

STATE OF CONNECTICUT CONNECTICUT SITING COUNCIL Ten Franklin Square, New Britain, CT 06051 Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov www.ct.gov/csc

VIA ELECTRONIC MAIL

October 10, 2019

Kristina Cottone Real Estate Specialist Smartlink, LLC 85 Rangeway Road, Building 3, Suite 102 Billerica, MA 01862

RE: **EM-AT&T-103-190916** – AT&T Mobility, LLC notice of intent to modify an existing telecommunications facility located at 600 Connecticut Avenue, Norwalk, Connecticut.

Dear Ms. Cottone:

The Connecticut Siting Council (Council) is in receipt of your correspondence of September 23, 2019 and October 7, 2019 submitted in response to the Council's September 20, 2019 and October 1, 2019 notification of an incomplete request for exempt modification with regard to the above-referenced matter.

The submissions render the request for exempt modification complete and the Council will process the request in accordance with the Federal Communications Commission 60-day timeframe.

Thank you for your attention and cooperation.

Sincerely,

Melanie A. Bachman Executive Director

MAB/IN/emr



Robidoux, Evan

From:	Kristina Cottone <kristina.cottone@smartlinkllc.com></kristina.cottone@smartlinkllc.com>
Sent:	Monday, October 07, 2019 10:59 AM
То:	Robidoux, Evan
Cc:	CSC-DL Siting Council
Subject:	RE: Council Incomplete Letter
Attachments:	10034974_DE118_181206_CTL02108_MA_PASS w Mods.pdf

Good morning,

Please see attached requested document to finish this outstanding CSC filing. Please let me know if you need anything else.

Thank you,



Kristina Cottone | Real Estate Specialist Smartlink

85 Rangeway Road – Building 3 Suite 102 North Billerica MA, 01862 (m) 978.551.8627 <u>Kristina.cottone@Smartlinkllc.com</u> <u>smartlinkllc.com</u>

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From: Robidoux, Evan <Evan.Robidoux@ct.gov>
Sent: Wednesday, October 2, 2019 10:37 AM
To: Kristina Cottone <kristina.cottone@smartlinkllc.com>
Cc: CSC-DL Siting Council <Siting.Council@ct.gov>
Subject: Council Incomplete Letter

Warning: This message was sent from outside the company and could contain attachments. Please do not open unless you recognize the source of this email and know the content is safe.

Please see the attached correspondence.

Evan Robidoux Clerk Typist Connecticut Siting Council 10 Franklin Square New Britain, CT 06051 December 5, 2018

RE:	AT&T LTE 4C/5C/6C/7C/ RRH ADD
Prepared For:	Smartlink / AT&T
Site Number:	CTL02108
FA Location:	10034974
Pace Number:	MRCTB025283/MRCTB025338/MRCTB025304/
	MRCTB026716/MRCTB017068
Site Name:	NORWALK WEST-CT AVE.
Site Address:	613 Connecticut Avenue
	Norwalk, CT 06850

To Whom It May Concern,

This structural assessment is in regards to the adequacy of the existing low profile platform with handrails for the AT&T LTE 4C/5C/6C/7C/RRH ADD project. The purpose was to determine conformance of the existing antenna mounting structure under the 2018 Connecticut State Building Code and the industry standard ANSI/TIA-222-G (Structural Standards for Steel Antenna Towers and Antenna Supporting Structures). The antenna and the equipment supports were rated to the code requirement of 121 mph ultimate design wind speed, 110 m ph (3-second gust) basic wind speed, and an ice thickness of 0.75in. In addition, the mount has been analyzed for various live loading conditions consisting of a 250-pound man live load applied individually at the midpoint and cantilevered ends of horizontal members as well as a 500-pound man live load applied individually at mount pipe locations using a 3-second gust wind speed of 30 mph.

Based on collected information via a site visit dated 10/22/2018, technical data of the proposed equipment, structural calculations and engineering judgment, the existing low-profile platform with handrails is **adequate** to support the proposed installation for the above-referenced program. For installation details, see latest construction drawings prepared by Fullerton Engineering.

This PE certification completed by Fullerton Engineering Consultants is inclusive of the existing antenna mounting structure that will support the existing and proposed loading provided by the client.

This certification assumes that all the existing structural members of the existing antenna mounting structure are in good condition and have not been altered from the manufacturer's original design. Prior to installation of new equipment, contractor shall inspect the condition of all relevant members and connectors. The contractor shall be responsible for the means and methods of construction.

Respectfully,

Henry M. Bellagamba, P.E.



NETWORK INTEGRITY STARTS HERE

FULLERTON ENGINEERING · DESIGN

Fullerton Engineering Consultants, Inc.

1100 E. Woodfield Road, Suite 500 Schaumburg, IL 60173 Tel: 847.908.8400 www.fullertonengineering.com

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Site Number: CTL02108 Site Name: Norwalk West-Ct Ave. Created By: RH Checked By: ВК 12/5/2018

Date: ANSI/TIA-222-G Code:

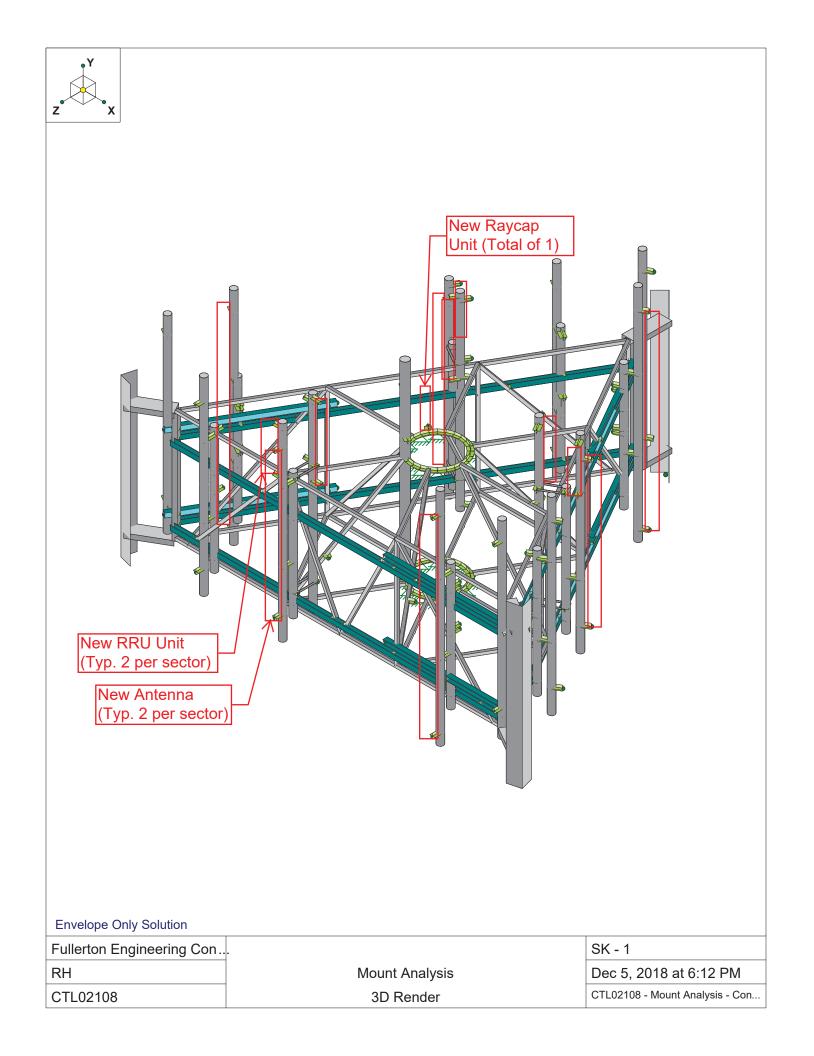
Base Structure Type	Type <mark>I</mark>	Monopole	
Structure Height Above Grade (ft)	Ht :	150.00	
RAD Center (ft)	z 🕻	135.00	
Windspeed no ice (mph, 3-sec gust)	V :	110.00	see wind maps
Windspeed with ice (mph, 3-sec gust)	Vi <mark>s</mark>	50.00	see wind maps
Windspeed for maintenance (mph, 3-sec gust)	Vm 🗄	30.00	Section 16.6
Ice Thickness	ti <mark>(</mark>	0.75	see ice maps
Exposure Category (B/C/D)	Exposure	В	Section 2.6.5.1
Topographic Category (1,2,3,4)	Торо 🕻	1	Section 2.6.6.2
Structure Class (I,II,III)	Class I	II.	Table 2-1
Crest Height (or assume 5ft)	C s	5.00	Section 2.6.6.4
Gust Effect Factor	Gh	D.85	Section 2.6.7.1
Design Ice Thickness	tiz	1.73	Section 2.6.8
Velocity Pressure for Maintenance	qzm 2	2.12	
Velocity Pressure With Ice	qzi (6.55	Section 2.6.9.6
Velocity Pressure No Ice	qz 3	31.68	Section 2.6.9.6

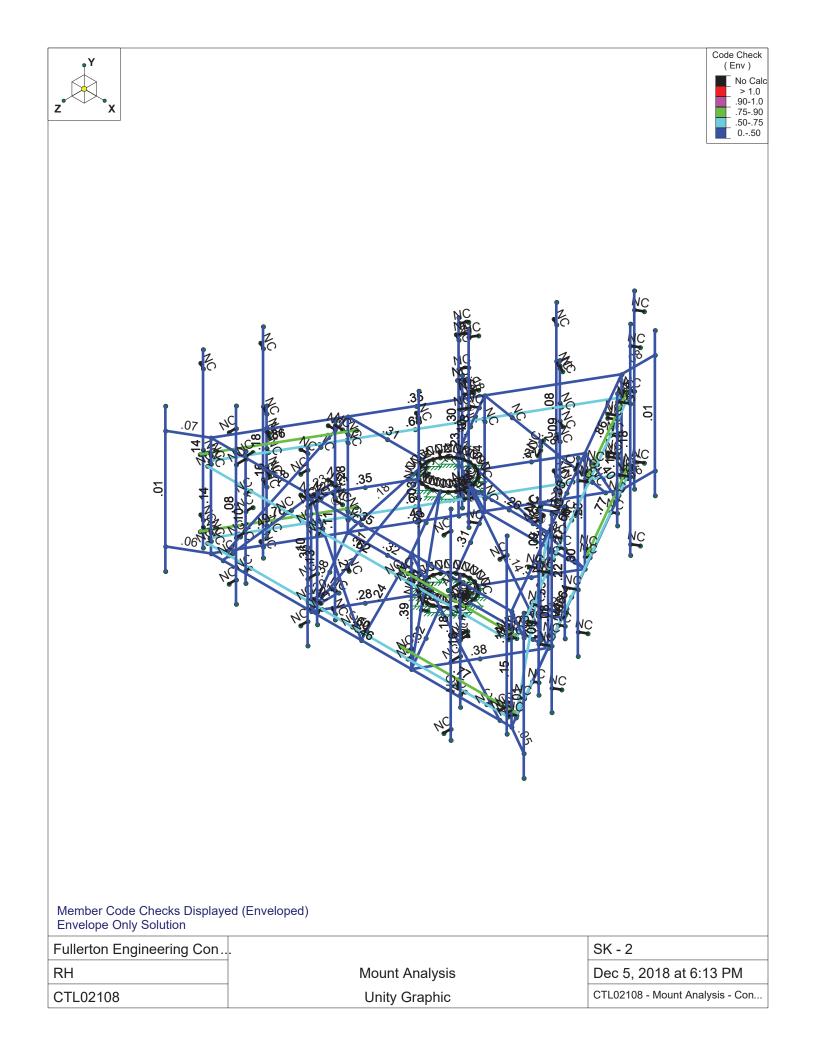
Appurtenance Properties Loads (force per connection) W Weight # Conn Wt Ice Wt Sm Manufacturer Model R/F D F no ice S no ice F ice S ice Fm L 72 Quintel 66512-2 Flat 12 9.6 111 55.5 85.7 99 82 26 23 2 7 Commscope SBNHH-1D65A Flat 55 11.9 7.1 43.5 2 21.8 53.8 71 47 20 14 5 43.0 Powerwave 7770 Flat 55 39 19.5 67 35 19 12 11 5 2 4 Ericsson RRUS 32 B2 Flat 27.2 12.1 53 2 26.5 28.9 33 20 10 7 2 7 Ericsson RRUS 4478 B14 Flat 16.5 13.4 7.7 59.5 29.8 22.5 22 2 13 5 1 Ericsson RRUS-11 Flat 19.7 17 7.2 50 2 25.0 26.0 34 14 10 5 2 Ericsson RRUS 32 Flat 27.2 12.1 60 30.0 28.9 33 20 10 7 2 2 Powerwave LGP-21401 Flat 14.4 9.2 2.6 14.1 2 7.1 10.0 13 4 5 2 1 Raycap DC6-48-60-18-8F Round 24 9.7 9.7 32.8 1 32.8 63.9 27 27 9 9 2 520.5 HSS1x1x8 Flat 126 10.5 0.0 6.6 1 1 0 4 4 4 4 0 C3x6 Flat 42 3 1.6 0 3.500 0.0 10.8 10 6 4 3 1 C5x6.7 Flat 0.0 14 5 1.8 0 1.167 14.9 12 5 5 3 1 L5x5x5 Flat 60 5 5 0 5 0.0 18.6 16 16 5 5 1 10.5 Unistrut Flat 126 1.6 1.6 0 0.0 8.4 6 6 0 4 4 0 Pipe 2.0 2.4 2.4 0 0.0 8.7 2 Round 72 6 6 6 2 0 Pipe 2.0 2.4 8 0.0 Round 96 2.4 0 8.7 6 6 3 3 0 0 . Pipe 2.5 2.9 9.8 Round 96 2.9 0 8 0.0 7 7 3 3 0

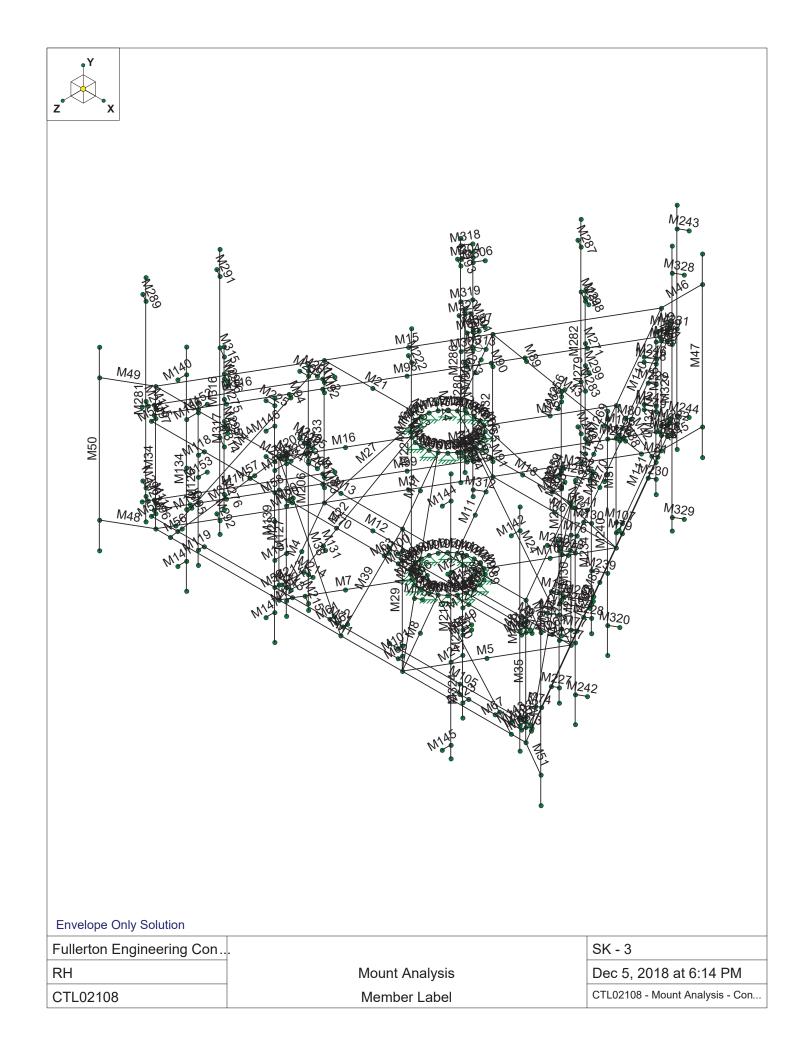
Sectors

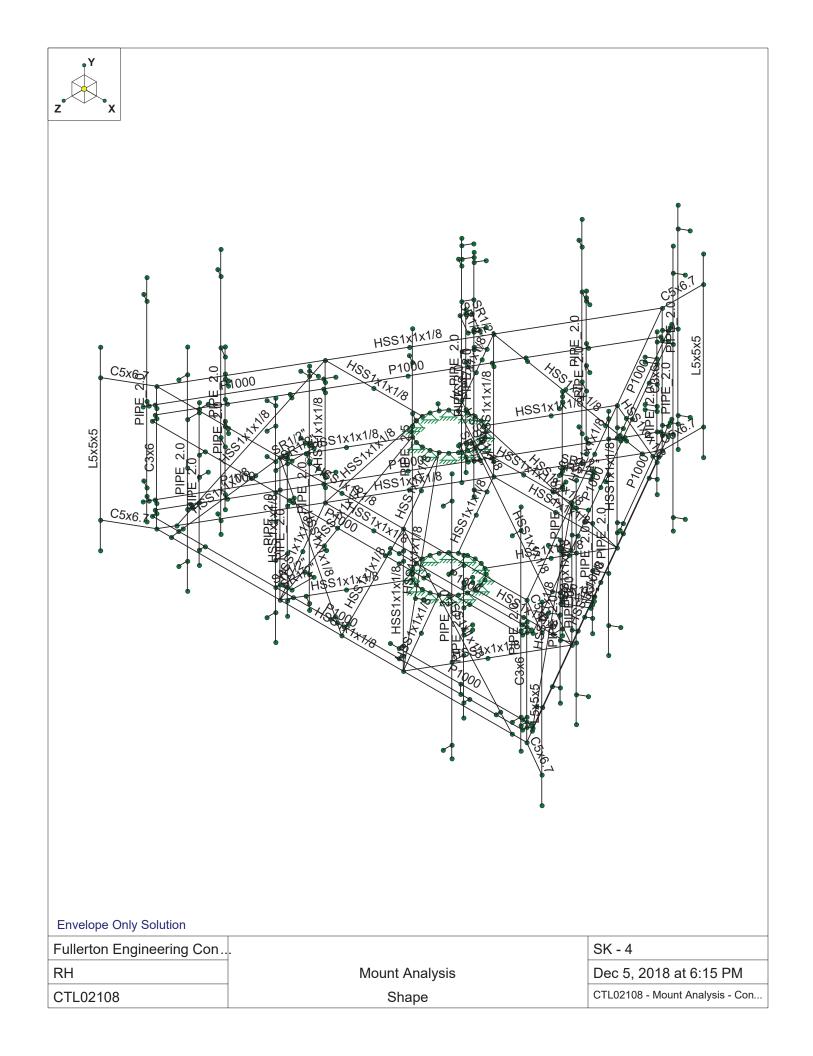
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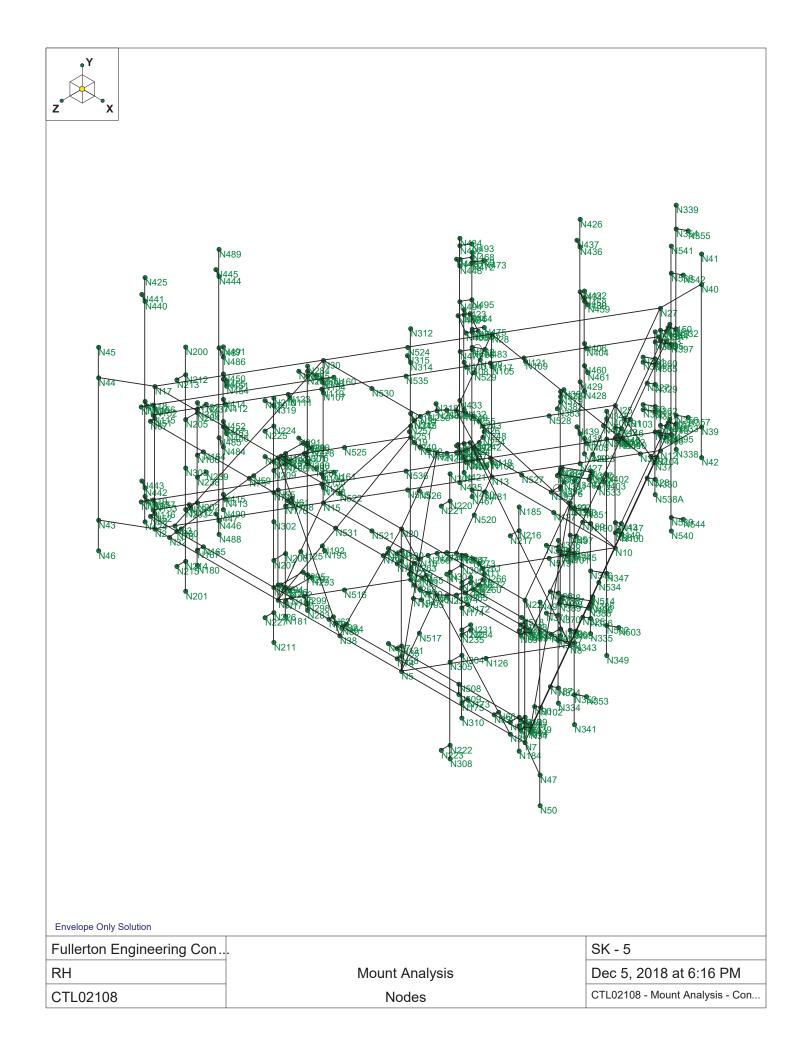
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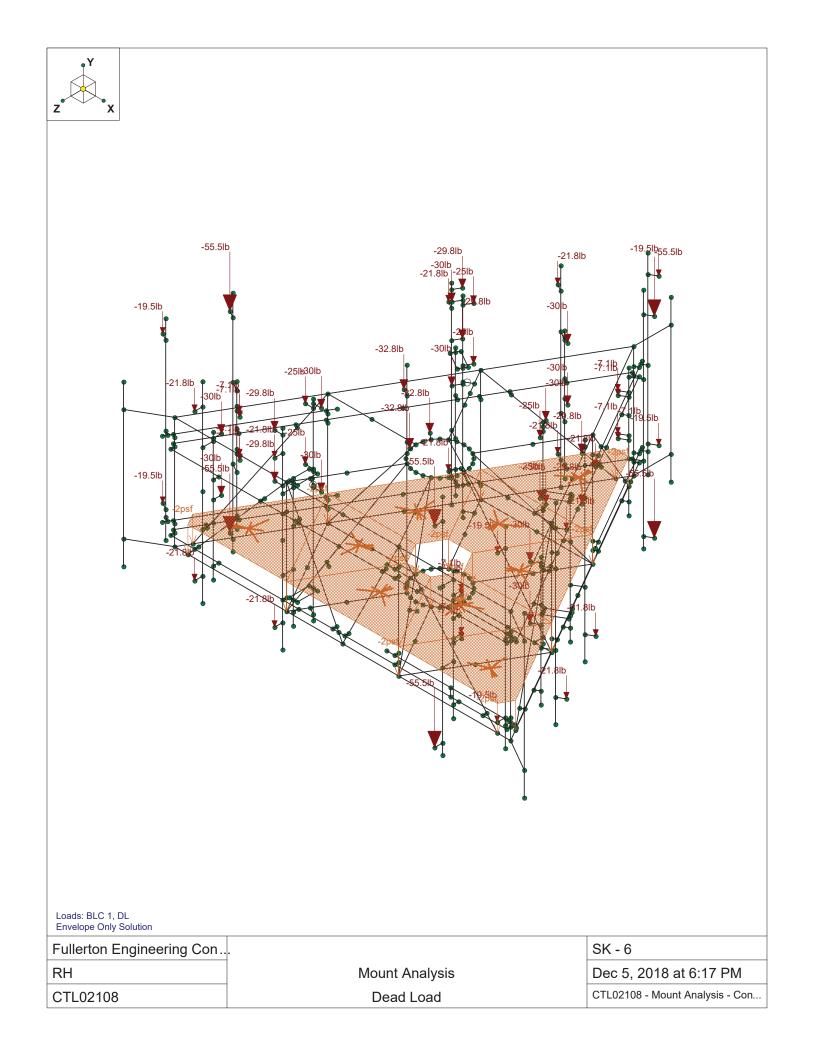


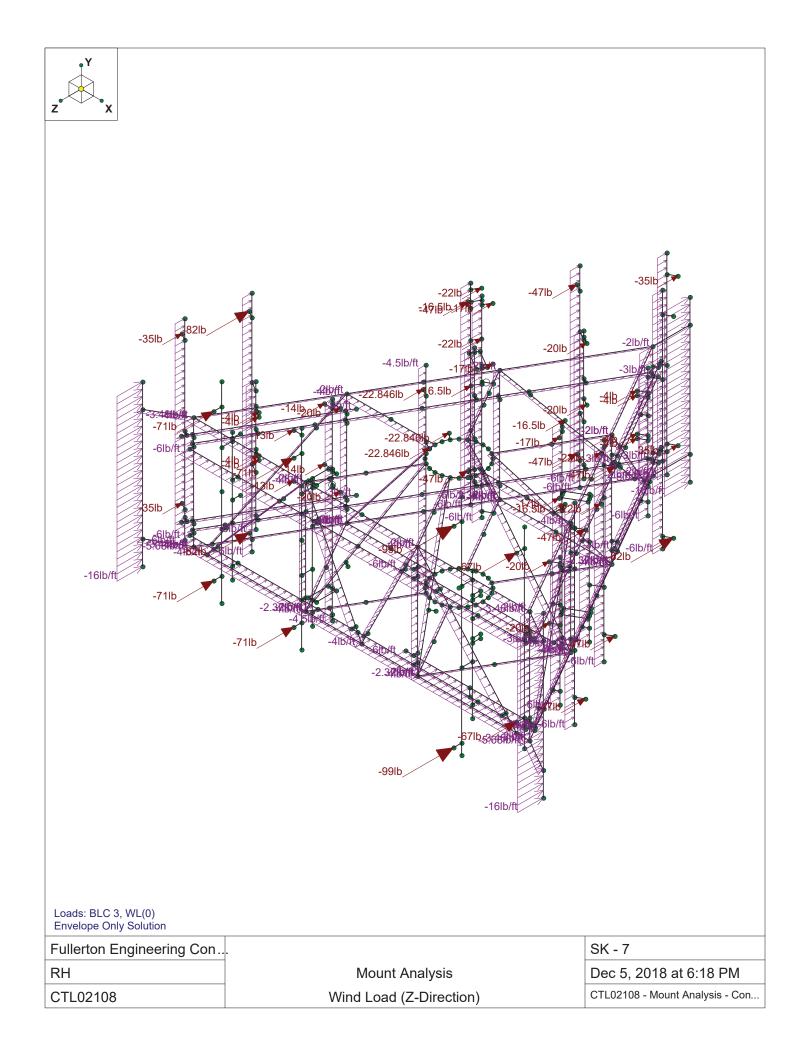


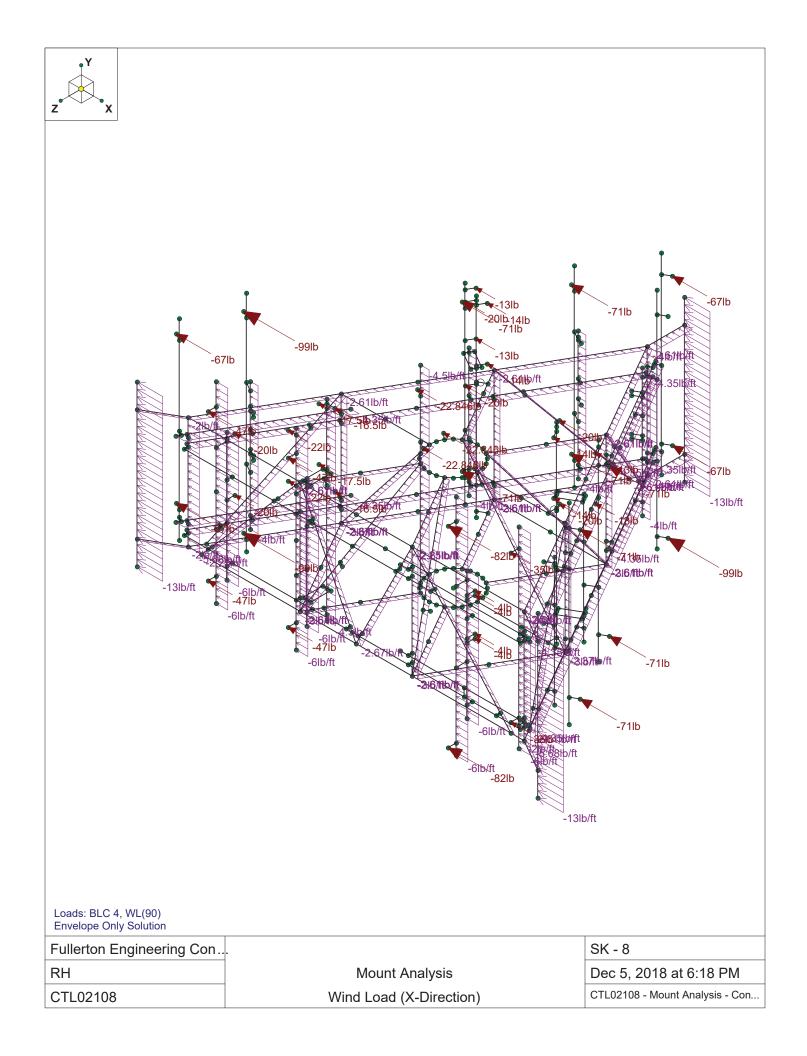


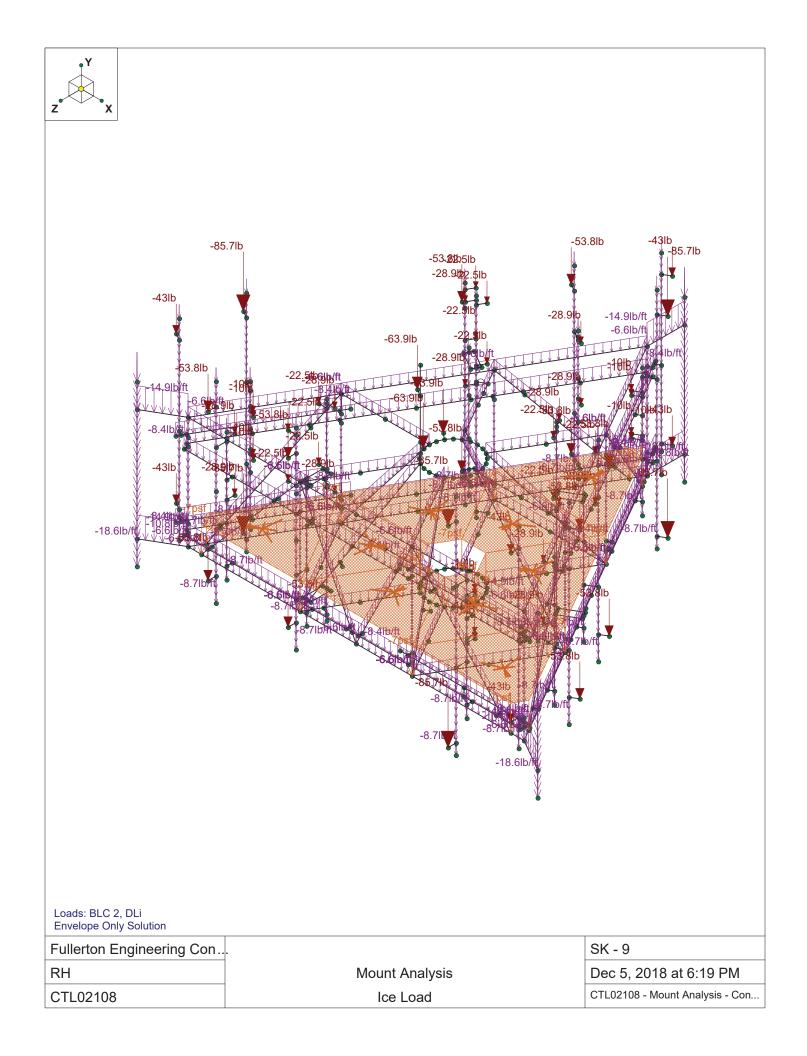


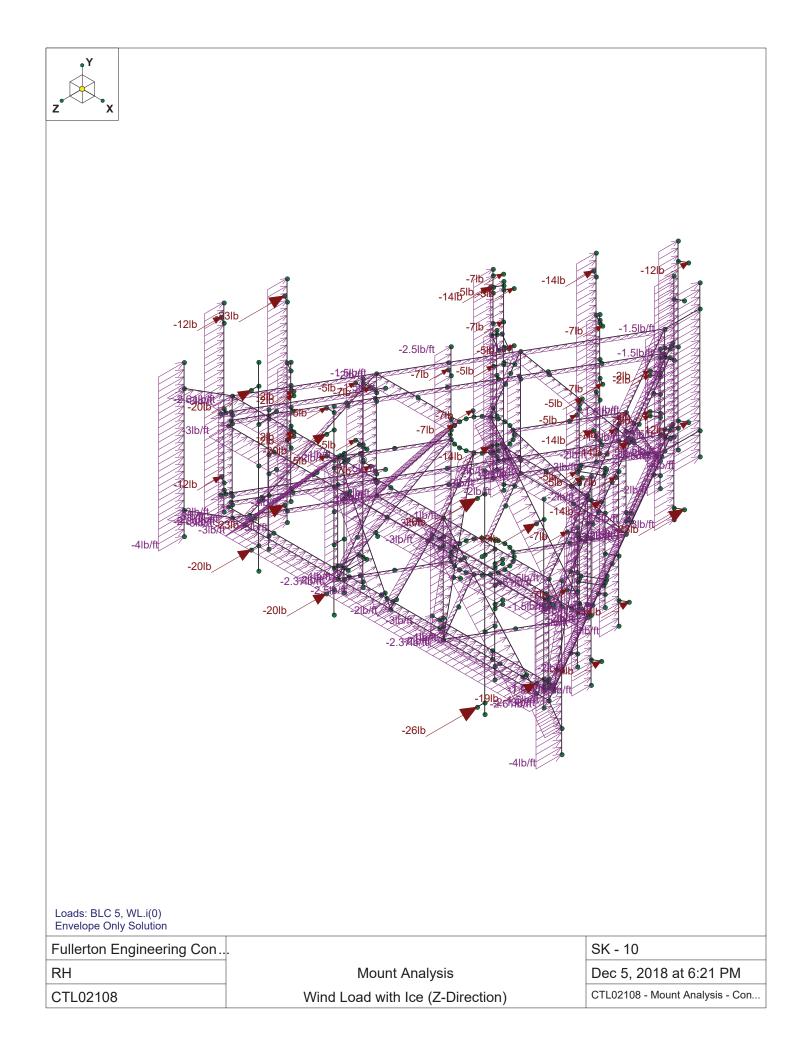


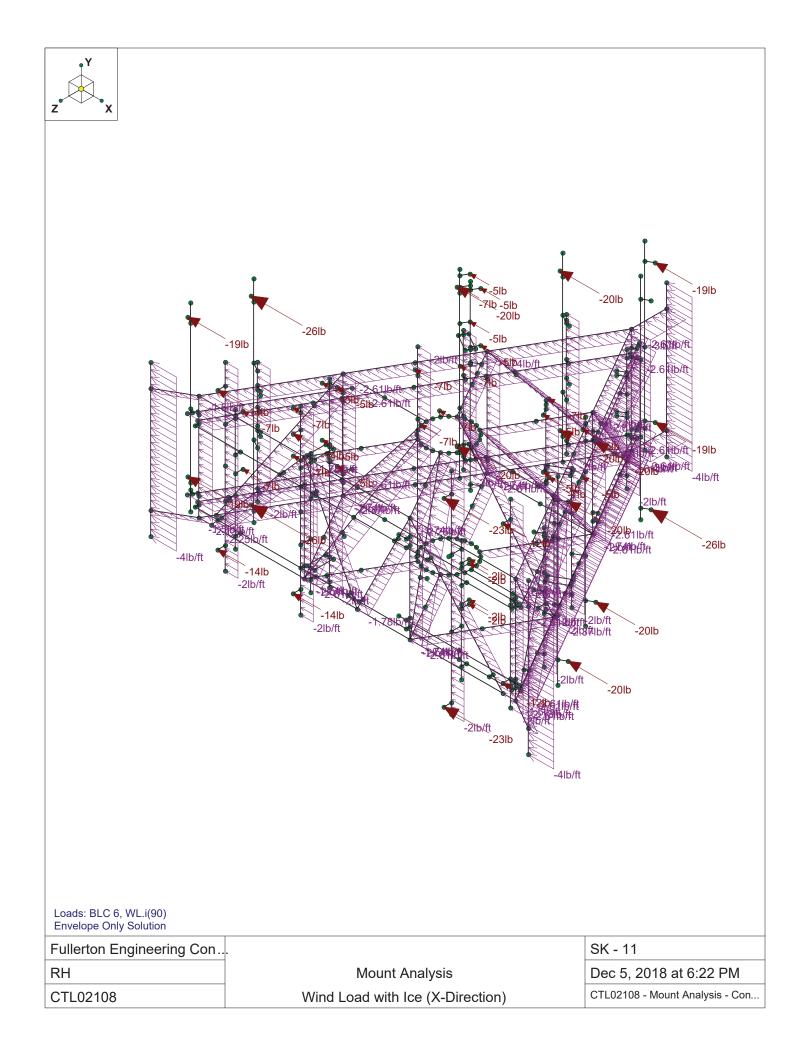


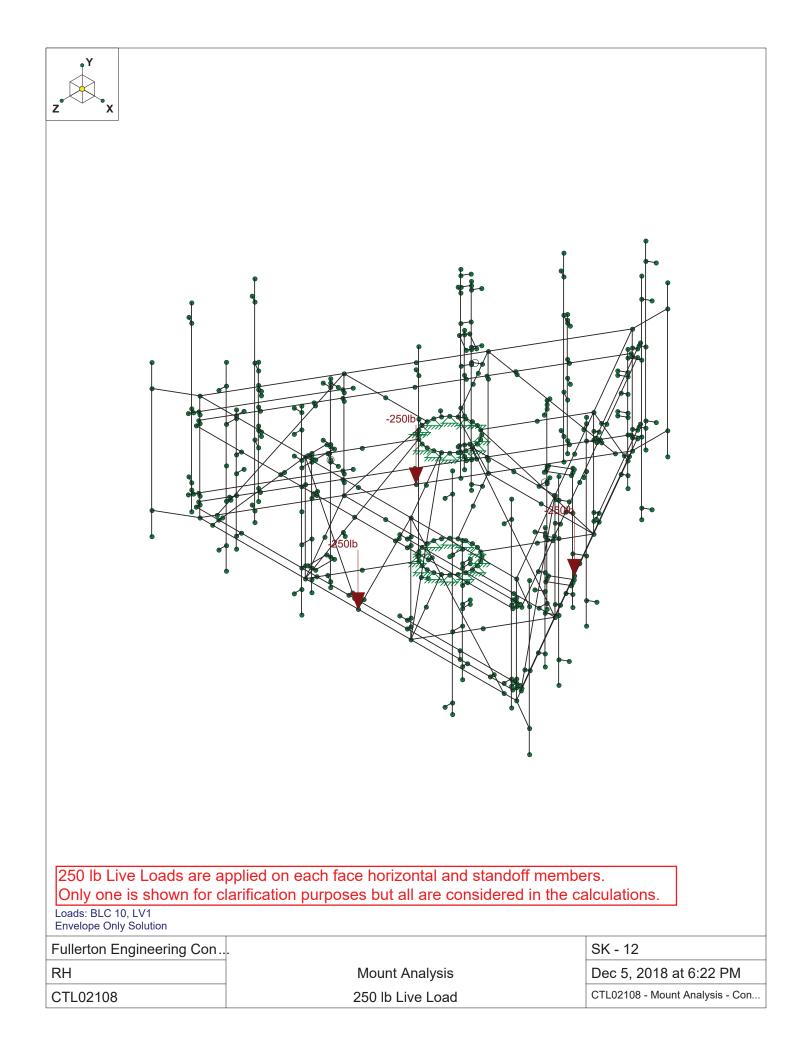


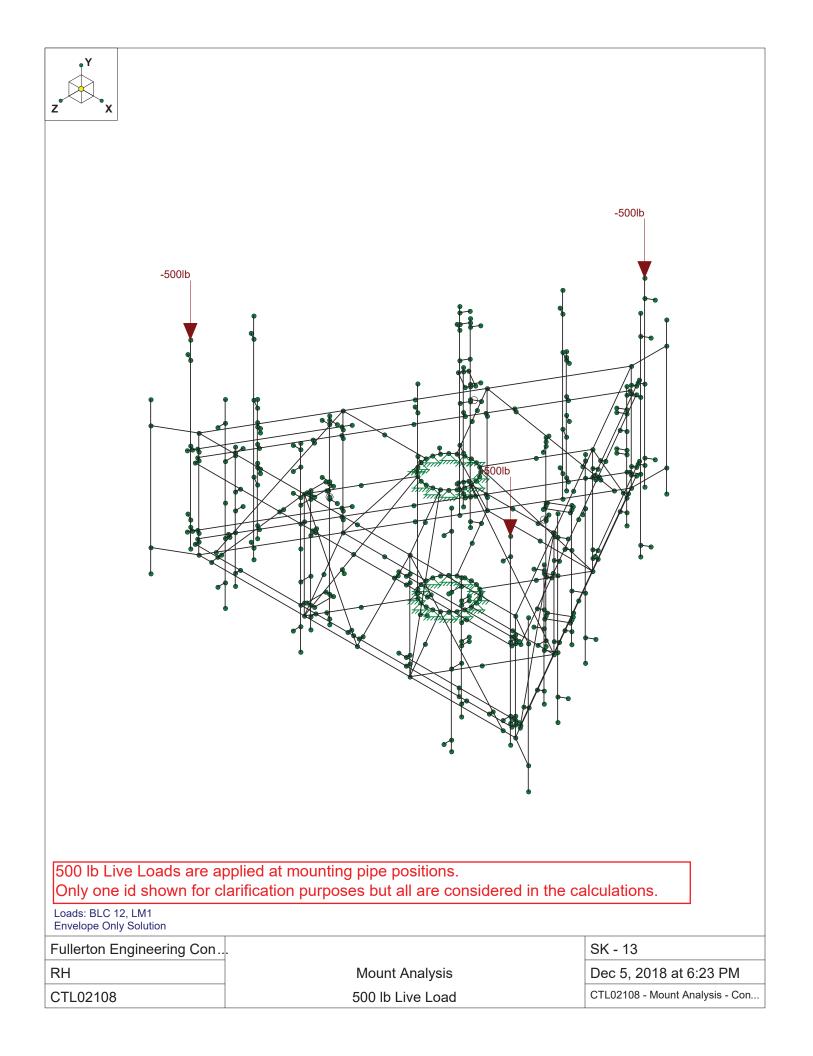














(Global) Model Settings

Min % Steel for Column

Max % Steel for Column

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in ²)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (in/sec^2)	386.4
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Υ
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver
Hot Rolled Steel Code	AISC 14th(360-10): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 14th(360-10): LRFD
Cold Formed Steel Code	AISI S100-12: LRFD
Wood Code	None
Wood Temperature	< 100F
Concrete Code	None
Masonry Code	None
Aluminum Code	None - Building
Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	Yes
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
	4

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8

(Global) Model Settings, Continued

Seismic Code	ASCE 7-10
Seismic Base Elevation (in)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	l or ll
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	4
Cd X	4
Rho Z	1
Rho X	1

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut.	Area(M.	Surface
1	DL	None		-1		63			9	
2	DLi	None				63		89	9	
3	WL(0)	None				56		81		
4	WL(90)	None				50		66		
5	WL.i(0)	None				56		81		
6	WL.i(90)	None				50		67		
7	T	None								
8	WM(0)	None				45		51		
9	WM(90)	None				43		45		
10	LV1	None				3				
11	LV2	None				3				
12	LM1	None				3				
13	LM2	None				3				
14	LM3	None				3				
15	LM4	None				3				
16	LM5	None				3				
17	LM6	None				3				
18	LM7	None				3				
19	LM8	None				1				
20	LV3	None				3				
21	LV4	None				3				
22	LV5	None				3				
23	LV6	None				6				
24	LV7	None				3				
25	LV8	None								
26	BLC 1 Transient Area Loads	None						153		
27	BLC 2 Transient Area Loads	None						153		



: Fullerton Engineering Consultants, Inc. : RH : CTL02108 : Mount Analysis

Load Combinations

	Description	<u>SP.</u>	<u>S</u>	<u>B</u>	<u>Fa.</u> .	<u>.B</u>	<u>Fac.</u>	<u>.B</u>	Fac.	<u>.B.</u>	Fac.	<u>.B.</u>	<u>Fa</u>	<u>B.</u>	<u>Fa</u>	<u>B</u>	<u>Fa.</u> .	<u>.B</u>	<u>Fa.</u>	<u>B</u>	<u>Fa</u>	<u>B.</u>	F
1	1.2*DL + 1.6 * WL(0)	Yes Y		1	1.2	3	1.6																
2	1.2*DL + 1.6* WL(30)	Yes Y		1	1.2	3	1.39	4	.8														
3	1.2*DL + 1.6* WL(60)	Yes Y		1	1.2	3	.8	4	1.39														
4	1.2*DL + 1.6*WL(90)	Yes Y					1.6																
5	1.2*DL + 1.6*WL(120)	Yes Y					8		1.39														
6	1.2*DL +1.6*WL(150)	Yes Y					-1.39																
7	1.2*DL + 1.6 * WL(180)	Yes Y		1	1.2	3	-1.6																
8	1.2*DL + 1.6* WL(210)	Yes Y					-1.39		8														
9	1.2*DL + 1.6*WL(240)	Yes Y					8																
10	$1.2^{\circ}DL + 1.6^{\circ}WL(270)$	Yes Y					-1.6																
11	1.2*DL + 1.6*WL(300)	Yes Y			1.2				-1.39														-
12	1.2*DL +1.6*WL(330)	Yes Y		1	1.2	3	1.39																-
	1.2*DL+1.0*DLi+1.0*WL.i(0)+1.0*T				1.2		1	5		7	1												-
	1.2*DL+1.0*DLi+1.0*WL.i(30)+1.0.				1.2		1		.866			7											-
	1.2*DL+1.0*DLi+1.0*WL.i(60)+1.0.				1.2		1	5		6	.866												-
	1.2*DL+1.0*DLi+1.0*WL.i(90)+1.0.				1.2		1	6		7	1	1											
	1.2*DL+1.0*DLi+1.0*WL.i(120)+1				1.2		1	5	5		.866	7											-
	1.2*DL+1.0*DLi+1.0*WL.i(150)+1			1	1.2	2	1		866			7											
	1.2*DL+1.0*DLi+1.0*WL.i(180)+1				1.2		1	5		7		1											F
	1.2*DL+1.0*DLi+1.0*WL.i(210)+1			1	1.2	2	1		866			7											
	1.2*DL+1.0*DLi+1.0*WL.i(240)+1				1.2		1		5		866												-
	1.2*DL+1.0*DLi+1.0*WL.i(270)+1			1	1.2	2	1		5	7		1											
	1.2*DL+1.0*DLi+1.0*WL.i(300)+1				1.2		1	5			866	7											-
	1.2*DL+1.0*DLi+1.0*WL.i(330)+1				1.2		1		.866														-
25	0.9*DL+1.6*WL(0)	Yes Y		1			1.6	5	.000	0	5	1											-
26	0.9*DL+1.6*WL(30)	Yes Y		1			1.39	Λ	.8														-
27	0.9*DL+1.6*WL(60)	Yes Y		1	.9		.8		1.39														-
28	0.9*DL+1.6*WL(90)	Yes Y		1	.9		1.6	4	1.59														⊢
		Yes Y						4	1 20														-
29	0.9*DL+1.6*WL(120)	Yes Y		1	.9 .9	3	- <u>.8</u> -1.39																-
30	0.9*DL+1.6*WL(150)	Yes Y							.0														-
31	0.9*DL+1.6*WL(180)	Yes Y		1	.9	3	-1.6 -1.39	4	0														-
32	0.9*DL+1.6*WL(210)	Yes Y		1																			
33	0.9*DL+1.6*WL(240)			1	.9		8		-1.39														
34	0.9*DL+1.6*WL(270)	Yes Y		1	.9		-1.6		4.20														
35	0.9*DL+1.6*WL(300)	Yes Y	_	1		3			-1.39														_
36	0.9*DL+1.6*WL(330)	Yes Y		1			1.39	4	8														-
37	1.2*DL+1.5*LV1	Yes Y					1.5																
38	1.2*DL+1.5*LV2	Yes Y					1.5																
	1.2*DL+1.5*LM1+1.0*WM(0)	Yes Y		1	1.2	12	1.5	8	1	•	_												
40	1.2*DL+1.5*LM1+1.0*WM(30)	Yes Y	_						.866														
41	1.2*DL+1.5*LM1+1.0*WM(60)	Yes Y					1.5			9	.866												
42	1.2*DL+1.5*LM1+1.0*WM(90)	Yes Y	_				1.5			6	0.000												
43	1.2*DL+1.5*LM1+1.0*WM(120)	Yes Y					1.5				.866												-
44	1.2*DL+1.5*LM1+1.0*WM(150)	Yes Y							866	9	.5												
45	1.2*DL+1.5*LM1+1.0*WM(180)	Yes Y	_				1.5			-					_								
46	1.2*DL+1.5*LM1+1.0*WM(210)	Yes Y					1.5		866														
47	1.2*DL+1.5*LM1+1.0*WM(240)	Yes Y					1.5			9	866												
48	1.2*DL+1.5*LM1+1.0*WM(270)	Yes Y	_				1.5																
49	1.2*DL+1.5*LM1+1.0*WM(300)	Yes Y					1.5				866												
50	1.2*DL+1.5*LM1+1.0*WM(330)	Yes Y	_						.866	9	5												
51	1.2*DL+1.5*LM2+1.0*WM(0)						1.5																
52	1.2*DL+1.5*LM2+1.0*WM(30)	Yes Y							.866		.5												
53	1.2*DL+1.5*LM2+1.0*WM(60)	Yes Y		1	1.2	13	1.5	8	.5	9	.866												
54	1.2*DL+1.5*LM2+1.0*WM(90)	Yes Y					1.5																
55	1.2*DL+1.5*LM2+1.0*WM(120)	Yes Y		1			1.5			9	.866												
56	1.2*DL+1.5*LM2+1.0*WM(150)	Yes Y		1			1.5		866	9	.5												

Load Combinations (Continued)

Ξ

Description S. P. S. B. Fab. Fab. Fab. Fab. Fab. Fab. Fab. Fab	2000																					
										B	Fac	. <u>B</u> ,Fa	<u>а,В</u>	<u>. Fa</u>	<u>B</u>	Fa	.В	<u>Fa</u>	В	Fa	B	Fa
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $																						
60 12*0L*1*5*UM*1*0*WM200 Yes Y 1 12<13:15	58	1.2*DL+1.5*LM2+1.0*WM(210)	Yes Y	1	1.1	2 13	1.5	8	866	9	5											
	59	1.2*DL+1.5*LM2+1.0*WM(240)	Yes Y	1	1.1	2 13	1.5	8	5	9	866											
61 12*0:1*5:UM2+10*WM(30) Yest Y 1 1.2 12.15 8 6.9 6 63 1.2*0:L+1.5*UM2+10*WM(30) Yest Y 1 1.2 1.16 8 8 9 5 64 1.2*0:L+1.5*UM3+10*WM(0) Yest Y 1 1.2 1.16 8 8 9 .5 66 1.2*0:L+1.5*UM3+10*WM(0) Yest Y 1 1.2 1.4 1.5 8 1.6 1.2 1.15 8 .6 9 .5 67 1.2*0:L+1.5*UM3+10*WM(10) Yest Y 1 1.2 1.15 8 .6 9 .5 68 1.2*0:L+1.5*UM3+10*WM(10) Yest Y 1 1.2 1.15 8 .6 9 .5 71 1.2*0:L+1.5*UM3+10*WM(20) Yest Y 1 1.2 1.4 1.5 8 .6 9 .5 73 1.2*0:L+1.5*UM3+10*WM(20) Yest Y 1 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.	60	1.2*DL+1.5*LM2+1.0*WM(270)	Yes Y																			
										a	- 866											
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $																						
64 1:2'DL+1:5'LM31-0'WM(60) Yei Y 1 1:2 14:1:5 8.5 9 866 65 1:2'DL+1:5'LM31-0'WM(60) Yei Y 1 1:2 14:1:5 8.5 9 866 66 1:2'DL+1:5'LM31-0'WM(120) Yei Y 1 1:2 14:1:5 8.5 9 866 9 69 1:2'DL+1:5'LM3+10'WM(120) Yei Y 1 1:2 14:1:5 8.66 9 5 71 1:2'DL+1:5'LM3+10'WM(20) Yei Y 1 1:2 14:1:5 8.66 9 .5 71 1:2'DL+1:5'LM3+10'WM(20) Yei Y 1 1:2 14:1:5 8.66 9 .5 71 1:2'DL+1:5'LM3+10'WM(20) Yei Y 1<1:2 14:1:5										9	5	_	-	-				-			-	_
65 1.2'DL+1'5'LM31-0'WM(0) Yes' Y 1 1.2'L4 1.5 9 1.6' 61 1.2'DL+1'5'LM31-0'WM(130) Yes' Y 1 1.2'L4 1.5 8 5.5 9 866 63 1.2'DL+1'5'LM31-0'WM(130) Yes' Y 1 1.2'L4 1.5 8 866 9 5 70 1.2'DL+1'5'LM31-0'WM(210) Yes' Y 1 1.2'L4 1.5 8 866 9 5 71 1.2'DL+1'5'LM31-0'WM(20) Yes' Y 1 1.2'L4 1.5 8 5.9 9 866 9 5 1 1 1.2'L4 1.5 8 5.9 9 866 9 .5 1 1 1.2'L4 1.5 8 5 9 866 1 1 1.2'L4 1.5 8 5 9 866 1 1 1.2'L4 1.5 8 5 9 866 1 1 1.2'L5 1.5 1.5 1.5 1.5 1.5 1 1 1.5'L4 1.5 1.5'L4 1.5 1										0	-							-			_	
66 12*0L+15*UA81-0*WM(20) Yes Y 1 12*14 15 8 5 9 866 9 5 68 12*0L+15*UA81-0*WM(130) Yes Y 1 12*14 15 8 8 96 5 9 9 12*0L+15*UA81-0*WM(120) Yes Y 1 12*14 15 8 866 9 5 9 866 9 5 9 866 9 5 9 866 9 5 9 866 9 5 9 866 9 5 9 866 9 5 9 866 9 5 9 866 9 5 9 866 9 5 9 10 14 15 8 16 9 5 9 12 15 14 15 14 15 14 15 14 15 14 15 14 15 15 15 15 15 15 15 15 16 15 15 15 15 15 15 15 15 15													_	-								
67 12*DL+1:5*LM3+10*WM(120) Yes Y 1 1.2*L14 1.5 8.666										9	.866		_					<u> </u>				
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66 1.2*DL+1:5*LM3+1:0*WM(120) Yes Y 1 1.2:L141:5 8 .8:66 9 .5 71 1.2*DL+1:5*LM3+1:0*WM(20) Yes Y 1 1.2:L141:5 8 .5:S 9 .866 72 1.2*DL+1:5*LM3+1:0*WM(20) Yes Y 1 1.2:L141:5 8 .5:S 9 .666 74 1.2*DL+1:5*LM3+1:0*WM(30) Yes Y 1 1.2:L141:5 1.8 .6:S 9 .5:S	67																					
66 1.2*DL+1:5*LM3+1:0*WM(120) Yes Y 1 1.2:L141:5 8 .8:66 9 .5 71 1.2*DL+1:5*LM3+1:0*WM(20) Yes Y 1 1.2:L141:5 8 .5:S 9 .866 72 1.2*DL+1:5*LM3+1:0*WM(20) Yes Y 1 1.2:L141:5 8 .5:S 9 .666 74 1.2*DL+1:5*LM3+1:0*WM(30) Yes Y 1 1.2:L141:5 1.8 .6:S 9 .5:S	68	1.2*DL+1.5*LM3+1.0*WM(150)	Yes Y	1	1.	2 14	1.5	8	866	9	.5											
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	69	1.2*DL+1.5*LM3+1.0*WM(180)	Yes Y																			
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87 1.2*DL+1.5*LM5+1.0*WM(0) Yes Y 1 1.2.16 1.5 8 1					1.	2 15	1.5						_	-								
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$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	88																					
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	89	1.2*DL+1.5*LM5+1.0*WM(60)	Yes Y	1	1.	2 16	1.5	8	.5	9	.866											
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	90	1.2*DL+1.5*LM5+1.0*WM(90)	Yes Y	1	1.	2 16	1.5	9	1													
92 $1.2*DL+1.5*LM5+1.0*WM(150)$ YesY1 1.2 16 1.5 8 $.866$ 9 $.5$ 93 $1.2*DL+1.5*LM5+1.0*WM(210)$ YesY1 1.2 16 1.5 8 -1 094 $1.2*DL+1.5*LM5+1.0*WM(210)$ YesY1 1.2 16 1.5 8 -866 9 5 95 $1.2*DL+1.5*LM5+1.0*WM(210)$ YesY1 1.2 16 1.5 8 5 996 $1.2*DL+1.5*LM5+1.0*WM(20)$ YesY1 1.2 16 1.5 8 5 997 $1.2*DL+1.5*LM5+1.0*WM(30)$ YesY1 1.2 16 1.5 8 5 998 $1.2*DL+1.5*LM6+1.0*WM(30)$ YesY1 1.2 16 1.5 8 $.5$ 998 $1.2*DL+1.5*LM6+1.0*WM(30)$ YesY1 1.2 17 1.5 8 $.566$ 9 $.5$ 100 $1.2*DL+1.5*LM6+1.0*WM(30)$ YesY 1 1.2 17 1.5 8 $.5$ 9 $.666$ 101 $1.2*DL+1.5*LM6+1.0*WM(120)$ YesY 1 1.2 17 1.5 8 5 9 $.5$ 104 $1.2*DL+1.5*LM6+1.0*WM(180)$ YesY 1 1.2 17 1.5 8 5 9 $.5$ 105 $1.2*DL+1.5*LM6+1.0*WM(180)$ YesY 1 1.2 17 1.5 8	91	1.2*DL+1.5*LM5+1.0*WM(120)	Yes Y							9	.866											
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94 $1.2*DL+1.5*LM5+1.0*WM(210)$ YesY1 1.2 16 1.5 8 866 9 5 95 $1.2*DL+1.5*LM5+1.0*WM(240)$ YesY1 1.2 16 1.5 8 5 9 866 96 $1.2*DL+1.5*LM5+1.0*WM(300)$ YesY1 1.2 16 1.5 8 $.5$ 9 866 97 $1.2*DL+1.5*LM5+1.0*WM(300)$ YesY1 1.2 16 1.5 8 $.5$ 9 866 98 $1.2*DL+1.5*LM5+1.0*WM(30)$ YesY1 1.2 16 1.5 8 $.5$ 9 866 99 $1.2*DL+1.5*LM6+1.0*WM(30)$ YesY1 1.2 17 1.5 8 $.56$ 9 $.5$ 100 $1.2*DL+1.5*LM6+1.0*WM(30)$ YesY1 1.2 17 1.5 8 $.5$ 9 $.866$ 101 $1.2*DL+1.5*LM6+1.0*WM(120)$ YesY1 1.2 17 1.5 8 5 9 $.666$ 102 $1.2*DL+1.5*LM6+1.0*WM(120)$ YesY1 1.2 17 1.5 8 5 9 $.666$ 104 $1.2*DL+1.5*LM6+1.0*WM(20)$ YesY1 1.2 17 1.5 8 5 9 $.666$ 105 $1.2*DL+1.5*LM6+1.0*WM(20)$ YesY1 1.2 17 1.5 8 5 9 $.666$ 106 $1.2*DL+1.5*LM6+1.0*WM(30)$ YesY										<u> </u>	.0							-				
951.2*DL+1.5*LM5+1.0*WM(240)YesY11.2161.5859866961.2*DL+1.5*LM5+1.0*WM(270)YesY11.2161.58.591971.2*DL+1.5*LM5+1.0*WM(300)YesY11.2161.58.59866981.2*DL+1.5*LM5+1.0*WM(300)YesY11.2161.58991.2*DL+1.5*LM6+1.0*WM(30)YesY11.2171.581001.2*DL+1.5*LM6+1.0*WM(00)YesY11.2171.581.21.21.71.581.21.71.581.21.71.581.21.71.581.21.71.58.					1.4	2 16	1.5			0	5											
96 1.2*DL+1.5*LM5+1.0*WM(270) Yes Y 1 1.2 16 1.5 9 -1 97 1.2*DL+1.5*LM5+1.0*WM(300) Yes Y 1 1.2 16 1.5 8 .5 9 -866 98 1.2*DL+1.5*LM6+1.0*WM(300) Yes Y 1 1.2 16 1.5 8 .5 9 -866 99 1.2*DL+1.5*LM6+1.0*WM(30) Yes Y 1 1.2 17 1.5 8 .5 9 .866 100 1.2*DL+1.5*LM6+1.0*WM(90) Yes Y 1 1.2 17 1.5 8 .5 9 .866 101 1.2*DL+1.5*LM6+1.0*WM(120) Yes Y 1 1.2 17 1.5 8 .5 9 .666 102 1.2*DL+1.5*LM6+1.0*WM(180) Yes Y 1 1.2 17 1.5 8 .5 9 .666																					_	
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98 1.2*DL+1.5*LM5+1.0*WM(330) Yes Y 1 1.2 16 1.5 8 .5 9 866 99 1.2*DL+1.5*LM6+1.0*WM(30) Yes Y 1 1.2 17 1.5 8 .866 9 .5										_	000											
99 1.2*DL+1.5*LM6+1.0*WM(30) Yes Y 1 1.2 17 1.5 8 .866 9 .5										<u> </u>								-				
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101 1.2*DL+1.5*LM6+1.0*WM(90) Yes Y 1 1.2 17 1.5 9 1 1.2 17 1.5 9 1 1.2 17 1.5 9 1 1.2 17 1.5 9 1 1.2 17 1.5 9 1 1.2 17 1.5 9 1 1.2 17 1.5 9 1 1.2 17 1.5 9 1 1.2 17 1.5 9 1 1.2 17 1.5 9 1.2 17 1.5 9 1.2 17 1.5 8 5 9 .866 9 .5 1 1 1.2 17 1.5 8 5 9 .866 9 .5 1 1 1.2 17 1.5 8 5 9 866 1 1 1 1.2 17 1.5 8 5 9 866 1 1 1 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 <t< td=""><td>99</td><td></td><td></td><td> 1</td><td></td><td></td><td></td><td></td><td></td><td>9</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	99			1						9												
101 1.2*DL+1.5*LM6+1.0*WM(90) Yes Y 1 1.2 17 1.5 9 1	100	· · · · · · · · · · · · · · · · · · ·		1	1.	2 17	1.5	8	.5	9	.866											
102 1.2*DL+1.5*LM6+1.0*WM(120) Yes Y 1 1.2 17 1.5 8 5 9 .866 103 1.2*DL+1.5*LM6+1.0*WM(150) Yes Y 1 1.2 17 1.5 8 5 9 .866	101	1.2*DL+1.5*LM6+1.0*WM(90)	Yes Y	1	1.	2 17	1.5	9														
103 1.2*DL+1.5*LM6+1.0*WM(150) Yes Y 1 1.2 17 1.5 8 -866 9 .5 <					1.	2 17	1.5			9	.866											
104 1.2*DL+1.5*LM6+1.0*WM(180) Yes Y 1 1.2 17 1.5 8 -1 </td <td></td>																						
105 1.2*DL+1.5*LM6+1.0*WM(210) Yes Y 1 1.2 17 1.5 8 866 9 5										0												
106 1.2*DL+1.5*LM6+1.0*WM(240) Yes Y 1 1.2 17 1.5 8 5 9 866 107 1.2*DL+1.5*LM6+1.0*WM(270) Yes Y 1 1.2 17 1.5 8 5 9 866 108 1.2*DL+1.5*LM6+1.0*WM(300) Yes Y 1 1.2 17 1.5 8 .5 9 866 109 1.2*DL+1.5*LM6+1.0*WM(300) Yes Y 1 1.2 17 1.5 8 .5 9 866 109 1.2*DL+1.5*LM6+1.0*WM(300) Yes Y 1 1.2 17 1.5 8 .5 9 866 110 1.2*DL+1.5*LM7+1.0*WM(30) Yes Y 1 1.2 18 1.5 8 .56 9 .5 111 1.2*DL+1.5*LM7+1.0*WM(60) Yes Y 1 1.2 18 1.5 9 .866 1 1 112 1.2*DL+1.5*LM7+1.0*WM(120) Yes Y 1 1.2 18 1.5 9 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0</td><td>- 5</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>										0	- 5											
107 1.2*DL+1.5*LM6+1.0*WM(270) Yes Y 1 1.2 17 1.5 9 -1 </td <td></td> <td>· · · · · · · · · · · · · · · · · · ·</td> <td></td>		· · · · · · · · · · · · · · · · · · ·																				
108 1.2*DL+1.5*LM6+1.0*WM(300) Yes Y 1 1.2 17 1.5 8 .5 9 866					1.4		1.D			9	000											
109 1.2*DL+1.5*LM6+1.0*WM(330) Yes Y 1 1.2 17 1.5 8 .5 9 .866 <										~	0.00											
110 1.2*DL+1.5*LM7+1.0*WM(30) Yes Y 1 1.2 18 1.5 8 .866 9 .5 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>																						
111 1.2*DL+1.5*LM7+1.0*WM(60) Yes Y 1 1.2 18 1.5 8 .5 9 .866 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td><td></td></t<>										<u> </u>								<u> </u>				
112 1.2*DL+1.5*LM7+1.0*WM(90) Yes Y 1 1.2 18 1.5 9 1 Image: Second	110			1						9												
112 1.2*DL+1.5*LM7+1.0*WM(90) Yes Y 1 1.2 18 1.5 9 1 Image: Second	111			1	1.	2 18	1.5	8	.5	9	.866											
113 1.2*DL+1.5*LM7+1.0*WM(120) Yes Y 1 1.2 18 1.5 8 5 9 .866			Yes Y	1																		
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Load Combinations (Continued)

	Description	S P	S	В	Fa	В	Fac	.B	Fac	.B	Fac	.B	Fa	В	Fa	.в	Fa	.B	Fa	.B	Fa	.в	Fa
114	1.2*DL+1.5*LM7+1.0*WM(150)	Yes Y		1	1.2	18	1.5	8	866	9	.5												
115	1.2*DL+1.5*LM7+1.0*WM(180)	Yes Y		1	1.2	18	1.5	8	-1														
116	1.2*DL+1.5*LM7+1.0*WM(210)	Yes Y		1	1.2	18	1.5	8	866	9	5												
117	1.2*DL+1.5*LM7+1.0*WM(240)	Yes Y		1	1.2	18	1.5	8	5	9	866												
118	1.2*DL+1.5*LM7+1.0*WM(270)	Yes Y		1	1.2	18	1.5	9	-1														
119	1.2*DL+1.5*LM7+1.0*WM(300)	Yes Y		1	1.2	18			.5	9	866												
120	1.2*DL+1.5*LM7+1.0*WM(330)	Yes Y		1	1.2	18	1.5	8	.5	9	866												
121	1.2*DL+1.5*LM8+1.0*WM(30)	Yes Y		1	1.2	19	1.5	8	.866	9	.5												
122	1.2*DL+1.5*LM8+1.0*WM(60)	Yes Y		1	1.2	19	1.5	8	.5	9	.866												
123	1.2*DL+1.5*LM8+1.0*WM(90)	Yes Y		1	1.2	19	1.5	9	1														
124	1.2*DL+1.5*LM8+1.0*WM(120)	Yes Y		1	1.2	19	1.5	8	5	9	.866												
125	1.2*DL+1.5*LM8+1.0*WM(150)	Yes Y		1	1.2	19	1.5	8	866	9	.5												
126	1.2*DL+1.5*LM8+1.0*WM(180)	Yes Y		1	1.2	19	1.5	8	-1														
127	1.2*DL+1.5*LM8+1.0*WM(210)	Yes Y		1	1.2	19	1.5	8	866	9	5												
128	1.2*DL+1.5*LM8+1.0*WM(240)	Yes Y		1	1.2	19	1.5	8	5	9	866												
129	1.2*DL+1.5*LM8+1.0*WM(270)	Yes Y		1	1.2	19	1.5	9	-1														
130	1.2*DL+1.5*LM8+1.0*WM(300)	Yes Y		1	1.2	19	1.5	8	.5	9	866												
131	1.2*DL+1.5*LM8+1.0*WM(330)	Yes Y		1	1.2	19	1.5	8	.5	9	866												
132	1.2*DL+1.5*LV3	Yes Y		1	1.2	20	1.5																
133	1.2*DL+1.5*LV4	Yes Y		1	1.2	21	1.5																
134	1.2*DL+1.5*LV5	Yes Y		1	1.2	22	1.5																
135	1.2*DL+1.5*LV6	Yes Y		1	1.2	23	1.5																
136	1.2*DL+1.5*LV7	Yes Y		1	1.2	24	1.5																
137	1.2*DL+1.5*LV8	Yes Y		1	1.2	25	1.5																

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N240	max	912.644	6	1012.194	5	539.537	36	0	1	0	1	0	1
2		min	-579.272	36	-454.728	35	-811.514	6	0	1	0	1	0	1
3	N241	max	218.246	25	1147.02	8	637.028	26	0	1	0	1	0	1
4		min	-257.314	7	-762.785	26	-1000.665	8	0	1	0	1	0	1
5	N242	max	304.947	29	1064.673	13	104.863	29	0	1	0	1	0	1
6		min	-903.556	23	-234.316	30	-311.477	23	0	1	0	1	0	1
7	N243	max	153.189	28	636.275	10	429.102	10	.096	135	.035	30	.136	135
8		min	-517.638	22	-394.869	28	-260.161	28	003	34	065	12	018	28
9	N244	max	215.926	3	1141.179	16	977.404	2	0	1	0	1	0	1
10		min	-115.936	33	-61.653	34	-457.023	32	0	1	0	1	0	1
11	N245	max	733.377	2	891.963	13	193.921	2	0	1	0	1	0	1
12		min	-389.58	32	-392.797	31	-103.358	32	0	1	0	1	0	1
13	N246	max	542.271	26	1054.882	9	494.025	27	0	1	0	1	0	1
14		min	-836.226	8	-670.936	27	-712.64	9	0	1	0	1	0	1
15	N247	max	704.015	30	1073.098	13	324.873	11	0	1	0	1	0	1
16		min	-1191.005	12	-416.425	31	-147.894	29	0	1	0	1	0	1
17	N248	max	48.436	78	521.5	135	585.302	11	0	1	0	1	0	1
18		min	-74.632	60	-237.626	28	-316.031	29	0	1	0	1	0	1
19	N249	max	749.671	15	1176.969	16	755.737	15	0	1	0	1	0	1
20		min	-336.894	33	-121.297	33	-331.742	33	0	1	0	1	0	1
21	N250	max	624.301	15	789.688	13	92.573	33	0	1	0	1	0	1
22		min	-239.158	32	-370.646	31	-278.968	15	0	1	0	1	0	1
23	N251	max	332.432	6	1207.885	5	773.613	36	.071	36	.122	6	.066	18
24		min	-238.997	36	-588.454	35	-1251.242	6	142	6	077	36	017	135
25	N258	max	41.997	28	186.016	38	355.46	22	0	1	0	1	0	1
26		min	-403.253	23	-161.007	132	-91.312	28	0	1	0	1	0	1
27	N259	max	100.066	7	279.254	132	419.186	16	0	1	0	1	0	1
28		min	-85.303	25	-107.688	38	-102.822	34	0	1	0	1	0	1

LC LC Joint X [lb] LC Y [lb] LC MX [k-ft] LC MY [k-ft] LC MZ [k-ft] Z [lb] N260 max 1147.949 190.199 230.714 Ō min -818.122 -160.119-124.92 N261 280.733 max 629.868 464.508 -503.823 -109.065 -531.639 min N262 <u>33</u> max 265.853 191.517 547.112 -159.998-912.199 min | -341.005 N263 <u>35</u> 281.661 234.172 max 885.182 min -1037.238 12 -107.193 -309.7 N264 max 327.073 15 271.66 311.596 -108.883 min -145.227 34 <u>-192.443</u> N265 1087.916 193.767 205.164 max min -753.12 -159.2 -319.859 N266 322.966 272.56 max 773.051 -323.41 -112.245 -921.014 min N267 482.75 195.295 396.262 max -766.236 -159.636-657.479 min N268 918.627 272.709 232.792 max -1078.07 -112.063 -144.379 min N269 72.268 191.984 578.849 max 12.632 -138.087 -160.647min <u>49</u> Totals: max 5154.786 9683.888 5854.973 min -5154.788 10 -5854.981 2559.137

Envelope Joint Reactions (Continued)

Envelope AISI S100-12: LRFD Cold Formed Steel Code Checks

	Member	Shape	Code Che	Loc[in]	LC	Shear Check	Loc[in]		LC	phi*Pn[phi*T	phi*M	.phi*M	. Cb	Cm	Cm	. Eqn
1	M116	P1000	.864	46.5	47	.860	45	y	47	6344.4	 1327	.442	.515	3.5	.6	.85	C3.3
2	M110	P1000	.863	46.5	42	.859	45	y	42	6344.4	1327	.442	.515	3.3	.6		C3.3
3	M104	P1000	.859	46.5	50	.856	45	ý	50	6344.4	1327	.442	.515	3.4	.6	.85	C3.3
4	M105	P1000	.771	46.5	45	.765	45	y	45	6344.4	1327	.442	.515	3.0	.6	.85	C3.3
5	M111	P1000	.765	46.5	48	.757	45	y	48	6344.4	1327	.442	.515	4.1	.6	.85	C3.3
6	M117	P1000	.764	46.5	41	.756	45	y	41	6344.4	1327	.442	.515	4.1	.6	.85	C3.3
7	M84	P1000	.684	126	56	.400	42	z	84	6382.9	1327	.262	.497	2.2	.85	.76	C5.1
8	M98	P1000	.681	126	55	.455	126	y	2	6382.9	1327	.262	.497	2.22	.85	.797	C5.1
9	M99	P1000	.640	108.9	60	.500	116	z	61	6542.57	1327	.442	.515	2.1	.85	.687	C3.3
10	M85	P1000	.640	108.9	55	.499	116			6542.57	1327	.442	.515	2.2	.85	.716	C3.3
11	M70	P1000	.619	•	108		47.25	z	84	6382.9	1327	.262	.497	2.1	.85	.843	C5.1
12	M71	P1000	.604	17.063	99	.472	9.188	z	102	6542.57	1327	.442	.515	1.0	.85	.625	C3.3

Envelope AISC 14th(360-10): LRFD Steel Code Checks

	Manahan	Chana	Cada Chaak	lu a altina	10	Chase	Leefinl		10					Ch.	
	Member	Shape	Code Check	koe[in]	LC	Shear Che	.Locliul			<u>phi*Pnc [</u>		P			Eqn
1	M41	HSS1x1x1/8	.525	0	30	.101	0	V	12	4110.119	18133.2	.5	.5		H1-1a
2	M37	HSS1x1x1/8	.490	0	25	.096	0	y	7	4110.118	18133.2	.5	.5	4.33	H1-1a
3	M44	HSS1x1x1/8	.485	55.973	31	.092	55.973	ý	1	4110.118	18133.2	.5	.5	3.926	H1-1a
4	M40	HSS1x1x1/8	.467	55.973	36	.093	55.973	y	6	4110.118	18133.2	.5	.5	4.345	H1-1a
5	M2	HSS1x1x1/8	.462	0	12	.278	3.938	ý	12	17900.38	18133.2	.5	.5	1.503	H1-1b
6	M1	HSS1x1x1/8	.459	0	7	.273	122	v	6	17900.381	18133.2	.5	.5	1.491	H1-1b
7	M3	HSS1x1x1/8	.437	126	1	.269	122	ý	1	17900.381	18133.2	.5	.5	2.205	H1-1b
8	M42	HSS1x1x1/8	.398	55.973	28	.068	50.143	y	54	4110.118	18133.2	.5	.5	4.185	H1-1a
9	M29	HSS1x1x1/8	.389	0	8	.073	4.813	ý	56	7285.833	18133.2	.5	.5	2.921	H1-1a
10	M6	HSS1x1x1/8	.384	21	135	.051	42	y	135	7285.833	18133.2	.5	.5	1.758	H1-1b
11	M5	HSS1x1x1/8	.382	21	135	.051	42	ý	135	7285.833	18133.2	.5	.5	1.766	H1-1b
12	M4	HSS1x1x1/8	.382	21	135	.052	42	y	135	7285.833	18133.2	.5	.5	1.763	H1-1b
13	M28	HSS1x1x1/8	.364	0	6	.055	0	ý	6	7285.833	18133.2	.5	.5	3.772	H1-1a
14	M15	HSS1x1x1/8	.352	63	134	.050	84	y	134	14436.956	18133.2	.5	.5	2.244	H1-1b

Company	: Fullerton Engineering Consultants, Inc.
Designer	: RH
Job Number	: CTL02108
Model Name	: Mount Analysis

Stress ratio <1. Members are adequate.

Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)

	Member	Shape	Code Cheek		LC	Shear the	Loc[in]		LC	phi*Pnc [phi*Pnt			Cb	Eqn
15	M14	HSS1x1x1/8	.351	63	134	.050	84			14436.956		.5	.5	2.248	
16	M13	HSS1x1x1/8	.346	63	134	.050	84			14436.956		.5	.5	2.251	
17	M16	HSS1x1x1/8	.346	0	1	.096	0			10327.805		.5	.5	3.526	
18	M32	HSS1x1x1/8	.341	4.375	14	.101	0			7285.833		.5	.5	3.845	H1-1a
19	M20	HSS1x1x1/8	.335	0	8	.089	0			10327.805		.5	.5	3.598	H1-1b
20	M23	HSS1x1x1/8	.330	53.413	26	.011	53.413	z	11	4513.495	18133.2	.5	.5	1.723	H1-1a
21	M30	HSS1x1x1/8	.328	4.375	23	.100	0	v	37	7285.833	18133.2	.5	.5	4.033	H1-1a
22	M12	HSS1x1x1/8	.321	33	132	.061	33	V	132	10327.805	18133.2	.5	.5	1.857	H1-1b
23	M10	HSS1x1x1/8	.320	33	132	.061	33	v	132	10327.805	18133.2	.5	.5	1.856	H1-1b
24	M8	HSS1x1x1/8	.319	33	132	.061	33	v	132	10327.805	18133.2	.5	.5	1.862	H1-1b
25	M21	HSS1x1x1/8	.311	33	135	.061	33			10327.805		.5	.5	1.853	H1-1b
26	M19	HSS1x1x1/8	.310	33	135	.061	33			10327.805		.5	.5	1.853	H1-1b
27	M11	HSS1x1x1/8	.309	6.187	92	.138	0			10327.805		.5		3.135	
28	M22	HSS1x1x1/8	.307	53.413	35		53.413			4513.495		.5	.5	+ +	H1-1a
29	M9	HSS1x1x1/8	.304	6.188	88	.137	0	-		10327.805		.5	.5	3.154	
30	M17	HSS1x1x1/8	.304	33	135	.058	33			10327.805		.5	.5	1.872	
31	M286	PIPE 2.0	.300	24.75	1	.031	24.75			20866.733		1.872	1.872		
32	M240	PIPE 2.0	.297	24.75	7	.034	24.75	-		20866.733	22120	1.872			
33	M43	HSS1x1x1/8	.285	5.831	107	.074	0	v		4110.118		.5	.5	3.422	
							0		· ·	10327.805				3.197	
34	M7	HSS1x1x1/8		6.187	93	.127		-	<u>92</u> 7	7285.833		.5	.5	4.625	
35	M31	HSS1x1x1/8	.279	0	135	.143	0 4.813	y	1	7285.833		.5	.5	4.613	
36	M33	HSS1x1x1/8	.279	0	135	.122		-				.5		3.812	
37	M38	HSS1x1x1/8	.273	42.066	10	.033	0	y		5839.909		.5		+ +	
38	M18	HSS1x1x1/8	.259	0	5	.091	0	У		10327.805		.5	.5	3.717	
39	M202	SR1/2"	.237	7.5	95	.028	7.5			5263.413			.000	2.271	
40	M39	HSS1x1x1/8	.237	0	28	.029	5.381	Ζ	7	5839.909		.5	.5	1.608	
41	M260	SR1/2"	.234	7.5	97	.019	7.5			5263.413				2.255	
42	M203	SR1/2"	.233	0	8	.026	7.5			5263.413				2.216	
43	M308	SR1/2"	.232	7.5	89	.022	7.5		1	5263.413				2.255	
44	M280	PIPE_2.0	.231	18.5	2	.079	18.5			26521.424		1.872	1.872		
45	M261	SR1/2"	.229	7.5	97	.019	7.5		2	5263.413				2.254	
46	M309	SR1/2"	.229	7.5	90	.021	7.5		1	5263.413				2.255	
47	M234	PIPE 2.0	.221	18.5	11	.089	18.5		2	26521.424		1.872	1.872		
48	M252	SR1/2"	.207	0	88	.043	7.5		2	5263.413	6361.725	.053		2.252	
49	M211	SR1/2"	.205	7.5	95	.013	7.5			5263.413		.053	.053	2.265	H1-1b
50	M212	SR1/2"	.203	7.5	95	.013	7.5		93	5263.413	6361.725	.053		2.265	
51	M300	SR1/2"	.202	0	93	.047	7.5		6	5263.413	6361.725	.053	.053	2.253	H1-1b
52	M253	SR1/2"	.182	0	87	.040	7.5		2	5263.413	6361.725	.053	.053	2.247	H1-1b
53	M301	SR1/2"	.180	0	90	.044	7.5		6	5263.413	6361.725		.053	2.244	H1-1b
54	M219	PIPE 2.0	.179	28	1		55.125		10	17855.085	32130	1.872		2.594	H1-1b
55	M316	PIPE 2.0	.178	28	10		55.125			17855.085		1.872		1.832	H1-1b
56	M327	PIPE 2.0	.178	28	4	.037	28			17855.085					
57	M27	HSS1x1x1/8	.177	0	31			v		4513.495		.5	.5		H1-1b*
58	M317	PIPE 2.0	.159	32.5	12	.070	40	,		26521.424					
59	M220	PIPE 2.0	.155	32.5	4	.067	40			26521.424					
60	M327A	PIPE 2.0	.151	18.5	4	.066	18.5			26521.424		1.872			
61	M35	C3x6	.148	0	1			v		37162.504					
62	M128	PIPE 2.0	.143	36	7	.027	10.5			20866.733					
63	M235	PIPE 2.0	.142	36	10	.027	35.25			20866.733					
64	M233	PIPE 2.0	.142	36	4	.024	7.5			20866.733					
65	M24	HSS1x1x1/8	.142	53.413	30			7		4513.495		.5			H1-1b*
66	M34	C3x6	.140	0	1					37162.504		1 572	6.525		
		PIPE 2.0		-	4	1	45	У		26521.424					
67	M127		.127	32.5 53.413		.071		_		4513.495				1.715	
68	M25	HSS1x1x1/8	.124		28							.5			
69	M36	C3x6	.115	0	5	.064				37162.504					
70	M26	HSS1x1x1/8		53.413	22					4513.495		.5	_	2.145	
71	M206	PIPE_2.0	.110	44.25	6	082	44.25		7	20866.733	32130	1.8/2	1.872	1.015	r1 i - 1D
		ersion 15.0.4			100/04		alvaia		TLO	0100 M			2 41	Page	- 7

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Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)

	Member	Shape	Code Check	Loc[in]	LC	Shear Che	Loc[in]		LC	phi*Pnc [.phi*Pnt	phi*Mn	phi*Mn.	. Cb	Eqn
72	M303	PIPE 2.0	.099	44.25	2	.060	44.25		2	20866.733	32130	1.872	1.872	2.054	H1-1b
73	M139	PIPE 2.0	.097	51	5	.030	51		9	20866.733	32130	1.872	1.872		H1-1b
74	M126	PIPE 2.0	.095	32.5	5	.043	32.5		10	26521.424	32130	1.872	1.872	2.091	H1-1b
75	M233	PIPE 2.0	.095	32.5	2	.047	32.5		2	26521.424	32130	1.872	1.872	1.871	H1-1b
76	M279	PIPE 2.0	.093	32.5	1	.049	32.5		6	26521.424	32130	1.872	1.872	1.475	H1-1b
77	M255	PIPE_2.0	.092	44.25	11	.054	44.25		11	20866.733	32130	1.872			H1-1b
78	M134	PIPE 2.0	.081	24	1	.021	24		4	20866.733	32130	1.872	1.872	2.454	H1-1b
79	M282	PIPE 2.0	.080	24	10	.024	24		5	20866.733	32130	1.872	1.872	1.827	H1-1b
80	M236	PIPE 2.0	.080	24	4	.024	24		3	20866.733	32130	1.872	1.872	1.781	H1-1b
81	M46	C5x6.7	.077	0	12	.022	7	z	11	83481.735	88650	2.227	13.313	1.907	H1-1b
82	M49	C5x6.7	.071	0	4	.020	7	z	3	83481.738	88650	2.227	13.313	1.699	H1-1b
83	M52	C5x6.7	.070	0	8	.020	7	z	7	83481.738	88650	2.227	13.313	1.741	H1-1b
84	M48	C5x6.7	.058	0	6	.019	7	z	6	83481.738	88650	2.227	13.313	1.651	H1-1b
85	M45	C5x6.7	.056	0	5	.019	7	z	4	83481.735	88650	2.227	13.313	1.624	H1-1b
86	M51	C5x6.7	.050	0	2	.016	7	z	1	83481.738	88650	2.227	13.313	1.649	H1-1b
87	M221	PIPE 2.5	.032	31.5	5	.006	24.75		12	37773.818	50715	3.596	3.596	2.476	H1-1b
88	M53	L5x5x5	.015	50.625	20	.006	9.375	y	1	76065.401	99468	6.383	12.944	1.255	H2-1
89	M47	L5x5x5	.015	50.625	24	.009	9.375	y	5	76065.401	99468	6.383	12.757	1.155	H2-1
90	M50	L5x5x5	.015	50.625	16	.005	9.375	y	8	76065.401	99468	6.383	12.743	1.148	H2-1

Stress ratio <1.0. Members are adequate.

Fullerton Engineering Consultants, Inc.

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Mount-to-Tower Connection Calculations

Existing Platform is connected to the monopole via (12) 3/4" \$\phi\$ Bolts, grade A307 (conservatively assumed).

Maximum Reactions from Risa Mount Analysis Node "N251":

Envelope Joint Reactions

с. 	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
17	N248	max	48.436	78	521.501	135	585.3	11	0	1	0	1	0	1
18		min	-74.631	60	-237.628	28	-316.027	29	0	1	0	1	0	1
19	N249	max	749.682	15	1176.979	16	755.748	15	0	1	0	1	0	1
20		min	-336.88	33	-121.293	33	-331.725	33	0	1	0	1	0	1
21	N250	max	624.309	15	789.688	13	92.57	33	0	1	0	1	0	1
22		min	-239.14	32	-370.649	31	-278.972	15	0	1	0	1	0	1
23	N251	max	332.435	6	1207.877	5	773.629	36	.071	36	.122	6	.066	18
24		min	-239.001	36	-588.448	35	-1251.255	6	142	6	077	36	017	135
25	N258	max	42.007	28	186.016	38	355.45	22	0	1	0	1	0	1
26		min	-403.239	23	-161.007	132	-91.322	28	0	1	0	1	0	1
27	N259	max	100.074	7	279.254	132	419.195	16	0	1	0	1	0	1
28		min	-85.31	25	-107.688	38	-102.818	34	0	1	0	1	0	1
29	N260	max	1147.935	2	190.199	38	230.71	2	0	1	0	1	0	1
30		min	-818.105	32	-160.119	132	-124.913	32	0	1	0	1	0	1

X := 332.435/bf	Maximum Reaction - X direction	
Y := 1207.877 lbf	Maximum Reaction - Y direction	
Z := 1251.255/bf	Maximum Reaction - Z direction	
$P_t := Y$	$P_t = 1207.88 lbf$	Factored Tensile Force
$P_V := \sqrt{\chi^2 + \chi^2}$	$P_V = 1294.66 lbf$	Factored Shear Force
$d_b := 0.75 in$		Diameter of rod
$A_b := 0.25\pi \cdot d_b^2$	$A_b = 0.44 \cdot in^2$	Area of rod
$P_{t_bolt} := P_t$	$P_{\underline{t}_bolt} = 1207.88 lbf$	Tension/Compression at rod
$P_{v_bolt} := P_v$	$P_{v_bolt} = 1294.66 lbf$	Shear at rod

CCI Site No.: CTL02108 CCI Site Name: Norwalk West-CT Ave Prepared By: RH Checked By: BK

Tensile and Shear Strength of Threaded Rods

Fullerton Engineering Consultants, Inc.

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Nominal tensile strength per AISC 360-10, Table J3.2

Nominal shear strength per AISC 360-10, Table J3.2

Resistance Factor (LRFD - AISC 360, Section J3-6)

Design Nominal Tensile Strength (AISC 360, Section J3-1)

Design Nominal Shear Strength (AISC 360, Section J3-1)

 $R_{nv} := \phi_{bolt} F_{nv} A_b$

 $R_{nt} := \phi_{bolt} F_{nt} A_b$

 $F_{nt} := 45 ksi$

 $F_{DV} := 27 ksi$

 $\phi_{\textit{bolt}} := .75$

 $\frac{P_{t_bolt}}{R_{nt}} = 8.1 \cdot \%$

 $\frac{P_{V_bolt}}{R_{nv}} = 14.47 \cdot \%$

Check = "Bolts are adequate. Effects of combined stress don't need to be investigated because ratio of either tension or shear is under 30% "

R_{nt} = 14.91∙*kip*

 $R_{nv} = 8.95 \cdot kip$