

EXHIBIT C



Centered on Solutions<sup>SM</sup>

## Structural Analysis Report

85-ft Ballast Monopole

Proposed Temporary Antenna Installation

AT&T Site Ref: CT5990

T-Mobile Site Ref: CTNL010A

Ancient Highway  
East Lyme, CT

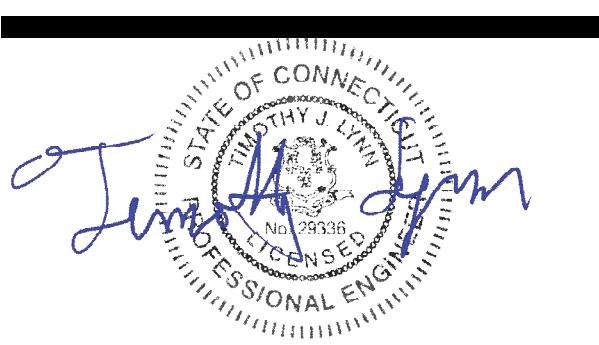
Centek Project No. 15021.000

Date: March 13, 2015

**Prepared for:**

AT&T Mobility  
500 Enterprise Drive,  
Suite 3A  
Rocky Hill, CT 06067

T-Mobile USA  
35 Griffin Road  
Bloomfield, CT 06002



**CENTEK** Engineering, Inc.

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East Lyme, CT

March 13, 2015

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## Introduction

The purpose of this report is to summarize the results of the non-linear, P- $\Delta$  structural analysis of the temporary antenna installation proposed by AT&T Mobility and T-Mobile on the ballast monopole (tower) located in East Lyme, CT.

The host tower is a 85-ft tall, three-section, ballasted monopole. Original design information was unavailable for use in this report. The tower geometry was obtained from a previous structural analysis prepared by Centek job no 14071.000 dated April 29, 2014.

Antenna and appurtenance information were obtained from AT&T and T-Mobile RF data sheets.

The tower consists of three (3) vertical steel pipe sections conforming to ASTM A53 Grade B (35ksi). The diameter of the pole (flat-flat) is 6.00-in at the top and 24.00-in at the base.

AT&T proposes the installation of three (3) panel antennas and three (3) TMA's on the temporary ballast monopole. Refer to the Antenna and Appurtenance Summary below for a detailed description of the proposed antenna and appurtenance configuration.

T-Mobile proposes the installation of three (3) panel antennas and six (6) TMA's on the temporary ballast monopole. Refer to the Antenna and Appurtenance Summary below for a detailed description of the proposed antenna and appurtenance configuration.

## Antenna and Appurtenance Summary

The existing, proposed and future loads considered in this analysis consist of the following:

- **AT&T (Proposed):**

**Antennas:** Three (3) KMW AM-X-CD-16-65-00T panel antennas and three (3) CCI DTMABP7819VG12A TMA's flush mounted with a RAD center elevation of 82-ft above grade level.

**Coax Cables:** Six (6) 7/8"  $\varnothing$  coax cables running on the inside of the monopole.

- **T-MOBILE (Proposed):**

**Antennas:** Three (3) RFS APX16DWV-16DWVS panel antennas and six (6) RFS ATMAA1412D-1A20 TMA's flush mounted with a RAD center elevation of 72-ft above grade level.

**Coax Cables:** Twelve (12) 7/8"  $\varnothing$  coax cables running on the inside of the monopole.

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Structural Analysis - 85-ft Ballast Monopole

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### Primary Assumptions Used in the Analysis

- The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- The tower carries the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- Tower is properly installed and maintained.
- Tower is in plumb condition.
- Tower loading for antennas and mounts as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original tower design documents.
- All members are “hot dipped” galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.
- All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.
- **All coax cables routed as specified in Section 3 of this report.**

## Analysis

The existing tower was analyzed using a comprehensive computer program entitled tnxTower. The program analyzes the tower, considering the worst case loading condition. The tower is considered as loaded by concentric forces along the tower shaft, and the model assumes that the shaft members are subjected to bending, axial, and shear forces.

The existing tower was analyzed for the controlling basic wind speed (fastest mile) with no ice and a 75% reduction of wind force with ½ inch accumulative ice to determine stresses in members as per guidelines of TIA/EIA-222-F-96 entitled “Structural Standards for Steel Antenna Towers and Antenna Supporting Structures”, the American Institute of Steel Construction (AISC) and the Manual of Steel Construction; Allowable Stress Design (ASD).

The controlling wind speed is determined by evaluating the local available wind speed data as provided in Appendix K of the CSBC<sup>1</sup> and the wind speed data available in the TIA/EIA-222-F-96 Standard. The higher of the two wind speeds is utilized in preparation on the tower analysis.

## Tower Loading

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA/EIA-222-F, gravity loads of the tower structure and its components, and the application of ½" radial ice on the tower structure and its components.

Basic Wind Speed:	New London; $v = 85$ mph (fastest mile) East Lyme; $v = 115$ mph (3 second gust) equivalent to $v = 95$ mph (fastest mile)	[Section 16 of TIA/EIA-222-F-96] [Appendix K of the 2005 CT Building Code Supplement]
Load Cases:	<u>Load Case 1</u> ; 95 mph wind speed w/ no ice plus gravity load – used in calculation of tower stresses and rotation.  <u>Load Case 2</u> ; 82 mph wind speed w/ ½" radial ice plus gravity load – used in calculation of tower stresses. The 82 mph wind speed velocity represents 75% of the wind pressure generated by the 95 mph wind speed.	[Section 2.3.16 of TIA/EIA-222-F-96] [Section 2.3.16 of TIA/EIA-222-F-96]
	<u>Load Case 3</u> ; Seismic – not checked	[Section 1614.5 of State Bldg. Code 2005] does not control in the design of this structure type

<sup>1</sup> The 2005 Connecticut State Building Code as amended by the 2009 CT State Supplement. (CSBC)

## Tower Capacity

Tower stresses were calculated utilizing the structural analysis software tnxtower. Allowable stresses were determined based on Table 5 of the TIA/EIA code with a 1/3 increase per Section 3.1.1.1 of the same code.

- Calculated stresses were found to be within allowable limits. In Load Case 1, per tnxtower “Section Capacity Table”, this tower was found to be at **87.3%** of its total capacity.

Tower Section	Elevation (AGL)	Stress Ratio (percentage of capacity)	Result
Pole Shaft (L1)	66.5'-86.5'	87.3%	<b>PASS</b>
Pole Shaft (L2)	36.5'-66.5'	32.0%	<b>PASS</b>
Pole Shaft (L3)	1.5'-36.5'	74.8%	<b>PASS</b>

## Anchors and Ballast

The base of the tower is connected to the ballast frame by means of (20) 1.00"Ø, ASTM A325 anchor bolts on a 27" Ø bolt circle.

- The tower reactions developed from the governing Load Case 1 were used in the verification of the foundation:

Reactions	Vector	Proposed Base Reactions
Base	Shear	6 kips
	Compression	8 kips
	Moment	306 kip-ft

- The anchor bolts were found to be within allowable limits.

Tower Component	Component	Stress Ratio (percentage of capacity)	Result
Anchor Bolts	Combined Compression and Shear	82.3%	<b>PASS</b>
Base Plate	Bending	71.4%	<b>PASS</b>

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- The ballast frame was found to be within allowable limits.

Foundation	Design Limit	IBC 2003/2005 CT State Building Code Section 3108.4.2 (FS) <sup>(1)</sup>	Proposed Loading (FS) <sup>(1)</sup>	Result
Ballast frame w/ 83,500 lbs of conc. blocks	OTM <sup>(2)</sup>	2.0	2.25	<b>PASS</b>

Note 1: FS denotes Factor of Safety.

Note 2: OTM denotes Overturning Moment

### Conclusion

This analysis shows that the subject tower **is adequate** to support the proposed antenna configuration.

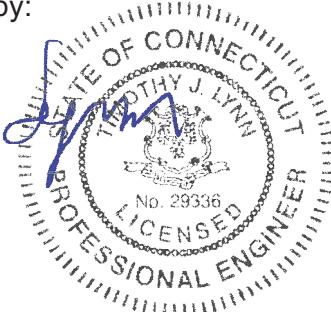
The analysis is based, in part, on the information provided to this office by AT&T and T-Mobile. If the existing conditions are different than the information in this report, Centek Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:



Timothy J. Lynn, PE  
Structural Engineer



**CENTEK** Engineering, Inc.

*Structural Analysis - 85-ft Ballast Monopole*

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*East Lyme, CT*

*March 13, 2015*

*Standard Conditions for Furnishing of  
Professional Engineering Services on  
Existing Structures*

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of CENTEK engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to CENTEK engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the “as new” condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. CENTEK engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

**CENTEK** Engineering, Inc.

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## General Description of Structural Analysis Program

tnxTower, is an integrated structural analysis and design software package for Designed specifically for the telecommunications industry, tnxTower, formerly ERITower, automates much of the tower analysis and design required by the TIA/EIA 222 Standard.

### tnxTower Features:

- tnxTower can analyze and design 3- and 4-sided guyed towers, 3- and 4-sided self-supporting towers and either round or tapered ground mounted poles with or without guys.
- The program analyzes towers using the TIA-222-G (2005) standard or any of the previous TIA/EIA standards back to RS-222 (1959). Steel design is checked using the AISC ASD 9th Edition or the AISC LRFD specifications.
- Linear and non-linear (P-delta) analyses can be used in determining displacements and forces in the structure. Wind pressures and forces are automatically calculated.
- Extensive graphics plots include material take-off, shear-moment, leg compression, displacement, twist, feed line, guy anchor and stress plots.
- tnxTower contains unique features such as True Cable behavior, hog rod take-up, foundation stiffness and much more.

Section	3	2	1
Size	P24x38	P24x38	P6x432
Length (ft)	35.00	30.00	20.00
Grade			A53-B-35
Weight (K)	6.7	3.3	2.8
			0.6

## DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
AM-X-CD-16-65-00T-RET(72") (ATT Proposed)	82	APX16DWV-16DWVS-E-A20 (T-Mobile Proposed)	72
AM-X-CD-16-65-00T-RET(72") (ATT Proposed)	82	Valmont Uni-Tri Bracket (T-Mobile Proposed)	72
AM-X-CD-16-65-00T-RET(72") (ATT Proposed)	82	ATMAA1412D-1A20 TMA (T-Mobile Proposed)	68
Valmont Uni-Tri Bracket (ATT Proposed)	82	ATMAA1412D-1A20 TMA (T-Mobile Proposed)	68
DTMABP7819VG12A TMA (ATT Proposed)	78	ATMAA1412D-1A20 TMA (T-Mobile Proposed)	68
DTMABP7819VG12A TMA (ATT Proposed)	78	ATMAA1412D-1A20 TMA (T-Mobile Proposed)	68
DTMABP7819VG12A TMA (ATT Proposed)	78	ATMAA1412D-1A20 TMA (T-Mobile Proposed)	68
APX16DWV-16DWVS-E-A20 (T-Mobile Proposed)	72	ATMAA1412D-1A20 TMA (T-Mobile Proposed)	68
APX16DWV-16DWVS-E-A20 (T-Mobile Proposed)	72		

## MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A53-B-35	35 ksi	63 ksi			

## TOWER DESIGN NOTES

1. Tower designed for a 95 mph basic wind in accordance with the TIA/EIA-222-F Standard.
2. Tower is also designed for a 82 mph basic wind with 0.50 in ice.
3. Deflections are based upon a 50 mph wind.
4. TOWER RATING: 87.3%



### REACTIONS - 95 mph WIND

**Centek Engineering Inc.**  
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Phone: (203) 488-0580  
FAX: (203) 488-8587

Job: **15021.000 - CT5990/CTNL010A**  
Project: **85-ft Temporary Monopole - East Lyme, CT**  
Client: **AT&T/T-Mobile** Drawn by: **TJL** App'd:  
Code: **TIA/EIA-222-F** Date: **03/13/15** Scale: **NT**  
Path: **J:\Jobs\15021.000\W04\Structural\Backup Documentation\CalcER582 Monopole - West Hartford CT.xls** Dwg No. **E**

<b>tnxTower</b>  <b>Centek Engineering Inc.</b> 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	<b>Job</b> 15021.000 - CT5990/CTNL010A	<b>Page</b> 1 of 17
	<b>Project</b> 85-ft Temporary Monopole - East Lyme, CT	<b>Date</b> 09:18:22 03/13/15
	<b>Client</b> AT&T/T-Mobile	<b>Designed by</b> TJL

## Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Basic wind speed of 95 mph.

Nominal ice thickness of 0.5000 in.

Ice density of 56 pcf.

A wind speed of 82 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.333.

Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs	Distribute Leg Loads As Uniform	Treat Feedline Bundles As Cylinder
Consider Moments - Horizontals	Assume Legs Pinned	Use ASCE 10 X-Brace Ly Rules
Consider Moments - Diagonals	✓ Assume Rigid Index Plate	Calculate Redundant Bracing Forces
Use Moment Magnification	Use Clear Spans For Wind Area	Ignore Redundant Members in FEA
✓ Use Code Stress Ratios	Use Clear Spans For KL/r	SR Leg Bolts Resist Compression
✓ Use Code Safety Factors - Guys	Retention Guys To Initial Tension	All Leg Panels Have Same Allowable
Escalate Ice	✓ Bypass Mast Stability Checks	Offset Girt At Foundation
Always Use Max Kz	Use Azimuth Dish Coefficients	Consider Feedline Torque
Use Special Wind Profile	✓ Project Wind Area of Appurt.	Include Angle Block Shear Check
Include Bolts In Member Capacity	Autocalc Torque Arm Areas	
Leg Bolts Are At Top Of Section	SR Members Have Cut Ends	
Secondary Horizontal Braces Leg	✓ Sort Capacity Reports By Component	
Use Diamond Inner Bracing (4 Sided)	Triangulate Diamond Inner Bracing	
Add IBC .6D+W Combination		

## Pole Section Geometry

Section	Elevation ft	Section Length ft	Pole Size	Pole Grade	Socket Length ft
L1	86.50-66.50	20.00	P6x.432	A53-B-35 (35 ksi)	
L2	66.50-36.50	30.00	P24x3/8	A53-B-35 (35 ksi)	
L3	36.50-1.50	35.00	P24x3/8	A53-B-35 (35 ksi)	

<b>tnxTower</b>  <b>Centek Engineering Inc.</b> 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	15021.000 - CT5990/CTNL010A	Page
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	Client	AT&T/T-Mobile	Designed by TJL

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_f$	Adjust. Factor $A_r$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals
ft	ft <sup>2</sup>	in					in	in
L1 86.50-66.50				1	1	1		
L2 66.50-36.50				1	1	1		
L3 36.50-1.50				1	1	1		

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	$C_A A_A$	Weight	
						ft <sup>2</sup> /ft	plf	
7/8 (AT&T Proposed)	C	No	Inside Pole	83.50 - 4.50	6	No Ice	0.00	0.54
						1/2" Ice	0.00	0.54
7/8 (T-Mobile Proposed)	C	No	Inside Pole	73.50 - 4.50	12	No Ice	0.00	0.54
						1/2" Ice	0.00	0.54

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation	Face	$A_R$	$A_F$	$C_A A_A$ In Face	$C_A A_A$ Out Face	Weight
	ft		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	
L1	86.50-66.50	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.10
L2	66.50-36.50	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.29
L3	36.50-1.50	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.31

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation	Face or Leg	Ice Thickness	$A_R$	$A_F$	$C_A A_A$ In Face	$C_A A_A$ Out Face	Weight
	ft		in	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	
L1	86.50-66.50	A	0.500	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.000	0.10
L2	66.50-36.50	A	0.500	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.000	0.29
L3	36.50-1.50	A	0.500	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.000	0.31

### Discrete Tower Loads

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	<b>Project</b>	85-ft Temporary Monopole - East Lyme, CT	<b>Date</b>
	<b>Client</b>	AT&T/T-Mobile	<b>Designed by</b> TJL

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	<i>C<sub>A</sub>A<sub>A</sub></i>	<i>C<sub>A</sub>A<sub>A</sub></i>	Weight K	
						Front	Side		
AM-X-CD-16-65-00T-RET(7 2") (AT&T Proposed)	A	From Face	0.50 0.00 0.00	0.0000	82.00	No Ice 1/2" Ice	8.26 8.81	4.64 5.09	0.05 0.10
AM-X-CD-16-65-00T-RET(7 2") (AT&T Proposed)	B	From Face	0.50 0.00 0.00	0.0000	82.00	No Ice 1/2" Ice	8.26 8.81	4.64 5.09	0.05 0.10
AM-X-CD-16-65-00T-RET(7 2") (AT&T Proposed)	C	From Face	0.50 0.00 0.00	0.0000	82.00	No Ice 1/2" Ice	8.26 8.81	4.64 5.09	0.05 0.10
DTMABP7819VG12A TMA (AT&T Proposed)	A	From Face	0.50 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice	1.59 1.76	0.58 0.70	0.02 0.03
DTMABP7819VG12A TMA (AT&T Proposed)	B	From Face	0.50 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice	1.59 1.76	0.58 0.70	0.02 0.03
DTMABP7819VG12A TMA (AT&T Proposed)	C	From Face	0.50 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice	1.59 1.76	0.58 0.70	0.02 0.03
Valmont Uni-Tri Bracket (AT&T Proposed)	C	None		0.0000	82.00	No Ice 1/2" Ice	1.75 1.94	1.75 1.94	0.29 0.31
APX16DWV-16DWVS-E-A 20 (T-Mobile Proposed)	A	From Face	0.50 0.00 0.00	0.0000	72.00	No Ice 1/2" Ice	7.07 7.52	2.15 2.49	0.04 0.07
APX16DWV-16DWVS-E-A 20 (T-Mobile Proposed)	B	From Face	0.50 0.00 0.00	0.0000	72.00	No Ice 1/2" Ice	7.07 7.52	2.15 2.49	0.04 0.07
APX16DWV-16DWVS-E-A 20 (T-Mobile Proposed)	C	From Face	0.50 0.00 0.00	0.0000	72.00	No Ice 1/2" Ice	7.07 7.52	2.15 2.49	0.04 0.07
ATMAA1412D-1A20 TMA (T-Mobile Proposed)	A	From Face	0.50 1.00 0.00	0.0000	68.00	No Ice 1/2" Ice	1.17 1.31	0.47 0.57	0.01 0.02
ATMAA1412D-1A20 TMA (T-Mobile Proposed)	B	From Face	0.50 1.00 0.00	0.0000	68.00	No Ice 1/2" Ice	1.17 1.31	0.47 0.57	0.01 0.02
ATMAA1412D-1A20 TMA (T-Mobile Proposed)	C	From Face	0.50 1.00 0.00	0.0000	68.00	No Ice 1/2" Ice	1.17 1.31	0.47 0.57	0.01 0.02
ATMAA1412D-1A20 TMA (T-Mobile Proposed)	A	From Face	0.50 -1.00 0.00	0.0000	68.00	No Ice 1/2" Ice	1.17 1.31	0.47 0.57	0.01 0.02
ATMAA1412D-1A20 TMA (T-Mobile Proposed)	B	From Face	0.50 -1.00 0.00	0.0000	68.00	No Ice 1/2" Ice	1.17 1.31	0.47 0.57	0.01 0.02
ATMAA1412D-1A20 TMA (T-Mobile Proposed)	C	From Face	0.50 -1.00 0.00	0.0000	68.00	No Ice 1/2" Ice	1.17 1.31	0.47 0.57	0.01 0.02
Valmont Uni-Tri Bracket (T-Mobile Proposed)	C	None		0.0000	72.00	No Ice 1/2" Ice	1.75 1.94	1.75 1.94	0.29 0.31

## Tower Pressures - No Ice

 $G_H = 1.690$ 

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub> c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
L1 86.50-66.50	76.50	1.272	29	11.042	A	0.000	11.042	11.042	100.00	0.000	0.000
					B	0.000	11.042				
					C	0.000	11.042				
L2 66.50-36.50	51.50	1.136	26	60.000	A	0.000	60.000	60.000	100.00	0.000	0.000
					B	0.000	60.000				
					C	0.000	60.000				
L3 36.50-1.50	19.00	1	23	70.000	A	0.000	70.000	70.000	100.00	0.000	0.000
					B	0.000	70.000				
					C	0.000	70.000				

## Tower Pressure - With Ice

 $G_H = 1.690$ 

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	t <sub>Z</sub>	A <sub>G</sub>	F <sub>a</sub> c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	in	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
L1 86.50-66.50	76.50	1.272	22	0.5000	12.708	A	0.000	12.708	12.708	100.00	0.000	0.000
						B	0.000	12.708				
						C	0.000	12.708				
L2 66.50-36.50	51.50	1.136	20	0.5000	62.500	A	0.000	62.500	62.500	100.00	0.000	0.000
						B	0.000	62.500				
						C	0.000	62.500				
L3 36.50-1.50	19.00	1	17	0.5000	72.917	A	0.000	72.917	72.917	100.00	0.000	0.000
						B	0.000	72.917				
						C	0.000	72.917				

## Tower Pressure - Service

 $G_H = 1.690$ 

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub> c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
L1 86.50-66.50	76.50	1.272	8	11.042	A	0.000	11.042	11.042	100.00	0.000	0.000
					B	0.000	11.042				
					C	0.000	11.042				
L2 66.50-36.50	51.50	1.136	7	60.000	A	0.000	60.000	60.000	100.00	0.000	0.000
					B	0.000	60.000				
					C	0.000	60.000				
L3 36.50-1.50	19.00	1	6	70.000	A	0.000	70.000	70.000	100.00	0.000	0.000
					B	0.000	70.000				
					C	0.000	70.000				

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**Tower Forces - No Ice - Wind Normal To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	plf	
L1 86.50-66.50	0.10	0.57	A	1	0.646	1	1	1	11.042	0.35	17.72	C
			B	1	0.646	1	1	1	11.042			
			C	1	0.646	1	1	1	11.042			
L2 66.50-36.50	0.29	2.84	A	1	0.59	1	1	1	60.000	1.57	52.32	C
			B	1	0.59	1	1	1	60.000			
			C	1	0.59	1	1	1	60.000			
L3 36.50-1.50	0.31	3.31	A	1	0.59	1	1	1	70.000	1.61	46.07	C
			B	1	0.59	1	1	1	70.000			
			C	1	0.59	1	1	1	70.000			
Sum Weight:	0.70	6.73						OTM	133.28 kip-ft	3.54		

**Tower Forces - No Ice - Wind 45 To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	plf	
L1 86.50-66.50	0.10	0.57	A	1	0.646	1	1	1	11.042	0.35	17.72	C
			B	1	0.646	1	1	1	11.042			
			C	1	0.646	1	1	1	11.042			
L2 66.50-36.50	0.29	2.84	A	1	0.59	1	1	1	60.000	1.57	52.32	C
			B	1	0.59	1	1	1	60.000			
			C	1	0.59	1	1	1	60.000			
L3 36.50-1.50	0.31	3.31	A	1	0.59	1	1	1	70.000	1.61	46.07	C
			B	1	0.59	1	1	1	70.000			
			C	1	0.59	1	1	1	70.000			
Sum Weight:	0.70	6.73						OTM	133.28 kip-ft	3.54		

**Tower Forces - No Ice - Wind 60 To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	plf	
L1 86.50-66.50	0.10	0.57	A	1	0.646	1	1	1	11.042	0.35	17.72	C
			B	1	0.646	1	1	1	11.042			
			C	1	0.646	1	1	1	11.042			
L2 66.50-36.50	0.29	2.84	A	1	0.59	1	1	1	60.000	1.57	52.32	C
			B	1	0.59	1	1	1	60.000			
			C	1	0.59	1	1	1	60.000			
L3 36.50-1.50	0.31	3.31	A	1	0.59	1	1	1	70.000	1.61	46.07	C
			B	1	0.59	1	1	1	70.000			
			C	1	0.59	1	1	1	70.000			
Sum Weight:	0.70	6.73						OTM	133.28 kip-ft	3.54		

<b>tnxTower</b>  <b>Centek Engineering Inc.</b> 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 15021.000 - CT5990/CTNL010A										Page 6 of 17
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### Tower Forces - No Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
L1 86.50-66.50	0.10	0.57	A	1	0.646	1	1	1	11.042	0.35	17.72	C
			B	1	0.646	1	1	1	11.042			
			C	1	0.646	1	1	1	11.042			
L2 66.50-36.50	0.29	2.84	A	1	0.59	1	1	1	60.000	1.57	52.32	C
			B	1	0.59	1	1	1	60.000			
			C	1	0.59	1	1	1	60.000			
L3 36.50-1.50	0.31	3.31	A	1	0.59	1	1	1	70.000	1.61	46.07	C
			B	1	0.59	1	1	1	70.000			
			C	1	0.59	1	1	1	70.000			
Sum Weight:	0.70	6.73						OTM	133.28 kip-ft	3.54		

### Tower Forces - With Ice - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
L1 86.50-66.50	0.10	0.66	A	1	0.779	1	1	1	12.708	0.37	18.44	C
			B	1	0.779	1	1	1	12.708			
			C	1	0.779	1	1	1	12.708			
L2 66.50-36.50	0.29	3.29	A	1	0.59	1	1	1	62.500	1.23	40.88	C
			B	1	0.59	1	1	1	62.500			
			C	1	0.59	1	1	1	62.500			
L3 36.50-1.50	0.31	3.84	A	1	0.59	1	1	1	72.917	1.26	36.00	C
			B	1	0.59	1	1	1	72.917			
			C	1	0.59	1	1	1	72.917			
Sum Weight:	0.70	7.79						OTM	111.02 kip-ft	2.85		

### Tower Forces - With Ice - Wind 45 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
L1 86.50-66.50	0.10	0.66	A	1	0.779	1	1	1	12.708	0.37	18.44	C
			B	1	0.779	1	1	1	12.708			
			C	1	0.779	1	1	1	12.708			
L2 66.50-36.50	0.29	3.29	A	1	0.59	1	1	1	62.500	1.23	40.88	C
			B	1	0.59	1	1	1	62.500			
			C	1	0.59	1	1	1	62.500			
L3 36.50-1.50	0.31	3.84	A	1	0.59	1	1	1	72.917	1.26	36.00	C
			B	1	0.59	1	1	1	72.917			
			C	1	0.59	1	1	1	72.917			

<b>tnxTower</b>  <b>Centek Engineering Inc.</b> 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 15021.000 - CT5990/CTNL010A										Page 7 of 17
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Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
Sum Weight:	0.70	7.79						OTM	111.02 kip-ft	2.85		

### Tower Forces - With Ice - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
L1 86.50-66.50	0.10	0.66	A B C	1 1 1	0.779 0.779 0.779	1 1 1	1 1 1	1 1 1	12.708 12.708 12.708	0.37	18.44	C
L2 66.50-36.50	0.29	3.29	A B C	1 1 1	0.59 0.59 0.59	1 1 1	1 1 1	1 1 1	62.500 62.500 62.500	1.23	40.88	C
L3 36.50-1.50	0.31	3.84	A B C	1 1 1	0.59 0.59 0.59	1 1 1	1 1 1	1 1 1	72.917 72.917 72.917	1.26	36.00	C
Sum Weight:	0.70	7.79						OTM	111.02 kip-ft	2.85		

### Tower Forces - With Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
L1 86.50-66.50	0.10	0.66	A B C	1 1 1	0.779 0.779 0.779	1 1 1	1 1 1	1 1 1	12.708 12.708 12.708	0.37	18.44	C
L2 66.50-36.50	0.29	3.29	A B C	1 1 1	0.59 0.59 0.59	1 1 1	1 1 1	1 1 1	62.500 62.500 62.500	1.23	40.88	C
L3 36.50-1.50	0.31	3.84	A B C	1 1 1	0.59 0.59 0.59	1 1 1	1 1 1	1 1 1	72.917 72.917 72.917	1.26	36.00	C
Sum Weight:	0.70	7.79						OTM	111.02 kip-ft	2.85		

### Tower Forces - Service - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
L1 86.50-66.50	0.10	0.57	A B	1 1	1.2 1.2	1 1	1 1	1 1	11.042 11.042	0.18	9.11	C

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Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	plf	
L2 66.50-36.50	0.29	2.84	C	1	1.2	1	1	1	11.042	0.43	14.49	C
			A	1	0.59	1	1	1	60.000			
			B	1	0.59	1	1	1	60.000			
L3 36.50-1.50	0.31	3.31	C	1	0.59	1	1	1	60.000	0.45	12.76	C
			A	1	0.59	1	1	1	70.000			
			B	1	0.59	1	1	1	70.000			
Sum Weight:	0.70	6.73	C	1	0.59	1	1	1	70.000	43.22		
								OTM	kip-ft	1.06		

**Tower Forces - Service - Wind 45 To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	plf	
L1 86.50-66.50	0.10	0.57	A	1	1.2	1	1	1	11.042	0.18	9.11	C
			B	1	1.2	1	1	1	11.042			
			C	1	1.2	1	1	1	11.042			
L2 66.50-36.50	0.29	2.84	A	1	0.59	1	1	1	60.000	0.43	14.49	C
			B	1	0.59	1	1	1	60.000			
			C	1	0.59	1	1	1	60.000			
L3 36.50-1.50	0.31	3.31	A	1	0.59	1	1	1	70.000	0.45	12.76	C
			B	1	0.59	1	1	1	70.000			
			C	1	0.59	1	1	1	70.000			
Sum Weight:	0.70	6.73						OTM	kip-ft	1.06		

**Tower Forces - Service - Wind 60 To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	plf	
L1 86.50-66.50	0.10	0.57	A	1	1.2	1	1	1	11.042	0.18	9.11	C
			B	1	1.2	1	1	1	11.042			
			C	1	1.2	1	1	1	11.042			
L2 66.50-36.50	0.29	2.84	A	1	0.59	1	1	1	60.000	0.43	14.49	C
			B	1	0.59	1	1	1	60.000			
			C	1	0.59	1	1	1	60.000			
L3 36.50-1.50	0.31	3.31	A	1	0.59	1	1	1	70.000	0.45	12.76	C
			B	1	0.59	1	1	1	70.000			
			C	1	0.59	1	1	1	70.000			
Sum Weight:	0.70	6.73						OTM	kip-ft	1.06		

**Tower Forces - Service - Wind 90 To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	plf	
L1 86.50-66.50	0.10	0.57	A	1	1.2	1	1	1	11.042	0.18	9.11	C
			B	1	1.2	1	1	1	11.042			
			C	1	1.2	1	1	1	11.042			
L2 66.50-36.50	0.29	2.84	A	1	0.59	1	1	1	60.000	0.43	14.49	C
			B	1	0.59	1	1	1	60.000			
			C	1	0.59	1	1	1	60.000			
L3 36.50-1.50	0.31	3.31	A	1	0.59	1	1	1	70.000	0.45	12.76	C
			B	1	0.59	1	1	1	70.000			
			C	1	0.59	1	1	1	70.000			
Sum Weight:	0.70	6.73						OTM	43.22 kip-ft	1.06		

## Force Totals

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, M <sub>x</sub> kip-ft	Sum of Overturning Moments, M <sub>z</sub> kip-ft	Sum of Torques kip-ft
Leg Weight	6.73					
Bracing Weight	0.00					
Total Member Self-Weight	6.73			0.00	0.00	
Total Weight	8.40			0.00	0.00	
Wind 0 deg - No Ice		0.00	-5.76	-300.93	0.00	0.00
Wind 30 deg - No Ice		2.88	-4.99	-260.61	-150.46	0.00
Wind 45 deg - No Ice		4.07	-4.07	-212.79	-212.79	0.00
Wind 60 deg - No Ice		4.99	-2.88	-150.46	-260.61	0.00
Wind 90 deg - No Ice		5.76	0.00	0.00	-300.93	0.00
Wind 120 deg - No Ice		4.99	2.88	150.46	-260.61	0.00
Wind 135 deg - No Ice		4.07	4.07	212.79	-212.79	0.00
Wind 150 deg - No Ice		2.88	4.99	260.61	-150.46	0.00
Wind 180 deg - No Ice		0.00	5.76	300.93	0.00	0.00
Wind 210 deg - No Ice		-2.88	4.99	260.61	150.46	0.00
Wind 225 deg - No Ice		-4.07	4.07	212.79	212.79	0.00
Wind 240 deg - No Ice		-4.99	2.88	150.46	260.61	0.00
Wind 270 deg - No Ice		-5.76	0.00	0.00	300.93	0.00
Wind 300 deg - No Ice		-4.99	-2.88	-150.46	260.61	0.00
Wind 315 deg - No Ice		-4.07	-4.07	-212.79	212.79	0.00
Wind 330 deg - No Ice		-2.88	-4.99	-260.61	150.46	0.00
Member Ice	1.06					
Total Weight Ice	9.83			0.00	0.00	
Wind 0 deg - Ice		0.00	-4.68	-248.54	0.00	0.00
Wind 30 deg - Ice		2.34	-4.06	-215.24	-124.27	0.00
Wind 45 deg - Ice		3.31	-3.31	-175.75	-175.75	0.00
Wind 60 deg - Ice		4.06	-2.34	-124.27	-215.24	0.00
Wind 90 deg - Ice		4.68	0.00	0.00	-248.54	0.00
Wind 120 deg - Ice		4.06	2.34	124.27	-215.24	0.00
Wind 135 deg - Ice		3.31	3.31	175.75	-175.75	0.00
Wind 150 deg - Ice		2.34	4.06	215.24	-124.27	0.00
Wind 180 deg - Ice		0.00	4.68	248.54	0.00	0.00
Wind 210 deg - Ice		-2.34	4.06	215.24	124.27	0.00
Wind 225 deg - Ice		-3.31	3.31	175.75	175.75	0.00
Wind 240 deg - Ice		-4.06	2.34	124.27	215.24	0.00
Wind 270 deg - Ice		-4.68	0.00	0.00	248.54	0.00
Wind 300 deg - Ice		-4.06	-2.34	-124.27	215.24	0.00
Wind 315 deg - Ice		-3.31	-3.31	-175.75	175.75	0.00
Wind 330 deg - Ice		-2.34	-4.06	-215.24	124.27	0.00

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Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, $M_x$ kip-ft	Sum of Overturning Moments, $M_z$ kip-ft	Sum of Torques kip-ft
Total Weight	8.40			0.00	0.00	
Wind 0 deg - Service		0.00	-1.68	-89.66	0.00	0.00
Wind 30 deg - Service		0.84	-1.46	-77.65	-44.83	0.00
Wind 45 deg - Service		1.19	-1.19	-63.40	-63.40	0.00
Wind 60 deg - Service		1.46	-0.84	-44.83	-77.65	0.00
Wind 90 deg - Service		1.68	0.00	0.00	-89.66	0.00
Wind 120 deg - Service		1.46	0.84	44.83	-77.65	0.00
Wind 135 deg - Service		1.19	1.19	63.40	-63.40	0.00
Wind 150 deg - Service		0.84	1.46	77.65	-44.83	0.00
Wind 180 deg - Service		0.00	1.68	89.66	0.00	0.00
Wind 210 deg - Service		-0.84	1.46	77.65	44.83	0.00
Wind 225 deg - Service		-1.19	1.19	63.40	63.40	0.00
Wind 240 deg - Service		-1.46	0.84	44.83	77.65	0.00
Wind 270 deg - Service		-1.68	0.00	0.00	89.66	0.00
Wind 300 deg - Service		-1.46	-0.84	-44.83	77.65	0.00
Wind 315 deg - Service		-1.19	-1.19	-63.40	63.40	0.00
Wind 330 deg - Service		-0.84	-1.46	-77.65	44.83	0.00

## Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 45 deg - No Ice
5	Dead+Wind 60 deg - No Ice
6	Dead+Wind 90 deg - No Ice
7	Dead+Wind 120 deg - No Ice
8	Dead+Wind 135 deg - No Ice
9	Dead+Wind 150 deg - No Ice
10	Dead+Wind 180 deg - No Ice
11	Dead+Wind 210 deg - No Ice
12	Dead+Wind 225 deg - No Ice
13	Dead+Wind 240 deg - No Ice
14	Dead+Wind 270 deg - No Ice
15	Dead+Wind 300 deg - No Ice
16	Dead+Wind 315 deg - No Ice
17	Dead+Wind 330 deg - No Ice
18	Dead+Ice+Temp
19	Dead+Wind 0 deg+Ice+Temp
20	Dead+Wind 30 deg+Ice+Temp
21	Dead+Wind 45 deg+Ice+Temp
22	Dead+Wind 60 deg+Ice+Temp
23	Dead+Wind 90 deg+Ice+Temp
24	Dead+Wind 120 deg+Ice+Temp
25	Dead+Wind 135 deg+Ice+Temp
26	Dead+Wind 150 deg+Ice+Temp
27	Dead+Wind 180 deg+Ice+Temp
28	Dead+Wind 210 deg+Ice+Temp
29	Dead+Wind 225 deg+Ice+Temp
30	Dead+Wind 240 deg+Ice+Temp
31	Dead+Wind 270 deg+Ice+Temp
32	Dead+Wind 300 deg+Ice+Temp
33	Dead+Wind 315 deg+Ice+Temp
34	Dead+Wind 330 deg+Ice+Temp

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<i>Comb. No.</i>	<i>Description</i>
35	Dead+Wind 0 deg - Service
36	Dead+Wind 30 deg - Service
37	Dead+Wind 45 deg - Service
38	Dead+Wind 60 deg - Service
39	Dead+Wind 90 deg - Service
40	Dead+Wind 120 deg - Service
41	Dead+Wind 135 deg - Service
42	Dead+Wind 150 deg - Service
43	Dead+Wind 180 deg - Service
44	Dead+Wind 210 deg - Service
45	Dead+Wind 225 deg - Service
46	Dead+Wind 240 deg - Service
47	Dead+Wind 270 deg - Service
48	Dead+Wind 300 deg - Service
49	Dead+Wind 315 deg - Service
50	Dead+Wind 330 deg - Service

### Maximum Member Forces

<i>Section No.</i>	<i>Elevation ft</i>	<i>Component Type</i>	<i>Condition</i>	<i>Gov. Load Comb.</i>	<i>Force</i>	<i>Major Axis Moment kip-ft</i>	<i>Minor Axis Moment kip-ft</i>
L1	86.5 - 66.5	Pole	Max Tension	23	0.00	0.00	0.00
			Max. Compression	18	-2.10	0.00	0.00
			Max. Mx	6	-1.57	-27.12	0.00
			Max. My	2	-1.57	0.00	27.12
			Max. Vy	6	2.62	-27.12	0.00
			Max. Vx	2	-2.62	0.00	27.12
			Max. Torque	7			-0.00
L2	66.5 - 36.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	18	-5.68	0.00	0.00
			Max. Mx	6	-4.69	-130.18	0.00
			Max. My	2	-4.69	0.00	130.18
			Max. Vy	6	4.24	-130.18	0.00
			Max. Vx	2	-4.24	0.00	130.18
			Max. Torque	5			0.00
L3	36.5 - 1.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	18	-9.83	0.00	0.00
			Max. Mx	6	-8.40	-305.94	0.00
			Max. My	2	-8.40	0.00	305.94
			Max. Vy	6	5.77	-305.94	0.00
			Max. Vx	2	-5.77	0.00	305.94
			Max. Torque	15			-0.00

### Maximum Reactions

<i>Location</i>	<i>Condition</i>	<i>Gov. Load Comb.</i>	<i>Vertical K</i>	<i>Horizontal, X K</i>	<i>Horizontal, Z K</i>
Pole	Max. Vert	19	9.83	0.00	4.68
	Max. H <sub>x</sub>	14	8.40	5.76	0.00
	Max. H <sub>z</sub>	2	8.40	0.00	5.76
	Max. M <sub>x</sub>	2	305.94	0.00	5.76
	Max. M <sub>z</sub>	6	305.94	-5.76	0.00
	Max. Torsion	5	0.00	-4.99	2.88

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Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
	Min. Vert	1	8.40	0.00	0.00
	Min. H <sub>x</sub>	6	8.40	-5.76	0.00
	Min. H <sub>z</sub>	10	8.40	0.00	-5.76
	Min. M <sub>x</sub>	10	-305.94	0.00	-5.76
	Min. M <sub>z</sub>	14	-305.94	5.76	0.00
	Min. Torsion	15	-0.00	4.99	2.88

### Tower Mast Reaction Summary

Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overswing Moment, M <sub>x</sub>	Overswing Moment, M <sub>z</sub>	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	8.40	0.00	0.00	0.00	0.00	0.00
Dead+Wind 0 deg - No Ice	8.40	0.00	-5.76	-305.94	0.00	0.00
Dead+Wind 30 deg - No Ice	8.40	2.88	-4.99	-264.95	-152.97	0.00
Dead+Wind 45 deg - No Ice	8.40	4.07	-4.07	-216.33	-216.33	0.00
Dead+Wind 60 deg - No Ice	8.40	4.99	-2.88	-152.97	-264.95	-0.00
Dead+Wind 90 deg - No Ice	8.40	5.76	0.00	0.00	-305.94	0.00
Dead+Wind 120 deg - No Ice	8.40	4.99	2.88	152.97	-264.95	0.00
Dead+Wind 135 deg - No Ice	8.40	4.07	4.07	216.33	-216.33	0.00
Dead+Wind 150 deg - No Ice	8.40	2.88	4.99	264.95	-152.97	-0.00
Dead+Wind 180 deg - No Ice	8.40	0.00	5.76	305.94	0.00	0.00
Dead+Wind 210 deg - No Ice	8.40	-2.88	4.99	264.95	152.97	0.00
Dead+Wind 225 deg - No Ice	8.40	-4.07	4.07	216.33	216.33	0.00
Dead+Wind 240 deg - No Ice	8.40	-4.99	2.88	152.97	264.95	-0.00
Dead+Wind 270 deg - No Ice	8.40	-5.76	0.00	0.00	305.94	0.00
Dead+Wind 300 deg - No Ice	8.40	-4.99	-2.88	-152.97	264.95	0.00
Dead+Wind 315 deg - No Ice	8.40	-4.07	-4.07	-216.33	216.33	0.00
Dead+Wind 330 deg - No Ice	8.40	-2.88	-4.99	-264.95	152.97	-0.00
Dead+Ice+Temp	9.83	0.00	0.00	0.00	0.00	0.00
Dead+Wind 0 deg+Ice+Temp	9.83	0.00	-4.68	-253.60	0.00	0.00
Dead+Wind 30 deg+Ice+Temp	9.83	2.34	-4.06	-219.63	-126.80	0.00
Dead+Wind 45 deg+Ice+Temp	9.83	3.31	-3.31	-179.33	-179.33	0.00
Dead+Wind 60 deg+Ice+Temp	9.83	4.06	-2.34	-126.80	-219.63	-0.00
Dead+Wind 90 deg+Ice+Temp	9.83	4.68	0.00	0.00	-253.60	0.00
Dead+Wind 120 deg+Ice+Temp	9.83	4.06	2.34	126.80	-219.63	0.00
Dead+Wind 135 deg+Ice+Temp	9.83	3.31	3.31	179.33	-179.33	0.00
Dead+Wind 150 deg+Ice+Temp	9.83	2.34	4.06	219.63	-126.80	-0.00
Dead+Wind 180 deg+Ice+Temp	9.83	0.00	4.68	253.60	0.00	0.00
Dead+Wind 210 deg+Ice+Temp	9.83	-2.34	4.06	219.63	126.80	0.00
Dead+Wind 225 deg+Ice+Temp	9.83	-3.31	3.31	179.33	179.33	0.00
Dead+Wind 240 deg+Ice+Temp	9.83	-4.06	2.34	126.80	219.63	-0.00
Dead+Wind 270 deg+Ice+Temp	9.83	-4.68	0.00	0.00	253.60	0.00
Dead+Wind 300 deg+Ice+Temp	9.83	-4.06	-2.34	-126.80	219.63	0.00
Dead+Wind 315 deg+Ice+Temp	9.83	-3.31	-3.31	-179.33	179.33	0.00
Dead+Wind 330 deg+Ice+Temp	9.83	-2.34	-4.06	-219.63	126.80	-0.00
Dead+Wind 0 deg - Service	8.40	0.00	-1.68	-91.19	0.00	0.00
Dead+Wind 30 deg - Service	8.40	0.84	-1.46	-78.97	-45.59	0.00
Dead+Wind 45 deg - Service	8.40	1.19	-1.19	-64.48	-64.48	0.00
Dead+Wind 60 deg - Service	8.40	1.46	-0.84	-45.59	-78.97	0.00
Dead+Wind 90 deg - Service	8.40	1.68	0.00	0.00	-91.19	0.00
Dead+Wind 120 deg - Service	8.40	1.46	0.84	45.59	-78.97	0.00
Dead+Wind 135 deg - Service	8.40	1.19	1.19	64.48	-64.48	0.00
Dead+Wind 150 deg - Service	8.40	0.84	1.46	78.97	-45.59	0.00
Dead+Wind 180 deg - Service	8.40	0.00	1.68	91.19	0.00	0.00
Dead+Wind 210 deg - Service	8.40	-0.84	1.46	78.97	45.59	0.00
Dead+Wind 225 deg - Service	8.40	-1.19	1.19	64.48	64.48	0.00

Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overturning Moment, M <sub>x</sub>	Overturning Moment, M <sub>z</sub>	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 240 deg - Service	8.40	-1.46	0.84	45.59	78.97	0.00
Dead+Wind 270 deg - Service	8.40	-1.68	0.00	0.00	91.19	0.00
Dead+Wind 300 deg - Service	8.40	-1.46	-0.84	-45.59	78.97	0.00
Dead+Wind 315 deg - Service	8.40	-1.19	-1.19	-64.48	64.48	0.00
Dead+Wind 330 deg - Service	8.40	-0.84	-1.46	-78.97	45.59	0.00

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-8.40	0.00	0.00	8.40	0.00	0.000%
2	0.00	-8.40	-5.76	0.00	8.40	5.76	0.000%
3	2.88	-8.40	-4.99	-2.88	8.40	4.99	0.000%
4	4.07	-8.40	-4.07	-4.07	8.40	4.07	0.000%
5	4.99	-8.40	-2.88	-4.99	8.40	2.88	0.000%
6	5.76	-8.40	0.00	-5.76	8.40	0.00	0.000%
7	4.99	-8.40	2.88	-4.99	8.40	-2.88	0.000%
8	4.07	-8.40	4.07	-4.07	8.40	-4.07	0.000%
9	2.88	-8.40	4.99	-2.88	8.40	-4.99	0.000%
10	0.00	-8.40	5.76	0.00	8.40	-5.76	0.000%
11	-2.88	-8.40	4.99	2.88	8.40	-4.99	0.000%
12	-4.07	-8.40	4.07	4.07	8.40	-4.07	0.000%
13	-4.99	-8.40	2.88	4.99	8.40	-2.88	0.000%
14	-5.76	-8.40	0.00	5.76	8.40	0.00	0.000%
15	-4.99	-8.40	-2.88	4.99	8.40	2.88	0.000%
16	-4.07	-8.40	-4.07	4.07	8.40	4.07	0.000%
17	-2.88	-8.40	-4.99	2.88	8.40	4.99	0.000%
18	0.00	-9.83	0.00	0.00	9.83	0.00	0.000%
19	0.00	-9.83	-4.68	0.00	9.83	4.68	0.000%
20	2.34	-9.83	-4.06	-2.34	9.83	4.06	0.000%
21	3.31	-9.83	-3.31	-3.31	9.83	3.31	0.000%
22	4.06	-9.83	-2.34	-4.06	9.83	2.34	0.000%
23	4.68	-9.83	0.00	-4.68	9.83	0.00	0.000%
24	4.06	-9.83	2.34	-4.06	9.83	-2.34	0.000%
25	3.31	-9.83	3.31	-3.31	9.83	-3.31	0.000%
26	2.34	-9.83	4.06	-2.34	9.83	-4.06	0.000%
27	0.00	-9.83	4.68	0.00	9.83	-4.68	0.000%
28	-2.34	-9.83	4.06	2.34	9.83	-4.06	0.000%
29	-3.31	-9.83	3.31	3.31	9.83	-3.31	0.000%
30	-4.06	-9.83	2.34	4.06	9.83	-2.34	0.000%
31	-4.68	-9.83	0.00	4.68	9.83	0.00	0.000%
32	-4.06	-9.83	-2.34	4.06	9.83	2.34	0.000%
33	-3.31	-9.83	-3.31	3.31	9.83	3.31	0.000%
34	-2.34	-9.83	-4.06	2.34	9.83	4.06	0.000%
35	0.00	-8.40	-1.68	0.00	8.40	1.68	0.000%
36	0.84	-8.40	-1.46	-0.84	8.40	1.46	0.000%
37	1.19	-8.40	-1.19	-1.19	8.40	1.19	0.000%
38	1.46	-8.40	-0.84	-1.46	8.40	0.84	0.000%
39	1.68	-8.40	0.00	-1.68	8.40	0.00	0.000%
40	1.46	-8.40	0.84	-1.46	8.40	-0.84	0.000%
41	1.19	-8.40	1.19	-1.19	8.40	-1.19	0.000%
42	0.84	-8.40	1.46	-0.84	8.40	-1.46	0.000%
43	0.00	-8.40	1.68	0.00	8.40	-1.68	0.000%
44	-0.84	-8.40	1.46	0.84	8.40	-1.46	0.000%
45	-1.19	-8.40	1.19	1.19	8.40	-1.19	0.000%
46	-1.46	-8.40	0.84	1.46	8.40	-0.84	0.000%
47	-1.68	-8.40	0.00	1.68	8.40	0.00	0.000%

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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
48	-1.46	-8.40	-0.84	1.46	8.40	0.84	0.000%
49	-1.19	-8.40	-1.19	1.19	8.40	1.19	0.000%
50	-0.84	-8.40	-1.46	0.84	8.40	1.46	0.000%

## Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00000001
3	Yes	4	0.00000001	0.00043599
4	Yes	4	0.00000001	0.00050062
5	Yes	4	0.00000001	0.00043599
6	Yes	4	0.00000001	0.00000001
7	Yes	4	0.00000001	0.00043599
8	Yes	4	0.00000001	0.00050062
9	Yes	4	0.00000001	0.00043599
10	Yes	4	0.00000001	0.00000001
11	Yes	4	0.00000001	0.00043599
12	Yes	4	0.00000001	0.00050062
13	Yes	4	0.00000001	0.00043599
14	Yes	4	0.00000001	0.00000001
15	Yes	4	0.00000001	0.00043599
16	Yes	4	0.00000001	0.00050062
17	Yes	4	0.00000001	0.00043599
18	Yes	4	0.00000001	0.00000001
19	Yes	4	0.00000001	0.00071694
20	Yes	5	0.00000001	0.00002390
21	Yes	5	0.00000001	0.00002578
22	Yes	5	0.00000001	0.00002390
23	Yes	4	0.00000001	0.00071694
24	Yes	5	0.00000001	0.00002390
25	Yes	5	0.00000001	0.00002578
26	Yes	5	0.00000001	0.00002390
27	Yes	4	0.00000001	0.00071694
28	Yes	5	0.00000001	0.00002390
29	Yes	5	0.00000001	0.00002578
30	Yes	5	0.00000001	0.00002390
31	Yes	4	0.00000001	0.00071694
32	Yes	5	0.00000001	0.00002390
33	Yes	5	0.00000001	0.00002578
34	Yes	5	0.00000001	0.00002390
35	Yes	4	0.00000001	0.00000001
36	Yes	4	0.00000001	0.00000001
37	Yes	4	0.00000001	0.00000001
38	Yes	4	0.00000001	0.00000001
39	Yes	4	0.00000001	0.00000001
40	Yes	4	0.00000001	0.00000001
41	Yes	4	0.00000001	0.00000001
42	Yes	4	0.00000001	0.00000001
43	Yes	4	0.00000001	0.00000001
44	Yes	4	0.00000001	0.00000001
45	Yes	4	0.00000001	0.00000001
46	Yes	4	0.00000001	0.00000001
47	Yes	4	0.00000001	0.00000001
48	Yes	4	0.00000001	0.00000001

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49	Yes	4	0.00000001	0.00000001
50	Yes	4	0.00000001	0.00000001

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	86.5 - 66.5	6.848	35	0.8177	0.0000
L2	66.5 - 36.5	3.819	35	0.4290	0.0000
L3	36.5 - 1.5	1.367	35	0.3287	0.0000

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
82.00	AM-X-CD-16-65-00T-RET(72")	35	6.112	0.7142	0.0000	12434
78.00	DTMABP7819VG12A TMA	35	5.471	0.6263	0.0000	7314
72.00	APX16DWV-16DWVS-E-A20	35	4.563	0.5100	0.0000	4287
68.00	ATMAA1412D-1A20 TMA	35	4.012	0.4481	0.0000	3439

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	86.5 - 66.5	22.660	2	2.6800	0.0000
L2	66.5 - 36.5	12.711	2	1.4229	0.0000
L3	36.5 - 1.5	4.564	2	1.0951	0.0000

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
82.00	AM-X-CD-16-65-00T-RET(72")	2	20.244	2.3452	0.0000	3864
78.00	DTMABP7819VG12A TMA	2	18.142	2.0610	0.0000	2273
72.00	APX16DWV-16DWVS-E-A20	2	15.162	1.6849	0.0000	1332
68.00	ATMAA1412D-1A20 TMA	2	13.347	1.4847	0.0000	1068

### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual		Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
								P K	K		
L1	86.5 - 66.5 (1)	P6x.432	20.00	0.00	0.0	21.000	8.4049	-1.57	176.50	0.009	
L2	66.5 - 36.5 (2)	P24x3/8	30.00	0.00	0.0	21.000	27.8325	-4.69	584.48	0.008	
L3	36.5 - 1.5 (3)	P24x3/8	35.00	0.00	0.0	21.000	27.8325	-8.40	584.48	0.014	

### Pole Bending Design Data

Section No.	Elevation ft	Size	Actual M <sub>x</sub> kip-ft	Actual f <sub>bx</sub> ksi	Allow. F <sub>bx</sub> ksi	Ratio f <sub>bx</sub> F <sub>bx</sub>	Actual M <sub>y</sub> kip-ft	Actual f <sub>by</sub> ksi	Allow. F <sub>by</sub> ksi	Ratio f <sub>by</sub> F <sub>by</sub>
L1	86.5 - 66.5 (1)	P6x.432	27.12	26.620	23.100	1.152	0.00	0.000	23.100	0.000
L2	66.5 - 36.5 (2)	P24x3/8	130.18	9.651	23.100	0.418	0.00	0.000	23.100	0.000
L3	36.5 - 1.5 (3)	P24x3/8	305.94	22.682	23.100	0.982	0.00	0.000	23.100	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V K	Actual f <sub>v</sub> ksi	Allow. F <sub>v</sub> ksi	Ratio f <sub>v</sub> F <sub>v</sub>	Actual T kip-ft	Actual f <sub>t</sub> ksi	Allow. F <sub>vt</sub> ksi	Ratio f <sub>t</sub> F <sub>vt</sub>
L1	86.5 - 66.5 (1)	P6x.432	2.62	0.624	14.000	0.045	0.00	0.000	14.000	0.000
L2	66.5 - 36.5 (2)	P24x3/8	4.24	0.305	14.000	0.022	0.00	0.000	14.000	0.000
L3	36.5 - 1.5 (3)	P24x3/8	5.77	0.414	14.000	0.030	0.00	0.000	14.000	0.000

### Pole Interaction Design Data

Section No.	Elevation ft	Ratio P P <sub>a</sub>	Ratio f <sub>bx</sub> F <sub>bx</sub>	Ratio f <sub>by</sub> F <sub>by</sub>	Ratio f <sub>v</sub> F <sub>v</sub>	Ratio f <sub>vt</sub> F <sub>vt</sub>	Comb. Stress Ratio	Allow. Stress Ratio	Criteria	
									Ratio P P <sub>a</sub>	Ratio f <sub>bx</sub> F <sub>bx</sub>
L1	86.5 - 66.5 (1)	0.009	1.152	0.000	0.045	0.000	1.163	1.333	H1-3+VT	✓
L2	66.5 - 36.5 (2)	0.008	0.418	0.000	0.022	0.000	0.426	1.333	H1-3+VT	✓
L3	36.5 - 1.5 (3)	0.014	0.982	0.000	0.030	0.000	0.997	1.333	H1-3+VT	✓

### Section Capacity Table

<b>Job</b>	15021.000 - CT5990/CTNL010A	<b>Page</b>
<b>Project</b>	85-ft Temporary Monopole - East Lyme, CT	<b>Date</b> 09:18:22 03/13/15
<b>Client</b>	AT&T/T-Mobile	<b>Designed by</b> TJL

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
L1	86.5 - 66.5	Pole	P6x.432	1	-1.57	235.28	87.3	Pass
L2	66.5 - 36.5	Pole	P24x3/8	2	-4.69	779.12	32.0	Pass
L3	36.5 - 1.5	Pole	P24x3/8	3	-8.40	779.12	74.8	Pass
						Summary		
						Pole (L1)	87.3	Pass
						<b>RATING =</b>	<b>87.3</b>	<b>Pass</b>

**Anchor Bolt and Base Plate Analysis:**

**Input Data:**

Tower Reactions:

Oversetting Moment =	OM := 306 ft-kips	(Input From tnTower)
Shear Force =	Shear := 6-kips	(Input From tnTower)
Axial Force =	Axial := 8-kips	(Input From tnTower)

Anchor Bolt Data:

Use ASTM A325

Number of Anchor Bolts =	N := 20	(User Input)
Diameter of Bolt Circle =	D <sub>bc</sub> := 27.00-in	(User Input)
Bolt "Column" Distance =	I := 3.0-in	(User Input)
Bolt Ultimate Strength =	F <sub>u</sub> := 120-ksi	(User Input)
Bolt Yield Strength =	F <sub>y</sub> := 92-ksi	(User Input)
Bolt Modulus =	E := 29000-ksi	(User Input)
Diameter of Anchor Bolts =	D := 1.0-in	(User Input)
Threads per Inch =	n := 8	(User Input)

Base Plate Data:

Use ASTM A572-50

Plate Yield Strength =	F <sub>y</sub> <sub>bp</sub> := 50-ksi	(User Input)
Base Plate Thickness =	t <sub>bp</sub> := 1.00-in	(User Input)
Base Plate Diameter =	D <sub>bp</sub> := 30-in	(User Input)
Outer Pole Diameter =	D <sub>pole</sub> := 24-in	(User Input)

**Geometric Layout Data:**
Distance from Bolts to Centroid of Pole:

$$\text{Radius of Bolt Circle} =: R_{bc} := \frac{D_{bc}}{2} = 13.5\text{-in}$$

$$\text{Distance to Bolts} = i := 1..N$$

$$d_i := \begin{cases} \theta \leftarrow 2\pi \cdot \left( \frac{i}{N} \right) & d_1 = 4.17\text{-in} \\ d \leftarrow R_{bc} \cdot \sin(\theta) & d_2 = 7.94\text{-in} \\ & d_3 = 10.92\text{-in} \\ & d_4 = 12.84\text{-in} \\ & d_5 = 13.50\text{-in} \\ & d_6 = 12.84\text{-in} \end{cases} \begin{matrix} d_7 = 10.92\text{-in} \\ d_8 = 7.94\text{-in} \\ d_9 = 4.17\text{-in} \\ d_{10} = 0.00\text{-in} \\ d_{11} = -4.17\text{-in} \\ \text{etc.} \end{matrix}$$

Critical Distances For Bending in Plate:

$$\text{Outer Pole Radius} = R_{pole} := \frac{D_{pole}}{2} = 12\text{-in}$$

$$\text{Moment Arms of Bolts about Neutral Axis} =$$

$$MA_i := \text{if}(d_i \geq R_{pole}, d_i - R_{pole}, 0\text{in})$$

$$\begin{matrix} MA_1 = 0.00\text{-in} & MA_7 = 0.00\text{-in} \\ MA_2 = 0.00\text{-in} & MA_8 = 0.00\text{-in} \\ MA_3 = 0.00\text{-in} & MA_9 = 0.00\text{-in} \\ MA_4 = 0.84\text{-in} & MA_{10} = 0.00\text{-in} \\ MA_5 = 1.50\text{-in} & MA_{11} = 0.00\text{-in} \\ MA_6 = 0.84\text{-in} & \text{etc} \end{matrix}$$

$$\text{Effective Width of Baseplate for Bending} =$$

$$B_{eff} := .82 \cdot \sqrt{\left( \frac{D_{bp}}{2} \right)^2 - \left( \frac{D_{pole}}{2} \right)^2} = 14.4\text{-in}$$

### Anchor Bolt Analysis:

#### Calculated Anchor Bolt Properties:

Polar Moment of Inertia =

$$I_p := \sum_i (d_i)^2 = 1.822 \times 10^3 \text{ in}^2$$

Gross Area of Bolt =

$$A_g := \frac{\pi}{4} \cdot D^2 = 0.785 \cdot \text{in}^2$$

Net Area of Bolt =

$$A_n := \frac{\pi}{4} \left( D - \frac{0.9743 \cdot \text{in}}{n} \right)^2 = 0.606 \cdot \text{in}^2$$

Net Diameter =

$$D_n := \frac{2 \cdot \sqrt{A_n}}{\sqrt{\pi}} = 0.878 \cdot \text{in}$$

Radius of Gyration of Bolt =

$$r := \frac{D_n}{4} = 0.22 \cdot \text{in}$$

Section Modulus of Bolt =

$$S_x := \frac{\pi \cdot D_n^3}{32} = 0.066 \cdot \text{in}^3$$

#### Check Anchor Bolt Tension Force:

Maximum Tensile Force =

$$T_{Max} := OM \cdot \frac{R_{bc}}{I_p} - \frac{\text{Axial}}{N} = 26.8 \text{ kips}$$

Allowable Tensile Force =

$$T_{ALL.Gross} := 1.333 \cdot (0.33 \cdot A_g \cdot F_u) = 41.5 \text{ kips}$$

 (1.333 increase  
allowed per TIA/EIA)

$$T_{ALL.Net} := 1.333 \cdot (0.60 \cdot A_n \cdot F_y) = 44.572 \text{ kips}$$

 (1.333 increase  
allowed per TIA/EIA)

Bolt Tension % of Capacity =

$$\frac{T_{Max}}{T_{ALL.Net}} \cdot 100 = 60 \quad \text{Bolts are "upset bolts". Use net area per AISC}$$

Condition1 =

$$\text{Condition1} := \text{if} \left( \frac{T_{Max}}{T_{ALL.Net}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

**Condition1 = "OK"**

#### Check Anchor Bolt Bending Stress:

Maximum Bending Moment =

$$M_x := \left( \frac{\text{Shear}}{N} \right) \cdot I = 0.075 \cdot \text{ft-kips}$$

Maximum Bending Stress =

$$f_{bx} := \frac{M_x}{S_x} = 13.5 \text{ ksi}$$

Allowable Bending Stress =

$$F_{bx} := 1.333 \cdot 0.6 \cdot F_y = 73.6 \text{ ksi}$$

 (1.333 increase  
allowed per TIA/EIA)

Check Combined Stress Requirement:

Per ASCE Manual 72: "If the clearance between the base plate and concrete does not exceed two times the bolt diameter a bending stress analysis of the bolts is NOT normally required.

$$I := \begin{cases} I & \text{if } I > 2 \cdot D_n \\ 0 & \text{otherwise} \end{cases} = 3\text{-in}$$

$$f_{bx} := \begin{cases} f_{bx} & \text{if } I > 2 \cdot D_n \\ 0 & \text{otherwise} \end{cases} = 13.5\text{-ksi}$$

Check Anchor Bolt Compression/Combined Stress:

Maximum Compressive Force =

$$C_{Max} := OM \cdot \frac{R_{bc}}{I_p} + \frac{\text{Axial}}{N} = 27.6\text{-kips}$$

Maximum Compressive Stress =

$$f_a := \frac{C_{Max}}{A_n} = 45.6\text{-ksi}$$

$$K := 0.65$$

$$C_c := \sqrt{\frac{2 \cdot \pi^2 \cdot E}{F_y}} = 78.881$$

$$F_a := \begin{cases} \left[ 1 - \frac{\left( \frac{K \cdot I}{r} \right)^2}{2 \cdot C_c^2} \right] \cdot F_y & \text{if } \frac{K \cdot I}{r} \leq C_c \\ \frac{5}{3} + \frac{3 \left( \frac{K \cdot I}{r} \right)}{8 \cdot C_c} - \frac{\left( \frac{K \cdot I}{r} \right)^3}{8 \cdot C_c^3} & \\ \frac{12 \cdot \pi^2 \cdot E}{23 \left( \frac{K \cdot I}{r} \right)^2} & \text{if } \frac{K \cdot I}{r} > C_c \end{cases} = 53.5\text{-ksi}$$

Allowable Compressive Stress =

$$F_a := 1.333 \cdot F_a = 71.3\text{-ksi}$$

 (1.333 increase  
 allowed per TIA/EIA)

Combined Stress % of Capacity =

$$\left( \frac{f_a}{F_a} + \frac{f_{bx}}{F_{bx}} \right) \cdot 100 = 82.3$$

Condition 2 =

$$\text{Condition2} := \text{if} \left( \frac{f_a}{F_a} + \frac{f_{bx}}{F_{bx}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition2 = "OK"

**Base Plate Analysis:**

Force from Bolts =

$$C_i := \frac{OM \cdot d_i}{I_p} + \frac{Axial}{N}$$

$$C_1 = 8.8\text{-kips}$$

$$C_7 = 22.4\text{-kips}$$

$$C_2 = 16.4\text{-kips}$$

$$C_8 = 16.4\text{-kips}$$

$$C_3 = 22.4\text{-kips}$$

$$C_9 = 8.8\text{-kips}$$

$$C_4 = 26.3\text{-kips}$$

$$C_{10} = 0.4\text{-kips}$$

$$C_5 = 27.6\text{-kips}$$

$$C_{11} = -8.0\text{-kips}$$

$$C_6 = 26.3\text{-kips}$$

etc.

Maximum Bending Stress in Plate =

$$f_{bp} := \sum_i \frac{6 \cdot C_i \cdot M A_i}{(B_{eff} t_{bp})^2} = 35.6\text{-ksi}$$

Allowable Bending Stress in Plate =

$$F_{bp} := 1.33 \cdot 0.75 \cdot F_y = 49.9\text{-ksi}$$

Plate Bending Stress % of Capacity =

$$\frac{f_{bp}}{F_{bp}} \cdot 100 = 71.4$$

Condition3 =

$$\text{Condition3} := \text{if} \left( \frac{f_{bp}}{F_{bp}} < 1.00, \text{"Ok"}, \text{"Overstressed"} \right)$$

Condition3 = "Ok"

### Ballast Calculation:

#### Input Data:

##### Tower Reactions:

OVERTURNING MOMENT =	OM := 306-ft·kips	(Input From tnxTower)
Shear Force =	Shear := 6-kips	(Input From tnxTower)
Axial Force =	Axial := 8-kips	(Input From tnxTower)
OVERTURNING Factor of Safety Required =	FS <sub>req</sub> := 2.0	(User Input)

##### Ballast Data:

Weight of Base Frame =	WT <sub>frame</sub> := 3kips	(User Input)
Distance From Center of Monopole to Extreme Edge of Base Frame =	c := 7.5-ft	(User Input)
Distance From Frame Toe to Front Ballast String =	d <sub>1</sub> := 3.0-ft	(User Input)
Distance From Frame Toe to Back Ballast String =	d <sub>2</sub> := 12-ft	(User Input)
Depth of Ballast Frame =	d <sub>f</sub> := 1.50-ft	(User Input)
Weight of Concrete =	γ <sub>c</sub> := 145pcf	(User Input)
Block Width =	w <sub>b</sub> := 6-ft	(User Input)
Block Length =	l <sub>b</sub> := 6-ft	(User Input)
Block Thickness =	t <sub>b</sub> := 1-ft	(User Input)
Individual Block Weight =	W <sub>b</sub> := w <sub>b</sub> ·l <sub>b</sub> ·t <sub>b</sub> ·γ <sub>c</sub> = 5220-lb	
Total Overturning Moment About Toe of Base Frame =	M <sub>tot</sub> := OM + Shear·d <sub>f</sub> = 315-ft·kips	
Total Dead Weight =	P <sub>tot</sub> := Axial + WT <sub>frame</sub> = 11-kips	
Net Resisting Moment Required =	M <sub>rnet</sub> := (FS <sub>req</sub> ·M <sub>tot</sub> ) - (P <sub>tot</sub> ·c) = 547.5-kip·ft	
Ballast Required Per Side of Base Frame =	W <sub>req</sub> := $\frac{M_{rnet}}{(d_1 + d_2)} = 36.5\text{-kips}$	
Total Ballast Weight Required =	W <sub>totreq</sub> := W <sub>req</sub> ·2 = 73-kips	
Ballast Weight Required Per Quadrant =	W <sub>reqquad</sub> := $\frac{W_{req}}{2} = 18.25\text{-kips}$	
Number of Blocks Required per Quadrant =	N <sub>b</sub> := $\frac{W_{totreq}}{W_b \cdot (4) \cdot (0.9)} = 3.88$	
	N <sub>buse</sub> := 4	



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Subject:

Ballast Calculation

Location:

85-ft Temporary Ballast Monopole  
East Lyme, CT

Rev. 0: 3/13/15

Prepared by: T.J.L. Checked by: C.F.C.  
Job No. 15021.000

$$\text{Resisting Moment} = M_r := [(W_b) \cdot N_{buse} \cdot 2.0 \cdot (d_1 + d_2)] + (P_{tot} \cdot c) = 708.9 \text{-kip}\cdot\text{ft}$$

$$\text{Actual Factor of Safety} = FS := \frac{M_r}{M_{tot}} = 2.25$$

$$\text{FOS\_Check} := \text{if}(FS \geq FS_{req}, \text{"Okay"}, \text{"No Good"})$$

FOS\_Check = "Okay"

Section 1 - RFDS GENERAL INFORMATION						
RFDS NAME:	CT5990	DATE:	2/12/2015 0:00	RF DESIGN ENG:	Radu Alecsandru	RF PERF ENG:
ISSUE:	Final	Approved? (Y/N)	Y	RF DESIGN PHONE:	8605137598	RF PERF PHONE:
REVISION:	V02	RF MANAGER:	Cameron Syme	RF DESIGN EMAIL:		RF PERF EMAIL:
INITIATIVE / PROJECT:	Temporary COW					
USID:	168399	FA LOCATION CODE:	13068061	LOCATION NAME:	N Main Street	ORACLE PRUT #1:
REGION:	NORTHEAST	MARKET CLUSTER:	NEW ENGLAND	MARKET:	CT	ORACLE PRUT #2:
ADDRESS:	ANCIENT WAY	CITY:	EAST LYME	STATE:	CT	ORACLE PRUT #3:
ZIP CODE:	06107	COUNTY:	NEW LONDON	MSA/RSA:	TBD	ORACLE PRUT #4:
LATITUDE (D-M-S):	41 21' 36.2"	LONGITUDE (D-M-S):	72° 13' 35.4"	LAT (DEC. DEG.):		SEARCH RING NAME:
DIRECTIONS, ACCESS AND EQUIPMENT LOCATION:	TBD					
TRIDENT:						
GSM FREQUENCY:						
UMTS FREQUENCY:						
LTE FREQUENCY:						
U-PLAN JOB # 1:						
U-PLAN JOB # 2:						
U-PLAN JOB # 3:						
U-PLAN JOB # 4:						
Section 2 - LOCATION INFORMATION						
USID:	168399	FA LOCATION CODE:	13068061	LOCATION NAME:	N Main Street	ORACLE PRUT #1:
REGION:	NORTHEAST	MARKET CLUSTER:	NEW ENGLAND	MARKET:	CT	ORACLE PRUT #2:
ADDRESS:	ANCIENT WAY	CITY:	EAST LYME	STATE:	CT	ORACLE PRUT #3:
ZIP CODE:	06107	COUNTY:	NEW LONDON	MSA/RSA:	TBD	ORACLE PRUT #4:
LATITUDE (D-M-S):	41 21' 36.2"	LONGITUDE (D-M-S):	72° 13' 35.4"	LAT (DEC. DEG.):		SEARCH RING NAME:
DIRECTIONS, ACCESS AND EQUIPMENT LOCATION:	TBD					
SEARCH RING ID:						
ITAC:						
LONG (DEC. DEG.):						
BORDER CELL WITH CON:						
AM STUDY REQ'D (Y/N):						
FREQ COORD:						
Section 3 - LICENSE COVERAGE/FILING INFORMATION						
CGSA - NO FILING TRIGGERED:	TBD	CGSA LOSS:	TBD	PCS REDUCED - UPS ZIP:	TBD	
CGSA - MINOR FIING NEEDED:	TBD	CGSA EXT AGMT NEEDED:	TBD	PCS POPS REDUCED:	TBD	
CGSA - MAJOR FIUNG NEEDED:	TBD	CGSA SCORECARD UPDATED:	TBD			
Section 4 - TOWER/REGULATORY INFORMATION						
STRUCTURE AT T OWNED?:	TBD	GROUND ELEVATION (ft):		STRUCTURE TYPE:	MONOPOLE	MKT LOCATION 850 MHZ CALL SIGN(S):
ADDITIONAL REGULATORY?:	TBD	HEIGHT OVERALL (ft):		FCC ASR NUMBER:	TBD	MKT LOCATION 1900 MHZ CALL SIGN(S):
SUB-LEASE RIGHTS?:	TBD	STRUCTURE HEIGHT (ft):				MKT LOCATION 700 MHZ CALL SIGN(S):
LIGHTING TYPE:						MKT LOCATION AWS MHZ CALL SIGN(S):
Section 5 - E-911 INFORMATION						
PSAP NAME:		PSAP ID:	E911 PHASE:	MPC SVC PROVIDER:	LMU REQUIRED:	ESRN:
ALPHA	TBD	TBD	TBD	TBD	TBD	TBD
BETA	TBD	TBD	TBD	TBD	TBD	TBD
GAMMA	TBD	TBD	TBD	TBD	TBD	TBD
DELTA						
EPSILON						
PSI						
Section 6 - RBS GENERAL INFORMATION						
4-DIGIT SITE ID:	1173	COW OR TOY?:	NO	CELLULAR NETWORK:	GO	
CELL SITE TYPE:	SECTORIZED	SITE TYPE:	COW	DPS DISTRICT:	TB	
BTS LOCATION ID:	TBD	ORIGINATING CO:	ATT	BS DISTRICT:	TB	
Section 7 - RBS SPECIFIC INFORMATION						
GSM RBSs	UMTS 1ST CARRIER RBSs	UMTS 2ND CARRIER RBSs	UMTS 3RD CARRIER RBSs	UMTS 4TH CARRIER RBSs		
MSC	TBD	TBD	TBD	TBD		N/A
BSC/RNC	TBD	MDTWCTNCRB05	MDTWCTNCRB05	MDTWCTNCRB05		N/A
LAC	TBD	5990	5990	5990		N/A
RAC	TBD	255	255	255		N/A
EQUIPMENT VENDOR	NOKIA	ERICSSON	ERICSSON	ERICSSON		N/A
EQUIPMENT TYPE	TBD	RBS3206	1900 Radio Kit	850 RRUW OBIF		N/A
LOCATION	TBD	TBD	TBD	TBD		N/A
CABINET LOCATION	TBD	TBD	TBD	TBD		N/A
Section 8 - RBS INDIVIDUAL INFORMATION						
GSM 850 RBS	GSM 1900 RBS	UMTS 850 RBS	UMTS 1900 RBS	UMTS 2ND 850 RBS	UMTS 3RD 850 RBS	UMTS 4TH 850 RBS
CELL ID/BCF	184G5990	NA	CTV5990	NA	CTU5990	N/A
CIS COMMON ID	184G5990	NA	CTV5990	NA	CTU5990	N/A
Section 9 - SOFT SECTOR ID						
GSM 850 RBS	GSM 1900 RBS	UMTS 850 RBS	UMTS 1900 RBS	UMTS 2ND 850 RBS	UMTS 3RD 850 RBS	UMTS 4TH 1900 RBS
ALPHA (OR OMNI)	184G599001	TBD	CTV59901	NA	CTU59907	CTV5990A
BETA	184G599002	TBD	CTV59902	NA	CTU59908	CTV5990B
GAMMA	184G599003	TBD	CTV59903	NA	CTU59909	CTV5990C
DELTA						
EPSILON						
PSI						
Section 10 - CID/SAC						
GSM 850 RBS	GSM 1900 RBS	UMTS 850 RBS	UMTS 1900 RBS	UMTS 2ND 850 RBS	UMTS 3RD 1900 RBS	UMTS 4TH 850 RBS
ALPHA (OR OMNI)	59901	TBD	59901	NA	59907	49901
BETA	59902	TBD	59902	NA	59908	49902
GAMMA	59903	TBD	59903	NA	59909	49903
DELTA						
EPSILON						
PSI						
Section 11 - CURRENT RADIO COUNTS (Existing)						
GSM 850 RBS	GSM 1900 RBS	UMTS 850 RBS	UMTS 1900 RBS	UMTS 2ND 850 RBS	UMTS 3RD 1900 RBS	UMTS 4TH 1900 RBS
ALPHA	3	NA	1	NA	NA	NA
BETA	2	NA	1	NA	NA	NA
GAMMA	2	NA	1	NA	NA	NA
DELTA						
EPSILON						
PSI						
Section 12 - CURRENT BASE BAND CONFIGURATION (Existing)						
GSM 1st Cabinet	GSM 2nd Cabinet	UMTS 1st Cabinet	UMTS 2nd Cabinet	UMTS 3rd Cabinet		
# T1s	TBD	TBD	TBD	N/A		
LINK PROFILE						
RF Combining						
Fiber or Ethernet?	TBD	TBD	TBD	TBD		
Tx Board Model						
Tx Board QTY						
BBU Board Model						
BBU Board QTY						
RRU - Type[Qty-Model]						
Fiber Jumper						
DC Cable						
DC/Fiber Dem. Box						
Bundled Fiber Cable						
Bundled DC Cable						
Section 13 - NEW/PROPOSED RADIO COUNTS						
GSM 850 RBS	GSM 1900 RBS	UMTS 850 RBS	UMTS 1900 RBS	UMTS 2ND 850 RBS	UMTS 3RD 1900 RBS	UMTS 4TH 850 RBS
ALPHA (OR OMNI)	1	NA	1	NA	1	N/A
BETA	1	NA	1	NA	1	N/A
GAMMA	1	NA	1	NA	1	N/A
DELTA						
EPSILON						
PSI						
Section 14 - NEW/PROPOSED BASE BAND CONFIGURATION						
GSM 1st Cabinet	GSM 2nd Cabinet	UMTS 1st Cabinet	UMTS 2nd Cabinet	UMTS 3rd Cabinet		
# T1s	TBD	TBD	TBD	N/A		
LINK PROFILE						
RF Combining						
Fiber or Ethernet?						
Tx Board Model						
Tx Board QTY						
BBU Board Model						
BBU Board QTY						
RRU - Type[Qty-Model]						
Fiber Jumper						
DC Cable						
DC/Fiber Dem. Box						
Bundled Fiber Cable						
Bundled DC Cable						

Section 15A - CURRENT SECTOR/CELL INFORMATION - ALPHA (OR OMNI)				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?				
TECHNOLOGY				
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE				
Feeder Length (feet)				
ANTENNA ATOLL				
ANTENNA MAKE - MODEL				
ANTENNA VENDOR				
ANTENNA SIZE (H x W x D)				
ANTENNA WEIGHT				
ANTENNA GAIN				
AZIMUTH				
RADIATION CENTER (feet)				
ANTENNA TIP HEIGHT				
ELECTRICAL TILT (700/850/1900/AWS)				
MECHANICAL DOWNTILT				
FEEDER AMOUNT				
Antenna RET Motor (QTY/MODEL)				
Antenna RET Splitter (QTY/MODEL)				
Antenna RET Earth Grounding) Clamp (QTY/MODEL)				
Antenna RET Surge Arrestor (QTY/MODEL)				
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site				
DC BLOCK (QTY/MODEL)				
TMA/NA (QTY/MODEL)				
CURRENT INJECTOR FOR TMA (QTY/MODEL)				
POU FOR TMAS (QTY/MODEL) usually per site				
SURGE ARRESTOR (QTY/MODEL)				
DIPLEXER (QTY/MODEL)				
HYBRID COMBINER (QTY/MODEL)				
DUPLEXER (QTY/MODEL)				
FILTER (QTY/MODEL)				
RRAT KIT MODULE?				
TRIPLXER or NARROW BAND LLC (QTY/MODEL)				
SCPA/MCPA MODULE?				
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION				
HATCHPLATE POWER (Watts)				
ERP (Watts)				
Local Market Note1				
Local Market Note2				
Local Market Note3				
Section 15B - CURRENT SECTOR/CELL INFORMATION - BETA				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?				
TECHNOLOGY				
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE				
Feeder Length (feet)				
ANTENNA ATOLL				
ANTENNA MAKE - MODEL				
ANTENNA VENDOR				
ANTENNA SIZE (H x W x D)				
ANTENNA WEIGHT				
ANTENNA GAIN				
AZIMUTH				
RADIATION CENTER (feet)				
ANTENNA TIP HEIGHT				
ELECTRICAL TILT (700/850/1900/AWS)				
MECHANICAL DOWNTILT				
FEEDER AMOUNT				
Antenna RET Motor (QTY/MODEL)				
Antenna RET Splitter (QTY/MODEL)				
Antenna RET Earth Grounding) Clamp (QTY/MODEL)				
Antenna RET Surge Arrestor (QTY/MODEL)				
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site				
DC BLOCK (QTY/MODEL)				
TMA/NA (QTY/MODEL)				
CURRENT INJECTOR FOR TMA (QTY/MODEL)				
POU FOR TMAS (QTY/MODEL) usually per site				
SURGE ARRESTOR (QTY/MODEL)				
DIPLEXER (QTY/MODEL)				
HYBRID COMBINER (QTY/MODEL)				
DUPLEXER (QTY/MODEL)				
FILTER (QTY/MODEL)				
RRAT KIT MODULE?				
TRIPLXER or NARROW BAND LLC (QTY/MODEL)				
SCPA/MCPA MODULE?				
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION				
HATCHPLATE POWER (Watts)				
ERP (Watts)				
Local Market Note1				
Local Market Note2				
Local Market Note3				
Section 15C - CURRENT SECTOR/CELL INFORMATION - GAMMA				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?				
TECHNOLOGY				
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE				
Feeder Length (feet)				
ANTENNA ATOLL				
ANTENNA MAKE - MODEL				
ANTENNA VENDOR				
ANTENNA SIZE (H x W x D)				
ANTENNA WEIGHT				
ANTENNA GAIN				
AZIMUTH				
RADIATION CENTER (feet)				
ANTENNA TIP HEIGHT				
ELECTRICAL TILT (700/850/1900/AWS)				
MECHANICAL DOWNTILT				
FEEDER AMOUNT				
Antenna RET Motor (QTY/MODEL)				
Antenna RET Splitter (QTY/MODEL)				
Antenna RET Earth Grounding) Clamp (QTY/MODEL)				
Antenna RET Surge Arrestor (QTY/MODEL)				
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site				
DC BLOCK (QTY/MODEL)				
TMA/NA (QTY/MODEL)				
CURRENT PHASE SHIFTER FOR TMA (QTY/MODEL)				
POU FOR TMAS (QTY/MODEL) usually per site				
SURGE ARRESTOR (QTY/MODEL)				
DIPLEXER (QTY/MODEL)				
HYBRID COMBINER (QTY/MODEL)				
DUPLEXER (QTY/MODEL)				
FILTER (QTY/MODEL)				
RRAT KIT MODULE?				
TRIPLXER or NARROW BAND LLC (QTY/MODEL)				
SCPA/MCPA MODULE?				
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION				
HATCHPLATE POWER (Watts)				
ERP (Watts)				
Local Market Note1				
Local Market Note2				
Local Market Note3				

Section 15D - CURRENT SECTOR/CELL INFORMATION - DELTA				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?				
TECHNOLOGY				
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE				
Feeder Length (feet)				
ANTENNA ATOLL				
ANTENNA MAKE - MODEL				
ANTENNA VENDOR				
ANTENNA SIZE (H x W x D)				
ANTENNA WEIGHT				
ANTENNA GAIN				
AZIMUTH				
RADIATION CENTER (feet)				
ANTENNA TIP HEIGHT				
ELECTRICAL TILT (700/850/1900/AWS)				
MECHANICAL DOWNTILT				
FEEDER AMOUNT				
Antenna RET Motor (QTY/MODEL)				
Antenna RET Splitter (QTY/MODEL)				
Antenna RET Earth Grounding Clamp (QTY/MODEL)				
Antenna RET Surge Arrestor (QTY/MODEL)				
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site				
DC BLOCK (QTY/MODEL)				
TMA/LNA (TYPE/MODEL)				
CURRENT INJECTORS FOR TMA (QTY/MODEL)				
PDU FOR TMAS (QTY/MODEL) usually per site				
SURGE ARRESTOR (QTY/MODEL)				
DIPLEXER (QTY/MODEL)				
HYBRID COMBINER (QTY/MODEL)				
DUPLEXER (QTY/MODEL)				
FILTER (QTY/MODEL)				
RAVEN MODULE?				
TRIPLExER or NARROW BAND LLC (QTY/MODEL)				
SCPA/MCPA MODULE?				
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION				
HATCHPLATE POWER (Watts)				
ERP (Watts)				
Local Market Note1				
Local Market Note2				
Local Market Note3				
Section 15E - CURRENT SECTOR/CELL INFORMATION - EPSILON				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?				
TECHNOLOGY				
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE				
Feeder Length (feet)				
ANTENNA ATOLL				
ANTENNA MAKE - MODEL				
ANTENNA VENDOR				
ANTENNA SIZE (H x W x D)				
ANTENNA WEIGHT				
ANTENNA GAIN				
AZIMUTH				
RADIATION CENTER (feet)				
ANTENNA TIP HEIGHT				
ELECTRICAL TILT (700/850/1900/AWS)				
MECHANICAL DOWNTILT				
FEEDER AMOUNT				
Antenna RET Motor (QTY/MODEL)				
Antenna RET Splitter (QTY/MODEL)				
Antenna RET Earth Grounding Clamp (QTY/MODEL)				
Antenna RET Surge Arrestor (QTY/MODEL)				
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site				
DC BLOCK (QTY/MODEL)				
TMA/LNA (TYPE/MODEL)				
CURRENT INJECTORS FOR TMA (QTY/MODEL)				
PDU FOR TMAS (QTY/MODEL) usually per site				
SURGE ARRESTOR (QTY/MODEL)				
DIPLEXER (QTY/MODEL)				
HYBRID COMBINER (QTY/MODEL)				
DUPLEXER (QTY/MODEL)				
FILTER (QTY/MODEL)				
RAVEN MODULE?				
TRIPLExER or NARROW BAND LLC (QTY/MODEL)				
SCPA/MCPA MODULE?				
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION				
HATCHPLATE POWER (Watts)				
ERP (Watts)				
Local Market Note1				
Local Market Note2				
Local Market Note3				
Section 15F - CURRENT SECTOR/CELL INFORMATION - ZETA				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?				
TECHNOLOGY				
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE				
Feeder Length (feet)				
ANTENNA ATOLL				
ANTENNA MAKE - MODEL				
ANTENNA VENDOR				
ANTENNA SIZE (H x W x D)				
ANTENNA WEIGHT				
ANTENNA GAIN				
AZIMUTH				
RADIATION CENTER (feet)				
ANTENNA TIP HEIGHT				
ELECTRICAL TILT (700/850/1900/AWS)				
MECHANICAL DOWNTILT				
FEEDER AMOUNT				
Antenna RET Motor (QTY/MODEL)				
Antenna RET Splitter (QTY/MODEL)				
Antenna RET Earth Grounding Clamp (QTY/MODEL)				
Antenna RET Surge Arrestor (QTY/MODEL)				
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site				
DC BLOCK (QTY/MODEL)				
TMA/LNA (TYPE/MODEL)				
CURRENT INJECTORS FOR TMA (QTY/MODEL)				
PDU FOR TMAS (QTY/MODEL) usually per site				
SURGE ARRESTOR (QTY/MODEL)				
DIPLEXER (QTY/MODEL)				
HYBRID COMBINER (QTY/MODEL)				
DUPLEXER (QTY/MODEL)				
FILTER (QTY/MODEL)				
RAVEN MODULE?				
TRIPLExER or NARROW BAND LLC (QTY/MODEL)				
SCPA/MCPA MODULE?				
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION				
HATCHPLATE POWER (Watts)				
ERP (Watts)				
Local Market Note1				
Local Market Note2				
Local Market Note3				

Section 16A - NEW/PROPOSED SECTOR/CELL INFORMATION - ALPHA (OR OMNI)				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?	TxRx-TxRx	TxRx-TxRx		
TECHNOLOGY	LTE / UMTS / GSM BOTTOM	N/A		
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE?	7/8" - Andrew	7/8" - Andrew		
Feeder Length (feet)	95'	95'		
ANTENNA ATOL:				
ANTENNA MAKE - MODEL	AM-X-CD-16-65-00T-RET			
ANTENNA VENDOR	KMW			
ANTENNA SIZE (H x W x D)	72.0 x 11.8 x 5.9			
ANTENNA WEIGHT	48.5			
ANTENNA GAIN	17.1 dBi			
AZIMUTH	0°			
RADIATION CENTER (feet)	82'			
ANTENNA TIP HEIGHT	85'			
ELECTRICAL TILT (PRO/850/1900/AWS)	0°	0°		
MECHANICAL DOWNTILT	0°			
FEEDER AMOUNT	2			
Antenna RET Motor (QTY/MODEL)	N/A / KMW / Built-in RET Equipment			
Antenna RET Splitter (QTY/MODEL)	N/A			
Antenna RET Earth Grounding Clamp (QTY/MODEL)	N/A			
Antenna RET Surge Arrestor (QTY/MODEL)	N/A			
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site	N/A			
DC BLOCK (QTY/MODEL)	N/A			
TMA/LNA (TYPE/MODEL)	1 / CCI / DTMAPBP7819VG12A			
CURRENT INJECTORS FOR TMA (QTY/MODEL)	1 / Kathrein / 782-11055			
PDU FOR TMAS (QTY/MODEL) usually per site	Kathrein / 860-10006			
SURGE ARRESTOR (QTY/MODEL)	rew / APTDC-BDDFM-DBW/RRH BOTT			
DIPLEXER (QTY/MODEL)	NO Diplexer, use existing Triplexer			
HYBRID COMBINER (QTY/MODEL)	N/A			
DUPLEXER (QTY/MODEL)	use existing included with 850 LLC			
FILTER (QTY/MODEL)	N/A			
RAIL (QTY/MODEL)	RxAlt - 850 Band			
TRIPLEXER or NARROW BAND LCC (QTY/MODEL)	2 / LLC - 850 Band PCS-AWS Triplexer, DC through to PCS-AWS Port, CCI			
SCPA/MCPA MODULE?	N/A	N/A		
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION	-14°			
HATCHPLATE POWER (Watts)	N/A	N/A		
ERP (Watts)	N/A	N/A		
Local Market Note1				
Local Market Note2				
Local Market Note3				

Section 16B - NEW/PROPOSED SECTOR/CELL INFORMATION - BETA				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?	TxRx-TxRx	TxRx-TxRx		
TECHNOLOGY	LTE / UMTS / GSM BOTTOM	N/A		
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE?	7/8" - Andrew	7/8" - Andrew		
Feeder Length (feet)	95'	95'		
ANTENNA ATOL:				
ANTENNA MAKE - MODEL	AM-X-CD-16-65-00T-RET			
ANTENNA VENDOR	KMW			
ANTENNA SIZE (H x W x D)	72.0 x 11.8 x 5.9			
ANTENNA WEIGHT	48.5			
ANTENNA GAIN	17.1 dBi			
AZIMUTH	120°			
RADIATION CENTER (feet)	82'			
ANTENNA TIP HEIGHT	85'			
ELECTRICAL TILT (PRO/850/1900/AWS)	0°	0°		
MECHANICAL DOWNTILT	0°			
FEEDER AMOUNT	2			
Antenna RET Motor (QTY/MODEL)	N/A / KMW / Built-in RET Equipment			
Antenna RET Splitter (QTY/MODEL)	N/A			
Antenna RET Earth Grounding Clamp (QTY/MODEL)	N/A			
Antenna RET Surge Arrestor (QTY/MODEL)	N/A			
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site	N/A			
DC BLOCK (QTY/MODEL)	N/A			
TMA/LNA (TYPE/MODEL)	1 / CCI / DTMAPBP7819VG12A			
CURRENT INJECTORS FOR TMA (QTY/MODEL)	1 / Kathrein / 782-11055			
PDU FOR TMAS (QTY/MODEL) usually per site	Kathrein / 860-10006			
SURGE ARRESTOR (QTY/MODEL)	rew / APTDC-BDDFM-DBW/RRH BOTT			
DIPLEXER (QTY/MODEL)	NO Diplexer, use existing Triplexer			
HYBRID COMBINER (QTY/MODEL)	N/A			
DUPLEXER (QTY/MODEL)	use existing included with 850 LLC			
FILTER (QTY/MODEL)	N/A			
RAIL (QTY/MODEL)	RxAlt - 850 Band			
TRIPLEXER or NARROW BAND LCC (QTY/MODEL)	2 / LLC - 850 Band PCS-AWS Triplexer, DC through to PCS-AWS Port, CCI			
SCPA/MCPA MODULE?	N/A	N/A		
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION	-14°			
HATCHPLATE POWER (Watts)	N/A	N/A		
ERP (Watts)	N/A	N/A		
Local Market Note1				
Local Market Note2				
Local Market Note3				

Section 16C - NEW/PROPOSED SECTOR/CELL INFORMATION - GAMMA				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?	TxRx-TxRx	TxRx-TxRx		
TECHNOLOGY	LTE / UMTS / GSM BOTTOM	N/A		
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE?	7/8" - Andrew	7/8" - Andrew		
Feeder Length (feet)	95'	95'		
ANTENNA ATOL:				
ANTENNA MAKE - MODEL	AM-X-CD-16-65-00T-RET			
ANTENNA VENDOR	KMW			
ANTENNA SIZE (H x W x D)	72.0 x 11.8 x 5.9			
ANTENNA WEIGHT	48.5			
ANTENNA GAIN	17.1 dBi			
AZIMUTH	240°			
RADIATION CENTER (feet)	82'			
ANTENNA TIP HEIGHT	85'			
ELECTRICAL TILT (PRO/850/1900/AWS)	0°	0°		
MECHANICAL DOWNTILT	0°			
FEEDER AMOUNT	2			
Antenna RET Motor (QTY/MODEL)	N/A / KMW / Built-in RET Equipment			
Antenna RET Splitter (QTY/MODEL)	N/A			
Antenna RET Earth Grounding Clamp (QTY/MODEL)	N/A			
Antenna RET Surge Arrestor (QTY/MODEL)	N/A			
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site	N/A			
DC BLOCK (QTY/MODEL)	N/A			
TMA/LNA (TYPE/MODEL)	1 / CCI / DTMAPBP7819VG12A			
CURRENT INJECTORS FOR TMA (QTY/MODEL)	1 / Kathrein / 782-11055			
PDU FOR TMAS (QTY/MODEL) usually per site	Kathrein / 860-10006			
SURGE ARRESTOR (QTY/MODEL)	rew / APTDC-BDDFM-DBW/RRH BOTT			
DIPLEXER (QTY/MODEL)	NO Diplexer, use existing Triplexer			
HYBRID COMBINER (QTY/MODEL)	N/A			
DUPLEXER (QTY/MODEL)	use existing included with 850 LLC			
FILTER (QTY/MODEL)	N/A			
RAIL (QTY/MODEL)	RxAlt - 850 Band			
TRIPLEXER or NARROW BAND LCC (QTY/MODEL)	2 / LLC - 850 Band PCS-AWS Triplexer, DC through to PCS-AWS Port, CCI			
SCPA/MCPA MODULE?	N/A	N/A		
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION	-14°			
HATCHPLATE POWER (Watts)	N/A	N/A		
ERP (Watts)	N/A	N/A		
Local Market Note1				
Local Market Note2				
Local Market Note3				

Section 16D - NEW/PROPOSED SECTOR/CELL INFORMATION - DELTA				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?				
TECHNOLOGY				
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE				
Feeder Length (feet)				
ANTENNA ATOLL				
ANTENNA MAKE - MODEL				
ANTENNA VENDOR				
ANTENNA SIZE (H x W x D)				
ANTENNA WEIGHT				
ANTENNA GAIN				
AZIMUTH				
RADIATION CENTER (feet)				
ANTENNA TIP HEIGHT				
ELECTRICAL TILT (PRO/850/1900/AWS)				
MECHANICAL DOWNTILT				
FEEDER AMOUNT				
Antenna RET Motor (QTY/MODEL)				
Antenna RET Splitter (QTY/MODEL)				
Antenna RET Earth Grounding Clamp (QTY/MODEL)				
Antenna RET Surge Arrestor (QTY/MODEL)				
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site				
DC BLOCK (QTY/MODEL)				
TMA/LNA (TYPE/MODEL)				
CURRENT INJECTORS FOR TMA (QTY/MODEL)				
PDU FOR TMAS (QTY/MODEL) usually per site				
SURGE ARRESTOR (QTY/MODEL)				
DIPLEXER (QTY/MODEL)				
HYBRID COMBINER (QTY/MODEL)				
DUPLEXER (QTY/MODEL)				
FILTER (QTY/MODEL)				
RAVEN MODULE?				
TRIPLExER or NARROW BAND LLC (QTY/MODEL)				
SCPA/MCPA MODULE?				
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION				
HATCHPLATE POWER (Watts)				
ERP (Watts)				
Local Market Note1				
Local Market Note2				
Local Market Note3				
Section 16E - NEW/PROPOSED SECTOR/CELL INFORMATION - EPSILON				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?				
TECHNOLOGY				
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE				
Feeder Length (feet)				
ANTENNA ATOLL				
ANTENNA MAKE - MODEL				
ANTENNA VENDOR				
ANTENNA SIZE (H x W x D)				
ANTENNA WEIGHT				
ANTENNA GAIN				
AZIMUTH				
RADIATION CENTER (feet)				
ANTENNA TIP HEIGHT				
ELECTRICAL TILT (PRO/850/1900/AWS)				
MECHANICAL DOWNTILT				
FEEDER AMOUNT				
Antenna RET Motor (QTY/MODEL)				
Antenna RET Splitter (QTY/MODEL)				
Antenna RET Earth Grounding Clamp (QTY/MODEL)				
Antenna RET Surge Arrestor (QTY/MODEL)				
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site				
DC BLOCK (QTY/MODEL)				
TMA/LNA (TYPE/MODEL)				
CURRENT INJECTORS FOR TMA (QTY/MODEL)				
PDU FOR TMAS (QTY/MODEL) usually per site				
SURGE ARRESTOR (QTY/MODEL)				
DIPLEXER (QTY/MODEL)				
HYBRID COMBINER (QTY/MODEL)				
DUPLEXER (QTY/MODEL)				
FILTER (QTY/MODEL)				
RAVEN MODULE?				
TRIPLExER or NARROW BAND LLC (QTY/MODEL)				
SCPA/MCPA MODULE?				
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION				
HATCHPLATE POWER (Watts)				
ERP (Watts)				
Local Market Note1				
Local Market Note2				
Local Market Note3				
Section 16F - NEW/PROPOSED SECTOR/CELL INFORMATION - ZETA				
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?				
TECHNOLOGY				
RRH LOCATION (Top/Bottom/None)				
FEEDERS TYPE				
Feeder Length (feet)				
ANTENNA ATOLL				
ANTENNA MAKE - MODEL				
ANTENNA VENDOR				
ANTENNA SIZE (H x W x D)				
ANTENNA WEIGHT				
ANTENNA GAIN				
AZIMUTH				
RADIATION CENTER (feet)				
ANTENNA TIP HEIGHT				
ELECTRICAL TILT (PRO/850/1900/AWS)				
MECHANICAL DOWNTILT				
FEEDER AMOUNT				
Antenna RET Motor (QTY/MODEL)				
Antenna RET Splitter (QTY/MODEL)				
Antenna RET Earth Grounding Clamp (QTY/MODEL)				
Antenna RET Surge Arrestor (QTY/MODEL)				
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site				
DC BLOCK (QTY/MODEL)				
TMA/LNA (TYPE/MODEL)				
CURRENT INJECTORS FOR TMA (QTY/MODEL)				
PDU FOR TMAS (QTY/MODEL) usually per site				
SURGE ARRESTOR (QTY/MODEL)				
DIPLEXER (QTY/MODEL)				
HYBRID COMBINER (QTY/MODEL)				
DUPLEXER (QTY/MODEL)				
FILTER (QTY/MODEL)				
RAVEN MODULE?				
TRIPLExER or NARROW BAND LLC (QTY/MODEL)				
SCPA/MCPA MODULE?				
Additional Component1				
Additional Component2				
Additional Component3				
MAGNETIC DECLINATION				
HATCHPLATE POWER (Watts)				
ERP (Watts)				
Local Market Note1				
Local Market Note2				
Local Market Note3				

## AM-X-CD-16-65-00T-RET(6' 65° Dual Broadband Antenna)

Dual Band Electrical DownTilt Antenna

698 ~ 894MHz, X-pol., H65° / V12°

1710 ~ 2170MHz, X-pol., H65° / V6.0°

### Electrical Specification

Frequency Range	698~894MHz	1710~2170MHz
Impedance	50Ω	
Polarization	Dual, Slant ±45°	
Gain	15.5dBi / 13.35dBd @ 698-806MHz 16.0dBi / 13.85dBd @ 824-894MHz	17.3dBi / 15.15dBd @ 1710-1755MHz 17.4dBi / 15.25dBd @ 1850-1900MHz 17.1dBi / 14.95dBd @ 2110-2155MHz
Beamwidth	Horizontal 65° @ 698-806MHz 63° @ 824-894MHz	65° @ 1710-1755MHz 67° @ 1850-1900MHz 69° @ 2110-2155MHz
	Vertical 12.3° @ 698-806MHz 11.5° @ 824-894MHz	6.5° @ 1710-1755MHz 6.0° @ 1850-1900MHz 5.7° @ 2110-2155MHz
VSWR	≤1.5:1	
Front-to-Back Ratio	≥27 dB	
Electrical Downtilt Range	2° ~ 16°	0° ~ 10°
Isolation Between Ports	≥30 dB	
Isolation Between Ports of Different Frequency Elements	≥35 dB	
Cross Pole Discrimination	10.0 dB @ ±60° 15.0 dBi @ 0°	
First Upper Side Lobe Suppression	16dB	
Side Lobe Suppression	> 16 dB @ 0-6° Tilt >> 18 dB @ 7-12° Tilt (Up to 10° from Boresight)	> 16 dB @ 0-6° Tilt >> 18 dB @ 7-10° Tilt (Up to 10° from Boresight)
Passive Intermodulation	≤ -150 dBc @ 2x20w	
Input Maximum CW Power	500 W	300 W
Environmental Compliance	IP65 for Radome IP67 for Connectors	
RET Motor Configuration	Field Replaceable RET Electronic Control Module / RET Motor is internal to antenna & not field replaceable	
Compliant with AISG 1.1 and 2.0	AISG 1.1 and 2.0	

### Mechanical Specification

Dimension (W×D×H)	11.8×5.9×72 inches (300×150×1829mm)
Weight (Without clamp)	48.5 lbs (22.0 kg)
Connector	4 x 7/16 DIN(F), Long Neck
Max Wind Speed	150 mph
Wind Load (@150 mph)	1891 N

## Twin Triple Band “Active PCS with 700 and 850 Band Pass-thru” Dual Duplexed TMA

Tel: 201-342-3338

Fax: 201-342-3339

[www.cciproducts.com](http://www.cciproducts.com)



CCI's Twin Triple Band (700 Band, Cellular and PCS) TMA contains two triple band TMA's in a single housing. The PCS TMA is full band and fully duplexed, while the 700 Band and Cellular RF is bypassed and combined (Dplexed) with the PCS RF signal. High linearity improves the uplink sensitivity and the receive performance of base stations. The TMA is fully compliant with the latest AISG 2.0 specification. The TMA supports EDGE/GSM, UMTS and LTE BTS equipment. It provides a convenient package for sites upgraded to triple or quad antenna configurations. The twin TMA package reduces tower loading, leasing, and installation costs. Unit count on the tower is cut in half. An excellent match for two branch receive diversity applications using triple polarization antennas. The input and output connectors are located inline for ease of installation in space constrained areas such as uni-pole structures and stealth antennas.

### Technical Description

The TMA system consists of a twin outdoor triple band tower mount unit which combine separate PCS, 700 Band & Cellular antennas onto a single BTS port. The PCS path of the tower mount unit is dual duplexed to separate the low-power uplink signals from the high-power downlink signals at the antenna port, amplifies the low-level uplink signals using an ultra-low noise amplifier (LNA), and recombines the two paths at the BTS port. The 700 Band & Cellular path is ultra low loss and passive. Both paths are dplexed at the BTS port. The tower mount units consist of eight band-pass filters, two redundant low-noise amplifiers, bypass failure circuitry, and bias tee's which are all housed in an IP65 moisture proof enclosure, with IP68 Immersion proof connectors suited to long-life masthead mounting. The unit provides protection against lightning strikes via a multi-stage surge protection circuit. DC power and control is provided via the feeder cable from the BTS or a Power Distribution Unit (PDU). Optional AISG 2.0 DC power and control is provided via the feeder cable from the BTS using the AISG 2.0 and 3GPP standard. The optional AISG TMA detects which BTS port has DC Voltage/AISG Sampling applied and automatically switches to utilize that port. Additionally the AISG TMA operates at constant power when powered by an AISG 2.0 Compatible Site Control Unit, but may be powered by a "Standard Power distribution Unit. A separate AISG connector is also provided to allow direct AISG connection or "Daisy Chaining" to multiple AISG products at the top of the tower.

An optional indoor site control unit (SCU) is available to power up to up to 32 AISG modules per sector and to provide the all the monitoring and alarm functions for the system. The SCU is housed in a single (1U) 1.75" x 19" rack and contains triple redundant power supplies capable of being "hot swapped" that provide a regulated DC supply voltage on the RF coax for the tower mount amplifiers.



Model  
DTMABP7819VG12A

### Contents:

General Info and Technical Description	1
Electrical & Mechanical Specs (AISG TMA)	2
Block Diagram & Outline Drawing (AISG TMA)	3

### Features:

- Small, lightweight, twin unit
- Triple Band Dual Duplexed (PCS with 700 Band & Cellular Bypass)
- Optional AISG 2.0 compatible unit
- AISG TMA detects BTS port that DC voltage and AISG sampling is applied to, and automatically switches to utilize that port
- AISG TMA operates at constant power
- AISG TMA may be powered by a standard PDU
- High linearity
- Lightning protected
- Fail-safe bypass mode
- High reliability

## Twin Triple Band "Active AWS with 700 and 850 Band Pass-thru" TMA Typical Specifications



Description		Typical Specifications
<b>Electrical Specifications</b>		
700 Band & Cellular Frequency Range		698 to 894 MHz
PCS Receive Frequency Range		1850 – 1910 MHz
PCS Transmit Frequency Range		1930 - 1990 MHz
PCS Amplifier Gain		6 to 12 dB Adjustable in 0.25 dB steps via AISG
PCS Gain Variation		±1.0 dB
PCS System Noise Figure		1.4 dB (@ +25°C), 1.6 dB (@ +65°C), At 1910 MHz: 1.7 dB (@ +25°C), 1.9 dB (@ +65°C)
PCS Input Third Order Intercept Point		+12 dBm Min @ Max. Gain
Input/Output Return Loss		18 dB Min. all ports, 15 dB Min. Bypass Mode
<b>Insertion Loss</b>		
700 Band & Cellular Passband		< 0.2 dB, 0.1 dB typical
PCS Transmit Passband		0.4 dB Typical
PCS Transmit Passband Ripple		±0.2 dB
PCS Bypass Mode, Rx Passband		1.6 dB (@ +25°C), 1.8 dB (@ +65°C), At 1910 MHz: 2.3 dB (@ +25°C), 2.5 dB (@ +65°C)
PCS Bypass Mode, Rx Passband Ripple		±1 dB
<b>Filter Characteristics</b>		
700 Band & Cellular Path Rejection		70 dB @ 1850 - 1990 MHz
PCS Path Rejection		80 dB @ 698 - 894 MHz
Continuous Average Power		200 Watts max
Peak Envelope Power		2 kW max
<b>Intermodulation Performance</b>		
IMD at ANT port in Rx Band		-112 dBm Min. (2 x +43 dBm tones)
Operating Voltage		+10V to +30V DC provided via coax or AISG
Power Consumption		≤ 2.1 Watts
<b>Mechanical Specifications</b>		
Connectors		DIN 7-16 Female (Long Neck) x 6, AISG x 1
Dimensions (Body Only)		10.63" (H) x 11.02" (W) x 3.78" (D); (270 (H) x 280 (W) x 96 (D) mm)
Dimensions (with Bracket)		14.25" (H) x 11.46" (W) x 4.17" (D); (362 (H) x 291 (W) x 106 (D) mm)
Weight (w/o Bracket)		19.18 Lbs. (8.7 Kg)
Mounting		Pole/Wall Mounting Bracket
<b>Environmental Specifications</b>		
Operating Temperature		-40° C to +65° C
Lightning Protection		8/20us, ±2KA max, 10 strikes each, IEC61000-4-5
Enclosure		IP65 (Unit Body), IP68 (Connector)
MTBF		>500,000 hours

All specifications are subject to change. The latest specifications are available at [www.cciproducts.com](http://www.cciproducts.com)

**Communication Components Inc.**

Tel: 201-342-3338

CCI Confidential

Fax: 201-342-3339

Network Modernization RFDS v3.0

• • T-Mobile •

<b>Site ID</b>	<b>CTNL010A</b>	<b>Latitude</b>	41.36006
		<b>Longitude</b>	-72.22650
<b>Site Name</b>	Temp Site	<b>Site Type</b>	Structure (Non-Building)
<b>Address</b>	Ancient Hwy, East Lyme	<b>Site Class</b>	Monopole
<b>Market</b>	CONNECTICUT	<b>Landlord</b>	

Configuration	Approvals		
4B	Market RF		
	Market Development		
	RFDS Revision		Date 03/11/2015
	RFDS Final		
	Work Order #		NOC# (888) 218-6664

## Site Information

## Existing Configuration

### Proposed Configuration

Cabinet #	1	2	3	4
Technology	GSM/UMTS/LTE			
Cabinet type	3106			
CBU				
DUW30	2			
DUL20	1			
DUG20	1			
DUS41				
RBS6601				
dTRU/TRX				
RU22 B4				
RUS01 B2	6			
RUS01 B4	6			

### Scope of Work

- Relocate cabinet
- Add cabinet
- Swap cabinet
- Remove cabinet
- Make cabinet dark

Add 3106 cabinet. Add 2 DUW30, DUL20, DUG20, 6 RUS01 B2 and 6 RUS01 B4 radios to 3106 cabinet.

ALPHA - Scope of Work

<input checked="" type="checkbox"/>	Add new mount	<input type="checkbox"/>	Add RRU
<input type="checkbox"/>	Relocate antenna	<input type="checkbox"/>	Swap existing RRU
<input checked="" type="checkbox"/>	Add antenna	<input type="checkbox"/>	Remove RRU
<input type="checkbox"/>	Swap antenna	<input type="checkbox"/>	Consolidate coax cables
<input type="checkbox"/>	Remove antenna	<input checked="" type="checkbox"/>	Add coax cables
<input checked="" type="checkbox"/>	Add TMA	<input checked="" type="checkbox"/>	Add fiber cables
<input type="checkbox"/>	Swap TMA	<input type="checkbox"/>	Add hybrid combiner
<input type="checkbox"/>	Remove TMA	<input type="checkbox"/>	Add filter combiner

Add 1 Quad Pole Antenna . Add PCS dd BB TMA at position 1/left. Add AWS dd B4 TMA at position 2/right. Add 2 Coax lines at position 1/left for PCS GSM/UMTS. Add 2 coax lines at position 2/right for AWS UMTS/LTE. Connect PCS GSM/UMTS and AWS UMTS/LTE in cabinet radio units to passive antenna at position 2/left and /right respectively via coax lines.

## BETA - Scope of Work

<input checked="" type="checkbox"/>	Add new mount	<input type="checkbox"/>	Add RRU
<input type="checkbox"/>	Relocate antenna	<input type="checkbox"/>	Swap existing RRU
<input checked="" type="checkbox"/>	Add antenna	<input type="checkbox"/>	Remove RRU
<input type="checkbox"/>	Swap antenna	<input type="checkbox"/>	Consolidate coax cables
<input type="checkbox"/>	Remove antenna	<input checked="" type="checkbox"/>	Add coax cables
<input checked="" type="checkbox"/>	Add TMA	<input checked="" type="checkbox"/>	Add fiber cables
<input type="checkbox"/>	Swap TMA	<input type="checkbox"/>	Add hybrid combiner
<input type="checkbox"/>	Remove TMA	<input type="checkbox"/>	Add filter combiner

Add 1 Quad Pole Antenna . Add PCS dd B2 TMA at position 1/left. Add AWS dd B4 TMA at position 2/right. Add 2 Coax lines at position 1/left for PCS GSM/UMTS. Add 2 coax lines at position 2/right for AWS UMTS/LTE. Connect PCS GSM/UMTS and AWS UMTS/LTE in cabinet radio units to passive antenna at position 2/left and /right respectively via coax lines.

GAMMA - Scope of Work

<input checked="" type="checkbox"/>	Add new mount	<input type="checkbox"/>	Add RRU
<input type="checkbox"/>	Relocate antenna	<input type="checkbox"/>	Swap existing RRU
<input checked="" type="checkbox"/>	Add antenna	<input type="checkbox"/>	Remove RRU
<input type="checkbox"/>	Swap antenna	<input type="checkbox"/>	Consolidate coax cables
<input type="checkbox"/>	Remove antenna	<input checked="" type="checkbox"/>	Add coax cables
<input checked="" type="checkbox"/>	Add TMA	<input checked="" type="checkbox"/>	Add fiber cables
<input type="checkbox"/>	Swap TMA	<input type="checkbox"/>	Add hybrid combiner
<input type="checkbox"/>	Remove TMA	<input type="checkbox"/>	Add filter combiner

Add 1 Quad Pole Antenna . Add PCS dd BB TMA at position 1/left. Add AWS dd B4 TMA at position 2/right. Add 2 Coax lines at position 1/left for PCS GSM/UMTS. Add 2 coax lines at position 2/right for AWS UMTS/LTE. Connect PCS GSM/UMTS and AWS UMTS/LTE in cabinet radio units to passive antenna at position 2/left and /right respectively via coax lines.

DELTA - Scope of Work

	Add new mount
	Relocate antenna
	Add antenna
	Swap antenna
	Remove antenna
	Add TMA
	Swap TMA
	Remove TMA
	Add RRU
	Swap existing RRU
	Remove RRU
	Consolidate coax cables
	Add coax cables
	Add fiber cables
	Add hybrid combiner
	Add filter combiner

# Network Modernization RFDS v3.0

• T • Mobile

Site ID	CTNL010A	Latitude	41.36006
Site Name	Temp Site	Longitude	-72.22650
Address	Ancient Hwy, East Lyme	Site Type	Structure (Non-Building)
Market	CONNECTICUT	Site Class	Monopole
		Landlord	

Configuration	Approvals
4B	Market RF
	Market Development
	RFDS Revision
	RFDS Final
	Date 03/11/2015

ALPHA (view from behind)							
Existing Configuration				Proposed Configuration			
				Technology	GSM/UMTS	UMTS	
				Band	B2	B4	
				Active/Passive	P	P	
				Ant. Type	Quad pole		
				Ant. Model	APX16DWV_16DWVS		
				Ant. Vendor	RFS		
				Ant. Height	72		
				Azimuth	100		
				RET deployed	Yes	Yes	
				E-Tilt	2	2	
				M-Tilt			
				TMA #	1	1	
				TMA Type	dd B2	dd B4	
				RRU #			
				RRU Type			
				Used Coax #	2	2	
				Coax Type	7/8"	7/8"	
				Coax Length (ft)	85		
				Fiber (CPRI) #			
				Splitter #			
				Combiner #			
				Combiner Type			
	Add new mount		Add RRU				
	Relocate antenna		Swap existing RRU				
	Add antenna		Remove RRU				
	Swap antenna		Consolidate coax cables				
	Remove antenna		Add coax cables				
	Add TMA		Add fiber cables				
	Swap TMA		Add hybrid combiner				
	Remove TMA		Add filter combiner				
Scope of work							
Add 1 Quad Pole Antenna . Add PCS dd B2 TMA at position 1/left. Add AWS dd B4 TMA at position 2/right. Add 2 Coax lines at position 1/left for PCS GSM/UMTS. Add 2 coax lines at position 2/right for AWS UMTS/LTE. Connect PCS GSM/UMTS and AWS UMTS/LTE in cabinet radio units to passive antenna at position 2/left and /right respectively via coax lines.							

BETA (view from behind)							
Existing Configuration				Proposed Configuration			
				Technology	GSM/UMTS	UMTS	
				Band	B2	B4	
				Active/Passive	P	P	
				Ant. Type	Quad pole		
				Ant. Model	APX16DWV_16DWVS		
				Ant. Vendor	RFS		
				Ant. Height	72		
				Azimuth	220		
				RET deployed	Yes	Yes	
				E-Tilt	2	2	
				M-Tilt			
				TMA #	1	1	
				TMA Type	dd B2	dd B4	
				RRU #			
				RRU Type			
				Used Coax #	2	2	
				Coax Type	7/8"	7/8"	
				Coax Length (ft)	85		
				Fiber (CPRI) #			
				Splitter #			
				Combiner #			
				Combiner Type			
	Add new mount		Add RRU				
	Relocate antenna		Swap existing RRU				
	Add antenna		Remove RRU				
	Swap antenna		Consolidate coax cables				
	Remove antenna		Add coax cables				
	Add TMA		Add fiber cables				
	Swap TMA		Add hybrid combiner				
	Remove TMA		Add filter combiner				
Scope of work							
Add 1 Quad Pole Antenna . Add PCS dd B2 TMA at position 1/left. Add AWS dd B4 TMA at position 2/right. Add 2 Coax lines at position 1/left for PCS GSM/UMTS. Add 2 coax lines at position 2/right for AWS UMTS/LTE. Connect PCS GSM/UMTS and AWS UMTS/LTE in cabinet radio units to passive antenna at position 2/left and /right respectively via coax lines.							

# Network Modernization RFDS v3.0

• T • Mobile

Site ID	<b>CTNL010A</b>	Latitude	41.36006
Site Name	Temp Site	Longitude	-72.22650
Address	Ancient Hwy, East Lyme	Site Type	Structure (Non-Building)
Market	CONNECTICUT	Site Class	Monopole
		Landlord	

Configuration	Approvals
<b>4B</b>	Market RF
	Market Development
	RFDS Revision
	RFDS Final
	Date 03/11/2015

GAMMA (view from behind)							
Existing Configuration				Proposed Configuration			
				Technology	GSM/UMTS	UMTS	
				Band	B2	B4	
				Active/Passive	A	P	
				Ant. Type	Quad pole		
				Ant. Model	APX16DWV_16DWVS		
				Ant. Vendor	RFS		
				Ant. Height	72		
				Azimuth	340		
				RET deployed	Yes	Yes	
				E-Tilt	2	2	
				M-Tilt			
				TMA #	1	1	
				TMA Type	dd B2	dd B4	
				RRU #			
				RRU Type			
				Used Coax #	2	2	
				Coax Type	7/8"	7/8"	
				Coax Length (ft)	85		
				Fiber (CPRI) #			
				Splitter #			
				Combiner #			
				Combiner Type			
				Scope of work			
Add new mount	Add RRU	Add 1 Quad Pole Antenna . Add PCS dd B2 TMA at position 1/left. Add AWS dd B4 TMA at position 2/right. Add 2 Coax lines at position 1/left for PCS GSM/UMTS. Add 2 coax lines at position 2/right for AWS UMTS/LTE. Connect PCS GSM/UMTS and AWS UMTS/LTE in cabinet radio units to passive antenna at position 2/left and /right respectively via coax lines.					
Relocate antenna	Swap existing RRU						
Add antenna	Remove RRU						
Swap antenna	Consolidate coax cables						
Remove antenna	Add coax cables						
Add TMA	Add fiber cables						
Swap TMA	Add hybrid combiner						
Remove TMA	Add filter combiner						

DELTA (view from behind)							
Existing Configuration				Proposed Configuration			
				Technology			
				Band			
				Active/Passive			
				Ant. Type			
				Ant. Model			
				Ant. Vendor			
				Ant. Height			
				Azimuth			
				RET deployed			
				E-Tilt			
				M-Tilt			
				TMA #			
				TMA Type			
				RRU #			
				RRU Type			
				Used Coax #			
				Coax Type			
				Coax Length (ft)			
				Fiber (CPRI) #			
				Splitter #			
				Combiner #			
				Combiner Type			
				Scope of work			
Add new mount	Add RRU						
Relocate antenna	Swap existing RRU						
Add antenna	Remove RRU						
Swap antenna	Consolidate coax cables						
Remove antenna	Add coax cables						
Add TMA	Add fiber cables						
Swap TMA	Add hybrid combiner						
Remove TMA	Add filter combiner						

Optimizer® Side-by-Side Dual Polarized Antenna, 1710-2200, 65deg, 18.4dBi, 1.4m, VET, 0-10deg RET

## Product Description

A combination of two X-Polarized antennas in a single radome, this pair of variable tilt antennas provides exceptional suppression of all upper sidelobes at all downtilt angles. It also features a wide downtilt range. This antenna is optimized for performance across the entire frequency band (1710-2200 MHz). The antenna comes pre-connected with two antenna control units (ACU).



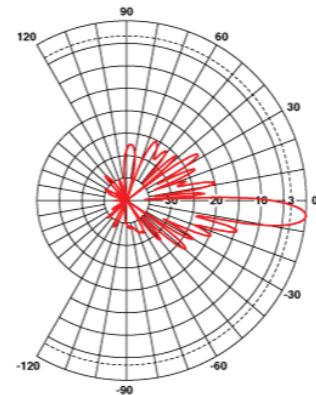
## Features/Benefits

- Variable electrical downtilt - provides enhanced precision in controlling intercell interference. The tilt is infiel adjustable 0-10 deg.
- High Suppression of all Upper Sidelobes (Typically <-20dB).
- Gain tracking – difference between AWS UL (1710-1755 MHz) and DL (2110-2155 MHz) <1dB.
- Two X-Polarised panels in a single radome.
- Azimuth horizontal beamwidth difference <4deg between AWS UL (1710-1755 MHz) and DL (2110-2155 MHz).
- Low profile for low visual impact.
- Dual polarization; Broadband design.
- Includes (2) AISG 2.0 Compatible ACU-A20-N antenna control units.

## Technical Specifications

### Electrical Specifications

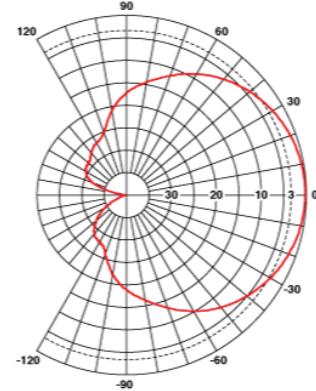
Frequency Range, MHz	1710-2200
Horizontal Beamwidth, deg	65
Vertical Beamwidth, deg	5.9 to 7.7
Electrical Downtilt, deg	0-10
Gain, dBi (dBd)	18.4 (16.3)
1st Upper Sidelobe Suppression, dB	> 18 (typically > 20)
Upper Sidelobe Suppression, dB	> 18 all (typically > 20)
Front-To-Back Ratio, dB	>26 (typically 28)
Polarization	Dual pol +/-45°
VSWR	< 1.5:1
Isolation between Ports, dB	> 30
3rd Order IMP @ 2 x 43 dBm, dBc	> 150 (155 Typical)
Impedance, Ohms	50
Maximum Power Input, W	300
Lightning Protection	Direct Ground
Connector Type	(4) 7-16 Long Neck Female



### Mechanical Specifications

Dimensions - HxWxD, mm (in)	1420 x 331 x 80 (55.9 x 13 x 3.15)
Weight w/o Mtg Hardware, kg (lb)	18.5 (40.7)
Survival Wind Speed, km/h (mph)	200 (125)
Rated Wind Speed, km/h (mph)	160 (100)
Max Wind Loading Area, m² (ft²)	0.47 (5.03)
Front Thrust @ Rated Wind, N (lbf)	756 (170)
Maximum Thrust @ Rated Wind, N (lbf)	756 (170)
Wind Load - Side @ Rated Wind, N (lbf)	231 (52)
Wind Load - Rear @ Rated Wind, N (lbf)	408 (92)
Radome Material	Fiberglass
Radome Color	Light Grey RAL7035
Mounting Hardware Material	Diecasted Aluminum
Shipping Weight, kg (lb)	24.5 (53.9)
Packing Dimensions, HxWxD, mm (in)	1520 x 408 x 198 (59.8 x 16 x 7.8)

Vertical Pattern



Horizontal Pattern

### Ordering Information

Mounting Hardware	APM40-2 + APM40-E2
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## AWS Twin Wideband Dual Duplex TMA

## Product Description

Designed for use in AWS projects, these units improve base station receiver sensitivity and enhance coverage. Use of these TMAs can increase data rates without a reduction in capacity. These TMAs are wideband and cover the entire 45 MHz in the AWS frequency band. The unit is extremely lightweight, weighing just 13 lbs (5.9 kg) for a twin unit. It is easy to install and meets IP66 requirements for ingress protection. The TMA has a metallic base and the radome cap is light grey allowing them to blend with antenna radomes. Its dual-duplex configuration enables the use of a single feeder for both Downlink and Uplink.



## Features/Benefits

- AISG 2.0 compliant
- Two TMAs in a single enclosure – Reduces tower load and installation time.
- Low noise figure overcomes feeder losses and enhances site coverage
- Filtering improves Tx-Rx isolation by reducing noise and interference
- Dual-duplex configuration enables use of a single feeder for both Downlink and Uplink
- Low insertion loss of Tx filter provides increased downlink coverage
- Extremely light weight – Reduces tower loading and facilitates installation.
- Equipped with breather valve – Guards against internal condensation.
- Option: AISG connector location at bottom or top

## Technical Specifications

Product Type	Tower Mount Amplifier
Frequency Band, MHz	1710-1755, 2110-2155
Noise Figure, Typical, dB	1.3 @ midband, 1.5 @ band edge
Gain, dB	12 ± 1
Configuration	AWS double dual-duplex TMA
Mounting	Wall, pole
Uplink Frequency, MHz	1710-1755
Downlink Frequency, MHz	2110-2155
Bandwidth Tx & Rx, MHz	45
Input IP3, Min, dBm	+13
Tx Loss, Max, dB	0.4
Return Loss All Ports, Min, dB	18
Tx Rejection in Rx Branch, Min, dB	80
Rx Rejection in Tx Branch, Min, dB	60
Tx Power Handling, Max, W	250 cw, 5000 peak
IMP Level at the ANT Port, Min, dBm	-117 @ 2 * 43
Nominal Current (ATMAA1412D-1A20), mA	AISG Mode: AWS 1 Port = 120-200 (AISG RS485 port), AWS 2 Port = 100 ± 20 ; Non-AISG Mode: Each port = 100 ± 20
Alarm Current (ATMAA1412D-1A20), mA	AISG Mode: AWS 1 port = AISG alarm, AWS 2 port = 190 ± 10 ; Non-AISG Mode: Each port = 190 ± 10
Impedance, Ohms	50
Temperature Range, °C (°F)	-40 to +65 (-40 to +149)
Ingress Protection	IP66
Connectors	7/16-Female Long-neck
Weight, kg (lb)	5.9 (13)
Application	AWS
Dimensions, H x W x D, mm (in)	305 x 254 x 101 (12 x 10 x 4), includes connector length
Supporting Power Distribution Unit	CNI-P1A20 and CNI-P2A20 with bias-T BITA2S-AL20

## Notes

EXHIBIT D



## VISIBILITY ASSESSMENT

To: David Vivian  
SAI Communications, Inc.  
500 Enterprise Drive, Suite 3A  
Rocky Hill, CT 06067

Date: March 28, 2015

Re: CT1345T - East Lyme Relo  
Temporary Ballast Tower  
Ancient Highway  
East Lyme, Connecticut

From: Michael Libertine

---

New Cingular Wireless PCS, LLC (d/b/a “AT&T”) has identified a potential site candidate location for development of a new, temporary wireless telecommunications facility (“Facility”) on property off Ancient Highway in East Lyme, Connecticut (Map 30, Lot 1; the “host Property”). The proposed Facility would consist of an 85-foot tall, temporary ballast monopole within a 30-foot by 51-foot gravel based, fence-enclosed equipment compound. AT&T would install an approximately 11-foot tall, 12-foot by 20-foot equipment shelter within the compound. Additional space is also being made available for temporary relocation of T-Mobile antennas and equipment. The temporary Facility is required while AT&T secures a new permanent location in this area.

At the request of SAI Communications, Inc. and on behalf of AT&T, All-Points Technology Corporation, P.C. (“APT”) prepared viewshed mapping to evaluate the potential visibility associated with the proposed temporary Facility. To conduct this assessment, a predictive computer model was developed specifically for this project. The predictive model provides an initial estimate of potential visibility throughout a pre-defined Study Area, in this case a two-mile radius surrounding the proposed Facility location.

Computer modeling tools were used to predict those areas where at least a portion of the Facility is estimated to be visible including TerrSet, an image analysis program developed by Clark Labs at Clark University. Project- and Study Area-specific data were incorporated into the computer model, including the site location, its ground elevation and the proposed Facility height, as well as the surrounding topography and existing vegetation, which are the primary features that can block direct lines of sight.

Information used in the model included lidar<sup>1</sup>-based digital elevation data and customized land use data layers developed specifically for this analysis. Lidar is a remote-sensing technology that develops

---

<sup>1</sup> Lidar (a word invented to mean “light radar”) may also be referred to as LiDAR, an acronym for Light Detection and Ranging. It is a technology that utilized lasers to determine the distance to an object or surface. LiDAR is similar to radar, but incorporates laser pulses rather than sound waves. It measures the time delay between transmission and reflection of the laser pulse.

elevation data in meters by measuring the time it takes for laser light to return from the surface to the instrument's sensors. The varying reflectivity of objects also means that the returns can be classified based on the characteristics of the reflected light, normally into categories such as "bare earth," "vegetation," "road," or "building." The system is also designed to capture many more data points than older radar-based systems. Thus, lidar-based digital elevation models ("DEM's) have a much finer resolution and can also identify the different features of the landscape at the time that it was captured.

Viewshed analysis using lidar data provide a much more detailed view of the potential obstacles (especially trees and buildings), and therefore the viewshed modeling produces results with many smaller areas of visibility than those produced by using radar-based DEMs. Its precision makes lidar a superior source of data, but at present it is only available for limited areas of the state. The viewshed results are also checked against the most current aerial photographs in case significant changes (a new housing development, for example) have occurred since the time the lidar data was captured.

The lidar-based DEM created for this analysis represents topographic information for the state of Connecticut that was derived through the spatial interpolation of airborne LiDAR-based data collected in the years 2007 through 2012 and has a horizontal resolution of approximately two (2) feet. In addition, multiple land use data layers were created from the Natural Resources Conservation Service (through the USDA) aerial photography (1-meter resolution, flown in 2012) using IDRISI image processing tools. The IDRISI tools develops light reflective classes defined by statistical analysis of individual pixels, which are then grouped based on common reflective values such that distinctions can be made automatically between deciduous and coniferous tree species, as well as grassland, impervious surface areas, surface water and other distinct land use features.

With these data inputs, the model is then queried to determine where the top of the Facility can be seen from any point(s) within the Study Area, given the intervening existing topography and vegetation. The results of the preliminary analysis are depicted on the attached maps and are intended to provide a representation of those areas where portions of the Facility may potentially be visible to the human eye without the aid of magnification, based on a viewer eye-height of 5 feet above the ground and the combination of intervening topography and tree canopy (year-round) and tree trunks (seasonally, when the leaves are off the deciduous trees). The shaded areas of predicted visibility shown on the map denote locations from within the Study Area which the proposed Facility may potentially be visible year-round (in yellow) above the tree canopy and/or seasonally, through the trees (during "leaf-off" conditions; depicted in orange). The Facility however may not necessarily be visible from all locations within those shaded areas. It is important to note that the computer model cannot account for mass density, the height, diameter and branching variability of the trees, or the degradation of views that occur with distance. In addition, each point – or pixel - represents about one square meter in area, and thus is not predicting visibility from all viewpoints through all possible obstacles. Although large portions of the predicted viewshed may theoretically offer visibility of the Facility, because of these unavoidable limitations the quality of those views may not be sufficient for the human eye to recognize the tower or discriminate it from other surrounding objects. Visibility also varies seasonally with

increased, albeit obstructed, views occurring during “leaf-off” conditions. Beyond the density of woodlands found within the given Study Area, each individual tree has its own unique trunk, pole timber and branching pattern characteristics that provide varying degrees of screening in leafless conditions which cannot be precisely modeled.

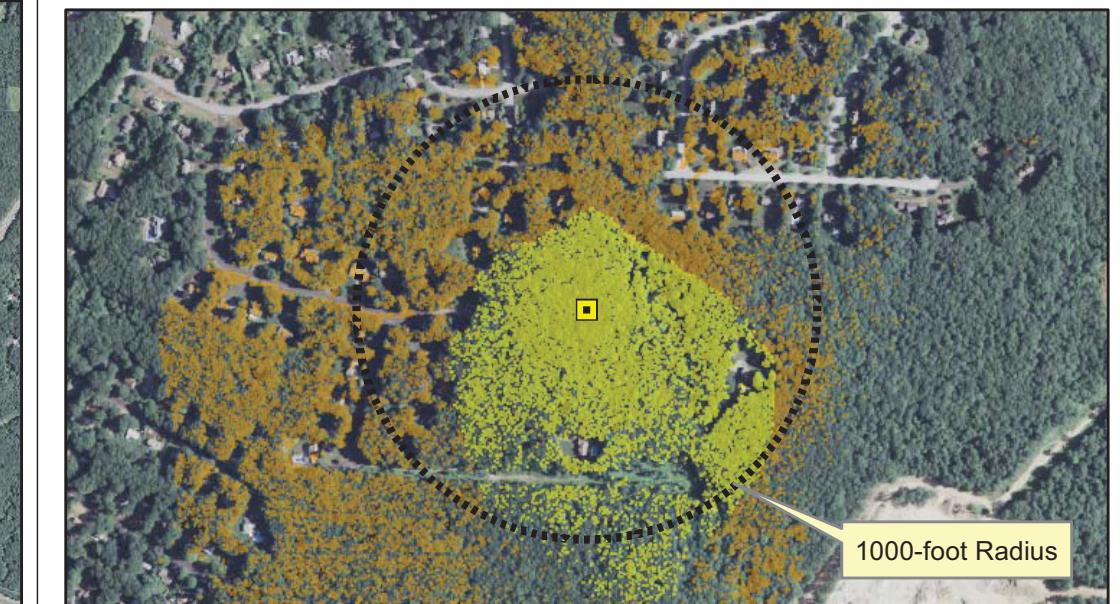
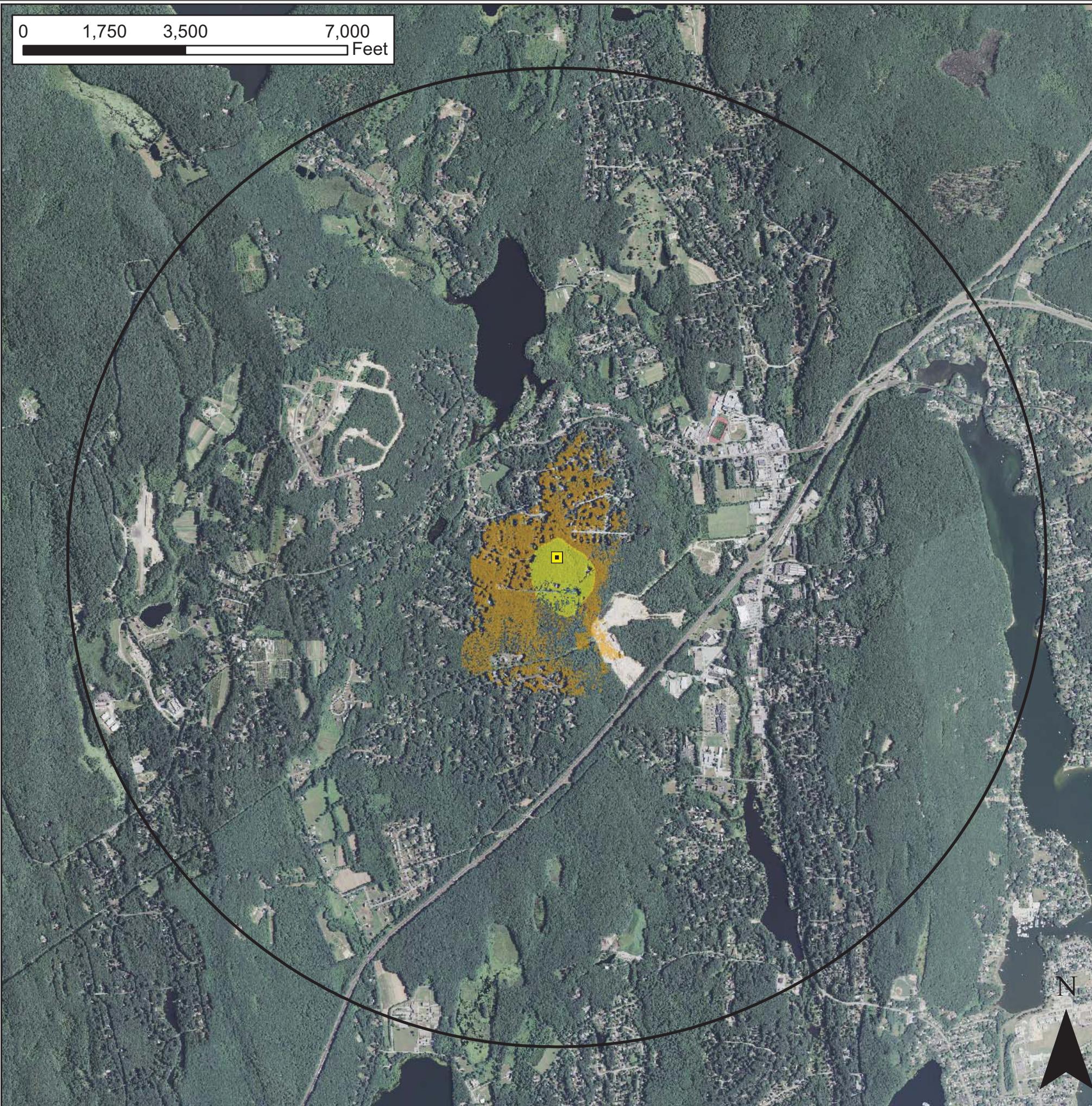
The preliminary viewshed mapping results indicate that year-round visibility associated with the proposed Facility could extend out distances of approximately 0.25 mile primarily to the south of the host Property. Seasonal visibility (when the leaves are off the deciduous trees) may allow views of at least a portion of the Facility at distances of approximately 0.5 mile. On a purely quantitative basis, areas from where the proposed Facility is predicted to be visible above the tree canopy year-round constitute approximately 37 acres. Seasonal views through the intervening pole timber and branches are anticipated to occur over an additional  $178\pm$  acres of land.

APT visited the site on March 27, 2015 to photo-document existing conditions. The attached photo-log map and accompanying photographs depict views from the site and nearby locations. As demonstrated in the photographs, the thick understory and tree cover will prohibit direct views of the compound and lower portions of the temporary tower from surrounding locations, including the nearest homes. Seasonal views, at this time of year when the leaves are off the deciduous trees, may be attained of upper portions of the tower from some nearby locations; however, these potential views would be heavily obscured by intervening trees. Once the leaves are on the trees, no substantial views of the temporary tower are anticipated.

The minimal visibility associated with the proposed temporary Facility is the result of the tower’s relatively low height of 85 feet and the dense tree cover in the area, with several trees reaching heights of 60 to 70 feet.

#### Attachments

## ATTACHMENTS



### Viewshed Map – Topo Base

#### Proposed Temporary Ballast Tower Ancient Highway, East Lyme, CT

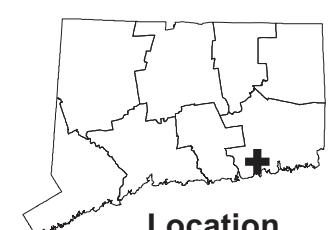
This Visibility Analysis map relies solely on computer modeling and interpretation of aerial photographs and topographic maps. The information presented herein has not been field verified.

#### NOTES

- Viewshed analysis conducted using Clark University's TerrSet.
- Areas of potential visibility are calculated based on facility location and height, Study Area topography, and Study Area vegetation.
- Proposed facility height is 85 feet AGL.
- Forest canopy height is variable, based on the lidar DEM.
- Study area encompasses a two-mile radius and includes 8,042 acres of land.

#### DATA SOURCES

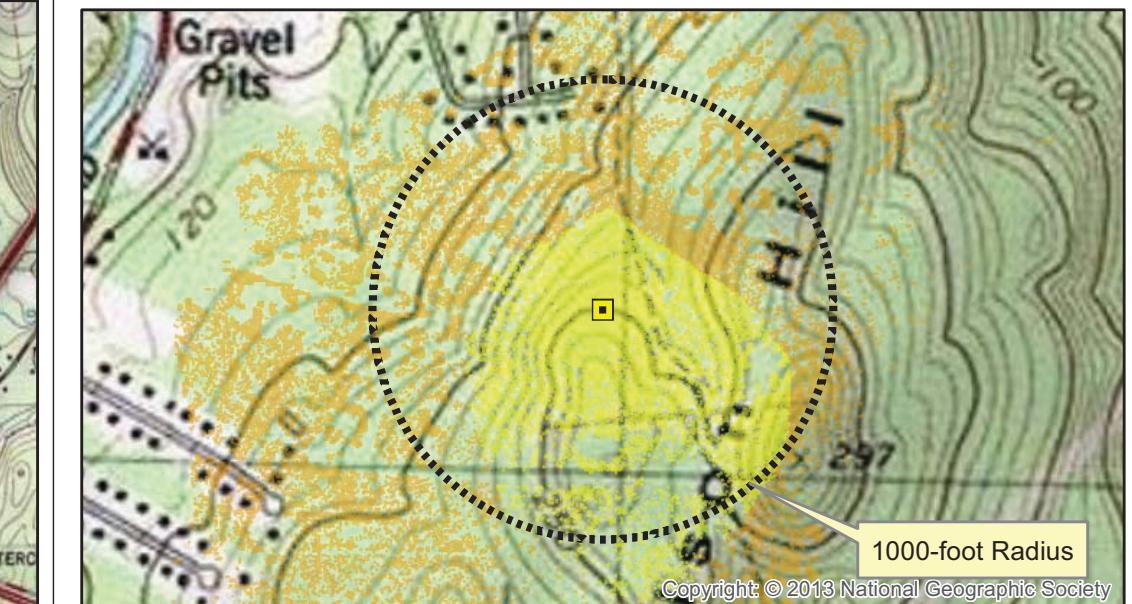
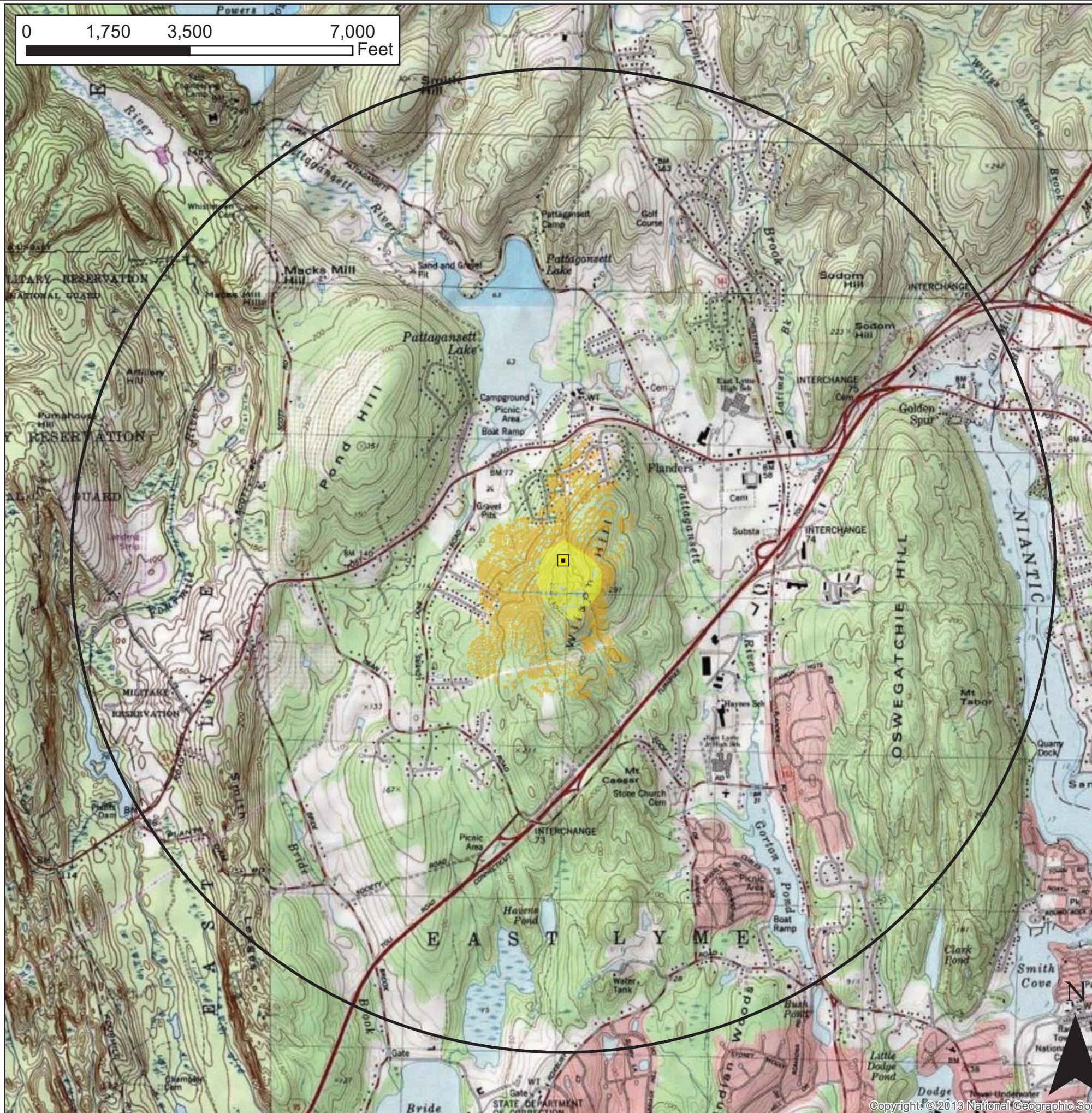
- Digital elevation model (DEM) derived from 0.64-meter USGS lidar data obtained from NOAA.
- Forest areas are generated with TerrSet (Clark University) image processing from the lidar data and 2012 NRCS/NAIP digital orthophotos with 1-meter pixel resolution.
- Municipal Open Space, State Recreation Areas, Trails, County Recreation Areas, and Town Boundary data obtained from CT DEEP and the towns.



### Legend

- Proposed Tower
- Predicted Seasonal Visibility (37 Acres)
- Predicted Year-Round Visibility (178 Acres)
- Towns
- 2-Mile Study Area





### Viewshed Map – Topo Base

#### Proposed Temporary Ballast Tower Ancient Highway, East Lyme, CT

This Visibility Analysis map relies solely on computer modeling and interpretation of aerial photographs and topographic maps. The information presented herein has not been field verified.

#### NOTES

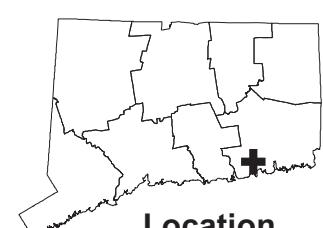
- Viewshed analysis conducted using Clark University's TerrSet.
- Areas of potential visibility are calculated based on facility location and height, Study Area topography, and Study Area vegetation.
- Proposed facility height is 85 feet AGL.
- Forest canopy height is variable, based on the lidar DEM.
- Study area encompasses a two-mile radius and includes 8,042 acres of land.

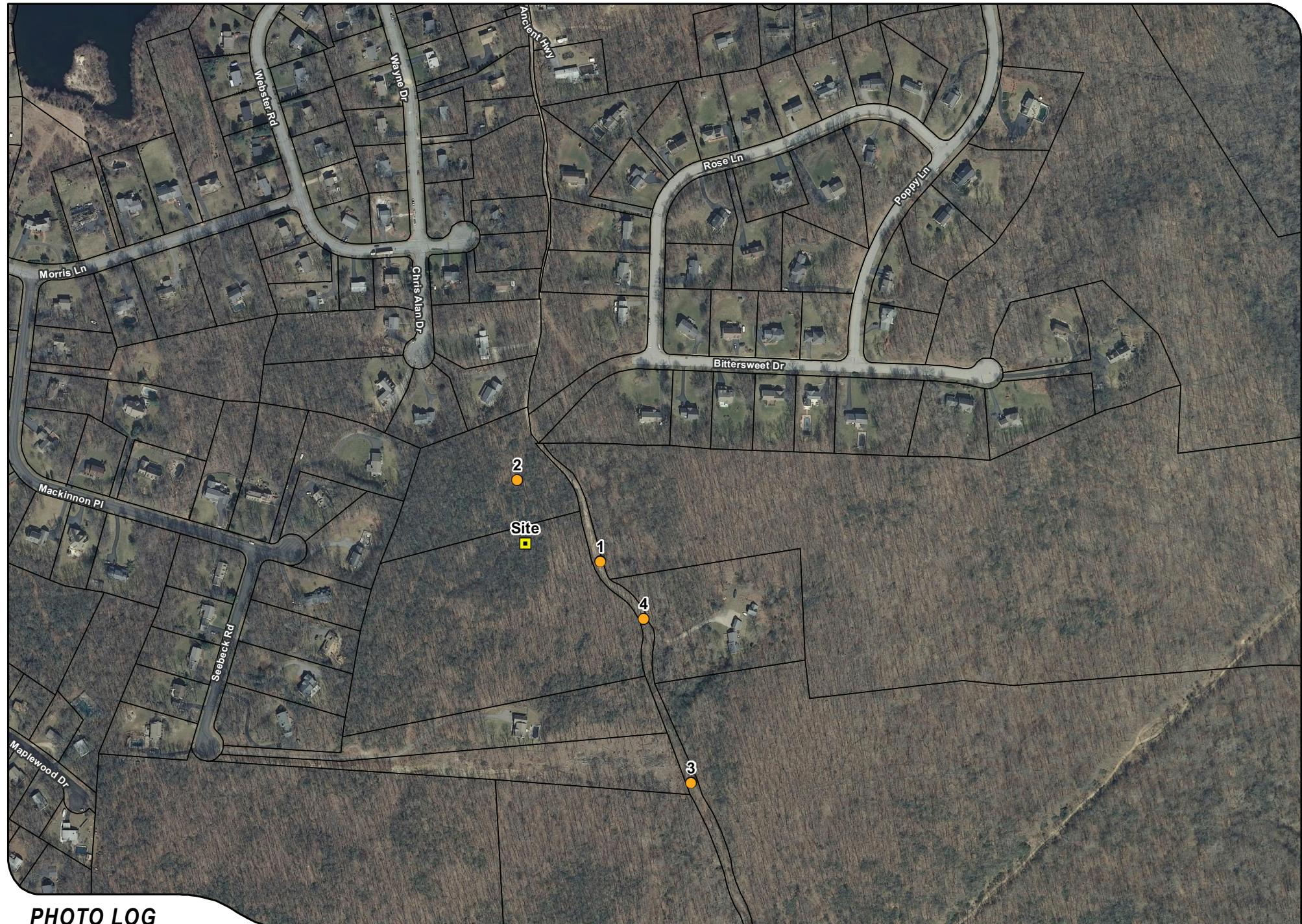
#### DATA SOURCES

- Digital elevation model (DEM) derived from 0.64-meter USGS lidar data obtained from NOAA.
- Forest areas are generated with TerrSet (Clark University) image processing from the lidar data and 2012 NRCS/NAIP digital orthophotos with 1-meter pixel resolution.
- Municipal Open Space, State Recreation Areas, Trails, County Recreation Areas, and Town Boundary data obtained from CT DEEP and the towns.

### Legend

- Proposed Tower
- Predicted Seasonal Visibility (37 Acres)
- Predicted Year-Round Visibility (178 Acres)
- Towns
- 2-Mile Study Area





## PHOTO LOG

### Legend

■ Site   ● Photo Location   □ Approximate Parcel Boundary (CTDEEP)

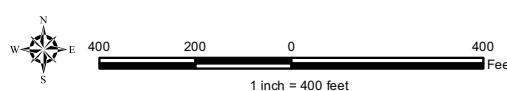




Photo 1: View from Site, looking south.



Photo 2: View from Site, looking north.



Photo 3: View from Site, looking west.



Photo 4: View from Site, looking east.



Photo Location 1: Looking north.



Photo Location 1: Looking southeast.



Photo Location 1: Looking west.



Photo Location 1: Looking east.



Photo Location 2: Looking north.



Photo Location 2: Looking northwest.



Photo Location 3: Looking northwest.



Photo Location 4: Looking east.

EXHIBIT E

Daniel L. Goulet  
C Squared Systems, LLC  
65 Dartmouth Drive  
Auburn, NH 03032  
603-644-2800  
Dan.Goulet@csquaredsystems.com



April 09, 2015

Connecticut Siting Council

Subject: New Cingular Wireless PCS, LLC (“AT&T”) – (CT1345T) – Ancient Highway, East Lyme, CT

Dear Connecticut Siting Council:

C Squared Systems has been retained by New Cingular Wireless PCS, LLC (“AT&T”) to investigate RF Power Density levels for the AT&T and T-Mobile antenna arrays, to be installed on a portable temporary tower, to be located off of Ancient Highway, East Lyme, CT.

Calculations were done in accordance with FCC OET Bulletin 65. These worst-case calculations assume that all transmitters are simultaneously operating at full power and that there is 0 dB of cable loss. The calculation point is 6 feet above ground level to model the RF power density at the head of a person standing at the base of the tower.

Due to the directional nature of the proposed AT&T and T-Mobile antennas, the majority of the RF power is focused out towards the horizon. As a result, there will be less RF power directed below the antennas relative to the horizon, and consequently lower power density levels around the base of the tower. Please refer to the Attachment for the vertical patterns of the proposed AT&T and T-Mobile antennas. The calculated results below include a nominal 10 dB off-beam pattern loss to account for the lower relative gain directly below the antennas.

Location	Carrier	Vertical Distance to Antenna (Ft.)	Operating Frequency (MHz)	Number of Trans.	Effective Radiated Power (ERP) Per Transmitter (Watts)	Power Density (mw/cm <sup>2</sup> )	Limit	%MPE
Ground Level	AT&T LTE	82	710	2	1313	0.0164	0.4733	3.46%
	AT&T GSM	82	880	1	491	0.0031	0.5867	0.52%
	AT&T UMTS	82	880	2	1964	0.0245	0.5867	4.17%
	AT&T UMTS	82	1900	2	2711	0.0338	1.0000	3.38%
	T-Mobile UMTS	72	1900	2	2355	0.0389	1.0000	3.89%
	T-Mobile GSM	72	1900	4	1178	0.0389	1.0000	3.89%
	T-Mobile UMTS	72	2100	2	2524	0.0417	1.0000	4.17%
	T-Mobile LTE	72	2100	2	3786	0.0625	1.0000	6.25%
							Total	29.73%

**Summary:** Under worst-case assumptions, RF Power Density levels for the proposed AT&T antenna arrays will not exceed 29.73%<sup>1</sup> of the FCC MPE limit for General Public/Uncontrolled Environments.

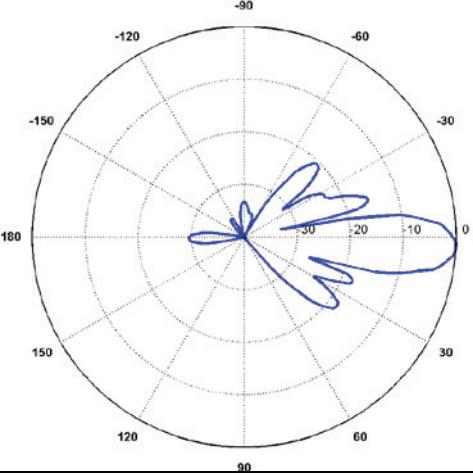
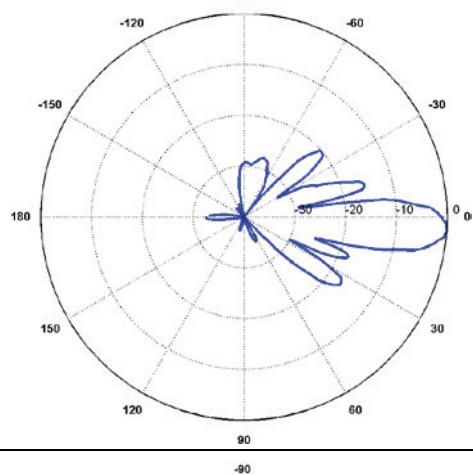
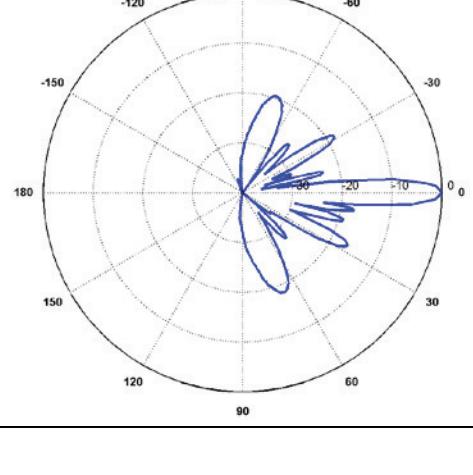
Sincerely,

A handwritten signature in black ink, appearing to read "Daniel L. Goulet".

Daniel L. Goulet  
C Squared Systems, LLC

<sup>1</sup> The total %MPE is a summation of each unrounded contribution. Therefore, summing each rounded value may not reflect the total value listed in the table.

**Attachment: AT&T's Antenna Data Sheets and Electrical Patterns**

<b>750 MHz</b>  Manufacturer: KMW Products Model #: AM-X-CD-16-65-RET Frequency Band: 698-806 MHz Gain: 13.4 dBi Vertical Beamwidth: 12.3° Horizontal Beamwidth: 65° Polarization: Dual Pol ± 45° Size L x W x D: 72" x 11.8" x 5.9"	
<b>850 MHz</b>  Manufacturer: KMW Products Model #: AM-X-CD-16-65-RET Frequency Band: 824-894 MHz Gain: 13.9 dBi Vertical Beamwidth: 11.5° Horizontal Beamwidth: 63° Polarization: Dual Pol ± 45° Size L x W x D: 72" x 11.8" x 5.9"	
<b>1900 MHz</b>  Manufacturer: KMW Products Model #: AM-X-CD-16-65-RET Frequency Band: 824-894 MHz Gain: 15.3 dBi Vertical Beamwidth: 6.0° Horizontal Beamwidth: 67° Polarization: Dual Pol ± 45° Size L x W x D: 72" x 11.8" x 5.9"	

### Attachment: T-Mobile's Antenna Data Sheets and Electrical Patterns

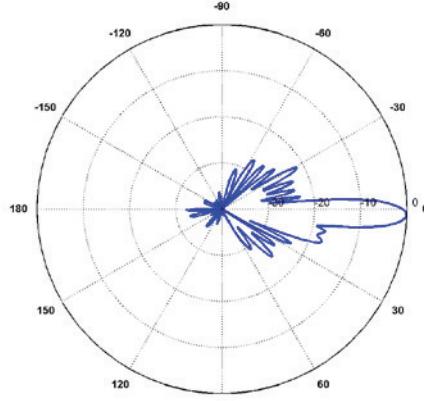
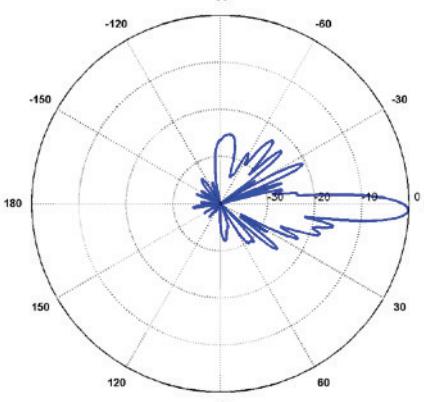
<b>1900 MHz</b>  Manufacturer: RFS Products Model #: APX16DWV-16DWVS Frequency Band: 1850-1990 MHz Gain: 15.6 dBd Vertical Beamwidth: 7.7° Horizontal Beamwidth: 64° Polarization: Dual Pol ± 45° Size L x W x D: 55.9" x 13" x 3.15"	
<b>2100 MHz</b>  Manufacturer: RFS Products Model #: APX16DWV-16DWVS Frequency Band: 1900-2200 MHz Gain: 15.9 dBd Vertical Beamwidth: 6.6° Horizontal Beamwidth: 65° Polarization: Dual Pol ± 45° Size L x W x D: 55.9" x 13" x 3.15"	

EXHIBIT F

CT2022 Incremental

Incremental Coverage from CT2022 Site (850 MHz UMTS)		
<b>Population Coverage:<sup>1</sup></b>	( $\geq$ -74 dBm)	1,370
	( $\geq$ -82 dBm)	2,389
<b>Area Covered (mi<sup>2</sup>):</b>	( $\geq$ -74 dBm)	3.06
	( $\geq$ -82 dBm)	6.25
<b>Roadway Coverage (mi):</b>	Main:	4.18
	Secondary:	16.10
	<b>Total:</b>	<b>20.28</b>

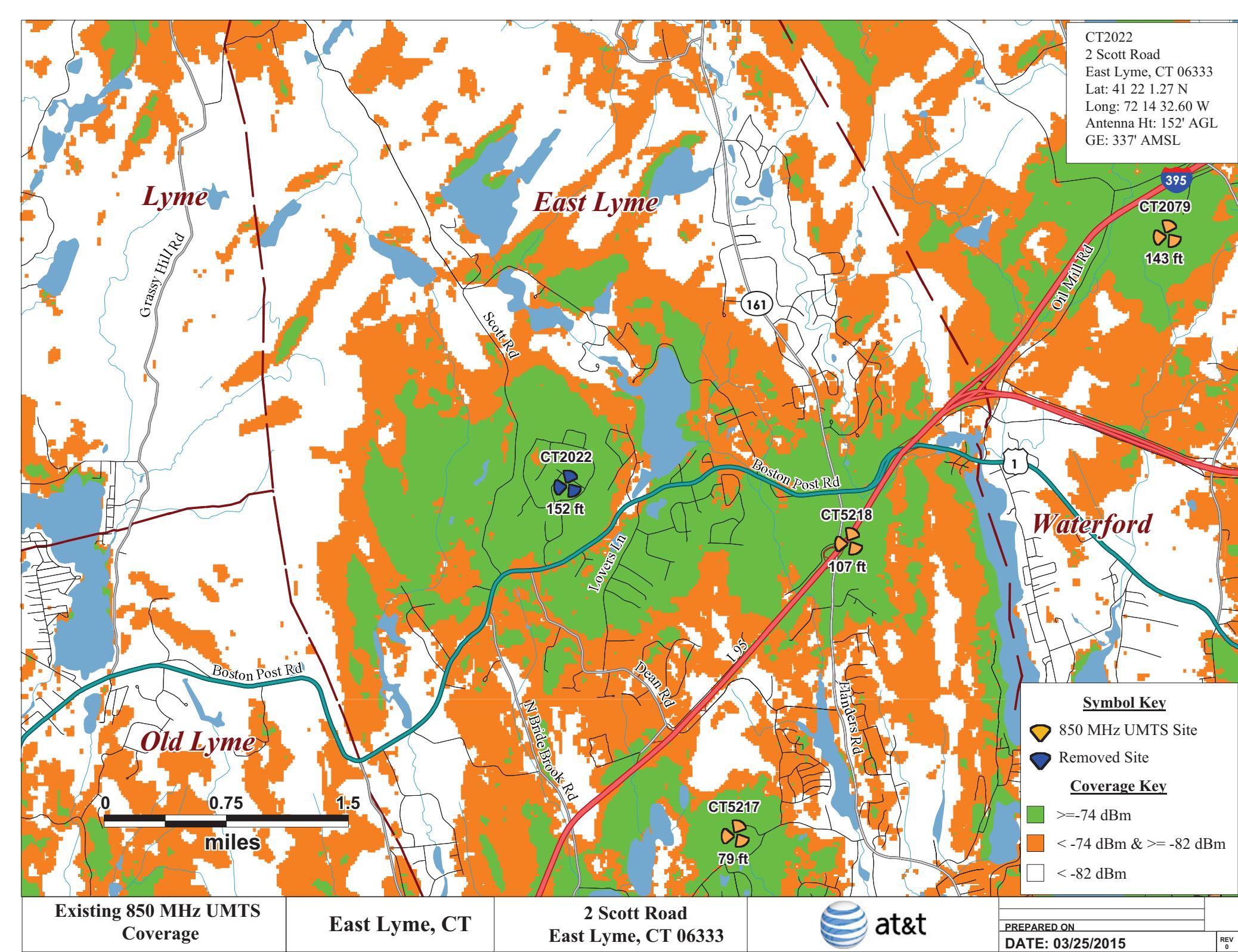
Temporary Tower Incremental

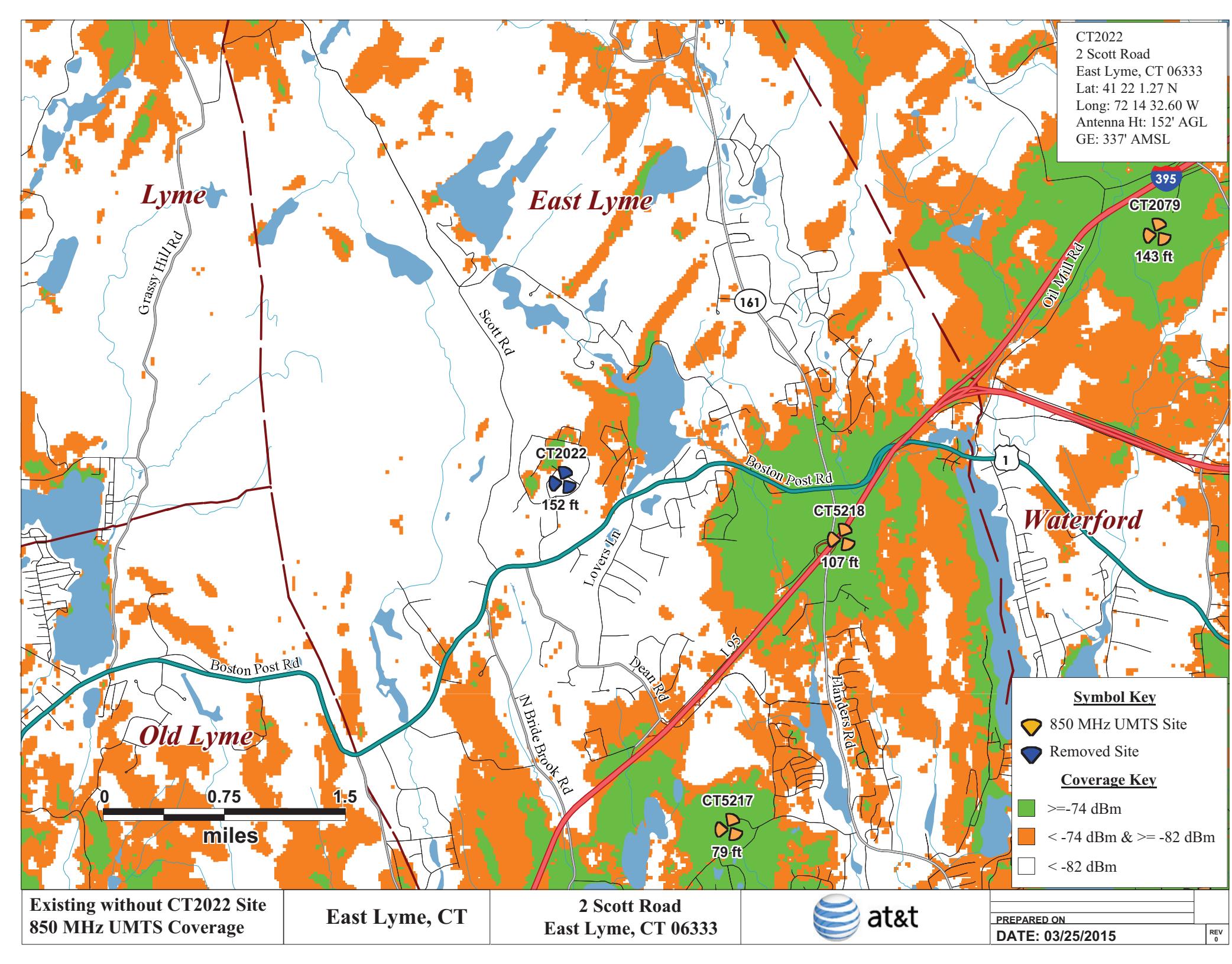
Incremental Coverage from CT1345T (Temporary) Site (850 MHz UMTS)		
<b>Population Coverage:<sup>2</sup></b>	( $\geq$ -74 dBm)	907
	( $\geq$ -82 dBm)	1,660
<b>Area Covered (mi<sup>2</sup>):</b>	( $\geq$ -74 dBm)	1.71
	( $\geq$ -82 dBm)	3.54
<b>Roadway Coverage (mi):</b>	Main:	3.54
	Secondary:	10.05
	<b>Total:</b>	<b>13.59</b>

<sup>1</sup> Population figures are based upon 2010 US Census Block Data

<sup>2</sup> Population figures are based upon 2010 US Census Block Data

CT2022  
2 Scott Road  
East Lyme, CT 06333  
Lat: 41 22 1.27 N  
Long: 72 14 32.60 W  
Antenna Ht: 152' AGL  
GE: 337' AMSL





CT1345-COW  
Ancient Way  
East Lyme, CT 06333  
Lat: 41 21 36.2 N  
Long: 72 13 35.4 W  
Antenna Ht: 82' AGL  
GE: 254' AMSL

*Lyme*

*East Lyme*

Grassy Hill Rd

Scott Rd

161

395  
CT2079

143 ft

Old Mill Rd

*Old Lyme*

miles

0

0.75

1.5

N Bride Brook Rd

Deans Rd

Lovers Ln

195

Flanders Rd

Boston Post Rd

CT5218

107 ft

CT5217

79 ft

CT2022

82 ft

*Waterford*

Symbol Key

850 MHz UMTS Site

Removed Site

Temporary Site

Coverage Key

$\geq -74$  dBm

$< -74$  dBm &  $\geq -82$  dBm

$< -82$  dBm

Existing with CT1345 - COW  
850 MHz UMTS Coverage

East Lyme, CT

Ancient Way  
East Lyme, CT 06333



PREPARED ON  
DATE: 03/25/2015

REV 0

EXHIBIT G

April 2, 2015

**VIA CERTIFIED MAIL**

Re: New Cingular Wireless PCS, LLC (“AT&T”)  
Proposed Temporary Tower Facility  
Ancient Highway, East Lyme Connecticut

Dear Sir or Madam:

We are writing to you on behalf of our client New Cingular Wireless PCS, LLC (“AT&T”) with respect to the above referenced matter and our client’s intent to file a petition with the State of Connecticut Siting Council for approval of a proposed temporary wireless communications tower facility (the “Facility”) within the Town of East Lyme.

State law requires that record owners of property abutting a parcel on which a facility is proposed be sent notice of an applicant’s intent to file a petition with the Siting Council. Because the property has no assigned postal address, we have enclosed a copy of the site plan for your assistance in identifying the location of the proposed temporary tower site location

Included with this letter please find a Notice of this petition with details of the proposed temporary tower Facility. Of note, the location, height and other features of the Facility are subject to review and potential change by the Connecticut Siting Council under the provisions of Connecticut General Statutes §16-50g et seq.

If you have any questions concerning this petition, please contact the Connecticut Siting Council or the undersigned after April 9, 2015, the date which the petition is expected to be on file.

Very truly yours,

Christopher B. Fisher  
Enclosure

## NOTICE

Notice is hereby given, pursuant to Section 16-50j-40(a) of the Regulations of Connecticut State Agencies of a Petition to be filed with the Connecticut Siting Council (“Siting Council”) on or after April 9, 2015 by New Cingular Wireless PCS, LLC (“AT&T” or the “Petitioner”). AT&T will seek a declaratory ruling that a temporary tower proposed on property located off of Ancient Highway in the Town of East Lyme, Connecticut (the “Site”) is either an exempt modification pursuant to Siting Council regulations and/or a tower that does not have significant adverse environmental effects which might otherwise require a certificate of environmental compatibility and public need (“Certificate”).

A temporary tower is being proposed by AT&T to partially replace service that will be disrupted when an existing 150' tall tower located on Scott Road is decommissioned at the requirement of the underlying property owner. The proposed temporary tower will provide limited service for AT&T and T-Mobile until a permanent and relocated tower site can be approved, constructed and made operational. AT&T anticipates filing a technical report for a permanent site and application for a Certificate from the Siting Council in 2015.

AT&T’s proposed temporary tower facility consists of an approximately 85' tall ballast tower, with three (3) AT&T antennas located at a centerline height of 82' AGL. Additionally, T-Mobile would locate three (3) antennas on the temporary tower at a centerline height of approximately 72' AGL. A 30' x 51' gravel equipment compound would be located at the base of the temporary tower, enclosed by a temporary 6' high chain link fence, and include an AT&T unmanned 12' by 20' equipment shelter and T-Mobile equipment cabinets. Access to the facility would be over a proposed gravel driveway from Ancient Highway. Utility connections would be run underground from CL&P utility pole #7479 at Ancient Highway. The temporary tower would be removed upon approval, construction and operation of a permanent tower site location and the site reseeded.

Because the property has no assigned postal address, we have enclosed a copy of the site plan for your assistance in identifying the location of the temporary tower site location. The Petition will provide details of the facility and explain why the Petitioner submits that the proposed temporary tower presents no significant adverse environmental effects. The location, height and other features of the facility are subject to review and potential change under provisions of the Connecticut General Statutes Sections 16-50g et. seq.

Copies of the Petition will be available for review during normal business hours on or after April 9, 2015 at the Connecticut Siting Council:

Connecticut Siting Council  
10 Franklin Square  
New Britain, Connecticut 06051

Town of East Lyme  
Town Clerk  
PO Box 519  
Niantic, CT 06357

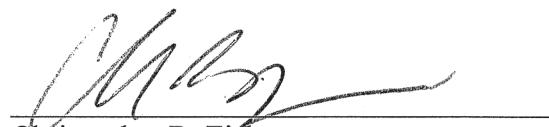
or the offices of the undersigned. All inquiries should be addressed to the Connecticut Siting Council or to the undersigned.

Christopher B. Fisher, Esq.  
Cuddy & Feder LLP  
445 Hamilton Ave, 14th Floor  
White Plains, New York 10601  
(914) 761-1300  
Attorneys for the Petitioner

## CERTIFICATION OF SERVICE

I hereby certify that on the 2d of April 2015, a copy of the foregoing letter and notice were mailed by certified mail, return receipt requested to each of the abutting properties owners on the accompanying list.

4/7/15  
Date



Christopher B. Fisher  
Cuddy & Feder LLP  
445 Hamilton Avenue, 14<sup>th</sup> Floor  
White Plains, New York 10601

Attorneys for:  
New Cingular Wireless PCS, LLC ("AT&T")

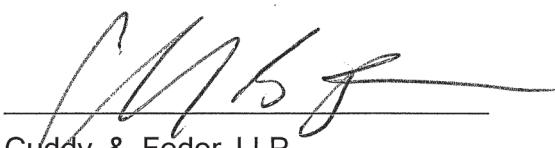
**ADJACENT PROPERTY OWNERS**  
**Ancient Highway**

Christopher J. & Christine M. Charland 8 Seedbeck Rd East Lyme, CT 06333	John A. & Linda T. Rhodes 6 Seebeck Rd East Lyme, CT 06333`
Vivian L. Weinberger 25 Mackinnon Pl East Lyme, CT 06333	Dane & Colleen Proctor 4 Seebeck Rd East Lyme, CT 06333
James W. Patria M. Fleming 10 Seebeck Rd East Lyme, CT 06333	Weng Mei Hui Li Yan 27 Mackinnon Pl East Lyme, CT 06333
Gateway Development East Lyme LLC 342 North Main St. Ste 200 West Hartford, CT 06117	Helen M. Drabik 18 Drabik Rd East Lyme, CT 06333
Carol A. Marelli 74 Ancient Highway East Lyme, CT 06333	

## CERTIFICATION OF SERVICE

I hereby certify that on the 21 day of April 2015, copies of the attached notice of filing of a Petition with the Connecticut Siting Council for a declaratory ruling were sent by certified mail, return receipt requested, to the following:

Dated 4/7/15



Cuddy & Feder LLP

445 Hamilton Avenue, 14<sup>th</sup> Floor

White Plains, New York 10601

Attorneys for:

New Cingular Wireless PCS LLC ("AT&T")

### State and Regional

The Honorable George Jepsen  
Attorney General  
Office of the Attorney General  
55 Elm Street  
Hartford, CT 06106

Connecticut Department of Emergency  
Services & Public Protection  
Division of Emergency Management and  
Homeland Security  
Dora B. Schiro, Commissioner  
25 Sigourney Street, 6th Floor  
Hartford, CT 06106-5042

Department of Energy & Environmental  
Protection  
Rob Klee, Commissioner  
79 Elm Street  
Hartford, CT 06106

Department of Economic & Community  
Development  
Catherine Smith, Commissioner  
505 Hudson Street  
Hartford, CT 06106

Department of Public Health  
Dr. Jewel Mullen, Commissioner  
410 Capitol Avenue  
P.O. Box 340308  
Hartford, CT 06134

Department of Transportation  
James P. Redeker, Commissioner  
2800 Berlin Turnpike  
Newington, CT 06111

Council on Environmental Quality  
Susan D. Merrow, Chair  
79 Elm Street  
Hartford, CT 06106

Department of Energy & Environmental Protection  
Public Utilities Regulatory Authority  
Chairman Arthur House  
Ten Franklin Square  
New Britain, CT 06051

Office of Policy and Management  
Benjamin Barnes, Secretary  
450 Capitol Avenue  
Hartford, CT 06106-1379

Department of Economic and Community Development-Offices of Culture and Tourism  
Daniel Forrest, State Historic Preservation Officer  
One Constitution Plaza, 2<sup>nd</sup> Floor  
Hartford, CT 06103

Department of Agriculture  
Steven Reviczky, Commissioner  
165 Capitol Avenue  
Hartford, CT 06106

State House Representative 37<sup>th</sup> District  
Ed Jutila  
Connecticut House Democrats  
L.O.B. Room 4046  
Hartford, CT 06106

State Senator District S20  
Paul M. Formica  
Legislative Office Building  
Room 3400  
Hartford, CT 06106

James S. Butler, Executive Director  
Southeastern Connecticut Council of Governments  
5 Connecticut Avenue  
Norwich, CT 06360

## Federal

Federal Aviation Administration  
800 Independence Avenue, SW  
Washington, DC 20591

Federal Communications Commission  
445 12<sup>th</sup> Street SW  
Washington, D.C. 20554

Congressman Joe Courtney  
2<sup>nd</sup> Congressional District  
55 Main Street, Suite 250  
Norwich, CT 06360

United States Senator Richard Blumenthal  
90 State House Square, 10<sup>th</sup> Floor  
Hartford, CT 06103

United States Senator Christopher S.  
Murphy  
One Constitution Plaza, 7th Fl.  
Hartford, Connecticut 06103

## Town of East Lyme

First Selectman Mark C. Nickerson  
Town of East Lyme  
P.O. Box 519  
108 Pennsylvania Avenue  
Niantic, CT 06357

Inland Wetlands Commission  
Cheryl Lozanov, Chairwoman  
Town of East Lyme  
P.O. Box 519  
108 Pennsylvania Avenue  
Niantic, CT 06357

Conservation of Natural Resources  
Commission  
Arthur Carlson, Chairman  
Town of East Lyme  
P.O. Box 519  
108 Pennsylvania Avenue  
Niantic, CT 06357

Lesley Blais, Town Clerk  
Town of East Lyme  
P.O. Box 519  
108 Pennsylvania Avenue  
Niantic, CT 06357

Planning Commission  
Brian Schuch, Chairman  
Town of East Lyme  
P.O. Box 519  
108 Pennsylvania Avenue  
Niantic, CT 06357

Zoning Commission  
Mathew Walker, Chairman  
Town of East Lyme  
P.O. Box 519  
108 Pennsylvania Avenue  
Niantic, CT 06357