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October 25, 2018

***VIA FEDERAL EXPRESS AND  
ELECTRONIC MAIL***

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*Siting.council@ct.gov*

Ms. Melanie A. Bachman, Esq., Executive Director  
Connecticut Siting Council  
Ten Franklin Square  
New Britain, CT 06501

**Re: Petition of T-Mobile Northeast, LLC for a Declaratory Ruling that a Certificate of Environmental Compatibility and Public Need is not Required for the Installation of a Rooftop Telecommunications Facility.**

Dear Attorney Bachman:

This office represents T-Mobile Northeast, LLC (“T-Mobile”). On behalf of T-Mobile, I have enclosed an original and fifteen (15) copies of the above-mentioned Petition for Declaratory Ruling as well as the filing fee related thereto.

Please do not hesitate to contact me with any questions.

Very truly yours,

Jesse A. Langer

Enclosures

STATE OF CONNECTICUT  
CONNECTICUT SITING COUNCIL

RE: PETITION OF T-MOBILE NORTHEAST, LLC FOR A  
DECLARATORY RULING THAT A CERTIFICATE OF  
ENVIRONMENTAL COMPATIBILITY AND PUBLIC NEED  
IS NOT REQUIRED FOR THE INSTALLATION OF A  
ROOFTOP TELECOMMUNICATIONS FACILITY

PETITION FOR DECLARATORY RULING

OCTOBER 25, 2018

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## **ATTACHMENTS**

Attachment A – Site Plan

Attachment B – Antenna Specifications

Attachment C – Structural Analysis

Attachment D – Service List of Abutters and Sample Letter to Abutters

Attachment E – Service List of Municipal Officials and Government Agencies, with Letter to Host Municipality

Attachment F – Visual Assessment and Photo-Simulations

Attachment G – EME

Attachment H – FAA Compliance Report

**STATE OF CONNECTICUT  
CONNECTICUT SITING COUNCIL**

PETITION OF T-MOBILE	:	OCTOBER 25, 2018
NORTHEAST, LLC FOR A	:	
DECLARATORY RULING THAT A	:	
CERTIFICATE OF ENVIRONMENTAL	:	
COMPATIBILITY AND PUBLIC NEED	:	
IS NOT REQUIRED FOR THE	:	
INSTALLATION OF A ROOFTOP	:	
TELECOMMUNICATIONS FACILITY	:	

**PETITION FOR DECLARATORY RULING**

In accordance with General Statutes § 4-176 (a), § 16-50k (a) and Regs., Conn. State Agencies § 16-50j-38 *et seq.*, T-Mobile Northeast, LLC (“T-Mobile”) respectfully seeks a declaratory ruling from the Connecticut Siting Council (“Council”) that a Certificate of Environmental Compatibility and Public Need is not required for the installation of a rooftop telecommunications facility (“Rooftop Facility”) proposed to be located within the midtown campus of Western Connecticut Statue University (“University”), specifically on the rooftop of the Ruth Haas Library (“Property”).<sup>1</sup>

**I. AUTHORITY FOR REQUESTED RELIEF**

General Statutes § 4-176 (a) provides that “[a]ny person may petition an agency . . . for a declaratory ruling as to the validity of any regulation, or the applicability to specified circumstances of a provision of the general statutes, a regulation, or a final decision on a matter within the jurisdiction of the agency.”<sup>2</sup> *Bingham v. Dept. of Public Works*, 286 Conn. 698, 706, 945 A.2d 927 (2008). The Council may approve a proposal concerning a telecommunications

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<sup>1</sup> The general street address for the midtown campus is 181 White Street, Danbury, Connecticut.

<sup>2</sup> General Statutes § 4-166 (9) defines “person” to mean “any individual, partnership, corporation, limited liability company, association, governmental subdivision, agency or public or private organization of any character, but does not include the agency conducting the proceeding.”

facility, or a modification to such a facility, by declaratory ruling if it determines that the proposal does not have a substantial adverse environmental effect in the State. General Statutes § 16-50k (a).

## **II. CONTACT INFORMATION**

T-Mobile is a limited liability company organized under the laws of the State of Delaware, and is duly registered with the State of Connecticut. All correspondence or communications may be addressed to T-Mobile's legal counsel as follows:

Jesse A. Langer  
Updike, Kelly & Spellacy, P.C.  
8 Frontage Road  
East Haven, CT 06512  
(203) 786-8317  
jlanger@uks.com

## **III. BACKGROUND**

### **A. The Property**

The Property consists of the Ruth Haas Library, which rests on two parcels totaling approximately fifteen acres. The Property is located in the City of Danbury ("City") within a High-Rise Residential District (RH-3). An RH-3 District is a mixed residential district, which is intended to provide for "a compatible mix of high density residential, limited commercial, institutional and neighborhood uses in the urban core of the City." *Danbury Zoning Regs.*, § 4.D.1. The immediately adjacent land use consists largely of the University, including a multi story parking garage, a concert hall and other relatively large campus buildings. Beyond the University campus are some residential and commercial properties within the City proper. Please see T-Mobile's Site Plan, specifically Page C-1, which is appended hereto as Attachment A.

## **B. The Proposed Rooftop Facility**

As a wireless carrier licensed by the Federal Communications Commission (“FCC”), T-Mobile seeks out wireless sites that will meet its coverage and capacity objectives so that T-Mobile may provide reliable coverage throughout its network. T-Mobile has identified the Ruth Haas Library building within the midtown campus at the University for a rooftop telecommunications facility to address such coverage and capacity objectives in the area.

The proposed Rooftop Facility would consist of the installation of nine (9) panel antennas on three (3) sectors and a future microwave dish, all to be mounted to the roof of the library on the Property. Please see the antenna specifications appended hereto as Attachment B. The Rooftop Facility would be located at approximately sixty-feet (60) above grade level (“AGL”). The Rooftop Facility would include a Mansard roof screening system to conceal the installation from public view. The top of the screening system would be approximately 70'4" AGL. The centerline of the panel antennas would be located at 65'5" AGL. The equipment associated with T-Mobile’s installation would be on a 10 x 12 steel platform on the parapet of the lower roof, which is approximately 48'5" AGL. The roof screening system would completely conceal this equipment. The cables connecting T-Mobile’s antennas to the attendant equipment would come from existing power and telephone service originating in the library’s basement. Please see Attachment A. The Rooftop Facility would also fall well within the loading limits of the library and, accordingly, the proposal would be structurally sound. Please see the Structural Analysis appended hereto as Attachment C.

## **IV. NOTICE TO ABUTTERS, OFFICIALS AND AGENCIES**

In accordance with § 16-50j-40 of the Regulations of Connecticut State Agencies, on October 25, 2018, T-Mobile sent a notice of its intent to file this Petition, via certified mail,

return receipt requested and regular mail, to each person appearing as a record owner of the properties which abut the Property, each person appearing as the record owner of the properties on which the Rooftop Facility would be located and the appropriate municipal officials and government agencies. A service list of abutters and a sample letter to the abutters are appended hereto as Attachment D. The service list of municipal officials and government agencies, as well as a copy of the letter sent to the host municipality, are appended hereto as Attachment E.

## **V. NO SUBSTANTIAL ADVERSE ENVIRONMENTAL EFFECT**

The proposed Rooftop Installation would not have a substantial adverse environmental effect.

### **A. Environmental Effects**

The proposed Rooftop Facility would be located on the roof of the Ruth Haas Library within the University's campus, located in midtown Danbury. The surrounding area is extensively developed and T-Mobile has submitted a proposal so as not to have a substantial adverse environmental effect.

### **B. Visual Effects**

The proposed Rooftop Facility would not have any adverse visual effects. The proposed antennas would be concealed behind a Mansard screening system to shield the installation from public view. T-Mobile has proposed a wireless site which is visually responsible and takes into account the aesthetic of the surrounding area. Please see the visual assessment and photo-simulations, which are appended hereto as Attachment F.

### **C. Compliance with the FCC**

The proposed Rooftop Facility would comply with the limits for maximum permissible exposure ("MPE") as promulgated by the FCC. Please see the Radio Frequency -

Electromagnetic Energy Compliance Report appended hereto as Attachment G. As the Report demonstrates, the proposed facility would be well below the MPE limits set by the FCC.

**D. Compliance with the Federal Aviation Authority**

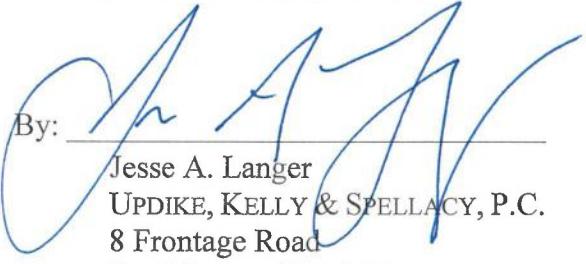
The proposed Rooftop Facility would not constitute a hazard to air navigation and otherwise require any additional measures or authorizations from the Federal Aviation Authority (“FAA”). Please see FAA Compliance Report appended hereto as Attachment H.

**VI. CONCLUSION**

This Petition and the appended attachments demonstrate that the proposed Rooftop Facility would not have a substantial adverse environmental effect. Therefore, a Certificate of Environmental Compatibility and Public Need is not required in accordance with the General Statutes § 16-50k.

Respectfully submitted by,

T-MOBILE NORTHEAST LLC

By: 

Jesse A. Langer  
UPDIKE, KELLY & SPELLACY, P.C.  
8 Frontage Road  
East Haven, CT 06512  
(203) 786-8310  
Email: jlanger@uks.com

**ATTACHMENT A**

**Site Plan**

# ••T••Mobile

## WIRELESS COMMUNICATIONS FACILITY

### WCSU DANBURY

### SITE ID: CTFF039A

### 181 WHITE STREET

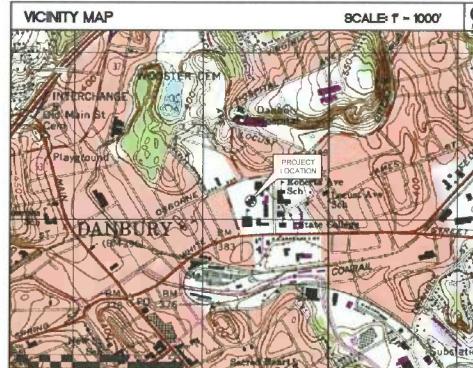
### DANBURY, CT 06810

#### GENERAL NOTES

- ALL WORK SHALL BE IN ACCORDANCE WITH THE 2012 INTERNATIONAL BUILDING CODE AS MODIFIED BY THE 2016 CONNECTICUT SUPPLEMENT, INCLUDING THE IBC/EA-222 REVISION "G" STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWER AND SUPPORT STRUCTURES, 2018 CONNECTICUT FIRE SAFETY CODE, NATIONAL ELECTRICAL CODE AND LOCAL ORDINANCES.
- CONTRACTOR SHALL REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL NOT SHIFT THE ATTENTION OF THE T-MOBILE CONSTRUCTION TEAM DURING THE BIDDING PROCESS. THE CONTRACTOR SHALL NOT SHIFT SUBCONTRACTORS AND ALL RELATED PARTIES. THE SUBCONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
- CONTRACTOR SHALL PROVIDE A COMPLETE BUILD-OUT WITH ALL DRAWDOWNS, STANCHIONS, TRENCHES, AND ELEVATED CONCRETE AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON THE DRAWINGS OR IN THE WRITTEN SPECIFICATIONS.
- CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT EQUIPMENT AND MATERIALS FOR THE CONSTRUCTION AND ELEVATED CONCRETE AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON THE DRAWINGS OR IN THE WRITTEN SPECIFICATIONS.
- CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE ISSUANCE OF PERMITS AND INSPECTIONS. THE CONTRACTOR SHALL PAY FOR THE ISSUANCE OF PERMITS AND INSPECTIONS AS PROVIDED IN THE CONTRACT.
- CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS AND SPECIFICATIONS ON SITE AT ALL TIMES AND INSURE DISTRIBUTION OF NEW DRAWINGS TO SUBCONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE ISSUED. ALL DRAWINGS AND SPECIFICATIONS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. THE CONTRACTOR SHALL FURNISH AN "AS-BUILT" SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
- LOCATION OF EQUIPMENT, ANTI-THEFT EQUIPMENT, AND OTHER EQUIPMENT SHALL BE DETERMINED BY THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE LOCATIONS AND DIMENSIONS SUBJECT TO STRUCTURAL CONDITIONS AND APPROVALS BY THE CONTRACTOR.
- THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURES AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE USE OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY.
- DRAWDINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL BE RESPONSIBLE FOR CORRECTING THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
- ALL UTILITY WORK SHALL BE IN ACCORDANCE WITH LOCAL UTILITY COMPANY REQUIREMENTS AND SPECIFICATIONS.

#### SITE DIRECTIONS

FROM:	TO:
FROM: 32 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06020	TO: 181 WHITE STREET DANBURY, CT 06810
1. START OUT GOING NORTH ON GRIFFIN RD S TOWARD HARTMAN RD;	0.30 MI
2. TAKE 2ND RIGHT ONTO DAY HILL RD;	0.14 MI
3. TAKE 1ST RIGHT ONTO BLUE HILLS AVENUE EXIT CT-187, CONTINUE TO FOLLOW CT-187;	1.89 MI
4. TURN LEFT ONTO CT-305/OLD WINDSOR RD. CONTINUE TO FOLLOW CT-305.	2.33 MI
5. MERGE ONTO I-84 N TOWARD NEW YORK CITY.	5.66 MI
6. MERGE ONTO I-84 W VIA EXIT 32A TOWARD WATERBURY.	13.29 MI
7. TAKE 1ST RIGHT ONTO Rte 84 TOWARD WATERBURY.	40.71 MI
8. MERGE ONTO NEWTON ROAD EXIT TOWARD BETHEL.	1.27 MI
9. NEWTON ROAD BECOMES WHITE STREET.	0.69 MI
12. END AT 181 WHITE STREET ON THE LEFT.	



#### PROJECT SUMMARY

- THE PROPOSED SCOPE OF WORK CONSISTS OF THE INSTALLATION OF A PROPOSED UNMANNED TELECOMMUNICATIONS FACILITY INCLUDING THE FOLLOWING:
  - INSTALLATION OF (3) NEW T-MOBILE PANEL ANTENNAS PER SECTOR (AND ASSOCIATED APPURTENANCES), (3) SECTORS FOR A TOTAL OF (9) PANEL ANTENNAS AND (1) FUTURE MICROWAVE DISH.
  - ALL SECTOR ANTENNAS TO BE MOUNTED TO, AND BEHIND, A PROPOSED MANSARD ROOF SCREENING SYSTEM ATOP THE HIGH ROOF OF THE EXISTING BUILDING. THE COLOR OF THE SCREENING SHALL BE PRESENT AT EACH ANTENNA SECTOR LOCATION AND WILL MATCH THE COLOR AND ARCHITECTURAL APPEARANCE OF THE EXISTING MANSARD SCREENING ON THE HIGH ROOF.
  - EXPOSED CABLES AND/OR CABLE TRAY SHALL BE PAINTED TO MATCH THE COLOR OF THE EXISTING BUILDING FAÇADE.
  - A 10'x12' STEEL EQUIPMENT PLATFORM IS PROPOSED ON THE EXISTING BUILDING'S LOW-HIGHT ROOF.
  - ELECTRICAL AND TELCO UTILITIES SHALL BE ROUTED TO THE PROPOSED EQUIPMENT LOCATION FROM EXISTING UTILITY DEMARCS LOCATED WITHIN THE EXISTING BUILDING'S BASEMENT LEVEL.

#### PROJECT INFORMATION

SITE NAME: DANBURY  
SITE ID: CTFF039A  
SITE ADDRESS: 181 WHITE STREET  
DANBURY, CT 06810  
PARCEL ID(S): H132360000  
J135010000

ZONE: R3

APPLICANT: T-MOBILE NORTHEAST, LLC  
55-2 NORTH BRADFORD  
BLOOMFIELD, CT 06002  
DAN REED (PROJECT MANAGER)  
TRANSCEND WIRELESS, LLC  
(203) 592-8291

CONTACT PERSON: DAN REED (PROJECT MANAGER)  
TRANSCEND WIRELESS, LLC  
(203) 592-8291  
ENGINEER: CENTER ENGINEERING, INC.  
63-2 NORTH BRADFORD RD.  
BRADFORD, CT 06402  
PROJECT COORDINATES: LATITUDE: 41° 24' -03.721" N  
LONGITUDE: 72° 40' -070.892" W  
GROUND ELEVATION: 362.537' A.M.S.L.  
COORDINATES AND GROUND ELEVATION  
REFERRED FROM FAA 2-C CERTIFICATION  
PREPARED FOR T-MOBILE NORTHEAST, LLC BY  
CENTER ENGINEERING, INC., DATED MAY 5, 2018.

#### SHEET INDEX

SHT. NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	E
C-1	SITE LOCATION PLAN	E
C-1A	ABUTTERS MAP	E
C-1B	ABUTTERS LIST	E
C-2	ROOF PLAN AND ELEVATIONS	E
C-3	BUILDING ELEVATION	E
C-4	EQUIPMENT & ANTENNA SPECIFICATIONS AND DETAILS	E
S-1	EQUIPMENT PLATFORM PLANS AND DETAILS	E
S-2	MANSARD ROOF SCREENING PLAN AND DETAILS	E

PROFESSIONAL ENGINEER'S SIGNATURE	PROFESSIONAL ENGINEER'S NAME
STATE OF CONNECTICUT PROFESSIONAL ENGINEER'S SIGNATURE	
PROFESSIONAL ENGINEER'S NAME	

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PROFESSIONAL ENGINEER'S NAME	

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DANBURY, CT 06810

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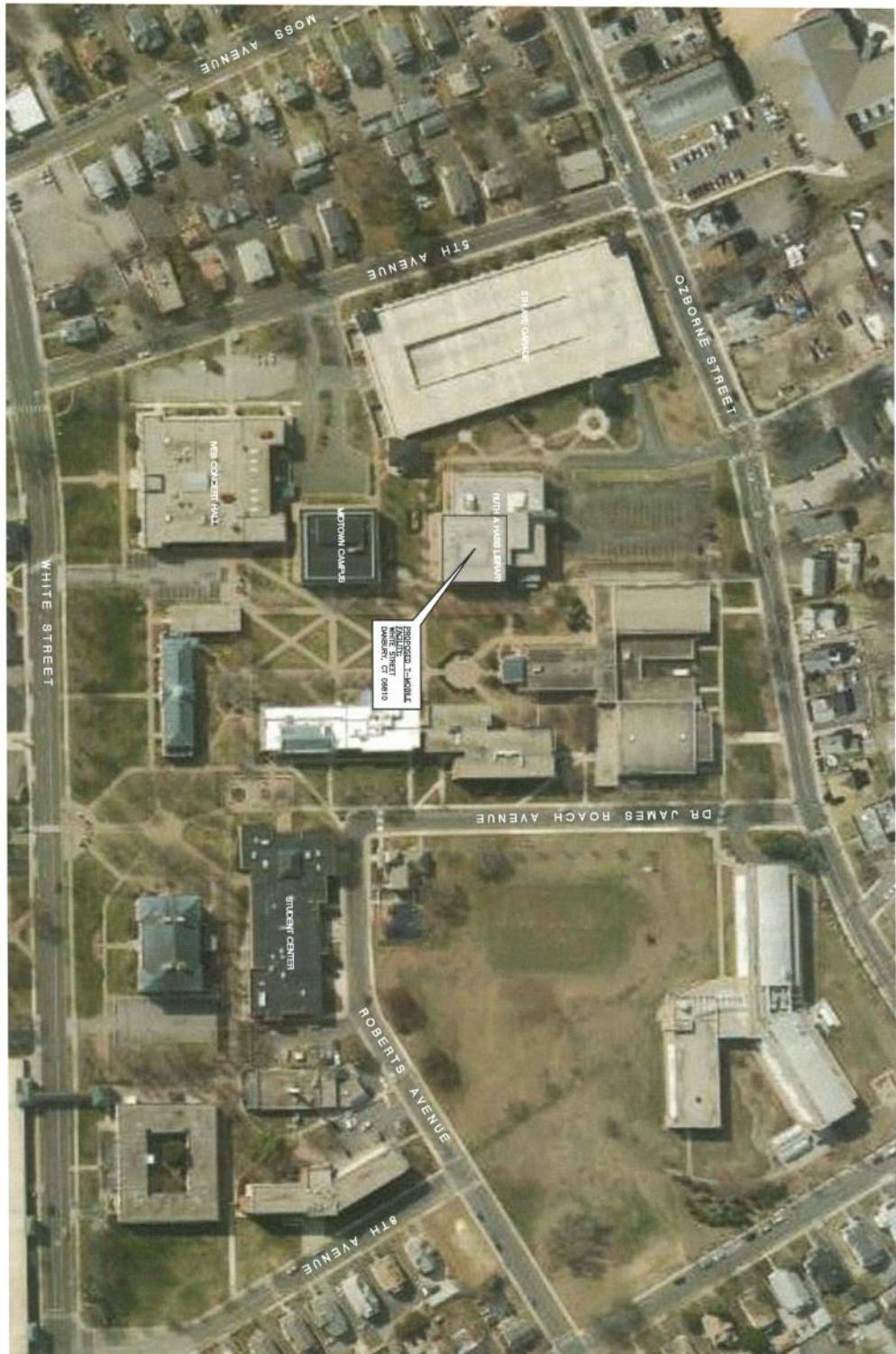
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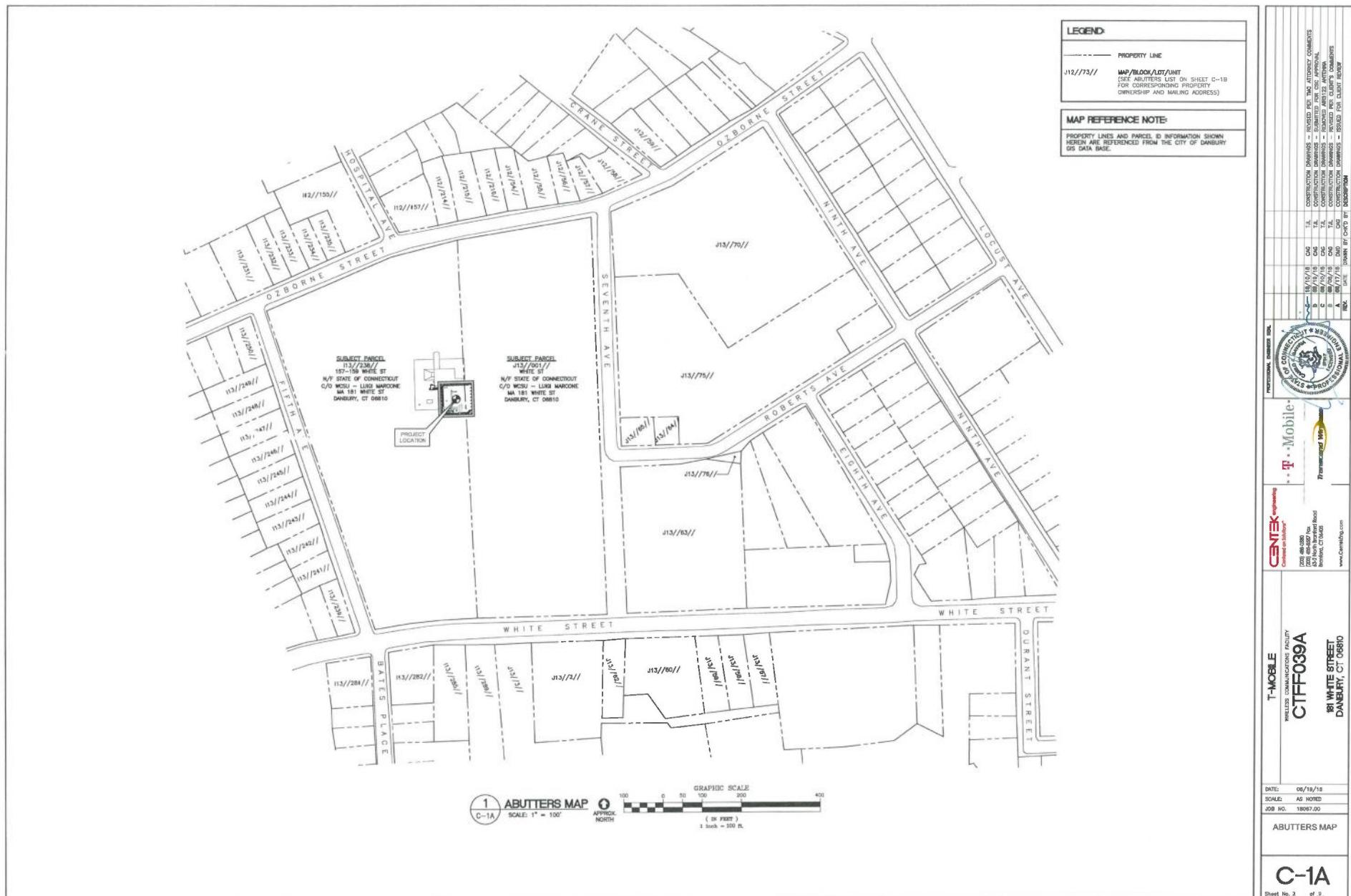
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DANBURY, CT 06810

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WIRELESS COMMUNICATIONS FACILITY  
181 WHITE STREET  
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**1 SITE LOCATION PLAN**  
 C-1  
 SCALE: 1" = 70'  
 (1 in. = 70 ft.)  
 NORTH  
 GRAPHIC SCALE



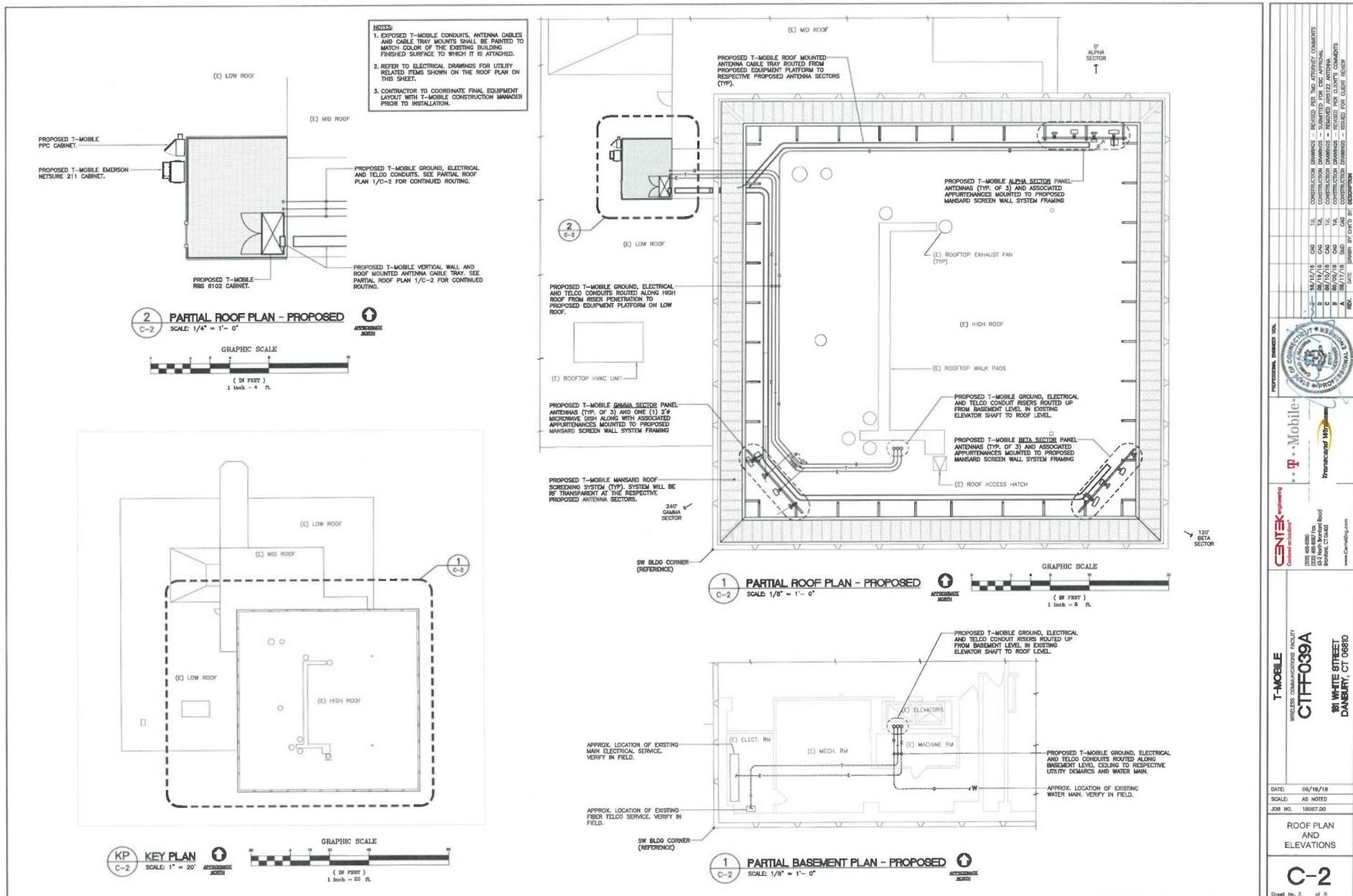
<b>T-MOBILE</b> WIRELESS COMMUNICATIONS FACILITY <b>CTFF039A</b>		<b>CENTEK engineering</b> Centek on Solutions™ (203) 488-0280 (203) 488-0287 Fax 532 North Bradford Road Brentwood, CT 06432 <a href="http://www.CentekEng.com">www.CentekEng.com</a>	<b>TRANSCEND WIRELESS</b>	<b>PROFESSIONAL ENGINEER'S SEAL</b>
DATE: 06/17/18 SCALE: AS NOTED JOB NO. 18087-002 SITE LOCATION PLAN	<b>T-Mobile</b>			REV. DATE DRAWN BY CHGD BY DESCRIPTION A 06/17/18 CAD TAL CONSTRUCTION DRAWINGS - ISSUED FOR TWO ATTORNEY COMMENTS B 06/17/18 CAD TAL CONSTRUCTION DRAWINGS - SUBMITTED FOR CSC APPROVAL B 06/17/18 CAD TAL CONSTRUCTION DRAWINGS - REMOVED AIR8122 ANTENNA A 06/08/18 CAD CAD CONSTRUCTION DRAWINGS - REVISED PER CLIENT'S COMMENTS A 06/17/18 CAD CAD CONSTRUCTION DRAWINGS - ISSUED FOR CLIENT REVIEW

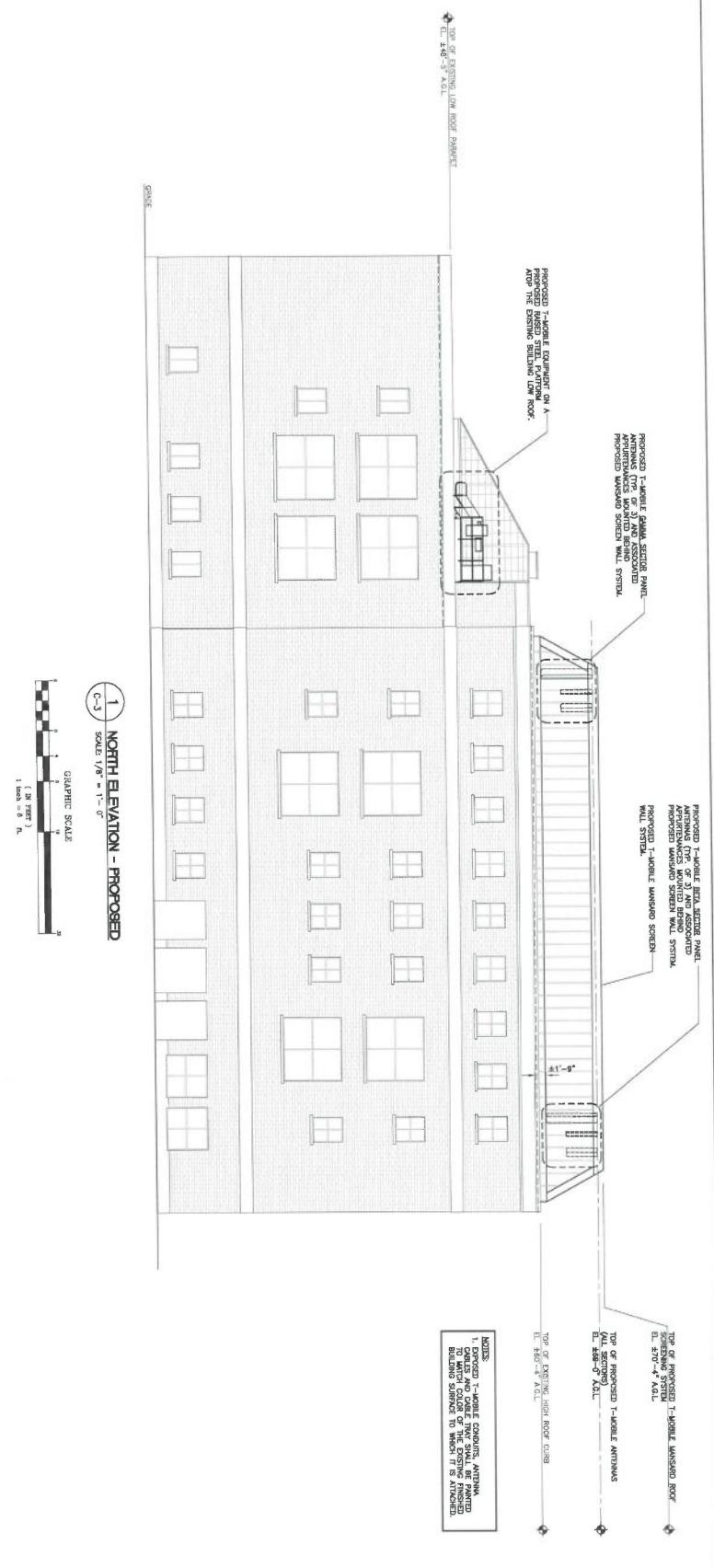


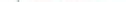
ABUTTER LIST REFERENCE NOTE

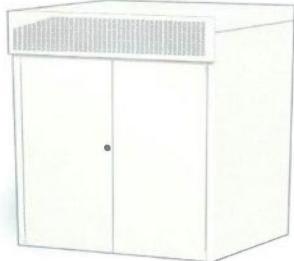
PROPERTY OWNERSHIP AND MAILING ADDRESS INFORMATION  
SHOWN HEREIN ARE PROVIDED BY THE CITY OF  
DETROIT, MICHIGAN.

<b>T-MOBILE</b> WIRELESS COMMUNICATIONS FACILITY <b>CTFF039A</b>		<b>CENTEK engineering</b> Centek on Solutions™	 <i>Transcend Wireless</i>	
DATE 08/17/18	SHEET 001/02	REV. AS-NOTED 100-02	16 08/10/18 CAD TAB CONSTRUCTION DRAWINGS - REVISED PER TMO ATTORNEY COMMENTS D 08/19/18 CAD TAB CONSTRUCTION DRAWINGS - SUBMITTED FOR CSC APPROVAL C 09/12/18 CAD TAB CONSTRUCTION DRAWINGS - REMOVED A102 22 ANTENA B 09/05/18 CAD TAB CONSTRUCTION DRAWINGS - REVISED PER CLIENT'S COMMENTS A 09/10/18 CAD TAB CONSTRUCTION DRAWINGS - ISSUED FOR CLIENT REVIEW	DATE DRAWN BY CEN'K B ST DESCRIPTION
<b>ABUTTERS LIST</b>				



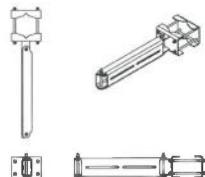


<b>T-MOBILE</b>		 Certified on Solutions™	  
WIRELESS COMMUNICATIONS FACILITY	CTFF039A		
161 WHITE STREET DANBURY, CT 06810		 PROFESSIONAL ENGINEER SEAL STATE OF CONNECTICUT DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS PROFESSIONAL ENGINEER LICENSED	
DATE:	06/19/18	16/06/18	CONSTRUCTION DRAWINGS - REVISED FOR THE ATTORNEY COMMENTS
EXPIRE:	AS NOTED	09/19/18	CONSTRUCTION DRAWINGS - SUBMITTED FOR CSC APPROVAL
JOB NO.:	160729	09/19/18	CONSTRUCTION DRAWINGS - REVISED AIRS112 ANTENNA
BUILDING ELEVATION		09/19/18	CONSTRUCTION DRAWINGS - REVISED FOR CLIENT'S COMMENTS
		08/17/18	CONSTRUCTION DRAWINGS - ISSUED FOR CLIENT REVIEW
REV.		BY CAG	BY CSC BY
			DESCRIPTION



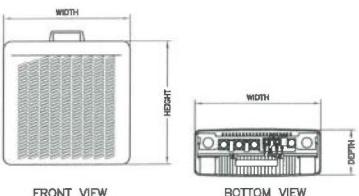
EQUIPMENT CABINET		DIMENSIONS	WEIGHT
EQUIPMENT			
MAKE: ERICSSON MODEL: 8102		87. "W x 51.18" H x 27.56" D	727.53-LBS

3 ERICSSON RADIO CABINET PARTS  
C-4 SCALE: NTS



RRU DUAL SWIVEL MOUNT		
EQUIPMENT	DIMENSIONS	WEIGHT
MADE: PART NO.: SITE PRO 1 RRUSM3A	27.75" L x 6.5" W x 4.7" D	30.4 LBS.

4 RRH DUAL SWIVEL MOUNT DETAIL  
C-4 NOT TO SCALE



FRONT VIEW

### BOTTOM VIEW

RRH (REMOTE RADIO HEAD)		
EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: ERICSSON MODEL: RRU 4446 B27+812	14.9" H x 13.2" W x 10.4" D	±74 LBS
MAKE: ERICSSON MODEL: RRU 4415 B25	16.5" H x 13.4" W x 5.9" D	±46 LBS
MAKE: ERICSSON MODEL: RRU 2217 B65A	13.8" H x 11.7" W x 4.4" D	±26.2 LBS

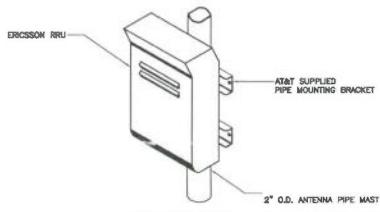
**NOTES:**

- 1. CONTRACTOR TO COORDINATE FINAL EQUIPMENT MODEL SELECTION WITH T-MOBILE CONSTRUCTION MANAGER PRIOR TO ORDERING.

**NOTES:**

1. CONTRACTOR TO COORDINATE FINAL EQUIPMENT MODEL SELECTION WITH T-MOBILE CONSTRUCTION MANAGER PRIOR TO ORDERING.
2. REFER TO RRU MANUFACTURER FOR REQUIRED INSTALLATION CLEARANCE REQUIREMENTS.

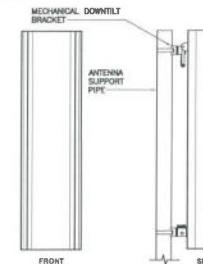
2 REMOTE RADIO HEAD (RRH) DETAIL (TYP)  
C-4 SCALE: NTS



**NOTES:** ISOMETRIC VIEW

1. T-MOBILE MOBILE SUPPLY RRU, AND RRU POLE-MOUNTING BRACKET. CONTRACTOR SHALL SUPPLY POLE/PIPE AND INSTALL ALL MOUNTING HARDWARE INCLUDING ERICSSON RRU POLE-MOUNTING BRACKET. CONTRACTOR SHALL INSTALL RRU AND MAKES CABLE TERMINATIONS.
2. NO PAINTING OF THE RRU OR SOLAR SHIELD IS ALLOWED.

**5** TYPICAL RRU MOUNTING DETAIL  
C-4 SCALE: NTS

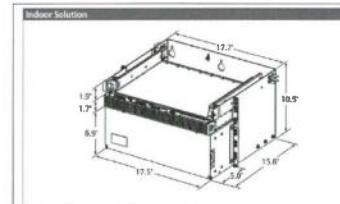


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ALPHA/BETA/GAMMA/DELTA ANTENNA EQUIPMENT	DIMENSIONS	WEIGHT	POSITION
MAKE: MODEL: ERICSSON AIR3246 B86	58.1" H x 15.7" W x 9.4" D	180-LBS	2
MAKE: MODEL: RFS APX160WV-E-180WVS-E-A20	55.9" H x 13.0" W x 3.15" D	40.7-LBS	3
MAKE: MODEL: RFS APXWV24-43-U-NA20	95.9" H x 24" W x 8.7" D	153-LBS	4

1 PROPOSED ANTENNAS SCHEDULE  
C-4 SCALE: NTS



Electrical	Indoor Solution	Outdoor Solution
System Voltage, Nominal	120 VAC single phase	19" ITU up to 8 A
Output Voltage	-42 VDC to -58 VDC	0.4 kW @ 120 VAC
System Capacity	19" ITU up to 10 A	19" ITU up to 10 position GMT type face panel
Rectifier Capacity	0.5 kW @ 120 VAC	19" ITU up to 15 A
DC Distribution	19" ITU up to 10 position GMT type face panel	
Controller	SCU+ controller	
<b>Physical Characteristics:</b>		
Framework Type	Rack in rack	Front/Bottom Compact Enclosure
Available Space	18" x 19" W	18" x 19" W
Dimensions (H x W x D)	DC power system: 1.7" x 19" x 12" (Solenoid: 10.5" x 19" x 15"	Enclosure: 24" x 24" x 16" battery tray: 22" x 13" D
Mounting	Rack or wall mount	Wall or front panel, per request
Weight, Equipped	System: 35.5 lbs. w/out batteries Front 4" batteries: 36 lbs. total	Enclosure: 61 lbs. w/out batteries Front 4" batteries: 35 lbs. total
Access	Front for batteries, control and distribution, rear for AC	Front
<b>Environmental:</b>		
Climate System	Fan-cooled front to rear	Heat Exchanger
Operating Temp.	-40 °C to +75 °C	> 0 °C to +52 °C
Storage Temp.	-40 °C to +75 °C	> -40 °C to +75 °C
Relative Humidity	0% to 95% non-condensing	100%
BILL/RFI	Conforms to FCC rules Part 15, Subpart B, Class B and EN55022	
Safety Compliance	UL60950 recognized IEC60950 Level 3 Compliance	UL60950 Recognized IEC60950 Level 3 IEC62368-1 IEC62368-2-487

6 EMERSON NETSURE 211 POWER SYSTEM  
C-4 SCALE: NTS



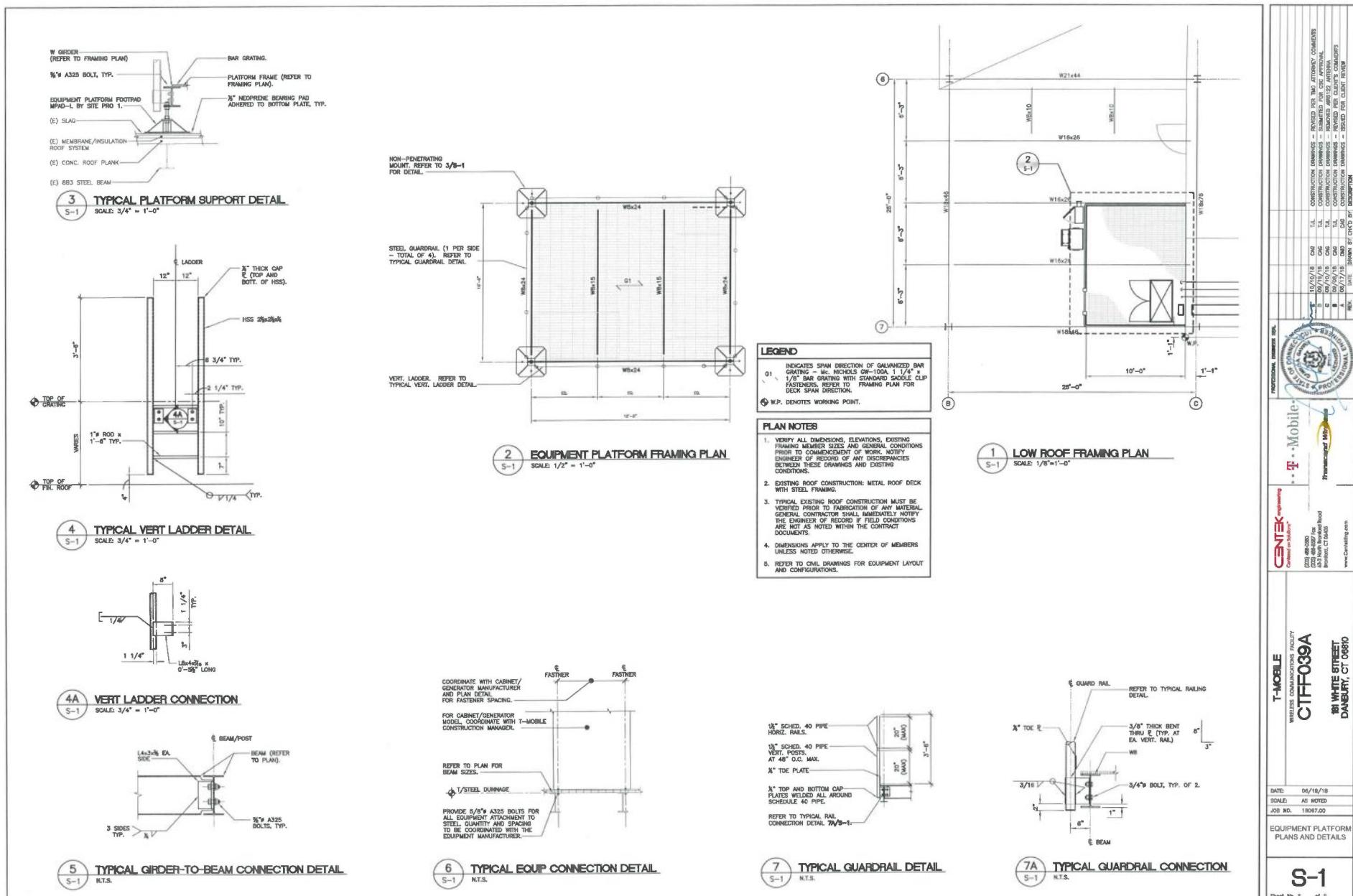
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CTFF039A  
181 WHITE STREET  
MANHATTAN, NY 10007  
181 WHITE STREET  
WANBURY, CT 06890

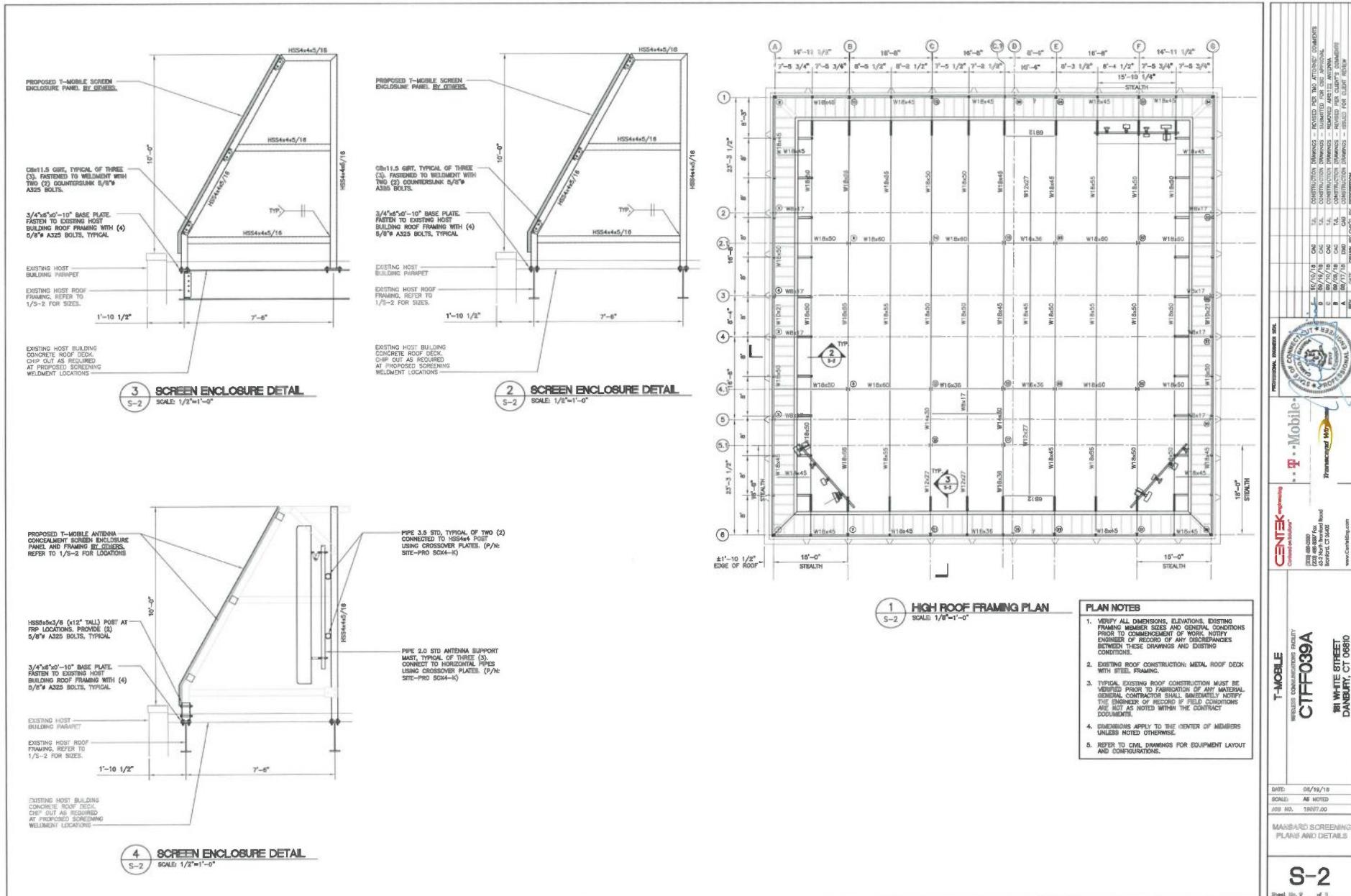
DATE:	06/19/18
SCALE:	AS NOTED
JOB NO.	180617-00

EQUIPMENT & ANTENN  
SPECIFICATIONS AND  
DETAILS

C-4

Sheet No. 7 of 9





**ATTACHMENT B**

Antenna Specifications



## Dual Slant Polarized Quad Band (8 Port) Antenna, 617-746/617-746/1695-2200/1695-2200MHz, 65deg, 15/15/18/18dBi, 2.4m (8ft), VET, RET, 0-12°/0-12°/2-12°/2-12°

### FEATURES / BENEFITS

This antenna provides a 8 Port multi-band flexible platform for advanced use for flexible use in deployment scenarios for encompassing 600MHz, 700MHz, AWS & PCS applications.



- 24 Inch Width For Easier Zoning
- Field Replaceable (Integrated) AISG RET platform for reduced environmental exposure and long lasting quality
- Superior elevation pattern performance across the entire electrical down tilt range
- Includes three AISG RET motors - Includes 0.5m AISG jumper for optional daisy chain of two high band RET motors for one single AISG point of high band tilt control.
- Low band arrays driven by a single RET motor

### Technical Features

#### LOW BAND LEFT ARRAY (617-746 MHZ) [R1]

Frequency Band	MHz	617-698	698-746
Gain	dBi	15.1	15.5
Horizontal Beamwidth @3dB	Deg	65	62
Vertical Beamwidth @3dB	Deg	11.4	10.4
Electrical Downtilt Range	Deg	0-12	0-12
Upper Side Lobe Suppression 0 to +20	dB	19	20
Front-to-Back, at +/-30°, Copolar	dB	25	24
Cross Polar Discrimination (XPD) @ Boresight	dB	19	19
Cross Polar Discrimination (XPD) @ +/-60	dB	5	3
3rd Order PIM 2 x 43dBm	dBc		-153
VSWR	-	1.5:1	1.5:1
Cross Polar Isolation	dB	25	25
Maximum Effective Power per Port	Watt	250	250

#### LOW BAND RIGHT ARRAY (617-746 MHZ) [R2]

Frequency Band	MHz	617-698	698-746
Gain	dBi	14.8	15.1
Horizontal Beamwidth @3dB	Deg	65	62
Vertical Beamwidth @3dB	Deg	11.4	10.3
Electrical Downtilt Range	Deg	0-12	0-12
Upper Side Lobe Suppression 0 to +20	dB	19	20
Front-to-Back, at +/-30°, Copolar	dB	25	23
Cross Polar Discrimination (XPD) @ Boresight	dB	19	19
Cross Polar Discrimination (XPD) @ +/-60	dB	5	3
3rd Order PIM 2 x 43dBm	dBc		-153
VSWR	-	1.5:1	1.5:1
Cross Polar Isolation	dB	25	25
Maximum Effective Power per Port	Watt	250	250



**Dual Slant Polarized Quad Band (8 Port) Antenna, 617-746/617-746/1695-2200/1695-2200MHz, 65deg, 15/15/18/18dBi, 2.4m (8ft), VET, RET, 0-12°/0-12°/2-12°/2-12°**

**HIGH BAND LEFT ARRAY (1695-2200 MHZ) [B1]**

Frequency Band	MHz	1695-1880	1850-1990	1920-2200
Gain	dBi	17.3	17.8	18.5
Horizontal Beamwidth @3dB	Deg	66	59	59
Vertical Beamwidth @3dB	Deg	5.3	4.7	4.3
Electrical Downtilt Range	Deg	2-12	2-12	2-12
Upper Side Lobe Suppression 0 to +20	dB	15	15	15
Front-to-Back, at +/-30°, Copolar	dB	25	25	25
Cross Polar Discrimination (XPD) @ Boresight	dB	19	17	16
Cross Polar Discrimination (XPD) @ +/-60	dB	4	6	4
3rd Order PIM 2 x 43dBm	dBc	-153	-153	-153
VSWR	-	1.5:1	1.5:1	1.5:1
Cross Polar Isolation	dB	25	25	25
Maximum Effective Power per Port	Watt	250	250	250

**HIGH BAND RIGHT ARRAY (1695-2200 MHZ) [B2]**

Frequency Band	MHz	1695-1880	1850-1990	1920-2200
Gain	dBi	17.1	17.8	18.5
Horizontal Beamwidth @3dB	Deg	66	59	59
Vertical Beamwidth @3dB	Deg	5.2	4.7	4.3
Electrical Downtilt Range	Deg	2-12	2-12	2-12
Upper Side Lobe Suppression 0 to +20	dB	15	15	15
Front-to-Back, at +/-30°, Copolar	dB	25	24	25
Cross Polar Discrimination (XPD) @ Boresight	dB	20	17	16
Cross Polar Discrimination (XPD) @ +/-60	dB	4	6	5
3rd Order PIM 2 x 43dBm	dBc	-153	-153	-153
VSWR	-	1.5:1	1.5:1	1.5:1
Cross Polar Isolation	dB	25	25	25
Maximum Effective Power per Port	Watt	250	250	250



## Dual Slant Polarized Quad Band (8 Port) Antenna, 617-746/617-746/1695-2200/1695-2200MHz, 65deg, 15/15/18/18dBi, 2.4m (8ft), VET, RET, 0-12°/0-12°/2-12°/2-12°

### ELECTRICAL SPECIFICATIONS

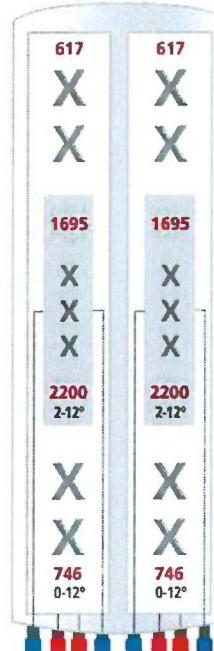
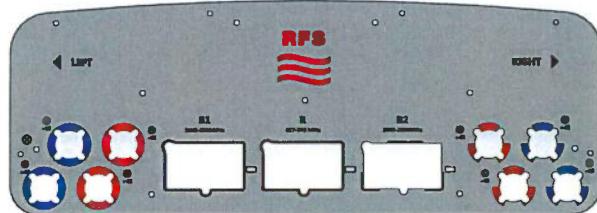
Impedance	Ohm	50.0
Polarization	Deg	±45°

### MECHANICAL SPECIFICATIONS

Dimensions - H x W x D	mm (in)	2436 x 609 x 222 (95.9 x 24 x 8.7)
Weight (Antenna Only)	kg (lb)	58 (128)
Weight (Mounting Hardware only)	kg (lb)	11.5 (25.3)
Shipping Weight	kg (lb)	80 (176)
Connector type		8 x 4.3-10 female at bottom + 6 AISG connectors (3 male, 3 female)
Adjustment mechanism		Integrated RET solution AISG compliant (Field Replaceable) + Manual Override + External Tilt Indicator
Mounting Hardware Material		Galvanized steel
Radome Material / Color		Fiber Glass / Light Grey RAL7035

### TESTING AND ENVIRONMENTAL

Temperature Range	°C (°F)	-40 to 60 (-40 to 140)
Lightning protection		IEC 61000-4-5
Survival/Rated Wind Velocity	km/h	241 (150)
Environmental		ETSI 300-019-2-4 Class 4.1E



### ORDERING INFORMATION

Order No.	Configuration	Mounting Hardware	Mounting pipe Diameter	Shipping Weight
APXVAARR24_43-U-NA20	Field Replace RET included (3)	APM40-5E Beam tilt kit (included)	60-120mm	80 Kg



**Dual Slant Polarized Quad Band (8 Port) Antenna, 617-746/617-746/1695-2200/1695-2200MHz, 65deg, 15/15/18/18dBi, 2.4m (8ft), VET, RET, 0-12°/0-12°/2-12°/2-12°**

**External Document Links**

APM40\_Series\_Installation\_Instructions  
Manual\_Overdrive\_Instructions  
Global RFS Website

**Notes**

All electrical parameters are compliant with BASTA NGMN 9.6 requirements.

Available Configurations

APXVAARR24\_43-U-NA20 -- External ACU is included -- shipping weight 80kg.

For additional mounting information please click "External Document Links".

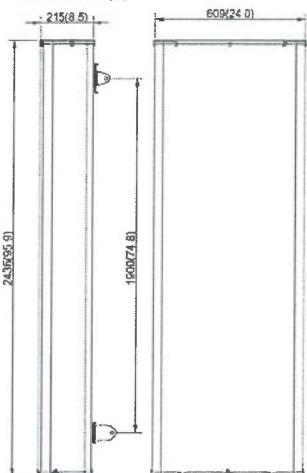
This data is provisional and subject to changes.

**External Link Reference**

Global RFS Website

<http://www.rfsworld.com>

Dimensions: mm (in)



This drawing is a general representation of the antenna – it does NOT accurately depict the connectors or radio frequency



# AIR 3246 update 12/18 - 17

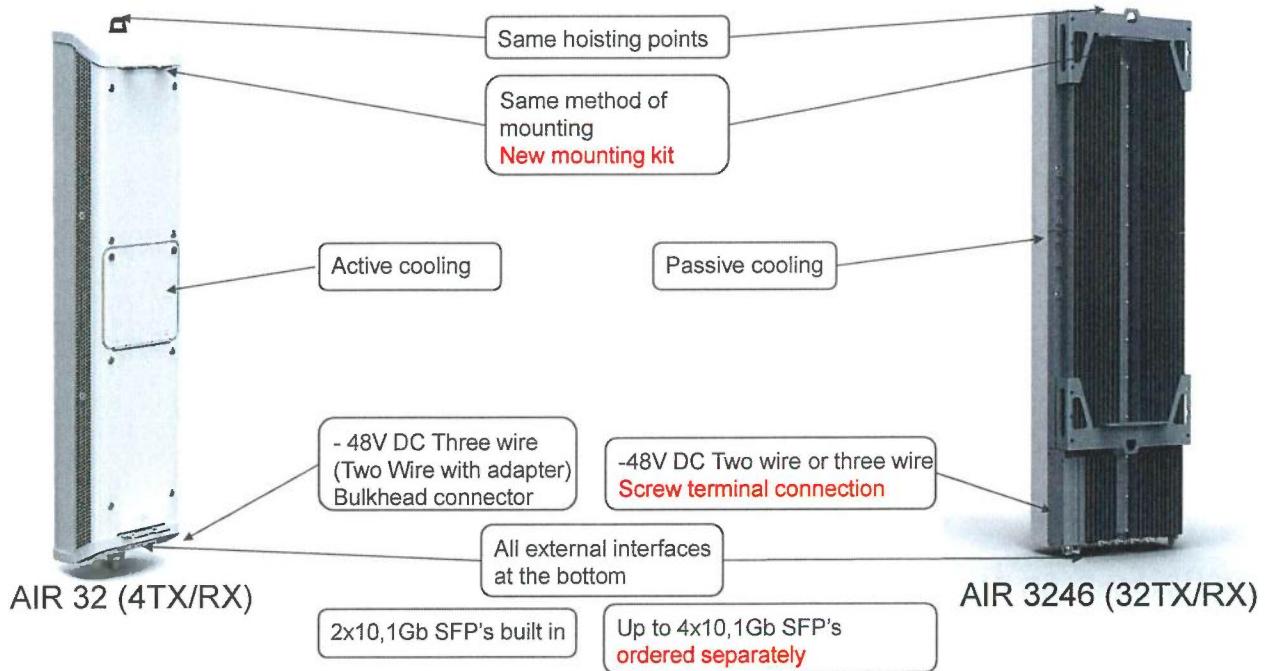
Kenth Höglund – AIR3246 product manager  
Evangelos Paravalos – PjM RAN SW development Ottawa R&D

# Agenda



- › AIR3246 site considerations
- › AIR3246 specifications
- › FD-MIMO dual band

# Installation Comparison



# POWER SYSTEM ON RAIL

## POWER 6302 & BATTERY 6312/13

**Power:** AC input 172-275VAC, 50-60 Hz, 2.3 kW DC -48V output power

**Battery:** Capacity dimensioned for typical 10 and 50 minutes back-up time for 2kW user load

Lithium-Ion: Long battery lifetime

**All:**

O&M monitoring integrated

Ericsson Rail mounting

Convection cooled

IP 65



Battery  
on Rail



# POWER 6303

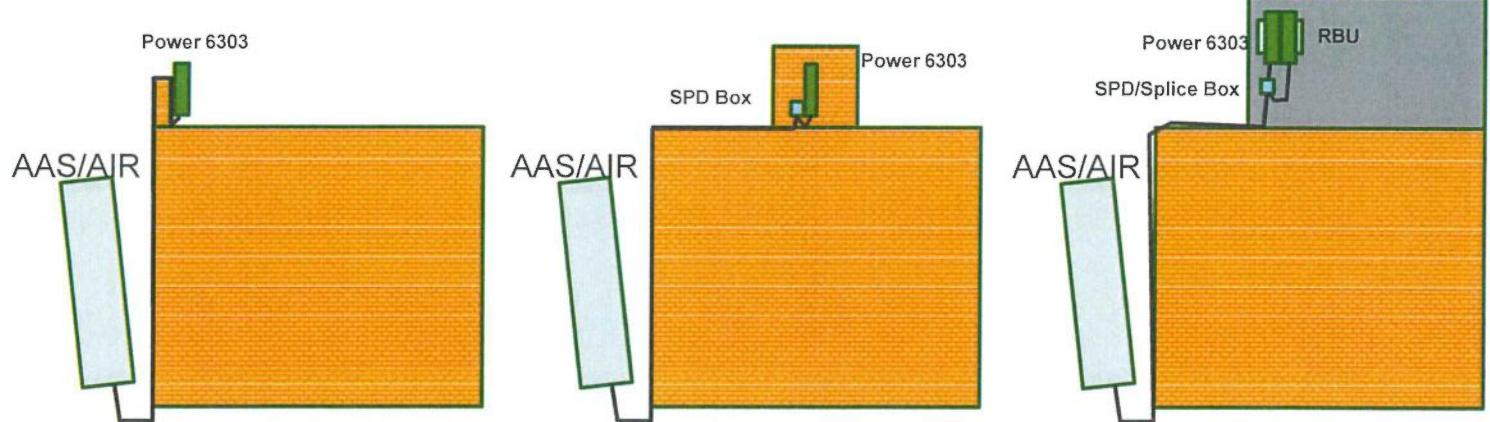
## - 2KW FOR ERS RADIOS

- › Rationale
  - Enable AC/400 VDC feed to new Air radio units that do not have internal AC/DC conversion
- › Product overview:
  - 2 kW output power
- › One output with shielded 2x10mm<sup>2</sup> cable
- › Power input “connector”, hatch and screw terminal



# POWER 6303

## - INSTALLATION EXAMPLES WALL/ROOF

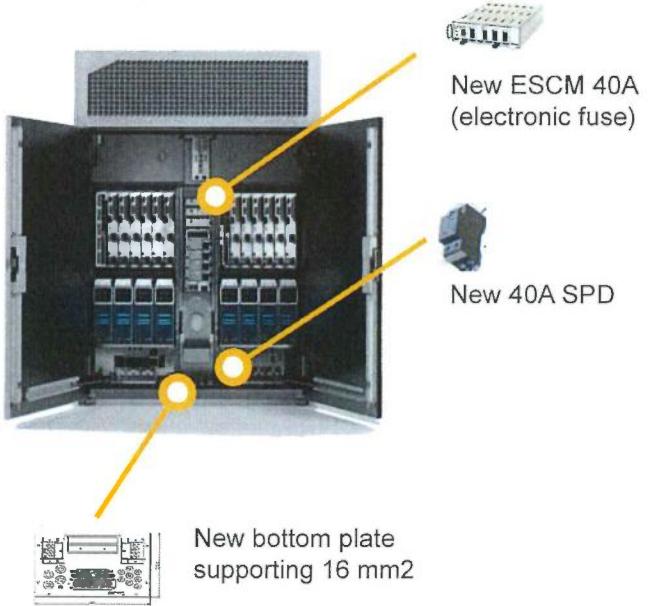


# 6K POWER EXPANSION FOR 5G RADIOS

- › Enable larger cables, new cable inlet components
- › New components for higher current, SPD and distribution unit
- › Allow a larger voltage drop over the distribution cable (reduce cost for installation material)



Example RBS 6102

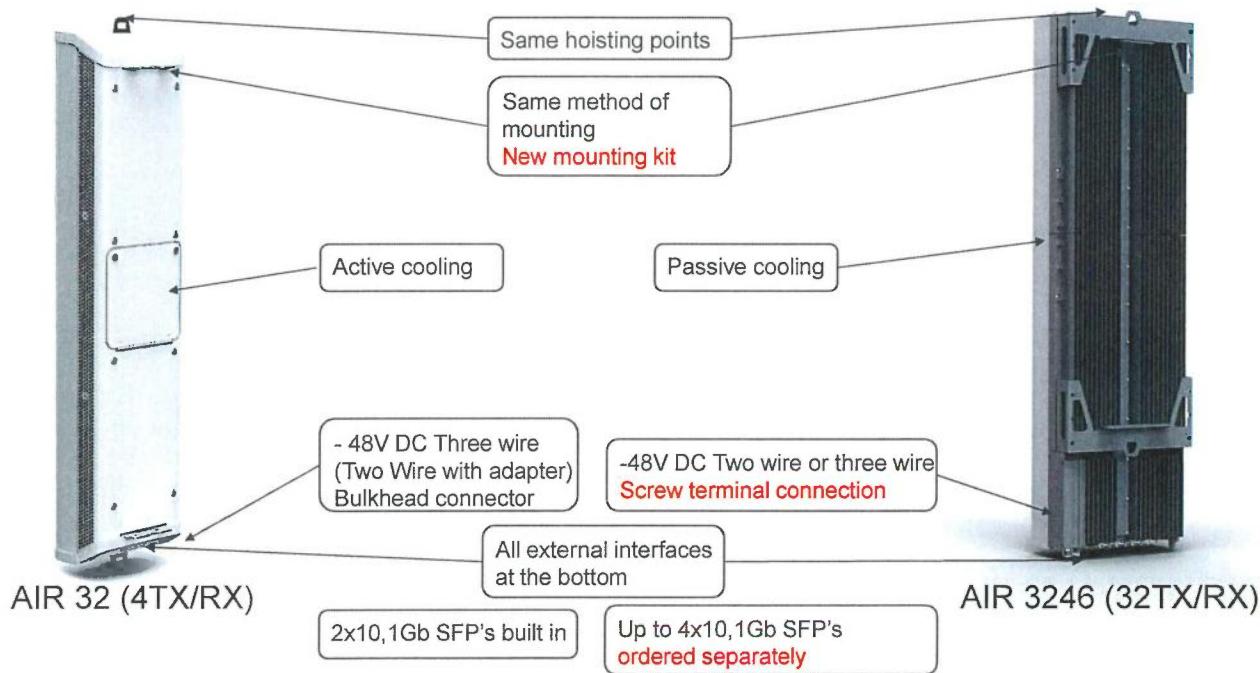


# Agenda



- › AIR3246 site considerations
- › AIR3246 specifications
- › FD-MIMO dual band

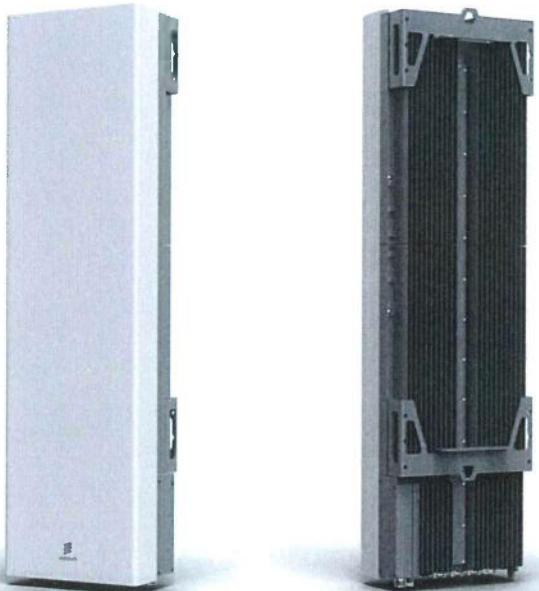
# Installation Comparison



# AIR 3246 BAND 66 (1/2)



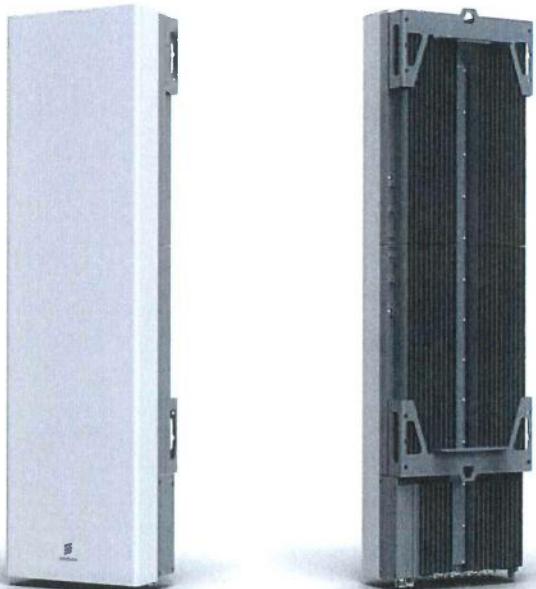
- › Radio
  - 32 TX/RX
  - 90 MHz IBW
  - 60 MHz LTE CBW
  - Up to 3 carriers LTE
  - 160 W total RF conducted power
- › Baseband interface 4 x 10.1 Gbps CPRI
- › Mechanical properties
  - Size (H x W x D): 1475x400x238 mm
  - Weight : 81 Kg (estimated)
- › Power
  - -48v DC, 3 wire or 2 wire
  - Max Power consumption: < 1350 w (estimated)
  - 120/230 VAC via supervised external PSU



## AIR 3246 BAND 66 (2/2)

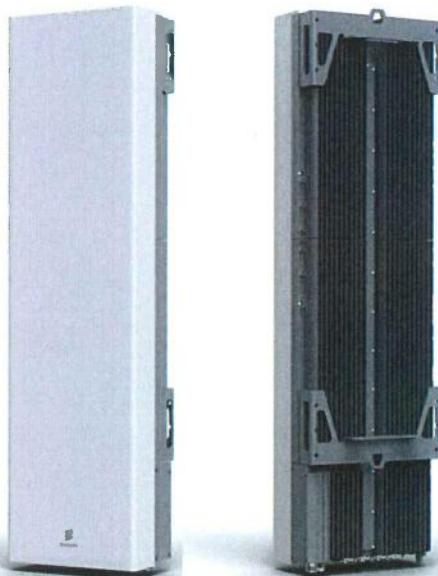


- › Antenna and beamforming properties
  - 96 X-polarized elements split by..
  - 4 rows and 4 columns of subarrays
  - Subarrays 3x1 X-pol element.
  - Beamforming capabilities. SW defined by baseband functionality.  
For legacy terminals with capability of reporting 4 CSI or less, static cell specific beamforming selectable from a range of predefined patterns.  
For terminals capable of reporting 8 or more, CSI precoder based user specific beamforming according to 3GPP up to Release 14.
  - Broadcast beam, typical values
    - › Horiz. HPBW 65 degrees
    - › Vert. HPBW 6 degrees
    - › Gain 18 dBi
    - › Downtilt 2-12 degrees
  - Traffic beams, typical values
    - › Horiz. HPBW 24 degrees
    - › Vert. HPBW 6 degrees
    - › Gain 23 dBi
    - › Horizontal pointing range +-53 degrees
    - › Vertical pointing range: Up 5 deg, down 19 degrees



## AIR 3246 BAND 25

- › 32 TX/RX
- › 160 W total RF output power
- › EIRP CRS Beam 70dBm
- › 65 MHz IBW
- › 60 MHz LTE CBW
- › 4 x 10.1 Gbps CPRI
- › Size (H x W x D):1475x400x238 mm
- › Weight : 81 Kg (estimated)
- › -48v DC, 3 wire or 2 wire
- › Max Power consumption: < 1440 w
- › 120/230 VAC via external PSU
- › Availability Q4-2018



# Supported Beams (Preliminary)



- › TM4 and common channels:
  - MACRO (default = DUALPOLARIZED65 which is EB)
  - MACRO2 (default = SECTORIZED1 which is MB6)
  - MACRO\_NARROW (default = NARROW which is narrow beam)
  - MACRO\_WIDE (default = BROAD which is broad beam)
- › TM9 and CSI-RS (not configurable)
  - Always default to broad beam

# Agenda

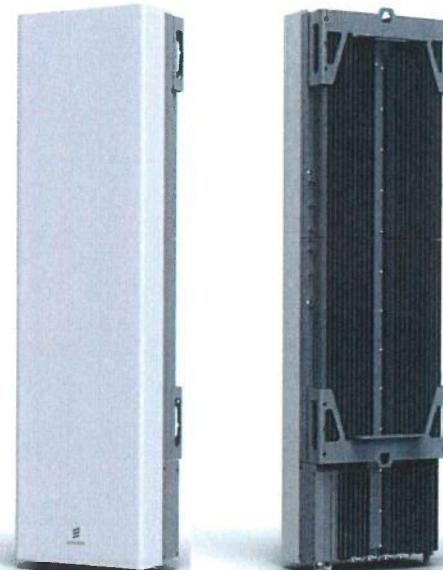


- › AIR3246 site considerations
- › AIR3246 specifications
- › FD-MIMO dual band

# AIR 3246 DUAL BAND



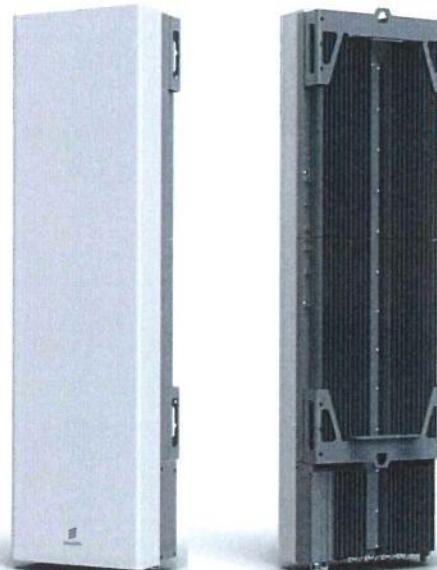
- › 32 TX/RX per band
- › Frequency bands: B66/B25
- › 320 W total RF output power
- › 90/65 MHz IBW
- › 60 MHz LTE CBW / Band
- › Interface: 4 x 25Gb CPRI
- › Size (H x W x D): 1475x400x300 mm (estimated)
- › Weight : TBD Kg
- › -48v DC, 3 wire or 2 wire
- › Optional 120/240 VAC
- › Target availability late Q4-2019



# AIR 88XX DUAL BAND



- › 8 TX/RX per band
- › Frequency bands: B66/B25
- › 320 W total RF output power
- › 90/65 MHz IBW
- › 60 MHz LTE CBW / Band
- › Interface: 4 x 10,1Gb CPRI
- › Size (H x W x D):1475x400x238 mm (estimated)
- › Weight : TBD Kg
- › -48v DC, 3 wire or 2 wire
- › 120/230 VAC via external PSU
- › Target availability Q3-2019



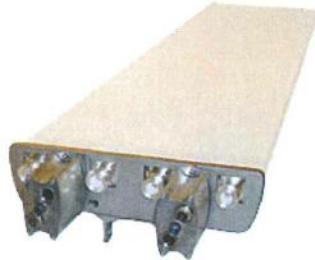


**ERICSSON**

Optimizer® Side-by-Side Dual Polarized Antenna, 1710-2200, 65deg, 18dBi, 1.4m, VET, 0-10deg RET

**Product Description**

A combination of two X-Polarized antennas in a single radome, this pair of variable tilt antennas provides exceptional suppression of all upper sidelobes at all downtilt angles. It also features a wide downtilt range. This antenna is optimized for performance across the entire frequency band (1710-2200 MHz). The antenna comes pre-connected with two antenna control units (ACU).

**Features/Benefits**

- Variable electrical downtilt - provides enhanced precision in controlling intercell interference. The tilt is infiield adjustable 0-10 deg.
- High Suppression of all Upper Sidelobes (Typically <-20dB).
- Gain tracking – difference between AWS UL (1710-1755 MHz) and DL (2110-2155 MHz) <1dB.
- Two X-Polarised panels in a single radome.
- Azimuth horizontal beamwidth difference <4deg between AWS UL (1710-1755 MHz) and DL (2110-2155 MHz).
- Low profile for low visual impact.
- Dual polarization; Broadband design.
- Includes (2) AISG 2.0 Compatible ACU-A20-N or ACU-A20-S antenna control units.

**Technical Specifications****Electrical Specifications**

Frequency Range, MHz	1710-2200
Horizontal Beamwidth, deg	65
Vertical Beamwidth, deg	5.9 to 7.7
Electrical Downtilt Range, deg	0-10
Gain, dBi (dBd)	18 (15.9)
1st Upper Sidelobe Suppression, dB	> 18 (typically > 20)
Upper Sidelobe Suppression, dB	> 18 all (typically > 20)
Front-To-Back Ratio, dB	>26 (typically 28)
Polarization	Dual pol +/-45°
VSWR	< 1.5:1
Isolation between Ports, dB	> 30
3rd Order IMP @ 2 x 43 dBm, dBc	> 150 (155 Typical)
Impedance, Ohms	50
Maximum Power Input, W	300
Lightning Protection	Direct Ground
Connector Type/Location	(4) 7-16 Long Neck Female/Bottom

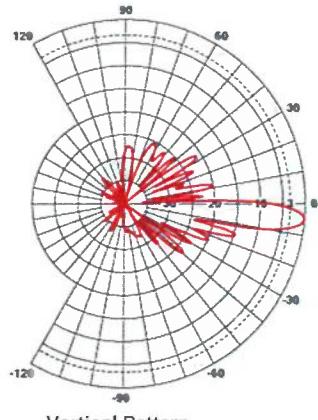
**Mechanical Specifications**

Dimensions - HxWxD, mm (in)	1420 x 331 x 80 (55.9 x 13 x 3.15)
Weight w/o Mtg Hardware, kg (lb)	18.5 (40.7)
Survival/Rated Wind Speed, km/h (mph)	200 (125) / 160 (100)
Applied Wind Load Standard	DIN 1055-4
Wind Load @ Rated Wind, Front, N (lbf)	756 (170)
Wind Load @ Rated Wind, Max., N (lbf)	756 (170)
Wind Load @ Rated Wind, Side, N (lbf)	231 (52)
Wind Load @ Rated Wind, Rear, N (lbf)	408 (92)
Operation temperature, °C (°F)	-40 to +60 (-40 to +140)
Radome Material/Color	Fiberglass/Light Grey RAL7035
Mounting Hardware Material	Diecasted Aluminum
Radiating Element Material	Brass
Reflector Material	Aluminum
Shipping Weight, kg (lb)	24.5 (53.9)
Packing Dimensions, HxWxD, mm (in)	1520 x 408 x 198 (59.8 x 16 x 7.8)

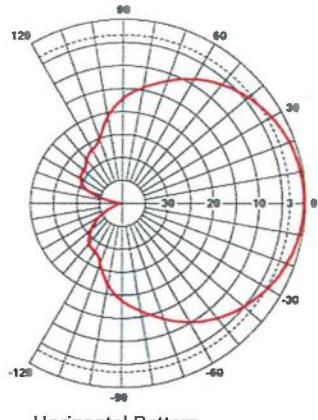
**Ordering Information**

Mounting Hardware	APM40-2 + APM40-E2
Mounting Pipe Diameter, mm (in)	60-120 (2.36-4.72)
Mounting Hardware Weight, kg (lb)	3.5 (7.7)

Optimizer® Side-by-Side Dual Polarized Antenna, 1710-2200, 65deg, 18dBi, 1.4m, VET, 0-10deg RET



Vertical Pattern



Horizontal Pattern

**Notes**

For additional mounting information please click "External Document Link" below.

**External Document Links**

APM40 Series Datasheet: [APM40 Series Datasheet](#)

APM40 Series Installation Instructions: [APM40 Series Installation Instructions](#)

## **ATTACHMENT C**

### Structural Analysis



Centered on Solutions<sup>SM</sup>

## Structural Analysis Report

New Site Development (NSD)

Proposed T-Mobile  
Telecommunications Facility

Site Ref: CTFF039A

181 White Street  
Danbury, CT

CENTEK Project No. 18067.00

Date: September 8, 2018



**Prepared for:**

T-Mobile USA  
35 Griffin Road  
Bloomfield, CT 06002

**CENTEK** Engineering, Inc.  
Structural Analysis – WCSU Danbury  
T-Mobile – New Site Development – CTFF039A  
Danbury, CT  
September 8, 2018

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- INTRODUCTION
- ANTENNA AND APPURTENANCE SUMMARY
- PRIMARY ASSUMPTIONS USED IN THE ANALYSIS
- ANALYSIS
- HOST STRUCTURE LOADING
- STRUCTURE CAPACITY
- CONCLUSION

### **SECTION 2 – CONDITIONS & SOFTWARE**

- STANDARD ENGINEERING CONDITIONS

### **SECTION 3 – CALCULATIONS**

- DESIGN BASIS – EXISTING ROOF LOADS
- EX. LOW ROOF FRAMING ANALYSIS – RTP SUPPORT
- WIND LOAD CALCULATION
- RISA-3D REPORT – CONCEALMENT ENCLOSURE
- EX. HIGH ROOF FRAMING ANALYSIS – CONCEALMENT ENCLOSURE

### **SECTION 4 – REFERENCE MATERIAL (NOT ATTACHED)**

- T-MOBILE RF DATA SHEET, DATED APRIL, 24<sup>TH</sup>, 2018
- EXISTING DRAWINGS AS PREPARED BY PHILIP N. AND WILLIAM WEBB SUNDERLAND DATED MAY 5<sup>TH</sup>, 1966.

**CENTEK** Engineering, Inc.  
Structural Analysis – WCSU Danbury  
T-Mobile – New Site Development – CTFF039A  
Danbury, CT  
September 8, 2018

## Introduction

The purpose of this report is to summarize the results of the non-linear, P-Δ structural analysis for the telecommunications facility as proposed by T-Mobile on the existing roof of the host building located in Danbury, Connecticut.

The host structure is a ±61-ft tall, four-story building constructed circa 1966 and used as an educational institution. The host building geometry, structure member sizes and foundation system information were obtained from existing drawings as prepared by Philip N. and William Webb Sunderland, dated May 5<sup>th</sup>, 1966.

Antenna and appurtenance information were provided to this office by T-Mobile RF Data sheet dated April 24<sup>th</sup>, 2018. Additional information was obtained by CENTEK personnel during a site visit conducted on March 27<sup>th</sup>, 2018.

## Antenna and Appurtenance Summary

The proposed loads considered in this analysis consist of the following:

- **T-MOBILE (PROPOSED):**

**Antennas:** Three (3) Ericsson AIR3246 B66 panel antennas, three (3) RFS APX16DWV-16DWV-S-E-A20 panel antennas, three (3) RFS APXVAARR24\_43-U-NA20 panel antennas, three (3) Ericsson 4415 B25 remote radio units, three (3) Ericsson 2217 B66A remote radio units, and three (3) Ericsson 4449 B7/B12 remote radio mounted on antenna sector frames behind antenna concealment enclosure with a RAD center elevation of ±65'-6" above grade level.

**Coax Cables:** Three (3) Ericsson 6x12 Hybrid Cable System (HCS) routed from the equipment platform on the lower roof and inside non-penetrating cable tray to each antenna sector on the upper roof.

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Structural Analysis – WCSU Danbury  
T-Mobile – New Site Development – CTFF039A  
Danbury, CT  
September 8, 2018

### Primary Assumptions Used in the Analysis

- The host building's theoretical capacity does not include any assessment of the condition of the structure.
- The host building structure transfers the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- The host building structure was properly installed and maintained.
- The host building is in plumb condition.
- Superimposed loading, existing and proposed, experienced by the host structure as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original building design documents.
- All members exposed to the elements were "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All existing member protective coatings are in good condition.
- All host building structure members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.
- All coax cables to be installed as indicated in this report and construction drawings prepared by this office.

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Structural Analysis – WCSU Danbury  
T-Mobile – New Site Development – CTFF039A  
Danbury, CT  
September 8, 2018

### Analysis

The proposed antenna concealment enclosure was analyzed using a comprehensive finite element computer program entitled RISA 3D. The program analyzes the proposed concealment enclosure, considering the worst case loading condition. The enclosure is considered as loaded by concentric forces along the main structural supports, and the model assumes that the enclosure members are subjected to bending, axial, and shear forces. In addition to the enclosure the existing host building framing members were analyzed using a structural analysis software entitled TEDDS.

The proposed enclosure and existing framing members were analyzed using Allowable Stress Design (ASD).

The controlling wind speed is determined by evaluating the local available wind speed data as provided in Appendix N of the CSBC<sup>1</sup>.

### LOADING

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA/EIA-222-F, gravity loads of the tower structure and its components, and the application of ½" radial ice on the tower structure and its components.

Ultimate Design Wind Speed:	Burlington; $V_{ULT} = 120$ mph	[Appendix N of the 2016 CT Building Code Supplement]
Load Cases (ASD):	<u>Load Case 1</u> : Dead Load <u>Load Case 2</u> : Dead Load + Snow Load <u>Load Case 3</u> : Dead Load + (0.6) Wind Load	[Section 1605.3.1 of 2012 IBC]
Snow Load (Flat roof):	30 psf (Minimum)	[Section 1608.1.1 of 2016 CT Building Code Supplement]
Snow Load (Drift Conditions):	60.534 psf (Max surcharge) Width of Drift = 13.527-ft	[Section 1608.1.1 of 2016 CT Building Code Supplement]

<sup>1</sup> The 2012 International Building Code (IBC) as amended by the 2016 Connecticut State Building Code.

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Structural Analysis – WCSU Danbury  
T-Mobile – New Site Development – CTFF039A  
Danbury, CT  
September 8, 2018

## Design/Analysis Capacities

Host structure member stresses and proposed concealment enclosure stresses were calculated utilizing the structural analysis software RISA 3D.

- Existing Host Structure Members Stresses:

Section	Bending Ratio (percentage of capacity)	Shear Ratio (percentage of capacity)	Result
(E) W16x26 (Low Roof)	82.8%	20.5%	PASS
(E) W18x50 (High Roof)	74.6%	19.7%	PASS
(E) W18x45 (High Roof)	38.7%	16.9%	PASS

(1) Refer to section 3.0 for additional information.

- Proposed Concealment enclosure member stresses:

Tower Component	Stress Ratio (percentage of capacity)	Result
HSS5x5x3/8 (Stub Posts)	3.9%	PASS
HSS4x4x5/16 (Weldment)	7.5%	PASS
Pipe 3.5 STD (Horiz.)	15.8%	PASS
Pipe 2.0 STD (Vert.)	57.2%	PASS

## Conclusion

This analysis shows that the subject structure **is adequate** to support the proposed superimposed loading due to the proposed telecommunications facility.

The analysis is based, in part, on the information provided to this office by T-Mobile and information provided by the host building management. If the existing conditions are different than the information in this report, Centek Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:

Camilo A. Gaviria, PE  
Structural Engineer

REPORT



**CENTEK** Engineering, Inc.  
Structural Analysis – WCSU Danbury  
T-Mobile – New Site Development – CTFF039A  
Danbury, CT  
September 8, 2018

Standard Conditions for Furnishing of  
Professional Engineering Services on  
Existing Structures

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of Centek Engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to Centek Engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the "as new" condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of the governing state building code and all applicable referenced standards.
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. Centek Engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

## Roof Dead Load Summaries

(include: roofing, ballast, shingles, decking, sheathing, ceilings, joists/beam/girders, trusses, rafters, bridging, future reroofing, misc./mechanical/electrical, etc.)

### *Roof Type 1: Lower Roof Construction*

### *Roof Type 2: High Roof Construction*

### *Roof Type 2:*

psf  
psf  
psf  
psf  
psf  
psf  
psf

Total = 0.0 psf

Project TMO WCSU NSD		Job Ref. 18067.00	
Section Existing W16x26 (RTP Loading)		Sheet no./rev. 1	
Calc. by CAG	Date 9/9/2018	Chk'd by	Date

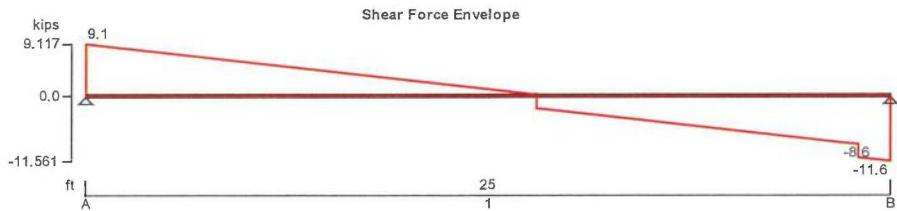
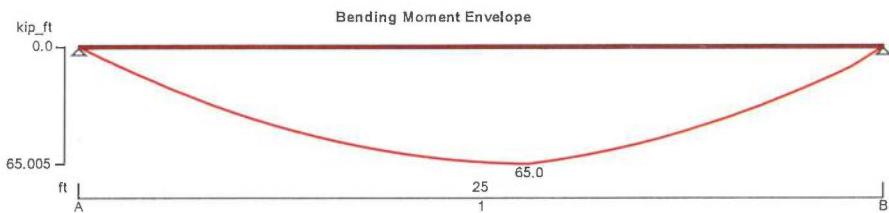
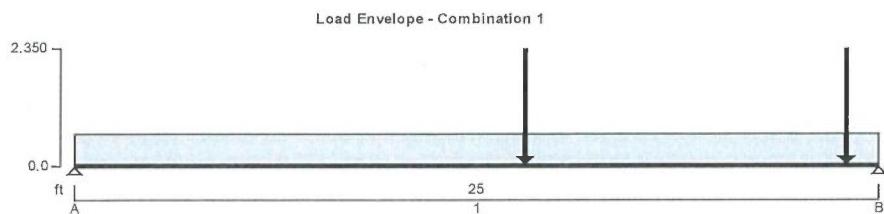
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Date

### STEEL BEAM ANALYSIS & DESIGN (AISC360-10)

In accordance with AISC360 14<sup>th</sup> Edition published 2010 using the ASD method

Tedds calculation version 3.0.12



#### Support conditions

Support A      Vertically restrained  
                    Rotationally free

Support B      Vertically restrained  
                    Rotationally free

#### Applied loading

Beam loads      Self - Dead self weight of beam × 1  
                    Roof Dead - Dead full UDL 0.425 kips/ft  
                    Snow - Snow full UDL 0.188 kips/ft  
                    RTP DL - Dead point load 1.15 kips at 288.00 in  
                    RTP LL - Live point load 1.2 kips at 288.00 in  
                    RTP DL - Dead point load 1.15 kips at 168.00 in  
                    RTP LL - Live point load 1.2 kips at 168.00 in

Project TMO WCSU NSD				Job Ref. 18067.00	
Section Existing W16x26 (RTP Loading)				Sheet no./rev. 2	
Calc. by CAG	Date 9/9/2018	Chk'd by	Date	App'd by	Date

### Load combinations

Load combination 1	Support A	Dead × 1.00 Live × 1.00 Snow × 1.00
	Span 1	Dead × 1.00 Live × 1.00 Snow × 1.00
	Support B	Dead × 1.00 Live × 1.00 Snow × 1.00

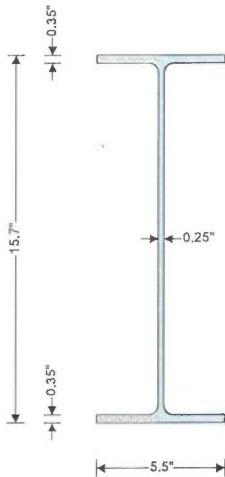
### Analysis results

Maximum moment	$M_{max} = 65$ kips_ft	$M_{min} = 0$ kips_ft
Maximum moment span 1 segment 1	$M_{s1\_seg1\_max} = 44.5$ kips_ft	$M_{s1\_seg1\_min} = 0$ kips_ft
Maximum moment span 1 segment 2	$M_{s1\_seg2\_max} = 64$ kips_ft	$M_{s1\_seg2\_min} = 0$ kips_ft
Maximum moment span 1 segment 3	$M_{s1\_seg3\_max} = 65$ kips_ft	$M_{s1\_seg3\_min} = 0$ kips_ft
Maximum moment span 1 segment 4	$M_{s1\_seg4\_max} = 47.4$ kips_ft	$M_{s1\_seg4\_min} = 0$ kips_ft
Maximum shear	$V_{max} = 9.1$ kips	$V_{min} = -11.6$ kips
Maximum shear span 1 segment 1	$V_{s1\_seg1\_max} = 9.1$ kips	$V_{s1\_seg1\_min} = 0$ kips
Maximum shear span 1 segment 2	$V_{s1\_seg2\_max} = 5.1$ kips	$V_{s1\_seg2\_min} = 0$ kips
Maximum shear span 1 segment 3	$V_{s1\_seg3\_max} = 1.1$ kips	$V_{s1\_seg3\_min} = -5.2$ kips
Maximum shear span 1 segment 4	$V_{s1\_seg4\_max} = 0$ kips	$V_{s1\_seg4\_min} = -11.6$ kips
Deflection segment 5	$\delta_{max} = 0$ in	$\delta_{min} = 0$ in
Maximum reaction at support A	$R_{A\_max} = 9.1$ kips	$R_{A\_min} = 9.1$ kips
Unfactored dead load reaction at support A	$R_{A\_Dead} = 6.2$ kips	
Unfactored live load reaction at support A	$R_{A\_Live} = 0.6$ kips	
Unfactored snow load reaction at support A	$R_{A\_Snow} = 2.4$ kips	
Maximum reaction at support B	$R_{B\_max} = 11.6$ kips	$R_{B\_min} = 11.6$ kips
Unfactored dead load reaction at support B	$R_{B\_Dead} = 7.4$ kips	
Unfactored live load reaction at support B	$R_{B\_Live} = 1.8$ kips	
Unfactored snow load reaction at support B	$R_{B\_Snow} = 2.4$ kips	

### Section details

Section type W 16x26 (AISC 14th Edn 2010) ASTM steel designation A36

Project TMO WCSU NSD				Job Ref. 18067.00
Section Existing W16x26 (RTP Loading)				Sheet no./rev. 3
Calc. by CAG	Date 9/9/2018	Chkd by	Date	App'd by



## Design of members for shear - Chapter G

Required shear strength  $V_r = 11.561$  kips

Allowable shear strength  $V_c = 56.520$  kips

**PASS - Allowable shear strength exceeds required shear strength**

Design of members for flexure in the major axis - Chapter F

Required flexural strength  $M_r = 65.005$  kips·ft

Allowable flexural strength  $M_c = 78.549 \text{ kips}_\text{ft}$

**PASS - Allowable flexural strength exceeds required flexural strength**

## Design of members for vertical deflection

Consider deflection due to loads

Limiting deflection  $\delta_{lim} = 1.25$  in

**PASS - Maximum deflection does not exceed deflection limit**

**Design Wind Load on Other Structures:**

(Based on IBC 2012, CSBC 2016 and ASCE 7-10)

Wind Speed =	$V := 120$	mph	(User Input)	(CSBC Appendix-N)
Risk Category =	$BC := II$		(User Input)	(IBC Table 1604.5)
Exposure Category =	$Exp := B$		(User Input)	
Height Above Grade =	$Z := 70.33$	ft	(User Input)	
Structure Type =	StructureType := Solid_Sign		(User Input)	
Structure Height =	$Height := 10$	ft	(User Input)	
Horizontal Dimension of Structure =	$Width := 8.0$	ft	(User Input)	

**Terrain Exposure Constants:**

Nominal Height of the Atmospheric Boundary Layer =

$$zg := \begin{cases} 1200 & \text{if } Exp = B \\ 900 & \text{if } Exp = C \\ 700 & \text{if } Exp = D \end{cases} = 1.2 \times 10^3 \quad (\text{Table 26.9-1})$$

3-Sec Gust Speed Power Law Exponent =

$$\alpha := \begin{cases} 7 & \text{if } Exp = B \\ 9.5 & \text{if } Exp = C \\ 11.5 & \text{if } Exp = D \end{cases} = 7 \quad (\text{Table 26.9-1})$$

Integral Length Scale Factor =

$$l := \begin{cases} 320 & \text{if } Exp = B \\ 500 & \text{if } Exp = C \\ 650 & \text{if } Exp = D \end{cases} = 320 \quad (\text{Table 26.9-1})$$

Integral Length Scale Power Law Exponent =

$$E := \begin{cases} \frac{1}{3} & \text{if } Exp = B \\ \frac{1}{5} & \text{if } Exp = C \\ \frac{1}{8} & \text{if } Exp = D \end{cases} = 0.333 \quad (\text{Table 26.9-1})$$

Turbulence Intensity Factor =

$$c := \begin{cases} 0.3 & \text{if } Exp = B \\ 0.2 & \text{if } Exp = C \\ 0.15 & \text{if } Exp = D \end{cases} = 0.3 \quad (\text{Table 26.9-1})$$

Exposure Constant =

$$Z_{min} := \begin{cases} 30 & \text{if } Exp = B \\ 15 & \text{if } Exp = C \\ 7 & \text{if } Exp = D \end{cases} = 30 \quad (\text{Table 26.9-1})$$

Exposure Coefficient =

$$K_Z := \begin{cases} 2.01 \left( \frac{Z}{zg} \right)^{\left( \frac{2}{\alpha} \right)} & \text{if } 15 \leq Z \leq zg \\ 2.01 \left( \frac{15}{zg} \right)^{\left( \frac{2}{\alpha} \right)} & \text{if } Z < 15 \end{cases} = 0.89 \quad (\text{Table 29.3-1})$$

Topographic Factor =  $K_{zt} := 1$  (Eq. 26.8-2)

Wind Directionality Factor =  $K_d = 0.85$  (Table 26.6-1)

Velocity Pressure =  $q_z := 0.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V^2 = 28$  (Eq. 29.3-1)

Peak Factor for Background Response =  $g_Q := 3.4$  (Sec 26.9.4)

Peak Factor for Wind Response =  $g_V := 3.4$  (Sec 26.9.4)

Equivalent Height of Structure =  $z := \begin{cases} Z_{min} & \text{if } Z_{min} > 0.6 \cdot \text{Height} \\ 0.6 \cdot \text{Height} & \text{otherwise} \end{cases} = 30$  (Sec 26.9.4)

Intensity of Turbulence =  $I_z := c \cdot \left( \frac{33}{z} \right)^{\left( \frac{1}{6} \right)} = 0.305$  (Eq. 26.9-7)

Integral Length Scale of Turbulence =  $L_z := I_z \cdot \left( \frac{z}{33} \right)^E = 309.993$  (Eq. 26.9-9)

Background Response Factor =  $Q := \sqrt{\frac{1}{1 + 0.63 \left( \frac{\text{Width} + \text{Height}}{L_z} \right)^{0.63}}} = 0.951$  (Eq. 26.9-8)

Gust Response Factor =  $G := 0.925 \left[ \frac{\left( 1 + 1.7 \cdot g_Q \cdot I_z \cdot Q \right)}{1 + 1.7 \cdot g_V \cdot I_z} \right] = 0.896$  (Eq. 26.9-6)

Force Coefficient =  $C_f = 1.2$  (Fig 29.5-1 - 29.5-3)

Wind Force =

$F := q_z \cdot G \cdot C_f = 30$

psf

**Development of Wind & Ice Load on Antennas**
**Antenna Data:**

Antenna Model =	Ericsson AIR3246 B66		
Antenna Shape =	Flat	(User Input)	
Antenna Height =	$L_{ant} := 58.1$	in	(User Input)
Antenna Width =	$W_{ant} := 15.7$	in	(User Input)
Antenna Thickness =	$T_{ant} := 9.4$	in	(User Input)
Antenna Weight =	$WT_{ant} := 180$	lbs	(User Input)
Number of Antennas =	$N_{ant} := 1$		(User Input)

**Wind Load (Front)**

$$\text{Surface Area for One Antenna} = \frac{L_{ant} \cdot W_{ant}}{144} = 6.3 \text{ sf}$$

$$\text{Antenna Projected Surface Area} = A_{ant} := SA_{ant} \cdot N_{ant} = 6.3 \text{ sf}$$

$$\text{Total Antenna Wind Force} = F_{ant} := F \cdot A_{ant} = 191 \text{ lbs}$$

**Wind Load (Side)**

$$\text{Surface Area for One Antenna} = \frac{L_{ant} \cdot T_{ant}}{144} = 3.8 \text{ sf}$$

$$\text{Antenna Projected Surface Area} = A_{ant} := SA_{ant} \cdot N_{ant} = 3.8 \text{ sf}$$

$$\text{Total Antenna Wind Force} = F_{ant} := F \cdot A_{ant} = 114 \text{ lbs}$$

**Gravity Load (without ice)**

$$\text{Weight of All Antennas} = WT_{ant} \cdot N_{ant} = 180 \text{ lbs}$$



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Subject:

Wind Load on Equipment per ASCE 7-10

Location:

Danbury, CT

Rev. 0: 09/08/18

Prepared by: CAG Checked by: CFC  
Job No. 18067.00

#### Development of Wind & Ice Load on Antennas

##### Antenna Data:

Antenna Model =	RFSAPXVAARR24-43		
Antenna Shape =	Flat	(User Input)	
Antenna Height =	$L_{ant} := 95.9$	in	(User Input)
Antenna Width =	$W_{ant} := 24$	in	(User Input)
Antenna Thickness =	$T_{ant} := 8.7$	in	(User Input)
Antenna Weight =	$WT_{ant} := 153$	lbs	(User Input)
Number of Antennas =	$N_{ant} := 1$	(User Input)	

#### Wind Load (Front)

$$\text{Surface Area for One Antenna} = \text{SA}_{ant} := \frac{L_{ant} \cdot W_{ant}}{144} = 16 \text{ sf}$$

$$\text{Antenna Projected Surface Area} = A_{ant} := \text{SA}_{ant} \cdot N_{ant} = 16 \text{ sf}$$

$$\text{Total Antenna Wind Force} = F_{ant} := F \cdot A_{ant} = 481 \text{ lbs}$$

#### Wind Load (Side)

$$\text{Surface Area for One Antenna} = \text{SA}_{ant} := \frac{L_{ant} \cdot T_{ant}}{144} = 5.8 \text{ sf}$$

$$\text{Antenna Projected Surface Area} = A_{ant} := \text{SA}_{ant} \cdot N_{ant} = 5.8 \text{ sf}$$

$$\text{Total Antenna Wind Force} = F_{ant} := F \cdot A_{ant} = 175 \text{ lbs}$$

#### Gravity Load (without ice)

$$\text{Weight of All Antennas} = WT_{ant} \cdot N_{ant} = 153 \text{ lbs}$$

Development of Wind & Ice Load on Antennas

Antenna Data:

Antenna Model =	RFSAPX16DWV-16DWWS-A20		
Antenna Shape =	Flat	(User Input)	
Antenna Height =	$L_{ant} := 55.9$	in	(User Input)
Antenna Width =	$W_{ant} := 13$	in	(User Input)
Antenna Thickness =	$T_{ant} := 3.15$	in	(User Input)
Antenna Weight =	$WT_{ant} := 40.7$	lbs	(User Input)
Number of Antennas =	$N_{ant} := 1$	(User Input)	

Wind Load (Front)

$$SA_{ant} := \frac{L_{ant} \cdot W_{ant}}{144} = 5 \quad \text{sf}$$

$$A_{ant} := SA_{ant} \cdot N_{ant} = 5 \quad \text{sf}$$

$$F_{ant} := F \cdot A_{ant} = 152 \quad \text{lbs}$$

Wind Load (Side)

$$SA_{ant} := \frac{L_{ant} \cdot T_{ant}}{144} = 1.2 \quad \text{sf}$$

$$A_{ant} := SA_{ant} \cdot N_{ant} = 1.2 \quad \text{sf}$$

$$F_{ant} := F \cdot A_{ant} = 37 \quad \text{lbs}$$

Gravity Load (without ice)

$$WT_{ant} \cdot N_{ant} = 41 \quad \text{lbs}$$



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Subject:

Wind Load on Equipment per ASCE 7-10

Location:

Danbury, CT

Rev. 0: 09/08/18

Prepared by: CAG Checked by: CFC  
Job No. 18067.00

#### Development of Wind & Ice Load on RRHs

##### RRUS Data:

RRUS Model = Ericsson 4449 B71/B12  
RRUS Shape = Flat (User Input)  
RRUS Height =  $L_{RRH} := 14.9$  in (User Input)  
RRUS Width =  $W_{RRH} := 13.2$  in (User Input)  
RRUS Thickness =  $T_{RRH} := 10.4$  in (User Input)  
RRUS Weight =  $WT_{RRH} := 74$  lbs (User Input)  
Number of RRUS's =  $N_{RRH} := 1$  (User Input)

#### Wind Load (Front)

$$SA_{RRH} := \frac{L_{RRH} \cdot W_{RRH}}{144} = 1.4 \quad \text{sf}$$

$$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 1.4 \quad \text{sf}$$

$$F_{RRH} := F \cdot A_{RRH} = 41 \quad \text{lbs}$$

#### Wind Load (Side)

$$SA_{RRH} := \frac{L_{RRH} \cdot T_{RRH}}{144} = 1.1 \quad \text{sf}$$

$$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 1.1 \quad \text{sf}$$

$$F_{RRH} := F \cdot A_{RRH} = 32 \quad \text{lbs}$$

#### Gravity Load (without ice)

$$WT_{RRH} \cdot N_{RRH} = 74 \quad \text{lbs}$$

**Development of Wind & Ice Load on RRHs**

**RRUS Data:**

RRUS Model =	Ericsson 4415 B25		
RRUS Shape =	Flat	(User Input)	
RRUS Height =	$L_{RRH} := 16.5$	in	(User Input)
RRUS Width =	$W_{RRH} := 13.4$	in	(User Input)
RRUS Thickness =	$T_{RRH} := 5.9$	in	(User Input)
RRUS Weight =	$WT_{RRH} := 46$	lbs	(User Input)
Number of RRUS's =	$N_{RRH} := 1$	(User Input)	

**Wind Load (Front)**

SurfaceArea for One RRH =	$SA_{RRH} := \frac{L_{RRH} \cdot W_{RRH}}{144} = 1.5$	sf
RRH Projected SurfaceArea =	$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 1.5$	sf
Total RRH Wind Force =	$F_{RRH} := F \cdot A_{RRH} = 46$	lbs

**Wind Load (Side)**

SurfaceArea for One RRH =	$SA_{RRH} := \frac{L_{RRH} \cdot T_{RRH}}{144} = 0.7$	sf
RRH Projected SurfaceArea =	$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 0.7$	sf
Total RRH Wind Force =	$F_{RRH} := F \cdot A_{RRH} = 20$	lbs

**Gravity Load (without ice)**

Weight of All RRHs =	$WT_{RRH} \cdot N_{RRH} = 46$	lbs
----------------------	-------------------------------	-----

**Development of Wind & Ice Load on RRHs**

**RRUS Data:**

RRUS Model =	Ericsson 2217 B66A		
RRUS Shape =	Flat	(User Input)	
RRUS Height =	$L_{RRH} := 13.8$	in	(User Input)
RRUS Width =	$W_{RRH} := 11.7$	in	(User Input)
RRUS Thickness =	$T_{RRH} := 5.4$	in	(User Input)
RRUS Weight =	$WT_{RRH} := 28.2$	lbs	(User Input)
Number of RRUS's =	$N_{RRH} := 1$		(User Input)

**Wind Load (Front)**

$$SA_{RRH} := \frac{L_{RRH} \cdot W_{RRH}}{144} = 1.1 \quad \text{sf}$$

$$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 1.1 \quad \text{sf}$$

$$\text{Total RRH Wind Force} = F_{RRH} := F \cdot A_{RRH} = 34 \quad \text{lbs}$$

**Wind Load (Side)**

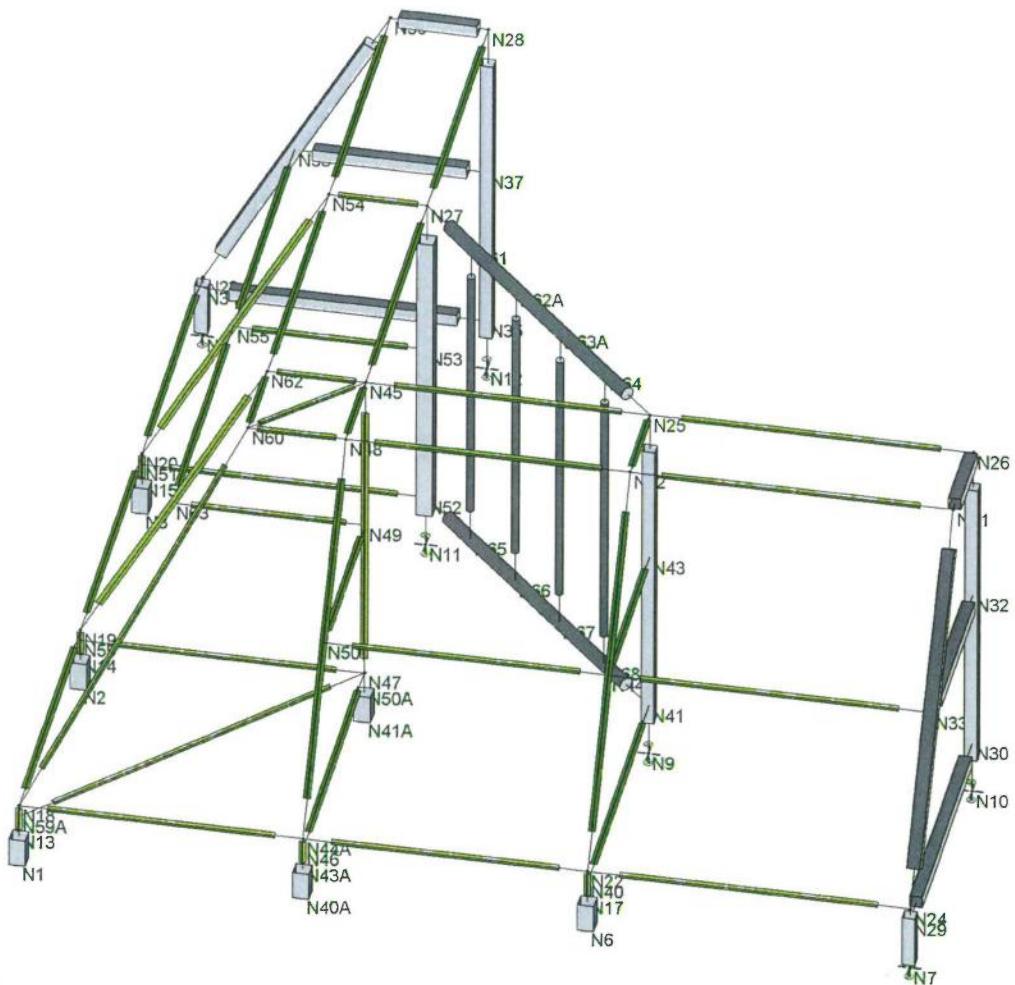
$$SA_{RRH} := \frac{L_{RRH} \cdot T_{RRH}}{144} = 0.5 \quad \text{sf}$$

$$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 0.5 \quad \text{sf}$$

$$\text{Total RRH Wind Force} = F_{RRH} := F \cdot A_{RRH} = 16 \quad \text{lbs}$$

**Gravity Load (without ice)**

$$\text{Weight of All RRHs} = WT_{RRH} \cdot N_{RRH} = 28 \quad \text{lbs}$$



Envelope Only Solution

CENTEK

CAG

18067.00

CTFF039A WCSU Danbury

Isometric View

SK - 1

Sept 9, 2018 at 10:40 AM

18067.00 CTFF039A WCSU Danbu...

Company : CENTEK  
Designer : CAG  
Job Number : 18067.00  
Model Name : CTFF039A WCSU Danbury

Sept 9, 2018  
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## ***Hot Rolled Steel Section Sets***

Label		Shape	Type	Design List	Material	Design ...	A [in2]	Iyy [in4]	Izz [in4]	J [in4]
1	HSS Stub Posts	HSS5X5X6	Column	Tube	A500 Gr.36	Typical	6.18	21.7	21.7	36.1
2	Weldment	HSS4X4X5	None	None	A500 Gr.36	Typical	4.1	9.14	9.14	15.3
3	ANT SUPPORTS (HORI...)	PIPE 3.5	Beam	Pipe	A53 Gr.B	Typical	2.5	4.52	4.52	9.04
4	ANT SUPPORTS (VERT)	PIPE 2.0	Column	Wide Flange	A53 Gr.B	Typical	1.02	.627	.627	1.25

## **Load Combinations**

## *Envelope Joint Reactions*

Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC MZ [k...]	LC	
1	N1	max	.265	14	1.2	10	.285	4	.151	4	.006	5 .142	5
2		min	-.265	5	-1.587	5	-.285	15	-.15	15	-.006	7 -.14	14
3	N6	max	.265	14	2.584	3	1.541	4	.779	4	.006	12 .142	5
4		min	-.265	5	.026	13	-1.54	15	-.777	15	-.006	7 -.14	14
5	N2	max	.592	14	2.09	10	.285	4	.151	4	.006	5 .306	5
6		min	-.592	5	-1.32	5	-.285	15	-.15	15	-.006	7 -.304	14
7	N3	max	1.637	14	2.525	3	.285	4	.151	4	.006	12 .829	5
8		min	-1.638	5	-.008	12	-.285	15	-.15	15	-.006	7 -.826	14
9	N4	max	.547	7	1.201	10	.002	13	0	15	.001	12 0	15
10		min	-.533	12	-.415	12	-.002	6	0	1	-.001	7 0	1
11	N7	max	.002	6	1.252	11	.584	13	0	15	.001	6 0	15
12		min	-.002	13	-.46	13	-.601	6	0	1	-.001	13 0	1
13	N10	max	0	13	1.21	9	.213	4	0	15	0	6 0	15
14		min	0	6	-.377	15	-.205	11	0	1	0	13 0	1
15	N12	max	.187	10	1.094	8	0	7	0	15	0	12 0	15
16		min	-.199	5	-.337	14	0	12	0	1	0	7 0	1
17	N9	max	.091	7	.545	9	.029	13	0	15	0	12 0	15
18		min	-.091	12	.02	15	-.029	6	0	1	0	7 0	1
19	N40A	max	.265	14	1.996	8	.583	4	.3	4	.006	12 .142	5
20		min	-.265	5	-1.273	14	-.583	15	-.299	15	-.006	7 -.14	14
21	N41A	max	.592	14	2.886	8	.583	4	.3	4	.006	12 .306	5
22		min	-.592	5	-1.112	14	-.583	15	-.299	15	-.006	7 -.304	14

Company : CENTEK  
 Designer : CAG  
 Job Number : 18067.00  
 Model Name : CTFF039A WCSU Danbury

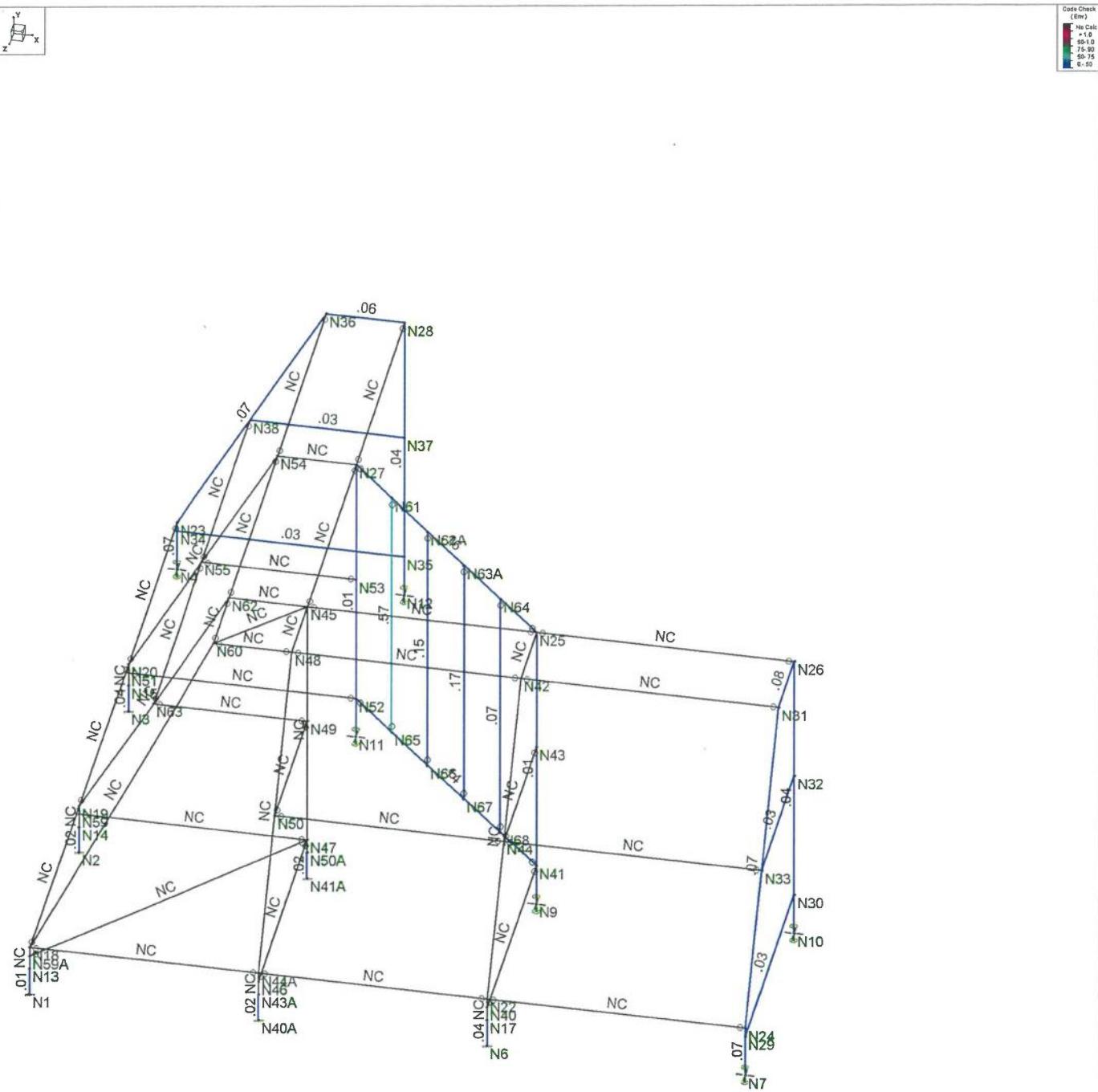
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### Envelope Joint Reactions (Continued)

Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC MZ [k-...]	LC
23	N11	max	.071	7	.764	8	.174	13	0	15	0	12 0
24		min	-.07	12	.014	14	-.175	6	0	1	0	7 0
25	Totals:	max	4.508	14	15.57	3	4.558	13				
26		min	-4.508	5	1.547	15	-4.558	6				

### Envelope AISC 14th(360-10): ASD Steel Code Checks

Member	Shape	Code Check	Loc[ft]	LC	Shear Che..Lo.....	LC	Pnc/...Pnt/o..Mny...Mnz.....	Eqn
1 M1	HSS5X5X6	.014	0	4	.007 0 z	4	169... 170... 24.33 124.331...	H1...
2 M3	HSS5X5X6	.020	0	5	.013 0 y	14	169... 170... 24.33 124.331...	H1...
3 M4	HSS5X5X6	.039	0	7	.036 0 y	5	169... 170... 24.33 124.331...	H1...
4 M5	HSS5X5X6	.036	0	6	.034 0 z	4	169... 170... 24.33 124.331...	H1...
5 M6	HSS4X4X5	.045	6.107	9	.007 0 z	4	68.926112... 12.83 112.831...	H1...
6 M7	HSS4X4X5	.074	1.489	6	.025 1... z	6	111... 112... 12.83 112.831...	H1...
7 M8	HSS4X4X5	.033	8	4	.005 8 y	4	85.517112... 12.83 112.831...	H1...
8 M9	HSS4X4X5	.074	0	9	.018 0 y	9	70.862112... 12.83 112.831...	H1...
9 M10	HSS4X4X5	.075	2.583	9	.025 2... y	9	109... 112... 12.83 112.831...	H1...
10 M11	HSS4X4X5	.029	0	9	.005 0 y	9	99.769112... 12.83 112.831...	H1...
11 M12	HSS4X4X5	.039	6.107	8	.007 0 y	5	68.926112... 12.83 112.831...	H1...
12 M13	HSS4X4X5	.067	1.489	7	.023 1... y	7	111... 112... 12.83 112.831...	H1...
13 M14	HSS4X4X5	.065	0	8	.022 0 y	8	109... 112... 12.83 112.831...	H1...
14 M15	HSS4X4X5	.067	10.104	8	.018 10..y	8	72.471112... 12.83 112.831...	H1...
15 M16	HSS4X4X5	.031	7.5	5	.005 7.5 y	5	88.446112... 12.83 112.831...	H1...
16 M17	HSS4X4X5	.027	0	8	.005 0 y	8	100... 112... 12.83 112.831...	H1...
17 M18	HSS4X4X5	.013	1.444	7	.003 0 y	7	68.926112... 12.83 112.831...	H1...
18 M23A	HSS5X5X6	.019	0	6	.013 0 z	15	169... 170... 24.33 124.331...	H1...
19 M29A	HSS5X5X6	.020	0	5	.013 0 y	14	169... 170... 24.33 124.331...	H1...
20 M31	HSS5X5X6	.012	1.444	6	.004 0 z	6	124... 170... 24.33 124.331...	H1...
21 M66	PIPE 3.5	.158	4.455	5	.019 0	7	32.09252.395 5.292 5.292 ...	H1...
22 M67	PIPE 3.5	.144	4.455	5	.018 0	5	32.09252.395 5.292 5.292 ...	H1...
23 M68	PIPE 2.0	.572	4.008	5	.033 0	5	7.8 21.377 1.245 1.245 ...	H1...
24 M69	PIPE 2.0	.145	2.481	5	.013 0	5	7.8 21.377 1.245 1.245 ...	H1...
25 M70	PIPE 2.0	.170	2.576	6	.015 0	5	7.8 21.377 1.245 1.245 ...	H1...
26 M71	PIPE 2.0	.067	6.297	4	.012 0	5	7.8 21.377 1.245 1.245 ...	H1...

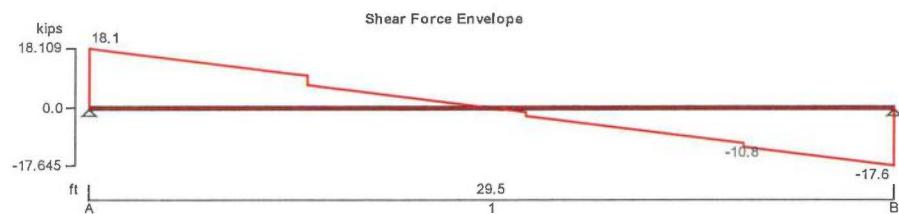
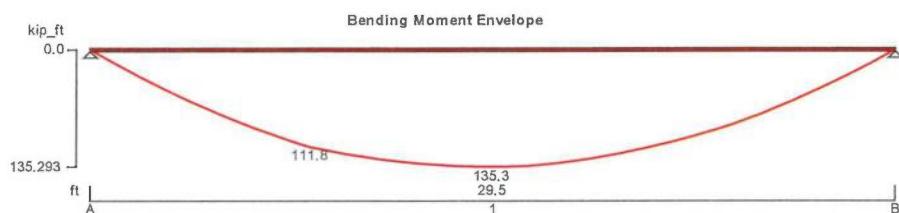
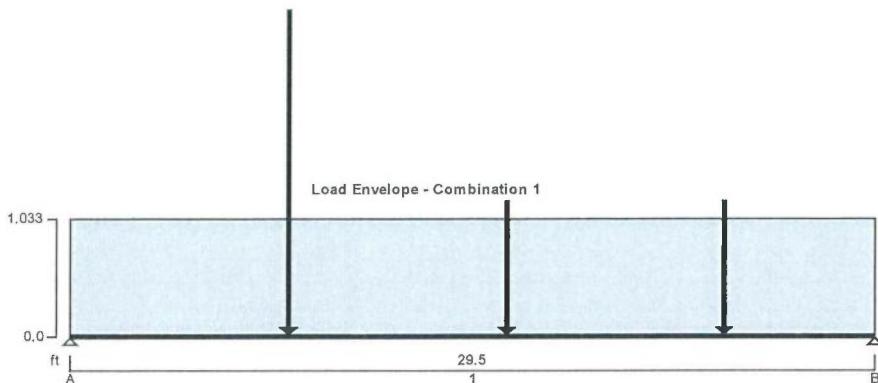


## Member Code Checks Displayed (Enveloped) Envelope Only Solution

CENTEK		SK - 2
CAG	CTFF039A WCSU Danbury	Sept 9, 2018 at 10:40 AM
18067.00	Unity Check	18067.00 CTFF039A WCSU Danbu...

**STEEL BEAM ANALYSIS & DESIGN (AISC360-05)**In accordance with AISC360 13<sup>th</sup> Edition published 2005 using the ASD method

Tedd's calculation version 3.0.12

**Support conditions**

Support A

Vertically restrained

Rotationally free

Support B

Vertically restrained

Rotationally free

**Applied loading**

Beam loads

self - Dead self weight of beam × 1

roof dead - Dead full UDL 0.533 kips/ft

Snow (drift) - Snow full UDL 0.45 kips/ft

Enclosure - Dead point load 2.88 kips at 96.00 in  
Enclosure - Dead point load 1.2 kips at 192.00 in  
Enclosure - Dead point load 1.2 kips at 288.00 in

### Load combinations

Load combination 1

Support A

Dead  $\times$  1.00

Snow  $\times$  1.00

Span 1

Dead  $\times$  1.00

Snow  $\times$  1.00

Support B

Dead  $\times$  1.00

Snow  $\times$  1.00

### Analysis results

Maximum moment

$M_{max} = 135.3$  kips\_ft

$M_{min} = 0$  kips\_ft

Maximum shear

$V_{max} = 18.1$  kips

$V_{min} = -17.6$  kips

Deflection

$\delta_{max} = 0.9$  in

$\delta_{min} = 0$  in

Maximum reaction at support A

$R_{A\_max} = 18.1$  kips

$R_{A\_min} = 18.1$  kips

Unfactored dead load reaction at support A

$R_{A\_Dead} = 11.5$  kips

Unfactored snow load reaction at support A

$R_{A\_Snow} = 6.6$  kips

Maximum reaction at support B

$R_{B\_max} = 17.6$  kips

$R_{B\_min} = 17.6$  kips

Unfactored dead load reaction at support B

$R_{B\_Dead} = 11$  kips

Unfactored snow load reaction at support B

$R_{B\_Snow} = 6.6$  kips

### Section details

Section type

W 18x50 (AISC 14th Edn 2010)

ASTM steel designation

A36

Steel yield stress

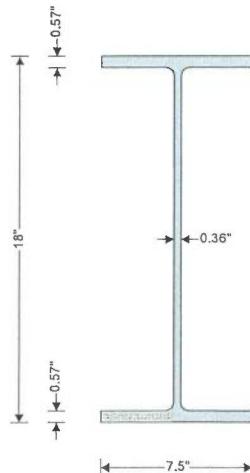
$F_y = 36$  ksi

Steel tensile stress

$F_u = 58$  ksi

Modulus of elasticity

$E = 29000$  ksi



### Safety factors

Safety factor for tensile yielding

$\Omega_{ly} = 1.67$

Safety factor for tensile rupture

$\Omega_{tr} = 2.00$

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	Section (E) W18x50				Sheet no./rev. 3	
	Calc. by CAG	Date 9/9/2018	Chk'd by	Date	App'd by	Date

Safety factor for compression  $\Omega_c = 1.67$

Safety factor for flexure  $\Omega_b = 1.67$

Safety factor for shear  $\Omega_v = 1.50$

#### Lateral bracing

Span 1 has continuous lateral bracing

#### Classification of sections for local buckling - Section B4.1

##### Classification of flanges in flexure - Table B4.1 (case 1)

Width to thickness ratio  $b_f / (2 \times t_f) = 6.58$

Limiting ratio for compact section  $\lambda_{pff} = 0.38 \times \sqrt{E/F_y} = 10.79$

Limiting ratio for non-compact section  $\lambda_{rff} = 1.0 \times \sqrt{E/F_y} = 28.38$  Compact

##### Classification of web in flexure - Table B4.1 (case 9)

Width to thickness ratio  $(d - 2 \times k) / t_w = 45.23$

Limiting ratio for compact section  $\lambda_{pwf} = 3.76 \times \sqrt{E/F_y} = 106.72$

Limiting ratio for non-compact section  $\lambda_{rwf} = 5.70 \times \sqrt{E/F_y} = 161.78$  Compact

**Section is compact in flexure**

#### Design of members for shear - Chapter G

Required shear strength  $V_r = \max(\text{abs}(V_{\max}), \text{abs}(V_{\min})) = 18.109 \text{ kips}$

Web area  $A_w = d \times t_w = 6.39 \text{ in}^2$

Web plate buckling coefficient  $k_v = 5$

Web shear coefficient - eq G2-2  $C_v = 1.000$

Nominal shear strength - eq G2-1  $V_n = 0.6 \times F_y \times A_w \times C_v = 138.024 \text{ kips}$

Allowable shear strength  $V_c = V_n / \Omega_v = 92.016 \text{ kips}$

**PASS - Allowable shear strength exceeds required shear strength**

#### Design of members for flexure in the major axis - Chapter F

Required flexural strength  $M_r = \max(\text{abs}(M_{s1\_max}), \text{abs}(M_{s1\_min})) = 135.293 \text{ kips\_ft}$

#### Yielding - Section F2.1

Nominal flexural strength for yielding - eq F2-1  $M_{nyld} = M_p = F_y \times Z_x = 303 \text{ kips\_ft}$

Nominal flexural strength  $M_n = M_{nyld} = 303.000 \text{ kips\_ft}$

Allowable flexural strength  $M_c = M_n / \Omega_b = 181.437 \text{ kips\_ft}$

**PASS - Allowable flexural strength exceeds required flexural strength**

#### Design of members for vertical deflection

Consider deflection due to dead and snow loads

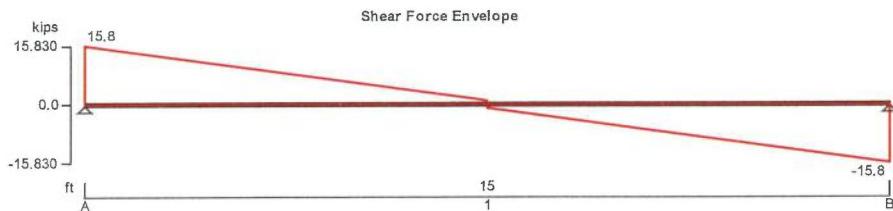
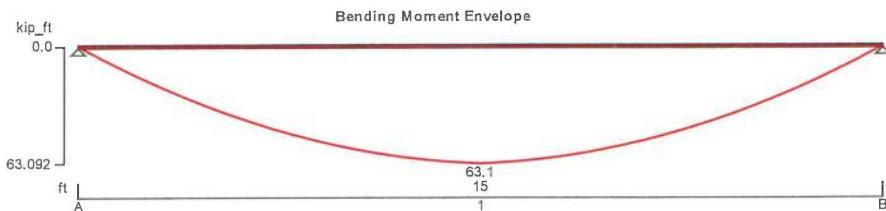
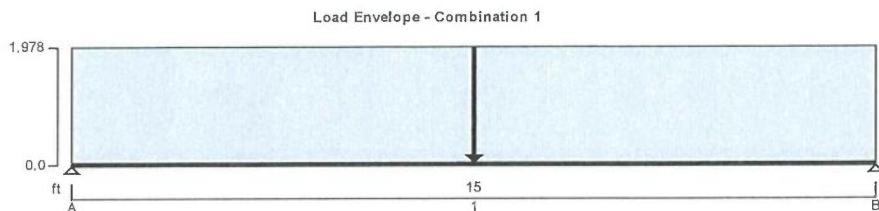
Limiting deflection  $\delta_{lim} = L_{s1} / 240 = 1.475 \text{ in}$

Maximum deflection span 1  $\delta = \max(\text{abs}(\delta_{\max}), \text{abs}(\delta_{\min})) = 0.916 \text{ in}$

**PASS - Maximum deflection does not exceed deflection limit**

**STEEL BEAM ANALYSIS & DESIGN (AISC360-10)**In accordance with AISC360 14<sup>th</sup> Edition published 2010 using the ASD method

Tedd's calculation version 3.0.12

**Support conditions**

Support A	Vertically restrained Rotationally free
Support B	Vertically restrained Rotationally free

**Applied loading**

Beam loads	self - Dead self weight of beam × 1 roof dead - Dead full UDL 1.047 kips/ft snow drift - snow full UDL 0.885 kips/ft Enclosure - Dead point load 1.99 kips at 90.00 in
------------	---

**Load combinations**

Load combination 1	Support A	Dead × 1.00 snow × 1.00
	Span 1	Dead × 1.00

snow x 1.00

Support B

Dead x 1.00

snow x 1.00

### Analysis results

Maximum moment

$M_{\max} = 63.1 \text{ kips}_\text{ft}$

$M_{\min} = 0 \text{ kips}_\text{ft}$

Maximum shear

$V_{\max} = 15.8 \text{ kips}$

$V_{\min} = -15.8 \text{ kips}$

Deflection

$\delta_{\max} = 0.1 \text{ in}$

$\delta_{\min} = 0 \text{ in}$

Maximum reaction at support A

$R_{A\_max} = 15.8 \text{ kips}$

$R_{A\_min} = 15.8 \text{ kips}$

Unfactored dead load reaction at support A

$R_{A\_Dead} = 9.2 \text{ kips}$

Unfactored snow load reaction at support A

$R_{A\_snow} = 6.6 \text{ kips}$

Maximum reaction at support B

$R_{B\_max} = 15.8 \text{ kips}$

$R_{B\_min} = 15.8 \text{ kips}$

Unfactored dead load reaction at support B

$R_{B\_Dead} = 9.2 \text{ kips}$

Unfactored snow load reaction at support B

$R_{B\_snow} = 6.6 \text{ kips}$

### Section details

Section type

W 18x46 (AISC 14th Edn 2010)

ASTM steel designation

A36

Steel yield stress

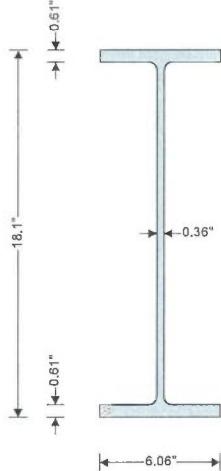
$F_y = 36 \text{ ksi}$

Steel tensile stress

$F_u = 58 \text{ ksi}$

Modulus of elasticity

$E = 29000 \text{ ksi}$



### Safety factors

Safety factor for tensile yielding

$\Omega_{ly} = 1.67$

Safety factor for tensile rupture

$\Omega_{lr} = 2.00$

Safety factor for compression

$\Omega_c = 1.67$

Safety factor for flexure

$\Omega_b = 1.67$

Safety factor for shear

$\Omega_v = 1.50$

### Lateral bracing

Span 1 has continuous lateral bracing

<b>CENTEK</b> engineering Centered on Solutions™ Centek Engineering, Inc. 63-2 North Branford Road Branford, CT 06405	Project CTFF039A WCSU Danbury				Job Ref. 18067.00	
	Section (E) W18x45				Sheet no./rev. 3	
	Calc. by CAG	Date 9/9/2018	Chkd by	Date	App'd by	Date

### Classification of sections for local buckling - Section B4.1

#### Classification of flanges in flexure - Table B4.1b (case 10)

Width to thickness ratio  $b_f / (2 \times t_f) = 5.01$

Limiting ratio for compact section  $\lambda_{pff} = 0.38 \times \sqrt{[E / F_y]} = 10.79$

Limiting ratio for non-compact section  $\lambda_{nff} = 1.0 \times \sqrt{[E / F_y]} = 28.38$  Compact

#### Classification of web in flexure - Table B4.1b (case 15)

Width to thickness ratio  $(d - 2 \times k) / t_w = 44.67$

Limiting ratio for compact section  $\lambda_{pwf} = 3.76 \times \sqrt{[E / F_y]} = 106.72$

Limiting ratio for non-compact section  $\lambda_{nwf} = 5.70 \times \sqrt{[E / F_y]} = 161.78$  Compact

**Section is compact in flexure**

### Design of members for shear - Chapter G

Required shear strength  $V_r = \max(\text{abs}(V_{\text{max}}), \text{abs}(V_{\text{min}})) = 15.830 \text{ kips}$

Web area  $A_w = d \times t_w = 6.516 \text{ in}^2$

Web plate buckling coefficient  $k_v = 5$

Web shear coefficient - eq G2-2  $C_v = 1.000$

Nominal shear strength - eq G2-1  $V_n = 0.6 \times F_y \times A_w \times C_v = 140.746 \text{ kips}$

Allowable shear strength  $V_c = V_n / \Omega_v = 93.830 \text{ kips}$

**PASS - Allowable shear strength exceeds required shear strength**

### Design of members for flexure in the major axis - Chapter F

Required flexural strength  $M_r = \max(\text{abs}(M_{s1\_max}), \text{abs}(M_{s1\_min})) = 63.092 \text{ kips\_ft}$

#### Yielding - Section F2.1

Nominal flexural strength for yielding - eq F2-1  $M_{nyld} = M_p = F_y \times Z_x = 272.1 \text{ kips\_ft}$

Nominal flexural strength  $M_n = M_{nyld} = 272.100 \text{ kips\_ft}$

Allowable flexural strength  $M_c = M_n / \Omega_b = 162.934 \text{ kips\_ft}$

**PASS - Allowable flexural strength exceeds required flexural strength**

### Design of members for vertical deflection

Consider deflection due to dead and snow loads

Limiting deflection  $\delta_{lim} = L_{s1} / 240 = 0.75 \text{ in}$

Maximum deflection span 1  $\delta = \max(\text{abs}(\delta_{\text{max}}), \text{abs}(\delta_{\text{min}})) = 0.121 \text{ in}$

**PASS - Maximum deflection does not exceed deflection limit**

## **ATTACHMENT D**

Service List of Abutters and Sample Letter to Abutters

## CERTIFICATION OF SERVICE

I hereby certify that on the 25<sup>th</sup> day of October, 2018, T-Mobile Northeast, LLC, provided notice of its Petition For A Declaratory Ruling That A Certificate of Environmental Compatibility And Public Need Is Not Required for the installation of a rooftop telecommunications facility proposed to be located at 181 White Street, Danbury, Connecticut, to the following:

### **Abutters**

4-6 Fifth Avenue  
Six Fifth Avenue Corp  
7 National Place  
Danbury, CT 06810

8-10 Fifth Avenue  
Manik & Valentina Roy  
P.O Box 117  
Danbury, CT 06813

12 Fifth Avenue  
Marc Burnett  
70 Cherniske Road  
New Milford, CT 06776

14 Fifth Avenue  
Craig Preveza  
34 Grammar School Drive  
Danbury, CT 06811

16 Fifth Avenue  
Paul Vitti & David Fiorita  
2 Belden Hill Road  
Brookfield, CT 06804

Fifth Avenue: Parcel I13//246//  
East Fifth Avenue Properties LLC  
3 Woodstone Court  
Danbury, CT 06811

20 Fifth Avenue  
Nuno & Celina Paulino  
5 Wildlife Drive  
New Milford, CT 06776

22 Fifth Avenue  
Nuno & Celina Paulino  
5 Wildlife Drive  
New Milford, CT 06776

24 Fifth Avenue  
24 Fifth Avenue Investors LLC  
24 Fifth Avenue  
Danbury, CT 06810

7 Hospital Avenue  
Joseph DaSilva, Jr.  
288 Main Street  
Danbury, CT 06810

2 Hospital Avenue  
Midwestern Connecticut Council  
of Alcoholism Inc.  
38 Old Ridgebury Road  
Danbury, CT 06810

67 Osborn Street  
City of Danbury Housing Authority  
2 Mill Ridge Road  
Danbury, CT 06810

69-71 Osborn Street  
John & Jill Hancock, Trustees  
69 ½ Osborn Street  
Danbury, CT 06810

73 ½ - 75 Osborn Street  
73 ½ - 75 Osborn St LLC  
P.O. Box 361  
Bethel, CT 06802

61 Osborn Street  
Steven Palmiotto  
P.O. Box 4352  
Danbury, CT 06813

51 Osborn Street  
City of Danbury  
155 Deer Hill Avenue  
Danbury, CT 06810

55 Osborn Street  
Alam Enterprises LLC  
P.O. Box 816  
Danbury, CT 06813

57 Osborn Street  
Alam Investment Company LLC  
P.O. Box 816  
Danbury, CT 06813

59 Osborn Street  
John Seo  
6 Jean Lake  
Rye Brook, NY 10573

50 Osborn Street  
CYMA LLC  
50 Osborne Street  
Danbury, CT 06810

69-71 Osborn Street  
John & Jill Hancock, Trustees  
69 ½ Osborn Street  
Danbury, CT 06810

77 Osborn Street  
Antonio & Rosa Ramos  
29 Tammany Trail  
Danbury, CT 06811

79 Osborn Street  
Ednilson DeOliveira &  
Celia Pereira Dos Santos  
79 Osborn Street  
Danbury, CT 06810

81 Osborn Street  
Carmen Batista & Jose Urena  
81 Osborn Street  
Danbury, CT 06810

83 Osborn Street  
Derek & Miriam DeMilio  
83 Osborn Street  
Danbury, CT 06810

85-87 Osborn Street  
V & L Ylagan Realty LLC  
85 Osborn Street  
Danbury, CT 06810

91 Osborn Street

Louis Butera, Trustee  
28 Westville Avenue  
Danbury, CT 06810

4 Roberts Avenue

State of Connecticut  
c/o Western Connecticut State University  
Attn: Luigi Marcone  
181 White Street  
Danbury, CT 06810

2 Roberts Avenue

State of Connecticut  
c/o Western Connecticut State University  
Attn: Luigi Marcone  
181 White Street  
Danbury, CT 06810

Roberts Avenue: Parcel J13//75//

State of Connecticut  
c/o Southern Connecticut State University  
Attn: Luigi Marcone  
181 White Street  
Danbury, CT 06810

Roberts Avenue: Parcel J13//76//

State of Connecticut  
210 Capital Avenue, Suite 1  
Hartford, CT 06106

155 White Street

William & Mary Lynn Mastro,  
Nicole Marie Mastro  
8 Farrell Road  
Newtown, CT 06470

162 White Street

Joaquim & Maria Narcisco  
104 Deer Hill Road  
Danbury, CT 06810

164 White Street

164 White Street LLC  
41 Corntassle Road  
Danbury, CT 06811

166 White Street

166 White Street LLC  
41 Corntassle Road  
Danbury, CT 06811

168-176 White Street

Callie Elliot & George Marnelakis, Trustees  
143 Variety Tree Circle  
Altamonte Springs, FL 32714

168-170 White Street

Hoffman Fuel Company of Danbury  
170 White Street  
Danbury, CT 06810

190 White Street

State of Connecticut  
210 Capital Avenue, Suite 1  
Hartford, CT 06106

188 White Street

State of Connecticut  
210 Capital Avenue, Suite 1  
Hartford, CT 06106

186 White Street

Western Connecticut State University  
181 White Street  
Danbury, CT 06810

182-184 White Street  
State of Connecticut  
c/o Western Connecticut State University  
Attn: Luigi Marcone  
181 White Street  
Danbury, CT 06810

178 White Street  
Dale Halas, Jr.  
3 Wheeler Drive  
Danbury, CT 06811

White Street: Parcel J13//63//  
State of Connecticut  
c/o Western Connecticut State University  
Attn: Luigi Marcone  
181 White Street  
Danbury, CT 06810

154 White Street  
154 White Street LLC  
85 Alberts Hill Road  
Sandy Hook, CT 06482

Dr. James Roach Avenue: Parcel J13//70//  
State of Connecticut  
c/o Western Connecticut State University  
Attn: Luigi Marcone  
181 White Street  
Danbury, CT 06810

### Property Owner

157-159 White Street  
State of Connecticut  
c/o Western Connecticut State University  
Attn: Luigi Marcone  
181 White Street  
Danbury, CT 06810

White Street: Parcel J13//001//  
State of Connecticut  
c/o Western Connecticut State University  
Attn: Luigi Marcone  
181 White Street  
Danbury, CT 06810

Respectfully submitted by,  
T-MOBILE NORTHEAST, LLC

By:   
Jesse A. Langer  
Updike, Kelly & Spellacy, P.C.  
8 Frontage Road  
East Haven, CT 06512  
(203) 786-8317  
Email: [jlangert@uks.com](mailto:jlangert@uks.com)



Jesse A. Langer  
(t) 203.786.8317  
(f) 203.772.2037  
jlanger@uks.com

October 25, 2018

**VIA CERTIFIED MAIL**  
**AND REGULAR MAIL**

Six Fifth Avenue Corp  
7 National Place  
Danbury, CT 06810

**RE: Proposed installation of rooftop telecommunications facility at 181 White Street, Danbury, Connecticut**

To Whom It May Concern:

I write on behalf of T-Mobile Northeast, LLC (“T-Mobile”). T-Mobile intends to file with the Connecticut Siting Council (“Council”) a petition for declaratory ruling (“Petition”) that a Certificate of Environmental Compatibility and Public Need is not required. The Petition addresses a proposed installation of a rooftop telecommunications facility (“Rooftop Facility”) proposed to be located within the midtown campus of Western Connecticut Statue University (“University”), specifically on the rooftop of the Ruth Haas Library (“Property”). The general address for the midtown campus is 181 White Street, Danbury, Connecticut.

As a wireless carrier licensed by the Federal Communications Commission, T-Mobile seeks out wireless sites that will meet its coverage and capacity objectives so that T-Mobile may provide reliable coverage throughout its network. T-Mobile has identified the Ruth Haas Library building within the midtown campus at the University for a rooftop telecommunications facility to address such coverage and capacity objectives in the area. The proposed Rooftop Facility would consist of the installation of nine (9) panel antennas on three (3) sectors and a future microwave dish, all to be mounted to the roof of the library on the Property.

This letter serves as notice to you as an abutting property owner pursuant to § 16-50j-40 of the Regulations of Connecticut State Agencies. T-Mobile will file the Petition on or about October 25, 2018, and will request that the Council place the Petition on some future agenda.

You may review the Petition at the office of the Council, which is located at 10 Franklin Square, New Britain, Connecticut, 06051, or at the City Hall for the City of Danbury. If you have any questions or concerns regarding this matter, please contact Jesse A. Langer of Updike, Kelly & Spellacy, P.C., at (203) 786-8317, or the Council.

Very truly yours,  
T-MOBILE NORTHEAST, LLC

By: \_\_\_\_\_

Jesse A. Langer  
Updike, Kelly & Spellacy, P.C.

## **ATTACHMENT E**

### **Service List of Municipal Officials and Government Agencies, with Letter to Host Municipality**

## **CERTIFICATION OF SERVICE**

I hereby certify that on the 25<sup>th</sup> day of October, 2018, T-Mobile Northeast, LLC, provided notice of its Petition For A Declaratory Ruling That A Certificate of Environmental Compatibility And Public Need Is Not Required for the installation of a rooftop telecommunications facility proposed to be located at 181 White Street, Danbury, Connecticut, to the following:

### **City of Danbury**

City of Danbury  
Mark D. Boughton, Mayor  
City Hall  
155 Deer Hill Avenue  
Danbury, CT 06810

City of Danbury  
Planning and Zoning Commission  
Sharon B. Calitro, Director  
City Hall  
155 Deer Hill Avenue  
Danbury, CT 06810

City of Danbury  
Janice R. Giegler, Town Clerk  
City Hall  
155 Deer Hill Avenue  
Danbury, CT 06810

City of Danbury  
Zoning Board of Appeals  
Richard S. Jowdy, Chairman  
City Hall  
155 Deer Hill Avenue  
Danbury, CT 06810

City of Danbury  
Environmental Impact Commission  
Bernard P. Gallo, Chairman  
City Hall  
155 Deer Hill Avenue  
Danbury, CT 06810

City of Danbury  
Conservation Commission  
Kim Botelho, Chair  
City Hall  
155 Deer Hill Avenue  
Danbury, CT 06810

### **State and Regional**

The Honorable George Jepsen  
Attorney General  
Office of the Attorney General  
55 Elm Street  
Hartford, CT 06106

Department of Emergency Services  
and Public Protection  
Division of Emergency Management  
and Homeland Security  
*c/o* William J. Hackett, Deputy Commissioner  
25 Sigourney Street, 6th Floor  
Hartford, CT 06106-5042

Department of Public Health  
*c/o* Raul Pino, MD, MPH  
Commissioner  
410 Capital Avenue  
Hartford, CT 06106

Council on Environmental Quality  
*c/o* Susan D. Merrow, Chair  
79 Elm Street  
Hartford, CT 06106

Department of Energy  
& Environmental Protection  
*c/o* Rob Klee, Commissioner  
79 Elm Street  
Hartford, CT 06106

Office of Policy and Management  
*c/o* Benjamin Barnes, Secretary  
450 Capitol Avenue  
Hartford, CT 06106-1379

Department of Economic and Community  
Development  
Offices of Culture and Tourism  
*c/o* Randy Fiveash, Director  
450 Columbus Boulevard, Suite 5  
Hartford, CT 06103

Department of Economic and Community  
Development  
State Historic Preservation Office  
*c/o* Kristina Newman-Scott, Director of  
Culture & State Historic Preservation Officer  
450 Columbus Boulevard, Suite 5  
Hartford, CT 06103

Michael A. McLachlan  
State Senate; 24<sup>th</sup> District  
Legislative Office Building, Room 3400  
Hartford, CT 06106-1591

Public Utilities Regulatory Authority  
*c/o* Katie Dykes, Chair  
Ten Franklin Square  
New Britain, CT 06051

Department of Economic  
and Community Development  
*c/o* Catherine H. Smith, Commissioner  
450 Columbus Boulevard, Suite 5  
Hartford, CT 06103

Department of Agriculture  
*c/o* Steven K. Reviczky, Commissioner  
450 Columbus Boulevard, Suite 701  
Hartford, CT 06103

Department of Transportation  
*c/o* James P. Redeker, Commissioner  
2800 Berlin Turnpike  
Newington, CT 06131-7546

Western Connecticut Council of Governments  
*c/o* Jayme Stevenson, Chairman  
1 Riverside Road  
Sandy Hook, CT 06482

David Arconti  
State Representative; 109<sup>th</sup> District  
Legislative Office Building, Room 4034  
Hartford, CT 06106-1591

**Federal**

U.S. Department of Transportation  
Federal Aviation Administration  
*c/o* Dan Elwell, Acting Administrator  
800 Independence Avenue, SW  
Washington, DC 20591

U.S. Senator Christopher Murphy  
Colt Gateway, Suite 401  
120 Huyshope Avenue  
Hartford, CT 06106

Federal Communications Commission  
*c/o* Ajit Pai, Chairman  
445 12th Street SW  
Washington, DC 20554

U.S. Representative Elizabeth Esty  
1 Grove Street, Suite 600  
New Britain, CT 06053

U.S. Senator Richard Blumenthal  
90 State House Square, 10th Floor  
Hartford, CT 06103

Respectfully submitted by,

T-MOBILE NORTHEAST, LLC

By:



Jesse A. Langer  
Updike, Kelly & Spellacy, P.C.  
8 Frontage Road  
East Haven, CT 06512  
(203) 786-8317  
Email: jlanger@uks.com

October 25, 2018

**VIA CERTIFIED MAIL**  
**AND REGULAR MAIL**

City of Danbury  
Mark D. Boughton, Mayor  
City Hall  
155 Deer Hill Avenue  
Danbury, CT 06810

**RE: Proposed installation of rooftop telecommunications facility at 181 White Street, Danbury, Connecticut**

To Whom It May Concern:

I write on behalf of T-Mobile Northeast, LLC (“T-Mobile”). T-Mobile intends to file with the Connecticut Siting Council (“Council”) a petition for declaratory ruling (“Petition”) that a Certificate of Environmental Compatibility and Public Need is not required. The Petition addresses a proposed installation of a rooftop telecommunications facility (“Rooftop Facility”) proposed to be located within the midtown campus of Western Connecticut Statue University (“University”), specifically on the rooftop of the Ruth Haas Library (“Property”). The general address for the midtown campus is 181 White Street, Danbury, Connecticut.

As a wireless carrier licensed by the Federal Communications Commission, T-Mobile seeks out wireless sites that will meet its coverage and capacity objectives so that T-Mobile may provide reliable coverage throughout its network. T-Mobile has identified the Ruth Haas Library building within the midtown campus at the University for a rooftop telecommunications facility to address such coverage and capacity objectives in the area. The proposed Rooftop Facility would consist of the installation of nine (9) panel antennas on three (3) sectors and a future microwave dish, all to be mounted to the roof of the library on the Property.

This letter serves as notice to you as an “appropriate municipal official[sic] and government agenc[y]” as that term is defined under § 16-50j-40 of the Regulations of Connecticut State Agencies. T-Mobile will file the Petition on or about October 25, 2018, and will request that the Council place the Petition on some future agenda.

Attached please find a copy of the Petition. If you have any questions or concerns regarding this matter, please contact Jesse A. Langer of Updike, Kelly & Spellacy, P.C., at (203) 786-8317, or the Council.

Very truly yours,  
T-MOBILE NORTHEAST, LLC

By:



Jesse A. Langer  
Updike, Kelly & Spellacy, P.C.

**ATTACHMENT F**

Visual Assessment and Photo-Simulations

**Photographic Simulation Package**

**Danbury - CTff039A**

**181 White Street  
Danbury, CT 06810**



**Centek Project No. 18067.00**

**Prepared For  
Transcend Wireless  
T-mobile**

**Prepared By  
Centek Engineering, Inc.  
63 North Branford Road  
Branford, CT 06405  
T: 203.488.0580  
F: 203.488.8587  
[www.centekeng.com](http://www.centekeng.com)**

**Date 10.09.2018**

**CENTEK** engineering  
Centered on Solutions<sup>SM</sup>

**Transcend Wireless**

**T-Mobile**



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**CENTEK** Engineering, Inc.  
Photographic Simulation Package  
T-Mobile – New Site Development – CTFF039A  
Danbury, CT  
October 9, 2018

At the request of Transcend Wireless, acting on behalf of T-Mobile, CENTEK Engineering, Inc. ("CENTEK") completed this visual assessment and prepared computer-generated photographic simulations depicting the proposed installation of a wireless telecommunications facility ("Facility") located at 181 White Street, Danbury, Connecticut which will be referred throughout this summary as "the host property."

The host property is located north of White Street and east of 5<sup>th</sup> Avenue on the campus of Western Connecticut State University ("WCSU"). See *Figure 1 – Photolog Key Legend*. The host property is located in a High-Rise Residential District (RH-3), which is a mixed residential district intended to provide for high density residential, limited commercial, institutional and neighborhood uses in the "urban core" of the City of Danbury. The WCSU campus includes a multi-story parking garage, the Ruth A. Haas Library ("Library"), a concert hall, recreational fields and other uses incident to a college campus. Beyond the school grounds, the surrounding land use is primarily residential with some limited commercial uses.

The proposed Facility would include twelve (12) panel antennas and nine remote radio units split over three (3) sectors on the high roof of the library located on the host property. All of the rooftop mounted antennas and associated appurtenances would be installed behind radio frequency (RF) transparent enclosure designed to resemble a decorative mansard roof similar to the one located on the adjacent building to the south. The RF transparent enclosure would be painted to match the patina found on the adjacent building's mansard roof and would extend approximately 10-feet above the roof. Associated support equipment would be placed within a ±10-ft x 12-ft elevated non-penetrating rooftop steel platform located on the existing low roof of the Haas library. The support equipment would be installed as close to the high roof façade as possible to eliminate visibility from grade. Utilities would be routed through the existing building via conduits within existing utility chases. The proposed Facility component locations are illustrated within construction drawings as prepared by CENTEK dated October 10<sup>th</sup>, 2018.

On August 8<sup>th</sup>, 2018, CENTEK personnel conducted a field visit to obtain photo-documentation of the existing conditions. At each photo location, the geographic coordinates were logged using global positioning system ("GPS") technology. Photographs were taken with a Cannon Rebel EOS T5 digital camera body and Canon 75 to 300 millimeter ("mm") zoom lens using a focal length of 75 mm for consistency.

Computer models were developed for the building and proposed telecommunications facility components within AutoCad and Revit. Photographic simulations were then created to depict to scale representations of the proposed installation. Using field data, site plan information and image editing software, the proposed Facility was scaled to the correct location and height, relative to the existing structure and surrounding area. A photo key map and copies of the existing conditions and photo-simulations are attached.

Three (3) photo-locations were simulated and represent unobstructed views towards the proposed installation(s). The table below provides a description of each location, view orientation, and approximate distance between where the photo was taken and the proposed Facility.

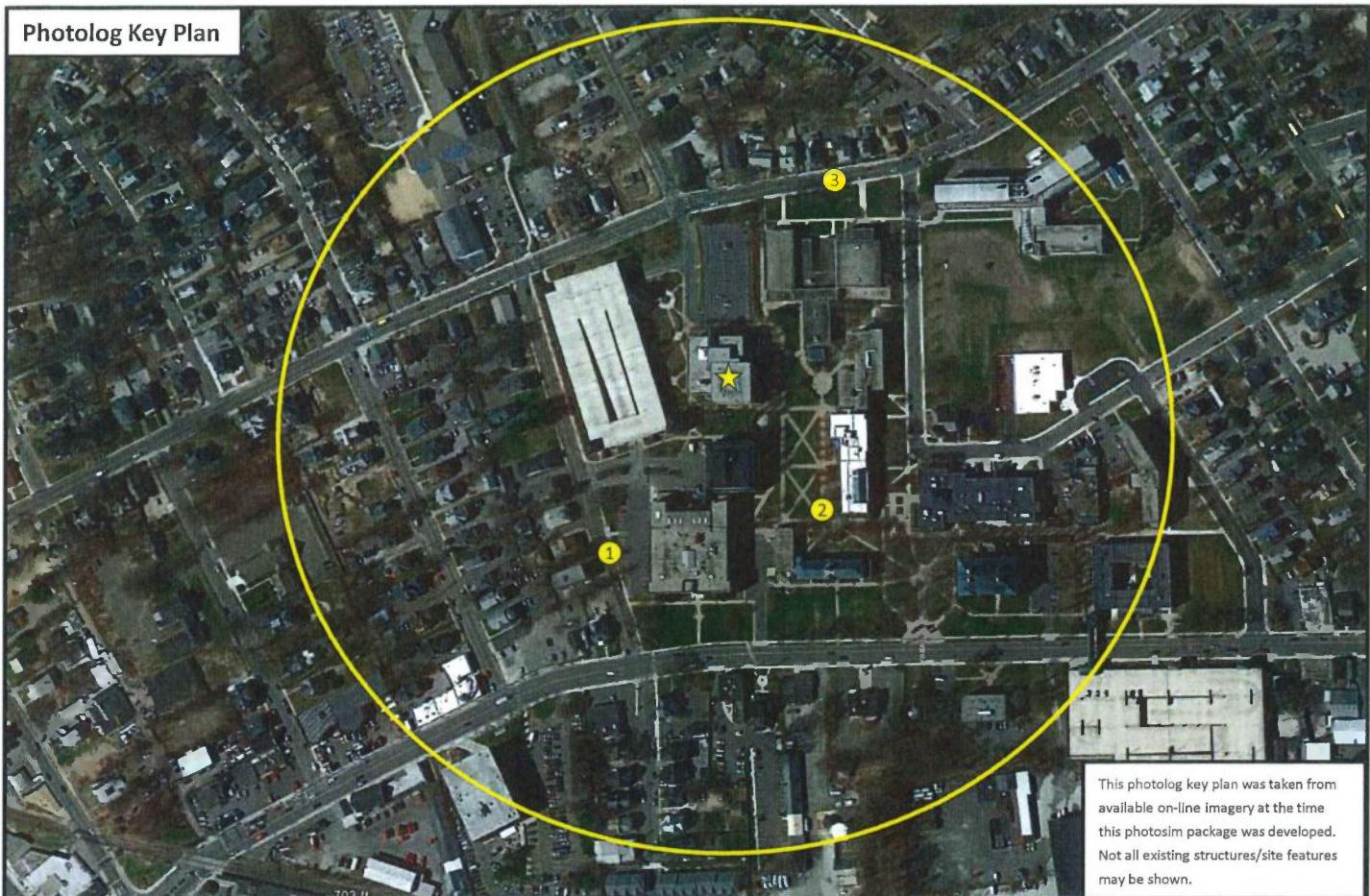
View	Location	Orientation	Distance to Site
1	Host Property	Northeast	<b>±367-ft</b>
2	Host Property	Northwest	<b>±230-ft</b>
3	Host Property	Southwest	<b>±446-ft</b>

In conclusion, the affected views of the proposed Facility would be limited to locations less than 1/8 of a mile on the host property and immediately abutting properties to the north and southwest of the library. Enclosing the proposed Facility components within the mansard enclosure would create fluency within the existing aesthetic of the surrounding buildings located in proximity of the host property.

Based on the results of this assessment, it is our opinion that the proposed installation of the Facility would not have an adverse visual impact on existing views of the Library or the character of the surrounding community.

### Assumptions

This photographic simulation package provides a representation of the Facility under similar conditions as those encountered during our field visit. This package is static in nature and does not necessarily fairly characterize the prevailing views from all locations within a given area. View of the Facility can change throughout the seasons and the time of day, and are dependent on weather and other atmospheric conditions (e.g., haze, fog, clouds, etc.); the location, angle and intensity of the sun; and the specific view location.



**T-Mobile Site -**

**Danbury-CTFF039A**  
 Centek Project #18067.00  
 181 White Street  
 Danbury, CT 06810

**CENTEK** engineering

Centered on Solutions™

63-2 North Branford Road, Branford, CT 06405 203.488.0580 Fax 203.488.8587 [www.CentekEng.com](http://www.CentekEng.com)



*Transcend Wireless*

**Photolog Legend**

- ★ Proposed RF Transparent Screening
- 1000' Radius
- Photo Location - (Year round visibility)



Centek Project # 18067.00

Existing Photo # : 1  
GPS Coordinates (Library): 41.40104 -73.44619  
Distance to Library: 367 Feet  
Orientation: Looking Northeast  
Visibility: Year Round

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2



Centek Project # 18067.00

Simulation Photo # : 1  
GPS Coordinates (Library): 41.40104 -73.44619  
Distance to Library: 267 Feet  
Orientation: Looking Northeast  
Visibility: Year Round

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Centek Project # 18067.00

Existing Photo #: 2  
GPS Coordinates (Library): 41.40104 -73.44619  
Distance to Library: 230 Feet  
Orientation: Looking Northwest  
Visibility: Year Round

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Centek Project # 18067.00

Simulation Photo # : 2  
GPS Coordinates (Library): 41.40104 -73.44619  
Distance to Library: 230 Feet  
Orientation: Looking Northwest  
Visibility: Year Round

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Centek Project # 18067.00

Existing Photo # : 3  
GPS Coordinates (Library): 41.40104 -73.44619  
Distance to Library: 446 Feet  
Orientation: Looking Southwest  
Visibility: Year Round

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Centek Project # 18067.00

Simulation Photo # : 3  
GPS Coordinates (Library): 41.40104 -73.44619  
Distance to Library: 446 Feet  
Orientation: Looking Southwest  
Visibility: Year Round

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**ATTACHMENT G**

EME



## RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CTFF039A

WCSU Cell Split  
181 White Street  
Danbury, CT 06810

**September 14, 2018**

**EBI Project Number: 6218006175**

Site Compliance Summary	
Compliance Status:	<b>COMPLIANT</b>
Site total MPE% of FCC general population allowable limit:	<b>17.43 %</b>



September 14, 2018

T-Mobile USA  
Attn: Jason Overbey, RF Manager  
35 Griffin Road South  
Bloomfield, CT 06002

## Emissions Analysis for Site: **CTFF039A – WCSU Cell Split**

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **181 White Street, Danbury, CT**, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately  $400 \mu\text{W}/\text{cm}^2$  and  $467 \mu\text{W}/\text{cm}^2$  respectively. The general population exposure limit for the 1900 MHz (PCS) and 2100 MHz (AWS) frequency bands is  $1000 \mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at **181 White Street, Danbury, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturers supplied specifications, minus 10 dB for directional panel antennas, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 1 GSM channels (PCS Band - 1900 MHz) was considered for each sector of the proposed installation. These Channels have a transmit power of 15 Watts per Channel.
- 2) 1 UMTS channel (AWS Band – 2100 MHz) was considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 3) 2 LTE channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 4) 4 LTE channels (AWS Band – 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 5) 2 LTE channels (600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 6) 2 LTE channels (700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 20 Watts per Channel.



- 7) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 8) For the following calculations the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 9) The antennas used in this modeling are the **Ericsson AIR 3246 B66 & RFS APX16DWV-16DWVS-E-A20** and the **RFS APXVAARR24\_43-U-NA20** for 600 MHz, 700 MHz, 1900 MHz and 2100 MHz channels. There is also one **Ericsson AIR 5121 n257** (5G) antenna to be installed per sector for future use. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 10) The antenna mounting height centerline of the proposed antennas is **65.5 feet** above ground level (AGL).
- 11) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
- 12) All calculations were done with respect to uncontrolled / general population threshold limits.



## T-Mobile Site Inventory and Power Data

Sector:	A	Sector:	B	Sector:	C
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	Ericsson AIR 3246 B66	Make / Model:	Ericsson AIR 3246 B66	Make / Model:	Ericsson AIR 3246 B66
Gain:	15.9 dBd	Gain:	15.9 dBd	Gain:	15.9 dBd
Height (AGL):	65.5 feet	Height (AGL):	65.5 feet	Height (AGL):	65.5 feet
Frequency Bands	2100 MHz (AWS)	Frequency Bands	2100 MHz (AWS)	Frequency Bands	2100 MHz (AWS)
Channel Count	4	Channel Count	4	Channel Count	4
Total TX Power(W):	160	Total TX Power(W):	160	Total TX Power(W):	160
ERP (W):	6,224.72	ERP (W):	6,224.72	ERP (W):	6,224.72
Antenna A1 MPE%	6.32	Antenna B1 MPE%	6.32	Antenna C1 MPE%	6.32
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	APX16DWV-16DWVS-E-A20	Make / Model:	APX16DWV-16DWVS-E-A20	Make / Model:	APX16DWV-16DWVS-E-A20
Gain:	16.3 dBd	Gain:	16.3 dBd	Gain:	16.3 dBd
Height (AGL):	65.5 feet	Height (AGL):	65.5 feet	Height (AGL):	65.5 feet
Frequency Bands	1900 MHz (PCS)	Frequency Bands	1900 MHz (PCS)	Frequency Bands	1900 MHz (PCS)
Channel Count	2	Channel Count	2	Channel Count	2
Total TX Power(W):	80	Total TX Power(W):	80	Total TX Power(W):	80
ERP (W):	3,412.64	ERP (W):	3,412.64	ERP (W):	3,412.64
Antenna A2 MPE%	3.47	Antenna B2 MPE%	3.47	Antenna C2 MPE%	3.47
Antenna #:	3	Antenna #:	3	Antenna #:	3
Make / Model:	APXVAARR24_43-U-NA20	Make / Model:	APXVAARR24_43-U-NA20	Make / Model:	APXVAARR24_43-U-NA20
Gain:	16.35 / 12.95 / 13.35 dBd	Gain:	16.35 / 12.95 / 13.35 dBd	Gain:	16.35 / 12.95 / 13.35 dBd
Height (AGL):	65.5 feet	Height (AGL):	65.5 feet	Height (AGL):	65.5 feet
Frequency Bands	2100 MHz / 600 MHz / 700 MHz	Frequency Bands	2100 MHz / 600 MHz / 700 MHz	Frequency Bands	2100 MHz / 600 MHz / 700 MHz
Channel Count	5	Channel Count	5	Channel Count	5
Total TX Power(W):	160	Total TX Power(W):	160	Total TX Power(W):	160
ERP (W):	4,169.10	ERP (W):	4,169.10	ERP (W):	4,169.10
Antenna A3 MPE%	7.64	Antenna B3 MPE%	7.64	Antenna C3 MPE%	7.64
Antenna #:	4	Antenna #:	4	Antenna #:	4
Make / Model:	Ericsson AIR 5121 n257 <b>(FUTURE USE)</b>	Make / Model:	Ericsson AIR 5121 n257 <b>(FUTURE USE)</b>	Make / Model:	Ericsson AIR 5121 n257 <b>(FUTURE USE)</b>
Gain:	15.05	Gain:	15.05	Gain:	15.05
Height (AGL):	65.5	Height (AGL):	65.5	Height (AGL):	65.5
Frequency Bands	NA	Frequency Bands	NA	Frequency Bands	NA
Channel Count	NA	Channel Count	NA	Channel Count	NA
Total TX Power(W):	0.00	Total TX Power(W):	0.00	Total TX Power(W):	0.00
ERP (W):	0.00	ERP (W):	0.00	ERP (W):	0.00
Antenna A3 MPE%	0.00	Antenna B3 MPE%	0.00	Antenna C3 MPE%	0.00



## Site Summary Tables

Site Composite MPE%	
Carrier	MPE%
T-Mobile (Per Sector Max)	17.43 %
No Additional Carriers on this Facility	NA
Site Total MPE %:	17.43 %

T-Mobile Sector A Total:	17.43 %
T-Mobile Sector B Total:	17.43 %
T-Mobile Sector C Total:	17.43 %
Site Total:	17.43 %

## T-Mobile Maximum MPE Power Values (Per Sector)

T-Mobile Frequency Band / Technology (Per Sector)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ( $\mu\text{W}/\text{cm}^2$ )	Frequency (MHz)	Allowable MPE ( $\mu\text{W}/\text{cm}^2$ )	Calculated % MPE
T-Mobile AWS - 2100 MHz LTE	4	1,556.18	65.5	63.21	AWS - 2100 MHz	1000.00	6.32%
T-Mobile PCS - 1900 MHz LTE	2	1,706.32	65.5	34.65	PCS - 1900 MHz	1000.00	3.47%
T-Mobile AWS - 2100 MHz UMTS	1	1,726.08	65.5	17.53	AWS - 2100 MHz	1000.00	1.75%
T-Mobile 600 MHz LTE	2	788.97	65.5	16.02	600 MHz	400.00	4.01%
T-Mobile 700 MHz LTE	2	432.54	65.5	8.78	700 MHz	467.00	1.88%
						Total:	17.43%

## Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)
Sector A:	17.43 %
Sector B:	17.43 %
Sector C:	17.43 %
T-Mobile Maximum MPE % (Per Sector):	17.43 %
Site Total:	17.43 %
Site Compliance Status:	<b>COMPLIANT</b>

The anticipated composite MPE value for this site assuming all carriers present is **17.43%** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

**ATTACHMENT H**  
**FAA Compliance Report**

September 19, 2018

Ms. Jenn Dupont  
T-Mobile USA  
c/o Transcend Wireless LLC  
35 Griffin Road  
Bloomfield, CT 06002

**Subject:** **Federal Aviation Administration (FAA) Compliance Results**  
**Proposed T-Mobile USA Project**  
**Site No. CTFF039A / Danbury**  
**181 White Street**  
**Danbury, CT 06810**  
**EBI Project No. 6118007484**

Dear Ms. Dupont

Enclosed please find the results of the Federal Aviation Administration (FAA) Compliance studies for the above-referenced site. The studies were completed based on information provided by Transcend Wireless LLC on behalf of T-Mobile USA, and gathered from the Land Survey and Site Plans, attached as Appendix A.

EBI utilized both commercially available and publicly accessible software that runs algorithms in accordance with FAA glide-slope calculations, referenced in Federal Aviation Regulation (FAR) Part 77 and FCC Rulepart 47 CFR 17, to determine the need for filing with the FAA and if registration with the FCC is required. For this site, our analysis demonstrated that notice to the FAA and an Antenna Structure Registration with the FCC are not required. Thus, the site may proceed from an FAA Compliance perspective.

If the proposed project location or proposed height of the structure changes, please notify EBI Consulting, and we will be happy to conduct FAA Compliance studies based on the changes.

Land Survey and Site Plans – Appendix A

Latitude (NAD 83): 41° 24' 3.721" N  
Longitude (NAD 83): 73° 26' 46.326" W  
Site Ground Elevation (AMSL): 392.53 feet  
Proposed Structure Height (AGL): 71.96 feet

Airspace© Studies – Appendix B

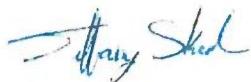
**PASS.** This site passed all Airspace studies, and notice to the FAA is not required,

FCC TOWAIR – Appendix C

**PASS.** This site does not require FCC registration based on the 6.10-meter (20-foot) rule.

Thank you for the opportunity to be of service to Transcend Wireless LLC (on behalf of T-Mobile USA), and please don't hesitate to contact us with any questions or if we can assist with any of your future regulatory needs.

Respectfully Submitted,



Ms. Tiffany Skrobiszewski  
Author/FAA Specialist  
TEL: 757-582-3866



Mr. Ian Swanson  
T-Mobile USA Program Manager  
TEL: 339-933-0448

Appendix A: Land Survey and Site Plans  
Appendix B: Airspace© Studies  
Appendix C: FCC TOWAIR Results



Centered on Solutions™

## FAA 2-C CERTIFICATION

**Applicant:** T-Mobile Northeast LLC  
35 Griffin Rd S  
Bloomfield, CT 06002

**Site Name:** CTFF039A

**Address:** 181 White Street  
Danbury, CT 06810

**Horizontal Datum Source:**

Ground Survey  GPS Survey  NAD 83  NAD 27

**Vertical Datum Source:**

Ground Survey  GPS Survey  NAVD 88  NGVD 29

**Structure Type:**

<input checked="" type="checkbox"/> Existing	<input type="checkbox"/> Monopole Tower	<input type="checkbox"/> Transmission Tower	<input type="checkbox"/> Utility Pole
<input type="checkbox"/> Proposed	<input type="checkbox"/> SST Lattice Tower	<input type="checkbox"/> Smokestack	<input checked="" type="checkbox"/> Roof Top
	<input type="checkbox"/> Guyed Lattice Tower	<input type="checkbox"/> Water Tank	<input type="checkbox"/> Other (describe)

**Latitude:** N 41° 24' 03.721" NAD83 N 41.4010335° NAD83

**Longitude:** W 73° 26' 46.326" NAD83 W 73.4462017° NAD83

**Ground Elevation:** 392.53 feet AMSL

**Top of Existing Roof:** 61.55 ± feet AGL 454.08 ± feet AMSL

**Top of Existing Roof Parapet:** 61.96 ± feet AGL 454.49 ± feet AMSL

**Top of Proposed Antenna:** 71.96 ± feet AGL 464.49 ± feet AMSL

**Top of Proposed Antenna Concealment Enclosure:** 71.96 ± feet AGL 464.49 ± feet AMSL

**Certification:** I certify that the Latitude and Longitude noted hereon are accurate to within ± 50 feet horizontally and that the site elevation is accurate to within ± 20 feet vertically. The top of proposed antenna height is 71.96 ± feet AGL (464.49 ± AMSL). The overall height is the top of proposed antenna as well as the proposed antenna concealment enclosure at 71.96 ± feet AGL (464.49 ± AMSL). The horizontal datum (coordinates) are in terms of the North American Datum of 1983 (NAD 83) and are expressed in degrees minutes and seconds to the nearest thousandth of a second. The vertical datum (heights) is in terms of the National Geodetic Vertical Datum of 1988 and expressed to the nearest hundredth of a foot.

Company:

Centek Engineering, Inc.

Signature:

PE Name & License No.:

Carlo F. Centore, PE (Lic. No. CT16694)

Date Issued:

5/9/2018



## TOWAIR Determination Results

### \*\*\* NOTICE \*\*\*

TOWAIR's findings are not definitive or binding, and we cannot guarantee that the data in TOWAIR are fully current and accurate. In some instances, TOWAIR may yield results that differ from application of the criteria set out in 47 C.F.R. Section 17.7 and 14 C.F.R. Section 77.13. A positive finding by TOWAIR recommending notification should be given considerable weight. On the other hand, a finding by TOWAIR recommending either for or against notification is not conclusive. It is the responsibility of each ASR participant to exercise due diligence to determine if it must coordinate its structure with the FAA. TOWAIR is only one tool designed to assist ASR participants in exercising this due diligence, and further investigation may be necessary to determine if FAA coordination is appropriate.

#### DETERMINATION Results

**Structure does not require registration. The structure meets the 6.10-meter (20-foot) Rule criteria.**

#### Your Specifications

#### NAD83 Coordinates

Latitude	41-24-03.7 north
Longitude	073-26-46.3 west

#### Measurements (Meters)

Overall Structure Height (AGL)	21.9
Support Structure Height (AGL)	18.9
Site Elevation (AMSL)	119.6

#### Structure Type

B - Building

#### [Tower Construction Notifications](#)

Notify Tribes and Historic Preservation Officers of your plans to build a tower.

[CLOSE WINDOW](#)