January 22, 2019
Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## RE: Notice of Exempt Modification for Crown Site BU: 823530 <br> AT\&T Site ID: 10107966 <br> 580 Chapel Street, Thomaston, Litchfield County, CT 06787 <br> Latitude: $41^{\circ} \mathbf{3 9} \mathbf{4 8 . 4 8 " /} /$ Longitude: $-73^{\circ} \mathbf{4}^{\prime} \mathbf{2 7 . 4 1 "}$

Dear Ms. Bachman:
AT\&T currently maintains (6) antennas at the 142 -foot level of the existing 175 -foot monopole at 580 Chapel Street, Thomaston, Connecticut 06787. The tower is owned by Crown Castle. The property is owned by the Town of Thomaston. AT\&T intends to replace (6) of the existing antennas with (6) new antennas, add (3) additional antennas, replace (6) existing RRHS with (12) RRHs, add (1) hybrid, and add (4) DC power cables.

The facility was approved by the Thomaston Zoning Board of Appeals on July 18, 2000 with the following conditions:

1. Conduct an annual RF inspection and submit the results to the Commission.
2. Regrade the driveway as noted in Land Tech's letter dated October 6, 2000.
3. Planmetics dated November 1, 2000, regarding items 12-15.
4. If the Town decides not to have the tower removed, then the site plan and mylar must be revised. Any undertaking regarding the Town's tower shall be done in accordance with the conditions of the signed contract.

AT\&T's proposed modification complied with all aforementioned conditions.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § $16-50 \mathrm{j}-73$, for construction that constitutes an exempt modification pursuant to R.C.S.A. § $16-50 \mathrm{j}-$ 72(b)(2). In accordance with R.S.C.A. § 16-50j-73, a copy of this letter is being sent to First Selectman Edmond V. Mone, Town of Thomaston, as the property owner, and Jeremy Leifert, Land Use Administrator and Zoning Enforcement Officer for the Town of Thomaston. Crown Castle is the tower owner.

1. The proposed modifications will not result in an increase in the height of the existing tower.

Page 2
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Sprint respectfully submits that the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § $16-$ 50j-72(b)(2). Please send approval/rejection letter to Attn: Anne Marie Zsamba.

Sincerely,
Anne Marie Zsamba, Esq.
Real Estate Specialist
3 Corporate Park Drive, Suite 101, Clifton Park, NY 12065
(201) 236-9224
annemarie.zsamba@crowncastle.com
Attachments:
Tab 1: Exhibit-A: Compound Plan and Elevation Depicting the Planned Changes
Tab 2: Exhibit-B: Structural Modification Report
Tab 3: Exhibit-C: General Power Density Table Report (RF Emissions Analysis Report)
cc: Edmond V. Mone, First Selectman
Thomaston Town Hall
158 Main Street
Thomaston, CT 06787
Jeremy Leifert
Land Use Administrator/Zoning Enforcement Officer
Thomaston Town Hall

Melanie A. Bachman
January 22, 2019
Page 3

158 Main Street
Thomaston, CT 06787
\&


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Use of this system constitutes your agreement to the service conditions in the current FedEx Service Guide, available on fedex.com. FedEx will not be responsible for any claim in excess of $\$ 100$ per package, whether the result of loss, damage, delay, non-delivery,misdelivery,or misinformation, unless you declare a higher value, pay an additional charge, document your actual loss and file a timely claim. Limitations found in the current FedEx Service Guide apply. Your right to recover from FedEx for any loss, including intrinsic value of the package, loss of sales, income interest, profit, attorney's fees, costs, and other forms of damage whether direct, incidental, consequential, or special is limited to the greater of $\$ 100$ or the authorized declared value. Recovery cannot exceed actual documented loss.Maximum for items of extraordinary value is $\$ 1,000$, e.g. jewelry, precious metals, negotiable instruments and other items listed in our ServiceGuide. Written claims must be filed within strict time limits, see current FedEx Service Guide.


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Town of Thomaston, Connecticut - Assessment Parcel Map
Parcel: 55-03-08
Address: 580 CHAPEL ST


## Thomaston, CT : Commercial Property Record Card

[ Back to Search Results ]
Search For Properties
$\square$
Account T0000001 Living Units 0

Owner Information
T Mobile (lessee) Town Of Thomaston (lessor) Crown Castle
Pmb331 4017 Washington Rd
Mcmurray PA 15317

## Deed Information

Book/Page:
Name


Deed Date:

Building Information
Building No: 1
Year Built: 1950
No of Units: 0
Structure Type: Phone/Electric Equipment Build
Grade: B
Identical Units: 1

| Valuation |  |
| :--- | ---: |
| Land: | $\$ 0$ |
| Building: | $\$ 473,714$ |
| Total: | $\$ 473,714$ |
| Net Assessment: | $\$ 331,600$ |

Sales History

| Book/Page | Date | Price | Type |
| :--- | :--- | :--- | :--- |
| Out Building Information <br> Structure Code |  |  |  |
| Width | Lgth/SqFt | Year |  |

## Exterior/Interior Information

Levels Size Use Type Ext. Walls Const. Type Partitions Heating A/C Plumbing Condition Func. Utility Unadj. RCNLD 01-01 1×620 Multi-Use Storage Brick/Stone Fireproof Normal None None Normal Good Good 14850

## Building Sketch

## Notice

## Tax Year 2015 Values

The information delivered through this on-line database is provided in the spirit of open access to government information and is intended as an enhanced service and convenience for citizens of Thomaston, CT.

The providers of this database: CLT, Big Room Studios, and Thomaston, CT assume no liability for any error or omission in the information provided here.

Currently All Values Have Not Been Finalized and Are Subject To Change.
Comments regarding this service should be directed to: Hudekfohomistone ape

Euitr sy

studios
$\%$

# THOMASTON ZONING BOARD OF APPEALS TOWN MALL THOMASTON, CT 06787 

## CERTIFICATE OF VARIANCE

This is to certify that the Thomaston Zoning Board of Appeals held a public hearing on July 18, 2000 , at 7.45 pm In Meeting Roon 1 of the Town Hall ori an application from Voice Stream Wireless Corporation of 100 Filley St, Bloonfield, CT, The applicants sought a vatance to permit their locating a grotind mounted tover for a wireless communioations facility on the west side of Chapel Street, approxinately 1,000 feet Gistait from the intersection of Chapel Street with Prospect Siret. The proposed tower is 175 feet in height The applieants requested permission to locate the tower 201 fet from the property line. The property so owned by the Townof Thomastogand is located in anRA 40 zone.

Sec 27.4. of the Zoning Regulations of the Town of Thomston provides that: , the minimum distance trom the base of any proposed ground atounted regulated foility to any property iline roadway, habitable dwelling, business or indistrial use, public receatonal areas, on public pathway Shall be the height of the facility and mount including any antennas or other appurtenances plus fifty per cent? Thus, 2625 feet was the equired setback.

With quorum present, the Board yoted unanimously to grant the variance. The reasons were, topordehic considerations soll confitions on other parts of the site, and concens over elevation on the sites

ATIEST: JosephF Wassong, Jr.


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& \text { Tomm of Thpmastan }
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$$

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\begin{aligned}
& 158 \text { 7hain Stret }
\end{aligned}
$$

Return Receipt Requested

November 9， 2000

Volce Strean Wireless
100 Filey street
Bloorifield，CT 06002

## Re：Specinl Permit Approval for a comercial <br> Cellular Telecommancations tower chapel street，Thomaston；Conn．

Dear sirts：
At lts meeting on Wednesday November 1，2000，the Thomaston Plafning and zoning Compission approved your Spedial Pempt Application to construct a comimetcial cellular comminications tower on municipal property the the of Chapel street．

The applioation wap approved wth the foltowing conditions：
1．Conduct an arnual RF inspecton and subnit the results to the comm 15 sion．

2．Regrade dhe dfeway as noted in Liand Tech＇s Letter datea． October 6；2000．

3．hgreed to，the terms and condtions s roted in a RXArom Phanmetrics dated November 1，2000，Tegneding items 12－ 15.

4．If the town deeldes not to haye the tower Lemoved，then the ste plari and inylu nust be revised．Any undertaring regarang the fownt tower shall be bon in acoordance： whth the condethons of the slgned conkrect．
sincerely．


Samuel Barto
stater HeZC
tand प⿱宀㠯 o olficer／zeo

Tufun of Thomaztm<br>SELECTMANSOFFICE TOWN HALL<br><br>THOMASTGN, CONNECTICUT O57B7 2353421<br>SEETECMEN'马 MEETIMG MINURES

At a meeting of the Board of Selectmen hald on April 25 , 2000 the following business wes condicted:
The meting opened at A:00 p.m. with the Entire Board in attendance: Elso attenaing were thomas C. Cuga of In felecom, Inc., Sam Barco Town Planner and ditorney George Seabourne.
Salectman Bramer read Fair Houshtg Resolution ant a Fif Housing Policy Sutement. (Cople st Attached)

Selectman pupont made motionto edopt the Rafr tousting Resolution and לhe setr Housing policy statement seconded by Selectmat o connell and Dassed than mously by Selectman Bander.
Selectian Bramer explained that as medphents of Smal elties Finding from the Deparment of Economic and Commutty Developrent we must adopt the above to reaffurn our comitment to Fair Houeting. Lariy Wagner the Town's Grants Coondinator hes been the administrator of the Town's projects an programs and Lorraine Bobb 15 our gestonated representative and is repponsible for the enforcement and limplementation of the fale hourng Regulathons.
gam berto feported to the board of setectilen that the rodoty system in Phese fit of the thghwood Earms gubdiyis on has ben hirpected by Town Engineer bob oley, Mighay Superintendent Gervy Grohosici and by himselitand te ts thein recomendathon that it beacopted es a Lown Road.
Seleeman otennell made motion to appove phase III Bectuon of the Hughwool Farms subdivision hs a Town approved road seonded by Selecthar Dupont and pased unenmoury by Gelectman Bramer.
Selectinn prpont made motion to ada Hughwod Farms pubivisionPhese to todey S Agend seconted by Splectan oformell and pased unanimously by Selectman Bramet:

 of gredit in the gthont of 60.000 .00 seconded by Selequman pupont: and passed unamimounly by seliectian Bramiet.
Copy of Hrevocable sendyy Heter of Erearumtented
Selectman Bramer teponted that Bepresentatises fom the fater compan
 to atsuss the desthn of the Water Extenshom to uppet ntgh street.

The Board of Betectmen brimply ment ower fown Attorney kybak ${ }^{1}$
 Thomaston and Omipoint Communicaeions, Inc. regafding the Comuhtoatigns Tover on Chapel Street.
Mr. Cusa said Iooking over the guggested changes, they will be acceptote, however icems that might imolve Fegeral pegtiations would be out of their eontroi.
Selectman olconnel made motion to acoept the propsed Lease Agtement between the 7bwn of Thomaston and omitpornt commundations; Inc. with tha sugestef ehanges made by Attorney Rybak and subject to the pppeval of Ehe Inland Wethends Gommeston; planitng and Zonng Comimssion and Town Merting Approvat seconded by selectman Dupont and Fasced inatimousty by belecench Bnammer.
Selectman bupent made motion to approve glent ce elars reguest that his renennhg yaretion hme for this year days) be hepe pate his ammersary dete of July 6,200 as ne is gotng on a eruse fh May of 2001 geconded by selectman otconnex and passed tnanimousty by Seleetman Bramet.

 Br anniet


Finst Selectuan


Selectan


# Torim at Thnometor  158 3 2 tuin 9 trest <br>  

Augusti 7, 2000

Volce Stream Wireless
Ioo Filley Street
Broomfleld, CT 06002
Attry Mr. Rick Frazier

Re: Special Permt Application tor a commechal Telecomunications Tower and Facility

## Deaf Mr; Frazler:

At its metting on Auguet 2, 2000, the Thomaston Plaming and Zontig compission accepted your Special Perait appleation. THe public hearing is scheduled. For Wedresday, septenber 6 , 2000, 解 7:00 ph. The meeting will be held in the tiena Morton att Gallery.

The comission has scheduled an on-ste inspection for Wednescay, August 30,2000 , at 6.30 pm . In accordance with the Zoning Regulttions, Section 277 , part L, the coraission tequests that you send ploft a ste taentricathon balioon on or Just prior to the dey of inspection. My ottice wil pubAish a legal notice prior to the ratelng. The Site walk will be ppen to the public.

PTease mare sure to aaress each of the tequirements in Artche XXVII at the pibilc hearing. This ghouta insure a very thorough and informathe publid hearing.

If you have any questions, comments onsuggestansp please Eeel free to call the lana Use office at: $283-8411$.


Samel Barto
Land Use ofticer

PLeas Note The bal100n
Bhall atso be ralsed at least daysprot to the publue hearlng.

# SPECIAL PERMIT APPLICATION <br> Town of Thomaston, Connecticut 



Date Received:

## Application Jor a special permit

applicant: Voice Stareqm/Omnipoint Wireless Address


The undersigned hereby fakes appliagtion to the planning and
 provisions of Section 3. 11 - schedule A permitted Use era Article IX of the Momaston zoning Regulations.


Section, Previous application

Hes a previous Special perm Application been fluedwhthe the Comiselon tor the same premises? Yes: $\qquad$

Sector 2. Placement on Agenda

In order for the compselon to consheryour application, it must be received $1 n$ the planing and zoning of the (Han duse. office no later that flue (5) working day prior to the next Hegharty scheduled meting.

Section 3. PLans and Dodutentation

A11 Special permit applications unless otherwise prescribed in the Zoning Regulations or directed by the commission, must. be accompanied by the following documentation:

Tivari of Thpmasten


158 3itain Street


Auqust 7, 2000

Voice Stream Wireless
100 Filley Street
Bloonfield, CT 06002
Atti: Mr. Rtok Frazier.

Re; Special pernit Application for a commercial
Telecomminations Tower and racility

Dear Mr. Hrazier:
At its meeting on Autust 2, 2000, the Thomaston Planning and Zoning Commission accepted your special permit Application. The public hearhig is schedulea for Wednesary, September 6 , 2000, 解 $7,00 \mathrm{p}$. The meeting will be held in Ghe Lena Morton Att galiery.

The Comisston has schecuied an on-site lnspection for tednesday, August 30,2000 , at 6,30 . .m. In accordanee whth the Zoning Regulttions, Section 27.7 , Fart 1 , the Commission wequests that you send aloft, site ldentlication balloon on or Just prior to the alay of inspection. My oftce wil pubthsh a legat notice prior te the ratsing the bite walk wil be open to the pubilo.

Please make sure to addesseach of the requirements in art LCle XXVII, the publie hearing, This should insure a very thorough end informative public heasing:

Tf you neve any questons, ooments or plggedtons, pease: reel Iree to deall the Lanc Use onfice at $283-8414$.
sinoenely.


Samuel Barto IAnA Use Officer

Please Note, The bailoon Shell atso be ratsed de Heat 3 dus prior to the pubtic herring.
A. A "gtatemgnt of Use" whtch shall detail the proposed use of the site,
b. Site Plan and Lendseaping plan.
C. Archifectural and construction PIan
d. FHopd Hapard Area Data
e. Soi 1 Fosion and Setimentation control Phan
f. 11 other pertinent infonmaton and oonmentation that fay be requared by the Commpstion in onder to mae a deciston on the appliedtion.

## Section 4. Application Fees

a. Standard Application Fee: $\$ 150.00$
b. Home Dccupation Permet $\$ 100.00$

Section 5. Watyer of Requirements

 or 9.3 .4 of the zonthg Regulations?

Yes $\qquad$ - Ho: $\qquad$
If yes, Whease spectut

Sectan 6. Fxtenslon of Replew Petrod

Wh the appleant ronsent to apornat extenston of time in ofder foz the conidspon to take action on this pppication?
Yes: $\qquad$ $\therefore$ No: $\qquad$
It yes, piease spertiy pertod or datez $\qquad$

Section 7. Failure to Submit

Failure by an applicant to submit any or all of the reguired or requested docinentation inder section 3.11 or Article IX may be grounds for the comission to oonstare the applicathon as being incomplete.

Section 8 . Review by Town Erigneer

The applicant shal he mesponsible for peylng all inspection and review costs, incurped by the Town Engineer during the fevew process.

If additionat on-site inspection and review is necessary and Tequired by the Comission after the appobed ls granted and prioe to completion of the project, the applicant shall also be Tesponsible for these costs.

The costs shal be no more per hour than phat ts assessed to the Town in any given Year by the Town Enguneer.

Section 9. Public Hearkg

The Thometon Plenning and ZOMAng Comitsion will oonduct a "publie Feering" on th, application. The appileant, or thelr athoriget pgent, must be present at the hearing gnd shouta Beprepared to present information showing how the proposed use of the fite along with the builange, structures, and tachlithes whil conform to the standards as spectifed frese. Regulations.

A1 standarde as specirtid in Anticle $4 x$ ate $1 n$ adatiton 60 other reguirenients as contuned in the Regurtions. when nay be applicoble $1 n$ the District in thich the spedial penit is proposed.
section 10. Inspection of Property

Whe Comiselon is authorized by the subission of this apozention to inepect the premises.

Section 11. Additional Information

The commission may obtain additional documentation ana infornation on its own initiative but will need to rely upon data presented to it by the applicant.

Section 22. Modification of Approval.

If approval is granted by the Planing and zoning Commission, it may be subject to toonfiertions deemed necessary to conform to specific standards of the Regulations. It may ale be Subject to appropriate conditions and safeguards nefesery to conserve public health kind safety, convenience, welfare and property values in the neighborhood.

Applicants signature:
 Home Phone: 6932721
 Business Phone: 860675529

OPRTCE USE
comisshon date when application was received. $\qquad$
Date of mutual pubile Hearing $\qquad$
public Hearing was continued to: $\qquad$

Date of approval e $\qquad$ Disapproval: $\qquad$
Was approval. iodine:
Yes: $\qquad$ No: $\qquad$
If yes, give specifics: $\qquad$
$\qquad$
$\qquad$








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Date: December 13, 2018
Heather Simeone
Crown Castle
3530 Toringdon Way Suite 300
Charlotte, NC 28277

Black \& Veatch Corp.
6800 W. 115th St., Suite 2292
Overland Park, KS 66211
(913) 458-8145

| Structural Analysis Report |  |
| :---: | :---: |
| AT\&T Mobility Co-Locate |  |
| Carrier Site Number: | 10107966 |
| Carrier Site Name: | CTL01062 |
| Crown Castle BU Number: | 823530 |
| Crown Castle Site Name: | CT364/Chapel St. |
| Crown Castle JDE Job Number: | 548514 |
| Crown Castle Work Order Number: | 1669286 |
| Crown Castle Order Number: | 471611 Rev. 0 |
| Black \& Veatch Corp. Project Number: | 400087 |
| 580 Chapel Street, Thomaston, Litchfield County, CT |  |
| Latitude $41^{\circ} 39^{\prime} 48.48^{\prime \prime}$, Longitude -73 ${ }^{\circ} \mathbf{4}^{\prime} \mathbf{2 7 . 4 1 "}$ |  |
| 175 Foot - Monopole Tower |  |

580 Chapel Street, Thomaston, Litchfield County, CT
175 Foot - Monopole Tower

## Subject:

## Carrier Designation:

## Crown Castle Designation:

Monopole

Engineering Firm Designation:
Site Data:

Dear Heather Simeone,
Black \& Veatch Corp. is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above-mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Proposed Equipment Configuration
Sufficient Capacity
This analysis utilizes an ultimate 3 -second gust wind speed of 120 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Structural analysis prepared by: Neeraj Jog

Respectfully submitted by:


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tnxTower Output
6) APPENDIX B

Base Level Drawing
7) APPENDIX C

Additional Calculations

## 1) INTRODUCTION

This tower is a 175 ft Monopole tower designed by PiRod Manufactures Inc.
2) ANALYSIS CRITERIA

| Building Code: | 2018 IBC |
| :--- | :--- |
| TIA-222 Revision: | TIA-222-H |
| Risk Category: | II |
| Wind Speed: | 120 mph |
| Exposure Category: | B |
| Topographic Factor: | 1 |
| lce Thickness: | 1.500 in |
| Wind Speed with Ice: | 50 mph |
| Service Wind Speed: | 60 mph |

Table 1 - Proposed Equipment Configuration

| Mounting <br> Level (ft) | Center Line Elevation (ft) | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 142.0 | 143.0 | 1 | cci antennas | HPA65R-BU4A w/ Mount Pipe | $\begin{gathered} 12 \\ 2 \\ 6 \end{gathered}$ | $\begin{gathered} 15 / 8 \\ 3 / 8 \\ 3 / 4 \end{gathered}$ |
|  |  | 2 | cci antennas | HPA65R-BU6A w/ Mount Pipe |  |  |
|  |  | 3 | ericsson | RADIO 4415 B30 |  |  |
|  |  | 3 | ericsson | RRUS 4449 B5/B12 |  |  |
|  |  | 3 | ericsson | RRUS 4478 B14 |  |  |
|  |  | 3 | ericsson | RRUS 8843 B2/B66A |  |  |
|  |  | 2 | kathrein | 80010964 w/ Mount Pipe |  |  |
|  |  | 4 | kathrein | 80010965 w/ Mount Pipe |  |  |
|  |  | 3 | powerwave technologies | 7770.00 w/ Mount Pipe |  |  |
|  |  | 6 | powerwave technologies | LGP21401 |  |  |
|  |  | 2 | raycap | DC6-48-60-18-8F |  |  |
|  | 142.0 | 1 | cci tower mounts | Miscellaneous [NA 507-1] |  |  |
|  |  | 1 | crown mounts | Platform Mount [LP 303-1] |  |  |
|  |  | 1 | raycap | DC6-48-60-18-8F |  |  |

Table 2 - Other Considered Equipment

| Mounting Level (ft) | Center Line Elevation (ft) | Nümber of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 172.0 | 175.0 | 2 | andrew | VHLP2.6 | $3$ | $\begin{gathered} 15 / 8 \\ 7 / 8 \end{gathered}$ |
|  | 172.0 | 1 | andrew | ATJB200-A01-007 |  |  |
|  |  | 2 | andrew | ETW190VS12UB |  |  |
|  |  | 1 | cci tower mounts | Platform Mount [LP 701-1] |  |  |
|  |  | 3 | commscope | ATBT-BOTTOM-24V |  |  |
|  |  | 3 | commscope | LNX-6515DS-VTM w/ Mount Pipe |  |  |


| Mounting Level (ft) | Center Line Elevation (ft) | $\left\lvert\, \begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}\right.$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 3 | ems wireless | $\underset{\substack{\text { RR90-17-02DP w/ Mount } \\ \text { Pipe }}}{ }$ |  |  |
|  | 168.0 | 1 | bird technologies group | OA20-67-DIN |  |  |
|  |  | 1 | lone star electronics | LS-230C |  |  |
| 168.0 | 171.0 | 1 | lone star electronics | LS-230C | 6 | 7/8 |
|  | 168.0 | 1 | cci tower mounts | $\text { Side Arm Mount [SO } 701 \text { - }$ |  |  |
| 162.0 | 162.0 | 3 | alcatel lucent | 800 MHz 2 X 50 W RRH WIFILTER | 4 | $11 / 4$ |
|  |  | 3 | alcatel lucent | PCS $1900 \mathrm{MHz} 2 \times 40 \mathrm{~W}$ |  |  |
|  |  | 3 | alcatel lucent | TD-RRH8×20-25 |  |  |
|  |  | 1 | cci tower mounts | Platform Mount [LP 712-1] |  |  |
|  |  | 3 | rfs celwave | APXVSPP18-C-A20 w/ Mount Pipe |  |  |
|  |  | 3 | rfs celwave | APXVTM14-C-120 w/ Mount Pipe |  |  |
| 152.0 | 152.0 | 6 | antel | LPA-80080/4CF w/ Mount <br> Pipe | 61 | $\begin{aligned} & 15 / 8 \\ & 13 / 8 \end{aligned}$ |
|  |  | 1 | cci tower mounts | Sector Mount [SM 801-3] |  |  |
|  |  | 6 | commscope | NNHH-65B-R4 w/ Mount Pipe |  |  |
|  |  | 1 | raycap | RVZDC-6600-PF-48 |  |  |
|  |  | 3 | samsung <br> telecommunications | RFV01U-D1A |  |  |
|  |  | 3 | $\begin{array}{\|c\|} \hline \text { samsung } \\ \text { telecommunications } \end{array}$ | RFV01U-D2A |  |  |
| 115.0 | 115.0 | 3 | rfs celwave | $\begin{gathered} \text { APXV18-206517S-C w/ } \\ \text { Mount Pipe } \end{gathered}$ | 6 | $15 / 8$ |
| 50.0 | 50.0 | 1 | cci tower mounts | Side Arm Mount [SO 701- $1]$ | 1 | 1/2 |
|  |  | 1 | pctel | GPS-TMG-HR-26NCM |  |  |

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| 4-GEOTECHNICAL REPORTS | FDH Engineering, Inc. | 3462674 | CCISITES |
| 4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS | Pirod, Inc. | 3464631 | CCISITES |
| 4-TOWER MANUFACTURER DRAWINGS | Pirod, Inc. | 3462695 | CCISITES |

## 3.1) Analysis Method

$\operatorname{tn} \times$ Tower (version 8.0.4.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases.
Selected output from the analysis is included in Appendix A.

## 3.2) Assumptions

1) Tower and structures were built in accordance with the manufacturer's specifications.
2) The tower and structures have been maintained in accordance with the manufacturer's specification.
3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
4) This analysis was performed under the assumption that all information provided to Black \& Veatch is current and correct. This is to include site data, appurtenance loading, tower/foundation details, and geotechnical data. The loading on the structure is based on CAD level drawings and carrier orders provided by the owner. If any of this information is not current and correct, this report should be considered obsolete and further analysis will be required.

This analysis may be affected if any assumptions are not valid or have been made in error. Black \& Veatch Corp. should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary) (Monopole Tower)

| Section No. | Elevation (ft) | Component Type | Size | Critical Element | $P(K)$ | SFPR allow (K) | $\%$ Capacity | Pass/Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 175-164.25 | Pole | TP26x22x0.25 | 1 | -4.15 | 1512.93 | 4.3 | Pass |
| L2 | $\begin{gathered} 164.25- \\ 129.67 \end{gathered}$ | Pole | TP34.0625x24.4135x0.3125 | 2 | -17.94 | 2472.98 | 30.9 | Pass |
| L3 | 129.67-96 | Pole | TP41.75×32.452x0.375 | 3 | -26.07 | 3620.12 | 42.9 | Pass |
| L4 | 96-63.17 | Pole | TP49.0625x39.8421×0.375 | 4 | -35.67 | 4051.65 | 54.2 | Pass |
| L5 | 63.17-31.17 | Pole | TP56.125x46.9602×0.375 | 5 | -46.67 | 4409.30 | 62.1 | Pass |
| L6 | 31.17-0 | Pole | TP62.9375×53.8475×0.375 | 6 | -60.95 | 4763.53 | 69.3 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Pole (L6) | 69.3 | Pass |
|  |  |  |  |  |  | Rating = | 69.3 | Pass |

Table 5 - Tower Component Stresses vs. Capacity (Monopole Tower) - LC7

| Notes | Component | Elevation (ft) | \% Capacity | Pass /Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Anchor Rods | 0 | 62.6 | Pass |
| 1,2 | Base Plate | 0 | - | Pass |
| 1 | Base Foundation | 0 | 66.6 | Pass |
| 1 | Base Foundation Soil Interaction | 0 | 65.4 | Pass |



Notes:

1) See additional documentation in "Appendix C-Additional Calculations" for calculations supporting the \% capacity consumed. Rating per TIA-222-H Section 15.5.
2) Base and flange plate design methodology of the manufacturer has been reviewed and found to be an acceptable means of designing to resist the full capacity of the bolts and shaft.

## 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration: No modifications are required at this time.

## APPENDIX A

## TNXTOWER OUTPUT


MATERIAL STRENGTH

| MATERIAL STRENGTH |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| GRADE | Fy | Fu | GRADE | Fy | Fu |
| A 472.65 | 65 ksi | 30 ksi |  |  |  |

## TOWER DESIGN NOTES

1. Tower is located in Litchfield County, Connecticut
2. Tower designed for Exposure B to the TIA-222-H Standard.
3. Tower designed for a 120 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 50 mph basic wind with 1.27 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TIA-222-H Annex S.
9. TOWER RATING: $69.3 \%$

| Client: Crown Castle | Drawn by: Josh Riley | App'd: |
| :---: | :---: | :---: |
| Code: TliA-222-H | Date: $12 / 13 / 18$ | Scale: NT ; |
|  |  | ${ }_{\text {di }}$ wig No. E - |

## Tower Input Data

The tower is a monopole.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:

1) Tower is located in Litchfield County, Connecticut.
2) Tower base elevation above sea level: 543.00 ft .
3) Basic wind speed of 120 mph .
4) Risk Category II.
5) Exposure Category B.
6) Simplified Topographic Factor Procedure for wind speed-up calculations is used.
7) Topographic Category: 1.
8) Crest Height 0.00 ft .
9) . Nominal ice thickness of 1.2750 in.
10) Ice thickness is considered to increase with height.
11) Ice density of 56 pcf.
12) A wind speed of 50 mph is used in combination with ice.
13) Temperature drop of $50^{\circ} \mathrm{F}$.
14) Deflections calculated using a wind speed of 60 mph .
15) TIA-222-H Annex S..
16) A non-linear (P-delta) analysis was used.
17) Pressures are calculated at each section.
18) Stress ratio used in pole design is 1.05 .
19) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

| Consider Moments - Legs | Distribute Leg Loads As Uniform | Use ASCE $10 \times$-Brace Ly Rules |
| :---: | :---: | :---: |
| Consider Moments - Horizontals | Assume Legs Pinned | Calculate Redundant Bracing Forces |
| Consider Moments - Diagonals | $\checkmark$ Assume Rigid Index Plate | Ignore Redundant Members in FEA |
| Use Moment Magnification | $\sqrt{ }$ Use Clear Spans For Wind Area | SR Leg Bolts Resist Compression |
| Use Code Stress Ratios | Use Clear Spans For KL/r | All Leg Panels Have Same Allowable |
| Use Code Safety Factors - Guys | Retension Guys To Initial Tension | Offset Girt At Foundation |
| Escalate lce | $\checkmark$ Bypass Mast Stability Checks | $\sqrt{ }$ Consider Feed Line Torque |
| Always Use Max Kz | $\checkmark$ Use Azimuth Dish Coefficients | Include Angle Block Shear Check |
| Use Special Wind Profile | $\sqrt{ } \sqrt{\text { Project Wind Area of Appurt. }}$ | Use TIA-222-H Bracing Resist. Exemption |
| Include Bolts In Member Capacity | Autocalc Torque Arm Areas | Use TIA-222-H Tension Splice Exemption |
| Leg Bolts Are At Top Of Section | Add IBC. $6 \mathrm{D}+\mathrm{W}$ Combination |  |
| Secondary Horizontal Braces Leg | Sort Capacity Reports By Component | $\sqrt{ }$ Include Shear-Torsion Interaction |
| Use Diamond Inner Bracing (4 Sided) | Triangulate Diamond Inner Bracing | Always Use Sub-Critical Flow |
| SR Members Have Cut Ends | Treat Feed Line Bundles As Cylinder | Use Top Mounted Sockets |
| SR Members Are Concentric | Ignore KL/ry For 60 Deg. Angle Legs | Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known |

## Tapered Pole Section Geometry

| Section | Elevation <br> ft | Section Length ft | Splice Length ft | Number of Sides | Top Diameter in | Bottom <br> Diameter <br> in | Wall Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 175.00-164.25 | 10.75 | 2.92 | 18 | 22.0000 | 26.0000 | 0.2500 | 1.0000 | $\begin{gathered} \hline \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L. 2 | 164.25-129.67 | 37.50 | 3.83 | 18 | 24.4135 | 34.0625 | 0.3125 | 1.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |

175 Ft Monopole Tower Structural Analysis
Project Number 400087, Order 471611, Revision 0

| Section | Elevation <br> ft | Section <br> Length <br> ft | Splice Length ft | Number of Sides | $\begin{gathered} \text { Top } \\ \text { Diameter } \\ \text { in } \end{gathered}$ | Bottom Diameter in | Wall <br> Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L3 | 129.67-96.00 | 37.50 | 4.67 | 18 | 32.4520 | 41.7500 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L4 | 96.00-63.17 | 37.50 | 5.50 | 18 | 39.8421 | 49.0625 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L5 | 63.17-31.17 | 37.50 | 6.25 | 18 | 46.9602 | 56.1250 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L6 | 31.17-0.00 | 37.42 |  | 18 | 53.8475 | 62.9375 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |

Tapered Pole Properties

| Section | Tip Dia. in | Area $i n^{2}$ | $1$ | $\begin{gathered} r \\ \text { in } \end{gathered}$ | $\begin{aligned} & C \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 1 / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{gathered} \hline i t / Q \\ i n^{2} \\ \hline \end{gathered}$ | $\begin{aligned} & w \\ & \text { in } \end{aligned}$ | w/t |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 22.3008 | 17.2586 | 1031.4832 | 7.7212 | 11.1760 | 92.2945 | 2064.3237 | 8.6310 | 3.4320 | 13.728 |
|  | 26.3625 | 20.4326 | 1711.6544 | 9.1412 | 13.2080 | 129.5922 | 3425.5610 | 10.2183 | 4.1360 | 16.544 |
| L2 | 25.5048 | 23.9052 | 1754.2801 | 8.5559 | 12.4021 | 141.4508 | 3510.8685 | 11.9549 | 3.7468 | 11.99 |
|  | 34.5398 | 33.4758 | 4817.4335 | 11.9812 | 17.3038 | 278.4040 | 9641.2058 | 16.7411 | 5.4450 | 17.424 |
| L3 | 33.8591 | 38.1797 | 4963.1505 | 11.3873 | 16.4856 | 301.0593 | 9932.8316 | 19.0935 | 5.0516 | 13.471 |
|  | 42.3362 | 49.2466 | $\begin{gathered} 10650.982 \\ 2 \end{gathered}$ | 14.6881 | 21.2090 | 502.1916 | $\begin{gathered} 21315.979 \\ 3 \end{gathered}$ | 24.6280 | 6.6880 | 17.835 |
| L4 | 41.5648 | 46.9757 | 9244.4482 | 14.0108 | 20.2398 | 456.7464 | $\begin{gathered} 18501.060 \\ 4 \end{gathered}$ | 23.4923 | 6.3522 | 16.939 |
|  | 49.7615 | 57.9503 | $\begin{gathered} 17355.137 \\ 8 \end{gathered}$ | 17.2841 | 24.9238 | 696.3293 | $\begin{gathered} 34733.111 \\ 9 \end{gathered}$ | 28.9807 | 7.9750 | 21.267 |
| L5 | 48.9917 | 55.4480 | $\begin{gathered} 15202.631 \\ 8 \end{gathered}$ | 16.5377 | 23.8558 | 637.2728 | $\begin{gathered} 30425.267 \\ 7 \end{gathered}$ | 27.7293 | 7.6050 | 20.28 |
|  | 56.9330 | 66.3564 | $\begin{gathered} 26056.150 \\ 6 \end{gathered}$ | 19.7913 | 28.5115 | 913.8821 | $\begin{gathered} 52146.586 \\ 5 \end{gathered}$ | 33.1845 | 9.2180 | 24.581 |
| L6 | 56.1620 | -63.6457 | $\begin{gathered} 22991.526 \\ 9 \end{gathered}$ | 18.9827 | 27.3545 | 840.5012 | $\begin{gathered} 46013.306 \\ 6 \end{gathered}$ | 31.8289 | 8.8172 | 23.512 |
|  | 63.8506 | 74.4650 | $\begin{gathered} 36822.894 \\ 6 \\ \hline \end{gathered}$ | 22.2097 | 31.9722 | 1151.7142 | $\begin{gathered} 73694.241 \\ 7 \\ \hline \end{gathered}$ | 37.2396 | 10.4170 | 27.779 |


| Tower Elevation $\qquad$ <br> ft | Gusset Area (per face) $\qquad$ $f^{2}$ | Gusset Thickness in | Gusset GradeAdjust. Factor $A_{f}$ | Adjust. Factor $A_{r}$ | Weight Mult. | $\begin{gathered} \text { Double Angle } \\ \text { Stitch Bolt } \\ \text { Spacing } \\ \text { Diagonals } \\ \text { in } \\ \hline \end{gathered}$ | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { L1 } 175.00- \\ 164.25 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L2 164.25- } \\ \quad 129.67 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L3 } 129.67- \\ 96.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L4 96.00- } \\ 63.17 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| ${ }_{31.17}^{\text {L5 } 63.17-}$ |  |  | 1 | 1 | 1 |  |  |  |
| L6 31.17-0.00 |  |  | 1 | 1 | 1 |  |  |  |

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Sector | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement <br> ft | Total Number | Number Per Row | Start/En <br> d <br> Position | Width or Diamete $r$ in | Perimete <br> $r$ <br> in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Safety Line 3/8 | A | No | Surface Ar (CaAa) | $\begin{gathered} 175.00- \\ 8.00 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 0.0000 |  | 0.22 |
| $\begin{gathered} \text { HB158-1-08U8-S8J18( } \\ \left.1-5 / 8^{\prime \prime}\right) \end{gathered}$ | A | No | Surface Af (CaAa) | $\begin{gathered} 152.00- \\ 8.00 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.060 \end{aligned}$ | 0.0000 | 3.9600 | 1.30 |


| Description | Sector | Exclude <br> From <br> Torque Calculation | $\begin{gathered} \hline \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement <br> ft | Total Number | Number Per Row | Start/En d Position | Width or Diamete $r$ in | Perimete $r$ in | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LDF7-50A(1-5/8) | C | No | $\begin{aligned} & \text { Surface Af } \\ & \text { (CaAa) } \end{aligned}$ | $\begin{gathered} 115.00- \\ 8.00 \end{gathered}$ | 6 | 6 | $\begin{gathered} -0.050 \\ 0.183 \end{gathered}$ | 0.0000 | 3.9600 | 0.82 |
| LDF4-50A(1/2) | C | No | Surface Af (CaAa) | $\begin{gathered} 50.00- \\ 8.00 \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.150 \\ & -0.090 \end{aligned}$ | 0.0000 | 1.2500 | 0.15 |

Feed Line/Linear Appurtenances - Entered As Area

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude From Torque Calculation | $\begin{gathered} \hline \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement $f t$ | Total Number |  | $\begin{aligned} & C_{A} A_{A} \\ & {f t^{2} / f t}^{2} \end{aligned}$ | Weight <br> $p l f$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| *** | Calculation |  |  |  |  |  |  |  |  |
| AVA5-50(7/8") | A | No | No | Inside Pole | 172.00-8.00 | 3 | No Ice | 0.00 | 0.30 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.30 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.30 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.30 |
| LDF7-50A(1-5/8') | A | No | No | Inside Pole | 172.00-8.00 | 12 | No lce | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.82 |
| *** |  |  |  |  |  |  |  |  |  |
| LDF5-50A(7/8') |  |  |  |  | B | No | No | Inside Pole | 168.00-8.00 | 6 | No Ice | 0.00 | 0.33 |
|  | 1/2" Ice | 0.00 | 0.33 |  |  |  |  |  |  |  |
|  | 1 1' Ice | 0.00 | 0.33 |  |  |  |  |  |  |  |
|  | 2 Ice | 0.00 |  |  |  |  |  |  |  |  |
| *** |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \text { HB114-1-08U4- } \\ & \text { M5J(1-1/4") } \end{aligned}$ | C | No | No | Inside Pole | 162.00-8.00 | 3 | No Ice | 0.00 | 1.08 |  |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 1.08 |  |
|  |  |  |  |  |  |  | 1 " Ice | 0.00 | 1.08 |  |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 1.08 |  |
| $\begin{gathered} \text { HB114-21U3M12- } \\ \text { XXXF(1-1/4) } \end{gathered}$ | C | No | No | Inside Pole | 162.00-8.00 | 1 | No lce | 0.00 | 1.22 |  |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 1.22 |  |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 1.22 |  |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 1.22 |  |
| *** |  |  |  |  |  |  |  |  |  |  |
| LDF7-50A(1-5/8") | A | No | No | Inside Pole | 152.00-8.00 | 6 | No Ice | 0.00 | 0.82 |  |
|  |  |  |  |  |  |  | 1/2" lce | 0.00 | 0.82 |  |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.82 |  |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.82 |  |
| *** |  |  |  |  |  |  |  |  |  |  |
| 2" innerduct conduit | B | No | No | Inside Pole | 142.00-8.00 | 2 |  | 0.00 |  |  |
|  |  |  |  |  |  |  | $1 / 2^{\prime \prime} \text { Ice }$ | 0.00 | 0.20 |  |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.20 |  |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.20 |  |
| AVA7-50(1-5/8) | B | No | No | Inside Pole | 142.00-8.00 | 12 | No lce | 0.00 | 0.70 |  |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.70 |  |
|  |  |  |  |  |  |  | 1 ' Ice | 0.00 | 0.70 |  |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.70 |  |
| WR-VG86STBRD(3/4) | B | No | No | Inside Pole | 142.00-8.00 | 6 |  | 0.00 | 0.58 |  |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.58 |  |
|  |  |  |  |  |  |  | 1 ' Ice | 0.00 | 0.58 |  |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.58 |  |
| $\begin{aligned} & \text { FB-L98-002-XXX( } \\ & \left.3 / 8^{\prime \prime}\right) \end{aligned}$ | B | No | No | Inside Pole | 142.00-8.00 | 1 | No lce | 0.00 | 0.06 |  |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.06 |  |
|  |  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.00 | 0.06 |  |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.06 |  |
| $\begin{gathered} \text { FB-L.98B-034- } \\ \text { XXX(3/8") } \end{gathered}$ | B | No | No | Inside Pole | 142.00-8.00 | 1 | No lce | 0.00 | 0.06 |  |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.06 |  |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.06 |  |
|  |  |  |  |  |  |  | 2"Ice | 0.00 | 0.06 |  |
| *** |  |  |  |  |  |  |  |  |  |  |

Feed Line/Linear Appurtenances Section Areas

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
\(n\)
\end{tabular} \& Tower Elevation ft \& Face \& \(A_{R}\)
\(f t^{2}\) \& \(A_{F}\)

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\ln \mathrm{Face} \\
\mathrm{ft}^{2}
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
f t^{2}
\end{gathered}
$$
\] \& Weight

$K$ <br>
\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{175.00-164.25} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.09 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{12} \& \multirow[t]{3}{*}{164.25-129.67} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.52 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.22 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.14 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{129.67-96.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.58 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.49 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.24 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{$96.00-63.17$} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.56 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.47 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.31 <br>
\hline \multirow[t]{3}{*}{L5} \& \multirow[t]{3}{*}{63.17-31.17} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.55 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.46 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.30 <br>
\hline \multirow[t]{3}{*}{L6} \& \multirow[t]{3}{*}{31.17-0.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.40 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.33 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.22 <br>
\hline
\end{tabular}

Feed Line/Linear Appurtenances Section Areas - With Ice

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
\(n\)
\end{tabular} \& Tower Elevation ft \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg } \\
\hline
\end{gathered}
\] \& ice
Thickness
in \& \(A_{R}\)

$f t^{2}$ \& $A_{F}$

$t^{2}$ \&  \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$ \& Weight

K <br>
\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{175.00-164.25} \& A \& \multirow[t]{3}{*}{1.502} \& 0.000 \& 0.000 \& 3.229 \& 0.000 \& 0.12 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.01 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{164.25-129.67} \& A \& \multirow[t]{3}{*}{1.480} \& 0.000 \& 0.000 \& 17.092 \& 0.000 \& 0.74 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.22 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.14 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{129.67-96.00} \& A \& \multirow[t]{3}{*}{1.441} \& 0.000 \& 0.000 \& 19.928 \& 0.000 \& 0.85 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.49 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.35 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{$96.00-63.17$} \& A \& \multirow[t]{3}{*}{1.392} \& 0.000 \& 0.000 \& 18.926 \& 0.000 \& 0.82 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.47 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.48 <br>
\hline \multirow[t]{3}{*}{L5} \& \multirow[t]{3}{*}{63.17-31.17} \& A \& \multirow[t]{3}{*}{1.321} \& 0.000 \& 0.000 \& 17.816 \& 0.000 \& 0.79 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.46 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 5.242 \& 0.000 \& 0.53 <br>
\hline \multirow[t]{3}{*}{16} \& \multirow[t]{3}{*}{31.17-0.00} \& A \& \multirow[t]{3}{*}{1.180} \& 0.000 \& 0.000 \& 12.246 \& 0.000 \& 0.55 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.33 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 6.123 \& 0.000 \& 0.40 <br>
\hline
\end{tabular}

## Feed Line Center of Pressure

| Section | Elevation | $C P_{X}$ | $C P_{Z}$ | $C P_{X}$ | $C P_{Z}$ <br> Ice |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | f | in | in | in | in |
|  | in |  |  |  |  |
| L1 | $175.00-164.25$ | 0.0000 | 0.0000 | -1.0288 | -0.5940 |
| L2 | $164.25-129.67$ | 0.0000 | 0.0000 | -1.6935 | -1.0942 |
| L3 | $129.67-96.00$ | 0.0000 | 0.0000 | -1.9374 | -1.2834 |
| L4 | $96.00-63.17$ | 0.0000 | 0.0000 | -1.9075 | -1.2636 |
| L5 | $63.17-31.17$ | 0.0000 | 0.0000 | -1.5357 | -0.6195 |
| L6 | $31.17-0.00$ | 0.0000 | 0.0000 | -0.9741 | -0.1633 |

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

Shielding Factor Ka

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{\mathrm{a}} \\ \text { No lce } \end{gathered}$ | $\begin{aligned} & K_{g} \\ & k e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L. 1 | 1 | Safety Line 3/8 | $\begin{array}{r} 164.25- \\ 175.00 \end{array}$ | 1.0000 | 1.0000 |
| L1 | 12 | HB158-1-08U8-S8J18( $1-$ $\left.5 / 88^{\prime \prime}\right)$ | $\begin{array}{r} 164.25- \\ 152.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 1 | Safety Line 3/8 | $\begin{array}{r} 129.67- \\ 164.25 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 12 | HB158-1-08U8-S8J18(1- | $\begin{array}{r} 129.67- \\ 152.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 20 | LDF7-50A(1-5/8) | 129.67 - | 1.0000 | 1.0000 |
| L3 | 1 | Safety Line 3/8 | 115.00 $96.00-$ | 1.0000 | 1.0000 |
|  |  |  | 129.67 |  |  |
| L3 | 12 | HB158-1-08U8-S8J18(1- | $\begin{aligned} & 96.00- \\ & 129.67 \end{aligned}$ | 1.0000 | 1.0000 |
| L3 | 20 | LDF7-50A(1-5/8) | $96.00-$ | 1.0000 | 1.0000 |
|  |  |  | 115.00 |  |  |
| 14 | 1 | Safety Line 3/8 | $\begin{array}{r} 63.17- \\ 96.00 \end{array}$ | 1.0000 | 1.0000 |
| L4 | 12 | HB158-1-08U8-S8J18( $1-$ | 63.17 - | 1.0000 | 1.0000 |
|  |  | LDF7-50A $(1-5 / 8)$ | 96.00 |  |  |
| L4 | 20 | LDF7-50A(1-5/8) | $\begin{array}{r} 63.17-1 \\ 96.00 \end{array}$ | 1.0000 | 1.0000 |
| L4 | 22 | LDF4-50A(1/2) | $63.17-$ | 1.0000 | 1.0000 |
|  |  |  | 50.00 |  |  |
| L5 | 1 | Safety Line 3/8 | $\begin{array}{r} 31.17 \\ 63.17 \end{array}$ | 1.0000 | 1.0000 |
| L5 | 12 | HB158-1-08U8-S8J18( $1-$ | $31.17-$ | 1.0000 | 1.0000 |
|  |  | $\left.5 / 8^{\prime \prime}\right)$ | 63.17 |  |  |
| L5 | 20 | LDF7-50A(1-5/8) | $\begin{array}{r} 31.17 \\ 63.17 \end{array}$ | 1.0000 | 1.0000 |
| L5 | 22 | LDF4-50A(1/2) | $31.17-$ | 1.0000 | 1.0000 |

## Discrete Tower Loads

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: Horz Lateral Vert ft ft ft | Azimuth Adjustmen $t$ <br> - | Placement |  | $C_{A} A_{A}$ Front $f^{2}$ | $C_{A} A_{A}$ Side $f^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lightning Rod 5/8"x6' | C | From Leg | 0.00 | 0.0000 | 175.00 | No Ice | 0.38 | 0.38 | 0.01 |
|  |  |  | 0.00 |  |  | 1/2' | 0.99 | 0.99 | 0.01 |
|  |  |  | 3.00 |  |  | Ice | 1.62 | 1.62 | 0.02 |
|  |  |  |  |  |  | $\begin{aligned} & \text { 1" lce } \\ & 2 " \text { lce } \end{aligned}$ | 2.46 | 2.46 | 0.05 |
| *** |  |  |  |  |  |  |  |  |  |
| Platform Mount [LP 701-1] | C | None |  | 0.0000 | 172.00 | No Ice | 59.15 | 59.15 | 2.75 |
|  |  |  |  |  |  | 1/2" | 71.12 | 71.12 | 3.42 |
|  |  |  |  |  |  | Ice | 83.09 | 83.09 | 4.10 |
|  |  |  |  |  |  | 1 Ice | 107.03 | 107.03 | 5.45 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| $4^{\prime} \times 2$ " Mount Pipe | A | From Face | 4.00 | 0.0000 | 172.00 | No lce | 0.87 | 0.87 | 0.01 |
|  |  |  | 3.50 |  |  | 1/2" | 1.11 | 1.11 | 0.02 |
|  |  |  | 0.00 |  |  | Ice | 1.36 | 1.36 | 0.03 |



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| :--- | ---: |
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December 13, 2018
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\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& $$
\begin{aligned}
& \text { Face } \\
& \text { or } \\
& \text { Leg }
\end{aligned}
$$ \& Offset Type \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen $t$ \& Placement

ft \& \& | $C_{\lambda} A_{A}$ Front |
| :--- |
| $f t^{2}$ | \& $C_{A} A_{A}$ side $4 t^{2}$ \& Weight

K <br>

\hline \multirow{5}{*}{TD-RRH8×20-25} \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Face} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{162.00} \& $$
\begin{aligned}
& \hline \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 5.10 \& 2.30 \& 0.20 <br>

\hline \& \& \& 3.00 \& \& \& No lce \& 4.05 \& 1.53 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 4.30 \& 1.71 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 4.56 \& 1.90 \& 0.13 <br>

\hline \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Face} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{162.00} \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 5.10 \& 2.30 \& 0.20 <br>

\hline \multirow[t]{5}{*}{800MHz 2X50W RRH WIFILTER} \& \& \& 0.50 \& \& \& No Ice \& 2.06 \& 1.93 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.24 \& 2.11 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.43 \& 2.29 \& 0.11 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{162.00} \& $1^{\prime \prime}$ Ice \& 2.83 \& 2.68 \& 0.17 <br>
\hline \& \& \& \& \& \& 2" lce \& \& \& <br>
\hline \multirow[t]{5}{*}{$800 \mathrm{MHz} 2 \times 50 \mathrm{~W}$ RRH WIFILTER} \& \& \& 0.50 \& \& \& No lce \& 2.06 \& 1.93 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.24 \& 2.11 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.43 \& 2.29 \& 0.11 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{162.00} \& 1" Ice \& 2.83 \& 2.68 \& 0.17 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>

\hline \multirow[t]{5}{*}{$$
800 \mathrm{MHz} 2 \times 50 \mathrm{~W} \text { RRH }
$$ W/FILTER} \& \& \& 0.50 \& \& \& Nolce \& 2.06 \& 1.93 \& 0.06 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.24 \& 2.11 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.43 \& 2.29 \& 0.11 <br>
\hline \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{162.00} \& 1" Ice \& 2.83 \& 2.68 \& 0.17 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{PCS 1900MHz 2x40W} \& \& \& 0.50 \& \& \& No Ice \& 2.35 \& 1.28 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.55 \& 1.43 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.75 \& 1.60 \& 0.08 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{162.00} \& 1 " lce \& 3.18 \& 1.95 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{PCS $1900 \mathrm{MHz} 2 \times 40 \mathrm{~W}$} \& \& \& 0.50 \& \& \& No lce \& 2.35 \& 1.28 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& 1/2' \& 2.55 \& 1.43 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.75 \& 1.60 \& 0.08 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{162.00} \& 1" Ice \& 3.18 \& 1.95 \& 0.14 <br>
\hline \& \& \& \& \& \& 2 Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{PCS 1900MHz 2x40W} \& \& \& 0.50 \& \& \& Nolce \& 2.35 \& 1.28 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.55 \& 1.43 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.75 \& 1.60 \& 0.08 <br>

\hline \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Face} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{162.00} \& | 1" Ice |
| :--- |
| 2" Ice | \& 3.18 \& 1.95 \& . 0.14 <br>

\hline \multirow[t]{4}{*}{6'x2" Mount Pipe} \& \& \& 3.00 \& \& \& No Ice \& 1.43 \& 1.43 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.92 \& 1.92 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.29 \& 2.29 \& 0.05 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{162.00} \& 1" Ice \& 3.06 \& 3.06 \& 0.09 <br>
\hline \multirow{4}{*}{6'x2" Mount Pipe} \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& \& \& \& No Ice \& \& 1.43 \& <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.92 \& 1.92 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.29 \& 2.29 \& 0.05 <br>
\hline \multirow{5}{*}{6'x2' Mount Pipe} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{162.00} \& 1" lce \& 3.06 \& 3.06 \& 0.09 <br>
\hline \& \& \& \& \& \& 2" lce \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No lce \& 1.43 \& 1.43 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2' \& 1.92 \& 1.92 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.29 \& 2.29 \& 0.05 <br>
\hline \multirow{5}{*}{4'x2' Mount Pipe} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{162.00} \& 1" Ice \& 3.06 \& 3.06 \& 0.09 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 0.50 \& \& \& No lce \& 0.87 \& 0.87 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.11 \& 1.11 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.36 \& 1.36 \& 0.03 <br>
\hline \multirow{5}{*}{4'x2' Mount Pipe} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{162.00} \& $1{ }^{\prime \prime}$ Ice \& 1.90 \& 1.90 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 0.50 \& \& \& No lce \& 0.87 \& 0.87 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.11 \& 1.11 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.36 \& 1.36 \& 0.03 <br>
\hline \multirow{6}{*}{4'x2" Mount Pipe} \& \multirow{6}{*}{C} \& \multirow{6}{*}{From Face} \& \& \multirow{6}{*}{0.0000} \& \multirow{6}{*}{162.00} \& $1{ }^{1 \prime}$ Ice \& 1.90 \& 1.90 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 0.50 \& \& \& No Ice \& 0.87 \& 0.87 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.11 \& 1.11 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.36 \& 1.36 \& 0.03 <br>
\hline \& \& \& \& \& \& 1 Ice \& 1.90 \& 1.90 \& 0.06 <br>
\hline
\end{tabular}

| 175 Ft Monopole Tower Structural Analysis Project Number 400087, Order 471611, Revision 0 |  |  |  |  |  |  |  | December 13. 2 CCI BU No 823 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Description | $\begin{gathered} \hline \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> ft <br> ft <br> ft | Azimuth Adjustmen $t$ | Placement |  | $C_{A} A_{A}$ Front <br> $f t^{2}$ | $C_{4} A_{A}$ <br> Side <br> $t^{2}$ | Weight K |
| ** 2" lce |  |  |  |  |  |  |  |  |  |
| Sector Mount [SM 801-3] | C | None |  | 0.0000 | 152.00 | No lce | 20.40 | 20.40 | 0.88 |
|  |  |  |  |  |  | $1 / 2$ " | 26.30 | 26.30 | 1.25 |
|  |  |  |  |  |  | Ice | 32.20 | 32.20 | 1.63 |
|  |  |  |  |  |  | $\begin{aligned} & \text { 1" Ice } \\ & \text { 2" Ice } \end{aligned}$ | 44.00 | 44.00 | 2.39 |
| NNHH-65B-R4 w/ Mount Pipe | A | From Leg | 3.00 | 0.0000 | 152.00 | No lce | 12.51 | 7.41 | 0.10 |
|  |  |  | -6.00 |  |  | 1/2" | 13.11 | 8.60 | 0.19 |
|  |  |  | 0.00 |  |  | Ice | 13.67 | 9.50 | 0.29 |
|  |  |  |  |  |  | 1" Ice | 14.82 | 11.33 | 0.52 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| NNHH-65B-R4 w/ Mount Pipe | A | From Leg | $3.00$ | 0.0000 | 152.00 | No lce | 12.51 | 7.41 | 0.10 |
|  |  |  | $-2.00$ |  |  | $1 / 2^{\prime \prime}$ | 13.11 | 8.60 | $0.19$ |
|  |  |  | 0.00 |  |  | Ice | 13.67 | 9.50 | 0.29 |
|  |  |  |  |  |  | 1" Ice | 14.82 | 11.33 | 0.52 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| LPA-80080/4CF w/ Mount Pipe | A | From Leg | 3.00 | 0.0000 | 152.00 | No Ice | 2.86 | 6.57 | 0.03 |
|  |  |  | 2.00 |  |  | 1/2" | 3.22 | 7.19 | 0.08 |
|  |  |  | 0.00 |  |  | Ice | 3.59 | 7.84 | 0.13 |
|  |  |  |  |  |  | 1" Ice | 4.34 | 9.17 | 0.25 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| LPA-80080/4CF w/ Mount Pipe | A | From Leg | 3.00 | 0.0000 | 152.00 | No Ice | 2.86 | 6.57 | 0.03 |
|  |  |  | 6.00 |  |  | 1/2" | 3.22 | 7.19 | 0.08 |
|  |  |  | 0.00 |  |  | Ice | 3.59 | 7.84 | 0.13 |
|  |  |  |  |  |  | 1" Ice | 4.34 | 9.17 | 0.25 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| NNHH-65B-R4 w/ Mount Pipe | B | From Leg | 3.00 | 0.0000 | 152.00 | No Ice | 12.51 | 7.41 | 0.10 |
|  |  |  | -6.00 |  |  | 1/2" | 13.11 | 8.60 | 0.19 |
|  |  |  | 0.00 |  |  | Ice | 13.67 | 9.50 | 0.29 |
|  |  |  |  |  |  | 1" Ice | 14.82 | 11.33 | 0.52 |
|  |  |  |  |  |  | 2"Ice |  |  |  |
| NNHH-65B-R4 w/ Mount Pipe | B | From Leg |  | 0.0000 | 152.00 | No lce | 12.51 | 7.41 | 0.10 |
|  |  |  | $-2.00$ |  |  | $1 / 2^{\prime \prime}$ | 13.11 | 8.60 | 0.19 |
|  |  |  | 0.00 |  |  | Ice | 13.67 | 9.50 | 0.29 |
|  |  |  |  |  |  | 1" Ice | 14.82 | 11.33 | 0.52 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| LPA-80080/4CF w/ Mount Pipe. | B | From Leg | 3.00 | 0.0000 | 152.00 | No Ice | 2.86 | 6.57 | 0.03 |
|  |  |  | 2.00 |  |  | 1/2" | 3.22 | 7.19 | 0.08 |
|  |  |  | 0.00 |  |  | Ice | 3.59 | 7.84 | 0.13 |
|  |  |  |  |  |  | 1" Ice | 4.34 | 9.17 | 0.25 |
|  |  |  |  |  |  | $2^{\prime \prime} \text { lce }$ |  |  |  |
| LPA-80080/4CF w/ Mount Pipe | B | From Leg | 3.00 | 0.0000 | 152.00 | No lce | 2.86 | 6.57 | 0.03 |
|  |  |  | 6.00 |  |  | 1/2" | 3.22 | 7.19 | 0.08 |
|  |  |  | 0.00 |  |  | Ice | 3.59 | 7.84 | 0.13 |
|  |  |  |  |  |  | 1" Ice | 4.34 | 9.17 | 0.25 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| LPA-80080/4CF w/ Mount Pipe | C | From Leg | 3.00 | 0.0000 | 152.00 | No lce | 2.86 | 6.57 | 0.03 |
|  |  |  | -6.00 |  |  | 1/2" | 3.22 | 7.19 | 0.08 |
|  |  |  | 0.00 |  |  | Ice | 3.59 | 7.84 | 0.13 |
|  |  |  |  |  |  | 1" Ice | 4.34 | 9.17 | 0.25 |
|  |  |  |  |  |  | 2"Ice |  |  |  |
| LPA-80080/4CF w/ Mount Pipe | c | From Leg |  | 0.0000 | 152.00 |  | 2.86 | 6.57 | 0.03 |
|  |  |  | -2.00 |  |  | $1 / 2^{\prime \prime}$ | 3.22 | 7.19 | 0.08 |
|  |  |  | 0.00 |  |  | Ice | 3.59 | 7.84 | 0.13 |
|  |  |  |  |  |  | 1" Ice | 4.34 | 9.17 | 0.25 |
|  |  |  |  |  |  | 2 'lce |  |  |  |
| NNHH-65B-R4 w/ Mount Pipe | C | From Leg |  | 0.0000 | 152.00 |  | 12.51 | 7.41 | $0.10$ |
|  |  |  | 2.00 |  |  | 1/2' | 13.11 | 8.60 | 0.19 |
|  |  |  | 0.00 |  |  | Ice | 13.67 | 9.50 | 0.29 |
|  |  |  |  |  |  | 1" Ice | 14.82 | 11.33 | 0.52 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| NNHH-65B-R4 w/ Mount Pipe | c | From Leg | 3.00 | 0.0000 | 152.00 | No lce | 12.51 | 7.41 | 0.10 |
|  |  |  | 6.00 |  |  | 1/2" | 13.11 | 8.60 | 0.19 |
|  |  |  | 0.00 |  |  | Ice | 13.67 | 9.50 | 0.29 |
|  |  |  |  |  |  | 1 ' Ice | 14.82 | 11.33 | 0.52 |

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\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& $$
\begin{aligned}
& \text { Face } \\
& \text { or } \\
& \text { Leg }
\end{aligned}
$$ \& Offset Type \& Offsets:
Horz
Lateral
Vert
ft
ft
tt \& Azimuth Adjustmen $t$ \& Placement \& \& $\mathrm{C}_{4} A_{A}$ Front
$$
f t^{2}
$$ \& $C_{A} A_{A}$ Side
$$
f t^{2}
$$ \& Weight

K <br>
\hline \multirow{5}{*}{6'x2" Mount Pipe} \& \multirow{4}{*}{B} \& \multirow{4}{*}{From Face} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{142.00} \& \multirow[t]{2}{*}{$2 "$ Ice
No lce} \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& \& 1.43 \& 1.43 \& 0.02 <br>
\hline \& \& \& 4.00 \& \& \& 1/2" \& 1.92 \& 1.92 \& 0.03 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 2.29 \& 2.29 \& 0.05 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{142.00} \& 1 ' Ice \& 3.06 \& 3.06 \& 0.09 <br>
\hline \multirow{4}{*}{6'x2' Mount Pipe} \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No lce \& 1.43 \& 1.43 \& 0.02 <br>
\hline \& \& \& 4.00 \& \& \& 1/2" \& 1.92 \& 1.92 \& 0.03 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 2.29 \& 2.29 \& 0.05 <br>
\hline \multirow{5}{*}{5'x2" Mount Pipe} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{142.00} \& 1" Ice \& 3.06 \& 3.06 \& 0.09 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 1.19 \& 1.19 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ \& 1.50 \& 1.50 \& 0.03 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 1.81 \& 1.81 \& 0.04 <br>
\hline \multirow{5}{*}{5'x2" Mount Pipe} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{142.00} \& $1^{\prime \prime}$ Ice \& 2.46 \& 2.46 \& 0.08 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 1.19 \& 1.19 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.50 \& 1.50 \& 0.03 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 1.81 \& 1.81 \& 0.04 <br>
\hline \multirow{6}{*}{5'x2" Mount Pipe} \& \multirow{6}{*}{C} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{142.00} \& 1 'Ice \& 2.46 \& 2.46 \& 0.08 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 1.19 \& 1.19 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.50 \& 1.50 \& 0.03 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 1.81 \& 1.81 \& 0.04 <br>
\hline \& \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \multirow{6}{*}{142.00} \& $1{ }^{\prime \prime}$ Ice \& 2.46 \& 2.46 \& 0.08 <br>
\hline \& \multirow{5}{*}{A} \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{7770.00 w/ Mount Pipe} \& \& \& 3.00 \& \& \& No Ice \& 5.75 \& 4.25 \& 0.06 <br>
\hline \& \& \& -6.00 \& \& \& 1/2' \& 6.18 \& 5.01 \& 0.10 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 6.61 \& 5.71 \& 0.16 <br>
\hline \& \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \& 1" Ice \& 7.49 \& 7.16 \& 0.29 <br>
\hline \& \multirow{4}{*}{B} \& \& \& \& \multirow{5}{*}{142.00} \& 2" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{7770.00 w/ Mount Pipe} \& \& \& \& \& \& No lce \& 5.75 \& 4.25 \& 0.06 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" \& 6.18 \& 5.01 \& 0.10 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 6.61 \& 5.71 \& 0.16 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Face} \& \& \multirow{5}{*}{0.0000} \& \& 1" Ice \& 7.49 \& 7.16 \& 0.29 <br>
\hline \multirow{5}{*}{7770.00 w/ Mount Pipe} \& \& \& \& \& \multirow{4}{*}{142.00} \& 2" Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No lce \& 5.75 \& 4.25 \& 0.06 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" \& 6.18 \& 5.01 \& 0.10 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 6.61 \& 5.71 \& 0.16 <br>
\hline \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{142.00} \& $1^{\prime \prime}$ Ice \& 7.49 \& 7.16 \& 0.29 <br>
\hline \multirow{5}{*}{HPA65R-BU6A w/ Mount Pipe} \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No lce \& 8.09 \& 7.19 \& 0.07 <br>
\hline \& \& \& -2.00 \& \& \& 1/2" \& 8.64 \& 8.36 \& 0.14 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 9.16 \& 9.24 \& 0.21 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{6}{*}{142.00} \& 1" lce \& 10.22 \& 11.05 \& 0.39 <br>
\hline \multirow{4}{*}{HPA65R-BU4A w/ Mount Pipe} \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No lce \& 5.20 \& 4.66 \& 0.05 <br>
\hline \& \& \& -2.00 \& \& \& 1/2" \& 5.58 \& 5.27 \& 0.10 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 5.97 \& 5.89 \& 0.15 <br>
\hline \multirow{5}{*}{HPA65R-BU6A w/ Mount Pipe} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \& 1 'Ice \& 6.79 \& 7.18 \& 0.28 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& \& \& \multirow[t]{4}{*}{142.00} \& No lce \& 8.09 \& 7.19 \& <br>
\hline \& \& \& -2.00 \& \& \& 1/2" \& 8.64 \& 8.36 \& 0.14 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 9.16 \& 9.24 \& 0.21 <br>
\hline \multirow{5}{*}{80010965 w/ Mount Pipe} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \& $1{ }^{\prime \prime}$ Ice \& 10.22 \& 11.05 \& 0.39 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \multirow[t]{3}{*}{142.00} \& No lce \& 14.05 \& 7.63 \& 0.13 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" \& 14.69 \& 8.90 \& 0.22 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 15.30 \& 9.96 \& 0.33 <br>
\hline \multirow{7}{*}{80010964 w/ Mount Pipe} \& \multirow{7}{*}{B} \& \multirow{7}{*}{From Leg} \& \& \multirow{7}{*}{0.0000} \& \multirow{7}{*}{142.00} \& 1 Ice \& 16.53 \& 11.92 \& 0.57 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 10.23 \& 5.51 \& 0.11 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" \& 10.74 \& 6.37 \& 0.18 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 11.24 \& 7.12 \& 0.26 <br>
\hline \& \& \& \& \& \& 1" Ice \& 12.25 \& 8.64 \& 0.45 <br>
\hline \& \& \& \& \& \& 2" lce \& \& \& <br>
\hline
\end{tabular}

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\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& Offsets: Horz Lateral Vert ft ft \(f t\) \& Azimuth Adjustmen \(t\) \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) Front \\
\(4 t^{2}\)
\end{tabular} \& \(C_{4} A_{A}\) Side
\[
f t^{2}
\] \& Weight

$K$ <br>
\hline \multirow[t]{4}{*}{80010965 w/ Mount Pipe} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{142.00} \& No Ice \& 14.05 \& 7.63 \& 0.13 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" \& 14.69 \& 8.90 \& 0.22 <br>
\hline \& \& \& \multirow[t]{2}{*}{1.00} \& \& \& Ice \& 15.30 \& 9.96 \& 0.33 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& 1^{\prime \prime} \text { Ice } \\
& 2^{\prime \prime} \text { Ice }
\end{aligned}
$$ \& 16.53 \& 11.92 \& 0.57 <br>

\hline \multirow[t]{5}{*}{80010965 w/ Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No lce \& 14.05 \& 7.63 \& 0.13 <br>
\hline \& \& \& 6.00 \& \& \& 1/2" \& 14.69 \& 8.90 \& 0.22 <br>
\hline \& \& \& \multirow[t]{3}{*}{1.00} \& \& \& Ice \& 15.30 \& 9.96 \& 0.33 <br>
\hline \& \& \& \& \& \& 1 ' Ice \& 16.53 \& 11.92 \& 0.57 <br>
\hline \& \& \& \& \& \& 2" lce \& \& \& <br>
\hline \multirow[t]{5}{*}{80010964 w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No lce \& 10.23 \& 5.51 \& 0.11 <br>
\hline \& \& \& 6.00 \& \& \& 1/2" \& 10.74 \& 6.37 \& 0.18 <br>
\hline \& \& \& \multirow[t]{3}{*}{1.00} \& \& \& Ice \& 11.24 \& 7.12 \& 0.26 <br>
\hline \& \& \& \& \& \& 1 Ice \& 12.25 \& 8.64 \& 0.45 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{80010965 w/ Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No Ice \& 14.05 \& 7.63 \& 0.13 <br>
\hline \& \& \& 6.00 \& \& \& 1/2" \& 14.69 \& 8.90 \& 0.22 <br>
\hline \& \& \& \multirow[t]{3}{*}{1.00} \& \& \& Ice \& 15.30 \& 9.96 \& 0.33 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 16.53 \& 11.92 \& 0.57 <br>
\hline \& \& \& \& \& \& 2 ' Ice \& \& \& <br>

\hline \multirow[t]{5}{*}{RADIO 4415 B30} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& $$
3.00
$$ \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No lce \& 1.64 \& 0.64 \& 0.04 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.80 \& 0.75 \& 0.05 <br>
\hline \& \& \& \multirow[t]{3}{*}{1.00} \& \& \& Ice \& 1.97 \& 0.87 \& 0.07 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.33 \& 1.13 \& 0.11 <br>

\hline \& \& \& \& \& \& $$
2^{\prime \prime} \text { Ice }
$$ \& \& \& <br>

\hline \multirow[t]{5}{*}{RADIO 4415 B30} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No Ice \& 1.64 \& 0.64 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& 1/2' \& 1.80 \& 0.75 \& 0.05 <br>
\hline \& \& \& \multirow[t]{3}{*}{1.00} \& \& \& Ice \& 1.97 \& 0.87 \& 0.07 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.33 \& 1.13 \& 0.11 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{RADIO 4415 B30} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No lce \& 1.64 \& 0.64 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.80 \& 0.75 \& 0.05 <br>
\hline \& \& \& \multirow[t]{3}{*}{1.00} \& \& \& Ice \& 1.97 \& 0.87 \& 0.07 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 2.33 \& 1.13 \& 0.11 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{RRUS 4449 B5/B12} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No Ice \& 1.97 \& 1.41 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.14 \& 1.56 \& 0.09 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 2.33 \& 1.73 \& 0.11 <br>
\hline \& \& \& \& \& \& $1{ }^{1 \prime}$ Ice \& 2.72 \& 2.07 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{RRUS 4449 B5/B12} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No lce \& 1.97 \& 1.41 \& <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.14 \& 1.56 \& 0.09 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 2.33 \& 1.73 \& 0.11 <br>
\hline \& \& \& \& \& \& 1" lce \& 2.72 \& 2.07 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" lce \& \& \& <br>
\hline \multirow[t]{5}{*}{RRUS $4449 \mathrm{~B} 5 / \mathrm{B} 12$} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No Ice \& 1.97 \& 1.41 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.14 \& 1.56 \& 0.09 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 2.33 \& 1.73 \& 0.11 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.72 \& 2.07 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{RRUS 4478 B14} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No Ice \& 1.84 \& 1.06 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.01 \& 1.20 \& 0.08 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 2.19 \& 1.34 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.57 \& 1.66 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{RRUS 4478 B14} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No lce \& 1.84 \& 1.06 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.01 \& 1.20 \& 0.08 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 2.19 \& 1.34 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.57 \& 1.66 \& 0.14 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{RRUS 4478 B14} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{142.00} \& No Ice \& 1.84 \& 1.06 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.01 \& 1.20 \& 0.08 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 2.19 \& 1.34 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.57 \& 1.66 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline RRUS 8843 B2/B66A \& A \& From Leg \& 3.00 \& 0.0000 \& 142.00 \& No lce \& 1.64 \& 1.35 \& 0.07 <br>
\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face. } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral Vert ft ft
\end{tabular} \& \[
\begin{gathered}
\text { Azimuth } \\
\text { Adjustmen } \\
t
\end{gathered}
\] \& Placement

ft \& \& | $C_{A} A_{4}$ Front |
| :--- |
| $t^{2}$ | \& \[

$$
\begin{aligned}
& C_{4} A_{A} \\
& \text { Side } \\
& \pi^{2}
\end{aligned}
$$
\] \& Weight

K <br>
\hline \multirow{7}{*}{RRUS 8843 B2/B66A} \& \multirow{7}{*}{B} \& \multirow{6}{*}{From Leg} \& 0.00 \& \& \& 1/2" \& 1.80 \& 1.50 \& 0.09 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 1.97 \& 1.65 \& 0.11 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 2.32 \& 1.99 \& 0.16 <br>

\hline \& \& \& 3.00 \& 0.0000 \& 142.00 \& No lce \& 1.64 \& 1.35 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ \& 1.80 \& 1.50 \& 0.09 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 1.97 \& 1.65 \& 0.11 <br>
\hline \& \& \multirow{5}{*}{From Leg} \& \& \& \& 1" Ice \& 2.32 \& 1.99 \& 0.16 <br>
\hline \multirow{5}{*}{RRUS 8843 B2/B66A} \& \multirow{5}{*}{c} \& \& \& \& \& $2{ }^{\text {" lce }}$ \& \& \& <br>
\hline \& \& \& 3.00 \& 0.0000 \& 142.00 \& No lce \& 1.64 \& 1.35 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.80 \& 1.50 \& 0.09 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 1.97 \& 1.65 \& 0.11 <br>
\hline \& \& \multirow{5}{*}{From Face} \& \& \& \& 1 1" Ice \& 2.32 \& 1.99 \& 0.16 <br>
\hline \multirow[t]{5}{*}{(2) LGP21401} \& \multirow[t]{4}{*}{A} \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 3.00 \& 0.0000 \& 142.00 \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 1.00 \& \& \& ice \& 1.38 \& 0.54 \& 0.03 <br>

\hline \& \multirow{4}{*}{B} \& \multirow{4}{*}{From Face} \& \& \& \& $$
\begin{aligned}
& \text { 1"Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 1.69 \& 0.77 \& 0.05 <br>

\hline \multirow[t]{4}{*}{(2) LGP21401} \& \& \& 3.00 \& 0.0000 \& 142.00 \& No Ice \& \& 0.35 \& 0.01 <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime}
$$ \& 1.24 \& 0.44 \& 0.02 <br>

\hline \& \& \& 1.00 \& \& \& lee \& 1.38 \& 0.54 \& 0.03 <br>
\hline \& \multirow{6}{*}{C} \& \multirow{5}{*}{From Face} \& \& \& \& 1" Ice \& 1.69 \& 0.77 \& 0.05 <br>
\hline \multirow{5}{*}{(2) LGP21401} \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 3.00 \& 0.0000 \& 142.00 \& No lce \& 1.10 \& 0.35 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 1.38 \& 0.54 \& 0.03 <br>
\hline \& \& \multirow{5}{*}{From Leg} \& \& \& \& 1" Ice \& 1.69 \& 0.77 \& 0.05 <br>
\hline \multirow{5}{*}{DC6-48-60-18-8F} \& \multirow{5}{*}{A} \& \& \& \& \& 2"Ice \& \& \& <br>
\hline \& \& \& 1.00 \& 0.0000 \& 142.00 \& No Ice \& 0.92 \& 0.92 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.46 \& 1.46 \& 0.04 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 1.64 \& 1.64 \& 0.06 <br>
\hline \& \& \multirow{6}{*}{From Leg} \& \& \& \& 1" Ice \& 2.04 \& 2.04 \& 0.11 <br>
\hline \multirow{5}{*}{DC6-48-60-18-8F} \& \multirow{5}{*}{B} \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 1.00 \& 0.0000 \& 142.00 \& No Ice \& 0.92 \& 0.92 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.46 \& 1.46 \& 0.04 <br>
\hline \& \& \& \& \& \& Ice \& 1.64 \& 1.64 \& 0.06 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.04 \& 2.04 \& 0.11 <br>
\hline \multirow{6}{*}{DC6-48-60-18-8F} \& \multirow{6}{*}{c} \& \multirow{6}{*}{From Face} \& \& \& \& 2 " Ice \& \& \& <br>
\hline \& \& \& 1.00 \& 0.0000 \& 142.00 \& No lce \& 0.92 \& 0.92 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.46 \& 1.46 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.64 \& 1.64 \& 0.06 <br>
\hline \& \& \& \& \& \& 1 1'Ice \& 2.04 \& 2.04 , \& 0.11 <br>
\hline \& \& \& \& \& \& 2"Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{APXV18-206517S-C wl Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& \& \& \& \& \& \& <br>

\hline \& \& \& $$
\begin{aligned}
& 1.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 115.00 \& \[

$$
\begin{aligned}
& \text { No lce } \\
& 1 /)^{\prime \prime}
\end{aligned}
$$
\] \& 5.40

5.96 \& 4.70
5.86 \& 0.05
0.10 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 6.48 \& 6.73 \& 0.15 <br>
\hline \& \& \& \& \& \& 1" Ice \& 7.55 \& 8.51 \& 0.28 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{APXV18-206517S-C w $/$
Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Face} \& 1.00 \& 0.0000 \& 115.00 \& No Ice \& 5.40 \& 4.70 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 5.96 \& 5.86 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 6.48 \& 6.73 \& 0.15 <br>
\hline \& \& \& \& \& \& 1" Ice \& 7.55 \& 8.51 \& 0.28 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{APXV18-206517S-C w $/$
Mount Pipe} \& \multirow[t]{5}{*}{c} \& \multirow[t]{5}{*}{From Face} \& 1.00 \& 0.0000 \& 115.00 \& No Ice \& 5.40 \& 4.70 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 5.96 \& 5.86 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& lce \& 6.48 \& 6.73 \& 0.15 <br>
\hline \& \& \& \& \& \& 1" Ice \& 7.55 \& 8.51 \& 0.28 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{Side Arm Mount [SO 7011]} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 0.50 \& 0.0000 \& 50.00 \& Nolce \& 0.85 \& 1.67 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.14 \& 2.34 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.43 \& 3.01 \& 0.09 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 2.01 \& 4.35 \& 0.12 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline
\end{tabular}

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> ft <br> ft <br> ft | Azimuth Adjustmen $t$ | Placement <br> $f t$ |  | $C_{\lambda} A_{\mu}$ Front $\pi^{2}$ | $C_{A} A_{A}$ Side $f t^{2}$ | Weight <br> K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GPS-TMG-HR-26NCM | A | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 50.00 | $\begin{gathered} \hline \text { No Ice } \\ 1 / 2^{\prime \prime} \\ \text { lce } \\ 1^{\prime \prime} \text { Ice } \\ 2^{\prime \prime} \text { Ice } \end{gathered}$ | $\begin{aligned} & 0.13 \\ & 0.18 \\ & 0.24 \\ & 0.37 \end{aligned}$ | $\begin{aligned} & \hline 0.13 \\ & 0.18 \\ & 0.24 \\ & 0.37 \end{aligned}$ | $\begin{aligned} & 0.00 \\ & 0.00 \\ & 0.01 \\ & 0.01 \end{aligned}$ |



## Load Combinations

| Comb. No. | Description |
| :---: | :---: |
| 1 | Dead Only |
| 2 | 1.2 Dead +1.0 Wind 0 deg - No Ice |
| 3 | 0.9 Dead+1.0 Wind 0 deg - No Ice |
| 4 | 1.2 Dead+1.0 Wind 30 deg - No lce |
| 5 | 0.9 Dead+1.0 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.0 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.0 Wind 60 deg - No lce |
| 8 | 1.2 Dead+1.0 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.0 Wind 90 deg - No lce |
| 10 | 1.2 Dead +1.0 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.0 Wind 120 deg - No lce |
| 12 | 1.2 Dead+1.0 Wind 150 deg - No lce |
| 13 | 0.9 Dead+1.0 Wind 150 deg - No Ice |
| 14 | 1.2 Dead +1.0 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.0 Wind 180 deg - No Ice |
| 16 | 1.2 Dead +1.0 Wind 210 deg - No Ice |
| 17 | 0.9 Dead+1.0 Wind 210 deg - No Ice |
| 18 | 1.2 Dead +1.0 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.0 Wind 240 deg - No Ice |
| 20 | 1.2 Dead +1.0 Wind 270 deg - No lce |
| 21 | 0.9 Dead+1.0 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.0 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.0 Wind 300 deg - No Ice |
| 24 | 1.2 Dead+1.0 Wind 330 deg - No lce |
| 25 | 0.9 Dead+1.0 Wind 330 deg - No Ice |
| 26 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 27 | 1.2 Dead+1.0 Wind 0 deg +1.0 Ice +1.0 Temp |
| 28 | 1.2 Dead +1.0 Wind 30 deg +1.0 Ice +1.0 Temp |
| 29 | 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp |

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| Comb. No. | Description |
| :---: | :---: |
| 30 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind $120 \mathrm{deg}+1.0 \mathrm{lce}+1.0$ Temp |
| 32 | 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp |
| 33 | 1.2 Dead+1.0 Wind $180 \mathrm{deg}+1.0 \mathrm{Ice}+1.0$ Temp |
| 34 | 1.2 Dead +1.0 Wind $210 \mathrm{deg}+1.0$ lce +1.0 Temp |
| 35. | 1.2 Dead+1.0 Wind $240 \mathrm{deg}+1.0 \mathrm{Ice}+1.0$ Temp |
| 36 | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp |
| 37 | 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp |
| 38 | 1.2 Dead+1.0 Wind $330 \mathrm{deg}+1.0 \mathrm{lce}+1.0$ Temp |
| 39 | Dead+Wind 0 deg - Service |
| 40 | Dead+Wind 30 deg - Service |
| 41 | Dead+Wind 60 deg - Service |
| 42 | Dead+Wind 90 deg - Service |
| 43 | Dead+Wind 120 deg - Service |
| 44 | Dead + Wind 150 deg - Service |
| 45 | Dead+Wind 180 deg - Service |
| 46 | Dead+Wind 210 deg - Service |
| 47 | Dead+Wind 240 deg - Service |
| 48 | Dead+Wind 270 deg - Service |
| 49 | Dead+Wind 300 deg - Service |
| 50 | Dead+Wind 330 deg - Service |

Maximum Member Forces

| $\begin{gathered} \text { Sectio } \\ n \\ \text { No. } \\ \hline \end{gathered}$ | Elevation ft | Component Type | Condition | Gov. Load Comb | Axial $K$ | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 175-164.25 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -9.02 | -1.14 | -4.63 |
|  |  |  | Max. Mx | 8 | -4.16 | -29.56 | -1.85 |
|  |  |  | Max. My | 14 | -4.19 | -1.21 | -28.14 |
|  |  |  | Max. Vy | 8 | 5.94 | -29.56 | -1.85 |
|  |  |  | Max. Vx | 14 | 5.64 | -1.21 | -28.14 |
|  |  |  | Max. Torque | 7 |  |  | -5.10 |
| L2 | $\begin{gathered} 164.25- \\ 129.67 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -38.88 | 1.04 | -0.68 |
|  |  |  | Max. Mx | 8 | -17.95 | -496.92 | -6.97 |
|  |  |  | Max. My | 2 | -18.00 | 9.78 | 485.21 |
|  |  |  | Max. Vy | 8 | 21.44 | -496.92 | -6.97 |
|  |  |  | Max. Vx | 14 | 21.17 | -7.80 | -484.67 |
|  |  |  | Max. Torque | 7 |  |  | -4.78 |
| L. 3 | 129.67-96 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -50.13 | 1.51 | -0.73 |
|  |  |  | Max. Mx | 8 | -26.07 | -1254.55 | -12.11 |
|  |  |  | Max. My | 2 | -26.11 | 16.41 | 1233.65 |
|  |  |  | Max. Vy | 8 | 24.76 | -1254.55 | -12.11 |
|  |  |  | Max. Vx | 14 | 24.49 | -13.79 | -1233.49 |
|  |  |  | Max. Torque | 16 |  |  | -1.16 |
| 14 | 96-63.17 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -62.66 | 2.09 | -1.07 |
|  |  |  | Max. Mx | 8 | -35.67 | -2092.13 | -17.27 |
|  |  |  | Max. My | 14 | -35.70 | -19.55 | -2062.74 |
|  |  |  | Max. Vy | 8 | 27.52 | -2092.13 | -17.27 |
|  |  |  | Max. Vx | 14 | 27.25 | -19.55 | -2062.74 |
|  |  |  | Max. Torque | 16 |  |  | -1.16 |
| L5 | $\begin{gathered} 63.17- \\ 31.17 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -76.87 | 2.99 | -1.44 |
|  |  |  | Max. Mx | 8 | -46.67 | -2992.41 | -22.07 |
|  |  |  | Max. My | 14 | -46.68 | -24.74 | -2955.33 |
|  |  |  | Max. Vy | 8 | 30.00 | -2992.41 | -22.07 |
|  |  |  | Max. Vx | 14 | 29.75 | -24.74 | -2955.33 |
|  |  |  | Max. Torque | 16 |  |  | $-1.30$ |
| L6 | 31.17-0 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -94.81 | 3.56 | -2.09 |
|  |  |  | Max. Mx | 8 | -60.95 | -4162.50 | -27.47 |
|  |  |  | Max. My | 14 | -60.95 | -30.76 | -4116.65 |

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175 Ft Monopole Tower Structural Analysis

| Sectio <br> $n$ No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Axial <br> K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Max. Vy | 8 | 32.47 | -4162.50 | -27.47 |
|  |  |  | Max. Vx | 14 | 32.23 | -30.76 | -4116.65 |
|  |  |  | Max. Torque | 16 |  |  | -1.30 |

## Maximum Reactions

| Location | Condition | Gov. Load Comb. | Vertical K | $\underset{K}{\text { Horizontal, } X}$ | Horizontal, Z K |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pole | Max. Vert | 36 | 94.81 | 8.93 | 0.00 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 20 | 60.96 | 32.30 | 0.11 |
|  | Max. $\mathrm{Hz}^{\text {I }}$ | 2 | 60.96 | 0.17 | 32.20 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 2 | 4114.57 | 0.17 | 32.20 |
|  | Max. $\mathrm{M}_{\mathrm{z}}$ | 8 | 4162.50 | -32.45 | -0.13 |
|  | Max. Torsion | 6 | 1.08 | -28.12 | 15.91 |
|  | Min. Vert | 5 | 45.72 | -16.20 | 27.79 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 9 | 45.72 | -32.45 | -0.13 |
|  | Min. $\mathrm{Hz}_{\mathrm{z}}$ | 15 | 45.72 | -0.16 | -32.20 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 14 | -4116.65 | -0.16 | -32.20 |
|  | Min. $\mathrm{M}_{\mathbf{z}}$ | 20 | -4139.71 | 32.30 | 0.11 |
|  | Min. Torsion | 16 | -1.30 | 16.17 | -27.79 |

Tower Mast Reaction Summary

| Load Combination | Vertical <br> K | Shear ${ }_{x}$ <br> K | Shear $_{z}$ $K$ | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ff | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 50.80 | 0.00 | 0.00 | 0.54 | 1.26 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg - | 60.96 | -0.17 | -32.20 | -4114.57 | 35.82 | -1.06 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 0 deg - | 45.72 | -0.17 | -32.20 | -4063.05 | 34.87 | -1.04 |
| No lce |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 30 deg - | 60.96 | 16.20 | -27.79 | -3543.66 | -2074.87 | -0.59 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 30 deg - | 45.72 | 16.20 | -27.79 | -3499.36 | -2049.17 | -0.56 |
| No lce |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 60 deg - | 60.96 | 28.12 | -15.91 | -2019.93 | -3607.06 | -1.08 |
| No lce |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 60 deg - | 45.72 | 28.12 | -15.91 | -1994.81 | -3562.05 | -1.06 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 90 deg - | 60.96 | 32.45 | 0.13 | 27.47 | -4162.50 | -0.99 |
| No lce |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 90 deg - | 45.72 | 32.45 | 0.13 | 26.89 | -4110.49 | -0.98 |
| No lce |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 120 deg | 60.96 | 28.18 | 16.17 | 2074:31 | -3620.06 | -0.46 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 120 deg | 45.72 | 28.18 | 16.17 | 2048.05 | -3574.85 | -0.45 |
| - No lce |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 150 deg | 60.96 | 16.45 | 27.89 | 3566.54 | -2124.39 | 0.06 |
| - No lce |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 150 deg | 45.72 | 16.45 | 27.89 | 3521.58 | -2097.94 | 0.05 |
| - No lce |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 180 deg | 60.96 | 0.16 | 32.20 | 4116.65 | -30.76 | 0.43 |
| - No lce |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 180 deg | 45.72 | 0.16 | 32.20 | 4064.77 | -30.69 | 0.41 |
| - No lce |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 210 deg | 60.96 | -16.17 | 27.79 | 3546.44 | 2072.38 | 1.30 |
| - No lce |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 210 deg | 45.72 | -16.17 | 27.79 | 3501.78 | 2045.92 | 1.28 |
| - No lce |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 240 deg | 60.96 | -27.99 | 15.93 | 2024.61 | 3587.15 | 1.28 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 240 deg | 45.72 | -27.99 | 15.93 | 1999.11 | 3541.63 | 1.25 |
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| Load Combination | Vertical <br> K | Shear ${ }_{x}$ <br> K | Shear ${ }_{z}$ | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 270 deg <br> - No.lce | 60.96 | -32.30 | -0.11 | -22.41 | 4139.71 | 1.05 |
| 0.9 Dead +1.0 Wind 270 deg <br> - No lce | 45.72 | -32.30 | -0.11 | -22.22 | 4087.24 | 1.04 |
| 1.2 Dead+1.0 Wind 300 deg <br> - No Ice | 60.96 | -28.04 | -16.13 | -2064.61 | 3598.18 | 0.52 |
| 0.9 Dead +1.0 Wind 300 deg <br> - No lce | 45.72 | -28.04 | -16.13 | -2038.81 | 3552.48 | 0.51 |
| 1.2 Dead+1.0 Wind 330 deg <br> - No Ice | 60.96 | -16.33 | -27.87 | -3561.42 | 2105.66 | -0.25 |
| 0.9 Dead+1.0 Wind 330 deg <br> - No Ice | 45.72 | -16.33 | -27.87 | -3516.85 | 2078.68 | -0.24 |
| 1.2 Dead+1.0 Ice+1.0 Temp | 94.81 | -0.00 | 0.00 | 2.09 | 3.56 | 0.00 |
| 1.2 Dead +1.0 Wind 0 deg+1.0 Ice+1.0 Temp | 94.81 | -0.02 | -8.91 | -1158.34 | 7.78 | -0.20 |
| 1.2 Dead+1.0 Wind 30 deg+1.0 Ice 1.0 Temp | 94.81 | 4.49 | -7.71 | -1000.38 | -583.60 | 0.02 |
| 1.2 Dead+1.0 Wind 60 deg+1.0 Ice +1.0 Temp | 94.81 | 7.78 | -4.43 | -573.09 | -1012.83 | 0.00 |
| 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp | 94.81 | 8.96 | 0.01 | 4.56 | -1167.52 | 0.04 |
| 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp | 94.81 | 7.77 | 4.46 | 583.04 | -1012.19 | 0.11 |
| 1.2 Dead+1.0 Wind 150 deg+1.0 Ice +1.0 Temp | 94.81 | 4.51 | 7.71 | 1006.10 | -588.28 | 0.12 |
| 1.2 Dead +1.0 Wind 180 deg+1.0 Ice +1.0 Temp | 94.81 | 0.01 | 8.91 | 1163.02 | 0.38 | 0.07 |
| 1.2 Dead+1.0 Wind 210 deg+1.0 Ice +1.0 Temp | 94.81 | -4.49 | 7.71 | 1005.21 | 590.14 | 0.13 |
| 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp | 94.81 | -7.75 | 4.44 | 578.32 | 1015.62 | 0.04 |
| 1.2 Dead+1.0 Wind 270 deg+1.0 Ice +1.0 Temp | 94.81 | -8.93 | -0.00 | 0.76 | 1169.68 | -0.02 |
| 1.2 Dead+1.0 Wind 300 deg+1.0 Ice +1.0 Temp | 94.81 | -7.74 | -4.45 | -576.71 | 1014.55 | -0.09 |
| 1.2 Dead+1.0 Wind 330 deg+1.0 Ice +1.0 Temp | 94.81 | -4.49 | -7.71 | -1000.76 | 591.32 | -0.15 |
| Dead+Wind 0 deg - Service | 50.80 | -0.04 | -7.20 | -913.23 | 8.92 | -0.24 |
| Dead+Wind 30 deg - Service | 50.80 | 3.62 | -6.22 | -786.46 | -459.74 | -0.13 |
| Dead+Wind 60 deg - Service | 50.80 | 6.29 | -3.56 | -448.14 | -799.96 | -0.24 |
| Dead+Wind 90 deg - Service | 50.80 | 7.26 | 0.03 | 6.49 | -923.32 | -0.22 |
| Dead+Wind 120 deg - | 50.80 | 6.30 | 3.62 | 461.01 | -802.87 | -0.10 |
| Service |  |  |  |  |  |  |
| Dead+Wind 150 deg Service | 50.80 | 3.68 | 6.24 | 792.36 | -470.73 | 0.01 |
| Dead+Wind 180 deg Service | 50.80 | 0.04 | 7.20 | 914.50 | -5.85 | 0.09 |
| Dead+Wind 210 deg Service | 50.80 | -3.62 | 6.22 | 787.88 | 461.14 | 0.29 |
| Dead+Wind 240 deg Service | 50.80 | -6.26 | 3.56 | 449.97 | 797.49 | 0.28 |
| Dead+Wind 270 deg Service | 50.80 | -7.23 | -0.02 | -4.57 | 920.20 | 0.24 |
| Dead+Wind 300 deg Service | 50.80 | -6.27 | -3.61 | -458.05 | 799.95 | 0.12 |
| Dead+Wind 330 deg Service | 50.80 | -3.65 | -6.23 | -790.42 | 468.53 | -0.06 |

Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | $P Y$ | $P Z$ | $P X$ | $P Y$ | $P Z$ | \% Error |
| Comb. | $K$ | $K$ | $K$ | $K$ | $K$ | $K$ |  |
| 1 | 0.00 | -50.80 | 0.00 | 0.00 | 50.80 | 0.00 | $0.000 \%$ |
| 2 | -0.17 | -60.96 | -32.20 | 0.17 | 60.96 | 32.20 | $0.000 \%$ |
| 3 | -0.17 | -45.72 | -32.20 | 0.17 | 45.72 | 32.20 | $0.000 \%$ |

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|  | Sum of Applied Forces |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Non-Linear Convergence Results

| Load <br> Combination | Converged? | Number <br> of Cycles | Displacement <br> Tolerance | Force <br> Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 4 | 0.00000001 | 0.00000001 |
| 2 | Yes | 5 | 0.00000001 | 0.00011704 |
| 3 | Yes | 5 | 0.00000001 | 0.00005461 |
| 4 | Yes | 6 | 0.00000001 | 0.00013601 |
| 5 | Yes | 6 | 0.00000001 | 0.00004637 |
| 6 | Yes | 6 | 0.00000001 | 0.00013695 |
| 7 | Yes | 6 | 0.0000001 | 0.00004667 |
| 8 | Yes | 5 | 0.00000001 | 0.00007307 |
| 9 | Yes | 4 | 0.00000001 | 0.00080607 |
| 10 | Yes | 6 | 0.0000001 | 0.00014044 |
| 11 | Yes | 6 | 0.00000001 | 0.00004760 |
| 12 | Yes | 6 | 0.00000001 | 0.00014107 |
| 13 | Yes | 6 | 0.00000001 | 0.00004783 |
| 14 | Yes | 5 | 0.00000001 | 0.00006454 |

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| 15 |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| 16 | Yes | 4 | 0.00000001 | 0.00070781 |
| 17 | Yes | 6 | 0.00000001 | 0.00013772 |
| 18 | Yes | 6 | 0.00000001 | 0.0000495 |
| 19 | Yes | 6 | 0.00000001 | 0.00013364 |
| 20 | Yes | 6 | 0.00000001 | 0.00004552 |
| 21 | Yes | 5 | 0.00000001 | 0.00010054 |
| 22 | Yes | 5 | 0.00000001 | 0.0000434 |
| 23 | Yes | 6 | 0.00000001 | 0.00013945 |
| 24 | Yes | 6 | 0.00000001 | 0.00004737 |
| 25 | Yes | 6 | 0.00000001 | 0.00014021 |
| 26 | Yes | 6 | 0.00000001 | 0.00004760 |
| 27 | Yes | 4 | 0.00000001 | 0.00000712 |
| 28 | Yes | 5 | 0.00000001 | 0.00086892 |
| 29 | Yes | 6 | 0.00000001 | 0.00012380 |
| 30 | Yes | 6 | 0.00000001 | 0.0001367 |
| 31 | Yes | 5 | 0.00000001 | 0.00087801 |
| 32 | Yes | 6 | 0.00000001 | 0.00012549 |
| 33 | Yes | 6 | 0.00000001 | 0.00012502 |
| 34 | Yes | 5 | 0.00000001 | 0.00087338 |
| 35 | Yes | 6 | 0.00000001 | 0.00012517 |
| 36 | Yes | 6 | 0.00000001 | 0.00012513 |
| 37 | Yes | 5 | 0.00000001 | 0.0008984 |
| 38 | Yes | 6 | 0.00000001 | 0.00012445 |
| 39 | Yes | 6 | 0.00000001 | 0.00012493 |
| 40 | Yes | 4 | 0.00000001 | 0.00013975 |
| 41 | Yes | 4 | 0.00000001 | 0.00057560 |
| 42 | Yes | 4 | 0.00000001 | 0.00058873 |
| 43 | Yes | 4 | 0.00000001 | 0.00013990 |
| 44 | Yes | 4 | 0.00000001 | 0.00059644 |
| 45 | Yes | 4 | 0.00000001 | 0.0005999 |
| 46 | Yes | 4 | 0.00000001 | 0.00012865 |
| 47 | Yes | 4 | 0.00000001 | 0.00059997 |
| 48 | Yes | 4 | 0.00000001 | 0.00055819 |
| 49 | Yes | 4 | 0.0000001 | 0.00014305 |
| 50 | Yes | 4 | 0.00000001 | 0.00059920 |
|  | Yes | 4 | 0.00000001 | 0.00060314 |

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | o |
| :---: | :---: | :---: | :---: | :---: | :---: | | ftist |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | ft | $175-164.25$ | 23.236 | 43 |
| L1 | $167.17-129.67$ | 21.395 | 43 | 1.1238 |
| L2 | $133.5-96$ | 13.857 | 43 | 0.1199 |
| L3 | $100.67-63.17$ | 7.840 | 43 | 0.9826 |
| L4 | $68.67-31.17$ | 3.616 | 43 | 0.7479 |
| L5 | $37.42-0$ | 1.084 | 43 | 0.4966 |
| L6 |  |  | 0.2615 | 0.0019 |

Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist 。 | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 175.00 | VHLP2.6 | 43 | 23.236 | 1.1238 | 0.0031 | 71097 |
| 172.00 | Platform Mount [LP 701-1] | 43 | 22.530 | 1.1231 | 0.0026 | 71097 |
| 168.00 | Side Arm Mount [SO 701-1] | 43 | 21.589 | 1.1208 | 0.0020 | 50895 |
| 162.00 | Platform Mount [LP 712-1] | 43 | 20.187 | 1.1114 | 0.0012 | 27766 |
| 152.00 | Sector Mount [SM 801-3] | 43 | 17.887 | 1.0798 | 0.0006 | 15860 |
| 142.00 | Platform Mount [LP 303-1] | 43 | 15.663 | 1.0322 | 0.0007 | 11100 |
| 115.00 | APXV18-206517S-C w/ Mount Pipe | 43 | 10.266 | 0.8564 | 0.0008 | 7876 |
| 50.00 | Side Arm Mount [SO 701-1] | 43 | 1.899 | 0.3540 | 0.0002 | 6798 |

## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | $175-164.25$ | 104.826 | 10 | 5.0777 |
| L1 | $167.17-129.67$ | 96.525 | 10 | 5.0610 | 0.0134 |
| L2 | $133.5-96$ | 62.518 | 10 | 4.4404 | 0.0077 |
| L3 | $100.67-63.17$ | 35.372 | 10 | 3.3780 | 0.0038 |
| L4 | $68.67-31.17$ | 16.312 | 10 | 2.2415 | 0.0022 |
| L5 | $37.42-0$ | 4.886 | 10 | 1.1795 | 0.0012 |
| L6 |  |  |  | 0.0006 |  |
|  |  |  |  |  |  |

Critical Deflections and Radius of Curvature - Design Wind

| Elevation ft | Appurtenance | Gov. Load <br> Comb. | Deflection <br> in | Tilt | Twist | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 175.00 | VHLP2.6 | 10 | 104.826 | 5.0777 | 0.0134 | 16675 |
| 172.00 | Platform Mount [LP 701-1] | 10 | 101.642 | 5.0747 | 0.0111 | 16675 |
| 168.00 | Side Arm Mount [SO 701-1] | 10 | 97.403 | 5.0646 | 0.0083 | 11898 |
| 162.00 | Platform Mount [LP 712-1] | 10 | 91.078 | 5.0225 | 0.0051 | 6366 |
| 152.00 | Sector Mount [SM 801-3] | 10 | 80.704 | 4.8801 | 0.0024 | 3579 |
| 142.00 | Platform Mount [LP 303-1] | 10 | 70.670 | 4.6650 | 0.0027 | 2487 |
| 115.00 | APXV18-206517S-C w/ Mount Pipe | 10 | 46.317 | 3.8690 | 0.0036 | 1757 |
| 50.00 | Side Arm Mount [SO 701-1] | 10 | 8.564 | 1.5975 | 0.0008 | 1508 |

Compression Checks,

| Pole Design Data |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | $L$ | $L_{u}$ | K/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
|  | \# |  | f | ft |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| L1 | $\frac{175-164.25}{(1)}$ | TP26x22x0.25 | 10.75 | 0.00 | 0.0 | $\begin{gathered} 19.570 \\ 5 \end{gathered}$ | -4.15 | 1440.89 | 0.003 |
| L2 | 164.25 - | TP34.0625 $\times 24.4135 \times 0.31$ | 37.50 | 0.00 | 0.0 | $32.498$ | -17.94 | 2355.22 | 0.008 |
| L3 | $\begin{gathered} 129.67(2) \\ 129.67-96 \\ \hline(3) \end{gathered}$ | TP41.75×32.452x0.375 | 37.50 | 0.00 | 0.0 | $\begin{array}{r} 47.868 \\ 4 \end{array}$ | -26.07 | 3447.73 | 0.008 |
| L4 | 96-63.17 (4) | $\begin{gathered} \mathrm{TP} 49.0625 \times 39.8421 \times 0.37 \\ 5 \end{gathered}$ | 37.50 | 0.00 | 0.0 | $\begin{gathered} 56.340 \\ 7 \end{gathered}$ | -35.67 | 3858.71 | 0.009 |
| L5 | $63.17-31.17$ <br> (5) | TP56.125x46.9602x0.375 | 37.50 | 0.00 | 0.0 | $\underset{4}{64.538}$ | -46.67 | 4199.33 | 0.011 |
| L6 | 31.17-0 (6) | TP62.9375×53.8475×0.37 | 37.42 | 0.00 | 0.0 | $\begin{gathered} 74.465 \\ 0 \end{gathered}$ | -60.95 | 4536.70 | 0.013 |

## Pole Bending Design Data

| Section No | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | $\begin{aligned} & \text { Ratio } \\ & M_{u x} \\ & \hline \end{aligned}$ | $M_{u y}$ | $\phi M_{n y}$ | $\begin{aligned} & \hline \text { Ratio } \\ & M_{u y} \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | kip-ft | kip-ft | $\phi M_{n x}$ | kip-ft | kip-ft | ${ }_{\text {¢ }} M_{n \gamma}$ |
| L1 | 175-164.25 | TP26x22x0.25 | 30.40 | 729.12 | 0.042 | 0.00 | 729.12 | 0.000 |
| 12 | (1) | TP34.0625×24.4135×0.31 | 499.51 | 1584.18 | 0.315 | 0.00 | 1584.18 | 0.000 |

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| Section No. | Elevation ft | Size | $M_{u x}$ <br> kip-ft | $\phi M_{n x}$ | Ratio $M_{\Delta x}$ | $M_{a y}$ <br> kip-ft | $\phi M_{n y}$ <br> kip-ft | Ratio $M_{u y}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| t |  |  |  |  | ${ }_{\phi} M_{n x}$ |  |  | $\phi M_{n v}$ |
|  | 129.67 (2) | 25 |  |  |  |  |  |  |
| L3 | 129.67-96 | TP41.75×32.452×0.375 | 1258.93 | 2847.12 | 0.442 | 0.00 | 2847.12 | 0.000 |
|  | (3) ${ }_{06-63.17}$ |  |  |  | 0.559 | 0.00 | 3755.71 | 0.000 |
| L4 | 96-63.17(4) | TP49.0625×39.8421×0.37 5 | 2098.34 | 3755.71 | 0.559 | 0.00 | 3755.71 | 0.000 |
| L5 | 63.17-31.17 | TP56.125x46.9602×0.375 | 3000.32 | 4686.62 | 0.640 | 0.00 | 4686.62 | 0.000 |
| L6 | $(5)$ $31.17-0(6)$ | TP62.9375×53.8475×0.37 5 | 4172.24 | 5847.24 | 0.714 | 0.00 | 5847.24 | 0.000 |

## Pole Shear Design Data

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | Ratio $V_{u}$ | Actual $T_{u}$ | $\phi T_{n}$ | Ratio $T_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $K$ | K | $\phi V_{n}$ | kip-ft | kip-ft | $\phi T_{n}$ |
| L1 | $175-164.25$ <br> (1) | TP26x22x0.25 | 6.01 | 343.46 | 0.017 | 2.79 | 726.88 | 0.004 |
| L2 | $\begin{gathered} 164.25- \\ 129.67(2) \end{gathered}$ | $\begin{gathered} \text { TP34.0625×24.4135x0.31 } \\ 25 \end{gathered}$ | 21.50 | 570.35 | 0.038 | 0.46 | 1605.45 | 0.000 |
| L3 | $\begin{gathered} 129.67-96 \\ \text { (3) } \end{gathered}$ | TP41.75×32.452x0.375 | 24.82 | 840.09 | 0.030 | 0.46 | 2903.88 | 0.000 |
| L4 | 96-63.17(4) | $\begin{gathered} \text { TP49.0625×39.8421×0.37 } \\ 5 \end{gathered}$ | 27.58 | 988.78 | 0.028 | 0.46 | 4034.18 | 0.000 |
| L5 | $63.17-31.17$ <br> (5) | TP56.125×46.9602×0.375 | 30.04 | 1132.65 | 0.027 | 0.46 | 5304.28 | 0.000 |
| L6 | 31.17-0 (6) | $\begin{gathered} \text { TP62.9375×53.8475×0.37 } \\ 5 \end{gathered}$ | 32.52 | 1306.86 | 0.025 | 0.46 | 7074.59 | 0.000 |


| Section No. | Elevation | Ratio <br> $P_{u}$ | Ratio <br> $M_{u x}$ | Ratio $M_{u y}$ | $\begin{gathered} \text { Ratio } \\ . V_{u} \\ \hline \end{gathered}$ | Ratio $T_{u}$ | Comb. <br> Stress <br> Ratio | Allow. Stress Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f$ | $\phi P_{n}$ | $\phi M_{n X}$ | $\phi M_{n v}$ | $\phi V_{n}$ | $\phi T_{n}$ |  |  |  |
| L1 | $175-164.25$ <br> (1) | 0.003 | 0.042 | 0.000 | 0.017 | 0.004 | 0.045 | 1.050 | 4.8 .2 |
| L2 | $\begin{gathered} 164.25- \\ 129.67(2) \end{gathered}$ | 0.008 | 0.315 | 0.000 | 0.038 | 0.000 | 0.324 | 1.050 | 4.8 .2 |
| L3 | $129.67-96$ <br> (3) | 0.008 | 0.442 | 0.000 | 0.030 | 0.000 | 0.451 | 1.050 | 4.8 .2 |
| L4 | 96-63.17 (4) | 0.009 | 0.559 | 0.000 | 0.028 | 0.000 | 0.569 | 1.050 | 4.8 .2 |
| L5 | $63.17-31.17$ <br> (5) | 0.011 | 0.640 | 0.000 | 0.027 | 0.000 | 0.652 | 1.050 1.050 | 4.8 .2 |
| L6 | 31.17-0 (6) | 0.013 | 0.714 | 0.000 | 0.025 | 0.000 | 0.728 | 1.050 | 4.8 .2 |

## Section Capacity Table

| Section No. | $\begin{aligned} & \text { Elevation } \\ & \hline \end{aligned}$ $f$ | Component Type | Size | Critical Element | $\begin{aligned} & \hline P \\ & K \\ & \hline \end{aligned}$ | $\begin{gathered} \emptyset P_{\text {alow }} \\ K \\ \hline \end{gathered}$ | $\begin{gathered} \% \\ \text { Capacity } \end{gathered}$ | $\begin{gathered} \hline \text { Pass } \\ \text { Fail } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 175-164.25 | Pole | TP26x22×0.25 |  | -4.15 | 1512.93 | 4.3 | Pass |
| L2 | 164.25-129.67 | Pole | TP34.0625 $24.4135 \times 0.3125$ | 2 | -17.94 | 2472.98 | 30.9 | Pass |
| L3 | 129.67-96 | Pole | TP41.75 3 32.452×0.375 | 3 | -26.07 | 3620.12 | 42.9 | Pass |
| L4 | 96-63.17 | Pole | TP49.0625 $39.8421 \times 0.375$ | 4 | -35.67 | 4051.65 | 54.2 | Pass |
| L5 | 63.17-31.17 | Pole | TP $56.125 \times 46.9602 \times 0.375$ | 5 | -46.67 | 4409.30 | 62.1 | Pass |
| L6 | 31.17-0 | Pole | TP62.9375×53.8475 $\times 0.375$ | 6 | -60.95 | 4763.53 | 69.3 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Pole (L6) | $69.3$ | Pass |

tnxTower Report - version 8.0.4.0

## APPENDIX B

## BASE LEVEL DRAWING

## APPENDIX C

## ADDITIONAL CALCULATIONS

## Monopole Base Plate Connection

| Site Info |  |
| ---: | :---: |
| BU \# | 823530 |
| Site Name | 864/Chapel St. Monop |
| Order \# | 471611 Rev. 0 |


| Analysis Considerations |  |
| ---: | :---: |
| TiA-222 Revision | H |
| Grout Considered: | No |
| $\mathrm{I}_{\mathrm{ar}}$ (in) | 0 |


| Applied Loads |  |  |
| :--- | :---: | :---: |
| Moment (kip-ft) |  |  |
| Axial Force (kips) |  |  |
| Shear Force (kips) |  | 4172.24 |



## Connection Properties

## Analysis Results

Anchor Rod Data
(45) 1-1/4" $ø$ bolts (Other N; Fy=105 ksi, Fu=150 ksi) on 68" BC

Base Plate Data
$71^{\prime \prime}$ OD $\times 1.5^{\prime \prime}$ Plate (A572-50; Fy=50 ksi, Fu=65 ksi)

Stiffener Data
(45) 12 " $\mathrm{H} \times$ 4"W $^{\text {" }}$ "T, Notch: $0.5^{"}$
plate: $F y=50 \mathrm{ksi}$; weld: $\mathrm{Fy}=70 \mathrm{ksi}$
horiz. weld: $0.5^{\prime \prime}$ fillet
vert. weld: 0.25 " fillet

## Pole Data

$62.9375^{\prime \prime} \times 0.375^{\prime \prime} 18$-sided pole (A572-65; Fy=65 ksi, Fu=80 ksi)

| Anchor Rod Summary | (units of kips, kip-in) |  |
| :---: | :---: | :---: |
| Pu _c $=66.79$ | ¢Pn_c = 101.75 | Stress Rating |
| $\mathrm{Vu}=0.72$ | $\phi \mathrm{Vn}=30.52$ | 62.6\% |
| $\mathrm{Mu}=\mathrm{n} / \mathrm{a}$ | $\phi \mathrm{Mn}=\mathrm{n} / \mathrm{a}$ | Pass |
| Base Plate Summary |  |  |
| Max Stress (ksi): | - |  |
| Allowable Stress (ksi): | - |  |
| Stress Rating: | Pirod OK |  |
| Stiffener Summary |  |  |
| Horizontal Weld: | Pirod OK |  |
| Vertical Weld: | Pirod OK |  |
| Plate Flexure+Shear: | Pirod OK |  |
| Plate Tension+Shear: | Pirod OK |  |
| Plate Compression: | Pirod OK |  |
| Pole Summary |  |  |
| Punching Shear: | Pirod OK |  |

## Pier and Pad Foundation

BU \# : 823530
Site Name: CT364/Chapel St.
App. Number: 471611 Rev. 0

TIA-222 Revision
Tower Type


Superstructure Analysis Reactions

| Compression, $\mathbf{P}_{\text {comp }}:$ | 61 | kips |
| ---: | :---: | :---: |
| Base Shear, Vu_comp: | 32 | kips |
|  |  |  |
|  |  |  |
| Moment, $\mathrm{M}_{\mathrm{u}}:$ | 4172 | ft-kips |
| Tower Height, $\mathrm{H}:$ | $\mathbf{1 7 5}$ | ft |
|  |  |  |
| BP Dist. Above Fdn, bp $_{\text {dist }}:$ | 2.5 | in |


| Pier Propertios |  |  |
| ---: | :---: | :--- |
| Pier Shape: | Circular |  |
| Pier Diameter, dpier: | 7.5 | ft |
| Ext. Above Grade, E: | 0.5 | ft |
| Pier Rebar Size, Sc: | 9 |  |
| Pier Rebar Quantity, mc: | 36 |  |
| Pier Tie/Spiral Size, St: | 4 |  |
| Pier Tie/Spiral Quantity, mt: | 10 |  |
| Pier Reinforcement Type: | Tie |  |
| Pier Clear Cover, cc $\mathrm{peier}^{2}$ | 3 | in |

Pad Properties

| Pad Propertios |  |  |
| :---: | :---: | :---: |
| Depth, D: | 8 | ft |
| Pad Width, W: | 22.5 | ft |
| Pad Thickness, T : | 2.8 | ft |
| Pad Rebar Size (Bottom), Sp: | 9 |  |
| Pad Rebar Quantity (Bottom), mp: | 23 |  |
| Pad Clear Cover, $\mathrm{cc}_{\text {pad }}$ : | 3 | in |


| Material Properties |  |  |
| ---: | :---: | :---: |
| Rebar Grade, Fy: |  | 60000 |
| psi |  |  |
| Concrete Compressive Strength, F'c: | 3000 | psi |
| Dry Concrete Density, $\delta \mathbf{c}:$ | 150 | pcf |

Soil Properties

| Soil Properties |  |  |
| ---: | :---: | :--- |
| Total Soil Unit Weight, $\gamma:$ | 121 | pcf |
| Ultimate Gross Bearing, Qult: | 30.000 | ksf |
| Cohesion, Cu: | 0.000 | ksf |
| Friction Angle, $\varphi:$ | 37 | degrees |
| SPT Blow Count, N blows: | 30 |  |
| Base Friction, $\mu:$ | 0.45 |  |
| Neglected Depth, $\mathrm{N}:$ | 3.30 | ft |
| Foundation Bearing on Rock? | No |  |
| Groundwater Depth, gw: | 12 | ft |


| Top \& Bot. Pad Rein. Different?: |  |
| ---: | :---: |
| Block Foundation?: |  |


| Foundation Analysis Checks |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating ${ }^{*}$ | Check |
|  |  |  |  |  |
| Lateral (Sliding) (kips) | 353.71 | 32.00 | $8.6 \%$ | Pass |
| Bearing Pressure (ksf) | 22.50 | 3.56 | $15.8 \%$ | Pass |
| Overturning (kip*f) | 6802.20 | 4450.67 | $65.4 \%$ | Pass |
| Pier Flexure (Comp.) (kip*f) | 6225.42 | 4354.40 | $66.6 \%$ | Pass |
|  |  |  |  |  |
| Pier Compression (kip) | 21089.12 | 106.33 | $0.5 \%$ | Pass |
| Pad Flexure (kip*ft) | 2888.25 | 1859.18 | $61.3 \%$ | Pass |
| Pad Shear - 1-way (kips) | 641.26 | 333.27 | $49.5 \%$ | Pass |
| Pad Shear - 2-way (Comp) (ksi) | 0.164 | 0.000 | $0.0 \%$ | Pass |
| Flexural 2-way (Comp) (kip*it) | 4012.99 | 2612.64 | $62.0 \%$ | Pass |

*Rating per TIA-222-H Section
15.5

Soil Rating
65.4\%

Structural Rating*:
$66.6 \%$

## ASCE 7 Hazards Report

Address:
No Address at This Location

Standard: ASCE/SE1 7-10
Risk Category: II
Soil Class: D-Stiff Soil

Elevation: 0 ft (NAVD 88)
Latitude: 41.663467
Longitude: -73.074281


## Date Accessed:

Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability $=$ $0.00143, \mathrm{MRI}=700$ years).

Site is in a hurricane-prone region as defined in ASCE/SEl 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

Site Soil Class:
Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.186 | $\mathrm{~S}_{\mathrm{DS}}:$ | 0.199 |
| :--- | :--- | :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.064 | $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.103 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.600 | $\mathrm{~T}_{\mathrm{L}}:$ | 6.000 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.400 | $\mathrm{PGA}:$ | 0.096 |
| $\mathrm{~S}_{\mathrm{MS}}:$ | 0.298 | $\mathrm{PGA}_{\mathrm{M}}:$ | 0.153 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.155 | $\mathrm{~F}_{\text {PGA }}:$ | 1.600 |
|  |  | $\mathrm{I}_{\mathrm{e}}:$ | 1 |

## Seismic Design Category

B


Data Accessed:
Date Source:

Tue Dec 112018
USGS Seismic Design Maps based on ASCE/SEl 7-10, incorporating Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.

AMERICAN SOCIETY OF CMIL ENGINEEAS

## Ice

## Results:

Ice Thickness: $\quad 0.75 \mathrm{in}$.

## Concurrent Temperature: 5 F

Gust Speed:
Data Source:
Date Accessed:

50 mph
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Tue Dec 112018

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

[^0]
## RF EMISSIONS COMPLIANCE REPORT

Crown Castle on behalf of AT\&T Mobility, LLC<br>Crown Castle Site Name: CT364/Chapel St. Monopole<br>Crown Castle Site ID: 823530<br>AT\&T Mobility, LLC FA \#: 10107966<br>580 Chapel Street<br>Thomaston, CT<br>1/14/2019

## Report Status:

## AT\&T Mobility, LLC Is Compliant



Klaus Bender
Registered Professional Engineer (Electrical)

Prepared By:

## Sitesafe, LLC

## Engineering Statement in Re :

Electromagnetic Energy Analysis
Crown Castle
Thomaston, CT
My signature on the cover of this document indicates:
That I am registered as a Professional Engineer in the jurisdiction indicated; and
That I have extensive professional experience in the wireless communications engineering industry; and

That I am an employee of Sitesafe, LLC in Vienna, Virginia; and
That I am thoroughly familiar with the Rules and Regulations of the Federal Communications Commission ("the FCC" and "the FCC Rules") both in general and specifically as they apply to the FCC's Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields; and

That the technical information serving as the basis for this report was supplied by Crown Castle (See attached Site Summary and Carrier documents), and that AT\&T Mobility, LLC's installations involve communications equipment, antennas and associated technical equipment at a location referred to as the "CT364/Chapel St. Monopole" ("the site"); and

That AT\&T Mobility, LLC proposes to operate at the site with transmit antennas listed in the carrier summary and with a maximum effective radiated power as specified by AT\&T Mobility, LLC and shown on the worksheet, and that worst-case $100 \%$ duty cycle have been assumed; and

That in addition to the emitters specified in the worksheet, there are additional collocated point-to-point microwave facilities on this structure and, the antennas used are highly directional oriented at angles at or just below the horizontal and, that the energy present at ground level is typically so low as to be considered insignificant and have not been included in this analysis; and

That this analysis has been performed with the assumption that the ground immediately surrounding the tower is primarily flat or falling; and

That at this time, the FCC requires that certain licensees address specific levels of radiofrequency energy to which workers or members of the public might possibly be exposed (at $\S 1.1307$ (b) of the FCC Rules); and

That such consideration of possible exposure of humans to radio-frequency radiation must utilize the standards set by the FCC, which is the Federal Agency having jurisdiction over communications facilities; and

That the FCC rules define two tiers of permissible exposure guidelines: 1) "uncontrolled environments," defined as situations in which persons may not be aware of (the "general public"), or may not be able to control their exposure to a transmission facility; and (2) "controlled environments," which defines situations in which persons are aware of their potential for exposure (industry personnel); and

That this statement specifically addresses the uncontrolled environment (which is more conservative than the controlled environment) and the limit set forth in the FCC rules for
licensees of AT\&T Mobility, LLC's operating frequency as shown on the attached antenna worksheet; and

That when applying the uncontrolled environment standards, the predicted Maximum Power Density at two meters above ground level from the proposed AT \&T Mobility, LLC operation is no more than $1.967 \%$ of the maximum in any accessible area on the ground and

That it is understood per FCC Guidelines and OET65 Appendix A, that regardless of the existent radio-frequency environment, only those licenses whose contributions exceed five percent of the exposure limit pertinent to their operation(s) bear any responsibility for bringing any noncompliant area(s) into compliance; and

That when applying the uncontrolled environment standards, the cumulative predicted energy density from the proposed operation is no more than $3.834 \%$ of the maximum in any accessible area up to two meters above the ground per OET-65; and

That the calculations provided in this report are based on data provided by the client and antenna pattern data supplied by the antenna manufacturer, in accordance with FCC guidelines listed in OET-65. Horizontal and vertical antenna patterns are combined for modeling purposes to accurately reflect the energy two meters above ground level where on-axis energy refers to maximum energy two meters above the ground along the azimuth of the antenna and where area energy refers to the maximum energy anywhere two meters above the ground regardless of the antenna azimuth, accounting for cumulative energy from multiple antennas for the carrier and frequency range indicated; and

That the Occupational Safety and Health Administration has policies in place which address worker safety in and around communications sites, thus individual companies will be responsible for their employees' training regarding Radio Frequency Safety.

In summary, it is stated here that the proposed operation at the site would not result in exposure of the Public to excessive levels of radio-frequency energy as defined in the FCC Rules and Regulations, specifically 47 CFR 1.1307 and that AT\&T Mobility, LLC's proposed operation is completely compliant.

Finally, it is stated that access to the tower should be restricted to communication industry professionals, and approved contractor personnel trained in radio-frequency safety; and that the instant analysis addresses exposure levels at two meters above ground level and does not address exposure levels on the tower, or in the immediate proximity of the antennas.

## Crown Castle CT364/Chapel St. Monopole Site Summary

Carrier Area MaxImum Percentage MPE

| AT\&T Mobility, LLC | $0.164 \%$ |
| :---: | :---: |
| AT\&T Mobility, LLC (Proposed) | $0.377 \%$ |
| AT\&T Mobility, LLC (Proposed) | $0.302 \%$ |
| AT\&T Mobility, LLC (Proposed) | $0.307 \%$ |
| AT\&T Mobility, LLC (Proposed) | $0.198 \%$ |
| AT\&T Mobility, LLC (Proposed) | $0.273 \%$ |
| AT\&T Mobility, LLC (Proposed) | $0.346 \%$ |
| Crown Castle (Decommissioned) | $0 \%$ |
| Sprint | $0.408 \%$ |
| Sprint | $0.057 \%$ |
| Sprint | $0.231 \%$ |
| T-Mobile | $0.146 \%$ |
| T-Mobile | $0.101 \%$ |
| Thomaston CT, Town of | $0.013 \%$ |
| Verizon Wireless | $0.364 \%$ |
| Verizon Wireless | $0.178 \%$ |
| Verizon Wireless | $0.249 \%$ |
| Verizon Wireless | $0.119 \%$ |

Composite Site MPE:
3.834 \%

## AT\&T Mobility, LLC CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: | 850 | MHz |
| :--- | :---: | :--- |
| Maximum Permissible Exposure (MPE): | 566.67 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Maximum power density at ground level: | 0.93145 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of Maximum Permissible Exposure: | 0.16437 | $\%$ |


| Antenna Make | Model | Helght (feet) | Orientation (degrees true) | ERP <br> (Watts) | On Axis |  | Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge} \mathbf{2}$ ) | Percent of MPE | Max Power Density <br> ( $\mu \mathrm{W} / \mathrm{cm}^{\mathrm{A}} \mathbf{2}$ ) | Percent of MPE |
| Powerwave | 7770 | 143 | 30 | 1094 | 0.515497 | 0.09097 | 0.796846 | 0.14062 |
| Powerwave | 7770 | 143 | 150 | 1094 | 0.51484 | 0.090854 | 0.796846 | 0.14062 |
| Powerwave | 7770 | 143 | 270 | 1094 | 0.51484 | 0.090854 | 0.796846 | 0.14062 |

# AT\&T Mobility, LLC (Proposed) <br> CT364/Chapel St. Monopole <br> Carrier Summary 

| Frequency: |  |  |  | 2100 | MHz |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Permissible Exposure (MPE): |  |  |  | 1000 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Maximum power density at ground level: |  |  |  | 3.7736 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Highest percentage of Maximum Permissible Exposure: |  |  |  | 0.37736 |  | ; |  |  |
|  |  |  |  |  | On Axis |  | Area |  |
| Antenna Make | Model | Helght (feet) | Orientation (degrees true) | ERP (Watts) | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}{ }^{\text {2 }}$ ) | $\begin{gathered} \text { Percent of } \\ \text { MPE } \end{gathered}$ | Max Power Density ( $\mathrm{HW} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE |
| Kathrein-Scala | 800-10965 | 143 | 30 | 7114 | 1.507398 | 0.15074 | 3.605002 | 0.3605 |
| Kathrein-Scala | 800-10964 | 143 | 150 | 5274 | 1.145413 | 0.114541 | 2.672426 | 0.267243 |
| Kathrein-Scala | 800-10965 | 143 | 270 | 7114 | 1.545119 | 0.154512 | 3.605002 | 0.3605 |

## AT\&T Mobility, LLC (Proposed) <br> CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: |  |  |  | 1900 | MHz |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Permiss | posure (MP |  |  | 1000 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Maximum power d | at ground le |  |  | 3.01505 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Highest percentag | ximum Per | Expos | ure: | 0.30151 | \% |  |  |  |
|  |  |  |  |  | On |  | Ar |  |
| Antenna Make | Model | $\begin{gathered} \text { Height } \\ \text { (feet) } \end{gathered}$ | Orientation (degrees true) | $\begin{aligned} & \text { ERP } \\ & \text { (Watts) } \end{aligned}$ | Max Power Density ( $\mathrm{HW} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\mathrm{A}} 2$ ) | Percent of MPE |
| Kathrein-Scala | 800-10965 | 143 | 30 | 6168 | 1.297139 | 0.129714 | 2.792729 | 0.279273 |
| Kathrein-Scala | 800-10964 | 143 | 150 | 5154 | 1.092579 | 0.109258 | 2.342057 | 0.234206 |
| Kathrein-Scala | 800-10965 | 143 | 270 | 6168 | 1.297139 | 0.129714 | 2.792729 | 0.279273 |

# AT\&T Mobility, LLC (Proposed) <br> CT364/Chapel St. Monopole <br> Carrier Summary 

| Frequency: | 763 | MHz |
| :--- | :---: | :--- |
| Maximum Permissible Exposure (MPE): | 508.67 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Maximum power density at ground level: | 1.56169 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of Maximum Permissible Exposure: | 0.30702 | $\%$ |


| Antenna Make | Model | Helght (feet) | Orientation (degrees true) | On Axis |  |  | Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \text { ERP } \\ & \text { (Watts) } \end{aligned}$ | Max Power Density ( $\mathrm{\mu W} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE | Max Power Density ( $\mathrm{\mu W} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE |
| Kathrein-Scala | 800-10965 | 143 | 30 | 2959 | 1.14122 | 0.224355 | 1.454571 | 0.285958 |
| Kathrein-Scala | 800-10964 | 143 | 150 | 2209 | 0.872606 | 0.171548 | 1.204042 | 0.236705 |
| Kathrein-Scala | 800-10965 | 143 | 270 | 2959 | 1.14122 | 0.224355 | 1.454571 | 0.285958 |

## AT\&T Mobility, LLC (Proposed) <br> CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: | 2300 | MHz |
| :--- | :---: | :--- |
| Maximum Permissible Exposure (MPE): | 1000 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Maximum power density at ground level: | 1.9767 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of Maximum Permlssible Exposure: | 0.19767 | $\%$ |


| Antenna Make | Model | Height (feet) | Orientation (degrees true) | $\begin{aligned} & \text { ERP } \\ & \text { (Watts) } \end{aligned}$ | On Axis |  | Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Max Power Density ( $\mathrm{HW} / \mathrm{cm}^{\wedge} 2$ ) | $\begin{gathered} \text { Percent of } \\ \text { MPE } \end{gathered}$ | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE |
| Kathrein-Scala | 800-10965 | 143 | 30 | 3954 | 1.005296 | 0.10053 | 1.871767 | 0.187177 |
| Kathrein-Scala | 800-10964 | 143 | 150 | 3516 | 0.80801 | 0.080801 | 1.788592 | 0.178859 |
| Kathrein-Scala | 800-10965 | 143 | 270 | 3954 | 1.003718 | 0.100372 | 1.871767 | 0.187177 |

## AT\&T Mobility, LLC (Proposed) CT364/Chapel St. Monopole Carrier Summary

| Frequency: | 850 | MHz |
| :--- | :---: | :--- |
| Maximum Permissible Exposure (MPE): | 566.67 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Maximum power density at ground level: | 1.54879 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of Maximum Permissible Exposure: | 0.27332 | $\%$ |


| Antenna Make | Model |  |  |  | On Axis |  | Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Height (feet) | Orientation (degrees true) | $\begin{aligned} & \text { ERP } \\ & \text { (Watts) } \end{aligned}$ | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}{ }^{2}$ ) | Percent of MPE | Max Power Density ( $\mathrm{HW} / \mathrm{cm}^{\wedge}$ ) | $\begin{gathered} \text { Percent of } \\ \text { MPE } \end{gathered}$ |
| Kathrein-Scala | 800-10965 | 143 | 30 | 3607 | 1.066637 | 0.18823 | 1.112151 | 0.196262 |
| Kathrein-Scala | 800-10964 | 143 | 150 | 2631 | 0.747523 | 0.131916 | 0.914984 | 0.161468 |
| Kathrein-Scala | 800-10965 | 143 | 270 | 3607 | 1.066637 | 0.18823 | 1.112151 | 0.196262 |

## AT\&T Mobility, LLC (Proposed)

## CT364/Chapel St. Monopole

Carrier Summary

| Frequency: |  |  |  | 737 | MHz |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Permissible Exposure (MPE): |  |  |  | 491.33 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Maximum power density at ground level: |  |  |  | 1.70012 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Highest percentage of Maximum Permissible Exposure: |  |  |  | 0.34602 | \% |  |  |  |
|  |  |  |  |  | On Axis |  | Area |  |
| Antenna Make | Model | Height (feet) | Orientation (degrees true) | ERP <br> (Watts) | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\mathrm{A}} \mathbf{2}$ ) | Percent of MPE | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE |
| CCI Antennas | HPA65R-BU6A | 143 | 30 | 2819 | 1.069303 | 0.217633 | 1.094544 | 0.22277 |
| CCI Antennas | HPA65R-BU4A | 143 | 150 | 1946 | 1.631718 | 0.3321 | 1.688769 | 0.343711 |
| CCI Antennas | HPA65R-BU6A | 143 | 270 | 2819 | 1.069303 | 0.217633 | 1.094544 | 0.22277 |

## Crown Castle (Decommissioned) <br> CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: |  |  |  | 1900 | MHz |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MaxImum Perm | ible Exposure (MPE) |  |  | 1000 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Maximum powe | ensity at ground lev |  |  | 0 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Highest percen | e of Maximum Perm | le Expo | ure: | 0 | \% |  |  |  |
|  |  |  |  |  | On A |  | Are |  |
| Antenna Make | Model | Height (feet) | Orientation (degrees true) | $\begin{aligned} & \text { ERP } \\ & \text { (Watts) } \\ & \hline \end{aligned}$ | Max Power Density ( $\mathrm{WW}^{\mathrm{W}} / \mathrm{cm}^{\wedge}$ ) | Percent of MPE | Max Power Density ( $\mathrm{H} / \mathrm{W} / \mathrm{cm}^{\wedge}$ ) | Percent of MPE |
| RFS | APXV18-206517S | 115 | 30 | 0 | 0 | 0 | 0 | 0 |
| RFS | APXV18-206517S | 115 | 150 | 0 | 0 | 0 | 0 | 0 |
| RFS | APXV18-206517S | 115 | 270 | 0 | 0 | 0 | 0 | 0 |

## Sprint <br> CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: | 1900 | MHz |
| :--- | :---: | :--- |
| Maximum Permissible Exposure (MPE): | 1000 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge}{ }^{\wedge}$ |
| Maximum power density at ground level: | 4.08206 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of Maximum Permissible Exposure: | 0.40821 | $\%$ |


| Antenna Make | Model | Height (feet) | Orientation (degrees true) | On Axis |  |  | Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ERP (Watts) | Max Power Density ( $\mu \mathbf{W} / \mathrm{cm}^{\wedge} 2$ ) | Percent of MPE | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ ) | Percent of MPE |
| RFS | APXVSPP18-C-A20 | 162 | 340 | 3804 | 0.706127 | 0.070613 | 1.290771 | 0.129077 |
| RFS | APXVSPP18-C-A20 | 162 | 340 | 3804 | 0.706127 | 0.070613 | 1.290771 | 0.129077 |
| RFS | APXVSPP18-C-A20 | 162 | 90 | 3804 | 0.702969 | 0.070297 | 1.290771 | 0.129077 |
| RFS | APXVSPP18-C-A20 | 162 | 90 | 3804 | 0.702969 | 0.070297 | 1.290771 | 0.129077 |
| RFS | APXVSPP18-C-A20 | 162 | 200 | 3804 | 0.702969 | 0.070297 | 1.290771 | 0.129077 |
| RFS | APXVSPP18-C-A20 | 162 | 200 | 3804 | 0.702969 | 0.070297 | 1.290771 | 0.129077 |

## Sprint <br> CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: | 862 | MHz |
| :--- | :---: | :--- |
| Maximum Permissible Exposure (MPE): | 574.67 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Maximum power density at ground level: | 0.33004 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of Maximum Permlssible Exposure: | 0.05743 | $\%$ |


| Antenna Make | Model | Height (feet) | Orientation (degrees true) | $\begin{aligned} & \text { ERP } \\ & \text { (Watts) } \end{aligned}$ | On Axis |  | Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}{ }^{2}$ ) | Percent of MPE | Max Power Density ( $\mathrm{HW} / \mathrm{cm}^{\wedge} 2$ ) | Percent of MPE |
| RFS | APXVSPP18-C-A20 | 162 | 340 | 1084 | 0.293205 | 0.051022 | 0.298318 | 0.051912 |
| RFS | APXVSPP18-C-A20 | 162 | 90 | 1084 | 0.292323 | 0.050868 | 0.298318 | 0.051912 |
| RFS | APXVSPP18-C-A20 | 162 | 200 | 1084 | 0.292323 | 0.050868 | 0.298318 | 0.051912 |

## Sprint <br> CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: | 2500 | MHz |
| :--- | :---: | :--- |
| Maximum Permissible Exposure (MPE): | 1000 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Maximum power density at ground level: | 2.31194 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of MaxImum Permissible Exposure: | 0.23119 | $\%$ |


| Antenna Make | Model | Height (feet) | Orientation (degrees true) | ERP (Watts) | Max Power Density ( $\mathrm{\mu W} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE | Max Power Density ( $\mathrm{HW} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RFS | APXVTM14-C-120 | 162 | 340 | 6168 | 0.840008 | 0.084001 | 1.600068 | 0.160007 |
| RFS | APXVTM14-C-120 | 162 | 90 | 6168 | 0.840008 | 0.084001 | 1.600069 | 0.160007 |
| RFS | APXVTM14-C-120 | 162 | 200 | 6168 | 0.839501 | 0.08395 | 1.600068 | 0.160007 |

## T-Mobile <br> CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: | 700 | MHz |
| :--- | :---: | :--- |
| Maximum Permissible Exposure (MPE): | 466.67 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Maximum power density at ground level: | 0.68235 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of Maximum Permissible Exposure: | 0.14622 | $\%$ |


| Antenna Make |  | Height (feet) | Orientation (degrees true) |  | On Axis |  | Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Model |  |  | ERP (Watts) | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge} \mathbf{2}$ ) | Percent of MPE | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ ) | Percent of MPE |
| ANDREW | LNX-6515DS-VTM | 172 | 10 | 2109 | 0.381151 | 0.081675 | 0.386046 | 0.082724 |
| ANDREW | LNX-6515DS-VTM | 172 | 190 | 2109 | 0.381151 | 0.081675 | 0.386046 | 0.082724 |
| ANDREW | LNX-6515DS-VTM | 172 | 280 | 2109 | 0.381151 | 0.081675 | 0.386046 | 0.082724 |

## T-Mobile <br> CT364/Chapel St. Monopole

## Carrier Summary

| Frequency: |  |  |  | 1900 | MHz |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Permiss | e Exposure (MPE): |  |  | 1000 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Maximum power | sity at ground leve |  |  | 1.00986 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Highest percentag | of Maximum Permis | e Expos |  | 0.10099 | \% |  |  |  |
|  |  |  |  |  | On |  | Ar |  |
| Antenna Make | Model | Height (feet) | Orientation (degrees true) | ERP (Watts) | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ ) | Percent of MPE |
| EMS | RR90-17-02DPL2 | 172 | 10 | 1653 | 0.391076 | 0.039108 | 0.582585 | 0.058259 |
| EMS | RR90-17-02DPL2 | 172 | 190 | 1653 | 0.391076 | 0.039108 | 0.582585 | 0.058259 |
| EMS | RR90-17-02DPL2 | 172 | 280 | 1653 | 0.391076 | 0.039108 | 0.582585 | 0.058259 |

# Thomaston CT, Town of CT364/Chapel St. Monopole <br> Carrier Summary 

| Frequency: |  |  |  | 450 | MHz |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Permissible Exposure (MPE): |  |  |  | 300 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Maximum power density at ground level: |  |  |  | 0.03804 | $\mu \mathrm{W} / \mathrm{cm}^{\text {A }} 2$ |  |  |  |
| Highest percentage of Maximum Permissible Exposure: |  |  |  | 0.01268 | \% |  |  |  |
|  |  |  |  |  | On Axis |  | Area |  |
| Antenna Make | Model | Helght (feet) | Orientation (degrees true) | ERP (Watts) | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ ) | Percent of MPE | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE |
| Lonestar | LS-230-C | 168 | 0 | 100 | 0.038045 | 0.012682 | 0.038045 | 0.012682 |

## Verizon Wireless <br> CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: | 850 | MHz |
| :--- | :---: | :--- |
| Maximum Permissible Exposure (MPE): | 566.67 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Maximum power density at ground level: | 2.06222 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of Maximum Permissible Exposure: | 0.36392 | $\%$ |


| Antenna Make | Model |  |  |  | On Axis |  | Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Height (feet) | Orientation (degrees true) | $\begin{aligned} & \text { ERP } \\ & \text { (Watts) } \end{aligned}$ | Max Power Density ( $\mathrm{\mu W} / \mathrm{cm}^{\wedge}$ 2) | $\begin{aligned} & \text { Percent of } \\ & \text { MPE } \end{aligned}$ | Max Power Density ( $\mathrm{HW} / \mathrm{cm}^{\wedge}$ 2) | Percent of MPE |
| Antel | LPA-80080-4CF | 152 | 120 | 1423 | 0.630999 | 0.111353 | 0.65529 | 0.115639 |
| Antel | LPA-80080-4CF | 152 | 120 | 1423 | 0.630999 | 0.111353 | 0.65529 | 0.115639 |
| Antef | LPA-80080-4CF | 152 | 240 | 1423 | 0.630487 | 0.111262 | 0.65529 | 0.115639 |
| Ante! | LPA-80080-4CF | 152 | 240 | 1423 | 0.630487 | 0.111262 | 0.65529 | 0.115639 |
| Antei | LPA-80080-4CF | 152 | 290 | 1423 | 0.630487 | 0.111262 | 0.65529 | 0.115639 |
| Antel | LPA-80080-4CF | 152 | 290 | 1423 | 0.630487 | 0.111262 | 0.65529 | 0.115639 |

## Verizon Wireless CT364/Chapel St. Monopole Carrier Summary

| Frequency: | 1900 | MHz |
| :--- | :---: | :--- |
| Maximum Permisslble Exposure (MPE): | 1000 | $\mathrm{WW} / \mathrm{cm}^{\wedge} 2$ |
| Maximum power density at ground level: | 1.78338 | $\mu \mathrm{~W} / \mathrm{cm}^{\wedge} 2$ |
| Highest percentage of Maximum Permissible Exposure: | 0.17834 | $\%$ |


| Antenna Make | Model | Height (feet) | Orientation (degrees true) | $\begin{aligned} & \text { ERP } \\ & \text { (Watts) } \end{aligned}$ | On Axis |  | Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Max Power Density ( $\mathrm{\mu W} / \mathrm{cm}^{\wedge}$ ) | Percent of MPE | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}$ 2) | $\begin{gathered} \text { Percent of } \\ \text { MPE } \end{gathered}$ |
| Commscope | NNHH-65B-R4 | 152 | 40 | 3848 | 0.713997 | 0.0714 | 1.476289 | 0.147629 |
| Commscope | NNHH-65B-R4 | 152 | 190 | 3848 | 0.712141 | 0.071214 | 1.476289 | 0.147629 |
| Commscope | NNHH-65B-R4 | 152 | 290 | 3848 | 0.713997 | 0.0714 | 1.476289 | 0.147629 |

## Verizon Wireless <br> CT364/Chapel St. Monopole <br> Carrier Summary

| Frequency: |  |  |  | 2100 | MHz |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Permiss | xposure (MPE): |  |  | 1000 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Maximum power d | at ground leve |  |  | 2.49366 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Highest percentag | Aaximum Permis | Exposu |  | 0.24937 | \% |  |  |  |
|  |  |  |  |  | On | xis | Ar |  |
| Antenna Make | Model | Height (feet) | Orientation (degrees true) | $\begin{aligned} & \text { ERP } \\ & \text { (Watts) } \end{aligned}$ | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}$ 2) | $\begin{gathered} \text { Percent of } \\ \text { MPE } \end{gathered}$ | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ ) | Percent of MPE |
| Commscope | NNHH-65B-R4 | 152 | 40 | 3591 | 1.298947 | 0.129895 | 2.34258 | 0.234258 |
| Commscope | NNHH-65B-R4 | 152 | 190 | 3591 | 1.336585 | 0.133658 | 2.34258 | 0.234258 |
| Commscope | NNHH-65B-R4 | 152 | 290 | 3591 | 1.298947 | 0.129895 | 2.34258 | 0.234258 |

## Verizon Wireless <br> CT364/Chapel St. Monopole Carrier Summary

| Frequency: |  |  |  | 751 | MHz |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maximum Permiss | Exposure (MPE): |  |  | 500.67 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Maximum power d | at ground leve |  |  | 0.59403 | $\mu \mathrm{W} / \mathrm{cm}^{\wedge} 2$ |  |  |  |
| Highest percentag | Maximum Permis | Exposu |  | 0.11865 | \% |  |  |  |
|  |  |  |  |  | On | Axis | Ar |  |
| Antenna Make | Model | Height (feet) | Orientation (degrees true) | ERP (Watts) | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}$ 2) | $\begin{gathered} \text { Percent of } \\ \text { MPE } \end{gathered}$ | Max Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{\wedge}$ 2) | $\begin{gathered} \text { Percent of } \\ \text { MPE } \end{gathered}$ |
| Commscope | NNHH-65B-R4 | 152 | 40 | 560 | 0.18481 | 0.036913 | 0.22437 | 0.044814 |
| Commscope | NNHH-65B-R4 | 152 | 40 | 560 | 0.18481 | 0.036913 | 0.22437 | 0.044814 |
| Commscope | NNHH-65B-R4 | 152 | 190 | 560 | 0.185282 | 0.037007 | 0.224371 | 0.044814 |
| Commscope | NNHH-65B-R4 | 152 | 190 | 560 | 0.185282 | 0.037007 | 0.224371 | 0.044814 |
| Commscope | NNHH-65B-R4 | 152 | 290 | 560 | 0.18481 | 0.036913 | 0.224371 | 0.044814 |
| Commscope | NNHH-65B-R4 | 152 | 290 | 560 | 0.18481 | 0.036913 | 0.224371 | 0.044814 |

```
Charles McGuirt
Crown Castle 3 Corporate Dr., St 101
Clifton Park, NY 12065
```

| Subject: | Mount Analysis Report |  |
| :---: | :---: | :---: |
| Carrier Designation: | AT\&T Mobility Co-Locate Carrier Site Number: Carrier Site Name: | $\begin{aligned} & 10107966 \\ & \text { CTL01062 } \end{aligned}$ |
| Crown Castle Designation: | Crown Castle BU Number: Crown Castle Site Name: Crown Castle JDE Job Number: Crown Castle Order Number: | 823530 <br> CT364/Chapel St. <br> 548514 <br> 471611 Rev. 0 |
| Engineering Firm Designation: | Infinigy Report Designation: | 400087 |
| Site Data: | 580 Chapel Street, Thomaston, Litchfield County, CT, 06787 Latitude $41^{\circ} 39^{\prime} 48.48^{\prime \prime}$ Longitude -73 $4^{\prime}$ '27.41" |  |
| Structure Information: | Tower Height \& Type: Mount Elevation: Mount Type: | 175 ft Monopole 142 ft <br> 14 ft Platform |
| Dear Charles McGuirt, |  |  |

Infinigy is pleased to submit this "Mount Analysis Report" to determine the structural integrity of AT\&T's antenna mounting system with the proposed appurtenance and equipment addition on the abovementioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point for fall protection or rigging is not part of this document.

The purpose of the analysis is to determine acceptability of the mount stress level. Based on our analysis we have determined the mount stress level to be:

## Platform

## Sufficient

The analysis has been performed in accordance with the 2015 International Building Code/ 2018 Connecticut Building Code and TIA-222-H Standard based upon an ultimate 3 -second gust wind speed of 120 mph . Exposure Category B with Risk Category II was/were used in this analysis.

Mount analysis prepared by: Ishan Patel, Respectfully Submitted by:

Joe Johnston, P.E.
VP Structural Engineering


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## 1) INTRODUCTION

This mount is a existing Commscope MC-PK14L. This Mount is installed at 142 ft . elevation on 3 sectors of the 175 ft monopole.

## 2) ANALYSIS CRITERIA

| Building Code: | 2015 IBC |
| :--- | :--- |
| TIA-222 Revision: | TIA-222-H |
| Risk Category: | II |
| UItimate Wind Speed: | 120 mph |
| Exposure Category: | C |
| Ice Thickness: | 1.28 in |
| Wind Speed with Ice: | 50 mph |
| Man Live Load at End-Points: | 250 lb |

Table 1 - Final Equipment Configuration

| Mount Centerline (ft) | Antenna Centerline (ft) | $\begin{aligned} & \text { Number } \\ & \text { of } \\ & \text { Antennas } \end{aligned}$ | Antenna Manufacturer | Mount Type |
| :---: | :---: | :---: | :---: | :---: |
| 142.0 | 142.0 | 1 | CCI HPA65R-BU4A | Platform |
|  |  | 2 | CCI HPA65R-BU6A |  |
|  |  | 2 | Kathrein 80010964 |  |
|  |  | 4 | Kathrein 80010965 |  |
|  |  | 3 | PWave 7770 |  |
|  |  | 3 | Ericsson RRUS-4415 B30 |  |
|  |  | 3 | Ericsson RRUS-4449 B5/B12 |  |
|  |  | 3 | Ericsson RRUS 4478 B14 |  |
|  |  | 3 | Ericsson RRUS 8843 B2/B66A |  |
|  |  | 6 | PNA ${ }^{\text {ave LGP21401 }}$ |  |
|  |  | 3 | Raycap DC6-48-60-18-8F |  |

3) ANALYSIS PROCEDURE

Table 2 - Documents Provided


## 3.1) Analysis Method

RISA-3D (Version 17.0.2), a commercially available analysis software package, was used to create a threedimensional model of the antenna mounting system and calculate member stresses for various loading cases.

## 3.2) Assumptions

1) The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specifications.
2) The configuration of antennas, mounts, and other appurtenances are as specified in Table 1 and the referenced drawings.
3) All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
4) Steel grades have been assumed as follows, unless noted otherwise:

| Channel, Solid Round, Angle, Plate | ASTM A36 (GR 36) |
| :--- | :--- |
| HSS (Rectangular) | ASTM A53 (GR 35) |
| Pipe | ASTM A53 (GR 35) |
| Connection Bolts | ASTM A325 |

This analysis may be affected if any assumptions are not valid or have been made in error. Infinigy should be notified to determine the effect on the structural integrity of the antenna mounting system.

## 4) ANALYSIS RESULTS

Table 3 - Mount Component Stresses vs. Capacity (Platform)



Notes:

1) See additional documentation in "Appendix C - Software Analysis Output" for calculations supporting the \% capacity consumed.
2) All sectors are typical

## 4.1) Recommendations

The Sector Frame Mount has sufficient capacity to support the proposed loading. No modifications are required at this time.

## APPENDIX A

WIRE FRAME AND RENDERED MODELS



Envelope Only Solution

| Infinigy | 8 | Existing Configuration |
| :--- | :--- | :--- |
| IP |  | Dec 26, 2018 at 4:25 PM |
| $600-003$ |  | $823530 . \mathrm{r3d}$ |



Envelope Only Solution

| Infinigy | 823530 | Existing Configuration |
| :---: | :---: | :---: |
| IP |  | Dec 26, 2018 at 4:25 PM |
| 600-003 |  | 823530.r3d |





| Loads: BLC 1, Self Weight |
| :--- |
| Envelope Only Solution |


| Infinigy |  | Existing Configuration |
| :--- | :--- | :--- |
| IP | 823530 | Dec 26, 2018 at 4:24 PM |
| $600-003$ |  | 823530.r3d |



Loads: BLC 2, Wind Load AZI 000
Envelope Only Solution

| Infinigy | 823530 | Existing Configuration |
| :---: | :---: | :---: |
| IP |  | Dec 26, 2018 at 4:24 PM |
| 600-003 |  | 823530.r3d |






Loads: BLC 6, Wind + Ice Load AZI 090
Envelope Only Solution

| Infinigy | 823530 | Existing Configuration |
| :---: | :---: | :---: |
| IP |  | Dec 26, 2018 at 4:24 PM |
| 600-003 |  | 823530.r3d |

## APPENDIX B



Rooftop Inputs:
Rooftop Wind Speed-Up?: NO N What

| Site Information Inputs: |  |
| :---: | :---: |
| Adopted Building Code: | 2015 BC |
| Structure Load Standard: | W1422-H5 |
| Antenna Load Standard: |  |
| Structure Risk Category: |  |
|  | 紋 |
| Structure Type: | Mount Mintoim |
| Number of Sectors: | 25k |
| Structure Shape 1: | Round |


| Wind Loading Inputs: |  |
| :---: | :---: |
|  | mph \{ultimate 3-second gust) |
|  | ft |
|  | degrees |
|  |  |
|  |  |


| Wind with No Ice |  |  |
| :---: | :---: | :---: |
| $\mathrm{q}_{2}$ (psf) | Gh | $\mathrm{F}_{\mathrm{ST}}$ (psf) |
| 37.51 | 1.00 | 45.01 |


| Wind with Ice |  |  |  |
| :---: | :---: | :---: | :---: |
| $\mathrm{q}_{2}$ (psf) | Gh | $\mathrm{F}_{\mathrm{sI}}$ (psf) |  |
| 6.51 | 1.00 | 16.42 |  |


|  | Ice Loading Inputs: |  |
| :---: | :---: | :---: |
| Is Ice Loading Needed?: |  |  |
| Ice Wind Velocity: |  | mph [ultimate 3-second gust) |
| Base Ice Thickness: | 1818 |  |

Input Appurtenance Information and Load Placements:

| Appurtenance Name | Elevation ( ft ) | Total Quantity | Kа | Front Shape | Side Shape | $\begin{gathered} \mathrm{q}_{\mathrm{z}} \\ \{\mathrm{psf}\} \end{gathered}$ | $\begin{aligned} & \text { EPA } \\ & \left(\mathrm{ft}^{2}\right) \end{aligned}$ | $\begin{gathered} \mathrm{Fz} \\ \text { (lbs) } \end{gathered}$ | $\begin{gathered} \mathrm{Fx} \\ (\mathrm{lbs}) \end{gathered}$ | $\begin{gathered} \mathrm{F} 2_{2}(60) \\ (\mathrm{lbs}) \end{gathered}$ | $\begin{gathered} \text { Fx( } 30\rangle \\ (\mathrm{lbs}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1.00 | Flat | Flat | 37.51 | 4.96 | 185.97 | 130.15 | 144.10 | 172.02 |
|  |  |  | 1.00 | Flat | Flat | 37.51 | 7.85 | 294.48 | 208.12 | 229.71 | 272.89 |
|  |  |  | 1.00 | Flat | Fiat | 37.51 | 10.00 | 375.01 | 153.95 | 209.21 | 319.74 |
|  |  |  | 1.00 | Flat | Flat | 37.51 | 13.81 | 518.17 | 218.81 | 293.65 | 443.33 |
|  |  |  | 1.00 | Flat | Flat | 37.51 | 5.51 | 206.63 | 109.84 | 134.04 | 182.43 |
|  |  |  | 1.00 | Flat | Flat | 37.51 | 1.64 | 61.63 | 23.98 | 33.39 | 52.22 |
|  |  |  | 1.00 | Flat | Flat | 37.51 | 1.97 | 73.80 | 52.82 | 58.07 | 68.56 |
|  |  |  | 1.00 | Flat | Flat | 37.51 | 1.84 | 69.11 | 39.71 | 47.06 | 61.76 |
|  |  |  | 1.00 | Flat | Flat | 37.51 | 1.64 | 61.48 | 50.77 | 53.45 | 58.80 |
|  | 23x ${ }^{3}$ |  | 1.00 | Flat | Flat | 37.51 | 1.10 | 41.41 | 13.02 | 20.12 | 34.31 |
|  |  |  | 1.00 | Round | Round | 37.51 | 1.21 | 45.45 | 45.45 | 45.45 | 45.45 |

## APPENDIX C

## SOFTWARE ANALYSIS OUTPUT

$\qquad$
Model Name

## Member Primary Data

|  | Label | 1 Joint | 3 Joint | K Joint | Rotate(deg) | Section/Shap | Type | Design List | Material | Design Rules |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | N1 | N2 |  |  | HSS 4"x4"x1/4" | Beam | None | A53 Gr.B | Typical |
| 2 | M2 | N74A | N4 |  |  | RIGID | None: | None | RIGID | Typical |
| 3 | M8 | N19 | N18 |  |  | 3" STD Pipe | Beam | None | A53 Gr.B | Typical |
| 4 | M11 | N28 | N76 |  |  | HSS 4"x4"x1/4" | Beam | None | A53 Gr.B | Typical |
| 5 | M18 | N40 | N43 |  | 270 | L2"x2"x ${ }^{\text {/ }} 16$ | Beam | None | A36 Gr. 36 | Typical |
| 6 | M29 | N79 | N78 |  |  | 2.375"OD. PI... | Beam | None | A53 Gr.B | Typical |
| 7 | M14 | N56 | N55 |  |  | 3" STD Pipe | Beam | None | A53 Gr.B | Typical |
| 8. | M18A | N64 | N63 |  |  | 2.375\%O.D. Plik | Beam | None | A53 Gri ${ }^{\text {a }}$ | Typical |
| 9 | M19 | N67 | N66 |  |  | 3" STD Pipe | Beam | None | A53 Gr.B | Typical |
| 10 | M23 | N75 | N74 |  |  | 2.375 OD. P\%. | Beam | None | A53 Gr.B | Typical |
| 11 | MP6 | N54 | N49 |  |  | 2.375" O.D. Pi... | Beam | None | A53 Gr.B | Typical |
| 12 | MP5 | N50 | N55A |  |  | 2.375" O.D.P.. | Beam | None | A53 Gr. ${ }^{\text {a }}$ | Typical |
| 13 | MP4 | N51 | N56A |  |  | 2.375" O.D. Pi... | Beam | None | A53 Gr.B | Typical |
| 14 | MP2 | N53 | N58 |  |  | 2,375 O:D Plico | Beam | None | A53 Gr.B | Typical |
| 15 | MP1 | N52 | N57 |  |  | 2.375" O.D. PI... | Beam | None | A53 Gr.B | Tupical |
| 16 | M20 | N41 | N42 |  |  | L2" $\times 2$ 1 $\times 3 / 16$ | Beam | None | A36 Gr. 36 | Tivpical |
| 17 | M17A | N59 | N60 |  |  | HSS 4"x4"x1/4" | Beam | None | A53 Gr.B | Typical |
| 18. | M18C | N9 | N75A |  |  | RIGID | None | None | RIGID | Typleal |
| 19 | M19B | N77 | N31 |  |  | HSS 4"x4"x1/4" | Beam | None | A53 Gr, B | Typical |
| 20 | M20A | N64A | N67A |  | 270 | $12^{\prime \prime} \times 2 \times 3 / 16$ | Beam | None | A36.Cr36 | Typical |
| 21 | M21 | N65 | N66A |  |  | L2" $\times 2$ "×3/16 | Beam | None | A36 Gr. 36 | Typical |
| 22 | M22 | N7OA | N71A | \% |  | HSS $4^{4 \times 4} \times 4^{4} \times 1 / 4{ }^{\text {a }}$ | Beam. | None | A53 GrB | Typloal |
| 23 | M23A | N79A | N72 |  |  | RIGID | None | None | RIGID | Typical |
| 24 | M24. | N74B | N80 |  |  | HSS 4 $4 \times 4 \times 4 \times 1 / 4{ }^{10}$ | Beam. | None | A53 GHB | Typlical |
| 25 | M25 | N75B | N78A |  | 270 |  | Beam | None | A36 Gr. 36 | Typical |
| 26. | M26 | N76A | N77A |  |  | L2"x2'x3/16 | Beam, | None | A36 Grib | Typlal |
| 27 | MP3 | N77B | N78B |  |  | 2.375 ${ }^{\prime \prime}$ O.D. Pl... | Beam | None | A53 Gr.B | Tvpical |
| 28. | MP/2 | N85 | N80A |  |  | 2375 O.D.Plis | Beam, | None | A53 Girb | Typical |
| 29 | MP11 | N81 | N86 |  |  | 2.375" O.D. Pl... | Beam | None | A53 Gr.B | Typical |
| 30 | MP10 | N82 | N87. |  |  | 2.375 ODD. ${ }^{\text {a }}$ | Beam. | None | A53 Gr.B | Typical |
| 31 | MP8 | N84 | N89 |  |  | 2.375" O.D. Pi... | Beam | None | A53 Gr.B | Typical |
| 32 | MP7. | N83 | N88. |  |  | 2,375\%0. ${ }^{\text {a }}$ / | Beam | None | A53 Gr. B | Typleal |
| 33 | MP9 | N90 | N91 |  |  | 2.375" O.D. Pi... | Beam | None | A53 Gr.B | Tvpical |
| 34 | MP18 | N98 | N93 | \%43 | , \% | 2,375. O,D.PI., | Beam | None | A53 Cr.B | Tyical |
| 35 | MP17 | N94 | N99 |  |  | 2.375" O.D. Pl... | Beam | None | A53 $\mathrm{Gr} . \mathrm{B}$ | Typical |
| 36 | MP16. | N95 | N100 |  |  | 2375 ODM | Beam. | None | A53 GrB | Typleal |
| 37 | MP14 | N97 | N102 |  |  | 2.375" O.D. Pl... | Beam | None | A53 Gr.B | Typical |
| 38. | MP13 | N96 | N101 |  |  | 2375\% OD. PIt | Beam | None | A53 Grib | Typical |
| 39 | MP15 | N103 | N104 |  |  | 2.375" O.D. Pl... | Beam | None | A53 Gr.B | Typical |

## Material Takeoff

| Material |  | Size | Pieces | Length[in] | Weight[K] |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | General |  |  |  |  |
| 2. |  | T, , <, , , \% | 4.3. ${ }^{\text {a }}$ | , 32.4 | W\% 0 |
| 3 | Total General |  | 3 | 32.4 | 0 |
| 4 |  | N, | , | , M, 32.4, | , , |
| 5 | Hot Rolled Steel |  |  |  |  |
| 6. | A36 Gr 36 | $\xrightarrow{\square} 2 \times 2 \times 3$ | W 6 | +, 303.1 | - $\quad 0$ |
| 7 | A53 Gr.B | HSS4X4X4 | 6 | 370.7 | . 4 |
| 8. | A53 GrB | $\cdots$ PIPE 2.0 | 21., | 1800 | . 5 |
| 9 | A53 Gr.B | PIPE 3.0 | 3 | 504 | . 3 |
| 10 | Total HR Steel | , 4, ${ }^{\text {a }}$, | \% 36 | - 2977.8 | 1.2 |

Dec 26, 2018
$\qquad$

Basic Load Cases

|  | BLC Description | Category | $X$ Gravity | Y Gravity | Z Gravity | Joint | Point | Distribut | dArea(Me... | Surface(... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Self Weight | DL |  | -1 |  |  | 42 |  | 4 |  |
| 2 | Wind Load AZI 000 | WLZ |  |  |  |  | 42 |  | 1 |  |
| 3 | Wind Load AZI 090 | WLX |  |  |  |  | 42 |  | 1 |  |
| 4 | Ice Weight | OL1 |  |  |  |  | 42 | 39 | 4 |  |
| 5 | Wind + Ice Load AZI 000 | OL2 |  |  |  |  | 42 |  | 1 |  |
| 6 | Wind + Ice Load AZ1 090 | OL3 |  |  |  |  | 42 |  | 1 |  |
| 7 | Service Live 1 | LL |  |  |  | 9 |  |  |  |  |
| 8. | BLC 1 Transient Area Loads | None |  | \% |  |  |  | 45 |  |  |
| 9 | BLC 2 Transient Area Loads | None |  |  |  |  |  | 38 |  |  |
| 10 | BLC 3 Transient Area Loads. | None |  |  |  |  |  | 33 | \% |  |
| 11 | BLC 4 Transient Area Loads | None |  |  |  |  |  | 45 |  |  |
| 12 | BLC 5 Transient Area Loads | None |  |  |  |  |  | 38 |  |  |
| 13 | BLC 6 Transient Area Loads | None |  |  |  |  |  | 33 |  |  |

## Load Combinations

| Description |  | Solve | PDelta |  | BLC | Factor | BLC | Factor | BLC | Factor | BLC | Fa. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.4D | Yes | Y |  | DL | 1.4 |  |  |  |  |  |  |  |  |  |  |
| 2 | $1.2 \mathrm{D}+1 \mathrm{WAZ} 000$ | Yes | $Y$ |  | DL | 1.2 | WLZ | 1 |  |  |  |  |  |  |  |  |
| 3 | 1.2D + 1W AZI 030 | Yes | Y |  | DL | 1.2 | WLZ | . 866 | WLX | 5 |  |  |  |  |  |  |
| 4 | $1.20+1$ WAZ 060 | Yes | $Y$ |  | DL | 1.2 | WL2 | 5 | WLX | 866 |  |  |  |  |  |  |
| 5 | 1.2D + 1W AZI 090 | Yes | Y |  | DL | 1.2 |  |  | WLX | 1 |  |  |  |  |  |  |
| 6 | $1.20+1 W A Z 120$ | Yes | $Y$ |  | DL. | 1.2 | WLZ | 4.5 | WLX | 866 |  |  |  |  |  |  |
| 7 | 1.2D+1WAZI 150 | Yes | $Y$ |  | DL | 1.2 | WLZ | -. 866 | WLX | . 5 |  |  |  |  |  |  |
| 8 | $120+1 W$ AZ1 180 | Yes | Y |  | DL. | 1.2 | WLZ | 1. |  |  |  |  |  |  |  |  |
| 9 | 1.2D + 1W AZI 210 | Yes | Y |  | DL | 1.2 | WLZ | -. 866 | WLX | -. 5 |  |  |  |  |  |  |
| 10 | $1.20+1 W A Z 240$ | Yes | $Y$ |  | DL. | 12 | WLZ | -5 | WLX | -866 |  |  |  |  |  |  |
| 11 | 1.2D + 1WAZI 270 | Yes | Y |  | DL | 1.2 |  |  | WLX | -1 |  |  |  |  |  |  |
| 12 | 1.20 + 1WAz300 | Yes | $\bigcirc$ |  | DL | 1.2 | WLZ | 5 | WLX | -866 |  |  |  |  |  |  |
| 13 | 1.2D + 1WAZI 330 | Yes | Y |  | DL | 1.2 | WLZ | . 866 | WLX | -. 5 |  |  |  |  |  |  |
| 14 | 0.90 + 1W AZ 000 | Yes. | \% $Y$ |  | DL. | 9 | WLZ | 1 | , |  |  |  |  |  |  |  |
| 15 | 0.9D + 1WAZI 030 | Yes | $Y$ |  | DL. | . 9 | WLZ | . 866 | WLX | 5 |  |  |  |  |  |  |
| 16 | $0.90+1 W$ AZ 1060 | Yes. | $Y$ |  | DL | 9 | WLZ | . 5. | WEX | 866 |  |  |  |  |  |  |
| 17 | 0.9D + 1W AZI 090 | Yes | $Y$ |  | DL | . 9 |  |  | WLX | 1 |  |  |  |  |  |  |
| 18. | 0.90 + 1W AZ 120 | Yes | $Y$ |  | DL | 9 | WLZ | 4.5 | WEX | 866 |  |  |  |  |  |  |
| 19 | $0.9 D+1$ W AZI 150 | Yes | Y |  | DL | . 9 | WLZ | -. 866 | WLX | . 5 |  |  |  |  |  |  |
| 20 | $0.90+1$ W AZI 180 | Yes | $Y$ |  | DL | 9 | WLZ | 1 |  |  | \% |  |  |  |  |  |
| 21 | 0.9D + 1W AZI 210 | Yes | $Y$ |  | DL | . 9 | WLZ | -. 866 | WLX | -. 5 |  |  |  |  |  |  |
| 22. | $0: 9 \mathrm{D}$ + 1 W AZ1 240 | Yes | $Y$ |  | DLI. | . 9 | WLZ | 45 | WLX | -866. |  |  |  |  |  |  |
| 23 | 0.9D + 1W AZI 270 | Yes | Y |  | DL | . 9 |  |  | WLX | -1 |  |  |  |  |  |  |
| 24 | $0.90+1$ W Az1 300 | Yes | ${ }^{*} \mathrm{Y}$ |  | DL. | 9 | WLZ | 5 | WEx | -866. |  | S |  |  |  |  |
| 25 | $0.90+1$ W AZI 330 | Yes | Y |  | DL | . 9 | WLZ | . 866 | WLX | -. 5 |  |  |  |  |  |  |
| 26. | 1.20 +1.0D1, | Yes. | $Y$ |  | DL | 1.2 | OL | $1{ }^{1}$ | , |  |  |  |  |  |  |  |
| 27 | 1.2D + 1.0Di + 1.0Wi AZI ... | Yes | Y |  | DL | 1.2 | OL1 | 1 | OL2 | 1 |  |  |  |  |  |  |
| 28. | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wl}$ Azl. | Yes | V, $\mathbf{Y}$ |  | DL. | 1.2 | OL1 | 1 | OL2 | 866 | OL3 | 5 |  |  |  |  |
| 29 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} \mathrm{AZI} \ldots$ | Yes | Y |  | DL | 1.2 | OL1 | 1 | OL2 | . 5 | OL3. | . 866 |  |  |  |  |
| 30. | $12 \mathrm{~L}+10 \mathrm{Dl}+10 \mathrm{WlAZl}$ | Yes | Y |  | DL | 1.2 | OL1 | 1 |  |  | OL3 | 1 |  |  |  |  |
| 31 | 1.2D + 1.0Di + 1.0Wi AZI ... | Yes | Y |  | DL | 1.2 | OL1 | 1 | OL2 | -. 5 | OL3. | . 866 |  |  |  |  |
| 32 | $112 \mathrm{t}+10 \mathrm{Di}+10 \mathrm{WVAZI}$. | Yes | Y |  | DL | 1.2 | 0 L 1 | 1. | OL2 | -866 | OL3 | 5. |  |  |  |  |
| 33 | 1.2D + 1.0Di + 1.0Wi AZI ... | Yes | Y |  | DL | 1.2 | OL. 1 | 1 | OL2 | -1 |  |  |  |  |  |  |
| 34. | 12,20 + 10Di + 100 WVAZI. | Yes | $Y$ |  | DL. | 1.2 | 0 L 1 | 1 | OL2 | -866 | 013 | -. 5 |  |  |  |  |
| 35 | 1.2D + 1.0Di + 1.0Wi AZI ... | Yes | Y |  | DL | 1.2 | OL1 | 1 | OL2 | -. 5 | OL3 | -.8... |  |  |  |  |
| 36 | $1.2 \mathrm{D}+10 \mathrm{Di}+1$ OWIAZI. | Yes | Y |  | DL. | 1.2 | OL1 | 1. |  | , | OL3 | -1. |  |  |  |  |
| 37 | 1.2D + 1.0Di + 1.0Wi AZI ... | Yes | Y |  | DL | 1.2 | OL-1 | 1 | OL2 | . 5 | OL3 | -.8... |  |  |  |  |
| 38 | 120 +10Di + 10 OVI AZI.. | Yes | $Y$ |  | DL | 1.2 | 014 | 1. | 012 | 866 | 013 | -. 5 |  |  |  | , |

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Checked By:

Load Combinations (Continued)

| Descriotion | Solve | PDelta |  |  | BL | Factor BLC | Factor | C | Fa. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39 1. $1.2 \mathrm{D}+1.5 \mathrm{~L}+1.0 \mathrm{WL}$ ( 30. | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | . 063 |  |  |  |  |  |
| $401.2 \mathrm{~L}+1.5 \mathrm{~L}+1.0 \mathrm{WL}$ ( $30 \ldots$ | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | 054 | WLX. | . 031 |  |  |  |
| $411.2 \mathrm{D}+1.5 \mathrm{~L}+1.0 \mathrm{WL}$ ( 30. | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | 031 | WLX. | . 054 |  |  |  |
| 42 1.2D + 1.5L + 1.0WL (30 ... | Yes | Y | DL | 1.2 | LL | 1.5 |  | WLX. | . 063 |  |  |  |
| $431.2 \mathrm{D}+1.5 \mathrm{~L}+1.0 \mathrm{WL}$ (30... | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | -. 031 | WLX. | . 054 |  |  |  |
| 44-1.2D + 1.5L + 1.0WL (30... | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | -. 054 | WLX. | . 031 |  |  |  |
| $451.2 \mathrm{D}+1.5 \mathrm{~L}+1.0 \mathrm{WL}$ (30... | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | -. 063 |  |  |  |  |  |
| 46. 1.2D + 1.5L + 1.0WL ( $30 \ldots$ | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | -054 | WLX | -0.. |  |  |  |
| 47 1.2D + 1.5L + 1.0WL (30... | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | -. 031 | WLX | -0.. |  |  |  |
| $48 \quad 1.2 \mathrm{D}+1.5 \mathrm{~L}+1.0 \mathrm{WL}$ (30... | Yes | Y | DL | 1.2 | LL | 1.5 |  | WLX |  |  |  |  |
| 49. 1.2D + 1.5L + 1.0WL (30 ... | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | . 031 | WLX |  |  |  |  |
| 50 1.2D +1.5L + 1.0WL ( $30 \ldots$ | Yes | Y | DL | 1.2 | LL | 1.5 WLZ | . 054 | WLX: | -0... |  |  |  |

## Envelope Joint Reactions

|  | Joint |  | [lb] | LC | Y [lb] | LC | Z [lb] | LC | MX [llb-ft] | LC | MY |  | MZ [lb-ft] | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N70A | max | 1446.088 | 17 | 2832.986 | 27 | 2334.686 | 14 | 4774.746 | 27. | 1487.173 | 22 | 1619.4 | 23 |
| 2 |  | min | -1447.012 | 23 | -313.351 | 20 | -2534.16 | 8 | -1413.46 | 20 | -1492.765 | 4 | -1681,626 | 5 |
| 3 | N59 | max | 2598.387 | 5 | 4238.75 | 35 | 2144.874 | 2 | 1634.804 | 14 | 2055.583 | 19 | 6684,343 | 36 |
| 4 |  | min | -2423.055 | 23 | 43.235 | 16 | -2044.382 | 20 | - 4057.065 | 33 | -2063.127 | 13 | -1082.716 | 17 |
| 5 | N1 | max | 1857.793 | 17 | 3187.877 | 31 | 1846.815 | 13 | 1391.727 | 25 | 853,403 | 15 | 1395.027 | 23 |
| 6 |  | min | -2032.471 | 11 | -208.92 | 24 | -1747.961 | 19 | -3532,392 | 32 | -864.788 | 9 | -4528.297 | 30 |
| 7 | N5 | max | 0 | 50 | 0 | 50 | 0 | 50 | 0 | 50 | 0 | 50 | 0 | 50 |
| 8 |  | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1. | 0 | 1 | 0 | 1 |
| 9 | Totals: | max | 5877.406 | 5 | 9302.463 | 29 | 6186.187 | 14 |  |  |  |  |  |  |
| 10 |  | min | -5877.406 | 23 | 2955.775 | 22 | -6186.187 | 8. |  |  |  |  |  | $\cdots$ |

Envelope AISC 14th(360-10): LRFD Steel Code Checks

|  | Member | Shape | Code Check | Loc[in] | LC | Shear. | oc[in] |  |  |  |  | phi*Mn y..p | phi*Mn z...co |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | MP1 | PIPE 2.0 | . 841 | 63 | 8 | 123 | 63 |  | 8 | 20866.7. | 32130 | 1871.625 | 1871.625 |  | -1-1b |
| 2 | MP2 | PIPE 2.0 | 725 | 63 | 8 | 111 | 63 |  | 8. | 20866.7... | 32130. | 1871.625 | 1871:625 |  | H1-1b |
| 3 | MP3 | PIPE 2.0 | . 670 | 63 | 2 | . 048 | 63 |  | 2 | 20866.7... | 32130 | 1871.625 | 1871.6252 |  | H1-1b |
| 4 | MP4 | PIPE 2.0 | . 666 | 63 | 2 | 111 | 63 |  | 2. | 20866.7.. | 32130. | 1871625 | 18716252 |  | Hi-1b |
| 5 | M17A | HSS4X4X4 | . 647 | 0 | 34 | . 278 | 0 | z | 13 | 101755... | 106155 | 12311.25 | 12311.25 | 1 | H1-1b |
| 6 | MP6 | PIPE 20 | 610 | 9 | 8 | 147 | 9 |  | 8 | 20866.7. | 32130 | 1871.625 | 1871.625 |  | H4-16 |
| 7 | MP5 | PIPE 2.0 | . 570 | 63 | 8 | . 154 | 63 |  | 8 | 20866.7... | 32130 | 1871.625 | 1871.625 |  | H1-1b |
| 8 | MP10 | PIPE 2.0 | 544 | 63 | 5 | 065 | 63 |  | 5 | 20866.7. | 32130 | 1871,625 | 1871.625 |  | H1-1b |
| 9 | MP12 | PIPE 2.0 | 475 | 9 | 6 | . 103 | 9 |  | 12 | 20866.7... | 32130 | 1871.625 | 1871.625 |  | H1-1b |
| 10 | MP9 | PIPE 2.0 | 474 | 63 | 5 | 075 | 63 |  | 11 | 20866.7. | 32130 | 1871,625 | 1871.625 | 1. | H1-1b |
| 11 | M1 | HSS4X4X4 | . 464 | 0 | 32 | . 242 | 0 | z | 9 | 101755.... | 106155 | 12311.25 | 12311.25 | 1 | H1-1b |
| 12 | M8. | PIPE 3.0 | .453 | 162.75 | 2 | 550 | 162.75 |  | 8. | 59302:8. | 65205. | 5748.75 | 5748.75 | 1 | H3-6. |
| 13 | MP11 | PIPE 2.0 | . 449 | 63 | 12 | . 107 | 63 |  | 12 | 20866.7.. | 32130 | 1871.625 | 1871.6251 |  | H1-1b |
| 14 | M22 | HSS4X4X4 | 441 | 0 | 3. | 214 | 0 | 2 | 5 | 101755.. | 106155 | 1231125 | 1231125 | 1 | H1-1b |
| 15 | MP8 | PIPE 2.0 | . 429 | 63 | 11 | . 110 | 63 |  | 11 | 20866.7.. | 32130 | 1871.625 | 1871.625 2 |  | -1-1b |
| 16 | MP7 | PIPE 2.0 | 420 | 63. | 12 | 092 | 63 |  | 12 | 208667. | 32130. | 1871.625 | 1871,625 |  | H1-1b |
| 17 | MP16 | PIPE 2.0 | . 388 | 63 | 10 | . 051 | 63 |  | 4 | 20866.7. | 32130 | 1871.625 | 1871.625 |  | H1-1b |
| 18 | MP15 | PIPE 2.0 | . 375 | 63 | 6 | 061 | 63 |  | 6. | 20866.7. | 32130. | 1871.625 | 1871.625 | 2. | H1-1b |
| 19 | M14 | PIPE 3.0 | . 346 | 5.25 | 7 | . 364 | 5.25 |  | 12 | 59302.8. | 65205 | 5748.75 | 5748.75 |  | H3-6 |
| 20 | MP13 | PIPE 2.0 | 340 | 63 | 10 | 060 | 63 |  | 5. | 20866.7. | 32130 | 1871.625 | 1871.625 |  | H1-16 |
| 21 | MP17 | PIPE 2.0 | . 340 | 63 | 5 | . 092 | 63 |  | 4 | 20866.7.. | 32130 | 1871.625 | 1871.625 |  | H1-1b |
| 22 | M19B | HSS $4 \times 4 \times 4$ | 337 | 30.657 | 36 | 193 | 61.314 | $z$ | 13 | 103885... | 106155 | 12311.25 | 12311.25 | 1. | H1-1b |
| 23 | MP18 | PIPE 2.0 | 336 | 9 | 4 | . 081 | 9 |  | 4 | 20866.7... | 32130 | 1871.625 | 1871.625 |  | H1-1b |
| 24 | MP14 | PIPE 2.0 | 306 | 63 | 4 | . 061 | 63. |  | 5 | 208667. | 32130 | 1871.625 | 1871.625 | 1 | $\mathrm{H} 1-1 \mathrm{~b}$ |
| 25 | M11 | HSS4X4X4 | 287 | 30.657 | 32 | . 203 | 3.832 | z | 2 | 103885.... | 106155 | 12311.25 | 12311.25 | 1 | H1-1b |
| 26 | M18A | PIPE 2.0 | 256 | 56 | 10 | 119 | 54:25 |  | 5 | 25978.8... | 32130 | 1871.625 | 1871.625 | 1 | H1-16 |

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## Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)



## Hot Rolled Steel Section Sets

| Label |  | Shape | Type | Design List | Material | Design | A [in2 | Iyy [in4] Izz [in4] |  | $\frac{J[\operatorname{in} 4]}{100}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | HSS 4"x4"x1/4" | HSS4X4X4 | Beam | None | A53 Gr.B | Typical | 3.37 | 7.8 | 7.8 |  |
| 2 | $3^{\prime \prime}$ STD Pjpe | PIPE. 3.0 | Beam | None | A53 GriB | Typical | 2.07 | 2.85 | 2.85 | 5.69 |
| 3 | L2'x2"x3/16 | $12 \times 2 \times 3$ | Beam | None | A36 Gr. 36 | Typical | . 722 | . 271 | 271 | 009 |
| 4 | 2375" ODP ${ }^{\text {P/m }}$ | PIPE 20 | Beam | None | A53 Grib | Typical | 1.02 | 627 | . 627 | 1.25 |
| 5 | L2.5X2.5X3 | L2.5×2.5×3 | Beam | None | A36 Gr. 36 | Typical | . 901 | . 535 | . 535 | 011 |

Joint Boundary Conditions

| Joint Label |  | $\mathrm{X}[\mathrm{k} / \mathrm{in}]$ | Y [k/in] | Z [k/in] | X Rot.[k-ft/rad] | Y Rot.[k-ft/rad] | Z Rot.[k-ft/rad] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N5 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 2 | - $\mathrm{N}_{1}$ - | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 3 | N59 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 4 | N70A | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |

## Member Advanced Data

|  | Label | 1 Release. | $J$ Release | 1 Offsetiin] | J Offset[in] | T/C Only | Physical | Defl Rat.... | Analysis. | Inactive | Seismic.. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 |  |  |  |  |  | Yes |  |  |  | None |
| 2 | M2 | - | , | $\cdots$ | \% | 3, +3. | Yes | ** NA** | . ${ }^{2}$ | \% | None |
| 3 | M8 |  |  |  |  |  | Yes |  |  |  | None |
| 4 | M11 | BenPIN | BenPIN | $\cdots$ | $\cdots$ | W, | Yes | \% $\quad$, | \% | , | None. |
| 5 | M18 |  |  |  |  |  | Yes |  |  |  | None |
| 6 | M29 |  | \%...* | , | 줏․․․ | $\cdots$ | Yes | 4v, | , ${ }^{\text {a }}$ |  | None |
| 7 | M14 |  |  |  |  |  | Yes |  |  |  | None |
| 8 | M18A | , | H\% \% ${ }^{\text {a }}$ | \% | - | \% \% ${ }^{\text {a }}$, | Yes | - | , |  | None |
| 9 | M19 |  |  |  |  |  | Yes |  |  |  | None |
| 10 | M23. | , | $3 \times$ | $\cdots$ |  | $\stackrel{ }{4}$ | Yes | , | - | \% , | None. |
| 11 | MP6 |  |  |  |  |  | Yes |  |  |  | None |
| 12. | MP5 | , \% ${ }^{2}$, |  | W, | 1, | 2, \% | Yes | 4, | 4, | , , , + , | None. |
| 13 | MP4 |  |  |  |  |  | Yes |  |  |  | None |
| 14 | MP2 | , $\square^{\text {a }}$, | 1, ${ }^{1}$ | \%, \% | \%. | \% ${ }^{\text {a }}$ | Yes | , ${ }^{+}$, | a |  | None. |
| 15 | MP1 |  |  |  |  |  | Yes |  |  |  | None |
| 16 | M20 | 5, ${ }^{\text {a }}$ | \% ${ }^{\text {a }}$ | , |  | \% $\quad$. | Yes |  | * |  | None |
| 17 | M17A |  |  |  |  |  | Yes |  |  |  | None |
| 18 | M18C. | 4\% |  | - |  | \% | Yes. | **NA ** |  |  | None. |
| 19 | M19B | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |
| 20 | M20A | , ${ }^{\text {a }}$, | Qr.as | , | , ${ }^{\text {a }}$ | $\cdots$ | Yes | 2. | , \% |  | None. |
| 21 | M21 |  |  |  |  |  | Yes |  |  |  | None |
| 22 | N22. | \%\% | W, \% ${ }^{\text {a }}$ | . 9 | $\bigcirc \times$ | , | Yes. | $\cdots$ | - | $\cdots \times$ | None |
| 23 | M23A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 24. | M24 | BenPIN | BenPIN | \% ${ }^{2}$ | $\cdots$ | \% | Yes | 1, \% ${ }^{\text {a }}$ | , \% | - ${ }^{2}$, | None |

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Member Advanced Data (Continued)

|  | Label | 1 Release | $J$ Release | 1 Offset[in] | J Offset[in] | T/C Only | Physical | Defl Rat. | Analysis ... | Inactive | Seismic. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | M25 |  |  |  |  |  | Yes |  |  |  | None |
| 26 | M26 |  |  |  |  |  | Yes |  |  |  | None |
| 27 | MP3 |  |  |  |  |  | Yes |  |  |  | None |
| 28 | MP12 |  |  |  |  |  | Yes |  |  |  | None |
| 29 | MP11 |  |  |  |  |  | Yes |  |  |  | None |
| 30 | MP10 | \% |  |  |  |  | Yes |  |  | $\cdots$ | None |
| 31 | MP8 |  |  |  |  |  | Yes |  |  |  | None |
| 32 | MP7 | * | $\cdots$ |  |  |  | Yes | … | $\square$ | , | None |
| 33 | MP9 |  |  | . |  |  | Yes |  |  |  | None |
| 34 | MP18 |  |  |  |  | $\ldots$ | Yes |  | \% | ? | None |
| 35 | MP17 |  |  |  |  |  | Yes |  |  |  | None |
| 36 | MP16 | \% | , |  |  |  | Yes | , |  |  | None |
| 37 | MP14 |  |  |  |  |  | Yes |  |  |  | None |
| 38 | MP13 | \% | \% | \% |  |  | Yes | $\bigcirc$ | \% | $\cdots$ | None |
| 39 | MP15 |  |  |  | , |  | Yes |  |  |  | None |

## Hot Rolled Steel Properties

| Label |  | E[ksi] | G [ksi] | Nu | Therm (11E...Density[k/ft... Yieldipsi] |  |  | Ry | Fu[psi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A992 | 29000 | 11154 | . 3 | . 65 | 49 | 50000 | 1.1 | 65000 | 1.1 |
| 2 | A36 Gr. 36 | 29000 | 11164 | 1.3 | . 65 | 49 | 36000 | 1.5 | 58000 | 1.2 |
| 3 | A572 Gr. 50 | 29000 | 11154 | . 3 | . 65 | 49 | 50000 | 1.1 | 65000 | 1.1 |
| 4 | A500 Gri R R D | 29000 | 11154 | . 3 | . 65 | . 527 | 42000 | 1.4 | 58000 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | . 3 | . 65 | . 527 | 46000 | 1.4 | 58000 | 1.3 |
| 6. | A53 Gr.B | 29000 | 11154 | - 3 | . 65 | - 4.49 | 35000 | 1.6 | 60000 | 1.2 |
| 7 | A1085 | 29000 | 11154 | . 3 | 65 | . 49 | 50000 | 1.4 | 65000 | 1.3 |

Joint Loads and Enforced Displacements (BLC 7 : Service Live 1)

| Joint Label |  | L.D.M | Direction | Magnitude[(lb, lb-ff), (in, rad). (lb* ${ }^{\wedge} s^{\wedge} 2 .$. |
| :---: | :---: | :---: | :---: | :---: |
| 1 | N19 | L | Y | -250 |
| 2 | , ${ }^{\text {a }}$ N18, | , L , , |  | , -250 . |
| 3 | N55 | L | Y | -250 |
| 4 | M, N56. | L, | , Y, | 2020, \% , , |
| 5 | N66 | L | Y | -250 |
| 6 | , ${ }^{\text {a }}$, 67 . | \}.L L | , ${ }^{\text {a }}$ Y | -250, |
| 7 | N126A | L | Y | -250 |
| 8 | N, N128A , , | L | , , Y, | , 250 |
| 9 | N130 | L | Y | -250 |

Member Point Loads (BLC 1 : Self Weight)

|  | Member Label | Direction | Magnitude [lb, 1 lb -ft] | Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | MP1 | Y | -14.35 | 24 |
| 2 | , M, MP3, | $Y$ | \% - -20.95 | $\cdots$, 0 |
| 3 | MP5 | Y | -41.9 | 13 |
| 4. | , MP4 | , | , 4, 48.8 | M, \% 0 |
| 5. | MP2 | Y | -17.5 | 17 |
| 6. | MP4 | Y | \% ${ }^{42.9}$ | , \% 26 , , \% |
| 7 | MP4 | Y | -71 | 26 |
| 8. | MP5 , , , | , , , Y Y | -59.9 | 26 |
| 9 | MP1 | Y | -72 | 26 |
| 10 | M MP2, | - Y , | -28.2 | 26 |
| 11 | MP3 | Y | -32.8 | 26 |
| 12 | MP1. . | V, $Y$ Y , | 4, 14.35 | 72 |

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Member Point Loads (BLC 1 : Self Weight) (Continued)

| Member Label |  | Direction | Magnitude[lb. lb -ft] | Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 13 | MP3 | Y | -20.95 | 72 |
| 14 | MP5 | Y | -41.9 | 72 |
| 15 | MP4 | Y | -48.8 | 72 |
| 16 | MP2 | $Y$ | -17.5 | 72 |
| 17 | MP9 | Y | -20.95 | 0 |
| 18 | MP11 | $Y$ | -41.9 | 13 |
| 19 | MP10 | Y | -48.8 | 0 |
| 20 | MP8 | $Y$ | \% 17.5 | 17 |
| 21 | MP10 | $Y$ | -42.9 | 26 |
| 22 | MP10 | $Y$ | -71 | 26 |
| 23 | MP11 | Y | -59.9 | 26 |
| 24 | MP7 | $Y$ | -72 | 26 |
| 25 | MP8 | $Y$ | -28.2 | 26 |
| 26. | MP9 | \% $Y$ | -32.8 | 26 26 |
| 27 | MP9 | Y | -20.95 | 72 |
| 28. | MP11 | Y | \% 41.9 | +72 |
| 29 | MP10 | Y | -48.8 | 72 |
| 30 | MP8 , , ${ }^{\text {a }}$ | $\bigcirc$ | -17.5 | \% 72 , |
| 31 | MP16 | Y | -48.8 | 0 |
| 32 | , M MP14 | Y , | - $\quad 17.5$ | S", 17\%, |
| 33 | MP16 | Y | -42.9 | 26 |
| 34 | M, MP16, , | Y $\mathrm{Y}^{\text {a }}$ |  | 26 . |
| 35 | MP17 | Y | -59.9 | 26 |
| 36 | , MP13 \% | $\bigcirc$ | \% 42. | - 26 |
| 37 | MP14 | $Y$ | -28.2 | 26 |
| 38 | , MP15, , , | Y | -32.8 | 26 |
| 39 | MP16 | $Y$ | -48.8 | 72 |
| 40 | W, MP14 ${ }^{\text {a }}$, | - $\mathrm{Y}^{\text {a }}$ | 3, | \% 72 , |
| 41 | MP2 | Y | -48.8 | 0 |
| 42 | \%- , MP2, | Y | , 48.8\% |  |

Member Point Loads (BLC 2 : Wind Load AZI 000)

|  | Member Label | Direction | Magnitude [lb, lb -ft] | Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | MP1 | Z | -92.99 | 24 |
| 2 | 4, MP3, | , , \% | -147.24 | O, 0, \% |
| 3 | MP5 | Z | -187.5 | 13 |
| 4 | , MP4 , , | , Z | , -259.08 | $\cdots \quad 0$. |
| 5 | MP2 | Z | -103.31 | 17 |
| 6 | W, MP4 , |  | , x. -64.63 | , 26. |
| 7 | MP4 | Z | -73.8 | 26 |
| 8 | , MP5, - , | Z | , \% - $69.11{ }^{\text {a }}$, | , 26. |
| 9 | MP1 | Z | -61.48 | 26 |
| 10. | , M MR2 \% |  | T, \% $\quad .82 .82$ | , \% 26 , |
| 11 | MP3 | Z | -45.45 | 26 |
| 12 | , MP1 , | , Z | - $\times \mathbf{- 9 2 . 9 9}$ | \% 72 \% |
| 13 | MP3 | Z | -147.24 | 72 |
| 14 | , MP5 , M, | , \%, \% | , -187.5... | \%- 72 , |
| 15 | MP4 | Z | -259.08 | 72 |
| 16 | , MP2 | , \% ${ }^{\text {2, }}$, | TY, 4103.31 | \% 72, |
| 17 | MP9 | Z | -114.85 | 0 |
| 18. | Ma, MP11, | , \% Z | .2. -104.61. | \% 13 |
| 19 | MP10 | Z | -109.41 | 0 |
| 20 | , ${ }^{\text {a }}$ MP8 | \%, Z, | , - $\mathrm{M}^{27.02 .2}$ | 17. |
| 21 | MP10 | Z | -33.39 | 26 |
| 22. | MP10, | , Z | , -58.07, , , | , 26, \% |
| 23 | MP11 | Z | -47.06 | 26 |

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Member Point Loads (BLC 2 : Wind Load AZI 000) (Continued)


## Member Point Loads (BLC 3; Wind Load AZI 090)

| Member Label |  | Direction | Magnitude [lb, 1 lb -ft] | Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | MP1 | X | -65.07 | 24 |
| 2 | - MP3 | $X$ | -104.06 | 0 |
| 3 | MP5 | X | -76.97 | 13 |
| 4 | MP4 | - ${ }^{\text {x }}$ | -109.41 | 0 |
| 5 | MP2 | X | -54.92 | 17 |
| 6 | MP4 | X | - 23.98 | 26 |
| 7 | MP4 | X | -52.82 | 26 |
| 8 | \% MP5 , , \% | - ${ }^{\text {P }}$ | , +39,7.1 | 26 |
| 9 | MP1 | X | -50.77 | 26 |
| 10 | , M MP2, , | X , | , \% 26.04 | + 26 |
| 11 | MP3 | X | -45.45 | 26 |
| 12 | , , MP9. ${ }^{\text {a }}$, | , $\mathrm{X}^{\text {a }}$, | , 6 - 65.07 | W, ${ }^{2}$ |
| 13 | MP3 | X | -104.06 | 72 |
| 14 | , MP5 , , , , | $\cdots$ | , प $\quad-76.97$. | 1\% +772 |
| 15 | MP4 | X | -109.41 | 72 |
| 16 | , \%, MP2 , | , $\quad$ X | -54.92 , | $\cdots 72$ |
| 17 | MP9 | X | -136.45 | 0 |
| 18 | N, MP11. | X | , -159,87, , , | - 13 |
| 19 | MP10 | X | -259.08 | 0 |
| 20 | , , MP8., , \% | , $\boldsymbol{X}$, | , -91.22, | , , 17. ${ }^{\text {a }}$, , , |
| 21 | MP10 | X | -52.22 | 26 |
| 22 | , , MP10, , , , | X | -68.56 , , | , \% 26. |
| 23 | MP11 | X | -61.76 | 26 |
| 24 | , \% M MP7. | X | $\cdots 58.8$ | , 26. |
| 25 | MP8 | X | -68.63 | 26 |
| 26. | MP'9 | X | , 45.45 | 4, \% 26 |
| 27 | MP9 | X | -136.45 | 72 |
| 28 | , MP11 | W, X, | - 1159.87 | , 72 |
| 29 | MP10 | X | -259.08 | 72 |
| 30 | , MP8 | X, | , \% 91.22. | $\square \quad 72$ |
| 31 | MP16 | X | -259.08 | 0 |
| 32 | , MP14, , , | X | . 91.22 | - 17 |
| 33 | MP16 | X | -52.22 | 26 |
| 34 | MP16., , , | L, X | \% - 68.56 , | 26. $\quad$, |

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## Member Point Loads (BLC 3 : Wind Load AZI 090) (Continued)



## Member Point Loads (BLC 4 : Ice Weight)

|  | Member Label | Direction | Magnitude[lb, lb -fi] | Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | MP1 | Y | -58.72 | 24 |
| 2 | MP3. | $Y$ | -83.41 | 0 |
| 3 | MP5 | $Y$ | -95.44 | 13 |
| 4 | MP4 | Y | -123.67 | 0 |
| 5 | MP2 | $Y$ | -55.4 | 17 |
| 6 | MP4 | $Y$ | -42.82 | 26 |
| 7 | MP4 | $Y$ | -63.21 | 26 |
| 8 | MP5 | - Y | - -54.86 | - 26 |
| 9 | MP1 | Y | -60.22 | 26 |
| 10 | MP2 | $Y$ | $\square \quad-53.8$ | 26. |
| 11 | MP3 | Y | -73.51 | 26 |
| 12 | , \% MP1, \%, | \%, $\mathbf{Y}$, | -58.72 | 72 |
| 13 | MP3 | Y | -83.41 | 72 |
| 14 | MP5 , \% | $\bigcirc$ | $\square \quad-95.44$ | 4, 72 |
| 15 | MP4 | Y | -123.67 | 72 |
| 16 | MP2 | Y , , | $\cdots \quad 55.4$ | 72 |
| 17 | MP9 | Y | -83.41 | 0 |
| 18 | \%, MP11, , , | , Y | 9. 95.44 , | $\square 13$ |
| 19 | MP10 | Y | -123.67 | 0 |
| 20 | - , MP8 | , Y , | , $\quad$-55.4...... | W, \% 17. |
| 21 | MP10 | $Y$ | -42.82 | 26 |
| 22 | , MP10, | M, Y, Y, |  | , 26 |
| 23 | MP11 | Y | -54.86 | 26 |
| 24 | , MP7, $\mathrm{Ma}^{\text {ar }}$ | , $\mathbf{Y}$, | , -60.22 , | , 26. |
| 25 | MP8 | Y | -53.8 | 26 |
| 26 | , MP9. $\quad$, |  | +, -73.51 , | , 26 , |
| 27 | MP9 | Y | -83.41 | 72 |
| 28 | , \% MP11 | , Y, Y , | , 9.9544 | $\bigcirc \quad 72$ |
| 29 | MP10 | $Y$ | -123.67 | 72 |
| 30. | * M M ${ }^{\text {a }}$ | , Y Y , | , $\quad$ 55.4, \% | , 72, |
| 31 | MP16 | $Y$ | -123.67 | 0 |
| 32 | M, MP14.4. , , , | , <, Y | \% - 5 55.4 \% | 12 17 \% |
| 33 | MP16 | Y | -42.82 | 26 |
| 34 | M MP16, , , , , | , $\boldsymbol{Y}$ |  | , 26 |
| 35 | MP17 | Y | -54.86 | 26 |
| 36. | , , MP13. $\quad$, | $\square$ | -60.22 | \% $\quad 26$ |
| 37 | MP14 | Y | -53.8 | 26 |
| 38 | M MP15 | M $Y$ | , 73.51 , ${ }^{\text {a }}$ | W, 26 |
| 39 | MP16 | $Y$ | -123.67 | 72 |
| 40 | \% MP14, \% ${ }^{\text {a }}$, | Y | \%\% - 55.4 | - 72 |
| 41 | MP2 | Y | -123.67 | 0 |
| 42 | , M M ${ }^{\text {a }}$, | Y | - $\quad 123.67$ | $\square 72$ |

## Member Point Loads (BLC 5: Wind + Ice Load AZI 000)

Member Point Loads (BLC. 5 : Wind + Ice Load AZI 000). (Continued)


Member Point Loads (BLC 6 : Wind + Ice Load AZI 090)

|  | Member Label | Direction | Magnitude [lb. $\mathrm{lb}-\mathrm{ft}]$ | Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | MP1 | X | -15.86 | 24 |
| 2 | \%\% MP3 | X | -24.77 | 0 |
| 3 | MP5 | X | -18.9 | 13 |
| 4 | MP4 | X | -26.27 | 0 |
| 5 | MP2 | X | -14.71 | 17 |
| 6 | MP4 | $X$ | 778 | 26 |
| 7 | MP4 | X | -14.04 | 26 |
| 8 | MP5 | X | - 11.26 | 26 $\times \quad 26$ |
| 9 | MP1 | X | -13.44 | 26 |
| 10 | MP2 | X | -10.72 | 26 |
| 11 | MP3 | X | -15.12 | 26 |

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Member Point Loads.(BLC 6: Wind + Ice Load AZI 090) (Continued)

|  | Member Label | Direction | Magnitude[ll. lb -ftl | Location ${ }^{\text {in. \% }}$ \% |
| :---: | :---: | :---: | :---: | :---: |
| 12 | MP1 | X | -15.86 | 72 |
| 13 | MP3 | X | -24.77 | 72 |
| 14 | MP5 | X | -18.9 | 72 |
| 15 | MP4 | X | -26.27 | 72 |
| 16 | MP2 | X | -14.71 | 72 |
| 17 | MP9 | X | -30.38 | 0 |
| 18 | MP11 | X | -33.89 | 13 |
| 19 | MP10 | X | -52.87 | 0 |
| 20 | MP8 | X | -21,15 | 17 |
| 21 | MP10 | X | -13.72 | 26 |
| 22 | MP10 | X | -17.23 | 26 |
| 23 | MP11 | X | -15.78 | 26 |
| 24 | MP7 | X | -15.11 | 26 |
| 25 | MP8 | X | -19.87 | 26 |
| 26 | MP9 | X | -23.22 | 26 |
| 27 | MP9 | X | -30.38 | 72 |
| 28 | MP11 | X | -33.89 | 72 |
| 29 | MP10 | X | -52.87 | 72 |
| 30 | MP8 | $X$ | -21,15 | $\bigcirc 72$ |
| 31 | MP16 | X | -52.87 | 0 |
| 32 | MP14, | X | -21.15 | 17 |
| 33 | MP16 | X | -13.72 | 26 |
| 34 | MP16 | X | -17.23 | 26 |
| 35 | MP17 | X | -15.78 | 26 |
| 36 | MP13 | X | -15.11 | 26 |
| 37 | MP14 | X | -19,87 | 26 |
| 38 | MP15 | $X$ | -23.22 | 26 |
| 39 | MP16 | $X$ | -52.87 | 72 |
| 40 | MP14, | X | , <-21.15 | 72 |
| 41 | MP2 | $X$ | -26.27 | 0 |
| 42 | MP2 | $X$, | -26.27 | 72 |

## Member Distributed Loads (BLC 4 : Ice Weight)

|  | Member Label | Direction | Start Magnitude[lb/ft.F.psf] | End Magnitude[lb/f. | Start Location[in.\%] | End Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Y | -12.628 | -12.628 | 0 | \%100 |
| 2 | M2 | $Y$ | -3.412 | -3.412 | 0 . | \%100 |
| 3 | M8 | Y | -9.013 | -9.013 | 0 | \%100 |
| 4 | M11. | Y | -12.628 | -12.628 | 0 | $\% 100$ |
| 5 | M18 | Y | -8.02 | -8.02 | 0 | \%100 |
| 6. | M29 | ¢ Y | -7.023 | -7.023 | 0 | $\% 100$ |
| 7 | M14 | Y | -9.013 | -9.013 | 0 | \%100 |
| 8. | M18A | Q Y | -7.023 | - 4.023 | $\bigcirc$ | \% $\% 100$ |
| 9 | M19 | Y | -9.013 | -9.013 | 0 | \%100 |
| 10 | M23 | Y Y | - $\quad 7.023$ | -7.023 | 0 | $\% 100$ |
| 11 | MP6 | Y | -7.023 | -7.023 | 0 | \%100 |
| 12 | MP5 | Y, | -7.023 | 7.023 | 0 | \% \%100 |
| 13 | MP4 | $Y$ | -7.023 | -7.023 | 0 | \%100 |
| 14. | MP2 | Y | -7.023 | -7.023 | 0 | \%100 |
| 15 | MP1 | Y | -7.023 | -7.023 | 0 | \%100 |
| 16 | M20 | $Y$ | -8.02 | -8.02 | 0 | $\% 100$ |
| 17 | M17A | $Y$ | -12.628 | -12.628 | 0 | \%100 |
| 18 | M18C | Y | -3.412 | -3.412 | 0 | \%100 |
| 19 | M19B | $Y$ | -12.628 | -12.628 | 0 | \%100 |
| 20 | M20A | $Y$ | -8.02 | -8.02 | - 0 | \%100 |
| 21 | M21 | Y | -8.02 | -8.02 | 0 | \%100 |

Company
Designer
Job Number
Infinigy
Dec 26, 2018

Model Name
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Member Distributed Loads (BLC 4 : Ice Weight) (Continued)


Member Distributed Loads (BLC 8: BLC 1 Transient Area Loads)


Company
Designer Job Number

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Dec 26, 2018
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Member Distributed Loads (BLC 8: BLC 1 Transient Area Loads) (Continued)

|  | Member Label | Direction | Start Magnitude[Ib/ft.F.psfl | End Maanitude[ll/f. | Start Locationfin. \% | End Location[in.\%I |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 36 | M25 | Y | -. 786 | -3.239 | 0 | 10.104 |
| 37 | M25 | Y | -3.239 | -4.227 | 10.104 | 20.208 |
| 38 | M25 | Y | -4.227 | -6.191 | 20.208 | 30.312 |
| 39 | M25 | Y | -6.191 | -8.579 | 30.312 | 40.416 |
| 40 | M25 | Y | -8.579 | -8.951 | 40.416 | 50.52 |
| 41 | M26 | Y | -. 785 | -3.242 | 0 | 10.104 |
| 42 | M26 | $Y$ | -3.242 | -4.231 | 10.104 | 20.208 |
| 43 | M26 | $Y$ | -4.231 | -6.195 | 20.208 | 30.312 |
| 44. | M26 | $Y$ | -6.195 | -8.581 | 30.312 | 40.416 |
| 45 | M26 | Y | -8.581 | -8.945 | 40.416 | 50.52 |

## Member Distributed Loads (BLC 9 : BLC 2 Transient Area Loads)

|  | Member Label | Direction | Start Magnitude[lb/ft.F.psf] | End Magnitude[lb/f. | Start Location[in, | End Locationfin.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | -12.993 | -12.993 | 0 | 62.25 |
| 2 | M2 | Z | 0 | 0 | 0 | 10,794 |
| 3 | M8 | Z | -13.128 | -13.128 | 0 | 168 |
| 4 | M11 | \% Z | -7.502 | -7.502 | 0 | 61.314 |
| 5 | M18 | Z | -7.502 | -7.502 | 0 | 50.52 |
| 6 | M29 | Z | - -8.908 | - 8.8 .908 | 0 | 168 |
| 7 | M14 | Z | -6,564 | -6.564 | 0 | 168 |
| 8 | M18A | Z | -4,454 | - 4.454 | 0 | 168 |
| 9 | M19 | Z | -6.564 | -6.564 | 0 | 168 |
| 10 | M23 | Z | -4.454 | -4,454 | 0 | 168 |
| 11 | MP6 | Z | -8.908 | -8.908 | 0 | 72 |
| 12 | MP5 | \% Z | -8,908 | -8.908 | 0 | 72 |
| 13 | MP4 | Z | -8.908 | -8.908 | 0 | 72 |
| 14 | MP2 | Z | -8.908 | -8.908 | 0 | - 72 |
| 15 | MP1 | Z | -8.908 | -8.908 | 0 | 72 |
| 16 | M20 | 2 | -3,751 \% | -3.751 | 0 | 50.52 |
| 17 | M17A | $Z$ | -12.993 | -12.993 | 0 | 62.25 |
| 18 | M18C | 2 | 0 - | - 0 | $\bigcirc 0$ | 10.794 |
| 19 | M19B | Z | -7.502 | -7.502 | 0 | 61.314 |
| 20 | M20A | Z | -3.751 | -3.751 | - 0 | \% 50.52 |
| 21 | M21 | Z | -7.502 | -7.502 | 0 | 50.52 |
| 22 | M23A | Z | 0 | 0. | 0 | 10.794 |
| 23 | M24 | Z | -15.003 | -15.003 | 0 | 61.314 |
| 24 | M ${ }^{\text {M25 }}$ | Z | -3.751 | -3.751 | 0 | 50.52 |
| 25 | M26 | Z | -3.751 | -3.751 | 0 | 50.52 |
| 26. | MP3 | Z | -8.908 | - 8.8 .908 | 0 . | 72 |
| 27 | MP12 | Z | -8.908 | -8.908 | 0 | 72 |
| 28 | MP11, | 2 | -8.908 | - 8.8 .908 | 0 , | -72 |
| 29 | MP10 | Z | -8.908 | -8.908 | 0 | 72 |
| 30 | MP8 | 2 | -8.908. | - -8.908 | 0 - | 72, |
| 31 | MP7 | Z | -8.908 | -8.908 | 0 | 72 |
| 32 | MP9 | Z | -8.908 | -8.908 | 0 | 72 |
| 33 | MP18 | Z | -8.908 | -8.908 | 0 | 72 |
| 34 | MP17 | Z | -8.908 | -8.908 | 0 | . 72 |
| 35 | MP16 | Z | -8.908 | -8.908 | 0 | 72 |
| 36. | MP14 | 2 | -8.908 | -8.908 | 0 | 72 |
| 37 | MP13 | Z | -8.908 | -8.908 | 0 | 72 |
| 38 | MP15 | - Z | -8.908 | -8.908 | 0 | - 72 |

## Member Distributed Loads (BLC 10 : BLC 3 Transient Area Loads)

|  | Member Label | Direction | Start Magnitude[lb/ft.F.psf] | End Magnitudelib/f.. | Start Location[in, \%] | End Location[in. \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | X | -7.502 | -7.502 | 0 | 62.25 |
| 2 | M2 | X | 0 | 0 | 0 | 10.794 - |

Company
Designer
Job Number
Model Name

Infinigy
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600-003
823530

Dec 26, 2018
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Member Distributed Loads (BLC 10: BLC 3 Transient Area Loads) (Continued)

|  | Member Label | Direction | Start Magnitude[li/ff.F.psf] | End Magnitudelliff. | Start Location[in. \% | End Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | M11 | X | -12.993 | -12.993 | 0 | 61.314 |
| 4 | M14 | X | -11.369 | -11.369 | 0 | 168 |
| 5 | M18A | X | -7.715 | -7.715 | 0 | 168 |
| 6 | M19 | X | -11.369 | -11.369 | 0 | 168 |
| 7 | M23 | $X$ | -7.715 | -7.715 | 0 | 168 |
| 8 | MP6 | X | -8.908 | -8.908 | 0 | 72 |
| 9 | MP5 | X | -8.908 | -8.908 | 0 | 72 |
| 10 | MP4 | X | -8.908 | -8.908 | 0 | 72 |
| 11 | MP2 | X | -8.908 | -8.908 | 0 | 72 |
| 12 | MP1 | X | -8.908 | -8.908 | 0 | 72 |
| 13 | M20 | X | -6.497 | -6.497 | 0 | 50.52 |
| 14. | M17A | X | -7.502 | -7.502 | 0 | 62.25 |
| 15 | M18C | X | 0 | 0 | 0 | 10.794 |
| 16 | M19B | X | -12.993 | -12993 | \% | 61.314 |
| 17 | M20A | X | -6.497 | -6.497 | 0 | 50.52 |
| 18 | M22 | $X$ | -15.003 | -15.003 | 0 | 62.25 |
| 19 | M25 | X | -6,497 | -6.497 | 0 | 50.52 |
| 20 | M26 | X | -6.497 | - 6.497 | 0 | 50.52 |
| 21 | MP3 | X | -8.908 | -8.908 | 0 | 72 |
| 22 | MP12 | , X . | -8.908 | 8.908 | - 0 | 72 , |
| 23 | MP11 | X | -8,908 | -8.908 | 0 | 72 |
| 24 | MP10 | $X$ | -8.908 | -8.908 | 0 | - 72 |
| 25 | MP8 | $X$ | -8.908 | -8.908 | 0 | 72 |
| 26 | MP7. | X | -8.908 | -8.908 | $0 \times$ | \% 72 |
| 27 | MP9 | X | -8.908 | -8.908 | 0 | 72 |
| 28. | MP18, | X | - $\quad$-8,908 | -8.908 | 0 | + 72 |
| 29 | MP17 | X | -8.908 | -8.908 | 0 | 72 |
| 30 | MP16 | X | -8.908 , | -8,908 | 0 | 72, |
| 31 | MP14 | X | -8.908 | -8.908 | 0 | 72 |
| 32 | MP13 | , X, | . 8.8 .908 | - 8,908 | 0 | $\begin{array}{r}72 \\ \hline 72\end{array}$ |
| 33 | MP15 | X | -8.908 | -8.908 | 0 | 72 |

## Member Distributed Loads (BLC 11 : BLC 4 Transient Area Loads)

|  | Member Label | Direction | Start Magnitude[lb/ft.E.psf] | End Magnitude [lb/f... | n[in,\%] | nd Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Y | -. 03 | -5.011 | 12.45 | 22.41 |
| 2 | M1 , | , Y | -5.011 | -7,7,59 | 22.41 | 32.37 |
| 3 | M1 | Y | -7.594 | -3.658 | 32.37 | 42.33 |
| 4 | M1 | \% Y | -3.658 | 4,82 | 42.33 | 52.29 |
| 5 | M1 | Y | -1.82 | -1.216 | 52.29 | 62.25 |
| 6 | M18. | , ${ }^{\top}$ | -282 | -1.163 | 0 | 10104 |
| 7 | M18 | Y | -1.163 | -1.518 | 10.104 | 20.208 |
| 8. | M118 | - Y | -1.518 | - 2.223 | 20.208 | 30.312 |
| 9 | M18 | Y | -2.223 | -3.08 | 30.312 | 40.416 |
| 10 | M18 | , Y | W, $\quad .3 .08$ | , 3.214 | 40,416 | 50.52 |
| 11 | M20 | Y | -. 282 | -1.164 | 0 | 10.104 |
| 12 | M20. | , Y | -1164 | -1.519 | 10.104 | 20.208 |
| 13 | M20 | Y | -1.519 | -2.224 | 20.208 | 30.312 |
| 14 | M20 | Y | , \% - - 2.224 | -3.081 | 30.312 | 40.416 |
| 15 | M20 | Y | -3.081 | -3.211 | 40.416 | 50.52 |
| 16. | M17A | \% Y | 1.806 | - 97706 | 12.45 | 22.41 |
| 17 | M17A | Y | -9.706 | -13.298 | 22.41 | 32.37 |
| 18 | M17A. | \% Y | , -13.298 | 4.916 | - 32.37 | 42.33 |
| 19 | M17A | Y | -7.916 | -4.296 | 42.33 | 52.29 |
| 20. | M17A | - Y | - $\quad 4.4296$ | - 2.124 | 52.29 | 62.25 |
| 21 | M20A | $Y$ | -. 789 | -2.404 | 0 | 10.104 |
| 22 | M20A | Y | -2.404 | -3.341 | 10.104 | 20.208 |

$\qquad$

Member Distributed Loads (BLC 11 : BLC 4 Transient Area Loads) (Continued).

|  | Member Label | Direction | Start Magnitude[lb/ft.F.psf] | End Magnitude[Ib/f. | Start Location[in.\%] | End Location[in, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 23 | M20A | Y | -3.341 | - 4.66 | 20.208 | 30.312 |
| 24 | M20A | Y | -4.66 | -6.272 | 30.312 | 40.416 |
| 25 | M20A | Y | -6.272 | -7.121 | 40.416 | 50.52 |
| 26 | M21 | $Y$ | -. 269 | -1.836 | 0 | 10.104 |
| 27 | M21 | $Y$ | -1.836 | -2.808 | 10.104 | 20.208 |
| 28 | M21 | $Y$ | -2.808 | 4.23 | 20.208 | 30.312 |
| 29 | M21 | Y | -4.23 | -6 | 30.312 | 40.416 |
| 30 | M21 | $Y$ | -6 | -7.032 | 40.416 | 50.52 |
| 31 | M22 | Y | -. 03 | -5.011 | 12.45 | 22.41 |
| 32 | M22 | $Y$ | -5.011 | -7.594 | 22.41 | 32.37 |
| 33 | M22 | Y | -7.594 | -3.658 | 32.37 | 42.33 |
| 34 | M22 | $Y$ | -3.658 | -1.82 | 42.33 | 52.29 |
| 35 | M22 | Y | -1.82 | -1.216 | 52.29 | 62.25 |
| 36 | M25 | $Y$ | . 282 | -1.163 | 0 | 10.104 |
| 37 | M25 | $Y$ | -1.163 | -1.518 | 10.104 | 20.208 |
| 38 | M25 | $Y$ | -1.518 | -2,223 | 20.208 | 30.312 |
| 39 | M25 | $Y$ | -2.223 | -3.08 | 30.312 | 40.416 |
| 40 | M25 | Y | -3.08 | - 3.214 | 40.416 | 50.52 |
| 41 | M26 | Y | -. 282 | -1.164 | 0 | 10.104 |
| 42 | M26 | $Y$ | -1.164 | -1.519 | 10,104 | 20.208 |
| 43 | M26 | $Y$ | -1.519 | -2.224 | 20.208 | 30.312 |
| 44 | M26 | $Y$ | $-2.224$ | -3.081 | 30.312 | 40.416 |
| 45 | M26 | $Y$ | -3.081 | -3.211 | 40.416 | 50.52 |

Member Distributed Loads (BLC 12: BLC 5 Transient Area Loads)

|  | Member Label | Direction | Start Magnitude[Ib/ft,F.psf] | End Magnitude[Ib/f. | Start Location[in. \%] | nd Location[in. \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | -4.74 | -4.74 | 0 | 62.25 |
| 2 | M2 | 2 | 0 | स, 0 | 0 | 10.794 |
| 3 | M8 | Z | -4.789 | -4.789 | 0 | 168 |
| 4 | M14 | Z | -2.737 | $-2.737$ | 0 | 61,314 |
| 5 | M18 | Z | -2.737 | -2.737 | 0 | 50.52 |
| 6 | - M29 | Z | -3.25 | -3,25. | 0 | 168 . |
| 7 | M14 | Z | -2.395 | -2.395 | 0 | 168 |
| 8 | M18A. | Z | -1.625 | 4.625 | 0 | 168 , |
| 9 | M19 | Z | -2.395 | -2.395 | 0 | 168 |
| 10 | M23 | Z | -1,625 | -1.625 | - 0 | 168 |
| 11 | MP6 | Z | -3.25 | -3.25 | 0 | 72 |
| 12 | MP5 | Z | -3.25 | -3.25 | 0 | 72. |
| 13 | MP4 | $\mathbf{Z}^{\text {i }}$ | -3.25 | -3.25 | 0 | 72 |
| 14 | MP2 | Z | -3.25 | -3.25 | 0 | - 72 |
| 15 | MP1 | Z | -3.25 | -3.25 | 0 | 72 |
| 16 | M20 | , Z | -1.368 | 1.368. | - 0 | 50.52 |
| 17 | M17A | Z | -4.74 | -4.74 | 0 | 62.25 |
| 18 | M18C | Z | , 0 | , 0, | 0 | 10.794 |
| 19 | M19B | Z | -2.737 | -2.737 | 0 | 61.314 |
| 20 | M20A | Z | -1.368 | -1.368 | 0 | 50.52 |
| 21 | M21 | Z | -2.737 | -2.737 | 0 | 50.52 |
| 22 | M23A | Z | 0 | 0 | 0 | 10.794 |
| 23 | M24 | Z | -5.473 | -5.473 | 0 | 61.314 |
| 24 | M25 | Z | -1.368 | -1.368 | 0 | 50.52 |
| 25 | M26 | Z | -1.368 | -1.368 | 0 | 50.52 |
| 26 | MP3 | Z | -3.25 | -3.25 | 0 | 72 |
| 27 | MP12 | Z | -3.25 | -3.25 | 0 | 72 |
| 28 | MP11 | Z | -3.25 | -3.25 | - 0 | 72 |
| 29 | MP10 | Z | -3.25 | -3.25 | 0 | 72 |
| 30 | M MP8 | Z | -3.25 | -3.25 | 0 | 72 |

$\qquad$

Member Distributed Loads (BLC 12 : BLC 5 Transient Area Loads) (Continued)

|  | Member Label | Direction | Start Magnitude[lb/ft. F.psi] | End Magnitude[lib/f... | Start Location[in.\%] | End Location[in. \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 31 | MP7 | Z | -3.25 | -3.25 | 0 | 72 |
| 32 | MP9 | Z | -3.25 | -3.25 | 0 | 72 |
| 33 | MP18 | Z | -3.25 | -3.25 | 0 | 72 |
| 34 | MP17 | Z | -3.25 | -3.25 | 0 | 72 |
| 35 | MP16 | Z | -3.25 | -3.25 | 0 | 72 |
| 36 | MP14 | Z | -3.25 | -3.25 | 0 | 72 |
| 37 | MP13 | Z | -3.25 | -3.25 | 0 | 72 |
| 38 | MP15 | Z | -3.25 | -3.25 | 0 | 72 |

## Member Distributed Loads (BLC 13 : BLC 6 Transient Area Loads)

|  | Member Label | Direction | Start Magnitude[lb/ft.F.psf] | End Magnitude[lb/f. | Start Location[in.\% | End Location[in.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | X | -2.737 | -2.737 | 0 | 62.25 |
| 2 | M2 | X | 0 | 0 | 0 | 10.794 |
| 3 | M11 | X | -4.74 | -4.74 | 0 | 61.314 |
| 4 | M14 | X | -4.148 | -4.1.48 | 0 | 168 |
| 5 | M18A | X | -2.814 | -2.814 | 0 | 168 |
| 6 | M19 | X | -4,148 | -4.148 | 0 | 168 |
| 7 | M23 | X | -2.814 | -2.814 | 0 | 168 |
| 8 | MP6 | X | -3.25 | -3,25 | 0 | - 72 |
| 9 | MP5 | X | -3.25 | -3.25 | 0 | 72 |
| 10 | MP4 | X | -3.25 | -3.25 | 0 | 72 |
| 11 | MP2 | X | -3.25 | -3.25 | 0 | 72 |
| 12 | MP1 | $X$ | -3.25 | -3.25 | 0 | 72 |
| 13 | M20 | X | -2.37 | -2.37 | 0 | 50.52 |
| 14 | M17A | X | $-2.737$ | -2.737 | 0 | 62.25 |
| 15 | M18C | X | 0 | 0 | 0 | 10,794 |
| 16 | M19B | X | -4.74 | -4.74 | 0 | 61.314 |
| 17 | M20A | X | -2.37 | -2.37 | 0 | 50.52 |
| 18 | M22 | Y $X$ | -5.473. ${ }^{\text {a }}$ | -5.473 | 0 | 62.25 |
| 19 | M25 | X | -2.37 | -2.37 | 0 | 50.52 |
| 20 | M26 | X | -2.37 . . | -2.37. | $\bigcirc 0$ | 50.52 , |
| 21 | MP3 | X | -3.25 | -3.25 | 0 | 72 |
| 22 | MP12 | X | -3.25 | -3.25 | 0 | 72 |
| 23 | MP11 | X | -3.25 | -3.25 | 0 | 72 |
| 24 | MP10 | X | -3.25 | -3.25 | 0 | - 72 |
| 25 | MP8 | X | -3.25 | -3.25 | 0 | 72 |
| 26 | MP7 | - X | -3.25 | -3.25 | $\bigcirc$ | \% 72 |
| 27 | MP9 | X | -3.25 | -3.25 | 0 | 72 |
| 28 | MP18 | X | -3.25 | -3.25 | 0 | . 72 |
| 29 | MP17 | X | -3.25 | -3.25 | 0 | 72 |
| 30 | MP16 | X | -3.25 | - -3.25 | $\bigcirc$ | $\bigcirc 72$ |
| 31 | MP14 | X | -3.25 | -3.25 | 0 | 72 |
| 32 | MP13 | X | - -3.25 | -3.25 | \% 0 | 72. |
| 33 | MP15 | X | -3.25 | -3.25 | 0 | 72 |

## APPENDIX D

## ADDITIONAL CALCUATIONS

| Date: | $12 / 26 / 2018$ |
| :---: | :---: |
| Client | Crown Castle |
| Carrier | AT\&T |
| Engineer: | $\mid P$ |
| Site: | 823530 |
| Job\#: | $600-003$ |


| Code: | LRFD |  |
| ---: | ---: | ---: |
| Axial: | 4238.70 |  |
| Shear: | lbs |  |
|  | 2334.68 | lbs |


| Bolt Capacity (1/2" A307 Bolt) |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: | :---: |
|  | Ult Load / Bolt |  |  |  |  |  | Factored Load ( $\phi=0.75$ ) | \# of Bolts | Factor Joint Capacity |
| Axial (Ib) | 8226.7 | 6170.0 | 2 | 12340 |  |  |  |  |  |
|  | Shear(Ib) | 5133.3 | 3850.0 | 2 |  |  |  |  |  |


| Interaction Check |  |
| ---: | ---: |
| $\mathrm{T} / \phi \mathrm{T}_{\mathrm{n}}$ | $34.3 \%$ |
| $\mathrm{~V} / \phi \vee \mathrm{n}$ |  |
| $\leq 1.0$ | $30.3 \%$ |
|  | $21.0 \%$ |
|  | OK |


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