STATE OF CONNECTICUT CONNECTICUT SITING COUNCIL

IN RE:	
IN KE.	•

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A PETITION OF CELLCO PARTNERSHIP : PETITION NO. ____

D/B/A VERIZON WIRELESS FOR A

DECLARATORY RULING ON THE NEED

TO OBTAIN A SITING COUNCIL

CERTIFICATE FOR THE INSTALLATION
OF A WIRELESS TELECOMMUNICATIONS

FACILITY AT 1300 HALL BOULEVARD,

BLOOMFIELD, CONNECTICUT : JUNE 29, 2022

PETITION FOR A DECLARATORY RULING: INSTALLATION HAVING NO SUBSTANTIAL ADVERSE ENVIRONMENTAL EFFECT

I. Introduction

Pursuant to Sections 16-50j-38 and 16-50j-39 of the Regulations of Connecticut State Agencies ("R.C.S.A."), Cellco Partnership d/b/a Verizon Wireless ("Cellco") hereby petitions the Connecticut Siting Council (the "Council") for a declaratory ruling ("Petition") that no Certificate of Environmental Compatibility and Public Need ("Certificate") is required under Section 16-50k(a) of the Connecticut General Statutes ("C.G.S.") for the installation of a wireless telecommunications facility on the roof of a 4-story commercial office building (the former Cigna Headquarters) on an approximately 37-acre parcel at 1300 Hall Boulevard in Bloomfield, Connecticut (the "Property"). *See* Attachment 1—Site Schematic Map (Aerial Photograph). The Property and several separate adjacent parcels are owned by The Atrium CT, LLC ("Atrium"). The Property is developed with two commercial office buildings, a structured parking garage, surface parking areas and related site improvements. A dipole antenna is currently attached to the mechanical penthouse of the roof of the building. According to Atrium, this antenna is used for on-property communications among the owner's staff.

The Property is surrounded by undeveloped land to the west; undeveloped land and ball fields to the south, the Gillette Ridge Golf Course to the north and additional commercial uses to the east on adjacent parcels also owned by Atrium. Cellco refers to its proposed facility as its Bloomfield 4 cell site (the "Bloomfield 4 Facility").

II. Proposed Construction Activity

A. Cellco's Proposed Bloomfield 4 Facility

The Bloomfield 4 Facility will consist of the installation of nine (9) panel type antennas and nine (9) remote radio heads ("RRHs") attached to a new steel lattice tower that would be constructed in the northeast portion of the roof. The new tower would extend approximately 12'-6" above an existing mechanical penthouse on the roof. Equipment associated with the antennas will be located on a steel dunnage platform on the roof of the building to the east of the mechanical penthouse. (*See* Cellco's Project Plans included in <u>Attachment 2</u>).

Cellco will provide wireless telecommunications services in its 700 MHz, 850 MHz, 1900 MHz, 2100 MHz and C-Band (3730 MHz and 3625 MHz) frequency ranges from the Bloomfield 4 Facility. Specifications for Cellco's antennas and remote radio heads are included in Attachment 3. The Bloomfield 4 Facility will be capable of providing 5G wireless service.

In cooperation with its engineering consultant Chappell Engineering Associates, LLC, a Structural Analysis and a separate Structural (Mount) Analysis have been performed and have confirmed that the host-building, the rooftop tower and proposed antenna mounting system will be structurally capable of supporting the Bloomfield 4 Facility. Copies of the two structural analyses referenced about are included in <u>Attachment 4</u>.

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III. Discussion

A. The Proposed Facility Will Not Have A Substantial Adverse Environmental Effect

The Public Utility Environmental Standards Act (the "Act"), C.G.S. § 16-50g et seq., provides for the orderly and environmentally compatible development of telecommunications facilities in the state to avoid "a significant impact on the environment and ecology of the State of Connecticut." C.G.S. § 16-50g. To achieve these goals, the Act established the Council, and requires a Certificate of Environmental Compatibility and Public Need for the construction of cellular telecommunication towers "that may, as determined by the council, have a substantial adverse environmental effect". C.G.S. § 16-50k(a).

1. Physical Environmental Effects

Cellco respectfully submits that the facility will not involve a significant impact on the physical and environmental characteristics of the Property or the surrounding community. All improvements associated with the Bloomfield 4 Facility will be located on the roof of the existing 4- story office building on the existing commercial office campus. No ground disturbance, tree removal or site grading is required to develop and maintain the Bloomfield 4 Facility.

2. Visual Effects

Given its location on the roof of an existing 4-story office building and the limited height of the proposed lattice tower structure, any visual effects associated with the proposed Bloomfield 4 Facility will be minimal and will not detract from the general appearance and characteristics of the building or the Property. Photo Simulations of the proposed rooftop lattice tower are included in <u>Attachment 5</u>. The top portion of the lattice tower would be visible from certain locations to the south of the building on the Property or on the adjacent parcel to the north

(Gillette Ridge Golf Course). These visual effects, however, are minor and will not adversely impact any adjacent recreational or residential development in the area.

3. FCC Compliance

Radio frequency ("RF") emissions from the Bloomfield 4 Facility will not exceed the maximum permissible exposure limits established by the Federal Communications Commission ("FCC"). Included in <u>Attachment 6</u> is a general power density table that demonstrates that Cellco's facility will operate within the FCC safety standards.

4. FAA Notification Not Required

Cellco prepared a Federal Airways and Airspace Report ("FAA Report") for the proposed Bloomfield 4 Facility. According to the FAA Report, the proposed Bloomfield 4 Facility will not constitute an airspace obstruction and therefore notice of the FAA is not required. A copy of the FAA Report is included in <u>Attachment 7</u>.

B. <u>Notice to the Town, Property Owner and Abutting Landowners</u>

On June 29, 2022, a copy of this Petition was sent to Bloomfield's Town Manager, Stanley Hawthorne; Jennifer Valentino-Rodriguez, Bloomfield's Director of Planning and Zoning; and The Atrium CT LLC, the Owner of the Property. Because the Property is located within 2,500 feet of the Town of West Hartford, copies of this Petition were also sent to West Hartford's Mayor, Shari Cantor and West Hartford's Town Planner, Todd Dumais. Copies of the letters sent to public officials and the Property owner are included in <u>Attachment 8</u>.

A copy of this Petition was also sent to the owners of land that abuts the Property. A sample abutter's letter and the list of those abutting landowners to whom notice was sent is included in Attachment 9.

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IV. Conclusion

Based on the information provided above, Cellco respectfully requests that the Council issue a determination, in the form of a declaratory ruling, that the installation of the proposed rooftop telecommunications tower described above, will not have a substantial adverse environmental effect and does not require the issuance of a Certificate of Environmental Compatibility and Public Need pursuant to § 16-50k of the General Statutes.

Respectfully submitted,

CELLCO PARTNERSHIP d/b/a VERIZON WIRELESS

Kenneth C. Baldwin, Esq.

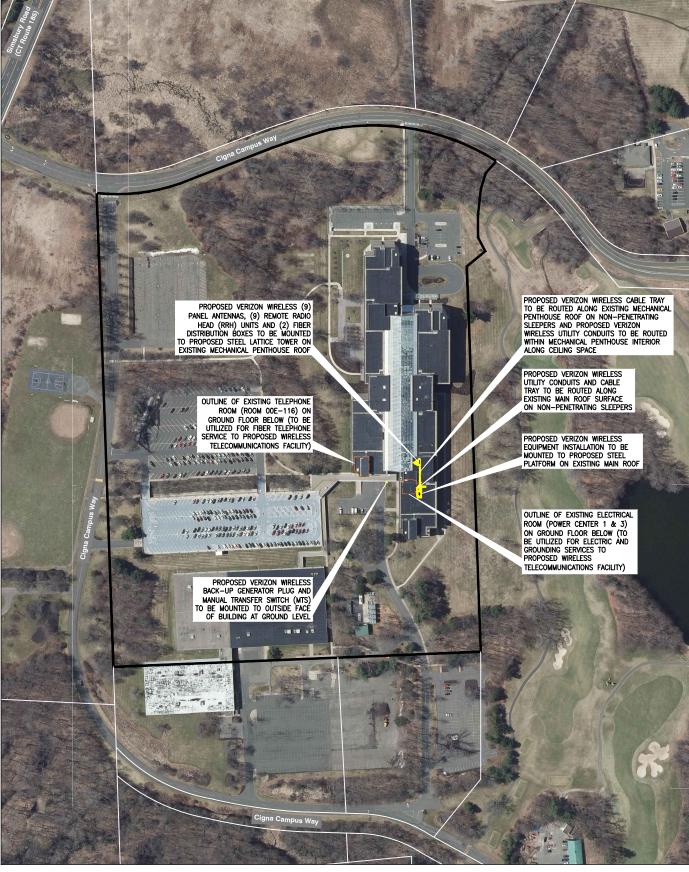
Robinson & Cole LLP 280 Trumbull Street

Hartford, CT 06103-3597

(860) 275-8200

Its Attorneys

ATTACHMENT 1



LEGEND

Proposed Verizon Wireless Equipment

Proposed Verizon Wireless Conduit and/or Cable Tray

Existing Ground Floor Utility Rooms

Subject Property

Approximate Parcel Boundary (Town Of Bloomfield, CT GIS)

NORTH 0' 75' 150' 300' 450'

Site Schematic

Proposed Wireless Telecommunications Facility Bloomfield 4 CT 1300 Hall Boulevard Bloomfield, CT 06002





ATTACHMENT 2



CHAPPELL ENGINEERING ASSOCIATES, ILC

ARCHITECT/ENGINEER:

R.K. EXECUTIVE CENTRE
201 BOSTON POST ROAD WEST
SUITE 101
MARILEOROUGH, MA 01752
(508) 481-7400
www.chappellengineering.com

Verizon

20 ALEXANDER DRIVE, WALLINGFORD, CT 06492

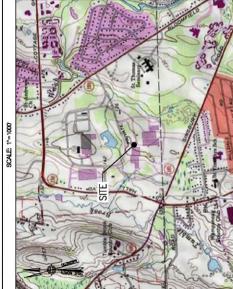
BLOOMFIELD 4 CT

1300 HALL BOULEVARD BLOOMFIELD, CT 06002 PROJECT TYPE: WIRELESS TELECOMMUNICATIONS INSTALLATION ON ROOFTOP OF EXISTING (4)-STORY STEEL FRAMED BUILDING

SITE INFORMATION:

N 41°-48'-30.48' (41.808467') (NAD '83) W 72°-44'-36.55' (72.743486') (NAD '83) HARTFORD COUNTY, CONNECTICUT SOUTHEAST CORNER OF EXISTING MECHANICAL PENTHOUSE THE ATRIUM CT LLC
SEARK AVENUE, 17TH FLOOR
NEW YORK, NY 10168
CELLCO PARTNERSHIP
CELLCO PARTNERSHIP
SO ALEXANDER DRIVE
WALLINGFORD, CT 06492 1300 HALL BOULEVARD BLOOMFIELD, CT 06002 ARCHITECT / ENGINEER SITE CONTROL POINT PROPERTY OWNER: SITE ADDRESS: APPLICANT: COUNTY:

VICINITY MAP



DRIVING DIRECTIONS

FROM WALLINGFORD, TAKE 191 NORTH. TAKE THE CT-218 EXIT TOWARD
WINDSORBLOOMED, THE TONTO CT-380 WST, USA THE LEFT STAKES TO THEN LOY TO CT-189 SOUTH, TUBN RIGHT THEN RIGHT AGAIN. THE SITE IS LOCATED STRANGHT AHEAD.
ONTO CT-189 SOUTH, TUBN RIGHT THEN RIGHT AGAIN. THE SITE IS LOCATED STRANGHT AHEAD.

DATE

ENGINEER/LAND SURVEYOR

	REV.	ю	ю	ın	10	10	ю	
SHEET INDEX	DESCRIPTION	TITLE SHEET	LOCATION PLAN	PROPERTY PLAN	PART ROOF PLAN AND SITE DETALS	NORTH BUILDING ELEVATION AND ENLARGED PART NORTH BUILDING ELEVATION	ANTENNA DETAILS AND ANCILLARY EQUIPMENT SPECIFICATIONS	
	DWG.	Ē	8	200	104	A02	PF01	

DO NOT SCALE DRAWINGS

TITLE SHEET

BLOOMFIELD 4 CT 1300 HALL BOULEVARD BLOOMFIELD, CT 06002

REVISED PER ATTORNEY COMMENTS

DESCRIPTION
ISSUED FOR REVIEW
REVISED PER 1A FINDINGS

ISSUED FOR ZONING (FINAL)

REVISIONS

REVISED CONDUIT ROUTING
REVISED PER LANDLORD COMMENT

LA LANE BESTING DUBLISHORS AND CONDITIONS AT THE PROPOSED PROJECT STEE SHALL BE VERTICED IN HER FEB. DO UNIVERSIGHT OF THE PROJECT OWNERS BE VERHELD IN HIER FIELD DUBLISH WHITHING OF THE PROJECT OWNERS PRESENTATIVE STEEL BE VERTICED BY ALTO SECHEMANICES IN METALLE IN THE PROPOSED WORK AFFECTED BY SLICH DISCREPANCES. IN PRECEIVED BY SLICH DISCREPANCES. IN THE PREVIOUS DELACOR SLICH HOUSE PROSTING STEEL BECOME THE RECOVER THE RECOVER THE RECOVER THE THE PROJECT OF SLICH PROSTING STEEL STEEL FOR COASITILE COME THE PREVIOUS DELACOR SLICH PROSTING STEEL STEEL FOR COASITILE COME THE PREVIOUS DELACOR STEEL PROJECT STEEL STE

PROJECT DESCRIPTION

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- 1. THIS IS AN UNMANNED AND RESTRICTED ACCESS EGUIPMENT INSTALLATION AND WILL BELSED FOR THE TRANSMISSION OF PAGAD OSMAL, TOPA THE EDS TRECOMMINICATIONS SERVICE.

 2. THIS FACILITY MILL CONSUMENT ON UNRECOVERABLE BENEVI.

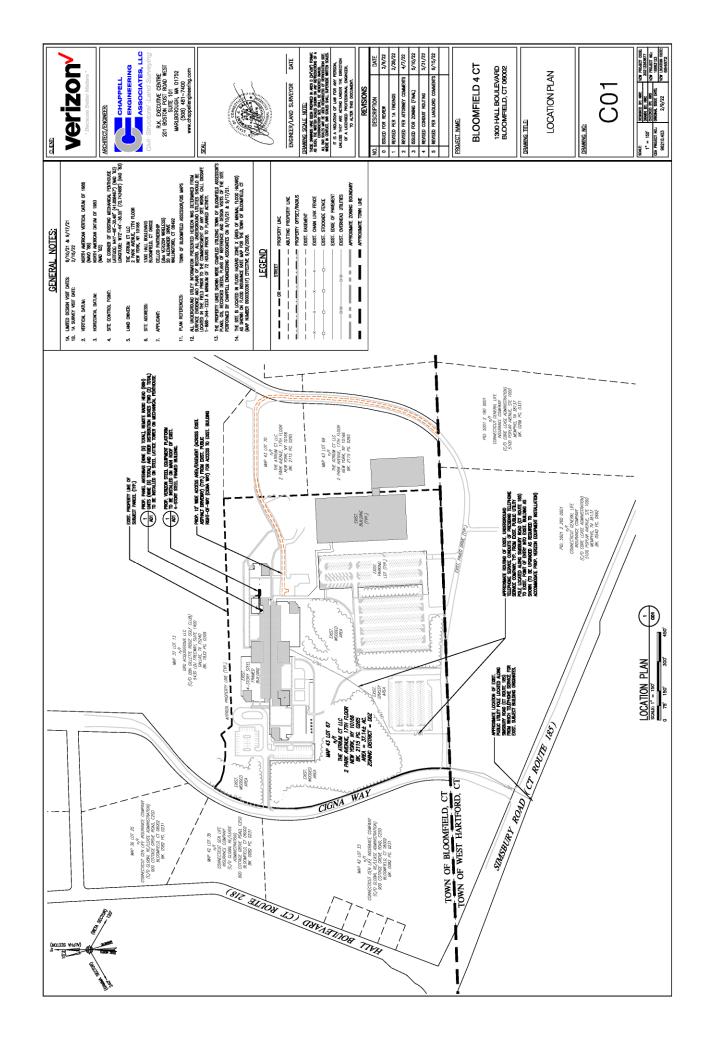
 3. NOT MALE WATERS SIDE OF PROVIDED, AT THIS LOCATION.

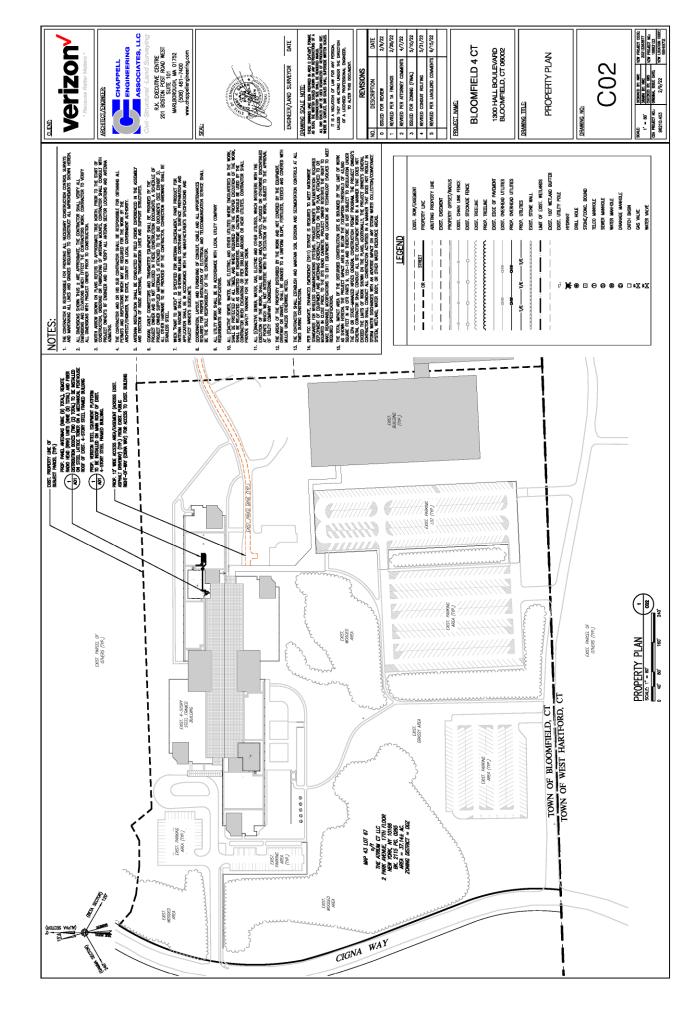
 4. NO WASTER WATERS VILLE GERBER TOLAT THIS LOCATION.

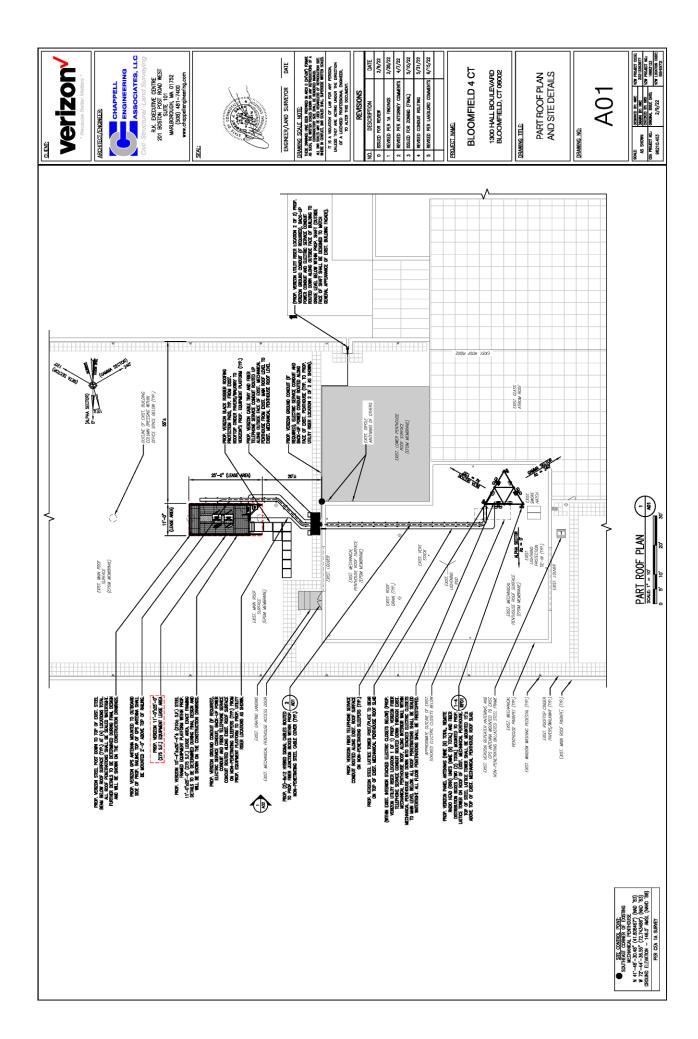
 5. NO SAGEN WATER WILL BE GERBER TOLAT THIS LOCATION.

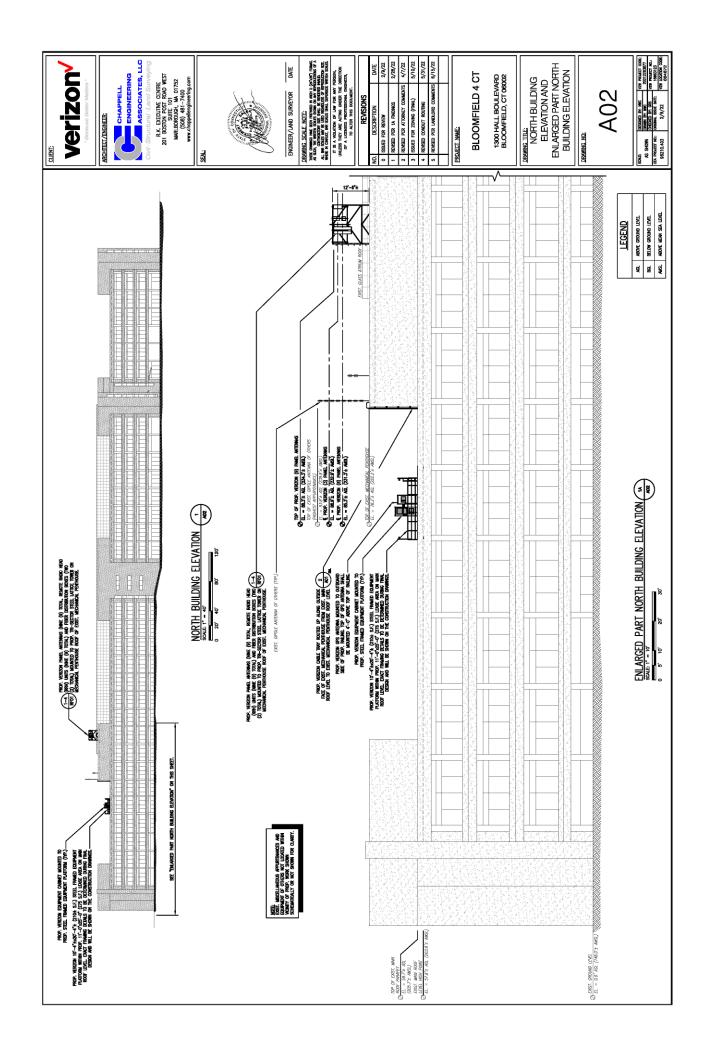
 5. NO SAGEN WATER WILL BE GERBER TOLAT THIS LOCATION.
- AS SHOWN CEA PROJECT NO. 96210.403

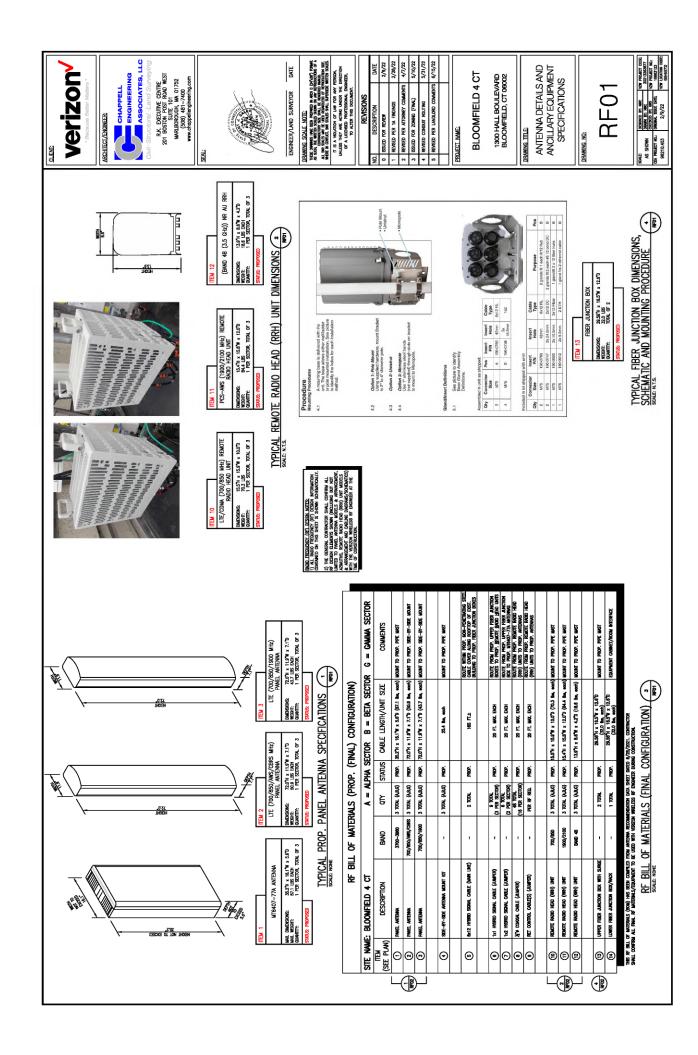












ATTACHMENT 3



6-port sector antenna, 2x 698–896 and 4x 1695–2360 MHz, 65° HPBW, 2x RET. Both high bands share the same electrical tilt.

- Interleaved dipole technology providing for attractive, low wind load mechanical package
- Internal SBT on low and high band allow remote RET control from the radio over the RF jumper cable
- Separate RS-485 RET input/output for low and high band
- One RET for low band and one RET for both high bands to ensure same tilt level for 4x Rx or 4x MIMO

General Specifications

Antenna TypeSectorBandMultibandColorLight gray

Grounding TypeRF connector body grounded to reflector and mounting bracket

Performance Note Outdoor usage | Wind loading figures are validated by wind tunnel

measurements described in white paper WP-112534-EN

Radome MaterialFiberglass, UV resistantRadiator MaterialLow loss circuit board

Reflector Material Aluminum

RF Connector Interface 4.3-10 Female

RF Connector LocationBottom

RF Connector Quantity, high band 4
RF Connector Quantity, low band 2
RF Connector Quantity, total 6

Remote Electrical Tilt (RET) Information

RET Interface 8-pin DIN Female | 8-pin DIN Male

RET Interface, quantity 2 female | 2 male

Input Voltage 10-30 Vdc

Internal Bias Tee Port 1 | Port 3

Internal RET High band (1) | Low band (1)

Power Consumption, idle state, maximum 2 W
Power Consumption, normal conditions, maximum 13 W

Page 1 of 4



Protocol 3GPP/AISG 2.0 (Single RET)

Dimensions

Width 301 mm | 11.85 in

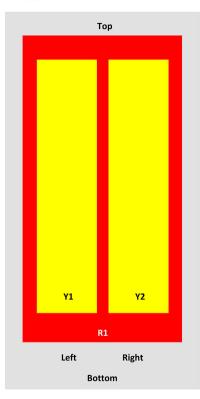
Depth 180 mm | 7.087 in

Length 1828 mm | 71.969 in

Net Weight, without mounting kit 19.8 kg | 43.651 lb

Array Layout

<u>NHH</u>



Array	Freq (MHz)	Conns	RET (SRET)	AISG RET UID
R1	698-896	1-2	1	ANxxxxxxxxxxxxxxx
Y1	1695-2360	3-4	2	ANxxxxxxxxxxxxxxxxxxxxx
			1	

View from the front of the antenna (Sizes of colored boxes are not true depictions of array sizes)

Electrical Specifications

Impedance 50 ohm

Operating Frequency Band 1695 – 2360 MHz | 698 – 896 MHz

COMMSCOPE®

Polarization ±45°

Total Input Power, maximum $900~\mathrm{W} \ @ \ 50~\mathrm{^{\circ}C}$

Electrical Specifications

Frequency Band, MHz	698-806	806-896	1695-1880	1850-1990	1920-2200	2300-2360
Gain, dBi	14.9	15	17.7	17.9	18.4	18.7
Beamwidth, Horizontal, degrees	65	60	71	69	64	57
Beamwidth, Vertical, degrees	12.4	11.2	5.7	5.2	4.9	4.6
Beam Tilt, degrees	0-14	0-14	0-7	0-7	0-7	0-7
USLS (First Lobe), dB	13	14	18	18	19	18
Front-to-Back Ratio at 180°, dB	30	29	31	30	29	31
Isolation, Cross Polarization, dB	25	25	25	25	25	25
Isolation, Inter-band, dB	30	30	30	30	30	30
VSWR Return loss, dB	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0
PIM, 3rd Order, 2 x 20 W, dBc	-153	-153	-153	-153	-153	-153
Input Power per Port at 50°C, maximum, watts	300	300	300	300	300	300

Electrical Specifications, BASTA

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Frequency Band, MHz	698-806	806-896	1695-1880	1850-1990	1920-2200	2300-2360
Gain by all Beam Tilts, average, dBi	14.5	14.5	17.3	17.7	18.1	18.5
Gain by all Beam Tilts Tolerance, dB	±0.6	±1.1	±0.4	±0.4	±0.5	±0.3
Gain by Beam Tilt, average, dBi	0° 14.4 7° 14.6 14° 14.3	0° 14.7 7° 14.7 14° 14.1	0° 17.2 4° 17.3 7° 17.3	0° 17.6 4° 17.7 7° 17.7	0° 18.0 4° 18.2 7° 18.1	0 ° 18.3 4 ° 18.5 7 ° 18.6
Beamwidth, Horizontal Tolerance, degrees	±2	±2.1	±3	±4.1	±6.5	±2.9
Beamwidth, Vertical Tolerance, degrees	±0.7	±0.7	±0.3	±0.2	±0.3	±0.2
USLS, beampeak to 20° above beampeak, dB	13	14	16	16	17	15
Front-to-Back Total Power at 180° ± 30°, dB	23	22	27	27	25	25
CPR at Boresight, dB	22	21	23	23	22	19

Page 3 of 4



CPR at Sector, dB 10 7 16 13 11 4

Mechanical Specifications

Effective Projective Area (EPA), frontal $0.26 \text{ m}^2 \mid 2.799 \text{ ft}^2$ Effective Projective Area (EPA), lateral $0.22 \text{ m}^2 \mid 2.368 \text{ ft}^2$

 Wind Loading @ Velocity, frontal
 278.0 N @ 150 km/h (62.5 lbf @ 150 km/h)

 Wind Loading @ Velocity, lateral
 230.0 N @ 150 km/h (51.7 lbf @ 150 km/h)

 Wind Loading @ Velocity, maximum
 537.0 N @ 150 km/h (120.7 lbf @ 150 km/h)

 Wind Loading @ Velocity, rear
 282.0 N @ 150 km/h (63.4 lbf @ 150 km/h)

Wind Speed, maximum 241 km/h | 149.75 mph

Packaging and Weights

 Width, packed
 409 mm | 16.102 in

 Depth, packed
 299 mm | 11.772 in

 Length, packed
 1952 mm | 76.85 in

 Weight, gross
 32.3 kg | 71.209 lb

Regulatory Compliance/Certifications

Agency Classification

CHINA-ROHS Below maximum concentration value

ISO 9001:2015 Designed, manufactured and/or distributed under this quality management system

ROHS Compliant



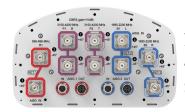
Included Products

BSAMNT-3 – Wide Profile Antenna Downtilt Mounting Kit for 2.4 - 4.5 in (60 - 115 mm) OD round members. Kit contains one scissor top bracket set and one bottom bracket set.

* Footnotes

Performance Note Severe environmental conditions may degrade optimum performance





10-port sector antenna, 2x 698–896, 4x 1695–2200 and 4x 3100-4200 MHz, 65° HPBW, 2x RETs and 2x SBTs. Both high bands share the same electrical tilt.

- Perfect antenna to add 3.5GHz CBRS to macro sites
- Low band and mid band performance mirrors the performance of existing NHH hex port antennas
- Interleaved dipole technology providing for attractive, low wind load mechanical package
- Internal SBT on low and high band allow remote RET control from the radio over the RF jumper cable
- One LB RET and one HB RET. Both high bands are controlled by one RET to ensure same tilt level for 4x MIMO

General Specifications

Antenna TypeSectorBandMultibandColorLight gray

Grounding TypeRF connector inner conductor and body grounded to reflector and mounting

bracket

Performance Note Outdoor usage

Radome MaterialFiberglass, UV resistantRadiator MaterialLow loss circuit board

Reflector Material Aluminum

RF Connector Interface 4.3-10 Female

RF Connector Location Bottom

RF Connector Quantity, high band 4
RF Connector Quantity, mid band 4
RF Connector Quantity, low band 2
RF Connector Quantity, total 10

Remote Electrical Tilt (RET) Information

RET Hardware CommRET v2

RET Interface 4x 8 pin connector as per IEC 60130-9 Daisy chain in: Male / Daisy chain out:

Female Pin3: RS485A(AISG_B), Pin5: RS485B(AISG_A), Pin6: DC 10~30V, Pin7:

DC_Return



RET Interface, quantity 2 female | 2 male

Input Voltage 10-30 Vdc

Internal RET High band (1) | Low band (1)

Power Consumption, active state, maximum 10 W Power Consumption, idle state, maximum 2 W

Protocol 3GPP/AISG 2.0 (Single RET)

Dimensions

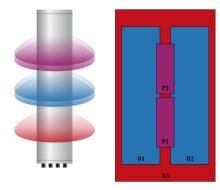
 Width
 301 mm | 11.85 in

 Depth
 181 mm | 7.126 in

 Length
 1828 mm | 71.969 in

 Net Weight, without mounting kit
 23.1 kg | 50.927 lb

Array Layout

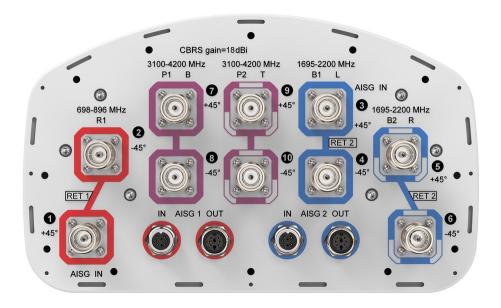


Array ID	Frequency (MHz)	RF Connector	RET (SRET)	AISG No.	AISG RET UID	
R1	698-896	1 - 2	1	AISG1	CPxxxxxxxxxxxxxxR1	
B1	1695-2200	3 - 4	2	AICCO	CPxxxxxxxxxxxxxxxxB1	
B2	1695-2200	5 - 6	2	AISG2	CPXXXXXXXXXXXXXX	
P1	3100-4200	7 - 8			N/4	
P2	3100-4200	9 - 10	N/A NA		N/A	

(Sizes of colored boxes are not true depictions of array sizes)

Port Configuration





Electrical Specifications

Impedance 50 ohm

Operating Frequency Band 1695 – 2200 MHz | 3100 – 4200 MHz | 698 – 896 MHz

Polarization ±45°

Total Input Power, maximum 1,000 W @ 50 °C

Electrical Specifications

Frequency Band, MHz	698-806	806-896	1695-188	0 1850-199	0 1920-220	0 3100-355	0 3550-370	0 3700-4200
Gain, dBi	14.8	15.2	17.4	17.8	18	17.7	17.3	17.9
Beamwidth, Horizontal, degrees	65	62	66	61	64	54	64	60
Beamwidth, Vertical, degrees	13	11.6	5.5	5.2	4.9	5.7	5.3	4.9
Beam Tilt, degrees	0-14	0-14	0-7	0-7	0-7	4	4	4
USLS (First Lobe), dB	15	15	16	18	18	16	17	18
Front-to-Back Ratio at 180°, dB	26	29	31	28	27	30	33	29
Isolation, Cross Polarization, dB	25	25	25	25	25	25	25	25
Isolation, Inter-band, dB	25	25	25	25	25	28	28	28
VSWR Return loss, dB	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0
PIM, 3rd Order, 2 x 20 W, dBc	-153	-153	-153	-153	-153	-140	-140	-140

Page 3 of 5



Input Power per Port at 50°C,	300	300	300	300	300	100	100	100
maximum, watts								

Electrical Specifications, BASTA

Frequency Band, MHz	698-806	806-896	1695-188	0 1850-199	0 1920-220	0 3100-355	0 3550-370	0 3700-4200
Gain by all Beam Tilts, average, dBi	14.6	14.8	17	17.5	17.7	17.3	17	17.2
Gain by all Beam Tilts Tolerance, dB	±0.4	±0.4	±0.6	±0.3	±0.4	±0.6	±0.7	±0.8
Gain by Beam Tilt, average, dBi	0° 14.6 7° 14.6 14° 14.4	0° 15.0 7° 14.9 14° 14.5	0° 16.9 3° 17.0 7° 16.8	0° 17.4 3° 17.5 7° 17.4	0° 17.5 3° 17.8 7° 17.6			
Beamwidth, Horizontal Tolerance, degrees	±1.7	±1.3	±7.2	±3.1	±6.2	±10	±6.7	±10.5
Beamwidth, Vertical Tolerance, degrees	±0.8	±0.8	±0.2	±0.2	±0.4	±0.4	±0.3	±0.4
USLS, beampeak to 20° above beampeak, dB	18	16	14	15	17	14		
Front-to-Back Total Power at 180° ± 30°, dB	22	25	25	25	24	26	25	24
CPR at Boresight, dB	24	17	16	21	19	15	17	14
CPR at Sector, dB	12	6	11	10	8	8	9	7

Mechanical Specifications

 Wind Loading @ Velocity, frontal
 278.0 N @ 150 km/h (62.5 lbf @ 150 km/h)

 Wind Loading @ Velocity, lateral
 230.0 N @ 150 km/h (51.7 lbf @ 150 km/h)

 Wind Loading @ Velocity, maximum
 537.0 N @ 150 km/h (120.7 lbf @ 150 km/h)

 Wind Loading @ Velocity, rear
 287.0 N @ 150 km/h (64.5 lbf @ 150 km/h)

 Wind Speed, maximum
 241 km/h | 149.75 mph

Packaging and Weights

 Width, packed
 1973 mm | 77.677 in

 Depth, packed
 441 mm | 17.362 in

 Length, packed
 337 mm | 13.268 in

 Weight, gross
 35.1 kg | 77.382 lb

Regulatory Compliance/Certifications

Agency Classification

CHINA-ROHS Above maximum concentration value

COMMSCOPE°

ROHS

Compliant/Exempted



Included Products

BSAMNT-3

Wide Profile Antenna Downtilt Mounting Kit for 2.4 - 4.5 in (60 - 115 mm) OD round members.
 Kit contains one scissor top bracket set and one bottom bracket set.

* Footnotes

Performance Note Severe environmental conditions may degrade optimum performance

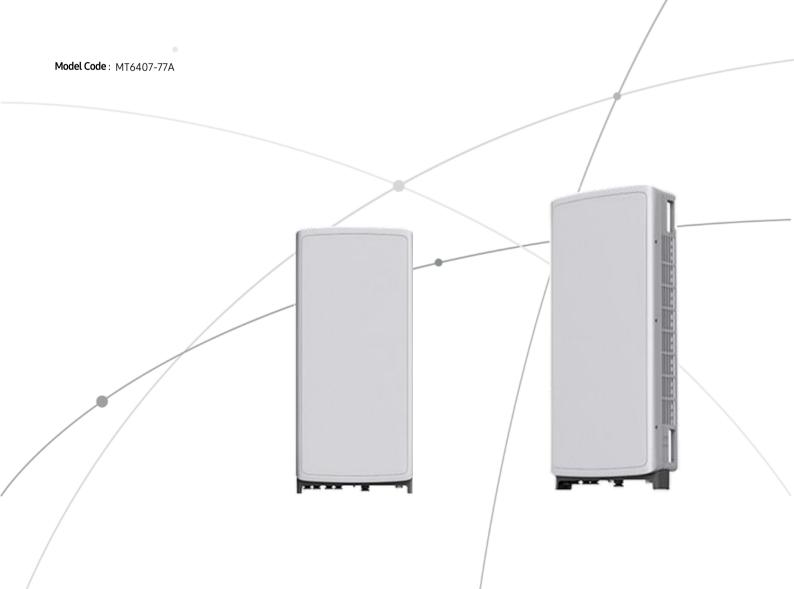


SAMSUNG

SAMSUNG C-Band 64T64R Massive MIMO Radio

for High Capacity and Wide Coverage

Samsung C-Band 64T64R Massive MIMO Radio enables mobile operators to increase coverage range, boost data speeds and ultimately offer enriched 5G experiences to users in the U.S..



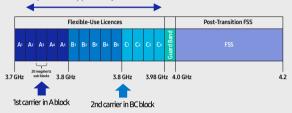
Points of Differentiation

Wide Bandwidth

With capability to support up to 2 CC carrier configuration, Samsung C-Band massive MIMO Radio supports 200 MHz bandwidth in the C-Band spectrum.

Samsung C-Band massive MIMO Radio covers the entire C-Band 280 MHz spectrum, so it can meet the operator's needs in current A block and future B/C blocks

C-Band spectrum supported by Massive MIMO Radio



Enhanced Performance

C-Band massive MIMO Radio creates sharp beams and extends networks' coverage on the critical mid-band spectrum using a large number of antenna elements and high output power to boost data speeds.

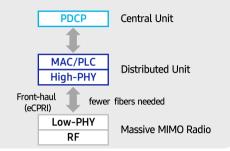
This helps operators reduce their CAPEX as they now need less products to cover the same area than before.

Furthermore, as C-Band massive MIMO Radio supports MU-MIMO(Multi-user MIMO), it enables to increase user throughput by minimizing interference.



Future Proof Product

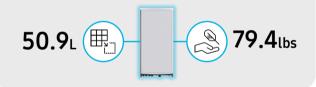
Samsung C-Band 64T64R Massive MIMO radio supports not only CPRI but also eCPRI as front-haul interface. It enables operators can cut down on OPEX/CAPEX by reducing front-haul bandwidth through low layer split and using ethernet based higher efficient line.



Well Matched Design

Samsung C-Band Massive MIMO radio utilizes 64 antennas, supports up to 280MHz bandwidth, and delivers a 200W output power. despite the above advanced performance, the Radio has a compact size of 50.9L and 79.4lbs. This makes it easy to install the Radio.

It is designed to look solid and compact, with a low profile appearance so that, when installed, harmonizes well with the surrounding environment..





Technical Specifications

Item	Specification
Tech	NR
Band	n77
Frequency Band	3700 - 3980 MHz
EIRP	78.5dBm (53.0 dBm+25.5 dBi)
IBW/OBW	280 MHz / 200 MHz
Installation	Pole/Wall
Size/ Weight	16.06 x 35.06 x 5.51 inch (50.86L)/ 79.4 lbs



About Samsung Electronics Co., Ltd.

Samsung inspires the world and shapes the future with transformative ideas and technologies. The company is redefining the worlds of TVs, smartphones, wearable devices, tablets, digital appliances, network systems, and memory, system LSI, foundry and LED solutions.

129 Samsung-ro, Yeongtong-gu, Suwon-si Gyeonggi-do, Korea

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SAMSUNG

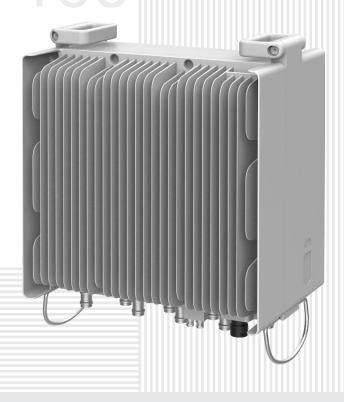
AWS/PCS MACRO RADIO

DUAL-BAND AND HIGH POWER FOR MACRO COVERAGE

Samsung's future proof dual-band radio is designed to help effectively increase the coverage areas in wireless networks. This AWS/PCS 4T4R dual-band radio has 4Tx/4Rx to 2Tx/2Rx RF chains options and a total output power of 320W, making it ideal for macro sites.

Model Code

RF4439d-25A

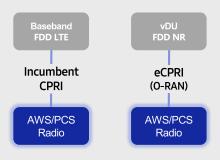




Points of Differentiation

Continuous Migration

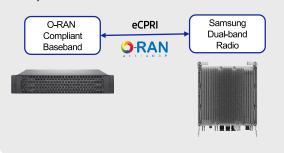
Samsung's AWS/PCS macro radio can support each incumbent CPRI interface as well as advanced eCPRI interfaces. This feature provides installable options for both legacy LTE networks and added NR networks.



O-RAN Compliant

A standardized O-RAN radio can help in implementing costeffective networks, which are capable of sending more data without compromising additional investments.

Samsung's state-of-the-art O-RAN technology will help accelerate the effort toward constructing a solid O-RAN ecosystem.



Optimum Spectrum Utilization

The number of required carriers varies according to site (region). Supporting many carriers is essential for using all frequencies that the operator has available.

The new AWS/PCS dual-band radio can support up to 3 carriers in the PCS (1.9GHz) band and 4 carriers in the AWS (2.1GHz) band, respectively.



Supports up to 7 carriers

Brand New Features in a Compact Size

Samsung's AWS/PCS macro radio offers several features, such as dual connectivity for baseband for both CDU and vDU, O-RAN capability, more carriers and an enlarged PCS spectrum, combined into an incumbent radio volume of 36.8L.



2 FH connectivity O-RAN capability

> More carriers and spectrum

Same as an incumbent radio volume



Technical Specifications

Item	Specification
Tech	LTE/NR
Brand	B25(PCS), B66(AWS)
Frequency Band	DL: 1930 – 1995MHz, UL: 1850 – 1915MHz DL: 2110 – 2200MHz, UL: 1710 – 1780MHz
RF Power	(B25) 4 × 40W or 2 × 60W (B66) 4 × 60W or 2 × 80W
IBW/OBW	(B25) 65MHz / 30MHz (B66) DL 90MHz, UL 70MHz / 60MHz
Installation	Pole, Wall
Size/ Weight	14.96 x 14.96 x 10.04inch (36.8L) / 74.7lb

SAMSUNG

700/850MHZ MACRO RADIO

DUAL-BAND AND HIGH POWER FOR MACRO COVERAGE

Samsung's future proof dual-band radio is designed to help effectively increase the coverage areas in wireless networks. This 700/850MHz 4T4R dual-band radio has 4Tx/4Rx to 2Tx/2Rx RF chains options and a total output power of 320W, making it ideal for macro sites.

Model Code

RF4440d-13A

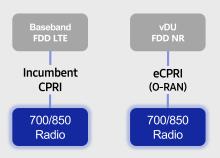




Points of Differentiation

Continuous Migration

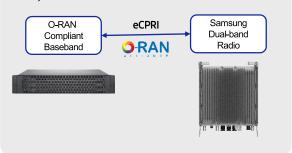
Samsung's 700/850MHz macro radio can support each incumbent CPRI interface as well as an advanced eCPRI interface. This feature provides installable options for both legacy LTE networks and added NR networks.



O-RAN Compliant

A standardized O-RAN radio can help when implementing cost-effective networks because it is capable of sending more data without compromising additional investments.

Samsung's state-of-the-art O-RAN technology will help accelerate the effort toward constructing a solid O-RAN ecosystem.



Optimum Spectrum Utilization

The number of required carriers varies according to site (region). The ability to support many carriers is essential for using all frequencies that the operator has available.

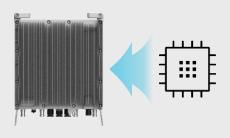
The new 700/850MHz dual-band radio can support up to 2 carriers in the B13 (700MHz) band and 3 carriers in the B5 (850MHz) band, respectively.



Secured Integrity

Access to sensitive data is allowed only to authorized

The Samsung radio's CPU can protect root of trust, which is credential information to verify SW integrity, and secure storage provides access control to sensitive data by using dedicated hardware (TPM).





Technical Specifications

Item	Specification
Tech	LTE / NR
Brand	B13(700MHz), B5(850MHz)
Frequency Band	DL: 746 – 756MHz, UL: 777 – 787MHz DL: 869 – 894MHz, UL: 824 – 849MHz
RF Power	(B13) 4 × 40W or 2 × 60W (B5) 4 × 40W or 2 × 60W
IBW/OBW	(B13) 10MHz / 10MHz (B5) 25MHz / 25MHz
Installation	Pole, Wall
Size/ Weight	14.96 x 14.96 x 9.05inch (33.2L) / 70.33 lb

Specifications

The table below outlines the main specifications of the RRH.

Table 1. Specifications

Item	RT4401-48A				
Air Technology	LTE				
Band	Band 48 (3.5 GHz)				
Operating Frequency (MHz)	3550 to 3700				
RF Chain	4TX/4RX				
Input Power	-48 V DC (-38 to -57 V DC, 1 SKU), with clip-on AC-DC converter (Option)				
Dimension (W × D × H) (mm)	8.55 in. (217.4) × 4.15 in. (105.5) × 13.91 in. (353.5) * RRH only				
	11.39 in. (289.4) × 5.45 in. (138.5) × 16.16 in. (410.5) * with Clip-on antenna, AC-DC power unit				
Cooling	Natural convection				
Unwanted Emission	3GPP 36.104 Category A				
	[B48]: FCC 47 CFR 96.41 e)				
Spectrum Analyzer	TX/RX Support				
Antenna Type	Integrated (Clip-on) antenna (Option),				
	External antenna (Option)				
Operating Humidity	5 to 100 [%] (RH), condensing, not to exceed 30 g/m ³ absolute humidity				
Altitude	-60 to 1,800 m				
Earthquake	Telcordia Earthquake Risk Zone4 (Telcordia GR-63-CORE)				
Vibration in Use	Office Vibration				
Transportation Vibration	Transportation Vibration				
Noise	Fanless (natural convection cooling)				
Wind Resistance	Telcordia GR-487-CORE, Section 3.34				
EMC	FCC Title 47, CFR Part 96				
Safety	UL 60950-1 2nd ED				



Item	RT4401-48A
	UL 62368-1
	UL 60950-22
RF	FCC Title 47, CFR Part 96

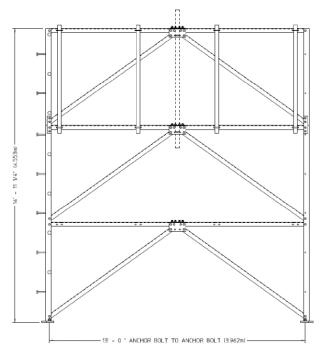
The table below outlines the AC/DC power unit specifications of the RRH system.

ATTACHMENT 4



20 Alexander Drive, 2nd Floor Wallingford, CT 06492

STRUCTURAL ANALYSIS BLOOMFIELD 4 CT



Address:

1300 HALL BOULEVARD BLOOMFIELD, CT 06002

LOCATION CODE: 684872

Date:

JUNE 2, 2022 (REVISION 0)



June 2, 2022



20 Alexander Drive, 2nd Floor Wallingford, CT 06492

RE:

Site Name: Bloomfield 4 CT

Site Location Code: 684872

Site Address: 1300 Hall Boulevard, Bloomfield, CT 06002

To whom it may concern:

Chappell Engineering Associates, LLC has performed a structural analysis of the proposed Verizon roof-mounted antenna frame at the above-referenced address at approximately 90ft AGL to analyze the effect of the proposed Verizon antenna installation on the subject frame.

The proposed antenna support structure will consist of a triangular 13ft x 13ft x 15ft high antenna frame supporting nine (9) individual antenna mounting pipes. Our analysis has considered the following total major equipment loads indicated on the antenna design summary (included in this report) to be installed on the proposed low-profile antenna frame.

<u>Appurtenance</u>	Size (HxWxD) (in)	<u>Weight</u>	Location	<u>Status</u>
(3) NHH-65B-R2B Panel Antennas	72.0x11.9x7.1	43.7lbs	Face of Mount	Proposed
(3) NHHSS-65B-R2B R2BT4 Panel Antennas	72.0x11.9x7.1	48.1lbs	Face of Mount	Proposed
(3) MT6407-77A Panel Antennas	35.2x16.1x5.6	87lbs	Face of Mount	Proposed
(3) 700/850 mHz RRH	15.0x15.0x9.0	70.3lbs	Face of Mount	Proposed
(3) 1900/2100 mHz RRH	15.0x15.0x10.0	84.4lbs	Face of Mount	Proposed
(3) RT4401-48A RRH	13.9x8.6x4.2	18.6lbs	Face of Mount	Proposed
(1) Fiber Junction Box	29.6x16.5x12.6	32.0lbs	Face of Mount	Proposed

The proposed antennas and ancillary hardware are shown on the enclosed Zoning Drawings and RF Data Sheets.

We have modeled the triangular antenna frame under both wind and wind/ice loads. Our analysis and results are included in this report.

Based upon our analysis of the antenna mounts being proposed, the proposed Valmont 3-Leg Roof Frame (Product Number 31-92103) has adequate capacity to support the proposed antenna configuration as shown on the zoning drawings. The maximum percentage stress capacity as determined by our analysis are the upper horizontal L's with a capacity of 41%. Our analysis assumes the proposed mount will be installed and maintained according to the manufacturers' recommendations.

If you have any questions regarding this matter, please do not hesitate to call.

Clement J Salek, P.E.
CJS/cjs



CHAPPELL ENGINEERING ASSOCIATES, LLC

ARCHITECT/ENGINEER:

R.K. EXECUTIVE CENTRE 201 BOSTON POST ROAD WEST SUITE 101 MARIEBORUCH, MA 01752 (508) 481—7400 www.choppellengineering.com

Verizon

20 ALEXANDER DRIVE, WALLINGFORD, CT 06492

BLOOMFIELD 4 CT

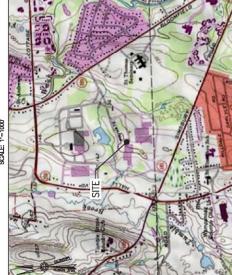
1300 HALL BOULEVARD BLOOMFIELD, CT 06002 PROJECT TYPE: WIRELESS TELECOMMUNICATIONS INSTALLATION ON ROOFTOP OF EXISTING (4)-STORY STEEL FRAMED BUILDING

SITE INFORMATION:

PROPERTY OWNER:	THE ATRIUM CT LLC 2 PARK AVENUE, 17TH FLOOR NEW YORK, NY 10166
APPLICANT:	CELLCO PARTNERSHIP (dba VERIZON WIRELESS) 20 ALEXANDER DRIVE WALLINGFORD, CT 06492
SITE ADDRESS:	1300 HALL BOULEVARD BLOOMFIELD, CT 06002
COUNTY:	HARTFORD COUNTY, CONNECTICUT
SITE CONTROL POINT:	SOUTHEAST CORNER OF EXISTING MECHANICAL PENTHOUSE
	N 41°-48°-30,48° (41,808467°) (NAD '83) W 72°-44°-36,55° (72,743486°) (NAD '83)
ARCHITECT / ENGINEER:	CHAPPELL ENGINEERING ASSOCIATES, LLC 201 BOSTON POST ROAD WEST, SUITE 101 MADI BOSTON ON A 2750

SCALE: 1"=1000

VICINITY MAP



DRIVING DIRECTIONS

FROM WALLINGFORD, TAKE 191 NORTH, TAKE THE CT-218 BOIT TOWARD WINDSOFREGORIELD, THEN FONTO CTS 188 WEST, USE THE LEFT STANDS THE HELD STRANGS TO ONTO CTS 198 SOUTH, TURN RIGHT THEN RIGHT AGAIN. THE STIFLE IS DON'TO STRANGS THE HELD.

SHEET INDEX

DATE

ENGINEER/LAND SURVEYOR

WG.	DESCRIPTION	Ä.
5	TITLE SHEET	4
10	LOCATION PLAN	4
05	PROPERTY PLAN	4
5	PART ROOF PLAN AND SITE DETAILS	4
88	NORTH BUILDING ELEVATION AND ENLARGED PART NORTH BUILDING ELEVATION	4
Š	ANTENNA DETAILS AND ANOUT ADVIDAGNT COCCUCIONATIONS	,

PROJECT DESCRIPTION

PARTY BY: NWC SHENGE BY: NWC SHENGE BY: NWC SHENGE BY: NWC 2/9/22

T01

DO NOT SCALE DRAWINGS

TITLE SHEET

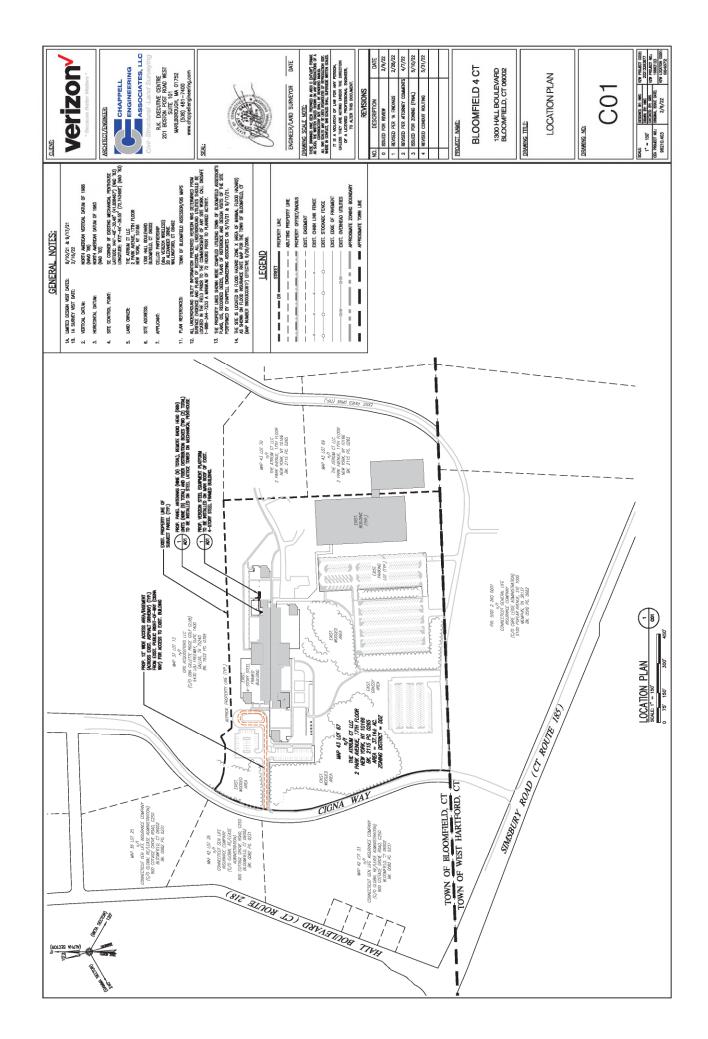
BLOOMFIELD 4 CT 1300 HALL BOULEVARD BLOOMFIELD, CT 06002

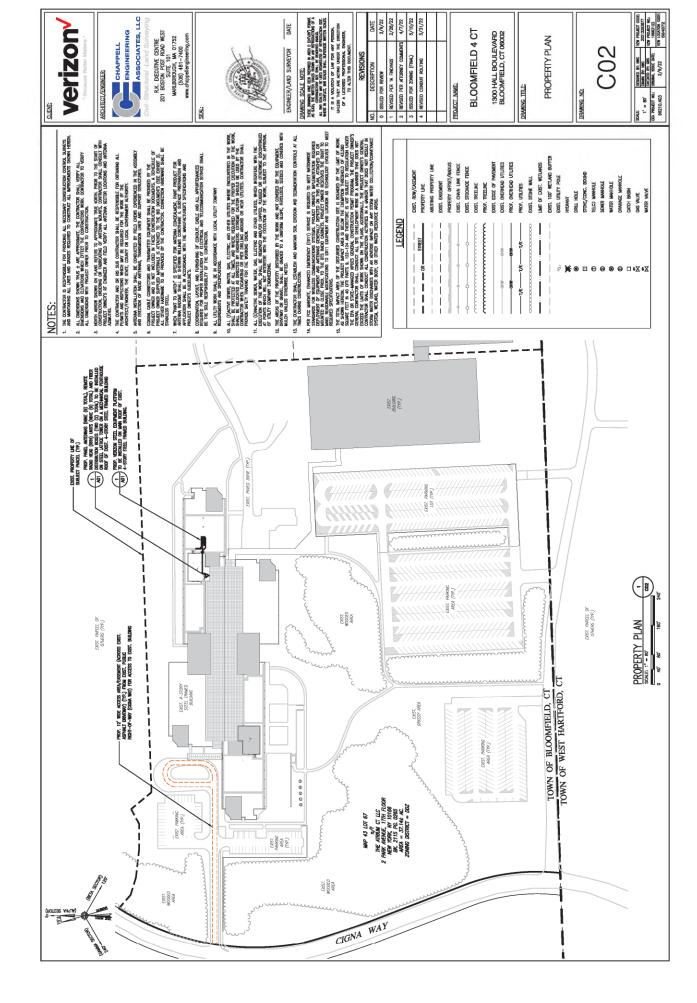
REVISED PER ATTORNEY COMMENTS

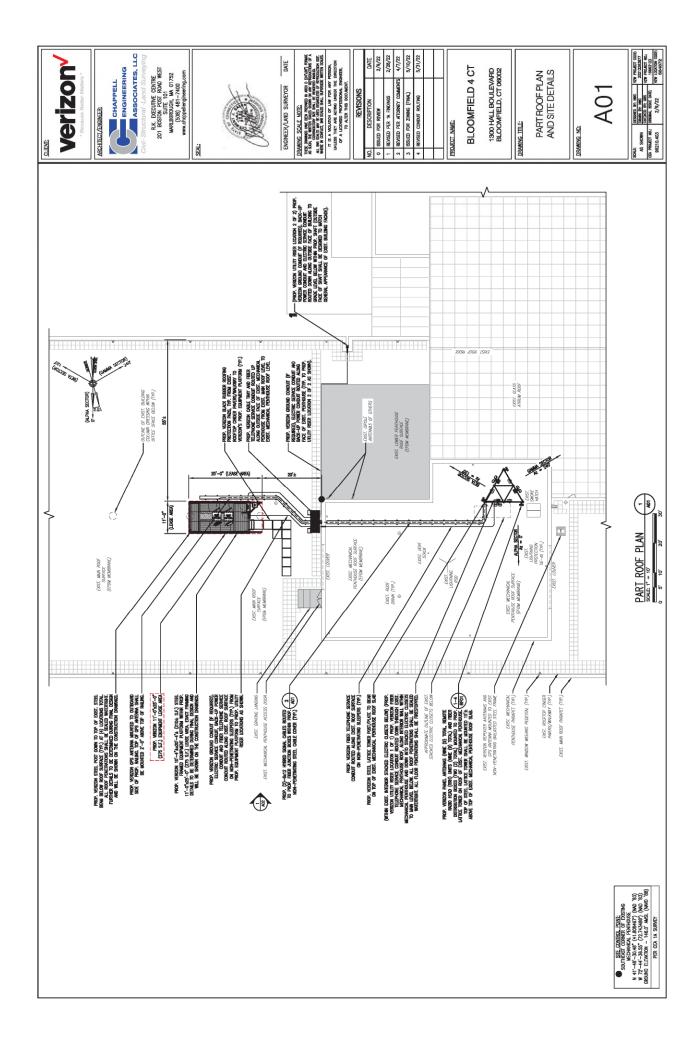
ISSUED FOR ZOHING (FINAL) REVISED PER 1A FINDINGS

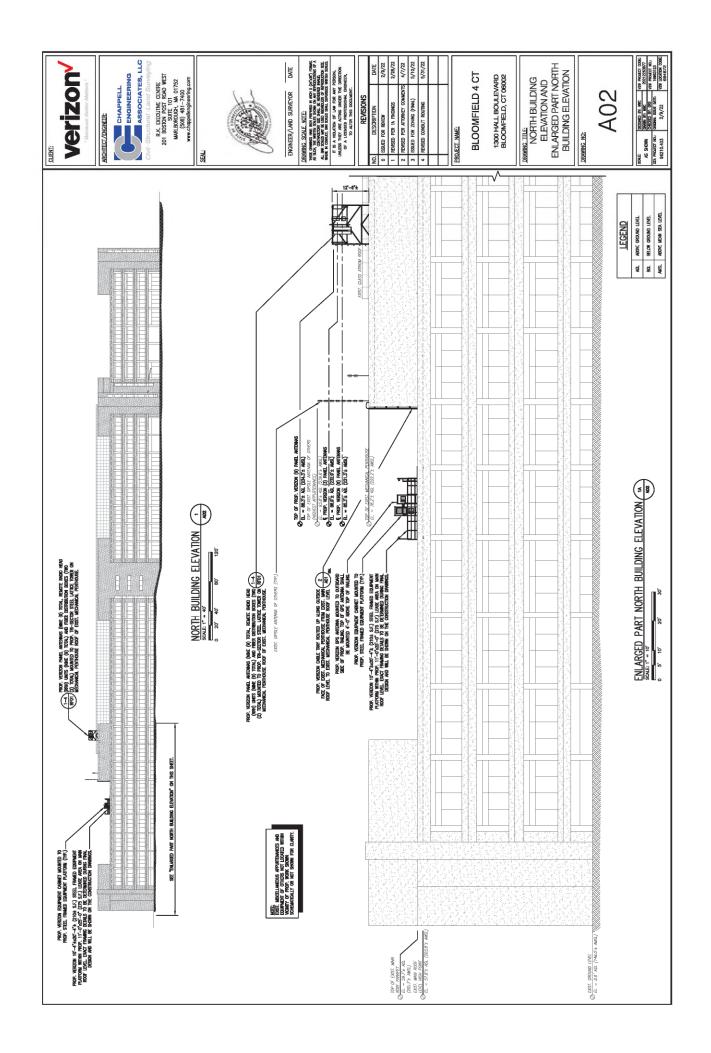
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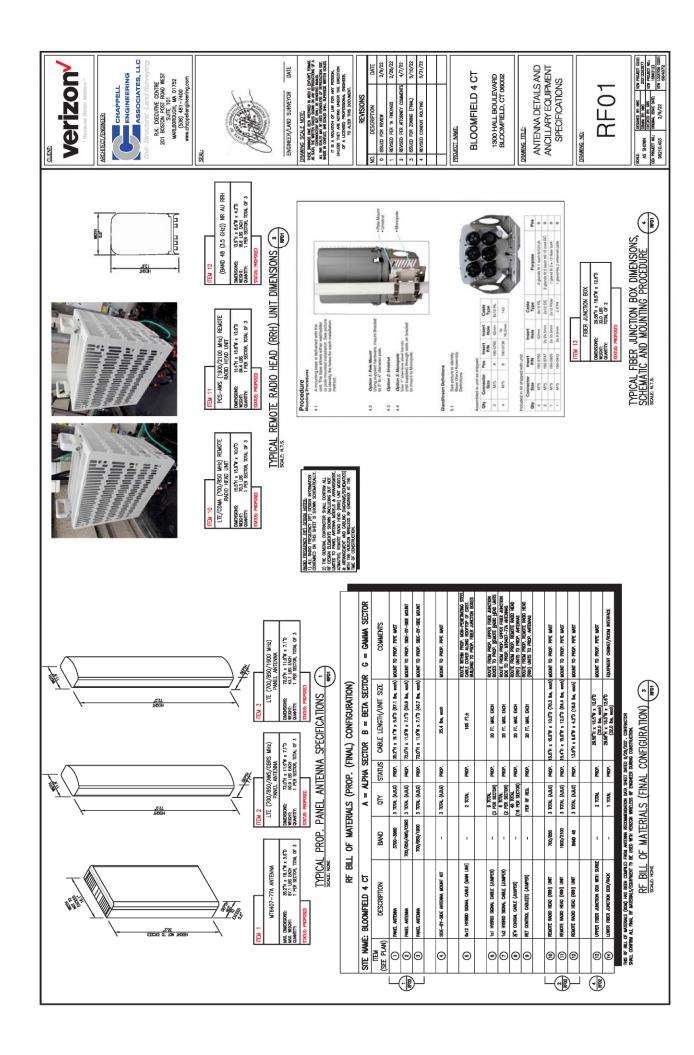
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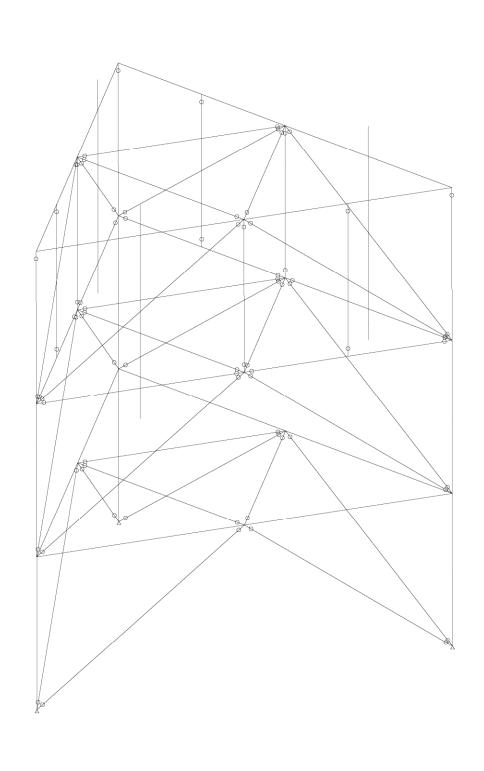




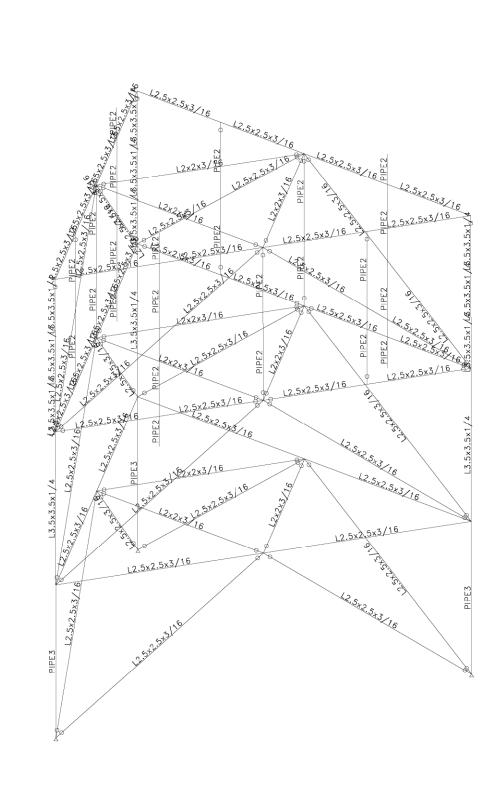




Verizon	Bloomfield	СТ	Antenna	Frame	962	210.403	
							X3 >X2
SCALE = 1	:34	L	JNITS: kip ft			DATE: 5/23/22	>X1



Verizon	Bloomfield	CT Antenna	Frame	96210.403	
					X3 >X2
SCALE =	1:34	UNITS: kip ft		DATE: 5/23/22	— >X1



Page: 1 Date: 5/23/22

Verizon Bloomfield CT Antenna Frame 96210.403

Load no. 1: Front No Ice (units - kips ft.)

/ JOINT LOADS

Prepared by:

FX2 -0.13 FX3 -0.05 N 68 69

FX2 -0.045 FX3 -0.044 N 49 51

FX2 -0.035 FX3 -0.044 N 47 48 53 55

FX2 -0.11 FX3 -0.05 N 66 67 63 65

/ JOINT LOADS

FX2 -0.03 FX3 -0.084 N 82 81 83 84 86 85

/ END

FORCE SUMMATION

FX1=0. kip

FX2=-1.11 kip

FX3=-1.068 kip

Load no. 2: Side No Ice (units - kips ft.)

/ JOINT LOADS

/ JOINT LOADS

/ JOINT LOADS

FX1 -0.035 FX3 -0.044 N 49 51

FX1 -0.11 FX3 -0.05 N 68 69

FX1 -0.11 FX3 -0.05 N 66 67 63 65

FX1 -0.03 FX3 -0.044 N 47 48 53 55

FX1 -0.03 FX3 -0.084 N 82 81 83 84 86 85

/ END

FORCE SUMMATION

FX1=-1.03 kip

FX2=0. kip

FX3=-1.068 kip

Load no. 3: Front Ice (units - kips ft.)

/ JOINT LOADS

/ JOINT LOADS

/ JOINT LOADS

FX2 -0.05 FX3 -0.16 N 68 69

FX2 -0.04 FX3 -0.016 N 66 67 63 65

FX2 -0.015 FX3 -0.075 N 49 51

FX2 -0.015 FX3 -0.075 N 47 48 53 55

FX2 -0.01 FX3 -0.123 N 82 81 83 84 86 85

/ END

FORCE SUMMATION

FX1=0. kip

FX2=-0.41 kip

FX3=-1.572 kip

Page: 2 **Date:** 5/23/22

Verizon Bloomfield CT Antenna Frame 96210.403

Prepared by:

Load no. 4: Side Ice (units - kips ft.)

/ JOINT LOADS

/ JOINT LOADS

/ JOINT LOADS

/ JOINT LOADS

FX1 -0.04 FX3 -0.16 N 68 69

FX1 -0.04 FX3 -0.16 N 66 67 63 65

FX1 -0.015 FX3 -0.075 N 49 51

FX1 -0.015 FX3 -0.075 N 47 48 53 55

FX1 -0.01 FX3 -0.123 N 82 81 83 84 86 85

/ END

FORCE SUMMATION

FX1=-0.39 kip

FX2=0. kip

FX3=-2.148 kip

Load no. 5: Selfweight (units - kips ft.)

/ BEAM LOADS

SELF X3 -1. B 1 TO 36 52 TO 60 81 TO 137

/ END

FORCE SUMMATION

FX1=0. kip

FX2=0. kip

FX3=-1.4249 kip

Load no. 6: Front Frame Ice (units - kips ft.)

/ BEAM LOADS

DIST GL FX2 -0.0015 B 1 TO 36 52 TO 60 81 TO 137

/ END

FORCE SUMMATION

FX1=0. kip

FX2=-0.6287 kip

FX3=0. kip

Page: 3 **Date:** 5/23/22

Verizon Bloomfield CT Antenna Frame 96210.403

Prepared by:

rioparoa by:

Load no. 7: Side Frame Ice (units - kips ft.)

/ BEAM LOADS

DIST GL FX1 -0.0015 B 1 TO 36 52 TO 60 81 TO 137

/ END

FORCE SUMMATION

FX1=-0.6287 kip

FX2=0. kip

FX3=0. kip

Load no. 8: Front Frame No Ice (units - kips ft.)

/ BEAM LOADS

DIST GL FX2 -0.0045 B 1 TO 36 52 TO 60 81 TO 137

/ END

FORCE SUMMATION

FX1=0. kip

FX2=-1.8861 kip

FX3=0. kip

Load no. 9: Side Frame No Ice (units - kips ft.)

/ BEAM LOADS

/ BEAM LOADS

DIST GL FX1 -0.0045 B 1 TO 36 52 TO 60 81 TO 137

/ END STATIC

FORCE SUMMATION

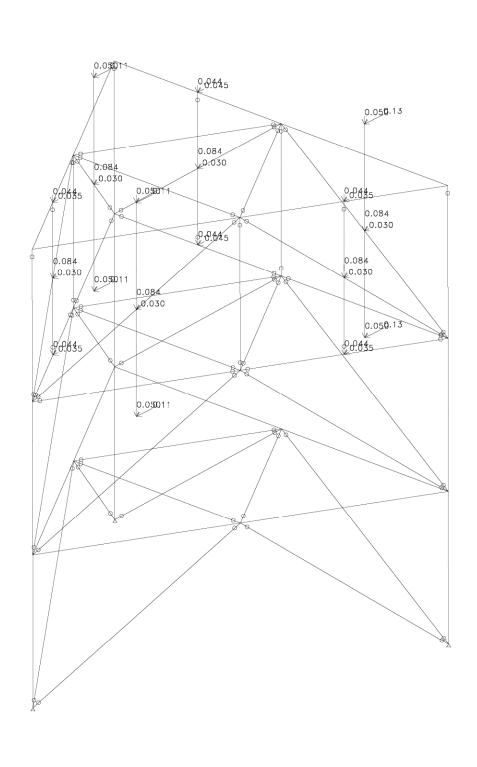
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FX2=0. kip

FX3=0. kip

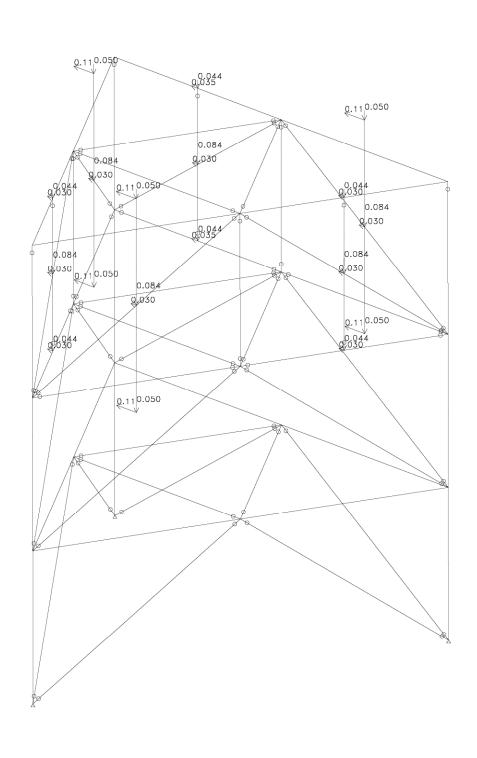
Verizon Bloomfield CT Antenna Frame 96210.403	
Load 1: Front No Ice	X3 X2 X1
	- / / I

UNITS: kip ft



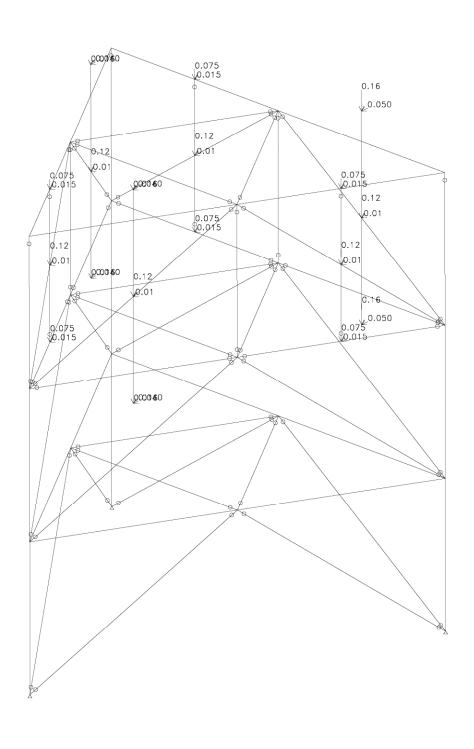
Verizon Bloomfield CT Antenna Frame 96210.403	
Load 2: Side No Ice	X3 >X2 >X1
, ,	- /\ I

UNITS: kip ft



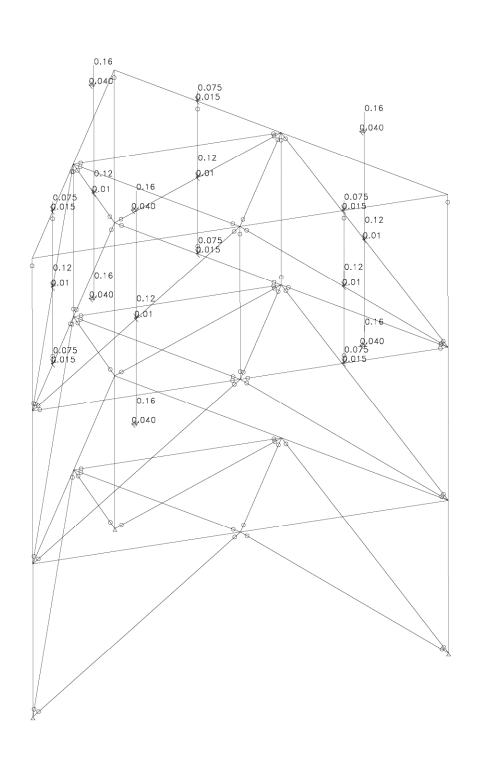
Verizon Bloomfield CT Antenna Frame 96210.403	
Load 3: Front Ice	X3 X2 X1
, ,	- /\ I

UNITS: kip ft



Verizon Bloomfield CT Antenna Frame 96210.403	
Load 4: Side Ice	X3 X2 X1
	- /\ I

UNITS: kip ft



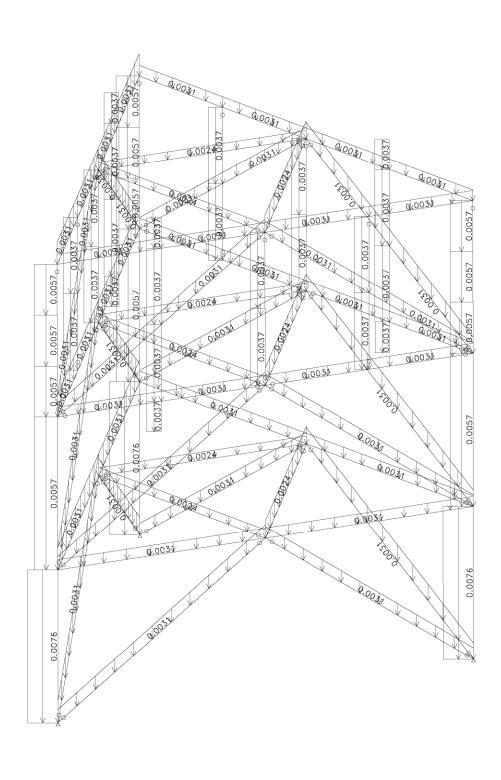
Verizon Bloomfield CT Antenna Frame 96210.403 Х3 Load 5: Selfweight

UNITS: kip ft

SCALE = 1:34

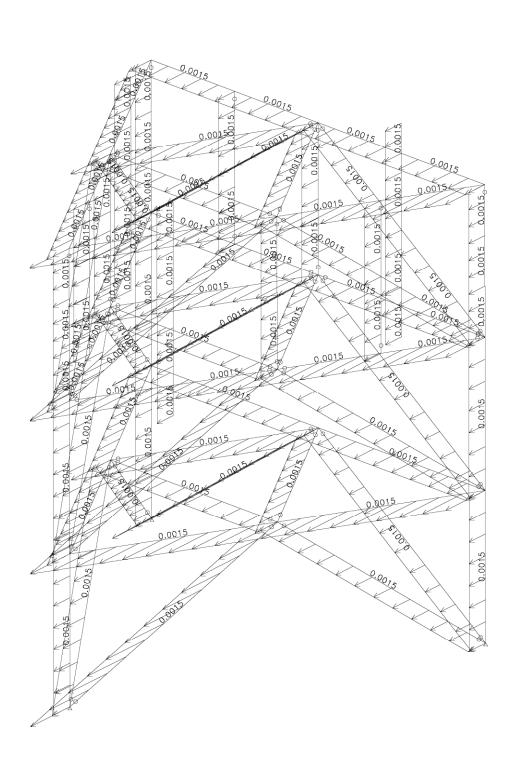
DATE: 5/23/22

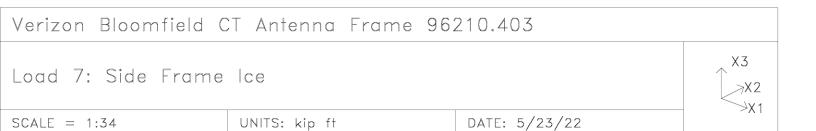


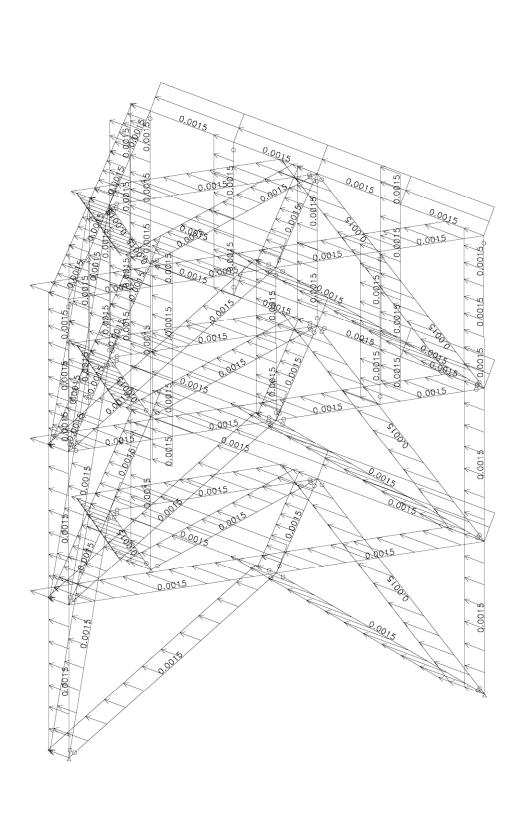


Verizon Bloomfield CT Antenna Frame 96210.403	
Load 6: Front Frame Ice	X3 X2

UNITS: kip ft

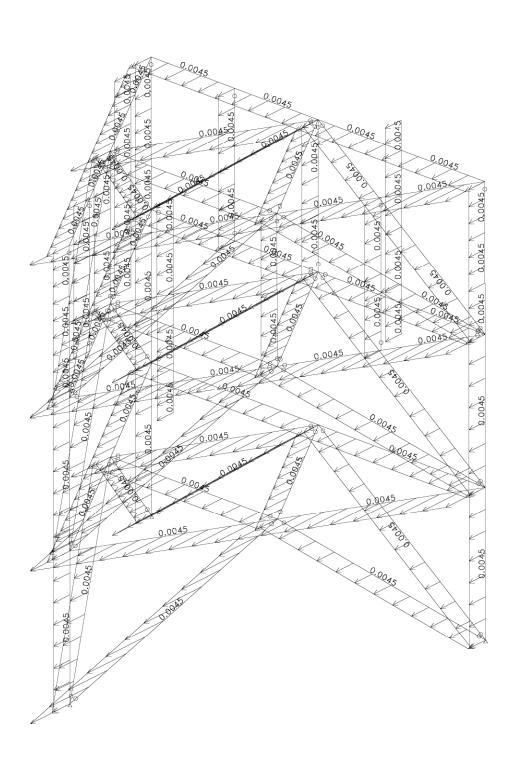






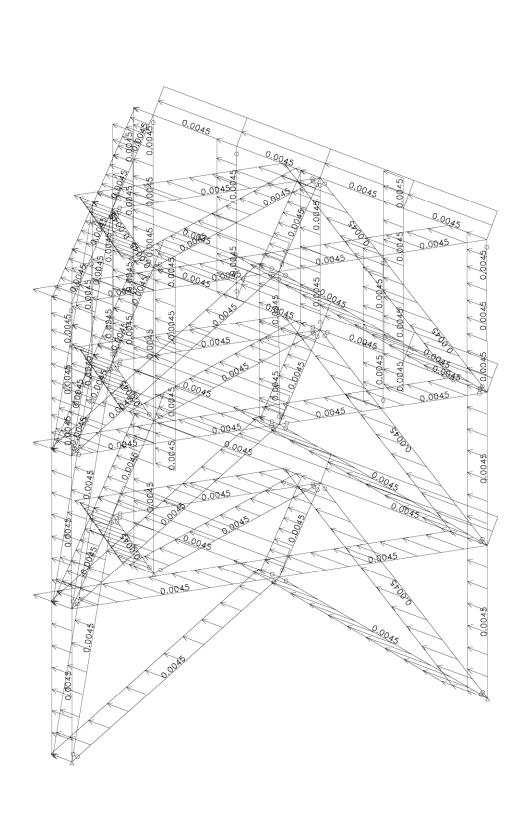
Verizon Bloomfield CT Antenna Frame 96210.403	
Load 8: Front Frame No Ice	X3 X2 X1

UNITS: kip ft

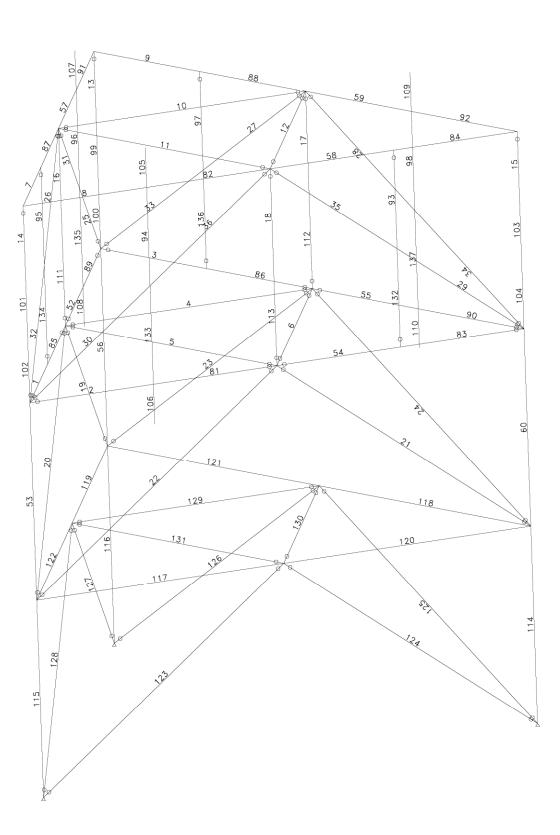


Verizon Bloomfield CT Antenna Frame 96210.403	
Load 9: Side Frame No Ice	X3 X2 X1

UNITS: kip ft



Verizon	Bloomfield	СТ	Antenna	Frame	96210.403	
						X3 X2 X1
SCALE = 1	:28			DATE: 5/	23/22	



Prepared by:

Code: AISC-LRFD Page: 3 Date: 5/23/22

		Resu	ılts	Su	m m a	ry	Tab	le			
						<u>.</u>		APAC	ITY	0	
Beam	Section	Com	Defl L/	Slen	Axial	Dir	Shear	Mom	LTB	Combined Axial+Mom	
1	L 2.5x2.5x3/16	2	1649	158	-0.03	MJ	0.00	0.10	0.10	0.20	
2	L 2.5x2.5x3/16	2	937	158	0.02	MJ	0.00	0.09	0.00	0.34	
3	L 2.5x2.5x3/16	1	1451	315	-0.13	MJ	0.01	0.20 0.19	0.00	0.41	**1
4	L 2x2x3/16	2	3317	198	-0.03	MJ	0.01 0.00 0.00	0.27	0.00	0.06	
5	L 2x2x3/16	1	2977	198	0.01	MJ	0.00	0.03 0.02 0.04	0.00 0.04 0.00	0.07	
6	L 2x2x3/16	2	3317	195	-0.05	MJ	0.00	0.02	0.04	0.09	
7	L 2.5x2.5x3/16	2	1967	158	-0.02	MJ	0.01 0.01	0.16 0.12	0.17 0.00	0.25	
8	L 2.5x2.5x3/16		1583	158	-0.01	MJ	0.01 0.01	0.22 0.14	0.23 0.00	0.29	
9	L 2.5x2.5x3/16		2806	238	-0.07	MI	0.01 0.01	0.21 0.18		0.37	
10	L 2x2x3/16	2	3317	198	-0.04		0.00	0.02 0.03	0.04	0.07	
11	L 2x2x3/16	1	2977	198	0.01	MJ	0.00	0.02 0.04	0.04	0.07	
12	L 2x2x3/16		3317	195	-0.06		0.00	0.02 0.03	0.04 0.00	0.09	
	PIPE 2		9999	74	-0.01	MI	0.00	0.01 0.01	0.01 0.00	0.01	
	PIPE 2		9999	74	-0.01	MI	0.00	0.01	0.01	0.01	
	PIPE 2	1	9999	74	-0.01	MI	0.00	0.01 0.01	0.01	0.01	
19	L 2.5x2.5x3/16	1	2907	199	-0.13		0.00	0.04 0.03	0.05	0.12	
20	L 2.5x2.5x3/16	1	2834	199	-0.20	MJ	0.00	0.04 0.03	0.04	0.13	
21	L 2.5x2.5x3/16	2	2833	199	-0.02	MJ	0.00	0.04 0.03	0.05 0.00	0.08	
22	L 2.5x2.5x3/16	1	3820	197	-0.20		0.00	0.02 0.03	0.04	0.23	
23	L 2.5x2.5x3/16	2	3016	197	-0.22	MJ	0.00	0.02		0.22	
24	L 2.5x2.5x3/16	2	2981	199	-0.06	MJ	0.00	0.05 0.04	0.05	0.09	
25	L 2.5x2.5x3/16	4	1752	199	-0.07	MJ	0.00	0.09 0.07	0.10	0.16	
26	L 2.5x2.5x3/16	2	1929	199	-0.10	MJ	0.00	0.08	0.08	0.14	
27	L 2.5x2.5x3/16	1	1845	183	-0.11	MJ	0.00	0.07 0.07	0.08	0.15	
28	L 2.5x2.5x3/16	3	1722	199	-0.05	MJ	0.00	0.09	0.10	0.16	
29	L 2.5x2.5x3/16	3	1851	199	-0.03	MJ	0.00	0.08 0.05	0.09	0.12	
30	L 2.5x2.5x3/16	4	1744	182	-0.10	MJ	0.00 0.00	0.09 0.07	0.10 0.00	0.16	
52	L 2.5x2.5x3/16	2	933	158	-0.05		0.01 0.01	0.20	0.23	0.34	
53	L 3.5x3.5x1/4	1	9999	139	-0.05	MJ	0.00	0.20 0.00 0.01	0.00 0.01 0.00	0.03	
54	L 2.5x2.5x3/16	2	1626	158	-0.05	MJ	0.00	0.11	0.00	0.19	
	L 3.5x3.5x1/4 L 2.5x2.5x3/16	4 4	9999 1602	141 129	-0.04 -0.02	MJ	0.00	0.01 0.22	0.01 0.23	0.03 0.29	
					3.02		0.01	0.13	0.00		

Prepared by:

Code: AISC-LRFD Page: 4 Date: 5/23/22

		Resu	ılts	Su	m m a	r y	T a b	l e			
							C	APAC	ITY		
Beam	Section	Com	Defl L/	Slen	Axial	Dir	Shear	Mom	LTB	Combined Axial+Mom	
58	L 2.5x2.5x3/16	2	1826	138	-0.02		0.01 0.01	0.16 0.11	0.17 0.00	0.23	
	L 3.5x3.5x1/4 PIPE 2		9999 1887	152 76	-0.03 0.00	MJ	0.00 0.00 0.01	0.00 0.05 0.08	0.00 0.05 0.00	0.03 0.12	
95	PIPE 2	4	2055	76	0.00		0.00	0.05 0.07	0.05	0.11	
97	PIPE 2	3	2119	76	0.00	MJ	0.01	0.08	0.08	0.09	
105	PIPE 2	2	1743	44	-0.01	MJ	0.01 0.01	0.07	0.07 0.00	0.18	
107	PIPE 2	2	1765	44	-0.01		0.01 0.01	0.07 0.10	0.07 0.00	0.18	
109	PIPE 2	1	1345	45	-0.01	MJ	0.01	0.13 0.07	0.13	0.15	
114	PIPE 3	3	9999	52	-0.01		0.00	0.00		0.01	
	PIPE 3	1		51	-0.04	MI	0.00	0.00	0.00	0.04	
	PIPE 3		9999	51	-0.04		0.00	0.00	0.00	0.04	
117	L 2.5x2.5x3/16	1	9999	315	-0.18		0.00	0.01	0.02	0.12	***
118	L 2.5x2.5x3/16	2	9999	315	-0.21	MJ	0.00 0.00 0.00	0.02 0.02 0.02	0.00 0.03 0.00	0.23	***
119	L 2.5x2.5x3/16	1	9999	315	-0.19	MJ	0.00	0.01 0.02	0.02	0.13	***
123	L 2.5x2.5x3/16	1	3820	197	-0.21	MJ	0.00	0.02	0.04 0.00	0.24	
124	L 2.5x2.5x3/16	2	2833	199	0.03	MJ	0.00	0.04 0.03	0.05	0.09	
125	L 2.5x2.5x3/16	2	2981	199	0.04		0.00	0.05 0.04	0.05 0.00	0.08	
126	L 2.5x2.5x3/16	2	3016	197	-0.24	MJ	0.00	0.02	0.04	0.24	
127	L 2.5x2.5x3/16	1	2907	199	-0.12	MJ	0.00	0.04	0.05	0.12	
128	L 2.5x2.5x3/16	1	2834	199	-0.21	MJ	0.00	0.04 0.03	0.04 0.00	0.24	
129	L 2x2x3/16	2	3317	198	-0.01	MJ	0.00	0.02		0.06	
130	L 2x2x3/16	2	3317	191	-0.02	MJ	0.00	0.02 0.03	0.04	0.07	
131	L 2x2x3/16	1	2977	198	0.01	MJ	0.00	0.02	0.04 0.00	0.07	

Verizon Bloomfield CT Antenna Frame 96210.403	
	X3 X2 X1
SCALE = 1:27 DATE: 6/ 1/22	- X I
127	

115

Actual/allowable Maximum result

Prepared by:

Page: 3 Date: 5/23/22

Code: AISC-LRFD

Detailed Results Table for Beam 3 - 90

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

X2 (Major axis) 2 3 Beam: 3, 86, 55, 90 -13.00

CONSTRAINTS

DESIGN DATA

- Sections : Check

-Kx = 1.00- Ky = 1.00

- Steel Grade: A36

- Allow. Slend.: 240 (compr.) 300 (tens.) - Allowable Deflection: 1/400

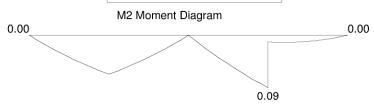
- Tension Area Reduction Factor: 1.00

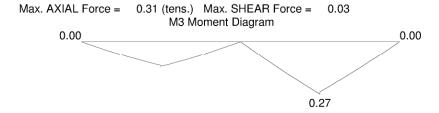
- Building type : Unbraced

Section: L 2.5x2.5x3/16

0.55 ly = 0.55 in4 Sx = 0.30 Sy = 0.30 in3 Area = 0.90Ix = 2.50 b = 2.50 in t = 0.19 ey = 1.82 in ex = 1.82 in0.01 Cw = 0.00 in 6 lv = 0.22 in 4

DESIGN COMBINATION = 1





Max. AXIAL Force = 0.31 (tens.) Max. SHEAR Force = 0.09

SECTION CLASSIFICATION: *** SLENDER ***

Limiting Ratios: Compact Non-Compact d/t = 13.2312.8 12.8

< b/t = 13.2315.3 <

(Fy= 36.0)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V2 Shear (F2-1)	Vu/(.9*Vn)<1.00 Vn=0.6*Fy*Av	Av = 0.43	Vu = 0.09 Vn = 9.20	0.01
M3 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.30 QS =0.986	M = 0.27 Mn = 1.14	0.27

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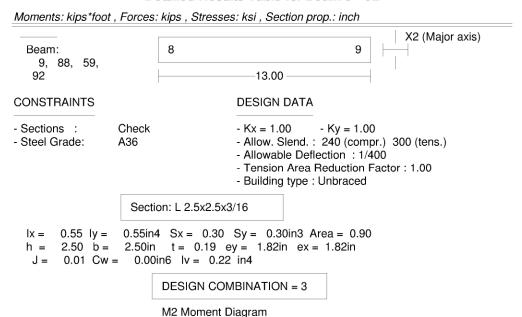
Code: AISC-LRFD Page: 4 Date: 5/23/22

Detailed Results Table for Beam 3 - 90

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M2 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.30 QS =0.986	M = 0.09 Mn = 1.14	0.09
Deflection	defl. L / 400 < 1.00		defl = 0.10749	0.28
Axial Force (D1-1)	Pu < 1.00 0.90AgFy	(kL/r)x =200 (kL/r)y =315	Pu = 0.31 Ag = 0.90 Fy = 36.00	0.01
Lateral Torsional Buckling (5-6)	M < 1.00 0.9Mn Critical Segment from Segment End Momen			0.29
Combined Forces (tension) (H1-1b)	Pu + Mux Muy 2φPn φMnx φMny < 1.00		Mux = 0.09 Muy = 0.27	0.41

Detailed Results Table for Beam 9 - 92



0.00

0.22

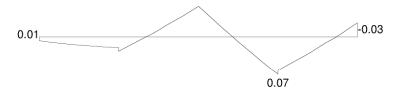
Prepared by:

Code: AISC-LRFD Page: 5 Date: 5/23/22

Detailed Results Table for Beam 9 - 92

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

Max. AXIAL Force = 0.02 (tens.), -0.13 (compr.) Max. SHEAR Force = 0.10 M3 Moment Diagram



Max. AXIAL Force = 0.02 (tens.), -0.13 (compr.) Max. SHEAR Force = 0.04

SECTION CLASSIFICATION: *** SLENDER ***

Limiting Ratios: Compact Non-Compact

d/t= 13.23 < 12.8 (Fy= 36.0)

b/t= 13.23 < 15.3

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M3 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.30 QS =0.986	M = 0.07 Mn = 1.14	0.07
V3 Shear (F2-1)	Vu/(.9*Vn)<1.00 Vn=0.6*Fy*Av	Av = 0.43	Vu = 0.10 Vn = 9.20	0.01
M2 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.30 QS =0.986	M = 0.22 Mn = 1.14	0.21
Deflection	defl. L / 400 < 1.00		defl = 0.05112	0.13
Axial Force (4-1),(4-2)	Pu	(kL/r)x = 151 (kL/r)y = 238 $\lambda c \sqrt{Q} = 2.66$ Q = 0.90	Pu = 0.13 Ag = 0.90 Fcr = 4.45	0.04
Lateral Torsional Buckling (5-6)	M < 1.00 0.9Mn Critical Segment from Segment End Momen		M = 0.22 Mn = 0.89 My = 0.91 Mob = 1.76 flange	0.27
Combined Forces (compress.) (H1-1b)	$\frac{Pu}{2\phi Pn} + \frac{Mux}{\phi Mnx} + \frac{Muy}{\phi Mny}$ < 1.00	Cmx = 1.00 Cmy = 1.00 Pex = 11.19 Pey = 4.51	Mux = 0.22 Muy = 0.07 B1x = 1.01 B1y = 1.03	0.37

Prepared by:

Page: 6 Date: 5/23/22

Code: AISC-LRFD

Detailed Results Table for Beam 14

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

X2 (Major axis) 7 14 Beam: 53, 102, 101, 10.00

CONSTRAINTS

DESIGN DATA

- Sections : Check -Kx = 1.00- Ky = 1.00

- Steel Grade: A36 - Allow. Slend.: 240 (compr.) 300 (tens.)

- Allowable Deflection: 1/400

- Tension Area Reduction Factor: 1.00

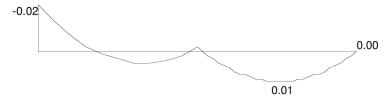
- Building type : Unbraced

Section: L 3.5x3.5x1/4

2.01 ly =2.01in4 Sx = 0.79 Sy = 0.79in3 Area = 1.69Ix = 3.50 b = 3.50 in t = 0.25 ey = 2.53 in ex = 2.53 in0.04 Cw = 0.00 in 6 Iv = 0.81 in 4

DESIGN COMBINATION = 1

M3 Moment Diagram



Max. AXIAL Force = -0.97 (compr.) Max. SHEAR Force = 0.01

SECTION CLASSIFICATION: *** SLENDER ***

Limiting Ratios: Compact Non-Compact

d/t = 14.1112.8 (Fy= 36.0)12.8

b/t = 14.1115.3 <

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M3 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.79 QS =0.962	M = 0.02 Mn = 2.98	0.01
Axial Force (4-1),(4-2)	Pu < 1.00 0.90AgFcr	(kL/r)x = 87 (kL/r)y = 137 $\lambda c \sqrt{Q} = 1.53$ Q = 1.69	Pu = 0.97 Ag = 1.69 Fcr = 13.42	0.05
Lateral Torsional Buckling (5-6)	M < 1.00 0.9Mn < 1 cm < 1.00 Critical Segment from Segment End Momen		M = 0.02 Mn = 2.68 My = 2.38 Mob = -1.00	0.01
Combined Forces (compress.) (H1-1b)	Pu + Mux Muy 2φPn φMnx φMny < 1.00	Cmx = 1.00 Cmy = 1.00 Pex = 61.75 Pey = 24.90	Mux = 0.00 Muy = 0.02 B1x = 1.02 B1y = 1.04	0.03

Prepared by:

Page: 7 **Date:** 5/23/22

Code: AISC-LRFD

Detailed Results Table for Beam 13

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

Beam: 13 8 X2 (Major axis)
56, 100, 99,
13 -10.00

CONSTRAINTS

DESIGN DATA

- Sections : Check

Check -Kx = 1.00 - Ky = 1.00

- Steel Grade: A36 - Allow. Slend.: 240 (compr.) 300 (tens.)

- Allowable Deflection: 1/400

- Tension Area Reduction Factor : 1.00

- Building type : Unbraced

Section: L 3.5x3.5x1/4

= 0.04 GW = 0.001110 IV = 0.01 1114

DESIGN COMBINATION = 4

Max. AXIAL Force = -0.87 (compr.) Max. SHEAR Force = 0.00

SECTION CLASSIFICATION: *** SLENDER ***

Limiting Ratios: Compact Non-Compact

d/t= 14.11 < 12.8 12.8

b/t= 14.11 < 15.3

(Fy= 36.0)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M2 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.79 QS =0.962	M = 0.01 Mn = 2.98	0.00
Axial Force (4-1),(4-2)	Pu < 1.00 0.90AgFcr	(kL/r)x = 88 (kL/r)y = 138 $\lambda c \sqrt{Q} = 1.55$ Q = 1.69	Pu = 0.87 Ag = 1.69 Fcr = 13.22	0.04
Lateral Torsional Buckling (5-6)	M < 1.00 0.9Mn < 1.00 Critical Segment from Segment End Momen		M = 0.01 Mn = 2.98 My = 2.38 Mob = 16.50 flange	0.00
Combined Forces (compress.) (H1-1b)	Pu + Mux Muy 2\phiPn + \phiMnx \phiMny < 1.00	Cmx = 1.00 Cmy = 1.00 Pex = 60.35 Pey = 24.54	Mux = 0.01 Muy = 0.00 B1x = 1.01 B1y = 1.04	0.03

Prepared by:

Code: AISC-LRFD Page: 8 Date: 5/23/22

Detailed Results Table for Beam 15

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

Beam: 15 9 X2 (Major axis)
60, 104, 103,
15 -10.00

CONSTRAINTS

DESIGN DATA

- Sections : Check - Kx = 1.00 - Ky = 1.00

- Steel Grade: A36 - Allow. Slend. : 240 (compr.) 300 (tens.)

- Allowable Deflection: 1/400

- Tension Area Reduction Factor: 1.00

- Building type : Unbraced

Section: L 3.5x3.5x1/4

04 OW = 0.001110 IV = 0.01 1114

DESIGN COMBINATION = 3

Max. AXIAL Force = -0.62 (compr.) Max. SHEAR Force = 0.00

SECTION CLASSIFICATION: *** SLENDER ***

Limiting Ratios: Compact Non-Compact

d/t= 14.11 < 12.8 12.8

b/t= 14.11 < 15.3

(Fy= 36.0)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
Axial Force (4-1),(4-2)	Pu < 1.00 0.90AgFcr	(kL/r)x = 89 (kL/r)y = 140 $\lambda c \sqrt{Q} = 1.57$ Q = 1.69	Pu = 0.62 Ag = 1.69 Fcr = 12.85	0.03
Lateral Torsional Buckling (5-6)	M < 1.00 0.9Mn Critical Segment from Segment End Momen			0.00
Combined Forces (compress.) (H1-1b)	Pu + Mux Muy 2φPn φMnx φMny < 1.00	Cmx = 1.00 Cmy = 1.00 Pex = 59.00 Pey = 23.85	Mux = 0.01 Muy = 0.00 B1x = 1.01 B1y = 1.03	0.02

Prepared by:

Code: AISC-LRFD Page: 9 Date: 5/23/22

Detailed Results Table for Beam 123

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

X2 (Major axis) 74 78 Beam: 123 8.20

CONSTRAINTS

DESIGN DATA

- Sections : Check - Kx = 1.00- Ky = 1.00

- Steel Grade: A36

- Allow. Slend.: 240 (compr.) 300 (tens.)

- Allowable Deflection: 1/400

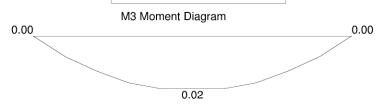
- Tension Area Reduction Factor: 1.00

- Building type : Unbraced

Section: L 2.5x2.5x3/16

0.55 ly = 0.55 in4 Sx = 0.30 Sy = 0.30 in3 Area = 0.90Ix = 2.50 b = 2.50 in t = 0.19 ey = 1.82 in ex = 1.82 in0.01 Cw = 0.00 in 6 lv = 0.22 in 4

DESIGN COMBINATION = 1



Max. AXIAL Force = -1.13 (compr.) Max. SHEAR Force =

SECTION CLASSIFICATION: *** SLENDER ***

Limiting Ratios: Compact Non-Compact

d/t = 13.2312.8 (Fy= 36.0)12.8 b/t = 13.2315.3 <

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M3 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.30 QS =0.986	M = 0.02 Mn = 1.14	0.02
M2 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.30 QS =0.986	M = 0.00 Mn = 1.14	0.00
Deflection	defl. L / 400 < 1.00		defl = 0.01436	0.06
Axial Force (4-1),(4-2)	Pu < 1.00 0.90AgFcr	(kL/r)x = 125 (kL/r)y = 197 $\lambda c \sqrt{Q} = 2.21$ Q = 0.90	Pu = 1.13 Ag = 0.90 Fcr = 6.49	0.21
Lateral Torsional Buckling (5-6)	M < 1.00 0.9Mn Critical Segment from Segment End Momen		M = 0.02 Mn = 1.02 My = 0.91 Mob = -1.00 flange	0.02

Prepared by:

Code: AISC-LRFD Page: 10 Date: 5/23/22

Detailed Results Table for Beam 123

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
Combined	Pu 8Mux 8Muy	Cmx = 1.00	Mux = 0.00	0.24
Forces	— + — + —	Cmy = 1.00	Muy = 0.02	
(compress.)	φPn 9φMnx 9φMny	Pex = 16.33	B1x = 1.07	
(H1-1a)	< 1.00	Pey = 6.58	B1y = 1.21	

Detailed Results Table for Beam 128

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

Beam: 74 80 X2 (Major axis)
128

CONSTRAINTS

0.00

DESIGN DATA

- Sections : Check - Kx = 1.00 - Ky = 1.00

- Steel Grade: A36 - Allow. Slend. : 240 (compr.) 300 (tens.)

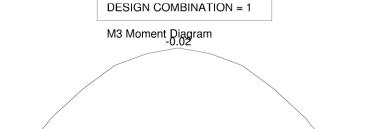
- Allowable Deflection: 1/400

- Tension Area Reduction Factor: 1.00

0.00

- Building type : Unbraced

Section: L 2.5x2.5x3/16



Max. AXIAL Force = -1.12 (compr.) Max. SHEAR Force = 0.01

SECTION CLASSIFICATION: *** SLENDER ***

Limiting Ratios: Compact Non-Compact

d/t= 13.23 < 12.8 12.8 (Fy= 36.0) b/t= 13.23 < 15.3

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	DESIGN	EQUATION	FACTORS	VALUES	RESULT
	(A-F1-1)	< 1.00			0.02

Prepared by:

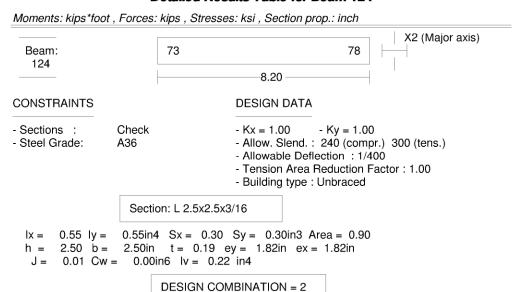
Code: AISC-LRFD Page: 11 Date: 5/23/22

Detailed Results Table for Beam 128

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M2 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.30 QS =0.986	M = 0.00 Mn = 1.14	0.00
Deflection	defl. L / 400 < 1.00		defl = 0.01436	0.06
Axial Force (4-1),(4-2)	Pu < 1.00 0.90AgFcr	(kL/r)x = 125 (kL/r)y = 197 $\lambda c \sqrt{Q} = 2.21$ Q = 0.90	Pu = 1.12 Ag = 0.90 Fcr = 6.49	0.21
Lateral Torsional Buckling (5-6)	M < 1.00 0.9Mn < 100 Critical Segment from Segment End Momen		M = 0.02 Mn = 1.02 My = 0.91 Mob = -1.00 lange	0.02
Combined Forces (compress.) (H1-1a)	Pu 8Mux 8Muy 	Cmx = 1.00 Cmy = 1.00 Pex = 16.33 Pey = 6.58	Mux = 0.00 Muy = 0.02 B1x = 1.07 B1y = 1.21	0.24

Detailed Results Table for Beam 124



0.00

M2 Moment Diagram

0.04

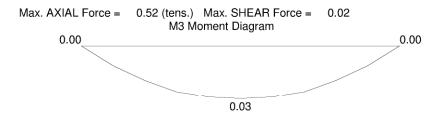
0.00

Prepared by:

Code: AISC-LRFD Page: 12 Date: 5/23/22

Detailed Results Table for Beam 124

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



Max. AXIAL Force = 0.52 (tens.) Max. SHEAR Force = 0.02

SECTION CLASSIFICATION: *** SLENDER ***

Limiting Ratios: Compact Non-Compact

d/t= 13.23 < 12.8 12.8 (Fy= 36.0)

b/t= 13.23 < 15.3

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M3 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.30 QS =0.986	M = 0.03 Mn = 1.14	0.03
M2 Moment (A-F1-1) without LTB	M 0.9Mn < 1.00	Z = 0.30 QS =0.986	M = 0.04 Mn = 1.14	0.04
Deflection	defl. L / 400 < 1.00		defl = 0.03473	0.14
Axial Force (D1-1)	Pu < 1.00 0.90AgFy	(kL/r)x =126 (kL/r)y =199	Pu = 0.52 Ag = 0.90 Fy = 36.00	0.02
Lateral Torsional Buckling (5-6)	M < 1.00 0.9Mn Critical Segment from Segment End Momen		M = 0.04 Mn = 0.99 My = 0.91 Mob = 2.64 flange	0.04
Combined Forces (tension) (H1-1b)	Pu + Mux Muy 2φPn φMnx φMny < 1.00		Mux = 0.04 Muy = 0.03	0.08



20 Alexander Drive, 2nd Floor Wallingford, CT 06492

STRUCTURAL ANALYSIS BLOOMFIELD 4 CT



Address:

1300 HALL BOULEVARD BLOOMFIELD, CT 06002

LOCATION CODE: 684872

Date:

JUNE 2, 2022 (REVISION 0)



June 2, 2022



RE:

Support Structure Structural Analysis

Verizon Site Name: Bloomfield 4 CT (Location Code:684872) Site Address: 1300 Hall Boulevard; Bloomfield, CT 06002

CEA Job Number: 96210.403

To whom it may concern:

Chappell Engineering Associates, LLC has performed a structural analysis of the proposed elevated steel rooftop frame at the above-referenced location. Verizon proposes to install an 25ft \times 11ft elevated steel frame to support one (1) BTS radio cabinet and one (1) BBU battery back-up cabinet. The proposed steel equipment frame will be secured to the existing main structural roof framing beams spaced at approximately 24ft o.c.

The existing roof framing consists of transverse roof beams spaced at approximately 24ft on-center. Roof decking is laid over the main roof beams. The existing transverse roof beams span approximately 53ft (from the exterior building wall to the first interior column support). A rubber membrane roof is laid over the roof deck. We have modeled the existing roof framing in the vicinity of the proposed Verizon equipment frame to determine the suitability of the existing roof framing to support the proposed equipment.

Based upon our site walks on 08-10-2021 and 09-17-2021, our investigation of the existing roof support beams, our review of the proposed loads, and our evaluation of the existing roof framing, Chappell Engineering Associates, LLC has determined that the existing roof framing steel **has adequate capacity** to support the proposed Verizon antenna and associated ancillary equipment loads as shown on the attached drawings. As currently configured, the Verizon framing is rated at 44% capacity.

If you have any questions regarding this matter, please do not hesitate to call.

Very truly yours,

Clement J. Salek, P.E.

Chappell Engineering Associates, LLC

SSIONAL EN

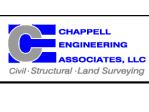
CJS/cjs











R.K. EXECUTIVE CENTRE 201 BOSTON POST RD WEST MARLBOROUGH MA MA 01742 P. (508) 481-7400 F. (508) 481-7406 www.chappellengineering.com

TITLE: 1300 Hall Boulevard, Bloomfield, CT 06002

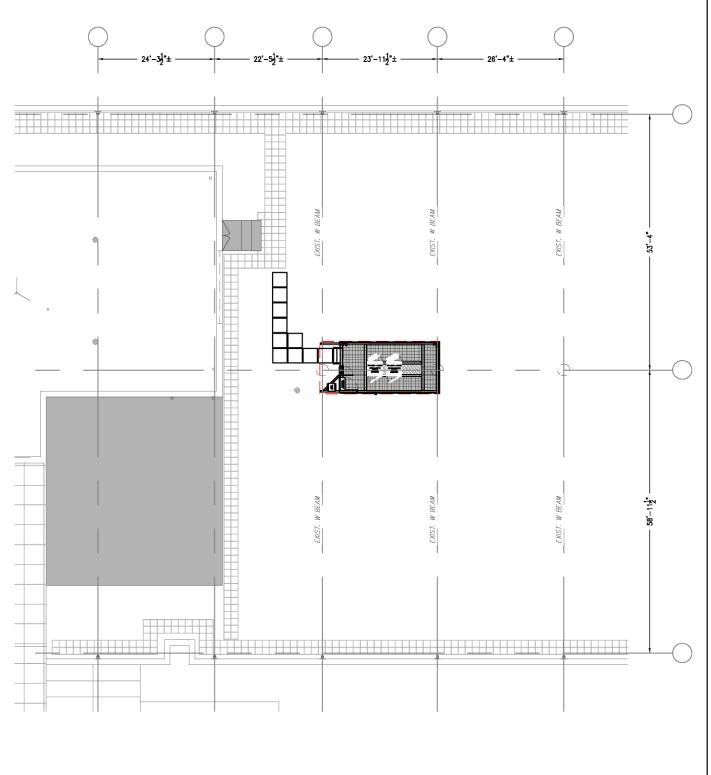
PROJECT #: Bloomfield 4 CT (96210.403)

DATE: May 19, 2022

BY: CJS

CHK: JMF

PAGE:





R.K. EXECUTIVE CENTRE 201 BOSTON POST RD WEST MARLBOROUGH MA MA 01742 P. (508) 481-7400 F. (508) 481-7406 www.chappellengineering.com

TITLE: 1300 Hall Boulevard, Bloomfield, CT 06002

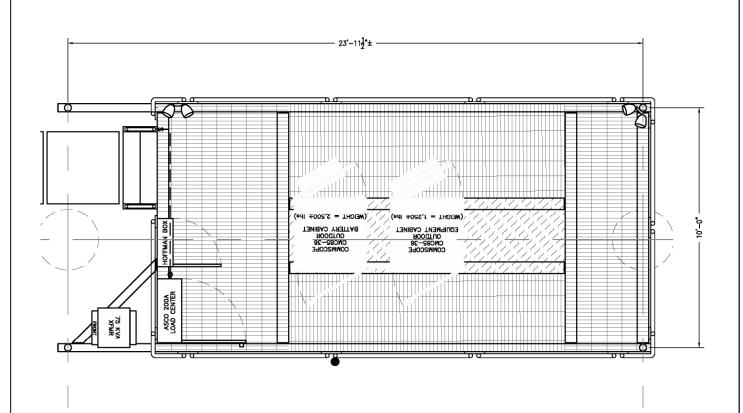
PROJECT #: Bloomfield 4 CT (96210.403)

DATE: May 19, 2022

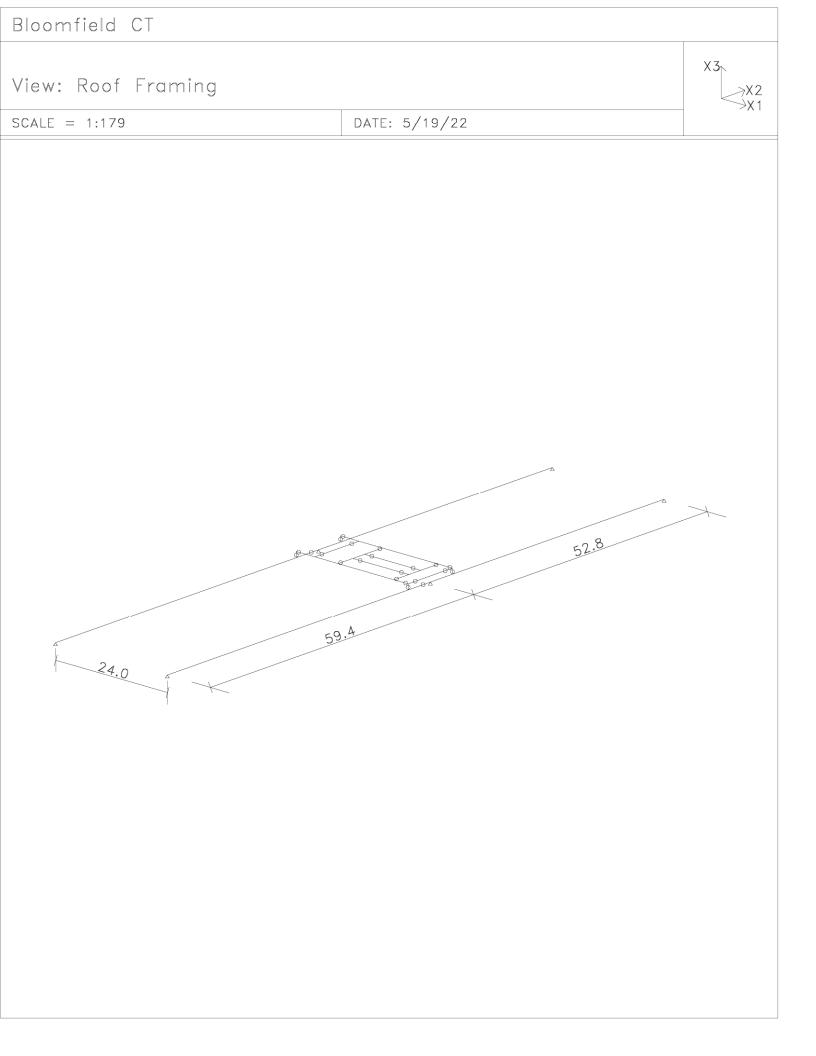
BY: CJS CH

CHK: JMF

PAGE:







Page: 1 **Date:** 5/19/22

Bloomfield CT

Prepared by:

Load no. 1: Existing Selfweight (units - kips ft.)

/ BEAM LOADS

SELF X3 -1. B 18 19 35 17 15 16 20 36

/ END

FORCE SUMMATION

FX1=0. kip FX2=0. kip

FX3=-32.85 kip

Load no. 2: Proposed Selfweight (units - kips ft.)

/ BEAM LOADS

SELF X3 -1. B 2 1 3 4 7 24 TO 26 6 21 22 23 5 10 30 28 9 29 27 8 11 12

/ END

FORCE SUMMATION

FX1=0. kip FX2=0. kip

FX3=-2.0521 kip

Load no. 3: Roof Dead Loads (units - kips ft.)

/ GLOBAL LOADS

DIST FX3 -0.02 PLANE 0. 0. 0. 112.26 0. 48.362 112.26 0. PT

0. 48.362 BEAMS

/ END

FORCE SUMMATION

FX1=0. kip

FX2=0. kip

FX3=-108.58 kip

Load no. 4: Roof Snow Loads (units - kips ft.)

/ GLOBAL LOADS

DIST FX3 -0.035 PLANE 0. 0. 0. 112.26 0. 48.362 112.26 0. PT

0. 48.362 BEAMS

/ END

FORCE SUMMATION

FX1=0. kip

FX2=0. kip

FX3=-190.01 kip

Bloomfield CT

 Prepared by:
 Page: 2

 Date: 5/19/22

Load no. 5: Proposed Grating (units - kips ft.)

/ GLOBAL LOADS

DIST FX3 -0.01 PLANE 15.189 54.439 1. 15.189 64.439 1. 35.189 64.439 1. PT 0. 20. BEAMS

/ END

FORCE SUMMATION

FX1=0. kip

FX2=0. kip

FX3=-2. kip

Load no. 6: Proposed Cabinets (units - kips ft.)

/ GLOBAL LOADS

DIST FX3 -0.24 PLANE 20.689 57.439 1. 20.689 60.939 1. 23.689 60.939

1. PT 0.3. BEAMS

DIST FX3 -0.125 PLANE 24.189 57.439 1. 24.189 60.939 1. 27.189

60.939 1. PT 0. 3. BEAMS

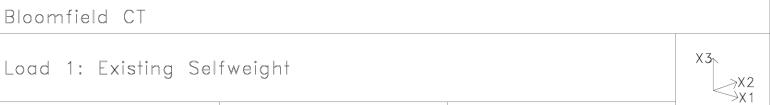
/ END STATIC

FORCE SUMMATION

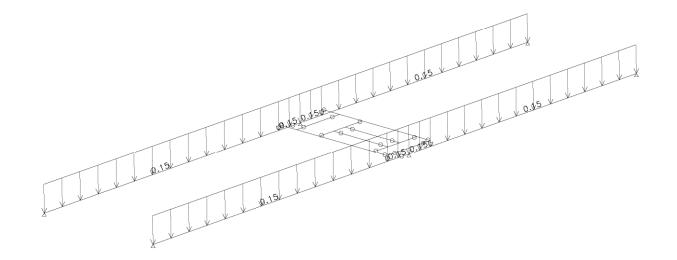
FX1=0. kip

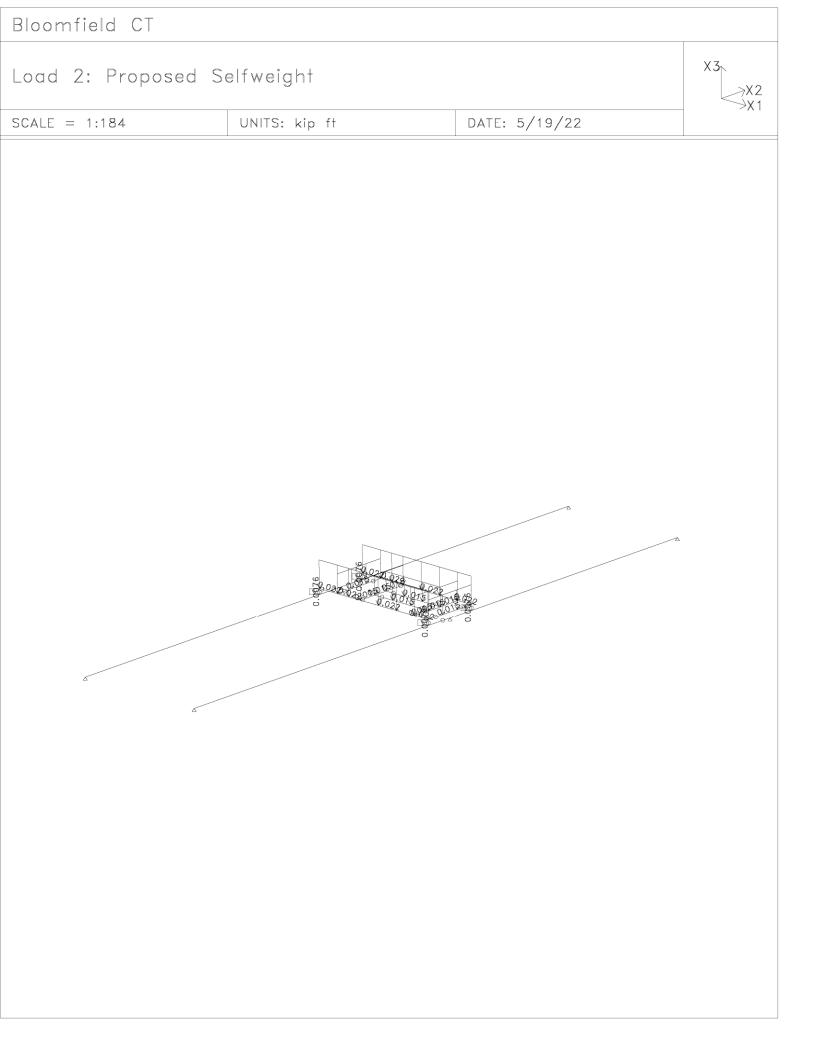
FX2=0. kip

FX3=-3.8325 kip

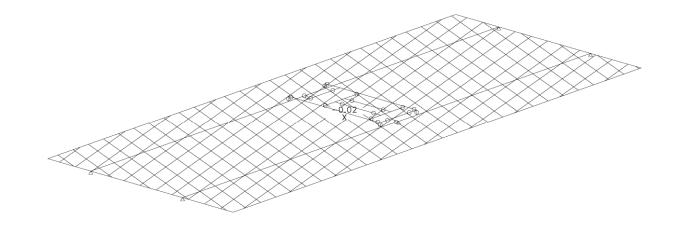




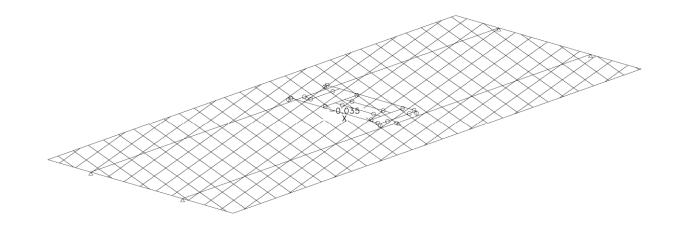












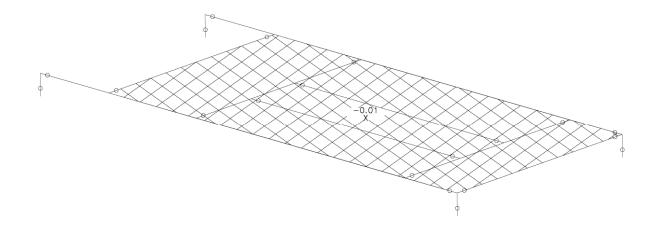
Bloomfield CT

Load 5: Proposed Grating
View: Verizon Frame

SCALE = 1:48

UNITS: kip ft

DATE: 5/19/22



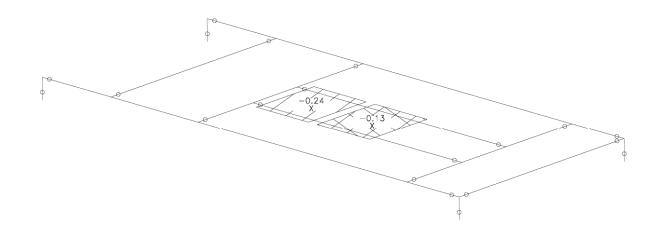
Bloomfield CT

Load 6: Proposed Cabinets
View: Verizon Frame

SCALE = 1:48

UNITS: kip ft

DATE: 5/19/22



Bloomfield CT

 Page: 1

 Prepared by:
 Date: 5/19/22

COMBINATIONS TABLE						
Comb.						
	Existing Beam Loads					
1	1 * 1.00 + 3 * 1.00 + 4 * 1.00 Proposed Beam Loads					
2	1 * 1.00 + 2 * 1.00 + 3 * 1.00 + 4 * 1.00 + 5 * 1.00 + 6 * 1.00					



UNITS: kip*ft

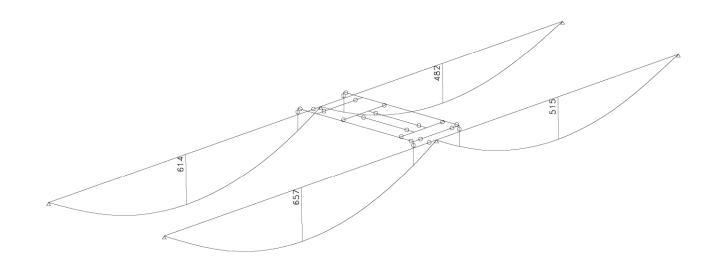
SCALE = 1:173

M2 MOMENT

COMB. NO. 1 Existing Beam Loads

DATE: 5/19/22





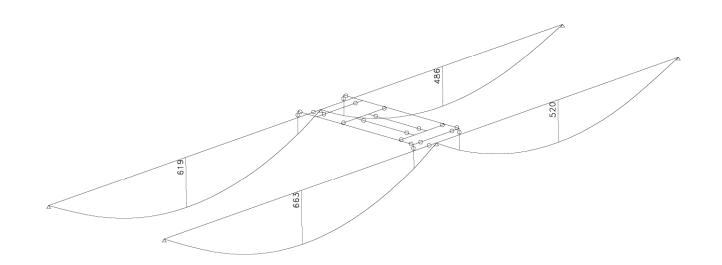


UNITS: kip*ft

SCALE = 1:173

M2 MOMENT

COMB. NO. 2 Proposed Beam Loads



Bloomfield CT View: Verizon Frame

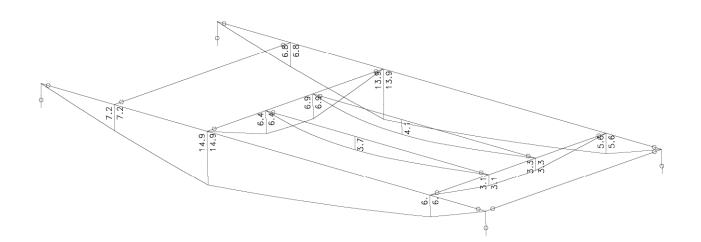
UNITS: kip*ft

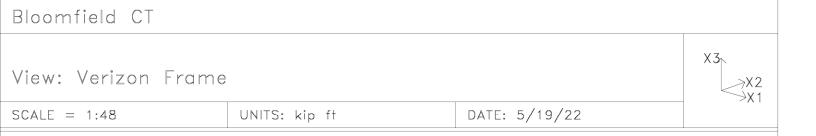
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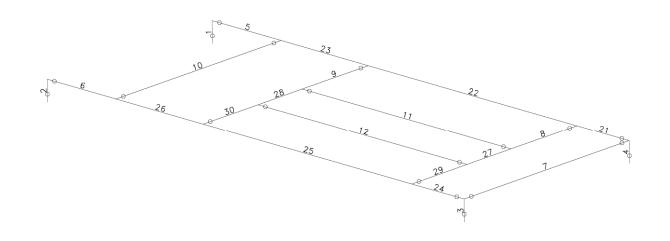
M2 MOMENT

COMB. NO. 2 Proposed Beam Loads

DATE: 5/19/22







Bloomfield CT

Code: AISC-ASD
Page: 2
Prepared by:

Date: 5/19/22

Results Summary Table										
				CAPACITY						
			Defl			Dir				Combined
Beam	Section	Com	L/	Slen	Axial		Shear	Mom	LTB	Axial+Mom
1	PIPE 3	2	9999	10	-0.04	МІ	0.00	0.00	0.00	0.04
2	PIPE 3	2	9999	10	-0.04	MI	0.00	0.00	0.00	0.04
3	PIPE 3	2	9999	10	-0.05	MI	0.00	0.00	0.00	0.05
4	PIPE 3	2	9999	10	-0.04	MI	0.00	0.00	0.00	0.04
5	W 12x22	2	997	170	0.00	MJ	0.04	0.28	0.41	0.41
6	W 12x22	2	936	170	0.00	MJ	0.04	0.30	0.44	0.44
7	W 8x15	2	9999	137	0.00	MJ	0.00	0.02	0.02	0.02
10	W 8x15	2	9999	137	0.00	MJ	0.01	0.02	0.03	0.03
11	W 8x15	2	1987	164	0.00	MJ	0.06	0.17	0.32	0.32
12	W 8x15	2	2174	164	0.00	MJ	0.05	0.16	0.29	0.29
29	W 8x15	2	2765	55	0.00	MJ	0.03	0.14	0.14	0.14
30	W 8x15	2	1345	55	0.00	MJ	0.07	0.29	0.29	0.29

Bloomfield CT		
		X3 X2 X1
SCALE = 1:38	DATE: 5/21/22	
3% 41% 3% 3% 3% 3% 3% 3% 3% 3% 3% 3% 3% 3% 3%	41% 19% 41% 41% 41% 44% 44% 44% 44%	41%
Actual/allowable Maximum result		

Bloomfield CT Code: AISC-ASD Page: 2 Prepared by: Date: 5/19/22

Detailed Results Table for Beam 6 - 24

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



CONSTRAINTS

DESIGN DATA

- Sections : Check - Kx = 1.00- Ky = 1.00

- Steel Grade: A36

- Allow. Slend.: 200 (compr.) 300 (tens.)

(Fy= 36.0 R = 0.000)

- Allowable Deflection: 1/240

- Tension Area Reduction Factor: 1.00

- Building type : Unbraced

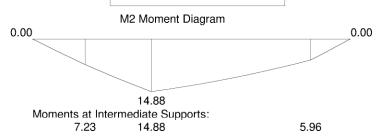
INTERMEDIATE SUPPORTS

L =	3.96	8.96	20.96
LatTors.	+ -	+ -	+ -
Compress.	ΧΥ	ΧΥ	ΧY

Section: W 12x22

Ix = 156.00 Iy =4.66in4 Sx = 25.34 Sy = 2.31in3 Area = 6.484.03in tw = 0.26 tf = 0.43inhw = 12.31 bf =0.29 Cw = 163.85 in 6

DESIGN COMBINATION = 2



Max. AXIAL Force = 0.00 (tens.) Max. SHEAR Force =

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact d/t = 47.38106.7 163.5 <

b/t = 4.7415.8

10.8

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V3 Shear (F4-1)	V/(Av*Fv) <1.00 Fv=0.4*Fy	Av = 3.20	V = 2.03 Fv = 14.40	0.04
M2 Moment (F1-1)	M S*Fb < 1.00	S = 25.34 Fb =0.660 *Fy	M = 14.88 S*Fb = 50.24	0.30
Deflection	defl. < 1.00 L / 240		defl = 0.30712	0.26

Bloomfield CT

Code: AISC-ASD
Page: 3

Prepared by:

Date: 5/19/22

Detailed Results Table for Beam 6 - 24

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
Combined Stresses (Local) (H1-2) (H2-1)	$\frac{\text{fa}}{0.6\text{Fy}} + \frac{\text{fbx}}{\text{Fbx}} + \frac{\text{fby}}{\text{Fby}}$ (Ft) < 1.00	fbx = 7.04 Fbx= 23.76 fby = 0.00 Fby= 0.00	P = 0.00 A = 6.48 Fu = 58.00 fb = M/S	0.30
Moment - noncompact (F1-8)	M < 1.00 S*Fb Critical Segment from Segment End Momen			0.44
Combined Stresses (tension) (H2-1)	$\frac{\text{fa}}{\text{Ft}} + \frac{\text{fbx}}{\text{Fbx}} + \frac{\text{fby}}{\text{Fby}} < 1.00$	Fbx = 15.98 Fby = 27.00	fbx = 7.04 fby = 0.00	0.44

Detailed Results Table for Beam 5 - 21

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



CONSTRAINTS

DESIGN DATA

- Sections : Check - Steel Grade: A36 - Kx = 1.00 - Ky = 1.00

- Allow. Slend.: 200 (compr.) 300 (tens.)

- Allowable Deflection: 1/240

- Tension Area Reduction Factor: 1.00

- Building type : Unbraced

INTERMEDIATE SUPPORTS

L =	3.96	8.96	20.96
LatTors.	+ -	+ -	+-
Compress.	ΧY	ΧY	ΧY

Section: W 12x22

lx = 156.00 ly = 4.66in4 Sx = 25.34 Sy = 2.31in3 Area = 6.48

hw = 12.31 bf = 4.03in tw = 0.26 tf = 0.43in

J = 0.29 Cw = 163.85 in 6

Bloomfield CT

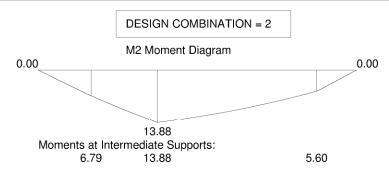
Code: AISC-ASD
Page: 4

Prepared by:

Date: 5/19/22

Detailed Results Table for Beam 5 - 21

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



Max. AXIAL Force = 0.00 (tens.) Max. SHEAR Force = 1.91

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact

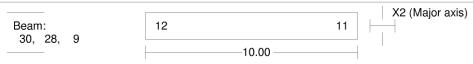
d/t=47.38 < 106.7 163.5 (Fy= 36.0 R = 0.000) b/t=4.74 < 10.8 15.8

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V3 Shear (F4-1)	V/(Av*Fv) <1.00 Fv=0.4*Fy	Av = 3.20	V = 1.91 Fv = 14.40	0.04
M2 Moment (F1-1)	M S*Fb < 1.00	S = 25.34 Fb =0.660 *Fy	M = 13.88 S*Fb = 50.24	0.28
Deflection	defl. L / 240 < 1.00		defl = 0.28834	0.24
Combined Stresses (Local) (H1-2) (H2-1)	$\frac{\text{fa}}{0.6\text{Fy}} + \frac{\text{fbx}}{\text{Fbx}} + \frac{\text{fby}}{\text{Fby}}$ (Ft) < 1.00	fbx = 6.56 Fbx= 23.76 fby = 0.00 Fby= 0.00	P = 0.00 A = 6.48 Fu = 58.00 fb = M/S	0.28
Moment - noncompact (F1-8)	M < 1.00 S*Fb Critical Segment from Segment End Momen		•	0.41
Combined Stresses (tension) (H2-1)	$\frac{fa}{Ft} + \frac{fbx}{Fbx} + \frac{fby}{Fby} < 1.00$	Fbx = 15.95 Fby = 27.00	fbx = 6.56 fby = 0.00	0.41

Bloomfield CT Code: AISC-ASD Page: 5 Prepared by: Date: 5/19/22

Detailed Results Table for Beam 30 - 9

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



CONSTRAINTS

DESIGN DATA

- Sections : Check - Kx = 1.00- Ky = 1.00

- Steel Grade: A36

- Allow. Slend.: 200 (compr.) 300 (tens.)

- Allowable Deflection: 1/240

- Tension Area Reduction Factor: 1.00

- Building type : Unbraced

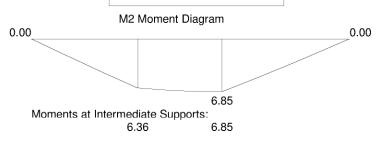
INTERMEDIATE SUPPORTS

L =	3.33	6.00
LatTors.	+ -	+ -
Compress.	ΧY	ΧΥ

Section: W 8x15

$$Ix = 48.00 \ Iy = 3.41 in4 \ Sx = 11.84 \ Sy = 1.70 in3 \ Area = 4.43 \ hw = 8.11 \ bf = 4.02 in \ tw = 0.24 \ tf = 0.31 in \ J = 0.14 \ Cw = 48.41 in6$$

DESIGN COMBINATION = 2



Max. AXIAL Force = 0.00 (tens.) Max. SHEAR Force = 1.97

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact d/t = 33.23106.7 163.5 <

(Fy= 36.0 R = 0.000)b/t = 6.3815.8

10.8

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V3 Shear (F4-1)	V/(Av*Fv) <1.00 Fv=0.4*Fy	Av = 1.98	V = 1.97 Fv = 14.40	0.07
M2 Moment (F1-1)	M S*Fb < 1.00	S = 11.84 Fb =0.660 *Fy	M = 6.85 S*Fb = 23.46	0.29
Deflection	defl. < 1.00 L / 240		defl = 0.08922	0.18

 Bloomfield CT
 Code: AISC-ASD

 Page: 6
 Page: 5/19/22

Detailed Results Table for Beam 30 - 9

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
Combined Stresses (Local) (H1-2) (H2-1)	$\frac{\text{fa}}{0.6\text{Fy}} + \frac{\text{fbx}}{\text{Fbx}} + \frac{\text{fby}}{\text{Fby}}$ (Ft) < 1.00	fbx = 6.94 Fbx= 23.76 fby = 0.00 Fby= 0.00	P = 0.00 A = 4.43 Fu = 58.00 fb = M/S	0.29
Combined Stresses (tension) (H2-1)	$\frac{fa}{Ft} + \frac{fbx}{Fbx} + \frac{fby}{Fby} < 1.00$	Fbx = 23.76 Fby = 27.00	fbx = 6.94 fby = 0.00	0.29

Detailed Results Table for Beam 29 - 8

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



CONSTRAINTS

DESIGN DATA

- Sections : Check - Steel Grade: A36

- Kx = 1.00 Ky = 1.00
- Allow. Slend.: 200 (compr.) 300 (tens.)
- Allowable Deflection: 1/240
- Tension Area Reduction Factor: 1.00
- Building type : Unbraced

INTERMEDIATE SUPPORTS

L =	3.33	6.00
LatTors.	+ -	+ -
Compress.	ΧY	ΧY

Section: W 8x15

Bloomfield CT

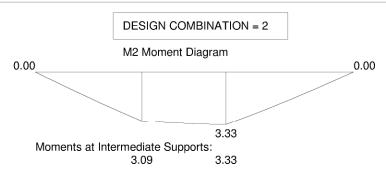
Code: AISC-ASD
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(Fy= 36.0 R = 0.000)

Detailed Results Table for Beam 29 - 8

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



Max. AXIAL Force = 0.00 (tens.) Max. SHEAR Force = 0.98

< 1.00

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact d/t= 33.23 < 106.7 163.5

b/t= 6.38 < 10.8 15.8

(H2-1)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V3 Shear (F4-1)	V/(Av*Fv) <1.00 Fv=0.4*Fy	Av = 1.98	V = 0.98 Fv = 14.40	0.03
M2 Moment (F1-1)	M S*Fb < 1.00	S = 11.84 Fb =0.660 *Fy	M = 3.33 S*Fb = 23.46	0.14
Deflection	defl. L / 240 < 1.00		defl = 0.04341	0.09
Combined Stresses (Local) (H1-2) (H2-1)	$\frac{\text{fa}}{0.6\text{Fy}} + \frac{\text{fbx}}{\text{Fbx}} + \frac{\text{fby}}{\text{Fby}}$ (Ft) < 1.00	fbx = 3.37 Fbx= 23.76 fby = 0.00 Fby= 0.00	P = 0.00 A = 4.43 Fu = 58.00 fb = M/S	0.14
Combined Stresses (tension)	$\frac{fa}{Ft} + \frac{fbx}{Fbx} + \frac{fby}{Fby}$	Fbx = 23.76 Fby = 27.00	fbx = 3.37 fby = 0.00	0.14

Bloomfield CT Code: AISC-ASD Page: 8 Prepared by: Date: 5/19/22

Detailed Results Table for Beam 12

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

X2 (Major axis) 17 Beam: 18 12 12.00

CONSTRAINTS

DESIGN DATA

- Sections : Check - Steel Grade: A36

- Kx = 1.00- Ky = 1.00

- Allow. Slend.: 200 (compr.) 300 (tens.) - Allowable Deflection: 1/240

- Tension Area Reduction Factor: 1.00

- Building type : Unbraced

Section: W 8x15

48.00 ly =3.41in4 Sx = 11.84 Sy = 1.70in3 Area = 4.43hw = 8.11 bf = 4.02in tw = 0.24 tf = 0.31in

0.14 Cw = 48.41 in 6

DESIGN COMBINATION = 2 M2 Moment Diagram 0.00 0.00 3.73

Max. AXIAL Force = 0.00 (tens.) Max. SHEAR Force = 1.51

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact d/t = 33.23106.7 163.5 b/t = 6.3810.8 15.8 <

(Fy= 36.0 R = 0.000)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V3 Shear (F4-1)	V/(Av*Fv) <1.00 Fv=0.4*Fy	Av = 1.98	V = 1.51 Fv = 14.40	0.05
M2 Moment (F1-1)	M S*Fb < 1.00	S = 11.84 Fb =0.660 *Fy	M = 3.73 S*Fb = 23.46	0.16
Deflection	defl. L / 240 < 1.00		defl = 0.06625	0.11
Combined Stresses (Local) (H1-2) (H2-1)	$\frac{fa}{0.6Fy} + \frac{fbx}{Fbx} + \frac{fby}{Fby}$ (Ft) < 1.00	fbx = 3.77 Fbx= 23.76 fby = 0.00 Fby= 0.00	P = 0.00 A = 4.43 Fu = 58.00 fb = M/S	0.16
Moment - noncompact (F1-8)	M < 1.00 S*Fb Critical Segment from Segment End Momen			0.29

Bloomfield CT

Code: AISC-ASD
Page: 9
Prepared by:

Date: 5/19/22

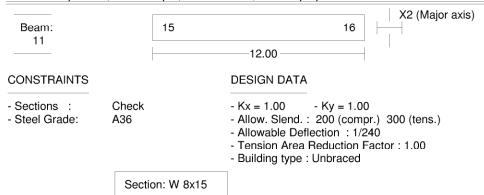
Detailed Results Table for Beam 12

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

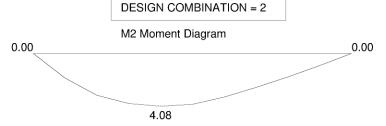
DESIGN	1	EQUATI	ON	F.	ACTORS	VALUES	RESULT
Combined Stresses (tension) (H2-1)	fa Ft	+	fby Fby 1.00	Fbx = Fby =	13.00 27.00	 = 3.77 = 0.00	0.29

Detailed Results Table for Beam 11

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



|x| = 48.00 |y| = 3.41in4 |Sx| = 11.84 |Sy| = 1.70in3 |Area| = 4.43 |Area| = 4.02in | |tw| = 0.24 |tf| = 0.31in | |J| = 0.14 |Cw| = 48.41in6



Max. AXIAL Force = 0.00 (tens.) Max. SHEAR Force = 1.66

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact d/t= 33.23 < 106.7 163.5 (Fy= 36.0 R = 0.000) b/t= 6.38 < 10.8 15.8

10 01100	1.66 14.40	0.06
	4.08 23.46	0.17

Bloomfield CT

Code: AISC-ASD
Page: 10

Prepared by:

Date: 5/19/22

Detailed Results Table for Beam 11

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
Deflection	defl. L / 240 < 1.00		defl = 0.07247	0.12
Combined Stresses (Local) (H1-2) (H2-1)	$\frac{\text{fa}}{0.6\text{Fy}} + \frac{\text{fbx}}{\text{Fbx}} + \frac{\text{fby}}{\text{Fby}}$ (Ft) < 1.00	fbx = 4.13 Fbx= 23.76 fby = 0.00 Fby= 0.00	P = 0.00 A = 4.43 Fu = 58.00 fb = M/S	0.17
Moment - noncompact (F1-8)	M < 1.00 S*Fb Critical Segment from Segment End Momen		M = 4.08 S*Fb= 12.83 Cb = 1.00 flange	0.32
Combined Stresses (tension) (H2-1)	$\frac{fa}{Ft} + \frac{fbx}{Fbx} + \frac{fby}{Fby}$ < 1.00	Fbx = 13.00 Fby = 27.00	fbx = 4.13 fby = 0.00	0.32



CHAPPELL ENGINEERING ASSOCIATES, LLC

ARCHITECT/ENGINEER:

R.K. EXECUTIVE CENTRE 201 BOSTON POST ROAD WEST SUITE 101 MARIEDROUCH, MA 01752 (5)39 A81—7400 www.choppellengineering.com

Verizon

20 ALEXANDER DRIVE, WALLINGFORD, CT 06492

BLOOMFIELD 4 CT

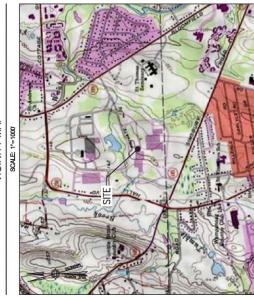
1300 HALL BOULEVARD BLOOMFIELD, CT 06002

PROJECT TYPE: WIRELESS TELECOMMUNICATIONS INSTALLATION ON ROOFTOP OF EXISTING (4)-STORY STEEL FRAMED BUILDING

SITE INFORMATION:

CHAPPELL ENGINEERING ASSOCIATES, LLC 201 BOSTON POST ROAD WEST, SUITE 101 MARIBOROUGH, MA 01752 N 41°-48-30.48" (41.808467") (NAD '83) W 72°-44'-36.55" (72.743488") (NAD '83) HARTFORD COUNTY, CONNECTICUT SOUTHEAST CORNER OF EXISTING MECHANICAL PENTHOUSE CELLCO PARTNERSHIP (dba VERIZON WIRELESS) 20 ALEXANDER DRIVE WALLINGFORD, CT 06492 THE ATRIUM CT LLC 2 PARK AVENUE, 17TH F NEW YORK, NY 10166 ARCHITECT / ENGINEER SITE CONTROL POINT PROPERTY OWNER: SITE ADDRESS APPLICANT: COUNTY:

VICINITY MAP



DRIVING DIRECTIONS

FROM WALLINGFORD, TAKE 191 NORTH, TAKE THE CT-218 BUT TOWARD
WINDSCHREUD, DINGE LIFT OF THE TOWARD TO THOR USE THE LEFT LANGES TO THRE LOON TO CT-195 SOUTH. THE STREET LEGAL TO STREET AGAIN THE STREET LOON TO CT-195 SOUTH.

SHEET INDEX

DATE

ENGINEER/LAND SURVEYOR

WG.	DESCRIPTION	TEV.
5	TITLE SHEET	4
10	LOCATION PLAN	4
205	PROPERTY PLAN	4
10	PART ROOF PLAN AND SITE DETAILS	4
20	NORTH BUILDING ELEVATION AND ENLARGED PART NORTH BUILDING ELEVATION	4
504	ANTENNA DETAILS AND ANOUT ADVIDMENT SPECIFICATIONS	*

DO NOT SCALE DRAWINGS

TITLE SHEET

BLOOMFIELD 4 CT 1300 HALL BOULEVARD BLOOMFIELD, CT 06002

REVISED PER ATTORNEY COMMENTS

REVISED PER 1A FINDINGS

REVISIONS

ISSUED FOR ZONING (FINAL)

AL ANS RESIDENCE DUBLISHOUS AND COLONIOUS AT THE PROPOSED PROLECT STEE SHALL BE SHELD DUBLISH STEEL DUBLISH SHELD SHELD DUBLISH SHELD SHEL

DRAWING NO:

PROJECT DESCRIPTION

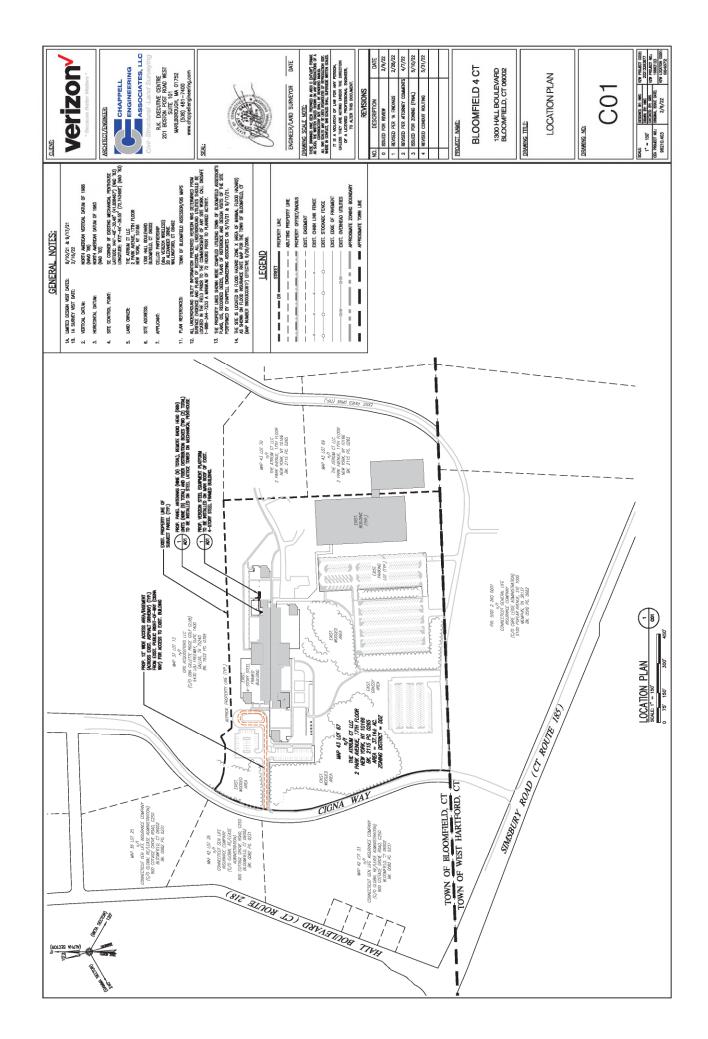
- 1 THIS IS AN UNIMANNED AND RESTRICTED ACCESS EQUIPMENT INSTALLATION AND WILL BELIESE THE THANSHISSION OF HADO SGRALL FOR THE PIPPOSE OF PROVIDING THOSE WHICH WILL CONSIDERATION ON UNIFOCULARIE BERGING.

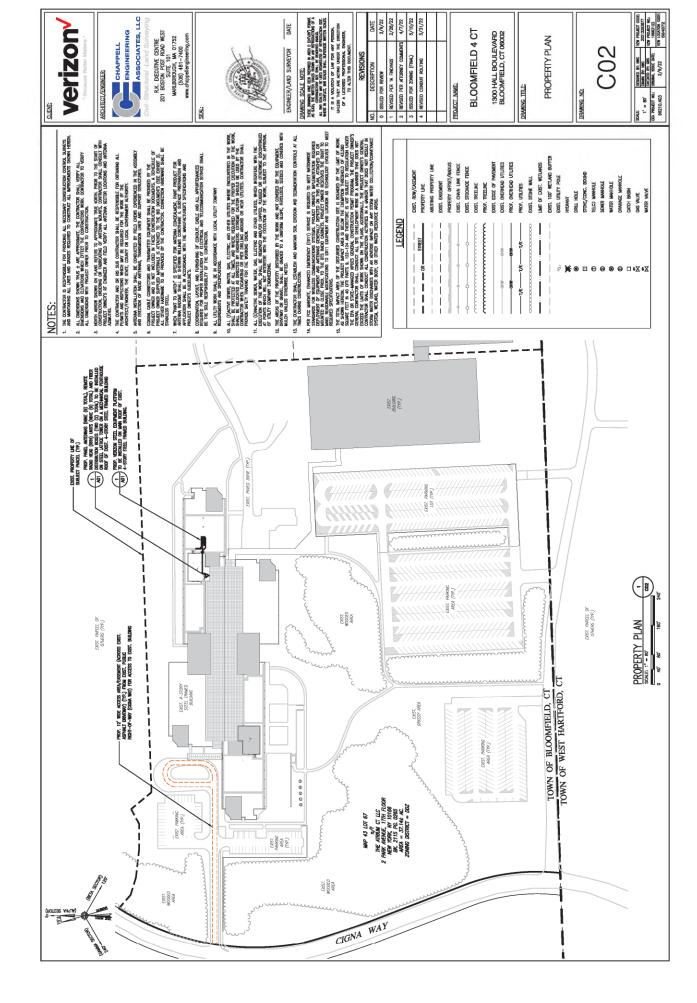
 S. NOF OTHER IN METER SIPPLY IS TO BE PROVIDED AT THIS LOCATION.

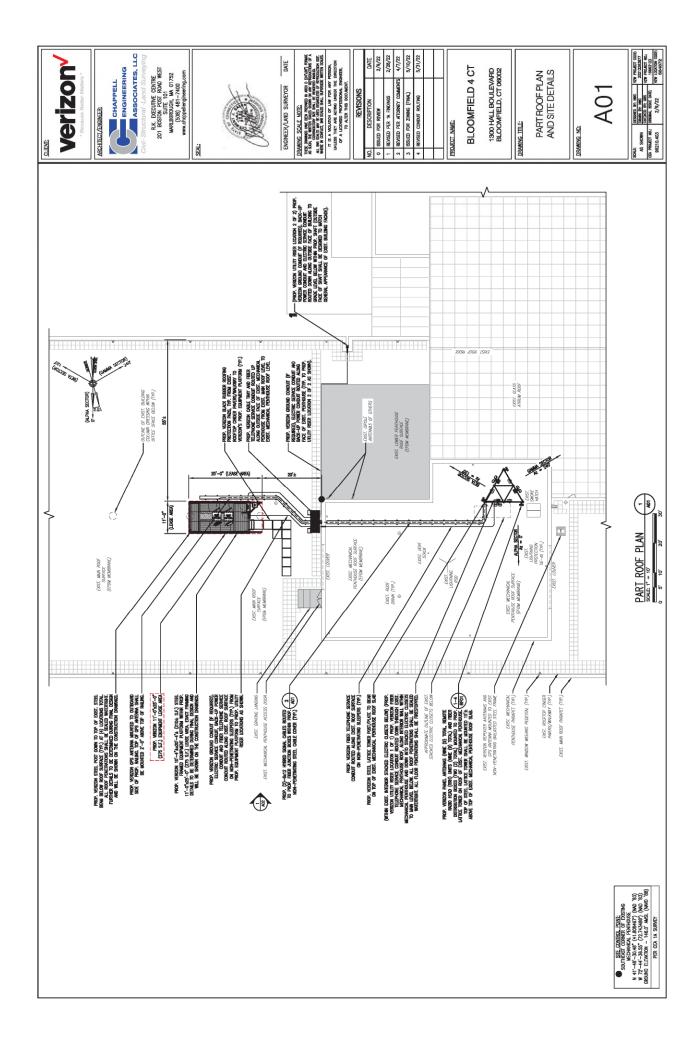
 A. NO WASTE WHITE PILE BE GENERATED AT THIS LOCATION.

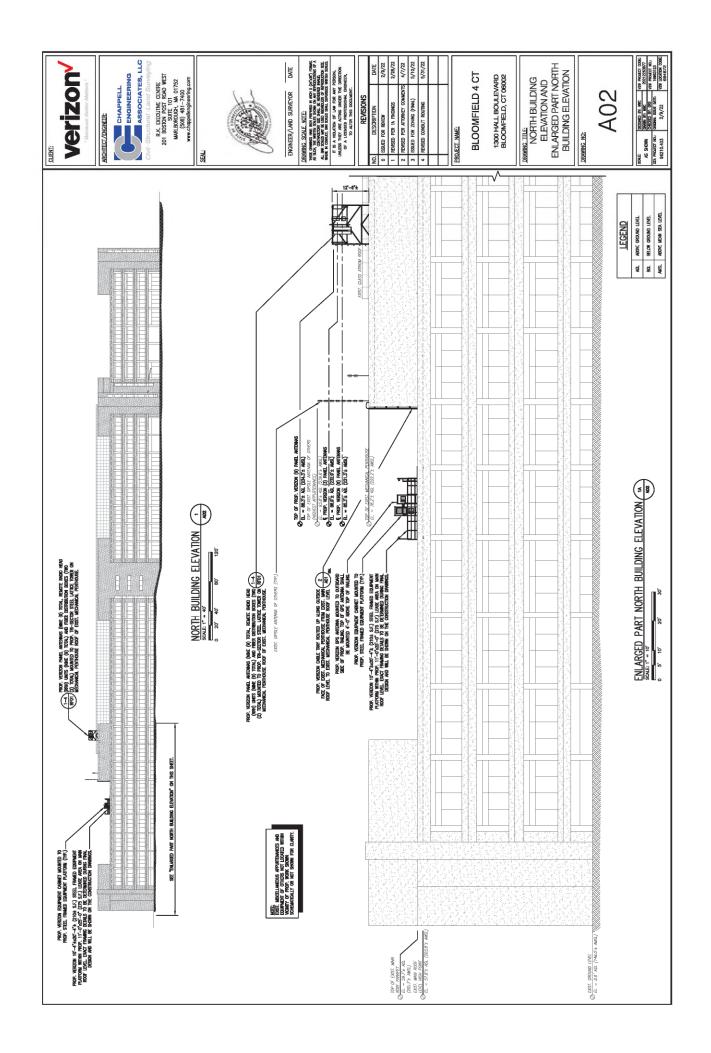
 S. NO SOCIOL WASTE WILL BE CENERATED AT THIS LOCATION.

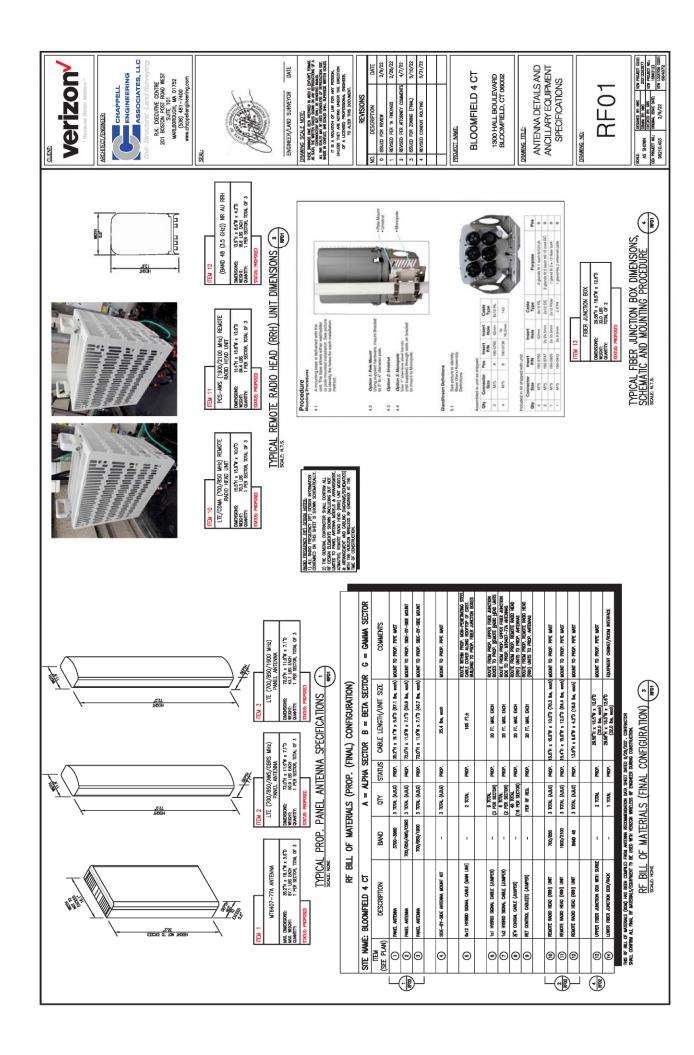
VZW PROJECT CODE: ZCZ12263877 VZW PROJECT NO.: 16863122 VZW LOOATON CODE:
DRAWN STE NIC CRUZACID IN: ORS CHIZACID IN: ORS CHIZACID IN: ORS 2/9/22
SOULE AS SHOWN CEN PROJECT NO.: 96210.403











ATTACHMENT 5



PHOTO SIMULATIONS FOR PROPOSED WIRELESS TELECOMMUNICATIONS INSTALLATION ON ROOFTOP OF EXISTING (4) STORY STEEL FRAMED BUILDING

Applicant Site Name: **BLOOMFIELD 4 CT**

Site Address:

1300 HALL BOULEVARD BLOOMFIELD, CT 06002

Date: APRIL 29, 2022 (REVISION 0)



R.K. Executive Centre ■ 201 Boston Post Road West ■ Suite 101 ■ Marlborough, MA 01752

PHOTO LOCATION MAP





Bloomfield 4 CT

1300 Hall Boulevard Bloomfield, CT 06002



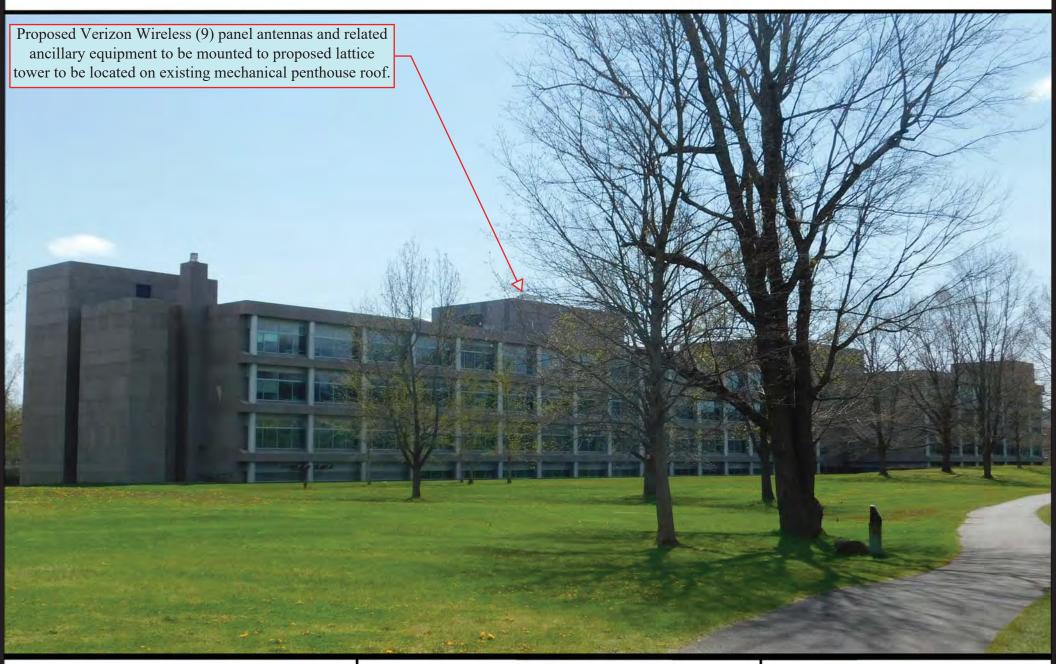




Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Taken 340' +/- Northeast of Existing Building







Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Simulation at 340' +/- Northeast of Existing Building



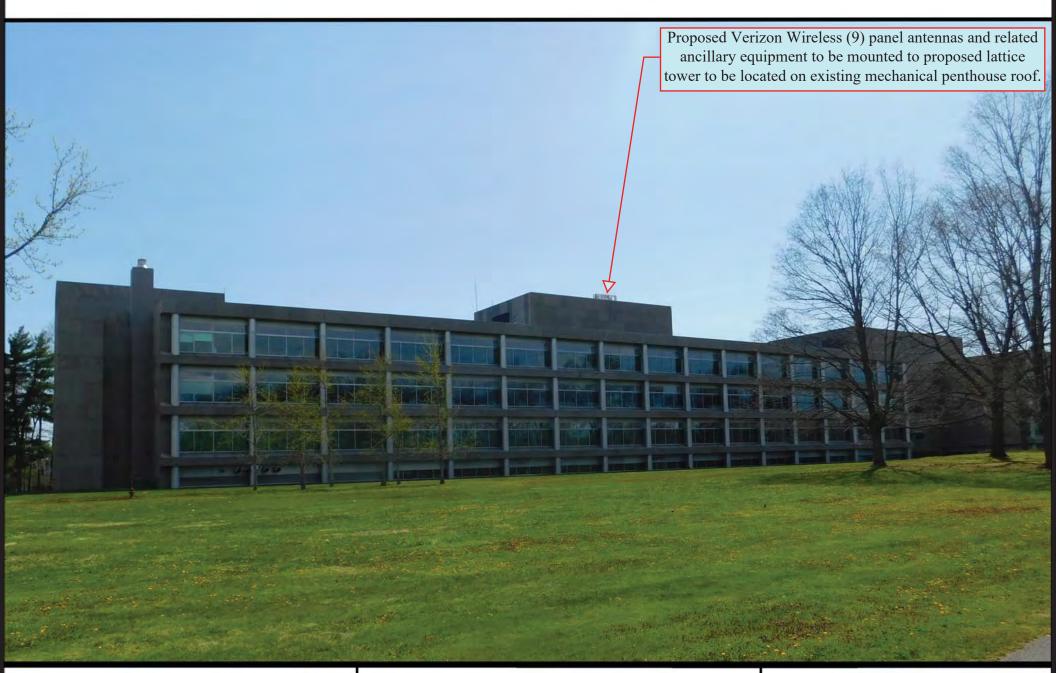




Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Taken 220' +/- North of Existing Building



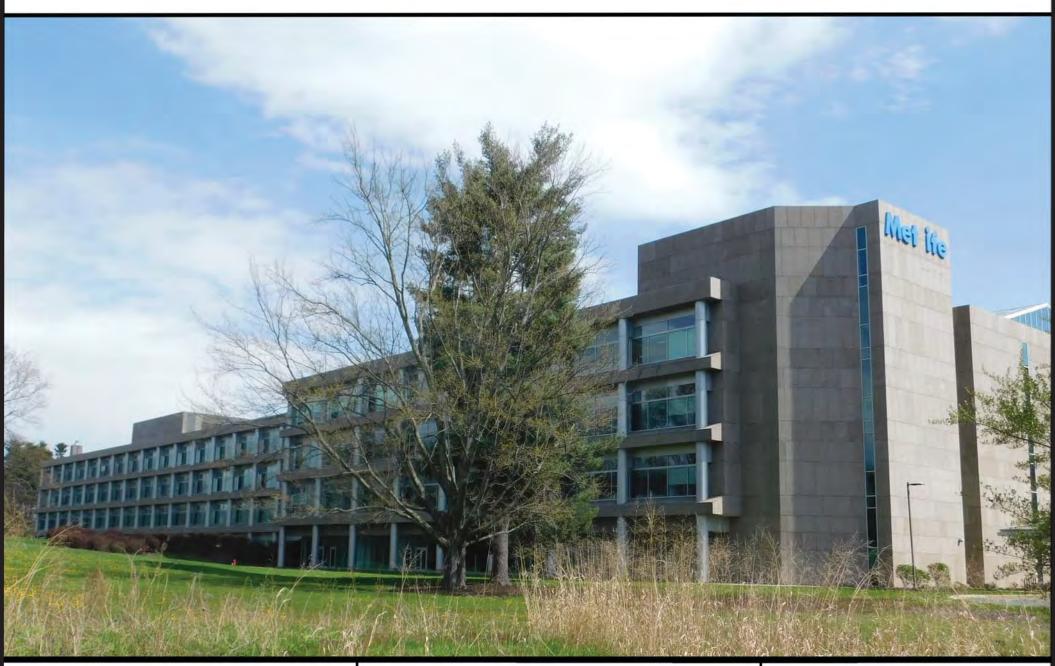




Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Simulation at 220' +/- North of Existing Building



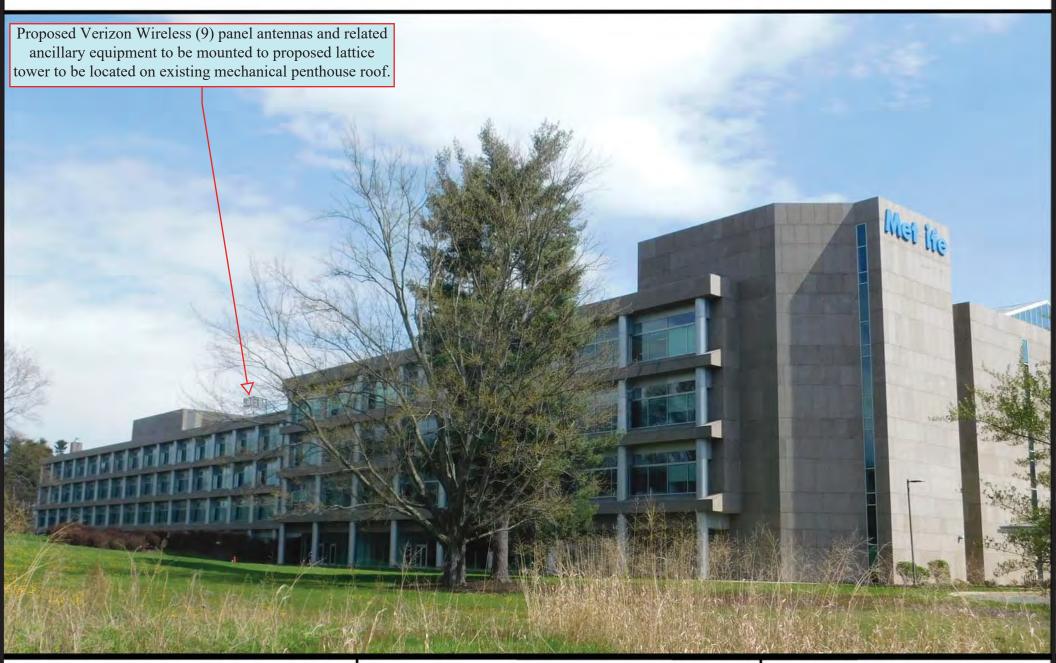




Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Taken 150' +/- Northwest of Existing Building







Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002Photo Simulation at 150' +/- Northwest of Existing Building







Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Taken 160' +/- Southwest of Existing Building



(No Proposed Installation Features Visible From This Location)





Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002
Photo Simulation at 160' +/- Southwest of Existing
Building







Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Taken 360' +/- Southeast of Existing Building







Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Simulation at 360' +/- Southeast of Existing Building







Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Taken 1,120' +/- North of Existing Building







Bloomfield 4 CT

1300 Hall Boulevard, Bloomfield, CT 06002 Photo Simulation at 1,120' +/- North of Existing Building



ATTACHMENT 6

Site Name: BLOOMFIELD 4 CT

Cumulative Power Density

Operator	Operating Numb		ERP Per Trans.	Total ERP	Distance to Target	Calculated Power Density	Maximum Permissible Exposure*	Fraction of MPE	
	(MHz)		(watts)	(watts)	(feet)	(mW/cm^2)	(mW/cm^2)	(%)	
VZW 700	751	4	689	2756	85.3	0.0136	0.5007	2.72%	
VZW Cellular	869	4	700	2800	85.3	0.0138	0.5793	2.39%	
VZW PCS	1980	4	1500	6000	85.3	0.0297	1.0000	2.97%	
VZW AWS	2125	4	1496	5984	85.3	0.0296	1.0000	2.96%	
VZW CBAND	3730	4	6531	26124	85.3	0.1291	1.0000	12.91%	
VZW CBRS	3625	4	12	48	85.3	0.0002	1.0000	0.02%	

Total Percentage of Maximum Permissible Exposure

23.97%

MHz = Megahertz mW/cm^2 = milliwatts per square centimeter ERP = Effective Radiated Power

Absolute worst case maximum values used.

^{*}Guidelines adopted by the FCC on August 1, 1996, 47 CFR Part 1 based on NCRP Report 86, 1986 and generally on ANSI/IEEE C95.1-1992

^{**}Calculation includes a -10 dB Off Beam Antenna Pattern Adjustment pursuant to Attachments B and C of the Siting Council's November 10, 2015 Memorandum for Exempt Modification filings

ATTACHMENT 7

* Summary Report: Existing Structure

Airspace User: Not Identified

File: BLOOMFIELD_4_CT

Location: Hartford, CT

Latitude: 41°-48'-30.48" Longitude: 72°-44'-36.55"

SITE ELEVATION AMSL.....146 ft. STRUCTURE HEIGHT......94 ft. OVERALL HEIGHT AMSL.....240 ft.

NOTICE CRITERIA

FAR 77.9(a): NNR (DNE 200 ft AGL)
FAR 77.9(b): NNR (DNE Notice Slope)
FAR 77.9(c): NNR (Not a Traverse Way)

FAR 77.9: NNR FAR 77.9 IFR Straight-In Notice Criteria for HFD FAR 77.9: NNR FAR 77.9 IFR Straight-In Notice Criteria for 4B9

FAR 77.9(d): NNR (Off Airport Construction)

NR = Notice Required

NNR = Notice Not Required

PNR = Possible Notice Required (depends upon actual IFR procedure)
For new construction review Air Navigation Facilities at bottom
of this report.

The location and analysis were based upon an existing structure. However, no existing aeronautical study number was identified. If the 'existing' structure penetrates an obstruction surface defined by CFR 77.17, 77.19, 77.21 or 77.23 (see below) it is strongly recommended the FAA be notified of the 'existing' structure to determine obstruction marking or lighting requirements. It is not uncommon for the FAA to issue a Determination of No Hazard (DNH) for an existing structure and modify the airspace to accommodate the structure, should that be required. If the FAA issues a DNH enter the aeronautical study number (ASN) in the space provided on the Airspace Analysis Window Form and re-run Airspace.

The below analysis reflects the aeronautical conditions that exist as of the date stamped on this analysis.

Notice to the FAA is not required at the analyzed location and height for slope, height or Straight-In procedures. Please review the 'Air Navigation' section for notice requirements for offset IFR procedures and EMI.

```
OBSTRUCTION STANDARDS
  FAR 77.17(a)(1): DNE 499 ft AGL
  FAR 77.17(a)(2): DNE - Airport Surface
 FAR 77.19(a): DNE - Horizontal Surface
FAR 77.19(b): DNE - Conical Surface
FAR 77.19(c): DNE - Primary Surface
FAR 77.19(d): DNE - Approach Surface
FAR 77.19(e): DNE - Approach Transitional Surface
FAR 77.19(e): DNE - Abeam Transitional Surface
VFR TRAFFIC PATTERN AIRSPACE FOR: HFD: HARTFORD-BRAINARD
Type: A RD: 35312.5 RE: 18.3
  FAR 77.17(a)(1):
                            DNE
  FAR 77.17(a)(1): DNE
FAR 77.17(a)(2): DNE - Greater Than 5.99 NM.
  VFR Horizontal Surface: DNE
  VFR Conical Surface:
                              DNE
  VFR Primary Surface:
                             DNE
 VFR Approach Surface: DNE
  VFR Transitional Surface: DNE
VFR TRAFFIC PATTERN AIRSPACE FOR: 4B9: SIMSBURY
         RD: 39330.03 RE: 177.1
Type: A
  FAR 77.17(a)(1):
                            DNE
  FAR 77.17(a)(1): DNE
FAR 77.17(a)(2): Does Not Apply.
  VFR Horizontal Surface: DNE
  VFR Conical Surface:
                             DNE
  VFR Primary Surface:
                            DNE
  VFR Approach Surface:
                              DNE
  VFR Transitional Surface: DNE
TERPS DEPARTURE PROCEDURE (FAA Order 8260.3, Volume 4)
  FAR 77.17(a)(3) Departure Surface Criteria (40:1)
  DNE Departure Surface
MINIMUM OBSTACLE CLEARANCE ALTITUDE (MOCA)
  FAR 77.17(a)(4) MOCA Altitude Enroute Criteria
  The Maximum Height Permitted is 17000 ft AMSL
PRIVATE LANDING FACILITIES
  FACTL
                                             BEARING
                                                        RANGE DELTA ARP FAA
  IDENT TYP NAME
                                             To FACIL IN NM ELEVATION IFR
  245.44
                                                         2.75
  CT04 HEL CHASE
                                                                  -460
  No Impact to Private Landing Facility
  Structure 460 ft below heliport.
  OCT5 HEL ST FRANCIS HOSPITAL
                                               135.51
                                                          2.84
                                                                    +56
  No Impact to Private Landing Facility
  Structure is beyond notice limit by 12256 feet.
```

	N AEROSPACE CORP		3.76	+76
•	rivate Landing Facility	•		
Structure is be	eyond notice limit by	17846 feet.		
CT06 HEL DELTA	A ONE	107.54	2 0	+219
	rivate Landing Facilit		3.9	TZ1 3
•		•		
Structure is be	eyond notice limit by	1869/ Teet.		
0CT9 HEL HARTI	FORD HOSPITAL	138.07	4 36	+29
	rivate Landing Facility		7.50	123
•	eyond notice limit by	•		
Jeraceare 13 be	cyona notice iimie by	21432 1000.		
CT75 HEL UCONI	N HFALTH	206.27	5.03	-100
	rivate Landing Facilit		3.03	
•	ft below heliport.	y		
Jei de cai e 100	ic below helipoic.			

AIR NAVIGATION ELECTRONIC FACILITIES

	FAC		ST			DIST	DELTA		GRND
APCH	IDNT	TYPE	ΑТ	FREO	VECTOR	(ft)	ELEVA S	T LOCATION	ANGLE
BEAR						(- /			
	BDL	RADAR	Т		19.3	50232	+4 C	T BRADIFY TNTI	0.00

No Impact. Existing Structures Do Not Require Notice based upon EMI. The FAA takes into account and adjusts radar facilities for reflection, clutter and false targets. The studied location is within 20 NM of an Air Traffic Radar facility.

The calculated Radar Line-Of-Sight (LOS) distance is: 38 NM. This location and height is within the Radar Line-Of-Sight.

BDL	VORTAC	D	109.0	17.19	50559	+80	СТ	BRADLEY	.09
HFD	VOR/DME	R	114.9	138.8	81148	-609	СТ	HARTFORD	43
BAF	VORTAC	R	113.0	3.29	129023	-27	MA	BARNES	01
CEF	TACAN	R	114.0	22.53	153575	+0	MA	WESTOVER	0.00
MAD	VOR/DME	I	110.4	175.56	180769	+24	СТ	MADISON	.01
CTR	VOR/DME	R	115.1	342.44	184625	-1360	MA	CHESTER	42

CFR Title 47, §1.30000-§1.30004

AM STUDY NOT REQUIRED: Structure is not near a FCC licensed AM station. Movement Method Proof as specified in §73.151(c) is not required. Please review 'AM Station Report' for details.

Nearest AM Station: WDRC @ 3970 meters.

Airspace® Summary Version 22.3.628

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04-06-2022 11:45:16

ATTACHMENT 8

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

June 29, 2022

Via Certificate of Mailing

Stanley Hawthorne, Town Manager Town of Bloomfield 800 Bloomfield Avenue Bloomfield, CT 06002

Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to its Existing Wireless Telecommunications Facility at 1300 Hall Boulevard, Bloomfield, Connecticut

Dear Mr. Hawthorne:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval for the installation of a wireless telecommunications facility on the roof of the building at 1300 Hall Boulevard in Bloomfield (the "Property").

The facility will consist of the installation of nine (9) panel type antennas and nine (9) remote radio heads attached to a new steel lattice tower extended approximately 12'-6" above a mechanical penthouse in the easterly portion of the roof. Equipment associated with the antennas will be placed on a steel platform also on the roof of the building.

A copy of the full Petition is attached for your review. Landowners whose parcels are considered to abut the Property were also sent notice of this filing along with a copy of the Petition.

Please contact me if you have any questions regarding this proposal.

Sincerely,

Kenneth C. Baldwin

Kunie gmu-

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

June 29, 2022

Via Certificate of Mailing

Jennifer Valentino-Rodriguez, Director of Planning and Zoning Town of Bloomfield 800 Bloomfield Avenue Bloomfield, CT 06002

Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to its Existing Wireless Telecommunications Facility at 1300 Hall Boulevard, Bloomfield, Connecticut

Dear Ms. Rodriguez:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval for the installation of a wireless telecommunications facility on the roof of the building at 1300 Hall Boulevard in Bloomfield (the "Property").

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Please contact me if you have any questions regarding this proposal.

Sincerely,

Kenneth C. Baldwin

Kunie gmu-

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

June 29, 2022

Via Certificate of Mailing

Shari Cantor, Mayor Town of West Hartford 50 South Main Street West Hartford, CT 06107

Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to its Existing Wireless Telecommunications Facility at 1300 Hall Boulevard, Bloomfield, Connecticut

Dear Mayor Cantor:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval for the installation of a wireless telecommunications facility on the roof of the building at 1300 Hall Boulevard in Bloomfield (the "Property").

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A copy of the full Petition is attached for your review. Landowners whose parcels are considered to abut the Property were also sent notice of this filing along with a copy of the Petition.

Please contact me if you have any questions regarding this proposal.

Sincerely,

Kenneth C. Baldwin

Kunie BMM

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

June 29, 2022

Via Certificate of Mailing

Todd Dumais, Town Planner Town of West Hartford 50 South Main Street West Hartford, CT 06107

Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to its Existing Wireless Telecommunications Facility at 1300 Hall Boulevard, Bloomfield, Connecticut

Dear Mr. Dumais:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval for the installation of a wireless telecommunications facility on the roof of the building at 1300 Hall Boulevard in Bloomfield (the "Property").

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A copy of the full Petition is attached for your review. Landowners whose parcels are considered to abut the Property were also sent notice of this filing along with a copy of the Petition.

Please contact me if you have any questions regarding this proposal.

Sincerely,

Kenneth C. Baldwin

Kunie BMM

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

June 29, 2022

Via Certificate of Mailing

The Atrium CT LLC 2 Park Avenue, 17th Floor New York, NY 10166

Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to its Existing Wireless Telecommunications Facility at 1300 Hall Boulevard, Bloomfield, Connecticut

Dear Sir or Madam:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval for the installation of a wireless telecommunications facility on the roof of the building at 1300 Hall Boulevard in Bloomfield (the "Property").

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Please contact me if you have any questions regarding this proposal.

Sincerely,

Kenneth C. Baldwin

Kung gmu-

ATTACHMENT 9

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

June 29, 2022

Via Certificate of Mailing

«Owners_and_Mailing_Address»

Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to an Existing Wireless Telecommunications Facility at 1300 Hall Boulevard, Bloomfield, Connecticut

Dear «Salutation»:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval for the installation of a wireless telecommunications facility on the roof of the building at 1300 Hall Boulevard in Bloomfield (the "Property").

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This notice and a full copy of the Petition is being sent to you because you are listed on the Town Assessor's records as an owner of land that abuts the Property. If you have any questions regarding the Petition, the Council's process for reviewing the Petition or the details of the filing itself, please feel free to contact me at the number listed above. You may also contact the Council directly at 860-827-2935.

Sincerely,

Kenneth C. Baldwin

Kunie gmu

CELLCO PARTNERSHIP D/B/A VERIZON WIRELESS

ABUTTING PROPERTY OWNERS

1300 HALL BOULEVARD BLOOMFIELD, CONNECTICUT

BLOOMFIELD

	Property Address	Owner's and Mailing Address
1.	1360 Hall Boulevard	GRG Acquisitions LLC c/o DBA Gillette Ridge Golf Club 5430 LBJ Freeway, Suite 1400 Dallas, TX 75240
2.	1348 Hall Boulevard	Connecticut General Life Insurance Company 900 Cottage Grove Road, C2S0 Bloomfield, CT 06002
3.	1340 Hall Boulevard	Connecticut General Life Insurance Company 900 Cottage Grove Road, C2S0 Bloomfield, CT 06002
4.	1330 Hall Boulevard	Connecticut General Life Insurance Company 900 Cottage Grove Road, C2S0 Bloomfield, CT 06002
5.	20 Cigna Campus Way	The Atrium CT LLC 2 Park Avenue, 17 th Floor New York, NY 10166
6.	30 Cigna Campus Way	The Atrium CT LLC 2 Park Avenue, 17 th Floor New York, NY 10166

WEST HARTFORD

7.	260 Simsbury Road	Connecticut General Life Insurance Company c/o CBRE Lease Administration
		5100 Poplar Avenue, Suite 1000
		Memphis, TN 38137