July 23, 2014
Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

| Re: | Notice of Exempt Modification <br> Proposal to Add Three (3) Remote Radio Heads |
| :--- | :--- |
| Property Address: | 1210 Highland Avenue, Torrington, CT 06790 (the "Property") |
| Applicant: | New Cingular Wireless PCS, LLC ("AT\&T") |

Dear Ms. Bachman:
AT\&T currently maintains a wireless telecommunications facility on an existing 260 -foot Self Support tower location on the Property, owned by SBA Properties, Inc. (the "Tower"). AT\&T's facility consists of nine (9) wireless telecommunication antennas at a height of 242-feet.

The Connecticut Siting Council (the "Council) approved AT\&T's use of the tower in the following prior decisions; EM-AT\&T-064-143-148-020225, EM-AT\&T-"UNIVERSAL"-030221, EM-CING-143-050914 and EM-CING-143-050914. In its decision dated February 8, 2013, (the "Decision"), the Council approved AT\&T to install six (6) Remote Radio Heads ("RRUs"), but AT\&T installed only three (3) RRUs. AT\&T now intends to install the remaining RRUs to complete the installation. This exempt modification application is necessary because the Decision is over one year old. Please refer to Tab 1 for further specifications of the RRUs.

Please accept this application as notification pursuant to R.C.S.A. §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16-50j72(b)(2). In accordance with R.C.S.A. §16-50j-73, a copy of this letter is being sent to the Mayor of Torrington, CT. A copy of this letter is also being sent to SBA Properties, Inc..

The planned modifications to AT\&T's facility fall squarely within those activities explicitly provided for in R.C.S.A. §16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the Tower. AT\&T's new RRUs will be installed at the 242 -foot level of the 260 -foot Self Support.

## smartlink

2. The proposed modifications will not involve any changes to ground-mounted equipment and, therefore, will not require and extension of the site boundary.
3. The proposed modifications will not increase the noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the modified facility will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. A RF emissions calculation for AT\&T's modified facility was provided in the application which led to the - Decision. See Tab 2 attached.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The Tower and its foundation can support AT\&T's proposed modifications. (See Structural Analysis Report included in Tab 3).

For the foregoing reasons, AT\&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitutes an exempt modification under R.C.S.A. §16-50j-72(b)(2).


Adam F. Braillard

cc:<br>SBA Properties, Inc<br>5900 Broken Sound Parkway NW 2nd Floor<br>Boca Raton FL 33487-2797

Town of Torrington
140 Main Street,
Torrington, CT 06790

TAB 1


## general notes













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CONCRETE AND REINFORCING STEEL NOTES:












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SOIL COMPACTON NOTES FOR SLAB ON GRADE:





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## ELECTHICAL INSTALLATION NOTES:


















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1210 HIGHLAND AVE, ORRINGTON, CT 0679

SHEET TME
GENERAL NOTES



| EXISTING ANTENNA SCHEDULE |  |  |  |
| :---: | :---: | :---: | :---: |
| sector | make | moded | SIIE (INCHES) |
| APPA: |  |  |  |
| 日etas | $\begin{aligned} & \text { POMERMAVE } \\ & \text { KOHRTRENE } \\ & \text { POWRWAVE } \end{aligned}$ | $\begin{aligned} & 7700 \\ & \hline 800 \\ & 770 \end{aligned}$ |  |
| саммя: |  |  | $\begin{aligned} & 55 \times 11 \times 5.2 \times 7.87 \\ & 555 \times 11 \times .67 .87 \end{aligned}$ |
| PROPOSED ANTENNA SCHEDULE |  |  |  |
| sector | make | moder | SIIE-(NCHES) |
| ALPH: | $\begin{gathered} \text { Powerwave } \\ \text { Ropwerwave } \\ \text { Pot } \end{gathered}$ | 7770 AM-X-CD-16-65-00T-RET 7770 |  |
| 日eta |  | $\begin{aligned} & 7770 \\ & 8007 \\ & 770704 \end{aligned}$ | $\begin{aligned} & 55 \times 11 \times 5 \\ & 55.2 \times 11.8 \times 6.0 \\ & 55 \times 1 \times 5 \end{aligned}$ |
| самм: |  |  |  |
| EXISTING RRUS SCHEDULE |  |  |  |
| sector | Make | modal | SIIE (1)CHIS) |
| apha: | ERCSSon | RRUS-11 | 19.78×17.087. 2 |
| BEA: | ERICSSON | RRUS-11 | 19.7x17.0x.7. 2 |
| camme | ERICSSON | RRUS-11 | 19.7x17.0x7.2 |
| PROPOSED RRUS SCHEDULE |  |  |  |
| sector | make | Hopes | SIIE (IMCHES) |
| ALPPA: | ERRCsson | ${ }_{\text {RRUSS }}^{\text {RRS }}$ 11 | ${ }^{19,79 \times 17.70 \times 7.7} 1$ |
| betas | ERRCSS50N | ${ }_{\text {RRUS }}^{\text {RRS }}$ R11 | ${ }_{19}^{19.7 \times 1777.077 .07 .2}$ |
| Ganme | ERRCSSON | $\underset{\substack{\text { RRUSS-11 } \\ \text { RRUS-11 }}}{ }$ | ${ }_{19}^{99.7 \times 1 \times 777.0 \times 7.2}$ |



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3. CONRRM RECOURED EQUIFUEN WTH LITES RTDS

RRU \& A2 MODULE 1



TAB 2

| Control Number | Site | Carrier | \#Channels | ERP/Ch |
| :---: | :---: | :---: | :---: | :---: |
| EM-Marcus-143-020214 | Torrington-1210 Highland Avenue | Marcus | 1 | 100 |
| EM-VER-143-121204 | Torrington - 1210 Highland Avenue | Verizon PCS | 11 | 211 |
| EM-VER-143-121204 | Torrington - 1210 Highland Avenue | Verizon cellular | 9 | 231 |
| EM-VER-143-121204 | Torrington-1210 Highland Avenue | Verizon AWS | 1 | 1750 |
| EM-VER-143-121204 | Torrington-1210 Highland Avenue | Verizon LTE | 1 | 768 |
| EM-CING-143-130122 | Torrington - 1210 Highland Avenue | AT\&T UMTS | 2 | 565 |
| EM-CING-143-130122 | Torrington - 1210 Highland Avenue | AT\&T UMTS | 2 | 875 |
| EM-CING-143-130122 | Torrington - 1210 Highland Avenue | AT\&T GSM | 1 | 283 |
| EM-CING-143-130122 | Torrington - 1210 Highland Avenue | AT\&T GSM | 4 | 525 |
| EM-CING-143-130122 | Torrington - 1210 Highland Avenue | AT\&T LTE | 1 | 1615 |

:ions

| Ant Ht | Power Den | MHz | S | \%MPE | Site Total |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 0.0036 | 5800 | 1.0000 | 25.50\% | Results of field measurements AT\&T took of s |
| 200 | 0.0209 | 1970 | 1.0000 | 2.09\% |  |
| 200 | 0.0187 | 869 | 0.5793 | 3.23\% |  |
| 200 | 0.0157 | 2145 | 1.0000 | 1.57\% |  |
| 200 | 0.0069 | 698 | 0.4653 | 1.48\% |  |
| 245 | 0.0068 | 880 | 0.5867 | 1.15\% |  |
| 245 | 0.0105 | 1900 | 1.0000 | 1.05\% |  |
| 245 | 0.0017 | 880 | 0.5867 | 0.29\% |  |
| 245 | 0.0126 | 1900 | 1.0000 | 1.26\% |  |
| 245 | 0.0097 | 734 | 0.4893 | 1.98\% | 39.60\% |

ite on 2/8/2002

TAB 3

## Structural Analysis for

 SBA Network Services, Inc.
## 260' Guyed Tower

## SBA Site Name: Torrington 2

SBA Site ID: CT02303-A
AT\&T Site ID: CT1253
AT\&T Site Name: Torrington Highland Avenue
FDH Project Number 12-08779E S1 (R1)
Analysis Results

| Tower Components | $\mathbf{1 1 1 . 6 \%}$ | Insufficient |
| :---: | :---: | :---: |
| Foundation | $68.1 \%$ | Sufficient |

Prepared By:


Daniel Chang, El
Project Engineer

Reviewed By:


Christopher M Murphy, PE
President
CT PE License No. 25842

FDH Engineering, Inc.
6521 Meridian Drive
Raleigh, NC 27616
(919) 755-1012
info@fdh-inc.com


October 12, 2012

## TABLE OF CONTENTS

EXECUTIVE SUMMARY ..... 3
Conclusions ..... 3
Recommendations ..... 3
APPURTENANCE LISTING ..... 4
RESULTS ..... 8
GENERAL COMMENTS ..... 11
LIMITATIONS ..... 11
APPENDIX ..... 12

## EXECUTIVE SUMMARY

At the request of SBA Network Services, Inc., FDH Engineering, Inc. performed a structural analysis of the existing guyed tower located in Torrington, CT to determine whether the tower is structurally adequate to support both the existing and proposed loads pursuant to the Structural Standards for Steel Antenna Towers and Antenna Supporting Structures, TIA/EIA-$222-F$ and 2005 Connecticut Building Code. Information pertaining to the existing/proposed antenna loading, current tower geometry, the member sizes, and foundation dimensions was obtained from:
] PiRod, Inc. (File No. A-107657) original design drawings dated September 23, 1996

- All-Points Technology Corporation, P.C. (Project No. CT122160) structural analysis report dated January 21, 2002
- FDH Engineering, Inc. (Project No. 05-0827E) Modification Drawings for a 260 ' Guyed Tower dated August 29, 2005
- FDH, Inc. (Job No. 12-07062T T1) TIA Inspection Report dated July 25, 2012
- FDH Engineering, Inc. (Project No. 12-08779E G1) Geotechnical Evaluation of Subsurface Conditions dated October 8, 2012
- SBA Network Services, Inc.

The basic design wind speed per the TIA/EIA-222-F standards and 2005 Connecticut Building Code is 80 mph without ice and 28 mph with 1 " radial ice. Ice is considered to increase in thickness with height.

## Conclusions

With the existing and proposed antennas from AT\&T in place at 245 ft , the tower does not meet the requirements of the TIA/EIA-222-F standards and 2005 Connecticut Building Code. However, provided the foundations were constructed per the original design drawings (see PiRod File No. A-107657) and based on the given soil parameters (see FDH Project No. 1208779E G1), the foundations should have the necessary capacity to support both the proposed and existing loading. For a more detailed description of the analysis of the tower, see the Results section of this report.

Our structural analysis has been performed assuming all information provided to FDH Engineering, Inc. is accurate (i.e., the steel data, tower layout, existing antenna loading, and proposed antenna loading) and that the tower has been properly erected and maintained per the original design drawings.

## Recommendations

To ensure the requirements of the TIA/EIA-222-F standards and 2005 Connecticut Building Code are met with the existing and proposed loading in place, we have the following recommendations:

1. Coax lines must be installed as shown in Figure 1.
2. The existing TMAs and diplexers should be installed directly behind the proposed and existing panel antennas.
3. Reinforcement of the tower legs is required to support the existing and proposed loading. See the Results section of this report for locations.
4. Reinforcement of the tower diagonals is required to support the existing and proposed loading. See the Results section of this report for locations.

We would anticipate the construction cost for a turnkey design/build modification project of this nature to range in price from approximately $\$ 10,000$ to $\$ 20,000$ (which should include the engineering design fees, inspection fees, and construction fees).

## APPURTENANCE LISTING

The proposed and existing antennas with their corresponding cables/coax lines are shown in Table 1. If the actual layout determined in the field deviates from the layout, FDH Engineering, Inc. should be contacted to perform a revised analysis.

Table 1 - Appurtenance Loading

## Existing Loading:

| Antenna Elevation ( t ) | Description | Coax and Lines | Coax No. | Carrier | Mount Elevation (ft) | Mount Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 264 | (1) Antel 11.5' $\times 2.5$ " omni | (1) 1-5/8" | 39 | --- | 258 | (3) 10' Standoffs |
| 269.5 | (1) Telewave $21{ }^{\prime} \times 2.5$ " omni | (1) 1-5/8" | 38 | --- |  |  |
| 268.5 | (1) $21{ }^{\prime} \times 2.4{ }^{\prime \prime} \mathrm{mmi}$ |  |  |  |  |  |
| 259 | (1) $4^{\prime \prime} \times 13.75$ " $\times 3$ " TMA |  |  |  |  |  |
| 251 | (1) $14^{\prime} \times 2.5{ }^{\prime \prime}$ omni (inverted) | (1) $7 / 8$ " | 28 | --- |  |  |
| 266.5 | (1) Radio Labs SRL480 omni | (1) $7 / 8 "$ <br> (1) $1 / 2^{\prime \prime}$ | 29,32 | --- |  |  |
| 255 | (1) 24 " $\times 20$ " $\times 11^{\prime \prime}$ TMA |  |  |  | 255 | Direct |
| 245 | (6) Powerwave 7770 w/ Mount Pipe <br> (6) Powerwave LGP13519 TMAs <br> (12) Powerwave LGP21401 TMAs | (12) 1-5/8" | 15-26 | AT\&T | 242.5 | (3) 12.5' T-Frames |
| 228.5 | (1) $14^{\prime} \times 2.4$ " omni | (1) 1-5/8" | 27 | --- | 221.5 | (1) 4.5' Standoff |
| 226 | (1) 11.5 ' $\times 2.4$ " omni | (1) 1-1/4" | 44 | --- | 226 | (1) 13.5 ' $\times 2.4$ " Pipe Mount |
| 225.5 | (1) Celwave 458-2 Omni | (1) 1-1/4" | 37 | --- | 218 | (3) 10' Standoffs |
| 224.5 | (1) $11.5^{\prime} \times 2.4$ " omni | --- | --- | --- |  |  |
| 223 | (1) Antel BCD 8706 NE omni | (1) 1-1/4" | 47 | Page Net |  |  |
| 222.5 | (1) $7.5^{\prime} \times 2.4$ " omni | (1) 1-1/4" | 30 | --- |  |  |
| 212 | (1) Decibel 11.5' $\times$ 3" omni (inverted) | (1) 1-1/4" | 46 | --- |  |  |
| 211.5 | (1) Decibel 11' $\times 3$ " omni (inverted) | (1) $1-1 / 4^{\prime \prime}$ <br> (1) $7 / 8 "$ | 11-12 | --- |  |  |
| 211 | (1) Decibel 11' $\times 3$ " omni (inverted) | (2) 1-1/4" | 9-10 | Metro Comm |  |  |
| 209.5 | (1) Decibel 14' ${ }^{\prime \prime}$ " omni (inverted) | (1) $7 / 8$ " | 31 | --- |  |  |
| 203 | (1) Decibel 731DG85V1EXM <br> (2) 14 " $x 9$ " $\times 2.5$ " TMAs | --- | --- | --- | 203 | (1) 63 " $\times 2.4$ " Pipe Mount |
| 202 | (2) Clear Comm 7.5" $\times 4$ " $\times 4$ " TMAs |  |  |  |  |  |
| 199 | (3) Antel BXA-80063/4CF w/ Mount Pipe <br> (3) Antel BXA-185063/8CF w/ Mount Pipe | (12) 1-5/8" | $\begin{gathered} \hline 3-8, \\ 48-53 \\ \hline \end{gathered}$ | Verizon | 198 | (3) 10' T-Frames |
| 183 | (1) Andrew 11.5' x 3" omni | (1) $7 / 8$ " | 45 | --- | 177.5 | (1) 48" Standoff |
| 184 | (1) Andrew PG1N0F-0090-310 omni | (1) $7 / 8{ }^{\prime \prime}$ | 36 | --- | 178.5 | (1) 27" Standoff |
| 174.5 | (1) 6.5 " 20.5 " $\times 4.5$ " TMA |  |  |  | 174.5 | Direct |
| 180 | (1) Radio Labs SRL 6139 dipole | (1) 7/8" | 41 | --- | 175.5 | (1) 36 " Standoff |
| 179.5 | (1) 8' ${ }^{\text {c }}$ " omni | (1) 1-1/4" | 40 |  |  |  |
| 174 | (1) Scala 9 Element Yagi (27" $\times 7$ ") | --- | --- | --- |  |  |
| 174.5 | (1) $22^{\prime \prime} \times .75$ " GPS | (1) $1 / 2$ " | 1 | --- | 173.5 | (1) 17" Standoff |
| 173 | (1) $13.5{ }^{\prime} \times 1.8$ " omni | (1) $7 / 8$ " | 14 | --- | 167 | (1) 72 " Standoff |
| 163.5 | (1) Andrew 11'2" $\times 3$ " omni | (1) 1-1/4" | 43 | --- | 158.5 | (1) 15" Standoff |
| 166.5 | (1) 8' ${ }^{1 \prime}$ 1" omni | (1) $7 / 8$ " | 42 | Torrington PD | 162.5 | (1) 18 " Standoff |
| 147 | (1) $11.5^{\prime} \times 2.4$ " omni | (1) $7 / 8$ " | 35 | American Mess | 141.5 | (1) 32 " Standoff |
| 118.5 | (1) Shivley $20{ }^{\prime} \times 2.5{ }^{\prime} 3$ Bay FM | (1) 1-5/8" | 13 | WZBC 97.3 | 118.5 | (4) $16^{\prime \prime}$ Standoffs |
| 84.5 | (1) Shivley 4' x 2.5' 1-Bay FM | (1) $7 / 8$ " | 33 | WAPJ 89.8 | 83.5 | (1) 20 " Standoff |
| 66.5 | (1) 12.5 " 9 9" TMA | (1) $1 / 2$ " | 34 | Marcus Comm. | 66.5 | Direct |
| 64.5 | (1) Radiowaves SP2-2.4NS Dish |  |  |  | 64.5 | Direct |

## Proposed Loading:

| Antenna Elevation (ft) | Description | Coax and Lines | Coax No. | Carrier | Mount Elevation (ft) | Mount Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 245 | (6) Powerwave 7770 w/ Mount Pipe <br> (2) KMW AM-X-CD-16-65-00T-RET w/ Mount Pipe <br> (1) Kathrein 80010764 w/ Mount Pipe <br> (12) Powerwave LGP21401 TMAs <br> (6) Ericsson RRUS-11 RRUs <br> (1) Andrew ABT-DF-DMADBH Surge <br> Arrestor <br> (1) Raycap DC6-48-60-18-8F Surge Arrestor | (12) 1-5/8" <br> (1) $7 / 16$ " Fiber Cable ${ }^{1}$ <br> (2) $3 / 4$ " DC Power ${ }^{1}$ | $\begin{gathered} 15-26, \\ 54 \end{gathered}$ | AT\&T | 242.5 | (3) 12.5' T-Frames |



Figure 1-Coax Layout

## RESULTS

The following yield strength of steel for individual members was used for analysis:
Table 2 - Material Strength

| Member Type | Yield Strength |
| :---: | :---: |
| Legs | 50 ksi |
| Bracing | $50 \mathrm{ksi} \& 36 \mathrm{ksi}$ |

Table 3 displays the summary of the ratio (as a percentage) of force in the member to their capacities. Values greater than $100 \%$ indicate locations where the maximum force in the member exceeds its capacity. Table 4 displays the maximum foundation reactions.

If the assumptions outlined in this report differ from actual field conditions, FDH Engineering, Inc. should be contacted to perform a revised analysis. Furthermore, as no information pertaining to the allowable twist and sway requirements for the existing or proposed appurtenances was provided, deflection and rotation were not taken into consideration when performing this analysis.

See the Appendix for detailed modeling information
Table 3 - Summary of Working Percentage of Structural Components

| Section No. | Elevation ft | Component Type | Size | \% Capacity* | Pass |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 260-257 | Leg | $11 / 2$ | 5.6 | Pass |
|  |  | Diagonal | 9/16 | 18.9 | Pass |
|  |  | Top Girt | 3/4 | 0.8 | Pass |
| T2 | 257-254.667 | Leg | $11 / 2$ | 8.6 | Pass |
|  |  | Diagonal | 9/16 | 47.8 | Pass |
| T3 | 254.667-252.333 | Leg | $11 / 2$ | 13.0 | Pass |
|  |  | Diagonal | 9/16 | 46.7 | Pass |
| T4 | 252.333-250 | Leg | $11 / 2$ | 17.0 | Pass |
|  |  | Diagonal | 9/16 | 50.4 | Pass |
| T5 | 250-247.667 | Leg | $11 / 2$ | 21.8 | Pass |
|  |  | Diagonal | 9/16 | 47.6 | Pass |
|  |  | Top Girt | 3/4 | 3.0 | Pass |
| T6 | 247.667-245.333 | Leg | $11 / 2$ | 26.2 | Pass |
|  |  | Diagonal | 9/16 | 60.0 | Pass |
| T7 | 245.333-243 | Leg | $11 / 2$ | 41.3 | Pass |
|  |  | Diagonal | 9/16 | 78.3 | Pass |
|  |  | Top Girt | C3x6 | 12.3 | Pass |
| T8 | 243-240 | Leg | 11/2 | 56.0 | Pass |
|  |  | Diagonal | 9/16 | 106.6 | Fail |
|  |  | Top Girt | C3x6 | 24.0 | Pass |
|  |  | Bottom Girt | 3/4 | 87.9 | Pass |
| T9 | 240-220 | Leg | 11/2 | 55.8 | Pass |
|  |  | Diagonal | 9/16 | 56.2 | Pass |
|  |  | Top Girt | 3/4 | 39.3 | Pass |
|  |  | Bottom Girt | 3/4 | 2.8 | Pass |


| Section No. | Elevation ft | Component Type | Size | \% Capacity* | Pass Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Mid Girt | 3/4 | 1.2 | Pass |
|  |  | Guy A@239.333 | 5/8 | 79.7 | Pass |
|  |  | Guy B@239.333 | 5/8 | 79.5 | Pass |
|  |  | Guy C@239.333 | 5/8 | 79.5 | Pass |
| T10 | 220-200 | Leg | 11/2 | 80.2 | Pass |
|  |  | Diagonal | 9/16 | 84.2 | Pass |
|  |  | Top Girt | 3/4 | 1.9 | Pass |
|  |  | Bottom Girt | 3/4 | 23.7 | Pass |
|  |  | Mid Girt | 3/4 | 3.5 | Pass |
| T11 | 200-197 | Leg | $11 / 2$ | 94.7 | Pass |
|  |  | Diagonal | 9/16 | 81.7 | Pass |
|  |  | Top Girt | 3/4 | 71.2 | Pass |
| T12 | 197-194.667 | Leg | $11 / 2$ | 111.6 | Fail |
|  |  | Diagonal | 9/16 | 68.5 | Pass |
|  |  | Top Girt | C3x6 | 28.3 | Pass |
| T13 | 194.667-192.333 | Leg | $11 / 2$ | 110.5 | Fail |
|  |  | Diagonal | 9/16 | 68.5 | Pass |
|  |  | Top Girt | C3x6 | 21.9 | Pass |
|  |  | Guy A@194.667 | 1/2 | 73.0 | Pass |
|  |  | Guy B@194.667 | 1/2 | 72.0 | Pass |
|  |  | Guy C@194.667 | 1/2 | 73.2 | Pass |
|  |  | Torque Arm Top@194.667 | L3 3 3x1/2 | 8.9 | Pass |
|  |  | Torque Arm Bottom@194.667 | L3×3x1/2 | 12.4 | Pass |
| T14 | 192.333-190 | Leg | $11 / 2$ | 97.4 | Pass |
|  |  | Diagonal | 9/16 | 74.3 | Pass |
|  |  | Top Girt | C3x6 | 24.0 | Pass |
| T15 | 190-187.667 | Leg | $11 / 2$ | 81.6 | Pass |
|  |  | Diagonal | 9/16 | 86.2 | Pass |
|  |  | Top Girt | 3/4 | 64.3 | Pass |
| T16 | 187.667-185.333 | Leg | $11 / 2$ | 74.6 | Pass |
|  |  | Diagonal | 9/16 | 71.4 | Pass |
| T17 | 185.333-183 | Leg | $11 / 2$ | 67.7 | Pass |
|  |  | Diagonal | 9/16 | 65.1 | Pass |
| T18 | 183-180 | Leg | 11/2 | 66.3 | Pass |
|  |  | Diagonal | 9/16 | 91.2 | Pass |
|  |  | Bottom Girt | 3/4 | 17.6 | Pass |
| T19 | 180-160 | Leg | $11 / 2$ | 72.4 | Pass |
|  |  | Diagonal | 9/16 | 93.7 | Pass |
|  |  | Top Girt | 3/4 | 19.5 | Pass |
|  |  | Bottom Girt | 3/4 | 0.7 | Pass |
|  |  | Mid Girt | 3/4 | 1.1 | Pass |
| T20 | 160-140 | Leg | $11 / 2$ | 77.7 | Pass |
|  |  | Diagonal | 9/16 | 66.9 | Pass |
|  |  | Top Girt | 3/4 | 1.5 | Pass |
|  |  | Bottom Girt | 3/4 | 15.1 | Pass |
|  |  | Mid Girt | 3/4 | 1.1 | Pass |
| T21 | 140-120 | Leg | 11/2 | 91.8 | Pass |
|  |  | Diagonal | 9/16 | 72.4 | Pass |


| Section No. | Elevation ft | Component Type | Size | \% Capacity* | Pass Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Top Girt | 3/4 | 27.0 | Pass |
|  |  | Bottom Girt | 3/4 | 10.4 | Pass |
|  |  | Mid Girt | 3/4 | 2.4 | Pass |
|  |  | Guy A@139.333 | 1/2 | 76.5 | Pass |
|  |  | Guy B@139.333 | 1/2 | 76.4 | Pass |
|  |  | Guy C@139.333 | 1/2 | 76.6 | Pass |
| T22 | 120-100 | Leg | $11 / 2$ | 96.9 | Pass |
|  |  | Diagonal | 9/16 | 58.6 | Pass |
|  |  | Top Girt | 3/4 | 6.9 | Pass |
|  |  | Bottom Girt | 3/4 | 8.1 | Pass |
|  |  | Mid Girt | 3/4 | 1.3 | Pass |
| T23 | 100-80 | Leg | $13 / 4$ | 68.6 | Pass |
|  |  | Diagonal | 5/8 | 88.8 | Pass |
|  |  | Top Girt | 3/4 | 10.2 | Pass |
|  |  | Bottom Girt | 3/4 | 23.4 | Pass |
|  |  | Mid Girt | 3/4 | 2.0 | Pass |
| T24 | 80-60 | Leg | $13 / 4$ | 83.6 | Pass |
|  |  | Diagonal | 5/8 | 91.5 | Pass |
|  |  | Top Girt | 3/4 | 26.4 | Pass |
|  |  | Bottom Girt | 3/4 | 21.8 | Pass |
|  |  | Mid Girt | 3/4 | 47.5 | Pass |
|  |  | Guy A@70 | 1/2 | 56.8 | Pass |
|  |  | Guy B@70 | 1/2 | 55.6 | Pass |
|  |  | Guy C@70 | 1/2 | 56.8 | Pass |
|  |  | Torque Arm Top@70 | L3x3x1/2 | 6.9 | Pass |
|  |  | Torque Arm <br> Bottom@70 | L3x3x1/2 | 7.3 | Pass |
| T25 | 60-40 | Leg | $13 / 4$ | 82.4 | Pass |
|  |  | Diagonal | 5/8 | 64.4 | Pass |
|  |  | Top Girt | 3/4 | 18.4 | Pass |
|  |  | Bottom Girt | 3/4 | 7.0 | Pass |
|  |  | Mid Girt | 3/4 | 2.3 | Pass |
| T26 | 40-20 | Leg | $13 / 4$ | 85.5 | Pass |
|  |  | Diagonal | 5/8 | 27.6 | Pass |
|  |  | Top Girt | 3/4 | 5.8 | Pass |
|  |  | Bottom Girt | 3/4 | 1.5 | Pass |
|  |  | Mid Girt | 3/4 | 2.4 | Pass |
| T27 | 20-5.33334 | Leg | $13 / 4$ | 87.6 | Pass |
|  |  | Diagonal | 5/8 | 24.2 | Pass |
|  |  | Top Girt | 3/4 | 3.5 | Pass |
|  |  | Mid Girt | 3/4 | 5.2 | Pass |
| T28 | 5.33334-0 | Leg | 13/4 | 89.4 | Pass |
|  |  | Diagonal | 5/8 | 12.6 | Pass |
|  |  | Top Girt | 3/4 | 63.3 | Pass |

* Capacities include 1/3 allowable stress increase for wind per TIA/EIA-222-F.

Table 4 - Maximum Base Reactions

|  | Current Analysis* <br> (TIA/EIA-222-F) |  | Original Design <br> $(T I A / E I A-222-F) ~$ |  |
| :--- | :---: | :---: | :---: | :---: |
| Reaction | Horizontal | Vertical | Horizontal | Vertical |
| Tower Base | 2 k | 142 k | 4 k | 87 k |
| Anchor | 47 k | 36 k | 52 k | 38 k |

*Foundation adequate based on independent analysis.

## GENERAL COMMENTS

This engineering analysis is based upon the theoretical capacity of the structure. It is not a condition assessment of the tower and its foundation. It is the responsibility of SBA Network Services, Inc. to verify that the tower modeled and analyzed is the correct structure (with accurate antenna loading information) modeled. If there are substantial modifications to be made or the assumptions made in this analysis are not accurate, FDH Engineering, Inc. should be notified immediately to perform a revised analysis.

## LIMITATIONS

All opinions and conclusions are considered accurate to a reasonable degree of engineering certainty based upon the evidence available at the time of this report. All opinions and conclusions are subject to revision based upon receipt of new or additional/updated information. All services are provided exercising a level of care and diligence equivalent to the standard and care of our profession. No other warranty or guarantee, expressed or implied, is offered. Our services are confidential in nature and we will not release this report to any other party without the client's consent. The use of this engineering work is limited to the express purpose for which it was commissioned and it may not be reused, copied, or distributed for any other purpose without the written consent of FDH Engineering, Inc.

## APPENDIX



