



STATE OF CONNECTICUT  
CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: [siting.council@ct.gov](mailto:siting.council@ct.gov)

[www.ct.gov/csc](http://www.ct.gov/csc)

July 20, 2012

Stephanie Wenderoth  
Nexlink Global Services  
Suite A, Building 2  
800 Marshall Phelps Road  
Windsor, CT 06095

RE: **EM-AT&T-064-120705** – AT&T Mobility notice of intent to modify an existing telecommunications facility located at 223 Brainard Road, Hartford, Connecticut.

Dear Ms. Wenderoth:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies with the following conditions:

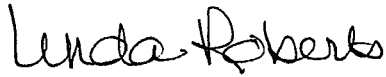
- Any deviation from the proposed modification as specified in this notice and supporting materials with Council shall render this acknowledgement invalid;
- Any material changes to this modification as proposed shall require the filing of a new notice with the Council;
- Not less than 45 days after completion of construction, the Council shall be notified in writing that construction has been completed;
- The validity of this action shall expire one year from the date of this letter; and
- The applicant may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration;

The proposed modifications including the placement of all necessary equipment and shelters within the tower compound are to be implemented as specified here and in your notice dated June 29, 2012. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Thank you for your attention and cooperation.



Very truly yours,

A handwritten signature in black ink that reads "Linda Roberts". The signature is written in a cursive, flowing style.

Linda Roberts  
Executive Director

LR/CDM/cm

- c: The Honorable Pedro E. Segarra, Mayor, City of Hartford
- David B. Panagore, Chief Operating Officer, City of Hartford
- Roger J. O'Brien, Director of Planning, City of Hartford
- Metropolitan District



STATE OF CONNECTICUT  
CONNECTICUT SITING COUNCIL

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E-Mail: [siting.council@ct.gov](mailto:siting.council@ct.gov)  
[www.ct.gov/csc](http://www.ct.gov/csc)

July 5, 2012

The Honorable Pedro E. Segarra  
Mayor  
City of Hartford  
Municipal Building  
550 Main Street  
Hartford, CT 06103

RE: **EM-AT&T-064-120705** – AT&T Mobility notice of intent to modify an existing telecommunications facility located at 223 Brainard Road, Hartford, Connecticut.

Dear Mayor Segarra:

The Connecticut Siting Council (Council) received this request to modify an existing telecommunications facility, pursuant to Regulations of Connecticut State Agencies Section 16-50j-72.

If you have any questions or comments regarding this proposal, please call me or inform the Council by July 19, 2012.

Thank you for your cooperation and consideration.

Very truly yours,

*Linda Roberts* <sup>WAB</sup>

Linda Roberts  
Executive Director

LR/cm

Enclosure: Notice of Intent

c: David B. Panagore, Chief Operating Officer, City of Hartford  
Roger J. O'Brien, Director of Planning, City of Hartford

June 29, 2012

VIA UPS Delivery

Ms. Linda Roberts, Executive Director  
Connecticut Siting Council  
Ten Franklin Square  
New Britain, CT 06051

RE: AT&T Mobility - Notice of Exempt Modification  
223 Brainard Road, Hartford CT

RECEIVED  
JUL - 5 2012

Dear Ms. Roberts:

CONNECTICUT  
SITING COUNCIL

This letter and attachments are submitted on behalf of AT&T Mobility ("AT&T"). AT&T is enhancing the capabilities of its wireless system in Connecticut by implementing LTE technology. In order to do so, AT&T will modify antenna and equipment configurations at a number of existing sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and attachments is being sent to the Mayor of Hartford.

AT&T plans to modify the existing facility at 223 Brainard Road, owned by The Metropolitan District (coordinates 41.732792 N, 72.661899 W). Attached are drawings depicting the planned changes, and documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration. Also included is a power density calculation reflecting the modification to AT&T's operations at the site.

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in R.C. S.A. Section | 6-50j-1 2(b)(2).

1. The height of the overall structure will be unaffected. The existing antennas will remain and AT&T will add three (3) new antennas, six (6) RRU's and one (1) surge arrester. Additionally, AT&T will install one (1) fiber cable and two (2) DC control cables following existing coax.

2. The proposed changes will not extend the site boundaries. AT&T will install additional equipment in the existing equipment shelter. Thus, there will be no effect on the site compound.

3. The proposed changes will not increase the noise level at the existing facility by six decibels or more. The incremental effect of the proposed change will be negligible.

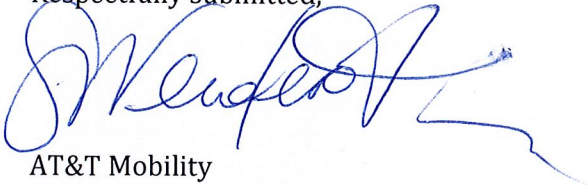
4. The changes to the facility will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environment as calculated for a mixed frequency site. As indicated in the attached



power density calculations, AT&T's operations at the site will result in a power density of 3.04%; the combined site operations will result in a total power density of 33.67%.

Please feel free to call me with any questions or concerns regarding this matter.  
Thank you for your consideration.

Respectfully submitted,

A handwritten signature in blue ink, appearing to read 'Stephanie Wenderoth', with a long horizontal flourish extending to the right.

AT&T Mobility  
Stephanie Wenderoth, Consultant  
wenderoths@nexlinkgs.com  
401.477.2938

Cc:  
Pedro E Segarra; Mayor  
Municipal Building  
550 Main Street  
Hartford, Ct 06103

**CONNECTICUT SITING COUNCIL  
NOTICE OF INTENT TO MODIFY AN EXISTING TOWER FACILITY  
EXEMPT MODIFICATION FILING FORM**

Public Utility Environmental Standards Act, Connecticut General Statutes §§ 16-50g - 16-50aa  
Regulations of Connecticut State Agencies §§ 16-50j-72(b)(2) and 16-50j-73

**TO BE COMPLETED BY FILER**

Date: 6/29/12

Filer Name and Contact Information

Name: Stephanie Wenderoth  
Address: Nexlink Global Services; Suite A Building 2  
800 Marshall Phelps Road, Windsor, CT 06095  
Phone Number: 401.477.2938

Wireless Carrier: AT&T

Tower Owner: AT&T

Tower Site Address: 223 Brainard Road, Hartford CT

Municipality and Name of Chief Elected Official Provided A Copy Of This Notice:  
Pedro E Segarra; Mayor

Description of Exempt Modification (including antenna and equipment changes):  
Add 3 LTE Antennas, new conduit, RRUs and surge arrestor.

Attachments

- Plans
- Power density calculations if applicable
- Tower structural report if applicable
- \$625.00 Filing Fee

If required:

Municipality w/i 2,500' & Name of Chief Elected Official Provided A Copy Of This Notice:

Underlying Property Owner Provided A Copy Of This Notice:

**FOR STAFF USE ONLY**

- 
- Modification will not result in an increase in tower height
  - Modification is within existing site boundaries
  - Modification will not increase noise levels at the site boundary by 6 dbA or more, or to levels that exceed State & local criteria
  - Modification will meet FCC and DEEP MPE limits

- \_\_\_\_\_ Modification will not result in significant adverse change in physical or environmental characteristics of the site
- \_\_\_\_\_ Modification will not impair the structural integrity of the facility as determined by PE
- \_\_\_\_\_ If yes to all of the above, approval of acknowledgement letter



C Squared Systems, LLC  
65 Dartmouth Drive, Unit A3  
Auburn, NH 03032  
(603) 644-2800  
support@csquaredsystems.com

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Calculated Radio Frequency Emissions



CT5126 – East Hartford Hochanum  
223 Brainard Road, Hartford, CT 06114

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June 22, 2012

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## 1. Introduction

The purpose of this report is to investigate compliance with applicable FCC regulations for the proposed modifications to the existing AT&T antenna arrays mounted on the monopole tower located at 223 Brainard Road in Hartford, CT. The coordinates of the tower are 41° 43' 58.0512" N, -72° 39' 42.8364" W.

AT&T is proposing the following modifications:

- 1) Install three 700 MHz LTE antennas (one per sector).

## 2. FCC Guidelines for Evaluating RF Radiation Exposure Limits

In 1985, the FCC established rules to regulate radio frequency (RF) exposure from FCC licensed antenna facilities. In 1996, the FCC updated these rules, which were further amended in August 1997 by OET Bulletin 65 Edition 97-01. These new rules include Maximum Permissible Exposure (MPE) limits for transmitters operating between 300 kHz and 100 GHz. The FCC MPE limits are based upon those recommended by the National Council on Radiation Protection and Measurements (NCRP), developed by the Institute of Electrical and Electronics Engineers, Inc., (IEEE) and adopted by the American National Standards Institute (ANSI).

The FCC general population/uncontrolled limits set the maximum exposure to which most people may be subjected. General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

Public exposure to radio frequencies is regulated and enforced in units of milliwatts per square centimeter ( $\text{mW}/\text{cm}^2$ ). The general population exposure limits for the various frequency ranges are defined in the attached "FCC Limits for Maximum Permissible Exposure (MPE)" in Attachment B of this report.

Higher exposure limits are permitted under the occupational/controlled exposure category, but only for persons who are exposed as a consequence of their employment and who have been made fully aware of the potential for exposure, and they must be able to exercise control over their exposure. General population/uncontrolled limits are five times more stringent than the levels that are acceptable for occupational, or radio frequency trained individuals. Attachment B contains excerpts from OET Bulletin 65 and defines the Maximum Exposure Limit.

Finally, it should be noted that the MPE limits adopted by the FCC for both general population/uncontrolled exposure and for occupational/controlled exposure incorporate a substantial margin of safety and have been established to be well below levels generally accepted as having the potential to cause adverse health effects.

### 3. RF Exposure Prediction Methods

The emission field calculation results displayed in the following figures were generated using the following formula as outlined in FCC bulletin OET 65:

$$\text{Power Density} = \left( \frac{1.6^2 \times \text{EIRP}}{4\pi \times R^2} \right) \times \text{Off Beam Loss}$$

Where:

EIRP = Effective Isotropic Radiated Power

R = Radial Distance =  $\sqrt{(H^2 + V^2)}$

H = Horizontal Distance from antenna in meters

V = Vertical Distance from radiation center of antenna in meters

Ground reflection factor of 1.6

Off Beam Loss is determined by the selected antenna pattern

These calculations assume that the antennas are operating at 100 percent capacity and power, and that all channels are transmitting simultaneously. Obstructions (trees, buildings, etc.) that would normally attenuate the signal are not taken into account. The calculations assume even terrain in the area of study and do not take into account actual terrain elevations which could attenuate the signal. As a result, the predicted signal levels reported below are much higher than the actual signal levels will be from the finished modifications.

#### 4. Calculation Results

Table 1 below outlines the power density information for the site. Because the proposed AT&T antennas are directional in nature, the majority of the RF power is focused out towards the horizon. As a result, there will be less RF power directed below the antennas relative to the horizon, and consequently lower power density levels around the base of the tower. Please refer to Attachment C for the vertical pattern of the proposed AT&T antennas. The calculated results for AT&T in Table 1 include a nominal 10 dB off-beam pattern loss to account for the lower relative gain below the antennas.

Carrier	Antenna Height (Feet)	Operating Frequency (MHz)	Number of Trans.	ERP Per Transmitter (Watts)	Power Density (mw/cm <sup>2</sup> )	Limit	%MPE
AT&T/Cingular GSM	98	1900	2	427	0.0320	1.0000	3.20%
AT&T/Cingular GSM	98	880	4	296	0.0443	0.5867	7.56%
AT&T/Cingular UMTS	98	980	1	500	0.0187	0.5867	3.19%
Verizon	88	1970	3	375	0.0522	1.0000	5.22%
Verizon	88	880	9	271	0.1132	0.5867	19.30%
Clearwire	80	2496	2	153	0.0172	1.0000	1.72%
Clearwire	80	18 GHz	1	211	0.0119	1.0000	1.19%
AT&T UMTS	103	880	2	565	0.0038	0.5867	0.65%
AT&T UMTS	103	1900	2	875	0.0059	1.0000	0.59%
AT&T LTE	102	734	1	1313	0.0045	0.4893	0.93%
AT&T GSM	103	880	1	283	0.0010	0.5867	0.16%
AT&T GSM	103	1900	4	525	0.0071	1.0000	0.71%
						<b>Total</b>	<b>33.67%</b>

**Table 1: Carrier Information**<sup>1 2 3</sup>

<sup>1</sup> The existing CSC filing for Cingular should be removed and replaced with the updated AT&T technologies and values provided in Table 1. The power density information for carriers other than AT&T was taken directly from the CSC database dated 3/29/2012. Please note that %MPE values listed are rounded to two decimal points. The total %MPE listed is a summation of each unrounded contribution. Therefore, summing each rounded value may not reflect the total value listed in the table.

<sup>2</sup> In the case where antenna models are not uniform across all 3 sectors for the same frequency band, the antenna model with the highest gain was used for the calculations to present a worse-case scenario.

<sup>3</sup> Antenna height listed for AT&T is in reference to the B&T Engineering, Inc. Structural Analysis dated May 29, 2012



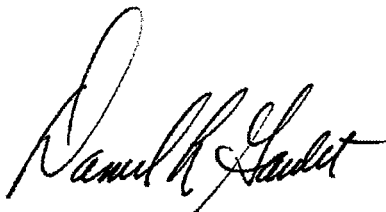
## 5. Conclusion

The above analysis verifies that emissions from the existing site will be below the maximum power density levels as outlined by the FCC in the OET Bulletin 65 Ed. 97-01. Even when using conservative methods, the cumulative power density from the proposed transmit antennas at the existing facility is well below the limits for the general public. The highest expected percent of Maximum Permissible Exposure at ground level is **33.67% of the FCC limit**.

As noted previously, obstructions (trees, buildings, etc.) that would normally attenuate the signal are not taken into account. As a result, the predicted signal levels are more conservative (higher) than the actual signal levels will be from the finished modifications.

## 6. Statement of Certification

I certify to the best of my knowledge that the statements in this report are true and accurate. The calculations follow guidelines set forth in ANSI/IEEE Std. C95.3, ANSI/IEEE Std. C95.1 and FCC OET Bulletin 65 Edition 97-01.



Daniel L. Goulet  
C Squared Systems, LLC

June 22, 2012

Date

## Attachment A: References

OET Bulletin 65 - Edition 97-01 - August 1997 Federal Communications Commission Office of Engineering & Technology

ANSI C95.1-1982, American National Standard Safety Levels With Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 300 kHz to 100 GHz. IEEE-SA Standards Board

IEEE Std C95.3-1991 (Reaff 1997), IEEE Recommended Practice for the Measurement of Potentially Hazardous Electromagnetic Fields - RF and Microwave. IEEE-SA Standards Board

**Attachment B: FCC Limits for Maximum Permissible Exposure (MPE)**

<b>(A) Limits for Occupational/Controlled Exposure<sup>4</sup></b>				
Frequency Range (MHz)	Electric Field Strength (E) (V/m)	Magnetic Field Strength (E) (A/m)	Power Density (S) (mW/cm <sup>2</sup> )	Averaging Time  E  <sup>2</sup> ,  H  <sup>2</sup> or S (minutes)
0.3-3.0	614	1.63	(100)*	6
3.0-30	1842/f	4.89/f	(900/f <sup>2</sup> )*	6
30-300	61.4	0.163	1.0	6
300-1500	-	-	f/300	6
1500-100,000	-	-	5	6

<b>(B) Limits for General Population/Uncontrolled Exposure<sup>5</sup></b>				
Frequency Range (MHz)	Electric Field Strength (E) (V/m)	Magnetic Field Strength (E) (A/m)	Power Density (S) (mW/cm <sup>2</sup> )	Averaging Time  E  <sup>2</sup> ,  H  <sup>2</sup> or S (minutes)
0.3-1.34	614	1.63	(100)*	30
1.34-30	824/f	2.19/f	(180/f <sup>2</sup> )*	30
30-300	27.5	0.073	0.2	30
300-1500	-	-	f/1500	30
1500-100,000	-	-	1.0	30

f = frequency in MHz \* Plane-wave equivalent power density

**Table 2: FCC Limits for Maximum Permissible Exposure (MPE)**

<sup>4</sup> Occupational/controlled limits apply in situations in which persons are exposed as a consequence of their employment provided those persons are fully aware of the potential for exposure and can exercise control over their exposure. Limits for occupational/controlled exposure also apply in situations when an individual is transient through a location where occupational/controlled limits apply provided he or she is made aware of the potential for exposure

<sup>5</sup> General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure

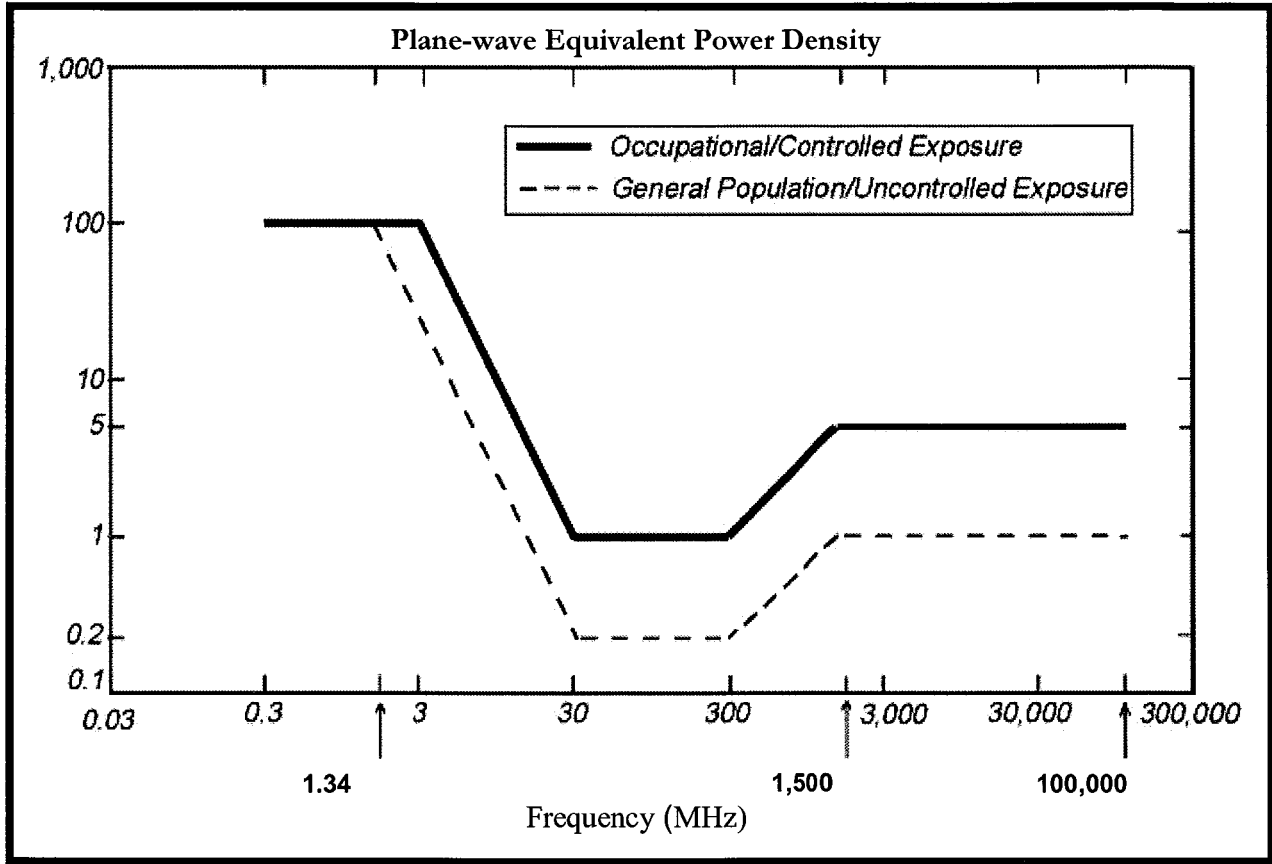
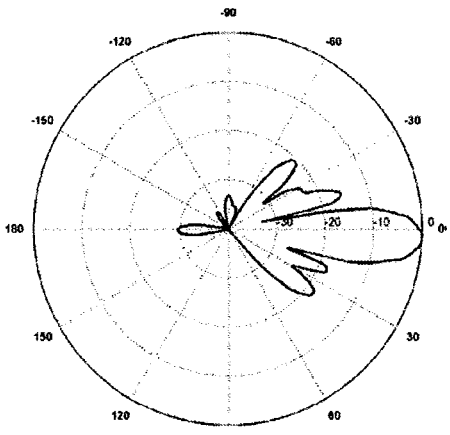
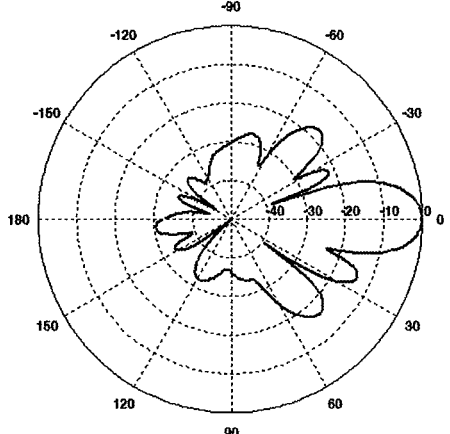
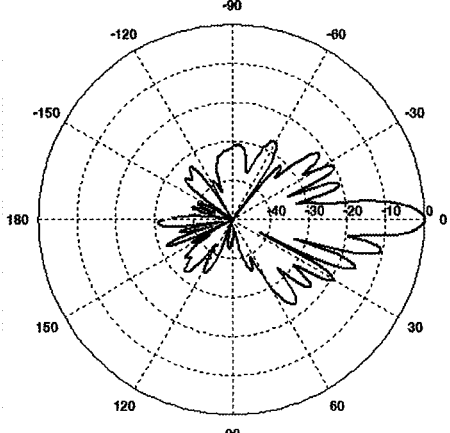


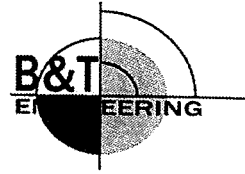
Figure 1: Graph of FCC Limits for Maximum Permissible Exposure (MPE)

**Attachment C: AT&T Antenna Data Sheets and Electrical Patterns**

<p><b>700 MHz</b></p> <p>Manufacturer: KMW            Model #: AM-X-CD-16-65-00T            Frequency Band: 698-806 MHz            Gain: 13.4 dBd            Vertical Beamwidth: 12.3°            Horizontal Beamwidth: 65°            Polarization: Dual Slant <math>\pm 45^\circ</math>            Size L x W x D: 72"×11.8"×5.9"</p>	
<p><b>850 MHz</b></p> <p>Manufacturer: Powerwave            Model #: 7770            Frequency Band: 824-896 MHz            Gain: 11.5 dBd            Vertical Beamwidth: 15°            Horizontal Beamwidth: 85°            Polarization: Dual Linear <math>\pm 45^\circ</math>            Size L x W x D: 55.4"×11.0"×5.0"</p>	
<p><b>1900 MHz</b></p> <p>Manufacturer: Powerwave            Model #: 7770            Frequency Band: 1850-1990 MHz            Gain: 13.4 dBd            Vertical Beamwidth: 7°            Horizontal Beamwidth: 90°            Polarization: Dual Linear <math>\pm 45^\circ</math>            Size L x W x D: 55.4"×11.0"×5.0"</p>	



**Nexlink Global Services, Inc.**  
 800 Marshall Phelps Road  
 Windsor, CT 06095  
 May 29, 2012



**B&T Engineering, Inc.**  
 1717 S. Boulder, Suite 300  
 Tulsa, OK 74119  
 B&T No.: 84436.000.0001

**STRUCTURAL ANALYSIS**  
**99.4' Monopole Tower**

**AT&T DESIGNATION:** Site ID: 4539 (CT5126)  
 Site FA: 10071011  
 Site Name: EAST HARTFORD HOCHANUM  
 AT&T Project: MOD LTE W3 020912

**ANALYSIS CRITERIA:** Codes: TIA/EIA-222-F (80 mph fastest mile)  
 IBC 2003  
 2005 CT State Building Code

**SITE DATA:** 223 Brainard Road, Hartford, CT, Hartford County  
 Latitude 41.732792°, Longitude -72.661899°  
 Market MA/RI/VT/NH/ME/CT

Ms. Stephanie Wenderoth,

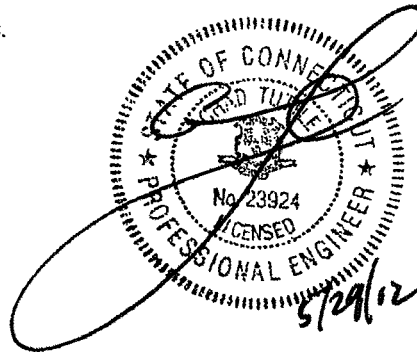
B&T Engineering, Inc. is pleased to submit this Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

**Analysis Results**

Tower Stress Level with Proposed Equipment: **77.9% Pass**  
 Foundation Ratio with Proposed Equipment: **Unknown**

We at B&T Engineering, Inc. appreciate the opportunity of providing our continuing professional services to you and Nexlink Global Services, Inc.. If you have any questions or need further assistance on this or any other project please give us a call.

Respectfully Submitted by: B&T Engineering, Inc.  
 Analysis Prepared by: Kristin Mears, E.I.  
 Analysis Reviewed by: Chad E. Tuttle, P.E.



**ANALYSIS RESULTS:**

**Table 1 - Section Capacity (Summary)**

Component (Tower Section)	% Capacity	Pass / Fail
99.42 - 77.08	30.2	Pass
77.08 - 40.42	65.1	Pass
40.42 - 0	77.8	Pass

**Table 2 - Tower Component Stresses vs. Capacity**

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	Base	77.9	<b>Pass</b>
1	Base Plate	Base	48.7	<b>Pass</b>
2	Base Foundation	Base	--	--

<b>Structure Rating (max from all components) =</b>	<b>77.9%</b>
---	--------------

Notes:

- 1.) See additional documentation in "Appendix B - Calculations" for calculation supporting the % capacity consumed.
- 2.) The base foundation could not be analyzed as part of this analysis, as foundation and geotechnical information was not available. It is assumed that the foundation was designed with capacities similar to the tower itself and is therefore considered sufficient for the purposes of this analysis.

**Recommendations:**

N/A

## ANALYSIS PROCEDURE:

**Table 4 - Documents Provided**

Document	Description	Date	Source
Tower Data	BTE Management; Job No. 15085	4/27/2012	On File
Foundation Information	Information Not Available	N/A	N/A
Geotech Report	Information Not Available	N/A	N/A
Loading	Equip Mod Form	2/9/2012	Siterra
	Tower Mapping by BTE Management; Job No.	4/27/2012	On File
	Previous SA by GPD	9/26/2011	Siterra
Previous Structural Analysis	GPD (SL)	9/26/2011	Siterra
	GPD	11/23/2010	Siterra
	GPD	6/23/2010	Siterra

## ANALYSIS METHOD:

tnxTower, a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix B.

## ASSUMPTIONS:

1. Tower and structures were built in accordance with the manufacturer's specifications.
2. The tower and structures have been maintained in accordance with the manufacturer's specifications.
3. The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Appendix A of this report.
4. Mount areas and weights are assumed based on photographs provided.
5. Refer to the base level drawing for transmission line distribution.
6. Manufacturer's drawings were not available, therefore, material grades were assumed.
7. Nominal sizes were assumed based on measured thicknesses from the BTE tower mapping.
8. Lap splices were assumed.

If any of these assumptions have been made in error, B&T Engineering should be notified to determine the effect on the structural integrity of the tower.

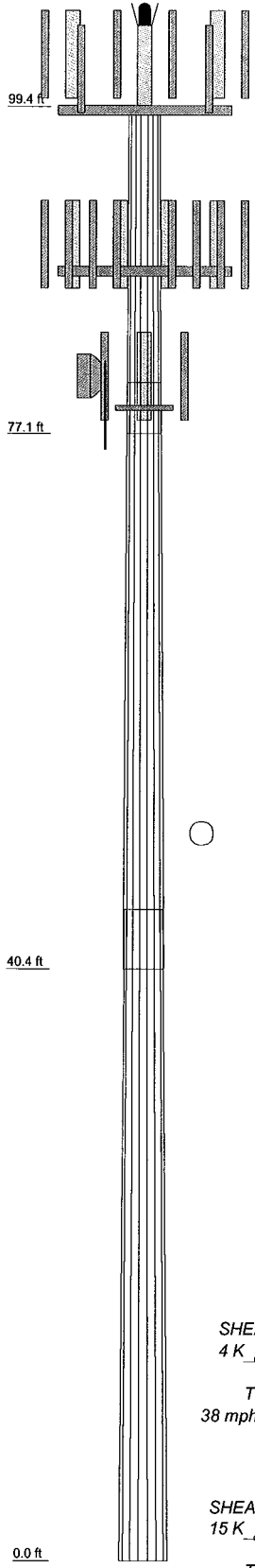


**APPENDIX A**  
**TOWER ANALYSIS LOADING**



**APPENDIX B**  
**CALCULATIONS**

Section	1	2	3
Length (ft)	22.340	40.160	44.503
Number of Sides	18	18	18
Thickness (in)	0.188	0.250	0.313
Socket Length (ft)	3.500	4.083	32.366
Top Dia (in)	25.320	27.526	39.090
Bot Dia (in)	28.580	33.470	
Grade		A572-60	
Weight (K)	1.2	3.3	5.3



**DESIGNED APPURTENANCE LOADING**

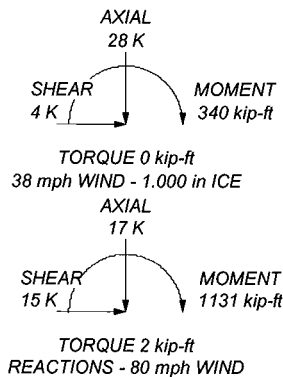
TYPE	ELEVATION	TYPE	ELEVATION
Beacon (E)	105	(2) LPA-80063/4CF w/ Mount Pipe (Verizon-E)	90
(2) RA21.7770.00 w/ Mount Pipe (ATI-E)	103	(2) LPA-185063/8CF w/ Mount Pipe (Verizon-E)	90
(2) RA21.7770.00 w/ Mount Pipe (ATI-E)	103	(2) LPA-185063/8CF w/ Mount Pipe (Verizon-E)	90
(2) RA21.7770.00 w/ Mount Pipe (ATI-E)	103	(2) LPA-185063/8CF w/ Mount Pipe (Verizon-E)	90
(4) LGP21401 (ATI-E)	103	(2) LPA-185063/8CF w/ Mount Pipe (Verizon-E)	90
(4) LGP21401 (ATI-E)	103	Platform Mount [LP 304-1] (E)	88.5
(4) LGP21401 (ATI-E)	103	LLPX310R-V4 w/Mount Pipe (Clearwire-E)	81
AM-X-CD-16-65-00T-RET w/ Mount Pipe (ATI-P)	102	LLPX310R-V4 w/Mount Pipe (Clearwire-E)	81
AM-X-CD-16-65-00T-RET w/ Mount Pipe (ATI-P)	102	LLPX310R-V4 w/Mount Pipe (Clearwire-E)	81
AM-X-CD-16-65-00T-RET w/ Mount Pipe (ATI-P)	102	RRH-2WB0 (Clearwire-E)	81
(2) RBS 6601 (ATI-P)	100	RRH-2WB0 (Clearwire-E)	81
(2) RBS 6601 (ATI-P)	100	RRH-2WB0 (Clearwire-E)	81
(2) RBS 6601 (ATI-P)	100	18"x17"x11" TMA (Clearwire-E)	81
DC6-48-60-18-8F (ATI-P)	100	VHLP2.5-18-DW1 (E)	81
Platform Mount [LP 601-1] (E)	99.5	6' x 2" Mount Pipe (Clearwire-E)	79
(2) LPA-80080/4CF w/Mount Pipe (Verizon-E)	90	6' x 2" Mount Pipe (Clearwire-E)	79
(2) LPA-80063/4CF w/ Mount Pipe (Verizon-E)	90	Side Arm Mount [SO 103-3] (E)	79
		6' x 2" Mount Pipe (Clearwire-E)	79

**MATERIAL STRENGTH**

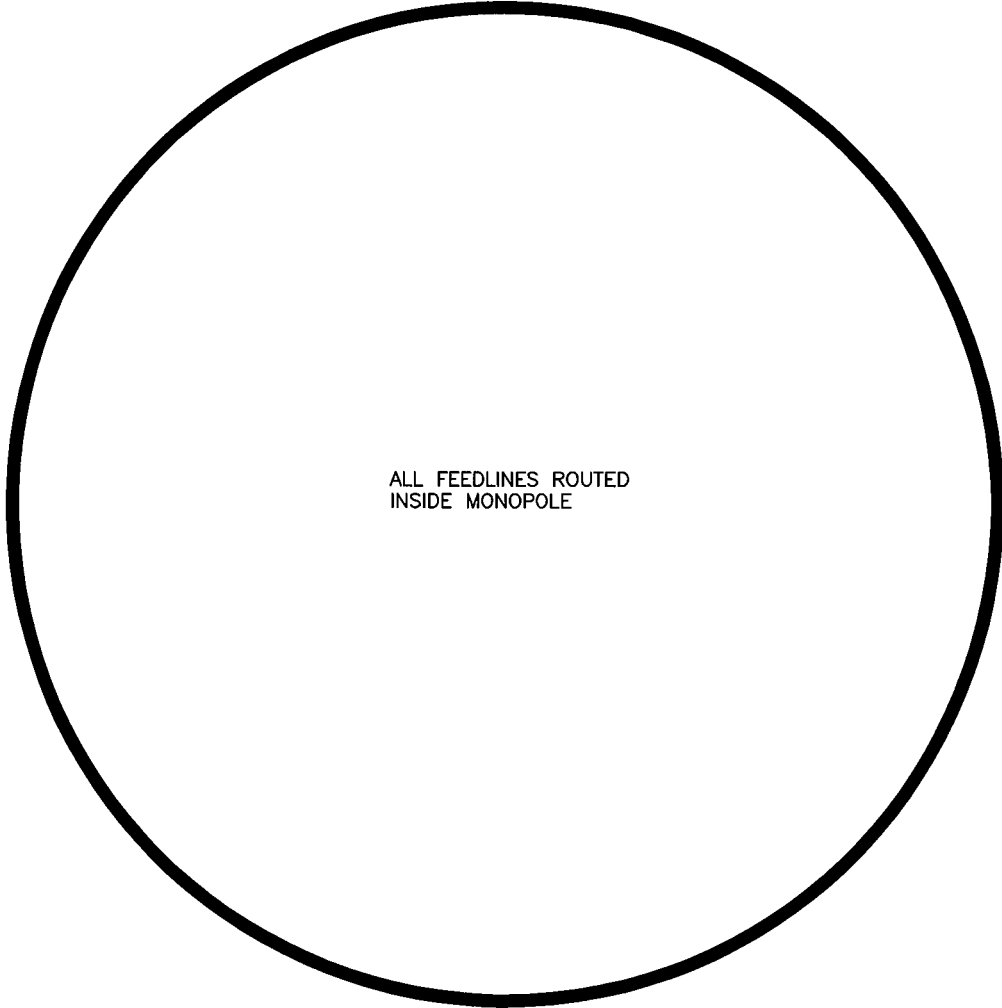
GRADE	Fy	Fu	GRADE	Fy	Fu
A572-60	60 ksi	75 ksi			

**TOWER DESIGN NOTES**

1. Tower is located in Hartford County, Connecticut.
2. Tower designed for a 80 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 38 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 50 mph wind.
5. TOWER RATING: 77.8%



<p><b>B&amp;T Engineering, Inc.</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265</p>	Job: <b>84436.000.0001 - East Hartford Hochanum, CT (USID# 453)</b>
	Project: <b>99.4' Monopole / AT&amp;T Co-Locate</b>
	Client: Nexlink
	Drawn by: K. Mears
	App'd:
Code: TIA/EIA-222-F	Date: 05/29/12
Path:	Scale: NTS
	Dwg No. E-1



ALL FEEDLINES ROUTED  
INSIDE MONOPOLE

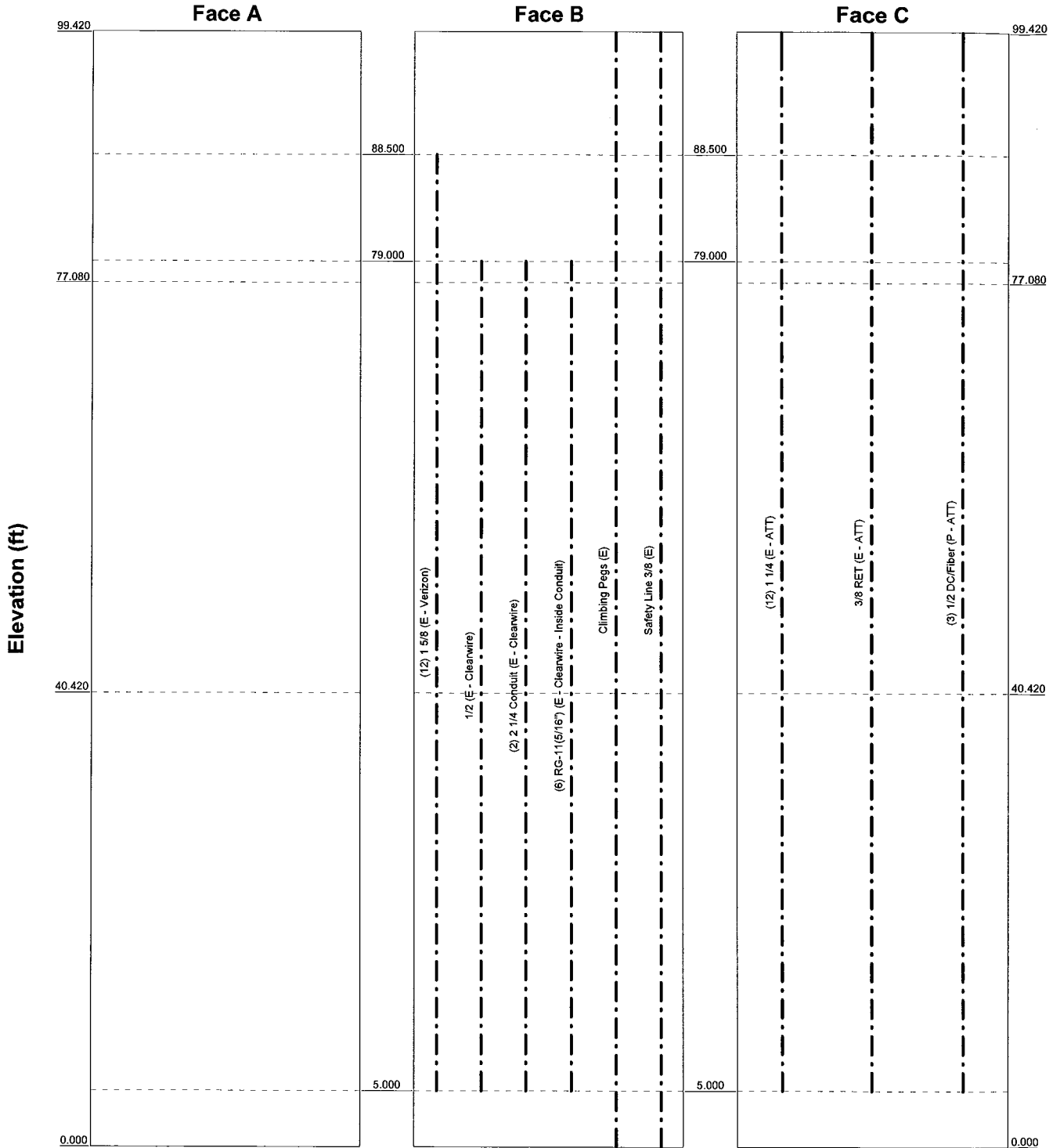
PROJECT#: 84436

NOT TO SCALE

# Feedline Distribution Chart

0' - 99'5-1/32"

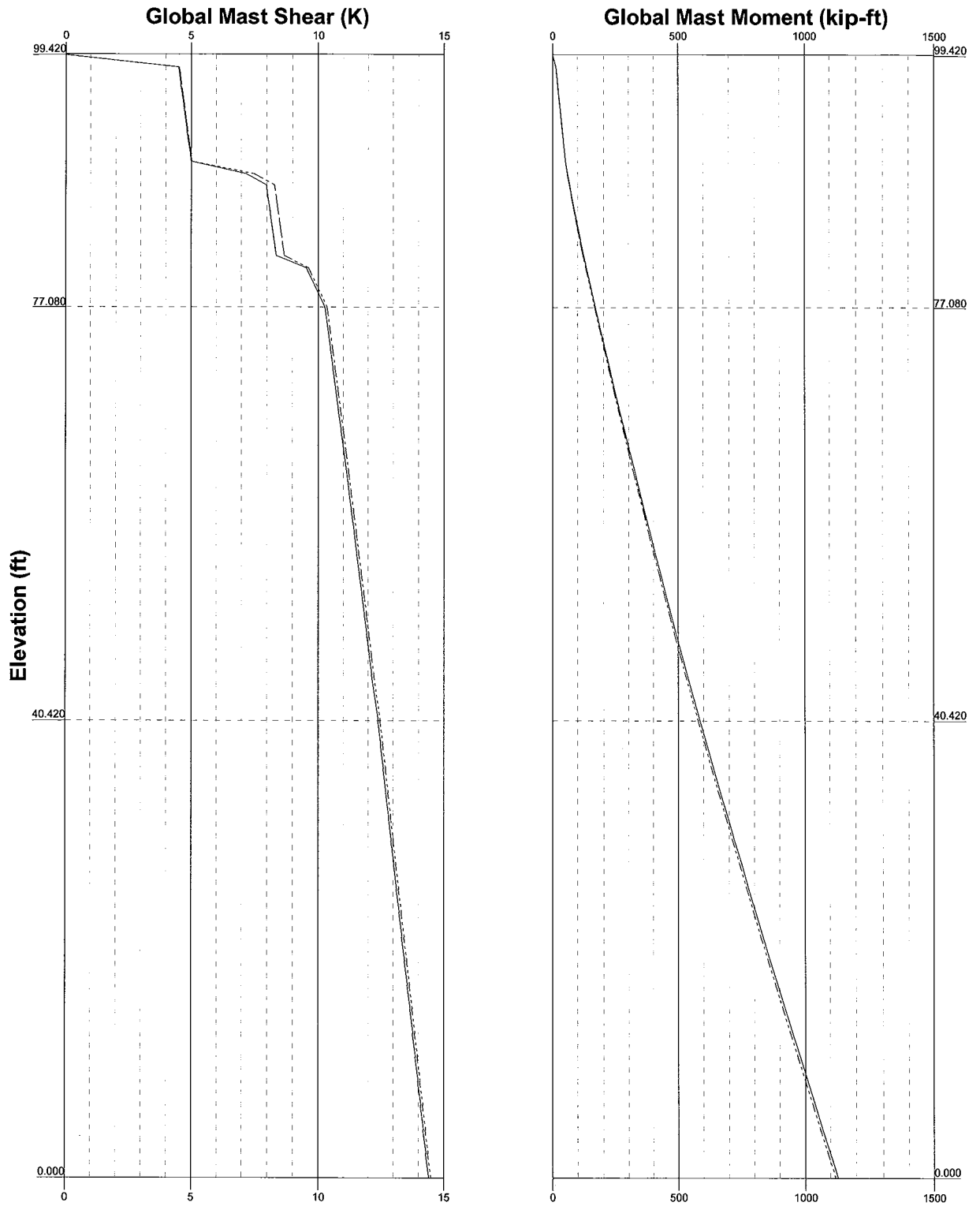
Round \_\_\_\_\_ Flat \_\_\_\_\_ App In Face \_\_\_\_\_ App Out Face \_\_\_\_\_ Truss Leg \_\_\_\_\_




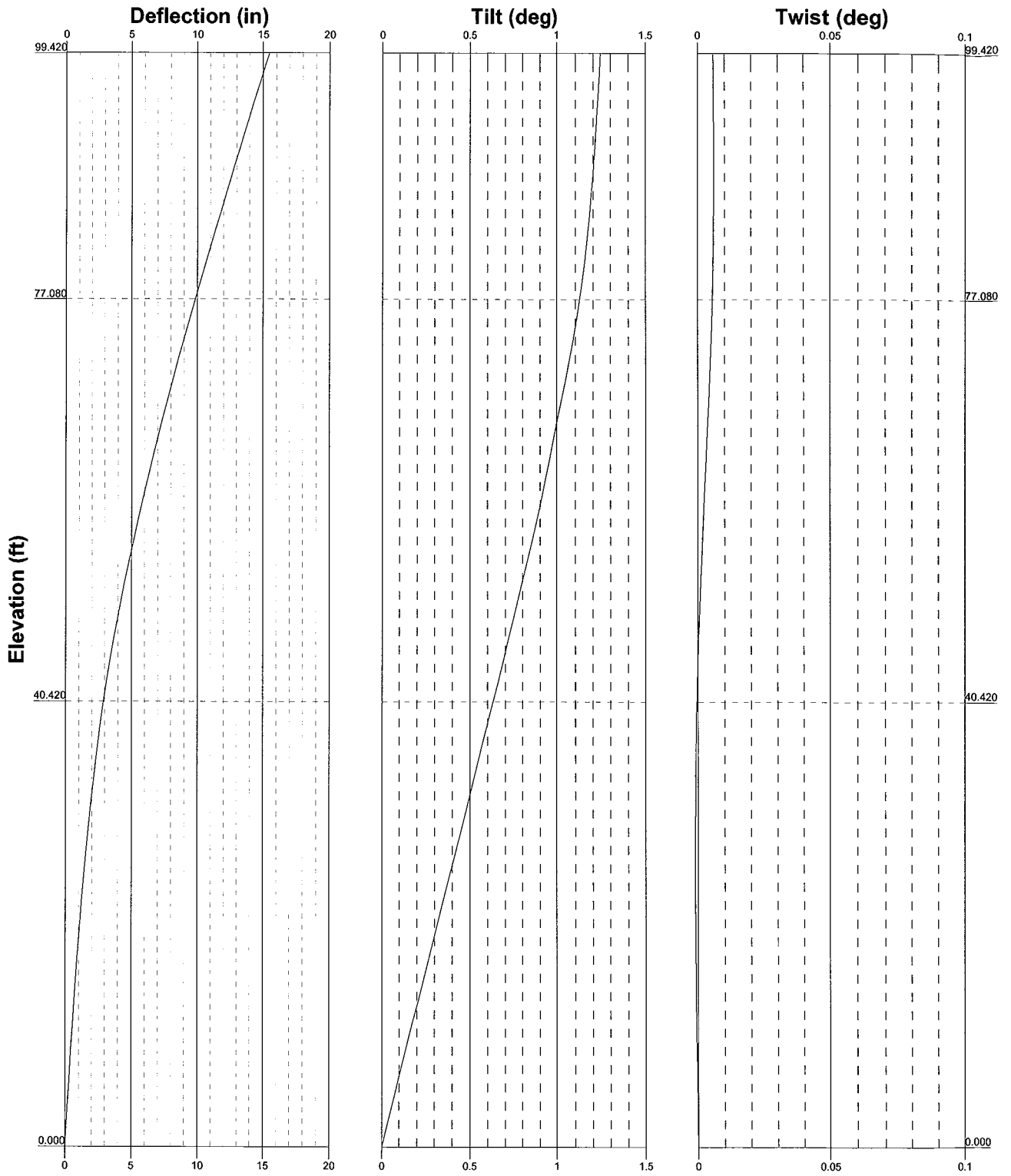
	<b>B&amp;T Engineering, Inc.</b>		Job: <b>84436.000.0001 - East Hartford Hohanum, CT (USID# 453)</b>		
	1717 S. Boulder, Suite 300		Project: <b>99.4' Monopole / AT&amp;T Co-Locate</b>		
	Tulsa, OK 74119		Client: Nexlink	Drawn by: K. Mears	App'd:
	Phone: (918) 587-4630		Code: TIA/EIA-222-F	Date: 05/29/12	Scale: NTS
	FAX: (918) 295-0265		Path:		Dwg No. E-7


—— Vx      - - - - Vz

—— Mx      - - - - Mz



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	Project: <b>99.4' Monopole / AT&amp;T Co-Locate</b>		
	Client: Nexlink	Drawn by: K. Mears	App'd:
	Code: TIA/EIA-222-F	Date: 05/29/12	Scale: NTS
	Path:		Dwg No. E-4



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	<b>Project: 99.4' Monopole / AT&amp;T Co-Locate</b>		
	Client: Nexlink	Drawn by: K. Mears	App'd:
	Code: TIA/EIA-222-F	Date: 05/29/12	Scale: NTS
	Path:		Dwg No. E-5



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	<b>Project</b> 99.4' Monopole / AT&T Co-Locate	<b>Date</b> 10:32:19 05/29/12
	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

## Tower Input Data

There is a pole section.  
This tower is designed using the TIA/EIA-222-F standard.  
The following design criteria apply:

- Tower is located in Hartford County, Connecticut.
- Basic wind speed of 80 mph.
- Nominal ice thickness of 1.000 in.
- Ice thickness is considered to increase with height.
- Ice density of 56.000 pcf.
- A wind speed of 38 mph is used in combination with ice.
- Temperature drop of 50.000 °F.
- Deflections calculated using a wind speed of 50 mph.
- A non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- Stress ratio used in pole design is 1.333.
- Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

## Options

- |  |  |  |
|--|--|--|
| <ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>√ Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>Include Bolts In Member Capacity</li> <li>Leg Bolts Are At Top Of Section</li> <li>Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>Add IBC .6D+W Combination</li> </ul> | <ul style="list-style-type: none"> <li>Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>Use Clear Spans For KL/r</li> <li>Retension Guys To Initial Tension</li> <li>√ Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <li>Autocalc Torque Arm Areas</li> <li>SR Members Have Cut Ends</li> <li>Sort Capacity Reports By Component</li> <li>Triangulate Diamond Inner Bracing</li> </ul> | <ul style="list-style-type: none"> <li>Treat Feedline Bundles As Cylinder</li> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feedline Torque</li> <li>Include Angle Block Shear Check Poles</li> <li>√ Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> </ul> |
|--|--|--|

## Tapered Pole Section Geometry

Section	Elevation	Section Length	Splice Length	Number of Sides	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft		in	in	in	in	
L1	99.420-77.080	22.340	3.500	18	25.320	28.380	0.188	0.750	A572-60 (60 ksi)
L2	77.080-40.420	40.160	4.083	18	27.526	33.470	0.250	1.000	A572-60 (60 ksi)
L3	40.420-0.000	44.503		18	32.366	39.090	0.313	1.250	A572-60 (60 ksi)

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	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

**Tapered Pole Properties**

Section	Tip Dia. in	Area in <sup>2</sup>	I in <sup>4</sup>	r in	C in	I/C in <sup>3</sup>	J in <sup>4</sup>	I/Q in <sup>2</sup>	w in	w/t
L1	25.711	14.957	1193.583	8.922	12.863	92.795	2388.737	7.480	4.126	22.007
	28.818	16.778	1684.792	10.008	14.417	116.861	3371.802	8.391	4.665	24.879
L2	28.476	21.643	2034.262	9.683	13.983	145.481	4071.201	10.824	4.405	17.618
	33.986	26.360	3675.219	11.793	17.003	216.154	7355.275	13.183	5.451	21.803
L3	33.491	31.793	4126.732	11.379	16.442	250.991	8258.893	15.899	5.146	16.468
	39.693	38.462	7306.911	13.766	19.858	367.963	14623.436	19.235	6.330	20.255

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals
ft	ft <sup>2</sup>	in					in	in
L1 99.420-77.080				1	1	1		
L2 77.080-40.420				1	1	1		
L3 40.420-0.000				1	1	1		

**Feed Line/Linear Appurtenances - Entered As Round Or Flat**

Description	Face or Leg	Allow Shield	Component Type	Placement	Total Number	Number Per Row	Clear Spacing	Width or Diameter	Perimeter	Weight
				ft			in	in	in	klf
**										

**Feed Line/Linear Appurtenances - Entered As Area**

Description	Face or Leg	Allow Shield	Component Type	Placement	Total Number	C <sub>AA</sub>	Weight
				ft		ft <sup>2</sup> /ft	klf
1 1/4 (E - ATT)	C	No	Inside Pole	99.420 - 5.000	12	No Ice	0.000
						1/2" Ice	0.000
						1" Ice	0.000
						2" Ice	0.000
						4" Ice	0.000
3/8 RET (E - ATT)	C	No	Inside Pole	99.420 - 5.000	1	No Ice	0.000
						1/2" Ice	0.000
						1" Ice	0.000
						2" Ice	0.000
						4" Ice	0.000
1/2 DC/Fiber (P - ATT)	C	No	Inside Pole	99.420 - 5.000	3	No Ice	0.000
						1/2" Ice	0.000
						1" Ice	0.000
						2" Ice	0.000
						4" Ice	0.000
1 5/8 (E - Verizon)	B	No	Inside Pole	88.500 - 5.000	12	No Ice	0.000
						1/2" Ice	0.000
						1" Ice	0.000
						1" Ice	0.000

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	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		C <sub>A</sub> A <sub>1</sub> ft <sup>2</sup> /ft	Weight klf
						2" Ice	0.000	0.001
						4" Ice	0.000	0.001
*/*								
1/2 (E - Clearwire)	B	No	Inside Pole	79.000 - 5.000	1	No Ice	0.000	0.000
						1/2" Ice	0.000	0.000
						1" Ice	0.000	0.000
						2" Ice	0.000	0.000
						4" Ice	0.000	0.000
2 1/4 Conduit (E - Clearwire)	B	No	Inside Pole	79.000 - 5.000	2	No Ice	0.000	0.001
						1/2" Ice	0.000	0.001
						1" Ice	0.000	0.001
						2" Ice	0.000	0.001
						4" Ice	0.000	0.001
RG-11(5/16") (E - Clearwire - Inside Conduit)	B	No	Inside Pole	79.000 - 5.000	6	No Ice	0.000	0.000
						1/2" Ice	0.000	0.000
						1" Ice	0.000	0.000
						2" Ice	0.000	0.000
						4" Ice	0.000	0.000
*/*								
Climbing Pegs (E)	B	No	CaAa (Out Of Face)	99.420 - 0.000	1	No Ice	0.088	0.001
						1/2" Ice	0.188	0.001
						1" Ice	0.287	0.003
						2" Ice	0.487	0.008
						4" Ice	0.887	0.024
Safety Line 3/8 (E)	B	No	CaAa (Out Of Face)	99.420 - 0.000	1	No Ice	0.037	0.000
						1/2" Ice	0.137	0.001
						1" Ice	0.238	0.001
						2" Ice	0.437	0.002
						4" Ice	0.838	0.004
*/*								

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>1</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>1</sub> Out Face ft <sup>2</sup>	Weight K
L1	99.420-77.080	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	2.793	0.165
		C	0.000	0.000	0.000	0.000	0.196
L2	77.080-40.420	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	4.583	0.599
		C	0.000	0.000	0.000	0.000	0.321
L3	40.420-0.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	5.053	0.582
		C	0.000	0.000	0.000	0.000	0.310

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>1</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>1</sub> Out Face ft <sup>2</sup>	Weight K
L1	99.420-77.080	A	1.125	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	0.000	12.845	0.256
		C		0.000	0.000	0.000	0.000	0.196
L2	77.080-40.420	A	1.071	0.000	0.000	0.000	0.000	0.000

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	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>MA</sub> In Face ft <sup>2</sup>	C <sub>MA</sub> Out Face ft <sup>2</sup>	Weight K
L3	40.420-0.000	B		0.000	0.000	0.000	21.079	0.748
		C		0.000	0.000	0.000	0.000	0.321
		A	1.000	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	0.000	22.375	0.734
		C		0.000	0.000	0.000	0.000	0.310

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>X</sub> in	CP <sub>Z</sub> in	CP <sub>X</sub> Ice in	CP <sub>Z</sub> Ice in
L1	99.420-77.080	0.154	0.089	0.557	0.322
L2	77.080-40.420	0.155	0.089	0.576	0.332
L3	40.420-0.000	0.156	0.090	0.578	0.334

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>MA</sub> Front ft <sup>2</sup>	C <sub>MA</sub> Side ft <sup>2</sup>	Weight K	
Beacon (E)	C	None		0.000	105.000	No Ice	1.500	1.500	0.200
						1/2" Ice	2.250	2.250	0.300
						1" Ice	3.000	3.000	0.400
						2" Ice	4.500	4.500	0.600
						4" Ice	7.500	7.500	1.000
*/*									
(2) RA21.7770.00 w/ Mount Pipe (AT&T-E)	C	From Leg	4.000 0.000 0.000	10.000	103.000	No Ice	7.031	5.002	0.060
						1/2" Ice	7.608	5.960	0.112
						1" Ice	8.165	6.747	0.174
						2" Ice	9.310	8.370	0.322
						4" Ice	11.721	11.872	0.746
(2) RA21.7770.00 w/ Mount Pipe (AT&T-E)	B	From Leg	4.000 0.000 0.000	10.000	103.000	No Ice	7.031	5.002	0.060
						1/2" Ice	7.608	5.960	0.112
						1" Ice	8.165	6.747	0.174
						2" Ice	9.310	8.370	0.322
						4" Ice	11.721	11.872	0.746
(2) RA21.7770.00 w/ Mount Pipe (AT&T-E)	A	From Leg	4.000 0.000 0.000	10.000	103.000	No Ice	7.031	5.002	0.060
						1/2" Ice	7.608	5.960	0.112
						1" Ice	8.165	6.747	0.174
						2" Ice	9.310	8.370	0.322
						4" Ice	11.721	11.872	0.746
(4) LGP21401 (AT&T-E)	C	From Leg	4.000 0.000 0.000	10.000	103.000	No Ice	1.288	0.233	0.014
						1/2" Ice	1.445	0.313	0.021
						1" Ice	1.611	0.403	0.030
						2" Ice	1.969	0.608	0.055
						4" Ice	2.788	1.121	0.135
(4) LGP21401 (AT&T-E)	B	From Leg	4.000 0.000	10.000	103.000	No Ice	1.288	0.233	0.014
						1/2" Ice	1.445	0.313	0.021

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	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>A</sub> A <sub>1</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>2</sub> Side ft <sup>2</sup>	Weight K
			0.000			1" Ice 1.611	0.403	0.030
						2" Ice 1.969	0.608	0.055
						4" Ice 2.788	1.121	0.135
(4) LGP21401 (AT&T-E)	A	From Leg	4.000	10.000	103.000	No Ice 1.288	0.233	0.014
			0.000			1/2" Ice 1.445	0.313	0.021
			0.000			1" Ice 1.611	0.403	0.030
						2" Ice 1.969	0.608	0.055
						4" Ice 2.788	1.121	0.135
AM-X-CD-16-65-00T-RET w/ Mount Pipe (AT&T-P)	C	From Leg	4.000	0.000	102.000	No Ice 8.498	6.304	0.074
			0.000			1/2" Ice 9.149	7.479	0.136
			0.000			1" Ice 9.767	8.368	0.210
						2" Ice 11.031	10.179	0.385
						4" Ice 13.679	14.024	0.874
AM-X-CD-16-65-00T-RET w/ Mount Pipe (AT&T-P)	B	From Leg	4.000	0.000	102.000	No Ice 8.498	6.304	0.074
			0.000			1/2" Ice 9.149	7.479	0.136
			0.000			1" Ice 9.767	8.368	0.210
						2" Ice 11.031	10.179	0.385
						4" Ice 13.679	14.024	0.874
AM-X-CD-16-65-00T-RET w/ Mount Pipe (AT&T-P)	A	From Leg	4.000	0.000	102.000	No Ice 8.498	6.304	0.074
			0.000			1/2" Ice 9.149	7.479	0.136
			0.000			1" Ice 9.767	8.368	0.210
						2" Ice 11.031	10.179	0.385
						4" Ice 13.679	14.024	0.874
(2) RBS 6601 (AT&T-P)	C	From Leg	4.000	0.000	100.000	No Ice 2.942	1.190	0.055
			0.000			1/2" Ice 3.172	1.351	0.074
			0.000			1" Ice 3.410	1.521	0.097
						2" Ice 3.913	1.887	0.151
						4" Ice 5.023	2.721	0.302
(2) RBS 6601 (AT&T-P)	B	From Leg	4.000	0.000	100.000	No Ice 2.942	1.190	0.055
			0.000			1/2" Ice 3.172	1.351	0.074
			0.000			1" Ice 3.410	1.521	0.097
						2" Ice 3.913	1.887	0.151
						4" Ice 5.023	2.721	0.302
(2) RBS 6601 (AT&T-P)	A	From Leg	4.000	0.000	100.000	No Ice 2.942	1.190	0.055
			0.000			1/2" Ice 3.172	1.351	0.074
			0.000			1" Ice 3.410	1.521	0.097
						2" Ice 3.913	1.887	0.151
						4" Ice 5.023	2.721	0.302
DC6-48-60-18-8F (AT&T-P)	C	From Leg	4.000	0.000	100.000	No Ice 2.567	4.317	0.019
			0.000			1/2" Ice 2.798	4.596	0.050
			0.000			1" Ice 3.038	4.885	0.085
						2" Ice 3.543	5.488	0.167
						4" Ice 4.658	6.797	0.383
Platform Mount [LP 601-1] (E)	C	None		0.000	99.500	No Ice 28.470	28.470	1.122
						1/2" Ice 33.590	33.590	1.514
						1" Ice 38.710	38.710	1.905
						2" Ice 48.950	48.950	2.689
						4" Ice 69.430	69.430	4.255
*/*								
(2) LPA-80080/4CF w/Mount Pipe (Verizon-E)	C	From Leg	4.000	15.000	90.000	No Ice 3.110	7.482	0.034
			0.000			1/2" Ice 3.585	8.378	0.080
			0.000			1" Ice 4.022	9.152	0.137
						2" Ice 5.013	10.752	0.270
						4" Ice 7.153	14.168	0.651
(2) LPA-80063/4CF w/ Mount Pipe (Verizon-E)	B	From Leg	4.000	15.000	90.000	No Ice 7.248	7.260	0.038
			0.000			1/2" Ice 7.719	7.957	0.102
			0.000			1" Ice 8.200	8.672	0.175

<b>tnxTower</b>  <b>B&amp;T Engineering, Inc.</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 84436.000.0001 - East Hartford Hochanum, CT (USID# 4539)	<b>Page</b> 6 of 14
	<b>Project</b> 99.4' Monopole / AT&T Co-Locate	<b>Date</b> 10:32:19 05/29/12
	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>1</sub> Front	C <sub>A</sub> A <sub>1</sub> Side	Weight	
			Horz	Lateral Vert						°
(2) LPA-80063/4CF w/ Mount Pipe (Verizon-E)	A	From Leg	4.000	0.000	15.000	90.000	2" Ice	9.195	10.156	0.344
							4" Ice	11.320	13.391	0.796
							No Ice	7.248	7.260	0.038
							1/2" Ice	7.719	7.957	0.102
							1" Ice	8.200	8.672	0.175
							2" Ice	9.195	10.156	0.344
(2) LPA-185063/8CF w/ Mount Pipe (Verizon-E)	C	From Leg	4.000	0.000	15.000	90.000	4" Ice	11.320	13.391	0.796
							No Ice	3.277	3.904	0.027
							1/2" Ice	3.679	4.507	0.060
							1" Ice	4.103	5.142	0.102
							2" Ice	4.983	6.524	0.204
							4" Ice	6.880	9.560	0.511
(2) LPA-185063/8CF w/ Mount Pipe (Verizon-E)	B	From Leg	4.000	0.000	15.000	90.000	No Ice	3.277	3.904	0.027
							1/2" Ice	3.679	4.507	0.060
							1" Ice	4.103	5.142	0.102
							2" Ice	4.983	6.524	0.204
							4" Ice	6.880	9.560	0.511
							No Ice	3.277	3.904	0.027
(2) LPA-185063/8CF w/ Mount Pipe (Verizon-E)	A	From Leg	4.000	0.000	15.000	90.000	1/2" Ice	3.679	4.507	0.060
							1" Ice	4.103	5.142	0.102
							2" Ice	4.983	6.524	0.204
							4" Ice	6.880	9.560	0.511
							No Ice	3.277	3.904	0.027
							1/2" Ice	3.679	4.507	0.060
Platform Mount [LP 304-1] (E)	C	None	0.000	0.000	88.500	No Ice	17.460	17.460	1.349	
						1/2" Ice	22.440	22.440	1.625	
						1" Ice	27.420	27.420	1.900	
						2" Ice	37.380	37.380	2.451	
						4" Ice	57.300	57.300	3.554	
						No Ice	5.429	3.382	0.051	
LLPX310R-V4 w/Mount Pipe (Clearwire-E)	C	From Leg	2.000	0.000	60.000	81.000	1/2" Ice	5.990	4.151	0.090
							1" Ice	6.506	4.796	0.139
							2" Ice	7.574	6.194	0.255
							4" Ice	9.862	9.254	0.597
							No Ice	5.429	3.382	0.051
							1/2" Ice	5.990	4.151	0.090
LLPX310R-V4 w/Mount Pipe (Clearwire-E)	B	From Leg	2.000	0.000	50.000	81.000	1" Ice	6.506	4.796	0.139
							2" Ice	7.574	6.194	0.255
							4" Ice	9.862	9.254	0.597
							No Ice	5.429	3.382	0.051
							1/2" Ice	5.990	4.151	0.090
							1" Ice	6.506	4.796	0.139
LLPX310R-V4 w/Mount Pipe (Clearwire-E)	A	From Leg	2.000	0.000	70.000	81.000	2" Ice	7.574	6.194	0.255
							4" Ice	9.862	9.254	0.597
							No Ice	5.429	3.382	0.051
							1/2" Ice	5.990	4.151	0.090
							1" Ice	6.506	4.796	0.139
							2" Ice	7.574	6.194	0.255
RRH-2WB0 (Clearwire-E)	C	From Leg	2.000	0.000	0.000	81.000	4" Ice	9.862	9.254	0.597
							No Ice	2.689	0.851	0.044
							1/2" Ice	2.912	1.012	0.059
							1" Ice	3.144	1.182	0.077
							2" Ice	3.634	1.548	0.121
							4" Ice	4.717	2.385	0.250
RRH-2WB0 (Clearwire-E)	C	From Leg	2.000	0.000	0.000	81.000	No Ice	2.689	0.851	0.044
							1/2" Ice	2.912	1.012	0.059
							1" Ice	3.144	1.182	0.077
							2" Ice	3.634	1.548	0.121
							4" Ice	4.717	2.385	0.250
							No Ice	2.689	0.851	0.044
RRH-2WB0 (Clearwire-E)	C	From Leg	2.000	0.000	0.000	81.000	1/2" Ice	2.912	1.012	0.059
							1" Ice	3.144	1.182	0.077
							2" Ice	3.634	1.548	0.121
							4" Ice	4.717	2.385	0.250
							No Ice	2.689	0.851	0.044
							1/2" Ice	2.912	1.012	0.059

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	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A		Weight
			Horz	Lateral			Front	Side	
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
18"x17"x11" TMA (Clearwire-E)	C	From Leg	2.000		0.000	81.000	4" Ice 4.717	2.385	0.250
			0.000				No Ice 2.975	1.925	0.010
			0.000				1/2" Ice 3.206	2.117	0.034
							1" Ice 3.446	2.318	0.061
							2" Ice 3.952	2.746	0.126
6' x 2" Mount Pipe (Clearwire-E)	C	From Leg	2.000		0.000	79.000	4" Ice 5.066	3.705	0.301
			0.000				No Ice 1.425	1.425	0.022
			0.000				1/2" Ice 1.925	1.925	0.033
							1" Ice 2.294	2.294	0.048
							2" Ice 3.060	3.060	0.090
6' x 2" Mount Pipe (Clearwire-E)	B	From Leg	2.000		0.000	79.000	4" Ice 4.702	4.702	0.231
			0.000				No Ice 1.425	1.425	0.022
			0.000				1/2" Ice 1.925	1.925	0.033
							1" Ice 2.294	2.294	0.048
							2" Ice 3.060	3.060	0.090
6' x 2" Mount Pipe (Clearwire-E)	A	From Leg	2.000		0.000	79.000	4" Ice 4.702	4.702	0.231
			0.000				No Ice 1.425	1.425	0.022
			0.000				1/2" Ice 1.925	1.925	0.033
							1" Ice 2.294	2.294	0.048
							2" Ice 3.060	3.060	0.090
Side Arm Mount [SO 103-3] (E)	C	None			0.000	79.000	4" Ice 4.702	4.702	0.231
							No Ice 9.500	9.500	0.224
							1/2" Ice 11.800	11.800	0.317
							1" Ice 14.100	14.100	0.410
							2" Ice 18.700	18.700	0.596
						4" Ice 27.900	27.900	0.968	

\*/\*

## Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight
				Horz	Lateral						
				ft	ft	°	°	ft	ft	ft <sup>2</sup>	K
VHLP2.5-18-DW1 (E)	C	Paraboloid w/Shroud (HP)	From Leg	2.000		0.000		81.000	2.917	No Ice 6.681	0.048
				0.000						1/2" Ice 7.069	0.077
				0.000						1" Ice 7.456	0.106
										2" Ice 8.230	0.164
										4" Ice 9.779	0.280

\*/\*

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	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

## Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

## Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	99.42 - 77.08	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-12.211	1.139	-0.765
			Max. Mx	11	-5.334	129.927	0.924
			Max. My	8	-5.320	-0.740	-132.949
			Max. Vy	5	9.527	-128.852	-1.562
			Max. Vx	2	-9.611	1.702	132.281
			Max. Torque	13			1.799
L2	77.08 - 40.42	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-18.589	0.963	-0.889
			Max. Mx	5	-9.711	-528.899	0.891
			Max. My	8	-9.705	1.727	-535.538



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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L3	40.42 - 0	Pole	Max. Vy	5	12.146	-528.899	0.891
			Max. Vx	2	-12.230	-2.814	535.319
			Max. Torque	13			1.798
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-27.642	0.703	-1.039
			Max. Mx	5	-16.753	-1120.570	3.922
			Max. My	2	-16.752	-8.418	1130.600
			Max. Vy	5	14.416	-1120.570	3.922
			Max. Vx	2	-14.497	-8.418	1130.600
			Max. Torque	13			1.779

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	21	27.642	0.018	-4.219
	Max. H <sub>x</sub>	11	16.764	14.343	-0.050
	Max. H <sub>z</sub>	2	16.764	-0.124	14.483
	Max. M <sub>x</sub>	2	1130.600	-0.124	14.483
	Max. M <sub>z</sub>	5	1120.570	-14.402	0.068
	Max. Torsion	13	1.760	7.184	12.509
	Min. Vert	1	16.764	0.000	0.000
	Min. H <sub>x</sub>	5	16.764	-14.402	0.068
	Min. H <sub>z</sub>	8	16.764	0.067	-14.470
	Min. M <sub>x</sub>	8	-1130.268	0.067	-14.470
	Min. M <sub>z</sub>	11	-1116.641	14.343	-0.050
	Min. Torsion	7	-1.755	-7.138	-12.536

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	16.764	0.000	0.000	0.378	0.480	0.000
Dead+Wind 0 deg - No Ice	16.764	0.124	-14.483	-1130.600	-8.418	-1.524
Dead+Wind 30 deg - No Ice	16.764	7.260	-12.558	-979.699	-563.767	-1.085
Dead+Wind 60 deg - No Ice	16.764	12.478	-7.273	-566.607	-970.190	-0.386
Dead+Wind 90 deg - No Ice	16.764	14.402	-0.068	-3.922	-1120.570	0.415
Dead+Wind 120 deg - No Ice	16.764	12.485	7.134	558.171	-972.053	1.133
Dead+Wind 150 deg - No Ice	16.764	7.138	12.536	979.928	-555.972	1.755
Dead+Wind 180 deg - No Ice	16.764	-0.067	14.470	1130.268	4.696	1.651
Dead+Wind 210 deg - No Ice	16.764	-7.215	12.516	976.971	560.990	1.123
Dead+Wind 240 deg - No Ice	16.764	-12.428	7.244	564.959	966.973	0.391
Dead+Wind 270 deg - No Ice	16.764	-14.343	0.050	3.194	1116.641	-0.448
Dead+Wind 300 deg - No Ice	16.764	-12.445	-7.177	-560.917	969.728	-1.265
Dead+Wind 330 deg - No Ice	16.764	-7.184	-12.509	-976.987	560.709	-1.760
Dead+Ice+Temp	27.642	-0.000	0.000	1.039	0.703	-0.000
Dead+Wind 0 deg+Ice+Temp	27.642	0.033	-4.222	-337.722	-1.686	-0.356
Dead+Wind 30 deg+Ice+Temp	27.642	2.118	-3.661	-292.567	-168.539	-0.218
Dead+Wind 60 deg+Ice+Temp	27.642	3.642	-2.121	-168.837	-290.610	-0.028
Dead+Wind 90 deg+Ice+Temp	27.642	4.203	-0.019	-0.174	-335.646	0.170
Dead+Wind 120 deg+Ice+Temp	27.642	3.642	2.083	168.379	-290.930	0.328

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Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead+Wind 150 deg+Ice+Temp	27.642	2.084	3.654	294.429	-166.286	0.451
Dead+Wind 180 deg+Ice+Temp	27.642	-0.018	4.219	339.596	1.962	0.389
Dead+Wind 210 deg+Ice+Temp	27.642	-2.106	3.651	293.829	169.054	0.226
Dead+Wind 240 deg+Ice+Temp	27.642	-3.630	2.113	170.374	291.012	0.028
Dead+Wind 270 deg+Ice+Temp	27.642	-4.188	0.014	1.947	335.867	-0.178
Dead+Wind 300 deg+Ice+Temp	27.642	-3.632	-2.094	-167.120	291.561	-0.361
Dead+Wind 330 deg+Ice+Temp	27.642	-2.096	-3.647	-291.721	168.716	-0.452
Dead+Wind 0 deg - Service	16.764	0.048	-5.657	-441.619	-2.984	-0.596
Dead+Wind 30 deg - Service	16.764	2.836	-4.906	-382.644	-220.023	-0.426
Dead+Wind 60 deg - Service	16.764	4.874	-2.841	-221.199	-378.858	-0.152
Dead+Wind 90 deg - Service	16.764	5.626	-0.027	-1.293	-437.628	0.162
Dead+Wind 120 deg - Service	16.764	4.877	2.787	218.381	-379.586	0.444
Dead+Wind 150 deg - Service	16.764	2.788	4.897	383.211	-216.977	0.689
Dead+Wind 180 deg - Service	16.764	-0.026	5.652	441.967	2.141	0.647
Dead+Wind 210 deg - Service	16.764	-2.818	4.889	382.054	219.548	0.440
Dead+Wind 240 deg - Service	16.764	-4.855	2.830	221.031	378.210	0.153
Dead+Wind 270 deg - Service	16.764	-5.603	0.019	1.487	436.701	-0.176
Dead+Wind 300 deg - Service	16.764	-4.861	-2.804	-218.975	379.288	-0.495
Dead+Wind 330 deg - Service	16.764	-2.806	-4.886	-381.583	219.440	-0.689

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.000	-16.764	0.000	0.000	16.764	0.000	0.000%
2	0.124	-16.764	-14.483	-0.124	16.764	14.483	0.000%
3	7.260	-16.764	-12.558	-7.260	16.764	12.558	0.000%
4	12.478	-16.764	-7.273	-12.478	16.764	7.273	0.000%
5	14.402	-16.764	-0.068	-14.402	16.764	0.068	0.000%
6	12.485	-16.764	7.134	-12.485	16.764	-7.134	0.000%
7	7.138	-16.764	12.536	-7.138	16.764	-12.536	0.000%
8	-0.067	-16.764	14.470	0.067	16.764	-14.470	0.000%
9	-7.215	-16.764	12.516	7.215	16.764	-12.516	0.000%
10	-12.428	-16.764	7.244	12.428	16.764	-7.244	0.000%
11	-14.343	-16.764	0.050	14.343	16.764	-0.050	0.000%
12	-12.445	-16.764	-7.177	12.445	16.764	7.177	0.000%
13	-7.184	-16.764	-12.509	7.184	16.764	12.509	0.000%
14	0.000	-27.642	0.000	0.000	27.642	-0.000	0.000%
15	0.033	-27.642	-4.222	-0.033	27.642	4.222	0.000%
16	2.118	-27.642	-3.661	-2.118	27.642	3.661	0.000%
17	3.642	-27.642	-2.121	-3.642	27.642	2.121	0.000%
18	4.203	-27.642	-0.019	-4.203	27.642	0.019	0.000%
19	3.642	-27.642	2.083	-3.642	27.642	-2.083	0.000%
20	2.084	-27.642	3.654	-2.084	27.642	-3.654	0.000%
21	-0.018	-27.642	4.219	0.018	27.642	-4.219	0.000%
22	-2.106	-27.642	3.651	2.106	27.642	-3.651	0.000%
23	-3.630	-27.642	2.113	3.630	27.642	-2.113	0.000%
24	-4.188	-27.642	0.014	4.188	27.642	-0.014	0.000%
25	-3.632	-27.642	-2.094	3.632	27.642	2.094	0.000%
26	-2.096	-27.642	-3.647	2.096	27.642	3.647	0.000%
27	0.048	-16.764	-5.657	-0.048	16.764	5.657	0.000%
28	2.836	-16.764	-4.906	-2.836	16.764	4.906	0.000%
29	4.874	-16.764	-2.841	-4.874	16.764	2.841	0.000%
30	5.626	-16.764	-0.027	-5.626	16.764	0.027	0.000%
31	4.877	-16.764	2.787	-4.877	16.764	-2.787	0.000%
32	2.788	-16.764	4.897	-2.788	16.764	-4.897	0.000%
33	-0.026	-16.764	5.652	0.026	16.764	-5.652	0.000%

<b>tnxTower</b>  <b>B&amp;T Engineering, Inc.</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 84436.000.0001 - East Hartford Hochanum, CT (USID# 4539)	<b>Page</b> 11 of 14
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	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
34	-2.818	-16.764	4.889	2.818	16.764	-4.889	0.000%
35	-4.855	-16.764	2.830	4.855	16.764	-2.830	0.000%
36	-5.603	-16.764	0.019	5.603	16.764	-0.019	0.000%
37	-4.861	-16.764	-2.804	4.861	16.764	2.804	0.000%
38	-2.806	-16.764	-4.886	2.806	16.764	4.886	0.000%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	5	0.00000001	0.00002688
3	Yes	5	0.00000001	0.00013102
4	Yes	5	0.00000001	0.00014441
5	Yes	4	0.00000001	0.00024373
6	Yes	5	0.00000001	0.00015182
7	Yes	5	0.00000001	0.00012630
8	Yes	5	0.00000001	0.00003239
9	Yes	5	0.00000001	0.00015384
10	Yes	5	0.00000001	0.00013560
11	Yes	4	0.00000001	0.00032526
12	Yes	5	0.00000001	0.00012958
13	Yes	5	0.00000001	0.00016173
14	Yes	4	0.00000001	0.00000001
15	Yes	5	0.00000001	0.00009302
16	Yes	5	0.00000001	0.00011452
17	Yes	5	0.00000001	0.00011502
18	Yes	5	0.00000001	0.00009119
19	Yes	5	0.00000001	0.00011758
20	Yes	5	0.00000001	0.00011516
21	Yes	5	0.00000001	0.00009417
22	Yes	5	0.00000001	0.00011900
23	Yes	5	0.00000001	0.00011646
24	Yes	5	0.00000001	0.00009185
25	Yes	5	0.00000001	0.00011473
26	Yes	5	0.00000001	0.00011964
27	Yes	4	0.00000001	0.00024441
28	Yes	4	0.00000001	0.00045606
29	Yes	4	0.00000001	0.00054765
30	Yes	4	0.00000001	0.00006240
31	Yes	4	0.00000001	0.00061723
32	Yes	4	0.00000001	0.00044864
33	Yes	4	0.00000001	0.00027454
34	Yes	4	0.00000001	0.00063381
35	Yes	4	0.00000001	0.00048576
36	Yes	4	0.00000001	0.00007195
37	Yes	4	0.00000001	0.00045400
38	Yes	4	0.00000001	0.00070143

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**Maximum Tower Deflections - Service Wind**

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	99.42 - 77.08	15.453	33	1.241	0.007
L2	80.58 - 40.42	10.681	33	1.152	0.005
L3	44.503 - 0	3.444	33	0.694	0.002

**Critical Deflections and Radius of Curvature - Service Wind**

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
105.000	Beacon	33	15.453	1.241	0.007	30537
103.000	(2) RA21.7770.00 w/ Mount Pipe	33	15.453	1.241	0.007	30537
102.000	AM-X-CD-16-65-00T-RET w/ Mount Pipe	33	15.453	1.241	0.007	30537
100.000	(2) RBS 6601	33	15.453	1.241	0.007	30537
99.500	Platform Mount [LP 601-1]	33	15.453	1.241	0.007	30537
90.000	(2) LPA-80080/4CF w/Mount Pipe	33	13.034	1.206	0.006	16209
88.500	Platform Mount [LP 304-1]	33	12.653	1.199	0.006	13982
81.000	VHLP2.5-18-DW1	33	10.784	1.155	0.005	8295
79.000	6' x 2" Mount Pipe	33	10.297	1.139	0.005	7492

**Maximum Tower Deflections - Design Wind**

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	99.42 - 77.08	39.484	8	3.171	0.018
L2	80.58 - 40.42	27.296	8	2.943	0.013
L3	44.503 - 0	8.807	2	1.775	0.005

**Critical Deflections and Radius of Curvature - Design Wind**

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
105.000	Beacon	8	39.484	3.171	0.018	12040
103.000	(2) RA21.7770.00 w/ Mount Pipe	8	39.484	3.171	0.018	12040
102.000	AM-X-CD-16-65-00T-RET w/ Mount Pipe	8	39.484	3.171	0.018	12040
100.000	(2) RBS 6601	8	39.484	3.171	0.018	12040
99.500	Platform Mount [LP 601-1]	8	39.484	3.171	0.018	12040
90.000	(2) LPA-80080/4CF w/Mount Pipe	8	33.306	3.081	0.016	6390
88.500	Platform Mount [LP 304-1]	8	32.333	3.064	0.015	5512
81.000	VHLP2.5-18-DW1	8	27.558	2.951	0.014	3269
79.000	6' x 2" Mount Pipe	8	26.316	2.912	0.013	2951

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	<b>Project</b> 99.4' Monopole / AT&T Co-Locate	<b>Date</b> 10:32:19 05/29/12
	<b>Client</b> Nexlink	<b>Designed by</b> K. Mears

### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>n</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
L1	99.42 - 77.08 (1)	TP28.38x25.32x0.188	22.340	0.000	0.0	36.000	16.493	-5.320	593.739	0.009
L2	77.08 - 40.42 (2)	TP33.47x27.526x0.25	40.160	0.000	0.0	36.000	25.881	-9.705	931.698	0.010
L3	40.42 - 0 (3)	TP39.09x32.366x0.313	44.503	0.000	0.0	36.000	38.462	-16.752	1384.650	0.012

### Pole Bending Design Data

Section No.	Elevation ft	Size	Actual M <sub>x</sub> kip-ft	Actual f <sub>bx</sub> ksi	Allow. F <sub>bx</sub> ksi	Ratio $\frac{f_{bx}}{F_{bx}}$	Actual M <sub>y</sub> kip-ft	Actual f <sub>by</sub> ksi	Allow. F <sub>by</sub> ksi	Ratio $\frac{f_{by}}{F_{by}}$
L1	99.42 - 77.08 (1)	TP28.38x25.32x0.188	132.952	14.130	36.000	0.393	0.000	0.000	36.000	0.000
L2	77.08 - 40.42 (2)	TP33.47x27.526x0.25	535.541	30.847	36.000	0.857	0.000	0.000	36.000	0.000
L3	40.42 - 0 (3)	TP39.09x32.366x0.313	1130.63	36.872	36.000	1.024	0.000	0.000	36.000	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V K	Actual f <sub>v</sub> ksi	Allow. F <sub>v</sub> ksi	Ratio $\frac{f_v}{F_v}$	Actual T kip-ft	Actual f <sub>vt</sub> ksi	Allow. F <sub>vt</sub> ksi	Ratio $\frac{f_{vt}}{F_{vt}}$
L1	99.42 - 77.08 (1)	TP28.38x25.32x0.188	9.598	0.582	24.000	0.049	1.715	0.089	24.000	0.004
L2	77.08 - 40.42 (2)	TP33.47x27.526x0.25	12.217	0.472	24.000	0.039	1.687	0.047	24.000	0.002
L3	40.42 - 0 (3)	TP39.09x32.366x0.313	14.497	0.377	24.000	0.031	1.525	0.024	24.000	0.001

### Pole Interaction Design Data

Section No.	Elevation ft	Ratio $\frac{P}{P_a}$	Ratio $\frac{f_{bx}}{F_{bx}}$	Ratio $\frac{f_{by}}{F_{by}}$	Ratio $\frac{f_v}{F_v}$	Ratio $\frac{f_{vt}}{F_{vt}}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	99.42 - 77.08 (1)	0.009	0.393	0.000	0.049	0.004	0.402	1.333	H1-3+VT ✓
L2	77.08 - 40.42 (2)	0.010	0.857	0.000	0.039	0.002	0.868	1.333	H1-3+VT ✓
L3	40.42 - 0 (3)	0.012	1.024	0.000	0.031	0.001	1.037	1.333	H1-3+VT ✓

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**Section Capacity Table**

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
L1	99.42 - 77.08	Pole	TP28.38x25.32x0.188	1	-5.320	791.454	30.2	Pass
L2	77.08 - 40.42	Pole	TP33.47x27.526x0.25	2	-9.705	1241.953	65.1	Pass
L3	40.42 - 0	Pole	TP39.09x32.366x0.313	3	-16.752	1845.738	77.8	Pass
Summary								
Pole (L3)							77.8	Pass
<b>RATING =</b>							<b>77.8</b>	<b>Pass</b>

## Square, Stiffened / Unstiffened Base Plate, Any Rod Material - Rev. F / G

- Assumptions:**
- 1) Rod groups at corners. Total # rods divisible by 4. Maximum total # of rods = 48 (12 per Corner).
  - 2) Rod Spacing = Straight Center-to-Center distance between any (2) adjacent rods (same corner)
  - 3) Clear space between bottom of leveling nut and top of concrete **not** exceeding  $(1) \times (\text{Rod Diameter})$

### Site Data

Site#: 4539
Site Name: East Hartford Hohanum, C

### Anchor Rod Data

Qty:	8	
Diam:	2.25	in
Rod Material:	A615-J	
Yield, Fy:	75	ksi
Strength, Fu:	100	ksi
Bolt Circle:	44.09	in
Anchor Spacing:	6	in

### Plate Data

W=Side:	44	in
Thick:	2.75	in
Grade:	50	ksi
Clip Distance:	6	in

### Stiffener Data (Welding at both sides)

Configuration:	Unstiffened	
Weld Type:		**
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

### Pole Data

Diam:	39.09	in
Thick:	0.3125	in
Grade:	60	ksi
# of Sides:	18	"0" IF Round

### Stress Increase Factor

ASD ASIF:	1.333
-----------	-------

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

### Base Reactions

TIA Revision:	F	
Unfactored Moment, M:	1131	ft-kips
Unfactored Axial, P:	17	kips
Unfactored Shear, V:	14	kips

### Anchor Rod Results

TIA F --> Maximum Rod Tension	151.8 Kips
Allowable Tension:	195.0 Kips
Anchor Rod Stress Ratio:	77.9% Pass

### Base Plate Results

Base Plate Stress:	24.3 ksi	Flexural Check
Allowable PL Bending Stress:	50.0 ksi	
Base Plate Stress Ratio:	48.7% Pass	

### PL Ref. Data

Yield Line (in):	23.14
Max PL Length:	23.14

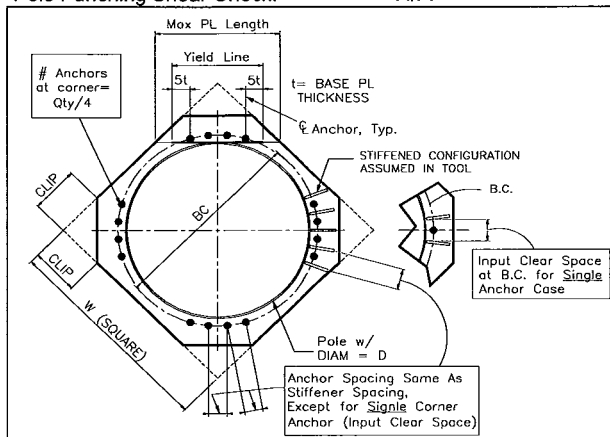
### N/A - Unstiffened

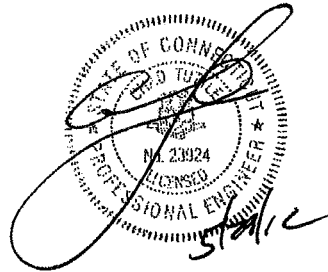
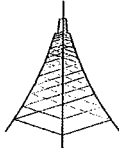
### Stiffener Results

Horizontal Weld :	N/A
Vertical Weld:	N/A
Plate Flex+Shear, $f_b/F_b + (f_v/F_v)^2$ :	N/A
Plate Tension+Shear, $f_t/F_t + (f_v/F_v)^2$ :	N/A
Plate Comp. (AISC Bracket):	N/A

### Pole Results

Pole Punching Shear Check:	N/A
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**Letter of Explanation (LOE)**  
**MUST be attached to any Structural Analysis**

**Site Name** EAST HARTFORD HOCHANUM  
**Site Number** 4539 (CT6126)  
**PE of Record** Chad E. Tuttle, P.E.

ALL STRUCTURES	Statement in COL A is Correct	Value from Col A	N/A	Alternate Value / Concept Used	Explanation	Yes	No	N/A	Comments / References
Structure Analyzed to F Code	X								
<i>Note: ALL G analysis MUST be justified. A simple notation of jurisdiction equipment will suffice. FULL TOWERS in G Code jurisdictions MUST have the new "5% Grace" Test Applied. G to be applied ONLY where this is exceeded. This 5% test applies to "like for like" only</i>									
Guy Tensions Adjusted Within Code to Find Optimum Tension / Minimum Reinforcement (Applies to Guyed Tower Failures Only). Note : AT&T requires a pulse chart for altered Tensions			X						
Antenna Azimuths Inputted Per AT&T Information. NOTE that new antennas should be calculated at 0 degrees to allow flexibility.	X								
All Yield Stresses > = 60 ksi (legs)			X		Monopole; Shaft = 60 ksi				
All Yield Stresses > = 25 ksi (Diagonals and Horizontals)			X		Monopole				
Structures Designated Class II (G Only)			X						
Exposure B Rating Used (Topography)			X						
K value for Slenderness ratio < 1.0			X		Monopole				
Shielding of All Apertures Used when Appropriate PER 2.6.9.4 (G Code Only)			X						
0.75 Reduction "Shape" Factor (Figure 2.6) for platform mounts, 0.8 for T-Boom Mounts Used (G Only)			X						
Pipes and round Members have 1.0 Drag Factors. Note If Pipe is attached to flat antenna, these must be considered separately if differing Drag factors are Used		X			In compliance with the TIA-222-F Table 3				
Are Tower Diagonals Designed as "Tension Only"			X		Monopole				







**PROJECT INFORMATION**

SCOPE OF WORK: TELECOMMUNICATIONS FACILITY UPGRADE (LTE):  
 1. INSTALL (3) NEW LTE ANTENNAS, (6) RRH'S, SURGE ARRESTOR, (1) FIBER LINE (2) DC POWER LINES & (1) GPS ANTENNA.  
 2. INSTALL LTE 6601 CABINET

SITE ADDRESS: 223 BRAINARD ROAD  
 EAST HARTFORD, CT 06114

LATITUDE: 41.7328 N 41° 43' 58.08" N  
 LONGITUDE: 72.6619 W 72° 39' 42.84" W  
 JURISDICTION: NATIONAL, STATE & LOCAL CODES OR ORDINANCES  
 CURRENT USE: TELECOMMUNICATIONS FACILITY  
 PROPOSED USE: TELECOMMUNICATIONS FACILITY



**SITE NUMBER: CT5126**  
**SITE NAME: AWE - EAST HARTFORD HOCHANUM**

**DRAWING INDEX**

**REV**

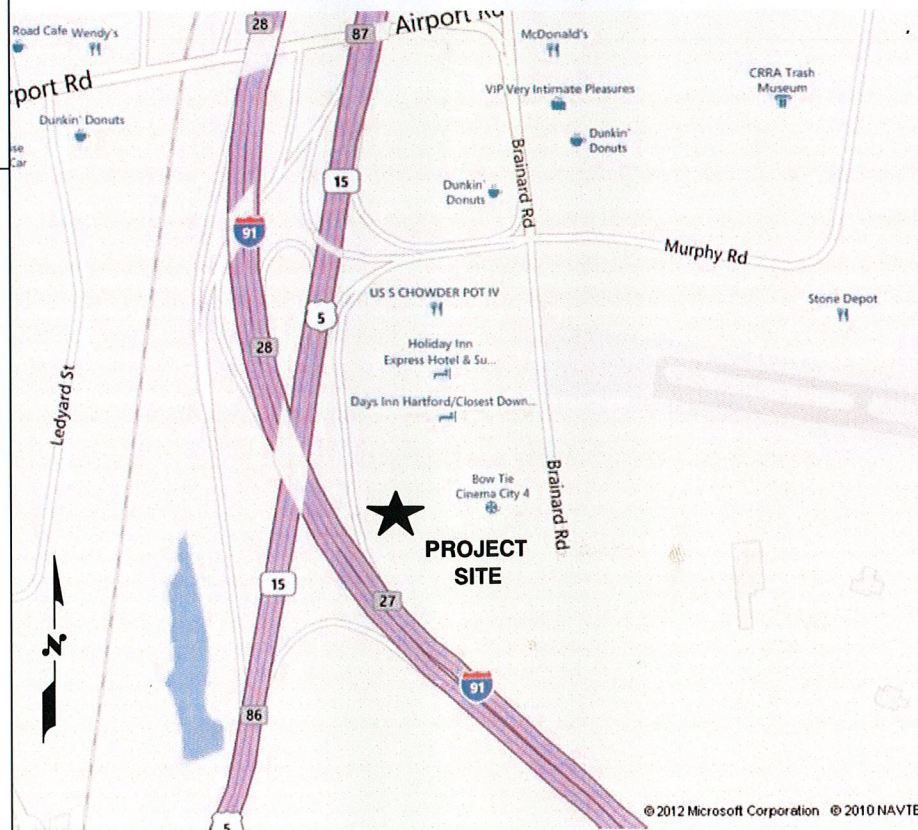
**VICINITY MAP**

**GENERAL NOTES**

- T-1 TITLE SHEET
- GN-1 GENERAL NOTES
- A-1 COMPOUND & EQUIPMENT PLAN
- A-2 ANTENNA LAYOUT AND ELEVATION
- A-3 DETAILS
- G-1 PLUMBING DIAGRAM & GROUNDING DETAILS

- 1
- 1
- 1
- 1
- 1
- 1

DIRECTIONS TO SITE:  
 DEPART ENTERPRISE DR TOWARD CAPITOL BLVD 0.4 MI TURN LEFT ONTO CAPITOL BLVD 0.2 MI TURN LEFT ONTO WEST ST 0.2 MI TAKE RAMP LEFT FOR I-91 NORTH 6.6 MI AT EXIT 27, TAKE RAMP RIGHT FOR BRAINARD RD TOWARD BRAINARD AIRPORT / AIRPORT RD 0.5 MI TURN RIGHT ONTO BRAINARD RD 0.2 MI ARRIVE AT 223 BRAINARD RD, HARTFORD, CT 06114



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2. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
3. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.

72 HOURS  
 BEFORE YOU DIG   
 CALL TOLL FREE 800-922-4455

UNDERGROUND SERVICE ALERT

1600 OSGOOD STREET  
 BUILDING 20 NORTH, SUITE 2-101  
 N. ANDOVER, MA 01845  
 TEL: (978) 557-5553  
 FAX: (978) 336-5586

a UniTek GLOBAL SERVICES company  
 800 MARSHALL PHELPS ROAD UNIT#: 2A  
 WINDSOR, CT 06095

**SITE NUMBER: CT5126**  
**SITE NAME: AWE - EAST HARTFORD HOCHANUM**  
 223 BRAINARD ROAD  
 EAST HARTFORD, CT 06114  
 HARTFORD COUNTY

500 ENTERPRISE DRIVE, SUITE 3A  
 ROCKY HILL, CT 06067

NO.		DATE	REVISIONS	BY	CHK	APP	JOB NUMBER		DRAWING NUMBER		REV
1	04/18/12		ISSUED FOR CONSTRUCTION	DB	DC	DPH	20220		T-1		1
0	03/26/12		ISSUED FOR REVIEW	DB	DC	DPH					
SCALE:		DESIGNED BY:		DRAWN BY:							
AS SHOWN		DC		DB							



AT&T  
 TITLE SHEET  
 (LTE)



**GROUNDING NOTES**

1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTNING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OFF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.
5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
7. APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR.
9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWS COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
12. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50

**GENERAL NOTES**

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:  
 CONTRACTOR - NEXLINK  
 SUBCONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION)  
 OWNER - AT&T MOBILITY
  2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.
  3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
  4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
  5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
  6. "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.
  7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
  8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
  9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
  10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
  11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
  12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
  13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.
  14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.
  15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
  16. CONSTRUCTION SHALL COMPLY WITH UMTS SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T MOBILITY SITES."
  17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
  18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
  19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.
  20. APPLICABLE BUILDING CODES:  
 SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.  
 BUILDING CODE: 2003 IBC WITH 2005 CT SUPPLEMENT & 2009 CT AMENDMENTS  
 ELECTRICAL CODE: REFER TO ELECTRICAL DRAWINGS  
 LIGHTENING CODE: REFER TO ELECTRICAL DRAWINGS
- SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:
- AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE;
  - AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC) MANUAL OF STEEL CONSTRUCTION, ASD, NINTH EDITION;
  - TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-F, STRUCTURAL STANDARDS FOR STEEL
  - ANTENNA TOWER AND ANTENNA SUPPORTING STRUCTURES; REFER TO ELECTRICAL DRAWINGS FOR SPECIFIC ELECTRICAL STANDARDS.
- FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

**ABBREVIATIONS**

AGL	ABOVE GRADE LEVEL	G.C.	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
AWG	AMERICAN WIRE GAUGE	MGB	MASTER GROUND BUS		
BCW	BARE COPPER WIRE	MIN	MINIMUM	TBD	TO BE DETERMINED
BTS	BASE TRANSCIEVER STATION	PROPOSED	NEW	TBR	TO BE REMOVED
EXISTING	EXISTING	N.T.S.	NOT TO SCALE	TBRR	TO BE REMOVED AND REPLACED
EG	EQUIPMENT GROUND	REF	REFERENCE		
EGR	EQUIPMENT GROUND RING	REQ	REQUIRED	TYP	TYPICAL

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**NEXLINK**  
 GLOBAL SERVICES  
 a UniTek GLOBAL SERVICES company  
 800 MARSHALL PHELPS ROAD UNIT#: 2A  
 WINDSOR, CT 06095

**SITE NUMBER: CT5126**  
**SITE NAME: AWE - EAST HARTFORD HOCHANUM**  
 223 BRAINARD ROAD  
 EAST HARTFORD, CT 06114  
 HARTFORD COUNTY

500 ENTERPRISE DRIVE, SUITE 3A  
 ROCKY HILL, CT 06067

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1	04/18/12	ISSUED FOR CONSTRUCTION	DB	DC	DPI
0	03/26/12	ISSUED FOR REVIEW	DB	DC	DPI
SCALE: AS SHOWN		DESIGNED BY: DC	DRAWN BY: DB		



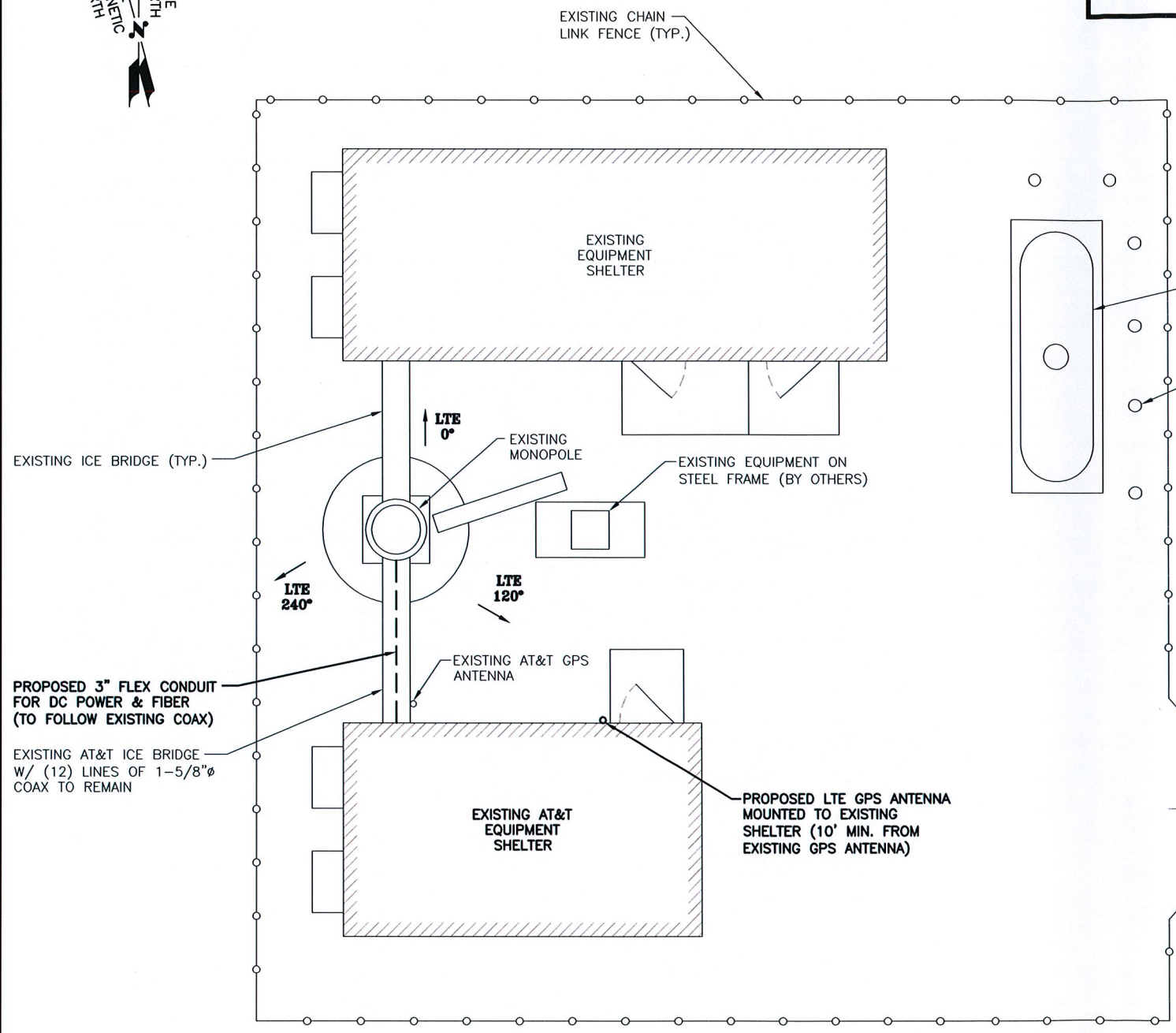
AT&T	
GENERAL NOTES (LTE)	
DRAWING NUMBER	REV
GN-1	1



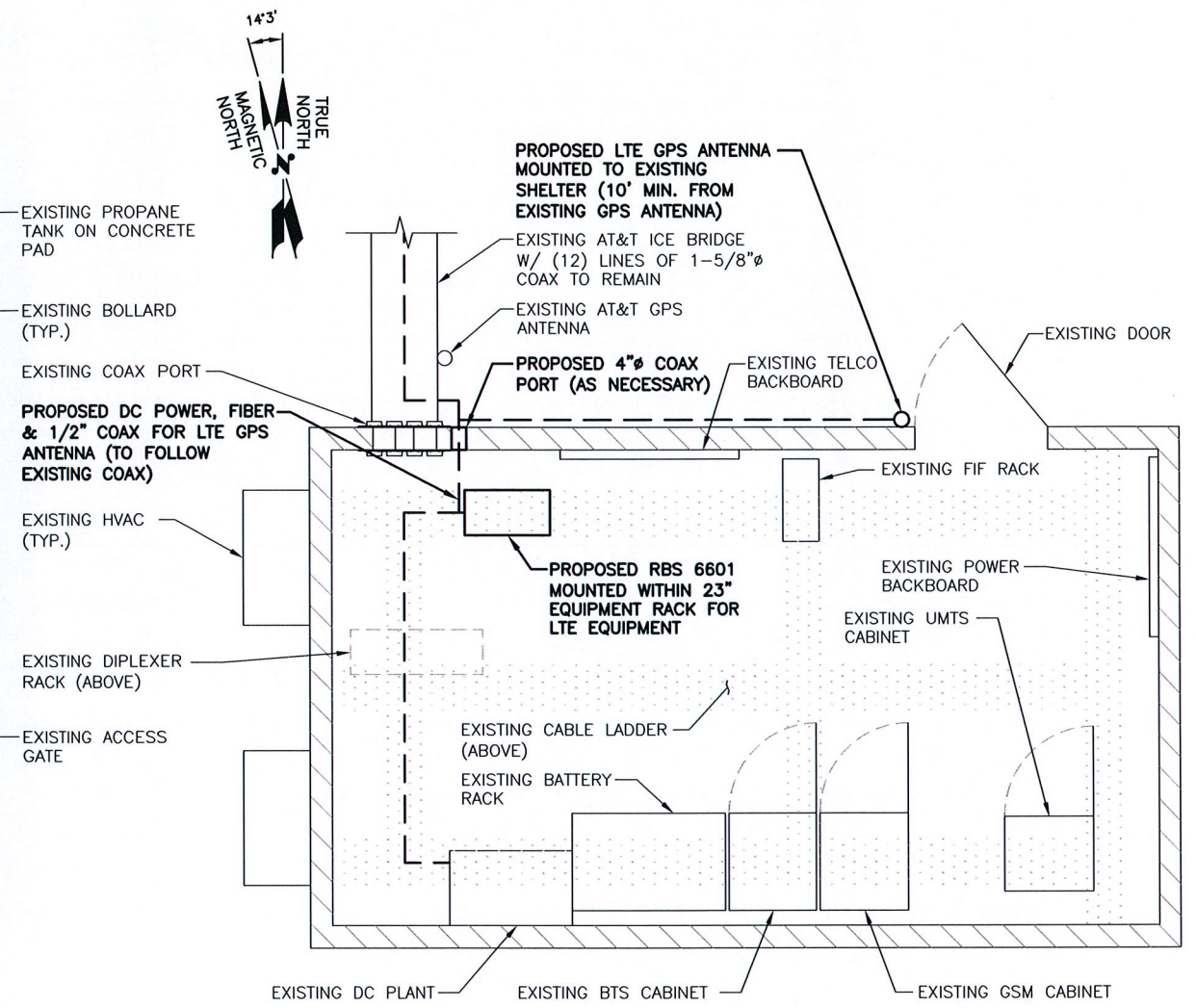


**NOTE:**  
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

**NOTE:**  
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION.



**COMPOUND PLAN**  
SCALE: 1/8"=1'-0"  
0 4'-0" 8'-0" 16'-0" 24'-0"



**EQUIPMENT PLAN**  
SCALE: 1/2"=1'-0"  
0 1'-0" 2'-0" 4'-0" 6'-0"

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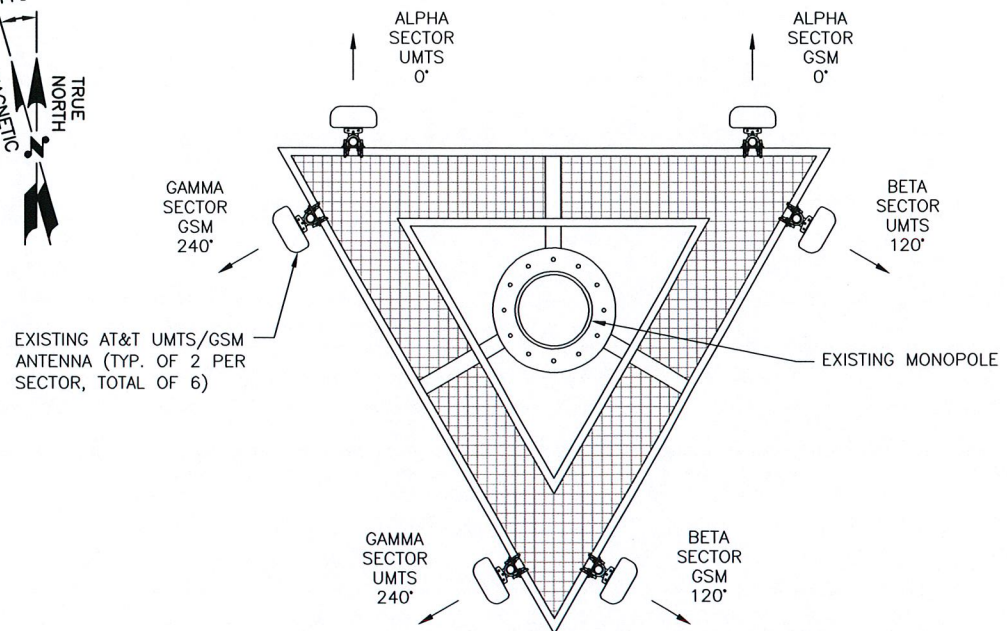
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AT&T	
COMPOUND & EQUIPMENT PLAN (LTE)	
JOB NUMBER	DRAWING NUMBER
01	A-1
REV	1





**EXISTING UMTS/GSM ANTENNA PLAN**

SCALE: N.T.S.

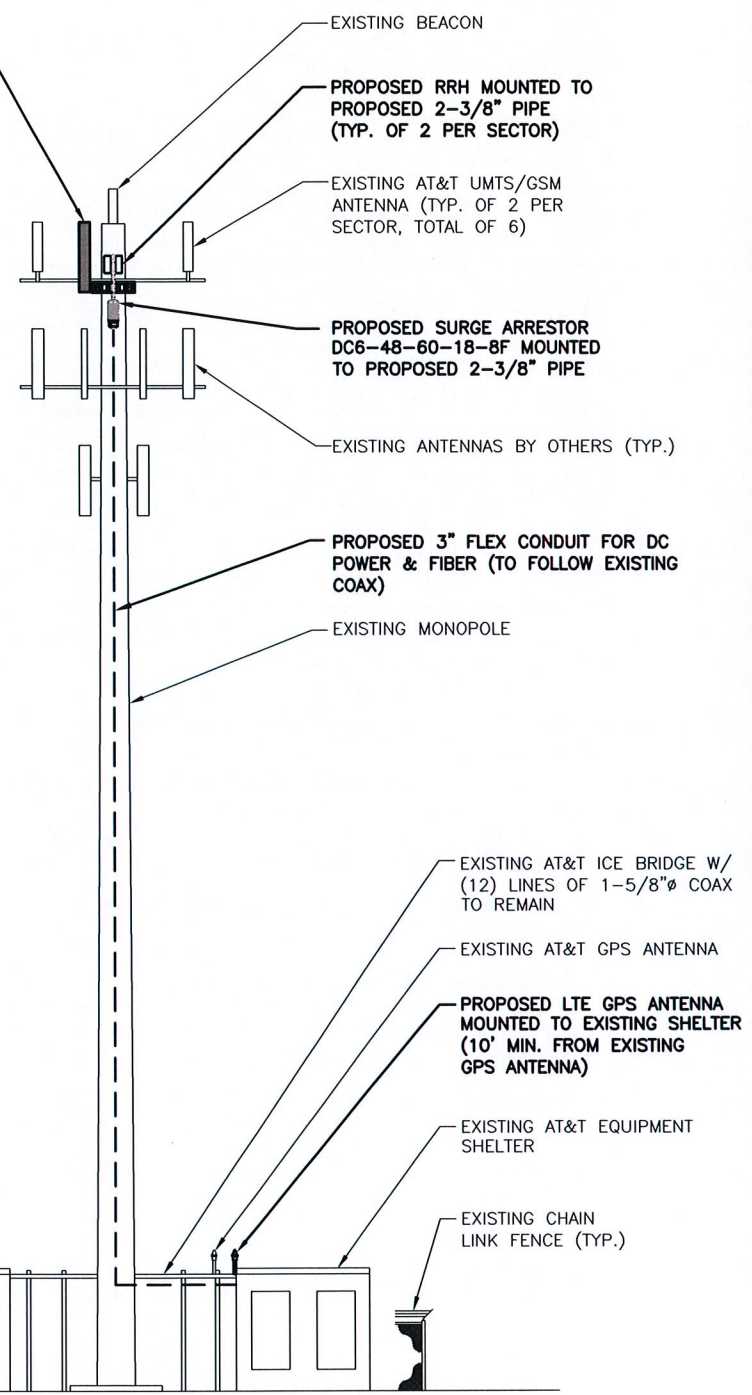
**NOTE:**  
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

**NOTE:**  
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**NOTE:**  
PAINT ALL VISIBLE PROPOSED & EXISTING AT&T EQUIPMENT FAA ORANGE & WHITE

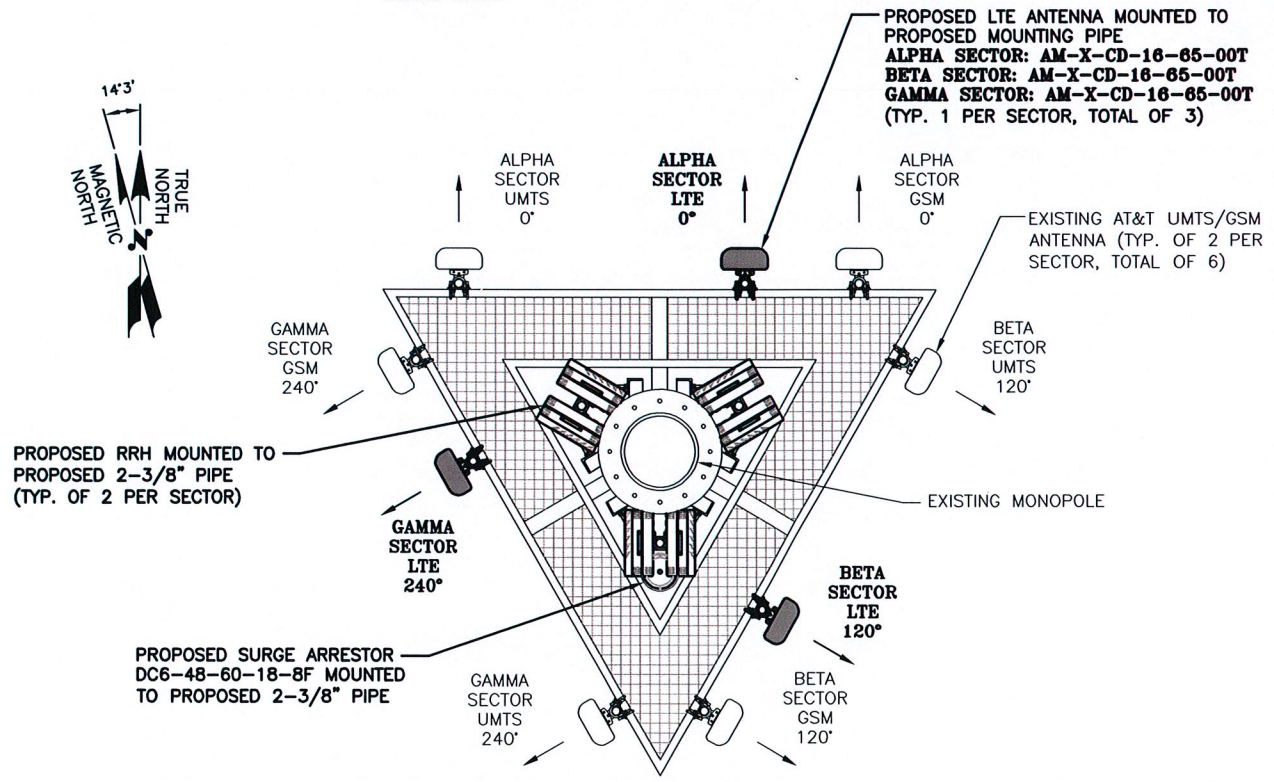
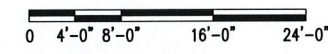
PROPOSED LTE ANTENNA MOUNTED TO PROPOSED MOUNTING PIPE  
**ALPHA SECTOR: AM-X-CD-16-65-00T**  
**BETA SECTOR: AM-X-CD-16-65-00T**  
**GAMMA SECTOR: AM-X-CD-16-65-00T**  
 (TYP. 1 PER SECTOR, TOTAL OF 3)

- CENTER OF EXISTING UMTS/GSM ANTENNAS  
ELEV. 103'-0"± (AGL)
- CENTER OF PROPOSED AT&T ANTENNAS (LTE)  
ELEV. 102'-0"± (AGL)
- PROPOSED AT&T RRH'S & SURGE ARRESTOR  
ELEV. 102'-0"± (AGL)
- TOP OF MONOPOLE  
ELEV. 100'-0"± (AGL)



**WEST ELEVATION**

SCALE: 1/8"=1'-0"



**PROPOSED LTE ANTENNA PLAN**

SCALE: N.T.S.

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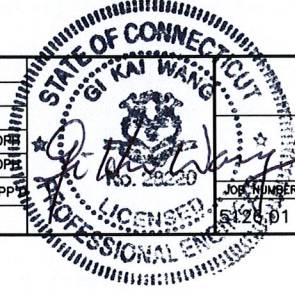
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1		04/18/12	ISSUED FOR CONSTRUCTION	DB	DC	DP	122501		A-2		1
0		03/26/12	ISSUED FOR REVIEW	DB	DC	DP	122501		A-2		

SCALE: AS SHOWN    DESIGNED BY: DC    DRAWN BY: DB



**AT&T**  
 ANTENNA LAYOUT AND ELEVATION (LTE)

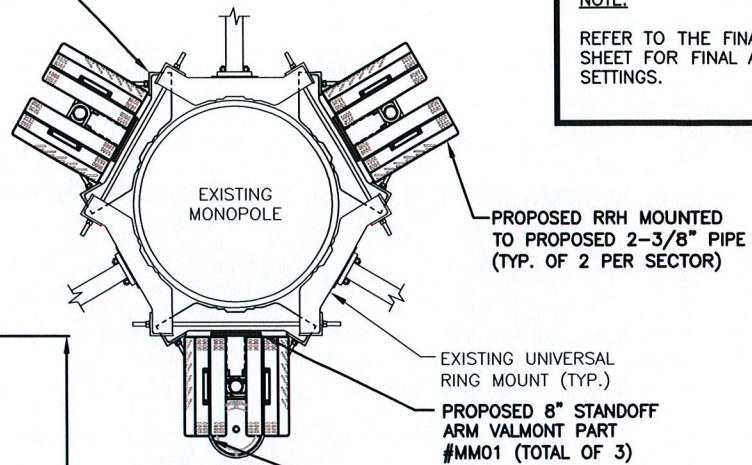


PROPOSED UNIVERSAL RING MOUNT VALMONT PART #LWRM OR #RM-ADK

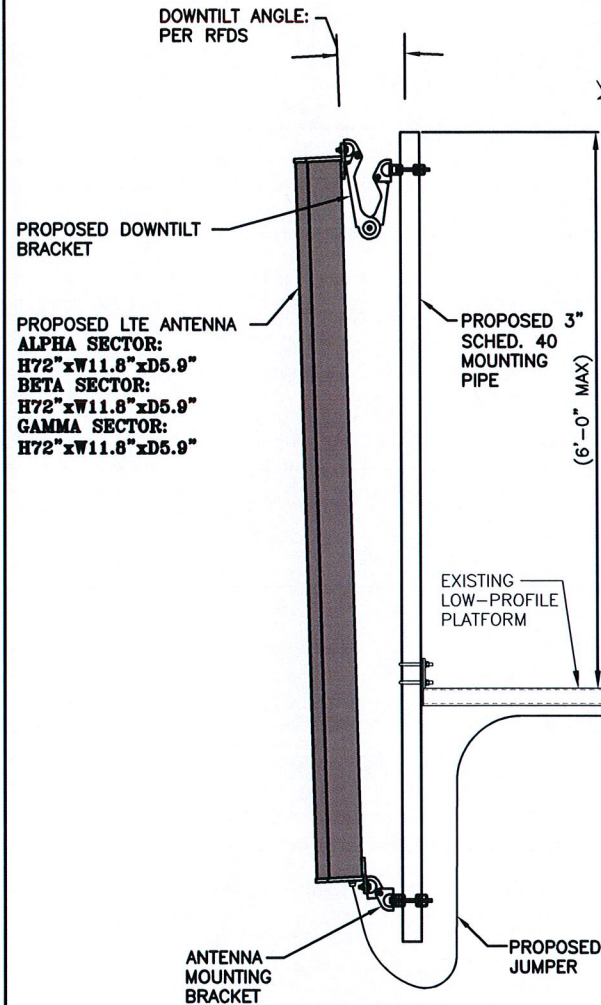
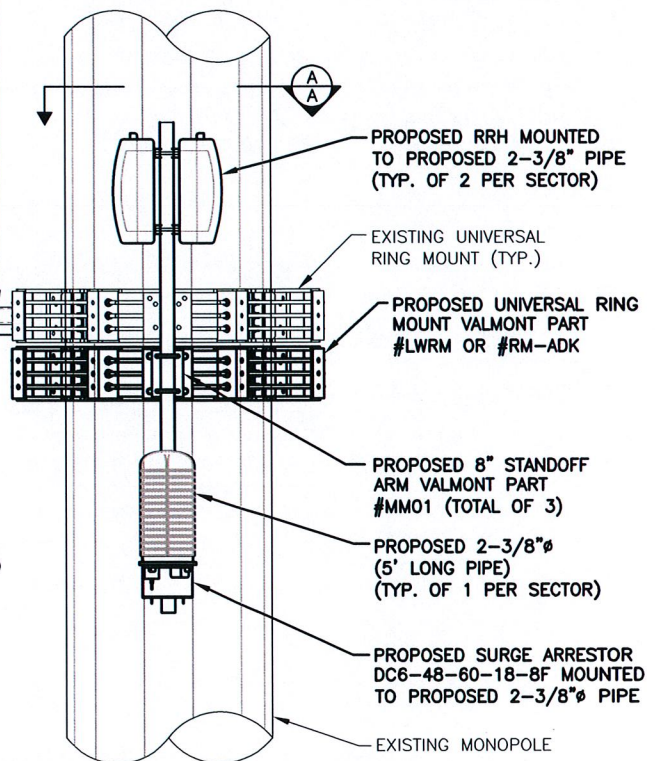
**NOTE:**  
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

**NOTE:**  
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION.

**NOTE:**  
PAINT ALL VISIBLE PROPOSED & EXISTING AT&T EQUIPMENT FAA ORANGE & WHITE



**SECTION A-A**



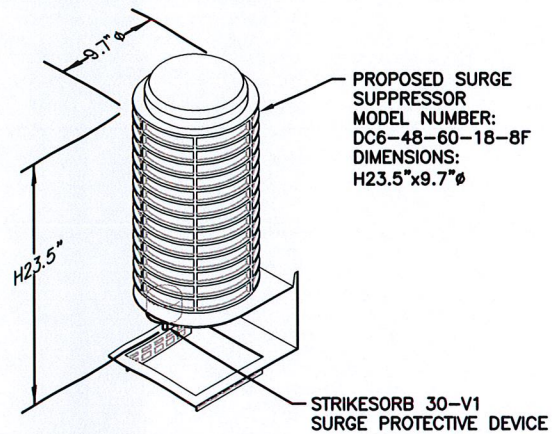
PROPOSED LTE ANTENNA  
ALPHA SECTOR:  
H72"xW11.8"xD5.9"  
BETA SECTOR:  
H72"xW11.8"xD5.9"  
GAMMA SECTOR:  
H72"xW11.8"xD5.9"

**NOTE:**  
1. MINIMUM MONOPOLE DIAMETER OF 2'-0" AT BANDING LOCATION. IF SMALLER, STACK RRH'S 3 OVER 3  
2. CONTRACTOR TO ENSURE THAT RRH MOUNTING DOES NOT INTERFERE WITH CLIMBING LADDER

PART #	VMI PART #	SIZE RANGE
LWRM	801068	12"-45"
RM-ADK	157286	36"-60" ADAPTER KIT

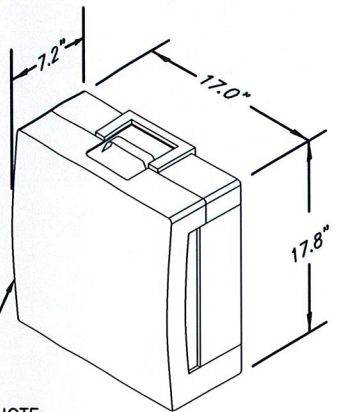
**NOTES:**  
1. REFER TO RFDS & SECTOR SCHEMATICS FOR ANTENNA MODEL, TYPE & QUANTITY REQUIRED PER SECTOR

**PROPOSED RRH & SURGE ARRESTOR MOUNTING DETAIL**  
SCALE: N.T.S.



**NOTE:**  
MOUNT PER MANUFACTURER'S SPECIFICATIONS.

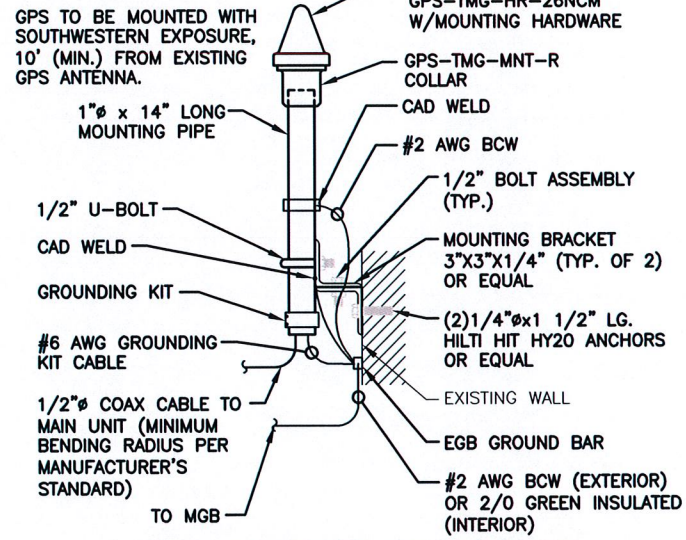
**DC SURGE SUPPRESSOR DETAIL**  
SCALE: N.T.S.



**NOTE:**  
MOUNT PER MANUFACTURER'S SPECIFICATIONS.

**RRH DETAIL**  
SCALE: N.T.S.

**NOTE:**



**GPS MOUNTED TO SHELTER**  
SCALE: N.T.S.

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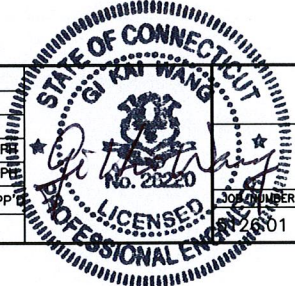
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**SITE NUMBER: CT5126**  
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EAST HARTFORD, CT 06114  
HARTFORD COUNTY

**at&t**  
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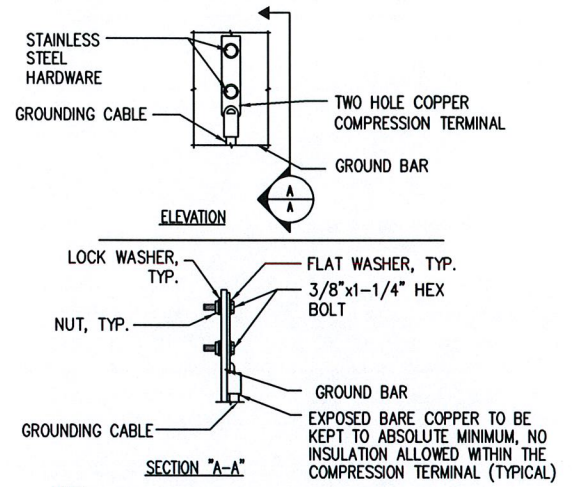
NO.	DATE	REVISIONS	BY	CHK	APP	JOB NUMBER	DRAWING NUMBER	REV
1	04/18/12	ISSUED FOR CONSTRUCTION	DB	DC	DP			
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SCALE: AS SHOWN    DESIGNED BY: DC    DRAWN BY: DB



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DETAILS (LTE)  
DRAWING NUMBER: A-3  
REV: 1

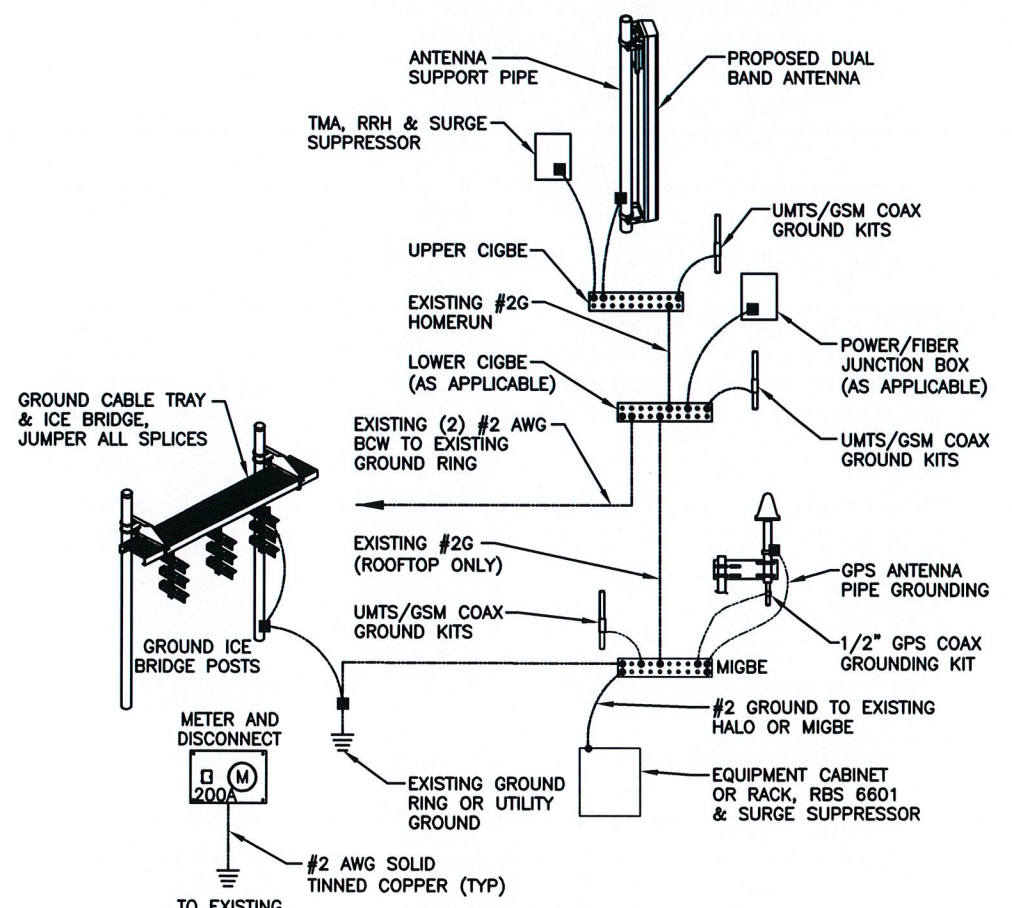




NOTE:  
 1. "DOUBLING UP" OR "STACKING" OF CONNECTION IS NOT PERMITTED.  
 2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATIONS.  
 3. CADWELD DOWNLEADS FROM UPPER EGB, LOWER EGB, AND MGB.

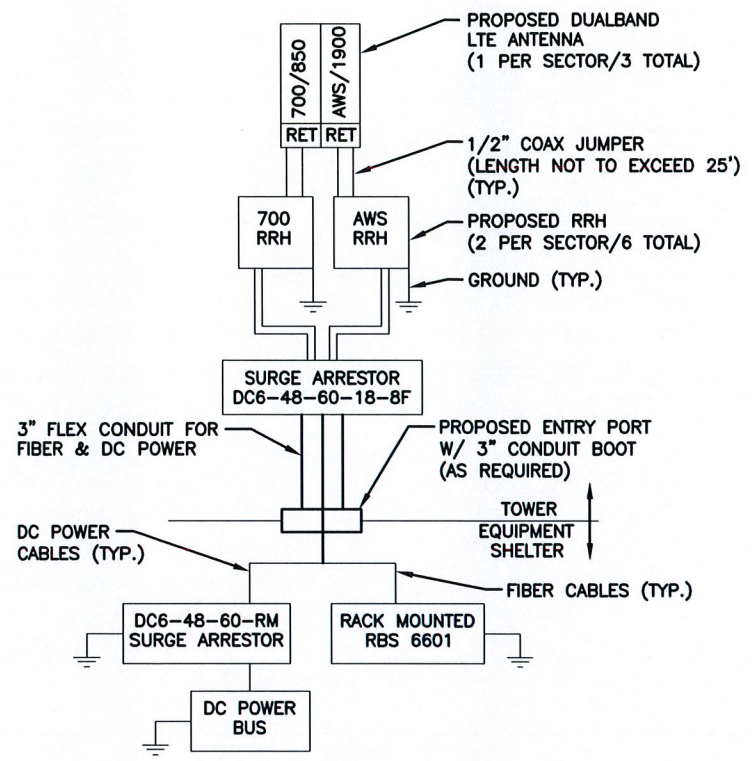
**TYPICAL GROUND BAR CONNECTION DETAIL**

1  
 -  
 N.T.S.



**GROUNDING RISER DIAGRAM**

3  
 -  
 N.T.S.



**LTE PLUMBING DIAGRAM**

2  
 -  
 N.T.S.

EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS ORIGIN AND DESTINATION.

**SECTION "P" - SURGE PRODUCERS**

- CABLE ENTRY PORTS (HATCH PLATES) (#2)
- GENERATOR FRAMEWORK (IF AVAILABLE) (#2)
- TELCO GROUND BAR
- COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2)
- +24V POWER SUPPLY RETURN BAR (#2)
- 48V POWER SUPPLY RETURN BAR (#2)
- RECTIFIER FRAMES.

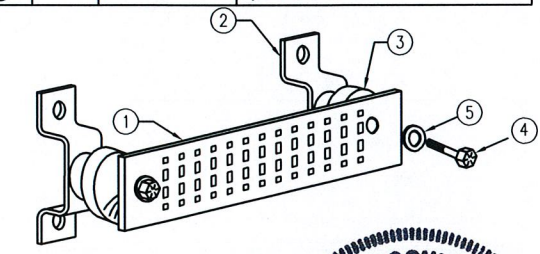
**SECTION "A" - SURGE ABSORBERS**

- INTERIOR GROUND RING (#2)
- EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2)
- METALLIC COLD WATER PIPE (IF AVAILABLE) (#2)
- BUILDING STEEL (IF AVAILABLE) (#2)

WIRELESS SOLUTIONS INC.			
NO.	REQ.	PART NO.	DESCRIPTION
1	1	HLGB-0420-IS	SOLID GND. BAR (20"x4"x1/4")
2	2		WALL MTG. BRKT.
3	2		INSULATORS
4	4		5/8"-11x1" H.H.C.S.
5	4		5/8 LOCKWASHER

**GROUND BAR - DETAIL**

4  
 -  
 N.T.S.



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AT&T

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SCALE: AS SHOWN    DESIGNED BY: DC    DRAWN BY: DB

DRAWING NUMBER: G-1    REV: 1

