

Office of Education and Data Management

Spring 2018
Career Development

**May 2018** 

Demystifying the Structural Requirements of the International Residential Code and Roofing

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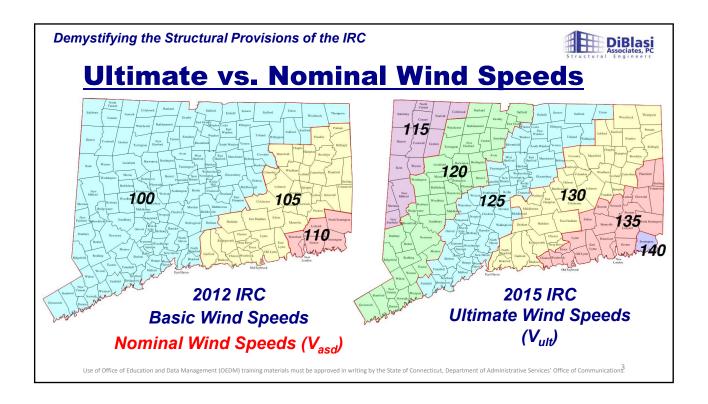
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# **Topics of Discussion**

- · Ultimate vs. Nominal Wind Speeds
- Windborne Debris Regions
- Wind Exposure Categories
- Component and Cladding Wind Loads
- Attic Live Loads
- Basement Wall Nomenclature
- · Basement Wall Reinforcing
- Non-Tabulated Loading Conditions for Joists & Rafters
- Hurricane Anchor Requirements
- Tied Rafters with Raised Ceilings
- I-Joists
- Prefabricated Wood Truss Bracing





#### **Ultimate vs. Nominal Wind Speeds**

#### Why the Change?

- · Bring into alignment with IBC
  - · Inconsistencies with recurrence intervals
  - · Ultimate loads were used for seismic design

<u>2012 IRC</u> <u>2015 IRC</u>

LRFD:  $1.2D + f_1L + 1.6W$  LRFD:  $1.2D + f_1L + 1.0W$ 

0.9D + 1.6W 0.9D + 1.0W

ASD: D + 0.75(L + 1.0W) ASD: D + 0.75(L + 0.6W)

0.6D + 1.0W 0.6D + 0.6W



## **Ultimate vs. Nominal Wind Speeds**

#### What is the impact?

	IRC	2015	IRC 2012
Location	$V_{ult}$	V asd	V
Stonington	140	108	105
New Haven	125	97	100
Greenwich	120	93	100
Salisbury	115	89	90
Enfield	125	97	100
Thompson	130	101	100

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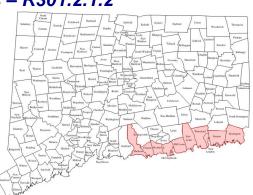
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# **Windborne Debris Regions**

- Per CT Supplement: Limited to areas south of I-95 from Madison to Stonington
- Protection of Openings R301.2.1.2

> Areas more than one mile from coastal mean highwater line as certified by a Registered Design Professional are exempt.





# **Windborne Debris Regions**

- Protection of Openings R301.2.1.2
  - Glazed Openings: Must meet requirements of Large Missile Test of ASTM E 1996 and ASTM E1886
  - Glazing in garage doors must meet approved impact-resisting standard or ANSI/DASMA 115.
  - In lieu of impact-rated glazing, wood structural panels may be used for opening protection.
    - · Panels must be pre-cut
    - · Panels must be pre-drilled
    - Anchors must be corrosionresistant
    - Anchors must be permanently attached to building
    - For h ≤ 45', fastening per Table R301.2.1.2 is permissible

TABLE R301.2.1.2
WINDBORNE DEBRIS PROTECTION FASTENING
SCHEDULE FOR WOOD STRUCTURAL PANELS<sup>A, 5, c, d</sup>

	FASTENER SPACING (inches) <sup>1, b</sup>							
FASTENER TYPE	Panel span ≤ 4 feet	4 feet < panel span ≤ 6 feet	6 feet < panel span ≤ 8 feet					
No. 8 wood screw based anchor with 2-inch embedment length	16	10	8					
No. 10 wood screw based anchor with 2-inch embedment length	16	12	9					
1/4-inch lag screw based anchor with 2-inch embedment length	16	16	16					

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# **Wind Exposure Categories**

- Why are they important?
  - Significant impact on wind pressure and suction loads

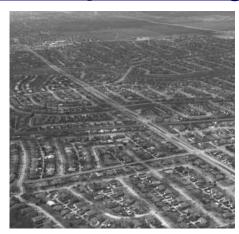
#### Example:

Dwelling with 30' mean roof height

- Exposure Category C loads are 40% higher than Exposure Category B
- Exposure Category D loads are 66% higher than Exposure Category B and 19% higher than Exposure Category C
- Impact wide array of elements including component and cladding loads, braced walls, rafter anchorage, etc.
- Change in IRC definitions for 2018 CSBC
  - Will now align with IBC



#### **Wind Exposure Categories**





Surface Roughness B

Urban and suburban areas, wooded areas and other terrain with numerous closely spaced obstructions having the size of single-family dwellings or larger.

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#### **Wind Exposure Categories**



#### **Surface Roughness C**

Open terrain with scattered obstructions generally less than 30 feet. This category includes flat, open country, and grasslands.



#### **Wind Exposure Categories**



#### Surface Roughness D

Flat, unobstructed areas and water surfaces. This category includes smooth mud flats, slat flats and unbroken ice.

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## **Wind Exposure Categories**

#### Exposure B

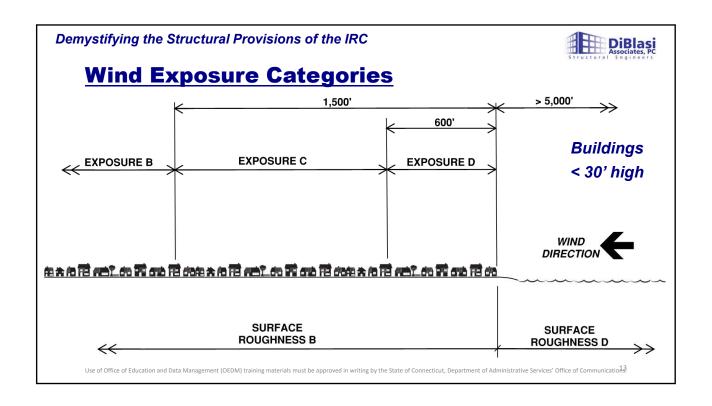
• For buildings with mean roof height up to 30', Surface Roughness B prevails in the upwind direction for a distance of at least 1,500' (2,600' for mean roof height > 30').

#### **Exposure C**

Applies where Exposures B and D do not apply

#### Exposure D

• For buildings where Surface Roughness D prevails in the upwind direction for a distance of at least 5,000'. Also applies upwind of the site a distance of 600' or 20 times the building height from the Exposure D condition.





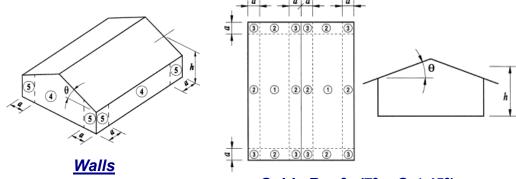
# **Component & Cladding Wind Loads**

- Load Performance Requirements for wall coverings, curtain walls, roof coverings, windows, skylights, doors, garage doors, etc. (§R301.2.1)
- Function of:
  - Wind speed
  - Exposure
  - · Mean roof height
  - · Effective wind area
  - Roof pitch
  - · Location on dwelling



## **Component & Cladding Wind Loads**

Pressure Zone Locations [Figure R301.2(7)]:



Gable Roofs (7° <  $\Theta \le 45$ °)

- Also diagrams for hip roofs and lower pitch gable roofs
- $a = 4^{2}$

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#### **Component & Cladding Wind Loads**

Effective Wind Area:

- The smaller the area, the greater the potential for exposure to a higher, localized wind pressure/suction
- Effective wind area is often but not always the same as tributary area.
- Table R301.2(2) Footnote a

The effective wind area shall be equal to the span length multiplied by an effective width. This width is permitted to be not less than one-third the span length.

- > 3' x 5' window:  $A_{TRIB} = 15$  s.f. =  $A_{EFF}$
- > 3' x 6'-8" door:  $A_{TRIB} = 20 \text{ s.f.} = A_{EFF}$
- > 9' high wall stud spaced @ 16"o.c.:  $A_{TRIB} = 12 \text{ s.f.}$ ;  $A_{EFF} = 9' \times 9'/3 = 27 \text{ s.f.}$
- > Fasteners: effective wind area not greater than area tributary to an indidual fastener (footnote a)



## **Component & Cladding Wind Loads**

- Pressure and suction load tabulations [Table R301.2(2)]
  - 30' High Exposure B

TABLE R301.2(2)
COMPONENT AND CLADDING LOADS FOR A BUILDING WITH A MEAN ROOF HEIGHT OF 30 FEET LOCATED IN EXPOSURE B (ASD) (psf)\*\*.b.c.d.\*

_		EFFECTIVE		ULTIMATE DESIGN WIND SPEED, V <sub>IAT</sub> (mph)												
ı	ZONE	WIND AREA		OLITIMATE DESIGN WIND SPEED, V <sub>ULT</sub> (mpn)												
	ZONE	(feet²)	110		115		120		130		140		150		160	
Г	1	10	10.0	-13.0	10.0	-14.0	10.0	-15.0	10.0	-18.0	10.0	-21.0	9.9	-24.0	11.2	-27.0
ı	1	20	10.0	-12.0	10.0	-13.0	10.0	-15.0	10.0	-17.0	10.0	-20.0	9.2	-23.0	10.6	-26.0
ı	1	50	10.0	-12.0	10.0	-13.0	10.0	-14.0	10.0	-17.0	10.0	-19.0	8.5	-22.0	10.0	-26.0
es	1	100	10.0	-11.0	10.0	-13.0	10.0	-14.0	10.0	-16.0	10.0	-19.0	7.8	-22.0	10.0	-25.0
degrees	2	10	10.0	-21.0	10.0	-23.0	10.0	-26.0	10.0	-30.0	10.0	-35.0	9.9	-40.0	11.2	-46.0
2 de	2	20	10.0	-19.0	10.0	-21.0	10.0	-23.0	10.0	-27.0	10.0	-31.0	9.2	-36.0	10.6	-41.0
9	2	50	10.0	-16.0	10.0	-18.0	10.0	-19.0	10.0	-23.0	10.0	-26.0	8.5	-30.0	10.0	-34.0
Roof 0	2	100	10.0	-14.0	10.0	-15.0	10.0	-16.0	10.0	-19.0	10.0	-22.0	7.8	-26.0	10.0	-30.0
æ	3	10	10.0	-33.0	10.0	-36.0	10.0	-39.0	10.0	-46.0	10.0	-53.0	9.9	-61.0	11.2	-69.0
ı	3	20	10.0	-27.0	10.0	-29.0	10.0	-32.0	10.0	-38.0	10.0	-44.0	9.2	-50.0	10.6	-57.0
	3	50	10.0	-19.0	10.0	-21.0	10.0	-23.0	10.0	-27.0	10.0	-32.0	8.5	-36.0	10.0	-41.0
	3	100	10.0	-14.0	10.0	-15.0	10.0	-16.0	10.0	-19.0	10.0	-22.0	7.8	-26.0	10.0	-30.0

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#### **Component & Cladding Wind Loads**

- Pressure and suction load tabulations [Table R301.2(2)]
  - 30' High Exposure B
  - $V_{ULT} = 130 \text{ mph}$
  - Roof with Slope: 0° to 7°

Effective Wind Area		Zone											
	1		2		3		4		5				
10 s.f.	10.0	-18.0	10.0	-30.0	10.0	-46.0	18.2	-19.0	18.2	-24.0			
20 s.f.	10.0	-17.0	10.0	-27.0	10.0	-38.0	17.4	-19.0	17.4	-22.0			
50 s.f.	10.0	-17.0	10.0	-23.0	10.0	-27.0	16.3	-17.0	16.3	-20.0			
100 s.f.	10.0	-16.0	10.0	-19.0	10.0	-19.0	15.5	-17.0	15.5	-19.0			



#### **Component & Cladding Wind Loads**

 Pressure and suction load adjustment factors for height and exposure [Table R301.2(3)]

MEAN ROOF	EXPOSURE							
HEIGHT	В	С	D					
15	1.00	1.21	1.47					
20	1.00	1.29	1.55					
25	1.00	1.35	1.61					
30	1.00	1.40	1.66					
35	1.05	1.45	1.70					
40	1.09	1.49	1.74					
45	1.12	1.53	1.78					

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# **Component & Cladding Wind Loads**

Example: 8' wide x 7' high garage door in Haddam – 18" high door panels

- Wind speed = 130 mph
- Exposure: C (adjacent to open terrain)
- Mean roof height: 30'
- Pressure Zone Location: 4 (more than 4' from corner)
- Effective Wind Area Panelized Door Spanning Horizontally: Tributary Area of Panel = 1.5' x 8' = 12 s.f. Per footnote 'a', the effective width shall be permitted to be not less than 1/3 the span length. Effective Wind Area = 8' x 8'/3 = 21 s.f.

#### Table R310.2(2):

• For 20 s.f. Effective Wind Area, C&C Pressure = 17.4 psf; C&C Suction = 19.0 psf

#### From Table R301.2(3):

Height and Exposure Adjustment = 1.40

Design Pressure =  $1.40 \times 17.4 \text{ psf}$  = 24.4 psfDesign Suction =  $1.40 \times 19.0 \text{ psf}$  = 26.6 psf





# **Attic Live Loads**

#### **Table R301.5**

- Habitable Attics and Attics with Fixed Stairs: 30 psf
- Uninhabitable Attics with Limited Storage: 20 psf
- Uninhabitable Attics with No Storage: 10 psf (not concurrent with other live loads)

# What differentiates Uninhabitable Attics with Limited Storage from those with No Storage? For Limited Storage:

- 20"x30" access opening at point of minimum 30" clear height required
- Slope of joists or truss bottom chords ≤ 2V:12H
- Required insulation depth < joist or truss bottom chord depth</li>
- · Height/opening limitations

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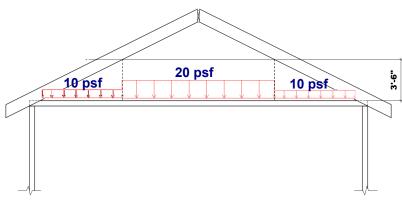
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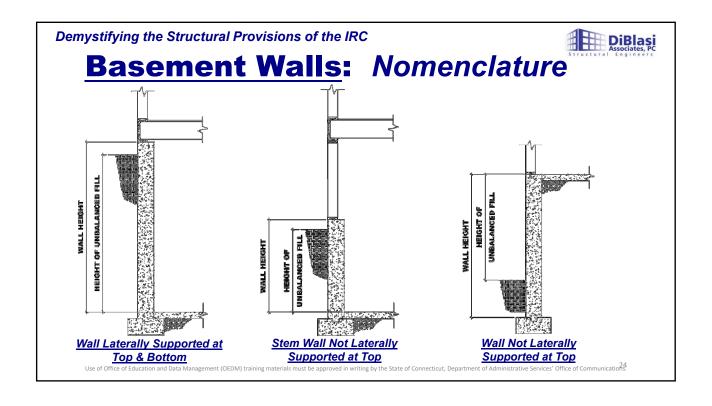
#### **Attic Live Loads**

Limited Storage: Joist Construction

• Clear Height Between Joists and Rafters ≥ 42"



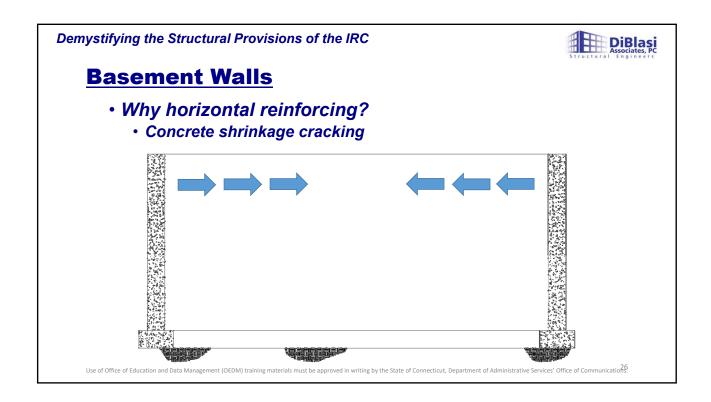
# Demystifying the Structural Provisions of the IRC Attic Live Loads Limited Storage - Truss Construction • Clear Height Between Truss Bottom and Top Chords ≥ 42" • Web Configuration Can Accommodate 42"H x 24"W Rectangle Between 2 or More Trusses

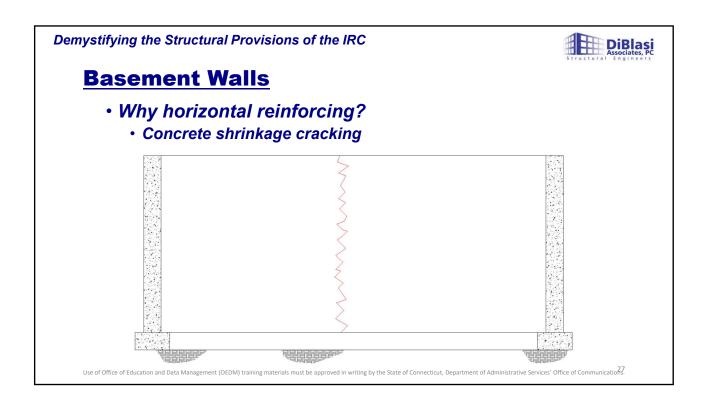


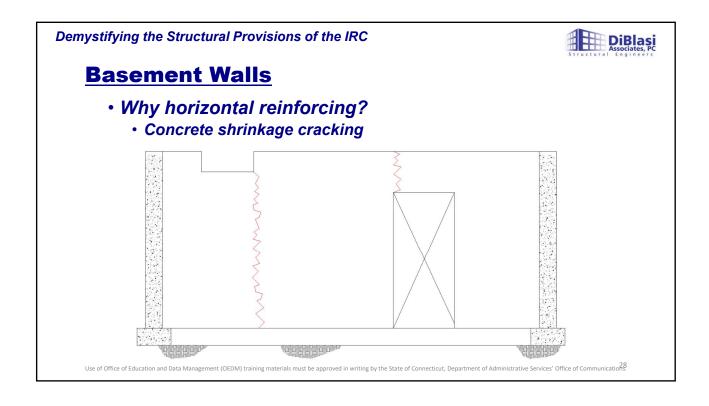


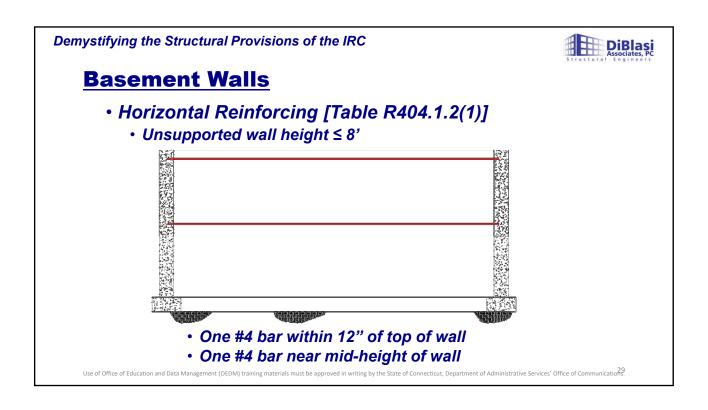
# **Basement Walls**

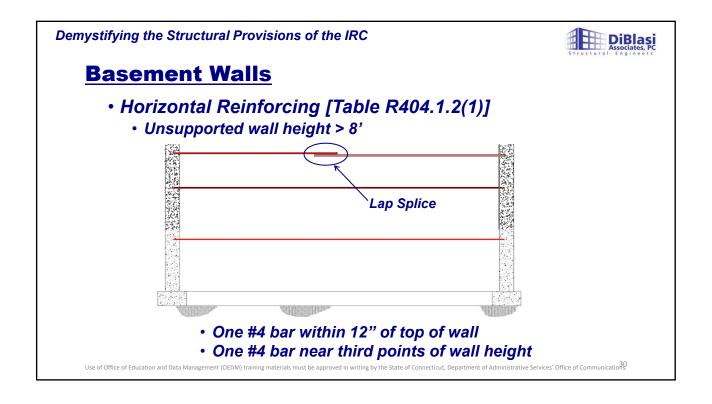
- When is reinforcing required?
  - · Horizontal Reinforcing: Required in all basement walls
  - Vertical Reinforcing: Function of:
    - · Unsupported Wall Height
    - Unbalanced Backfill Height
    - · Soil Type
    - · Wall Thickness

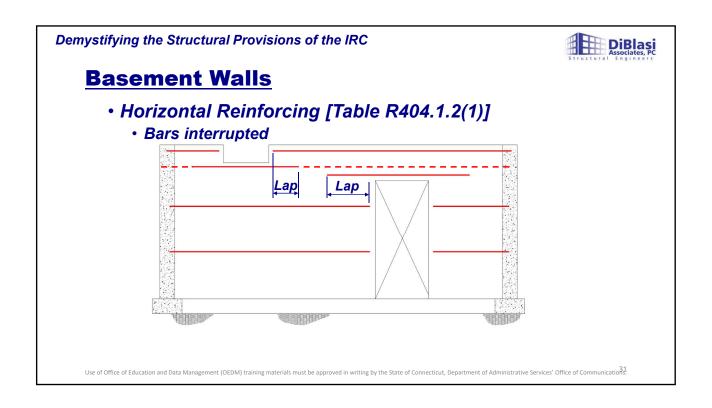


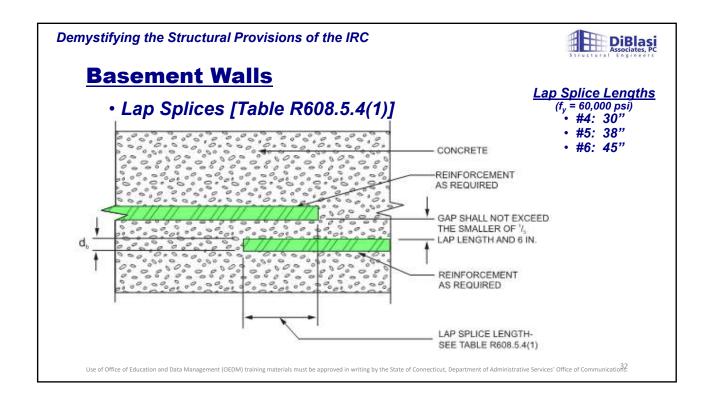














## **Basement Walls**

- · Vertical Reinforcing
  - Soil Types USCS Table R405.1

TABLE R405.1
PROPERTIES OF SOILS CLASSIFIED ACCORDING TO THE UNIFIED SOIL CLASSIFICATION SYSTEM

SOIL GROUP	UNIFIED SOIL CLASSIFICATION SYSTEM SYMBOL	SOIL DESCRIPTION	DRAINAGE CHARACTERISTICS <sup>a</sup>	FROST HEAVE POTENTIAL	VOLUME CHANGE POTENTIAL EXPANSION <sup>b</sup>
	GW	Well-graded gravels, gravel sand mixtures, little or no fines	Good	Low	Low
Group I	GP	Poorly graded gravels or gravel sand mixtures, little or no fines	Good	Low	Low
	SW	Well-graded sands, gravelly sands, little or no fines	Good	Low	Low
	SP	Poorly graded sands or gravelly sands, little or no fines	Good	Low	Low
	GM	Silty gravels, gravel-sand-silt mixtures	Good	Medium	Low
	SM	Silty sand, sand-silt mixtures	Good	Medium	Low
	GC	Clayey gravels, gravel-sand-clay mixtures	Medium	Medium	Low
	SC	Clayey sands, sand-clay mixture	Medium	Medium	Low
Group II	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity	Medium	High	Low
	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	Medium	Medium	Medium to Low

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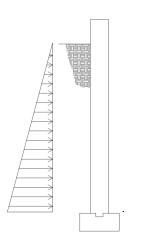
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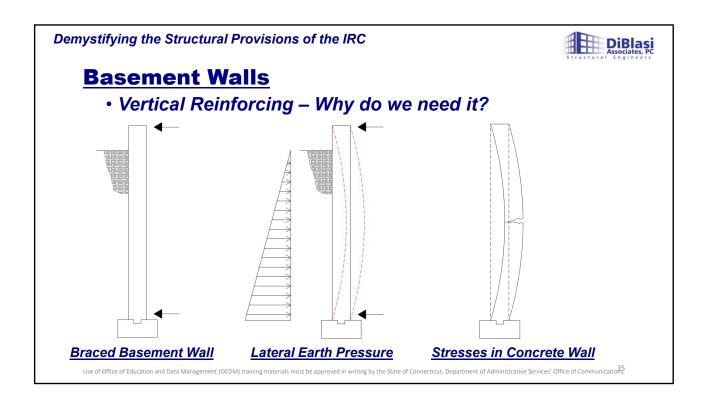


#### **Basement Walls**

- Vertical Reinforcing
  - Soil Types USCS

DESIGN LATERAL SOIL PRESSURES						
BASED ON SOIL CLASS						
Soil Class	Lateral Soil Pressure					
GW, GP, SW, SP	30 psf/foot of depth					
GM, GC, SM SM-SC, ML	45 psf/foot of depth					
SC, ML-CL Inorganic CL	60 psf/foot of depth					







#### **Basement Walls**

· Vertical Reinforcing - Why do we need it?

TABLE R404.1.2(3)
MINIMUM VERTICAL REINFORCEMENT FOR 8-INCH (203 mm) NOMINAL FLAT CONCRETE BASEMENT WALLS<sup>8, c, d, e, l, b, l, l</sup>

		MINIMUM VERTICAL REINFORCEMENT-BAR SIZE AND SPACING (inches)  Soil classes* and design lateral soil (psf per foot of depth)							
MAXIMUM UNSUPPORTED WALL HEIGHT	MAXIMUM UNBALANCED BACKFILL HEIGHT <sup>©</sup>								
(feet)	(feet)	GW, GP, SW, SP 30	GM, GC, SM, SM-SC and ML 45	SC, ML-CL and inorganic CL 60					
	4	NR	NR	NR					
	5	NR	NR	NR					
0	6	NR	NR	6@35					
,	7	NR	6@35	6@32					
	8	6@36	6 @ 32	6@23					
	9	6@35	6@25	6@18					

8" wall - 9' high - 8' unbalanced fill height - 45 pcf soil

• From Table R404.1.2(3), use #6 @ 32"o.c.

Reinforcing Inhibits Cracking

**READ THE FOOTNOTES!!!** 

· Footnote b: vertical bars located at center of the wall



#### **Basement Walls**

- Vertical Reinforcing
  - Flat Basement Walls 6" to 12" Thick
    - Tables R404.1.2(2) to R404.1.2(5) Bars in center of wall (per footnote b): #6 @ 32" required per previous example

				MINIM	NUM VERT	ICAL REIN	FORCEME	NT-BAR SI	ZE AND S	PACING (ir	nches)				
MAXIMUM	MAXIMUM		Soil classes* and design lateral soil (psf per foot of depth)												
WALL HEIGHT	UNBALANCED BACKFILL HEIGHT <sup>9</sup>		GW, GP			GM, GC, SM, SM-SC and ML 45				SC, ML-CL and inorganic CL 60					
(feet)	(feet)	Minimum nominal wall thickness (inches)													
		6	8	10	12	6	8	10	12	6	8	10	12		
	4	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR		
	5	NR	NR	NR	NR	4@35	NR1	NR	NR	5@40	NR	NR	NR		
o	6	4@34	NRI	NR	NR	6@48	NR	NR	NR	6@36	6@39	NR1	NR		
,	7	5@36	NR	NR	NR	6@34	5@37	NR	NR	6@33	6@38	5@37	NR		
	8	6@38	5@41	NR <sup>1</sup>	NR	6@33	6@38	5 @ 37	NR <sup>1</sup>	6@24	6@29	6@39	4@48"		
	9	6@34	6@46	NR	NR	6@26	6@30	6@41	NR	6@19	6@23	6@30	6@39		

• Table R404.1.2(8) – Bars located 11/4" clear from inside face of wall (per footnote h): #6 @ 38"o.c. required for same wall

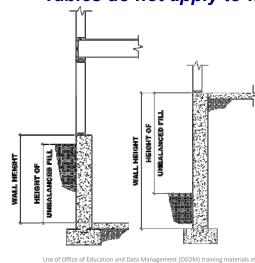
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#### **Basement Walls**

• Tables do not apply to walls not laterally supported at top!



- §R404.1.1: Design in accordance with accepted engineering practice is required for walls supporting more than 48" of unbalanced backfill that do not have permanent lateral support at the top or bottom.
- §R404.1.3.2.2: Stem walls not laterally supported at top with more than 48" of unbalanced fill references to §R404.1.1\* above and §R404.4 (retaining walls; design in accordance with accepted engineering practice)



# **Joist and Rafter Spans**

- Floor Joist Span Tables R502.3.1(1) to R502.3.1(2)
- Ceiling Joist Span Tables R802.4(1) to R802.4(2)
- Rafter Span Tables R802.5.1(1) to R802.5.1(8)

#### Variety of:

- >Lumber Species
- >Lumber Grades
- **➢ Joist/Rafter Spacings**
- **▶Dead Loads**
- >Live/Snow Loads
- > Deflection Criteria



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## **Joist and Rafter Spans**

- How to deal with non-tabulated loading conditions
  - · For Rafters with Ground Snow Loads Between 30-50 psf:
  - ➤ Use linear interpolation in the span charts (permitted by R802.5 2018 CT Amendments
  - ➤ Use AWC STJR, "Span Tables for Joists and Rafters," as permitted by R802.5

(http://awc.org/codes-standards/publications/stjr-2015)

- ➤ Use rafter span handout from OSBI (limited to No. 2 DF, HF, SoP, SPF 35 & 40 psf snow)
- ➤ Use AWC Maximum Span Calculator for Wood Joists & Rafters

(http://awc.org/codes-standards/calculators-software/spancalc)





## **Joist and Rafter Spans**

- · How to deal with non-tabulated loading conditions
  - For Floor Joists with Higher Live Loads or Different Dead Loads:
    - ➤ Use AWC STJR as permitted by R502.3
    - ➤ Use AWC Maximum Span Calculator for Wood Joists & Rafters

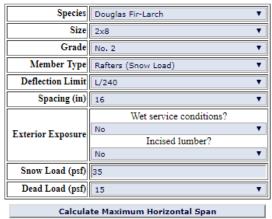
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## **Joist and Rafter Spans**

- How to deal with non-tabulated loading conditions
  - AWC Maximum Span Calculator Example:



The Maximum Horizontal Span is:

#### 13 ft. 8 in.

with a minimum bearing length of **0.49 in.** required at each end of the member.

Property	Value
Species	Douglas Fir-Larch
Grade	No. 2
Size	2x8
Modulus of Elasticity (E)	1600000 psi
Bending Strength (F <sub>b</sub> )	1428.3 psi
Bearing Strength (F <sub>cp</sub> )	625 psi
Shear Strength (F <sub>V</sub> )	207 psi



# **Roof Tie-Down Anchorage**

- · When are tie-down anchors necessary?
  - §R802.11: Fastening per Table R602.3(1) (toe nails) is permitted when uplift force is less than 200 pounds

RAFTER OR TRUSS UPLIFT CONNECTION FORCES FROM WIND (POUNDS PER CONNECTION)<sup>a, b, c, d, e, f, g, h</sup>

Table R802.11

Uplift Connx. Forces

						EXPO:	SURE C				
RAFTER	ROOF				Ultima	te Design Wi	nd Speed $V_{oc}$	<sub>7</sub> (mph)			
OR TRUSS SPACING	SPAN	1	10	1	15	1	20	1:	30	1	40
	(feet)	Roof Pitch		Roof Pitch		Roof	Roof Pitch		Roof Pitch		Roof Pitch
		< 5:12	≥ 5:12	< 5:12	≥ 5:12	< 5:12	≥ 5:12	< 5:12	≥ 5:12	< 5:12	≥ 5:12
	12	126	117	146	136	168	157	214	201	263	247
	18	161	148	188	174	217	201	277	259	342	322
	24	197	181	230	213	266	246	340	318	422	396
16" o.c.	28	221	202	259	238	299	277	384	358	476	446
10 0.0.	32	245	223	287	265	331	307	427	398	529	496
	36	269	246	315	291	364	338	469	438	583	547
	42	305	279	358	330	415	384	535	499	664	622
	48	340	311	402	370	464	430	599	559	745	697

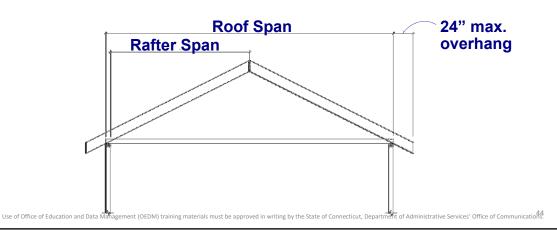
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#### **Roof Tie-Down Anchorage**

- · When are tie-down anchors necessary?
  - Note: Table is based on Roof Span, not Rafter Span!





#### **Roof Tie-Down Anchorage**

- Table R802.11 Read the Footnotes!!!
  - Tables are based on Exposures B & C. For Exposure D, use next highest tabulated value in Exposure C (e.g. for 130 mph **Exposure D, use values from 140 mph Exposure C)**
  - Table not valid for roof overhangs greater than 24"
  - Table not valid for mean roof height > 33'
  - · For connections more than 8' from building corners, uplift forces can be reduced by multiplying by 0.75
  - For connections at hip roofs with pitch ≥ 5:12, uplift forces can be reduced by multiplying by 0.70

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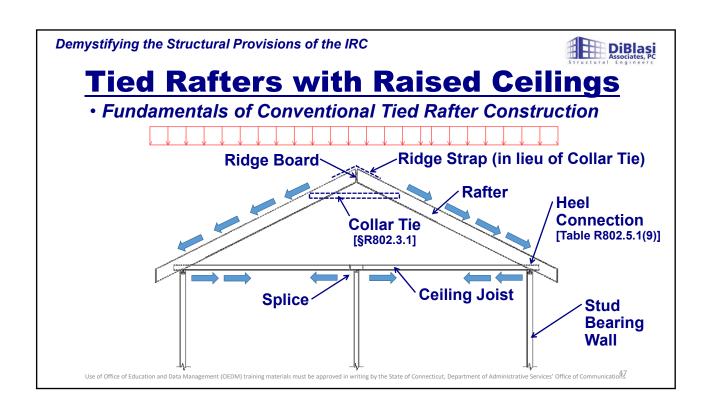


#### **Roof Tie-Down Anchorage**

- Example
  - Given: Trusses/Rafters spaced @ 24"o.c.; overhang ≤ 24"
  - Find: The allowable roof span for which standard toe-nailed connections are permissible?

Wind Spood	Roof Pitch	Allo	owable Roof S	pan
Wind Speed	ROOT PILCH	Exposure B	Exposure C	Exposure D
115 mmh	< 5:12	28'-5"	*	*
115 mph	≥ 5:12	33'-4"	*	*
120 mmh	< 5:12	21'-5"	*	*
120 mph	≥ 5:12	24'-9"	*	*
125 mmh	< 5:12	17'-3"	*	*
125 mph	≥ 5:12	19'-10"	*	*
120 mmh	< 5:12	13'-2"	*	*
130 mph	≥ 5:12	15'-0"	*	*
125 mmh	< 5:12	*	*	*
135 mph	≥ 5:12	*	*	*
140 mph	< 5:12	*	*	*
140 mpn	≥ 5:12	*	*	*

\*Uplift load exceeds 200# on minimum tabulate span of 12'-0".







#### **Tied Rafters with Raised Ceilings**

• Heel connection requirements – Table R802.5.1(9)

TABLE R802.5.1(9)	
RAFTER/CEILING JOIST HEEL JOINT CONNECTIONS <sup>8, 6, 6, 6</sup>	, e, f, h

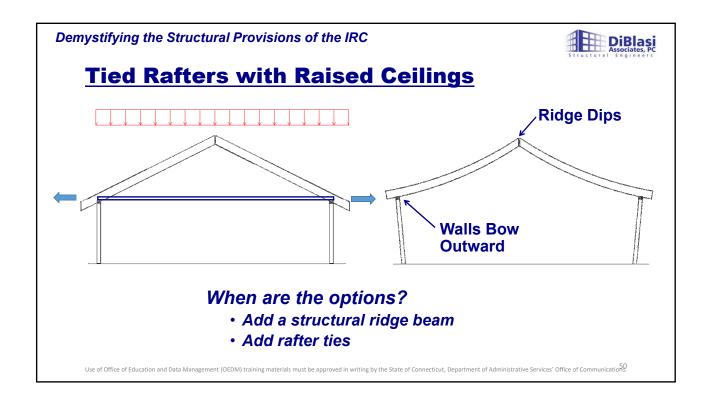
		GROUND SNOW LOAD (psf)															
			2	0 <sub>3</sub>			3	10			5	0			7	0	
	RAFTER	Roof span (feet)															
SLOPE	SPACING (inches)	12	20	28	36	12	20	28	36	12	20	28	36	12	20	28	36
		Required number of 16d common nails <sup>a, b</sup> per heel joint splices <sup>c, d, a, r</sup>															
	12	4	6	8	10	4	6	8	11	5	8	12	15	6	11	15	20
3:12	16	5	8	10	13	5	8	11	14	6	11	15	20	8	14	20	26
	24	7	11	15	19	7	11	16	21	9	16	23	30	12	21	30	39
	12	3	5	6	8	3	5	6	8	4	6	9	11	5	8	12	15
4:12	16	4	6	8	10	4	6	8	11	5	8	12	15	6	11	15	20
	24	5	8	12	15	5	9	12	16	7	12	17	22	9	16	23	29
	12	3	4	5	6	3	4	5	7	3	5	7	9	4	7	9	12
5:12	16	3	5	6	8	3	5	7	9	4	7	9	12	5	9	12	16
	24	4	7	9	12	4	7	10	13	6	10	14	18	7	13	18	23
	12	3	4	4	5	3	3	4	5	3	4	5	7	3	5	7	9
7:12	16	3	4	5	6	3	4	5	6	3	5	7	9	4	6	9	11
	24	3	5	7	9	3	5	7	9	4	7	10	13	5	9	13	17



## **Tied Rafters with Raised Ceilings**

- Heel connection requirements Table R802.5.1(9)
  - 30 psf Ground Snow Load
  - 28' Roof Span
  - 24" Rafter Spacing

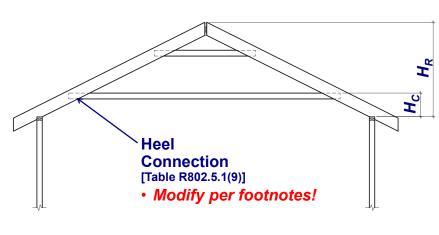
Rafter Slope	16d Nails Required
3:12	16
4:12	12
5:12	10
7:12	7
9:12	6
12:12	4





## **Tied Rafters with Raised Ceilings**

• Rafter span reductions – Tables R802.5.1(1) to (8)



H <sub>c</sub> /H <sub>R</sub>	Rafter Span Adjustment Factor					
''C'''R	IRC 2012 IRC 2015	IRC 2003				
2/3 or greater	Not Allowed	0.50				
1/2	Not Allowed	0.58				
1/3	0.67	0.67				
1/4	0.76	0.76				
1/5	0.83	0.83				
1/6	0.90	0.90				
1/7.5 and less	1.00	1.00				
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#### **Tied Rafters with Raised Ceilings**

• Rafter/Ceiling Joist Heel Connections - Table R802.5.1(9)

#### **Footnotes**

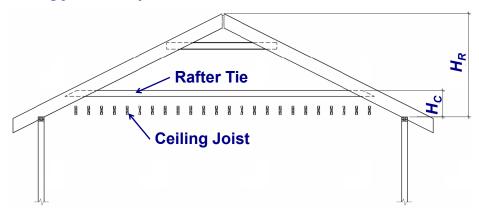
- f. Where rafter ties are subjected for ceiling joists, the heel joint requirements shall be taken see the latter ties are subjected for ceiling joists, the heel joint connection repair to two-thirds of the actual rafter slope.
- h. Tabulated heel joint connections assume that ceiling joists or rafter ties are located at the bottom of the attic space. Where ceiling joists or rafter ties are located higher in the attic, heel joint connection requirements shall be increased by the following factors.

H <sub>c</sub> /H <sub>R</sub>	Heel Joist Connection Adjustment Factor
1/3	1.5
1/4	1.33
1/5	1.25
1/6	1.2
1/10 or less	1.11



#### **Tied Rafters with Raised Ceilings**

- Rafter span reductions Tables R802.5.1(1) to (8)
  - · Ceiling joists not parallel to rafters



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#### **Tied Rafters with Raised Ceilings**

#### Given:

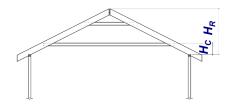
- Gable Roof
- · 28' roof span w/ 2' overhang
- 7:12 pitch
- No. 2 S-P-F
- · 8' Plate Height
- 9'-9" Ceiling Height
- 2x6 Stud Walls
- 130 mph Wind Zone Exp. B
- 30 psf Ground Snow Load (Ceiling Attached to Rafters)
- · Uninhabitable Attic with No Storage
- 10 psf Roof Dead Load
- 2"x10 @ 16"o.c. Rafters
- 2"x6" @ 16" Ceiling Joists

- 1. Are rafters adequate? Find: 2. Are ceiling joists adequate?

  - 3. What is the required connection between the ceiling joists and rafters?
  - 4. Are hurricane ties required between the rafter and stud wall?



#### **Tied Rafters with Raised Ceilings**



#### **Basic Geometry**

- Roof Span = 28'
- Rafter Span = 28'/2 6" (wall) = 13'-6"
- $H_C \approx 9'-9''$  (clg. ht.) 8'-0" (plate ht.) + 6" (clg. joist depth) = 2'-3"
- $H_R \approx 28^{\circ}/2 \times 7/12$  (pitch) + 8" (rafter ht. above plate at outside of wall) = 8'-10"
- $H_C/H_R = 2.25^{\circ}/8.83^{\circ} = 0.254 \approx \frac{1}{4}$
- Ceiling Joist Span = [13'-6" (1'-9" x 12/7)] x 2 = 21'-0"

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#### **Tied Rafters with Raised Ceilings**

#### 1. Are Rafters Adequate?

- Table R802.5.1(5): Allowable span for 2"x10" @ 16"o.c. rafters (No. 2 S-P-F) with 30 psf snow load, 10 psf dead load and attached ceiling = 18'-5".
- From footnote "a", Rafter Span Adjustment Factor for  $H_C/H_R$  of  $\frac{1}{4}$  = 0.76.
- Modified Allowable Rafter Span = 0.76 x 18'-5" = 14'-0" > 13'-6" actual rafter span ➤ Rafters are O.K.

#### 2. Are Ceiling Joists Adequate?

- Table R802.4(1): Allowable span for 2"x6" @ 16"o.c. ceiling joists (No. 2 S-P-F) with 10 psf live load (no storage) = 16'-11" < 21'-0" actual ceiling joist span.
  - > 2"x6" ceiling joists are N.G.
  - ➤ Use 2"x8" ceiling joists instead allowable span = 22'-4"



#### **Tied Rafters with Raised Ceilings**

- 3. What is the Required Connection Between the Ceiling Joists and the Rafters?
  - Table R802.5.1(9): For a roof span of 28', ground snow load of 30 psf, rafter slope of 7:12 and rafter spacing of 16"o.c., five (5) 16d nails are required at the rafter/ceiling heel joint connection.
  - From footnote "h", a Heel Joint Connection Adjustment Factor is to be applied when the ceiling joists are located above the wall plate. For  $H_C/H_R = 1/4$ , this adjustment factor is 1.33.
  - Number of nails required =  $1.33 \times 5 = 6.7$ 
    - > Use seven (7) 16d nails at the rafter/ceiling heel joint connection

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#### **Tied Rafters with Raised Ceilings**

- 4. Are Hurricane Anchors Required Between the Rafter and Stud Wall?
  - Table R802.11: For a 130 wind speed in Exposure B with rafters spaced @ 16"o.c., a roof span of 28' with a 24" overhang and a 7:12 roof pitch, the rafter uplift connection force = 203#.
    - ➤ As the connection force exceeds 200#, the standard toe-nailed connections in the Fastening Schedule are not permissible and a hurricane anchor (or acceptable alternative connection) would be required.
    - > Per footnote "d", the tabulated connection forces at locations more than 8'-0" from the building corners may be multiplied by 0.70. The design connection force in these areas would be 0.70 x 203# = 142#; toe-nailed connections in accordance with Table R602.3(1) would be permissible in these locations.



# **Special Considerations for I-Joists**

- Benefits
  - Dimensionally stable
  - Longer spans
  - Larger openings



- Challenges
  - More complicated installation
  - Plethora of details to follow
  - Footnotes galore
  - Specific design criteria not contained within IRC



Evaluation Service Reports

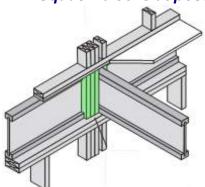
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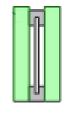
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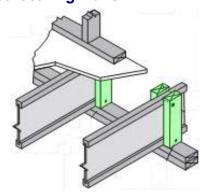


## **Special Considerations for I-Joists**

- Concentrated Loads
  - · Squash blocks at post loads and stacked bearing walls





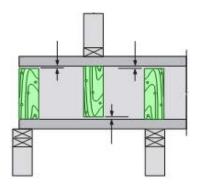


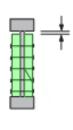
At exterior bearing walls, rim joists can often eliminate need for squash blocks below bearing walls above; squash blocks are generally still required at posts



## **Special Considerations for I-Joists**

- Web stiffeners
  - Sometimes required at points of bearing and when supporting concentrated loads required locations identified on drawings





Stiffener thickness and nailing requirements per manufacturer

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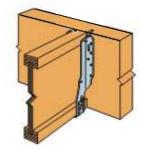


#### **Special Considerations for I-Joists**

- Joist Hangers
  - Hangers must provide lateral restraint of top flange; otherwise web stiffeners required







Hanger Restrains Top Flange



# **Special Considerations for I-Joists**

Joist Hangers



Hanger Does Not Restrain Top Flange

➤ Web Stiffener Required



Hanger Restrains Top Flange

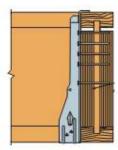
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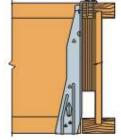


#### **Special Considerations for I-Joists**

- Joist Hangers
  - When I-Joists are used as headers, backer blocks are required at hanger connections.



Backer Blocks on Both Sides at Face-Mount Hangers (to bear flush with bottom flange)

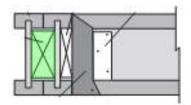


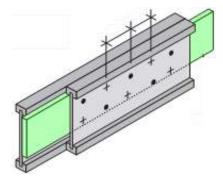
Backer Blocks on Hanger Side at Top-Flange Hangers (to bear flush with top flange)



## **Special Considerations for I-Joists**

- Double I-Joists
  - When double I-Joists are used as headers or to support concentrated loads, they must be interconnected with filler blocks to act as a unit.





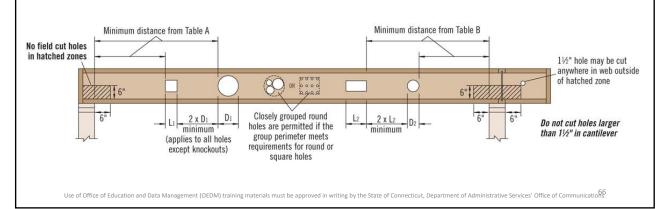
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#### **Special Considerations for I-Joists**

- Joist Penetrations
  - I-Joists can accommodate considerably larger penetrations that than sawn lumber
  - · Read the footnotes!!!





8'-6"

# Special Considerations for I-Joists CLOSEST DISTANCE TO SUPPORT

 Joist Penetrations
 Example Based on LPI 42Plus Joists

Joist **Circular Hole Diameter** 5" 6" Depth 2" 8" 3'-4" 9½" 1'-3" 2'-3" 4'-4" 5'-5" 11%" 3'-2" 3'-10" 4'-7" 5'-3" 6'-0" 6'-9" 7'-8" 5'-7" 14" 4'-5" 6'-1" 7'-3" 8'-0" 5'-0" 6'-8"

#### **CLOSEST DISTANCE TO SUPPORT**

6'-10"

7'-4"

7'-10"

6'-4"

Joist	Rectangular Hole Maximum Dimension								Rectangular Hole Maximum Dimension								
Depth	2"	3"	4"	5"	6"	7"	8"										
9½"	5′-8″	6'-6"	7′-4″	8'-2"	9'-3"	9'-7"	9'-11"										
11%"	7′-2″	8'-0"	9'-0"	10'-0"	10'-11"	12'-1"	13'-8"										
14"	4'-4"	4'-2"	6'-0"	6'-10"	7'-10"	9'-1"	10'-10"										
16"	5′-3″	6'-0"	6'-9"	7′-7″	8'-6"	9'-8"	11'-2"										

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16"

5'-4"

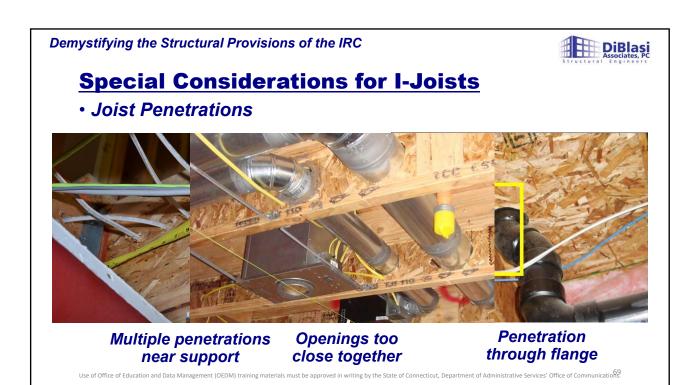
5'-10"

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#### **Special Considerations for I-Joists**

- Joist Penetrations
  - These web hole tables are valid for simple and continuous spans with <u>uniform loads only</u>, as sized from tables contained in LP's current I-Joist product guides. Larger holes and nonuniform loading conditions and/or closer proximity to supports may be possible, <u>but require further analysis</u> using LP's design software.







## **Special Considerations for I-Joists**

• Issues with Other Trades - Ductwork Conflicts







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## **Special Considerations for I-Joists**

• Issues with Other Trades - Ductwork Conflicts





Joists cut – increases load on adjacent joists



## **Metal-Plate-Connected Wood Trusses**

• Permanent Bracing Requirements

R802.10.3 Bracing. Trusses shall be braced to prevent rotation and provide lateral stability in accordance with the requirements specified in the construction documents and on the individual truss design drawings. In the absence of specific bracing requirements, trusses shall be braced in accordance with accepted industry practices, such as, the SCBA "Building Component Safety Information (BCSI) Guide to Good Practice for Handling, Installing & Bracing of Metal-Plate-Connected Wood Trusses."



www.sbcindustry.com

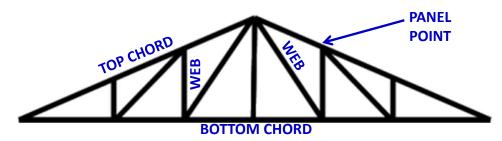
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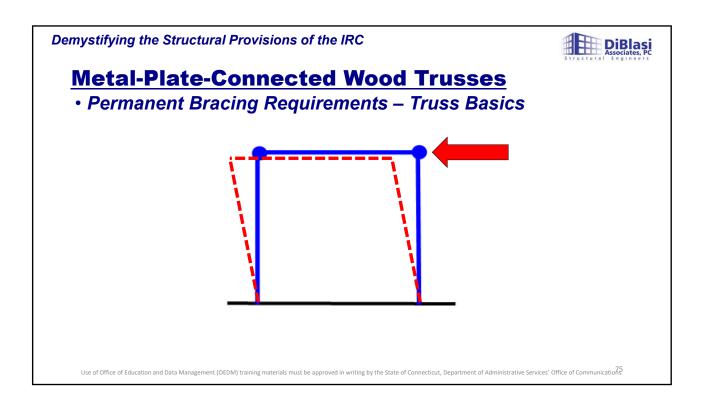
#### **Metal-Plate-Connected Wood Trusses**

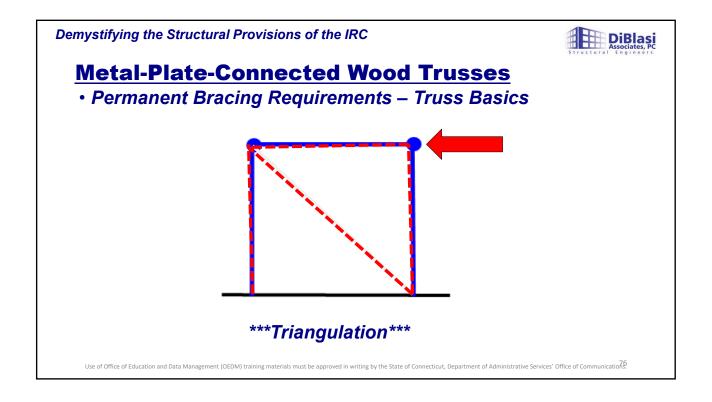
• Permanent Bracing Requirements – Truss Basics



- Primary stresses in truss members:
  - ➤ Top Chord: compression ➤ Bottom Chord: tension
  - > Webs: some compression, some tension
- Permanent bracing inhibits buckling of compression members

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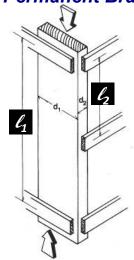






#### **Metal-Plate-Connected Wood Trusses**

• Permanent Bracing Requirements



Slenderness Ratio l<sub>e</sub>/d

How does the slenderness ratio affect the allowable compression strength?

• 2"x4" - No. 1/No. 2 Spruce-Pine-Fir -Snow Load Condition

$\ell_e/d$	P <sub>allow</sub>
10	7,270#
26	2,924#
50	861#

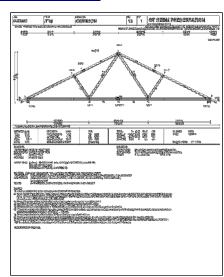
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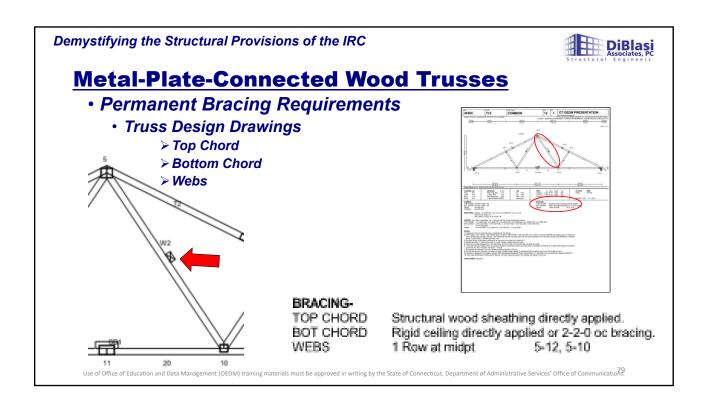
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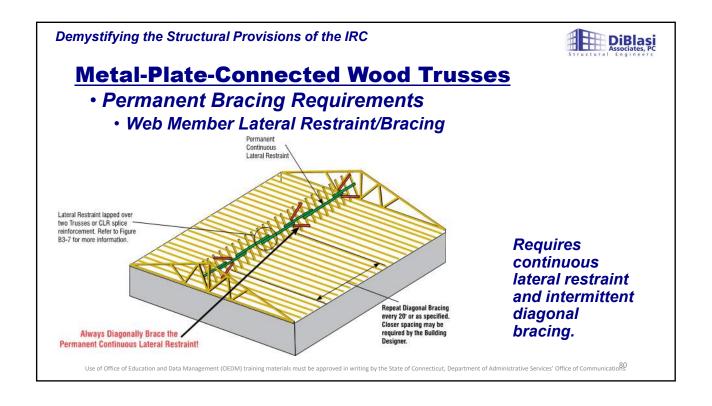


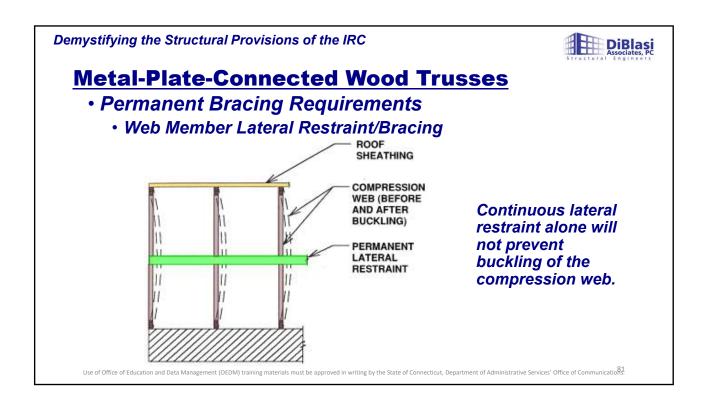
#### **Metal-Plate-Connected Wood Trusses**

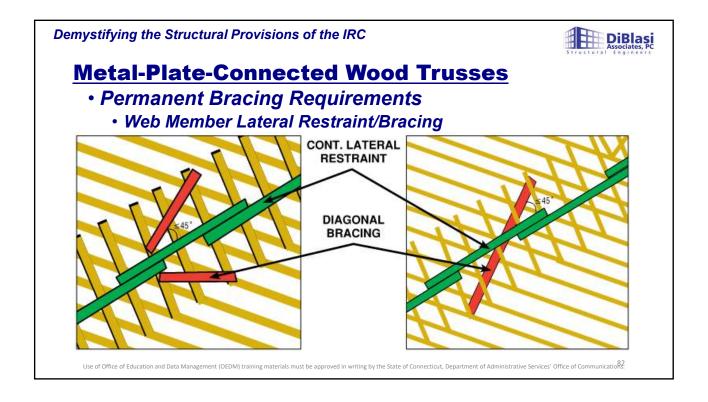
- Permanent Bracing Requirements
  - Truss Design Drawings
    - Truss IDs
    - Geometry
    - · Truss Bearing
    - Lumber
    - Plates
    - Permanent Restraint/Bracing
    - Forces
    - Deflections
    - Design Loads
    - · Design Criteria
    - · Multi-Ply Girder Fastening

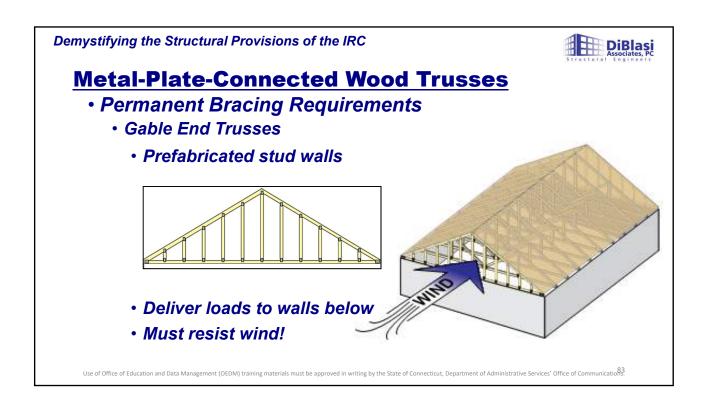


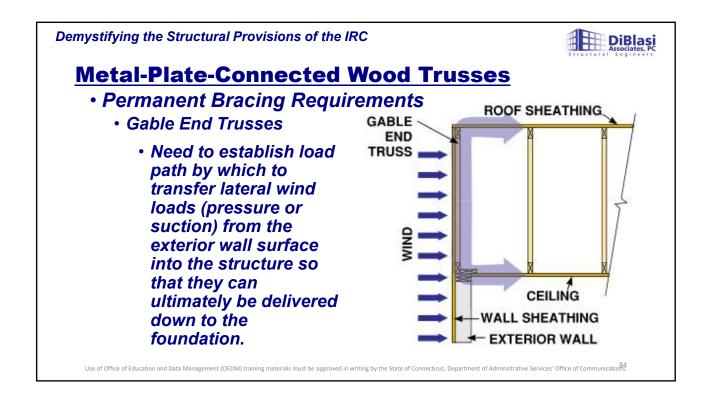


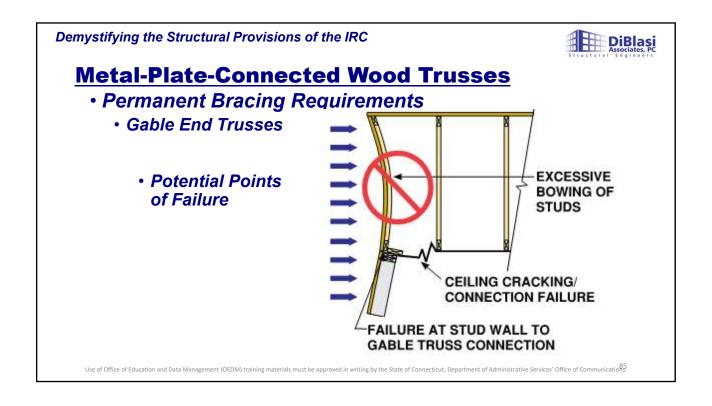










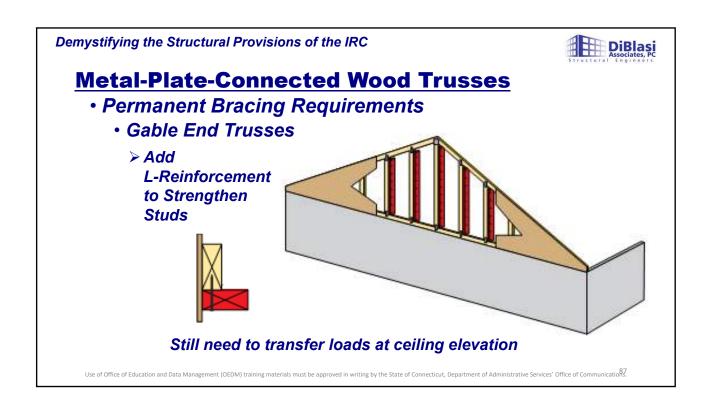


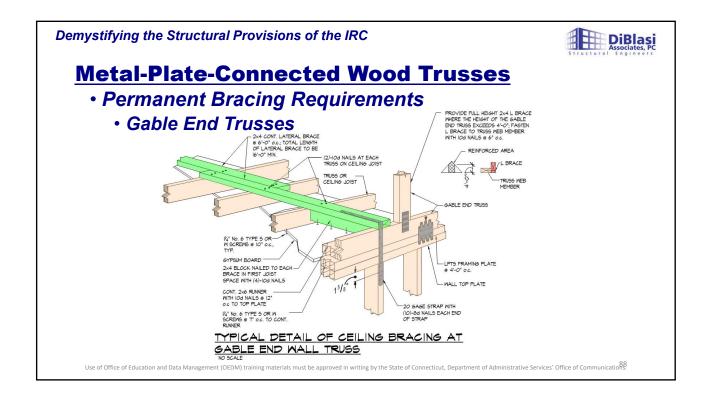


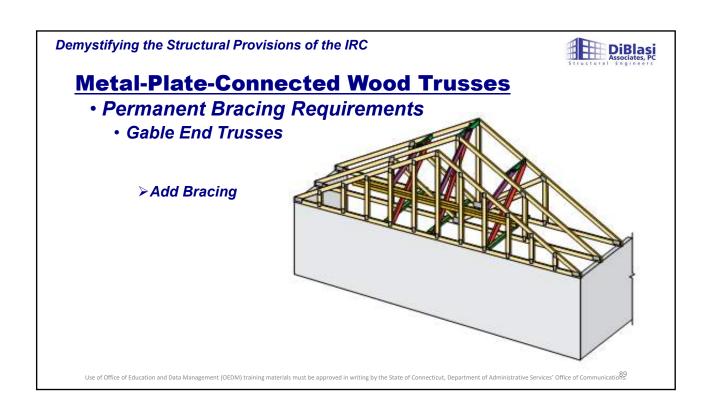
#### **Metal-Plate-Connected Wood Trusses**

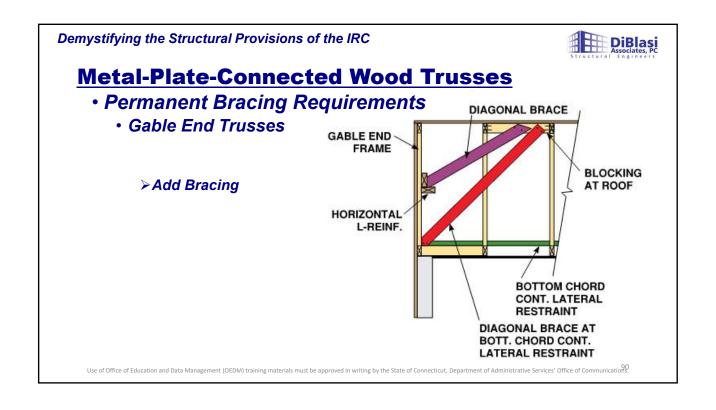
- Permanent Bracing Requirements
  - Gable End Trusses















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