

Jack Andrews  
Zoning Manager, Empire Telecom  
o/b/o AT&T Wireless  
10130 Donleigh Drive  
Columbia, MD 21046  
443-286-4007  
jandrews@empiretelecomm.com

April 18, 2018

Melanie Bachman  
Acting Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

**NOTICE OF EXEMPT MODIFICATION**

1030 NEW BRITAIN AVENUE, WEST HARTFORD, CT 06110

Lat: 41-43-52.69 (41.73130278)  
Long. 72-43-25.82 (-72.72383889)

Dear Ms. Bachman:

AT&T Wireless currently maintains 9 antennas at the 180-foot level of an existing 185-foot lattice tower located at 1030 New Britain Avenue, in West Hartford, CT. The tower is owned by the Ten Thirty Tower Company, LLC. The property is owned by the Ten Thirty Tower Company, LLC. AT&T Wireless now seeks to install 3 additional antennas at the 180-foot level of the tower, as well as replace 3 existing Remote Radio Units ("RRU") with 3 new RRUS-32 B2 RRUs; install 3 new RRUS-B14 4478 RRUs; install 3 new RRUS-32 B66 RRUs; replace existing GSM line components with low band combiners; and install a single new surge suppressor, all at the 180-foot level of the tower. In addition, the applicant seeks to install 2 new DC power cables along the existing cable route on the side of the tower. AT&T also intends to install 3 new RRUS-E2 and 3 new RRU-12 units at grade on the existing mounting pipes. Five (5) equipment cabinets are currently on grade, 1 cabinet will be decommissioned. AT&T will replace 2 DUS with two (2) 5216 units and replace the IDL2 with an IDLE and add a second XMU within one of the existing at-grade cabinets.

The facility was approved by the Connecticut Siting Council in EM-CING-155-160503 on May 23, 2016. Six conditions were enumerated in the Council's decision: 1) Any deviation from the modification as specified in the Notice and supporting documentation shall render the acknowledgement invalid; 2) Any material changes to the modification as proposed shall require the filing of a new Notice with the Council; 3) Within 45 days after the completion of construction the Council shall be notified in writing that the construction has been completed; 4) Any nonfunctioning antenna and associated antenna mounting equipment on this facility owned and operated by AT&T shall be removed within 60 days of the date the antenna ceased to function; 5)

the validity of the action shall expire one year from the date of the letter; and 6) the applicant may file a request an extension of time beyond the one year deadline provided that such a request is submitted to the Council not less than 60 days prior to the expiration.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies section 16-50j-73 for construction that constitutes an exempt modification pursuant to RCSA section 16-50j-72(b)(2). In accordance with RCSA section 16-50j-73, a copy of this letter and attachments is being sent to the Honorable Shari Cantor, Mayor of West Hartford; Todd Dumais, the Town Planner; as well as to the Ten Thirty Tower Company, LLC, the tower owner, and to the Ten Thirty Tower Company, LLC, the property owner.

The planned modifications to the facility fall squarely within those activities expressly provided for in RCSA section 50j-72(b)(2).

1. The proposed modifications will not result in an increase in height of the existing structure.
2. The proposed modifications will not require an extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that will exceed state and local limits.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, AT&T Wireless respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under RCSA section 16-50j-72(b)(2).

Respectfully submitted,



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o/b/o AT&T Wireless  
10130 Donleigh Drive  
Columbia, MD 21046  
443-286-4007  
[jandrews@empiretelecomm.com](mailto:jandrews@empiretelecomm.com)

Enclosures

cc: Honorable Shari Cantor, Mayor of West Hartford  
Todd Dumais, West Hartford Town Planner  
Ten Thirty Company, LLC, the tower owner and property owner.

April 18, 2018

Ten Thirty Tower Company, LLC, by Hirschfield Management, Inc.  
1030 New Britain Ave.  
West Hartford, CT 06110  
ATTN: Ian Ormesher

RE: AT&T Wireless Modifications to Telecommunication Facility –  
1030 NEW BRITAIN AVENUE, WEST HARTFORD, CT 06110

Dear Mr. Ormesher:

In order to accommodate technological changes, implement the Uniform Mobile Telecommunications System and enhance system performance in the State of Connecticut, AT&T Wireless ("AT&T") will be changing its equipment configuration at the above referenced telecommunications facility. AT&T Wireless currently maintains 9 antennas at the 180-foot level of an existing 185-foot lattice tower located at 1030 New Britain Avenue, in West Hartford, CT. The tower is owned by the Ten Thirty Company, LLC. The property is owned by the Ten Thirty Company, LLC.

AT&T Wireless now seeks to install 3 additional antennas at the 180-foot level of the tower, as well as replace 3 existing Remote Radio Units ("RRU") with 3 new RRUS-32 B2 RRUs; install 3 new RRUS-B14 4478 RRUs; install 3 new RRUS-32 B66 RRUs; replace existing GSM line components with low band combiners; and install a single new surge suppressor, all at the 180-foot level of the tower. In addition, the applicant seeks to install 2 new DC power cables along the existing cable route on the side of the tower. AT&T also intends to install 3 new RRUS-E2 and 3 new RRU-12 units at grade on the existing mounting pipes. Five (5) equipment cabinets are currently on grade, 1 cabinet will be decommissioned. AT&T will replace 2 DUS with 2 5216 units and replace the IDL2 with an IDLE and add a second XMU within one of the existing at-grade cabinets.

This letter is intended to serve as the required notice to the tower owner and the property owner. As required by the Regulations of Connecticut State Agencies ("RCSA") section 16-50j-73, the Connecticut Siting Council ("CSC") has been notified of the proposed changes and will review AT&T's proposal. Please accept this letter as notification under RCSA section 16-50j-73 of construction which constitutes an exempt modification pursuant to RCSA section 16-50j-72(b)(2).

The enclosed letter and documents to the CSC fully describes AT&T's proposal for the above referenced site. However, if you have any questions or require any additional information concerning our plans or the CSC procedures, please contact me at 443-286-4006 or contact Melanie Bachman, Acting Executive Director of the CSC at 860-872-2935.

Respectfully submitted,



Jack Andrews  
Zoning Manager, Empire Telecom  
o/b/o AT&T Wireless  
10130 Donleigh Drive  
Columbia, MD 21046  
443-677-0144  
[jandrews@empiretelecomm.com](mailto:jandrews@empiretelecomm.com)

Enclosures

cc: Melanie Bachman, Connecticut Siting Council

April 18, 2018

Todd Dumais  
Town Hall, 50 South Main Street, Room 214  
West Hartford, CT 06107

RE: AT&T Wireless Modifications to Telecommunication Facility –  
1030 NEW BRITAIN AVENUE, WEST HARTFORD, CT 06110

Dear Mr. Dumais:

In order to accommodate technological changes, implement the Uniform Mobile Telecommunications System and enhance system performance in the State of Connecticut, AT&T Wireless ("AT&T") will be changing its equipment configuration at the above referenced telecommunication facility. AT&T Wireless currently maintains 9 antennas at the 180-foot level of an existing 185-foot lattice tower located at 1030 New Britain Avenue, in West Hartford, CT. The tower is owned by the Ten Thirty Company, LLC. The property is owned by the Ten Thirty Company, LLC.

AT&T Wireless now seeks to install 3 additional antennas at the 180-foot level of the tower, as well as replace 3 existing Remote Radio Units ("RRU") with 3 new RRUS-32 B2 RRUs; install 3 new RRUS-B14 4478 RRUs; install 3 new RRUS-32 B66 RRUs; replace existing GSM line components with low band combiners; and install a single new surge suppressor, all at the 180-foot level of the tower. In addition, the applicant seeks to install 2 new DC power cables along the existing cable route on the side of the tower. AT&T also intends to install 3 new RRUS-E2 and 3 new RRU-12 units at grade on the existing mounting pipes. Five (5) equipment cabinets are currently on grade, 1 cabinet will be decommissioned. AT&T will replace 2 DUS with 2 5216 units and replace the IDL2 with an IDLE and add a second XMU within one of the existing at-grade cabinets.

This letter is intended to serve as notice to the chief of planning for the municipality. As required by the Regulations of Connecticut State Agencies ("RCSA") section 16-50j-73, the Connecticut Siting Council ("CSC") has been notified of the proposed changes and will review AT&T's proposal. Please accept this letter as notification under RCSA section 16-50j-73 of construction which constitutes an exempt modification pursuant to RCSA section 16-50j-72(b)(2).

The enclosed letter and documents to the CSC fully describes AT&T's proposal for the above referenced site. However, if you have any questions or require any additional information concerning our plans or the CSC procedures, please contact me at 443-677-0144 or contact Melanie Bachman, Acting Executive Director of the CSC at 860-872-2935.

Respectfully submitted,



Jack Andrews  
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Enclosures

cc: Melanie Bachman, Connecticut Siting Council

April 18, 2018

The Honorable Shari Cantor  
Town Hall, 50 South Main Street  
West Hartford, CT 06107

RE: AT&T Wireless Modifications to Telecommunication Facility –  
1030 NEW BRITAIN AVENUE, WEST HARTFORD, CT 06110

Dear Mayor Cantor:

In order to accommodate technological changes, implement the Uniform Mobile Telecommunications System and enhance system performance in the State of Connecticut, AT&T Wireless ("AT&T") will be changing its equipment configuration at the above referenced telecommunications facility. AT&T Wireless currently maintains 9 antennas at the 180-foot level of an existing 185-foot lattice tower located at 1030 New Britain Avenue, in West Hartford, CT. The tower is owned by the Ten Thirty Company, LLC. The property is owned by the Ten Thirty Company, LLC.

AT&T Wireless now seeks to install 3 additional antennas at the 180-foot level of the tower, as well as replace 3 existing Remote Radio Units ("RRU") with 3 new RRUS-32 B2 RRUs; install 3 new RRUS-B14 4478 RRUs; install 3 new RRUS-32 B66 RRUs; replace existing GSM line components with low band combiners; and install a single new surge suppressor, all at the 180-foot level of the tower. In addition, the applicant seeks to install 2 new DC power cables along the existing cable route on the side of the tower. AT&T also intends to install 3 new RRUS-E2 and 3 new RRU-12 units at grade on the existing mounting pipes. Five (5) equipment cabinets are currently on grade, 1 cabinet will be decommissioned. AT&T will replace 2 DUS with 2 5216 units and replace the IDL2 with an IDLE and add a second XMU within one of the existing at-grade cabinets.

This letter is intended to serve as the required notice to the chief elected official of the municipality. As required by the Regulations of Connecticut State Agencies ("RCSA") section 16-50j-73, the Connecticut Siting Council ("CSC") has been notified of the proposed changes and will review AT&T's proposal. Please accept this letter as notification under RCSA section 16-50j-73 of construction which constitutes an exempt modification pursuant to RCSA section 16-50j-72(b)(2).

The enclosed letter and documents to the CSC fully describes AT&T's proposal for the above referenced site. However, if you have any questions or require any additional information concerning our plans or the CSC procedures, please contact me at 443-677-0144 or contact Melanie Bachman, Acting Executive Director of the CSC at 860-872-2935.

Respectfully submitted,



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jandrews@empiretelecomm.com

Enclosures

cc: Melanie Bachman, Connecticut Siting Council





# Radio Frequency Emissions Analysis Report

AT&T Existing Facility

Site ID: CT5259

FA: 10071358

Hartford - Elmwood  
1030 New Britain Avenue  
West Hartford, CT 06110

**February 1, 2018**

**Centerline Communications Project Number: 950006-092**

Site Compliance Summary	
Compliance Status:	<b>COMPLIANT</b>
Site total MPE% of FCC general population allowable limit:	<b>7.00 %</b>



February 1, 2018

AT&T Mobility – New England  
Attn: John Benedetto, RF Manager  
550 Cochituate Road  
Suite 550 – 13&14  
Framingham, MA 06040

### Emissions Analysis for Site: **CT5259 – Hartford - Elmwood**

Centerline Communications, LLC (“Centerline”) was directed to analyze the proposed AT&T facility located at **1030 New Britain Avenue, West Hartford, CT**, for the purpose of determining whether the emissions from the Proposed AT&T Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limits for the 700 and 850 MHz Bands are approximately  $467 \mu\text{W}/\text{cm}^2$  and  $567 \mu\text{W}/\text{cm}^2$  respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 2300 MHz (WCS) bands is  $1000 \mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.



## CALCULATIONS

Calculations were performed for the proposed AT&T Wireless antenna facility located at **1030 New Britain Avenue, West Hartford, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since AT&T is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in *Table 1*:

Technology	Frequency Band	Channel Count	Transmit Power per Channel (W)
UMTS – Antenna 1	850 MHz	1	30
LTE – Antenna 2	700 MHz	2	60
LTE – Antenna 2	850 MHz	2	30
LTE – Antenna 2	2300 MHz (WCS)	4	30
LTE – Antenna 3	700 MHz (Band 14)	4	40
LTE – Antenna 3	2100 MHz (AWS)	4	30
LTE – Antenna 4	700 MHz	2	60
LTE – Antenna 4	1900 MHz (PCS)	4	80

*Table 1: Channel Data Table (per sector)*

The following antennas listed in *Table 2* were used in the modeling for transmission in the 700 MHz, 850 MHz, 1900 MHz (PCS), 2100 MHz (AWS) and 2300 MHz (WCS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

Sector	Antenna Number	Antenna Make / Model	Antenna Centerline (ft)
A	1	Powerwave 7770	180
A	2	CCI OPA-65R-LCUU-H6	180
A	3	Kathrein 800-10965	180
A	4	CCI OPA-65R-LCUU-H6	180
B	1	Powerwave 7770	180
B	2	CCI OPA-65R-LCUU-H6	180
B	3	Kathrein 800-10965	180
B	4	CCI OPA-65R-LCUU-H6	180
C	1	Powerwave 7770	180
C	2	CCI OPA-65R-LCUU-H6	180
C	3	Kathrein 800-10965	180
C	4	CCI OPA-65R-LCUU-H6	180

*Table 2: Antenna Data*

All calculations were done with respect to uncontrolled / general population threshold limits.



## RESULTS

Per the calculations completed for the proposed AT&T configurations *Table 3* shows resulting emissions power levels and percentages of the FCC’s allowable general population limit.

Antenna ID	Antenna Make / Model	Frequency Bands	Antenna Gain (dBd)	Channel Count	Total TX Power (W)	ERP (W)	MPE %
Antenna A1	Powerwave 7770	850 MHz	11.4	1	30	414.12	0.09
Antenna A2	CCI OPA-65R-LCUU-H6	700 MHz / 850 MHz / 2300 MHz (WCS)	11.65 / 12.45 / 15.45	8	300	7,018.39	1.17
Antenna A3	Kathrein 800-10965	700 MHz / 2100 MHz (AWS)	12.65 / 16.15	8	280	7,890.41	1.34
Antenna A4	CCI OPA-65R-LCUU-H6	700 MHz / 1900 MHz (PCS)	11.65 / 14.85	6	440	11,530.36	1.61
Sector A Composite MPE%							<b>4.20</b>
Antenna B1	Powerwave 7770	850 MHz	11.4	1	30	414.12	0.09
Antenna B2	CCI OPA-65R-LCUU-H6	700 MHz / 850 MHz / 2300 MHz (WCS)	11.65 / 12.45 / 15.45	8	300	7,018.39	1.17
Antenna B3	Kathrein 800-10965	700 MHz / 2100 MHz (AWS)	12.65 / 16.15	8	280	7,890.41	1.34
Antenna B4	CCI OPA-65R-LCUU-H6	700 MHz / 1900 MHz (PCS)	11.65 / 14.85	6	440	11,530.36	1.61
Sector B Composite MPE%							<b>4.20</b>
Antenna C1	Powerwave 7770	850 MHz	11.4	1	30	414.12	0.09
Antenna C2	CCI OPA-65R-LCUU-H6	700 MHz / 850 MHz / 2300 MHz (WCS)	11.65 / 12.45 / 15.45	8	300	7,018.39	1.17
Antenna C3	Kathrein 800-10965	700 MHz / 2100 MHz (AWS)	12.65 / 16.15	8	280	7,890.41	1.34
Antenna C4	CCI OPA-65R-LCUU-H6	700 MHz / 1900 MHz (PCS)	11.65 / 14.85	6	440	11,530.36	1.61
Sector C Composite MPE%							<b>4.20</b>

*Table 3: AT&T Emissions Levels*



The Following table (*table 4*) shows all additional carriers on site and their MPE% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum AT&T MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, all three sectors have the same configuration yielding the same results on all three sectors. *Table 5* below shows a summary for each AT&T Sector as well as the composite MPE value for the site.

<b>Site Composite MPE%</b>	
<b>Carrier</b>	<b>MPE%</b>
AT&T – Max Sector Value	<b>4.20 %</b>
T-Mobile	2.45 %
Clearwire	0.08 %
Nextel	0.27 %
<b>Site Total MPE %:</b>	<b>7.00 %</b>

*Table 4: All Carrier MPE Contributions*

AT&T Sector A Total:	4.20 %
AT&T Sector B Total:	4.20 %
AT&T Sector C Total:	4.20 %
<b>Site Total:</b>	<b>7.00 %</b>

*Table 5: Site MPE Summary*



FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. *Table 6* below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated AT&T sector(s). For this site, all three sectors have the same configuration yielding the same results on all three sectors.

AT&T _ Frequency Band / Technology (Per Sector)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ( $\mu\text{W}/\text{cm}^2$ )	Frequency (MHz)	Allowable MPE ( $\mu\text{W}/\text{cm}^2$ )	Calculated % MPE
AT&T 850 MHz UMTS	1	414.12	180	0.49	850 MHz	567	0.09%
AT&T 700 MHz LTE	2	877.31	180	2.08	700 MHz	467	0.45%
AT&T 850 MHz LTE	2	527.38	180	1.25	850 MHz	567	0.22%
AT&T 2300 MHz (WCS) LTE	4	1,052.26	180	5.00	2300 MHz (WCS)	1000	0.50%
AT&T 700 MHz LTE	4	736.31	180	3.50	700 MHz	467	0.75%
AT&T 2100 MHz (AWS) LTE	4	1,236.29	180	5.87	2100 MHz (AWS)	1000	0.59%
AT&T 700 MHz LTE	2	877.31	180	2.08	700 MHz	467	0.45%
AT&T 1900 MHz (PCS) LTE	4	2,443.94	180	11.61	1900 MHz (PCS)	1000	1.16%
						<b>Total:</b>	<b>4.20%</b>

*Table 6: AT&T Maximum Sector MPE Power Values*





## Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the AT&T facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

AT&T Sector	Power Density Value (%)
Sector A:	4.20 %
Sector B:	4.20 %
Sector C:	4.20 %
AT&T Maximum Total (per sector):	4.20 %
Site Total:	7.00 %
Site Compliance Status:	<b>COMPLIANT</b>

The anticipated composite MPE value for this site assuming all carriers present is **7.00 %** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

A handwritten signature in black ink, appearing to read 'Scott Heffernan', is positioned above the contact information.

Scott Heffernan  
RF Engineering Director  
**Centerline Communications, LLC**  
95 Ryan Drive, Suite 1  
Raynham, MA 02767



**SITE NAME: WEST HARTFORD-ELMWOOD**  
**PROJECT: LTE - 4C/5C/6C/7C/RETROFIT**  
**FA NUMBER: 10071358**  
**SITE NUMBER: CTL05259**  
**1030 NEW BRITAIN AVENUE**  
**WEST HARTFORD, CT 06110**  
**HARTFORD COUNTY**  
**FIRSTNET**



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NEW CINGULAR WIRELESS PCS, LLC  
 550 COCHITUATE ROAD  
 FRAMINGHAM, MA 01701



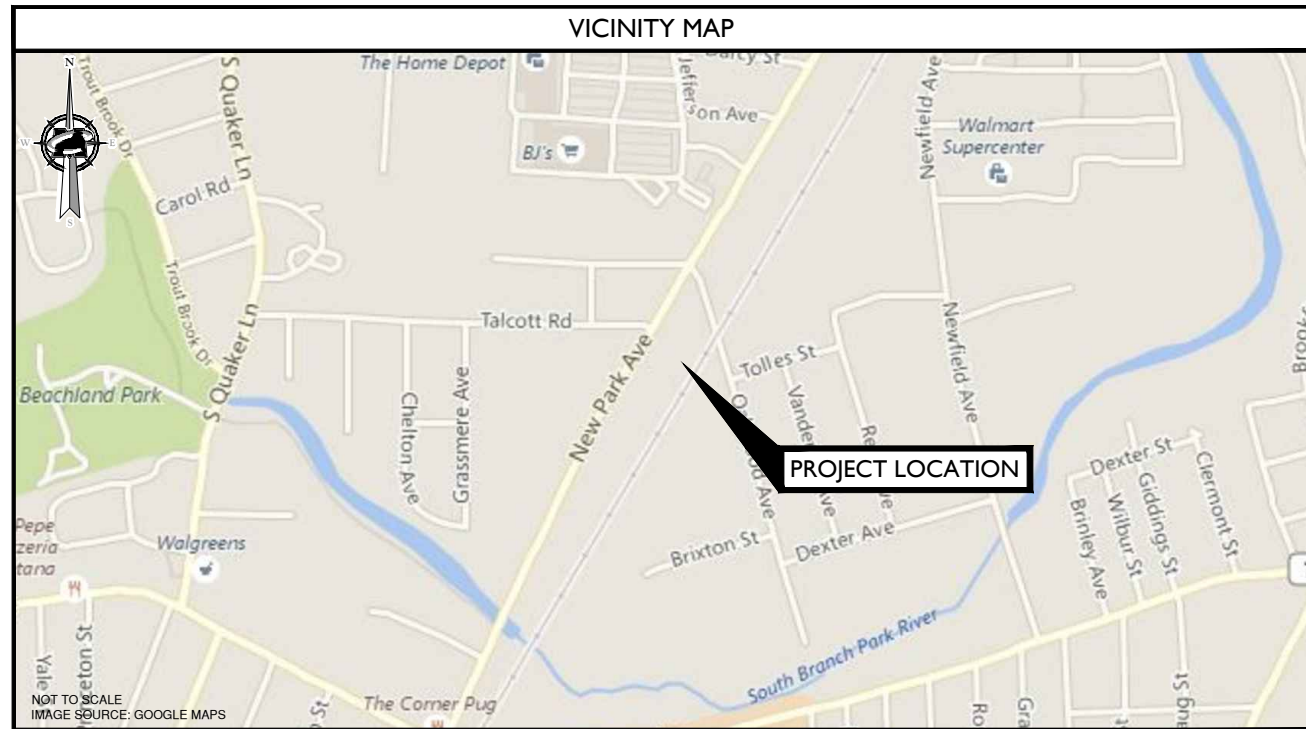
16 ESQUIRE ROAD  
 BILLERICA, MA 01862



**PROTECT YOURSELF**  
 ALL STATES REQUIRE NOTIFICATION OF EXCAVATORS, DESIGNERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.  
 Know what's below. Call before you dig.  
 FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

PROJECT TEAM	
<b>CLIENT REPRESENTATIVE</b>	
COMPANY:	EMPIRE TELECOM
ADDRESS:	16 ESQUIRE ROAD
CITY, STATE, ZIP:	BILLERICA, MA 01862
CONTACT:	DAVID COOPER
E-MAIL:	DCOOPER@EMPIRETEL.COM
<b>ENGINEER</b>	
COMPANY:	MASER CONSULTING CONNECTICUT
ADDRESS:	331 NEWMAN SPRINGS ROAD, SUITE 203
CITY, STATE, ZIP:	RED BANK, NJ 07701
CONTACT:	MICHAEL CLEARY
PHONE:	(856) 717-0412 x4105
E-MAIL:	MCCLEARY@MASERCONSULTING.COM
<b>RF ENGINEER</b>	
COMPANY:	NEW CINGULAR WIRELESS PCS, LLC
ADDRESS:	550 COCHITUATE ROAD
CITY, STATE, ZIP:	FRAMINGHAM, MA 01701
CONTACT:	MUHAMMAD MINHAJ HUSSAIN
E-MAIL:	MH705R@ATT.COM

SITE INFORMATION	
<b>APPLICANT/LESSEE</b>	
NEW CINGULAR WIRELESS PCS, LLC 550 COCHITUATE RD. FRAMINGHAM, MA 01701	
<b>TOWER OWNER:</b>	
NAME:	TEN THIRTY TOWER COMPANY, LLC
ADDRESS:	1030 NEW BRITAIN AVENUE
CITY, STATE, ZIP:	WEST HARTFORD, CT 06110
LATITUDE:	41.7360919° N
LONGITUDE:	72.7204989° W
LAT/LONG. TYPE:	NAD 83
AREA OF CONSTRUCTION:	EXISTING OUTDOOR EQUIPMENT AND LATTICE TOWER
ZONING/JURISDICTION:	CITY OF WEST HARTFORD
CURRENT USE/PROPOSED USE:	UNMANNED TELECOMMUNICATIONS FACILITY
HANDICAP REQUIREMENTS:	FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION. HANDICAPPED ACCESS NOT REQUIRED.
CONSTRUCTION TYPE:	IIB
USE GROUP:	U



**DRIVING DIRECTIONS**

DIRECTIONS FROM AT&T OFFICE AT 550 COCHITUATE ROAD, FRAMINGHAM, MA:  
 DEPART RT-30 WEST/COCHITUATE ROAD TOWARD BURR STREET. TURN BACK ON RT-30 EAST/COCHITUATE ROAD. TAKE RAMP RIGHT FOR I-90 WEST TOWARD SPRINGFIELD/WORCESTER. AT EXIT 9, TAKE RAMP RIGHT FOR I-84 TOWARD HARTFORD/NEW YORK CITY. AT EXIT 45, TAKE RAMP LEFT AND FOLLOW SIGNS FOR FLATBUSH AVENUE. TURN RIGHT ONTO FLATBUSH AVENUE. TURN LEFT ONTO NEW PARK AVENUE. TURN LEFT ONTO OAKWOOD AVENUE.

CODE COMPLIANCE	
ALL WORK AND MATERIALS SHALL BE PERFORMED AND INSTALLED IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THE LATEST EDITIONS OF THE FOLLOWING CODES.	
1. 2016 CONNECTICUT STATE BUILDING CODE, INCORPORATING THE 2012 IBC	7. EIA/TIA-222 REVISION G
2. 2014 NATIONAL ELECTRICAL CODE-NFPA 70	8. TIA 607 FOR GROUNDING
3. 2012 NFPA 101	9. INSTITUTE FOR ELECTRICAL AND ELECTRONICS ENGINEERS 81
4. LIGHTNING PROTECTION CODE 2011	10. IEEE C2 LATEST EDITION
5. AMERICAN CONCRETE INSTITUTE 318	11. TELCORDIA GR-1275
6. AMERICAN INSTITUTE OF STEEL CONSTRUCTION 360-10	12. ANSI T1.311

GENERAL CONTRACTOR NOTES	
<b>DO NOT SCALE DRAWINGS</b>	
CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE ARCHITECT/ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.	

GENERAL NOTES	
THE FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION. A TECHNICIAN WILL VISIT THE SITE AS REQUIRED FOR ROUTINE MAINTENANCE. THE PROJECT WILL NOT RESULT IN ANY SIGNIFICANT DISTURBANCE OR EFFECT ON DRAINAGE; NO SANITARY SEWER SERVICE, POTABLE WATER, OR TRASH DISPOSAL IS REQUIRED AND NO COMMERCIAL SIGNAGE IS PROPOSED.	

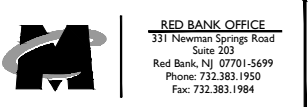
SHEET	DESCRIPTION
T-1	TITLE SHEET
GN-1	GENERAL NOTES
A-1	COMPOUND AND EQUIPMENT PLAN
A-2	ELEVATION VIEW, DETAILS AND ANTENNA SCHEDULE
A-3	ANTENNA LAYOUTS
A-4	DETAILS
A-5	DETAILS
A-6	DETAILS
A-7	RF PLUMBING DIAGRAMS
G-1	GROUNDING DETAILS

PROJECT DESCRIPTION/SCOPE OF WORK	
THIS PROJECT WILL BE COMPRISED OF:	
<ul style="list-style-type: none"> <li>INSTALL (3) NEW AT&amp;T ANTENNAS, (1) PER SECTOR</li> <li>INSTALL (3) NEW RRUS-E2 WITH SURGE ARRESTORS, AT GRADE</li> <li>INSTALL (3) NEW RRUS-12 WITH SURGE ARRESTORS, AT GRADE</li> <li>(3) NEW RRUS-32 B2 TO REPLACE (3) EXISTING RRUS12+A2, (1) PER SECTOR</li> <li>INSTALL (3) NEW RRUS-B14 4478, (1) PER SECTOR</li> <li>INSTALL (3) NEW RRUS-32 B66, (1) PER SECTOR</li> <li>INSTALL (1) NEW DC-6 SURGE SUPPRESSION DOME</li> <li>INSTALL (2) 6/C DC CABLES</li> <li>REMOVE EXISTING RX/AT</li> <li>REPLACE EXISTING GSM LINE COMPONENTS WITH LOW BAND COMBINERS</li> <li>REPLACE (2) DUS WITH (2) 5216</li> <li>REPLACE IDL2 WITH IDL6 AND ADD 2ND XMU</li> </ul>	

SCALE:	JOB NUMBER:
AS SHOWN	17963019A



**SITE NAME:**  
 WEST HARTFORD-ELMWOOD  
 FA#:10071358  
 SITE #: CTL05259  
 1030 NEW BRITAIN AVENUE  
 WEST HARTFORD, CT 06110  
 HARTFORD COUNTY



SHEET TITLE:	TITLE SHEET
SHEET NUMBER:	T-1

**GENERAL NOTES:**

1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GESS) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 50 HNS OR LESS.
4. THE SUBCONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENCING GROUNDING AND UNDERGROUND CONDUIT INSTALLATION AS TO PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO THE CONDUIT.
5. METAL CONDUIT AND TRAY SHALL BE GROUNDED AND MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH #6 AWG COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
6. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.
7. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE EQUIPMENT GROUND RING WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS; 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
8. CONNECTIONS TO THE GROUND BUS SHALL NOT BE DOUBLED UP OR STACKED. BACK TO BACK CONNECTIONS ON OPPOSITE SIDES OF THE GROUND BUS ARE PERMITTED.
9. ALL EXTERIOR GROUND CONDUCTORS BETWEEN EQUIPMENT/GROUND BARS AND THE GROUND RING, SHALL BE #2 AWG SOLID TINNED COPPER UNLESS OTHERWISE INDICATED.
10. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
11. USE OF 90° BENDS IN THE PROTECTION GROUNDING CONDUCTORS SHALL BE AVOIDED WHEN 45° BENDS CAN BE ADEQUATELY SUPPORTED. ALL BENDS SHALL BE MADE WITH 12" RADIUS OR LARGER.
12. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
13. ALL GROUND CONNECTIONS ABOVE GRADE (INTERIOR) SHALL BE FORMED USING HIGH PRESS CRIMPS EXCEPT FOR GROUND BAR CONNECTION FROM MGB TO OUTSIDE EXTERIOR GROUND SHALL ALL BE CADWELD CONNECTIONS.
14. COMPRESSION GROUND CONNECTIONS MAY BE REPLACED BY EXOTHERMIC WELD CONNECTIONS.
15. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED TO THE TOWER GROUND BAR.
16. APPROVED ANTIOXIDANT COATINGS (I.E. CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
17. ALL EXTERIOR AND INTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERIAL.
18. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
19. BOND ALL METALLIC OBJECTS WITHIN 6 FT OF MAIN GROUND WIRES WITH 1-#2 AWG TIN-PLATED COPPER GROUND CONDUCTOR.
20. GROUND CONDUCTORS USED IN THE FACILITY GROUND AND LIGHTNING PROTECTION SYSTEMS SHALL NOT BE ROUTED THROUGH METALLIC OBJECTS THAT FORM A RING AROUND THE CONDUCTOR, SUCH AS METALLIC CONDUITS, METAL SUPPORT CLIPS OR SLEEVES THROUGH WALLS OR FLOORS. WHEN IT IS REQUIRED TO BE HOUSED IN CONDUIT TO MEET CODE REQUIREMENTS OR LOCAL CONDITIONS, NON-METALLIC MATERIAL SUCH AS PVC PLASTIC CONDUIT SHALL BE USED. WHERE USE OF METAL CONDUIT IS UNAVOIDABLE (E.G. NON-METALLIC CONDUIT PROHIBITED BY LOCAL CODE) THE GROUND CONDUCTOR SHALL BE BONDED TO EACH END OF THE METAL CONDUIT.
21. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/4" IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50.
22. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:  
 CONTRACTOR - EMPIRE TELECOM  
 SUBCONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION)  
 OWNER - AT&T (NEW CINGULAR WIRELESS PCS, LLC)
23. ALL SITE WORK SHALL BE COMPLETED AS INDICATED ON THE DRAWINGS AND PROJECT SPECIFICATIONS.
24. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
25. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK.
26. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.

27. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
28. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
29. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
30. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
31. THE SUBCONTRACTOR SHALL CONTACT UTILITY LOCATING SERVICES PRIOR TO THE START OF CONSTRUCTION.
32. ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC, AND OTHER UTILITIES WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES, AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SHALL BE RELOCATED AS DIRECTED BY THE RESPONSIBLE ENGINEER. EXTREME CAUTION SHOULD BE USED BY THE SUBCONTRACTOR WHEN EXCAVATING OR DRILLING PIERS AROUND OR NEAR UTILITIES. SUBCONTRACTOR SHALL PROVIDE SAFETY TRAINING FOR THE WORKING CREW. THIS WILL INCLUDE BUT NOT BE LIMITED TO A) FALL PROTECTION B) CONFINED SPACE C) ELECTRICAL SAFETY D) TRENCHING & EXCAVATION.
33. ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES, WHICH INTERFERE WITH THE EXECUTION OF THE WORK, SHALL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, AS DIRECTED BY THE RESPONSIBLE ENGINEER, AND SUBJECT TO THE APPROVAL OF THE OWNER AND/OR LOCAL UTILITIES.
34. THE AREAS OF THE OWNER'S PROPERTY DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUIPMENT OR DRIVEWAY SHALL BE GRADED TO A UNIFORM SLOPE AND STABILIZED TO PREVENT EROSION.
35. SUBCONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES, IF REQUIRED DURING CONSTRUCTION, SHALL BE IN CONFORMANCE WITH THE LOCAL GUIDELINES FOR EROSION AND SEDIMENT CONTROL.
36. NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OR EMBANKMENT.
37. THE SUBGRADE SHALL BE COMPACTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE APPLICATION.
38. THE SITE SHALL BE GRADED TO CAUSE SURFACE WATER TO FLOW AWAY FROM THE BTS EQUIPMENT AND TOWER AREAS.
39. IF NECESSARY, RUBBISH, STUMPS, DEBRIS, STICKS, STONES AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.
40. THE SUBCONTRACTOR SHALL PROVIDE SITE SIGNAGE IN ACCORDANCE WITH THE TECHNICAL SPECIFICATION FOR SITE SIGNAGE.
41. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
42. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF THE CONTRACTOR.
43. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND TI CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
44. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.
45. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS.
46. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
47. CONSTRUCTION SHALL COMPLY WITH SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T MOBILITY SITES."
48. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
49. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION, ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
50. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN ALERT OF DANGEROUS EXPOSURE LEVELS.

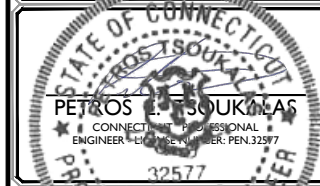


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SCALE:	JOB NUMBER:
AS SHOWN	17963019A

REV	DATE	DESCRIPTION	DRAWN BY	CHECKED BY
0	02/28/18	FOR CONSTRUCTION	AJC	PET
2	02/13/18	REVISED PER COMMENTS	AJC	PET
1	01/23/18	ISSUED FOR REVIEW	AJC	RA

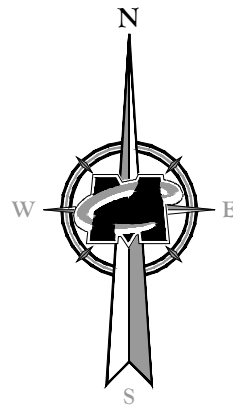


IT IS THE DUTY OF THE ENGINEER TO VERIFY THE ACCURACY OF THE INFORMATION PROVIDED TO HIM BY THE CLIENT AND TO BE RESPONSIBLE FOR THE DESIGN AND CONSTRUCTION OF THE PROJECT. THE ENGINEER SHALL BE RESPONSIBLE FOR THE DESIGN AND CONSTRUCTION OF THE PROJECT.

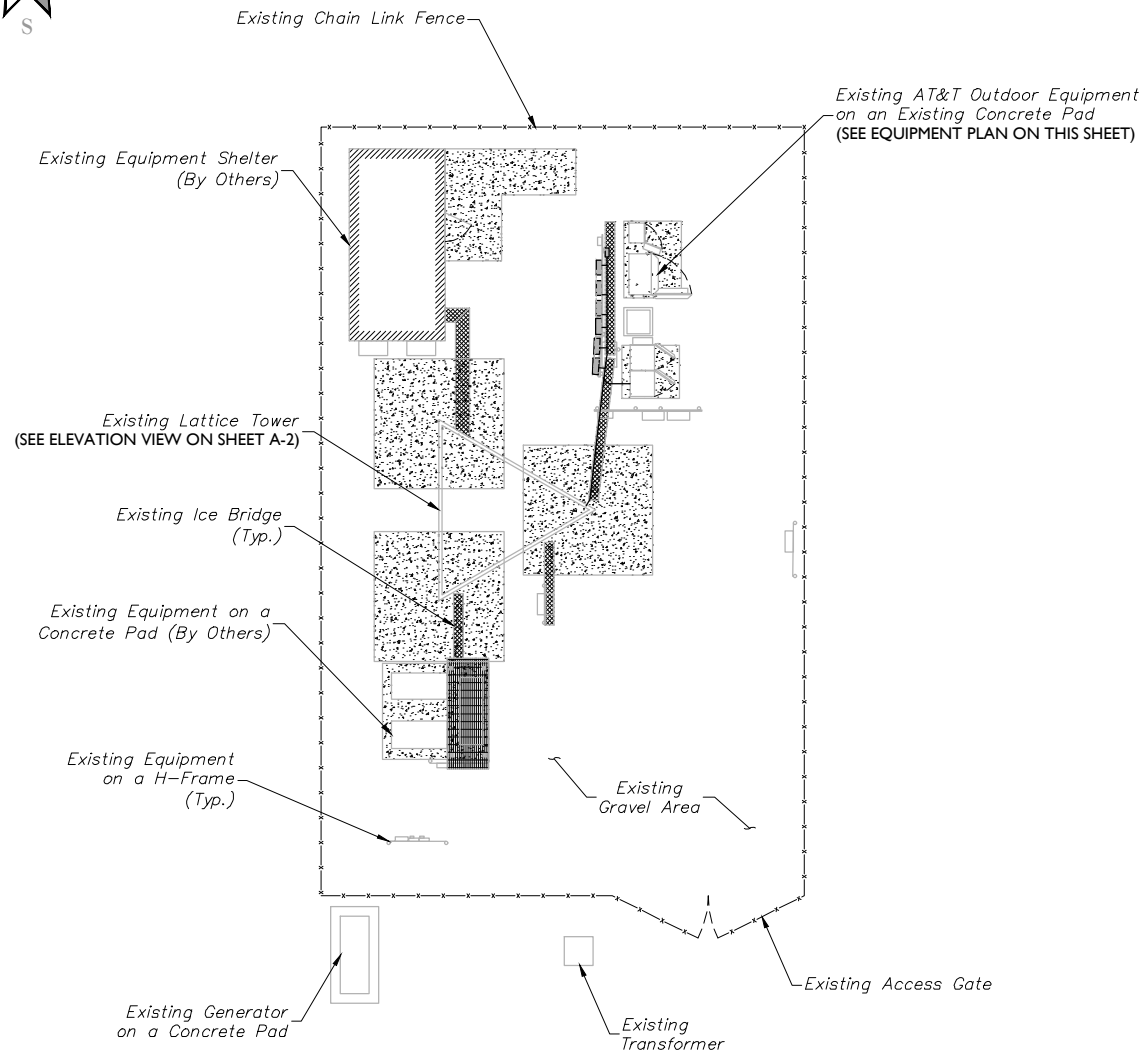
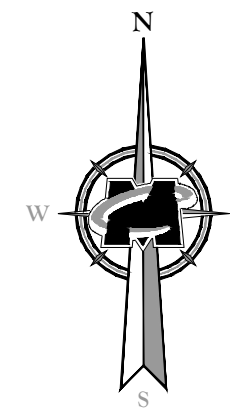
**SITE NAME:**  
 WEST HARTFORD-ELMWOOD  
 FA#:10071358  
 SITE #: CTL05259  
 1030 NEW BRITAIN AVENUE  
 WEST HARTFORD, CT 06110  
 HARTFORD COUNTY



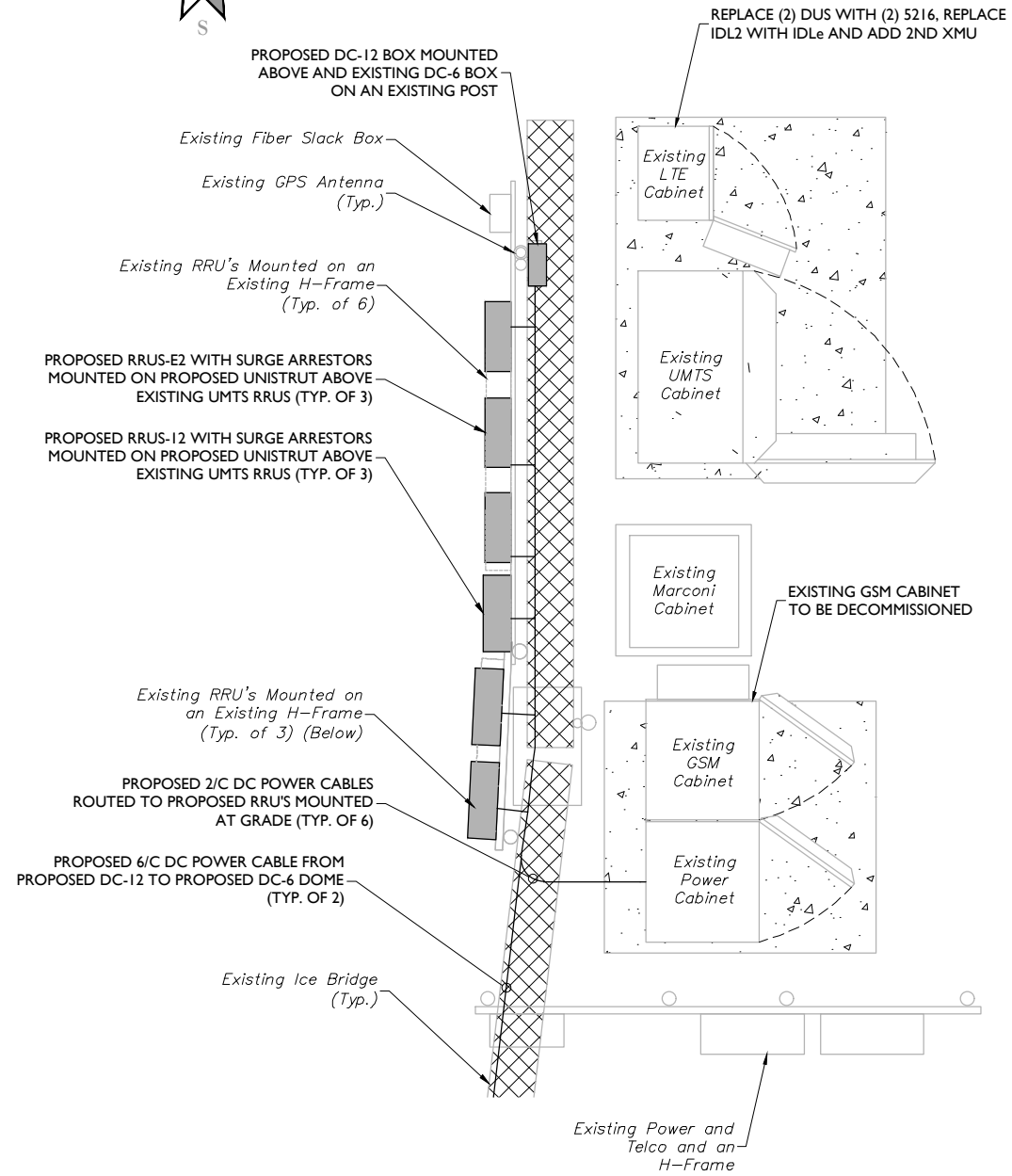
SHEET TITLE:  
**GENERAL NOTES**  
 SHEET NUMBER:  
**GN-1**



NOTE:  
 SITE INFORMATION OBTAINED FROM THE FOLLOWING:  
 A. PLAN ENTITLED "AVON - MONTEVIDEO ROAD" PREPARED BY COM EX CONSULTANTS, LAST REVISED 04/29/2016.



**COMPOUND PLAN**  
 GRAPHIC SCALE  
 (IN FEET)  
 SCALE: 1" = 10' FOR 24"x36" DRAWINGS  
 (DO NOT SCALE 11"x17" DRAWINGS)



**EQUIPMENT PLAN**  
 GRAPHIC SCALE  
 (IN FEET)  
 SCALE: 1" = 2' FOR 24"x36" DRAWINGS  
 (DO NOT SCALE 11"x17" DRAWINGS)

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**at&t**  
 NEW CINGULAR WIRELESS PCS, LLC  
 550 COCHITUATE ROAD  
 FRAMINGHAM, MA 01701

**EMPIRE telecom**  
 16 ESQUIRE ROAD  
 BILLERICA, MA 01862

**811** PROTECT YOURSELF  
 ALL STATES REQUIRE NOTIFICATION OF EXCAVATORS, DESIGNERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.  
 Know what's below. Call before you dig.  
 FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

SCALE	JOB NUMBER			
AS SHOWN	17963019A			
0	02/28/18	FOR CONSTRUCTION	AJC	PET
2	02/13/18	REVISED PER COMMENTS	AJC	PET
1	01/23/18	ISSUED FOR REVIEW	AJC	RA
REV	DATE	DESIGNED BY	DRAWN BY	CHECKED BY

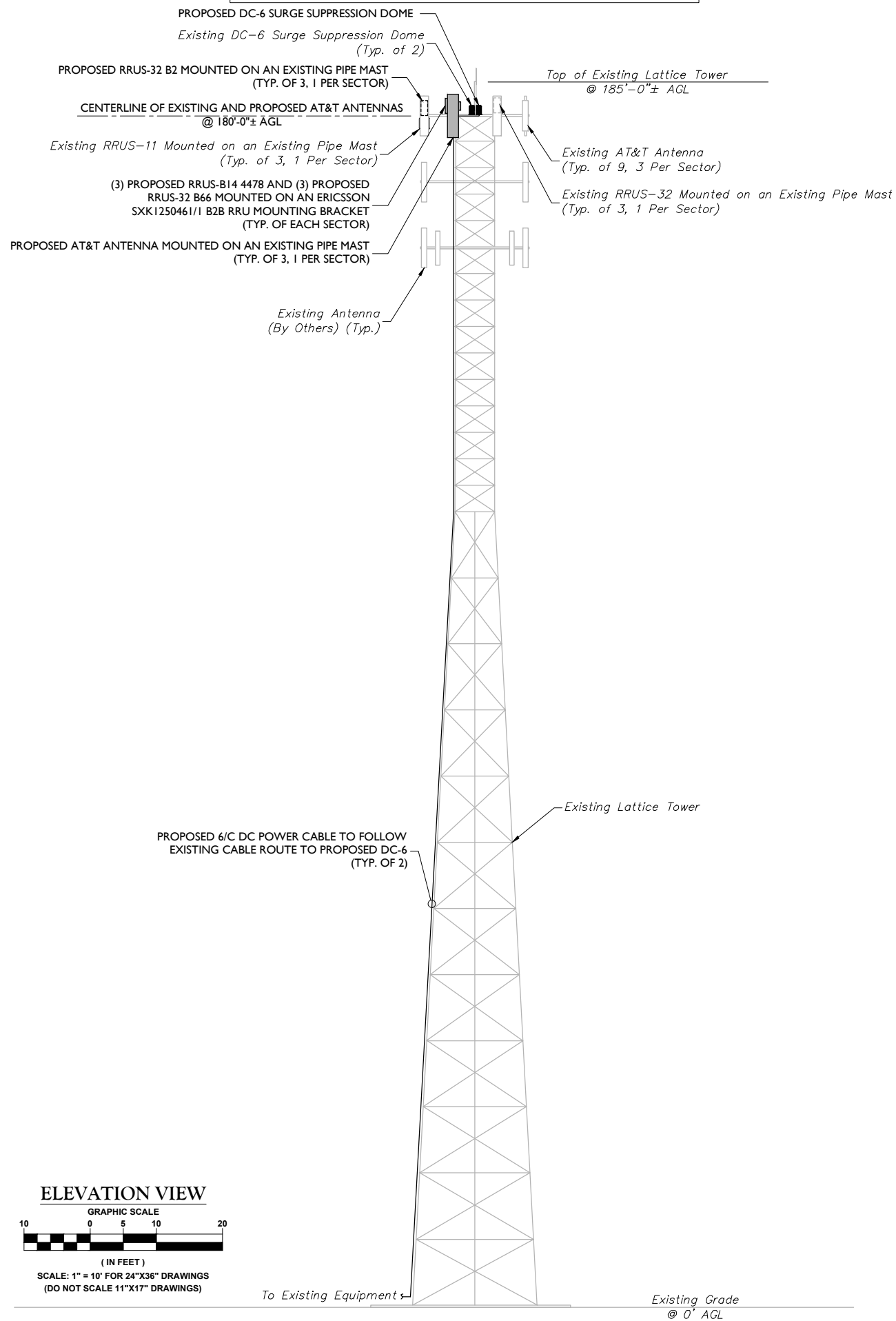
STATE OF CONNECTICUT  
**PETROS TSOUKALAS**  
 CONNECTICUT PROFESSIONAL ENGINEER - LICENSE NUMBER: PEN-32577  
 32577  
 IT IS THE DUTY OF THE ENGINEER TO EXERCISE HIS OR HER PROFESSIONAL SKILLS AND JUDGMENT IN THE PERFORMANCE OF HIS OR HER PROFESSIONAL SERVICES AND TO BE RESPONSIBLE FOR THE ACCURACY AND COMPLETENESS OF HIS OR HER WORK AND TO MAINTAIN THE INTEGRITY OF HIS OR HER PROFESSIONAL REPUTATION.

**SITE NAME:**  
 WEST HARTFORD-ELMWOOD  
 FA#:10071358  
 SITE #: CTL05259  
 1030 NEW BRITAIN AVENUE  
 WEST HARTFORD, CT 06110  
 HARTFORD COUNTY

**RED BANK OFFICE**  
 331 Newnam Springs Road  
 Suite 203  
 Red Bank, NJ 07701-5699  
 Phone: 732.383.1950  
 Fax: 732.383.1984

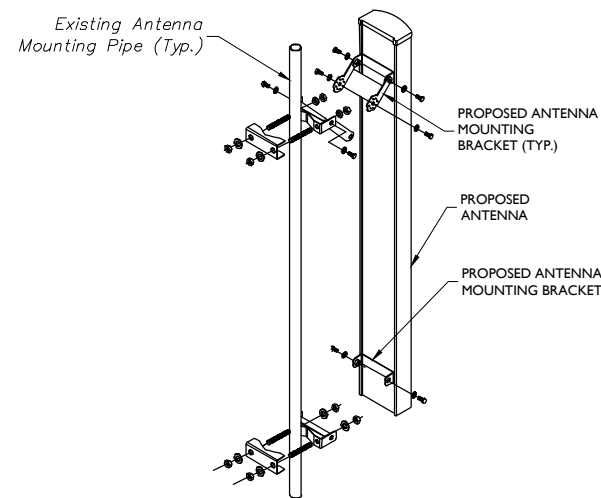
SHEET TITLE:  
**COMPOUND AND EQUIPMENT PLAN**  
 SHEET NUMBER:  
**A-1**

3 FEET MINIMUM SEPARATION BETWEEN LTE ANTENNAS  
6 FEET MINIMUM SEPARATION BETWEEN 700BC & 700 DE

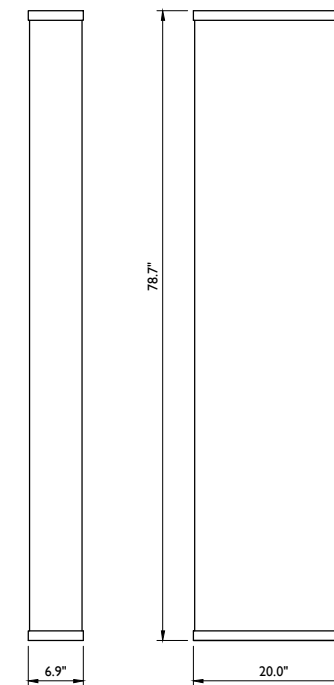


PROPOSED ANTENNA AND RRUS CONFIGURATION																
SECTOR	EXISTING ANTENNA CONFIGURATION	PROPOSED ANTENNA CONFIGURATION	TECHNOLOGY	ANTENNA STATUS	HEIGHT (ft)	WIDTH (ft)	DEPTH (ft)	WEIGHT (lbs)	ANTENNA AZIMUTH	ANT. CL. ELEV. (ft)	RRUS/TMA CONFIGURATION	STATUS	FEEDER #	FEEDER TYPE	FEEDER STATUS	
ALPHA	A1	Povernave 7770	Povernave 7770	UMTS	REMAIN	55.00	11.00	5.00	35.00	0°	180°	(2) LGP21401	-	2	1-56" COAX	REMAIN
	A2	CCI OPA-65R-LCUU-H6	CCI OPA-65R-LCUU-H6	LTE	REMAIN	72.00	14.80	7.40	73.00	0°	180°	(1) RRUS-32 (1) RRUS-E2 (AT GRADE) (1) RRUS-12 (AT GRADE)	REMAIN NEW NEW	2 1 2	1-56" COAX FIBER DC	REMAIN NEW NEW
	A3	-	Kathrein 800-10965	LTE	NEW	78.70	20.00	6.90	108.60	0°	180°	(1) RRUS-B14 4478 (1) RRUS-32 B66	NEW NEW		FIBER DC	REMAIN
	A4	CCI OPA-65R-LCUU-H6	CCI OPA-65R-LCUU-H6	LTE	REMAIN	72.00	14.80	7.40	73.00	0°	180°	(1) RRUS-11 (1) RRUS-32 B2	REMAIN NEW		FIBER DC	REMAIN
BETA	B1	Povernave 7770	Povernave 7770	UMTS	REMAIN	55.00	11.00	5.00	35.00	120°	180°	(2) LGP21401	-	2	1-56" COAX	REMAIN
	B2	CCI OPA-65R-LCUU-H6	CCI OPA-65R-LCUU-H6	LTE	REMAIN	72.00	14.80	7.40	73.00	120°	180°	(1) RRUS-32 (1) RRUS-E2 (AT GRADE) (1) RRUS-12 (AT GRADE)	REMAIN NEW NEW	2 1 2	1-56" COAX FIBER DC	REMAIN
	B3	-	Kathrein 800-10965	LTE	NEW	78.70	20.00	6.90	108.60	120°	180°	(1) RRUS-B14 4478 (1) RRUS-32 B66	NEW NEW		FIBER DC	REMAIN
	B4	CCI OPA-65R-LCUU-H6	CCI OPA-65R-LCUU-H6	LTE	REMAIN	72.00	14.80	7.40	73.00	120°	180°	(1) RRUS-11 (1) RRUS-32 B2	REMAIN NEW		FIBER DC	REMAIN
GAMMA	C1	Povernave 7770	Povernave 7770	UMTS	REMAIN	55.00	11.00	5.00	35.00	240°	180°	(2) LGP21401	-	2	1-56" COAX	REMAIN
	C2	CCI OPA-65R-LCUU-H6	CCI OPA-65R-LCUU-H6	LTE	REMAIN	72.00	14.80	7.40	73.00	240°	180°	(1) RRUS-32 (1) RRUS-E2 (AT GRADE) (1) RRUS-12 (AT GRADE)	REMAIN NEW NEW	2 1 2	1-56" COAX FIBER DC	REMAIN
	C3	-	Kathrein 800-10965	LTE	NEW	78.70	20.00	6.90	108.60	240°	180°	(1) RRUS-B14 4478 (1) RRUS-32 B66	NEW NEW		FIBER DC	REMAIN
	C4	CCI OPA-65R-LCUU-H6	CCI OPA-65R-LCUU-H6	LTE	REMAIN	72.00	14.80	7.40	73.00	240°	180°	(1) RRUS-11 (1) RRUS-32 B2	REMAIN NEW		FIBER DC	REMAIN

ANTENNA SCHEDULE



ANTENNA MOUNTING DETAIL  
NOT TO SCALE



WEIGHT = 108.6 LBS  
KATHREIN 800-10965  
ANTENNA DETAIL  
NOT TO SCALE

NOTE:  
SITE INFORMATION OBTAINED FROM THE FOLLOWING:  
A. PLAN ENTITLED "AVON - MONTEVIDEO ROAD" PREPARED BY COM EX CONSULTANTS, LAST REVISED 04/29/2016.

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FRAMINGHAM, MA 01701

**EMPIRE telecom**  
16 ESQUIRE ROAD  
BILLERICA, MA 01862

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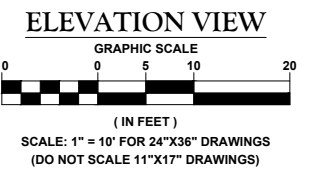
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REV	DATE	DESIGNED BY	CHECKED BY
0	02/28/18	FOR CONSTRUCTION	AJC PET
2	02/13/18	REVISED PER COMMENTS	AJC PET
1	01/23/18	ISSUED FOR REVIEW	AJC RA

STATE OF CONNECTICUT  
PETROS E. SOUKKILAS  
CONNECTICUT PROFESSIONAL ENGINEER LICENSE NUMBER: PEN.32577  
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SITE NAME:  
WEST HARTFORD-ELMWOOD  
FA#: 10071358  
SITE #: CTL05259  
1030 NEW BRITAIN AVENUE  
WEST HARTFORD, CT 06110  
HARTFORD COUNTY

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SHEET TITLE:  
ELEVATION VIEW, DETAILS AND ANTENNA SCHEDULE  
SHEET NUMBER:  
A-2





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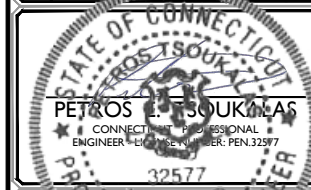


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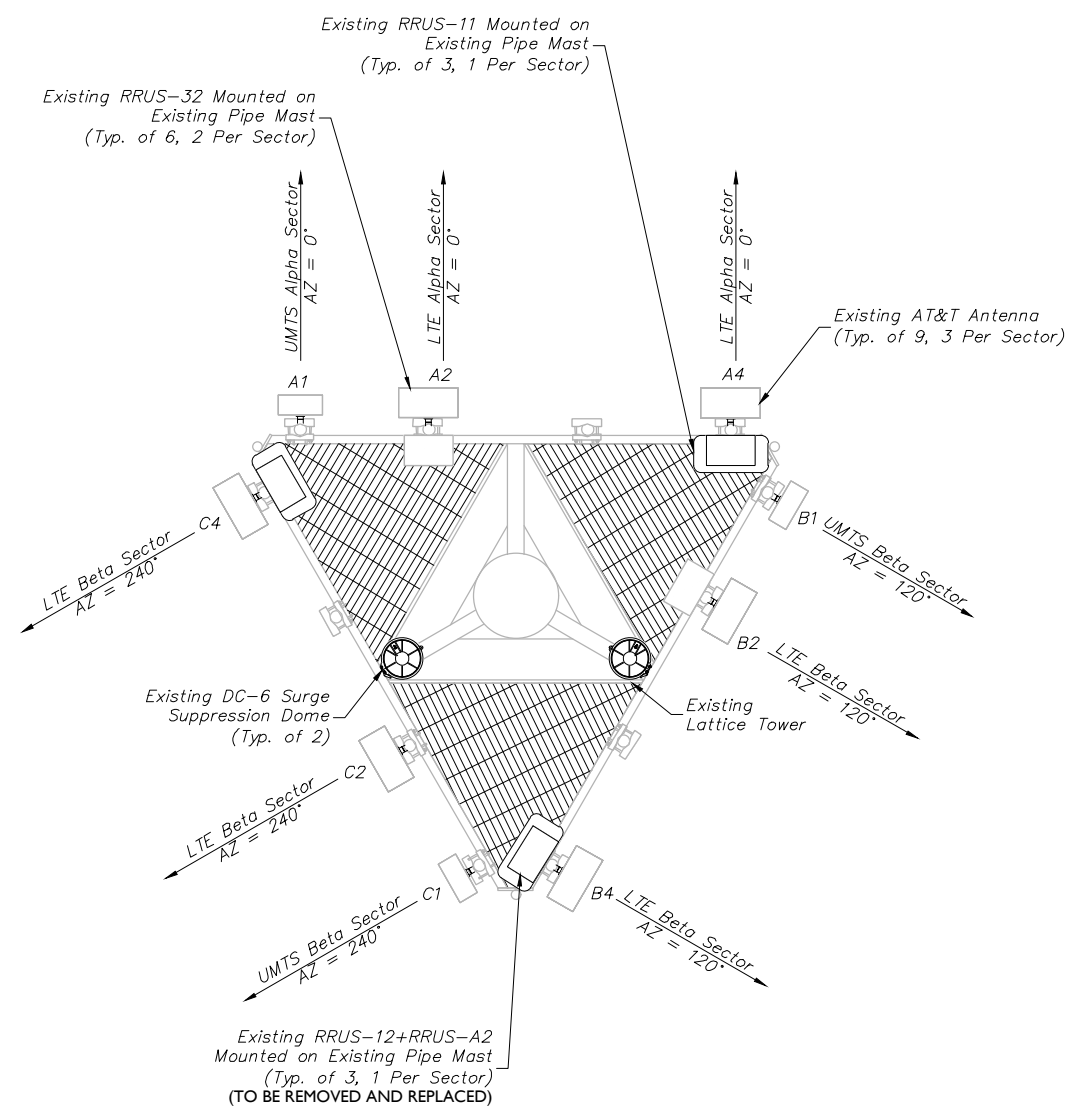
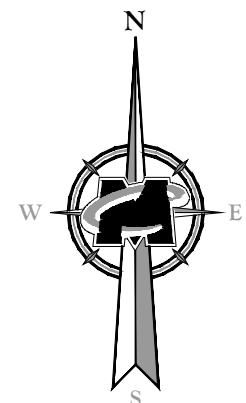
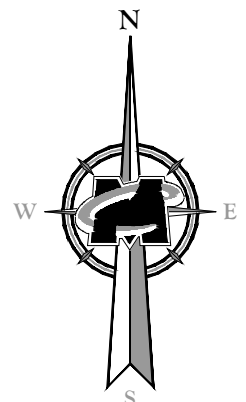
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SHEET TITLE:  
**ANTENNA LAYOUTS**

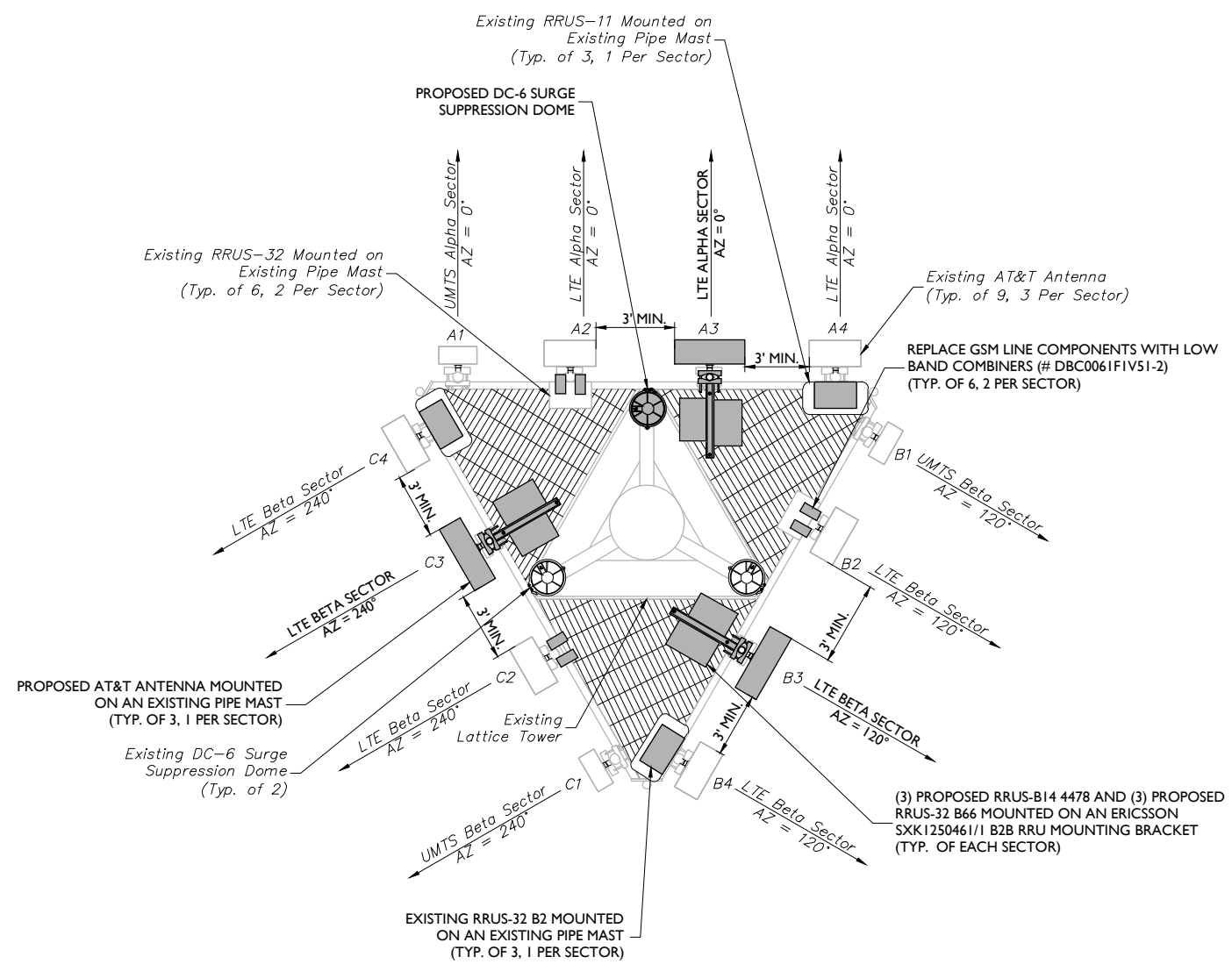
SHEET NUMBER:  
**A-3**

3 FEET MINIMUM SEPARATION BETWEEN LTE ANTENNAS  
6 FEET MINIMUM SEPARATION BETWEEN 700BC & 700 DE

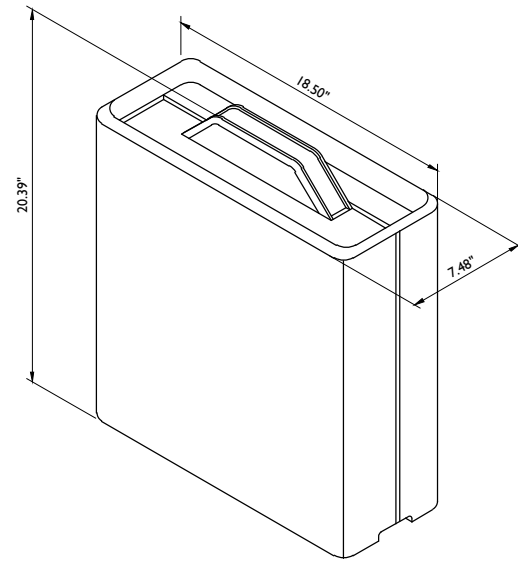


**EXISTING - ANTENNA LAYOUT**  
NOT TO SCALE

**NOTE:**  
SITE INFORMATION OBTAINED FROM THE FOLLOWING:  
A. PLAN ENTITLED "AVON - MONTEVIDEO ROAD" PREPARED BY COM EX CONSULTANTS, LAST REVISED 04/29/2016.



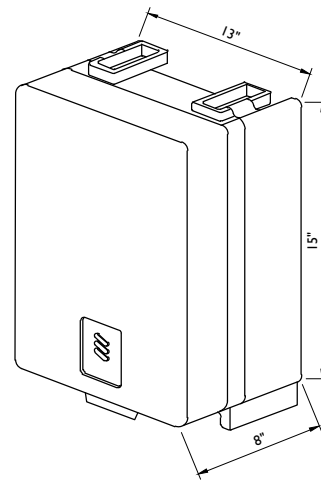
**PROPOSED - ANTENNA LAYOUT**  
NOT TO SCALE



RRUS-32 B66 DIMENSIONS (H X W X D): 20.39" X 18.5" X 7.48"  
(INCLUDES HANDLES)

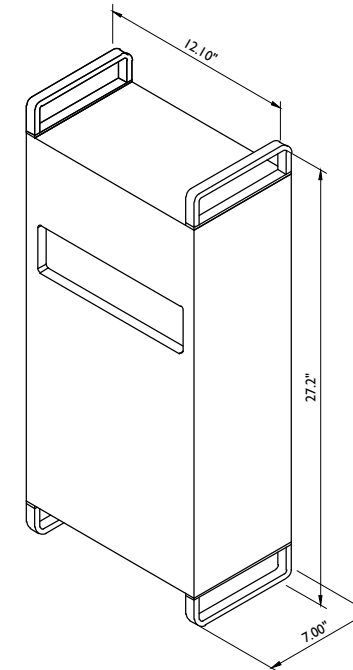
WEIGHT: 53 LBS

**RRUS E2 DETAIL**  
NOT TO SCALE



DIMENSIONS (H X W X D): 15"H X 13"W X 8"D (INCLUDES SUNSHIELD)  
WEIGHT: 60 LBS

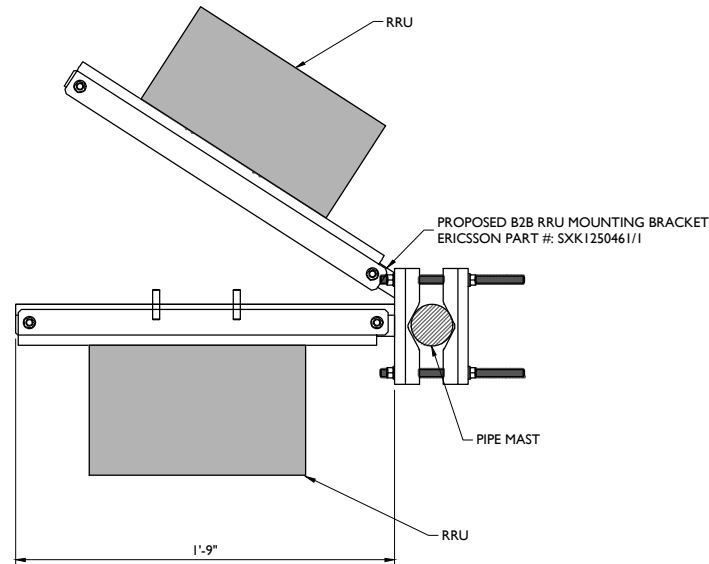
**RRU-4478-B14 DETAIL**  
NOT TO SCALE



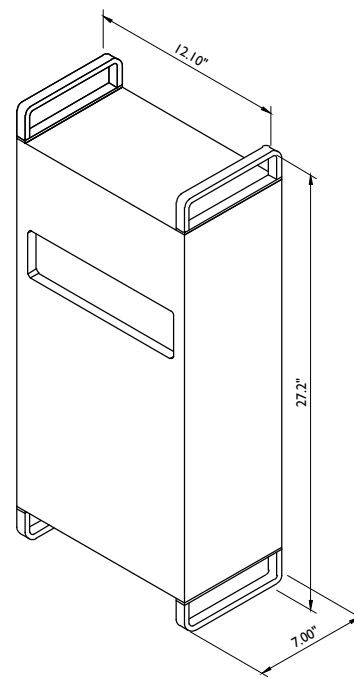
RRUS-32 B66 DIMENSIONS (H X W X D): 27.2" X 12.1" X 7.0"  
(INCLUDES HANDLES, FEET AND SUNSHIELD)

WEIGHT: 53 LBS

**RRUS-32 B66 DETAIL**  
NOT TO SCALE



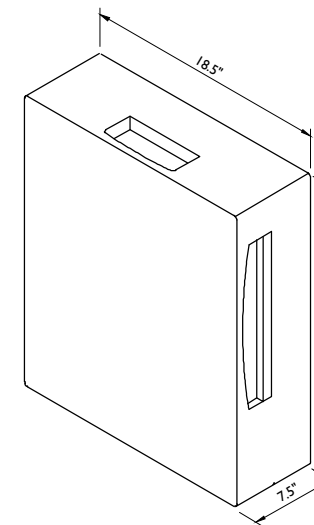
**RRU MOUNTING DETAIL**  
NOT TO SCALE



RRUS-32 B2 DIMENSIONS (H X W X D): 27.2" X 12.1" X 7.0"  
(INCLUDES HANDLES, FEET AND SUNSHIELD)

WEIGHT: 53 LBS

**RRUS-32 B2 DETAIL**  
NOT TO SCALE



RRUS-12 DIMENSIONS (H X W X D): 20.4" X 18.5" X 7.5" (INCLUDES SUNSHIELD)  
WEIGHT: 58 LBS

**RRUS-12 DETAIL**  
NOT TO SCALE



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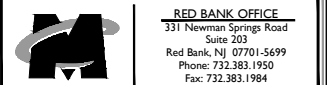
SCALE:	JOB NUMBER:
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1	01/23/18	ISSUED FOR REVIEW	AJC	RA



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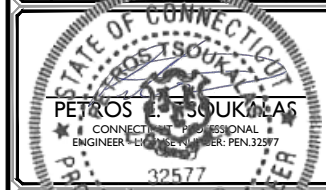


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SHEET TITLE:  
DETAILS


SHEET NUMBER:  
A-4

REV	DATE	DESCRIPTION	DRAWN BY	CHECKED BY
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1	01/23/18	ISSUED FOR REVIEW	AJC	RA



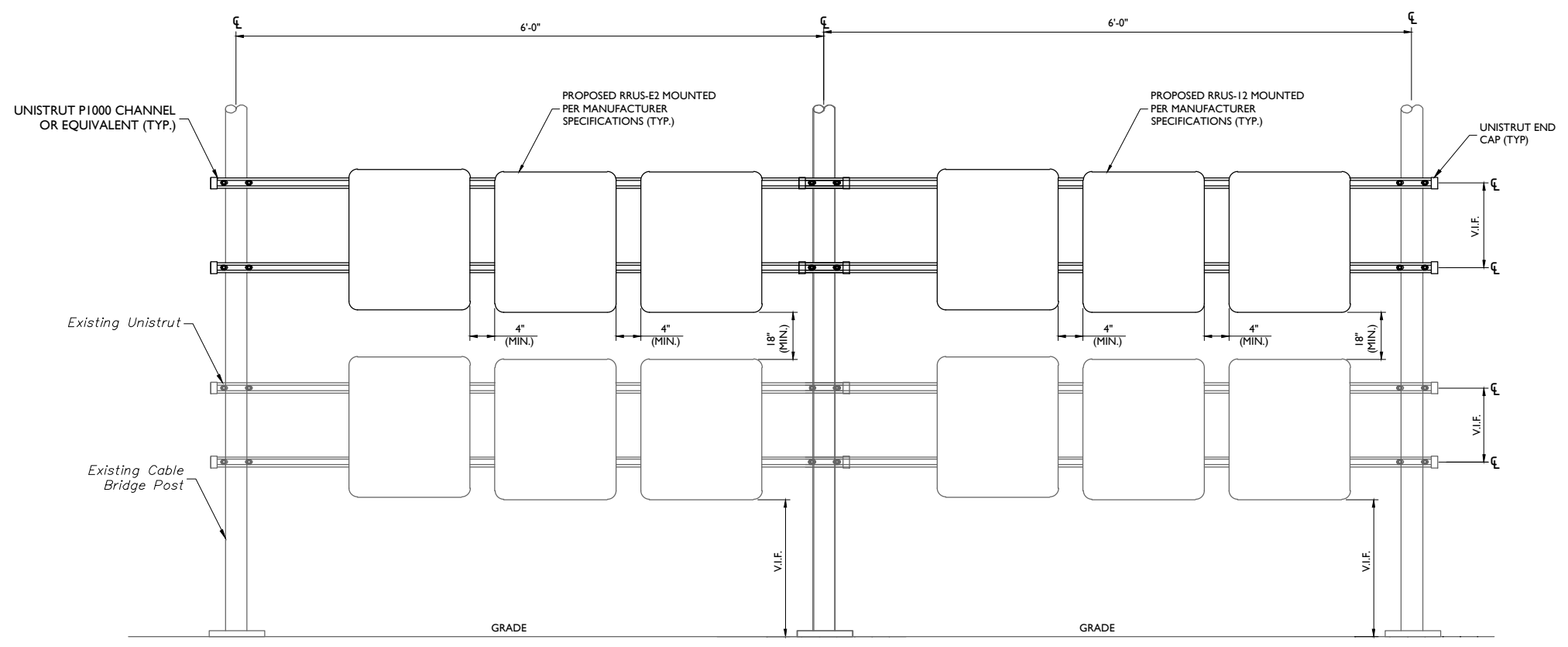
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SHEET TITLE: **DETAILS**

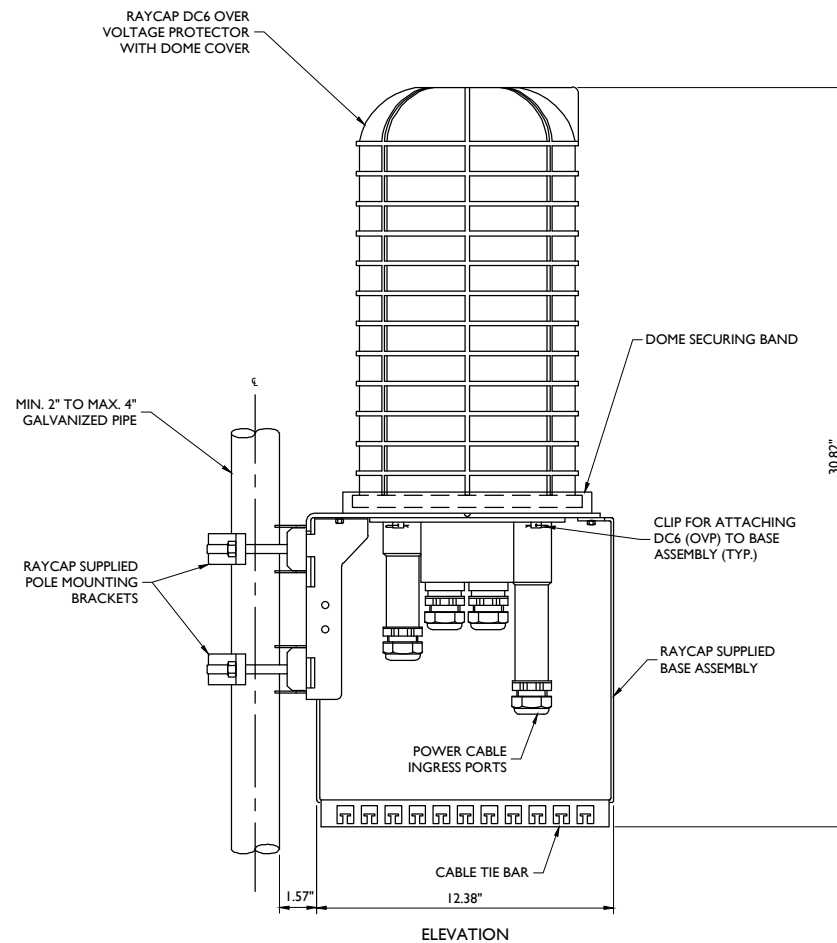
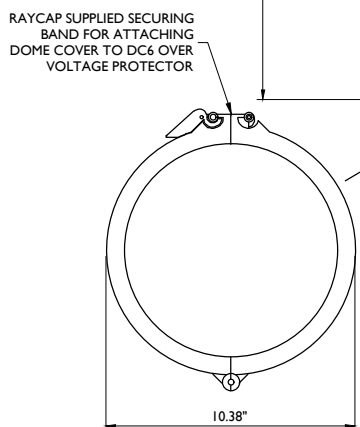
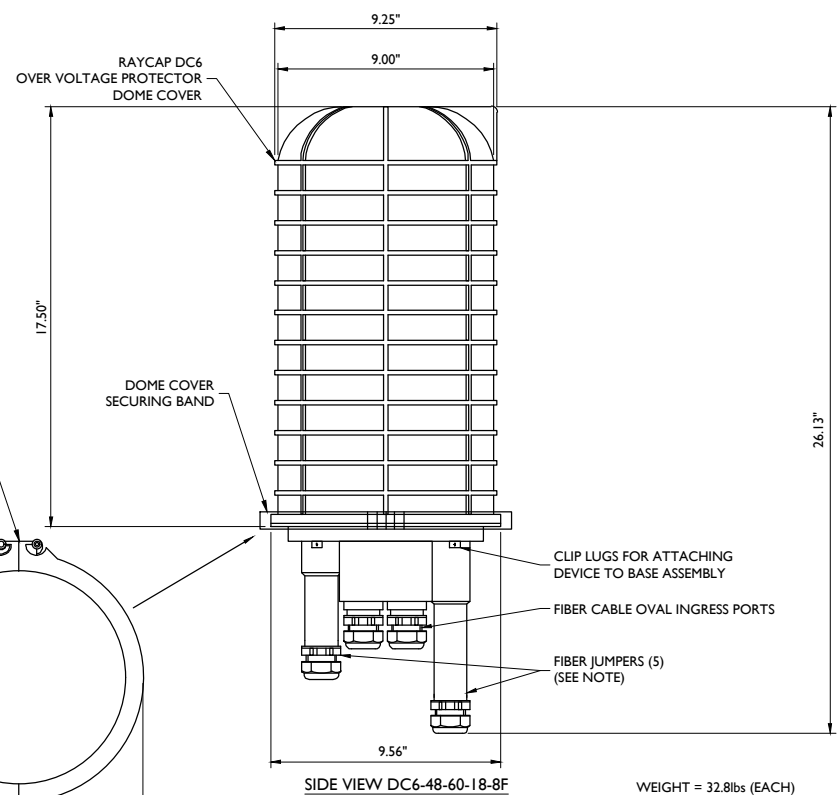
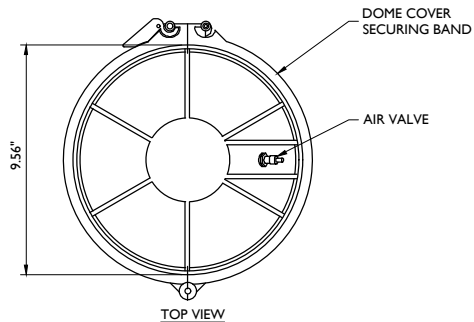
SHEET NUMBER: **A-5**



- NOTES:**
1. INSTALL VERTICAL UNISTRUT CHANNELS AS REQUIRED TO ALIGN FRAME WITH EQUIPMENT MOUNTING HOLES. FASTEN UNISTRUT CHANNELS TOGETHER WITH 3/8" UNISTRUT BOLTING HARDWARE AND SPRING NUTS.
  2. MOUNT RRUS TO UNISTRUT PER MANUFACTURER'S SPECIFICATIONS.
  3. MOUNT FRAME AS CLOSE TO PLATFORM AS POSSIBLE.
  4. NO PAINTING OF THE RRUS IS ALLOWED.

**RRUS DETAIL TO UNISTRUT FRAME DETAIL**  
NOT TO SCALE

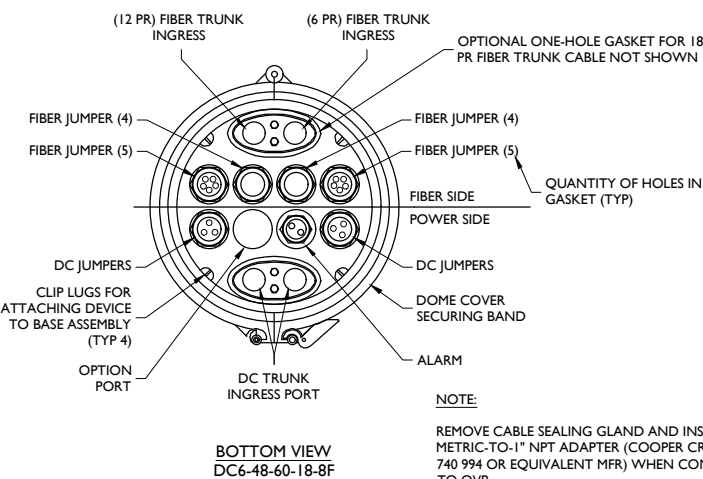
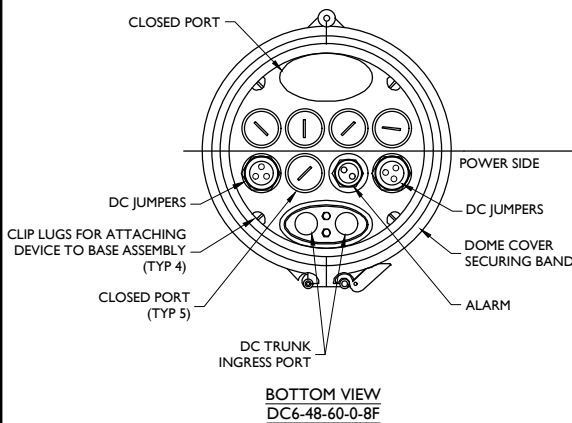




**NOTES:**

RAYCAP VIA AT&T SUPPLIES THE DC6 OVER VOLTAGE PROTECTOR AND PIPE MOUNTING BRACKETS. SUBCONTRACTOR SHALL SUPPLY THE PIPE.

**RAYCAP DC6-48-60-18-8F & DC6-48-60-0-8F  
DC POWER OVER VOLTAGE PROTECTOR (OVP)  
POLE MOUNT BASE ASSEMBLY**  
NOT TO SCALE



**NOTE:**

REMOVE CABLE SEALING GLAND AND INSTALL M32x1.5 METRIC-TO-1" NPT ADAPTER (COOPER CROUSE-HINES P/N CAP 740 994 OR EQUIVALENT MFR) WHEN CONNECTING CONDUIT TO OVP.

**DC6 SURGE SUPPRESSION DOME DETAIL**

NOT TO SCALE



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SHEET TITLE:

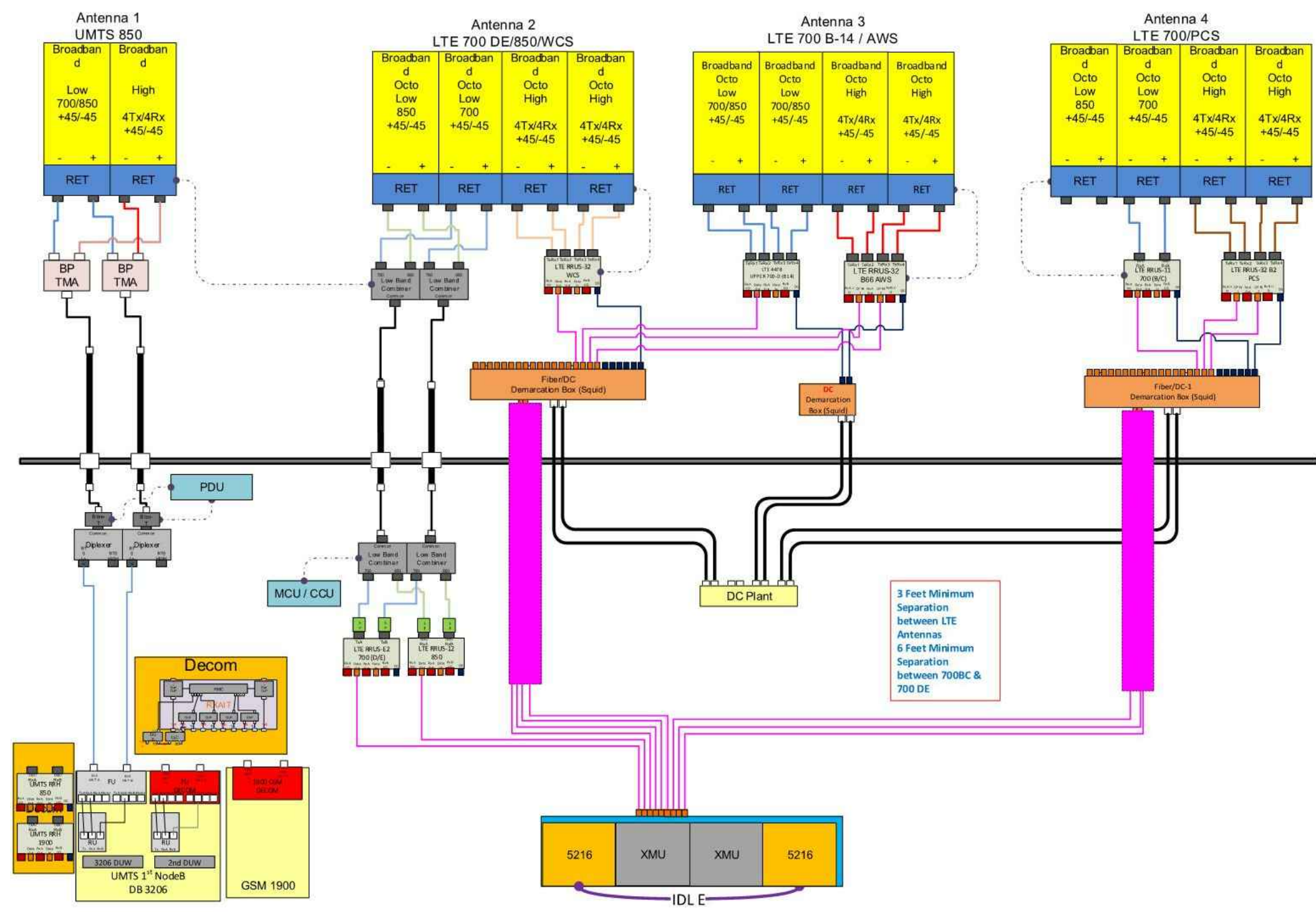
DETAILS

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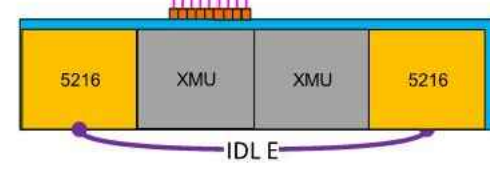
A-6

Diagram - Sector A Diagram File Name - CT5259\_LTE\_4C\_5C\_6C\_7C\_PCS\_4T4R\_Rev.1.vsd  
 Atoll Site Name - CTL05259 Location Name - WEST HARTFORD-ELMWOOD Market - CONNECTICUT Market Cluster - NEW ENGLAND  
 Comments: "Important Note: For detailed radio to antenna wiring refer to the latest 4T4R Antenna/ radio Port connections Field Notice (RF-HW-2016-265)"

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3 Feet Minimum Separation between LTE Antennas  
 6 Feet Minimum Separation between 700BC & 700 DE



ALL SECTORS

BASED ON: "NEW-ENGLAND\_CONNECTICUT\_CTL05259\_2018-LTE-Next-Carrier\_LTE\_dr701e\_2051A0ACHR\_10071358\_25914\_04-21-2017\_Final-RF-Approval\_v1.00" Last Updated: 10/09/2017.

RF PLUMBING DIAGRAMS

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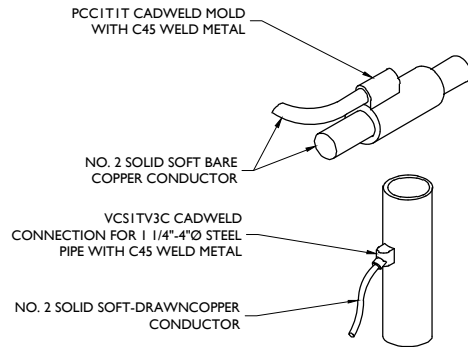
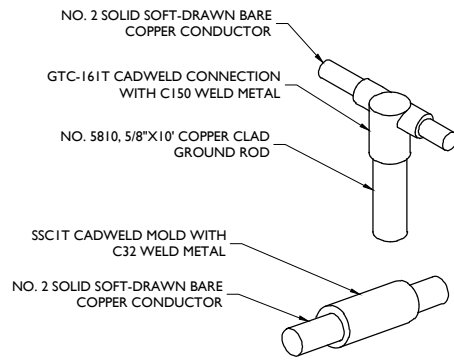
SCALE	JOB NUMBER			
AS SHOWN	17963019A			
0	02/28/18 FOR CONSTRUCTION AJC PET			
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STATE OF CONNECTICUT  
**PETROS TSOUKALAS**  
 CONNECTICUT PROFESSIONAL ENGINEER LICENSE NUMBER: PEN.32577  
 32577

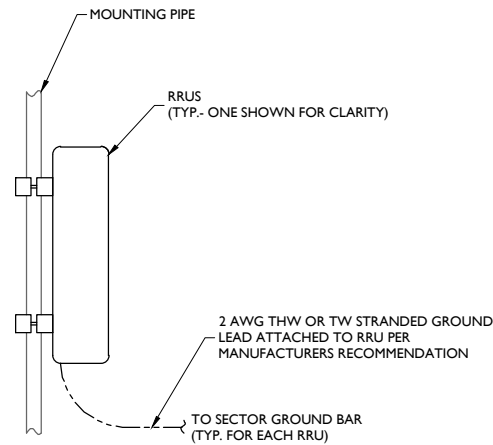
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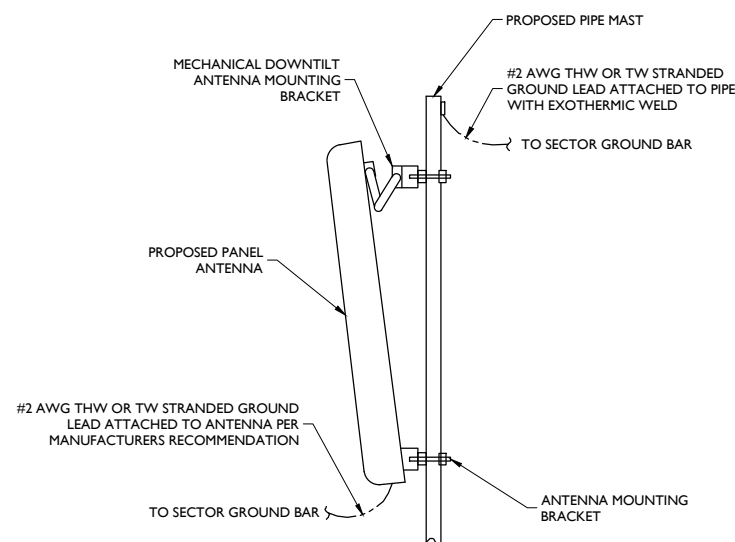
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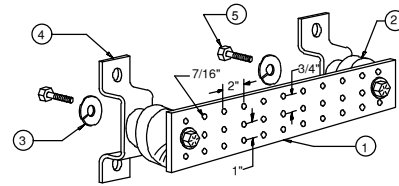
**CADWELD DETAILS**  
NOT TO SCALE



**RRU GROUNDING DETAIL**  
NOT TO SCALE



**ANTENNA GROUNDING**  
NOT TO SCALE



**LEGEND**

- 1- TINNED COPPER GROUND BAR, 1/4"x4"x20", NEWTON INSTRUMENT CO. CAT. NO. B-6142 OR EQUAL. HOLE CENTERS TO MATCH NEMA DOUBLE LUG CONFIGURATION.
- 2- INSULATORS, NEWTON INSTRUMENT CAT. NO. 3061-4
- 3- 5/8" LOCKWASHERS, NEWTON INSTRUMENT CO. CAT. NO. 3015-8
- 4- WALL MOUNTING BRACKET, NEWTON INSTRUMENT CO. CAT. NO. A-5056
- 5- 5/8-11 X 1" HHCS BOLTS, NEWTON INSTRUMENT CO. CAT. NO. 3012-1
- 6- EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS ORIGIN AND DESTINATION.

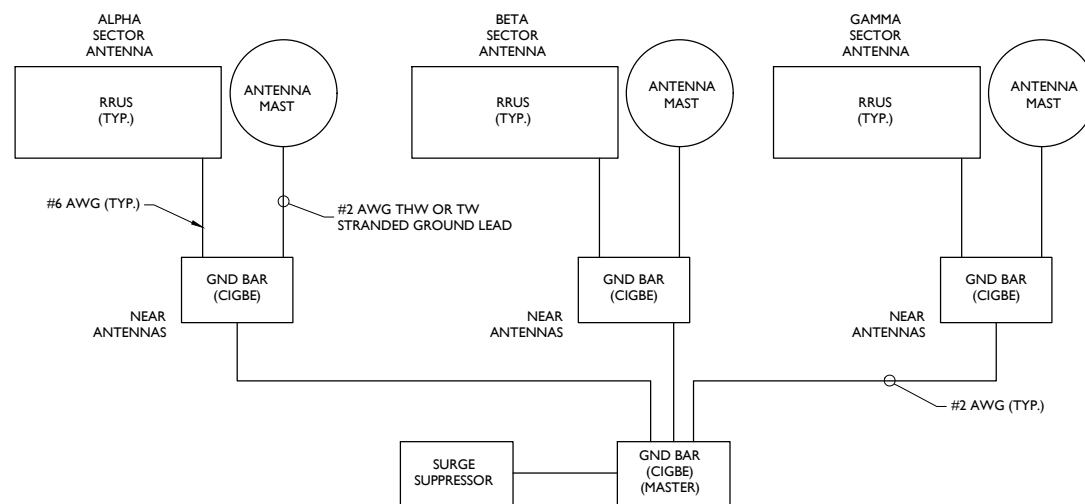
**SECTION "P" - SURGE PRODUCERS**

- CABLE ENTRY PORTS (HATCH PLATES) (#2)
- GENERATOR FRAMEWORK (IF AVAILABLE) (#2)
- TELCO GROUND BAR
- COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2)
- +24V POWER SUPPLY RETURN BAR (#2)
- 48V POWER SUPPLY RETURN BAR (#2)
- RECTIFIER FRAMES.

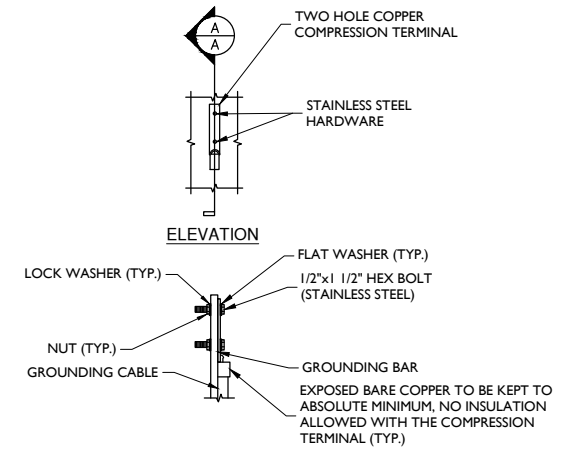
**SECTION "A" - SURGE ABSORBERS**

- INTERIOR GROUND RING (#2)
- EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2)
- METALLIC COLD WATER PIPE (IF AVAILABLE) (#2)
- BUILDING STEEL (IF AVAILABLE) (#2)

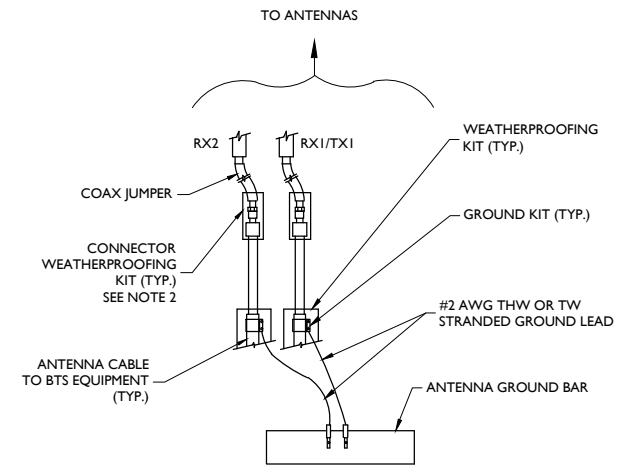
**MASTER GROUND BAR**  
NOT TO SCALE



**SCHEMATIC DIAGRAM GROUNDING SYSTEM**



**TYPICAL GROUND BAR CONNECTION DETAIL**  
NOT TO SCALE



**NOTES:**

1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO ANTENNA GROUND BAR.
2. WEATHER PROOFING SHALL BE TWO-PART TAPE KIT, COLD SHRINK SHALL NOT BE USED.

**TYPICAL GROUND WIRE TO GROUNDING BAR**  
NOT TO SCALE

SCALE: AS SHOWN	JOB NUMBER: 17963019A
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**Report Date:** March 27, 2018

**Client:** Hirschfeld Communications LLC  
1030 New Britain Avenue  
West Hartford, CT 06110  
Attn: Ian Ormesher  
(703) 447-1350  
iormesher@hirschfeldcos.com

**Structure:** Existing 185-ft Self Support  
**Site Name:** WestHartford\_DEXTERST  
**Site Reference #:** CT001  
**City, County, State:** West Hartford, Hartford County, CT  
**Latitude, Longitude:** 41.736092, -72.720499

**PJF Project:** A64118-0001.001.8700

Paul J. Ford and Company is pleased to submit this "Structural Analysis Report" to determine the tower stress level.

**Analysis Criteria:**

Reference Standard: 2016 Connecticut State Building Code with the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception #5 of Section 1609.1.1.

Ultimate Wind Speed: 122 mph 3-second gust wind speed without ice  
Nominal Wind Speed: 95 mph 3-second gust wind speed without ice  
Ice Wind Speed: 50 mph 3-second gust wind speed with 1" ice  
Service Wind Speed: 60.0 mph (Serviceability) without ice  
IBC Site Criteria: Risk Category II, Topographic Category 1, Exposure Category C

**Proposed Appurtenance Loads:**

The structure was analyzed with the addition of the proposed appurtenance loads shown in Table 1 combined with the existing and reserved loads shown in Table 2 of this report.

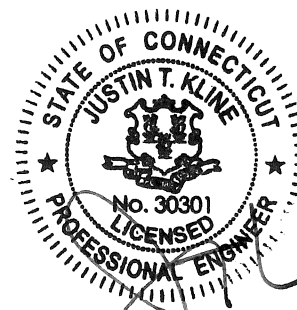
**Summary of Analysis Results:**

Existing Structure: 93.7% Pass  
Existing Foundation: 33.1% Pass

We at Paul J. Ford and Company appreciate the opportunity of providing our continuing professional services to you and Hirschfeld Communications LLC. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully Submitted by:  
Paul J. Ford and Company

  
Jonathan Sommer, EI  
Structural Designer JSR  
[jsommer@pjfweb.com](mailto:jsommer@pjfweb.com)



3-27-18

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## 1) INTRODUCTION

This tower is a 180 ft Self Support tower designed by PiRod in June of 1998. The tower was originally designed for a wind speed of 80 mph per EIA/TIA-222-F.

## 2) ANALYSIS CRITERIA

This analysis has been performed in accordance with the 2016 Connecticut State Building Code based upon an ultimate 3-second gust wind speed of 122 mph converted to a nominal 3-second gust wind speed of 95 mph per Section 1609.3 and Appendix N as required for use in the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception #5 of Section 1609.1.1. Risk Category II, Exposure Category C and Topographic Category 1.0 with a maximum Topographic Factor, Kzt, of 1 were used in this analysis.

**Table 1 - Proposed Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
180.0	180.0	3	ericsson	RRUS 32 B2	2	3/4	-
		3	ericsson	RRUS 32 B66			
		3	ericsson	RRUS 4478 B14			
		3	kathrein	80010965 w/ Mount Pipe			
		1	raycap	DC6-48-60-18-8F			

**Table 2 - Existing and Reserved Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
180.0	180.0	6	cci antennas	OPA-65R-LCUU-H6 w/ Mount Pipe	12 2 2	1-5/8 1/2 3/4	1
		3	ericsson	RRUS 11			
		3	ericsson	RRUS 12			
		3	ericsson	RRUS 32			
		3	ericsson	RRUS A2 MODULE			
		1	miscl	GPS			
		3	powerwave technologies	7770.00 w/ Mount Pipe			
		6	powerwave technologies	LGP21401			
		2	raycap	DC6-48-60-18-8F			
		1	tower mounts	Platform Mount [LP 405-1]			
		6	powerwave technologies	LGP21901			
		-	-	-	-	2	1/2

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
165.0	165.0	3	commscope	LNX-6515DS-A1M w/ Mount Pipe	6 2	1-5/8 Fiber	1
		3	ericsson	AIR 21 B2A/B4P w/ Mount Pipe			
		3	ericsson	AIR 32 B4A/B2P w/ Mount Pipe			
		3	ericsson	KRY 112 71			
		3	ericsson	RRUS 11 B12			
		1	tower mounts	Sector Mount [SM 402-3]			

Notes:

- 1) Existing Equipment
- 2) Reserved Equipment
- 3) Equipment To Be Removed

### 3) ANALYSIS PROCEDURE

**Table 3 - Documents Provided**

Document	Remarks
Manufacturer Drawings	PiROD Inc., 203949-B, 6/10/1998
Geotechnical Report	PiROD Inc., 6/5/1998
Pile Driving Report	Simeon Beer, 7/13/1998
Construction Drawings	AT&T, 2/13/2018

#### 3.1) Analysis Method

tnxTower (version 7.0.5.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

#### 3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) The existing base plate grout was considered in this analysis. Grout must be maintained and inspected periodically, and must be replaced if damaged or cracked.
- 5) Feedlines are stacked as shown in Appendix B of this report.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford and Company should be notified to determine the effect on the structural integrity of the tower.

### 4) ANALYSIS RESULTS

**Table 4 - Section Capacity (Summary)**

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
T1	180 - 170	Leg	1 1/2" solid	3	-18.97	54.43	34.9	Pass

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
T2	170 - 150	Leg	2" solid	39	71.92	106.69	67.4	Pass
T3	150 - 130	Leg	2 1/4" solid	101	-132.48	148.69	89.1	Pass
T4	130 - 120	Leg	Pirod 105216 (12x1.25)	165	-133.47	142.49	93.7	Pass
T5	120 - 100	Leg	Pirod 105217 (12x1.5)	175	-160.20	214.86	74.6	Pass
T6	100 - 80	Leg	Pirod 105217 (12x1.5)	190	-182.81	214.86	85.1	Pass
T7	80 - 60	Leg	Pirod 105218 (12x1.75)	205	-206.10	300.68	68.5	Pass
T8	60 - 40	Leg	Pirod 105218 (12x1.75)	220	-229.38	300.68	76.3	Pass
T9	40 - 20	Leg	Pirod 105219 (12x2)	235	-253.59	399.87	63.4	Pass
T10	20 - 0	Leg	Pirod 105219 (12x2)	250	-276.44	399.87	69.1	Pass
T1	180 - 170	Diagonal	3/4" solid	15	-3.34	6.09	54.9	Pass
T2	170 - 150	Diagonal	7/8" solid	50	-5.48	9.34	58.8	Pass
T3	150 - 130	Diagonal	1" solid	164	-6.22	15.16	41.1	Pass
T4	130 - 120	Diagonal	L 2.5 x 2.5 x 3/16	172	-7.02	13.56	51.7 61.4 (b)	Pass
T5	120 - 100	Diagonal	L 2.5 x 2.5 x 3/16	188	-4.73	11.92	39.7 42.1 (b)	Pass
T6	100 - 80	Diagonal	L 2.5 x 2.5 x 3/16	196	-4.60	8.66	53.1	Pass
T7	80 - 60	Diagonal	L 3 x 3 x 3/16	210	-5.01	12.12	41.3	Pass
T8	60 - 40	Diagonal	L 3 x 3 x 3/16	225	-5.51	9.79	56.3	Pass
T9	40 - 20	Diagonal	L 3 x 3 x 5/16	240	-6.14	12.87	47.7	Pass
T10	20 - 0	Diagonal	L 3 x 3 x 5/16	255	-7.37	10.64	69.3	Pass
T1	180 - 170	Horizontal	7/8" solid	30	-0.55	6.14	9.0	Pass
T2	170 - 150	Horizontal	7/8" solid	59	-1.04	5.22	19.9	Pass
T3	150 - 130	Horizontal	7/8" solid	158	-1.84	4.79	38.5	Pass
T1	180 - 170	Top Girt	7/8" solid	6	-1.75	6.14	28.5	Pass
T2	170 - 150	Top Girt	7/8" solid	42	-1.92	6.22	30.8	Pass
T3	150 - 130	Top Girt	1" solid	105	-2.08	8.40	24.8	Pass
T1	180 - 170	Bottom Girt	7/8" solid	7	-1.49	6.14	24.3	Pass
T2	170 - 150	Bottom Girt	7/8" solid	43	-2.58	4.94	52.2	Pass
T3	150 - 130	Bottom Girt	1" solid	107	-2.72	6.83	39.9	Pass
							Summary	
						Leg (T4)	93.7	Pass
						Diagonal (T10)	69.3	Pass
						Horizontal (T3)	38.5	Pass
						Top Girt (T2)	30.8	Pass
						Bottom Girt (T2)	52.2	Pass
						Bolt Checks	65.5	Pass
						RATING =	93.7	Pass



**Table 5 - Tower Component Stresses vs. Capacity**

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	42.2	Pass
1	Base Foundation Structural	0	9.1	Pass
1	Base Foundation Soil Interaction	0	33.1	Pass

<b>Structure Rating (max from all components) =</b>	<b>93.1%</b>
---	--------------

Notes:

- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

#### 4.1) Recommendations

The tower and its foundations have sufficient capacity to carry the proposed loading configuration. No modifications are required at this time.

**APPENDIX A**  
**TNXTOWER OUTPUT**

## Tower Input Data

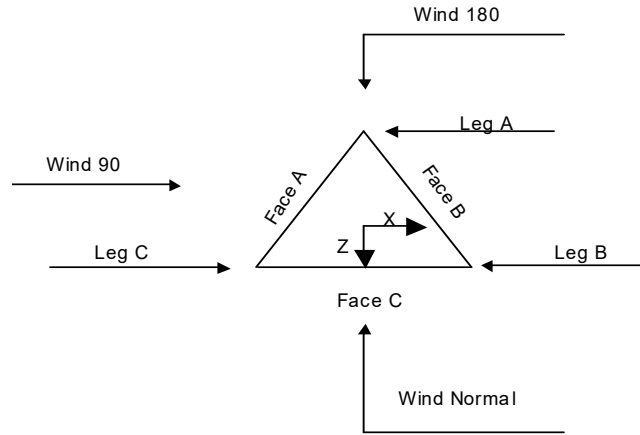
The main tower is a 3x free standing tower with an overall height of 180.00 ft above the ground line.  
 The base of the tower is set at an elevation of 0.00 ft above the ground line.  
 The face width of the tower is 4.00 ft at the top and 18.00 ft at the base.  
 This tower is designed using the TIA-222-G standard.

The following design criteria apply:

- 1) Tower is located in Hartford County, Connecticut.
- 2) ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).
- 3) Basic wind speed of 95.0 mph.
- 4) Structure Class II.
- 5) Exposure Category C.
- 6) Topographic Category 1.
- 7) Crest Height 0.00 ft.
- 8) Nominal ice thickness of 1.00 in.
- 9) Ice thickness is considered to increase with height.
- 10) Ice density of 56 pcf.
- 11) A wind speed of 50.0 mph is used in combination with ice.
- 12) Deflections calculated using a wind speed of 60.0 mph.
- 13) A non-linear (P-delta) analysis was used.
- 14) Pressures are calculated at each section.
- 15) Stress ratio used in tower member design is 1.
- 16) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

- |  |  |  |
|--|--|--|
| <ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <br/> <li>√ Include Bolts In Member Capacity</li> <br/> <li>Leg Bolts Are At Top Of Section</li> <li>√ Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>√ SR Members Have Cut Ends</li> <li>SR Members Are Concentric</li> </ul> | <ul style="list-style-type: none"> <li>Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>√ Use Clear Spans For KL/r</li> <li>Retention Guys To Initial Tension</li> <li>Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <br/> <li>Autocalc Torque Arm Areas</li> <br/> <li>Add IBC .6D+W Combination</li> <li>√ Sort Capacity Reports By Component</li> <li>Triangulate Diamond Inner Bracing</li> <li>Treat Feed Line Bundles As Cylinder</li> </ul> | <ul style="list-style-type: none"> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>√ Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>√ SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feed Line Torque</li> <li>√ Include Angle Block Shear Check</li> <li>Use TIA-222-G Bracing Resist. Exemption</li> <li>Use TIA-222-G Tension Splice Exemption</li> <br/> <li style="text-align: center;"><b>Poles</b></li> <li>Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> </ul> |
|--|--|--|



**Triangular Tower**

**Tower Section Geometry**

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T1	180.00-170.00		106778 (48)	4.00	1	10.00
T2	170.00-150.00		100246 (48/54)	4.00	1	20.00
T3	150.00-130.00		119703 (54/60)	4.50	1	20.00
T4	130.00-120.00		U06 105218 [L2.5 x 3/16]	5.00	1	10.00
T5	120.00-100.00		U08 105217 [L2.5 x 3/16]	6.00	1	20.00
T6	100.00-80.00		U10 105217 [L2.5 x 3/16]	8.00	1	20.00
T7	80.00-60.00		U12 105218 [L3 x 3/16]	10.00	1	20.00
T8	60.00-40.00		U14 105218 [L3 x 3/16]	12.00	1	20.00
T9	40.00-20.00		U16 105219 [L3 x 5/16]	14.00	1	20.00
T10	20.00-0.00		U18 105219 [L3 x 5/16]	16.00	1	20.00

**Tower Section Geometry (cont'd)**

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	180.00-170.00	2.25	X Brace	No	Steps	6.00	6.00
T2	170.00-150.00	2.36	X Brace	No	Steps	6.80	6.80
T3	150.00-130.00	2.36	X Brace	No	Steps	6.80	6.80
T4	130.00-120.00	10.00	X Brace	No	No	0.00	0.00
T5	120.00-100.00	10.00	X Brace	No	No	0.00	0.00
T6	100.00-80.00	10.00	X Brace	No	No	0.00	0.00
T7	80.00-60.00	10.00	X Brace	No	No	0.00	0.00
T8	60.00-40.00	10.00	X Brace	No	No	0.00	0.00
T9	40.00-20.00	10.00	X Brace	No	No	0.00	0.00
T10	20.00-0.00	10.00	X Brace	No	No	0.00	0.00

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 180.00-170.00	Solid Round	1 1/2" solid	A572-50 (50 ksi)	Solid Round	3/4" solid	A572-50 (50 ksi)
T2 170.00-150.00	Solid Round	2" solid	A572-50 (50 ksi)	Solid Round	7/8" solid	A572-50 (50 ksi)
T3 150.00-130.00	Solid Round	2 1/4" solid	A572-50 (50 ksi)	Solid Round	1" solid	A572-50 (50 ksi)
T4 130.00-120.00	Truss Leg	Pirod 105216 (12x1.25)	A572-50 (50 ksi)	Single Angle	L 2.5 x 2.5 x 3/16	A36 (36 ksi)
T5 120.00-100.00	Truss Leg	Pirod 105217 (12x1.5)	A572-50 (50 ksi)	Single Angle	L 2.5 x 2.5 x 3/16	A36 (36 ksi)
T6 100.00-80.00	Truss Leg	Pirod 105217 (12x1.5)	A572-50 (50 ksi)	Single Angle	L 2.5 x 2.5 x 3/16	A36 (36 ksi)
T7 80.00-60.00	Truss Leg	Pirod 105218 (12x1.75)	A572-50 (50 ksi)	Single Angle	L 3 x 3 x 3/16	A36 (36 ksi)
T8 60.00-40.00	Truss Leg	Pirod 105218 (12x1.75)	A572-50 (50 ksi)	Single Angle	L 3 x 3 x 3/16	A36 (36 ksi)
T9 40.00-20.00	Truss Leg	Pirod 105219 (12x2)	A572-50 (50 ksi)	Single Angle	L 3 x 3 x 5/16	A36 (36 ksi)
T10 20.00-0.00	Truss Leg	Pirod 105219 (12x2)	A572-50 (50 ksi)	Single Angle	L 3 x 3 x 5/16	A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 180.00-170.00	Solid Round	7/8" solid	A572-50 (50 ksi)	Solid Round	7/8" solid	A572-50 (50 ksi)
T2 170.00-150.00	Solid Round	7/8" solid	A572-50 (50 ksi)	Solid Round	7/8" solid	A572-50 (50 ksi)
T3 150.00-130.00	Solid Round	1" solid	A572-50 (50 ksi)	Solid Round	1" solid	A572-50 (50 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T1 180.00-170.00	None	Solid Round		A572-50 (50 ksi)	Solid Round	7/8" solid	A572-50 (50 ksi)
T2 170.00-150.00	None	Solid Round		A36 (36 ksi)	Solid Round	7/8" solid	A572-50 (50 ksi)
T3 150.00-130.00	None	Solid Round		A572-50 (50 ksi)	Solid Round	7/8" solid	A572-50 (50 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor A <sub>r</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontal in	Double Angle Stitch Bolt Spacing Redundants in
T1 180.00-170.00	0.00	0.00	A36 (36 ksi)	1	1	1.02	Mid-Pt	Mid-Pt	Mid-Pt
T2 170.00-150.00	0.00	0.00	A36 (36 ksi)	1	1	1.03	Mid-Pt	Mid-Pt	Mid-Pt

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_r$	Adjust. Factor $A_r$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals	Double Angle Stitch Bolt Spacing Redundants
ft	ft <sup>2</sup>	in					in	in	in
T3 150.00-130.00	0.00	0.00	A36 (36 ksi)	1	1	1.03	Mid-Pt	Mid-Pt	Mid-Pt
T4 130.00-120.00	0.00	0.50	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	Mid-Pt
T5 120.00-100.00	0.00	0.50	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	Mid-Pt
T6 100.00-80.00	0.00	0.50	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	Mid-Pt
T7 80.00-60.00	0.00	0.50	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	Mid-Pt
T8 60.00-40.00	0.00	0.50	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	Mid-Pt
T9 40.00-20.00	0.00	0.50	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	Mid-Pt
T10 20.00-0.00	0.00	0.75	A36 (36 ksi)	1	1	1.05	Mid-Pt	Mid-Pt	Mid-Pt

### Tower Section Geometry (cont'd)

Tower Elevation	Calc K Single Angles	Calc K Solid Rounds	Legs	K Factors <sup>1</sup>							
				X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace	
											X
ft				Y	Y	Y	Y	Y	Y	Y	
T1 180.00-170.00	No	Yes	1	1	1	1	1	1	1	0.7	1
T2 170.00-150.00	No	Yes	1	1	1	1	1	1	1	0.7	1
T3 150.00-130.00	No	Yes	1	1	1	1	1	1	1	0.7	1
T4 130.00-120.00	Yes	No	1	1	1	1	1	1	1	1	1
T5 120.00-100.00	Yes	No	1	1	1	1	1	1	1	1	1
T6 100.00-80.00	Yes	No	1	1	1	1	1	1	1	1	1
T7 80.00-60.00	Yes	No	1	1	1	1	1	1	1	1	1
T8 60.00-40.00	Yes	No	1	1	1	1	1	1	1	1	1
T9 40.00-20.00	Yes	No	1	1	1	1	1	1	1	1	1
T10 20.00-0.00	Yes	No	1	1	1	1	1	1	1	1	1

<sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

### Tower Section Geometry (cont'd)

Tower Elevation ft	Truss-Leg K Factors					
	Truss-Legs Used As Leg Members			Truss-Legs Used As Inner Members		
	Leg Panels	X Brace Diagonals	Z Brace Diagonals	Leg Panels	X Brace Diagonals	Z Brace Diagonals
T4 130.00-120.00	1	0.5	0.85	1	0.5	0.85
T5 120.00-100.00	1	0.5	0.85	1	0.5	0.85
T6 100.00-80.00	1	0.5	0.85	1	0.5	0.85
T7 80.00-60.00	1	0.5	0.85	1	0.5	0.85
T8 60.00-40.00	1	0.5	0.85	1	0.5	0.85
T9 40.00-20.00	1	0.5	0.85	1	0.5	0.85
T10 20.00-0.00	1	0.5	0.85	1	0.5	0.85

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 180.00-170.00	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
T2 170.00-150.00	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
T3 150.00-130.00	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
T4 130.00-120.00	0.00	1	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75
T5 120.00-100.00	0.00	1	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75
T6 100.00-80.00	0.00	1	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75
T7 80.00-60.00	0.00	1	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75
T8 60.00-40.00	0.00	1	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75
T9 40.00-20.00	0.00	1	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75
T10 20.00-0.00	0.00	1	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75	0.00	0.75

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.		
T1 180.00-170.00	Sleeve DS	0.63 A325N	5	0.00 A325N	0	0.00 A325N	0	0.00 A325N	0	0.63 A325N	0	0.00 A325N	0	0.63 A325N	0

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T2 170.00-150.00	Sleeve DS	0.75	5	0.00	0	0.00	0	0.00	0	0.00	0	0.00	0	0.00	0
T3 150.00-130.00	Flange	A325N	6	A325N	0	A325N	0	A325N	0	A325N	0	A325N	0	A325N	0
T4 130.00-120.00	Flange	1.00	6	A325N	1	A325N	0	A325N	0	A325N	0	A325N	0	A325N	0
T5 120.00-100.00	Flange	1.00	6	A325N	1	A325N	0	A325N	0	A325N	0	A325N	0	A325N	0
T6 100.00-80.00	Flange	1.00	6	A325N	1	A325N	0	A325N	0	A325N	0	A325N	0	A325N	0
T7 80.00-60.00	Flange	1.00	6	A325N	1	A325N	0	A325N	0	A325N	0	A325N	0	A325N	0
T8 60.00-40.00	Flange	1.00	6	A325N	1	A325N	0	A325N	0	A325N	0	A325N	0	A325N	0
T9 40.00-20.00	Flange	1.25	6	A325N	1	A325N	0	A325N	0	A325N	0	A325N	0	A325N	0
T10 20.00-0.00	Flange	1.25	0	A325N	1	A325N	0	A325N	0	A325N	0	A325N	0	A325N	0
		F1554-105		A325N		A325N		A325N		A325N		A325N		A325N	

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Shield Leg	Allow	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
LDF7-50A (1 5/8" foam)	A	No	Ar (CaAa)	180.00 - 8.00	0.00	0.2	12	6	1.00	1.98		0.92
FSJ4-50B(1/2")	A	No	Ar (CaAa)	180.00 - 8.00	0.00	0.2	2	2	2.00	0.52		0.14
9776( 3/4")	A	No	Ar (CaAa)	180.00 - 8.00	0.00	0.2	4	4	2.00	0.73		0.31
***									0.50			
T-Brackets (Af)	C	No	Ar (CaAa)	165.00 - 8.00	0.00	-0.45	1	1	1.00	1.00		8.40
LDF7-50A (1 5/8" foam)	C	No	Ar (CaAa)	165.00 - 8.00	0.00	-0.45	8	6	1.00	1.98		0.92
LDF7-50A (1 5/8" foam)	C	No	Ar (CaAa)	165.00 - 8.00	0.00	-0.45	2	2	1.00	1.98		0.92
*****									0.50			

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment	Placement ft	C <sub>A</sub> A <sub>A</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Side ft <sup>2</sup>	Weight K
Platform Mount [LP 405-1]	C	None		0.000	180.00	No Ice 20.80 1/2" 28.10 Ice 35.40	20.80 28.10 35.40	1.80 2.07 2.33
7770.00 w/ Mount Pipe	A	From Leg	4.00 0.00 0.00	0.000	180.00	No Ice 5.75 1/2" 6.18 Ice 6.61 1" Ice	4.25 5.01 5.71	0.06 0.10 0.16
7770.00 w/ Mount Pipe	B	From Leg	4.00	0.000	180.00	No Ice 5.75	4.25	0.06



Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K	
			0.00			1/2"	6.18	5.01	0.10
			0.00			Ice	6.61	5.71	0.16
7770.00 w/ Mount Pipe	C	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	5.75	4.25	0.06
			0.00			1/2"	6.18	5.01	0.10
			0.00			Ice	6.61	5.71	0.16
(2) OPA-65R-LCUU-H6 w/ Mount Pipe	A	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	9.90	7.18	0.10
			0.00			1/2"	10.47	8.36	0.18
			0.00			Ice	11.01	9.26	0.26
(2) OPA-65R-LCUU-H6 w/ Mount Pipe	B	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	9.90	7.18	0.10
			0.00			1/2"	10.47	8.36	0.18
			0.00			Ice	11.01	9.26	0.26
(2) OPA-65R-LCUU-H6 w/ Mount Pipe	C	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	9.90	7.18	0.10
			0.00			1/2"	10.47	8.36	0.18
			0.00			Ice	11.01	9.26	0.26
(2) LGP21401	A	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	1.10	0.35	0.01
			0.00			1/2"	1.24	0.44	0.02
			0.00			Ice	1.38	0.54	0.03
(2) LGP21401	B	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	1.10	0.35	0.01
			0.00			1/2"	1.24	0.44	0.02
			0.00			Ice	1.38	0.54	0.03
(2) LGP21401	C	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	1.10	0.35	0.01
			0.00			1/2"	1.24	0.44	0.02
			0.00			Ice	1.38	0.54	0.03
RRUS 32	A	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	2.86	1.78	0.06
			0.00			1/2"	3.08	1.97	0.08
			0.00			Ice	3.32	2.17	0.10
RRUS 32	B	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	2.86	1.78	0.06
			0.00			1/2"	3.08	1.97	0.08
			0.00			Ice	3.32	2.17	0.10
RRUS 32	C	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	2.86	1.78	0.06
			0.00			1/2"	3.08	1.97	0.08
			0.00			Ice	3.32	2.17	0.10
RRUS 11	A	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	2.79	1.19	0.05
			0.00			1/2"	3.00	1.34	0.07
			0.00			Ice	3.21	1.50	0.10
RRUS 11	B	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	2.79	1.19	0.05
			0.00			1/2"	3.00	1.34	0.07
			0.00			Ice	3.21	1.50	0.10
RRUS 11	C	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	2.79	1.19	0.05
			0.00			1/2"	3.00	1.34	0.07
			0.00			Ice	3.21	1.50	0.10
DC6-48-60-18-8F	A	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	0.92	0.92	0.02
			0.00			1/2"	1.46	1.46	0.04
			0.00			Ice	1.64	1.64	0.06
DC6-48-60-18-8F	B	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	0.92	0.92	0.02
			0.00			1/2"	1.46	1.46	0.04
			0.00			Ice	1.64	1.64	0.06
RRUS 12	A	From Leg	4.00	0.000	180.00	1" Ice			
			0.00			No Ice	3.15	1.29	0.06
			0.00				3.36	1.44	0.08

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
			0.00			1/2" Ice 3.59	1.60	0.11
RRUS 12	B	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 3.59	1.29 1.44 1.60	0.06 0.08 0.11
RRUS 12	C	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 3.59	1.29 1.44 1.60	0.06 0.08 0.11
RRUS A2 MODULE	A	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 1.92	0.38 0.47 0.57	0.02 0.03 0.04
RRUS A2 MODULE	B	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 1.92	0.38 0.47 0.57	0.02 0.03 0.04
RRUS A2 MODULE	C	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 1.92	0.38 0.47 0.57	0.02 0.03 0.04
GPS	C	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 0.31	0.13 0.24 0.31	0.02 0.02 0.02
80010965 w/ Mount Pipe	A	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 15.30	7.63 8.90 9.96	0.13 0.22 0.33
80010965 w/ Mount Pipe	B	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 15.30	7.63 8.90 9.96	0.13 0.22 0.33
80010965 w/ Mount Pipe	C	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 15.30	7.63 8.90 9.96	0.13 0.22 0.33
DC6-48-60-18-8F	C	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 1.64	0.92 1.46 1.64	0.02 0.04 0.06
RRUS 4478 B14	A	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 2.19	1.06 1.20 1.34	0.06 0.08 0.09
RRUS 4478 B14	B	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 2.19	1.06 1.20 1.34	0.06 0.08 0.09
RRUS 4478 B14	C	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 2.19	1.06 1.20 1.34	0.06 0.08 0.09
RRUS 32 B66	A	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 3.19	1.67 1.86 2.05	0.05 0.07 0.10
RRUS 32 B66	B	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 3.19	1.67 1.86 2.05	0.05 0.07 0.10
RRUS 32 B66	C	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice 1/2" Ice 3.19	1.67 1.86 2.05	0.05 0.07 0.10

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft		C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
			0.00			1/2" Ice	3.19	2.05	0.10
RRUS 32 B2	A	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice	2.73	1.67	0.05
						1/2" Ice	2.95	1.86	0.07
						1" Ice	3.18	2.05	0.10
RRUS 32 B2	B	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice	2.73	1.67	0.05
						1/2" Ice	2.95	1.86	0.07
						1" Ice	3.18	2.05	0.10
RRUS 32 B2	C	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice	2.73	1.67	0.05
						1/2" Ice	2.95	1.86	0.07
						1" Ice	3.18	2.05	0.10
(2) LGP21901	A	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice	0.23	0.16	0.01
						1/2" Ice	0.29	0.21	0.01
						1" Ice	0.36	0.28	0.01
(2) LGP21901	B	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice	0.23	0.16	0.01
						1/2" Ice	0.29	0.21	0.01
						1" Ice	0.36	0.28	0.01
(2) LGP21901	C	From Leg	4.00 0.00 0.00	0.000	180.00	1" Ice No Ice	0.23	0.16	0.01
						1/2" Ice	0.29	0.21	0.01
						1" Ice	0.36	0.28	0.01
***									
Sector Mount [SM 402-3]	C	From Leg	0.00 0.00 0.00	0.000	165.00	No Ice	18.91	18.91	0.85
						1/2" Ice	26.78	26.78	1.23
						1" Ice	34.65	34.65	1.62
AIR 21 B2A/B4P w/ Mount Pipe	A	From Leg	4.00 0.00 0.00	0.000	165.00	1" Ice No Ice	6.16	5.55	0.10
						1/2" Ice	6.60	6.30	0.16
						1" Ice	7.03	7.00	0.22
AIR 21 B2A/B4P w/ Mount Pipe	B	From Leg	4.00 0.00 0.00	0.000	165.00	1" Ice No Ice	6.16	5.55	0.10
						1/2" Ice	6.60	6.30	0.16
						1" Ice	7.03	7.00	0.22
AIR 21 B2A/B4P w/ Mount Pipe	C	From Leg	4.00 0.00 0.00	0.000	165.00	1" Ice No Ice	6.16	5.55	0.10
						1/2" Ice	6.60	6.30	0.16
						1" Ice	7.03	7.00	0.22
LNX-6515DS-A1M w/ Mount Pipe	A	From Leg	4.00 0.00 0.00	0.000	165.00	1" Ice No Ice	11.68	9.84	0.08
						1/2" Ice	12.40	11.37	0.17
						1" Ice	13.14	12.91	0.27
LNX-6515DS-A1M w/ Mount Pipe	B	From Leg	4.00 0.00 0.00	0.000	165.00	1" Ice No Ice	11.68	9.84	0.08
						1/2" Ice	12.40	11.37	0.17
						1" Ice	13.14	12.91	0.27
LNX-6515DS-A1M w/ Mount Pipe	C	From Leg	4.00 0.00 0.00	0.000	165.00	1" Ice No Ice	11.68	9.84	0.08
						1/2" Ice	12.40	11.37	0.17
						1" Ice	13.14	12.91	0.27
AIR 32 B4A/B2P w/ Mount Pipe	A	From Leg	4.00 0.00 0.00	0.000	165.00	1" Ice No Ice	7.09	6.37	0.13
						1/2" Ice	7.56	7.23	0.19
						1" Ice	8.02	7.97	0.26
AIR 32 B4A/B2P w/ Mount Pipe	B	From Leg	4.00 0.00 0.00	0.000	165.00	1" Ice No Ice	7.09	6.37	0.13
						1/2" Ice	7.56	7.23	0.19
						1" Ice	8.02	7.97	0.26

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz	Lateral					
AIR 32 B4A/B2P w/ Mount Pipe	C	From Leg	4.00	0.000	165.00	No Ice	7.09	6.37	0.13
			0.00			1/2"	7.56	7.23	0.19
			0.00			Ice	8.02	7.97	0.26
KRY 112 71	A	From Leg	4.00	0.000	165.00	No Ice	0.58	0.40	0.01
			0.00			1/2"	0.69	0.49	0.02
			0.00			Ice	0.80	0.59	0.03
KRY 112 71	B	From Leg	4.00	0.000	165.00	No Ice	0.58	0.40	0.01
			0.00			1/2"	0.69	0.49	0.02
			0.00			Ice	0.80	0.59	0.03
KRY 112 71	C	From Leg	4.00	0.000	165.00	No Ice	0.58	0.40	0.01
			0.00			1/2"	0.69	0.49	0.02
			0.00			Ice	0.80	0.59	0.03
RRUS 11 B12	A	From Leg	4.00	0.000	165.00	No Ice	2.83	1.18	0.05
			0.00			1/2"	3.04	1.33	0.07
			0.00			Ice	3.26	1.48	0.10
RRUS 11 B12	B	From Leg	4.00	0.000	165.00	No Ice	2.83	1.18	0.05
			0.00			1/2"	3.04	1.33	0.07
			0.00			Ice	3.26	1.48	0.10
RRUS 11 B12	C	From Leg	4.00	0.000	165.00	No Ice	2.83	1.18	0.05
			0.00			1/2"	3.04	1.33	0.07
			0.00			Ice	3.26	1.48	0.10
*****									

### Truss-Leg Properties

Section Designation	Area	Area Ice	Self Weight	Ice Weight	Equiv. Diameter	Equiv. Diameter	Leg Area
	in <sup>2</sup>	in <sup>2</sup>	K	K	r	r	in <sup>2</sup>
					in	Ice in	
Pirod 105216 (12x1.25)	2176.93	6534.58	0.60	2.48	7.56	22.69	3.68
Pirod 105217 (12x1.5)	2303.92	6585.93	0.71	2.51	8.00	22.87	5.30
Pirod 105217 (12x1.5)	2303.92	6554.05	0.71	2.49	8.00	22.76	5.30
Pirod 105218 (12x1.75)	2432.86	6587.02	0.85	2.51	8.45	22.87	7.22
Pirod 105218 (12x1.75)	2432.86	6536.27	0.85	2.47	8.45	22.70	7.22
Pirod 105219 (12x2)	2608.79	6534.42	1.22	2.45	9.06	22.69	9.42
Pirod 105219 (12x2)	2608.79	6387.80	1.22	2.28	9.06	22.18	9.42

### Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice

Comb. No.	Description
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

**Maximum Reactions**

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg C	Max. Vert	18	282.35	22.92	-13.20
	Max. H <sub>x</sub>	18	282.35	22.92	-13.20
	Max. H <sub>z</sub>	7	-250.94	-20.47	11.81
	Min. Vert	7	-250.94	-20.47	11.81
	Min. H <sub>x</sub>	7	-250.94	-20.47	11.81
	Min. H <sub>z</sub>	18	282.35	22.92	-13.20
Leg B	Max. Vert	10	283.27	-22.88	-13.31
	Max. H <sub>x</sub>	23	-250.26	20.41	11.88
	Max. H <sub>z</sub>	23	-250.26	20.41	11.88
	Min. Vert	23	-250.26	20.41	11.88
	Min. H <sub>x</sub>	10	283.27	-22.88	-13.31
	Min. H <sub>z</sub>	10	283.27	-22.88	-13.31
Leg A	Max. Vert	2	282.48	0.11	26.46
	Max. H <sub>x</sub>	21	11.11	0.76	0.90

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
	Max. H <sub>z</sub>	2	282.48	0.11	26.46
	Min. Vert	15	-250.84	-0.09	-23.63
	Min. H <sub>x</sub>	11	-122.43	-0.76	-11.75
	Min. H <sub>z</sub>	15	-250.84	-0.09	-23.63

**Maximum Tower Deflections - Service Wind**

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 170	7.97	46	0.482	0.018
T2	170 - 150	6.91	44	0.470	0.017
T3	150 - 130	4.98	44	0.413	0.010
T4	130 - 120	3.38	44	0.320	0.003
T5	120 - 100	2.76	44	0.264	0.001
T6	100 - 80	1.79	44	0.196	0.001
T7	80 - 60	1.08	42	0.135	0.001
T8	60 - 40	0.59	42	0.094	0.001
T9	40 - 20	0.26	42	0.055	0.001
T10	20 - 0	0.07	43	0.027	0.000

**Critical Deflections and Radius of Curvature - Service Wind**

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
180.00	Platform Mount [LP 405-1]	46	7.97	0.482	0.018	35068
165.00	Sector Mount [SM 402-3]	44	6.40	0.460	0.016	16953

**Maximum Tower Deflections - Design Wind**

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 170	31.93	16	1.926	0.074
T2	170 - 150	27.69	12	1.878	0.071
T3	150 - 130	19.94	12	1.652	0.039
T4	130 - 120	13.54	12	1.281	0.015
T5	120 - 100	11.05	12	1.059	0.009
T6	100 - 80	7.16	12	0.784	0.004
T7	80 - 60	4.32	8	0.541	0.005
T8	60 - 40	2.34	8	0.376	0.004
T9	40 - 20	1.02	8	0.222	0.003
T10	20 - 0	0.28	10	0.109	0.001

**Critical Deflections and Radius of Curvature - Design Wind**

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
180.00	Platform Mount [LP 405-1]	16	31.93	1.926	0.074	8823
165.00	Sector Mount [SM 402-3]	12	25.64	1.838	0.065	4281

### Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
T1	180	Leg	A325N	0.63	5	4.36	24.85	0.175	1	Bolt DS
T2	170	Leg	A325N	0.75	5	15.67	35.78	0.438	1	Bolt DS
T3	150	Leg	A325N	1.00	6	21.37	53.01	0.403	1	Bolt Tension
T4	130	Leg	A325N	1.00	6	21.06	53.01	0.397	1	Bolt Tension
		Diagonal	A325N	1.00	1	6.55	10.66	0.614	1	Member Block Shear
T5	120	Leg	A325N	1.00	6	25.00	53.01	0.472	1	Bolt Tension
		Diagonal	A325N	1.00	1	4.49	10.66	0.421	1	Member Block Shear
T6	100	Leg	A325N	1.00	6	28.22	53.01	0.532	1	Bolt Tension
		Diagonal	A325N	1.00	1	4.06	10.66	0.381	1	Member Block Shear
T7	80	Leg	A325N	1.00	6	31.48	53.01	0.594	1	Bolt Tension
		Diagonal	A325N	1.00	1	4.64	11.68	0.397	1	Member Block Shear
T8	60	Leg	A325N	1.00	6	34.73	53.01	0.655	1	Bolt Tension
		Diagonal	A325N	1.00	1	5.11	11.68	0.437	1	Member Block Shear
T9	40	Leg	A325N	1.25	6	37.96	82.83	0.458	1	Bolt Tension
		Diagonal	A325N	1.25	1	5.80	20.30	0.285	1	Member Block Shear
T10	20	Diagonal	A325N	1.25	1	6.67	20.30	0.328	1	Member Block Shear

### Compression Checks

### Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio P <sub>u</sub> / φP <sub>n</sub>
T1	180 - 170	1 1/2" solid	10.00	2.25	72.0 K=1.00	1.77	-18.97	54.43	0.349 <sup>1</sup>
T2	170 - 150	2" solid	20.00	2.36	56.6 K=1.00	3.14	-73.80	111.84	0.660 <sup>1</sup>
T3	150 - 130	2 1/4" solid	20.00	2.36	50.3 K=1.00	3.98	-132.48	148.69	0.891 <sup>1</sup>
T4	130 - 120	Pirod 105216 (12x1.25)	10.02	10.02	45.4 K=1.00	3.68	-133.47	142.49	0.937 <sup>1</sup>
T5	120 - 100	Pirod 105217 (12x1.5)	20.03	10.02	37.8 K=1.00	5.30	-160.20	214.86	0.746 <sup>1</sup>
T6	100 - 80	Pirod 105217 (12x1.5)	20.03	10.02	37.8 K=1.00	5.30	-182.81	214.86	0.851 <sup>1</sup>
T7	80 - 60	Pirod 105218 (12x1.75)	20.03	10.02	32.4 K=1.00	7.22	-206.10	300.68	0.685 <sup>1</sup>
T8	60 - 40	Pirod 105218 (12x1.75)	20.03	10.02	32.4 K=1.00	7.22	-229.38	300.68	0.763 <sup>1</sup>
T9	40 - 20	Pirod 105219 (12x2)	20.03	10.02	28.4 K=1.00	9.42	-253.59	399.87	0.634 <sup>1</sup>
T10	20 - 0	Pirod 105219 (12x2)	20.03	10.02	28.4 K=1.00	9.42	-276.44	399.87	0.691 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	$L_d$ ft	$Kl/r$	$\phi P_n$ K	$A$ in <sup>2</sup>	$V_u$ K	$\phi V_n$ K	Stress Ratio
T4	130 - 120	0.5	1.48	121.0	165.67	0.20	1.11	3.29	0.337
T5	120 - 100	0.5	1.47	120.0	238.57	0.20	0.88	3.34	0.265
T6	100 - 80	0.5	1.47	120.0	238.57	0.20	0.25	3.34	0.076
T7	80 - 60	0.5	1.46	119.0	324.71	0.20	0.21	3.38	0.062
T8	60 - 40	0.5	1.46	119.0	324.71	0.20	0.25	3.38	0.073
T9	40 - 20	0.625	1.45	94.4	424.12	0.31	0.25	6.96	0.037
T10	20 - 0	0.625	1.45	94.4	424.12	0.31	0.93	6.96	0.135

### Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	$L$ ft	$L_u$ ft	$Kl/r$	$A$ in <sup>2</sup>	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 170	3/4" solid	4.59	2.22	128.0 K=0.90	0.44	-3.34	6.09	0.549 <sup>1</sup>
T2	170 - 150	7/8" solid	5.04	2.44	120.6 K=0.90	0.60	-5.48	9.34	0.588 <sup>1</sup>
T3	150 - 130	1" solid	5.12	2.47	107.6 K=0.91	0.79	-6.22	15.16	0.411 <sup>1</sup>
T4	130 - 120	L 2.5 x 2.5 x 3/16	11.42	4.98	120.8 K=1.00	0.90	-7.02	13.56	0.517 <sup>1</sup>
T5	120 - 100	L 2.5 x 2.5 x 3/16	11.93	5.38	130.5 K=1.00	0.90	-4.73	11.92	0.397 <sup>1</sup>
T6	100 - 80	L 2.5 x 2.5 x 3/16	13.80	6.33	153.4 K=1.00	0.90	-4.60	8.66	0.531 <sup>1</sup>
T7	80 - 60	L 3 x 3 x 3/16	15.24	7.08	142.5 K=1.00	1.09	-5.01	12.12	0.413 <sup>1</sup>
T8	60 - 40	L 3 x 3 x 3/16	16.80	7.88	158.6 K=1.00	1.09	-5.51	9.79	0.563 <sup>1</sup>
T9	40 - 20	L 3 x 3 x 5/16	18.45	8.68	176.8 K=1.00	1.78	-6.14	12.87	0.477 <sup>1</sup>
T10	20 - 0	L 3 x 3 x 5/16	20.16	9.54	194.4 K=1.00	1.78	-7.37	10.64	0.693 <sup>1</sup>

<sup>1</sup>  $P_u / \phi P_n$  controls

### Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	$L$ ft	$L_u$ ft	$Kl/r$	$A$ in <sup>2</sup>	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 170	7/8" solid	4.00	3.88	148.8 K=0.70	0.60	-0.55	6.14	0.090 <sup>1</sup>
T2	170 - 150	7/8" solid	4.37	4.20	161.3 K=0.70	0.60	-1.04	5.22	0.199 <sup>1</sup>
T3	150 - 130	7/8" solid	4.57	4.39	168.4 K=0.70	0.60	-1.84	4.79	0.385 <sup>1</sup>

<sup>1</sup>  $P_u / \phi P_n$  controls



### Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 170	7/8" solid	4.00	3.88	148.8 K=0.70	0.60	-1.75	6.14	0.285 <sup>1</sup>
T2	170 - 150	7/8" solid	4.01	3.85	147.7 K=0.70	0.60	-1.92	6.22	0.308 <sup>1</sup>
T3	150 - 130	1" solid	4.51	4.33	145.4 K=0.70	0.79	-2.08	8.40	0.248 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Bottom Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 170	7/8" solid	4.00	3.88	148.8 K=0.70	0.60	-1.49	6.14	0.243 <sup>1</sup>
T2	170 - 150	7/8" solid	4.49	4.32	165.9 K=0.70	0.60	-2.58	4.94	0.522 <sup>1</sup>
T3	150 - 130	1" solid	4.99	4.80	161.2 K=0.70	0.79	-2.72	6.83	0.399 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 170	1 1/2" solid	10.00	0.50	16.0	1.77	18.59	79.52	0.234 <sup>1</sup>
T2	170 - 150	2" solid	20.00	0.57	13.6	2.19	71.92	106.69	0.674 <sup>1</sup> #
T3	150 - 130	2 1/4" solid	20.00	0.57	12.1	3.98	128.22	178.92	0.717 <sup>1</sup>
T4	130 - 120	Pirod 105216 (12x1.25)	10.02	10.02	45.4	3.68	126.33	165.67	0.763 <sup>1</sup>
T5	120 - 100	Pirod 105217 (12x1.5)	20.03	10.02	37.8	5.30	149.98	238.57	0.629 <sup>1</sup>
T6	100 - 80	Pirod 105217 (12x1.5)	20.03	10.02	37.8	5.30	169.34	238.57	0.710 <sup>1</sup>
T7	80 - 60	Pirod 105218 (12x1.75)	20.03	10.02	32.4	7.22	188.90	324.71	0.582 <sup>1</sup>
T8	60 - 40	Pirod 105218 (12x1.75)	20.03	10.02	32.4	7.22	208.41	324.71	0.642 <sup>1</sup>
T9	40 - 20	Pirod 105219 (12x2)	20.03	10.02	28.4	9.42	227.74	424.12	0.537 <sup>1</sup>
T10	20 - 0	Pirod 105219 (12x2)	20.03	10.02	28.4	9.42	245.69	424.12	0.579 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

# Based on net area of leg in section below

### Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	L <sub>d</sub> ft	Kl/r	φP <sub>n</sub> K	A in <sup>2</sup>	V <sub>u</sub> K	φV <sub>n</sub> K	Stress Ratio
T4	130 - 120	0.5	1.48	121.0	165.67	0.20	1.11	3.29	0.337

Section No.	Elevation ft	Diagonal Size	$L_d$ ft	$KI/r$	$\phi P_n$ K	$A$ in <sup>2</sup>	$V_u$ K	$\phi V_n$ K	Stress Ratio
T5	120 - 100	0.5	1.47	120.0	238.57	0.20	0.88	3.34	0.265
T6	100 - 80	0.5	1.47	120.0	238.57	0.20	0.25	3.34	0.076
T7	80 - 60	0.5	1.46	119.0	324.71	0.20	0.21	3.38	0.062
T8	60 - 40	0.5	1.46	119.0	324.71	0.20	0.25	3.38	0.073
T9	40 - 20	0.625	1.45	94.4	424.12	0.31	0.25	6.96	0.037
T10	20 - 0	0.625	1.45	94.4	424.12	0.31	0.93	6.96	0.135

### Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	$L$ ft	$L_u$ ft	$KI/r$	$A$ in <sup>2</sup>	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 170	3/4" solid	4.59	2.22	142.3	0.44	3.36	19.88	0.169 <sup>1</sup>
T2	170 - 150	7/8" solid	5.04	2.44	134.0	0.60	5.61	27.06	0.207 <sup>1</sup>
T3	150 - 130	1" solid	5.12	2.47	118.7	0.79	5.92	35.34	0.168 <sup>1</sup>
T4	130 - 120	L 2.5 x 2.5 x 3/16	11.42	4.98	80.0	0.52	6.55	22.55	0.290 <sup>1</sup>
T5	120 - 100	L 2.5 x 2.5 x 3/16	11.93	5.38	86.2	0.52	4.49	22.55	0.199 <sup>1</sup>
T6	100 - 80	L 2.5 x 2.5 x 3/16	13.80	6.33	100.7	0.52	4.06	22.55	0.180 <sup>1</sup>
T7	80 - 60	L 3 x 3 x 3/16	15.24	7.08	93.1	0.66	4.64	28.67	0.162 <sup>1</sup>
T8	60 - 40	L 3 x 3 x 3/16	16.80	7.88	103.4	0.66	5.11	28.67	0.178 <sup>1</sup>
T9	40 - 20	L 3 x 3 x 5/16	18.45	8.68	116.3	1.01	5.80	44.05	0.132 <sup>1</sup>
T10	20 - 0	L 3 x 3 x 5/16	20.16	9.54	127.6	1.01	6.67	44.05	0.151 <sup>1</sup>

<sup>1</sup>  $P_u / \phi P_n$  controls

### Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	$L$ ft	$L_u$ ft	$KI/r$	$A$ in <sup>2</sup>	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 170	7/8" solid	4.00	3.88	212.6	0.60	0.73	27.06	0.027 <sup>1</sup>
T2	170 - 150	7/8" solid	4.37	4.20	230.5	0.60	1.24	27.06	0.046 <sup>1</sup>
T3	150 - 130	7/8" solid	4.57	4.39	240.6	0.60	2.06	27.06	0.076 <sup>1</sup>

<sup>1</sup>  $P_u / \phi P_n$  controls

### Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	$L$ ft	$L_u$ ft	$KI/r$	$A$ in <sup>2</sup>	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 170	7/8" solid	4.00	3.88	212.6	0.60	1.74	27.06	0.064 <sup>1</sup>
T2	170 - 150	7/8" solid	4.01	3.85	211.1	0.60	1.98	27.06	0.073 <sup>1</sup>
T3	150 - 130	1" solid	4.51	4.33	207.7	0.79	2.28	35.34	0.064 <sup>1</sup>

<sup>1</sup>  $P_u / \phi P_n$  controls

### Bottom Girt Design Data (Tension)

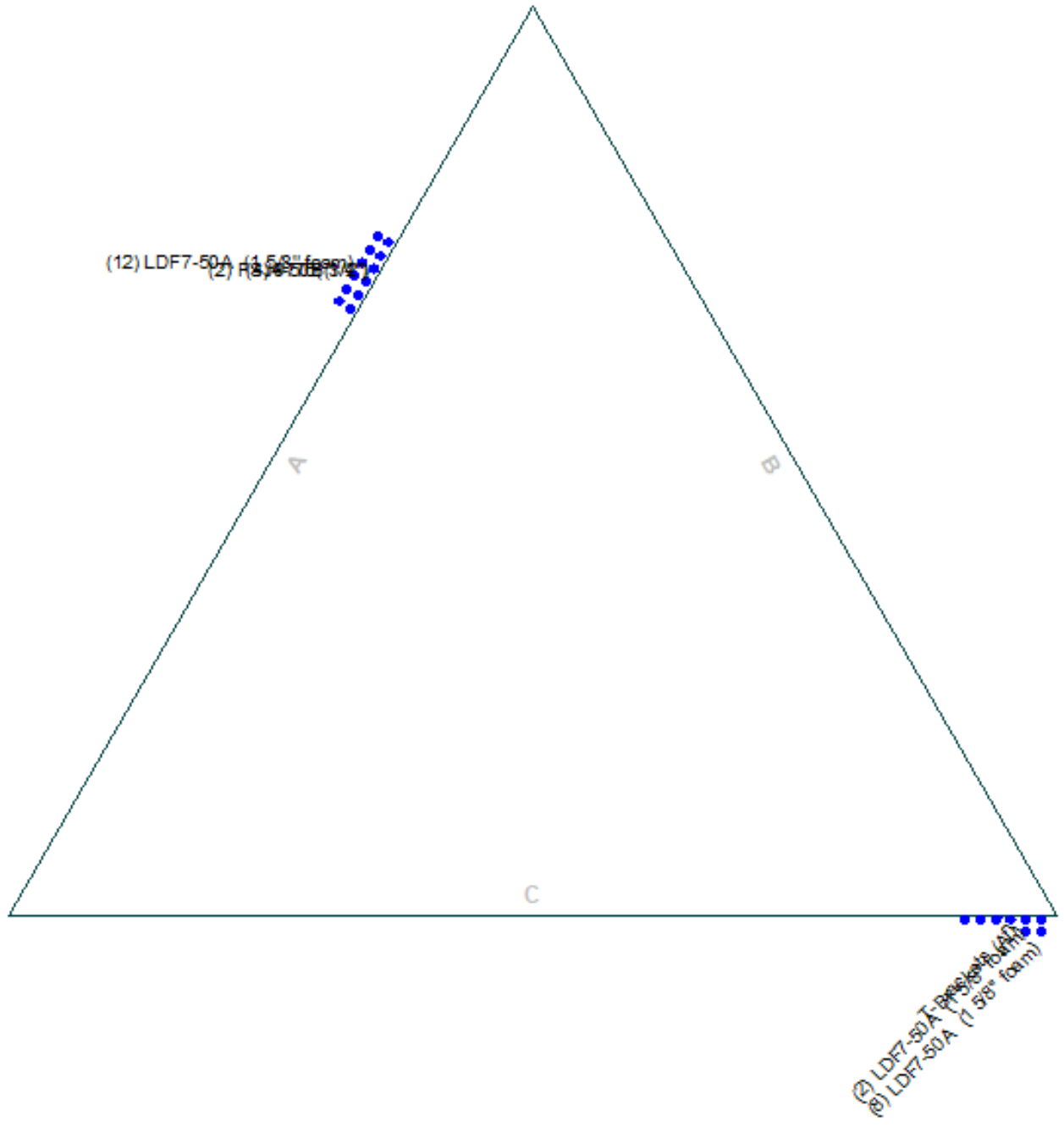
Section No.	Elevation ft	Size	L ft	$L_u$ ft	Kl/r	A in <sup>2</sup>	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 170	7/8" solid	4.00	3.88	212.6	0.60	1.50	27.06	0.055 <sup>1</sup>
T2	170 - 150	7/8" solid	4.49	4.32	236.9	0.60	2.50	27.06	0.092 <sup>1</sup>
T3	150 - 130	1" solid	4.99	4.80	230.3	0.79	2.99	35.34	0.085 <sup>1</sup>

<sup>1</sup>  $P_u / \phi P_n$  controls

### Section Capacity Table

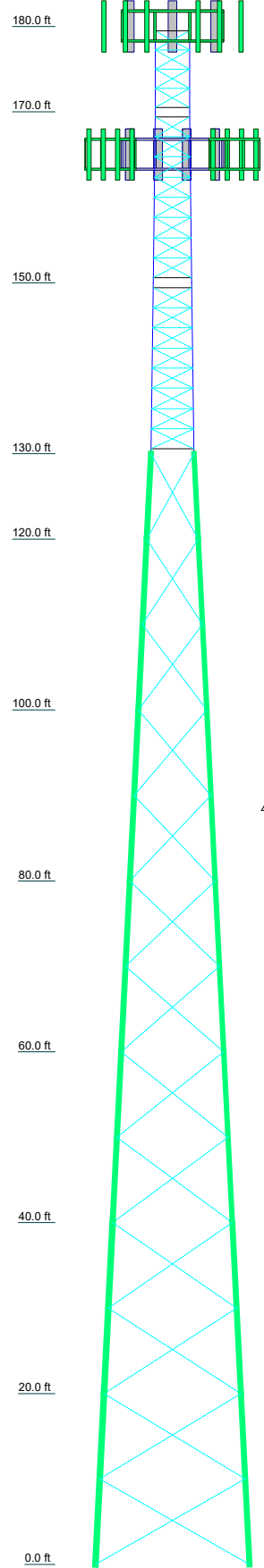
Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail	
T1	180 - 170	Leg	1 1/2" solid	3	-18.97	54.43	34.9	Pass	
T2	170 - 150	Leg	2" solid	39	71.92	106.69	67.4	Pass	
T3	150 - 130	Leg	2 1/4" solid	101	-132.48	148.69	89.1	Pass	
T4	130 - 120	Leg	Pirod 105216 (12x1.25)	165	-133.47	142.49	93.7	Pass	
T5	120 - 100	Leg	Pirod 105217 (12x1.5)	175	-160.20	214.86	74.6	Pass	
T6	100 - 80	Leg	Pirod 105217 (12x1.5)	190	-182.81	214.86	85.1	Pass	
T7	80 - 60	Leg	Pirod 105218 (12x1.75)	205	-206.10	300.68	68.5	Pass	
T8	60 - 40	Leg	Pirod 105218 (12x1.75)	220	-229.38	300.68	76.3	Pass	
T9	40 - 20	Leg	Pirod 105219 (12x2)	235	-253.59	399.87	63.4	Pass	
T10	20 - 0	Leg	Pirod 105219 (12x2)	250	-276.44	399.87	69.1	Pass	
T1	180 - 170	Diagonal	3/4" solid	15	-3.34	6.09	54.9	Pass	
T2	170 - 150	Diagonal	7/8" solid	50	-5.48	9.34	58.8	Pass	
T3	150 - 130	Diagonal	1" solid	164	-6.22	15.16	41.1	Pass	
T4	130 - 120	Diagonal	L 2.5 x 2.5 x 3/16	172	-7.02	13.56	51.7	Pass	
T5	120 - 100	Diagonal	L 2.5 x 2.5 x 3/16	188	-4.73	11.92	39.7	Pass	
T6	100 - 80	Diagonal	L 2.5 x 2.5 x 3/16	196	-4.60	8.66	53.1	Pass	
T7	80 - 60	Diagonal	L 3 x 3 x 3/16	210	-5.01	12.12	41.3	Pass	
T8	60 - 40	Diagonal	L 3 x 3 x 3/16	225	-5.51	9.79	56.3	Pass	
T9	40 - 20	Diagonal	L 3 x 3 x 5/16	240	-6.14	12.87	47.7	Pass	
T10	20 - 0	Diagonal	L 3 x 3 x 5/16	255	-7.37	10.64	69.3	Pass	
T1	180 - 170	Horizontal	7/8" solid	30	-0.55	6.14	9.0	Pass	
T2	170 - 150	Horizontal	7/8" solid	59	-1.04	5.22	19.9	Pass	
T3	150 - 130	Horizontal	7/8" solid	158	-1.84	4.79	38.5	Pass	
T1	180 - 170	Top Girt	7/8" solid	6	-1.75	6.14	28.5	Pass	
T2	170 - 150	Top Girt	7/8" solid	42	-1.92	6.22	30.8	Pass	
T3	150 - 130	Top Girt	1" solid	105	-2.08	8.40	24.8	Pass	
T1	180 - 170	Bottom Girt	7/8" solid	7	-1.49	6.14	24.3	Pass	
T2	170 - 150	Bottom Girt	7/8" solid	43	-2.58	4.94	52.2	Pass	
T3	150 - 130	Bottom Girt	1" solid	107	-2.72	6.83	39.9	Pass	
							Summary		
							Leg (T4)	93.7	Pass
							Diagonal (T10)	69.3	Pass
							Horizontal (T3)	38.5	Pass
							Top Girt (T2)	30.8	Pass
							Bottom Girt (T2)	52.2	Pass
							Bolt Checks	65.5	Pass
							<b>RATING =</b>	<b>93.7</b>	<b>Pass</b>

### APPENDIX B BASE LEVEL DRAWING



**APPENDIX C**  
**ADDITIONAL CALCULATIONS**

Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10
Legs	SR 1 1/2" solid	SR 2" solid	SR 2 1/4" solid	A	Pirod 105217 (12x1.5)	Pirod 105218 (12x1.75)	Pirod 105219 (12x2)			
Leg Grade	SR 3/4" solid	SR 7/8" solid	SR 1" solid		L 2.5 x 2.5 x 3/16	L 3 x 3 x 3/16	L 3 x 3 x 5/16			
Diagonals		A572-50				A36				
Diagonal Grade						N.A.				
Top Girts		SR 7/8" solid	SR 1" solid			N.A.				
Bottom Girts		SR 7/8" solid	SR 1" solid			N.A.				
Horizontals			SR 7/8" solid			N.A.				
Face Width (ft)	4	4.5	5	6	8	10	12	14	16	18
# Panels @ (ft)	4 @ 2.25	16 @ 2.35833	16 @ 2.35833	16 @ 2.35833	16 @ 2.35833	13 @ 10	13 @ 10	13 @ 10	13 @ 10	13 @ 10
Weight (K)	0.4	1.3	1.7	1.1	2.6	2.7	3.3	5.0	5.2	26.5



### DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
Platform Mount [LP 405-1]	180	RRUS 4478 B14	180
7770.00 w/ Mount Pipe	180	RRUS 4478 B14	180
7770.00 w/ Mount Pipe	180	RRUS 4478 B14	180
7770.00 w/ Mount Pipe	180	RRUS 32 B66	180
(2) OPA-65R-LCUU-H6 w/ Mount Pipe	180	RRUS 32 B66	180
(2) OPA-65R-LCUU-H6 w/ Mount Pipe	180	RRUS 32 B66	180
(2) OPA-65R-LCUU-H6 w/ Mount Pipe	180	RRUS 32 B2	180
(2) LGP21401	180	RRUS 32 B2	180
(2) LGP21401	180	RRUS 32 B2	180
(2) LGP21401	180	(2) LGP21901	180
RRUS 32	180	(2) LGP21901	180
RRUS 32	180	(2) LGP21901	180
RRUS 32	180	Sector Mount [SM 402-3]	165
RRUS 11	180	AIR 21 B2A/B4P w/ Mount Pipe	165
RRUS 11	180	AIR 21 B2A/B4P w/ Mount Pipe	165
RRUS 11	180	AIR 21 B2A/B4P w/ Mount Pipe	165
DC6-48-60-18-8F	180	LNx-6515DS-A1M w/ Mount Pipe	165
DC6-48-60-18-8F	180	LNx-6515DS-A1M w/ Mount Pipe	165
RRUS 12	180	LNx-6515DS-A1M w/ Mount Pipe	165
RRUS 12	180	AIR 32 B4A/B2P w/ Mount Pipe	165
RRUS 12	180	AIR 32 B4A/B2P w/ Mount Pipe	165
RRUS A2 MODULE	180	AIR 32 B4A/B2P w/ Mount Pipe	165
RRUS A2 MODULE	180	KRY 112 71	165
RRUS A2 MODULE	180	KRY 112 71	165
GPS	180	KRY 112 71	165
80010965 w/ Mount Pipe	180	RRUS 11 B12	165
80010965 w/ Mount Pipe	180	RRUS 11 B12	165
80010965 w/ Mount Pipe	180	RRUS 11 B12	165
DC6-48-60-18-8F	180		

### SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	Pirod 105216 (12x1.25)		

### MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A36	36 ksi	58 ksi

### TOWER DESIGN NOTES

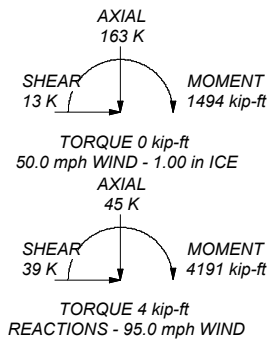
1. Tower is located in Hartford County, Connecticut.
2. Tower designed for Exposure C to the TIA-222-G Standard.
3. Tower designed for a 95.0 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50.0 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60.0 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: 93.7%

ALL REACTIONS  
ARE FACTORED

MAX. CORNER REACTIONS AT BASE:

DOWN: 283 K  
SHEAR: 26 K

UPLIFT: -251 K  
SHEAR: 24 K



TORQUE 4 kip-ft  
REACTIONS - 95.0 mph WIND

**Paul J. Ford and Company**  
250 East Broad St., Suite 600  
Columbus, OH 43215  
Phone: (614) 221-6679  
FAX:

Job: **180-ft Self-Support Tower / WESTHARTFORD\_DEXTERS**  
Project: **PJF# 64118-0001 / CT0001**  
Client: **Hirschfeld Communications, LLC** Drawn by: **jsomme** App'd:  
Code: **TIA-222-G** Date: **03/26/18** Scale: **NTS**  
Path:  Dwg No. **E-1**

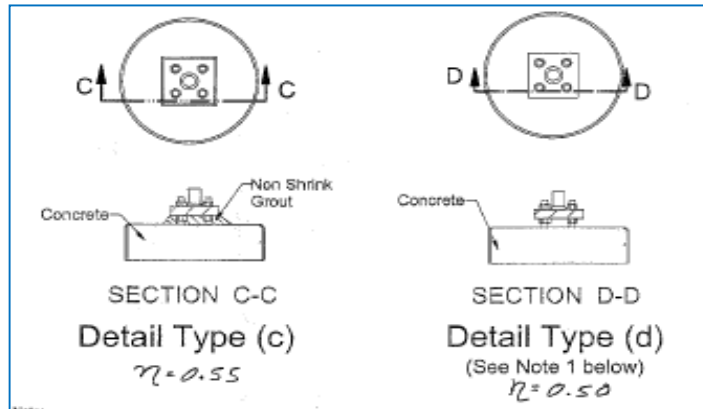
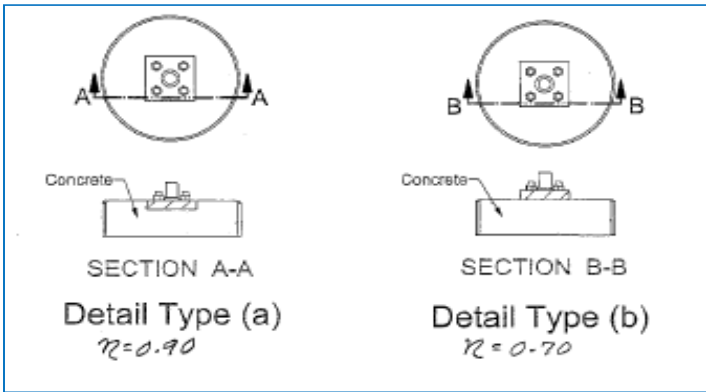
**Self-Support Tower Anchor Rod Capacity - TIA-G**

**Loads**

Uplift :	251	kips	1.00	Maximum Ratio
Shear :	24	kips		

**Existing Anchor Rods**

Anchor Rod Condition (n) :	0.55	
Anchor Rod $\phi$ :	1 1/4	in
Anchor Rod Quantity :	6	
Anchor Rod Grade :	A687	
$F_y$ :	105	ksi
$F_u$ :	150	ksi
Threads per Inch	7	
Total Net Tensile Area	5.81	in <sup>2</sup>
$\phi$ :	0.8	
Total Anchor Rod Capacity $\phi R_{nt}$ :	697.76	kip
Anchor Rod Ratio :	0.422	



**Factored Foundation Loads:**

Factored Axial Load (+Comp, -Ten) =	<b>283</b>	<b>-251</b>	kips
Factored Horiz. Load at Top of Pier =	<b>26</b>	<b>24</b>	kips
Factored OTM at Top of Pier =	<b>0</b>	<b>0</b>	k-ft

**LRFD Resistance and Load Factors:**

$\Phi$	Dead Load Factors		
Soil Bearing =	<b>0.75</b>	1.2	0.9
Soil Weight =	<b>0.75</b>	1.2	0.9
Concrete Weight =	<b>0.75</b>	1.2	0.9

**Soil Properties:**

Depth to Water Table =	<b>99</b>	ft
Uplift Cone from	<b>Top</b>	of footing
Depth to Ignore for Uplift and PP =	<b>3.33</b>	ft

Layer Thk ft	Soil Density pcf	Cohesion ksf	Friction Angle degrees	Ult Bearing ksf	Depth ft
<b>3.5</b>	<b>100</b>	<b>0</b>	<b>28</b>	<b>12</b>	<b>3.50</b>

**Dimensions:**

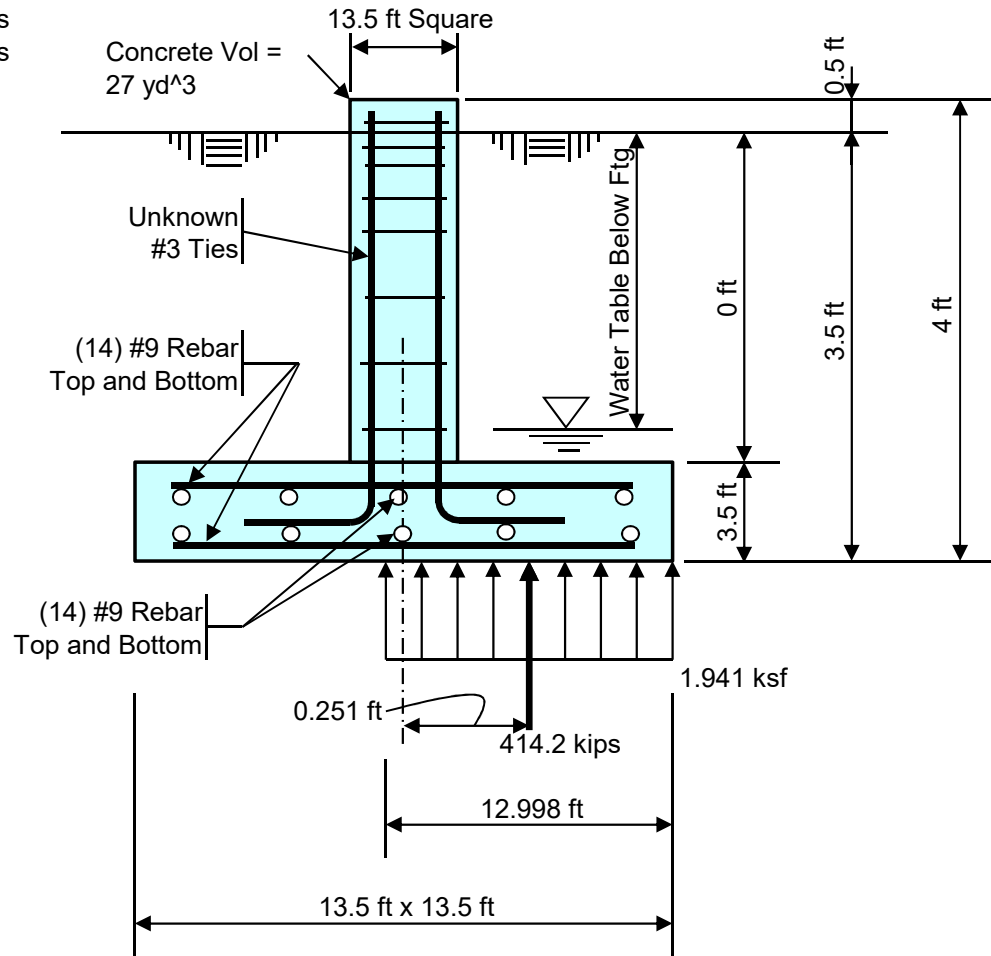
Pier Shape =	<b>Square</b>
Pier Width =	<b>13.5</b> ft Square
Pier Height above Grade =	<b>0.5</b> ft
Depth to Bottom of Footing =	<b>3.5</b> ft
Footing Thickness =	<b>3.5</b> ft
Footing Width, B =	<b>13.5</b> ft
Footing Length, L =	<b>13.5</b> ft

**Concrete:**

Concrete Strength =	<b>3</b>	ksi
Rebar Strength =	<b>60</b>	ksi

**Summary Results:**

Maximum Net Soil Bearing =	<b>1.941</b>	ksf	Required	<b>9.000</b>	ksf	Available
Punching Shear Stress =	<b>0.000</b>	ksi		<b>0.159</b>	ksi	
Bending Shear Stress =	<b>-4.7</b>	kips		<b>496.6</b>	kips	
Bending Moment =	<b>0.004</b>	in / in		<b>0.0</b>	in / in	
Conc Pier Reinforcing Steel =						Rebar Unknown



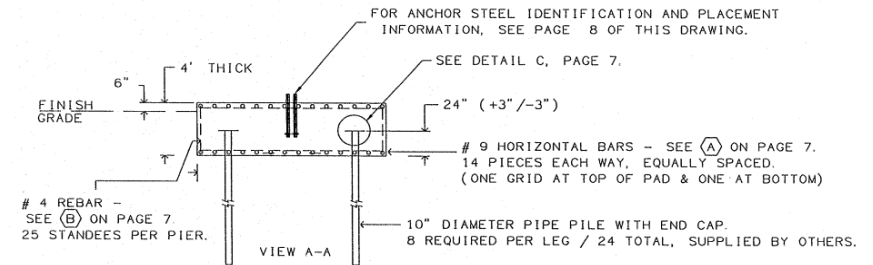
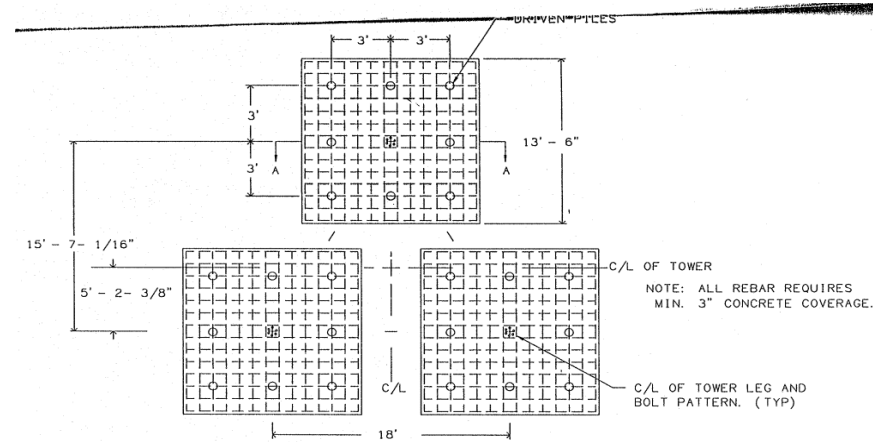
Total Pad Reinf Stl =	<b>28.00</b>	in <sup>2</sup> >= 12.25 in <sup>2</sup> = Min Stl, OK
Total Pier Reinf Stl =		
Footing Thickness =	<b>3.50</b>	ft >= 0.75 ft = Min Ftg Thk, OK

Stress Ratio =	<b>21.6%</b>	in Soil Bearing
Stress Ratio =	<b>0.0%</b>	in Punching Shear
Stress Ratio =	<b>0.9%</b>	in Bending Shear
Stress Ratio =	<b>9.1%</b>	in Bending Moment
Stress Ratio =		in Pier Rebar



**West Hartford Foundation Analysis**

Uplift (kips):	251
Compression (kips):	283
Concrete Weight (kcf):	0.15
Mat Length/Width (ft):	13.5
Mat Depth (ft):	4
Mat Weight (kips):	109.4
Mat Bearing Area (ft <sup>2</sup> ):	182.3
Pile Quantity	8
Pile Diameter (in):	10
Pile Length (ft):	50
Depth to Ignore (ft):	8
Total Pile Surface Area (ft <sup>2</sup> ):	879.6
Ultimate Bearing Pressure (ksf):	12
Ultimate Skin Friction (ksf):	1
$\phi_{soil}$ :	0.75
Mat Bearing Capacity (kips):	1640.3
Skin Friction Capacity (kips):	659.7
Total Uplift Load (kips):	251.0
Total Compression Load (kips):	414.2



Uplift Capacity (kips):	758.1
Compression Capacity (kips):	2300.0
<b>Uplift Usage Capacity:</b>	<b>33.1%</b>
<b>Compression Usage Capacity:</b>	<b>18.0%</b>

**STANDARD CONDITIONS FOR FURNISHING OF PROFESSIONAL ENGINEERING SERVICES ON EXISTING STRUCTURES BY PAUL J. FORD AND COMPANY**

- 1) Paul J. Ford and Company has not performed a site visit to verify the tower member sizes or the antenna/coax loading. If the existing conditions are not as represented on these drawings, we should be contacted immediately to evaluate the significance of the deviation.
- 2) No allowance was made for any damaged, missing, or rusted members. The analysis of this tower assumes that no physical deterioration has occurred in any of the structural components of the tower and that all the tower members have the same load carrying capacity as the day the tower was erected.
- 3) It is not possible to have all the detailed information to perform a thorough analysis of every structural sub-component of an existing tower. The structural analysis by Paul J. Ford and Company verifies the adequacy of the main structural members of the tower. Paul J. Ford and Company provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc.
- 4) This tower has been analyzed according to the minimum design wind loads recommended by the Telecommunications Industry Association Standard ANSI/TIA-222-G. If the owner or local or state agencies require a higher design wind load, Paul J. Ford and Company should be made aware of this requirement.
- 5) The attached sketches are a schematic representation of the tower that we have analyzed. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions and for the proper fit and clearance in the field.
- 6) Miscellaneous items such as antenna mounts etc. have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.



MASER CONSULTING  
— CONNECTICUT —

## Platform Mount Analysis

FOR  
CT5259 – West Hartford-Elmwood

FA # 10071358  
LTE – 4C/5C/6C/7C/Retrofit  
1030 New Britain Avenue  
West Hartford, CT 06110  
Hartford County

**Mount Utilization: 92.9%**

April 5, 2018

*Prepared For*

**AT&T**  
550 Cochituate Road  
Framingham, MA 01701

*Prepared By*

**Maser Consulting Connecticut**  
331 Newman Springs Road, Suite 203  
Red Bank, NJ 07701  
T: 732.383.1950



Petros E. Tsoukalas, P.E.  
Geographic Discipline Leader  
Connecticut License No. 32557



### **Objective:**

The objective of this report is to determine the capacity of the existing platform mount at the subject facility for the final wireless telecommunications configuration, per the applicable codes and standards.

### **Introduction:**

Maser Consulting Connecticut has reviewed the following documents in completing this report:

- RFDS 1737849 provided by Empire Telecom, dated October 9, 2017.
- Mount Structural Analysis Report prepared by Destek Engineering, dated August 19, 2015.
- As-Built Construction Drawings provided by Empire Telecom, dated October 10, 2016.

The proposed **AT&T** equipment is to be supported on the existing platform mount constructed of structural steel antenna support pipes supported by pipes and tubes at a centerline of approximately 180'-0" above ground level. This report is based only upon this information.

### **Codes, Standards and Loading:**

Maser Consulting Connecticut utilized the following codes and standards:

- 2016 Connecticut State Building Code
- Structural Standards for Antenna Supporting Structures and Antennas ANSI/TIA-222-G
  - Ultimate Wind Speed – 125 mph (3 Second Gust)
  - Nominal Wind Speed – 97 mph (3 Second Gust)
  - Exposure Category – B
  - Structural Class – II
  - Topographic Category – 1
  - Ice Wind – 50 mph
  - Ice Thickness – 1"
- Specification for Structural Steel Buildings ANSI/AISC 360-10, American Institute of Steel Construction (AISC)

Loading used in this analysis is found in **Appendix A** of this report.

### **Analysis Approach & Assumptions:**

The analysis approach used in this structural analysis is based on the premise that if the existing platform mount is structurally adequate to support the proposed equipment per the aforementioned codes and standards, or if the increase in the forces in the structure is deemed to be negligible or acceptable, then the proposed equipment can be installed as intended.

The existing platform mount has been modeled in RISA-3D, a comprehensive structural analysis program. The program performs design checks of structures under user specified loads. The user specified loads have been calculated separately based on the requirements of the above referenced codes. The program performs an analysis based on the steel code to determine the adequacy of the members, and produces the reactions at the connection points of the mounts to the existing structure. Additional calculations were then prepared to analyze the mount connection points with the proposed loading conditions.

### **General Site Design Assumption:**

- All engineering services are performed on the basis that the information used is current and correct.
- It is assumed that the telecommunication equipment supports, antenna supports, and existing structure have been designed by a registered licensed professional engineer for the existing loads acting on the structure, as required by all applicable codes, prior to the proposed modifications listed within this report, if any.
- It is assumed that information provided by the client regarding the structure itself, the antenna models, feed lines, and other relevant information is current and correct.
- It is the responsibility of the client to ensure that the information provided to Maser Consulting Connecticut and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that the original design, material production, fabrication, and erection of the existing structure was performed in accordance with accepted industry design standards and in accordance with all applicable codes. Further, it is assumed that the existing structure and appurtenances have been properly maintained in accordance with all applicable codes and manufacturer's specifications and no structural defects and/or deterioration to the structural members has occurred.
- It is assumed all other existing appurtenances, antennas, cables, etc. belonging to others have been installed and supported per code and per specifications so as not to damage any existing structural support members, and that any contributing loads from adjacent equipment has been taken into consideration for their design.
- All services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. Maser Consulting Connecticut is not responsible for the conclusion, opinions, and recommendations made by others based on the information we supply.

### **Site Specific Design Assumptions:**

The following design parameters have been utilized in this report:

- *Structural Steel HSS Tubes are constructed of A500 Grade B Steel*
- *The existing antenna pipes are 7'-0" long 2.0 STD pipes, constructed of A53 Grade B Steel*

### **Note about the Proposed Installation:**

- The proposed antennas shall be installed on existing antenna pipes in position 3 in all sectors.
- The proposed RRUS-32 B2 shall replace the existing RRUS-12+RRUS-A2, on the existing antenna pipe masts.
- The proposed RRUS-32 shall be installed on the existing antenna pipe masts, behind the antenna in position 2 in all sectors.
- The proposed RRUS-B14 4478 and RRUS-32 B66 shall be installed on proposed Ericsson SXX1250461/1 B2B RRU Mounting Brackets, which shall be attached to the existing antenna pipe masts in position 3 in all sectors.
- The proposed DC-6 shall be installed on a proposed 3'-0" long 2.0 STD pipe, which shall be attached to the existing bottom horizontals via crossover plates.

Please refer to the Final Construction Drawings for more details.

**Calculations:**

The calculations are found in Appendix A of this report.

**Conclusion:**

Maser Consulting Connecticut has determined the existing platform mount has **ADEQUATE** structural capacity to support the proposed loading. The existing platform mount has been determined to be stressed to a maximum of **92.9%** of its structural capacity with the maximum usage occurring at the antenna support pipes. Therefore, the proposed **AT&T** installation **CAN** be installed as intended.

The conclusions reached by Maser Consulting Connecticut in this evaluation are only applicable for the existing and proposed structural members supporting the proposed **AT&T** telecommunications installation described herein. Further, no structural qualifications are made or implied by this document for the existing structure.

Maser Consulting Connecticut reserves the right to amend this report if additional information about the existing members is provided. The conclusions reached by Maser Consulting Connecticut in this report are only valid for the appurtenances listed in this report. Any change to the installation will require a revision to this structural analysis.

We appreciate the opportunity to be of service on this project. If you should have any questions or require any additional information, please do not hesitate to call our office.

Sincerely,

Maser Consulting Connecticut



Petros E. Tsoukalas, P.E.  
Geographic Discipline Leader



Clara Basanti  
Project Engineer



MASER CONSULTING  
— CONNECTICUT —

## **APPENDIX A**



Client:	ATT	Computed By:	CB
Site Name:	CT05259 - West Hartford-Elmwood	Date:	4/5/2018
Project No.	17963019A	Verified By:	SMS
Title:	Antenna Mount Analysis	Page:	2

## ANALYSIS AND DESIGN





Client:	ATT	Computed By:	CB
Site Name:	CT05259 - West Hartford-Elmwood	Date:	4/5/2018
Project No.:	17963019A	Verified By:	SMS
Title:	Antenna Mount Analysis	Page:	1

Version 3.3

## 1. LOADING SUMMARY

Quantity	Manufacturer	Antenna/ Appurtenance	Status	Sector
3	POWERWAVE	7770	Existing	Alpha, Beta, & Gamma
6	CCI	OPA-65R-LCUU-H6	Existing	Alpha, Beta, & Gamma
<b>3</b>	<b>KATHREIN</b>	<b>80010965</b>	<b>Proposed</b>	<b>Alpha, Beta, &amp; Gamma</b>
<b>3</b>	<b>RAYCAP</b>	<b>DC6-48-60-18-8F</b>	<b>Existing/Proposed</b>	<b>Alpha, Beta, &amp; Gamma</b>
6	POWERWAVE	LGP 21401 TMA	Existing	Alpha, Beta, & Gamma
3	ERICSSON	RRUS 32	Existing	Alpha, Beta, & Gamma
3	ERICSSON	RRUS 11	Existing	Alpha, Beta, & Gamma
<b>3</b>	<b>ERICSSON</b>	<b>RRUS 4478 B14</b>	<b>Proposed</b>	<b>Alpha, Beta, &amp; Gamma</b>
<b>3</b>	<b>ERICSSON</b>	<b>RRUS 32 B66</b>	<b>Proposed</b>	<b>Alpha, Beta, &amp; Gamma</b>
<b>3</b>	<b>ERICSSON</b>	<b>RRUS 32 B2</b>	<b>Proposed</b>	<b>Alpha, Beta, &amp; Gamma</b>
<b>3</b>	<b>ERICSSON</b>	<b>RRUS E2 B29</b>	<b>Proposed</b>	<b>Alpha, Beta, &amp; Gamma</b>
<b>3</b>	<b>ERICSSON</b>	<b>RRUS 12</b>	<b>Proposed</b>	<b>Alpha, Beta, &amp; Gamma</b>
<b>6</b>	<b>KAELUS</b>	<b>DBC0061F1V51-2 Diplexer</b>	<b>Proposed</b>	<b>Alpha, Beta, &amp; Gamma</b>

(At ground level)

(At ground level)



Client:	ATT	Computed By:	CB
Site Name:	CT05259 - West Hartford-Elmwood	Date:	4/5/2018
Project No.:	17963019A	Verified By:	SMS
Title:	Antenna Mount Analysis	Page:	3

## I. DESIGN INPUTS

Calculations for gravity and lateral loading on equipment and support mounts are determined as per the ANSI/TIA-222-G Code, Addendum 2

### Wind Load Inputs Parameters

		Reference	Equation
Antenna Centerline	$z$ 180 ft		
Ultimate Wind Speed	$V_U$ 125 mph		
Nominal Wind Speed (3 sec. Gust):	$V$ 97 mph	Ref. 1, Eqn. 16-33	
Nominal Wind Speed with Ice (3 sec. gust):	$V_i$ 50.0 mph	(Figure a5-2a, p. 233)	
Service Wind Speed:	$V_s$ 60.0 mph	(Figure a5-2a, p. 233)	
Design Ice Thickness:	$t_i$ 1.00 in	(Figure A1-2a, p. 233)	
Exposure Category:	B	Ref. 3, Section 2.6.5.1	
Structure Class:	II	Ref. 3, Table 2-1	
Gust Effect Factor:	$G_h$ 0.85	Ref. 3, Section 2.6.7	
Wind Directionality Factor:	$K_d$ 0.85	Ref. 3, Table 2-2	
Topographic Category:	1	Ref. 3, Section 2.6.6.2	

### Wind Load Coefficients

#### Importance Factors:

Non-Iced:	$I$ 1	Ref. 3, Table 2-3
Iced:	$I_{ice}$ 1	(Table 2-3, P. 39)

#### Exposure Category Coefficients:

3-s Gust-Speed Power Law Exponent:	$\alpha$ 7.0	Ref. 3, Table 2-4	
Nominal Height of the Atmospheric Boundary Layer:	$Z_g$ 1200 ft	Ref. 3, Table 2-4	
Min. Value for $k_z$ :	$K_{z_{min}}$ 0.70	Ref. 3, Table 2-4	
Terrain Constant:	$K_e$ 0.90	Ref. 3, Table 2-4	
Velocity Pressure Exposure Coefficient:	$K_z$ 1.169	Ref. 3, Section 2.6.5.2	$=2.01 \cdot (z/z_g)^{2\alpha}$

#### Topographic Category Coefficients:

Topographic Constant:	$K_t$ N/A	Ref. 3, Table 2-5	
Height Attenuation Factor:	$f$ N/A	Ref. 3, Table 2-5	
Height Reduction Factor:	$K_h$ N/A	Ref. 3, Section 2.6.6.4	$=e^{-(z/H)}$
Topographic Factor:	$K_{zt}$ 1.00	Ref. 3, Section 2.6.6.4	$=[1+(K_e \cdot K_t/K_h)]^2$

#### Ice Accumulation:

Ice Velocity Pressure Exposure Coefficient:	$K_{iz}$ 1.18		$=(z/33)^{0.10}$
Factored Ice Thickness:	$t_{iz}$ 2.37 in	(Section 2.6.8, p. 16)	$=2.0 \cdot t_i \cdot I \cdot K_{iz} \cdot K_{zt}$
Ice Density:	$\rho_i$ 56.00 pcf		

#### Design Wind Pressures:

Velocity Pressure:	$q_z$ 23.85 psf	Ref. 3, Section 2.6.9.6	$=0.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V^2 \cdot I$
Velocity Pressure (With Ice):	$q_{zi}$ 6.36 psf	(Section 2.6.9.6, P. 25)	$=.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V_i^2 \cdot I$
Velocity Pressure (Service):	$q_{zs}$ 9.16 psf	(Section 2.6.9.6, P. 25)	$=.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V_s^2 \cdot I$



## II. CALCULATIONS

### • Wind Load on Appurtenances

Dimensions and Force Coefficients

Antenna/ Appurtenance	Non-Iced Condition								Iced Condition							
	Mounting Pipe			Equipment					Mounting Pipe			Equipment				
	Length (in)	Diameter (in)	Force Coefficient C <sub>a</sub>	Height (in)	Width (in)	Depth (in)	Force Coefficient		Length (in)	Diameter (in)	Force Coefficient C <sub>a</sub>	Height (in)	Width (in)	Depth (in)	Force Coefficient	
							C <sub>a Front</sub>	C <sub>a Side</sub>							C <sub>a Front</sub>	C <sub>a Side</sub>
7770	84.0	2.375	1.200	55.00	11.00	5.00	1.31	1.53	88.7	7.1	0.922	59.74	15.74	9.74	1.26	1.36
OPA-65R-LCUU-H6	84.0	2.375	1.200	72.30	14.40	7.30	1.31	1.50	88.7	7.1	0.922	77.04	19.14	12.04	1.27	1.37
80010965	84.0	2.375	1.200	78.70	20.00	6.90	1.26	1.55	88.7	7.1	0.922	83.44	24.74	11.64	1.24	1.41
DC6-48-60-18-8F	36.0	2.375	0.981	31.40	10.20	10.20	0.71	0.71	40.7	7.1	0.772	36.14	14.94	14.94	0.70	0.70
LGP 21401 TMA	0.0	0.000	0.000	13.80	14.40	3.70	1.20	1.25	0.0	0.0	0.000	18.54	19.14	8.44	1.20	1.20
RRUS 32	0.0	0.000	0.000	27.20	12.00	7.00	1.20	1.26	0.0	0.0	0.000	31.94	16.74	11.74	1.20	1.21
RRUS 11	0.0	0.000	0.000	19.70	2.60	7.20	1.42	1.21	0.0	0.0	0.000	24.44	7.34	11.94	1.24	1.20
RRUS 4478 B14	0.0	0.000	0.000	18.10	13.40	8.30	1.20	1.20	0.0	0.0	0.000	22.84	18.14	13.04	1.20	1.20
RRUS 32 B66	0.0	0.000	0.000	27.20	12.00	7.00	1.20	1.26	0.0	0.0	0.000	31.94	16.74	11.74	1.20	1.21
RRUS 32 B2	0.0	0.000	0.000	27.20	12.00	7.00	1.20	1.26	0.0	0.0	0.000	31.94	16.74	11.74	1.20	1.21
DBC0061F1V51-2 Diplexer	0.0	0.000	0.000	8.00	6.20	3.20	1.20	1.20	0.0	0.0	0.000	12.74	10.94	7.94	1.20	1.20

Antenna/ Appurtenance	# of Brackets	Non-Iced Condition				Iced Condition			
		Wind Force (lbs.)		Controlling Wind Force (lbs.)	Gravity (lbs.)	Wind Force (lbs.)		Controlling Wind Force (lbs.)	Gravity (lbs.)
		F <sub>N</sub>	F <sub>T</sub>			F <sub>N</sub>	F <sub>T</sub>		
7770	2	61.6	46.5	61.6	17.5	26.8	25.8	26.8	104.2
OPA-65R-LCUU-H6	2	98.5	72.4	98.5	20.3	37.0	34.8	37.0	172.1
80010965	2	141.1	76.0	141.1	54.3	48.8	36.5	48.8	236.8
DC6-48-60-18-8F	1	33.6	43.9	43.9	26.2	15.4	22.6	22.6	109.6
LGP 21401 TMA	1	33.6	9.0	33.6	30.0	16.0	7.0	16.0	77.1
RRUS 32	1	55.1	33.8	55.1	52.9	24.1	17.0	24.1	125.3
RRUS 11	1	10.2	24.2	24.2	55.7	8.3	13.1	13.1	59.1
RRUS 4478 B14	2	20.5	12.7	20.5	29.7	9.3	6.7	9.3	50.0
RRUS 32 B66	2	27.6	16.9	27.6	25.4	12.0	8.5	12.0	62.7
RRUS 32 B2	2	27.6	16.9	27.6	26.5	12.0	8.5	12.0	62.7
DBC0061F1V51-2 Diplexer	1	8.4	4.3	8.4	9.5	6.3	4.6	6.3	28.7

(Partially shielded by antenna)  
(Partially shielded by antenna)  
(Partially shielded by antenna)  
(Partially shielded by antenna)  
(Partially shielded by antenna)

\* ALL CALCULATED LOADS ARE PER MOUNTING BRACKET. TO GET THE TOTAL EQUIPMENT LOAD, MULTIPLY THE INDIVIDUAL LOADS BY THE NUMBER OF BRACKETS

### • Wind Load on Framing Members

Member Category	Member Shape	Length (in)	Member Surface	Non-Iced Condition					Iced Condition				
				Exposed Wind Height (in)	Force Coefficient C <sub>a</sub>	Wind Load (plf)	Exposed Wind Height (in)	Depth (in)	Length (in)	Force Coefficient C <sub>a</sub>	Wind Load (plf)	Ice Weight (plf)	
Pipe	Pipe 3.5	192	Round	4.00	1.20	8.11	8.74	8.74	196.74	1.14	4.50	18.44	
Pipe	Pipe 2.0	84	Round	2.38	1.20	4.81	7.11	7.11	88.74	0.92	2.95	13.74	
Pipe	Pipe 2.0	192	Round	2.38	1.20	4.81	7.11	7.11	196.74	1.20	3.85	13.74	
Pipe	Pipe 2.0	72	Round	2.38	1.20	4.81	7.11	7.11	76.74	0.88	2.83	13.74	
Pipe	Pipe 2.0	36	Round	2.38	0.98	3.94	7.11	7.11	40.74	0.77	2.47	13.74	
Square HSS	HSS 5x5	56.5	Square	5.00	1.54	13.03	9.74	9.74	61.24	1.37	6.00	27.33	
											Grating	24.45	



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## BASIC EQUATIONS

### ANSI/TIA-222-G Reference

Importance Factor:  $I := \begin{cases} 1.0 & \text{if Class} = \text{"II"} \\ 1.15 & \text{if Class} = \text{"III"} \end{cases}$  Table 2-3, Pg. 39

Force Coefficient:  
(Square)  $C_{f\_square}(h, w) := \begin{cases} 1.2 & \text{if } \frac{h}{w} \leq 2.5 \\ \left[ 1.2 + \frac{0.2}{4.5} \cdot \left( \frac{h}{w} - 2.5 \right) \right] & \text{if } \frac{h}{w} > 2.5 \wedge \frac{h}{w} \leq 7 \\ \left[ 1.4 + \frac{0.6}{18} \cdot \left( \frac{h}{w} - 7 \right) \right] & \text{if } \frac{h}{w} > 7 \wedge \frac{h}{w} \leq 25 \\ 2.0 & \text{otherwise} \end{cases}$  Table 2-8, P. 42

Force Coefficient:  
(Round)  $C_{f\_round}(h, w) := \begin{cases} 0.7 & \text{if } \frac{h}{w} \leq 2.5 \\ \left[ 0.7 + \frac{0.1}{4.5} \cdot \left( \frac{h}{w} - 2.5 \right) \right] & \text{if } \frac{h}{w} > 2.5 \wedge \frac{h}{w} \leq 7 \\ \left[ 0.8 + \frac{0.4}{18} \cdot \left( \frac{h}{w} - 7 \right) \right] & \text{if } \frac{h}{w} > 7 \wedge \frac{h}{w} \leq 25 \\ 1.2 & \text{otherwise} \end{cases}$  Table 2-8, P. 42

Terrain Exposure Constants: Table 2-4, P. 40

$$\alpha := \begin{cases} 7.0 & \text{if Exp} = \text{"B"} \\ 9.5 & \text{if Exp} = \text{"C"} \\ 11.5 & \text{if Exp} = \text{"D"} \end{cases} \quad Z_g := \begin{cases} 1200\text{ft} & \text{if Exp} = \text{"B"} \\ 900\text{ft} & \text{if Exp} = \text{"C"} \\ 700\text{ft} & \text{if Exp} = \text{"D"} \end{cases} \quad K_{zmin} := \begin{cases} 0.70 & \text{if Exp} = \text{"B"} \\ 0.85 & \text{if Exp} = \text{"C"} \\ 1.03 & \text{if Exp} = \text{"D"} \end{cases}$$



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## BASIC EQUATIONS

### ANSI/TIA-222-G Reference

Velocity Pressure Coefficient:

$$K_z(z) := \begin{cases} K_z \leftarrow \max \left[ 2.01 \cdot \left( \frac{z}{Z_g} \right)^{\frac{2}{\alpha}}, K_{zmin} \right] \\ K_z \leftarrow \min(K_z, 2.01) \end{cases}$$

$$K_z := K_z(z)$$

Section 2.6.5, P. 13

$$K_{zt}(z) := K_{zt} \leftarrow \begin{cases} 1.0 & \text{if Topo} = "1" \\ \text{otherwise} \\ \begin{cases} K_e \leftarrow \begin{cases} 0.90 & \text{if Exp} = "B" \\ 1.00 & \text{if Exp} = "C" \\ 1.10 & \text{if Exp} = "D" \end{cases} \\ K_t \leftarrow \begin{cases} 0.43 & \text{if Topo} = "2" \\ 0.53 & \text{if Topo} = "3" \\ 0.72 & \text{if Topo} = "4" \end{cases} \\ f \leftarrow \begin{cases} 1.25 & \text{if Topo} = "2" \\ 2.00 & \text{if Topo} = "3" \\ 1.50 & \text{if Topo} = "4" \end{cases} \\ K_h \leftarrow e^{\left( \frac{f \cdot z}{CH} \right)} \\ \left( 1 + \frac{K_e \cdot K_t}{K_h} \right)^2 \end{cases} \end{cases}$$

Section 2.6.6.4, p. 14

Table 2-4 p. 40

Table 2-5 p. 40

Table 2-5 p. 40

Section 2.6.6.4, P. 14

Section 2.6.6.4, P. 14

$$K_{zt} := K_{zt}(z)$$

Velocity Pressure:

Section 2.6.9.6, P. 25

$$q_z := 0.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V^2 \cdot I \text{ psf}$$



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## LOAD EQUATIONS

### WIND LOAD

Area (Normal):	$AN_{area} = H_{ant} \cdot W_{ant}$
Area (Side):	$AT_{area} = H_{ant} \cdot D_{ant}$
Force Coefficient (Normal):	$C_{fn} = C_{fsquare}(H_{ant}, W_{ant})$
Force Coefficient (Side):	$C_{fs} = C_{fsquare}(H_{ant}, D_{ant})$
Pipe Area (Normal):	$AN_p = \max[(L_p - H_{ant}) * D_p, 0]$
Pipe Area (Side):	$AT_p = L_p \cdot D_p$
Force Coefficient (Normal):	$C_{fp} = C_{fround}(L_p, D_p)$
Normal Effective Projected Area:	$E_{pan} = (C_{fn} \cdot AN_{area}) + (C_{fp} \cdot AN_p)$
Side Effective Projected Area:	$E_{pat} = (C_{fs} \cdot AT_{area}) + (C_{fp} \cdot AT_p)$
Effective Projected Area:	$EPA = \max(E_{pan}, E_{pat})$
Wind Force:	$F_{ant} = q_z \cdot Gh \cdot EPA$

### ICE DEAD LOAD

Largest Out-to-Out Dimension:	$D_{ant} = \sqrt{D_{ant}^2 + W_{ant}^2}$
Cross Sectional Area of Ice:	$A_{ice\_ant} = \pi \cdot t_{iz} \cdot (D_{ant} + t_{iz})$
Total Ice Dead Load:	$DL_{ice\_ant} = \rho_i \cdot (A_{ice\_ant} \cdot H_{ant})$

### ICE WIND LOAD

Dimensions:	$H_{i\_ant} = H_{ant} + 2t_{iz}$
	$W_{i\_ant} = W_{ant} + 2t_{iz}$
	$D_{i\_ant} = D_{ant} + 2t_{iz}$
Area (Normal):	$AIN_{area} = H_{i\_ant} \cdot W_{i\_ant}$
Area (Side):	$AIT_{area} = H_{i\_ant} \cdot D_{i\_ant}$
Force Coefficient (Normal):	$Ci_{fn} = C_{fsquare}(H_{i\_ant}, W_{i\_ant})$
Force Coefficient (Side):	$Ci_{fs} = C_{fsquare}(H_{i\_ant}, D_{i\_ant})$
Pipe Area (Normal):	$AN_p = \max[(L_{ip} - H_{i\_ant}) * D_{ip}, 0]$
Pipe Area (Side):	$AT_p = L_{ip} \cdot D_{ip}$
Force Coefficient (Normal):	$C_{fp} = C_{fround}(L_{ip}, D_{ip})$
Normal Effective Projected Area:	$E_{pain} = (Ci_{fn} \cdot AIN_{area}) + (C_{fp} \cdot AN_p)$
Side Effective Projected Area:	$E_{pait} = (Ci_{fs} \cdot AIT_{area}) + (C_{fp} \cdot AT_p)$
Effective Projected Area:	$EPA_i = \max(E_{pain}, E_{pait})$
Wind Force:	$F_{i\_ant} = q_z \cdot Gh \cdot EPA_i$



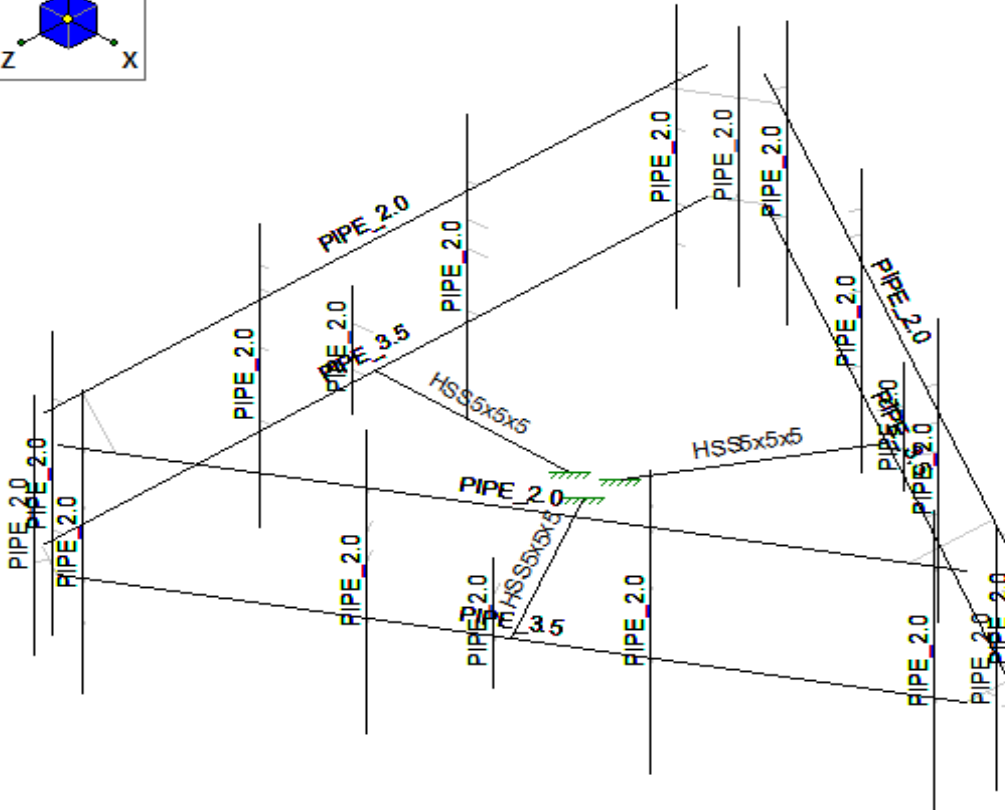
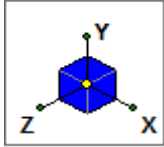
Client:	ATT	Computed By:	CB
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### III. ATTACHMENTS



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### RISA MODEL



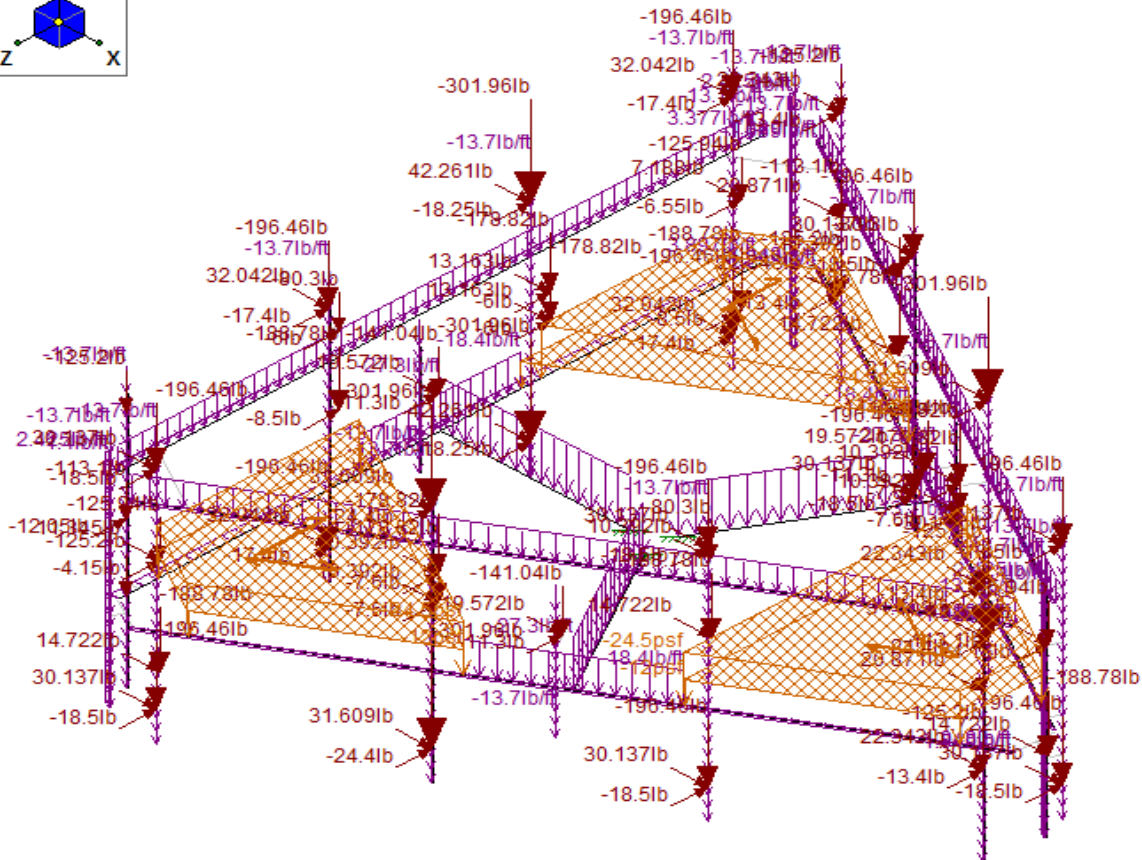
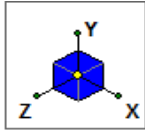




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### RISA WORST CASE LOADING

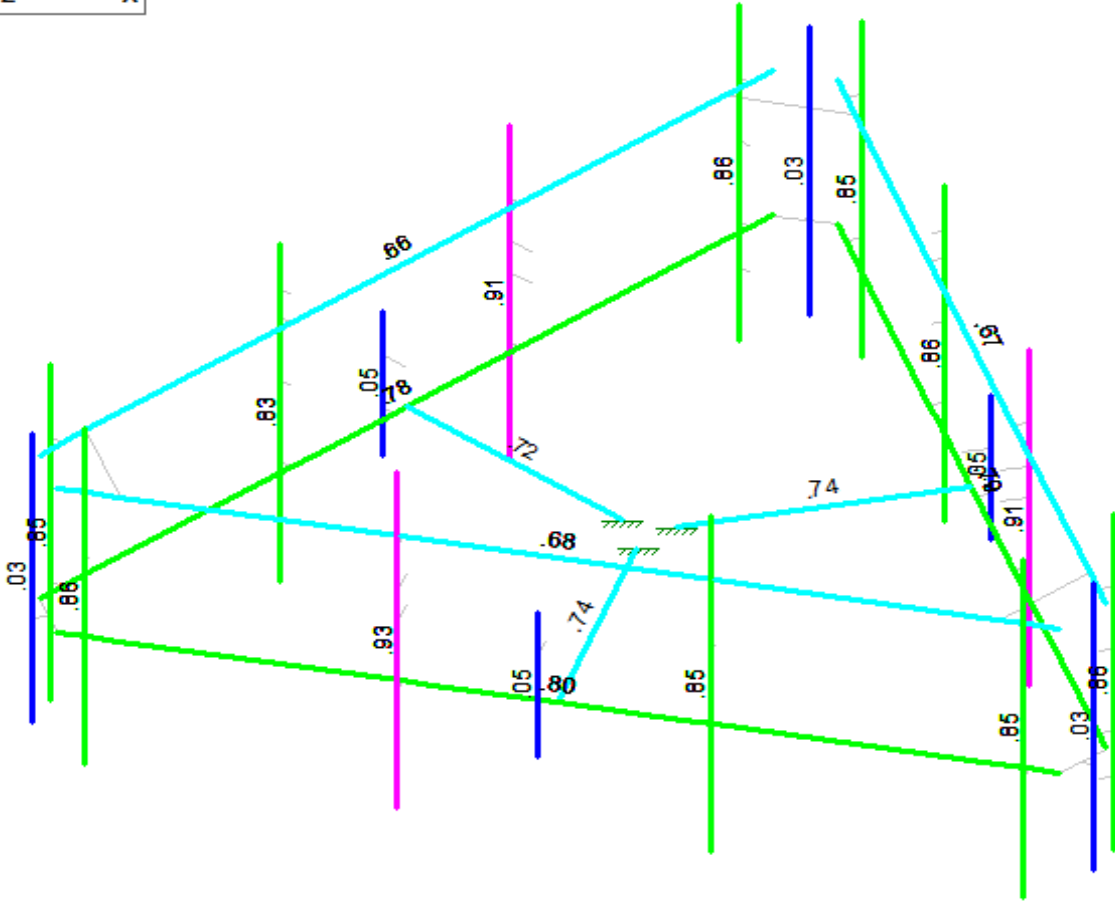
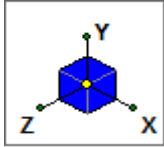


Loads: LC 26, 1.2D+1.0ICE+1.0W12ICE  
Envelope Only Solution



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### RISA CODE CHECK



### Member Primary Data

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M1	N8	N2			Pipe 3.5	Beam	Pipe	A53 Gr.B	Typical
2	M2	N7	N6			Pipe 3.5	Beam	Pipe	A53 Gr.B	Typical
3	M3	N5	N1			Pipe 3.5	Beam	Pipe	A53 Gr.B	Typical
4	M4	N1	N2			RIGID	None	None	RIGID	Typical
5	M6	N5	N6			RIGID	None	None	RIGID	Typical
6	M7	N7	N8			RIGID	None	None	RIGID	Typical
7	M8	N9	N10			RIGID	None	None	RIGID	Typical
8	M9	N11	N12			RIGID	None	None	RIGID	Typical
9	M10	N13	N14			RIGID	None	None	RIGID	Typical
10	M11	N15	N16			RIGID	None	None	RIGID	Typical
11	M12	N17	N18			RIGID	None	None	RIGID	Typical
12	M13	N19	N20			RIGID	None	None	RIGID	Typical
13	M14	N21	N22			RIGID	None	None	RIGID	Typical
14	M15	N23	N24			RIGID	None	None	RIGID	Typical
15	M16	N25	N26			RIGID	None	None	RIGID	Typical
16	M17	N27	N28			RIGID	None	None	RIGID	Typical
17	M18	N29	N30			RIGID	None	None	RIGID	Typical
18	M19	N31	N32			RIGID	None	None	RIGID	Typical
19	M20	N33	N34			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
20	M21	N35	N36			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
21	M22	N37	N38			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
22	M23	N39	N40			RIGID	None	None	RIGID	Typical
23	M24	N41	N42			RIGID	None	None	RIGID	Typical
24	M25	N43	N44			RIGID	None	None	RIGID	Typical
25	M26	N45	N46			RIGID	None	None	RIGID	Typical
26	M27	N47	N48			RIGID	None	None	RIGID	Typical
27	M28	N49	N50			RIGID	None	None	RIGID	Typical
28	M29	N51	N52			RIGID	None	None	RIGID	Typical
29	M30	N53	N54			RIGID	None	None	RIGID	Typical
30	M31	N55	N56			RIGID	None	None	RIGID	Typical
31	M32	N57	N58			RIGID	None	None	RIGID	Typical
32	M33	N59	N60			RIGID	None	None	RIGID	Typical
33	M34	N61	N62			RIGID	None	None	RIGID	Typical
34	M35	N63	N64			RIGID	None	None	RIGID	Typical
35	M36	N65	N66			RIGID	None	None	RIGID	Typical
36	M37	N67	N68			RIGID	None	None	RIGID	Typical
37	M38	N69	N70			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
38	M39	N71	N72			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
39	M40	N73	N74			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
40	M41	N75	N76			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
41	M42	N77	N78			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
42	M43	N79	N80			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
43	M44	N81	N82			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
44	M45	N83	N84			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
45	M46	N85	N86			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
46	M47	N87	N88			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
47	M48	N89	N90			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
48	M49	N91	N92			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
49	M50	N93	N94			RIGID	None	None	RIGID	Typical
50	M51	N95	N96			RIGID	None	None	RIGID	Typical
51	M52	N97	N98			RIGID	None	None	RIGID	Typical

**Member Primary Data (Continued)**

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
52	M53	N99	N100			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
53	M54	N101	N102			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
54	M55	N103	N104			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
55	M56	N105	N106			RIGID	None	None	RIGID	Typical
56	M57	N107	N108			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
57	M58	N109	N110			RIGID	None	None	RIGID	Typical
58	M59	N111	N112			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
59	M60	N113	N114			RIGID	None	None	RIGID	Typical
60	M61	N115	N116			Pipe 2.0	Beam	Pipe	A53 Gr.B	Typical
61	M62	N117	N118			HSS5x5x5	Beam	SquareTube	A500 Gr.B...	Typical
62	M63	N119	N120			HSS5x5x5	Beam	SquareTube	A500 Gr.B...	Typical
63	M64	N121	N122			HSS5x5x5	Beam	SquareTube	A500 Gr.B...	Typical
64	M65	N123	N124			RIGID	None	None	RIGID	Typical
65	M66	N125	N126			RIGID	None	None	RIGID	Typical
66	M67	N127	N128			RIGID	None	None	RIGID	Typical
67	M68	N129	N130			RIGID	None	None	RIGID	Typical
68	M69	N131	N132			RIGID	None	None	RIGID	Typical
69	M70	N133	N134			RIGID	None	None	RIGID	Typical
70	M71	N135	N136			RIGID	None	None	RIGID	Typical
71	M72	N137	N138			RIGID	None	None	RIGID	Typical
72	M73	N139	N140			RIGID	None	None	RIGID	Typical
73	M74	N141	N142			RIGID	None	None	RIGID	Typical
74	M75	N143	N144			RIGID	None	None	RIGID	Typical
75	M76	N145	N146			RIGID	None	None	RIGID	Typical
76	M77	N147	N148			RIGID	None	None	RIGID	Typical
77	M78	N149	N150			RIGID	None	None	RIGID	Typical
78	M79	N151	N152			RIGID	None	None	RIGID	Typical
79	M80	N153	N154			RIGID	None	None	RIGID	Typical
80	M81	N155	N156			RIGID	None	None	RIGID	Typical
81	M82	N157	N158			RIGID	None	None	RIGID	Typical
82	M83	N159	N160			RIGID	None	None	RIGID	Typical
83	M84	N161	N162			RIGID	None	None	RIGID	Typical
84	M85	N163	N164			RIGID	None	None	RIGID	Typical

**Joint Loads and Enforced Displacements (BLC 1 : Dead)**

	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*s^2/in, lb*s^2*in)]
1	N194	L	Y	-17.5
2	N195	L	Y	-17.5
3	N196	L	Y	-17.5
4	N197	L	Y	-17.5
5	N198	L	Y	-17.5
6	N199	L	Y	-17.5
7	N132	L	Y	-26.2
8	N142	L	Y	-26.2
9	N164	L	Y	-26.2
10	N200	L	Y	-30
11	N201	L	Y	-30
12	N202	L	Y	-30
13	N176A	L	Y	-20.3
14	N178	L	Y	-20.3



**Joint Loads and Enforced Displacements (BLC 1 : Dead) (Continued)**

	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*s^2/in, lb*s^2*in)]
15	N179	L	Y	-20.3
16	N181	L	Y	-20.3
17	N182	L	Y	-20.3
18	N184	L	Y	-20.3
19	N185	L	Y	-20.3
20	N187	L	Y	-20.3
21	N188	L	Y	-20.3
22	N190	L	Y	-20.3
23	N191	L	Y	-20.3
24	N193	L	Y	-20.3
25	N177	L	Y	-54.3
26	N180	L	Y	-54.3
27	N183	L	Y	-54.3
28	N186	L	Y	-54.3
29	N189	L	Y	-54.3
30	N192	L	Y	-54.3
31	N134	L	Y	-52.9
32	N144	L	Y	-52.9
33	N156	L	Y	-52.9
34	N128	L	Y	-55.7
35	N138	L	Y	-55.7
36	N152	L	Y	-55.7
37	N124	L	Y	-55.1
38	N126	L	Y	-55.1
39	N148	L	Y	-55.1
40	N150	L	Y	-55.1
41	N160	L	Y	-55.1
42	N162	L	Y	-55.1
43	N130	L	Y	-52.9
44	N140	L	Y	-52.9
45	N154	L	Y	-52.9
46	N136	L	Y	-19
47	N146	L	Y	-19
48	N158	L	Y	-19

**Joint Loads and Enforced Displacements (BLC 2 : Wx)**

	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*s^2/in, lb*s^2*in)]
1	N195	L	X	46.515
2	N196	L	X	46.515
3	N198	L	X	46.515
4	N199	L	X	46.515
5	N132	L	X	43.995
6	N142	L	X	43.995
7	N164	L	X	43.995
8	N201	L	X	33.6
9	N202	L	X	33.6
10	N179	L	X	72.45
11	N181	L	X	72.45
12	N182	L	X	72.45
13	N184	L	X	72.45
14	N188	L	X	72.45



***Joint Loads and Enforced Displacements (BLC 3 : Wz) (Continued)***

	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*s^2/in, lb*s^2*in)]
21	N180	L	Z	141.12
22	N183	L	Z	141.12
23	N189	L	Z	141.12
24	N192	L	Z	141.12
25	N177	L	Z	76.02
26	N186	L	Z	76.02
27	N134	L	Z	33.81
28	N138	L	Z	10.185
29	N152	L	Z	10.185
30	N128	L	Z	24.15
31	N148	L	Z	29.61
32	N150	L	Z	29.61
33	N160	L	Z	29.61
34	N162	L	Z	29.61
35	N124	L	Z	27.615
36	N126	L	Z	27.615
37	N130	L	Z	33.81
38	N136	L	Z	8.4

***Joint Loads and Enforced Displacements (BLC 4 : Wx Ice)***

	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*s^2/in, lb*s^2*in)]
1	N195	L	X	25.8
2	N196	L	X	25.8
3	N198	L	X	25.8
4	N199	L	X	25.8
5	N132	L	X	22.6
6	N142	L	X	22.6
7	N164	L	X	22.6
8	N201	L	X	24.1
9	N202	L	X	24.1
10	N179	L	X	34.8
11	N181	L	X	34.8
12	N182	L	X	34.8
13	N184	L	X	34.8
14	N188	L	X	34.8
15	N190	L	X	34.8
16	N191	L	X	34.8
17	N193	L	X	34.8
18	N176A	L	X	37
19	N178	L	X	37
20	N185	L	X	37
21	N187	L	X	37
22	N180	L	X	36.5
23	N183	L	X	36.5
24	N189	L	X	36.5
25	N192	L	X	36.5
26	N177	L	X	48.8
27	N186	L	X	48.8
28	N144	L	X	17
29	N156	L	X	17
30	N138	L	X	13.1



**Joint Loads and Enforced Displacements (BLC 4 : Wx Ice) (Continued)**

	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*s^2/in, lb*s^2*in)]
31	N152	L	X	13.1
32	N128	L	X	8.3
33	N148	L	X	12
34	N150	L	X	12
35	N160	L	X	12
36	N162	L	X	12
37	N124	L	X	15.2
38	N126	L	X	15.2
39	N140	L	X	17
40	N154	L	X	17
41	N146	L	X	12
42	N158	L	X	12

**Joint Loads and Enforced Displacements (BLC 5 : Wz Ice)**

	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*s^2/in, lb*s^2*in)]
1	N195	L	Z	26.8
2	N196	L	Z	26.8
3	N198	L	Z	26.8
4	N199	L	Z	26.8
5	N132	L	Z	22.6
6	N142	L	Z	22.6
7	N164	L	Z	22.6
8	N200	L	Z	24.1
9	N179	L	Z	37
10	N181	L	Z	37
11	N182	L	Z	37
12	N184	L	Z	37
13	N188	L	Z	37
14	N190	L	Z	37
15	N191	L	Z	37
16	N193	L	Z	37
17	N176A	L	Z	34.8
18	N178	L	Z	34.8
19	N185	L	Z	34.8
20	N187	L	Z	34.8
21	N180	L	Z	48.8
22	N183	L	Z	48.8
23	N189	L	Z	48.8
24	N192	L	Z	48.8
25	N177	L	Z	36.5
26	N186	L	Z	36.5
27	N134	L	Z	17
28	N138	L	Z	8.3
29	N152	L	Z	8.3
30	N128	L	Z	13.1
31	N148	L	Z	15.2
32	N150	L	Z	15.2
33	N160	L	Z	15.2
34	N162	L	Z	15.2
35	N124	L	Z	12
36	N126	L	Z	12









**Member Distributed Loads (BLC 5 : Wz Ice) (Continued)**

	Member Label	Direction	Start Magnitude[lb...	End Magnitude[lb/ft,F]	Start Location[in, %]	End Location[in, %]
3	M3	PZ	4.5	4.5	0	0
4	M20	PZ	3.9	3.9	0	0
5	M21	PZ	3.9	3.9	0	0
6	M22	PZ	3.9	3.9	0	0
7	M57	PZ	2.8	2.8	0	0
8	M59	PZ	2.8	2.8	0	0
9	M61	PZ	2.8	2.8	0	0

**Member Distributed Loads (BLC 6 : Ice Weight)**

	Member Label	Direction	Start Magnitude[lb...	End Magnitude[lb/ft,F]	Start Location[in, %]	End Location[in, %]
1	M1	Y	-18.4	-18.4	72	120
2	M2	Y	-18.4	-18.4	72	120
3	M3	Y	-18.4	-18.4	72	120
4	M62	Y	-27.3	-27.3	0	0
5	M63	Y	-27.3	-27.3	0	0
6	M64	Y	-27.3	-27.3	0	0
7	M20	Y	-13.7	-13.7	0	0
8	M21	Y	-13.7	-13.7	0	0
9	M22	Y	-13.7	-13.7	0	0
10	M38	Y	-13.7	-13.7	0	0
11	M39	Y	-13.7	-13.7	0	0
12	M40	Y	-13.7	-13.7	0	0
13	M41	Y	-13.7	-13.7	0	0
14	M42	Y	-13.7	-13.7	0	0
15	M43	Y	-13.7	-13.7	0	0
16	M44	Y	-13.7	-13.7	0	0
17	M45	Y	-13.7	-13.7	0	0
18	M46	Y	-13.7	-13.7	0	0
19	M47	Y	-13.7	-13.7	0	0
20	M48	Y	-13.7	-13.7	0	0
21	M49	Y	-13.7	-13.7	0	0
22	M53	Y	-13.7	-13.7	0	0
23	M54	Y	-13.7	-13.7	0	0
24	M55	Y	-13.7	-13.7	0	0
25	M57	Y	-13.7	-13.7	0	0
26	M59	Y	-13.7	-13.7	0	0
27	M61	Y	-13.7	-13.7	0	0

**Member Distributed Loads (BLC 7 : BLC 1 Transient Area Loads)**

	Member Label	Direction	Start Magnitude[lb...	End Magnitude[lb/ft,F]	Start Location[in, %]	End Location[in, %]
1	M1	Y	-2	-8.208	115.2	130.56
2	M1	Y	-8.208	-18.686	130.56	145.92
3	M1	Y	-18.686	-28.024	145.92	161.28
4	M1	Y	-28.024	-32.891	161.28	176.64
5	M1	Y	-32.891	-34.826	176.64	192
6	M4	Y	-28.933	-29.003	0	2.451
7	M4	Y	-29.003	-29.595	2.451	4.901
8	M4	Y	-29.595	-21.217	4.901	7.352
9	M4	Y	-21.217	-19.413	7.352	9.802
10	M4	Y	-19.413	-33.676	9.802	12.253
11	M62	Y	-41.991	-35.478	0	7.91







**Load Combinations (Continued)**

	Description	So...	PDelta	S...	BLCFac...	BLC	Fac...	BLC	Fac...	BLCFac...	BLCFac...	BLCFac...	BLCFac...	BLCFac...	BLCFac...
15	1.2D+1.0ICE+1.0W1ICE	Yes	Y		1 1.2	6	1	4	1	5					
16	1.2D+1.0ICE+1.0W2ICE	Yes	Y		1 1.2	6	1	4	.866	5	.5				
17	1.2D+1.0ICE+1.0W3ICE	Yes	Y		1 1.2	6	1	4	.5	5	.866				
18	1.2D+1.0ICE+1.0W4ICE	Yes	Y		1 1.2	6	1	4		5	1				
19	1.2D+1.0ICE+1.0W5ICE	Yes	Y		1 1.2	6	1	4	-.5	5	.866				
20	1.2D+1.0ICE+1.0W6ICE	Yes	Y		1 1.2	6	1	4	-.866	5	.5				
21	1.2D+1.0ICE+1.0W7ICE	Yes	Y		1 1.2	6	1	4	-1	5					
22	1.2D+1.0ICE+1.0W8ICE	Yes	Y		1 1.2	6	1	4	-.866	5	-.5				
23	1.2D+1.0ICE+1.0W9ICE	Yes	Y		1 1.2	6	1	4	-.5	5	-.866				
24	1.2D+1.0ICE+1.0W10ICE	Yes	Y		1 1.2	6	1	4		5	-1				
25	1.2D+1.0ICE+1.0W11ICE	Yes	Y		1 1.2	6	1	4	.5	5	-.866				
26	1.2D+1.0ICE+1.0W12ICE	Yes	Y		1 1.2	6	1	4	.866	5	-.5				

**Envelope Joint Reactions**

Joint	X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-ft]	LC	MY [lb-ft]	LC	MZ [lb-ft]	LC		
1	N118	max	1491.532	7	5147.043	17	1675.732	11	-2594.454	10	6108.23	7	10891.094	16
2		min	-1440.813	13	997.25	10	-1586.973	5	-19181.701	17	-6108.62	13	1292.728	9
3	N120	max	1277.026	8	5084.028	21	1526.143	11	877.026	11	5126.496	11	-3361.67	2
4		min	-1381.544	2	1047.118	2	-1524.754	5	-720.052	5	-5125.249	5	-21633.63	21
5	N122	max	1768.308	8	5111.151	25	1510.556	11	18754.051	25	7192.648	3	11145.099	26
6		min	-1715.569	2	1010.036	6	-1600.709	5	2630.071	6	-7192.139	9	1501.093	7
7	Totals:	max	4520.367	8	14950.718	23	4712.431	11						
8		min	-4520.388	2	4315.275	4	-4712.436	5						

**Envelope AISC 13th(360-05): LRFD Steel Code Checks**

Member	Shape	Code Check	Lo... LC	Shear Check	Lo... LC	phi*P...	phi*P...	phi*P...	phi*P...	Eqn		
1	M48	PIPE 2.0	.929	53...26	.186	37...	16	1785...	32130	1871...	1871...	H1...
2	M44	PIPE 2.0	.908	53...22	.184	37...	24	1785...	32130	1871...	1871...	H1...
3	M40	PIPE 2.0	.907	53...18	.184	37...	20	1785...	32130	1871...	1871...	H1...
4	M43	PIPE 2.0	.860	53...16	.179	34...	26	1785...	32130	1871...	1871...	H1...
5	M45	PIPE 2.0	.858	53...21	.102	18...	26	1785...	32130	1871...	1871...	H1...
6	M41	PIPE 2.0	.857	53...17	.102	34...	20	1785...	32130	1871...	1871...	H1...
7	M49	PIPE 2.0	.857	53...25	.106	18...	18	1785...	32130	1871...	1871...	H1...
8	M46	PIPE 2.0	.852	53...21	.105	18...	17	1785...	32130	1871...	1871...	H1...
9	M38	PIPE 2.0	.852	53...24	.105	36...	23	1785...	32130	1871...	1871...	H1...
10	M42	PIPE 2.0	.850	53...17	.106	36...	26	1785...	32130	1871...	1871...	H1...
11	M47	PIPE 2.0	.847	53...20	.179	18...	18	1785...	32130	1871...	1871...	H1...
12	M39	PIPE 2.0	.830	53...24	.178	34...	22	1785...	32130	1871...	1871...	H1...
13	M3	PIPE 3.5	.798	96 18	.258	96	23	2769...	78750	7953...	7953...	H1...
14	M2	PIPE 3.5	.788	96 26	.254	96	19	2769...	78750	7953...	7953...	H1...
15	M1	PIPE 3.5	.777	96 22	.254	96	15	2769...	78750	7953...	7953...	H1...
16	M62	HSS5x5x5	.739	56.5 19	.102	56.5 y	20	2051...	2177...	31602	31602	H1...
17	M64	HSS5x5x5	.736	56.5 15	.101	56.5 y	15	2051...	2177...	31602	31602	H1...
18	M63	HSS5x5x5	.717	56.5 19	.098	56.5 y	23	2051...	2177...	31602	31602	H1...
19	M22	PIPE 2.0	.682	180 26	.377	180	22	3842...	32130	1871...	1871...	H3-6
20	M21	PIPE 2.0	.669	66 15	.372	180	18	3842...	32130	1871...	1871...	H1...
21	M20	PIPE 2.0	.663	66 19	.371	10	26	3842...	32130	1871...	1871...	H1...
22	M53	PIPE 2.0	.053	12 15	.028	12	5	2884...	32130	1871...	1871...	H1...
23	M54	PIPE 2.0	.053	12 23	.028	12	7	2884...	32130	1871...	1871...	H1...



Company : Maser Consulting P.A.  
 Designer : CB  
 Job Number : 17963019A  
 Model Name : Platform Mount Analysis

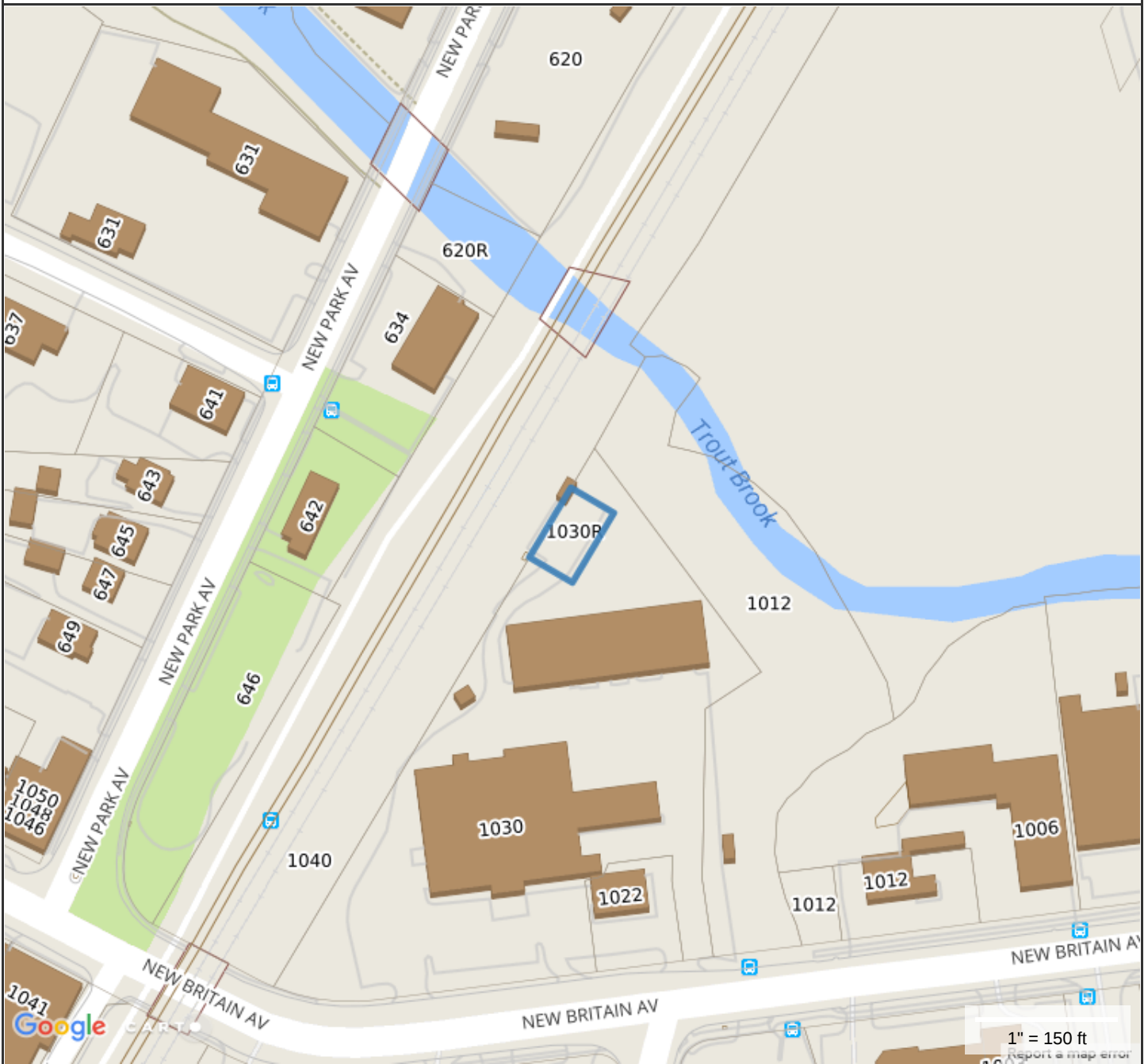
Apr 5, 2018

Checked By: SMS

***Envelope AISC 13th(360-05): LRFD Steel Code Checks (Continued)***

Member	Shape	Code Check	Lo... LC	Shear Check	Lo... LC	phi*P...phi*P...phi*... phi*... .. Eqn	
24	M55	PIPE_2.0	.051	12 19	.028	12 9	2884...321301871...1871... H1-...
25	M61	PIPE_2.0	.030	45... 6	.003	45... 6	2086...321301871...1871... H1-...
26	M59	PIPE_2.0	.030	45...10	.003	45... 10	2086...321301871...1871... H1-...
27	M57	PIPE_2.0	.030	45...13	.003	45... 13	2086...321301871...1871... H1-...

### CT5259 1030 New Britain Ave., West Hartford CT



**Property Information**

**Property ID** 3771 2 1030R 0001  
**Location** 1030R NEW BRITAIN AVENUE  
**Owner** TEN THIRTY TOWER COMPANY LLC



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Parcels updated 5/1/2016  
Properties updated Daily