist. from leg to edge: | $O = (W - 0.866 * w) / 2$ | O = | 5.675 | ft |
| Additional offset of Wt: | $O_a = (2 / 3 * 0.866 * w' + O) - W / 2$ | O _a = | 3.608 | ft |
| Resisting moments: | $M_{wt} = P * W / 2 - W_t * O_a$ | M _{wt} = | 16238.41 | ft-kips |
| | $M_{pp} = P_{pb}' * A_{pp} * (D - N) / 3$ | M _{pp} = | 0.00 | ft-kips |
| | $M_{msw} = W_{sw} * (W + D * \text{TAN}(\phi) / 3)$ | M _{msw} = | 0.00 | ft-kips |
| Total resisting: | $M_t = (M_{wt} + M_{pp} + M_{msw}) * \phi_r$ | M _t = | 12178.81 | ft-kips |
| $\phi_r = 0.75$ | | | | |
| Total overturning: | $M_o = M + S * (D + E)$ | M _o = | 11839.00 | ft-kips |

| | | | | |
|-------|-----------------------------------|----|-----------------------------------|----|
| Check | M _t = 12178.81 ft-kips | >= | M _o = 11839.00 ft-kips | OK |
|-------|-----------------------------------|----|-----------------------------------|----|

Bearing Resistance due to Pressure Distribution:

| | | | | |
|------------------------|---|--------------------|--------|-----------------|
| Area of mat: | $\text{area} = W^2$ | area = | 1089.0 | ft ² |
| Section modulus: | $SM = W^3 / 6$ | SM = | 5989.5 | ft ³ |
| Factored total weight: | $P' = W + 0.9 * (W_c + W_s)$ | P' = | 903.2 | kjp |
| Pressure exerted: | $P_{pos} = P' / \text{area} + M_o / SM$ | P _{pos} = | 2.806 | ksf |
| | $P_{neg} = P' / \text{area} - M_o / SM$ | P _{neg} = | -1.147 | ksf |

Note: The stress resultant is NOT within the kern. Bearing area has been adjusted below.

| | | | | |
|------------------------|---|--------------------|-------|-----|
| Load eccentricity: | $e_o = M_o / P'$ | e _o = | 13.11 | ft |
| | $P_{adj} = 2 * P' / (3 * W * (W / 2 - e_o))$ | P _{adj} = | 5.4 | ksf |
| Adj. applied pressure: | $q_a = \text{IF}(P_{neg} >= 0, P_{pos}, P_{adj})$ | q _a = | 5.378 | ksf |
| $\phi_r = 0.75$ | | | | |

| | | | | |
|-------|----------------------------|----|---------------------------------------|----|
| Check | q _a = 5.378 ksf | <= | B _c * ϕ_r = 7.500 ksf | OK |
|-------|----------------------------|----|---------------------------------------|----|

Concrete Shear Strength:

One way beam action at d₁ from tower

| | | | | |
|-------------------------------|--|-------------------|--------|------|
| Effective depth: | $d_e = T - cc - db_p / 2$ | d _e = | 17.500 | in |
| Factored Intensity: | $q_s = C / \text{area}$ | q _s = | 0.487 | ksf |
| Required shear: | $V_{n1} = q_s * (O - d_i / 2 - dc) * W / \phi_s$ | V _{n1} = | 52.82 | kips |
| $\phi_s = 0.75$ (ACI 9.3.2.3) | | | | |
| Available shear: | $V_{c1} = 2 * \sqrt{(F'c)} * W * dc$ | V _{c1} = | 929.76 | kips |
| (ACI 12.2.4) | | | | |

| | | | | |
|-------|-------------------------------|----|------------------------------|----|
| Check | V _{c1} = 929.76 kips | >= | V _{n1} = 52.82 kips | OK |
|-------|-------------------------------|----|------------------------------|----|

Two way beam action at $d_f / 2$ from tower

| | | | |
|--|--|-------------------|------|
| Parameter: | $P_o = (d_f + d_c) * \pi$ | $P_o = 15.58$ | ft |
| Required shear: $\phi_s = 0.75$ [ACI 9.3.2.3] | $V_{n2} = \phi_s / \phi_s * (\text{area} - (d_f + d_c) * \pi / 4)$ | $V_{n2} = 694.14$ | kips |
| Available shear: [ACI 12.2.2] | $V_{c2} = 4 * \sqrt{F_c} * P_o * d_c$ | $V_{c2} = 877.75$ | kips |

| | | | | |
|-------|------------------------|--------|------------------------|----|
| Check | $V_{c2} = 877.75$ kips | \geq | $V_{n2} = 694.14$ kips | OK |
|-------|------------------------|--------|------------------------|----|

Column Compression Capacity:

| | | | |
|--|--|----------------|------|
| Compression reaction: $\phi_c = 0.65$ [ACI 9.3.2.2] | $P_o = \phi_c * 0.8 * F_c * (d_f^2 / 4 * \pi)$ | $P_o = 3241.9$ | kips |
|--|--|----------------|------|

| | | | | |
|-------|----------------------|--------|-------------------|----|
| Check | $P_c = 3241.94$ kips | \geq | $C = 530.00$ kips | OK |
|-------|----------------------|--------|-------------------|----|

Pier Reinforcement:

| | | | |
|---|---------------------------|-------------------|-----------------|
| Cross-sectional area: | $A_g = d_f^2 * \pi / 4$ | $A_g = 1385.44$ | in ² |
| Min. area of steel (pier): [ACI 10.9.1] & [ACI 10.8.4] | $A_{st,c} = A_g * 0.005$ | $A_{st,c} = 6.93$ | in ² |
| Core circle: | $d_o = d_f - 2 * cc$ | $d_o = 36.00$ | in |
| Rebar: | $s_e = 9$ | $d_{b,c} = 1.128$ | in |
| | $m_c = 19$ | $A_{b,c} = 1$ | in ² |
| | $A_{s,c} = A_{b,c} * m_c$ | $A_{s,c} = 19.00$ | in ² |

| | | | | |
|-------|-----------------------------------|--------|-----------------------------------|----|
| Check | $A_{s,c} = 19.00$ in ² | \geq | $A_{st,c} = 6.93$ in ² | OK |
|-------|-----------------------------------|--------|-----------------------------------|----|

| | | | |
|-----------------------|---|----------------------|---------|
| Actual moment: | $M_{max} = (D - T + E) * S / 2$ | $M_{max} = 220.50$ | ft-kips |
| Pier moment capacity: | M_{allow} per Maxmomnt.xls (see attached) | $M_{allow} = 406.65$ | ft-kips |

| | | | | |
|-------|------------------------------|--------|----------------------------|----|
| Check | $M_{allow} = 406.65$ ft-kips | \geq | $M_{max} = 220.50$ ft-kips | OK |
|-------|------------------------------|--------|----------------------------|----|

| | | | |
|-----------------|--------------------------------------|------------------|----|
| Bar separation: | $B_{s,c} = (d_o * \pi) / m_c - db_c$ | $B_{s,c} = 4.82$ | in |
|-----------------|--------------------------------------|------------------|----|

| | | | | | | |
|-------|-------|--------|---------------------|--------|------|----|
| Check | 10.87 | \geq | $B_{s,c} = 4.82$ in | \geq | 4.5" | OK |
|-------|-------|--------|---------------------|--------|------|----|

Vertical Rebar Development Length:

| | | |
|---|---|---------------------------|
| Reinforcement location: [ACI 12.2.4] | $\psi_{l,c} =$ if the space under the rebar > 12 in, use 1.3, else use 1.0 | $\psi_{l,c} = 1.3$ |
| Epoxy coating: [ACI 12.2.4] | $\psi_{e,c} =$ if epoxy-coated bars are not used, use 1.0; but if epoxy-coated bars are used, then if $B_s < 6 * db$ or $cc < 3 * db$, use 1.5, else 1.2 | $\psi_{e,c} = 1.0$ |
| Max term: [ACI 12.2.4] | $\psi_1 \psi_{e,c} =$ the product of ψ_1 & $\psi_{e,c}$, need not be taken larger than 1.7 | $\psi_1 \psi_{e,c} = 1.3$ |
| Reinforcement size: [ACI 12.2.4] | $\psi_{s,c} =$ if the bar size is 6 or less, then use 0.8, else use 1.0 | $\psi_{s,c} = 1$ |
| Light weight concrete: [ACI 12.2.4] | $\lambda_c =$ if lightweight concrete is used, 1.3, else use 1.0 | $\lambda_c = 1.0$ |
| Spacing/cover: [ACI 12.2.4] | $c_c =$ the smaller of: half the bar spacing or the concrete edge distance | $c_c = 3.54$ in |
| Transverse bars: [ACI 12.2.3] | $k_{tr,c} = 0$ in (per simplification) | $k_{tr,c} = 0$ in |
| Max term: [ACI 12.2.3] | $c_c' = \text{MIN}(2.5, (c_c + k_{tr,c}) / db_c)$ | $c_c' = 2.500$ |
| Excess reinforcement: [ACI 12.2.5] | $R_o = M_{max} / M_{allow}$ | $R_o = 0.54$ |
| Development (tensile): [ACI 12.2.2] | $L_{d,c}^t = (3 / 40) * (F_y / \sqrt{F_c}) * (\psi_1 \psi_{e,c} * \psi_{s,c} * \lambda_c * R_o / c_c') * db_c$ | $L_{d,c}^t = 21.34$ in |
| Minimum length: [ACI 12.2.1] | $L_{d,min} = 12$ inches | $L_{d,min} = 12.0$ in |
| Development length: | $L_{d,c} = \text{MAX}(L_{d,min}, L_{d,c}^t)$ | $L_{d,c} = 21.34$ in |
| Development (comp.): [ACI 12.3.2] | $L_{d,c}^c = 0.02 * db_c * F_y * R_o / \sqrt{F_c}$ | $L_{d,c}^c = 10.94$ in |
| | $L_{dc,c}^c = 0.0003 * db_c * F_y * R_o$ | $L_{dc,c}^c = 11.01$ in |
| Development length: | $L_{dc,c} = \text{MAX}(8, L_{dc,c}^c, L_{d,c}^c)$ | $L_{dc,c} = 11.01$ in |
| Length available in pier: | $L_{vc} = D - T + E - cc$ | $L_{vc} = 60.0$ in |

| | | | | |
|-------|--------------------|--------|---------------------|----|
| Check | $L_{vc} = 60.0$ in | \geq | $L_{d,c} = 21.3$ in | OK |
|-------|--------------------|--------|---------------------|----|

| | | | | |
|-------|--------------------|--------|----------------------|----|
| Check | $L_{vc} = 60.0$ in | \geq | $L_{dc,c} = 11.0$ in | OK |
|-------|--------------------|--------|----------------------|----|

| | | | |
|--------------------------|-------------------|-----------------|----|
| Length available in pad: | $L_{vp} = T - cc$ | $L_{vp} = 18.0$ | in |
|--------------------------|-------------------|-----------------|----|

| | | | | |
|-------|--------------------|--------|---------------------|-------|
| Check | $L_{vp} = 18.0$ in | \geq | $L_{d,c} = 21.3$ in | HOOKS |
|-------|--------------------|--------|---------------------|-------|

| | | | | |
|-------|--------------------|--------|----------------------|----|
| Check | $L_{vp} = 18.0$ in | \geq | $L_{dc,c} = 11.0$ in | OK |
|-------|--------------------|--------|----------------------|----|

Vertical Rebar Hook Ending:

| | | |
|---|---|--------------------------|
| Bar size & clear cover: [ACI 12.6.3] | α_h if the bar size ≤ 11 and side cc $\geq 2.5'$, use 0.7, else use 1.0 | $\psi_{Lh} = 0.7$ |
| Epoxy coating: [ACI 12.6.2] | β_h if epoxy-coated bars are used, use 1.2, else use 1.0 | $\psi_{eh} = 1.0$ |
| Light weight concrete: [ACI 12.6.2] | λ_h if lightweight concrete is used, 1.3, else use 1.0 | $\lambda_h = 1.0$ |
| Development (hook): [ACI 12.5.2] | $L_{dh} = 0.02 \cdot \psi_{Lh} \cdot \psi_{eh} \cdot \lambda_h \cdot F_y / \sqrt{F_c} \cdot db_c$ | $L_{dh} = 14.1$ in |
| Minimum length: [ACI 12.6.1] | $L_{dh_{min}}$ the larger of: 8 * db or 8 in | $L_{dh_{min}} = 9.0$ in |
| Development length: | $L_{dh} = \text{MAX}(L_{dh_{min}}, L_{dh})$ | $L_{dh} = 14.1$ in |
| Hook tail length: | $L_{h_{tail}} = 12 \cdot db$ beyond the bend radius | $L_{h_{tail}} = 19.2$ in |
| Length available in pad: | $L_{h_{pad}} = (W - W' - d) / 2$ | $L_{h_{pad}} = 27$ in |
| | Check $L_{h_{pad}} = 27.0$ in \geq $L_{h_{tail}} = 19.2$ in OK | |
| | Check $L_{dp} = 18.0$ in \geq $L_{dh} = 14.1$ in OK | |

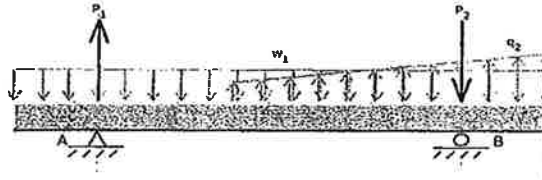
Pier Ties:

| | | |
|---|--|---------------------------------|
| Minimum size: [ACI 7.10.5.1] | $s_{t_{min}} = \text{IF}(s_c \leq 10, 3, 4)$ | $s_{t_{min}} = 3$ |
| z factor: | $z = 0.5$ if the seismic zone is less than 2, else 1.0 | $z = 1$ |
| Tie parameters: | $s_t = 4$ | $d_{s_t} = 0.5$ in |
| | $m_t = 10$ | $A_{s_t} = 0.2$ in ² |
| Allowable tie spacing: | | |
| per vertical rebar [ACI 7.10.5.2] & [ACI 21.3.3.2] | $B_{s_t_{max1}} = 8 / z \cdot db_c$ | $B_{s_t_{max1}} = 9.024$ in |
| per tie size [ACI 7.10.5.2] & [ACI 21.3.3.2] | $B_{s_t_{max2}} = 24 / z \cdot db_t$ | $B_{s_t_{max2}} = 12$ in |
| per pier diameter [ACI 7.10.5.2] & [ACI 21.3.3.2] | $B_{s_t_{max3}} = d / (4 \cdot z^2)$ | $B_{s_t_{max3}} = 10.5$ in |
| per seismic zone [ACI 7.10.5.2] & [ACI 21.3.3.2] | $B_{s_t_{max4}} = 12'$ in active seismic zones, else 18" | $B_{s_t_{max4}} = 12$ in |
| | $B_{s_t_{max}} = \text{MIN}(B_{s_t_{max1}}, B_{s_t_{max2}}, B_{s_t_{max3}}, B_{s_t_{max4}})$ | $B_{s_t_{max}} = 9.024$ in |
| | $m_{t_{min}} = (D - T + E) / B_{s_t_{max}} + 2$ | $m_{t_{min}} = 9.0$ |
| | Check $m_t = 10.0$ \geq $m_{t_{min}} = 9.0$ OK | |

Anchor Steel:

| | | |
|------------------------|---|----------------------------|
| A/S parameters: | $P_{ss} = 103183$ | $L_{ss} = 60$ in |
| | $d_{ss} = 1.25$ in | $E_{ss} = 51.50$ in |
| Development available: | L_{dss} per Anchor Bolts (see attached) | $L_{dss} = 41.50$ in |
| Required development: | $L_{dss_{min}}$ per Anchor Bolts (see attached) | $L_{dss_{min}} = 21.34$ in |
| | Check $L_{dss} = 41.50$ in \geq $L_{dss_{min}} = 21.34$ in OK | |
| To bottom rebar grid: | $E_{ss_{max}} = D + E - cc - 2 \cdot db_p$ | $E_{ss_{max}} = 79$ in |
| | Check $E_{ss} = 51.50$ in \leq $E_{ss_{max}} = 79.00$ in OK | |
| To top rebar grid: | rebar @ = D + E - T + cc | rebar @ = 66.00 in |
| | Check 66 + 6 in \geq $E_{ss} = 51.50$ in or \leq 66 in OK | |
| Min. cage dia: | $d_{o_{min}}$ per ancsteel.xls (see attached) | $d_{o_{min}} = 33.89$ in |
| | Check $d_o = 36.00$ in \geq $d_{o_{min}} = 33.89$ in OK | |

Pad Reactions:



MDSolids Geometry Input (Option 1)

Total Beam Length:

$$B_{L2,1} = W$$

$$B_{L2,1} = 33 \text{ ft}$$

Location of Left Support:

$$S_{L2,1} = 0$$

$$S_{L2,1} = 5.675 \text{ ft}$$

Location of Right Support:

$$S_{R2,1} = W - 0$$

$$S_{R2,1} = 27.33 \text{ ft}$$

MDSolids Geometry Input (Option 2)

Total Beam Length:

$$B_{L2,2} = W$$

$$B_{L2,2} = 33.0 \text{ ft}$$

Location of Left Support:

$$S_{L2,2} = (W - W) / 2$$

$$S_{L2,2} = 4.00 \text{ ft}$$

Location of Right Support:

$$S_{R2,2} = S_{L1,2} + W$$

$$S_{R2,2} = 29.00 \text{ ft}$$

MDSolids Load Input (Option 1 & Option 2)

Uplift:

$$P_{2,1} = U$$

$$P_{2,1} = 473.0 \text{ kips}$$

Compression:

$$P_{2,2} = C$$

$$P_{2,2} = 530.00 \text{ kips}$$

Weight of Overburden:
(Distributed)

$$W_{2,1} = 0.9 * (W_c + W_s) / W$$

$$W_{2,1} = 25.58 \text{ klf}$$

Applied over the beam starting at 0' and ending at W=33ft.

Distributed Soil Pressure:
(Linearly Increasing)

$$q_{2,2L} = 0$$

$$q_{2,2L} = 0.00 \text{ klf}$$

$$q_{2,2R} = q_{2,1} * W$$

$$q_{2,2R} = 177.48 \text{ klf}$$

This linearly increasing load is applied from e=13.1ft to W=33ft

MDSolids Design Result

Option 1:

$$M_{\text{max}2,1} = M_{\text{max}2,1} \text{ (Max. Moment calculated from MDSolids for Option 1)}$$

$$M_{\text{max}2,1} = 2175.00 \text{ ft*kips}$$

Option 2:

$$M_{\text{max}2,2} = M_{\text{max}2,2} \text{ (Max. Moment calculated from MDSolids for Option 2)}$$

$$M_{\text{max}2,2} = 1121.00 \text{ ft*kips}$$

Max moment:

$$M_{\text{maxp}} = \text{Max}(M_{\text{max}2,1}, M_{\text{max}2,2})$$

$$M_{\text{maxp}} = 2175.00 \text{ ft*kips}$$

Required moment:
 $\phi_t = 0.9$ [ACI 9.3.2.1]

$$M_n = M_{\text{maxp}} / \phi_t$$

$$M_n = 2416.67 \text{ ft*kips}$$

Pad Reinforcement:

| | | | |
|------------------|---|---|-----------|
| | $\beta = \text{IF}(F'c \leq 4000, 0.85, \text{IF}(F'c > 6000, 0.65, 0.85 - (F'c - 4000) * 0.05))$ | $\beta = 0.825$ | |
| Effective width: | $W_e = w * 0.866 + d_i$ | $W_e = 25.150 \text{ ft}$ | |
| | $A_{st,p} = Mn / (0.9 * F_y * dc)$ | $A_{st,p} = 30.688 \text{ in}^2$ | |
| Required steel: | $a_p = A_{st,p} * F_y / (\beta * F'c * W_e)$ | $a_p = 1.64 \text{ in}$ | |
| Shrinkage: | $A_{st,p,sh} = Mn / (F_y * (dc - a_p / 2)) * (W / W_e)$ | $A_{st,p,sh} = 38.025 \text{ in}^2$ | |
| | $\rho_{sh} = \text{IF}(F_y > 60000, 0.0018, 0.002)$ | $\rho_{sh} = 0.0018$ | |
| | $A_{st,p,sh} = \rho_{sh} * W * T / 2$ | $A_{st,p,sh} = 7.484 \text{ in}^2$ | |
| | $A_{st,p} = \text{MAX}(A_{st,p,sl}, A_{st,p,sh})$ | $A_{st,p} = 38.025 \text{ in}^2$ | |
| Rebar: | $s_p = 8$ Equally spaced, top and bottom, both directions. | $d_{b,p} = 1 \text{ in}$ $A_{b,p} = 0.79 \text{ in}^2$ | |
| | $m_p = 49$ | | |
| | $A_{s,p} = A_{b,p} * m_p$ | $A_{s,p} = 38.71 \text{ in}^2$ | |
| | Check $A_{s,p} = 38.71 \text{ in}^2 \geq A_{st,p} = 38.03 \text{ in}^2$ | | OK |
| Bar separation: | $B_{s,p} = (W - 2 * cc - db_p) / (m_p - 1) - db_p$ | $B_{s,p} = 7.10 \text{ in}$ | |
| | Check $11 \geq B_{s,p} = 7.10 \text{ in} \geq 4.5"$ | | OK |

Pad Development Length:

| | | | |
|---|--|-------------------------------|-----------|
| Reinforcement location: [ACI 12.2.4] | $\psi_{t,p} = \text{if the space under the rebar} > 12 \text{ in, use } 1.3, \text{ else use } 1.0$ | $\psi_{t,p} = 1.3$ | |
| Epoxy coating: [ACI 12.2.4] | $\psi_{e,p} = \text{if epoxy-coated bars are not used, use } 1.0; \text{ but if epoxy-coated bars are used, then if } B_s < 8 * db \text{ or } cc < 3 * db, \text{ use } 1.5, \text{ else } 1.2$ | $\psi_{e,p} = 1.0$ | |
| Max term: [ACI 12.2.4] | $\psi_i \psi_{e,p} = \text{the product of } \psi_t \text{ \& } \psi_e, \text{ need not be taken larger than } 1.7$ | $\psi_i \psi_{e,p} = 1.3$ | |
| Reinforcement size: [ACI 12.2.4] | $\psi_{s,p} = \text{if the bar size is } 6 \text{ or less, then use } 0.8, \text{ else use } 1.0$ | $\psi_{s,p} = 1$ | |
| Light weight concrete: [ACI 12.2.4] | $\lambda_p = \text{if lightweight concrete is used, } 1.3, \text{ else use } 1.0$ | $\lambda_p = 1.0$ | |
| Spacing/cover: [ACI 12.2.4] | $c_p = \text{the smaller of: half the bar spacing or the concrete edge distance}$ | $c_p = 3.50 \text{ in}$ | |
| Transverse bars: [ACI 12.2.3] | $k_{tr,p} = 0 \text{ in (per simplification)}$ | $k_{tr,p} = 0 \text{ in}$ | |
| Max term: [ACI 12.2.3] | $c_p' = \text{MIN}(2.5, (c_p + k_{tr,p}) / db_p)$ | $c_p' = 2.500$ | |
| Excess reinforcement: [ACI 12.2.5] | $R_p = A_{sl,p} / A_{s,p}$ | $R_p = 0.98$ | |
| Development (tensile): [ACI 12.2.2] | $L_d = (3 / 40) * (F_y / \sqrt{F'c}) * \psi_t \psi_{e,p} * \psi_s * \lambda_p * R_p * db_p / c_p'$ | $L_{dp}' = 34.3 \text{ in}$ | |
| Minimum length: [ACI 12.2.1] | $L_{d,min} = 12 \text{ inches}$ | $L_{d,min} = 12.0 \text{ in}$ | |
| Development length: | $L_{dp} = \text{MAX}(L_{d,min}, L_{dp}')$ | $L_{dp} = 34.3 \text{ in}$ | |
| Length available in pad: | $L_{pad} = (W / 2 - w / 2) - cc$ | $L_{pad} = 45.0 \text{ in}$ | |
| | Check $L_{pad} = 45.00 \text{ in} \geq L_{dp} = 34.27 \text{ in}$ | | OK |

**THIS SPREADSHEET IS SET UP FOR A MAXIMUM OF 56 BARS.
MAXIMUM FACTORED MOMENT OF A CIRCULAR SECTION**

| Loading | |
|----------------------------|-------------|
| (negative for compression) | |
| Axial load = | 473.00 kips |

| Foundation | |
|----------------------|------------------------|
| <i>Concrete</i> | |
| Pier diameter = | 3.50 ft |
| Pier area = | 1385.4 in ² |
| <i>Reinforcement</i> | |
| Clear cover = | 3.00 in |
| Cage diameter = | 2.91 ft |
| Bar size = | 9 |
| Bar diameter = | 1.128 in |
| Bar area = | 0.999 in ² |
| Number of bars = | 19 |

| Material Strengths | | |
|---------------------------------|---------|-----|
| Concrete compressive strength = | 4500 | psi |
| Reinforcement yield strength = | 60000 | psi |
| Modulus of elasticity = | 29000 | ksi |
| Reinforcement yield strain = | 0.00207 | |
| Limiting compressive strain = | 0.003 | |

(per ACI 10.3.5 - OK)

| Seismic | |
|---------------------|-----|
| Seismic Zone = | 2 |
| Are hooks required? | yes |

Minimum Area of Steel

Required area of steel = 6.93 in²
 Actual area of steel = 18.99 in² OK
 Bar spacing = 4.82 in

Axial Loading

Load factor = 1.00
 Reduction factor = 0.65575 (per ACI 9.3.1 & 2)
 Factored axial load = 721.31 kips

Neutral Axis

Distance from extreme edge to neutral axis = 4.32 in
 Equivalent compression zone factor = 0.825 (per ACI 10.2.7.3)
 Distance from extreme edge to
 Equivalent compression zone factor = 3.56 in
 Distance from centroid to neutral axis = 16.68 in

Compression Zone

Area of steel in compression zone = 0.00 in²
 Angle from centroid of pier to intersection of
 equivalent compression zone and edge of pier = 33.85 deg
 Area of concrete in compression = 56.54 in²
 Force in concrete = $0.85 * f_c * Acc$ = 216.28 kips (per ACI 10.3.6.2)
 Total reinforcement forces = -937.59 kips
 Factored axial load = 721.31 kips
 Force in concrete = -216.28 kips

 Sum of the forces in concrete = 0.00 kips OK

Maximum Moment

First moment of the concrete area in compression about the centroid = 1067.25 in³
 Distance between centroid of concrete in compression and centroid of pier = 18.87 in
 Moment of concrete in compression = 4082.25 in-kips
 Total reinforcement moment = 3359.43 in-kips
 Nominal moment strength of column = 7441.67 in-kips
 Factored moment strength of column = 4879.86 in-kips 406.65 ft-kips

| | |
|--|--|
| Maximum allowable moment of the pier = 406.65 ft-kips | |
|--|--|

Individual Bars

| Bar # | Angle from first bar (deg) | Distance to centroid (in) | Distance to neutral axis (in) | Distance to equivalent comp. zone (in) | Strain | Area of steel in compression (in ²) | Axial force (kips) | Moment (in-kips) |
|-------|----------------------------|---------------------------|-------------------------------|--|----------|---|--------------------|------------------|
| 1 | 0.00 | 0.00 | -16.68 | -17.44 | -0.0116 | 0.00 | -59.96 | 0.00 |
| 2 | 18.95 | 5.66 | -11.02 | -11.78 | -0.00766 | 0.00 | -59.96 | -339.46 |
| 3 | 37.89 | 10.71 | -5.98 | -6.73 | -0.00415 | 0.00 | -59.96 | -642.13 |
| 4 | 56.84 | 14.60 | -2.09 | -2.84 | -0.00145 | 0.00 | -42.07 | -614.05 |
| 5 | 75.79 | 16.90 | 0.22 | -0.54 | 0.00015 | 0.00 | 4.39 | 74.13 |
| 6 | 94.74 | 17.38 | 0.69 | -0.06 | 0.00048 | 0.00 | 13.94 | 242.15 |
| 7 | 113.68 | 15.97 | -0.72 | -1.47 | -0.0005 | 0.00 | -14.45 | -230.78 |
| 8 | 132.63 | 12.83 | -3.86 | -4.61 | -0.00268 | 0.00 | -59.96 | -769.17 |
| 9 | 151.58 | 8.30 | -8.39 | -9.14 | -0.00583 | 0.00 | -59.96 | -497.58 |
| 10 | 170.53 | 2.87 | -13.81 | -14.57 | -0.0096 | 0.00 | -59.96 | -172.08 |
| 11 | 189.47 | -2.87 | -19.55 | -20.31 | -0.01359 | 0.00 | -59.96 | 172.08 |
| 12 | 208.42 | -8.30 | -24.98 | -25.74 | -0.01737 | 0.00 | -59.96 | 497.58 |
| 13 | 227.37 | -12.83 | -29.51 | -30.27 | -0.02052 | 0.00 | -59.96 | 769.17 |
| 14 | 246.32 | -15.97 | -32.65 | -33.41 | -0.0227 | 0.00 | -59.96 | 957.40 |
| 15 | 265.26 | -17.38 | -34.06 | -34.82 | -0.02368 | 0.00 | -59.96 | 1041.89 |
| 16 | 284.21 | -16.90 | -33.59 | -34.34 | -0.02335 | 0.00 | -59.96 | 1013.47 |
| 17 | 303.16 | -14.60 | -31.28 | -32.04 | -0.02175 | 0.00 | -59.96 | 875.22 |
| 18 | 322.11 | -10.71 | -27.39 | -28.15 | -0.01904 | 0.00 | -59.96 | 642.13 |
| 19 | 341.05 | -5.66 | -22.35 | -23.10 | -0.01554 | 0.00 | -59.96 | 339.46 |

DEVELOPMENT LENGTH CHECK OF PIER REINFORCEMENT

| | | | |
|-------------|--------------------------|--|--|
| Foundation: | Pier diameter = 3.5 ft | Cover between side of pier and cage = 3.00 in. | |
| | Cage diameter = 3 ft | Cover between top of pier and cage = 3.00 in. | |
| | Rebar size = 8 | Compressive strength of concrete = 4500 psi | |
| | Number of bars = 49 | Rebar yield strength = 60000 psi | |
| | Clear spacing = 7.10 in. | | |
| | Are there hooks? n | | |
| | Check Compression? n | | |

| | | | |
|---------------|-----------------------------|---|--|
| Anchor Steel: | Part number: 103183 | Actual Bending Moment = 220.50 ft-kips | |
| | Embedment length = 51.5 in. | Allowable Bending Moment = 406.65 ft-kips | |
| | Bolt Diameter = 1.25" | Excess Reinforcement Ratio = 0.542 | |

| | | |
|---------------|----------------------|--|
| Anchor Plate: | Part number: 212009 | |
| | Plate width = 22 in. | |

| | |
|--|-----------|
| Required development length (compression) = 999.00 in. | |
| Required development length (tension) = 39.35 in. | |
| Required development length (tension) = 21.34 in. | (reduced) |
| Available development length = 41.500 in. | |

OK

The length available in the pier for the development of the vertical reinforcement exceeds the required length (ACI 318-02, section 12.2).

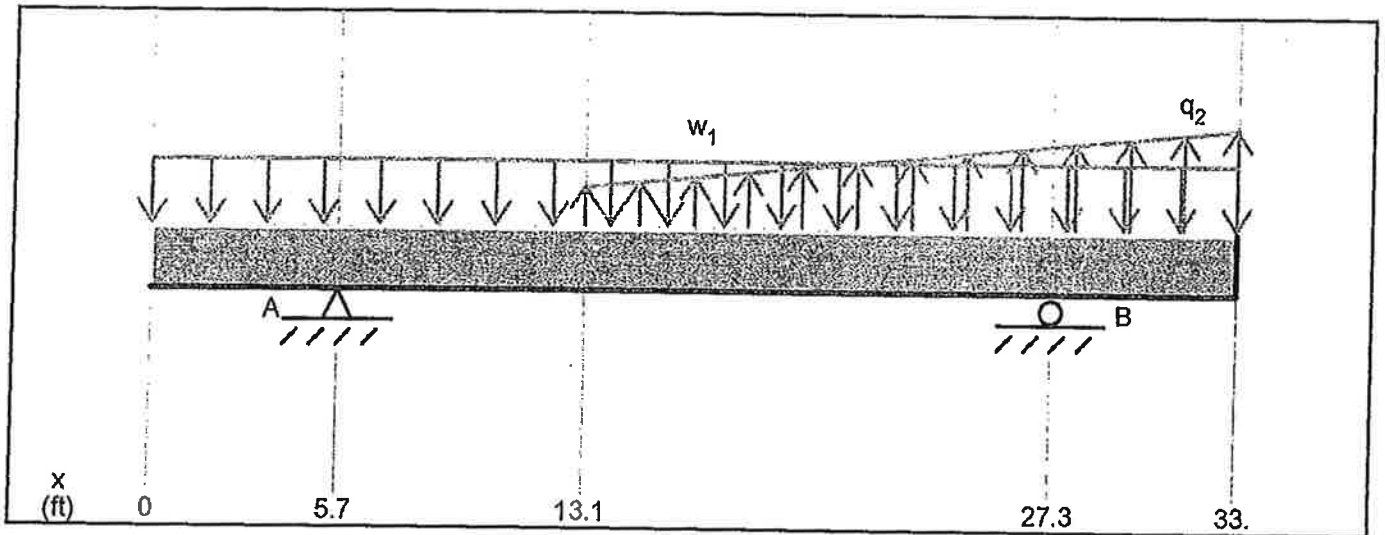
CHECK EMBEDMENT PLATE CLEARANCE IN THE PIER

| | | | |
|---------------|-----------------------------------|---|--|
| Foundation: | Pier diameter = 3.5 ft | Cover between side of pier and cage = 3.00 in. | |
| | Cage diameter = 3 ft | Minimum cover between A/S and cage = 3.00 in. | |
| Anchor Steel: | Part number: 103183 | Angle of anchor steel in foundation = 3.3 degrees | |
| | Embedment length = 51.5 in. | | |
| Anchor Plate: | Part number: 212009 | | |
| | Largest plate width = 22.00 in. | | |
| | Bolt Diameter = 1.25 in. | | |
| | Minimum cage diameter = 33.89 in. | | |
| | Actual cage diameter = 36 in. | | |

OK

The available space exceeds the minimum cage diameter required for anchor steel installed in the pier at an angle.

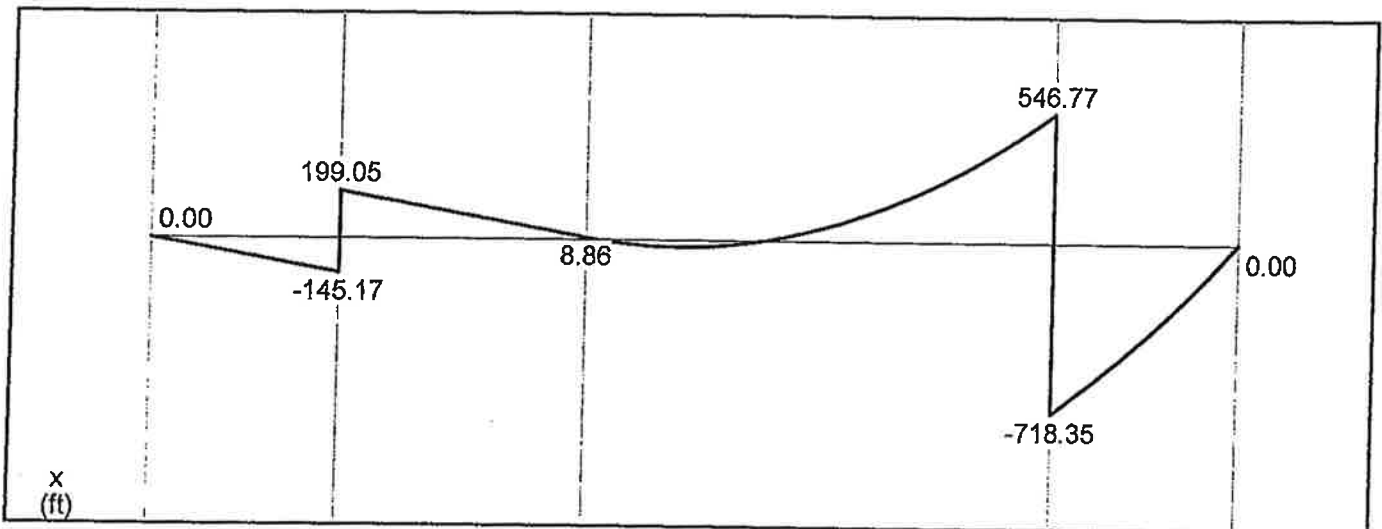
LC2- OPTION 1



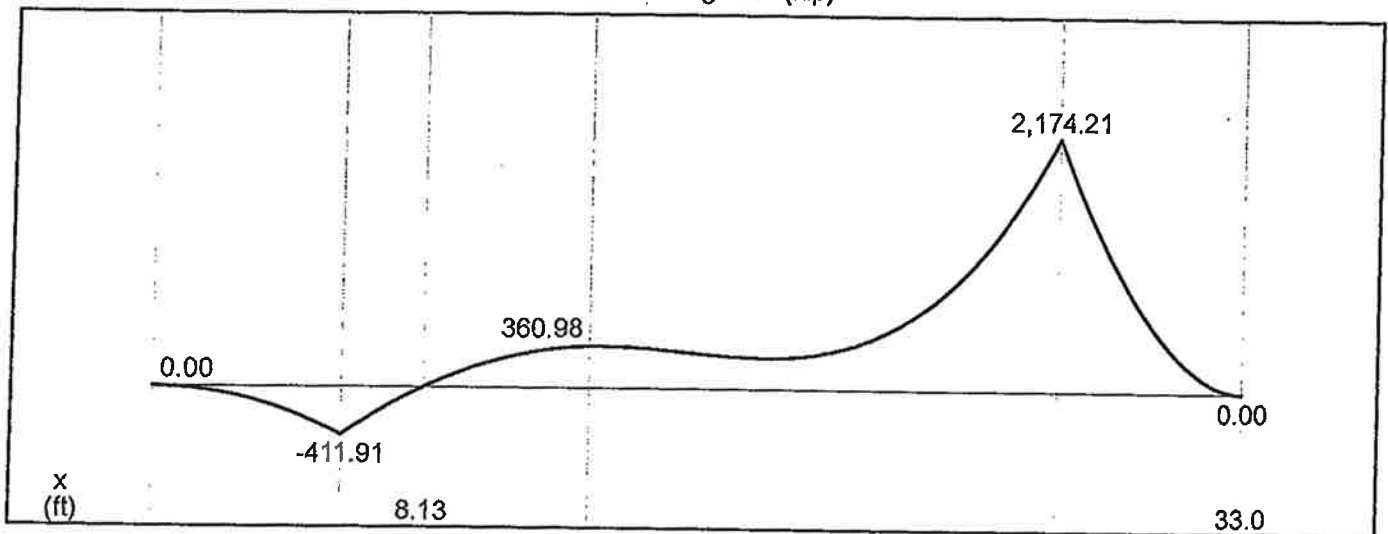
Load Diagram

$w_1 = 25.58$ kip/ft (down)
 $q_2 = 0.0$ to 177.48 kip/ft (up)

$A_y = 344.21$ kip (up)
 $B_y = 1,265.11$ kip (down)

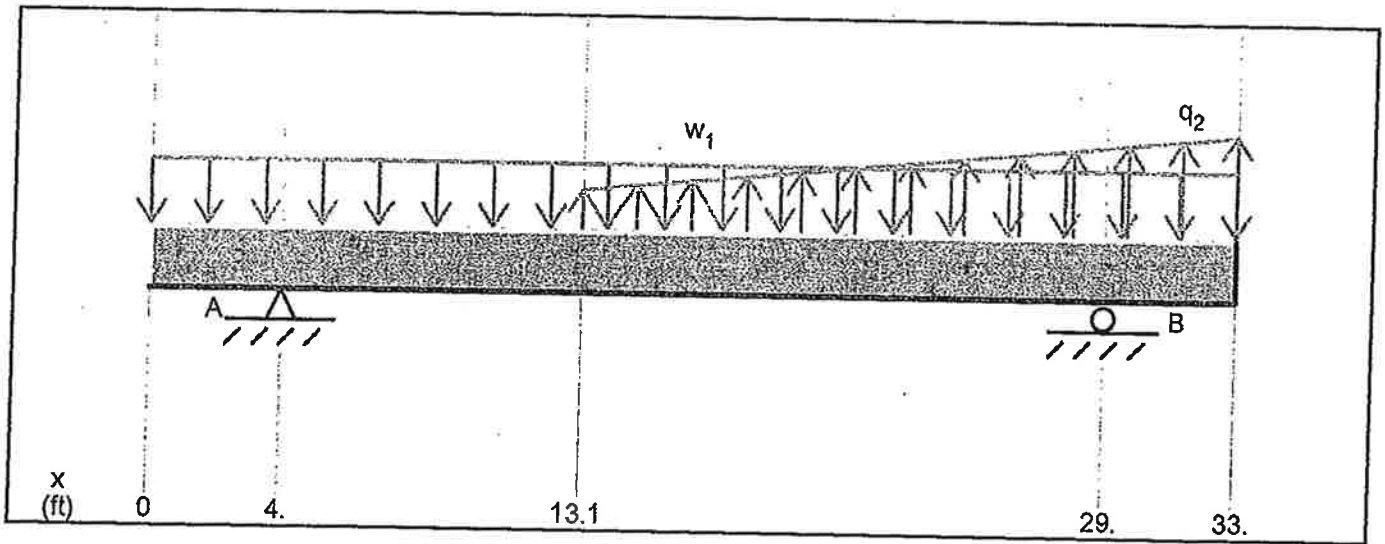


Shear Diagram (kip)



Moment Diagram (kip-ft)

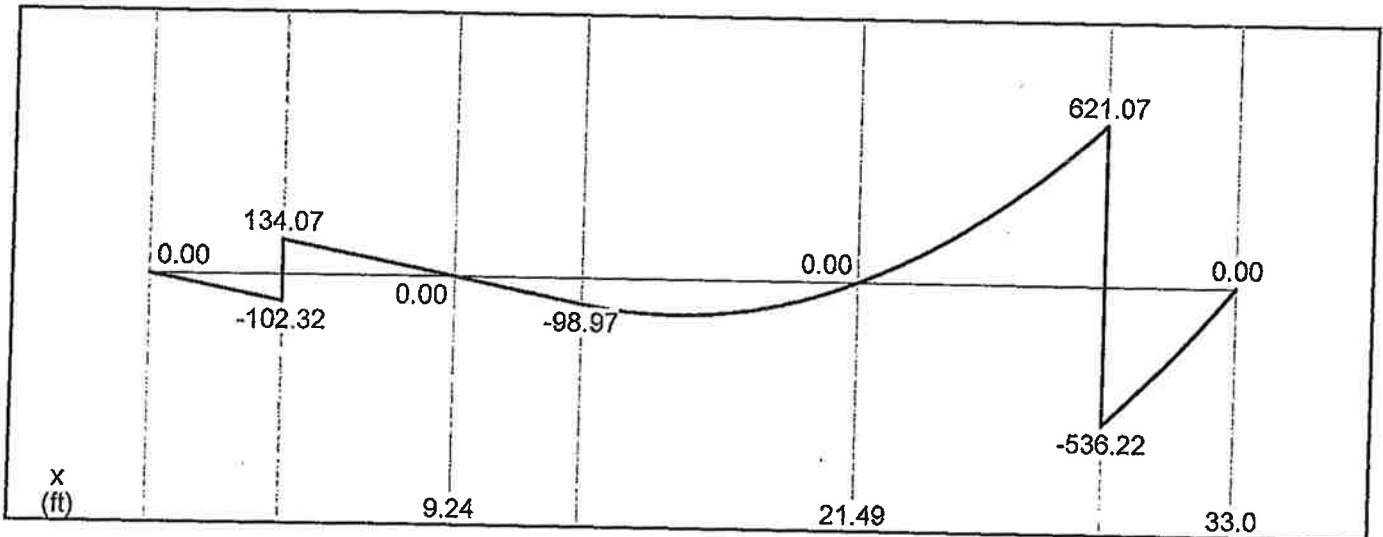
LC2- OPTION 2



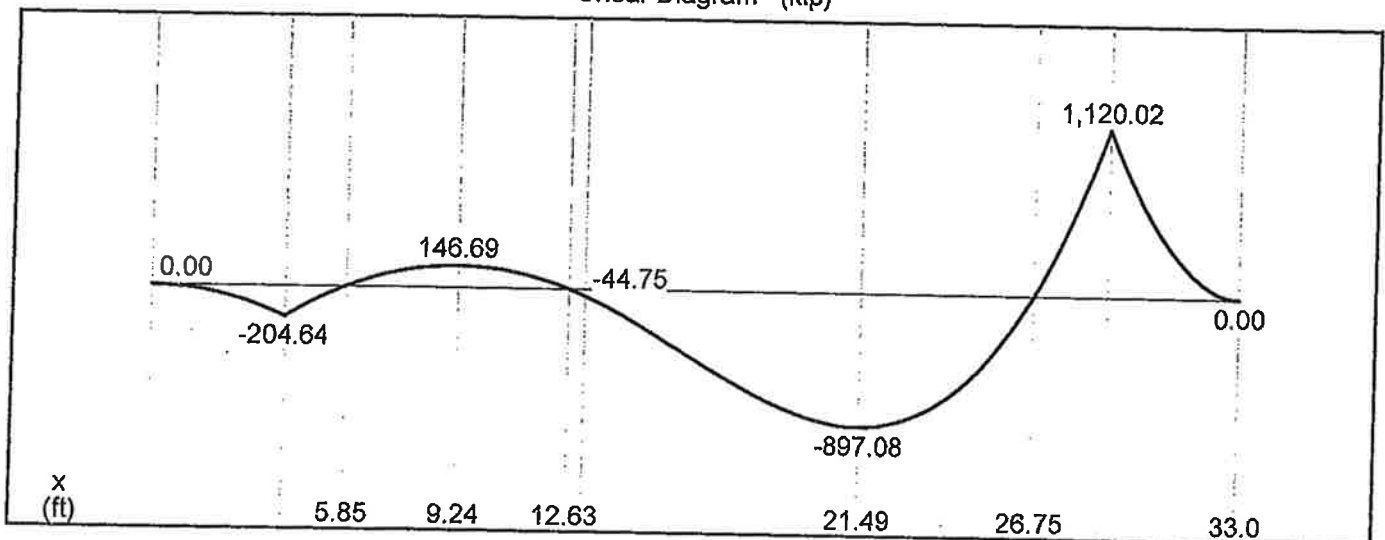
Load Diagram

$w_1 = 25.58$ kip/ft (down)
 $q_2 = 0.0$ to 177.48 kip/ft (up)

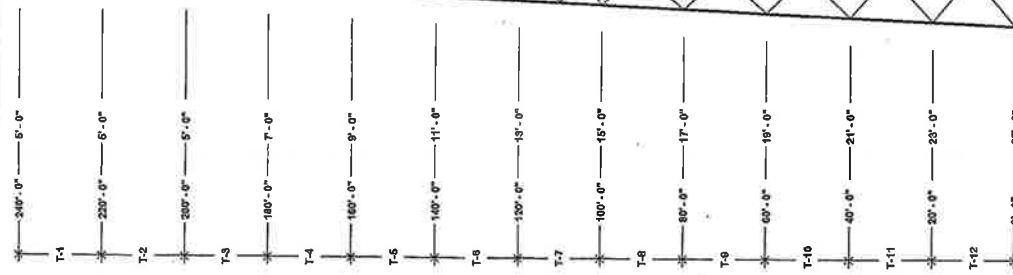
$A_y = 236.39$ kip (up)
 $B_y = 1,157.29$ kip (down)



Shear Diagram (kip)



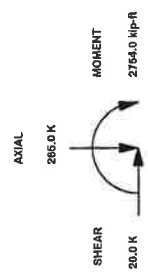
Moment Diagram (kip-ft)



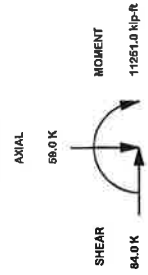
SEE PAGES FOR APURTINANCES

APPLICABLE CODES & STANDARDS
 Building Code: 2009 International Building Code
 Design Standard: TIA-222-G
TOWER DESIGN CRITERIA
 Basic Wind Speed: 110 mph (no ice)
 60 mph (1" RFE)
 Snow (definition only)
 Structure Class: C
 Exposure: 0
 Topographic Category: 1
 Great Height: 0

MATERIAL STRENGTHS
 (rod dia. ^{3/8})
 (3/4 thru 1" dia.)
 (1" dia.)
 Solid Rod A36
 A572 Gr.50
 A572 Gr.50
 A572 Gr.50
 Pipe A500 Gr. B
 A500 Gr. B
 Angle A36 Gr. 28
 Plate A572 Gr. 50
 Bolts A-325A-4.8
 (leg & angle)
 Anchor Bolt F1554 GRADE 105 OR A487



MAX. CORNER REACTIONS AT BASE:
 DOWN: 539.8 K
 UPLIFT: 473.0 K
 SHEAR: 52.0 K



MAX. CORNER REACTIONS AT BASE:
 DOWN: 539.8 K
 UPLIFT: 473.0 K
 SHEAR: 52.0 K

| SECTION | ELEVATION | FACE WIDTH | PANELS | LEG SIZE | LEG STYLE | LEG BOLT QTY & DIA | DIAGONAL BRACING SIZE | HORIZONTAL BRACING SIZE | BRACING BOLT QTY & DIA | SECTION WEIGHT |
|---------|-----------|------------|--------|----------|-----------|--------------------|-------------------------|-------------------------|------------------------|----------------|
| T1 | 220'-240' | 5'-0" | 4 | 2.60" | V | 4 x 3/4" | 1/8" x 2" x 2" | 3/16" x 2" x 2" | 3/4" x 1 | 844.41 |
| T2 | 200'-220' | 5'-0" | 3 | 4.00" | V | 6 x 3/4" | 3/16" x 2-1/2" x 2-1/2" | 3/16" x 2" x 2" | 3/4" x 1 | 1378.35 |
| T3 | 180'-200' | 7'-0" | 3 | 5.00" | V | 8 x 3/4" | 3/16" x 2-1/2" x 2-1/2" | 3/16" x 2" x 2" | 3/4" x 1 | 1011.60 |
| T4 | 160'-180' | 9'-0" | 3 | 5.00" | V | 8 x 1" | 3/16" x 2-1/2" x 2-1/2" | 3/16" x 2" x 2" | 3/4" x 1 | 2289.30 |
| T5 | 140'-160' | 11'-0" | 2 | 1.60" | 120DPH | 6 x 1" | 3/16" x 3" x 3" | 3/16" x 3" x 3" | 1" x 1 | 2488.15 |
| T6 | 120'-140' | 13'-0" | 2 | 1.75" | 120DPH | 6 x 1 1/4" | 3/16" x 3" x 3" | 3/16" x 3" x 3" | 1" x 1 | 3154.83 |
| T7 | 100'-120' | 15'-0" | 2 | 1.75" | 120DPH | 6 x 1 1/4" | 3/16" x 3" x 3" | 3/16" x 3" x 3" | 1" x 1 | 3906.40 |
| T8 | 80'-100' | 17'-0" | 1 | 2.00" | 120DH2 | 12 x 1" | 3/16" x 3" x 3" | 3/16" x 3" x 3" | 7/8" x 1 | 4106.91 |
| T9 | 60'-80' | 19'-0" | 1 | 2.00" | 120DH2 | 12 x 1" | 3/16" x 3" x 3" | 3/16" x 3" x 3" | 7/8" x 1 | 5302.51 |
| T10 | 40'-60' | 21'-0" | 1 | 2.25" | 120DH2 | 12 x 1" | 1/4" x 3-1/2" x 3-1/2" | 1/4" x 3-1/2" x 3-1/2" | 7/8" x 1 | 5977.89 |
| T11 | 20'-40' | 23'-0" | 1 | 2.50" | 120DH2 | 12 x 1" | 1/4" x 3-1/2" x 3-1/2" | 1/4" x 3-1/2" x 3-1/2" | 7/8" x 1 | 6485.69 |
| T12 | 0'-20' | 25'-0" | 1 | 2.50" | 120DH2 | 12 x 1" | 1/4" x 3-1/2" x 3-1/2" | 1/4" x 3-1/2" x 3-1/2" | 7/8" x 1 | 6238.02 |

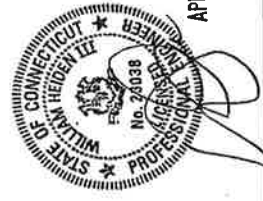


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| | | | |
|--|--|----------------------------------|---|
| | 1-877-467-4766 Plymouth, IN 1-800-547-2151 Salem, OR | | ENG. FILE NO. 284859 DWS. NO. 259147T |
| | PAGE 1 OF 14 | | |
| DESCRIPTION Tower View Page 1 | STRUCTURE APPROVAL 3/30/2015 | FOUNDATION APPROVAL 3/30/2015 | REV DESCRIPTION OF REVISIONS CPD BY DATE REVISION HISTORY |
| SITE ASHFORD, CT VERIZON WIRELESS U 25 X 240' | COPYRIGHT 2013 THE DATA AND TECHNOLOGIES CONTAINED IN THIS DRAWING ARE PROPRIETARY INFORMATION OF VALMONT INDUSTRIES AND CONSIDERED A TRADE SECRET. ANY USE OR DISCLOSURE WITHOUT THE CONSENT OF VALMONT INDUSTRIES IS STRICTLY PROHIBITED. | | |

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DWG. NO. 2591477



DESCRIPTION
Tower View Page 2

STRUCTURE APPROVAL 3/30/2015
FOUNDATION APPROVAL 3/30/2015

SITE
ASHFORD, CT
VERIZON WIRELESS
U 25 X 240'

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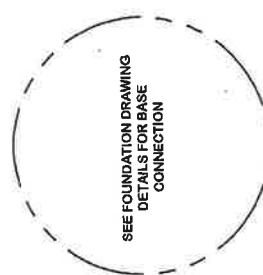
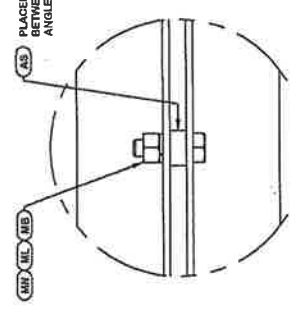
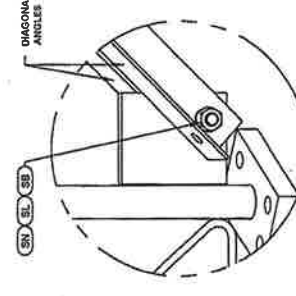
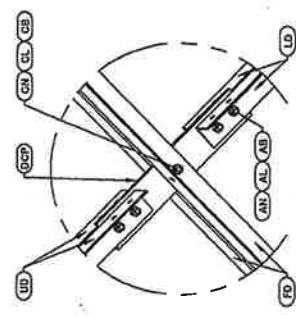
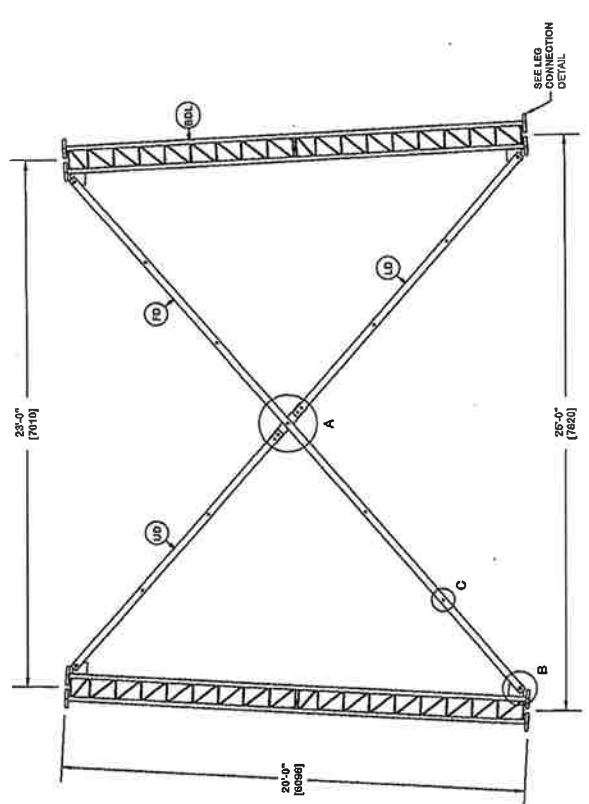
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| REV | DESCRIPTION OF REVISIONS | CPD | BY | DATE |
|-----|--------------------------|-----|----|------|
| | REVISION HISTORY | | | |

| DESIGNED AP FURTHERANCE LOADING | TYPE | ELEVATION |
|---|------|-----------|
| (1) 12" X 4" LIGHTNING ROD | | 240' |
| (2) 12" V FRAME | | 240' |
| (3) 2" X 84" SCH. 40 | | 240' |
| (4) ALCATEL-LUCENT RRH200A-AWS | | 240' |
| (5) ALCATEL-LUCENT RRM200B-PCS | | 240' |
| (6) BEACON | | 240' |
| (7) BEACON EXTENDER (4) 803062 | | 240' |
| (8) DB-T1-402-8A8-AZ ASSUMED: (10.0) X 11.22" X | | 240' |
| (9) H302-65 TDS-VTM | | 240' |
| (10) LUC-6514DS-VTM | | 240' |
| (11) 24" STANDOFF | | 221" |
| (12) WHIP (2.88" X 12) | | 221" |
| (13) 24" STANDOFF | | 218" |
| (14) WHIP (2.88" X 12) | | 195" |
| (15) 12" V FRAME | | 195" |
| (16) 2" X 96" SCH. 40 | | 195" |
| (17) 770.00 | | 195" |
| (18) AMX-CD-17-65-001-RET | | 185" |
| (19) POLYPHASER (12" X 12" X 6") | | 185" |
| (20) POWERWAVE TDS-60 QUAD-BAND-RET | | 185" |
| (21) POWERWAVE LGP2140X-TMA-CD-1800 | | 185" |
| (22) POWERWAVE LGP21803 | | 185" |
| (23) RRU511 (20" X 17" X 7") | | 185" |

PARTS LIST

| ITEM | QTY | PART NO. | PART DESCRIPTION | UNIT WT. | NET WT. |
|-----------------|-----|----------|---|-----------|-------------|
| BOL | 3 | 105862 | #12 LEG SECT - 3/16" TO 2" THIN LEG - 1/2" BRACE | 1335.4 | 4005.1 |
| UD | 6 | 215312 | ANGLE U-26 UP 13° 8' | 85.3 | 495.8 |
| LD | 6 | 215316 | ANGLE U-25 LOW 13° 11' 7/32" | 90.9 | 545.8 |
| FD | 6 | 215377 | ANGLE U-26 LONG 20° 4' 23/32" | 180.0 | 1080.1 |
| HL | 24 | 315123 | 58° GALVANIZED LOCKWASHER (S3-22230) | 0.0 | 0.0 |
| MN | 24 | 312671 | 58°-11 HOT DIPPED GALVANIZED NUT | 0.1 | 2.3 |
| AS | 24 | 104291 | SPACER 1/2" THICK 13/16" HOLE | 0.6 | 12.0 |
| MB | 24 | 101885 | 58°-11 X 2 1/4" A-308 BOLT 1 1/4" THREAD | 0.3 | 8.2 |
| AB/CL | 16 | 161886 | 58°-11 X 2 1/4" A-308 BOLT 1 1/4" THREAD | 0.3 | 3.9 |
| AL/CL | 16 | 312123 | 58° GALVANIZED LOCKWASHER (S3-22230) | 0.0 | 0.3 |
| AN/ON | 16 | 312671 | 58°-11 HOT DIPPED GALVANIZED NUT | 0.1 | 1.6 |
| DCP | 3 | 211883 | MID BRACE CONNECTION PLATE FOR #12 BID LEG ANGLES | 20.6 | 61.8 |
| SL | 12 | 312183 | 78° GALVANIZED LOCKWASHER | 0.1 | 0.1 |
| SN | 12 | 312216 | 78°-9 HOT DIPPED GALVANIZED NUT | 0.3 | 3.6 |
| SB | 12 | 172276 | 78°-9 X 3/16" A-308 BOLT WITH 1-1/2" THREAD | 1.2 | 14.9 |
| Total Wt | | | | 6259.0 lb | (2832.8 kg) |



| | | | |
|--|---|--|---------------------------|
| <p>ASHFORD, CT VERIZON WIRELESS U 25 X 240'</p> <p style="font-size: small;">COPYRIGHT 2013</p> | <p>SECTION U-25.0 (0' - 20' ELEVATION)</p> | <p>STRUCTURE APPROVAL 3/30/2015</p> <p>FOUNDATION APPROVAL 3/30/2015</p> | <p>DESCRIPTION</p> |
| <p>BASE CONNECTION</p> | | <p>DETAIL A ANGLE INTERSECTION CONNECTION</p> | |
| <p>DETAIL B END SIDE PLATE ANGLE CONNECTION</p> | | <p>DETAIL C STITCH BOLT CONNECTION</p> | |
| <p>ANGLE INTERSECTION CONNECTION</p> | | <p>BASE CONNECTION</p> | |



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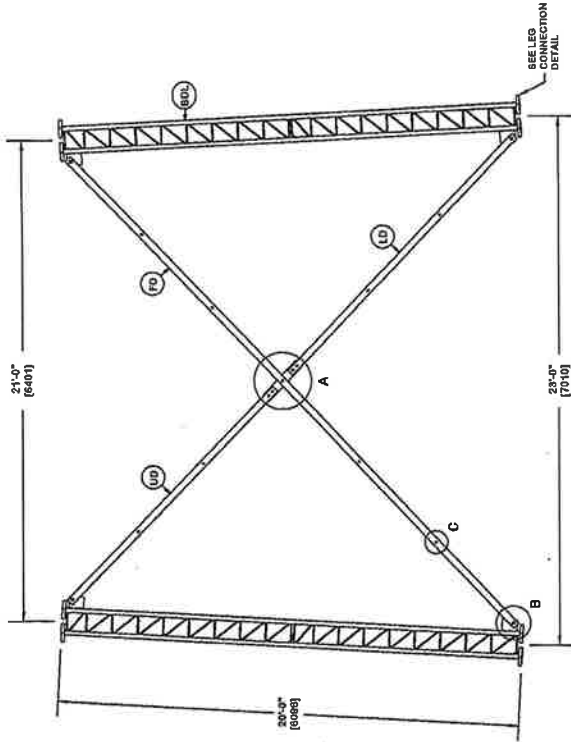
valmont
STRUCTURES

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1-800-547-2751 Salem, OR

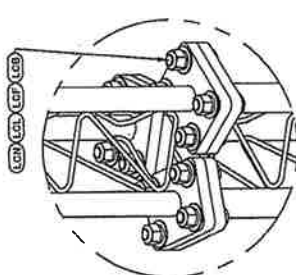
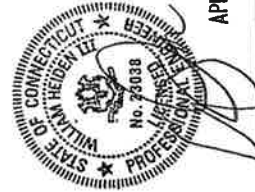
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|-----------------------------|---------------------|
| ENG. FILE NO. 284859 | PAGE 3 OF 14 |
| DWG. NO. 2591477 | |

| REV | DESCRIPTION OF REVISIONS | CPD | BY | DATE |
|------------------|--------------------------|-----|----|------|
| REVISION HISTORY | | | | |

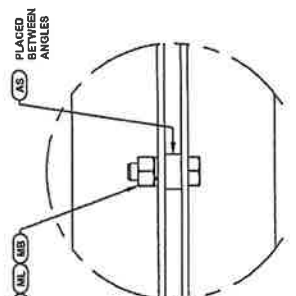
ORIENT ANGLES WITH STAMPED
END TOWARD TOP OF SECTION



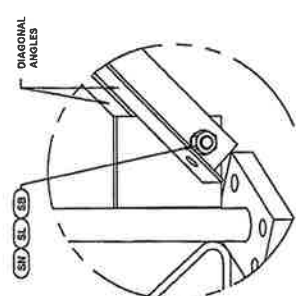
| ITEM | QTY | PART NO. | PART DESCRIPTION | UNIT WT. | NET WT. |
|----------|-----|----------|---|------------------------|---------|
| BOL | 3 | 188960 | #12 LEG SECTION - 3/16" LEG - 1/2" BRACE - 78" B | 1100.5 | 3301.6 |
| UD | 8 | 216304 | ANGLE U-23 UP 12'-10 25/32" | 78.8 | 471.4 |
| UD | 8 | 216304 | ANGLE U-23 LOW 14'-2 1/16" | 88.8 | 598.4 |
| FD | 8 | 216373 | ANGLE U-23 LONG 28'-0 15/16" | 171.0 | 1006.1 |
| ML | 24 | 312123 | 8/8" GALVANIZED LOCKWASHER (83-22200) | 0.0 | 0.6 |
| AS | 24 | 312501 | 6/8"-11 HOT DIPPED GALVANIZED NUT | 0.1 | 2.9 |
| MB | 24 | 104251 | SPACER 1/2" THICK 181/16" HOLE | 0.5 | 12.0 |
| MB | 24 | 161895 | 6/8"-11 X 2 1/4" A-305 BOLT 1 1/4" THREAD | 0.3 | 8.2 |
| AB/GB | 16 | 181895 | 6/8"-11 X 2 1/4" A-305 BOLT 1 1/4" THREAD | 0.0 | 0.3 |
| AL/CL | 16 | 312123 | 6/8" GALVANIZED LOCKWASHER (83-22200) | 0.0 | 0.3 |
| AN/ON | 3 | 214883 | MID BRACE CONNECTION PLATE FOR #12 BID LEG ANGLES | 25.6 | 61.8 |
| DGP | 12 | 312199 | 7/8" GALVANIZED LOCKWASHER | 0.1 | 0.6 |
| SL | 12 | 312215 | 7/8"-9 HOT DIPPED GALVANIZED NUT | 0.3 | 3.6 |
| SN | 12 | 172215 | 7/8"-9 X 2-1/2" A-305 BOLT WITH 1-1/2" THREAD | 1.2 | 14.8 |
| SB | 12 | 172215 | 1"-8 X 5" A-305 BOLT WITH 1-3/4" THREAD | 0.8 | 30.2 |
| LGB | 36 | 172201 | 1" GALVANIZED FLAT WASHER (F430) | 0.1 | 10.1 |
| LCL | 36 | 312222 | 1" GALVANIZED LOCKWASHER | 0.1 | 2.9 |
| LGN | 36 | 312504 | 1"-9 HOT DIPPED GALVANIZED NUT | 0.4 | 15.5 |
| Total Wt | | | | 5166.8 lbs (2346.0 kg) | |



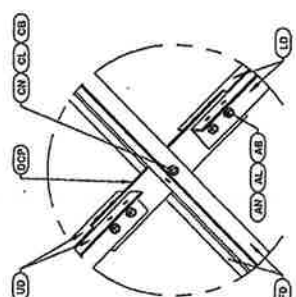
LEG TO LEG CONNECTION
(SIDE PLATES NOT SHOWN FOR CLARITY)



DETAIL C
STITCH BOLT CONNECTION



DETAIL B
END SIDE PLATE ANGLE CONNECTION



DETAIL A
ANGLE INTERSECTION CONNECTION

valmont STRUCTURES
1-877-467-4783 Plymouth, IN
1-800-547-2151 Salem, OR

ENG. FILE NO. **284859**
DRG. NO. **259147T**

DESCRIPTION
SECTION U-23.0 (20' - 40' ELEVATION)

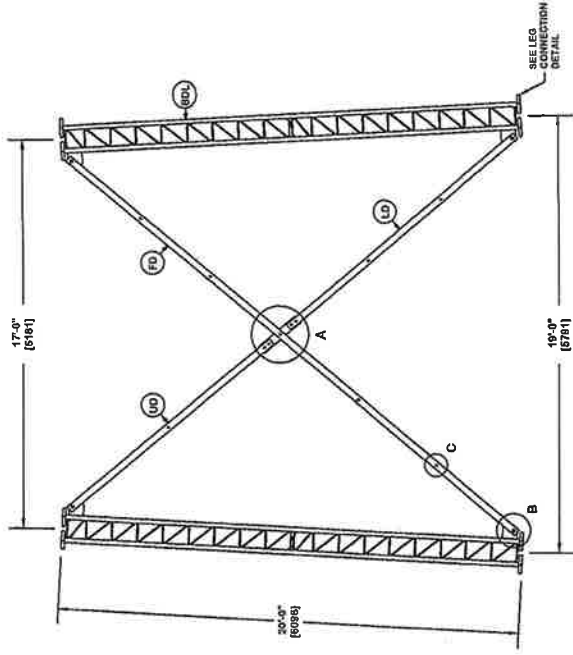
SITE
**ASHFORD, CT
VERIZON WIRELESS
U 25 X 240'**

| REV | DESCRIPTION OF REVISIONS | CPD | BY | DATE |
|-----|--------------------------|-----|----|-----------|
| | FOUNDATION APPROVAL | | | 3/30/2015 |
| | STRUCTURE APPROVAL | | | 3/30/2015 |

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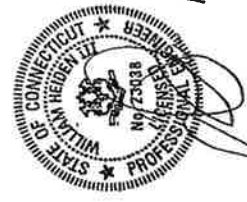
REVISION HISTORY

ORIENT ANGLES WITH STAMPED END TOWARD TOP OF SECTION

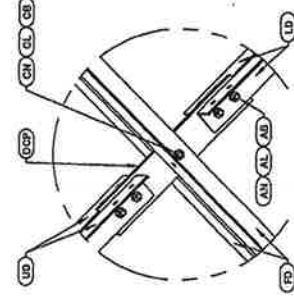
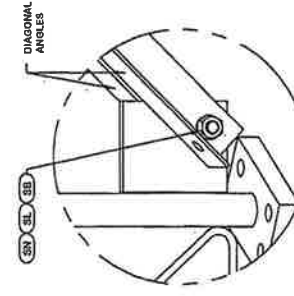
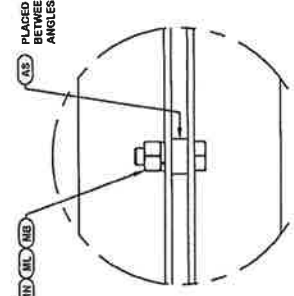
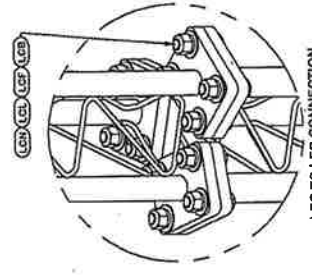


| ITEM | QTY | PART NO. | PART DESCRIPTION | UNIT WT. | NET WT. |
|----------|-----|----------|---|-----------------------|---------|
| BOL | 3 | 18659 | #12 LEG SECTION - 2" LEG - 1/2" BRACE - 7/8" BOLT | 926.9 | 2780.9 |
| UD | 6 | 21628B | ANGLE U-19 UP 11-5 1182" | 41.8 | 267.4 |
| LD | 6 | 21629 | ANGLE U-19 LOW 12-11 792" | 50.4 | 302.2 |
| FD | 6 | 21694 | ANGLE U-19 LONG 20-4 1022" | 98.7 | 592.3 |
| ML | 21 | 31213 | 68" GALVANIZED LOCKWASHER (S5-22230) | 0.0 | 0.4 |
| MN | 21 | 31261 | 68"-11 HOT DIPPED GALVANIZED NUT | 0.1 | 2.5 |
| AS | 21 | 104281 | SPACER 12" THICK 1318" HOLE | 0.6 | 10.3 |
| M8 | 21 | 161895 | 68"-11 X 2 1/4" A-325 BOLT 1 1/4" THREAD | 0.3 | 6.5 |
| ABWB | 16 | 161895 | 68"-11 X 2 1/4" A-325 BOLT 1 1/4" THREAD | 0.3 | 3.8 |
| AL/CL | 16 | 31213 | 68" GALVANIZED LOCKWASHER (S5-22230) | 0.0 | 0.3 |
| AN/ON | 3 | 31261 | 68"-11 HOT DIPPED GALVANIZED NUT | 0.1 | 1.4 |
| DCP | 3 | 21833 | MID BRACE CONNECTION PLATE FOR #12 BID LEG ANGLES | 20.8 | 61.9 |
| SL | 12 | 31285 | 7/8" GALVANIZED LOCKWASHER | 0.1 | 0.6 |
| SN | 12 | 312215 | 7/8"-9 HOT DIPPED GALVANIZED NUT | 0.3 | 3.6 |
| BB | 12 | 172276 | 7/8"-9 X 5-1/2" A-305 BOLT WITH 1-1/2" THREAD | 3.2 | 14.8 |
| LCB | 36 | 172281 | 1"-8 X 6" A-325 BOLT WITH 1-3/4" THREAD | 0.8 | 30.2 |
| LCL | 72 | 312222 | 1" GALVANIZED FLAT WASHER (F438) | 0.1 | 10.1 |
| LGL | 36 | 312228 | 1" GALVANIZED LOCKWASHER | 0.1 | 2.9 |
| LCN | 36 | 312584 | 1"-8 HOT DIPPED GALVANIZED NUT | 0.4 | 15.5 |
| Total Wt | | | | 4107.1 lb [1862.7 kg] | |

APR 01 2015



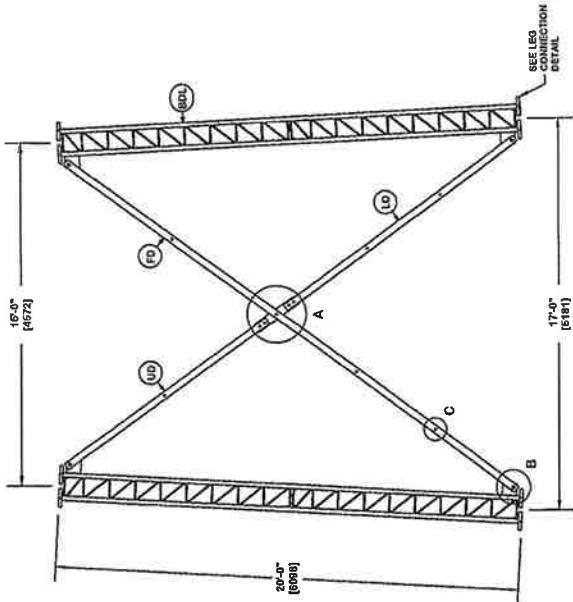
valmont STRUCTURES
 1-877-487-4763 Plymouth, IN
 1-800-547-2151 Salem, OR
 ENG. FILE NO. 284859
 DWG. NO. 259147T



| REV | DESCRIPTION OF REVISIONS | CFD | BY | DATE | REVISION HISTORY |
|-----|--|-----|----|------|-------------------------------|
| | SECTION U-19.0 (60' - 80' ELEVATION) | | | | FOUNDATION APPROVAL 3/30/2015 |
| | ASHFORD, CT VERIZON WIRELESS U 25 X 240' | | | | STRUCTURE APPROVAL 3/30/2015 |

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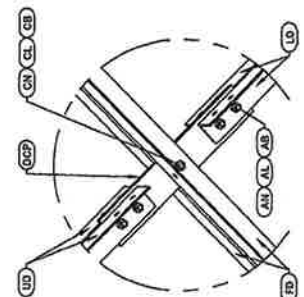
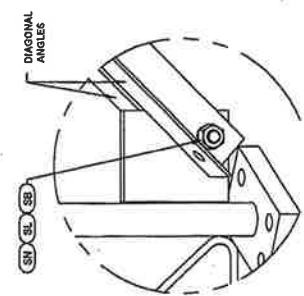
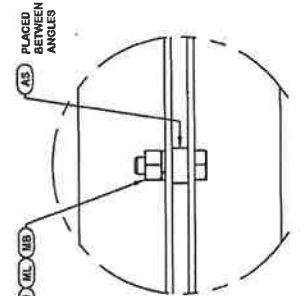
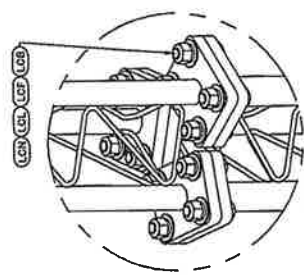
ORIENT ANGLES WITH STAMPED END TOWARD TOP OF SECTION



| ITEM | QTY | PART NO. | PART DESCRIPTION | UNIT WT. | NET WT. |
|-----------|-----|----------|--|------------------------|---------|
| BOL | 3 | 166937 | #12 LEG SECT - 2" TO 1-3/4" TRANS LEG - 1/2" BRACE | 996.9 | 2720.6 |
| UD | 8 | 215280 | ANGLE U-17 UP 16" X 8" 5/16" | 47.9 | 261.5 |
| LD | 8 | 215284 | ANGLE U-17 LOW 12" X 8" 5/16" | 46.2 | 269.4 |
| FD | 8 | 215281 | ANGLE U-17 LONG 24" X 8" 5/16" | 93.9 | 563.2 |
| HL | 16 | 312193 | 68" GALVANIZED LOCKWASHER (S-22230) | 0.0 | 0.4 |
| HN | 16 | 312651 | 68"-11 HOT DIPPED GALVANIZED NUT | 0.1 | 2.2 |
| AS | 16 | 104291 | SPACER 1/2" THICK 13/16" HOLE | 0.6 | 9.0 |
| MB | 16 | 161685 | 68"-11 X 2 1/4" A-325 BOLT 1 1/4" THREAD | 0.3 | 4.7 |
| AGKCB | 16 | 161685 | 68"-11 X 2 1/4" A-325 BOLT 1 1/4" THREAD | 0.3 | 3.9 |
| AL/CL | 16 | 312193 | 68" GALVANIZED LOCKWASHER (S-22230) | 0.0 | 0.3 |
| AN/ON | 15 | 312651 | 68"-11 HOT DIPPED GALVANIZED NUT | 0.1 | 1.8 |
| DCP | 3 | 211833 | MID BRACE CONNECTION PLATE FOR #12 BID LEG ANGLES | 20.8 | 61.8 |
| SL | 12 | 312193 | 78" GALVANIZED LOCKWASHER | 0.1 | 0.6 |
| SN | 12 | 312215 | 78"-9 HOT DIPPED GALVANIZED NUT | 0.8 | 3.6 |
| SB | 12 | 172276 | 78"-9 X 5-1/2" A-325 BOLT WITH 1-4/2" THREAD | 1.2 | 14.8 |
| LCB | 36 | 172281 | 1"-8 X 5-1/2" A-325 BOLT WITH 1-3/4" THREAD | 0.8 | 30.2 |
| LCF | 72 | 312222 | 1" GALVANIZED FLAT WASHER (F-458) | 0.1 | 10.1 |
| LCL | 36 | 312223 | 1" GALVANIZED LOCKWASHER | 0.1 | 2.6 |
| LCN | 36 | 312564 | 1"-8 HOT DIPPED GALVANIZED NUT | 0.4 | 16.6 |
| Total WT. | | | | 3980.6 lb. [1810.0 kg] | |



APR 01 2015



LEG TO LEG CONNECTION (SIDE PLATES NOT SHOWN FOR CLARITY)

DETAIL C STITCH BOLT CONNECTION

DETAIL B END SIDE PLATE ANGLE CONNECTION

DETAIL A ANGLE INTERSECTION CONNECTION

valmont STRUCTURES
 1-877-467-4789 Plymouth, IN
 1-800-547-2161 Salem, OR
 ENG. FILE NO. 284859
 DWG. NO. 259147T

DESCRIPTION
 SECTION U-17.0 (80' - 100' ELEVATION)
 STRUCTURE APPROVAL 3/30/2015
 FOUNDATION APPROVAL 3/30/2015

SITE
 ASHFORD, CT
 VERIZON WIRELESS
 U 25 X 240'
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| REV | DESCRIPTION OF REVISIONS | CPD | BY | DATE |
|-----|--------------------------|-----|----|------|
| | | | | |
| | | | | |

REVISION HISTORY

valmont STRUCTURES
1-877-467-4769 Plymouth, IN
1-800-647-2151 Salem, OR

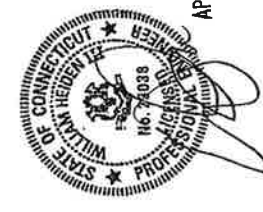
ENG. FILE NO.
DWS. NO.

DESCRIPTION

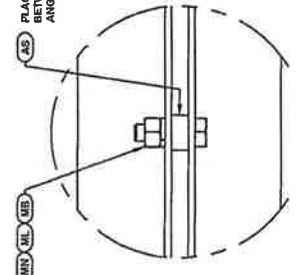
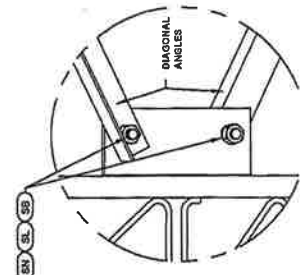
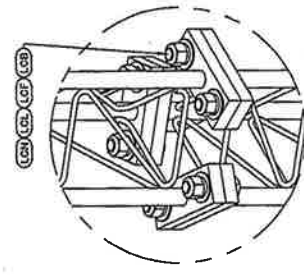
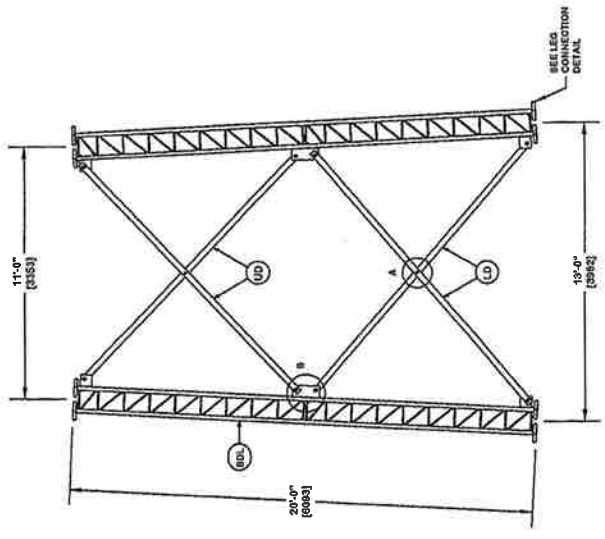
SECTION U-13.0 (120' - 140' ELEVATION)

DATE

APR 0 1 2015



| PARTS LIST | | | | NET WT. |
|------------|-----|----------|--|------------------------|
| ITEM | QTY | PART NO. | PART DESCRIPTION | UNIT WT. |
| BDL | 3 | 186213 | #12 LEG SECT. - 1 3/4" TO 1 1/2" TRANS LEG - 10' B | 786.9 |
| LD | 6 | 106576 | DIAG BRACE 3/16" X 3" X 3" 14'- 6.5032" LONG (A-3) | 55.9 |
| A3 | 6 | 104251 | SPACER 1/2" THICK 1/215" HOLE | 0.5 |
| LN | 6 | 312602 | 3/4"-10 HOT DRIPPED GALVANIZED NUT | 0.2 |
| ML | 6 | 312153 | 3/4" GALVANIZED LOCKWASHER | 0.0 |
| MB | 6 | 186427 | 3/4"-10 X 3" A-325GT BOLT WITH FULL THREAD | 0.5 |
| SL | 24 | 312223 | 1" GALVANIZED LOCKWASHER | 0.1 |
| SH | 24 | 312604 | 1"-8 NOT DRIPPED GALVANIZED NUT | 0.4 |
| SB | 24 | 172286 | 1"-8 X 2-1/4" A-325 BOLT WITH 1-3/4" THREAD | 0.8 |
| UD | 6 | 106574 | DIAG BRACE 3/16" X 3" X 3" 18'- 8.5032" LONG (A-3) | 55.1 |
| LCB | 18 | 222022 | 1-1/4" X 5-1/2" A-325 BOLT WITH 2" THREAD | 2.5 |
| LCF | 36 | 312282 | 1-1/4" GALVANIZED PLAT WASHER (F438) | 0.1 |
| LCL | 18 | 312283 | 1-1/4" GALVANIZED LOCKWASHER | 0.2 |
| LCN | 18 | 312607 | 1-1/4" X 7 HOT DRIPPED GALVANIZED NUT | 0.7 |
| Total Wt | | | | 2977.8 lb. (1351.9 kg) |



ORIENT ANGLES WITH STAMPED END TOWARD TOP OF SECTION

DETAIL A ANGLE INTERSECTION CONNECTION
DETAIL B MID SIDE PLATE ANGLE CONNECTION
LEG TO LEG CONNECTION (SIDE PLATES NOT SHOWN FOR CLARITY)

REVISION HISTORY

DESCRIPTION OF REVISIONS

DATE

BY

CPD

REV

REVISION HISTORY

DESCRIPTION OF REVISIONS

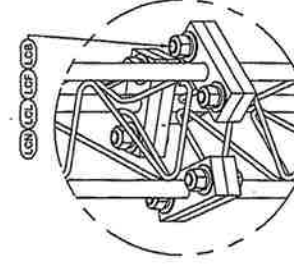
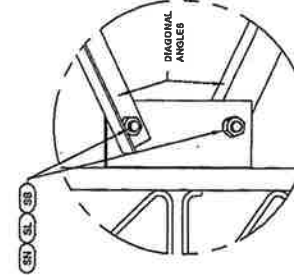
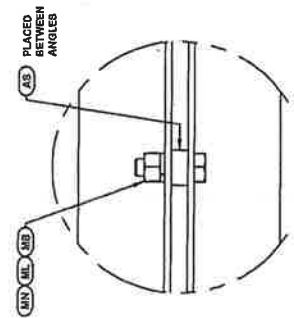
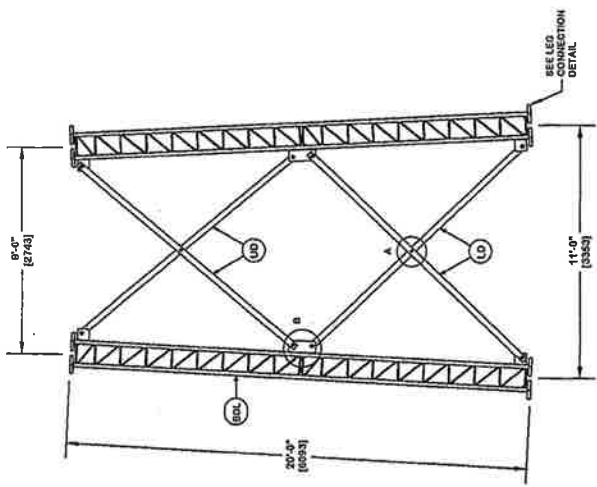
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BY

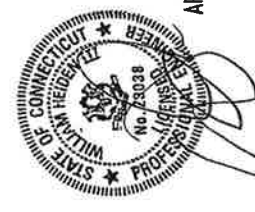
CPD

REV

ORIENT ANGLES WITH STAMPED
END TOWARD TOP OF SECTION



| PARTS LIST | | | | UNIT WT. | NET WT. |
|------------|-----|----------|--|------------------------|---------|
| ITEM | QTY | PART NO. | PART DESCRIPTION | | |
| BDL | 3 | 184651 | #12 LEG SECTION - 1-1/2" LEG - 1/2" BRACE - 1" BCL | 802.8 | 1808.6 |
| LD | 6 | 104571 | ANGLE U-12 UP 12-11 21652 | 50.3 | 302.0 |
| AS | 6 | 104381 | SPACER 1/2" THICK 13HP HOLE | 0.6 | 3.0 |
| MM | 6 | 312502 | 5/4"-10 HOT DIPPED GALVANIZED NUT | 0.2 | 1.1 |
| ML | 6 | 312163 | 5/4" GALVANIZED LOCKWASHER | 0.2 | 1.1 |
| MB | 6 | 104427 | 5/4"-10 X 3" A-325T BOLT WITH FULL THREAD | 0.6 | 2.8 |
| SL | 24 | 312223 | 1" GALVANIZED LOCKWASHER | 0.1 | 1.5 |
| SN | 24 | 312594 | 1"-8 HOT DIPPED GALVANIZED NUT | 0.4 | 10.3 |
| SB | 24 | 172295 | 1"-8 X 2-1/4" A-325 BOLT WITH 1-3/4" THREAD | 0.8 | 20.2 |
| UD | 6 | 105588 | ANGLE U-10 LOW 1/2" X 3/8" | 47.8 | 288.7 |
| LCB | 18 | 172281 | 1"-8 X 1/2" A-325 BOLT WITH 1-3/4" THREAD | 0.8 | 16.1 |
| LCF | 36 | 312222 | 1" GALVANIZED FLAT WASHER (F438) | 0.1 | 5.0 |
| LCL | 18 | 312223 | 1" GALVANIZED LOCKWASHER | 0.1 | 1.4 |
| LCL | 18 | 312594 | 1"-8 HOT DIPPED GALVANIZED NUT | 0.4 | 7.7 |
| Total Wt | | | | 2485.0 Lb. (1119.5 kg) | |



APR 01 2015

valmont
STRUCTURES
1-877-487-4763 Plymouth, IN
1-800-547-2151 Salem, OR

| | |
|------------------|---------|
| ENG. FILE NO. | 284859 |
| DWG. NO. | 259147T |
| PAGE 10 OF 14 | |

DESCRIPTION
SECTION U-11.0 (140' - 160' ELEVATION)

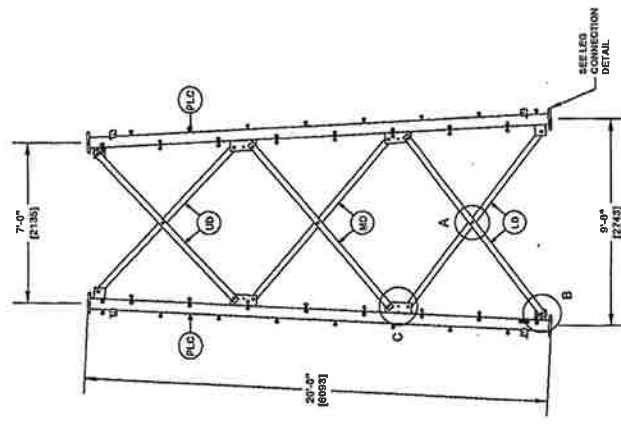
SITE
ASHFORD, CT
VERIZON WIRELESS
U 25 X 240'

| | |
|---------------------|-----------|
| STRUCTURE APPROVAL | 3/30/2015 |
| FOUNDATION APPROVAL | 3/30/2015 |

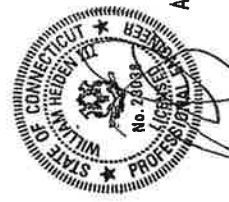
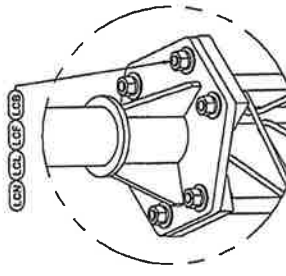
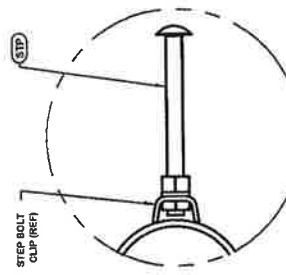
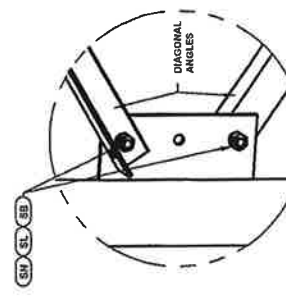
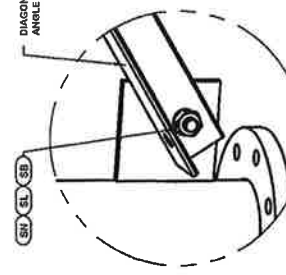
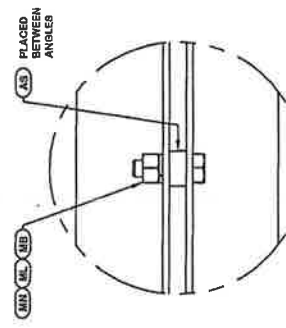
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|-----|--------------------------|-----|----|------|
| REV | DESCRIPTION OF REVISIONS | CPD | BY | DATE |
| | REVISION HISTORY | | | |

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ORIENT ANGLES WITH STAMPED
END TOWARD TOP OF SECTION



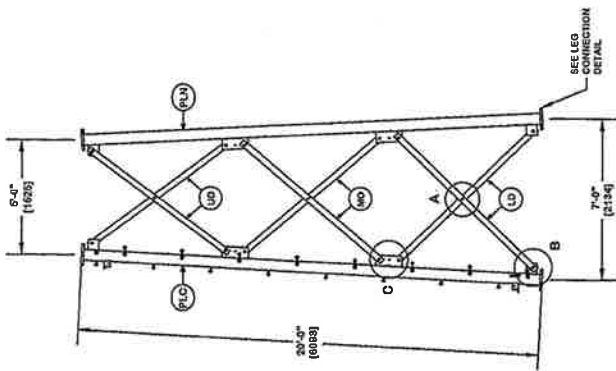
| ITEM | QTY | PART NO. | PART DESCRIPTION | UNIT WT. | NET WT. |
|----------|-----|----------|---|-----------|------------|
| FLC | 3 | 225377 | PIPE LEG SECTION 20"x6" (CLIMBING) 8" SCH. 40 V&E | 637.9 | 1813.8 |
| STP | 48 | 226189 | STEP BOLT ASSY 1/2"-11 X 7" W/ LOCK WASHER HEAVY | 1.1 | 52.8 |
| LD | 6 | 231345 | ANGLE V&B LOW 119 6032" (WAS CLIPPED) | 31.5 | 189.0 |
| MB | 9 | 227580 | 68"-11 X 3/4" 133BT HOT DIPPED GALV. BOLT /RULL | 0.8 | 7.2 |
| AS | 9 | 124636 | MID-DIAGONAL SPACER 1 1/8" HOLE 3/8" THICK | 0.5 | 4.5 |
| MN | 9 | 312501 | 58"-11 HOT DIPPED GALVANIZED NUT | 0.1 | 0.9 |
| ML | 9 | 312123 | 58" GALVANIZED LOCKWASHER (63-22230) | 0.0 | 0.0 |
| SL | 36 | 312163 | 3/4" GALVANIZED LOCKWASHER | 0.0 | 0.0 |
| SN | 36 | 312502 | 3/4"-10 HOT DIPPED GALVANIZED NUT | 0.2 | 7.2 |
| SB | 36 | 172280 | 3/4"-10 X 2" A-308 BOLT WITH 1-3/8" THREAD | 0.7 | 25.2 |
| MD | 6 | 225034 | ANGLE V&B MID 112 2692" | 30.3 | 181.8 |
| UD | 6 | 225035 | ANGLE V&B UPPER 106 2902" | 28.7 | 172.2 |
| LCB | 18 | 222016 | 1"-9 X 4-9/16" A-308 BOLT WITH 1-3/4" THREAD | 1.4 | 25.2 |
| LCF | 18 | 312222 | 1" GALVANIZED FLAT WASHER (F 490) | 0.1 | 1.8 |
| LCL | 18 | 312223 | 1" GALVANIZED LOCKWASHER | 0.1 | 1.8 |
| LCN | 18 | 312504 | 1"-8 HOT DIPPED GALVANIZED NUT | 0.4 | 7.2 |
| Total Wt | | | | 2280.3 lb | 10330.4 kg |



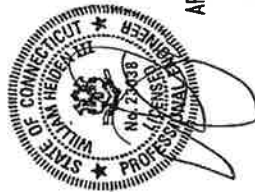
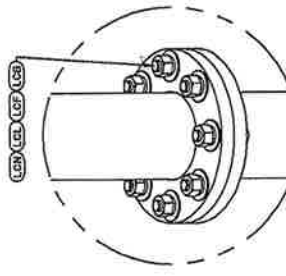
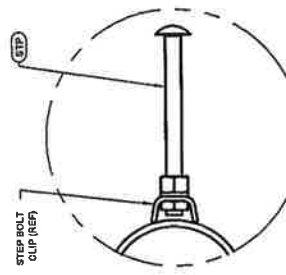
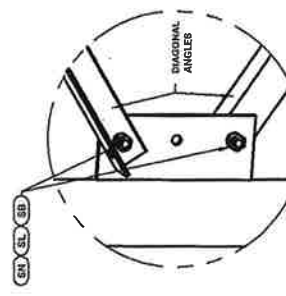
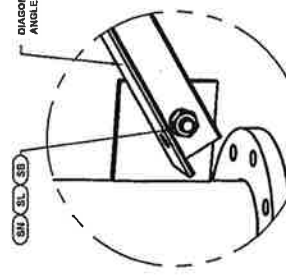
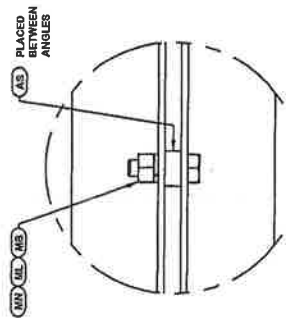
APR 01 2015

| | | | |
|--|---|---|---------------------------------|
| <p>valmont STRUCTURES</p> <p>1-877-467-4783 Plymouth, IN 1-800-647-2151 Salem, OR</p> | | <p>ENG. FILE NO. 284859</p> <p>DWG. NO. 259147T</p> | <p>PAGE 11 OF 14</p> |
| <p>DESCRIPTION</p> <p>SECTION V-9.0 (160° - 180° ELEVATION)</p> | <p>FOUNDATION APPROVAL</p> <p>3/30/2015</p> | <p>STRUCTURE APPROVAL</p> <p>3/30/2015</p> | <p>REVISION HISTORY</p> |
| <p>SITE</p> <p>ASHFORD, CT VERIZON WIRELESS U 25 X 240°</p> | <p>COPYRIGHT 2013</p> | <p>CPD</p> <p>BY</p> <p>DATE</p> | <p>DESCRIPTION OF REVISIONS</p> |

ORIENT ANGLES WITH STAMPED
END TOWARD TOP OF SECTION



| PARTS LIST | | | | UNIT WT. | NET WT. |
|------------|-----|----------|--|----------------------|---------|
| ITEM | QTY | PART NO. | PART DESCRIPTION | | |
| PLC | 1 | 226200 | PIPE LEG SECTION 20'-0" (CLIMBING) 6" SCH. 40 X 5E | 389.8 | 389.8 |
| PLN | 2 | 226201 | PIPE LEG SECTION 20'-0" (NON-CLIMBING) 6" SCH. 40 | 389.3 | 772.6 |
| STP | 16 | 228168 | STEP BOLT ASSY 68"-11 X 7" W/ LOCK WASHER HEAVY | 1.1 | 17.6 |
| LD | 6 | 228162 | ANGLE V-7 LOW 101 3/16" (W/AS CLIPPED) | 21.8 | 129.6 |
| MB | 9 | 227850 | 88"-11 X 3/4" ASSET HOT DIPPED GALV. BOLT (FULL) | 0.6 | 6.6 |
| AS | 9 | 124838 | MID-DIAGONAL SPACER 1 1/8" HOLE 3/8" THICK | 0.5 | 4.1 |
| NN | 9 | 312591 | 58"-11 HOT DIPPED GALVANIZED NUT | 0.1 | 1.1 |
| NL | 9 | 312593 | 58" GALVANIZED LOCKWASHER (S-22230) | 0.0 | 0.2 |
| SL | 36 | 312453 | 84" GALVANIZED LOCKWASHER | 0.0 | 1.1 |
| SN | 36 | 312602 | 3/4"-10 HOT DIPPED GALVANIZED NUT | 0.2 | 6.6 |
| SB | 36 | 172290 | 3/4"-10 X 2" A-325 BOLT WITH 1-3/8" THREAD | 0.7 | 24.1 |
| MD | 6 | 228169 | ANGLE V-7 MID 96 1/8" X 1 1/8" | 20.5 | 122.6 |
| UD | 6 | 228160 | ANGLE V-7 UP 90 2 7/8" | 19.4 | 118.3 |
| LCB | 24 | 312788 | 3/4"-10 X 3/4" A-325 BOLT WITH FULL THREAD | 0.6 | 13.9 |
| LCP | 24 | 312162 | 3/4" GALVANIZED FLAT WASHER (F-498) | 0.1 | 1.2 |
| LCL | 24 | 312163 | 3/4" GALVANIZED LOCKWASHER | 0.0 | 0.7 |
| LCN | 24 | 312602 | 3/4"-10 HOT DIPPED GALVANIZED NUT | 0.2 | 4.8 |
| Total Wt. | | | | 1811.8 lb (791.9 kg) | |



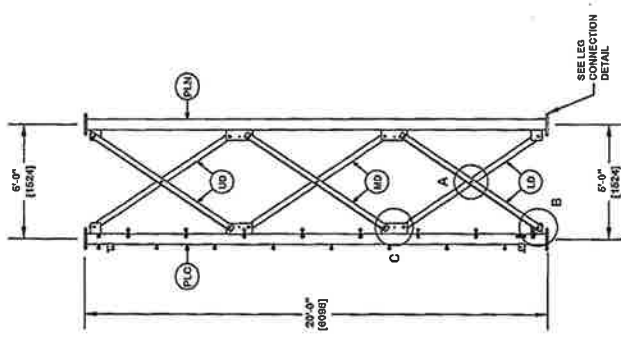
APR 01 2015

| | | |
|---|---|------------------------------|
| <p>DESCRIPTION</p> <p>SECTION V-7.0 (180' - 200' ELEVATION)</p> | <p>FOUNDATION APPROVAL</p> <p>3/30/2015</p> | <p>DATE</p> <p>3/30/2015</p> |
| <p>SITE</p> <p>ASHFORD, CT VERIZON WIRELESS U 25 X 240'</p> | <p>STRUCTURE APPROVAL</p> <p>3/30/2015</p> | <p>DATE</p> <p>3/30/2015</p> |
| <p>REV</p> | <p>DESCRIPTION OF REVISIONS</p> | <p>CPD BY</p> |
| <p>valmont STRUCTURES</p> <p>1-877-487-4763 Plymouth, IN 1-800-547-2151 Salem, OR</p> | | <p>284859</p> <p>259147T</p> |
| <p>ENG. FILE NO.</p> | | <p>PAGE</p> <p>12 OF 14</p> |

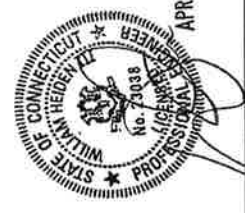
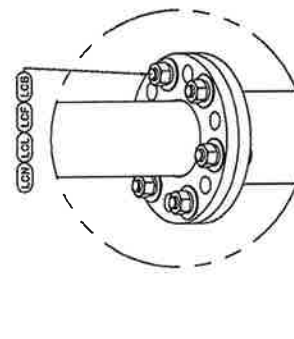
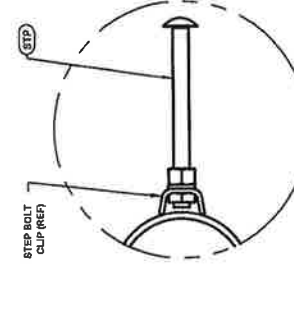
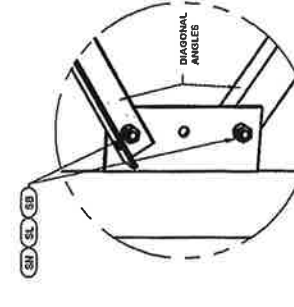
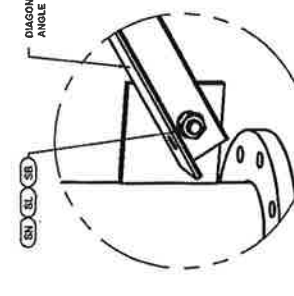
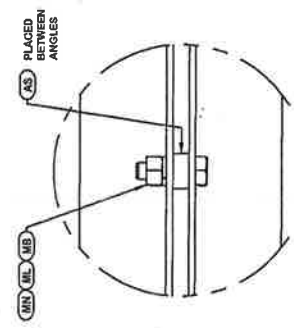
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ORIENT ANGLES WITH STAMPED END TOWARD TOP OF SECTION



| ITEM | QTY | PART NO. | PART DESCRIPTION | UNIT WT. | NET WT. |
|----------|-----|----------|---|----------------------|---------|
| PLN | 1 | 228184 | PIPE LEG SECTION 20'-0" (CLIMBING) 4" SCH. 40 USE | 302.1 | 302.1 |
| PLN | 2 | 228185 | PIPE LEG SECTION 20'-0" (NON-CLIMBING) 4" SCH. 40 | 284.7 | 586.8 |
| STP | 16 | 228189 | STEP BOLT ASSY 6/8"-11 X 7" W/ LOCK WASHER HEAVY | 1.1 | 17.6 |
| FD | 18 | 217946 | 1/4-5 DIA. H. 1/2" X 2 1/2" X 3 1/2" X 3/16" | 24.1 | 432.9 |
| ML | 9 | 312123 | 5/8" GALVANIZED LOCKWASHER (CS-22250) | 0.0 | 0.2 |
| AS | 0 | 116487 | SPACER 1/4" THICK 1 1/2" DIA HOLE | 0.3 | 2.3 |
| MB | 0 | 227650 | 5/8"-11 X 2-1/4" A325T HOT DIPPED GALV. BOLT (FULL) | 0.6 | 6.8 |
| MN | 9 | 312151 | 5/8"-11 HOT DIPPED GALVANIZED NUT | 0.1 | 1.1 |
| SN | 98 | 312153 | 3/4"-10 HOT DIPPED GALVANIZED NUT | 0.0 | 1.1 |
| SL | 36 | 172260 | 3/4"-10 X 2" A-325 BOLT WITH 1-3/8" THREAD | 0.2 | 8.6 |
| SB | 18 | 227668 | 3/4"-10 X 2-1/2" A-325 BOLT WITH FULL THREAD | 0.7 | 24.1 |
| LCB | 18 | 312162 | 3/4" GALVANIZED PLAT WASHER (F-438) | 0.1 | 1.4 |
| LCF | 18 | 312163 | 3/4" GALVANIZED LOCKWASHER | 0.0 | 0.6 |
| LCL | 18 | 312692 | 3/4"-10 HOT DIPPED GALVANIZED NUT | 0.2 | 3.4 |
| LCN | 18 | 312692 | 3/4"-10 HOT DIPPED GALVANIZED NUT | 0.2 | 3.4 |
| Total Wt | | | | 1378.3 lb (625.8 kg) | |



| REV | DESCRIPTION OF REVISIONS | CPD | BY | DATE |
|-----|--------------------------|-----|----|------|
| | REVISION HISTORY | | | |

SITE: ASHFORD, CT
VERIZON WIRELESS
U 26 X 240'

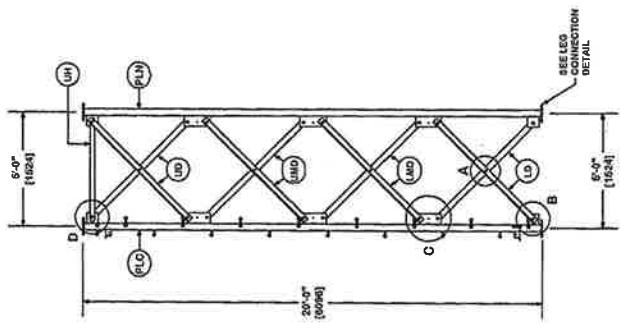
DESCRIPTION: SECTION V-5.0 (200' - 220' ELEVATION)

STRUCTURE APPROVAL: 3/30/2015
FOUNDATION APPROVAL: 3/30/2015

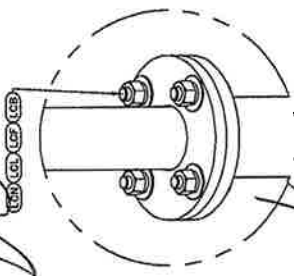
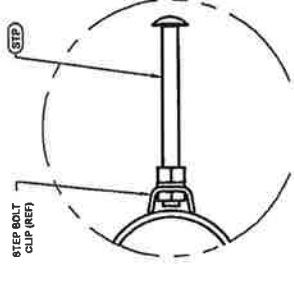
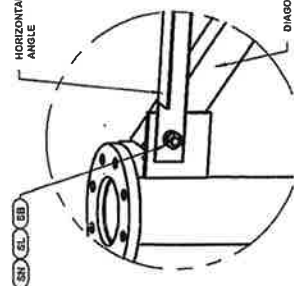
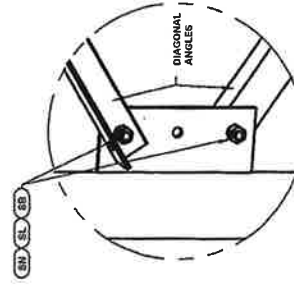
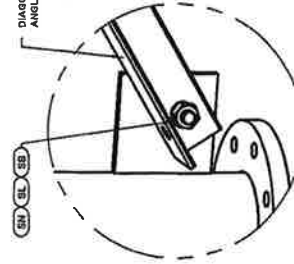
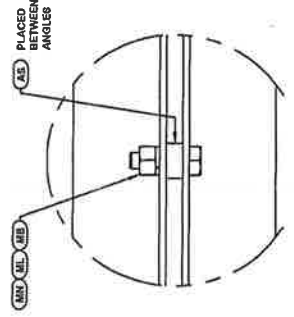
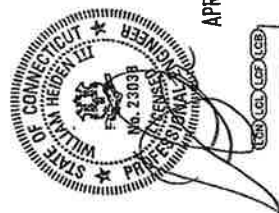
valmont STRUCTURES
1-877-467-4763 Plymouth, IN
1-800-647-2151 Salem, OR

ENG. FILE NO. 284859
DWG. NO. 2591477

INSTALL ANGLES WITH STAMPED END TOWARD TOP OF SECTION



| ITEM | QTY | PART NO. | PART DESCRIPTION | UNIT WT. | NET WT. |
|----------|-----|----------|---|---------------------|---------|
| PLG | 1 | 228180 | PIPE LEG SECTION 20'-0" (CLIMBING) 2 1/2" SCH. 40 | 184.4 | 184.4 |
| PLN | 2 | 228161 | PIPE LEG SECTION 20'-0" (NON-CLIMBING) 2 1/2" SCH. 40 | 166.2 | 332.4 |
| STP | 18 | 228189 | STEP BOLT ASSY 5/8"-11 X 7" W/ LOCK WASHER HEAVY | 1.1 | 19.8 |
| FD | 24 | 221077 | ANGLE V-5 STR 74 7/8" - 2" X 2" X 1/8" ANGLE (A38) | 10.7 | 257.0 |
| ML | 12 | 312123 | 5/8" GALVANIZED LOCKWASHER (S3-22280) | 0.0 | 0.0 |
| AS | 12 | 116467 | SPACER 1/4" THICK 1 1/8" DIA HOLE | 0.3 | 3.6 |
| MB | 12 | 227680 | 5/8"-11 X 5-1/8" A-3251 HOT DIPPED GALV. BOLT (FULL) | 0.6 | 7.2 |
| MN | 12 | 312501 | 5/8"-11 HOT DIPPED GALVANIZED NUT | 0.1 | 1.2 |
| SL | 48 | 312163 | 3/4" GALVANIZED LOCKWASHER | 0.0 | 0.0 |
| SN | 48 | 312602 | 3/4"-10 X 2" A-306 BOLT WITH 1-3/8" THREAD | 0.2 | 9.6 |
| SB | 48 | 172650 | 3/4"-10 HOT DIPPED GALVANIZED NUT | 0.7 | 32.4 |
| UH | 3 | 227684 | UPPER HORIZONTAL BRACE ANGLE FOR V-SERIES TOWER (2) | 10.8 | 32.4 |
| LB | 12 | 221668 | 3/4"-10 X 3-1/2" A-3251 BOLT WITH FULL THREAD | 0.6 | 7.2 |
| LCF | 12 | 312162 | 3/4" GALVANIZED FLAT WASHER (F-430) | 0.1 | 1.2 |
| LCL | 12 | 312163 | 3/4" GALVANIZED LOCKWASHER | 0.0 | 0.0 |
| LCN | 12 | 312602 | 3/4"-10 HOT DIPPED GALVANIZED NUT | 0.2 | 2.4 |
| Total WT | | | | 944.4 lb (428.8 kg) | |



DETAIL A ANGLE INTERSECTION CONNECTION

DETAIL B END SIDE PLATE ANGLE CONNECTION

DETAIL C MID SIDE PLATE ANGLE CONNECTION

DETAIL D UPPER HORIZONTAL ANGLE CONNECTION

STEP BOLT CLIP (REF)

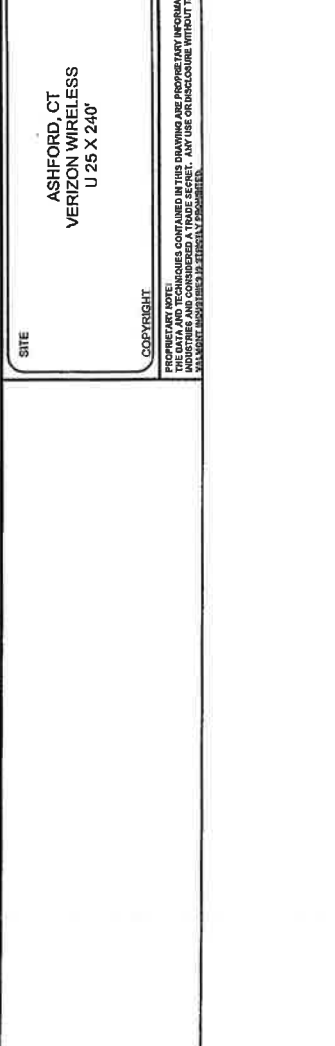
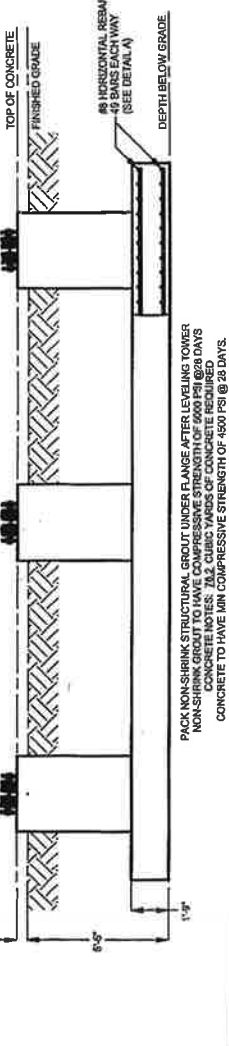
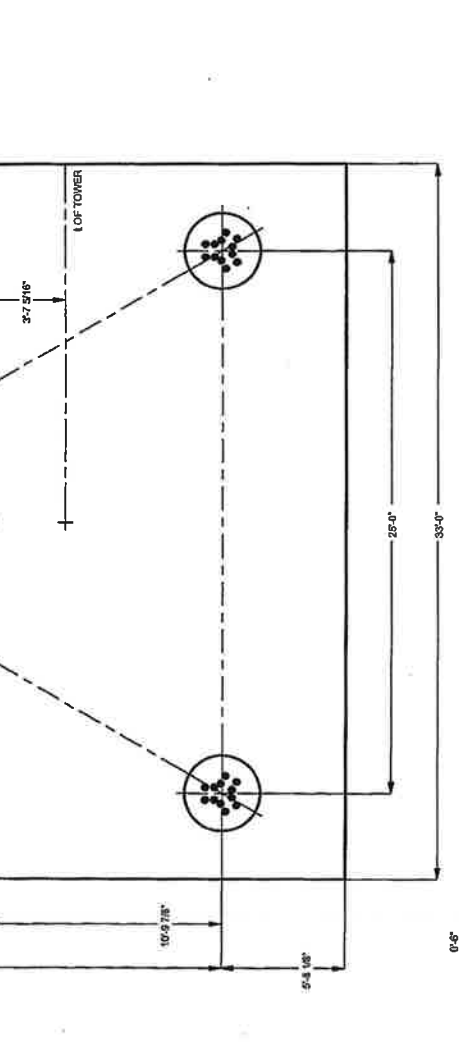
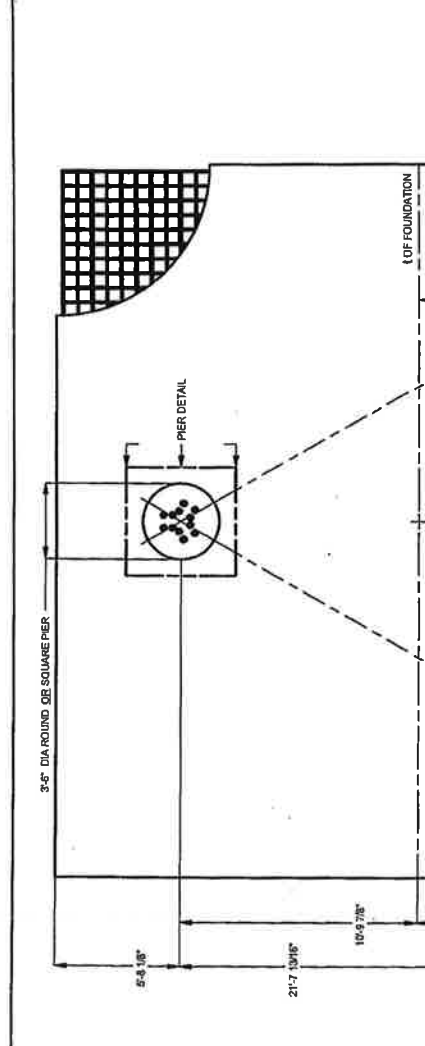
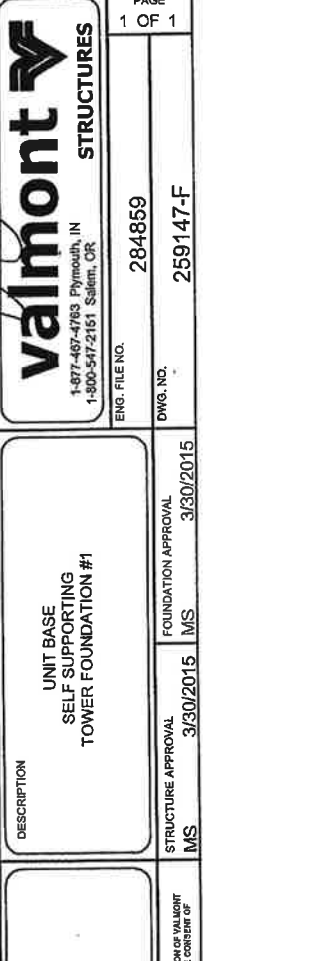
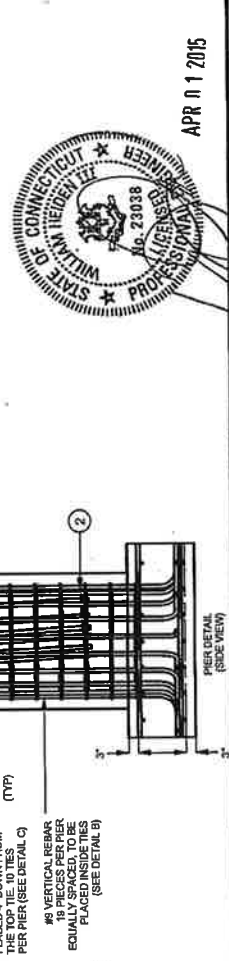
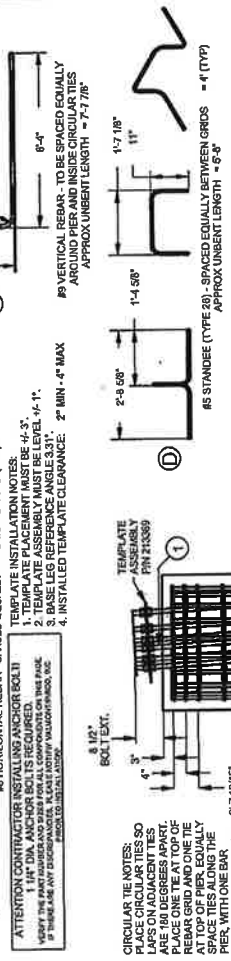
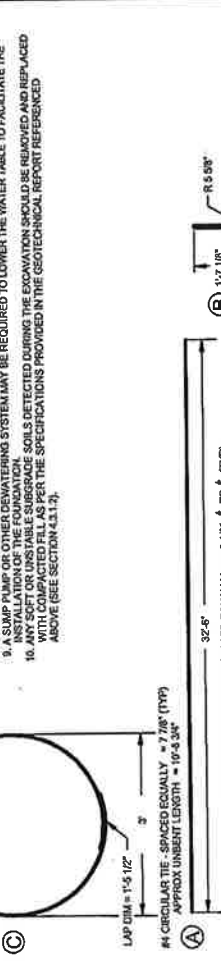
LEG TO LEG CONNECTION (SIDE PLATES NOT SHOWN FOR CLARITY)

| | | | |
|---|--|--|--|
| SITE ASHFORD, CT VERIZON WIRELESS U 25 X 240' | | DESCRIPTION SECTION V-5.0 (220' - 240' ELEVATION) | |
| STRUCTURE APPROVAL 3/30/2015 | | FOUNDATION APPROVAL 3/30/2015 | |
| REV DESCRIPTION OF REVISIONS CPD BY DATE | | REV DESCRIPTION OF REVISIONS CPD BY DATE | |
| REVISION HISTORY | | REVISION HISTORY | |
| COPYRIGHT 2013 | | ENG. FILE NO. 284859 | |
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| VALMONT STRUCTURES 1-877-467-4763 Plymouth, IN 1-800-547-2161 Salem, OR | | PAGE 14 OF 14 | |

| REBAR/ANCHOR STEEL TABLE | | | |
|--------------------------|-----|---|----------|
| ITEM | QTY | PART DESCRIPTION | UNIT WT. |
| 1 | 38 | 1 1/4" DIA. x 80" LONG ANCHOR BOLT - 103183 | 20.91 |
| 2 | 3 | EMBEDMENT PLATE - 217971 | 105.50 |
| A | 198 | HORIZONTAL REBAR (#4 REBAR) | 86.98 |
| B | 57 | VERTICAL REBAR (#8 REBAR) | 28.07 |
| C | 30 | CIRCULAR TIE (#4 REBAR) | 1485.98 |
| D | 100 | STAND-EE (#6 REBAR) | 216.31 |
| | | | 5.93 |
| | | | 592.80 |
| | | | 20200.19 |

REBAR NOTES: ALL REINFORCING BARS MUST CONFORM TO ASTM A615 GRADE 60 SPECIFICATIONS.
 APPROX TOTAL WT #

FOUNDATION NOTES:
 1. SOIL AS PER REPORT BY TERRACON, DATED 02/26/14, PROJECT#1265514.
 2. CONCRETE TO BE 4500 PSI @ 28 DAYS. REINFORCING BARS TO CONFORM TO ASTM A615 GRADE 60 SPECIFICATIONS. CONCRETE INSTALLATION TO CONFORM TO ACI 318 (2008) BUILDING REQUIREMENTS FOR REINFORCED CONCRETE. ALL CONCRETE TO BE PLACED AGAINST FORMWORK WITH A MINIMUM COVER AND ALL REINFORCEMENT TO BE PROTECTED WITH A MINIMUM COVER OF 1 1/2" IN ALL DIRECTIONS.
 3. REINFORCEMENT WELDING OF REBAR NOT PERMITTED.
 4. A COLD JOINT IS PERMISSIBLE UPON CONSULTATION WITH PROCD. ALL COLD JOINTS SHALL BE COATED WITH BONDING AGENTS PRIOR TO SECOND POUR.
 5. ALL JOINTS SHALL BE REINFORCED WITH 6" LAPS OF MORE THAN 1/4" THICK FILL MATERIALS SHOULD BE TO 50% OF MODIFIED PROCTOR MAXIMUM DRY DENSITY IN ACCORDANCE WITH ASTM D1557.
 6. BONDING, STRAIGHTENING OR REALIGNING (HOT OR COLD) OF THE ANCHOR BOLTS BY ANY METHOD IS PROHIBITED.
 7. THE ON-SITE GEOTECHNICAL ENGINEER SHALL CONFIRM THAT THE INSITU SOIL STRENGTHS MEET OR EXCEED THOSE PARAMETERS GIVEN IN THE SOIL REPORT.
 8. GRADE THE SITE TO DRAIN AWAY FROM THE TOWER.
 9. A DRAINAGE SYSTEM SHALL BE INSTALLED TO FACILITATE THE INSTALLATION OF THE FOUNDATION.
 10. ANY SOFT OR UNSATURABLE SUBGRADE SOILS DETECTED DURING THE EXCAVATION SHOULD BE REMOVED AND REPLACED WITH COMPACTED FILL AS PER THE SPECIFICATIONS PROVIDED IN THE GEOTECHNICAL REPORT REFERENCED ABOVE (SEE SECTION 4.3.1.4).



PACK NONSHRINK STRUCTURAL GROUT UNDER FLANGE AFTER LEVELING TOWER NONSHRINK GROUT TO BE PLACED AGAINST FORMWORK WITH A MINIMUM COVER AND ALL CONCRETE NOTES. TALL CUBIC YARDS OF CONCRETE REQUIRED. CONCRETE TO HAVE MIN COMPRESSIVE STRENGTH OF 4500 PSI @ 28 DAYS.

ASHFORD, CT
 VERIZON WIRELESS
 U 25 X 240"

UNIT BASE
 SELF SUPPORTING
 TOWER FOUNDATION #1

DESCRIPTION