



Filed by:

Kri Pelletier, Property Specialist - SBA Communications
134 Flanders Rd., Suite 125, Westborough, MA 01581
508.251.0720 x 3804 - kpelletier@sbsite.com

September 15, 2016

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

Notice of Exempt Modification

2577 Main Street, Glastonbury, CT 06033

41 42 51.8

-72 36 46.9

AT&T #: 10071041_LTE – CT5273

Dear Ms. Bachman:

AT&T currently maintains nine (9) antennas at the 110-foot level of the existing 130-foot Self-Support Tower at 2577 Main Street. The tower is owned by SBA 2012 TC Assets, LLC. The property is owned by Saint Paul's Roman Catholic Church. AT&T now intends to replace three (3) existing cell antennas with (3) newer antennas. These antennas would be installed at the 110-foot level of the tower. AT&T's proposed full scope of work is as follows:

Remove: None

Remove and Replace:

- Remove (2) KMW Panel antennas AM-X-CD-16-OOT and replace with (2) CCI panel antennas HPA-65R-RUU-H6
- Remove (1) Andrew Panel antenna SBNH-1D6565C and replace with (1) CCI panel antenna HPA-65R-BUU-H8
- Remove (3) RRU Ericsson RRUS-11 and replace with (3) RRU Ericsson RRUS-12

Install:

- (3) RRU Ericsson RRUS-A2
- (6) Powerwave LGP21901 Diplexer
- (3) Andrew Bias T ATSBT-TOP-MF-4G

Existing Equipment to Remain (Including entitlements):

- (6) Kathrein Panel antennas 7770
- (18) 1-1/4" coax
- (36) 1/2" fiber
- (6) TMA Powerwave LGP21401 DB-850
- (12) Kathrein RET 860-10025
- (18) 3/8" lines
- (3) RRU Ericsson RRUS 11
- (1) Raycap surge protector

This facility was approved prior to the Council assuming jurisdiction. On 7/18/2000 the Town of Glastonbury and the Inland Wetlands and Watercourses Agency approved a 130' replacement tower within the wetlands' conservation buffer area at 2577 Main Street, west of St. Paul's Church. A preconstruction meeting was to be held to discuss environmental safeguards to be taken during construction and to determine any stabilization efforts for disturbed land areas. The gravel access driveway was to be a minimum of 12 feet in width. The Town has not provided any further restrictions and this modification complies with the aforementioned condition(s).

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16.50j-72(b)(2). In accordance with R.C.S.A. § 16.50j-73, a copy of this letter is being sent to Richard J. Johnson, Town Manager for the Town of Glastonbury, as well as the property owner. (Separate notice is not being sent to tower owner, as it belongs to SBA.)

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. §16.50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modification will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modification will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above-referenced telecommunication facility constitute an exempt modifications under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

A handwritten signature in black ink, appearing to read "Kri Pelletier", is written over a light blue horizontal line.

Kri Pelletier
Property Specialist
SBA COMMUNICATIONS CORPORATION
134 Flanders Rd., Suite 125
Westborough, MA 01581

508.251.0720 x3804 + T
508.366.2610 + F
203.446.7700 + C
kpelletier@sbsite.com

Attachments

cc: Town Manager, Richard J. Johnson – as elected official
Town of Glastonbury, 2155 Main Street, Glastonbury, CT 06033
Saint Paul's Roman Catholic Church – as property owner
2577 Main St. Glastonbury CT 06033-2023

POWER DENSITY

AT&T Site Inventory and Power Data by Antenna

Sector:	A	Sector:	B	Sector:	C
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	Kathrein 800-10121	Make / Model:	Kathrein 800-10121	Make / Model:	Kathrein 800-10121
Gain:	11.45 / 14.35 dBd	Gain:	11.45 / 14.35 dBd	Gain:	11.45 / 14.35 dBd
Height (AGL):	110 feet	Height (AGL):	110 feet	Height (AGL):	110 feet
Frequency Bands	850 MHz / 1900 MHz (PCS)	Frequency Bands	850 MHz / 1900 MHz (PCS)	Frequency Bands	850 MHz / 1900 MHz (PCS)
Channel Count	4	Channel Count	4	Channel Count	4
Total TX Power(W):	120 Watts	Total TX Power(W):	120 Watts	Total TX Power(W):	120 Watts
ERP (W):	2,471.44	ERP (W):	2,471.44	ERP (W):	2,471.44
Antenna A1 MPE%	1.03 %	Antenna B1 MPE%	1.03 %	Antenna C1 MPE%	1.03 %
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	CCI HPA-65R-BUU-H6	Make / Model:	CCI HPA-65R-BUU-H8	Make / Model:	CCI HPA-65R-BUU-H6
Gain:	11.95 / 14.75 dBd	Gain:	11.95 / 14.75 dBd	Gain:	11.95 / 14.75 dBd
Height (AGL):	110 feet	Height (AGL):	110 feet	Height (AGL):	110 feet
Frequency Bands	700 MHz / 1900 MHz (PCS)	Frequency Bands	700 MHz / 1900 MHz (PCS)	Frequency Bands	700 MHz / 1900 MHz (PCS)
Channel Count	4	Channel Count	4	Channel Count	4
Total TX Power(W):	240 Watts	Total TX Power(W):	240 Watts	Total TX Power(W):	240 Watts
ERP (W):	5,462.56	ERP (W):	6,229.75	ERP (W):	5,462.56
Antenna A2 MPE%	2.53 %	Antenna B2 MPE%	3.01 %	Antenna C2 MPE%	2.53 %
Antenna #:	3	Antenna #:	3	Antenna #:	3
Make / Model:	Kathrein 800-10121	Make / Model:	Kathrein 800-10121	Make / Model:	Kathrein 800-10121
Gain:	11.45 / 0 / 0 / 0 dBd	Gain:	11.45 / 0 / 0 / 0 dBd	Gain:	11.45 / 0 / 0 / 0 dBd
Height (AGL):	110 feet	Height (AGL):	110 feet	Height (AGL):	110 feet
Frequency Bands	850 MHz	Frequency Bands	850 MHz	Frequency Bands	850 MHz
Channel Count	2	Channel Count	2	Channel Count	2
Total TX Power(W):	60 Watts	Total TX Power(W):	60 Watts	Total TX Power(W):	60 Watts
ERP (W):	837.82	ERP (W):	837.82	ERP (W):	837.82
Antenna A3 MPE%	0.49 %	Antenna B3 MPE%	0.49 %	Antenna C3 MPE%	0.49 %

Site Composite MPE%	
Carrier	MPE%
AT&T - Max per sector	4.54 %
T-Mobile	5.32 %
MetroPCS	1.38 %
Sprint	0.03 %
Clearwire	0.13 %
Nextel	0.38 %
Verizon Wireless	12.92 %
Site Total MPE %:	24.70 %

AT&T Sector A Total:	4.05 %
AT&T Sector B Total:	4.54 %
AT&T Sector C Total:	4.05 %
Site Total:	24.70 %



Owner of Record

GIS ID: 41402577
Owner: ST PAULS ROMAN CATHOLIC CHURCH
Co-Owner:
Address: 2577 MAIN ST
City, State ZIP: GLASTONBURY, CT 06033-2023

Account Number: 41402577

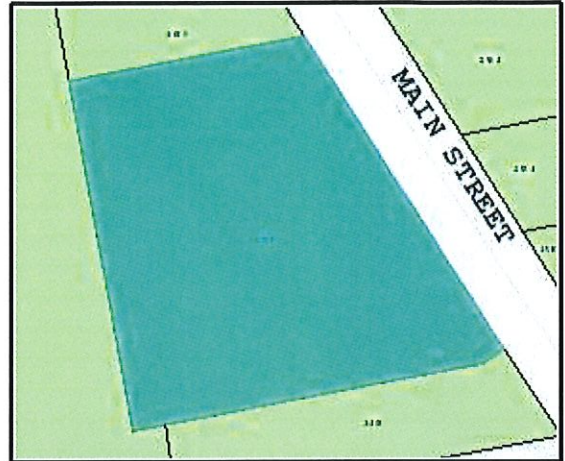
Property Address: 2577 MAIN ST

Parcel Information

Map/Street/Lot D5 / 4140 / W0038 **Property ID:** 12111
Developer Lot ID: **Water:** Public-MDC
Parcel Acreage: 4.11 **Sewer:** Sewer Tax Rec
Zoning Code: PBD **Census:** 5203

Valuation Summary

Item	Appraised Value	Assessed Value
Buildings	1998600	1399000
Land	712300	498600
Appurtenances	14500	10200
Total	2725400	1907800



Property highlighted in blue

Owner of Record

ST PAULS ROMAN CATHOLIC CHURCH

Deed / Page Sale Date Sale Price

0450/0069 10/04/1988 0





Town of Glastonbury GIS Parcel Report

Report Generated 8/16/2016 12:04:03 PM

Basement, Finished	3965	0
Porch, Open	664	0
Basement	-60	0
First Floor	1368	1368
Porch, Open	50	0
Upper Story, Finished	1064	1064
Basement	1368	0
Utility, Storage, Unfinished	20	0



RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

AT&T Existing Facility

Site ID: CT5273

Glastonbury - NW
2577 Main Street
Glastonbury, CT 06033

September 3, 2016

EBI Project Number: 6216003860

Site Compliance Summary	
Compliance Status:	COMPLIANT
Site total MPE% of FCC general public allowable limit:	24.70 %



September 3, 2016

AT&T Mobility – New England
Attn: Cameron Syme, RF Manager
550 Cochituate Road
Suite 550 – 13&14
Framingham, MA 06040

Emissions Analysis for Site: **CT5273 – Glastonbury - NW**

EBI Consulting was directed to analyze the proposed AT&T facility located at **2577 Main Street, Glastonbury, CT**, for the purpose of determining whether the emissions from the Proposed AT&T Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limits for the 700 and 850 MHz Bands are approximately $467 \mu\text{W}/\text{cm}^2$ and $567 \mu\text{W}/\text{cm}^2$ respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 2300 MHz (WCS) bands is $1000 \mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed AT&T Wireless antenna facility located at **2577 Main Street, Glastonbury, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since AT&T is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 UMTS channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) 2 UMTS channels (1900 MHz (PCS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 3) 2 LTE channels (700 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 4) 2 LTE channels (1900 MHz (PCS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 5) 2 GSM channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.



- 6) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 7) For the following calculations the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 8) The antennas used in this modeling are the **Kathrein 800-10121**, **CCI HPA-65R-BUU-H6 and the CCI HPA-65R-BUU-H8** for transmission in the 700 MHz, 850 MHz and 1900 MHz (PCS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 9) The antenna mounting height centerlines of the proposed antennas are **110 feet** above ground level (AGL) for **Sector A**, **110 feet** above ground level (AGL) for **Sector B** and **110 feet** above ground level (AGL) for Sector C.
- 10) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.



AT&T Site Inventory and Power Data by Antenna

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Gain:	11.45 / 0 / 0 / 0 dBd	Gain:	11.45 / 0 / 0 / 0 dBd	Gain:	11.45 / 0 / 0 / 0 dBd
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Frequency Bands	850 MHz	Frequency Bands	850 MHz	Frequency Bands	850 MHz
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Antenna A3 MPE%	0.49 %	Antenna B3 MPE%	0.49 %	Antenna C3 MPE%	0.49 %

Site Composite MPE%	
Carrier	MPE%
AT&T – Max per sector	4.54 %
T-Mobile	5.32 %
MetroPCS	1.38 %
Sprint	0.03 %
Clearwire	0.13 %
Nextel	0.38 %
Verizon Wireless	12.92 %
Site Total MPE %:	24.70 %

AT&T Sector A Total:	4.05 %
AT&T Sector B Total:	4.54 %
AT&T Sector C Total:	4.05 %
Site Total:	24.70 %

AT&T _ Max Values Per Sector (Sector B)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ($\mu\text{W}/\text{cm}^2$)	Frequency (MHz)	Allowable MPE ($\mu\text{W}/\text{cm}^2$)	Calculated % MPE
AT&T 850 MHz UMTS	2	418.91	110	2.78	850 MHz	567	0.49%
AT&T 1900 MHz (PCS) UMTS	2	816.81	110	5.43	1900 MHz (PCS)	1000	0.54%
AT&T 700 MHz LTE	2	1,239.23	110	8.24	700 MHz	467	1.76%
AT&T 1900 MHz (PCS) LTE	2	1,875.65	110	12.47	1900 MHz (PCS)	1000	1.25%
AT&T 850 MHz GSM	2	418.91	110	2.78	850 MHz	567	0.49%
						Total:	4.54%



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the AT&T facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

AT&T Sector	Power Density Value (%)
Sector A:	4.05 %
Sector B:	4.54 %
Sector C:	4.05 %
AT&T Maximum Total (per sector):	4.54 %
Site Total:	24.70 %
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **24.70 %** of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.



CONSULTING GROUP, INC.

9221 Lyndon B. Johnson Freeway, #204, Dallas, TX 75243 ★ PHONE 972-231-8893 ★ FAX 1-866-364-8375
www.allprocgi.com ★ e-mail: info@allprocgi.com

**Tower Structural Analysis Report for
SBA Network Services, Inc.**



Existing 130' Self-Support Tower
SBA Site Name: Glastonbury-main St.
SBA Site ID: CT46126-A -01

Carrier Name: AT&T
Carrier Site Name: 10071041
Site Location:
2577 Main Street
Glastonbury, CT 06033

Latitude: 41.714389°
Longitude: -72.613028°

ACGI Job # 16-2859

ANALYSIS RESULTS		
Tower Components	98.7%	Pass
Tower Foundation	62.7%	Pass
Net Change in Tower Stress	+2.30%	From previous structural analysis by B+T Group, Job # 101341.001.01a, dated 09/29/2015

Prepared By:
Moises Perez, EIT
Staff Engineer



08/16/2016
Approved By
Joji M. George, PE.
CT PE# 24444

TABLE OF CONTENTS

ANALYSIS SUMMARY 3

SCOPE & SOURCE OF INFORMATION..... 3

 SOURCE OF INFORMATION..... 3

ANALYSIS METHODS & DATA..... 4

 SITE DATA..... 4

 TOWER DATA 4

 TOWER HISTORY 4

CONCLUSIONS..... 5

 RESULT SUMMARY..... 5

 FOUNDATION CAPACITY 5

DISCLAIMER..... 6

APPURTENANCE LISTING 7

 EXISTING LOAD DESCRIPTION..... 7

 EXISTING LOAD DESCRIPTION Continuation... 8

 AT&T FINAL LOAD DESCRIPTION 8

SUMMARY OF WORKING PERCENTAGE OF STRUCTURAL COMPONENTS 9

APPENDIX..... 11

1. ANALYSIS SUMMARY

The existing 130’ Self-support Tower located in Glastonbury, Connecticut was analyzed by Allpro Consulting Group, Inc. (ACGI) for the existing and the proposed AT&T antennas, radios and coaxes as authorized by SBA Communication Corp. Based on the results of the analysis, the existing tower with below mentioned proposed and existing loading is found to be **in code compliance** with TIA/EIA-222-F, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and the 2003 International Building Code.

2. SCOPE & SOURCE OF INFORMATION

The purpose of this structural analysis is to determine whether the existing structure is capable of supporting additional proposed loads.

SOURCE OF INFORMATION		
Tower Data:	FRED A. NUDD Corporation	Original Tower Design by FRED A. NUDD Corporation PJ No. 6893, Sept, 1999
	FDH Engineering Inc.	Modification Drawings by FDH, Project No. 1338401400, dated 06/17/2013
	FDH Engineering Inc.	Modification Inspection Report by FDH, Project No. 1304001700, dated 11/01/2013
	FDH Engineering Inc.	Modification Inspection Report by FDH, Project No. 1305911700, dated 02/25/2014
	B+T Group	Existing Tower data as per previous structural analysis by B+T Group, Job # 101341.001.01a, dated 09/29/2015
Foundation Data:	FRED A. NUDD Corporation	Original Tower Design by FRED A. NUDD Corporation PJ No. 6893, Sept, 1999
Geotechnical Report:	Tectonic Engineering	Geotechnical Report by Tectonic Engineering Project # 1170.C057, dated 08/26/1999
Loading Data:	B+T Group	Existing loading as per previous structural analysis by B+T Group, Job # 101341.001.01a, dated 09/29/2015
	SBA Communication Corp.	Site Summary dated 08/02/2016 Proposed final loading for AT&T as per Application ID # 39946, v1 downloaded from SBA portal
Authorization:	SBA Communication Corp.	

3. ANALYSIS METHODS & DATA

The analysis was performed in accordance with Telecommunication Industry Association specification TIA/EIA-222-F. The tower was modeled using TNX Tower, a 3-D finite element program. TNX Tower is a general-purpose modeling, analysis, and design program created specifically for communication towers using the EIA-222-C, EIA-222-D, TIA/EIA-222-F or TIA/EIA-222-G standards. The 3-D model included the tower, with existing appurtenances and all proposed loads.

SITE DATA	
SBA Site Name:	Glastonbury main st.
SBA Site Number:	CT146126-A-01
Carrier Site Name:	AT&T/10071041
City, State:	Glastonbury, CT
County:	Hartford
Code Wind Load Requirement:	ANSI/TIA-222-F (80 mph basic wind speed) & 2003 International Building Code.
Wind Load Used:	ANSI/TIA-222-F Code: <ul style="list-style-type: none"> • Basic wind speed of 80 mph • A wind speed of 38 mph is used in combination with ice. • Nominal ice thickness of 1.0 in.

TOWER DATA	
Tower Type:	3 Sided Self-support Tower
Height:	130'
Cross Section:	Triangular
Steel Strength:	Legs – 50 ksi, Braces – 36 ksi
Type of Foundation:	Individual concrete pad with square pedestal

TOWER HISTORY	
Tower Manufacturer / Model:	ROHN/ SSV TOWER
Date of Original Design:	September 1999
Previous Modifications:	Modification Drawings by FDH, Project No. 1338401400, dated 06/17/2013
Original Design Code Reqt:	TIA/EIA 222-F 1996, 85mph + 1/2" ice

4. CONCLUSIONS

RESULT SUMMARY		
<i>MEMBER</i>	<i>% Capacity</i>	<i>Pass/Fail</i>
Leg	97.0 %	Pass
Diagonal	95.8 %	Pass
Horizontal	4.20 %	Pass
Sec. Horizontal	98.7 %	Pass
Girts	14.2 %	Pass
Bolt Checks	98.7 %	Pass
Overall Tower rating 98.7 %		

FOUNDATION CAPACITY		
<i>Direction</i>	<i>% Capacity</i>	<i>Pass/Fail</i>
Overturning	62.7 %	Pass
Net Soil Bearing Pressure	30.9 %	Pass
Horizontal shear capacity	18.1%	Pass
Overall 62.7 %		

As per the results of the analysis, the existing tower is **in code compliance** for the new and existing antenna loads.

Maximum tower member stress **less than allowable**, making it **in code compliance** under the EIA/TIA-222-F code and **2003 International Building Code** requirements.

5.

DISCLAIMER

Installation procedures and related loading are not within the scope of this analysis. A contractor experienced in similar work should perform all installation work. The engineering services provided by Allpro Consulting Group, Inc. (ACGI) are limited to the computer analysis and calculations of the structure with the proposed and existing loads. This analysis is considered void if the loading mentioned in this report is changed or is different as installed. It is assumed that the existing structure is properly maintained and is in good condition free of any defects. Scope of this analysis does not include existing connections, except as noted in this report.

ACGI does not make any warranties, expressed or implied in connection with this engineering analysis report and disclaims any liability arising from deficiencies or any existing conditions of the original structure. ACGI will not be responsible for consequential or incidental damages sustained by any parties as a result of any data or conclusions included in this Report. The maximum liability of ACGI pursuant to this report shall be limited to the consulting fee received for the preparation of the report.

6.

APPURTENANCE LISTING

EXISTING LOAD DESCRIPTION					
<u>ELEV</u> <u>(ft.)</u>	<u>Qty.</u>	<u>Antenna Description</u>	<u>Mount Type & Qty.</u>	<u>TX. LINE (in)</u>	<u>TENANT</u>
130±	1	Andrew VHLP2.5	(3) T-Frames @128'	(6) 5/16 (4) 1/2	Sprint
128±	3	Unknown 24"x14"x9"			
	2	Argus Tech. LLPX310R			
	1	Kathrein 840 10054			
	1	Motorola TIMING 2000			
126±	1	Andrew VHLP2.5			
124±	3	Unknown MODEM			
	1	Andrew VHLP2.5			
120±	3	Alcatel Lucent TD-RRH8x20-25	(3) T-Arms @118.5'	(4) 1-1/4"	Sprint
	3	Rfs Celwave APXVTM14-C-120			
118.5±	3	Ericsson 1900 MHz			
	4	RFS ACU-A20-N RETs			
	3	Ericsson 800 MHz			
	1	Powerwave P40-16-XLPP-RR-A			
	2	RFS APXVSP18-C-A20			
3	Samsung 800 MHz Filter				
110±	6	Allgon 7700.00	(3) T-Frames @110'	(12) 1-1/4 (1) 3/8	AT&T
	1	Andrew SBNH-1D6565C			
	6	Ericsson RRUS-11 1900MHz			
	2	KMW AM-X-CD-16-65-00T-RET			
	6	Powerwave LGP13519			
	6	Powerwave LGP21401			
	1	Raycap DC6-48-60-18-8F			
93±	3	Ericsson AIR 21 B2A/B4P	(3) T-Frames (1) MT-195-12 (1) VSR-TS-B @93'	(13) 1-5/8	T-MOBILE
	3	Ericsson AIR 21 B4A/B2P			
	3	Ericsson KRY 112 144/1 TMA			
	3	Commscope LNX-6515DS-A1M			
	3	Ericsson S11B12			
80±	3	Alcatel Lucent RRH2X60-PCS	(3) T-Frames @80'	(2) 1-5/8	VERIZON
	3	Alcatel Lucent RRH2x60-700			
	3	Alcatel Lucent RRH2x60-AWS			
	6	Andrew HBXX-6517DS-A2M			
	6	Andrew LNX-6514DS-A1M			
	2	RFS DB-T1-6Z-8AB-0Z			

EXISTING LOAD DESCRIPTION			Continuation...		
<u>ELEV (ft.)</u>	<u>Qty.</u>	<u>Antenna Description</u>	<u>Mount Type & Qty.</u>	<u>TX. LINE (in)</u>	<u>TENANT</u>
55.5±	1	GPS Antenna	(2) Side-Arm @55.5'	(1) 1/2	
50.5±	2	GPS Antennas	(2) Side-Arm @50.5'	(2) 1/2	

AT&T FINAL LOAD DESCRIPTION					
<u>ELEV (ft.)</u>	<u>Qty.</u>	<u>Antenna Description</u>	<u>Mount Type & Qty.</u>	<u>TX. LINE (in)</u>	<u>TENANT</u>
110±	2	CCI HPA-65R-BUU-H6 Antennas	(3) T-Frames @110'	(36) 1/2 fiber (18) 1-1/4 coax (18) 3/8"	AT&T
	1	CCI HPA-65R-BUU-H8 Antennas			
	6	Kathrein 800 10121 Antennas			
	3	Ericsson RRUS 11			
	3	Ericsson RRUS 12			
	3	Ericsson RRUS A2			
	6	Powerwave LGP 21401 DB-850 TMA			
	12	Kathrein 860-10025 RET			
	6	Powerwave LGP21901 diplexers			
	3	Andrew ATSBT-TOP-MF-4G			
	1	Raycap			

Notes:

1. ACGI should be notified of any discrepancies found in the data listed in this report.
2. Notify Allpro Consulting Group, Inc. of any potential physical & other interference with existing antennas for a redesign.

7. SUMMARY OF WORKING PERCENTAGE OF STRUCTURAL COMPONENTS

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P _{allow} K	% Capacity	Pass Fail
T1	130 - 120	Leg	1 1/2	2	-7.914	42.280	18.7	Pass
T2	120 - 117.143	Leg	2	44	-12.819	83.570	15.3	Pass
T3	117.143 - 114.286	Leg	2	56	-19.281	83.570	23.1	Pass
T4	114.286 - 111.43	Leg	2	65	-26.000	82.306	31.6	Pass
T5	111.43 - 108.573	Leg	2	74	-34.196	82.306	41.5	Pass
T6	108.573 - 105.716	Leg	2	83	-44.659	82.306	54.3	Pass
T7	105.716 - 102.859	Leg	2	92	-56.490	82.306	68.6	Pass
T8	102.859 - 100	Leg	2	101	-67.042	101.583	66.0	Pass
T9	100 - 96	Leg	P4.5 x 0.237	116	-76.726	122.309	67.3 (b)	Pass
T10	96 - 92	Leg	P4.5 x 0.237	125	-89.534	122.309	62.7	Pass
T11	92 - 88	Leg	P4.5 x 0.237	134	-98.353	130.687	73.2	Pass
T12	88 - 84	Leg	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	146	-112.008	191.515	75.3	Pass
T13	84 - 80	Leg	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	158	-124.569	191.536	58.5	Pass
T14	80 - 75	Leg	P6.625x0.280	170	-141.999	220.348	65.0	Pass
T15	75 - 70	Leg	P6.625x0.280	179	-160.866	220.348	64.4	Pass
T16	70 - 65	Leg	P6.625x0.280	188	-178.357	220.348	73.0	Pass
T17	65 - 60	Leg	P6.625x0.280	188	-178.357	220.348	80.9	Pass
T18	60 - 55	Leg	P6.625x0.280	197	-194.360	220.348	88.2	Pass
T19	55 - 50	Leg	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	206	-206.358	231.994	88.9	Pass
T20	50 - 45	Leg	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	218	-224.229	295.949	75.8	Pass
T21	45 - 40	Leg	BT101341- P6.625x0.280 w/ HP7.625x0.301	227	-236.930	295.949	80.1	Pass
T22	40 - 33.3333	Leg	P6.625x.432	236	-247.859	306.666	80.8	Pass
T23	33.3333 - 26.6667	Leg	P6.625x.432	248	-262.992	316.102	83.2	Pass
T24	26.6667 - 20	Leg	P6.625x.432	256	-279.148	316.102	88.3	Pass
T25	20 - 13.3333	Leg	P6.625x.432	265	-293.304	316.102	92.8	Pass
T26	13.3333 - 6.66666	Leg	P6.625x.432	274	-306.610	316.102	97.0	Pass
T27	6.66666 - 0	Leg	P6.625x.432	283	-318.292	343.191	92.7	Pass
T28		Leg	BT101341- P6.625 x .432 w/ HP7.625x0.301	295	-330.259	382.811	86.3	Pass
T1	130 - 120	Diagonal	1/2	13	-1.472	1.872	78.7	Pass
T2	120 - 117.143	Diagonal	3/4	52	-2.302	7.257	31.7	Pass
T3	117.143 - 114.286	Diagonal	3/4	61	-3.107	7.257	42.8	Pass
T4	114.286 - 111.43	Diagonal	3/4	70	-2.903	7.203	40.3	Pass
T5	111.43 - 108.573	Diagonal	3/4	79	-3.911	7.203	54.3	Pass
T6	108.573 - 105.716	Diagonal	3/4	88	-4.966	7.203	68.9	Pass
T7	105.716 - 102.859	Diagonal	3/4	97	-4.894	7.203	67.9	Pass
T8	102.859 - 100	Diagonal	3/4	109	-5.131	7.255	70.7	Pass
T9	100 - 96	Diagonal	L1 1/2x1 1/2x3/16	121	-4.091	9.776	41.8	Pass
T10	96 - 92	Diagonal	L2x2x1/4	130	-4.898	19.502	94.6 (b)	Pass
T11	92 - 88	Diagonal	2L1 1/2x1 1/2x3/16x3/8	139	-7.547	24.551	25.1	Pass
T12	88 - 84	Diagonal	2L1 1/2x1 1/2x3/16x3/8	151	-7.023	24.298	62.4 (b)	Pass
T13	84 - 80	Diagonal	2L1 1/2x1 1/2x3/16x3/8	163	-6.180	24.039	30.7	Pass
							86.6 (b)	
							28.9	Pass
							81.5 (b)	
							25.7	Pass



CT46126-A-01 Glastonbury-main St. – 130' SST

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P _{allow} K	% Capacity	Pass Fail	
T14	80 - 75	Diagonal	L2x2x1/4	175	-6.485	17.786	71.8 (b) 36.5	Pass	
T15	75 - 70	Diagonal	2L1 1/2x1 1/2x3/16x3/8	184	-7.194	22.921	82.6 (b) 31.4	Pass	
T16	70 - 65	Diagonal	2L1 1/2x1 1/2x3/16x3/8	193	-6.372	22.566	79.9 (b) 28.2	Pass	
T17	65 - 60	Diagonal	2L1 1/2x1 1/2x3/16x3/8	202	-6.544	22.200	69.3 (b) 29.5	Pass	
T18	60 - 55	Diagonal	2L1 1/2x1 1/2x3/16x3/8	208	-7.919	21.395	72.2 (b) 37.0	Pass	
T19	55 - 50	Diagonal	2L1 1/2x1 1/2x3/16x3/8	220	-5.190	21.434	88.7 (b) 24.2	Pass	
T20	50 - 45	Diagonal	2L1 1/2x1 1/2x3/16x3/8	229	-6.133	21.034	56.9 (b) 29.2	Pass	
T21	45 - 40	Diagonal	L2x2x1/4	238	-6.602	15.634	68.0 (b) 42.2	Pass	
T22	40 - 33.3333	Diagonal	2L1 3/4x1 3/4x3/16x3/8	250	-5.911	23.756	84.1 (b) 24.9	Pass	
T23	33.3333 - 26.6667	Diagonal	2L1 3/4x1 3/4x3/16x3/8	259	-6.180	23.231	53.8 (b) 26.6	Pass	
T24	26.6667 - 20	Diagonal	2L1 3/4x1 3/4x3/16x3/8	268	-5.709	22.687	56.2 (b) 25.2	Pass	
T25	20 - 13.3333	Diagonal	L2x2x3/16	277	-5.784	8.144	51.9 (b) 71.0	Pass	
T26	13.3333 - 6.66666	Diagonal	L2x2x3/16	286	-5.586	7.345	95.8 (b) 76.1	Pass	
T27	6.66666 - 0	Diagonal	2L2x2x3/16x3/8	298	-7.138	27.363	93.2 (b) 26.1	Pass	
T1	130 - 120	Horizontal	L1 1/4x1 1/4x3/16	36	-0.257	6.068	64.9 (b) 4.2	Pass	
T8	102.859 - 100	Secondary Horizontal	L2x2x1/8	112	-1.161	9.513	12.2	Pass	
T11	92 - 88	Secondary Horizontal	4x3/8	142	-2.884	14.141	20.4	Pass	
T12	88 - 84	Secondary Horizontal	4x3/8	154	-3.539	12.213	55.4 (b) 29.0	Pass	
T13	84 - 80	Secondary Horizontal	4x3/8	166	-3.048	10.644	69.1 (b) 28.6	Pass	
T18	60 - 55	Secondary Horizontal	L2x2x1/8	214	3.577	11.778	58.4 (b) 30.4	Pass	
T21	45 - 40	Secondary Horizontal	L3x3x5/16	244	4.295	45.945	98.7 (b) 9.3	Pass	
T26	13.3333 - 6.66666	Secondary Horizontal	L2x2x1/4	292	-5.515	21.369	78.1 (b) 25.8	Pass	
T1	130 - 120	Top Girt	L1 1/4x1 1/4x3/16	6	-0.061	6.068	64.2 (b) 1.0	Pass	
T2	120 - 117.143	Top Girt	L1 1/4x1 1/4x3/16	48	-0.031	6.152	0.5	Pass	
T1	130 - 120	Bottom Girt	L1 1/4x1 1/4x3/16	9	-0.208	6.068	3.4	Pass	
T8	102.859 - 100	Bottom Girt	L1 1/4x1 1/4x3/16	105	-0.875	6.152	14.2	Pass	
							Summary		
							Leg (T25)	97.0	Pass
							Diagonal (T25)	95.8	Pass
							Horizontal (T1)	4.2	Pass
							Secondary Horizontal (T18)	98.7	Pass
							Top Girt (T1)	1.0	Pass
							Bottom Girt (T8)	14.2	Pass
							Bolt Checks	98.7	Pass
							RATING =	98.7	Pass

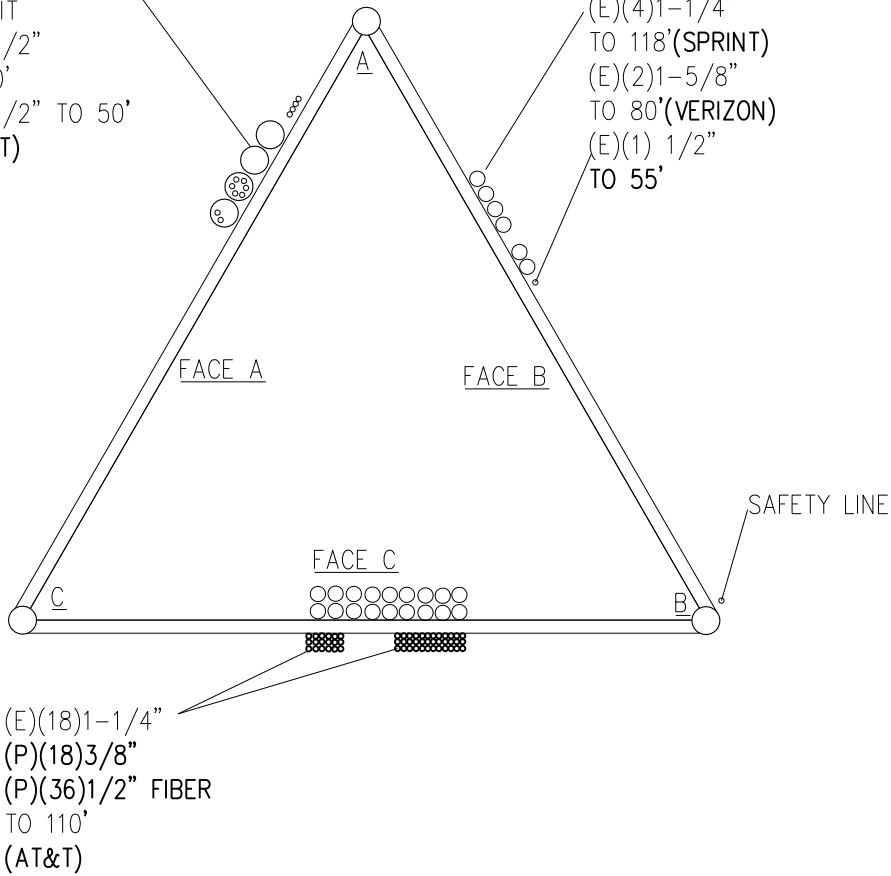
APPENDIX

COAX LAYOUT

CT46126-A -01/
Glastonbury-main St.
130' SST

(E)(2)2" CONDUIT
(E)(6)5/16" INSIDE
CONDUIT
(E)(2)1/2" INSIDE
CONDUIT
(E)(2)1/2"
TO 130'
(E)(2)1/2" TO 50'
(SPRINT)

(E)(4)1-1/4"
TO 118'(SPRINT)
(E)(2)1-5/8"
TO 80'(VERIZON)
(E)(1) 1/2"
TO 55'

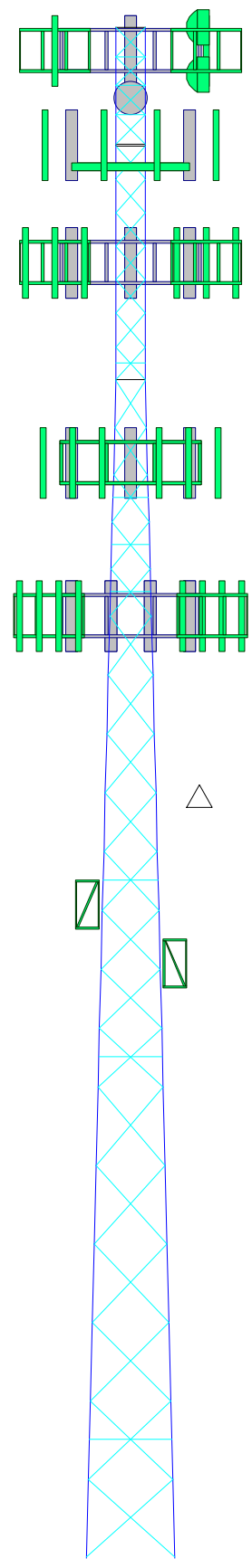


COAX LAYOUT

TOWER ELEVATION DRAWING

Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11	T12	T13	T14	T15	T16	T17	T18	T19	T20	T21	T22	T23	T24	T25	T26	T27	
Legs	SR 1 1/2		SR 2		SR 3/4		SR 3/4		SR 3/4		SR 3/4		SR 3/4		SR 3/4		SR 3/4		SR 3/4		SR 3/4		SR 3/4		SR 3/4		SR 3/4	
Leg Grade	A570-45																											
Diagonals	P4.5 x 0.237																											
Diagonal Grade	A36																											
Top Girts	L1 1/4x1 1/4x3/16																											
Bottom Girts	L1 1/4x1 1/4x3/16																											
Horizontal	L1 1/4x1 1/4x3/16																											
Sec. Horizontals	N.A.																											
Face Width (ft)	7.5																											
# Panels @ (ft)	5 @ 6.6667																											
Weight (K)	11.9																											

130.0 ft	
120.0 ft	
117.1 ft	
114.3 ft	
111.4 ft	
108.6 ft	
105.7 ft	
102.9 ft	
100.0 ft	
96.0 ft	
92.0 ft	
88.0 ft	
84.0 ft	
80.0 ft	
75.0 ft	
70.0 ft	
65.0 ft	
60.0 ft	
55.0 ft	
50.0 ft	
45.0 ft	
40.0 ft	
33.3 ft	
26.7 ft	
20.0 ft	
13.3 ft	
6.7 ft	
0.0 ft	



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
LLPX310R w/ Mount Pipe (E)	128	(4) (P) Kathrein 860-10025 RET	110
LLPX310R w/ Mount Pipe (E)	128	(4) (P) Kathrein 860-10025 RET	110
840 10054 w/ Mount Pipe (E)	128	(4) (P) Kathrein 860-10025 RET	110
24"x14"x9" (E)	128	(2) (P) Powerwave LGP21901	110
24"x14"x9" (E)	128	(2) (P) Powerwave LGP21901	110
24"x14"x9" (E)	128	(2) (P) Powerwave LGP21901	110
TIMING 2000 (E)	128	(2) LGP13519 (E)	110
MODEM (E)	128	(2) LGP13519 (E)	110
MODEM (E)	128	(2) LGP13519 (E)	110
MODEM (E)	128	AIR 21 B2A/B4P (E)	93
Sector Mount [SM 803-3] (E)	128	AIR 21 B2A/B4P (E)	93
VHLP2.5 (E)	128	AIR 21 B2A/B4P (E)	93
VHLP2.5 (E)	128	AIR 21 B4A/B2P (E)	93
VHLP2.5 (E)	128	AIR 21 B4A/B2P (E)	93
APXVSP18-C-A20 w/ Mount Pipe (E)	118.5	AIR 21 B4A/B2P (E)	93
APXVSP18-C-A20 w/ Mount Pipe (E)	118.5	KRY 112 144/1 TMA (E)	93
P40-16-XLPP-RR-A w/ Mount Pipe (E)	118.5	KRY 112 144/1 TMA (E)	93
TD-RRH8x20-25 (E)	118.5	KRY 112 144/1 TMA (E)	93
TD-RRH8x20-25 (E)	118.5	LNx-6515DS-A1M w/ Mount Pipe (P)	93
TD-RRH8x20-25 (E)	118.5	LNx-6515DS-A1M w/ Mount Pipe (P)	93
1900 MHz (E)	118.5	LNx-6515DS-A1M w/ Mount Pipe (P)	93
1900 MHz (E)	118.5	S11B12 (P)	93
1900 MHz (E)	118.5	S11B12 (P)	93
800 MHz (E)	118.5	S11B12 (P)	93
800 MHz (E)	118.5	Sector Mount [SM 402-3] (E-2 Pipes Included)	93
800 MHz (E)	118.5	Miscellaneous [NA 507-1] (P-MT-195-12)	93
(2) ACU-A20-N RETs (E)	118.5	VSR-TS-B Stabilizer Kit (P)	93
ACU-A20-N RETs (E)	118.5	(2) HBXX-6517DS-A2M w/ Mount Pipe (E)	80
800 MHz Filter (E)	118.5	(2) HBXX-6517DS-A2M w/ Mount Pipe (E)	80
800 MHz Filter (E)	118.5	(2) HBXX-6517DS-A2M w/ Mount Pipe (E)	80
800 MHz Filter (E)	118.5	(2) HBXX-6517DS-A2M w/ Mount Pipe (E)	80
6' x 2" Mount Pipe (E)	118.5	RRH2x60-700 (E)	80
6' x 2" Mount Pipe (E)	118.5	RRH2x60-700 (E)	80
T-Arm Mount [TA 601-3] (E)	118.5	RRH2x60-AWS (E)	80
APXVTM14-C-120 w/ Mount Pipe (E)	118.5	RRH2x60-AWS (E)	80
APXVTM14-C-120 w/ Mount Pipe (E)	118.5	RRH2x60-AWS (E)	80
APXVTM14-C-120 w/ Mount Pipe (E)	118.5	RRH2x60-AWS (E)	80
(2) LGP21401 (E)	110	RRH2x60-PCS (E)	80
(2) LGP21401 (E)	110	RRH2x60-PCS (E)	80
(2) LGP21401 (E)	110	RRH2x60-PCS (E)	80
(2) RRUS-11 1900MHz (E)	110	RRH2x60-PCS (E)	80
(2) RRUS-11 1900MHz (E)	110	(2) DB-T1-6Z-8AB-0Z (E)	80
(2) RRUS-11 1900MHz (E)	110	Sector Mount [SM 104-3] (E)	80
DC6-48-60-18-8F (E)	110	(2) LNX-6514DS-A1M w/ Mount Pipe (E)	80
Sector Mount [SM 409-3] (E)	110	(2) LNX-6514DS-A1M w/ Mount Pipe (E)	80
(P) HPA-65R-BUU-H6	110	(2) LNX-6514DS-A1M w/ Mount Pipe (E)	80
(P) HPA-65R-BUU-H6	110	GPS-QBW-20N (Reference)	55.5
(2) (P) KATH 800-10121	110	GPS (E)	55.5
(2) (P) KATH 800-10121	110	GPS (E)	55.5
(2) (P) KATH 800-10121	110	Side Arm Mount [SO 701-1] (E)	50.5
(2) (P) KATH 800-10121	110	Side Arm Mount [SO 701-1] (E)	50.5
(P) HPA-65R-BUU-H8	110	GPS (E)	50.5
(P) RRUS 12	110	Side Arm Mount [SO 701-1] (E)	50.5
(P) RRUS 12	110	GPS (E)	50.5
(P) RRUS 12	110	Side Arm Mount [SO 701-1] (E)	50.5
(P) RRUS A2	110	GPS (E)	50.5
(P) RRUS A2	110	Side Arm Mount [SO 701-1] (E)	50.5
(P) RRUS A2	110		

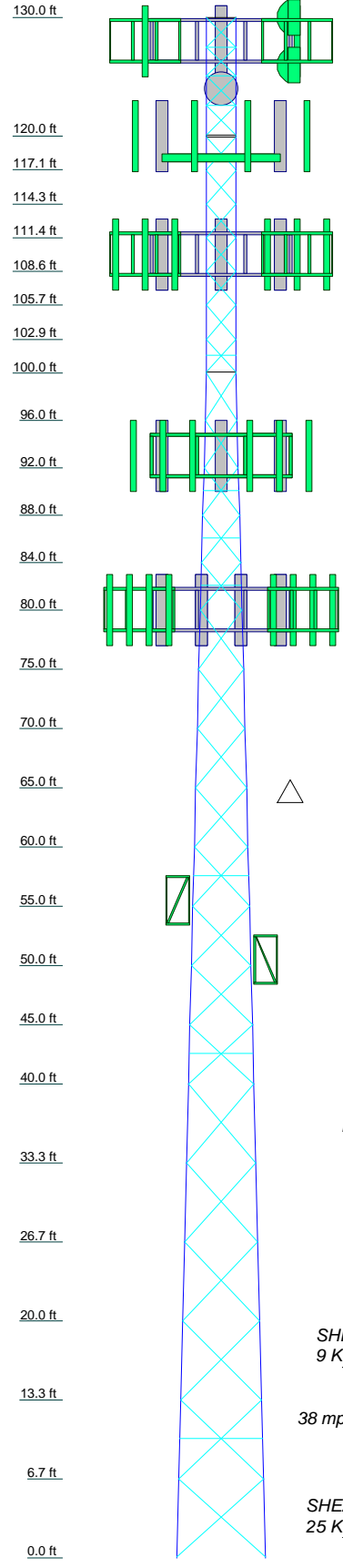
SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	H	2L2x2x3/16x3/8
B	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	J	L1 1/4x1 1/4x3/16
C	BT101341- P6.625x0.280 w/ HP7.625x0.301	J	L2x2x1/8
D	BT101341- P6.625 x .432 w/ HP7.625x0.301	K	L3x3x5/16
E	L1 1/2x1 1/2x3/16	L	1 @ 2.77604
F	L2x2x1/4	M	1 @ 6.58333
G	2L1 1/2x1 1/2x3/16x3/8		

ALLPRO CONSULTING GROUP
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 FAX: 866-364-8375

Job: **16-2859 130 SST**
 Project: **Glastonbury-main st, CT (CT46126-A-01)**
 Client: **SBA Communications Corporation** Drawn by: **mperez** App'd:
 Code: **TIA/EIA-222-F** Date: **08/12/16** Scale: **NTS**
 Path: **P:\2016\Structural\16-2859 CT46126-A-01 Glastonbury Structural Analysis\TNCX146126-A-02 Glastonbury-main st.dwg** Dwg No. **E-1**

Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11	T12	T13	T14	T15	T16	T17	T18	T19	T20	T21	T22	T23	T24	T25	T26	T27
Legs	SR 1 1/2											SR 2															
Leg Grade	A570-45											A500M-54															
Diagonals	SR 1/2											SR 3/4															
Diagonal Grade	L1 1/4x1 1/4x3/16											A36															
Top Girts	L1 1/4x1 1/4x3/16											N.A.															
Bottom Girts	L1 1/4x1 1/4x3/16											N.A.															
Horizontal	L1 1/4x1 1/4x3/16											N.A.															
Sec. Horizontals	N.A.											N.A.															
Face Width (ft)	2.5											4															
# Panels @ (ft)	4 @ 2.47917											5 @ 4															
Weight (K)	0.3											0.4															



SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	H	2L2x2x3/16x3/8
B	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	I	L1 1/4x1 1/4x3/16
C	BT101341- P6.625x0.280 w/ HP7.625x0.301	J	L2x2x1/8
D	BT101341- P6.625x0.280 w/ HP7.625x0.301	K	L3x3x5/16
E	L1 1/2x1 1/2x3/16	L	1 @ 2.77604
F	L2x2x1/4	M	1 @ 6.58333

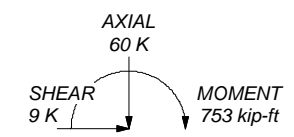
MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A570-45	45 ksi	60 ksi	A500M-54	54 ksi	70 ksi
A36	36 ksi	58 ksi			

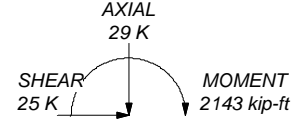
- ### TOWER DESIGN NOTES
1. Tower is located in Hartford County, Connecticut.
 2. Tower designed for a 80 mph basic wind in accordance with the TIA/EIA-222-F Standard.
 3. Tower is also designed for a 38 mph basic wind with 1.00 in ice.
 4. Deflections are based upon a 50 mph wind.
 5. TOWER RATING: 98.7%

MAX. CORNER REACTIONS AT BASE:
 DOWN: 339 K
 SHEAR: 18 K

UPLIFT: -318 K
 SHEAR: 17 K



TORQUE 1 kip-ft
 38 mph WIND - 1.000 in ICE



TORQUE 2 kip-ft
 REACTIONS - 80 mph WIND

ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job: 16-2859 130 SST
	Project: Glastonbury-main st, CT (CT46126-A-01)
	Client: SBA Communications Corporation Drawn by: mperez App'd:
	Code: TIA/EIA-222-F Date: 08/11/16 Scale: NTS
	Path: <small>P:\2016\Structural\16-2859-CT46126-A-01-Glastonbury-Structural-Analysis\TNO\CT46126-A-02-Glastonbury-main st.dwg</small>
	Dwg No. E-1

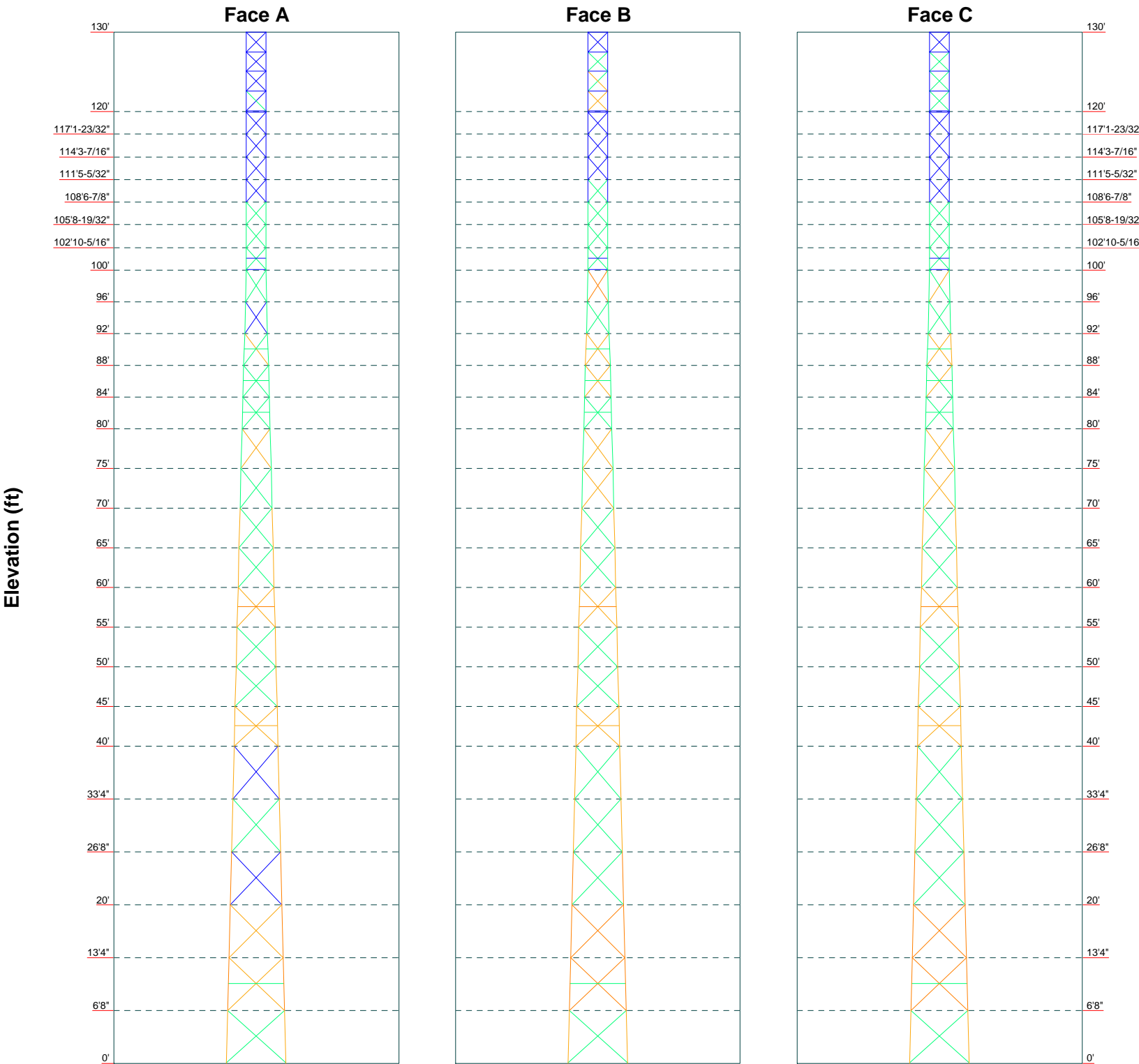


MISCELLANEOUS PLOTS

Stress Distribution Chart

0' - 130'

■ > 100%
 ■ 90%-100%
 ■ 75%-90%
 ■ 50%-75%
 ■ < 50% Overstress



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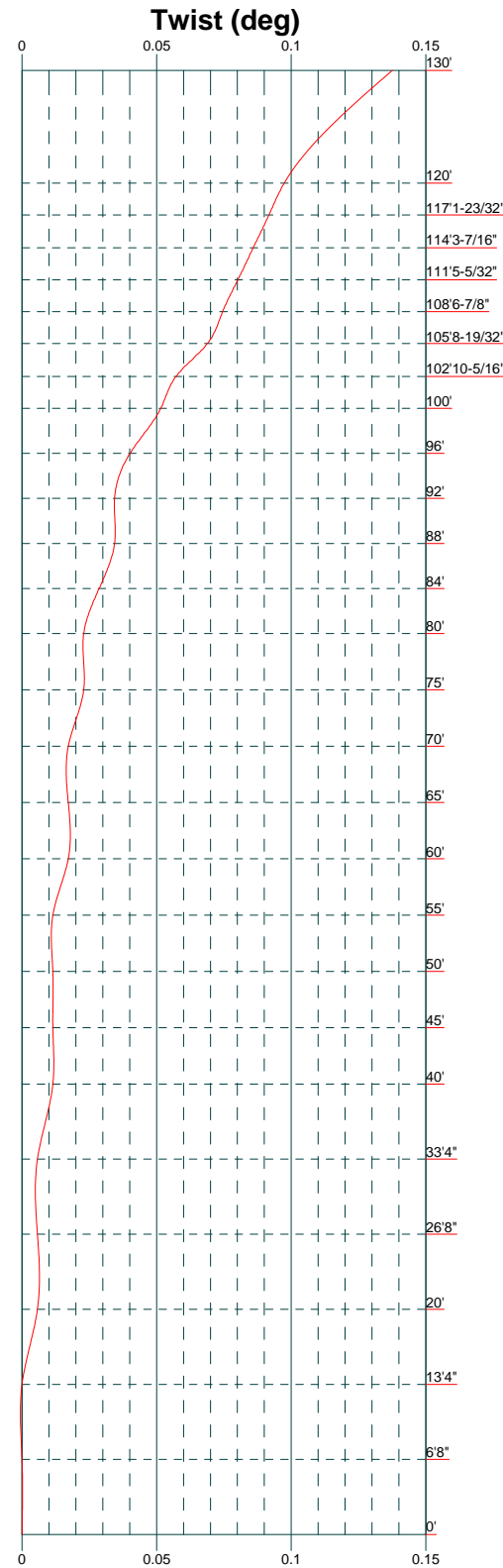
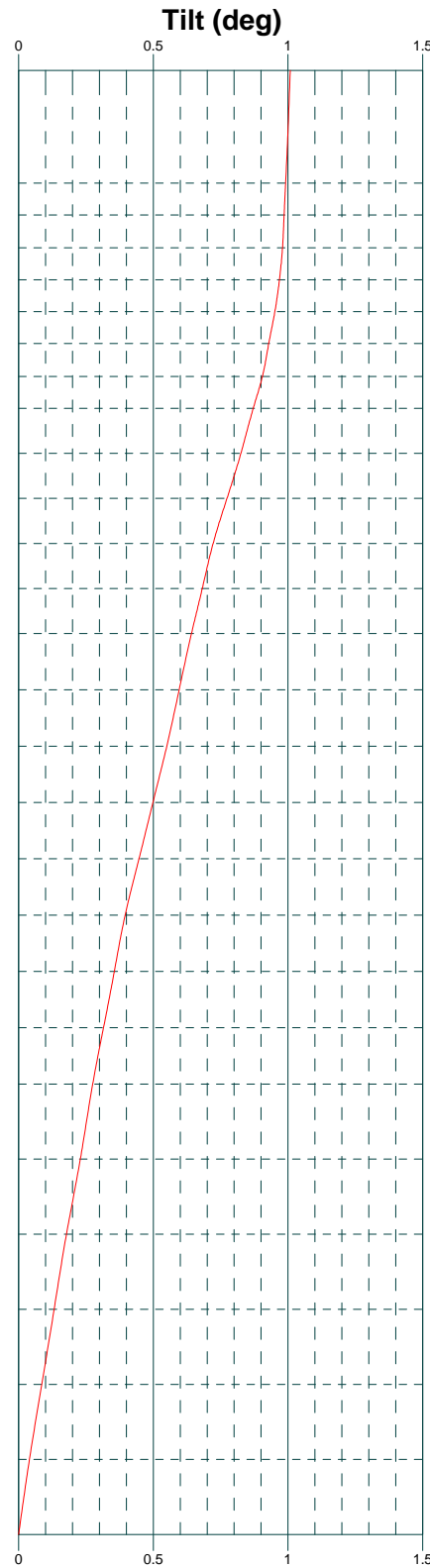
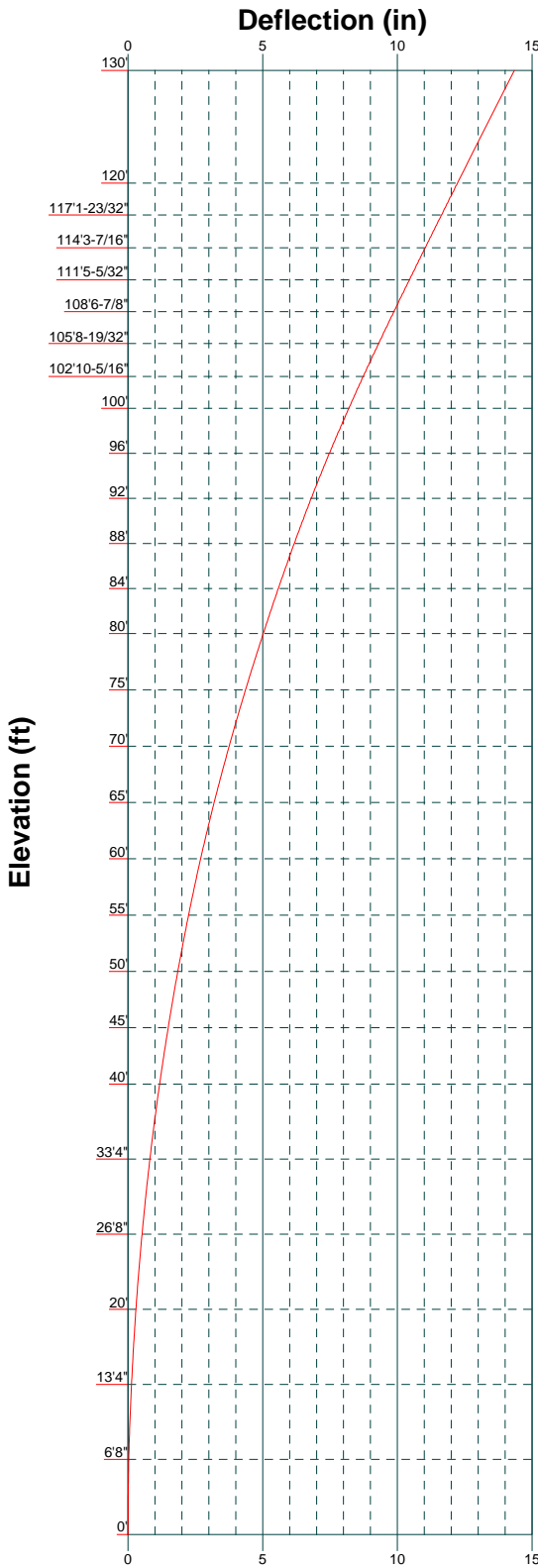
Job: **16-2859 130 SST**

Project: **Glastonbury-main st, CT (CT46126-A-01)**

Client: **SBA Communications Corporation** Drawn by: **mperez** App'd:

Code: **TIA/EIA-222-F** Date: **08/12/16** Scale: **NTS**

Path: P:\2016\Structural\16-2859 CT46126-A-01 Glastonbury Structural Analysis\TNC\CT46126-A-02_Glastonbury-main st.dwg Dwg No. **E-8**



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 FAX: 866-364-8375

Job: 16-2859 130 SST		
Project: Glastonbury-main st, CT (CT46126-A-01)		
Client: SBA Communications Corporation	Drawn by: mperez	App'd:
Code: TIA/EIA-222-F	Date: 08/12/16	Scale: NTS
Path:	Dwg No. E-5	

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CALCULATION PRINTOUT

<p style="text-align: center;"><i>tnxTower</i></p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">1 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Tower Input Data

The main tower is a 3x free standing tower with an overall height of 130' above the ground line.

The base of the tower is set at an elevation of 0' above the ground line.

The face width of the tower is 2'6" at the top and 7'6" at the base.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Hartford County, Connecticut.

Basic wind speed of 80 mph.

Nominal ice thickness of 1.000 in.

Ice density of 56.000 pcf.

A wind speed of 38 mph is used in combination with ice.

Temperature drop of 50.000 °F.

Deflections calculated using a wind speed of 50 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

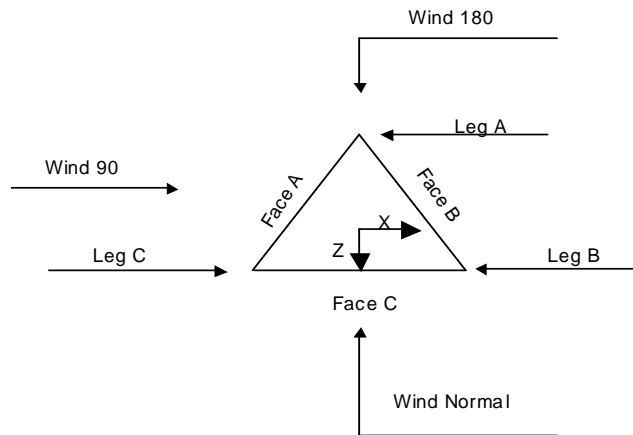
Stress ratio used in tower member design is 1.333.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

<ul style="list-style-type: none"> Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification √ Use Code Stress Ratios √ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile √ Include Bolts In Member Capacity Leg Bolts Are At Top Of Section √ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric 	<ul style="list-style-type: none"> Distribute Leg Loads As Uniform Assume Legs Pinned √ Assume Rigid Index Plate √ Use Clear Spans For Wind Area √ Use Clear Spans For KL/r Retention Guys To Initial Tension √ Bypass Mast Stability Checks √ Use Azimuth Dish Coefficients √ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination √ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder 	<ul style="list-style-type: none"> Use ASCE 10 X-Brace Ly Rules √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA √ SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable √ Offset Girt At Foundation √ Consider Feed Line Torque √ Include Angle Block Shear Check Use TIA-222-G Bracing Resist. Exemption Use TIA-222-G Tension Splice Exemption
		<p>Poles</p> <ul style="list-style-type: none"> Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 2 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
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Triangular Tower

Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	<i>ft</i>			<i>ft</i>		<i>ft</i>
T1	130'-120'			2'6"	1	10'
T2	120'-117'1-23/32"			2'6"	1	2'10-9/32"
T3	117'1-23/32"-114'3-7/16"			2'6"	1	2'10-9/32"
T4	114'3-7/16"-111'5-5/32"			2'6"	1	2'10-9/32"
T5	111'5-5/32"-108'6-7/8"			2'6"	1	2'10-9/32"
T6	108'6-7/8"-105'8-19/32"			2'6"	1	2'10-9/32"
T7	105'8-19/32"-102'10-5/16"			2'6"	1	2'10-9/32"
T8	102'10-5/16"-100'96"			2'6"	1	2'10-5/16"
T9	100'-96'			2'6"	1	4'
T10	96'-92'			2'8-13/32"	1	4'
T11	92'-88'			2'10-13/16"	1	4'
T12	88'-84'			3'1-3/16"	1	4'
T13	84'-80'			3'3-19/32"	1	4'
T14	80'-75'			3'6"	1	5'
T15	75'-70'			3'9"	1	5'
T16	70'-65'			4'	1	5'
T17	65'-60'			4'3"	1	5'
T18	60'-55'			4'6"	1	5'
T19	55'-50'			4'9"	1	5'
T20	50'-45'			5'	1	5'
T21	45'-40'			5'3"	1	5'

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job	16-2859 130 SST	Page	3 of 45
	Project	Glastonbury-main st, CT (CT46126-A-01)	Date	11:19:26 08/11/16
	Client	SBA Communications Corporation	Designed by	mperez

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T22	40'-33'4"			5'6"	1	6'8"
T23	33'4"-26'8"			5'10"	1	6'8"
T24	26'8"-20'			6'2"	1	6'8"
T25	20'-13'4"			6'6"	1	6'8"
T26	13'4"-6'8"			6'10"	1	6'8"
T27	6'8"-0'			7'2"	1	6'8"

Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	130'-120'	2'5-3/4"	X Brace	No	Yes	0.000	1.000
T2	120'-117'1-23/32"	2'9-9/32"	X Brace	No	Yes	1.000	0.000
T3	117'1-23/32"-114'3-7/16"	2'9-9/32"	X Brace	No	Yes	1.000	0.000
T4	114'3-7/16"-111'5-5/32"	2'10-9/32"	X Brace	No	Yes	0.000	0.000
T5	111'5-5/32"-108'6-7/8"	2'10-9/32"	X Brace	No	Yes	0.000	0.000
T6	108'6-7/8"-105'8-19/32"	2'10-9/32"	X Brace	No	Yes	0.000	0.000
T7	105'8-19/32"-102'10-5/16"	2'10-9/32"	X Brace	No	Yes	0.000	0.000
T8	102'10-5/16"-100'	2'9-5/16"	X Brace	No	Yes	0.000	1.000
T9	100'-96'	4'	X Brace	No	Yes	0.000	0.000
T10	96'-92'	4'	X Brace	No	Yes	0.000	0.000
T11	92'-88'	4'	X Brace	No	Yes	0.000	0.000
T12	88'-84'	4'	X Brace	No	Yes	0.000	0.000
T13	84'-80'	4'	X Brace	No	Yes	0.000	0.000
T14	80'-75'	5'	X Brace	No	Yes	0.000	0.000
T15	75'-70'	5'	X Brace	No	Yes	0.000	0.000
T16	70'-65'	5'	X Brace	No	Yes	0.000	0.000
T17	65'-60'	5'	X Brace	No	Yes	0.000	0.000
T18	60'-55'	5'	X Brace	No	Yes	0.000	0.000
T19	55'-50'	5'	X Brace	No	Yes	0.000	0.000
T20	50'-45'	5'	X Brace	No	Yes	0.000	0.000
T21	45'-40'	5'	X Brace	No	Yes	0.000	0.000
T22	40'-33'4"	6'8"	X Brace	No	Yes	0.000	0.000
T23	33'4"-26'8"	6'8"	X Brace	No	Yes	0.000	0.000
T24	26'8"-20'	6'8"	X Brace	No	Yes	0.000	0.000
T25	20'-13'4"	6'8"	X Brace	No	Yes	0.000	0.000
T26	13'4"-6'8"	6'8"	X Brace	No	Yes	0.000	0.000
T27	6'8"-0'	6'7"	X Brace	No	Yes	0.000	1.000

Tower Section Geometry (cont'd)

Tower Elevation	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
ft						
T1 130'-120'	Solid Round	1 1/2	A570-45	Solid Round	1/2	A36

<p style="text-align: center;"><i>tnxTower</i></p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">4 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T2 120'-117'-23/32"	Solid Round	2	(45 ksi) A570-45	Solid Round	3/4	(36 ksi) A36
T3 117'-23/32"-114' 3-7/16"	Solid Round	2	(45 ksi) A570-45	Solid Round	3/4	(36 ksi) A36
T4 114'-3-7/16"-111' -5/32"	Solid Round	2	(45 ksi) A570-45	Solid Round	3/4	(36 ksi) A36
T5 111'-5-5/32"-108' -7/8"	Solid Round	2	(45 ksi) A570-45	Solid Round	3/4	(36 ksi) A36
T6 108'-6-7/8"-105' 8-19/32"	Solid Round	2	(45 ksi) A570-45	Solid Round	3/4	(36 ksi) A36
T7 105'-8-19/32"-102' 10-5/16"	Solid Round	2	(45 ksi) A570-45	Solid Round	3/4	(36 ksi) A36
T8 102'-10-5/16"-100'	Solid Round	2	(45 ksi) A570-45	Solid Round	3/4	(36 ksi) A36
T9 100'-96'	Pipe	P4.5 x 0.237	A500M-54 (54 ksi)	Equal Angle	L1 1/2x1 1/2x3/16	(36 ksi) A36
T10 96'-92'	Pipe	P4.5 x 0.237	A500M-54 (54 ksi)	Equal Angle	L2x2x1/4	(36 ksi) A36
T11 92'-88'	Pipe	P4.5 x 0.237	A500M-54 (54 ksi)	Double Equal Angle	2L1 1/2x1 1/2x3/16x3/8	(36 ksi) A36
T12 88'-84'	Pipe	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	A500M-54 (54 ksi)	Double Equal Angle	2L1 1/2x1 1/2x3/16x3/8	(36 ksi) A36
T13 84'-80'	Pipe	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	A500M-54 (54 ksi)	Double Equal Angle	2L1 1/2x1 1/2x3/16x3/8	(36 ksi) A36
T14 80'-75'	Pipe	P6.625x0.280	A500M-54 (54 ksi)	Equal Angle	L2x2x1/4	(36 ksi) A36
T15 75'-70'	Pipe	P6.625x0.280	A500M-54 (54 ksi)	Double Equal Angle	2L1 1/2x1 1/2x3/16x3/8	(36 ksi) A36
T16 70'-65'	Pipe	P6.625x0.280	A500M-54 (54 ksi)	Double Equal Angle	2L1 1/2x1 1/2x3/16x3/8	(36 ksi) A36
T17 65'-60'	Pipe	P6.625x0.280	A500M-54 (54 ksi)	Double Equal Angle	2L1 1/2x1 1/2x3/16x3/8	(36 ksi) A36
T18 60'-55'	Pipe	P6.625x0.280	A500M-54 (54 ksi)	Double Equal Angle	2L1 1/2x1 1/2x3/16x3/8	(36 ksi) A36
T19 55'-50'	Pipe	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	A500M-54 (54 ksi)	Double Equal Angle	2L1 1/2x1 1/2x3/16x3/8	(36 ksi) A36
T20 50'-45'	Pipe	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	A500M-54 (54 ksi)	Double Equal Angle	2L1 1/2x1 1/2x3/16x3/8	(36 ksi) A36
T21 45'-40'	Pipe	BT101341- P6.625x0.280 w/ HP7.625x0.301	A500M-54 (54 ksi)	Equal Angle	L2x2x1/4	(36 ksi) A36
T22 40'-33'4"	Pipe	P6.625x.432	A500M-54 (54 ksi)	Double Equal Angle	2L1 3/4x1 3/4x3/16x3/8	(36 ksi) A36
T23 33'4"-26'8"	Pipe	P6.625x.432	A500M-54 (54 ksi)	Double Equal Angle	2L1 3/4x1 3/4x3/16x3/8	(36 ksi) A36
T24 26'8"-20'	Pipe	P6.625x.432	A500M-54 (54 ksi)	Double Equal Angle	2L1 3/4x1 3/4x3/16x3/8	(36 ksi) A36
T25 20'-13'4"	Pipe	P6.625x.432	A500M-54 (54 ksi)	Equal Angle	L2x2x3/16	(36 ksi) A36
T26 13'4"-6'8"	Pipe	P6.625x.432	A500M-54 (54 ksi)	Equal Angle	L2x2x3/16	(36 ksi) A36
T27 6'8"-0'	Pipe	BT101341- P6.625 x .432 w/ HP7.625x0.301	A500M-54 (54 ksi)	Double Equal Angle	2L2x2x3/16x3/8	(36 ksi) A36

<p style="text-align: center;"><i>tnxTower</i></p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	Job 16-2859 130 SST	Page 5 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 130'-120'	Equal Angle	L1 1/4x1 1/4x3/16	A36 (36 ksi)	Equal Angle	L1 1/4x1 1/4x3/16	A36 (36 ksi)
T2 120'-117'-23/32"	Equal Angle	L1 1/4x1 1/4x3/16	A36 (36 ksi)	Equal Angle		A36 (36 ksi)
T8 102'10'-5/16"-100'	Solid Round		A36 (36 ksi)	Equal Angle	L1 1/4x1 1/4x3/16	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T1 130'-120'	None	Flat Bar		A36 (36 ksi)	Equal Angle	L1 1/4x1 1/4x3/16	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Secondary Horizontal Type	Secondary Horizontal Size	Secondary Horizontal Grade	Inner Bracing Type	Inner Bracing Size	Inner Bracing Grade
T8 102'10'-5/16"-100'	Equal Angle	L2x2x1/8	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)
T11 92'-88'	Flat Bar	4x3/8	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)
T12 88'-84'	Flat Bar	4x3/8	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)
T13 84'-80'	Flat Bar	4x3/8	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)
T18 60'-55'	Equal Angle	L2x2x1/8	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)
T21 45'-40'	Equal Angle	L3x3x5/16	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)
T26 13'4"-6'8"	Equal Angle	L2x2x1/4	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)

Tower Section Geometry (cont'd)

<p style="text-align: center;"><i>tnxTower</i></p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">6 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A_f	Adjust. Factor A_r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
ft	ft ²	in							
T1 130'-120'	0.000	0.000	A36 (36 ksi)	1	1	1.05	0.000	0.000	36.000
T2 120'-117'-23/32"	0.000	0.000	A36 (36 ksi)	1	1	1.05	0.000	0.000	36.000
T3 117'-23/32"-14'3-7/16"	0.000	0.000	A36 (36 ksi)	1	1	1.05	0.000	0.000	36.000
T4 114'3-7/16"-11'5-5/32"	0.000	0.000	A36 (36 ksi)	1	1	1.05	0.000	0.000	36.000
T5 111'5-5/32"-10'8'-7/8"	0.000	0.000	A36 (36 ksi)	1	1	1.05	0.000	0.000	36.000
T6 108'6-7/8"-105'8-19/32"	0.000	0.000	A36 (36 ksi)	1	1	1.05	0.000	0.000	36.000
T7 105'8-19/32"-102'10-5/16"	0.000	0.000	A36 (36 ksi)	1	1	1.05	0.000	0.000	36.000
T8 102'10-5/16"-100'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T9 100'-96'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T10 96'-92'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T11 92'-88'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T12 88'-84'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T13 84'-80'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T14 80'-75'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T15 75'-70'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T16 70'-65'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T17 65'-60'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T18 60'-55'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T19 55'-50'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T20 50'-45'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T21 45'-40'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T22 40'-33'4"	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T23 33'4"-26'8"	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T24 26'8"-20'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T25 20'-13'4"	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000
T26 13'4"-6'8"	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 7 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A_f	Adjust. Factor A_r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
ft	ft ²	in							
T27 6'8"-0'	0.000	0.000	A36 (36 ksi)	1.05	1	1.05	0.000	0.000	36.000

Tower Section Geometry (cont'd)

Tower Elevation	Calc K Single Angles	Calc K Solid Rounds	Legs	K Factors ¹							
				X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace	
											X
ft				Y	Y	Y	Y	Y	Y	Y	Y
T1 130'-120'	Yes	Yes	1	1	1	1	1	1	1	1	1
T2 120'-117'-23/32"	Yes	Yes	1	1	1	1	1	1	1	1	1
T3 117'-23/32"-114'3-7/16"	Yes	Yes	1	1	1	1	1	1	1	1	1
T4 114'3-7/16"-11'5-5/32"	Yes	Yes	1	1	1	1	1	1	1	1	1
T5 111'5-5/32"-108'6-7/8"	Yes	Yes	1	1	1	1	1	1	1	1	1
T6 108'6-7/8"-105'8-19/32"	Yes	Yes	1	1	1	1	1	1	1	1	1
T7 105'8-19/32"-102'10-5/16"	Yes	Yes	1	1	1	1	1	1	1	1	1
T8 102'10-5/16"-100'	Yes	No	1	1	1	1	1	1	1	1	1
T9 100'-96'	Yes	No	1	1	1	1	1	1	1	1	1
T10 96'-92'	Yes	No	1	1	1	1	1	1	1	1	1
T11 92'-88'	No	No	1	1	1	1	1	1	0.5	1	1
T12 88'-84'	No	No	1	1	1	1	1	1	0.5	1	1
T13 84'-80'	No	No	1	1	1	1	1	1	0.5	1	1
T14 80'-75'	Yes	No	1	1	1	1	1	1	1	1	1
T15 75'-70'	Yes	No	1	1	1	1	1	1	1	1	1
T16 70'-65'	Yes	No	1	1	1	1	1	1	1	1	1
T17 65'-60'	Yes	No	1	1	1	1	1	1	1	1	1
T18 60'-55'	No	No	1	1	1	1	1	1	0.5	1	1
T19 55'-50'	Yes	No	1	1	1	1	1	1	0.5	1	1

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">9 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T12 88'-84'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T13 84'-80'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T14 80'-75'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T15 75'-70'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T16 70'-65'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T17 65'-60'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T18 60'-55'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T19 55'-50'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T20 50'-45'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T21 45'-40'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T22 40'-33'4"	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T23 33'4"-26'8"	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T24 26'8"-20'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T25 20'-13'4"	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T26 13'4"-6'8"	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T27 6'8"-0'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75

Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1 130'-120'	Flange	1.000	1	0.500	0	0.625	0	0.625	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T2 120'-117'1"-23/32"	Flange	0.750	0	0.500	0	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T3 117'1"-23/32"-14'3"-7/16"	Flange	0.750	0	0.500	0	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T4 114'3"-7/16"-11'5"-5/32"	Flange	0.750	0	0.500	0	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T5 111'5"-5/32"-10'8"-7/8"	Flange	0.750	0	0.500	0	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T6 108'6"-7/8"-105'8"-19/32"	Flange	0.750	0	0.500	0	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T7 105'8"-19/32"-102'10"-5/16"	Flange	0.750	0	0.500	0	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T8 102'10"-5/16"-100'	Flange	0.750	4	0.500	0	0.625	0	0.625	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T9 100'-96'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T10 96'-92'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325X		A325N		A325N		A325N		A325N		A325N	

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 10 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T11 92'-88'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	1
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T12 88'-84'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	1
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T13 84'-80'	Flange	1.000	8	0.500	1	0.625	0	0.625	0	0.625	0	0.625	0	0.500	1
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T14 80'-75'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325X		A325N		A325N		A325N		A325N		A325N	
T15 75'-70'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T16 70'-65'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T17 65'-60'	Flange	1.000	8	0.500	1	0.625	0	0.625	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T18 60'-55'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	1
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T19 55'-50'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T20 50'-45'	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T21 45'-40'	Flange	1.000	8	0.500	1	0.625	0	0.625	0	0.625	0	0.625	0	0.500	1
		A325N		A325X		A325N		A325N		A325N		A325N		A325N	
T22 40'-33'4"	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T23 33'4"-26'8"	Flange	1.000	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T24 26'8"-20'	Flange	1.000	8	0.500	1	0.625	0	0.625	0	0.625	0	0.625	0	0.500	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T25 20'-13'4"	Flange	1.500	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.500	0
		A36M-55		A325X		A325N		A325N		A325N		A325N		A325N	
T26 13'4"-6'8"	Flange	1.500	0	0.500	1	0.625	0	0.000	0	0.625	0	0.625	0	0.625	1
		A36M-55		A325X		A325N		A325N		A325N		A325N		A325N	
T27 6'8"-0'	Flange	1.500	6	0.500	1	0.625	0	0.625	0	0.625	0	0.625	0	0.500	0
		A36M-55		A325N		A325N		A325N		A325N		A325N		A325N	

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight klf
ATCB-B01-04 0(5/16") (E-Inside Conduit)	A	Yes	Ar (CfAe)	128' - 6'	0.000	0.2	6	6	0.315	0.000		0.000
LDF4-50A(1/ 2") (E-Inside Conduit)	A	Yes	Ar (CfAe)	128' - 6'	0.000	0.2	2	2	0.500 0.630	0.000		0.000
2" Rigid Conduit (E)	A	Yes	Ar (CfAe)	128' - 0'	0.000	0.2	2	2	2.000	2.000		0.003
LDF4P-50A(1 /2") (E)	A	Yes	Ar (CfAe)	128' - 6'	0.000	0.1	2	2	0.630	0.630		0.000

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 11 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight klf
LDF4P-50A(1/2") (E) Feedline Ladder (Af) (E) *R*	A	Yes	Ar (CfAe)	50'6" - 6'	0.000	0.02	2	2	0.630	0.630		0.000
LDF6-50A(1-1/4") (E) Feedline Ladder (Af) (E) *R*	B	Yes	Ar (CfAe)	118'6" - 6'	-1.000	0	4	4	0.850 0.750	1.550		0.001
LDF6-50A(1-1/4") (E) Feedline Ladder (Af) (E) *R*	B	Yes	Af (CfAe)	118'6" - 0'	-1.000	0	1	1	3.000	3.000	12.000	0.008
LDF6-50A(1-1/4") (E) Feedline Ladder (Af) (E) *R*	C	Yes	Ar (CfAe)	110' - 6'	-1.000	0	18	6	0.850 0.750	1.550		0.001
LDF6-50A(1-1/4") (E) Feedline Ladder (Af) (E) *R*	C	Yes	Af (CfAe)	60' - 0'	-1.000	0	2	1	3.000 1.500	3.000	12.000	0.008
LDF6-50A(1-1/4") (E) Feedline Ladder (Af) (E) *R*	C	Yes	Af (CfAe)	93' - 60'	-1.000	0	1	1	3.000 1.500	3.000	12.000	0.008
LDF7-50A(1 5/8") (E)	B	Yes	Ar (CfAe)	80' - 6'	-1.000	0.1	2	2	0.850 0.750	1.980		0.001
LDF4P-50A(1/2") (E) *R*	B	Yes	Ar (CfAe)	55'6" - 6'	-1.000	-0.08	1	1	0.630	0.630		0.000
Safety Line 3/8 (E) *R*	B	Yes	Ar (CfAe)	130' - 0'	0.000	-0.5	1	1	0.375	0.375		0.000
*****(P) 3/8"	C	Yes	Ar (CfAe)	110' - 6'	0.000	0	18	6	0.250	0.440		0.000
(P) (1/2") FIBER	C	Yes	Ar (CfAe)	110' - 6'	0.000	0	36	12	0.250	0.630		0.000

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	C _{AA} ft ² /ft	Weight klf
R							

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
T1	130'-120'	A	3.507	0.000	0.000	0.000	0.053

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">12 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
		B	0.313	0.000	0.000	0.000	0.002
		C	0.000	0.000	0.000	0.000	0.000
T2	120'-117'1-23/32"	A	1.252	0.000	0.000	0.000	0.019
		B	0.790	0.339	0.000	0.000	0.016
		C	0.000	0.000	0.000	0.000	0.000
T3	117'1-23/32"-114' 3-7/16"	A	1.252	0.000	0.000	0.000	0.019
		B	1.565	0.714	0.000	0.000	0.032
		C	0.000	0.000	0.000	0.000	0.000
T4	114'3-7/16"-111'5- 5/32"	A	1.252	0.000	0.000	0.000	0.019
		B	1.565	0.714	0.000	0.000	0.032
		C	0.000	0.000	0.000	0.000	0.000
T5	111'5-5/32"-108'6- 7/8"	A	1.252	0.000	0.000	0.000	0.019
		B	1.565	0.714	0.000	0.000	0.032
		C	2.319	0.000	0.000	0.000	0.032
T6	108'6-7/8"-105'8-1 9/32"	A	1.252	0.000	0.000	0.000	0.019
		B	1.565	0.714	0.000	0.000	0.032
		C	4.642	0.000	0.000	0.000	0.064
T7	105'8-19/32"-102' 10-5/16"	A	1.252	0.000	0.000	0.000	0.019
		B	1.565	0.714	0.000	0.000	0.032
		C	4.642	0.000	0.000	0.000	0.064
T8	102'10-5/16"-100'	A	1.253	0.000	0.000	0.000	0.019
		B	1.567	0.715	0.000	0.000	0.032
		C	4.646	0.000	0.000	0.000	0.064
T9	100'-96'	A	1.753	0.000	0.000	0.000	0.027
		B	2.192	1.000	0.000	0.000	0.045
		C	6.500	0.000	0.000	0.000	0.089
T10	96'-92'	A	1.753	0.000	0.000	0.000	0.027
		B	2.192	1.000	0.000	0.000	0.045
		C	6.500	0.250	0.000	0.000	0.098
T11	92'-88'	A	1.753	0.000	0.000	0.000	0.027
		B	2.192	1.000	0.000	0.000	0.045
		C	6.500	1.000	0.000	0.000	0.123
T12	88'-84'	A	1.753	0.000	0.000	0.000	0.027
		B	2.192	1.000	0.000	0.000	0.045
		C	6.500	1.000	0.000	0.000	0.123
T13	84'-80'	A	1.753	0.000	0.000	0.000	0.027
		B	2.192	1.000	0.000	0.000	0.045
		C	6.500	1.000	0.000	0.000	0.123
T14	80'-75'	A	2.192	0.000	0.000	0.000	0.033
		B	4.390	1.250	0.000	0.000	0.065
		C	8.125	1.250	0.000	0.000	0.154
T15	75'-70'	A	2.192	0.000	0.000	0.000	0.033
		B	4.390	1.250	0.000	0.000	0.065
		C	8.125	1.250	0.000	0.000	0.154
T16	70'-65'	A	2.192	0.000	0.000	0.000	0.033
		B	4.390	1.250	0.000	0.000	0.065
		C	8.125	1.250	0.000	0.000	0.154
T17	65'-60'	A	2.192	0.000	0.000	0.000	0.033
		B	4.390	1.250	0.000	0.000	0.065
		C	8.125	1.250	0.000	0.000	0.154
T18	60'-55'	A	2.192	1.250	0.000	0.000	0.075
		B	4.416	1.250	0.000	0.000	0.065
		C	8.125	1.250	0.000	0.000	0.196
T19	55'-50'	A	2.244	1.250	0.000	0.000	0.075
		B	4.652	1.250	0.000	0.000	0.065
		C	8.125	1.250	0.000	0.000	0.196
T20	50'-45'	A	2.717	1.250	0.000	0.000	0.077
		B	4.652	1.250	0.000	0.000	0.065
		C	8.125	1.250	0.000	0.000	0.196
T21	45'-40'	A	2.717	1.250	0.000	0.000	0.077
		B	4.652	1.250	0.000	0.000	0.065

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job	16-2859 130 SST	Page	13 of 45
	Project	Glastonbury-main st, CT (CT46126-A-01)	Date	11:19:26 08/11/16
	Client	SBA Communications Corporation	Designed by	mperez

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
T22	40'-33'4"	C	8.125	1.250	0.000	0.000	0.196
		A	3.622	1.667	0.000	0.000	0.102
		B	6.203	1.667	0.000	0.000	0.087
T23	33'4"-26'8"	C	10.833	1.667	0.000	0.000	0.261
		A	3.622	1.667	0.000	0.000	0.102
		B	6.203	1.667	0.000	0.000	0.087
T24	26'8"-20'	C	10.833	1.667	0.000	0.000	0.261
		A	3.622	1.667	0.000	0.000	0.102
		B	6.203	1.667	0.000	0.000	0.087
T25	20'-13'4"	C	10.833	1.667	0.000	0.000	0.261
		A	3.622	1.667	0.000	0.000	0.102
		B	6.203	1.667	0.000	0.000	0.087
T26	13'4"-6'8"	C	10.833	1.667	0.000	0.000	0.261
		A	3.622	1.667	0.000	0.000	0.102
		B	6.203	1.667	0.000	0.000	0.087
T27	6'8"-0'	C	10.833	1.667	0.000	0.000	0.261
		A	2.362	1.667	0.000	0.000	0.094
		B	0.808	1.667	0.000	0.000	0.060
		C	1.083	1.667	0.000	0.000	0.127

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
T1	130'-120'	A	1.000	7.087	4.890	0.000	0.000	0.180
		B		1.979	0.000	0.000	0.000	0.019
		C		0.000	0.000	0.000	0.000	0.000
T2	120'-117'-23/32"	A	1.000	2.531	1.746	0.000	0.000	0.064
		B		0.967	1.304	0.000	0.000	0.043
		C		0.000	0.000	0.000	0.000	0.000
T3	117'-23/32"-114' 3-7/16"	A	1.000	2.531	1.746	0.000	0.000	0.064
		B		1.411	2.746	0.000	0.000	0.086
		C		0.000	0.000	0.000	0.000	0.000
T4	114'-3-7/16"-111'5- 5/32"	A	1.000	2.531	1.746	0.000	0.000	0.064
		B		1.411	2.746	0.000	0.000	0.086
		C		0.000	0.000	0.000	0.000	0.000
T5	111'5-5/32"-108'6- 7/8"	A	1.000	2.531	1.746	0.000	0.000	0.064
		B		1.411	2.746	0.000	0.000	0.086
		C		1.025	2.989	0.000	0.000	0.115
T6	108'6-7/8"-105'8-1 9/32"	A	1.000	2.531	1.746	0.000	0.000	0.064
		B		1.411	2.746	0.000	0.000	0.086
		C		2.052	5.983	0.000	0.000	0.230
T7	105'8-19/32"-102' 10-5/16"	A	1.000	2.531	1.746	0.000	0.000	0.064
		B		1.411	2.746	0.000	0.000	0.086
		C		2.052	5.983	0.000	0.000	0.230
T8	102'10-5/16"-100'	A	1.000	2.533	1.748	0.000	0.000	0.064
		B		1.412	2.748	0.000	0.000	0.086
		C		2.054	5.988	0.000	0.000	0.230
T9	100'-96'	A	1.000	3.543	2.445	0.000	0.000	0.090
		B		1.975	3.844	0.000	0.000	0.120
		C		2.873	8.377	0.000	0.000	0.322
T10	96'-92'	A	1.000	3.543	2.445	0.000	0.000	0.090
		B		1.975	3.844	0.000	0.000	0.120
		C		2.873	8.738	0.000	0.000	0.337
T11	92'-88'	A	1.000	3.543	2.445	0.000	0.000	0.090
		B		1.975	3.844	0.000	0.000	0.120
		C		2.873	9.821	0.000	0.000	0.381

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">14 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
T12	88'-84'	A	1.000	3.543	2.445	0.000	0.000	0.090
		B		1.975	3.844	0.000	0.000	0.120
		C		2.873	9.821	0.000	0.000	0.381
T13	84'-80'	A	1.000	3.543	2.445	0.000	0.000	0.090
		B		1.975	3.844	0.000	0.000	0.120
		C		2.873	9.821	0.000	0.000	0.381
T14	80'-75'	A	1.000	4.429	3.056	0.000	0.000	0.113
		B		4.127	5.985	0.000	0.000	0.192
		C		3.592	12.276	0.000	0.000	0.476
T15	75'-70'	A	1.000	4.429	3.056	0.000	0.000	0.113
		B		4.127	5.985	0.000	0.000	0.192
		C		3.592	12.276	0.000	0.000	0.476
T16	70'-65'	A	1.000	4.429	3.056	0.000	0.000	0.113
		B		4.127	5.985	0.000	0.000	0.192
		C		3.592	12.276	0.000	0.000	0.476
T17	65'-60'	A	1.000	4.429	3.056	0.000	0.000	0.113
		B		4.127	5.985	0.000	0.000	0.192
		C		3.592	12.276	0.000	0.000	0.476
T18	60'-55'	A	1.000	4.429	4.862	0.000	0.000	0.185
		B		4.237	5.985	0.000	0.000	0.193
		C		3.592	12.276	0.000	0.000	0.548
T19	55'-50'	A	1.000	4.539	4.914	0.000	0.000	0.187
		B		5.223	5.985	0.000	0.000	0.203
		C		3.592	12.276	0.000	0.000	0.548
T20	50'-45'	A	1.000	5.525	5.387	0.000	0.000	0.203
		B		5.223	5.985	0.000	0.000	0.203
		C		3.592	12.276	0.000	0.000	0.548
T21	45'-40'	A	1.000	5.525	5.387	0.000	0.000	0.203
		B		5.223	5.985	0.000	0.000	0.203
		C		3.592	12.276	0.000	0.000	0.548
T22	40'-33'4"	A	1.000	7.367	7.182	0.000	0.000	0.270
		B		6.964	7.980	0.000	0.000	0.270
		C		4.789	16.369	0.000	0.000	0.731
T23	33'4"-26'8"	A	1.000	7.367	7.182	0.000	0.000	0.270
		B		6.964	7.980	0.000	0.000	0.270
		C		4.789	16.369	0.000	0.000	0.731
T24	26'8"-20'	A	1.000	7.367	7.182	0.000	0.000	0.270
		B		6.964	7.980	0.000	0.000	0.270
		C		4.789	16.369	0.000	0.000	0.731
T25	20'-13'4"	A	1.000	7.367	7.182	0.000	0.000	0.270
		B		6.964	7.980	0.000	0.000	0.270
		C		4.789	16.369	0.000	0.000	0.731
T26	13'4"-6'8"	A	1.000	7.367	7.182	0.000	0.000	0.270
		B		6.964	7.980	0.000	0.000	0.270
		C		4.789	16.369	0.000	0.000	0.731
T27	6'8"-0'	A	1.000	2.737	4.885	0.000	0.000	0.200
		B		1.884	2.965	0.000	0.000	0.126
		C		0.479	3.804	0.000	0.000	0.248

Feed Line Shielding

Section	Elevation ft	Face	A _R ft ²	A _R Ice ft ²	A _F ft ²	A _F Ice ft ²
T1	130'-120'	A	0.165	3.809	0.183	0.624
		B	0.015	0.629	0.016	0.103
		C	0.000	0.000	0.000	0.000

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">15 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Section	Elevation	Face	A_R	A_R	A_F	A_F
			ft^2	Ice ft^2	ft^2	Ice ft^2
T2	120'-117'1-23/32"	A	0.082	1.274	0.046	0.156
		B	0.074	0.699	0.041	0.086
		C	0.000	0.000	0.000	0.000
T3	117'1-23/32"-114'3-7/16"	A	0.082	1.025	0.000	0.000
		B	0.149	1.034	0.000	0.000
		C	0.000	0.000	0.000	0.000
T4	114'3-7/16"-111'5-5/32"	A	0.083	1.042	0.000	0.000
		B	0.151	1.051	0.000	0.000
		C	0.000	0.000	0.000	0.000
T5	111'5-5/32"-108'6-7/8"	A	0.083	1.042	0.000	0.000
		B	0.151	1.051	0.000	0.000
		C	0.154	0.978	0.000	0.000
T6	108'6-7/8"-105'8-19/32"	A	0.083	1.042	0.000	0.000
		B	0.151	1.051	0.000	0.000
		C	0.308	1.957	0.000	0.000
T7	105'8-19/32"-102'10-5/16"	A	0.083	1.042	0.000	0.000
		B	0.151	1.051	0.000	0.000
		C	0.308	1.957	0.000	0.000
T8	102'10-5/16"-100'	A	0.082	1.524	0.119	0.405
		B	0.149	1.538	0.216	0.409
		C	0.304	2.864	0.440	0.762
T9	100'-96'	A	0.000	0.915	0.201	0.687
		B	0.000	0.924	0.366	0.693
		C	0.000	1.720	0.745	1.290
T10	96'-92'	A	0.000	0.870	0.255	0.870
		B	0.000	0.878	0.464	0.878
		C	0.000	1.695	0.981	1.695
T11	92'-88'	A	0.000	1.081	0.329	1.123
		B	0.000	1.091	0.598	1.133
		C	0.000	2.332	1.406	2.422
T12	88'-84'	A	0.000	1.048	0.322	1.098
		B	0.000	1.058	0.585	1.108
		C	0.000	2.261	1.375	2.369
T13	84'-80'	A	0.000	1.020	0.315	1.077
		B	0.000	1.029	0.574	1.086
		C	0.000	2.200	1.349	2.323
T14	80'-75'	A	0.000	0.850	0.249	0.850
		B	0.000	1.180	0.640	1.180
		C	0.000	1.834	1.065	1.834
T15	75'-70'	A	0.000	0.815	0.179	0.611
		B	0.000	1.131	0.460	0.848
		C	0.000	1.757	0.765	1.318
T16	70'-65'	A	0.000	0.784	0.172	0.588
		B	0.000	1.088	0.443	0.816
		C	0.000	1.691	0.737	1.268
T17	65'-60'	A	0.000	0.758	0.166	0.568
		B	0.000	1.052	0.428	0.789
		C	0.000	1.634	0.712	1.226
T18	60'-55'	A	0.000	1.258	0.368	1.023
		B	0.000	1.381	0.606	1.123
		C	0.000	2.123	1.003	1.727
T19	55'-50'	A	0.000	0.929	0.250	0.697
		B	0.000	1.097	0.423	0.823
		C	0.000	1.542	0.671	1.156
T20	50'-45'	A	0.000	1.042	0.277	0.782
		B	0.000	1.070	0.412	0.802
		C	0.000	1.504	0.655	1.128
T21	45'-40'	A	0.000	1.392	0.559	1.578
		B	0.000	1.429	0.832	1.620
		C	0.000	2.008	1.322	2.277
T22	40'-33'4"	A	0.000	1.152	0.357	1.008

<p style="text-align: center;"><i>tnxTower</i></p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p style="text-align: center;">Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p style="text-align: center;">Page</p> <p style="text-align: center;">16 of 45</p>
	<p style="text-align: center;">Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p style="text-align: center;">Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p style="text-align: center;">Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p style="text-align: center;">Designed by</p> <p style="text-align: center;">mperez</p>

Section	Elevation	Face	A_R	A_R	A_F	A_F
	ft		ft ²	Ice ft ²	ft ²	Ice ft ²
T23	33'4"-26'8"	B	0.000	1.182	0.532	1.034
		C	0.000	1.662	0.844	1.454
		A	0.000	1.115	0.346	0.976
T24	26'8"-20'	B	0.000	1.145	0.515	1.001
		C	0.000	1.609	0.817	1.408
		A	0.000	1.083	0.336	0.948
T25	20'-13'4"	B	0.000	1.112	0.500	0.973
		C	0.000	1.563	0.794	1.367
		A	0.000	1.055	0.374	1.055
T26	13'4"-6'8"	B	0.000	1.083	0.556	1.083
		C	0.000	1.522	0.884	1.522
		A	0.000	1.403	0.497	1.403
T27	6'8"-0'	B	0.000	1.440	0.740	1.440
		C	0.000	2.025	1.176	2.025
		A	0.000	0.537	0.271	0.537
		B	0.000	0.351	0.166	0.351
		C	0.000	0.313	0.185	0.313

Feed Line Center of Pressure

Section	Elevation	CP_x	CP_z	CP_x	CP_z
	ft	in	in	Ice in	Ice in
T1	130'-120'	-0.978	-1.909	-0.043	-0.507
T2	120'-117'1-23/32"	-0.126	-2.131	0.145	-0.722
T3	117'1-23/32"-114'3-7/16"	0.705	-2.568	0.403	-1.215
T4	114'3-7/16"-111'5-5/32"	0.703	-2.559	0.402	-1.197
T5	111'5-5/32"-108'6-7/8"	0.545	0.147	0.341	-0.058
T6	108'6-7/8"-105'8-19/32"	0.445	1.863	0.296	0.781
T7	105'8-19/32"-102'10-5/16"	0.445	1.863	0.296	0.781
T8	102'10-5/16"-100'	0.366	1.533	0.294	0.631
T9	100'-96'	0.333	1.339	0.270	0.677
T10	96'-92'	0.351	1.383	0.295	0.736
T11	92'-88'	0.346	1.475	0.307	0.812
T12	88'-84'	0.380	1.547	0.327	0.852
T13	84'-80'	0.412	1.617	0.347	0.891
T14	80'-75'	0.868	1.550	0.450	0.938
T15	75'-70'	1.002	1.741	0.517	1.028
T16	70'-65'	1.082	1.837	0.559	1.082
T17	65'-60'	1.162	1.931	0.601	1.136
T18	60'-55'	0.853	1.361	0.369	0.720
T19	55'-50'	1.021	1.441	0.579	0.620
T20	50'-45'	0.907	1.369	0.550	0.591
T21	45'-40'	0.804	1.185	0.506	0.587
T22	40'-33'4"	1.026	1.475	0.630	0.628
T23	33'4"-26'8"	1.101	1.543	0.675	0.649
T24	26'8"-20'	1.176	1.610	0.720	0.670
T25	20'-13'4"	1.217	1.634	0.753	0.688
T26	13'4"-6'8"	1.194	1.574	0.730	0.691
T27	6'8"-0'	-0.283	-1.824	-0.052	-1.863

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job	16-2859 130 SST	Page	17 of 45
	Project	Glastonbury-main st, CT (CT46126-A-01)	Date	11:19:26 08/11/16
	Client	SBA Communications Corporation	Designed by	mperez

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft		C _{AA} Front ft ²	C _{AA} Side ft ²	Weight K
LLPX310R w/ Mount Pipe (E)	A	From Leg	4.000	0.000	128'	No Ice	5.065	2.985	0.045
			0'			1/2" Ice	5.480	3.528	0.083
			0'			1" Ice	5.905	4.087	0.126
LLPX310R w/ Mount Pipe (E)	B	From Leg	4.000	0.000	128'	No Ice	5.065	2.985	0.045
			0'			1/2" Ice	5.480	3.528	0.083
			0'			1" Ice	5.905	4.087	0.126
840 10054 w/ Mount Pipe (E)	C	From Leg	4.000	0.000	128'	No Ice	5.413	2.385	0.051
			0'			1/2" Ice	5.833	2.917	0.088
			0'			1" Ice	6.263	3.466	0.129
24"x14"x9" (E)	A	From Leg	4.000	0.000	128'	No Ice	3.442	2.639	0.064
			0'			1/2" Ice	3.696	2.870	0.091
			0'			1" Ice	3.959	3.111	0.122
24"x14"x9" (E)	B	From Leg	4.000	0.000	128'	No Ice	3.442	2.639	0.064
			0'			1/2" Ice	3.696	2.870	0.091
			0'			1" Ice	3.959	3.111	0.122
24"x14"x9" (E)	C	From Leg	4.000	0.000	128'	No Ice	3.442	2.639	0.064
			0'			1/2" Ice	3.696	2.870	0.091
			0'			1" Ice	3.959	3.111	0.122
TIMING 2000 (E)	C	From Leg	4.000	0.000	128'	No Ice	0.126	0.126	0.001
			0'			1/2" Ice	0.177	0.177	0.002
			0'			1" Ice	0.237	0.237	0.005
MODEM (E)	A	From Leg	4.000	0.000	128'	No Ice	0.130	0.107	0.002
			0'			1/2" Ice	0.183	0.157	0.003
			-4'			1" Ice	0.244	0.215	0.005
MODEM (E)	B	From Leg	4.000	0.000	128'	No Ice	0.130	0.107	0.002
			0'			1/2" Ice	0.183	0.157	0.003
			-4'			1" Ice	0.244	0.215	0.005
MODEM (E)	C	From Leg	4.000	0.000	128'	No Ice	0.130	0.107	0.002
			0'			1/2" Ice	0.183	0.157	0.003
			-4'			1" Ice	0.244	0.215	0.005
Sector Mount [SM 803-3] (E)	C	None		0.000	128'	No Ice	40.400	40.400	0.985
						1/2" Ice	51.200	51.200	1.226
						1" Ice	62.000	62.000	1.467
R									
APXVTM14-C-120 w/ Mount Pipe (E)	A	From Leg	4.000	0.000	118'6"	No Ice	7.134	4.959	0.077
			0'			1/2" Ice	7.662	5.754	0.131
			1'6"			1" Ice	8.183	6.472	0.193
APXVTM14-C-120 w/ Mount Pipe (E)	B	From Leg	4.000	0.000	118'6"	No Ice	7.134	4.959	0.077
			0'			1/2" Ice	7.662	5.754	0.131
			1'6"			1" Ice	8.183	6.472	0.193
APXVTM14-C-120 w/ Mount Pipe (E)	C	From Leg	4.000	0.000	118'6"	No Ice	7.134	4.959	0.077
			0'			1/2" Ice	7.662	5.754	0.131
			1'6"			1" Ice	8.183	6.472	0.193
APXVSPP18-C-A20 w/ Mount Pipe (E)	A	From Leg	4.000	0.000	118'6"	No Ice	8.498	6.946	0.083
			0'			1/2" Ice	9.149	8.127	0.151
			0'			1" Ice	9.767	9.021	0.227
APXVSPP18-C-A20 w/ Mount Pipe (E)	B	From Leg	4.000	0.000	118'6"	No Ice	8.498	6.946	0.083
			0'			1/2" Ice	9.149	8.127	0.151
			0'			1" Ice	9.767	9.021	0.227
P40-16-XLPP-RR-A w/ Mount Pipe	C	From Leg	4.000	0.000	118'6"	No Ice	9.373	4.825	0.073
			0'			1/2" Ice	9.912	5.571	0.136

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 18 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Lateral					
(E)									
TD-RRH8x20-25	A	From Leg	4.000	0'	0.000	118'6"	1" Ice 10.450	6.265	0.205
(E)				0'			No Ice 4.720	1.703	0.070
(E)				1'6"			1/2" Ice 5.014	1.920	0.097
TD-RRH8x20-25	B	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				1'6"			1/2" Ice 5.014	1.920	0.097
TD-RRH8x20-25	C	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				1'6"			1/2" Ice 5.014	1.920	0.097
1900 MHz	A	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
1900 MHz	B	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
1900 MHz	C	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
800 MHz	A	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
800 MHz	B	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
800 MHz	C	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
800 MHz	A	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
800 MHz	B	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
800 MHz	C	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
(2) ACU-A20-N RETs	A	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
ACU-A20-N RETs	B	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
ACU-A20-N RETs	C	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
800 MHz Filter	A	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
800 MHz Filter	B	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
800 MHz Filter	C	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
6' x 2" Mount Pipe	A	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
6' x 2" Mount Pipe	B	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
6' x 2" Mount Pipe	C	From Leg	4.000	0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097
T-Arm Mount [TA 601-3]	C	None		0'	0.000	118'6"	1" Ice 5.316	2.145	0.128
(E)				0'			No Ice 4.720	1.703	0.070
(E)				0'			1/2" Ice 5.014	1.920	0.097

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job	16-2859 130 SST	Page	20 of 45
	Project	Glastonbury-main st, CT (CT46126-A-01)	Date	11:19:26 08/11/16
	Client	SBA Communications Corporation	Designed by	mperez

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA}		Weight
			Horz	Vert			Front	Side	
			ft	ft	°	ft	ft ²	ft ²	K
KRY 112 144/1 TMA (E)	B	From Leg	4.000	0.000	93'	No Ice	0.411	0.189	0.011
			0'			1/2" Ice	0.500	0.256	0.014
			0'			1" Ice	0.597	0.332	0.018
KRY 112 144/1 TMA (E)	C	From Leg	4.000	0.000	93'	No Ice	0.411	0.189	0.011
			0'			1/2" Ice	0.500	0.256	0.014
			0'			1" Ice	0.597	0.332	0.018
LNX-6515DS-A1M w/ Mount Pipe (P)	A	From Leg	4.000	0.000	93'	No Ice	11.683	9.842	0.083
			0'			1/2" Ice	12.404	11.366	0.173
			0'			1" Ice	13.135	12.914	0.273
LNX-6515DS-A1M w/ Mount Pipe (P)	B	From Leg	4.000	0.000	93'	No Ice	11.683	9.842	0.083
			0'			1/2" Ice	12.404	11.366	0.173
			0'			1" Ice	13.135	12.914	0.273
LNX-6515DS-A1M w/ Mount Pipe (P)	C	From Leg	4.000	0.000	93'	No Ice	11.683	9.842	0.083
			0'			1/2" Ice	12.404	11.366	0.173
			0'			1" Ice	13.135	12.914	0.273
S11B12 (P)	A	From Leg	4.000	0.000	93'	No Ice	3.306	1.361	0.051
			0'			1/2" Ice	3.550	1.540	0.072
			0'			1" Ice	3.802	1.728	0.096
S11B12 (P)	B	From Leg	4.000	0.000	93'	No Ice	3.306	1.361	0.051
			0'			1/2" Ice	3.550	1.540	0.072
			0'			1" Ice	3.802	1.728	0.096
S11B12 (P)	C	From Leg	4.000	0.000	93'	No Ice	3.306	1.361	0.051
			0'			1/2" Ice	3.550	1.540	0.072
			0'			1" Ice	3.802	1.728	0.096
Sector Mount [SM 402-3] (E-2 Pipes Included)	C	None		0.000	93'	No Ice	18.910	18.910	0.851
						1/2" Ice	26.780	26.780	1.233
						1" Ice	34.650	34.650	1.616
Miscellaneous [NA 507-1] (P-MT-195-12)	C	None		0.000	93'	No Ice	4.800	4.800	0.245
						1/2" Ice	6.700	6.700	0.294
						1" Ice	8.600	8.600	0.343
VSR-TS-B Stabilizer Kit (P)	C	None		0.000	93'	No Ice	14.500	14.500	0.376
						1/2" Ice	17.400	17.400	0.396
						1" Ice	20.300	20.300	0.417
R									
(2) LNX-6514DS-A1M w/ Mount Pipe (E)	A	From Leg	4.000	0.000	80'	No Ice	8.648	7.082	0.065
			0'			1/2" Ice	9.305	8.273	0.134
			0'			1" Ice	9.930	9.185	0.211
(2) LNX-6514DS-A1M w/ Mount Pipe (E)	B	From Leg	4.000	0.000	80'	No Ice	8.648	7.082	0.065
			0'			1/2" Ice	9.305	8.273	0.134
			0'			1" Ice	9.930	9.185	0.211
(2) LNX-6514DS-A1M w/ Mount Pipe (E)	C	From Leg	4.000	0.000	80'	No Ice	8.648	7.082	0.065
			0'			1/2" Ice	9.305	8.273	0.134
			0'			1" Ice	9.930	9.185	0.211
(2) HBXX-6517DS-A2M w/ Mount Pipe (E)	A	From Leg	4.000	0.000	80'	No Ice	8.976	6.963	0.067
			0'			1/2" Ice	9.647	8.182	0.137
			0'			1" Ice	10.291	9.144	0.215
(2) HBXX-6517DS-A2M w/ Mount Pipe (E)	B	From Leg	4.000	0.000	80'	No Ice	8.976	6.963	0.067
			0'			1/2" Ice	9.647	8.182	0.137
			0'			1" Ice	10.291	9.144	0.215
(2) HBXX-6517DS-A2M w/ Mount Pipe (E)	C	From Leg	4.000	0.000	80'	No Ice	8.976	6.963	0.067
			0'			1/2" Ice	9.647	8.182	0.137
			0'			1" Ice	10.291	9.144	0.215
RRH2x60-700 (E)	A	From Leg	4.000	0.000	80'	No Ice	3.957	1.816	0.060
			0'			1/2" Ice	4.272	2.075	0.083
			0'			1" Ice	4.596	2.360	0.109
RRH2x60-700 (E)	B	From Leg	4.000	0.000	80'	No Ice	3.957	1.816	0.060
			0'			1/2" Ice	4.272	2.075	0.083

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job	16-2859 130 SST	Page	21 of 45
	Project	Glastonbury-main st, CT (CT46126-A-01)	Date	11:19:26 08/11/16
	Client	SBA Communications Corporation	Designed by	mperez

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Vert					
			ft	ft	°	ft	ft ²	ft ²	K
RRH2x60-700 (E)	C	From Leg	0'	4.000	0.000	80'	1" Ice 4.596	2.360	0.109
			No Ice 3.957	1.816	0.060				
			1/2" Ice 4.272	2.075	0.083				
RRH2x60-AWS (E)	A	From Leg	0'	4.000	0.000	80'	1" Ice 4.596	2.360	0.109
			No Ice 3.957	1.816	0.060				
			1/2" Ice 4.272	2.075	0.083				
RRH2x60-AWS (E)	B	From Leg	0'	4.000	0.000	80'	1" Ice 4.596	2.360	0.109
			No Ice 3.957	1.816	0.060				
			1/2" Ice 4.272	2.075	0.083				
RRH2x60-AWS (E)	C	From Leg	0'	4.000	0.000	80'	1" Ice 4.596	2.360	0.109
			No Ice 3.957	1.816	0.060				
			1/2" Ice 4.272	2.075	0.083				
RRH2X60-PCS (E)	A	From Leg	0'	4.000	0.000	80'	1" Ice 4.596	2.360	0.109
			No Ice 2.567	2.011	0.055				
			1/2" Ice 2.791	2.218	0.075				
RRH2X60-PCS (E)	B	From Leg	0'	4.000	0.000	80'	1" Ice 3.025	2.435	0.099
			No Ice 2.567	2.011	0.055				
			1/2" Ice 2.791	2.218	0.075				
RRH2X60-PCS (E)	C	From Leg	0'	4.000	0.000	80'	1" Ice 3.025	2.435	0.099
			No Ice 2.567	2.011	0.055				
			1/2" Ice 2.791	2.218	0.075				
(2) DB-T1-6Z-8AB-0Z (E)	C	From Leg	0'	4.000	0.000	80'	1" Ice 3.025	2.435	0.099
			No Ice 5.600	2.333	0.044				
			1/2" Ice 5.915	2.558	0.080				
Sector Mount [SM 104-3] (E)	C	None	0'		0.000	80'	1" Ice 6.240	2.791	0.120
			No Ice 30.020	30.020	0.953				
			1/2" Ice 40.480	40.480	1.405				
R GPS-QBW-20N (Reference)	C	From Leg	0'	3.000	0.000	55'6"	1" Ice 0.273	0.273	0.005
			No Ice 0.151	0.151	0.000				
			1/2" Ice 0.208	0.208	0.002				
GPS (E)	C	From Leg	0'	3.000	0.000	55'6"	1" Ice 0.273	0.273	0.005
			No Ice 0.151	0.151	0.000				
			1/2" Ice 0.208	0.208	0.002				
Side Arm Mount [SO 701-1] (E)	C	From Leg	0'	1.500	0.000	55'6"	1" Ice 0.273	0.273	0.005
			No Ice 0.850	1.670	0.065				
			1/2" Ice 1.140	2.340	0.079				
R GPS (E)	A	From Leg	0'	3.000	0.000	50'6"	1" Ice 0.273	0.273	0.005
			No Ice 0.151	0.151	0.000				
			1/2" Ice 0.208	0.208	0.002				
GPS (E)	B	From Leg	0'	3.000	0.000	50'6"	1" Ice 0.273	0.273	0.005
			No Ice 0.151	0.151	0.000				
			1/2" Ice 0.208	0.208	0.002				
Side Arm Mount [SO 701-1] (E)	A	From Leg	0'	1.500	0.000	50'6"	1" Ice 0.273	0.273	0.005
			No Ice 0.850	1.670	0.065				
			1/2" Ice 1.140	2.340	0.079				
Side Arm Mount [SO 701-1] (E)	B	From Leg	0'	1.500	0.000	50'6"	1" Ice 0.273	0.273	0.005
			No Ice 0.850	1.670	0.065				
			1/2" Ice 1.140	2.340	0.079				
R ***** (P) HPA-65R-BUU-H6	A	From Leg	0'	4.000	0.000	110'	1" Ice 11.263	6.405	0.164
			No Ice 10.122	5.486	0.043				
			1/2" Ice 10.688	5.942	0.100				
(P) HPA-65R-BUU-H6	B	From Leg	0'	4.000	0.000	110'	1" Ice 11.263	6.405	0.164
			No Ice 10.122	5.486	0.043				
			1/2" Ice 10.688	5.942	0.100				

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job	16-2859 130 SST	Page	22 of 45
	Project	Glastonbury-main st, CT (CT46126-A-01)	Date	11:19:26 08/11/16
	Client	SBA Communications Corporation	Designed by	mperez

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Lateral					
(2) (P) KATH 800-10121	C	From Leg	4.000	0.000	110'	1/2" Ice	10.688	5.942	0.100
			0'			1" Ice	11.263	6.405	0.164
			0'			No Ice	5.458	3.293	0.046
			0'			1/2" Ice	5.882	3.639	0.079
(2) (P) KATH 800-10121	A	From Leg	4.000	0.000	110'	1" Ice	6.315	3.994	0.117
			0'			No Ice	5.458	3.293	0.046
			0'			1/2" Ice	5.882	3.639	0.079
			0'			1" Ice	6.315	3.994	0.117
(2) (P) KATH 800-10121	B	From Leg	4.000	0.000	110'	No Ice	5.458	3.293	0.046
			0'			1/2" Ice	5.882	3.639	0.079
			0'			1" Ice	6.315	3.994	0.117
(P) HPA-65R-BUU-H8	C	From Leg	4.000	0.000	110'	No Ice	5.162	3.293	0.046
			0'			1/2" Ice	5.664	3.716	0.079
			0'			1" Ice	6.166	4.139	0.112
(P) RRUS 12	A	From Leg	3.500	0.000	110'	No Ice	1.488	3.669	0.058
			0'			1/2" Ice	1.673	3.926	0.081
			0'			1" Ice	1.866	4.191	0.108
(P) RRUS 12	B	From Leg	3.500	0.000	110'	No Ice	1.488	3.669	0.058
			0'			1/2" Ice	1.673	3.926	0.081
			0'			1" Ice	1.866	4.191	0.108
(P) RRUS 12	C	From Leg	3.500	0.000	110'	No Ice	1.488	3.669	0.058
			0'			1/2" Ice	1.673	3.926	0.081
			0'			1" Ice	1.866	4.191	0.108
(P) RRUS A2	A	From Leg	3.500	0.000	110'	No Ice	2.411	0.533	0.022
			0'			1/2" Ice	2.619	0.665	0.035
			0'			1" Ice	2.837	0.806	0.050
(P) RRUS A2	B	From Leg	3.500	0.000	110'	No Ice	2.411	0.533	0.022
			0'			1/2" Ice	2.619	0.665	0.035
			0'			1" Ice	2.837	0.806	0.050
(P) RRUS A2	C	From Leg	3.500	0.000	110'	No Ice	2.411	0.533	0.022
			0'			1/2" Ice	2.619	0.665	0.035
			0'			1" Ice	2.837	0.806	0.050
(4) (P) Kathrein 860-10025 RET	A	From Leg	3.500	0.000	110'	No Ice	0.110	0.100	0.001
			0'			1/2" Ice	0.190	0.170	0.002
			0'			1" Ice	0.270	0.240	0.003
(4) (P) Kathrein 860-10025 RET	B	From Leg	3.500	0.000	110'	No Ice	0.110	0.100	0.001
			0'			1/2" Ice	0.190	0.170	0.002
			0'			1" Ice	0.270	0.240	0.003
(4) (P) Kathrein 860-10025 RET	C	From Leg	3.500	0.000	110'	No Ice	0.110	0.100	0.001
			0'			1/2" Ice	0.190	0.170	0.002
			0'			1" Ice	0.270	0.240	0.003
(2) (P) Powerwave LGP21901	A	From Leg	3.500	0.000	110'	No Ice	0.230	0.110	0.000
			0'			1/2" Ice	0.320	0.180	0.000
			0'			1" Ice	0.410	0.250	0.000
(2) (P) Powerwave LGP21901	B	From Leg	3.500	0.000	110'	No Ice	0.230	0.110	0.000
			0'			1/2" Ice	0.320	0.180	0.000
			0'			1" Ice	0.410	0.250	0.000
(2) (P) Powerwave LGP21901	C	From Leg	3.500	0.000	110'	No Ice	0.230	0.110	0.000
			0'			1/2" Ice	0.320	0.180	0.000
			0'			1" Ice	0.410	0.250	0.000

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">23 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight
				Horz Lateral	Vert						
				ft	°	°	ft	ft	ft ²	K	
VHLP2.5 (E)	A	Paraboloid w/Shroud (HP)	From Leg	4.000	0.000	128'	2.917	No Ice	6.681	0.048	
				0'				1/2" Ice	7.069	0.077	
				-4'				1" Ice	7.456	0.106	
VHLP2.5 (E)	B	Paraboloid w/Shroud (HP)	From Leg	4.000	0.000	128'	2.917	No Ice	6.681	0.048	
				0'				1/2" Ice	7.069	0.077	
				2'				1" Ice	7.456	0.106	
VHLP2.5 (E)	B	Paraboloid w/Shroud (HP)	From Leg	4.000	0.000	128'	2.917	No Ice	6.681	0.048	
				0'				1/2" Ice	7.069	0.077	
				-2'				1" Ice	7.456	0.106	

R

Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 24 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Comb. No.	Description
38	Dead+Wind 330 deg - Service

Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T1	130 - 120	Leg	Max Tension	12	8.353	0.039	0.018
			Max. Compression	6	-9.516	-0.122	-0.079
			Max. Mx	5	-0.357	0.159	-0.003
			Max. My	8	-0.467	0.007	0.156
			Max. Vy	10	-1.070	0.132	-0.060
			Max. Vx	2	-1.190	0.021	0.142
		Diagonal	Max Tension	13	1.431	0.000	0.000
			Max. Compression	13	-1.472	0.000	0.000
			Max. Mx	18	0.236	-0.001	0.000
			Max. My	9	-0.964	-0.001	-0.001
			Max. Vy	18	0.002	-0.001	-0.000
			Max. Vx	9	-0.000	0.000	0.000
		Horizontal	Max Tension	10	0.291	0.000	0.000
			Max. Compression	12	-0.257	0.000	0.000
			Max. Mx	14	0.051	-0.004	0.000
			Max. My	9	0.011	0.000	0.000
			Max. Vy	14	0.006	0.000	0.000
			Max. Vx	9	-0.000	0.000	0.000
		Top Girt	Max Tension	6	0.055	0.000	0.000
			Max. Compression	12	-0.061	0.000	0.000
			Max. Mx	14	-0.001	-0.004	0.000
			Max. My	9	0.004	0.000	0.000
			Max. Vy	14	0.006	0.000	0.000
			Max. Vx	9	-0.000	0.000	0.000
Bottom Girt	Max Tension	12	0.235	0.000	0.000		
	Max. Compression	6	-0.208	0.000	0.000		
	Max. Mx	14	0.018	-0.004	0.000		
	Max. My	9	-0.004	0.000	0.000		
	Max. Vy	14	0.006	0.000	0.000		
	Max. Vx	9	-0.000	0.000	0.000		
T2	120 - 117.143	Leg	Max Tension	12	10.548	0.203	0.140
			Max. Compression	6	-12.819	-0.056	-0.037
			Max. Mx	5	-0.176	0.426	-0.004
			Max. My	8	-6.605	-0.022	0.422
			Max. Vy	10	-1.069	0.221	-0.102
			Max. Vx	2	-1.189	0.040	0.242
		Diagonal	Max Tension	8	2.383	0.000	0.000
			Max. Compression	2	-2.302	0.000	0.000
			Max. Mx	6	0.283	-0.003	-0.000
			Max. My	9	-1.065	-0.002	-0.001
			Max. Vy	18	0.003	-0.001	-0.000
			Max. Vx	9	-0.000	0.000	0.000
		Top Girt	Max Tension	10	0.058	0.000	0.000
			Max. Compression	12	-0.031	0.000	0.000
			Max. Mx	14	0.021	-0.004	0.000
			Max. My	9	0.016	0.000	0.000
			Max. Vy	14	0.006	0.000	0.000
			Max. Vx	9	-0.000	0.000	0.000
T3	117.143 - 114.286	Leg	Max Tension	12	16.916	0.239	0.161
			Max. Compression	6	-19.281	0.085	0.057
			Max. Mx	5	13.989	-0.258	0.058

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job	16-2859 130 SST	Page	25 of 45
	Project	Glastonbury-main st, CT (CT46126-A-01)	Date	11:19:26 08/11/16
	Client	SBA Communications Corporation	Designed by	mperez

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T4	114.286 - 111.43	Diagonal	Max. My	8	16.287	-0.018	-0.286
			Max. Vy	10	-2.308	0.251	-0.146
			Max. Vx	2	-2.598	0.018	0.285
			Max Tension	13	3.114	0.000	0.000
			Max. Compression	13	-3.107	0.000	0.000
			Max. Mx	10	-0.074	-0.004	-0.000
			Max. My	8	-2.846	-0.001	-0.002
		Leg	Max. Vy	18	-0.003	-0.002	-0.000
			Max. Vx	8	-0.001	0.000	0.000
			Max Tension	12	23.659	-0.086	-0.057
			Max. Compression	6	-26.000	-0.221	-0.148
			Max. Mx	11	-22.162	0.244	-0.030
			Max. My	2	-25.539	0.022	0.265
			Max. Vy	5	0.119	-0.243	0.027
T5	111.43 - 108.573	Diagonal	Max. Vx	2	-0.136	0.022	0.265
			Max Tension	13	2.869	0.000	0.000
			Max. Compression	13	-2.903	0.000	0.000
			Max. Mx	11	1.524	-0.003	-0.000
			Max. My	9	-2.056	0.001	-0.001
			Max. Vy	19	0.003	-0.002	-0.000
			Max. Vx	9	0.001	0.001	-0.001
		Leg	Max Tension	12	31.058	0.219	0.147
			Max. Compression	6	-34.196	-0.186	-0.124
			Max. Mx	5	-1.453	0.452	-0.007
			Max. My	8	-18.920	0.024	0.477
			Max. Vy	11	-0.505	0.265	-0.000
			Max. Vx	2	-0.525	-0.016	0.267
			Max Tension	13	3.914	0.000	0.000
T6	108.573 - 105.716	Diagonal	Max. Compression	13	-3.911	0.000	0.000
			Max. Mx	11	2.425	-0.004	-0.000
			Max. My	8	-3.293	0.000	-0.002
			Max. Vy	20	0.003	-0.002	-0.000
			Max. Vx	8	-0.001	0.000	0.000
			Max Tension	12	40.858	0.191	0.127
			Max. Compression	6	-44.659	-0.046	-0.021
		Leg	Max. Mx	11	-3.472	0.265	-0.000
			Max. My	2	20.436	-0.016	0.267
			Max. Vy	11	0.106	0.265	-0.000
			Max. Vx	2	0.106	-0.016	0.267
			Max Tension	13	4.896	0.000	0.000
			Max. Compression	13	-4.966	0.000	0.000
			Max. Mx	11	2.635	-0.005	-0.000
T7	105.716 - 102.859	Diagonal	Max. My	8	-4.374	0.000	-0.002
			Max. Vy	19	0.004	-0.002	-0.000
			Max. Vx	8	-0.001	0.000	0.000
			Max Tension	12	52.520	0.037	0.016
			Max. Compression	6	-56.490	0.034	0.017
			Max. Mx	11	-3.845	0.189	-0.013
			Max. My	13	-3.056	0.084	0.170
		Leg	Max. Vy	11	-0.080	0.189	-0.013
			Max. Vx	3	-0.078	-0.083	0.169
			Max Tension	13	4.839	0.000	0.000
			Max. Compression	13	-4.894	0.000	0.000
			Max. Mx	11	2.245	-0.005	-0.000
			Max. My	8	-4.515	0.001	-0.003
			Max. Vy	11	-0.004	-0.005	-0.000
Max. Vx	8	-0.001	0.000	0.000			

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 26 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T8	102.859 - 100	Leg	Max Tension	12	69.316	0.065	0.032	
			Max. Compression	6	-73.555	-0.353	-0.223	
			Max. Mx	10	-72.599	0.365	-0.195	
			Max. My	2	-72.743	0.029	0.412	
			Max. Vy	10	-3.622	0.365	-0.195	
			Max. Vx	2	-4.115	0.029	0.412	
			Diagonal	Max Tension	13	5.018	-0.002	0.001
				Max. Compression	13	-5.131	0.000	0.000
				Max. Mx	6	3.785	-0.006	0.002
				Max. My	8	-2.778	0.005	-0.003
				Max. Vy	6	0.004	-0.006	0.002
				Max. Vx	8	0.002	0.005	-0.003
		Secondary Horizontal	Max Tension	6	1.161	0.000	0.000	
			Max. Compression	6	-1.161	0.010	-0.004	
			Max. Mx	12	0.612	0.023	-0.002	
			Max. My	2	1.148	0.009	-0.004	
			Max. Vy	12	0.019	0.023	-0.002	
			Max. Vx	2	-0.003	0.009	-0.004	
			Bottom Girt	Max Tension	12	0.877	0.000	0.000
				Max. Compression	6	-0.875	0.000	0.000
				Max. Mx	14	0.048	-0.004	0.000
				Max. My	9	-0.015	0.000	0.000
				Max. Vy	14	0.006	0.000	0.000
				Max. Vx	9	-0.000	0.000	0.000
T9	100 - 96	Leg	Max Tension	12	72.865	-0.419	-0.018	
			Max. Compression	6	-76.726	1.211	0.042	
			Max. Mx	12	72.811	-1.226	-0.036	
			Max. My	9	-3.725	0.001	1.638	
			Max. Vy	12	0.225	-1.226	-0.036	
			Max. Vx	9	-0.392	0.001	1.638	
		Diagonal	Max Tension	8	3.943	0.038	0.008	
			Max. Compression	2	-4.091	0.000	0.000	
			Max. Mx	13	2.204	0.041	0.001	
			Max. My	13	-3.815	-0.029	-0.016	
			Max. Vy	13	0.018	0.041	0.001	
			Max. Vx	13	0.007	0.000	0.000	
T10	96 - 92	Leg	Max Tension	12	84.481	-1.226	-0.036	
			Max. Compression	6	-89.534	0.087	0.011	
			Max. Mx	12	84.481	-1.226	-0.036	
			Max. My	9	-4.177	0.001	1.638	
			Max. Vy	6	0.536	1.211	0.042	
			Max. Vx	7	0.672	-0.045	-1.307	
		Diagonal	Max Tension	7	4.581	0.096	-0.004	
			Max. Compression	13	-4.898	0.000	0.000	
			Max. Mx	11	-2.535	-0.129	0.005	
			Max. My	9	-3.604	-0.095	0.016	
			Max. Vy	11	0.057	0.000	0.000	
			Max. Vx	9	-0.007	-0.095	0.016	
T11	92 - 88	Leg	Max Tension	12	92.637	-0.225	-0.008	
			Max. Compression	6	-98.484	3.535	-0.004	
			Max. Mx	6	-98.484	3.535	-0.004	
			Max. My	11	-5.242	-0.198	-1.882	
			Max. Vy	6	2.717	3.535	-0.004	
			Max. Vx	13	-0.962	-0.180	1.878	
		Diagonal	Max Tension	8	7.220	-0.056	-0.001	
			Max. Compression	2	-7.547	0.000	0.000	
			Max. Mx	6	2.207	-0.081	0.011	
			Max. My	9	-3.650	0.066	-0.023	
			Max. Vy	6	0.036	-0.081	0.011	
			Max. Vx	8	0.009	0.078	-0.023	

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 27 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T12	88 - 84	Secondary Horizontal	Max Tension	13	3.042	-0.080	0.007	
			Max. Compression	13	-2.884	0.062	-0.006	
			Max. Mx	11	1.854	-0.113	0.003	
		Leg	Max. My	13	3.042	-0.080	0.007	
			Max. Vy	11	-0.079	-0.113	0.003	
			Max. Vx	13	0.004	-0.080	0.007	
			Max Tension	12	105.721	1.732	-0.018	
			Max. Compression	6	-112.145	3.772	-0.002	
			Max. Mx	6	-112.145	3.772	-0.002	
			Max. My	11	-5.560	-0.198	-1.882	
			Max. Vy	6	-3.018	3.772	-0.002	
			Max. Vx	11	-1.033	-0.198	-1.882	
			Diagonal	Max Tension	8	6.792	-0.039	-0.002
				Max. Compression	2	-7.023	0.000	0.000
				Max. Mx	6	1.635	-0.057	0.006
Max. My	3	2.475		-0.052	0.016			
Max. Vy	6	0.026		-0.057	0.006			
Max. Vx	3	-0.006		0.000	0.000			
T13	84 - 80	Secondary Horizontal	Max Tension	13	3.797	-0.051	0.004	
			Max. Compression	13	-3.539	0.028	-0.004	
			Max. Mx	11	2.069	-0.076	0.002	
		Leg	Max. My	13	3.797	-0.051	0.004	
			Max. Vy	11	-0.052	-0.076	0.002	
			Max. Vx	13	0.003	0.000	0.000	
			Max Tension	12	117.755	1.626	-0.013	
			Max. Compression	6	-124.599	3.652	-0.007	
			Max. Mx	6	-124.599	3.652	-0.007	
			Max. My	11	-5.851	-0.140	-1.620	
			Max. Vy	6	-2.855	3.652	-0.007	
			Max. Vx	11	-0.868	-0.140	-1.620	
			Diagonal	Max Tension	8	5.981	-0.046	-0.016
				Max. Compression	2	-6.180	0.000	0.000
				Max. Mx	7	3.116	-0.054	-0.012
Max. My	7	-5.771		0.036	-0.020			
Max. Vy	7	0.025		-0.054	-0.012			
Max. Vx	7	-0.007		0.000	0.000			
T14	80 - 75	Secondary Horizontal	Max Tension	13	3.211	0.062	0.004	
			Max. Compression	13	-3.048	-0.054	-0.004	
			Max. Mx	13	3.211	0.062	0.004	
		Leg	Max. My	11	-3.003	-0.054	-0.004	
			Max. Vy	13	0.041	0.000	0.000	
			Max. Vx	13	0.002	0.000	0.000	
			Max Tension	12	134.039	0.264	-0.040	
			Max. Compression	6	-141.999	2.871	0.025	
			Max. Mx	12	133.294	-2.896	-0.006	
			Max. My	11	-6.995	0.025	-3.191	
			Max. Vy	4	-0.754	0.270	-0.016	
			Max. Vx	7	-1.080	-0.070	-1.517	
			Diagonal	Max Tension	13	6.102	0.069	-0.006
				Max. Compression	13	-6.485	0.000	0.000
				Max. Mx	12	5.526	0.084	0.004
Max. My	8	-5.316		-0.035	0.012			
Max. Vy	12	0.030		0.084	0.004			
Max. Vx	8	-0.004		0.000	0.000			
T15	75 - 70	Leg	Max Tension	12	151.848	-2.896	-0.006	
			Max. Compression	6	-160.866	2.496	0.016	
			Max. Mx	12	151.848	-2.896	-0.006	
			Max. My	11	-7.202	0.025	-3.191	

<i>tnxTower</i> ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 28 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft			
T16	70 - 65	Diagonal	Max. Vy	12	-0.117	-2.896	-0.006			
			Max. Vx	9	0.272	0.011	3.180			
			Max Tension	13	6.663	-0.047	-0.002			
			Max. Compression	13	-7.194	0.000	0.000			
			Max. Mx	6	5.754	-0.056	-0.003			
			Max. My	9	-6.669	0.042	-0.009			
		Leg	Max. Vy	6	0.022	-0.056	-0.003			
			Max. Vx	9	0.003	0.041	-0.009			
			Max Tension	12	168.835	-2.484	-0.005			
			Max. Compression	6	-178.357	2.973	0.023			
			Max. Mx	6	-178.357	2.973	0.023			
			Max. My	11	-7.455	0.034	-2.955			
			Max. Vy	10	-0.126	2.966	0.036			
			Max. Vx	9	-0.221	0.023	2.935			
Diagonal	Max Tension	13	5.775	-0.048	0.005					
	Max. Compression	13	-6.372	0.000	0.000					
	Max. Mx	12	4.813	-0.057	-0.003					
	Max. My	8	-5.689	0.023	-0.009					
	Max. Vy	6	0.021	-0.055	-0.004					
	Max. Vx	8	0.003	0.000	0.000					
	T17	65 - 60	Leg	Max Tension	12	184.082	-2.950	-0.005		
				Max. Compression	6	-194.360	0.433	0.022		
				Max. Mx	6	-194.237	2.973	0.023		
				Max. My	11	-7.710	-0.082	-3.267		
Max. Vy				6	0.537	2.973	0.023			
Max. Vx				9	-0.098	-0.087	3.247			
Diagonal			Max Tension	13	6.021	-0.049	-0.005			
			Max. Compression	13	-6.544	0.000	0.000			
			Max. Mx	6	5.075	-0.059	-0.005			
			Max. My	9	-6.080	0.043	-0.012			
			Max. Vy	6	0.022	-0.059	-0.005			
			Max. Vx	9	0.004	0.041	-0.012			
			T18	60 - 55	Leg	Max Tension	12	195.672	-0.713	-0.004
						Max. Compression	6	-206.457	7.590	0.010
Max. Mx	6	-206.457				7.590	0.010			
Max. My	11	-7.576				-0.082	-3.267			
Max. Vy	6	-2.955				7.590	0.010			
Max. Vx	13	0.925				-0.084	3.262			
Diagonal	Max Tension	4			7.392	-0.047	0.010			
	Max. Compression	10			-7.919	0.000	0.000			
	Max. Mx	6			2.242	-0.057	0.021			
	Max. My	7			-0.220	-0.048	-0.023			
	Max. Vy	6			0.022	-0.057	0.021			
	Max. Vx	10			0.007	0.000	0.000			
	Secondary Horizontal	Max Tension			6	3.577	-0.002	-0.020		
		Max. Compression			6	-3.577	0.000	0.000		
Max. Mx		10	-0.326	0.009	0.000					
Max. My		11	-3.422	0.001	0.024					
Max. Vy		23	-0.011	0.008	-0.000					
Max. Vx		11	0.011	0.000	0.000					
T19		55 - 50	Leg	Max Tension	12	212.340	-0.600	-0.006		
				Max. Compression	6	-224.229	3.267	0.021		
	Max. Mx			6	-224.229	3.267	0.021			
	Max. My			11	-8.303	0.003	-3.588			
	Max. Vy			10	-0.628	3.265	0.036			
	Max. Vx			9	-0.257	-0.006	3.567			
	Diagonal		Max Tension	5	4.741	0.000	0.000			
			Max. Compression	11	-5.190	0.000	0.000			
			Max. Mx	12	3.894	-0.044	-0.005			
			Max. My	4	-4.751	0.014	0.011			

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 29 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T20	50 - 45	Leg	Max. Vy	19	0.018	-0.024	-0.001	
			Max. Vx	4	-0.003	0.000	0.000	
			Max Tension	12	224.238	-3.232	-0.001	
			Max. Compression	6	-236.930	0.422	0.013	
			Max. Mx	6	-236.780	3.267	0.021	
			Max. My	11	-8.407	0.003	-3.588	
		Diagonal	Max. Vy	10	0.595	3.265	0.036	
			Max. Vx	9	0.294	-0.006	3.567	
			Max Tension	11	5.665	0.000	0.000	
			Max. Compression	11	-6.133	0.000	0.000	
			Max. Mx	6	4.630	-0.046	-0.008	
			Max. My	9	-5.726	0.029	-0.017	
			Max. Vy	19	0.020	-0.028	-0.004	
			Max. Vx	9	0.005	0.028	-0.017	
T21	45 - 40	Leg	Max Tension	12	234.415	-0.592	-0.002	
			Max. Compression	6	-247.912	8.260	0.001	
			Max. Mx	6	-247.783	8.260	0.001	
			Max. My	11	-8.656	-0.051	-3.104	
			Max. Vy	6	-3.221	8.260	0.001	
			Max. Vx	9	-1.146	-0.055	3.103	
		Diagonal	Max Tension	4	6.251	0.054	-0.019	
			Max. Compression	10	-6.602	0.000	0.000	
			Max. Mx	10	2.383	0.065	-0.012	
			Max. My	10	-6.593	-0.048	0.021	
			Max. Vy	10	-0.023	0.065	-0.012	
			Max. Vx	10	0.006	0.000	0.000	
			Secondary Horizontal	Max Tension	6	4.295	-0.022	-0.020
				Max. Compression	6	-4.295	0.000	0.000
T22	40 - 33.3333	Leg	Max. Mx	9	-3.851	0.034	0.027	
			Max. My	3	-3.828	0.034	0.027	
			Max. Vy	22	-0.023	0.017	0.009	
			Max. Vx	3	0.010	0.000	0.000	
			Max Tension	12	248.902	-0.952	-0.001	
			Max. Compression	6	-262.992	2.674	0.019	
		Diagonal	Max. Mx	12	248.683	-2.696	-0.000	
			Max. My	11	-9.282	-0.031	-3.638	
			Max. Vy	6	-0.320	2.674	0.019	
			Max. Vx	9	-0.115	-0.038	3.617	
			Max Tension	4	5.268	0.000	0.000	
			Max. Compression	11	-5.911	0.000	0.000	
			Max. Mx	12	5.017	-0.070	0.013	
			Max. My	11	-5.896	0.046	-0.023	
T23	33.3333 - 26.6667	Leg	Max. Vy	19	0.024	-0.038	-0.004	
			Max. Vx	11	0.006	0.000	0.000	
			Max Tension	12	264.048	-2.696	-0.000	
			Max. Compression	10	-279.148	2.982	0.022	
			Max. Mx	10	-279.148	2.982	0.022	
			Max. My	11	-9.571	-0.031	-3.638	
		Diagonal	Max. Vy	2	-0.077	2.968	-0.027	
			Max. Vx	9	0.325	-0.038	3.617	
			Max Tension	5	5.368	0.000	0.000	
			Max. Compression	11	-6.180	0.000	0.000	
			Max. Mx	10	4.733	-0.072	-0.009	
			Max. My	9	-5.748	0.044	-0.015	
			Max. Vy	19	0.025	-0.043	-0.004	
			Max. Vx	9	0.003	0.043	-0.015	
T24	26.6667 - 20	Leg	Max Tension	12	276.967	-2.917	0.001	
			Max. Compression	10	-293.304	2.259	-0.003	
			Max. Mx	10	-293.086	2.982	0.022	

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job	16-2859 130 SST	Page	30 of 45
	Project	Glastonbury-main st, CT (CT46126-A-01)	Date	11:19:26 08/11/16
	Client	SBA Communications Corporation	Designed by	mperez

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T25	20 - 13.3333	Diagonal	Max. My	11	-10.164	-0.072	-3.292
			Max. Vy	2	0.139	2.968	-0.027
			Max. Vx	13	-0.272	-0.072	3.278
			Max Tension	11	4.885	0.000	0.000
			Max. Compression	11	-5.709	0.000	0.000
			Max. Mx	12	4.121	-0.066	0.005
		Leg	Max. My	4	-5.023	0.020	0.011
			Max. Vy	19	0.026	-0.042	-0.001
			Max. Vx	4	-0.003	0.000	0.000
			Max Tension	12	288.846	-2.337	-0.001
			Max. Compression	10	-306.610	0.719	0.022
			Max. Mx	12	288.846	-2.337	-0.001
			Max. My	11	-10.317	-0.072	-3.292
			Max. Vy	6	0.262	2.260	0.022
T26	13.3333 - 6.66666	Diagonal	Max. Vx	13	0.188	-0.072	3.278
			Max Tension	11	5.207	0.000	0.000
			Max. Compression	11	-5.784	0.000	0.000
			Max. Mx	10	4.013	0.051	0.002
			Max. My	9	-5.360	-0.031	0.008
			Max. Vy	19	-0.018	0.031	0.002
		Leg	Max. Vx	9	-0.002	-0.031	0.008
			Max Tension	12	299.295	-0.829	0.001
			Max. Compression	10	-318.291	0.302	0.090
			Max. Mx	10	-318.180	8.437	-0.002
			Max. My	9	-10.371	-0.245	6.738
			Max. Vy	10	2.398	8.437	-0.002
			Max. Vx	9	-1.982	-0.245	6.738
			Max Tension	4	5.066	0.042	-0.010
T27	6.66666 - 0	Diagonal	Max. Compression	11	-5.586	0.000	0.000
			Max. Mx	10	2.967	0.046	-0.007
			Max. My	10	-5.476	-0.033	0.013
			Max. Vy	23	-0.020	0.035	-0.003
			Max. Vx	10	0.003	0.000	0.000
			Max Tension	10	5.515	0.000	0.000
		Secondary Horizontal	Max. Compression	10	-5.515	-0.004	-0.010
			Max. Mx	17	-0.979	0.024	0.006
			Max. My	9	-3.475	0.013	0.017
			Max. Vy	17	0.021	0.024	0.006
			Max. Vx	9	-0.005	0.000	0.000
			Max Tension	12	318.250	0.631	-0.001
			Max. Compression	10	-339.853	0.000	0.000
			Max. Mx	15	-131.432	1.346	-0.024
Leg	Max. My	9	-10.556	-0.245	6.738		
	Max. Vy	10	-8.702	0.000	0.000		
	Max. Vx	9	1.049	-0.245	6.738		
	Max Tension	4	6.373	0.000	0.000		
	Max. Compression	10	-7.138	0.000	0.000		
	Max. Mx	10	2.931	-0.087	-0.026		
	Max. My	9	-5.721	0.044	-0.041		
	Max. Vy	19	0.030	-0.040	-0.011		
Diagonal	Max. Vx	9	0.009	0.042	-0.041		

Maximum Reactions

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">31 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg C	Max. Vert	10	339.487	15.665	-8.906
	Max. H _x	10	339.487	15.665	-8.906
	Max. H _z	4	-316.096	-14.880	8.444
	Min. Vert	4	-316.096	-14.880	8.444
	Min. H _x	4	-316.096	-14.880	8.444
	Min. H _z	10	339.487	15.665	-8.906
Leg B	Max. Vert	6	339.208	-15.592	-8.962
	Max. H _x	12	-317.874	14.868	8.573
	Max. H _z	12	-317.874	14.868	8.573
	Min. Vert	12	-317.874	14.868	8.573
	Min. H _x	6	339.208	-15.592	-8.962
	Min. H _z	6	339.208	-15.592	-8.962
Leg A	Max. Vert	2	337.702	0.084	17.941
	Max. H _x	5	8.318	0.983	0.280
	Max. H _z	2	337.702	0.084	17.941
	Min. Vert	8	-316.438	-0.118	-17.089
	Min. H _x	11	11.366	-0.993	0.377
	Min. H _z	8	-316.438	-0.118	-17.089

Tower Mast Reaction Summary

Load Combination	Vertical K	Shear _x K	Shear _z K	Overturning Moment, M _x kip-ft	Overturning Moment, M _z kip-ft	Torque kip-ft
Dead Only	28.631	0.000	0.000	2.444	-0.331	-0.000
Dead+Wind 0 deg - No Ice	28.631	-0.151	-25.105	-2131.449	22.555	1.491
Dead+Wind 30 deg - No Ice	28.631	12.455	-21.448	-1827.224	-1063.136	2.423
Dead+Wind 60 deg - No Ice	28.631	21.473	-12.311	-1046.839	-1837.906	1.844
Dead+Wind 90 deg - No Ice	28.631	24.858	0.019	7.962	-2123.744	0.817
Dead+Wind 120 deg - No Ice	28.631	21.762	12.602	1078.336	-1849.905	0.250
Dead+Wind 150 deg - No Ice	28.631	12.448	21.463	1837.409	-1067.182	-0.650
Dead+Wind 180 deg - No Ice	28.631	0.064	24.703	2117.313	-11.837	-1.725
Dead+Wind 210 deg - No Ice	28.631	-12.399	21.533	1843.405	1054.504	-2.424
Dead+Wind 240 deg - No Ice	28.631	-21.890	12.501	1059.709	1862.751	-1.753
Dead+Wind 270 deg - No Ice	28.631	-24.949	-0.084	-11.836	2135.044	-0.813
Dead+Wind 300 deg - No Ice	28.631	-21.485	-12.392	-1062.865	1841.987	-0.108
Dead+Wind 330 deg - No Ice	28.631	-12.505	-21.484	-1835.093	1074.398	0.647
Dead+Ice+Temp	60.056	0.000	-0.000	7.318	-1.194	-0.000
Dead+Wind 0 deg+Ice+Temp	60.056	-0.038	-8.872	-739.597	4.701	0.385
Dead+Wind 30 deg+Ice+Temp	60.056	4.329	-7.466	-628.515	-370.006	0.583
Dead+Wind 60 deg+Ice+Temp	60.056	7.418	-4.261	-356.415	-636.598	0.432
Dead+Wind 90 deg+Ice+Temp	60.056	8.644	0.005	8.869	-738.284	0.183
Dead+Wind 120 deg+Ice+Temp	60.056	7.688	4.449	383.257	-648.561	0.034
Dead+Wind 150 deg+Ice+Temp	60.056	4.327	7.470	644.746	-371.089	-0.195
Dead+Wind 180 deg+Ice+Temp	60.056	0.016	8.543	739.333	-4.186	-0.436
Dead+Wind 210 deg+Ice+Temp	60.056	-4.314	7.487	646.265	365.549	-0.583
Dead+Wind 240 deg+Ice+Temp	60.056	-7.720	4.423	378.427	649.597	-0.419
Dead+Wind 270 deg+Ice+Temp	60.056	-8.667	-0.022	3.736	738.940	-0.182
Dead+Wind 300 deg+Ice+Temp	60.056	-7.421	-4.282	-360.568	635.417	0.004
Dead+Wind 330 deg+Ice+Temp	60.056	-4.342	-7.475	-630.556	370.691	0.194
Dead+Wind 0 deg - Service	28.631	-0.059	-9.807	-831.258	8.610	0.584
Dead+Wind 30 deg - Service	28.631	4.866	-8.378	-712.392	-415.548	0.928
Dead+Wind 60 deg - Service	28.631	8.388	-4.809	-407.483	-718.254	0.720
Dead+Wind 90 deg - Service	28.631	9.710	0.007	4.637	-829.950	0.339
Dead+Wind 120 deg - Service	28.631	8.501	4.923	422.824	-722.978	0.098
Dead+Wind 150 deg - Service	28.631	4.862	8.385	719.375	-417.166	-0.274
Dead+Wind 180 deg - Service	28.631	0.025	9.650	828.722	-4.827	-0.676

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 32 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Load Combination	Vertical K	Shear _x K	Shear _z K	Overturning Moment, M _x kip-ft	Overturning Moment, M _z kip-ft	Torque kip-ft
Dead+Wind 210 deg - Service	28.631	-4.843	8.412	721.709	411.806	-0.928
Dead+Wind 240 deg - Service	28.631	-8.551	4.883	415.539	727.582	-0.684
Dead+Wind 270 deg - Service	28.631	-9.746	-0.033	-3.099	833.949	-0.337
Dead+Wind 300 deg - Service	28.631	-8.393	-4.841	-413.739	719.438	-0.043
Dead+Wind 330 deg - Service	28.631	-4.886	-8.392	-715.463	419.545	0.273

Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.000	-28.631	0.000	-0.000	28.631	0.000	0.000%
2	-0.151	-28.631	-25.105	0.151	28.631	25.105	0.000%
3	12.457	-28.631	-21.448	-12.455	28.631	21.448	0.004%
4	21.474	-28.631	-12.312	-21.473	28.631	12.311	0.003%
5	24.859	-28.631	0.018	-24.858	28.631	-0.019	0.004%
6	21.762	-28.631	12.602	-21.762	28.631	-12.602	0.000%
7	12.448	-28.631	21.465	-12.448	28.631	-21.463	0.004%
8	0.064	-28.631	24.704	-0.064	28.631	-24.703	0.003%
9	-12.398	-28.631	21.535	12.399	28.631	-21.533	0.004%
10	-21.890	-28.631	12.501	21.890	28.631	-12.501	0.000%
11	-24.950	-28.631	-0.086	24.949	28.631	0.084	0.004%
12	-21.486	-28.631	-12.392	21.485	28.631	12.392	0.003%
13	-12.507	-28.631	-21.484	12.505	28.631	21.484	0.004%
14	0.000	-60.056	0.000	-0.000	60.056	0.000	0.000%
15	-0.038	-60.056	-8.871	0.038	60.056	8.872	0.000%
16	4.329	-60.056	-7.466	-4.329	60.056	7.466	0.000%
17	7.418	-60.056	-4.261	-7.418	60.056	4.261	0.000%
18	8.644	-60.056	0.005	-8.644	60.056	-0.005	0.000%
19	7.688	-60.056	4.448	-7.688	60.056	-4.449	0.000%
20	4.327	-60.056	7.470	-4.327	60.056	-7.470	0.000%
21	0.016	-60.056	8.543	-0.016	60.056	-8.543	0.000%
22	-4.314	-60.056	7.488	4.314	60.056	-7.487	0.000%
23	-7.720	-60.056	4.423	7.720	60.056	-4.423	0.000%
24	-8.667	-60.056	-0.022	8.667	60.056	0.022	0.000%
25	-7.421	-60.056	-4.282	7.421	60.056	4.282	0.000%
26	-4.342	-60.056	-7.475	4.342	60.056	7.475	0.000%
27	-0.059	-28.631	-9.807	0.059	28.631	9.807	0.000%
28	4.866	-28.631	-8.378	-4.866	28.631	8.378	0.000%
29	8.388	-28.631	-4.809	-8.388	28.631	4.809	0.000%
30	9.710	-28.631	0.007	-9.710	28.631	-0.007	0.000%
31	8.501	-28.631	4.923	-8.501	28.631	-4.923	0.000%
32	4.862	-28.631	8.385	-4.862	28.631	-8.385	0.000%
33	0.025	-28.631	9.650	-0.025	28.631	-9.650	0.000%
34	-4.843	-28.631	8.412	4.843	28.631	-8.412	0.000%
35	-8.551	-28.631	4.883	8.551	28.631	-4.883	0.000%
36	-9.746	-28.631	-0.033	9.746	28.631	0.033	0.000%
37	-8.393	-28.631	-4.841	8.393	28.631	4.841	0.000%
38	-4.886	-28.631	-8.392	4.886	28.631	8.392	0.000%

Non-Linear Convergence Results

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">33 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00000924
3	Yes	4	0.00000001	0.00003637
4	Yes	4	0.00000001	0.00002101
5	Yes	4	0.00000001	0.00003631
6	Yes	4	0.00000001	0.00001074
7	Yes	4	0.00000001	0.00003736
8	Yes	4	0.00000001	0.00001914
9	Yes	4	0.00000001	0.00003668
10	Yes	4	0.00000001	0.00001090
11	Yes	4	0.00000001	0.00003685
12	Yes	4	0.00000001	0.00002109
13	Yes	4	0.00000001	0.00003753
14	Yes	4	0.00000001	0.00000001
15	Yes	4	0.00000001	0.00008883
16	Yes	4	0.00000001	0.00009314
17	Yes	4	0.00000001	0.00009567
18	Yes	4	0.00000001	0.00009174
19	Yes	4	0.00000001	0.00009022
20	Yes	4	0.00000001	0.00009310
21	Yes	4	0.00000001	0.00009449
22	Yes	4	0.00000001	0.00009300
23	Yes	4	0.00000001	0.00008994
24	Yes	4	0.00000001	0.00009172
25	Yes	4	0.00000001	0.00009568
26	Yes	4	0.00000001	0.00009310
27	Yes	4	0.00000001	0.00001027
28	Yes	4	0.00000001	0.00001159
29	Yes	4	0.00000001	0.00001197
30	Yes	4	0.00000001	0.00001137
31	Yes	4	0.00000001	0.00001042
32	Yes	4	0.00000001	0.00001158
33	Yes	4	0.00000001	0.00001183
34	Yes	4	0.00000001	0.00001160
35	Yes	4	0.00000001	0.00001040
36	Yes	4	0.00000001	0.00001142
37	Yes	4	0.00000001	0.00001201
38	Yes	4	0.00000001	0.00001161

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	130 - 120	14.342	31	1.006	0.137
T2	120 - 117.143	12.229	31	0.994	0.100
T3	117.143 - 114.286	11.632	31	0.988	0.094
T4	114.286 - 111.43	11.037	31	0.979	0.087
T5	111.43 - 108.573	10.450	31	0.967	0.081
T6	108.573 - 105.716	9.868	31	0.952	0.074
T7	105.716 - 102.859	9.295	31	0.931	0.067
T8	102.859 - 100	8.736	31	0.904	0.059
T9	100 - 96	8.197	31	0.872	0.052
T10	96 - 92	7.474	31	0.824	0.041
T11	92 - 88	6.801	31	0.773	0.035
T12	88 - 84	6.171	31	0.719	0.032
T13	84 - 80	5.580	31	0.681	0.028

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 34 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T14	80 - 75	5.021	31	0.640	0.026
T15	75 - 70	4.362	31	0.595	0.022
T16	70 - 65	3.755	31	0.547	0.020
T17	65 - 60	3.198	31	0.497	0.018
T18	60 - 55	2.696	31	0.446	0.016
T19	55 - 50	2.249	31	0.394	0.014
T20	50 - 45	1.849	35	0.355	0.012
T21	45 - 40	1.492	35	0.315	0.011
T22	40 - 33.3333	1.174	35	0.275	0.009
T23	33.3333 - 26.6667	0.812	35	0.227	0.008
T24	26.6667 - 20	0.521	35	0.179	0.006
T25	20 - 13.3333	0.294	35	0.131	0.005
T26	13.3333 - 6.66666	0.131	35	0.085	0.003
T27	6.66666 - 0	0.029	35	0.038	0.001

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
130'	VHLP2.5	31	14.342	1.006	0.137	39457
128'	LLPX310R w/ Mount Pipe	31	13.918	1.004	0.128	39457
126'	VHLP2.5	31	13.494	1.002	0.120	39457
124'	VHLP2.5	31	13.071	0.999	0.113	33125
118'6"	APXVTM14-C-120 w/ Mount Pipe	31	11.916	0.991	0.097	38600
110'	(2) LGP13519	31	10.158	0.960	0.078	13125
93'	AIR 21 B2A/B4P	31	6.965	0.786	0.036	4217
80'	(2) LNX-6514DS-A1M w/ Mount Pipe	31	5.021	0.640	0.026	6731
55'6"	GPS-QBW-20N	31	2.292	0.399	0.014	6314
50'6"	GPS	35	1.887	0.358	0.012	6838

Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	130 - 120	36.644	12	2.569	0.350
T2	120 - 117.143	31.244	11	2.542	0.257
T3	117.143 - 114.286	29.720	11	2.528	0.240
T4	114.286 - 111.43	28.198	11	2.506	0.224
T5	111.43 - 108.573	26.699	11	2.475	0.208
T6	108.573 - 105.716	25.213	11	2.435	0.191
T7	105.716 - 102.859	23.750	11	2.381	0.171
T8	102.859 - 100	22.322	11	2.313	0.152
T9	100 - 96	20.943	11	2.232	0.133
T10	96 - 92	19.097	11	2.108	0.104
T11	92 - 88	17.377	11	1.975	0.091
T12	88 - 84	15.768	11	1.839	0.081
T13	84 - 80	14.256	11	1.740	0.073
T14	80 - 75	12.828	11	1.636	0.066
T15	75 - 70	11.143	11	1.521	0.058

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 35 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T16	70 - 65	9.591	10	1.399	0.051
T17	65 - 60	8.171	10	1.271	0.045
T18	60 - 55	6.890	10	1.139	0.040
T19	55 - 50	5.748	10	1.007	0.036
T20	50 - 45	4.725	10	0.906	0.032
T21	45 - 40	3.813	10	0.804	0.028
T22	40 - 33.3333	3.000	10	0.701	0.024
T23	33.3333 - 26.6667	2.075	10	0.579	0.020
T24	26.6667 - 20	1.332	10	0.457	0.016
T25	20 - 13.3333	0.753	10	0.336	0.013
T26	13.3333 - 6.66666	0.334	10	0.216	0.007
T27	6.66666 - 0	0.076	10	0.097	0.002

Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
130'	VHLP2.5	12	36.644	2.569	0.350	16031
128'	LLPX310R w/ Mount Pipe	12	35.559	2.565	0.329	16031
126'	VHLP2.5	12	34.475	2.561	0.308	16031
124'	VHLP2.5	12	33.393	2.556	0.289	13459
118'6"	APXVTM14-C-120 w/ Mount Pipe	11	30.443	2.536	0.248	15744
110'	(2) LGP13519	11	25.953	2.456	0.200	5158
93'	AIR 21 B2A/B4P	11	17.796	2.010	0.093	1643
80'	(2) LNX-6514DS-A1M w/ Mount Pipe	11	12.828	1.636	0.066	2632
55'6"	GPS-QBW-20N	10	5.856	1.019	0.036	2470
50'6"	GPS	10	4.822	0.915	0.032	2661

Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria	
T1	130	Leg	A325N	1.000	1	8.353	34.462	0.242	✓	1.333	Bolt Tension
T8	102.859	Leg	A325N	0.750	4	17.329	19.316	0.897	✓	1.333	Bolt Tension
T9	100	Diagonal	A325N	0.500	1	3.943	3.127	1.261	✓	1.333	Member Block Shear
T10	96	Diagonal	A325X	0.500	1	4.898	5.890	0.832	✓	1.333	Bolt Shear
T11	92	Diagonal	A325N	0.500	1	7.220	6.253	1.155	✓	1.333	Member Block Shear
		Secondary Horizontal	A325N	0.500	1	3.042	4.123	0.738	✓	1.333	Bolt Shear
T12	88	Diagonal	A325N	0.500	1	6.792	6.253	1.086	✓	1.333	Member Block Shear
		Secondary Horizontal	A325N	0.500	1	3.797	4.123	0.921	✓	1.333	Bolt Shear
T13	84	Leg	A325N	1.000	8	14.702	34.554	0.425	✓	1.333	Bolt Tension

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	Project	Glastonbury-main st, CT (CT46126-A-01)	Date	11:19:26 08/11/16
	Client	SBA Communications Corporation	Designed by	mperez

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria	
T14	80	Diagonal	A325N	0.500	1	5.981	6.253	0.957	✓	1.333	Member Block Shear
		Secondary Horizontal	A325N	0.500	1	3.211	4.123	0.779	✓	1.333	Bolt Shear
T15	75	Diagonal	A325X	0.500	1	6.485	5.890	1.101	✓	1.333	Bolt Shear
T16	70	Diagonal	A325N	0.500	1	6.663	6.253	1.066	✓	1.333	Member Block Shear
T17	65	Diagonal	A325N	0.500	1	5.775	6.253	0.923	✓	1.333	Member Block Shear
T18	60	Leg	A325N	1.000	8	23.010	34.557	0.666	✓	1.333	Bolt Tension
		Diagonal	A325N	0.500	1	6.021	6.253	0.963	✓	1.333	Member Block Shear
T19	55	Diagonal	A325N	0.500	1	7.392	6.253	1.182	✓	1.333	Member Block Shear
		Secondary Horizontal	A325N	0.500	1	3.577	2.719	1.316	✓	1.333	Member Bearing
T20	50	Diagonal	A325N	0.500	1	4.741	6.253	0.758	✓	1.333	Member Block Shear
T21	45	Diagonal	A325N	0.500	1	5.665	6.253	0.906	✓	1.333	Member Block Shear
T22	40	Leg	A325N	1.000	8	29.272	34.551	0.847	✓	1.333	Bolt Tension
		Diagonal	A325X	0.500	1	6.602	5.890	1.121	✓	1.333	Bolt Shear
T23	33.3333	Secondary Horizontal	A325N	0.500	1	4.295	4.123	1.042	✓	1.333	Bolt Shear
		Diagonal	A325N	0.500	1	5.911	8.247	0.717	✓	1.333	Bolt Shear
T24	26.6667	Diagonal	A325N	0.500	1	6.180	8.247	0.749	✓	1.333	Bolt Shear
T25	20	Leg	A325N	1.000	8	34.621	34.557	1.002	✓	1.333	Bolt Tension
		Diagonal	A325N	0.500	1	5.709	8.247	0.692	✓	1.333	Bolt Shear
T26	13.3333	Diagonal	A325X	0.500	1	5.207	4.078	1.277	✓	1.333	Member Bearing
T27	6.66666	Diagonal	A325X	0.500	1	5.066	4.078	1.242	✓	1.333	Member Bearing
		Secondary Horizontal	A325N	0.625	1	5.515	6.443	0.856	✓	1.333	Bolt Shear
T27	6.66666	Leg	A36M-55	1.500	6	53.042	49.568	1.070	✓	1.333	Bolt Tension
		Diagonal	A325N	0.500	1	7.138	8.247	0.866	✓	1.333	Bolt Shear

Compression Checks

Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T1	130 - 120	1 1/2	10'	2'5-3/4"	79.3 K=1.00	17.949	1.767	-7.914	31.718	0.250 ✓
T2	120 - 117.143	2	2'10-9/32'	2'9-9/32"	66.6 K=1.00	19.956	3.142	-12.819	62.693	0.204

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	<p style="text-align: center;">Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p style="text-align: center;">Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p style="text-align: center;">Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p style="text-align: center;">Designed by</p> <p style="text-align: center;">mperez</p>

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T3	117.143 - 114.286	2	2'10-9/32'	2'9-9/32"	66.6 K=1.00	19.956	3.142	-19.281	62.693	0.308
T4	114.286 - 111.43	2	2'10-9/32'	2'10-9/32"	68.6 K=1.00	19.654	3.142	-26.000	61.745	0.421
T5	111.43 - 108.573	2	2'10-9/32'	2'10-9/32"	68.6 K=1.00	19.654	3.142	-34.196	61.745	0.554
T6	108.573 - 105.716	2	2'10-9/32'	2'10-9/32"	68.6 K=1.00	19.654	3.142	-44.659	61.745	0.723
T7	105.716 - 102.859	2	2'10-9/32'	2'10-9/32"	68.6 K=1.00	19.654	3.142	-56.490	61.745	0.915
T8	102.859 - 100	2	2'10-5/16'	1'4-21/32"	33.3 K=1.00	24.257	3.142	-67.042	76.206	0.880
T9	100 - 96	P4.5 x 0.237	4'1/32"	4'1/32"	31.8 K=1.00	28.908	3.174	-76.726	91.755	0.836
T10	96 - 92	P4.5 x 0.237	4'1/32"	4'1/32"	31.8 K=1.00	28.908	3.174	-89.534	91.755	0.976
T11	92 - 88	P4.5 x 0.237	4'1/32"	2'13/16"	16.4 K=1.00	30.888	3.174	-98.353	98.040	1.003
T12	88 - 84	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	4'1/32"	2'25/32"	16.8 K=1.00	30.841	4.658	-112.008	143.672	0.780
T13	84 - 80	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	4'1/32"	2'23/32"	16.8 K=1.00	30.844	4.658	-124.569	143.688	0.867
T14	80 - 75	P6.625x0.280	5'1/32"	5'1/32"	26.7 K=1.00	29.617	5.581	-141.999	165.302	0.859
T15	75 - 70	P6.625x0.280	5'1/32"	5'1/32"	26.7 K=1.00	29.617	5.581	-160.866	165.302	0.973
T16	70 - 65	P6.625x0.280	5'1/32"	5'1/32"	26.7 K=1.00	29.617	5.581	-178.357	165.302	1.079
T17	65 - 60	P6.625x0.280	5'1/32"	5'1/32"	26.7 K=1.00	29.617	5.581	-194.360	165.302	1.176
T18	60 - 55	P6.625x0.280	5'1/32"	2'6-13/16"	13.7 K=1.00	31.182	5.581	-206.358	174.039	1.186
T19	55 - 50	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	5'1/32"	5'1/32"	27.1 K=1.00	29.561	7.511	-224.229	222.017	1.010
T20	50 - 45	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	5'1/32"	5'1/32"	27.1 K=1.00	29.561	7.511	-236.930	222.017	1.067
T21	45 - 40	BT101341- P6.625x0.280 w/ HP7.625x0.301	5'1/32"	2'6-23/32"	13.9 K=1.00	31.166	7.382	-247.859	230.057	1.077
T22	40 - 33.3333	P6.625x.432	6'8-1/32"	6'8-1/32"	36.5 K=1.00	28.214	8.405	-262.992	237.136	1.109
T23	33.3333 - 26.6667	P6.625x.432	6'8-1/32"	6'8-1/32"	36.5 K=1.00	28.214	8.405	-279.148	237.136	1.177
T24	26.6667 - 20	P6.625x.432	6'8-1/32"	6'8-1/32"	36.5 K=1.00	28.214	8.405	-293.304	237.136	1.237
T25	20 - 13.3333	P6.625x.432	6'8-1/32"	6'8-1/32"	36.5 K=1.00	28.214	8.405	-306.610	237.136	1.293
T26	13.3333 - 6.66666	P6.625x.432	6'8-1/32"	3'4-31/32"	18.7 K=1.00	30.632	8.405	-318.292	257.458	1.236
T27	6.66666 - 0	BT101341- P6.625 x .432 w/ HP7.625x0.301	6'8-1/32"	6'7-1/32"	36.5 K=1.00	28.201	10.183	-330.259	287.180	1.150

<p>tnxTower</p> <p>ALLPRO CONSULTING GROUP</p> <p>9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p>16-2859 130 SST</p>	<p>Page</p> <p>38 of 45</p>
	<p>Project</p> <p>Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p>11:19:26 08/11/16</p>
	<p>Client</p> <p>SBA Communications Corporation</p>	<p>Designed by</p> <p>mperez</p>

Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T1	130 - 120	1/2	3'6-1/4"	1'8-1/16"	144.5 K=0.90	7.152	0.196	-1.472	1.404	1.049
T2	120 - 117.143	3/4	3'8-13/16"	1'8-29/32"	105.1 K=0.94	12.322	0.442	-2.302	5.444	0.423
T3	117.143 - 114.286	3/4	3'8-13/16"	1'8-29/32"	105.1 K=0.94	12.322	0.442	-3.107	5.444	0.571
T4	114.286 - 111.43	3/4	3'9-9/16"	1'9-1/4"	105.8 K=0.93	12.231	0.442	-2.903	5.403	0.537
T5	111.43 - 108.573	3/4	3'9-9/16"	1'9-1/4"	105.8 K=0.93	12.231	0.442	-3.911	5.403	0.724
T6	108.573 - 105.716	3/4	3'9-9/16"	1'9-1/4"	105.8 K=0.93	12.231	0.442	-4.966	5.403	0.919
T7	105.716 - 102.859	3/4	3'9-9/16"	1'9-1/4"	105.8 K=0.93	12.231	0.442	-4.894	5.403	0.906
T8	102.859 - 100	3/4	3'8-27/32"	1'8-29/32"	105.1 K=0.94	12.320	0.442	-5.131	5.443	0.943
T9	100 - 96	L1 1/2x1 1/2x3/16	4'9-1/4"	2'7/16"	92.5 K=1.11	13.907	0.527	-4.091	7.334	0.558
T10	96 - 92	L2x2x1/4	4'10-19/32"	2'15/16"	77.8 K=1.22	15.597	0.938	-4.898	14.630	0.335
T11	92 - 88	2L1 1/2x1 1/2x3/16x3/8	5'	2'3-1/4"	59.7 K=1.00	17.463	1.055	-7.547	18.418	0.410
T12	88 - 84	2L1 1/2x1 1/2x3/16x3/8	5'1-15/32"	2'4-3/32"	61.5 K=1.00	17.283	1.055	-7.023	18.228	0.385
T13	84 - 80	2L1 1/2x1 1/2x3/16x3/8	5'3"	2'4-31/32"	63.4 K=1.00	17.098	1.055	-6.180	18.034	0.343
T14	80 - 75	L2x2x1/4	6'2-1/8"	2'7-3/16"	89.8 K=1.13	14.225	0.938	-6.485	13.343	0.486
T15	75 - 70	2L1 1/2x1 1/2x3/16x3/8	6'3-29/32"	2'8-17/32"	71.2 K=1.00	16.303	1.055	-7.194	17.195	0.418
T16	70 - 65	2L1 1/2x1 1/2x3/16x3/8	6'5-25/32"	2'9-5/8"	73.6 K=1.00	16.051	1.055	-6.372	16.928	0.376
T17	65 - 60	2L1 1/2x1 1/2x3/16x3/8	6'7-23/32"	2'10-23/32"	76.0 K=1.00	15.790	1.055	-6.544	16.654	0.393
T18	60 - 55	2L1 1/2x1 1/2x3/16x3/8	6'9-23/32"	3'1-3/32"	81.2 K=1.00	15.218	1.055	-7.919	16.050	0.493
T19	55 - 50	2L1 1/2x1 1/2x3/16x3/8	6'11-13/16"	3'31/32"	81.0 K=1.00	15.246	1.055	-5.190	16.080	0.323
T20	50 - 45	2L1 1/2x1 1/2x3/16x3/8	7'1-29/32"	3'2-1/8"	83.5 K=1.00	14.961	1.055	-6.133	15.779	0.389
T21	45 - 40	L2x2x1/4	7'4-3/32"	3'4-9/16"	103.7 K=1.00	12.503	0.938	-6.602	11.728	0.563
T22	40 - 33.3333	2L1 3/4x1 3/4x3/16x3/8	8'9"	3'11-11/16"	88.8 K=1.00	14.347	1.242	-5.911	17.821	0.332
T23	33.3333 - 26.6667	2L1 3/4x1 3/4x3/16x3/8	8'11-5/8"	4'1-1/8"	91.5 K=1.00	14.030	1.242	-6.180	17.428	0.355
T24	26.6667 - 20	2L1 3/4x1 3/4x3/16x3/8	9'2-11/32"	4'2-9/16"	94.2 K=1.00	13.701	1.242	-5.709	17.020	0.335

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 39 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T25	20 - 13.3333	L2x2x3/16	9'5-5/32"	4'4-1/16"	132.2 K=1.00	8.547	0.715	-5.784	6.110	0.947
T26	13.3333 - 6.66666	L2x2x3/16	9'8"	4'6-13/16"	139.2 K=1.00	7.708	0.715	-5.586	5.510	1.014
T27	6.66666 - 0	2L2x2x3/16x3/8	9'10-1/4"	4'6-3/4"	88.7 K=1.00	14.355	1.430	-7.138	20.527	0.348

Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T1	130 - 120	L1 1/4x1 1/4x3/16	2'6"	2'4-1/2"	118.5 K=1.01	10.498	0.434	-0.257	4.552	0.056

Secondary Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T8	102.859 - 100	L2x2x1/8	2'6"	2'4"	82.4 K=1.84	14.733	0.484	-1.161	7.136	0.163
T11	92 - 88	4x3/8	2'11-31/32"	2'7-15/32"	145.3 K=0.50	7.072	1.500	-2.884	10.608	0.272
T12	88 - 84	4x3/8	3'2-11/32"	2'9-27/32"	156.4 K=0.50	6.108	1.500	-3.539	9.162	0.386
T13	84 - 80	4x3/8	3'4-3/4"	3'1/4"	167.5 K=0.50	5.324	1.500	-3.048	7.985	0.382
T18	60 - 55	L2x2x1/8	4'7-15/32"	4'27/32"	39.0 K=0.50	18.668	0.484	-3.577	9.042	0.396
T21	45 - 40	L3x3x5/16	5'4-15/32"	4'9-27/32"	31.4 K=0.50	19.844	1.780	-4.295	35.322	0.122
T26	13.3333 - 6.66666	L2x2x1/4	6'11-15/16"	6'5-5/16"	63.5 K=0.50	17.090	0.938	-5.515	16.030	0.344

Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T1	130 - 120	L1 1/4x1 1/4x3/16	2'6"	2'4-1/2"	118.5 K=1.01	10.498	0.434	-0.061	4.552	0.013
T2	120 - 117.143	L1 1/4x1 1/4x3/16	2'6"	2'4"	117.5 K=1.02	10.643	0.434	-0.031	4.615	0.007

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 40 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
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Bottom Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T1	130 - 120	L1 1/4x1 1/4x3/16	2'6"	2'4-1/2"	118.5 K=1.01	10.498	0.434	-0.208	4.552	0.046 ✓
T8	102.859 - 100	L1 1/4x1 1/4x3/16	2'6"	2'4"	117.5 K=1.02	10.643	0.434	-0.875	4.615	0.190 ✓

Tension Checks

Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T1	130 - 120	1 1/2	10'	1"	2.7	27.000	1.767	8.353	47.713	0.175 ✓
T2	120 - 117.143	2	2'10-9/32'	2'9-9/32"	66.6	27.000	3.142	10.548	84.823	0.124 ✓
T3	117.143 - 114.286	2	2'10-9/32'	2'9-9/32"	66.6	27.000	3.142	16.916	84.823	0.199 ✓
T4	114.286 - 111.43	2	2'10-9/32'	2'10-9/32'	68.6	27.000	3.142	23.659	84.823	0.279 ✓
T5	111.43 - 108.573	2	2'10-9/32'	2'10-9/32'	68.6	27.000	3.142	31.058	84.823	0.366 ✓
T6	108.573 - 105.716	2	2'10-9/32'	2'10-9/32'	68.6	27.000	3.142	40.858	84.823	0.482 ✓
T7	105.716 - 102.859	2	2'10-9/32'	2'10-9/32'	68.6	27.000	3.142	52.520	84.823	0.619 ✓
T8	102.859 - 100	2	2'10-5/16'	1"	2.0	27.000	3.142	69.316	84.823	0.817 ✓
T9	100 - 96	P4.5 x 0.237	4'1/32"	4'1/32"	31.8	32.400	3.174	72.865	102.839	0.709 ✓
T10	96 - 92	P4.5 x 0.237	4'1/32"	4'1/32"	31.8	32.400	3.174	84.481	102.839	0.821 ✓
T11	92 - 88	P4.5 x 0.237	4'1/32"	1'11-7/32'	15.4	32.400	3.174	92.637	102.839	0.901 ✓
T12	88 - 84	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	4'1/32"	1'11-1/4"	15.8	32.400	4.658	105.721	150.934	0.700 ✓
T13	84 - 80	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	4'1/32"	1'11-5/16'	15.9	32.400	4.658	117.755	150.934	0.780 ✓
T14	80 - 75	P6.625x0.280	5'1/32"	5'1/32"	26.7	32.400	5.581	134.039	180.836	0.741 ✓

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">41 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T15	75 - 70	P6.625x0.280	5'1/32"	5'1/32"	26.7	32.400	5.581	151.848	180.836	0.840
T16	70 - 65	P6.625x0.280	5'1/32"	5'1/32"	26.7	32.400	5.581	168.835	180.836	0.934
T17	65 - 60	P6.625x0.280	5'1/32"	5'1/32"	26.7	32.400	5.581	184.082	180.836	1.018
T18	60 - 55	P6.625x0.280	5'1/32"	2'5-3/16"	13.0	32.400	5.581	195.673	180.836	1.082
T19	55 - 50	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	5'1/32"	5'1/32"	27.1	32.400	7.511	212.340	243.342	0.873
T20	50 - 45	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	5'1/32"	5'1/32"	27.1	32.400	7.511	224.238	243.342	0.921
T21	45 - 40	BT101341- P6.625x0.280 w/ HP7.625x0.301	5'1/32"	2'5-5/16"	13.2	32.400	7.382	234.415	239.163	0.980
T22	40 - 33.3333	P6.625x.432	6'8-1/32"	6'8-1/32"	36.5	32.400	8.405	248.902	272.320	0.914
T23	33.3333 - 26.6667	P6.625x.432	6'8-1/32"	6'8-1/32"	36.5	32.400	8.405	264.048	272.320	0.970
T24	26.6667 - 20	P6.625x.432	6'8-1/32"	6'8-1/32"	36.5	32.400	8.405	276.967	272.320	1.017
T25	20 - 13.3333	P6.625x.432	6'8-1/32"	6'8-1/32"	36.5	32.400	8.405	288.846	272.320	1.061
T26	13.3333 - 6.66666	P6.625x.432	6'8-1/32"	3'3-1/16"	17.8	32.400	8.405	299.295	272.320	1.099
T27	6.66666 - 0	BT101341- P6.625 x .432 w/ HP7.625x0.301	6'8-1/32"	1"	0.5	32.400	10.183	318.250	329.942	0.965

Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T1	130 - 120	1/2	3'6-1/4"	1'8-1/16"	160.6	21.600	0.196	1.431	4.241	0.337
T2	120 - 117.143	3/4	3'8-13/16'	1'8-29/32'	111.5	21.600	0.442	2.383	9.543	0.250
T3	117.143 - 114.286	3/4	3'8-13/16'	1'8-29/32'	111.5	21.600	0.442	3.114	9.543	0.326
T4	114.286 - 111.43	3/4	3'9-9/16"	1'9-1/4"	113.4	21.600	0.442	2.869	9.543	0.301
T5	111.43 - 108.573	3/4	3'9-9/16"	1'9-1/4"	113.4	21.600	0.442	3.914	9.543	0.410
T6	108.573 - 105.716	3/4	3'9-9/16"	1'9-1/4"	113.4	21.600	0.442	4.896	9.543	0.513
T7	105.716 - 102.859	3/4	3'9-9/16"	1'9-1/4"	113.4	21.600	0.442	4.839	9.543	0.507
T8	102.859 - 100	3/4	3'8-27/32'	1'8-29/32'	111.6	21.600	0.442	5.018	9.543	0.526
T9	100 - 96	L1 1/2x1 1/2x3/16	4'9-1/4"	2'7/16"	56.3	29.000	0.308	3.943	8.921	0.442

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 42 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T10	96 - 92	L2x2x1/4	4'10-19/32"	2'15/16"	43.4	29.000	0.586	4.581	17.003	0.269
T11	92 - 88	2L1 1/2x1 1/2x3/16x3/8	5'	2'3-1/4"	59.7	29.000	0.615	7.220	17.842	0.405
T12	88 - 84	2L1 1/2x1 1/2x3/16x3/8	5'1-15/32"	2'4-3/32"	61.5	29.000	0.615	6.792	17.842	0.381
T13	84 - 80	2L1 1/2x1 1/2x3/16x3/8	5'3"	2'4-31/32"	63.4	29.000	0.615	5.981	17.842	0.335
T14	80 - 75	L2x2x1/4	6'2-1/8"	2'7-3/16"	53.7	29.000	0.586	6.102	17.003	0.359
T15	75 - 70	2L1 1/2x1 1/2x3/16x3/8	6'3-29/32"	2'8-17/32"	74.0	29.000	0.615	6.663	17.842	0.373
T16	70 - 65	2L1 1/2x1 1/2x3/16x3/8	6'5-25/32"	2'9-5/8"	76.4	29.000	0.615	5.775	17.842	0.324
T17	65 - 60	2L1 1/2x1 1/2x3/16x3/8	6'7-23/32"	2'10-23/32"	78.8	29.000	0.615	6.021	17.842	0.337
T18	60 - 55	2L1 1/2x1 1/2x3/16x3/8	6'9-23/32"	3'1-3/32"	81.2	29.000	0.615	7.392	17.842	0.414
T19	55 - 50	2L1 1/2x1 1/2x3/16x3/8	6'11-13/16"	3'31/32"	83.7	29.000	0.615	4.741	17.842	0.266
T20	50 - 45	2L1 1/2x1 1/2x3/16x3/8	7'1-29/32"	3'2-1/8"	86.2	29.000	0.615	5.665	17.842	0.318
T21	45 - 40	L2x2x1/4	7'4-3/32"	3'4-9/16"	66.6	29.000	0.586	6.251	17.003	0.368
T22	40 - 33.3333	2L1 3/4x1 3/4x3/16x3/8	8'9"	3'11-11/16"	91.1	29.000	0.756	5.268	21.920	0.240
T23	33.3333 - 26.6667	2L1 3/4x1 3/4x3/16x3/8	8'11-5/8"	4'1-1/8"	93.8	29.000	0.756	5.368	21.920	0.245
T24	26.6667 - 20	2L1 3/4x1 3/4x3/16x3/8	9'2-11/32"	4'2-9/16"	96.5	29.000	0.756	4.885	21.920	0.223
T25	20 - 13.3333	L2x2x3/16	9'5-5/32"	4'4-1/16"	86.3	29.000	0.448	5.207	12.999	0.401
T26	13.3333 - 6.66666	L2x2x3/16	9'8"	4'6-13/16"	88.8	29.000	0.448	5.066	12.999	0.390
T27	6.66666 - 0	2L2x2x3/16x3/8	9'10-1/4"	4'6-3/4"	90.8	29.000	0.897	6.373	26.005	0.245

Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T1	130 - 120	L1 1/4x1 1/4x3/16	2'6"	2'4-1/2"	75.7	21.600	0.434	0.291	9.366	0.031

Secondary Horizontal Design Data (Tension)

tnxTower ALLPRO CONSULTING GROUP 9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375	Job 16-2859 130 SST	Page 43 of 45
	Project Glastonbury-main st, CT (CT46126-A-01)	Date 11:19:26 08/11/16
	Client SBA Communications Corporation	Designed by mperez

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio $\frac{P}{P_a}$
T8	102.859 - 100	L2x2x1/8	2'6"	2'4"	44.7	21.600	0.484	1.161	10.463	0.111 ✓
T11	92 - 88	4x3/8	2'11-31/32"	2'7-15/32"	290.6	29.000	0.949	3.042	27.527	0.111 ✓
T12	88 - 84	4x3/8	3'2-11/32"	2'9-27/32"	312.7	29.000	0.949	3.797	27.527	0.138 ✓
T13	84 - 80	4x3/8	3'4-3/4"	3'1/4"	335.0	29.000	0.949	3.211	27.527	0.117 ✓
T18	60 - 55	L2x2x1/8	4'7-15/32"	4'27/32"	78.0	29.000	0.305	3.577	8.836	0.405 ✓
T21	45 - 40	L3x3x5/16	5'4-15/32"	4'9-27/32"	62.7	29.000	1.189	4.295	34.467	0.125 ✓
T26	13.3333 - 6.66666	L2x2x1/4	6'11-15/16"	6'5-5/16"	127.0	29.000	0.563	5.515	16.323	0.338 ✓

Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio $\frac{P}{P_a}$
T1	130 - 120	L1 1/4x1 1/4x3/16	2'6"	2'4-1/2"	75.7	21.600	0.434	0.055	9.366	0.006 ✓
T2	120 - 117.143	L1 1/4x1 1/4x3/16	2'6"	2'4"	74.4	21.600	0.434	0.058	9.366	0.006 ✓

Bottom Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _a ft	Kl/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio $\frac{P}{P_a}$
T1	130 - 120	L1 1/4x1 1/4x3/16	2'6"	2'4-1/2"	75.7	21.600	0.434	0.235	9.366	0.025 ✓
T8	102.859 - 100	L1 1/4x1 1/4x3/16	2'6"	2'4"	74.4	21.600	0.434	0.877	9.366	0.094 ✓

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P _{allow} K	% Capacity	Pass Fail
T1	130 - 120	Leg	1 1/2	2	-7.914	42.280	18.7	Pass
T2	120 - 117.143	Leg	2	44	-12.819	83.570	15.3	Pass
T3	117.143 - 114.286	Leg	2	56	-19.281	83.570	23.1	Pass
T4	114.286 - 111.43	Leg	2	65	-26.000	82.306	31.6	Pass

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p style="text-align: center;">Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p style="text-align: center;">Page</p> <p style="text-align: center;">44 of 45</p>
	<p style="text-align: center;">Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p style="text-align: center;">Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p style="text-align: center;">Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p style="text-align: center;">Designed by</p> <p style="text-align: center;">mperez</p>

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P _{allow} K	% Capacity	Pass Fail
T5	111.43 - 108.573	Leg	2	74	-34.196	82.306	41.5	Pass
T6	108.573 - 105.716	Leg	2	83	-44.659	82.306	54.3	Pass
T7	105.716 - 102.859	Leg	2	92	-56.490	82.306	68.6	Pass
T8	102.859 - 100	Leg	2	101	-67.042	101.583	66.0	Pass
T9	100 - 96	Leg	P4.5 x 0.237	116	-76.726	122.309	67.3 (b)	Pass
T10	96 - 92	Leg	P4.5 x 0.237	125	-89.534	122.309	62.7	Pass
T11	92 - 88	Leg	P4.5 x 0.237	134	-98.353	130.687	73.2	Pass
T12	88 - 84	Leg	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	146	-112.008	191.515	75.3	Pass
T13	84 - 80	Leg	BT101341- P4.5 x 0.237 w/ HP5.625x0.375	158	-124.569	191.536	58.5	Pass
T14	80 - 75	Leg	P6.625x0.280	170	-141.999	220.348	65.0	Pass
T15	75 - 70	Leg	P6.625x0.280	179	-160.866	220.348	64.4	Pass
T16	70 - 65	Leg	P6.625x0.280	188	-178.357	220.348	73.0	Pass
T17	65 - 60	Leg	P6.625x0.280	188	-178.357	220.348	80.9	Pass
T18	60 - 55	Leg	P6.625x0.280	197	-194.360	220.348	88.2	Pass
T19	55 - 50	Leg	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	206	-206.358	231.994	88.9	Pass
T20	50 - 45	Leg	BT101341- P6.625x0.280 w/ HP7.625x0.301(45'-55')	218	-224.229	295.949	75.8	Pass
T21	45 - 40	Leg	BT101341- P6.625x0.280 w/ HP7.625x0.301	227	-236.930	295.949	80.1	Pass
T22	40 - 33.3333	Leg	P6.625x.432	236	-247.859	306.666	80.8	Pass
T23	33.3333 - 26.6667	Leg	P6.625x.432	248	-262.992	316.102	83.2	Pass
T24	26.6667 - 20	Leg	P6.625x.432	256	-279.148	316.102	88.3	Pass
T25	20 - 13.3333	Leg	P6.625x.432	265	-293.304	316.102	92.8	Pass
T26	13.3333 - 6.66666	Leg	P6.625x.432	274	-306.610	316.102	97.0	Pass
T27	6.66666 - 0	Leg	BT101341- P6.625 x .432 w/ HP7.625x0.301	283	-318.292	343.191	92.7	Pass
T1	130 - 120	Diagonal	1/2	295	-330.259	382.811	86.3	Pass
T2	120 - 117.143	Diagonal	3/4	13	-1.472	1.872	78.7	Pass
T3	117.143 - 114.286	Diagonal	3/4	52	-2.302	7.257	31.7	Pass
T4	114.286 - 111.43	Diagonal	3/4	61	-3.107	7.257	42.8	Pass
T5	111.43 - 108.573	Diagonal	3/4	70	-2.903	7.203	40.3	Pass
T6	108.573 - 105.716	Diagonal	3/4	79	-3.911	7.203	54.3	Pass
T7	105.716 - 102.859	Diagonal	3/4	88	-4.966	7.203	68.9	Pass
T8	102.859 - 100	Diagonal	3/4	97	-4.894	7.203	67.9	Pass
T9	100 - 96	Diagonal	L1 1/2x1 1/2x3/16	109	-5.131	7.255	70.7	Pass
T10	96 - 92	Diagonal	L2x2x1/4	121	-4.091	9.776	41.8	Pass
T11	92 - 88	Diagonal	2L1 1/2x1 1/2x3/16x3/8	130	-4.898	19.502	94.6 (b)	Pass
T12	88 - 84	Diagonal	2L1 1/2x1 1/2x3/16x3/8	139	-7.547	24.551	25.1	Pass
T13	84 - 80	Diagonal	2L1 1/2x1 1/2x3/16x3/8	151	-7.023	24.298	62.4 (b)	Pass
T14	80 - 75	Diagonal	L2x2x1/4	163	-6.180	24.039	30.7	Pass
T15	75 - 70	Diagonal	2L1 1/2x1 1/2x3/16x3/8	175	-6.485	17.786	86.6 (b)	Pass
T16	70 - 65	Diagonal	2L1 1/2x1 1/2x3/16x3/8	184	-7.194	22.921	28.9	Pass
				193	-6.372	22.566	81.5 (b)	
							71.8 (b)	
							36.5	Pass
							82.6 (b)	
							31.4	Pass
							79.9 (b)	
							28.2	Pass
							69.3 (b)	

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">ALLPRO CONSULTING GROUP</p> <p style="text-align: center;">9221 LYNDON B. JOHNSON FWY 204 DALLAS, TX Phone: (972)231-8893 FAX: 866-364-8375</p>	<p>Job</p> <p style="text-align: center;">16-2859 130 SST</p>	<p>Page</p> <p style="text-align: center;">45 of 45</p>
	<p>Project</p> <p style="text-align: center;">Glastonbury-main st, CT (CT46126-A-01)</p>	<p>Date</p> <p style="text-align: center;">11:19:26 08/11/16</p>
	<p>Client</p> <p style="text-align: center;">SBA Communications Corporation</p>	<p>Designed by</p> <p style="text-align: center;">mperez</p>

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P _{allow} K	% Capacity	Pass Fail	
T17	65 - 60	Diagonal	2L1 1/2x1 1/2x3/16x3/8	202	-6.544	22.200	29.5	Pass	
T18	60 - 55	Diagonal	2L1 1/2x1 1/2x3/16x3/8	208	-7.919	21.395	72.2 (b) 37.0	Pass	
T19	55 - 50	Diagonal	2L1 1/2x1 1/2x3/16x3/8	220	-5.190	21.434	88.7 (b) 24.2	Pass	
T20	50 - 45	Diagonal	2L1 1/2x1 1/2x3/16x3/8	229	-6.133	21.034	56.9 (b) 29.2	Pass	
T21	45 - 40	Diagonal	L2x2x1/4	238	-6.602	15.634	68.0 (b) 42.2	Pass	
T22	40 - 33.3333	Diagonal	2L1 3/4x1 3/4x3/16x3/8	250	-5.911	23.756	84.1 (b) 24.9	Pass	
T23	33.3333 - 26.6667	Diagonal	2L1 3/4x1 3/4x3/16x3/8	259	-6.180	23.231	53.8 (b) 26.6	Pass	
T24	26.6667 - 20	Diagonal	2L1 3/4x1 3/4x3/16x3/8	268	-5.709	22.687	56.2 (b) 25.2	Pass	
T25	20 - 13.3333	Diagonal	L2x2x3/16	277	-5.784	8.144	51.9 (b) 71.0	Pass	
T26	13.3333 - 6.66666	Diagonal	L2x2x3/16	286	-5.586	7.345	95.8 (b) 76.1	Pass	
T27	6.66666 - 0	Diagonal	2L2x2x3/16x3/8	298	-7.138	27.363	93.2 (b) 26.1	Pass	
T1	130 - 120	Horizontal	L1 1/4x1 1/4x3/16	36	-0.257	6.068	64.9 (b) 4.2	Pass	
T8	102.859 - 100	Secondary Horizontal	L2x2x1/8	112	-1.161	9.513	12.2	Pass	
T11	92 - 88	Secondary Horizontal	4x3/8	142	-2.884	14.141	20.4	Pass	
T12	88 - 84	Secondary Horizontal	4x3/8	154	-3.539	12.213	55.4 (b) 29.0	Pass	
T13	84 - 80	Secondary Horizontal	4x3/8	166	-3.048	10.644	69.1 (b) 28.6	Pass	
T18	60 - 55	Secondary Horizontal	L2x2x1/8	214	3.577	11.778	58.4 (b) 30.4	Pass	
T21	45 - 40	Secondary Horizontal	L3x3x5/16	244	4.295	45.945	98.7 (b) 9.3	Pass	
T26	13.3333 - 6.66666	Secondary Horizontal	L2x2x1/4	292	-5.515	21.369	78.1 (b) 25.8	Pass	
T1	130 - 120	Top Girt	L1 1/4x1 1/4x3/16	6	-0.061	6.068	64.2 (b) 1.0	Pass	
T2	120 - 117.143	Top Girt	L1 1/4x1 1/4x3/16	48	-0.031	6.152	0.5	Pass	
T1	130 - 120	Bottom Girt	L1 1/4x1 1/4x3/16	9	-0.208	6.068	3.4	Pass	
T8	102.859 - 100	Bottom Girt	L1 1/4x1 1/4x3/16	105	-0.875	6.152	14.2	Pass	
							Summary		
							Leg (T25)	97.0	Pass
							Diagonal (T25)	95.8	Pass
							Horizontal (T1)	4.2	Pass
							Secondary Horizontal (T18)	98.7	Pass
							Top Girt (T1)	1.0	Pass
							Bottom Girt (T8)	14.2	Pass
							Bolt Checks	98.7	Pass
							RATING =	98.7	Pass

MATHCAD CALCULATION PRINTOUT

SELF SUPPORTING TOWER

MAT FOUNDATION CHECK

Existing 130' Self-Support Tower

SBA Site Name: Glastonbury-main St.

SBA Site ID: CT46126-A -01

Carrier Name: AT&T

Carrier Site Name: 10071041

Site Location:

2577 Main Street

Glastonbury, CT 06033

Latitude: 41.714389°

Longitude: -72.613028°

ACGI Job # 16-2859

By:

Allpro Consulting Group, Inc.

9221 Lyndon B. Johnson Freeway, #204

Dallas, TX 75243

Phone: 972-231-8893

Fax: 866-364-8375

Foundation check

-Foundation Reactions-

((As per tnx Tower Printout) TIA-222-F

Total Shear	$S := 25 \cdot \text{kips}$	Compression on Pedestal:	$P_c := 339 \cdot \text{kips}$
Moment	$M := 2143 \cdot \text{ft}_K$	Uplift on Pedestal:	$P_{up} := 318 \cdot \text{kips}$
Down load, Tower weight	$P_v := 29 \cdot \text{kips}$	Shear on Pedestal:	$Sh := 18 \cdot \text{kips}$

-Soil Properties- Soil data as per Geotechnical Report by Tectonic Engineering
Project # 1170.C057, dated 08/26/1999 & previous structural analysis by B+T Group, Job # 101341.001.01a, dated 09/29/2015

Allowable Bearing Capacity	$Brg_{allw} := 3 \cdot \text{ksf}$
Internal angle of friction for soil,	$\phi := 0 \cdot \text{deg}$
Unit wt. of soil,	$\gamma_s := 0.12 \cdot \text{kcf}$
Allowable Passive Pressure	see next page
Cohesion of soil,	$c_u := 0 \cdot \text{ksf}$
Friction Factor	$FF := 0.35$
Depth to be neglected	$L_{neg} := 3.3 \cdot \text{ft}$

-Material Parameters-

Conforming to the design requirements as in ACI 318-99

Unit wt. of concrete,	$\gamma_c := 0.150 \cdot \text{kcf}$
Concrete compressive strength,	$f_c := 3000 \cdot \text{psi}$
Rebar yield strength,	$f_y := 60000 \cdot \text{psi}$

-Factor of Safety for soil strength-

$FS_{SOIL} := 2$

DIMENSIONS: Original Tower Design by FRED A. NUDD Corporation PJ No. 6893, Sept, 1999

Tower face width TFWF := 7.5-ft Tower ht. Tw_{ht} := 130-ft

The tower location is eccentric by L_{pe} := 0-ft
with respect to the mat foundation
center towards the base

Type of column, col.t=0 for circular,=1 for rectangular/square col_t := 0

Depth of mat, D_f := 4-ft No. of pedestals Nped := 3
Thickness of mat, T_f := 3-ft
Pedestal size, Ped_s := 3-ft
Extension above the grade, E_g := 6-in

Mat Dimensions, LxB L := 26-ft x B := L B = 26ft

Brg_{allw} = 3·ksf FS := 2.0

MAT SIZING CALCULATIONS

$$K_p := \tan\left(45\text{-deg} + \frac{\phi}{2}\right)^2 \quad K_p = 1$$

$$P_{\text{pave}} := \frac{(D_f - T_f - L_{\text{neg}}) \cdot K_p \cdot \gamma_s + (D_f - L_{\text{neg}}) \cdot K_p \cdot \gamma_s}{2} \quad P_{\text{pave}} = -0.096 \cdot \text{ksf}$$

Calculate safety against overturning and location of resultant on the base

**Resisting Moments about mid axis
parallel to base**

$$\text{Area}_{\text{ped}} := \text{if}\left(\text{col}_t = 1, \text{Ped}_s^2, \frac{\pi}{4} \cdot \text{Ped}_s^2\right) \quad \text{Area}_{\text{ped}} = 7.069 \text{ ft}^2$$

component	value, kips	lever arm, ft	resisting moment, ft-kips
1) Concrete wt.	$C_w := L \cdot B \cdot T_f \cdot (\gamma_c) + \text{Area}_{\text{ped}} \cdot \gamma_c \cdot (D_f + E_g - T_f) \cdot N_{\text{ped}}$ $C_w = 308.971 \cdot \text{kips}$	$L_c := \frac{L}{2}$ $L_c = 13 \text{ ft}$	$R_c := C_w \cdot L_c$ $R_c = 4016.627 \cdot \text{ft}_K$
2) Soil wt.	$S_w := [L \cdot B \cdot (D_f - T_f) - \text{Area}_{\text{ped}} \cdot (D_f - T_f) \cdot N_{\text{ped}}] \cdot \gamma_s$ $S_w = 78.575 \cdot \text{kips}$	$L_s := \frac{L}{2}$ $L_s = 13 \text{ ft}$	$R_s := S_w \cdot L_s$ $R_s = 1021.479 \cdot \text{ft}_K$
3) Wt. of soil wedge	$W_w := (D_f) \cdot \frac{1}{2} \cdot (D_f \cdot \tan(\phi)) \cdot B \cdot (\gamma_s)$ $W_w = 0 \cdot \text{kips}$	$L_w := \left(L + D_f \cdot \frac{\tan(\phi)}{3} \right)$ $L_w = 26 \text{ ft}$	$R_w := W_w \cdot L_w$ $R_w = 0 \cdot \text{ft}_K$
4) Passive pressure	$Pe_p := T_f \cdot B \cdot P_{\text{pave}}$ $Pe_p = -7.488 \cdot \text{kips}$	$L_p := \frac{T_f}{3}$ $L_p = 1 \text{ ft}$	$R_p := Pe_p \cdot L_p$ $R_p = -7.488 \cdot \text{ft}_K$
5) Vertical	$P_v = 29 \cdot \text{kips}$ $S_{w1} := L \cdot B \cdot D_f \cdot \gamma_s$ $S_{w1} = 324.48 \cdot \text{kips}$	$L_v := \frac{L}{2}$ $L_v = 13 \text{ ft}$	$R_v := P_v \cdot L_v$ $R_v = 377 \cdot \text{ft}_K$
Total weight	$T_w := C_w + S_w + W_w + P_v$ $T_w = 416.547 \cdot \text{kips}$		

Total resisting Moment= $M_r := R_c + R_s + R_w + R_p + R_v$ $M_r = 5407.618 \cdot \text{ft}_K$

Overturning Moments

component	value, kips	lever arm, ft	Overturning Moment ft-kips
1) Moment on foundation due to eccentric location of tower	$P_v = 29 \cdot \text{kips}$	$L_{pe} = 0$	$M_{pe} := L_{pe} \cdot P_v$ $M_{pe} = 0 \cdot \text{ft}_K$
2) Moment on foundation	-	-	$M = 2143 \cdot \text{ft}_K$
3) Moment due to horizontal shear	$S_t := S$	$L_{hs} := D_f + E_g$ $L_{hs} = 4.5 \text{ ft}$	$O_{hs} := L_{hs} \cdot S_t$ $O_{hs} = 112.5 \cdot \text{ft}_K$

Total Overturning Moment= $M_o := M + O_{hs} + M_{pe}$ $M_o = 2255.5 \cdot \text{ft}_K$

Check Safety Factor against Overturning about mid axis parallel to base

$SF := \frac{M_r}{M_o}$ $SF = 2.398 > 1.5$ **O.K!** Calculate eccentricity, e $e := \frac{M_o}{T_w}$ $e = 5.415 \text{ ft}$

Check location of eccentricity and determine pressure distribution under the mat

$$L_{loc} := \frac{L}{6} \quad L_{loc} = 4.333 \text{ ft} \quad \text{For net bearing calcs } T_{w1} := S_{w1} + W_w \quad T_{w1} = 324.48 \cdot \text{kips}$$

$$P_{max1} := \text{if} \left[e \leq L_{loc}, \frac{T_w}{L \cdot B} \cdot \left[1 + \left(6 \cdot \frac{e}{L} \right) \right], 4 \cdot \frac{T_w}{3 \cdot B \cdot (L - 2 \cdot e)} \right] \quad P_{max1} = 1.408 \cdot \text{ksf}$$

$$P_{max2} := \left(\frac{T_{w1}}{L \cdot B} \right) \quad P_{max2} = 0.48 \cdot \text{ksf} \quad P_{net} := P_{max1} - P_{max2} \quad P_{max} := P_{net}$$

Net soil pressure, $P_{net} = 0.928 \cdot \text{ksf} < Brg_{allw} = 3 \cdot \text{ksf}$ **O.K.!**

$$P_{min} := \text{if} \left[e \leq L_{loc}, \frac{T_w}{L \cdot B} \cdot \left[1 - \left(6 \cdot \frac{e}{L} \right) \right], 0 \cdot \text{ksf} \right] \quad P_{min} = 0 \cdot \text{ksf}$$

Check for horizontal shear $P_{hor} := P_e + T_w \cdot 0.35$

$$P_{hor} = 138.303 \cdot \text{kips} \quad S = 25 \cdot \text{kips} \quad \text{Since } P_{hor} > S \quad \text{it is safe!}$$

Check for uplift

Component **Down load value, kips**

1) Soil Weight $S_{ww} := [L \cdot B \cdot (D_f - T_f) - \text{Area}_{ped} \cdot (D_f - T_f) \cdot N_{ped}] \cdot \gamma_s$
 $S_w = 78.575 \cdot \text{kips}$

2) Wt. of soil wedge $W_{ww} := (D_f) \cdot \frac{1}{2} \cdot (D_f \cdot \tan(\phi)) \cdot B \cdot (\gamma_s)$
 $W_w = 0 \cdot \text{kips}$

3) Concrete wt. $C_{ww} := L \cdot B \cdot T_f \cdot (\gamma_c) + \text{Area}_{ped} \cdot \gamma_c \cdot (D_f + E_g - T_f) \cdot N_{ped}$
 $C_w = 308.971 \cdot \text{kips}$

Total down load:

$$TWT1 := S_w + W_w + C_w \quad TWT1 = 387.547 \cdot \text{kips} \quad \text{Total down load}$$

Skin friction around footing:

$$SKF := FF \cdot c_u \cdot (L + B) \cdot 2 \cdot 1.5 \cdot \text{ft} \quad SKF = 0 \cdot \text{kips}$$

$$T_{down} := (TWT1 + SKF) \quad T_{down} = 387.547 \cdot \text{kips} > P_{up} = 318 \cdot \text{kips} \quad \text{OK!}$$

REINFORCED CONCRETE REVIEW

General Input parameters

Concrete Cover, $cc := 3.0\text{ in}$ $RC_{fac} := 1.3$

Reduction factors as per respective ACI sections

$$\phi_{shear} := 0.75 \quad \text{as per ACI 9.3.2.3} \quad \phi_{compr} := 0.75 \quad \text{as per ACI 9.3.2.2}$$
$$\phi_{axten} := 0.9 \quad \text{as per ACI 9.3.2.2 a}$$

Check for wide beam or single shear in mat

Allowable shear stress in concrete for wide beam shear criteria=

$$\nu_{wide} := 2 \cdot \phi_{shear} \cdot \sqrt{f_c \cdot \text{psi}} \quad \nu_{wide} = 82.158 \cdot \text{psi}$$

Effective depth of steel := $T_f - cc$ $d = 33\text{ in}$ $L_{eff} := \text{if}(e \leq L_{loc}, L, L - 2 \cdot e)$ $L_{eff} = 15.17\text{ ft}$

$$\text{dist} := \text{if}\left[N_{ped} = 3, \left(\frac{L}{2} - \frac{1}{3} \cdot \sin(60 \cdot \text{deg}) \cdot \text{TWW} - \frac{1}{2} \cdot \text{Ped}_s - d\right), \left(\frac{L}{2} - \frac{\text{TWW}}{2} - \frac{1}{2} \cdot \text{Ped}_s - d\right)\right]$$

Factor load by RC $P_{maxf} := P_{max} \cdot RC_{fac}$ $P_{minf} := P_{min} \cdot RC_{fac}$

shear on the face of concrete=

$$\text{Shear}_{wide} := (\text{dist}) \cdot B \cdot \left[\frac{P_{maxf} + \left[P_{maxf} - \frac{P_{maxf} - P_{minf}}{L_{eff}} \cdot (\text{dist}) \right]}{2} \right] \quad \text{Shear}_{wide} = 161.734 \cdot \text{kips}$$

Area of concrete in shear = $A_{shear} := B \cdot d$ $A_{shear} = 10296 \cdot \text{in}^2$

Shear stress acting on concrete $\nu_{act} := \frac{\text{Shear}_{wide}}{A_{shear}}$ $\nu_{act} = 15.708 \cdot \text{psi}$

$$\nu_{act} = 15.708 \cdot \text{psi} < \nu_{wide} = 82.158 \cdot \text{psi} \quad \mathbf{O.K!}$$

Check for punching or two-way shear in mat

Calculate allowable shear stress in concrete for punching/two-way shear

$$\beta := \frac{L}{B} \quad \beta = 1 \quad \nu_{punch} := \text{if}\left[\left(2 + \frac{4}{\beta}\right) \cdot \phi_{shear} \cdot \sqrt{f_c \cdot \text{psi}} \leq 4 \cdot \phi_{shear} \cdot \sqrt{f_c \cdot \text{psi}}, \left(2 + \frac{4}{\beta}\right) \cdot \phi_{shear} \cdot \sqrt{f_c \cdot \text{psi}}, 4 \cdot \phi_{shear} \cdot \sqrt{f_c \cdot \text{psi}}\right]$$

$$\nu_{punch} = 164.317 \cdot \text{psi} \quad \text{Area}_{col} := \text{if}\left[\text{col}_t = 0, \frac{\pi}{4} \cdot (\text{Ped}_s + d)^2, (\text{Ped}_s + d)^2\right]$$

$$P_{avg} := \frac{P_{maxf} + P_{minf}}{2} \quad \text{Peri}_{col} := \text{if}\left[\text{col}_t = 0, 2 \cdot \pi \cdot \frac{\text{Ped}_s + d}{2}, 4 \cdot (\text{Ped}_s + d)\right]$$

Factor vertical load $P_{vf} := RC_{fac} \cdot P_v$

Shear stress acting on the concrete face = $\nu_{act} := \frac{P_c - \text{Area}_{col} \cdot P_{avg}}{\text{Peri}_{col} \cdot d \cdot 4}$

$$\nu_{act} = 11.3 \cdot \text{psi} < \nu_{punch} = 164.317 \cdot \text{psi} \quad \mathbf{O.K!}$$

Concrete pedestal
steel check

Effective
diameter/size=

$$D_{\text{pier}} := \text{Ped}_s$$

$$D_{\text{eff}} := \text{Ped}_s - cc \cdot 2 \quad D_{\text{eff}} = 30\text{-in} \quad h := \text{Ped}_s \quad h = 36\text{-in}$$

Effective pier diameter $D_{\text{eff}} := D_{\text{pier}} - cc \cdot 2 \quad D_{\text{eff}} = 2.5\text{ft}$

-Minimum required area of steel per ACI-

$$\text{Area}_{\text{stlmin}} := 0.005 \cdot \frac{\pi}{4} \cdot D_{\text{pier}}^2 \quad \text{-(ACI 10.8.4) \& (ACI 10.9.1)}$$

$$\text{Area}_{\text{stlmin}} = 5.089 \cdot \text{in}^2$$

-Rebar details-

Selected rebar size $d_{\text{bar}} := 8$

-Number of vertical rebars required-

$$\text{NRB} := \text{ceil} \left(\frac{\text{Area}_{\text{stlmin}}}{\text{Area}_{\text{abar}}} \right) \quad \text{NRB} = 7 \quad \text{Area}_{\text{stluse}} := \text{Area}_{\text{abar}} \cdot \text{NRB} \quad \text{Area}_{\text{stluse}} = 5.53 \cdot \text{in}^2$$

Rebar used $\text{NRB} := 11 \quad \text{Area}_{\text{stluse1}} := \text{Area}_{\text{abar}} \cdot \text{NRB} = 8.69 \cdot \text{in}^2 \quad \text{OK!}$

$M_n := 10232 \cdot \text{in-kips}$ from L-PILE OUTPUT. Moment capacity of pedestal

$0.75 \cdot M_n = 639.5 \cdot \text{kips-ft} > M_s := O_{hs} = 112.5 \cdot \text{kips-ft} \quad \text{OK}$

(NRB = 11) $d_{\text{bar}} = 8$ vertical bars OK!

Evaluation of mat footing 26'x26'

$C_{\text{wped}} := \text{Area}_{\text{ped}} \cdot \gamma_c \cdot (D_f + E_g - T_f) \cdot N_{\text{ped}}$ Wt. of concrete pedestals

$P_{\text{upnet}} := P_{\text{up}} - \frac{C_{\text{wped}} + 0.95S_w}{N_{\text{ped}}} \quad P_{\text{upnet}} = 291.527 \cdot \text{kips}$ Net uplift acting at mat level creating bending moment in the slab. Soil wt. reduced by 5 % to account for variation in compaction . ACI 9.3.2.2

Calculate bending moment for mat design:

$\phi_{\text{bend}} := 0.9 \quad \text{Langle} := \text{if}(N_{\text{ped}} = 3, \sin(60\text{-deg}), 1)$

$$\beta_1 := \text{if} \left[f_c \leq 4000 \cdot \text{psi}, 0.85, \text{if} \left[f_c \geq 8000 \cdot \text{psi}, 0.65, 0.85 - \left(\frac{f_c}{\text{psi}} - 4000 \right) \cdot 0.05 \right] \right] \quad \text{ACI 10.2.7.3}$$

$$B_{mo} := RC_{\text{fac}} \cdot \left[(\text{TWW} \cdot P_{\text{up}}) \cdot \text{Langle} + \text{Sh} \cdot (D_f + E_g) - (C_w + S_w) \cdot \left(\text{TWW} \cdot \text{Langle} \cdot \frac{1}{3} \right) \right]$$

$$B := L \quad B = 26 \text{ ft}$$

$$B_{mo} = 1699.63 \cdot \text{ft}_K$$

$$B_{mo1} := \frac{P_{\text{max}} - P_{\text{min}}}{(L - 2 \cdot e) \cdot 2} \cdot \left(\text{TWW} \cdot \text{Langle} \cdot \frac{1}{3} + \frac{\text{Ped}_s}{2} \right) \cdot \left[\left[(L - 2 \cdot e) - \left(\text{TWW} \cdot \text{Langle} \cdot \frac{1}{3} + \frac{\text{Ped}_s}{2} \right) \right]^2 \cdot 0.5 \right] \cdot B$$

$$W_e := \text{TWW} \cdot \text{Langle} + \text{Ped}_s \quad W_e = 9.495 \text{ ft}$$

Reinforcement middle
bandwidth.

$$B_{mo1} = 192.925 \cdot \text{ft}_K$$

$$\text{required } R_u \quad R_u := \frac{B_{mo}}{\phi_{\text{bend}} \cdot B \cdot d^2}$$

$$R_u = 66.698 \cdot \text{psi}$$

$$m := \frac{f_y}{\beta_1 \cdot f_c} \quad m = 23.529$$

$$\rho := \frac{1}{m} \cdot \left[1 - \sqrt{1 - \left(\frac{2 \cdot m \cdot R_u}{f_y} \right)} \right] \quad \rho = 0.001$$

required area of steel for mat =

$$A_{st_f} := \rho \cdot B \cdot d \quad A_{st_f} = 11.599 \cdot \text{in}^2$$

Provided bar size to be
used

$$f_{\text{bar}} := 8$$

$$f_{\text{dia}} := \frac{f_{\text{bar}}}{8} \cdot \text{in} \quad f_{\text{dia}} = 1 \cdot \text{in}$$

Bar area =

$$f_{\text{abar}} := \pi \cdot \frac{f_{\text{dia}}^2}{4} \quad f_{\text{abar}} = 0.785 \cdot \text{in}^2$$

$$N_{\text{req}} := \frac{(A_{st_f})}{f_{\text{abar}}} = 14.768$$

OK!!! 17 # 8 INSTALLED

minimum area of steel required,

$$A_{st_{\text{minf}}} := .0018 \cdot B \cdot T_f$$

$$A_{st_{\text{minf}}} = 20.218 \cdot \text{in}^2$$

$$A_{st_{\text{fuse}}} := \text{if} (A_{st_f} > A_{st_{\text{minf}}}, A_{st_f}, A_{st_{\text{minf}}})$$

$$A_{st_{\text{fuse}}} = 20.218 \cdot \text{in}^2$$

$$\text{Number of bars required} = N_{\text{bars}} := \text{if} \left(A_{st_{\text{fuse}}} = A_{st_{\text{minf}}}, \frac{A_{st_{\text{fuse}}}}{f_{\text{abar}}}, \frac{A_{st_{\text{fuse}}}}{f_{\text{abar}}} \cdot \frac{L}{W_e} \right)$$

$$N_{\text{bars}} = 25.742$$

Total used 34 # 8 T& B

OK!

Summary

-Foundation Reactions-

Shear $S = 25\text{-kips}$
Down load $P_v = 29\text{-kips}$
Uplift load $P_{up} = 318\text{-kips}$
Moment; $M = 2143\text{-ft}_K$

Stability Calculations

Safety Factor against Overturning $SF = 2.398 > 1.5$ **O.K.!**

Net soil pressure, $P_{net} = 0.928\text{-ksf} < Brg_{allw} = 3\text{-ksf}$ **O.K.!**

Check for horizontal shear $P_{hor} = 138.303\text{-kips}$ $S = 25\text{-kips}$ Since $P_{hor} > S$ it is safe!

Size of Mat

$L = 26\text{ft}$ $B = 26\text{ft}$

Depth of base of mat $D_f = 4\text{ft}$ Thickness of Mat $T_f = 3\text{ft}$

Pedestal size $Ped_s = 3\text{ft}$

RESULTS: Based on the above calculations the existing Mat foundation will be able to support the load imposed from the self supporting tower.

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LPILE Plus for Windows, Version 5.0 (5.0.47)

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method

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This program is licensed to:

allpro
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Files Used for Analysis

Path to file locations: P:\2016\Structural\16-2859 CT46126-A-01 Glastonbury
Structural Analysis\LPILE\
Name of input data file: 36 PEDESTAL.lpd
Name of output file: 36 PEDESTAL.lpo
Name of plot output file: 36 PEDESTAL.lpp
Name of runtime file: 36 PEDESTAL.lpr

Time and Date of Analysis

Date: August 12, 2016 Time: 9:38:31

Problem Title

New LPILE Plus 5.0 Data File

Program Options

Units Used in Computations - US Customary Units: Inches, Pounds

Basic Program Options:

Analysis Type 2:
- Computation of Ultimate Bending Moment of Cross Section (Section Design)

 Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Number of sections = 1

Pile Section No. 1

The sectional shape is a circular drilled shaft (bored pile).

Outside Diameter = 36.0000 in

Material Properties:

Compressive Strength of Concrete = 3.000 kip/in**2
 Yield Stress of Reinforcement = 60. kip/in**2
 Modulus of Elasticity of Reinforcement = 29000. kip/in**2
 Number of Reinforcing Bars = 11
 Area of Single Bar = 0.79000 in**2
 Number of Rows of Reinforcing Bars = 11
 Area of Steel = 8.690 in**2
 Area of Shaft = 1017.876 in**2
 Percentage of Steel Reinforcement = 0.854 percent
 Cover Thickness (edge to bar center) = 3.700 in

Unfactored Axial Squash Load Capacity = 3094.82 kip

Distribution and Area of Steel Reinforcement

Row Number	Area of Reinforcement in**2	Distance to Centroidal Axis in
1	0.790	14.154
2	0.790	13.008
3	0.790	10.807
4	0.790	7.731
5	0.790	4.029
6	0.790	0.000
7	0.790	-4.029
8	0.790	-7.731
9	0.790	-10.807
10	0.790	-13.008
11	0.790	-14.154

Axial Thrust Force = -318000.00 lbs

Bending Max. Steel Moment Stress in-lbs psi	Bending Stiffness lb-in2	Bending Curvature rad/in	Maximum Strain in/in	Neutral Axis Position inches	Max. Concrete Stress psi
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353194.94438	2.825560E+11	0.00000125	1.341105E-12	0.00000107	0.00000
1165.59865					
697346.65086	2.789387E+11	0.00000250	2.682209E-12	0.00000107	0.00000
2331.19730					
1032455.	2.753214E+11	0.00000375	4.023314E-12	0.00000107	0.00000
3496.79595					
1032455.	2.064910E+11	0.00000500	5.364418E-12	0.00000107	0.00000
4662.39460					
1032455.	1.651928E+11	0.00000625	6.705523E-12	0.00000107	0.00000
5827.99326					
1032455.	1.376607E+11	0.00000750	8.046627E-12	0.00000107	0.00000
6993.59191					
1032455.	1.179949E+11	0.00000875	9.387732E-12	0.00000107	0.00000
8159.19056					
1032455.	1.032455E+11	0.00001000	1.072884E-11	0.00000107	0.00000
9324.78921					
1032455.	9.177379E+10	0.00001125	1.206994E-11	0.00000107	0.00000
10490.38786					
1032455.	8.259641E+10	0.00001250	1.341105E-11	0.00000107	0.00000
11655.98651					
1032455.	7.508765E+10	0.00001375	1.475215E-11	0.00000107	0.00000
12821.58516					
1032455.	6.883034E+10	0.00001500	1.609325E-11	0.00000107	0.00000
13987.18381					
1032455.	6.353570E+10	0.00001625	1.743436E-11	0.00000107	0.00000
15152.78246					
1032455.	5.899744E+10	0.00001750	1.877546E-11	0.00000107	0.00000
16318.38111					
1032455.	5.506427E+10	0.00001875	2.011657E-11	0.00000107	0.00000
17483.97977					
1032455.	5.162276E+10	0.00002000	2.145767E-11	0.00000107	0.00000
18649.57842					
1032455.	4.858612E+10	0.00002125	2.279878E-11	0.00000107	0.00000
19815.17707					
1032455.	4.588689E+10	0.00002250	2.413988E-11	0.00000107	0.00000
20980.77572					
1032455.	4.347179E+10	0.00002375	2.548099E-11	0.00000107	0.00000
22146.37437					
1032455.	4.129820E+10	0.00002500	2.682209E-11	0.00000107	0.00000
23311.97302					
1032455.	3.933162E+10	0.00002625	2.816319E-11	0.00000107	0.00000
24477.57167					
1032455.	3.754382E+10	0.00002750	2.950430E-11	0.00000107	0.00000
25643.17032					
1032455.	3.591148E+10	0.00002875	3.084540E-11	0.00000107	0.00000
26808.76897					
1032455.	3.441517E+10	0.00003000	3.218651E-11	0.00000107	0.00000
27974.36763					
1032455.	3.303856E+10	0.00003125	3.352761E-11	0.00000107	0.00000
29139.96628					
1032455.	3.176785E+10	0.00003250	3.486872E-11	0.00000107	0.00000
30305.56493					
1032455.	3.059126E+10	0.00003375	3.620982E-11	0.00000107	0.00000
31471.16358					

1032455.	2.949872E+10	0.00003500	3.755093E-11	0.00000107	0.00000
32636.76223					
1032455.	2.848152E+10	0.00003625	3.889203E-11	0.00000107	0.00000
33802.36088					
1032455.	2.753214E+10	0.00003750	4.023314E-11	0.00000107	0.00000
34967.95953					
1032455.	2.664400E+10	0.00003875	4.157424E-11	0.00000107	0.00000
36133.55818					
1032455.	2.581138E+10	0.00004000	4.291534E-11	0.00000107	0.00000
37299.15683					
1062879.	2.576676E+10	0.00004125	4.425645E-11	0.00000107	0.00000
38464.75548					
1095087.	2.576676E+10	0.00004250	4.559755E-11	0.00000107	0.00000
39630.35414					
1127296.	2.576676E+10	0.00004375	4.693866E-11	0.00000107	0.00000
40795.95279					
1159504.	2.576676E+10	0.00004500	4.827976E-11	0.00000107	0.00000
41961.55144					
1191713.	2.576676E+10	0.00004625	4.962087E-11	0.00000107	0.00000
43127.15009					
1223921.	2.576676E+10	0.00004750	5.096197E-11	0.00000107	0.00000
44292.74874					
1256130.	2.576676E+10	0.00004875	5.230308E-11	0.00000107	0.00000
45458.34739					
1320547.	2.576676E+10	0.00005125	5.498528E-11	0.00000107	0.00000
47789.54469					
1384963.	2.576676E+10	0.00005375	5.766749E-11	0.00000107	0.00000
50120.74199					
1449380.	2.576676E+10	0.00005625	6.034970E-11	0.00000107	0.00000
52451.93930					
1513797.	2.576676E+10	0.00005875	6.303191E-11	0.00000107	0.00000
54783.13660					
1578214.	2.576676E+10	0.00006125	6.571412E-11	0.00000107	0.00000
57114.33390					
1642631.	2.576676E+10	0.00006375	6.839633E-11	0.00000107	0.00000
59445.53120					
1687181.	2.546688E+10	0.00006625	7.107854E-11	0.00000107	0.00000
60000.00000					
1706810.	2.482633E+10	0.00006875	7.376075E-11	0.00000107	0.00000
60000.00000					
1722058.	2.416924E+10	0.00007125	7.644296E-11	0.00000107	0.00000
60000.00000					
1739451.	2.358578E+10	0.00007375	0.00001828	0.24788439	0.00000
60000.00000					
1771884.	2.323782E+10	0.00007625	0.00005142	0.67430842	89.09508462
60000.00000					
1805018.	2.292086E+10	0.00007875	0.00008455	1.07365716	188.26949
60000.00000					
1847427.	2.273756E+10	0.00008125	0.00011311	1.39210403	271.80103
60000.00000					
1886711.	2.252790E+10	0.00008375	0.00014313	1.70902956	358.10787
60000.00000					
1935716.	2.244308E+10	0.00008625	0.00016809	1.94885337	428.22115
60000.00000					
1972682.	2.222741E+10	0.00008875	0.00019301	2.17473829	497.08749
60000.00000					

2002376.	2.194385E+10	0.00009125	0.00021602	2.36735094	559.51592
60000.00000					
2039078.	2.175017E+10	0.00009375	0.00023347	2.49033558	605.70777
60000.00000					
2071509.	2.152217E+10	0.00009625	0.00025423	2.64136755	660.35395
60000.00000					
2103800.	2.130430E+10	0.00009875	0.00027505	2.78535712	714.38080
60000.00000					
2135950.	2.109581E+10	0.00010125	0.00029594	2.92283857	767.78468
60000.00000					
2173519.	2.094958E+10	0.00010375	0.00031203	3.00749981	807.94674
60000.00000					
2207562.	2.077705E+10	0.00010625	0.00033115	3.11674941	855.45408
60000.00000					
2241480.	2.061131E+10	0.00010875	0.00035034	3.22148860	902.44576
60000.00000					
2270707.	2.041085E+10	0.00011125	0.00036843	3.31170309	946.04983
60000.00000					
2290965.	2.014035E+10	0.00011375	0.00038433	3.37868965	983.66545
60000.00000					
2311157.	1.988092E+10	0.00011625	0.00040026	3.44311845	1020.92643
60000.00000					
2331282.	1.963185E+10	0.00011875	0.00041624	3.50515044	1057.82926
60000.00000					
2351339.	1.939248E+10	0.00012125	0.00043225	3.56494009	1094.37241
60000.00000					
2363136.	1.909605E+10	0.00012375	0.00044550	3.59999979	1123.96639
60000.00000					
2395164.	1.897159E+10	0.00012625	0.00045770	3.62534344	1150.80481
60000.00000					
2415688.	1.876263E+10	0.00012875	0.00047272	3.67159116	1183.89220
60000.00000					
2436155.	1.856118E+10	0.00013125	0.00048777	3.71632183	1216.65685
60000.00000					
2456562.	1.836682E+10	0.00013375	0.00050285	3.75962126	1249.09629
60000.00000					
2476910.	1.817916E+10	0.00013625	0.00051796	3.80157101	1281.20866
60000.00000					
2497199.	1.799783E+10	0.00013875	0.00053311	3.84224617	1312.99190
60000.00000					
2517427.	1.782249E+10	0.00014125	0.00054829	3.88171756	1344.44419
60000.00000					
2537593.	1.765282E+10	0.00014375	0.00056351	3.92004740	1375.56254
60000.00000					
2557699.	1.748854E+10	0.00014625	0.00057876	3.95730007	1406.34596
60000.00000					
2573231.	1.729903E+10	0.00014875	0.00059268	3.98443329	1433.97410
60000.00000					
2594722.	1.687624E+10	0.00015375	0.00061777	4.01802528	1482.57670
60000.00000					
2616085.	1.647927E+10	0.00015875	0.00064294	4.05001009	1530.25819
60000.00000					
2637319.	1.610576E+10	0.00016375	0.00066819	4.08054650	1577.01109
60000.00000					
2658421.	1.575361E+10	0.00016875	0.00069352	4.10976970	1622.82600
60000.00000					

2679390.	1.542095E+10	0.00017375	0.00071894	4.13779986	1667.69347
60000.00000					
2700226.	1.510616E+10	0.00017875	0.00074445	4.16474855	1711.60535
60000.00000					
2720925.	1.480776E+10	0.00018375	0.00077004	4.19071019	1754.55142
60000.00000					
2732141.	1.447492E+10	0.00018875	0.00079275	4.19999921	1791.41683
60000.00000					
2737739.	1.413027E+10	0.00019375	0.00081375	4.19999921	1824.54318
60000.00000					
2784196.	1.400853E+10	0.00019875	0.00083643	4.20845997	1859.68824
60000.00000					
2804589.	1.376485E+10	0.00020375	0.00086137	4.22760236	1897.56754
60000.00000					
2824852.	1.353222E+10	0.00020875	0.00088639	4.24618256	1934.49264
60000.00000					
2843606.	1.330342E+10	0.00021375	0.00091093	4.26168144	1969.63198
60000.00000					
2853186.	1.304313E+10	0.00021875	0.00093193	4.26023304	1998.54832
60000.00000					
2862693.	1.279416E+10	0.00022375	0.00095296	4.25904429	2026.78800
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2872124.	1.255573E+10	0.00022875	0.00097404	4.25809801	2054.34598
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2881480.	1.232719E+10	0.00023375	0.00099516	4.25738132	2081.21813
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2890761.	1.210790E+10	0.00023875	0.00101633	4.25688350	2107.40057
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2899965.	1.189729E+10	0.00024375	0.00103754	4.25659168	2132.88829
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2909093.	1.169484E+10	0.00024875	0.00105880	4.25649726	2157.67727
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2918142.	1.150007E+10	0.00025375	0.00108011	4.25658953	2181.76247
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2927113.	1.131252E+10	0.00025875	0.00110146	4.25685990	2205.13921
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2936004.	1.113177E+10	0.00026375	0.00112286	4.25729978	2227.80248
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2944817.	1.095746E+10	0.00026875	0.00114431	4.25790489	2249.74829
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2953550.	1.078922E+10	0.00027375	0.00116581	4.25866663	2270.97110
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2962201.	1.062673E+10	0.00027875	0.00118736	4.25957859	2291.46574
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2970769.	1.046967E+10	0.00028375	0.00120895	4.26063430	2311.22684
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2979256.	1.031777E+10	0.00028875	0.00123060	4.26183164	2330.24997
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2987661.	1.017076E+10	0.00029375	0.00125230	4.26316416	2348.52929
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2995979.	1.002838E+10	0.00029875	0.00127406	4.26462543	2366.05879
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3004215.	9.890420E+09	0.00030375	0.00129586	4.26621544	2382.83392
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3012365.	9.756647E+09	0.00030875	0.00131772	4.26792777	2398.84825
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3020427.	9.626859E+09	0.00031375	0.00133964	4.26975811	2414.09579
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3028404.	9.500875E+09	0.00031875	0.00136161	4.27170646	2428.57128
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3036291.	9.378505E+09	0.00032375	0.00138363	4.27376640	2442.26786
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3044090.	9.259590E+09	0.00032875	0.00140571	4.27593791	2455.17987
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3051801.	9.143973E+09	0.00033375	0.00142786	4.27821887	2467.30098
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3059420.	9.031499E+09	0.00033875	0.00145005	4.28060496	2478.62428
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3066947.	8.922027E+09	0.00034375	0.00147231	4.28309405	2489.14311
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3071696.	8.807731E+09	0.00034875	0.00149257	4.27975738	2497.92458
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3077558.	8.578559E+09	0.00035875	0.00153053	4.26628411	2512.47188
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3083191.	8.361197E+09	0.00036875	0.00156864	4.25394595	2524.68845
60000.00000					
3088594.	8.154705E+09	0.00037875	0.00160691	4.24266350	2534.54470
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3093761.	7.958228E+09	0.00038875	0.00164533	4.23236167	2542.00957
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3098692.	7.771015E+09	0.00039875	0.00168391	4.22298038	2547.05150
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3103379.	7.592365E+09	0.00040875	0.00172266	4.21445739	2549.63713
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3107638.	7.421224E+09	0.00041875	0.00176157	4.20674336	2547.08926
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3107638.	6.774142E+09	0.00045875	0.00192675	4.19999921	2539.18102
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3107638.	6.629627E+09	0.00046875	0.00196875	4.19999921	2544.89171
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3107638.	6.491149E+09	0.00047875	0.00201075	4.19999921	2548.48445
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3107638.	6.358338E+09	0.00048875	0.00205275	4.19999921	2549.95925
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3107638.	6.230853E+09	0.00049875	0.00209475	4.19999921	2545.34820
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3107638.	5.990627E+09	0.00051875	0.00217875	4.19999921	2533.77136
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3107638.	5.877329E+09	0.00052875	0.00222075	4.19999921	2527.98294
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3107638.	5.768237E+09	0.00053875	0.00226275	4.19999921	2523.61262
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3107638.	5.369568E+09	0.00057875	0.00243075	4.19999921	2546.87061
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3107638.	5.278366E+09	0.00058875	0.00247275	4.19999921	2549.14062
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3107638.	5.190209E+09	0.00059875	0.00251475	4.19999921	2549.99283
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3107638.	5.104949E+09	0.00060875	0.00255675	4.19999921	2545.74288
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3107638.	5.022445E+09	0.00061875	0.00259875	4.19999921	2541.00690
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3107638.	4.942565E+09	0.00062875	0.00264075	4.19999921	2536.27092
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3107638.	4.865186E+09	0.00063875	0.00268275	4.19999921	2531.53494
60000.00000					
3107638.	4.790193E+09	0.00064875	0.00272475	4.19999921	2526.79896
60000.00000					

Axial Thrust Force = 339000.00 lbs

Bending Max. Steel Moment Stress in-lbs psi	Bending Stiffness lb-in2	Bending Curvature rad/in	Maximum Strain in/in	Neutral Axis Position inches	Max. Concrete Stress psi
337260.14478	2.698081E+11	0.00000125	0.00012388	99.10780871	374.14819
3453.25676					
674442.60361	2.697770E+11	0.00000250	0.00014658	58.63121903	438.59209
3971.96076					
1011501.	2.697337E+11	0.00000375	0.00016935	45.15934575	502.28235
4492.87492					
1348391.	2.696781E+11	0.00000500	0.00019219	38.43865693	565.20908
5016.00001					
1684825.	2.695721E+11	0.00000625	0.00021511	34.41772091	627.34996
5541.20537					
2022072.	2.696096E+11	0.00000750	0.00023813	31.75065672	688.77618
6069.35998					
2355924.	2.692485E+11	0.00000875	0.00026116	29.84699214	749.23715
6597.86508					
2686653.	2.686653E+11	0.00001000	0.00028420	28.41979516	808.71417
7126.53011					
3016523.	2.681354E+11	0.00001125	0.00030731	27.31661332	867.38984
7657.43330					
3341311.	2.673048E+11	0.00001250	0.00033036	26.42901671	924.90117
8186.50546					
3341311.	2.430044E+11	0.00001375	0.00033568	24.41292250	937.29749
8201.23844					
3341311.	2.227540E+11	0.00001500	0.00035360	23.57307565	980.93724
8581.47219					

3341311.	2.056191E+11	0.00001625	0.00037115	22.83972752	1023.07924
8951.00456					
3341311.	1.909320E+11	0.00001750	0.00038850	22.19999921	1064.17878
9314.88126					
3445738.	1.837727E+11	0.00001875	0.00040525	21.61333144	1103.28413
9661.22932					
3555771.	1.777886E+11	0.00002000	0.00042188	21.09383476	1141.57954
10004.00320					
3661465.	1.723042E+11	0.00002125	0.00043828	20.62490523	1178.84357
10340.27558					
3763820.	1.672809E+11	0.00002250	0.00045451	20.20055401	1215.22225
10671.63791					
3860251.	1.625369E+11	0.00002375	0.00047036	19.80472004	1250.24947
10991.87604					
3955809.	1.582324E+11	0.00002500	0.00048619	19.44760430	1284.76298
11311.48692					
4050206.	1.542935E+11	0.00002625	0.00050199	19.12351191	1318.75533
11630.34593					
4138068.	1.504752E+11	0.00002750	0.00051727	18.80982435	1351.15334
11934.00610					
4228490.	1.470779E+11	0.00002875	0.00053284	18.53369415	1383.74897
12246.23736					
4312595.	1.437532E+11	0.00003000	0.00054785	18.26177609	1414.71054
12542.11376					
4396472.	1.406871E+11	0.00003125	0.00056289	18.01236069	1445.30412
12838.66913					
4481214.	1.378835E+11	0.00003250	0.00057806	17.78650796	1475.77062
13541.78218					
4561763.	1.351633E+11	0.00003375	0.00059283	17.56533730	1504.99149
14279.09075					
4645549.	1.327300E+11	0.00003500	0.00060804	17.37262809	1534.69043
15003.54580					
4723169.	1.302943E+11	0.00003625	0.00062255	17.17388928	1562.58919
15748.31090					
4800580.	1.280155E+11	0.00003750	0.00063709	16.98897350	1590.14088
16492.45202					
4877782.	1.258782E+11	0.00003875	0.00065164	16.81654823	1617.34408
17235.96332					
4956941.	1.239235E+11	0.00004000	0.00066652	16.66299498	1644.76397
17970.08390					
5031613.	1.219785E+11	0.00004125	0.00068083	16.50485837	1670.71549
18720.81994					
5106084.	1.201432E+11	0.00004250	0.00069515	16.35651720	1696.32779
19470.94801					
5180352.	1.184081E+11	0.00004375	0.00070950	16.21713245	1721.59921
20220.46735					
5257075.	1.168239E+11	0.00004500	0.00072430	16.09548247	1747.28558
20956.94822					
5329190.	1.152257E+11	0.00004625	0.00073841	15.96554768	1771.37179
21713.36070					
5401111.	1.137076E+11	0.00004750	0.00075254	15.84288275	1795.12619
22469.17923					
5472838.	1.122633E+11	0.00004875	0.00076669	15.72693193	1818.54745
23224.39889					
5618808.	1.096353E+11	0.00005125	0.00079564	15.52475774	1865.35020
24715.87509					

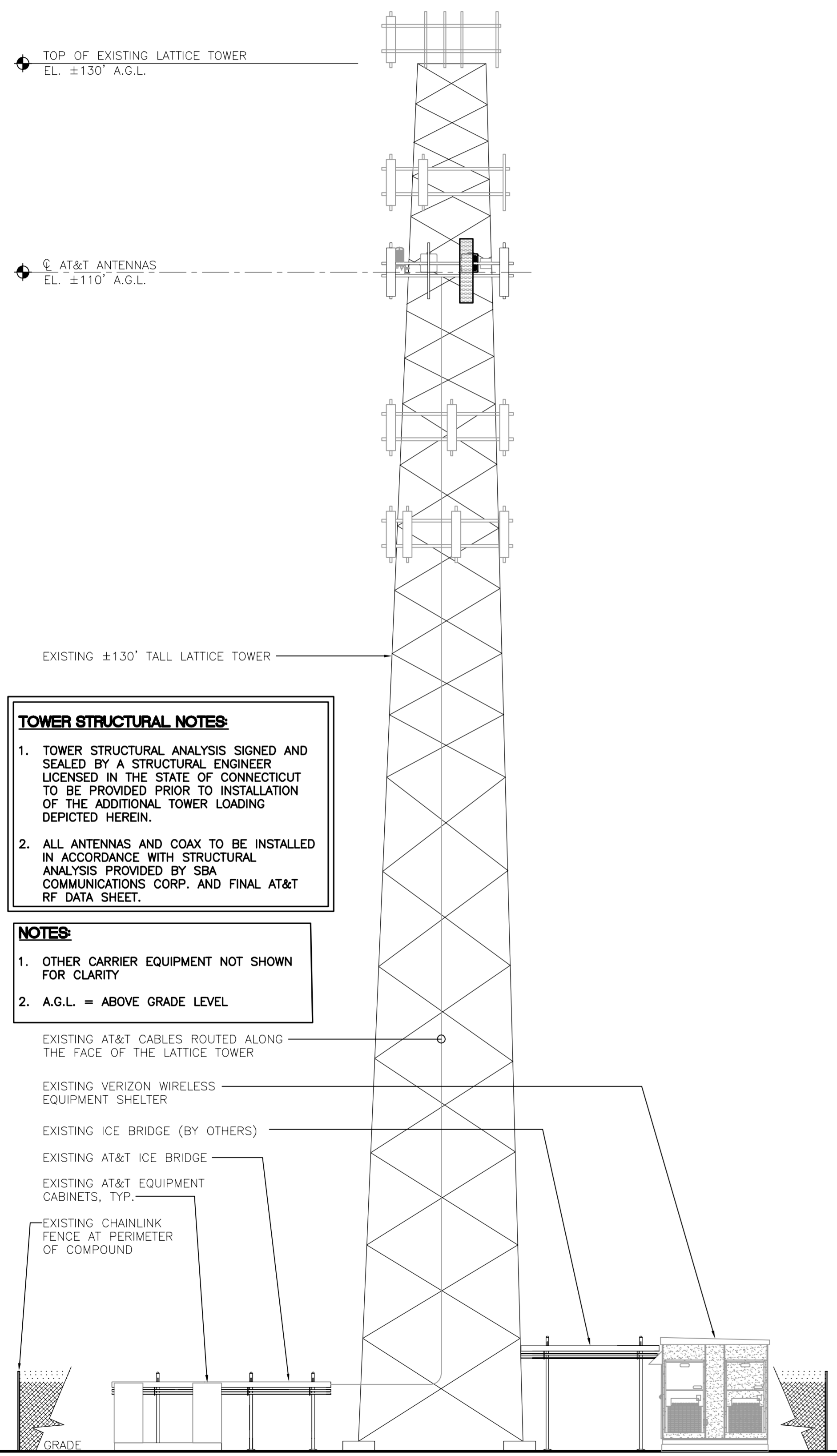
26237.45256	5758086.	1.071272E+11	0.00005375	0.00082356	15.32207930	1908.96771
27756.65333	5896611.	1.048286E+11	0.00005625	0.00085156	15.13887370	1951.27480
29246.74031	6038353.	1.027805E+11	0.00005875	0.00088057	14.98834813	1993.61559
30775.32845	6173192.	1.007868E+11	0.00006125	0.00090824	14.82843482	2032.52201
32301.51299	6307294.	9.893794E+10	0.00006375	0.00093600	14.68236387	2070.13161
33825.26382	6440649.	9.721734E+10	0.00006625	0.00096384	14.54858387	2106.43269
35346.55153	6573246.	9.561085E+10	0.00006875	0.00099177	14.42576873	2141.41328
36838.08281	6708215.	9.415039E+10	0.00007125	0.00102073	14.32597339	2176.19562
38367.08577	6837769.	9.271551E+10	0.00007375	0.00104839	14.21542346	2207.94208
39893.54247	6966580.	9.136498E+10	0.00007625	0.00107614	14.11327422	2238.37666
41417.41931	7094637.	9.009062E+10	0.00007875	0.00110398	14.01874030	2267.48673
42938.67281	7221930.	8.888529E+10	0.00008125	0.00113190	13.93113720	2295.25974
44457.27037	7348445.	8.774263E+10	0.00008375	0.00115993	13.84985769	2321.68240
45926.86568	7477961.	8.670100E+10	0.00008625	0.00118964	13.79288113	2348.15866
47450.59387	7601957.	8.565586E+10	0.00008875	0.00121748	13.71808183	2371.45156
48971.50045	7725185.	8.465956E+10	0.00009125	0.00124542	13.64844739	2393.39273
50489.54130	7847630.	8.370805E+10	0.00009375	0.00127346	13.58358085	2413.96787
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53516.81670	8090123.	8.192530E+10	0.00009875	0.00132984	13.46677601	2450.96148
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56531.99177	8329334.	8.028273E+10	0.00010375	0.00138664	13.36525118	2482.31110
58034.89763	8447674.	7.950752E+10	0.00010625	0.00141521	13.31959140	2495.82966
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60000.00000	10045133.	4.699477E+10	0.00021375	0.00251105	11.74760234	2545.21082
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10242908.	3.811315E+10	0.00026875	0.00304860	11.34362733	2539.75781
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10258506.	3.747399E+10	0.00027375	0.00309634	11.31084216	2543.23863
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10273544.	3.685576E+10	0.00027875	0.00314440	11.28035080	2546.03803
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10333351.	3.293498E+10	0.00031375	0.00349053	11.12520969	2539.18818
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10336101.	3.242698E+10	0.00031875	0.00353829	11.10051835	2542.26482
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10338796.	3.193450E+10	0.00032375	0.00358612	11.07681406	2544.83785
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10349019.	3.010624E+10	0.00034375	0.00377819	10.99108851	2549.95521
60000.00000					
10349393.	2.967568E+10	0.00034875	0.00382795	10.97620332	2547.98784
60000.00000					

Unfactored (Nominal) Moment Capacity at Concrete Strain of 0.003 = 10232.92656
in-kip

The analysis ended normally.



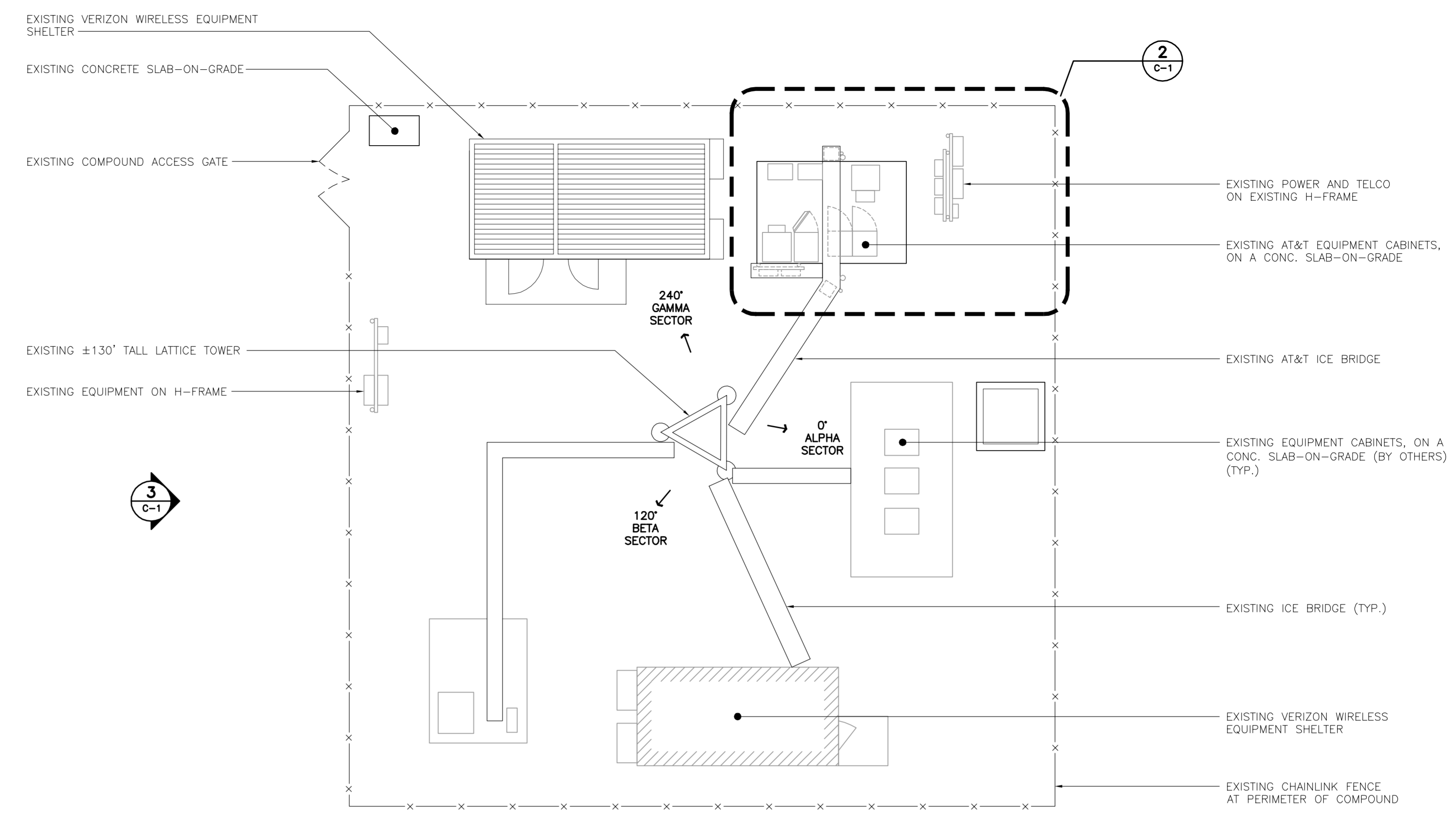
3 NORTH TOWER ELEVATION
 C-1 SCALE: 1/8" = 1'-0"
 GRAPHIC SCALE
 (IN FEET)
 1 inch = 8 ft.

TOWER STRUCTURAL NOTES:

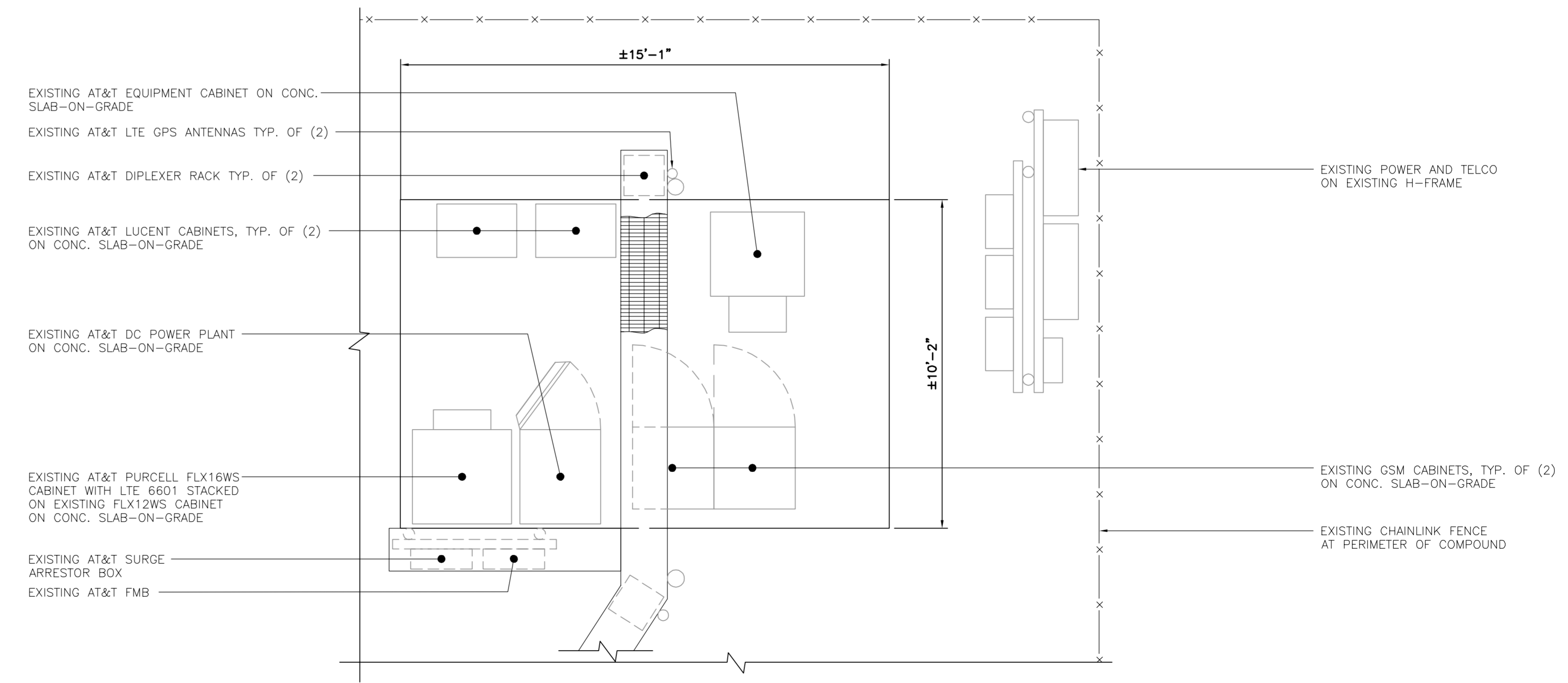
1. TOWER STRUCTURAL ANALYSIS SIGNED AND SEALED BY A STRUCTURAL ENGINEER LICENSED IN THE STATE OF CONNECTICUT TO BE PROVIDED PRIOR TO INSTALLATION OF THE ADDITIONAL TOWER LOADING DEPICTED HEREIN.
2. ALL ANTENNAS AND COAX TO BE INSTALLED IN ACCORDANCE WITH STRUCTURAL ANALYSIS PROVIDED BY SBA COMMUNICATIONS CORP. AND FINAL AT&T RF DATA SHEET.

NOTES:

1. OTHER CARRIER EQUIPMENT NOT SHOWN FOR CLARITY
2. A.G.L. = ABOVE GRADE LEVEL

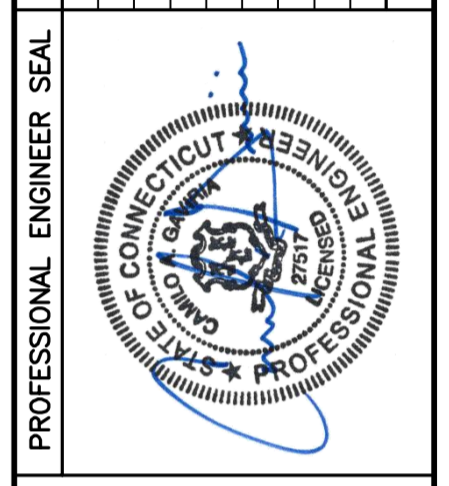


1 COMPOUND PLAN
 C-1 SCALE: 1/8" = 1'-0"
 TRUE NORTH
 GRAPHIC SCALE
 (IN FEET)
 1 inch = 8 ft.



2 EQUIPMENT LAYOUT PLAN
 C-1 SCALE: 3/8" = 1'-0"
 TRUE NORTH

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 SCALE: AS NOTED
 JOB NO. 16071.36

PLANS AND NORTH ELEVATION

C-1
 Sheet No. 3 of 8

AT&T PANEL ANTENNA POS. 1
(ALPHA AND GAMMA SECTOR)
(P/N: CCI HPA-65R-BUU-H6), TYP.
OF (1) PER SECTOR/(2) TOTAL.

EXISTING ±130' TALL LATTICE TOWER

EXISTING RRUS-11, TYP. OF (1)
PER SECTOR/(3) TOTAL.

EXISTING AT&T PANEL ANTENNA
POS. 1&4 (P/N: KATHREIN 800-10121)
TYP. OF (2) PER SECTOR/(6) TOTAL.

240' GSM
GAMMA
SECTOR

240' LTE
GAMMA
SECTOR

EXISTING TMA, TYP. OF (2)
PER SECTOR/(6) TOTAL.

240' UMS
GAMMA
SECTOR

2
C-2

PROPOSED ANTENNA PLAN

SCALE: 1/2" = 1'-0"



4
C-2

AT&T PANEL ANTENNA POS. 1
(BETA SECTOR)
(P/N: CCI HPA-65R-BUU-H8), TYP.
OF (1) PER SECTOR/(1) TOTAL.

EXISTING REPOSITIONED T-ARM TYP. OF (3),
(1) PER SECTOR.

120' UMS
BETA
SECTOR

AT&T RRUS-12+A2, TYP. OF
(1) PER SECTOR/(3) TOTAL.

EXISTING AT&T SURGE
ARRESTOR, TYP. OF (1).

EXISTING AT&T PANEL ANTENNA POS. 1
(ALPHA & GAMMA SECTOR) (P/N: KMW
AM-X-CD-16-65-00T-RET) TYP. OF
(1) PER SECTOR/(2) TOTAL. **TO BE
REMOVED, RELOCATED AND REPLACED.**

EXISTING T-ARM TYP. OF (3)
PER SECTOR **TO BE REORIENTED
FOR PROPOSED AZIMUTH.**

EXISTING RRUS-11, TYP. OF (2)
PER SECTOR/(6) TOTAL.

EXISTING TMA, TYP. OF (2)
PER SECTOR/(6) TOTAL.

240' LTE
GAMMA
SECTOR

315' UMS
GAMMA
SECTOR

315' GSM
GAMMA
SECTOR

1
C-2

EXISTING ANTENNA PLAN

SCALE: 1/2" = 1'-0"



3
C-2

EXISTING AT&T SURGE
ARRESTOR, TYP. OF (1).

EXISTING AT&T PANEL ANTENNA POS. 1
(BETA SECTOR) (P/N: ANDREW
SBNH-1D6565C) TYP. OF (1) PER
SECTOR/(1) TOTAL. **TO BE REMOVED,
RELOCATED AND REPLACED**

120' LTE
BETA
SECTOR

EXISTING AT&T PANEL ANTENNA
POS. 3&4 (P/N: KATHREIN 800-10121)
TYP. OF (2) PER SECTOR/(6) TOTAL.

130' UMS
BETA
SECTOR

EXISTING ±130' TALL LATTICE TOWER

EXISTING RRUS-11, TYP. OF (1)
PER SECTOR/(3) TOTAL.

EXISTING AT&T SURGE
ARRESTOR, TYP. OF (1).

EXISTING REPOSITIONED T-ARM TYP. OF (3)
PER SECTOR

EXISTING ±130' TALL LATTICE TOWER

AT&T PANEL ANTENNA POS. 2 TYP. OF
(1) PER SECTOR/(3) TOTAL:
• ALPHA/GAMMA SECTOR: (P/N: CCI
HPA-65R-BUU-H6)
• BETA SECTOR: (P/N: CCI HPA-65R
-BUU-H8)

EXISTING TMA, TYP. OF (2)
PER SECTOR/(6) TOTAL.

EXISTING AT&T PANEL ANTENNA
POS. 1&4 (P/N: KATHREIN 800-10121)
TYP. OF (2) PER SECTOR/(6) TOTAL

AT&T ANTENNAS
EL. ±110' (A.G.L.)

AT&T RRUS-12+A2, TYP. OF
(1) PER SECTOR/(3) TOTAL.

4
C-2

PROPOSED ANTENNA ELEVATION

SCALE: 3/8" = 1'-0"

EXISTING AT&T PANEL ANTENNA
POS. 3&4 (P/N: KATHREIN 800-10121)
TYP. OF (2) PER SECTOR/(6) TOTAL

EXISTING AT&T SURGE
ARRESTOR, TYP. OF (1).

EXISTING T-ARM TYP. OF (3)
PER SECTOR **TO BE REORIENTED
FOR PROPOSED AZIMUTH.**

EXISTING ±130' TALL LATTICE TOWER

EXISTING AT&T PANEL ANTENNA POS. 1
TYP. OF (1) PER SECTOR/(3) TOTAL.
TO BE REMOVED AND REPLACED:
• ALPHA/GAMMA SECTOR: (P/N: KMW
AM-X-CD-16-65-00T-RET)
• BETA SECTOR: (P/N: ANDREW
SBNH-1D6565C)

AT&T ANTENNAS
EL. ±110' (A.G.L.)

EXISTING TMA, TYP. OF (2)
PER SECTOR/(6) TOTAL.

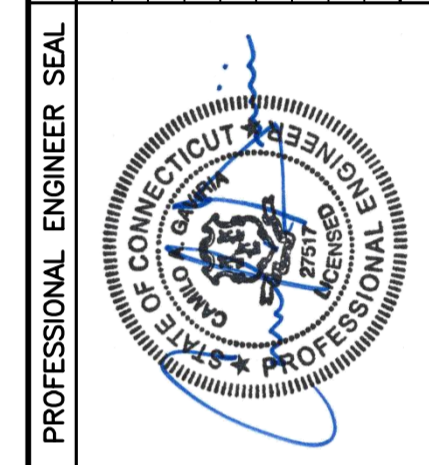
EXISTING RRUS-11, TYP. OF (2)
PER SECTOR/(6) TOTAL.

3
C-2

EXISTING ANTENNA ELEVATION

SCALE: 3/8" = 1'-0"

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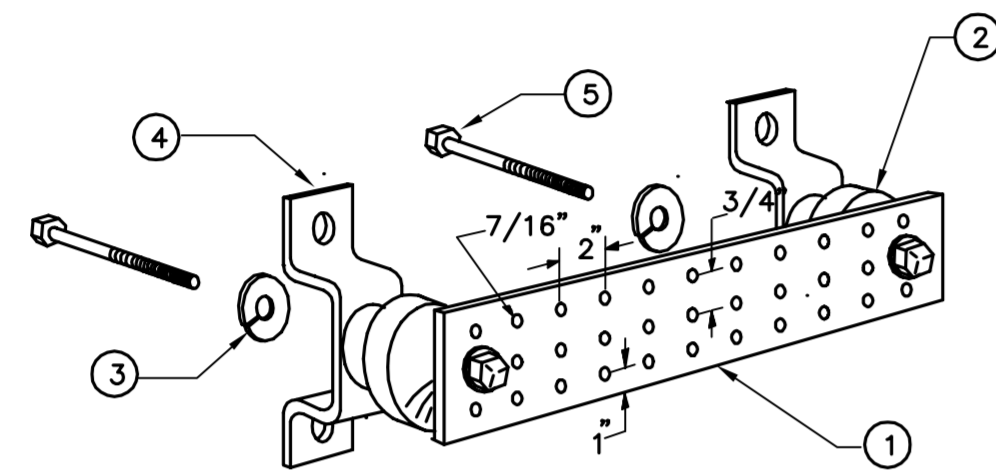
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LTE
EQUIPMENT
DETAILS

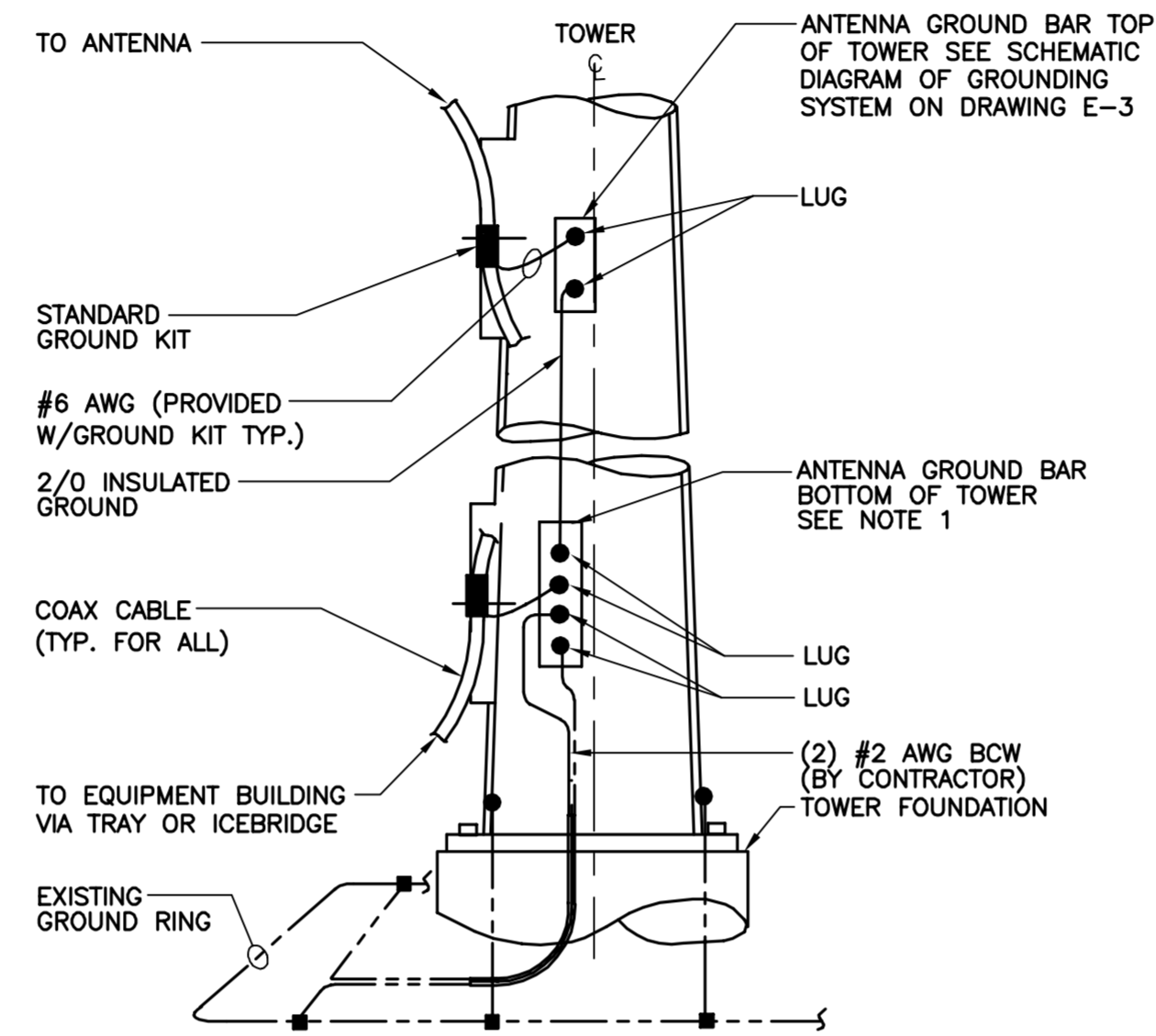
C-2
Sheet No. 4 of 8



LEGEND

1. TINNED COPPER GROUND BAR, 1/4"x 4"x 20", NEWTON INSTRUMENT CO. HOLE CENTERS TO MATCH NEMA DOUBLE LUG .
2. INSULATORS, NEWTON INSTRUMENT CAT. NO. 2. 3061-4.
3. 5/8" LOCK WASHERS, NEWTON INSTRUMENT CO. CAT. NO. 3015-8.
4. WALL MOUNTING BRACKET, NEWTON INSTRUMENT CO. CAT. NO. A-6056.
5. STAINLESS STEEL SECURITY SCREWS.

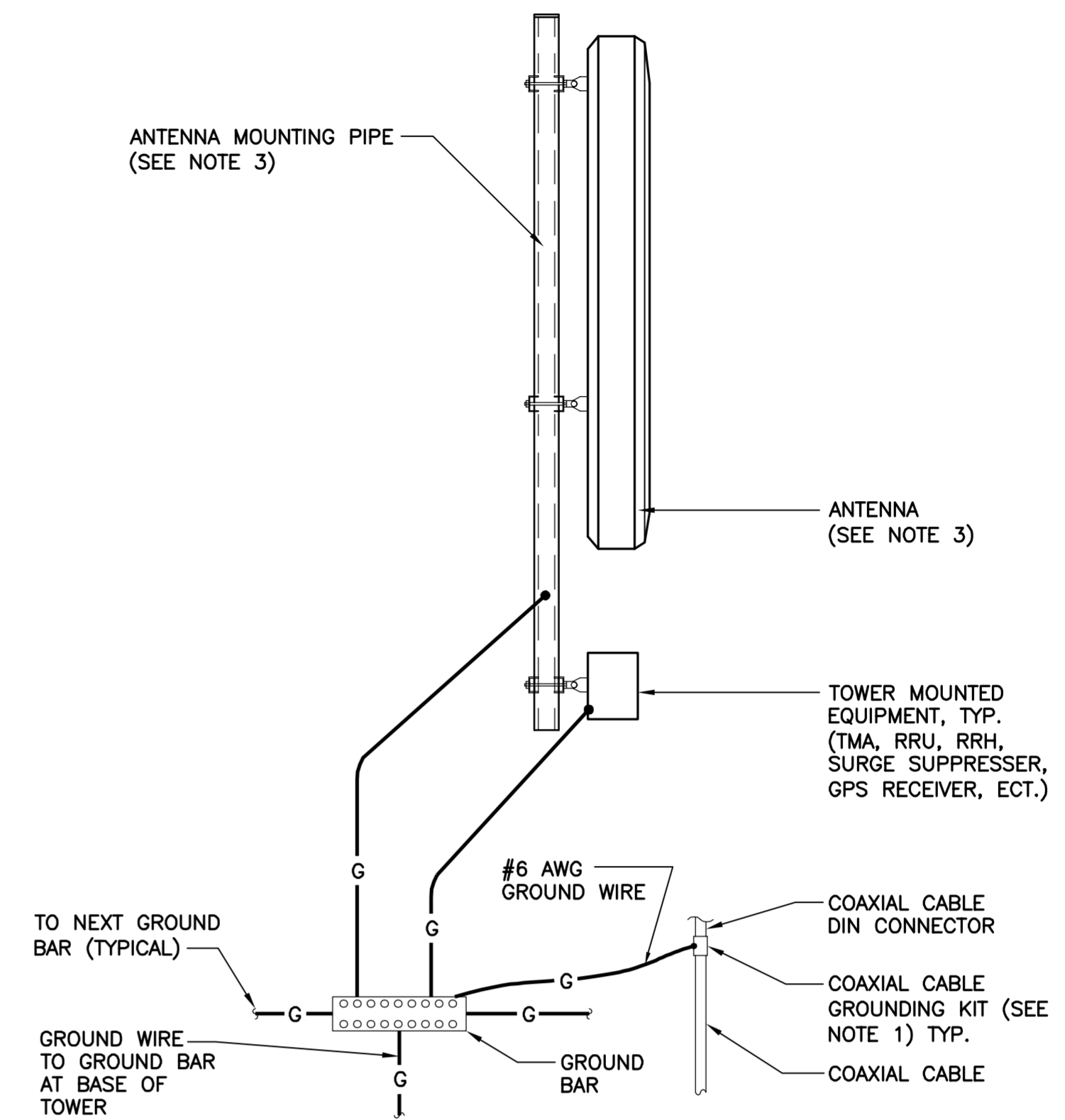
3 GROUND BAR DETAIL
E-3 NOT TO SCALE



NOTES:

1. NUMBER OF GROUND BARS MAY VARY DEPENDING ON THE TYPE OF TOWER, LOCATION AND CONNECTION ORIENTATION. PROVIDE AS REQUIRED.
2. A SEPARATE GROUND BAR TO BE USED FOR GPS ANTENNA IF REQUIRED.

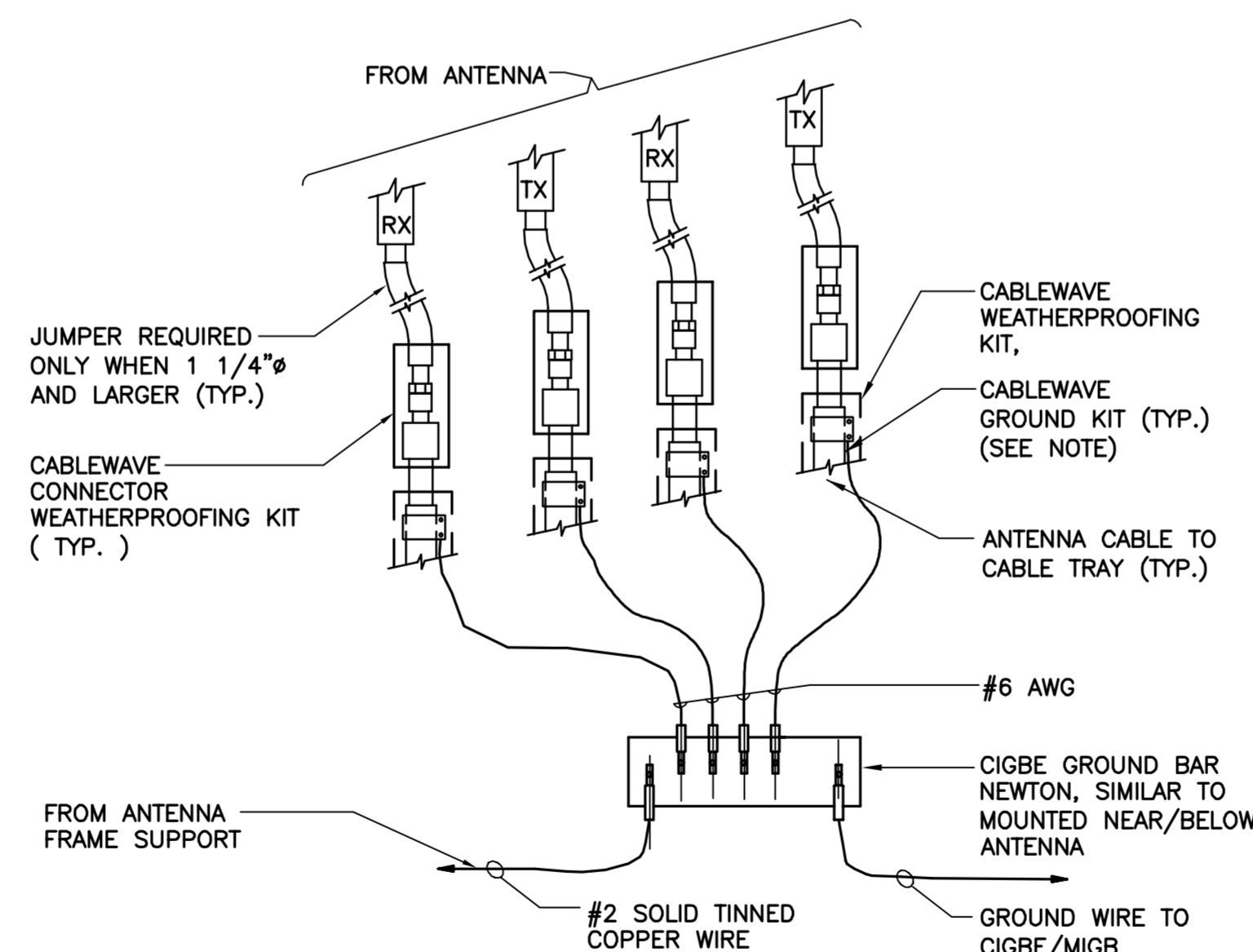
2 ANTENNA CABLE GROUNDING - TOWER
E-3 NOT TO SCALE



NOTES:

1. BOND COAXIAL CABLE GROUND KITS TO EACH OWNER'S GROUND BAR ALONG ENTIRE COAX RUN FROM ANTENNA TO SHELTER.
2. BOND ALL EQUIPMENT TO GROUND PER NEC AND MANUFACTURERS SPECIFICATIONS.
3. DETAIL IS TYPICAL FOR ALL ANTENNA SECTORS, INCLUDING GPS ANTENNA.

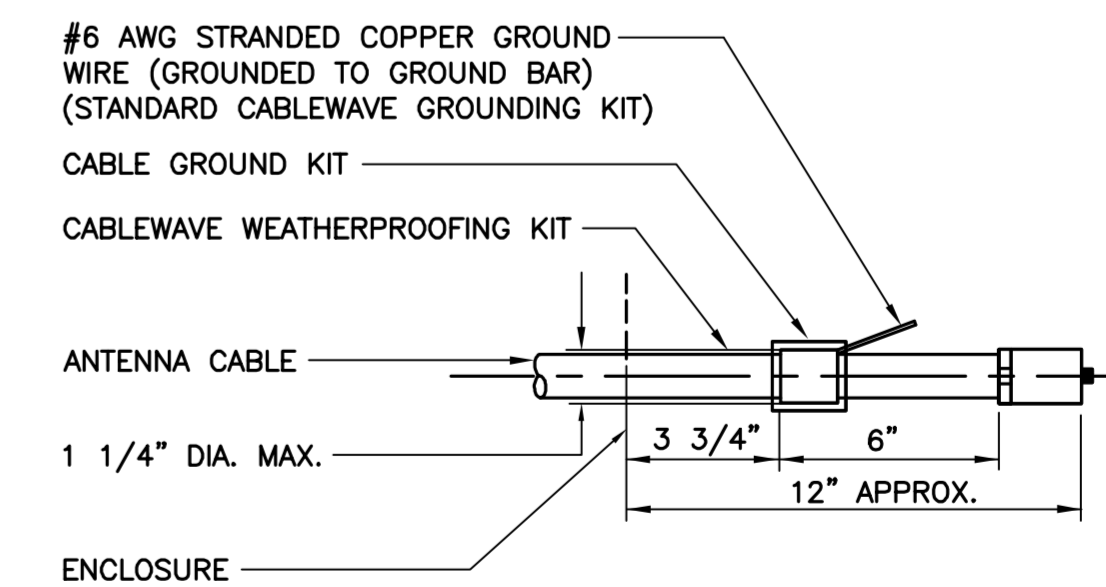
1 TYPICAL ANTENNA GROUNDING DETAIL
E-3 NOT TO SCALE



NOTE:

1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE

5 CONNECTION OF GROUND WIRES TO GROUND BAR
E-3 NOT TO SCALE

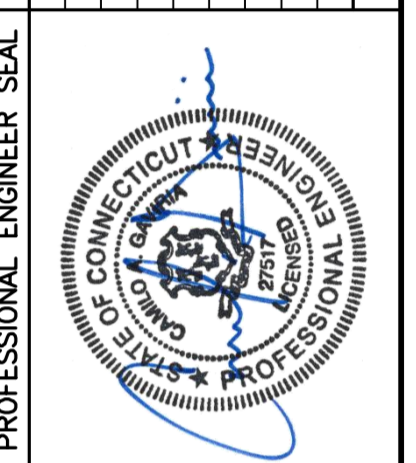


NOTE:

1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO GROUND BAR.

4 ANTENNA CABLE GROUNDING DETAIL
E-3 NOT TO SCALE

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TYPICAL ELECTRICAL DETAILS
E-3
Sheet No. 8 of 8