



STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: siting.council@ct.gov

www.ct.gov/csc

VIA ELECTRONIC MAIL

July 19, 2018

Mary Caulfield, Site Acquisition Consultant
c/o New Cingular Wireless, PCS LLC
Centerline Communications
750 West Center Street, Suite 301
West Bridgewater, MA 02379

RE: **EM-CING-134-180305** - New Cingular Wireless PCS, LLC notice of intent to modify an existing telecommunications facility located at 64 Tolland Avenue, Stafford, Connecticut.

Dear Ms. Caulfield:

The Connecticut Siting Council (Council) is in receipt of your correspondence of July 18, 2018 submitted in response to the Council's March 16, 2018 notification of an incomplete request for exempt modification with regard to the above-referenced matter.

The submission renders the request for exempt modification complete and the Council will process the request in accordance with the Federal Communications Commission 60-day timeframe.

Thank you for your attention and cooperation.

Sincerely,

Melanie A. Bachman
Executive Director

MAB/CMW/jmb

From: Mary Caulfield [<mailto:mcaulfield@clinellc.com>]
Sent: Wednesday, July 18, 2018 1:01 PM
To: Barton, Jenna <Jenna.Barton@ct.gov>
Cc: CSC-DL Siting Council <Siting.Council@ct.gov>
Subject: RE: Councils Response to Fourth Extension Request for EM-CING-134-180305-TollandAve-Stafford

Good Afternoon Jenna,

On behalf of my colleague, Adam Wolfrey, please find attached an updated submittal addressing your concerns via the letter of incompleteness to modify an existing telecommunication facility located at 64 Tolland Avenue (AKA 50 Tolland Avenue), Stafford, CT.

I've enclosed the requested signed and stamped Structural Analysis Report as well as proof the filings have been mailed to the additional required parties.

As your letter states, the Capital Regional Council of Governments online geographical information system does show the property hosting the existing tower to be located at 50 Tolland Avenue; although, all prior documentation indicates the address as 64 Tolland Avenue, including a the Database of CSC-Approved Telecommunications Site and the Comprehensive List of Sites as well as an Exempt Modification Approval dated September 7, 2012 which I've included in the attached file.

In hope to clarify, I've referenced both addresses in the revised letter.

Please let me know if anything additional is needed for approval.

Thanks,
Mary



Mary Caulfield | Site Acquisition Consultant
750 West Center Street, Suite 301 | West Bridgewater, MA 02379
Cell: 978.994.0252 | Fax: 508.819.3017
mcaulfield@clinellc.com | www.centerlinecommunications.com

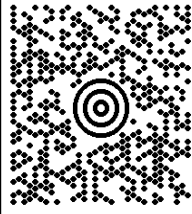
1 OF 1

1 LBS

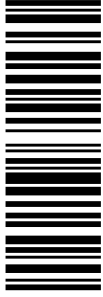
MARY CAULFIELD
978-994-0252
CENTERLINE COMMUNICATIONS
750 WEST CENTER STREET
WEST BRIDGEWATER MA 02379

SHIP TO:

MARY MITTA, FIRST SELECTMAN
TOWN OF STAFFORD
2ND FL, TOWN HALL
1 MAIN STREET
STAFFORD SPRINGS CT 06076-1412

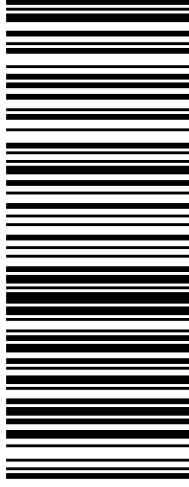


CT 061 9-01



UPS GROUND

TRACKING #: 1Z 9Y4 503 03 1465 3701



BILLING: P/P

Reference#1: CT1185: CSC to 1st Selectman



UIS 20.5.12. WNTNVS0 03.0A.07/2018

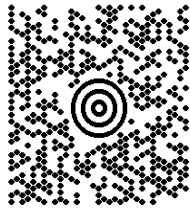
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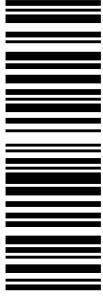
MARY CAULFIELD
978-994-0252
CENTERLINE COMMUNICATIONS
750 WEST CENTER STREET
WEST BRIDGEWATER MA 02379

SHIP TO:

DAVID PERKINS, ZONING
TOWN OF STAFFORD
1ST FL, TOWN HALL
1 MAIN STREET
STAFFORD SPRINGS CT 06076-1412

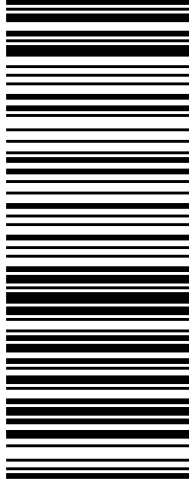


CT 061 9-01



UPS GROUND

TRACKING #: 1Z 9Y4 503 03 0539 6711



BILLING: P/P

Reference#1: CTT185: CSC to ZEO



UIS 20.5.12. WNTNVS0 03.0A.07/2018

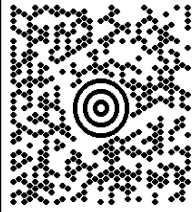
1 OF 1

1 LBS

MARY CAULFIELD
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750 WEST CENTER STREET
WEST BRIDGEWATER MA 02379

SHIP TO:

JENNIFER J DAVIS
TERRA ALTA INC
114 STAFFORD STREET
STAFFORD SPRINGS CT 06076-4335

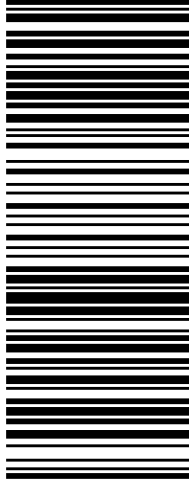


CT 061 9-01



UPS GROUND

TRACKING #: 1Z 9Y4 503 03 0474 1723



BILLING: P/P

Reference#1: CT1185: CSC to Property Owner



UIS 20.5.12. WNTNVS0 03.04.07/2018

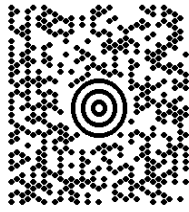
1 OF 1

1 LBS

MARY CAULFIELD
978-994-0252
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WEST BRIDGEWATER MA 02379

SHIP TO:

MARK LEGAULT
CORDLESS DATA TRANSFER, INC.
600 OLD HARTFORD ROAD
COLCHESTER CT 06415-2417

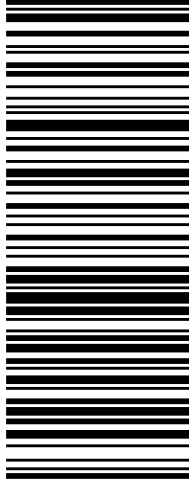


CT 063 0-01



UPS GROUND

TRACKING #: 1Z 9Y4 503 03 1308 8735



BILLING: P/P

Reference#1: CT1185: CSC to Tower Owner



UIS 20.5.12. WNTNVS0 03.0A.07/2018



Mary Caulfield, Site Acquisition Consultant
c/o New Cingular Wireless, PCS LLC (AT&T)
Centerline Communications, LLC
750 West Center Street, Suite 301
West Bridgewater, MA 02379
Mobile: (978) 994-0252
MCaulfield@centerlinecommunications.com

July 18, 2018

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

**RE: Notice of Exempt Modification // Site Number: CT1185 (Name: Stafford Springs Tolland Avenue)
64 Tolland Avenue (aka 50 Tolland Avenue), Stafford, CT 06076
N 41.9446722222222 // W -72.3176472222222**

Dear Ms. Bachman:

New Cingular Wireless, PCS, LLC (“AT&T”) currently maintains 9 total antennas at the 177-foot level on the existing 180-foot Guyed Tower, located at 64 Tolland Avenue (aka 50 Tolland Ave.), Stafford Springs, CT. The tower is owned by Cordless Data Transfer, Inc. and the property owned by Terra Alta Inc. AT&T now intends to replace three (3) of its existing antennas with three (3) new LTE (1900/2300 band) antennas for its LTE upgrade. AT&T also intends to install six (6) new remote radios; and certain in-cabinet upgrades at the base.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Mary Mitta, First Selectman for the Town of Stafford, David Perkins, Zoning Enforcement Officer for the Town of Stafford, Terra Alta Inc, Property Owner and Cordless Data Transfer, Inc., the tower owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

Attached to accommodate this filing are construction drawings dated February 20, 2018 by Hudson Design Group LLC, a structural analysis signed and stamped dated February 20, 2018 by

Fred A. Nudd Corporation and an Emissions Analysis Report dated February 26, 2018 by Centerline Communications, LLC.

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause an ineligible change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading, pursuant to the structural analysis by Fred A. Nudd Corporation, signed and stamped dated February 20, 2018.

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Mary Caulfield, Site Acquisition Consultant
c/o New Cingular Wireless, PCS LLC (AT&T)
Centerline Communications, LLC
750 West Center Street, Suite 301
West Bridgewater, MA 02379
Mobile: (978) 994-0252
MCaulfield@centerlinecommunications.com

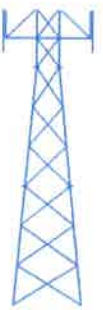
cc: Mary Mitta, First Selectman, Town of Stafford
David Perkins, Zoning Enforcement Officer, Town of Stafford
Terra Alta Inc, Property Owner
Cordless Data Transfer, Inc., Tower Owner



FRED A. NUDD CORPORATION

1743 ROUTE 104, BOX 577
ONTARIO, NY 14519
(315) 524-2531 FAX (315) 524-4249

www.nuddtowers.com



Mark LeGault
Cordless Data Transfer, Inc.
600 Old Hartford Road
Colchester, CT 06415
December 29, 2017

Nudd Job Number: 117-23243.8

Site Location: Tolland Avenue (64 Tolland Avenue, Stafford, CT 06076, Tolland County)

Subject: Structural Analysis of an existing 180 ft Guyed Tower

Fred A. Nudd Corporation has completed a structural analysis of an existing 180 ft guyed tower. The tower was originally designed by Fred A. Nudd Corporation. The design loading criteria and strength design are per the ANSI/TIA-222-G standard, which is the recommended design standard per the 2012 International Building Code (Sec. 1609 & 3108), and the 2016 Connecticut State Building Code. Tower and foundation dimensions have been taken from drawings by Fred A. Nudd, project number 9898, dated December 29, 2003. Additional foundation dimensions and installation data was provided by Cordless Data Transfer. Design criteria per each analysis are noted on the following page. The tower is assumed to be in good, undamaged and equivalent to as new condition and has been maintained / inspected per criteria by TIA-222.

The purpose of this analysis is to determine the structure's ability to support new AT&T equipment. The new equipment to be installed, which included antennas, coax, mounts and associated hardware are listed on the following page, along with already installed cellular equipment, in the appurtenance loading table.

Results of the analysis indicate the tower will be able to support the design loads noted in the appurtenance loading table on the following page. Specific section design loads, capacities and stress ratios are provided on the following pages. Maximum member usage was found to be 92%. Detailed calculation of the applied forces and member capacities are provided in the following pages.

The tower base foundation and anchor design loads were analyzed considering the aforementioned foundation data and assumed soil properties. Based on this, the base foundation and anchors are adequate to support the existing and new loading.

In conclusion, the tower superstructure and substructure can support the proposed AT&T equipment.

We trust this report satisfies your needs. Please contact us with any questions or concerns regarding this report.

Best Regards,



Fred. A. Nudd Corporation

Code Design Criteria

ANSI/TIA-222-G

Windspeed = 98 mph, 3-second gust, V_{asd} / 124 mph, 3-second gust, V_{ult}

Exposure = B

Radial Ice = 1.0 inch

Ice Windspeed = 50 mph, 3-second gust

Structure Class = II

Topographic Category = 1

$S_s < 1.0$, thus seismic loading does not need to be considered

Proposed Appurtenance Loading – AT&T

Elevation (ft) ¹	Antenna	Mount	Coax ²
177	(1) Andrew SBNH-1D6565C (3) Powerwave 7770 (2) CCI TPA-65R-LCUUUU-H8 (1) Quintel QS46512-2 (1) KMW AM-X-CD-14-65-00T-RET (1) Powewave P65-17-XLH-RR (3) Ericsson RRUS-11 (6) Ericsson RRUS-32 (6) Powerwave LGP21401 (6) Powerwave DBC0061F1V51-2 (6) Kaelus LGP21901	(3) 12 ft Boom / Frame	(12) 1-5/8 (3) 1-5/8 Fiber (2) 3/8 Fiber (4) DC

¹Note elevation is measured from grade to center of antenna

²Additional coax is to be installed on the same tower face as the existing coax

Maximum Member Usage Results

Member	Usage (%) ¹
Legs	92
Diagonals	71
Horizontals	59
Guy Wires	48
Splice Bolts	37

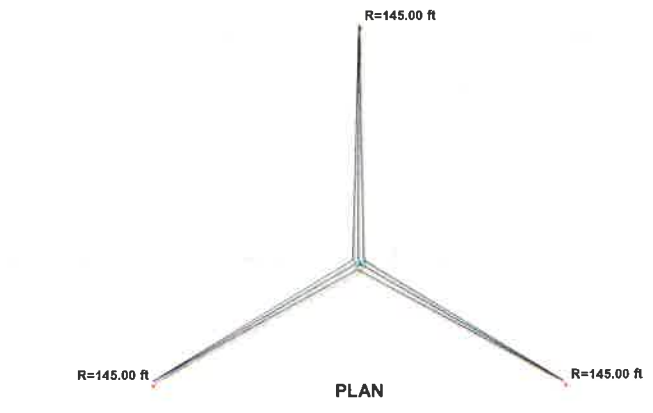
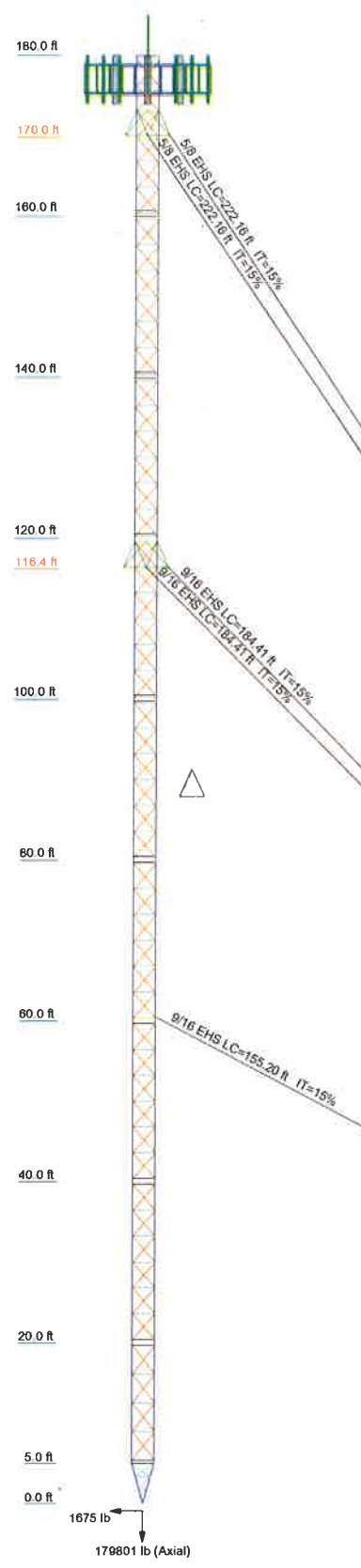
¹Usage above 100% indicates the applied design load exceeds the member strength capacity and requires strengthening

Foundation Usage Results

Base Reaction	Capacity (kip-ft)	Analysis (kip-ft)	Usage (%) ¹
Base Axial	217.8	179.8	86
Anchor Uplift	93.1	29.0	31
Anchor Shear	52.2	38.5	74

¹Usage above 100% indicates the applied design load exceeds the foundation strength capacity and requires strengthening

Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10
Legs					P2.5x.203					
Leg Grade					A500M-54					
Diagonals					SR 5/8					
Diagonal Grade					A36					
Top Girts										
Bottom Girts										
Horizontal										
Top Guy Pull-Offs										
Bot Guy Pull-Offs										
Face Width (ft)										
# Panels @ (ft)										
Weight (lb)										



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
Lightning Rod	180	(2) Kaelus LGP21901 (ATI)	177
Sector Frame Mount (ATI)	177	(2) Kaelus LGP21901 (ATI)	177
Sector Frame Mount (ATI)	177	(2) Kaelus LGP21901 (ATI)	177
Sector Frame Mount (ATI)	177	(2) Powerwave LGP21401 (ATI)	177
Powerwave 7770 (ATI)	177	(2) Powerwave LGP21401 (ATI)	177
Powerwave 7770 (ATI)	177	(2) Powerwave LGP21401 (ATI)	177
Powerwave 7770 (ATI)	177	CCI TPA-65R-LCUUUU-H8 (ATI)	177
KMW AM-X-CD-14-65-00T (ATI)	177	CCI TPA-65R-LCUUUU-H8 (ATI)	177
Powerwave P85-17-XLH-RR (ATI)	177	Quintel QS48512-2 (ATI)	177
Commscope SBNH-1D8565C (ATI)	177	(2) Powerwave DBC0061F1V51-2 (ATI)	177
Ericsson RRUS11 (ATI)	177	(2) Powerwave DBC0061F1V51-2 (ATI)	177
Ericsson RRUS11 (ATI)	177	(2) Powerwave DBC0061F1V51-2 (ATI)	177
Ericsson RRUS11 (ATI)	177	(2) Powerwave DBC0061F1V51-2 (ATI)	177
(2) Ericsson RRUS32 (ATI)	177	(2) Powerwave DBC0061F1V51-2 (ATI)	177
(2) Ericsson RRUS32 (ATI)	177	(2) Powerwave DBC0061F1V51-2 (ATI)	177
(2) Ericsson RRUS32 (ATI)	177	(2) Powerwave DBC0061F1V51-2 (ATI)	177

SYMBOL LIST

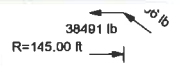
MARK	SIZE	MARK	SIZE
A	3 @ 1.66667		

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A500M-54	54 ksi	70 ksi	A36	36 ksi	58 ksi

TOWER DESIGN NOTES

1. Tower is located in Tolland County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 98 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
- 6.



Phone: FAX:	Job: 117-23243.8
	Project: Tolland Ave., CT
	Client: CDT Drawn by: FAN App'd:
	Code: TIA-222-G Date: 12/29/17 Scale: NTS
	Path: Dwg No E-1

RISATower Phone: FAX:	Job 117-23243.8	Page 1 of 44
	Project Tolland Ave., CT	Date 01:32:09 12/29/17
	Client CDT	Designed by FAN

Tower Input Data

The main tower is a 3x guyed tower with an overall height of 180.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 3.50 ft at the top and tapered at the base.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in Tolland County, Connecticut.

Basic wind speed of 98 mph.

Structure Class II.

Exposure Category B.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

Weld together tower sections have flange connections..

Tension only take-up is 0.0313 in.

Pressures are calculated at each section.

Safety factor used in guy design is 1.

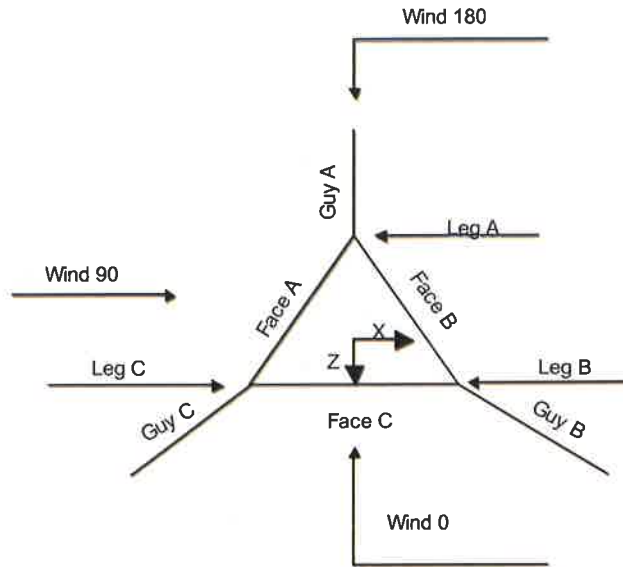
Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

Options

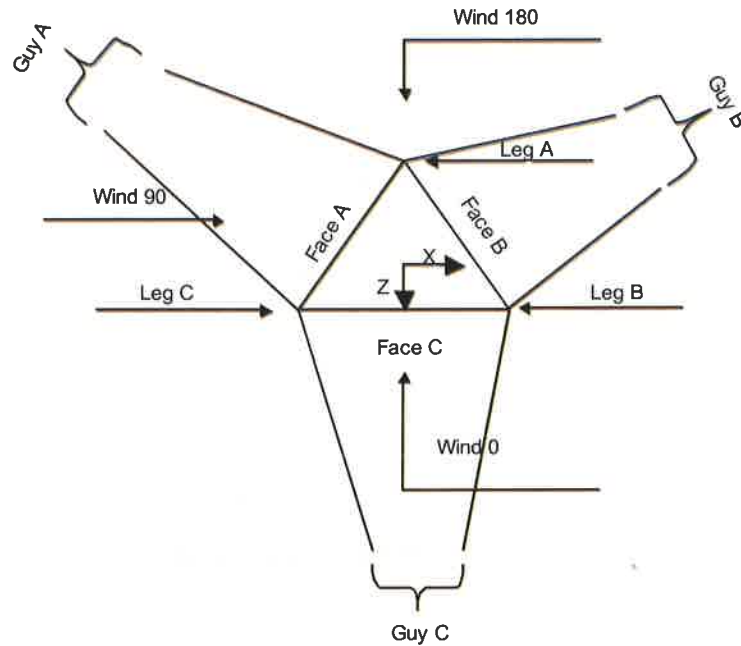
<ul style="list-style-type: none"> Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification √ Use Code Stress Ratios √ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile √ Include Bolts In Member Capacity √ Leg Bolts Are At Top Of Section √ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination 	<ul style="list-style-type: none"> Distribute Leg Loads As Uniform Assume Legs Pinned √ Assume Rigid Index Plate √ Use Clear Spans For Wind Area √ Use Clear Spans For KL/r √ Retension Guys To Initial Tension Bypass Mast Stability Checks √ Use Azimuth Dish Coefficients √ Project Wind Area of Appurt. √ Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component √ Triangulate Diamond Inner Bracing 	<ul style="list-style-type: none"> Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression √ All Leg Panels Have Same Allowable Offset Girt At Foundation √ Consider Feedline Torque Include Angle Block Shear Check <li style="text-align: center;">Poles Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets
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<i>RISA</i>Tower Phone: FAX:	Job 117-23243.8	Page 2 of 44
	Project Tolland Ave., CT	Date 01:32:09 12/29/17
	Client CDT	Designed by FAN



Corner & Starmount Guyed Tower

RISATower Phone: FAX:	Job 117-23243.8	Page 3 of 44
	Project Tolland Ave., CT	Date 01:32:09 12/29/17
	Client CDT	Designed by FAN



Face Guyed

Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T1	180.00-160.00			3.50	1	20.00
T2	160.00-140.00			3.50	1	20.00
T3	140.00-120.00			3.50	1	20.00
T4	120.00-100.00			3.50	1	20.00
T5	100.00-80.00			3.50	1	20.00
T6	80.00-60.00			3.50	1	20.00
T7	60.00-40.00			3.50	1	20.00
T8	40.00-20.00			3.50	1	20.00
T9	20.00-5.00			3.50	1	15.00
T10	5.00-0.00			3.50	1	5.00

Tower Section Geometry (cont'd)

RISA Tower Phone: FAX:	Job	117-23243.8	Page	4 of 44
	Project	Tolland Ave., CT	Date	01:32:09 12/29/17
	Client	CDT	Designed by	FAN

Tower Section	Tower Elevation <i>ft</i>	Diagonal Spacing <i>ft</i>	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset <i>in</i>	Bottom Girt Offset <i>in</i>
T1	180.00-160.00	3.21	TX Brace	No	Yes	4.5000	4.5000
T2	160.00-140.00	3.21	TX Brace	No	Yes	4.5000	4.5000
T3	140.00-120.00	3.21	TX Brace	No	Yes	4.5000	4.5000
T4	120.00-100.00	3.21	TX Brace	No	Yes	4.5000	4.5000
T5	100.00-80.00	3.21	TX Brace	No	Yes	4.5000	4.5000
T6	80.00-60.00	3.21	TX Brace	No	Yes	4.5000	4.5000
T7	60.00-40.00	3.21	TX Brace	No	Yes	4.5000	4.5000
T8	40.00-20.00	3.21	TX Brace	No	Yes	4.5000	4.5000
T9	20.00-5.00	3.56	TX Brace	No	Yes	4.5000	4.5000
T10	5.00-0.00	1.67	X Brace	No	Yes	0.0000	0.0000

Tower Section Geometry (cont'd)

Tower Elevation <i>ft</i>	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 180.00-160.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)
T2 160.00-140.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)
T3 140.00-120.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)
T4 120.00-100.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)
T5 100.00-80.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)
T6 80.00-60.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)
T7 60.00-40.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)
T8 40.00-20.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)
T9 20.00-5.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)
T10 5.00-0.00	Pipe	P2.5x.203	A500M-54 (54 ksi)	Solid Round	5/8	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation <i>ft</i>	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 180.00-160.00	Equal Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)	Equal Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T2 160.00-140.00	Equal Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)	Equal Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T3 140.00-120.00	Equal Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)	Equal Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T4 120.00-100.00	Equal Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)	Equal Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T5 100.00-80.00	Equal Angle	L1 1/2x1 1/2x3/16	A36	Equal Angle	L1 1/2x1 1/2x3/16	A36

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Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T6 80.00-60.00	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36
T7 60.00-40.00	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36
T8 40.00-20.00	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36
T9 20.00-5.00	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36
T10 5.00-0.00	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36

Tower Section Geometry (cont'd)

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T1 180.00-160.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T2 160.00-140.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T3 140.00-120.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T4 120.00-100.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T5 100.00-80.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T6 80.00-60.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T7 60.00-40.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T8 40.00-20.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T9 20.00-5.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T10 5.00-0.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Gusset Area (per face) ft ²	Gusset Thickness in	Gusset Grade	Adjust. Factor A _f	Adjust. Factor A _r	Weight Mult.	Double Angle Sitch Bolt Spacing Diagonals in	Double Angle Sitch Bolt Spacing Horizontals in
T1 180.00-160.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000
T2 160.00-140.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000
T3	0.00	0.0000	A36	1	1	1	36.0000	36.0000

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Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A_f	Adjust. Factor A_r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in
ft	ft ²	in						
140.00-120.00			(36 ksi)					
T4	0.00	0.0000	A36	1	1	1	36.0000	36.0000
120.00-100.00			(36 ksi)					
T5	0.00	0.0000	A36	1	1	1	36.0000	36.0000
100.00-80.00			(36 ksi)					
T6	0.00	0.0000	A36	1	1	1	36.0000	36.0000
80.00-60.00			(36 ksi)					
T7	0.00	0.0000	A36	1	1	1	36.0000	36.0000
60.00-40.00			(36 ksi)					
T8	0.00	0.0000	A36	1	1	1	36.0000	36.0000
40.00-20.00			(36 ksi)					
T9	0.00	0.0000	A36	1	1	1	36.0000	36.0000
20.00-5.00			(36 ksi)					
T10	0.00	0.0000	A36	1	1	1	36.0000	36.0000
5.00-0.00			(36 ksi)					

Tower Section Geometry (cont'd)

Tower Elevation	Calc K Single Angles	Calc K Solid Rounds	Legs	K Factors ¹						
				X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
				X Y	X Y	X Y	X Y	X Y	X Y	X Y
T1	No	Yes	1	1	1	1	0.65	0.65	1	1
180.00-160.00				1	1	1	0.65	0.65	1	1
T2	No	Yes	1	1	1	1	0.65	0.65	1	1
160.00-140.00				1	1	1	0.65	0.65	1	1
T3	No	Yes	1	1	1	1	0.65	0.65	1	1
140.00-120.00				1	1	1	0.65	0.65	1	1
T4	No	Yes	1	1	1	1	0.65	0.65	1	1
120.00-100.00				1	1	1	0.65	0.65	1	1
T5	No	Yes	1	1	1	1	0.65	0.65	1	1
100.00-80.00				1	1	1	0.65	0.65	1	1
T6	No	Yes	1	1	1	1	0.65	0.65	1	1
80.00-60.00				1	1	1	0.65	0.65	1	1
T7	No	Yes	1	1	1	1	0.65	0.65	1	1
60.00-40.00				1	1	1	0.65	0.65	1	1
T8	No	Yes	1	1	1	1	0.65	0.65	1	1
40.00-20.00				1	1	1	0.65	0.65	1	1
T9	No	Yes	1	1	1	1	0.65	0.65	1	1
20.00-5.00				1	1	1	0.65	0.65	1	1
T10	No	Yes	1	1	1	1	0.65	0.65	1	1
5.00-0.00				1	1	1	0.65	0.65	1	1

¹Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

Tower Section Geometry (cont'd)

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Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 180.00-160.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T2 160.00-140.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T3 140.00-120.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T4 120.00-100.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T5 100.00-80.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T6 80.00-60.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T7 60.00-40.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T8 40.00-20.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T9 20.00-5.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T10 5.00-0.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75

Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1 180.00-160.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T2 160.00-140.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T3 140.00-120.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T4 120.00-100.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T5 100.00-80.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T6 80.00-60.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T7 60.00-40.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T8 40.00-20.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T9 20.00-5.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T10 5.00-0.00	Flange	0.7500	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0

Guy Data

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Guy Elevation	Guy Grade	Guy Size	Initial Tension	%	Guy Modulus	Guy Weight	L_0	Anchor Radius	Anchor Azimuth Adj.	Anchor Elevation	End Fitting Efficiency
ft			lb		ksi	plf	ft	ft	°	ft	%
170	EHS	A 5/8	6360.00	15%	21000	0.813	221.88	145.00	0.0000	0.00	100%
		B 5/8	6360.00	15%	21000	0.813	221.88	145.00	0.0000	0.00	100%
		C 5/8	6360.00	15%	21000	0.813	221.88	145.00	0.0000	0.00	100%
116.417	EHS	A 9/16	5250.00	15%	21000	0.671	184.18	145.00	0.0000	0.00	100%
		B 9/16	5250.00	15%	21000	0.671	184.18	145.00	0.0000	0.00	100%
		C 9/16	5250.00	15%	21000	0.671	184.18	145.00	0.0000	0.00	100%
60.375	EHS	A 9/16	5250.00	15%	21000	0.671	155.01	145.00	0.0000	0.00	100%
		B 9/16	5250.00	15%	21000	0.671	155.01	145.00	0.0000	0.00	100%
		C 9/16	5250.00	15%	21000	0.671	155.01	145.00	0.0000	0.00	100%

Guy Data (cont'd)

Guy Elevation	Mount Type	Torque-Arm Spread	Torque-Arm Leg Angle	Torque-Arm Style	Torque-Arm Grade	Torque-Arm Type	Torque-Arm Size
ft		ft	°				
170	Torque Arm	7.00	30.0000	Dog Ear	A36 (36 ksi)	Single Angle	L2x2x5/16 L3x3x1/4
116.417	Torque Arm	7.00	30.0000	Dog Ear	A36 (36 ksi)	Single Angle	L2x2x5/16 L3x3x1/4
60.375	Corner						

Guy Data (cont'd)

Guy Elevation	Diagonal Grade	Diagonal Type	Upper Diagonal Size	Lower Diagonal Size	Is Strap.	Pull-Off Grade	Pull-Off Type	Pull-Off Size
ft								
170.00	A572-50 (50 ksi)	Solid Round			No	A36 (36 ksi)	Equal Angle	L1 1/2x1 1/2x3/16
116.42	A572-50 (50 ksi)	Solid Round			No	A36 (36 ksi)	Equal Angle	L1 1/2x1 1/2x3/16
60.38	A572-50 (50 ksi)	Solid Round			No	A36 (36 ksi)	Equal Angle	L1 1/2x1 1/2x3/16

Guy Data (cont'd)

Guy Elevation	Cable Weight A	Cable Weight B	Cable Weight C	Cable Weight D	Tower Intercept A	Tower Intercept B	Tower Intercept C	Tower Intercept D
ft	lb	lb	lb	lb	ft	ft	ft	ft
170	180.38	180.38	180.38		3.12	3.12	3.12	
116.417	123.58	123.58	123.58		3.0 sec/pulse	3.0 sec/pulse	3.0 sec/pulse	
					2.15	2.15	2.15	
60.375	104.01	104.01	104.01		2.5 sec/pulse	2.5 sec/pulse	2.5 sec/pulse	
					1.53	1.53	1.53	
					2.1 sec/pulse	2.1 sec/pulse	2.1 sec/pulse	

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Guy Data (cont'd)

Guy Elevation ft	Calc K Single Angles	Calc K Solid Rounds	Torque Arm		Pull Off		Diagonal	
			K _x	K _y	K _x	K _y	K _x	K _y
170	No	No			0.65	0.65		
116.417	No	No			0.65	0.65		
60.375	No	No			0.65	0.65		

Guy Data (cont'd)

Guy Elevation ft	Torque-Arm				Pull Off				Diagonal			
	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U
170	0.7500 A325N	2	0.0000	1	0.0000 A325N	0	0.0000	1	0.6250 A325N	0	0.0000	1
116.417	0.7500 A325N	2	0.0000	1	0.0000 A325N	0	0.0000	1	0.6250 A325N	0	0.0000	1
60.375	0.6250 A325N	0	0.0000	0.75	0.0000 A325N	0	0.0000	1	0.6250 A325N	0	0.0000	1

Guy Pressures

Guy Elevation ft	Guy Location	z ft	q _z psf	q _z Ice psf	Ice Thickness in
170	A	85.00	20	5	2.1985
	B	85.00	20	5	2.1985
	C	85.00	20	5	2.1985
116.417	A	58.21	18	5	2.1168
	B	58.21	18	5	2.1168
	C	58.21	18	5	2.1168
60.375	A	30.19	15	4	1.9823
	B	30.19	15	4	1.9823
	C	30.19	15	4	1.9823

Guy-Mast Forces (Excluding Wind) - No Ice

Guy Elevation ft	Guy Location	Chord Angle °	Guy Tension Top Bottom lb	F _x lb	F _y lb	F _z lb	M _x lb-ft	M _y lb-ft	M _z lb-ft
170	A	49.9259	6498.03 6360.00	-101.28	5009.66	-4137.32	-10123.16	14685.27	-17533.82
	A	49.9259	6498.03	101.28	5009.66	-4137.32	-10123.16	-14685.27	17533.82

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Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom lb	F _x	F _y	F _z	M _x	M _y	M _z	
ft		°	lb	lb	lb	lb	lb-ft	lb-ft	lb-ft	
116.417	B	49.9259	6360.00	3633.66	5009.66	1980.95	20246.31	14685.27	0.00	
			6498.03							
	B	49.9259	49.9259	6360.00	3532.39	5009.66	2156.37	-10123.16	-14685.27	-17533.82
				6498.03						
	C	49.9259	49.9259	6360.00	-3532.39	5009.66	2156.37	-10123.16	14685.27	17533.82
				6498.03						
	C	49.9259	49.9259	6360.00	-3633.66	5009.66	1980.95	20246.31	-14685.27	0.00
				6498.03						
	A	39.1448	39.1448	Sum:	0.00	30057.98	0.00	-0.00	0.00	0.00
				5328.01	-100.37	3400.60	-4100.44	-6871.68	14554.35	-11902.11
A	39.1448	39.1448	5250.00	100.37	3400.60	-4100.44	-6871.68	-14554.35	11902.11	
			5328.01	3601.27	3400.60	1963.29	13743.37	14554.35	0.00	
B	39.1448	39.1448	5250.00	3500.89	3400.60	2137.14	-6871.68	-14554.35	-11902.11	
			5328.01	-3500.89	3400.60	2137.14	-6871.68	14554.35	11902.11	
C	39.1448	39.1448	5250.00	-3601.27	3400.60	1963.29	13743.37	-14554.35	0.00	
			5328.01	0.00	20403.61	0.00	-0.00	0.00	0.00	
A	22.8926	22.8926	Sum:	0.00	2102.12	-4854.90	-4247.81	0.00	0.00	
			5290.46	4204.47	2102.12	2427.45	2123.90	0.00	-3678.71	
B	22.8926	22.8926	5250.00	-4204.47	2102.12	2427.45	2123.90	-0.00	3678.71	
			5290.46	0.00	6306.36	0.00	0.00	0.00	0.00	
C	22.8926	22.8926	5250.00	0.00	6306.36	0.00	0.00	0.00	0.00	
			5290.46							

Guy-Mast Forces (Excluding Wind) - Ice

Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom lb	F _x	F _y	F _z	M _x	M _y	M _z	
ft		°	lb	lb	lb	lb	lb-ft	lb-ft	lb-ft	
170	A	49.9259	11340.86	-166.93	9060.16	-6819.14	-18308.10	24204.30	-31710.56	
			9916.02							
	A	49.9259	49.9259	11340.86	166.93	9060.16	-6819.14	-18308.10	-24204.30	31710.56
				9916.02						
	B	49.9259	49.9259	11340.86	5989.01	9060.16	3265.01	36616.20	24204.30	0.00
				9916.02						
	B	49.9259	49.9259	11340.86	5822.09	9060.16	3554.13	-18308.10	-24204.30	-31710.56
				9916.02						
	C	49.9259	49.9259	11340.86	-5822.09	9060.16	3554.13	-18308.10	24204.30	31710.56
				9916.02						
C	49.9259	49.9259	11340.86	-5989.01	9060.16	3265.01	36616.20	-24204.30	0.00	
			9916.02							
A	39.1448	39.1448	Sum:	0.00	54360.96	0.00	-0.00	0.00	0.00	
			9479.64	-171.09	6401.99	-6989.19	-12936.67	24807.90	-22406.97	
A	39.1448	39.1448	8596.54	171.09	6401.99	-6989.19	-12936.67	-24807.90	22406.97	
			9479.64							

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Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom lb	F _x	F _y	F _z	M _x	M _y	M _z	
ft		°		lb	lb	lb	lb-ft	lb-ft	lb-ft	
60.375	B	39.1448	8596.54	6138.36	6401.99	3346.43	25873.34	24807.90	0.00	
			9479.64							
	B	39.1448	8596.54	5967.27	6401.99	3642.76	-12936.67	-24807.90	-22406.97	
			9479.64							
	C	39.1448	8596.54	-5967.27	6401.99	3642.76	-12936.67	24807.90	22406.97	
			9479.64							
	C	39.1448	8596.54	-6138.36	6401.99	3346.43	25873.34	-24807.90	0.00	
			9479.64							
	A	22.8926	22.8926	Sum:	0.00	38411.94	0.00	-0.00	0.00	0.00
				8905.54	0.00	3912.05	-8000.28	-7905.18	0.00	0.00
	B	22.8926	22.8926	8493.69	6928.45	3912.05	4000.14	3952.59	0.00	-6846.09
				8905.54						
C	22.8926	22.8926	8493.69	-6928.45	3912.05	4000.14	3952.59	-0.00	6846.09	
			8905.54							
			Sum:	0.00	11736.15	-0.00	0.00	0.00	0.00	

Guy-Mast Forces (Excluding Wind) - Service

Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom lb	F _x	F _y	F _z	M _x	M _y	M _z
ft		°		lb	lb	lb	lb-ft	lb-ft	lb-ft
170	A	49.9259	6498.03	-101.28	5009.66	-4137.32	-10123.16	14685.27	-17533.82
			6360.00						
	A	49.9259	6498.03	101.28	5009.66	-4137.32	-10123.16	-14685.27	17533.82
			6360.00						
	B	49.9259	6498.03	3633.66	5009.66	1980.95	20246.31	14685.27	0.00
			6360.00						
	B	49.9259	6498.03	3532.39	5009.66	2156.37	-10123.16	-14685.27	-17533.82
			6360.00						
	C	49.9259	6498.03	-3532.39	5009.66	2156.37	-10123.16	14685.27	17533.82
			6360.00						
	C	49.9259	6498.03	-3633.66	5009.66	1980.95	20246.31	-14685.27	0.00
			6360.00						
A	39.1448	39.1448	Sum:	0.00	30057.98	0.00	-0.00	0.00	0.00
			5328.01	-100.37	3400.60	-4100.44	-6871.68	14554.35	-11902.11
A	39.1448	39.1448	5250.00	100.37	3400.60	-4100.44	-6871.68	-14554.35	11902.11
			5328.01						
B	39.1448	39.1448	5328.01	3601.27	3400.60	1963.29	13743.37	14554.35	0.00
			5250.00						
B	39.1448	39.1448	5328.01	3500.89	3400.60	2137.14	-6871.68	-14554.35	-11902.11
			5250.00						
C	39.1448	39.1448	5328.01	-3500.89	3400.60	2137.14	-6871.68	14554.35	11902.11
			5250.00						
C	39.1448	39.1448	5328.01	-3601.27	3400.60	1963.29	13743.37	-14554.35	0.00
			5250.00						
A	22.8926	22.8926	Sum:	0.00	20403.61	0.00	-0.00	0.00	0.00
			5290.46	0.00	2102.12	-4854.90	-4247.81	0.00	0.00
B	22.8926	22.8926	5250.00	4204.47	2102.12	2427.45	2123.90	0.00	-3678.71
			5290.46						

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Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom lb	F _x	F _y	F _z	M _x	M _y	M _z
ft		°		lb	lb	lb	lb-ft	lb-ft	lb-ft
	C	22.8926	\$250.00 \$290.46 \$250.00	-4204.47	2102.12	2427.43	2123.90	-0.00	3678.71
			Sum:	0.00	6306.36	0.00	0.00	0.00	0.00

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	Number Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
1 5/8 (AT&T)	C	No	Ar (CaAa)	178.00 - 0.00	12	12	1.9800	1.9800		1.04
1 5/8 Fiber (AT&T)	C	No	Ar (CaAa)	178.00 - 0.00	3	3	1.9800	1.9800		1.04
Safety Line 3/8 Fiber (AT&T)	A	No	Ar (CaAa)	180.00 - 0.00	1	1	0.3750	0.3750		0.22
DC (AT&T)	C	No	Ar (CaAa)	178.00 - 0.00	2	2	0.3750	0.3750		0.22
	C	No	Ar (CaAa)	178.00 - 0.00	4	4	0.5800	0.5800		0.25

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight lb
T1	180.00-160.00	A	0.000	0.000	0.750	0.000	4.40
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	58.986	0.000	306.72
T2	160.00-140.00	A	0.000	0.000	0.750	0.000	4.40
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	65.540	0.000	340.80
T3	140.00-120.00	A	0.000	0.000	0.750	0.000	4.40
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	65.540	0.000	340.80
T4	120.00-100.00	A	0.000	0.000	0.750	0.000	4.40
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	65.540	0.000	340.80
T5	100.00-80.00	A	0.000	0.000	0.750	0.000	4.40
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	65.540	0.000	340.80
T6	80.00-60.00	A	0.000	0.000	0.750	0.000	4.40
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	65.540	0.000	340.80
T7	60.00-40.00	A	0.000	0.000	0.750	0.000	4.40
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	65.540	0.000	340.80
T8	40.00-20.00	A	0.000	0.000	0.750	0.000	4.40
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	65.540	0.000	340.80
T9	20.00-5.00	A	0.000	0.000	0.563	0.000	3.30
		B	0.000	0.000	0.000	0.000	0.00

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Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{A A} In Face ft ²	C _{A A} Out Face ft ²	Weight lb
T10	5.00-0.00	C	0.000	0.000	49.133	0.000	253.60
		A	0.000	0.000	0.188	0.000	1.10
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	16.383	0.000	85.20

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _{A A} In Face ft ²	C _{A A} Out Face ft ²	Weight lb
T1	180.00-160.00	A	2.356	0.000	0.000	10.175	0.000	161.65
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	190.704	0.000	3330.61
T2	160.00-140.00	A	2.327	0.000	0.000	10.058	0.000	158.03
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	211.126	0.000	3658.35
T3	140.00-120.00	A	2.294	0.000	0.000	9.926	0.000	153.99
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	210.262	0.000	3610.79
T4	120.00-100.00	A	2.256	0.000	0.000	9.774	0.000	149.42
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	209.269	0.000	3556.40
T5	100.00-80.00	A	2.211	0.000	0.000	9.594	0.000	144.12
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	208.099	0.000	3492.61
T6	80.00-60.00	A	2.156	0.000	0.000	9.375	0.000	137.76
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	206.667	0.000	3415.04
T7	60.00-40.00	A	2.085	0.000	0.000	9.089	0.000	129.71
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	204.808	0.000	3315.07
T8	40.00-20.00	A	1.981	0.000	0.000	8.674	0.000	118.45
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	202.107	0.000	3171.37
T9	20.00-5.00	A	1.815	0.000	0.000	6.007	0.000	76.14
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	148.349	0.000	2209.43
T10	5.00-0.00	A	1.545	0.000	0.000	1.733	0.000	19.22
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	47.708	0.000	647.77

Feed Line Center of Pressure

Section	Elevation ft	CP _X in	CP _Z in	CP _X Ice in	CP _Z Ice in
T1	180.00-160.00	-0.0254	2.4288	-0.0752	1.0915
T2	160.00-140.00	-0.0234	2.4928	-0.0716	1.1732
T3	140.00-120.00	-0.0234	2.4928	-0.0719	1.1947
T4	120.00-100.00	-0.0234	2.4928	-0.0722	1.2192
T5	100.00-80.00	-0.0234	2.4928	-0.0725	1.2480
T6	80.00-60.00	-0.0234	2.4928	-0.0728	1.2831
T7	60.00-40.00	-0.0234	2.4928	-0.0730	1.3283
T8	40.00-20.00	-0.0234	2.4928	-0.0730	1.3936

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Section	Elevation	CP _X	CP _Z	CP _X Ice	CP _Z Ice
	ft	in	in	in	in
T9	20.00-5.00	-0.0235	2.5044	-0.0744	1.3408
T10	5.00-0.00	-0.0233	2.4763	-0.0161	0.3865

Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K _a No Ice	K _a Ice
T1	1	1 5/8	160.00 - 178.00	0.6000	0.2654
T1	2	1 5/8 Fiber	160.00 - 178.00	0.6000	0.2654
T1	3	Safety Line 3/8	160.00 - 180.00	0.6000	0.2654
T1	4	Fiber	160.00 - 178.00	0.6000	0.2654
T1	5	DC	160.00 - 178.00	0.6000	0.2654
T2	1	1 5/8	140.00 - 160.00	0.6000	0.2713
T2	2	1 5/8 Fiber	140.00 - 160.00	0.6000	0.2713
T2	3	Safety Line 3/8	140.00 - 160.00	0.6000	0.2713
T2	4	Fiber	140.00 - 160.00	0.6000	0.2713
T2	5	DC	140.00 - 160.00	0.6000	0.2713
T3	1	1 5/8	120.00 - 140.00	0.6000	0.2781
T3	2	1 5/8 Fiber	120.00 - 140.00	0.6000	0.2781
T3	3	Safety Line 3/8	120.00 - 140.00	0.6000	0.2781
T3	4	Fiber	120.00 - 140.00	0.6000	0.2781
T3	5	DC	120.00 - 140.00	0.6000	0.2781
T4	1	1 5/8	100.00 - 120.00	0.6000	0.2859
T4	2	1 5/8 Fiber	100.00 - 120.00	0.6000	0.2859
T4	3	Safety Line 3/8	100.00 - 120.00	0.6000	0.2859
T4	4	Fiber	100.00 - 120.00	0.6000	0.2859
T4	5	DC	100.00 - 120.00	0.6000	0.2859
T5	1	1 5/8	80.00 - 100.00	0.6000	0.2952
T5	2	1 5/8 Fiber	80.00 - 100.00	0.6000	0.2952
T5	3	Safety Line 3/8	80.00 - 100.00	0.6000	0.2952
T5	4	Fiber	80.00 - 100.00	0.6000	0.2952
T5	5	DC	80.00 - 100.00	0.6000	0.2952
T6	1	1 5/8	60.00 - 80.00	0.6000	0.3065
T6	2	1 5/8 Fiber	60.00 - 80.00	0.6000	0.3065
T6	3	Safety Line 3/8	60.00 - 80.00	0.6000	0.3065

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Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
T6	4	Fiber	60.00 - 80.00	0.6000	0.3063
T6	5	DC	60.00 - 80.00	0.6000	0.3063
T7	1	1 5/8	40.00 - 60.00	0.6000	0.3214
T7	2	1 3/8 Fiber	40.00 - 60.00	0.6000	0.3214
T7	3	Safety Line 3/8	40.00 - 60.00	0.6000	0.3214
T7	4	Fiber	40.00 - 60.00	0.6000	0.3214
T7	5	DC	40.00 - 60.00	0.6000	0.3214
T8	1	1 3/8	20.00 - 40.00	0.6000	0.3431
T8	2	1 5/8 Fiber	20.00 - 40.00	0.6000	0.3431
T8	3	Safety Line 3/8	20.00 - 40.00	0.6000	0.3431
T8	4	Fiber	20.00 - 40.00	0.6000	0.3431
T8	5	DC	20.00 - 40.00	0.6000	0.3431
T9	1	1 5/8	5.00 - 20.00	0.6000	0.3992
T9	2	1 5/8 Fiber	5.00 - 20.00	0.6000	0.3992
T9	3	Safety Line 3/8	5.00 - 20.00	0.6000	0.3992
T9	4	Fiber	5.00 - 20.00	0.6000	0.3992
T9	5	DC	5.00 - 20.00	0.6000	0.3992
T10	1	1 5/8	0.00 - 5.00	0.6000	0.0344
T10	2	1 5/8 Fiber	0.00 - 5.00	0.6000	0.0344
T10	3	Safety Line 3/8	0.00 - 5.00	0.6000	0.0344
T10	4	Fiber	0.00 - 5.00	0.6000	0.0344
T10	5	DC	0.00 - 5.00	0.6000	0.0344

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment °	Placement ft	$C_A A_A$ Front ft^2	$C_A A_A$ Side ft^2	Weight lb	
Sector Frame Mount (AT&T)	A	From Leg	1.50	0.0000	177.00	No Ice	18.00	9.00	465.00
			0.00			1/2" Ice	22.00	11.00	600.00
			0.00			1" Ice	23.20	23.20	735.00
Sector Frame Mount (AT&T)	B	From Leg	1.50	0.0000	177.00	No Ice	18.00	9.00	465.00
			0.00			1/2" Ice	22.00	11.00	600.00
			0.00			1" Ice	23.20	23.20	735.00
Sector Frame Mount (AT&T)	C	From Leg	1.50	0.0000	177.00	No Ice	18.00	9.00	465.00
			0.00			1/2" Ice	22.00	11.00	600.00
			0.00			1" Ice	23.20	23.20	735.00
Lightning Rod	C	None		0.0000	180.00	No Ice	1.00	1.00	40.00
						1/2" Ice	2.02	2.02	49.26
						1" Ice	3.05	3.05	64.89
Powerwave 7770 (AT&T)	A	From Leg	3.00	0.0000	177.00	No Ice	5.51	2.93	35.00
			0.00			1/2" Ice	6.21	3.64	105.10
			0.00			1" Ice	6.93	4.33	195.10
Powerwave 7770 (AT&T)	B	From Leg	3.00	0.0000	177.00	No Ice	5.51	2.93	35.00
			0.00			1/2" Ice	6.21	3.64	105.10
			0.00			1" Ice	6.93	4.33	195.10
Powerwave 7770 (AT&T)	C	From Leg	3.00	0.0000	177.00	No Ice	5.51	2.93	35.00
			0.00			1/2" Ice	6.21	3.64	105.10
			0.00			1" Ice	6.93	4.33	195.10
KMW AM-X-CD-14-65-00T (AT&T)	A	From Leg	3.00	0.0000	177.00	No Ice	4.99	2.83	36.40
			0.00			1/2" Ice	5.62	3.44	104.80

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C _A A _A Front ft ²	C _A A _A Side ft ²	Weight lb	
Powerwave P65-17-XLH-RR (AT&T)	B	From Leg	0.00	0.0000	177.00	1" Ice	6.27	4.05	191.70
			3.00			No Ice	11.47	6.80	62.00
			0.00			1/2" Ice	12.69	8.12	193.70
Commscope SBNH-1D6565C (AT&T)	C	From Leg	0.00	0.0000	177.00	1" Ice	13.90	9.35	356.50
			3.00			No Ice	11.45	7.70	51.80
			0.00			1/2" Ice	12.67	8.99	191.20
Ericsson RRUS11 (AT&T)	A	From Leg	0.00	0.0000	177.00	1" Ice	13.89	10.22	362.10
			3.00			No Ice	2.78	1.19	55.00
			0.00			1/2" Ice	3.16	1.47	99.60
Ericsson RRUS11 (AT&T)	B	From Leg	0.00	0.0000	177.00	1" Ice	3.57	1.79	157.10
			3.00			No Ice	2.78	1.19	55.00
			0.00			1/2" Ice	3.16	1.47	99.60
Ericsson RRUS11 (AT&T)	C	From Leg	0.00	0.0000	177.00	1" Ice	3.57	1.79	157.10
			3.00			No Ice	2.78	1.19	55.00
			0.00			1/2" Ice	3.16	1.47	99.60
(2) Ericsson RRUS32 (AT&T)	A	From Leg	0.00	0.0000	177.00	1" Ice	3.57	1.79	157.10
			3.00			No Ice	2.69	1.57	60.00
			0.00			1/2" Ice	3.09	1.93	103.90
(2) Ericsson RRUS32 (AT&T)	B	From Leg	0.00	0.0000	177.00	1" Ice	3.52	2.31	161.20
			3.00			No Ice	2.69	1.57	60.00
			0.00			1/2" Ice	3.09	1.93	103.90
(2) Ericsson RRUS32 (AT&T)	C	From Leg	0.00	0.0000	177.00	1" Ice	3.52	2.31	161.20
			3.00			No Ice	2.69	1.57	60.00
			0.00			1/2" Ice	3.09	1.93	103.90
(2) Kaelus LGP21901 (AT&T)	A	From Leg	0.00	0.0000	177.00	1" Ice	3.52	2.31	161.20
			3.00			No Ice	0.23	0.11	10.00
			0.00			1/2" Ice	0.35	0.20	15.90
(2) Kaelus LGP21901 (AT&T)	B	From Leg	0.00	0.0000	177.00	1" Ice	0.52	0.33	26.90
			3.00			No Ice	0.23	0.11	10.00
			0.00			1/2" Ice	0.35	0.20	15.90
(2) Kaelus LGP21901 (AT&T)	C	From Leg	0.00	0.0000	177.00	1" Ice	0.52	0.33	26.90
			3.00			No Ice	0.23	0.11	10.00
			0.00			1/2" Ice	0.35	0.20	15.90
(2) Powerwave LGP21401 (AT&T)	A	From Leg	0.00	0.0000	177.00	1" Ice	0.52	0.33	26.90
			3.00			No Ice	1.67	0.47	31.00
			0.00			1/2" Ice	1.96	0.67	55.30
(2) Powerwave LGP21401 (AT&T)	B	From Leg	0.00	0.0000	177.00	1" Ice	2.30	0.90	89.40
			3.00			No Ice	1.67	0.47	31.00
			0.00			1/2" Ice	1.96	0.67	55.30
(2) Powerwave LGP21401 (AT&T)	C	From Leg	0.00	0.0000	177.00	1" Ice	2.30	0.90	89.40
			3.00			No Ice	1.67	0.47	31.00
			0.00			1/2" Ice	1.96	0.67	55.30
CCI TPA-65R-LCUUUU-H8 (AT&T)	A	From Leg	0.00	0.0000	177.00	1" Ice	2.30	0.90	89.40
			3.00			No Ice	13.80	8.82	81.60
			0.00			1/2" Ice	14.51	10.08	248.40
CCI TPA-65R-LCUUUU-H8 (AT&T)	B	From Leg	0.00	0.0000	177.00	1" Ice	15.73	11.30	447.70
			3.00			No Ice	13.80	8.82	81.60
			0.00			1/2" Ice	14.51	10.08	248.40
Quintel QS46512-2 (AT&T)	C	From Leg	0.00	0.0000	177.00	1" Ice	15.73	11.30	447.70
			3.00			No Ice	5.55	5.08	75.00
			0.00			1/2" Ice	6.22	5.75	170.20
(2) Powerwave DBC0061F1V51-2 (AT&T)	A	From Leg	0.00	0.0000	177.00	1" Ice	6.92	6.43	286.30
			3.00			No Ice	0.41	0.43	25.40
			0.00			1/2" Ice	0.57	0.59	37.50
(2) Powerwave DBC0061F1V51-2	B	From Leg	0.00	0.0000	177.00	1" Ice	0.77	0.79	56.60
			3.00			No Ice	0.41	0.43	25.40
			0.00			1/2" Ice	0.57	0.59	37.50

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	Project	Tolland Ave., CT	Date	01:32:09 12/29/17
	Client	CDT	Designed by	FAN

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	C _A A _A Front	C _A A _A Side	Weight
			ft	°	ft	ft ²	ft ²	lb
(AT&T)			0.00			1" Ice 0.77	0.79	36.60
(2) Powerwave DBC0061F1V51-2	C	From Leg	3.00	0.0000	177.00	No Ice 0.41	0.43	25.40
(AT&T)			0.00			1/2" Ice 0.57	0.59	37.50
			0.00			1" Ice 0.77	0.79	36.60

Tower Pressures - No Ice

$G_H = 0.850$

Section Elevation	z	K _Z	q _z	A _G	F a c e	A _F	A _R	A _{leg}	Leg %	C _A A _A In Face	C _A A _A Out Face
ft	ft		psf	ft ²	e	ft ²	ft ²	ft ²		ft ²	ft ²
T1 180.00-160.00	170.00	1.15	24	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.05	58.986
T2 160.00-140.00	150.00	1.11	23	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.05	65.540
T3 140.00-120.00	130.00	1.065	22	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.05	65.540
T4 120.00-100.00	110.00	1.016	21	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.05	65.540
T5 100.00-80.00	90.00	0.959	20	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.05	65.540
T6 80.00-60.00	70.00	0.892	19	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.05	65.540
T7 60.00-40.00	50.00	0.811	17	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.05	65.540
T8 40.00-20.00	30.00	0.701	15	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.05	65.540
T9 20.00-5.00	12.50	0.7	15	56.094	A	2.038	9.126	7.188	64.38	0.563	0.000
					B	2.038	9.126			0.000	0.000
					C	2.038	9.126			64.38	49.155
T10 5.00-0.00	2.50	0.7	15	10.019	A	0.785	3.127	2.584	66.05	0.188	0.000
					B	0.785	3.127			0.000	0.000
					C	0.785	3.127			66.05	16.385

Tower Pressure - With Ice

$G_H = 0.850$

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Section Elevation ft	z ft	K _Z	q _z psf	t _z in	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _d A _A In Face ft ²	C _d A _A Out Face ft ²
T1 180.00-160.00	170.00	1.15	6	2.3563	82.646	A	2.853	57.862	25.292	41.66	10.175	0.000
						B	2.853	57.862			0.000	0.000
						C	2.853	57.862			190.704	0.000
T2 160.00-140.00	150.00	1.11	6	2.3270	82.548	A	2.853	57.296	25.096	41.72	10.058	0.000
						B	2.853	57.296			0.000	0.000
						C	2.853	57.296			211.126	0.000
T3 140.00-120.00	130.00	1.065	6	2.2939	82.438	A	2.853	56.658	24.876	41.80	9.926	0.000
						B	2.853	56.658			0.000	0.000
						C	2.853	56.658			210.262	0.000
T4 120.00-100.00	110.00	1.016	6	2.2559	82.311	A	2.853	55.923	24.623	41.89	9.774	0.000
						B	2.853	55.923			0.000	0.000
						C	2.853	55.923			209.269	0.000
T5 100.00-80.00	90.00	0.959	5	2.2111	82.162	A	2.853	55.058	24.324	42.00	9.594	0.000
						B	2.853	55.058			0.000	0.000
						C	2.853	55.058			208.099	0.000
T6 80.00-60.00	70.00	0.892	5	2.1562	81.979	A	2.853	53.998	23.958	42.14	9.375	0.000
						B	2.853	53.998			0.000	0.000
						C	2.853	53.998			206.667	0.000
T7 60.00-40.00	50.00	0.811	4	2.0849	81.741	A	2.853	52.620	23.482	42.33	9.089	0.000
						B	2.853	52.620			0.000	0.000
						C	2.853	52.620			204.808	0.000
T8 40.00-20.00	30.00	0.701	4	1.9810	81.395	A	2.853	50.614	22.790	42.62	8.674	0.000
						B	2.853	50.614			0.000	0.000
						C	2.853	50.614			202.107	0.000
T9 20.00-5.00	12.50	0.7	4	1.8150	60.631	A	2.038	34.390	16.262	44.64	6.007	0.000
						B	2.038	34.390			0.000	0.000
						C	2.038	34.390			148.349	0.000
T10 5.00-0.00	2.50	0.7	4	1.5452	11.383	A	0.785	10.207	5.362	48.78	1.733	0.000
						B	0.785	10.207			0.000	0.000
						C	0.785	10.207			47.708	0.000

Tower Pressure - Service

$G_H = 0.850$

Section Elevation ft	z ft	K _Z	q _z psf	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _d A _A In Face ft ²	C _d A _A Out Face ft ²
T1 180.00-160.00	170.00	1.15	9	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			58.986	0.000
T2 160.00-140.00	150.00	1.11	9	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			65.540	0.000
T3 140.00-120.00	130.00	1.065	8	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			65.540	0.000
T4 120.00-100.00	110.00	1.016	8	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			65.540	0.000
T5 100.00-80.00	90.00	0.959	8	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			65.540	0.000

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Section Elevation	z	K _Z	q _z	A _G	F a c e	A _F	A _R	A _{leg}	Leg %	C _A A ₁ In Face	C _A A ₁ Out Face
ft	ft		psf	ft ²		ft ²	ft ²	ft ²		ft ²	ft ²
T6 80.00-60.00	70.00	0.892	7	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.540	0.000
T7 60.00-40.00	30.00	0.811	6	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.540	0.000
T8 40.00-20.00	30.00	0.701	5	74.792	A	2.853	12.348	9.583	63.05	0.750	0.000
					B	2.853	12.348			0.000	0.000
					C	2.853	12.348			63.540	0.000
T9 20.00-5.00	12.50	0.7	5	56.094	A	2.038	9.126	7.188	64.38	0.563	0.000
					B	2.038	9.126			0.000	0.000
					C	2.038	9.126			64.38	49.155
T10 5.00-0.00	2.50	0.7	5	10.019	A	0.785	3.127	2.584	66.05	0.188	0.000
					B	0.785	3.127			0.000	0.000
					C	0.785	3.127			66.05	16.385

Tower Forces - No Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-160.00	311.12	658.24 TA 214.38	A	0.203	2.585	24	1	1	9.953	1257.84	62.89	C
			B	0.203	2.585							
			C	0.203	2.585							
T2 160.00-140.00	345.20	658.24	A	0.203	2.585	23	1	1	9.953	1291.16	64.56	C
			B	0.203	2.585							
			C	0.203	2.585							
T3 140.00-120.00	345.20	658.24	A	0.203	2.585	22	1	1	9.953	1239.44	61.97	C
			B	0.203	2.585							
			C	0.203	2.585							
T4 120.00-100.00	345.20	658.24 TA 214.38	A	0.203	2.585	21	1	1	9.953	1181.67	59.08	C
			B	0.203	2.585							
			C	0.203	2.585							
T5 100.00-80.00	345.20	658.24	A	0.203	2.585	20	1	1	9.953	1115.82	55.79	C
			B	0.203	2.585							
			C	0.203	2.585							
T6 80.00-60.00	345.20	658.24	A	0.203	2.585	19	1	1	9.953	1038.51	51.93	C
			B	0.203	2.585							
			C	0.203	2.585							
T7 60.00-40.00	345.20	658.24	A	0.203	2.585	17	1	1	9.953	943.32	47.17	C
			B	0.203	2.585							
			C	0.203	2.585							
T8 40.00-20.00	345.20	658.24	A	0.203	2.585	15	1	1	9.953	815.22	40.76	C
			B	0.203	2.585							
			C	0.203	2.585							
T9 20.00-5.00	258.90	480.27	A	0.199	2.599	15	1	1	7.279	606.19	40.41	C
			B	0.199	2.599							
			C	0.199	2.599							
T10 5.00-0.00	86.30	167.93	A	0.39	2.083	15	1	1	2.762	195.19	39.04	C
			B	0.39	2.083							
			C	0.39	2.083							
Sum Weight:	3072.72	6342.91								9684.35		

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Tower Forces - No Ice - Wind 60 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T1 180.00-160.00	311.12	658.24 TA 214.38	A	0.203	2.585	24	0.8	1	9.383	1227.71	61.39	C
			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T2 160.00-140.00	345.20	658.24	A	0.203	2.585	23	0.8	1	9.383	1262.09	63.10	C
			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T3 140.00-120.00	345.20	658.24	A	0.203	2.585	22	0.8	1	9.383	1211.53	60.58	C
			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T4 120.00-100.00	345.20	658.24 TA 214.38	A	0.203	2.585	21	0.8	1	9.383	1155.06	57.75	C
			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T5 100.00-80.00	345.20	658.24	A	0.203	2.585	20	0.8	1	9.383	1090.70	54.53	C
			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T6 80.00-60.00	345.20	658.24	A	0.203	2.585	19	0.8	1	9.383	1015.13	50.76	C
			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T7 60.00-40.00	345.20	658.24	A	0.203	2.585	17	0.8	1	9.383	922.08	46.10	C
			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T8 40.00-20.00	345.20	658.24	A	0.203	2.585	15	0.8	1	9.383	796.86	39.84	C
			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T9 20.00-5.00	258.90	480.27	A	0.199	2.599	15	0.8	1	6.871	593.01	39.53	C
			B	0.199	2.599		0.8	1	6.871			
			C	0.199	2.599		0.8	1	6.871			
T10 5.00-0.00	86.30	167.93	A	0.39	2.083	15	0.8	1	2.605	191.12	38.22	C
			B	0.39	2.083		0.8	1	2.605			
			C	0.39	2.083		0.8	1	2.605			
Sum Weight:	3072.72	6342.91								9465.28		

Tower Forces - No Ice - Wind 90 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T1 180.00-160.00	311.12	658.24 TA 214.38	A	0.203	2.585	24	0.85	1	9.526	1235.24	61.76	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T2 160.00-140.00	345.20	658.24	A	0.203	2.585	23	0.85	1	9.526	1269.36	63.47	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T3 140.00-120.00	345.20	658.24	A	0.203	2.585	22	0.85	1	9.526	1218.50	60.93	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T4 120.00-100.00	345.20	658.24 TA 214.38	A	0.203	2.585	21	0.85	1	9.526	1161.71	58.09	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			

<h1 style="color: red; margin: 0;">RISATower</h1> <p style="font-size: small; margin-top: 10px;">Phone: FAX:</p>	Job 117-23243.8	Page 21 of 44
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	Client CDT	Designed by FAN

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T5 100.00-80.00	345.20	658.24	A	0.203	2.585	20	0.85	1	9.526	1096.98	34.85	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T6 80.00-60.00	345.20	658.24	A	0.203	2.585	19	0.85	1	9.526	1020.97	31.05	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T7 60.00-40.00	345.20	658.24	A	0.203	2.585	17	0.85	1	9.526	927.39	46.37	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T8 40.00-20.00	345.20	658.24	A	0.203	2.585	15	0.85	1	9.526	801.45	40.07	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T9 20.00-5.00	258.90	480.27	A	0.199	2.599	15	0.85	1	6.973	596.31	39.75	C
			B	0.199	2.599		0.85	1	6.973			
			C	0.199	2.599		0.85	1	6.973			
T10 5.00-0.00	86.30	167.93	A	0.39	2.083	15	0.85	1	2.644	192.14	38.43	C
			B	0.39	2.083		0.85	1	2.644			
			C	0.39	2.083		0.85	1	2.644			
Sum Weight:	3072.72	6342.91								9520.05		

Tower Forces - With Ice - Wind Normal To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T1 180.00-160.00	3492.26	3976.13	A	0.735	1.782	6	1	1	51.234	768.99	38.45	C
			TA	0.735	1.782		1	1	51.234			
			C	0.735	1.782		1	1	51.234			
T2 160.00-140.00	3816.38	3909.50	A	0.729	1.781	6	1	1	50.509	769.36	38.47	C
			B	0.729	1.781		1	1	50.509			
			C	0.729	1.781		1	1	50.509			
T3 140.00-120.00	3764.79	3835.10	A	0.722	1.779	6	1	1	49.698	737.06	36.85	C
			B	0.722	1.779		1	1	49.698			
			C	0.722	1.779		1	1	49.698			
T4 120.00-100.00	3705.82	3750.58 TA 989.70	A	0.714	1.778	6	1	1	48.775	701.21	35.06	C
			B	0.714	1.778		1	1	48.775			
			C	0.714	1.778		1	1	48.775			
T5 100.00-80.00	3636.73	3652.29	A	0.705	1.776	5	1	1	47.699	660.62	33.03	C
			B	0.705	1.776		1	1	47.699			
			C	0.705	1.776		1	1	47.699			
T6 80.00-60.00	3552.80	3533.98	A	0.693	1.776	5	1	1	46.400	613.32	30.67	C
			B	0.693	1.776		1	1	46.400			
			C	0.693	1.776		1	1	46.400			
T7 60.00-40.00	3444.79	3383.50	A	0.679	1.776	4	1	1	44.741	555.58	27.78	C
			B	0.679	1.776		1	1	44.741			
			C	0.679	1.776		1	1	44.741			
T8 40.00-20.00	3289.82	3171.29	A	0.657	1.78	4	1	1	42.387	478.68	23.93	C
			B	0.657	1.78		1	1	42.387			
			C	0.657	1.78		1	1	42.387			
T9 20.00-5.00	2285.57	2054.98	A	0.601	1.803	4	1	1	27.634	360.75	24.05	C
			B	0.601	1.803		1	1	27.634			
			C	0.601	1.803		1	1	27.634			
T10 5.00-0.00	666.99	591.24	A	0.966	2.032	4	1	1	10.992	77.38'	15.48	C

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	Project	Tolland Ave., CT	Date	01:32:09 12/29/17
	Client	CDT	Designed by	FAN

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
Sum Weight:	31655.94	33886.77	B C	0.966 0.966	2.032 2.032		1 1	1 1	10.992 10.992		5722.94	

Tower Forces - With Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-160.00	3492.26	3976.13	A TA B	0.735 0.735 0.735	1.782 1.782 1.782	6	0.8 0.8 0.8	1 1 1	50.663 50.663 50.663	763.58	38.18	C
T2 160.00-140.00	3816.38	3909.50	A B C	0.729 0.729 0.729	1.781 1.781 1.781	6	0.8 0.8 0.8	1 1 1	49.938 49.938 49.938	764.15	38.21	C
T3 140.00-120.00	3764.79	3835.10	A B C	0.722 0.722 0.722	1.779 1.779 1.779	6	0.8 0.8 0.8	1 1 1	49.127 49.127 49.127	732.06	36.60	C
T4 120.00-100.00	3705.82	3750.58 TA 989.70	A B C	0.714 0.714 0.714	1.778 1.778 1.778	6	0.8 0.8 0.8	1 1 1	48.204 48.204 48.204	696.44	34.82	C
T5 100.00-80.00	3636.73	3652.29	A B C	0.705 0.705 0.705	1.776 1.776 1.776	5	0.8 0.8 0.8	1 1 1	47.128 47.128 47.128	656.12	32.81	C
T6 80.00-60.00	3552.80	3533.98	A B C	0.693 0.693 0.693	1.776 1.776 1.776	5	0.8 0.8 0.8	1 1 1	45.829 45.829 45.829	609.14	30.46	C
T7 60.00-40.00	3444.79	3383.50	A B C	0.679 0.679 0.679	1.776 1.776 1.776	4	0.8 0.8 0.8	1 1 1	44.170 44.170 44.170	551.78	27.59	C
T8 40.00-20.00	3289.82	3171.29	A B C	0.657 0.657 0.657	1.78 1.78 1.78	4	0.8 0.8 0.8	1 1 1	41.817 41.817 41.817	475.39	23.77	C
T9 20.00-5.00	2285.57	2054.98	A B C	0.601 0.601 0.601	1.803 1.803 1.803	4	0.8 0.8 0.8	1 1 1	27.226 27.226 27.226	358.38	23.89	C
T10 5.00-0.00	666.99	591.24	A B C	0.966 0.966 0.966	2.032 2.032 2.032	4	0.8 0.8 0.8	1 1 1	10.835 10.835 10.835	76.76	15.35	C
Sum Weight:	31655.94	33886.77								5683.79		

Tower Forces - With Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	

RISATower Phone: FAX:	Job 117-23243.8	Page 23 of 44
	Project Tolland Ave., CT	Date 01:32:09 12/29/17
	Client CDT	Designed by FAN

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-160.00	3492.26	3976.13	A	0.735	1.782	6	0.85	1	30.806	764.93	38.25	C
		TA	B	0.735	1.782		0.85	1	30.806			
		1038.49	C	0.735	1.782		0.85	1	30.806			
T2 160.00-140.00	3816.38	3909.50	A	0.729	1.781	6	0.85	1	30.081	765.45	38.27	C
			B	0.729	1.781		0.85	1	30.081			
			C	0.729	1.781		0.85	1	30.081			
T3 140.00-120.00	3764.79	3835.10	A	0.722	1.779	6	0.85	1	49.270	733.31	36.67	C
			B	0.722	1.779		0.85	1	49.270			
			C	0.722	1.779		0.85	1	49.270			
T4 120.00-100.00	3705.82	3750.58	A	0.714	1.778	6	0.85	1	48.347	697.63	34.88	C
		TA	B	0.714	1.778		0.85	1	48.347			
		989.70	C	0.714	1.778		0.85	1	48.347			
T5 100.00-80.00	3636.73	3652.29	A	0.705	1.776	5	0.85	1	47.271	657.25	32.86	C
			B	0.705	1.776		0.85	1	47.271			
			C	0.705	1.776		0.85	1	47.271			
T6 80.00-60.00	3552.80	3533.98	A	0.693	1.776	5	0.85	1	45.972	610.18	30.51	C
			B	0.693	1.776		0.85	1	45.972			
			C	0.693	1.776		0.85	1	45.972			
T7 60.00-40.00	3444.79	3383.50	A	0.679	1.776	4	0.85	1	44.313	552.73	27.64	C
			B	0.679	1.776		0.85	1	44.313			
			C	0.679	1.776		0.85	1	44.313			
T8 40.00-20.00	3289.82	3171.29	A	0.657	1.78	4	0.85	1	41.959	476.21	23.81	C
			B	0.657	1.78		0.85	1	41.959			
			C	0.657	1.78		0.85	1	41.959			
T9 20.00-5.00	2285.57	2054.98	A	0.601	1.803	4	0.85	1	27.328	358.97	23.93	C
			B	0.601	1.803		0.85	1	27.328			
			C	0.601	1.803		0.85	1	27.328			
T10 5.00-0.00	666.99	591.24	A	0.966	2.032	4	0.85	1	10.874	77.02	15.40	C
			B	0.966	2.032		0.85	1	10.874			
			C	0.966	2.032		0.85	1	10.874			
Sum Weight:	31655.94	33886.77								5693.68		

Tower Forces - Service - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-160.00	311.12	658.24	A	0.203	2.585	9	1	1	9.953	471.49	23.57	C
		TA	B	0.203	2.585		1	1	9.953			
		214.38	C	0.203	2.585		1	1	9.953			
T2 160.00-140.00	345.20	658.24	A	0.203	2.585	9	1	1	9.953	483.98	24.20	C
			B	0.203	2.585		1	1	9.953			
			C	0.203	2.585		1	1	9.953			
T3 140.00-120.00	345.20	658.24	A	0.203	2.585	8	1	1	9.953	464.59	23.23	C
			B	0.203	2.585		1	1	9.953			
			C	0.203	2.585		1	1	9.953			
T4 120.00-100.00	345.20	658.24	A	0.203	2.585	8	1	1	9.953	442.94	22.15	C
		TA	B	0.203	2.585		1	1	9.953			
		214.38	C	0.203	2.585		1	1	9.953			
T5 100.00-80.00	345.20	658.24	A	0.203	2.585	8	1	1	9.953	418.26	20.91	C
			B	0.203	2.585		1	1	9.953			
			C	0.203	2.585		1	1	9.953			
T6 80.00-60.00	345.20	658.24	A	0.203	2.585	7	1	1	9.953	389.28	19.46	C

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	Project	Tolland Ave., CT	Date	01:32:09 12/29/17
	Client	CDT	Designed by	FAN
Phone: FAX:				

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
80.00-60.00			B	0.203	2.585		1	1	9.953			
			C	0.203	2.585		1	1	9.953			
T7	345.20	658.24	A	0.203	2.585	6	1	1	9.953	353.60	17.68	C
60.00-40.00			B	0.203	2.585		1	1	9.953			
			C	0.203	2.585		1	1	9.953			
T8	345.20	658.24	A	0.203	2.585	5	1	1	9.953	305.58	15.28	C
40.00-20.00			B	0.203	2.585		1	1	9.953			
			C	0.203	2.585		1	1	9.953			
T9	258.90	480.27	A	0.199	2.599	5	1	1	7.279	227.22	15.15	C
20.00-5.00			B	0.199	2.599		1	1	7.279			
			C	0.199	2.599		1	1	7.279			
T10	86.30	167.93	A	0.39	2.083	5	1	1	2.762	73.16	14.63	C
5.00-0.00			B	0.39	2.083		1	1	2.762			
			C	0.39	2.083		1	1	2.762			
Sum Weight:	3072.72	6342.91								3630.12		

Tower Forces - Service - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1	311.12	658.24	A	0.203	2.585	9	0.8	1	9.383	460.20	23.01	C
180.00-160.00		TA 214.38	B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T2	345.20	658.24	A	0.203	2.585	9	0.8	1	9.383	473.09	23.65	C
160.00-140.00			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T3	345.20	658.24	A	0.203	2.585	8	0.8	1	9.383	454.13	22.71	C
140.00-120.00			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T4	345.20	658.24	A	0.203	2.585	8	0.8	1	9.383	432.97	21.65	C
120.00-100.00		TA 214.38	B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T5	345.20	658.24	A	0.203	2.585	8	0.8	1	9.383	408.84	20.44	C
100.00-80.00			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T6	345.20	658.24	A	0.203	2.585	7	0.8	1	9.383	380.51	19.03	C
80.00-60.00			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T7	345.20	658.24	A	0.203	2.585	6	0.8	1	9.383	345.64	17.28	C
60.00-40.00			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T8	345.20	658.24	A	0.203	2.585	5	0.8	1	9.383	298.70	14.93	C
40.00-20.00			B	0.203	2.585		0.8	1	9.383			
			C	0.203	2.585		0.8	1	9.383			
T9	258.90	480.27	A	0.199	2.599	5	0.8	1	6.871	222.29	14.82	C
20.00-5.00			B	0.199	2.599		0.8	1	6.871			
			C	0.199	2.599		0.8	1	6.871			
T10	86.30	167.93	A	0.39	2.083	5	0.8	1	2.605	71.64	14.33	C
5.00-0.00			B	0.39	2.083		0.8	1	2.605			
			C	0.39	2.083		0.8	1	2.605			
Sum Weight:	3072.72	6342.91								3548.00		

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	Project	Tolland Ave., CT	Date	01:32:09 12/29/17
	Client	CDT	Designed by	FAN

Tower Forces - Service - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-160.00	311.12	658.24 TA 214.38	A	0.203	2.585	9	0.85	1	9.526	463.02	23.15	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T2 160.00-140.00	345.20	658.24	A	0.203	2.585	9	0.85	1	9.526	475.81	23.79	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T3 140.00-120.00	345.20	658.24	A	0.203	2.585	8	0.85	1	9.526	456.75	22.84	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T4 120.00-100.00	345.20	658.24 TA 214.38	A	0.203	2.585	8	0.85	1	9.526	435.46	21.77	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T5 100.00-80.00	345.20	658.24	A	0.203	2.585	8	0.85	1	9.526	411.20	20.56	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T6 80.00-60.00	345.20	658.24	A	0.203	2.585	7	0.85	1	9.526	382.71	19.14	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T7 60.00-40.00	345.20	658.24	A	0.203	2.585	6	0.85	1	9.526	347.63	17.38	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T8 40.00-20.00	345.20	658.24	A	0.203	2.585	5	0.85	1	9.526	300.42	15.02	C
			B	0.203	2.585		0.85	1	9.526			
			C	0.203	2.585		0.85	1	9.526			
T9 20.00-5.00	258.90	480.27	A	0.199	2.599	5	0.85	1	6.973	223.52	14.90	C
			B	0.199	2.599		0.85	1	6.973			
			C	0.199	2.599		0.85	1	6.973			
T10 5.00-0.00	86.30	167.93	A	0.39	2.083	5	0.85	1	2.644	72.02	14.40	C
			B	0.39	2.083		0.85	1	2.644			
			C	0.39	2.083		0.85	1	2.644			
Sum Weight:	3072.72	6342.91								3568.53		

Discrete Appurtenance Pressures - No Ice $G_H = 0.850$

Description	Aiming Azimuth °	Weight lb	Offset _x ft	Offset _z ft	z ft	K _z	q _z psf	C _{AAC} Front ft ²	C _{AAC} Side ft ²
Torque Arm Face C	180.0000	0.00	0.00	2.53	170.89	1.152	24	3.54	5.32
Torque Arm Face B	60.0000	0.00	2.19	-1.26	170.89	1.152	24	3.54	5.32
Torque Arm Face A	300.0000	0.00	-2.19	-1.26	170.89	1.152	24	3.54	5.32
Torque Arm Face C	180.0000	0.00	0.00	2.53	117.30	1.034	22	3.54	5.32
Torque Arm Face B	60.0000	0.00	2.19	-1.26	117.30	1.034	22	3.54	5.32
Torque Arm Face A	300.0000	0.00	-2.19	-1.26	117.30	1.034	22	3.54	5.32
Sector Frame Mount	0.0000	465.00	0.00	-3.52	177.00	1.163	24	18.00	9.00
Sector Frame Mount	120.0000	465.00	3.05	1.76	177.00	1.163	24	18.00	9.00
Sector Frame Mount	240.0000	465.00	-3.05	1.76	177.00	1.163	24	18.00	9.00
Lightning Rod	0.0000	40.00	0.00	0.00	180.00	1.169	24	1.00	1.00
Powerwave 7770	0.0000	35.00	0.00	-5.02	177.00	1.163	24	5.51	2.93

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	Project	Tolland Ave., CT		Date	01:32:09 12/29/17
	Client	CDT		Designed by	FAN
Phone: FAX:					

Description	Aiming Azimuth °	Weight lb	Offset _x ft	Offset _y ft	z ft	K _c	q _z psf	C _d A _c Front ft ²	C _d A _c Side ft ²	t _c in
Ericsson RRUS11	0.0000	366.68	0.00	-5.02	177.00	1.163	6	8.82	6.29	2.3658
Ericsson RRUS11	120.0000	366.68	4.35	2.51	177.00	1.163	6	8.82	6.29	2.3658
Ericsson RRUS11	240.0000	366.68	-4.35	2.51	177.00	1.163	6	8.82	6.29	2.3658
Ericsson RRUS32	0.0000	733.37	0.00	-5.02	177.00	1.163	6	17.64	12.58	2.3658
Ericsson RRUS32	120.0000	733.37	4.35	2.51	177.00	1.163	6	17.64	12.58	2.3658
Ericsson RRUS32	240.0000	733.37	-4.35	2.51	177.00	1.163	6	17.64	12.58	2.3658
Kaelus LGP21901	0.0000	733.37	0.00	-5.02	177.00	1.163	6	17.64	12.58	2.3658
Kaelus LGP21901	120.0000	733.37	4.35	2.51	177.00	1.163	6	17.64	12.58	2.3658
Kaelus LGP21901	240.0000	733.37	-4.35	2.51	177.00	1.163	6	17.64	12.58	2.3658
Powerwave LGP21401	0.0000	733.37	0.00	-5.02	177.00	1.163	6	17.64	12.58	2.3658
Powerwave LGP21401	120.0000	733.37	4.35	2.51	177.00	1.163	6	17.64	12.58	2.3658
Powerwave LGP21401	240.0000	733.37	-4.35	2.51	177.00	1.163	6	17.64	12.58	2.3658
CCI	0.0000	366.68	0.00	-5.02	177.00	1.163	6	8.82	6.29	2.3658
TPA-65R-LCUUUU-H8										
CCI	120.0000	366.68	4.35	2.51	177.00	1.163	6	8.82	6.29	2.3658
TPA-65R-LCUUUU-H8										
Quintel QS46512-2	240.0000	366.68	-4.35	2.51	177.00	1.163	6	8.82	6.29	2.3658
Powerwave	0.0000	733.37	0.00	-5.02	177.00	1.163	6	17.64	12.58	2.3658
DBC0061F1V51-2										
Powerwave	120.0000	733.37	4.35	2.51	177.00	1.163	6	17.64	12.58	2.3658
DBC0061F1V51-2										
Powerwave	240.0000	733.37	-4.35	2.51	177.00	1.163	6	17.64	12.58	2.3658
DBC0061F1V51-2										
Sum Weight:		16661.95								

Discrete Appurtenance Pressures - Service *G_H* = 0.850

Description	Aiming Azimuth °	Weight lb	Offset _x ft	Offset _y ft	z ft	K _c	q _z psf	C _d A _c Front ft ²	C _d A _c Side ft ²
Torque Arm Face C	180.0000	0.00	0.00	2.53	170.89	1.152	9	3.54	5.32
Torque Arm Face B	60.0000	0.00	2.19	-1.26	170.89	1.152	9	3.54	5.32
Torque Arm Face A	300.0000	0.00	-2.19	-1.26	170.89	1.152	9	3.54	5.32
Torque Arm Face C	180.0000	0.00	0.00	2.53	117.30	1.034	8	3.54	5.32
Torque Arm Face B	60.0000	0.00	2.19	-1.26	117.30	1.034	8	3.54	5.32
Torque Arm Face A	300.0000	0.00	-2.19	-1.26	117.30	1.034	8	3.54	5.32
Sector Frame Mount	0.0000	465.00	0.00	-3.52	177.00	1.163	9	18.00	9.00
Sector Frame Mount	120.0000	465.00	3.05	1.76	177.00	1.163	9	18.00	9.00
Sector Frame Mount	240.0000	465.00	-3.05	1.76	177.00	1.163	9	18.00	9.00
Lightning Rod	0.0000	40.00	0.00	0.00	180.00	1.169	9	1.00	1.00
Powerwave 7770	0.0000	35.00	0.00	-5.02	177.00	1.163	9	5.51	2.93
Powerwave 7770	120.0000	35.00	4.35	2.51	177.00	1.163	9	5.51	2.93
Powerwave 7770	240.0000	35.00	-4.35	2.51	177.00	1.163	9	5.51	2.93
KMW	0.0000	36.40	0.00	-5.02	177.00	1.163	9	4.99	2.83
AM-X-CD-14-65-00T									
Powerwave	120.0000	62.00	4.35	2.51	177.00	1.163	9	11.47	6.80
P65-17-XLH-RR									
Commscope	240.0000	51.80	-4.35	2.51	177.00	1.163	9	11.45	7.70
SBNH-1D6565C									
Ericsson RRUS11	0.0000	55.00	0.00	-5.02	177.00	1.163	9	2.78	1.19
Ericsson RRUS11	120.0000	55.00	4.35	2.51	177.00	1.163	9	2.78	1.19
Ericsson RRUS11	240.0000	55.00	-4.35	2.51	177.00	1.163	9	2.78	1.19
Ericsson RRUS32	0.0000	120.00	0.00	-5.02	177.00	1.163	9	5.38	3.14
Ericsson RRUS32	120.0000	120.00	4.35	2.51	177.00	1.163	9	5.38	3.14
Ericsson RRUS32	240.0000	120.00	-4.35	2.51	177.00	1.163	9	5.38	3.14
Kaelus LGP21901	0.0000	20.00	0.00	-5.02	177.00	1.163	9	0.46	0.22
Kaelus LGP21901	120.0000	20.00	4.35	2.51	177.00	1.163	9	0.46	0.22

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Description	Aiming Azimuth °	Weight lb	Offset _x ft	Offset _y ft	z ft	K _z	q _z psf	C _A Ac Front ft ²	C _A Ac Side ft ²
Kaelus I.GP21901	240.0000	20.00	-4.35	2.51	177.00	1.163	9	0.46	0.22
Powerwave I.GP21401	0.0000	62.00	0.00	-5.02	177.00	1.163	9	3.34	0.94
Powerwave I.GP21401	120.0000	62.00	4.35	2.51	177.00	1.163	9	3.34	0.94
Powerwave I.GP21401	240.0000	62.00	-4.35	2.51	177.00	1.163	9	3.34	0.94
CCI	0.0000	81.60	0.00	-5.02	177.00	1.163	9	13.80	8.82
TPA-65R-LCUUUU-H8									
CCI	120.0000	81.60	4.35	2.51	177.00	1.163	9	13.80	8.82
TPA-65R-LCUUUU-H8									
Quintel QS46512-2	240.0000	75.00	-4.35	2.51	177.00	1.163	9	5.55	5.08
Powerwave	0.0000	50.80	0.00	-5.02	177.00	1.163	9	0.82	0.86
DBC0061F1V51-2									
Powerwave	120.0000	50.80	4.35	2.51	177.00	1.163	9	0.82	0.86
DBC0061F1V51-2									
Powerwave	240.0000	50.80	-4.35	2.51	177.00	1.163	9	0.82	0.86
DBC0061F1V51-2									
Sum Weight:		2851.80							

Force Totals (Does not include forces on guys)

Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Torques lb-ft
Leg Weight	3138.04			
Bracing Weight	3204.87			
Total Member Self-Weight	6342.91			
Guy Weight	2135.83			
Total Weight	14403.26			
Wind 0 deg - No Ice		-38.87	-12370.04	185.02
Wind 30 deg - No Ice		6067.51	-10551.04	1252.02
Wind 60 deg - No Ice		10690.40	-6151.36	2012.51
Wind 90 deg - No Ice		12202.35	38.87	2183.01
Wind 120 deg - No Ice		10729.27	6218.69	1827.49
Wind 150 deg - No Ice		6134.84	10589.91	930.99
Wind 180 deg - No Ice		38.87	12370.04	-185.02
Wind 210 deg - No Ice		-6067.51	10551.04	-1252.02
Wind 240 deg - No Ice		-10690.40	6151.36	-2012.51
Wind 270 deg - No Ice		-12202.35	-38.87	-2183.01
Wind 300 deg - No Ice		-10729.27	-6218.69	-1827.49
Wind 330 deg - No Ice		-6134.84	-10589.91	-930.99
Member Ice	27543.86			
Guy Ice	20618.60			
Total Weight Ice	104959.08			
Wind 0 deg - Ice		15.65	-7622.87	-34.40
Wind 30 deg - Ice		3819.40	-6584.09	263.84
Wind 60 deg - Ice		6625.08	-3824.99	493.73
Wind 90 deg - Ice		7611.69	-15.65	586.95
Wind 120 deg - Ice		6609.42	3797.88	528.12
Wind 150 deg - Ice		3792.29	6568.44	323.11
Wind 180 deg - Ice		-15.65	7622.87	34.40
Wind 210 deg - Ice		-3819.40	6584.09	-263.84
Wind 240 deg - Ice		-6625.08	3824.99	-493.73
Wind 270 deg - Ice		-7611.69	15.65	-586.95
Wind 300 deg - Ice		-6609.42	-3797.88	-528.12
Wind 330 deg - Ice		-3792.29	-6568.44	-323.11
Total Weight	14403.26			
Wind 0 deg - Service		-14.57	-4636.83	69.35

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Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Torques lb-ft
Wind 30 deg - Service		2274.37	-3954.99	469.31
Wind 60 deg - Service		4007.23	-2305.80	754.38
Wind 90 deg - Service		4573.97	14.57	818.29
Wind 120 deg - Service		4021.80	2331.04	685.02
Wind 150 deg - Service		2299.61	3969.56	348.97
Wind 180 deg - Service		14.57	4636.83	-69.35
Wind 210 deg - Service		-2274.37	3954.99	-469.31
Wind 240 deg - Service		-4007.23	2305.80	-754.38
Wind 270 deg - Service		-4573.97	-14.57	-818.29
Wind 300 deg - Service		-4021.80	-2331.04	-685.02
Wind 330 deg - Service		-2299.61	-3969.56	-348.97

Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy
3	1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy
4	1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy
5	1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy
6	1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy
7	1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy
8	1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy
9	1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy
10	1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy
11	1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy
12	1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy
13	1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy
14	1.2 Dead+1.0 Ice+1.0 Temp+Guy
15	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy
16	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy
17	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy
18	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy
19	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy
20	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy
21	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy
22	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy
23	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy
24	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy
25	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy
26	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy
27	Dead+Wind 0 deg - Service+Guy
28	Dead+Wind 30 deg - Service+Guy
29	Dead+Wind 60 deg - Service+Guy
30	Dead+Wind 90 deg - Service+Guy
31	Dead+Wind 120 deg - Service+Guy
32	Dead+Wind 150 deg - Service+Guy
33	Dead+Wind 180 deg - Service+Guy
34	Dead+Wind 210 deg - Service+Guy
35	Dead+Wind 240 deg - Service+Guy
36	Dead+Wind 270 deg - Service+Guy
37	Dead+Wind 300 deg - Service+Guy
38	Dead+Wind 330 deg - Service+Guy

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Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal, X lb	Horizontal, Z lb	
Mast	Max. Vert	23	179800.57	397.59	-68.14	
	Max. H _x	11	73501.20	1604.97	11.43	
	Max. H _z	2	72803.29	-0.04	1674.52	
	Max. M _x	1	0.00	-0.25	18.33	
	Max. M _z	1	0.00	-0.25	18.33	
	Max. Torsion	1	0.00	-0.25	18.33	
	Min. Vert	1	69032.24	-0.25	18.33	
	Min. H _x	5	73501.58	-1605.58	10.87	
	Min. H _z	8	74124.91	-0.60	-1561.27	
	Min. M _x	1	0.00	-0.25	18.33	
	Min. M _z	1	0.00	-0.25	18.33	
	Min. Torsion	1	0.00	-0.25	18.33	
	Guy C @ 145 ft Elev 0 ft Azimuth 240 deg	Max. Vert	10	-7604.09	-7428.12	4296.65
		Max. H _x	10	-7604.09	-7428.12	4296.65
	Max. H _z	17	-28799.59	-33199.88	19165.71	
	Min. Vert	4	-29953.67	-30527.96	17615.05	
	Min. H _x	17	-28799.59	-33199.88	19165.71	
	Min. H _z	10	-7604.09	-7428.12	4296.65	
Guy B @ 145 ft Elev 0 ft Azimuth 120 deg	Max. Vert	6	-7518.86	7368.91	4261.80	
	Max. H _x	25	-28785.79	33189.11	19159.29	
	Max. H _z	25	-28785.79	33189.11	19159.29	
	Min. Vert	12	-30047.08	30594.13	17654.33	
	Min. H _x	6	-7518.86	7368.91	4261.80	
	Min. H _z	6	-7518.86	7368.91	4261.80	
Guy A @ 145 ft Elev 0 ft Azimuth 0 deg	Max. Vert	2	-7584.43	0.53	-8564.30	
	Max. H _x	24	-24105.21	949.22	-32359.08	
	Max. H _z	2	-7584.43	0.53	-8564.30	
	Min. Vert	8	-30032.62	-0.91	-35308.71	
	Min. H _x	18	-24079.40	-949.17	-32338.57	
	Min. H _z	21	-29021.43	0.15	-38490.91	

Tower Mast Reaction Summary

Load Combination	Vertical lb	Shear _x lb	Shear _z lb	Overturning Moment, M _x lb-ft	Overturning Moment, M _z lb-ft	Torque lb-ft
Dead Only	69032.24	0.25	-18.33	0.00	0.00	0.00
1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy	72803.29	0.04	-1674.52	0.00	0.00	0.00
1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy	73492.11	794.38	-1416.68	0.00	0.00	0.00
1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy	74112.54	1371.49	-812.46	0.00	0.00	0.00
1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy	73501.58	1605.58	-10.87	0.00	0.00	0.00

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Load Combination	Vertical lb	Shear _x lb	Shear _z lb	Overturning Moment, M _x lb-ft	Overturning Moment, M _z lb-ft	Torque lb-ft
1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy	72812.43	1431.21	803.11	0.00	0.00	0.00
1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy	73515.17	811.32	1363.66	0.00	0.00	0.00
1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy	74124.91	0.60	1361.27	0.00	0.00	0.00
1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy	73498.75	-810.17	1363.39	0.00	0.00	0.00
1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy	72804.00	-1430.33	804.63	0.00	0.00	0.00
1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy	73501.20	-1604.97	-11.43	0.00	0.00	0.00
1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy	74130.64	-1371.13	-812.96	0.00	0.00	0.00
1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy	73508.31	-794.22	-1416.99	0.00	0.00	0.00
1.2 Dead+1.0 Ice+1.0 Temp+Guy	178330.76	5.11	-168.72	0.00	0.00	0.00
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy	179782.73	5.05	-629.75	0.00	0.00	0.00
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy	179248.16	218.48	-566.64	0.00	0.00	0.00
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy	178746.64	387.26	-385.54	0.00	0.00	0.00
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy	179249.61	459.45	-148.88	0.00	0.00	0.00
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy	179797.79	407.15	67.83	0.00	0.00	0.00
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy	179272.48	245.64	221.29	0.00	0.00	0.00
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy	178777.21	4.68	277.18	0.00	0.00	0.00
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy	179274.48	-236.22	221.48	0.00	0.00	0.00
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy	179800.57	-397.59	68.14	0.00	0.00	0.00
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy	179250.14	-449.68	-148.51	0.00	0.00	0.00
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy	178745.38	-377.30	-385.19	0.00	0.00	0.00
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy	179246.65	-208.38	-566.45	0.00	0.00	0.00
Dead+Wind 0 deg - Service+Guy	69174.08	0.20	-405.09	0.00	0.00	0.00
Dead+Wind 30 deg - Service+Guy	69134.05	189.46	-347.44	0.00	0.00	0.00
Dead+Wind 60 deg - Service+Guy	69095.22	326.72	-206.69	0.00	0.00	0.00
Dead+Wind 90 deg - Service+Guy	69133.53	379.98	-17.46	0.00	0.00	0.00
Dead+Wind 120 deg - Service+Guy	69173.44	335.23	175.22	0.00	0.00	0.00
Dead+Wind 150 deg - Service+Guy	69133.39	190.76	310.31	0.00	0.00	0.00
Dead+Wind 180 deg - Service+Guy	69094.96	0.32	358.79	0.00	0.00	0.00
Dead+Wind 210 deg - Service+Guy	69133.79	-190.13	310.24	0.00	0.00	0.00
Dead+Wind 240 deg - Service+Guy	69173.89	-334.64	175.10	0.00	0.00	0.00
Dead+Wind 270 deg - Service+Guy	69133.75	-379.46	-17.60	0.00	0.00	0.00

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Load Combination	Vertical lb	Shear _x lb	Shear _z lb	Overturning Moment, M _x lb-ft	Overturning Moment, M _z lb-ft	Torque lb-ft
Service+Guy Dead+Wind 300 deg -	69095.12	-326.27	-206.81	0.00	0.00	0.00
Service+Guy Dead+Wind 330 deg -	69133.88	-189.06	-347.51	0.00	0.00	0.00

Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX lb	PY lb	PZ lb	PX lb	PY lb	PZ lb	
1	0.00	-14402.80	0.00	0.00	14402.80	0.02	0.000%
2	-62.19	-17024.38	-22546.72	62.21	17024.35	22540.10	0.023%
3	11082.11	-16856.29	-19261.67	-11081.94	16856.23	19252.79	0.032%
4	19186.68	-16688.20	-11044.24	-19180.85	16688.13	11040.76	0.025%
5	22271.95	-16856.29	62.19	-22264.06	16856.21	-58.07	0.032%
6	19552.43	-17024.38	11327.22	-19546.58	17024.33	-11324.00	0.024%
7	11189.84	-16856.29	19323.87	-11182.03	16856.23	-19319.23	0.032%
8	62.19	-16688.20	22196.20	-62.07	16688.14	-22189.43	0.024%
9	-11082.11	-16856.29	19261.67	11074.51	16856.23	-19257.12	0.032%
10	-19490.24	-17024.38	11219.50	19484.46	17024.33	-11216.29	0.023%
11	-22271.95	-16856.29	-62.19	22264.20	16856.22	66.25	0.031%
12	-19248.88	-16688.20	-11151.96	19243.11	16688.13	11148.39	0.024%
13	-11189.84	-16856.29	-19323.87	11189.70	16856.23	19314.92	0.032%
14	0.00	-107407.72	0.00	-0.01	107406.44	0.19	0.001%
15	15.65	-107633.17	-11296.85	-15.65	107632.10	11271.54	0.023%
16	5652.08	-107407.72	-9758.38	-5645.73	107406.66	9739.55	0.018%
17	9772.94	-107182.27	-5642.41	-9750.04	107180.84	5629.24	0.025%
18	11277.04	-107407.72	-15.65	-11257.65	107406.66	19.39	0.018%
19	9791.19	-107633.17	5634.87	-9769.36	107632.10	-5622.54	0.023%
20	5624.96	-107407.72	9742.72	-5611.92	107406.66	-9728.19	0.018%
21	-15.65	-107182.27	11257.71	15.60	107180.83	-11231.81	0.024%
22	-5652.08	-107407.72	9758.38	5639.01	107406.66	-9743.85	0.018%
23	-9806.84	-107633.17	5661.98	9785.01	107632.10	-5649.64	0.023%
24	-11277.04	-107407.72	15.65	11257.65	107406.66	-11.90	0.018%
25	-9757.29	-107182.27	-5615.30	9734.38	107180.84	5602.16	0.025%
26	-5624.96	-107407.72	-9742.72	5618.63	107406.66	9723.89	0.018%
27	-14.57	-14442.18	-5282.19	14.57	14442.18	5281.41	0.005%
28	2596.29	-14402.80	-4512.57	-2595.93	14402.80	4511.94	0.005%
29	4495.01	-14363.42	-2587.42	-4494.38	14363.42	2587.04	0.005%
30	5217.81	-14402.80	14.57	-5217.09	14402.80	-14.58	0.005%
31	4580.69	-14442.18	2653.71	-4580.02	14442.18	-2653.34	0.005%
32	2621.53	-14402.80	4527.15	-2621.16	14402.80	-4526.53	0.005%
33	14.57	-14363.42	5200.07	-14.57	14363.42	-5199.36	0.005%
34	-2596.29	-14402.80	4512.57	2595.92	14402.80	-4511.95	0.005%
35	-4566.12	-14442.18	2628.47	4565.44	14442.18	-2628.09	0.005%
36	-5217.81	-14402.80	-14.57	5217.09	14402.80	14.56	0.005%
37	-4509.58	-14363.42	-2612.65	4508.96	14363.42	2612.29	0.005%
38	-2621.53	-14402.80	-4527.15	2621.17	14402.80	4526.52	0.005%

Non-Linear Convergence Results

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Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	13	0.00000001	0.00000001
2	Yes	13	0.00000001	0.00007673
3	Yes	13	0.00000001	0.00008320
4	Yes	13	0.00000001	0.00006872
5	Yes	13	0.00000001	0.00008729
6	Yes	13	0.00000001	0.00007607
7	Yes	13	0.00000001	0.00008792
8	Yes	13	0.00000001	0.00006790
9	Yes	13	0.00000001	0.00008480
10	Yes	13	0.00000001	0.00007750
11	Yes	13	0.00000001	0.00008489
12	Yes	13	0.00000001	0.00006815
13	Yes	13	0.00000001	0.00008597
14	Yes	14	0.00132056	0.00119920
15	Yes	15	0.00128545	0.00102677
16	Yes	15	0.00110055	0.00102517
17	Yes	14	0.00147397	0.00120734
18	Yes	15	0.00109099	0.00102447
19	Yes	15	0.00126408	0.00102587
20	Yes	15	0.00107954	0.00102528
21	Yes	14	0.00145458	0.00120876
22	Yes	15	0.00107899	0.00102522
23	Yes	15	0.00126339	0.00102584
24	Yes	15	0.00109159	0.00102448
25	Yes	14	0.00147583	0.00120741
26	Yes	15	0.00110185	0.00102523
27	Yes	13	0.00000001	0.00001541
28	Yes	13	0.00000001	0.00001379
29	Yes	13	0.00000001	0.00001262
30	Yes	13	0.00000001	0.00001365
31	Yes	13	0.00000001	0.00001511
32	Yes	13	0.00000001	0.00001343
33	Yes	13	0.00000001	0.00001214
34	Yes	13	0.00000001	0.00001361
35	Yes	13	0.00000001	0.00001529
36	Yes	13	0.00000001	0.00001367
37	Yes	13	0.00000001	0.00001246
38	Yes	13	0.00000001	0.00001360

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 160	0.824	33	0.0272	0.0232
T2	160 - 140	0.724	33	0.0226	0.0253
T3	140 - 120	0.616	33	0.0293	0.0281
T4	120 - 100	0.491	37	0.0193	0.0257
T5	100 - 80	0.467	27	0.0035	0.0429
T6	80 - 60	0.447	27	0.0107	0.0603
T7	60 - 40	0.390	27	0.0111	0.0725
T8	40 - 20	0.348	27	0.0191	0.0830
T9	20 - 5	0.221	27	0.0425	0.0891
T10	5 - 0	0.060	35	0.0547	0.0912

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Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
180.00	Lightning Rod	33	0.824	0.0272	0.0232	Inf
177.00	Sector Frame Mount	33	0.809	0.0259	0.0234	Inf
170.00	Guy	33	0.774	0.0234	0.0239	Inf
116.42	Guy	37	0.479	0.0158	0.0273	34249
60.38	Guy	27	0.391	0.0111	0.0723	85108

Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 160	3.946	12	0.1331	0.1122
T2	160 - 140	3.443	12	0.1150	0.1205
T3	140 - 120	2.902	12	0.1437	0.1314
T4	120 - 100	2.285	12	0.0985	0.1187
T5	100 - 80	2.116	4	0.0271	0.1861
T6	80 - 60	1.973	4	0.0544	0.2602
T7	60 - 40	1.693	4	0.0532	0.3122
T8	40 - 20	1.493	10	0.0852	0.3571
T9	20 - 5	0.949	10	0.1823	0.3833
T10	5 - 0	0.258	10	0.2351	0.3921

Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
180.00	Lightning Rod	12	3.946	0.1331	0.1122	506558
177.00	Sector Frame Mount	12	3.870	0.1279	0.1129	506558
170.00	Guy	12	3.693	0.1178	0.1149	253278
116.42	Guy	12	2.223	0.0828	0.1250	7618
60.38	Guy	4	1.697	0.0533	0.3113	19299

Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt lb	Allowable Load lb	Ratio Load Allowable	Allowable Ratio	Criteria
T1	180	Leg	A325N	0.7500	4	6.07	29820.60	0.000	✓	1 Bolt Tension
		Torque Arm Top@170	A325N	0.7500	2	6693.75	17892.40	0.374	✓	1 Bolt Shear
		Torque Arm Bottom@170	A325N	0.7500	2	3794.55	17892.40	0.212	✓	1 Bolt Shear

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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt lb	Allowable Load lb	Ratio Load Allowable	Allowable Ratio	Criteria
T2	160	Leg	A325N	0.7500	4	2109.84	29820.60	0.071 ✓	1	Bolt Tension
T3	140	Leg	A325N	0.7500	4	2317.69	29820.60	0.078 ✓	1	Bolt Tension
T4	120	Leg	A325N	0.7500	4	2935.21	29820.60	0.098 ✓	1	Bolt Tension
		Torque Arm Top@116.417	A325N	0.7500	2	4817.44	17892.40	0.269 ✓	1	Bolt Shear
		Torque Arm Bottom@116.417	A325N	0.7500	2	2353.34	17892.40	0.132 ✓	1	Bolt Shear
T5	100	Leg	A325N	0.7500	4	3752.80	29820.60	0.126 ✓	1	Bolt Tension
T6	80	Leg	A325N	0.7500	4	4041.32	29820.60	0.136 ✓	1	Bolt Tension
T7	60	Leg	A325N	0.7500	4	4464.50	29820.60	0.150 ✓	1	Bolt Tension
T8	40	Leg	A325N	0.7500	4	4944.27	29820.60	0.166 ✓	1	Bolt Tension
T9	20	Leg	A325N	0.7500	4	5140.04	29820.60	0.172 ✓	1	Bolt Tension
T10	5	Leg	A325N	0.7500	4	5371.61	29820.60	0.180 ✓	1	Bolt Tension

Guy Design Data

Section No.	Elevation ft	Size	Initial Tension lb	Breaking Load lb	Actual T_n lb	Allowable ϕT_n lb	Required S.F.	Actual S.F.
T1	170.00 (A) (559)	5/8 EHS	6360.00	42399.99	12129.30	25440.00	1.000	2.097 ✓
	170.00 (A) (560)	5/8 EHS	6360.00	42399.99	12127.80	25440.00	1.000	2.098 ✓
	170.00 (B) (553)	5/8 EHS	6360.00	42399.99	11963.50	25440.00	1.000	2.126 ✓
	170.00 (B) (554)	5/8 EHS	6360.00	42399.99	11959.30	25440.00	1.000	2.127 ✓
	170.00 (C) (547)	5/8 EHS	6360.00	42399.99	11966.80	25440.00	1.000	2.126 ✓
	170.00 (C) (548)	5/8 EHS	6360.00	42399.99	11972.00	25440.00	1.000	2.125 ✓
T4	116.42 (A) (577)	9/16 EHS	5250.00	35000.04	9926.60	21000.00	1.000	2.116 ✓
	116.42 (A) (578)	9/16 EHS	5250.00	35000.04	9927.46	21000.00	1.000	2.115 ✓
	116.42 (B) (571)	9/16 EHS	5250.00	35000.04	9940.64	21000.00	1.000	2.113 ✓
	116.42 (B) (572)	9/16 EHS	5250.00	35000.04	9910.20	21000.00	1.000	2.119 ✓
	116.42 (C) (565)	9/16 EHS	5250.00	35000.04	9912.08	21000.00	1.000	2.119 ✓
	116.42 (C) (566)	9/16 EHS	5250.00	35000.04	9940.95	21000.00	1.000	2.112 ✓
T6	60.38 (A) (585)	9/16 EHS	5250.00	35000.04	9811.14	21000.00	1.000	2.140 ✓
	60.38 (B) (584)	9/16 EHS	5250.00	35000.04	9866.54	21000.00	1.000	2.128 ✓
	60.38 (C) (583)	9/16 EHS	5250.00	35000.04	9866.93	21000.00	1.000	2.128 ✓

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Compression Checks

Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	Mast Stability Index	P _u lb	φP _n lb	Ratio P _u / φP _n
T1	180 - 160	P2.5x203	20.00	3.21	40.6 K=1.00	1.7040	1.00	-28526.60	72691.90	0.392 ¹
T2	160 - 140	P2.5x203	20.00	3.21	40.6 K=1.00	1.7040	1.00	-31097.80	72691.90	0.428 ¹
T3	140 - 120	P2.5x203	20.00	3.21	40.6 K=1.00	1.7040	1.00	-37486.80	72691.90	0.516 ¹
T4	120 - 100	P2.5x203	20.00	3.21	40.6 K=1.00	1.7040	1.00	-49461.00	72691.90	0.680 ¹
T5	100 - 80	P2.5x203	20.00	3.21	40.6 K=1.00	1.7040	1.00	-50186.60	72691.90	0.690 ¹
T6	80 - 60	P2.5x203	20.00	3.21	40.6 K=1.00	1.7040	1.00	-53554.90	72691.90	0.737 ¹
T7	60 - 40	P2.5x203	20.00	3.21	40.6 K=1.00	1.7040	0.98	-60085.90	71502.80	0.840 ¹
T8	40 - 20	P2.5x203	20.00	3.21	40.6 K=1.00	1.7040	0.98	-62656.90	71509.50	0.876 ¹
T9	20 - 5	P2.5x203	15.00	3.56	45.1 K=1.00	1.7040	1.00	-62009.10	70516.80	0.879 ¹
T10	5 - 0	P2.5x203	5.39	1.80	22.8 K=1.00	1.7040	0.90	-65726.80	71600.70	0.918 ¹

¹ P_u / φP_n controls

Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio P _u / φP _n
T10	5 - 0	5/8	2.44	1.46	105.4 K=0.94	0.3068	-3915.31	5538.29	0.707 ¹

¹ P_u / φP_n controls

Horizontal Design Data (Compression)

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-6306.64	11503.00	0.548 ¹
T2	160 - 140	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-4878.13	11503.00	0.424 ¹
T3	140 - 120	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-4863.00	11503.00	0.423 ¹
T4	120 - 100	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-4161.94	11503.00	0.362 ¹
T5	100 - 80	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-4206.74	11503.00	0.366 ¹
T6	80 - 60	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-4391.54	11503.00	0.382 ¹
T7	60 - 40	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-4045.38	11503.00	0.352 ¹
T8	40 - 20	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-4168.43	11503.00	0.362 ¹
T9	20 - 5	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-3603.52	11503.00	0.313 ¹
T10	5 - 0	L1 1/2x1 1/2x3/16	2.33	2.09	55.7 K=0.65	0.5273	-1203.55	14513.70	0.083 ¹

¹ P_u / φP_n controls

Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-3019.11	11503.00	0.262 ¹
T2	160 - 140	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-2568.24	11503.00	0.223 ¹
T3	140 - 120	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-2653.61	11503.00	0.231 ¹
T5	100 - 80	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-2317.11	11503.00	0.201 ¹
T6	80 - 60	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-2255.16	11503.00	0.196 ¹
T7	60 - 40	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-2070.69	11503.00	0.180 ¹
T8	40 - 20	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-2052.54	11503.00	0.178 ¹
T9	20 - 5	L1 1/2x1 1/2x3/16	3.50	3.26	86.7 K=0.65	0.5273	-1957.72	11503.00	0.170 ¹

¹ P_u / φP_n controls

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Bottom Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r K=0.65	A in ²	P _u lb	φP _n lb	Ratio P _u / φP _n
T1	180 - 160	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-2669.94	11503.00	0.232 ¹
T2	160 - 140	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-2554.07	11503.00	0.222 ¹
T3	140 - 120	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-3262.64	11503.00	0.284 ¹
T4	120 - 100	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-2333.22	11503.00	0.203 ¹
T5	100 - 80	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-2151.86	11503.00	0.187 ¹
T7	60 - 40	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-2286.95	11503.00	0.199 ¹
T8	40 - 20	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-2081.49	11503.00	0.181 ¹
T9	20 - 5	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-22.16	11503.00	0.002 ¹

¹ P_u / φP_n controls

Top Guy Pull-Off Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r K=0.65	A in ²	P _u lb	φP _n lb	Ratio P _u / φP _n
T1	180 - 160	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-7224.84	11503.00	0.628 ¹
T4	120 - 100	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-3363.92	11503.00	0.292 ¹
T6	80 - 60	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-708.63	11503.00	0.062 ¹

¹ P_u / φP_n controls

Bottom Guy Pull-Off Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r K=0.65	A in ²	P _u lb	φP _n lb	Ratio P _u / φP _n
T1	180 - 160	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-5468.50	11503.00	0.475 ¹
T4	120 - 100	L1 1/2x1 1/2x3/16	3.50	3.26	86.7	0.5273	-6022.88	11503.00	0.524 ¹

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¹ $P_u / \phi P_n$ controls

Torque-Arm Bottom Design Data

Section No.	Elevation <i>ft</i>	Size	<i>L</i> <i>ft</i>	<i>L_n</i> <i>ft</i>	<i>Kl/r</i>	<i>A</i> <i>in²</i>	<i>P_u</i> <i>lb</i>	ϕP_n <i>lb</i>	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160 (551)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-7351.54	36439.50	0.202 ¹
T1	180 - 160 (552)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-7589.10	36439.50	0.208 ¹
T1	180 - 160 (557)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-7435.71	36439.50	0.204 ¹
T1	180 - 160 (558)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-7436.73	36439.50	0.204 ¹
T1	180 - 160 (563)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-7344.47	36439.50	0.202 ¹
T1	180 - 160 (564)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-7583.62	36439.50	0.208 ¹
T4	120 - 100 (569)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-4476.81	36439.50	0.123 ¹
T4	120 - 100 (570)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-4490.54	36439.50	0.123 ¹
T4	120 - 100 (575)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-4706.68	36439.50	0.129 ¹
T4	120 - 100 (576)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-4705.53	36439.50	0.129 ¹
T4	120 - 100 (581)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-4482.28	36439.50	0.123 ¹
T4	120 - 100 (582)	L3x3x1/4	3.50	3.38	68.5 K=1.00	1.4400	-4494.87	36439.50	0.123 ¹

¹ $P_u / \phi P_n$ controls

Tension Checks

Leg Design Data (Tension)

Section No.	Elevation <i>ft</i>	Size	<i>L</i> <i>ft</i>	<i>L_n</i> <i>ft</i>	<i>Kl/r</i>	<i>A</i> <i>in²</i>	<i>P_u</i> <i>lb</i>	ϕP_n <i>lb</i>	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160	P2.5x203	20.00	3.21	40.6	1.7040	0.01	82816.80	0.000 ¹

¹ $P_u / \phi P_n$ controls

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Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	KI/r	A in ²	P _u lb	φP _n lb	Ratio P _u / φP _n
T1	180 - 160	5/8	4.75	4.42	339.7	0.3068	5620.03	9940.20	0.565 ¹
T2	160 - 140	5/8	4.75	4.42	339.7	0.3068	3914.38	9940.20	0.394 ¹
T3	140 - 120	5/8	4.75	4.42	339.7	0.3068	4829.95	9940.20	0.486 ¹
T4	120 - 100	5/8	4.75	4.42	339.7	0.3068	4241.28	9940.20	0.427 ¹
T5	100 - 80	5/8	4.75	4.42	339.7	0.3068	3866.63	9940.20	0.389 ¹
T6	80 - 60	5/8	4.75	4.42	339.7	0.3068	4050.12	9940.20	0.407 ¹
T7	60 - 40	5/8	4.75	4.42	339.7	0.3068	4106.29	9940.20	0.413 ¹
T8	40 - 20	5/8	4.75	4.42	339.7	0.3068	3280.90	9940.20	0.330 ¹
T9	20 - 5	5/8	4.99	4.65	357.3	0.3068	3292.98	9940.20	0.331 ¹

¹ P_u / φP_n controls

Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	KI/r	A in ²	P _u lb	φP _n lb	Ratio P _u / φP _n
T1	180 - 160	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	494.10	17085.90	0.029 ¹
T2	160 - 140	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	538.63	17085.90	0.032 ¹
T3	140 - 120	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	649.29	17085.90	0.038 ¹
T4	120 - 100	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	856.69	17085.90	0.050 ¹
T5	100 - 80	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	869.26	17085.90	0.051 ¹
T6	80 - 60	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	927.60	17085.90	0.054 ¹
T7	60 - 40	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	1040.72	17085.90	0.061 ¹
T8	40 - 20	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	1085.25	17085.90	0.064 ¹
T9	20 - 5	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	1074.03	17085.90	0.063 ¹
T10	5 - 0	L1 1/2x1 1/2x3/16	2.33	2.09	55.0	0.5273	3507.01	17085.90	0.205 ¹

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¹ $P_u / \phi P_n$ controls

Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in ²	P_u lb	ϕP_n lb	Ratio $\frac{P_u}{\phi P_n}$
T9	20 - 5	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	50.32	17085.90	0.003 ¹
T10	5 - 0	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	9976.70	17085.90	0.584 ¹

¹ $P_u / \phi P_n$ controls

Bottom Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in ²	P_u lb	ϕP_n lb	Ratio $\frac{P_u}{\phi P_n}$
T9	20 - 5	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	3485.64	17085.90	0.204 ¹

¹ $P_u / \phi P_n$ controls

Top Guy Pull-Off Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in ²	P_u lb	ϕP_n lb	Ratio $\frac{P_u}{\phi P_n}$
T6	80 - 60	L1 1/2x1 1/2x3/16	3.50	3.26	85.7	0.5273	3336.23	17085.90	0.195 ¹

¹ $P_u / \phi P_n$ controls

Torque-Arm Top Design Data

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in ²	P_u lb	ϕP_n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160 (549)	L2x2x5/16	4.75	4.59	91.6	1.1500	13294.40	37260.00	0.357 ¹
T1	180 - 160 (550)	L2x2x5/16	4.75	4.59	91.6	1.1500	13375.30	37260.00	0.359 ¹
T1	180 - 160 (555)	L2x2x5/16	4.75	4.59	91.6	1.1500	13227.70	37260.00	0.355 ¹

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Section No.	Elevation ft	Size	L ft	L _u ft	KI/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160 (556)	L2x2x5/16	4.75	4.59	91.6	1.1500	13221.80	37260.00	0.355 ¹
T1	180 - 160 (561)	L2x2x5/16	4.75	4.59	91.6	1.1500	13312.40	37260.00	0.357 ¹
T1	180 - 160 (562)	L2x2x5/16	4.75	4.59	91.6	1.1500	13387.50	37260.00	0.359 ¹
T4	120 - 100 (567)	L2x2x5/16	4.75	4.59	91.6	1.1500	9477.59	37260.00	0.254 ¹
T4	120 - 100 (568)	L2x2x5/16	4.75	4.59	91.6	1.1500	9634.88	37260.00	0.259 ¹
T4	120 - 100 (573)	L2x2x5/16	4.75	4.59	91.6	1.1500	9547.23	37260.00	0.256 ¹
T4	120 - 100 (574)	L2x2x5/16	4.75	4.59	91.6	1.1500	9550.55	37260.00	0.256 ¹
T4	120 - 100 (579)	L2x2x5/16	4.75	4.59	91.6	1.1500	9480.13	37260.00	0.254 ¹
T4	120 - 100 (580)	L2x2x5/16	4.75	4.59	91.6	1.1500	9634.64	37260.00	0.259 ¹

¹ P_u / φP_n controls

Torque-Arm Bottom Design Data

Section No.	Elevation ft	Size	L ft	L _u ft	KI/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 160 (551)	L3x3x1/4	3.50	3.38	43.6	1.4400	326.48	46656.00	0.007 ¹
T1	180 - 160 (552)	L3x3x1/4	3.50	3.38	43.6	1.4400	373.17	46656.00	0.008 ¹
T1	180 - 160 (557)	L3x3x1/4	3.50	3.38	43.6	1.4400	459.66	46656.00	0.010 ¹
T1	180 - 160 (558)	L3x3x1/4	3.50	3.38	43.6	1.4400	407.17	46656.00	0.009 ¹
T1	180 - 160 (563)	L3x3x1/4	3.50	3.38	43.6	1.4400	371.82	46656.00	0.008 ¹
T1	180 - 160 (564)	L3x3x1/4	3.50	3.38	43.6	1.4400	365.31	46656.00	0.008 ¹
T4	120 - 100 (569)	L3x3x1/4	3.50	3.38	43.6	1.4400	1512.41	46656.00	0.032 ¹
T4	120 - 100 (570)	L3x3x1/4	3.50	3.38	43.6	1.4400	1499.94	46656.00	0.032 ¹
T4	120 - 100 (575)	L3x3x1/4	3.50	3.38	43.6	1.4400	1710.93	46656.00	0.037 ¹
T4	120 - 100 (576)	L3x3x1/4	3.50	3.38	43.6	1.4400	1709.60	46656.00	0.037 ¹
T4	120 - 100 (581)	L3x3x1/4	3.50	3.38	43.6	1.4400	1517.14	46656.00	0.033 ¹

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T4	120 - 100 (582)	L3x3x1/4	3.50	3.38	43.6	1.4400	1503.31	46656.00	0.032 ¹

¹ P_u / φP_n controls

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	φP _{allow} lb	% Capacity	Pass Fail	
T1	180 - 160	Leg	P2.5x.203	2	-28526.60	72691.90	39.2	Pass	
		Diagonal	5/8	46	5620.03	9940.20	56.5	Pass	
		Horizontal	L1 1/2x1 1/2x3/16	54	-6306.64	11503.00	54.8	Pass	
		Top Girt	L1 1/2x1 1/2x3/16	6	-3019.11	11503.00	26.2	Pass	
		Bottom Girt	L1 1/2x1 1/2x3/16	7	-2669.94	11503.00	23.2	Pass	
		Guy A@170	5/8	559	12129.30	25440.00	47.7	Pass	
		Guy B@170	5/8	553	11963.50	25440.00	47.0	Pass	
		Guy C@170	5/8	548	11972.00	25440.00	47.1	Pass	
		Top Guy	L1 1/2x1 1/2x3/16	45	-7224.84	11503.00	62.8	Pass	
		Pull-Off@170							
		Bottom Guy	L1 1/2x1 1/2x3/16	36	-5468.50	11503.00	47.5	Pass	
		Pull-Off@170							
		Torque Arm Top@170	L2x2x5/16	562	13387.50	37260.00	35.9	Pass	
		Torque Arm Bottom@170	L3x3x1/4	552	-7589.10	36439.50	20.8	Pass	
T2	160 - 140	Leg	P2.5x.203	62	-31097.80	72691.90	42.8	Pass	
		Diagonal	5/8	115	3914.58	9940.20	39.4	Pass	
		Horizontal	L1 1/2x1 1/2x3/16	113	-4878.13	11503.00	42.4	Pass	
		Top Girt	L1 1/2x1 1/2x3/16	66	-2568.24	11503.00	22.3	Pass	
		Bottom Girt	L1 1/2x1 1/2x3/16	67	-2554.07	11503.00	22.2	Pass	
T3	140 - 120	Leg	P2.5x.203	121	-37486.80	72691.90	51.6	Pass	
		Diagonal	5/8	131	4829.95	9940.20	48.6	Pass	
		Horizontal	L1 1/2x1 1/2x3/16	138	-4863.00	11503.00	42.3	Pass	
		Top Girt	L1 1/2x1 1/2x3/16	125	-2653.61	11503.00	23.1	Pass	
		Bottom Girt	L1 1/2x1 1/2x3/16	127	-3262.64	11503.00	28.4	Pass	
T4	120 - 100	Leg	P2.5x.203	181	-49461.00	72691.90	68.0	Pass	
		Diagonal	5/8	226	4241.28	9940.20	42.7	Pass	
		Horizontal	L1 1/2x1 1/2x3/16	198	-4161.94	11503.00	36.2	Pass	
		Bottom Girt	L1 1/2x1 1/2x3/16	187	-2333.22	11503.00	20.3	Pass	
		Guy A@116.417	9/16	578	9927.46	21000.00	47.3	Pass	
		Guy B@116.417	9/16	571	9940.64	21000.00	47.3	Pass	
		Guy C@116.417	9/16	566	9940.95	21000.00	47.3	Pass	
		Top Guy	L1 1/2x1 1/2x3/16	184	-3363.92	11503.00	29.2	Pass	
		Pull-Off@116.417							
		Bottom Guy	L1 1/2x1 1/2x3/16	234	-6022.88	11503.00	52.4	Pass	
		Pull-Off@116.417							
		Torque Arm Top@116.417	L2x2x5/16	568	9634.88	37260.00	25.9	Pass	
		Torque Arm Bottom@116.417	L3x3x1/4	575	-4706.68	36439.50	12.9	Pass	
		T5	100 - 80	Leg	P2.5x.203	242	-50186.60	72691.90	69.0
Diagonal	5/8			295	3866.63	9940.20	38.9	Pass	
Horizontal	L1 1/2x1 1/2x3/16			257	-4206.74	11503.00	36.6	Pass	
Top Girt	L1 1/2x1 1/2x3/16			246	-2317.11	11503.00	20.1	Pass	
Bottom Girt	L1 1/2x1 1/2x3/16			247	-2151.86	11503.00	18.7	Pass	

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Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	σP_{allow} lb	% Capacity	Pass Fail		
T6	80 - 60	Leg	P2.5x.203	301	-53554.90	72691.90	73.7	Pass		
		Diagonal	5/8	313	4030.12	9940.20	40.7	Pass		
		Horizontal	L1 1/2x1 1/2x3/16	317	-4391.34	11303.00	38.2	Pass		
		Top Girt	L1 1/2x1 1/2x3/16	303	-2253.16	11303.00	19.6	Pass		
		Guy A@60.375	9/16	585	9811.14	21000.00	46.7	Pass		
		Guy B@60.375	9/16	584	9866.34	21000.00	47.0	Pass		
		Guy C@60.375	9/16	583	9866.93	21000.00	47.0	Pass		
		Top Guy	L1 1/2x1 1/2x3/16	309	3336.23	17085.90	19.5	Pass		
		Pull-Off@60.375								
		T7	60 - 40	Leg	P2.5x.203	361	-60085.90	71502.80	84.0	Pass
Diagonal	5/8			415	4106.29	9940.20	41.3	Pass		
Horizontal	L1 1/2x1 1/2x3/16			377	-4045.38	11303.00	35.2	Pass		
Top Girt	L1 1/2x1 1/2x3/16			365	-2070.69	11303.00	18.0	Pass		
Bottom Girt	L1 1/2x1 1/2x3/16			367	-2286.95	11303.00	19.9	Pass		
T8	40 - 20	Leg	P2.5x.203	421	-62656.90	71509.50	87.6	Pass		
		Diagonal	5/8	476	3280.90	9940.20	33.0	Pass		
		Horizontal	L1 1/2x1 1/2x3/16	437	-4168.43	11303.00	36.2	Pass		
		Top Girt	L1 1/2x1 1/2x3/16	425	-2052.54	11303.00	17.8	Pass		
		Bottom Girt	L1 1/2x1 1/2x3/16	427	-2081.49	11303.00	18.1	Pass		
T9	20 - 5	Leg	P2.5x.203	481	-62009.10	70516.80	87.9	Pass		
		Diagonal	5/8	492	3292.98	9940.20	33.1	Pass		
		Horizontal	L1 1/2x1 1/2x3/16	497	-3603.52	11303.00	31.3	Pass		
		Top Girt	L1 1/2x1 1/2x3/16	485	-1957.72	11303.00	17.0	Pass		
		Bottom Girt	L1 1/2x1 1/2x3/16	488	3485.64	17085.90	20.4	Pass		
T10	5 - 0	Leg	P2.5x.203	523	-65726.80	71600.70	91.8	Pass		
		Diagonal	5/8	536	-3915.31	5538.29	70.7	Pass		
		Horizontal	L1 1/2x1 1/2x3/16	538	3507.01	17085.90	20.5	Pass		
		Top Girt	L1 1/2x1 1/2x3/16	526	9976.70	17085.90	58.4	Pass		
		Summary								
			Leg (T10)					91.8	Pass	
			Diagonal (T10)					70.7	Pass	
			Horizontal (T1)					54.8	Pass	
			Top Girt (T10)					58.4	Pass	
			Bottom Girt (T3)					28.4	Pass	
			Guy A (T1)					47.7	Pass	
			Guy B (T4)					47.3	Pass	
			Guy C (T4)					47.3	Pass	
	Top Guy					62.8	Pass			
	Pull-Off (T1)									
	Bottom Guy					52.4	Pass			
	Pull-Off (T4)									
	Torque Arm					37.4	Pass			
	Top (T1)									
	Torque Arm					21.2	Pass			
	Bottom (T1)									
	Bolt Checks					37.4	Pass			
	RATING =					91.8	Pass			

Site Name: **Stafford Tolland Ave.**
 Job Number: **117-22243.8**
 Date: **12/29/2018**

Design Base Loads (Factored) per TIA-222-G

Moment (M_u):	0.0 k-ft	Concrete Compressive Strength (f'_c):	3000 psi
Shear/Leg (V_u):	1.7 k	Vertical Steel Rebar Size #:	5
Compression/Leg (P_u):	179.8 k	Vertical Steel Rebar Area:	0.31 in ²
Uplift/Leg (T_u):	0.0 k	# of Vertical Steel Rebars:	5
Tower Type (GT / SST):	GT	Vertical Steel Rebar Yield Strength (F_y):	60 ksi
Diameter of Prismatic Portion of Pier (d):	1.0 ft	Tie / Stirrup Size #:	4
Depth to Base of Foundation:	5.0 ft	Tie / Stirrup Area:	0.20 in ²
Pier Height Above Ground (h):	0.25 ft	Tie / Stirrup Spacing:	10.0 in
Length / Width of Pad (w):	5.5 ft	Tie / Stirrup Steel Yield Strength (F_y):	40 ksi
Thickness of Pad (t):	5.5 ft	Rebar Cage Diameter:	4.0 in
Depth Below Ground Surface to Water Table (w):	10.0 ft	Bending/Tension Reduction Factor (ϕ_B):	0.90
Unit Weight of Concrete:	150.0 pcf	Shear Reduction Factor (ϕ_V):	0.75
Unit Weight of Water:	62.4 pcf	Compression Reduction Factor (ϕ_C):	0.65
Unit Weight of Soil Above Water Table:	110.0 pcf	Steel Elastic Modulus:	29000 ksi
Unit Weight of Soil Below Water Table:	55.0 pcf	Pad Steel Rebar Size #:	5
Friction Angle of Uplift from Top of Pad:	30 Degrees	Pad Steel Rebar Area:	0.31 in ²
Friction Angle of Uplift from Base of Pad:	30 Degrees	Pad Steel Rebar Yield Strength (F_y):	60 ksi
Uplift Angle Started at Top or Base of Pad (T/B):	T	# of Rebar in Top of Pad:	0
Ultimate Skin Friction:	0 psf	# of Rebar in Base of Pad:	5
Ultimate Compressive Bearing Pressure:	12000 psf	Pad Clear Cover:	3 in
Capacity Increase (Due to Transient Loads):	1.00		
Bearing Strength Reduction Factor (ϕ_s):	0.60		
Uplift Strength Reduction Factor (ϕ_s):	0.75		

Axial Capacities and Design Moment

Weight of Concrete (Bouyancy Considered):	24.9 k
Weight of Soil (Bouyancy Considered):	0.0 k
Ultimate Skin Friction Resistance:	0.0 k
Controlling Failure Mode (Top / Base):	Top

Nominal Uplift Capacity per Leg ($\phi_s T_n$):	17.6 k
Nominal Compressive Capacity per Leg ($\phi_s P_n$):	217.8 k
P_u :	187.8 k
$T_u / \phi_s T_n$:	0.00 Result: OK
$P_u / \phi_s P_n$:	0.86 Result: OK

Depth (ft)		Ultimate Lateral Bearing Pressure (psf)	Increment (psf/ft)	γ_{soil} (pcf)	Cohesion (psf)	ϕ (degree)
Top	Bottom					
0.0	2.0	0.0	110.0	110	0	0
2	-0.5	660.0	330.0	110	0	30

Inflection Point (Below Ground Surface):	0.0 ft
Factored Design Moment At Inflection Point (M_u):	0.0 k-ft

Pad Strength Capacity

β :	0.85 ACI318-05 - 10.2.7.3
Lower Pad Flexural Reinforcement Ratio:	0.0004 OK - Minimum Reinforcement Ratio Met - f
Upper Pad Flexural Reinforcement Ratio:	0.0000 OK - Minimum Reinforcement Ratio Met - f
Lower Pad Flexural Reinforcement Spacing:	15 in - Pad Reinforcing Spacing OK - ACI7.12.2.2 & 10.5.4
Upper Pad Flexural Reinforcement Spacing:	0 in - Pad Reinforcing Spacing OK - ACI7.12.2.2 & 10.5.4
One Way Design Shear (V_u):	0.0 k
One Way Shear Capacity (ϕV_c):	341.5 k - ACI318-05 - 11.3.1.1
$V_u / \phi V_c$:	0.00 Result: OK
Punching Design Shear (V_u):	0.0 k
Nominal Punching Shear Capacity ($\phi_c V_n$):	2416.9 k - ACI318-05 - 11.12.2.1
$V_u / \phi V_c$:	0.00 Result: OK
Flexural Loading Due to Soil Pressure (M_u):	85.8 k-ft
Lower Steel Pad Moment Capacity (ϕM_n):	435.3 k-ft - ACI318-05 - 10.3
$M_u / \phi M_n$:	0.20 Result: OK
Flexural Loading Due to Uplift (M_u):	0.0 k-ft
Upper Steel Pad Moment Capacity (ϕM_n):	0.0 k-ft - ACI318-05 - 10.3
$M_u / \phi M_n$:	0.00 Result: OK

Site Name:
 Site Number:
 Date:

Stafford Tolland Ave.
 117-23243.8
 1/3/2018

Design Standard per TIA-222-G

Anchor Radius:	145.0 ft
Uplift (Factored - P_u):	29.0 k
Shear (Factored - V_u):	38.5 k
Anchor Base Depth (d):	8.5 ft
Width of Anchor (W):	5.5 ft
Length of Anchor (L):	11.5 ft
Thickness of Anchor (t):	2.0 ft
Depth Below Ground Surface to Water Table (w):	10.0 ft
Soil Uplift at Base / Top of Anchor (B/T):	T
Unit Weight of Concrete:	150.0 pcf
Unit Weight of Soil Above Water Table:	110.0 pcf
Unit Weight of Water:	62.4 pcf
Submerged Soil Unit Weight:	50.0 pcf
Internal Angle of Friction:	30 Degrees
Cohesion:	0 psf
Ultimate Skin Friction of Pad Sides to Soil:	0 psf
Ultimate Coefficient of Shear Friction:	0.30
Maximum Top Conical Failure Angle:	30 Degrees
Maximum Base Conical Failure Angle:	30 Degrees
Uplift Strength Reduction Factor (ϕ_u):	0.75
Shear Strength Reduction Factor (ϕ_v):	0.75
Concrete Uplift Strength Reduction Factor (ϕ_{uc}):	0.90

Uplift

Weight of Concrete (Buoyancy Effect Considered):	19.0 k
Weight of Soil (Buoyancy Effect Considered):	101.4 k
Ultimate Uplift Resistance from Skin Friction:	0.0 k
Nominal Factored Uplift Resistance ($\phi_u P_n$):	93.1 k
$P_u / \phi_u P_n$:	0.31 Result: OK

Shear

Ultimate Shear Friction Resistance Due to Normal Force - Uplift:	12.7 k
Passive Pressure:	2475 psf
Ultimate Passive Pressure Resistance:	56.9 k
Nominal Shear Resistance ($\phi_v V_n$):	52.2 k
$V_u / \phi_v V_n$:	0.74 Result: OK

Anchor Rod Capacity

# of Anchor Rods:	1	Rod F_y :	49 ksi
Anchor Rod Gross Area:	1.77 in ²	Rod F_u :	62 ksi
Anchor Rod Net Area:	1.77 in ²	ϕ_y :	0.80
Resultant Tensile Load (T_u):	48.2 k	ϕ_t :	0.65
Anchor Rod Tensile Resistance (ϕT_n):	69.3 k		
$T_u / \phi T_n$:	0.70 Result: OK		

Strength Analysis of Reinforced Concrete

Concrete Compressive Strength (f'_c):	3000 psi
Longitudinal Rebar Yield Strength:	60000 psi
# Longitudinal Rebar (Top):	9
# Longitudinal Rebar (1 Side):	3
Rebar Size:	4
Strength Reduction Factor for Shear (ϕ_v):	0.75
Strength Reduction Factor for Flexure (ϕ_b):	0.9
Compression Zone Factor (β_1):	0.85
Area of Single Rebar:	0.20 in ²
One Way Shear due to Shear Load (V_u):	10.6 k
Nominal One Way Shear Capacity for Shear Load ($\phi_v V_n$):	122.3 k
$V_u/\phi_v V_n$:	0.09 Result: OK
One Way Shear due to Uplift (V_u):	12.4 k
Nominal One Way Shear Capacity for Uplift ($\phi_v V_n$):	108.4 k
$V_u/\phi_v V_n$:	0.11 Result: OK
Pad Flexure due to Shear Load (M_u):	55.3 k-ft
Nominal Flexural Capacity for Shear Load ($\phi_b M_n$):	167.4 k-ft
Pad Flexure due to Uplift (M_u):	41.7 k-ft
Nominal Flexural Capacity for Uplift ($\phi_b M_n$):	161.9 k-ft
$M_u/\phi_b M_n$ (Max.):	0.33 Result: OK

Based on our analysis, we have determined that the existing antenna mounts **ARE CAPABLE** of supporting the proposed antenna installation.

	Member	Controlling Load Case	Stress Ratio	Pass/Fail
Existing LTE 2C/3C Mount Rating	31	LC9	87%	PASS

This analysis was conducted in accordance with EIA/TIA-222-G, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and the International Building Code 2012 with 2005 Connecticut Supplement with 2016 Amendments. (See the attached analysis).

This determination was based on the following limitations and assumptions:

1. HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
4. The existing mount has been adequately secured to the tower structure per the mount manufacturer's specifications.
5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
6. HDG performed a localized analysis on the mount itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted,
Hudson Design Group LLC



Michael Cabral
Structural Dept. Head



Daniel P. Hamm, PE
Principal

FIELD PHOTOS:







HUDSON
Design Group LLC

Wind & Ice Calculations

Date: 1/26/2018
 Project Name: STAFFORD SPRINGS TOLLAND AVENUE
 Project Number: CT1185
 Designed By: BD Checked By: MSC



2.6.5.2 Velocity Pressure Coeff:

$$K_z = 2.01 (z/z_g)^{2/\alpha}$$

$K_z =$ **1.163** $z =$ 177 (ft)
 $z_g =$ 1200 (ft)
 $\alpha =$ 7.0

$K_{zmin} \leq K_z \leq 2.01$

Table 2-4

Exposure	Z_g	α	K_{zmin}	K_e
B	1200 ft	7.0	0.70	0.9
C	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

2.6.6.4 Topographic Factor:

Table 2-5

Topo. Category	K_t	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} = [1 + (K_e K_t / K_h)]^2$$

$$K_h = e^{(f * z / H)}$$

$K_{zt} =$ **#DIV/0!**

$K_h =$ #DIV/0!

$K_e =$ 0 (from Table 2-4)

$K_t =$ 0 (from Table 2-5)

$f =$ 0 (from Table 2-5)

$z =$ 177

$H =$ 0 (Ht. of the crest above surrounding terrain)

$K_{zt} =$ 1.00

(If Category 1 then $K_{zt} = 1.0$)

Category = 1

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2.6.7 Gust Effect Factor

2.6.7.1 Self Supporting Lattice Structures

Gh = 1.0 Latticed Structures > 600 ft

Gh = 0.85 Latticed Structures 450 ft or less

$Gh = 0.85 + 0.15 [h/150 - 3.0]$

h= ht. of structure

h= 180

Gh= 0.85

2.6.7.2 Guyed Masts

Gh= 0.85

2.6.7.3 Pole Structures

Gh= 1.1

2.6.9 Appurtenances

Gh= 1.0

2.6.7.4 Structures Supported on Other Structures

(Cantilivered tubular or latticed spines, pole, structures on buildings (ht. : width ratio > 5)

Gh= 1.35

Gh= 1.00

2.6.9.2 Design Wind Force on Appurtenances

$F = q_z * Gh * (EPA)_A$

$q_z = 0.00256 * K_z * K_{zt} * K_d * V_{max}^2 * I$

$K_z = 1.163$

$K_{zt} = 1.0$

$K_d = 0.85$

$V_{max} = 105$

$V_{max(ice)} = 50$

$I = 1.0$

$q_z = 27.91$

$q_z(ice) = 6.33$

Table 2-2

Structure Type	Wind Direction Probability Factor, Kd
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95

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Determine Ca:

Table 2-8

Force Coefficients (Ca) for Appurtenances				
Member Type		Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
		Ca	Ca	Ca
Flat		1.2	1.4	2.0
Round	C < 32 (Subcritical)	0.7	0.8	1.2
	32 ≤ C ≤ 64 (Transitional)	$3.76/(C^{0.485})$	$3.37/(C^{0.415})$	$38.4/(C^{1.0})$
	C > 64 (Supercritical)	0.5	0.6	0.6

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.
(Aspect ratio is independent of the spacing between support points of a linear appurtenance, and the section length considered to have uniform wind load).

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness = **1.00 in**

Appurtenances	Height	Width	Depth	Flat Area	Aspect Ratio	Ca	Force (lbs)	Force (lbs) (1" Ice)
7770 Antenna	55.0	11.0	5.0	4.20	5.00	1.31	154	43
SBNH-1D6565C Antenna	96.4	11.9	7.1	7.97	8.10	1.44	319	86
P65-17-XLH-RR Antenna	96.0	12.0	6.0	8.00	8.00	1.43	320	86
AM-X-CD-14-65-OOT-RET Antenna	48.0	11.8	5.9	3.93	4.07	1.27	139	39
TPA-65R-LCUUUU-H8 Antenna	96.0	14.4	8.6	9.60	6.67	1.39	371	98
QS46512-1 Antenna	52.0	12.0	10.8	4.33	4.33	1.28	155	43
RRU-11 RRH	19.7	17.0	7.2	2.33	1.16	1.20	78	22
RRU-32 B2 RRH	27.2	12.1	7.0	2.29	2.25	1.20	77	22
RRU-32 RRH	27.2	12.1	7.0	2.29	2.25	1.20	77	22
LGP 21401 TMA	14.0	7.0	2.7	0.68	2.00	1.20	23	8
DBC0061F1V51-2 Diplexer	8.0	6.2	6.5	0.34	1.29	1.20	12	4
DC6-48-60-18-8F Surge Arrestor	24.0	9.7	9.7	1.62	2.47	1.20	54	16

WIND LOADS

Angle = **30** (deg)

WIND LOADS WITH NO ICE:

<u>Appurtenances</u>	<u>Height</u>	<u>Width</u>	<u>Depth</u>	<u>Flat Area (normal)</u>	<u>Flat Area (side)</u>	<u>Ratio (normal)</u>	<u>Ratio (side)</u>	<u>Ca (normal)</u>	<u>Ca (side)</u>	<u>Force (lbs) (normal)</u>	<u>Force (lbs) (side)</u>	<u>Force (lbs) (angle)</u>
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	136
SBNH-1D6565C Antenna	96.4	11.9	7.1	7.97	4.75	8.10	13.58	1.44	1.62	319	215	293
P65-17-XLH-RR Antenna	96.0	12.0	6.0	8.00	4.00	8.00	16.00	1.43	1.70	320	190	287
AM-X-CD-14-65-OOT-RET Antenna	48.0	11.8	5.9	3.93	1.97	4.07	8.14	1.27	1.44	139	79	124
TPA-65R-LCUUUU-H8 Antenna	96.0	14.4	8.6	9.60	5.73	6.67	11.16	1.39	1.54	371	246	340
QS46512-1 Antenna	52.0	12.0	10.8	4.33	3.90	4.33	4.81	1.28	1.30	155	142	152
RRU-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21	78	33	67
RRU-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	69
RRU-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	69
LGP 21401 TMA	14.0	7.0	2.7	0.68	0.26	2.00	5.19	1.20	1.32	23	10	20
DBC0061F1V51-2 Diplexer	8.0	6.2	6.5	0.34	0.36	1.29	1.23	1.20	1.20	12	12	12
DC6-48-60-18-8F Surge Arrestor	24.0	9.7	9.7	1.62	1.62	2.47	2.47	1.20	1.20	54	54	54

WIND LOADS

Angle = 60 (deg)

WIND LOADS WITH NO ICE:

<u>Appurtenances</u>	<u>Height</u>	<u>Width</u>	<u>Depth</u>	<u>Flat Area (normal)</u>	<u>Flat Area (side)</u>	<u>Ratio (normal)</u>	<u>Ratio (side)</u>	<u>Ca (normal)</u>	<u>Ca (side)</u>	<u>Force (lbs) (normal)</u>	<u>Force (lbs) (side)</u>	<u>Force (lbs) (angle)</u>
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	100
SBNH-1D6565C Antenna	96.4	11.9	7.1	7.97	4.75	8.10	13.58	1.44	1.62	319	215	241
P65-17-XLH-RR Antenna	96.0	12.0	6.0	8.00	4.00	8.00	16.00	1.43	1.70	320	190	222
AM-X-CD-14-65-OOT-RET Antenna	48.0	11.8	5.9	3.93	1.97	4.07	8.14	1.27	1.44	139	79	94
TPA-65R-LCUUUU-H8 Antenna	96.0	14.4	8.6	9.60	5.73	6.67	11.16	1.39	1.54	371	246	277
QS46512-1 Antenna	52.0	12.0	10.8	4.33	3.90	4.33	4.81	1.28	1.30	155	142	145
RRU-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21	78	33	44
RRU-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	54
RRU-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	54
LGP 21401 TMA	14.0	7.0	2.7	0.68	0.26	2.00	5.19	1.20	1.32	23	10	13
DBC0061F1V51-2 Diplexer	8.0	6.2	6.5	0.34	0.36	1.29	1.23	1.20	1.20	12	12	12
DC6-48-60-18-8F Surge Arrestor	24.0	9.7	9.7	1.62	1.62	2.47	2.47	1.20	1.20	54	54	54

WIND LOADS

Angle = **90** (deg)

WIND LOADS WITH NO ICE:

<u>Appurtenances</u>	<u>Height</u>	<u>Width</u>	<u>Depth</u>	<u>Flat Area (normal)</u>	<u>Flat Area (side)</u>	<u>Ratio (normal)</u>	<u>Ratio (side)</u>	<u>Ca (normal)</u>	<u>Ca (side)</u>	<u>Force (lbs)</u>	<u>Force (lbs)</u>	<u>Force (lbs)</u>
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	82
SBNH-1D6565C Antenna	96.4	11.9	7.1	7.97	4.75	8.10	13.58	1.44	1.62	319	215	215
P65-17-XLH-RR Antenna	96.0	12.0	6.0	8.00	4.00	8.00	16.00	1.43	1.70	320	190	190
AM-X-CD-14-65-OOT-RET Antenna	48.0	11.8	5.9	3.93	1.97	4.07	8.14	1.27	1.44	139	79	79
TPA-65R-LCUUUU-H8 Antenna	96.0	14.4	8.6	9.60	5.73	6.67	11.16	1.39	1.54	371	246	246
QS46512-1 Antenna	52.0	12.0	10.8	4.33	3.90	4.33	4.81	1.28	1.30	155	142	142
RRU-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21	78	33	33
RRU-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	47
RRU-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	47
LGP 21401 TMA	14.0	7.0	2.7	0.68	0.26	2.00	5.19	1.20	1.32	23	10	10
DBC0061F1V51-2 Diplexer	8.0	6.2	6.5	0.34	0.36	1.29	1.23	1.20	1.20	12	12	12
DC6-48-60-18-8F Surge Arrestor	24.0	9.7	9.7	1.62	1.62	2.47	2.47	1.20	1.20	54	54	54

Date: 1/26/2018
 Site No.: CT1185
 Site Name: STAFFORD SPRINGS TOLLAND AVENUE
 Done by: BD Checked by: MSC



ICE WEIGHT CALCULATIONS

Thickness of ice (in): 1.00
 * Density of ice used = 56 PCF

7770 Antenna

Weight of ice based on total radial SF area:
 Depth (in): 5.0
 height (in): 55.0
 Width (in): 11.0
 Total weight of ice on object: 61 lbs
 Weight of object: 35 lbs
Combined weight of ice and object: 96 lbs

P65-17-XLH-RR Antenna

Weight of ice based on total radial SF area:
 Depth (in): 6.0
 height (in): 96.0
 Width (in): 12.0
 Total weight of ice on object: 117 lbs
 Weight of object: 70 lbs
Combined weight of ice and object: 187 lbs

TPA-65R-LCUUUU-H8 Antenna

Weight of ice based on total radial SF area:
 Depth (in): 8.6
 height (in): 96.0
 Width (in): 14.4
 Total weight of ice on object: 151 lbs
 Weight of object: 75 lbs
Combined weight of ice and object: 226 lbs

RRU-11 RRH

Weight of ice based on total radial SF area:
 Depth (in): 7.2
 height (in): 19.7
 Width (in): 17.0
 Total weight of ice on object: 39 lbs
 Weight of object: 51 lbs
Combined weight of ice and object: 90 lbs

RRU-32 B2 RRH

Weight of ice based on total radial SF area:
 Depth (in): 7.0
 height (in): 27.2
 Width (in): 12.1
 Total weight of ice on object: 39 lbs
 Weight of object: 60 lbs
Combined weight of ice and object: 99 lbs

DBC0061F1V51-2 Dplxers

Weight of ice based on total radial SF area:
 Depth (in): 6.5
 height (in): 8.0
 Width (in): 6.2
 Total weight of ice on object: 9 lbs
 Weight of object: 26 lbs
Combined weight of ice and object: 35 lbs

HSS 3x3

Weight of ice based on total radial SF area:
 Depth (in): 3
 height (in): 12
 Width (in): 3
Per foot weight of ice on object: 5 lbs/ft

L 2-1/2x2-1/2x3/16

Weight of ice based on total radial SF area:
 Depth (in): 2.5
 height (in): 12
 Width (in): 2.5
Per foot weight of ice on object: 4 lbs/ft

LU 3x2x1/4

Weight of ice based on total radial SF area:
 Depth (in): 2
 height (in): 12
 Width (in): 3
Per foot weight of ice on object: 4 lbs/ft

SBNH-1D6565C Antenna

Weight of ice based on total radial SF area:
 Depth (in): 7.1
 height (in): 96.4
 Width (in): 11.9
 Total weight of ice on object: 124 lbs
 Weight of object: 66 lbs
Combined weight of ice and object: 190 lbs

AM-X-CD-14-65-OOT-RET Antenna

Weight of ice based on total radial SF area:
 Depth (in): 5.9
 height (in): 48.0
 Width (in): 11.8
 Total weight of ice on object: 60 lbs
 Weight of object: 37 lbs
Combined weight of ice and object: 97 lbs

QS46512-1 Antenna

Weight of ice based on total radial SF area:
 Depth (in): 10.8
 height (in): 52.0
 Width (in): 12.0
 Total weight of ice on object: 85 lbs
 Weight of object: 75 lbs
Combined weight of ice and object: 160 lbs

RRU-32 RRH

Weight of ice based on total radial SF area:
 Depth (in): 7.0
 height (in): 27.2
 Width (in): 12.1
 Total weight of ice on object: 39 lbs
 Weight of object: 60 lbs
Combined weight of ice and object: 99 lbs

LGP 21401 TMA

Weight of ice based on total radial SF area:
 Depth (in): 2.7
 height (in): 14.0
 Width (in): 7.0
 Total weight of ice on object: 10 lbs
 Weight of object: 19 lbs
Combined weight of ice and object: 29 lbs

DC6-48-60-18-8F Surge Arrestor

Per foot weight of ice:
 Diameter (in): 9.7
 height (in): 24
 Total weight of ice on object: 12 lbs
 Weight of object: 33 lbs
Combined weight of ice and object: 45 lbs

2" pipe

Per foot weight of ice:
 diameter (in): 2.375
Per foot weight of ice on object: 3 lbs/ft

2-1/2" pipe

Per foot weight of ice:
 diameter (in): 2.875
Per foot weight of ice on object: 4 lbs/ft

L 2x2x3/16

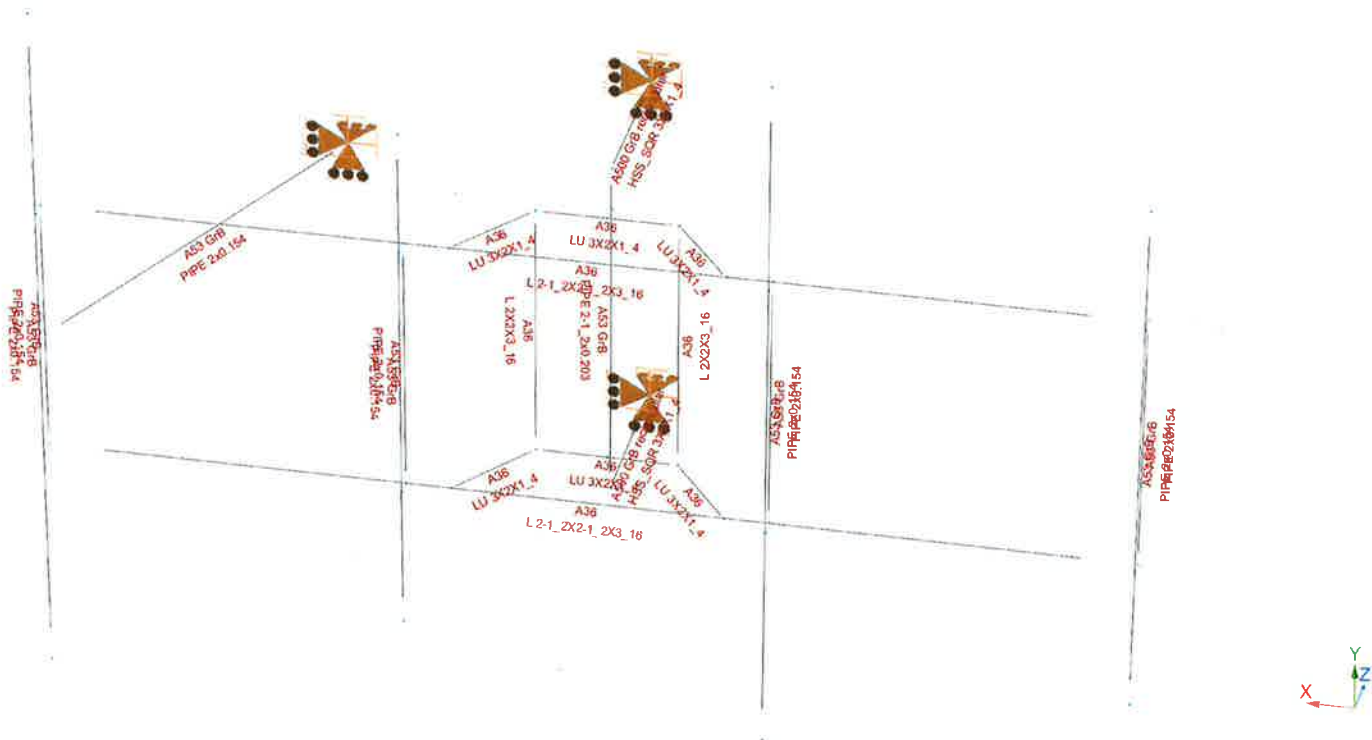
Weight of ice based on total radial SF area:
 Depth (in): 2.5
 height (in): 12
 Width (in): 2.5
Per foot weight of ice on object: 4 lbs/ft

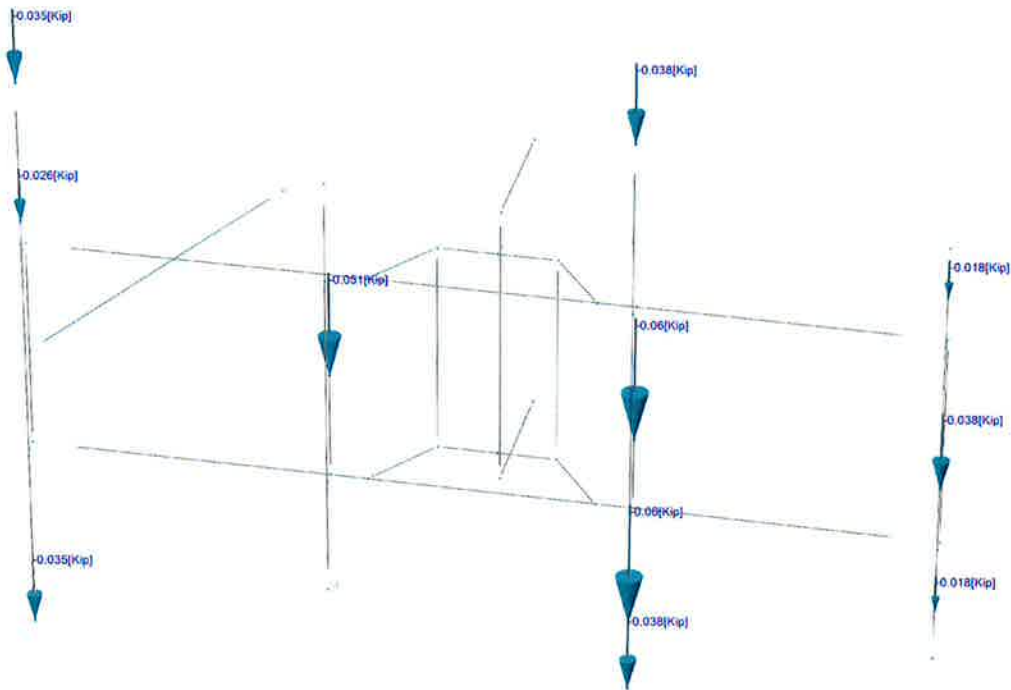


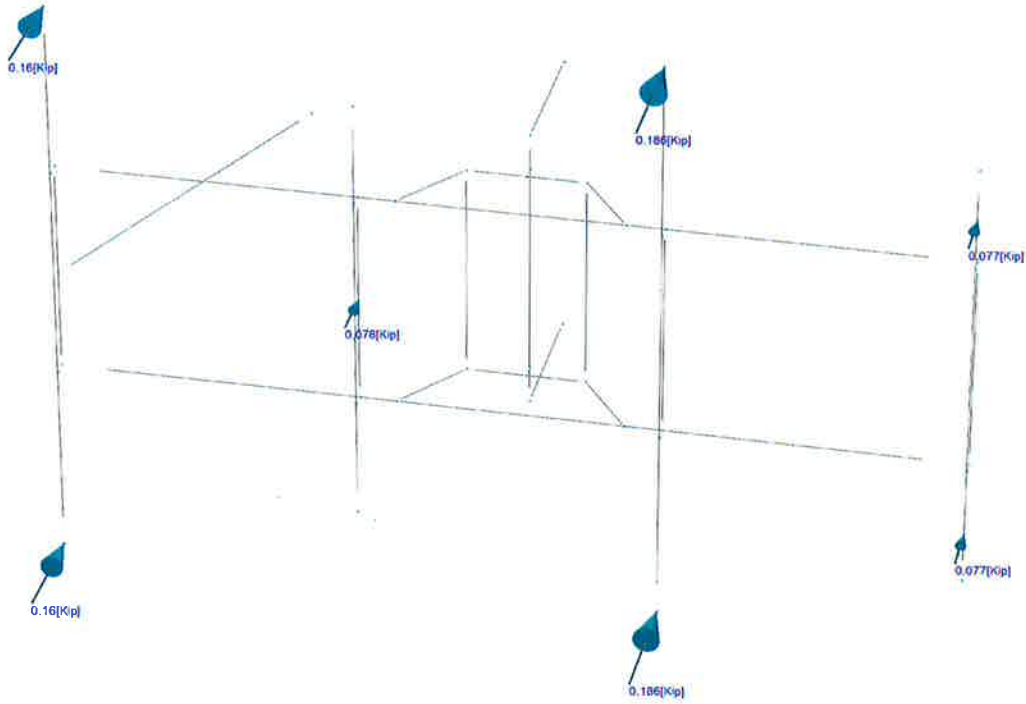
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**Mount Calculations
(Existing Conditions)**



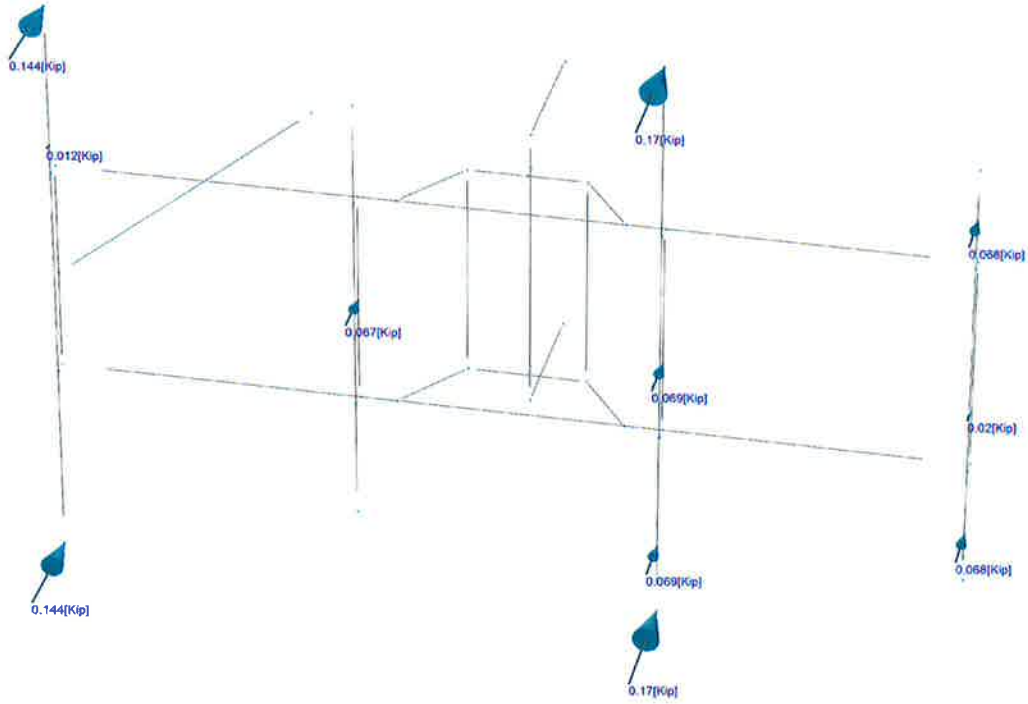






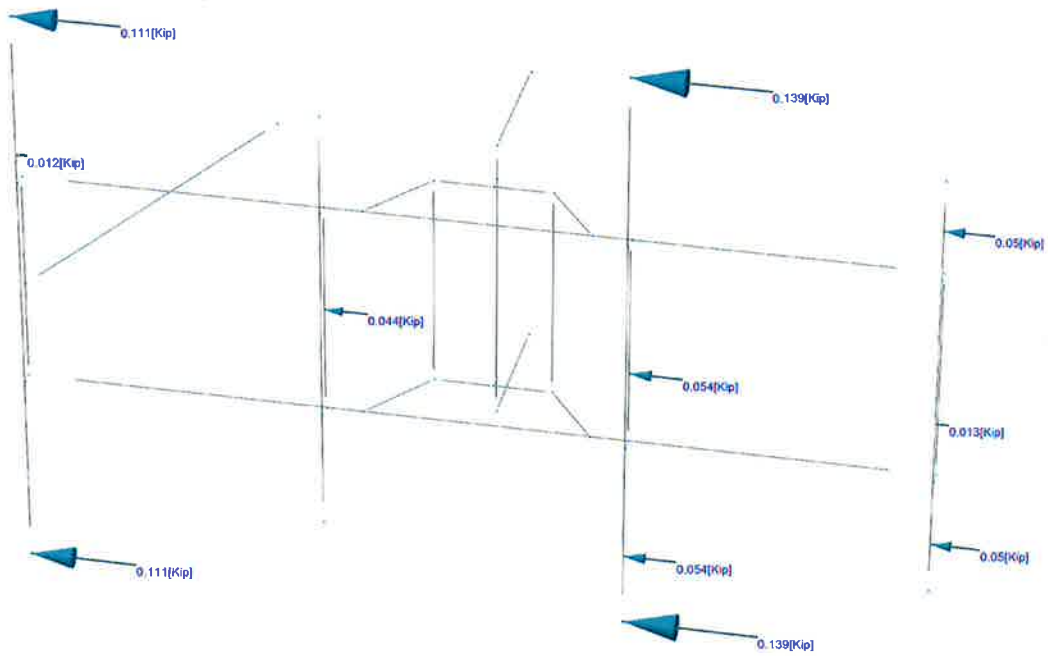
Loads

■ Concentrated user loads - Members



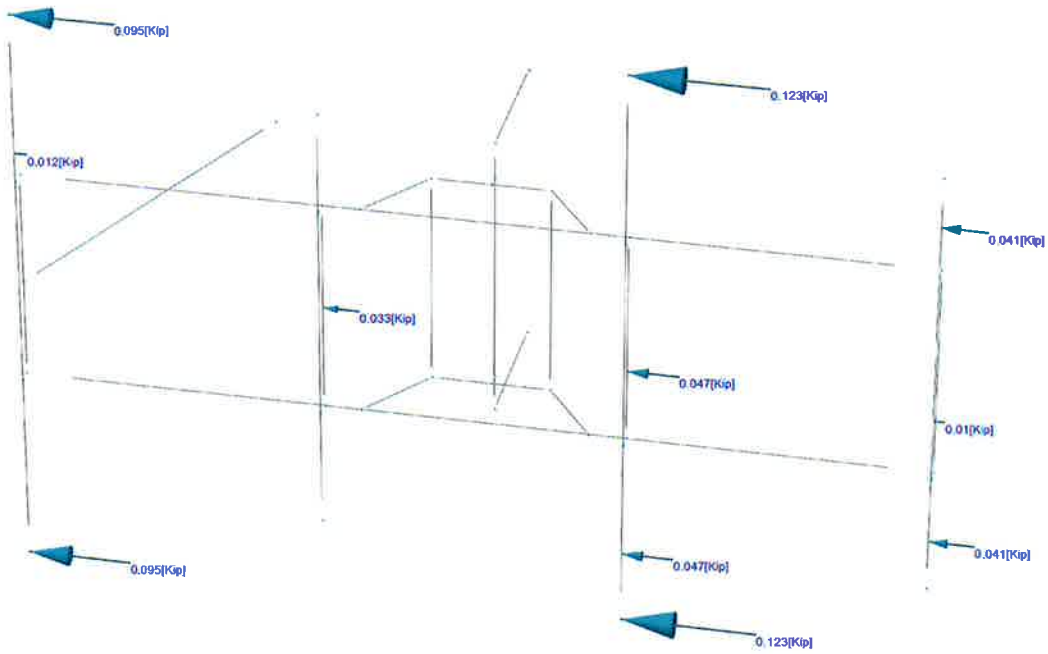
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Concentrated user loads - Members



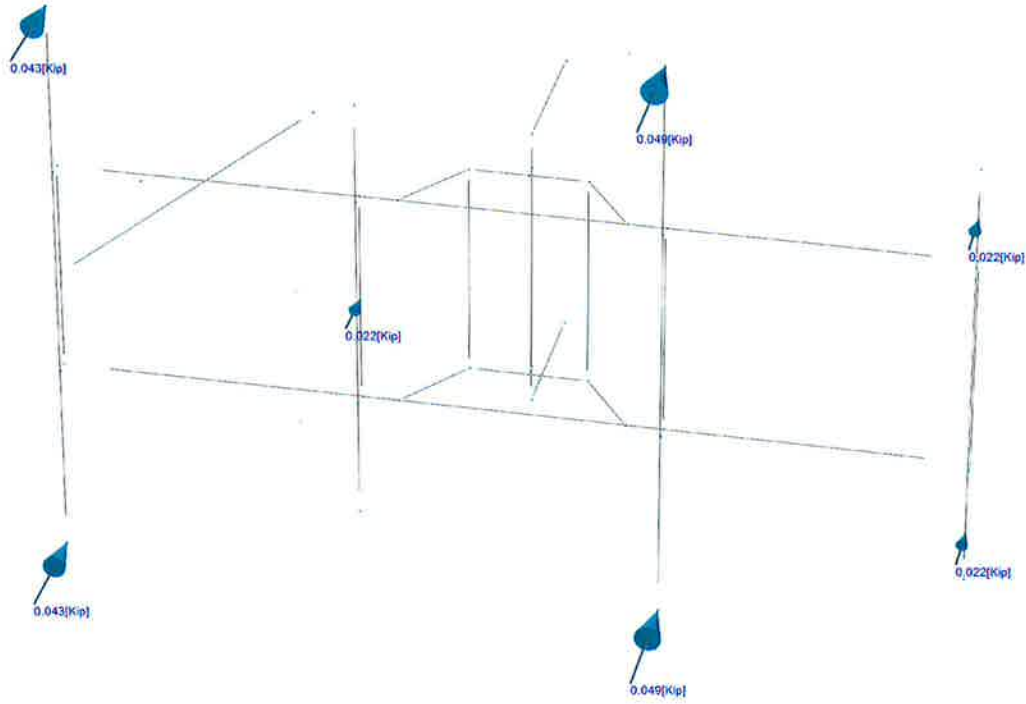
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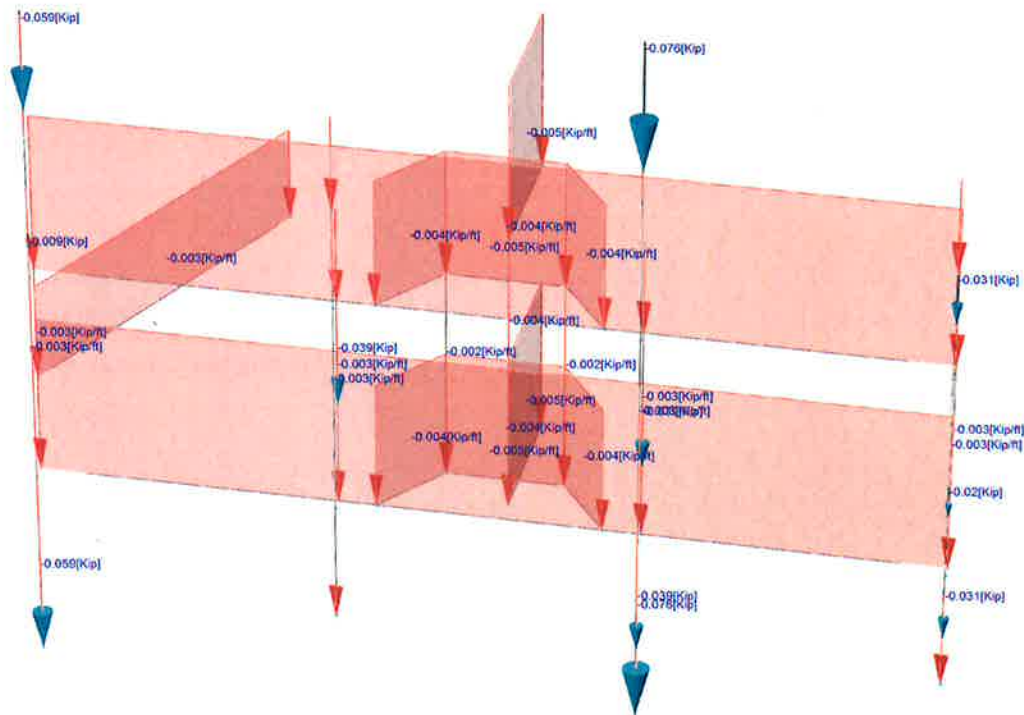
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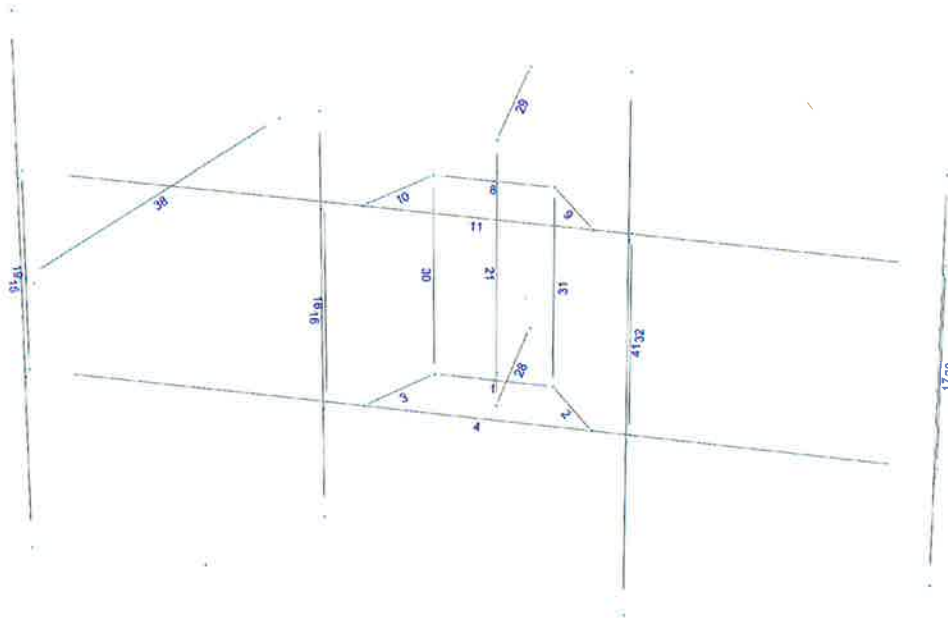
■ Concentrated user loads - Members







Loads

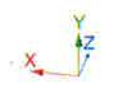
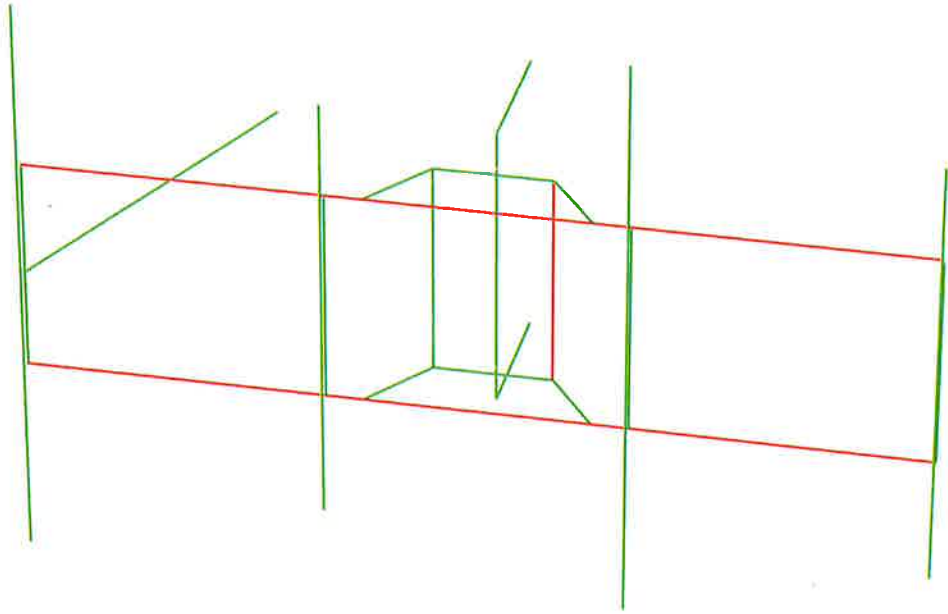
- Distributed user loads - Members
- Concentrated user loads - Members





Design status

-  Not designed
-  Error on design
-  Design O.K.
-  With warnings



Rebecca Campbell

From: Rebecca Campbell
Sent: Sunday, January 28, 2018 10:40 AM
To: Rebecca Campbell
Subject: finish ME drop box for ProV

From: Rebecca Campbell
Sent: Sunday, January 28, 2018 10:13 AM
To: Rebecca Campbell <rcampbell@hudsondesigngroupllc.com>
Subject: timesheet from weekend

Timesheet

Prov – Sprint/Smartlink site drop box data 1.5 hr

SAI/AT+T – scheduling mapping meeting makers 1.5

Becky Campbell
Field Tech Manager

Hudson Design Group LLC
45 Beechwood Drive
North Andover, MA 01845



office: 978.557.5553 x247
mobile: 978.729.5191
www.hudsondesigngroupllc.com

Current Date: 1/29/2018 9:37 AM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1185\CT1185.etz\

Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design :

- LC1=1.2D+1.6Wo
- LC2=1.2D+1.6W30
- LC3=1.2D+1.6W60
- LC4=1.2D+1.6W90
- LC5=0.9D+1.6Wo
- LC6=0.9D+1.6W30
- LC7=0.9D+1.6W60
- LC8=0.9D+1.6W90
- LC9=1.2D+Wi+Di
- LC10=1.2D
- LC11=0.9D

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	<i>HSS_SQR 3X3X1_4</i>	28	LC1 at 100.00%	0.19	OK	
			LC10 at 0.00%	0.12	OK	
			LC11 at 0.00%	0.09	OK	
			LC2 at 100.00%	0.23	OK	Eq. H1-1b
			LC3 at 0.00%	0.42	OK	Eq. H1-1b
			LC4 at 0.00%	0.38	OK	
			LC5 at 100.00%	0.18	OK	
			LC6 at 100.00%	0.21	OK	
			LC7 at 0.00%	0.39	OK	
			LC8 at 0.00%	0.35	OK	
			LC9 at 0.00%	0.22	OK	
		29	LC1 at 0.00%	0.14	OK	
			LC10 at 0.00%	0.12	OK	
			LC11 at 0.00%	0.09	OK	
			LC2 at 0.00%	0.15	OK	
			LC3 at 0.00%	0.33	OK	Eq. H1-1b
			LC4 at 0.00%	0.30	OK	
			LC5 at 0.00%	0.11	OK	
			LC6 at 0.00%	0.12	OK	
			LC7 at 0.00%	0.31	OK	
			LC8 at 0.00%	0.28	OK	
			LC9 at 0.00%	0.24	OK	
	<i>L 2-1_2X2-1_2X3_16</i>	4	LC1 at 36.25%	1.31	N.G.	
			LC10 at 100.00%	0.37	With warnings	
			LC11 at 100.00%	0.28	With warnings	
			LC2 at 36.25%	1.38	N.G.	Eq. H2-1
			LC3 at 62.50%	0.81	With warnings	
			LC4 at 62.50%	0.70	With warnings	
			LC5 at 36.25%	1.26	N.G.	
			LC6 at 36.25%	1.33	N.G.	
			LC7 at 62.50%	0.80	With warnings	
			LC8 at 62.50%	0.69	With warnings	
			LC9 at 33.75%	0.76	With warnings	
		11	LC1 at 36.25%	1.12	N.G.	
			LC10 at 100.00%	0.30	With warnings	

		LC11 at 100.00%	0.22	With warnings	
		LC2 at 36.25%	1.20	N.G.	Eq. H2-1
		LC3 at 62.50%	0.64	With warnings	
		LC4 at 62.50%	0.55	With warnings	
		LC5 at 36.25%	1.12	N.G.	
		LC6 at 36.25%	1.20	N.G.	
		LC7 at 62.50%	0.63	With warnings	
		LC8 at 62.50%	0.54	With warnings	
		LC9 at 67.50%	0.63	With warnings	Eq. H2-1
L 2X2X3_16	30	LC1 at 100.00%	0.38	OK	
		LC10 at 0.00%	0.42	OK	
		LC11 at 0.00%	0.31	OK	
		LC2 at 100.00%	0.40	OK	
		LC3 at 0.00%	0.45	OK	
		LC4 at 0.00%	0.45	OK	
		LC5 at 100.00%	0.30	OK	
		LC6 at 100.00%	0.32	OK	
		LC7 at 0.00%	0.35	OK	
		LC8 at 0.00%	0.34	OK	
		LC9 at 0.00%	0.80	OK	Sec. F1
	31	LC1 at 100.00%	0.55	OK	
		LC10 at 100.00%	0.56	OK	
		LC11 at 100.00%	0.42	OK	
		LC2 at 100.00%	0.51	OK	
		LC3 at 100.00%	0.55	OK	
		LC4 at 100.00%	0.55	OK	
		LC5 at 100.00%	0.41	OK	
		LC6 at 100.00%	0.37	OK	
		LC7 at 100.00%	0.41	OK	
		LC8 at 100.00%	0.41	OK	
		LC9 at 100.00%	1.08	N.G.	Sec. F1
LU 3X2X1_4	1	LC1 at 46.88%	0.63	OK	
		LC10 at 46.88%	0.21	OK	
		LC11 at 46.88%	0.16	OK	
		LC2 at 46.88%	0.80	OK	Eq. H2-1
		LC3 at 46.88%	0.28	OK	
		LC4 at 46.88%	0.27	OK	
		LC5 at 46.88%	0.59	OK	
		LC6 at 46.88%	0.76	OK	
		LC7 at 46.88%	0.23	OK	
		LC8 at 46.88%	0.22	OK	
		LC9 at 46.88%	0.42	OK	
	2	LC1 at 100.00%	0.78	OK	
		LC10 at 0.00%	0.20	OK	
		LC11 at 0.00%	0.15	OK	
		LC2 at 100.00%	0.86	OK	Eq. H2-1
		LC3 at 0.00%	0.31	OK	
		LC4 at 0.00%	0.29	OK	
		LC5 at 100.00%	0.76	OK	
		LC6 at 100.00%	0.85	OK	
		LC7 at 0.00%	0.27	OK	
		LC8 at 0.00%	0.25	OK	
		LC9 at 0.00%	0.38	OK	
	3	LC1 at 100.00%	0.61	OK	
		LC10 at 0.00%	0.31	OK	
		LC11 at 0.00%	0.23	OK	
		LC2 at 100.00%	0.74	OK	Eq. H2-1
		LC3 at 100.00%	0.43	OK	
		LC4 at 100.00%	0.37	OK	

		LC5 at 100.00%	0.60	OK	
		LC6 at 100.00%	0.74	OK	
		LC7 at 100.00%	0.43	OK	
		LC8 at 100.00%	0.37	OK	
		LC9 at 0.00%	0.61	OK	Eq. H2-1
8		LC1 at 46.88%	0.55	OK	
		LC10 at 46.88%	0.29	OK	
		LC11 at 46.88%	0.22	OK	
		LC2 at 46.88%	0.53	OK	
		LC3 at 100.00%	0.43	OK	Eq. H2-1
		LC4 at 100.00%	0.39	OK	
		LC5 at 46.88%	0.57	OK	Eq. H2-1
		LC6 at 46.88%	0.55	OK	
		LC7 at 100.00%	0.39	OK	
		LC8 at 100.00%	0.35	OK	
		LC9 at 50.00%	0.50	OK	Eq. H2-1
9		LC1 at 100.00%	0.59	OK	
		LC10 at 0.00%	0.42	OK	
		LC11 at 0.00%	0.31	OK	
		LC2 at 100.00%	0.61	OK	
		LC3 at 0.00%	0.46	OK	
		LC4 at 0.00%	0.46	OK	
		LC5 at 100.00%	0.59	OK	
		LC6 at 100.00%	0.62	OK	Eq. H2-1
		LC7 at 0.00%	0.36	OK	
		LC8 at 0.00%	0.35	OK	
		LC9 at 0.00%	0.81	OK	Eq. H2-1
10		LC1 at 100.00%	0.62	OK	
		LC10 at 0.00%	0.15	OK	
		LC11 at 0.00%	0.11	OK	
		LC2 at 100.00%	0.65	OK	
		LC3 at 100.00%	0.49	OK	
		LC4 at 100.00%	0.43	OK	
		LC5 at 100.00%	0.64	OK	
		LC6 at 100.00%	0.67	OK	Eq. H2-1
		LC7 at 100.00%	0.47	OK	
		LC8 at 100.00%	0.41	OK	
		LC9 at 0.00%	0.33	OK	
PIPE 2-1_2x0.203	21	LC1 at 100.00%	0.36	OK	
		LC10 at 100.00%	0.14	OK	
		LC11 at 100.00%	0.10	OK	
		LC2 at 100.00%	0.45	OK	Eq. H3-6
		LC3 at 0.00%	0.19	OK	
		LC4 at 0.00%	0.18	OK	
		LC5 at 100.00%	0.32	OK	
		LC6 at 100.00%	0.40	OK	
		LC7 at 87.50%	0.17	OK	
		LC8 at 0.00%	0.15	OK	
		LC9 at 100.00%	0.27	OK	
PIPE 2x0.154	15	LC1 at 31.25%	0.52	OK	Eq. H1-1b
		LC10 at 68.75%	0.04	OK	
		LC11 at 68.75%	0.03	OK	
		LC2 at 31.25%	0.46	OK	
		LC3 at 31.25%	0.36	OK	
		LC4 at 31.25%	0.31	OK	
		LC5 at 31.25%	0.51	OK	
		LC6 at 31.25%	0.46	OK	
		LC7 at 31.25%	0.36	OK	
		LC8 at 31.25%	0.31	OK	

	LC9 at 33.33%	0.11	OK	
16	LC1 at 75.00%	0.06	OK	
	LC10 at 27.08%	0.03	OK	
	LC11 at 27.08%	0.02	OK	
	LC2 at 75.00%	0.05	OK	
	LC3 at 27.08%	0.06	OK	
	LC4 at 27.08%	0.05	OK	
	LC5 at 75.00%	0.05	OK	
	LC6 at 75.00%	0.04	OK	
	LC7 at 27.08%	0.05	OK	
	LC8 at 27.08%	0.04	OK	
	LC9 at 75.00%	0.07	OK	Eq. H1-1b
17	LC1 at 25.00%	0.08	OK	Eq. H1-1b
	LC10 at 75.00%	0.04	OK	
	LC11 at 75.00%	0.03	OK	
	LC2 at 27.08%	0.08	OK	Eq. H1-1b
	LC3 at 27.08%	0.06	OK	
	LC4 at 27.08%	0.05	OK	
	LC5 at 25.00%	0.08	OK	
	LC6 at 25.00%	0.07	OK	
	LC7 at 27.08%	0.05	OK	
	LC8 at 27.08%	0.05	OK	
	LC9 at 75.00%	0.07	OK	Eq. H1-1b
18	LC1 at 0.00%	0.17	OK	
	LC10 at 0.00%	0.11	OK	
	LC11 at 0.00%	0.08	OK	
	LC2 at 0.00%	0.15	OK	
	LC3 at 100.00%	0.14	OK	
	LC4 at 100.00%	0.13	OK	
	LC5 at 0.00%	0.15	OK	
	LC6 at 0.00%	0.12	OK	
	LC7 at 100.00%	0.11	OK	
	LC8 at 100.00%	0.11	OK	
	LC9 at 0.00%	0.22	OK	Eq. H1-1b
19	LC1 at 53.13%	0.28	OK	Eq. H1-1b
	LC10 at 100.00%	0.10	OK	
	LC11 at 100.00%	0.07	OK	
	LC2 at 53.13%	0.25	OK	
	LC3 at 0.00%	0.25	OK	Eq. H1-1b
	LC4 at 0.00%	0.23	OK	
	LC5 at 53.13%	0.27	OK	
	LC6 at 53.13%	0.25	OK	
	LC7 at 0.00%	0.23	OK	
	LC8 at 0.00%	0.21	OK	
	LC9 at 0.00%	0.20	OK	Eq. H1-1b
20	LC1 at 100.00%	0.10	OK	
	LC10 at 100.00%	0.09	OK	
	LC11 at 100.00%	0.07	OK	
	LC2 at 100.00%	0.09	OK	
	LC3 at 0.00%	0.09	OK	
	LC4 at 0.00%	0.09	OK	
	LC5 at 100.00%	0.07	OK	
	LC6 at 100.00%	0.07	OK	
	LC7 at 0.00%	0.07	OK	
	LC8 at 0.00%	0.07	OK	
	LC9 at 100.00%	0.17	OK	Eq. H1-1b
32	LC1 at 0.00%	0.26	OK	
	LC10 at 0.00%	0.14	OK	

LC11 at 0.00%	0.11	OK
LC2 at 0.00%	0.32	OK
LC3 at 0.00%	0.29	OK
LC4 at 0.00%	0.27	OK
LC5 at 100.00%	0.23	OK
LC6 at 0.00%	0.29	OK
LC7 at 0.00%	0.25	OK
LC8 at 0.00%	0.24	OK
LC9 at 0.00%	0.29	OK

Eq. H1-1b
Eq. H1-1b

38

LC1 at 0.00%	0.32	OK
LC10 at 0.00%	0.14	OK
LC11 at 0.00%	0.10	OK
LC2 at 0.00%	0.39	OK
LC3 at 0.00%	0.33	OK
LC4 at 0.00%	0.30	OK
LC5 at 0.00%	0.29	OK
LC6 at 0.00%	0.36	OK
LC7 at 0.00%	0.30	OK
LC8 at 0.00%	0.27	OK
LC9 at 0.00%	0.30	OK

Eq. H1-1b

41

LC1 at 31.25%	0.60	OK
LC10 at 33.33%	0.07	OK
LC11 at 33.33%	0.05	OK
LC2 at 31.25%	0.68	OK
LC3 at 31.25%	0.55	OK
LC4 at 31.25%	0.49	OK
LC5 at 31.25%	0.60	OK
LC6 at 31.25%	0.68	OK
LC7 at 31.25%	0.55	OK
LC8 at 31.25%	0.49	OK
LC9 at 33.33%	0.17	OK

Eq. H1-1b

Current Date: 1/29/2018 9:37 AM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1185\CT1185.etz

Geometry data

GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
1	-0.875	0.00	0.00	0
2	11.125	0.00	0.00	0
4	5.125	0.00	1.00	0
5	6.625	0.00	0.00	0
6	3.625	0.00	0.00	0
7	5.9167	0.00	1.00	0
8	4.3333	0.00	1.00	0
9	7.125	0.00	0.00	0
10	3.125	0.00	0.00	0
11	7.125	0.00	-0.20	0
12	-0.875	0.00	-0.20	0
13	11.125	0.00	-0.20	0
14	-0.875	2.96	0.00	0
15	11.125	2.96	0.00	0
17	5.125	2.96	1.00	0
18	6.625	2.96	0.00	0
19	3.625	2.96	0.00	0
20	5.9167	2.96	1.00	0
21	4.3333	2.96	1.00	0
22	7.125	2.96	0.00	0
23	3.125	2.96	0.00	0
24	7.125	2.96	-0.20	0

25	-0.875	2.96	-0.20	0
26	11.125	2.96	-0.20	0
40	7.125	4.375	-0.20	0
41	-0.875	4.375	-0.20	0
42	11.125	5.375	-0.20	0
43	7.125	-1.625	-0.20	0
44	-0.875	-1.625	-0.20	0
45	11.125	-2.625	-0.20	0
47	5.125	0.00	1.20	0
49	5.125	2.96	1.20	0
50	5.125	3.46	1.20	0
51	5.125	-0.50	1.20	0
54	5.125	-0.50	3.28	0
55	5.125	3.46	3.28	0
65	11.125	1.375	0.00	0
66	9.00	1.375	5.00	0
67	3.125	5.375	-0.20	0
68	3.125	-2.625	-0.20	0
69	3.125	0.00	-0.20	0
70	3.125	2.96	-0.20	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
54	1	1	1	1	1	1
55	1	1	1	1	1	1
66	1	1	1	1	1	1

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
1	8	7		LU 3X2X1_4	A36	0.00	0.00	0.00
2	8	6		LU 3X2X1_4	A36	0.00	0.00	0.00
3	7	5		LU 3X2X1_4	A36	0.00	0.00	0.00
4	1	2		L 2-1_2X2-1_2X3_16	A36	0.00	0.00	0.00
8	21	20		LU 3X2X1_4	A36	0.00	0.00	0.00
9	21	19		LU 3X2X1_4	A36	0.00	0.00	0.00
10	20	18		LU 3X2X1_4	A36	0.00	0.00	0.00
11	14	15		L 2-1_2X2-1_2X3_16	A36	0.00	0.00	0.00
15	45	42		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
16	43	40		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
18	22	9		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
19	15	2		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
20	14	1		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
21	50	51		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
28	54	51		HSS_SQR 3X3X1_4	A500 GrB rectangular	0.00	0.00	0.00
29	55	50		HSS_SQR 3X3X1_4	A500 GrB rectangular	0.00	0.00	0.00
30	20	7		L 2X2X3_16	A36	0.00	0.00	0.00
31	21	8		L 2X2X3_16	A36	0.00	0.00	0.00
32	10	23		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

38	66	65	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
41	68	67	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
17	44	41	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

Orientation of local axes

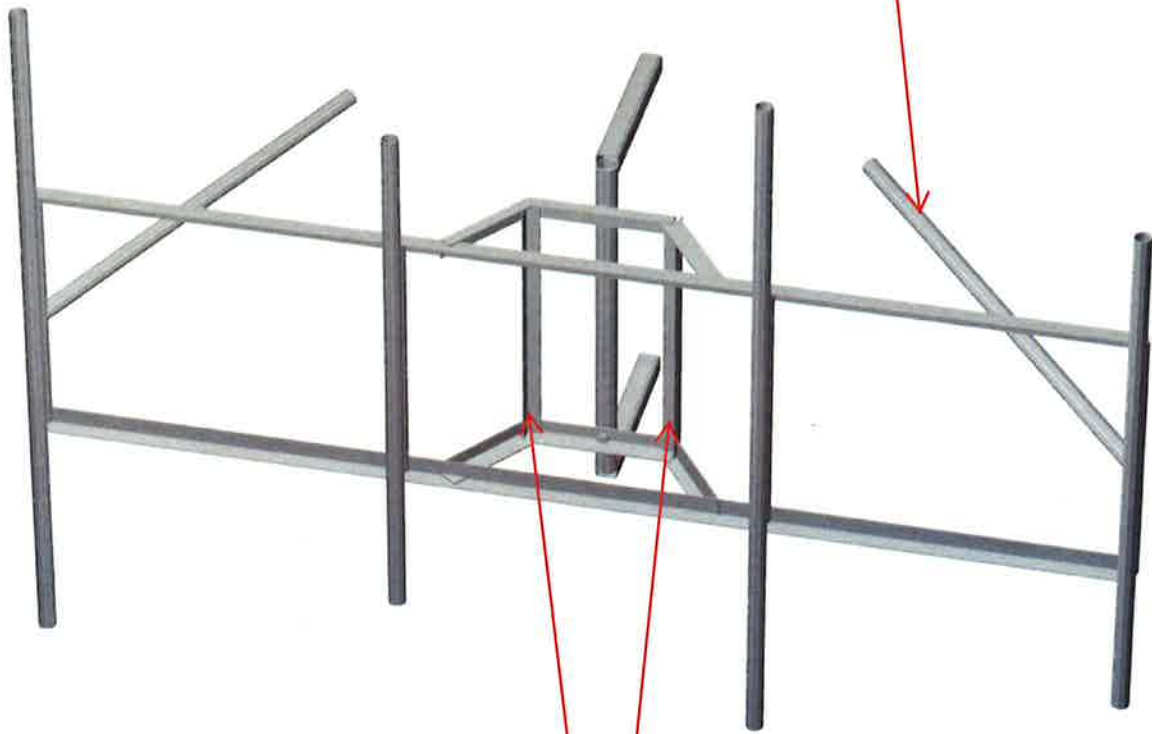
Member	Rotation [Deg]	Axes23	NX	NY	NZ
1	270.00	0	0.00	0.00	0.00
3	270.00	0	0.00	0.00	0.00
4	270.00	0	0.00	0.00	0.00
8	180.00	0	0.00	0.00	0.00
9	90.00	0	0.00	0.00	0.00
10	180.00	0	0.00	0.00	0.00
11	180.00	0	0.00	0.00	0.00
30	180.00	0	0.00	0.00	0.00
31	270.00	0	0.00	0.00	0.00



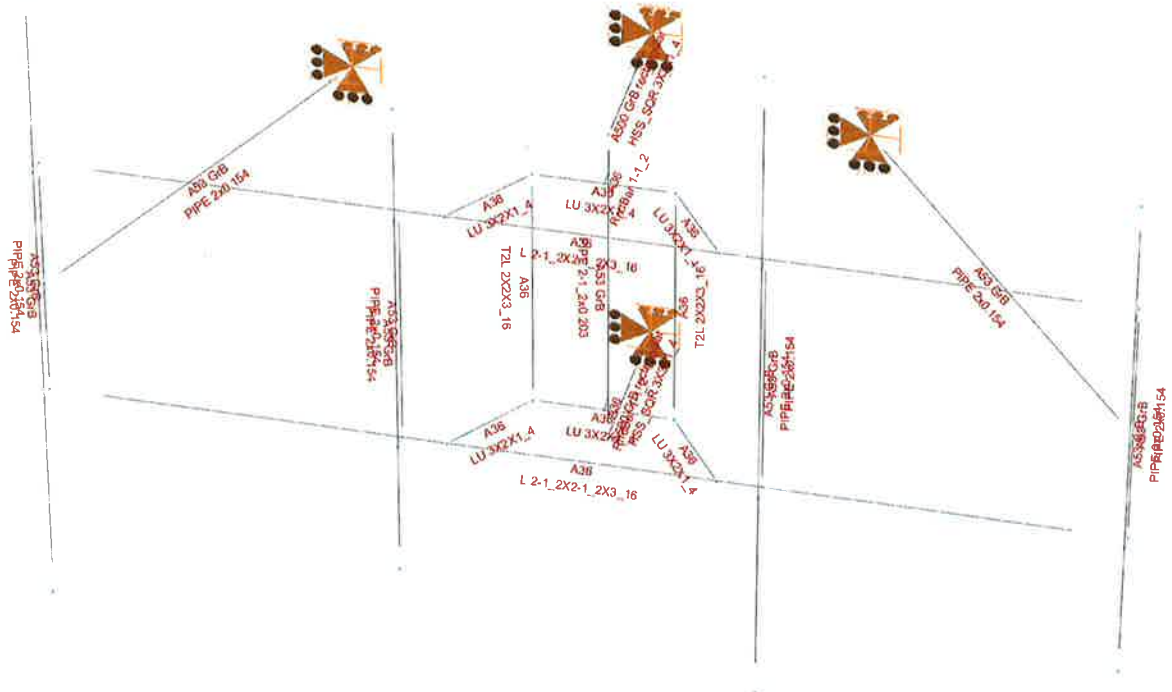
HUDSON
Design Group LLC

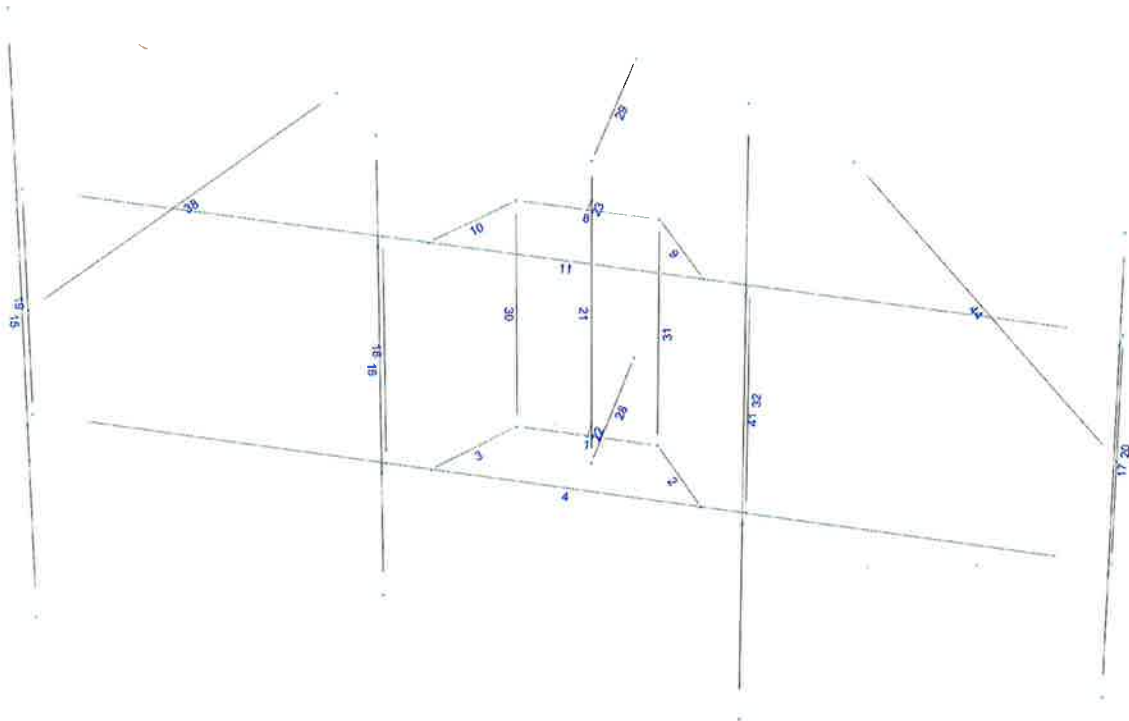
**Mount Calculations
(Proposed Conditions)**

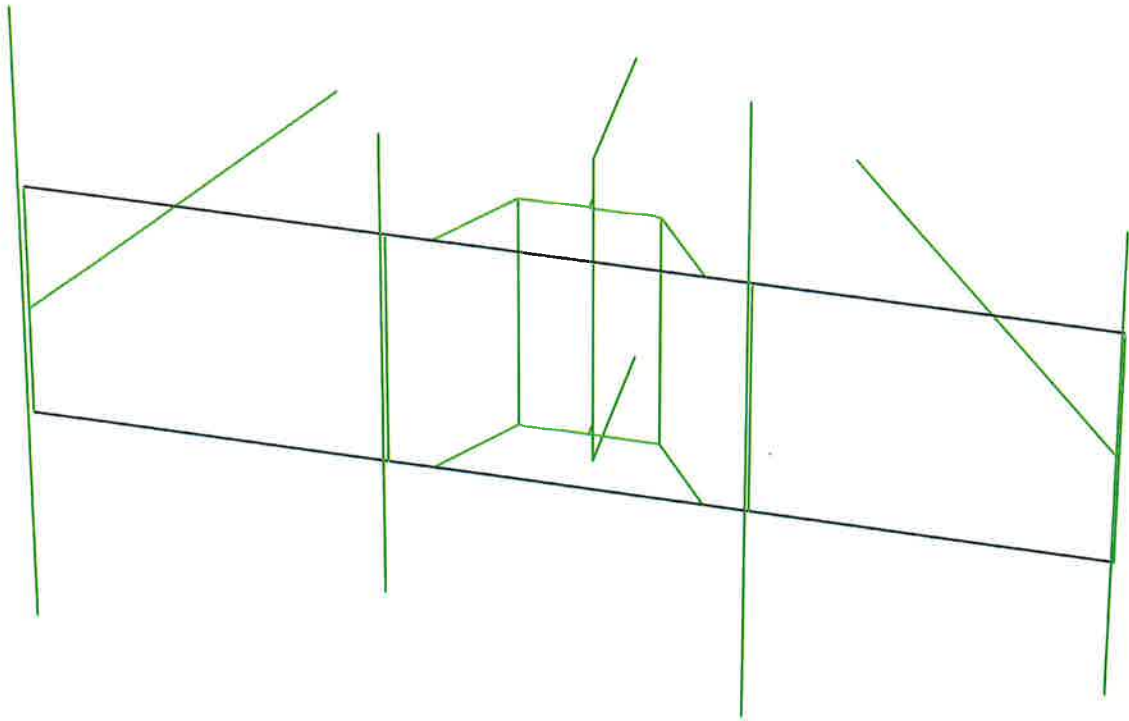
Install new 2" std. (2.38" O.D.) steel pipe brace secured to the existing mount and tower (typ. of 1 per sector, total of 3).



Reinforce the existing 2"x2"x3/16" angle with new 2"x2"x3/16" steel angle (typ. of 2 per sector, total of 6).







Current Date: 1/29/2018 9:35 AM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT1185\CT1185 (MOD.).etx\

Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design :

- LC1=1.2D+1.6Wo
- LC2=1.2D+1.6W30
- LC3=1.2D+1.6W60
- LC4=1.2D+1.6W90
- LC5=0.9D+1.6Wo
- LC6=0.9D+1.6W30
- LC7=0.9D+1.6W60
- LC8=0.9D+1.6W90
- LC9=1.2D+Wi+Di
- LC10=1.2D
- LC11=0.9D

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	HSS_SQR 3X3X1_4	28	LC1 at 0.00%	0.13	OK	
			LC10 at 0.00%	0.12	OK	
			LC11 at 0.00%	0.09	OK	
			LC2 at 0.00%	0.14	OK	
			LC3 at 0.00%	0.40	OK	Eq. H1-1b
			LC4 at 0.00%	0.36	OK	
			LC5 at 0.00%	0.10	OK	
			LC6 at 100.00%	0.12	OK	
			LC7 at 0.00%	0.37	OK	
			LC8 at 0.00%	0.33	OK	
			LC9 at 0.00%	0.22	OK	
		29	LC1 at 0.00%	0.13	OK	
			LC10 at 0.00%	0.12	OK	
			LC11 at 0.00%	0.09	OK	
			LC2 at 0.00%	0.14	OK	
			LC3 at 0.00%	0.32	OK	Eq. H1-1b
			LC4 at 0.00%	0.29	OK	
			LC5 at 0.00%	0.10	OK	
			LC6 at 0.00%	0.11	OK	
			LC7 at 0.00%	0.30	OK	
			LC8 at 0.00%	0.27	OK	
			LC9 at 0.00%	0.22	OK	
	L 2-1_2X2-1_2X3_16	4	LC1 at 62.50%	0.37	With warnings	
			LC10 at 100.00%	0.38	With warnings	
			LC11 at 100.00%	0.28	With warnings	
			LC2 at 62.50%	0.50	With warnings	
			LC3 at 36.25%	0.88	With warnings	Eq. H2-1
			LC4 at 36.25%	0.78	With warnings	
			LC5 at 62.50%	0.33	With warnings	
			LC6 at 62.50%	0.46	With warnings	
			LC7 at 36.25%	0.84	With warnings	
			LC8 at 36.25%	0.74	With warnings	
			LC9 at 100.00%	0.72	With warnings	Eq. H2-1
		11	LC1 at 67.50%	0.40	With warnings	
			LC10 at 100.00%	0.30	With warnings	

LU 3X2X1_4

	LC11 at 100.00%	0.22	With warnings	
	LC2 at 67.50%	0.41	With warnings	
	LC3 at 32.50%	0.57	With warnings	Sec. F1
	LC4 at 32.50%	0.52	With warnings	
	LC5 at 67.50%	0.33	With warnings	
	LC6 at 67.50%	0.34	With warnings	
	LC7 at 32.50%	0.51	With warnings	
	LC8 at 32.50%	0.47	With warnings	
	LC9 at 100.00%	0.61	With warnings	Eq. H2-1
1	LC1 at 46.88%	0.36	OK	
	LC10 at 46.88%	0.22	OK	
	LC11 at 46.88%	0.16	OK	
	LC2 at 46.88%	0.49	OK	Eq. H2-1
	LC3 at 46.88%	0.32	OK	
	LC4 at 46.88%	0.30	OK	
	LC5 at 46.88%	0.31	OK	
	LC6 at 46.88%	0.45	OK	
	LC7 at 46.88%	0.26	OK	
	LC8 at 46.88%	0.25	OK	
	LC9 at 46.88%	0.42	OK	
2	LC1 at 0.00%	0.27	OK	
	LC10 at 0.00%	0.22	OK	
	LC11 at 0.00%	0.16	OK	
	LC2 at 0.00%	0.31	OK	
	LC3 at 0.00%	0.36	OK	
	LC4 at 0.00%	0.34	OK	
	LC5 at 0.00%	0.22	OK	
	LC6 at 0.00%	0.26	OK	
	LC7 at 100.00%	0.32	OK	
	LC8 at 0.00%	0.29	OK	
	LC9 at 0.00%	0.42	OK	Eq. H2-1
3	LC1 at 0.00%	0.28	OK	
	LC10 at 0.00%	0.27	OK	
	LC11 at 0.00%	0.20	OK	
	LC2 at 0.00%	0.29	OK	
	LC3 at 0.00%	0.24	OK	
	LC4 at 0.00%	0.25	OK	
	LC5 at 0.00%	0.22	OK	
	LC6 at 100.00%	0.25	OK	
	LC7 at 100.00%	0.24	OK	Eq. H2-1
	LC8 at 100.00%	0.20	OK	
	LC9 at 0.00%	0.52	OK	Eq. H2-1
8	LC1 at 50.00%	0.25	OK	
	LC10 at 46.88%	0.33	OK	
	LC11 at 46.88%	0.25	OK	
	LC2 at 50.00%	0.24	OK	
	LC3 at 50.00%	0.39	OK	
	LC4 at 50.00%	0.37	OK	
	LC5 at 50.00%	0.18	OK	
	LC6 at 50.00%	0.18	OK	
	LC7 at 50.00%	0.31	OK	
	LC8 at 50.00%	0.30	OK	
	LC9 at 46.88%	0.61	OK	Eq. H2-1
9	LC1 at 0.00%	0.39	OK	
	LC10 at 0.00%	0.36	OK	
	LC11 at 0.00%	0.27	OK	
	LC2 at 0.00%	0.38	OK	
	LC3 at 0.00%	0.45	OK	
	LC4 at 0.00%	0.43	OK	

		LC5 at 0.00%	0.31	OK	
		LC6 at 0.00%	0.29	OK	
		LC7 at 0.00%	0.36	OK	
		LC8 at 0.00%	0.35	OK	
		LC9 at 0.00%	0.71	OK	Eq. H2-1
	10	LC1 at 0.00%	0.25	OK	
		LC10 at 0.00%	0.16	OK	
		LC11 at 0.00%	0.12	OK	
		LC2 at 0.00%	0.25	OK	
		LC3 at 0.00%	0.29	OK	
		LC4 at 0.00%	0.27	OK	
		LC5 at 0.00%	0.21	OK	
		LC6 at 0.00%	0.22	OK	
		LC7 at 100.00%	0.27	OK	
		LC8 at 100.00%	0.24	OK	
		LC9 at 0.00%	0.33	OK	Eq. H2-1
PIPE 2-1_2x0.203	21	LC1 at 100.00%	0.20	OK	
		LC10 at 100.00%	0.14	OK	
		LC11 at 100.00%	0.10	OK	
		LC2 at 100.00%	0.22	OK	
		LC3 at 0.00%	0.18	OK	
		LC4 at 0.00%	0.17	OK	
		LC5 at 100.00%	0.16	OK	
		LC6 at 100.00%	0.18	OK	
		LC7 at 87.50%	0.15	OK	
		LC8 at 0.00%	0.14	OK	
		LC9 at 100.00%	0.27	OK	Eq. H1-1b
PIPE 2x0.154	15	LC1 at 31.25%	0.52	OK	Eq. H1-1b
		LC10 at 68.75%	0.04	OK	
		LC11 at 68.75%	0.03	OK	
		LC2 at 31.25%	0.46	OK	
		LC3 at 31.25%	0.36	OK	
		LC4 at 31.25%	0.31	OK	
		LC5 at 31.25%	0.51	OK	
		LC6 at 31.25%	0.46	OK	
		LC7 at 31.25%	0.36	OK	
		LC8 at 31.25%	0.31	OK	
		LC9 at 33.33%	0.11	OK	
	16	LC1 at 75.00%	0.04	OK	
		LC10 at 75.00%	0.03	OK	
		LC11 at 75.00%	0.02	OK	
		LC2 at 75.00%	0.03	OK	
		LC3 at 27.08%	0.05	OK	
		LC4 at 27.08%	0.05	OK	
		LC5 at 75.00%	0.03	OK	
		LC6 at 75.00%	0.02	OK	
		LC7 at 27.08%	0.04	OK	
		LC8 at 27.08%	0.04	OK	
		LC9 at 75.00%	0.06	OK	Eq. H1-1b
	17	LC1 at 27.08%	0.10	OK	
		LC10 at 75.00%	0.03	OK	
		LC11 at 75.00%	0.02	OK	
		LC2 at 27.08%	0.11	OK	Eq. H1-1b
		LC3 at 25.00%	0.05	OK	
		LC4 at 27.08%	0.04	OK	
		LC5 at 27.08%	0.09	OK	
		LC6 at 27.08%	0.10	OK	
		LC7 at 25.00%	0.05	OK	
		LC8 at 25.00%	0.04	OK	

	LC9 at 27.08%	0.06	OK	
18	LC1 at 0.00%	0.13	OK	
	LC10 at 0.00%	0.11	OK	
	LC11 at 0.00%	0.08	OK	
	LC2 at 0.00%	0.11	OK	
	LC3 at 0.00%	0.12	OK	
	LC4 at 100.00%	0.12	OK	
	LC5 at 0.00%	0.11	OK	
	LC6 at 0.00%	0.08	OK	
	LC7 at 100.00%	0.10	OK	
	LC8 at 100.00%	0.10	OK	
	LC9 at 0.00%	0.22	OK	Eq. H1-1b
19	LC1 at 53.13%	0.37	OK	Eq. H1-1b
	LC10 at 100.00%	0.10	OK	
	LC11 at 100.00%	0.07	OK	
	LC2 at 53.13%	0.35	OK	
	LC3 at 0.00%	0.24	OK	Eq. H1-1b
	LC4 at 0.00%	0.22	OK	
	LC5 at 53.13%	0.37	OK	
	LC6 at 53.13%	0.35	OK	
	LC7 at 0.00%	0.22	OK	
	LC8 at 0.00%	0.20	OK	
	LC9 at 0.00%	0.20	OK	
20	LC1 at 53.13%	0.26	OK	Eq. H1-1b
	LC10 at 100.00%	0.08	OK	
	LC11 at 100.00%	0.06	OK	
	LC2 at 56.25%	0.27	OK	
	LC3 at 0.00%	0.11	OK	
	LC4 at 0.00%	0.10	OK	
	LC5 at 53.13%	0.26	OK	
	LC6 at 56.25%	0.27	OK	Eq. H1-1b
	LC7 at 56.25%	0.11	OK	
	LC8 at 56.25%	0.09	OK	
	LC9 at 0.00%	0.17	OK	
32	LC1 at 0.00%	0.27	OK	
	LC10 at 0.00%	0.13	OK	
	LC11 at 0.00%	0.10	OK	
	LC2 at 0.00%	0.34	OK	Eq. H1-1b
	LC3 at 0.00%	0.27	OK	
	LC4 at 0.00%	0.25	OK	
	LC5 at 0.00%	0.24	OK	
	LC6 at 0.00%	0.31	OK	
	LC7 at 0.00%	0.23	OK	
	LC8 at 0.00%	0.22	OK	
	LC9 at 0.00%	0.27	OK	
38	LC1 at 0.00%	0.20	OK	
	LC10 at 0.00%	0.13	OK	
	LC11 at 0.00%	0.10	OK	
	LC2 at 0.00%	0.24	OK	
	LC3 at 0.00%	0.26	OK	Eq. H1-1b
	LC4 at 0.00%	0.25	OK	
	LC5 at 0.00%	0.16	OK	
	LC6 at 0.00%	0.21	OK	
	LC7 at 0.00%	0.23	OK	
	LC8 at 0.00%	0.21	OK	
	LC9 at 0.00%	0.27	OK	Eq. H1-1b
41	LC1 at 31.25%	0.60	OK	
	LC10 at 33.33%	0.07	OK	

T2L 2X2X3_16

	LC11 at 33.33%	0.05	OK	
	LC2 at 31.25%	0.68	OK	Eq. H1-1b
	LC3 at 31.25%	0.55	OK	
	LC4 at 31.25%	0.49	OK	
	LC5 at 31.25%	0.60	OK	
	LC6 at 31.25%	0.68	OK	
	LC7 at 31.25%	0.55	OK	
	LC8 at 31.25%	0.49	OK	
	LC9 at 33.33%	0.16	OK	
44	LC1 at 0.00%	0.16	OK	
	LC10 at 0.00%	0.12	OK	
	LC11 at 0.00%	0.09	OK	
	LC2 at 0.00%	0.18	OK	
	LC3 at 0.00%	0.27	OK	Eq. H1-1b
	LC4 at 0.00%	0.25	OK	
	LC5 at 0.00%	0.13	OK	
	LC6 at 0.00%	0.15	OK	
	LC7 at 0.00%	0.24	OK	
	LC8 at 0.00%	0.22	OK	
	LC9 at 0.00%	0.23	OK	
30	LC1 at 100.00%	0.21	OK	
	LC10 at 100.00%	0.21	OK	
	LC11 at 100.00%	0.16	OK	
	LC2 at 100.00%	0.22	OK	
	LC3 at 0.00%	0.22	OK	
	LC4 at 0.00%	0.21	OK	
	LC5 at 100.00%	0.16	OK	
	LC6 at 100.00%	0.17	OK	
	LC7 at 0.00%	0.17	OK	
	LC8 at 0.00%	0.16	OK	
	LC9 at 100.00%	0.40	OK	Eq. H2-1
31	LC1 at 100.00%	0.39	OK	
	LC10 at 100.00%	0.39	OK	
	LC11 at 100.00%	0.29	OK	
	LC2 at 100.00%	0.39	OK	
	LC3 at 100.00%	0.36	OK	
	LC4 at 100.00%	0.37	OK	
	LC5 at 100.00%	0.29	OK	
	LC6 at 100.00%	0.29	OK	
	LC7 at 100.00%	0.26	OK	
	LC8 at 100.00%	0.27	OK	
	LC9 at 100.00%	0.76	OK	Eq. H2-1

Current Date: 1/29/2018 9:35 AM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1185\CT1185 (MOD.).etz\

Geometry data

GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
1	-0.875	0.00	0.00	0
2	11.125	0.00	0.00	0
4	5.125	0.00	1.00	0
5	6.625	0.00	0.00	0
6	3.625	0.00	0.00	0
7	5.9167	0.00	1.00	0
8	4.3333	0.00	1.00	0
9	7.125	0.00	0.00	0
10	3.125	0.00	0.00	0
11	7.125	0.00	-0.20	0
12	-0.875	0.00	-0.20	0
13	11.125	0.00	-0.20	0
14	-0.875	2.96	0.00	0
15	11.125	2.96	0.00	0
17	5.125	2.96	1.00	0
18	6.625	2.96	0.00	0
19	3.625	2.96	0.00	0
20	5.9167	2.96	1.00	0
21	4.3333	2.96	1.00	0
22	7.125	2.96	0.00	0
23	3.125	2.96	0.00	0
24	7.125	2.96	-0.20	0

25	-0.875	2.96	-0.20	0
26	11.125	2.96	-0.20	0
40	7.125	4.375	-0.20	0
41	-0.875	4.375	-0.20	0
42	11.125	5.375	-0.20	0
43	7.125	-1.625	-0.20	0
44	-0.875	-1.625	-0.20	0
45	11.125	-2.625	-0.20	0
47	5.125	0.00	1.20	0
49	5.125	2.96	1.20	0
50	5.125	3.46	1.20	0
51	5.125	-0.50	1.20	0
54	5.125	-0.50	3.28	0
55	5.125	3.46	3.28	0
65	11.125	1.375	0.00	0
66	9.00	1.375	5.00	0
67	3.125	5.375	-0.20	0
68	3.125	-2.625	-0.20	0
69	3.125	0.00	-0.20	0
70	3.125	2.96	-0.20	0
71	-0.875	1.35	0.00	0
72	3.00	1.35	5.00	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
54	1	1	1	1	1	1
55	1	1	1	1	1	1
66	1	1	1	1	1	1
72	1	1	1	1	1	1

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	lg factor
1	8	7		LU 3X2X1_4	A36	0.00	0.00	0.00
2	8	6		LU 3X2X1_4	A36	0.00	0.00	0.00
3	7	5		LU 3X2X1_4	A36	0.00	0.00	0.00
4	1	2		L 2-1_2X2-1_2X3_16	A36	0.00	0.00	0.00
8	21	20		LU 3X2X1_4	A36	0.00	0.00	0.00
9	21	19		LU 3X2X1_4	A36	0.00	0.00	0.00
10	20	18		LU 3X2X1_4	A36	0.00	0.00	0.00
11	14	15		L 2-1_2X2-1_2X3_16	A36	0.00	0.00	0.00
15	45	42		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
16	43	40		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
17	44	41		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
18	22	9		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
19	15	2		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
20	14	1		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
21	50	51		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
28	54	51		HSS_SQR 3X3X1_4	A500 GrB rectangular	0.00	0.00	0.00

29	55	50	HSS_SQR 3X3X1_4	A500 GrB rectangular	0.00	0.00	0.00
30	20	7	T2L 2X2X3_16	A36	0.00	0.00	0.00
31	21	8	T2L 2X2X3_16	A36	0.00	0.00	0.00
32	10	23	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
38	66	65	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
41	68	67	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
44	72	71	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
1	270.00	0	0.00	0.00	0.00
3	270.00	0	0.00	0.00	0.00
4	270.00	0	0.00	0.00	0.00
8	180.00	0	0.00	0.00	0.00
9	90.00	0	0.00	0.00	0.00
10	180.00	0	0.00	0.00	0.00
11	180.00	0	0.00	0.00	0.00
31	180.00	0	0.00	0.00	0.00



Radio Frequency Emissions Analysis Report

AT&T Existing Facility

Site ID: CT1185

FA#: 10092207

Stafford Springs Tolland Avenue

64 Tolland Avenue

Stafford, CT 06076

February 26, 2018

Centerline Communications Project Number: 950012-024

Site Compliance Summary	
Compliance Status:	COMPLIANT
Site total MPE% of FCC general population allowable limit:	1.88 %



February 26, 2018

AT&T Mobility – New England
Attn: John Benedetto, RF Manager
550 Cochituate Road
Suite 550 – 13&14
Framingham, MA 06040

Emissions Analysis for Site: **CT1185 – Stafford Springs Tolland Avenue**

Centerline Communications, LLC (“Centerline”) was directed to analyze the proposed AT&T facility located at **64 Tolland Avenue, Stafford, CT**, for the purpose of determining whether the emissions from the Proposed AT&T Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limits for the 700 and 850 MHz Bands are approximately $467 \mu\text{W}/\text{cm}^2$ and $567 \mu\text{W}/\text{cm}^2$ respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 2300 MHz (WCS) bands is $1000 \mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.



CALCULATIONS

Calculations were performed for the proposed AT&T Wireless antenna facility located at **64 Tolland Avenue, Stafford, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since AT&T is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in *Table 1*:

Technology	Frequency Band	Channel Count	Transmit Power per Channel (W)
UMTS	850 MHz	2	30
UMTS	1900 MHz (PCS)	2	30
LTE	700 MHz	2	30
LTE	1900 MHz (PCS)	4	60
LTE	2300 MHz (WCS)	4	30

Table 1: Channel Data Table



The following antennas listed in *Table 2* were used in the modeling for transmission in the 700 MHz, 850 MHz, 1900 MHz (PCS) and 2300 MHz (WCS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

Sector	Antenna Number	Antenna Make / Model	Antenna Centerline (ft)
A	1	Powerwave 7770	177
A	2	Commscope SBNH-1D6565C	177
A	3	CCI TPA-65R-LCUUUU-H8	177
B	1	Powerwave 7770	177
B	2	Powerwave P65-17-XLH-RR	177
B	3	CCI TPA-65R-LCUUUU-H8	177
C	1	Powerwave 7770	177
C	2	KMW AM-X-CD-14-65-00T-RET	177
C	3	Quintel QS46512-2	177

Table 2: Antenna Data

All calculations were done with respect to uncontrolled / general population threshold limits.

RESULTS

Per the calculations completed for the proposed AT&T configurations *Table 3* shows resulting emissions power levels and percentages of the FCC’s allowable general population limit.

Antenna ID	Antenna Make / Model	Frequency Bands	Antenna Gain (dBd)	Channel Count	Total TX Power (W)	ERP (W)	MPE %
Antenna A1	Powerwave 7770	850 MHz / 1900 MHz (PCS)	11.4 / 13.4	4	120	2,140.89	0.34
Antenna A2	Commscope SBNH-1D6565C	700 MHz	13.65	2	60	1,390.44	0.37
Antenna A3	CCI TPA-65R-LCUUUU-H8	1900 MHz (PCS) / 2300 MHz (WCS)	13.75 / 14.45	8	360	9,034.64	1.11
Sector A Composite MPE%							1.82
Antenna B1	Powerwave 7770	850 MHz / 1900 MHz (PCS)	11.4 / 13.4	4	120	2,140.89	0.34
Antenna B2	Powerwave P65-17-XLH-RR	700 MHz	14.3	2	60	1,614.92	0.43
Antenna B3	CCI TPA-65R-LCUUUU-H8	1900 MHz (PCS) / 2300 MHz (WCS)	13.75 / 14.45	8	360	9,034.64	1.11
Sector B Composite MPE%							1.88
Antenna C1	Powerwave 7770	850 MHz / 1900 MHz (PCS)	11.4 / 13.4	4	120	2,140.89	0.34
Antenna C2	KMW AM-X-CD-14-65-00T-RET	700 MHz	11.85	2	60	918.65	0.24
Antenna C3	Quintel QS46512-2	1900 MHz (PCS) / 2300 MHz (WCS)	13.15 / 14.05	8	360	8,006.08	0.98
Sector C Composite MPE%							1.57

Table 3: AT&T Emissions Levels



The Following table (*table 4*) shows all additional carriers on site and their MPE% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum AT&T MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, the sector with the largest calculated MPE% is Sector B. *Table 5* below shows a summary for each AT&T Sector as well as the composite MPE value for the site.

Site Composite MPE%	
Carrier	MPE%
AT&T – Max Sector Value	1.88 %
No Additional Carriers Listed per CSC Active MPE Database	N/A
Site Total MPE %:	1.88 %

Table 4: All Carrier MPE Contributions

AT&T Sector A Total:	1.82 %
AT&T Sector B Total:	1.88 %
AT&T Sector C Total:	1.57 %
Site Total:	1.88 %

Table 5: Site MPE Summary



FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. *Table 6* below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated AT&T sector(s). For this site, the sector with the largest calculated MPE% is Sector B.

AT&T _ Frequency Band / Technology Max Power Values (Sector B)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ($\mu\text{W}/\text{cm}^2$)	Frequency (MHz)	Allowable MPE ($\mu\text{W}/\text{cm}^2$)	Calculated % MPE
AT&T 850 MHz UMTS	2	414.12	177	1.02	850 MHz	567	0.18%
AT&T 1900 MHz (PCS) UMTS	2	656.33	177	1.61	1900 MHz (PCS)	1000	0.16%
AT&T 700 MHz LTE	2	807.46	177	1.99	700 MHz	467	0.43%
AT&T 1900 MHz (PCS) LTE	4	1,422.82	177	7.00	1900 MHz (PCS)	1000	0.70%
AT&T 2300 MHz (WCS) LTE	4	835.84	177	4.11	2300 MHz (WCS)	1000	0.41%
						Total:	1.88%

Table 6: AT&T Maximum Sector MPE Power Values



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the AT&T facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

AT&T Sector	Power Density Value (%)
Sector A:	1.82 %
Sector B:	1.88 %
Sector C:	1.57 %
AT&T Maximum Total (per sector):	1.88 %
Site Total:	1.88 %
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **1.88 %** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

A handwritten signature in black ink, appearing to read 'Scott Heffernan', is positioned above the printed name.

Scott Heffernan

RF Engineering Director

Centerline Communications, LLC

95 Ryan Drive, Suite 1

Raynham, MA 02767

50 TOLLAND AVE

Location 50 TOLLAND AVE

Mblu 67 / 11 /

Acct# 00445300

Owner TERRA ALTA INC

Assessment \$191,410

Appraisal \$581,300

PID 5047

Building Count 1

Current Value

Appraisal			
Valuation Year	Improvements	Land	Total
2015	\$3,000	\$578,300	\$581,300

Assessment			
Valuation Year	Improvements	Land	Total
2015	\$2,100	\$189,310	\$191,410

Owner of Record

Owner TERRA ALTA INC

Sale Price \$0

Co-Owner C/O JENNIFER J DAVIS

Certificate 1

Address 114 STAFFORD ST

Book & Page 272/ 673

STAFFORD SPRINGS, CT 06076

Sale Date 01/30/1990

Instrument

Ownership History

Ownership History					
Owner	Sale Price	Certificate	Book & Page	Instrument	Sale Date
TERRA ALTA INC	\$0	1	272/ 673		01/30/1990
JULIAN MICHAEL, LEO J, ETAL	\$0	2	232/ 620		11/24/1986

Building Information

Building 1 : Section 1

Year Built:

Living Area: 0

Replacement Cost: \$0

Building Percent

Good:

Replacement Cost

Less Depreciation: \$0

Building Attributes

Field	Description
Style	Vacant Ind
Model	
Grade:	
Occupancy	
Exterior Wall 1	
Exterior Wall 2	
Roof Structure	
Roof Cover	
Interior Wall 1	
Interior Wall 2	
Interior Flr 1	
Interior Flr 2	
Heat Fuel	
Heat Type:	
AC Type:	
Total Bedrooms:	
Full Bthrms:	
Half Baths:	
Extra Fixtures	
Total Rooms:	
Bath Style:	
Kitchen Style:	
Num Kitchens	
Fireplaces	
Extra Openings	
Prefab Fpl(s)	
Attic Type	
Bsmt Type	
Bsmt Garage(s)	
Fin Bsmnt	
Fn. Bmt. Qual.	
Unfin Area	

Building Photo



(<http://images.vgsi.com/photos2/StaffordCTPhotos//\00\01\26\2>)

Building Layout

(<http://images.vgsi.com/photos2/StaffordCTPhotos//Sketches/50>)

Building Sub-Areas (sq ft)	Legend
No Data for Building Sub-Areas	

Extra Features

Extra Features	Legend
No Data for Extra Features	

Land

Land Use

Use Code 300
Description Ind Land
Zone
Neighborhood 504
Alt Land Appr No
Category

Land Line Valuation

Size (Acres) 143.02
Frontage
Depth
Assessed Value \$189,310
Appraised Value \$578,300

Outbuildings

Outbuildings						<u>Legend</u>
Code	Description	Sub Code	Sub Description	Size	Value	Bldg #
FN3	FENCE-6' CHAIN			320 L.F.	\$1,400	1
SHD1	Shed	MS	Masonry	200 S.F.	\$1,600	1

Valuation History

Appraisal			
Valuation Year	Improvements	Land	Total
2017	\$3,000	\$578,300	\$581,300
2016	\$3,000	\$578,300	\$581,300
2014	\$0	\$398,300	\$398,300

Assessment			
Valuation Year	Improvements	Land	Total
2017	\$2,100	\$189,310	\$191,410
2016	\$2,100	\$189,310	\$191,410
2014	\$0	\$52,410	\$52,410

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50 Tolland Ave Stafford CT,



Property Information

Property ID 09013134-67/11
 Location 50 TOLLAND AVE
 Owner TERRA ALTA INC



**MAP FOR REFERENCE ONLY
 NOT A LEGAL DOCUMENT**

CRCOG makes no claims and no warranties, expressed or implied, concerning the validity or accuracy of the GIS data presented on this map.

PROJECT INFORMATION

SCOPE OF WORK: ****BIRD NEST****
ITEMS TO BE MOUNTED ON THE EXISTING TOWER:
 • INSTALL (1) NEW AT&T (TPA-65R-LCUUUU-H8) (TYP. OF 1 PER ALPHA & BETA SECTORS, TOTAL OF 2)
 • INSTALL (1) NEW AT&T (QS46512-2) (TOTAL OF 1, GAMMA SECTOR
 • NEW AT&T RRUS: RRUS-32 B2 (PCS) (TYP. OF 1 PER SECTOR, TOTAL OF 3)
 • NEW AT&T RRUS: RRUS-32 (WCS) (TYP. OF 1 PER SECTOR, TOTAL OF 3)
 • NEW JUMPER CABLES: COAX JUMPER (4) PER SECTOR FROM EACH RRU (TOTAL OF 12)
 • NEW FIBER JUMPERS: FIBER JUMPERS (2) FROM THE SQUID TO EACH RRU (TOTAL OF 6)
 • REPLACE EXISTING (6)GSM DIPLEXERS WITH (3) DBC0061F1V51-2 LBC
 • INSTALL (1) DC6-48-60-18-8C SURGE ARRESTOR WITH (2) DC POWER, (1) FIBER, & (1) ALARM CABLE.
ITEMS TO BE MOUNTED INSIDE EXISTING EQUIPMENT SHELTER:
 • INSTALL (1) FIBER MANAGEMENT BOX ON EXISTING ICE BRIDGE POST.
 • INSTALL (3) DBC0061F1V51-2 LOW BAND COMBINERS TO REPLACE GSM DIPLEXERS.
 • REPLACE EXISTING DUL BBU WITH 5216 AND ADD (1) XMU.
 • INSTALL (1) 48V CONVERTER SHELF WITH (4) CONVERTER MODS IN EXISTING RACK WITH (6) 30AMP BREAKERS AND (1) 25AMP BREAKER. INSTALL (1) CONVERTER MOD TO EXISTING SHELF.
 • INSTALL (2) 150AMP BREAKERS TO EXISTING POWER PLANT.
ITEMS TO REMAIN:
 • (6) ANTENNAS, (3) RRU'S, (1) SURGE ARRESTOR, (12) COAX (2) DC POWER CABLES, & (1) FIBER RUN.
SQUID ALARMING (NOT TO BE DAISY CHAINED).
 • THE 1ST SQUID INSTALLED WILL BE ALARMED TO THE LOWEST BAND (OR FIRST INSTALLED RRH/RRU ON THE ALPHA SECTOR, IN THE EVENT THE ALARM CABLE CANNOT BE CONNECTED TO ALPHA IT WILL BE ACCEPTABLE TO ALARM TO THE CLOSEST PHYSICAL SECTOR ON AN EXCEPTION BASIS.
 • 2ND SQUID INSTALLED WILL BE ALARMED TO THE LOWEST BAND (OR FIRST INSTALLED) RRH/RRU ON THE BETA SECTOR.

SITE ADDRESS: 64 TOLLAND AVENUE
 STAFFORD, CT 06076

LATITUDE: 41.944675° N 41° 56' 40.83" N
 LONGITUDE: 72.317648° W 72° 19' 03.53" W
 TYPE OF SITE: GUYED TOWER, INDOOR EQUIPMENT
 TOWER HEIGHT: 180'± A.G.L
 RAD CENTER: 177'± A.G.L
 CURRENT USE: TELECOMMUNICATIONS FACILITY
 PROPOSED USE: TELECOMMUNICATIONS FACILITY



SITE NUMBER: CT1185

SITE NAME: STAFFORD SPRINGS TOLLAND AVENUE

PROJECT: LTE 2C/3C 2018 UPGRADE

VICINITY MAP

DIRECTIONS TO SITE:

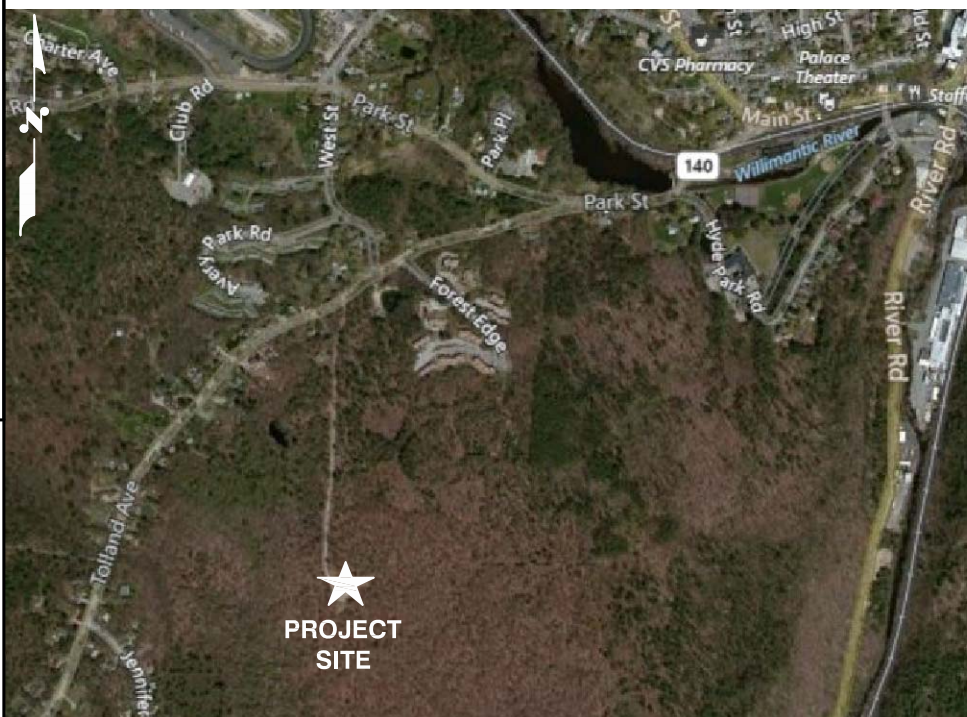
DEPART ENTERPRISE DR TOWARD CAPITOL BLVD. 0.4 MI. TURN LEFT ONTO CAPITOL BLVD. 0.3 MI. TURN LEFT ONTO WEST ST. 0.2 MI. TAKE RAMP LEFT FOR I-91 N. 7.8 MI. AT EXIT 29, TAKE RAMP RIGHT FOR CT-15 NORTH / US-5 NORTH TOWARD BOSTON / E. HARTFORD. 0.6 MI. KEEP STRAIGHT ONTO CT-15 N. 1.5 MI. KEEP STRAIGHT ONTO I-84 E / US-6 E. 20.5 MI. AT EXIT 70, TAKE RAMP RIGHT FOR CT-32 TOWARD STAFFORD SPRINGS. 0.2 MI. TURN LEFT ONTO CT-32 / RIVER RD. 4.3 MI. AT ROUNDABOUT, TAKE 2ND EXIT ONTO CT-32 / CT-190 / MAIN ST 0.2 MI. BEAR LEFT ONTO CT-140. 0.3 MI. KEEP LEFT ONTO TOLLAND AVE. 0.3 MI. ARRIVE AT ENTRANCE TO SITE ON THE LEFT.

GENERAL NOTES

1. THIS DOCUMENT IS THE CREATION, DESIGN, PROPERTY AND COPYRIGHTED WORK OF AT&T. ANY DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. DUPLICATION AND USE BY GOVERNMENT AGENCIES FOR THE PURPOSES OF CONDUCTING THEIR LAWFULLY AUTHORIZED REGULATORY AND ADMINISTRATIVE FUNCTIONS IS SPECIFICALLY ALLOWED.
2. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
3. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T MOBILITY REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.
4. CONSTRUCTION DRAWINGS ARE VALID FOR SIX MONTHS AFTER ENGINEER OF RECORD'S STAMPED AND SIGNED SUBMITTAL DATE LISTED HEREIN.

DRAWING INDEX

SHEET NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	1
GN-1	GENERAL NOTES	1
A-1	COMPOUND & EQUIPMENT PLANS	1
A-2	ANTENNA PLANS & ELEVATION	1
A-3	DETAILS	1
RF-1	RF PLUMBING DIAGRAM	1
G-1	GROUNDING DETAILS	1



72 HOURS

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 CALL TOLL FREE 1-800-922-4455
 OR CALL 811

UNDERGROUND SERVICE ALERT

HUDSON Design Group LLC
 45 BEECHWOOD DRIVE
 NORTH ANDOVER, MA 01845
 TEL: (978) 557-5553
 FAX: (978) 336-5586

CENTERLINE COMMUNICATIONS
 95 RYAN DRIVE
 RAYNHAM, MA 02767

SITE NUMBER: CT1185
SITE NAME: STAFFORD SPRINGS TOLLAND AVENUE
 64 TOLLAND AVENUE
 STAFFORD, CT 06076
 TOLLAND COUNTY

at&t
 500 ENTERPRISE DRIVE, SUITE 3A
 ROCKY HILL, CT 06067

NO.	DATE	REVISIONS	BY	CHK	APP'D
1	02/20/18	ISSUED FOR CONSTRUCTION	SG	AT	[Signature]
A	10/16/17	ISSUED FOR REVIEW	SB	AT	[Signature]

SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: SB

AT&T		
TITLE SHEET (LTE 2C/3C)		
SITE NUMBER	DRAWING NUMBER	REV
CT1185	T-1	1

GROUNDING NOTES

1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.
5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
7. APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO GROUND BAR.
9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWS COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
12. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50

GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:
 CONTRACTOR – CENTERLINE
 SUBCONTRACTOR – GENERAL CONTRACTOR (CONSTRUCTION)
 OWNER – AT&T MOBILITY
2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.
3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
6. "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.
7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.

14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.
15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
16. CONSTRUCTION SHALL COMPLY WITH SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T SITES."
17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.
20. APPLICABLE BUILDING CODES:
 SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.
 BUILDING CODE: IBC 2012 WITH 2016 CT BUILDING CODE AMENDMENTS
 ELECTRICAL CODE: REFER TO ELECTRICAL DRAWINGS
 LIGHTNING CODE: REFER TO ELECTRICAL DRAWINGS

 SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:

 AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE;

 AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC)
 MANUAL OF STEEL CONSTRUCTION, ASD, FOURTEENTH EDITION;

 TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-G,
 STRUCTURAL STANDARDS FOR STEEL

 EQUIPMENT AND ANTENNA SUPPORTING STRUCTURES; REFER TO ELECTRICAL DRAWINGS FOR SPECIFIC ELECTRICAL STANDARDS.

 FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

ABBREVIATIONS

AGL	ABOVE GRADE LEVEL	EQ	EQUAL	REQ	REQUIRED
AWG	AMERICAN WIRE GAUGE	GC	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
BBU	BATTERY BACKUP UNIT	GRC	GALVANIZED RIGID CONDUIT	TBD	TO BE DETERMINED
BTCW	BARE TINNED SOLID COPPER WIRE	MGB	MASTER GROUND BAR	TBR	TO BE REMOVED
BGR	BURIED GROUND RING	MIN	MINIMUM	TBRR	TO BE REMOVED AND REPLACED
BTS	BASE TRANSCEIVER STATION	P	PROPOSED	TYP	TYPICAL
E	EXISTING	NTS	NOT TO SCALE	UG	UNDER GROUND
EGB	EQUIPMENT GROUND BAR	RAD	RADIATION CENTER LINE (ANTENNA)	VIF	VERIFY IN FIELD
EGR	EQUIPMENT GROUND RING	REF	REFERENCE		

45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
FAX: (978) 336-5586

95 RYAN DRIVE
RAYNHAM, MA 02767

SITE NUMBER: CT1185
SITE NAME: STAFFORD SPRINGS
TOLLAND AVENUE
 64 TOLLAND AVENUE
 STAFFORD, CT 06076
 TOLLAND COUNTY

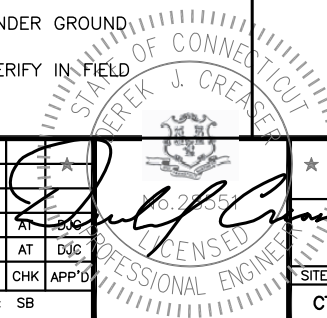
500 ENTERPRISE DRIVE, SUITE 3A
ROCKY HILL, CT 06067

NO.	DATE	REVISIONS	BY	CHK	APP'D
1	02/20/18	ISSUED FOR CONSTRUCTION	SG	AT	
A	10/16/17	ISSUED FOR REVIEW	SB	AT	DJC

SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: SB

AT&T
GENERAL NOTES
(LTE 2C/3C)

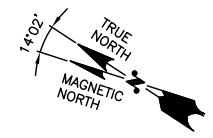
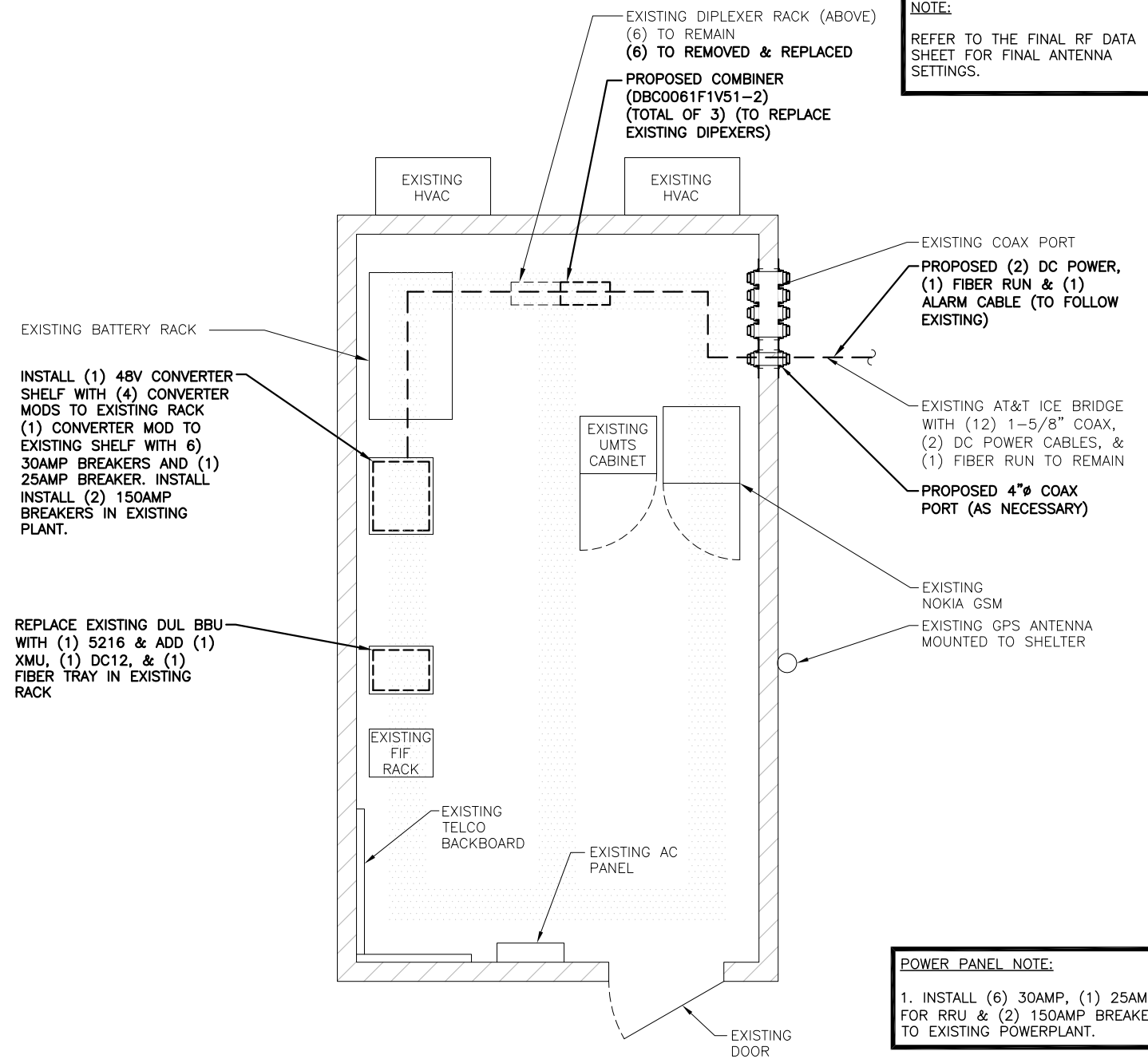
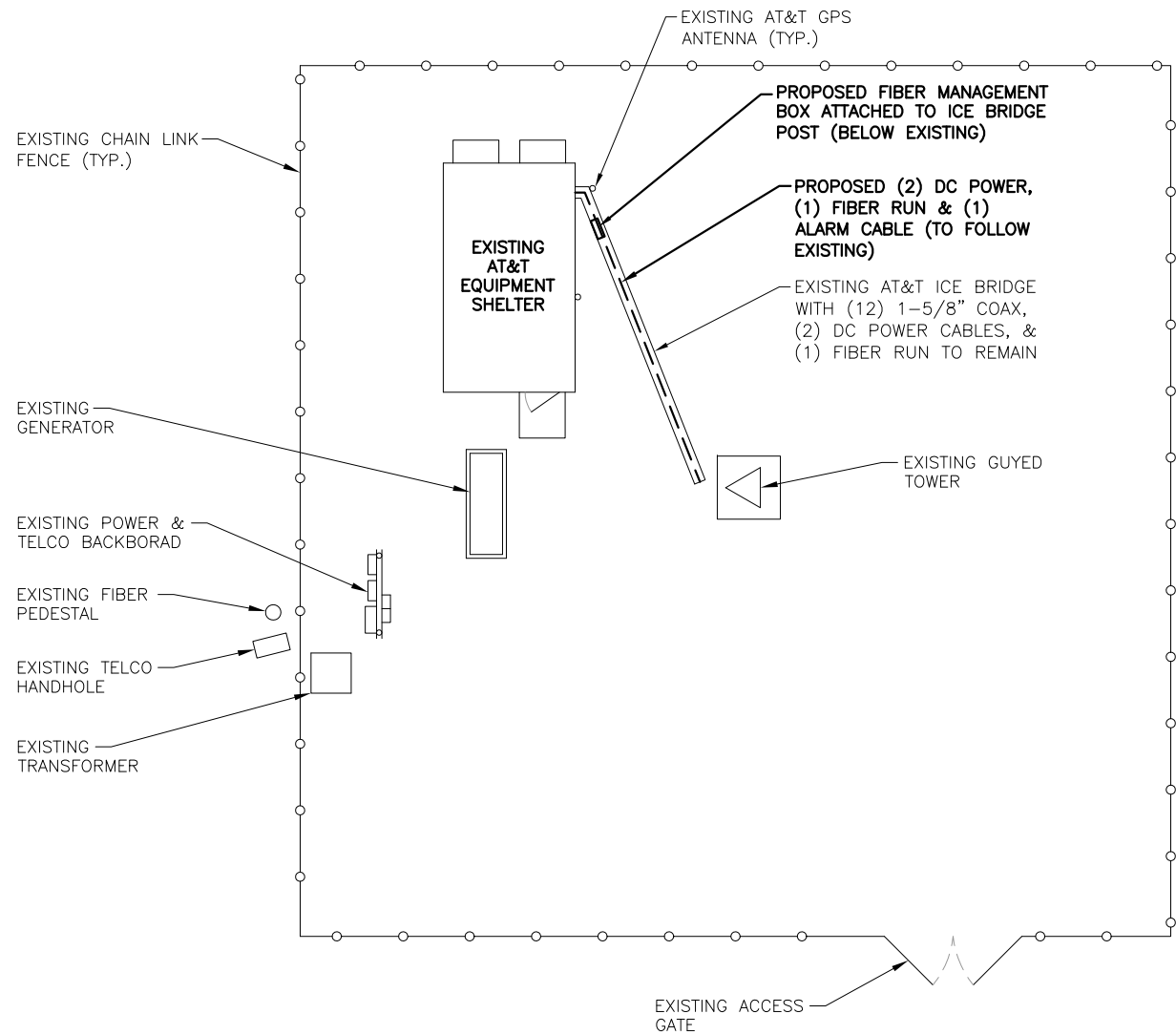
SITE NUMBER	DRAWING NUMBER	REV
CT1185	GN-1	1



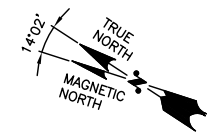
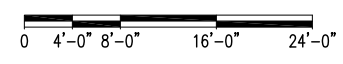
NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING **ANTENNA MOUNT** TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: JANUARY 26, 2018

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION.

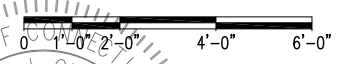
NOTE:
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.



COMPOUND PLAN
22x34 SCALE: 1/8"=1'-0"
11x17 SCALE: 1/16"=1'-0"



EQUIPMENT PLAN
22x34 SCALE: 1/2"=1'-0"
11x17 SCALE: 1/4"=1'-0"



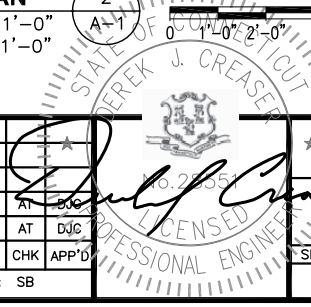
HUDSON Design Group LLC
45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
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CENTERLINE COMMUNICATIONS
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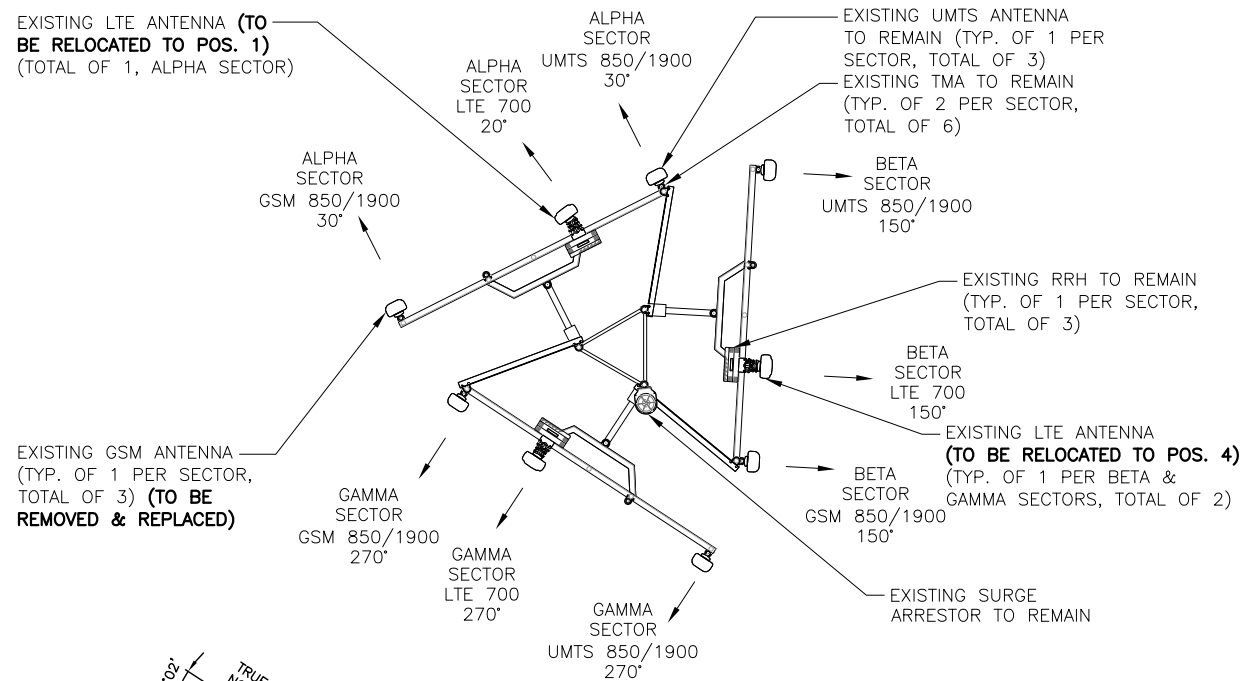
at&t
500 ENTERPRISE DRIVE, SUITE 3A
ROCKY HILL, CT 06067

1	02/20/18	ISSUED FOR CONSTRUCTION	SG	AT	SB
A	10/16/17	ISSUED FOR REVIEW	SB	AT	DJC
NO.	DATE	REVISIONS	BY	CHK	APP'D
SCALE: AS SHOWN		DESIGNED BY: AT	DRAWN BY: SB		

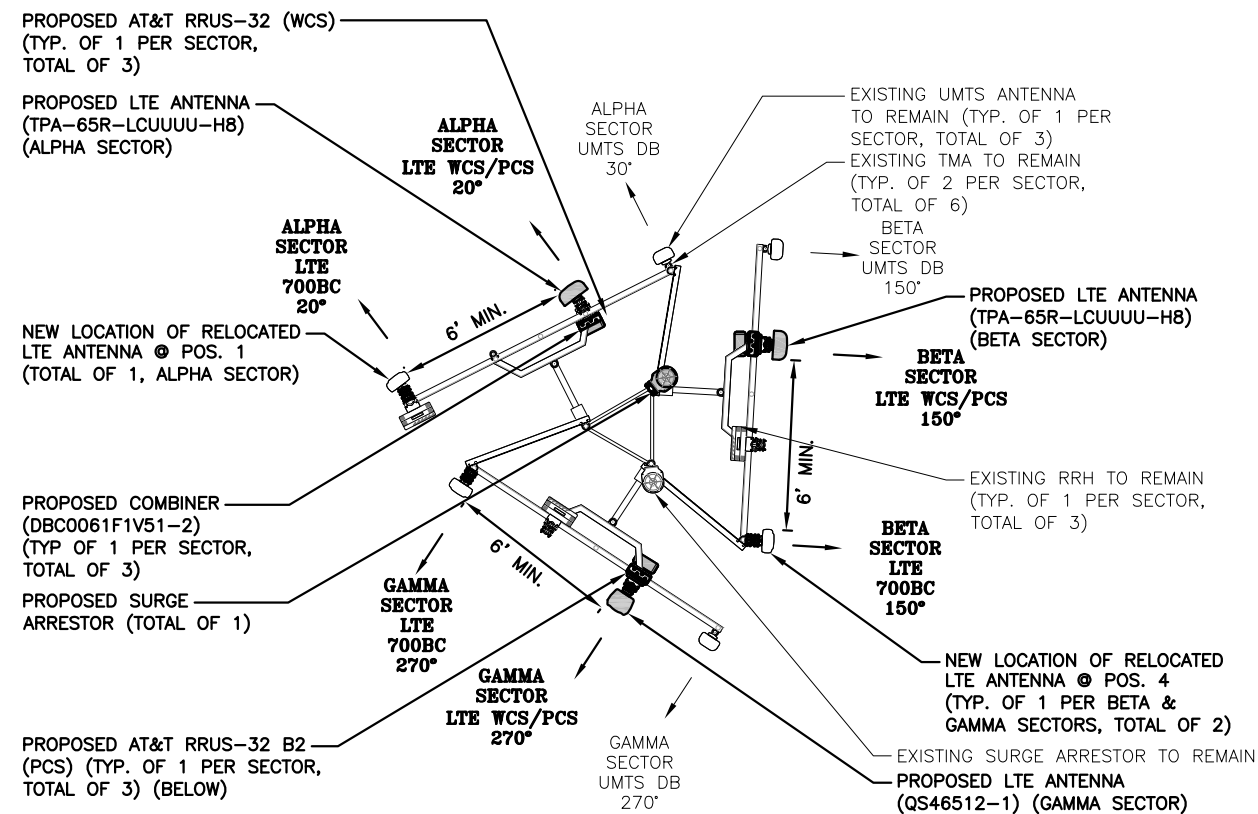


AT&T
COMPOUND & EQUIPMENT PLANS
(LTE 2C/3C)

SITE NUMBER	DRAWING NUMBER	REV
CT1185	A-1	1



EXISTING ANTENNA LAYOUT (1)
SCALE: N.T.S.

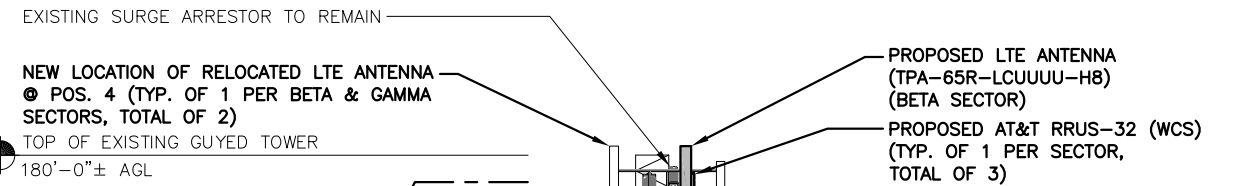


PROPOSED ANTENNA LAYOUT (2)
SCALE: N.T.S.

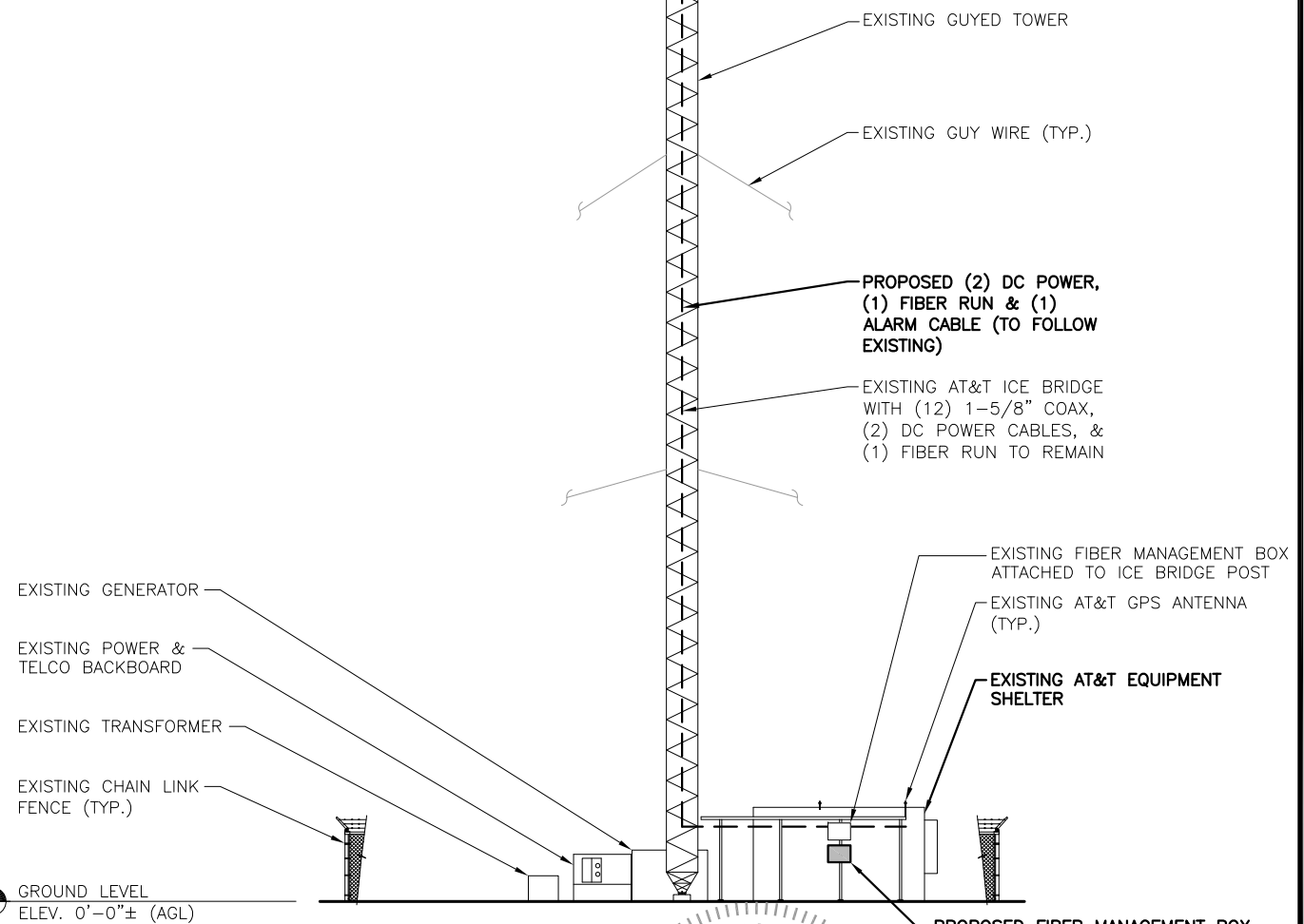
NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING ANTENNA MOUNT TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: JANUARY 26, 2018

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION.

NOTE:
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.



EXISTING SURGE ARRESTOR TO REMAIN
NEW LOCATION OF RELOCATED LTE ANTENNA @ POS. 4 (TYP. OF 1 PER BETA & GAMMA SECTORS, TOTAL OF 2)
TOP OF EXISTING GUYED TOWER
180'-0"± AGL
CENTER OF EXISTING & PROPOSED AT&T ANTENNAS
177'-0"± (AGL)
EXISTING RRH TO REMAIN (TYP. OF 1 PER SECTOR, TOTAL OF 3)
PROPOSED AT&T RRUS-32 B2 (PCS) (TYP. OF 1 PER SECTOR, TOTAL OF 3)



EXISTING GUYED TOWER
EXISTING GUY WIRE (TYP.)
PROPOSED (2) DC POWER, (1) FIBER RUN & (1) ALARM CABLE (TO FOLLOW EXISTING)
EXISTING AT&T ICE BRIDGE WITH (12) 1-5/8" COAX, (2) DC POWER CABLES, & (1) FIBER RUN TO REMAIN
EXISTING FIBER MANAGEMENT BOX ATTACHED TO ICE BRIDGE POST
EXISTING AT&T GPS ANTENNA (TYP.)
EXISTING AT&T EQUIPMENT SHELTER
PROPOSED FIBER MANAGEMENT BOX ATTACHED TO ICE BRIDGE POST
GROUND LEVEL
ELEV. 0'-0"± (AGL)

ELEVATION
22x34 SCALE: 3/32"=1'-0"
11x17 SCALE: 3/64"=1'-0"

HUDSON Design Group LLC
45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
FAX: (978) 336-5586

CENTERLINE COMMUNICATIONS
95 RYAN DRIVE
RAYNHAM, MA 02767

SITE NUMBER: CT1185
SITE NAME: STAFFORD SPRINGS
TOLLAND AVENUE
64 TOLLAND AVENUE
STAFFORD, CT 06076
TOLLAND COUNTY

at&t
500 ENTERPRISE DRIVE, SUITE 3A
ROCKY HILL, CT 06067

NO.	DATE	REVISIONS	BY	CHK	APP'D
1	02/20/18	ISSUED FOR CONSTRUCTION	SG	AT	
A	10/16/17	ISSUED FOR REVIEW	SB	AT	DJC

SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: SB

AT&T
ANTENNA PLANS & ELEVATION
(LTE 2C/3C)
SITE NUMBER: CT1185 DRAWING NUMBER: A-2 REV: 1

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING ANTENNA MOUNT TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: JANUARY 26, 2018

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION.

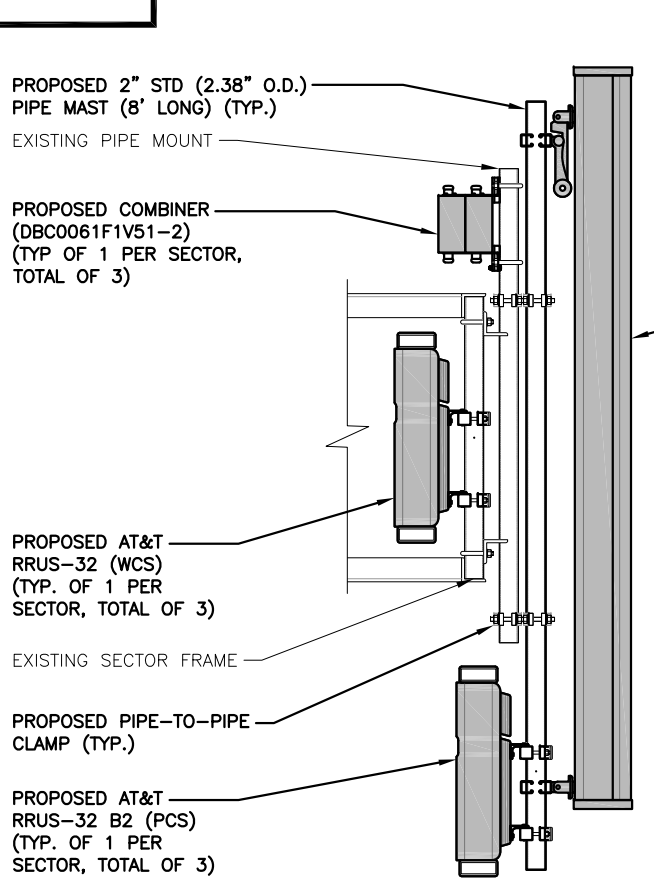
NOTE:
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

***COAX JUMPER NOTE:**
COAX JUMPERS (4) PER SECTOR, SECTOR FROM EACH RRU (TOTAL OF 12).

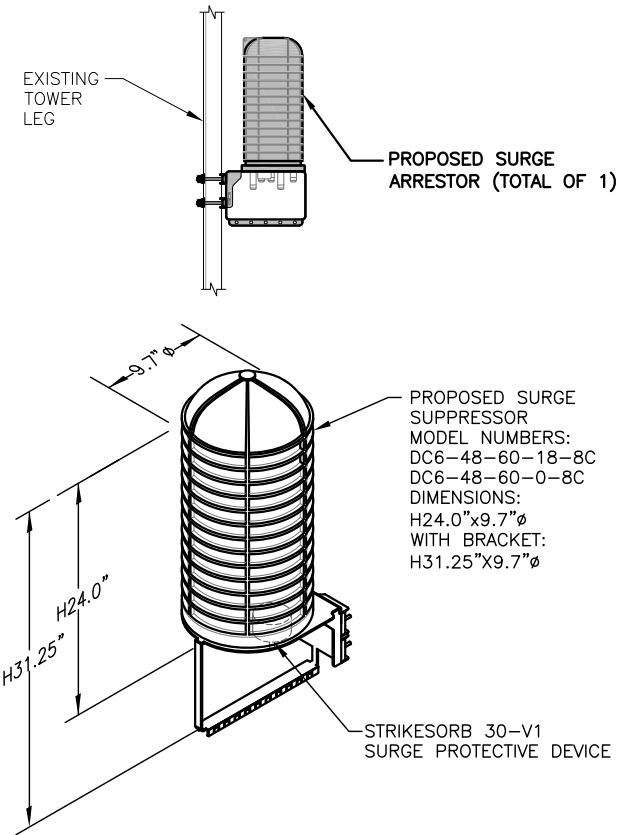
****FIBER JUMPER NOTE:**
FIBER JUMPERS (2) PER SECTOR FROM THE SQUID TO EACH RRU (TOTAL OF 6).

FINAL ANTENNA SCHEDULE													
SECTOR	BAND	ANTENNA	SIZE (INCHES) (L x W x D)	RAD CENTER	AZIMUTH	COMBINERS	TMA'S	RRU'S	SIZE (INCHES) (L x W x D)	COAX JUMPERS	FIBER JUMPERS	COAX	
ALPHA	LTE 700 BC	EXISTING	SBNH-1D6565C	96.4x11.9x7.1	177'-0"±	20°	-	EXISTING	RRUS-11 (700)	-	-	-	
	-	-	-	-	-	-	-	-	-	-	-	-	
	LTE PCS/WCS	PROPOSED	TPA-65R-LCUUUU-H8	96.0x14.4x8.6	177'-0"±	20°	PROPOSED G PROPOSED	(1)DBC0061F1V51-2 (1)DBC0061F1V51-2	PROPOSED RRUS-32 (WCS) RRUS-32-B2 (PCS)	27.2X12.1X7.0 27.2X12.1X7.0	2* 2*	1** 1**	(2) 1-5/8"
BETA	UMTS DB	EXISTING	7770	55.0x11.0x5.0	177'-0"±	30°	-	EXISTING	(2)LGP21401	-	-	(2) 1-5/8"	
	UMTS 850	EXISTING	7770	55.0x11.0x5.0	177'-0"±	150°	-	EXISTING	(2)LGP21401	-	-	(2) 1-5/8"	
	LTE 850/700 BC/PCS/WCS	PROPOSED	TPA-65R-LCUUUU-H8	96X14.4X8.6	177'-0"±	150°	PROPOSED G PROPOSED	(1)DBC0061F1V51-2 (1)DBC0061F1V51-2	PROPOSED RRUS-32 (WCS) RRUS-32-B2 (PCS)	27.2X12.1X7.0 27.2X12.1X7.0	2* 2*	1** 1**	(2) 1-5/8"
GAMMA	LTE 700 BC	EXISTING	P65-17-XLH-RR	96.0x12.0x6.0	177'-0"±	150°	-	EXISTING	RRUS-11 (700)	-	-	-	
	UMTS 850	EXISTING	7770	55.0x11.0x5.0	177'-0"±	270°	-	EXISTING	(2)LGP21401	-	-	(2) 1-5/8"	
	LTE 850/700 BC/PCS/WCS	PROPOSED	QS46512-1	52.0x12.0x10.8	177'-0"±	270°	PROPOSED G PROPOSED	(1)DBC0061F1V51-2 (1)DBC0061F1V51-2	PROPOSED RRUS-32 (WCS) RRUS-32-B2 (PCS)	27.2X12.1X7.0 27.2X12.1X7.0	2* 2*	1** 1**	(2) 1-5/8"
GAMMA	LTE 700 BC	EXISTING	AM-X-CD-14-65-00T-RET	48.0x11.8x5.9	177'-0"±	270°	-	EXISTING	RRUS-11 (700)	-	-	-	

FINAL ANTENNA CONFIGURATION TABLE 5
A-3



PROPOSED ANTENNA AND RRH MOUNTING DETAIL 1
A-3
SCALE: N.T.S.



DC SURGE SUPPRESSOR DETAIL 2
A-3
SCALE: N.T.S.

RRH CHART				
QUANTITY	MODEL	L	W	D
3(E)	RRUS-11	19.7"	17.0"	7.2"
6(P)	RRUS-32	27.2"	12.1"	7.0"

NOTE:
MOUNT PER MANUFACTURER'S SPECIFICATIONS

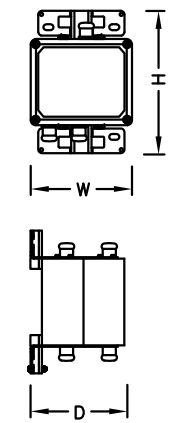
NOTE:
SEE RFDS FOR RRH FREQUENCY AND MODEL NUMBER

PROPOSED RRH REFER TO THE FINAL RFDS AND CHART FOR QUANTITY, MODEL AND DIMENSIONS

NOTE:
MOUNT PER MANUFACTURER'S SPECIFICATIONS.

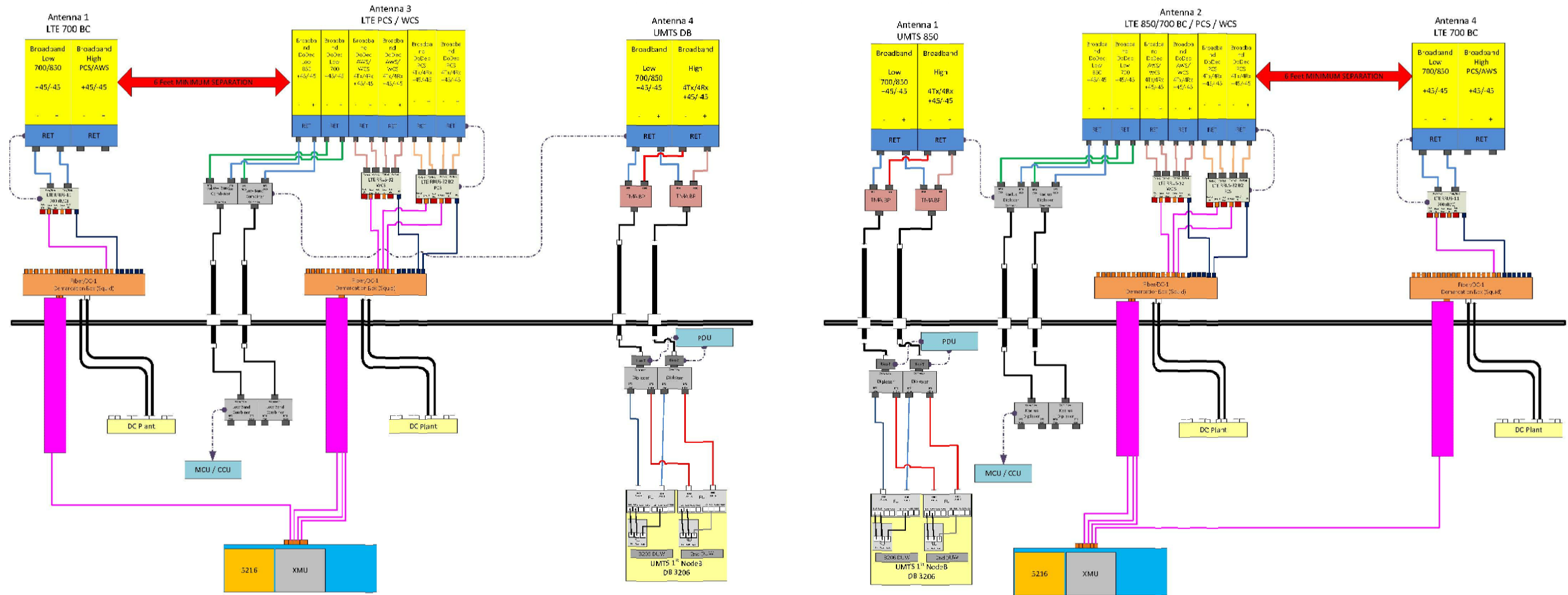
PROPOSED RRH DETAIL 3
A-3
SCALE: N.T.S.

COMBINER DIMENSIONS	
MODEL #	DBC0061F1V51-2
MANUF.	KAELUS
HEIGHT	10.24"
WIDTH	7.98"
DEPTH	7.65"



PROPOSED COMBINER 4
A-3
SCALE: N.T.S.

<p>45 BEECHWOOD DRIVE NORTH ANDOVER, MA 01845 TEL: (978) 557-5553 FAX: (978) 336-5586</p>	<p>95 RYAN DRIVE RAYNHAM, MA 02767</p>	<p>SITE NUMBER: CT1185 SITE NAME: STAFFORD SPRINGS TOLLAND AVENUE 64 TOLLAND AVENUE STAFFORD, CT 06076 TOLLAND COUNTY</p>	<p>500 ENTERPRISE DRIVE, SUITE 3A ROCKY HILL, CT 06067</p>	<p>1 02/20/18 ISSUED FOR CONSTRUCTION SG AT</p> <p>A 10/16/17 ISSUED FOR REVIEW SB AT DJC</p> <p>NO. DATE REVISIONS BY CHK APP'D</p>	<p>AT&T DETAILS (LTE 2C/3C)</p>
				<p>SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: SB</p>	<p>SITE NUMBER: CT1185 DRAWING NUMBER: A-3 REV: 1</p>

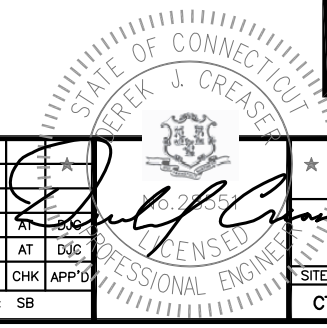


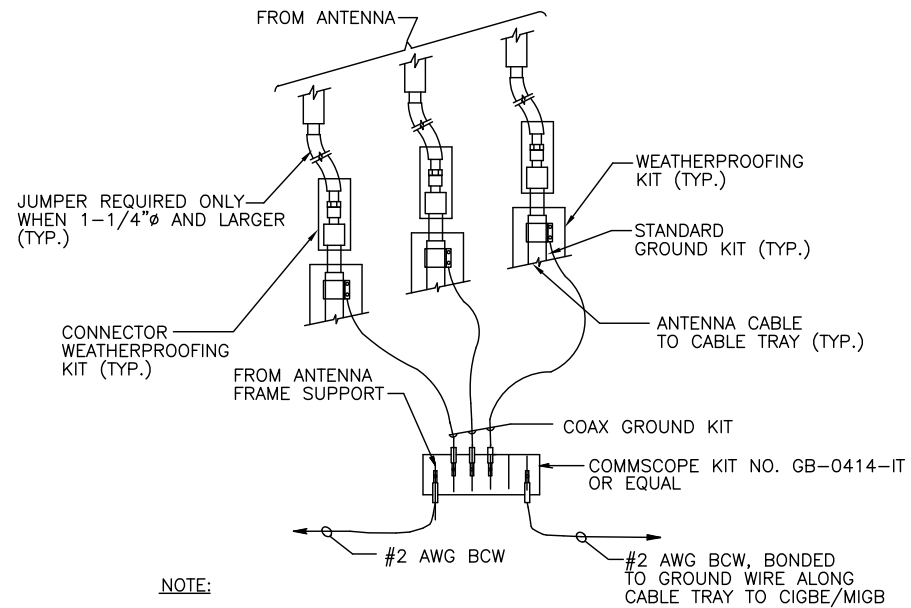
**RF PLUMBING DIAGRAM
ALPHA SECTOR**
SCALE: N.T.S. 1
RF-1

**RF PLUMBING DIAGRAM
BETA & GAMMA SECTORS**
SCALE: N.T.S. 2
RF-1

NOTE:
1. CONTRACTOR TO CONFIRM ALL PARTS.
2. INSTALL ALL EQUIPMENT TO MANUFACTURER'S RECOMMENDATIONS

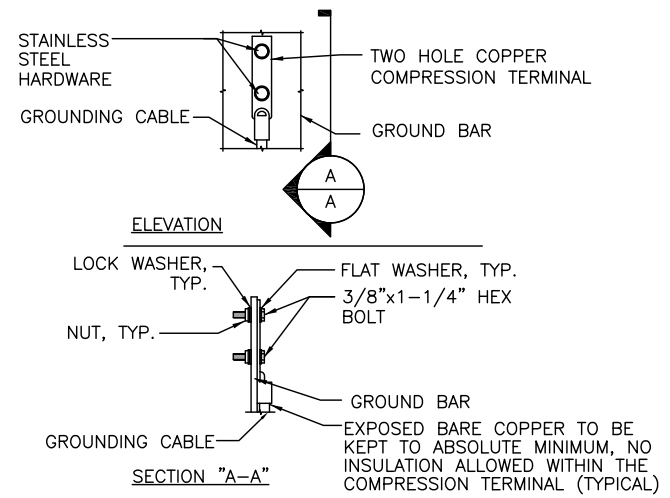
NOTE:
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.





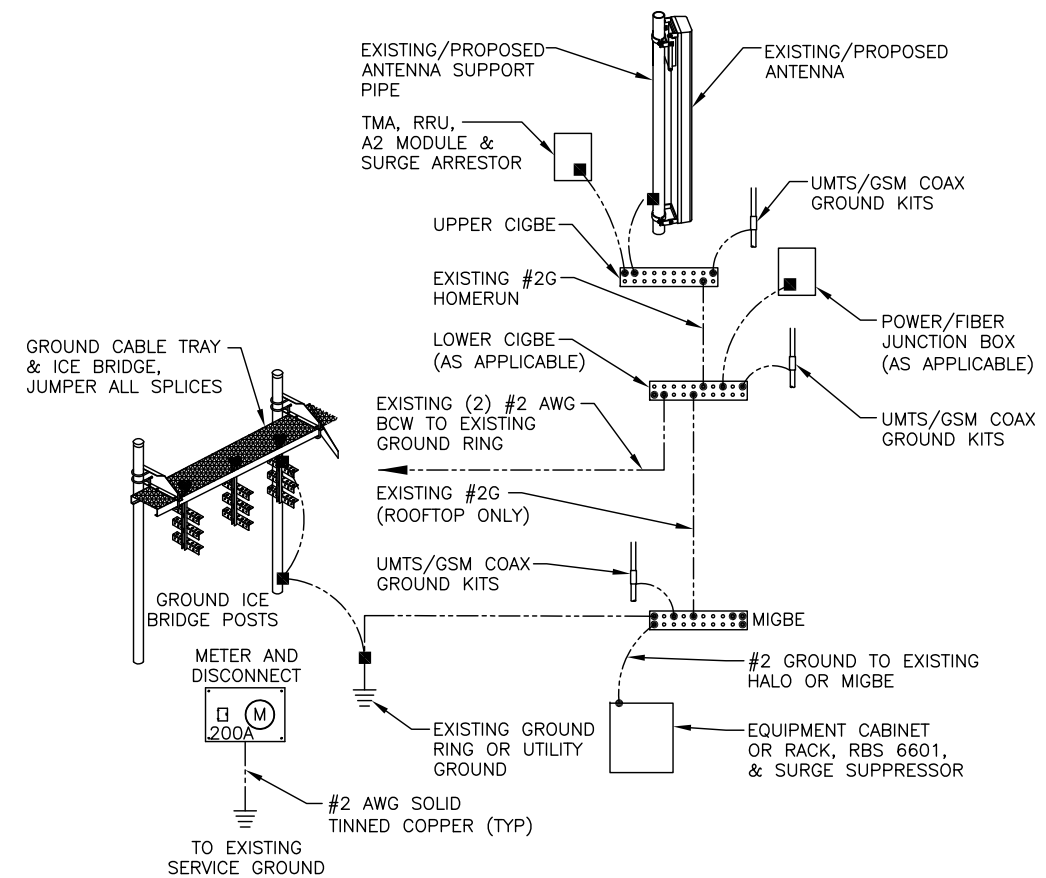
NOTE:
 1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

GROUND WIRE TO GROUND BAR CONNECTION DETAIL 1
 SCALE: N.T.S. G-1



NOTE:
 1. "DOUBLING UP" OR "STACKING" OF CONNECTION IS NOT PERMITTED.
 2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATION.
 3. CADWELD DOWNLEADS FROM UPPER EGB, LOWER EGB, AND MGB

TYPICAL GROUND BAR CONNECTION DETAIL 3
 SCALE: N.T.S. G-1



GROUNDING RISER DIAGRAM 2
 SCALE: N.T.S. G-1

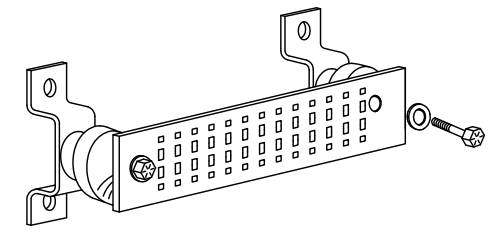
EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS ORIGIN AND DESTINATION.

SECTION "P" - SURGE PRODUCERS

- CABLE ENTRY PORTS (HATCH PLATES) (#2)
- GENERATOR FRAMEWORK (IF AVAILABLE) (#2)
- TELCO GROUND BAR
- COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2)
- +24V POWER SUPPLY RETURN BAR (#2)
- 48V POWER SUPPLY RETURN BAR (#2)
- RECTIFIER FRAMES.

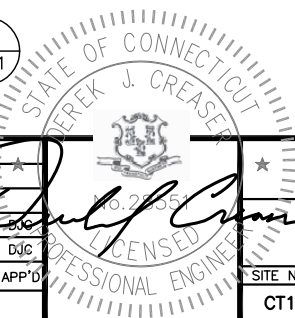
SECTION "A" - SURGE ABSORBERS

- INTERIOR GROUND RING (#2)
- EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2)
- METALLIC COLD WATER PIPE (IF AVAILABLE) (#2)
- BUILDING STEEL (IF AVAILABLE) (#2)

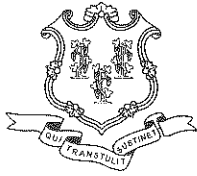


GROUND BAR - DETAIL 4
 SCALE: N.T.S. G-1

NO.	DATE	REVISIONS	BY	CHK	APP'D
1	02/20/18	ISSUED FOR CONSTRUCTION	SG	AT	
A	10/16/17	ISSUED FOR REVIEW	SB	AT	DJC
SCALE: AS SHOWN		DESIGNED BY: AT	DRAWN BY: SB		



AT&T		
GROUNDING DETAILS (LTE 2C/3C)		
SITE NUMBER	DRAWING NUMBER	REV
CT1185	G-1	1



STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051
Phone: (860) 827-2935 Fax: (860) 827-2950
E-Mail: siting.council@ct.gov
www.ct.gov/csc

September 7, 2012

Jennifer Young Gaudet
HPC Wireless Services
46 Mill Plain Road, Floor 2
Danbury, CT 06811

RE: **EM-CING-134-120820A** – New Cingular Wireless PCS, LLC notice of intent to modify an existing telecommunications facility located at **64 Tolland Avenue**, Stafford Springs, Connecticut.

Dear Ms. Gaudet:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies with the following conditions:

- Any deviation from the proposed modification as specified in this notice and supporting materials with Council shall render this acknowledgement invalid;
- Any material changes to this modification as proposed shall require the filing of a new notice with the Council;
- Not less than 45 days after completion of construction, the Council shall be notified in writing that construction has been completed;
- The validity of this action shall expire one year from the date of this letter; and
- The applicant may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration;

The proposed modifications including the placement of all necessary equipment and shelters within the tower compound are to be implemented as specified here and in your notice dated August 17, 2012. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding

the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Thank you for your attention and cooperation.

Very truly yours,



Linda Roberts
Executive Director

LR/CDM/cm

c: The Honorable Richard L. Shuck, First Selectman, Town of Stafford
Richard L. Shuck, Zoning Enforcement Officer, Town of Stafford
Cordless Data Transfer