
***Connecticut Cable Resonance Study for
Synchronous Condenser Option 2
(Case 5d) in Middletown to Norwalk
Project***

***Summary Report
August 2004***

**Prepared for:
Northeast Utilities**

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Foreword

This document was prepared by General Electric Company in Schenectady, New York. It is submitted to Northeast Utilities (NU). Technical and commercial questions and any correspondence concerning this document should be referred to:

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Introduction

GE Energy's Energy Consulting group has performed a resonance study of "Synchronous Condenser Option 2" (Case 5d) in the Northeast Utilities (NU) Middletown to Norwalk 345 kV transmission cable project that is proposed in southwestern Connecticut. This option connects a 500 MVA synchronous condenser at East Devon 345 kV through a GSU and another 500 MVA synchronous condenser at Singer 345 kV. In this study, the two cables between Norwalk and Singer and the two cables between Singer and East Devon were represented as 3000 kcmil XLPE cable rather than 2500 kcmil HPFF cable, and one of the two HPFF cables between Plumtree and Norwalk was removed.

The objectives of this study were

- to investigate the change in the first resonance with the above modifications as compared to the proposed HPFF double circuit configuration and the XLPE alternative, and
- to investigate the effect of representing reduced generation in the area.

The study has been performed with the Electromagnetic Transients Program (ATP/EMTP), which is recognized as an industry standard for simulating the transient performance and frequency response of electric utility systems [www.emtp.org].

System Representation

The system model used in the Middletown to Norwalk study was used in this study with modifications.

Two 500 MVA synchronous condensers were connected through GSUs: one at East Devon 345 kV and another at Singer 345 kV. The synchronous condenser was modeled as a voltage source behind a subtransient reactance X_d'' , assumed to be 25% (on 500 MVA base) which is similar to that of 4-pole turbine-generator units.¹ A 500 MVA GSU transformer with 10% impedance (on 500 MVA base) was assumed.

The charging capacitance of the 3000 kcmil XLPE cables is approximately 60% of that of the 2500 kcmil HPFF cables. The following parameters were used to represent the 3000 kcmil XLPE cables (per circuit in pu on a 100 MVA base):

Singer to Norwalk - 15.5 miles

Rpos=0.0003477 pu
Rzero=0.00358118 pu
Xpos=0.00416198 pu
Xzero=0.0023779 pu
Bposzero=1.9637 pu

East Devon to Singer - 8.1 miles

Rpos=0.0001817 pu

¹ T.J.E. Miller, *Reactive Power Control in Electric Systems*, John Wiley & Sons, Inc., 1982, p. 277.

Rzero=0.0018715 pu
 Xpos=0.00217497 pu
 Xzero=0.0012426 pu
 Bposzero=1.0261907 pu

In addition to the above changes, one of the two 9.7-mile HPFF cable circuits between Plumtree and Norwalk was removed. The overhead line between East Devon and Beseck was the same as in the Middletown to Norwalk project.

NU determined that the two capacitor banks at Norwalk 115 kV would be removed with the addition of the Middletown to Norwalk project, and were removed from the model accordingly. Table 1 shows the modified capacitor bank data for this study, and indicates the total MVAR at each bus and the capacitor bank MVAR in service under peak and light load conditions. This study considered conditions with all capacitor banks in service and all capacitor banks out of service. Table 2 shows the generators included in the original ASPEN file, and the modified status originally provided for the Middletown to Norwalk (M/N) project, which indicates the generators that are on or off during peak and light load conditions. An additional generator dispatch scenario is given for “Light Post-Project,” which depicts a more realistic scenario with more local generation off. This study considered the original light load dispatch of generators and the Light Post-Project dispatch with more local generation off.

Table 1. Modified Shunt Capacitor Conditions for System Model

Shunt Capacitors			All Banks	Peak Load	Light Load
Substation	Voltage (kV)	# Units	MVAR (total)	MVAR	MVAR
Southington 1	115	3	157.2	157.2	
Southington 2	115	3	157.2	157.2	
Frost Bridge	115	5	262.0	262.0	
Berlin	115	3	132.0	132.0	
Plumtree	115	2	92.2	0	
Glenbrook	115	5	190.8*	151.2	
Darien	115	1	39.6	39.6	
Waterside	115	1	39.6	39.6	
Norwalk	115	0	0	0	
East Shore	115	2	84.0	84.0	
No. Haven	115	1	42.0	42.0	
Sackett	115	1	42.0	42.0	
Rocky River	115	1	25.2	25.2	
Stony Hill	115	1	25.2	25.2	
Cross Sound Filters	200	3	103.0 (61 – 25 th , 32 – 41 st , 10 – 21 st)	103.0	103.0

* Actual maximum including Glenbrook Statcom is 335 MVAR (additional MVAR not included in analysis)

Table 2. Modified Generator Conditions for System Model

GENERATOR	KV	ID	ST	STATUS (PEAK)	STATUS (LIGHT)	Light Post-Project	IDENTIFICATION NOTES
MILLSTON	22.8	1	1	on	on	On	
MILLSTON	22.8	1	1	on	on	On	
RESCO	115	1	1	on	on	On	Bridgeport
ROCKY RV	13.8	1	1	on	on	Off	
ROCKY RV	13.8	1	1	on	on	Off	
ROCKY RV	13.8	1	1	on	on	Off	
STEVENSO	6.9	1	1	off	off	Off	
NORWALK	27.6	1	0	off	off	Off	
BULLS BR	27.6	1	1	on	on	Off	
FORESTVI	13.8	1	1	on	on	On	
brdgphbr	18.4	2	1	off	off	Off	
brdgphbr	20.2	3	1	on	on	Off	
brdgphbr	13.68	jt	1	off	off	Off	
COSCOBGE	13.8	1	1	off	off	Off	
COSCOBGE	13.8	2	1	off	off	Off	
COSCOBGE	13.8	3	1	off	off	Off	
DEVON 11	13.8	1	1	off	off	Off	
DEVON 12	13.8	1	1	off	off	Off	
DEVON 13	13.8	1	1	off	off	Off	
DEVON 14	13.8	1	1	off	off	Off	
English	13.68	8	1	off	off	Off	
English	13.68	7	1	off	off	Off	
ESHOREGE	13.8	1	1	on	on	Off	New Haven
G1/G2	13.8	1	1	off	off	Off	Wallingford
G3/G4	13.8	1	1	off	off	Off	Wallingford
G5	13.8	1	1	off	off	Off	Wallingford
GT1 (11)	16	1	1	off	off	Off	BE
GT2 (12)	16	1	1	off	off	Off	BE
Middleto	22	1	1	on	off	Off	Middletown
Milford	20.9	1	1	on	on	Off	
Milford	20.9	1	1	off	off	Off	
one (Meriden)	21	1	1	on	off	Off	Meriden
Shepaug	13.8	1	1	on	on	Off	
so norwa	4.8	1	1	off	off	Off	
so norwa	4.8	1	1	off	off	Off	
so norwa	13.8	1	1	off	off	Off	
ST1 (10)	16	1	1	off	off	Off	BE
Temp Gen (Waterside)	13.8	3	0	off	off	Off	Waterside
Temp Gen (Waterside)	13.8	1	0	off	off	Off	Waterside
Temp Gen (Waterside)	13.8	2	0	off	off	Off	Waterside
three (Meriden)	21	1	1	on	off	Off	Meriden

GENERATOR	KV	ID	ST	STATUS (PEAK)	STATUS (LIGHT)	Light Post-Project	IDENTIFICATION NOTES
two (Meriden)	21	1	1	on	off	Off	Meriden
Unit 10	13.8	1	1	off	off	Off	Devon 10
Unit 6J- (Norwalk)	17.1	1	1	off	off	Off	Norwalk-1
Unit 6J- (Norwalk)	13.8	1	1	off	off	Off	Norwalk -10
Unit 6J- (Norwalk)	19	1	1	off	on	Off	Norwalk-2
Unit 7	13.2	1	1	on	off	Off	Devon
Unit 8	13.2	1	1	on	off	Off	Devon
walrecge	4.16	1	1	on	off	Off	

Resonance Results

The resonance effects of Synchronous Condenser Option 2 (Case 5d), including XLPE cables from East Devon to Singer and Singer to Norwalk and removal of one HPFF cable between Plumtree and Norwalk, was analyzed by evaluating the driving-point impedance versus frequency at various locations, with all capacitor banks in and out of service, and with the original light load and light post-project generator (local generation off) dispatches.

Table 3 shows the cases that were performed for Synchronous Condenser Option 2 and the resonant frequencies that were observed along with the corresponding impedance value at those frequencies, with the original light load generation dispatch. The resonant frequency is indicated by its harmonic number (HN), in per unit of 60 Hz, and impedance magnitude is in ohms. The corresponding driving-point impedance plots are provided in Appendix A. Table 4 shows the results with the local generation off (light post-project generator dispatch), and the corresponding driving-point impedance plots are provided in Appendix B.

Table 3. Resonant Frequencies for M/N-XLPE Project with Light Load Generation
A 500 MVA Synchronous Condenser at East Devon & Singer 345 kV Buses

Case	Location	Capacitor Banks	Resonant Frequency & Impedance (pu of 60Hz, Ohm)					
			Low		Middle		High	
			HN	Z(Ω)	HN	Z(Ω)	HN	Z(Ω)
M/N-XLPE-SC2_1B	Plumtree 345 kV	All in Service	3.0	117	5.7	131	13.6	1480
M/N-XLPE-SC2_1C	Plumtree 345 kV	All Out of Service	3.9	218			11.8	330
M/N-XLPE-SC2_2B	Plumtree 115 kV	All in Service	2.9	19	6.9	74	9.7	63
M/N-XLPE-SC2_2C	Plumtree 115 kV	All Out of Service	3.8	23			11.8 15.0	128 96
M/N-XLPE-SC2_3B	Norwalk 345 kV	All in Service	3.0	123	5.8	182		
M/N-XLPE-SC2_3C	Norwalk 345 kV	All Out of Service	3.9	270				
M/N-XLPE-SC2_4B	Norwalk 115 kV	All in Service	3.0	14	4.6	16		
M/N-XLPE-SC2_4C	Norwalk 115 kV	All Out of Service	3.8	19			8.3 16.1	24 33
M/N-XLPE-SC2_5B	Southington 345 kV	All in Service	3.0	78	4.6	55	8.2 12.4	86 115
M/N-XLPE-SC2_5C	Southington 345 kV	All Out of Service	3.8	72			10.6	260
M/N-XLPE-SC2_6B	Southington 115 kV	All in Service	2.9	12	4.5 5.3	22 33	9.4	127
M/N-XLPE-SC2_6C	Southington 115 kV	All Out of Service	3.8	10			10.3	29
M/N-XLPE-SC2_7B	East Shore 345 kV	All in Service	2.9	65	6.2	224	12.4 14.6	247 514
M/N-XLPE-SC2_7C	East Shore 345 kV	All Out of Service	3.7	70			10.3	245
M/N-XLPE-SC2_8B	Devon 115 kV	All in Service	2.9	11				
M/N-XLPE-SC2_8C	Devon 115 kV	All Out of Service	3.8	13				
M/N-XLPE-SC2_9B	Frost Bridge 115 kV	All in Service	3.0	20	4.6 5.8	23 39	8.3	34
M/N-XLPE-SC2_9C	Frost Bridge 115 kV	All Out of Service	3.8	13			10.3	27
M/N-XLPE-SC2_10B	Glenbrook 115 kV	All in Service	2.9	16	4.6 5.8	30 38		
M/N-XLPE-SC2_10C	Glenbrook 115 kV	All Out of Service	3.8	17	8.3	43	16.2	55
M/N-XLPE-SC2_11B	Singer 345 kV	All in Service	3.0	113	5.8	185	13.6	403
M/N-XLPE-SC2_11C	Singer 345 kV	All Out of Service	3.9	253				
M/N-XLPE-SC2_12B	Devon 345 kV	All in Service	3.0	108	5.7	166	13.6	515
M/N-XLPE-SC2_12C	Devon 345 kV	All Out of Service	3.9	234				
M/N-XLPE-SC2_13B	Beseck 345 kV	All in Service	2.9	66			12.5	307
M/N-XLPE-SC2_13C	Beseck 345 kV	All Out of Service	3.8	79			10.6	264

Table 4. Resonant Frequencies for M/N-XLPE Project with Local Generators Off
A 500 MVA Synchronous Condenser at East Devon & Singer 345 kV Buses

Case	Location	Capacitor Banks	Resonant Frequency & Impedance (pu of 60Hz, Ohm)					
			Low		Middle		High	
			HN	Z(Ω)	HN	Z(Ω)	HN	Z(Ω)
M/N-XLPE2-SC2_1B	Plumtree 345 kV	All in Service	2.7	94	5.7	131	13.6	1427
M/N-XLPE2-SC2_1C	Plumtree 345 kV	All Out of Service	3.6	161			11.8	296
M/N-XLPE2-SC2_2B	Plumtree 115 kV	All in Service	2.7	16	6.8	62	9.5	63
M/N-XLPE2-SC2_2C	Plumtree 115 kV	All Out of Service	3.6	19			11.7 14.9	118 87
M/N-XLPE2-SC2_3B	Norwalk 345 kV	All in Service	2.7	101	5.7	184		
M/N-XLPE2-SC2_3C	Norwalk 345 kV	All Out of Service	3.7	199				
M/N-XLPE2-SC2_4B	Norwalk 115 kV	All in Service	3.0	14	4.6	16		
M/N-XLPE2-SC2_4C	Norwalk 115 kV	All Out of Service	3.6	16			8.1 16.0	23 32
M/N-XLPE2-SC2_5B	Southington 345 kV	All in Service	2.7	65	4.5	54	8.2 12.4	92 113
M/N-XLPE2-SC2_5C	Southington 345 kV	All Out of Service	3.5	62			10.4	238
M/N-XLPE2-SC2_6B	Southington 115 kV	All in Service	2.7	11	4.5 5.2	21 27	9.4	119
M/N-XLPE2-SC2_6C	Southington 115 kV	All Out of Service	3.5	9			10.1	28
M/N-XLPE2-SC2_7B	East Shore 345 kV	All in Service	2.6	73	6.1	247	12.4 14.2	267 373
M/N-XLPE2-SC2_7C	East Shore 345 kV	All Out of Service	3.5	76			10.1	274
M/N-XLPE2-SC2_8B	Devon 115 kV	All in Service	2.7	12				
M/N-XLPE2-SC2_8C	Devon 115 kV	All Out of Service	3.5	14				
M/N-XLPE2-SC2_9B	Frost Bridge 115 kV	All in Service	2.7	16	4.5 5.7	21 39	8.3	35
M/N-XLPE2-SC2_9C	Frost Bridge 115 kV	All Out of Service	3.5	11			10.1	26
M/N-XLPE2-SC2_10B	Glenbrook 115 kV	All in Service	2.7	15	4.5 5.8	29 35		
M/N-XLPE2-SC2_10C	Glenbrook 115 kV	All Out of Service	3.6	16	8.1	41	16.1	53
M/N-XLPE2-SC2_11B	Singer 345 kV	All in Service	2.7	94	5.7	187	13.6	385
M/N-XLPE2-SC2_11C	Singer 345 kV	All Out of Service	3.7	188				
M/N-XLPE2-SC2_12B	Devon 345 kV	All in Service	2.7	90	5.7	168	13.6	498
M/N-XLPE2-SC2_12C	Devon 345 kV	All Out of Service	3.7	175				
M/N-XLPE2-SC2_13B	Beseck 345 kV	All in Service	2.6	56			12.4	297
M/N-XLPE2-SC2_13C	Beseck 345 kV	All Out of Service	3.6	66			10.4	239

Conclusions

Table 5 summarizes the variation in frequencies of the first resonance points for the M/N project, for the XLPE alternative, for Synchronous Condenser Option 1, and for Synchronous Condenser Option 2, with the original light load generator dispatch. Table 6 summarizes the variation in frequencies of the first resonance points in the light post-project dispatch with more local generation off. With Synchronous Condenser Option 2 and with the original light load generator dispatch, the first resonance is between 3.0 and 3.9 pu of 60 Hz at most 345 kV buses, with all capacitor banks in and out of service, respectively. With Synchronous Condenser Option 2 and with more local generation off, the first resonance is between 2.7 and 3.6 pu of 60 Hz at most 345 kV buses, with all capacitor banks in and out of service, respectively.

Table 5. Variation in Frequency of First Resonance Points (pu 60 Hz)
with Original Light Load Generator Dispatch

115 kV Capacitor Bank Conditions	M/N Project with HPFF Cable	M/N Project with XLPE Cable	Synchronous Condenser Option 1 (Case 5c)	Synchronous Condenser Option 2 (Case 5d)
All in service	2.4	2.8	2.9	3.0
All out of service	2.8	3.5	3.7	3.9

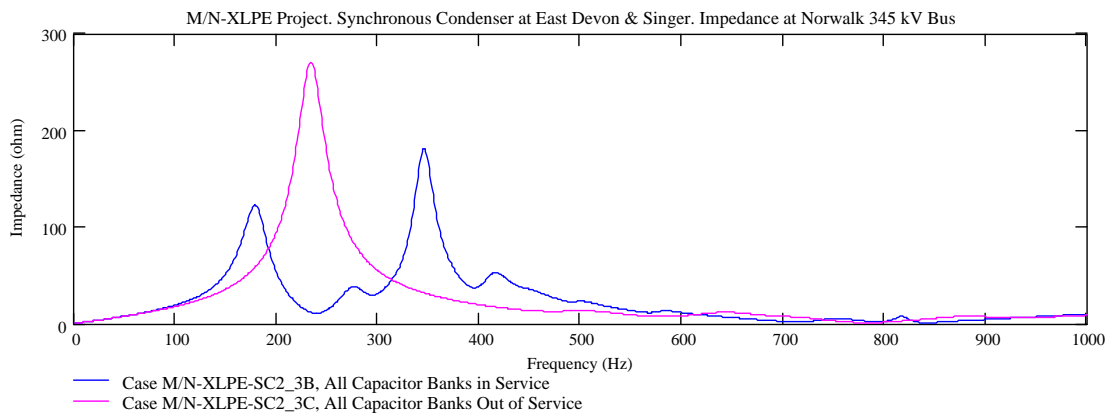
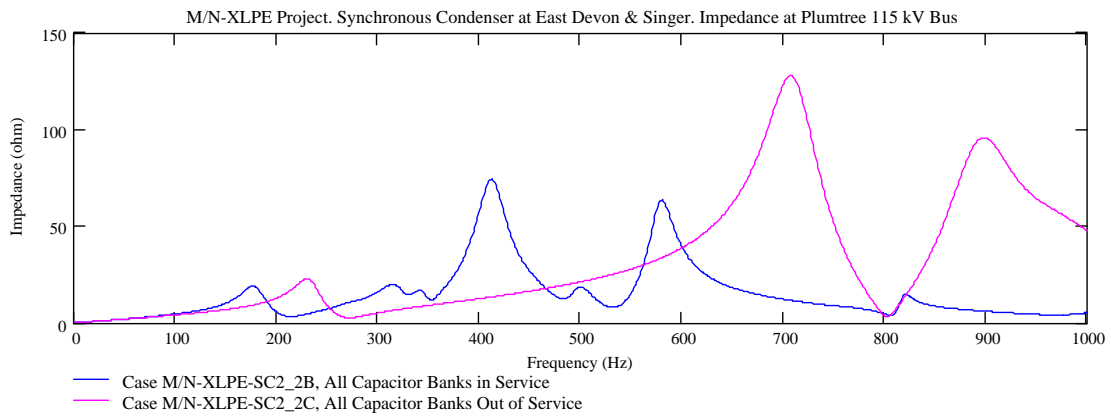
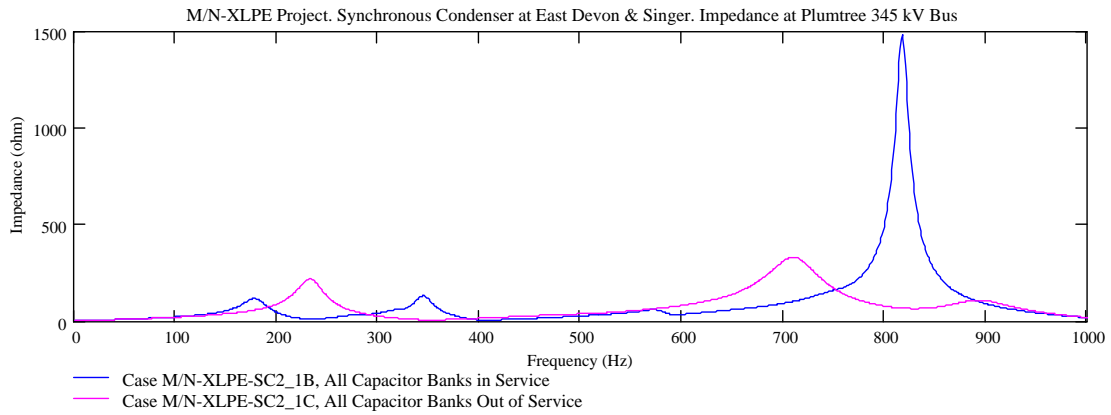
Table 6. Variation in Frequency of First Resonance Points (pu 60 Hz)
in Light Post-Project Dispatch with More Local Generators Off

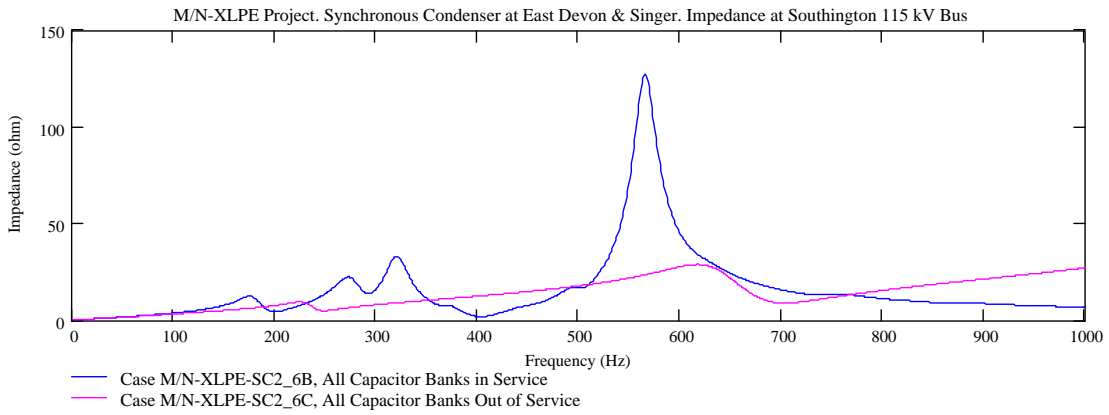
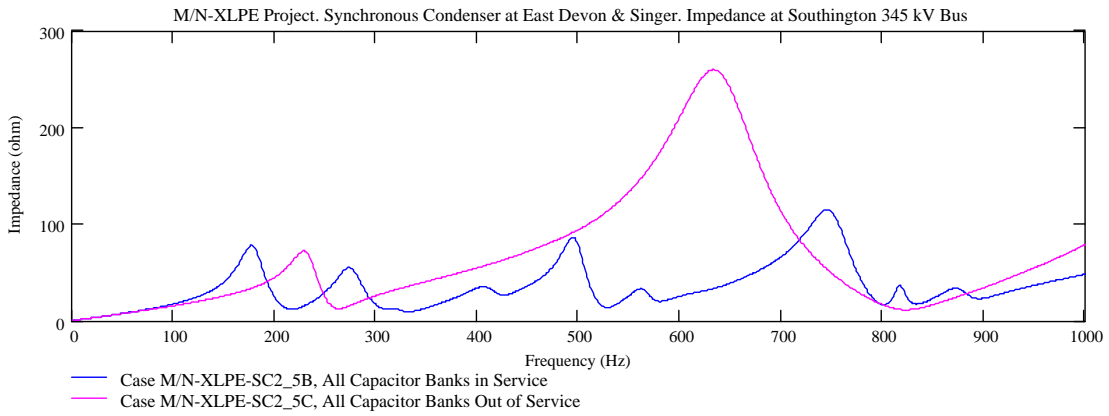
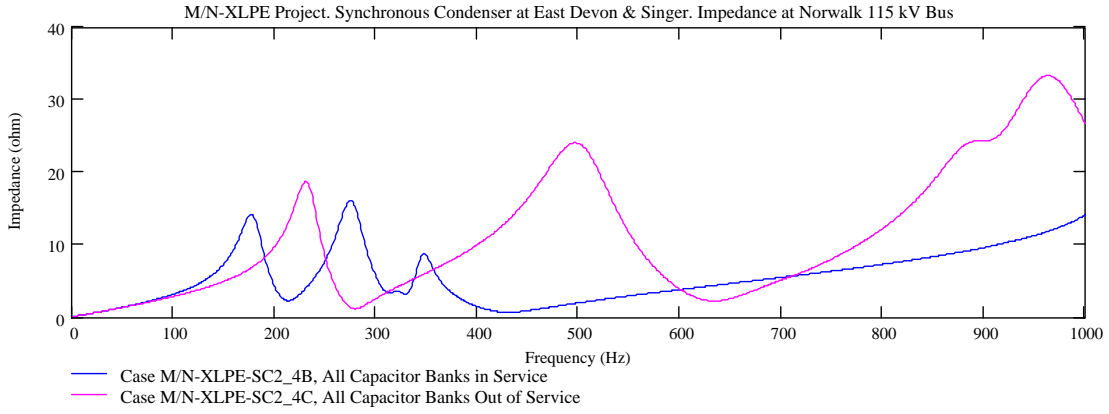
115 kV Capacitor Bank Conditions	M/N Project with HPFF Cable	M/N Project with XLPE Cable	Synchronous Condenser Option 1 (Case 5c)	Synchronous Condenser Option 2 (Case 5d)
All in service	-	2.5	2.6	2.7
All out of service	-	3.3	3.5	3.6

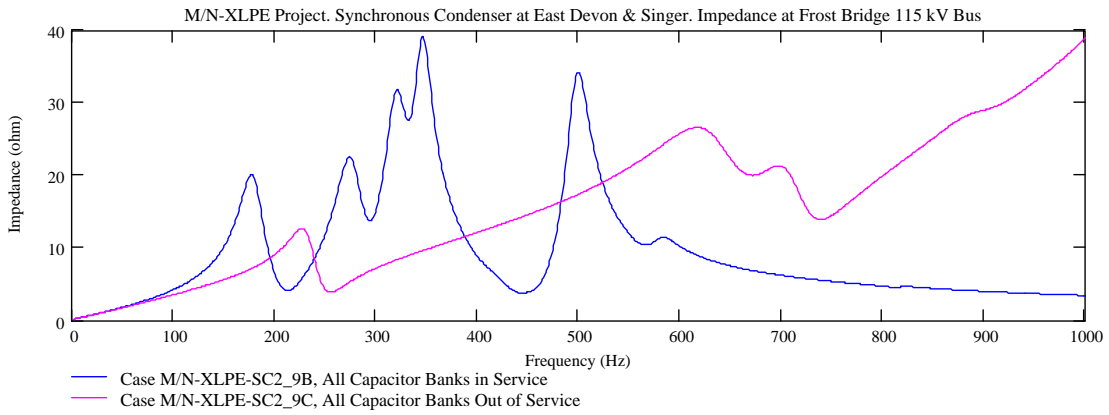
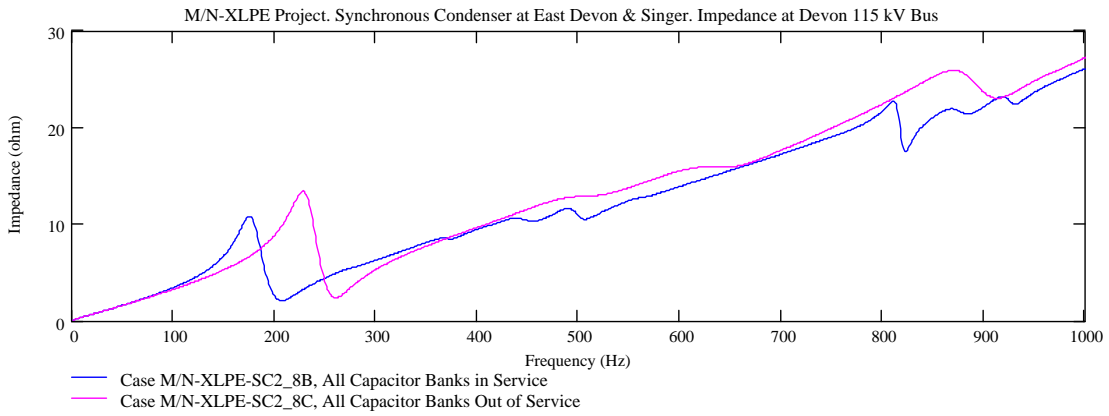
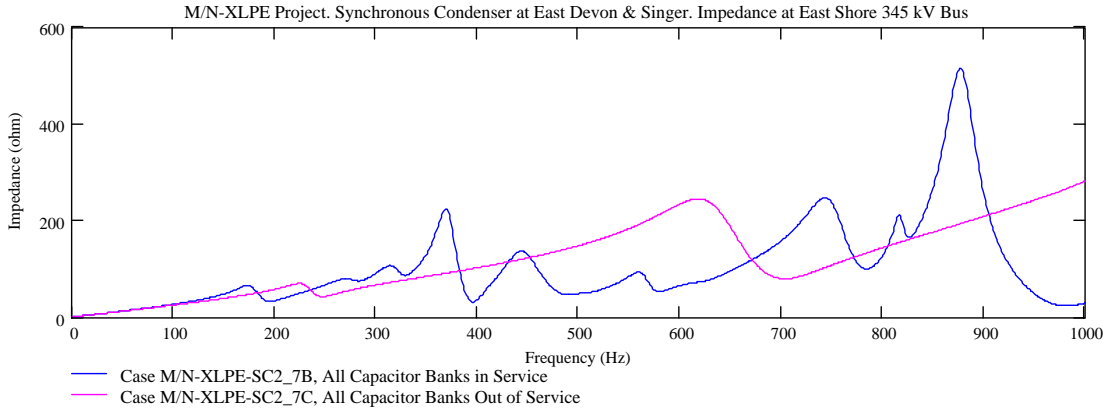
The addition of a second 500 MVA synchronous condenser at Singer results in a slightly higher frequency of the first resonance, as compared to the single synchronous condenser at East Devon. Since the short-circuit contribution at 345 kV of a 500 MVA synchronous

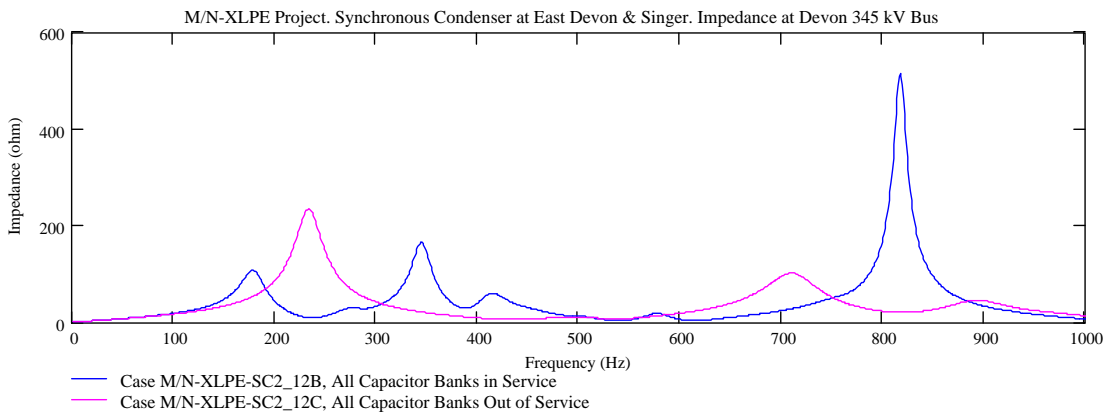
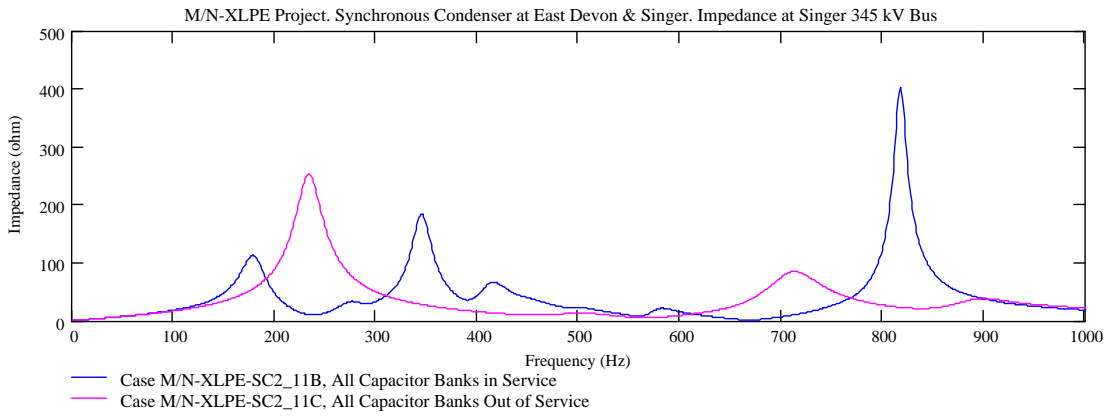
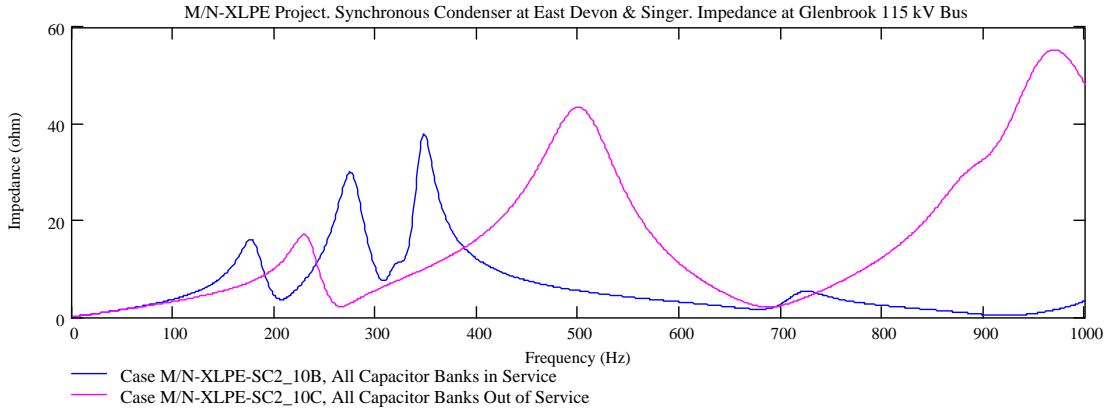
condenser, with assumed impedances including GSU, is relatively small (about 2.4 kA) compared with the existing short-circuit levels, it has a relatively small impact on the resonant frequency. With the original light load generator dispatch and all capacitor banks in service, the frequency is 3.0 pu of 60 Hz. Risk of sustained overvoltages due to transformer inrush is increased when resonances are near 3rd harmonic or below. System outages are another important consideration, since a variety of outages would similarly cause variation in resonant frequencies, because of the effect of changing either the strength of the system or the effective charging capacitance in the system. Consideration of minimum generator dispatches and system outages (such as an outage of the line from East Devon to Beseck) which would weaken the system together with the maximum allowable 115 kV capacitor bank dispatches and 345 kV cable charging capacitance would result in the lowest frequencies of the first resonance. If all first resonances were located above 3rd harmonic, under such a range of variations, the risk of sustained overvoltages due to transformer inrush would be reduced. However, if varying system conditions result in resonances below 3rd harmonic, then extensive transient studies should be performed to investigate transformer inrush scenarios, under a range of system conditions. Fault and clear scenarios are particularly critical since special circuit breaker closing enhancements have no effect. If the Synchronous Condenser Option 2 (Case 5d) studied here is to be considered, then extensive transient studies would be recommended.

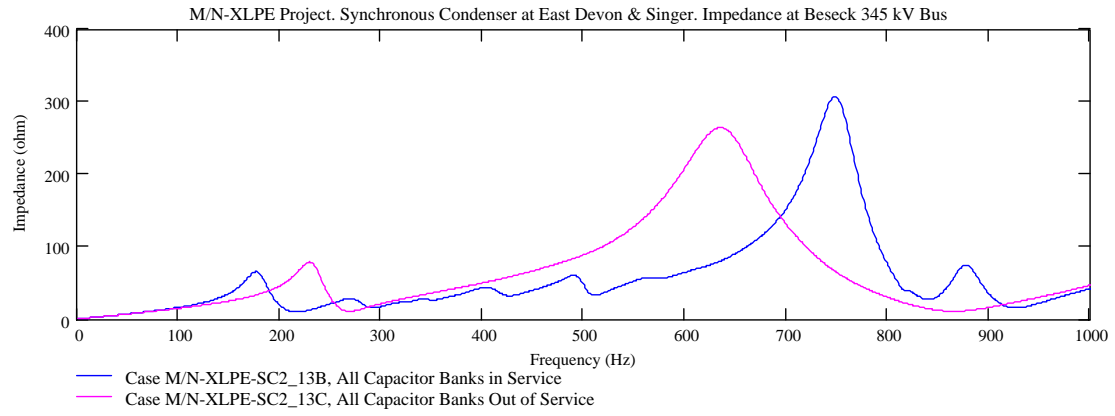
Appendix A Driving-Point Impedance Plots with Light Load Generation











Appendix B Driving-Point Impedance Plots with Local Generators Off

