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September 19, 2023

DELIVERED VIA EMAIL AND U.S. MAIL

Melanie Bachman
Executive Director
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

Re: Petition No. 1583; Petition Of TRITEC Americas, LLC For A Declaratory Ruling That No Certificate Of Environmental Compatibility And Public Need Is Required For The Construction, Operation, Maintenance, And Decommissioning Of A 0.999 MW AC Solar Photovoltaic Project In Bethany, Connecticut – Responses to the Council's Pre-Hearing Interrogatories (First Set).

Dear Attorney Bachman:

On behalf of TRITEC Americas, LLC ("Petitioner"), I am attaching the original and fifteen copies of the Petitioner's Responses to the Council's Pre-Hearing Interrogatories for Petition No. 1583. Electronic copies of these Responses have also been sent to the Council and the Intervenors today.

If you have any questions or need additional information, please do not hesitate to contact me.

Sincerely,

A handwritten signature in blue ink that reads 'Paul R. Michaud'.

Paul R. Michaud

Petition No. 1583
TRITEC Americas, LLC
Parcel Nos. 113-1 and 113-1-A
428 Bethmour Road, Bethany, Connecticut
Pre-Hearing Interrogatories to TRITEC
September 5, 2023

PETITIONER'S RESPONSES

PRE-HEARING INTERROGATORIES - FIRST SET

SEPTEMBER 19, 2023

Project Development

1. Is the project, or any portion of the project, proposed to be undertaken by state departments, institutions, or agencies or to be funded in whole or in part by the state through any contract or grant?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

No.

2. Has TRITEC received any comments from persons who are not parties or intervenors to the proceeding since the petition was submitted to the Council? If yes, summarize the comments and state how these comments were addressed.

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

No.

3. If the project is approved, identify all permits necessary for construction and operation and which entity will hold the permit(s).

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

If approved by the Siting Council, the proposed project would require a General (Stormwater) Permit from the Connecticut Department of Energy and Environmental Protection and a Building Permit and Electrical Permit from the Town of Bethany. In addition, the project would need to execute a utility interconnection easement with Eversource Energy.

4. If TRITEC transfers the facility to another entity, would TRITEC provide the Council with a written agreement as to the entity responsible for any outstanding conditions of the Declaratory Ruling and quarterly assessment charges under CGS §16-50v(b)(2) that may be associated with this facility, including contact information for the individual acting on behalf of the transferee?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

Yes.

5. Referring to Petition p. 4, when and how was the “alternative project site plan” on the Town of Bethany (Town) property at 755 Amity Road submitted to the Town?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

The alternative project site plan was developed by TRITEC’s engineering consultant, Solli Engineering, based on a recommendation from several abutters at an abutter outreach teleconference held on October 6, 2022. Attorney Michaud emailed the alternative site plan to the First Selectman for the Town of Bethany on October 12, 2022.

6. Why was an “alternative project site plan” developed for the Town property at 755 Amity Road with an output of 11.45 MW AC?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

The alternative site plan was developed to inform the Town of Bethany regarding the maximum solar potential at the site and the possible locations of the arrays to invite a discussion between TRITEC and the Town of Bethany.

7. Did the Town direct TRITEC to other Town-owned properties that may be suitable to host a solar facility? If yes, provide details.

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

No. However, at the recent Pre-Hearing Conference before the Siting Council, the attorney for the Town of Bethany indicated that the Town may be able to offer an alternative project site on privately owned land within the Town. The Town attorney provided the alternative project site earlier today, and TRITEC is conducting the necessary due diligence to determine feasibility of the site.

Proposed Site

8. Submit a map clearly depicting the boundaries of the solar facility site and the boundaries of the host parcel(s). Under Regulations of Connecticut State Agencies (RCSA) §16-50j-2a(29), “**Site**” means a contiguous parcel of property with specified boundaries, including, but not limited to, the leased area, right-of-way, access and easements on which a facility and associated equipment is located, shall be located or is proposed to be located.

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Please see Sheet 2.10 in Attachment A: Detailed Site Design, delineating the solar facility site to include the proposed limit of disturbance. Anything outside of this boundary is not considered to be part of the solar facility site although it may be proposed in conjunction with this development.

9. What is the length of the lease agreement with the property owner?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

Up to a three-year due diligence period, plus twenty years, plus two additional five-year extensions.

10. In the lease agreement with the property owner, are there any provisions related to decommissioning or Site restoration at the end of the project’s useful life? If so, please describe and/or provide any such provisions.

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

Yes, the lease includes the following provision:

13.13 Decommissioning. At the termination or expiration of the Lease, whether as to the entire Property or only as to part, Lessee shall cease commercial operation of the Solar Energy Project on the Property or the part as to which the Lease has terminated or expired. Lessee shall, as soon as practicable thereafter and at its sole cost and expense, remove all above-ground and below-ground Solar Energy Project, excluding the portion of foundations that are below a depth of two feet below grade from the natural surface of the Property or of the portion as to which this Lease was terminated, infrastructure and underground conduit that cannot be removed without damage to the Property, and dispose of such removed components per applicable law (the "Decommissioning Obligations"). Lessee shall leave the Property in substantially the same condition as before the Effective Date (except for removal of trees and foliage permitted hereunder) and shall restore the soil surface to a condition reasonably similar to its original condition, reasonable wear, and tear, and casualty excepted. Lessee shall post a decommissioning performance bond to secure its performance of its obligations under this Section 13.13. The provisions of this section shall not affect any continuing rights or obligations that by the terms of this Lease survive the Term or any termination or expiration of this Lease. The provisions of this section shall survive any termination or expiration of this Lease.

11. Does the lease agreement with the property owner contain provisions for agricultural co-uses at the Site? If yes, describe the co-uses.

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

Yes, the lease agreement contains provisions for agricultural co-uses at the Site. The lease agreement does not specify the co-uses as the lease agreement was executed before the Petitioner could analyze the environmental aspects and status of the Site to determine the best agricultural uses.

12. Is the site, or any portion of the host parcel, part of the Public Act 490 Program? If so, how does the municipal land use code classify the parcel(s)? How would the project affect the use classification?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

No portion of the host parcel is part of the Public Act 490 Program.

13. Has the State of Connecticut Department of Agriculture purchased any development rights for the facility site or any portion of the facility site as part of the State Program for the Preservation of Agricultural Land?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

No.

14. Are any portions of the site under lease by any third party? If yes, when does the lease expire?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

No.

15. Referring to Petition p. 12, in what areas of the Site have the apiaries been established? What entity is managing the apiaries? Have the apiaries been registered with the State Entomologist?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

The apiaries have been established at the southwest corner of the 50' building setback mark. The apiaries are managed by Neckers Farm, a family farm based out of Branford, Connecticut. The apiaries have been registered with the State Entomologist.

16. Who would be responsible for responding to concerns and/or complaints related to agricultural co-use on the Site? How would contact information be provided for complaints?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

Horton Electric, the Operations and Maintenance (O&M") Company for the site, in conjunction with Necker's Farm (Beekeeper), would be responsible for responding to concerns and/or complaints related to agricultural co-use on the Site. TRITEC intends to maintain a "project" website containing pertinent information regarding the project, including contact information.

17. Referring to Petition p. 11, will sap be obtained from maple trees within the Site boundaries? What entity is managing maple syrup production?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

Sap has been obtained and will continue to be obtained from maple trees within the Site boundaries until construction of the proposed projects prevents further sap collection within said boundaries. Once construction begins, Rosson Maple Farm, the local farmer managing maple syrup production at the Site, will continue to obtain sap on maple trees located outside the Site boundaries and elsewhere on the property.

18. Petition page 5 states, "the solar array setback is fifty feet from the property line, consistent with the Town of Bethany's zoning regulations." What part of the proposed facility would maintain a 50-foot buffer (e.g., solar panel, perimeter fence, interconnection) from the property line? What portions of the proposed facility are within 50 feet of the property line?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

The solar panels and transformer pads will maintain a minimum 50' setback from all property lines. The only site element which encroaches within 50' of the property line will be the proposed 7' tall perimeter fence, for screening purposes.

19. Provide the distance, direction, and address of the nearest property line and nearest off-site residence from the solar field perimeter fence, transformer pads, and the proposed access drive.

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Please refer to the table below for distances, directions, and addresses of the applicable neighboring properties:

	DISTANCE (IN FEET)	DIRECTION	ADDRESS
PERIMETER FENCE TO PROPERTY LINE	12'	SOUTH	3 GLENWOOD COURT
PERIMETER FENCE TO RESIDENCE	74'	NORTH	432 BETHMOUR ROAD
TRANSFORMER PAD TO PROPERTY LINE	57'	NORTH	432 BETHMOUR ROAD
TRANSFORMER PAD TO RESIDENCE	127'	NORTH	432 BETHMOUR ROAD
ACCESS DRIVE TO PROPERTY LINE	34'	NORTH	432 BETHMOUR ROAD
ACCESS DRIVE TO RESIDENCE	87'	NORTH	432 BETHMOUR ROAD

20. Referring to the Boundary and Topographic Map EX-1 - General Note 1C, when was the field resurvey conducted? During the resurvey, were the remains of an old fence/barb wire evident in the area of 11 Glenwood Court? Does the alignment of this fence line up with the Map Reference Note B ("Glenwood Map of Lots... April 2, 1964...")?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Per General Note 5 on the Boundary And Topographic Map EX-1, a third-party civil engineering firm, BL Companies, performed fieldwork for the resurvey on January 5, 2022. Solli cannot confirm whether the remains of an old fence/barbed wire were evident in the area of 11 Glenwood Court, or whether the alignment of this fence lined up with the Map Reference Note B.

Energy Output

21. Referring to Petition p. 11, provide the following:

a) additional information as to how the energy from the facility and the associated renewable energy certificates are allocated under the Non-Residential Renewable Energy Solutions Program (NRES).

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

The Non-Residential Renewable Energy Solutions (NRES) Program requires participants to match project generation output with the usage of State, Agricultural, and Municipal (SAM) entities. For example, if a town's annual usage totals one million kilowatt hours (kWh) per year, then the project's solar generation can't exceed one million kilowatt hours per year.

Here, the proposed project will generate about 2.2 million kWh a year. Petitioner allocated 2.4 million kWh of accounts owned by the Cities of Torrington and Meriden to the project, and in return, Petitioner paid the Cities for allowing Petitioner to allocate said accounts.

Petitioner will sell the solar energy and associated renewable energy certificates directly to Eversource under the NRES Program and the terms of the subsequent Tariff Agreement.

b) Is there a renewal option beyond the 20-year contract term?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

Yes. The lease contains two five-year extensions.

c) Is there a project benefit to Town of Bethany residents?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

Yes. If approved by the Siting Council, the project would provide the Town of Bethany with several benefits. First, the project would produce clean, carbon-free energy for the electric grid, thus reducing the town's reliance on fossil fuels and helping to decrease greenhouse gas emissions and combat climate change, contributing to a more sustainable future.

Second, the project would produce long-term (at least 20 years) stable electricity for the electric grid, which can help lower electricity costs for the town and its residents over the long term.

Third, the project would generate additional revenue for the town through property taxes and other fees - on the land and equipment, which would benefit the local government.

Fourth, the project would reduce air and water pollution associated with fossil fuel power plants, improving local air quality and protecting natural resources. The project would also conserve water, as solar panels do not require water for cooling like traditional power plants.

Fifth, the project could serve as an educational tool for the local school to teach the students, about renewable energy, sustainability, and environmental conservation.

Sixth, the project would result in substantial grid improvements in the area of the solar array, thus resulting in electric grid resiliency for town residents.

Lastly, the project would allow the town to help meet Connecticut's law to achieve 100% carbon-free generation by 2040.

22. If the facility operates beyond the terms of the NRES contract, will TRITEC decommission the facility or seek other revenue mechanisms for the power produced by the facility?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

TRITEC will seek other revenue mechanisms for the power produced by the facility if it operates beyond the terms of the NRES contract.

23. Is the project being designed to accommodate a potential future battery storage system? If so, please indicate the anticipated size of the system, where it may be located on the site, and the impact it may have on the NRES contract(s).

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

The project has not been designed to accommodate a potential future battery storage system. A battery storage system would not impact the NRES contract.

24. If one section of the solar array experiences electrical problems causing the section to shut down, could other sections of the system still operate and transmit power to the grid? By what mechanism are sections electrically isolated from each other?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

The electrical system is isolated by strings of DC circuits that are wired to a Combiner; each DC circuit is protected by Fuses. These fuses will protect other strings within the system and allow the balance of the system to produce. Furthermore, the DC strings connect to separate invertors, and these invertors are connected to AC breakers. If the invertor fails, then it will only affect the DC strings attached to that specific invertor.

25. Would TRITEC participate in an ISO-NE Forward Capacity Auction? If yes, which auction(s) and capacity commitment period(s)?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

TRITEC intends to explore the possibility of participating in the ISO-NE Forward Capacity Auction.

Proposed Facility and Associated Equipment

26. List the equipment that would be installed on the two concrete pads in the northwest corner of the site. Provide dimensions of the equipment.

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

The medium voltage switchgear equipment will be installed on one pad, and the solar transformer will be installed on the second pad. Final dimensions will be available when the equipment is ordered.

27. Petition Exhibit L contains specification sheets for two different solar panels. Which solar panels would be installed at the site? What solar panel output was used to calculate the generation capacity of the site?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

The Trina Solar TSM-DEG19C.20-540 modules will be used for this project and were the ones used to calculate the generation capacity for the site.

28. The Petition Exhibit E site plans specify a six-foot high fence, whereas the Exhibit L Site Plans specify a 7-foot fence. Both plan sets have the same date. Which set of plans is correct?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

The correct fence height is 7'. All site plans and exhibits have been revised to reflect the correct fence height and are attached. See Attachment B: Environmental Assessment.

29. Petition Exhibit E Site Plan 2.11 provides the vegetated aisle width. How does the aisle width comply with the Soil Array Spacing Detail on Site Plan 3.01, given that slopes within the array attain 9.5 percent?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Per the detail on Sheet 3.01 in Attachment A, the proposed vegetated aisle width, or “disconnection length” shall be equal to or greater than the solar panel width. As shown on Sheet 2.11, the width of the solar panels is $\pm 7.8'$, while the proposed vegetated aisle width is $10'$.

30. What is the width of the installed solar panels?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

The solar panel width is $7.8'$.

31. What is the minimum and maximum height of the solar panels above grade?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

The minimum height is $4'$ when the solar panels are in a flat position. The maximum height is $7'6''$ when the solar panels are at full tilt.

32. Was an alternate location of the access drive extending from Bethmour Road considered? If yes, in what location? If no, describe the feasibility of relocating the access drive towards the center of the parcel.

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

The proposed access drive location was chosen because it is near the existing driveway location. Relocating the access drive to the center of the parcel would result in greater disturbance to the land and a disruption to the design of the proposed solar photovoltaic array, impacting the ability to provide a system capable of producing 0.99 MW AC as intended. In order to obtain the desired string lengths for the solar modules, it is important to have the access drive located outside the array itself, which would be compromised if the access drive were to be located in the center of the parcel.

Additionally, the proposed access drive location will minimize the number of utility poles needed to develop the project. Currently, the project would only require a minimum of three utility-owned poles. Moving the access road to the center of the parcel could result in installing additional poles.

33. Can the string inverters be located on panel row ends in the center of the facility? Explain

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

No, string inverters cannot be located in the center of the facility because the proposed project is a tracker system. Locating invertors in the center of each row would impede the tracking.

Electrical Interconnection

34. Did the interconnection agreement with Eversource require a review from ISO-NE?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

No. According to Eversource Energy, projects under 1 MW AC typically do not require ISO-NE review.

35. Referring to Petition p. 7, what offsite upgrades are necessary to facilitate the Project interconnection?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

The only necessary offsite upgrades will be completed by Eversource Energy regarding utility poles and overhead wiring.

36. Referencing Site Plan 2.11,

a) What is the height of the utility poles above ground level after installation?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

The utility standard height for utility poles is 35 to 40'.

b) What equipment is mounted on each pole?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

Utility owned and operated equipment.

c) Can the number of poles be reduced by consolidating equipment?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

No.

37. Have there been any discussions with Eversource to use pad-mounted equipment rather than pole-mounted equipment? Provide cost estimates for both an overhead and underground interconnection.

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

Eversource Energy does not pad-mount their equipment. Petitioner is discussing the feasibility of overhead versus underground interconnection routes and associated cost estimates of each route with Eversource.

Public Safety

38. Would the project comply with the current Connecticut State Building Code and National Electrical Code?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

Yes.

39. What are industry Best Management Practices for Electric and Magnetic Fields at solar facilities? Would the site design conform to these practices?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

The industry Best Management Practices for Electric and Magnetic Fields and National Electrical Code require a 7' fence around the array. The Site design conforms to these practices.

40. In the event of a brush or electrical fire, how are potential electric hazards that could be encountered by emergency response personnel mitigated? What type of media and/or specialized equipment would be necessary to extinguish a solar panel/electrical component fire?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response: The 7' fence required under the National Electrical Code mitigates potential electrical hazards. Also, the project equipment consists of numerous fail-safes to further mitigate electrical fires. Petitioner is not aware of any media or specialized equipment needed to extinguish solar fires.

41. What type of oil is within the transformer? Does the transformer have a containment system in the event of a leak? Can the SCADA system detect an insulating oil leak?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

Currently, all manufactured transformers contain mineral oil, and mineral oil is not a danger to the environment. SCADA only detects if a transformer is on or off. These transformers are standard and used industry wide, including by the electrical distribution companies.

42. Identify the distance/direction of the nearest federally-obligated airport from the proposed site. Is an aviation glare analysis required for this airport?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Waterbury-Oxford Airport is the nearest federally-obligated airport, located approximately 7.6 miles northwest of the Site. An aviation glare analysis is not required for this airport per the FAA's Determination of No Hazard for this project. See Appendix E from the Environmental Assessment for additional information.

43. Are there any water wells on the site or in the vicinity of the site? If so, would the installation of racking posts affect well water quality from construction impacts, such as vibrations and sedimentation?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

The properties in the vicinity of 428 Bethmour Road are not serviced by a public water supply, and therefore are assumed to have private water wells. Vibrations from the installation of racking posts are not anticipated to cause any sedimentation release and should result in no disruption to well water flow and water quality. The contractor shall follow the guidelines of the Soil Erosion and Sediment Control Plan for this project, which will minimize the potential impacts to the groundwater and surface water quality for the Site and its surrounding areas.

44. What chemicals, if any, would be used during the operation of the facility?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

None.

45. Describe how the solar panels are constructed. Would rainwater penetrate the panels over time and leach out chemicals/substances?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

Each solar panel consists of a glass cover, aluminum pane, and a sealed back sheet. Rainwater will not penetrate the panels.

46. What noise-generating equipment would be installed at the site? Provide noise profile information for all noise-generating equipment during site operation.

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

The only noise-generating equipment that will be installed at the site will be the inverters. Please see Attachment C: Noise Level Test Report.

47. Based on the noise profile information for the selected equipment, what is the collective operational noise level of the equipment at the nearest property boundary? Does this noise level meet applicable Department of Energy and Environmental Protection (DEEP) Noise Standards?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

The collective operational noise level of the inverters at the nearest property boundary is 39.3 dB. This noise level meets the applicable DEEP Noise Standards, and these noise levels will effectively be reduced to zero during night-time hours and when the array is not generating electricity.

Environmental Effects and Mitigation Measures

48. Provide a site plan that clearly shows the limit of tree removal and site grubbing.

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Sheet 2.11 in Attachment A has been revised to show the proposed limits of tree clearing and site grubbing.

49. What types of seed mix would be used for final stabilization?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Seed mix notes have been added to Sheet 2.11 in Attachment A. ERNMX-147 will be used for final stabilization within the solar array. ERNMX-610 will be used outside the fence line and in non-array areas. New England Erosion Control/Restoration No Mow Mix will be used in the stormwater basin.

50. What type of evergreen species are planned to be planted?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

A total of (89) evergreen trees will be planted along the fence line. Per the Planting Schedule on Sheet 2.11 in Attachment A, those species are classified as American Arborvitae, White Fir, White Spruce & Colorado Blue Spruce. These trees will have an installed height of 7-8 feet and a mature height of 20 feet.

51. The Geotechnical Report references dry-stacked stone walls cross the property. Would any stone walls be affected by the development of the solar facility? If yes, could the stone walls be rebuilt, and where could they be rebuilt?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

The existing stone walls within the perimeter fence will be affected by the development. It is the intent of the Petitioner to rebuild these stone walls outside the perimeter fence. See Sheet 2.11 in Attachment A for additional information.

52. Submit photographic site documentation with notations linked to the site plans or a detailed aerial image that identify locations of site-specific and representative site features. The submission should include photographs of the site from the public road(s) or publicly accessible area(s) as well as Site-specific locations depicting site features including, but not necessarily limited to, the following locations as applicable:

For each photo, please indicate the photo viewpoint direction and stake or flag the locations of site-specific and representative site features. Site-specific and representative site features include, but are not limited to, as applicable:

1. wetlands, watercourses, and vernal pools;
2. forest/forest edge areas;
3. agricultural soil areas;
4. sloping terrain;
5. Proposed stormwater control features;
6. nearest residences;
7. Site access and interior access road(s);
8. Utility pads/electrical interconnection(s);
9. clearing limits/property lines;
10. mitigation areas, and
11. any other noteworthy features relative to the Project.

A photolog graphic must accompany the submission, using a site plan or a detailed aerial image depicting each numbered photograph for reference. For each photo, indicate the photo location number and viewpoint direction, and clearly identify the locations of site-specific and representative site features shown (e.g., physical staking/flagging or other means of marking the subject area).

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

A photolog has been prepared and is included as part of the interrogatory response package. Please see [Attachment D: Remote Field Review](#).

Facility Construction

53. Submit a construction fuel materials storage, refueling, and spill response plan.

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

A construction fuel materials storage, refueling, and spill response plan is not available at this time, but it can be provided prior to construction.

54. Has TRITEC submitted an application for a stormwater permit? If yes, what is the status of such permit?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

TRITEC is in the process of preparing the stormwater permit application and it should be submitted within the next 60 days.

55. Referring to Petition Exhibit L, Geotechnical Report, Test Pit 4 is in the location of the proposed stormwater basin. The test pit indicates bedrock occurs at a depth of approximately 594.5 feet above mean sea level (amsl). The stormwater basin will be excavated to a depth of 589 feet amsl. How will the basin promote infiltration through bedrock?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Test Pit 4 indicates that the depth to bedrock in that location is approximately 5.5' below existing grade. The basin is not intended to promote infiltration. Furthermore, the basin has been modified to raise the bottom so as to minimize or eliminate the potential for rock excavation.

56. Will blasting be required to construct the stormwater basin? If not, how will bedrock be removed?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Based on the bottom elevation of the proposed basin and the results of the nearby Test Pit 4, it is expected that any bedrock that could be encountered during the construction of the basin could be removed by rock hammering, however, one cannot determine what methods until the bedrock is exposed.

57. The Geotechnical Report stated that due to shallow bedrock at the site, a ballast-mount tracker system is an alternative to the proposed pile foundations. Why were driven pile foundations selected over a ballast mount system?

Responsible Party: Warren Horton, Horton Electrical Services, LLC, and Squirrel Enterprises, Inc.

Response:

Driven pile foundations were selected over a ballast mount system because driven pile systems can be installed in or through bedrock, with use of a rock drill. This is the preferred system of installation based on stability of the piles.

58. Referring to Site Plan 2.31, Phase II includes the construction of temporary sediment traps and associated swales, followed by the construction of the site. Do the *2002 Connecticut Guidelines for Soil Erosion and Sediment Control* require that these stormwater control features be stabilized prior to further site disturbance? What time interval is anticipated to achieve stabilization of these stormwater control areas?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

The proposed temporary sediment trap is to be installed during the initial phase of construction, whereas the two (2) permanent water quality swales will be installed during Phase 2 of construction. The 2002 Connecticut Guidelines for Soil Erosion and Sediment Control states that the contractor shall, “stabilize the earthen embankment using any of the following measures: temporary seeding, permanent seeding, or stone slope protection immediately after installation.” The time interval to achieve stabilization will be based on site specific conditions and will be monitored by qualified personnel per the inspection requirements associated with the general permit.

59. What effect would runoff from the drip edge of each row of solar panels have on site drainage patterns? Would channelization below the drip edge be expected?

Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Runoff from the panel drip edges is not anticipated to create significant dripline erosion. The proposed tracker system panel configuration will shed runoff to the east and west with changing aspects throughout the day. As a result, channelization below the drip edge is not expected.

Facility Maintenance/Decommissioning

60. Has the manufacturer of the proposed solar panels conducted Toxicity Characteristic Leaching Procedure (TCLP) testing to determine if the panels would be characterized as hazardous waste at the time of disposal under current regulatory criteria? If so, submit information that indicates the proposed solar modules would not be characterized as hazardous waste. If not, would TRITEC agree to install solar panels that are not classified as hazardous waste through TCLP testing?

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

The manufacturer, Trina Solar Co., Ltd., has conducted Toxicity Characteristic Leaching Procedure (TCLP) testing of the proposed solar panels. The solar panels are not classified as hazardous waste. Please see Attachment E: TCLP Test Results.

61. The Petition Decommissioning Plan (Exhibit E) contains information for a different location. Submit a decommissioning plan specific to the proposed site.

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

The Decommissioning Plan has been updated for the proposed site. Please see Attachment F: Decommissioning Plan.

62. Revise the Petition Operations and Maintenance Plan (Exhibit G) to include procedures for vegetation maintenance, stormwater control inspections and repair, pesticide/herbicide use, panel washing, and landscape vegetation replacement.

Responsible Party: Howie Reed, TRITEC Americas, LLC

Response:

The revised Operations and Maintenance Plan is attached and includes procedures for vegetation maintenance, stormwater control inspections and repair, pesticide/herbicide use, and landscape vegetation replacement. The solar panels do not require washing. Please see Attachment G: Operations and Maintenance Plan.

63. Would project decommissioning include stormwater management features? If yes, how would the stormwater management system be removed?

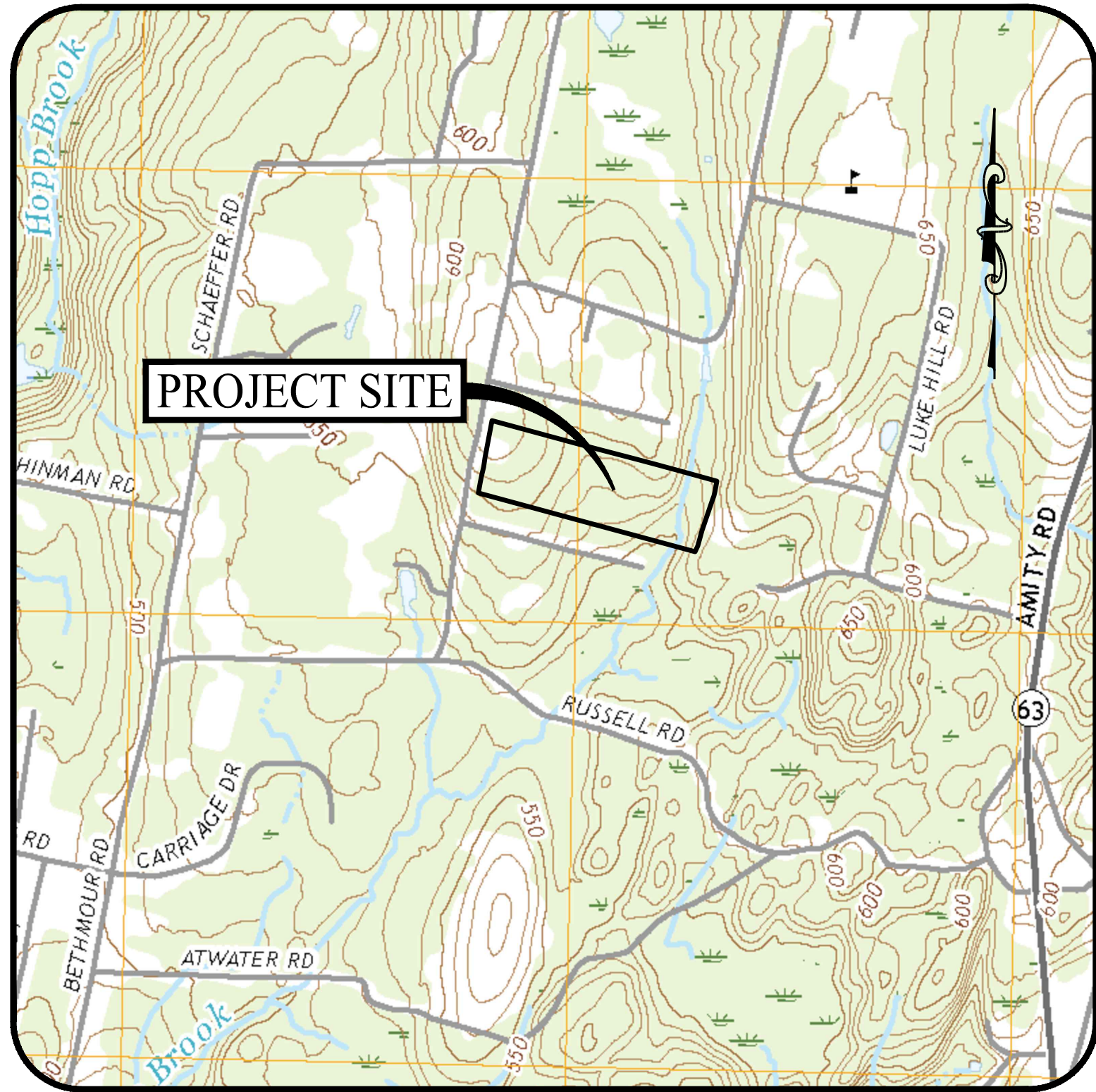
Responsible Party: Rob Pryor, Solli Engineering, LLC

Response:

Stormwater management features, including but not limited to basins and swales, may remain if there is a benefit to the property owner. If these features are to be eliminated, they shall be removed and restored in a manner to minimize disturbance and to match pre-development grades to the maximum extent practicable.

ATTACHMENT A

Detailed Site Design

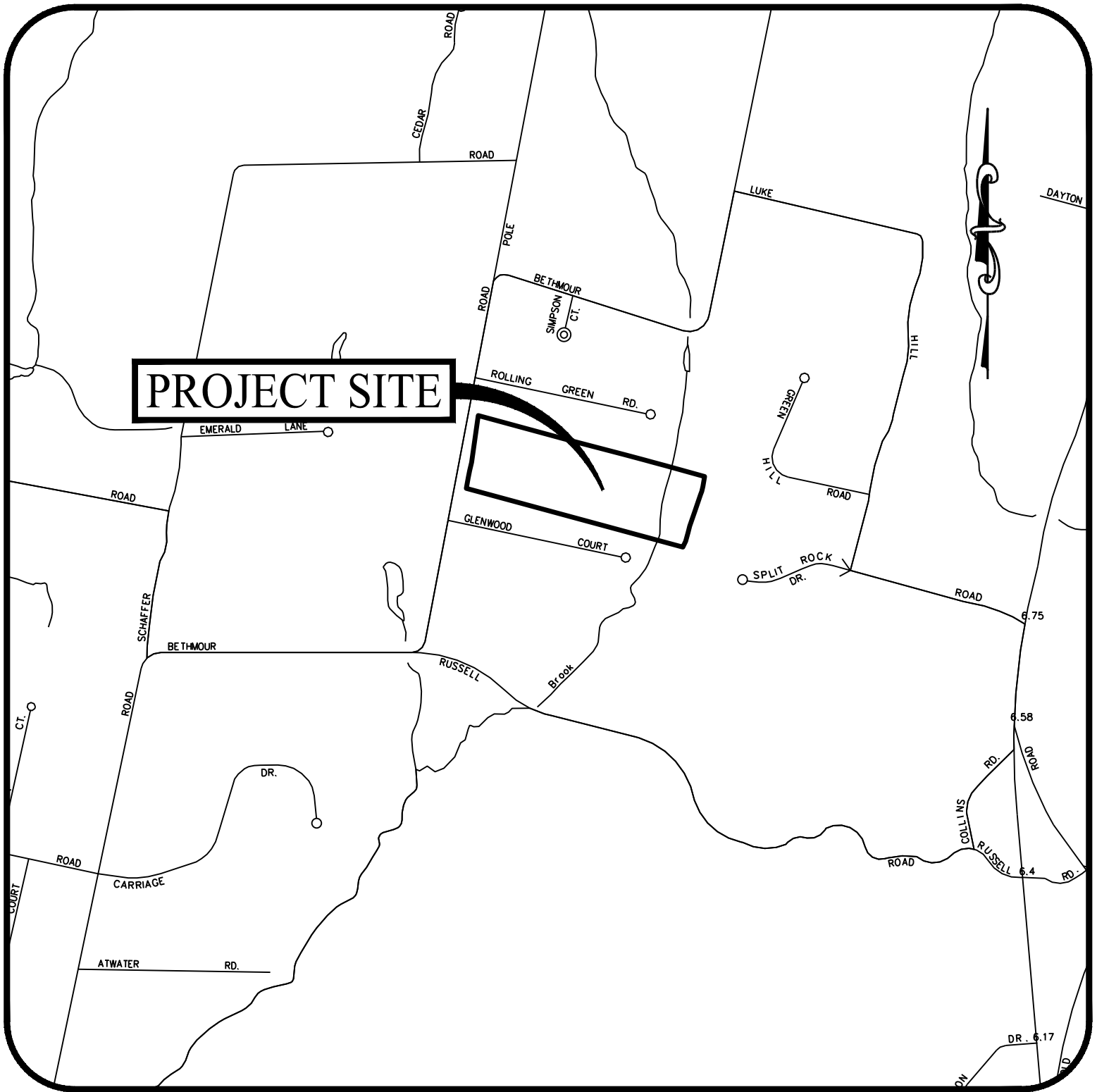


USGS MAP

SCALE: 1" = 1,000'

PROPOSED SOLAR PHOTOVOLTAIC ARRAY

428 BETHMOUR ROAD
BETHANY, CONNECTICUT



LOCATION MAP

SCALE: 1" = 1,000'

PREPARED FOR:



888 PROSPECT STREET, SUITE 200
LA JOLLA, CALIFORNIA

PREPARED BY:



501 MAIN STREET, MONROE, CONNECTICUT 06468
11 VANDERBILT AVENUE, NORWOOD, MASSACHUSETTS 02062

DRAWING LIST

SHEET #	SHEET NAME	PLAN DATE	LATEST REVISION
0.00	COVER SHEET	04/18/23	09/19/23
EX-1	EXISTING CONDITIONS MAP	01/05/22	N/A
2.10	OVERALL SITE LAYOUT PLAN	09/19/23	N/A
2.11	SITE LAYOUT PLAN	04/18/23	09/19/23
2.21	GRADING AND DRAINAGE PLAN	04/18/23	09/19/23
2.31	SOIL EROSION & SEDIMENT CONTROL PLAN	04/18/23	09/19/23
2.41	SOIL EROSION & SEDIMENT CONTROL NOTES & DETAILS	04/18/23	09/19/23
3.01	CONSTRUCTION DETAILS	04/18/23	09/19/23

OWNER

THE NEVAR COMPANY
PO BOX 743
CHESHIRE, CONNECTICUT 06410

APPLICANT

TRITEC AMERICAS, LLC
888 PROSPECT STREET, SUITE 200
LA JOLLA, CALIFORNIA 92307

PROPERTY INFORMATION

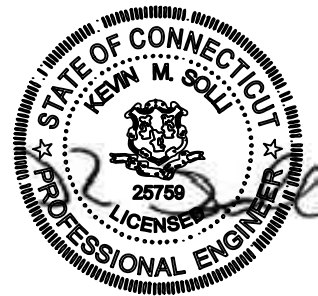
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MAP-BLOCK-LOT: 113-1 & 113-1-A
ZONE: R-65
AREA: ±21.22 AC
BOOK/PAGE: 0215/0543

SOIL SCIENTIST

WILLIAM KENNY
WILLIAM KENNY ASSOCIATES
195 TUNXIS HILL CUTOFF SOUTH
FAIRFIELD, CT 06825
(203) 366-0588

ELECTRICAL ENGINEER

PURE POWER ENGINEERING, INC.
111 RIVER STREET, SUITE 1110
HOBOKEN, NJ 07030
(201) 687-9975



SITE / CIVIL ENGINEER

KEVIN SOLLI, P.E., CPESC, LEED AP BD+C
LICENSE NO. 25759
SOLLI ENGINEERING, LLC
501 MAIN STREET
MONROE, CONNECTICUT 06468
(203) 880-5455

LANDSCAPE ARCHITECT

MARY BLACKBURN, P.L.A.,
LICENSE CT NO. 1499
SOLLI ENGINEERING, LLC
501 MAIN STREET
MONROE, CONNECTICUT 06468
(203) 880-5455

SURVEYOR OF RECORD

PATRICK J CORLESS, JR. LICENSE NO. 70015
BL COMPANIES
355 RESEARCH PARKWAY
MERIDEN, CONNECTICUT 06450
(203) 630-1406

1	09/19/23	Response to CSC Interrogatories
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Rev. #: Date Description

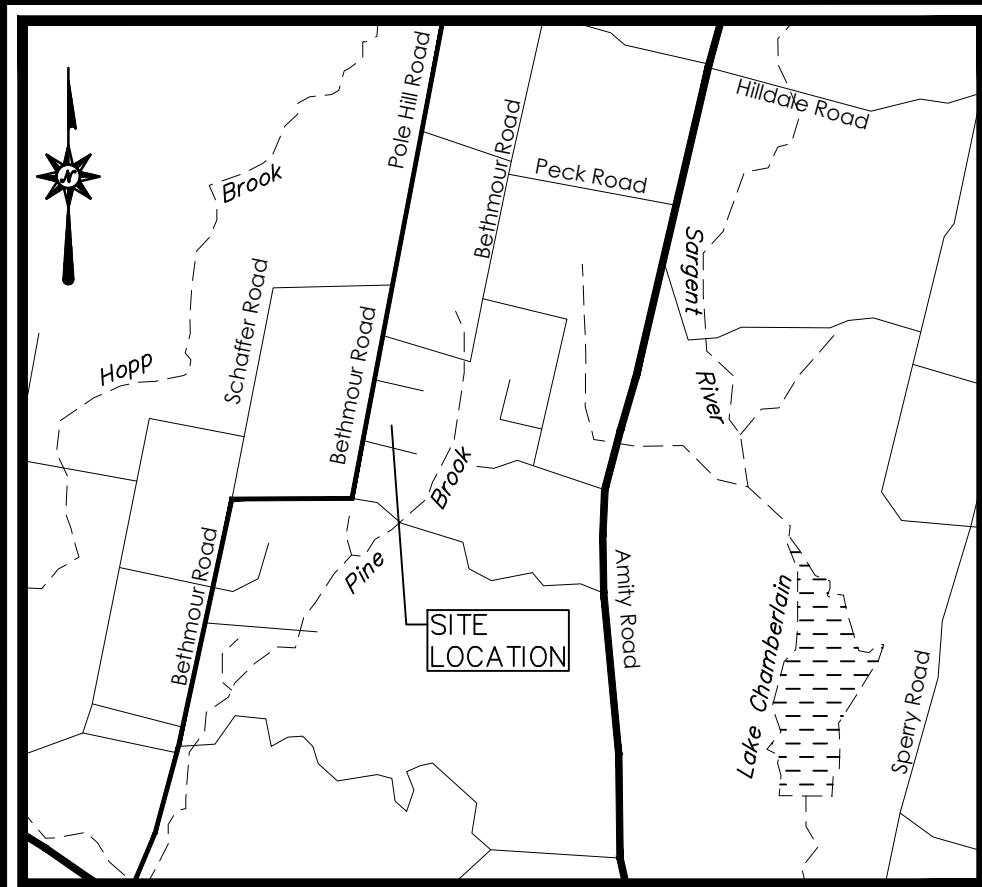
Project:
PROPOSED SOLAR PHOTOVOLTAIC ARRAY
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Sheet Title:

COVER SHEET

Sheet #:

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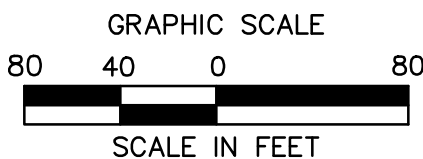


LOCATION MAP
NOT TO SCALE



LEGEND

	Property Line
	Easement Line
	Setback Line
	Edge of Water
	Limit of Wetlands
	Wetlands/Marsh
	Treeline
	Brushline
	Major Contour
	Minor Contour
	Stone Wall
	Retaining Wall
	Fence
	Overhead Wires
	Utility Pole
	Utility Pole w/ Light
	Catch Basin



MAP REFERENCES

- A. "MAP OF LAND IN BETHANY CONN., BELONGING TO THE DRAZEN LUMBER CO., OF NEW HAVEN CONN." SCALE 1"=100', DATE 11/16/1935, CERTIFIED SUBSTANTIALLY CORRECT BY A.M. WELLINGTON AND FILED AS MAP A101 IN THE TOWN OF BETHANY CLERKS OFFICE.
- B. "'GLENWOOD' MAP OF LOTS OWNED & DEVELOPED BY THE BERNER LOHNE CO., INC., BETHANY, CONN." SCALE 1"=50', DATE 4/2/1964, CERTIFIED SUBSTANTIALLY CORRECT BY RICHARD J. NOWAKOWSKI AND FILED AS MAP A200 IN THE TOWN OF BETHANY CLERKS OFFICE.
- C. "ROLLING GREEN ACRES-EAST, SECTION ONE, OWNED AND DEVELOPED BY ROLLING GREEN ACRES INC., BETHANY, CONN." SCALE 1"=50', DATE 5/1965, CERTIFIED SUBSTANTIALLY CORRECT BY WILLIAM O. DOLL AND FILED AS MAP A201 IN THE TOWN OF BETHANY CLERKS OFFICE.
- D. "LOTS 4 THRU 13, FINAL, ROLLING GREEN ACRES, SECTION 2 EAST, BETHANY CONN." SCALE 1"=50', DATE 10/1965, REVISED 11/15/1965, ADDITIONS 04/18/1966, SURVEYED BY CAHN ENGINEERS, NEW HAVEN, CT AND FILED AS MAP A209 IN THE TOWN OF BETHANY CLERKS OFFICE.
- E. "MAP OF GREEN HULL ACRES, BETHANY, CONNECTICUT" SCALE 1"=100', DATE 9/5/1972, SURVEYED BY ROBERT G. SWELL AND FILED AS MAP A284 IN THE TOWN OF BETHANY CLERKS OFFICE.
- F. "MAP OF LAND OF LENA KRUPIEN, BETHANY, CONNECTICUT" SCALE 1"=40', DATE 7/18/1980, SURVEYED BY WILLIAM E. GILBERT ASSOCIATES, CONSULTING ENGINEERS, BETHANY, CT AND FILED AS MAP A403 IN THE TOWN OF BETHANY CLERKS OFFICE.
- G. "SUBDIVISION PLAN, SPLIT ROCK, 55 LUKE HILL ROAD, BETHANY, CT." SCALE 1"=100', DATE 11/16/1994, PREPARED BY JOHN PAUL GARCIA & ASSOC. P.C. ENGINEERS AND SURVEYORS, BETHANY, CT AND FILED AS MAP A709 IN THE TOWN OF BETHANY CLERKS OFFICE.

GENERAL NOTES

1. A) THIS MAP HAS BEEN PREPARED IN ACCORDANCE WITH THE REGULATIONS OF CONNECTICUT STATE AGENCIES, SECTIONS 20-300b-1 THROUGH 20-300b-20 AND THE "STANDARDS AND SUGGESTED METHODS AND PROCEDURES FOR SURVEYS AND MAPS IN THE STATE OF CONNECTICUT" PREPARED AND ADOPTED BY THE CONNECTICUT ASSOCIATION OF LAND SURVEYORS, INC. AUGUST 29, 2019.
- B) THIS PLAN CONFORMS TO HORIZONTAL ACCURACY CLASS A-2 AND TOPOGRAPHIC ACCURACY CLASS 1-2.
- C) BOUNDARY DETERMINATION IS BASED UPON A RESURVEY.
- D) THE TYPE OF SURVEY PERFORMED IS A EXISTING CONDITIONS SURVEY AND IS INTENDED TO DEPICT THE BOUNDARY, EASEMENTS, AND EXISTING CONDITIONS WITH RESPECT TO MONUMENTATION FOUND, STRUCTURES, EASEMENTS, ENCROACHMENTS, VISIBLE UTILITIES, ROADWAYS AND CONTOURS.
2. NORTH ARROW AND BEARINGS REFER TO THE CONNECTICUT STATE PLANE COORDINATE SYSTEM (CT NAD 83 - EPOCH 2011) AND ARE BASED ON GPS OBSERVATIONS PERFORMED BY BL COMPANIES DURING NOVEMBER, 2021 UTILIZING THE SMARTNET VRS NETWORK.
3. ELEVATIONS REFER TO THE NORTH AMERICAN DATUM OF 1988 (NAVD 88). THE DATUM WAS DETERMINED BY USING (GEOID 18) AND IS BASED ON GPS OBSERVATIONS PERFORMED BY BL COMPANIES IN NOVEMBER, 2021 UTILIZING THE SMARTNET VRS NETWORK.
4. PARCEL IS LOCATED IN AN OTHER AREA "X". (AREAS DETERMINED TO BE OUTSIDE THE 0.2% ANNUAL CHANCE FLOODPLAIN) AS DEPICTED ON F.I.R.M. MAP NUMBER 09009C0267H, PANEL 267 OF 635. WITH EFFECTIVE DATE DECEMBER 17, 2010.
5. WETLAND BOUNDARY DETERMINED BY BL COMPANIES ON JANUARY 5, 2022 AND LOCATED BY FIELD SURVEY BY BL COMPANIES ON JANUARY 5, 2022.
6. THE UNDERGROUND UTILITIES DEPICTED HAVE BEEN PLOTTED FROM FIELD SURVEY INFORMATION AND EXISTING DRAWINGS. THE SURVEYOR MAKES NO GUARANTEES THAT THE UNDERGROUND UTILITIES DEPICTED COMPRISE ALL SUCH UTILITIES IN THE AREA, EITHER IN SERVICE OR ABANDONED. THE SURVEYOR FURTHER DOES NOT WARRANT THAT THE UNDERGROUND UTILITIES DEPICTED ARE IN THE EXACT LOCATION INDICATED THOUGH THEY ARE PLOTTED AS ACCURATELY AS POSSIBLE FROM INFORMATION AVAILABLE. THE SURVEYOR HAS NOT PHYSICALLY EXPOSED THE UNDERGROUND UTILITIES. PER CONNECTICUT STATE LAW THE CONTRACTOR SHALL CONFIRM THE LOCATION OF ALL UTILITIES PRIOR TO THE COMMENCEMENT OF EXCAVATION. CALL BEFORE YOU DIG 1-800-922-4455.



355 Research Parkway
Meriden, CT 06450
(203) 630-1406
(203) 630-2615 Fax

LAND OF
THE NEVAR COMPANY
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

REVISIONS	No.	Date	Desc.
Surveyed	KJ		
Drawn	JW		
Reviewed	PJC		
Scale	1"=80'		
Project No.	2101190		
Date	01/05/2022		
Field Book	564		
CAD File:	EX210119001		

EXISTING
CONDITIONS
MAP

Sheet No.

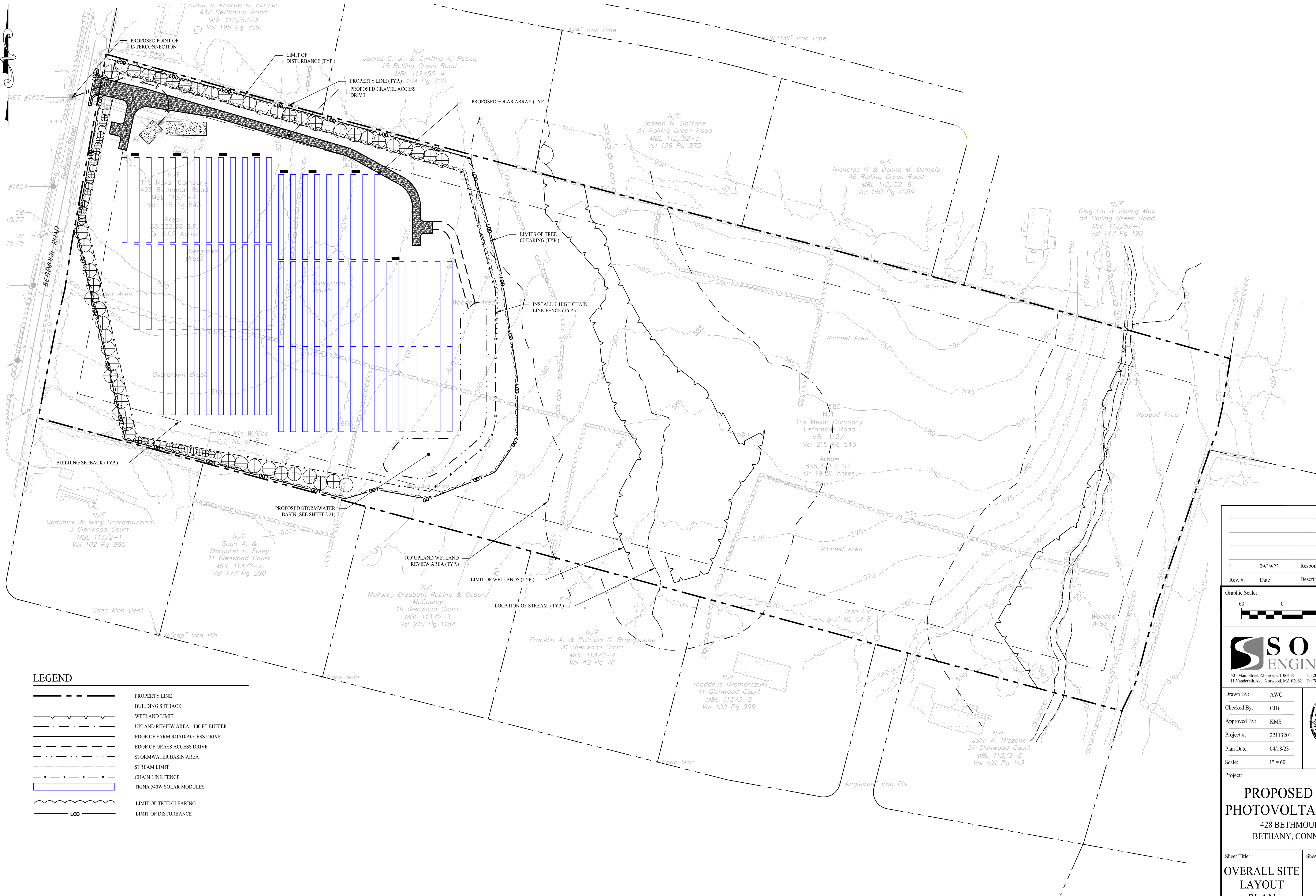
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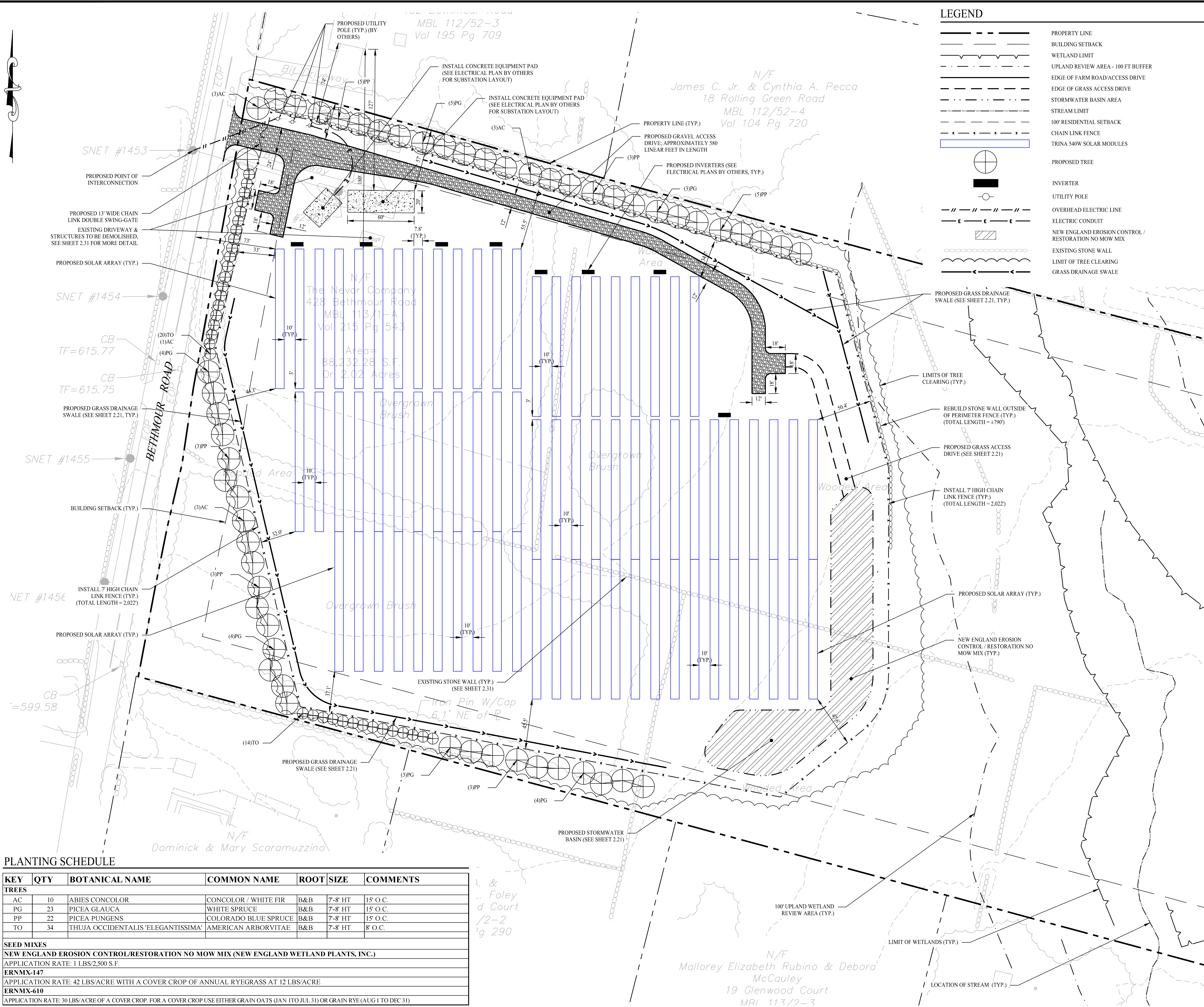
TO MY KNOWLEDGE AND BELIEF THIS MAP IS SUBSTANTIALLY CORRECT AS NOTED HEREON.

Patrick J. Corless, Jr.
1/5/2022
PATRICK J. CORLESS, JR., L.S. #70015

NO CERTIFICATION IS EXPRESSED OR IMPLIED UNLESS THIS MAP BEARS THE ORIGINAL SIGNATURE AND EMBOSSED SEAL OF THE ABOVE NAMED LAND SURVEYOR.



1 09/19/23 Response to CSC Interrogatories	
Rev. #:	Date Description
Graphic Scale: 60 0 60 120	
SOLLI ENGINEERING 501 Main Street, Monroe, CT 06468 T: (203) 880-5455 F: (203) 880-9695 11 Vanderbilt Ave, Norwood, MA 02062 T: (781) 352-8491 F: (203) 880-9695	
Drawn By: AWC	
Checked By: CJB	
Approved By: KMS	
Project #: 22113201	
Plan Date: 04/18/23	
Scale: 1" = 60'	
Project:	
PROPOSED SOLAR PHOTOVOLTAIC ARRAY 428 BETHMOUR ROAD BETHANY, CONNECTICUT	
Sheet Title: OVERALL SITE LAYOUT PLAN	Sheet #: 2.10



PLANTING SCHEDULE

KEY	QTY	BOTANICAL NAME	COMMON NAME	ROOT	SIZE	COMMENTS
TREES						
AC	10	ABIES CONCOLOR	CONCOLOR / WHITE FIR	B&B	7'-8' HT	15' O.C.
PG	23	PICEA GLAUCA	WHITE SPRUCE	B&B	7'-8' HT	15' O.C.
PP	22	PICEA PUNGENS	COLORADO BLUE SPRUCE	B&B	7'-8' HT	15' O.C.
TO	34	THUJA OCCIDENTALIS 'ELEGANTISSIMA'	AMERICAN ARBORVITAE	B&B	7'-8' HT	8' O.C.
SEED MIXES						
NEW ENGLAND EROSION CONTROL/RESTORATION NO MOW MIX (NEW ENGLAND WETLAND PLANTS, INC.)						
APPLICATION RATE: 1 LBS/2,500 S.F.						
ERNMX-147						
APPLICATION RATE: 42 LBS/ACRE WITH A COVER CROP OF ANNUAL RYEGRASS AT 12 LBS/ACRE						
ERNMX-610						
APPLICATION RATE: 30 LBS/ACRE OF A COVER CROP. FOR A COVER CROP USE EITHER GRAIN OATS (JAN 1 TO JUL 31) OR GRAIN RYE (AUG 1 TO DEC 31)						

GENERAL NOTES

- THESE PLANS ARE FOR PERMITTING PURPOSES ONLY AND ARE NOT FOR CONSTRUCTION. NO CONSTRUCTION OR DEMOLITION SHALL BEGIN UNTIL FINAL APPROVAL OF THIS PLAN IS GRANTED.
- ALL PROPOSED SITE WORK TO BE COMPLETED IN ACCORDANCE WITH ALL PERMITS, APPROVALS AND CONDITIONS OF APPROVALS ISSUED BY LOCAL, STATE AND/OR FEDERAL REVIEWING AGENCIES.
- EXISTING BOUNDARY, TOPOGRAPHY AND SITE CONDITIONS INFORMATION TAKEN FROM A PLAN ENTITLED "EXISTING CONDITIONS MAP, 428 BETHMOUR ROAD, BETHANY, CONNECTICUT, EX-1," DATED JANUARY 05, 2022, SCALE: 1"=80', BY BL COMPANIES.
- REFER TO THE EXISTING CONDITIONS MAP FOR THE ENTIRE PROPERTY BOUNDARY AND EXISTING CONDITIONS INFORMATION. THE PLAN HEREON DEPICTS A PORTION OF THE PROPERTY IN WHICH THE SITE WORK IS BEING PROPOSED.
- THE SUBJECT PARCEL CONSISTS OF A TOTAL AREA OF APPROXIMATELY 21.23+ ACRES, LOCATED IN THE RESIDENTIAL-65 (R-65) DISTRICT IN THE TOWN OF BETHANY, CONNECTICUT.
- WETLAND BOUNDARY DETERMINED AND LOCATED BY FIELD SURVEY BY BL COMPANIES ON 01/05/2022.
- PORTIONS OF THE SITE ARE LOCATED WITHIN FEMA DESIGNATED FLOOD HAZARD AREA "X" AS DEPICTED ON F.I.R.M. MAP NUMBER 09090C0267H, PANEL 267 OF 635, WITH EFFECTIVE DATE DECEMBER 17, 2010.
- ALL CONSTRUCTION SHALL COMPLY WITH THE TOWN OF BETHANY, CONNECTICUT DEEP, AND CONNECTICUT DEPARTMENT OF TRANSPORTATION STANDARDS AND SPECIFICATIONS IN THE ABOVE REFERENCED INCREASING HIERARCHY. IF SPECIFICATIONS ARE IN CONFLICT, THE MORE STRINGENT SPECIFICATION SHALL APPLY. ALL CONSTRUCTION SHALL BE PERFORMED IN ACCORDANCE WITH ALL APPLICABLE OSHA, FEDERAL, STATE AND LOCAL REGULATIONS.
- PRIOR TO DEMOLITION OR CONSTRUCTION, THE CONTRACTOR SHALL CONTACT "CALL BEFORE YOU DIG" 72 HOURS BEFORE THE COMMENCEMENT OF WORK AT (800) 922-4455 AND VERIFY ALL UTILITY AND STORM DRAINAGE SYSTEM LOCATIONS. INFORMATION ON EXISTING UTILITIES AND STORM DRAINAGE SYSTEMS HAS BEEN COMPILED FROM AVAILABLE INFORMATION INCLUDING UTILITY PROVIDER AND MUNICIPAL RECORD MAPS AND/OR FIELD SURVEY AND IS NOT GUARANTEED CORRECT OR COMPLETE. UTILITIES AND STORM DRAINAGE SYSTEMS ARE SHOWN TO ALERT THE CONTRACTOR TO THEIR PRESENCE AND THE CONTRACTOR IS SOLELY RESPONSIBLE FOR DETERMINING ACTUAL LOCATIONS AND ELEVATIONS OF ALL UTILITIES AND STORM DRAINAGE SYSTEMS INCLUDING SERVICES.
- SHOULD ANY UNCHARTED OR INCORRECTLY CHARTED, EXISTING PIPING OR OTHER UTILITY BE UNCOVERED DURING EXCAVATION, CONSULT THE CIVIL ENGINEER IMMEDIATELY FOR DIRECTIONS BEFORE PROCEEDING FURTHER WITH WORK IN THIS AREA.
- THE OWNER IS RESPONSIBLE FOR OBTAINING ALL NECESSARY ZONING PERMITS REQUIRED BY GOVERNMENT AGENCIES PRIOR TO CONSTRUCTION. THE CONTRACTOR SHALL OBTAIN ALL LOCAL AND STATE PERMITS. THE CONTRACTOR SHALL POST ALL BONDS, PAY ALL FEES, PROVIDE PROOF OF INSURANCE AND PROVIDE TRAFFIC CONTROLS NECESSARY FOR THIS PROJECT.
- THE CONTRACTOR SHALL RESTORE ANY DRAINAGE STRUCTURE, PIPE, UTILITY, PAVEMENT, CURBS, SIDEWALKS, LANDSCAPED AREAS OR SIGNAGE DISTURBED DURING CONSTRUCTION TO THEIR ORIGINAL CONDITION OR BETTER, AS APPROVED BY THE CIVIL ENGINEER OF RECORD. DURING CONSTRUCTION THE CONTRACTOR IS TO HAVE THE SITE MAINTAINED FREE OF ALL TRASH, LITTER, DEBRIS AND OVERGROWN VEGETATION.
- THE OWNER SHALL BE RESPONSIBLE FOR MAINTAINING THE SITE FREE OF ALL TRASH, LITTER, DEBRIS AND OVERGROWN VEGETATION THROUGHOUT CONSTRUCTION.
- ALTERNATIVE METHODS AND PRODUCTS OTHER THAN THOSE SPECIFIED MAY BE USED IF REVIEWED AND APPROVED BY THE OWNER, CIVIL ENGINEER, AND REGULATORY AGENCY PRIOR TO INSTALLATION DURING THE BIDDING PROCESS.

SOLAR ARRAY SYSTEM INFORMATION

	TOTAL
SIZE DC	1.399 MW
SIZE AC	0.999 MW
INVERTER LOAD RATIO	1.40
MODULE TYPE	TRACKING TRINASOLAR TSM-540-DEG19C.20 (540W)
MODULE QUANTITY	2,590
INVERTER	SUNGROW SG125HV 125KW
INVERTER QUANTITY	8
UTILITY	EVERSOURCE



501 Main Street, Monroe, CT 06468 T: (203) 880-5455 F: (203) 880-9695
11 Vanderbilt Ave., Norwood, MA 02062 T: (781) 352-8491 F: (203) 880-9695

Drawn By: AWC

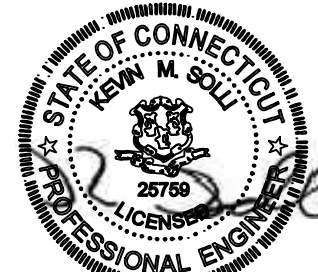
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Approved By: KMS

Project #: 22115201

Plan Date: 04/18/23

Scale: 1" = 40'



Kevin Solli, P.E.
CT 25759

Project:

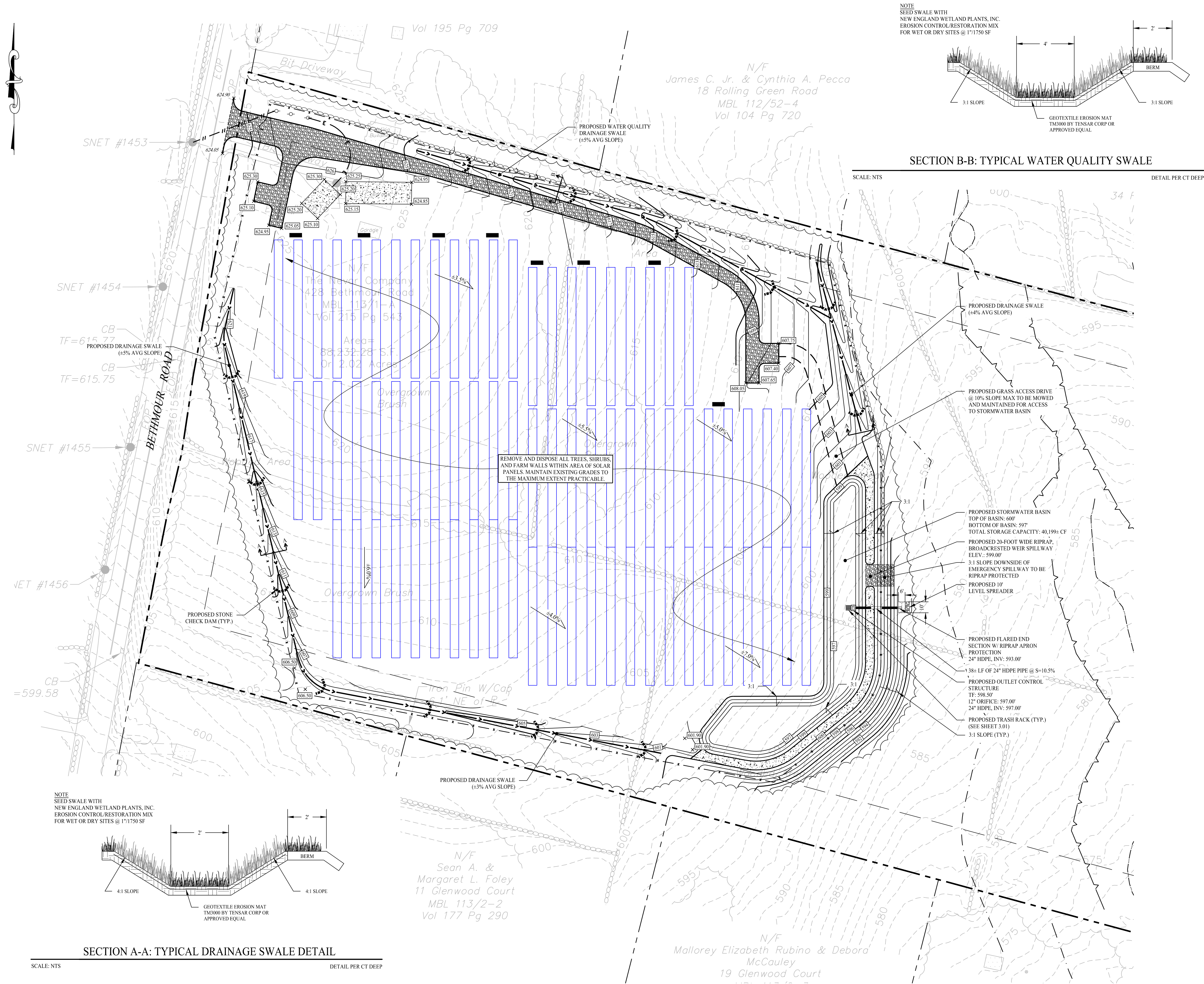
PROPOSED SOLAR PHOTOVOLTAIC ARRAY
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Sheet Title:

SITE LAYOUT PLAN

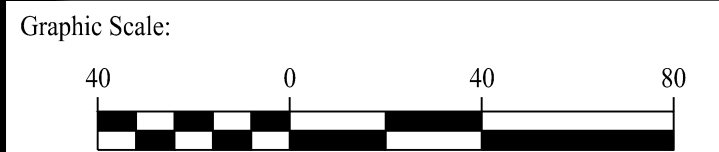
Sheet #:

2.11



1 09/19/23 Response to CSC Interrogatories

Rev. #:	Date	Description
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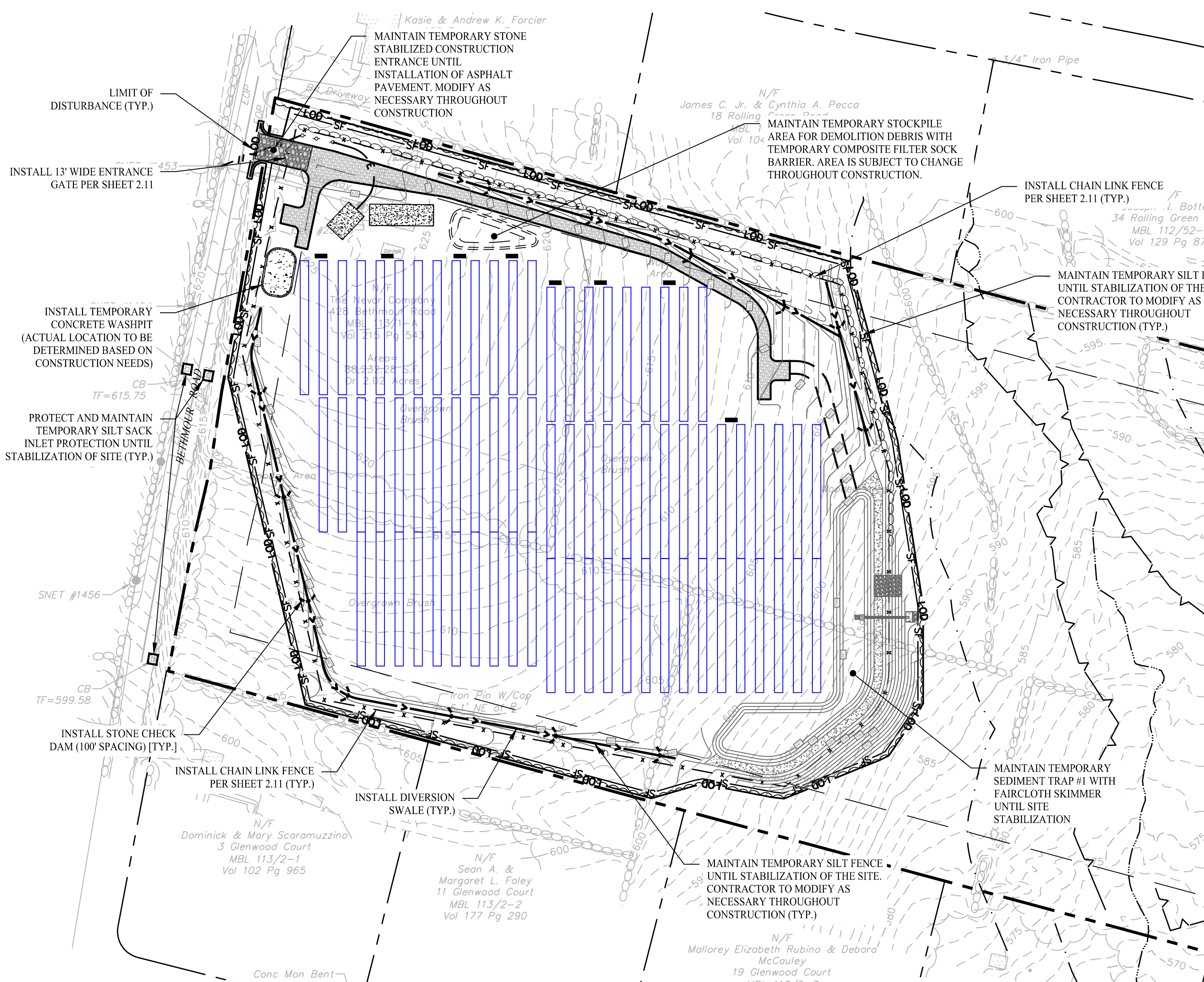
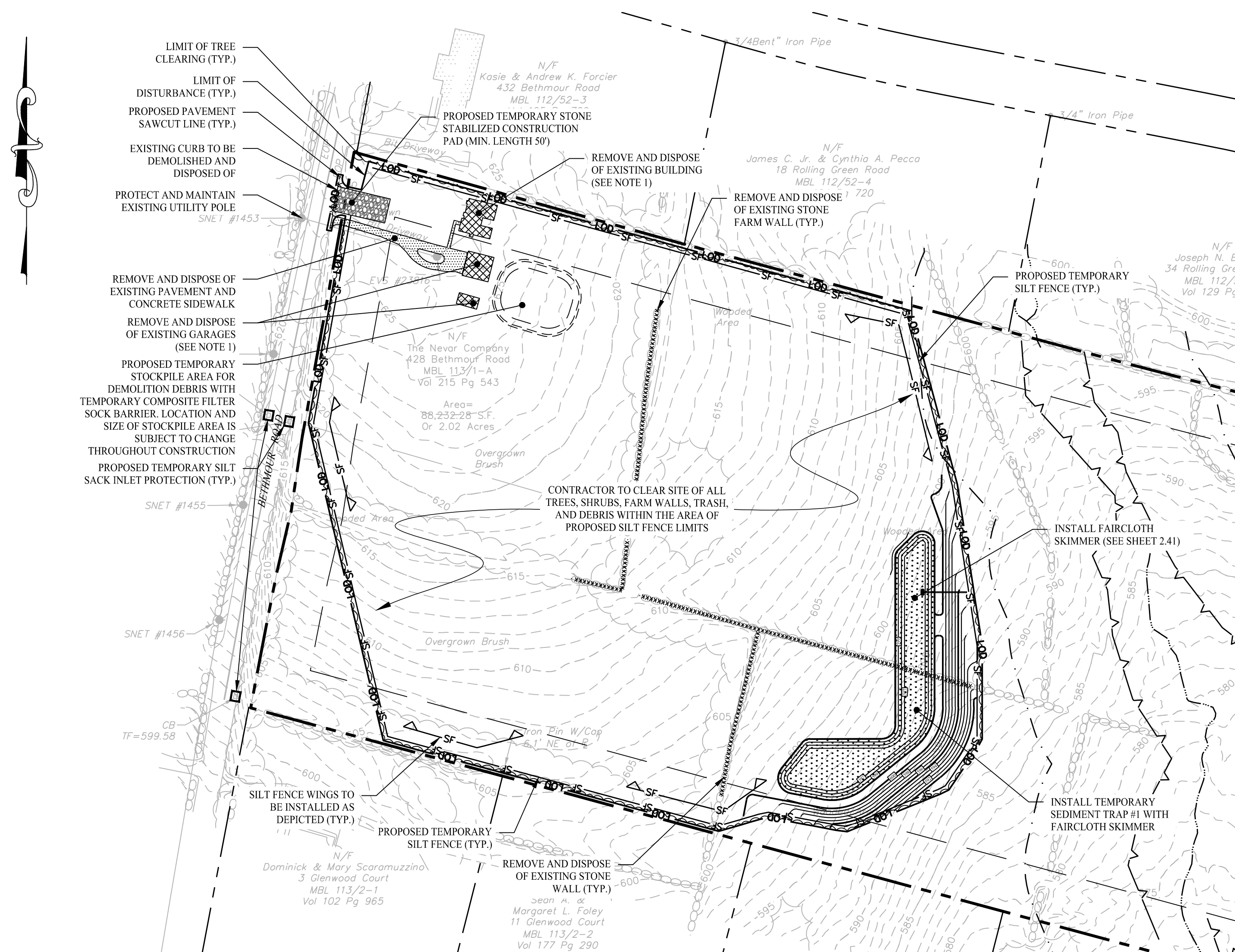
SOLLI ENGINEERING
501 Main Street, Monroe, CT 06468 T: (203) 880-5455 F: (203) 880-9695
11 Vanderbilt Ave, Norwood, MA 02062 T: (781) 352-8491 F: (203) 880-9695

Drawn By: AWC
Checked By: CJB
Approved By: KMS
Project #: 22112201
Plan Date: 04/18/23
Scale: 1" = 40'

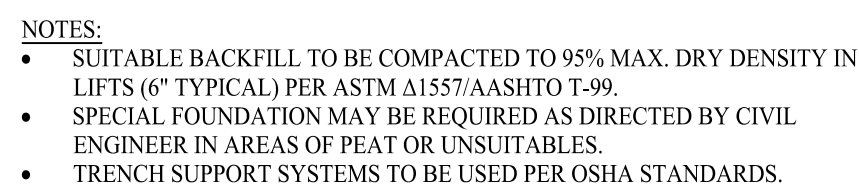
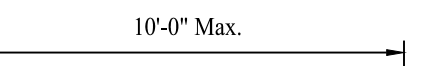
STATE OF CONNECTICUT
Professional Engineer
Kevin Solli, P.E.
CT 25759

PROPOSED SOLAR PHOTOVOLTAIC ARRAY
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Sheet Title: GRADING & DRAINAGE PLAN
Sheet #: 2.21



- NOTES:**
1. THE CONTRACTOR SHALL CONTACT CT CALL BEFORE YOU DIG (CByD) A MINIMUM OF 72 HOURS PRIOR TO BEGINNING CONSTRUCTION.
 2. TRANSITIONS BETWEEN TYPICAL ACCESS ROAD SECTIONS SHALL OCCUR OVER 50 FEET. (TYPICAL)



Graphic Scale



Sheet Title

Sheet #

3.01

ATTACHMENT B

Environmental Assessment



Environmental Assessment

Proposed Solar Photovoltaic Array 428 Bethmour Road Bethany, Connecticut

Prepared For
Tritec Americas, LLC
888 Prospect Street, Suite 200
La Jolla, California 92037

May 8, 2023
Revised: September 19, 2023



501 Main Street, Suite 2A
Monroe, CT 06468
Office: (203) 880-5455



11 Vanderbilt Avenue, Suite 240
Norwood, MA 02062
Office: (781) 352-8491

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Appendix E: FAA
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Appendix G: Geotechnical Report

1.0 INTRODUCTION

Solli Engineering (Solli) has prepared this Environmental Assessment (EA) on behalf of TRITEC Americas, LLC. (the Petitioner) for the proposed 0.99 megawatt (MW) solar photovoltaic array located on a portion of the property of 428 Bethmour Road in Bethany, Connecticut. The EA is included as an exhibit to the submission to the Connecticut Siting Council of a petition for declaratory ruling that no Certificate of Environmental Compatibility and Public Need is required for the construction, maintenance, and operation of the proposed solar photovoltaic array.

2.0 PROJECT DESCRIPTION

2.1 EXISTING SITE CONDITIONS

The project area is located on the property of 428 Bethmour Road in Bethany, Connecticut, which consists of two parcels totaling $21.22 \pm$ acres. The project area is situated at the western portion of the property, adjacent to Bethmour Road, and consists of approximately $7.4 \pm$ acres of land. The project area is currently improved with a residential building and associated garages, driveway, lawn area, wooded area, and stone farm walls.

Elevations within the project area range from approximately 585 feet at the southeastern corner of the project area to approximately 626 feet at the northwestern corner of the project area along Bethmour Road. Slopes range from 2.5% in the northwest corner of the property, near Bethmour Road, to 40% in the southwest corner of the project area.

2.2 PROPOSED DEVELOPMENT

The proposed solar photovoltaic array will consist of approximately 2,590 TrinaSolar TSM-DEG19C20 540W modules, 8 Sungrow SG125HV 125kW inverters, one 2,000 kVA transformer, and one service interconnection line. The system will consist of a ground-mounted, single-axis tracking system. A gravel access driveway is proposed to access the proposed array, and the development will be surrounded by a 7-ft tall chain link fence to provide adequate security and screening. Several utility poles are proposed on-site to provide overhead electrical service which will provide interconnection to the existing Eversource distribution system on Bethmour Road. The project area will cover approximately $7.4 \pm$ acres of the property.

2.2.1 ACCESS

The project area will be accessed from Bethmour Road via a gravel driveway which covers a total distance of approximately 600 feet. The proposed driveway is located approximately 1,000 feet south of the intersection of Bethmour Road with Pole Hill Road. The driveway will provide access to the proposed array and will generate minimal traffic, for the primary use of operation and maintenance of the photovoltaic array. A 26-ft wide entrance gate is proposed at the entrance to the site on Bethmour Road.

2.2.2 PUBLIC HEALTH AND SAFETY

The proposed development has been designed to meet all applicable local, state, national and industrial health and safety standards related to electric power generation. The proposed solar photovoltaic array will not consume any raw materials, will not produce any by-products and will be unstaffed under normal operating conditions.

A 7-ft tall chain link fence is proposed to surround the development, and a 26-ft wide gate is proposed at the entrance to the project area and will limit access to authorized personnel only. Town emergency

response personnel will have access to the project area via a Knox padlock. The photovoltaic array will have the ability to be de-energized remotely in case of an emergency.

2.2.3 LAND USE PLAN

The solar photovoltaic array has been designed in accordance with state and federal policies and will support the State of Connecticut's energy goals by constructing a renewable energy resource with no substantial adverse environmental impact.

Although the Town of Bethany currently does not have any land use requirements related to solar photovoltaic arrays, the development was designed to meet the Town's land use regulations to the maximum extent practicable.

The project area is located within the Residential Zone (R-65) and the photovoltaic array has been designed to have a minimum setback of 50 feet from all abutting residential properties. The nearest residential property to the north of the array is 18 Rolling Green Road, located approximately 63 feet from the nearest solar panel. The nearest residential property to the east of the array is 20 Split Rock Road, located approximately 1072 feet from the nearest solar panel. The nearest residential property to the south of the array is 3 Glenwood Court, located approximately 50 feet from the nearest solar panel. The nearest residential property to the west of the array is 419 Bethmour Road, located approximately 103 feet from the nearest solar panel.

The Petitioner believes that this project will benefit the local community by improving electrical service for existing and future development with the availability of a local, renewable energy source.

2.2.4 STORMWATER MANAGEMENT PLAN

The project will provide approximately 12,600± square feet of impervious/gravel area, an increase in overall impervious surfaces compared to existing conditions. The proposed stormwater conveyance system consists of drainage swales and a stormwater basin. The drainage swale to the north of the proposed access drive will treat and attenuate the Water Quality Volume to effectively clean the stormwater runoff prior to discharging into the existing wetlands on-site.

The proposed stormwater management system has been designed to be in compliance with the *2004 Connecticut Stormwater Quality Manual*, CT DEEP Appendix I of the Stormwater General Permit, and the *2002 Connecticut Guidelines for Soil Erosion and Sediment Control* while taking prevailing site conditions and practical considerations into account. Please refer to Section 3.3.3 for more information regarding stormwater management on site.

2.2.5 LANDSCAPE PLAN

Vegetation buffers are proposed within the project area to shield the proposed solar photovoltaic array from neighboring properties. Plant materials consists of a mix of evergreen species to provide year-round screening on the north, west and south portions of the property. An existing wetland provides a buffer on the east side of the property.

3.0 ENVIRONMENTAL CONDITIONS

This section provides a summary of the existing environmental conditions in and around the project area, as well as the potential impacts on the environment from the proposed photovoltaic array development. The results discussed in this section demonstrate that the development complies with CT DEEP air and water quality standards and will have no adverse effect on the existing environment and ecology.

3.1 AIR QUALITY

The nature of solar energy generating facilities results in a condition where no air emissions are generated during the operations of the facility. Therefore, this development will have no adverse effect on air quality and will not require a permit.

During construction, temporary mobile source emissions may occur due to the presence of construction vehicles and equipment. Any of these potential air emissions that occur during the construction of the solar photovoltaic array can be considered de minimis. These emissions will be mitigated using measures such as limited idling times of equipment, regular maintenance of all vehicles and equipment, and watering/spraying of vehicles and equipment to minimize dust and particulate releases. Additionally, all equipment will meet the latest standards for diesel emissions as prescribed by the United States Environmental Protection Agency.

3.2 WATER RESOURCES

Wetlands and watercourses onsite were field delineated by BL Companies in October 2021. William Kenny Associates (WKA) conducted additional field investigations including our inventory and assessment of onsite wetland and watercourse conditions on February 27, 2023. Based on our investigations, we concur with BL Companies that there are two wetland and watercourse systems on the property, and we concur with the locations of the wetland boundaries that BL Companies field marked (flagged). These wetland areas are located to the east of the project area, approximately 100 feet away at its closest point. No wetlands or resource areas were found within the project area limits.

3.2.1 WETLANDS AND WATERCOURSES

Central Wetland & Watercourse

The first wetland and watercourse system, located in the central portion of the property, consists of an intermittent watercourse, extending and flowing north to south and bordering woodland wetland habitat. This wetland is located approximately 100 feet away from the northeastern corner of the project area and tapers away approximately 160 feet from the southeastern corner of the project area. The existing watercourse is located within this wetland and the closest point from the project area to the watercourse is approximately 163 feet away. The principal source of hydrology for this wetland and watercourse system is groundwater discharge and surface water flow. The intermittent watercourse originates from a hillside seep in the northern portion of the system and follows the topographic gradient of the hillside flowing offsite to the south. Soils within this system consist of poorly drained sandy loams formed from lodgement glacial till with a shallow hardpan that perches groundwater and causes seeps. At the time of WKA's investigation, the watercourse had one to two inches of water flowing through it and its streambed consisted of moss-covered cobbles and boulders. The woodland wetland bordering the intermittent watercourse consists of primarily the same vegetation found in the adjacent young woodland uplands. The canopy of the wetland is dominated by red maple and includes some pignut hickory and dead or dying green ash trees. The understory is dominated by black birch and includes yellow birch, black tupelo, and American hornbeam. The shrub strata of the woodland wetland is dominated by invasive Japanese barberry and multiflora rose shrubs and native spicebush shrubs and also includes some invasive burning bush shrubs along the fringes of the system. Groundcovers within the wetland include skunk cabbage and Christmas fern. The hydrogeomorphic classification of this wetland and watercourse system is gently sloping and the USFWS classification for this system is Palustrine, Forested, Broad-Leaved Deciduous (PFO1).

Eastern Wetland & Watercourse (Pine Brook)

The second wetland and watercourse system, located in the eastern portion of the property, consists of a perennial watercourse, Pine Brook, extending and flowing north to south, and bordering woodland wetland habitat. This wetland is approximately 770 feet from the project area, and the watercourse associated with this wetlands is approximately 850 feet from the project area. The principal source of hydrology for this

wetland and watercourse system is surface water conveyed by Pine Brook. Pine Brook originates from a large swamp approximately 1,800 feet north of the project site and eventually connects to Bladens River approximately 1.75 miles southwest of the project site. Soils within this system consist of poorly drained sandy loams formed from lodgement glacial till with a shallow hardpan that perches groundwater and causes seeps. At the time of WKA's investigation, Pine Brook, which has a stream width of approximately ten feet throughout the site, had a water depth of approximately three to four inches and a streambed consisting of moss-covered cobbles and boulders. The woodland wetland bordering the watercourse consists of primarily the same vegetation found in the adjacent mature woodland uplands. The canopy is comprised of primarily red maples and the understory is comprised primarily of yellow birch trees. Invasive Japanese barberry and multiflora rose shrubs and native spicebush shrubs are present and groundcovers consist of skunk cabbage and Christmas fern. The hydrogeomorphic classification of this wetland and watercourse system is riverine and the USFWS classification for this system is Riverine, Lower Perennial, Unconsolidated Bottom, Cobble-Gravel (RIUB1).

3.2.2 VERNAL POOL

Based on the field investigation performed by BL Companies, there was no evidence of the existence of any vernal pools within the project area or on the property of 428 Bethmour Road.

3.2.3 WETLAND IMPACTS

Land development has the potential to cause direct and indirect impacts to inland wetlands and watercourses in the short- and long-term from activities such as vegetation clearing, soil filling, soil excavation and/or pollution of stormwater. The proposed site improvements are designed to avoid indirect impacts in the short and long-term through the incorporation of various best management practices (BMPs) such as soil erosion and sediment control measures and stormwater management measures (further discussed in Section 3.3.3). No activities are proposed within wetlands and watercourses, and, as such, no direct impacts will occur.

Table 1: Wetlands Impacts Table

Wetlands Impacts		
Direct Impacts to Wetland 1	0 Acres	
Direct Impacts to Wetland 2	0 Acres	
Direct Impacts to Upland Review Area of Wetland 1	±0.02 Acres (Tree Clearing)	
Direct Impacts to Upland Review Area of Wetland 2	0 Acres	
Limit of Disturbance to Wetland	Western Portion	Eastern Portion
Wetland 1	0 Feet	0 Feet
Wetland 2	0 Feet	0 Feet

3.2.4 FLOODPLAIN AREAS

WKA reviewed the most recent available mapping from the Federal Emergency Management Agency (FEMA) in regard to the presence of floodplain or flood prone areas onsite. According to the FEMA Flood Map Service Center (MSC), flood map number 09009C0267H, effective on 12/17/2010, the subject project area falls within "Zone X" as defined by FEMA. Zone X is defined as "are the areas between the limits of the base flood and the 0.2-percent-annual-chance (or 500-year) flood". This indicates that the project area is not within a flood zone and requires no special considerations relative to flooding for its implementation. For more information regarding the FEMA Floodplain Boundaries refer to Figure 3, FEMA Flood Map.

3.3 WATER QUALITY

The proposed solar array facility will have no potable water uses or sanitary discharges due to the unmanned nature of the facility. The proposed development will result in an increase in impervious cover within the project area. As such, the development includes a stormwater management plan to mitigate the increase in stormwater runoff resulting from the increase in impervious cover.

3.3.1 GROUNDWATER

WKA reviewed the CT DEEP Water Quality Classifications Map, dated October 2018, in order to assess the quality of ground and surface water within the project area. The map classifies that the project area falls within an area classified by 'GA' groundwater quality. 'GA' is defined as "existing private and potential public or private supplies of water suitable for drinking without treatment and baseflow for hydraulically-connected surface water bodies." For more information regarding the water classifications refer to Figure 4, Water Quality Classification Map.

According to the CT DEEP Public Water Supply Map, the project area does not fall within an aquifer protection area. It is labeled as a private well parcel; however, the nature of the project as a solar farm dictates that no potable water uses are required.

Overall, the project will have no direct adverse environmental impact on groundwater quality. Inadvertent adverse impacts will be mitigated via stormwater management BMPs (further discussed in Section 3.3.3).

3.3.2 SURFACE WATER

The project area is situated within the Pine Brook Local Drainage Basin (6919-01) and the Bladens River Subregional Drainage Basin (6919). These drainage basins are part of the larger Naugatuck Regional Drainage Basin (69) and Housatonic Major Drainage Basin (6). Pine Brook is characterized by the CT DEEP as a first order stream with 'class 1 stream flow' which means that it is a free-flowing stream. The water quality of Pine Brook is listed as 'class A' surface water quality. Class A surface water quality is defined as "Class A designated uses are habitat for fish and other aquatic life and wildlife; potential drinking water supplies; recreation; navigation; and water supply for industry and agriculture".

According to the CT DEEP Public Water Supply Map, the project area does not fall within a drinking water watershed. Pine Brook serves as habitat for fish and other aquatic wildlife and flora; however, the onsite portion does not appear to serve as aquatic wildlife or flora habitat. Pine Brook does not sustain a trout population according to the CT DEEP Connecticut Trout Stocking Map nor does it have a cold-water habitat according to the CT DEEP Cold Water Habitat Map. For more information, please refer to Figure 5, Public Supply Watershed Map.

3.3.3 STORMWATER MANAGEMENT & EROSION CONTROL

In the short-term, wetlands can be indirectly impacted from sediment laden stormwater from the proposed construction activities. All development is proposed outside of wetlands and watercourses and their 100-foot upland review areas. Nevertheless, the project proposes the installation of soil erosion and sedimentation controls before construction and the maintenance of these controls throughout construction to prevent adverse indirect impacts to inland wetlands and watercourses from soil erosion and sedimentation. These controls are designed to comply with standards set by the *2002 Connecticut Guidelines for Soil Erosion and Sediment Control* published by the CT DEP (the predecessor to the CT DEEP) to manage the land disturbance from the development and protect surface water features. Such controls include but are not limited to temporary silt fencing and construction fencing surrounding the perimeter of the work zone, an anti-tracking pad at the construction entrance, silt sack inlet protection in catch basins along the street and temporary sediment traps. The silt fencing proposed around the perimeter of the project area is to retain exposed sediment to the site, preventing its migration downslope to inland wetlands and watercourses. The reinforcement of the silt fencing with construction fencing is to deter access to the site by wildlife and civilians. The anti-tracking pad is proposed to prevent sediment from being tracked into the street. The silt sacks are proposed to prevent sediment that does manage to leave the site from impacting the adjacent storm sewer with sediment laden water. The temporary sediment trap is proposed to act as internal areas to store sediment laden stormwater runoff and allow for particulates to settle and stormwater to recharge into underlying soils. These control measures have been provided to

maximize protection to wetlands and watercourses and the monitoring and maintenance of all control measures are required to ensure efficacy throughout all phases of construction.

In the long-term, and if not properly mitigated, wetlands and watercourses can be indirectly adversely impacted by stormwater runoff that flows from buildings, pavement, and vegetated surfaces. The proposed project will not cause post-construction long-term adverse impacts from stormwater runoff due to the proposed stormwater management plan, which will mitigate changes to stormwater runoff resulting a proposed increase in impervious cover. A stormwater basin is proposed on the southeast portion of the project area, within the area of the young woodland habitat. Stormwater flowing to the basin will sheet flow across the array area and additional runoff from the project area will follow grass-lined swales proposed along the western, southern, and eastern sides of the solar array to mimic existing drainage patterns. The implementation and maintenance of this BMP will result in decreased peak flows up to the 100-year storm event.

3.4 HABITAT & WILDLIFE

Three habitat communities are present throughout the project area and surrounding areas. They include shrubland, woodland and wetlands and watercourses. These habitat types are further discussed in Sections 3.4.1 and 3.4.2. Wildlife species at or that can utilize the project area are species common to suburban residential landscapes. These species are further discussed in Section 3.4.3. For more information about the habitat makeup of the project area, please refer to Figure 6, Habitat Cover Map.

3.4.1 HABITAT TYPES

Shrubland

The western portion of the project area consists of shrubland habitat. This habitat previously was a grassland habitat but has significantly succeeded into a shrubland habitat over time. Several recent cut paths extend through the shrubland. The shrubland extends from Bethmour Road to an old stone farm wall in the eastern portion of the project area. Woodland habitat is east of the wall. The existing dwelling, detached garage, storage shed, and asphalt driveway are present in the northwestern portion of this habitat. The shrubland is dominated primarily by invasive autumn olive and multiflora rose shrubs. Some native eastern red cedar and sassafras saplings are interspersed throughout. Some canopy trees are present and include pole-to-saw timber-sized American elm, shagbark hickory and dead or dying white ash. Trees and shrubs are also entwined by invasive oriental bittersweet vines. The groundcover is dominated by various species of grasses and forbs including goldenrod, switchgrass, and mullein. Soils within this portion of the project area are primarily well drained sandy loams formed from lodgment glacial till. To make way for the solar array, the majority of this habitat, except for a small portion in the southwestern portion of the site, is proposed to be eliminated. Please see Table 2 for the total acreage of habitat alteration.

Woodland

The majority of the project area consists of woodland habitat. The woodland stretches over the central and eastern portions of the project area and is comprised of a younger woodland in its central reaches and an older more mature woodland in its eastern reaches. The younger woodland stretches from an old stone farm wall that separates it from the shrubland habitat to the west to the central wetland and watercourse that bisects the center of the property. Other old stone farm walls cross the woodland, sectioning out areas that likely were pasture historically. The younger woodland is dominated by a canopy of pole-to-saw timber-sized red maple trees, some of which along the border with the shrubland habitat, were tapped for their sap. Other common canopy trees include shagbark hickory, red oak, and black oak. Understory trees include black birch, black cherry, black tupelo, American beech, and American hornbeam. Many of the canopy trees appeared topped by storm damage and various tip-ups were present throughout the younger woodland habitat. The younger portion of the woodland is dominated by invasive Japanese barberry and multiflora shrubs and native spicebush shrubs which form thickets. These shrub thickets are entwined with invasive

oriental bittersweet vines and native grape vines, greenbrier vines and/or poison ivy vines. Groundcovers consist mainly of goldenrod species along the fringes of the habitat.

The older, eastern woodland differs from its younger, central counterpart with a shift in dominant canopy species and a much barer ground layer due to heavier shading. This portion of the woodland stretches from the eastern edge of the central wetland and watercourse system to Pine Brook along the eastern property boundary. Large tulip poplars and pin oaks are the dominant canopy trees in the mature eastern woodland with other species such as sugar maple and white oak also present. Shrubs are sparser in this portion of the woodland and only a few invasive Japanese barberry and native high bush blueberry are present. Groundcovers also are sparse and primarily consist of Christmas fern. Soils within these portions of the project site consist of well drained to moderately well drained sandy loams formed from lodgment glacial till. A majority of the younger, central portion of the woodland is proposed to be eliminated by the proposed project. The mature eastern portion of the woodland will remain and not be disturbed. Please see Table 2 for the total acreage of habitat alteration.

Wetlands & Watercourses

Two wetland and watercourse areas were identified and evaluated. Further details in regard to the ecological communities of these wetlands and watercourses are described below in Section 3.2.1. Overall, the wetlands and watercourses are not proposed to be impacted by the project. Please see Table 2 for the total acreage of habitat alteration.

Table 2: Habitat Area Table

Habitat Type	Total Area On Property (±Acres)	Project Area (±Acres)
Shrubland	4.7	4.2
Woodland	12.8	3.2
Wetlands	3.7	0

3.4.2 CORE FOREST DETERMINATION

The Connecticut Department of Energy and the Environment (CT DEEP) defines ‘core forests’ as “forests surrounded by other forests, and in Connecticut, it has been defined as forest features that are relatively far (more than 300 feet) from the forest-nonforest boundary. Core forests provide habitat for many species of wildlife that cannot tolerate significant disturbance. The loss of core forest cover diminishes water purification and habitat values, and could result in heavier runoff, which might lead to poorer water quality and impaired habitat.”

The CT DEEP 2020 Connecticut Forest Plan Priority Areas Map (Appendix A, Figure 11) was reviewed as well as core forest mapping provided by the Housatonic Valley Association. According to the CT DEEP map, approximately 3.27 acres of the property is considered Small Core Forest. This Small Core Forest is fragmented throughout various properties within surrounding neighborhoods and throughout Bethany. The project is only anticipated to impact approximately 0.5 acres of this Small Core Forest within the younger woodland habitat discussed in Section 3.4.1. The closest Large Core Forest, according to the CT DEEP map and the Housatonic Valley Association’s map is approximately 2,800 feet to the west of the project area and consists of a 730-acre forest.

3.4.3 WILDLIFE

The project will eliminate all but a small portion of the shrubland habitat and a portion of the younger central woodland habitat. These habitats support various wildlife including mammalian, amphibian, reptilian and avian species. The shrubland habitat serves small mammalian species, such as woodchuck, fox, skunk, eastern cottontail, opossum, raccoon and voles, moles, and mice, offering them protection from raptor species and larger mammalian predators as well as nesting within the safe confines of the shrub thickets. As mentioned, avian species such as birds of prey will utilize the shrubland as hunting ground for

small game, perching in the few canopy trees within this community or along the woodland at its edges. Other avian species such as warblers and sparrows will also use the shrub thickets for nesting and cover.

The young woodland habitat serves the aforementioned small mammalian species that may utilize the shrubland as well as other mammalian species such as grey squirrel, eastern chipmunk, white-tailed deer, bobcats, and coyotes. Evidence of deer and possible coyote scat was identified within this ecosystem at the time of our investigation. The woodland provides foraging opportunities for these species in the forms on nuts and seeds, plants or in the terms of larger predators, small game. The woodland, being adjacent to wetland and watercourse systems may serve as the terrestrial habitat for wood frogs and spring peepers. It is also likely common reptile species such as eastern garter snakes utilize both the woodland and adjacent shrubland. Avian species such as turkeys are likely to forage in the ground layer of the woodland while songbirds likely perch in the canopy above. Due to the central woodland's young age and its proximity to the shrubland and neighboring properties, it can be assumed that the woodland serves as habitat for more edge tolerant species that are tolerant of habitat fragmentation and human disturbance. The older eastern woodland likely serves the same habitat functions as the younger central woodland due to its proximity to the younger central woodland, small size, and adjacency to edge habitat (i.e., surrounding residential properties). It is unlikely species common to core forests reside within the project area, even in the eastern woodland, due to the forest being isolated from a larger tract.

The adjacent wetlands and watercourses serve as habitat for all aforementioned species and provide them a source of drinking water. The adjacent wetlands and watercourses do not function as vernal pools and no vernal pool areas were identified adjacent to the project area (within 100 feet) via observations made from the project area, public right-of-ways, and information gathered from publicly available sources (i.e., town maps, topographic maps, aerial imagery, etc.). The central watercourse likely does not function as habitat for finfish due to its shallow, intermittent nature, but the eastern watercourse, Pine Brook, potentially serves as finfish habitat. According to the CT DEEP Atlas of the Crayfish of Connecticut, the nearest location where crayfish have been identified is approximately 1.6 miles southwest of the project site in the Bladens River. The species identified in this river is not a State listed species. Additionally, Pine Brook likely does not serve as habitat for freshwater mussels due to its narrow width and low flow. Please see Section 3.2.1 for information regarding Wetland and Watercourse conditions and 3.3.2 for more information regarding Surface Water conditions.

Due to the proposed project, the abundance of wildlife species will decrease slightly but not the diversity of wildlife that utilize the property under current conditions. Additionally, the development is not anticipated to affect endangered, threatened or species of special concern, as, according to State and Federal resources and onsite field investigations, none of these species inhabit the project area (see Sections 3.5, 3.5.1 and 3.5.2). Of the species that inhabit the project area, all are common, and habitat exists for them to use in other areas of Bethany and beyond. As such, the project will not have significant adverse impacts to wildlife.

3.5 RARE SPECIES

WKA reviewed publicly available state and federal information to determine whether listed species and/or critical habitats were present onsite or adjacent to the project area. WKA also investigated for the potential for listed species and/or critical habitat (including the presence of vernal pools) to be present within the project area and surrounding onsite areas and found that no listed species or critical habitat were present within these areas.

3.5.1 NATURAL DIVERSITY DATA BASE

The CT DEEP Natural Diversity Data Base (NDDB) is a collection of maps that show the approximate locations of state endangered, threatened, and special concern species and important natural communities in Connecticut. The locations shown on the maps are based on information collected over the years by

DEEP personnel and others. The maps are intended to serve as a pre-screening tool for preventing potential impacts to listed species. Maps are generated for each town. The map for the Town of Bethany is dated December 2022. The map indicates areas where listed species have been identified in a hatched buffer area and areas of critical habitat in green polygons. The hatched buffer areas are intentionally left inaccurate to protect protected species; therefore, if the project area fell within or near a buffer, a request for determination would have to be filed with the CT DEEP NDDDB for more accurate information and field work would need to occur to determine the presence or absence of these species onsite. According to the Town of Bethany NDDDB map, this project area does not fall within a hatched buffer area and is approximately 5,850 feet from the nearest area to the southeast of the site at Lake Chamberlain. As such, no request for determination was filed for the property. For more information, please refer to Figure 7, Natural Diversity Database Map.

3.5.2 USFWS CONSULTATION

The US Fish and Wildlife Service (USFWS) provides an online planning tool, its Information for Planning and Consultation (IPaC) system, allowing for project planners the ability to perform a regulatory review for protected species under the Endangered Species Act (ESA) that inhabit or potentially may inhabit their project sites. This resource is designed to provide a list of potential ESA-protected and/or candidate species, migratory bird species protected under the Migratory Bird Treaty Act and the Bald and Golden Eagle Protection Act, critical habitats, as well as the ability to consult whether a proposed project has the potential to result in “take” of listed species. “Take” refers to any means to “harass, harm, shoot, wound, kill, trap, capture or collect, or attempt to engage in any such conduct to threatened and endangered species”. In consulting this resource, projects can determine whether they are in compliance with the ESA and other federal acts. Solli Engineering filed on January 30, 2023, an IPaC review of the project site and received a letter report from the USFWS titled *“List of threatened and endangered species that may occur in your proposed project location or may be affected by your proposed project”*. This report is attached in Appendix C. The report specifies that one endangered species, one candidate species and eleven migratory bird species have the potential to be impacted by the proposed project. The endangered species is the Northern Long Eared Bat, the candidate species is the Monarch Butterfly and the migratory birds are listed in the report in the attached Appendix C.

The Northern Long Eared Bat is listed as endangered under the ESA. This species range encompasses the entirety of Connecticut. The CT DEEP has compiled a map of towns with known Northern Long Eared Bat and other bat hibernacula within the state, and no known hibernacula are located within the Town of Bethany. The nearest hibernacula according to the map is within the Town of North Branford, approximately 12 miles southwest of the project area. For more information regarding the locations of NLEB areas of concern, refer to Figure 7, Natural Diversity Database Map. Regardless, to stay in compliance with the ESA, the IPaC Consultation Package Builder (CPB) was utilized to assess whether the project would result in the “take” of Northern Long Eared Bats. The results of the CPB can be found in the attached report *“Consistency letter for the ‘Proposed Solar Photovoltaic Array’ project indicating that any take of the northern long-eared bat that may occur as a result of the Action is not prohibited under the ESA Section 4(d) rule adopted for this species at 50 CFR § 17.40(o)”* found in the attached Appendix C. The results of this report indicate that the project is not likely to result in the unauthorized “take” of Northern Long Eared Bats and therefore does not require a permit from the USFWS.

The monarch butterfly is a candidate species for protection under the ESA. Candidate species are “species which the USFWS has sufficient information to propose as endangered or threatened under the ESA, but for which their development of a proposed listing regulation is precluded by other higher priority listing activities”. As such, until they are proposed for listing, these species are not officially entitled to legal protection under the ESA, and they are not considered when making a determination as to “take”.

3.6 SOILS & GEOLOGY

The project grading is expected to generate a net import of approximately 830 cubic yards of material. Before any fill material is removed or used, the topsoil will be stripped and stockpiled for later seeding of disturbed areas. Any soil exposed due to construction will be treated according to the *2002 Connecticut Guidelines for Soil Erosion and Sediment Control*.

A Geotechnical Report for the property was prepared by GEI Consultants, Inc. in July 2022. The results of this report indicate that bedrock is present on-site, with depths ranging from approximately 4-9 feet below existing ground level. Based on the proposed grading of the project, it is not anticipated that bedrock will be encountered during construction. For more information regarding the results of this report, please refer to Appendix G of this report.

The following soils currently exist on-site and in surrounding areas:

1. Paxton and Montauk fine sandy loams, 3 to 8 percent slopes.
2. Paxton and Montauk fine sandy loams, 8 to 15 percent slopes.
3. Paxton and Montauk fine sandy loams, 15 to 24 percent slopes.
4. Ridgebury, Leicester and Whitman soils, 0 to 8 percent slopes, extremely stony.
5. Woodbridge fine sandy loam, 0 to 3 percent slopes.
6. Woodbridge fine sandy loam, 3 to 15 percent slopes, extremely stony.

For more information, refer to the map Figure 8, Prime Farmland Map.

3.6.1 PRIME FARMLAND SOILS

Solli Engineering has reviewed the listed soils in accordance with the Code of Federal Regulations (“CFR”) Title 7, part 657. Prime Farmland Soils are distinguishable based on soil type. These soils are to be identified under CFR Title 7, part 657 in order to know the extent and location of the best land for producing food, feed, fiber forage and oilseed crops. Upon review, the project contains prime farmland. For more information, refer to Figure 8, Prime Farmland Map.

Undeveloped forest and associated wetlands cover the majority of the property. Because the expected use of the project area will have a finite lifespan, the Petitioner proposes to use minimally intrusive methods during construction when possible. Grading will be limited by the use of solar panel tracker systems and construction of solar panels in existing areas where grades are similar to proposed conditions. There will be some excavation and regrading that takes place on prime farmland to install stormwater management basins and to properly develop the Site as a whole. In areas where Prime Farmland Soils are disturbed, the developer will remove the topsoil, segregate it from underlying horizons, and stockpile and spread it throughout the Site as necessary to re-establish vegetation growth.

When the solar panel facility reaches the end of its finite lifespan, the facility will be decommissioned. Upon this development, all areas disturbed by the facility will be top dressed with native soils and reseeded with the same (or approved equivalent) pollinator blend that exists within the area of the solar panel facility. These proposed design strategies will not materially affect the prime farmland. According to Public Act No. 17-218, “for a solar photovoltaic facility with a capacity of two or more megawatts, to be located on prime farmland or forestland... the Department of Agriculture represents, in writing, to the council that such project will not materially affect the status of such land as prime farmland or the Department of Energy and Environmental Protection represents, in writing, to the council that such project will not materially affect the status of such land as core forest.” The project is a 0.99 MW AC solar photovoltaic facility; therefore, a letter to the Council of the Department of Agriculture is not necessary in this exhibit.

3.7 HISTORIC & ARCHAEOLOGICAL RESOURCES

Archaeological Consulting Services LLC performed a Phase 1A cultural resources assessment survey on behalf of Solli Engineering and the Petitioner. Their report discloses that a property National Register of Historic Places does not exist within the Site. This conclusion was reached by means of a literature search for previously recorded cultural resources in the area, a review of historical maps and aerial imagery depicting the project area, and a pedestrian survey complete with photo documentation of the project area to determine archaeological sensitivity.

A portion of the project area has been identified as having a moderate-to-high probability of yielding intact archaeological sites and/or deposits due to its gentle slope, hardwood forestation, and soil makeup. Archaeological Consulting Services LLC recommends a Phase 1B survey be performed on the Site within 300 feet of Bethmour Road in advance of construction impacts. This survey would likely contain a number of standard-size shovel tests. For more information refer to the Phase 1A report in Appendix D, Cultural Resources.

3.8 SCENIC AND RECREATIONAL AREAS

All state and local roads and scenic areas are located over one mile away from the project. As such, no state road, local road, or scenic area will be affected physically or impaired visually by the project. No hiking trail exists on or near the project area. The closest open space is located at Amity Junior High School, approximately one-half mile northeast of the property. For more information regarding resources located within one mile of the site refer to Figure 9, Scenic & Recreation Map.

3.9 LIGHTING

Exterior lighting is not planned for the project. There may be on-site equipment that have small lights which will only be activated during maintenance.

3.10 FAA DETERMINATION

Solli Engineering has submitted required project information to the Federal Aviation Administration (FAA) for review. The FAA reviewed multiple sample points to determine whether a potential hazard exists for air navigation. Upon review, the FAA issued a Determination of No Hazard to Air Navigation for all points. A glare analysis is not required at this time. For more information see Appendix E, FAA Determinations.

3.11 VISIBILITY

There will be solar trackers a maximum of 6 ft off finished grade within the solar panel facility. All disturbed areas will be contained within a 7 ft chain link fence. Trees will be cleared on-site for the development of this project, however, the perimeter tree-line along the property lines will be preserved and maintained to the best of the developer's ability. Most neighbors in the vicinity of the property will not be able to view the solar panel facility due to tree coverage; however, the facility may be visible to one neighbor year-round from the site driveway (433 Bethmour Road). This visibility will be mitigated by the proposed chain-link double-swing gate as well as existing foliage on the neighbor's property. For more information refer to Figure 10, Proposed Conditions Viewshed Map.

The solar panel products are designed in such a way that they are not highly reflective. Because solar panels have tracking features, the panels will not reflect one direction for extended durations.

3.12 NOISE

The project area is currently occupied by a single-family house, with the majority of the Site containing undeveloped land.

Noise from the construction of the solar panel facility is exempted under Connecticut regulations for the control of noise. For more information refer to RCSA 22a-69-1.8(h). During construction, the increase in

noise will likely lead to a subsequent elevation in ambient sound levels in the immediate vicinity of the project area. Standard construction equipment will be used for the project, and the highest level of noise generated from this equipment – such as backhoes, bulldozers, cranes, and trucks – is expected to be approximately 88 dBA from the origin.

When construction ceases, noise from the solar panel facility will be minimal. The facility would be considered a class C emitter (industrial) to a class A emitter (residential) which regulates noise from exceeding 61 dBA during the day and 51 dBA at night. The maximum amount of noise will be generated during operation hours – the inverters will emit 61 decibels measured one meter from the inverter. Outside the perimeter of the project area, this noise will be negligible. The nearest residential use is 127 feet from proposed electrical equipment; the sound in decibels heard from this distance is 0.067 dbA after applying the inverse square law. Sound would further be reduced by vegetation buffers, rendering the noise negligible. For more information regarding the inverter product information refer to the specification sheets in Appendix F.

4.0 CONCLUSION

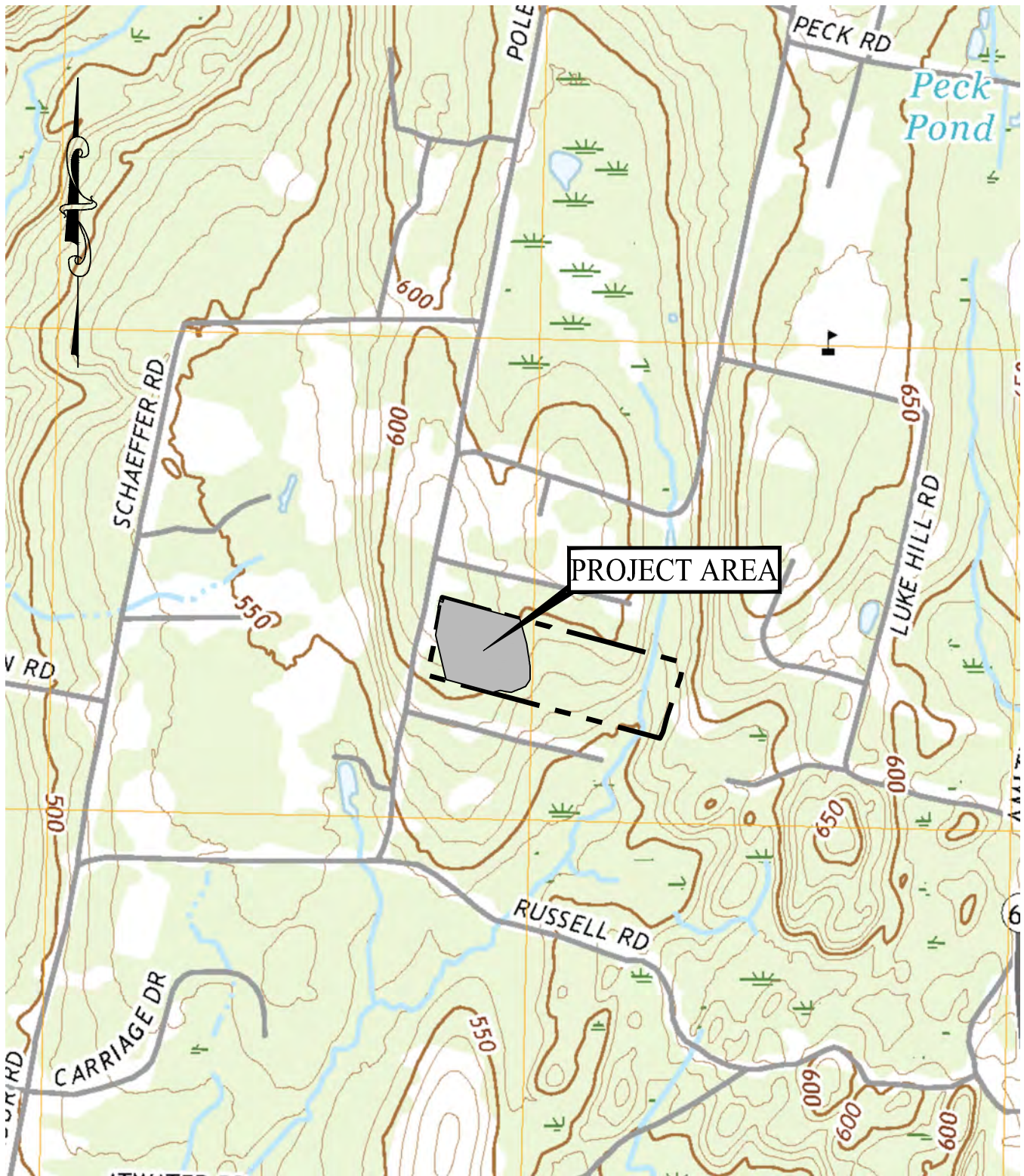
The solar panel facility proposed in this Environmental Assessment will not disproportionately affect the environment and ecology on the project area and surrounding properties, and will not disturb scenic, historic, cultural, or recreational resources within and nearby the project area. The project meets CT DEEP air and water quality standards. There will be minimal traffic to the project area once the facility is active; the only traffic generated will be for maintenance purposes. Wetlands, watercourses, and vernal pools will not be directly impacted by the facility; no vernal pools were found within the project area and property, and the limit of disturbance will be a minimum of 100 feet to all wetland boundaries. Erosion and sediment control will be utilized to protect these resources as mandated by the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control.

The project is designed to minimize impervious surfaces and regrading. Some excavation will be necessary while developing the project area and constructing stormwater management basins; however, this work will be minor and keep the character of the land intact. Stormwater runoff will be managed utilizing the proposed basin. The Petitioner will implement a SWPCP in accordance with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control. Provisions will be written into this SWPCP to account for the monitoring of the project through its construction phase, including the formation of erosion and sediment controls that will need to be observed.

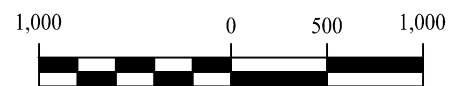
A portion of the project area contains Prime Farmland Soils. These soils will be protected via proactive measures such as limiting earthwork, regrading and other disturbance and arranging that all soils remain on the Site after the project is completed. When the facility reaches the end of its lifespan, all solar panels and associated equipment can be removed, and the site can be top-dressed and reseeded as necessary. The project area would be rehabilitated without issue.

Federal or state threatened, endangered or special concern species is expected to be negatively impacted by this development. State-list species have not been identified within the Site boundaries. The Northern Long-eared Bat was identified as a species that could occur within the Site boundaries, but upon review, the project should not produce negative consequences for the species such as incidental take.

Appendix A: Figures



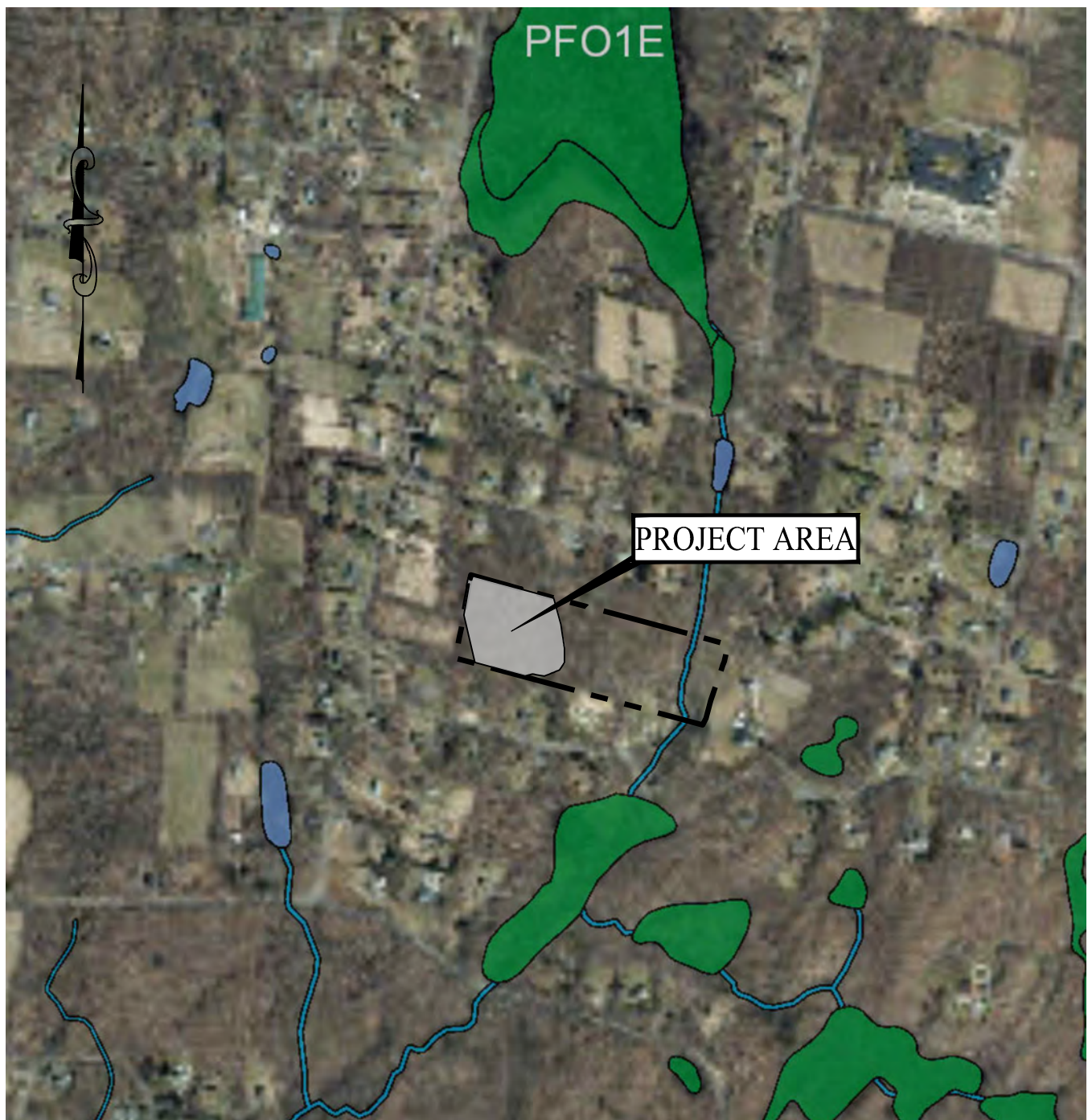
NOTE: BASE MAP INFORMATION TAKEN FROM USGS
 NAUGATUCK CONNECTICUT QUADRANGLE
 7.5-MINUTE SERIES. NGA REF. NO. USGSX24K31411



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SITE LOCATION MAP
 428 BETHMOUR ROAD
 BETHANY, CONNECTICUT

Project #:	22113201
Plan Date:	07/10/2023
Scale:	1" = 1,000'
Figure:	1



Wetlands

- Estuarine and Marine Deepwater
- Estuarine and Marine Wetland

- Freshwater Emergent Wetland
- Freshwater Forested/Shrub Wetland
- Freshwater Pond

- Lake
- Other
- Riverine

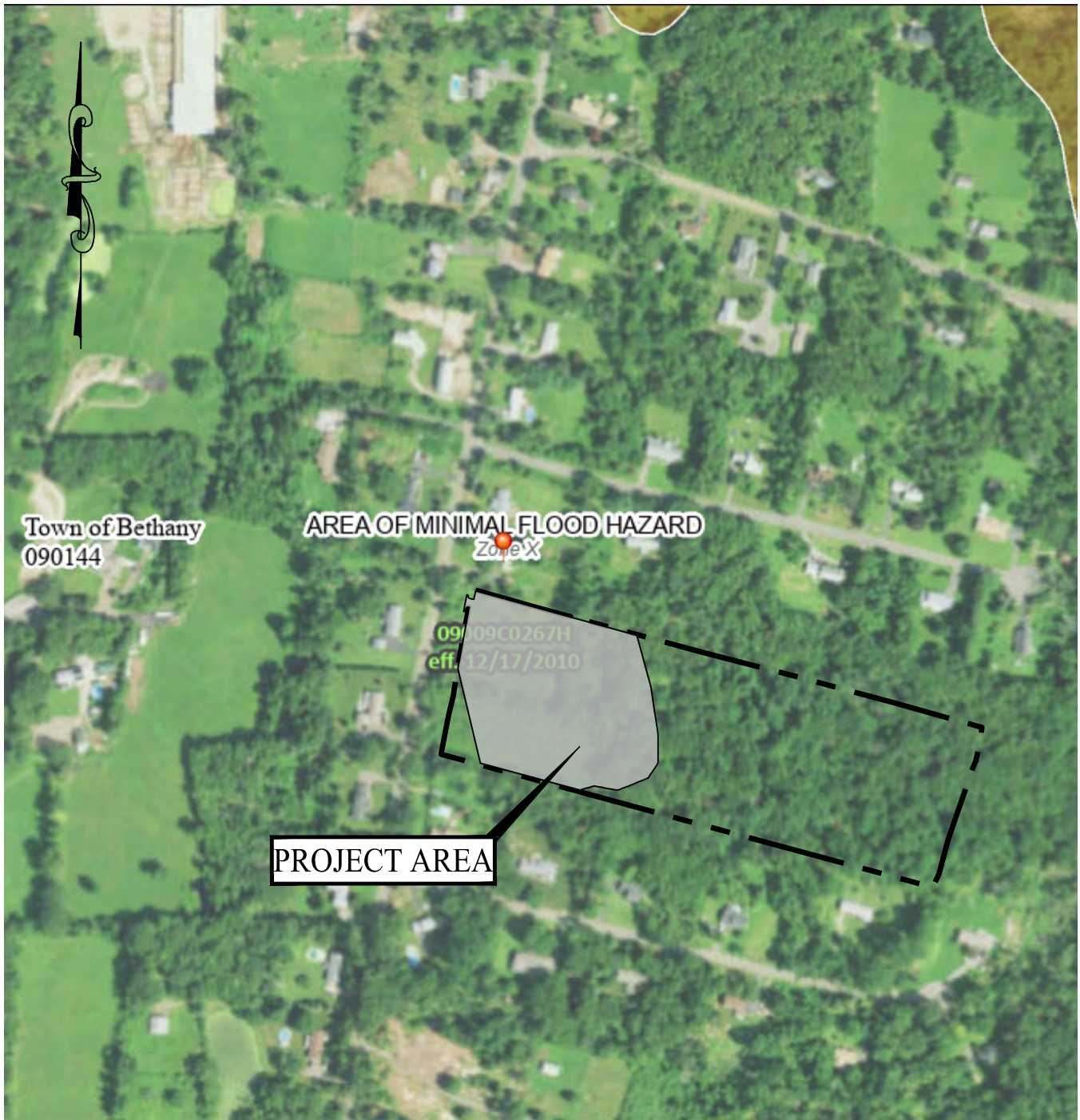
NOTE: BASE MAP INFORMATION TAKEN
FROM U.S. FISH AND WILDLIFE SERVICE
NATIONAL WETLANDS INVENTORY



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**WETLANDS &
WATERCOURSES MAP**
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Project #:	22113201
Plan Date:	07/10/2023
Scale:	1" = 1,000'
Figure:	2



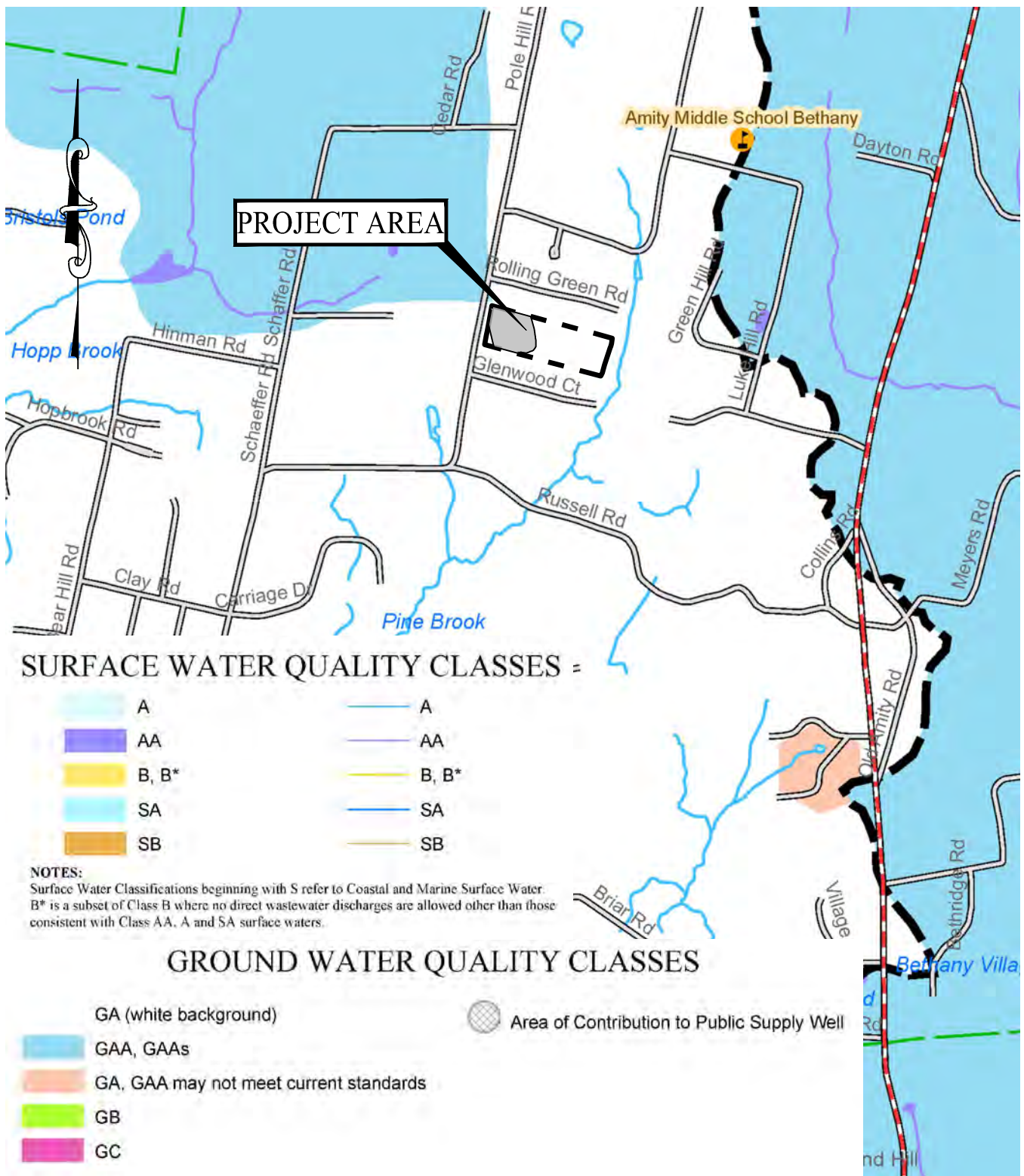
NOTE: BASE MAP INFORMATION TAKEN FROM
FEMA FLOOD INSURANCE RATE MAP, MAP
NUMBER 09009C0267H, EFFECTIVE 12/17/2010.



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FEMA FLOOD MAP
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Project #:	22113201
Plan Date:	07/10/2023
Scale:	1" = 500'
Figure:	3



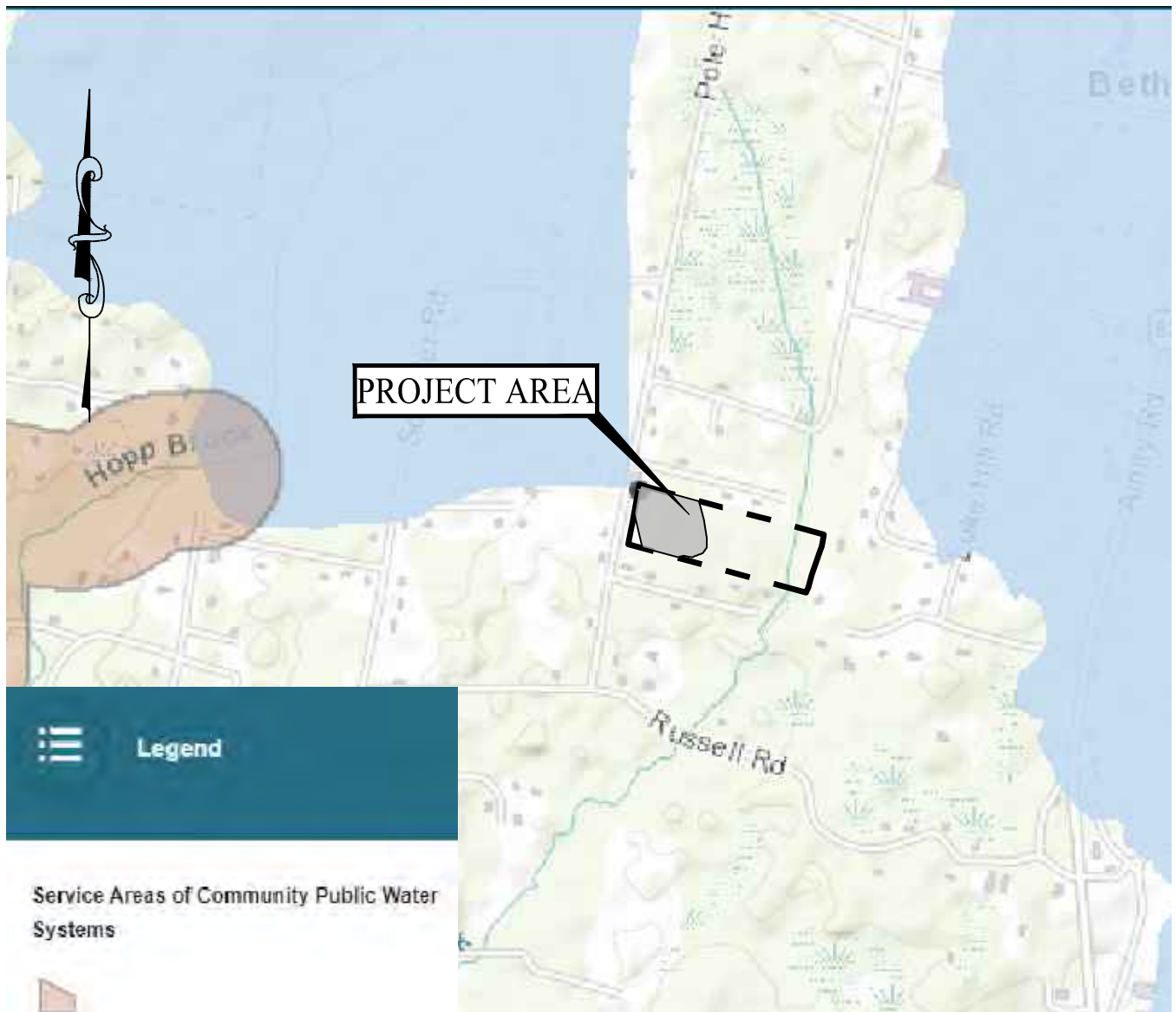
NOTE: BASE MAP INFORMATION TAKEN FROM CT
 DEEP, DATED: OCTOBER, 2018.



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**WATER QUALITY
 CLASSIFICATION MAP**
 428 BETHMOUR ROAD
 BETHANY, CONNECTICUT

Project #:	22113201
Plan Date:	07/10/2023
Scale:	1" = 2,000'
Figure:	4

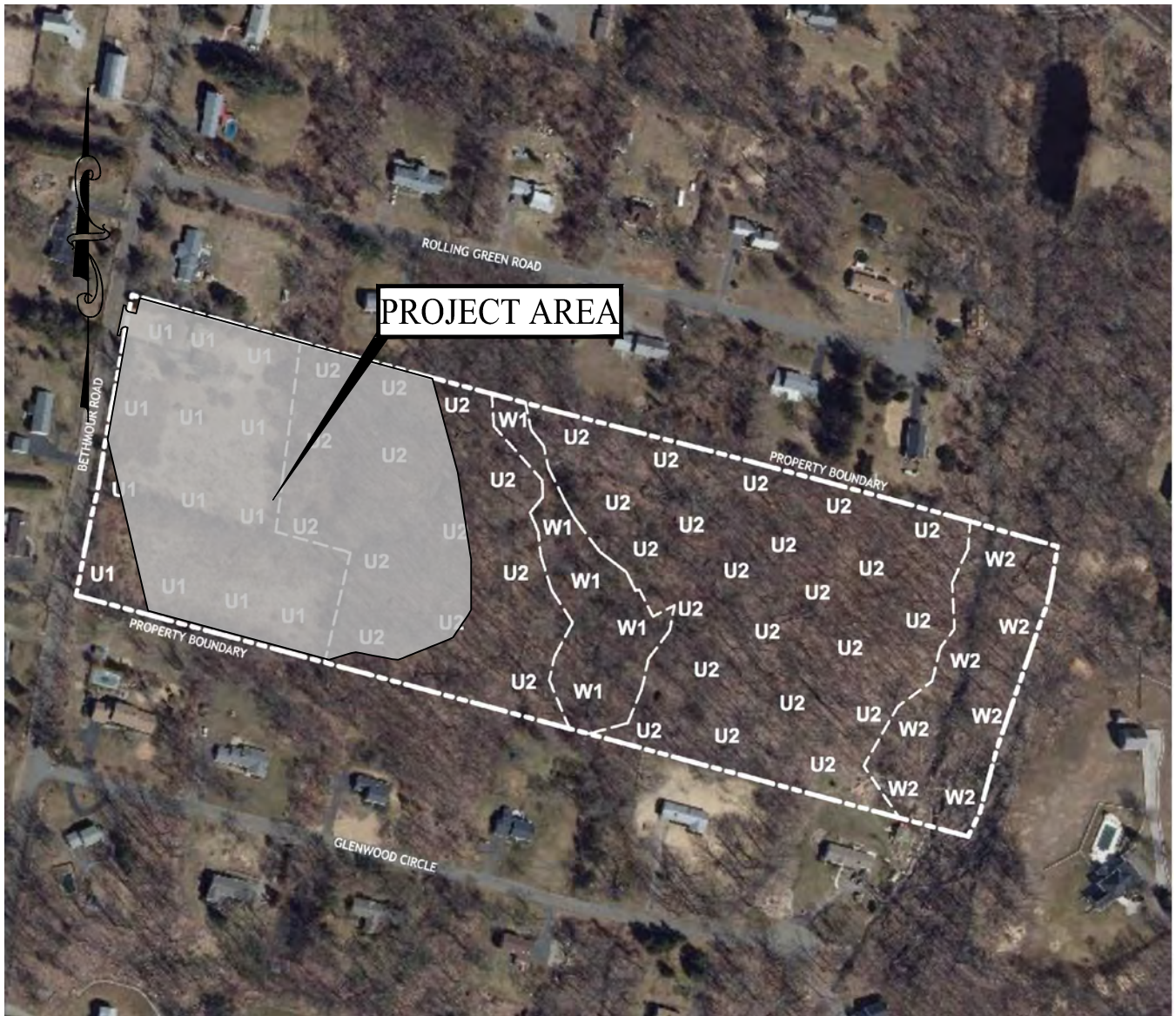


NOTE: BASE MAP INFORMATION TAKEN FROM CONNECTICUT STATE DEPARTMENT OF PUBLIC HEALTH GIS MAP.

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**PUBLIC SUPPLY
WATERSHED MAP**
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

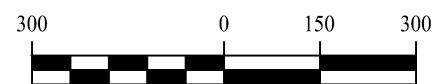
Project #:	22113201
Plan Date:	07/10/2023
Scale:	1" = 1,500'
Figure:	5



ECOLOGICAL COMMUNITY

SYM.	NAME
UPLAND	
U1	SHRUBLAND
U2	WOODLAND
WETLAND	
W1	WOODLAND WETLAND WITH INTERMITTENT WATERCOURSE
W2	WOODLAND WETLAND WITH STREAM (PINE BROOK)

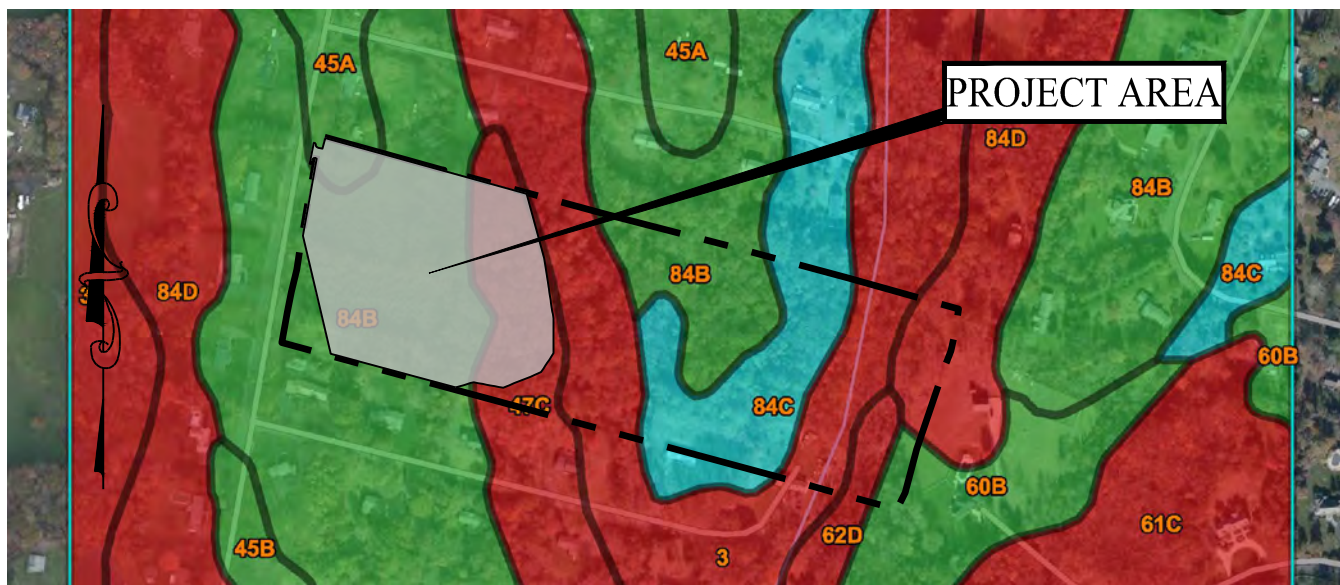
NOTE: BASE MAP INFORMATION TAKEN FROM
ECOLOGICAL COMMUNITIES MAP PREPARED BY
WILLIAM KENNY ASSOCIATES



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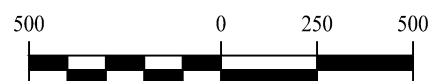
HABITAT COVER MAP
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Project #: 22113201
Plan Date: 07/10/2023
Scale: 1" = 300'
Figure: 6



Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	Not prime farmland	24.2	18.7%
45A	Woodbridge fine sandy loam, 0 to 3 percent slopes	All areas are prime farmland	5.7	4.4%
45B	Woodbridge fine sandy loam, 3 to 8 percent slopes	All areas are prime farmland	1.7	1.3%
60B	Canton and Charlton fine sandy loams, 3 to 8 percent slopes	All areas are prime farmland	6.5	5.0%
61C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony	Not prime farmland	9.4	7.3%
62D	Canton and Charlton fine sandy loams, 15 to 35 percent slopes, extremely stony	Not prime farmland	1.9	1.5%
84B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes	All areas are prime farmland	44.6	34.5%
84C	Paxton and Montauk fine sandy loams, 8 to 15 percent slopes	Farmland of statewide importance	10.0	7.7%
84D	Paxton and Montauk fine sandy loams, 15 to 25 percent slopes	Not prime farmland	18.8	14.5%
86D	Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony	Not prime farmland	0.1	0.1%

NOTE: BASE MAP RESOURCES TAKEN FROM THE
NATURAL RESOURCES CONSERVATION SERVICE, URL:
<https://websoilsurvey.sc.egov.usda.gov>



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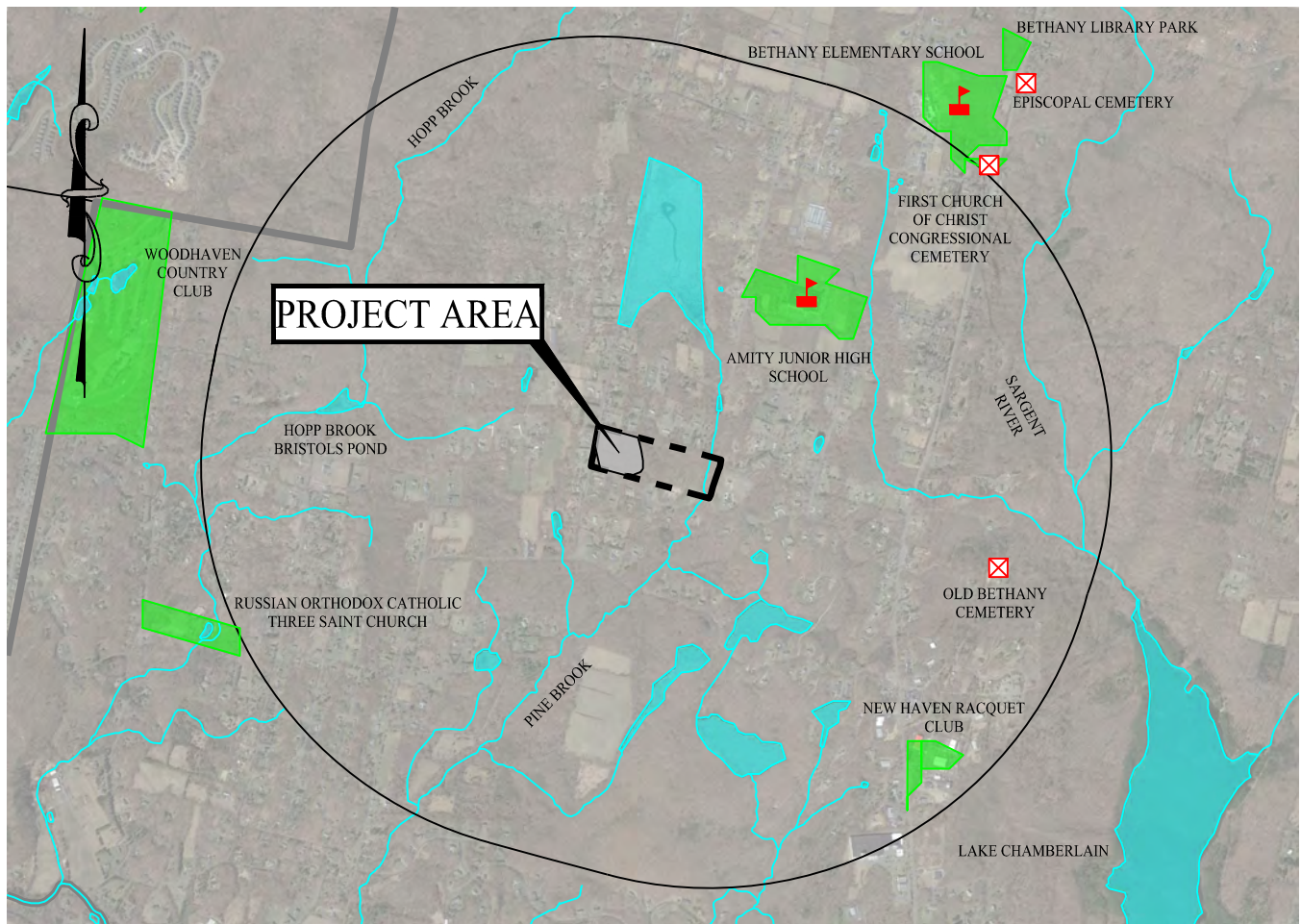
PRIME FARMLAND MAP
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Project #: 22113201

Plan Date:

Scale: 1" = 500'

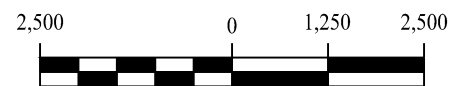
Figure: 8



LEGEND

	PROPERTY LINE		OPEN WATER (CT DEEP)
	1 MILE RADIUS		OPEN SPACE (CT ECO)
	TOWN BOUNDARY		SCHOOL
	NTL. SCENIC ROADWAY		CEMETERY
	STATE SCENIC ROADWAY		PARK
	HIKING TRAIL		
	WATERCOURSES (CT DEEP)		

NOTE: BASE MAP RESOURCES TAKEN FROM CT ECO
OPEN SPACE MAPPING AND CT DEEP HYDROGRAPHY



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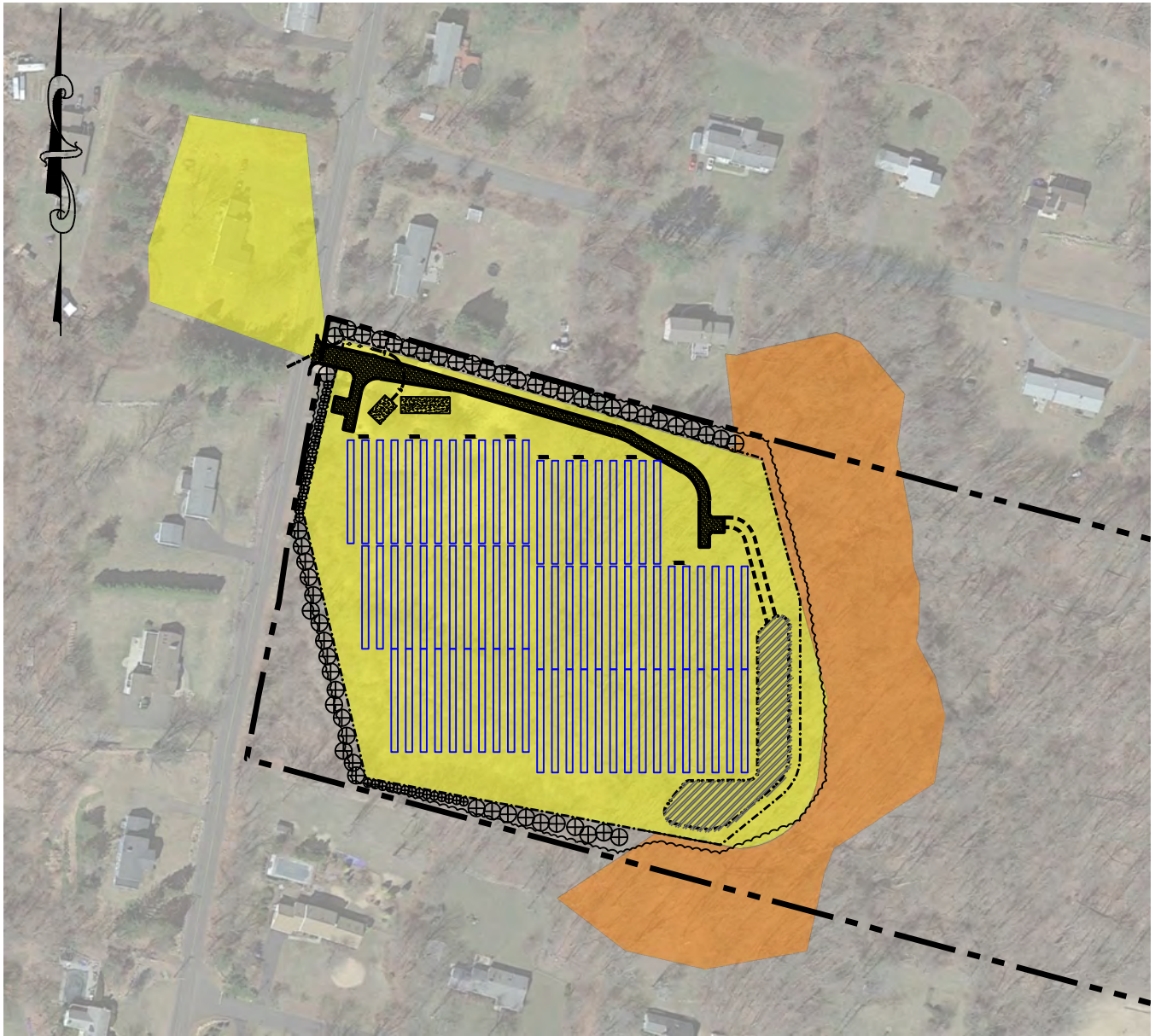
SCENIC & RECREATION MAP
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Project #: 22113201

Plan Date: 07/10/2023

Scale: 1" = 2,500'

Figure: 9



LEGEND



PROPERTY LINE



PREDICTED YEAR-ROUND VISIBILITY



PREDICTED SEASONAL VISIBILITY



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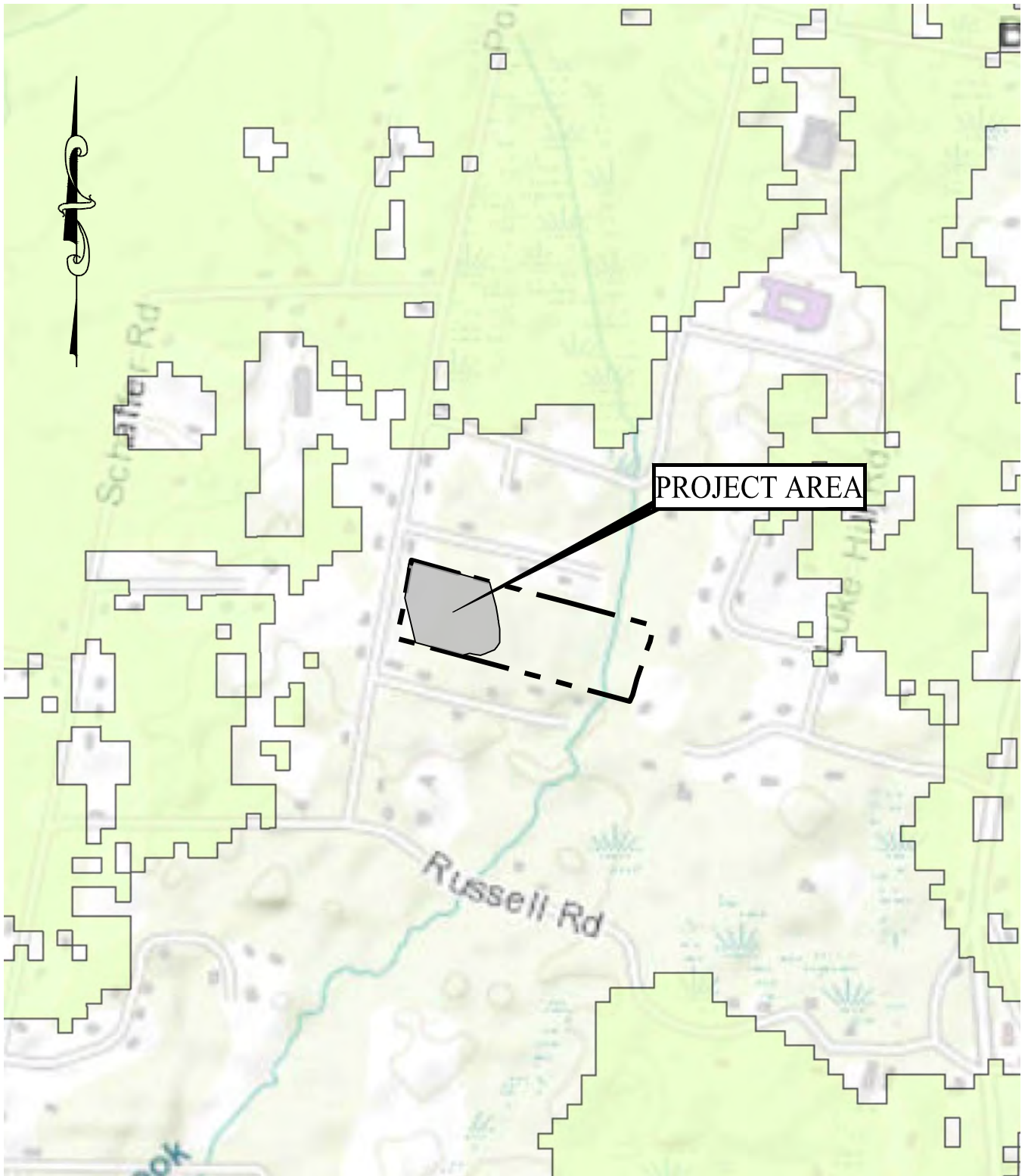
PROPOSED CONDITIONS VIEWSHED MAP
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Project #: 22113201

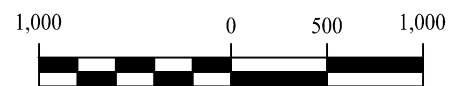
Plan Date: 07/10/2023

Scale: 1" = 200'

Figure: 10



NOTE: BASE MAP RESOURCES TAKEN FROM ARCGIS
FORESTLAND HABITAT IMPACT MAP

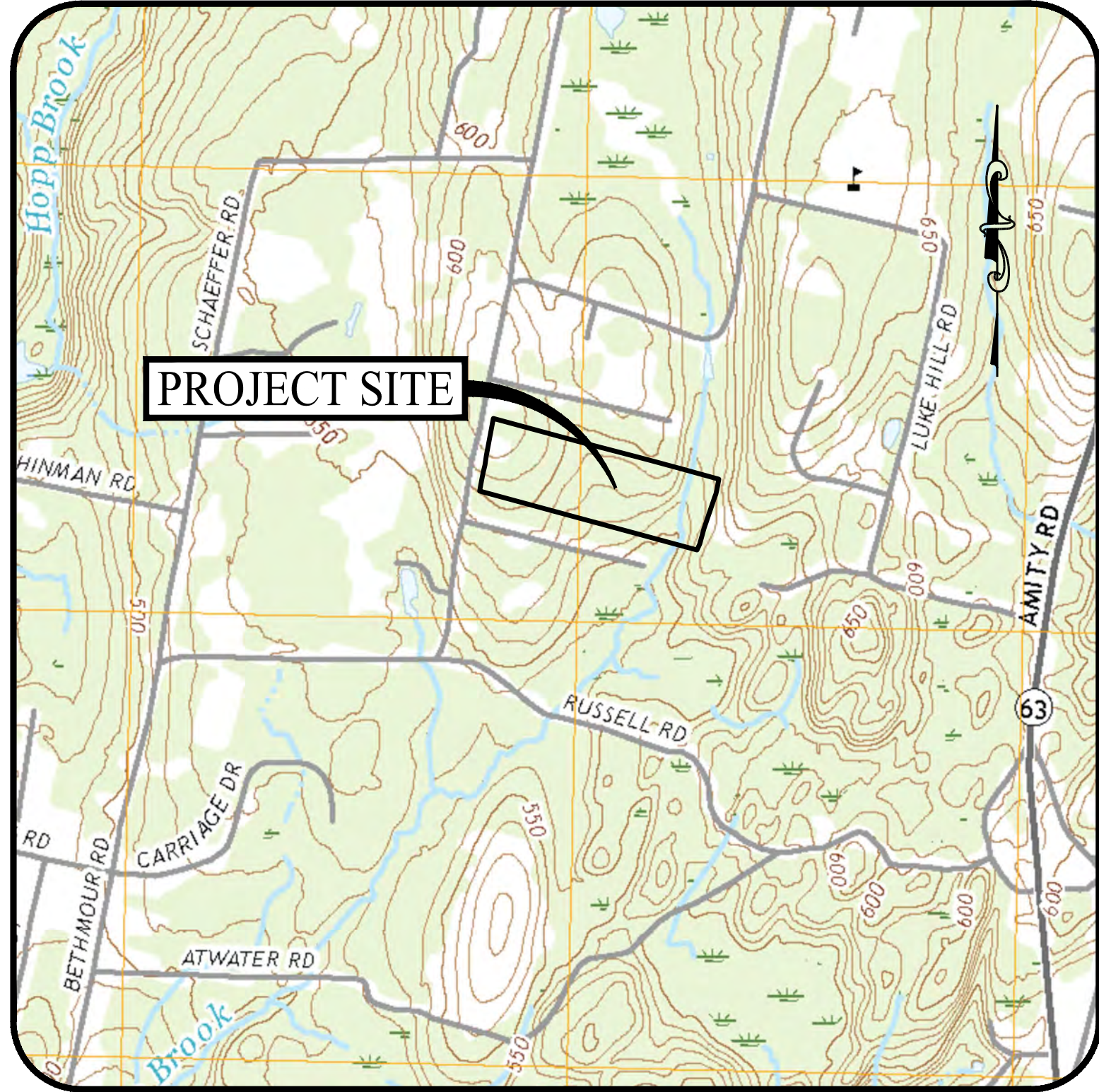


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CORE FOREST MAP
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Project #:	22113201
Plan Date:	07/10/2023
Scale:	1" = 1,000'
Figure:	11

Appendix B: Site Plans

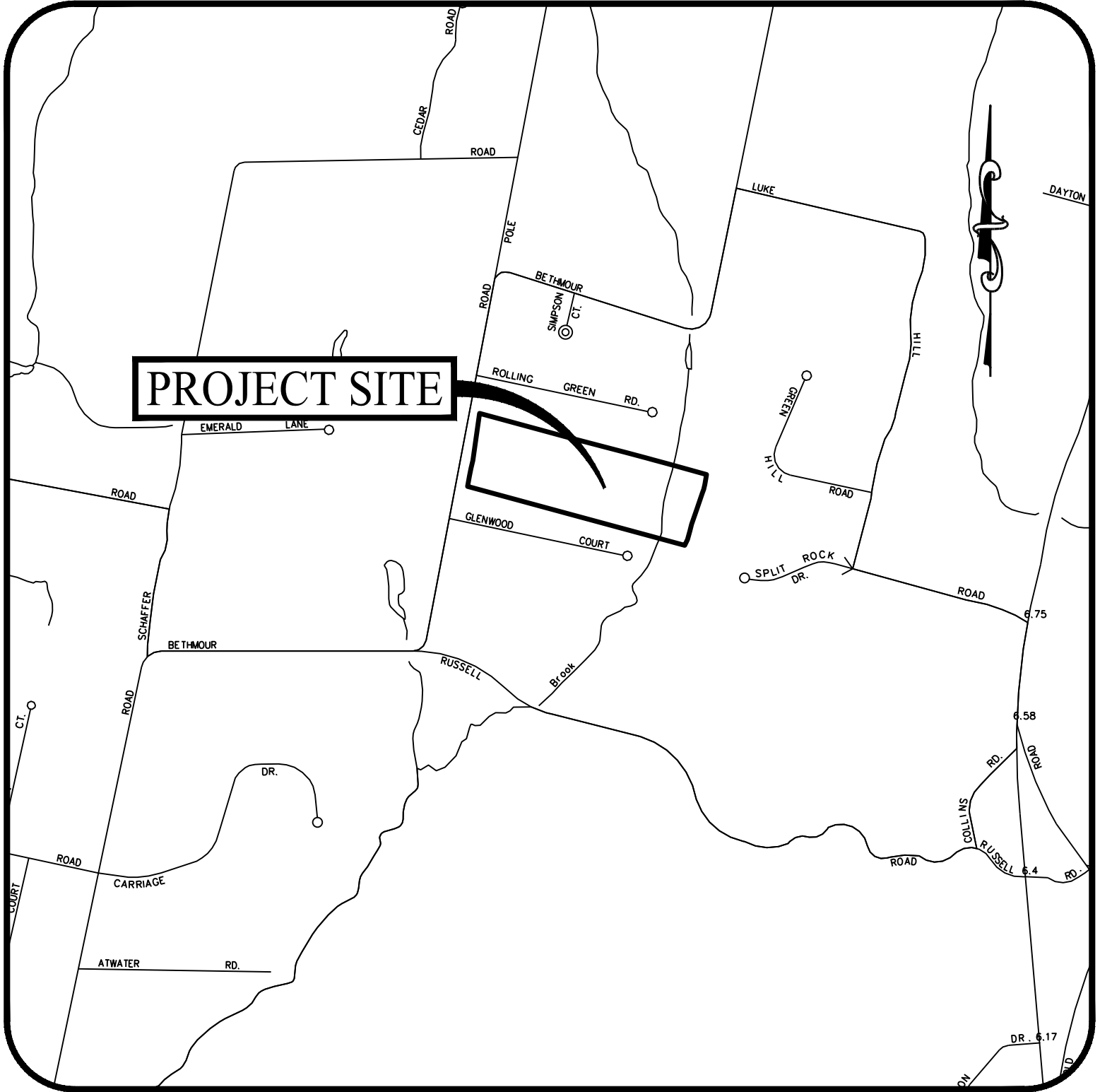


USGS MAP

SCALE: 1" = 1,000'

PROPOSED SOLAR PHOTOVOLTAIC ARRAY

428 BETHMOUR ROAD
BETHANY, CONNECTICUT



LOCATION MAP

SCALE: 1" = 1,000'

PREPARED FOR:



888 PROSPECT STREET, SUITE 200
LA JOLLA, CALIFORNIA

PREPARED BY:



501 MAIN STREET, MONROE, CONNECTICUT 06468
11 VANDERBILT AVENUE, NORWOOD, MASSACHUSETTS 02062

DRAWING LIST

SHEET #	SHEET NAME	PLAN DATE	LATEST REVISION
0.00	COVER SHEET	04/18/23	09/19/23
EX-1	EXISTING CONDITIONS MAP	01/05/22	N/A
2.10	OVERALL SITE LAYOUT PLAN	09/19/23	N/A
2.11	SITE LAYOUT PLAN	04/18/23	09/19/23
2.21	GRADING AND DRAINAGE PLAN	04/18/23	09/19/23
2.31	SOIL EROSION & SEDIMENT CONTROL PLAN	04/18/23	09/19/23
2.41	SOIL EROSION & SEDIMENT CONTROL NOTES & DETAILS	04/18/23	09/19/23
3.01	CONSTRUCTION DETAILS	04/18/23	09/19/23

OWNER

THE NEVAR COMPANY
PO BOX 743
CHESHIRE, CONNECTICUT 06410

APPLICANT

TRITEC AMERICAS, LLC
888 PROSPECT STREET, SUITE 200
LA JOLLA, CALIFORNIA 92307

PROPERTY INFORMATION

ADDRESS: 428 BETHMOUR ROAD, BETHANY, CONNECTICUT
MAP-BLOCK-LOT: 113-1 & 113-1-A
ZONE: R-65
AREA: ±21.22 AC
BOOK/PAGE: 0215/0543

SOIL SCIENTIST

WILLIAM KENNY
WILLIAM KENNY ASSOCIATES
195 TUNXIS HILL, CUTOFF SOUTH
FAIRFIELD, CT 06825
(203) 366-0588

ELECTRICAL ENGINEER

PURE POWER ENGINEERING, INC.
111 RIVER STREET, SUITE 1110
HOBOKEN, NJ 07030
(201) 687-9975



SITE / CIVIL ENGINEER

KEVIN SOLLI, P.E., CPESC, LEED AP BD+C
LICENSE NO. 25759
SOLLI ENGINEERING, LLC
501 MAIN STREET
MONROE, CONNECTICUT 06468
(203) 880-5455

LANDSCAPE ARCHITECT

MARY BLACKBURN, P.L.A.,
LICENSE CT NO. 1499
SOLLI ENGINEERING, LLC
501 MAIN STREET
MONROE, CONNECTICUT 06468
(203) 880-5455

SURVEYOR OF RECORD

PATRICK J CORLESS, JR. LICENSE NO. 70015
BL COMPANIES
355 RESEARCH PARKWAY
MERIDEN, CONNECTICUT 06450
(203) 630-1406

1	09/19/23	Response to CSC Interrogatories
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Rev. #: Date Description

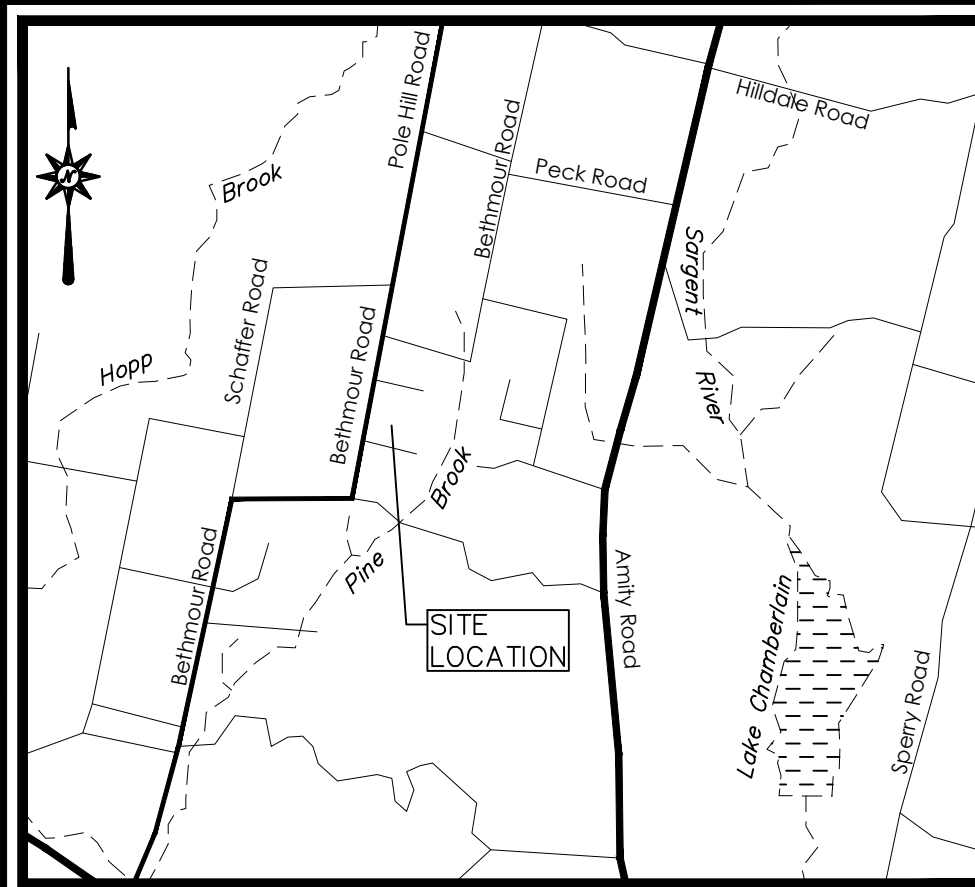
Project:
**PROPOSED SOLAR
PHOTOVOLTAIC ARRAY**
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Sheet Title:

COVER
SHEET

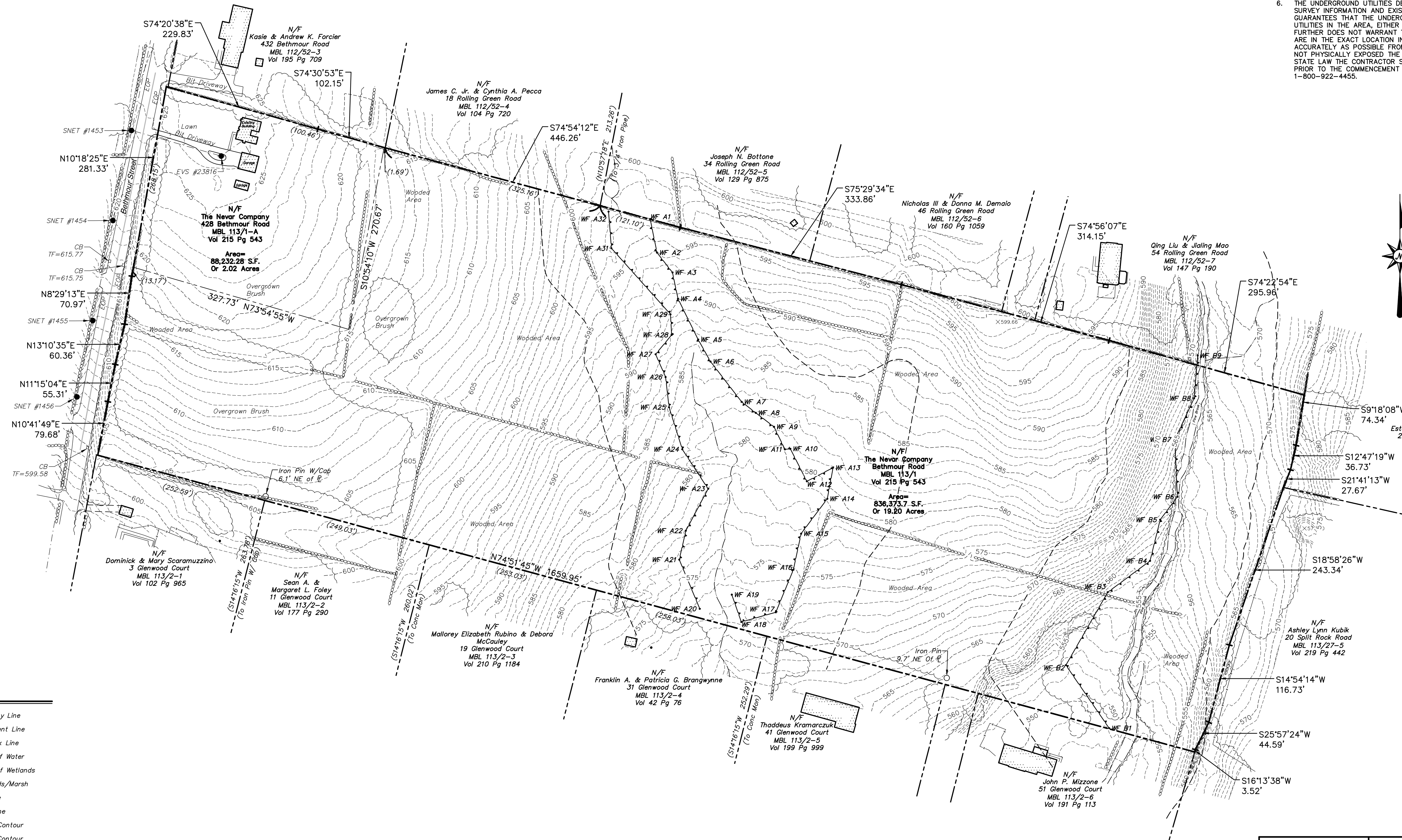
Sheet #:

0.00



LOCATION MAP

NOT TO SCALE



LEGEND

	Property Line
	Easement Line
	Setback Line
	Edge of Water
	Limit of Wetlands
	Wetlands/Marsh
	Treeline
	Brushline
	Major Contour
	Minor Contour
	Stone Wall
	Retaining Wall
	Fence
	Overhead Wires
	Utility Pole
	Utility Pole w/ Light
	Catch Basin

MAP REFERENCES

A. "MAP OF LAND IN BETHANY CONN., BELONGING TO THE DRAZEN LUMBER CO., OF NEW HAVEN CONN." SCALE 1"=100', DATE 11/16/1935. CERTIFIED SUBSTANTIALLY CORRECT BY A.M. WELLINGTON AND FILED AS MAP A101 IN THE TOWN OF BETHANY CLERKS OFFICE.

B. "GLENWOOD" MAP OF LOTS OWNED & DEVELOPED BY THE BERNER LOHNE CO., INC., BETHANY, CONN." SCALE 1"=50', DATE 4/2/1964. CERTIFIED SUBSTANTIALLY CORRECT BY RICHARD J. NOWAKOWSKI AND FILED AS MAP A200 IN THE TOWN OF BETHANY CLERKS OFFICE.

C. "ROLLING GREEN ACRES-EAST, SECTION ONE, OWNED AND DEVELOPED BY ROLLING GREEN ACRES INC., BETHANY, CONN." SCALE 1"=50', DATE 5/1965. CERTIFIED SUBSTANTIALLY CORRECT BY WILLIAM O. DOLL AND FILED AS MAP A201 IN THE TOWN OF BETHANY CLERKS OFFICE.

D. "LOTS 4 THRU 13, FINAL, ROLLING GREEN ACRES, SECTION 2 EAST, BETHANY CONN." SCALE 1"=50', DATE 10/1965, REVISED 11/15/1965, ADDITIONS 04/18/1966. SURVEYED BY CAHN ENGINEERS, NEW HAVEN, CT AND FILED AS MAP A209 IN THE TOWN OF BETHANY CLERKS OFFICE.

E. "MAP OF GREEN HULL ACRES, BETHANY, CONNECTICUT" SCALE 1"=100', DATE 9/5/1972. SURVEYED BY ROBERT G. SWELL AND FILED AS MAP A284 IN THE TOWN OF BETHANY CLERKS OFFICE.

F. "MAP OF LAND OF LENA KRUPIEN, BETHANY, CONNECTICUT" SCALE 1"=40', DATE 7/18/1980. SURVEYED BY WILLIAM E. GILBERT ASSOCIATES, CONSULTING ENGINEERS, BETHANY, CT AND FILED AS MAP A403 IN THE TOWN OF BETHANY CLERKS OFFICE.

G. "SUBDIVISION PLAN, SPLIT ROCK, 55 LUKE HILL ROAD, BETHANY, CT." SCALE 1"=100', DATE 11/16/1994. PREPARED BY JOHN PAUL GARCIA & ASSOC. P.C. ENGINEERS AND SURVEYORS, BETHANY, CT AND FILED AS MAP A709 IN THE TOWN OF BETHANY CLERKS OFFICE.

GENERAL NOTES

1. A) THIS MAP HAS BEEN PREPARED IN ACCORDANCE WITH THE REGULATIONS OF CONNECTICUT STATE AGENCIES, SECTIONS 20-306-1 THROUGH 1-20-306-20 AND THE "STANDARDS AND SUGGESTED METHODS AND PROCEDURES FOR SURVEYS AND MAPS IN THE STATE OF CONNECTICUT" PREPARED AND ADOPTED BY THE CONNECTICUT ASSOCIATION OF LAND SURVEYORS, INC. AUGUST 29, 2019.
- B) THIS PLAN CONFORMS TO HORIZONTAL ACCURACY CLASS A-2 AND TOPOGRAPHIC ACCURACY CLASS T-2.
- C) BOUNDARY DETERMINATION IS BASED UPON A RESURVEY.
- D) THE TYPE OF SURVEY REQUIRED IS A EXISTING CONDITIONS SURVEY AND IS INTENDED TO DEPICT THE BOUNDARY, EASEMENTS, AND EXISTING CONDITIONS WITH RESPECT TO MONUMENTATION FOUND, STRUCTURES, EASEMENTS, ENCROACHMENTS, VISIBLE UTILITIES, ROADWAYS AND CONTOURS.
2. NORTH ARROW AND BEARINGS REFER TO THE CONNECTICUT STATE PLANE COORDINATE SYSTEM (CT NAD 83 - EPOCH 2011) AND ARE BASED ON GPS OBSERVATIONS PERFORMED BY BL COMPANIES DURING NOVEMBER, 2021 UTILIZING THE SMARTNET VRS NETWORK.
3. ELEVATIONS REFER TO THE NORTH AMERICAN DATUM OF 1988 (NAVD 88). THE DATUM WAS DETERMINED BY USING (GEOID 18) AND IS BASED ON GPS OBSERVATIONS PERFORMED BY BL COMPANIES IN NOVEMBER, 2021 UTILIZING THE SMARTNET VRS NETWORK.
4. PARCEL IS LOCATED IN A OTHER AREA "X", (AREAS DETERMINED TO BE OUTSIDE THE 0.2% ANNUAL CHANCE FLOOD PLAIN) AS DEPICTED ON F.I.R.M. MAP NUMBER 0900002678, PANEL 267 OF 635, WITH EFFECTIVE DATE DECEMBER 17, 2010.
5. WETLAND BOUNDARY DETERMINED BY BL COMPANIES ON JANUARY 5, 2022 AND LOCATED BY FIELD SURVEY BY BL COMPANIES ON JANUARY 5, 2022.
6. THE UNDERGROUND UTILITIES DEPICTED HAVE BEEN PLOTTED FROM FIELD SURVEY INFORMATION AND EXISTING DRAWINGS. THE SURVEYOR MAKES NO GUARANTEES THAT THE UNDERGROUND UTILITIES DEPICTED COMPRISE ALL SUCH UTILITIES IN THE AREA, EITHER IN SERVICE OR ABANDONED. THE SURVEYOR FURTHER DOES NOT WARRANT THAT THE UNDERGROUND UTILITIES DEPICTED ARE IN THE EXACT LOCATION INDICATED THOUGH THEY ARE PLOTTED AS ACCURATELY AS POSSIBLE FROM INFORMATION AVAILABLE. THE SURVEYOR HAS NOT PHYSICALLY EXPOSED THE UNDERGROUND UTILITIES. PER CONNECTICUT STATE LAW THE CONTRACTOR SHALL CONFIRM THE LOCATION OF ANY UTILITIES PRIOR TO THE COMMENCEMENT OF EXCAVATION. CALL BEFORE YOU DIG 1-800-922-4455.



5 Research Parkway
Meriden, CT 06450
(203) 630-1406
(203) 630-2615 Fax

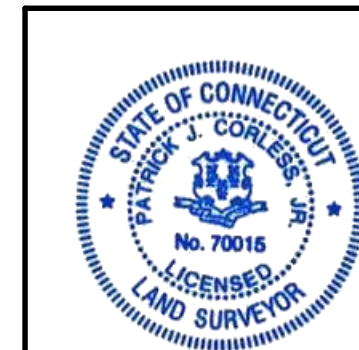
LAND OF
THE NEVAR COMPANY
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

No.	Date	Desc.
Reviewed		KJ
Drawn		JW
Reviewed		PJC
Date		1"=80'
Project No.		2101190
Date		01/05/2022
Old Book		564
AD File:		EX210119001

EXISTING CONDITIONS MAP

Sheet No.

EX-1



TO MY KNOWLEDGE AND BELIEF THIS MAP
IS SUBSTANTIALLY CORRECT AS NOTED HEREON.

 1/5/2022
PATRICK J. CORLESS, JR., L.S. #70015

NO CERTIFICATION IS EXPRESSED OR IMPLIED UNLESS
THIS MAP BEARS THE ORIGINAL SIGNATURE AND EMBOSSED
SEAL OF THE ABOVE NAMED LAND SURVEYOR.



- ## GENERAL NOTES

1. THESE PLANS ARE FOR PERMITTING PURPOSES ONLY AND ARE NOT FOR CONSTRUCTION. NO CONSTRUCTION OR DEMOLITION SHALL BEGIN UNTIL FINAL APPROVAL OF THIS PLAN IS GRANTED.
2. ALL PROPOSED SITE WORK TO BE COMPLETED IN ACCORDANCE WITH ALL PERMITS, APPROVALS AND CONDITIONS OF APPROVALS ISSUED BY LOCAL, STATE AND/OR FEDERAL REVIEWING AGENCIES.
3. EXISTING BOUNDARY, TOPOGRAPHY AND SITE CONDITIONS INFORMATION TAKEN FROM A PLAN ENTITLED "EXISTING CONDITIONS MAP, 428 BETHMOOR ROAD, BETHANY, CONNECTICUT, EX-1-10-10, DATED 10-10-10, BY BETHANY PLANNING & ZONING DEPARTMENT, BETHANY, CT.
4. REFER TO THE EXISTING CONDITIONS MAP FOR THE ENTIRE PROPERTY BOUNDARY AND EXISTING CONDITIONS INFORMATION. THE PLAN HEREON DEPICTS A PORTION OF THE PROPERTY IN WHICH THE SITE WORK IS BEING PROPOSED.
5. THE PROPOSED PARCEL CONSISTS OF A TOTAL AREA OF APPROXIMATELY 21.2± ACRES, LOCATED IN THE RESIDENTIAL R-1 (65) DISTRICT IN THE TOWN OF BETHANY, CONNECTICUT.
6. WETLAND BOUNDARY DETERMINED AND LOCATED BY FIELD SURVEY BY B.L. COMPANIES ON 01/10/2022.
7. PORTIONS OF THE SITE ARE LOCATED WITHIN FEMA DESIGNATED FLOOD HAZARD AREA "X" AS SHOWN ON F.I.R.M. MAP NUMBER 1609003C267H, PANEL 267 OF 655, WITH EFFECTIVE DATE DECEMBER 17, 2010.
8. ALL CONSTRUCTION SHALL COMPLY WITH THE TOWN OF BETHANY, CONNECTICUT DEEP AND CONNECTICUT DEPARTMENT OF TRANSPORTATION STANDARDS AND SPECIFICATIONS IN THE LATEST EDITION. IN ADDITION, ALL CONSTRUCTION SHALL COMPLY WITH THE STATE OF CONNECTICUT'S MOST RECENT "DESIGN SPECIFICATION" SHALL APPLY. ALL CONSTRUCTION SHALL BE PERFORMED IN ACCORDANCE WITH ALL APPLICABLE OSHA, FEDERAL, STATE AND LOCAL REGULATIONS.
9. PRIOR TO DEMOLITION OR CONSTRUCTION, THE CONTRACTOR SHALL CONTACT "CALL BEFORE YOU DIG" 72 HOURS BEFORE THE COMMENCEMENT OF WORK AT (800) 922-4455" AND VERIFY ALL UTILITIES AND DRAINAGE SYSTEMS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR LOCATING ALL UTILITIES AND DRAINAGE SYSTEMS HAS BEEN COMPILED FROM AVAILABLE INFORMATION INCLUDING UTILITY PROVIDER AND MUNICIPAL RECORD MAPS AND/OR FIELD SURVEY AND IS NOT GUARANTEED CORRECT OR COMPLETE. UTILITIES AND STORM DRAINAGE SYSTEMS ARE SHOWN TO ALERT THE CONTRACTOR TO THE LOCATION OF UTILITIES AND DRAINAGE SYSTEMS. THE CONTRACTOR SHALL DETERMINE ACTUAL LOCATIONS AND ELEVATIONS OF ALL UTILITIES AND STORM DRAINAGE SYSTEMS INCLUDING SERVICES.
10. SHOULD ANY UNCHARTED OR INCORRECTLY CHARTED, EXISTING PIPING OR OTHER UTILITY BE DISCOVERED DURING CONSTRUCTION, THE CONTRACTOR SHALL NOTIFY AN ENGINEER IMMEDIATELY FOR DIRECTIONS AND FOR PRECEDENCE. FURTHER, THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROTECTION OF THE UTILITY.
11. THE OWNER IS RESPONSIBLE FOR OBTAINING ALL NECESSARY ZONING PERMITS REQUIRED BY GOVERNMENT AGENCIES PRIOR TO CONSTRUCTION. THE CONTRACTOR SHALL OBTAIN ALL LOCAL AND STATE PERMITS. THE CONTRACTOR SHALL POST ALL BONDS, PAY ALL FEES, PROVIDE PROOF OF INSURANCE AND PROVIDE TRAFFIC CONTROLS NECESSARY FOR THIS PROJECT.
12. THE CONTRACTOR SHALL RESTORE ANY DRAINAGE STRUCTURE, PIPE, UTILITY, PAVEMENT, CURBS, SIDEWALKS, LANDSCAPED AREAS OR SIGNAGE DISTURBED DURING CONSTRUCTION TO THEIR ORIGINAL CONDITION OR BETTER, AS APPROVED BY THE CIVIL ENGINEER OF RECORD, DURING OR AFTER CONSTRUCTION. THE CONTRACTOR SHALL MAINTAIN THE SITE MAINTAINED FREE OF ALL TRASH, LITTER, DEBRIS AND OVERGROWN VEGETATION.
13. THE CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING THE SITE FREE OF ALL TRASH, LITTER, DEBRIS AND OVERGROWN VEGETATION THROUGHOUT CONSTRUCTION.
14. ALTERNATIVE METHODS AND PRODUCTS OTHER THAN THOSE SPECIFIED MAY BE USED IF THEY ARE APPROVED BY THE CIVIL ENGINEER AND REGULATORY AGENCY PRIOR TO INSTALLATION DURING THE BIDDING PROCESS.

SOLAR ARRAY SYSTEM INFORMATION

	TOTAL
SIZE DC	1,399 MW
SIZE AC	0,999 MW
INVERTER LOAD RATIO	1.40
MODULE TYPE	TRACKING TRINASOLAR TSM-540-DEG19C.2D (540W)
MODULE QUANTITY	2,590
INVERTER	SUNGROW SGH251H 125KW
INVERTER QUANTITY	8
UTILITY	EVERSOURCE

1	09/19/23	Response to CSC Interrogatories
Rev. #:	Date	Description

Graphic Scale:



501 Main Street, Monroe, CT 06468 T: (203) 880-5455 F: (203) 880-9699
11 Vanderbilt Ave, Norwood, MA 02062 T: (781) 352-8491 F: (203) 880-9699

Drawn By: AWC

Checked By: CJB

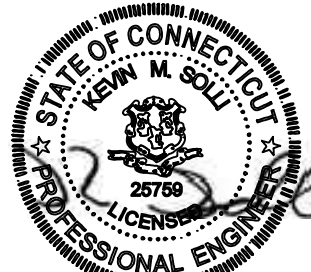
Approved By: KMS

Project #: 2211320

Plan Date: 04/18/23

Scale: 1" = 40'

Project:



Kevin Solli, P.E.
CT 25759

PROPOSED SOLAR
PHOTOVOLTAIC ARRAY
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Sheet Title:

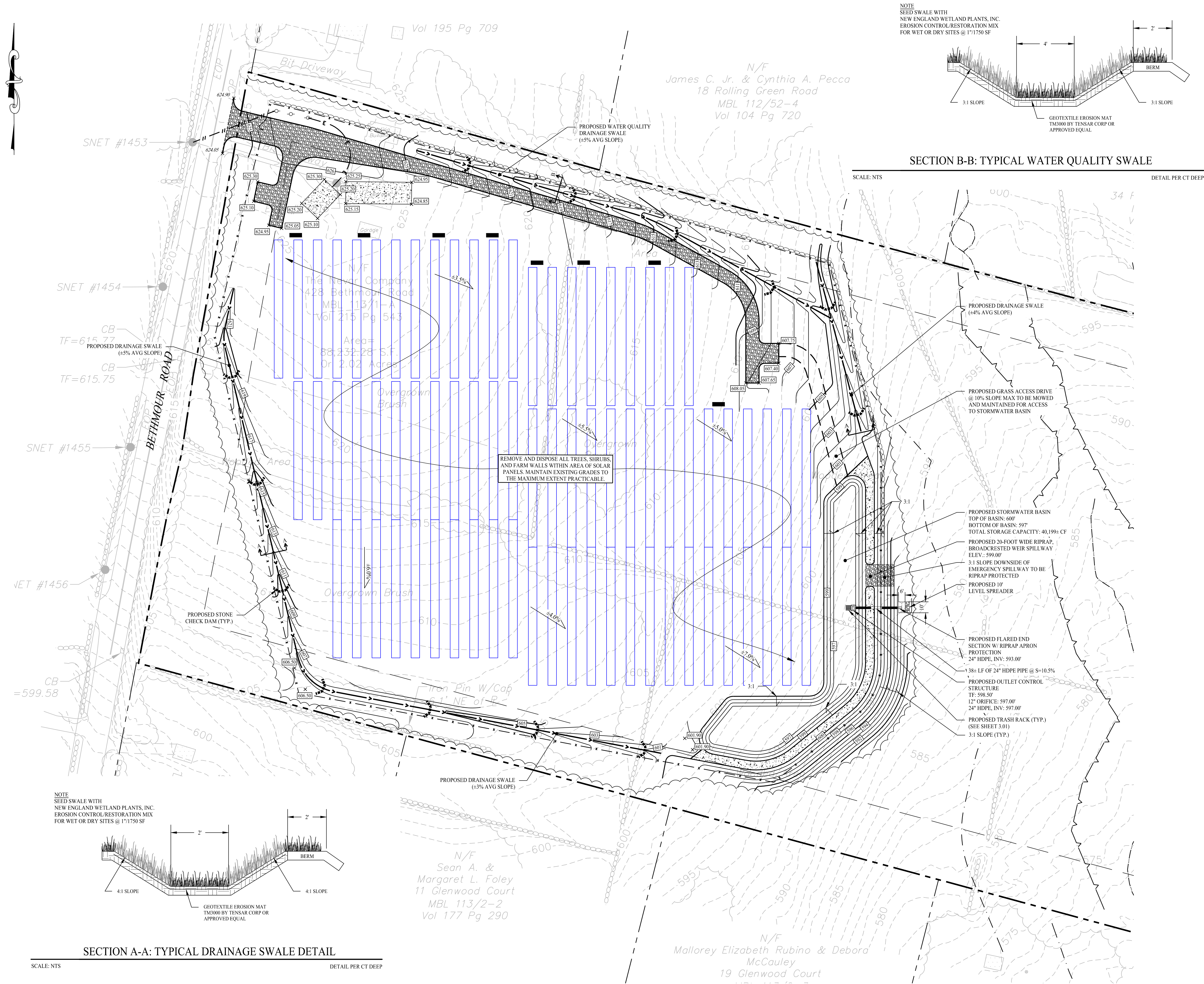
Sheet #:

SITE LAYOUT PLAN

2.11

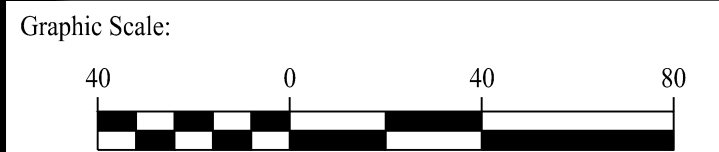
PLANTING SCHEDULE

KEY	QTY	BOTANICAL NAME	COMMON NAME	ROOT	SIZE	COMMENTS
TREES						
AC	10	ABIES CONCOLOR	CONCOLOR / WHITE FIR	B&B	7-8' HT	15' O.C.
PG	23	PICEA GLAUCA	WHITE SPRUCE	B&B	7-8' HT	15' O.C.
PP	22	PICEA PUNGENS	COLORADO BLUE SPRUCE	B&B	7-8' HT	15' O.C.
TO	34	THUJA OCCIDENTALIS 'ELEGANTISSIMA'	AMERICAN ARBORVITAE	B&B	7-8' HT	8' O.C.
SEED MIXES						
NEW ENGLAND EROSION CONTROL/RESTORATION NO MOW MIX (NEW ENGLAND WETLAND PLANTS, INC.)						
APPLICATION RATE: 1 LBS/2,500 S.F.						
ERNMX-147						
APPLICATION RATE: 42 LBS/ACRE WITH A COVER CROP OF ANNUAL RYEGRASS AT 12 LBS/ACRE						
ERNMX-610						
APPLICATION RATE: 30 LBS/ACRE OF A COVER CROP. FOR A COVER CROP USE EITHER GRAIN OATS (JAN 1 TO JUL 31) OR GRAIN RYE (AUG 1 TO DEC 31)						



1 09/19/23 Response to CSC Interrogatories

Rev. #:	Date	Description
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SOLLI ENGINEERING
501 Main Street, Monroe, CT 06468 T: (203) 880-5455 F: (203) 880-9695
11 Vanderbilt Ave, Norwood, MA 02062 T: (781) 352-8491 F: (203) 880-9695

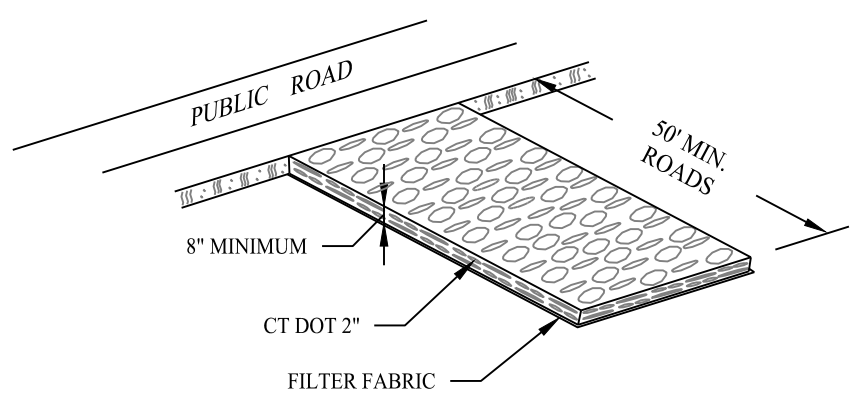
Drawn By: AWC
Checked By: CJB
Approved By: KMS
Project #: 22112201
Plan Date: 04/18/23
Scale: 1" = 40'

STATE OF CONNECTICUT
Professional Engineer
Kevin Solli, P.E.
CT 25759

PROPOSED SOLAR PHOTOVOLTAIC ARRAY
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Sheet Title: GRADING & DRAINAGE PLAN
Sheet #: 2.21





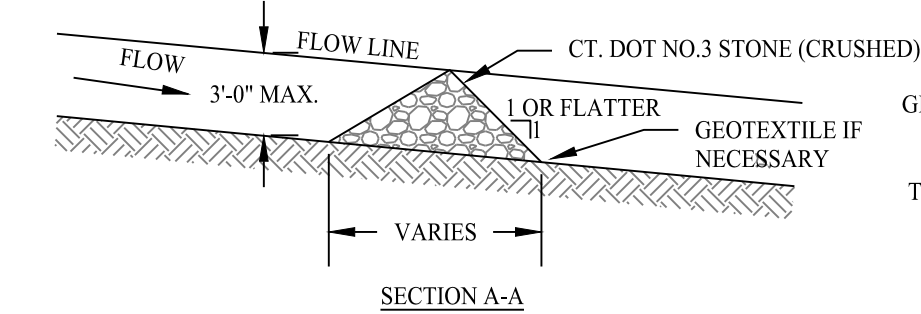
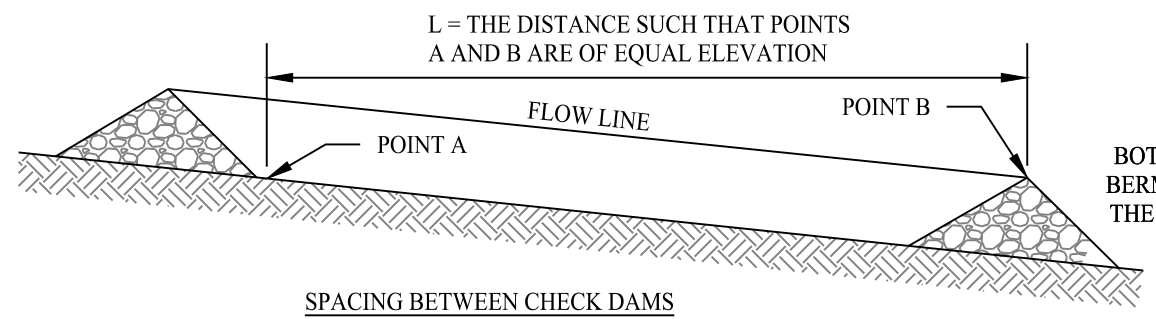
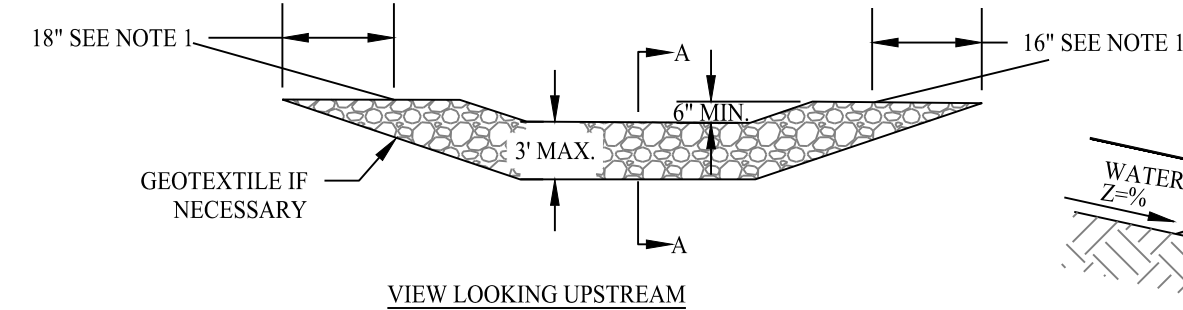
GRADATION TABLE

SQUARE MESH SIEVES	CONN. DOT 2" CRUSHED GRAVEL		ASTM C-33 NO. 2		ASTM C-33 NO. 3	
	% FINER	% FINER	% FINER	% FINER	% FINER	% FINER
2 1/2 INCHES	100	95-100	90-100	100	90-100	100
2 INCHES	95-100	35-70	0-15	35-70	0-15	35-70
1 1/2 INCHES	0-25	—	—	—	—	—
1 1/4 INCHES	0-10	—	—	—	—	—
1 INCHES	—	—	—	—	—	—
3/4 INCHES	—	—	—	—	—	—
1/2 INCHES	—	—	—	—	—	—
3/8 INCHES	—	—	—	—	—	—

SOURCE:
U.S. DEPARTMENT OF AGRICULTURE, SOIL CONSERVATION SERVICE,
STORRS, CONNECTICUT

CONSTRUCTION ENTRANCE

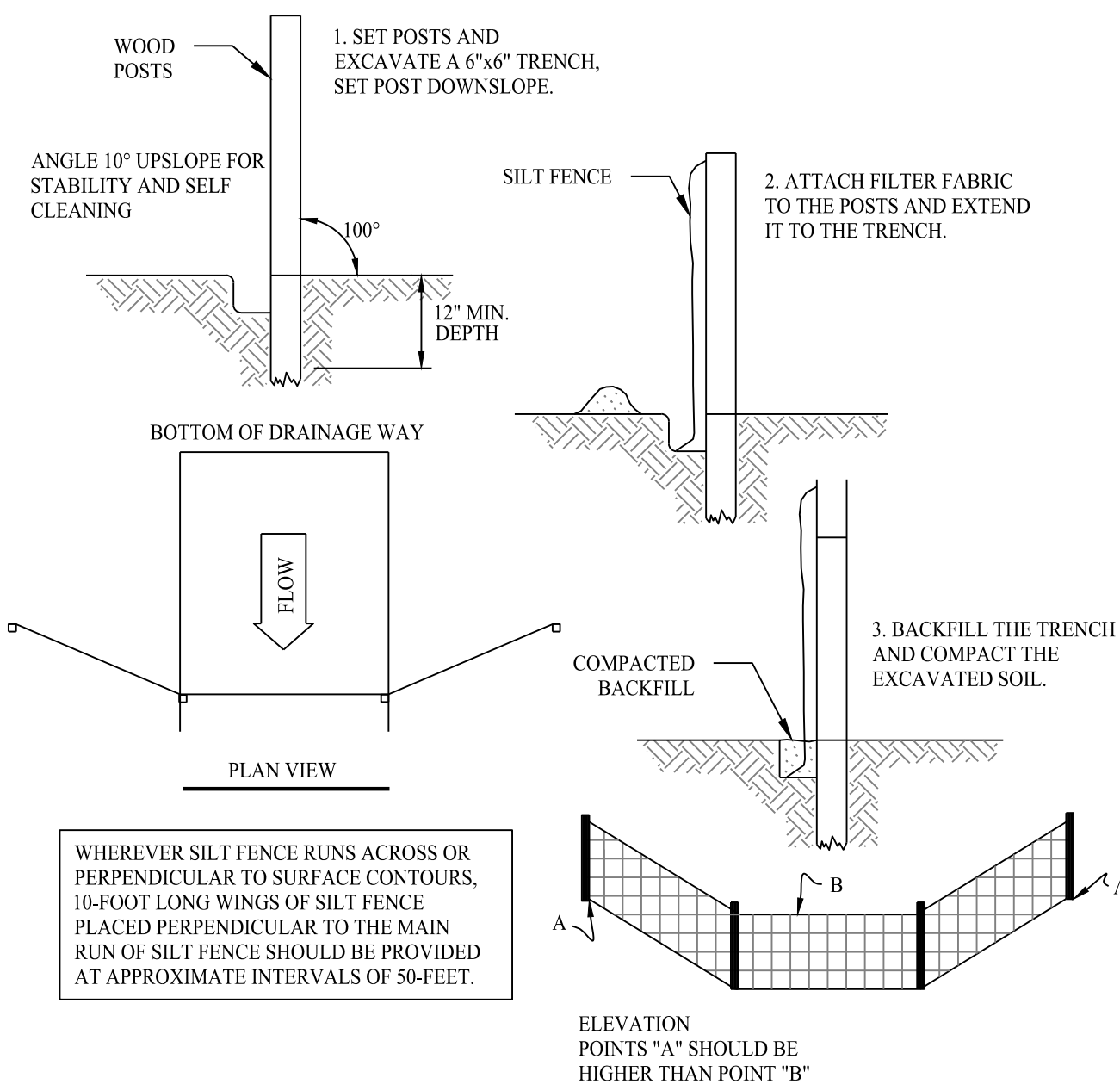
SCALE: NTS



- NOTES:
- KEY STONE INTO THE DITCH BANKS AND EXTEND INTO THE ABUTMENTS A MINIMUM OF 18" TO PREVENT FLOW FROM FLANKING THE DAM.
 - THE MINIMUM DESIGN CAPACITY SHALL CONVEY A 2 YEAR-24 HOUR PEAK FLOW.

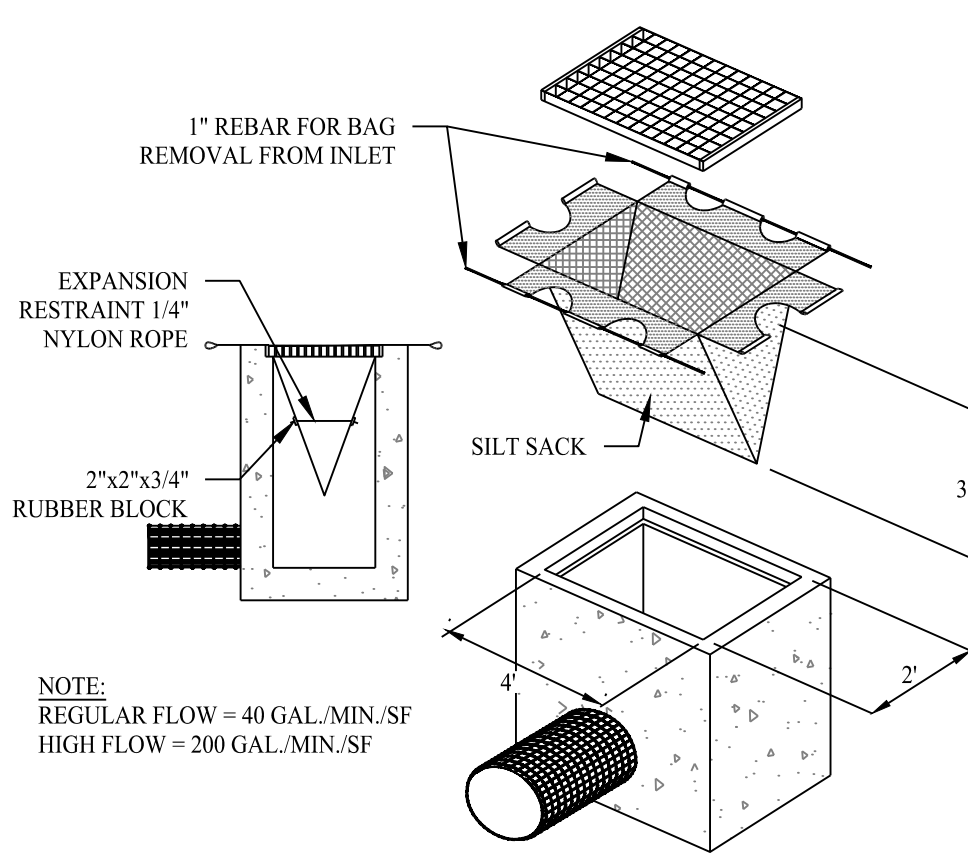
STONE CHECK DAM DETAIL

SCALE: NTS



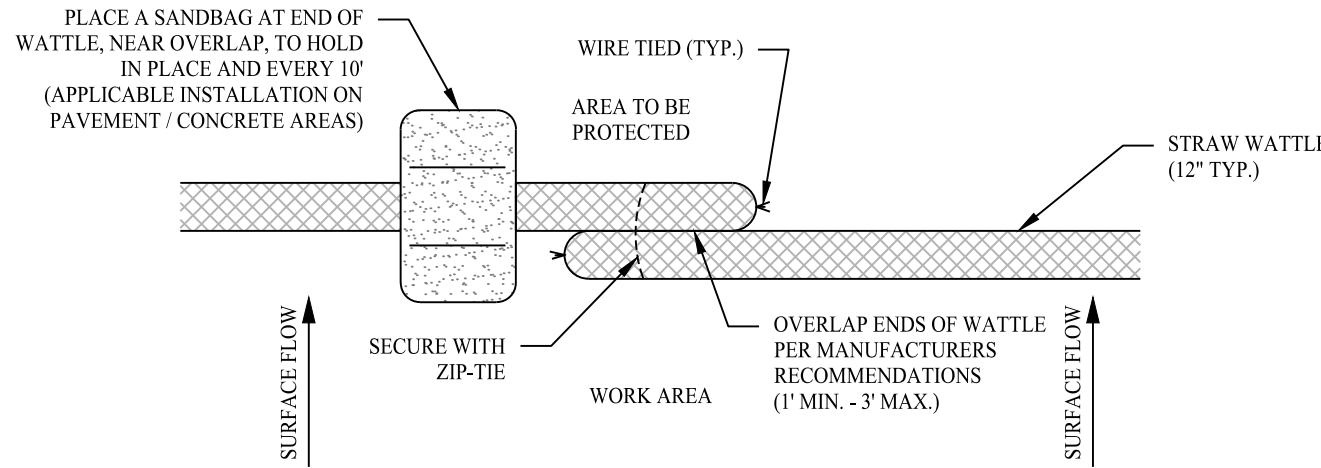
SILT FENCE PROTECTION DETAIL

SCALE: NTS



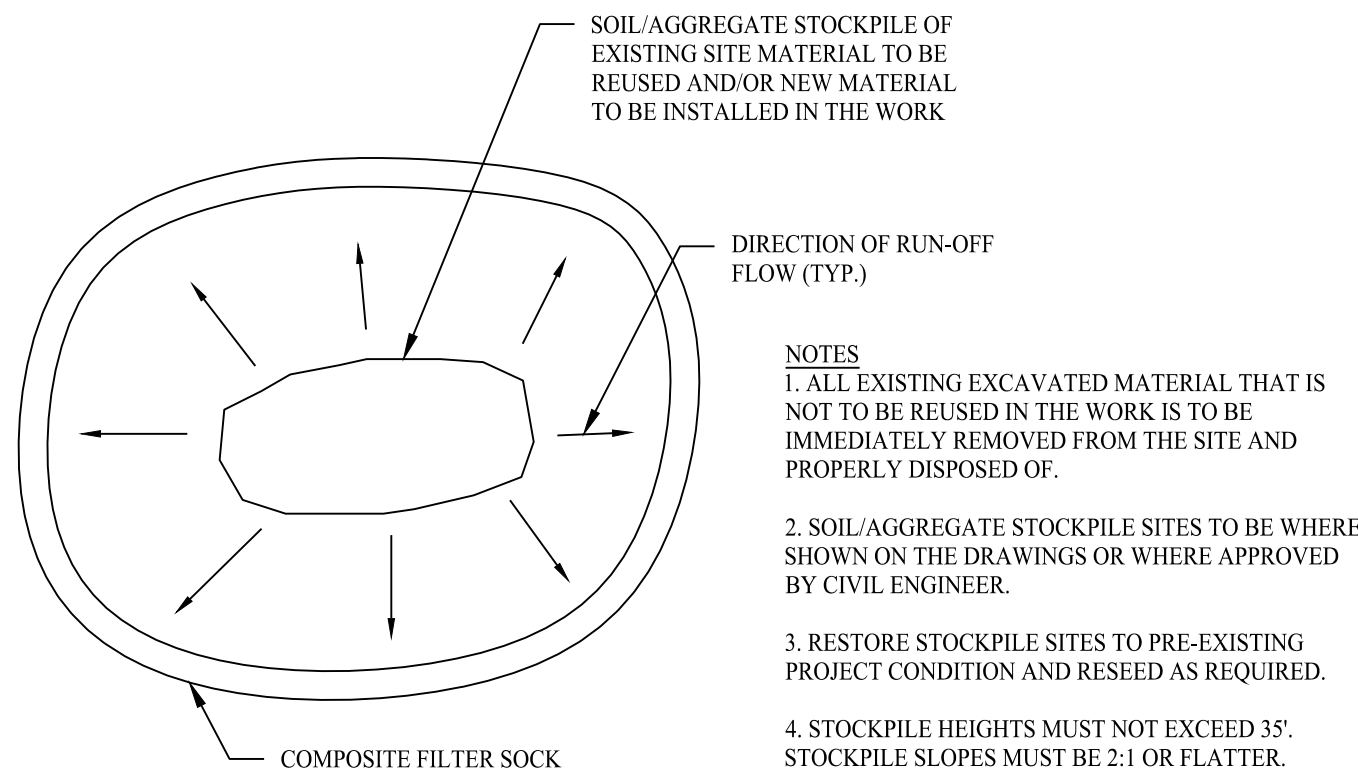
SILT SACK DETAIL

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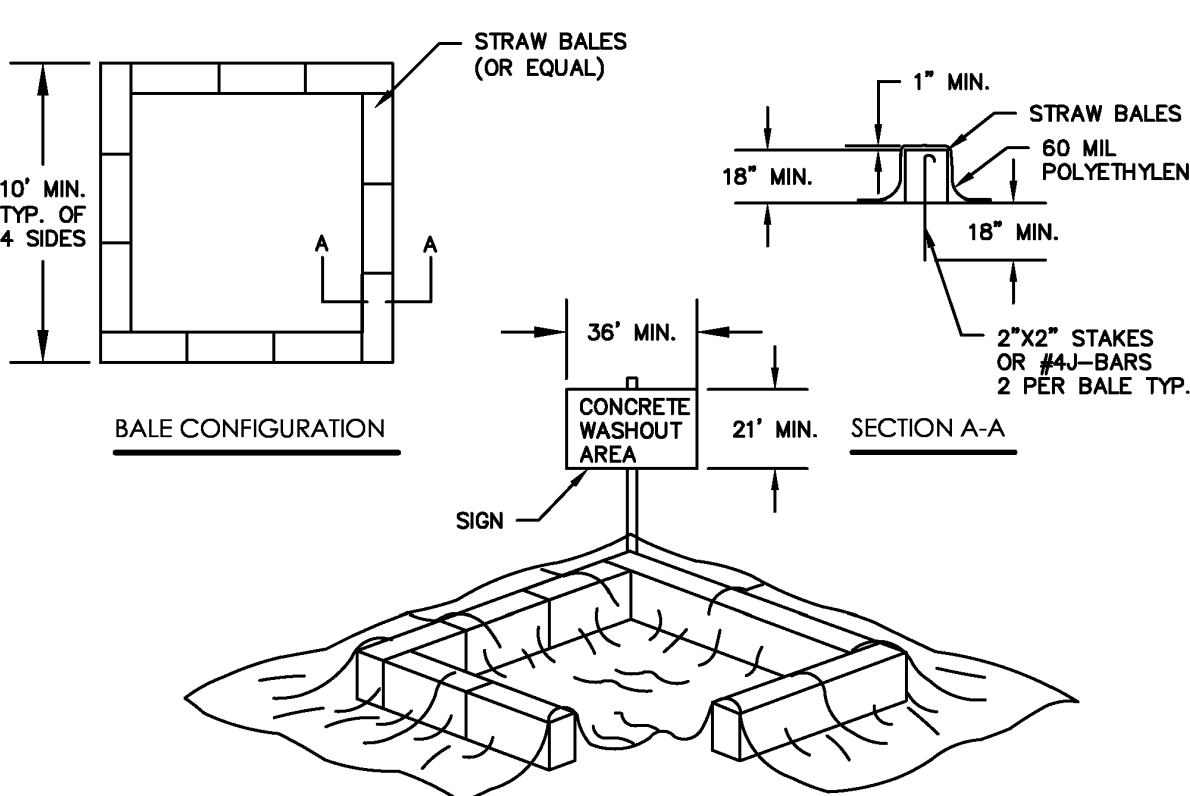
COMPOSITE FILTER SOCK

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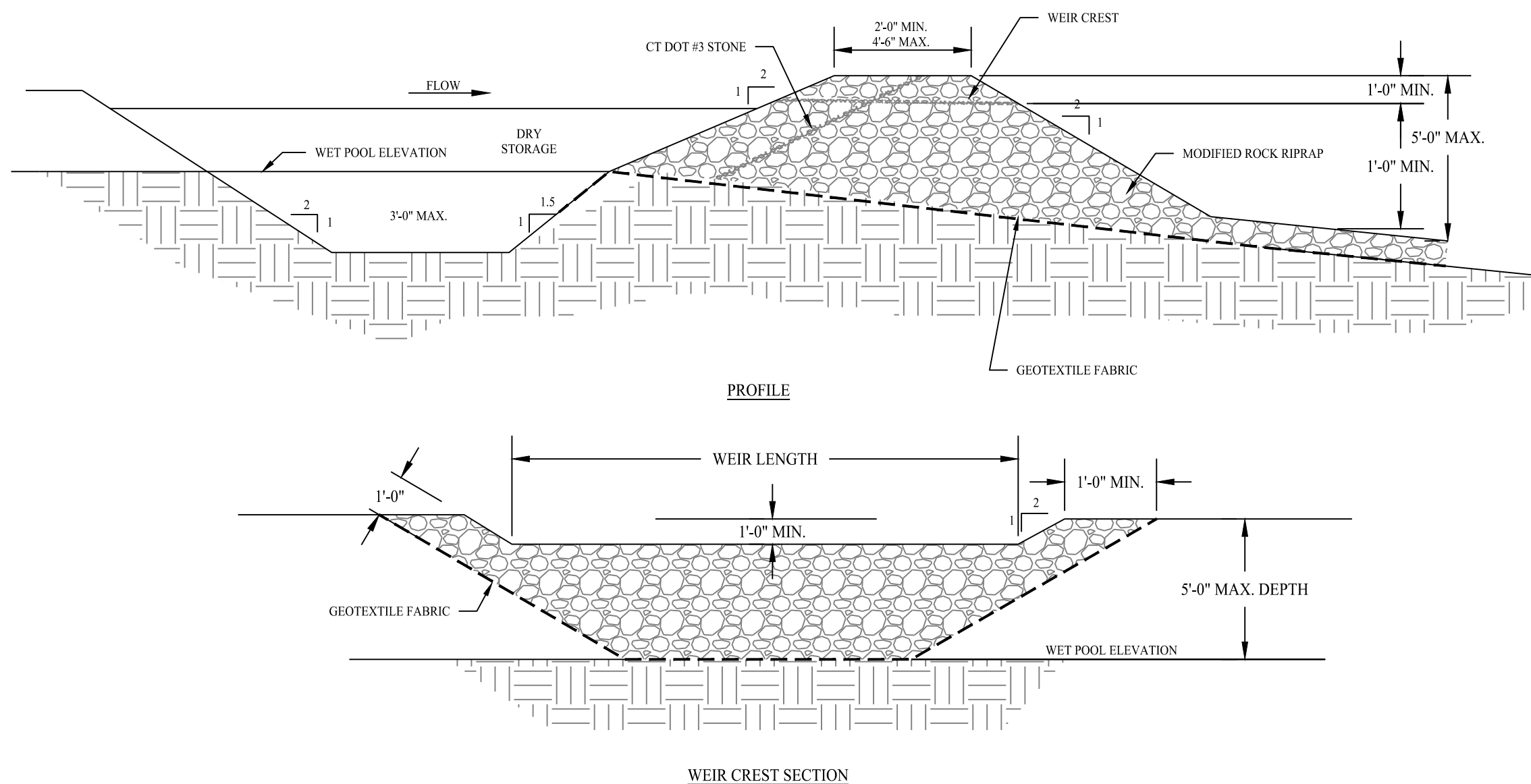
MATERIALS STOCKPILE DETAIL

SCALE: NTS



CONCRETE WASHOUT PIT

SCALE: NTS



EMERGENCY SPILLWAY DETAIL

SCALE: NTS

SOIL EROSION & SEDIMENT CONTROL NOTES

SEDIMENT & EROSION CONTROL NARRATIVE

THE SEDIMENT AND EROSION CONTROL PLAN WAS DEVELOPED TO PROTECT THE EXISTING ROADWAY AND STORM DRAINAGE SYSTEMS, ADJACENT PROPERTIES, AND ANY ADJACENT WETLAND AREA AND WATER COURSE FROM SEDIMENT LADEN SURFACE RUNOFF AND EROSION.

CONSTRUCTION SCHEDULE

THE ANTICIPATED STARTING DATE FOR CONSTRUCTION IS SPRING 2024 WITH COMPLETION ANTICIPATED BY FALL 2024. APPROPRIATE EROSION CONTROL MEASURES AS DESCRIBED HEREIN, SHALL BE INSTALLED BY THE CONTRACTOR PRIOR TO THE COMMENCEMENT OF ALL SITE CLEARING OR CONSTRUCTION ACTIVITY. SCHEDULE WORK TO MINIMIZE THE LENGTH OF TIME THAT BARE SOIL WILL BE EXPOSED.

CONTINGENCY EROSION PLAN

THE CONTRACTOR SHALL INSTALL ALL SPECIFIED EROSION CONTROL MEASURES AND WILL BE REQUIRED TO MAINTAIN THEM IN THEIR INTENDED FUNCTIONING CONDITION. THE AGENTS OF THE SOUTHWEST CONSERVATION DISTRICT AND ENGINEER OF RECORD SHALL HAVE THE AUTHORITY TO REQUIRE SUPPLEMENTAL MAINTENANCE OR ADDITIONAL MEASURES IF FIELD CONDITIONS ARE ENCOUNTERED BEYOND WHAT WOULD NORMALLY BE ANTICIPATED.

OPERATION REQUIREMENTS

CLEARING, GRUBBING & DEMOLITION OPERATIONS:

- ALL SEDIMENTATION AND EROSION CONTROL MEASURES WILL BE INSTALLED PRIOR TO THE START OF CLEARING, GRUBBING AND DEMOLITION OPERATIONS.
- FOLLOWING INSTALLATION OF ALL SEDIMENTATION AND EROSION CONTROL MEASURES, THE CONTRACTOR SHALL NOT PROCEED WITH GRADING, FILLING OR OTHER CONSTRUCTION OPERATIONS UNTIL THE ENGINEER OF RECORD HAS INSPECTED AND APPROVED ALL INSTALLATIONS.
- THE CONTRACTOR SHALL TAKE EXTREME CARE DURING CLEARING, GRUBBING AND DEMOLITION OPERATIONS SO AS NOT TO DISTURB SEDIMENTATION AND EROSION CONTROL DEVICES AS WELL AS EXISTING LANDSCAPED AREAS.
- FOLLOWING THE COMPLETION OF CLEARING, GRUBBING AND DEMOLITION OPERATIONS, ALL AREAS SHALL BE STABILIZED WITH TOPSOIL AND SEEDING, PROCESSED AGGREGATE STONE OR DISPERSED HAY AS SOON AS PRACTICAL.

PLACEMENT OF DRAINAGE STRUCTURES, UTILITIES, AND ROADWAY CONSTRUCTION OPERATIONS:

- SILT FENCES SHALL BE INSTALLED AT THE DOWNHILL SIDES OF TEMPORARY TRAPS, MUD PUMP DISCHARGES, AND UTILITY TRENCH MATERIAL STOCKPILES. HAY BALES MAY BE USED IF SHOWN ON THE EROSION CONTROL PLANS OR IF DIRECTED BY THE ENGINEER OF RECORD.

FINAL GRADING AND PAVING OPERATIONS:

- ALL INLET AND OUTLET PROTECTION SHALL BE PLACED AND MAINTAINED AS SHOWN ON EROSION CONTROL PLANS AND DETAILS, AND AS DESCRIBED IN SPECIFICATIONS AND AS DESCRIBED HEREIN.
- NO CUT OR FILL SLOPES SHALL EXCEED 2:1 EXCEPT WHERE STABILIZED BY ROCK FACED EMBANKMENTS OR EROSION CONTROL BLANKETS, JUTE MESH AND VEGETATION. ALL SLOPES SHALL BE SEED, AND ANY ROAD OR DRIVEWAY SHOULDER AND BANKS SHALL BE STABILIZED IMMEDIATELY UPON COMPLETION OF FINAL GRADING UNTIL TURF IS ESTABLISHED.
- PAVEMENT SUB-BASE AND BASE COURSES SHALL BE INSTALLED OVER AREAS TO BE PAVED AS SOON AS FINAL SUB-GRADES ARE ESTABLISHED AND UNDERGROUND UTILITIES AND STORM DRAINAGE SYSTEMS HAVE BEEN INSTALLED.
- AFTER CONSTRUCTION OF PAVEMENT, TOPSOIL, FINAL SEEDING, MULCH AND LANDSCAPING, REMOVE ALL TEMPORARY EROSION CONTROL DEVICES ONLY AFTER ALL AREAS HAVE BEEN PAVED AND/OR GRASS HAS BEEN WELL ESTABLISHED AND THE SITE HAS BEEN INSPECTED AND APPROVED BY THE TOWN OF BETHANY LAND USE AGENT AND/OR ENGINEER OF RECORD.

INSTALLATION OF SEDIMENTATION AND EROSION CONTROL MEASURES

I. SILTATION FENCE:

- DIG A SIX INCH TRENCH ON THE UPHILL SIDE OF THE DESIGNATED FENCE LINE LOCATION.
- POSITION THE POST AT THE BACK OF THE TRENCH (DOWNHILL SIDE), AND HAMMER THE POST AT LEAST 1.5 FEET INTO THE GROUND.
- LAY THE BOTTOM SIX INCHES OF THE FABRIC INTO THE TRENCH TO PREVENT UNDERMINING BY STORM WATER RUN-OFF.

II. SILT SACK INLET PROTECTION:

- REMOVE ALL DAMAGED BASIN GRATE AND PROPERLY PLACE THE SILT SACK INTO THE FRAME OF THE CATCH BASIN.
- PLACE GRATE BACK ONTO FRAME AND ENSURE NO PORTIONS OF THE SILT SACK HAVE SAGGED INTO THE CATCH BASIN.
- ONCE GRATE IS PLACED BACK ONTO FRAME OBSERVE TO SEE IF SILT SACK IS INSTALLED IN A MANNER THAT WILL ALLOW FOR SEDIMENT TO BE FILTERED OUT DURING STORM EVENTS.

III. COMPOSITE FILTER SOCK:

- COMPOSITE FILTER SOCK TO BE PLACED IN ACCORDANCE WITH SHEET 2.3.1. ALL DAMAGED SOCKS AND POSTS SHALL BE REPLACED AND PROPERLY REPOSITIONED AS NECESSARY.
- COMPOSITE FILTER SOCK TO BE SECURED BY EITHER SAND BAG (IMPERVIOUS AREAS) OR BY WOOD STAKE HAMMERED INTO GROUND (PERVIOUS AREAS).
- SEDIMENT DEPOSITS SHALL BE REMOVED FROM BEHIND THE FENCE WHEN THEY EXCEED 3-4 INCHES IN HEIGHT.

IV. CONSTRUCTION ENTRANCE:

- REMOVE ALL VEGETATION AND OTHER MATERIALS FROM THE FOUNDATION AREA. GRADE AND CROWN FOUNDATION FOR POSITIVE DRAINAGE.
- PLACE 1-3" STONE A MINIMUM OF 100FT ALONG THE FULL WIDTH OF THE CONSTRUCTION ACCESS ROAD. AGGREGATE SHOULD BE PLACED AT LEAST 6" THICK.
- GEOTEXTILE FILTER FABRIC SHALL BE PLACED BETWEEN STONE FILL AND EARTH SURFACE TO REDUCE THE MIGRATION OF SOIL PARTICLES FROM THE UNDERLYING SOIL INTO THE STONE AND VICE VERSA.
- ALL SURFACE WATER THAT IS FLOWING TO OR DIVERTED TOWARD THE CONSTRUCTION ENTRANCE SHALL BE PIPED BENEATH THE ENTRANCE.
- FILTER FABRIC FENCE SHALL BE INSTALLED DOWN GRADIENT FROM THE CONSTRUCTION ENTRANCE IN ORDER TO CONTAIN ANY SEDIMENT-LADEN RUNOFF FROM THE ENTRANCE.

V. CHECK DAM

- CHECK DAMS MAY BE CONSTRUCTED OF ROCK, SAND BAGS FILLED WITH PEA GRAVEL, OR LOGS.
- ENSURE DAMS ARE SPACED SO THAT THE ELEVATION OF THE TOE OF THE UPSTREAM DAM IS EQUAL TO THE ELEVATION OF THE TOP OF THE DOWNSTREAM DAM.
- LOG DAMS SHALL BE CONSTRUCTED OF UP TO 6-INCH DIAMETER LOGS EMBEDDED AT LEAST 18 INCHES DEEP INTO THE SOIL.
- PLACE ROCK BY HAND OR MECHANICALLY TO ENSURE COMPLETE COVERAGE OF SWALE.

OPERATION AND MAINTENANCE OF SEDIMENTATION AND EROSION CONTROL MEASURES

I. SILTATION FENCE:

- ALL SILTATION FENCES SHALL BE INSPECTED AS A MINIMUM WEEKLY OR AFTER EACH RAINFALL. ALL DETERIORATED FABRIC AND DAMAGED POSTS SHALL BE REPLACED AND PROPERLY REPOSITIONED IN ACCORDANCE WITH THIS PLAN.
- SEDIMENT DEPOSITS SHALL BE REMOVED FROM BEHIND THE FENCE WHEN THEY EXCEED A HEIGHT OF ONE FOOT.

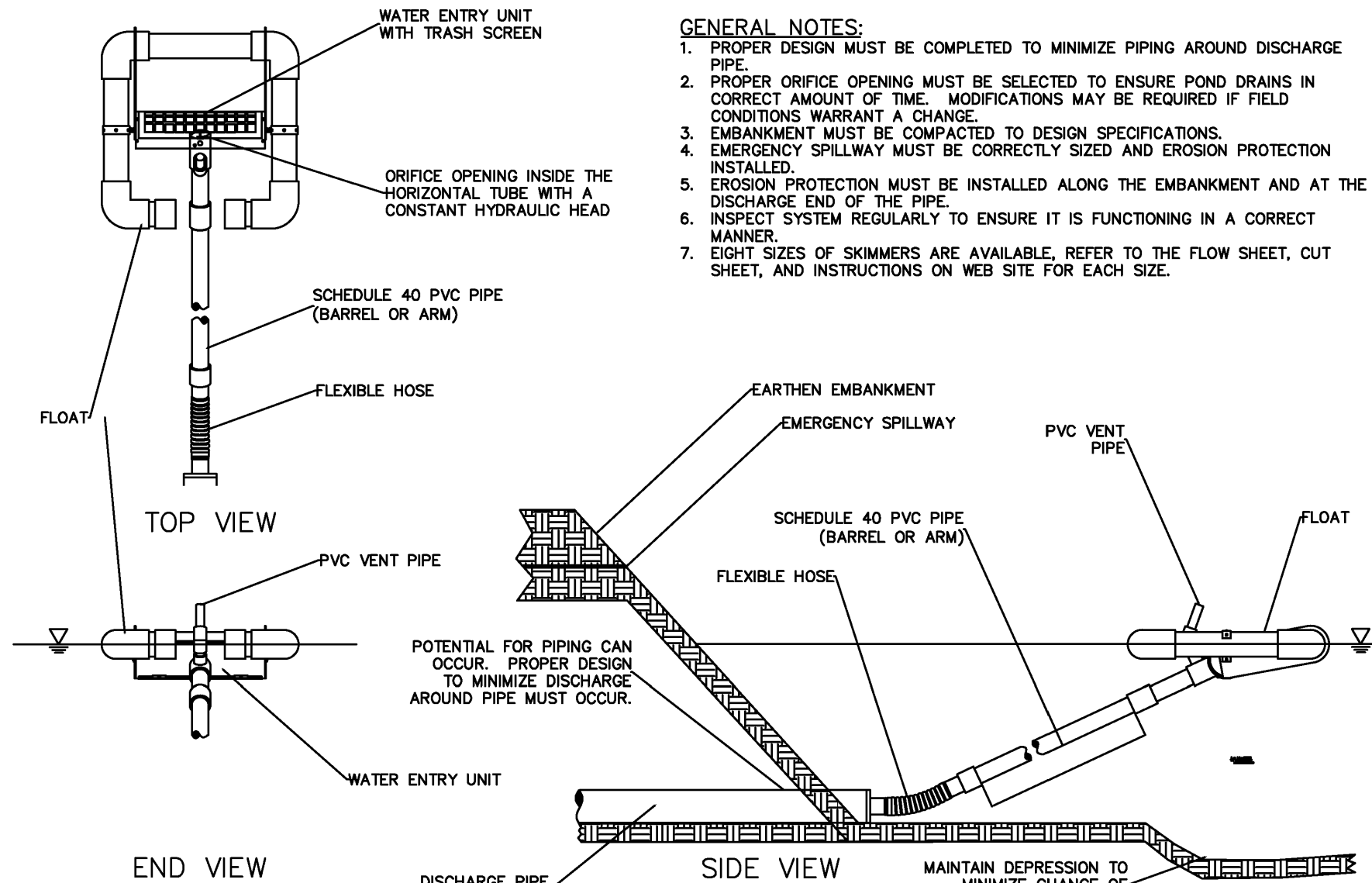
II. SILT SACK INLET PROTECTION:

- ALL SILT SACK INLET PROTECTION DEVICES SHALL BE INSPECTED AS A MINIMUM WEEKLY OR AFTER EACH RAINFALL. ALL DETERIORATED SILT SACKS AND SACKS THAT APPEAR TO HAVE AN EXCESS OF SEDIMENT SHALL BE REPLACED AND PROPERLY REPOSITIONED IN ACCORDANCE WITH THIS PLAN.
- SEDIMENT DEPOSITS SHALL BE REMOVED FROM THE SILT SACKS WHEN THEY EXCEED A COUPLE INCHES OF SEDIMENT WITHIN THE CATCH BASIN.

III. COMPOSITE FILTER SOCK:

- ALL COMPOSITE FILTER SOCKS SHALL BE INSPECTED AS A MINIMUM WEEKLY OR AFTER EACH RAINFALL. ALL DETERIORATED FABRIC AND DAMAGED POSTS SHALL BE REPLACED AND PROPERLY REPOSITIONED IN ACCORDANCE WITH THIS PLAN.
- SEDIMENT DEPOSITS SHALL BE REMOVED FROM THE SILT SACKS WHEN THEY EXCEED A HEIGHT OF 4 INCHES.

IV. CONSTRUCTION ENTRANCE:



FAIRCLOTH SKIMMER DISCHARGE SYSTEM

SCALE: NTS

PROVIDED BY: J. W. FAIRCLOTH & SON INC.

1	09/19/23	Response to CSC Interrogatories
Rev. #:	Date	Description

Graphic Scale:



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11 Vanderbilt Ave., Norwood, MA 02062 T: (781) 352-8491 F: (203) 880-9695

Drawn By: CMH

Checked By: CJB

Approved By: KMS

Project #: 22115201

Plan Date: 04/18/23

Scale: NTS

Project:

PROPOSED SOLAR PHOTOVOLTAIC ARRAY
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Sheet Title:

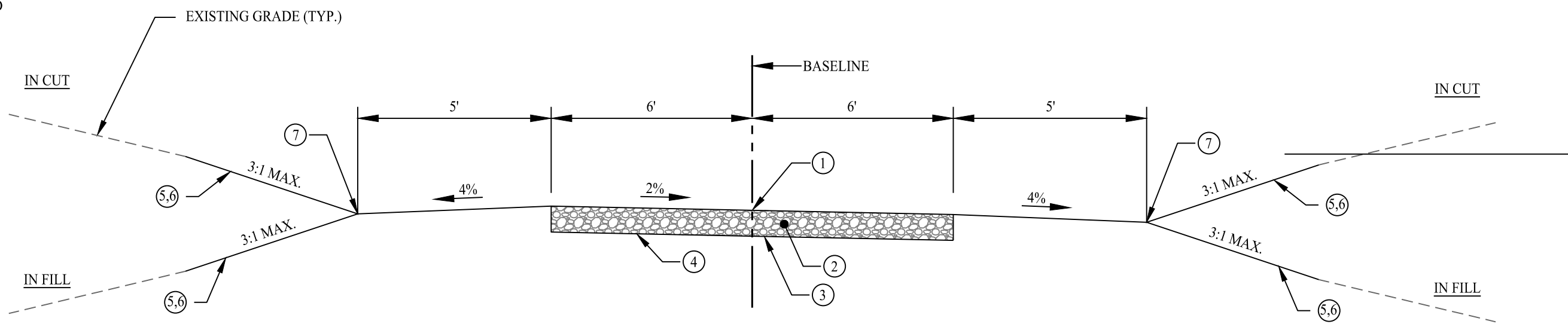
SOIL EROSION & SEDIMENT CONTROL NOTES & DETAILS

Sheet #:

2.41

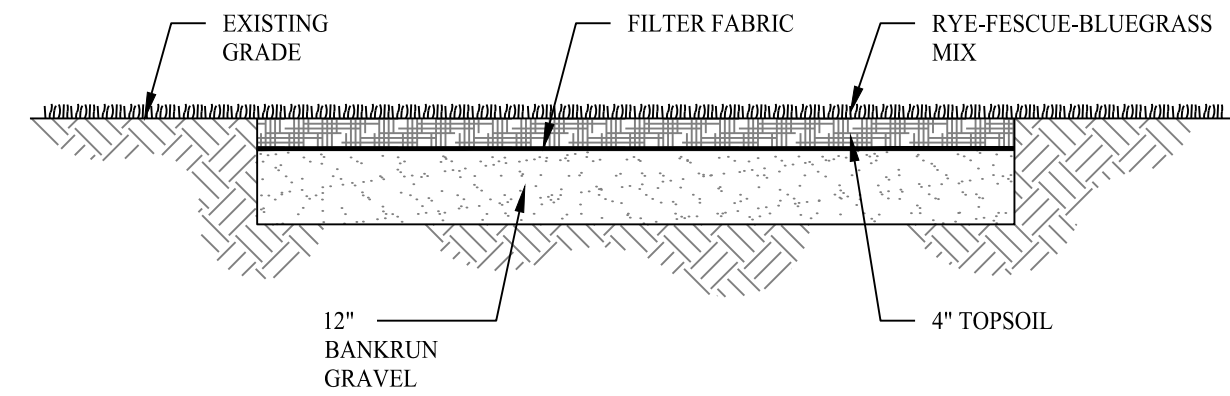
- ① POINT OF APPLICATION OF GRADE OR MATCH EXISTING GROUND
② 8" LAYER CRUSHER RUN GRAVEL
③ NONWOVEN GEOTEXTILE (MIRAFI 140N OR EQUAL)
④ LIMIT OF EXCAVATION OR LIMIT OF COMPACTION
⑤ EROSION CONTROL BLANKET ON SLOPES 3:1 OR GREATER
⑥ 6" TOPSOIL AND SEED
⑦ VEGETATED CHANNEL

NOTES:
1. THE CONTRACTOR SHALL CONTACT CT CALL BEFORE YOU DIG (CBYD) A MINIMUM OF 72 HOURS PRIOR TO BEGINNING CONSTRUCTION.
2. TRANSITIONS BETWEEN TYPICAL ACCESS ROAD SECTIONS SHALL OCCUR OVER 50 FEET. (TYPICAL)



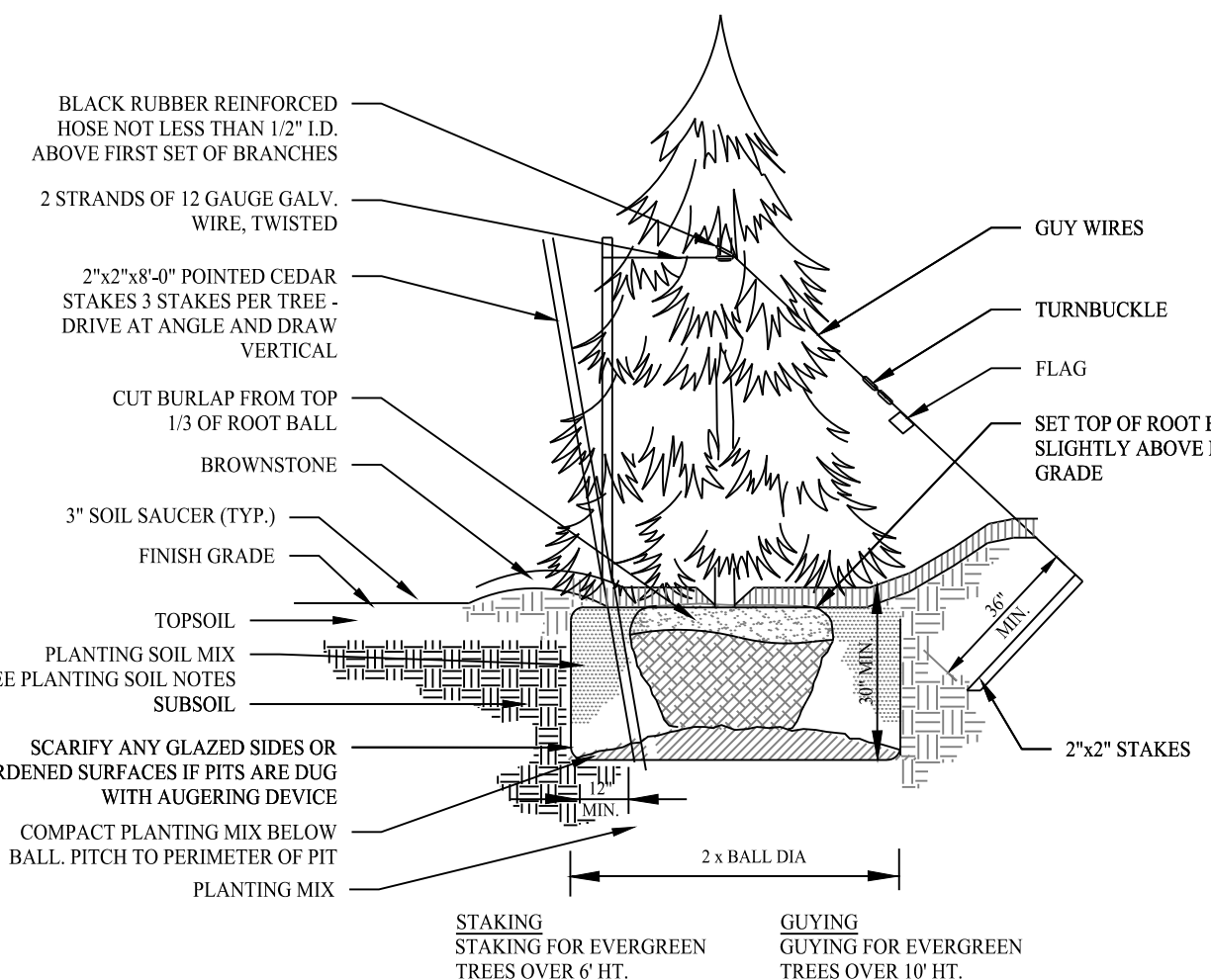
TYPICAL GRAVEL ROADWAY SECTION

SCALE: NTS



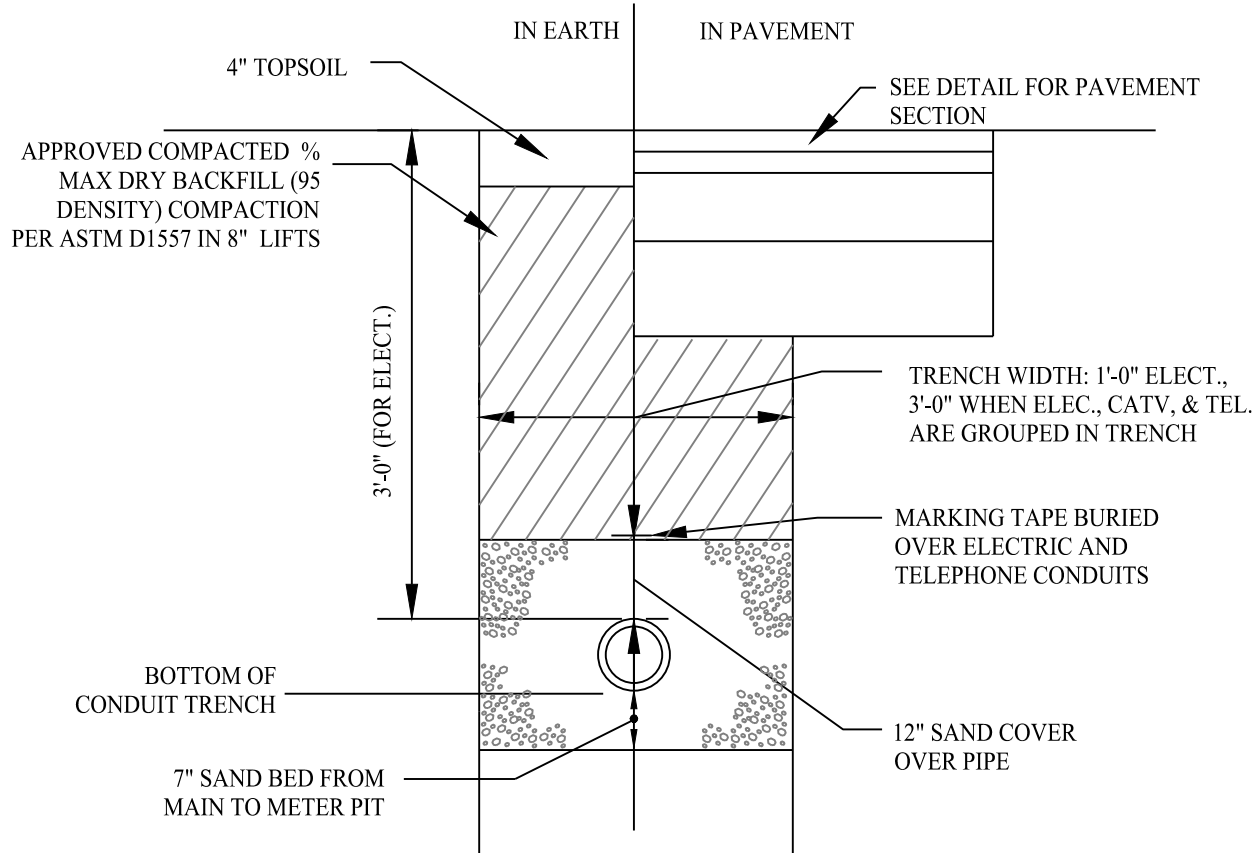
GRASS ACCESS DRIVE

SCALE: NTS



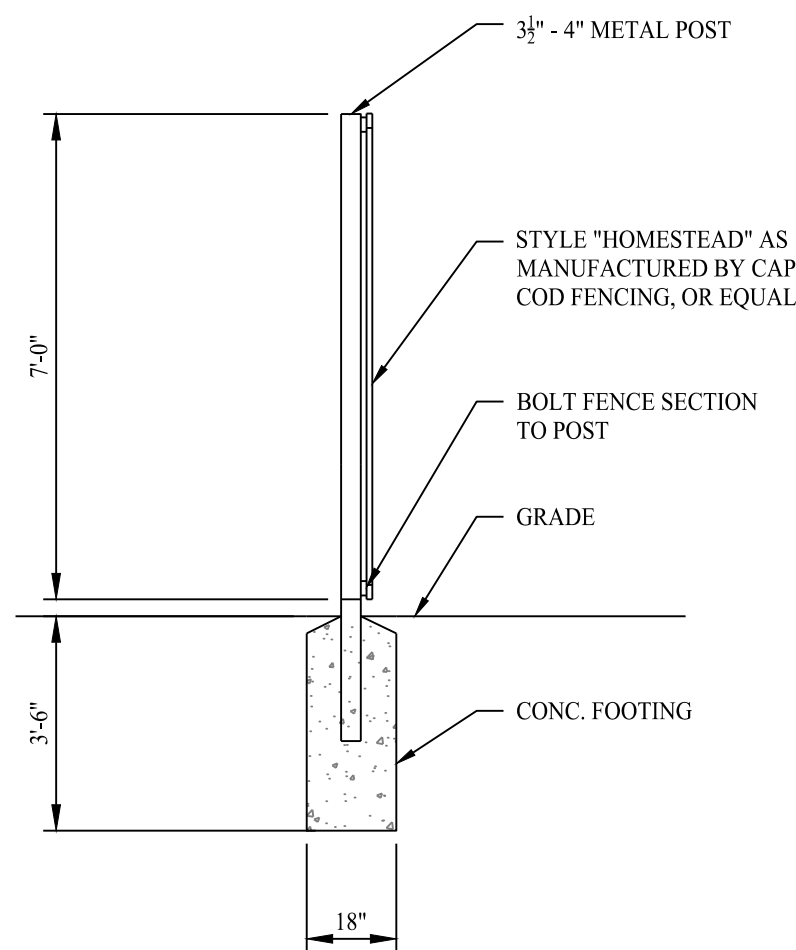
EVERGREEN TREE PLANTING

SCALE: NTS



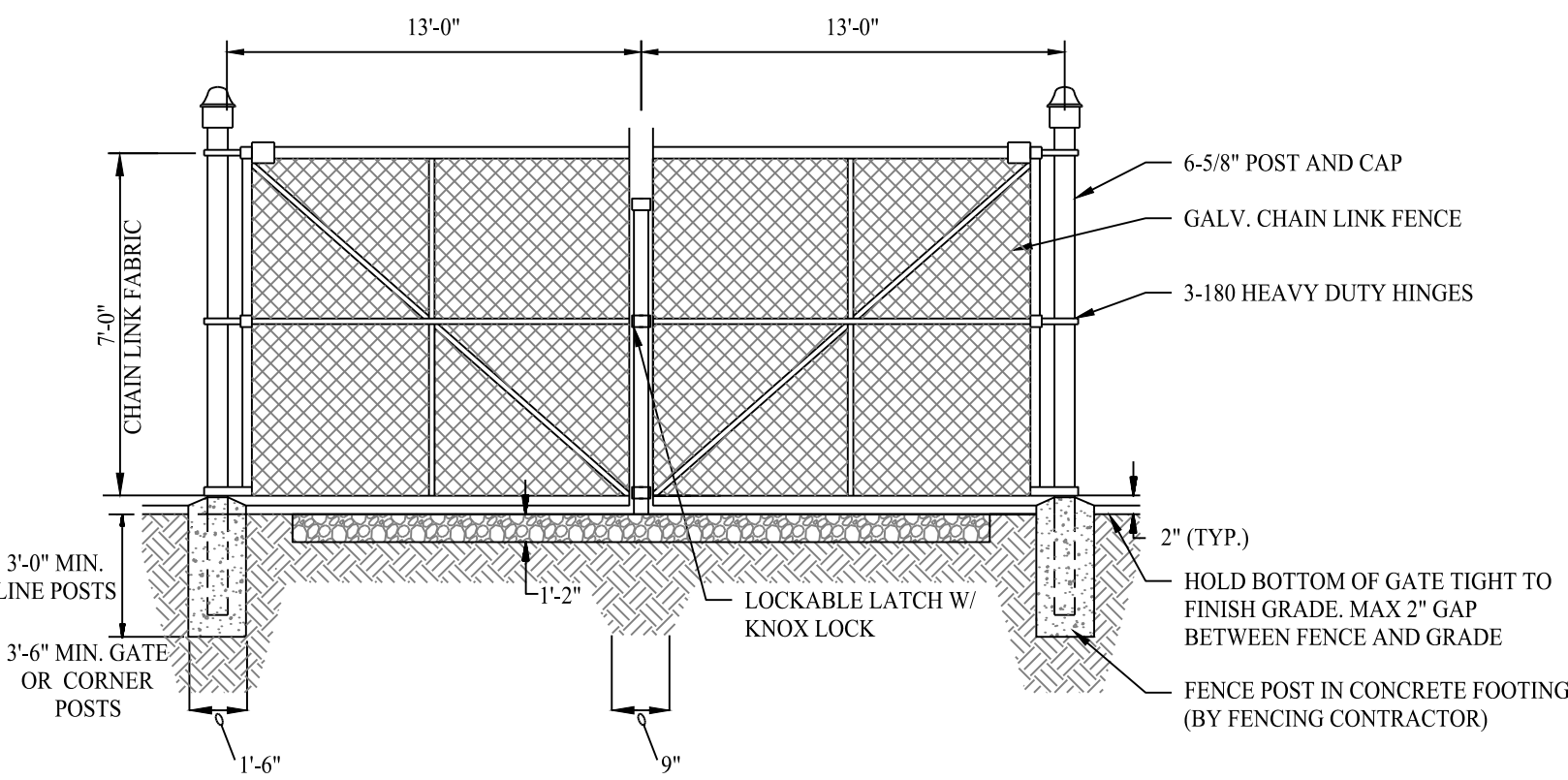
TYPICAL ELECTRICAL/TELEPHONE/CABLE AND GAS TRENCH

SCALE: NTS



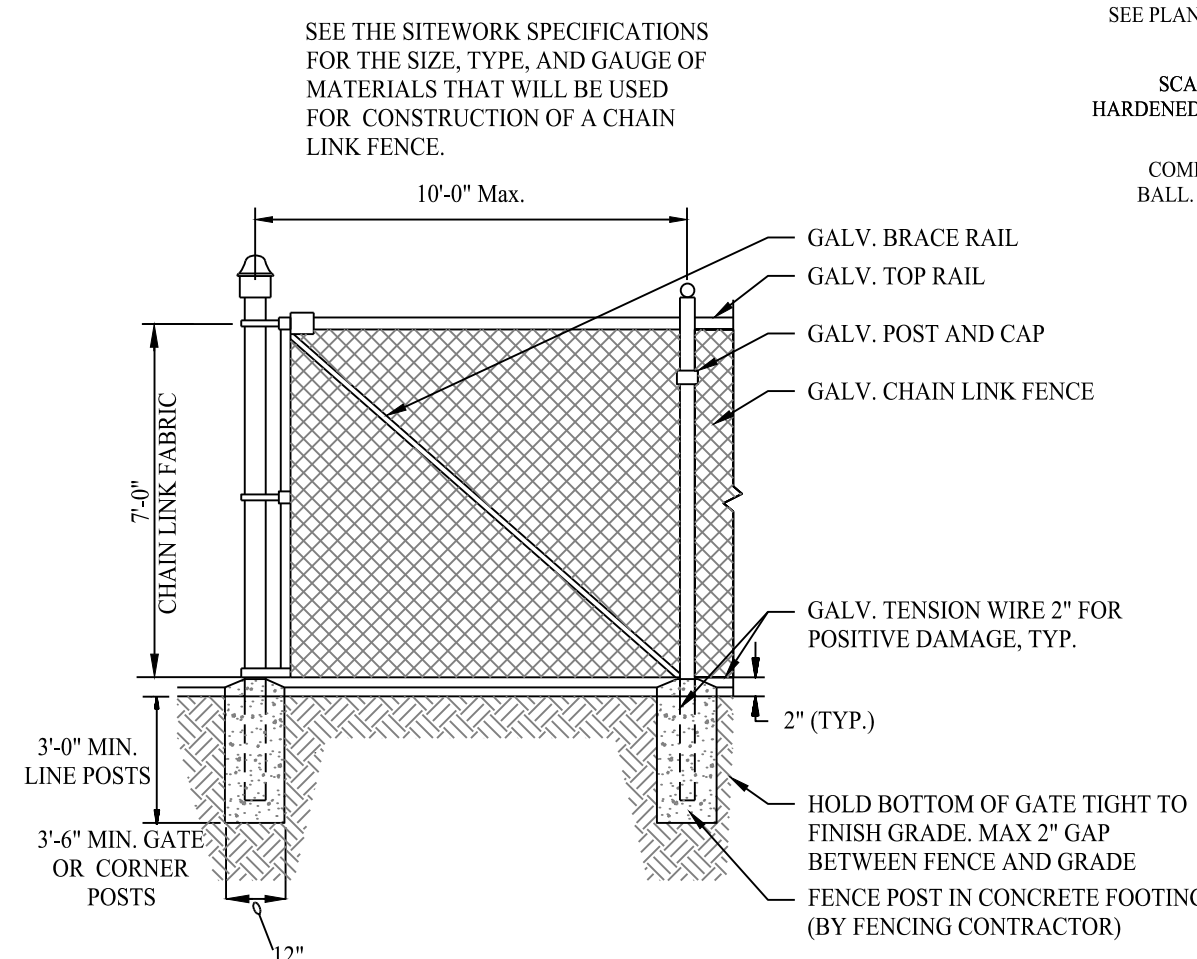
FENCE POST INSTALLATION

SCALE: NTS



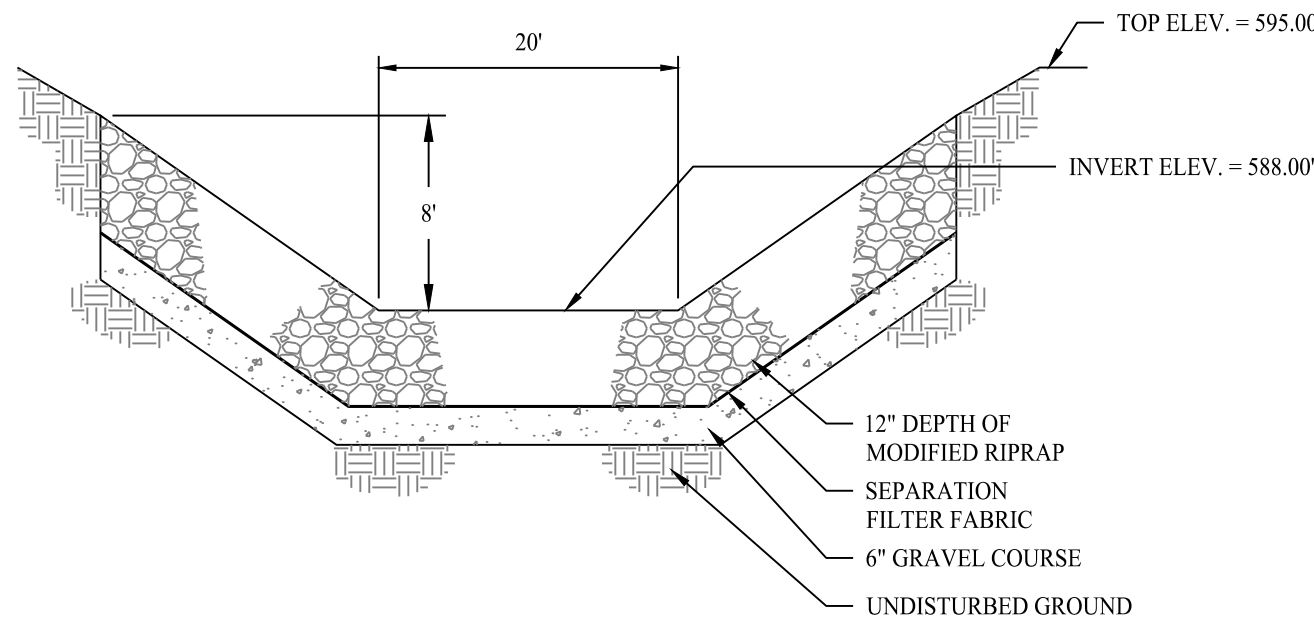
DOUBLE SWING GATE DETAIL

SCALE: NTS



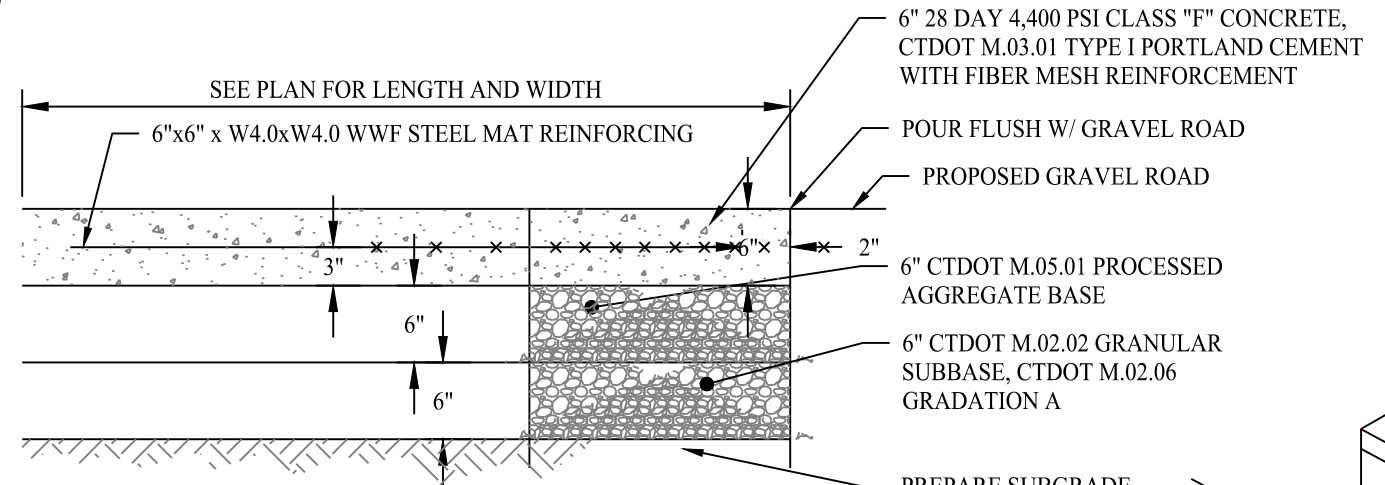
7' HIGH CHAIN LINK FENCE DETAIL

SCALE: NTS



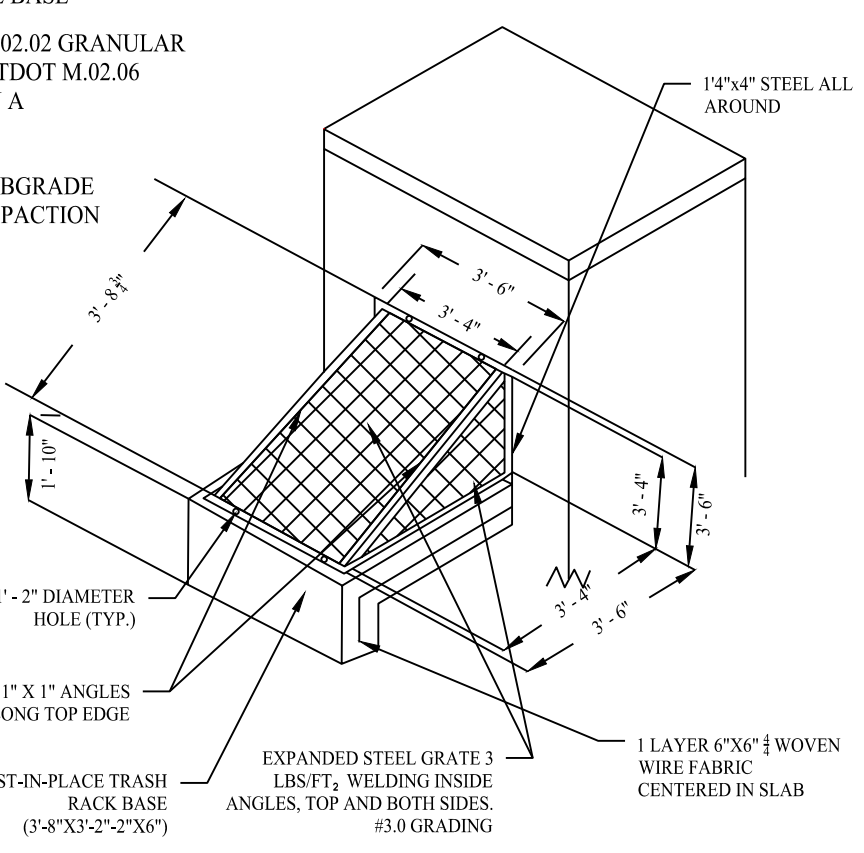
BROADCRESTED WEIR SPILLWAY

SCALE: NTS



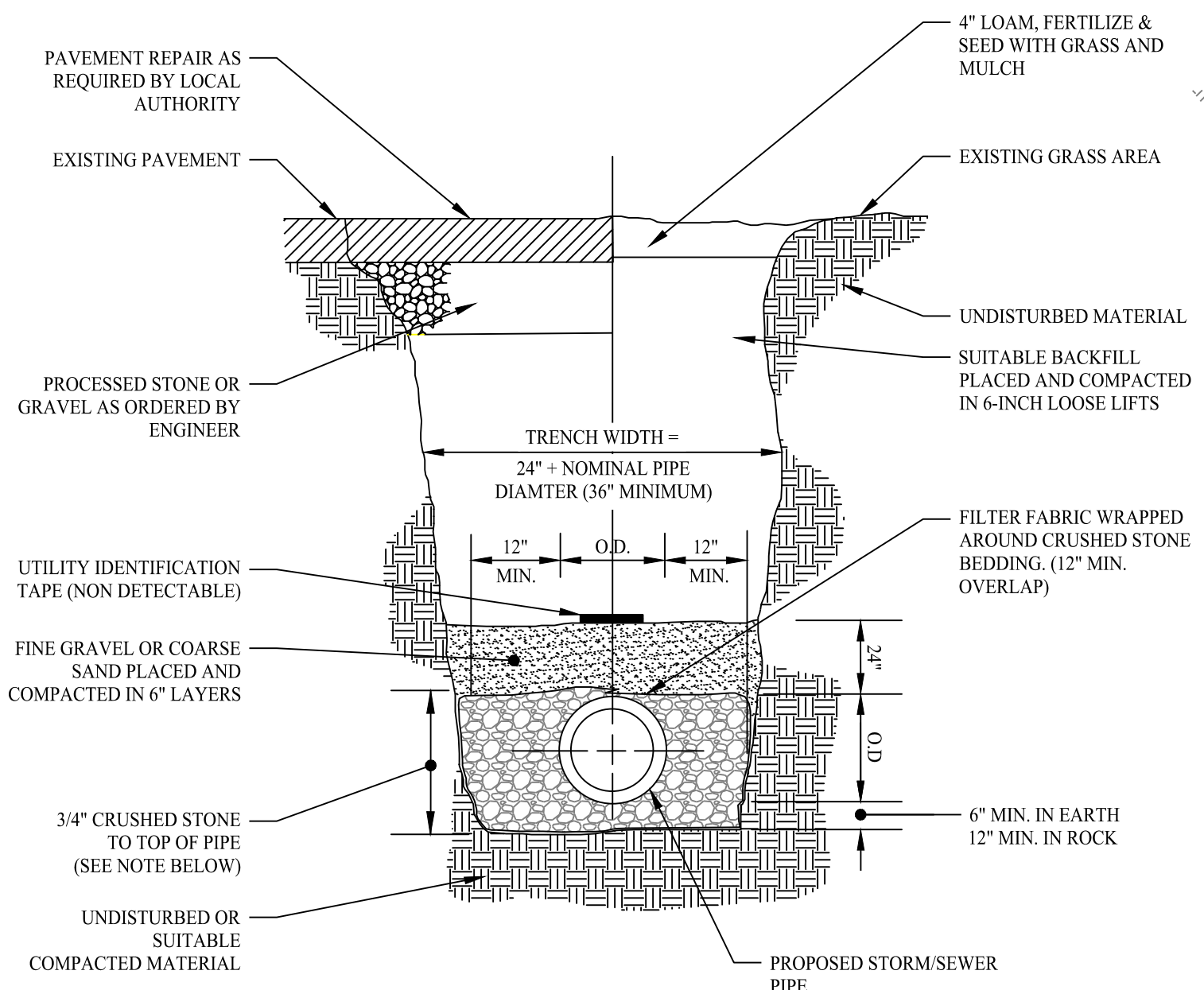
CONCRETE UTILITY PAD

SCALE: NTS



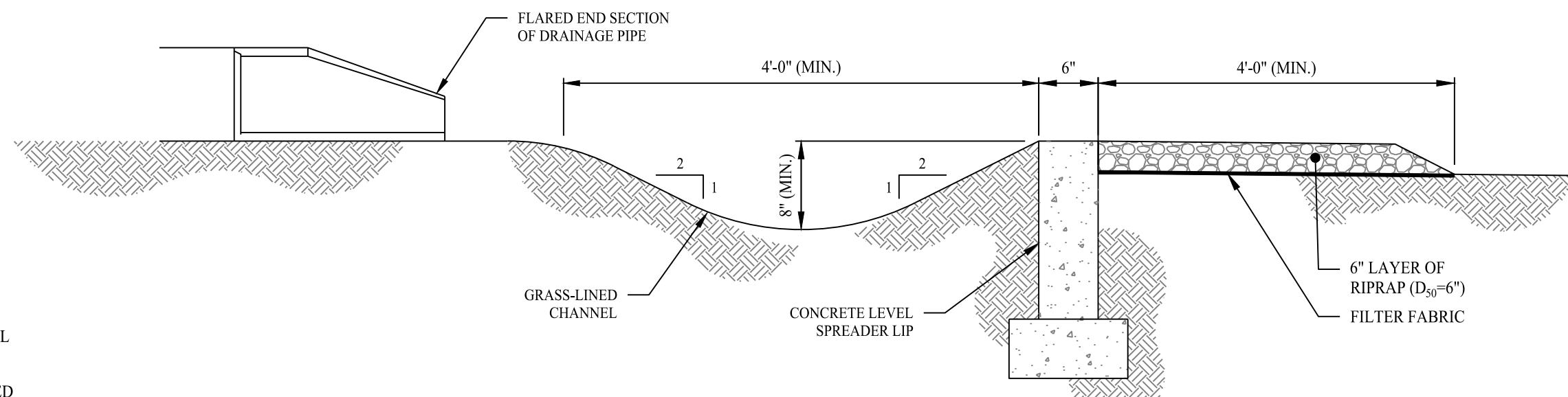
PRIMARY OUTLET TRASH RACK DETAIL

SCALE: NTS



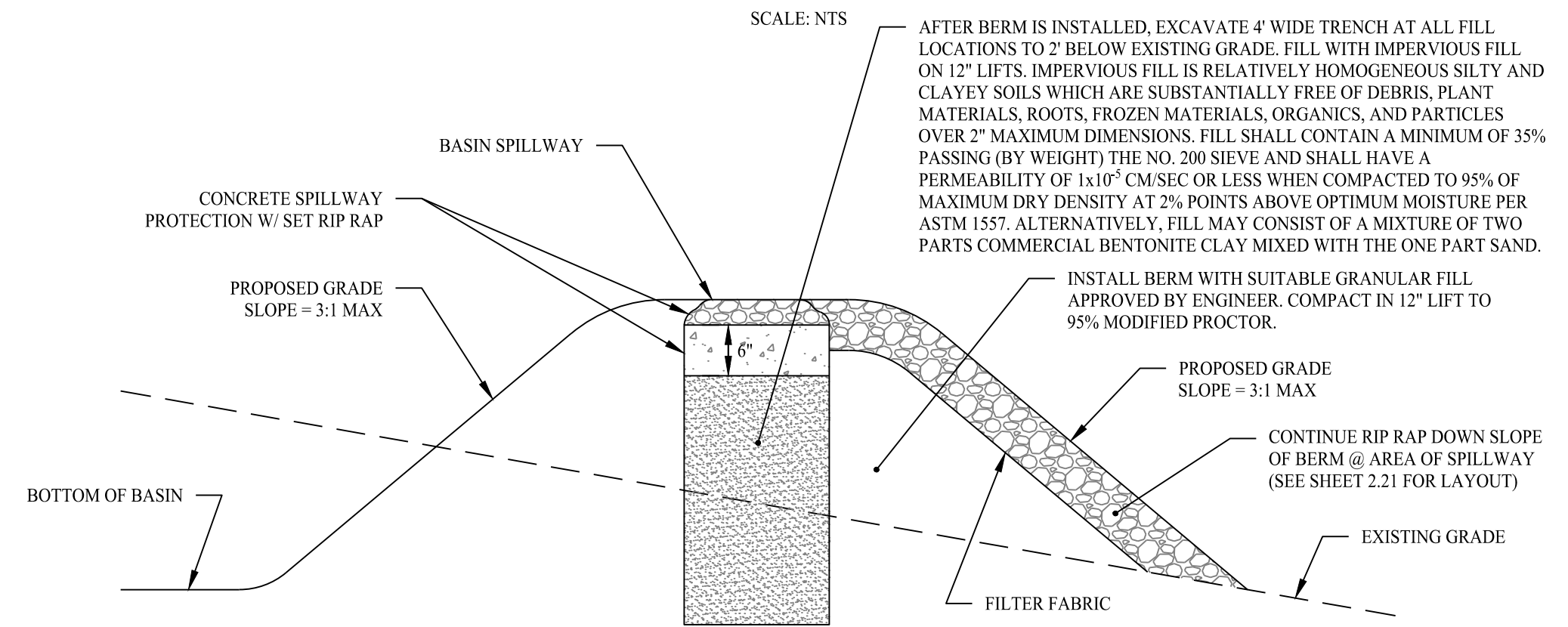
STORM TRENCH SECTION DETAIL

SCALE: NTS



LEVEL SPREADER DETAIL

SCALE: NTS



TYPICAL SPILLWAY IN FILL SECTION DETAIL

SCALE: NTS

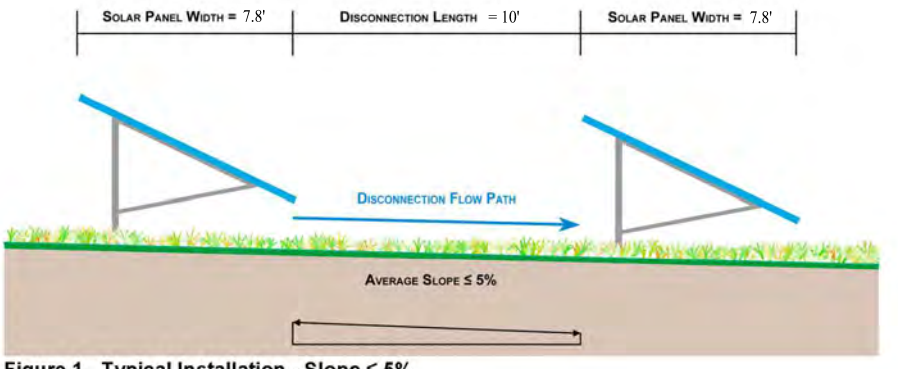


Figure 1. Typical Installation - Slope < 5%

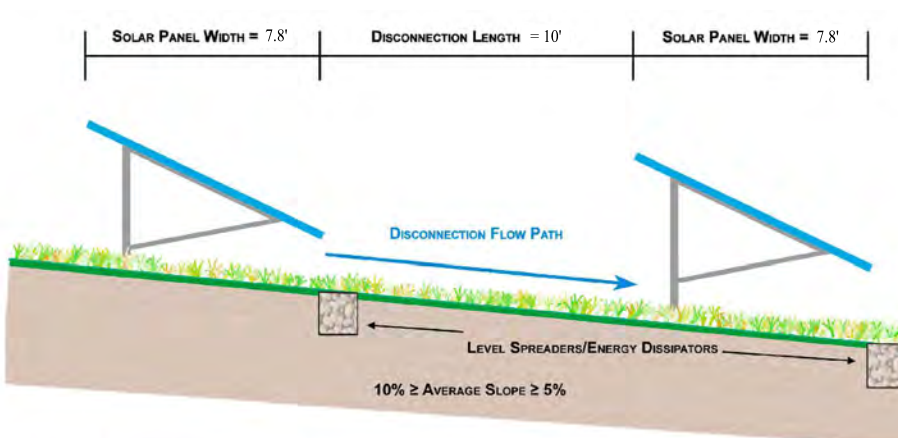


Figure 2. Typical Installation - Slope > 5% but < 10%

SOLAR ARRAY SPACING

SCALE: NTS

DETAIL PER MARYLAND DEPARTMENT OF THE ENVIRONMENT STORMWATER DESIGN GUIDE

1	09/19/23	Response to CSC Interrogatories
Rev. #:	Date	Description

Graphic Scale:



SOLLI ENGINEERING

501 Main Street, Moomoo, CT 06468 T: (203) 880-5455 F: (203) 880-9695
11 Vanderbilt Ave, Norwood, MA 02062 T: (781) 352-8491 F: (203) 880-9695

Drawn By: CMH
Checked By: CJB
Approved By: KMS
Project #: 22115201
Plan Date: 04/18/23
Scale: NTS



PROPOSED SOLAR PHOTOVOLTAIC ARRAY
428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Sheet Title: CONSTRUCTION DETAILS
Sheet #: 3.01

Appendix C: USFWS



United States Department of the Interior

FISH AND WILDLIFE SERVICE
New England Ecological Services Field Office
70 Commercial Street, Suite 300
Concord, NH 03301-5094
Phone: (603) 223-2541 Fax: (603) 223-0104



In Reply Refer To:
Project Code: 2023-0039468
Project Name: Proposed Solar Photovoltaic Array

January 30, 2023

Subject: List of threatened and endangered species that may occur in your proposed project location or may be affected by your proposed project

To Whom It May Concern:

Updated 12/27/2022 - Please review this letter each time you request an Official Species List, we will continue to update it with additional information and links to websites may change.

About Official Species Lists

The purpose of the Act is to provide a means whereby threatened and endangered species and the ecosystems upon which they depend may be conserved. Federal and non-Federal project proponents have responsibilities under the Act to consider effects on listed species.

The enclosed species list identifies threatened, endangered, proposed, and candidate species, as well as proposed and final designated critical habitat, that may occur within the boundary of your proposed project and/or may be affected by your proposed project. The species list fulfills the requirements of the U.S. Fish and Wildlife Service (Service) under section 7(c) of the Endangered Species Act (Act) of 1973, as amended (16 U.S.C. 1531 et seq.).

New information based on updated surveys, changes in the abundance and distribution of species, changed habitat conditions, or other factors could change this list. Please note that under 50 CFR 402.12(e) of the regulations implementing section 7 of the Act, the accuracy of this species list should be verified after 90 days. The Service recommends that verification be completed by visiting the ECOS-IPaC website at regular intervals during project planning and implementation for updates to species lists and information. An updated list may be requested by returning to an existing project's page in IPaC.

Endangered Species Act Project Review

Please visit the “**New England Field Office Endangered Species Project Review and Consultation**” website for step-by-step instructions on how to consider effects on listed

species and prepare and submit a project review package if necessary:

<https://www.fws.gov/office/new-england-ecological-services/endangered-species-project-review>

NOTE Please do not use the **Consultation Package Builder** tool in IPaC except in specific situations following coordination with our office. Please follow the project review guidance on our website instead and reference your **Project Code** in all correspondence.

Northern Long-eared Bat - (Updated 12/27/2022) Please visit our New England Field Office Project Review webpage at the link above for updated northern long-eared bat consultation guidance. The Service published a final rule to reclassify the northern long-eared bat (NLEB) as endangered on November 30, 2022. The final rule will go into effect on **January 30, 2023**. After that date, the current 4(d) rule for NLEB will no longer be in effect, and the 4(d) determination key will no longer be available. New compliance tools will be available by mid- to late-January, and information will be posted on our New England Field Office Project Review webpage in January, so please check this site often for updates.

Depending on the type of effects a project has on NLEB, the change in the species' status may trigger the need to re-initiate consultation for any actions that are not completed and for which the Federal action agency retains discretion once the new listing determination becomes effective. If your project may result in incidental take of NLEB after the new listing goes into effect, this will need to be addressed in an updated consultation that includes an Incidental Take Statement. Many of these situations will be addressed through the new compliance tools. If your project may require re-initiation of consultation, please wait for information on the new tools to appear on our website or contact our office at newengland@fws.gov for additional guidance.

Additional Info About Section 7 of the Act

Under section 7(a)(2) of the Act and its implementing regulations (50 CFR 402 et seq.), Federal agencies are required to determine whether projects may affect threatened and endangered species and/or designated critical habitat. If a Federal agency, or its non-Federal representative, determines that listed species and/or designated critical habitat may be affected by the proposed project, the agency is required to consult with the Service pursuant to 50 CFR 402. In addition, the Federal agency also may need to consider proposed species and proposed critical habitat in the consultation. 50 CFR 402.14(c)(1) specifies the information required for consultation under the Act regardless of the format of the evaluation. More information on the regulations and procedures for section 7 consultation, including the role of permit or license applicants, can be found in the "Endangered Species Consultation Handbook" at:

<https://www.fws.gov/service/section-7-consultations>

In addition to consultation requirements under Section 7(a)(2) of the ESA, please note that under sections 7(a)(1) of the Act and its implementing regulations (50 CFR 402 et seq.), Federal agencies are required to utilize their authorities to carry out programs for the conservation of threatened and endangered species. Please contact NEFO if you would like more information.

Candidate species that appear on the enclosed species list have no current protections under the

ESA. The species' occurrence on an official species list does not convey a requirement to consider impacts to this species as you would a proposed, threatened, or endangered species. The ESA does not provide for interagency consultations on candidate species under section 7, however, the Service recommends that all project proponents incorporate measures into projects to benefit candidate species and their habitats wherever possible.

Migratory Birds

In addition to responsibilities to protect threatened and endangered species under the Endangered Species Act (ESA), there are additional responsibilities under the Migratory Bird Treaty Act (MBTA) and the Bald and Golden Eagle Protection Act (BGEPA) to protect native birds from project-related impacts. Any activity, intentional or unintentional, resulting in take of migratory birds, including eagles, is prohibited unless otherwise permitted by the U.S. Fish and Wildlife Service (50 C.F.R. Sec. 10.12 and 16 U.S.C. Sec. 668(a)). For more information regarding these Acts see:

<https://www.fws.gov/program/migratory-bird-permit>

<https://www.fws.gov/library/collections/bald-and-golden-eagle-management>

Please feel free to contact us at **newengland@fws.gov** with your **Project Code** in the subject line if you need more information or assistance regarding the potential impacts to federally proposed, listed, and candidate species and federally designated and proposed critical habitat.

Attachment(s): Official Species List

Attachment(s):

- Official Species List

Official Species List

This list is provided pursuant to Section 7 of the Endangered Species Act, and fulfills the requirement for Federal agencies to "request of the Secretary of the Interior information whether any species which is listed or proposed to be listed may be present in the area of a proposed action".

This species list is provided by:

New England Ecological Services Field Office

70 Commercial Street, Suite 300

Concord, NH 03301-5094

(603) 223-2541

Project Summary

Project Code: 2023-0039468

Project Name: Proposed Solar Photovoltaic Array

Project Type: Power Gen - Solar

Project Description: Development of a 0.99 MW AC solar photovoltaic array with associated improvements

Project Location:

Approximate location of the project can be viewed in Google Maps: <https://www.google.com/maps/@41.41145755,-73.01363032324062,14z>



Counties: New Haven County, Connecticut

Endangered Species Act Species

There is a total of 2 threatened, endangered, or candidate species on this species list.

Species on this list should be considered in an effects analysis for your project and could include species that exist in another geographic area. For example, certain fish may appear on the species list because a project could affect downstream species.

IPaC does not display listed species or critical habitats under the sole jurisdiction of NOAA Fisheries¹, as USFWS does not have the authority to speak on behalf of NOAA and the Department of Commerce.

See the "Critical habitats" section below for those critical habitats that lie wholly or partially within your project area under this office's jurisdiction. Please contact the designated FWS office if you have questions.

-
1. NOAA Fisheries, also known as the National Marine Fisheries Service (NMFS), is an office of the National Oceanic and Atmospheric Administration within the Department of Commerce.

Mammals

NAME

STATUS

Northern Long-eared Bat *Myotis septentrionalis*

Endangered

No critical habitat has been designated for this species.

Species profile: <https://ecos.fws.gov/ecp/species/9045>

Insects

NAME

STATUS

Monarch Butterfly *Danaus plexippus*

Candidate

No critical habitat has been designated for this species.

Species profile: <https://ecos.fws.gov/ecp/species/9743>

Critical habitats

THERE ARE NO CRITICAL HABITATS WITHIN YOUR PROJECT AREA UNDER THIS OFFICE'S JURISDICTION.

IPaC User Contact Information

Agency: Solli Engineering

Name: Anthony Capuano

Address: 11 Vanderbilt Avenue, Suite 240

City: Norwood

State: MA

Zip: 02062

Email: anthony@sollillc.com

Phone: 7813528491



United States Department of the Interior

FISH AND WILDLIFE SERVICE
New England Ecological Services Field Office
70 Commercial Street, Suite 300
Concord, NH 03301-5094
Phone: (603) 223-2541 Fax: (603) 223-0104



In Reply Refer To:
Project code: 2023-0045225
Project Name: Bethany Solar Farm

February 14, 2023

Subject: Consistency letter for the 'Bethany Solar Farm' project indicating that any take of the northern long-eared bat that may occur as a result of the Action is not prohibited under the ESA Section 4(d) rule adopted for this species at 50 CFR §17.40(o).

Dear Samuel Ulfsson:

The U.S. Fish and Wildlife Service (Service) received on February 14, 2023 your effects determination for the 'Bethany Solar Farm' (the Action) using the northern long-eared bat (*Myotis septentrionalis*) key within the Information for Planning and Consultation (IPaC) system. You indicated that no Federal agencies are involved in funding or authorizing this Action. This IPaC key assists users in determining whether a non-Federal action may cause "take"^[1] of the northern long-eared bat that is prohibited under the Endangered Species Act of 1973 (ESA) (87 Stat.884, as amended; 16 U.S.C. 1531 et seq.).

Based upon your IPaC submission, any take of the northern long-eared bat that may occur as a result of the Action is not prohibited under the ESA Section 4(d) rule adopted for this species at 50 CFR §17.40(o). Unless the Service advises you within 30 days of the date of this letter that your IPaC-assisted determination was incorrect, this letter verifies that the Action is not likely to result in unauthorized take of the northern long-eared bat.

Additionally, please note that on March 23, 2022, the Service published a proposal to reclassify the northern long-eared bat (NLEB) as endangered under the Endangered Species Act. The U.S. District Court for the District of Columbia has ordered the Service to complete a new final listing determination for the NLEB by November 2022 (Case 1:15-cv-00477, March 1, 2021). The bat, currently listed as threatened, faces extinction due to the range-wide impacts of white-nose syndrome (WNS), a deadly fungal disease affecting cave-dwelling bats across the continent. The proposed reclassification, if finalized, would remove the current 4(d) rule for the NLEB, as these rules may be applied only to threatened species. Depending on the type of effects a project has on NLEB, the change in the species' status may trigger the need to re-initiate consultation for any actions that are not completed and for which the Federal action agency retains discretion once the new listing determination becomes effective (anticipated to occur by December 30, 2022). If your project may result in incidental take of NLEB after the new listing goes into effect this will

first need to be addressed in an updated consultation that includes an Incidental Take Statement. If your project may require re-initiation of consultation, please contact our office for additional guidance.

Please report to our office any changes to the information about the Action that you entered into IPaC, the results of any bat surveys conducted in the Action area, and any dead, injured, or sick northern long-eared bats that are found during Action implementation.

If your Action proceeds as described and no additional information about the Action's effects on species protected under the ESA becomes available, no further coordination with the Service is required with respect to the northern long-eared bat.

The IPaC-assisted determination for the northern long-eared bat **does not** apply to the following ESA-protected species that also may occur in your Action area:

- Monarch Butterfly *Danaus plexippus* Candidate

You may coordinate with our Office to determine whether the Action may cause prohibited take of the animal species listed above.

[1] Take means to harass, harm, pursue, hunt, shoot, wound, kill, trap, capture, or collect, or to attempt to engage in any such conduct [ESA Section 3(19)].

Action Description

You provided to IPaC the following name and description for the subject Action.

1. Name

Bethany Solar Farm

2. Description

The following description was provided for the project 'Bethany Solar Farm':

The proposed development is for a solar photovoltaic array that will produce .99 MW AC. The property is located at 428 Bethmour Road, Bethany CT. The property is 21.22 acres. 5.66 acres will be impacted by the development. No wetlands will be impacted by the development. No work is expected to be done within the 100' Upland Wetland Review Area (100' Wetland Buffer).

Approximate location of the project can be viewed in Google Maps: <https://www.google.com/maps/@41.411761299999995,-73.01510739515678,14z>

**Determination Key Result**

This non-Federal Action may affect the northern long-eared bat; however, any take of this species that may occur incidental to this Action is not prohibited under the final 4(d) rule at 50 CFR §17.40(o).

Determination Key Description: Northern Long-eared Bat 4(d) Rule

This key was last updated in IPaC on **May 15, 2017**. Keys are subject to periodic revision.

This key is intended for actions that may affect the threatened northern long-eared bat.

The purpose of the key for non-Federal actions is to assist determinations as to whether proposed actions are excepted from take prohibitions under the northern long-eared bat 4(d) rule.

If a non-Federal action may cause prohibited take of northern long-eared bats or other ESA-listed animal species, we recommend that you coordinate with the Service.

Determination Key Result

Based upon your IPaC submission, any take of the northern long-eared bat that may occur as a result of the Action is not prohibited under the ESA Section 4(d) rule adopted for this species at 50 CFR §17.40(o).

Qualification Interview

1. Is the action authorized, funded, or being carried out by a Federal agency?

No

2. Will your activity purposefully **Take** northern long-eared bats?

No

3. Have you contacted the appropriate agency to determine if your project is near a known hibernaculum or maternity roost tree?

Location information for northern long-eared bat hibernacula is generally kept in state Natural Heritage Inventory databases – the availability of this data varies state-by-state. Many states provide online access to their data, either directly by providing maps or by providing the opportunity to make a data request. In some cases, to protect those resources, access to the information may be limited. A web page with links to state Natural Heritage Inventory databases and other sources of information on the locations of northern long-eared bat roost trees and hibernacula is available at www.fws.gov/media/nleb-roost-tree-and-hibernacula-state-specific-data-links-0.

Yes

4. Will the action affect a cave or mine where northern long-eared bats are known to hibernate (i.e., hibernaculum) or could it alter the entrance or the environment (physical or other alteration) of a hibernaculum?

No

5. Will the action involve Tree Removal?

Yes

6. Will the action only remove hazardous trees for the protection of human life or property?

Yes

Project Questionnaire

If the project includes forest conversion, report the appropriate acreages below. Otherwise, type '0' in questions 1-3.

1. Estimated total acres of forest conversion:

0

2. If known, estimated acres of forest conversion from April 1 to October 31

0

3. If known, estimated acres of forest conversion from June 1 to July 31

0

If the project includes timber harvest, report the appropriate acreages below. Otherwise, type '0' in questions 4-6.

4. Estimated total acres of timber harvest

1

5. If known, estimated acres of timber harvest from April 1 to October 31

0

6. If known, estimated acres of timber harvest from June 1 to July 31

0

If the project includes prescribed fire, report the appropriate acreages below. Otherwise, type '0' in questions 7-9.

7. Estimated total acres of prescribed fire

0

8. If known, estimated acres of prescribed fire from April 1 to October 31

0

9. If known, estimated acres of prescribed fire from June 1 to July 31

0

If the project includes new wind turbines, report the megawatts of wind capacity below. Otherwise, type '0' in question 10.

10. What is the estimated wind capacity (in megawatts) of the new turbine(s)?

0

IPaC User Contact Information

Agency: Solli Engineering LLC

Name: Samuel Ulfsson

Address: 501 Main Street #2A

City: Monroe

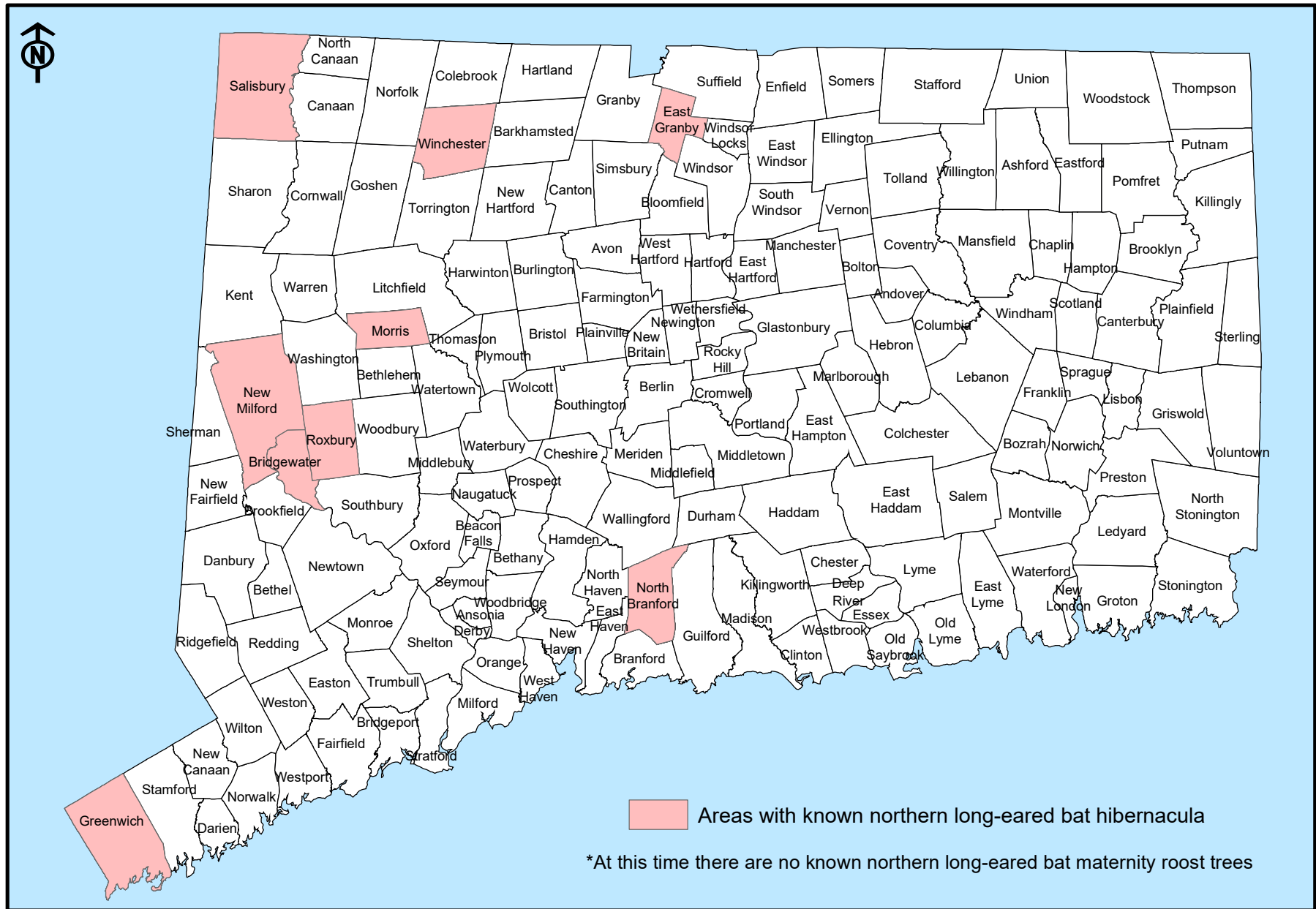
State: CT

Zip: 06468

Email sulfsson@sollllc.com

Phone: 2033216572

Northern long-eared bat areas of concern in Connecticut to assist with Federal Endangered Species Act Compliance



March 6, 2019

For information on federal requirements visit <http://www.fws.gov/midwest/endangered/mammals/nlebat/>

Appendix D: Cultural Resources

**Phase Ia Archaeological Assessment Survey
Proposed Solar Photovoltaic Array
Town of Bethany, Connecticut**

March, 2023



ACS

◆ *Archaeological Consulting Services* ◆

**Phase Ia Archaeological Assessment Survey
Proposed Solar Photovoltaic Array
Town of Bethany, Connecticut**

by

**Gregory F. Walwer, Ph.D.
and
Dorothy N. Walwer, M.A.**

of

ACS

for

Solli Engineering
501 Main Street, Suite 2A
Monroe, CT 06468
(203) 880-5455

March, 2023

ACS

◆ *Archaeological Consulting Services* ◆

**118 Whitfield Street
Guilford, Connecticut 06437
(203) 458-0550
www.acsarchaeology.com
*acsinfo@yahoo.com***

Abstract

This report contains the results of a Phase Ia archaeological assessment survey conducted by ACS (Archaeological Consulting Services) during the month of March, 2023. The project calls for an evaluation of potential cultural resources to be affected by the construction of a solar farm on a property that measures about 22 acres in Bethany, Connecticut. The project property consists of two lots, including a two-acre house lot at 428 Bethmour Road in Bethany on the east side of the road, and an additional undeveloped 20-acre lot to the east. The project is being coordinated by Solli Engineering, a civil engineering firm based in Monroe, Connecticut. Solli supplied site plans which show the proposed development and existing conditions. The project is subject to review by the Connecticut Siting Council and the Connecticut State Historic Preservation Office (SHPO).

The project area lies in southwest Bethany, on the east side of Bethmour Road. Background research indicates a low sensitivity for potential prehistoric cultural resources, with a statistical prehistoric landscape sensitivity model developed and utilized by ACS indicating a high score of only 6.5 out of a potential 100.0, and therefore within the low sensitivity range (0-20). The low score can be attributed to rocky soil contexts and considerable distance to the nearest major water source, which is Pine Brook that flows through the eastern end of the project property but relatively far from the project area that is concentrated in the far western end of the property. The property bears a higher sensitivity for historic cultural resources, given its location on Bethmour Road that was occupied since at least the early 19th century.

Land records and historic maps indicate the presence of the Tolles house and farmstead to the north of the project area by the 1850s, which may be the same as the Greek Revival Street B. Todd house appearing on maps at a slightly different location by the 1860s. Neither house exists today, although there is an existing house on the property built in 1949. That house and its associated outbuildings are not architecturally distinctive, and therefore not eligible for the National Register of Historic Places (NRHP), nor are the various stone wall alignments on the property which have been sufficiently documented on historic and recent survey maps. Because of the possibility that previous historic occupations could have been located elsewhere on Bethmour Road, including within the project property, ACS recommends a Phase Ib archaeological reconnaissance survey, limited to an area within 300 feet of Bethmour Road and within the project impact area, prior to any construction activities and subject to review by the Connecticut State Historic Preservation Office (SHPO).

Project Summary

Project Name: Proposed Solar Photovoltaic Array, Bethany, Connecticut.

Project Purpose: To investigate possible cultural resources which may be impacted by the construction of a solar farm in Bethany, Connecticut, in compliance with requirements of the Connecticut Siting Council and the Connecticut State Historic Preservation Office.

Project Funding: The Nevar Company, Cheshire, Connecticut.

Project Location: 428 Bethmour Road, Bethany, Connecticut.

Project Size: ~22 acres.

Investigation Type: Phase Ia archaeological assessment survey.

Investigation Methods: Background research, pedestrian surface survey.

Dates of Investigation: March, 2023.

Performed by: ACS (Archaeological Consulting Services), 118 Whitfield Street, Guilford, Connecticut 06437, (203) 458-0550 (telephone), (203) 672-2442 (fax), acsinfo@yahoo.com.

Principal Investigators: Gregory F. Walwer, Ph.D. and Dorothy N. Walwer, M.A.

Submitted to:

Solli Engineering (Robert Pryor, Director of Site / Civil Engineering), 501 Main Street, Suite 2A, Monroe, CT 06468, (203) 880-5455.

Connecticut Office of State Archaeology (Dr. Sarah Sportman, State Archaeologist), University of Connecticut, 354 Mansfield Road, Storrs, Connecticut 06269-1176, (860) 486-5248.

Reviewing Agency:

Connecticut State Historic Preservation Office (Catherine Labadia, Staff Archaeologist), 450 Columbus Boulevard, Hartford, Connecticut 06103, (860) 500-2329.

Recommendations: Phase Ib archaeological reconnaissance survey of areas to be impacted within 300 feet of Bethmour Road. The existing 1949 house is not eligible for the National Register of Historic Places, nor are stone wall alignments which have been sufficiently recorded on survey maps.

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CHAPTER 1: INTRODUCTION

Project Description

This report provides the results of a Phase Ia archaeological assessment survey conducted by ACS for the planned development of a solar voltaic array, or solar farm, in Bethany, New Haven County, Connecticut. The owner of the property is The Nevar Company of Cheshire, Connecticut. The project consists of two lots, including a house lot at 428 Bethmour Road (Tax Map 113, Lot 1A) measuring 2.05 acres, and the adjacent lot to the rear of the house (Tax Map 113, Lot 1) that measures 19.65 acres. The project area is in southwest Bethany, on the east side of the road, and consists of a long parcel running west to east. The house lot contains a small, 620 square-foot home built in 1949.

ACS was contacted by Solli Engineering, a civil engineering firm based in Monroe, Connecticut to conduct the archaeological assessment survey for the project. Solli supplied ACS with a survey map, indicating that the survey was likely required for review by the Connecticut State Historic Preservation Office (SHPO) and Connecticut Siting Council. The survey map shows existing conditions, including topography and wetlands, as well as the location of the existing house and detached garage. The bulk of the proposed development would be in the western third of the overall property, with the demolition of the existing structures where an access drive is proposed.

ACS conducted the assessment survey in conformance with the *Environmental Review Primer for Connecticut Archaeological Resources* issued by SHPO. The assessment survey evaluated the potential need, if any, for a Phase Ib archaeological reconnaissance survey. The archaeological assessment survey consisted of a thorough background research effort and pedestrian surface survey to evaluate the potential sensitivity of the project area for any prehistoric and/or historic cultural resources, with SHPO to serve as review agency for the final report.

CHAPTER 2: BACKGROUND

Environmental Setting

The project area is located in the Town of Bethany, New Haven County, Connecticut. The project setting is in the Southwest Hills (IV-A) ecoregion of Connecticut. The project area lies in the southwest part of Bethany, a couple of miles to the east of Route 8. The area contains a mix of residential neighborhoods and small agricultural plots. The house at 428 Bethmour Road and associated outbuildings occupy the northwest corner of the project area on the east side of the road (Figure 1).

Underlying bedrock is a unit of Ordovician Granitic Gneiss (Og), an Ordovician formation on the order of 440 to 500 million years old (Rodgers 1985). Jurassic basalt intrusives appear within the formation that is steeply inclined, on the order of 65 to 80 degrees to the northwest. The property is set on a large glacial moraine, with one test bore to the north revealing 130 feet of till above bedrock (Stone et al. 1992). The project area is within the Bladens River drainage basin (#6919) that empties west into the Naugatuck River (McElroy 1991). A tributary of Bladens River named Pine Brook flows south through the very eastern end of the parcel and into Bladens River about one mile to the south of the project area (Figure 2). There is also a lesser wetlands body lying towards the center of the property, entirely to the east of the proposed development. The house at the western end of the property is set on a low hill peak at about 630 feet above mean sea level, with a generally southeast dipping surface to 600 feet above mean sea level at the eastern end of the development, and about 550 feet above mean sea level at the far eastern end of the property. The area surrounding the structures at the western end is mostly clear of vegetation other than a grass lawn and some thick scrub growth, while the rest of the property is wooded.

The project area contains three principal soil types (Figure 3) within an area designated as the Paxton-Woodbridge-Ridgebury soil association (Reynolds 1979; USDA NRCS websoil survey 2023). A unit of Woodbridge fine sandy loam (WxA / 45A) surrounds the house and outbuildings at the low hill peak. The moderately well drained soil typically has a profile with a topsoil of dark brown fine sandy loam to seven inches deep, followed by a fine sandy loam subsoil of dark yellowish brown over olive brown to 25 inches below the surface, and a substratum of olive, very firm gravelly fine sandy loam to five feet deep or more. Well drained Paxton fine sandy loam (PbB / 84B) is on the surrounding gentle hill slope, having a typical topsoil of dark brown fine sandy loam to eight inches deep, followed by a subsoil of dark yellowish brown and olive brown fine sandy loam to 25 inches deep, and a substratum of olive, very firm gravelly fine sandy loam to five feet deep or more. The Woodbridge and Paxton soils are very similar, with possibly better drainage characteristics for the Paxton soil. The rockier version of Woodbridge fine sandy loam (WzC / 47C) occurs downslope in steeper contexts, and with a similar profile to that of the less rocky version, but with a much thinner two-inch topsoil, and thicker subsoil to the same 25-inch depth. The less rocky soils would have been suitable for historic agricultural pursuits. Wetlands on the property are associated with poorly drained Ridgebury, Leicester, and Whitman fine sandy loam (RN).

Figure 1: Map of the Project Area

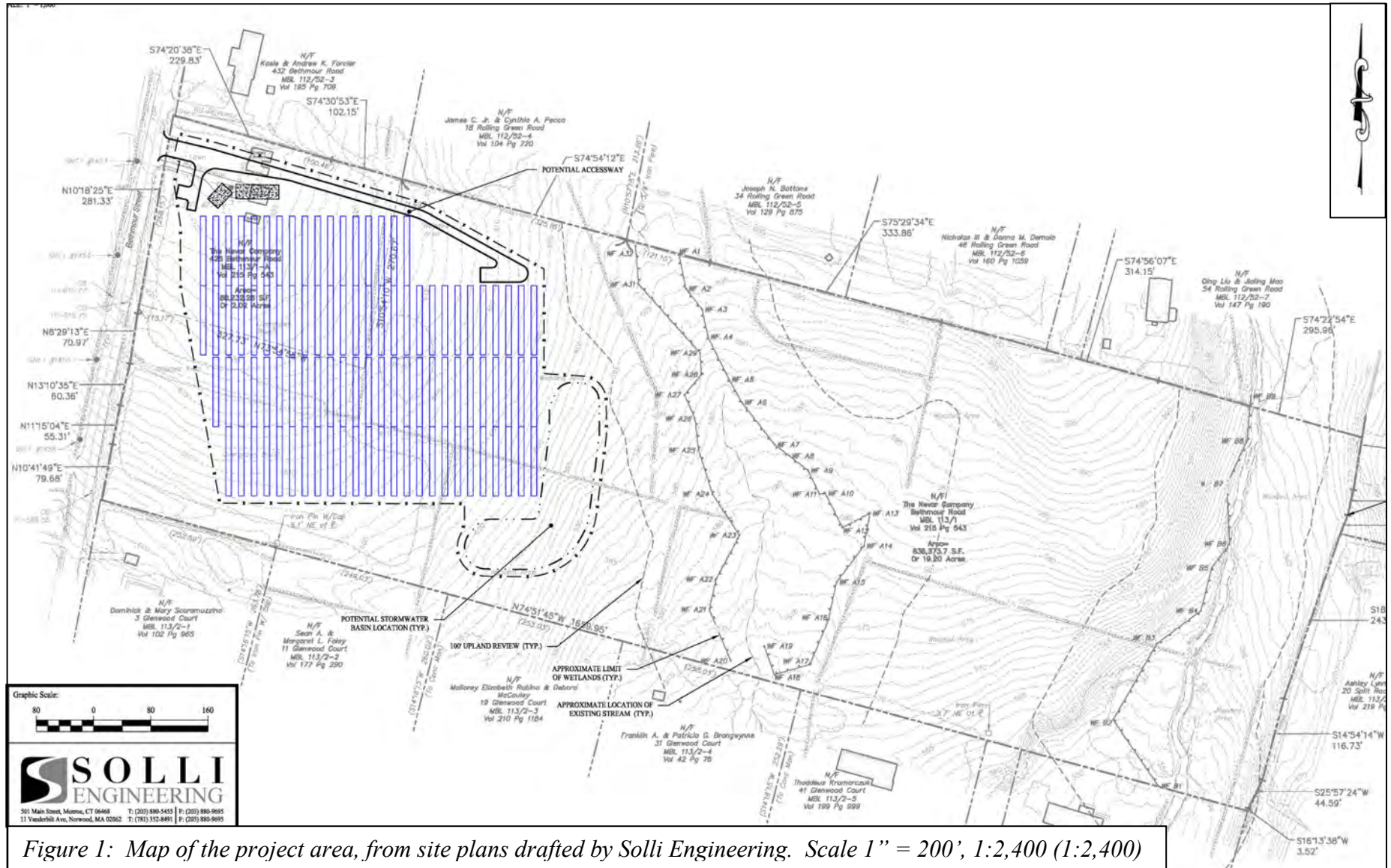


Figure 2: USGS 7.5' Topographic Map, Naugatuck Quadrangle

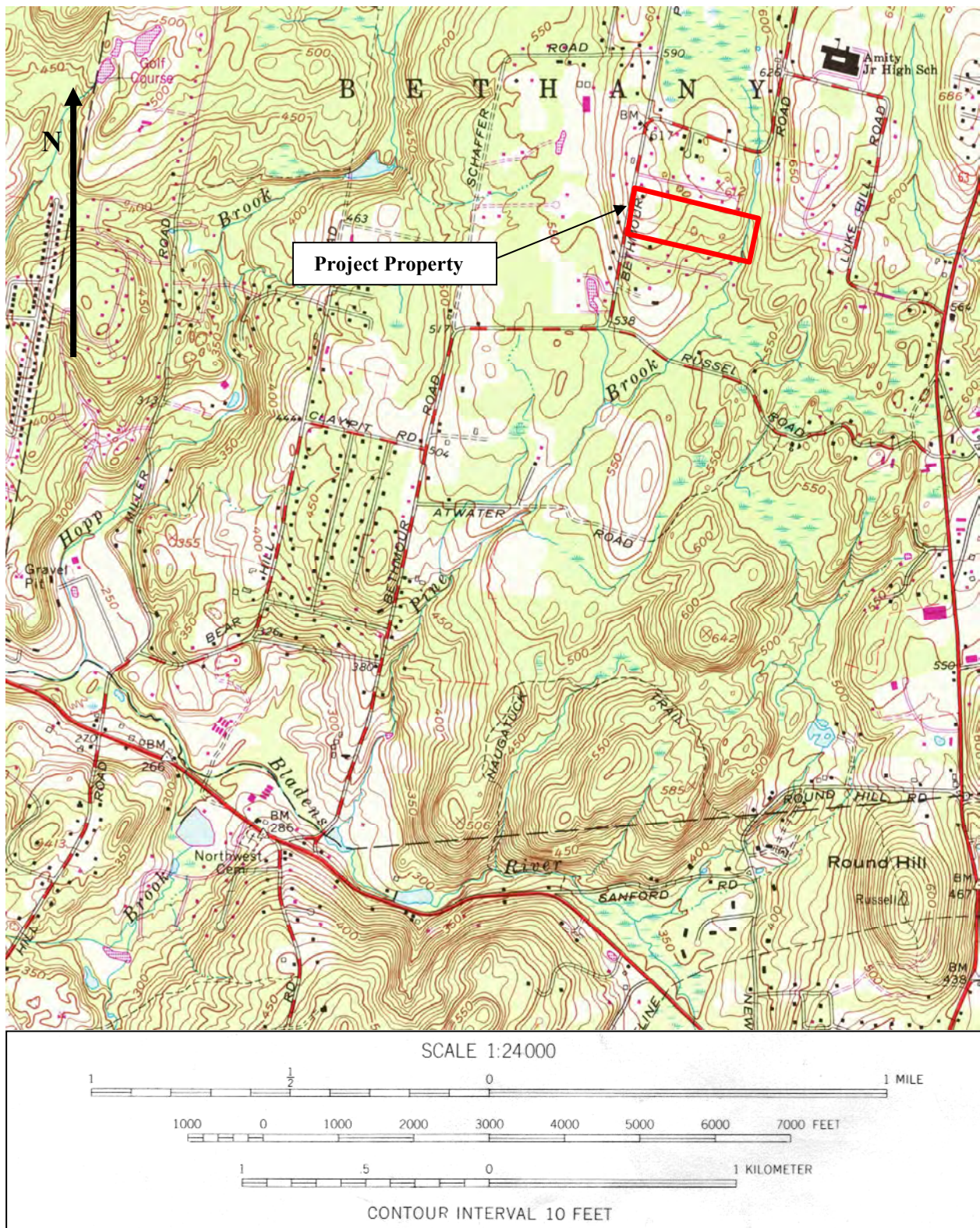


Figure 2: From USGS 1984.

Figure 3: USDA Websoil Survey Map



Figure 3: From USDA NRCS websoil survey.

Cultural Setting

Regional Prehistory

The prehistory of the project region and New England in general can be broadly divided into periods reflecting changes in environment, Native American subsistence and settlement patterns, and the material culture which is preserved in the archaeological record. Although it remains controversial today, the conservative estimates for the first occupations of North America are about 18,000 to 15,000 years ago, just after the maximum extent of the last glaciation and the broadest extent of the Bering land bridge (Kehoe 1981:7; Parker 1987:4; Jennings 1989:52). Southern Connecticut itself remained glaciated until about 15,200 B.P. (Snow 1980:103; Gordon 1983:71; Parker 1987:5; McWeeney 1994:181, 1999:6).

Paleo-Indian

The Paleo-Indian period is documented in Connecticut after 12,000 years ago and extends to roughly 9,500 B.P. (Swigart 1974; Snow 1980:101; Lavin 1984:7; Moeller 1984, 1999). This was a period of climatic amelioration from full glacial conditions, and a rise in sea levels which fell short of inundating the continental shelf. It was during this time that tundra vegetation was replaced by patches of boreal forests dominated by spruce trees (Snow 1980:114; Parker 1987:5-6), and eventually white pine and several pioneering deciduous genera (McWeeney 1994:182, 1999:7). Early in the period, the environment was conducive to the existence of large herbivores and a low population density of humans who procured these animals as a major subsistence resource, although warming temperatures and denser forests contributed to the extinction of certain species. The projected human social and settlement patterns are those of small bands of semi-nomadic or restricted wandering people who hunted mammoth, mastodon, bison, elk, caribou, musk ox, and several smaller mammals (Ritchie 1969:10-11; Snow 1980:117-120). Episodes of sparse vegetation during this period encouraged the use of high lookout points over hollows and larger valleys by people in pursuit of large game. The southern part of New England had an earlier recovery from glacial conditions when compared to areas to the north, however, with a higher density of vegetation that might have precluded Paleo-Indians of Connecticut from focussing heavily on the larger mammals (McWeeney 1994:182).

The cultural material associated with this period includes large to medium-sized, fluted projectile points (cf. Clovis), in addition to knives, drills, pieces esquillees and graters, scrapers, perforators, awls, abraders, spokeshaves, retouched pieces, utilized flakes, and hammerstones (Wilbur 1978:5; Snow 1980:122-127; Moeller 1980). Although numerous finds from this period have been found in Connecticut, only a few, small *in situ* sites exist throughout the state. Finds tend to be located near very large streams in the lower Connecticut River Valley, and in rockshelters of other regions (McBride 1981). A survey performed by the Connecticut Office of State Archaeology and the Archaeological Society of Connecticut resulted in the documentation of 53 Paleo-Indian "find spots" in Connecticut (Bellantoni and Jordan 1995).

Early Archaic

The Early Archaic period lasted from approximately 9,500 B.P. to 7,500 B.P. (Snow 1980:159; Lavin 1984:9; Moeller 1984). Sea levels and temperatures continued to rise during this period as denser stands of forests dominated by pine and various deciduous species replaced the vegetation of the former period (Davis 1969:418-419; Snow 1980:114; Parker 1987:9; McWeeney 1994:184-185, 1999:8-9). This environmental change was rapid and caused a major shift in the animals it supported, including deer, moose, other small to medium-sized mammals, migratory birds, fish, and shellfish. The material culture changed along with the environmental conditions to include the atlatl and smaller stemmed and bifurcated projectile points (Stanly, cf. Kanawha and Lecroy) for procuring smaller, faster game in more closed settings (Wilbur 1978:6-7). The expanded tool set included choppers and anvil stones. Settlement patterns were probably becoming more territorialized towards a central-based wandering character (Snow 1980:171; see also Forrest 1999). The Early Archaic period is poorly represented in Connecticut and the lower coastal river valleys, probably resulting from a combined effect of low population densities in response to rapidly changing environmental conditions, as well as site location and preservation factors (Snow 1980:168; McBride 1981; McBride and Dewar 1981:45; Lavin 1984:9; McWeeney 1986; see also Forrest 1999).

Middle Archaic

The Middle Archaic period extended from approximately 7,500 B.P. to 6,000 B.P. (Snow 1980:173; Lavin 1984:9; McBride 1984; Jones 1999). It was by the end of this period of increased warming that sea levels and coastal configurations had stabilized and approached their present conditions (Kehoe 1981:211; Gordon 1983:82; Parker 1987:9). The period is marked by the establishment of forests with increasing proportions of deciduous hardwoods in relation to the pine predecessors in Connecticut (Davis 1969; Snow 1980:114; McWeeney 1999:10). The material culture included square or contracting-stemmed points (Neville, Stark, and Merrimac), semi-lunar groundstone knives, ground and winged banner stones for atlatls, plummets for nets, gouges, denticulates, perforators, percussed celts and adzes and grooved axes for woodworking (Snow 1980:183-184), as well as tools used in previous periods. This more extensive range of material culture indicates a broader subsistence base than in previous periods, including greater fish and shellfish procurement (Wilbur 1978:8; Snow 1980:178-182) which was associated with the stabilization of sea levels towards the end of the period. The increased breadth of subsistence resources had the effect of increasing scheduling efforts and may have caused settlement patterns to take on more of a central-based or seasonally circulating pattern with bands joining and dispersing on a seasonal basis (Snow 1980:183). Sites found in the lower Connecticut River Valley region suggest that a wider range of environments and associated site types were exploited, including both large and special task sites in upland areas (McBride 1981, 1984:56). This regional pattern may confirm the suggested settlement pattern of central-based, seasonally circulating or restricted circulating groups of people supported by logistical procurement sites throughout the state. Middle Archaic sites are fairly rare in Connecticut, again a combined product of rising sea levels and poor site preservation (see Forrest 1999).

Late Archaic

The Late Archaic period ranged from approximately 6,000 B.P. to 3,700 B.P. (Snow 1980:187; Lavin 1984:11; McBride 1984; Pfeiffer 1984; Cassedy 1999). This period is marked by a warm-dry maximum evident from pollen cores in the region (Davis 1969:414; Ogden 1977). Hardwood, oak-dominated forests very similar in character to ones established today covered most of Connecticut by the Late Archaic (Parker 1987:10). The Late Archaic in Connecticut has been divided into two traditions: the Laurentian and the Narrow Point (Lavin 1984:11), with the former perhaps being distributed more in the interior. The Laurentian tradition is defined by wider-bladed, notched and eared triangular points, and ground slate points and ulus, while the Narrow Point tradition includes smaller, thicker, and narrower points. The tool kit and general material culture became even more expanded during this period, with the advent of ground stone manos, nut mortars, pestles, and bowls, as well as stone pipes, bone tools, corner-notched (Vosburg, Brewerton, and Vestal), side-notched (Otter Creek, Brewerton, Normanskill), smaller narrow-stemmed (Dustin, Lamoka, Squibnocket, and Wading River), and triangular points (Squibnocket, Brewerton, and Beekman), grooved and perforated weights, fish weirs and harpoons, and decorative gorgets (Wilbur 1978:15-24; Snow 1980:228-231). The groundstone material has been inferred as being associated with an increased vegetable diet that consisted of berries, nuts, and seeds (Snow 1980:231; Lavin 1984:13), including acorn, butternut, chestnut, walnut, hickory, bayberry, blackberry, goose foot, cranberry, partridge berry, service berry, strawberry, and swamp current (Cruson 1991:29). Deer continued to be the predominant meat source, although animal remains recovered from archaeological sites in the region include black bear, raccoon, woodchuck, rabbit, otter, gray squirrel, red fox, gray fox, wolf, wild turkey, grouse, pigeon, migratory fowl, and anadromous and freshwater fish and shellfish (Cruson 1991:28-29). Various sea mammals and fish were procured along the coast.

The increasing breadth of the subsistence base and material culture was in turn associated with a central-based settlement pattern in which a restricted range of seasonally scheduled and used areas were exploited in a more semi-sedentary fashion than previously (Lavin 1984:13; Dincauze 1990:25). Sites in the lower Connecticut River Valley suggest that the larger rivers served more as long-term bases within a central-based circulating system than in the Middle Archaic (McBride 1981; McBride and Dewar 1981:48). The interior uplands of Connecticut may have supported a relatively independent set of seasonally circulating groups which used larger wetlands as long-term bases (Wadleigh 1981). Mortuary practices of the time suggest some sedentism for certain groups of people who were buried in specialized secondary cremation cemeteries and who may have had some control over restricted resources (e.g. riparian transportation routes) (Walwer 1996). Although the cremation sites largely include utilitarian funerary objects, some contain non-local materials which suggest trade association with cultures to the west of Connecticut (Walwer 1996).

Terminal Archaic

The Terminal Archaic period extended from approximately 3,700 B.P. to 2,700 B.P., as defined by the Susquehanna and Small-Stemmed traditions (Swigart 1974; Snow 1980:235; Lavin 1984:14; Pfeiffer 1984; Pagoulatos 1988; Cruson 1991; Cassedy 1999). Steatite, or soapstone, was a frequently used material by this time, and could be fashioned into bowls and other objects. The mass, permanency, and labor intensiveness of creating these heavy items have

led to the inference of more sedentary base camps, especially on large rivers where the development of a canoe technology had become fully established and increased the effective catchment area within which groups of people were gathering resources on a continuous basis. The material culture of the period was very similar to the Late Archaic, with a proliferation of stemmed projectile point types including Snook Kill, Bare Island and Poplar Island stemmed points, Orient Fishtail points, Sylvan and Vestal side-notched points, and Susquehanna corner-notched points. The resource base continued to consist of deer and small mammals, nuts, shellfish, turtles, and birds (Snow 1980:249). The first signs of ceramics (Vinette I pottery) tempered with steatite fragments appeared during this period (Lavin 1984:15; Lavin and Kra 1994:37; see also Cassedy 1999:131), and archaeological evidence of trade with other regions becomes more substantial for this time (Pfeiffer 1984:84).

The distribution of sites and site types in the lower Connecticut River Valley during this period suggests that there was a change in settlement to one with fewer, yet larger sites in riverine settings, and associated satellite task-specific sites in the uplands (McBride 1981; McBride and Dewar 1981:49). The implications are less foraging-strategy residential movement and more task-oriented collection activities within a radiating settlement pattern, but probably one in which some degree of seasonal circulation of settlement took place. Pagoulatos (1988) has shown that while sites associated with the Small-Stemmed tradition tend to suggest a more mobile settlement pattern in the interior uplands, sites of the Susquehanna tradition indicate a semi-sedentary collector strategy in major riverine and estuarine environments. At least certain groups exhibited semi-sedentism and some control over restricted resources, as indicated by the elaborate burials of the Terminal Archaic (Walwer 1996). Mortuary practices from the period include secondary cremation interments in formalized cemetery areas, with individual pits containing fragmented utilitarian material from communal cremation areas, as well as highly stylized funerary objects from non-local material (Walwer 1996). The lack of other, less formalized burial types evident in the archaeological record may be a matter of poor preservation, in which case it has been proposed that the cremation cemeteries are representative of a hierarchical society in which a portion of the people (of the Susquehanna "tradition") were able to generate a surplus economy that supported a semi-sedentary settlement pattern. This surplus may have been generated by the procurement and control over the transportation of steatite from various areas in Connecticut and surrounding territory.

Early Woodland

The Early Woodland period in Connecticut extended from about 2,700 B.P. to 2,000 B.P. (Lavin 1984:17; Juli and McBride 1984; Cruson 1991; Juli 1999). A cooling trend during the Early Woodland (Davis 1969:414; Parker 1987:10; McWeeney 1999:11) is thought to have reduced population sizes and regional ethnic distinction as the hickory nut portion of the resource base was significantly decreased, although the apparent decline in populations may possibly be related to other factors such as the inability to confidently distinguish Early Woodland sites from those of other periods (Filios 1989; Concannon 1993). Climatic deterioration and depopulation are in turn thought to have inhibited the progression towards, and association with, more complex social structures and networks that were developing further to the west and south (Kehoe 1981:215). A proliferation of tobacco pipes may indicate the beginnings of agricultural

efforts in the northeast. The Early Woodland of this region, however, exhibits no direct traces of subsistence crop remains, indicating continuity with previous periods in terms of subsistence practices (Lavin 1984:18).

Materially, the period is marked by a substantial development of a ceramic technology, with the Early Windsor tradition of pottery being dominant in the Early Woodland of Connecticut (Rouse 1980:68; Lavin 1984:17, 1987). Both Early Windsor cord-marked and Linear Dentate ceramic forms were being produced at this time. Diagnostic projectile points can be developmentally traced to indigenous points of previous periods, consisting of many stemmed forms in addition to Meadowood and Fulton side-notched points, Steubenville points, and Adena-Rossville types, but now may have been used in conjunction with the bow and arrow (Lavin 1984:18). Adena-like boatstones are also found in this period. Although rare contact with the Adena culture is evident throughout assemblages of the period, the Early Woodland in southern New England remained a very gradual transitional period (Snow 1980:279,287; Lavin 1984:19).

A heightened use of ceramics has been erroneously promoted as an automatic indication of increased sedentism in many areas. Instead, central-based camps with restricted seasonal encampments appear to be the dominant settlement pattern (Snow 1980:287). Minimal archaeological evidence from the lower Connecticut River Valley appears to suggest a similar settlement pattern to the Terminal Archaic in which large riverine sites served as central bases with upland seasonal dispersal or specific task sites (McBride 1981; McBride and Dewar 1981:49), but with a lesser degree of sedentism. Interior uplands populations also decreased during the Woodland era, perhaps related to the intensification of agricultural resources along major riverine and coastal areas (Wadleigh 1981:83). The trend towards greater mobility may in part be attributed to the decline in the use of steatite that no longer gave certain groups control over critical and restricted resources, as indicated by the declining ceremonialism of burial sites at the time which were more often located in habitation sites and exhibited combinations of secondary cremation features and primary inhumations (Walwer 1996). This transition in the socio-economics of the region was brought about by the decrease in importance of steatite as ceramics obscured its value for producing durable containers. Partially preserved primary inhumations appear for the first time in the region based on preservation considerations.

Middle Woodland

The Middle Woodland period lasted from about 2,000 B.P. to 1,000 B.P. (Lavin 1984:19; Juli and McBride 1984; Cruson 1991; Juli 1999). The climate was returning to the conditions basically witnessed today (Davis 1969:420; McWeeney 1999:11). It is a period which exhibited considerable continuity with previous periods in terms of both subsistence and material culture. Cylindrical pestles and groundstone hoes are tools diagnostic of the period and reflect developing agricultural efforts, including the cultivation of squash, corn, and beans on a seasonally tended basis (Snow 1980:279). Direct evidence for agriculture in the form of preserved vegetal remains, however, does not generally appear until the early Late Woodland (Lavin 1984:21) when corn is thought to have been introduced into the Connecticut River Valley from the upper Susquehanna and Delaware River Valleys (Bendremer and Dewar 1993:386). Projectile point forms from the period include Snyders corner-notched, LongBay and Port Maitland side-notched, Rossville

stemmed, and Greene lanceolate types. A proliferation of ceramic styles was witnessed during the Middle Woodland (Rouse 1980; Lavin 1984:19-20, 1987; Lavin and Kra 1984:37), including Rocker Dentate, Windsor Brushed, Sebonac Stamped, Hollister Stamped, Selden Island, and Windsor Plain types that were all also produced in the Late Woodland, with the exception of the Rocker Dentate. Ceramic forms from the Early Woodland were still being produced as well. Minor traces of the Hopewell cultures to the west are also present in the archaeological record of this period. Site types and distributions in the lower Connecticut River Valley imply that a moderate increase of sedentism with aspects of a radiating settlement pattern took place on large rivers, supported by differentiated upland task sites (McBride 1981; McBride and Dewar 1981:49). This trend may have been supported by the expansion of tidal marshes up larger rivers (McBride 1992:14).

Late Woodland

The Late Woodland period extended from approximately 1,000 B.P. to 1600 A.D., the time of widespread European contact in the broader region (Snow 1980:307; Kehoe 1981:231; Lavin 1984:21; Feder 1984, 1999). A warmer climate and increased employment of large scale agriculture for subsistence in New England were associated with increased population densities, more sedentary settlements, and more permanent living structures and facilities in larger villages. Settlements in Connecticut, however, tended to remain smaller with only small scale agricultural efforts, and as part of a seasonal round in which smaller post-harvest hunting and task-specific settlements were established in fall, and protected settlements occupied in winter (Guillette 1979:CI5-6; McBride and Bellantoni 1982; Lavin 1984:23; Starna 1990:36-37). Instead of maintaining permanent villages near agricultural plots, aboriginal populations engaged in the slashing and burning new plots and let old plots lie fallow periodically (Salwen 1983:89). In this area, domestic resources included corn, beans, squash, Jerusalem artichoke, and tobacco (Guillette 1979:CI5; Starna 1990:35). Agriculture was largely maintained by women, with the exception of tobacco (Salwen 1983:89; Starna 1990:36). Deer, small mammals, fish and shellfish, migratory birds, nuts and berries, and other wild foods continued to contribute significantly to the diet (Waters 1965:10-11; Russell 1980). Many of the foods produced were dried and/or smoked and stored in baskets and subterranean holes or trenches.

The increasing diversity of wild estuary resources may have served to increase sedentism in the coastal ecoregions of Connecticut (Lavin 1988:110; Bragdon 1996:67), while agriculture and sedentism may have been even more prominent along the larger river bottoms (Bragdon 1996:71). Late Woodland settlement patterns of groups in the uplands interior ecozones of Connecticut may have included the highest degree of mobility, while many sites from the central lowlands represent task-specific sites associated with larger settlements along the Connecticut River (McBride 1992:16). House structures consisted of wigwams or dome-shaped wooden pole frameworks lashed and covered with hides or woven mats, and clothing was made from animal hides (Guillette 1979:CI7-8; Starna 1990:37-38). Pottery for the period is defined as the Late Windsor tradition in Connecticut (Rouse 1980:68; Lavin 1984:22, 1987). Most of the ceramic forms of the Middle Woodland were still being produced, in addition to the newer Niantic Stamped and Hackney Pond forms. Ceramics of the East River tradition also appear in the area during the Late Woodland, having originated and been concentrated in the New York area (Rouse 1980; Wiegand 1987; Lavin 1987). The period exhibits some continuity in terms of

projectile point forms, although the Jack's Reef, Madison triangular, and Levanna points are considered diagnostic for the period. As likely with earlier periods, the material culture included various textile products such as baskets and mats, and wooden utensils such as bowls, cups, and spoons (Willoughby 1935; Russell 1980:56).

Unlike groups of the Mississippi valley, the overall cultural pattern for the entire Connecticut Woodland era exhibits considerable continuity. Interregional contact increased during this period, however, with non-local lithic materials increasing from as low as 10% to as high as 90% from the early Middle Woodland to the Late Woodland (McBride and Bellantoni 1982:54; Feder 1984:105), although most trade appears to have been done between neighboring groups rather than initiated through long-distance forays (Salwen 1983:94). The lack of enormous agricultural surpluses for the time is indicated by the low density of small storage features in habitation sites, as well as the ubiquitous primary inhumation of people without a select portion of graves exhibiting special treatment that would require high energy expenditure (Walwer 1996). As confirmed by early ethnohistoric accounts, this suggests a largely egalitarian and relatively mobile society for the Late Woodland despite the fact that this period marks the highest development of food production (i.e. agriculture) during the course of prehistory in the region. Corn was undoubtedly important, however, as a disproportionate amount of the simple, flexed burials were oriented towards the southwest which was the aboriginally acknowledged direction for the origins of corn and the Spirit Land.

Local Sites and Surveys

According to site files of the Connecticut Office of State Archaeology (CT OSA 2023) and Connecticut State Historic Preservation Office (CT SHPO 2023), there are ten previously recorded prehistoric archaeological sites within one mile of the project area (Figure 4). At about one mile to the southeast, the Uniroyal Nursery site (8-001) was surface collected by an amateur archaeologist, and produced a lanceolate quartz projectile point and debitage. More quartz tools and debitage were recorded at Bernard Berge's Site (8-025) nearby. The Claypit Field site (8-004) is about one-half mile to the southeast of the project area, where another surface collection procured a dentate stamped pipe stem, thus Woodland era to Contact period, and a similar find occurred about one mile to the southwest at the Carrington Site (8-019). The Krupien Site (8-027) is located about one mile to the west of the project area, where a narrow stemmed quartz projectile point was recovered. The Hinman Firehouse site (8-031) reportedly yielded hundreds of projectile points from a site just over one-half mile to the west. A Late Archaic Brewerton side-notched projectile point was recovered from the Paprosky's Vegetable Garden site (8-028) at about one mile east of the project area. Other sites (8-018; 020; 023) of the area do not have substantive information other than site location.

Summary

A low to moderate density of archaeological sites has been recorded in the region immediately surrounding the project area. Together with information from other surveys and previously recorded sites of the area, regional subsistence-settlement models described above are represented, with a variety of sites including smaller upland camp sites given the small stream environments in the area. The distribution of previously recorded sites is dispersed among the various tributaries of Bladens River, with most sites found by amateur archaeological surface collections, and possibly imprecise recording and mapping in some cases.

Figure 4: Prehistoric Sites of the Region

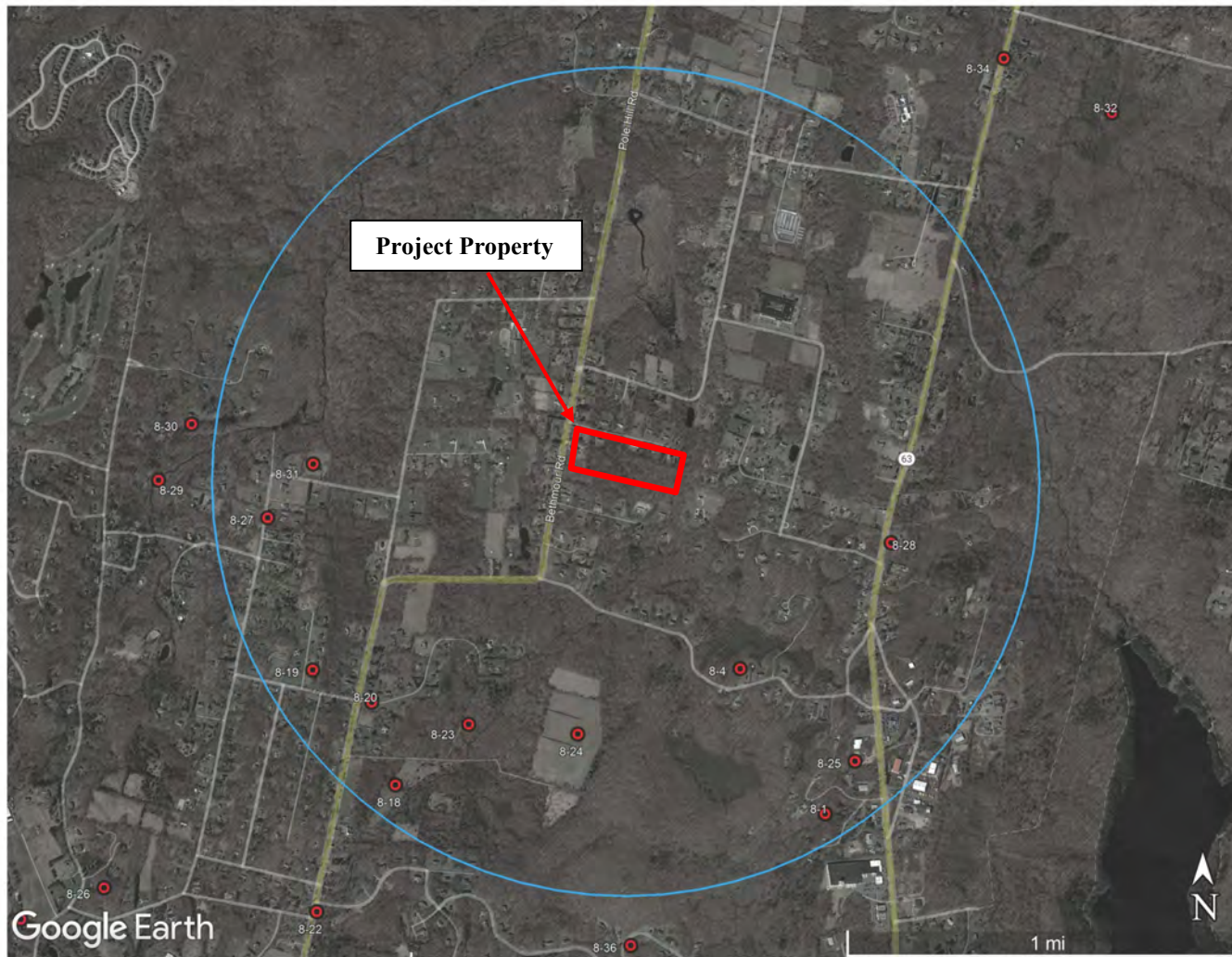


Figure 4: From CT SHPO 2023. Red dots are previously identified archaeological site locations, all prehistoric within the one-mile radius of 428 Bethmour Road.

Local History

Contact Period

The Contact period is designated here as the time ranging from the first substantial contact between Europeans and Native American inhabitants of the area, to the time the area was thoroughly occupied by Euroamerican settlers, from roughly 1600 to 1700. The first contact between aboriginal populations of the broader region and European explorers occurred in 1524 when Verrazano reached the coast of New England (Terry 1917:16). Others followed in the first decade of the 1600s (Salwen 1983). In 1614, Dutch explorers reached the Connecticut River (DeForest 1852:70; DeLaet 1909 [1625-1640]:43), and in 1625 they were met by the Quinnipiac in New Haven Harbor (Brusic 1986:9) when they established fur trading relationships with the native inhabitants in the region until the early 1630s (Guillette 1979:WP2-4). Substantial English settlements in the area started in 1635-1636. DeForest (1852:48) estimated about 6,000 to 7,000 Native Americans in Connecticut at this time, while Winthrop had estimated somewhere between 12,000 and 15,000 and most others (Trumbull 1818:40; Gookin 1970[1674]; Cook 1976; Snow 1980:35; Bragdon 1996:25) estimate between 16,000 and 20,000.

The composition of the tribes at the time of contact is fairly well known, although boundaries fluctuated significantly, as did the political alliances by which the tribes could be defined (Thomas 1985:138). Three major divisions of Algonkian speaking groups can be delineated, and their territories conform well to ecozone distributions (see Dowhan and Craig 1976:26 and Speck 1928:Plate 20), including the Mohegan-Pequot range in the Southeast Hills and Eastern Coastal ecoregions, the Nipmucks in the Northeast Hills and Northern Uplands ecoregions, and tribes of the Wappinger-Mattabesec Confederacy in the North Central Uplands and most of western Connecticut. The validity of the Wappinger-Mattabesec Confederacy as a cultural entity has been challenged (Salwen 1983:108-109), with many smaller and somewhat independent tribes occupying much of the western half of the state.

The Paugussetts and Naugatucks occupied the territory surrounding the project area at the time of initial contact, with the Paugussetts on the western side of the Housatonic and lower Naugatuck Rivers, and the Naugatucks to the north near the town of the same name, although records of various early land transactions suggest that the Paugussetts and Naugatucks were very integrated and closely affiliated, along with the nearby Pequannocks, Pootatucks, and Wepawaugs who have all been loosely termed Paugussetts (DeForest 1852:49-50; Guillette 1979:GH-1-2). The Paugussett confederacy of these five tribes occupied an area loosely defined by the West River of West Haven to the east, Sasco Brook in Fairfield to the west, the confluence of the Shepaug and Housatonic Rivers to the north, and further north along the Naugatuck River drainage (Spiess 1933:31; Guillette 1979:GH-2). According to Speck (1928), the Paugussetts were linguistically part of the larger Wappinger-Mattabesec Confederacy of tribes that extended west of the Connecticut River and onto Long Island.

Ethnohistoric sources yield clues to aboriginal Final Woodland and early Contact settlement patterns (McBride and Bellantoni 1982; Starna 1990:36-37). Spring settlements were located to take advantage of anadromous fish runs in larger drainages and along the coast. Late spring attention focussed on tending corn fields. Semi-sedentary settlements near these fields were supported by special task hunting and gathering sites. Dispersal in the late fall and winter brought smaller groups into protected, upland or interior valleys where hunting and gathering continued, for a longer duration in the Contact period than earlier and by a smaller subsistence

unit (family). Fortified villages were likely a response to very early Contact period intertribal political strife resulting from increased economic pressures of sedentism and territoriality (Salwen 1983:94; McBride 1990:101; but see Thomas 1985:136). One such fortified village of the Paugussetts is said to have been located on the Housatonic less than a mile north of its confluence with the Naugatuck River (DeForest 1852:51). Large villages were found to be associated with a central-based circulating settlement pattern with family units dispersing from and returning to the major settlement on a seasonal basis in the lower Connecticut River Valley and surrounding region in the early Contact period (McBride 1981). Eventually, however, many Native American populations had been dispersed and afflicted by disease, warfare, and intertribal conflict to the point that small, scattered reservations served as the last community sites for various aboriginal populations in the area. Small Native American settlements of the late 17th century may have been located at Hospital Bluff on the west side of the Naugatuck, and near East Mountain on Mad River to the east (Anderson 1896(1)).

The early Contact period economic base for Native Americans in Connecticut continued to consist of hunting deer and small mammals, gathering berries, nuts and roots, and procuring shellfish and fish on larger drainages and along the coast (Waters 1965:7; Salwen 1970:5). This basic subsistence strategy was supported by varying intensities of horticulture, including the production of corn as the staple, as well as squash, beans, Jerusalem artichoke, and tobacco (Guillette 1979:CI5; Starna 1990:35). The importance of corn is evident in the description of ritual activities, including the Green Corn Festival and similar ceremonies that extended with various groups into the present day (Speck 1909:194-195; Speck 1928:255; Tantaquidgeon 1972:81; Fawcett 1995:54-57). Elderly women held extensive knowledge of wild plants which provided a host of medicines and treatments (Tantaquidgeon 1972; Russell 1980:35-37). Wigwams continued to serve as the principal form of housing, in some cases well into the 18th century (Sturtevant 1975).

The material culture included a mix of aboriginal forms as well as some European goods such as metal kettles and other metal implements (knives, projectile points), cloth, glass beads, and kaolin pipes (Salwen 1966, 1983:94-96). Wampum served as an important trade item for the Native Americans with European traders, but more significantly had served as symbolic signs of allegiance or reciprocity and sacred markers or tokens of honor in the form of belts (Guillette 1979:CI8; Ceci 1990:58-59; Salisbury 1990:87; Fawcett 1995:59). With European metal drill bits, tribes along the coast were now mass producing wampum for trade with the Dutch and English who in turn used the shell beads to trade with other tribes further inland (Salwen 1983:96; Ceci 1990:58). Late Contact period Euroamerican goods included various metal tools, glass bottles, ceramic vessels, kaolin clay tobacco pipes, and nails (McBride and Grumet 1992). Unlike the Late Woodland, Contact aboriginal lithic products were once again mostly manufactured from local sources (McBride and Bellantoni 1982:54). Dugout canoes may have continued to provide a major form of transportation in larger drainages (Salwen 1983:91). While colonization brought new material goods to Native Americans in the area in exchange for land and services, the indigenous inhabitants became increasingly subject to legislative and economic restrictions by the colonists (Salisbury 1990:83).

Sachems and councils of leading males formed the basic political unit for groups of villages (Gookin 1970; Simmons 1986:12-13), along with clan mothers whose authoritative roles became diminished as a result of a strong European male-leadership bias (Fawcett 1995).

Tributes paid to sachems were generally used as reserves for the tribe at large. Although sachems were generally assigned by hereditary lineage, this was not always the case (Bragdon 1996:140-141). Authority was usually enforced by persuasion of a council. Shamans were "magico-religious" specialists of the tribes who also had a considerable role in leadership and decision-making (Speck 1909:195-196; Simmons 1986:43; Starna 1990:42-43). Rules of obligation and reciprocity operated on all levels of tribal-wide decision-making (Bragdon 1996:131-134), serving to diffuse centralized authority. Other special status roles included warriors and persons who had visions, thus social status was largely based on achievement and recognition. While the assignment of lineality (i.e. matrilineal vs. patrilineal) for the area tribes is still largely debated (Bragdon 1996:157), the well established practice of bride-pricing supports the contention of patrilineal social organization (Speck 1909:193; Salwen 1983:97). Post-marital residence appears to have been ambilocal.

On a larger scale, more powerful tribes demanded tributes from smaller ones, often resulting in loose alliances between the latter. This process resulted in a dynamic political situation that prompted intertribal conflict, especially after contact with Euroamericans (Guillette 1979; Bragdon 1996). The European settlers would eventually use this embedded rivalry system to their advantage. In the period between 1616 and 1619, and more severely around 1633, disease epidemics would initiate a trend of drastic reductions in the native population that aided in Euroamerican settlements of the area (Snow and Lanphear 1988; Snow and Starna 1989; Starna 1990:45-46). Diseases introduced into the Americas included chicken pox, cholera, diphtheria, malaria, measles, oncocercosis, poliomyelitis, scarlet fever, smallpox, tapeworms, trachoma, trichinosis, typhoid fever, whooping cough, and yellow fever (Newman 1976:671).

In 1637, the Paugussetts provided refuge for Pequots who were fleeing after their defeat in the Pequot "War", although this resulted in the defeat of the hosts by the colonists (Guillette 1979:GH-2). The Paugussetts may have been centered along the Naugatuck in western Ansonia at this time (Larson 1976:1). First land transactions between the Paugussetts and English settlers occurred in Milford about 1639 (Guillette 1979:GH-3-4).

Trade between the English colonists and the Paugussetts was apparently peaceful in the early part of the Contact period, but after the war between Hudson River tribes and the Dutch in the early 1640s, colonists in Connecticut became concerned about the possibility of "uprisings" and proceeded to enact laws which would restrict Native American activity (Guillette 1979:GH-4). Friction increased as the Paugussetts began to become familiar with the consequences of their previous land transactions as well as agreements to pay tribute to Connecticut for protection against the Mohawks. English settlers let livestock feed freely in Native American corn fields, and an effort by Wepawaugs to burn underbrush for ecological purposes in Milford resulted in a larger fire that was interpreted by colonists to be a Native American attack (DeForest 1852:222). Other tensions of the 1640s included personal skirmishes and issues over European weapon and liquor procurement by Native Americans in the area. As colonist populations grew and the perceived Native American threat diminished, land purchases proliferated in the 1650s. Early settlers of the Naugatuck Valley region were granted rights to mine graphite in the area by 1657. By 1665, almost all property in the southern portions of Paugussett territory had been sold by Ansantawae and the other sachems without full realization of the consequences (DeForest 1852:270; Orcutt 1972 [1882]:14-15).

The aboriginal populations of the area found it increasingly difficult to continue their original adaptations, and were allotted areas on Golden Hill (Pequannocks) in Bridgeport in 1659, and Turkey Hill (Wepawaugs) in Derby on the Housatonic in 1671 to serve as reservations (DeForest 1852:264; Orcutt 1972 [1882]:13; Guillette 1979:GH1) where many subsequently tried to subsist by manufacturing baskets and engaging in other small industries. Land disputes continued after this time, and in 1680 these conflicts led to the establishment of the Corum Hill Reservation in Huntington, the agreement for which included the rights of the Paugussetts to procure fish and game in the Derby area (DeForest 1852:270; Guillette 1979:GH-8). Native American populations declined throughout the Contact period, and many in southwestern Connecticut emigrated to the north and west after King Philip's War of 1675.

As early as 1639, Euroamerican settlers from New Haven started to occupy the greater Milford area, the town then including the western part of Bethany. Bethany territory itself was not occupied by Euroamerican settlers until Alexander Bryan of Milford purchased land from Nehantond, a Naugatuck tribal member, in 1664. As with their southern counterparts, these late sales resulted in the effective removal of northern Paugussetts to areas not yet occupied by English settlers to the north and west. By 1710, approximately 500 Paugussetts remained in the greater Housatonic valley region (Cook 1976:68).

18th Century

In 1731, the Paugussett Nation was dismantled (DeForest 1852:354; Guillette 1979) as removals continued. Waterbury had a short-lived Quinnipiac reservation on the southeast part of East Mountain at this time (Anderson 1896(1):357). The Turkey Hill reservation population was supposedly reduced to four persons by 1774, and the Golden Hill reservation population reduced to seven by 1765 (DeForest 1852:354-355). The end of the 18th century witnessed the continued decline of reservation populations due to land sales, Euroamerican encroachments on the land, as well as migrations to other parts of the state and New York during the "Brothertown" movement (Guillette 1979:GH-8,9). These combined factors essentially led to the end of aboriginal adaptations by the end of the 18th century when most Native Americans of the region were forced to become somewhat integrated into Euroamerican communities. By 1850, very few Paugussetts were in the area, most having moved to join the Scaghticokes or Iroquois further to the north (Spiess 1933:31).

A substantial land purchase in 1700 by Milford settlers was known as the "Two-Bit Purchase," signifying the small amount of compensation for what was not likely fully comprehended as exclusive, indefinite land-use rights. Other land sales followed in the early 18th century. Amity Road (Route 63) was a well established route through Bethany by the first quarter of the 18th century, connecting Waterbury and New Haven. Amity Parish was incorporated by the General Assembly in 1738, consisting of most of Bethany and Woodbridge territory (Whitlock 1982:10; Sharpe 1989:41), and the Congregational Church was built at the Woodbridge town green a few years later. The first schoolhouse of Amity was constructed at the intersection of Old Amity Road and Meyers Road about one-half mile east of the project area in 1750 (Sharpe 1989:104). In 1762, Bethany and Woodbridge were divided, with Bethany Parish receiving its name from a biblical reference (Lines 1905:2; Whitlock 1982:143-144; Sharpe 1989:2,9). The first Congregational Church in Bethany was built at intersection of Amity Road and Dayton Road, also about one-half mile east / northeast of the project area, and completed by

1773. Bethany supplied men and provisions to the militia effort of New Haven following an attack by the British in the summer of 1779, although Tories of the area were still active. The town of Woodbridge was formally incorporated in 1784, and at that time included Bethany territory (Whitlock 1982:148). Litchfield Turnpike (Route 69) was built and improved by the Straits Turnpike Company in 1797 (Sharpe 1989:111). Bethany Union Library was founded in 1798, and the Episcopal Church was organized in 1799.

19th Century

The project property was probably part of the Daniel Tolles family land holdings of the early 19th century, and it was likely farmed at that time. A mid-19th century map (Whiteford 1852) shows N. (Nehemiah) Tolles as the owner of a homestead to the north of the project property on Bethmour Road, with no other homes on the east side of the road at that time (Figure 5a). Early 19th century industry in Bethany was focused on wool production (Sharpe 1989:45). The town of Bethany was not separated from Woodbridge and incorporated as its own town until 1832 (Lines 1905:6; Whitlock 1982:142,149; Sharpe 1989:2). In an unfortunate event to follow, the first selectmen removed a last indigenous Native American family to Derby, who were then mostly wiped out by smallpox. New schools and churches were built (Sharpe 1989), and the town reached a population of 1,170 by 1840, followed by an overall decline in population until the early 20th century due to the migration of farmers and others westward (Whitlock 1982:149). A railroad line from Cheshire to Plainville was built in 1848 to within two miles of Bethany to the east.

By the mid to late 19th century, the Johnson family owned the project property and other lands on the east side of Bethmour Road. Nearby the project property, the Street B. Todd family owned a 22-acre parcel with a dwelling acquired from his father-in-law Spencer Hotchkiss according to land records (Land Records Volume 5, page 208 - 1857), with the Johnsons owning land on all sides except for the highway to the west. The house was a Greek Revival structure (Bunton 1972), likely built in the 1830s to 1850s, thus possibly the same as Tolles house but mapped to the south of the project property, likely in error (Figure 5b). Unlike the Todd parcel, there was no mention of any particular structures on parcels owned by the Johnson family that surrounded the 22-acre parcel.

The late 19th century of Bethany was marked by the development of utilities. In 1888, the West River was dammed to form Lake Watrous that was managed by the New Haven Water Company, followed by the creation of other lakes over the next decade (Sharpe 1989:44). The telephone was introduced to Bethany by 1898.

20th Century+

At the start of the 20th century, the town population was reduced to 517, about one-half its peak from the prior century (Lines 1905:7). A chestnut blight in 1910 depleted an important lumber supply in town. A town hall was built in 1914, and the Bethany Grange was organized the following year. Amity Road was paved in 1918. 1920 witnessed the low point in Bethany population at just 411 people, followed by steady population increases. In 1934, the school system began to consolidate, with the Bethany Community School on Peck Road replacing four one-room schoolhouses. In 1936, Clark Memorial Library was established.

[illegible]

19

In 1915, Dwight L. Johnson sold 37 acres of land inclusive of the project property to Morris Liebman and others (LR Volume 12, page 248). Fifteen years later, rights were conveyed to the Drazen Lumber Company, and by 1936 Lena Krupien had ownership of the property. A survey map from 1935 shows the Drazen Lumber Company land before acquisition by Krupien, with an existing house directly to the north of the project property that is listed as Parcel “V,” and the same map showing the delineation of stone wall alignments that still exist today. The house to the north likely relates to the Street B. Todd house (Town Historian William Brinton, pers. comm. 2023), and it is likely that the depiction of that house on the Beers 1868 map to the south of the project property was in error (see Figures 5c and 5d).

The housing boom that followed World War II reached Bethany. The small house that occupies the project property was built in 1949 according to the town assessor’s office. By 1950, the population of the town was 1,318, triple that of the low point three decades earlier. By 1960, the population nearly doubled again, to 2,384, and by 1970 it nearly tripled to 3,857. The Rolling Green Acres subdivision of the 1960s directly to the north of the project property and on other land nearby included the Street B. Todd homestead site, with the project property listed in land records and on survey maps as Parcel “V,” including the 2.51 house lot of the project property and the 19+ acres to the rear. A survey map from 1980 shows the existing house and detached garage on 2.05 acres, surrounded by other land owned by Krupien and some Rolling Green Acres subdivision land directly to the north, where the Street B. Todd house was razed in 1964 (Bunton 1972).

Local Sites and Surveys

The only property in Bethany recorded with the National Register of Historic Places (NRHP) consists of the Wheeler - Beecher House on Amity Road over one mile northeast of the project area (Clouette 1976). The house was built in 1807 by David Hoadley (builder of the United Church in New Haven) for first owner Darius Beecher, who subsequently moved west and reportedly lost his family fortune (Sharpe 1989:101). The Street B. Todd house, a Greek Revival House owned by father-in-law Spencer Hotchkiss, was located to the south of the project property on Bethmour Road, and was razed in 1964 as the only historic house in the area at that time (Bunton 1972). There have only been two professional archaeological surveys in Bethany, one related to an electric transmission line through Bethany (Raber 2013), the other related to the Bethany Farms subdivision located in the southern part of town (CAS 1994). There are no historic archaeological sites previously recorded within one mile of the project area.

Summary

Originally a part of the larger town of Woodbridge, Bethany was not incorporated until 1832, and remained very agricultural until the middle of the 20th century. The project property was owned by the Johnson family by the middle of the 19th century, although it appears to have remained as open land until the 1930s when the Drazen Lumber Company had control of the property for a brief time. The 1949 existing house was set on a two-acre lot carved off a larger parcel, with the land owned by the Krupien family for much of the 20th century.

Figure 5c: Historic Sites of the Area (1934 Map)



Figure 5c: From Fairchild 1934.

Figure 5d: Historic Sites of the Area (1947 Map)

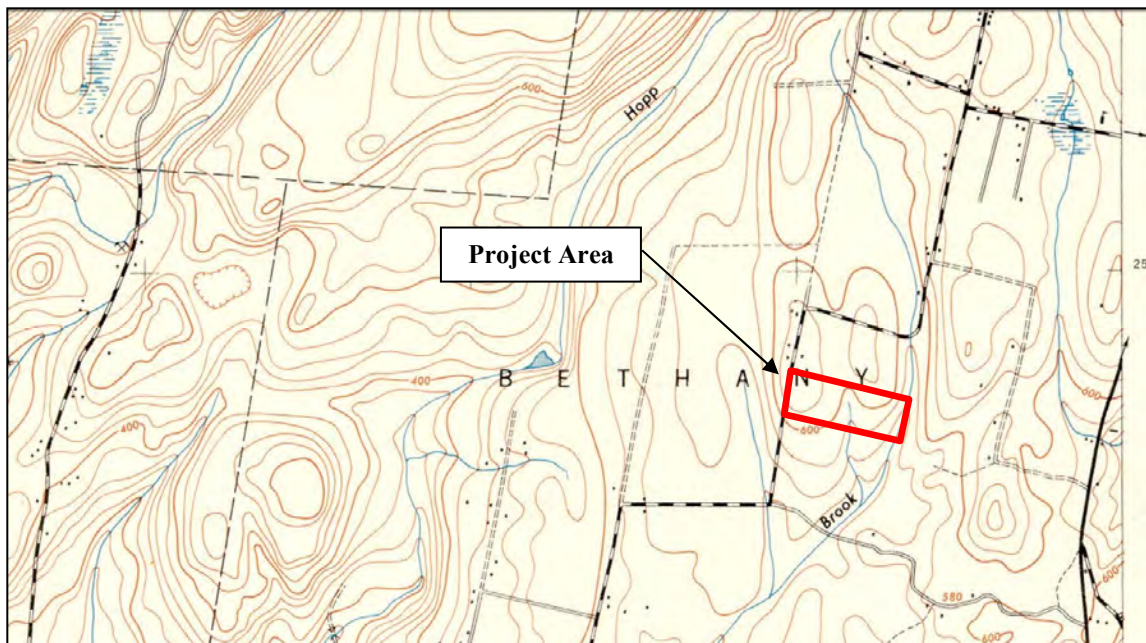


Figure 5d: From USGS 1947.

CHAPTER 3: CONCLUSION

Prehistoric Sensitivity

Background research and the pedestrian surface survey indicate a low sensitivity for potential prehistoric cultural resources in the project area. A statistical prehistoric landscape sensitivity model developed and employed by ACS utilizes eight environmental variables to rank sections of project properties relative to a scale of 100.0 (www.acsarcheology.com/sensitivity-model.html). In this case, the project area scores no higher than 6.5 out of a possible 100.0, and therefore solidly within the low (0-20) sensitivity range. Factors contributing to this low sensitivity score include great distance to the nearest major water source for the project area, rocky hill slope context, and fine particle fraction for dominant soils. Pine Brook does flow through the very eastern end of the project property, although this section of the property is on the order of 1,000 feet to the east of the project area of development, and only a minor body of wetlands lies in close proximity to the eastern end of the project area where there are moderate slopes and very rocky soil contexts. A review of previously recorded prehistoric sites in the region reveals none in close proximity to the project area, with sites concentrated close to substantial water sources, particularly on glacial meltwater landforms and alluvial terraces. No further archaeological conservation efforts are required for the proposed project development with respect to potential prehistoric cultural resources.

Historic Sensitivity

Historically, the project area has a moderate sensitivity for historic cultural resources. The project setting was probably on the outskirts of Naugatuck settlement range during the Contact period, a tumultuous time when indigenous populations were experiencing significant impact from non-indigenous disease, land occupation by Euroamerican settlement, and removal to other regions. Euroamerican settlement was minimal during the latter part of the 17th century, and was relatively sparse by agriculturalists until the early 20th century. Amity Road (Route 63) and then Litchfield Turnpike (Route 69) were early traveled routes through Bethany, which was not incorporated as a town until 1832. By the 1850s, the project property and surrounding lands were owned by the Tolles family, with the Nehemiah Tolles homestead located to the north on Bethmour Road. By the 1860s, the Greek Revival house owned by Spencer Hotchkiss had been conveyed to his son-in-law, Street B. Todd, mapped in error by then to the south of the project property, with that homestead sold many times during the 20th century and finally razed in 1964. The surrounding land, including the project property, was owned by the Johnson family for much of the 19th century, likely acquired from the Tolles family. Land records and historic maps reveal that the existing house on the project property was built in 1949 on land owned by Lena Krupien and acquired from the Drazen Lumber Company and otherwise apparently vacant from the mid-19th century through the present, although it is possible that the Tolles family or predecessors could have constructed earlier homesteads along Bethmour Road in the vicinity of the project property.

The existing house on the project property that was constructed in 1949 is one story and measures only 620 square feet (Figure 6). It bears a concrete foundation, asphalt shingle pitched roof, and vinyl siding. A small detached garage just south of the house dates to 1952 (see Figure 6), and an associated shed dates to approximately 1980. The house and barn are in excess of 50 years old, but they do not bear distinctive architectural qualities that could render them eligible for the National Register of Historic Places (NRHP). Both are within an open field with tall grass and thick scrub growth reflecting lack of recent occupation (Figure 7). The ground surface surrounding the house and throughout the surrounding fields appear to be relatively undisturbed, and are separated from the wooded section of the project property to the east by a historic stone wall alignment (Figure 8). Constructed of locally available granitic gneiss, the various stone wall alignments of the property are depicted on current and historic survey maps (Figure 9), and are likely on the order of 200 years old, although they are not well formed. Their principal historic value is in their mapping, which could be useful information regarding historic agricultural lot sizes, particularly where there were different uses of the land within historic farms.

ACS recommends that any part of the development project within 300 feet of Bethmour Road be subject to a Phase Ib archaeological reconnaissance survey in advance of any construction impacts (Figure 10). The historic route of Bethmour Road is known to have contained homes dating back to the early 19th century and possibly earlier, and there could be traces of homesteads preceding those that appear on available historic maps or in land records confidently associated with prior land owners. Any such remains could reveal important information regarding Euroamerican population expansion into the frontier parts of early colonial settlements. Any further archaeological study of the project property should be subject to review by the Connecticut State Historic Preservation Office (SHPO).

Figure 6: House and Garage



Figure 6: East view of the house and garage at 428 Bethmour Road.

Figure 7: Field



Figure 7: Southeast view of the open field containing the house, with scrub growth.

Figure 8: Stone Wall – Field Edge



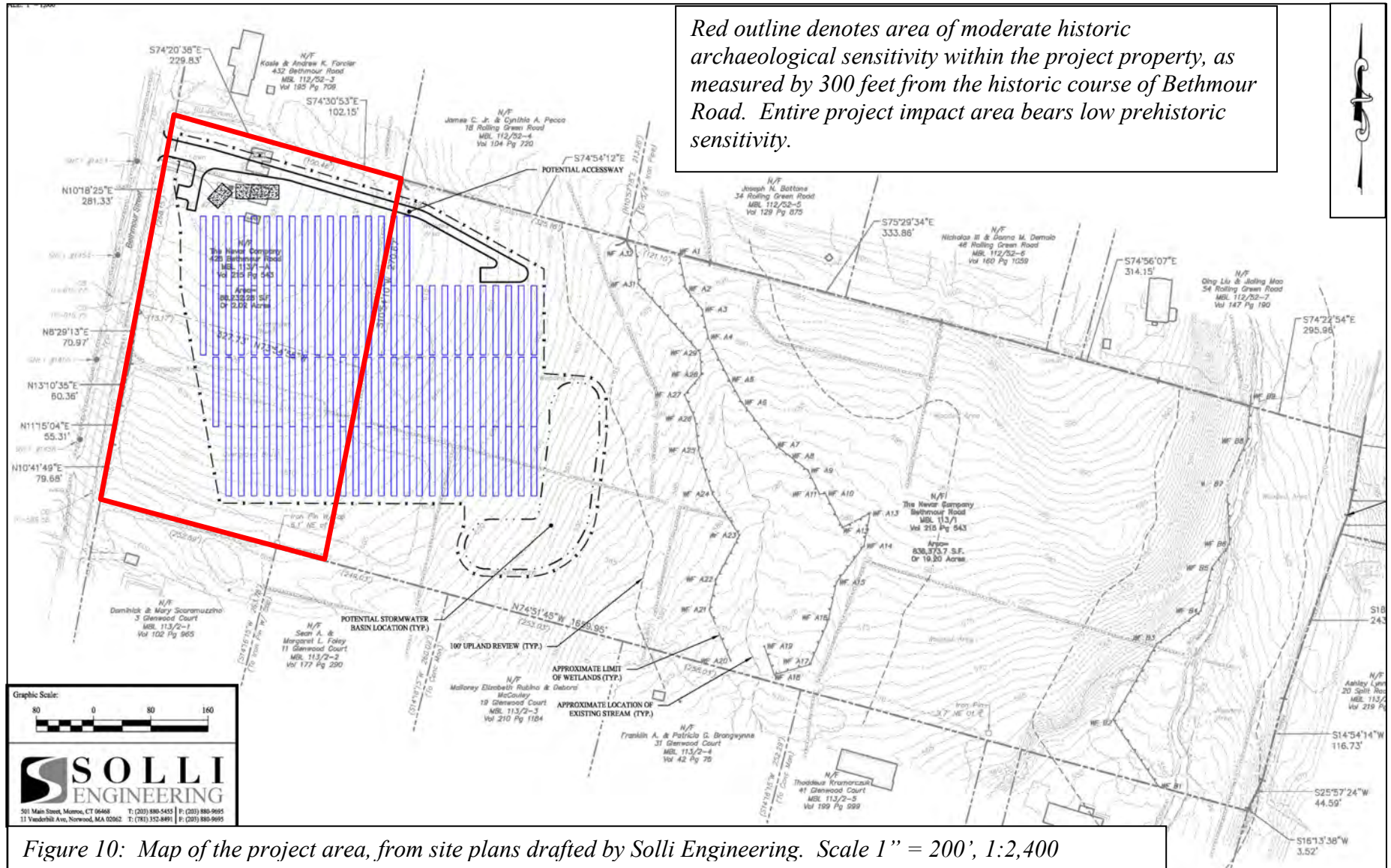
Figure 8: Southwest view of weakly developed stone wall alignment separating the open field in background from the wooded section of the property. A piece of oxidized farm equipment rests on the wall, scale bar five feet.

Figure 9: Stone Wall – Wooded Section



Figure 9: Southwest view of stone wall alignment in the wooded section of the project area.

Figure 10: Cultural Resource Sensitivity Map



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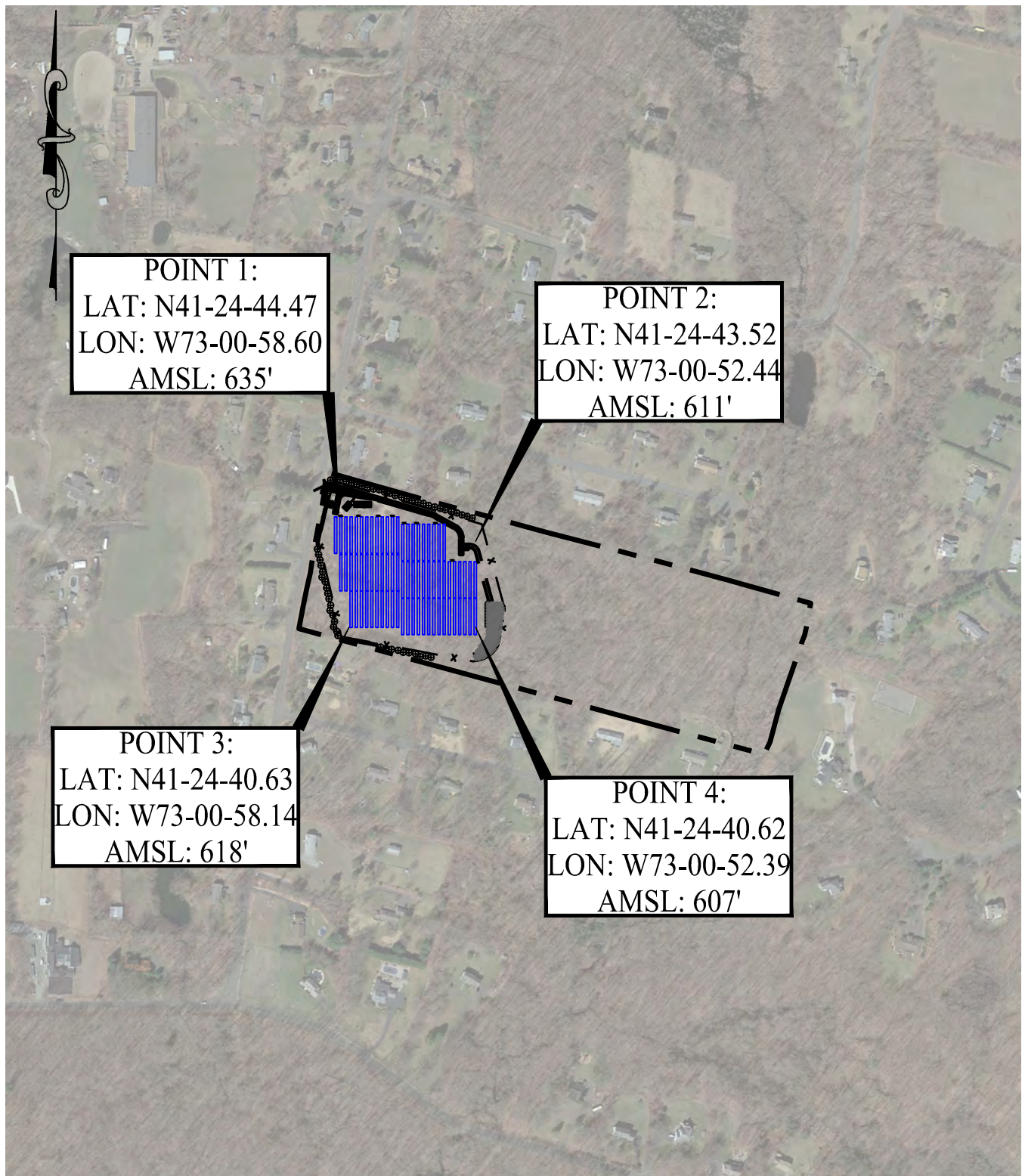
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Appendix E: FAA





Mail Processing Center
Federal Aviation Administration
Southwest Regional Office
Obstruction Evaluation Group
10101 Hillwood Parkway
Fort Worth, TX 76177

Aeronautical Study No.
2023-ANE-1235-OE

Issued Date: 02/23/2023

David H Trepeck
TRITEC Americas, LLC
888 Prospect Street, Suite 200
La Jolla, CA 92037

**** DETERMINATION OF NO HAZARD TO AIR NAVIGATION ****

The Federal Aviation Administration has conducted an aeronautical study under the provisions of 49 U.S.C., Section 44718 and if applicable Title 14 of the Code of Federal Regulations, part 77, concerning:

Structure:	Solar Panel Point 1
Location:	Bethany, CT
Latitude:	41-24-44.47N NAD 83
Longitude:	73-00-58.60W
Heights:	625 feet site elevation (SE) 10 feet above ground level (AGL) 635 feet above mean sea level (AMSL)

This aeronautical study revealed that the structure does not exceed obstruction standards and would not be a hazard to air navigation provided the following condition(s), if any, is(are) met:

Based on this evaluation, marking and lighting are not necessary for aviation safety. However, if marking/lighting are accomplished on a voluntary basis, we recommend it be installed in accordance with FAA Advisory circular 70/7460-1 M.

This determination expires on 08/23/2024 unless:

- (a) the construction is started (not necessarily completed) and FAA Form 7460-2, Notice of Actual Construction or Alteration, is received by this office.
- (b) extended, revised, or terminated by the issuing office.
- (c) the construction is subject to the licensing authority of the Federal Communications Commission (FCC) and an application for a construction permit has been filed, as required by the FCC, within 6 months of the date of this determination. In such case, the determination expires on the date prescribed by the FCC for completion of construction, or the date the FCC denies the application.

NOTE: REQUEST FOR EXTENSION OF THE EFFECTIVE PERIOD OF THIS DETERMINATION MUST BE E-FILED AT LEAST 15 DAYS PRIOR TO THE EXPIRATION DATE. AFTER RE-EVALUATION OF CURRENT OPERATIONS IN THE AREA OF THE STRUCTURE TO DETERMINE THAT NO

SIGNIFICANT AERONAUTICAL CHANGES HAVE OCCURRED, YOUR DETERMINATION MAY BE ELIGIBLE FOR ONE EXTENSION OF THE EFFECTIVE PERIOD.

This determination is based, in part, on the foregoing description which includes specific coordinates, heights, frequency(ies) and power. Any changes in coordinates, heights, and frequencies or use of greater power, except those frequencies specified in the Colo Void Clause Coalition; Antenna System Co-Location; Voluntary Best Practices, effective 21 Nov 2007, will void this determination. Any future construction or alteration, including increase to heights, power, or the addition of other transmitters, requires separate notice to the FAA. This determination includes all previously filed frequencies and power for this structure.

If construction or alteration is dismantled or destroyed, you must submit notice to the FAA within 5 days after the construction or alteration is dismantled or destroyed.

This determination does include temporary construction equipment such as cranes, derricks, etc., which may be used during actual construction of the structure. However, this equipment shall not exceed the overall heights as indicated above. Equipment which has a height greater than the studied structure requires separate notice to the FAA.

This determination concerns the effect of this structure on the safe and efficient use of navigable airspace by aircraft and does not relieve the sponsor of compliance responsibilities relating to any law, ordinance, or regulation of any Federal, State, or local government body.

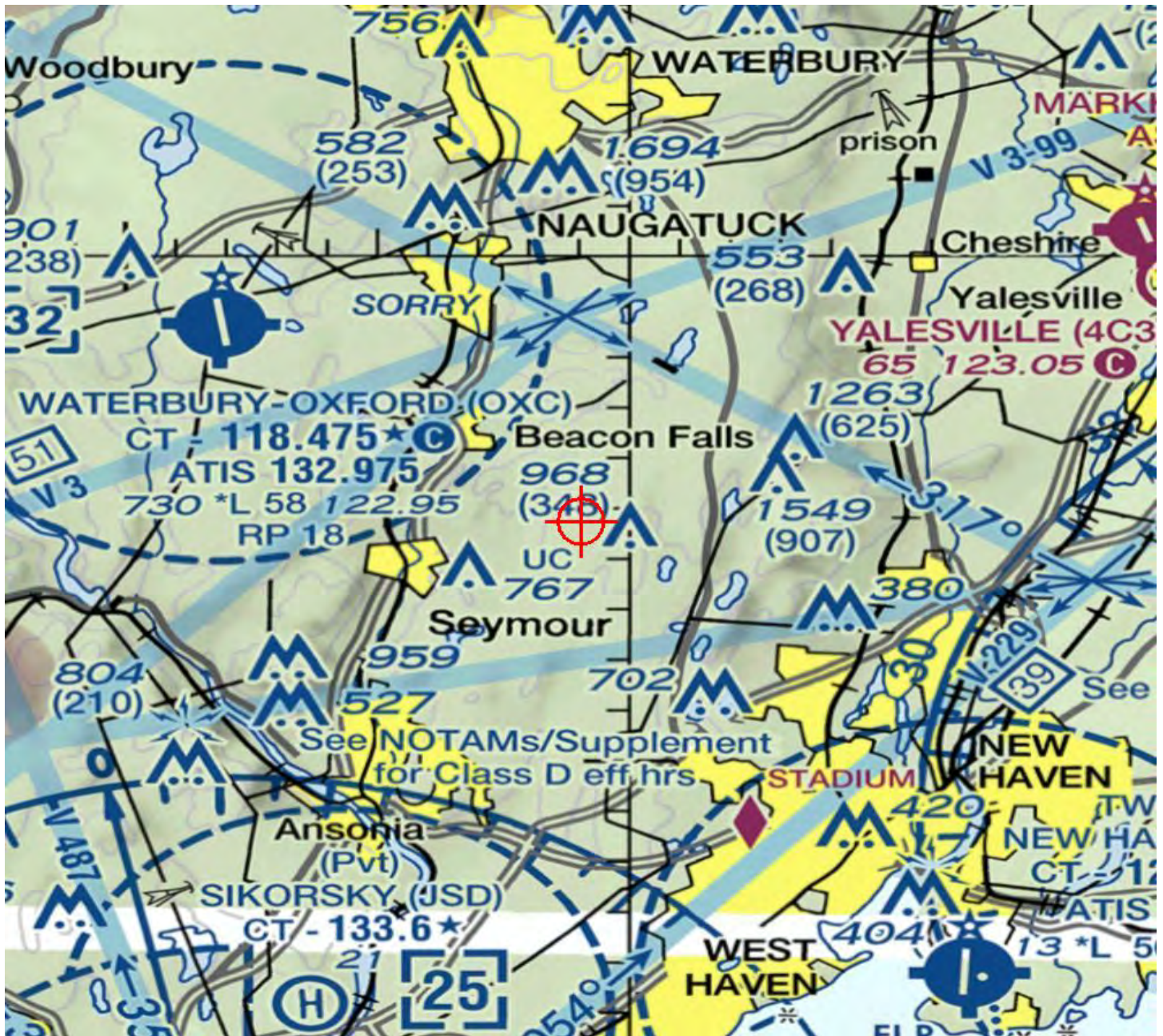
If we can be of further assistance, please contact our office at (404) 305-6430, or kelly.r.nelson@faa.gov. On any future correspondence concerning this matter, please refer to Aeronautical Study Number 2023-ANE-1235-OE.

Signature Control No: 572764419-573963113

(DNE)

Kelly Nelson
Specialist

Attachment(s)
Map(s)





Mail Processing Center
Federal Aviation Administration
Southwest Regional Office
Obstruction Evaluation Group
10101 Hillwood Parkway
Fort Worth, TX 76177

Aeronautical Study No.
2023-ANE-1236-OE

Issued Date: 02/23/2023

David H Trepeck
TRITEC Americas, LLC
888 Prospect Street, Suite 200
La Jolla, CA 92037

**** DETERMINATION OF NO HAZARD TO AIR NAVIGATION ****

The Federal Aviation Administration has conducted an aeronautical study under the provisions of 49 U.S.C., Section 44718 and if applicable Title 14 of the Code of Federal Regulations, part 77, concerning:

Structure:	Solar Panel Point 2
Location:	Bethany, CT
Latitude:	41-24-43.52N NAD 83
Longitude:	73-00-52.44W
Heights:	601 feet site elevation (SE) 10 feet above ground level (AGL) 611 feet above mean sea level (AMSL)

This aeronautical study revealed that the structure does not exceed obstruction standards and would not be a hazard to air navigation provided the following condition(s), if any, is(are) met:

Based on this evaluation, marking and lighting are not necessary for aviation safety. However, if marking/lighting are accomplished on a voluntary basis, we recommend it be installed in accordance with FAA Advisory circular 70/7460-1 M.

This determination expires on 08/23/2024 unless:

- (a) the construction is started (not necessarily completed) and FAA Form 7460-2, Notice of Actual Construction or Alteration, is received by this office.
- (b) extended, revised, or terminated by the issuing office.
- (c) the construction is subject to the licensing authority of the Federal Communications Commission (FCC) and an application for a construction permit has been filed, as required by the FCC, within 6 months of the date of this determination. In such case, the determination expires on the date prescribed by the FCC for completion of construction, or the date the FCC denies the application.

NOTE: REQUEST FOR EXTENSION OF THE EFFECTIVE PERIOD OF THIS DETERMINATION MUST BE E-FILED AT LEAST 15 DAYS PRIOR TO THE EXPIRATION DATE. AFTER RE-EVALUATION OF CURRENT OPERATIONS IN THE AREA OF THE STRUCTURE TO DETERMINE THAT NO

SIGNIFICANT AERONAUTICAL CHANGES HAVE OCCURRED, YOUR DETERMINATION MAY BE ELIGIBLE FOR ONE EXTENSION OF THE EFFECTIVE PERIOD.

This determination is based, in part, on the foregoing description which includes specific coordinates, heights, frequency(ies) and power. Any changes in coordinates, heights, and frequencies or use of greater power, except those frequencies specified in the Colo Void Clause Coalition; Antenna System Co-Location; Voluntary Best Practices, effective 21 Nov 2007, will void this determination. Any future construction or alteration, including increase to heights, power, or the addition of other transmitters, requires separate notice to the FAA. This determination includes all previously filed frequencies and power for this structure.

If construction or alteration is dismantled or destroyed, you must submit notice to the FAA within 5 days after the construction or alteration is dismantled or destroyed.

This determination does include temporary construction equipment such as cranes, derricks, etc., which may be used during actual construction of the structure. However, this equipment shall not exceed the overall heights as indicated above. Equipment which has a height greater than the studied structure requires separate notice to the FAA.

This determination concerns the effect of this structure on the safe and efficient use of navigable airspace by aircraft and does not relieve the sponsor of compliance responsibilities relating to any law, ordinance, or regulation of any Federal, State, or local government body.

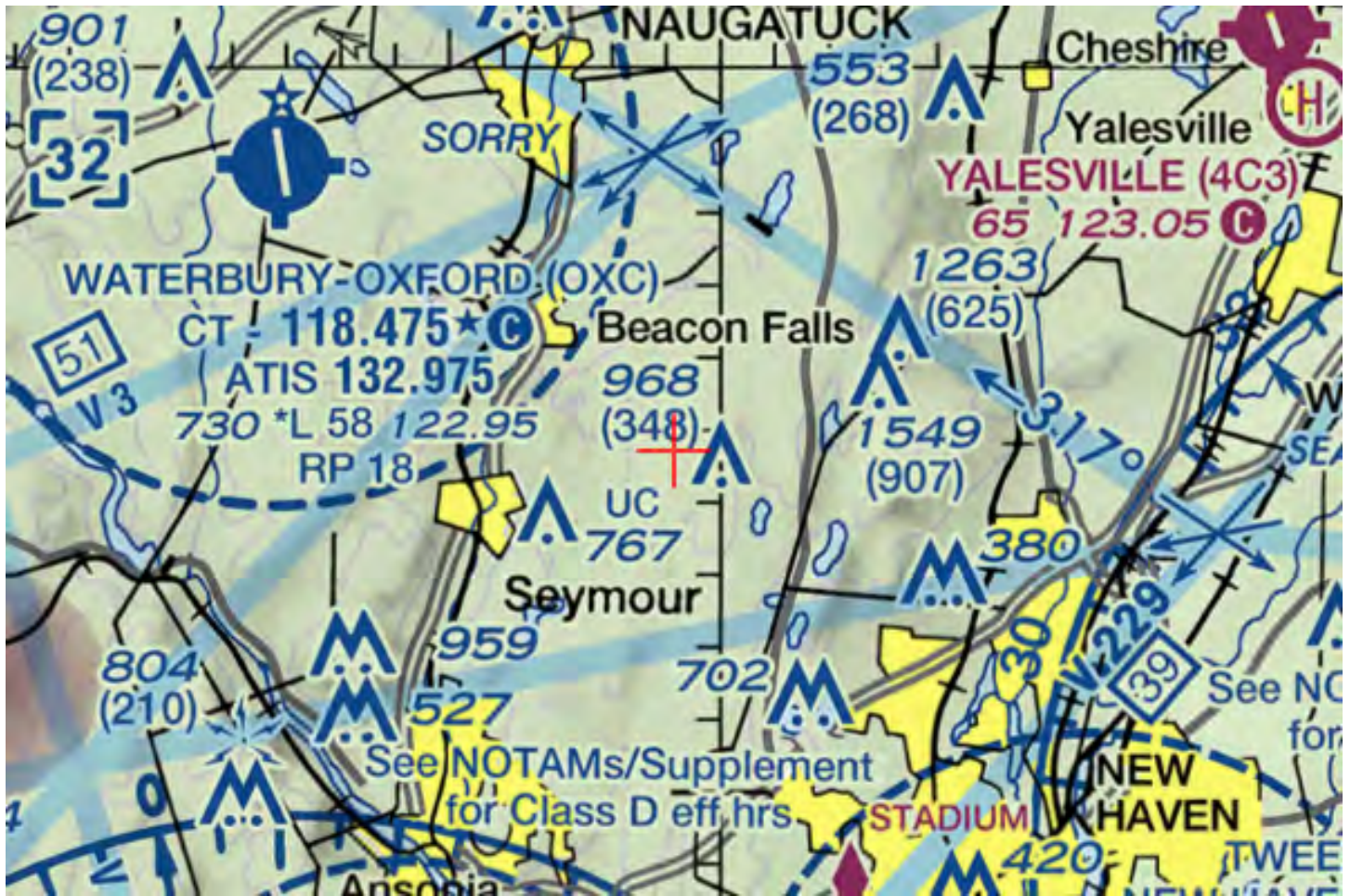
If we can be of further assistance, please contact our office at (404) 305-6430, or kelly.r.nelson@faa.gov. On any future correspondence concerning this matter, please refer to Aeronautical Study Number 2023-ANE-1236-OE.

Signature Control No: 572764420-573963115

(DNE)

Kelly Nelson
Specialist

Attachment(s)
Map(s)





Mail Processing Center
Federal Aviation Administration
Southwest Regional Office
Obstruction Evaluation Group
10101 Hillwood Parkway
Fort Worth, TX 76177

Aeronautical Study No.
2023-ANE-1237-OE

Issued Date: 02/23/2023

David H Trepeck
TRITEC Americas, LLC
888 Prospect Street, Suite 200
La Jolla, CA 92037

**** DETERMINATION OF NO HAZARD TO AIR NAVIGATION ****

The Federal Aviation Administration has conducted an aeronautical study under the provisions of 49 U.S.C., Section 44718 and if applicable Title 14 of the Code of Federal Regulations, part 77, concerning:

Structure:	Solar Panel Point 3
Location:	Bethany, CT
Latitude:	41-24-40.63N NAD 83
Longitude:	73-00-58.14W
Heights:	608 feet site elevation (SE) 10 feet above ground level (AGL) 618 feet above mean sea level (AMSL)

This aeronautical study revealed that the structure does not exceed obstruction standards and would not be a hazard to air navigation provided the following condition(s), if any, is(are) met:

Based on this evaluation, marking and lighting are not necessary for aviation safety. However, if marking/lighting are accomplished on a voluntary basis, we recommend it be installed in accordance with FAA Advisory circular 70/7460-1 M.

This determination expires on 08/23/2024 unless:

- (a) the construction is started (not necessarily completed) and FAA Form 7460-2, Notice of Actual Construction or Alteration, is received by this office.
- (b) extended, revised, or terminated by the issuing office.
- (c) the construction is subject to the licensing authority of the Federal Communications Commission (FCC) and an application for a construction permit has been filed, as required by the FCC, within 6 months of the date of this determination. In such case, the determination expires on the date prescribed by the FCC for completion of construction, or the date the FCC denies the application.

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SIGNIFICANT AERONAUTICAL CHANGES HAVE OCCURRED, YOUR DETERMINATION MAY BE ELIGIBLE FOR ONE EXTENSION OF THE EFFECTIVE PERIOD.

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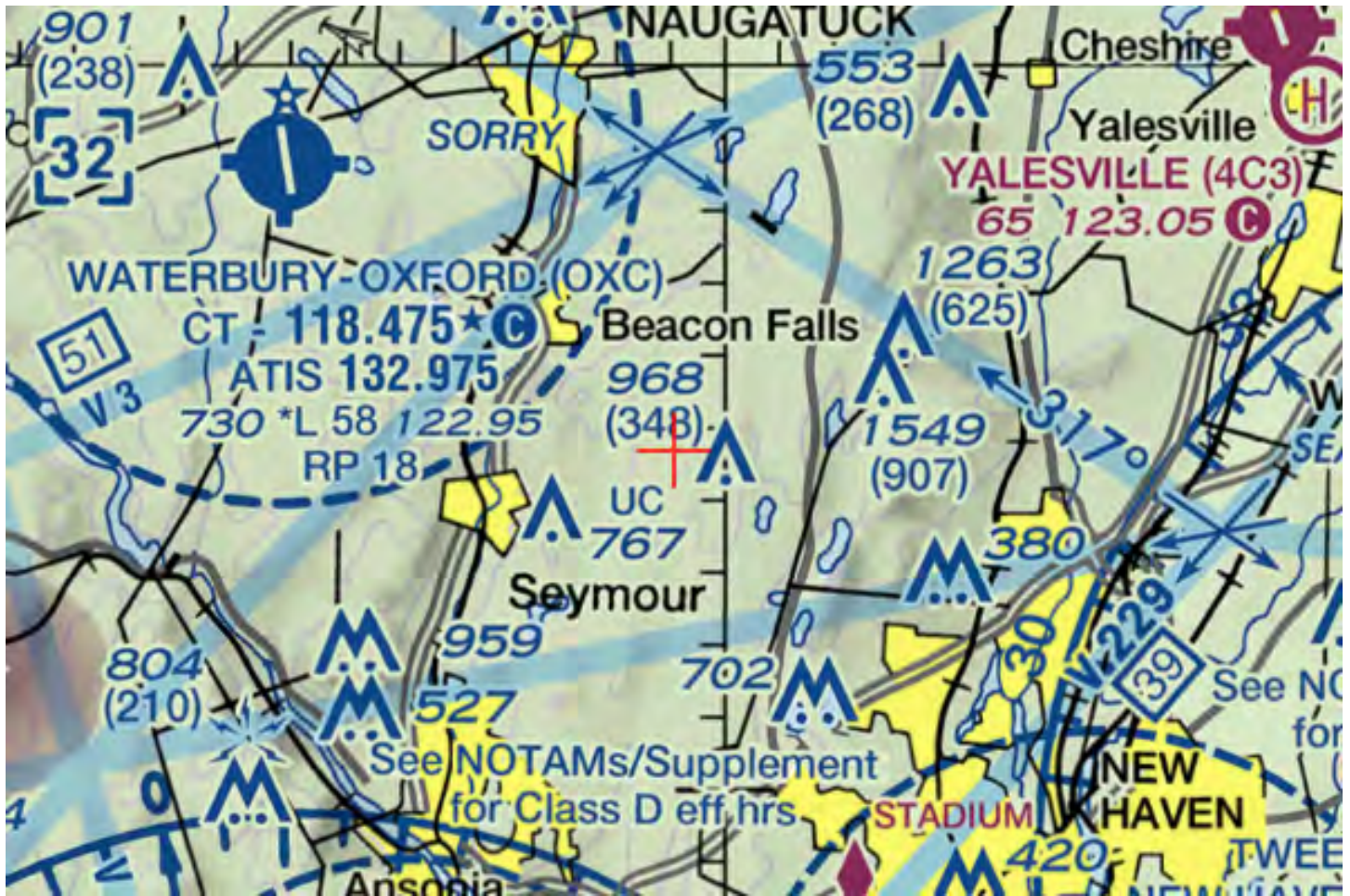
If we can be of further assistance, please contact our office at (404) 305-6430, or kelly.r.nelson@faa.gov. On any future correspondence concerning this matter, please refer to Aeronautical Study Number 2023-ANE-1237-OE.

Signature Control No: 572764421-573963114

(DNE)

Kelly Nelson
Specialist

Attachment(s)
Map(s)





Mail Processing Center
Federal Aviation Administration
Southwest Regional Office
Obstruction Evaluation Group
10101 Hillwood Parkway
Fort Worth, TX 76177

Aeronautical Study No.
2023-ANE-1238-OE

Issued Date: 02/23/2023

David H Trepeck
TRITEC Americas, LLC
888 Prospect Street, Suite 200
La Jolla, CA 92037

**** DETERMINATION OF NO HAZARD TO AIR NAVIGATION ****

The Federal Aviation Administration has conducted an aeronautical study under the provisions of 49 U.S.C., Section 44718 and if applicable Title 14 of the Code of Federal Regulations, part 77, concerning:

Structure:	Solar Panel Point 4
Location:	Bethany, CT
Latitude:	41-24-40.62N NAD 83
Longitude:	73-00-52.39W
Heights:	597 feet site elevation (SE) 10 feet above ground level (AGL) 607 feet above mean sea level (AMSL)

This aeronautical study revealed that the structure does not exceed obstruction standards and would not be a hazard to air navigation provided the following condition(s), if any, is(are) met:

Based on this evaluation, marking and lighting are not necessary for aviation safety. However, if marking/lighting are accomplished on a voluntary basis, we recommend it be installed in accordance with FAA Advisory circular 70/7460-1 M.

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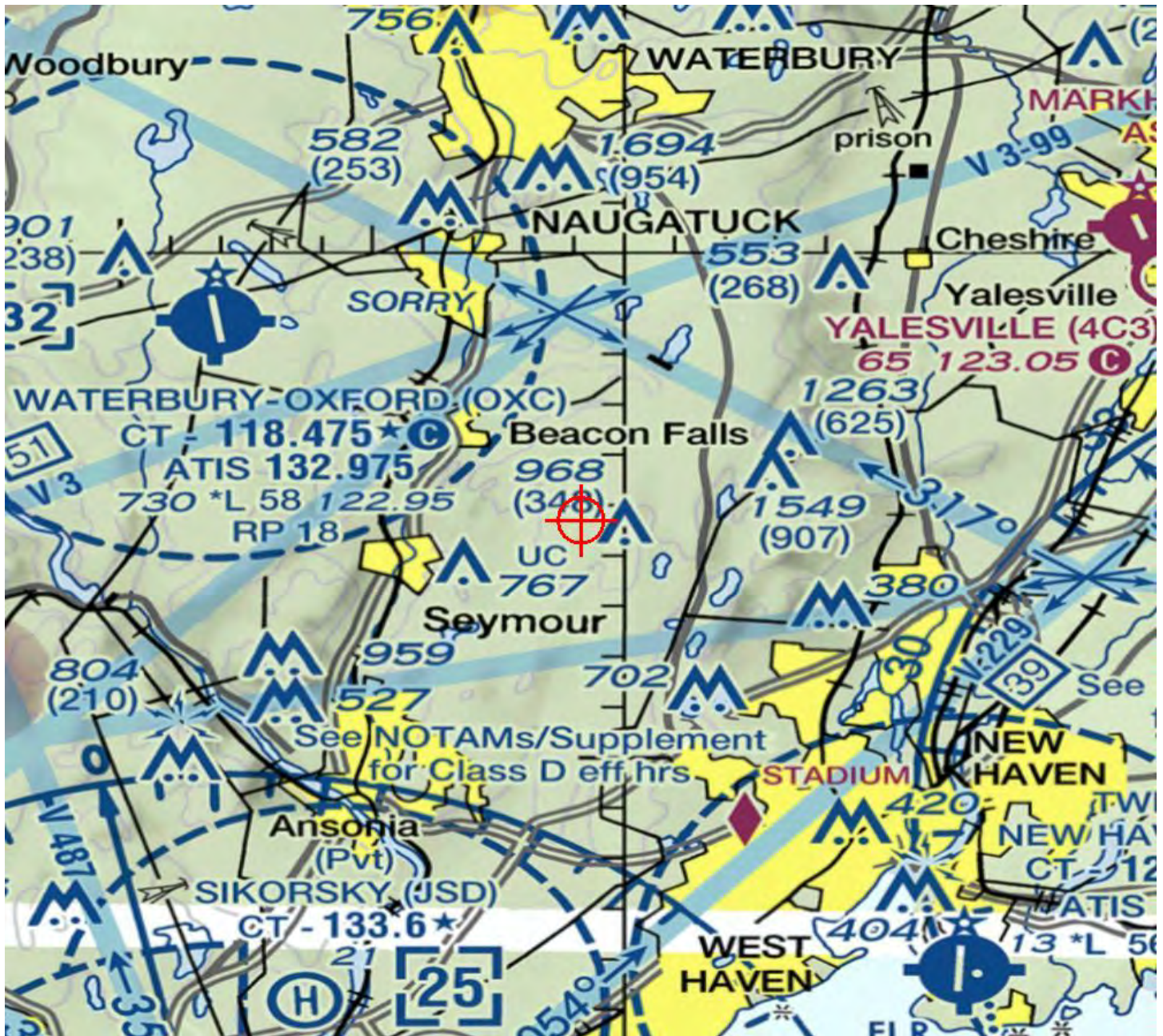
If we can be of further assistance, please contact our office at (404) 305-6430, or kelly.r.nelson@faa.gov. On any future correspondence concerning this matter, please refer to Aeronautical Study Number 2023-ANE-1238-OE.

Signature Control No: 572764424-573963116

(DNE)

Kelly Nelson
Specialist

Attachment(s)
Map(s)



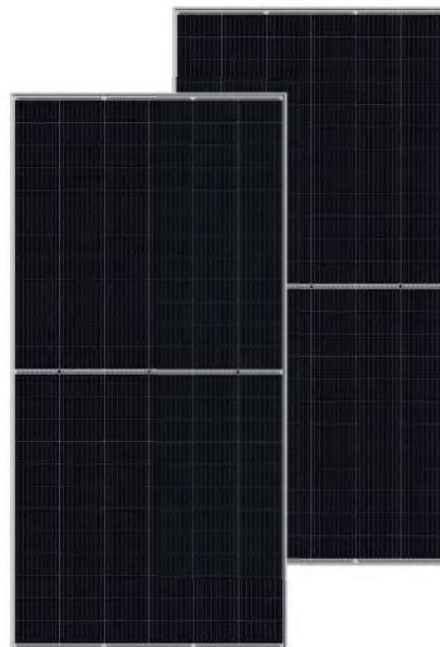
Appendix F: Product Information

BIPRO

TP6G72M
TP6G72M(H) **144 half-cell**

390 - 415W

bifacial transparent single glass
9BB half-cut mono perc



KEY FEATURES



9BB half-cut cell technology

New circuit design, lower internal current, lower Rs loss



Industry leading high yield

Bifacial PERC cell technology,
5%-25% more yield depends on different conditions



Excellent Anti-PID performance

2 times of industry standard Anti-PID test by TUV SUD



Wider application

No water-permeability and high wear-resistance,
can be widely used in high-humid, windy and dusty area



IP68 junction box

High waterproof level

SYSTEM & PRODUCT CERTIFICATES

- IEC 61215 / IEC 61730 / UL 1703
- ISO 9001: 2015 Quality Management System
- ISO 14001: 2015 Environment Management System
- ISO 45001: 2018 Occupational Health and Safety Management Systems

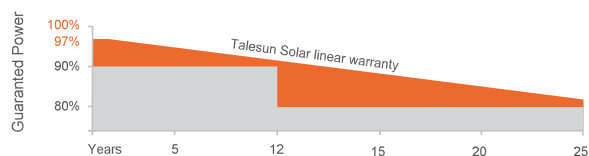


PERFORMANCE WARRANTY

12 years
Quality
insurance

25 years
Power output
guarantee

■ Talesun standard
■ Industry standard



ELECTRICAL PARAMETERS

Performance at STC (Power Tolerance 0 ~ +3%)

Maximum Power (Pmax/W)	390	395	400	405	410	415
Operating Voltage (Vmpp/V)	40.8	41.1	41.4	41.7	42.0	42.3
Operating Current (Impp/A)	9.56	9.61	9.67	9.72	9.77	9.82
Open-Circuit Voltage (Voc/V)	48.7	48.9	49.1	49.3	49.5	49.7
Short-Circuit Current (Isc/A)	10.08	10.14	10.20	10.26	10.32	10.38
Module Efficiency $\eta_m(\%)$	19.06	19.3	19.55	19.79	20.04	20.28

Performance at NMOT

Maximum Power (Pmax/W)	291.5	295.1	298.8	302.4	306.1	309.8
Operating Voltage (Vmpp/V)	38.1	38.3	38.5	38.8	39.0	39.2
Operating Current (Impp/A)	7.65	7.70	7.75	7.80	7.86	7.91
Open-Circuit Voltage (Voc/V)	45.6	45.7	45.9	46.1	46.3	46.4
Short-Circuit Current (Isc/A)	8.13	8.18	8.23	8.27	8.32	8.37

STC: Irradiance 1000W/m², Cell Temperature 25°C, Air Mass AM1.5 NMOT: Irradiance at 800W/m², Ambient Temperature 20°C, Air Mass AM1.5, Wind Speed 1m/s

Electrical characteristics with different rear side power gain (refer to 400W front)

Pmax gain	Pmax/W	Vmpp/V	Impp/A	Voc/V	Isc/A
5%	420	41.4	10.14	49.1	10.71
10%	440	41.4	10.63	49.1	11.22
15%	460	41.4	11.11	49.1	11.73
20%	480	41.4	11.59	49.1	12.24
25%	500	41.4	12.08	49.1	12.75

MECHANICAL SPECIFICATION

Cell Type	Half-cell 9 busbar
Cell Dimensions	158.75*158.75mm (6inches)
Cell Arrangement	144 (6*24)
Weight	23.5kg (51.8lbs)
Module Dimensions	2030*1008*35mm (79.72*39.68*1.38inches)
Cable Length (Portrait)	(+)300mm (11.81inches) / (-)300mm (11.81inches)
Cable Length (Landscape)	(+)1200mm (47.24inches) / (-)1200mm (47.24inches)
Cable Cross Section Size	4mm ² (0.006inches ²)
Front Glass	3.2mm High Transmission, Tempered Glass
No. of Bypass Diodes	3/6
Packing Configuration(1)	31pcs/carton, 682pcs/40hq
Packing Configuration(2)	31+3pcs/carton, 715pcs/40hq
Frame	Anodized Aluminium Alloy
Junction Box	IP68

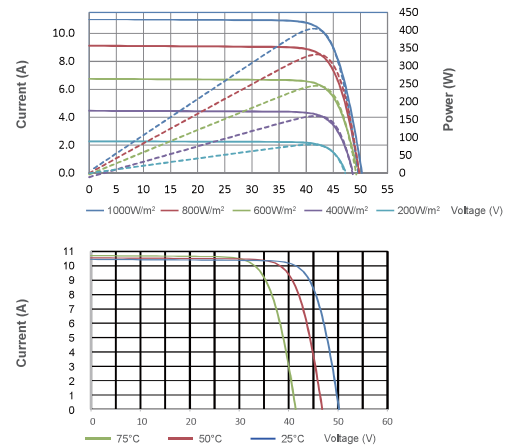
OPERATING CONDITIONS

Maximum System Voltage	1000V/1500V/DC(IEC)
Operating Temperature	-40°C ~ +85°C
Maximum Series Fuse	20A
Static Loading	5400pa
Conductivity at Ground	≤0.1Ω
Safety Class	II
Resistance	≥100MΩ
Connector	MC4 Compatible
Backside Output Ratio*	60% - 80%
*Under STC: Backside Output Ratio = $P_{\max(\text{rear})} / P_{\max(\text{front})}$	

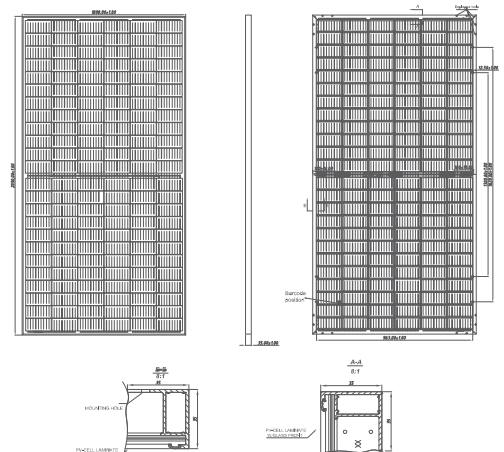
TEMPERATURE COEFFICIENT

Temperature Coefficient Pmax	-0.36%/°C
Temperature Coefficient Voc	-0.26%/°C
Temperature Coefficient Isc	+0.043%/°C
NMOT	42±2°C

I-V CURVE



TECHNICAL DRAWINGS



TDP™ 2.0 TURNKEY SOLAR TRACKER

With *BalanceTrac*

™ TDP is a trademark of Solar FlexRack

Tough, Reliable Tracker & Team of Experts at Your Service



Solar FlexRack's new TDP 2.0 Turnkey Solar Tracker with complete project support services for commercial and utility-scale solar installations introduces an advanced design featuring new *BalanceTrac*. This next-generation technology enables solar power plants to increase energy yield while significantly reducing project risks. That translates to smart installation cost-savings across your project budget.

The Only Tracker Solution with:

- Full Design
- Installation
- Commissioning Services

Increased Energy Yield

TDP 2.0 with new *BalanceTrac* is efficiently designed to support more modules per row, a rotational range of up to 110°, and is compatible with 1,000 and 1500V modules. These key features enable significant energy production gains in solar power plants.

Greater Adjustability To Maximize Performance

TDP 2.0 Tracker has up to a 10% slope tolerance that can eliminate the need to level land. Independently driven rows provide easy access for mowing, cleaning and maintenance. Autonomous tables increase design flexibility to maximize ground coverage on irregular and non-adjacent lots. Programmable granular backtracking, snow shedding and new wind damper technology mitigate inclement climatic events and reduce risk of tracker damage. All of these features compound to increase system performance.

Installations Fly with Solar FlexRack

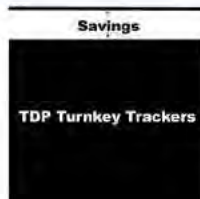
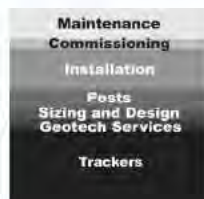
No special equipment or additional steps are required to square your racking. The proprietary design allows modules to easily slide into place, accelerating the process, and reducing installation time.

Complete Support Services Reduce Project Risks And Costs

A tracker solution that comes with all the critical associated support services and an unmatched team of experts that will significantly reduce your risks and project costs. Project management is simplified, redundancies are eliminated, and you have one highly-experienced supplier-instead of many.

Increased Yield & Reduced Costs

- More modules per row (up to 90)
- Rotational range of up to 110° (±55°)
- Optimized for 1,000 & 1,500V modules
- Lower per-unit fixed costs for balance of system savings
- Allows shorter piles
- Programmable technology to mitigate inclement climatic conditions
- installations fly with no prying, adjusting or special tools
- Built to last, the robust design reduces amount of tracker components and wear
- Autonomous tables increase design flexibility to maximize land use
- Smart backtracking reduces row shading to optimize energy production
- Independently driven rows provide easy access for mowing, cleaning and other maintenance



TDP™ 2.0 Turnkey Solar Tracker with *BalanceTrac*

TESTING

Rain, wind, sleet, snow, heat – every day and everywhere, our products are battling the elements.

We perform ongoing extensive testing in these key areas: wind tunnel, structural load, electrical bonding, and life cycle.

Solar FlexRack trackers also undergo wind tunnel testing performed by RWDI, per American Society Of Civil Engineers Standard ASCE 7.

UL COMPLIANCE

All Solar FlexRack systems have gone through UL testing.

Each component-connection point within the system conforms to NEC codes for electrically bonded and conductive systems.

Testing is performed by TUV Rheinland in accordance with UL 2703.

Certification covers both United States and Canada.

Find out more about Solar FlexRack product reliability and testing at <http://solarflexrack.com/products/testing>



Learn more about our Preferred Installer Program: <http://solarflexrack.com/resources/preferred-installer-program/>

TRACKING	
Tracking method	Single-axis horizontal, distributed drive
Backtracking	Smart backtracking - customized to terrain for maximum production
Tracking range	Up to 110° (± 55°)
Ground coverage ratio (GCR)	Configurable (0.33 to 0.50)
Tracking accuracy	2°
Stow Angle	Configurable

ARRAY CONFIGURATION	
Panels per tracker	Up to 90
Trackers per controller	1
String voltage	Up to 1,500 Volts
Panel configurations	1 in portrait (crystalline) 2 in landscape (crystalline) 4 in landscape (thin film)
Drive type	Slew 24 Volts dc

OPERATIONS & MAINTENANCE	
Scheduled maintenance	None
Warranty	10 Years: Structural and Controllers 5 Years: Drives and Electrical
Certifications	UL 2703
Dynamic load management	Limited progressive damping technology
Snow management	Programmable snow shedding

INSTALLATION & TOLERANCES	
North-south slope tolerance	Up to 10%
North-south post spacing	± 1.5 inches
East-west post alignment	± 0.625 inches
Post height	± 1 inch
Post plumb	± 1°
Post twist	± 2°
Tube twist	± 2°

CONSTRUCTION	
Structural materials	Hot dip galvanized steel
Bearings	UV-rated engineering plastic, no lubrication needed
Mechanical connections	Bolted - no welding, drilling or cutting required

CONTROL SYSTEM	
Data feed	Ethernet, Zigbee, SCADA
Power consumption	31 kWh per tracker per year

ENVIRONMENTAL	
Operating temperature	-30 °C to +60 °C
Wind	105 mph (Up to 130 mph)
Stow	35 mph
Snow load	10 psf (standard) Higher snow load available upon request



TDP 2.0 TURNKEY SOLAR TRACKER
With *BalanceTrac*

Support Services

- ✓ Geotechnical Services
- ✓ Structural Analysis
- ✓ Layout & Design
- ✓ Foundation Design Services
- ✓ Post Driving
- ✓ Pull Testing
- ✓ Tracking System Installation
- ✓ Visual Inspection of Trackers
- ✓ Preferred Installer Network
- ✓ Post, Rack & Module Installation
- ✓ Configuration of Tracker Controls
- ✓ Configuration of Network Controls
- ✓ Project Management
- ✓ PE Stamp
- ✓ Onsite Training
- ✓ Commissioning
- ✓ Remote Data Monitoring & Reporting

Over 2.0 Gigawatts of Solar FlexRack Installed

Solar FlexRack, a division of Northern States Metals, is an integrated solar company that offers custom-designed, fixed tilt ground mount and single-axis solar tracking systems in the commercial, community solar and utility-scale solar mounting industries. Solar FlexRack offers full turnkey packages including engineering, geotechnical, pullout testing, field, layout, and installation services to address the actual site conditions of an installation and provide a full scope of services from design to delivery and installation. Solar FlexRack has completed over 2 GW of solar racking installations in 40 states across America and five countries globally.

For more information on Solar FlexRack visit: www.solarflexrack.com



BIFACIAL DUAL GLASS MONOCRYSTALLINE MODULE

PRODUCT: **TSM-DEG19C.20**

PRODUCT RANGE: **525-550W**

550W+

MAXIMUM POWER OUTPUT

0~+5W

POSITIVE POWER TOLERANCE

21.0%

MAXIMUM EFFICIENCY



High customer value

- Lower LCOE (Levelized Cost Of Energy), reduced BOS (Balance of System) cost, shorter payback time
- Lowest guaranteed first year and annual degradation
- Designed for compatibility with existing mainstream system components
- High return on Investment



High power up to 550W

- Up to 21.0% module efficiency with high density interconnect technology
- Multi-busbar technology for better light trapping effect, lower series resistance and improved current collection



High reliability

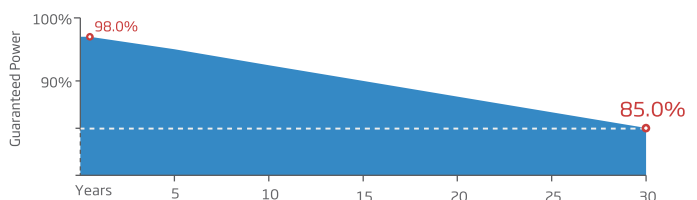
- Minimized micro-cracks with innovative non-destructive cutting technology
- Ensured PID resistance through cell process and module material control
- Resistant to harsh environments such as salt, ammonia, sand, high temperature and high humidity areas
- Mechanical performance up to 5400 Pa positive load and 2400 Pa negative load



High energy yield

- Excellent IAM (Incident Angle Modifier) and low irradiation performance, validated by 3rd party certifications
- The unique design provides optimized energy production under inter-row shading conditions
- Lower temperature coefficient (-0.34%) and operating temperature
- Up to 25% additional power gain from back side depending on albedo

Trina Solar's Vertex Bifacial Dual Glass Performance Warranty

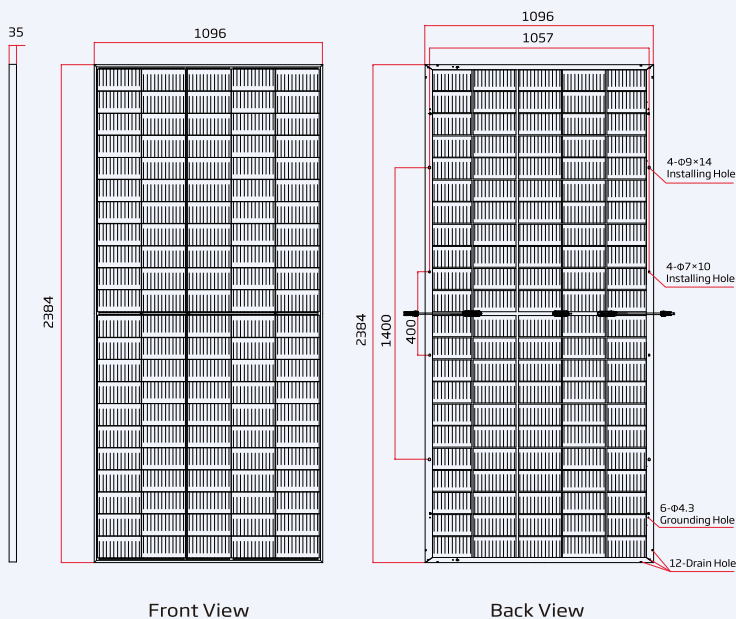


Comprehensive Products and System Certificates

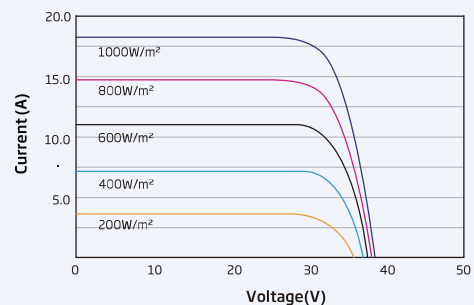


IEC61215/IEC61730/IEC61701/IEC62716/UL61730
 ISO 9001: Quality Management System
 ISO 14001: Environmental Management System
 ISO14064: Greenhouse Gases Emissions Verification
 ISO45001: Occupational Health and Safety Management System

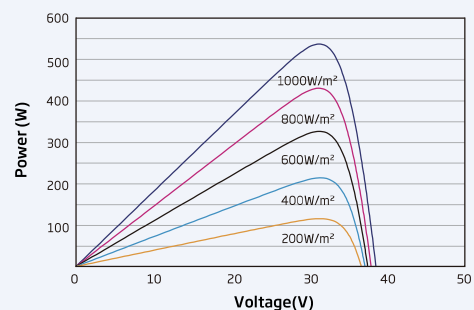
DIMENSIONS OF PV MODULE(mm)



I-V CURVES OF PV MODULE (540 W)



P-V CURVES OF PV MODULE(540 W)



ELECTRICAL DATA (STC)

Peak Power Watts-P _{MAX} (Wp)*	525	530	535	540	545	550
Power Tolerance-P _{MAX} (W)	0 ~ +5					
Maximum Power Voltage-V _{MPP} (V)	30.8	31.0	31.2	31.4	31.6	31.8
Maximum Power Current-I _{MPP} (A)	17.04	17.11	17.16	17.21	17.24	17.29
Open Circuit Voltage-V _{OC} (V)	37.1	37.3	37.5	37.7	37.9	38.1
Short Circuit Current-I _{SC} (A)	18.14	18.19	18.24	18.30	18.35	18.39
Module Efficiency η _m (%)	20.1	20.3	20.5	20.7	20.9	21.0

STC: Irradiance 1000W/m², Cell Temperature 25°C, Air Mass AM1.5. *Measuring tolerance: ±3%.

Electrical characteristics with different power bin (reference to 10% Irradiance ratio)**

Total Equivalent power -P _{MAX} (Wp)	562	567	573	578	583	589
Maximum Power Voltage-V _{MPP} (V)	30.8	31.0	31.2	31.4	31.6	31.8
Maximum Power Current-I _{MPP} (A)	18.23	18.31	18.36	18.41	18.45	18.50
Open Circuit Voltage-V _{OC} (V)	37.1	37.3	37.5	37.7	37.9	38.1
Short Circuit Current-I _{SC} (A)	19.41	19.46	19.52	19.58	19.63	19.68
Irradiance ratio (rear/front)	10%					

Power Bifaciality: 70±5%.

ELECTRICAL DATA (NOCT)

Maximum Power-P _{MAX} (Wp)	398	401	405	409	413	416
Maximum Power Voltage-V _{MPP} (V)	28.6	28.8	29.0	29.2	29.4	29.5
Maximum Power Current-I _{MPP} (A)	13.88	13.93	13.97	14.02	14.08	14.10
Open Circuit Voltage-V _{OC} (V)	35.0	35.1	35.3	35.5	35.7	35.9
Short Circuit Current-I _{SC} (A)	14.62	14.66	14.70	14.75	14.79	14.82

NOCT: Irradiance at 800W/m², Ambient Temperature 20°C, Wind Speed 1m/s.

MECHANICAL DATA

Solar Cells	Monocrystalline 210mm PERC
No. of cells	110 cells
Module Dimensions	2384×1096×35 mm (93.86×43.15×1.38 inches)
Weight	32.6 kg (71.9 lb)
Front Glass	2.0 mm (0.08 inches), High Transmission, AR Coated Heat Strengthened Glass
Encapsulant material	EVA/POE
Back Glass	2.0 mm (0.08 inches), Heat Strengthened Glass (White Grid Glass)
Frame	35mm (1.38 inches) Anodized Aluminium Alloy
J-Box	IP 68 rated
Cables	Photovoltaic Technology Cable 4,0mm² (0,006 inches²), Portrait: 280/280 mm (11.02/11.02 inches) Landscape: 1400/1400 mm (55.12/55.12 inches)
Connector	Trina TS4*/MC4 EV02

*Please specify connector on your order

TEMPERATURE RATINGS

NOCT (Nominal Operating Cell Temperature)	43°C (±2°C)
Temperature Coefficient of P _{MAX}	- 0.34%/°C
Temperature Coefficient of V _{OC}	- 0.25%/°C
Temperature Coefficient of I _{SC}	0.04%/°C

MAXIMUM RATINGS

Operational Temperature	-40~+85°C
Maximum System Voltage	1500V DC (IEC)
	1500V DC (UL)
Max Series Fuse Rating	35A

WARRANTY

12 year Product Workmanship Warranty
30 year Power Warranty
2% first year degradation
0.45% Annual Power Attenuation

(Please refer to product warranty for details)

PACKAGING CONFIGURATION

Modules per box: 31 pieces
Modules per 40' container: 527 pieces

** Back-side power gain varies depending upon the specific project albedo

SG125HV

String Inverter for 1500 Vdc System

SUNGROW

Clean power for all



HIGH YIELD

- Patented five-level topology, max. efficiency 98.9 %, European efficiency 98.7 %, CEC efficiency 98.5 %
- Full power operation without derating at 50 °C
- Patented anti-PID function

EASY O&M

- Virtual central solution, easy for O&M
- Compact design and light weight for easy installation

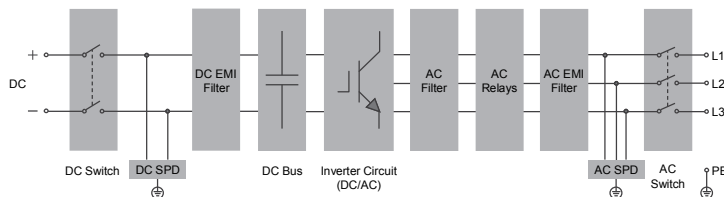
SAVED INVESTMENT

- DC 1500V, AC 600V, low system initial investment
- 1 to 5MW power block design for lower AC transformer and labor cost
- Max.DC/AC ratio up to 1.5

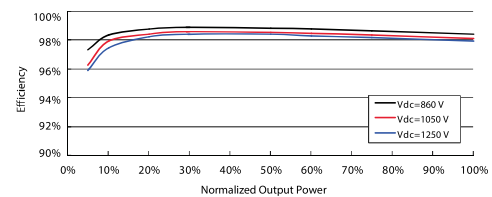
GRID SUPPORT

- Compliance with both IEC and UL safety, EMC and grid support regulations
- Low/High voltage ride through(L/HVRT)
- Active & reactive power control and power ramp rate control

CIRCUIT DIAGRAM



EFFICIENCY CURVE



Type designation	SG125HV
Input (DC)	
Max. PV input voltage	1500 V
Min. PV input voltage / Start-up input voltage	860 V / 920 V
Nominal PV input voltage	1050 V
MPP voltage range	860 – 1450 V
MPP voltage range for nominal power	860 – 1250 V
No. of independent MPP inputs	1
No. of DC inputs	1
Max. PV input current	148 A
Max. DC short-circuit current	250 A
Output (AC)	
AC output power	125 kVA @ 50 °C
Max. AC output current	120 A
Nominal AC voltage	3 / PE, 600 V
AC voltage range	480 – 690 V
Nominal grid frequency / Grid frequency range	50 Hz / 45 – 55 Hz, 60 Hz / 55 – 65 Hz
THD	< 3 % (at nominal power)
DC current injection	< 0.5 % I _n
Power factor at nominal power / Adjustable power factor	> 0.99 / 0.8 leading - 0.8 lagging
Feed-in phases / connection phases	3 / 3
Efficiency	
Max. efficiency / European efficiency	98.9% / 98.7%
CEC efficiency	98.5%
Protection	
DC reverse connection protection	Yes
AC short-circuit protection	Yes
Leakage current protection	Yes
Grid monitoring	Yes
DC switch	Yes
AC switch	Yes
Q at night function	optional
Anti-PID function	Yes
Overvoltage protection	DC Type II / AC Type II
General Data	
Dimensions (W*H*D)	670*902*296 mm 26.4"*35.5"*11.7"
Weight	76 kg 167.5 lb
Isolation method	Transformerless
Degree of protection	IP 65 NEMA 4X
Night power consumption	< 4 W
Operating ambient temperature range	-30 to 60 °C (> 50 °C derating) -22 to 140 °F (> 122 °F derating)
Allowable relative humidity range (non-condensing)	0 – 100 %
Cooling method	Smart forced air cooling
Max. operating altitude	4000 m (> 3000 m derating) 13123 ft (> 9843 ft derating)
Display / Communication	LED, Bluetooth+APP / RS485
DC connection type	OT or DT terminal (Max. 185 mm ² 350 Kcmil)
AC connection type	OT or DT terminal (Max. 185 mm ² 350 Kcmil)
Compliance	UL1741, UL1741SA, IEEE1547, IEEE1547.1, CSA C22.2 107.1-01-2001, FCC Part15 Sub-part B Class A Limits, California Rule 21, IEC 62109-1/-2, IEC 61000-6-2/-4, IEC 61727, IEC62116, BDEW, EN50549,VDE-AR-N 4110:2018, VDE-AR-N 4120:2018, UNE 206007-1:2013, P.O.12.3, UTE C15-712-1:2013, CEI 0-16:2017, IEC 61683, PEA, NTCO
Grid Support	LVRT, HVRT, ZVRT, active & reactive power regulation, PF control, soft start/stop



Appendix G: Geotechnical Report



Consulting
Engineers and
Scientists

Geotechnical Report Bethany Solar

428 Bethmour Road
Bethany, Connecticut

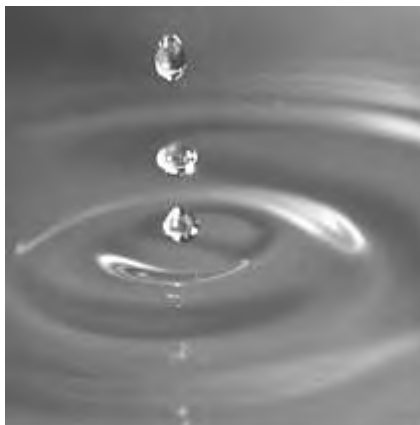
Submitted to:

BL Companies
355 Research Parkway
Meriden, CT 06450

Submitted by:

GEI Consultants, Inc.
455 Winding Brook Drive, Suite 201
Glastonbury, CT 06033
860-368-5300

July 5, 2022
Project No. 2201295



Matthew Glunt, P.E.
Senior Geotechnical Engineer

Anna M. Hernberg, P.E.
Geotechnical Engineer

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- 1 Recommended Geotechnical Design Parameters
- 2 USDA Soil Texture, NRCS Soil Group, and Infiltration Rate

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- 1 Exploration Location Plan

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- A Test Pit Logs
- B Laboratory Test Results
- C NAVFAC Load Carrying Capacity of Single Pile
- D Recommended Material Specifications

1. Introduction

1.1 Project Summary

GEI Consultants, Inc. (GEI) prepared this report to present the results of a subsurface exploration program and foundation recommendations for the proposed ground-mounted photovoltaic (PV) array in Bethany, Connecticut. On behalf of Tritec, BL Companies has engaged GEI to provide geotechnical engineering services for this project.

1.2 Scope of Services

GEI completed the following scope of services for this report. These services were performed to investigate the subsurface conditions at the Site:

- Marked out test pit locations in preparation for the public utility service mark out (Call Before You Dig).
- Conducted a subsurface exploration program consisting of six (6) test pits.
- Assigned three (3) sieve analyses with hydrometer and moisture content laboratory tests.
- Graphed the grain size distribution test results on the USDA Soil Texture Triangle, obtained the NRCS Hydrologic Soil Group, and estimated a soil infiltration rate.
- Assigned soil resistivity, pH, sulfates, and chlorides testing to one (1) composite soil sample.
- Provided soil corrosivity analysis.
- Developed recommendations for a ballast-supported PV array, should this be evaluated as an option by the design team.
- Developed soil parameters that can be used in the design of a pile-supported PV array.
- Developed frost parameters that can be used in the design of a pile-supported PV array and the solar developer's risk evaluation.
- Developed recommendations for the access roadway cross section.
- Prepared this *Geotechnical Report* presenting the results of the subsurface explorations and our recommendations.

We performed these services in general accordance with the Connecticut Building Code (Building Code), which is comprised of the 2015 International Building Code (IBC) and a separate package of state-specific amendments.

1.3 Authorization

Our work was performed in general accordance with our proposal dated February 11, 2022, and the resulting Subconsultant Agreement executed March 22, 2022.

1.4 GEI Team

The following GEI personnel performed the services for this report:

- Matthew Glunt, P.E. Project Manager / Technical Review
- Anna Hernberg, P.E. Geotechnical Engineer
- Thomas Rezzani, E.I.T. Geotechnical Professional

1.5 Vertical and Horizontal Reference

Elevations provided in this report are in feet and are referenced to the contours on the plan titled “Sketch Plan”, Sheet No. SK-7, prepared by BL Companies dated January 2022.

Test pit locations were geo-referenced at the site using a handheld GPS unit with accuracy on the order of 5 to 10 feet. These locations were overlaid onto the provided site plan and sketched on Figure 1. Test pit locations shown should be considered approximate.

2. Site and Project Description

2.1 Site Description

The site is a 21.23-acre property located at 428 Bethmour Road. The site is bound by residential properties to the north, east, and south, and Bethmour Road to the west.

The proposed development area is generally brush-covered, with thinner vegetation along previously disturbed areas near Bethmour Road, and woods at the eastern end of the property. A vacant house and associated outbuildings are located at the northeast corner of the site. Several dry-stacked stone walls cross the property.

The grade slopes from El. 625 at the northwest property corner down to El. 590 at the eastern extent of the proposed limit of disturbance. Existing wetlands are located along the east side of the property, beyond the proposed limit of disturbance.

2.2 Proposed Construction

We were provided with a copy of the preliminary Site Plan drawing (SK-7) by BL Companies. We understand an approximate 1.25 MW DC/1.0 MW AC ground-mounted solar array will be sited on the property. Based on the provided preliminary Site Plan, in addition to the PV array, the development will consist of the following:

- One concrete electrical equipment pad and one substation, both located at the northwest corner of the site.
- One stormwater management basin located to the southeast of the PV array.
- A 12-ft wide gravel road ringing the solar array.
- A small gravel parking area for maintenance personnel.
- A new permanent entrance from Bethmour Road.

We understand the preference of the solar developer is to support the array on pile foundations. Recommendations for design and construction of racking pile foundations, as well as a ballast foundation alternative, are provided in Sections 5.3 and 5.4.

We expect that most of the proposed solar array will generally follow the existing contours.

3. Exploration Procedures

3.1 Field Testing Procedures

The test pit locations were laid out within areas of interest on the site based on the provided sketch plan using a handheld GPS unit. Approximate test pit locations relative to the site plan are shown in Figure 1. The appropriate one-call utility location service (Call Before You Dig) was contacted prior to our arrival.

Six (6) test pits were excavated within or near the proposed development footprint on April 7, 2022, using an excavator to depths of 4.5 to 8.7 feet each. Several (5 of 6) test pits were terminated based on excavator refusal. The test pits were logged and photographed by GEI. Test pit logs are attached in Appendix A.

Representative samples were placed in appropriately identified sealed bags and transported to our office for laboratory assignment. Upon completion, each test pit was backfilled with excavated spoils in lifts tamped with the excavator bucket.

3.2 Laboratory Testing

Laboratory testing was conducted on representative soil samples to confirm field identification of the soils and establish engineering characteristics for design. Tests performed by GeoTesting Express, under subcontract to GEI, included the following:

- Three (3) grain-size analyses with standard sieve set and hydrometer (ASTM D6913/D7928)
- Three (3) moisture content tests (ASTM D2216)
- The following corrosion tests on one sample from test pit TP-1, composited from depths ranging from 0.7 to 4.5 feet deep:
 - pH (ASTM D4972)
 - Sulfates (ASTM D516)
 - Chlorides (ASTM D512)
 - Electrical resistivity (ASTM G57).

Results of the laboratory testing program are attached in Appendix B.

4. Subsurface Conditions

4.1 Geologic Setting

Local geologic maps identify that the referenced area is underlain by thick deposits of glacial till (DEP 2009). Glacial till deposits typically overlay the bedrock surface.

Bedrock underlying the site is mapped (Rodgers 1985) as the Beardsley Member of Harrison Gneiss, which is described as gray to dark gray, medium-grained, well-layered and lineated gneiss.

4.2 Subsurface Conditions

The generalized subsurface conditions at the site are described below, in order of increasing depth. The subsurface conditions between exploration locations may differ. The nature and extent of variations between the sampling points will not become evident until construction.

Topsoil – Topsoil in the test pits was measured at 8 to 14 inches thick. These soils were generally characterized as silty sand (SM) or sandy silt (ML) and contained roots and organic fibers. The topsoil in TP-1 contained approximately 10% gravel and small cobbles.

Silty Sand – A 1-foot-thick layer of silty sand (SM) was encountered below the topsoil layer in TP-2. The sand contained approximately 30 percent fines.

Glacial Till – Glacial till was encountered beneath the topsoil and silty sand layers to test pit termination. These soils were characterized as variable proportions of sand, silt, and gravel, and were most often classified as silty sand with gravel (SM), silty gravel with sand (GM), and widely graded sand with silt and gravel (SW-SM). The proportion of silty fines generally ranged from 15 to 35 percent. Interspersed cobbles and boulders were noted below 1.5 feet deep.

Excavator Refusal – Other than TP-5, the test pits were terminated based on excavator refusal at depths ranging from 4.5 to 8.2 feet (El. 620.5 at the northwest corner to El. 594.5 at the southwest corner). Refusal was generally most shallow at the northwest and southeast corners of the proposed development area.

Excavator refusal may have resulted from encountering very dense glacial till, weathered rock, cobbles or boulders, or the upper surface of sound bedrock. Diamond core sampling would be required to determine the character and continuity of material below the refusal of excavator.

4.3 Groundwater Conditions

Groundwater intrusion was observed in five test pits at depths of 2.3 to 3.8 feet. Groundwater intrusion was not observed in TP-4. We note that dense glacial till deposits may exhibit very slow infiltration and recharge rates. Therefore, groundwater may be present within these soils but not observed as free water within test excavations until several hours after the hole is opened. Samples in dense glacial till below groundwater may have been described as “damp” or “moist” due to the compact matrix of the stratum.

Groundwater levels are subject to seasonal and weather-related variations. Groundwater measurements made at different times and different locations may be significantly different than the measurements taken as part of this investigation.

5. Design Recommendations

5.1 Design Load Recommendations

The foundation of the ground mounted PV array should be designed to resist the forces caused by the load combinations in the Building Code for a Risk Category I structure.

We recommend that wind and snow loading from the Building Code be considered when developing foundation designs as follows:

- Wind load should be calculated in accordance with Chapter 6 of ASCE 7 with the exception of basic wind speed, which is specified in Chapter 16 of the Building Code Table 1604.11. The ultimate wind speed, V_{ult} , for Risk Category I for Bethany is 115 mph.
- Snow load should be calculated in accordance with Chapter 7 of ASCE 7 with the exception of ground snow load, which is specified in Chapter 16 of the Building Code, Table 1604.11. The ground snow load for Bethany is 30 lb/ft².

5.2 Allowable Soil Bearing Capacity

The maximum allowable bearing pressures that should be used for the design of equipment pads or PV ballast pads, should they be used, are listed below. Based on the results of this investigation, the equipment pad will likely be founded on glacial till.

Bearing Stratum	Net Allowable Bearing Pressure
Native Glacial Till or Structural Fill	2.0 tons/ft ²

The natural soils may be susceptible to frost heave. We recommend that the proposed equipment pads or other slabs or footings bear on Structural Fill that extends below the frost depth. If some seasonal movement of the equipment pads is acceptable, we recommend all organics, and the top foot of existing frost susceptible material below the slab should be removed and replaced with compacted Structural Fill. At least 18 inches of Structural Fill should be placed below the slab in all areas.

5.3 Pile-supported PV Array Recommendations

We understand that piles will likely be favored by the solar developer to support the PV array in the in-situ soils. Recommended geotechnical parameters for pile design are provided in Table 1.

Dense glacial till containing cobbles and boulders should be expected across the site. Difficulties such as shallow pile refusal on rock and misalignments due to cobble and boulder obstructions should be expected. These conditions may result in misalignments or difficulty reaching depth requirements. Capabilities of foundation products for installation in these difficult conditions will vary by manufacturer, some of which may have proprietary solutions for working in this type of environment. We recommend forwarding the results of this investigation to pile suppliers/designers, who will have a better understanding of the capabilities and limitations of their specific foundation products, as well as potential mitigation options.

Potential pile-support systems include but are not limited to ground screw piles and driven piles. Ground screws have been advertised as a cost-effective solution to rocky soil environments. We understand that pilot holes for the ground screws can be drilled through boulders or into bedrock.

For lateral pile capacity calculations in soil, we recommend using the passive earth pressure coefficients, K_p , for each soil type provided in Table 1. The pile designer must also consider potential lateral pile movements. Movements of several inches may be needed to develop the lateral capacity.

For axial loading, we recommend that piles be designed using an allowable skin friction and allowable end bearing based on the NAVFAC DM 7.02 analysis procedure provided in Appendix C. Alternatively, the pile designer can opt to perform on-site load tests to estimate the allowable loads.

The soil chemical and resistivity test results in Section 5.8 are provided so that the pile designer can perform a corrosivity analysis based on the materials of the pile.

The pile designer should consider the forces caused by frost on the piles, compared to the pile tension capacity. Recommended adfreeze and frost depth consideration are discussed below.

5.4 Ballast-supported PV Array Recommendations

An alternative to the proposed pile foundation is a ballast system. Potential Ballast-Support systems include but are not limited to:

- Precast Concrete Ballast
- Cast-in-Place Concrete Ballast

If the PV array or a portion of the PV array is supported by ballast ground-mount systems, the subgrade should be proof-rolled with a 5-ton vibratory roller before placing the ballast system. Where fill is added, we recommend that Structural Fill, Ordinary Fill, or on-site soils be placed and compacted to at least 92 percent of its maximum dry density determined in accordance with ASTM D1557 (Modified Proctor).

We recommend a maximum allowable soil bearing pressure as shown in the Allowable Soil Bearing Capacity table in Section 5.2.

The details of the surface preparation for the ballast system depend on the system selected. Generally, the bearing surface for each ballast system element should be level.

The natural soils and Ordinary Fill may be susceptible to frost heave. Therefore, some movement of the ballast foundation should be expected.

5.5 Adfreeze/Freezing Conditions

Soil in contact with foundations near the ground surface can freeze to the foundation and develop a substantial adfreeze bond. If the soil in contact with the foundation is frost susceptible, heave can transmit uplift forces to the foundation. Based on the test pit and laboratory results, soils expected to be in contact with racking piles contain up to about 35 percent fines and are therefore potentially frost susceptible.

We recommend using the average value of adfreeze bond stress of 100 kPa (approximately 2,100 lb/ft²) and 65 kPa (approximately 1,300 lb/ft²) for fine-grained soils frozen to steel and concrete, respectively, as reported in the Canadian Foundation Engineering Manual 4th Edition.

5.6 Frost Depth

The Connecticut State Building Code specifies a minimum embedment of 42 inches for frost protection of foundations for buildings and structures.

5.7 Seismic Design

The 2018 edition of the Connecticut Building Code document mirrors the 2015 International Building Code, with exception of the revisions and supplemental information provided by state building officials.

Based on the criteria of Building Code Section 1613.3.2 and the conditions observed in the test pits, we recommend the use of Site Class D for seismic design. The Site Class was used

in conjunction with the seismic hazard (S_S , S_I) for this location to determine spectral design values, as follows:

Corresponding spectral response design parameters are as follows:

2018 Connecticut Building Code	
Site Class	D
Risk Category	I
Use/Occupancy Group	U
S_S	0.189 g
S_I	0.063 g
S_{DS}	0.202 g
S_{D1}	0.101 g
PGA_M	0.147 g
Seismic Design Category	B

We calculated the spectral response parameters for the Site using general procedures outlined in Building Code Section 1613.3. Peak ground acceleration (PGA_M) is adjusted for Site Class effects, per ASCE 7-10 Section 11.8.3.

Soils present below the site are not judged to be susceptible to liquefaction and this does not need to be accounted for in the design.

5.8 Soil Corrosivity

Electrical resistivity is a broad indicator of soil corrosivity because corrosion reactions are electrochemical in nature and proceed most rapidly when resistivity (i.e., resistance to the flow of ions and electrical current) is low. Specifically, resistivity is a measure of how strongly a given material opposes the flow of electrical current. The composite sample collected from test pit TP-1 at depths 0.7 to 4.5 feet had an electrical resistivity reading of 113,634 Ω -cm, indicating a non-corrosive environment.

Sulfates in soil and groundwater in concentrations greater than 1,000 mg/kg are generally considered to be corrosive to structural elements. The American Concrete Institute recommends that Type II cement be used if sulfate concentrations exceed 1,000 mg/kg. Sample test results indicate sulfates concentrations of less than 10 mg/kg, which is less than 1,000 mg/kg.

Chloride concentrations above 500 mg/kg are generally considered to be corrosive to structural elements. Sample test results indicate chloride concentrations of 12 mg/kg, which is less than 1,000 mg/kg.

We summarized our evaluation of the soil corrosivity to structural elements shown in the table below by comparing the laboratory test results to some available corrosivity references.

Test	Laboratory Results	Reference	Corrosivity to Structural Elements
pH	6.7	Caltrans - Corrosion Guidelines January 2015	Not corrosive
Electrical Resistivity	113,634 Ω -cm	EPRI - Environmental Factors Governing Corrosion Rates, Report 1021854 December 2011	Not corrosive
Chlorides	12 mg/kg	Caltrans - Corrosion Guidelines January 2015	Not corrosive
Sulfates	<10 mg/kg	Caltrans - Corrosion Guidelines January 2015	Not corrosive

5.9 Estimated Infiltration Rate

As currently shown, we expect the bottom of the proposed stormwater basin will be in poorly draining dense glacial tills. We evaluated the USDA soil texture of the sample collected in this region by plotting the grain size analysis results on the USDA Soil Texture Triangle. The soil texture class for this sample is “Sandy Loam.”

We then evaluated the NRCS hydrologic soil group and infiltration rate based on the USDA soil textures. The NRCS hydrologic soil group and estimated infiltration rate for “Sandy Loam” are “B” and 1.0 inches/hour, respectively. NRCS data is summarized in Table 2.

6. Construction Considerations

6.1 Subgrade Preparation

6.1.1 General

To prepare the site for grading operations, topsoil, organic matter, existing pavements, demolished structure remnants, and other deleterious material should be stripped from the site improvement areas. Soft, wet, loose, or otherwise unsuitable soils should be removed and replaced, or potentially re-compacted in-place.

6.1.2 Demolition of Existing Structures and Utilities

All existing structures should be removed in their entirety from within the equipment pad, substation, and solar array footprints. Where existing structures fall at least 10 feet from site improvements, below grade portions of these structures may remain in place.

Existing utilities to remain in use should be rerouted around the proposed structure footprints. Remove or grout existing utilities to be abandoned prior to construction. If not removed, any pipes over 3 inches in diameter should be filled with flowable fill or grout. Otherwise, these pipes may serve as conduits for subsurface erosion resulting in formation of voids below structures. Where existing utilities are left in place and plugged within foundations, it may be necessary to undercut poorly compacted backfill to provide adequate support for foundations.

6.1.3 Equipment Pad

Excavations to final subgrade for the equipment pad should be performed in such a way that limits disturbing or loosening subgrade soils. After stripping and cutting and prior to placing pad base materials, the resulting subgrade should be firm, stable, and unyielding. Stabilization, where required, may consist of removing unsuitable material and replacement with compacted Structural Fill, or where unsuitable soils are relatively thin, drying and compacting in place.

Equipment pad soil subgrades should be proof-rolled with at least four (4) passes of a minimum 5-ton vibratory roller.

We recommend that a GEI representative observe the final preparation of all subgrades prior to equipment pad construction.

6.1.4 Access Roads

We understand that the access roads at the site will be gravel surface roads. The following roadway sections are suitable for the access roads:

- 12 inches of CTDOT M.02.03 Gravel Surface over a geotextile. Geotextile fabric for roadway underlayment should be a heavy-duty woven product, consisting of GEOTEX 200ST or an approved equivalent.

We recommend that the gravel road section be compacted with at least four (4) passes of a vibratory roller imparting an impact load of at least 10 tons. The resulting subgrade should be firm, stable, and unyielding. Water should be added to materials as needed during compaction. We note that areas of exposed soils will be highly susceptible to disturbance by moisture and equipment movements.

We recommend that the road surface be graded with a minimum cross slope of $\frac{1}{2}$ inch per foot of road width to allow water to drain. Drainage ditches should be provided along the edges of the road to direct surface water and runoff away from the road and subbase.

We recommend that a GEI representative observe the final preparation of all subgrades prior to access road construction.

6.2 Excavation

Excavations will be primarily through dense glacial tills. Cobbles, small boulders, and moderately difficult excavation should be expected within native soils, especially below 4 feet deep. We expect that excavation through soils can be accomplished with conventional earthmoving equipment.

All excavations should be sloped or shored in accordance with the local, state, and federal regulations, including Occupational Safety and Health Agency (OSHA 29 CFR Part 1926) excavation trench safety standards.

Excavation below approximately 2 to 4 feet will require dewatering in most locations. We expect that this can be accomplished using filtered sumps and pumps.

The site soils will be susceptible to moisture intrusion and softening. Therefore, surface water should be controlled during construction.

6.3 Freezing Conditions

The soils at the site are frost susceptible. Therefore, if construction is performed during freezing weather, special precautions will be required to prevent the subgrade soils from freezing. Freezing of the soil beneath the foundation during construction may result in subsequent settlement of the structure.

All subgrades should be free of frost before placement of concrete. Frost-susceptible soils that have frozen should be removed and replaced with compacted Structural Fill. The footing and the soil adjacent to the footing should be insulated until they are backfilled. Soil placed as fill should be free of frost, as should the ground on which it is placed.

If slabs-on-grade or footings are built and left exposed during the winter, precautions should be taken to prevent freezing of the underlying soil.

6.4 Backfilling and Compaction

We recommend that all final cut and fill slopes be constructed at no steeper than 2H:1V grade to allow for the planting and maintenance of grass cover. These slopes should be protected and seeded as soon as practicable after they are completed to reduce the potential for surface erosion.

Recommended specifications for gradation and compaction of backfill soils are provided in the attached recommended Material Specifications (Appendix D).

Existing native glacial till soils can likely be re-used on site as Structural Fill or Ordinary Fill, provided they do not contain oversize, organic, or otherwise deleterious material and can meet the appropriate compaction and moisture requirements. Cobbles and small boulders should be expected within these soils. We caution some of these materials will be difficult to work if allowed to become wet, and placement may be very difficult during certain times of the year.

Fill imported from off site should meet the attached gradation requirements. Fill placed within structural limits, under the access roadway, equipment pad, and substation, and behind any retaining walls should meet the compaction requirements for Structural Fill. Backfill placed in non-structural areas should meet the compaction requirements for Ordinary Fill. Proposed borrow materials that fall slightly outside of these specifications may also be suitable for use, subject to review and approval by GEI.

7. Closure

7.1 Follow-on Services

We recommend that GEI be kept on the project through the final design and construction phases for the following services:

- Review geotechnical-related contractor submittals and assist in developing responses to questions from the contractor (i.e. RFI's).
- Provide periodic site visits during construction to view subgrades and consult on geotechnical-related issues that occur.

7.2 Limitations

This report was prepared for the use of the project team, exclusively. Our recommendations are based on the project information provided to us at the time of this report and may require modification if there are any changes in the nature, design, or location of the proposed PV array. We cannot accept responsibility for designs based on our recommendations unless we are engaged to review the final plans and specifications to determine whether any changes in the project affect the validity of our recommendations, and whether our recommendations have been properly implemented in the design.

Our professional services for this project have been performed in accordance with generally accepted engineering practices. No warranty, express or implied, is made.

Tables

Table 1. Recommended Geotechnical Design Parameters

Bethany Solar

Bethany, Connecticut

Soil Material	Total Unit Weight					
	Above Water Table	Drained Friction Angle	Undrained Strength	Earth Pressure Coefficients ⁽²⁾		
	γ_t (pcf)	ϕ' (degrees)	C' (ksf)	K_o	K_a	K_p
Ordinary Fill (92% Compaction) ⁽³⁾	120	32	0	0.47	0.31	3.25
Structural Fill (95% Compaction) ⁽⁴⁾	125	35	0	0.43	0.27	3.69
Native Glacial Till	125	36	0	0.41	0.26	3.85

Notes:

1. The values of soil properties in this table are based on empirical correlations using the soil classifications, laboratory index tests, and engineering judgment.
2. K_o = Coefficient of Earth Pressure at Rest K_a = Active Earth Pressure Coefficient (Rankine) K_p = Passive Earth Pressure Coefficient (Rankine).
3. For material compacted to ~92% of Modified Proctor maximum dry density in accordance with ASTM D1557.
4. For material compacted to ~95% of Modified Proctor maximum dry density in accordance with ASTM D1557.

Table 2. USDA Soil Texture, NRCS Soil Group, and Infiltration Rate

Bethany Solar

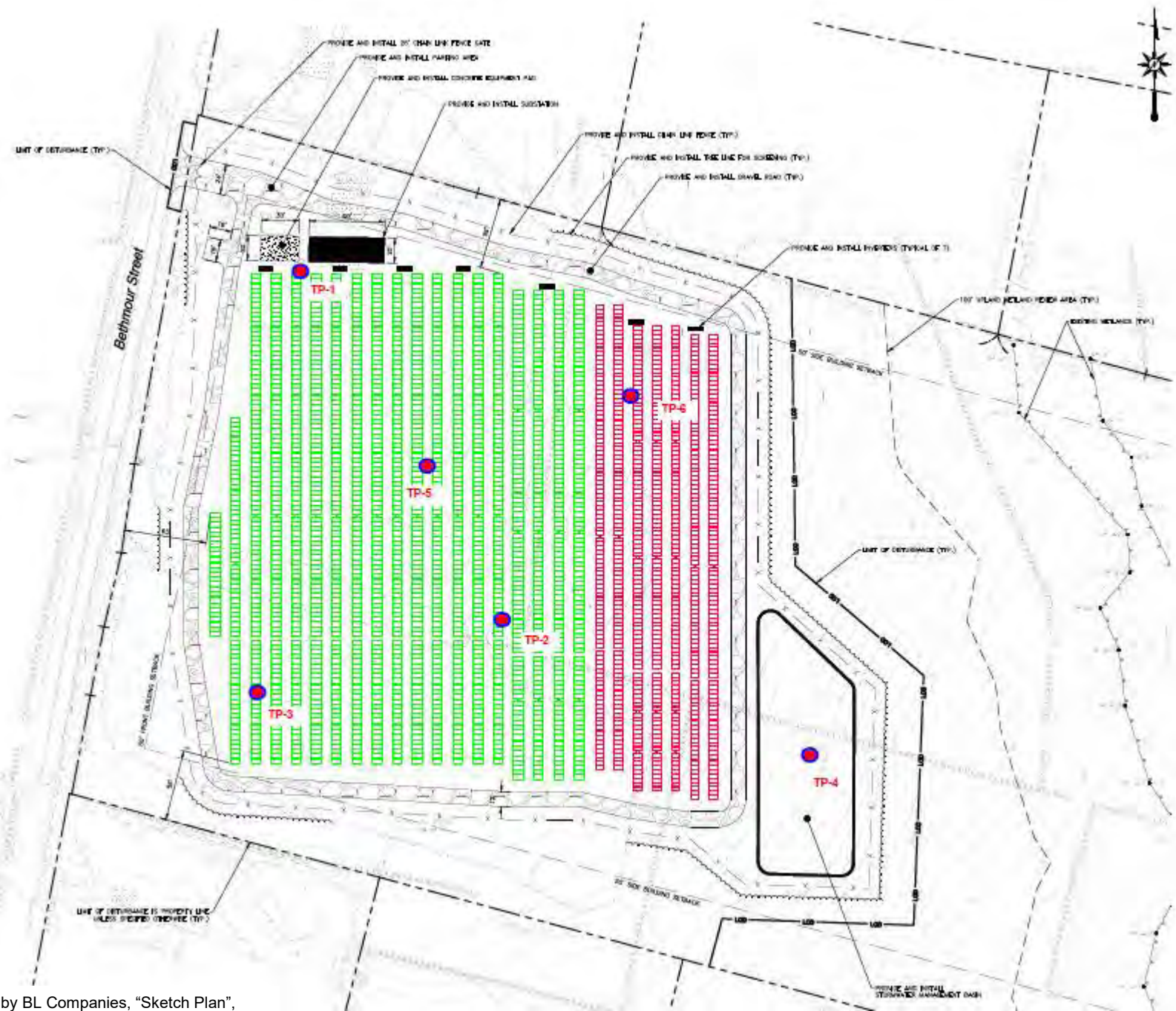
Bethany, Connecticut

Test Pit ID	Sample Depth (feet)	Percent Sand ¹	Percent Silt ¹	Percent Clay ¹	USDA Soil Texture ²	NRCS Hydrologic Soil Group ³	Infiltration Rate (inches/hour) ³
TP-3 (G4)	4.7-8.7	74.6	20.9	4.5	Loamy Sand / Sandy Loam	B	1.5
TP-4 (G3)	2-5	65.9	27.1	7.1	Sandy Loam	B	1.0
TP-6 (G2)	1-4	67.1	27.0	5.9	Sandy Loam	B	1.0


Notes:

1. USDA classification of soil particle sizes (mm): Sand: 0.05 to 2, Silt: 0.002 to 0.05, Clay: <0.002. Percentage of gravel removed from results to include only sand, silt, and clay proportions.
2. USDA soil texture is based on the soil texture triangle.
3. National Resources Conservation Service (NRCS) Hydrologic Soil Group and Infiltration Rate (referred to as Rawls rate) are based on Soil Texture Class and Table 7-1 of the NRCS Part 630 Hydrology National Engineering Handbook (2009) and Rawls et al 1982 "Estimation of Soil Water Properties."

Figures



SOURCE:
 Base map prepared by BL Companies, "Sketch Plan",
 Sheet No. SK-7, dated 1/2022

LEGEND:
 Approximate Test Pit Location

Appendix A

Test Pit Logs

GEI



GEI Consultants, Inc.
455 Winding Brook Drive
Glastonbury, CT 06033
(860) 368-5300

CLIENT: BL Companies

PROJECT: Tritec Bethany Solar

CITY/STATE: Bethany, CT

GEI PROJECT NUMBER: 2201295

TEST PIT LOG

PAGE

1

TP-1




GROUND SURFACE ELEVATION (FT):	625.0	LOCATION:	See Plan.
NORTHING: NM	EASTING: NM	TOTAL DEPTH:	4.5 FT
OBSERVED BY: Tom Rezzani		TOTAL LENGTH:	10 FT
CHECKED BY: Anna Hernberg		TOTAL WIDTH:	3.5 FT
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.:	Per SK-7 / NM
WEATHER: 40-50° F Cloudy		DATE START / END	4/7/2022


DEPTH FT.	SAMPLE TYPE & ID	SAMPLE DEPTH (FT)	SOIL DESCRIPTION
0	G-1	0 - 0.7	SILTY SAND (SM); ~70% F-C sand, ~20% NP fines, ~10% F-C gravel and cobbles up to 4", brown, moist, contains organic fibers and roots. TOPSOIL
1			
2	G-2	0.7 - 2.7	SANDY SILT (ML); ~50% NP fines, ~30% F-C sand, ~20% F-C gravel and cobbles, olive, damp, few organic fibers. GLACIAL TILL
3			Red seam of silt at 3'. East corner of Test Pit contains cobbles up to 6" at 3' deep.
4	G-3	2.7 - 4.5	WIDELY GRADED SAND WITH GRAVEL (SW); ~80% F-C sand (mostly M-C), ~20% F-C gravel and cobbles, grayish brown, wet. GLACIAL TILL
			<i>Excavator refusal at 4.5' deep. Possible bedrock</i>





Bottom of test pit at 4.5 feet. Backfilled with excavated soil placed in lifts and tamped with excavator bucket.


Note: Groundwater intrusion at 3.8 FT.





F=FINE M=MEDIUM NP= NONPLASTIC NM= NOT MEASURED
C=COARSE LP=LOW PLASTICITY MP=MEDIUM PLASTICITY

 GEI Consultants GEI Consultants, Inc. 455 Winding Brook Drive Glastonbury, CT 06033 (860) 368-5300	CLIENT: BL Companies		TEST PIT LOG	
	PROJECT: Tritec Bethany Solar		PAGE	TP-1
	CITY/STATE: Bethany, CT		2	
	GEI PROJECT NUMBER: 2201295			
GROUND SURFACE ELEVATION (FT):		625.0	LOCATION:	
NORTHING:	NM	EASTING:	NM	TOTAL DEPTH:
OBSERVED BY:	Tom Rezzani		TOTAL LENGTH:	10 FT
CHECKED BY:	Anna Hernberg		TOTAL WIDTH:	3.5 FT
EQUIPMENT:	HITACHI 135 G		DATUM VERT. / HORZ.:	Per SK-7 / NM
WEATHER:	40-50° F Cloudy		DATE START / END	4/7/2022
PHOTOGRAPHIC LOG				
<div style="display: flex; justify-content: space-around;">   </div>				
Bottom of test pit at 4.5 feet. Pictures showing soil strata at Test Pit 1				
NOTES: IN. = INCHES NM= NOT MEASURED FT. = FEET				

 <div> <div>GEI Consultants, Inc.</div> <div>455 Winding Brook Drive</div> <div>Glastonbury, CT 06033</div> <div>(860) 368-5300</div> </div>		CLIENT: BL Companies		TEST PIT LOG	
		PROJECT: Tritec Bethany Solar		PAGE	TP-2
		CITY/STATE: Bethany, CT		1	
		GEI PROJECT NUMBER: 2201295			
GROUND SURFACE ELEVATION (FT): 614.0		LOCATION: See Plan.			
NORTHING: NM EASTING: NM		TOTAL DEPTH: 8.2 FT			
OBSERVED BY: Tom Rezzani		TOTAL LENGTH: 10.5 FT			
CHECKED BY: Anna Hernberg		TOTAL WIDTH: 5.5 FT			
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.: Per SK-7 / NM			
WEATHER: 40-50° F Cloudy		DATE START / END 4/7/2022			
DEPTH FT.	SAMPLE TYPE & ID	SAMPLE DEPTH (FT)	SOIL DESCRIPTION		
0	G-1	0 - 1.0	SILTY SAND (SM); ~70% F-M sand, ~30% NP fines, brown, some roots and organic fibers, moist. TOPSOIL		
1		1.0 - 2.0	Similar to G-1, reddish brown, absent organic fibers. SILTY SAND		
2	G-3	2.0 - 6.0	SILTY GRAVEL WITH SAND (GM); ~35% F-C gravel and cobbles, ~35% NP fines, ~30% F-C sand, gray, damp to wet. GLACIAL TILL		
3					
4		6.0 - 8.2	SILTY SAND WITH GRAVEL (SM); ~65% F-C sand, ~20% NP fines, ~15% F-C gravel and cobbles, olive to brown, soil mottling, wet. Cobbles and boulders at 6.2' deep. GLACIAL TILL		
5					
6					
7					
8					
#	Excavator refusal at 8.2' deep. Possible bedrock				
Bottom of test pit at 8.2 feet. Backfilled with excavated soil placed in lifts and tamped with excavator bucket.					
Note: Groundwater intrusion at 2.3 FT.					
<div> <div>F=FINE</div> <div>M=MEDIUM</div> <div>NP= NONPLASTIC</div> <div>NM= NOT MEASURED</div> </div> <div> <div>C=COARSE</div> <div>LP=LOW PLASTICITY</div> <div>MP=MEDIUM PLASTICITY</div> </div>					

 GEI Consultants, Inc. 455 Winding Brook Drive Glastonbury, CT 06033 (860) 368-5300	CLIENT: BL Companies		TEST PIT LOG	
	PROJECT: Tritec Bethany Solar		PAGE 2	TP-2
	CITY/STATE: Bethany, CT			
	GEI PROJECT NUMBER: 2201295			
GROUND SURFACE ELEVATION (FT): 614.0		LOCATION: See Plan.		
NORTHING: NM	EASTING: NM	TOTAL DEPTH: 8.2 FT		
OBSERVED BY: Tom Rezzani		TOTAL LENGTH: 10.5 FT		
CHECKED BY: Anna Hernberg		TOTAL WIDTH: 5.5 FT		
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.: Per SK-7 / NM		
WEATHER: 40-50° F Cloudy		DATE START / END 4/7/2022		
PHOTOGRAPHIC LOG				
  				
Bottom of test pit at 8.2 feet. Pictures showing soil strata at Test Pit 2				
NOTES: IN. = INCHES NM= NOT MEASURED FT. = FEET				

 <div> GEI Consultants, Inc. 455 Winding Brook Drive Glastonbury, CT 06033 (860) 368-5300 </div>		CLIENT: BL Companies		TEST PIT LOG	
		PROJECT: Tritec Bethany Solar		PAGE 1	TP-3
		CITY/STATE: Bethany, CT			
		GEI PROJECT NUMBER: 2201295			
GROUND SURFACE ELEVATION (FT): 612.0		LOCATION: See Plan.			
NORTHING: NM	EASTING: NM	TOTAL DEPTH: 8.7 FT			
OBSERVED BY: Tom Rezzani		TOTAL LENGTH: 7 FT			
CHECKED BY: Anna Hernberg		TOTAL WIDTH: 4 FT			
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.: Per SK-7 / NM			
WEATHER: 40-50° F Cloudy		DATE START / END: 4/7/2022			
DEPTH FT.	SAMPLE TYPE & ID	SAMPLE DEPTH (FT)	SOIL DESCRIPTION		
0	G-1	0 - 0.8	SILTY SAND (SM); ~70% F-M sand, ~30% NP fines, dark brown, organic fibers, moist. TOPSOIL		
1	G-2	0.8 - 2.5	WIDELY GRADED SAND WITH SILT AND GRAVEL (SW-SM); ~65% F-C sand, ~25% F-C gravel and cobbles, ~10% NP fines, little organic fibers, moist. Increase in cobbles at 2' deep. GLACIAL TILL		
3	G-3	2.5- 4.7	SILTY GRAVEL WITH SAND (GM); ~55% F-C gravel and cobbles up to 6", ~30% F-C sand, ~15% NP fines, gray to grayish brown, moist to damp. GLACIAL TILL		
5	G-4	4.7 - 8.7	WIDELY GRADED SAND WITH GRAVEL (SW); 49.8% F-C sand, 29.7% F-C gravel and cobbles, 20.5% NP fines. Moisture content = 9.7%. GLACIAL TILL		
6			Increase in boulders and cobbles at 7' deep.		
7			Excavator refusal at 8.7' deep. Possible bedrock		
8					
Bottom of test pit at 8.7 feet. Backfilled with excavated soil placed in lifts and tamped with excavator bucket.					
Note: Groundwater intrusion at 3.7 FT.					
F=FINE M=MEDIUM NP= NONPLASTIC NM= NOT MEASURED C=COARSE LP=LOW PLASTICITY MP=MEDIUM PLASTICITY					

 GEI Consultants 455 Winding Brook Drive Glastonbury, CT 06033 (860) 368-5300	CLIENT: BL Companies		TEST PIT LOG	
	PROJECT: Tritec Bethany Solar		PAGE 2	TP-3
	CITY/STATE: Bethany, CT			
	GEI PROJECT NUMBER: 2201295			
GROUND SURFACE ELEVATION (FT): 612.0		LOCATION: See Plan.		
NORTHING: NM	EASTING: NM	TOTAL DEPTH: 8.7 FT		
OBSERVED BY: Tom Rezzani		TOTAL LENGTH: 7 FT		
CHECKED BY: Anna Hernberg		TOTAL WIDTH: 4 FT		
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.: Per SK-7 / NM		
WEATHER: 40-50° F Cloudy		DATE START / END 4/7/2022		
PHOTOGRAPHIC LOG				
<div style="display: flex; justify-content: space-around;">   </div> <div style="display: flex; justify-content: space-around; margin-top: 10px;">  </div>				
Bottom of test pit at 8.7 feet. Pictures showing soil strata at Test Pit 3				
NOTES: IN. = INCHES NM= NOT MEASURED FT. = FEET				



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CLIENT: BL Companies

PROJECT: Tritec Bethany Solar

CITY/STATE: Bethany, CT

GEI PROJECT NUMBER: 2201295

TEST PIT LOG

PAGE

1

TP-4

GROUND SURFACE ELEVATION (FT): 600.0

NORTHING: NM

EASTING: NM

LOCATION: See Plan.

TOTAL DEPTH: 5.5 FT

OBSERVED BY: Tom Rezzani

TOTAL LENGTH: 10 FT

CHECKED BY: Anna Hernberg

TOTAL WIDTH: 4.5 FT

EQUIPMENT: HITACHI 135 G

DATUM VERT. / HORZ.: Per SK-7 / NM

WEATHER: 40-50° F Cloudy

DATE START / END 4/7/2022

DEPTH FT.	SAMPLE TYPE & ID	SAMPLE DEPTH (FT)	SOIL DESCRIPTION
0	G-1	0 - 0.7	SILTY SAND (SM); ~80% F-C sand, ~20% NP fines, dark brown, moist, organic fibers. TOPSOIL
1		0.7 - 1.8	SILTY SAND WITH GRAVEL (SM); ~70% F-C sand, ~15% NP fines, ~15% F-C gravel, orange-brown, moist, little organic fibers. GLACIAL TILL
2	G-3	1.8 - 5.5	SILTY SAND (SM); 56.3% F-C sand, 32.9% NP fines, 10.8% gravel and cobbles, gray-brown, moist. Moisture content = 11.6%. GLACIAL TILL Increase in boulders and cobbles at 4.5' <i>Excavator refusal at 5.5' deep. Possible bedrock</i>
3			
4			
5			

Bottom of test pit at 5.5 feet. Backfilled with excavated soil placed in lifts and tamped with excavator bucket.

Note: No groundwater intrusion observed.

F=FINE M=MEDIUM NP= NONPLASTIC NM= NOT MEASURED
C=COARSE LP=LOW PLASTICITY MP=MEDIUM PLASTICITY



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CLIENT: BL Companies

PROJECT: Tritec Bethany Solar

CITY/STATE: Bethany, CT

GEI PROJECT NUMBER: 2201295

TEST PIT LOG

PAGE

2

TP-4

GROUND SURFACE ELEVATION (FT):	600.0	LOCATION:	See Plan.
NORTHING: NM	EASTING: NM	TOTAL DEPTH:	5.5 FT
OBSERVED BY: Tom Rezzani		TOTAL LENGTH:	10 FT
CHECKED BY: Anna Hernberg		TOTAL WIDTH:	4.5 FT
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.:	Per SK-7 / NM
WEATHER: 40-50° F Cloudy		DATE START / END	4/7/2022

PHOTOGRAPHIC LOG




Bottom of test pit at 5.5 feet.
Pictures showing soil strata at Test pit 4

NOTES:

IN. = INCHES

NM= NOT MEASURED

FT. = FEET

 <div> GEI Consultants, Inc. 455 Winding Brook Drive Glastonbury, CT 06033 (860) 368-5300 </div>		CLIENT: BL Companies		TEST PIT LOG	
		PROJECT: Tritec Bethany Solar		PAGE	TP-5
		CITY/STATE: Bethany, CT		1	
		GEI PROJECT NUMBER: 2201295			
GROUND SURFACE ELEVATION (FT): 620.5		LOCATION: See Plan.			
NORTHING: NM EASTING: NM		TOTAL DEPTH: 8.3 FT			
OBSERVED BY: Tom Rezzani		TOTAL LENGTH: 10 FT			
CHECKED BY: Anna Hernberg		TOTAL WIDTH: 5.5 FT			
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.: Per SK-7 / NM			
WEATHER: 40-50° F Cloudy		DATE START / END: 4/7/2022			
DEPTH FT.	SAMPLE TYPE & ID	SAMPLE DEPTH (FT)	SOIL DESCRIPTION		
0	G-1	0 - 1.2	SILTY SAND (SM); ~65% F-M sand, ~35% NP fines, brown, moist, organic fibers. TOPSOIL		
1					
2	G-2	1.2 - 3.2	SILTY GRAVEL WITH SAND (GM); ~65% F-C gravel and cobbles up to 12", ~20% F-C sand, ~15% NP fines, olive, damp to wet. Increase in cobbles at 2.5' deep. GLACIAL TILL		
3					
4	G-3	3.2 - 8.3	SILTY SAND WITH GRAVEL (GM); ~50% F-C sand, ~35% NP fines, ~15% F-C gravel and cobbles, brown, wet. GLACIAL TILL		
5					
6					
7					
8					
Bottom of test pit at 8.3 feet. Planned extent. Backfilled with excavated soil placed in lifts and tamped with excavator bucket.					
Note: Groundwater intrusion at 2.7 FT.					
F=FINE M=MEDIUM NP= NONPLASTIC NM= NOT MEASURED C=COARSE LP=LOW PLASTICITY MP=MEDIUM PLASTICITY					



GEI Consultants, Inc.
455 Winding Brook Drive
Glastonbury, CT 06033
(860) 368-5300

CLIENT: BL Companies

PROJECT: Tritec Bethany Solar

CITY/STATE: Bethany, CT

GEI PROJECT NUMBER: 2201295

TEST PIT LOG

PAGE

2

TP-5

GROUND SURFACE ELEVATION (FT):	620.5	LOCATION:	See Plan
NORTHING: NM	EASTING: NM	TOTAL DEPTH:	8.3 FT
OBSERVED BY: Tom Rezzani		TOTAL LENGTH:	10 FT
CHECKED BY: Anna Hernberg		TOTAL WIDTH:	5.5 FT
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.:	Per SK-7 / NM
WEATHER: 40-50° F Cloudy		DATE START / END	4/7/2022

PHOTOGRAPHIC LOG




Bottom of test pit at 8.3 feet.
Pictures showing soil strata at Test Pit 5.






NOTES:

IN. = INCHES

NM= NOT MEASURED

FT. = FEET

 <div> GEI Consultants, Inc. 455 Winding Brook Drive Glastonbury, CT 06033 (860) 368-5300 </div>		CLIENT: BL Companies		TEST PIT LOG	
		PROJECT: Tritec Bethany Solar		PAGE	TP-6
		CITY/STATE: Bethany, CT		1	
		GEI PROJECT NUMBER: 2201295			
GROUND SURFACE ELEVATION (FT): 616.0		LOCATION: See Plan.			
NORTHING: NM EASTING: NM		TOTAL DEPTH: 7.8 FT			
OBSERVED BY: Tom Rezzani		TOTAL LENGTH: 10 FT			
CHECKED BY: Anna Hernberg		TOTAL WIDTH: 4.5 FT			
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.: Per SK-7 / NM			
WEATHER: 40-50° F Cloudy		DATE START / END: 4/7/2022			
DEPTH FT.	SAMPLE TYPE & ID	SAMPLE DEPTH (FT)	SOIL DESCRIPTION		
0	G-1	0 - 1.0	SANDY SILT (ML); ~65% NP fines, ~35% F-C sand (mostly F), black, moist, interspersed roots and fibers. TOPSOIL		
1					
2	G-2	1.0 - 4.3	SILTY SAND WITH GRAVEL (SM); 48.6% F-C sand, 30.3% NP fines, 21.1% F-C gravel and cobbles, light brown to orange-brown, damp to wet. Cobbles at 1.5' deep. Increase in cobbles at 2.7' deep. Moisture content = 12.6%. GLACIAL TILL		
3					
4					
5	G-3	4.3 - 7.8	WIDELY GRADED SAND WITH SILT AND GRAVEL (SW-SM); ~45% F-C sand, ~45% F-C gravel and cobbles, ~10% NP fines, gray-brown, wet. Large Boulder observed in northeast corner at 6.5' deep. GLACIAL TILL		
6					
7					
8			Excavator refusal at 7.8' deep. Possible bedrock		
Bottom of test pit at 7.8 feet. Backfilled with excavated soil placed in lifts and tamped with excavator bucket.					
Note: Groundwater intrusion observed at 3.0 FT.					
F=FINE M=MEDIUM NP= NONPLASTIC NM= NOT MEASURED C=COARSE LP=LOW PLASTICITY MP=MEDIUM PLASTICITY					

 GEI Consultants GEI Consultants, Inc. 455 Winding Brook Drive Glastonbury, CT 06033 (860) 368-5300	CLIENT: BL Companies		TEST PIT LOG	
	PROJECT: Tritec Bethany Solar		PAGE 2	TP-6
	CITY/STATE: Bethany, CT			
	GEI PROJECT NUMBER: 2201295			
GROUND SURFACE ELEVATION (FT): 616.0		LOCATION: See Plan		
NORTHING: NM	EASTING: NM	TOTAL DEPTH: 7.8 FT		
OBSERVED BY: Tom Rezzani		TOTAL LENGTH: 10 FT		
CHECKED BY: Anna Hernberg		TOTAL WIDTH: 4.5 FT		
EQUIPMENT: HITACHI 135 G		DATUM VERT. / HORZ.: Per SK-7 / NM		
WEATHER: 40-50° F Cloudy		DATE START / END 4/7/2022		
PHOTOGRAPHIC LOG				
 				
 				
Bottom of test pit at 7.8 feet. Pictures showing soil strata at Test Pit 6				
NOTES: IN. = INCHES NM= NOT MEASURED FT. = FEET				

Appendix B

Laboratory Test Results



Client:	GEI Consultants, Inc.		
Project:	Bethany Solar		
Location:	Bethany, CT		Project No: GTX-315402
Boring ID:	---	Sample Type:	---
Sample ID:	---	Test Date:	05/11/22
Depth :	---	Test Id:	665909
		Tested By:	ckg
		Checked By:	jdt

Moisture Content of Soil and Rock - ASTM D2216

Boring ID	Sample ID	Depth	Description	Moisture Content, %
TP-3	G4	4.67-8.67'	Moist, dark brown gray silty sand with gravel	9.7
TP-4	G3	2-5'	Moist, dark brownish gray silty sand	11.6
TP-6	G2	1-4'	Moist, brown silty sand with gravel	12.6

Notes: Temperature of Drying : 110° Celsius



Client:	GEI Consultants, Inc.				
Project:	Bethany Solar				
Location:	Bethany, CT		Project No:	GTX-315402	
Boring ID:	TP-1	Sample Type:	bag	Tested By:	amp
Sample ID:	Composite-1	Test Date:	05/05/22	Checked By:	jdt
Depth :	0.7-4.5'	Test Id:	665903		
Test Comment:	---				
Visual Description:	Moist, brown silty sand with gravel				
Sample Comment:	---				

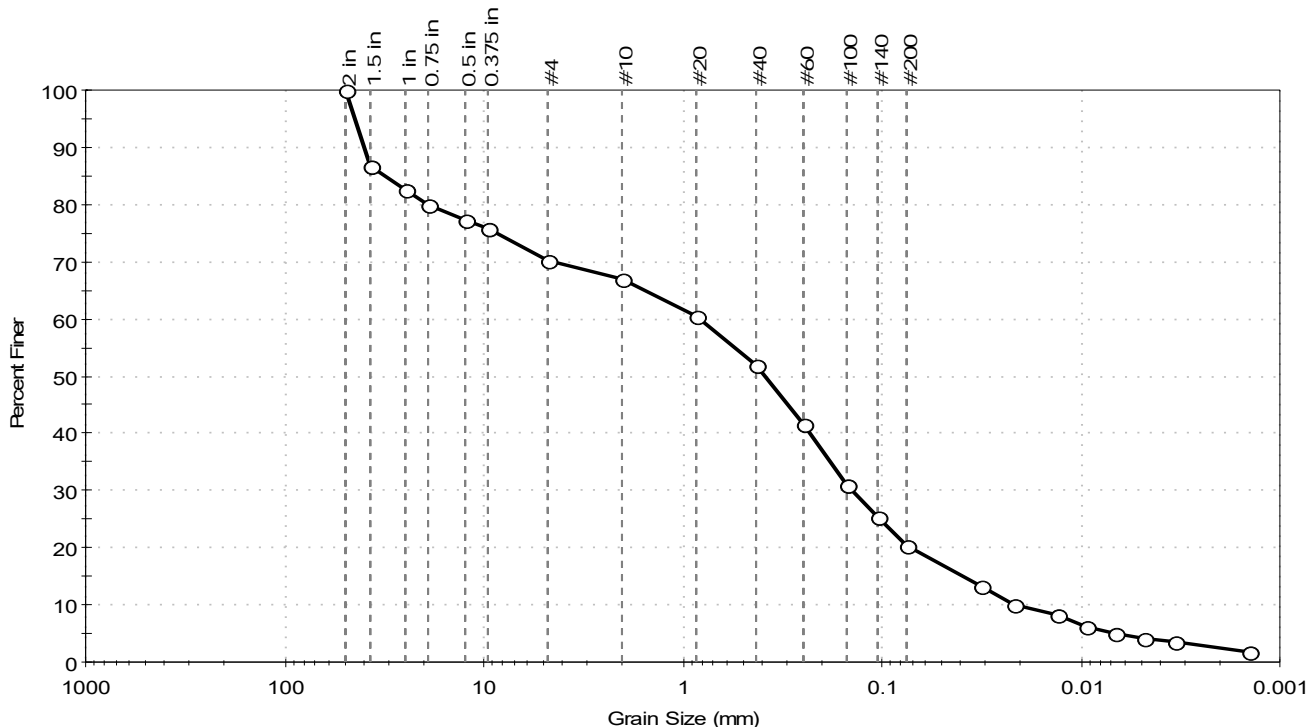
pH of Soil by ASTM D4972

Boring ID	Sample ID	Depth	Visual Description	pH of Soil in Distilled Water	pH of Soil in Calcium Chloride
TP-1	Composite-1	0.7-4.5'	Moist, brown silty sand with gravel	6.7	5.7

Notes: Sample Preparation: screened through #10 sieve
Method A, pH meter used

Client: GEI Consultants, Inc.	Project No: GTX-315402
Project: Bethany Solar	
Location: Bethany, CT	
Boring ID: TP-3	Sample Type: bag
Sample ID: G4	Test Date: 05/11/22
Depth: 4.67-8.67'	Test Id: 665905
Test Comment: ---	Tested By: ckg
Visual Description: Moist, dark brown gray silty sand with gravel	Checked By: jdt
Sample Comment: ---	

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	29.7	49.8	20.5

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
2 in	50.00	100		
1.5 in	37.50	87		
1 in	25.00	83		
0.75 in	19.00	80		
0.5 in	12.50	77		
0.375 in	9.50	76		
#4	4.75	70		
#10	2.00	67		
#20	0.85	61		
#40	0.42	52		
#60	0.25	42		
#100	0.15	31		
#140	0.11	25		
#200	0.075	20		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0320	13		
---	0.0217	10		
---	0.0131	8		
---	0.0094	6		
---	0.0067	5		
---	0.0048	4		
---	0.0034	4		
---	0.0014	2		

Coefficients

$D_{85} = 31.3644$ mm $D_{30} = 0.1419$ mm
 $D_{60} = 0.8143$ mm $D_{15} = 0.0388$ mm
 $D_{50} = 0.3855$ mm $D_{10} = 0.0216$ mm
 $C_u = 37.699$ $C_c = 1.145$

Classification

ASTM N/A

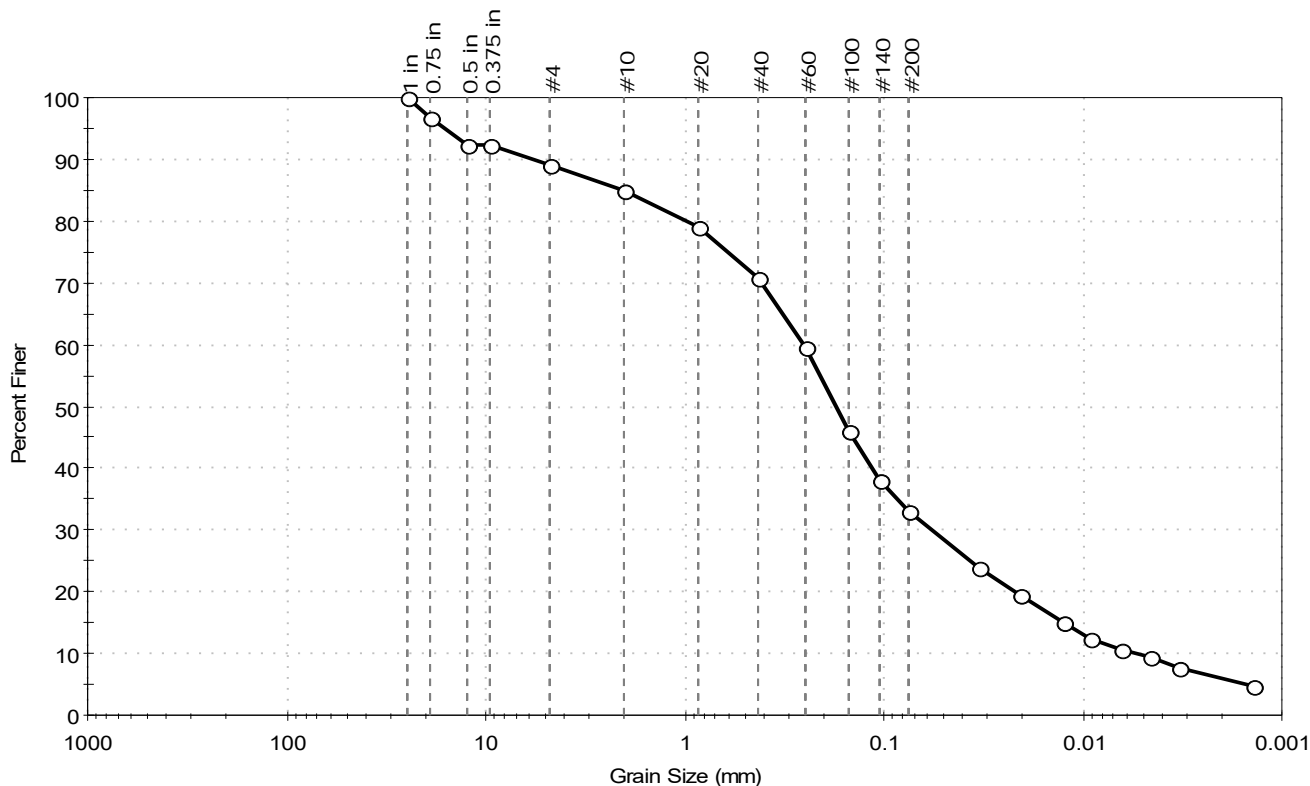
AASHTO Silty Gravel and Sand (A-2-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: GEI Consultants, Inc.	Project No: GTX-315402
Project: Bethany Solar	
Location: Bethany, CT	
Boring ID: TP-4	Sample Type: bag
Sample ID: G3	Tested By: ckg
Depth: 2-5'	Test Date: 05/11/22
	Checked By: jdt
Test Id: 665904	
Test Comment: ---	
Visual Description: Moist, dark brownish gray silty sand	
Sample Comment: ---	

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	10.8	56.3	32.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	97		
0.5 in	12.50	92		
0.375 in	9.50	92		
#4	4.75	89		
#10	2.00	85		
#20	0.85	79		
#40	0.42	71		
#60	0.25	60		
#100	0.15	46		
#140	0.11	38		
#200	0.075	33		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0333	24		
---	0.0209	20		
---	0.0126	15		
---	0.0091	12		
---	0.0065	11		
---	0.0046	9		
---	0.0033	8		
---	0.0014	5		

Coefficients

D₈₅ = 2.0146 mm D₃₀ = 0.0575 mm
 D₆₀ = 0.2549 mm D₁₅ = 0.0125 mm
 D₅₀ = 0.1749 mm D₁₀ = 0.0055 mm
 C_u = 46.345 C_c = 2.358

Classification

ASTM N/A

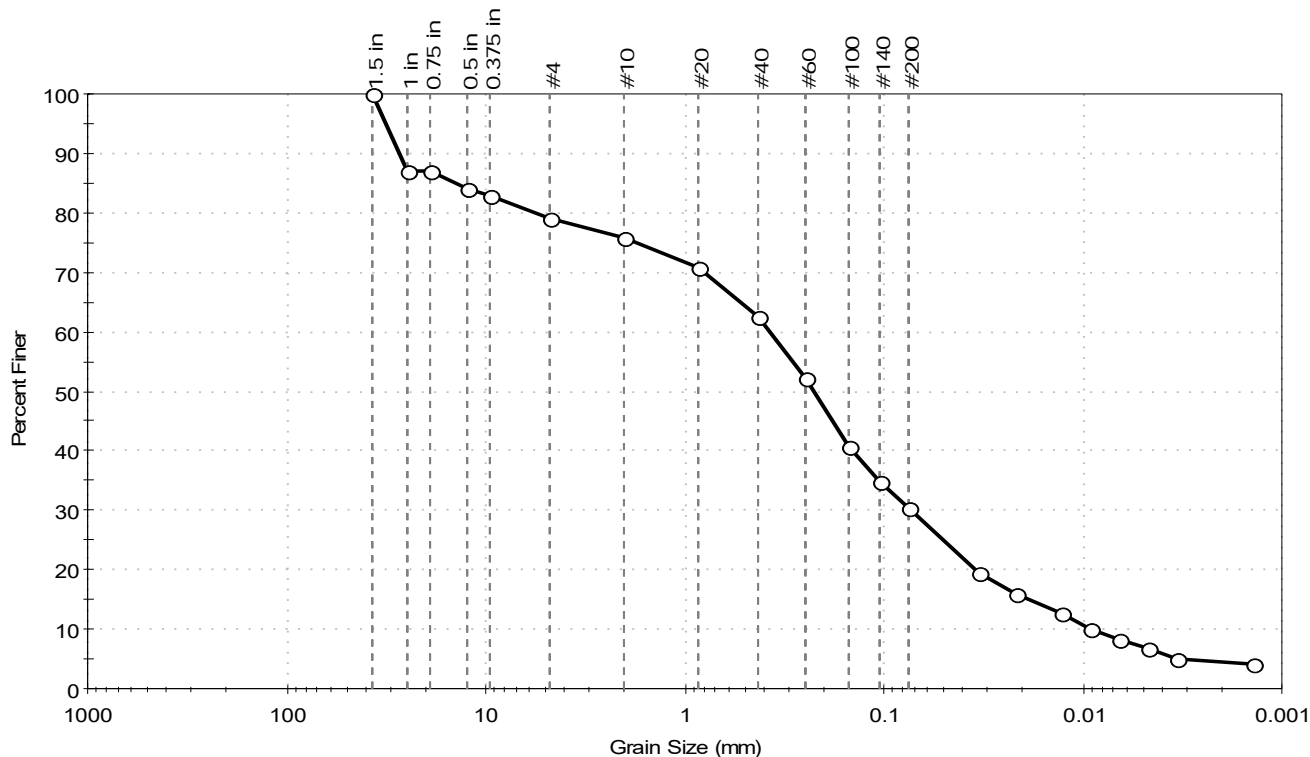
AASHTO Silty Gravel and Sand (A-2-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: Sieve

Client: GEI Consultants, Inc.	Project No: GTX-315402
Project: Bethany Solar	
Location: Bethany, CT	
Boring ID: TP-6	Sample Type: bag
Sample ID: G2	Test Date: 05/11/22
Depth: 1-4'	Test Id: 665906
Test Comment: ---	Tested By: ckg
Visual Description: Moist, brown silty sand with gravel	Checked By: jdt
Sample Comment: ---	

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	21.1	48.6	30.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1.5 in	37.50	100		
1 in	25.00	87		
0.75 in	19.00	87		
0.5 in	12.50	84		
0.375 in	9.50	83		
#4	4.75	79		
#10	2.00	76		
#20	0.85	71		
#40	0.42	63		
#60	0.25	52		
#100	0.15	41		
#140	0.11	35		
#200	0.075	30		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.034	19		
---	0.0216	16		
---	0.0128	13		
---	0.0093	10		
---	0.0066	8		
---	0.0047	7		
---	0.0034	5		
---	0.0014	4		

Coefficients

$D_{85} = 14.2744 \text{ mm}$ $D_{30} = 0.0733 \text{ mm}$
 $D_{60} = 0.3721 \text{ mm}$ $D_{15} = 0.0184 \text{ mm}$
 $D_{50} = 0.2255 \text{ mm}$ $D_{10} = 0.0092 \text{ mm}$
 $C_u = 40.446$ $C_c = 1.569$

Classification

ASTM N/A

AASHTO Silty Gravel and Sand (A-2-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR

Sand/Gravel Hardness : HARD

Dispersion Device : Apparatus A - Mech Mixer

Dispersion Period : 1 minute

Est. Specific Gravity : 2.65

Separation of Sample: #200 Sieve



Client:	GEI Consultants, Inc.
Project:	Bethany Solar
Location:	Bethany, CT
GTX#:	315402
Test Date:	05/05/22
Tested By:	amp
Checked By:	jdt

Laboratory Measurement of Soil Resistivity Using the Wenner Four-Electrode Method by ASTM G57 (Laboratory Measurement)

Boring ID	Sample ID	Depth, ft.	Sample Description	Electrical Resistivity, ohm-cm	Electrical Conductivity, (ohm-cm) ⁻¹
TP-1	Composite-1	0.7-4.5	Moist, brown silty sand with gravel	113,634	8.80E-06

Notes: Test Equipment: Nilsson Model 400 Soil Resistance Meter, MC Miller Soil Box
Water added to sample to create a thick slurry prior to testing (saturated condition).
Electrical Conductivity is calculated as inverse of Electrical Resistivity (per ASTM G57)
Test conducted in standard laboratory atmosphere: 68-73 F



GEOTESTING EPXRESS INCORPORATED
125 NAGOG PARK
ACTON MA 01720-3451
USA

Analysis No.	TS-A2210280
Report Date	09 May 2022
Date Sampled	29 April 2022
Date Received	06 May 2022
Where Sampled	Acton, MA USA
Sampled By	Client

When examined to the applicable requirements of:

ASTM D 516-16 “Standard Test Method for Sulfate Ion in Water”

ASTM D512 - Chloride Method B

NOTE: ¹Percent by weight after drying and prepared as per the Standard. *Withdrawn 2021 without Replacement

ASTM D 516 – Sulfates (Soluble)

NOTE: ¹Percent by weight after drying and prepared as per the Standard.

END OF ANALYSIS

USEPA Laboratory ID UT00930

Merrill Lee

Merrill Gee P.E. – Engineer in Charge

Page 1 of 1

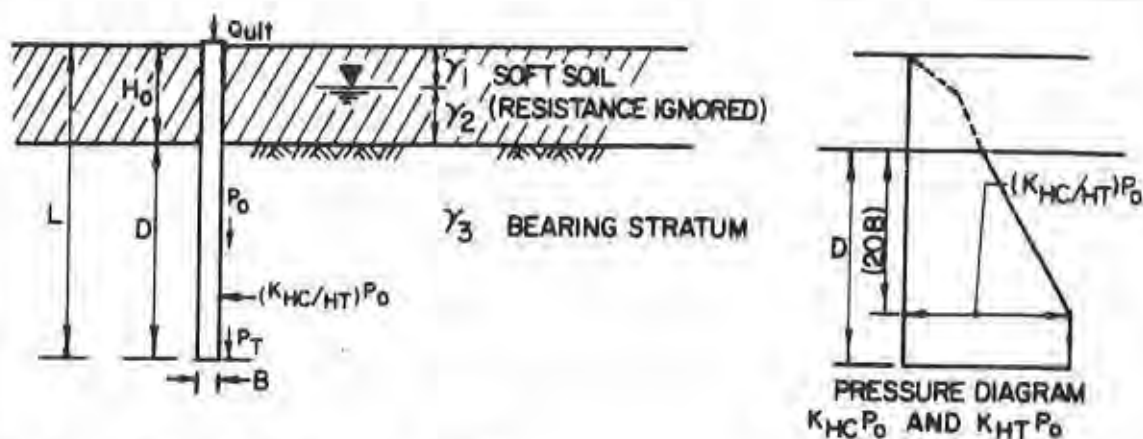
Appendix C

NAVFAC DM 7.02

Naval Facilities Engineering Command
200 Stovall Street
Alexandria, Virginia 22332-2300 APPROVED FOR PUBLIC RELEASE

Foundations &
Earth Structures

DESIGN MANUAL 7.02
REVALIDATED BY CHANGE 1 SEPTEMBER 1986



(A) ULTIMATE LOAD CAPACITY IN COMPRESSION

$$Q_{ult} = P_T N_q A_T + \sum_{H=H_0}^{H=H_0+D} (K_{HC}) P_0 (\tan \delta) (S)$$

WHERE Q_{ult} = ULTIMATE LOAD CAPACITY IN COMPRESSION

P_T = EFFECTIVE VERTICAL STRESS AT PILE TIP (SEE NOTE 1)

N_q = BEARING CAPACITY FACTOR (SEE TABLE, FIGURE 1 CONTINUED)

A_T = AREA OF PILE TIP

K_{HC} = RATIO OF HORIZONTAL TO VERTICAL EFFECTIVE STRESS ON SIDE OF ELEMENT WHEN ELEMENT IS IN COMPRESSION.

P_0 = EFFECTIVE VERTICAL STRESS OVER LENGTH OF EMBEDMENT, D (SEE NOTE 1)

δ = FRICTION ANGLE BETWEEN PILE AND SOIL (SEE TABLE, FIGURE 1 CONTINUED)

S = SURFACE AREA OF PILE PER UNIT LENGTH

FOR CALCULATING Q_{all} , USE F_S OF 2 FOR TEMPORARY LOADS, 3 FOR PERMANENT LOADS. (SEE NOTE 2)

(B) ULTIMATE LOAD CAPACITY IN TENSION

$$T_{ult} = \sum_{H=H_0}^{H=H_0+D} (K_{HT}) (P_0) (\tan \delta) (S) (H)$$

WHERE: T_{ult} = ULTIMATE LOAD CAPACITY IN TENSION, PULLOUT

K_{HT} = RATIO OF HORIZONTAL TO VERTICAL EFFECTIVE STRESS ON SIDE OF ELEMENT WHEN ELEMENT IS IN TENSION

FOR CALCULATING T_{all} , USE $F_S = 3$ ON T_{ult} PLUS THE WEIGHT OF THE PILE (W_p), THUS $T_{all} = \frac{T_{ult}}{3} + W_p$ (SEE NOTE 2)

NOTE-1: EXPERIMENTAL AND FIELD EVIDENCE INDICATE THAT BEARING PRESSURE AND SKIN FRICTION INCREASE WITH VERTICAL EFFECTIVE STRESS P_0 UP TO A LIMITING DEPTH OF EMBEDMENT, DEPENDING ON THE RELATIVE DENSITY OF THE GRANULAR SOIL AND POSITION OF THE WATER TABLE. BEYOND THIS LIMITING DEPTH ($10B \pm$ TO $40B \pm$) THERE IS VERY LITTLE INCREASE IN END BEARING, AND INCREASE IN SIDE FRICTION IS DIRECTLY PROPORTIONAL TO THE SURFACE AREA OF THE PILE. THEREFORE, IF D IS GREATER THAN $20B$, LIMIT P_0 AT THE PILE TIP TO THAT VALUE CORRESPONDING TO $D = 20B$.

NOTE-2: IF BUILDING LOADS AND SUBSURFACE CONDITION ARE WELL DOCUMENTED IN THE OPINION OF THE ENGINEER, A LESSER FACTOR OF SAFETY CAN BE USED BUT NOT LESS THAN 2.0 PROVIDED PILE CAPACITY IS VERIFIED BY LOAD TEST AND SETTLEMENTS ARE ACCEPTABLE.

FIGURE 1
Load Carrying Capacity of Single Pile in Granular Soils

BEARING CAPACITY FACTORS - N_q

ϕ^* (DEGREES)	26	28	30	31	32	33	34	35	36	37	38	39	40
N_q (DRIVEN PILE DISPLACEMENT)	10	15	21	24	29	35	42	50	62	77	86	120	145
N_q^{**} (DRILLED PIERS)	5	8	10	12	14	17	21	25	30	38	43	60	72

EARTH PRESSURE COEFFICIENTS K_{HC} AND K_{HT}

PILE TYPE	K_{HC}	K_{HT}
DRIVEN SINGLE H-PILE	0.5 - 1.0	0.3 - 0.5
DRIVEN SINGLE DISPLACEMENT PILE	1.0 - 1.5	0.6 - 1.0
DRIVEN SINGLE DISPLACEMENT TAPERED PILE	1.5 - 2.0	1.0 - 1.3
DRIVEN JETTED PILE	0.4 - 0.9	0.3 - 0.6
DRILLED PILE (LESS THAN 24" DIAMETER)	0.7	0.4

FRICTION ANGLE - δ

PILE TYPE	δ
STEEL	20°
CONCRETE	$3/4 \phi$
TIMBER	$3/4 \phi$

* LIMIT ϕ TO 28° IF JETTING IS USED

** (A) IN CASE A BAILER OR GRAB BUCKET IS USED BELOW GROUNDWATER TABLE, CALCULATE END BEARING BASED ON ϕ NOT EXCEEDING 28°.

(B) FOR PIERS GREATER THAN 24-INCH DIAMETER, SETTLEMENT RATHER THAN BEARING CAPACITY USUALLY CONTROLS THE DESIGN. FOR ESTIMATING SETTLEMENT, TAKE 50% OF THE SETTLEMENT FOR AN EQUIVALENT FOOTING RESTING ON THE SURFACE OF COMPARABLE GRANULAR SOILS. (CHAPTER 5, DM-7.1).

FIGURE 1 (continued)
Load Carrying Capacity of Single Pile in Granular Soils

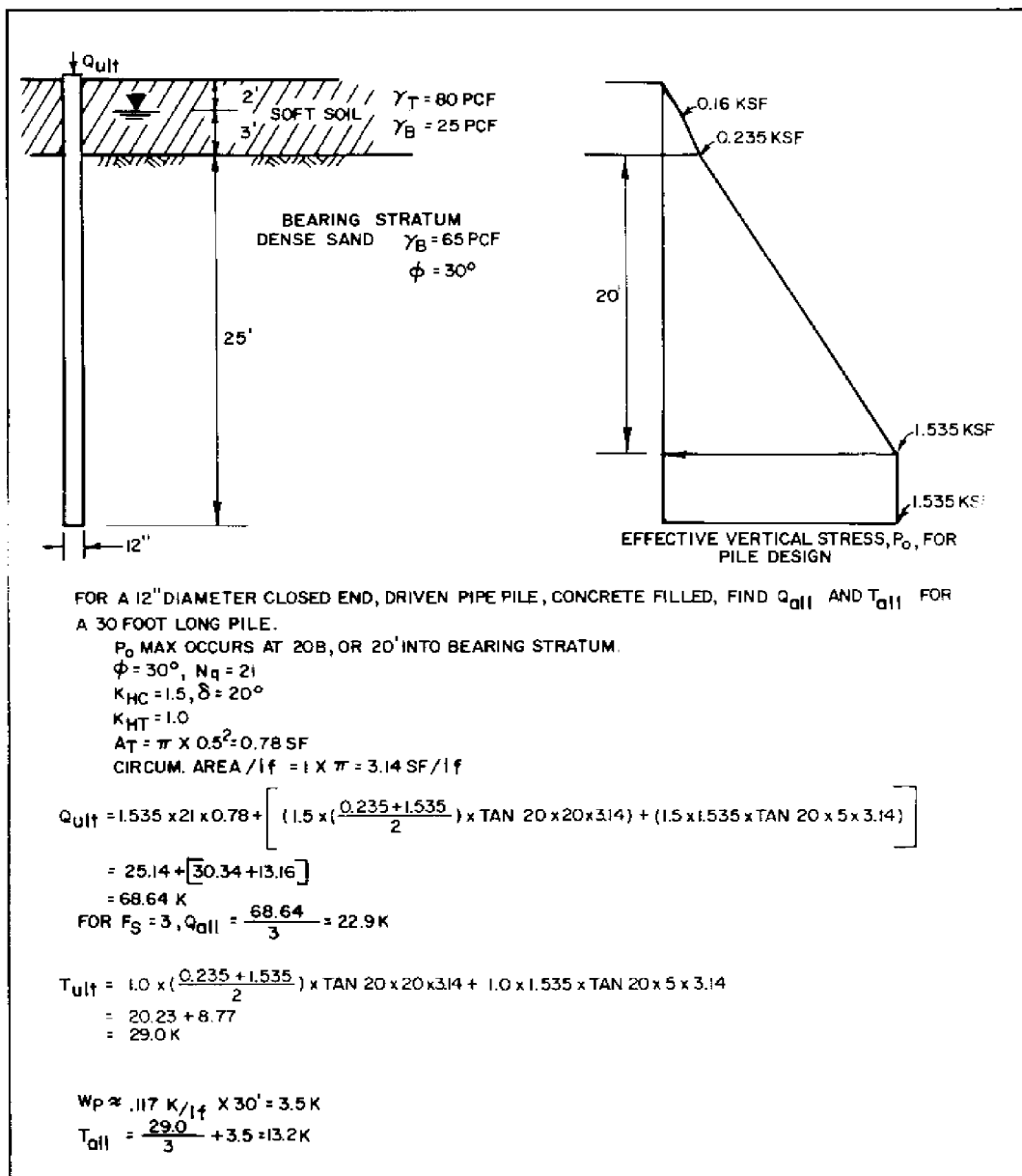
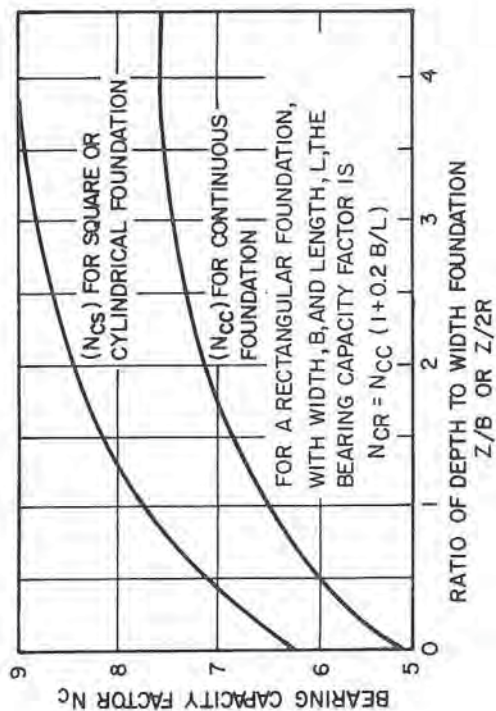
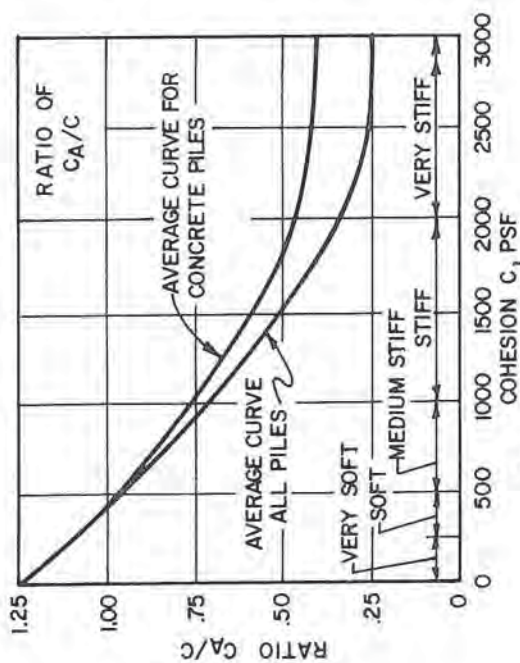


FIGURE 1 (continued)
Load Carrying Capacity of Single Pile in Granular Soils



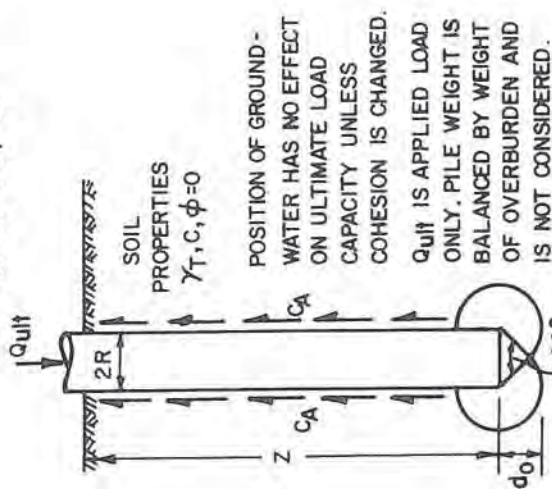
RECOMMENDED VALUES OF ADHESION

PILE TYPE	CONSISTENCY OF SOIL	COHESION, C PSF	ADHESION, C_A PSF
TIMBER AND CONCRETE	VERY SOFT	0 - 250	0 - 250
	SOFT	250 - 500	250 - 480
	MED. STIFF	500 - 1000	480 - 750
	STIFF	1000 - 2000	750 - 950
	VERY STIFF	2000 - 4000	950 - 1300
STEEL	VERY SOFT	0 - 250	0 - 250
	SOFT	250 - 500	250 - 460
	MED. STIFF	500 - 1000	460 - 700
	STIFF	1000 - 2000	700 - 720
	VERY STIFF	2000 - 4000	720 - 750

ULTIMATE LOAD CAPACITY IN TENSION

$$T_{ult} = C_A 2\pi RZ$$

T_{ult} UNDER SUSTAINED LOAD MAY BE LIMITED BY OTHER FACTORS, SEE TEXT.



ULTIMATE LOAD CAPACITY IN COMPRESSION

$$Q_{ult} = c(N_{cs}) \pi R^2 + C_A 2\pi RZ (N_{cc})$$

FIGURE 2
Ultimate Load Capacity of Single Pile or Pier in Cohesive Soils

(3) Drilled Piers. For drilled piers greater than 24 inches in diameter settlement rather than bearing capacity may control. A reduced end bearing resistance may result from entrapment of bentonite slurry if used to maintain an open excavation to the pier's tip. Bells, or enlarged bases, are usually not stable in granular soils.

(4) Piles and Drilled Piers in Cohesive Soils. See Figure 2 and Table 3. Experience demonstrates that pile driving permanently alters surface adhesion of clays having a shear strength greater than 500 psf (see Figure 2). In softer clays the remolded material consolidates with time, regaining adhesion approximately equal to original strength. Shear strength for point-bearing resistance is essentially unchanged by pile driving. For drilled piers, use Table 3 from Reference 4, Soils and Geology, Procedures for Foundation Design of Buildings and Other Structures, by the Departments of Army and Air Force, for determining side friction. Ultimate resistance to pullout cannot exceed the total resistance of reduced adhesion acting over the pile surface or the effective weight of the soil mass which is available to react against pullout. The allowable sustained pullout load usually is limited by the tendency for the pile to move upward gradually while mobilizing an adhesion less than the failure value.

Adhesion factors in Figure 2 may be very conservative for evaluating piles driven into stiff but normally consolidated clays. Available data suggests that for piles driven into normally to slightly overconsolidated clays, the side friction is about 0.25 to 0.4 times the effective overburden.

(5) Piles Penetrating Multi-layered Soil Profile. Where piles penetrate several different strata, a simple approach is to add supporting capacity of the individual layers, except where a soft layer may consolidate and relieve load or cause drag on the pile. For further guidance on bearing capacity when a pile penetrates layered soil and terminates in granular strata see Reference 5, Ultimate Bearing Capacity of Foundations on Layered Soils Under Inclined Loads, by Meyerhoff and Hanna, which considers the ultimate bearing capacity of a deep member in sand underlying a clay layer and for the case of a sand bearing stratum overlying a weak clay layer.

(6) Pile Buckling. For fully embedded piles, buckling usually is not a problem. For a fully embedded, free headed pile with length equal to or greater than $4T$, the critical load for buckling is as follows (after Reference 6, Design of Pile Foundations, by Vesic):

$$P_{crit} = 0.78 T^3 f \quad \text{for } L \geq 4T$$

where: P_{crit} = critical load for buckling

f = coefficient of variation of lateral subgrade reaction (see Figure 10)

T = relative stiffness factor (see Figure 10)

L = length of pile.

TABLE 3
Design Parameters for Side Friction for Drilled Piers in Cohesive Soils

Design Category	Side Resistance		Remarks
	C_A/C	Limit on side shear - tsf	
A. Straight-sided shafts in either homogeneous or layered soil with no soil of exceptional stiffness below the base 1. Shafts installed dry or by the slurry displacement method 2. Shafts installed with drilling mud along some portion of the hole with possible mud entrapment	0.6	2.0	(a) C_A/C may be increased to 0.6 and side shear increased to 2.0 tsf for segments drilled dry
	0.3(a)	0.5(a)	
B. Belled shafts in either homogeneous or layered clays with no soil of exceptional stiffness below the base 1. Shafts installed dry or by the slurry displacement methods 2. Shafts installed with drilling mud along some portion of the hole with possible mud entrapment	0.3	0.5	(b) C_A/C may be increased to 0.3 and side shear increased to 0.5 tsf for segments drilled dry
	0.15(b)	0.3(b)	

Appendix D

Recommended Material Specifications

Recommended Material Specifications
Bethany Solar
428 Bethmour Road
Bethany, CT

Structural Fill and Ordinary Fill shall consist of hard, durable sand and gravel, free of clay, organic matter, surface coatings, and other deleterious materials. Soil finer than the No. 200 sieve (the “fines”) should be nonplastic. On-site materials can be re-used as Structural Fill or Ordinary Fill, provided they can meet the appropriate compaction and moisture requirements indicated below and do not contain deleterious materials. Soils to be used as fill imported from off site should also meet the gradation requirements given below.

Structural Fill

Structural Fill should consist of hard, durable sand and gravel. It should be free of clay, organic matter, surface coatings, and other deleterious materials. Soil finer than the No. 200 sieve (the “fines”) should be nonplastic. Structural Fill shall meet the following gradation requirements:

Sieve Size	Percent Passing by Weight
3 inches	100
1 - ½ inch	55 – 100
No. 4	35 – 85
No. 16	20 – 65
No. 50	5 – 40
No. 200 (fines)	0 – 10

Structural Fill should be compacted in maximum 12-inch-thick, loose lifts to at least 95 percent of the maximum dry density determined in accordance with ASTM D1557 (Modified AASHTO Compaction). The moisture content should be held to within +/- 3 percent of optimum moisture content (as determined by ASTM D1557).

ATTACHMENT C

Noise Level Test Report

SG125HV Noise Level Test Report

Version	Date	Author	Approved by
V10	2017,May, 28	Bale, Yang	Chen W

1.Introduction

This document describes the noise level test for SG125HV. The test is conducted in the Sungrow Testing Center, which is a WMT testing lab (Witnessed Manufacturer's Testing) accredited by TUV, CSA and UL.

The test procedures are in accordance with the standard ISO3746 and the sound pressure level fulfills the requirements in the IEC62109-1 standard.

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2.Noise Level Test

The noise test was completed in the shielding room using the test platform shown below:

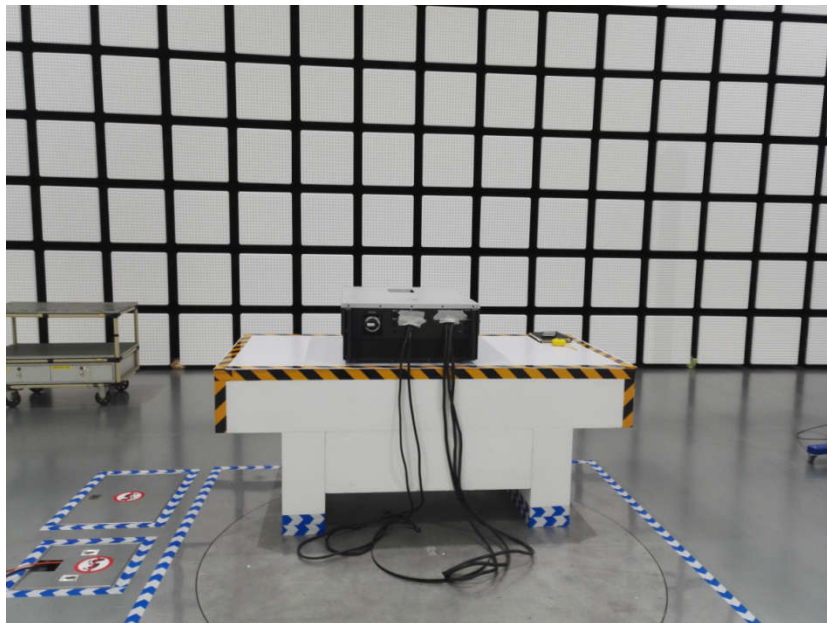


Fig-1 Noise Test Platform

During the test, the noise test instrument is located at a distance of 1m from the inverter, the inverter's operating DC voltage is 1050V and its output power is 125kW. The test data for the four directions and background noise are as follows:

Direction	Test Data
Bottom	61.6dB
Left Side	56.9dB
Top	53.7dB
Right Side	53.2dB
Background Noise	31.1dB

Appendix: Testing Pictures



Fig-2 Background Noise



Fig-3 Bottom Side



Fig-4 Left Side

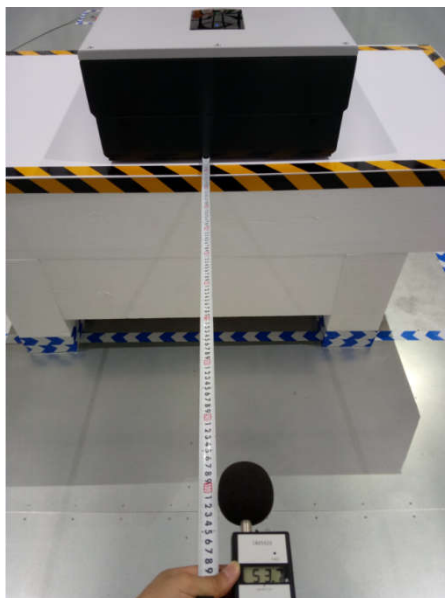


Fig-5Top Side



Fig-6Right Side

ATTACHMENT D

Remote Field Review

Remote Field Review



CT Siting Council Docket No. 1583
Response to Interrogatory #52
Proposed Solar Energy Facility
428 Bethmour Road
Bethany, Connecticut

Prepared For:
TRITEC Americas, LLC

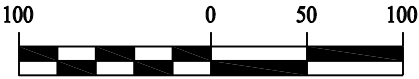
Prepared By:
Solli Engineering, LLC
501 Main Street #2A
Monroe, CT 06468





LEGEND

- PROPERTY LINE
- BUILDING SETBACK
- WETLAND LIMIT
- UPLAND REVIEW AREA - 100 FT BUFFER
- EDGE OF FARM ROAD/ACCESS DRIVE
- EDGE OF GRASS ACCESS DRIVE
- STORMWATER BASIN AREA
- STREAM LIMIT
- CHAIN LINK FENCE
- TRINA 540W SOLAR MODULES
- PROPOSED TREE
- UTILITY POLE
- OVERHEAD ELECTRIC LINE
- ELECTRIC CONDUIT
- LIMIT OF TREE CLEARING
- GRASS DRAINAGE SWALE
- PHOTO POINT LOCATION
- EXISTING STONE WALL



Rev. #:	Date	Description



SOLLI
ENGINEERING

501 Main Street, Monroe, CT 06468
T: (203) 880-5455 | F: (203) 880-9695

Drawn By:	SFU
Checked By:	KMS
Project #:	22113201
Plan Date:	09/08/23
Scale:	1" = 100'

Project:

**PROPOSED SOLAR
PHOTOVOLTAIC ARRAY**

428 BETHMOUR ROAD
BETHANY, CONNECTICUT

Sheet Title:

**REMOTE FIELD
REVIEW FIGURE**

SHEET #:

FIG.1



Photo 1: Bethmour Road looking East



Photo 2: Bethmour Road looking East





Photo 3: Bethmour Road looking East



- Proposed Concrete Pad
- Proposed Chain Link Fence
- Proposed Utility Poles
- Proposed Tree
- Proposed Gravel Road

Photo 4: Bethmour Road looking East



- Proposed Parking Area
- Proposed Gravel Road
- Proposed Utility Poles
- Proposed Chain Link Fence

Photo 5A: Looking South



Proposed Gravel Road
Proposed Chain Link
Fence

Photo 5B: Looking East



Proposed Chain Link Fence

Proposed Utility Poles

Proposed Gravel Road

Proposed Tree

Photo 6A: Looking Northwest



Proposed Chain Link Fence

Proposed Utility Poles

Proposed Gravel Road

Photo 6B: Looking North





Proposed Concrete Pad

Proposed Gravel Road

Photo 6C: Looking Northeast



Photo 7: Looking South



Photo 8: Looking East



Photo 9A: Looking South



Photo 9B: Looking East

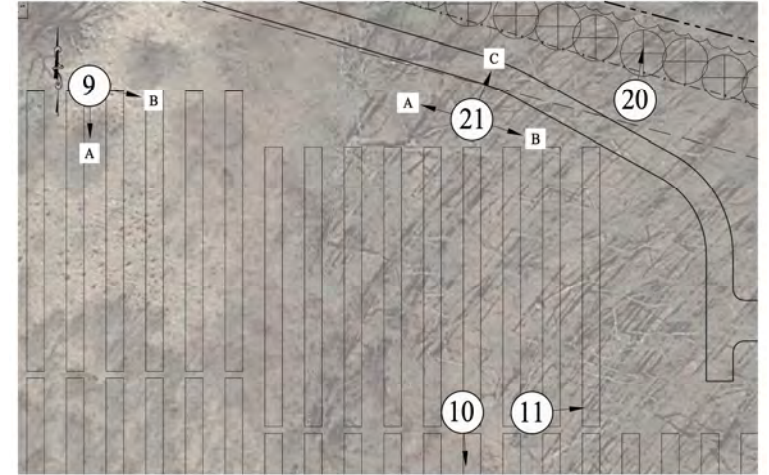
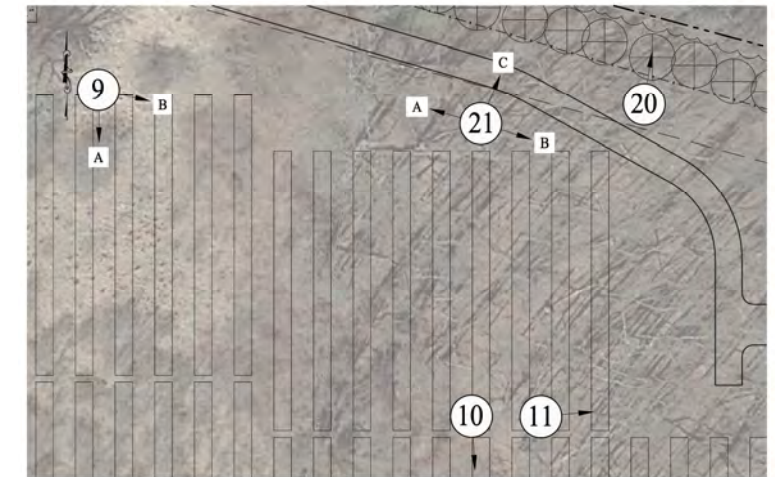
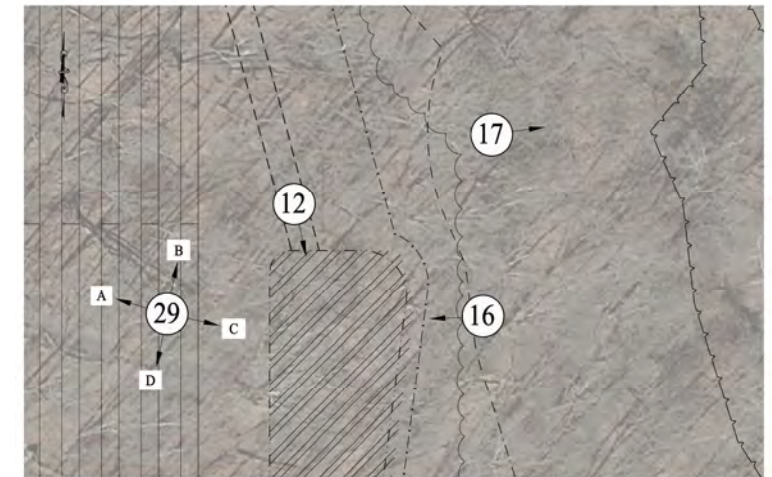


Photo 10: Looking South



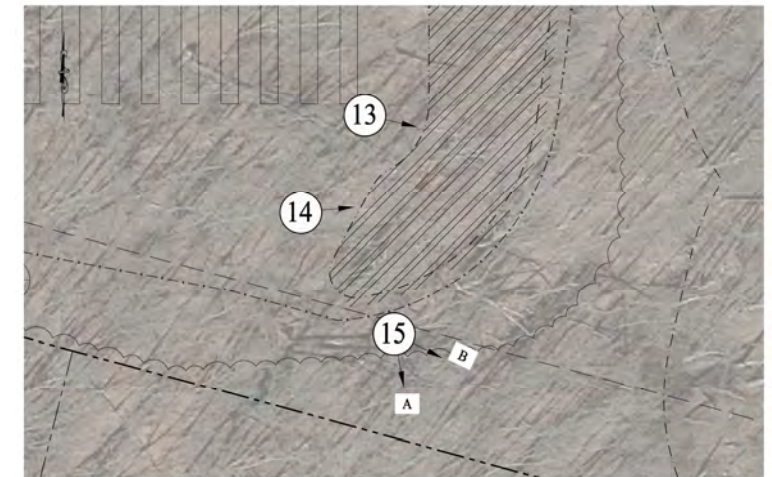
Proposed End of
Gravel Road

Photo 11: Looking East



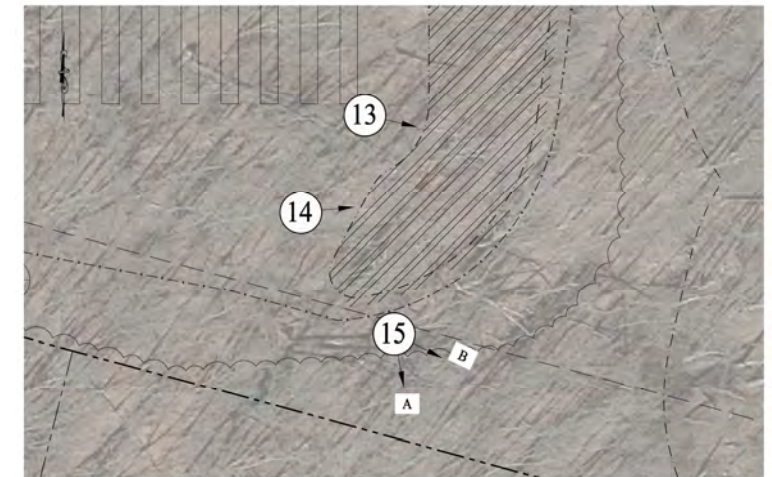
Proposed Detention
Basin

Photo 12: Looking South



Proposed Detention
Basin

Photo 13: Looking East



Proposed Detention
Basin

Photo 14: Looking East

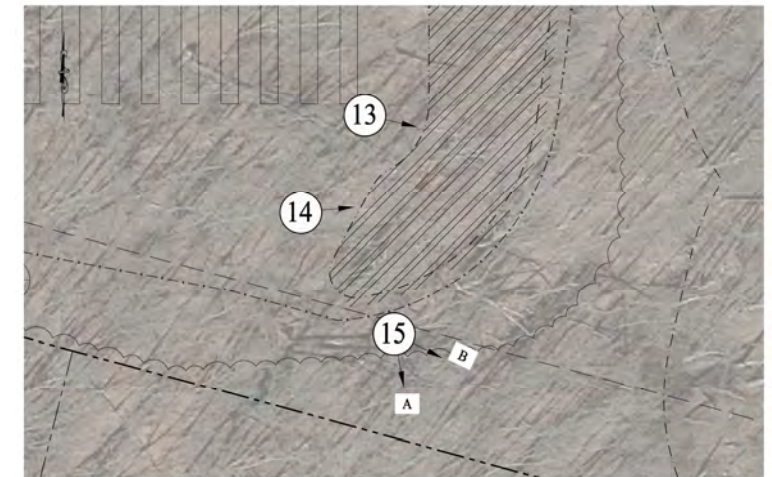


Photo 15A: Looking South towards Adjacent Properties

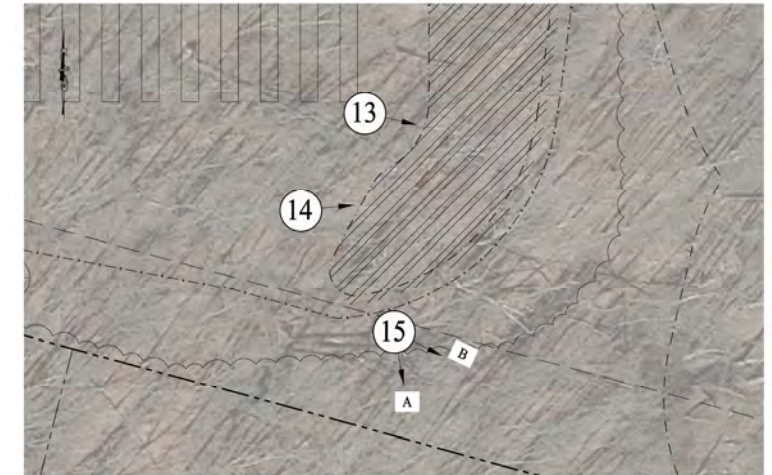
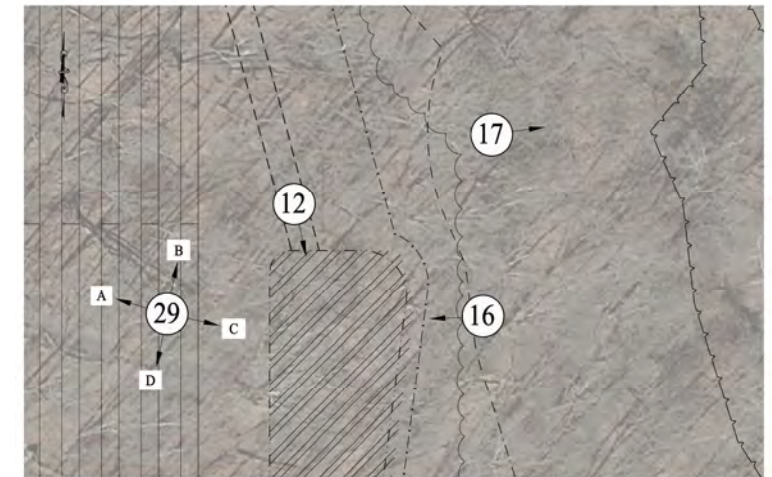


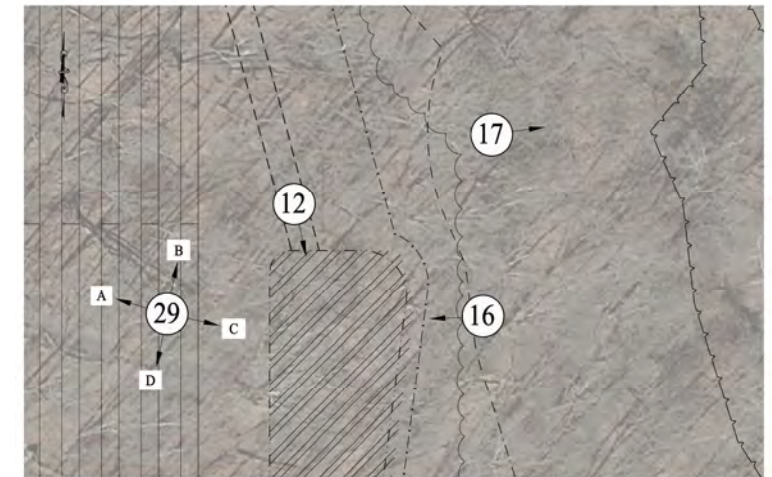
Photo 15B: Looking Southeast towards Adjacent Properties



Proposed Detention
Basin

Proposed Chain Link
Fence

Photo 16: Looking West



Existing Stone Wall

Photo 17: Looking East towards Wetlands



Photo 18: Looking Northeast towards Wetlands and Adjacent Property



Proposed Chain Link Fence

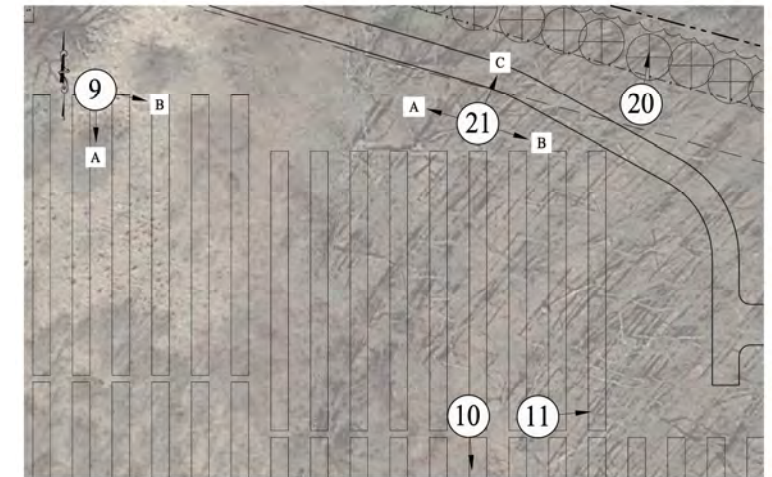
Photo 19: Looking South



Proposed Treeline

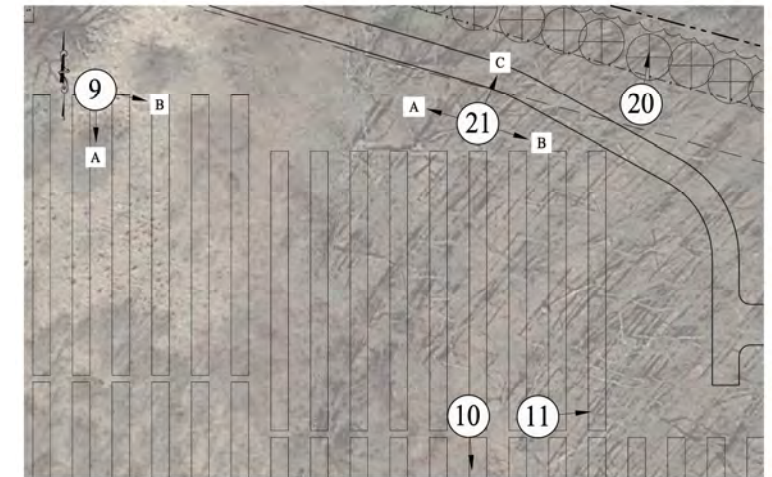
Photo 20: Looking North towards Adjacent Property





- Proposed Treeline
- Proposed Chain Link Fence
- Proposed Gravel Road
- Existing Stone Wall

Photo 21A: Looking West



Proposed Gravel Road

Photo 21B: Looking East

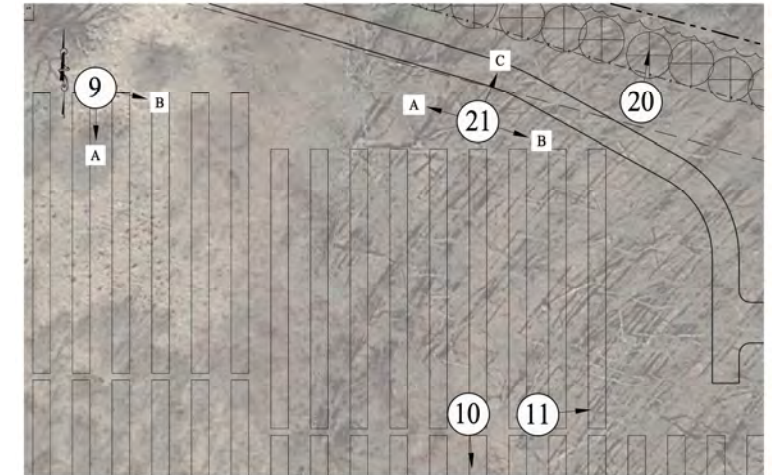


Photo 21C: Looking North towards Adjacent Properties



Proposed Concrete Pad

Photo 22: Looking West



Photo 23A: Looking South



Proposed Gravel Road

Photo 23B: Looking North



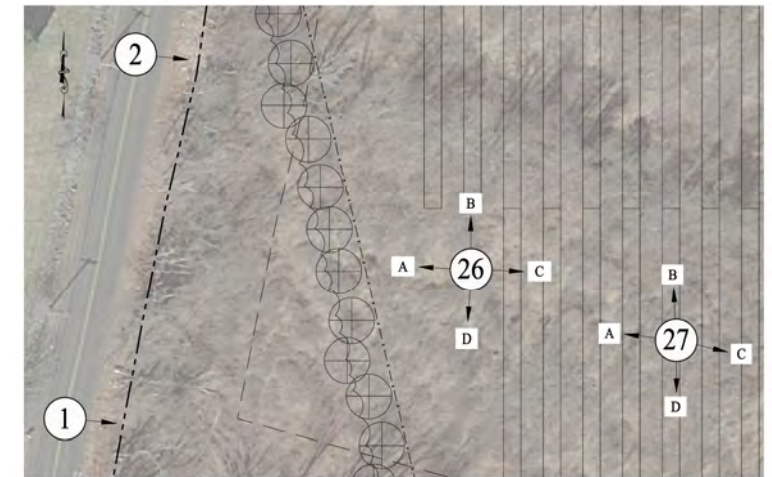
Photo 24A: Looking South



Photo 24B: Looking Northwest



Photo 25: Looking Southeast



Proposed Chain Link Fence

Existing Agrivoltaic
Features

Photo 26A: Looking West



Photo 26B: Looking North

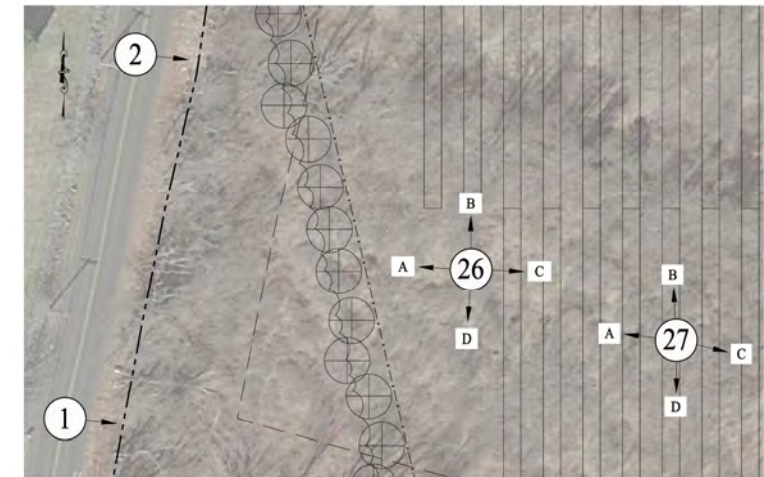
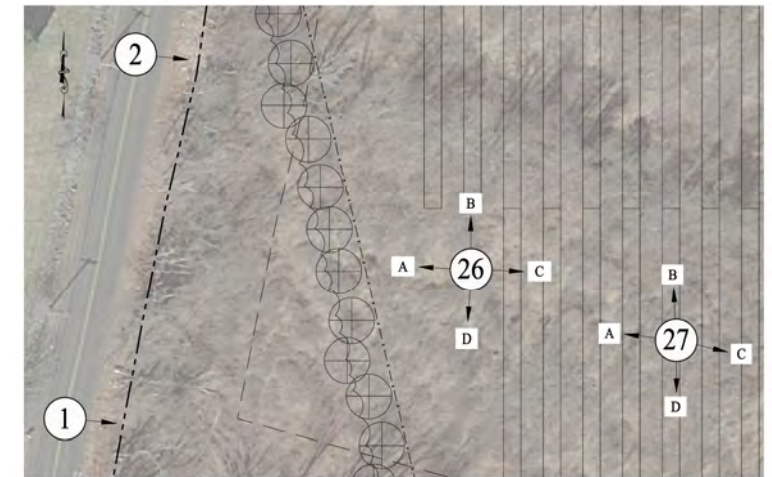


Photo 26C: Looking West



Proposed Chain Link Fence

Proposed Treeline

Photo 26D: Looking South towards Adjacent Properties



Proposed Chain Link Fence

Photo 27A: Looking West



Photo 27B: Looking North



Photo 27C: Looking West



Photo 27D: Looking South



Existing Stone Wall

Photo 28A: Looking West



Photo 28B: Looking North



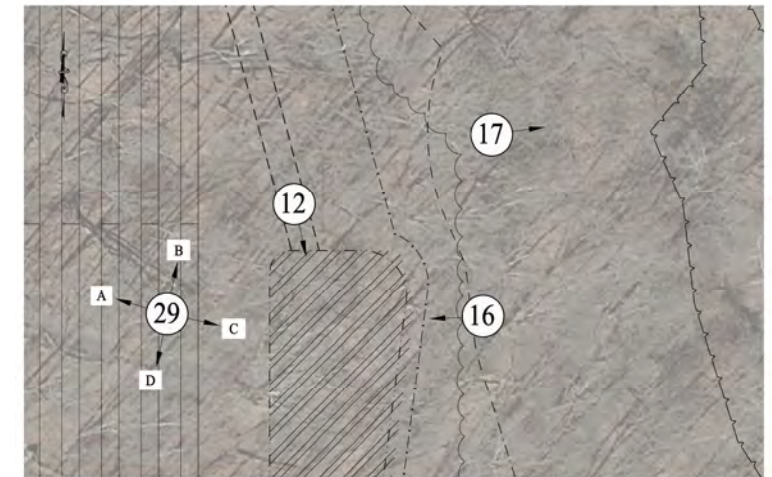
Existing Stone Wall

Photo 28C: Looking West



Existing Stone Wall

Photo 28D: Looking South



Existing Stone Wall

Photo 29A: Looking West

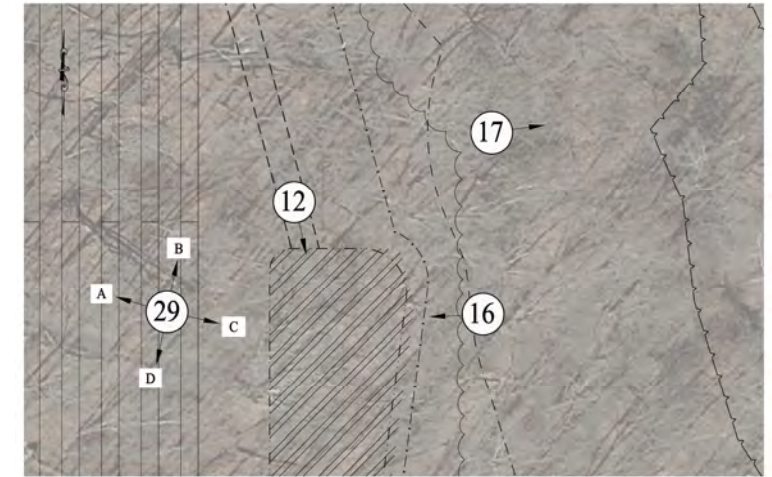
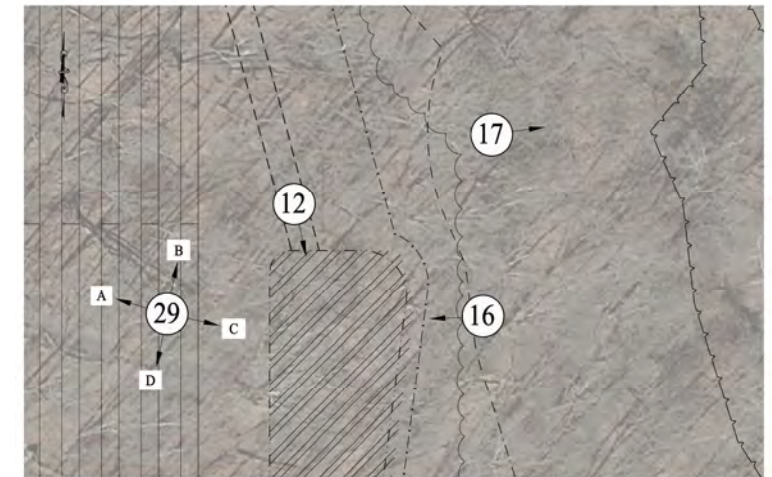


Photo 29B: Looking North



Proposed Detention
Basin

Existing Stone Wall

Photo 29C: Looking West

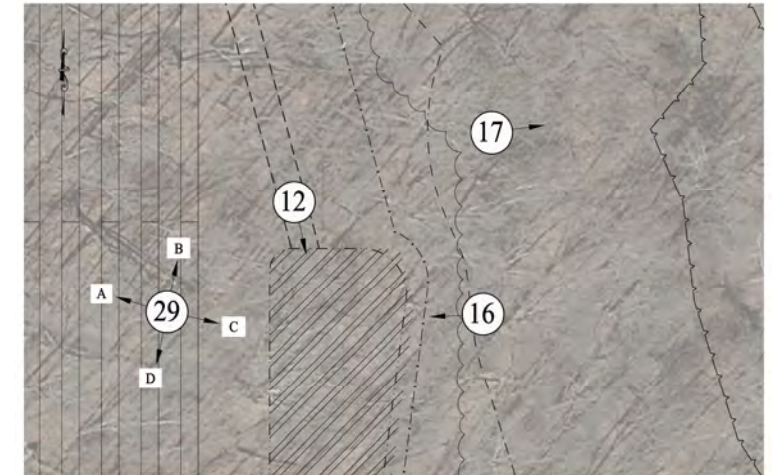


Photo 29D: Looking South

ATTACHMENT E

TCLP Test Results

Test Report

REPORT No.: SHE21-01442/1

DATE RECEIVED: 2021/02/24

ATTENTION: Ya XIAO

ANALYSIS DATE : 2021/02/24~2021/03/10

CUSTOMER: Trina Solar Co., Ltd.

DATE REPORTED: 2021/03/10

No.2 TianHe Road, Trina PV
Industrial Park, New District,
Changzhou City, Jiangsu Province
213031

SAMPLE (S): Solid waste (1)

REFERENCE: -

REMARKS

- 1.The results apply to the sample(s) as received
- 2.The report is translated from SHE21-01442.

Edited by:

Min ZHOU

Reviewed by:

Jun MENG

Approved by:

Honglou WANG

Statement

1. The test report is invalid without the official seal of the laboratory.
2. This test report cannot be reproduced in any way, except in full content, without prior approval in writing by the laboratory.
3. The test report is invalid without the signature of the compiler, the checker and the approver
4. The test report is invalid if altered.
5. The test report has been drafted in Chinese and translated into English (if applicable) for convenience only. In the event of discrepancy, the Chinese version shall prevail.
6. Should you have any queries or objection to the test report, please contact us within 10 days after receiving the report.

Legend

NA The sample was not analysed for this analyte

↑ Detection limit raised

↓ Detection limit lowered

ND Not Detected

INORGANIC & ORGANIC ANALYSIS

Report No.: SHE21-01442/1

Customer Reference: -

Lab ID	SHE21-01442.001
Customer ID	TSM-530DEG19C.20
Order No	SHES2102003321TX
Serial No	A08210100400137
Date Received	2021/02/24

TCLP ITEM	METHOD	MDL	UNIT	Limit	Solid waste
Arsenic (As)	USEPA 200.8-1994	0.050	mg/L	≤5	<0.050
Barium (Ba)	USEPA 200.8-1994	0.010	mg/L	≤100	0.195
Cadmium (Cd)	USEPA 200.8-1994	0.001	mg/L	≤1	<0.001
Chromium (Cr)	USEPA 200.8-1994	0.010	mg/L	≤5	<0.010
Lead (Pb)	USEPA 200.8-1994	0.010	mg/L	≤5	<0.010
Selenium (Se)	USEPA 200.8-1994	0.050	mg/L	≤1	<0.050
Silver (Ag)	USEPA 200.8-1994	0.010	mg/L	≤5	<0.010
Mercury (Hg)	USEPA 7473-2007	0.005	mg/L	≤0.2	<0.005
2,4-D	USEPA 8151A-1996	0.0005	mg/L	≤10	<0.0005
2,4,5-TP (Silvex, Fenopop)	USEPA 8151A-1996	0.0005	mg/L	≤1	<0.0005
Benzene	USEPA 8260D-2018	0.0005	mg/L	≤0.5	<0.0005
Carbon tetrachloride	USEPA 8260D-2018	0.0005	mg/L	≤0.5	<0.0005
Chlorobenzene	USEPA 8260D-2018	0.0005	mg/L	≤100	<0.0005
Chloroform	USEPA 8260D-2018	0.0005	mg/L	≤6	<0.0005
1,4-Dichlorobenzene	USEPA 8260D-2018	0.0005	mg/L	≤7.5	<0.0005
1,2-Dichloroethane	USEPA 8260D-2018	0.0005	mg/L	≤0.5	<0.0005
1,1-Dichloroethene	USEPA 8260D-2018	0.0005	mg/L	≤0.7	<0.0005
2-butanone(MEK)	USEPA 8260D-2018	0.020	mg/L	≤200	<0.020
Tetrachloroethene	USEPA 8260D-2018	0.0005	mg/L	≤0.7	<0.0005
Trichloroethene	USEPA 8260D-2018	0.0005	mg/L	≤0.5	<0.0005
Vinyl chloride	USEPA 8260D-2018	0.0005	mg/L	≤0.2	<0.0005
2,4-Dinitrotoluene	USEPA 8270E-2018	0.0005	mg/L	≤0.13	<0.0005
Hexachlorobenzene	USEPA 8270E-2018	0.0005	mg/L	≤0.13	<0.0005
Hexachlorobutadiene	USEPA 8270E-2018	0.0005	mg/L	≤0.5	<0.0005



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e sgs.china@sgs.com

INORGANIC & ORGANIC ANALYSIS

Report No.: SHE21-01442/1

Customer Reference: -

Lab ID	SHE21-01442.001
Customer ID	TSM-530DEG19C.20
Order No	SHES2102003321TX
Serial No	A08210100400137
Date Received	2021/02/24
Limit	
Solid waste	

TCLP ITEM	METHOD	MDL	UNIT		
Hexachloroethane	USEPA 8270E-2018	0.0005	mg/L	≤3	<0.0005
Nitrobenzene	USEPA 8270E-2018	0.0005	mg/L	≤2	<0.0005
Pentachlorophenol	USEPA 8270E-2018	0.0025	mg/L	≤100	<0.0025
Pyridine	USEPA 8270E-2018	0.002	mg/L	≤5.0	<0.002
2,4,5-Trichlorophenol	USEPA 8270E-2018	0.0005	mg/L	≤400	<0.0005
2,4,6-Trichlorophenol	USEPA 8270E-2018	0.0005	mg/L	≤2	<0.0005
Methylphenol	USEPA 8270E-2018	0.001	mg/L	≤200	<0.001
2-Methylphenol	USEPA 8270E-2018	0.0005	mg/L	≤200	<0.0005
3&4-Methylphenol	USEPA 8270E-2018	0.0005	mg/L	≤200	<0.0005
Endrin	USEPA 8270E-2018	0.0005	mg/L	≤0.02	<0.0005
γ-BHC	USEPA 8270E-2018	0.0005	mg/L	≤0.4	<0.0005
Toxaphene	USEPA 8270E-2018	0.050	mg/L	≤0.5	<0.050
Methoxychlor	USEPA 8270E-2018	0.0005	mg/L	≤10	<0.0005
Heptachlor	USEPA 8270E-2018	0.0005	mg/L	≤0.008	<0.0005
Chlordane(Total)	USEPA 8270E-2018	0.001	mg/L	≤0.03	<0.001

Remark:

- 1.Preparative method:USEPA1311-1992(Toxicity Characteristic Leaching Procedure)
- 2.The Limits comes from CFR(code of federal regulations) title 40 part 261.24.



Method List

USEPA 200.8-1994 Metals ICP-MS
 USEPA 7473-2007 Metals-Hg
 USEPA 8151A-1996 Acid Herbicides in Water by GC-MS
 USEPA 8260D-2018 VOCs
 USEPA 8270E-2018 SVOCs

Equipment Information

Method:USEPA 200.8-1994

Equipment Name	Model	Equipment Number	Serial Number
ICP-MS	Agilent 7900	CHEM-998	JP16311502

Method:USEPA 7473-2007

Equipment Name	Model	Equipment Number	Serial Number
Hg analyzer	Milestone DMA-80	CHEM-958	16041979

Method:USEPA 8151A-1996

Equipment Name	Model	Equipment Number	Serial Number
GC-MS	Agilent 7890A/5975C	CHEM-ENV085	CN12371032/US12362A17

Method:USEPA 8260D-2018

Equipment Name	Model	Equipment Number	Serial Number
PT-GC-MS	AQUATEk100&Agilent7890B/5975A	CHEM-937	US15240014/CN15423234/US1541L452

Method:USEPA 8270E-2018

Equipment Name	Model	Equipment Number	Serial Number
GC-MS	Agilent 7890B/5977B	CHEM-1175	CN18293008/US1824R018

Method:USEPA 8270E-2018

Equipment Name	Model	Equipment Number	Serial Number
GC-MS	Agilent 7890B/5977B	CHEM-1175	CN18293008/US1824R018



APPENDIX 1

Report No.:SHE21-01442/1

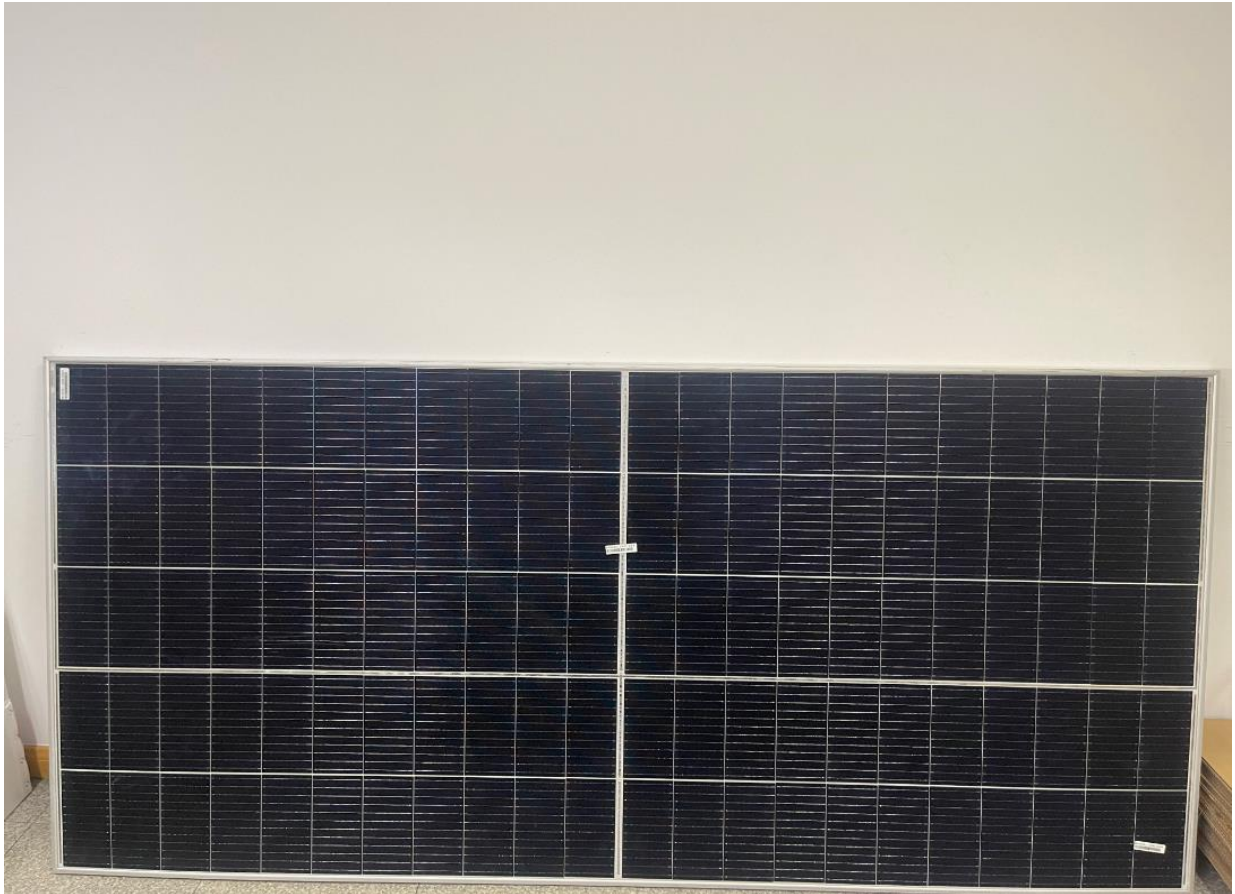
Customer Reference: -



APPENDIX 2

Report No.:SHE21-01442/1

Customer Reference: -



Page 7 of 8



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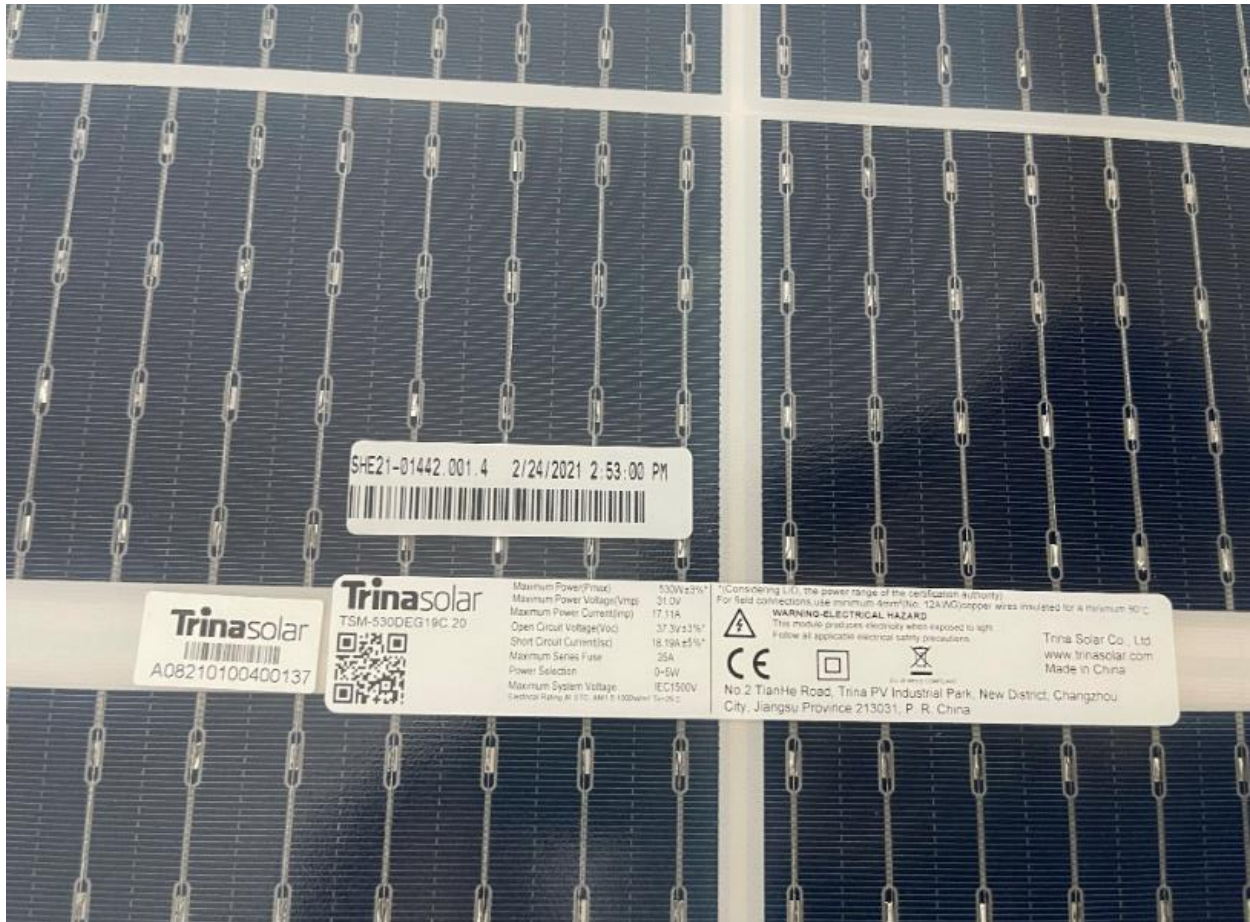
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中国·上海·徐汇区宜山路889号3号楼 邮编: 200233 t (86-21) 61072828 f (86-21) 61152164 e sgs.china@sgs.com

Member of the SGS Group (SGS SA)

APPENDIX 3

Report No.:SHE21-01442/1

Customer Reference: -



End of report



SGS-CTC (Shanghai) Technical Service Co., Ltd.
Testing Center-Environmental Technology Service

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ATTACHMENT F

Decommissioning Plan

DECOMMISSIONING PLAN

I. Summary

The decommissioning of the solar photovoltaic project includes the removal of all components associated with the project and the restoration of the site to its condition at the time of commencement of construction. The goal of which is to remove all equipment installed for the purpose of power. The decommission process will include the de-energization of the solar project, the removal of PV modules, the removal of the PV module steel racking system, the removal of driven steel foundations, the removal of concrete pads, the removal of all buried conduit and conductors, the removal of inverters, the removal of transformers, the removal of security fencing, the removal of access roads and the revegetation of the site. Many of the components including electrical components, steel structures, PV modules and conductors can be recycled. All aspects of the decommissioning process will be in accordance with local permitting requirements as well as all applicable federal, state, and local laws. An on-site manager will be designated to the decommissioning process. The on-site manager will be responsible for the successful completion of the decommissioning process as well as the safety of the workers, public health, and environment of the project site for the duration of the work. TRITEC Americas, LLC ("Petitioner") will be responsible for the decommissioning of the project in accordance with this scope.

II. Decommissioning and Restoration Process

Petitioner will remove all associated components of the Project in approximately eight (8) weeks. Debris and recyclable material will be placed in temporary storage locations on-Site pending permanent removal. Approximately 95% of materials are recyclable and will be transported to the appropriate recycling facilities. Any non-recyclable material will be transported to a nearby landfill and properly disposed of in accordance with state and federal law. The total decommissioning process will be comprised of five (5) steps as more thoroughly discussed below:

- a. Mobilization:** The decommissioning process will require the mobilization of construction equipment, tools, trash containers, and material transportation trucks.
- b. Module and Rack Disassembly:** The first component to address in the decommissioning process is the photovoltaic array and its associated racking structure. Certified electricians will de-energize the circuits and confirm the array is safe for disassembly. Modules will then be removed individually and temporarily stored on-site. The modules will be assessed for value at the time of decommissioning and either recycled or transported to an appropriate disposal site.

The steel racking structure will be unbolted and disassembled. Steel posts embedded in the ground that support the module racking system will be removed using construction equipment. Since the posts have no concrete foundation, associated holes will be small during the removal process. Any resulting holes

will be backfilled with local soil to match existing soil conditions. All steel associated with the module racking structure will be transported to a steel recycling site.

- c. **Electrical Component Removal:** Certified electricians will de-energize circuits and confirm the components are safe for removal. The transformers contain an environmentally safe mineral oil which will be contained and recycled separately from the equipment. The equipment will be removed, aggregated on-site, and transported to an appropriate electrical recycling facility.

There will be two (2) concrete pads, one for the transformer and one for the medium voltage switchgear equipment. The pads are proposed to be about 20' x 30' and 20' x 60' each (final pad sizes will be determined when the equipment is procured). The concrete will be demolished using jackhammers and hauled to an appropriate concrete disposal site.

The electrical conductors/wiring will be removed from above ground and underground locations. Underground conduit is assumed to be excavated to a depth of 3' below grade. All excavated areas will be filled, compacted and regraded. All electrical conductors and associated conduit will be removed and recycled. The overhead interconnection circuit which connects the solar project to the utility distribution circuit on Bethmour Road is owned and operated by Eversource Energy. At the time of decommissioning, the circuit consisting of three (3) overhead utility poles may remain in place if the landowner prefers this circuit for future use on the site. If the circuit is not to be used, the associated poles and conductors will be removed.

- d. **Perimeter Fence:** The seven-foot (7') steel perimeter security fence will remain in place during the decommissioning process for security and public safety. Once power generation materials have been properly disposed, the security fence will be dismantled. Components will be transported to an appropriate recycling site.
- e. **Civil Site Restoration:** The gravel access road will remain in place during the decommissioning process. Once associated components and materials have been properly disposed, the gravel access road will be removed.

The civil site restoration will target the restoration of the property to pre-project conditions. Any excavated areas will be backfilled and compacted with local soils to match surrounding topography. Any compacted areas that will inhibit the growth of new vegetation will be aerated to encourage new vegetative cover. Aeration, de-compaction, disking and seeding processes will be utilized as needed to encourage full vegetative coverage.

ATTACHMENT G

Operations and Maintenance Plan

	O&M Scope	Frequency per Year	Description
1.	General Site Inspection	1x per year	<ul style="list-style-type: none"> - Verify safety and Identification labeling is present and legible. - Inspect site access/egress locations are free of obstructions and hazards. - Equipment access lanes are free of obstructions and hazards. - Inspect for changes of environmental conditions such as nearby construction activity, agricultural activities, bird migrations, water table changes, acts of vandalism, and shading.
2.	Mechanical System Inspection	1x per year	<ul style="list-style-type: none"> - Racking structures visual and mechanical inspection. - Mechanical inspection 2% of Module-to-racking attachments for torque specification. - Module visual inspection. - DC Optimizer operation verification via monitoring equipment (when applicable). - Ballast block, foundations, driven piers, mechanical attachments, and earth screw visual inspection. - Roof protection installation methods and materials. - Equipment Grounding Conductor electrical continuity inspection. - Equipment bonding to ground electrical continuity inspection.

3.	DC & AC Electrical System Inspection	1x per year	<ul style="list-style-type: none"> - Verify safety and Identification labeling is present and legible. - Enclosure mounting, gaskets, interior, and exterior visual inspection. - Grounding and bonding inspection. - Terminations (conductors) thermography scanning. - Visual inspection of conductor termination torque markings. - Fuse and breaker thermography scanning. - Vacuum clean interiors. - Visual inspection of conduits, fittings, junctions/splice boxes, and enclosures. - Exercise operation of all protective devices. - Switchgear inspection. - Use infrared camera to inspect for hot spots, bypass.
4.	Inverter Inspection	1x per year	<ul style="list-style-type: none"> - Verify safety and Identification labeling is present and legible. - Enclosure mounting, gaskets, Interior, and exterior visual inspection. - Grounding and bonding inspection. - Inverter operation verification. - Use an infrared camera to check connections. - Vacuum clean interior. - Clean air intake/exhaust screens, fans, and filters. - Complete all other manufacturer specific maintenance procedures not listed above.
5.	Data Acquisition System Inspection	1x per year	<ul style="list-style-type: none"> - Verify safety and Identification labeling is present and legible. - Meteorological data sensor cleaning, positioning, and operation. - Inverter communication (when applicable).
6.	Reporting	1x per year	<ul style="list-style-type: none"> - Provide digital commissioning report including results from all steps with responses noting Pass, Values, or Failure with explanation. - Photo report of deficiencies.
7.	Inverter Replacement	As Needed	<ul style="list-style-type: none"> - Additional site visits related to inverter failure will be billed to Asset Manager on a time and materials basis. - Site visits will be followed with a report on site conditions and findings within three (3) business days.

8.	Testing	1x per year	<ul style="list-style-type: none"> - Perform performance test: measure incident sunlight and simultaneously observe temperature and calculate the balance of system efficiency. Compare readings with diagnostic benchmark (original efficiency of system).
9.	Vegetation Maintenance	Varies	<ul style="list-style-type: none"> - Inspect site for vegetation growth or accumulation which could shade arrays and impact PV production (4x per year) - Mow, clear, and/or apply herbicides or pre-emergent (where allowed by applicable laws and regulations) to manage site vegetation (4x per year). - Inspect arrays for soiling, evidence of pest infestation, water pooling, vegetation growth, shading or damage (2x per year). - Photo-document general condition of each array, noting any corrective actions and location of any issues requiring remediation beyond project manager visit time allocation (2x per year).
10.	Stormwater Control Management	As Needed	<ul style="list-style-type: none"> - Perform the steps to be outlined in the Stormwater Pollution Control Plan, approved by the Connecticut Department of Energy and Environmental Protection, and in compliance with the 2004 Connecticut Stormwater Quality Manual and 2002 Connecticut Guidelines for Soil Erosion and Sediment Control.