STATE OF CONNECTICUT



CONNECTICUT SITING COUNCIL
Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov www.ct.gov/csc

April 26, 2019

Paul R. Michaud, Esq. Michaud Law Group LLC 515 Centerpoint Drive, Suite 502 Middletown, CT 06457

RE: **PETITION NO. 1312** - Candlewood Solar LLC declaratory ruling that no Certificate of Environmental Compatibility and Public Need is required for the proposed construction, maintenance and operation of a 20 megawatt AC (26.5 megawatt DC) solar photovoltaic electric generating facility located on a 163 acre parcel at 197 Candlewood Mountain Road and associated electrical interconnection to Eversource Energy's Rocky River Substation on Kent Road in New Milford, Connecticut. **Development and Management Plan.**

Dear Attorney Michaud:

At a public meeting of the Connecticut Siting Council (Council) held on April 25, 2019, the Council considered and approved the Development and Management (D&M) Plan submitted for this project on January 28, 2019 with the following conditions:

- 1. Pursuant to RCSA §16-50j-62, submit the applicable revisions including, but not limited to, the solar array layout, clearing limits, fence design and stormwater management plan for Council review and approval prior to the commencement of construction; and
- 2. Submit a copy of the Department of Energy and Environmental Protection (DEEP) General Permit and DEEP-approved stormwater management plan prior to commencement of construction.

This approval applies only to the D&M Plan submitted on January 28, 2019 and supplemental data dated March 5, 2019 and April 4, 2019. Requests for any changes to the D&M Plan shall be approved by Council staff in accordance with Regulations of Connecticut State Agencies (RCSA) §16-50j-62(b). Furthermore, the project developer is responsible for reporting requirements pursuant to RCSA §16-50j-62.

This decision is under the exclusive jurisdiction of the Council and is not applicable to any other modification or construction. All work is to be implemented as specified in the Council's decision on the petition dated December 22, 2017 and in the D&M Plan dated January 28, 2019.

Enclosed is a copy of the staff report on this D&M Plan, dated April 25, 2019.

Thank you for your attention and cooperation.

Sincerely,

Melanie A. Bachman Executive Director

RS/MP/laf

Enclosure: Staff Report dated April 25, 2019

c: Parties and Intervenors

The Honorable Pete Bass, Mayor, Town of New Milford
Laura Regan, Zoning Enforcement Officer, Town of New Milford
The Honorable Stephen C. Dunn, First Selectman, Town of Brookfield
Francis Lollie, Zoning Enforcement Officer, Town of Brookfield
Alice Dew, Wetlands Enforcement Officer & Land Use Manager, Town of Brookfield
The Honorable Patricia Del Monaco, First Selectman, Town of New Fairfield
Evan White, Zoning Enforcement Officer, Town of New Fairfield



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Petition No. 1312
Candlewood Solar, LLC
Development & Management Plan
197 Candlewood Mountain Road, New Milford
Staff Report
April 25, 2019

On December 21, 2017, the Connecticut Siting Council (Council) issued a Declaratory Ruling to Candlewood Solar, LLC (CS), pursuant to Connecticut General Statutes (CGS) §4-176 and §16-50k, for the construction, maintenance, and operation of an approximately 20 megawatt (MW) alternating current (AC) solar photovoltaic electric generating facility and associated electrical interconnection at 197 Candlewood Mountain Road, New Milford, Connecticut. In its Declaratory Ruling, the Council required CS to submit a Development and Management Plan (D&M Plan). On January 28, 2019, CS submitted its D&M Plan for this project. On or about January 28, 2019, copies of the D&M Plan were provided to the Town of New Milford, the Town of Brookfield, the Town of New Fairfield, as well as all parties on the service list.¹

On February 19, 2019, the Council issued Set One interrogatories to CS. On March 5, 2019, CS submitted responses to Council interrogatories. Pursuant to Section 16-50j-60(d) of the Regulations of Connecticut State Agencies (RCSA), the 60-day deadline for the Council to approve, modify, or disapprove the D&M Plan was March 29, 2019. By letter dated March 5, 2019, the Council requested an extension of the D&M Plan deadline until May 10, 2019. By letter dated March 13, 2019, CS consented to the extension of the D&M Plan deadline to May 10, 2019. On March 7, 2019, the Council issued Set Two interrogatories to CS. By letter dated March 19, 2019, CS noted that the Department of Energy and Environmental Protection (DEEP) issued a Notice of Rejection without prejudice in connection with CS's January 2, 2019 General Permit (GP) registration, and thus, CS requested a two-week extension of time to respond to Set Two of the Council's interrogatories. By letter dated March 19, 2019, the Council granted an extension of time to April 4, 2019 to respond to the Set Two interrogatories. On April 4, 2019, CS submitted revised responses to Set One interrogatories and responses to the Set Two interrogatories.

Pursuant to CGS §22a-430b, DEEP retains final jurisdiction over stormwater management. The solar array layout and stormwater design are currently being revised/redesigned based on a reduced limit of work area. The design will be finalized to obtain DEEP approval of the GP. This reduced limit of work, including an increased natural buffer on the western side of the site, will also reduce tree clearing. Council staff notes that this D&M Plan review is based on the current design before the Council. Any changes to the D&M Plan, prompted by a revised stormwater design or by settlement through litigation, are required to be submitted by CS per RCSA §16-50j-62 for Council review and approval.

No comments on the D&M Plan were received. However, on February 28, 2019, the Town of New Milford submitted a petition (Petition No. 1362) for a declaratory ruling, pursuant to CGS §4-176, for a determination that the January 28, 2019 D&M Plan submitted by CS in Petition No. 1312 conflicts and/or is inconsistent with the Council's December 21, 2017 final decision on Petition No. 1312. In support of its petition, the Town of New Milford submitted an affidavit from Milone & MacBroom, Inc. (MM), a consulting firm that was not a witness for the Town in the proceedings held on Petition No. 1312, detailing concerns about the D&M Plan. CS's responses to MM's affidavit are attached hereto.

The solar array portion of the project will be on an approximately 163 acre parcel (Array Parcel) of property located on the southern flank of Candlewood Mountain. The electrical connection route will cross the eastern portion of the array parcel and then two additional parcels to reach Rocky River Substation off of Route 7. The array parcel is zoned

¹ The Town of New Milford is also a party.



Major Planned Residential Development District. The approved solar project includes solar arrays totaling about 20 MW AC with a total disturbance area of about 83.4 acres.

The Declaratory Ruling requires the following information to be included in the D&M Plan:

a. A final site plan including, but not limited to, the solar array, fence design, and the electrical interconnection line and corridor;

The final site plan provided illustrates the solar array, fence design, and the electrical interconnection line and corridor. This plan is consistent with the footprint approved by the Council on December 21, 2017. Approximately 60,000 solar panels at 400 Watts DC each (for a total of about 24 MW DC) will be installed.

CS will install a seven-foot chain link fence. Consistent with the Council's approval, no wildlife gap is proposed. Notwithstanding, there will be an approximately two-inch gap at the bottom to provide clearance above grade per Drawing No. C-304.

A roughly 4-mile long existing dirt access road off of Candlewood Mountain Road will be improved with gravel for use during construction and operation of the solar facility. The access road will be approximately 16 feet wide outside of the fenced array area. Inside the fenced array area, the access road width will increase to about 24 feet wide. Internal access road widths will be approximately 20 feet wide, with grass strips to accommodate movement of the slimy salamander (See Section m).

Approximately 9.34 acres of the tree clearing will be required to accommodate the approximately 1.3-mile long by 60 feet wide electrical interconnection corridor. The interconnection line will consist of two, overhead approximately 10 megavolt-ampere (MVA) circuits to be installed on approximately 18 single wood poles and 19 double wood poles. The heights of the wood poles will vary with the terrain, but the expected heights will range from between approximately 38-feet 8-inches to about 61 feet 2-inches above grade, with the majority less than 50 feet above grade. The plans for the interconnection line as depicted in CS's D&M Plan terminate immediately south of Kent Road (Route 7) at this time. CS will coordinate with Eversource on the crossing of Kent Road to reach Eversource's Rocky River Substation (RRSS), which is located directly on the opposite side or north side of Route 7. Eversource would file a petition with the Council for its final interconnection into the RRSS because Eversource will own the final interconnection into RRSS.

b. Consideration of locating a portion of the solar panels within the approximately 5-acre open field area and associated visual screening of such panels as necessary;

CS considered the feasibility of locating a portion of the solar panels within the approximately 5-acre open field area and associated visual screening of the panels as necessary. While CS technically could relocate some of the solar panels to this area, it notes several drawback associated with this alternative:

- a) In the Phase 1B Report submitted to the State Historic Preservation Office (SHPO), it was noted that this area will be used during construction for parking and storage. As such, construction matting was suggested to lessen the potential impact to undisturbed resources. A change in the use of this area from a temporary parking and "laydown" area to a location of permanent solar panel installation would require further consultation with SHPO to determine potential impacts to resources and potential avoidance and minimization measures;
- b) While mature trees could be planted to visually screen the panels from nearby residences and Candlelight Farms Inn, a complete screening may not be possible because tree plantings would need to be planted so as to prevent shading on the solar panels; and
- c) A new electric interconnection line would be required to connect the solar panels within this 5-acre area to the main solar facility on Candlewood Mountain.

Accordingly, CS contends that this alternative is neither prudent nor preferable to the approved layout and location.

c. Construction hours and days of the week;

Work hours will typically be 7:00 a.m. to 5:00 p.m., Monday through Friday, while complying with the Town of New Milford's regulations, to minimize the length of the calendar time the temporary construction impacts affect the area.

However, should the schedule require it, additional work may be performed on Saturdays. For example, because portions of the project involve work on an existing power system (interconnection) to serve customers, there may also be times when work needs to occur outside of these hours to avoid impacts to energy delivery and customer service. In addition, there are certain operations that, due to their nature or scope, must be accomplished in part outside the specified working hours. CS will coordinate with the municipality when work outside of these hours is necessary.

d. Construction traffic measures;

The primary (and only) access to the site will be from Candlewood Mountain Road. In accordance with the Town of New Milford Code and Ordinances, §18-78 Protection of Public During Construction, "During construction, the permittee shall not create a hazard to the traveling public and shall furnish such protective devices or police protection as the Director of Public Works may require at the permittee's expense." Accordingly, CS will work with the Town of New Milford to arrange traffic control if required during periods of frequent material deliveries during construction.

e. Erosion and sedimentation control plan consistent with the 2002 Connecticut Guidelines for Erosion and Sedimentation Control including, but not limited to, seeding the site for stabilization purposes prior to installation of racking systems and panels;

CS has provided its erosion and sedimentation control (E&S Control) plan as part of the Stormwater Pollution Control Plan (SWPCP). CS contends that the E&S Control measures are consistent with the 2002 Connecticut Guidelines for Erosion and Sedimentation Control. The E&S Control measures include, but are not limited to, seeding the site for stabilization purposes prior to installation of racking systems and panels.

f. Site clearing, grubbing, stabilization, and stormwater controls phasing plan;

CS has provided its Project Phasing and Control Plan, which includes clearing, grubbing, stabilization and stormwater controls phasing plans, as part of its SWPCP. The five phases are listed as follows:

- a) Phase I Install Perimeter Erosion Control Measures and Clear Trees;
- b) Phase II Access Road Construction;
- c) Phase III* Solar Array Installation;
 - i. Phase III.1 Grub Stumps, Install Sediment Traps, Perform Minimal Grading and Stabilize.
 - ii. Phase III.2 Once Vegetation is Stable, Install Solar Array Equipment.
 - iii. Phase III.3 Install Electrical Equipment.
 - iv. Phase III.4 Convert Sediment Trap to Sand Filter, Clean and Restore Areas as Required..
- d) Phase IV Interconnection Route; and
- e) Phase V Perimeter Fence Installation.

*Phase III will be broken up into several, smaller sub-phases. Stump removal and limited grading will be performed such that the total area of disturbed, exposed ground surface contributing stormwater runoff to a common point is restricted to five acres or less.

g. A stormwater management plan consistent with the 2004 Connecticut Stormwater Quality Manual, including an analysis on the potential impact of driveways on stormwater flows, including but not limited to, potential diversion of stormwater away from wetlands;

CS submitted a copy of the Stormwater Management Plan (SWMP). The SWMP includes an analysis on the potential impact of driveways on stormwater flows, including but not limited to, potential diversion of stormwater away from wetlands. The SWMP was developed consistent with the 2004 Connecticut Stormwater Quality Manual.

h. Plans to comply with the recommendations from DEEP outlined in "Stormwater Management at Solar Farm Construction Projects" dated September 8, 2017;

CS has developed plans to comply with the recommendations of the September 8, 2017 DEEP document on stormwater management at solar farms and to comply with more stringent Minnesota stormwater management guidelines for solar photovoltaic construction.

i. FAA marking/lighting plan, as necessary;

The Federal Aviation Administration (FAA) aeronautical study determined that the northern portion of the fence must be marked with red obstruction lighting at the corners and at (spacing) intervals not exceeding 150 feet. CS will install approximately 14 ea. L-810 LED TRO series red obstruction lights per those spacing requirements along the top of the fence in response to the FAA evaluation. Such lighting design will comply with the FAA Advisory circular 70/7460-1 L Change 1 as specified in FAA's No Hazard Determination letters.

Power for the FAA lighting will be delivered from the closest transformer pad and will be available 24/7 via the utility connection to the transformer. All wiring will be underground from the transformer pad to the lighting fixtures.

j. Vegetation Management Plan including, but not limited to, provisions for frequency of mowing and vegetation maintenance that incorporate any DEEP-required seasonal restrictions, post-construction site inspections on a quarterly basis, and removal of any accumulated sediment and debris that could affect stormwater patterns;

In order to maintain vegetation, the grass will be mowed twice per year during the growing season. Vegetation that becomes established outside the fence line but within the proposed limit of clearing will be removed or trimmed as needed. Herbicides or pesticides will not be used as part of the vegetation management plan.

Post-construction stormwater best management practices (BMPs) will be inspected in accordance with DEEP guidelines. Inspections will be documented and any vegetation maintenance required for removal of sediment or restoration to re-establish vegetation will be performed as-needed in order to properly maintain stormwater BMP function.

k. Decommissioning plan;

CS provided a decommissioning plan. The decommissioning process will, include, but not be limited to, the installation of temporary erosion and sedimentation controls, disconnecting power, removal of wiring and cables, removal of solar panels, removal of racks, removal of rack foundations, removal of electrical equipment,

removal of concrete pads, removal of power poles, removal of the fence, removal of access roads, and final restoration including grading and seeding disturbed areas.

All dismantled/removed equipment and materials will be categorized into those that could be reused, salvaged, recycled or disposed of. Generally, steel, aluminum, glass, copper, and plastics can be recycled. The crystalline silicon panels are considered landfill safe because they do not contain hazardous materials such as lead or cadmium. The panels contain recyclable materials such as aluminum, copper and glass. The panels will be dismantled and packaged per manufacturer or approved recycler specifications.

1. Plans to comply with the SHPO's recommended precautionary measures as specified in the letter dated November 28, 2017; and

By letter dated November 28, 2017, SHPO notes that cultural resource Locus No. 7 (a prehistoric lithic workshop) is potentially eligible for listing on the National Register of Historic Places. Accordingly, CS developed an avoidance and construction management plan to protect Locus No. 7 and Area 4, located in the southwestern portion of the project area and to be used for parking and material and equipment storage, and submitted such plan to SHPO. This plan includes the following measures:

- a) A buffer of approximately 69 feet that will separate the limits of work (LOW) and the limits of tree clearing from the area of archaeological sensitivity;
- b) Provide a distance of about 129 feet from the fence line (surrounding the facility) to Locus No. 7;
- c) Allow tree stumps to remain in the tree clearing area between the LOW and fence line;
- d) Install an exclusion barrier consisting of standard silt fence along the LOW;
- e) A 100-acre conservation restriction (which includes Locus No. 7); and
- f) Avoid grading, additional tree clearing and stone wall alterations in Area 4 to lessen potential impacts to undisturbed resources.

Additionally, SHPO suggests that construction matting be used in Area 4 to lessen the potential impacts to undisturbed resources. SHPO notes that, with these precautionary measures, the solar facility will not have an adverse effect on cultural resources. Accordingly, CS will implement all of the above protective measures.

m. Final wildlife protection measures and/or seasonal restriction timelines for all DEEP-identified Natural Diversity Database species except for golden-winged warbler.

By letter dated November 15, 2018, DEEP provided an updated Natural Diversity Database determination letter. While not required as part of the D&M Plan, DEEP concurred that, due to lack of habitat, no protection measures are required for the golden-winged warbler. DEEP also provided a Tree Roosting Bat Protection plan, which will limit tree clearing to between November 1 and March 30 to be protective of three state-listed tree roosting bat species. DEEP concurred with CS's vernal pool protection strategies (Vernal Pool Protection Plan) and noted that it will benefit the Jefferson salamander complex, a state-listed Species of Special Concern. DEEP also provided a recommended protection plan (Turtle Protection Plan) for wood turtles and eastern box turtles, both state-listed Species of Special Concern. Accordingly, CS will comply with the Tree Roosting Bat Protection Plan, Vernal Pool Protection Plan and the Turtle Protection Plan.

With respect to the slimy salamander, a state-listed Threatened Species, DEEP believes that the project would result in the incidental take of this species. However, the following actions are planned to avoid, minimize and mitigate the impacts to the "take" of the slimy salamander. Such measures include limiting tree clearing impacts and the overall footprint of the project; providing a 100-acre conservation easement; three-years of monitoring and reporting; and the addition of grassy strips to the access roads.

Specifically, the approved site plan limits the impact to about 1.3 acres of about 49 acres of high-quality forested salamander habitat. The 100-acre conservation easement was also included in the approved project layout. Grassy strips will replace the gravel for the full width of the roadway in areas proximate to forested habitat where the salamanders would presumably be emanating from. Lastly, CS will work with a qualified herpetologist to conduct the required survey, monitoring and reporting to DEEP.

Recommendations

If approved, staff recommends following conditions:

- 1. Pursuant to RCSA §16-50j-62, submit the applicable revisions including, but not limited to, the solar array layout, clearing limits, fence design and stormwater management plan for Council review and approval prior to the commencement of construction; and
- 2. Submit a copy of the DEEP General Permit and DEEP-approved stormwater management plan prior to commencement of construction.

ATTACHMENT A: Response to Milone & MacBroom Inc. affidavit dated February 26, 2019

- 5. The plans submitted to the CSC as part of the D&M Plan are represented as being "For construction." The plans are not suitable for construction, in our opinion, because they lack detail specific to the conditions on this subject site, are not adequate to allow a responsible contractor to implement the improvements in the field, and allow CSC to verify that the improvements have been constructed in accordance with the approved plans. Note the following:
- Based on our experience with the design of similar facilities, it is customary engineering practice to provide site layout plans with appropriate dimensions showing the precise limits of clearing and the location of all improvements, grading plans having 2-foot contour intervals showing existing and proposed finished grades including what will be beneath the solar arrays, and detailed drainage plans showing the precise slope sizes and inverts of pipes and other structures. This information is in addition to the required Erosion and Sedimentation Control Plans. Without having refined plans, the impacts of the proposed development cannot be adequately assessed.

Response: The Issued for Construction plans dated December 19, 2018 are in the process of being revised in order to provide additional information to construct the project.

- The existing and proposed topography is presented in 2-ft intervals as shown on the Grading and Drainage Plans (Sheets 9-12). The proposed grading is only shown where it differs from the existing conditions, otherwise the existing topography will remain. Proposed grading is shown as solid lines that tie into existing dashed grade lines (for example, the 830 elevation contour is being slightly regraded as shown on the northwest portion of the array on Sheet 11). The Grading and Drainage Plans do not show the solar PV components in order to provide clarity on the grading and drainage design. Note that the stormwater design is in the process of being revised based on a reduced limit of work as a result of the solar PV array redesign. This reduced limit of work, including an increased natural buffer on the western side of the site, will reduce the tree clearing. Additional clarification on this response will be provided once the re-design is complete.
- Callouts for the proposed tree clearing limits are depicted on the site layout plans (Sheets 4-8). Dimensions have been added depicting the distance between tree clearing limits and proposed panels.
- Erosion and sedimentation controls including construction phasing, site plans, notes, and specific details for each control measure are provided in the Erosion and Sedimentation Control Plans (Sheets 13-22). The detailed phasing plan is described on Sheet 13. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete, which will include additional detail on the phasing plan as well as specific proposed dates that correspond to the construction schedule (see further comment response related to the construction schedule below (comment 7.5)).
- The design of stormwater and erosion control features was prepared based on the Connecticut Department of Energy & Environmental Protection (CTDEEP) regulations including the 2002 Connecticut Guidelines for Erosion and Sedimentation Control, the 2004 Connecticut Stormwater Quality Manual, and the 2017 Stormwater Management at Solar Farm Construction Projects. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete.

The project calls for the clearing and grubbing of the site in order to install the solar arrays, access drives, and other related facilities. However, except for some drainage swales and other drainage improvements located on the perimeter of the disturbed site (83.4 acres), there are no grading plans that show how the topography will be regraded once the existing vegetation and stumps have been removed and prior to restoration and the implementation of site improvements.

Response: The site topography will remain largely unchanged with minimal site grading proposed to construct the access roads, stormwater features, and minor land grading as shown on the Grading and Drainage Plans (Sheets 9-12) of the Issued for Construction plan set dated December 19, 2018. Once the trees are cleared and stumps are removed within the proposed fence line, the land will be graded to match existing conditions, unless otherwise shown on the Grading and Drainage Plans (see response above). Stumps will remain in place in the area between the fence line and the limit of work. Note that the proposed access road within the array is flush with the surrounding grade as explained in the testimony to the Siting Council. For this reason, proposed grades are not shown in the majority of the proposed access roads within the array, however, proposed grading for the access road from Candlewood Mountain Road to the limits of the array are shown Sheet 10. Details for the flush access drive and the raised access road are provided as details B3 and C1, respectively on Sheet 24. Also note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete.

5.3 The site construction details included in the plans are generic, accompanied by standard tables. The critical details related to drainage structures have not been customized to be applied to this site and rely on field interpretation during construction.

Response: The site construction details presented in the Issued for Construction set are specific to the site development, including the surface sand filter (Detail C3 on Sheet 23) and sediment trap (Detail C1 on Sheet 22) design tables which specify the design elevations for each structure. These tables are included below for your convenience. The surface sand filter water quality volume calculations are also included in Appendix B-3.1 and are summarized in Table B3-2. These details reference the 2002 Connecticut Guidelines for Soil Erosion & Sediment Control, the 2004 Connecticut Stormwater Quality Manual and also the Minnesota Stormwater Manual's Stormwater Management for Solar Projects. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response, including physical dimensions of each BMP for construction, will be provided once the re-design is complete.

						CTDE	EP SEDIMEI	NT TRAP TAE	LE					
Sediment Trap No.	Drainage Area	Acreage	Initial Storage Capacity	Trap Bottom Elevation	Outlet Base Elevation (Wet Pool)	Max. Trap Depth Below Outlet, ft (D _w)	Outlet Top Elevation (Overflow)	Rise of Stone Outlet, ft (D _d)	Wet Pool Surface Area, sf (A _w)	High Pool Surface Area, sf (A _d)	Wet Storage Volume Provided*, cf (V _w)	Wet Storage Volume Required, cf (V _w)	Dry Storage Volume Provided*, cf	Dry Storage Volume Required, cf (V _d)
1A	1AS	3.71	13,405	805.00	808.00	3.00	810.00	2.00	3,936	5.117	10,037	6,702	9.053	6,702
1B	185	2.34	8,455	805.00	808.00	3.00	809.54	1.54	5,702	7,413	14.540	4,228	· · · · · · · · · · · · · · · · · · ·	
2A**	2AS	2.46	8,915	791.00	794.00	3.00	795.50	1.50	1,046	3,151	4,457	4,457	10,098 4,457	4,228 4,457
			<u> </u>	•	Perform a	Idditional grad	ing to a mini	mum area of:	1,748	4,195	,,,,,,,	1 3,137	1 -2,407	4,437
2B**	28\$	4.54	16,437	772.00	775.00 Perform a	3.00 additional grad	776.76	1.76	2,353 3.223	5,599 6.116	8,218	8,218	8,218	8,218
2011	200	3.58	12,967	766.00	769.00	3.00	770.81	1.81	1,408	3.027	6,483	6,483	6,483	C 402
2C**	2CS					dditional grad			2.543	4.622	0,483	(0,463	0,463	6,483
3A**	3AS	4.31	15,575	722.00	725.00	3.00	727.00	2.00	2,841	6,027	7,788	7,788	8,868	7,788
3A	3A3	<u> </u>			Perform a	Idditional grad	ing to a mini		3.054	.,	,,,,,,,	,,,,,,	0,000	7,700
3B**	3BS	3.88	14,049	729.50	732.50	3.00	734.25	1.75	2,566	5,694	7,024.	7,024	7,228	7,024
		·			Perform a	dditional grad	ing to a mini	num area of:	2,755				,	.,024
4A**	4AS	4.00	14,472	719.00	722.00	3.00	723.71	1.71	1,647	5,420	7,236	7,236	7,060	7,236
			<u> </u>	, ,	Perform a	dditional grad	ng to a mini	num area of:	2,838					
4B**	48s	4.02	14,548	727.00	730.00	3.00	730.99	0.99	1,410	4,332	7,274	7,274	7,274	7,274
						dditional grad			2,853	11,842				.'
5A**	5AS	2.76	9,971	792.00	795.00	3.00	796.06	1.06	1,540	4,126	4,986	4,986	3,003	4,986
5B	58S	2.03	7.377	797.00		dditional grad			1,955	1.	1 1			
	363	1.30	7,337 4,685	802.00	800.00 805.00	3.00	802.00	2.00	1,977	4,640	5,041	3,669	6,617	3,669
6A**	6AS	1.50	4,000	802.00			806.62	1.62	636	6,907	2,343	2,343	6,110	2,343
		2.03	7,341	799.00	802.00	dditional grad	803.56	num area or: 1.56	919	7700				
6B**	6BS	2.03	1,	755.00		dditional grad			583	7,728	3,670	3,670	6,483	3,670
		2.85	10.304	764.84	767.84	. 3.00	769.67	1.83	1,439 1,384	3.453		5 453		<u> </u>
6C**	6CS		10,504	1 70-0- 1		dditional gradi			2,334	3,453 3, 610	5,152	5,152	5,152	5,152
7A**		2.98	10.771	786.93	789.93	3.00	791.76	1.83	961	3.276	5,385	5,385	5,385	C 20C
/A**	7AS				Perform a	dditional gradi	إرز ومعجم به	7		3,774	3,363	دەدرد ا	l e pi a l	5,385
			6.000			NO CIDEEP SEE						-		
7C	7CS	1.44	5,210	718.04	721.04	3.00	722.87	1.83	1,700	6,822	6,822	2,605	7,798	2,605
8A**	8AS	4.38	15,843	760.00	763.00	3.00	764.56	1.56	1,073	3,008	7,922	7.922	7,738	7,922
OPA .	343		3 P. S. S.	机铁 粉	Performa	dditional gradi	ng to a mini	num area of:	3,197	7,849		.,,,,,,	,,322	1,322
8B**	88S	4.86	17,580	744.00	747.00	3.00	748.64	1.64	1,125	3,174	8,790	8,790	8,790	8,790
				<u> </u>	Perform a	dditional gradi	ng to a mini	num area of:	3,447	7,272			7	-,,,,,
9A**	9AS	3.46	12,522	754.00	757.00	3.00	758.14	1.14	1,693	5,755	6,261	6,261	6,261	6,261
				<u>,</u>		dditional gradi	ng to a mini	num area of:	2,455	8,529	3 1 2			
9B**	985	4.93	17,837	752.00	755.00	3.00	757.19	2.19	1,673	3,974	8,918	8,918	8,918	8,918
	1					dditional gradi			3,497	4,647				
10	105	3.53	12,753	751.50	754.50	3.00	757.19	2.69	2,724	8,698	6,946	6,377	15,363	6,377
12	12S	0.42	1,523	696.25	700.25	3.00	701.70	1.45 -	945	1,425	2,410	762	1,718	762

Notes

^{*} Storage volumes provided are shown on the drawings for most sediment traps as the grading contours for the permanent sand filters. Following construction, temporary sediment traps will be converted to permanent water quality sand filters.

^{**} Sediment traps require additional grading beyond what is shown on the drawings to meet the required storage volume(s).

^{1.} Wet storage volume: V_w = 0.85 * A_w * D_w

^{2.} Dry Storage volume: $V_a = (A_w + A_o)/2 * D_o$

				CTDEEP SURFACE S	AND FILTER TABLE				
SURFACE SAND FILTER	TOP OF FILTER ELEVATION (FT)	FILTER INVERT ELEVATION (FT)	UNDERDRAIN INVERT ELEVATION (FT)	TOP OF BERM ELEVATION (FT)	WATER QUALITY HGL ELEVATION (FT)	10 YEAR HGL ELEVATION (FT)	25 YEAR HGL ELEVATION (FT)	100 YEAR HGL ELEVATION (FT)	100 YEAR FREEBOARD HEIGHT (FT)
1A	810.00	808.17	807.17	812.50	807.43	810.66	810.86	811.18	1.32
18	809.54	807.71	806.71	811.37	806.75	809.85	810.05	810.36	1.01
· 2A	795.50	793.67	792.67	798.45	795.04	797.22	797.29	797.36	1.09
2B	776,76	774.93	773.93	780.58	774.83	779.16	779.35	779.57	1.01
2C	770.81	768.98	767.98	774.90	768.35	773.44	773.62	773.82	1.08
3A	727.00	725,17	724.17	730.49	724.31	728.91	729.11	729.39	1.10
3B	734.25	732,42	731.42	738.62	731.56	737.06	737.30	737.62	1.00
4A	723.71	721.88	720.88	728.20	721.23	726.70	726.99	727.20	1.00
4B	730.99	729.16	728.16	734,90	728.43	733.47	733.65	733.90	1.00
5A	796.06	794.23	793.23	799.35	793.49	798.12	798.22	798.34	1.01
5B	802.00	800.17	799.17	805.25	799.38	803.90	804.02	804.16	1.09
6A	806.62	804.79	803.79	809.12	803.98	807.92	808.01	808.12	1.00
	803.56	801.73	800.73	806.06	801.11	804.07	804.16	804.31	1.75
6B 6C	769.67	767.84	766.84	772.67	767.27	771.27	771.38	771.54	1.13
7A	791.76	789.93	788.93	794.30	789.22	793.08	793.14	793.24	1.06
	751.70	705.55		DEP Surface Sand	Filter for Subcatch	ment 7B			
	722.87	721.04	720.04	726.25	720.89	724.64	725.03	725.24	1.01
7C	764.56	762.73	761.73	768.63	762.32	767.39	767.49	767.63	1.00
	748.64	746.81	745.81	752.30	746,22	751.03	751.12	751.26	1.04
8B	758.14	756.31	755.31	761.64	755,73	760.36	760.47	760.60	1.04
9A		755.36	754.36	759.44	754.79	758.23	758.30	758.43	1.01
9B	757.19	794.47	793,47	798.96	793.74	797.65	797.76	797.91	1.05
10	796.30	/94.47 NA	/33.47 NA	702.20	701.08	702.03	702.07	702.15	0.05
Wet Swale 12B	NA NA	I NA	I NA	1 /02.20					

In reviewing other solar installations and based on our experience, the ratio between the panels and the space between arrays should be approximately 50/50 to facilitate adequate maintenance and provide for sunlight for the vegetation to grow beneath the panels. The plans show that the solar arrays are separated by aisles having a width as narrow as 5 feet, which is too narrow to allow maintenance and promote a healthy vegetative community. Moreover, it will cause the vegetation in the aisles and beneath the panels to be shaded, thus affecting the long-term sustainability and quality of the vegetation.

Response: Shade tolerant seed mixes have been specified for restoration of the array portion of the site to account for the potential increase in shade due to the row spacing. The stabilization seed mix installed after clearing and grubbing but before the array installation will be the Quick Erosion Control Cover Mix (ERNMX-104). Once the array is installed, the site will be restored by overseeding with either the Solar Farm Seed Mix (ERNMX-186) or the Conservation Shade Mix (ERNMX-129) both of which require as little as 2 hours of indirect sunlight per day to promote a healthy vegetated cover. Seeding will be performed by hydroseeding.

As a conservative approach and per CTDEEP direction, the stormwater design was revised to incorporate the Minnesota Stormwater Manual's Stormwater Management for Solar Projects and Determining Compliance with NPDES Construction Stormwater Permit to provide additional stormwater quality volume treatment.

In addition, the stormwater design is being revised for the reduced size limit of work area and revised to achieve a consistent interrow spacing.

- 6. The stormwater analysis presented by the applicant is fundamentally flawed as noted below:
- The plans are based on outdated rainfall data. Both CTDEEP and the Connecticut Department of Transportation (CTDOT) require the use of rainfall precipitation data from National Oceanic and Atmospheric Administration (NOAA) Atlas 14, not TP-40 (See Appendix B in Chapter 6 of the 2000 DOT Drainage Manual, as undated on the DOT webpage, now referencing NOAA Atlas 14 Volume 10). The NOAA Atlas 14 rainfall data is 15% to 20% higher than the old data in TP-40 and would have a significant impact on the outcome of the modeling and the actual design.

Response: The approach of the stormwater design was to follow Table 7-2 of the CTDEEP 2004 Stormwater Quality Manual. Based on these comments and comments from DEEP, the stormwater analysis has been revised to include the updated rainfall data provided by the National Oceanic

and Atmospheric Administration Atlas 14 (NOAA Atlas 14) Precipitation Frequency Estimates. The revised stormwater calculations will be included with the revised design plans. The table below shows a comparison of the Table 7-2 rainfall data (for Litchfield County) vs. the NOAA Atlas 14 rainfall data for the site (Candlewood Mountain) for the 24-hour storm event.

24 Hour Design Rainfall Event	CTDEEP Table 7-2 Rainfall Amount for Litchfield County	NOAA Atlas 14 Rainfall Amount for Station ID 06-6966
2-year	3.2	3.42
10-year	4.7	5.42
25-year	5.5	6.68
100-year	7.0	8.61

The NOAA Atlas 14 rainfall data was used to recalculate the peak discharge from the site under pre and post construction conditions. A summary table with the peak flow rate result from each surface sand filter is provided below which demonstrates that 5 of the surface sand filters will require additional capacity to accommodate the increase in flow for the 100-year storm event and the surface sand filters for Point of Analysis 6 would require additional capacity for the 10-, 25-, and 100-year storm events. The NOAA Atlas 14 rainfall data will be used in the stormwater analysis to be completed for the reduced limit of work area.

	24-hour Storm	Existing Condition Peak	Proposed Condition Peak	Difference in Peak Flow
Watershed	Event	Outflow (cfs)	Outflow (cfs)	(cfs)
	10	14.73	0.00	-14.73
DA-1	25	20.88	0.05	-20.83
	100	30.69	3.22	-27.47
	10	32.83	28.50	-4.33
DA-2	25	45.78	43.81	-1.97
	100	66.21	64.02	-2.19
	10	11.06	6.68	-4.38
DA-3	25	15.92	15.10	-0.82
	100	23.79	26.36	2.57
	10	13.59	10.44	-3.15
DA-4	25	19.57	18.94	-0.63
	100	29.16	30.39	1.23
	10	7.43	4.79	-2.64
DA-5	25	10.68	10.42	-0.26
	100	15:95	17.25	1.30
	10	9.26	9.63	0.37
DA-6	25	13.23	14.57	1.34
	100	19.61	21.98	2.37
,	10	16.83	13.20	-3.63
DA-7	25	23.50	21.24	-2.26
	100	34.06	32.63	-1.43
	10	22.60	15.44	-7.16
DA-8	25	31.56	22.61	-8.95
	100	45.72	33.82	-11.90
	10	13.52	11.98	-1.54
DA-9	25	19.16	18.58	-0.58
	100 .	28.17	27.89	-0.28
	10	7.33	4.91	-2.42
DA-10	25	10.31	7.89	-2.42
	100	15.05	12.05	-3.00
	10	2.12	2.12	0.00
DA-11	25	2.91	2.91	0.00
	100	4.13	4.13	0.00
	10	1.80	1.72	-0.08
DA-12	25	2.36	2.22	-0.14
	100	3.23	3.31	0.08

24-hour average rainfall data referenced from NOAA Atlas 14, Volume 10, Version 2 ROCKY RIVER DAM for Station ID: 06-6966 New Milford, Connecticut.

10-year = 5.43 inches

25-year = 6.69 inches

100-year = 8.62 inches

The HydroCAD model output provided in the Stormwater Pollution Control Plan indicates the use of infiltration in the design of the proposed sand filters. However, it does not appear that In-situ soil testing has been performed to determine if surface sand filters are an acceptable stormwater practice for the site.

Response: Soil test pitting is proposed to be completed in the Spring of 2019 to evaluate the soil characterization at each BMP location. The test pits will be completed at each surface sand filter location to evaluate soil type, depth to groundwater and presence of ledge. Following the test pit activities, the stormwater analysis will be updated to include the information collected at each test

pit, following Table II-P3-I from the 2004 Connecticut Stormwater Quality Manual (below). If unfavorable soil types for infiltration, high groundwater or ledge are present at the proposed BMP locations, the BMPs will be relocated to a more favorable location.

Group	Soil Texture	Minimum Infiltration Rate (in/hr)
Α	sand, loamy sand, or sandy loam	0.3-0.45
В	silt loam or loam	0.15-0.3
C .	sandy clay loam	0.05-0.15
D	lab loam, silty loam, sandy clay, silty clay, or clay	0-0.05

6.3 The CTDEEP Stormwater Quality Manual provides guidelines for stormwater filtering practices that have not been followed in the proposed design. The manual states that filtering practices are designed as offline systems to treat the water quality volume and bypass larger flows. Also, the manual recommends the Water Quality Volume should be diverted into a pretreatment sediment forebay or settling chamber to reduce the amount of sediment that reaches the filter. (See Filtering Practices in Chapter 11 of the 2004 DEEP Water Quality Manual, page 11-P4-I) The proposed design directs all of the runoff to the surface sand filter with no pretreatment. The manual contains a list of the limitations of stormwater filters that pertain to the proposed design: 1) Pretreatment is required to prevent filter media from dogging; 2) Frequent maintenance is required; 3) Surface sand filters are not feasible in areas of high groundwater; 4) Surface sand filters should not be used in areas of heavy sediment loads; 5) Surface sand filters provide little or no stormwater quantity control; and 6) Surface and perimeter filters may be susceptible to freezing. The design of the proposed stormwater management needs to be designed with greater attention to site conditions.

Response: The majority of the drainage areas are proposed to have water quality swales collect and pretreat the stormwater prior to discharge at the surface sand filters. For surface discharge of stormwater to the surface sand filter, there is an upgradient vegetated buffer to provide pretreatment and sediment filtration. As discussed in the Stormwater Management Plan, the Operation and Maintenance (O&M) Plan will provide more detail on the frequency and method of cleaning each filter as discussed in 6.3.2 below. Once the site is considered stabilized, it will not be considered an area of high pollutant load, therefore, the sedimentation rate is anticipated to be very low as discussed further in 6.3.4 below.

- 1. The site is proposed to have water quality swales and vegetated buffers which collect and treat the stormwater flow to the surface sand filters. This is allowable per the 2004 Connecticut Stormwater Quality Manual page 3-5, however, the stormwater analysis will be revised to include pretreatment measures at each surface sand filter in accordance with the 2004 Connecticut Stormwater Quality Manual Chapter 11 Primary Treatment Practice 4 (Filtering Practice) which will include:
 - a. Primary pretreatment within a sediment chamber or stilling basin (to be included in the revised stormwater analysis);
 - b. Secondary pretreatment through water quality swales
 - c. Tertiary pretreatment through vegetated filter strips.

Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete.

2. The site will have a standing O&M Plan that will address the frequency and required maintenance for each design feature as discussed in Section 8 of the Stormwater Management Plan dated January 3, 2019 submitted as part of the Development and Management Plan dated January 14, 2019. This O&M Plan will address inspection, maintenance and access to each stormwater BMP along with the responsibilities of each person in charge. The O&M Plan will

be updated to include BMP specific maintenance measures. The specific inspection and maintenance requirements for the surface sand filter are provided below:

- a. Each surface sand filter will be inspected in accordance with the Connecticut General Permit for the Discharge of Stormwater and Dewatering Wastewaters from Construction Activities. The inspection will generally be conducted after every major storm (rainfall that generates a discharge from each surface sand filter and/or a storm event that generates 0.5 inches of rainfall or greater) during the first 6 months after construction. Based on the results of the inspections, the surface sand filters will be inspected every 6 months thereafter. The inspections will include:
 - i. Checking the filter surface for standing water or other evidence of clogging such as discolored or accumulated sediments;
 - ii. Checking the pretreatment stilling basin, water quality swales and vegetated filter strips contributing to the surface sand filter for sediment accumulation, trash, and debris;
 - Checking inlets, outlets, and overflow spillway for blockage, structural integrity and evidence of erosion.
- b. Sedimentation should be removed from the sedimentation chamber or pretreatment collection systems when it accumulates to a depth of more than 12 inches or 10 percent of the pretreatment volume. All outlet devices should be cleaned when drawdown times exceed 36 hours.
- c. Sediment should be removed from the filter bed when the accumulation exceeds 1 inch or when there is evidence that the infiltration capacity of the filter bed has been significantly reduced (i.e., observed water level above the filter exceeds the design level or drawdown time exceeds 36 to 48 hours).
- d. The top layer (approximately 6 to 12 inches) of the filter bed should be removed and replaced annually or more frequently if necessary. The material should be removed with rakes rather than heavy equipment to avoid compaction of the filter bed. Heavy equipment may be used if the system is designed in a configuration where the heavy equipment can access the filter material from outside the BMP.
- 3. Per the 2004 Connecticut Stormwater Manual page 11-P4-4, 'At least 3 feet of separation is recommended between the bottom of the filter and the seasonally high groundwater table ...". As discussed in Response 6.2, soil test pitting is proposed to be completed prior to construction to assess the seasonally high groundwater elevation, presence of ledge and soil type at each proposed surface sand filter location. The groundwater elevation relative to the bottom of the surface sand filter media will dictate if groundwater recharge, while not required at all locations, can be accounted for in the stormwater analysis. The groundwater recharge volume required is approximately 3,000 ft³ for the site which is based on the increase in impervious area proposed (see documentation in Appendix B-3). This recharge volume is accounted for in 17 of the stormwater BMPs, therefore not all BMPs have to infiltrate stormwater to meet the groundwater recharge requirements. In addition, the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete.
- 4. The surface sand filters are proposed to be installed after the solar array construction is complete and the vegetation is restored. The site is considered restored when 80% of the vegetated cover is established, therefore, all potential erosion and sedimentation sources will have been stabilized and the sedimentation rate from the site is expected to be minimal. Also, once stabilization is achieved, the roadway will be very infrequently traveled, and there is no fueling or storage of oils proposed at the site. The site will, therefore, not be considered an area of high pollutant load.

- 5. The surface sand filters were designed to meet the post-development water quality volume and water quantity rate for the site through the use of the constructed earthen berms of the surface sand filter proposed to retain and treat the stormwater runoff. The surface sand filters were designed to accommodate the 25 and 100 year storm events through controlling the discharge with the spillway design elevations. The berm and spillway design elevations work together to control the peak stormwater runoff to ensure the pre-construction stormwater rates of runoff are met once construction is complete. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete.
- 6. Per the 2004 Connecticut Stormwater Manual Figure 11-P4-1, the surface sand filters have been designed with an underdrain collection system to allow the sand filters to drain completely and not pond water for durations exceeding 24 hours. During periods of thaw the surface sand filters will, therefore, drain appropriately so that there is no standing water which may freeze during periods of low temperature conditions. The surface sand filters will be inspected and maintained in accordance with the O&M Plan for the project as discussed in Response 6.3 above to address any underdrain maintenance or repairs that may be required due to clogging and/or damage. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete.
- 6.4 It is appropriate to assume a meadow coverage condition for the proposed conditions HydroCAD model only if continuous vegetation is permanently established and maintained under the solar panels. However, it is expected that the new vegetation will struggle to grow under the panels due to the density size, and short height of the panels in relation to the ground. The only possible portion of the site where the arrays are proposed that could have a continuous meadow coverage would be the open space in between the panel rows that are illustrated to be as narrow as 5 feet. The hydrologic computations need to be revised to assume a poorer ground coverage under the proposed solar panels. This is likely to result in the need for stormwater detention that is not part of the plans as now presented.

Response: Shade tolerant seed mixes have been specified for restoration of the array portion of the site to account for the potential increase in shade due to the row spacing. The stabilization seed mix installed (by hydroseeding) after clearing and grubbing but before the array installation will be the Quick Erosion Control Cover Mix (ERNMX-104). Once the array is installed, the site will be restored by overseeding with either the Solar Farm Seed Mix (ERNMX-186) or the Conservation Shade Mix (ERNMX-129) both of which require as little as 2 hours of indirect sunlight per day to promote a healthy vegetated cover.

Soil test pits are proposed to be conducted in the Spring of 2019. The stormwater analysis will be revised based on the soil conditions including the presence of groundwater and/or ledge. Stormwater detention will be evaluated as part of the redesign.

The post development peak discharge rates for Points of Analysis 5 and 6 show an increase from the predevelopment conditions. A technical explanation as to why these increases will not cause negative impacts downstream has not been provided.

Response: The overall stormwater discharge from the site decreases (Table B4-1), however, one of the goals for post-construction stormwater design is to ensure the rate of runoff to each off-site property is equal to or less than the pre-construction flow rate. This analysis shows that the hydrology of the site is not drastically different from pre-construction conditions and one area of the site is not contributing a larger stormwater runoff rate when compared to others. Points of Analysis 5 and 6 met the pre-construction rate of runoff for all storm events except for the 100-year storm. The stormwater design will be revised based on the reduced limit of work area. This analysis will

demonstrate the rate of runoff for all Points of Analysis at the site are less than, or equal to, the pre-construction conditions.

At present, much of the runoff from the western portion of the site that drains to abutting properties to the west does so in an even, shallow, concentrated flow. The introduction of the spillway outlets will result in runoff being consolidated and concentrated in a few distinct locations. This will fundamentally change the nature of the discharge from the subject parcels and could result in long-term risk of erosion and damage to downgradient parcels. This condition also exists on the eastern side of the parcel where runoff is concentrated and not spread out in a manner more consistent with existing conditions.

Response: The basis of the stormwater design related to attenuation was to design so the post-construction rates of runoff are equal to, or less than existing conditions at each point of analysis (see Table in response to comment 6.1). The spillway from the surface sand filter is proposed to discharge over an energy dissipator (Detail A1, Sheet 23) which also includes a table (included below) specifying the design for each location. This design references Chapter 10 of the 2002 Connecticut Guidelines for Soil Erosion and Sedimentation Control and redistributes the stormwater discharge from the surface sand filter over a larger area to mimic existing conditions. The energy dissipators vary in length from 10 to 20 feet based on the contributing flow rate. Also, the stormwater design, including the energy dissipators, will be revised based on the reduced limit of work area and further clarification will be provided related to this comment.

	ENERGY DIS	SIPATOR TABLE		
SURFACE SAND FILTER	LENGTH (FT)	WIDTH (FT)	DEPTH (FT)	
1A	20.00	6.00	0.60	
18	10.00	6.00	0.50	
2A	20.00	6.00	0.60	
2B	10.00	6.00	0.50	
2C	20.00	6.00	0.60	
3A	10.00	6.00	0.50	
3B	10.00	6.00	0.50	
4A	10.00	6.00	0.50	
4B	10.00	6.00	0.50	
5A	10.00	6.00	0.50	
5B	10.00	6.00	0.50	
бA	10.00	6.00	0.50	
6B .	10.00	6.00	0.50	
6C	10.00	6.00	0.50	
7A	10.00	6.00	0.50	
7B	10.00	6.00	0.50	
	io Surface Sand Fil	ter for Subcatchm	ent 7B	
7C	10.00	6.00	0.50	
8A	10.00	6.00	0.50	
88	10.00	6.00	0.50	
8C	10.00	6.00	0.50	
9A	10.00	6.00	0.50	
98	10.00	6.00	0.50	
10	10.00	6.00	0.50	
11	10.00	6.00	0.50	

Dimensions per CTDEEP Guidelines for Soil Erosion and Sediment Control Manual Chapter 5-10 - Energy Dissipators - Figure LS-1 - Minimum Dimensions for Level Spreaders Design computations for the drainage swales and culverts have not been provided to demonstrate that they are adequately sized to convey the contributing stormwater runoff.

Response: Due to the size of the HydroCAD file, only the summary tables were included in the Stormwater Pollution Control Plan per DEEP's request. The full HydroCAD model output is attached that reflects the December 19, 2018 submittal. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete.

There are no supporting calculations demonstrating the velocity of runoff that is expected at the outlets of the basins.

Response: The full HydroCAD model output is attached which includes supporting documentation for the velocity of stormwater runoff expected at the site. Discharge flows from the sand filters were compared to the length of proposed energy dissipators to estimate a discharge velocity for each Point of Analysis for the 25- and 100-year storm events (see table below). Velocities were compared to allowable discharge velocities by soil texture type outlined in Section 5 Table OP-1 of the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control. The erosion control matting on the downslope side of each basin was specified based on the expected discharge velocity. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. The current design shows exceedance of allowable discharge velocities at sand filters 2B, 8B and 9B. Additional clarification on this response will be provided, including revised energy dissipator sizing, once the re-design is complete.

		xisting C	onditions				Proj	osed Can	ditions			
Drainage Area	Storm Event	Flow (cfs)	Area ¹ (sq ft)	Velocity (fps)	Sand Filter ID	Storm Event	BMP Outflow (cfs)	Area ² (sq ft)	Actual Discharge Velocity	Soil Type at Discharge	Allowable Discharge Velocity ⁴	
									(fps)	Point ³	(fps)	
	25-year	15.06	235	0.06	1A	25-year	0	6.7	0.0	HSG C Fine	3.5	
DA-1	100-year	22.43	255	0.10		100-year	0	6.7	0.0	Sandy		
DA-1					1B	25-year	0	3.3	0.0	HSG C Fine	3.5	
						100-year	0.45	3.3	0.1	Sandy HSG D Rock		
	25-year	33.54	167.5	. 0.20	2Á	25-year	8.95	6.7 6.7	1.9	Outcrap	6.0	
	100-year	49.02		0.29		100-year	1269 123	3.3	3.7	HSG C Fine		
DA-2	[2B	25-year 100-year	19.8	3.3	5.9	Sandy	3.5	
					ļ	25-уеаг	8.77	6.7	1,3	HSG C Fine		
					2C	100-year	14.75	6.7	- 2.2	Sandy	3.5	
		11.22		0.07	ļ	25-year	9.41	3.3	2.8	HSG C Fine		
	25-year	11.32	155	0.11	3A	100-year	9.41	3.3	2.8	Sandy	3.5	
DA-3	100-year	17.17		0.11		25-year	2.98	3.3	0.9	HSG C Fine		
					3B	100-year	7.79	3.3	2.3	Sandy	3.5	
	25 vp2r	13.92		0.06	 	25-year	5.13	3.3	1.5	HSG C Fine	3.5	
	25-year 100-year	21.08	215	0.10	4A	100-year	10.07	3.3	3.0	Sandy	3,3	
DA-4	100-year	2100		0.10		25-year	6.96	3.3	2.1	HSG C Fine	3.5	
					48	100-year	11.4	3.3	3.4	Sandy	3.3	
	25-year	7.61		0.03		25-year	4.34	3.3	1.3	HSG C Fine	3.5	
	100-year	11.51	250	0.05	5A	100-year	7.3	3.3	2.2	Sandy		
DA-5	200 / 200				5B	25-year	2.01	3.3	0.6	HSG C Fine	3.5	
					38	100-year	4.81	3.3	1.4	Sandy		
	25-year	9.47	140	0.07	6A	25-year	2.45	3.3	0.7	HSG C Fine	3.5	
	100-year	14.24	140	0.10	UA	100-year	3.92	3.3	1.2	Sandy		
DA-6					6B	25-year	3.69	3.3	1.1	HSG C Fine	3.5	
DA-6						100-year	5.98	3.3	L8	Sandy		
					6C	25-year	5.12	3.3	1.5	HSG C Fine	3.5	
						100-year	7.72	3.3	2.3 1.5	Sandy HSG C Fine		
	25-year	17.19	52.5	0.33	7A	25-year	5.1 7.68	3.3 3.3	2.3	Sandy	3.5	
DA-7	100-year	25.18		0.48		100-year	0.15	3.3	0.0	HSG D Roc	k	
					7C	25-year 100-year	2.85	3.3	0.9	Outcrop	6.0	
		22.00		0.20	 	25-year	7.42	3.3	2.2	HSG C Fine		
1	25-year	23.09 33.81	115	0.20	8A	100-year	11.38	. 3.3	3.4	Sandy	3.5	
DA-8	100-year	33.01		0.23		25-year	8.58	3.3	2.6	HSG C Fine		
					8B	100-year	13.14	3.3	3.9	Sandy	3,5	
L	25-year	13.82		0.11	 	25-year	4.69	3.3	L4	HSG C Fine	3.5	
	100-year	20.58	1.25	0.16	9A	100-year	8.23	3.3	2.5	Sandy	3.9	
DA-9	Too-year	20.00		0.20		25-year	7.9	3.3	2.4	HSG C Fine	3.5	
					9B	100-year	11.86	3.3	3.5	Sandy	ال.بال	
 	25-year	7.49		0.05	10	25-year	5.08	3.3	1.5	HSG C Fin	3.5	
DA-10	100-year	2.50	160	0.02	10	100-year	8.57	3.3	2.6	Sandy	٠	

Notes:

- 1. Area of discharge for existing conditions was assumed to be a half foot of the total downstream length of the drainage area.
- 2. Area of discharge for proposed conditions is the cross-sectional area of level spreader as shown in Detail S-1 on C-303 (sheet 23 of 26) Issued For Construction dated December 19, 2018.
- 3. Soil types based on NRCS Soil Maps.
- 4. Allowable velocities taken from Figure OP-1 Allowable Velocities for Various Soils Section 5-10 of the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control. Red velocities denote exceedance of allowable velocities for the existing soil type.
- 6.9 The use of sheet flow in the time of concentration calculations where solar panels are proposed is not a reasonable expectation given the concentrated nature of the runoff from the panels themselves. The runoff generated from the drip line of the panels will travel downgradient in a manner more consistent with shallow concentrated flow.

Response: In our experience, sheet flow has been the industry standard for modeling this runoff, however, the stormwater analysis will be revised to model shallow concentrated flow from the panels. A gravel strip will be incorporated into the solar design within areas where the existing topography is greater than or equal to 10% as demonstrated in Figure 1 attached. A more detailed O&M Plan will be developed that addresses potential erosion from the drip line which, in our experience, has not been an issue for sites with established vegetation. The O&M Plan will include a detailed discussion of inspections, turf mowing frequency, and additional required maintenance and contingencies so that erosion is easily identified and corrected in a timely manner.

6.10 The grading of the driveway from Candlewood Mountain includes riprap swales along both sides of the road, with runoff directed to sand filter 7C. The uphill swale appears to simply discharge across the driveway to the sand filter. The uphill swale in particular is likely to convey significant flows that will cause erosion across the driveway in an unprotected manner. Also, there does not appear to be any supporting calculations on the design of the roadside or other swales on site.

Response: The uphill swale along the access road is not designed to discharge across the roadway. Since this swale will collect stormwater from undeveloped portions of land from above, it is simply a collection swale which discharges to a culvert farther down the proposed access road. The flat section of the swale shown opposite the sand filter 7C is a result of the grading of the access road to accommodate the sand filter (see the Grading and Drainage Plan - 2, Sheet 10). A minimum slope of 0.8% is, however, maintained within the swale to promote positive drainage. The plans will be revised to clarify this approach. See Response 6.7 above for calculations.

6.11 The roadway swales ultimately discharge into two 18-inch culverts beneath the driveway that will channelize the flow and result in point discharges that currently do not occur on site. Also, the 18-inch culvert along the road is shown within the town right-of-way, requiring approval from the New Milford Public Works Department Calculations for the 18-inch culverts have not been provided.

Response: The location of the culverts will be revised to be installed within the project's property lines. Any impacts to Candlewood Mountain Road or the existing drainage system will be coordinated with the Town of New Milford and their Department of Public Works for approval. The culvert design information is included in the attached HydroCAD report.

6.12 The riprap spillway depth is not specified for the sand filter details. Assuming that the outflow from the spillway is calculated to begin at the crest and not the bottom of the riprap, the basins will begin to drain at the interface between the earth embankment and the bottom of the riprap, significantly reducing the effective storage within the basins.

Response: Details A2 and C3 on Sheet 23 of the Issued for Construction plan set dated December 19, 2018 will be revised to address this comment. The surface sand filter design was modeled with a soil berm retaining the stormwater. This stormwater would be retained within the surface sand filter by the berm, percolate through the filter media and eventually either be discharged through the underdrain or infiltrated back into the ground (soil test pits are proposed to confirm this design as discussed above). The berm was designed to retain the rainfall runoff from the 25 year storm event and the spillway was designed to discharge during the 100-year storm event. Details A2 and C3 will be revised to accurately depict the design of the stormwater model since, as the review notes, outflow will begin at that crest.

6.13 The berms of the sand filters are shown at a 2:1 slope. Recommended slopes on constructed berms generally require an average slope of 2.5 between the inside and outside slopes of the berm.

Response: The design is being re-evaluated and the berm slope will be modified in the re-design.

6.14 Sand filter 7C does not include a berm as shown in the calculations and merely drains from elevation 726 to 724.

Response: Surface sand filter 7C has a top of berm design height of 726.25 ft as shown on the design table on Sheet 23 of the Issued for Construction plan set dated December 19, 2018 and also included as Table B3-2 (below) of the Stormwater Pollution Control Plan. The sand filter 100 year hydraulic grade line is 725.24 ft providing 1.01 ft of freeboard with the proposed berm. The Grading and Drainage Plan - 2 (Sheet 10) will be revised for clarity. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete.

Surface Sand Filter	Top of Filter Elevation (Ft)	Filter Invert Elevation (Ft)	Underdrain Invert Elevation (Ft)	Spillway Crest Elevation (Ft)		100 Year HGL Elevation (Ft)	100 Year Freeboard Height (Ft)
1A	810	808.17	807.17	811.50	812.5	811.18	1.32
1B	809.54	807.71	806.71	810.29	811.37	810.36	1.01
2A	795.50	793.67	792.67	796.80	798.45	797.36	1.09
2B	776.76	774.93	773.93	778.75	780.58	779.57	1.01
2C	770,81	768.98	767.98	773.15	774.90	773.82	1.08
3A	727.00	725.17	724.17	728.60	730.49	729.39	1.10
3B	734.25	732.42	731.42	736.92	738.62	737.62	1.00
4A	723.71	721.88	720.88	726.37	728.20	727.20	1.00
4B	730.99	729.16	728.16	733.00	734.90	733.90	1.00
5A	796.06	794.23	793.23	797.91	799.35	798.34	1.01
5B	802.00	800.17	799.17	803.83	805.25	804.16	1.09
6A	806.62	804.79	803.79	807.68	809.12	808.12	1.00
6B	803.56	801.73	800.73	803.64	806.06	804.31	1.75
6C	769.67	767.84	766.84	770.87	772.67	771.54	1.13
7A	791.76	789.93	788.93	792.80	794.30	793.24	1.06
7C	722.87	721.04	720.04	725.00	726.25	725.24	1.01
8A	764.56	762.73	761.73	767.07	768.63	767.63	1.00
8B	748.64	746.81	745.81	750.64	752.30	751.26	1.04
9A	758.14	756.31	755.31	760.14	761.64	760.60	1.04
9B	757.19	755.36	754.36	758.85	759.44	758.43	1.01
10	796.30	794.47	793.47	797.46	798.96	797.91	1.05

6.15 The plans call for a narrow sand filter strip within the bottom of some sand filter basins. The soil media should be placed within the entire bottom of the sand filters.

Response: The filter media is proposed to be installed to ensure the entire bottom of the sand filter is operational as shown on Details C2 and C3, Sheet 23 of the Issued for Construction plan set. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete.

6.16 Water quality basins 2A, 2B, 4A, and 4B are proposed on existing grades approaching 25%, resulting in significant grading along the property line. These basins need to be relocated upgradient to flatter existing slopes that are more suitable for construction of stormwater control features.

Response: The stormwater design is in the process of being revised based on a reduced limit of work area. The revisions will include relocation of these BMPs. Additional clarification on this response will be provided once the re-design is complete.

6.17 Portions of the site grading, drainage, and site improvements are shown directly against property lines and the town right-of-way. The submitted documents indicate that the property lines are based on tax maps and not based on surveyed property lines. Assessor's mapping is approximate and should not be used as a basis for design of construction plans particularly when activity is proposed right up to a property line. An A-2 boundary survey should have been completed prior to submission of the Stormwater General Permit application.

Response: A A-2 boundary survey has been completed by Robert Green Associates, LLC. The boundary lines are very similar to those shown on the design plans submitted with the permit applications. The stormwater design is in the process of being revised based on a reduced limit of work area, however, the design is not expected to change based on the recently conducted boundary survey.

6.18 The grading plan for basin 1A requires the installation of a constructed berm that will impound stormwater up to a couple feet in depth beneath portions of the solar panels. Based on the limited area of sand filter that is shown only in a small portion of the area impounded by the basin nearest to the eastern berm, extended periods of standing water may exist beneath panels after a rainstorm.

Response: Based on the results of the soil test pits (confirming soil type, depth to groundwater and presence of ledge) and the re-design of the solar array, the grading plan for surface sand filter 1A will be revised to be located outside the solar array footprint.

- 7. The phasing plan described in the Stormwater Pollution Control Plan (Appendix D) is simplistic and does not adequately address the potential erosion and sedimentation that should be anticipated from the disturbance of 83.4 acres (see Section 2.1in the Stormwater Pollution Control Plan) on a steep hillside. Note the following:
- 7.1 The plans do not clearly show how no more than 5 acres at a time will be disturbed before stabilization and prior to the installation of the panels.

Response: The phasing plan depicted on Sheet 13 of the Issued for Construction plan set shows the areas to be constructed as Phase IIA, IIB, etc. The text on Sheet 13 also describes how the phasing will occur to ensure no more than 5 acres will be disturbed at one time in accordance with the DEEP Stormwater Erosion Control Guidance. This phasing plan will be revised based on the revised solar PV array design. Note that temporary stabilization will be implemented as part of the phasing plan.

7.2 The plan states that the solar array will be installed after vegetative cover is "initiated," but there is no metric for determining when the soil has been stabilized.

Response: Phase III. 1.9 on Sheet 13 of the Issued for Construction plan set states that a stabilized vegetative cover exists when 80% of the area is covered with growth mature enough to control soil erosion and survive severe weather conditions as dictated on page 5-3-3 of the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control. The phasing plan will be updated based on the revised design which will include temporary (e.g., hydroseed with tackifier) and permanent stabilization measures.

7.3 The plans call for the clear-cutting of trees as one continuous operation, leaving the stumps in place. Such forest operations can cause soil erosion, but the applicant is not proposing to install erosion control measures until after the clearing operation is finished.

Response: The phasing plan depicted on Sheet 13 of the Issued for Construction plan set describes Phase I – Install Perimeter Erosion Control and Site Clearing which includes establishing perimeter controls prior to tree clearing. This will also include survey staking of each angle point of the phase subareas.

Phase I - Install Perimeter Erosion Control and Site Clearing

This phase will consist of the installation of all perimeter erosion control measures and clearing above ground large growth trees from the site. The contractor shall be responsible for survey layout and flagging of the limit of clearing prior to the start of activities associated with this phase.

1. Survey and stake limits of disturbance for Phase I activities, as shown on the drawings.

2. Hold a pre-construction meeting

- 3. Install perimeter sediment controls as shown on the drawings
- 4. Install the construction entrance along Candlewood Mountain Road and prepare the temporary staging area.
- 5. Cut above ground vegetation, within the limits of disturbance. Chip cleared vegetation and save for future use as mulch or wood chip mulch berms around the perimeter of the site. Avoid disturbing vegetation outside the limits of clearing.

The phasing plan will be updated to reflect the revised design.

The second phase of the operation calls for the grubbing (removal of stumps) to be done in 5-acre increments, but the locations of those "plots" have not been clearly defined; this will be left to field survey at the time of construction. Furthermore, the method of grubbing has not been presented. If not performed with appropriate equipment, there is likely to be a loss of topsoil and an increase in the potential for erosion on the steep slopes. It appears from the plans that it is the applicant's intention to perform the operations in a continuum rather that in discrete and separate disturbance plots that will allow for separation of the disturbed areas and for vegetation to become established.

Response: This will be addressed in the redesigned submittal. Hydroseeding with tackifier will be performed as grubbing and grading are completed with a goal of no more than 5 acres of unstabilized soil at one time. The redesign will also address additional erosion control measured on longer, steep exposed side slopes.

7.5 Temporary seeding is proposed in areas that will be disturbed by subsequent construction activity with permanent seeding occurring at a later time. It is not clear how, when, and where permanent seeding will occur.

Response: Phase III.1.8 on Sheet 13 of the Issued for Construction plan set describes that the site shall be temporarily seeded within 72 hours of final grading in a given area and that permanent seeding may be initiated in lieu of temporary seeding in areas that are not anticipated to be disturbed during later phases.

Phase III.4.3 on Sheet 13 of the Issued for Construction plan set also describes that the site shall be cleaned, restored, and reseeded as required after the solar and electrical equipment is installed.

The seed mix installed after clearing and grubbing but before the array installation will be the Quick Erosion Control Cover Mix (ERNMX-104). This seed mix will be combined with a fertilizer and polymer (First Stop or similar) which will harden and hold the soil and seed in place. This seed/fertilizer/polymer mix will then be covered with a continuous application of hay mulch (approximately 4 tons/acre). The final step in stabilization will be to reapply a polymer to the hay mulch to act as a 'glue' to hold the seed, mulch and soil in place. This stabilization sequence has been completed successfully at other large solar PV installations in Connecticut.

Once the array is installed, the site will be restored by overseeding with either the Solar Farm Seed Mix (ERNMX-186) or the Conservation Shade Mix (ERNMX-129) both of which are shade tolerant seed mixes. This site restoration will be completed in the same stabilization sequence noted above on an as-needed basis following site inspections. Additional information on phasing and seed specifications will be provided with the redesign submittal.

Other temporary erosion and sedimentation controls such as erosion control blanket, flocculants, and/or soil stabilizers (Envirotac II, Posi-Shell, or similar) will be proposed on steep and/or long slopes to ensure the site remains stable at all times throughout construction.

The final construction schedule will depend on the final date of approval.

7.6 It is not appropriate to assume that once germination occurs that the land is stabilized and the 5-acre phase is ready for the installation of foundations. It is our experience on sites where grass needs to be established prior to having activity on the site that it takes a substantial period of time before sod becomes adequately established. Permanent seed, which should include drought- and shade-tolerant species, takes 3 weeks or so to germinate and takes months, not weeks, to develop a root system that can withstand traffic. The actual time for turf establishment depends on the time of year that seed is placed, temperature, and moisture. The turf needs to be moved to promote density. In this instance, we would expect a full growing season for the grass to become fully established.

Response: The phasing plan on Sheet 13 of the Issued for Construction plan set provides response actions necessary for reseeding if re-disturbance of the vegetation takes place.

The temporary seed mix installed after clearing and grubbing but before the array installation will be the Quick Erosion Control Cover Mix (ERNMX-104). In sensitive areas, a clover mix may also be used in conjunction with the Quick Erosion Control Cover Mix such as a Crownvetch Seeding Mix (ERNMX-109) and also the Native Steep Slope Mix w/Annual Ryegrass (ERNMX-181) for areas with steep slopes and poor soils. The seed mix will be combined with a fertilizer and polymer (First Stop or similar) which will harden and hold the soil and seed in place. This seed/fertilizer/polymer mix will then be covered with a continuous application of hay mulch (approximately 4 tons/acre). The final step in stabilization will be to reapply a polymer to the hay mulch to act as a 'glue' to hold the seed, mulch and soil in place. This stabilization sequence has been completed successfully at other large solar PV installations in Connecticut.

Once the array is installed, the site will be restored by overseeding with either the Solar Farm Seed Mix (ERNMX-186) or the Conservation Shade Mix (ERNMX-129) both of which are shade tolerant seed mixes. This site restoration will be completed in the same stabilization sequence noted above on an as needed basis following site inspections.

Temporary erosion and sedimentation controls such as erosion control blanket, flocculants, and/or soil stabilizers (Envirotac II, Posi-Shell, or approved equal) will be proposed on steep and/or long slopes to ensure the site remains stable at all times throughout construction.

The phasing plan and construction schedule will be revised based on the revised solar PV layout.

7.7 As described in the plan, the foundations for the solar arrays will be ground screws that, in our experience, are installed using a skid-steer vehicle (a Bobcat). The movement of such equipment will tearapart the grass, likely resulting in erosion unless the grass is fully established.

Response: The site will be monitored for erosion and precautionary measures will be taken to ensure the construction activities have minimal impact on the vegetation. Temporary equipment access roads and/or low-ground pressure (typically 7 psi or less) equipment will be used to minimize disturbance of the restored areas. The temporary roads may be built with gravel or an erosion control product such as TMax High-Performance Turf Reinforcement Mat or approved equal. Vehicles operating on the vegetated surface shall only operate on the existing or temporary gravel access roads, except for low ground pressure construction equipment. Low ground pressure construction equipment operating off the designated access drives shall limit turning on the stabilized vegetation as much as possible. If the full-time on-site inspector and/or engineer determines that the use of equipment is creating the potential for damage to the vegetation, the usage of such equipment shall immediately cease and a revised operation plan shall be

implemented. All operators of the equipment shall be clearly instructed by the on-site inspector and/or engineer regarding the requirements of this project prior to mobilization. Any ruts or rills identified during inspections will be filled and appropriately stabilized promptly.

7.8 The phasing plan attempts to break up the stabilization and construction of the site based on contributing watersheds. This does not seem to be a practical means to construct the improvements, particularly given the potential of subwatersheds being changed or modified as a result of ongoing construction activities. Sediment control measures including sediment traps and diversion swales should be installed and in place in phases immediately adjacent to phases that are under active construction to ensure that downgradient protections are in place should the topography not precisely match what is shown on the plans or if construction activities divert runoff across the estimated watershed limits.

Response: The sediment traps and diversion swales will be installed taking into account the cleared area of land to ensure the topography is accurately depicted and will contribute to the drainage area of each sediment trap without uncontrolled runoff. Per discussions with CT DEEP, on-site representation will monitor for potential changes to subwatersheds. Sheet 13 of the Issued for Construction plan set specifies each sub-area and how these areas are to be developed in series. All perimeter and sediment controls will be installed prior to earth disturbance. The phasing plan will be updated based on the reduced limit of work area.

7.9 The temporary sediment traps (TST) are shown on the plans in the identical manner that sand filter/Water quality basins are shown. The supporting calculations shown on the details sheets include bottom elevations of the TSTs that are up to 3 feet below the bottom of the sand filter, well below the finished grade. The sediment and erosion control plans should reflect the grading of the TSTs shown in the supporting calculations.

Response: Grading detail for each of the temporary sediment traps will be shown on the Erosion and Sedimentation Control Plans (Sheets 17 – 20). The revised design will incorporate the results of the soil test pits.

7.10 Long slopes several hundred feet in length (as much as 700 feet) with average slopes exceeding 10% of disturbed, exposed soil are proposed prior to any sediment control measures. Unprotected long and steep slopes represent a significantly high risk of erosion. Long, steep slopes are required to be broken up by benching, terracing, or diversions to avoid erosion problems (pages 3 through 7 of the 2002 Connecticut Guidelines for Erosion and Sediment Control). Detailed site grading plans should be provided to show these site modifications.

Response: The proposed topography mimics the existing topography unless shown otherwise. There will be on-site personnel monitoring erosion and sediment control to ensure there are adequate protections installed for the site (including perimeter controls and sediment traps). Temporary erosion and sedimentation controls such as erosion control blanket, hay mulch and/or soil stabilizers (Envirotac II, Posi-Shell, or approved equal) will be proposed on steep and/or long slopes to ensure the site remains stable at all times throughout construction. Note that the stormwater design is in the process of being revised based on a reduced limit of work area. Additional clarification on this response will be provided once the re-design is complete, which will include mid-slope E&S controls on longer disturbed slopes. Any ruts or rills identified during inspections will be filled and appropriately stabilized promptly.

7.11 The sediment barrier shown on the perimeter of the site will channelize and direct runoff to the low points along the slope, concentrating runoff from sediment trap outlets. The sediment barrier/silt fence locations need to be placed in a manner that will not result in channelizing the discharge from the basins.

Response: It is acknowledged that the sediment barrier will be installed along consistent contour intervals to avoid channeling or re-directing stormwater flow. For example, a continuous segment of sediment barrier will be installed along contour 280' and a new length of sediment barrier will be

installed along contour 282' when the 280' contour deviates from the surveyed limit of work. The erosion and sedimentation control plans and details of the Issued for Construction plan set will be revised to address this comment, which will include E-Fence or similar product at the outfall of the sediment traps.

7.12 Soil stockpile locations are not shown.

Response: The material staging and stockpiles areas will be shown on the revised plan set. The stockpiles will be surrounded with perimeter controls according the General Construction Details note 5 on Sheet 21 and Detail B4 on Sheet 22 of the Issued for Construction plan set. The stockpiles that are intended to be left dormant for 30 days or longer will also be seeded and stabilized within 15 days.

7.13 Much of the clearing and installation of overhead wires occurs on a slope that exceeds 25% in grade. While the activities proposed in that area are intended to be minor in nature, disturbed soil on a slope this steep will require temporary diversions and at least temporary erosion control matting to allow for vegetation to become established.

Response: Figure 1 attached has been prepared demonstrating the areas of the site where existing topography is equal to or exceeds a 10% and a 25% slope. This figure represents the areas where temporary erosion and sedimentation controls such as erosion control blanket, hydroseed with tackifier, flocculants, and/or soil stabilizers (Envirotac II, Posi-Shell, or approved equal) will be proposed on steep and/or long slopes to ensure the site remains stable at all times throughout construction. A polymer will also be used during the seeding process as discussed above, which will hold the soils, seed and erosion control in place. A detail for slope erosion control matting is provided as Detail A3 on Sheet 22 of the Issued for Construction plan set which states that the biodegradable erosion control matting shall be installed on slopes greater than or equal to 10%.

7.14 There are no long-term stabilization measures shown along the drip line of the panels. Particularly in areas exceeding 10% in grade, there exists the potential for erosion of the soil, which over time will result in increased sediment loads to downgradient areas.

Response: A gravel strip will be incorporated into the solar design within areas where the existing topography is greater than or equal to 10% as demonstrated in Figure 1 attached.

- 8. The document prepared by CTDEEP entitled Stormwater Management at Solar Farm Construction Projects includes clarification on procedure, design goals, and construction monitoring requirements that reiterate the goals of design documents referenced in Comment 3 above. The submitted documents fail to adhere to the recommendations of CTDEEP guidelines as noted below:
- 8.1 The CTDEEP document requires that the methods of "an approvable SWPCP will include methods for avoiding compaction of soils, disconnection of and reduction of runoff...avoidance of concentration of stormwater, and other measures necessary to maintain or improve pre-construction hydrology conditions." For the reasons stated in Comment 6, it is our opinion that the post construction hydrology will degrade and exacerbate preconstruction hydrology.

Response: The majority of the equipment proposed for construction at the site will be track equipment which is typically lower ground pressure than rubber tire equipment which will reduce the compaction of existing soils on-site. The contractor will be directed to use access roads for as much site traffic as possible. In addition, while the majority of the site was modeled with poorly infiltrating soils with a high runoff potential (hydrologic soil group (HSG) C and D), the stormwater model will be adjusted for the remainder of the site to be modeled with more conservative hydrologic soil types (such as HSG D) to accommodate potentially compacted soil within the solar PV array area. This will also address the post-construction stormwater design should soils be significantly

compacted (as commented on by DEEP). The response to comment 6.8, above, addresses discharge velocities.

The CTDEEP document requires that the design professional be well versed in erosion and sedimentation guidelines, particularly Chapter 4 for large construction sites. For the reasons we stated in Comment 7, the D&M Plan does not meet these criteria.

Response: Candlewood Solar will address the comments noted above and incorporate these updates into a revised Stormwater Pollution Control Plan. We will work with the Siting Council and DEEP to ensure all concerns are met which includes:

- Completion of soil test pits at each stormwater BMP location;
- Revising the stormwater design to ensure the analysis represents the existing hydrologic conditions at the site;
- Updated temporary and permanent soil stabilization measures;
- Revised perimeter E&S control measures; and
- Revising the solar PV layout including consistent interrow spacing; revising the E&S control
 approach to include minimization of grading, use of compost filter socks to diffuse
 channelized flows, and promptly restoring ruts and rills; and adjusting the stormwater
 analysis accordingly.
- 8.3 The document states an approvable SWPCP shall include, but not be limited to, the location of all erosion, sediment and stormwater control measures including detailed design cut sheets with supporting calculations, construction means and methods, project phasing (i.e. site planning pre-construction, construction, and post- construction stabilization, etc.), construction sequencing and a construction schedule." For the reasons stated in Comment 7, the phasing plan lacks sufficient detail, and the timing of construction activities will result in large tracts of disturbed land with a lack of mature vegetation needed to limit the potential for transport of sediment during construction.

Response: We have summarized the locations within the SWPCP where the requested information can be located. The HydroCAD model output for pre and post construction conditions is also attached, which contains these supporting calculations. We will revise the application to ensure the information is clear and complete:

- The location of all erosion, sediment and stormwater control measures such as sediment barriers, silt fence, construction exits, outlet protection, and notes/references for temporary and permanent seed mixes are included on:
 - Sheets 14 20 for temporary erosion and sedimentation controls
 - Sheets 9 12 for permanent erosion and sedimentation controls
- Detailed design cut sheets with supporting calculations:
 - o All construction details including specific design details are provided on Sheets 22 23
 - o All detailed calculations are provided in Appendix B of the SWPCP
- Construction means and methods, project phasing and construction sequencing:
 - All project phasing is provided on the Erosion and Sedimentation Controls Overview and Phasing Plan (Sheet 13)
- Construction Schedule: provided in response 7.5 above and will be included in the revised plan set.
- 9. In summary, the plans submitted to the CSC as part of the D&M Plan are inadequate and lack the necessary information to assure that there will not be erosion and sedimentation caused by the construction activities that could impact the waters of the stated as noted below:
- 9.1 Contrary to representations made by the petitioner, the hydrology of the site will be permanently altered and will impact adjoining properties.

Response: While the conditions of the site will be altered for the construction of the solar PV array, the stormwater design was developed based on the Connecticut requirements. Existing drainage patterns will be maintained, and the intent of the design is to model the post construction stormwater hydrology to generate an equal or less rate of stormwater runoff from the site, compared to existing conditions, with better stormwater quality as demonstrated in Appendix B of the SWPCP. The discharge of each surface sand filter will flow over an energy dissipator designed to reduce the discharge velocity and redistribute the stormwater to promote sheet flow. This response will be further clarified upon submittal of the re-design.

9.2 The Candlewood Solar project should be distinguished from other projects that come before the CSC. Whereas transmission line projects, for example, disturb land in a linear manner where impacts from erosion and sedimentation are manageable and stabilization can occur quickly, the Candlewood Solar project will require the clearing, grubbing, and regrading of a large block of land on steep slopes where it will be difficult to manage impacts.

Response: The construction plan will be revised based on the re-design and the project schedule.

9.3 The establishment of grass cover adequate to prevent long-term erosion will require regrading of the site prior to seeding. The time that it will take to achieve well-established grass should be measured in months, not weeks. By developing the site in "rolling" 5-acre increments without establishing thick turf before installing the solar arrays is highly likely to cause both short-term and long-term erosion and sedimentation.

Response: The construction phasing plan will be revised as discussed above based on the redesign. The overall strategy is to provide as much time for seed germination as possible prior to installing the racking and panels. To augment this, additional stabilization measures will be provided as outlined in the response to comment 7.6

The density of the solar arrays will severely restrict sunlight to the grass beneath the panels and make it very difficult to maintain the grass that will allow for its long-term health.

Response: Shade tolerant seed mixes have been specified for restoration of the array portion of the site to account for the potential increase in shade due to the row spacing. The stabilization seed mix installed after clearing and grubbing but before the array installation will be the Quick Erosion Control Cover Mix (ERNMX-104). Once the array is installed, the site will be restored by overseeding with either the Solar Farm Seed Mix (ERNMX-186) or the Conservation Shade Mix (ERNMX-129) both of which require as little as 2 hours of indirect sunlight to promote a healthy vegetated cover. Also, the array design will be re-designed with a consistent interrow spacing. The revised inter-row spacing will be shown on the redesign submittal.

9.5 If the CSC requires the petitioner to modify and resubmit the plan and supporting documents in accordance with the foregoing comments, it is quite possible that the configuration of the solar arrays will need to be modified and further reduced in number.

Response: The solar PV array layout is being redesigned to address these comments. The design will be finalized to obtain DEEP approval.