## STATE OF CONNECTICUT CONNECTICUT SITING COUNCIL

| IN RE:                              | :   |                |
|-------------------------------------|-----|----------------|
| ::                                  | 100 |                |
| A PETITION OF SOLARCITY CORPORATION |     | PETITION NO    |
| TO APPROVE BY DECLARATORY RULING    |     |                |
| THE CONSTRUCTION AND OPERATION OF   |     |                |
| A SOLAR PHOTOVOLTAIC ELECTRIC       | :   |                |
| GENERATING FACILITY OFF OLD FORGE   | :   |                |
| ROAD, ROCKY HILL, CONNECTICUT       | :   | MARCH 24, 2016 |

## PETITION FOR A DECLARATORY RULING: INSTALLATION HAVING NO SUBSTANTIAL ADVERSE ENVIRONMENTAL EFFECT

## I. Introduction

Pursuant to Section 16-50k(a) of the Connecticut General Statutes ("C.G.S.") and Sections 16-50j-38 et seq. of the Regulations of Connecticut State Agencies ("R.C.S.A.), SolarCity Corporation ("SolarCity") hereby petitions the Connecticut Siting Council ("Council") to approve, by declaratory ruling, the proposed construction and operation of a 3.9 megawatt ("MW") solar photovoltaic electric generating facility (the "Facility") on property located off Old Forge Road in Rocky Hill, Connecticut.

Connecticut General Stat. § 16-50k(a) provides that:

Notwithstanding the provisions of this chapter or title 16a, the council shall, in the exercise of its jurisdiction over the siting of generating facilities, approve by declaratory ruling...(B) the construction or location ... of any customer-side distributed resources project or facility or grid-side distributed resources project or facility with a capacity of not more than sixty-five megawatts, as long as such project meets air and water quality standards of the Department of Energy and Environmental Protection....

As discussed more fully below, SolarCity respectfully submits that the Facility constitutes a grid-side distributed resources facility, satisfies the criteria of C.G.S. Section 16-

50k(a) and will not have a substantial adverse environmental effect.

## II. Petitioner

SolarCity is a Delaware Corporation with a local office at 714 Brook Street, Rocky Hill, Connecticut. SolarCity was established in 2006 and has quickly become the largest provider of solar power in the United States. SolarCity makes clean energy available to homeowners, businesses, schools and government organizations, like the Town of Rocky Hill, at lower cost. SolarCity has successfully secured Council approval for the development of grid-side solar generating facilities in Groton and Norwich, Connecticut<sup>1</sup>.

Correspondence and/or communication regarding this petition should be addressed to:

Nichole Seidell, Director of Environmental Permitting SolarCity Corporation Two Logan Square 100 N. 18<sup>th</sup> Street, Suite 1900 Philadelphia, PA 19103 267-457-4412 nseidell@solarcity.com

A copy of all such correspondence and/or communications should also be sent to the petitioners' attorneys:

Robinson & Cole LLP 280 Trumbull Street Hartford, CT 06103 860-275-8200 Kenneth C. Baldwin, Esq. kbaldwin@rc.com Joey Lee Miranda, Esq. jmiranda@rc.com

## III. Background

SolarCity has entered into a Solar Power Purchase Agreement ("PPA") with the Town of

<sup>&</sup>lt;sup>1</sup> See generally Siting Council Petition Nos. 1181, 1192, 1195.

Rocky Hill. Under the terms of the PPA, SolarCity will construct, maintain and operate a 3.9 MW solar photovoltaic electric generating facility on the northerly portion of an undeveloped 61.38-acre parcel off Old Forge Road in Rocky Hill (the "Property"). The Property is owned by the Town of Rocky Hill ("Town"). All of the power generated by the Facility will be purchased by the Town. The Town will receive an annual site use payment from SolarCity. Environmental attributes and environmental incentives associated with the Facility will be retained by SolarCity.

## IV. Property Description

The Property is located in the southerly portion of the Rocky Hill Industrial Park, in the Town's Office Park (OP) zone district. The Property is surrounded by existing commercial and light industrial uses to the north within the Industrial Park; Town-owned open space land including Dividend Pond and a portion of Dividend Brook to the west and north; an active rail line and undeveloped land to the east; and undeveloped land to the south. The Property and land of John Russo, Trustee to the south and southwest, were previously used as a part of a sand and gravel mining operation. Central portions of the Property are currently used by the Rocky Hill Department of Public Works ("DPW") for material storage (top soil, road millings, sand and gravel) and leaf composting. Access to these DPW use areas extends from Old Forge Road along an existing paved and gravel driveway. The remainder of the Property is undeveloped, maintaining some forested areas and early successional trees with a dense understory of mostly scrub/shrub and herbaceous growth.

Two (2) wetland areas proximate to the proposed Facility were evaluated by All-Points

Technology Corp. ("APT") for potential impacts from the proposed development activities.

Wetland 1 is located adjacent to Dividend Brook near the existing culvert that extends

<sup>&</sup>lt;sup>2</sup> The Property is identified as Map 18, Lot 93 on the Rocky Hill Assessor's records and is also known and referred to as R013 Old Forge Road.

underneath the access driveway (Dividend Road) in the northerly portion of the Property.

Dividend Brook extends further to the east, beyond the access drive and eventually discharges into the Connecticut River. A smaller, isolated wetland area, identified as Wetland 2, is located on an undeveloped parcel to the east of the Property on land owned by Gardiner Nursery Inc.

The nearest residential area is located approximately 820 feet to the west, along Briarwood Court. (See Attachment 1 – Existing Conditions Map).

## V. Project Description

The Facility and related improvements, including an access driveway, construction staging and laydown areas, will occupy an approximately twenty-four (24) acre area in the northerly portion of the Property (the "Project Area"). The Project Area is generally flat with a gentle grade sloping down from west to east toward the Connecticut River. Access to the Project Area will extend from Old Forge Road to the west of the Project Area, along a portion of an existing paved and gravel driveway used to access the Property and the DPW's materials storage areas. Project plans for the proposed Facility are included in <u>Attachment 2</u>. <sup>3</sup>

Solar TSM-PD14 photovoltaic modules; three (3) advanced Energy AE 500 TX 500 kW inverters; and three (3) electric transformers within the Project Area. A 23 kilo volt (kV) electric interconnect service line will extend, overhead, from the northerly portion of the Project Area to Old Forge Road and the existing Eversource electric distribution infrastructure. The Facility will utilize a post-driven RBI Solar Inc. panel racking system. The individual photovoltaic panels will be fixed at a 30 degree tilt to the south to promote maximum efficiency. The Facility will be

<sup>&</sup>lt;sup>3</sup> Project plans for the Facility are a compilation of engineering plans prepared by Westson & Sampson (Plan Sheets T-1, 6-1, D-1, C-1, C-2 and C-3); Electrical Details prepared by SolarCity (Plan Sheets PV-5, PV-6 and PV-7); and Racking System Details prepared by RBI Solar Inc. (Plan Sheets S-201 and S-301).

surrounded by an eight (8) foot security fence. Two (2), sixteen (16) foot wide access gates will be installed along the west side of the fenced Project Area. (See Attachment 2, Plan Sheet C-2).

SolarCity expects construction of the Facility to take approximately three (3) to four (4) months. Construction will commence immediately after SolarCity receives all necessary permits and approvals.

APT, on behalf of SolarCity, has completed an exhaustive Environmental Assessment ("EA") of the Property and has evaluated the potential environmental effects that may occur following the development of the Facility. A copy of the EA is included in <a href="Attachment 3">Attachment 3</a>. Based on the conclusions in the EA, SolarCity respectfully submits that the Facility will comply with the DEEP's Air and Water Quality Standards and will not have a substantial adverse effect on the Property or its surrounding environment.

VI. The Facility Will Comply with the Department of Energy and Environmental Protection (DEEP) Air and Water Quality Standards and Will Not Have a Substantial Adverse Effect on the Environment

## A. Air Quality Standards

Operation of the Facility will not produce emissions of any regulated air pollutants or greenhouse gases. No impacts to air quality are expected, and no DEEP air permit is required for the Facility. (*See* Attachment 3, p. 30).

## B. Water Quality Standards

The Facility is unstaffed and does not require the use of potable water or any sanitary facilities in the production of electricity. Any water utilized during construction for dust control will be minimal and have no impact on water quality in the vicinity of the Property. No liquid fuels are associated with the operation of the Facility.

The Property is located in Flood Zone X, designated as an area outside both the 100-year and 500-year flood plain. The Property is also located in the Gardner Expansion Aquifer

Protection Area ("APA"). The closest water supply wells, however, are located more than 1,000 feet to the southwest of the Property in the Town of Cromwell. There are no water supply wells located on the Property. (See Attachment 3, pp. 14-15). To protect the APA, SolarCity will establish and implement protective measures in the form of an Aquifer Protection Plan.

Protective measures in this plan include, but are not limited to, the monitoring of established sedimentation and erosion controls, the development of a detailed stormwater management plan and compliance with the filing requirements of the DEEP's General Permit for the Discharge of Stormwater and Dewatering Wastewater. A copy of a Stormwater Management Report "SWMP" for the Facility is included in Attachment 4. As demonstrated in the SWMP, there will be no negative stormwater impacts resulting from the development and operation of the Rocky Hill Facility.

No inland wetlands or watercourses will be directly impacted by the development of the Facility. All clearing and grading activity within the limits of the Project Area would maintain a setback of 370 feet to Wetland 1, located along the existing access drive, in the northern reaches of the Project Area. Wetland 2 is an isolated wetland located approximately 260 feet to the east of the Project Area, east of the existing rail line. Any potential short term temporary impacts on Wetland 1 or Wetland 2 will be minimal and mitigated by the use and maintenance of proper soil erosion and sedimentation controls throughout the construction period. SolarCity does not, therefore, expect any adverse impacts to area wetland resources. Likewise, no areas supporting vernal pool habitat are located within 750 feet of the Project Area and no vernal pool habitat was identified in either Wetland 1 or Wetland 2. (See Attachment 3, pp. 3-6 and 24).

<sup>&</sup>lt;sup>4</sup> The installation of a new utility pole, required for interconnection to the existing distribution system may occur within 160 feet of Wetland 1. The final location of new utility poles required for electric interconnection has not yet been determined.

## C. Vegetation and Wildlife

As mentioned above, a majority of the Project Area has been previously cleared during sand and gravel mining operations. Portions of the Project Area support early successional tree and scrub growth. While the construction of the Facility will alter vegetation and wildlife habitat within the Project Area, habitat beyond the limits of the Project Area will not be impacted. (*See* Attachment 3, pp. 6-9 and 25-26).

## D. <u>Bird Habitat Impact Analysis</u>

APT has completed a detailed Bird Habitat Impact Analysis for the Project Area. Habitat loss is an unavoidable consequence of any type of land development including that necessary for the Facility. While development of the Facility will result in some loss of habitat, it will not result in fragmentation of the overall habitat matrix of the area. (*See Attachment 3*, pp. 26-27).

## E. Rare Species

According to the DEEP Natural Diversity Database ("NDDB"), the *Big Sand Tiger Beetle*, a Connecticut species of special concern, may occur in southwestern portions of the Property. In anticipation of the filing of this Petition, APT conducted a habitat-based survey of the Project Area, using known habitat requirements and determined that the Facility would not impact the *Big Sand Tiger Beetle*. Due to the potential presence of *Tiger Beetle* populations proximate to this Project Area, SolarCity has committed to the implementation of proactive protective measures to be utilized during construction. These protection measures have been developed and submitted to DEEP for review.

Further, APT determined that one federally listed "threatened" species, the *Northern*Long Eared Bat ("NLEB") may occur in the vicinity of the Property. The identified range of the NLEB encompasses the entire State of Connecticut. To assess the potential impact of the SolarCity project on the NLEB, APT evaluated the recently established U.S. Fish and Wildlife

Service (USFWS) NLEB impact criteria and determined that the facility would not result in an adverse effect on or incidental take of NLEB. (*See Attachment 3*, pp. 28-29).

## F. Scenic Areas

No State designated scenic areas would be physically or visually impacted by the development of the Facility. (*See Attachment 3*, p. 30).

## G. Historic and Archeological Resources

No historic resources listed on or eligible for listing on the National Register of Historic Places exist on or proximate to the Property. The nearest historic resource is located approximately one mile from the Project Area. There are reported archeological sites in the general vicinity of the Property. Due to the historic sand and gravel mining operations at the Property, it is unlikely that any of these resources, if they exist, would remain intact. The Project Area, therefore, no longer possesses any potential to yield intact archeological deposits. (*See Attachment 3*, pp. 15-16).

SolarCity has consulted with the Connecticut State Historic Preservation Office regarding seeking concurrence with its findings that the Facility and the potential that the project may impact historic or archeological resources of the State. The SHPO is currently reviewing the SolarCity findings. Based on research conducted by SolarCity's consultant team, it was determined that the Facility would not impact historic and archeological resources of the State. (See Attachment 3, pp. 15-16 and 30-31).

## H. <u>Recreational Resources</u>

The Facility will not impact any existing or proposed recreational resources in the Town of Rocky Hill. (See Attachment 3, p. 16).

#### Carbon Debt Analysis

The Facility will result in a net improvement in carbon reduction compared to the loss of

approximately twenty-four (24) acres of the forest woodland portions of the Property. The Carbon Debt Analysis included in <u>Attachment 5</u> accounts for the loss of trees on the Property and carbon associated with both the manufacturer of the solar panels and Facility construction activities. The results of this analysis demonstrate that the Facility would begin to have a measurable net improvement in carbon reduction in less than three (3) years.

### J. Noise

The only equipment associated with the Facility that generates noise are the fans associated with the three (3) 500 kW inverters. According to a Noise Report prepared for the proposed installation, the Facility will comply with all State and local noise standards. (See <a href="https://dx.doi.org/10.108/j.gov/Attachment3">Attachment 3</a>, pp. 17 and 31).

## K. Visibility

APT has completed a visual impact assessment for the proposed Facility. The Facility is setback sufficiently from all abutting properties and the nearest public roadways. Intervening vegetation between these adjacent points and the Facility provide adequate and complete visual screening. The Facility will, therefore, have minimal aesthetic impact on adjacent uses and/or properties. (*See Attachment 3*, p. 32).

### L. Traffic

Traffic to the Facility, after the initial construction period, would be minimal. Unless there is a problem with a particular piece of equipment, SolarCity anticipates the need for annual maintenance visits by technicians. In addition, typical grounds maintenance involves mowing of the area between the solar panels approximately four (4) times during a typical calendar year.

## M. <u>Decommissioning Plan</u>

SolarCity has developed a Decommissioning Plan to prepare for the eventual permanent closure of the Facility. The Decommissioning Plan describes the process for removal and

disposal or the recycling of all equipment and materials installed within the Project Area and the restoration of the land to its pre-development condition. A Decommissioning Plan is included in Attachment 6.

## VII. Notice to the Government Officials and Abutting Landowners

Copies of this Petition have been sent by certificate of mailing to municipal, regional and State officials, pursuant to the requirements of C.G.S. Section 16-50*l*(b). A Certificate of Service, along with the lists of the officials who were sent a copy of the Petition, are included in <a href="https://doi.org/10.2016/j.com/Attachment7">Attachment 7</a>. A Certificate of Service verifying that a copy of the Petition was also sent to all abutting landowners in accordance with R.C.S.A. Section 16-50j-40 along with a list of these abutters is included in <a href="https://doi.org/10.2016/j.com/Attachment8">Attachment 8</a>.

### VIII. Conclusion

For the reasons stated above, SolarCity respectfully requests that the Council approve the location and construction of the Facility by declaratory ruling.

Respectfully submitted,

CELLCO PARTNERSHIP d/b/a VERIZON WIRELESS

Kenneth C. Baldwin, Esq.

Joey Lee Miranda, Esq.

Robinson & Cole LLP

280 Trumbull Street

Hartford, CT 06103-3597

(860) 275-8200

Its Attorneys

## List of Attachments

- 1. Existing Conditions Map
- 2. Project Plans
- 3. Environmental Assessment
- 4. Stormwater Management Report
- 5. Carbon Debt Analysis
- 6. Decommissioning Plan
- 7. Notice to the Government Officials
- 8. Notice to Abutting Landowners

# ATTACHMENT 1



Town of Rocky Hill Property (+/-61.4 acres)

Existing Access Drive

Existing Materials Pile

2' Contour Line

10' Contour Line

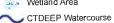
X=X= Proposed Fenced Facility (+/-19 acres)

•••• Existing Treeline/Clearing Limit

Project Area - Limit of Proposed Work (+/-24 acres)

Start/End Wetland Flag

Delineated Wetland Boundary



🛂 Wetland Area



Approximate Assessor Parcel Boundary (CTDEEP)



## Attachment 1 **Existing Conditions Map**

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut



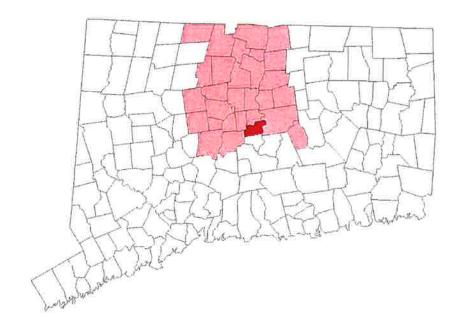


## **ATTACHMENT 2**

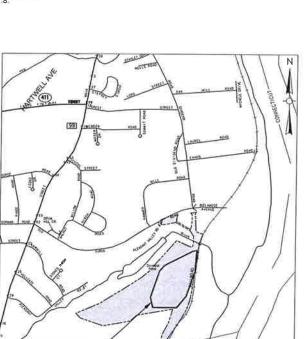
## ROCKY HILL, CONNECTICUT

SOLAR PHOTOVOLTAIC (PV) PROJECT

## R013 OLD FORGE ROAD ROCKY HILL, CONNECTICUT 06067



SCALE: N.T.S.



| PROJECT DI  | RECTORY   |
|---|---|
| DEVELOPER(S):<br>SOLAR CITY, INC<br>1376 LEAD HILL BLVD.<br>ROSEVILLE. CA 95661                     | RACKING SYSTEM DESIGNER:<br>RBI SOLAR<br>5513 VINE STREET<br>CINCINNATI, OH 45217 |
| CONTACT: JOSHUA TROGLIN<br>(650) 332-0412   | CONTACT: LOUIS "PAT" HUDEPOHL<br>513-618-2183                                     |
| HOST:<br>TOWN OF ROCKY HILL<br>R013 OLD FORGE ROAD<br>ROCKY HILL, CONNECTICUT 06067                 | UTILITY:<br>EVERSOURCE  |
| ENGINEER:<br>WESTON & SAMPSON ENGINEERS, INC.<br>273 DIVIDEND ROAD<br>ROCKY HILL, CONNECTICUT 08067 |   |
| CONTACT: JOHN FIGURELLI<br>(860) 513-1473   |   |
| ELECTRICAL ENGINEER:<br>PLUMP ENGINEERING, INC<br>914 E KATELLA AVENUE<br>ANAHEIM, CA 92805         |   |
| CONTACT: ANN D'ALESSANDRO<br>(518) 796-1030   |   |

| SHEET | SHEET TITLE                          |
|-------|--------------------------------------|
| T-1   | COVER SHEET                          |
| G-1   | ABBREVIATIONS, NOTES AND LEGEND      |
| D-1   | DETAILS                              |
| C-1   | EXISTING CONDITIONS                  |
| C-2   | LAYOUT PLAN                          |
| C-3   | EROSION & SEDIMENTATION CONTROL PLAN |

| F V-1 | EQUIPMENT DETAILS                     |
|-------|---------------------------------------|
|       | DRAWING INDEX - RBI SOLAR             |
| SHEET | SHEET TITLE                           |
| S-201 | ADDITIONAL POST SECTIONS & ELEVATIONS |
| S-301 | RACK SECTION & BAY PLAN VIEWS         |

STRUCTURAL DETAILS & INVERTER PADS
PV EQUIPMENT PLAN & ELEVATION

|             | SOLA                                | AR PHOTOVOLTAIC (PV) SYSTEM DESCRIPTION |                                     |
|-------------|-------------------------------------|---|-------------------------------------|
| SYSTEM      | MOUNTING PLANE I.D. 1               | MOUNTING PLANE I.D. 2                   | MOUNTING PLANE I.D. 3               |
| SYSTEM SIZE | 1,300,750 kW                        | 1,300,750 kW                            | 1,301,520 kW                        |
| MODULE      | (4,730) TRINA SOLAR TSM-PD14 (275W) | (4,730) TRINA SOLAR TSM-PD14 (275W)     | (4,488) TRINA SOLAR TSM-PD14 (290W) |
| TILT ANGLE  | 30 DEGREES                          | 30 DEGREES                              | 30 DEGREES                          |
| AZIMUTH     | 170 DEGREES                         | 170 DEGREES                             | 170 DEGREES                         |
| RACKING     | RBI RACKING                         | RBI RACKING                             | RBI RACKING                         |

PV-5

SHEET TITLE

Project:

ROCKY HILL
SOLAR PROJECT



R013 OLD FORGE ROAD ROCKY HILL CT 06067



3055 Clearview Way San Malao, CA 94402 (550) 638-1028 www.solarcity.com

Waster Service

273 DMolend Road Rocky Hal, Commedicat (960) 513-1483 (900) Sampson www.westonandsampson.com



Revisions:

Rev Date Description

Seal:



PERMIT PLANS
JOB NO. 2150769

 Date:
 03.16.2016

 Scale:
 AS SHOWN

 Drawn By:
 LEC

 Reviewed By:
 JSP

 Checked By:
 JSP

 Approved By:
 RGT

Drawing Title:

COVER SHEET

et Number:

T-1

0769 - Rocky Hill CAD 01 - Cover T-1, dwg

PROJECT AREA

| LEGEN                              | D          |         |
|------------------------------------|------------|---------|
| DESCRIPTION                        | EXISTING   | PROPOS  |
| CATCH BASIN                        |            |         |
| HYDRANT                            | ρ,         | +       |
| UTILITY POLE                       | -D         |         |
| POLE-MOUNTED LIGHT FIXTURE         | ¢          | -0      |
| EDGE OF PAVEMENT                   |            |         |
| EDGE OF UNPAVED ROAD               |            |         |
| PROJECT AREA                       |            |         |
| OVERHEAD WIRE (ELECTRICAL)         | 6          |         |
| ELECTRICAL CONDUIT (SUBGRADE)      | E          | — E -   |
| RAILROAD                           | 1111111    |         |
| STONE WALL                         | 0000000000 | 0000000 |
| RETAINING WALL                     |            |         |
| FENCE                              |            |         |
| INDIVIDUAL DECIDUOUS TREE          | O.         | 0       |
| INDIVIDUAL EVERGREEN TREE          | *          | *       |
| EDGE OF WOODS/ CLEARING            | unun       | ~~~     |
| DEBRIS / SOIL PILE / RUBBLE        |            |         |
| ELECTRIC METER                     |            |         |
| SURVEY MARKER                      |            |         |
| PROPERTY BOUNDARY                  |            |         |
| MOUNTING PLANE LIMIT               | 1          |         |
| SPOT ELEVATIONS                    | ×          | x 46    |
| CONTOUR LINES                      |            |         |
| RESOURCE FLAG                      | ■ TOB/BVW  |         |
| GUY WIRE                           | 0-         |         |
| EROSION CONTROL MATTING            |            |         |
| RIP RAP                            | ******     |         |
| SIGN                               | -          |         |
| BENCH MARK                         | •          |         |
| SEDIMENT/EROSION CONTROLS          | 1 1        |         |
| ROCK OUTCROP                       |            |         |
| SEWER MANHOLE                      | (5)        | _       |
| MANHOLE (MH) FOR UNDERDRAIN SYSTEM | 0          |         |
| DRAIN MANHOLE (DMH)                | 0          |         |
| UTILITY MANHOLE                    | 1 0        |         |
| GROUND-MOUNTED SOLAR PV MODULES    |            |         |
| (ELECTRICALLY CONNECTED)           |            |         |
| OVERHEAD WIRE                      | — он —     |         |
| BORDERED VEGETATED WETLAND BUFFER  |            |         |
| WETLAND FLAG                       | ▲ WF       |         |
| IRON PIN                           |            |         |

## **ABBREVIATIONS**

MORE OR LESS TYP TYPICAL

ACCMP

ALTERNATING CURRENT

CORRUGATED METAL PIPE

DC DIRECT CURRENT

RCP REINFORCED CONCRETE PIPE

FEU FLARED END UNIT

W/ WITH

WETLAND FLAG WF #1

REC RECOVERED

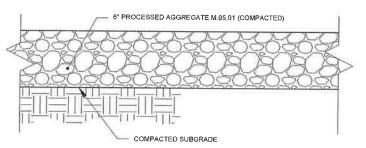
N/F NOW OR FORMERLY

CT CONNECTICUT

DEEP DEPARTMENT OF ENERGY AND ENVIRONMENTAL PROTECTION

#### CONSTRUCTION NOTES:

- 1. THE CONTRACTOR SHALL CALL BEFORE YOU DIG (CBYD) AT 811 OR 1-800-922-4455 AT LEAST 72 HOURS, SATURDAYS, SUNDAYS, AND HOLIDAYS EXCLUDED, PRIOR TO EXCAVATING AT ANY LOCATION, A COPY OF THE CALL BEFORE YOU DIG PROJECT REFERENCE NUMBER(S) SHALL BE GIVEN TO THE OWNER PRIOR TO EXCAVATION.
- 2. LOCATIONS OF EXISTING PIPES, CONDUITS, UTILITIES, FOUNDATIONS AND OTHER UNDERGROUND OBJECTS ARE NOT WARRANTED TO BE CORRECT AND THE CONTRACTOR SHALL HAVE NO CLAIM ON THAT ACCOUNT SHOULD THEY BE OTHER THAN SHOWN...
- STONE WALLS, FENCES, CURBS, ETC, SHALL BE REMOVED AND REPLACED AS NECESSARY TO PERFORM THE WORK, UNLESS OTHERWISE INDICATED, ALL SUCH WORK SHALL BE INCIDENTAL TO CONSTRUCTION OF THE PROJECT.
- $4_{\odot}$  ALL AREAS DISTURBED BY THE CONTRACTOR BEYOND THE PROJECT AREA SHALL BE RESTORED AT NO ADDITIONAL COST TO THE OWNER,





ROCKY HILL SOLAR PROJECT



R013 OLD FORGE ROAD ROCKY HILL, CT 06067



## Weston&Sampson

273 Dividend Road Rocky Hill, Connecticut (860) 513-1483 (800) Sampson





PERMIT PLANS JOB NO. 2150769

03 16 2016 AS SHOWN Drawn By: LEC Reviewed By: JSP Checked By: DCH

Drawing Title:

ABBREVIATIONS, NOTES, LEGEND, AND DETAILS

**G-1** 

ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE PERFORMED IN ACCORDANCE WITH THE "CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL" (MAY 2002), THE CONTRACTOR SHALL OWN AND MAINTAIN A COPY OF THE GUIDELINES ON-SITE DURING CONSTRUCTION.

ALL DISTURBED AREAS SHALL BE KEPT TO A MINIMUM, FINAL GRADING AND RESTORATION SHALL BE ACCOMPLISHED AS SOON AS PRACTICAL.

EROSION AND SEDIMENT CONTROL STRUCTURES SHALL BE INSTALLED PRIOR TO SITE WORK, IF IT IS NOT POSSIBLE TO DO SO, THE ENGINEER SHALL BE NOTIFIED IN ORDER TO MAINTAIN THE INTEGRITY OF

ALL CONTROL STRUCTURES SHALL BE MAINTAINED THROUGHOUT CONSTRUCTION AND REMOVED WHEN STABILIZATION HAS BEEN ATTAINED. IF THE PROPOSED CONTROL MEASURES ARE NOT SATISFACTORY, ADDITIONAL CONTROL MEASURES SHALL BE TAKEN

ALL RUNGEF FROM THE DISTURBED AREA SHALL BE CONTROLLED AND FILTERED NON-WOVEN SYNTHETIC FIBER FILTER FABRIC, STRAW BALES OR SILT SOCKS SHALL BE USED IN THE AREAS SHOWN ON THE SITE PLAN AND INSTALLED AS SHOWN ON THIS PLAN.

A CT DEEP GENERAL PERMIT FOR THE DISCHARGE OF STORMWATER AND DEWATERING WASTEWATERS FROM CONSTRUCTION ACTIVITIES WILL BE REQUIRED FOR THE PROPOSED PROJECT. THE CONTRACTOR SHALL BE RESPONSIBLE FOR IMPLEMENTATION AND COMPLIANCE WITH THE APPROVED STORMWATER POLLUTION CONTROL PLAN (SWPCP),

THE CONTRACTOR MUST OBTAIN COPIES OF THE ZONING, WETLANDS AND CTDEP STORMWATER

THE CONTRACTOR SHALL BE RESPONSIBLE FOR IMPLEMENTATION OF SEDIMENT AND EROSION CONTROL MEASURES, THIS RESPONSIBILITY INCLUDES THE ACQUISITION OF MATERIALS, INSTALLATION, AND MAINTENANCE OF EROSION AND SEDIMENT STRUCTURES, THE COMMUNICATION AND DETAILED EXPLANATION TO ALL PEOPLE INVOLVED IN THE SITE WORK OF THE REQUIREMENTS AND OBJECTIVE OF THE EROSION AND SEDIMENT CONTROL MEASURES.

TWO (2) WEEKS PRIOR TO THE START OF WORK THE CONTRACTOR SHALL PROVIDE THE NAME AND PHONE NUMBER OF THE INDIVIDUAL RESPONSIBLE FOR IMPLEMENTATION OF THIS PLAN

IN THE EVENT THE APPLICANT IS NOT OWNER OF THE PROPERTY. THE CURRENT OWNER SHALL HAVE ALL THE RESPONSIBILITIES LISTED IN THIS PARAGRAPH AND SHALL SUBMIT A WORKING PHONE NUMBER FOR CONTACT AT TIME OF APPLICATION FOR PERMITS, ANY CHANGE IN ENGINEER SHALL BE NOTED AT

THE ENGINEER, WESTON & SAMPSON ENGINEERS, INC. (860-513-1473) #273 DIVIDEND ROAD, ROCKY HILL, CT. 06067 SHALL BE NOTIFIED OF ANY PROPOSED ALTERATION TO THE EROSION AND SEDIMENT CONTROL PLAN, PRIOR TO ALTERING, IN ORDER TO ENSURE THE FEASIBILITY OF THE ADDITION, SUBTRACTION, OR CHANGE IN THE PLAN.

#### SEEDING WITHIN GROUND MOUNTED ARRAY AREA

NEW ENGLAND SEMI-SHADE GRASS AND FORBS MIX - THE NEW ENGLAND SEMI-SHADE GRASS AND FORB MIX CONTAINS A BROAD SPECTRUM OF NATIVE GRASSES AND FORBS THAT WILL TOLERATE SEMI-SHADE AND EDGE CONDITIONS, ALWAYS APPLY ON CLEAN BARE SOIL, THE MIX MAY BE APPLIED BY HYDRO-SEEDING, BY MECHANICAL SPREADER, OR ON SMALL SITES IT CAN BE SPREAD BY HAND. LIGHTLY RAKE, OR ROLL TO ENSURE PROPER SEED TO SOIL CONTACT. BEST RESULTS ARE OBTAINED WITH A SPRING SEEDING, LATE SPRING AND EARLY SUMMER SEEDING WILL BENEFIT WITH A LIGHT MULCHING OF WEED-FREE STRAW TO CONSERVE MOISTURE, IF CONDITIONS ARE DRIER THAN USUAL, WATERING WILL BE REQUIRED, LATE FALL AND WINTER DORMANT SEEDING REQUIRE AN INCREASE IN THE SEEDING RATE, FERTILIZER OR LIMING IS PROHIBITED, UNLESS PRIOR APPROVAL BY THE LOCAL CONSERVATION COMMISSION IS OBTAINED, PREPARATION OF A CLEAN WEED FREE SEED BED IS NECESSARY FOR OPTIMAL RESULTS, APPLICATION RATE 30 POUNDS PER ACRE,

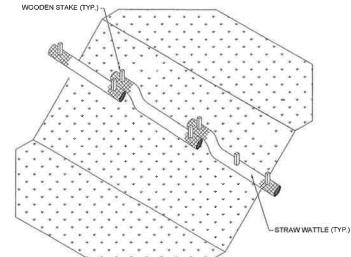
#### MAINTENANCE

MAINTENANCE OF SEEDED AREAS SHALL BE THE SOLE RESPONSIBILITY OF CONTRACTOR AS

- A, CONTRACTOR SHALL MAINTAIN THE ENTIRE SEEDED AREAS UNTIL FINAL ACCEPTANCE AT THE COMPLETION OF THE PROJECT OR FOR 90 DAY, WHICHEVER IS LONGER, MAINTENANCE SHALL INCLUDE WATERING AS SPECIFIED, WEEDING, REMOVAL OF STONES WHICH MAY APPEAR AND REGULAR CUTTINGS OF THE GRASS NO CLOSER THAN 10 DAYS APART, THE FIRST CUTTING SHALL BE ACCOMPLISHED WHEN THE GRASS IS FROM 2-1/2 TO 3 INCHES HIGH, WEEKLY WATERING SHALL PROVIDE THE SEEDED AREAS WITH THE EQUIVALENT OF 1 INCH OF RAINFALL PER WEEK, IF THE SEEDED AREAS ARE WATERED BY NORMAL RAINFALL OR THE NORMAL WATERING IS INADEQUATE DUE TO WEATHER THE CONTRACTOR MAY AT HIS/HER DISCRETION FLIMINATE OR INCREASE RESPECTIVELY, THE WATERING DURING A GIVEN WEEK, HOWEVER, SUCH ACTION BY CONTRACTOR SHALL IN NO WAY WAIVE CONTRACTOR'S RESPONSIBILITY FOR THE GROWTH AND HEALTH OF THE GRASS UNTIL FINAL ACCEPTANCE, CONTRACTOR SHALL FURNISH ALL TEMPORARY PIPE AND CONNECTIONS FOR SPRINKLING, CONTRACTOR SHALL FURNISH ALL REQUIRED WATER AT NO EXPENSE TO THE OWNER, GARDEN HOSE AND HAND SPRINKLING SHALL BE PERMITTED ONLY IN SPECIAL INSTANCES BY THE OWNER'S REPRESENTATIVE.
- B. ALL BARE SPOTS, WHICH BECOME APPARENT AS THE GRASS GERMINATES, SHALL BE RESEDED BY CONTRACTOR AT ITS OWN EXPENSE AS MANY TIMES AS NECESSARY TO SECURE A GOOD GROWTH AND THE ENTIRE AREA SHALL BE MAINTAINED AND CUT UNTIL ALL WORK HAS BEEN COMPLETED AND FINAL ACCEPTANCE HAS OCCURRED.
- C. CONTRACTOR SHALL TAKE WHATEVER MEASURES ARE NECESSARY TO PROTECT THE GRASS WHILE IT IS GERMINATING. THESE MEASURES SHALL INCLUDE FURNISHING OF WARNING SIGNS, BARRIERS, TEMPORARY FENCE OR ANY OTHER NECESSARY MEASURES OF PROTECTION.
- D. CONTRACTOR SHALL FURNISH, PROTECT, AND MAINTAIN ALL TEMPORARY BARRIERS UNTIL FINAL ACCEPTANCE OF THE SEEDED AREAS BY THE OWNER AND SHALL REMOVE THEM UPON SUCH FINAL ACCEPTANCE, THE BARRIERS SHALL REMAIN THE PROPERTY OF CONTRACTOR AT ALL TIMES.

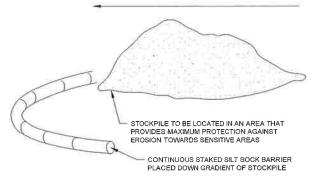
#### TEMPORARY EROSION CONTROL MEASURES:

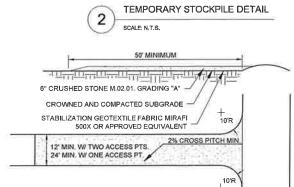
- EROSION CONTROL MEASURES SHALL BE IMPLEMENTED AS INDICATED ON THESE PLANS OR AS REQUIRED BY THE ON-SITE ENGINEER.
- 2. THE SMALLEST PRACTICAL AREA OF LAND SHALL BE EXPOSED AT ANY ONE TIME,
- 3. EROSION/SEDIMENT CONTROL MEASURES SHALL BE INSTALLED AS SHOWN ON PLANS. EROSION CONTROL BARRIERS ARE TO BE MAINTAINED AND CLEANED UNTIL ALL AREAS HAVE BEEN
- THE TEMPORARY AND PERMANENT STORMWATER CONTROLS SHALL BE PERIODICALLY CLEANED OF SEDIMENT, OR AS REQUIRED BY THE ENGINEER. THE SEDIMENT WILL BE REMOVED TO A SECURE LOCATION SO AS TO PREVENT SILTATION OF NATURAL WATER WAYS.
- SILT SOCK FILLED WITH COMPOST MUST BE A MINIMUM TUBE DIAMETER OF 12 INCHES (300mm) FOR SLOPES UP TO 50 FEET (15.24m) IN LENGTH WITH A SLOPE RATIO OF 3H:1V OR STEEPER. LONGER SLOPES OF 3H:11 MAY REQUIRE LARGER TUBE DIAMETER OR ADDITIONAL COURSING OF FILTER TUBES TO CREATE A FILTER BERM. SILT SOCK TO BE MADE OF BIODEGRADABLE BURLAP, SILT SOCK TO BE SEDIMENT FILTERMITT OR APPROVED EQUAL, OTHER REFER TO MANUFACTURER'S RECOMMENDATIONS FOR INSTALLATION INSTRUCTIONS.
- 6. INSTALL SOCK ALONG CONTOURS AND PERPENDICULAR TO SHEET OR CONCENTRATED FLOW.
- CONFIGURE SOCKS AROUND EXISTING SITE FEATURES TO MINIMIZE SITE DISTURBANCE AND MAXIMIZE CAPTURE AREA OF STORMWATER RUN-OFF.
- DISTURBED AREAS SHALL BE SEEDED IMMEDIATELY OR AS SOON AS PRACTICABLE.
- EROSION CONTROL MEASURES SHALL BE REMOVED WHEN DISTURBED AREA IS STABILIZED. DISTURBED AREA RESULTING FROM THE MEASURE REMOVAL OPERATION SHALL BE SEEDED IN ACCORDANCE WITH THE SPECIFICATIONS.
- 10. A CHECK LIST (PROVIDED BY THE ENGINEER) SHALL BE FILLED OUT BY THE CONTRACTOR EVERY WEEK OR AFTER EACH RAINFALL EVENT OF 1/2" OR GREATER AS NOTED ABOVE.
- 11, STRIP AND STOCKPILE TOPSOIL WITHIN THE LIMITS OF THE PROPOSED DEVELOPMENT, PROTECT STOCKPILE PERIMETER WITH EROSION CONTROLS. LOCATE STOCKPILES WHERE INDICATED ON PLANS. TREE STUMPS SHALL EITHER BE REMOVED OR CHIPPED IN PLACE.
- 12. CUT TREES WITHIN THE DEFINED CLEARING LIMITS AND REMOVE CUT WOOD. CHIP BRUSH AND SLASH, STOCKPILE CHIPS FOR USE ONSITE OR REMOVE OFF-SITE.





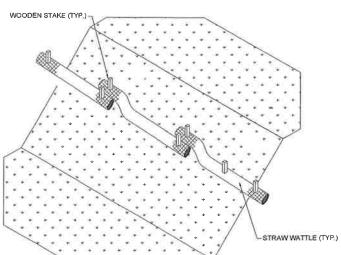
LONG AXIS OF STOCKPILE TO BE PERPENDICULAR TO CONTOUR





- 1. STABILIZATION FABRIC SHALL BE PLACED OVER THE ENTIRE ENTRANCE AREA PRIOR TO PLACING OF STONE, OVERLAP FABRIC PER MANUFACTURER'S SPECIFICATIONS.
- 2. ALL SURFACE WATER FLOWING OR DIVERTED TOWARDS THE CONSTRUCTION ENTRANCE SHALL BE PIPED BENEATH THE ENTRANCE ROAD.
- 3. WHEN EQUIPMENT WASHING IS REQUIRED IT SHALL BE DONE ON A SEPARATE AREA ADJACENT TO THE ENTRANCE ROAD AND STABILIZED WITH STONE FOLIPMENT WASHING WILL BE REQUIRED IF ROAD RECEIVES SIGNIFICANT SOILS OR DEBRIS ACCORDING TO JUDGMENT BY OWNER OR OWNER'S
- 4. KEEP ROADS CLEAR OF STONES, MUD, AND OTHER CONSTRUCTION DEBRIS. CLEAN PAVEMENT AS ACCUMULATIONS WARRANT AND AS ORDERED BY ENGINEER.
- 5. REMOVE SILT ACCUMULATIONS ROUTINELY AND DISPOSE OF PROPERLY SUCH THAT WATER QUALITY IS NOT IMPAIRED, DO NOT INTRODUCE SILT INTO DRAINAGE SYSTEM OR TOPSOIL/RESTORATION AREAS.





Weston & Sampson Idend Road Rocky Hill, Connecticut

R013 OLD FORGE ROAD ROCKY HILL, CT 06067

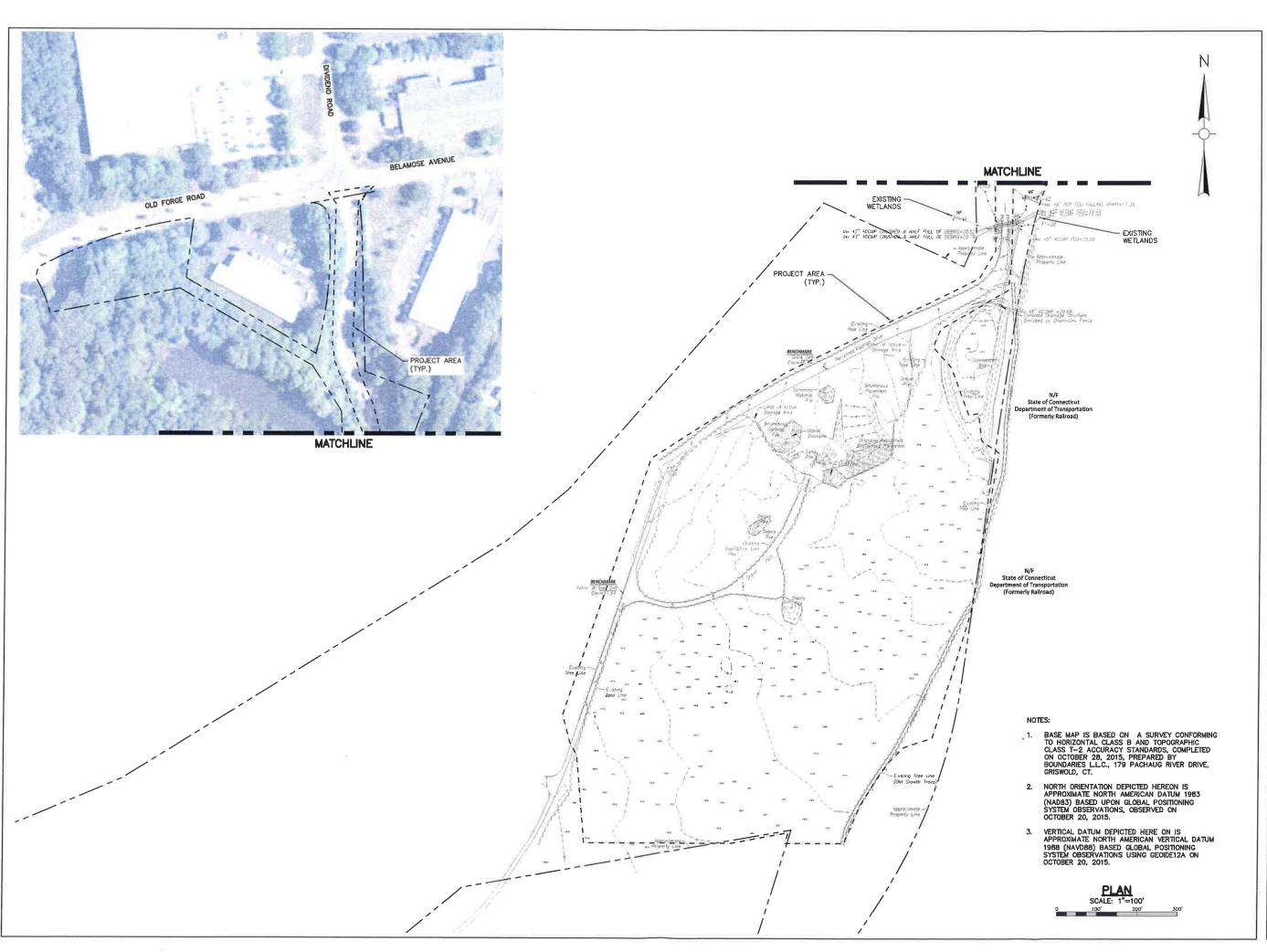
SolarCity



PERMIT PLANS JOB NO. 2150769

AS SHOW LEC JSP Approved By DCH

Drawing Title: DETAILS D-1



ROCKY H

ROCKY HILL SOLAR PROJEC



R013 OLD FORGE ROAD ROCKY HILL, CT 06067



9055 Climm/iew Way San Mairo, CA 94402 (550) 638-1028

## Weston&Sampson

273 Dividend Road Rocky HIII, Commodical (960) 513-1483 (900) Sampson www.westonandsampson.com



Revisions:

Rev Date Description



PERMIT PLANS JOB NO. 2150769

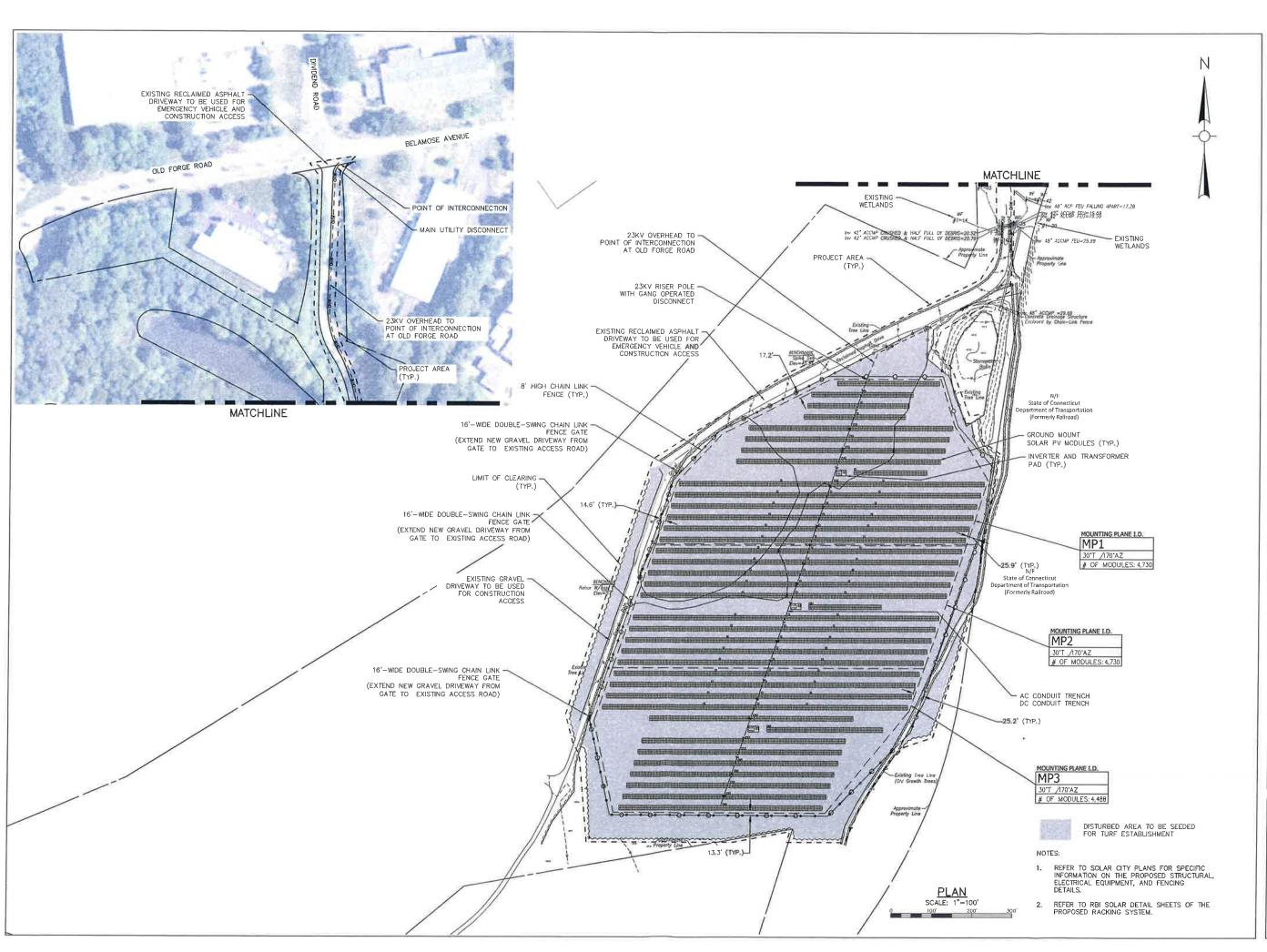
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| Reviewed By: | LEC        |
| Checked By:  | JSP        |
| Approved By: | RGT        |

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EXISTING CONDITIONS

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C-1



ROCKY HILL SOLAR PROJECT



R013 OLD FORGE ROAD ROCKY HILL, CT 06067



3055 Clearview Way San Maleo, CA 94402 (550) 538-1028 www.solarcity.com

## Weston & Sampson

273 Dividend Road Rocky HII, Connecticut (660) 513-1483 (600) Sampson www\_westonandsampson\_com



Revisions

Rev Date Description

Seat

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 03.16.2016

 Scale:
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 Drawn By:
 LEC

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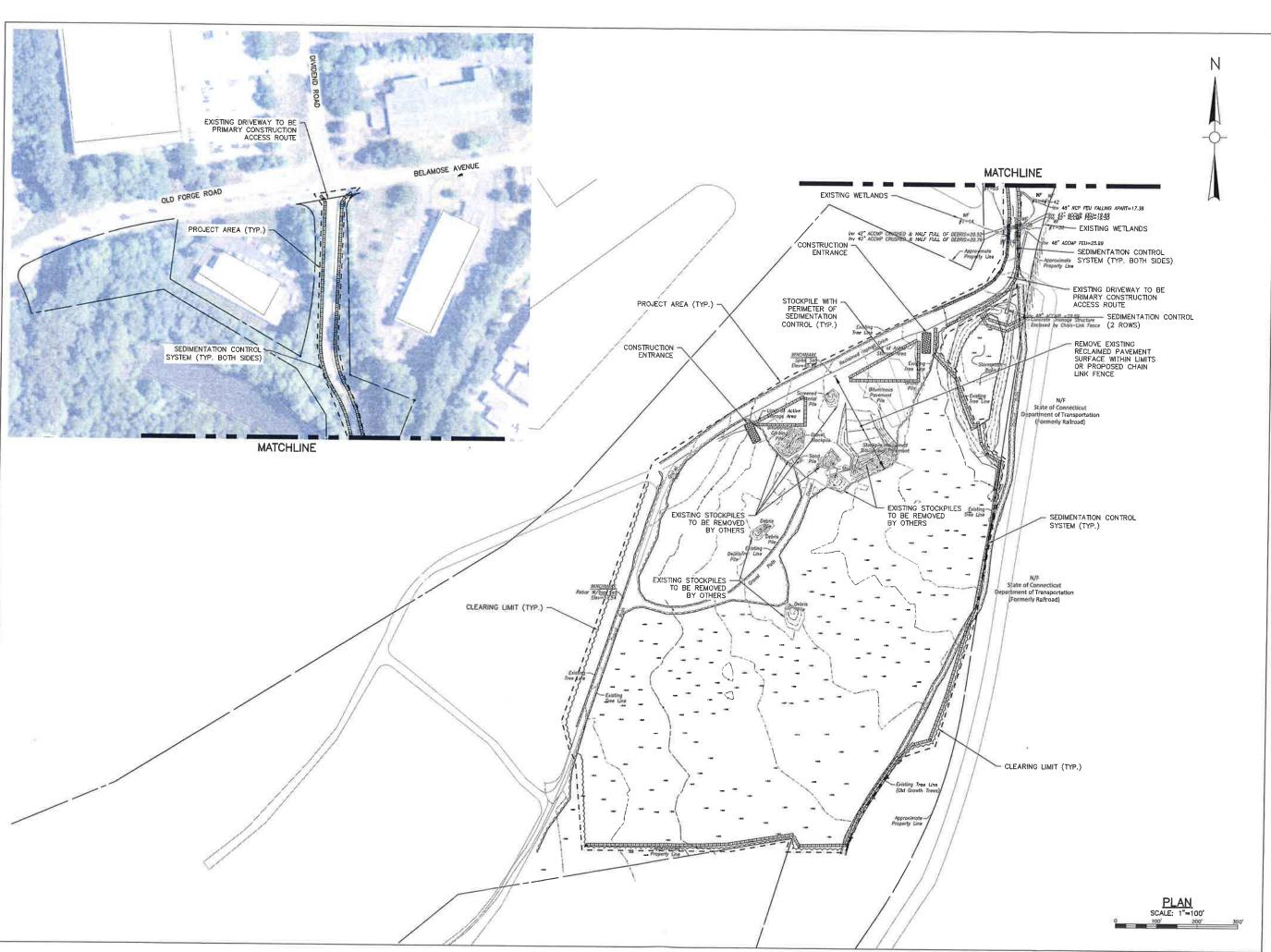
 Checked By:
 JSP

 Approved By:
 RGT

Drawing Title:

LAYOUT PLAN

**C-2** 



Project:

ROCKY HILL
SOLAR PROJECT



R013 OLD FORGE ROAD ROCKY HILL, CT 06067



3055 ClearNew Way San Malen, CA 94402 (550) 538-1028

## Wester & Sampson

273 Dividend Road Rocky Hill, Connecticut (660) 513-1483 (800) Sampson www.westonandsampson.com



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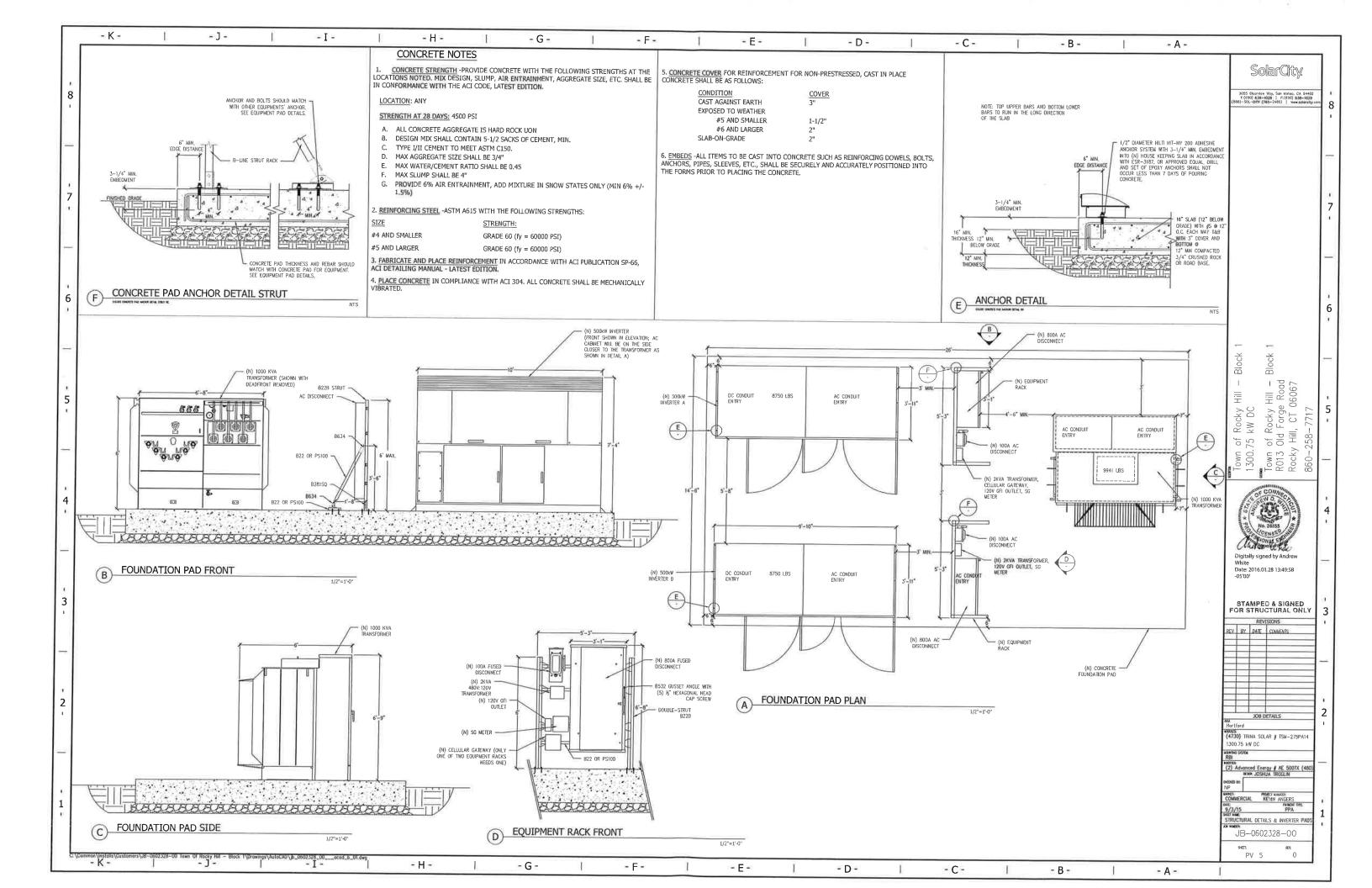
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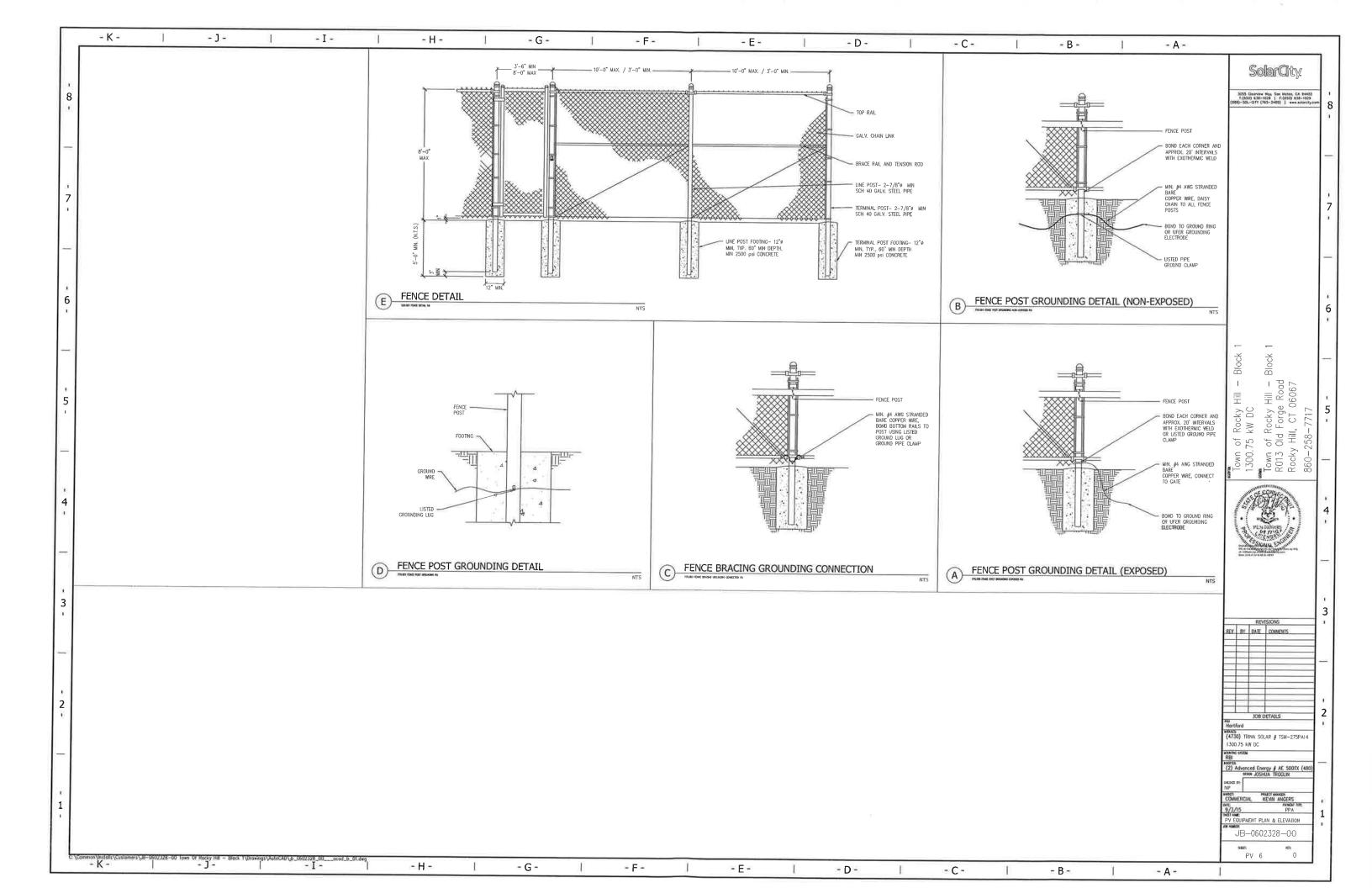
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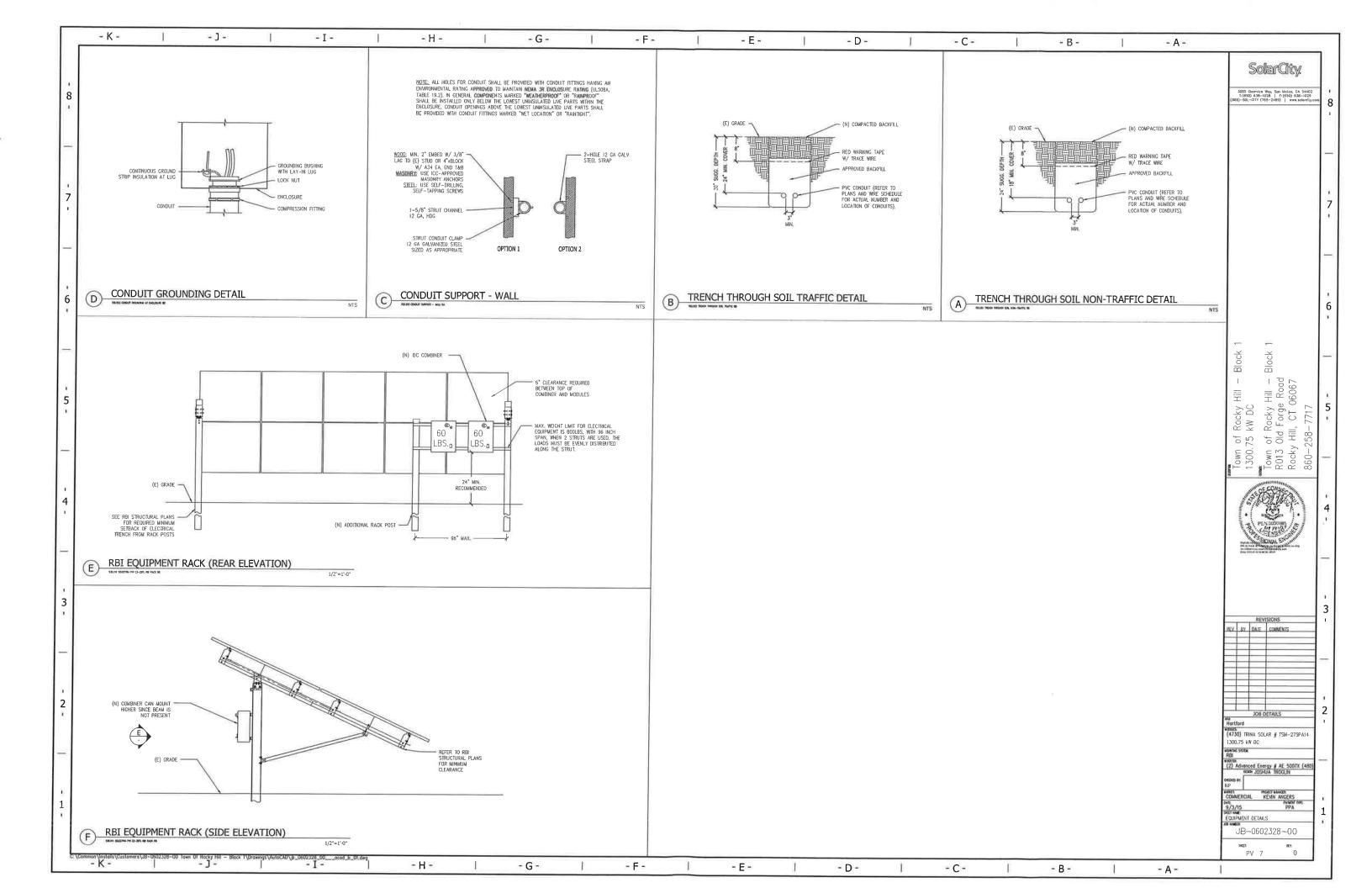
SEDIMENTATION AND EROSION CONTROL PLAN

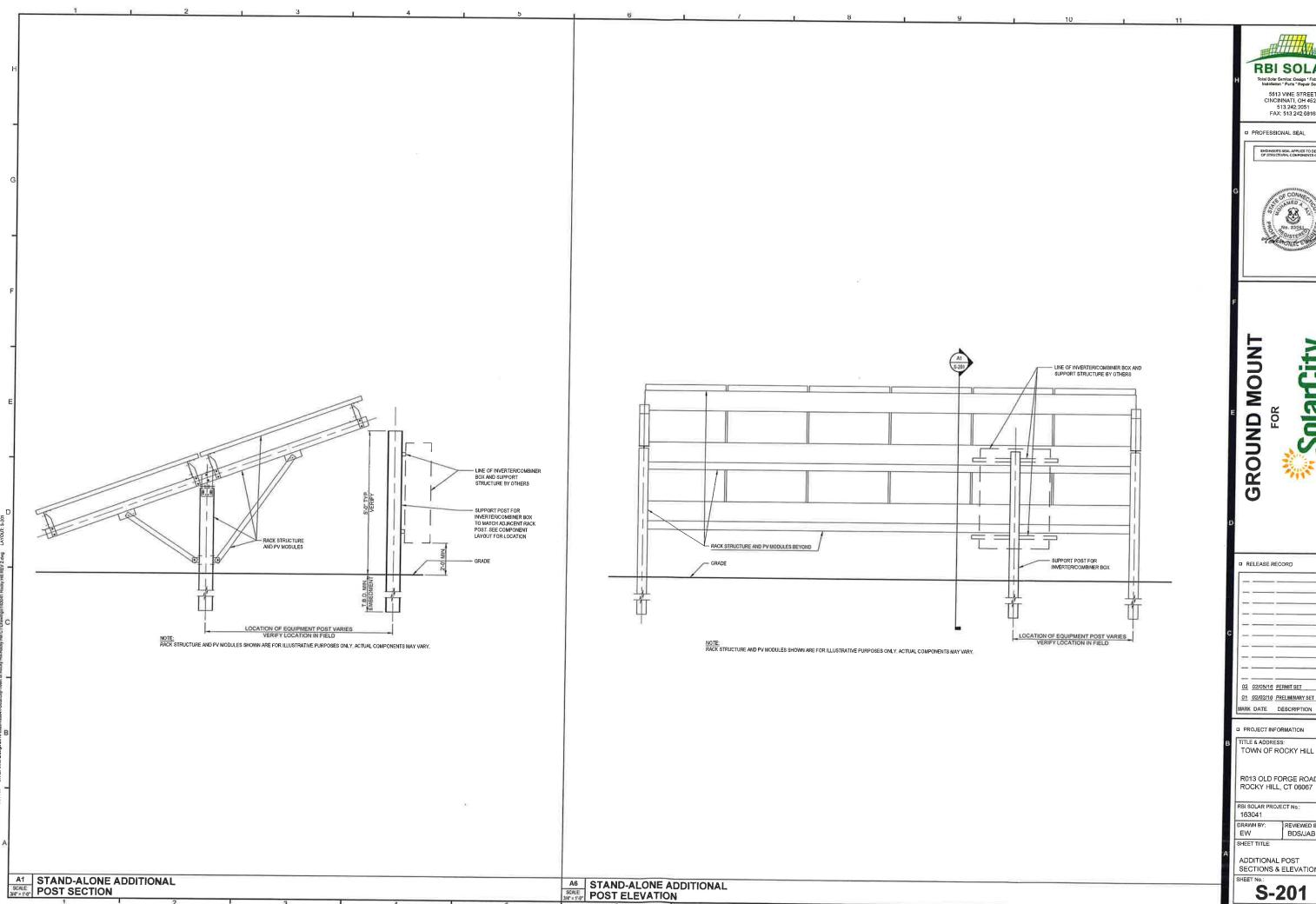
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C-3









**RBI SOLAR** 

5513 VINE STREET CINCINNATI, OH 45217 513 242 2051 FAX: 513 242 0816



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|   | 02 | 02/05/16 | PERMIT SET      |
|   | 01 | 02/02/16 | PRELIMINARY SET |

PROJECT INFORMATION

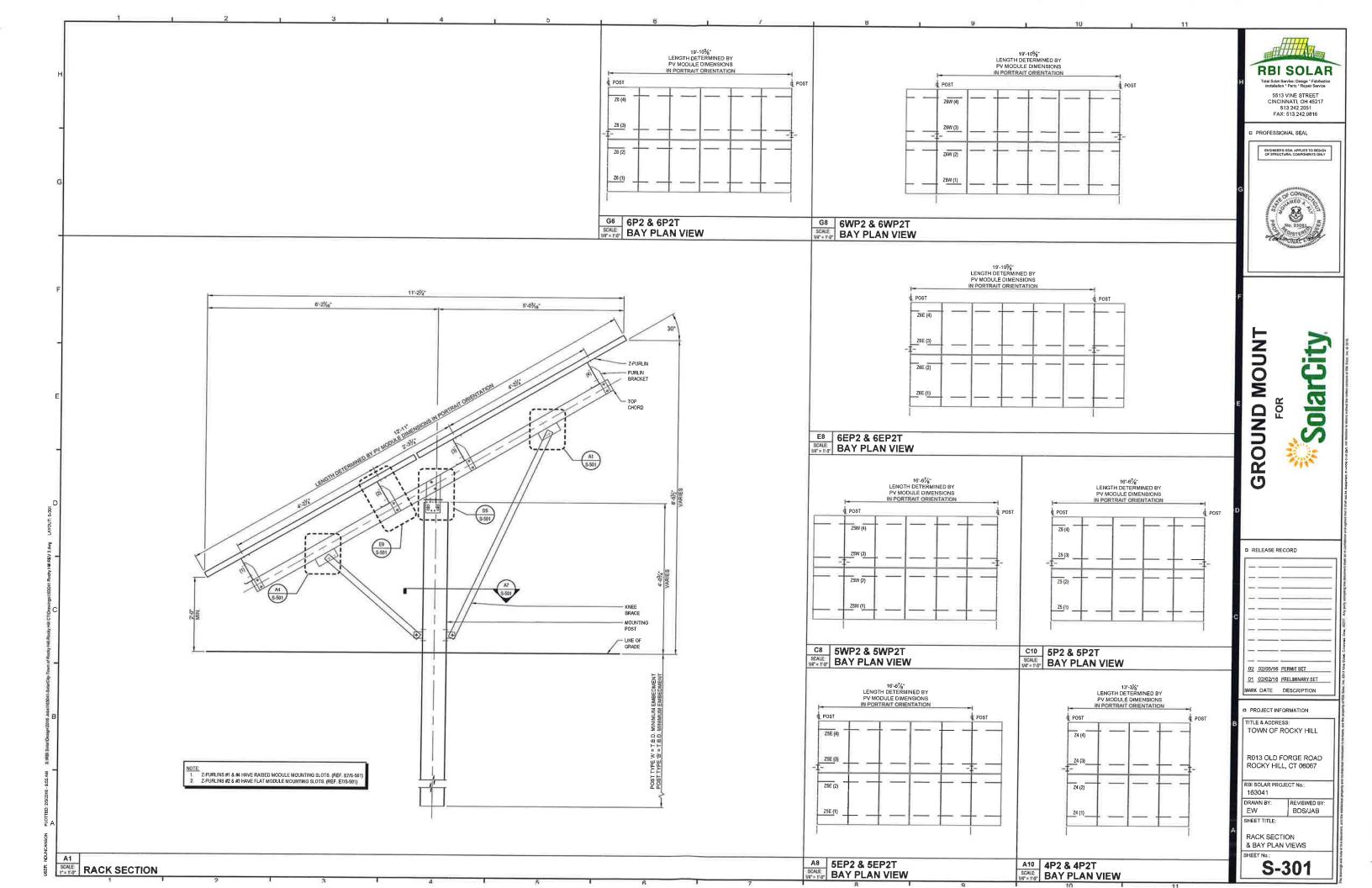
TITLE & ADDRESS: TOWN OF ROCKY HILL

R013 OLD FORGE ROAD ROCKY HILL, CT 06067

REVIEWED BY: BDS/JAB

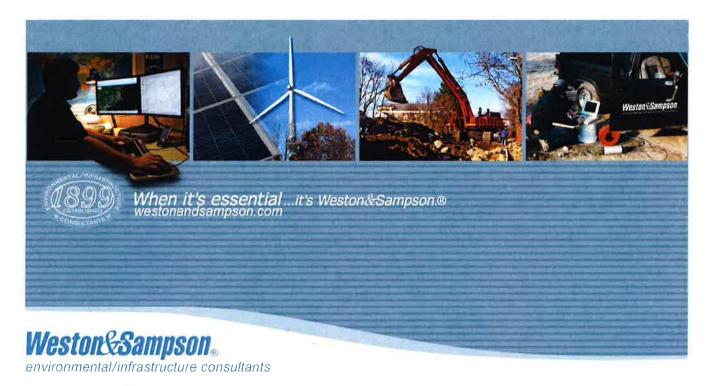
ADDITIONAL POST SECTIONS & ELEVATIONS

**S-201** 



# **ATTACHMENT 3**

# **ATTACHMENT 4**



273 Dividend Road, Rocky Hill, CT 06067 tel: 860-513-1473 fax: 860-513-1483

report



## Storm Water Management Report

**Prepared for:** SolarCity

Site Location: 13 Old Forge Road Rocky Hill, Connecticut

March 15, 2016

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#### **APPENDIX**

Location Map
Pre and Post Development Drainage Area Maps (DA-1 and DA-2)
TR-55 Data Sheet
Hydraflow Hydrograph Return Period Recap and Summary Reports
Hydraflow Hydrograph Reports

### INTRODUCTION

Weston & Sampson Engineers, Inc. (Weston & Sampson) was retained by Solar City to provide professional engineering services related to the proposed Rocky Hill Solar Project located on the Town of Rocky Hill owned property having driveway access from the intersection of Old Forge Road, Belamose Avenue, and Dividend Road. (See Location Map in the Appendix). This Stormwater Management Report has been prepared as part of the submittal to the Siting Council for a Certificate of Environmental Compatibility and Public Need (Declaratory Ruling).

#### 1.0 DESIGN METHODOLOGIES

Weston & Sampson estimated pre and post-development hydrographs using the hydrologic computer modeling program Hydraflow Hydrographs. The hydrologic methodology selected was the NRCS Method as detailed in Technical Release 55 (TR-55). Hydrographs were developed to determine peak rates of runoff for the 100-year design storm using a Type III (24-hour) distribution. The TR-55 method was used to develop times of concentration for multiple segment flow paths. Rainfall totals for Hartford County were taken from Appendix 6.B from the 2000 Connecticut DOT Drainage Manual.

According to NRCS Soils Mapping, the site is classified as "305 Udorthents- Pits complex, gravelly." The Udorthents was identified as Hydrologic Soil Group C by NRCS.

Runoff Curve Numbers (CN) used for pre-development analysis are as follows: 72 (cultivated fields), 89 (dirt/gravel pathways), 73 (woods), 79 (lawn), 71 (meadow), and 98 (reclaimed pavement). A weighted CN number was calculated based on these curve numbers and their associated drainage area.

Runoff Curve Numbers (CN) used for post-development analysis are as follows: 72 (cultivated fields), 89 (dirt/gravel pathways), 73 (woods), 79 (lawn), 71 (meadow), and 98 (impervious areas: reclaimed pavement and concrete utility pads). A weighted CN number was calculated based on these curve numbers and their associated drainage area. A tabulation of Runoff Curve Numbers and their associated subarea can be found in the Pre and Post Development Data Sheet in the Appendix section of this Stormwater Management Report.

An important aspect of this stormwater analysis is how the post-development peak flows are to be analyzed. The proposed development is for a raised solar panel system in which the lowest end of the panel is located approximately 3' off of existing grade. There is little to no grading proposed for this project. Solar panels shall be mounted to a racking system supported by posts driven into existing soil. Posts are to be designed by the manufacturer and will likely be steel H piles. Each array will be supported by a post at each end. The number panels per array and dimension between posts shall be designed by the manufacturer. The footprint of each post is negligible and will not be considered for impervious coverage.

The areas below and between the solar panels shall be seeded for turf establishment. This also shall be apply to the development areas beyond the solar arrays within the proposed security fence enclosure. Under this proposed design, stormwater runoff flow paths shall remain unchanged from pre to post-development conditions. This post-development analysis is also consistent with other analyses performed for similar raised panel photovoltaic systems throughout the country in which the post-development flow path(s) remain essentially unchanged from that of pre-development.

#### 2.0 PRE-DEVELOPMENT SITE CONDITIONS

The project site has a total area of approximately 98.0 acres. The Pre-Developed Drainage Area can be seen on the Pre-Developed Drainage Area Plan (DA-1). This area consists of a combination of wooded areas, cultivated fields, bare earth/dirt areas, gravel driveways, reclaimed pavement driveways, and a high grass meadow area where an existing stormwater basin is located at the lowest elevation of the watershed. There is an outlet control structure which mitigates the peak rate of runoff from the watershed area and ultimately discharges to an existing wetland area further north via a 48" RC pipe. The discharge point used in this analysis will be located in front of the existing outlet control structure. A time of concentration was calculated for the drainage area and used for calculation of a pre-development hydrograph.

A summary of the pre-development characteristics and peak runoff estimates can be seen in Tables 1 and 2. (Refer to the Appendix for detailed Hydrograph Reports)

#### 3.0 POST-DEVELOPMENT SITE CONDITIONS

For the proposed development, access to the development will be made using existing reclaimed pavement and gravel roadways. No additional roadways or improvements to existing roadways are proposed at this time. As mentioned previously, the entire PV development area within the proposed fencing will be seeded for turf establishment to control erosion and sediment transport as well as maintain the peak rate of runoff as close to existing as possible. Tree clearing will be performed only to the minimum extent required to prevent shading of the solar arrays. There is no regrading proposed for the solar development, only as required to prevent localized ponding of stormwater runoff and ensure that existing drainage patterns are maintained. All electrical conduits shall be constructed below grade and the interconnection to the existing distribution system shall be made at the intersection of Old Forge Road, Belamose Avenue, and Dividend Road.

Table 1
Drainage Area Characteristics

| Area<br>(Acres) | %<br>Impervious<br>(Pre) | %<br>Impervious<br>(Post) | CN<br>(Pre) | CN<br>(Post) |  |
|-----------------|--------------------------|---------------------------|-------------|--------------|--|
| 97.9            | 3.06                     | 0.7                       | 81          | 81           |  |

Stormwater runoff generally travels from the southwestern corner to the existing stormwater basin in the northeastern corner of the site. The runoff initially flows as sheet flow and then becomes shallow concentrated flow for the remainder of the distance. The stormwater eventually makes its way to the existing outlet control structure at the low point of the basin and it is at this point that the peak rate of runoff is determined and compared with that of predevelopment. FEMA flood mapping has been reviewed and the proposed project does not fall within a 100-year flood zone boundary.

The capacity of the existing stormwater basin and 48" discharge pipe have not been evaluated as part of this stormwater evaluation. It is presumed that these stormwater management features have been sufficiently designed to manage the applicable design storms for the current watershed configuration, groundcover, and resulting peak rates of runoff.

A summary of the post-development peak flow rates for each Subarea is shown below in Table 2 along with a summary of pre-development peak flow rates. (Refer to the Appendix for detailed Hydrograph Reports)

Table 2
Pre and Post-Development Peak Flows

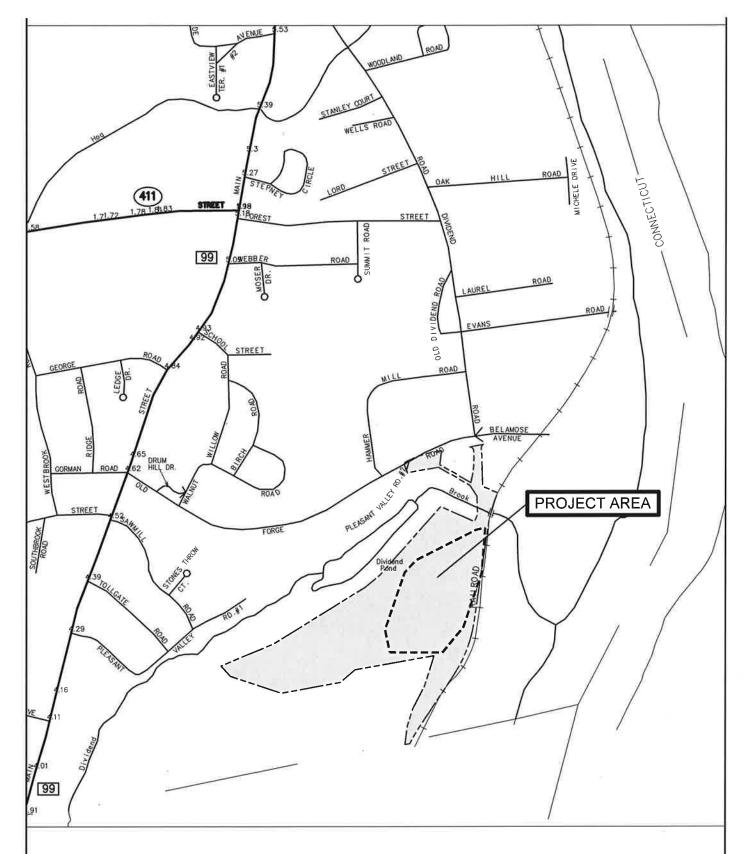
| 2-year, 24-hour<br>storm       |                                 | _                              |                                 |                                | 25-year, 24-<br>hour storm hour storm |                                |                                 | ear, 24-<br>storm              |                                 |
|--------------------------------|---------------------------------|--------------------------------|---------------------------------|--------------------------------|---------------------------------------|--------------------------------|---------------------------------|--------------------------------|---------------------------------|
| Peak<br>Flow<br>(cfs)<br>(Pre) | Peak<br>Flow<br>(cfs)<br>(Post) | Peak<br>Flow<br>(cfs)<br>(Pre) | Peak<br>Flow<br>(cfs)<br>(Post) | Peak<br>Flow<br>(cfs)<br>(Pre) | Peak<br>Flow<br>(cfs)<br>(Post)       | Peak<br>Flow<br>(cfs)<br>(Pre) | Peak<br>Flow<br>(cfs)<br>(Post) | Peak<br>Flow<br>(cfs)<br>(Pre) | Peak<br>Flow<br>(cfs)<br>(Post) |
| 47.5                           | 45.4                            | 158.8                          | 151.99                          | 249.4                          | 239.0                                 | 311.9                          | 299.1                           | 381.9                          | 366.4                           |

## 4.0 SUMMARY

Tables 1 and 2 demonstrate that there will be no negative stormwater impacts associated with the proposed solar PV development. The reduction in the percent of impervious area due to the reduction of reclaimed pavement combined with the addition of turf establishment within the solar PV development area and the resulting change in time of concentration results in a net decrease in the peak rate of runoff for post-development when compared with that of predevelopment.

## **APPENDIX**:

Location Map
Pre and Post Development Drainage Area Maps (DA-1 and DA-2)
TR-55 Data Sheet
Hydraflow Hydrograph Return Period Recap and Summary Reports
Hydraflow Hydrograph Reports



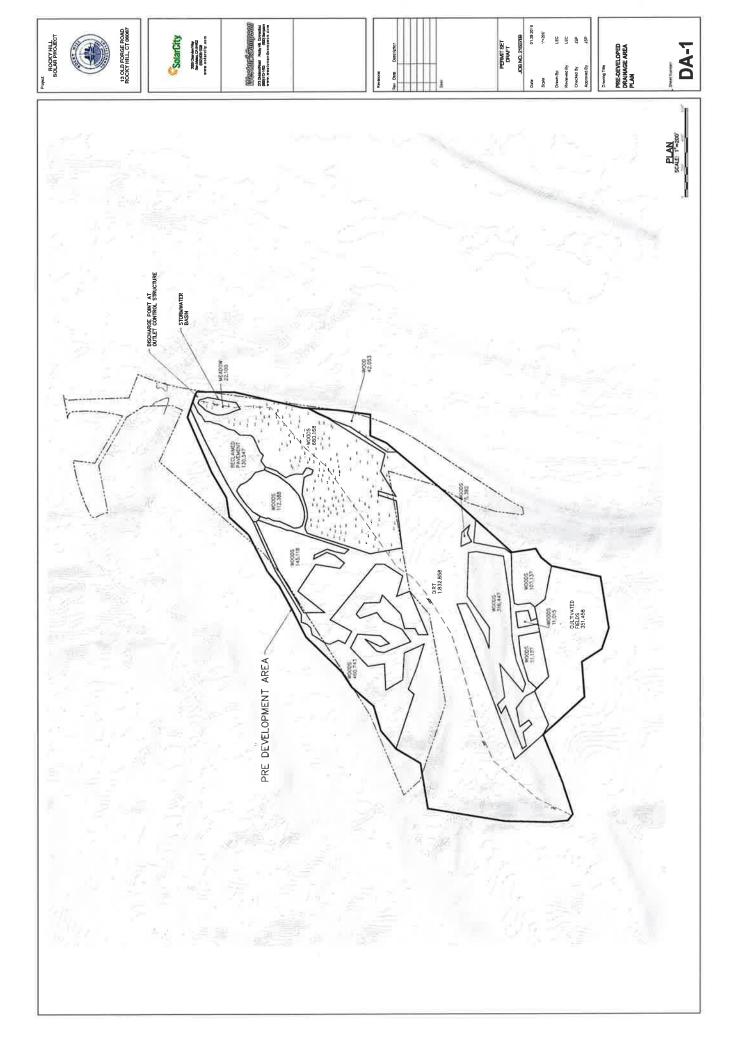
## FIGURE 1: LOCATION MAP

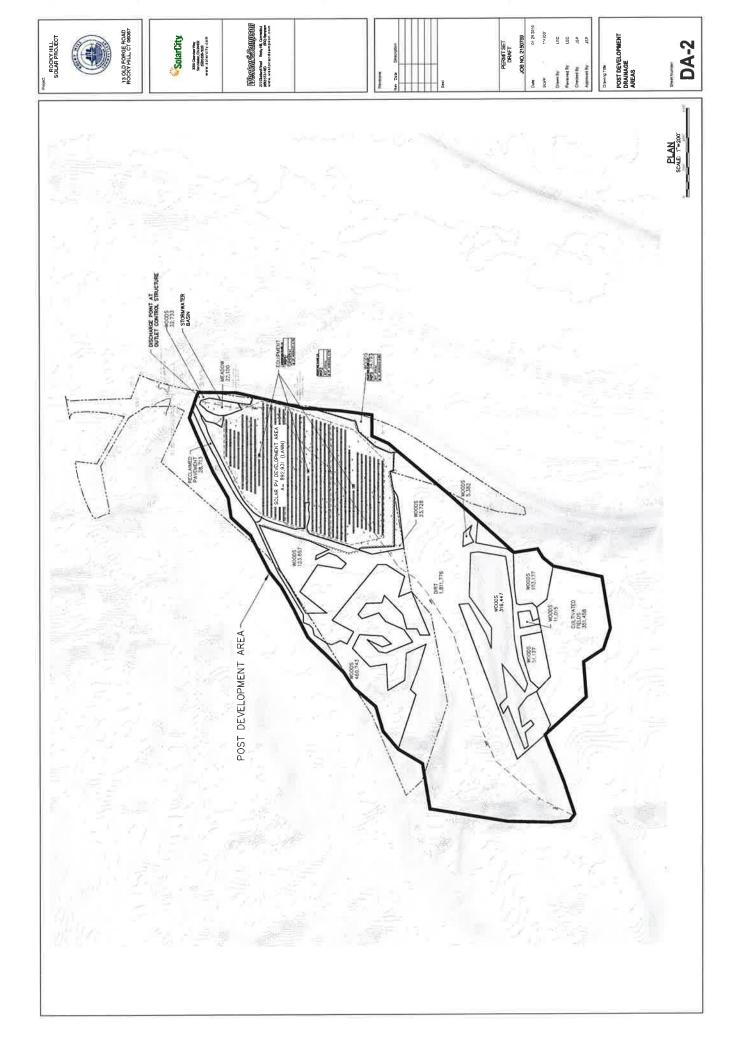
13 OLD FORGE ROAD, ROCKY HILL, CONNECTICUT

SCALE: 1"=1000'

SOURCE:

CONN DOT TRU MAP





SUBJECT

JOB NO.

Total

4,265,099

97.913

Solar City- Rocky Hill, CT

2150769

Pre & Post Drainage Areas

Weston&Sampson

SHEET NO. COMPUTED BY

1 OF LEC

DATE 1/26/2016

JSP DATE 1/26/2016

DATA SHEET FOR TR-55 METHOD STORM DRAINAGE DESIGN TIME OF CONCENTRATION- TR55 RUNOFF COEFFICIENT NODE AREA SLOPE COVER ELEV. DIFF. LENGTH Flow AREA AREA ACRES DESCRIPTION CN<sub>x</sub> п % value Type (S.F.) I.D. PRE-DEVELOPMENT 3230 0.011 sheet 44.251 Woods 73 55 260 21.15 Dirt Pre\_Dev 1,927,578 conc **Cultivated Fields** 581 4.24 351,458 8.068 72 36 849 unpaved 3745 conc 1,832,858 42.077 Dirt/Gravel 89 30 2559 1.17 paved 2.997 Reclaim Pave. 98 294 conc 130,547 414 2.42 unpaved 79 0 0.000 Lawn 0 Meadow 71 36 22,100 0.507 4,264,541 81 Total 97.900 0 POST-DEVELOPMENT Post\_Dev 1,162,362 26.684 Woods 73 1948 55 260 21.15 Dirt 0.011 sheet Cultivated Fields 72 581 4.24 conc 351,458 8.068 36 849 unpaved Dirt/Gravel 89 3691 1091 1,37 paved conc 1,806,395 41.469 15 Reclaim Pave/Equipment 98 conc 29,853 0.685 Pads 67 23.31 1882 1.24 unpaved 79 1619 892,931 20.499 Lawn (good C) 71 22,100 0.507 Meadow 36

81

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

| Hydrograph Return Period Recap | 1 |
|--------------------------------|---|
| 2 - Year<br>Summary Report     | 2 |
| 10 - Year<br>Summary Report    | 3 |
| 25 - Year<br>Summary Report    | 4 |
| 50 - Year<br>Summary Report    | 5 |
| 100 - Year<br>Summary Report   | 6 |

Hydrograph Return Period Recap Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

|    | Hydrograph Inflow |                      |         |       |   | Hydrograph |        |        |        |        |                  |
|----|-------------------|----------------------|---------|-------|---|------------|--------|--------|--------|--------|------------------|
| ). | type<br>(origin)  | hyd(s)               | 1-yr    | 2-уг  | 3-yr  | 5-yr       | 10-уг  | 25-уг  | 50-yr  | 100-yr | Description      |
|    | SCS Runoff        |                      |         | 47.49 | *********   | 24101112   | 158.76 | 249.42 | 311.90 | 381.94 | Pre Development  |
|    | SCS Runoff        | \$ <del>500000</del> | ROBBERG | 45.44 | HATE COMMITTEE OF THE PARTY OF |            | 151.99 | 239.04 | 299.07 | 366.39 | Post Development |
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|    |                   |                      |         |       |   |            |        |        |        |        |                  |
|    |                   |                      |         |       |   |            |        |        |        |        |                  |
|    | -                 |                      |         |       |   |            |        |        |        |        |                  |
|    |                   |                      |         |       |   |            |        |        |        |        |                  |
|    |                   |                      |         |       |   |            |        |        |        |        |                  |
|    |                   |                      |         |       |   |            |        |        |        |        | W                |
|    |                   |                      |         |       |   |            |        |        |        |        |                  |
|    |                   |                      |         |       |   |            |        |        |        |        |                  |
|    |                   |                      |         |       |   |            |        |        |        |        |                  |
|    |                   |                      |         |       |   |            |        |        |        |        |                  |

Proj. file: Pre\_Post Hydrograph\_RH.gpw

Friday, 01 / 29 / 2016

| Hyd.<br>No. | Hydrograph<br>type<br>(origin) | Peak<br>flow<br>(cfs) | Time<br>interval<br>(min) | Time to<br>Peak<br>(min) | Hyd.<br>volume<br>(cuft) | Inflow<br>hyd(s) | Maximum<br>elevation<br>(ft) | Total<br>strge used<br>(cuft) | _ Hydrograph<br>Description      |
|-------------|--------------------------------|-----------------------|---------------------------|--------------------------|--------------------------|------------------|------------------------------|-------------------------------|----------------------------------|
| 1 2         | SCS Runoff<br>SCS Runoff       | 47.49<br>45.44        | 2 2                       | 742<br>746               | 261,196<br>264,461       | 197944           |                              |                               | Pre Development Post Development |
|             |                                |                       |                           |                          |                          |                  |                              |                               | _                                |
|             |                                |                       | ×                         |                          |                          |                  |                              |                               |                                  |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                                  |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                                  |
| Pre         | e_Post Hydrog                  | <br>graph_RH          | .gpw                      |                          | Return P                 | eriod: 2 Ye      | ar                           | Friday, 01 /                  | 29 / 2016                        |

| Hyd.<br>No. | Hydrograph<br>type<br>(origin) | Peak<br>flow<br>(cfs) | Time<br>interval<br>(min) | Time to<br>Peak<br>(min) | Hyd.<br>volume<br>(cuft) | Inflow<br>hyd(s) | Maximum<br>elevation<br>(ft) | Total<br>strge used<br>(cuft) | Hydrograph<br>Description |
|-------------|--------------------------------|-----------------------|---------------------------|--------------------------|--------------------------|------------------|------------------------------|-------------------------------|---------------------------|
|             | SCS Runoff                     | 158.76                | 2                         | 740                      | 829,278                  | 000000V          | <del>XIIAANS</del> U         | S <u>318/275</u> 3            | Pre Development           |
| 2           | SCS Runoff                     | 151.99                | 2                         | 742                      | 839,644                  | 555555A          |                              |                               | Post Development          |
|             | ë'                             |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                | 6                     |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              | 20                            |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
| -<          |                                |                       |                           |                          |                          |                  |                              |                               | 4                         |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
| -           |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               | *                         |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
|             |                                |                       |                           |                          |                          |                  |                              |                               |                           |
| Pre         | _Post Hydrog                   | raph_RH               | l.gpw                     |                          | Return P                 | eriod: 10 Y      | 'ear                         | Friday, 01 /                  | 29 / 2016                 |

| Hyd.<br>No. | type          | Peak<br>flow<br>(cfs) | Time<br>interval<br>(min) | Peak       | Hyd.<br>volume<br>(cuft) | Inflow<br>hyd(s)    | Maximum<br>elevation<br>(ft) | Total<br>strge used<br>(cuft) | Hydrograph<br>Description        |
|-------------|---------------|-----------------------|---------------------------|------------|--------------------------|---------------------|------------------------------|-------------------------------|----------------------------------|
|             | SCS Runoff    | 249.42<br>239.04      | 2                         | 740<br>742 | 1,306,057<br>1,322,382   | ( <del>111111</del> |                              |                               | Pre Development Post Development |
|             |               |                       |                           |            |                          |                     |                              |                               |                                  |
|             |               |                       |                           |            |                          |                     |                              |                               |                                  |
|             |               |                       |                           |            |                          |                     |                              |                               |                                  |
|             |               |                       |                           |            |                          |                     |                              |                               |                                  |
|             |               |                       |                           |            |                          |                     |                              |                               |                                  |
|             |               |                       |                           |            |                          |                     |                              | ×                             |                                  |
|             |               |                       |                           |            | 's'                      |                     |                              |                               |                                  |
|             |               |                       |                           |            |                          |                     |                              |                               |                                  |
|             |               |                       |                           |            |                          |                     |                              |                               |                                  |
|             |               |                       |                           |            |                          |                     |                              |                               |                                  |
|             |               |                       |                           |            |                          |                     |                              |                               |                                  |
| Pre         | e_Post Hydrog | ]<br>graph_RF         | l.gpw                     |            | Return P                 | Period: 25 Y        | ear                          | Friday, 01 /                  | 29 / 2016                        |

| Hyd.<br>No. |                          | Peak<br>flow<br>(cfs) |       | Peak       | Hyd.<br>volume<br>(cuft) | Inflow<br>hyd(s) | Maximum<br>elevation<br>(ft) | Total<br>strge used<br>(cuft) | Hydrograph<br>Description        |
|-------------|--------------------------|-----------------------|-------|------------|--------------------------|------------------|------------------------------|-------------------------------|----------------------------------|
|             | SCS Runoff<br>SCS Runoff | 311.90<br>299.07      | 2     | 740<br>742 | 1,641,771<br>1,662,294   | :: <del></del>   |                              |                               | Pre Development Post Development |
|             |                          |                       |       |            |                          |                  | N2                           |                               |                                  |
|             |                          |                       |       |            |                          |                  | <b>1</b> 0                   |                               |                                  |
|             |                          |                       |       |            |                          |                  |                              |                               |                                  |
|             |                          | 30 E                  |       |            |                          |                  |                              |                               |                                  |
|             |                          |                       |       |            |                          |                  |                              |                               |                                  |
|             |                          |                       |       |            | ×                        |                  |                              |                               |                                  |
|             |                          |                       |       |            |                          |                  |                              |                               |                                  |
|             |                          |                       |       |            |                          |                  |                              |                               |                                  |
|             |                          |                       |       |            |                          |                  |                              |                               |                                  |
|             |                          |                       |       |            |                          |                  |                              |                               |                                  |
|             | 1                        |                       |       |            |                          |                  |                              |                               | -                                |
|             |                          |                       |       |            |                          |                  |                              |                               |                                  |
|             |                          |                       |       |            |                          |                  |                              |                               |                                  |
| Pre         | e_Post Hydrog            | raph_RH               | l.gpw |            | Return F                 | Period: 50 Y     | ′ear                         | Friday, 01 /                  | 29 / 2016                        |

| Hyd.<br>No. | Hydrograph<br>type<br>(origin) | Peak<br>flow<br>(cfs) | Time<br>interval<br>(min) | Time to<br>Peak<br>(min) | Hyd.<br>volume<br>(cuft) |             | Maximum<br>elevation<br>(ft) | Total<br>strge used<br>(cuft) | Hydrograph<br>Description        |
|-------------|--------------------------------|-----------------------|---------------------------|--------------------------|--------------------------|-------------|------------------------------|-------------------------------|----------------------------------|
| 1 2         | SCS Runoff<br>SCS Runoff       | 381.94<br>366.39      | 2                         | 740<br>742               | 2,024,122<br>2,049,422   |             |                              |                               | Pre Development Post Development |
|             |                                |                       |                           |                          |                          |             |                              |                               |                                  |
|             |                                |                       |                           |                          |                          |             |                              |                               |                                  |
|             |                                |                       |                           |                          |                          |             |                              |                               |                                  |
|             |                                |                       |                           |                          |                          |             |                              |                               |                                  |
|             |                                |                       |                           |                          | c                        |             |                              |                               |                                  |
|             |                                |                       |                           |                          |                          |             |                              |                               |                                  |
|             |                                |                       |                           |                          |                          |             |                              |                               | 9                                |
|             | ×                              |                       |                           |                          |                          |             |                              |                               |                                  |
|             |                                |                       |                           |                          |                          |             |                              |                               |                                  |
| Pre         | e_Post Hydro                   | graph_RF              | l.gpw                     |                          | Return F                 | Period: 100 | Year                         | Friday, 01 /                  | 29 / 2016                        |

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## **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

#### Hyd. No. 1

#### Pre Development

| Hydrograph type | = SCS Runoff | Peak discharge     | = 47.49 cfs    |
|-----------------|--------------|--------------------|----------------|
| Storm frequency | = 2 yrs      | Time to peak       | = 12.37 hrs    |
| Time interval   | = 2 min      | Hyd. volume        | = 261,196 cuft |
| Drainage area   | = 97.910 ac  | Curve number       | = 81.000*      |
| Basin Slope     | = 0.0 %      | Hydraulic length   | = 0 ft         |
| Tc method       | = TR55       | Time of conc. (Tc) | = 27.4 min     |
| Total precip.   | = 2.20 in    | Distribution       | = Type III     |
| Storm duration  | = 24 hrs     | Shape factor       | = 484          |

<sup>\*</sup> Composite (Area/CN) =  $[(44.250 \times 73) + (8.070 \times 72) + (42.080 \times 89) + (3.000 \times 98) + (0.510 \times 71)] / 97.910$ 

#### **Hydrograph Discharge Table**

( Printed values >= 1.00% of Qp.)

| Time (<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|--------------|-----------------|----------------|-----------------|
| 11.07          | 0.475           | 11.67          | 2.825           | 12.27        | 43.47           | 12.87          | 18.52           |
| 11.10          | 0.537           | 11.70          | 3.204           | 12.30        | 45.81           | 12.90          | 17.15           |
| 11.13          | 0.604           | 11.73          | 3.671           | 12.33        | 47.07           | 12.93          | 15.93           |
| 11.17          | 0.675           | 11.77          | 4.245           | 12.37        | 47.49           | 12.97          | 14.86           |
| 11.20          | 0.750           | 11.80          | 4.947           | 12.40        | 47.32           | 13.00          | 13.92           |
| 11.23          | 0.831           | 11.83          | 5.795           | 12.43        | 46.73           | 13.03          | 13.10           |
| 11.27          | 0.917           | 11.87          | 6.799           | 12.43        | 45.73           | 13.07          | 12.40           |
| 11.30          | 1.010           | 11.90          | 7.974           | 12.47        | 44.33           | 13.10          | 11.80           |
| 11.33          | 1.110           | 11.93          | 9.400           | 12.53        | 42.56           | 13.13          | 11.29           |
| 11.37          | 1.217           | 11.97          | 11.24           | 12.57        | 40.46           | 13.17          | 10.86           |
| 11.40          | 1.333           | 12.00          | 13.72           | 12.60        | 38.09           | 13.20          | 10.50           |
| 11.43          | 1.456           | 12.03          | 16.85           | 12.63        | 35.50           | 13.23          | 10.19           |
| 11.47          | 1.588           | 12.07          | 20.47           | 12.67        | 32.75           | 13.27          | 9.930           |
| 11.50          | 1.730           | 12.10          | 24.36           | 12.70        | 29.90           | 13.30          | 9.692           |
| 11.53          | 1.883           | 12.13          | 28.35           | 12.73        | 27.05           | 13.33          | 9.475           |
| 11.57          | 2.059           | 12.17          | 32.38           | 12.77        | 24.37           | 13.37          | 9.275           |
| 11.60          | 2.267           | 12.20          | 36.40           | 12.80        | 22.03           | 13.40          | 9.093           |
| 11.63          | 2.518           | 12.23          | 40.20           | 12.83        | 20.11           | 13.43          | 8.927           |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) |    | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|--------------|-----------------|----|----------------|-----------------|
| 13.47        | 8.775           | 14.37          | 6.345           | 15.27        | 5.081           |    | 16.17          | 3.803           |
| 13.50        | 8.636           | 14.40          | 6.283           | 15.30        | 5.035           |    | 16.20          | 3.759           |
| 13.53        | 8.509           | 14.43          | 6.225           | 15.33        | 4.989           |    | 16.23          | 3.716           |
| 13.57        | 8.393           | 14.47          | 6.169           | 15.37        | 4.943           |    | 16.27          | 3.675           |
| 13.60        | 8.285           | 14.50          | 6.116           | 15.40        | 4.897           |    | 16.30          | 3.637           |
| 13.63        | 8.185           | 14.53          | 6.065           | 15.43        | 4.850           |    | 16.33          | 3.600           |
| 13.67        | 8.091           | 14.57          | 6.016           | 15.47        | 4.804           |    | 16.37          | 3.566           |
| 13.70        | 8.001           | 14.60          | 5.969           | 15.50        | 4.757           |    | 16.40          | 3.534           |
| 13.73        | 7.915           | 14.63          | 5.923           | 15.53        | 4.710           |    | 16.43          | 3.504           |
| 13.77        | 7.830           | 14.67          | 5.878           | 15.57        | 4.663           |    | 16.47          | 3.475           |
| 13.80        | 7.746           | 14.70          | 5.834           | 15.60        | 4.616           | 51 | 16.50          | 3.448           |
| 13.83        | 7.660           | 14.73          | 5.791           | 15.63        | 4.569           |    | 16.53          | 3.422           |
| 13.87        | 7.574           | 14.77          | 5.748           | 15.67        | 4.522           |    | 16.57          | 3.397           |
| 13.90        | 7.488           | 14.80          | 5.704           | 15.70        | 4.474           |    | 16.60          | 3.373           |
| 13.93        | 7.401           | 14.83          | 5.661           | 15.73        | 4.426           |    | 16.63          | 3.351           |
| 13.97        | 7.313           | 14.87          | 5.618           | 15.77        | 4.379           |    | 16.67          | 3.328           |
| 14.00        | 7.225           | 14.90          | 5.574           | 15.80        | 4.331           |    | 16.70          | 3.307           |
| 14.03        | 7.136           | 14.93          | 5.530           | 15.83        | 4.283           |    | 16.73          | 3.286           |
| 14.07        | 7.048           | 14.97          | 5.486           | 15.87        | 4.234           |    | 16.77          | 3.264           |
| 14.10        | 6.961           | 15.00          | 5.441           | 15.90        | 4.186           |    | 16.80          | 3.243           |
| 14.13        | 6.874           | 15.03          | 5.397           | 15.93        | 4.138           |    | 16.83          | 3.222           |
| 14.17        | 6.790           | 15.07          | 5.352           | 15.97        | 4.089           |    | 16.87          | 3.201           |
| 14.20        | 6.707           | 15.10          | 5.307           | 16.00        | 4.040           |    | 16.90          | 3.180           |
| 14.23        | 6.628           | 15.13          | 5.263           | 16.03        | 3.992           |    | 16.93          | 3.159           |
| 14.27        | 6.551           | 15.17          | 5.217           | 16.07        | 3.944           |    | 16.97          | 3.138           |
| 14.30        | 6.479           | 15.20          | 5.172           | 16.10        | 3.896           |    | 17.00          | 3.117           |
| 14.33        | 6.410           | 15.23          | 5.127           | 16.13        | 3.849           |    | 17.03          | 3.095           |

| Time<br>(hrs | Outflow cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time (hrs | Outflow<br>cfs) |
|--------------|--------------|----------------|-----------------|----------------|-----------------|-----------|-----------------|
| 17.07        | 3.074        | 17.97          | 2.486           | 18.87          | 2.132           | 19.77     | 1.959           |
| 17.10        | 3.053        | 18.00          | 2.464           | 18.90          | 2.126           | 19.80     | 1.952           |
| 17.13        | 3.031        | 18.03          | 2.442           | 18.93          | 2.120           | 19.83     | 1.946           |
| 17.17        | 3.010        | 18.07          | 2.420           | 18.97          | 2.113           | 19.87     | 1.939           |
| 17.20        | 2.988        | 18.10          | 2.398           | 19.00          | 2.107           | 19.90     | 1.933           |
| 17.23        | 2.967        | 18.13          | 2.377           | 19.03          | 2.100           | 19.93     | 1.926           |
| 17.27        | 2.945        | 18.17          | 2.357           | 19.07          | 2.094           | 19.97     | 1.919           |
| 17.30        | 2.924        | 18.20          | 2.337           | 19.10          | 2.088           | 20.00     | 1.913           |
| 17.33        | 2.902        | 18.23          | 2.318           | 19.13          | 2.081           | 20.03     | 1.906           |
| 17.37        | 2.881        | 18.27          | 2.301           | 19.17          | 2.075           | 20.07     | 1.900           |
| 17.40        | 2.859        | 18.30          | 2.285           | 19.20          | 2.068           | 20.10     | 1.893           |
| 17.43        | 2.837        | 18.33          | 2.270           | 19.23          | 2.062           | 20.13     | 1.887           |
| 17.47        | 2.816        | 18.37          | 2.256           | 19.27          | 2.056           | 20.17     | 1.880           |
| 17.50        | 2.794        | 18.40          | 2.243           | 19.30          | 2.049           | 20.20     | 1.873           |
| 17.53        | 2.772        | 18.43          | 2.231           | 19.33          | 2.043           | 20.23     | 1.867           |
| 17.57        | 2.750        | 18.47          | 2.221           | 19.37          | 2.036           | 20.27     | 1.860           |
| 17.60        | 2.728        | 18.50          | 2.211           | 19.40          | 2.030           | 20.30     | 1.854           |
| 17.63        | 2.707        | 18.53          | 2.202           | 19.43          | 2.023           | 20.33     | 1.847           |
| 17.67        | 2.685        | 18.57          | 2.193           | 19.47          | 2.017           | 20.37     | 1.840           |
| 17.70        | 2.663        | 18.60          | 2.185           | 19.50          | 2.011           | 20.40     | 1.834           |
| 17.73        | 2.641        | 18.63          | 2.178           | 19.53          | 2.004           | 20.43     | 1.827           |
| 17.77        | 2.619        | 18.67          | 2.171           | 19.57          | 1.998           | 20.47     | 1.820           |
| 17.80        | 2.597        | 18.70          | 2.164           | 19.60          | 1.991           | 20.50     | 1.814           |
| 17.83        | 2.575        | 18.73          | 2.158           | 19.63          | 1.985           | 20.53     | 1.807           |
| 17.87        | 2.553        | 18.77          | 2.151           | 19.67          | 1.978           | 20.57     | 1.801           |
| 17.90        | 2.530        | 18.80          | 2.145           | 19.70          | 1.972           | 20.60     | 1.794           |
| 17.93        | 2.508        | 18.83          | 2.139           | 19.73          | 1.965           | 20.63     | 1.787           |

Continuos on nout noso

| Time (<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time ·<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|----------------|-----------------|--------------|-----------------|
| 20.67          | 1.781           | 21.57          | 1.598           | 22.47          | 1.682           | 23.37        | 1.389           |
| 20.70          | 1.774           | 21.60          | 1.592           | 22.50          | 1.664           | 23.40        | 1.384           |
| 20.73          | 1.767           | 21.63          | 1.585           | 22.53          | 1.645           | 23.43        | 1.379           |
| 20.77          | 1.760           | 21.67          | 1.578           | 22.57          | 1.626           | 23.47        | 1.373           |
| 20.80          | 1.754           | 21.70          | 1.571           | 22.60          | 1.606           | 23.50        | 1.368           |
| 20.83          | 1.747           | 21.73          | 1.564           | 22.63          | 1.586           | 23.53        | 1.363           |
| 20.87          | 1.740           | 21.77          | 1.557           | 22.67          | 1.565           | 23.57        | 1.358           |
| 20.90          | 1.734           | 21.80          | 1.551           | 22.70          | 1.544           | 23.60        | 1.353           |
| 20.93          | 1.727           | 21.83          | 1.544           | 22.73          | 1.522           | 23.63        | 1.347           |
| 20.97          | 1.720           | 21.87          | 1.537           | 22.77          | 1.500           | 23.67        | 1.342           |
| 21.00          | 1.713           | 21.90          | 1.530           | 22.80          | 1.477           | 23.70        | 1.337           |
| 21.03          | 1.707           | 21.93          | 1.523           | 22.83          | 1.471           | 23.73        | 1.332           |
| 21.07          | 1.700           | 21.97          | 1.516           | 22.87          | 1.466           | 23.77        | 1.327           |
| 21.10          | 1.693           | 22.00          | 1.509           | 22.90          | 1.461           | 23.80        | 1.321           |
| 21.13          | 1.687           | 22.03          | 1.533           | 22.93          | 1.456           | 23.83        | 1.316           |
| 21.17          | 1.680           | 22.07          | 1.559           | 22.97          | 1.451           | 23.87        | 1.311           |
| 21.20          | 1.673           | 22.10          | 1.585           | 23.00          | 1.446           | 23.90        | 1.306           |
| 21.23          | 1.666           | 22.13          | 1.612           | 23.03          | 1.441           | 23.93        | 1.300           |
| 21.27          | 1.659           | 22.17          | 1.640           | 23.07          | 1.435           | 23.97        | 1.295           |
| 21.30          | 1.653           | 22.20          | 1.670           | 23.10          | 1.430           | 24.00        | 1.290           |
| 21.33          | 1.646           | 22.23          | 1.700           | 23.13          | 1.425           | 24.03        | 1.273           |
| 21.37          | 1.639           | 22.27          | 1.732           | 23.17          | 1.420           | 24.07        | 1.245           |
| 21.40          | 1.632           | 22.30          | 1.764           | 23.20          | 1.415           | 24.10        | 1.206           |
| 21.43          | 1.626           | 22.33          | 1.749           | 23.23          | 1.410           | 24.13        | 1.155           |
| 21.47          | 1.619           | 22.37          | 1.733           | 23.27          | 1.404           | 24.17        | 1.094           |
| 21.50          | 1.612           | 22.40          | 1.716           | 23.30          | 1.399           | 24.20        | 1.021           |
| 21.53          | 1.605           | 22.43          | 1.699           | 23.33          | 1.394           | 24.23        | 0.937           |

| Time (<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|
| 24.27          | 0.841           |
| 24.30          | 0.735           |
| 24.33          | 0.636           |
| 24.37          | 0.545           |

...End

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

**Hyd. No. 1**Pre Development

| Description   | <u>A</u>                                       |   | <u>B</u>                              |   | <u>C</u>                         |   | <u>Totals</u> |
|---|--|---|---------------------------------------|---|----------------------------------|---|---------------|
| Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)                            | = 0.011<br>= 260.0<br>= 3.20<br>= 21.15        |   | 0.011<br>0.0<br>0.00<br>0.00          |   | 0.011<br>0.0<br>0.00<br>0.00     |   |               |
| Travel Time (min)   | = 1.01   | + | 0.00                                  | + | 0.00                             | = | 1.01          |
| Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)        | = 849.00<br>= 4.24<br>= Unpaved<br>=3.32       | d | 2559.00<br>1.17<br>Paved<br>2.20      |   | 414.00<br>2.42<br>Unpave<br>2.51 | d |               |
| Travel Time (min)   | = 4.26   | + | 19.40                                 | + | 2.75                             | = | 26.40         |
| Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) | = 0.00<br>= 0.00<br>= 0.00<br>= 0.015<br>=0.00 |   | 0.00<br>0.00<br>0.00<br>0.015<br>0.00 |   | 0.00<br>0.00<br>0.00<br>0.015    |   |               |
| Flow length (ft)  | ({0})0.0                                       |   | 0.0                                   |   | 0.0                              |   |               |
| Travel Time (min)   | = 0.00   | + | 0.00                                  | + | 0.00                             | = | 0.00          |
| Total Travel Time, Tc   |  |   |                                       |   |                                  |   |               |

## **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

#### Hyd. No. 2

#### Post Development

| Hydrograph type | = SCS Runoff | Peak discharge     | = 45.44 cfs    |
|-----------------|--------------|--------------------|----------------|
| Storm frequency | = 2 yrs      | Time to peak       | = 12.43 hrs    |
| Time interval   | = 2 min      | Hyd. volume        | = 264,461 cuft |
| Drainage area   | = 97.910 ac  | Curve number       | = 81.000*      |
| Basin Slope     | = 0.0 %      | Hydraulic length   | = 0 ft         |
| Tc method       | = TR55       | Time of conc. (Tc) | = 30.4 min     |
| Total precip.   | = 2.20 in    | Distribution       | = Type III     |
| Storm duration  | = 24 hrs     | Shape factor       | = 484          |

<sup>\*</sup> Composite (Area/CN) =  $[(26.680 \times 73) + (8.070 \times 72) + (41.470 \times 89) + (0.685 \times 98) + (20.499 \times 79) + (0.510 \times 71)] / 97.910$ 

#### **Hydrograph Discharge Table**

( Printed values >= 1,00% of Qp.)

| Time (<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|-----------------|
| 11.10          | 0.473           | 11.70          | 2.924           | 12.30          | 41.53           | 12.90          | 20.07           |
| 11.13          | 0.535           | 11.73          | 3.331           | 12.33          | 43.65           | 12.93          | 18.47           |
| 11.17          | 0.601           | 11.77          | 3.827           | 12.37          | 44.89           | 12.97          | 17.14           |
| 11.20          | 0.672           | 11.80          | 4.428           | 12.40          | 45.42           | 13.00          | 15.98           |
| 11.23          | 0.748           | 11.83          | 5.155           | 12.43          | 45.44           | 13.03          | 14.94           |
| 11.27          | 0.829           | 11.87          | 6.022           | 12.47          | 45.09           | 13.07          | 14.02           |
| 11.30          | 0.917           | 11.90          | 7.041           | 12.50          | 44.37           | 13.10          | 13.20           |
| 11.33          | 1.011           | 11.93          | 8.281           | 12.53          | 43.30           | 13.13          | 12.50           |
| 11.37          | 1.112           | 11.97          | 9.879           | 12.57          | 41.91           | 13.17          | 11.88           |
| 11.40          | 1.220           | 12.00          | 12.01           | 12.60          | 40.24           | 13.20          | 11.36           |
| 11.43          | 1.336           | 12.03          | 14.70           | 12.63          | 38.33           | 13.23          | 10.91           |
| 11.47          | 1.460           | 12.07          | 17.81           | 12.67          | 36.21           | 13.27          | 10.54           |
| 11.50          | 1.592           | 12.10          | 21.16           | 12.70          | 33.93           | 13.30          | 10.22           |
| 11.53          | 1.736           | 12.13          | 24.63           | 12.73          | 31.53           | 13.33          | 9.956           |
| 11.57          | 1.899           | 12.17          | 28.18           | 12.77          | 29.08           | 13.37          | 9.727           |
| 11.60          | 2.089           | 12.20          | 31.75           | 12.80          | 26.61           | 13.40          | 9.521           |
| 11.63          | 2.316           | 12.23          | 35.28           | 12.83          | 24.21           | 13.43          | 9.330           |
| 11.67          | 2.590           | 12.27          | 38.63           | 12.87          | 21.99           | 13.47          | 9.154           |
|                |                 |                |                 |                |                 |                |                 |

| Time<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow cfs) | Time<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|--------------|-----------------|--------------|--------------|--------------|-----------------|
| 13.50        | 8.992           | 14.40        | 6.459           | 15.30        | 5.159        | 16.20        | 3.869           |
| 13.53        | 8.842           | 14.43        | 6.395           | 15.33        | 5.113        | 16.23        | 3.825           |
| 13.57        | 8.703           | 14.47        | 6.334           | 15.37        | 5.067        | 16.27        | 3.782           |
| 13.60        | 8.574           | 14.50        | 6.276           | 15.40        | 5.020        | 16.30        | 3.741           |
| 13.63        | 8.455           | 14.53        | 6.220           | 15.43        | 4.973        | 16.33        | 3.702           |
| 13.67        | 8.344           | 14.57        | 6.166           | 15.47        | 4.926        | 16.37        | 3.665           |
| 13.70        | 8.240           | 14.60        | 6.115           | 15.50        | 4.879        | 16.40        | 3.629           |
| 13.73        | 8.141           | 14.63        | 6.065           | 15.53        | 4.832        | 16.43        | 3.596           |
| 13.77        | 7 8.048         | 14.67        | 6.017           | 15.57        | 4.785        | 16.47        | 3.564           |
| 13.80        | 7.957           | 14.70        | 5.970           | 15.60        | 4.737        | 16.50        | 3.534           |
| 13.80        | 7.869           | 14.73        | 5.924           | 15.63        | 4.689        | 16.53        | 3.506           |
| 13.87        | 7.783           | 14.77        | 5.878           | 15.67        | 4.642        | 16.57        | 3.478           |
| 13.90        | 7.696           | 14.80        | 5.834           | 15.70        | 4.594        | 16.60        | 3.452           |
| 13.90        | 7.609           | 14.83        | 5.790           | 15.73        | 4.546        | 16.63        | 3.427           |
| 13.97        | 7.521           | 14.87        | 5.746           | 15.77        | 4.497        | 16.67        | 3.403           |
| 14.00        | 7.432           | 14.90        | 5.702           | 15.80        | 4.449        | 16.70        | 3.379           |
| 14.03        | 7.343           | 14.93        | 5.658           | 15.83        | 4.401        | 16.73        | 3.357           |
| 14.0         | 7 7.255         | 14.97        | 5.613           | 15.87        | 4.352        | 16.77        | 3.334           |
| 14.10        | 7.166           | 15.00        | 5.569           | 15.90        | 4.303        | 16.80        | 3.313           |
| 14.13        | 3 7.079         | 15.03        | 5.524           | 15.93        | 4.254        | 16.83        | 3.291           |
| 14.1         | 7 6.993         | 15.07        | 5.479           | 15.97        | 4.205        | 16.87        | 3.270           |
| 14.20        | 6.908           | 15.10        | 5.434           | 16.00        | 4.156        | 16.90        | 3.248           |
| 14.23        | 3 6.826         | 15.13        | 5.388           | 16.03        | 4.107        | 16.93        | 3.227           |
| 14.2         | 7 6.746         | 15.17        | 5.343           | 16.07        | 4.058        | 16.97        | 3.206           |
| 14.30        | 0 6.669         | 15.20        | 5.297           | 16.10        | 4.010        | 17.00        | 3.184           |
| 14.3         | 3 6.595         | 15.23        | 5.251           | 16.13        | 3.962        | 17.03        | 3.163           |
| 14.3         | 7 6.525         | 15.27        | 5.206           | 16.17        | 3.915        | 17.07        | 3.141           |

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| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|-----------------|
| 17.10        | 3.120           | 18.00          | 2.525           | 18.90          | 2.161           | 19.80          | 1.985           |
| 17.13        | 3.098           | 18.03          | 2.502           | 18.93          | 2.155           | 19.83          | 1.979           |
| 17.17        | 3.076           | 18.07          | 2.480           | 18.97          | 2.148           | 19.87          | 1.972           |
| 17.20        | 3.055           | 18.10          | 2.458           | 19.00          | 2.142           | 19.90          | 1.965           |
| 17.23        | 3.033           | 18.13          | 2.436           | 19.03          | 2.135           | 19.93          | 1.959           |
| 17.27        | 3.011           | 18.17          | 2.415           | 19.07          | 2.129           | 19.97          | 1.952           |
| 17.30        | 2.989           | 18.20          | 2.395           | 19.10          | 2.122           | 20.00          | 1.946           |
| 17.33        | 2.968           | 18.23          | 2.375           | 19.13          | 2.116           | 20.03          | 1.939           |
| 17.37        | 2.946           | 18.27          | 2.357           | 19.17          | 2.109           | 20.07          | 1.932           |
| 17.40        | 2.924           | 18.30          | 2.339           | 19.20          | 2.103           | 20.10          | 1.926           |
| 17.43        | 2.902           | 18.33          | 2.322           | 19.23          | 2.096           | 20.13          | 1.919           |
| 17.47        | 2.880           | 18.37          | 2.307           | 19.27          | 2.090           | 20.17          | 1.912           |
| 17.50        | 2.858           | 18.40          | 2.293           | 19.30          | 2.084           | 20.20          | 1.906           |
| 17.53        | 2.836           | 18.43          | 2.279           | 19.33          | 2.077           | 20.23          | 1.899           |
| 17.57        | 2.814           | 18.47          | 2.267           | 19.37          | 2.071           | 20.27          | 1.892           |
| 17.60        | 2.792           | 18.50          | 2.255           | 19.40          | 2.064           | 20.30          | 1.886           |
| 17.63        | 2.770           | 18.53          | 2.245           | 19.43          | 2.057           | 20.33          | 1.879           |
| 17.67        | 2.748           | 18.57          | 2.235           | 19.47          | 2.051           | 20.37          | 1.872           |
| 17.70        | 2.725           | 18.60          | 2.226           | 19.50          | 2.044           | 20.40          | 1.866           |
| 17.73        | 2.703           | 18.63          | 2.217           | 19.53          | 2.038           | 20.43          | 1.859           |
| 17.77        | 2.681           | 18.67          | 2.209           | 19.57          | 2.031           | 20.47          | 1.852           |
| 17.80        | 2.659           | 18.70          | 2.201           | 19.60          | 2.025           | 20.50          | 1.845           |
| 17.83        | 2.637           | 18.73          | 2.194           | 19.63          | 2.018           | 20.53          | 1.839           |
| 17.87        | 2.614           | 18.77          | 2.187           | 19.67          | 2.012           | 20.57          | 1.832           |
| 17.90        | 2.592           | 18.80          | 2.180           | 19.70          | 2.005           | 20.60          | 1.825           |
| 17.93        | 2.569           | 18.83          | 2.174           | 19.73          | 1.998           | 20.63          | 1.819           |
| 17.97        | 2.547           | 18.87          | 2.167           | 19.77          | 1.992           | 20.67          | 1.812           |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) |   | Time (<br>(hrs | Outflow<br>cfs) | Time<br>(h <del>r</del> s | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|---|----------------|-----------------|---------------------------|-----------------|
| 20.70        | 1.805           | 21.60          | 1.621           |   | 22.50          | 1.690           | 23.40                     | 1.408           |
| 20.73        | 1.798           | 21.63          | 1.614           |   | 22.53          | 1.675           | 23.43                     | 1.403           |
| 20.77        | 1.791           | 21.67          | 1.607           |   | 22.57          | 1.660           | 23.47                     | 1.398           |
| 20.80        | 1.785           | 21.70          | 1.600           |   | 22.60          | 1.645           | 23.50                     | 1.392           |
| 20.83        | 1.778           | 21.73          | 1.593           |   | 22.63          | 1.629           | 23.53                     | 1.387           |
| 20.87        | 1.771           | 21.77          | 1.586           |   | 22.67          | 1.613           | 23.57                     | 1.382           |
| 20.90        | 1.764           | 21.80          | 1.579           | 3 | 22.70          | 1.596           | 23.60                     | 1.376           |
| 20.93        | 1.758           | 21.83          | 1.572           |   | 22.73          | 1.579           | 23.63                     | 1.371           |
| 20.97        | 1.751           | 21.87          | 1.565           |   | 22.77          | 1.561           | 23.67                     | 1.366           |
| 21.00        | 1.744           | 21.90          | 1.558           |   | 22.80          | 1.543           | 23.70                     | 1.361           |
| 21.03        | 1.737           | 21.93          | 1.551           |   | 22.83          | 1.525           | 23.73                     | 1.355           |
| 21.07        | 1.730           | 21.97          | 1.544           |   | 22.87          | 1.506           | 23.77                     | 1.350           |
| 21.10        | 1.724           | 22.00          | 1.538           |   | 22.90          | 1.486           | 23.80                     | 1.345           |
| 21.13        | 1.717           | 22.03          | 1.556           |   | 22.93          | 1.481           | 23.83                     | 1.340           |
| 21.17        | 1.710           | 22.07          | 1.575           |   | 22.97          | 1.476           | 23.87                     | 1.334           |
| 21.20        | 1.703           | 22.10          | 1.594           |   | 23.00          | 1.471           | 23.90                     | 1.329           |
| 21.23        | 1.696           | 22.13          | 1.615           |   | 23.03          | 1.466           | 23.93                     | 1.324           |
| 21.27        | 1.689           | 22.17          | 1.637           |   | 23.07          | 1.460           | 23.97                     | 1.318           |
| 21.30        | 1.683           | 22.20          | 1.659           |   | 23.10          | 1.455           | 24.00                     | 1.313           |
| 21.33        | 1.676           | 22.23          | 1.682           |   | 23.13          | 1.450           | 24.03                     | 1.299           |
| 21.37        | 1.669           | 22.27          | 1.707           |   | 23.17          | 1.445           | 24.07                     | 1.275           |
| 21.40        | 1.662           | 22.30          | 1.732           |   | 23.20          | 1.439           | 24.10                     | 1.242           |
| 21.43        | 1.655           | 22.33          | 1.758           |   | 23.23          | 1.434           | 24.13                     | 1.200           |
| 21.47        | 1.648           | 22.37          | 1.745           |   | 23.27          | 1.429           | 24.17                     | 1.149           |
| 21.50        | 1.641           | 22.40          | 1.732           |   | 23.30          | 1.424           | 24.20                     | 1.089           |
| 21.53        | 1.634           | 22.43          | 1.718           |   | 23.33          | 1.418           | 24.23                     | 1.019           |
| 21.57        | 1.628           | 22.47          | 1.704           |   | 23.37          | 1.413           | 24.27                     | 0.941           |

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| Time (<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|
| 24.30          | 0.854           |
| 24.33          | 0.758           |
| 24.37          | 0.668           |
| 24.40          | 0.584           |
| 24.43          | 0.505           |

...End

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

**Hyd. No. 2**Post Development

| Description   | A  |   | <u>B</u>                              |   | <u>C</u>                          |   | <u>Totals</u> |
|---|--|---|---------------------------------------|---|-----------------------------------|---|---------------|
| Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)                            | = 0.011<br>= 260.0<br>= 3.20<br>= 21.15        |   | 0.011<br>0.0<br>0.00<br>0.00          |   | 0.011<br>0.0<br>0.00<br>0.00      |   |               |
| Travel Time (min)   | = 1.01   | + | 0.00                                  | + | 0.00                              | = | 1.01          |
| Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)        | = 849.00<br>= 4.24<br>= Unpaved<br>=3.32       | d | 1091.00<br>1.37<br>Paved<br>2.38      | ) | 1882.00<br>1.24<br>Unpave<br>1.80 |   |               |
| Travel Time (min)   | = 4.26   | + | 7.64                                  | + | 17.46                             | = | 29.36         |
| Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) | = 0.00<br>= 0.00<br>= 0.00<br>= 0.015<br>=0.00 |   | 0.00<br>0.00<br>0.00<br>0.015<br>0.00 |   | 0.00<br>0.00<br>0.00<br>0.015     |   |               |
| Flow length (ft)  | ({0})0.0                                       |   | 0.0                                   |   | 0.0                               |   |               |
| Travel Time (min)   | = 0.00   | + | 0.00                                  | + | 0.00                              | = | 0.00          |
| Total Travel Time, Tc   |  |   |                                       |   |                                   |   |               |

## **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

#### Hyd. No. 1

#### Pre Development

| Hydrograph type | = SCS Runoff | Peak discharge     | = 158.76 cfs   |
|-----------------|--------------|--------------------|----------------|
| Storm frequency | = 10 yrs     | Time to peak       | = 12.33 hrs    |
| Time interval   | = 2 min      | Hyd. volume        | = 829,278 cuft |
| Drainage area   | = 97.910 ac  | Curve number       | = 81.000*      |
| Basin Slope     | = 0.0 %      | Hydraulic length   | = 0 ft         |
| Tc method       | = TR55       | Time of conc. (Tc) | = 27.4 min     |
| Total precip.   | = 4.25 in    | Distribution       | = Type III     |
| Storm duration  | = 24 hrs     | Shape factor       | = 484          |

<sup>\*</sup> Composite (Area/CN) =  $[(44.250 \times 73) + (8.070 \times 72) + (42.080 \times 89) + (3.000 \times 98) + (0.510 \times 71)] / 97.910$ 

#### **Hydrograph Discharge Table**

( Printed values >= 1,00% of Qp.)

| Time<br>(hrs | Outflow<br>cfs)    | Time C<br>(hrs | outflow<br>cfs) | Time<br>(hrs | Outflow cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|--------------------|----------------|-----------------|--------------|--------------|----------------|-----------------|
| 9.23         | 1.591              | 9.83           | 3.135           | 10.43        | 5.297        | 11.03          | 8.840           |
| 9.27         | 1.665              | 9.87           | 3.234           | 10.47        | 5.458        | 11.07          | 9.077           |
| 9.30         | 1.740              | 9.90           | 3.334           | 10.50        | 5.624        | 11.10          | 9.326           |
| 9.33         | 1.817              | 9.93           | 3.436           | 10.53        | 5.794        | 11.13          | 9.590           |
| 9.37         | 1.895              | 9.97           | 3.539           | 10.57        | 5.970        | 11.17          | 9.872           |
| 9.40         | 1.974              | 10.00          | 3.644           | 10.60        | 6.150        | 11.20          | 10.18           |
| 9.43         | 2.055              | 10.03          | 3.750           | 10.63        | 6.335        | 11.23          | 10.51           |
| 9.47         | 2.137              | 10.07          | 3.858           | 10.67        | 6.523        | 11.27          | 10.87           |
| 9.50         | 2.221              | 10.10          | 3.969           | 10.70        | 6.716        | 11.30          | 11.27           |
| 9.53         | 2.306              | 10.13          | 4.082           | 10.73        | 6.913        | 11.33          | 11.70           |
| 9.57         | 2.392              | 10.17          | 4.198           | 10.77        | 7.114        | 11.37          | 12.17           |
| 9.60         | 2.480              | 10.20          | 4.318           | 10.80        | 7.318        | 11.40          | 12.68           |
| 9.63         | 2.569              | 10.23          | 4.443           | 10.83        | 7.525        | 11.43          | 13.22           |
| 9.67         | 2.660              | 10.27          | 4.572           | 10.87        | 7.736        | 11.47          | 13.79           |
| 9.70         | 2.752 <sup>-</sup> | 10.30          | 4.706           | 10.90        | 7.950        | 11.50          | 14.39           |
| 9.73         | 2.846              | 10.33          | 4.846           | 10.93        | 8.167        | 11.53          | 15.05           |
| 9.77         | 2.941              | 10.37          | 4.991           | 10.97        | 8.388        | 11.57          | 15.81           |
| 9.80         | 3.037              | 10.40          | 5.141           | 11.00        | 8.612        | 11.60          | 16.71           |

| Time C<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time Outflow<br>(hrs cfs) |       | Time Outflow<br>(hrs cfs) |       |
|----------------|-----------------|----------------|-----------------|---------------------------|-------|---------------------------|-------|
| 11.63          | 17.82           | 12.50          | 139.88          | 13.40                     | 24.73 | 14.30                     | 17.14 |
| 11.67          | 19.18           | 12.53          | 132.74          | 13.43                     | 24.24 | 14.33                     | 16.94 |
| 11.70          | 20.85           | 12.57          | 124.80          | 13.47                     | 23.80 | 14.37                     | 16.76 |
| 11.73          | 22.89           | 12.60          | 116.20          | 13.50                     | 23.39 | 14.40                     | 16.58 |
| 11.77          | 25.37           | 12.63          | 107.13          | 13.53                     | 23.02 | 14.43                     | 16.42 |
| 11.80          | 28.35           | 12.67          | 97.76           | 13.57                     | 22.67 | 14.47                     | 16.26 |
| 11.83          | 31.87           | 12.70          | 88.27           | 13.60                     | 22.36 | 14.50                     | 16.10 |
| 11.87          | 35.94           | 12.73          | 78.99           | 13.63                     | 22.06 | 14.53                     | 15.96 |
| 11.90          | 40.55           | 12.77          | 70.44           | 13.67                     | 21.78 | 14.57                     | 15.82 |
| 11.93          | 45.95           | 12.80          | 63.15           | 13.70                     | 21.52 | 14.60                     | 15.68 |
| 11.97          | 52.69           | 12.83          | 57.27           | 13.73                     | 21.26 | 14.63                     | 15.55 |
| 12.00          | 61.37           | 12.87          | 52.46           | 13.77                     | 21.01 | 14.67                     | 15.43 |
| 12.03          | 71.98           | 12.90          | 48.35           | 13.80                     | 20.76 | 14.70                     | 15.30 |
| 12.07          | 83.83           | 12.93          | 44.72           | 13.83                     | 20.51 | 14.73                     | 15.18 |
| 12.10          | 96.18           | 12.97          | 41.54           | 13.87                     | 20.26 | 14.77                     | 15.05 |
| 12.13          | 108.53          | 13.00          | 38.77           | 13.90                     | 20.01 | 14.80                     | 14.93 |
| 12.17          | 120.70          | 13.03          | 36.38           | 13.93                     | 19.76 | 14.83                     | 14.81 |
| 12.20          | 132.46          | 13.07          | 34.33           | 13.97                     | 19.51 | 14.87                     | 14.69 |
| 12.23          | 143.17          | 13.10          | 32.58           | 14.00                     | 19.26 | 14.90                     | 14.56 |
| 12.27          | 151.77          | 13.13          | 31.11           | 14.03                     | 19.00 | 14.93                     | 14.44 |
| 12.30          | 157.04          | 13.17          | 29.87           | 14.07                     | 18.75 | 14.97                     | 14.32 |
| 12.33          | 158.76          | 13.20          | 28.82           | 14.10                     | 18.50 | 15.00                     | 14.19 |
| 12.37          | 157.79          | 13.23          | 27.93           | 14.13                     | 18.26 | 15.03                     | 14.07 |
| 12.37          | 157.79          | 13.27          | 27.16           | 14.17                     | 18.02 | 15.07                     | 13.94 |
| 12.40          | 155.07          | 13.30          | 26.47           | 14.20                     | 17.78 | 15.10                     | 13.82 |
| 12.43          | 146.05          | 13.33          | 25.84           | 14.23                     | 17.56 | 15.13                     | 13.69 |
| 12.41          | 140.00          | 13.37          | 25.26           | 14.27                     | 17.34 | 15.17                     | 13.57 |

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| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time -<br>(hrs | - Outflow<br>cfs) | Time<br>(hrs | Outflow cfs) |
|--------------|-----------------|----------------|-----------------|----------------|-------------------|--------------|--------------|
| 15.20        | 13.44           | 16.10          | 10.00           | 17.00          | 7.934             | 17.90        | 6.399        |
| 15.23        | 13.32           | 16.13          | 9.879           | 17.03          | 7.877             | 17.93        | 6.342        |
| 15.27        | 13.19           | 16.17          | 9.758           | 17.07          | 7.821             | 17.97        | 6.285        |
| 15.30        | 13.07           | 16.20          | 9.640           | 17.10          | 7.765             | 18.00        | 6.227        |
| 15.33        | 12.94           | 16.23          | 9.527           | 17.13          | 7.708             | 18.03        | 6.170        |
| 15.37        | 12.81           | 16.27          | 9.419           | 17.17          | 7.652             | 18.07        | 6.113        |
| 15.40        | 12.69           | 16.30          | 9.317           | 17.20          | 7.595             | 18.10        | 6.057        |
| 15.43        | 12.56           | 16.33          | 9.221           | 17.23          | 7.539             | 18.13        | 6.003        |
| 15.47        | 12.44           | 16.37          | 9.131           | 17.27          | 7.482             | 18.17        | 5.950        |
| 15.50        | 12.31           | 16.40          | 9.045           | 17.30          | 7.425             | 18.20        | 5.899        |
| 15.53        | 12.18           | 16.43          | 8.965           | 17.33          | 7.369             | 18.23        | 5.851        |
| 15.57        | 12.05           | 16.47          | 8.888           | 17.37          | 7.312             | 18.27        | 5.806        |
| 15.60        | 11.93           | 16.50          | 8.816           | 17.40          | 7.255             | 18.30        | 5.763        |
| 15.63        | 11.80           | 16.53          | 8.747           | 17.43          | 7.198             | 18.33        | 5.724        |
| 15.67        | 11.67           | 16.57          | 8.681           | 17.47          | 7.141             | 18.37        | 5.688        |
| 15.70        | 11.54           | 16.60          | 8.618           | 17.50          | 7.085             | 18.40        | 5.655        |
| 15.73        | 11.42           | 16.63          | 8.557           | 17.53          | 7.028             | 18.43        | 5.625        |
| 15.77        | 11.29           | 16.67          | 8.498           | 17.57          | 6.971             | 18.47        | 5.597        |
| 15.80        | 11.16           | 16.70          | 8.440           | 17.60          | 6.914             | 18.50        | 5.571        |
| 15.83        | 11.03           | 16.73          | 8.383           | 17.63          | 6.857             | 18.53        | 5.547        |
| 15.87        | 10.90           | 16.77          | 8.327           | 17.67          | 6.800             | 18.57        | 5.524        |
| 15.90        | 10.77           | 16.80          | 8.271           | 17.70          | 6.743             | 18.60        | 5.504        |
| 15.93        | 10.64           | 16.83          | 8.215           | 17.73          | 6.685             | 18.63        | 5.484        |
| 15.97        | 10.52           | 16.87          | 8.159           | 17.77          | 6.628             | 18.67        | 5.465        |
| 16.00        | 10.39           | 16.90          | 8.103           | 17.80          | 6.571             | 18.70        | 5.447        |
| 16.03        | 10.26           | 16.93          | 8.046           | 17.83          | 6.514             | 18.73        | 5.430        |
| 16.07        | 10.13           | 16.97          | 7.990           | 17.87          | 6.457             | 18.77        | 5.413        |

Continues on next neces

| Time<br>(hrs | · Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-------------------|----------------|-----------------|--------------|-----------------|----------------|-----------------|
| 18.80        | 5.396             | 19.70          | 4.939           | 20.60        | 4.476           | 21.50          | 4.008           |
| 18.83        | 5.380             | 19.73          | 4.922           | 20.63        | 4.459           | 21.53          | 3.991           |
| 18.87        | 5.363             | 19.77          | 4.905           | 20.67        | 4.441           | 21.57          | 3.974           |
| 18.90        | 5.346             | 19.80          | 4.888           | 20.70        | 4.424           | 21.60          | 3.956           |
| 18.93        | 5.329             | 19.83          | 4.871           | 20.73        | 4.407           | 21.63          | 3.939           |
| 18.97        | 5.312             | 19.87          | 4.853           | 20.77        | 4.390           | 21.67          | 3.921           |
| 19.00        | 5.295             | 19.90          | 4.836           | 20.80        | 4.372           | 21.70          | 3.904           |
| 19.03        | 5.278             | 19.93          | 4.819           | 20.83        | 4.355           | 21.73          | 3.887           |
| 19.07        | 5.261             | 19.97          | 4.802           | 20.87        | 4.338           | 21.77          | 3.869           |
| 19.10        | 5.245             | 20.00          | 4.785           | 20.90        | 4.321           | 21.80          | 3.852           |
| 19.13        | 5.228             | 20.03          | 4.768           | 20.93        | 4.303           | 21.83          | 3.834           |
| 19.17        | 5.211             | 20.07          | 4.751           | 20.97        | 4.286           | 21.87          | 3.817           |
| 19.20        | 5.194             | 20.10          | 4.734           | 21.00        | 4.269           | 21.90          | 3.799           |
| 19.23        | 5.177             | 20.13          | 4.717           | 21.03        | 4.251           | 21.93          | 3.782           |
| 19.27        | 5.160             | 20.17          | 4.699           | 21.07        | 4.234           | 21.97          | 3.764           |
| 19.30        | 5.143             | 20.20          | 4.682           | 21.10        | 4.217           | 22.00          | 3.747           |
| 19.33        | 5.126             | 20.23          | 4.665           | 21.13        | 4.199           | 22.03          | 3.806           |
| 19.37        | 5.109             | 20.27          | 4.648           | 21.17        | 4.182           | 22.07          | 3.868           |
| 19.40        | 5.092             | 20.30          | 4.631           | 21.20        | 4.165           | 22.10          | 3.933           |
| 19.43        | 5.075             | 20.33          | 4.614           | 21.23        | 4.147           | 22.13          | 4.000           |
| 19.47        | 5.058             | 20.37          | 4.596           | 21.27        | 4.130           | 22.17          | 4.069           |
| 19.50        | 5.041             | 20.40          | 4.579           | 21.30        | 4.113           | 22.20          | 4.142           |
| 19.53        | 5.024             | 20.43          | 4.562           | 21.33        | 4.095           | 22.23          | 4.217           |
| 19.57        | 5.007             | 20.47          | 4.545           | 21.37        | 4.078           | 22.27          | 4.295           |
| 19.60        | 4.990             | 20.50          | 4.528           | 21.40        | 4.061           | 22.30          | 4.375           |
| 19.63        | 4.973             | 20.53          | 4.510           | 21.43        | 4.043           | 22.33          | 4.336           |
| 19.67        | 4.956             | 20.57          | 4.493           | 21.47        | 4.026           | 22.37          | 4.296           |

| Time (<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time O             | utflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|--------------------|----------------|
| 22.40          | 4.254           | 23.30          | 3.459           | 24.20              | 2.517          |
| 22.43          | 4.212           | 23.33          | 3.446           | 24.23              | 2.309          |
| 22.47          | 4.168           | 23.37          | 3.432           | 24.27              | 2.075          |
| 22.50          | 4.122           | 23.40          | 3.419           | 24.30              | 1.813          |
| 22.53          | 4.076           | 23.43          | 3.406           | End                |                |
| 22.57          | 4.028           | 23.47          | 3.393           | <sub>zu</sub> LII0 |                |
| 22.60          | 3.979           | 23.50          | 3.380           |                    |                |
| 22.63          | 3.929           | 23.53          | 3.367           |                    |                |
| 22.67          | 3.877           | 23.57          | 3.354           |                    |                |
| 22.70          | 3.824           | 23.60          | 3.340           |                    |                |
| 22.73          | 3.769           | 23.63          | 3.327           |                    |                |
| 22.77          | 3.713           | 23.67          | 3.314           |                    |                |
| 22.80          | 3.655           | 23.70          | 3.301           |                    |                |
| 22.83          | 3.642           | 23.73          | 3.288           |                    |                |
| 22.87          | 3.629           | 23.77          | 3.275           |                    |                |
| 22.90          | 3.616           | 23.80          | 3.261           |                    |                |
| 22.93          | 3.603           | 23.83          | 3.248           |                    |                |
| 22.97          | 3.590           | 23.87          | 3.235           |                    |                |
| 23.00          | 3.577           | 23.90          | 3.222           |                    |                |
| 23.03          | 3.564           | , 23.93        | 3.209           |                    |                |
| 23.07          | 3.550           | 23.97          | 3.196           |                    |                |
| 23.10          | 3.537           | 24.00          | 3.182           |                    |                |
| 23.13          | 3.524           | 24.03          | 3.141           |                    |                |
| 23.17          | 3.511           | 24.07          | 3.072           |                    |                |
| 23.20          | 3.498           | 24.10          | 2.974           |                    |                |
| 23.23          | 3.485           | 24.13          | 2.849           |                    |                |
| 23.27          | 3.472           | 24.17          | 2.697           |                    |                |

## **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

#### Hyd. No. 2

#### Post Development

| Hydrograph type | = SCS Runoff | Peak discharge     | = 151.99 cfs   |
|-----------------|--------------|--------------------|----------------|
| Storm frequency | = 10 yrs     | Time to peak       | = 12.37 hrs    |
| Time interval   | = 2 min      | Hyd. volume        | = 839,644 cuft |
| Drainage area   | = 97.910 ac  | Curve number       | = 81.000*      |
| Basin Slope     | = 0.0 %      | Hydraulic length   | = 0 ft         |
| Tc method       | = TR55       | Time of conc. (Tc) | = 30.4 min     |
| Total precip.   | = 4.25 in    | Distribution       | = Type III     |
| Storm duration  | = 24 hrs     | Shape factor       | = 484          |

<sup>\*</sup> Composite (Area/CN) =  $[(26.680 \times 73) + (8.070 \times 72) + (41.470 \times 89) + (0.685 \times 98) + (20.499 \times 79) + (0.510 \times 71)] / 97.910$ 

#### **Hydrograph Discharge Table**

( Printed values >= 1.00% of Qp.)

| Time (<br>(hrs | Outflow cfs) | Time C<br>(hrs | outflow<br>cfs) | Time Outflow<br>(hrs cfs) |       |  | Time Outflow<br>(hrs cfs) |       |  |
|----------------|--------------|----------------|-----------------|---------------------------|-------|--|---------------------------|-------|--|
| 9.27           | 1.592        | 9.87           | 3.145           | 10.47                     | 5.329 |  | 11.07                     | 8.890 |  |
| 9.30           | 1.666        | 9.90           | 3.245           | 10.50                     | 5.490 |  | 11.10                     | 9.134 |  |
| 9.33           | 1.741        | 9.93           | 3.347           | 10.53                     | 5.655 |  | 11.13                     | 9.391 |  |
| 9.37           | 1.818        | 9.97           | 3.449           | 10.57                     | 5.826 |  | 11.17                     | 9.664 |  |
| 9.40           | 1.897        | 10.00          | 3.553           | 10.60                     | 6.001 |  | 11.20                     | 9.957 |  |
| 9.43           | 1.976        | 10.03          | 3.659           | 10.63                     | 6.181 |  | 11.23                     | 10.27 |  |
| 9.47           | 2.058        | 10.07          | 3.766           | 10.67                     | 6.366 |  | 11.27                     | 10.61 |  |
| 9.50           | 2.141        | 10.10          | 3.876           | 10.70                     | 6.555 |  | 11.30                     | 10.98 |  |
| 9.53           | 2.225        | 10.13          | 3.988           | 10.73                     | 6.748 |  | 11.33                     | 11.38 |  |
| 9.57           | 2.310        | 10.17          | 4.103           | 10.77                     | 6.945 |  | 11.37                     | 11.82 |  |
| 9.60           | 2.397        | 10.20          | 4.221           | 10.80                     | 7.146 |  | 11.40                     | 12.28 |  |
| 9.63           | 2.486        | 10.23          | 4.343           | 10.83                     | 7.351 |  | 11.43                     | 12.79 |  |
| 9.67           | 2.576        | 10.27          | 4.469           | 10.87                     | 7.560 |  | 11.47                     | 13.32 |  |
| 9.70           | 2.667        | 10.30          | 4.600           | 10.90                     | 7.772 |  | 11.50                     | 13.89 |  |
| 9.73           | 2.760        | 10.33          | 4.735           | 10.93                     | 7.988 |  | 11.53                     | 14.50 |  |
| 9.77           | 2.854        | 10.37          | 4.876           | 10.97                     | 8.206 |  | 11.57                     | 15.20 |  |
| 9.80           | 2.950        | 10.40          | 5.022           | 11.00                     | 8.429 |  | 11.60                     | 16.03 |  |
| 9.83           | 3.047        | 10.43          | 5.173           | 11.03                     | 8.656 |  | 11.63                     | 17.03 |  |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | Time Outflow<br>(hrs cfs) |  | Time Outflow<br>(hrs cfs) |       |  | Time Outflow<br>(hrs cfs) |       |  |
|--------------|-----------------|----------------|---------------------------|--|---------------------------|-------|--|---------------------------|-------|--|
| 11.67        | 18.24           | 12.53          | 137.82                    |  | 13.43                     | 25.39 |  | 14.33                     | 17.45 |  |
| 11.70        | 19.71           | 12.57          | 131.97                    |  | 13.47                     | 24.88 |  | 14.37                     | 17.25 |  |
| 11.73        | 21.48           | 12.60          | 125.40                    |  | 13.50                     | 24.40 |  | 14.40                     | 17.06 |  |
| 11.77        | 23.62           | 12.63          | 118.22                    |  | 13.53                     | 23.96 |  | 14.43                     | 16.88 |  |
| 11.80        | 26.17           | 12.67          | 110.57                    |  | 13.57                     | 23.56 |  | 14.47                     | 16.71 |  |
| 11.83        | 29.20           | 12.70          | 102.59                    |  | 13.60                     | 23.18 |  | 14.50                     | 16.54 |  |
| 11.87        | 32.73           | 12.73          | 94.42                     |  | 13.63                     | 22.83 |  | 14.53                     | 16.38 |  |
| 11.90        | 36.78           | 12.77          | 86.19                     |  | 13.67                     | 22.50 |  | 14.57                     | 16.23 |  |
| 11.93        | 41.54           | 12.80          | 78.06                     |  | 13.70                     | 22.20 |  | 14.60                     | 16.08 |  |
| 11.97        | 47.46           | 12.83          | 70.29                     |  | 13.73                     | 21.91 |  | 14.63                     | 15.94 |  |
| 12.00        | 55.04           | 12.87          | 63.24                     |  | 13.77                     | 21.63 |  | 14.67                     | 15.80 |  |
| 12.03        | 64.26           | 12.90          | 57.25                     |  | 13.80                     | 21.36 |  | 14.70                     | 15.67 |  |
| 12.07        | 74.58           | 12.93          | 52.38                     |  | 13.83                     | 21.11 |  | 14.73                     | 15.54 |  |
| 12.10        | 85.41           | 12.97          | 48.34                     |  | 13.87                     | 20.85 |  | 14.77                     | 15.41 |  |
| 12.13        | 96.34           | 13.00          | 44.87                     |  | 13.90                     | 20.60 |  | 14.80                     | 15.28 |  |
| 12.17        | 107.23          | 13.03          | 41.78                     |  | 13.93                     | 20.35 |  | 14.83                     | 15.16 |  |
| 12.20        | 117.90          | 13.07          | 39.05                     |  | 13.97                     | 20.09 |  | 14.87                     | 15.03 |  |
| 12.23        | 128.18          | 13.10          | 36.67                     |  | 14.00                     | 19.84 |  | 14.90                     | 14.91 |  |
| 12.27        | 137.57          | 13.13          | 34.60                     |  | 14.03                     | 19.58 |  | 14.93                     | 14.79 |  |
| 12.30        | 145.18          | 13.17          | 32.82                     |  | 14.07                     | 19.33 |  | 14.97                     | 14.66 |  |
| 12.33        | 150.05          | 13.20          | 31.29                     |  | 14.10                     | 19.07 |  | 15.00                     | 14.53 |  |
| 12.37        | 151.99          | 13.23          | 30.00                     |  | 14.13                     | 18.82 |  | 15.03                     | 14.41 |  |
| 12.40        | 151.65          | 13.27          | 28.91                     |  | 14.17                     | 18.58 |  | 15.07                     | 14.28 |  |
| 12.40        | 149.79          | 13.30          | 27.99                     |  | 14.20                     | 18.34 |  | 15.10                     | 14.16 |  |
| 12.43        | 146.83          | 13.33          | 27.22                     |  | 14.23                     | 18.11 |  | 15.13                     | 14.03 |  |
| 12.47        | 142.81          | 13.37          | 26.55                     |  | 14.27                     | 17.88 |  | 15.17                     | 13.91 |  |
| 12.50        | 142.01          | 13.40          | 25.95                     |  | 14.30                     | 17.66 |  | 15.20                     | 13.78 |  |

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|              |                 |                |                 |              |                 | <b></b> :      | S 161 |
|--------------|-----------------|----------------|-----------------|--------------|-----------------|----------------|-------|
| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | cfs)  |
| 15.23        | 13.65           | 16.13          | 10.17           | 17.03        | 8.052           | 17.93          | 6.499 |
| 15.27        | 13.53           | 16.17          | 10.05           | 17.07        | 7.995           | 17.97          | 6.440 |
| 15.30        | 13.40           | 16.20          | 9.929           | 17.10        | 7.938           | 18.00          | 6.382 |
| 15.33        | 13.27           | 16.23          | 9.812           | 17.13        | 7.881           | 18.03          | 6.324 |
| 15.37        | 13.14           | 16.27          | 9.698           | 17.17        | 7.824           | 18.07          | 6.267 |
| 15.40        | 13.02           | 16.30          | 9.589           | 17.20        | 7.766           | 18.10          | 6.210 |
| 15.43        | 12.89           | 16.33          | 9.486           | 17.23        | 7.709           | 18.13          | 6.154 |
| 15.47        | 12.76           | 16.37          | 9.387           | 17.27        | 7.652           | 18.17          | 6.100 |
| 15.50        | 12.63           | 16.40          | 9.294           | 17.30        | 7.595           | 18.20          | 6.047 |
| 15.53        | 12.50           | 16.43          | 9.206           | 17.33        | 7.537           | 18.23          | 5.997 |
| 15.57        | 12.38           | 16.47          | 9.122           | 17.37        | 7.480           | 18.27          | 5.948 |
| 15.60        | 12.25           | 16.50          | 9.042           | 17.40        | 7.422           | 18.30          | 5.902 |
| 15.63        | 12.12           | 16.53          | 8.965           | 17.43        | 7.365           | 18.33          | 5.859 |
| 15.67        | 11.99           | 16.57          | 8.892           | 17.47        | 7.307           | 18.37          | 5.819 |
| 15.70        | 11.86           | 16.60          | 8.823           | 17.50        | 7.250           | 18.40          | 5.782 |
| 15.73        | 11.73           | 16.63          | 8.756           | 17.53        | 7.192           | 18.43          | 5.747 |
| 15.77        | 11.60           | 16.67          | 8.691           | 17.57        | 7.135           | 18.47          | 5.715 |
| 15.80        | 11.47           | 16.70          | 8.629           | 17.60        | 7.077           | 18.50          | 5.685 |
| 15.83        | 11.34           | 16.73          | 8.568           | 17.63        | 7.019           | 18.53          | 5.657 |
| 15.87        | 11.21           | 16.77          | 8.509           | 17.67        | 6.962           | 18.57          | 5.631 |
| 15.90        | 11.08           | 16.80          | 8.451           | 17.70        | 6.904           | 18.60          | 5.607 |
| 15.93        | 10.95           | 16.83          | 8.393           | 17.73        | 6.846           | 18.63          | 5.584 |
| 15.97        | 10.82           | 16.87          | 8.336           | 17.77        | 6.788           | 18.67          | 5.563 |
| 16.00        | 10.69           | 16.90          | 8.279           | 17.80        | 6.730           | 18.70          | 5.543 |
| 16.03        | 10.56           | 16.93          | 8.223           | 17.83        | 6.672           | 18.73          | 5.523 |
| 16.07        | 10.43           | 16.97          | 8.166           | 17.87        | 6.615           | 18.77          | 5.505 |
| 16.10        | 10.30           | 17.00          | 8.109           | 17.90        | 6.557           | 18.80          | 5.487 |
|              |                 |                |                 |              |                 |                |       |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time<br>(hrs | Outflow cfs) | Time (<br>(hrs | Time Outflow<br>(hrs cfs) |  |  |
|--------------|-----------------|----------------|-----------------|--------------|--------------|----------------|---------------------------|--|--|
| 18.83        | 5.470           | 19.73          | 5.006           | 20.63        | 4.538        | 21.53          | 4.064                     |  |  |
| 18.87        | 5.452           | 19.77          | 4.989           | 20.67        | 4.520        | 21.57          | 4.047                     |  |  |
| 18.90        | 5.435           | 19.80          | 4.972           | 20.70        | 4.503        | 21.60          | 4.029                     |  |  |
| 18.93        | 5.418           | 19.83          | 4.954           | 20.73        | 4.485        | 21.63          | 4.012                     |  |  |
| 18.97        | 5.401           | 19.87          | 4.937           | 20.77        | 4.468        | 21.67          | 3.994                     |  |  |
| 19.00        | 5.384           | 19.90          | 4.920           | 20.80        | 4.450        | 21.70          | 3.976                     |  |  |
| 19.03        | 5.367           | 19.93          | 4.903           | 20.83        | 4.433        | 21.73          | 3.959                     |  |  |
| 19.07        | 5.350           | 19.97          | 4.885           | 20.87        | 4.415        | 21.77          | 3.941                     |  |  |
| 19.10        | 5.333           | 20.00          | 4.868           | 20.90        | 4.398        | 21.80          | 3.923                     |  |  |
| 19.13        | 5.316           | 20.03          | 4.851           | 20.93        | 4.380        | 21.83          | 3.906                     |  |  |
| 19.17        | 5.299           | 20.07          | 4.833           | 20.97        | 4.363        | 21.87          | 3.888                     |  |  |
| 19.20        | 5.281           | 20.10          | 4.816           | 21.00        | 4.345        | 21.90          | 3.870                     |  |  |
| 19.23        | 5.264           | 20.13          | 4.799           | 21.03        | 4.328        | 21.93          | 3.853                     |  |  |
| 19.27        | 5.247           | 20.17          | 4.781           | 21.07        | 4.310        | 21.97          | 3.835                     |  |  |
| 19.30        | 5.230           | 20.20          | 4.764           | 21.10        | 4.293        | 22.00          | 3.817                     |  |  |
| 19.33        | 5.213           | 20.23          | 4.747           | 21.13        | 4.275        | 22.03          | 3.862                     |  |  |
| 19.37        | 5.196           | 20.27          | 4.729           | 21.17        | 4.258        | 22.07          | 3.908                     |  |  |
| 19.40        | 5.179           | 20.30          | 4.712           | 21.20        | 4.240        | 22.10          | 3.957                     |  |  |
| 19.43        | 5.161           | 20.33          | 4.694           | 21.23        | 4.223        | 22.13          | 4.008                     |  |  |
| 19.47        | 5.144           | 20.37          | 4.677           | 21.27        | 4.205        | 22.17          | 4.061                     |  |  |
| 19.50        | 5.127           | 20.40          | 4.660           | 21.30        | 4.188        | 22.20          | 4.116                     |  |  |
| 19.53        | 5.110           | 20.43          | 4.642           | 21.33        | 4.170        | 22.23          | 4.173                     |  |  |
| 19.57        | 5.092           | 20.47          | 4.625           | 21.37        | 4.152        | 22.27          | 4.233                     |  |  |
| 19.60        | 5.075           | 20.50          | 4.607           | 21.40        | 4.135        | 22.30          | 4.295                     |  |  |
| 19.63        | 5.058           | 20.53          | 4.590           | 21.43        | 4.117        | 22.33          | 4.359                     |  |  |
| 19.67        | 5.041           | 20.57          | 4.573           | 21.47        | 4.100        | 22.37          | 4.327                     |  |  |
| 19.70        | 5.024           | 20.60          | 4.555           | 21.50        | 4.082        | 22.40          | 4.293                     |  |  |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|----------------|-----------------|
| 22.43        | 4.260           | 23.33          | 3.506           | 24.23          | 2.514           |
| 22.47        | 4.225           | 23.37          | 3.493           | 24.27          | 2.321           |
| 22.50        | 4.189           | 23.40          | 3.480           | 24.30          | 2.106           |
| 22.53        | 4.152           | 23.43          | 3.466           | 24.33          | 1.870           |
| 22.57        | 4.114           | 23.47          | 3.453           | 24.37          | 1.647           |
| 22.60        | 4.076           | 23.50          | 3.440           | End            |                 |
| 22.63        | 4.036           | 23.53          | 3.426           | EIIG           |                 |
| 22.67        | 3.995           | 23.57          | 3.413           |                |                 |
| 22.70        | 3.953           | 23.60          | 3.400           |                |                 |
| 22.73        | 3.910           | 23.63          | 3.387           |                |                 |
| 22.77        | 3.866           | 23.67          | 3.373           |                |                 |
| 22.80        | 3.821           | 23.70          | 3.360           |                |                 |
| 22.83        | 3.775           | 23.73          | 3.347           |                |                 |
| 22.87        | 3.727           | 23.77          | 3.333           |                |                 |
| 22.90        | 3.679           | 23.80          | 3.320           |                |                 |
| 22.93        | 3.665           | 23.83          | 3.307           |                |                 |
| 22.97        | 3.652           | 23.87          | 3.293           |                |                 |
| 23.00        | 3.639           | 23.90          | 3.280           | 78             |                 |
| 23.03        | 3.626           | 23.93          | 3.267           |                |                 |
| 23.07        | 3.612           | 23.97          | 3.253           | 41             |                 |
| 23.10        | 3.599           | 24.00          | 3.240           |                |                 |
| 23.13        | 3.586           | 24.03          | 3.204           |                |                 |
| 23.17        | 3.573           | 24.07          | 3.145           |                |                 |
| 23.20        | 3.559           | 24.10          | 3.064           |                |                 |
| 23.23        | 3.546           | 24.13          | 2.960           |                |                 |
| 23.27        | 3.533           | 24.17          | 2.833           |                |                 |
| 23.30        | 3.520           | 24.20          | 2.685           |                |                 |

## **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

#### Hyd. No. 1

### Pre Development

| Hydrograph type | = SCS Runoff | Peak discharge     | = 249.42 cfs      |
|-----------------|--------------|--------------------|-------------------|
| Storm frequency | = 25 yrs     | Time to peak       | = 12.33 hrs       |
| Time interval   | = 2 min      | Hyd. volume        | = 1,306,057  cuft |
| Drainage area   | = 97.910 ac  | Curve number       | = 81.000*         |
| Basin Slope     | = 0.0 %      | Hydraulic length   | = 0 ft            |
| Tc method       | = TR55       | Time of conc. (Tc) | = 27.4 min        |
| Total precip.   | = 5.77 in    | Distribution       | = Type III        |
| Storm duration  | = 24 hrs     | Shape factor       | = 484             |

<sup>\*</sup> Composite (Area/CN) =  $[(44.250 \times 73) + (8.070 \times 72) + (42.080 \times 89) + (3.000 \times 98) + (0.510 \times 71)] / 97.910$ 

#### **Hydrograph Discharge Table**

( Printed values >= 1,00% of Qp.)

| Time (<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) |   | Time Outflow<br>(hrs cfs) |       | Time<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|---|---------------------------|-------|--------------|-----------------|
| 8.50           | 2.541           | 9.10           | 4.473           | ģ | 9.70                      | 7.044 | 10.30        | 10.33           |
| 8.53           | 2.629           | 9.13           | 4.600           | 9 | 9.73                      | 7.204 | 10.33        | 10.56           |
| 8.57           | 2.720           | 9.17           | 4.728           | 9 | 9.77                      | 7.367 | 10.37        | 10.81           |
| 8.60           | 2.814           | 9.20           | 4.859           | 9 | 9.80                      | 7.531 | 10.40        | 11.06           |
| 8.63           | 2.910           | 9.23           | 4.991           |   | 9.83                      | 7.697 | 10.43        | 11.33           |
| 8.67           | 3.008           | 9.27           | 5.125           | 9 | 9.87                      | 7.865 | 10.47        | 11.60           |
| 8.70           | 3.109           | 9.30           | 5.261           | 9 | 9.90                      | 8.034 | 10.50        | 11.88           |
| 8.73           | 3.211           | 9.33           | 5.400           | 9 | 9.93                      | 8.205 | 10.53        | 12.17           |
| 8.77           | 3.316           | 9.37           | 5.540           | • | 9.97                      | 8.378 | 10.57        | 12.46           |
| 8.80           | 3.423           | 9.40           | 5.682           |   | 10.00                     | 8.553 | 10.60        | 12.77           |
| 8.83           | 3.532           | 9.43           | 5.826           |   | 10.03                     | 8.730 | 10.63        | 13.08           |
| 8.87           | 3.643           | 9.47           | 5.971           | , | 10.07                     | 8.909 | 10.67        | 13.40           |
| 8.90           | 3.755           | 9.50           | 6.119           |   | 10.10                     | 9.093 | 10.70        | 13.72           |
| 8.93           | 3.870           | 9.53           | 6.268           |   | 10.13                     | 9.281 | 10.73        | 14.05           |
| 8.97           | 3.987           | 9.57           | 6.420           |   | 10.17                     | 9.475 | 10.77        | 14.38           |
| 9.00           | 4.105           | 9.60           | 6.573           | , | 10.20                     | 9.675 | 10.80        | 14.72           |
| 9.03           | 4.226           | 9.63           | 6.728           | , | 10.23                     | 9.883 | 10.83        | 15.06           |
| 9.07           | 4.349           | 9.67           | 6.885           |   | 10.27                     | 10.10 | 10.87        | 15.40           |

| Time Outflow<br>(hrs cfs) |       | Time Outflow<br>(hrs cfs) |        |   | Time Outflow<br>(hrs cfs) |        |  | Time Outflow<br>(hrs cfs) |       |  |
|---------------------------|-------|---------------------------|--------|---|---------------------------|--------|--|---------------------------|-------|--|
| 10.90                     | 15.75 | 11.80                     | 49.54  | 1 | 2.67                      | 148.65 |  | 13.57                     | 33.52 |  |
| 10.93                     | 16.11 | 11.83                     | 55.34  | 1 | 2.70                      | 133.80 |  | 13.60                     | 33.04 |  |
| 10.97                     | 16.46 | 11.87                     | 62.00  | 1 | 2.73                      | 119.37 |  | 13.63                     | 32.59 |  |
| 11.00                     | 16.83 | 11.90                     | 69.49  | 1 | 2.77                      | 106.13 |  | 13.67                     | 32.17 |  |
| 11.03                     | 17.20 | 11.93                     | 78.22  | 1 | 2.80                      | 94.93  |  | 13.70                     | 31.77 |  |
| 11.07                     | 17.58 | 11.97                     | 89.00  | 1 | 2.83                      | 85.93  |  | 13.73                     | 31.39 |  |
| 11.10                     | 17.98 | 12.00                     | 102.76 | 1 | 12.87                     | 78.59  |  | 13.77                     | 31.01 |  |
| 11.13                     | 18.41 | 12.03                     | 119.40 | 1 | 2.90                      | 72.33  |  | 13.80                     | 30.63 |  |
| 11.17                     | 18.86 | 12.07                     | 137.83 | 1 | 2.93                      | 66.82  |  | 13.83                     | 30.26 |  |
| 11.20                     | 19.36 | 12.10                     | 156.90 | 1 | 2.97                      | 62.00  |  | 13.87                     | 29.88 |  |
| 11.23                     | 19.91 | 12.13                     | 175.84 | 1 | 3.00                      | 57.81  |  | 13.90                     | 29.50 |  |
| 11.27                     | 20.51 | 12.17                     | 194.33 | 1 | 3.03                      | 54.20  |  | 13.93                     | 29.12 |  |
| 11.30                     | 21.16 | 12.20                     | 212.05 | 1 | 3.07                      | 51.10  |  | 13.97                     | 28.74 |  |
| 11.33                     | 21.88 | 12.23                     | 228.01 | 1 | 13.10                     | 48.47  |  | 14.00                     | 28.36 |  |
| 11.37                     | 22.67 | 12.27                     | 240.53 | 1 | 13.13                     | 46.25  |  | 14.03                     | 27.98 |  |
| 11.40                     | 23.50 | 12.30                     | 247.74 | 1 | 13.17                     | 44.38  |  | 14.07                     | 27.61 |  |
| 11.43                     | 24.40 | 12.33                     | 249.42 | 1 | 13.20                     | 42.80  |  | 14.10                     | 27.23 |  |
| 11.47                     | 25.35 | 12.37                     | 246.95 | 1 | 13.23                     | 41.46  |  | 14.13                     | 26.86 |  |
| 11.50                     | 26.35 | 12.40                     | 241.82 | 1 | 13.27                     | 40.30  |  | 14.17                     | 26.51 |  |
| 11.53                     | 27.44 | 12.43                     | 234.86 | 1 | 13.30                     | 39.26  |  | 14.20                     | 26.16 |  |
| 11.57                     | 28.70 | 12.47                     | 226.20 | 1 | 13.33                     | 38.30  |  | 14.23                     | 25.82 |  |
| 11.60                     | 30.20 | 12.50                     | 215.95 | 1 | 13.37                     | 37.42  |  | 14.27                     | 25.49 |  |
| 11.63                     | 32.04 | 12.53                     | 204.29 | 1 | 13.40                     | 36.62  |  | 14.30                     | 25.19 |  |
| 11.67                     | 34.31 | 12.57                     | 191.48 | 1 | 13.43                     | 35.89  |  | 14.33                     | 24.89 |  |
| 11.70                     | 37.09 | 12.60                     | 177.76 | 1 | 13.47                     | 35.22  |  | 14.37                     | 24.62 |  |
| 11.73                     | 40.49 | 12.63                     | 163.39 | 1 | 13.50                     | 34.60  |  | 14.40                     | 24.36 |  |
| 11.77                     | 44.61 | 12.00                     |        | 1 | 13.53                     | 34.04  |  | 14.43                     | 24.11 |  |

Continues on next ness

| Time Outflow<br>(hrs cfs) |       | Time Outflow<br>(hrs cfs) |       | Time Outflow<br>(hrs cfs) |       |  | Time Outflow<br>(hrs cfs) |       |  |
|---------------------------|-------|---------------------------|-------|---------------------------|-------|--|---------------------------|-------|--|
| 14.47                     | 23.87 | 15.37                     | 18.73 | 16.27                     | 13.72 |  | 17.17                     | 11.12 |  |
| 14.50                     | 23.64 | 15.40                     | 18.54 | 16.30                     | 13.57 |  | 17.20                     | 11.04 |  |
| 14.53                     | 23.42 | 15.43                     | 18.35 | 16.33                     | 13.43 |  | 17.23                     | 10.96 |  |
| 14.57                     | 23.21 | 15.47                     | 18.17 | 16.37                     | 13.30 |  | 17.27                     | 10.87 |  |
| 14.60                     | 23.01 | 15.50                     | 17.98 | 16.40                     | 13.17 |  | 17.30                     | 10.79 |  |
| 14.63                     | 22.81 | 15.53                     | 17.79 | 16.43                     | 13.05 |  | 17.33                     | 10.71 |  |
| 14.67                     | 22.62 | 15.57                     | 17.60 | 16.47                     | 12.94 |  | 17.37                     | 10.62 |  |
| 14.70                     | 22.43 | 15.60                     | 17.41 | 16.50                     | 12.83 |  | 17.40                     | 10.54 |  |
| 14.73                     | 22.25 | 15.63                     | 17.23 | 16.53                     | 12.73 |  | 17.43                     | 10.46 |  |
| 14.77                     | 22.06 | 15.67                     | 17.04 | 16.57                     | 12.64 |  | 17.47                     | 10.37 |  |
| 14.80                     | 21.88 | 15.70                     | 16.85 | 16.60                     | 12.54 |  | 17.50                     | 10.29 |  |
| 14.83                     | 21.70 | 15.73                     | 16.66 | 16.63                     | 12.45 |  | 17.53                     | 10.21 |  |
| 14.87                     | 21.51 | 15.77                     | 16.47 | 16.67                     | 12.37 |  | 17.57                     | 10.12 |  |
| 14.90                     | 21.33 | 15.80                     | 16.28 | 16.70                     | 12.28 |  | 17.60                     | 10.04 |  |
| 14.93                     | 21.14 | 15.83                     | 16.09 | 16.73                     | 12.20 |  | 17.63                     | 9.957 |  |
| 14.97                     | 20.96 | 15.87                     | 15.90 | 16.77                     | 12.11 |  | 17.67                     | 9.874 |  |
| 15.00                     | 20.77 | 15.90                     | 15.71 | 16.80                     | 12.03 |  | 17.70                     | 9.790 |  |
| 15.03                     | 20.59 | 15.93                     | 15.52 | 16.83                     | 11.95 |  | 17.73                     | 9.707 |  |
| 15.07                     | 20.40 | 15.97                     | 15.33 | 16.87                     | 11.87 |  | 17.77                     | 9.623 |  |
| 15.10                     | 20.22 | 16.00                     | 15.14 | 16.90                     | 11.78 |  | 17.80                     | 9.539 |  |
| 15.13                     | 20.03 | 16.03                     | 14.95 | 16.93                     | 11.70 |  | 17.83                     | 9.456 |  |
| 15.17                     | 19.85 | 16.07                     | 14.77 | 16.97                     | 11.62 |  | 17.87                     | 9.372 |  |
| 15.20                     | 19.66 | 16.10                     | 14.58 | 17.00                     | 11.54 |  | 17.90                     | 9.288 |  |
| 15.23                     | 19.48 | 16.13                     | 14.40 | 17.03                     | 11.45 |  | 17.93                     | 9.204 |  |
| 15.27                     | 19.29 | 16.17                     | 14.22 | 17.07                     | 11.37 |  | 17.97                     | 9.121 |  |
| 15.30                     | 19.10 | 16.20                     | 14.05 | 17.10                     | 11.29 |  | 18.00                     | 9.037 |  |
| 15.33                     | 18.92 | 16.23                     | 13.88 | 17.13                     | 11.21 |  | 18.03                     | 8.953 |  |

| Time Outflow<br>(hrs cfs) |       | Time Outflow<br>(hrs cfs) |       |    | Time Outflow<br>(hrs cfs) |       |  | Time Outflow<br>(hrs cfs) |       |  |
|---------------------------|-------|---------------------------|-------|----|---------------------------|-------|--|---------------------------|-------|--|
| 18.07                     | 8.870 | 18.97                     | 7.697 | 1  | 9.87                      | 7.024 |  | 20.77                     | 6.347 |  |
| 18.10                     | 8.789 | 19.00                     | 7.673 | 19 | 9.90                      | 6.999 |  | 20.80                     | 6.321 |  |
| 18.13                     | 8.710 | 19.03                     | 7.648 | 19 | 9.93                      | 6.974 |  | 20.83                     | 6.296 |  |
| 18.17                     | 8.632 | 19.07                     | 7.623 | 1  | 9.97                      | 6.949 |  | 20.87                     | 6.271 |  |
| 18.20                     | 8.558 | 19.10                     | 7.598 | 2  | 0.00                      | 6.924 |  | 20.90                     | 6.246 |  |
| 18.23                     | 8.488 | 19.13                     | 7.573 | 2  | 0.03                      | 6.899 |  | 20.93                     | 6.220 |  |
| 18.27                     | 8.421 | 19.17                     | 7.548 | 2  | 0.07                      | 6.874 |  | 20.97                     | 6.195 |  |
| 18.30                     | 8.360 | 19.20                     | 7.523 | 2  | 0.10                      | 6.849 |  | 21.00                     | 6.170 |  |
| 18.33                     | 8.303 | 19.23                     | 7.499 | 2  | 0.13                      | 6.824 |  | 21.03                     | 6.145 |  |
| 18.37                     | 8.250 | 19.27                     | 7.474 | 2  | 0.17                      | 6.799 |  | 21.07                     | 6.120 |  |
| 18.40                     | 8.202 | 19.30                     | 7.449 | 2  | 0.20                      | 6.774 |  | 21.10                     | 6.094 |  |
| 18.43                     | 8.157 | 19.33                     | 7.424 | 2  | 0.23                      | 6.749 |  | 21.13                     | 6.069 |  |
| 18.47                     | 8.116 | 19.37                     | 7.399 | 2  | 0.27                      | 6.724 |  | 21.17                     | 6.044 |  |
| 18.50                     | 8.078 | 19.40                     | 7.374 | 2  | 0.30                      | 6.699 |  | 21.20                     | 6.019 |  |
| 18.53                     | 8.042 | 19.43                     | 7.349 | 2  | 0.33                      | 6.674 |  | 21.23                     | 5.993 |  |
| 18.57                     | 8.010 | 19.47                     | 7.324 | 2  | 0.37                      | 6.648 |  | 21.27                     | 5.968 |  |
| 18.60                     | 7.979 | 19.50                     | 7.299 | 2  | 0.40                      | 6.623 |  | 21.30                     | 5.943 |  |
| 18.63                     | 7.950 | 19.53                     | 7.274 | 2  | 0.43                      | 6.598 |  | 21.33                     | 5.917 |  |
| 18.67                     | 7.923 | 19.57                     | 7.249 | 2  | 0.47                      | 6.573 |  | 21.37                     | 5.892 |  |
| 18.70                     | 7.897 | 19.60                     | 7.224 | 2  | 0.50                      | 6.548 |  | 21.40                     | 5.867 |  |
| 18.73                     | 7.871 | 19.63                     | 7.199 | 2  | 0.53                      | 6.523 |  | 21.43                     | 5.842 |  |
| 18.77                     | 7.846 | 19.67                     | 7.174 | 2  | 0.57                      | 6.498 |  | 21.47                     | 5.816 |  |
| 18.80                     | 7.821 | 19.70                     | 7.149 | 2  | 0.60                      | 6.472 |  | 21.50                     | 5.791 |  |
| 18.83                     | 7.797 | 19.73                     | 7.124 | 2  | 0.63                      | 6.447 |  | 21.53                     | 5.766 |  |
| 18.87                     | 7.772 | 19.77                     | 7.099 | 2  | 0.67                      | 6.422 |  | 21.57                     | 5.740 |  |
| 18.90                     | 7.747 | 19.80                     | 7.074 | 2  | 0.70                      | 6.397 |  | 21.60                     | 5.715 |  |
| 18.93                     | 7.722 | 19.83                     | 7.049 | 2  | 0.73                      | 6.372 |  | 21.63                     | 5.690 |  |

| Time<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time O<br>(hrs | utflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|----------------|----------------|
| 21.67        | 5.664           | 22.57          | 5.814           | 23.47          | 4.893          |
| 21.70        | 5.639           | 22.60          | 5.743           | 23.50          | 4.874          |
| 21.73        | 5.614           | 22.63          | 5.670           | 23.53          | 4.855          |
| 21.77        | 5.588           | 22.67          | 5.595           | 23.57          | 4.836          |
| 21.80        | 5.563           | 22.70          | 5.518           | 23.60          | 4.817          |
| 21.83        | 5.538           | 22.73          | 5.438           | 23.63          | 4.798          |
| 21.87        | 5.512           | 22.77          | 5.357           | 23.67          | 4.778          |
| 21.90        | 5.487           | 22.80          | 5.274           | 23.70          | 4.759          |
| 21.93        | 5.461           | 22.83          | 5.255           | 23.73          | 4.740          |
| 21.97        | 5.436           | 22.87          | 5.236           | 23.77          | 4.721          |
| 22.00        | 5.411           | 22.90          | 5.217           | 23.80          | 4.702          |
| 22.03        | 5.496           | 22.93          | 5.198           | 23.83          | 4.683          |
| 22.07        | 5.585           | 22.97          | 5.179           | 23.87          | 4.664          |
| 22.10        | 5.678           | 23.00          | 5.160           | 23.90          | 4.645          |
| 22.13        | 5.774           | 23.03          | 5.141           | 23.93          | 4.626          |
| 22.17        | 5.875           | 23.07          | 5.122           | 23.97          | 4.606          |
| 22.20        | 5.979           | 23.10          | 5.103           | 24.00          | 4.587          |
| 22.23        | 6.087           | 23.13          | 5.084           | 24.03          | 4.528          |
| 22.27        | 6.200           | 23.17          | 5.065           | 24.07          | 4.428          |
| 22.30        | 6.316           | 23.20          | 5.046           | 24.10          | 4.287          |
| 22.33        | 6.259           | 23.23          | 5.026           | 24.13          | 4.107          |
| 22.37        | 6.201           | 23.27          | 5.007           | 24.17          | 3.887          |
| 22.40        | 6.141           | 23.30          | 4.988           | 24.20          | 3.628          |
| 22.43        | 6.079           | 23.33          | 4.969           | 24.23          | 3.329          |
| 22.47        | 6.015           | 23.37          | 4.950           | 24.27          | 2.990          |
| 22.50        | 5.950           | 23.40          | 4.931           | 24.30          | 2.613          |
| 22.53        | 5.883           | 23.43          | 4.912           | End            |                |

# **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

### Hyd. No. 2

### Post Development

| Hydrograph type | = SCS Runoff | Peak discharge     | = 239.04 cfs     |
|-----------------|--------------|--------------------|------------------|
| Storm frequency | = 25 yrs     | Time to peak       | = 12.37 hrs      |
| Time interval   | = 2 min      | Hyd. volume        | = 1,322,382 cuft |
| Drainage area   | = 97.910 ac  | Curve number       | = 81.000*        |
| Basin Slope     | = 0.0 %      | Hydraulic length   | = 0 ft           |
| Tc method       | = TR55       | Time of conc. (Tc) | = 30.4  min      |
| Total precip.   | = 5.77 in    | Distribution       | = Type III       |
| Storm duration  | = 24 hrs     | Shape factor       | = 484            |
|                 |              |                    |                  |

<sup>\*</sup> Composite (Area/CN) =  $[(26.680 \times 73) + (8.070 \times 72) + (41.470 \times 89) + (0.685 \times 98) + (20.499 \times 79) + (0.510 \times 71)] / 97.910$ 

### **Hydrograph Discharge Table**

( Printed values >= 1 00% of Qp.)

| Time (<br>(hrs | Outflow<br>cfs) | Time C<br>(h <b>r</b> s | outflow<br>cfs) | Tin<br>(hr |      | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|-------------------------|-----------------|------------|------|-----------------|----------------|-----------------|
| 8.50           | 2.466           | 9.10                    | 4.368           | 9.         | 70   | 6.924           | 10.30          | 10.18           |
| 8.53           | 2.552           | 9.13                    | 4.493           | 9.         | 73   | 7.084           | 10.33          | 10.41           |
| 8.57           | 2.641           | 9.17                    | 4.621           | 9.         | 77   | 7.246           | 10.37          | 10.64           |
| 8.60           | 2.732           | 9.20                    | 4.750           | 9.         | 80   | 7.410           | 10.40          | 10.89           |
| 8.63           | 2.826           | 9.23                    | 4.882           | 9.         | 83   | 7.575           | 10.43          | 11.15           |
| 8.67           | 2.922           | 9.27                    | 5.015           | 9.         | 87   | 7.743           | 10.47          | 11.41           |
| 8.70           | 3.020           | 9.30                    | 5.150           | 9.         | 90   | 7.912           | 10.50          | 11.68           |
| 8.73           | 3.121           | 9.33                    | 5.287           | 9.         | 93   | 8.083           | 10.53          | 11.96           |
| 8.77           | 3.224           | 9.37                    | 5.427           | 9.         | 97   | 8.256           | 10.57          | 12.25           |
| 8.80           | 3.329           | 9.40                    | 5.568           | 10         | 0.00 | 8.430           | 10.60          | 12.55           |
| 8.83           | 3.436           | 9.43                    | 5.711           | 10         | 0.03 | 8.607           | 10.63          | 12.85           |
| 8.87           | 3.546           | 9.47                    | 5.856           | 10         | 0.07 | 8.786           | 10.67          | 13.16           |
| 8.90           | 3.657           | 9.50                    | 6.003           | 10         | ).10 | 8.969           | 10.70          | 13.48           |
| 8.93           | 3.771           | 9.53                    | 6.152           | 10         | 0.13 | 9.155           | 10.73          | 13.80           |
| 8.97           | 3.886           | 9.57                    | 6.302           | 10         | 0.17 | 9.347           | 10.77          | 14.13           |
| 9.00           | 4.004           | 9.60                    | 6.455           | 10         | 0.20 | 9.545           | 10.80          | 14.46           |
| 9.03           | 4.123           | 9.63                    | 6.609           | 10         | ).23 | 9.749           | 10.83          | 14.80           |
| 9.07           | 4.244           | 9.67                    | 6.766           | 10         | ).27 | 9.960           | 10.87          | 15.14           |

| Time (<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|-----------------|
| 10.90          | 15.49           | 11.80          | 45.95           | 12.67          | 169.21          | 13.57          | 34.84           |
| 10.93          | 15.85           | 11.83          | 50.94           | 12.70          | 156.57          | 13.60          | 34.27           |
| 10.97          | 16.20           | 11.87          | 56.74           | 12.73          | 143.70          | 13.63          | 33.75           |
| 11.00          | 16.56           | 11.90          | 63.33           | 12.77          | 130.80          | 13.67          | 33.25           |
| 11.03          | 16.93           | 11.93          | 71.04           | 12.80          | 118.11          | 13.70          | 32.79           |
| 11.07          | 17.31           | 11.97          | 80.55           | 12.83          | 106.05          | 13.73          | 32.35           |
| 11,10          | 17.70           | 12.00          | 92.59           | 12.87          | 95.15           | 13.77          | 31.93           |
| 11.13          | 18.12           | 12.03          | 107.11          | 12.90          | 85.95           | 13.80          | 31.53           |
| 11.17          | 18.57           | 12.07          | 123.23          | 12.93          | 78.49           | 13.83          | 31.14           |
| 11.20          | 19.04           | 12.10          | 140.01          | 12.97          | 72.34           | 13.87          | 30.76           |
| 11.23          | 19.56           | 12.13          | 156.85          | 13.00          | 67.06           | 13.90          | 30.38           |
| 11.27          | 20.11           | 12.17          | 173.49          | 13.03          | 62.37           | 13.93          | 29.99           |
| 11.30          | 20.72           | 12.20          | 189.68          | 13.07          | 58.24           | 13.97          | 29.61           |
| 11.33          | 21.39           | 12.23          | 205.15          | 13.10          | 54.63           | 14.00          | 29.23           |
| 11.37          | 22.11           | 12.27          | 219.11          | 13.13          | 51.51           | 14.03          | 28.84           |
| 11.40          | 22.89           | 12.30          | 230.19          | 13.17          | 48.82           | 14.07          | 28.46           |
| 11.43          | 23.72           | 12.33          | 236.91          | 13.20          | 46.52           | 14.10          | 28.08           |
| 11.47          | 24.60           | 12.37          | 239.04          | 13.23          | 44.57           | 14.13          | 27.71           |
| 11.50          | 25.54           | 12.40          | 237.67          | 13.27          | 42.93           | 14.17          | 27.34           |
| 11.53          | 26.56           | 12.43          | 233.97          | 13.30          | 41.55           | 14.20          | 26.98           |
| 11.57          | 27.72           | 12.47          | 228.61          | 13.33          | 40.38           | 14.23          | 26.63           |
| 11.60          | 29.10           | 12.50          | 221.67          | 13.37          | 39.37           | 14.27          | 26.29           |
| 11.63          | 30.76           | 12.53          | 213.28          | 13.40          | 38.46           | 14.30          | 25.96           |
| 11.67          | 32.78           | 12.57          | 203.65          | 13.43          | 37.62           | 14.33          | 25.65           |
| 11.70          | 35.22           | 12.60          | 192.96          | 13.47          | 36.84           | 14.37          | 25.35           |
| 11.73          | 38.18           | 12.63          | 181.41          | 13.50          | 36.12           | 14.40          | 25.07           |
| 11.77          | 41.72           | 12.00          | 101.71          | 13.53          | 35.46           | 14.43          | 24.80           |

| Time<br>(hrs | · Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) |
|--------------|-------------------|----------------|-----------------|--------------|-----------------|--------------|-----------------|
| 14.47        | 24.54             | 15.37          | 19.21           | 16.2         | 7 14.13         | 17.17        | 11.37           |
| 14.50        | 24.29             | 15.40          | 19.03           | 16.3         | 0 13.97         | 17.20        | 11.29           |
| 14.53        | 24.05             | 15.43          | 18.84           | 16.3         | 3 13.82         | 17.23        | 11.21           |
| 14.57        | 23.82             | 15.47          | 18.65           | 16.3         | 7 13.67         | 17.27        | 11.12           |
| 14.60        | 23.60             | 15.50          | 18.46           | 16.4         | 0 13.54         | 17.30        | 11.04           |
| 14.63        | 23.39             | 15.53          | 18.27           | 16.4         | 3 13.41         | 17.33        | 10.95           |
| 14.67        | 23.18             | 15.57          | 18.08           | 16.4         | 7 13.28         | 17.37        | 10.87           |
| 14.70        | 22.98             | 15.60          | 17.89           | 16.5         | 0 13.17         | 17.40        | 10.78           |
| 14.73        | 22.79             | 15.63          | 17.69           | 16.5         | 3 13.05         | 17.43        | 10.70           |
| 14.77        | 22.59             | 15.67          | 17.50           | 16.5         | 7 12.95         | 17.47        | 10.62           |
| 14.80        | 22.40             | 15.70          | 17.31           | 16.6         | 0 12.84         | 17.50        | 10.53           |
| 14.83        | 22.22             | 15.73          | 17.12           | 16.6         | 3 12.74         | 17.53        | 10.45           |
| 14.87        | 22.03             | 15.77          | 16.93           | 16.6         | 7 12.65         | 17.57        | 10.36           |
| 14.90        | 21.84             | 15.80          | 16.74           | 16.7         | 0 12.56         | 17.60        | 10.28           |
| 14.93        | 21.66             | 15.83          | 16.55           | 16.7         | 3 12.47         | 17.63        | 10.19           |
| 14.97        | 21.47             | 15.87          | 16.36           | 16.7         | 7 12.38         | 17.67        | 10.11           |
| 15.00        | 21.28             | 15.90          | 16.17           | 16.8         | 0 12.30         | 17.70        | 10.03           |
| 15.03        | 21.10             | 15.93          | 15.97           | 16.8         | 3 12.21         | 17.73        | 9.941           |
| 15.07        | 20.91             | 15.97          | 15.78           | 16.8         | 7 12.13         | 17.77        | 9.856           |
| 15.10        | 20.72             | 16.00          | 15.59           | 16.9         | 0 12.04         | 17.80        | 9.771           |
| 15.13        | 20.53             | 16.03          | 15.40           | 16.9         | 3 11.96         | 17.83        | 9.687           |
| 15.17        | 20.35             | 16.07          | 15.21           | 16.9         | 7 11.88         | 17.87        | 9.602           |
| 15.20        | 20.16             | 16.10          | 15.02           | 17.0         | 0 11.79         | 17.90        | 9.517           |
| 15.23        | 19.97             | 16.13          | 14.83           | 17.0         | 3 11.71         | 17.93        | 9.432           |
| 15.27        | 19.78             | 16.17          | 14.65           | 17.0         | 7 11.62         | 17.97        | 9.348           |
| 15.30        | 19.59             | 16.20          | 14.47           | 17.1         | 0 11.54         | 18.00        | 9.263           |
| 15.33        | 19.40             | 16.23          | 14.30           | 17.1         | 3 11.46         | 18.03        | 9.178           |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow cfs) | Time<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|--------------|--------------|--------------|-----------------|
| 18.07        | 9.094           | 18.97          | 7.827           | 19.87        | 7.146        | 20.77        | 6.460           |
| 18.10        | 9.011           | 19.00          | 7.802           | 19.90        | 7.121        | 20.80        | 6.434           |
| 18.13        | 8.930           | 19.03          | 7.777           | 19.93        | 7.095        | 20.83        | 6.409           |
| 18.17        | 8.851           | 19.07          | 7.752           | 19.97        | 7.070        | 20.87        | 6.383           |
| 18.20        | 8.774           | 19.10          | 7.727           | 20.00        | 7.045        | 20.90        | 6.358           |
| 18.23        | 8.699           | 19.13          | 7.701           | 20.03        | 7.019        | 20.93        | 6.332           |
| 18.27        | 8.629           | 19.17          | 7.676           | 20.07        | 6.994        | 20.97        | 6.307           |
| 18.30        | 8.562           | 19.20          | 7.651           | 20.10        | 6.969        | 21.00        | 6.281           |
| 18.33        | 8.499           | 19.23          | 7.626           | 20.13        | 6.943        | 21.03        | 6.256           |
| 18.37        | 8.440           | 19.27          | 7.601           | 20.17        | 6.918        | 21.07        | 6.230           |
| 18.40        | 8.386           | 19.30          | 7.575           | 20.20        | 6.892        | 21.10        | 6.205           |
| 18.43        | 8.335           | 19.33          | 7.550           | 20.23        | 6.867        | 21.13        | 6.179           |
| 18.47        | 8.288           | 19.37          | 7.525           | 20.27        | 6.842        | 21.17        | 6.153           |
| 18.50        | 8.244           | 19.40          | 7.500           | 20.30        | 6.816        | 21.20        | 6.128           |
| 18.53        | 8.203           | 19.43          | 7.475           | 20.33        | 6.791        | 21.23        | 6.102           |
| 18.57        | 8.165           | 19.47          | 7.449           | 20.37        | 6.765        | 21.27        | 6.077           |
| 18.60        | 8.130           | 19.50          | 7.424           | 20.40        | 6.740        | 21.30        | 6.051           |
| 18.63        | 8.096           | 19.53          | 7.399           | 20.43        | 6.715        | 21.33        | 6.026           |
| 18.67        | 8.065           | 19.57          | 7.374           | 20.47        | 6.689        | 21.37        | 6.000           |
| 18.70        | 8.035           | 19.60          | 7.348           | 20.50        | 6.664        | 21.40        | 5.974           |
| 18.73        | 8.007           | 19.63          | 7.323           | 20.53        | 6.638        | 21.43        | 5.949           |
| 18.77        | 7.979           | 19.67          | 7.298           | 20.57        | 6.613        | 21.47        | 5.923           |
| 18.80        | 7.953           | 19.70          | 7.273           | 20.60        | 6.587        | 21.50        | 5.897           |
| 18.83        | 7.928           | 19.73          | 7.247           | 20.63        | 6.562        | 21.53        | 5.872           |
| 18.87        | 7.902           | 19.77          | 7.222           | 20.67        | 6.536        | 21.57        | 5.846           |
| 18.90        | 7.877           | 19.80          | 7.197           | 20.70        | 6.511        | 21.60        | 5.821           |
| 18.93        | 7.852           | 19.83          | 7.171           | 20.73        | 6.485        | 21.63        | 5.795           |

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| Time (<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time O<br>(hrs | utflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|----------------|----------------|
| 21.67          | 5.769           | 22.57          | 5.938           | 23.47          | 4.980          |
| 21.70          | 5.744           | 22.60          | 5.882           | 23.50          | 4.961          |
| 21.73          | 5.718           | 22.63          | 5.824           | 23.53          | 4.941          |
| 21.77          | 5.692           | 22.67          | 5.765           | 23.57          | 4.922          |
| 21.80          | 5.667           | 22.70          | 5.705           | 23.60          | 4.903          |
| 21.83          | 5.641           | 22.73          | 5.643           | 23.63          | 4.883          |
| 21.87          | 5.615           | 22.77          | 5.579           | 23.67          | 4.864          |
| 21.90          | 5.590           | 22.80          | 5.514           | 23.70          | 4.845          |
| 21.93          | 5.564           | 22.83          | 5.447           | 23.73          | 4.825          |
| 21.97          | 5.538           | 22.87          | 5.378           | 23.77          | 4.806          |
| 22.00          | 5.513           | 22.90          | 5.308           | 23.80          | 4.787          |
| 22.03          | 5.577           | 22.93          | 5.288           | 23.83          | 4.767          |
| 22.07          | 5.644           | 22.97          | 5.269           | 23.87          | 4.748          |
| 22.10          | 5.714           | 23.00          | 5.250           | 23.90          | 4.729          |
| 22.13          | 5.787           | 23.03          | 5.231           | 23.93          | 4.709          |
| 22.17          | 5.863           | 23.07          | 5.211           | 23.97          | 4.690          |
| 22.20          | 5.942           | 23.10          | 5.192           | 24.00          | 4.670          |
| 22.23          | 6.025           | 23.13          | 5.173           | 24.03          | 4.618          |
| 22.27          | 6.111           | 23.17          | 5.154           | 24.07          | 4.533          |
| 22.30          | 6.200           | 23.20          | 5.134           | 24.10          | 4.416          |
| 22.33          | 6.292           | 23.23          | 5.115           | 24.13          | 4.266          |
| 22.37          | 6.246           | 23.27          | 5.096           | 24.17          | 4.084          |
| 22.40          | 6.198           | 23.30          | 5.076           | 24.20          | 3.870          |
| 22.43          | 6.148           | 23.33          | 5.057           | 24.23          | 3.624          |
| 22.47          | 6.098           | 23.37          | 5.038           | 24.27          | 3.346          |
| 22.50          | 6.046           | 23.40          | 5.019           | 24.30          | 3.036          |
| 22.53          | 5.993           | 23.43          | 4.999           | 24.33          | 2.695          |

# **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

### Hyd. No. 1

### Pre Development

| Hydrograph type | = SCS Runoff | Peak discharge     | = 311.90 cfs     |
|-----------------|--------------|--------------------|------------------|
| Storm frequency | = 50 yrs     | Time to peak       | = 12.33 hrs      |
| Time interval   | = 2 min      | Hyd. volume        | = 1,641,771 cuft |
| Drainage area   | = 97.910 ac  | Curve number       | = 81.000*        |
| Basin Slope     | = 0.0 %      | Hydraulic length   | = 0 ft           |
| Tc method       | = TR55       | Time of conc. (Tc) | = 27.4 min       |
| Total precip.   | = 6.80 in    | Distribution       | = Type III       |
| Storm duration  | = 24 hrs     | Shape factor       | = 484            |
|                 |              |                    |                  |

<sup>\*</sup> Composite (Area/CN) =  $[(44.250 \times 73) + (8.070 \times 72) + (42.080 \times 89) + (3.000 \times 98) + (0.510 \times 71)] / 97.910$ 

### **Hydrograph Discharge Table**

( Printed values >= 1 00% of Qp.)

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs)   | Time<br>(hrs | Outflow<br>cfs) |   | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-------------------|--------------|-----------------|---|----------------|-----------------|
| 8.10         | 3.192           | 8.70           | 5.177             | 9.30         | 8.082           |   | 9.90           | 11.69           |
| 8.13         | 3.275           | 8.73           | 5.319             | 9.33         | 8.265           |   | 9.93           | 11.91           |
| 8.17         | 3.359           | 8.77           | 5.463             | 9.37         | 8.450           |   | 9.97           | 12.13           |
| 8.20         | 3.446           | 8.80           | 5.610 <sup></sup> | 9.40         | 8.637           |   | 10.00          | 12.36           |
| 8.23         | 3.536           | 8.83           | 5.759             | 9.43         | 8.826           |   | 10.03          | 12.58           |
| 8.27         | 3.629           | 8.87           | 5.910             | 9.47         | 9.017           |   | 10.07          | 12.81           |
| 8.30         | 3.726           | 8.90           | 6.064             | 9.50         | 9.211           |   | 10.10          | 13.05           |
| 8.33         | 3.827           | 8.93           | 6.219             | 9.53         | 9.406           |   | 10.13          | 13.29           |
| 8.37         | 3.932           | 8.97           | 6.377             | 9.57         | 9.604           |   | 10.17          | 13.53           |
| 8.40         | 4.041           | 9.00           | 6.538             | 9.60         | 9.804           |   | 10.20          | 13.79           |
| 8.43         | 4.153           | 9.03           | 6.700             | 9.63         | 10.01           |   | 10.23          | 14.06           |
| 8.47         | 4.269           | 9.07           | 6.865             | 9.67         | 10.21           |   | 10.27          | 14.33           |
| 8.50         | 4.389           | 9.10           | 7.032             | 9.70         | 10.42           |   | 10.30          | 14.62           |
| 8.53         | 4.512           | 9.13           | 7.202             | 9.73         | 10.62           |   | 10.33          | 14.93           |
| 8.57         | 4.639           | 9.17           | 7.374             | 9.77         | 10.83           |   | 10.37          | 15.24           |
| 8.60         | 4.769           | 9.20           | 7.547             | 9.80         | 11.04           |   | 10.40          | 15.57           |
| 8.63         | 4.902           | 9.23           | 7.724             | 9.83         | 11.26           |   | 10.43          | 15.91           |
| 8.67         | 5.038           | 9.27           | 7.902             | 9.87         | 11.47           | Ā | 10.47          | 16.26           |

| Time (<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|--------------|-----------------|--------------|-----------------|
| 10.50          | 16.62           | 11.40          | 31.42           | 12.30        | 310.35          | 13.17        | 54.19           |
| 10.53          | 17.00           | 11.43          | 32.57           | 12.33        | 311.90          | 13.20        | 52.25           |
| 10.57          | 17.38           | 11.47          | 33.78           | 12.37        | 308.31          | 13.23        | 50.61           |
| 10.60          | 17.77           | 11.50          | 35.06           | 12.40        | 301.44          | 13.27        | 49.18           |
| 10.63          | 18.17           | 11.53          | 36.45           | 12.43        | 292.34          | 13.30        | 47.90           |
| 10.67          | 18.57           | 11.57          | 38.06           | 12.43        | 281.16          | 13.33        | 46.73           |
| 10.70          | 18.99           | 11.60          | 39.98           | 12.47        | 268.05          | 13.37        | 45.65           |
| 10.73          | 19.40           | 11.63          | 42.34           | 12.53        | 253.24          | 13.40        | 44.66           |
| 10.77          | 19.83           | 11.67          | 45.25           | 12.57        | 237.04          | 13.43        | 43.76           |
| 10.80          | 20.26           | 11.70          | 48.81           | 12.60        | 219.77          | 13.47        | 42.94           |
| 10.83          | 20.69           | 11.73          | 53.16           | 12.63        | 201.75          | 13.50        | 42.18           |
| 10.87          | 21.13           | 11.77          | 58.43           | 12.67        | 183.31          | 13.53        | 41.49           |
| 10.90          | 21.58           | 11.80          | 64.73           | 12.70        | 164.78          | 13.57        | 40.85           |
| 10.93          | 22.02           | 11.83          | 72.13           | 12.73        | 146.81          | 13.60        | 40.26           |
| 10.97          | 22.48           | 11.87          | 80.59           | 12.77        | 130.37          | 13.63        | 39.71           |
| 11.00          | 22.93           | 11.90          | 90.10           | 12.80        | 116.49          | 13.67        | 39.19           |
| 11.03          | 23.40           | 11.93          | 101.13          | 12.83        | 105.37          | 13.70        | 38.70           |
| 11.07          | 23.88           | 11.97          | 114.71          | 12.87        | 96.30           | 13.73        | 38.22           |
| 11.10          | 24.39           | 12.00          | 131.96          | 12.90        | 88.58           | 13.77        | 37.76           |
| 11.13          | 24.92           | 12.03          | 152.75          | 12.93        | 81.79           | 13.80        | 37.30           |
| 11.17          | 25.51           | 12.07          | 175.69          | 12.97        | 75.86           | 13.83        | 36.83           |
| 11.20          | 26.14           | 12.10          | 199.35          | 13.00        | 70.70           | 13.87        | 36.37           |
| 11.23          | 26.83           | 12.13          | 222.76          | 13.03        | 66.26           | 13.90        | 35.91           |
| 11.27          | 27.59           | 12.17          | 245.54          | 13.07        | 62.45           | 13.93        | 35.44           |
| 11.30          | 28.43           | 12.20          | 267.29          | 13.10        | 59.22           | 13.97        | 34.97           |
| 11.33          | 29.35           | 12.23          | 286.77          | 13.13        | 56.49           | 14.00        | 34.51           |
| 11.37          | 30.35           | 12.27          | 301.89          |              |                 | 14.03        | 34.04           |

Continuos on nout nos

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time (hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|-----------|-----------------|----------------|-----------------|
| 14.07        | 33.58           | 14.97          | 25.44           | 15.87     | 19.27           | 16.77          | 14.67           |
| 14.10        | 33.12           | 15.00          | 25.21           | 15.90     | 19.04           | 16.80          | 14.57           |
| 14.13        | 32.67           | 15.03          | 24.99           | 15.93     | 18.81           | 16.83          | 14.46           |
| 14.17        | 32.23           | 15.07          | 24.76           | 15.97     | 18.58           | 16.87          | 14.36           |
| 14.20        | 31.80           | 15.10          | 24.53           | 16.00     | 18.35           | 16.90          | 14.26           |
| 14.23        | 31.39           | 15.13          | 24.31           | 16.03     | 18.12           | 16.93          | 14.16           |
| 14.27        | 30.99           | 15.17          | 24.08           | 16.07     | 17.89           | 16.97          | 14.06           |
| 14.30        | 30.62           | 15.20          | 23.85           | 16.10     | 17.66           | 17.00          | 13.96           |
| 14.33        | 30.26           | 15.23          | 23.63           | 16.13     | 17.44           | 17.03          | 13.86           |
| 14.37        | 29.92           | 15.27          | 23.40           | 16.17     | 17.23           | 17.07          | 13.76           |
| 14.40        | 29.60           | 15.30          | 23.17           | 16.20     | 17.02           | 17.10          | 13.66           |
| 14.43        | 29.29           | 15.33          | 22.94           | 16.23     | 16.81           | 17.13          | 13.56           |
| 14.47        | 29.00           | 15.37          | 22.71           | 16.27     | 16.62           | 17.17          | 13.46           |
| 14.50        | 28.72           | 15.40          | 22.49           | 16.30     | 16.44           | 17.20          | 13.36           |
| 14.53        | 28.45           | 15.43          | 22.26           | 16.33     | 16.27           | 17.23          | 13.26           |
| 14.57        | 28.20           | 15.47          | 22.03           | 16.37     | 16.11           | 17.27          | 13.16           |
| 14.60        | 27.95           | 15.50          | 21.80           | 16.40     | 15.95           | 17.30          | 13.06           |
| 14.63        | 27.71           | 15.53          | 21.57           | 16.43     | 15.81           | 17.33          | 12.95           |
| 14.67        | 27.47           | 15.57          | 21.34           | 16.47     | 15.67           | 17.37          | 12.85           |
| 14.70        | 27.24           | 15.60          | 21.11           | 16.50     | 15.54           | 17.40          | 12.75           |
| 14.73        | 27.02           | 15.63          | 20.88           | 16.53     | 15.42           | 17.43          | 12.65           |
| 14.77        | 26.79           | 15.67          | 20.65           | 16.57     | 15.30           | 17.47          | 12.55           |
| 14.80        | 26.57           | 15.70          | 20.42           | 16.60     | 15.19           | 17.50          | 12.45           |
| 14.83        | 26.34           | 15.73          | 20.19           | 16.63     | 15.08           | 17.53          | 12.35           |
| 14.87        | 26.12           | 15.77          | 19.96           | 16.67     | 14.97           | 17.57          | 12.25           |
| 14.90        | 25.89           | 15.80          | 19.73           | 16.70     | 14.87           | 17.60          | 12.15           |
| 14.93        | 25.67           | 15.83          | 19.50           | 16.73     | 14.77           | 17.63          | 12.04           |

| Time<br>(hrs | Outflow cfs) | Time C<br>(hrs | outflow<br>cfs) | Time<br>(hrs | · Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|--------------|----------------|-----------------|--------------|-------------------|----------------|-----------------|
| 17.67        | 11.94        | 18.57          | 9.682           | 19.47        | 8.849             | 20.37          | 8.029           |
| 17.70        | 11.84        | 18.60          | 9.645           | 19.50        | 8.819             | 20.40          | 7.999           |
| 17.73        | 11.74        | 18.63          | 9.610           | 19.53        | 8.789             | 20.43          | 7.968           |
| 17.77        | 11.64        | 18.67          | 9.577           | 19.57        | 8.758             | 20.47          | 7.938           |
| 17.80        | 11.54        | 18.70          | 9.545           | 19.60        | 8.728             | 20.50          | 7.907           |
| 17.83        | 11.44        | 18.73          | 9.514           | 19.63        | 8.698             | 20.53          | 7.877           |
| 17.87        | 11.33        | 18.77          | 9.484           | 19.67        | 8.667             | 20.57          | 7.846           |
| 17.90        | 11.23        | 18.80          | 9.453           | 19.70        | 8.637             | 20.60          | 7.816           |
| 17.93        | 11.13        | 18.83          | 9.423           | 19.73        | 8.607             | 20.63          | 7.785           |
| 17.97        | 11.03        | 18.87          | 9.393           | 19.77        | 8.576             | 20.67          | 7.755           |
| 18.00        | 10.93        | 18.90          | 9.363           | 19.80        | 8.546             | 20.70          | 7.724           |
| 18.03        | 10.83        | 18.93          | 9.333           | 19.83        | 8.516             | 20.73          | 7.693           |
| 18.07        | 10.73        | 18.97          | 9.303           | 19.87        | 8.485             | 20.77          | 7.663           |
| 18.10        | 10.63        | 19.00          | 9.272           | 19.90        | 8.455             | 20.80          | 7.632           |
| 18.13        | 10.53        | 19.03          | 9.242           | 19.93        | 8.424             | 20.83          | 7.602           |
| 18.17        | 10.44        | 19.07          | 9.212           | 19.97        | 8.394             | 20.87          | 7.571           |
| 18.20        | 10.35        | 19.10          | 9.182           | 20.00        | 8.364             | 20.90          | 7.541           |
| 18.23        | 10.26        | 19.13          | 9.152           | 20.03        | 8.333             | 20.93          | 7.510           |
| 18.27        | 10.18        | 19.17          | 9.121           | 20.07        | 8.303             | 20.97          | 7.480           |
| 18.30        | 10.11        | 19.20          | 9.091           | 20.10        | 8.272             | 21.00          | 7.449           |
| 18.33        | 10.04        | 19.23          | 9.061           | 20.13        | 8.242             | 21.03          | 7.418           |
| 18.37        | 9.974        | 19.27          | 9.031           | 20.17        | 8.212             | 21.07          | 7.388           |
| 18.40        | 9.915        | 19.30          | 9.000           | 20.20        | 8.181             | 21.10          | 7.357           |
| 18.43        | 9.861        | 19.33          | 8.970           | 20.23        | 8.151             | 21.13          | 7.327           |
| 18.47        | 9.811        | 19.37          | 8.940           | 20.27        | 8.120             | 21.17          | 7.296           |
| 18.50        | 9.765        | 19.40          | 8.910           | 20.30        | 8.090             | 21.20          | 7.266           |
| 18.53        | 9.722        | 19.43          | 8.879           | 20.33        | 8.059             | 21.23          | 7.235           |

| Time (<br>hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time ·<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) |
|---------------|-----------------|----------------|-----------------|----------------|-----------------|--------------|-----------------|
| 21.27         | 7.204           | 22.17          | 7.089           | 23.07          | 6.178           | 23.97        | 5.555           |
| 21.30         | 7.174           | 22.20          | 7.215           | 23.10          | 6.155           | 24.00        | 5.532           |
| 21.33         | 7.143           | 22.23          | 7.346           | 23.13          | 6.132           | 24.03        | 5.460           |
| 21.37         | 7.113           | 22.27          | 7.481           | 23.17          | 6.109           | 24.07        | 5.340           |
| 21.40         | 7.082           | 22.30          | 7.621           | 23.20          | 6.086           | 24.10        | 5.170           |
| 21.43         | 7.051           | 22.33          | 7.553           | 23.23          | 6.063           | 24.13        | 4.953           |
| 21.47         | 7.021           | 22.37          | 7.482           | 23.27          | 6.040           | 24.17        | 4.688           |
| 21.50         | 6.990           | 22.40          | 7.410           | 23.30          | 6.017           | 24.20        | 4.375           |
| 21.53         | 6.959           | 22.43          | 7.335           | 23.33          | 5.994           | 24.23        | 4.014           |
| 21.57         | 6.929           | 22.47          | 7.258           | 23.37          | 5.971           | 24.27        | 3.606           |
| 21.60         | 6.898           | 22.50          | 7.179           | 23.40          | 5.948           | 24.30        | 3.151           |
| 21.63         | 6.867           | 22.53          | 7.098           | 23.43          | 5.925           | End          |                 |
| 21.67         | 6.837           | 22.57          | 7.014           | 23.47          | 5.902           | one LIIU     |                 |
| 21.70         | 6.806           | 22.60          | 6.929           | 23.50          | 5.879           |              |                 |
| 21.73         | 6.775           | 22.63          | 6.840           | 23.53          | 5.856           |              |                 |
| 21.77         | 6.745           | 22.67          | 6.750           | 23.57          | 5.833           |              |                 |
| 21.80         | 6.714           | 22.70          | 6.657           | 23.60          | 5.809           |              |                 |
| 21.83         | 6.683           | 22.73          | 6.561           | 23.63          | 5.786           |              |                 |
| 21.87         | 6.653           | 22.77          | 6.463           | 23.67          | 5.763           |              |                 |
| 21.90         | 6.622           | 22.80          | 6.363           | 23.70          | 5.740           |              |                 |
| 21.93         | 6.591           | 22.83          | 6.340           | 23.73          | 5.717           | 2            |                 |
| 21.97         | 6.560           | 22.87          | 6.317           | 23.77          | 5.694           |              |                 |
| 22.00         | 6.530           | 22.90          | 6.294           | 23.80          | 5.671           |              |                 |
| 22.03         | 6.633           | 22.93          | 6.271           | 23.83          | 5.648           |              |                 |
| 22.07         | 6.740           | 22.97          | 6.248           | 23.87          | 5.625           |              |                 |
| 22.10         | 6.852           | 23.00          | 6.225           | 23.90          | 5.602           |              |                 |
| 22.13         | 6.968           | 23.03          | 6.202           | 23.93          | 5.578           |              |                 |

# **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

### Hyd. No. 2

### Post Development

| 12.37 hrs      |
|----------------|
| 1,662,294 cuft |
| 81.000*        |
| O ft           |
| 30.4 min       |
| Type III       |
| 484            |
|                |

<sup>\*</sup> Composite (Area/CN) =  $[(26.680 \times 73) + (8.070 \times 72) + (41.470 \times 89) + (0.685 \times 98) + (20.499 \times 79) + (0.510 \times 71)] / 97.910$ 

### **Hydrograph Discharge Table**

( Printed values >= 1,00% of Qp.)

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time ·<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|-----------------|
| 8.07         | 3.049           | 8.67           | 4.929           | 9.27           | 7.768           | 9.87           | 11.33           |
| 8.10         | 3.128           | 8.70           | 5.065           | 9.30           | 7.948           | 9.90           | 11.55           |
| 8.13         | 3.210           | 8.73           | 5.204           | 9.33           | 8.129           | 9.93           | 11.77           |
| 8.17         | 3.293           | 8.77           | 5.346           | 9.37           | 8.314           | 9.97           | 11.99           |
| 8.20         | 3.379           | 8.80           | 5.491           | 9.40           | 8.500           | 10.00          | 12.22           |
| 8.23         | 3.468           | 8.83           | 5.638           | 9.43           | 8.689           | 10.03          | 12.44           |
| 8.27         | 3.559           | 8.87           | 5.788           | 9.47           | 8.879           | 10.07          | 12.67           |
| 8.30         | 3.653           | 8.90           | 5.940           | 9.50           | 9.072           | 10.10          | 12.90           |
| 8.33         | 3.751           | 8.93           | 6.095           | 9.53           | 9.267           | 10.13          | 13.14           |
| 8.37         | 3.853           | 8.97           | 6.252           | 9.57           | 9.465           | 10.17          | 13.39           |
| 8.40         | 3.958           | 9.00           | 6.411           | 9.60           | 9.664           | 10.20          | 13.64           |
| 8.43         | 4.067           | 9.03           | 6.573           | 9.63           | 9.866           | 10.23          | 13.90           |
| 8.47         | 4.180           | 9.07           | 6.737           | 9.67           | 10.07           | 10.27          | 14.17           |
| 8.50         | 4.296           | 9.10           | 6.903           | 9.70           | 10.27           | 10.30          | 14.45           |
| 8.53         | 4.416           | 9.13           | 7.071           | 9.73           | 10.48           | 10.33          | 14.75           |
| 8.57         | 4.539           | 9.17           | 7.242           | 9.77           | 10.69           | 10.37          | 15.05           |
| 8.60         | 4.666           | 9.20           | 7.415           | 9.80           | 10.90           | 10.40          | 15.37           |
| 8.63         | 4.796           | 9.23           | 7.590           | 9.83           | 11.12           | 10.43          | 15.70           |

\$

# Hydrograph Discharge Table

| Time<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|--------------|--------------|----------------|-----------------|
| 10.47        | 16.04           | 11.37          | 29.66           | 12.27        | 275.59       | 13.13          | 62.95           |
| 10.50        | 16.39           | 11.40          | 30.65           | 12.30        | 288.98       | 13.17          | 59.64           |
| 10.53        | 16.75           | 11.43          | 31.72           | 12.33        | 296.88       | 13.20          | 56.82           |
| 10.57        | 17.12           | 11.47          | 32.85           | 12.37        | 299.07       | 13.23          | 54.43           |
| 10.60        | 17.50           | 11.50          | 34.04           | 12.40        | 296.91       | 13.27          | 52.41           |
| 10.63        | 17.89           | 11.53          | 35.34           | 12.40        | 290.91       | 13.30          | 50.71           |
| 10.67        | 18.28           | 11.57          | 36.83           | 12.43        | 284.79       | 13.33          | 49.27           |
| 10.70        | 18.69           | 11.60          | 38.59           | 12.47        | 275.78       | 13.37          | 48.03           |
| 10.73        | 19.10           | 11.63          | 40.72           | 12.53        | 265.02       | 13.40          | 46.91           |
| 10.77        | 19.52           | 11.67          | 43.30           | 12.57        | 252.73       | 13.43          | 45.88           |
| 10.80        | 19.95           | 11.70          | 46.43           | 12.57        | 239.18       | 13.47          | 44.93           |
| 10.83        | 20.38           | 11.73          | 50.22           | 12.63        | 224.60       | 13.50          | 44.04           |
| 10.87        | 20.82           | 11.77          | 54.75           | 12.67        | 209.25       | 13.53          | 43.23           |
| 10.90        | 21.26           | 11.80          | 60.15           | 12.70        | 193.39       | 13.57          | 42.47           |
| 10.93        | 21.71           | 11.83          | 66.51           | 12.73        | 177.27       | 13.60          | 41:77           |
| 10.97        | 22.16           | 11.87          | 73.89           | 12.77        | 161.17       | 13.63          | 41.12           |
| 11.00        | 22.62           | 11.90          | 82.26           | 12.80        | 145.35       | 13.67          | 40.51           |
| 11.03        | 23.08           | 11.93          | 92.02           | 12.83        | 130.34       | 13.70          | 39.94           |
| 11.07        | 23.56           | 11.97          | 104.01          | 12.87        | 116.81       | 13.73          | 39.40           |
| 11.10        | 24.06           | 12.00          | 119.14          | 12.90        | 105.41       | 13.77          | 38.89           |
| 11.13        | 24.59           | 12.03          | 137.31          | 12.93        | 96.19        | 13.80          | 38.40           |
| 11.17        | 25.15           | 12.07          | 157.40          | 12.97        | 88.60        | 13.83          | 37.92           |
| 11.20        | 25.75           | 12.10          | 178.26          | 13.00        | 82.09        | 13.87          | 37.45           |
| 11.23        | 26.41           | 12.13          | 199.12          | 13.03        | 76.31        | 13.90          | 36.98           |
| 11.27        | 27.12           | 12.17          | 219.67          | 13.07        | 71.23        | 13.93          | 36.51           |
| 11.30        | 27.89           | 12.20          | 239.60          | 13.10        | 66.79        | 13.97          | 36.04           |
| 11.33        | 28.74           | 12.23          | 258.57          |              |              | 14.00          | 35.57           |

Continuos on nout nos

| Time<br>(hrs | - Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-------------------|----------------|-----------------|--------------|-----------------|----------------|-----------------|
| 14.03        | 35.10             | 14.93          | 26.29           | 15.83        | 20.06           | 16.73          | 15.09           |
| 14.07        | 34.63             | 14.97          | 26.06           | 15.87        | 19.82           | 16.77          | 14.99           |
| 14.10        | 34.16             | 15.00          | 25.83           | 15.90        | 19.59           | 16.80          | 14.88           |
| 14.13        | 33.70             | 15.03          | 25.60           | 15.93        | 19.36           | 16.83          | 14.78           |
| 14.17        | 33.25             | 15.07          | 25.37           | 15.97        | 19.12           | 16.87          | 14.68           |
| 14.20        | 32.81             | 15.10          | 25.15           | 16.00        | 18.89           | 16.90          | 14.58           |
| 14.23        | 32.38             | 15.13          | 24.92           | 16.03        | 18.66           | 16.93          | 14.48           |
| 14.27        | 31.97             | 15.17          | 24.69           | 16.07        | 18.42           | 16.97          | 14.37           |
| 14.30        | 31.57             | 15.20          | 24.46           | 16.10        | 18.19           | 17.00          | 14.27           |
| 14.33        | 31.18             | 15.23          | 24.23           | 16.13        | 17.97           | 17.03          | 14.17           |
| 14.37        | 30.82             | 15.27          | 24.00           | 16.17        | 17.75           | 17.07          | 14.07           |
| 14.40        | 30.47             | 15.30          | 23.77           | 16.20        | 17.53           | 17.10          | 13.97           |
| 14.43        | 30.14             | 15.33          | 23.54           | 16.23        | 17.32           | 17.13          | 13.86           |
| 14.47        | 29.82             | 15.37          | 23.31           | 16.27        | 17.12           | 17.17          | 13.76           |
| 14.50        | 29.52             | 15.40          | 23.07           | 16.30        | 16.92           | 17.20          | 13.66           |
| 14.53        | 29.22             | 15.43          | 22.84           | 16.33        | 16.74           | 17.23          | 13.56           |
| 14.57        | 28.94             | 15.47          | 22.61           | 16.37        | 16.56           | 17.27          | 13.46           |
| 14.60        | 28.67             | 15.50          | 22.38           | 16.40        | 16.39           | 17.30          | 13.35           |
| 14.63        | 28.41             | 15.53          | 22.15           | 16.43        | 16.24           | 17.33          | 13.25           |
| 14.67        | 28.16             | 15.57          | 21.92           | 16.47        | 16.09           | 17.37          | 13.15           |
| 14.70        | 27.91             | 15.60          | 21.68           | 16.50        | 15.94           | 17.40          | 13.05           |
| 14.73        | 27.67             | 15.63          | 21.45           | 16.53        | 15.81           | 17.43          | 12.95           |
| 14.77        | 27.44             | 15.67          | 21.22           | 16.57        | 15.68           | 17.47          | 12.84           |
| 14.80        | 27.20             | 15.70          | 20.99           | 16.60        | 15.55           | 17.50          | 12.74           |
| 14.83        | 26.97             | 15.73          | 20.76           | 16.63        | 15.43           | 17.53          | 12.64           |
| 14.87        | 26.75             | 15.77          | 20.52           | 16.67        | 15.32           | 17.57          | 12.54           |
| 14.90        | 26.52             | 15.80          | 20.29           | 16.70        | 15.20           | 17.60          | 12.43           |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time (hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|-----------|-----------------|--------------|-----------------|
| 17.63        | 12.33           | 18.53          | 9.917           | 19.43     | 9.031           | 20.33        | 8.201           |
| 17.67        | 12.23           | 18.57          | 9.871           | 19.47     | 9.001           | 20.37        | 8.170           |
| 17.70        | 12.13           | 18.60          | 9.827           | 19.50     | 8.970           | 20.40        | 8.140           |
| 17.73        | 12.02           | 18.63          | 9.787           | 19.53     | 8.939           | 20.43        | 8.109           |
| 17.77        | 11.92           | 18.67          | 9.748           | 19.57     | 8.909           | 20.47        | 8.078           |
| 17.80        | 11.82           | 18.70          | 9.712           | 19.60     | 8.878           | 20.50        | 8.047           |
| 17.83        | 11.72           | 18.73          | 9.678           | 19.63     | 8.847           | 20.53        | 8.016           |
| 17.87        | 11.61           | 18.77          | 9.645           | 19.67     | 8.816           | 20.57        | 7.985           |
| 17.90        | 11.51           | 18.80          | 9.613           | 19.70     | 8.786           | 20.60        | 7.954           |
| 17.93        | 11.41           | 18.83          | 9.582           | 19.73     | 8.755           | 20.63        | 7.924           |
| 17.97        | 11.30           | 18.87          | 9.551           | 19.77     | 8.724           | 20.67        | 7.893           |
| 18.00        | 11.20           | 18.90          | 9.521           | 19.80     | 8.694           | 20.70        | 7.862           |
| 18.03        | 11.10           | 18.93          | 9.490           | 19.83     | 8.663           | 20.73        | 7.831           |
| 18.07        | 11.00           | 18.97          | 9.460           | 19.87     | 8.632           | 20.77        | 7.800           |
| 18.10        | 10.90           | 19.00          | 9.429           | 19.90     | 8.601           | 20.80        | 7.769           |
| 18.13        | 10.80           | 19.03          | 9.399           | 19.93     | 8.571           | 20.83        | 7.738           |
| 18.17        | 10.70           | 19.07          | 9.368           | 19.97     | 8.540           | 20.87        | 7.707           |
| 18.20        | 10.61           | 19.10          | 9.337           | 20.00     | 8.509           | 20.90        | 7.676           |
| 18.23        | 10.52           | 19.13          | 9.307           | 20.03     | 8.478           | 20.93        | 7.645           |
| 18.27        | 10.43           | 19.17          | 9.276           | 20.07     | 8.448           | 20.97        | 7.614           |
| 18.30        | 10.35           | 19.20          | 9.246           | 20.10     | 8.417           | 21.00        | 7.583           |
| 18.33        | 10.28           | 19.23          | 9.215           | 20.13     | 8.386           | 21.03        | 7.553           |
| 18.37        | 10.20           | 19.27          | 9.184           | 20.17     | 8.355           | 21.07        | 7.522           |
| 18.40        | 10.14           | 19.30          | 9.154           | 20.20     | 8.325           | 21.10        | 7.491           |
| 18.43        | 10.08           | 19.33          | 9.123           | 20.23     | 8.294           | 21.13        | 7.460           |
| 18.47        | 10.02           | 19.37          | 9.092           | 20.27     | 8.263           | 21.17        | 7.429           |
| 18.50        | 9.967           | 19.40          | 9.062           | 20.30     | 8.232           | 21.20        | 7.398           |

| Time (<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|-----------------|
| 21.23          | 7.367           | 22.13          | 6.983           | 23.03          | 6.310           | 23.93          | 5.679           |
| 21.27          | 7.336           | 22.17          | 7.075           | 23.07          | 6.287           | 23.97          | 5.656           |
| 21.30          | 7.305           | 22.20          | 7.171           | 23.10          | 6.263           | 24.00          | 5.633           |
| 21.33          | 7.274           | 22.23          | 7.270           | 23.13          | 6.240           | 24.03          | 5.570           |
| 21.37          | 7.243           | 22.27          | 7.374           | 23.17          | 6.217           | 24.07          | 5.467           |
| 21.40          | 7.212           | 22.30          | 7.481           | 23.20          | 6.193           | 24.10          | 5.325           |
| 21.43          | 7.181           | 22.33          | 7.593           | 23.23          | 6.170           | 24.13          | 5.145           |
| 21.47          | 7.150           | 22.37          | 7.536           | 23.27          | 6.147           | 24.17          | 4.925           |
| 21.50          | 7.119           | 22.40          | 7.478           | 23.30          | 6.123           | 24.20          | 4.667           |
| 21.53          | 7.088           | 22.43          | 7.419           | 23.33          | 6.100           | 24.23          | 4.370           |
| 21.57          | 7.057           | 22.47          | 7.358           | 23.37          | 6.077           | 24.27          | 4.035           |
| 21.60          | 7.026           | 22.50          | 7.295           | 23.40          | 6.053           | 24.30          | 3.661           |
| 21.63          | 6.995           | 22.53          | 7.231           | 23.43          | 6.030           | 24.33          | 3.250           |
| 21.67          | 6.964           | 22.57          | 7.165           | 23.47          | 6.007           | End            |                 |
| 21.70          | 6.932           | 22.60          | 7.097           | 23.50          | 5.983           | :::::L//G      |                 |
| 21.73          | 6.901           | 22.63          | 7.027           | 23.53          | 5.960           |                |                 |
| 21.77          | 6.870           | 22.67          | 6.956           | 23.57          | 5.937           |                |                 |
| 21.80          | 6.839           | 22.70          | 6.883           | 23.60          | 5.913           |                |                 |
| 21.83          | 6.808           | 22.73          | 6.808           | 23.63          | 5.890           |                |                 |
| 21.87          | 6.777           | 22.77          | 6.731           | 23.67          | 5.866           |                |                 |
| 21.90          | 6.746           | 22.80          | 6.652           | 23.70          | 5.843           |                |                 |
| 21.93          | 6.715           | 22.83          | 6.571           | 23.73          | 5.820           |                |                 |
| 21.97          | 6.684           | 22.87          | 6.488           | 23.77          | 5.796           |                |                 |
| 22.00          | 6.653           | 22.90          | 6.403           | 23.80          | 5.773           |                |                 |
| 22.03          | 6.730           | 22.93          | 6.380           | 23.83          | 5.750           |                |                 |
| 22.07          | 6.811_          | 22.97          | 6.357           | 23.87          | 5.726           |                |                 |
| 22.10          | 6.895           | 23.00          | 6.333           | 23.90          | 5.703           |                |                 |

# **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

### Hyd. No. 1

### Pre Development

| Hydrograph type | = SCS Runoff | Peak discharge     | = 381.94 cfs     |
|-----------------|--------------|--------------------|------------------|
| Storm frequency | = 100 yrs    | Time to peak       | = 12.33 hrs      |
| Time interval   | = 2 min      | Hyd. volume        | = 2,024,122 cuft |
| Drainage area   | = 97.910 ac  | Curve number       | = 81.000*        |
| Basin Slope     | = 0.0 %      | Hydraulic length   | = 0 ft           |
| Tc method       | = TR55       | Time of conc. (Tc) | = 27.4 min       |
| Total precip.   | = 7.95 in    | Distribution       | = Type III       |
| Storm duration  | = 24 hrs     | Shape factor       | = 484            |

<sup>\*</sup> Composite (Area/CN) =  $[(44.250 \times 73) + (8.070 \times 72) + (42.080 \times 89) + (3.000 \times 98) + (0.510 \times 71)] / 97.910$ 

### **Hydrograph Discharge Table**

( Printed values >= 1.00% of Qp.)

| Time<br>(hrs | Outflow cfs) | Time C<br>(hrs | Outflow<br>cfs) |       | Time<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | e Outflow<br>cfs) |
|--------------|--------------|----------------|-----------------|-------|--------------|-----------------|--------------|-------------------|
| 7.67         | 3.858        | 8.27           | 5.697           |       | 8.87         | 8.721           | 9.47         | 12.72             |
| 7.70         | 3.950        | 8.30           | 5.825           |       | 8.90         | 8.922           | 9.50         | 12.97             |
| 7.73         | 4.042        | 8.33           | 5.959           |       | 8.93         | 9.125           | 9.53         | 13.22             |
| 7.77         | 4.136        | 8.37           | 6.099           |       | 8.97         | 9.331           | 9.57         | 13.47             |
| 7.80         | 4.230        | 8.40           | 6.244           |       | 9.00         | 9.540           | 9.60         | 13.72             |
| 7.83         | 4.325        | 8.43           | 6.393           |       | 9.03         | 9.752           | 9.63         | 13.97             |
| 7.87         | 4.421        | 8.47           | 6.548           |       | 9.07         | 9.965           | 9.67         | 14.23             |
| 7.90         | 4.518        | 8.50           | 6.708           |       | 9.10         | 10.18           | 9.70         | 14.49             |
| 7.93         | 4.617        | 8.53           | 6.872           | 97.11 | 9.13         | 10.40           | 9.73         | 3 14.75           |
| 7.97         | 4.716        | 8.57           | 7.041           |       | 9.17         | 10.62           | 9.77         | 15.02             |
| 8.00         | 4.815        | 8.60           | 7.214           |       | 9.20         | 10.85           | 9.80         | 15.28             |
| 8.03         | 4.916        | 8.63           | 7.390           |       | 9.23         | 11.07           | 9.83         | 3 15.55           |
| 8.07         | 5.019        | 8.67           | 7.571           |       | 9.27         | 11.30           | 9.87         | 7 15.82           |
| 8.10         | 5.124        | 8.70           | 7.755           |       | 9.30         | 11.53           | 9.90         | 16.09             |
| 8.13         | 5.231        | 8.73           | 7.943           |       | 9.33         | 11.77           | 9.93         | 3 16.36           |
| 8.17         | 5.342        | 8.77           | 8.133           |       | 9.37         | 12.00           | 9.97         | 7 16.64           |
| 8.20         | 5.456        | 8.80           | 8.326           |       | 9.40         | 12.24           | 10.0         | 00 16.92          |
| 8.23         | 5.574        | 8.83           | 8.522           |       | 9.43         | 12.48           | 10.0         | 3 17.20           |

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| <b>-</b> · /   | N461  | T: C           | المراجعة | Tim  | e Ou  | #low             | Time  | Outflow |
|----------------|-------|----------------|----------|------|-------|------------------|-------|---------|
| Time (<br>(hrs | cfs)  | Time C<br>(hrs | cfs)     | (hrs |       | cfs)             | (hrs  | cfs)    |
| 10.07          | 17.48 | 10.97          | 29.51    | 11.  | 87 1  | 01.83            | 12.73 | 177.37  |
| 10.10          | 17.77 | 11.00          | 30.07    | 11.  | 90 1  | 13.59            | 12.77 | 157.35  |
| 10.13          | 18.07 | 11.03          | 30.65    | 11.  | 93 1  | 27.22            | 12.80 | 140.49  |
| 10.17          | 18.38 | 11.07          | 31.24    | 11.  | 97 1  | 43.94            | 12.83 | 126.99  |
| 10.20          | 18.70 | 11.10          | 31.86    | 12.  | .00 1 | 65.10            | 12.87 | 116.00  |
| 10.23          | 19.03 | 11.13          | 32.52    | 12.  | .03 1 | 90.53            | 12.90 | 106.66  |
| 10.27          | 19.37 | 11.17          | 33.24    | 12.  | .07 2 | 18.51            | 12.93 | 98.44   |
| 10.30          | 19.74 | 11.20          | 34.02    | 12.  | .10 2 | 47.28            | 12.97 | 91.27   |
| 10.33          | 20.12 | 11.23          | 34.88    | 12.  | .13 2 | 75.67            | 13.00 | 85.04   |
| 10.37          | 20.51 | 11.27          | 35.82    | 12.  | .17 3 | 03.22            | 13.03 | 79.67   |
| 10.40          | 20.92 | 11.30          | 36.87    | 12.  | .20 3 | 29.45            | 13.07 | 75.07   |
| 10.43          | 21.35 | 11.33          | 38.01    | 12.  | .23 3 | 52.82            | 13.10 | 71.16   |
| 10.47          | 21.79 | 11.37          | 39.26    | 12   | .27 3 | 370.79           | 13.13 | 67.87   |
| 10.50          | 22.24 | 11.40          | 40.60    | 12   | .30 3 | 80.59            | 13.17 | 65.10   |
| 10.53          | 22.71 | 11.43          | 42.02    | 12   | .33 3 | 81.94            | 13.20 | 62.76   |
| 10.57          | 23.18 | 11.47          | 43.54    | 12   | .37 3 | 377.06           | 13.23 | 60.78   |
| 10.60          | 23.67 | 11.50          | 45.13    |      |       | 368.19           | 13.27 | 59.05   |
| 10.63          | 24.17 | 11.53          | 46.85    |      |       |                  | 13.30 | 57.51   |
| 10.67          | 24.67 | 11.57          | 48.85    |      |       | 356.65<br>342.61 | 13.33 | 56.09   |
| 10.70          | 25.19 | 11.60          | 51.26    |      |       | 326.27           | 13.37 | 54.79   |
| 10.73          | 25.71 | 11.63          | 54.20    |      |       | 307.91           | 13.40 | 53.60   |
| 10.77          | 26.24 | 11.67          | 57.82    |      |       | 287.91           | 13.43 | 52.51   |
| 10.80          | 26.77 | 11.70          | 62.28    |      |       | 266.65           | 13.47 | 51.51   |
| 10.83          | 27.31 | 11.73          | 67.71    |      |       | 244.53           | 13.50 | 50.60   |
| 10.87          | 27.86 | 11.77          | 74.27    |      |       | 221.95           | 13.53 | 49.76   |
| 10.90          | 28.40 | 11.80          | 82.12    |      |       | 199.30           | 13.57 | 48.99   |
| 10.93          | 28.96 | 11.83          | 91.32    | 12   |       | 100.00           | 13.60 | 48.28   |
|                |       |                |          |      |       |                  |       |         |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|--------------|-----------------|----------------|-----------------|
| 13.63        | 47.61           | 14.53          | 34.04           | 15.43        | 26.59           | 16.33          | 19.41           |
| 13.67        | 46.98           | 14.57          | 33.73           | 15.47        | 26.32           | 16.37          | 19.22           |
| 13.70        | 46.39           | 14.60          | 33.43           | 15.50        | 26.04           | 16.40          | 19.04           |
| 13.73        | 45.81           | 14.63          | 33.14           | 15.53        | 25.77           | 16.43          | 18.87           |
| 13.77        | 45.25           | 14.67          | 32.86           | 15.57        | 25.49           | 16.47          | 18.70           |
| 13.80        | 44.70           | 14.70          | 32.58           | 15.60        | 25.22           | 16.50          | 18.55           |
| 13.83        | 44.14           | 14.73          | 32.31           | 15.63        | 24.94           | 16.53          | 18.40           |
| 13.87        | 43.58           | 14.77          | 32.04           | 15.67        | 24.67           | 16.57          | 18.26           |
| 13.90        | 43.02           | 14.80          | 31.77           | 15.70        | 24.39           | 16.60          | 18.12           |
| 13.93        | 42.46           | 14.83          | 31.50           | 15.73        | 24.12           | 16.63          | 17.99           |
| 13.97        | 41.90           | 14.87          | 31.23           | 15.77        | 23.84           | 16.67          | 17.86           |
| 14.00        | 41.34           | 14.90          | 30.96           | 15.80        | 23.56           | 16.70          | 17.74           |
| 14.03        | 40.77           | 14.93          | 30.68           | 15.83        | 23.29           | 16.73          | 17.62           |
| 14.07        | 40.22           | 14.97          | 30.41           | 15.87        | 23.01           | 16.77          | 17.50           |
| 14.10        | 39.67           | 15.00          | 30.14           | 15.90        | 22.74           | 16.80          | 17.38           |
| 14.13        | 39.12           | 15.03          | 29.87           | 15.93        | 22.46           | 16.83          | 17.26           |
| 14.17        | 38.59           | 15.07          | 29.60           | 15.97        | 22.18           | 16.87          | 17.14           |
| 14.20        | 38.08           | 15.10          | 29.32           | 16.00        | 21.91           | 16.90          | 17.02           |
| 14.23        | 37.58           | 15.13          | 29.05           | 16.03        | 21.63           | 16.93          | 16.90           |
| 14.27        | 37.10           | 15.17          | 28.78           | 16.07        | 21.36           | 16.97          | 16.78           |
| 14.30        | 36.65           | 15.20          | 28.51           | 16.10        | 21.09           | 17.00          | 16.65           |
| 14.33        | 36.22           | 15.23          | 28.23           | 16.13        | 20.82           | 17.03          | 16.53           |
| 14.37        | 35.81           | 15.27          | 27.96           | 16.17        | 20.56           | 17.07          | 16.41           |
| 14.40        | 35.42           | 15.30          | 27.69           | 16.20        | 20.31           | 17.10          | 16.29           |
| 14.43        | 35.05           | 15.33          | 27.41           | 16.23        | 20.07           | 17.13          | 16.17           |
| 14.47        | 34.70           | 15.37_         | 27.14           | 16.27        | 19.84           | 17.17          | 16.05           |
| 14.50        | 34.37           | 15.40          | 26.86           | 16.30        | 19.62           | 17.20          | 15.93           |

Continuos on nout nos

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|-----------------|
| 17.23        | 15.81           | 18.13          | 12.55           | 19.03          | 11.01           | 19.93          | 10.03           |
| 17.27        | 15.69           | 18.17          | 12.44           | 19.07          | 10.98           | 19.97          | 9.997           |
| 17.30        | 15.57           | 18.20          | 12.33           | 19.10          | 10.94           | 20.00          | 9.961           |
| 17.33        | 15.45           | 18.23          | 12.23           | 19.13          | 10.90           | 20.03          | 9.925           |
| 17.37        | 15.33           | 18.27          | 12.14           | 19.17          | 10.87           | 20.07          | 9.888           |
| 17.40        | 15.21           | 18.30          | 12.05           | 19.20          | 10.83           | 20.10          | 9.852           |
| 17.43        | 15.09           | 18.33          | 11.96           | 19.23          | 10.79           | 20.13          | 9.816           |
| 17.47        | 14.97           | 18.37          | 11.89           | 19.27          | 10.76           | 20.17          | 9.779           |
| 17.50        | 14.84           | 18.40          | 11.82           | 19.30          | 10.72           | 20.20          | 9.743           |
| 17.53        | 14.72           | 18.43          | 11.75           | 19.33          | 10.69           | 20.23          | 9.706           |
| 17.57        | 14.60           | 18.47          | 11.69           | 19.37          | 10.65           | 20.27          | 9.670           |
| 17.60        | 14.48           | 18.50          | 11.64           | 19.40          | 10.61           | 20.30          | 9.634           |
| 17.63        | 14.36           | 18.53          | 11.59           | 19.43          | 10.58           | 20.33          | 9.597           |
| 17.67        | 14.24           | 18.57          | 11.54           | 19.47          | 10.54           | 20.37          | 9.561           |
| 17.70        | 14.12           | 18.60          | 11.49           | 19.50          | 10.51           | 20.40          | 9.525           |
| 17.73        | 14.00           | 18.63          | 11.45           | 19.53          | 10.47           | 20.43          | 9.488           |
| 17.77        | 13.88           | 18.67          | 11.41           | 19.57          | 10.43           | 20.47          | 9.452           |
| 17.80        | 13.75           | 18.70          | 11.37           | 19.60          | 10.40           | 20.50          | 9.415           |
| 17.83        | 13.63           | 18.73          | 11.34           | 19.63          | 10.36           | 20.53          | 9.379           |
| 17.87        | 13.51           | 18.77          | 11.30           | 19.67          | 10.32           | 20.57          | 9.343           |
| 17.90        | 13.39           | 18.80          | 11.26           | 19.70          | 10.29           | 20.60          | 9.306           |
| 17.93        | 13.27           | 18.83          | 11.23           | 19.73          | 10.25           | 20.63          | 9.270           |
| 17.97        | 13.15           | 18.87          | 11.19           | 19.77          | 10.22           | 20.67          | 9.233           |
| 18.00        | 13.03           | 18.90          | 11.16           | 19.80          | 10.18           | 20.70          | 9.197           |
| 18.03        | 12.91           | 18.93          | 11.12           | 19.83          | 10.14           | 20.73          | 9.160           |
| 18.07        | 12.79           | 18.97          | 11.08           | 19.87          | 10.11           | 20.77          | 9.124           |
| 18.10        | 12.67           | 19.00          | 11.05           | 19.90          | 10.07           | 20.80          | 9.087           |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) |    | Time (<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|----|----------------|-----------------|----------------|-----------------|
| 20.83        | 9.051           | 21.73          | 8.064           |    | 22.63          | 8.140           | 23.53          | 6.966           |
| 20.87        | 9.014           | 21.77          | 8.028           |    | 22.67          | 8.032           | 23.57          | 6.939           |
| 20.90        | 8.978           | 21.80          | 7.991           |    | 22.70          | 7.921           | 23.60          | 6.911           |
| 20.93        | 8.941           | 21.83          | 7.955           |    | 22.73          | 7.807           | 23.63          | 6.884           |
| 20.97        | 8.905           | 21.87          | 7.918           |    | 22.77          | 7.691           | 23.67          | 6.856           |
| 21.00        | 8.869           | 21.90          | 7.881           |    | 22.80          | 7.571           | 23.70          | 6.829           |
| 21.03        | 8.832           | 21.93          | 7.845           |    | 22.83          | 7.543           | 23.73          | 6.801           |
| 21.07        | 8.796           | 21.97          | 7.808           |    | 22.87          | 7.516           | 23.77          | 6.773           |
| 21.10        | 8.759           | 22.00          | 7.771           |    | 22.90          | 7.488           | 23.80          | 6.746           |
| 21.13        | 8.723           | 22.03          | 7.894           |    | 22.93          | 7.461           | 23.83          | 6.718           |
| 21.17        | 8.686           | 22.07          | 8.022           |    | 22.97          | 7.434           | 23.87          | 6.691           |
| 21.20        | 8.650           | 22.10          | 8.155           |    | 23.00          | 7.406           | 23.90          | 6.663           |
| 21.23        | 8.613           | 22.13          | 8.293           |    | 23.03          | 7.379           | 23.93          | 6.636           |
| 21.27        | 8.576           | 22.17          | 8.437           |    | 23.07          | 7.351           | 23.97          | 6.608           |
| 21.30        | 8.540           | 22.20          | 8.587           | (Z | 23.10          | 7.324           | 24.00          | 6.581           |
| 21.33        | 8.503           | 22.23          | 8.742           |    | 23.13          | 7.296           | 24.03          | 6.495           |
| 21.37        | 8.467           | 22.27          | 8.903           |    | 23.17          | 7.269           | 24.07          | 6.351           |
| 21.40        | 8.430           | 22.30          | 9.070           |    | 23.20          | 7.241           | 24.10          | 6.150           |
| 21.43        | 8.394           | 22.33          | 8.988           |    | 23.23          | 7.214           | 24.13          | 5.892           |
| 21.47        | 8.357           | 22.37          | 8.904           |    | 23.27          | 7.186           | 24.17          | 5.576           |
| 21.50        | 8.321           | 22.40          | 8.818           |    | 23.30          | 7.159           | 24.20          | 5.204           |
| 21.53        | 8.284           | 22.43          | 8.729           |    | 23.33          | 7.131           | 24.23          | 4.774           |
| 21.57        | 8.247           | 22.47          | 8.637           |    | 23.37          | 7.104           | 24.27          | 4.289           |
| 21.60        | 8.211           | 22.50          | 8.543           |    | 23.40          | 7.076           | End            |                 |
| 21.63        | 8.174           | 22.53          | 8.446           |    | 23.43          | 7.049           | LIV            |                 |
| 21.67        | 8.138           | 22.57          | 8.347           |    | 23.47          | 7.021           |                |                 |
| 21.70        | 8.101           | 22.60          | 8.245           |    | 23.50          | 6.994           |                |                 |

# **Hydrograph Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

Friday, 01 / 29 / 2016

### Hyd. No. 2

### Post Development

| Hydrograph type<br>Storm frequency<br>Time interval<br>Drainage area<br>Basin Slope | = SCS Runoff<br>= 100 yrs<br>= 2 min<br>= 97.910 ac<br>= 0.0 % | Peak discharge Time to peak Hyd. volume Curve number Hydraulic length | = 366.39 cfs<br>= 12.37 hrs<br>= 2,049,422 cuft<br>= 81.000*<br>= 0 ft |
|---|--|---|--|
|   |  | •   | • •  |
| •   |  |   |  |
| •   |  |   |  |
| Tc method   | = TR55   | Time of conc. (Tc)  | = 30.4 min   |
| Total precip.   | = 7.95 in  | Distribution  | = Type III   |
| Storm duration  | = 24 hrs   | Shape factor  | = 484  |

<sup>\*</sup> Composite (Area/CN) =  $[(26.680 \times 73) + (8.070 \times 72) + (41.470 \times 89) + (0.685 \times 98) + (20.499 \times 79) + (0.510 \times 71)] / 97.910$ 

### **Hydrograph Discharge Table**

( Printed values >= 1.00% of Qp.)

| Time (<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow cfs) | Time C<br>(hrs | Outflow<br>cfs) |
|----------------|-----------------|----------------|-----------------|--------------|--------------|----------------|-----------------|
| 7.63           | 3.697           | 8.23           | 5.497           | 8.83         | 8.374        | 9.43           | 12.32           |
| 7.67           | 3.788           | 8.27           | 5.617           | 8.87         | 8.571        | 9.47           | 12.56           |
| 7.70           | 3.879           | 8.30           | 5.741           | 8.90         | 8.771        | 9.50           | 12.81           |
| 7.73           | 3.971           | 8.33           | 5.871           | 8.93         | 8.974        | 9.53           | 13.06           |
| 7.77           | 4.065           | 8.37           | 6.006           | 8.97         | 9.179        | 9.57           | 13.31           |
| 7.80           | 4.159           | 8.40           | 6.146           | 9.00         | 9.387        | 9.60           | 13.56           |
| 7.83           | 4.254           | 8.43           | 6.291           | 9.03         | 9.597        | 9.63           | 13.81           |
| 7.87           | 4.350           | 8.47           | 6.441           | 9.07         | 9.810        | 9.67           | 14.07           |
| 7.90           | 4.447           | 8.50           | 6.595           | 9.10         | 10.03        | 9.70           | 14.33           |
| 7.93           | 4.545           | 8.53           | 6.755           | 9.13         | 10.24        | 9.73           | 14.59           |
| 7.97           | 4.644           | 8.57           | 6.919           | 9.17         | 10.46        | 9.77           | 14.85           |
| 8.00           | 4.744           | 8.60           | 7.087           | 9.20         | 10.69        | 9.80           | 15.12           |
| 8.03           | 4.845           | 8.63           | 7.259           | 9.23         | 10.91        | 9.83           | 15.39           |
| 8.07           | 4.948           | 8.67           | 7.436           | 9.27         | 11.14        | 9.87           | 15.66           |
| 8.10           | 5.052           | 8.70           | 7.616           | 9.30         | 11.37        | 9.90           | 15.93           |
| 8.13           | 5.159           | 8.73           | 7.801           | 9.33         | 11.61        | 9.93           | 16.21           |
| 8.17           | 5.268           | 8.77           | 7.988           | 9.37         | 11.84        | 9.97           | 16.48           |
| 8.20           | 5.381           | 8.80           | 8.179           | 9.40         | 12.08        | 10.00          | 16.76           |

| Time<br>(hrs | Outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |    | Time (<br>(hrs       | Outflow<br>cfs) | Time (hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|----|----------------------|-----------------|-----------|-----------------|
| 10.03        | 17.04           | 10.93          | 28.59           |    | 11.83                | 84.33           | 12.70     | 234.45          |
| 10.07        | 17.33           | 10.97          | 29.15           |    | 11.87                | 93.50           | 12.73     | 214.71          |
| 10.10        | 17.62           | 11.00          | 29.71           |    | 11.90                | 103.87          | 12.77     | 195.02          |
| 10.13        | 17.91           | 11.03          | 30.28           |    | 11.93                | 115.94          | 12.80     | 175.70          |
| 10.17        | 18.22           | 11.07          | 30.87           |    | 11.97                | 130.71          | 12.83     | 157.39          |
| 10.20        | 18.53           | 11.10          | 31.48           |    | 12.00                | 149.30          | 12.87     | 140.92          |
| 10.23        | 18.86           | 11.13          | 32.13           |    | 12.03                | 171.55          | 12.90     | 127.07          |
| 10.27        | 19.19           | 11.17          | 32.82           |    | 12.07                | 196.09          | 12.93     | 115.88          |
| 10.30        | 19.54           | 11.20          | 33.57           |    | 12.10                | 221.50          | 12.97     | 106.69          |
| 10.33        | 19.91           | 11.23          | 34.38           |    | 12.13                | 246.84          | 13.00     | 98.80           |
| 10.37        | 20.29           | 11.27          | 35.26           |    | 12.17                | 271.74          | 13.03     | 91.82           |
| 10.40        | 20.69           | 11.30          | 36.22           | 72 | 12.20                | 295.82          | 13.07     | 85.67           |
| 10.43        | 21.10           | 11.33          | 37.27           |    | 12.23                | 318.68          | 13.10     | 80.31           |
| 10.47        | 21.52           | 11.37          | 38.42           |    | 12.27                | 339.09          | 13.13     | 75.67           |
| 10.50        | 21.96           | 11.40          | 39.66           | 17 | 12.30                | 355.00          | 13.17     | 71.67           |
| 10.53        | 22.41           | 11.43          | 40.98           |    | 12.33                | 364.19          | 13.20     | 68.26           |
| 10.57        | 22.88           | 11.47          | 42.39           |    | 12.37                | 366.39          | 13.23     | 65.38           |
| 10.60        | 23.35           | 11.50          | 43.88           |    | 12.40                | 363.31          | 13.27     | 62.94           |
| 10.63        | 23.84           | 11.53          | 45.49           |    | 12.43                | 356.73          | 13.30     | 60.89           |
| 10.67        | 24.33           | 11.57          | 47.34           |    | 12.47                | 347.69          | 13.33     | 59.16           |
| 10.70        | 24.84           | 11.60          | 49.54           |    | 12.50                | 336.33          | 13.37     | 57.66           |
| 10.73        | 25.35           | 11.63          | 52.19           |    | 12.53                | 322.86          | 13.40     | 56.31           |
| 10.77        | 25.88           | 11.67          | 55.41           |    | 12.57                | 307.59          | 13.43     | 55.06           |
| 10.80        | 26.41           | 11.70          | 59.32           |    | 12.60                | 290.81          | 13.47     | 53.91           |
| 10.83        | 26.94           | 11.73          | 64.04           |    | 12.63                | 272.82          | 13.50     | 52.84           |
| 10.87        | 27.49           | 11.77          | 69.70           |    | 12.67                | 253.93          | 13.53     | 51.86           |
| 10.90        | 28.04           | 11.80          | 76.42           |    | · <del>-</del> · • · |                 | 13.57     | 50.94           |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) |   | me<br>rs | Outflow<br>cfs) | Time (hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|---|----------|-----------------|-----------|-----------------|
| 13.60        | 50.10           | 14.50          | 35.32           | • | 15.40    | 27.57           | 16.30     | 20.20           |
| 13.63        | 49.31           | 14.53          | 34.97           |   | 15.43    | 27.29           | 16.33     | 19.98           |
| 13.67        | 48.58           | 14.57          | 34.63           |   | 15.47    | 27.01           | 16.37     | 19.77           |
| 13.70        | 47.89           | 14.60          | 34.30           |   | 15.50    | 26.74           | 16.40     | 19.57           |
| 13.73        | 47.24           | 14.63          | 33.99           |   | 15.53    | 26.46           | 16.43     | 19.38           |
| 13.77        | 46.62           | 14.67          | 33.68           |   | 15.57    | 26.18           | 16.47     | 19.20           |
| 13.80        | 46.02           | 14.70          | 33.39           | , | 15.60    | 25.90           | 16.50     | 19.03           |
| 13.83        | 45.44           | 14.73          | 33.10           | , | 15.63    | 25.62           | 16.53     | 18.86           |
| 13.87        | 44.88           | 14.77          | 32.81           | , | 15.67    | 25.35           | 16.57     | 18.71           |
| 13.90        | 44.31           | 14.80          | 32.53           |   | 15.70    | 25.07           | 16.60     | 18.56           |
| 13.93        | 43.74           | 14.83          | 32.26           |   | 15.73    | 24.79           | 16.63     | 18.41           |
| 13.97        | 43.18           | 14.87          | 31.98           |   | 15.77    | 24.51           | 16.67     | 18.27           |
| 14.00        | 42.61           | 14.90          | 31.71           |   | 15.80    | 24.23           | 16.70     | 18.14           |
| 14.03        | 42.04           | 14.93          | 31.43           |   | 15.83    | 23.95           | 16.73     | 18.01           |
| 14.07        | 41.48           | 14.97          | 31.16           |   | 15.87    | 23.67           | 16.77     | 17.88           |
| 14.10        | 40.92           | 15.00          | 30.88           |   | 15.90    | 23.39           | 16.80     | 17.76           |
| 14.13        | 40.36           | 15.03          | 30.61           |   | 15.93    | 23.11           | 16.83     | 17.63           |
| 14.17        | 39.82           | 15.07          | 30.33           |   | 15.97    | 22.83           | 16.87     | 17.51           |
| 14.20        | 39.29           | 15.10          | 30.06           |   | 16.00    | 22.55           | 16.90     | 17.39           |
| 14.23        | 38.77           | 15.13          | 29.78           |   | 16.03    | 22.27           | 16.93     | 17.27           |
| 14.27        | 38.27           | 15.17          | 29.51           |   | 16.07    | 22.00           | 16.97     | 17.15           |
| 14.30        | 37.79           | 15.20          | 29.23           |   | 16.10    | 21.72           | 17.00     | 17.03           |
| 14.33        | 37.33           | 15.23          | 28.95           |   | 16.13    | 21.45           | 17.03     | 16.90           |
| 14.37        | 36.89           | 15.27          | 28.68           |   | 16.17    | 21.18           | 17.07     | 16.78           |
| 14.40        | 36.47           | 15.30          | 28.40           |   | 16.20    | 20.92           | 17.10     | 16.66           |
| 14.43        | 36.07           | 15.33          | 28.12           |   | 16.23    | 20.67           | 17.13     | 16.54           |
| 14.47        | 35.69           | 15.37          | 27.85           |   | 16.27    | 20.43           | 17.17     | 16.42           |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | outflow<br>cfs) | Time (<br>(hrs | Outflow<br>cfs) |      | Time (<br>(hrs | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|----------------|-----------------|------|----------------|-----------------|
| 17.20        | 16.29           | 18.10          | 12.99           | 19.00          | 11.23           |      | 19.90          | 10.24           |
| 17.23        | 16.17           | 18.13          | 12.87           | 19.03          | 11.20           |      | 19.93          | 10.21           |
| 17.27        | 16.05           | 18.17          | 12.76           | 19.07          | 11.16           |      | 19.97          | 10.17           |
| 17.30        | 15.93           | 18.20          | 12.65           | 19.10          | 11.12           |      | 20.00          | 10.13           |
| 17.33        | 15.80           | 18.23          | 12.54           | 19.13          | 11.09           |      | 20.03          | 10.10           |
| 17.37        | 15.68           | 18.27          | 12.44           | 19.17          | 11.05           |      | 20.07          | 10.06           |
| 17.40        | 15.56           | 18.30          | 12.34           | 19.20          | 11.02           |      | 20.10          | 10.02           |
| 17.43        | 15.44           | 18.33          | 12.25           | 19.23          | 10.98           | (ii) | 20.13          | 9.987           |
| 17.47        | 15.32           | 18.37          | 12.16           | 19.27          | 10.94           |      | 20.17          | 9.951           |
| 17.50        | 15.19           | 18.40          | 12.08           | 19.30          | 10.91           |      | 20.20          | 9.914           |
| 17.53        | 15.07           | 18.43          | 12.01           | 19.33          | 10.87           |      | 20.23          | 9.877           |
| 17.57        | 14.95           | 18.47          | 11.94           | 19.37          | 10.83           |      | 20.27          | 9.840           |
| 17.60        | 14.83           | 18.50          | 11.88           | 19.40          | 10.80           |      | 20.30          | 9.803           |
| 17.63        | 14.70           | 18.53          | 11.82           | 19.43          | 10.76           |      | 20.33          | 9.766           |
| 17.67        | 14.58           | 18.57          | 11.76           | 19.47          | 10.72           |      | 20.37          | 9.730           |
| 17.70        | 14.46           | 18.60          | 11.71           | 19.50          | 10.69           |      | 20.40          | 9.693           |
| 17.73        | 14.34           | 18.63          | 11.66           | 19.53          | 10.65           |      | 20.43          | 9.656           |
| 17.77        | 14.21           | 18.67          | 11.62           | 19.57          | 10.61           |      | 20.47          | 9.619           |
| 17.80        | 14.09           | 18.70          | 11.57           | 19.60          | 10.58           |      | 20.50          | 9.582           |
| 17.83        | 13.97           | 18.73          | 11.53           | 19.63          | 10.54           |      | 20.53          | 9.545           |
| 17.87        | 13.84           | 18.77          | 11.49           | 19.67          | 10.50           |      | 20.57          | 9.508           |
| 17.90        | 13.72           | 18.80          | 11.45           | 19.70          | 10.47           |      | 20.60          | 9.472           |
| 17.93        | 13.60           | 18.83          | 11.42           | 19.73          | 10.43           |      | 20.63          | 9.435           |
| 17.97        | 13.48           | 18.87          | 11.38           | 19.77          | 10.39           |      | 20.67          | 9.398           |
| 18.00        | 13.35           | 18.90          | 11.34           | 19.80          | 10.36           |      | 20.70          | 9.361           |
| 18.03        | 13.23           | 18.93          | 11.31           | 19.83          | 10.32           |      | 20.73          | 9.324           |
| 18.07        | 13.11           | 18.97          | 11.27           | 19.87          | 10.28           |      | 20.77          | 9.287           |

| Time<br>(hrs | Outflow<br>cfs) | Time C<br>(hrs | Outflow<br>cfs) | Time<br>(hrs | Outflow<br>cfs) | Tim<br>(hrs |     | Outflow<br>cfs) |
|--------------|-----------------|----------------|-----------------|--------------|-----------------|-------------|-----|-----------------|
| 20.80        | 9.250           | 21.70          | 8.252           | 22.6         | 0 8.445         | 23          | .50 | 7.118           |
| 20.83        | 9.213           | 21.73          | 8.215           | 22.6         | 3 8.362         | 23          | .53 | 7.090           |
| 20.87        | 9.176           | 21.77          | 8.178           | 22.6         | 7 8.277         | 23          | .57 | 7.063           |
| 20.90        | 9.139           | 21.80          | 8.141           | 22.7         | 0 8.190         | 23          | .60 | 7.035           |
| 20.93        | 9.102           | 21.83          | 8.103           | 22.7         | 3 8.101         | 23          | .63 | 7.007           |
| 20.97        | 9.066           | 21.87          | 8.066           | 22.7         | 7 8.009         | 23          | .67 | 6.979           |
| 21.00        | 9.029           | 21.90          | 8.029           | 22.8         | 0 7.915         | 23          | .70 | 6.951           |
| 21.03        | 8.992           | 21.93          | 7.992           | 22.8         | 3 7.819         | 23          | .73 | 6.923           |
| 21.07        | 8.955           | 21.97          | 7.955           | 22.8         | 7 7.720         | 23          | .77 | 6.895           |
| 21.10        | 8.918           | 22.00          | 7.918           | 22.9         | 0 7.619         | 23          | .80 | 6.867           |
| 21.13        | 8.881           | 22.03          | 8.010           | 22.9         | 3 7.591         | 23          | .83 | 6.840           |
| 21.17        | 8.844           | 22.07          | 8.106           | 22.9         | 7 7.564         | 23          | .87 | 6.812           |
| 21.20        | 8.807           | 22.10          | 8.206           | 23.0         | 0 7.536         | 23          | .90 | 6.784           |
| 21.23        | 8.770           | 22.13          | 8.311           | 23.0         | 3 7.508         | 23          | .93 | 6.756           |
| 21.27        | 8.733           | 22.17          | 8.420           | 23.0         | 7.480           | 23          | .97 | 6.728           |
| 21.30        | 8.696           | 22.20          | 8.534           | 23.1         | 0 7.452         | 24          | .00 | 6.700           |
| 21.33        | 8.659           | 22.23          | 8.652           | 23.1         | 3 7.425         | 24          | .03 | 6.625           |
| 21.37        | 8.622           | 22.27          | 8.775           | 23.1         | 7 7.397         | 24          | .07 | 6.503           |
| 21.40        | 8.585           | 22.30          | 8.903           | 23.2         | 0 7.369         | 24          | .10 | 6.335           |
| 21.43        | 8.548           | 22.33          | 9.036           | 23.2         | 3 7.341         | 24          | .13 | 6.120           |
| 21.47        | 8.511           | 22.37          | 8.969           | 23.2         | 7.313           | 24          | .17 | 5.858           |
| 21.50        | 8.474           | 22.40          | 8.900           | 23.3         | 7.285           | 24          | .20 | 5.551           |
| 21.53        | 8.437           | 22.43          | 8.829           | 23.3         | 3 7.258         | 24          | .23 | 5.198           |
| 21.57        | 8.400           | 22.47          | 8.756           | 23.3         | 7.230           | 24          | .27 | 4.799           |
| 21.60        | 8.363           | 22.50          | 8.681           | 23.4         | 7.202           | 24          | .30 | 4.355           |
| 21.63        | 8.326           | 22.53          | 8.605           | 23.4         | 3 7.174         | 24          | .33 | 3.866           |
| 21.67        | 8.289           | 22.57          | 8.526           | 23.4         | 7.146           | 7274        | End |                 |

# **ATTACHMENT 5**

### Carbon Debt Analysis

SolarCity Corporation
Proposed 3.9 Megawatt Solar Facility
Old Forge Road
Rocky Hill, CT

SolarCity Corporation performed an analysis to determine whether the proposed solar array installation ("Project") at the referenced site ("Subject Property") has the ability to produce a net improvement in carbon reduction compared to the loss of approximately nine (9) acres of early successional woodland. This analysis accounts for the loss of the trees and the carbon associated with both the manufacture of the solar panels and the installation activities.

The Project requires the removal of 225 trees primarily consisting of autumn olive and similar small diameter species (less than 6" diameter at breast height). The results of this analysis demonstrate that the Project would begin to have a measurable net improvement in carbon reduction in less than three years. Consider the accounting of "carbon debt" in the following table - which includes the energy used and CO2 released during the manufacturing and installation of the solar arrays, as well as the existing and future carbon reduction derived from the trees to be displaced by the solar array<sup>1</sup> - and the subsequent payback analysis<sup>2</sup>.

<sup>&</sup>lt;sup>1</sup> The calculations used in determining amount of energy used and CO2e created in manufacture and installation of solar array uses industry standard data sourced from: The Environmental Protection Agency (EPA) CO2 emissions calculator; Franklin Life Cycle Analysis Database; NREL US Life Cycle Inventory; Aluminum Association Life Cycle Inventory; Ecoinvent Life Cycle Inventory; Annual Energy Review, EIA; DOE Life Cycle Inventory.

<sup>&</sup>lt;sup>2</sup> Tree CO2E calcs are based off volumetric equations by McClure, J. and Cost, N. (2010) and the component ratio method by Health et al. 2009. This estimation method is adopted by US Forest Service Forest Inventory Analysis (FIA) program and California's pre-compliance market (AB 32), is peer-reviewed and widely considered to be the standard methodology for calculating carbon sequestration. USDA/Forestry Service/ Northern Research Station: "Measurement guidelines for the sequestration of forest carbon." Pearson, Timothy R.H. Brown, Sandra L. Birdsey, Richard A. 2007.

| Carbon Debt &Payback of Solar Array (Original Case) | Energy (GJ) used in<br>Production | CO <sup>2</sup> e (Metric Tons) |  |  |
|---|-----------------------------------|---------------------------------|--|--|
| PV Modules  | 34524                             | 5959                            |  |  |
| Racking   | 862                               | 367                             |  |  |
| Module Interconnection                              | 65                                | 6                               |  |  |
| Junction Boxes                                      | 63                                | 16                              |  |  |
| Conduits and Fittings                               | 404                               | 79                              |  |  |
| Wire and Grounding Devices                          | 948                               | 136                             |  |  |
| Inverters and Transformers                          | 1629                              | 215                             |  |  |
| Grid Connections                                    | 157                               | 19                              |  |  |
| Office Facilities Concrete                          | 111                               | .32                             |  |  |
| Concrete  | 81                                | 38                              |  |  |
| Trees Removed (Current Stock2)                      | 0                                 | 225                             |  |  |
| Trees (Future Lost Carbon Reduction - 20<br>Years)  | 0                                 | 520                             |  |  |
| Total CO²e to Payback                               |                                   | 7613                            |  |  |
| Annual PV Production Benefits (- CO <sup>2</sup> e) | 5725                              | 3149                            |  |  |
| Carbon Payback of Solar Array (Yrs)                 |                                   | 2.4                             |  |  |

| System Size (W)           | 3,903,020 |
|---------------------------|-----------|
| System Size (MW)          | 3.9       |
| Acres Cleared (Estimated) | 9.0       |

# **ATTACHMENT 6**

### **Decommissioning Plan**

# SolarCity Corporation Old Forge Road Solar Facility Rocky Hill, CT

This Decommissioning Plan ("Plan") establishes the approach to conduct decommissioning activities for the permanent closure of the solar panels and appurtenant equipment at the Old Forge Road site ("Project" or "Facility") at the end of its useful life or the permanent cessation of its operation, whichever comes first. The Plan also describes the approach for removal and/or abandonment of facilities and equipment associated with the Facility and describes anticipated land-restoration activities.

As background, the Power Purchase Agreement ("PPA") for the Facility requires that no later than ninety (90) days after its expiration, all tangible property comprising the Facility must be removed from the site. The PPA also requires that the site be returned to its original condition, excepting ordinary wear and tear, including the removal of mounting and/or support structures for the solar modules.

# **DECOMMISSIONING ACTIVITIES**

In accordance with the PPA, decommissioning will involve removal and disposal or recycling of all Project components. All recyclable materials will be transported to the appropriate nearby recycling facilities. Any non-recyclable materials will be properly disposed of at a nearby landfill. Ninety-five percent (95%) or greater of the Facility's components will be recyclable.

### **Decommissioning Preparation**

Site decommissioning and equipment removal can take up to six (6) months to complete for a project of this size. Therefore, access roads, fencing and electrical power will temporarily remain in place for use by the decommissioning and site restoration workers until it is no longer needed. Demolition debris will be placed in temporary on-site storage areas pending final transportation and disposal/recycling according to the procedures listed below.

### Photovoltaic (PV) Equipment Removal and Recycling

During decommissioning, all Facility components that will not be used by the site owner will be removed from the site. Equipment removal will include any and all pad-mounted cabinets, wiring, solar modules, solar module racking, inverters, and panel boards. Pounded post foundations will be pulled up and removed. Any resulting holes will be backfilled with locally imported soil to match existing site soil conditions. The concrete transformer and interconnection equipment pads will be broken up and removed.

The demolition debris and removed equipment may be cut or dismantled in to pieces that can be safely lifted or carried with the on-site equipment being used. The majority of glass, steel and aluminum will be processed for transportation and delivery to the licensed off-site recycling

center. The solar modules will be transported to and recycled at the nearest facility that will accept them. Minimal non-recyclable materials are anticipated; these will be properly disposed of a the nearest qualified disposal facility.

### **Internal Power Collection System**

The DC and AC power collection system will be dismantled and removed. All conduit and cabling that is removed will be recycled.

#### **Access Roads**

The existing onsite access driveway will remain in place to accomplish decommissioning at the end of the Facility's life.

### **Security Fence**

The existing eight (8) foot high chain link perimeter security fence will remain in place and will not be removed during the decommissioning process.

#### **Interconnection Line**

The overhead interconnection cabling that connects the Facility to the Eversource distribution network will remain in place during decommissioning activities to provide electrics service onsite during decommissioning. At the time of decommissioning, if the Town determines that this electric service line will be beneficial for the future use of the site, the line may remain after decommissioning. If the line is not used, it will be removed pursuant to Eversource guidelines and transported offsite to the nearest recycling facility.

### SITE RECLAMATION

After the Project is completely decommissioned, and all Project equipment has been removed from the site, additional activities will be performed to return the property back to its preconstruction conditions, excepting ordinary wear and tear.

Any site restoration or monitoring activities completed on the site will comply with applicable regulations and requirements.

#### **Restoration Process**

The decommissioning process will remove Project-related structures and infrastructure as described in the previous sections. Following decommissioning, site reclamation activities will occur. Reclamation will restore landform features, vegetative cover, and hydrologic function after the closure of the facility. The process will involve (where needed) the replacement of topsoil and vegetation, as well as modification of site topography where necessary to bring the site back to substantially pre-construction conditions compatible with the adjacent surroundings.

Any excavated areas remain after removal of equipment pads or access road base material, will be backfilled and compacted with locally imported soil to match existing onsite soils, and hydro seeded with a seed mix to match existing onsite groundcover. Any other areas of lower than average ground surface level will receive similar treatment.

If any soils are compacted at levels that would affect successful re-vegetation, they will be decompacted. The method of de-compaction will depend on how compacted the soil has become over the life of the Project. Following de-compaction, re-contouring of the site will be conducted, if necessary, to return the site to approximately match the pre-construction surface conditions and the surrounding area conditions. Original site drainage characteristics will be restored if they have not been maintained. It is unlikely that a significant amount of earthwork will be required, because the Project construction plan calls for minimal disturbance of the site during Project construction. Grading activities will be limited to areas as shown on the design plans that require re-contouring. Efforts will be made to disturb as little of the natural drainages and existing natural vegetation that remain post-decommissioning as possible.

Any remaining bare earth areas will be hydro seeded with a seed mix to match existing onsite groundcover. Site restoration activities are anticipated to be limited, because the preconstruction conditions of the site are not planned to be significantly altered during Project construction. Also, any other activities that become necessary will be performed to return the site to a pre-construction condition.

### **Monitoring Activities**

The site will be monitored by SolarCity after site restoration activities are complete to confirm that any earthwork and re-vegetation were performed correctly. The site will be periodically inspected (at least quarterly) to check for any eroded earthwork or failed vegetation. Any deficiencies will be promptly corrected. This monitoring will continue for a period of one year, or until the site is re-developed for another future purpose, whichever comes first.

# **ATTACHMENT 7**

# Robinson + Cole

# [SAMPLE PUBLIC OFFICIALS LETTER]

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts

March 23, 2016

Via Certificate of Mailing

«Name\_and\_Address»

Re: SolarCity Corporation – Petition for Declaratory Ruling for the Construction and Operation of a Solar Photovoltaic Electric Generating Facility Off Old Forge Road in Rocky Hill, Connecticut

Dear «Salutation»:

This firm represents SolarCity Corporation ("SolarCity"). Pursuant to the requirements of Connecticut General Statutes § 16-50½(b), and Section 16-50½-40 of the Regulations of Connecticut State Agencies, enclosed is a copy of the above-referenced Petition for Declaratory Ruling. SolarCity intends to construct and operate a 3.9 MW solar photovoltaic electric generating facility on a portion of a 61.38-acre parcel off Old Forge Road in Rocky Hill. The property is owned by the Town of Rocky Hill. The SolarCity Petition will be filed with the Connecticut Siting Council on March 24, 2016.

If you have any questions regarding this Petition please contact me or the Siting Council directly at (860) 827-2935.

Sincerely,

Kenneth C. Baldwin

KCB/kmd Enclosure

14614114-v1

#### **CERTIFICATION OF SERVICE**

I hereby certify that on this 23<sup>rd</sup> day of March, 2016, copies of the Petition and attachments were sent first class mail, postage prepaid and via Certificate of Mailing, to the following:

#### **STATE OFFICIALS:**

The Honorable George Jepsen Attorney General Office of the Attorney General 55 Elm Street Hartford, CT 06106

Rob Klee, Commissioner Department of Energy and Environmental Protection 79 Elm Street Hartford, CT 06106

Raul Pino, M.D., M.P.H., Commissioner Department of Public Health 410 Capitol Avenue P.O. Box 340308, MS 13COM Hartford, CT 06134-0308

Karl J. Wagener, Executive Director Council on Environmental Quality 79 Elm Street P.O. Box 5066 Hartford, CT 06106

Steven K. Reviczky, Commissioner Department of Agriculture 165 Capital Avenue Hartford, CT 06106

Arthur House, Chairman Public Utilities Regulatory Authority 10 Franklin Square New Britain, CT 06051

Benjamin Barnes, Secretary Office of Policy and Management 450 Capitol Avenue Hartford, CT 06106 Catherine Smith, Commissioner Department of Economic and Community Development 505 Hudson Street Hartford, CT 06106

James P. Redeker, Commissioner Department of Transportation 2800 Berlin Turnpike Newington, CT 06111

Dora B. Schriro, Commissioner
Department of Emergency Services and Public Protection
Emergency Management and Homeland Security Division
1111 Country Club Road
Middletown, CT 06457

Jonathan A. Harris, Commissioner Department of Consumer Protection 115 Capitol Avenue Hartford, CT 06106

Melody A. Currey, Commissioner Department of Administrative Services 165 Capitol Avenue Hartford, CT 06106

Scott D. Jackson, Commissioner Department of Labor 200 Folley Brook Boulevard Wethersfield, CT 06109

### **ROCKY HILL TOWN OFFICIALS:**

Guy Scaife, Town Manager Town of Rocky Hill 761 Old Main Street Rocky Hill, CT 06067

Claudia Baio, Mayor Town of Rocky Hill 761 Old Main Street Rocky Hill, CT 06067 Philip Sylvestro, Chairman Planning and Zoning Commission Town of Rocky Hill 761 Old Main Street Rocky Hill, CT 06067

Kim Ricci Zoning Enforcement Officer, Town Planner Town of Rocky Hill 761 Old Main Street Rocky Hill, CT 06067

Edward Charamut, Chairman Open Space & Conservation Inland Wetlands Commission Town of Rocky Hill 761 Old Main Street Rocky Hill, CT 06067

### **CROMWELL TOWN OFFICIALS:**

Anthony J. Salvatore, Town Manager Town of Cromwell 41 West Street Cromwell, CT 06416

Enzo Faienza, Mayor Town of Cromwell 41 West Street Cromwell, CT 06416

Alice Kelly, Chairman
Planning and Zoning Commission
Town of Cromwell
41 West Street
Cromwell, CT 06416

Stuart Popper, Director Planning and Development Town of Cromwell 41 West Street Cromwell, CT 06416

Joseph Corlis, Chair
Inland Wetland and Watercourses Agency
Town of Cromwell
41 West Street
Cromwell, CT 06416

Scott Lamberson, Chairman Conservation Commission Town of Cromwell 41 West Street Cromwell, CT 06416

### STATE LEGISLATORS:

The Honorable Christie Carpino Representative – 32<sup>nd</sup> District Legislative Office Building, Room 4200 Hartford, CT 06106

The Honorable Antonio Guerrera Representative – 29<sup>th</sup> District Legislative Office Building, Room 2301 Hartford, CT 06106

The Honorable Paul Doyle Senator – 9<sup>th</sup> District Legislative Office Building, Room 3900 Hartford, CT 06106

### REGIONAL COUNCIL OF GOVERNMENTS:

Capital Region Council of Governments 241 Main Street, 4<sup>th</sup> Floor Hartford, CT 06106 Attn: Lyle Wray

Kenneth C. Baldwin, Esq. Robinson & Cole LLP

280 Trumbull Street Hartford, CT 06103

Telephone: (860) 275-8200

Attorneys for SolarCity Corporation

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|  | The Honorable George Jepsen Attorney General Office of the Attorney General 55 Elm Street Hartford, CT 06106                             |   |   |           |                  |                                  |
| a  | Rob Klee, Commissioner Department of Energy and Environmental Protection 79 Elm Street Hartford, CT 06106                                |   |   |           |                  | 2                                |
|  | Raul Pino, M.D., M.P.H., Commissioner Department of Public Health (10 Capitol, Avenue 10 D. Box 340308. MS 13COM Hartford, CT 06134-0308 |   |   |           |                  |                                  |
|  | Karl J. Wagener, Executive Director<br>Council on Environmental Quality<br>79 Em Street<br>P.O. Box 5066<br>Harrford, CT 06106           |   |   |           |                  |                                  |
| 1.0  | Steven K. Reviczky, Commissioner<br>Department of Agriculture<br>165 Capital Avenue<br>Hartford, CT 06106                                |   |   |           |                  |                                  |
| ·  | Arthur House, Chairman Public Utilities Regulatory Authority 10 Franklin Square New Britain, CT 06051                                    |   |   |           |                  |                                  |
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|  | Benjamin Bames, Secretary<br>Office of Policy and Management<br>4 50 Capitol Avenue<br>Hartford, CT 06106  |  | 7                        |   |                           |                |
| >  | Catherine Smith, Commissioner Department of Economic and Community Development 505 Hudson Street Hartford, CT 06106  |  |                          |   |                           |                |
| ia (ia   | James P. Redeker, Commissioner Department of Transportation 2800 Berlin Tumpike Newington, CT 06111  |  |                          |   |                           |                |
|  | Dora B. Schriro, Conmissioner Department of Emergency Services and Public Protection Emergency Management and Homeland Security Division HIII Country Clib Road Middletown, CT 06457 | Division                                       |                          |   |                           |                |
| *  | Jonathan A. Harris, Commissioner Department of Consumer Protection 115 Capitol Avenue Hartford, CT 06106   |  |                          |   |                           |                |
|  | Melody A. Currey, Commissioner<br>Department of Administrative Services<br>165 Capitol Avenue<br>Hartford, CT 06106  | vices  |                          |   |                           |                |
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|  | Scott D. Jackson, Commissioner Department of Labor -200 Folley Brook Boulevard Wethersfield, CT 06109                      |                  |   |   |                |
| g.   | Guy Scaife, Town Manager Town of Rocky Hill 761 Old Main Street Rocky Hill, CT 06067                                       |                  |   |   |                |
|  | Claudia Baio, Mayor<br>Town of Rocky Hill<br>7 fol Old Main Street<br>Rocky Hill, CT 06067                                 |                  | -   |   | >              |
|  | Philip Sylvestro, Chairman Planning and Zoning Commission Town of Rocky Hill 761 Old Main Street - Rocky Hill, CT 06067    |                  |   |   |                |
|  | Kim Ricci<br>Zoning Enforcement Officer, Town Planner<br>Town of Rocky Hill<br>761 Old Main Street<br>Rocky Hill, CT 06067 |                  |   |   |                |
|  | Edward Charamut, Chairman Open Space & Conservation Inland Wetlands Commission Town of Rocky Hill 761 Old Main Street      |                  |   |   | *              |
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|  | Anthony J. Salvatore, Town Manager Town of Cromwell 1 West Street Cromwell, CT 06416  | 150   |                                |   |   |                |
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|  | Alice Kelly, Chairman Planning and Zoning Commission Town of Conwell 14 Wes Street Cromwell, CT 06416                       |   |                                |   | 1   |                |
| E#   | Stuari Poppur, Director Planning and Development Town of Cronwell +1 West Street Cronwell, CT 06+16                         |   |                                |   | =   |                |
|  | Joseph Cortis, Chair<br>Infland Weltand and Watercourses Agency<br>Town of Cromwell<br>14 West Street<br>Cromwell, CT 06416 |   |                                |   |   |                |
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# **ATTACHMENT 8**

# Robinson + Cole

### [SAMPLE ABUTTERS LETTER]

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts

March 23, 2016

Via Certificate of Mailing

«Name and Address»

Re: SolarCity Corporation – Petition for Declaratory Ruling for the Construction and Operation of a Solar Photovoltaic Electric Generating Facility Off Old Forge Road in Rocky Hill, Connecticut

Dear «Salutation»:

This firm represents SolarCity Corporation ("SolarCity"). Pursuant to the requirements of Connecticut General Statutes § 16-50 $\underline{l}$ (b), and Section 16-50 $\underline{j}$ -40 of the Regulations of Connecticut State Agencies, enclosed is a copy of the above-referenced Petition for Declaratory. SolarCity intends to construct and operate a 3.9 MW solar photovoltaic electric generating facility on a portion of a 61.38-acre parcel off Old Forge Road in Rocky Hill. The property is owned by the Town of Rocky Hill. The SolarCity Petition will be filed with the Connecticut Siting Council on March 24, 2016. You are receiving this notice because you are listed as an owner of property that abuts the parcel on which the proposed solar generating facility is proposed to be located.

If you have any questions regarding this Petition please contact me or the Siting Council directly at (860) 827-2935.

Sincerely,

Kenneth C. Baldwin

Kung gmu-

Attachment

14603658-v1

### SOLARCITY CORPORATION

# ABUTTERS' CERTIFICATE OF MAILING MAP 18/LOT 93

# OLD FORGE ROAD ROCKY HILL, CONNECTICUT

I hereby certify that on this 23<sup>rd</sup> day of March, 2016, copies of the Petition and attachments were sent first class mail, postage prepaid and via Certificate of Mailing, to those abutting landowners listed below.

Kenneth C. Baldwin

### **ROCKY HILL**

|    | Map/Lot | Property Address     | Owner and Mailing Address   |
|----|---------|----------------------|---|
| 1, | 18/86   | 299 Dividend Road    | Harold O. Johndrow, Jr.<br>14 Chimney Crest Lane<br>Bristol, CT 06010                                   |
| 2. | 18/94   | 28 Belamose Avenue   | NOCARP LLC<br>P.O. Box 656<br>Rocky Hill, CT 06067  |
| 3  | 18/88   | 60 Belamose Avenue   | Belamose Business Park<br>c/o Semac Electrical Contractor<br>P.O. Box 638<br>New Britain, CT 06050-0638 |
| 4. | * 18/89 | R005 Belamose Avenue | Town of Rocky Hill<br>761 Old Main Street<br>Rocky Hill, CT 06067<br>Attn: Town Manager                 |
| 5, | 18/90   | R006 Belamose Avenue | Gardner Nurseries Inc.<br>460 Brook Street<br>Rocky Hill, CT 06067                                      |

|     | Map/Lot | Property Address                    | Owner and Mailing Address   |
|-----|---------|-------------------------------------|---|
| 6.  | 18/91   | R007Z Belamose Avenue               | John Russo, Tr.<br>321 West Service Road<br>Hartford, CT 06120  |
| 7.  | 18/92   | R006 Pleasant Valley Road           | John Russo, Tr.<br>321 West Service Road<br>Hartford, CT 06120  |
| 8.  | 17/157  | L002 Pleasant Valley Road           | Town of Rocky Hill<br>761 Old Main Street<br>Rocky Hill, CT 06067   |
| 9.  | 18/97   | 114 Old Forge Road                  | Trustees of The Sheet Metal Workers Local No. 40 Pension Fund 100 Old Forge Road Rocky Hill, CT 06067   |
| 10. | 18/83   | 89 Old Forge Road                   | Chemedray LLC<br>c/o Development Assocs.<br>P.O. Box 528<br>Agawam, MA 01001-0528   |
| 11. | 18/84   | 280 Dividend Road                   | McKesson Corporation<br>c/o Ryan LLC<br>2800 Post Oak Boulevard, Suite 4200<br>Houston, TX 77056  |
| 12. | 18/96   | 16 Old Forge Road                   | Sixteen Old Forge LLC<br>c/o Paul Uccello<br>101 Hammermill Road, Suite D<br>Rocky Hill, CT 06067   |
| 13. | 14/398  | L003Z Belamose Avenue<br>(Railroad) | Gareth D. Bye, Director of Legal Affairs Office of the Secretary State of Connecticut Office of Policy and Management 450 Capitol Avenue Hartford, CT 06106 |

### CROMWELL

|    | Map/Block/Lot | Property Address          | Owner and Mailing Address   |
|----|---------------|---------------------------|---|
| 1. | 60/51/77      | 674 Main Street           | Connecticut Light & Power P.O. Box 270 Hartford, CT 06106 Attn: Sal Giuliano, Corporate Property Management   |
| 2, | 53/63/17      | Wall Street<br>(Railroad) | Gareth D. Bye, Director of Legal Affairs Office of the Secretary State of Connecticut Office of Policy and Management 450 Capitol Avenue Hartford, CT 06106 |
| 3. | 69/50/44B     | Meadow Road               | Cromwell Fire District – Water Division<br>1 West Street<br>Cromwell, CT 06416  |



### Legend

Town of Rocky Hill Property (+/-61.4 acres)

X=X= Proposed Fenced Facility (+/-19 acres)

Existing Treeline/Clearing Limit
Project Area - Limit of Proposed Work (+/-24 acres)

→ CTDEEP Watercourse

### CTDEEP Waterbody

## Abutting Property Map/Lot: 1976 Approximate Assessor Parcel Boundary (CTDEEP)

(\_\_\_) Municipal Boundary

### **Abutters Map**

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut





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| Name and Address of Sender  Kenneth G. Baldwin, Esq.  Robinson & Cole LLP 280 Trumbull Street Hartford, CT 06103   | USPS Tracking Number<br>Firm-specific Identifier      |   |  |  |   |  |   |

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### **ENVIRONMENTAL ASSESSMENT**

# SOLAR FACILITY INSTALLATION OLD FORGE ROAD ROCKY HILL, CONNECTICUT HARTFORD COUNTY

Prepared for: SolarCity Corporation

**Prepared by:** 

All-Points Technology Corporation, P.C. 3 Saddlebrook Drive Killingworth, CT 06419

**March 2016** 

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# **Project Introduction**

All-Points Technology Corporation, P.C. ("APT") prepared this Environmental Assessment ("EA") on behalf of SolarCity Corporation ("SolarCity") for the proposed installation of an approximately 3.9 megawatt ("MW") solar-based electric generating facility the ("Project") in the Town of Rocky Hill, Connecticut (the "Town").

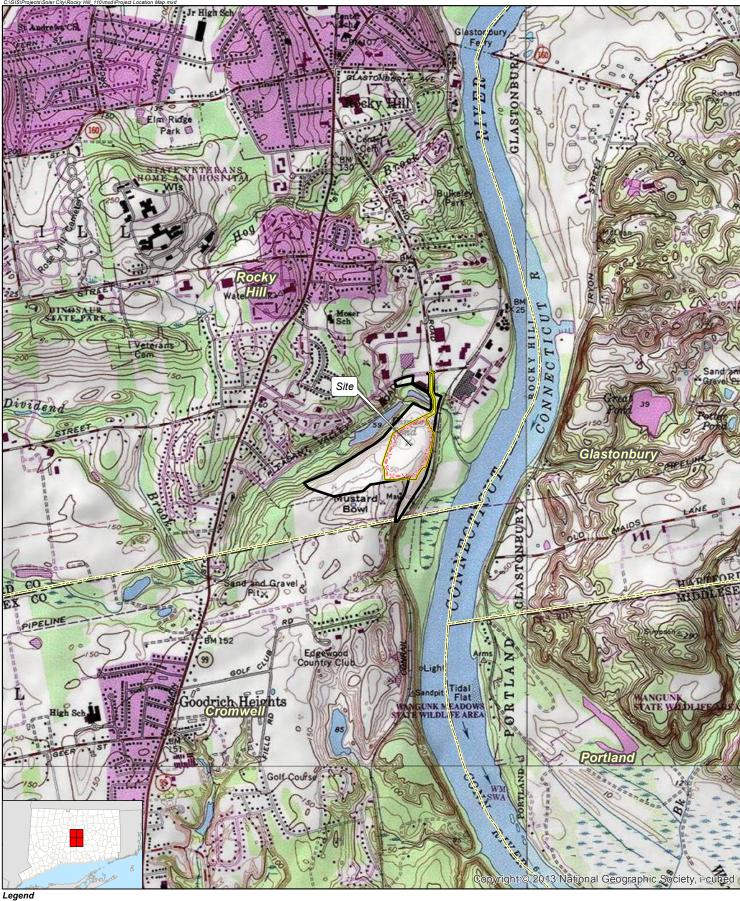
This EA has been completed to support SolarCity's submission of a petition for declaratory ruling that no Certificate of Environmental Compatibility and Public Need is required for the construction, maintenance, and operation of the Project.

The Project would be located south of Old Forge Road in Rocky Hill, Connecticut ("Site"). The municipally-owned Site consists of approximately 61.38 undeveloped acres, a portion of which is used by the Town for materials storage.

The Site is situated generally south of the intersection of Old Forge Road and Dividend Road, southeast of Town-owned open space (the "Dividend Pond Open Space Property"), west of an active rail line and the Connecticut River, and north of the municipal border with Cromwell. The immediate Site vicinity is characterized as a mix of residential and commercial development to the north and west, and undeveloped land to the east and south.

Upon its completion, the proposed solar array ("facility") would occupy approximately 19 acres of the Site. The facility would be comprised of approximately 9,460 – 275 watt and 4,488 – 290 watt Trina Solar TSM-PD14 modules, three (3) Advanced Energy AE 500TX 500 kW inverters, and three (3) transformers. The facility would use a post-driven RBI Solar Inc. racking system. To facilitate development of the facility, a total of approximately 24 acres require some level of disturbance ("Project Area").

Figure 1, Project Location Map, depicts the location of the Site and surrounding area.



Site Boundary

Project Area - Limit of Proposed Work (+/-24 acres) Proposed Fenced Facility (+/-19 acres)

Municipal Boundary

Map Notes:
Base Map Source: USGS 7.5 Minute Topographic Quadrangle Maps,
Glastonbury (1992), Harford South (1992), Middle Haddam (1984),
and Middletown (1992), CT
Site located on the Hartford South Quadrangle
Map Scale: 1:24,000
Map Date: February 2016



### Figure 1 **Project Location Map**

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut



# **Existing Conditions**

The purpose of this section is to describe current conditions of the Site. A detailed discussion of the proposed Project's effects on the environment is provided in following sections of this document.

### **Project Location**

The Site consists of a single, Town-owned parcel located south of Old Forge Road, encompassing a total of approximately 61.38 acres. The Site is undeveloped and portions are heavily disturbed by historic clearing and excavation activities. Several areas are currently used by the Town's Department of Public Works ("DPW") for materials storage, including asphalt millings, street sweepings, sand, top soil, leaves, brush and mulch.

The Project Area consists of approximately 24-acres of undeveloped, lightly wooded land, a portion of which is currently used by the Town for materials storage. Upon completion, the facility will occupy approximately 19 acres.

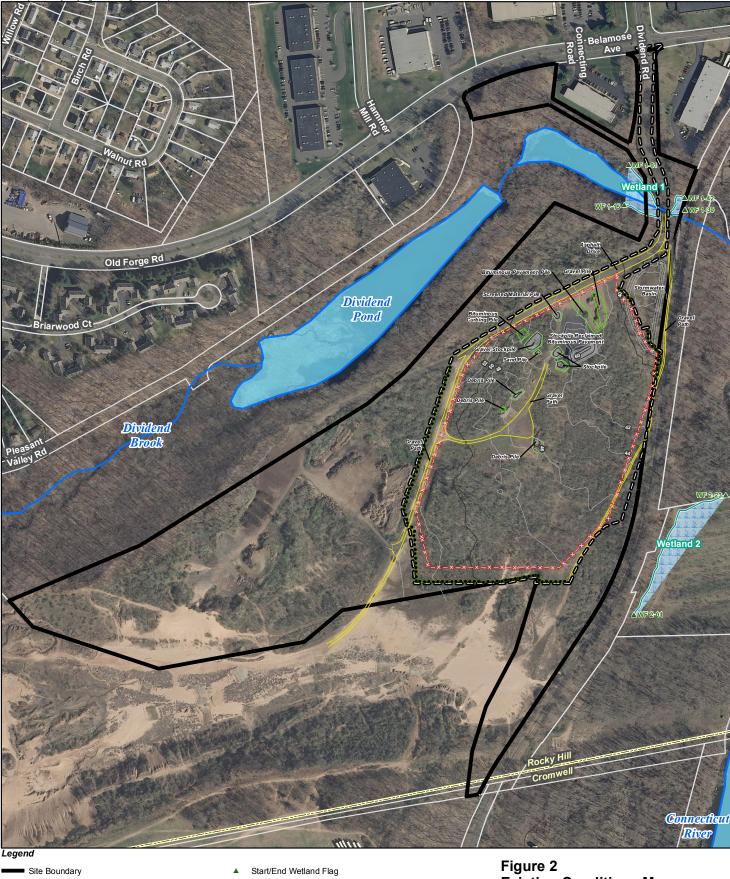
### **Site Access**

Access to the Site is over an existing, gated drive originating at the intersection of Old Forge Road and Dividend Road in its northern portion. The existing access drive extends south into the Site where it connects to a system of interior dirt roads.

Figure 2, *Existing Conditions Map*, depicts current conditions on the Site, its access, abutting properties, and several features discussed herein.

### **Wetlands and Watercourses**

Matthew Gustafson, a Connecticut registered Soil Scientist with APT, conducted an inspection of the Site on September 3, 2015 to determine the presence and extent of wetland resources proximate to the proposed Project Area. Two (2) wetland areas were delineated on the Site. A copy of the APT *Inland Wetland & Watercourse Report* prepared by Mr. Gustafson and *Photo-Documentation* of existing resources at the Site are included as Appendix A. The wetland resources are summarized below and depicted on Figure 2.



Existing Access Drive

Existing Materials Pile

10' Contour Line

2' Contour Line

X=X= Proposed Fenced Facility (+/-19 acres)

\*\*\*\* Existing Treeline/Clearing Limit

Project Area - Limit of Proposed Work (+/-24 acres)

Map Notes:
Base Map Source: 2012 Aerial Photograph (CTECO)
Map Scale: 1 inch = 400 feet
Map Date: February 2016

Delineated Wetland Boundary

Wetland Area

CTDEEP Watercourse CTDEEP Waterbody

Approximate Assessor Parcel Boundary (CTDEEP)

Municipal Boundary

# **Existing Conditions Map**

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut



**Wetland 1** consists of an open water resource ("Dividend Pond") located on the adjacent Dividend Pond Open Space Property and a perennial watercourse ("Dividend Brook"). This brook outlets from Dividend Pond, flowing eastward beneath the existing gravel access road through a large reinforced concrete pipe culvert, and, under an existing railroad line off the Site. It eventually enters the Connecticut River approximately 800 feet west of the Project Area. The margins of Wetland 1 are entirely forested with sparse scrub/shrub and emergent vegetation present. Banks to the resource are steeply sloping with little to no bordering vegetated wetland areas.

**Wetland 2** consists of the semi-active floodplain associated with several backwater wetland areas that border the Connecticut River. The western edge of the delineated resource consists of steeply sloping embankments. The northern edge is more moderately sloped with a broader transition zone from wetlands to uplands. The primary vegetation/ habitat class associated with Wetland 2 is open field with edge forested areas and transitional scrub/shrub ecotones separating the two. Observed soil profiles reveal these areas flood irregularly and are consistent with moderately well drained and well drained floodplain soils.

### **Vernal Pools**

Calhoun and Klemens (2002) provides the following operational definition of vernal pools:

Vernal pools are seasonal bodies of water that attain maximum depths in the spring or fall, and lack permanent surface water connections with other wetlands or water bodies. Pools fill with snowmelt or runoff in the spring, although some may be fed primarily by groundwater sources. The duration of surface flooding, known as hydroperiod, varies depending upon the pool and the year; vernal pool hydroperiods range along a continuum from less than 30 days to more than one year. Pools are generally small in size (<2 acres), with the extent of vegetation varying widely. They lack established fish populations, usually as a result of periodic drying, and support communities dominated by animals adapted to living in temporary, fishless pools. In the region, they provide essential breeding habitat for one or more wildlife species including Ambystomid salamanders (Ambystoma spp., called "mole salamanders" because they live in burrows), wood frogs (Rana sylvatica), and fairy shrimp (Eubranchipus spp.).

Vernal pool physical characteristics can vary widely while still providing habitat for indicator species. "Classic" vernal pools are natural depressions in a wooded upland with no hydrologic connection to other wetland systems. Often, vernal pools are depressions or impoundments

within larger wetland systems. These vernal pool habitats are commonly referred to as "cryptic" vernal pools.

A vernal pool habitat survey was performed in parallel with other wetland and biological surveys. Areas within 750 feet of the Site were inspected for the potential of supporting vernal pool breeding habitat. No areas potentially supporting vernal pool habitat are located within 750 feet of the Site. No vernal pool habitat was identified in either of the wetland areas (Wetlands 1 and 2) at the Site.

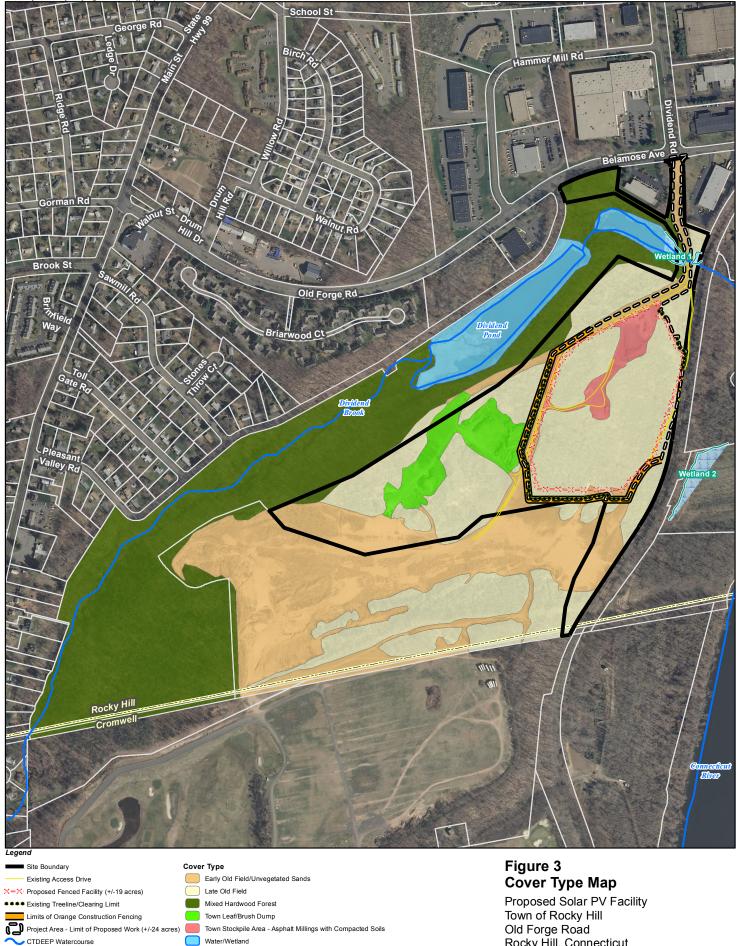
### **Vegetation and Wildlife**

The Project Area is located primarily within an area of Late Old Field habitat with limited areas currently used by Town of Rocky Hill DPW as "Town Stockpile Areas". The entirety of the Site was historically a sand/gravel quarry resulting in the mosaic of habitats. Additional habitat types are located in the vicinity of the Project Area including Early Old Field/Unvegetated Sands, Mixed Hardwood Forest, Town Leaf/Brush Dump, and Open Water/Wetland Areas. These vegetative communities are depicted on Figure 3, *Cover Type Map* and described below.

**Mixed Hardwood Forest:** This habitat type comprises the relatively small northern edges of the Site that extends off-Site to the north and west. These forested areas are dominated by complexes of sugar maple (*Acer saccharum*), red oak (*Quercus rubra*), and white ash (*Fraxinus americana*). The forest is characterized as even aged with a mix of open and closed canopy areas. Edge/open canopy forested areas consist of greater understory growth dominated by autumn olive (*Elaeagnus umbellata*), mugwort (*Artemisia vulgaris*), and various other invasive plant species. Richer forested areas are characterized by a more closed canopy with an understory dominated by spicebush (*Lindera benzoin*).

Since this small forest block has been fragmented (mostly consisting of 'edge' forest with limited 'core' forest habitat present located to the far west), habitat favored by larger wildlife species is not ideal. Generalist wildlife species that are tolerant of human disturbance would be expected such as raccoon (*Procyon lotor*), striped skunk (*Mephitis mephitis*), grey squirrel (*Sciurus carolinensis*), Virginia opossum (*Didelphus virginiana*), and eastern chipmunk (*Tamias striatus*).

<sup>&</sup>lt;sup>1</sup> Consistent with the extent of the *Critical Terrestrial Habitat* (750 feet) conservation zone surrounding vernal pools as established by Calhoun and Klemens.



Delineated Wetland Boundary Wetland Area Approximate Assessor Parcel Boundary (CTDEEP) Map Notes: Base Map Source: 2012 Aerial Photograph (CTECO) Map Scale:1 inch = 625 feet Map Date: February 2016

Municipal Boundary

Rocky Hill, Connecticut



Larger species such as coyote (*Canis latrans*), grey fox (*Urocyon cinereoargunteus*), white tailed deer (*Odocoileus virginianus*) and fisher (*Martes pennant*) also potentially take advantage of this habitat.

**Early Old Field/Unvegetated Sands:** This habitat type comprises the second largest area within the Site but is primarily located beyond the limits of the Project Area. The Early Old Field/Unvegetated Sands habitat type consists of large expanses of open sand escarpments in complex with herbaceous and scrub/shrub 'islands' or sparse intermixed vegetation. Any vegetation present in this habitat block is stunted as a result of the sandy substrate and infertile soils. Limited vegetation consists of mugwort, autumn olive, trembling aspen (seedling/sapling), solidago (goldenrods), and various other grasses/sedges/forbs. This habitat type is considered a rare habitat type in Connecticut. Discussion of the wildlife habitat value of this habitat type is discussed further in the Big Sand Tiger Beetle Habitat Assessment and Habitat Types and Their Importance to Birds sections.

Late Old Field Habitat: This represents the largest habitat type on the Site and within the Project Area. Late Old Field habitat is segmented by other habitat types as a result of current uses of the Site. This habitat type consists of a complex of early successional trees with a dense understory dominated by patches of both scrub/shrub and herbaceous growth. The tree stratum is dominated by trembling aspen (Populus trembloides) with individual black willow (Salix nigra) trees present. The scrub/shrub stratum is dominated by autumn olive, Bebb willow (Salix bebbiana), staghorn sumac (Rhus typhina). The herbaceous stratum is dominated by mugwort, rough horsetail (Equisetum hyemale), and solidago species. The dominance of the three strata varies across this habitat type resulting in complex vertical structure. This complex vertical structure, in combination with the early successional habitat type (an uncommon habitat type in Connecticut) is favored by many wildlife species. However, the dominance of invasive species somewhat diminishes the habitat value of these areas. Discussion of the wildlife value of this habitat type is discussed further in the Habitat Types and Their Importance to Birds section.

**Open Water/Wetland:** This habitat type comprises a small percentage of the Site and is associated with both the Connecticut River floodplain located to the east and Dividend Pond/Dividend Brook located to the north/northwest. Edges of Dividend Pond/Dividend Brook are primarily forested with little to no bordering vegetated wetland areas. This wetland

resource drains west to east eventually out-letting into the Connecticut River. An existing access road crossing provides entrance to the Project Area off Dividend Road. The Connecticut River floodplain area delineated as Wetland 2 is isolated from the Project Area by a railroad line that runs north to south bordering the eastern edge of the Project Area. Dominant vegetation is consistent with the information provided in the *Inland Wetland & Watercourse Report* (Appendix A).

**Town Stockpile Areas:** This habitat type is isolated to northern and central areas of the Project Area. The stockpile areas consist of material storage piles of asphalt millings underlain by compacted soils. Additional areas of this habitat type consist of a paved access drive that serves the DPW. These areas are largely devoid of vegetation making them generally unsuitable for wildlife use.

**Town Leaf/Brush Dump:** This habitat type comprises areas to the west of the Project Area and consists of large leaf and brush storage piles. This habitat type is largely devoid of mature vegetation and, due to the storage of brush and leaves, has limited value to wildlife (mostly small mammals and birds) for cover and foraging.

### **Rare Species**

The Connecticut Department of Energy and Environmental Protection ("CTDEEP") Natural Diversity Data Base ("NDDB") program performs hundreds of environmental reviews each year to determine the impact of proposed development projects on state listed species and to help landowners conserve the state's biodiversity. State agencies are required to ensure that any activity authorized, funded or performed by a state agency does not threaten the continued existence of endangered or threatened species. Maps have been developed to serve as a prescreening tool to help applicants determine if there is a potential impact to state listed species.

The NDDB maps represent approximate locations of endangered, threatened and special concern species and significant natural communities in Connecticut. The locations of species and natural communities depicted on the maps are based on data collected over the years by CTDEEP staff, scientists, conservation groups, and landowners. In some cases an occurrence represents a location derived from literature, museum records and/or specimens. These data are compiled and maintained in the NDDB. The general locations of species and communities are symbolized as shaded (or cross-hatched) areas on the maps. Exact locations have been

masked to protect sensitive species from collection and disturbance and to protect landowner's rights whenever species occur on private property.

APT reviewed the most recent CTDEEP NDDB mapping (August 2015) to determine if any such species or habitats occur within the vicinity of the Site. Based on the NDDB mapping, the southwestern portion of the Site is located within a shaded area. In addition, additional shaded areas are depicted immediately east of the Site. See Appendix B, *CTDEEP NDDB Mapping*. On September 5, 2015, APT submitted a review request to the CTDEEP NDDB with respect to this Project to determine what, if any, Threatened, Endangered, or Special Concern species or critical habitats exist at the Site. The CTDEEP responded via email on October 13, 2015 that State Special Concern Species *Cicindela formosa generosa* (Big Sand Tiger Beetle) is known to occur in the general area of the Site.<sup>2</sup>

The Big Sand Tiger Beetle ("tiger beetle") is a dry-habitat species that is found on yellow-to-white shifting sand with sparse vegetation. The species is found in short grass and weeds near the edges of sand dunes; in old, seldom-used road cuts, sand pits and seashores; and in pine barrens (Leonard and Bell, 1999). The species has a two-year life cycle and is active from spring through fall. They can be found from late April through July, rarely in August, and again in late August through September (Leonard and Bell, 1999).

While published information varies, it is generally accepted that adults die in early fall while larvae become inactive and overwinter in their burrows. Larval burrows are found in sand substrates that are loose, deep and well drained. *C. Formosa* larvae dig a small pit at the mouth of the burrow that serves as a pitfall for prey. The larval tunnel runs horizontally from the pit and then extends downward deep into the substrate. Sand about the pit and tunnel entrance is cemented by the larvae, which helps prevent the pit from collapsing.

### **Big Sand Tiger Beetle Habitat Assessment**

Due to the timing of the Project initiation and resultant CTDEEP correspondence, it was not possible to directly survey the Site for the physical presence of the tiger beetle. Therefore, a habitat-based survey was conducted using the known habitat requirements as summarized by

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<sup>&</sup>lt;sup>2</sup> CTDFFP NDDB #201505939

Leonard and Bell (1999). Assessments of the Site and immediately surrounding environs were conducted to identify areas that contained loose and shifting sparsely vegetated sandy soils.

The Site is part of a larger contiguous habitat matrix that includes three separate parcels: (1) the Site; (2) the Dividend Pond Open Space Property to the northwest; and, (3) a privately owned parcel to the south. Collectively, these three (3) parcels were formerly used as a sand and gravel borrow pit. The habitat which developed after abandonment of the mining operations includes environments that are optimal for tiger beetle. However, the habitats within the Project Area represent unsuitable or, at best, highly marginal habitat for tiger beetle.

The lack of optimal tiger beetle habitat within the Project Area is a result of both the current Town activities as well as natural vegetative succession. The Project Area includes land presently used by the Rocky Hill DPW to store asphalt millings as well as sand and topsoil. This area is actively used and includes a stockpile area with access drives entering from the north and west. The stockpile area and access drives have been graded, compacted and coated with asphalt millings. These areas encompass approximately two (2) acres of the total Project Area and do not constitute suitable habitat for tiger beetle due to the soil surface conditions. The remainder of the Project Area consists of Late Old Field habitat which is beginning to transition to immature woodland. The woody stem density is high throughout most of the Project Area, consisting predominately of mature autumn olive shrubs. Where woody vegetation is absent, a dense cover of common mugwort blankets the ground. As a result, the Project Area contains no appreciable unvegetated or sparsely vegetated loose sands.

Conversely, areas within the adjoining parcel to the south contain optimal tiger beetle habitat in the form of large expanses of loose, shifting unvegetated sands. Succession in these areas has been stunted to a large degree by four-wheel drive activity.

### **Breeding Bird Inventory**

Eric Davison of Davison Environmental, LLC conducted a breeding bird assessment of the Site on behalf of APT, Inc. This assessment focuses on species considered to be of high

conservation priority in Connecticut as designated in the 2015 Connecticut Wildlife Action Plan³ ("WAP"). The WAP was created to establish a framework for proactively conserving Connecticut's fish and wildlife, including their habitats. The WAP identifies Species of Greatest Conservation Need ("GCN species") that fall into three categories in descending order of significance from "most important" to "very important" and finally "important".

GCN species are those species that are considered of high conservation priority based on the consideration of such factors as: population trends and overall abundance; conservation threats associated with the species or its habitat; negative trends associated with the species' primary habitat; and the State's responsibility in the species overall conservation (i.e., the relative importance of Connecticut to the conservation of the species compared to other states in the species' range).

A total of 335 birds are found in Connecticut, over 170 of which nest in the State. There are a total of 95 GCN bird species in Connecticut, with 22 listed in the "most important" category, 38 are "very important" and 35 are "important".

The *Breeding Bird Inventory Table* provided in Appendix C includes a list of birds that potentially breed on the Site based on the presence of suitable habitat. This list was generated from a database that was developed by reviewing information on the habitat utilization of Connecticut's breeding birds. The primary resource for habitat utilization data was Bevier (Ed., 1994), with A. Poole (1995) and DeGraaf and Yamasaki (2001) utilized as secondary resources. The initial inventory, generated solely based on the presence of suitable habitat, was refined by considering such factors as bio-geographical distribution, the presence or absence of critical habitat features and minimum patch size requirements. The inventory is subdivided by habitat type. A species is listed under the habitat(s) which occupy the species typical home range. However, given that habitats are generally connected by transitional ecotones, a species should be considered to be potentially present within the ecotones associated with their primary habitat(s).

<sup>&</sup>lt;sup>3</sup> The Wildlife Action Plan, formerly Connecticut's Comprehensive Wildlife Conservation Strategy (2005) is currently in draft form on the CT DEEP website at: http://www.ct.gov/deep/cwp/view.asp?a=2723&g=329520&deepNav\_GID=1719#Review

Note that the inventory includes birds observed during habitat assessment work conducted on October 27, 2015. All birds seen or heard were noted as observed in the inventory table. Due to timing of field investigations, species observed were restricted to a small number of migratory and winter resident species.

### **Habitat Types and Their Importance to Birds**

The Project Area is part of a larger contiguous habitat matrix that includes the Dividend Pond Open Space Property and the fallow quarry property to the south. When considering this contiguous habit as a whole, a significant and high value early-successional habitat unit is present for shrubland birds.

A single habitat type - Late Old Field - dominates the 24-acre Project Area. Approximately three (3) of these acres is occupied by the active Town Stockpile Areas and approximately three (3) acres by Early/Old Field/Unvegetated Sands (existing roadways). These areas do not represent breeding or feeding habitat for birds of any kind. Therefore, the functional Old Field habitat present within the Project Area totals approximately 18 acres.

When evaluating the Project Area alone, several factors limit its value for birds. The late successional stage of the habitat has resulted in the development of a dense monoculture of autumn olive. As a result, both plant species diversity and vegetative structural diversity of this habitat is low and therefore less likely to support a wide array of Old Field habitat specialists. As succession continues to progress, the Project Area will no longer be as suitable for those shrubland birds that may now use this habitat. Despite the Project Area's degraded state and late successional stage, it is still capable of supporting several habitat specialists such as the field sparrow (*Spizella pusilla*) or blue-winged warbler (*Vermivora pinus*).

Due to the habitat homogeneity of the Project Area, the list of birds potentially breeding on the Site is small and restricted to species that utilize late old field habitat. A total of 20 birds are identified in the *Breeding Bird Inventory Table (Appendix C)*. This includes 10 GCN species (50%): three (3) "important" species; five (5) "very important" species; and, two (2) "most important" species. These species are all shrubland or non-forested habitat specialists classified as GCN species due to long-term regional population declines associated with habitat loss.

The inventory includes one state-listed species as potentially utilizing the Project Area; the brown thrasher<sup>4</sup>. Brown thrasher inhabit thickets, brushy hillsides and woodland edges in suburban and rural areas (Bevier, 1994). Maturation of forest and other factors causing loss of early successional habitat are driving the decline in this species. The Old Field represents suitable breeding habitat for thrasher.

Due to the timing of our field investigations during the fall migration, several species were observed feeding within the Project Area that are not expected to breed<sup>5</sup>; these include the white-throated sparrow (*Zonotrichia albicollis*), tufted titmouse (*Baeolophus bicolor*), black capped chickadee (*Poecile atricapillus*) and a flock of house finch (*Carpodacus mexicanus*) observed diligently feeding on autumn olive berries.

### **Water Quality**

Groundwater underlying the Site is classified by the CTDEEP as "GA". This classification indicates groundwater within the area is presumed to be suitable for human consumption without treatment. Designated uses in GA-classified areas include existing private and potential public or private supplies of drinking water and base flow for hydraulically-connected surface water bodies.

The majority of the Site and Project Area are located in the Gardiner Expansion Aquifer Protection Area No. 67. This level A Final Aquifer Protection Area ("APA") is anticipated to be reclassified as GAA groundwater areas during future CTDEEP reclassifications. Level A APAs represent land area that is contributing ground water to active public water supply wells or well fields that serve more than 1,000 people and are set in sand and gravel aquifers. No water supply wells are located on the Site. It appears that four (4) water supply wells are located southwest of the Site on nearby property in Cromwell, over 1,000 feet from the southern extent of the Project Area.

<sup>&</sup>lt;sup>4</sup> Brown thrasher was not included in the CTDEEP's correspondence regarding listed species potentially at the Site.

<sup>&</sup>lt;sup>5</sup> These species generally prefer other habitat types for nesting and breeding and were likely using the Site as a stopover during migration.

Based upon CTDEEP mapping, the Site is located in Major Drainage Basin 4 (Connecticut River), Subregional Drainage Basin 4000 (Connecticut River), Local Drainage Basin 4000-31 (Dividend Pond).

The nearest surface water body is Dividend Pond, located adjacent to the western and northern boundaries of the Site. Dividend Pond is classified by the CTDEEP as a Class A surface water body. Designated uses for Class A surface water bodies include habitat for fish and other aquatic life and wildlife; potential drinking water supplies; recreation; and water supply for industry and agriculture.

### **Scenic Areas**

No State or locally-designated scenic roads or other scenic areas are located proximate to the Site.

### **Historic and Archaeological Resources**

APT reviewed relevant historic and archaeological information to determine whether the Site holds potential cultural resource significance. No historical resources on or eligible for listing on the National register of Historic Places exist at or in close proximity to the Site. The nearest historic resource is located one mile away (see Table 1, *Non-Residential Features within Two Miles of the Site*).

There are reported archaeological sites<sup>6</sup> in the general area, all related to activities associated with the area's contributions to the industrial revolution in the 17<sup>th</sup> and 18<sup>th</sup> centuries. Collectively, these comprise the Dividend Brook Industrial Archaeological District, which encompasses the Dividend Pond Open Space Property. Some areas may extend onto the western side of the Site<sup>7</sup>; however, the Site has been historically mined for sand and gravel and it is unlikely that intact native soils are present today.

APT submitted Project and Site historic/cultural information to the State Historic Preservation Office ("SHPO") for agency review and comment. Based on this information, it is evident that

<sup>&</sup>lt;sup>6</sup> Archaeological Preserves are State Register districts developed from archaeological data.

<sup>&</sup>lt;sup>7</sup> These "reported sites" consist of locations that have been buffered so as not reveal the specific locations of potentially sensitive artifacts/human remains.

the Project Area has been thoroughly disturbed and no longer possesses the potential to yield intact archaeological deposits.

A copy of the *SHPO Submission* is included in Appendix D. The SHPO has not responded at the time of this report.

### **Geology and Soils**

Soils encompassing the Site and surrounding area are comprised of deposits of sand and gravel overlying sand, sand and gravel overlying sand overlying fines, and sand overlying fines. Soils located on the Site are identified as Penwood-Manchester-Hartford soils. Bedrock geology beneath the Site is identified as Hampden Basalt and Portland Arkose. Hampden Basalt is described as a greenish gray to black (weathers bright orange to brown), fine to medium grained, grading from basalt near contacts to fine grained gabbro in the interior, composed of pyroxene and plagioclase with accessory opaques and locally olivine or devitrified glass. Portland Arkose is described as a reddish brown to maroon micaceous arkose and siltstone and red to black fissile silty shale.

### Floodplain Areas

APT reviewed the United States Federal Emergency Management Agency ("FEMA") Flood Insurance Rate Map ("FIRM") for the Site. A FIRM is the official map of a community on which FEMA has delineated both the special hazard areas and risk premium zones applicable to the community. The area of the Site is mapped on FIRM PANEL #09003 C0519 F, dated September 26, 2008. Based upon the reviewed FIRM Map, the proposed Project Area is designated as Zone X, which is defined as an area of minimal flooding.

### **Recreational Areas**

The nearest recreational area to the Site is the Town's adjacent Dividend Pond Open Space parcel. Additional recreation areas are located in the Town but not proximate to the Site (see Table 1, *Non-Residential Features within Two Miles of the Site*).

### **Noise**

A Noise Evaluation Study was prepared for the Project by HMB Acoustics LLC of Avon, Connecticut<sup>8</sup>. Based on sound measurements obtained at the Site and adjacent locations, the average levels range from 25 to 30 dBA<sup>9</sup>.

### Lighting

No lighting exists at the Site today.

### **Other Surrounding Features**

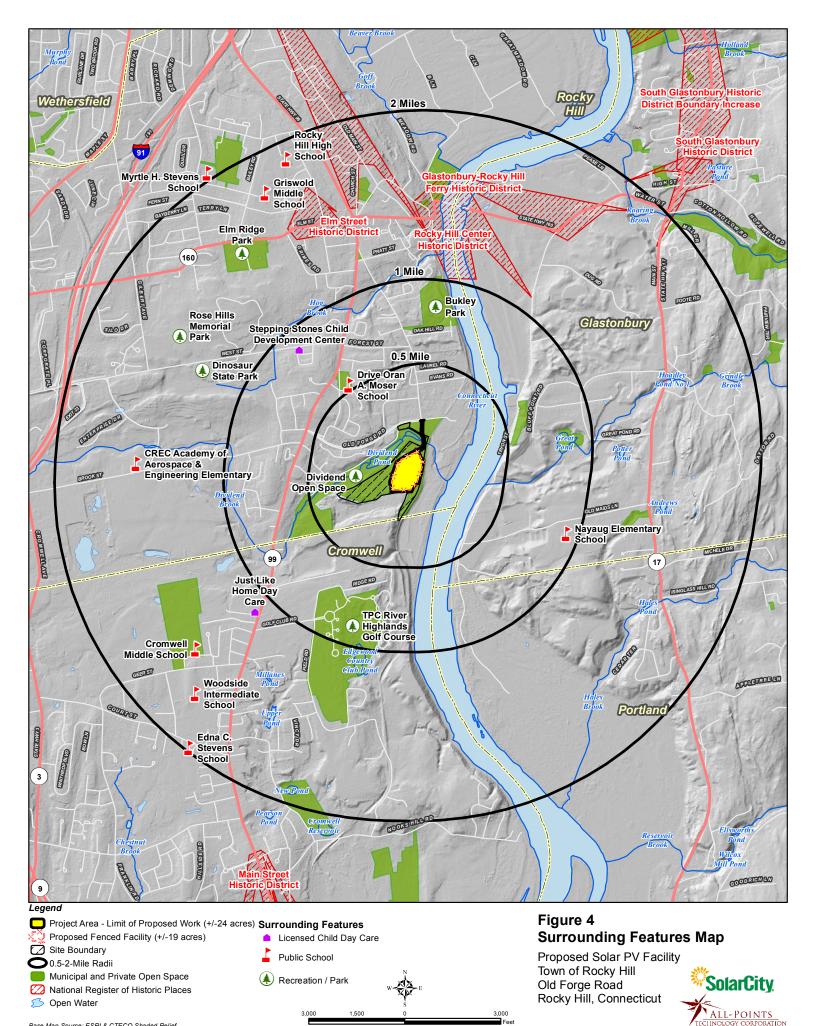
The locations of non-residential development and other resources within two miles of the Site are listed in Table 1 and depicted on Figure 4, *Surrounding Features Map*.

<sup>&</sup>lt;sup>8</sup> The HMB report is provided in Appendix I. See also the Noise discussion in Effects on Environment section of this document.

<sup>&</sup>lt;sup>9</sup> Sound measurements obtained on July 11, 2015 by HMB Acoustics LLC, of Avon, Connecticut.

Table 1: Non-Residential Features within Two Miles of the Site

| Туре               | Name Address                                       |                                 | Town        | Distance to Site |  |
|--------------------|--|---------------------------------|-------------|------------------|--|
|                    | Bulkley Park                                       | Oak Hill Road-Michelle<br>Drive | Rocky Hill  | 0.84 N           |  |
|                    | Dinosaur State Park                                | 400 West Street                 | Rocky Hill  | 1.28 NW          |  |
| Recreational/Parks | Dividend Pond Open Space                           | Pleasant Valley Road            | Rocky Hill  | 0.24 W           |  |
|                    | Elm Ridge Park                                     | 376 Elm Street                  | Rocky Hill  | 1.54 NW          |  |
|                    | Rose Hills Memorial Park                           | 580 Elm Street                  | Rocky Hill  | 1.49 NW          |  |
|                    | TPC River Highlands Golf Course                    | One Golf Club Road              | Cromwell    | 0.90 S           |  |
| Youth Camps        | None   | within 2 miles of the Site      |             |                  |  |
| Hospitals          | None   | within 2 miles of the Site      |             |                  |  |
| •                  | Just Like Home Day Care                            | 659 Main Street                 | Cromwell    | 1.14 SW          |  |
| Child Day Cares    | Stepping Stones Child<br>Development Center        | 196 West Street                 | Rocky Hill  | 0.88 NW          |  |
| Community Center   | None within 2 miles of the Site                    |                                 |             |                  |  |
| Senior Facilities  | None within 2 miles of the Site                    |                                 |             |                  |  |
|                    | CREC Academy of Aerospace & Engineering Elementary | 525 Brook Street                | Rocky Hill  | 1.53 W           |  |
|                    | Cromwell Middle School                             | 6 Mann Memorial Drive           | Cromwell    | 1.54 SW          |  |
|                    | Drive Oran A. Moser School                         | 10 School Street                | Rocky Hill  | 0.53 NW          |  |
|                    | Edna C. Stevens School 25 Court Street             |                                 | Cromwell    | 2.0 SW           |  |
| Schools            | Griswold Middle School 144 Bailey Road             |                                 | Rocky Hill  | 1.76 NW          |  |
|                    | Myrtle H. Stevens School                           | 322 Orchard Street              | Rocky Hill  | 2.04 NW          |  |
|                    | Nayaug Elementary School                           | 222 Old Maids Lane              | Glastonbury | 0.92 SE          |  |
|                    | Rocky Hill High School                             | 50 Chapin Avenue                | Rocky Hill  | 1.90 NW          |  |
|                    | West Hill School                                   | 95 Cronin Drive                 | Rocky Hill  | 2.77 NW          |  |
|                    | Woodside Intermediate School                       | 30 Woodside Road                | Cromwell    | 1.73 SW          |  |
| National Register  | Elm Street Historic District                       |                                 |             | 1.37 NW          |  |
|                    | Glastonbury-Rocky Hill Ferry<br>Historic District  |                                 |             | 1.0 N            |  |
| of Historic Places | Rocky Hill Center Historic District                |                                 | Rocky Hill  | 1.30 N           |  |
|                    | South Glastonbury Historic District                |                                 | Glastonbury | 1.82 NE          |  |



Base Map Source: ESRI & CTECO Shaded Relief Map Date: February 2016

### **Effects on the Environment**

The purpose of this section is to analyze and discuss the Project's potential effects on the environment and demonstrate that the proposed development will have no significant adverse effect on the surrounding environment.

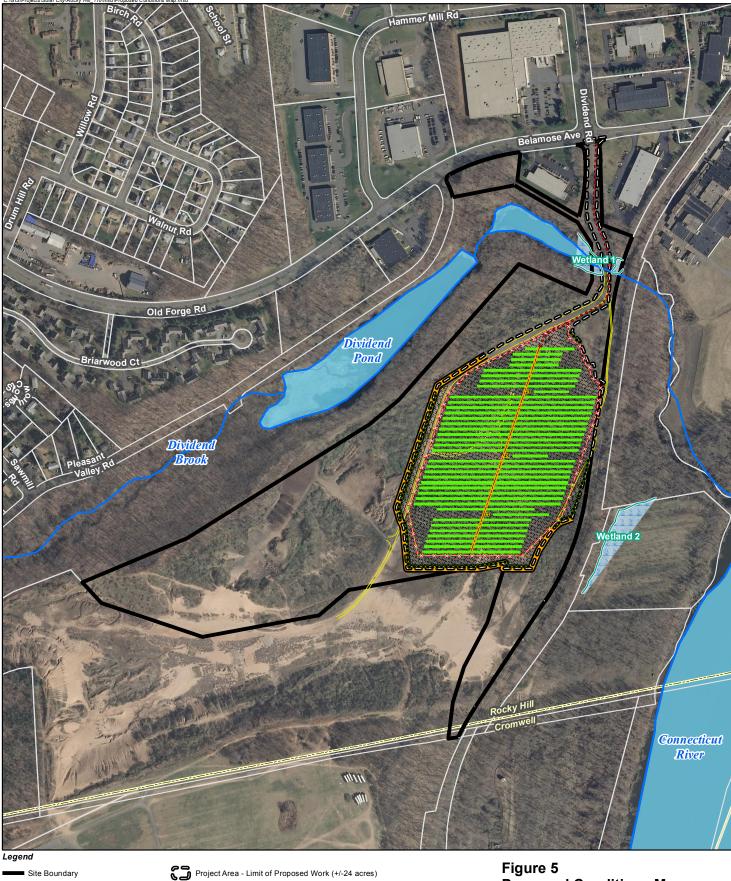
### **Proposed Project Development**

The Project will include an approximate 24-acre development on the Site. The solar array will be developed in the northern portion of the Site, which is primarily a mix of cleared land and early old field habitat, consisting of early successional trees<sup>10</sup> with a dense understory of scrub/shrub and herbaceous growth. New soil disturbances will be minimized to facilitate the installation of the solar arrays and associated equipment. The Project Area includes relatively level grades such that the development can be generally accomplished without significant cuts and/or fills.

The Project Area consists of previously disturbed land. A total of ±18 acres of early successional trees and associated dense understory will be cleared to accommodate the Project. The facility would be comprised of approximately 9,460 – 275 watt and 4,488 – 290 watt Trina Solar TSM-PD14 modules, three (3) Advanced Energy AE 500TX 500 kW inverters, and three (3) transformers. The facility would use a post-driven RBI Solar Inc. tracking system. Electrical connections would extend primarily overhead out to Old Forge Road. Once construction is complete, approximately 21 acres will be seeded for the establishment of permanent cover (turf).

Figure 5, *Proposed Conditions Map*, depicts the proposed Project layout.

 $<sup>^{10}</sup>$  No trees within the Project Area have a diameter at breast height exceeding six (6) inches.



Existing Access Drive

X=X= Proposed Fenced Facility (+/-19 acres)

Proposed Overhead Wire

Proposed Underground Trench

Existing Treeline/Clearing Limit

Proposed Solar Module Proposed Electrical

Map Notes: Base Map Source: 2012 Aerial Photograph (CTECO) Map Scale:1 inch = 500 feet Map Date: February 2016

Disturbed Area to be Seeded for Turf Establishment (+/-21 acres)

Limits of Orange Construction Fencing

CTDEEP Watercourse

CTDEEP Waterbody

**Delineated Wetland Boundary** 

Wetland Area

Approximate Assessor Parcel Boundary (CTDEEP)

Municipal Boundary



### **Proposed Conditions Map**

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut



### **Public Health and Safety**

The Project would be designed to applicable industry, State, and local codes and standards and would not pose a safety concern or create undue hazard to the general public. The facility would not consume any raw materials, would not produce any by-products and would be unstaffed during normal operating conditions. The individual modules of the facility will be secured behind a new 8-foot tall chain link fence enclosure. The Site's entrance is gated, limiting access to authorized personnel.

Overall, the Project will meet or exceed all health and safety requirements applicable to electric power generation. Each employee working on Site will:

- Receive required general and Site specific health and safety training;
- Comply with all health and safety controls as directed by local and state requirements;
- Understand and employ the Site health and safety plan while on the Site;
- Know the location of local emergency care facilities, travel times, ingress and egress routes; and
- Report all unsafe conditions to the construction manager.

Construction equipment will be required to access the Site during normal working hours. Please refer to the *Construction Schedule* and *Construction Work Hours/Days Letter* provided in Appendix E and Appendix F, respectively. After construction is complete and the facility (unstaffed) is operable, traffic at the Site will be minimal. Four times per year the site will be mowed. Maintenance of the electrical equipment will occur once per year. Any equipment that breaks down will be repaired on an as needed basis. Annual maintenance will typically be two technicians for a day. The solar modules are designed to absorb incoming solar radiation and minimize reflectivity, such that only a small percentage of incidental light will be reflected off the panels. This incidental light is significantly less reflective than common building materials, such as steel, or the surface of smooth water. The panels will be tilted up toward the southern sky at a fixed angle of 30 degrees, further reducing reflectivity.

### Local, State and Federal Land Use Plans

The Project is consistent with local, State, and Federal land use plans, including the 2014-2024 Capital Region Council of Government ("CRCOG") Plan of Conservation and Development which outlines the need for "taking measures to drastically reduce greenhouse gas emissions". CRCOG

states that the second largest producer of greenhouse gas emissions in the State is electric power generation. This Project will support CRCOG's policy by developing a renewable energy resource while not having a substantial adverse environmental effect.

### **Existing and Future Development**

SolarCity and the Town of Rocky Hill have partnered together to redevelop the Site into a 3.9 MW DC Solar facility. SolarCity and Rocky Hill have entered into a power purchase agreement (PPA) whereby Rocky Hill will purchase the output of the facility and take advantage of either the net metering or virtual net metering program to offset its electric consumption at one or more town facilities. Additionally, the Project would benefit the community by improving electrical service for existing and future municipal development through enhanced capacity.

### **Roads**

The existing access drive off Old Forge Road will be used. During construction, interior roads on both the east and west sides of the Project Area would be used to access multiple locations. Once construction is complete, permanent access to the facility will extend along the Project's west side. Two (2), sixteen (16) foot wide access gates will be installed along the west side of the fenced Project Area. The only upgrades required for the access road will be establishing a gravel apron at each gate location.

### Wetlands

No wetlands or watercourses will be directly impacted by the Project. The existing access road, which currently crosses Wetland 1 via culvert, will not require upgrading. The closest potential construction activity to this wetland could occur within approximately 160 feet (to the south) if placement of new support poles is required<sup>11</sup> (for the overhead utility routing). All clearing and grading limits for the facility's infrastructure (solar arrays and associated equipment) would maintain a setback of approximately ±370 feet to the south of Wetland 1.

All the Project-related activities are remote from Wetland 2 by a railroad track that extends in a north to south direction, separating the Project Area from this wetland resource area which is

<sup>&</sup>lt;sup>11</sup> Specific pole locations have not been determined to date.

approximately ±260 feet to the east. Due to the separating distance and intervening railroad infrastructure, no impacts are anticipated to Wetland 2.

The Connecticut River, located farther east of Wetland 2 (and  $\pm 850$  feet east of the Project Area and  $\pm 800$  feet east of the proposed limit of clearing) is not located in proximity to any proposed development areas. As such, no direct impacts are expected to occur to the Connecticut River.

Potential short term temporary impacts associated with the Project's construction activities will be minimized by the proposed sedimentation and erosion controls, which would be designed, installed and maintained during construction activities in accordance with the 2002 *Connecticut Guidelines for Soil Erosion and Sediment Control*. Potential long term secondary impacts to wetland resources possibly associated with the operation of this facility are minimized by the fact the development will be unstaffed (generating negligible traffic) and minimizes the creation of impervious surfaces by using an existing gravel access drive and treating the majority of the surface around the solar installation with native grass/vegetation. Based on a review of the Project plans, engineering documents, and the Stormwater Management Report (please see Attachment 4 of the Petition), the stormwater generated by the proposed development will be properly handled and treated in accordance with the 2004 *Connecticut Stormwater Quality Manual*. Due to implementation of these management techniques, the proposed Project development will not result in an adverse impact to wetland resources.

### **Vernal Pools**

No vernal pool habitat was identified on or near (within 750 feet) the Site. All open water areas associated with Wetland 1 consist of permanent waterbodies with known fish populations and perennial stream inlets and outlets. Wetland 2 is an upland floodplain area that does not contain any potential for vernal pool habitat. As no vernal pool habitat exists within or near the Project Area, no impacts to vernal pool resources will result from the proposed Project.

### **Vegetation and Wildlife**

The proposed Project will consist of approximately 24 acres of development, the majority of which is located within a mix of cleared land and early old field habitat, consisting of early successional trees with a dense understory of scrub/shrub and herbaceous growth. The solar arrays and gravel and grass surfaces associated with the construction of the Project will alter the habitat types present on the Site. Impacts to adjacent habitat types will be minimized through proper erosion and sedimentation controls. It is not anticipated that habitat types adjacent to the Project Area will be subjected to significant impacts. Provided below is an analysis of impact to the Site habitats.

**Town Stockpile Areas:** This habitat type exists in the northern extent of the Project Area. Of this habitat type, approximately three (3) acres will be directly impacted by the Project. As this area consists of entirely disturbed surfaces devoid of vegetation, little to no habitat value exists today. Therefore, habitat loss in these areas will not significantly affect wildlife populations utilizing the Site and will not result in significant negative impacts.

Late Old Field: Late Old Field habitat exists throughout the Project Area and the Site. Of this habitat type, approximately 18 acres will be removed as part of the Project. This habitat type is associated with transitioning early successional habitat. As a result of historic activities and current uses, similar habitat occurs to the west, north, and south of the Project Area. Late Old Field habitat within the Project Area will be eliminated, resulting in some habitat fragmentation. However, based on the small size of this block relative to the surrounding habitat that is to remain, development of the Project will not significantly impact Late Old Field habitat type in the surrounding area.

**Early Old Field/Unvegetated Sands:** The Early Old Field/Unvegetated Sands habitat type exists on the northern and western peripheries of the Project Area, all associated with the edges of an existing gravel access road. Totaling approximately three (3) acres in size, little of this habitat type will be removed as part of the proposed Project. It is expected that the use of this access road for construction and continued future use by the Town will result in some impacts to the habitat however, it will likely be minimal. These areas are compromised today by truck traffic. Once constructed and operative, primary access to the Project will be from the west. As the Project Area does not substantially encroach within this habitat type, it is not

anticipated that any significant impacts will result from the Project. Any potential impacts to this habitat type will be mitigated by the fact that the Project will result in additional edge Early Old Field/Unvegetated Sands habitat type through the removal of the Late Old Field habitat type.

### **Bird Habitat Impact Analysis**

Habitat loss and fragmentation continue to be the greatest threat to Connecticut's birds. Therefore, when analyzing the impact of a particular project on birds and bird habitat, it is critical to assess both the total habitat to be lost as well as whether or not that habitat loss results in habitat fragmentation.

Habitat loss is an unavoidable consequence of land development. When assessing the impact of habitat loss, the total area of habitat lost must be quantified. This loss should be evaluated against the overall "patch size" of the habitat being affected in order to determine whether or not that habitat patch is large enough to support rare area-sensitive species both pre- and post-development. If the habitat patch size is currently small or fragmented and therefore suitable only for more common generalist species, the impacts of habitat loss can be insignificant. Conversely, if the habitat loss will result in the degradation of the entire patch size, the impacts of habitat loss can be significant.

When assessing whether or not a project will increase habitat fragmentation, it is critical to determine if the project decreases core (i.e., interior) habitat. This depends upon where the development occurs, within the interior or along the edge of the habitat patch. Projects located within the interior of a habitat patch will more adversely affect core habitat and result in higher increases in edge habitat than projects sited on the periphery of the habitat patch. Reduction of core habitat and the increase of edge habitat are critical factors negatively affecting the distribution of some area-sensitive species.

In this specific instance, the term "habitat matrix" (or "block") is used to discuss the relatively contiguous and undeveloped area that includes the Site and surrounding land. In addition to the Site, this habitat matrix includes the Dividend Pond Open Space Property to the west/northwest and the property to the south. This habitat matrix is primarily composed of Mixed Hardwood Forest areas to the north/northwest and a mix of Early Old Field/Unvegetated Sands and Late Old Field habitats to the south and southwest. These areas are generally

fragmented by the presence of existing paved roads to the west (Pleasant Valley Road), north (Old Forge Road/Belamose Avenue) and south (an unnamed drive immediately beyond the Cromwell town line), as well as the railroad tracks to the east of the Site, thus limiting the size of this habitat block.

The Project Area occupies the northeast corner of a habitat matrix that lies across three separate parcels. Although considered relatively contiguous in nature for purposes of this discussion, the matrix has experienced some level of fragmentation over time. For instance, the active road network and Town Stockpile Areas have resulted in varying degrees of disturbance, from loss of habitat to routine traffic and equipment use. Although development of the Project will result in some loss of patch size within the Late Old Field habitat, it would not result in significant reduction of the core habitat block. Associated edge effects resulting from the proposed development will penetrate into the remaining Late Old Field habitat. Edge effects include human activity and associated noise which can deter birds from using the remaining habitat that lies immediately adjacent to the new development<sup>12</sup>. Such affects are favored by some species.

The overall contiguous habitat matrix totals 179 acres. This habitat matrix will be reduced by approximately 24 acres (an approximate 13% reduction) as a result of development of the proposed Project. This will directly affect a portion of the late old field patch (approximately 18 of 52 acres, or  $\pm 35\%$ ). Post-development, the remaining late old field habitat patches located elsewhere within the habitat matrix will still be large enough to support area-sensitive shrubland habitat specialists such as the field sparrow or brown thrasher, as most shrubland specialists have a minimum patch size requirement of less than or equal to 25 acres.

When considering the entire contiguous habitat matrix, siting the development within the proposed Project Area represents the least environmentally damaging alternative. This conclusion is based on several factors, most notably: (1) the Project will not result in fragmentation of the overall habitat matrix; and, (2) portions of the Project Area are currently in use by the Rocky Hill DPW and do not represent suitable habitat for target species.

<sup>&</sup>lt;sup>12</sup> While the edge effect is both species-dependent and land-use dependent, it generally affects avian use up to 300 feet from development.

### **Rare Species**

The Project will not result in disturbances to habitat anticipated to be used by the tiger beetle. Although no appreciable habitat suitable for tiger beetle exists within the Project Area, areas within the southwest corner of the Site and the adjoining parcel to the south contain optimal tiger beetle habitat in the form of loose, shifting unvegetated sands. Due to the potential presence of tiger beetle populations proximate to the Project Area, SolarCity is committed to implementing proactive protection measures during construction. The plan would consist of installing physical barriers to restrict access to those nearby locations with suitable habitat, conducting contractor awareness training and inspections of protective measures by a qualified environmental specialist. SolarCity has provided its proposed Big Sand Tiger Beetle Protection Plan to the CTDEEP for review and acceptance. SolarCity will provide the Council with a copy of the CTDEEP's response letter upon receipt.

A copy of the proposed Big Sand Tiger Beetle Protection Plan is provided in Appendix G.

One federally listed<sup>13</sup> threatened species, northern long-eared bat (*Myotis septentrionalis*) may occur within the vicinity of the Site. The range of northern long-eared bat ("NLEB") encompasses the entire State of Connecticut. Suitable NLEB roost habitat includes trees (live, dying, dead, or snag) with a diameter at breast height ("DBH") of three (3) inches or greater. The proposed activity will result in the clearing of trees greater than three inches DBH. As a result, SolarCity evaluated the proposed activity's compliance with Section 10 of the Endangered Species Act ("ESA") through initial consultation with the U.S. Fish and Wildlife Service's ("USFWS") Information, Planning, and Conservation System ("IPaC").<sup>14</sup>

To determine whether the planned activity complies with Section 10 of the ESA, SolarCity assessed the Project using the USFWS's *Key to the Northern Long-Eared Bat 4(d) Rule for Non-Federal Activities Key* ("USFWS Key"; January 13, 2016), as detailed below.

Will your activity purposefully take (see Definitions below) northern long-eared bats? For example, are you removing bats from a human structure or capturing bats for research?
 Response: No, the proposed activity does not include purposefully taking northern long-eared bats.

<sup>&</sup>lt;sup>13</sup> Listing under the federal Endangered Species Act.

<sup>&</sup>lt;sup>14</sup> IPaC Consultation Tracking Number: 05E1NE00-2016-SLI-1095; dated March 15, 2016.

2. Is your activity located outside the White-nose Syndrome Zone?

Response: No, the proposed activity is located inside the white-nose syndrome zone.

3. Will your activity take place within a cave or mine where northern long-eared bats hibernate (i.e., hibernaculum) or could it alter the entrance or the environment (physical or other alteration) of a hibernaculum?

Response: No, the proposed activity will not take place within a northern long-eared bat hibernaculum or alter its entrance or environment.

4. Will your action involve tree removal<sup>15</sup>?

Response: Yes.

5. Is your activity the removal of hazardous trees for protection of human life or property?

Response: No, the proposed activity is not removing hazardous trees.

6. Will your tree removal activities include one or both of the following: 1) removing a northern long-eared bat known occupied maternity roost tree or any trees within 150 feet of a known occupied maternity roost tree from June 1 through July 31; or 2) removing any trees within 0.25 miles of a northern long-eared bat hibernaculum at any time of year?

Response: No. There are currently no known NLEB maternity roost trees in Connecticut.  $^{16}$  The nearest NLEB habitat resource to the proposed activity is located in North Branford  $\pm 18$  miles to the southwest.

In accordance with the USFWS Key for NLEB, the Project would not result in an adverse effect or incidental take<sup>17</sup> to NLEB and does not require a permit from USFWS.

### **Water Quality**

The facility will be unstaffed and no potable water uses or sanitary discharges are planned. No liquid fuels are associated with the operations of the Project. Once operative, the stormwater generated by the proposed development will be properly handled and treated in accordance with the 2004 *Connecticut Stormwater Quality Manual*. Therefore, upon its completion the

<sup>&</sup>lt;sup>15</sup> "Tree removal" is defined in the 4(d) rule as cutting down, harvesting, destroying, trimming, or manipulating in any other way the trees, saplings, snags, or any other form of woody vegetation likely to be used by northern long-eared bats.

Northern long-eared bat areas of concern in Connecticut to assist with Federal Endangered Species Act Compliance map (February 1, 2016)

<sup>&</sup>lt;sup>17</sup> "Incidental take" is defined by the Endangered Species Act as take that is "incidental to, and not the purpose of, the carrying out of an otherwise lawful activity." For example, harvesting trees can kill bats that are roosting in the trees, but the purpose of the activity is not to kill bats.

Project would have no adverse environmental effect on wetlands, watercourses or other water resources.

The Site is located within the Gardiner Expansion APA. Water supply production wells are located on nearby property in Cromwell. The nearest well is located over 1,000 feet from the southern extent of the Project Area. To safeguard this resource from potential impacts during construction, SolarCity is committed to implementing protective measures in the form of an Aquifer Protection Plan. This Plan will include monitoring of established sedimentation and erosion controls that will be installed and maintained in accordance with the 2002 *Connecticut Guidelines for Soil Erosion and Sediment Control*. SolarCity will also apply for a *General Permit for the Discharge of Stormwater and Dewatering Wastewaters from Construction Activities* from CTDEEP. Therefore, with the incorporation of adequate protective measures, stormwater runoff from the Project development will not result in an adverse impact to water quality associated with the APA. A copy of the proposed *Aquifer Protection Plan* is provided in Appendix H.

### **Air Quality**

No emission sources are associated with the operations of the Project. Therefore, no impacts to air quality are anticipated as part of the proposed Project.

### **Scenic Areas**

No state designated scenic areas would be physically or visually impacted by development of the solar Project.

### **Historic and Archaeological Resources**

APT consulted with the SHPO for concurrence that no historic or archaeological resources would be affected by the Project. Based on the results of APT's research, the Project Area has been thoroughly disturbed and no longer possesses any potential to yield intact archaeological deposits. In addition, the Project would not result in any impacts to the viewshed of the Dividend Brook Industrial Archaeological District.

The SHPO is currently reviewing the Project. Once received, a copy of the SHPO determination letter will be provided to the Council.

### **Geology and Soils**

No adverse effects are anticipated on natural resources occurring at and/or nearby the Site. Once vegetative clearing activities are completed, minimal grading is required for construction of the Project.

### Floodplain Areas

The Site is located entirely outside of the 100-year and 500-year floodplains. Therefore, no special design elements are necessary with respect to flooding concerns. In addition, no impacts to floodplains are associated with the proposed Project.

### **Recreational Areas**

No recreational areas would be impacted by the Project.

### **Noise**

The only equipment proposed for the Project that would generate noise consists of the fans associated with the inverters. The Noise Evaluation Study prepared by HMB Acoustics LLC of Avon, Connecticut, determined that after the Project is constructed and in service, the combined noise levels will comply with CTDEEP criteria for Commercial Emitters to both Commercial and Residential Receiver Zones.

After the Project is constructed and in service, the highest noise levels at adjacent properties are anticipated to be 30 dBA, which is well below the most conservative criteria of 45 dBA for nighttime and 55 dBA for daytime, as established by the State of Connecticut Noise Control regulations (CGS 22a/22a-69-1 through 7). The inverters are inactive at night. During those times the inverters are operative, noise levels at nearby property lines and/or residences would not change and continue to be well below applicable criteria (estimated at 25 to 30 dBA based on existing background noise measurements obtained in July 2015).

Please refer to the *Noise Evaluation Report* provided in Appendix I.

### Lighting

No lighting is planned for the facility.

### **Other Surrounding Features**

No adverse effects are anticipated to the facilities identified in *Figure 4*, primarily because of their sufficient distances from the Project.

### **Visibility**

Covering approximately 19 acres in total, the fenced facility will consist of a total of 13,948 non-reflective solar panels. The fence will rise to a height of eight (8) feet above grade ("AG"). The solar panels and appurtenances will not exceed this height. Once installed, the top of the solar panels would extend to a height of approximately six  $(\pm 6)$  feet AG. The tallest equipment within the facility (inverters) would be approximately seven  $(\pm 7)$  feet high. New utility poles are required for interconnection with the existing distribution system on Old Forge Road. However, the Project is set back sufficiently from abutting properties and public roads, and is benefited by intervening vegetation, such that the facility component will not be visible from locations off the Site.

Figure 6, *Facility Setting Map*, depicts the lack of nearby receptor locations with direct views towards the Project Area.



### Legend

×=×= Proposed Fenced Facility

•••• Proposed Overhead Wire

---- Proposed Solar Module

Approximate Assessor Parcel Boundary (CTDEEP)

Municipal Boundary

### Figure 6 Facility Setting Map

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut





### **Conclusion**

As demonstrated in this EA, the Project will comply with CTDEEP air and water quality standards. Further, it will not have an undue adverse effect on the existing environment and ecology, nor would it affect the scenic, historic and recreational resources in the vicinity. Protective measures would be employed to safeguard potential populations of tiger beetle proximate to the Project Area during construction activities. Once operative the facility will be unstaffed and generate minimal traffic. The Project design minimizes the creation of impervious surfaces and stormwater generated by the proposed development will be handled and treated in a manner consistent with the 2004 *Connecticut Stormwater Manual*.

# APPENDIX A Inland Wetland & Watercourse Report and

**Photo-Documentation** 



### WETLAND INSPECTION

| September 14, 2015                 | APT Project No.: CT478110   |
|------------------------------------|---|
| Prepared For:                      | SolarCity<br>100 N. 18 <sup>th</sup> Street Suite 1900<br>Philadelphia, PA 19103<br>Attn: Nichole Seidell                     |
| Project Name:                      | Solar City Rocky Hill   |
| Site Address:                      | Old Forge Road<br>Rocky Hill, Connecticut   |
| Date(s) of Investigation:          | 9/3/2015  |
| Field Conditions:                  | Weather: sunny, mid 80's Soil Moisture: dry   |
| Wetland/Watercourse Delin          | eation Methodology*:  ⊠Connecticut Inland Wetlands and Watercourses □Connecticut Tidal Wetlands □U.S. Army Corps of Engineers |
| The wetlands inspection was        | performed by <sup>†</sup> :   |
| Matthew Gustafson, Register        | red Soil Scientist  |
| Enclosures: Wetland Delinea        | tion Field Forms & Wetland Inspection Map   |
| This report is provided as a briej | summary of findings from APT's wetland investigation of the referenced Study Area that  |

\* Wetlands and watercourses were delineated in accordance with applicable local, state and federal statutes, regulations and guidance.

activities and surveyed location of identified wetland and watercourse resources.

consists of proposed development activities and areas generally within 100 feet.‡ If applicable, APT is available to provide a more comprehensive wetland impact analysis upon receipt of site plans depicting the proposed development

<sup>†</sup> All established wetlands boundary lines are subject to change until officially adopted by local, state, or federal regulatory agencies.

<sup>&</sup>lt;sup>‡</sup> APT has relied upon the accuracy of information provided by by Brightfields Development, LLC regarding the proposed subject property for defining the study area within which wetlands and/or watercourses are to be identified.

### **Attachments**

- Wetland Delineation Field Forms
- Wetland Inspection Map

### **Wetland Delineation Field Form**

|                         |  | -                               |      |                                |  |
|-------------------------|--|---------------------------------|------|--------------------------------|--|
| Wetland I.D.:           | Wetland 1                                    |                                 |      |                                |  |
| Flag #'s:               | WF 1-01 to 1-15 and 1-30 to 1-42             |                                 |      |                                |  |
| Flag Location Method:   | Site Sketch                                  | $\boxtimes$                     | GPS  | (sub-meter) located ⊠          |  |
| WETLAND HYI             | OROLOGY:                                     |                                 |      |                                |  |
| NONTIDAL ⊠              |  |                                 |      |                                |  |
| Intermittently Flo      | oded 🗆                                       | Artificially Flooded □          |      | Permanently Flooded ⊠          |  |
| Semipermanently         | Flooded                                      | Seasonally Flooded □            |      | Temporarily Flooded □          |  |
| Permanently Satur       | rated $\square$                              | Seasonally Saturated – seepag   | ge 🗆 | Seasonally Saturated - perched |  |
| Comments: None          |  |                                 |      |                                |  |
| TIDAL □                 |  |                                 |      |                                |  |
| Subtidal                |  | Regularly Flooded               |      | Irregularly Flooded □          |  |
| Irregularly Flooded □   |  |                                 |      |                                |  |
| Comments: None          |  |                                 |      |                                |  |
| WETLAND TYP             | PE:  |                                 |      |                                |  |
|                         | _,   |                                 |      |                                |  |
| Estuarine $\square$     | SYSTEM:  Estuarine □ Riverine □ Palustrine □ |                                 |      |                                |  |
| Lacustrine   Lacustrine |  | Marine □                        |      | r diustillie 🖂                 |  |
| Comments: None          |  |                                 |      |                                |  |
| Comments: 140ne         |  |                                 |      |                                |  |
| CLASS:                  |  |                                 |      |                                |  |
| Emergent ⊠              |  | Scrub-shrub ⊠                   | ]    | Forested ⊠                     |  |
| Open Water ⊠            |  | Disturbed □                     | 1    | Wet Meadow □                   |  |
| Comments: Prima         | rily forested o                              | edges with core open water area | ıs.  |                                |  |
| WATERCOURS              | E TYPE:                                      |                                 |      |                                |  |
| Perennial ⊠             | -  | Intermittent                    | 7    | Γidal □                        |  |
| Watercourse Nam         | e: Dividend F                                | ond and outlet perennial strean | 1    |                                |  |
| S 5                     |  |                                 |      | 11 01 1                        |  |

Comments: Dividend Pond and the associated perennial stream outlet generally flows west to east under

the existing gravel access through a large reinforced concrete pipe culvert.

### **Wetland Delineation Field Form (Cont.)**

| SPECIAL AQUATIC HABITAT | <b>SPECIAL</b> | <b>AQUA</b> | TIC I | HABI | TAT |
|-------------------------|----------------|-------------|-------|------|-----|
|-------------------------|----------------|-------------|-------|------|-----|

| Vernal Pool Yes □ No ⊠ Potential □ | Other |
|------------------------------------|-------|
| Vernal Pool Habitat Type: None     |       |
| Comments: None                     |       |
|                                    |       |

### **SOILS:**

| Are field identified soils consistent with NRCS mapped soils? | Yes ⊠ | No □ |
|---|-------|------|
| If no, describe field identified soils                        |       |      |

### **DOMINANT PLANTS:**

| Red Maple (Acer rubrum)             | Silky Dogwood (Cornus amomum)  |
|-------------------------------------|--------------------------------|
| Poison Ivy (Toxicodendron radicans) | Specked Alder (Alnus rugosa)   |
| American Elm (Ulmus americana)      | Jewelweed (Impatiens capensis) |
| Autumn Olive* (Elaeagnus umbellate) | Mugwort* (Artemisia vulgaris)  |
| Fox Grape (Vitis labrusca)          |                                |

<sup>\*</sup> denotes Connecticut Invasive Species Council invasive plant species

#### **GENERAL COMMENTS:**

Wetland 1 consists of an open water resource identified as Dividend Pond and a perennial watercourse that outlets from the pond, flowing east eventually into the Connecticut River located approximately 800 feet west of the proposed Rocky Hill Solar PV Facility. An existing gravel access road crosses the watercourse through a large reinforced concrete pipe culvert. Wetland 1 eventually drains east under an existing railroad line and off the subject property. The margins of Wetland 1 are entirely forested with sparse scrub/shrub and emergent vegetation present. Banks to the resource are steeply sloping with little to no bordering vegetated wetland areas.

Based on APT's understanding of the Rocky Hill Solar PV Facility proposed by SolarCity, no direct impact to wetlands or watercourses would result from the development. The northeastern end of the proposed Facility would be located  $\pm 160$  feet south of Wetland 1 at the existing wetland and watercourse crossing. The northwestern corner of the proposed Facility would be located  $\pm 260$  feet southeast of Dividend Pond. Depending upon proposed improvements to the existing access road and utilities, work may occur in close proximity to wetlands located either side of this existing wetland and watercourse crossing. APT is available to provide a detailed evaluation of possible wetland and watercourse impacts associated with the proposed Rocky Hill Solar PV Facility.

### **Wetland Delineation Field Form**

| Wetland I.D.:            | Wetland 2       |                             |             |                                     |
|--------------------------|-----------------|-----------------------------|-------------|-------------------------------------|
| Flag #'s:                | WF 2-01 to 2-23 |                             |             |                                     |
| Flag Location<br>Method: | Site Sketch     | $\boxtimes$                 | GPS         | (sub-meter) located ⊠               |
| WETLAND HYI              | DROLOGY:        |                             |             |                                     |
| NONTIDAL ⊠               |                 |                             |             |                                     |
| Intermittently Flo       | oded 🗆          | Artificially Flooded □      |             | Permanently Flooded □               |
| Semipermanently          | Flooded         | Seasonally Flooded          |             | Temporarily Flooded ⊠               |
| Permanently Satu         | rated $\square$ | Seasonally Saturated – see  | epage 🗆     | Seasonally Saturated - perched      |
| Comments: Flood          | lplain associat | ed with the Connecticut Riv | ver.        |                                     |
| _                        |                 |                             |             |                                     |
| TIDAL                    |                 |                             |             |                                     |
|                          |                 | Regularly Flooded           |             | Irregularly Flooded □               |
| Irregularly Flooded □    |                 |                             |             |                                     |
| Comments: None           |                 |                             |             |                                     |
| WETLAND TYP              | DF.             |                             |             |                                     |
| WEILANDIII               | . 12.           |                             |             |                                     |
| SYSTEM:                  |                 |                             |             |                                     |
| Estuarine                |                 | Riverine □                  | ]           | Palustrine ⊠                        |
| Lacustrine □             |                 | Marine □                    |             |                                     |
| Comments: None           |                 |                             |             |                                     |
| CLASS:                   |                 |                             |             |                                     |
| Emergent □               |                 | Scrub-shrub ⊠               | ]           | Forested 🗵                          |
| Open Water               |                 | Disturbed                   | 1           | Wet Meadow ⊠                        |
| •                        | eated extents   | of wetland primarily consis | t of an ope | n field with edge forested areas.   |
| WATERCOURS               |                 |                             | *           | <u> </u>                            |
| Perennial ⊠              | <u> </u>        | Intermittent                | 7           | Γidal □                             |
| Watercourse Nam          | ne: Connecticu  | ıt River                    | L           |                                     |
|                          |                 |                             | ut River wa | as delineated, not the banks of the |
|                          |                 | -                           |             |                                     |

river.

### **Wetland Delineation Field Form (Cont.)**

| Vernal Pool Yes □ No ⊠ Potential □ | Other |  |
|------------------------------------|-------|--|
| Vernal Pool Habitat Type: None     |       |  |
| Comments: None                     |       |  |
|                                    |       |  |

### **SOILS:**

| Are field identified soils consistent with NRCS mapped soils? | Yes ⊠ | No 🗆 |
|---|-------|------|
| If no, describe field identified soils                        |       |      |

#### **DOMINANT PLANTS:**

| Sensitive Fern (Onoclea sensibilis)     | Spicebush (Lindera benzoin)         |
|---|-------------------------------------|
| Silky Dogwood (Cornus amomum)           | Poison Ivy (Toxicodendron radicans) |
| Purple Loosestrife* (Lythrum salicaria) | Autumn Olive* (Elaeagnus umbellate) |
| Weeping Willow (Salix babylonica)       | Mugwort* (Artemisia vulgaris)       |
| Staghorn Sumac (Rhus typhina)           |                                     |

<sup>\*</sup> denotes Connecticut Invasive Species Council invasive plant species

### **GENERAL COMMENTS:**

Wetland 2 consists of the semi-active floodplain associated with several associated backwater wetland areas that border on the Connecticut River. The western edge of the delineated resource consists of steeply sloping embankments. The northern edge is more moderately sloped with a broader transition zone from wetlands to uplands. The primary vegetation class associated with Wetland 2 is open field with edge forested areas and transitional scrub/shrub ecotones separating the two. Observed soil profiles reveals these areas flood irregularly and are consistent with moderately well drained and well drained floodplain soils.

Based on APT's understanding of the Rocky Hill Solar PV Facility proposed by SolarCity, no direct impact to wetlands or watercourses would result from the development. The southeastern corner of the proposed Facility would be located  $\pm 225$  feet west of Wetland 2. APT is available to provide a detailed evaluation of possible wetland and watercourse impacts associated with the proposed Rocky Hill Solar PV Facility.



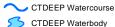
#### Legend



Approximate Project Area (+/-16 acres)

Subject Property

Approximate Assessor Parcel Boundary (CTDEEP)



CTDEEP Waterbody

Map Notes: Base Map Source: 2012 Aerial Photograph (CTECO) Map Scale:1 inch = 500 feet Map Date: September 2015

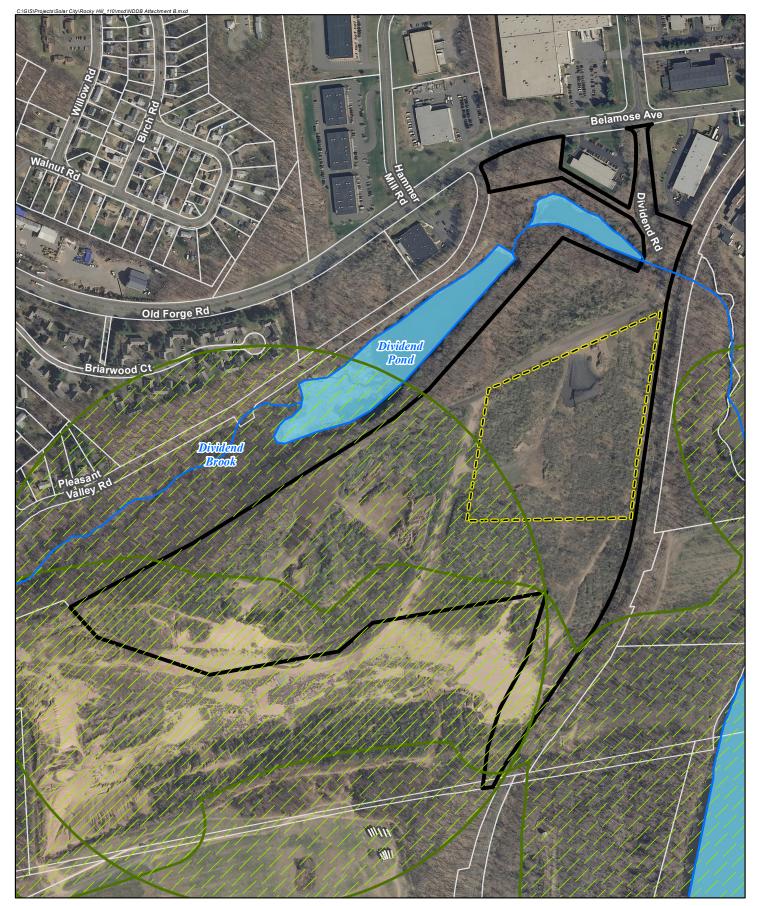


### **Wetland Inspection Map**

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut



# APPENDIX B CTDEEP NDDB Mapping

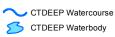


### Legend



Project Area (+/-14 acres)

Natural Diversity Database (NDDB; Sept. 2015)





### Appendix B Site Map

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut Lat: 41.64342847 Long: -72.633249



# APPENDIX C Breeding Bird Inventory Table

### **Breeding Bird Inventory Table**

| Common Name            | Scientific Name         | Observed | Status | Habitat Type |
|------------------------|-------------------------|----------|--------|--------------|
| American Redstart      | Setophaga ruticilla     |          |        | OF           |
| American Robin         | Turdus migratorius      | ОВ       |        | OF           |
| Blue-Jay               | Cyanocitta cristata     | ОВ       |        | OF           |
| Blue-winged Warbler    | Vermivora pinus         |          | MI     | OF           |
| Brown Thrasher         | Toxostoma rufum         |          | SC, VI | OF           |
| Cedar Waxwing          | Bombycilla cedrorum     | ОВ       |        | OF           |
| Chestnut-sided Warbler | Dendroica pensylvanica  |          | VI     | OF           |
| Common Yellowthroat    | Geothlypis trichas      |          |        | OF           |
| Eastern Kingbird       | Tyrannus tyrannus       |          | I      | OF           |
| Eastern Towhee         | Pipilo erythrophthalmus |          | VI     | OF           |
| Field Sparrow          | Spizella pusilla        |          | VI     | OF           |
| Gray Catbird           | Dumetella carolinensis  |          |        | OF           |
| Indigo Bunting         | Passerina cyanea        |          | VI     | OF           |
| Mourning Dove          | Zenaida macroura        | ОВ       |        | OF           |
| Northern Cardinal      | Cardinalis cardinalis   |          |        | OF           |
| Northern Oriole        | Icterus galbula         |          | I      | OF           |
| Prairie Warbler        | Dendroica discolor      |          | MI     | OF           |
| Rose-breasted Grosbeak | Pheucticus Iudovicianus |          | I      | OF           |
| Song Sparrow           | Melospiza Melodia       |          |        | OF           |
| White-eyed Vireo       | Vireo griseus           |          |        | OF           |

KEY
OB – species was observed on the site on 10/27/15 (migrant and winter residents only) WAP Conservation Status: IM – Important; VI – Very Important; MI – Most Important SC – State-listed species of special concern Habitat Types (observed and potential use): OF – old field

## APPENDIX D State Historic Preservation Office Submission





### **State Historic Preservation Office**

One Constitution Plaza | Hartford, CT 06103 | 860.256.2800 | Cultureandtourism.org

### PROJECT REVIEW COVER FORM

| 1.                 | This information relates to a previously submitted project.   | You do not need to complete the re<br>you have been previously issued a<br>Number. Please attach information<br>submit. | SHPO Project  |
|--------------------|---|---|---------------|
|                    | SHPO Project Number   | Sublint.  |               |
|                    | Project Address   |   |               |
| 2.                 | This is a new Project.  If you have checked this box, it is necessary to complete ALL entries on this form.   |   |               |
| Project            | Name Proposed Solar Facility Installation   |   | _             |
| Project            | Location 13 Old Forge Road  |   | _             |
| City or            | Town Rocky Hill Include street number, street name, and or Route Number. If no street address exists  | -   |               |
| County             | In addition to the village or hamlet name (if appropriate), the <u>municipality</u> must be in <a href="Hartford County">Hartford County</a> If the undertaking includes multiple addresses, please attach a list to this form. | cluded here.  |               |
| Date of            | Construction (for existing structures) N/A - Undeveloped land   |   |               |
|                    | ECT DESCRIPTION SUMMARY (include full description in attachment): ty Corporation proposes the construction of a solar powered electrical generation insta   | llation consisting of   |               |
|                    | oltaic (PV) module technology. The Site parcel is approximately 61.4 acres located a  |   | cky Hill, CT. |
|                    | oposed project area would encompass approximately 24 acres of undeveloped, lig  |   |               |
|                    | y used by the Town for materials storage. Upon completion, the facility will occupy approximately action of Old Forms Read and Dividend   | ·   |               |
|                    | an existing, gated drive originating at the intersection of Old Forge Road and Dividend drive extends south into the Site where it connects to a system of interior dirt roads.   | -   | _             |
|                    | closed Project Location Map and Site Figures. A Preliminary Archeological Assess  | •   | -             |
| LLC is             | enclosed.   |   |               |
| TYPE               | OF REVIEW REQUESTED   |   |               |
| a.                 | Does this undertaking involve funding or permit approval from a State or Federal Age  | ncy?  |               |
|                    | X Yes No  | State   | Federal       |
|                    | Name/Contact Type of Permit/Approval ng Council Petition that NO Certificate of Env   | ×   |               |
|                    | Compatibility and Public Need is required.  |   |               |
| b. Have            | you consulted the SHPO and UCONN Dodd Center files to determine the presence  | Yes   | No            |
|                    | nce of previously identified cultural resources within or adjacent to the project area?   | ×   |               |
| If yes:<br>Was the | e project site wholly or partially located within an identified archeologically sensitive are   | ea?   | X             |
|                    | e project site involve or is it substantially contiguous to a property listed or recommendent the CT State or National Registers of Historic Places?  | ed for  | ×             |
|                    | e project involve the rehabilitation, renovation, relocation, demolition or addition to any g or structure that is 50 years old or older?   |   |               |



### **State Historic Preservation Office**

One Constitution Plaza | Hartford, CT 06103 | 860.256.2800 | Cultureandtourism.org

### PROJECT REVIEW COVER FORM

The Historic Preservation Review Process in Connecticut Cultural Resource Review under the National Historic Preservation Act – Section 106 <a href="http://www.achp.gov/106summary.html">http://www.achp.gov/106summary.html</a> involves providing technical guidance and professional advice on the potential impact of publicly funded, assisted, licensed or permitted projects on the state's historic, architectural and archaeological resources. This responsibility of the State Historic Preservation Office (SHPO) is discharged in two steps: (1) identification of significant historic, architectural and archaeological resources; and (2) advisory assistance to promote compatibility between new development and preservation of the state's cultural heritage.

Project review is conducted in two stages. First, the SHPO assesses affected properties to determine whether or not they are listed or eligible for listing in the Connecticut State or National Registers of Historic Places. If so, it is deemed "historic" and worthy of protection and the second stage of review is undertaken. The project is reviewed to evaluate its impact on the properties significant materials and character. Where adverse effects are identified, alternatives are explored to avoid, or reduce project impacts; where this is unsuccessful, mitigation measures are developed and formal agreement documents are prepared stipulating these measures. For more information and guidance, please see our website at: <a href="http://www.cultureandtourism.org/cct/cwp/view.asp?a=3933&q=293820">http://www.cultureandtourism.org/cct/cwp/view.asp?a=3933&q=293820</a>

### ALL PROJECTS SUBMITTED FOR REVIEW MUST INCLUDE THE FOLLOWING MATERIALS\*:

|    | ×      | PROJECT DESCRIPTION Please attach a full description of the work that will be undertaken as a result of this project.         |
|----|--------|---|
| Þ  | ortion | as of environmental statements or project applications may be included. The project boundary of the project should be clearly |
| d  | efined | <b>!</b> **   |
| ſ  | ×      | PROJECT MAP This should include the precise location of the project – preferably a clear color image showing the nearest      |
| sī | treets | or roadways as well as all portions of the project. Tax maps, Sanborn maps and USGS quadrangle maps are all acceptable, but   |

Bing and Google Earth are also accepted if the information provided is clear and well labeled. The project boundary should be clearly

defined on the map and affected legal parcels should be identified.

PHOTOGRAPHS Clear, current images of the property should be submitted. Black and white photocopies will not be accepted. Include images of the areas where the proposed work will take place. May require: exterior elevations, detailed photos of elements to be repaired/replaced (windows, doors, porches, etc.) All photos should be clearly labeled.

| For Existing Structures  | Yes         | N/A         | Comments          |         |
|--|-------------|-------------|-------------------|---------|
| Property Card  | X           |             |                   |         |
| For New Construction   | Yes         | N/A         | Comments          |         |
| Project plans or limits of construction (if available)   | X           |             |                   |         |
| If project is located in a Historic District include renderings or elevation drawings  |             | $\boxtimes$ |                   |         |
| of the proposed structure  |             |             |                   |         |
| Soils Maps <a href="http://websoilsurvey.nrcs.usda.gov/app/HomePage.htm">http://websoilsurvey.nrcs.usda.gov/app/HomePage.htm</a> | $\times$    |             | Refer to Arch Ass | essment |
| Historic Maps <a href="http://magic.lib.uconn.edu/">http://magic.lib.uconn.edu/</a>  | $\boxtimes$ |             | Refer to Arch Ass | essment |
| For non-building-related projects (dams, culverts, bridge repair, etc)   | Yes         | N/S         | Comments          |         |
| Property Card  |             |             |                   |         |
| Soils Map (see above)  |             |             |                   |         |
| Historic Maps (see above)  |             |             |                   |         |
| SHPO USEONLY   | Above       | Date        | Below             | Date    |
| Indicate date of Review and Initials of Reviewer   |             |             |                   |         |

#### PROJECT CONTACT

| Name Nicole Castro                               | TitleProject Manager |
|--|----------------------|
| Firm/AgencyAll-Points Technology Corporation, P. | C.                   |
| Address 3 Saddlebrook Drive                      |                      |
| CityKillingworth                                 | StateCT Zip06419     |
| Phone 860-663-1697 x213 Cell860-558-503          | 7 Fax 860-663-0935   |
| Email ncastro@allpointstech.com                  |                      |

<sup>\*</sup>Note that he SHPO's ability to complete a timely project review depends largely on the quality of the materials submitted.

<sup>\*\*</sup> Please be sure to include the project name and location on each page of your submission.

### **State Historic Preservation Office**

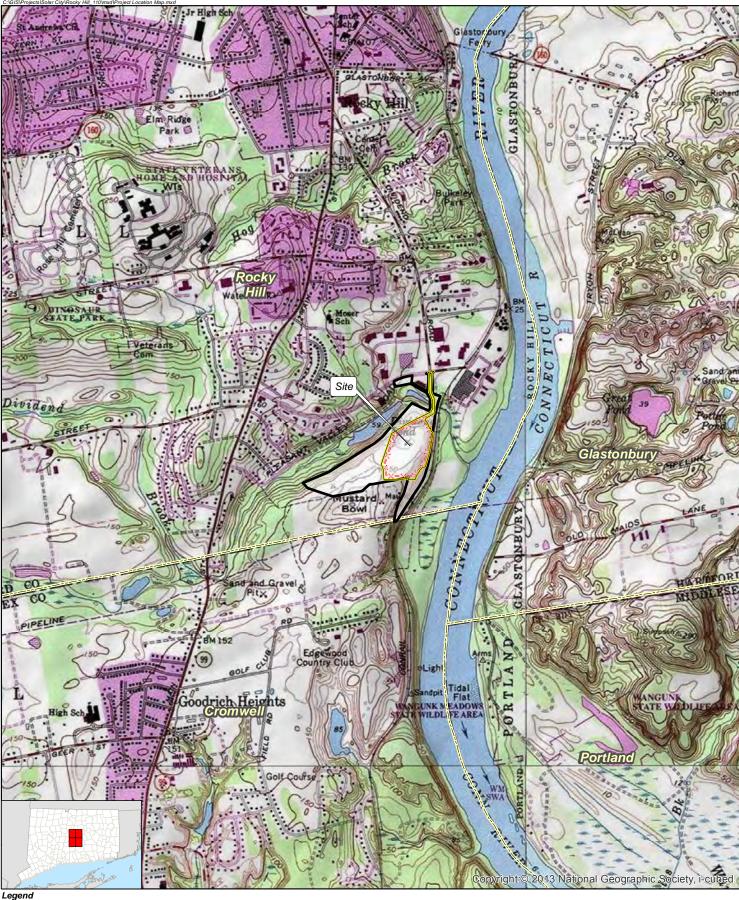
One Constitution Plaza | Hartford, CT 06103 | 860.256.2800 | Cultureandtourism.org

### PROJECT REVIEW COVER FORM

### SHPO USE ONLY

| Based on our review of the information provided to the State Historic Preservation Office, it is our op that:  | inion     |  |  |
|--|-----------|--|--|
| No historic properties will be affected by this project. No further review is requested.   |           |  |  |
| This project will cause no adverse effects to the following historic properties. No further revie requested:   | w is      |  |  |
| This project will cause no adverse effects to the following historic properties, <u>conditional</u> upon stipulations included in the attached letter:           | ı the     |  |  |
| Additional information is required to complete our review of this project. Please see the attach with our requests and recommendations.                          | ed letter |  |  |
| This project will adversely affect historic properties as it is currently designed or proposed. Please see the attached letter for further details and guidance. |           |  |  |
| Catherine Labadia Date State Historic Preservation Offier  | _         |  |  |

### Project Location Map



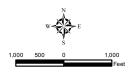
#### Legend

Site Boundary

Project Area - Limit of Proposed Work (+/-24 acres) Proposed Fenced Facility (+/-19 acres)

Municipal Boundary

Map Notes:
Base Map Source: USGS 7.5 Minute Topographic Quadrangle Maps,
Glastonbury (1992), Harford South (1992), Middle Haddam (1984),
and Middleburn (1992), CT
Site located on the Hartford South Quadrangle
Map Scale: 1.24,000
Map Date: February 2016



## **Project Location Map**

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut



# Project Description

The Site consists of a single, Town-owned parcel located at 13 Old Forge Road, encompassing a total of approximately 61.4 acres. The Site is undeveloped and portions heavily disturbed by historic clearing and excavation activities. Several areas are currently used by the Town's Department of Public Works ("DPW") for materials storage, including asphalt millings, street sweepings, sand, top soil, leaves, brush and mulch.

The Project Area consists of approximately 24-acres of undeveloped, lightly wooded land, a portion of which is currently used by the Town for materials storage. Upon completion, the facility will occupy approximately 19 acres. Access to the Site is over an existing, gated drive originating at the intersection of Old Forge Road and Dividend Road in its northern portion. The existing access drive extends south into the Site where it connects to a system of interior dirt roads.

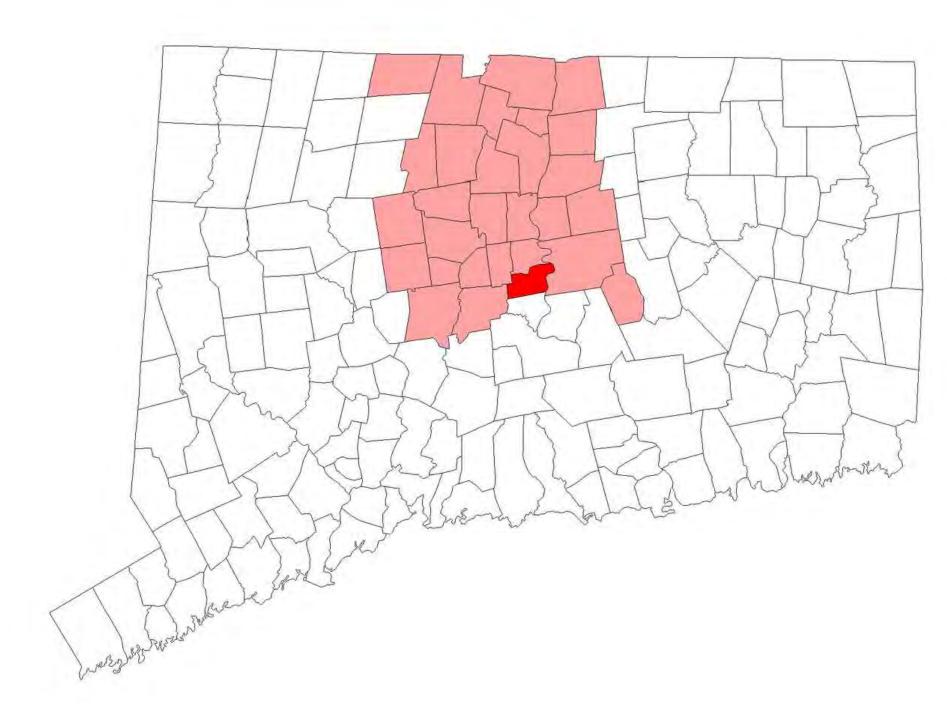
The Project will include an approximate 24-acre development on the Site. The solar array will be developed in the northern portion of the Site, which is primarily a mix of cleared land and early old field habitat, consisting of early successional trees with a dense understory of scrub/shrub and herbaceous growth. New soil disturbances will be minimized to facilitate the installation of the solar arrays and associated equipment. The Project Area includes relatively level grades such that the development can be generally accomplished without significant cuts and/or fills.

The Project Area consists of previously disturbed land. A total of  $\pm 18$  acres of early successional trees and associated dense understory will be cleared to accommodate the Project. The facility would be comprised of approximately 9,460-275 watt and 4,488-290 watt Trina Solar TSM-PD14 modules, three (3) Advanced Energy AE 500TX 500 kw inverters, and three (3) transformers. The facility would use a post-driven RBI Solar Inc. tracking system. Electrical connections would extend primarily overhead out to Old Forge Road. Once construction is complete, approximately 21 acres will be seeded for the establishment of permanent cover (turf).

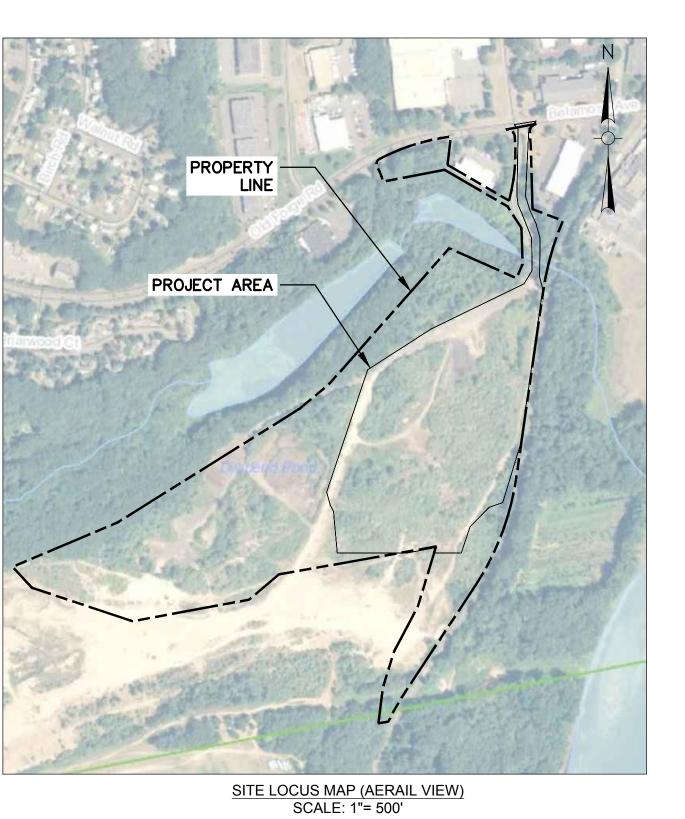
# Site Figures and Property Card

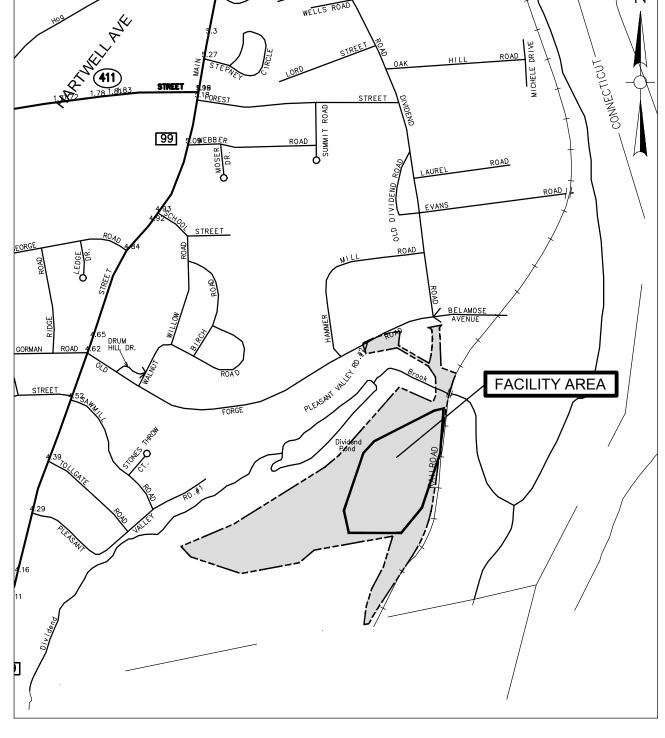
# ROCKY HILL, CONNECTICUT SOLAR PHOTOVOLTAIC (PV) PROJECT

# 13 OLD FORGE ROAD ROCKY HILL, CONNECTICUT 06067



CONNECTICUT MUNICIPAL MAP SCALE: N.T.S.





SITE LOCATION MAP SCALE: 1"=1000'

| PROJECT DIRECTORY  |   |  |  |  |
|--|---|--|--|--|
| DEVELOPER(S):<br>SOLAR CITY, INC.<br>1376 LEAD HILL BLVD.<br>ROSEVILLE, CA 95661   | RACKING SYSTEM DESIGNER:<br>RBI SOLAR<br>5513 VINE STREET<br>CINCINNATI, OH 45217 |  |  |  |
| CONTACT: JOSHUA TROGLIN<br>(650) 332-0412  | CONTACT: LOUIS "PAT" HUDEPOHL<br>513-618-2183                                     |  |  |  |
| HOST:<br>TOWN OF ROCKY HILL<br>13 OLD FORGE ROAD<br>ROCKY HILL, CONNECTICUT 06067  | UTILITY:<br>EVERSOURCE  |  |  |  |
| ENGINEER: WESTON & SAMPSON ENGINEERS, INC. 273 DIVIDEND ROAD ROCKY HILL, CONNECTICUT 06067  CONTACT: JOHN FIGURELLI (860) 513-1473 |   |  |  |  |
| ELECTRICAL ENGINEER: PLUMP ENGINEERING, INC 914 E KATELLA AVENUE ANAHEIM, CA 92805   |   |  |  |  |
| CONTACT: ANN D'ALESSANDRO<br>(518) 796-1030  |   |  |  |  |

| DRAWING INDEX - WESTON & SAMPSON         |                     |  |  |  |
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| SHEET SHEET TITLE                        |                     |  |  |  |
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| DRAWING INDEX - SOLAR CITY BLOCK 1 (JB: 0602328-00) |                                    |  |  |  |
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| SHEET   | SHEET TITLE                        |  |  |  |
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| PV-2  | SITE PLAN                          |  |  |  |
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| PV-9  | LINE DIAGRAM                       |  |  |  |
| PV-10   | MONITORING LINE DIAGRAM            |  |  |  |
| PV-11   | WARNING LABELS                     |  |  |  |
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| DRAWING INDEX - SOLAR CITY BLOCK 2 (JB: 0602329-00) |                                    |  |  |  |
|---|------------------------------------|--|--|--|
| SHEET SHEET TITLE                                   |                                    |  |  |  |
| PV-1  | COVER SHEET                        |  |  |  |
| PV-2  | SITE PLAN                          |  |  |  |
| PV-3  | ARRAY PLAN                         |  |  |  |
| PV-4  | ACCESS PLAN                        |  |  |  |
| PV-5  | STRUCTURAL DETAILS & INVERTER PADS |  |  |  |
| PV-6  | PV EQUIPMENT PLAN & ELEVATION      |  |  |  |
| PV-7  | EQUIPMENT DETAILS                  |  |  |  |
| PV-8  | ELECTRICAL SYMBOLS & NOTES         |  |  |  |
| PV-9  | LINE DIAGRAM                       |  |  |  |
| PV-10   | MONITORING LINE DIAGRAM            |  |  |  |
| PV-11   | WARNING LABELS                     |  |  |  |

| DRAWING INDEX - SOLAR CITY BLOCK 3 (JB: 0602330-00) |                                    |  |  |
|---|------------------------------------|--|--|
| SHEET SHEET TITLE                                   |                                    |  |  |
| PV-1  | COVER SHEET                        |  |  |
| PV-2  | SITE PLAN                          |  |  |
| PV-3  | ARRAY PLAN                         |  |  |
| PV-4  | ACCESS PLAN                        |  |  |
| PV-5  | STRUCTURAL DETAILS & INVERTER PADS |  |  |
| PV-6  | PV EQUIPMENT PLAN & ELEVATION      |  |  |
| PV-7  | EQUIPMENT DETAILS                  |  |  |
| PV-8  | ELECTRICAL SYMBOLS & NOTES         |  |  |
| PV-9  | LINE DIAGRAM                       |  |  |
| PV-10   | MONITORING LINE DIAGRAM            |  |  |
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|       | DRAWING INDEX - RBI SOLAR                  |
|-------|--|
| SHEET | SHEET TITLE                                |
| G-001 | COVER SHEET                                |
| G-002 | GENERAL NOTES/ MODULE SPECIFICATION SHEETS |
| S-101 | COMPONENT LAYOUT 1                         |
| S-102 | COMPONENT LAYOUT 2                         |
| S-103 | COMPONENT LAYOUT 3                         |
| S-201 | ADDITIONAL POST SECTIONS & ELEVATIONS      |
| S-301 | RACK SECTION & BAY PLAN VIEWS              |
| S-501 | DETAILS                                    |

|                              | SOLAR PHOTOVOLTAIC (PV) SYSTEM DESCRIPTION |                                     |                                     |  |  |
|------------------------------|--|-------------------------------------|-------------------------------------|--|--|
| SYSTEM MOUNTING PLANE I.D. 1 |  | MOUNTING PLANE I.D. 2               | MOUNTING PLANE I.D. 3               |  |  |
| SYSTEM SIZE                  | 1,300,750 kW                               | 1,300,750 kW                        | 1,301,520 kW                        |  |  |
| MODULE                       | (4,730) TRINA SOLAR TSM-PD14 (275W)        | (4,730) TRINA SOLAR TSM-PD14 (275W) | (4,488) TRINA SOLAR TSM-PD14 (290W) |  |  |
| TILT ANGLE                   | 30 DEGREES                                 | 30 DEGREES                          | 30 DEGREES                          |  |  |
| AZIMUTH                      | 170 DEGREES                                | 170 DEGREES                         | 170 DEGREES                         |  |  |
| RACKING                      | RBI RACKING                                | RBI RACKING                         | RBI RACKING                         |  |  |

ROCKY HILL SOLAR PROJECT



13 OLD FORGE ROAD ROCKY HILL, CT 06067



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PERMIT PLANS

JOB NO. 2150769

| Date:        | 03.04.20 |
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| Scale:       | AS SHO   |
| Drawn By:    | LEC      |
| Reviewed By: | JSP      |
| Checked By:  | JSP      |
| Approved By: | RGT      |

Drawing Title: COVER SHEET

Sheet Number:

| DECORIDATION   | EV/IOTIVIC      | DD 0.5.5.5      |
|--|-----------------|-----------------|
| DESCRIPTION  CATCH BASIN                                 | EXISTING        | PROPOS          |
| HYDRANT  | <b>III</b>      |                 |
| UTILITY POLE   | ~               | <del></del>     |
|  | O.              | •               |
| POLE-MOUNTED LIGHT FIXTURE                               | \$              |                 |
| EDGE OF PAVEMENT   |                 |                 |
| EDGE OF UNPAVED ROAD                                     |                 |                 |
| LIMIT OF WORK  |                 |                 |
| OVERHEAD WIRE (ELECTRICAL)                               | ——— G ———       |                 |
| ELECTRICAL CONDUIT (SUBGRADE)                            | — Е —           | —— Е –          |
| RAILROAD   | +++++           |                 |
| STONE WALL   | 000000000       |                 |
| RETAINING WALL   |                 |                 |
| FENCE  | <b></b>         | <del></del>     |
| INDIVIDUAL DECIDUOUS TREE                                | ₩               | $\Box$          |
| INDIVIDUAL EVERGREEN TREE                                | *               | *               |
| EDGE OF WOODS/ CLEARING                                  | Luuu            | $\sim\sim$      |
| DEBRIS / SOIL PILE / RUBBLE                              |                 |                 |
| ELECTRIC METER   |                 |                 |
| SURVEY MARKER  |                 |                 |
| PROPERTY BOUNDARY  |                 |                 |
| MOUNTING PLANE LIMIT                                     |                 |                 |
| SPOT ELEVATIONS  | x <sup>46</sup> | × <sup>46</sup> |
| CONTOUR LINES  | <del>46</del>   |                 |
| RESOURCE FLAG  | ⋈ TOB/BVW       |                 |
| GUY WIRE   | <b>O</b> -      |                 |
| EROSION CONTROL MATTING                                  |                 |                 |
| RIP RAP  | 33222222        |                 |
| SIGN   | -               |                 |
| BENCH MARK   | <b>•</b>        |                 |
| SEDIMENT/EROSION CONTROLS                                | ·               | •••             |
| ROCK OUTCROP   |                 |                 |
| SEWER MANHOLE  | S               | •               |
| MANHOLE (MH) FOR UNDERDRAIN SYSTEM                       | ©               |                 |
| DRAIN MANHOLE (DMH)                                      | 0               |                 |
| UTILITY MANHOLE  | 0               |                 |
| GROUND-MOUNTED SOLAR PV MODULES (ELECTRICALLY CONNECTED) |                 |                 |
| OVERHEAD WIRE  | OH              |                 |
| BORDERED VEGETATED WETLAND BUFFER                        |                 |                 |
| WETLAND FLAG   | ▲ WF            |                 |
| IRON PIN   | A VVF           |                 |

# **ABBREVIATIONS**

| ± | MORE OR LESS |
|---|--------------|
|   |              |

TYP TYPICAL

ACCMP ASPHALT COATED

CORRUGATED METAL PIPE

AC ALTERNATING CURRENT

DC DIRECT CURRENT

RCP REINFORCED CONCRETE PIPE

INV INVERT

FEU FLARED END UNIT

V/ WITH

WF #1 WETLAND FLAG

REC RECOVERED

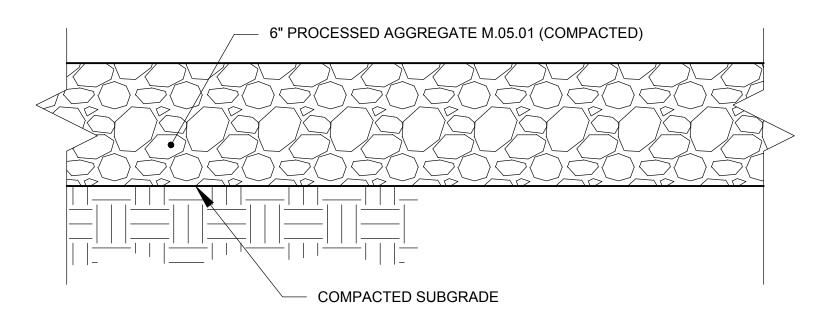
CT CONNECTICUT

DEEP DEPARTMENT OF ENERGY AND ENVIRONMENTAL PROTECTION

NOW OR FORMERLY

# **CONSTRUCTION NOTES:**

- 1. THE CONTRACTOR SHALL CALL BEFORE YOU DIG (CBYD) AT 811 OR 1-800-922-4455 AT LEAST 72 HOURS, SATURDAYS, SUNDAYS, AND HOLIDAYS EXCLUDED, PRIOR TO EXCAVATING AT ANY LOCATION. A COPY OF THE CALL BEFORE YOU DIG PROJECT REFERENCE NUMBER(S) SHALL BE GIVEN TO THE OWNER PRIOR TO EXCAVATION.
- 2. LOCATIONS OF EXISTING PIPES, CONDUITS, UTILITIES, FOUNDATIONS AND OTHER UNDERGROUND OBJECTS ARE NOT WARRANTED TO BE CORRECT AND THE CONTRACTOR SHALL HAVE NO CLAIM ON THAT ACCOUNT SHOULD THEY BE OTHER THAN SHOWN.
- 3. STONE WALLS, FENCES, CURBS, ETC. SHALL BE REMOVED AND REPLACED AS NECESSARY TO PERFORM THE WORK. UNLESS OTHERWISE INDICATED, ALL SUCH WORK SHALL BE INCIDENTAL TO CONSTRUCTION OF THE PROJECT.
- 4. ALL AREAS DISTURBED BY THE CONTRACTOR BEYOND PAYMENT LIMITS SHALL BE RESTORED AT NO ADDITIONAL COST TO THE OWNER.





**GRAVEL DRIVEWAY** 

SCALE: N.T.S.

Project:

ROCKY HILL
SOLAR PROJECT



13 OLD FORGE ROAD ROCKY HILL, CT 06067



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PERMIT PLANS

JOB NO. 2150769

Date: 03.04.2016

Scale: AS SHOWN

Drawn By: LEC

Reviewed By: JSP

Checked By: JSP

Drawing Title:

ABBREVIATIONS, NOTES, LEGEND, AND DETAILS

Sheet Number:

**G-1** 

# **GENERAL NOTES**

ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE PERFORMED IN ACCORDANCE WITH THE "CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL" (MAY 2002). THE CONTRACTOR SHALL OWN AND MAINTAIN A COPY OF THE GUIDELINES ON-SITE DURING CONSTRUCTION.

ALL DISTURBED AREAS SHALL BE KEPT TO A MINIMUM. FINAL GRADING AND RESTORATION SHALL BE ACCOMPLISHED AS SOON AS PRACTICAL.

EROSION AND SEDIMENT CONTROL STRUCTURES SHALL BE INSTALLED PRIOR TO SITE WORK. IF IT IS NOT POSSIBLE TO DO SO, THE ENGINEER SHALL BE NOTIFIED IN ORDER TO MAINTAIN THE INTEGRITY OF DESIGN.

ALL CONTROL STRUCTURES SHALL BE MAINTAINED THROUGHOUT CONSTRUCTION AND REMOVED WHEN STABILIZATION HAS BEEN ATTAINED. IF THE PROPOSED CONTROL MEASURES ARE NOT SATISFACTORY, ADDITIONAL CONTROL MEASURES SHALL BE TAKEN.

ALL RUNOFF FROM THE DISTURBED AREA SHALL BE CONTROLLED AND FILTERED. NON-WOVEN SYNTHETIC FIBER FILTER FABRIC, STRAW BALES OR SILT SOCKS SHALL BE USED IN THE AREAS SHOWN ON THE SITE PLAN AND INSTALLED AS SHOWN ON THIS PLAN.

A CT DEEP GENERAL PERMIT FOR THE DISCHARGE OF STORMWATER AND DEWATERING WASTEWATERS FROM CONSTRUCTION ACTIVITIES WILL BE REQUIRED FOR THE PROPOSED PROJECT. THE CONTRACTOR SHALL BE RESPONSIBLE FOR IMPLEMENTATION AND COMPLIANCE WITH THE APPROVED STORMWATER POLLUTION CONTROL PLAN (SWPCP).

THE CONTRACTOR MUST OBTAIN COPIES OF THE ZONING, WETLANDS AND CTDEP STORMWATER PERMITS PRIOR TO THE START OF WORK.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR IMPLEMENTATION OF SEDIMENT AND EROSION CONTROL MEASURES. THIS RESPONSIBILITY INCLUDES THE ACQUISITION OF MATERIALS, INSTALLATION, AND MAINTENANCE OF EROSION AND SEDIMENT STRUCTURES, THE COMMUNICATION AND DETAILED EXPLANATION TO ALL PEOPLE INVOLVED IN THE SITE WORK OF THE REQUIREMENTS AND OBJECTIVE OF THE EROSION AND SEDIMENT CONTROL MEASURES.

TWO (2) WEEKS PRIOR TO THE START OF WORK THE CONTRACTOR SHALL PROVIDE THE NAME AND PHONE NUMBER OF THE INDIVIDUAL RESPONSIBLE FOR IMPLEMENTATION OF THIS PLAN.

IN THE EVENT THE APPLICANT IS NOT OWNER OF THE PROPERTY, THE CURRENT OWNER SHALL HAVE ALL THE RESPONSIBILITIES LISTED IN THIS PARAGRAPH AND SHALL SUBMIT A WORKING PHONE NUMBER FOR CONTACT AT TIME OF APPLICATION FOR PERMITS. ANY CHANGE IN ENGINEER SHALL BE NOTED AT THIS TIME.

THE ENGINEER, WESTON & SAMPSON ENGINEERS, INC. (860-513-1473) #273 DIVIDEND ROAD, ROCKY HILL, CT, 06067 SHALL BE NOTIFIED OF ANY PROPOSED ALTERATION TO THE EROSION AND SEDIMENT CONTROL PLAN, PRIOR TO ALTERING, IN ORDER TO ENSURE THE FEASIBILITY OF THE ADDITION, SUBTRACTION, OR CHANGE IN THE PLAN.

# SEEDING WITHIN GROUND MOUNTED ARRAY AREA

NEW ENGLAND SEMI-SHADE GRASS AND FORBS MIX - THE NEW ENGLAND SEMI-SHADE GRASS AND FORB MIX CONTAINS A BROAD SPECTRUM OF NATIVE GRASSES AND FORBS THAT WILL TOLERATE SEMI-SHADE AND EDGE CONDITIONS. ALWAYS APPLY ON CLEAN BARE SOIL. THE MIX MAY BE APPLIED BY HYDRO-SEEDING, BY MECHANICAL SPREADER, OR ON SMALL SITES IT CAN BE SPREAD BY HAND. LIGHTLY RAKE, OR ROLL TO ENSURE PROPER SEED TO SOIL CONTACT. BEST RESULTS ARE OBTAINED WITH A SPRING SEEDING. LATE SPRING AND EARLY SUMMER SEEDING WILL BENEFIT WITH A LIGHT MULCHING OF WEED-FREE STRAW TO CONSERVE MOISTURE. IF CONDITIONS ARE DRIER THAN USUAL, WATERING WILL BE REQUIRED. LATE FALL AND WINTER DORMANT SEEDING REQUIRE AN INCREASE IN THE SEEDING RATE. FERTILIZER OR LIMING IS PROHIBITED, UNLESS PRIOR APPROVAL BY THE LOCAL CONSERVATION COMMISSION IS OBTAINED. PREPARATION OF A CLEAN WEED FREE SEED BED IS NECESSARY FOR OPTIMAL RESULTS. APPLICATION RATE 30 POUNDS PER ACRE.

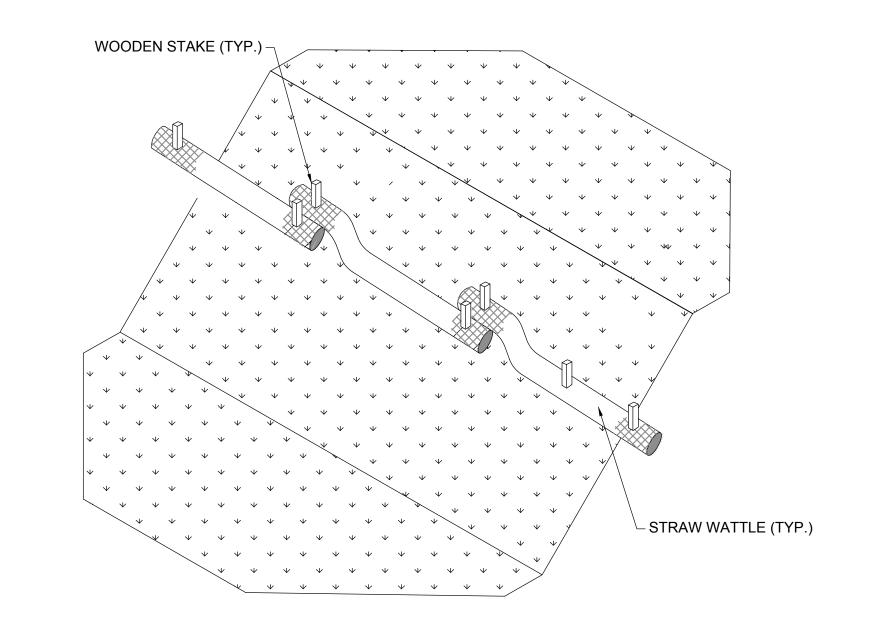
# MAINTENANCE

MAINTENANCE OF SEEDED AREAS SHALL BE THE SOLE RESPONSIBILITY OF CONTRACTOR AS DESCRIBED BELOW:

- A. CONTRACTOR SHALL MAINTAIN THE ENTIRE SEEDED AREAS UNTIL FINAL ACCEPTANCE AT THE COMPLETION OF THE PROJECT OR FOR 90 DAY, WHICHEVER IS LONGER. MAINTENANCE SHALL INCLUDE WATERING AS SPECIFIED, WEEDING, REMOVAL OF STONES WHICH MAY APPEAR AND REGULAR CUTTINGS OF THE GRASS NO CLOSER THAN 10 DAYS APART. THE FIRST CUTTING SHALL BE ACCOMPLISHED WHEN THE GRASS IS FROM 2-1/2 TO 3 INCHES HIGH. WEEKLY WATERING SHALL PROVIDE THE SEEDED AREAS WITH THE EQUIVALENT OF 1 INCH OF RAINFALL PER WEEK. IF THE SEEDED AREAS ARE WATERED BY NORMAL RAINFALL OR THE NORMAL WATERING IS INADEQUATE DUE TO WEATHER, THE CONTRACTOR MAY AT HIS/HER DISCRETION ELIMINATE OR INCREASE RESPECTIVELY, THE WATERING DURING A GIVEN WEEK. HOWEVER, SUCH ACTION BY CONTRACTOR SHALL IN NO WAY WAIVE CONTRACTOR'S RESPONSIBILITY FOR THE GROWTH AND HEALTH OF THE GRASS UNTIL FINAL ACCEPTANCE. CONTRACTOR SHALL FURNISH ALL TEMPORARY PIPE AND CONNECTIONS FOR SPRINKLING. CONTRACTOR SHALL FURNISH ALL REQUIRED WATER AT NO EXPENSE TO THE OWNER. GARDEN HOSE AND HAND SPRINKLING SHALL BE PERMITTED ONLY IN SPECIAL INSTANCES BY THE OWNER'S REPRESENTATIVE.
- B. ALL BARE SPOTS, WHICH BECOME APPARENT AS THE GRASS GERMINATES, SHALL BE RESEEDED BY CONTRACTOR AT ITS OWN EXPENSE AS MANY TIMES AS NECESSARY TO SECURE A GOOD GROWTH AND THE ENTIRE AREA SHALL BE MAINTAINED AND CUT UNTIL ALL WORK HAS BEEN COMPLETED AND FINAL ACCEPTANCE HAS OCCURRED.
- C. CONTRACTOR SHALL TAKE WHATEVER MEASURES ARE NECESSARY TO PROTECT THE GRASS WHILE IT IS GERMINATING. THESE MEASURES SHALL INCLUDE FURNISHING OF WARNING SIGNS, BARRIERS, TEMPORARY FENCE OR ANY OTHER NECESSARY MEASURES OF PROTECTION.
- D. CONTRACTOR SHALL FURNISH, PROTECT, AND MAINTAIN ALL TEMPORARY BARRIERS UNTIL FINAL ACCEPTANCE OF THE SEEDED AREAS BY THE OWNER AND SHALL REMOVE THEM UPON SUCH FINAL ACCEPTANCE, THE BARRIERS SHALL REMAIN THE PROPERTY OF CONTRACTOR AT ALL TIMES.

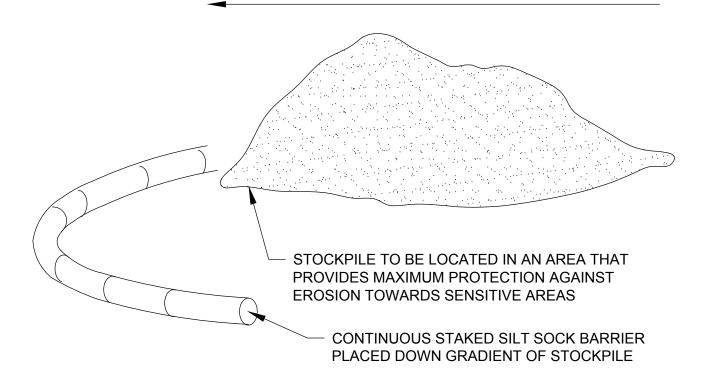
# **TEMPORARY EROSION CONTROL MEASURES:**

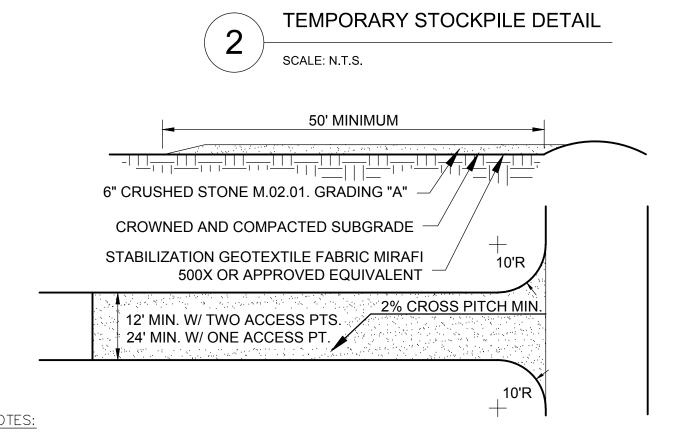
- 1. EROSION CONTROL MEASURES SHALL BE IMPLEMENTED AS INDICATED ON THESE PLANS OR AS REQUIRED BY THE ON-SITE ENGINEER.
- 2. THE SMALLEST PRACTICAL AREA OF LAND SHALL BE EXPOSED AT ANY ONE TIME.
- 3. EROSION/SEDIMENT CONTROL MEASURES SHALL BE INSTALLED AS SHOWN ON PLANS. EROSION CONTROL BARRIERS ARE TO BE MAINTAINED AND CLEANED UNTIL ALL AREAS HAVE BEEN ADEQUATELY STABILIZED.
- 4. THE TEMPORARY AND PERMANENT STORMWATER CONTROLS SHALL BE PERIODICALLY CLEANED OF SEDIMENT, OR AS REQUIRED BY THE ENGINEER. THE SEDIMENT WILL BE REMOVED TO A SECURE LOCATION SO AS TO PREVENT SILTATION OF NATURAL WATER WAYS.
- 5. SILT SOCK FILLED WITH COMPOST MUST BE A MINIMUM TUBE DIAMETER OF 12 INCHES (300mm) FOR SLOPES UP TO 50 FEET (15.24m) IN LENGTH WITH A SLOPE RATIO OF 3H:1V OR STEEPER. LONGER SLOPES OF 3H:1V MAY REQUIRE LARGER TUBE DIAMETER OR ADDITIONAL COURSING OF FILTER TUBES TO CREATE A FILTER BERM. SILT SOCK TO BE MADE OF BIODEGRADABLE BURLAP. SILT SOCK TO BE SEDIMENT FILTERMITT OR APPROVED EQUAL. OTHER REFER TO MANUFACTURER'S RECOMMENDATIONS FOR INSTALLATION INSTRUCTIONS.
- 6. INSTALL SOCK ALONG CONTOURS AND PERPENDICULAR TO SHEET OR CONCENTRATED FLOW.
- 7. CONFIGURE SOCKS AROUND EXISTING SITE FEATURES TO MINIMIZE SITE DISTURBANCE AND MAXIMIZE CAPTURE AREA OF STORMWATER RUN-OFF.
- 8. DISTURBED AREAS SHALL BE SEEDED IMMEDIATELY OR AS SOON AS PRACTICABLE.
- 9. EROSION CONTROL MEASURES SHALL BE REMOVED WHEN DISTURBED AREA IS STABILIZED. DISTURBED AREA RESULTING FROM THE MEASURE REMOVAL OPERATION SHALL BE SEEDED IN ACCORDANCE WITH THE SPECIFICATIONS.
- 10. A CHECK LIST (PROVIDED BY THE ENGINEER) SHALL BE FILLED OUT BY THE CONTRACTOR EVERY WEEK OR AFTER EACH RAINFALL EVENT OF 1/2" OR GREATER AS NOTED ABOVE.
- 11. STRIP AND STOCKPILE TOPSOIL WITHIN THE LIMITS OF THE PROPOSED DEVELOPMENT. PROTECT STOCKPILE PERIMETER WITH EROSION CONTROLS. LOCATE STOCKPILES WHERE INDICATED ON PLANS. TREE STUMPS SHALL EITHER BE REMOVED OR CHIPPED IN PLACE.
- 12. CUT TREES WITHIN THE DEFINED CLEARING LIMITS AND REMOVE CUT WOOD. CHIP BRUSH AND SLASH, STOCKPILE CHIPS FOR USE ONSITE OR REMOVE OFF-SITE.





# LONG AXIS OF STOCKPILE TO BE PERPENDICULAR TO CONTOUR





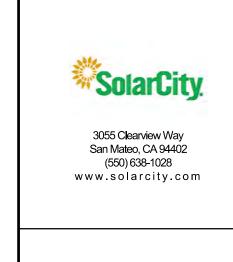
- 1. STABILIZATION FABRIC SHALL BE PLACED OVER THE ENTIRE ENTRANCE AREA PRIOR TO PLACING OF STONE. OVERLAP FABRIC PER MANUFACTURER'S SPECIFICATIONS.
- 2. ALL SURFACE WATER FLOWING OR DIVERTED TOWARDS THE CONSTRUCTION ENTRANCE SHALL BE PIPED BENEATH THE ENTRANCE ROAD.
- 3. WHEN EQUIPMENT WASHING IS REQUIRED IT SHALL BE DONE ON A SEPARATE AREA ADJACENT TO THE ENTRANCE ROAD AND STABILIZED WITH STONE. EQUIPMENT WASHING WILL BE REQUIRED IF ROAD RECEIVES SIGNIFICANT SOILS OR DEBRIS ACCORDING TO JUDGMENT BY OWNER OR OWNER'S REPRESENTATIVE.
- 4. KEEP ROADS CLEAR OF STONES, MUD, AND OTHER CONSTRUCTION DEBRIS. CLEAN PAVEMENT AS ACCUMULATIONS WARRANT AND AS ORDERED BY ENGINEER.
- 5. REMOVE SILT ACCUMULATIONS ROUTINELY AND DISPOSE OF PROPERLY SUCH THAT WATER QUALITY IS NOT IMPAIRED. DO NOT INTRODUCE SILT INTO DRAINAGE SYSTEM OR TOPSOIL/RESTORATION AREAS.







13 OLD FORGE ROAD ROCKY HILL, CT 06067



273 Dividend Road Rocky Hill, Connecticut (860) 513-1483 (800) Sampson www.westonandsampson.com



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PERMIT PLANS
JOB NO. 2150769

03.04.2016

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Reviewed By: JSP

Checked By: JSP

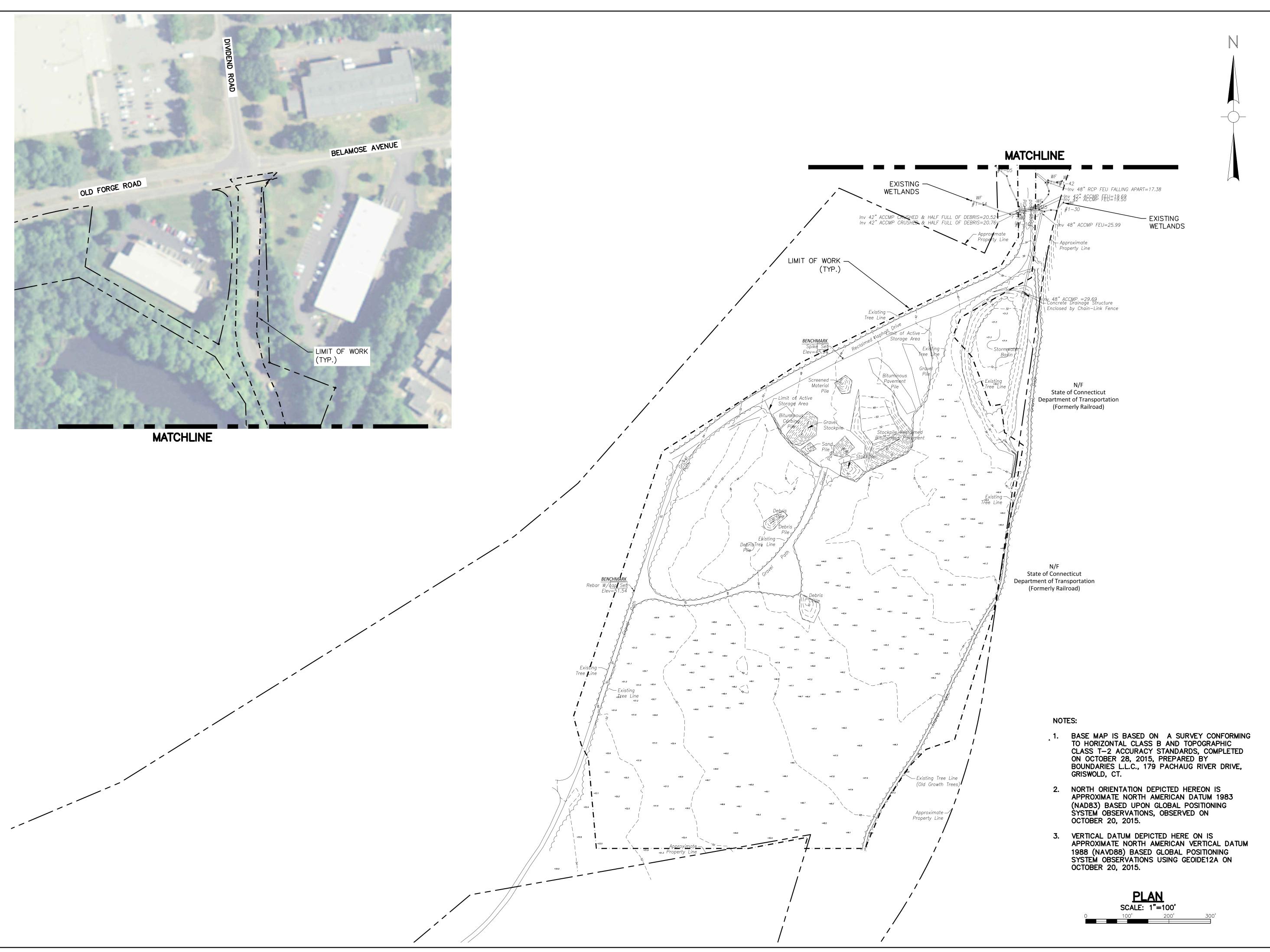
Approved By: DCH

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DETAILS

Sheet Number:

**D-1** 



ROCKY HILL SOLAR PROJECT



13 OLD FORGE ROAD ROCKY HILL, CT 06067

> 3055 Clearview Way San Mateo, CA 94402 (550) 638-1028 www.solarcity.com

# Veston&Sampson

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Cincinnati, OH 45217 (513) 618-2183

Revisions:

Rev Date Description

PERMIT PLANS

JOB NO. 2150769

Date: 03.04.2016

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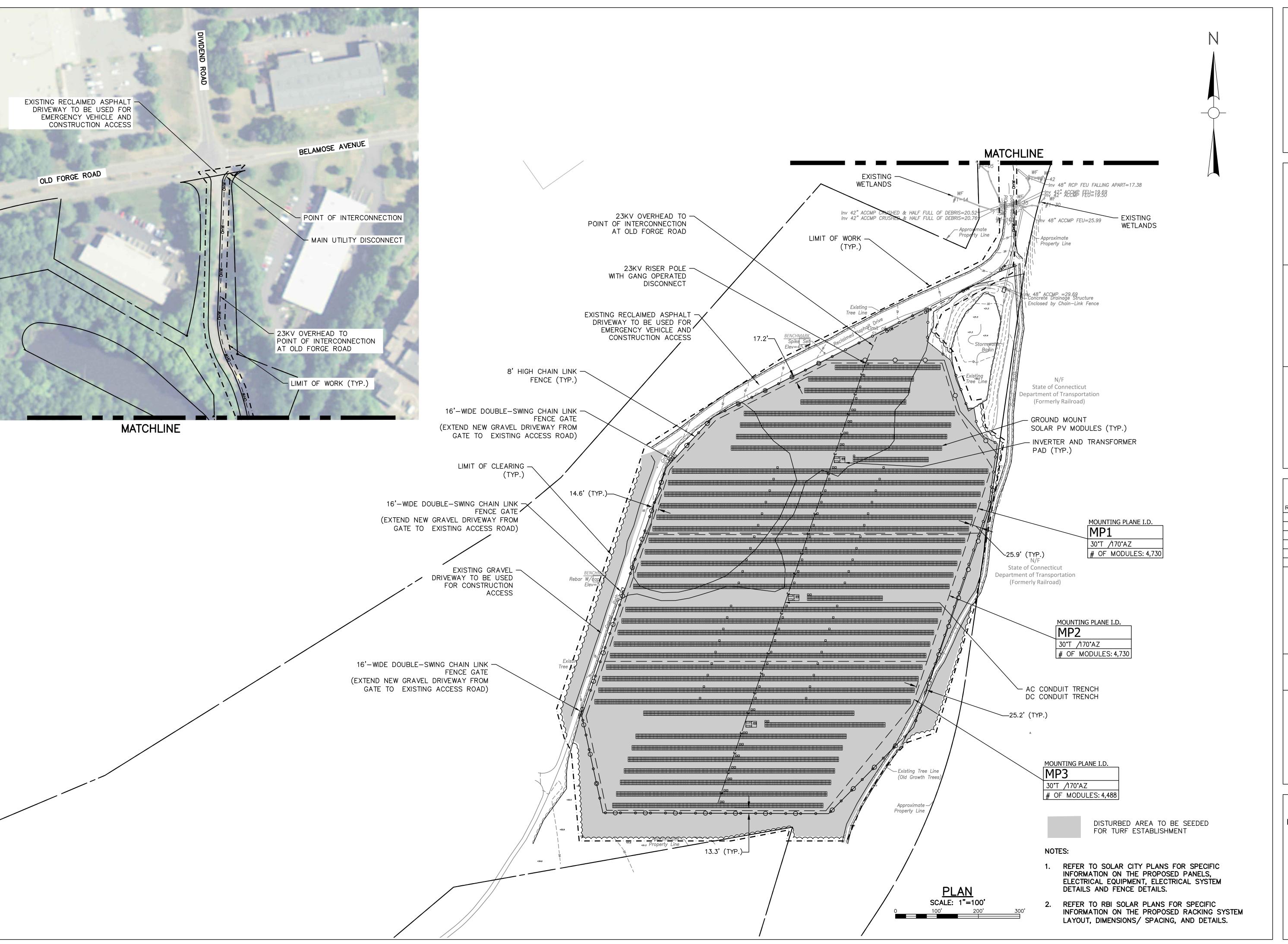
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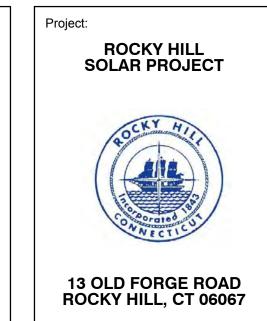
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**EXISTING CONDITIONS** 

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273 Dividend Road Rocky Hill, Connecticut





Rev Date Description

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Checked By: JSP

Approved By: RGT

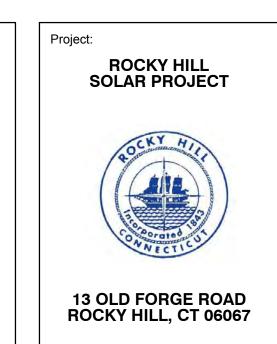
Drawing Title:

LAYOUT PLAN

Sheet Number:

**C-2** 







3055 Clearview Way San Mateo, CA 94402 (550) 638-1028 www.solarcity.com

Peston&ampson

273 Dividend Road Rocky Hill, Connecticut (860) 513-1483 (800) Sampson www.westonandsampson.com



Rev Date Description

Seal:

PERMIT PLANS

JOB NO. 2150769

Date: 03.04.2016

Scale: 1"=100'

Drawn By: LEC

Reviewed By: LEC

Checked By: JSP

Approved By: RGT

Drawing Title:

SEDIMENTATION AND EROSION CONTROL PLAN

Sheet Number:

**C-3** 



Site Boundary

Existing Access Drive

Existing Materials Pile

10' Contour Line

2' Contour Line

X=X= Proposed Fenced Facility (+/-19 acres)

\*\*\*\* Existing Treeline/Clearing Limit

Map Notes: Base Map Source: 2012 Aerial Photograph (CTECO) Map Scale:1 Inch = 400 feet Map Date: February 2016

Project Area - Limit of Proposed Work (+/-24 acres)

Start/End Wetland Flag

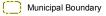
Delineated Wetland Boundary

Wetland Area

CTDEEP Watercourse

CTDEEP Waterbody

Approximate Assessor Parcel Boundary (CTDEEP)



# **Existing Conditions Map**

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut







Site Boundary

Existing Access Drive

X=X= Proposed Fenced Facility (+/-19 acres)

Proposed Overhead Wire

Proposed Underground Trench

Existing Treeline/Clearing Limit

Proposed Solar Module Proposed Electrical

Map Notes: Base Map Source: 2012 Aerial Photograph (CTECO) Map Scale:1 inch = 500 feet Map Date: February 2016



Disturbed Area to be Seeded for Turf Establishment (+/-21 acres)

Limits of Orange Construction Fencing

#### CTDEEP Watercourse

CTDEEP Waterbody

**Delineated Wetland Boundary** 

Wetland Area

Approximate Assessor Parcel Boundary (CTDEEP) Municipal Boundary



# **Proposed Conditions Map**

Proposed Solar PV Facility Town of Rocky Hill Old Forge Road Rocky Hill, Connecticut



# **Town of Rocky Hill Property Summary Report**

# **R013 OLD FORGE ROAD**

PARCEL ID: 18-093 ACCOUNT NUMBER: 007408

LOCATION: R013 OLD FORGE ROAD

OWNER NAME: ROCKY HILL TOWN OF



18-093-001 11/04/2012

#### **OWNER OF RECORD**

**ROCKY HILL TOWN OF** 

761 OLD MAIN STREET

ROCKY HILL, CT 06067-1517



| LI | VING AREA: | null | ZONING: | OP | ACREAGE: | 61.38 | ĺ |
|----|------------|------|---------|----|----------|-------|---|
|----|------------|------|---------|----|----------|-------|---|

| SALES HISTORY      |             |             |            |  |  |  |  |  |  |
|--------------------|-------------|-------------|------------|--|--|--|--|--|--|
| OWNER              | BOOK / PAGE | SALE DATE   | SALE PRICE |  |  |  |  |  |  |
| ROCKY HILL TOWN OF | 283/ 207    | 30-Aug-1994 | \$0.00     |  |  |  |  |  |  |

| CURRENT PARCEL VALUE |              |               |        |       |              |  |  |  |  |
|----------------------|--------------|---------------|--------|-------|--------------|--|--|--|--|
| TOTAL:               | \$129,640.00 | IMPROVEMENTS: | \$0.00 | LAND: | \$129,640.00 |  |  |  |  |

| ASSESSING HISTORY |                |                   |                |  |  |  |  |  |
|-------------------|----------------|-------------------|----------------|--|--|--|--|--|
| FISCAL YEAR       | TOTAL VALUE    | IMPROVEMENT VALUE | LAND VALUE     |  |  |  |  |  |
| 2014              | \$129,640.00   | \$0.00            | \$129,640.00   |  |  |  |  |  |
| 2013              | \$129,640.00   | \$0.00            | \$129,640.00   |  |  |  |  |  |
| 2012              | \$1,760,430.00 | \$0.00            | \$1,760,430.00 |  |  |  |  |  |
| 2011              | \$1,760,430.00 | \$0.00            | \$1,760,430.00 |  |  |  |  |  |
| 2010              | \$1,760,430.00 | \$0.00            | \$1,760,430.00 |  |  |  |  |  |
| 2009              | \$1,760,430.00 | \$0.00            | \$1,760,430.00 |  |  |  |  |  |
| 2008              | \$490,000.00   | \$0.00            | \$490,000.00   |  |  |  |  |  |
| 2007              | \$306,250.00   | \$0.00            | \$306,250.00   |  |  |  |  |  |
| 2006              | \$306,250.00   | \$0.00            | \$306,250.00   |  |  |  |  |  |

Preliminary Archeological Assessment with Historic Maps, Soil Map, and Site Photographs



### INTEGRATED HISTORIC PRESERVATION PLANNING

February 23, 2016

Ms. Nicole Castro All-Points Technology Corporation 3 Saddlebrook Drive Killingworth, Connecticut 06419

RE: Preliminary Archeological Assessment of a Proposed Solar Power Generation Facility Located Along Old Forge Road in Rocky Hill, Connecticut

Ms. Castro:

Heritage Consultants, LLC, is pleased to have this opportunity to provide All-Points Technology Corporation with the following preliminary archeological assessment of a proposed solar power generation facility located along Old Forge Road in Rocky Hill, Connecticut (Figure 1). The facility will contain a single large solar array with panels extending from ca., 6.5 ft above the ground surface. The current project entailed completion of an existing conditions cultural resources summary based on the examination of GIS data obtained from the Connecticut State Historic Preservation Office, as well as historical data, aerial photographs, and topographic quadrangles maintained by Heritage Consultants, LLC. This investigation is based upon project location information provided to Heritage Consultants, LLC by All-Points Technology Corporation. The objectives of this study were to gather and present data regarding previously identified cultural resources situated within 1.6 km (1 mi) of the proposed solar power generation facility and to investigate the Area of Potential Effect (APE) in terms of its natural and historical characteristics so that the need for completing additional cultural resources investigations could be evaluated.

Figures 2 and 3 show that although there was a developed road network and a rail line in the project region by the mid to late nineteenth century, the area encompassing the proposed solar power generation consisted largely an outlying parcel of land. However, there were two mills adjacent to the western border of the APE. They included the Bulkeley Corn Mill and the Billings Manufacturing Company. Both were powered by large mill ponds that are located adjacent to the western corner of the proposed project parcel. This interpretation is confirmed by Figure 4, an aerial image dating from 1934, which shows that the proposed solar array areas was situated within a forested area situated adjacent to two mill ponds. Figure 5, which is an aerial image taken in 1951, documents that no large scale changes had occurred in immediate vicinity of the proposed solar power generation facility as of the middle of the twentieth century; the area remained largely forested and undeveloped. Figure 6, an aerial image captured in 1962, shows large scale changes to the proposed project area, including massive sand and gravel operation that disturbed the northern third of the APE. Figure 7, an aerial image taken just eight years later in 1970, shows that the sand and gravel operation had been expanded throughout most of the proposed project area, resulting in massive disturbance of the soils therein. The subsequent aerial image, Figure 8, was taken in 1997, and it demonstrates that the entirety of the APE has been impacted by the removal of sand and gravel. This final aerial image show the APE in 2014, by which time some areas had been covered in scrub brush and was being used by the town for dumping construction debris and brush (Figure 9). The Nicole Castro February 23, 2016 Page 2

level of disturbance described above is confirmed by soil mapping of the APE, which shows that the vast majority of the area consists of Udorthent soils (Figure 10). These soils result from grading, smoothing, cutting, and filling operations. They retain no potential to yield intact archaeological deposits.

A review of previously recorded cultural resources on file with the Connecticut State Historic Preservation Office revealed that while no National Register of Historic Places properties have been identified within 1.6 km (1 mi) of the proposed solar power generation facility, the Dividend Brook Industrial Archaeological District is situated to the west of the APE (Figures 11 and 12). This district contains Sites 119-13, 119-14, 119-16, and 119-17. As mentioned above, these sites and landscape features include the Bulkeley Corn Mill and the Billings Manufacturing Company building; they also consist of a large stone dam that holds back the mill pond for these facilities, as well as an adjacent raceway and a second mill pond to the north. All of these items are significant from an archaeological perspective; however, the border of the Dividend Brook Industrial Archaeological District as it has been reproduced from the official State of Connecticut Site form in Figure 12 is in error. Figure 12 shows the district as overlapping with the APE. This overlap should be changed to follow the western and northwestern border of the proposed project area since the area it now encompasses in the northeast has been disturbed and contains no historic features.

A pedestrian survey of the proposed project parcel was completed on February 23, 2016 (Photos 1 through 10). The results of this effort confirmed the disturbed nature of the APE. The pedestrian survey also was conducted to assess the views from the APE toward the archaeological district and vice versa in order to determine whether or not the proposed project would have a visual impact on the Dividend Brook Industrial Archaeological District. As seen in Photo 2 the features associated with the Dividend Brook Industrial Archaeological District are not visible from the proposed project area due to the presence of a dense treeline, which will remain in place after construction of the solar facility. In addition, the APE could not be seen from the above ground features associated with the Dividend Brook Industrial Archaeological District due to the presence of the above-referenced treeline, as well as the lower topography in the vicinity of the historic building locations.

In sum, the proposed project area has been thoroughly disturbed and no longer possesses any potential to yield intact archaeological deposits. In addition, the proposed construction project will not result in any impacts to the viewshed of the Dividend Brook Industrial Archaeological District. As a result, it is the professional opinion of Heritage Consultants, LLC that no additional archaeological investigation of the APE is required prior to construction. If you have any questions regarding this Technical Memorandum, or if we may be of additional assistance with this or any other projects you may have, please do not hesitate to call us at 860-667-3001 or email me dgeorge@heritage-consultants.com. We are at your service.

Sincerely,

David R. George, M.A., R.P.A Heritage Consultants, LLC

Deul R. Hurge

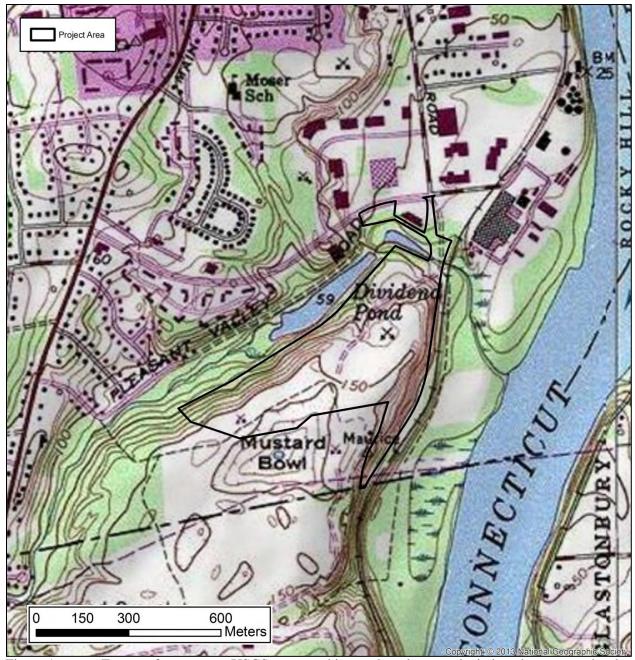


Figure 1. Excerpt from recent USGS topographic quadrangle map depicting the proposed solar system in Rocky Hill, Connecticut.

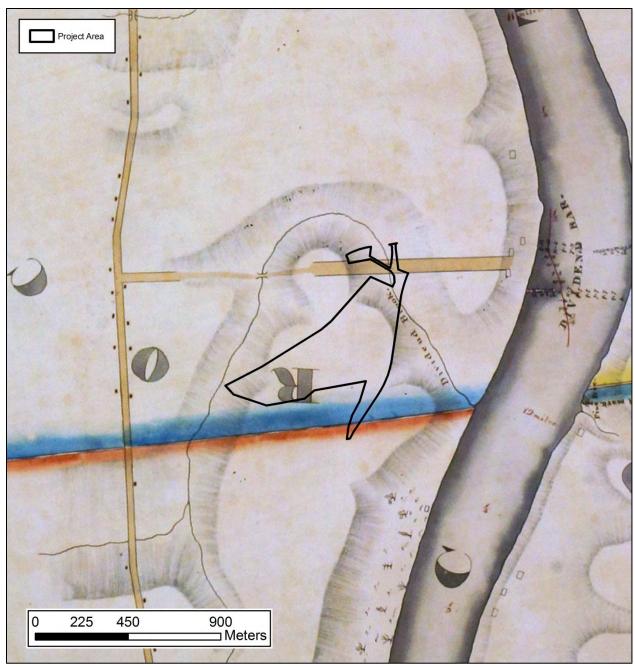


Figure 2. Excerpt from a 1846 historic map depicting the proposed solar system in Rocky Hill, Connecticut.

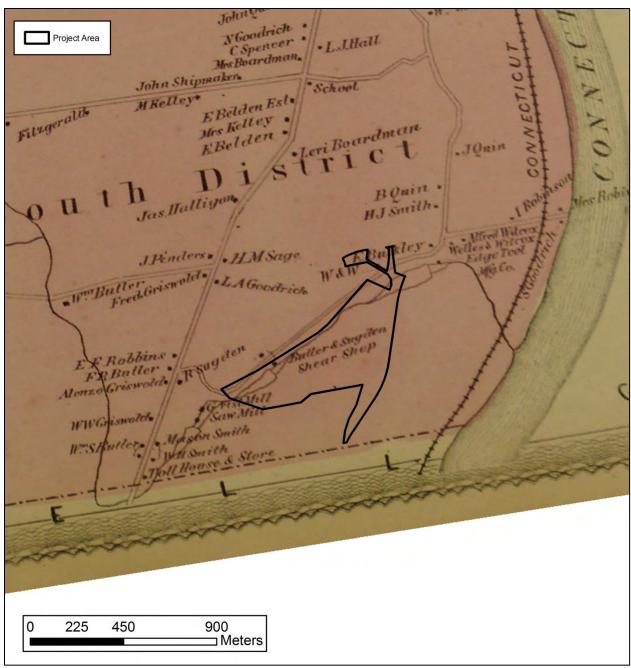


Figure 3. Excerpt from an 1869 historic map depicting the proposed solar system in Rocky Hill, Connecticut.

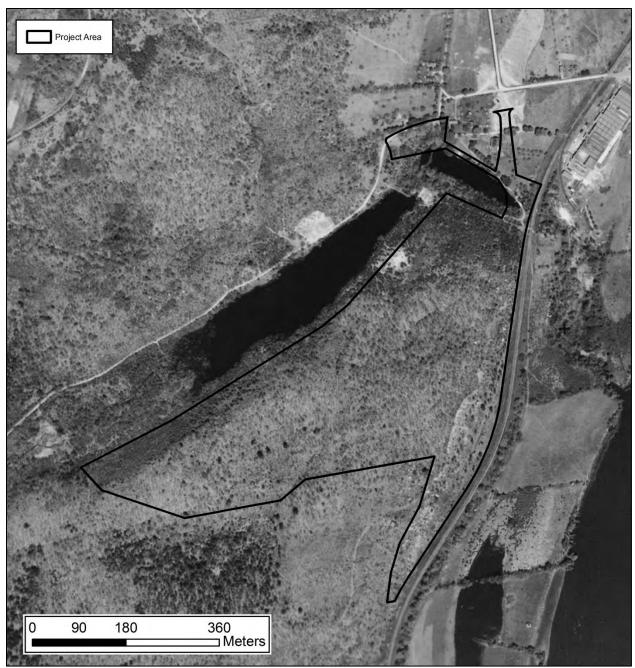


Figure 4. Excerpt from a 1934 aerial image depicting the proposed solar system in Rocky Hill, Connecticut.

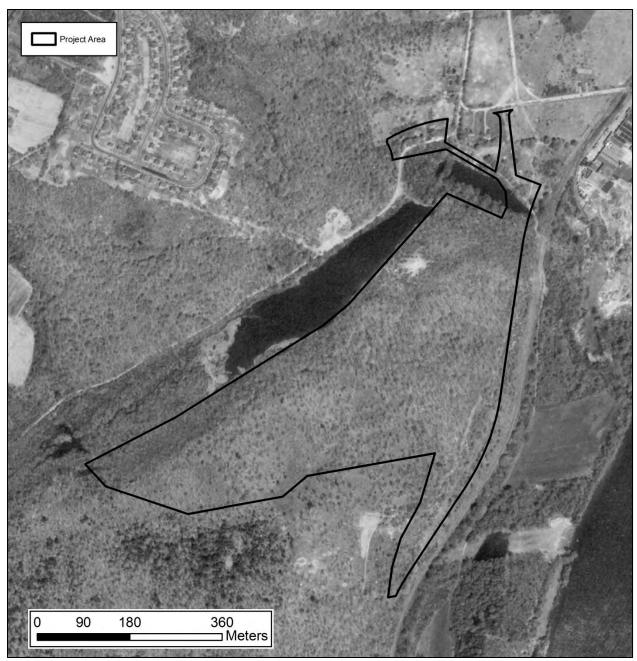


Figure 5. Excerpt from a 1951 aerial image depicting the proposed solar system in Rocky Hill, Connecticut.

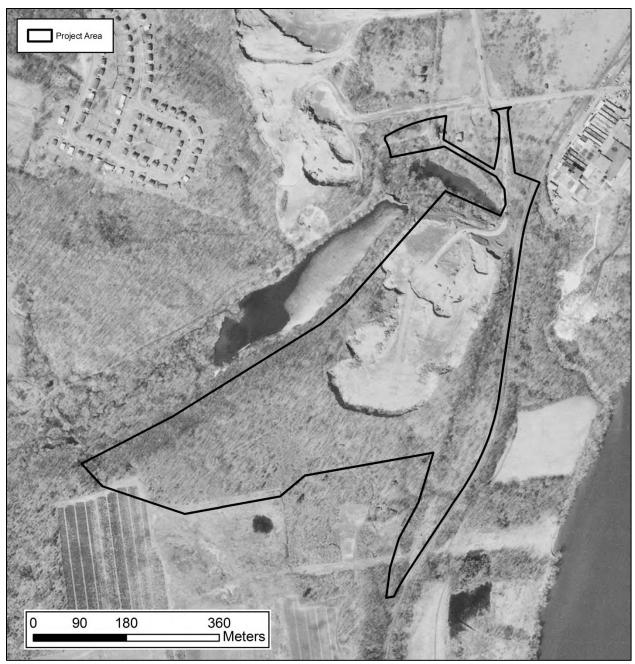


Figure 6. Excerpt from a 1962 aerial image depicting the proposed solar system in Rocky Hill, Connecticut.

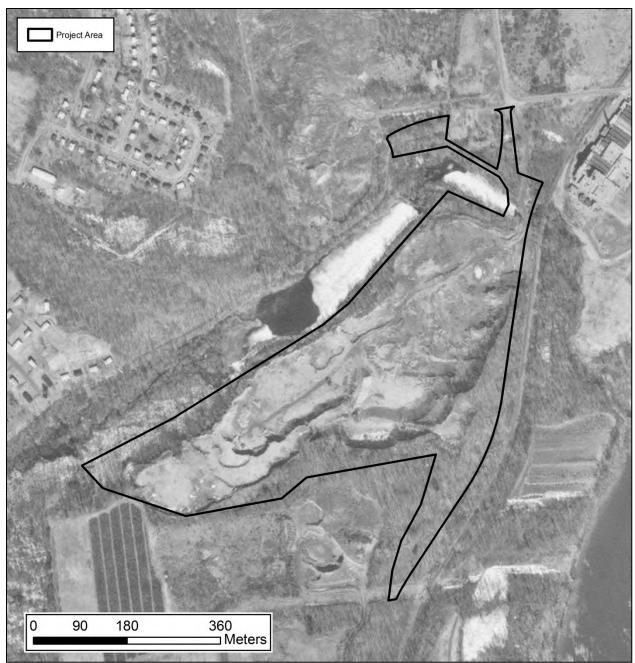


Figure 7. Excerpt from a 1970 aerial image depicting the proposed solar system in Rocky Hill, Connecticut.

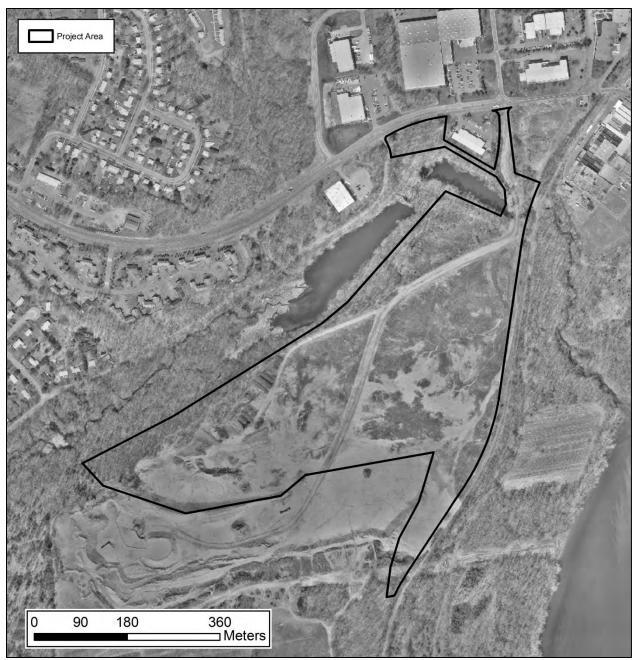


Figure 8. Excerpt from a 1997 aerial image depicting the proposed solar system in Rocky Hill, Connecticut.

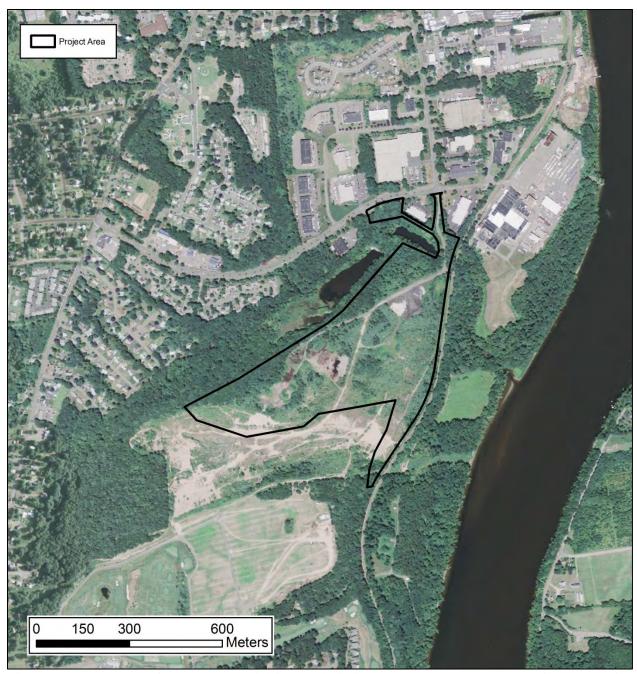


Figure 9. Excerpt from a 2014 aerial image depicting the proposed solar system in Rocky Hill, Connecticut.

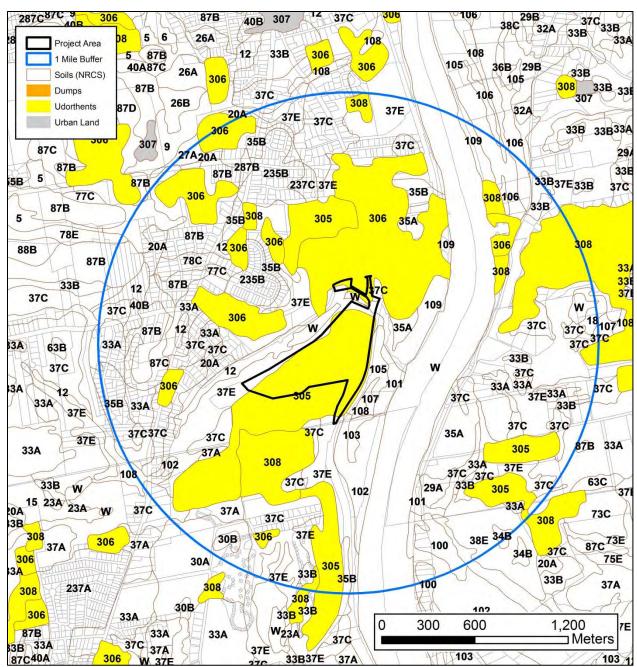


Figure 10. Digital map depicting the various soil types situated throughout the area of the proposed solar system in Rocky Hill, Connecticut (note soil code 305 consists of Udorthent soils associated with areas that have been substantially mined and disturbed).

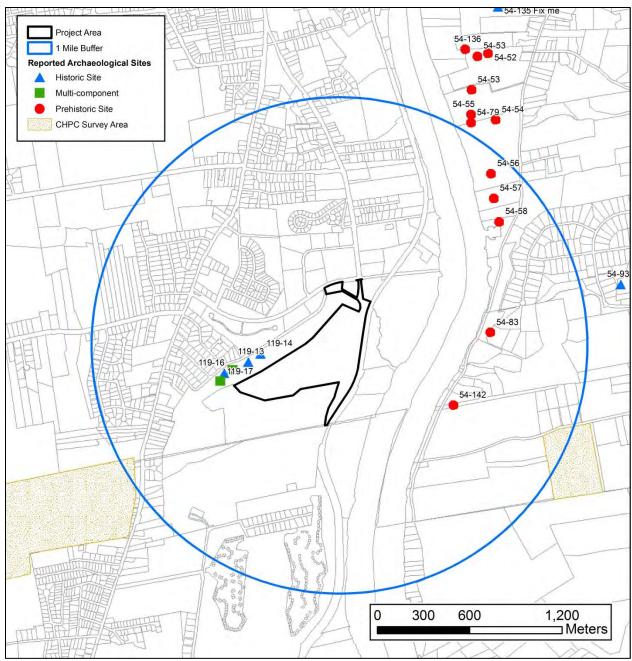


Figure 11. Digital map depicting the locations of previously recorded archaeological sites in the vicinity of the proposed solar system in Rocky Hill, Connecticut.

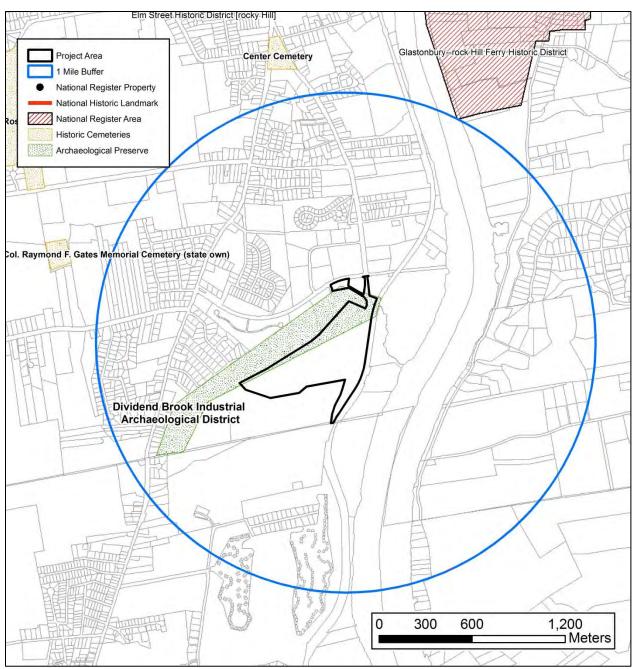


Figure 12. Digital map depicting the locations of previously National Register of Historic Places properties in the vicinity of the proposed solar system in Rocky Hill, Connecticut.



Figure 13. Aerial view of the proposed project area depicting the location and direction of each the following photographs.



Photo 1. Overview photo of the proposed tower location facing southwest.



Photo 2. Overview photo of the Dividend Brook Industrial Archaeological District facing southwest from the proposed project area.



Photo 3. Overview photo of the north central portion of the proposed project area location facing south.



Photo 4. Overview photo of the south central portion of the proposed project area facing south.



Photo 5. Overview photo of the southeastern portion of the proposed project area facing southeast.



Photo 6. Overview photo of the east central portion of the proposed project area facing east.



Photo 7. Overview photo of the north central portion of the proposed project area facing southeast facing north.



Photo 8. Overview photo from the proposed tower location facing east.



Photo 9. Overview photo of the Dividend Brook Industrial Archaeological District facing southeast toward the proposed project area (note that the project area is not visible from the district).



Photo 10. Overview photo of the eastern portion of the Dividend Brook Industrial Archaeological District facing southeast toward the proposed project area (note that the project area is not visible from the district).

# **APPENDIX E Construction Schedule**

#### **Construction Schedule for Rocky Hill Solar Array**

|  | Prerequisites to |        |        |        |        |        |        |        |        |        |         |         |         |
|--|------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|
| Activity                               | Construction     | Week 1 | Week 2 | Week 3 | Week 4 | Week 5 | Week 6 | Week 7 | Week 8 | Week 9 | Week 10 | Week 11 | Week 12 |
| Siting Council Approval                | X                |        |        |        |        |        |        |        |        |        |         |         |         |
| Rocky Hill Building/Electrical Permits | Х                |        |        |        |        |        |        |        |        |        |         |         |         |
| State Permits                          | X                |        |        |        |        |        |        |        |        |        |         |         |         |
| Remove Brush and Trees                 |                  | Χ      | Χ      |        |        |        |        |        |        |        |         |         |         |
| Establish Erosion Control              |                  |        | Χ      | Χ      |        |        |        |        |        |        |         |         |         |
| Site Grading                           |                  |        | Χ      | Х      | Χ      | Х      | Χ      |        |        |        |         |         |         |
| Install Racking and Solar Panels       |                  |        |        |        | Χ      | Χ      | Χ      | Χ      | Χ      | Χ      | Х       | Х       |         |
| Install Utility Equipment              |                  |        |        |        |        |        |        |        | Χ      | Χ      | Х       |         |         |
| Install Perimeter Fence                |                  |        |        |        |        |        |        |        |        | Χ      | Х       | Х       |         |
| Local Inspections                      |                  |        |        |        |        |        |        |        |        |        |         |         | Х       |

# APPENDIX F Construction Work Hours/Days Letter



3/17/2016

Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

RE: Solar Application, RO13, Rocky Hill, CT 06051

Work Hours at Site

To Whom It May Concern:

The following work schedule will be maintained during the construction of the Rocky Hill solar arrays:

Working hours will be 7am-7pm, 6 days a week, Monday thru Saturday.

Best regards,

Kevin Angers Project Manager SolarCity

# APPENDIX G Big Sand Tiger Beetle Protection Plan

### **BIG SAND TIGER BEETLE PROTECTION PLAN**

Due to the Project Area's proximity to optimal tiger beetle habitat (i.e., unvegetated sands), a comprehensive protection plan is proposed to avoid unintentional impact to this species during construction of the proposed facility. The Big Sand Tiger Beetle Protection Plan consists of various types of protection measures including protection of nearby "Early Old Field/Unvegetated Sands" habitat areas with installation of a restrictive barrier along the southern and western peripheries of the Project Areas, and implementation of contractor awareness training and environmental monitoring measures.

It is of the utmost importance that the Contractor complies with the Big Sand Tiger Beetle Protection Plan requirements for the implementation of protective measures and the education of its employees and subcontractors performing work within the Project Area. This protection program shall be implemented regardless of the time of year construction activities occur. All-Points Technology Corporation, P.C. ("APT") will serve as the Project Environmental Monitor for this project to ensure that the Big Sand Tiger Beetle Protection Plan is implemented properly. The Contractor shall contact Matthew Gustafson, Environmental Scientist at APT, at least five (5) business days prior to the pre-construction meeting. Mr. Gustafson can be reached by telephone at (860) 663-1697 ext. 202 or via email at mgustafson@allpointstech.com.

#### 1. Early Old Field/Unvegetated Sands Protection Measures

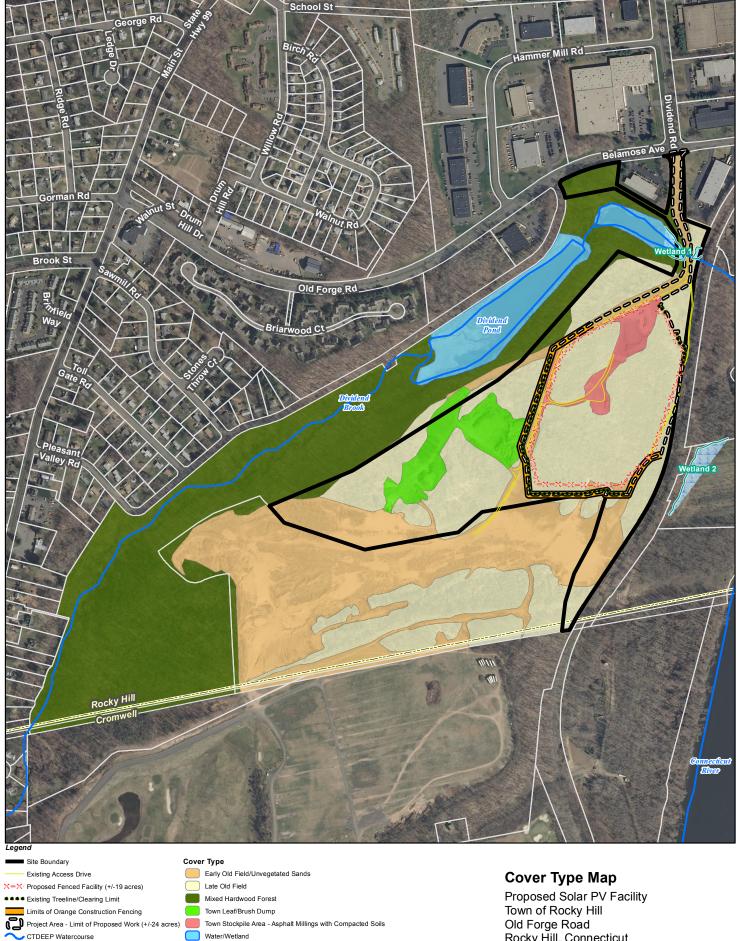
a. The limits of the Project Area shall be isolated from the majority of the Early Old Field/Unvegetated Sands located to the south and west through installation of orange construction fencing (limits depicted on Proposed Conditions Map provided in Attachment 1). The Contractor shall install orange construction fencing around the identified portion of the Project Area to isolate construction activities from potential encroachment into Early Old Field/Unvegetated Sands habitats throughout the duration of the construction project. APT will inspect the orange fencing installation prior to any construction activities or equipment mobilization to the Project Area. This isolation fencing shall be inspected daily by the Contractor to ensure that it is maintained in good condition. The Contractor shall repair any within 24 damaged fencing hours. No work, stockpiling/staging materials/vehicles/equipment, transport of vehicles, or work of any kind shall occur west or south of the orange construction fencing isolation barrier limits.

#### 2. Contractor Awareness Training

- a. Prior to work on site and initial deployment/mobilization of equipment and materials, the Contractor shall attend an educational session at the pre-construction meeting with the Project Environmental Monitor. This orientation and educational session will consist of information on the Big Sand Tiger Beetle (*Cicindela Formosa generosa*) and the associated Early Old Field/Unvegetated Sands habitat areas and the need to follow protective measures as described herein.
- b. The Contractor will be provided cell phone and email contacts for APT Environmental Monitoring staff to immediately report any encounters with Big Sand Tiger Beetle. Poster materials (example provided in Attachment 2) will be provided by APT to the Contractor for posting on the job site to maintain worker awareness, along with any visitors, to the sensitive environmental nature of the job site.

#### 3. Monitoring and Reporting

- a. Any observations of tiger beetles by the Contractor shall be immediately reported to APT.
- b. APT will provide periodic inspections of the isolation fencing throughout the duration of construction activities.
- c. Daily Compliance Monitoring Reports (brief narrative and applicable photos) will be prepared for any inspections performed by APT and submitted to SolarCity for compliance verification. Any observations of tiger beetles will be included in the reports.
- d. Following completion of the construction project, APT will provide a Compliance Monitoring Summary Report to SolarCity documenting the monitoring and maintenance of the barrier fence and erosion control measures and any turtle observations. SolarCity will provide a copy of the Compliance Monitoring Summary Report to the Connecticut Siting Council for compliance verification.
- e. Any observations of Big Sand Tiger Beetle will be reported to CTDEEP by APT, with photo-documentation (if possible) and with specific information on the location and disposition of the insect.



Municipal Boundary

Approximate Assessor Parcel Boundary (CTDEEP)

Delineated Wetland Boundary

Wetland Area

Rocky Hill, Connecticut



## **CAUTION**

### BIG SAND TIGER BEETLE ARE KNOWN TO INHABIT THIS AREA



**Identification:** Big Sand Tiger Beetle (*Cicindela Formosa generosa*) or "tiger beetle" is an invertebrate with usually shiny metallic bronze, blue, green, purple or orange body ranging from 10 - 21 mm. They are generally fast runners with long legs and long antennae that arise from the top of the head. Most are diurnal (daytime), sun loving species found in blowouts dunes, and other fin sparely vegetated sands. This sandy habitat is located on the southern and western peripheries of the Project Area, and extends outside the Project Area to the south and southwest.

What to do if you find a tiger beetle: Tiger beetles are protected by Connecticut's threatened and endangered species legislation and <u>cannot</u> be injured, killed, or retained as a specimen. If you find a tiger turtle, work shall be suspended in that area of the project. The tiger beetle should not be moved or disturbed in any manner as it is possible its burrow is close by (with the additional likelihood of other tiger beetle burrows in close proximity). The Project Environmental Monitor (listed below) should be immediately contacted, who will help assist in how to properly proceed.

Who to contact: Please report any observations of tiger beetle immediately to Matt Gustafson of All-Points Technology Corp., P.C. at (860) 617-0613.

# APPENDIX H Aquifer Protection Plan

#### **ENVIRONMENTAL NOTES**

#### **Gardiner Expansion APA No. 67 Aquifer Protection Area**

The 3.9 megawatt ("MG") solar based electric generating facility ("Project") proposed by SolarCity at 13 Old Forge Road in Rocky Hill, Connecticut is located within the Gardiner Expansion Aquifer Protection Area No. 67 ("APA").

The following precautions, protective measures, monitoring and notifications to protect this important resource shall be implemented during construction of the facility.

#### **Contractor Environmental Awareness Training & Notification**

The Rocky Hill Aquifer Protection Agency will be noticed at least 48 hours in advance of a preconstruction meeting with an invitation to attend. During the Project's pre-construction meeting, the contractor will be made aware of the special protective precautions noted above that are required due to the Project's location in the APA.

Prior to work on site, the Contractor shall attend an environmental awareness training session at the pre-construction meeting with All-Points Technology Corporation, P.C. ("APT"). This orientation and educational session will consist of an introductory meeting with APT stressing the environmentally sensitive nature of the Project due to its location within the APA. Caution poster materials will be provided by APT and displayed on the job site to maintain worker awareness as the project progresses.

#### **Best Management Practices for Water Quality**

The SolarCity construction Project will follow an approved soil erosion and sedimentation control plan designed in accordance with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control. The installed erosion devices will be inspected periodically throughout the construction period, with a focus on after significant rainfall events (e.g., greater than one quarter inch over a 24-hour period) to ensure that proper precautions are taken to avoid the release of sediment into nearby resource areas. In addition to the site contractor being responsible for the proper installation and daily inspection of erosion and sedimentation ("E&S") controls, staff from APT will periodically inspect E&S controls and document their conditions and recommend any actions necessary to bring the controls back into compliance. The E&S controls and inspection protocols will protect water quality within the APT. A summary report of APT's compliance monitoring inspections will be submitted to the Connecticut Siting Council following completion of construction. Any incidents of significant release of sediment will be immediately reported to the Connecticut Siting Council. In addition, Town of Rocky Hill staff will be allowed access to the Project during construction for periodic field inspections should they desire.

E&S control items subject to inspection include, but are not limited to the following:

- Construction Entrance Pad
- Sediment/ Detention Basins
- Catch Basin Silt Socks
- Seeding & Mulching
- Drainage Swale Check Dams
- Sediment Traps
- Temporary Soil Stockpile Areas
- Silt Fencing/Straw Bales/Straw Wattles/Compost Filter Socks
- Drainage Swales
- Other Site-Specific Erosion Control Devices

#### Petroleum/Hazardous Materials Storage and Spill Prevention Plan

Certain precautions are necessary to store petroleum and hazardous materials, refuel and contain and properly clean up any inadvertent fuel or petroleum (i.e., oil, hydraulic fluid, etc.) spill due to the Project's location in an APA. A spill containment kit consisting of a sufficient supply of absorbent pads and absorbent material will be maintained by the site contractor at the construction site throughout the duration of the Project. In addition, a waste drum will be kept on site to contain any used absorbent pads/material for proper disposal off site.

The following, but not limited to, restrictions, protective measures and procedures, will be adhered to by the contractor.

#### Petroleum and Hazardous Materials Storage and Refueling

- Servicing of machinery shall be completed outside of the APA.
- Refueling of vehicles or machinery shall occur a minimum of 100 feet from wetlands or watercourses and shall take place on an impervious pad with secondary containment designed to contain fuels.
- Fuel and other hazardous materials shall not be stored within the APA.
- Any fuel or hazardous materials that must be kept within the APA during working hours shall be stored on an impervious surface utilizing secondary containment.

#### **Initial Spill Response**

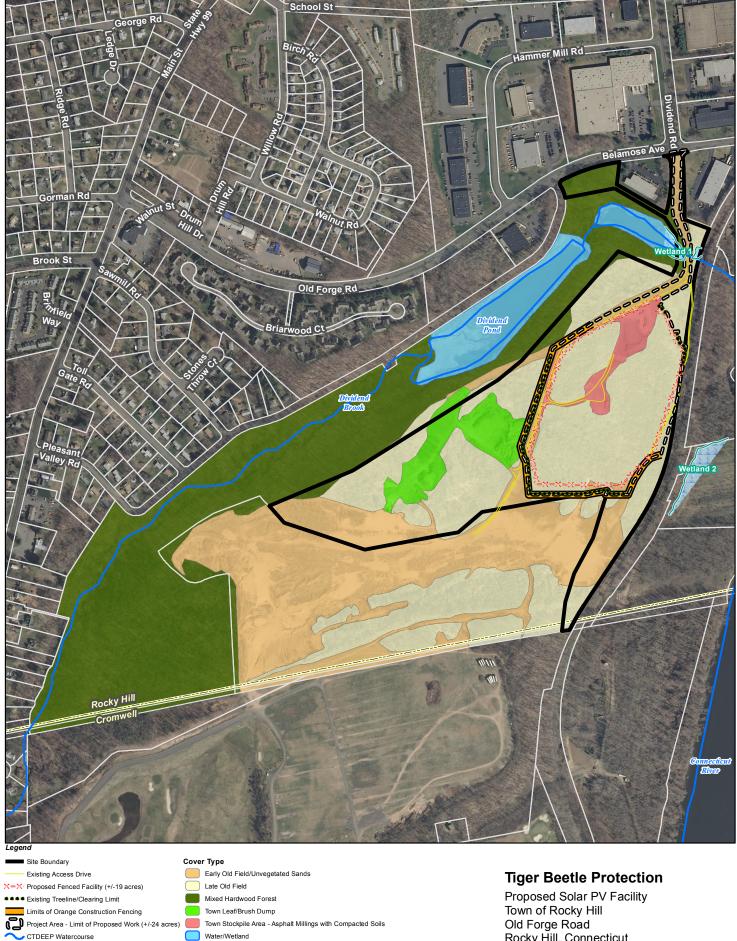
- Stop operations and shut off equipment.
- Remove any sources of spark or flame.
- Contain the source of the spill.
- Determine the approximate volume of the spill.
- Identify the location of natural flow paths to prevent the release of the spill to sensitive nearby waterways or wetlands.
- Ensure that fellow workers are notified of the spill.

#### Clean Up & Containment

- Obtain spill response materials from the on-site spill response kit.
- Place absorbent materials directly on the release area.
- Limit the spread of the spill by placing absorbent materials around the perimeter of the spill.
- Isolate and eliminate the spill source.
- Contact the Rocky Hill Aquifer Protection Agency (Planning and Zoning Commission), immediately at (860) 258-2761, along with other appropriate local, state and/or federal agencies, as necessary.
- Contact a disposal company to properly dispose of contaminated materials.

#### Reporting

- Complete an incident report.
- Submit a completed incident report to the Rocky Hill Aquifer Protection Agency, Connecticut Siting Council and other appropriate local, state and/or federal agencies, as necessary.



Municipal Boundary

Approximate Assessor Parcel Boundary (CTDEEP)

Delineated Wetland Boundary

Wetland Area

Old Forge Road Rocky Hill, Connecticut



### **APPENDIX I**

## **Noise Evaluation Report**



Noise Evaluation Study

Proposed Solar Farm Facility Solar City Corporation Old Forge Road Rocky Hill, CT 06067

January 28, 2016

Prepared For:
All-Points Technology Corporation
3 Saddlebrook Drive
Killingworth, CT 06419

Prepared By: Allan Smardin HMB Acoustics LLC 3 Cherry Tree Lane Avon, CT 06001

#### Introduction

I have reviewed site plans and specifications for equipment that is being proposed for the Solar Farm. The Solar Farm is to be located on Old Forge Road, Rocky Hill, CT. The site location is mixed Residential and Commercial. On July 11, 2015 existing background noise measurements were taken near the proposed site and in adjacent areas. The average levels were 25-30 dBA.

The purpose of this noise evaluation is to determine whether the proposed equipment will comply with the State of CT Noise Regulations. This report and the noise regulations utilize a dBA scale. This scale is used because it closely approximates the response characteristic of the human ear to loudness, and is the scale most commonly used in the measurement of community noise.

#### **Noise Regulations**

The State of CT has enacted regulations which limit the amount of noise which may be transferred from one property to another. In pertinent part, the Regulations provide as follows:

Daytime hours - The hours between 7 a.m. and 10 p.m. local time.

Nighttime hours - The hours between 10 p.m. and 7 a.m. local time.

The allowable noise level from a Class "B" Commercial Noise Zone Emitter to a Class "A" Residential Zone Receptor's property line is 55 dBA (daytime) and 45 dBA (nighttime).

(Sec. 22a-69-1.1 (h&n)).

The allowable noise level from a Class "B" Commercial Zone Emitter to a Class "B" Commercial Zone Receptor is 62 dBA (day / night).

(Sec. 22a-69-3.5 (b)).

#### **Noise Evaluation**

The noise levels listed in TABLE 1 take into account the effect of acoustical shielding provided by other structures on the property. The noise levels have been projected to the nearest property lines in the directions listed.

TABLE 1

| <u>Direction</u> | dBA Level |                                    |
|------------------|-----------|------------------------------------|
| North            | 25        | Residential (Belamose Avenue)      |
|                  | 30        | Commercial (Belamose Avenue)       |
| South            | 29        | Rocky Hill / Cromwell Town Line    |
| East             | 26        | Wetlands & The CT River            |
| West             | 21        | Residential (Pleasant Valley Road) |

#### **Noise Evaluation Results**

The noise level data in TABLE 1 demonstrates that the noise levels meet the conditions for compliance as set forth in the State of CT Noise Regulations at Residential and Commercial property line noise zones.