## STATE OF CONNECTICUT CONNECTICUT SITING COUNCIL

IN RE:	:	
	:	
A PETITION OF CELLCO PARTNERSHIP	:	PETITION NO.
D/B/A VERIZON WIRELESS FOR A	:	
DECLARATORY RULING ON THE NEED	:	
TO OBTAIN A SITING COUNCIL	:	
CERTIFICATE FOR MODIFICATIONS TO	:	
AN EXISTING WIRELESS	:	
TELECOMMUNICATIONS FACILITY AT 54	:	
MEADOW STREET, NEW HAVEN,	:	
CONNECTICUT	:	AUGUST 26, 2020

## PETITION FOR A DECLARATORY RULING: INSTALLATION HAVING NO SUBSTANTIAL ADVERSE ENVIRONMENTAL EFFECT

### I. <u>Introduction</u>

Pursuant to Sections 16-50j-38 and 16-50j-39 of the Regulations of Connecticut State Agencies ("R.C.S.A."), Cellco Partnership d/b/a Verizon Wireless ("Cellco") hereby petitions the Connecticut Siting Council (the "Council") for a declaratory ruling ("Petition") that no Certificate of Environmental Compatibility and Public Need ("Certificate") is required under Section 16-50k(a) of the Connecticut General Statutes ("C.G.S.") for modifications to its existing wireless telecommunications facility at 54 Meadow Street in New Haven, Connecticut (the "Property"). *See* Attachment 1 – Site Vicinity and Site Schematic Maps (Aerial Photograph).

## II. Factual Background

In April of 1991, Cellco received Council approval to establish a wireless

telecommunication facility on the roof of the building at the Property (Council Docket No. 140). Cellco currently maintains twelve (12) antennas (three (3) sectors of four (4) antennas) attached to the façade of the rooftop penthouse on the building. Equipment associated with the Cellco antennas is located in a secure equipment room inside the building. The Property is owned by Gateway Partners LLC (the "Owner"). MCM Holdings LLC manages the rooftop telecommunications facilities at the Property for the Owner.

## III. Proposed Construction Activity

### A. <u>Cellco's Proposed Modifications to the New Haven Facility</u>

The proposed facility modifications will involve the removal of nine (9) existing antennas and the installation of twelve (12) new antennas (fifteen (15) total) and ten (10) remote radio heads ("RRHs") at various locations on the roof of the building. Three (3) antennas will remain attached to the penthouse façade; four (4) new antennas will also be attached to the penthouse façade (Beta and Beta/Gamma Sector antennas); Two (2) existing antennas and four (4) new antennas will be attached to the existing mechanical screen wall in the northwest corner of the building rooftop (Alpha and Delta Sector antennas); and one (1) existing antenna and one (1) new antenna will be attached to the building façade along the southeast corner of the building (Beta and Gama Sector antennas). (*See* Cellco's Project Plans included in <u>Attachment 2</u>).

Cellco is licensed to provide wireless telecommunications services in the 850 MHz, 1900 MHz, 2100 MHz and 28 GHz frequency ranges in New Haven and throughout the State of Connecticut. The modified facility will utilize all of Cellco's frequency ranges. Specifications for Cellco's antennas and remote radio heads are included in <u>Attachment 3</u>. A Structural Assessment Letter confirming that the building's structural components and the antenna mounting systems can adequately support Cellco's proposed facility modifications is included in <u>Attachment 4</u>.

## IV. Discussion

## A. <u>The Proposed Facility Modifications Will Not Have A Substantial Adverse</u> <u>Environmental Effect</u>

The Public Utility Environmental Standards Act (the "Act"), C.G.S. § 16-50g et seq.,

-2-

provides for the orderly and environmentally compatible development of telecommunications facilities in the state to avoid "a significant impact on the environment and ecology of the State of Connecticut." C.G.S. § 16-50g. To achieve these goals, the Act established the Council, and requires a Certificate of Environmental Compatibility and Public Need for the construction of cellular telecommunication towers "that may, as determined by the council, have a substantial adverse environmental effect". C.G.S. § 16-50k(a).

## 1. <u>Physical Environmental Effects</u>

Cellco respectfully submits that the modifications to its roof-top facility will not involve a significant alteration in the physical and environmental characteristics of the Property.

## 2. Visual Effects

Portions of the existing building and Cellco's modified facility may be visible from the commercial and industrial properties that surround the Property. The modifications proposed by Cellco will not, however, increase the visibility of the Cellco facility or the building and will not detract from the general characteristics of the building at the Property. A Photo Documentation & Simulations report ("Visual Assessment") is included in <u>Attachment 5</u>.

## 3. <u>FCC Compliance</u>

Radio frequency ("RF") emissions from Cellco's modified facility will not exceed the maximum permissible exposure limits established by the Federal Communications Commission ("FCC"). Included in <u>Attachment 6</u> is a general power density table that demonstrates that Cellco's modified facility will operate within the FCC safety standards.

### 4. FAA Notification Not Required

Cellco has run an Obstruction Analysis Report ("FAA Report") for the proposed New Haven Facility modifications. According to the FAA Report, notice of the facility modifications to the FAA is not required. A copy of the FAA Report is included in <u>Attachment 7</u>.

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## B. Notice to the City, Property Owner and Abutting Landowners

On August 26, 2020, a copy of this Petition was sent to New Haven's Mayor, Justin Elicker; Aicha Woods, New Haven's Director of City Plan; Gateway Partners LLC, the Owner of the Property, and MCM Holdings LLC, the roof-top manager. Copies of the letters sent to Mayor Elicker, Ms. Woods, Gateway Partners LLC, and MCM Holdings LLC are included in Attachment 8.

A copy of this Petition was also sent to the owners of land that abut the Property. A sample abutter's letter and the list of those abutting landowners to whom notice was sent is included in <u>Attachment 9</u>.

V. <u>Conclusion</u>

Based on the information provided above, Cellco respectfully requests that the Council issue a determination, in the form of a declaratory ruling, that the replacement and relocation of antennas, RRHs and related equipment, as described above, will not have a substantial adverse environmental effect and does not require the issuance of a Certificate of Environmental Compatibility and Public Need pursuant to § 16-50k of the General Statutes.

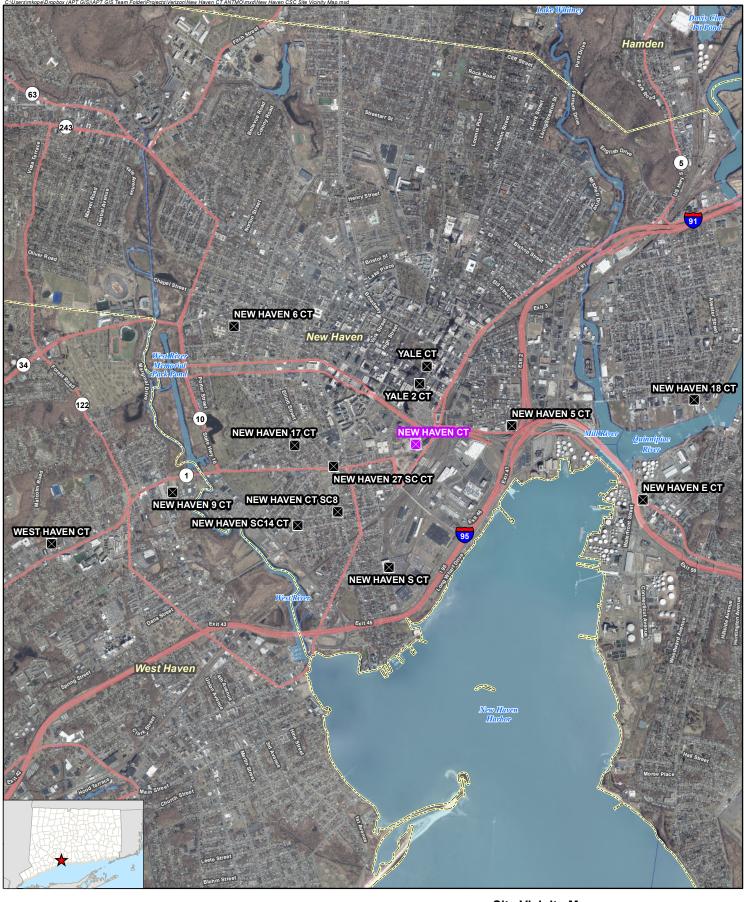
Respectfully submitted,

CELLCO PARTNERSHIP d/b/a VERIZON WIRELESS

By Kunne mm

Kenneth C. Baldwin, Esq. Robinson & Cole LLP 280 Trumbull Street Hartford, CT 06103-3597 (860) 275-8200 Its Attorneys

## **ATTACHMENT 1**



#### Legend

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- Proposed Verizon Wireless Facility  $\times$
- imesSurrounding Verizon Wireless Facilities
- Municipal Boundary 1

Base Map Source: CT ECO 2019 Imagery Map Scale:1 inch = 3,000 feet Map Date: June 2020

3,000 1,500 3,000

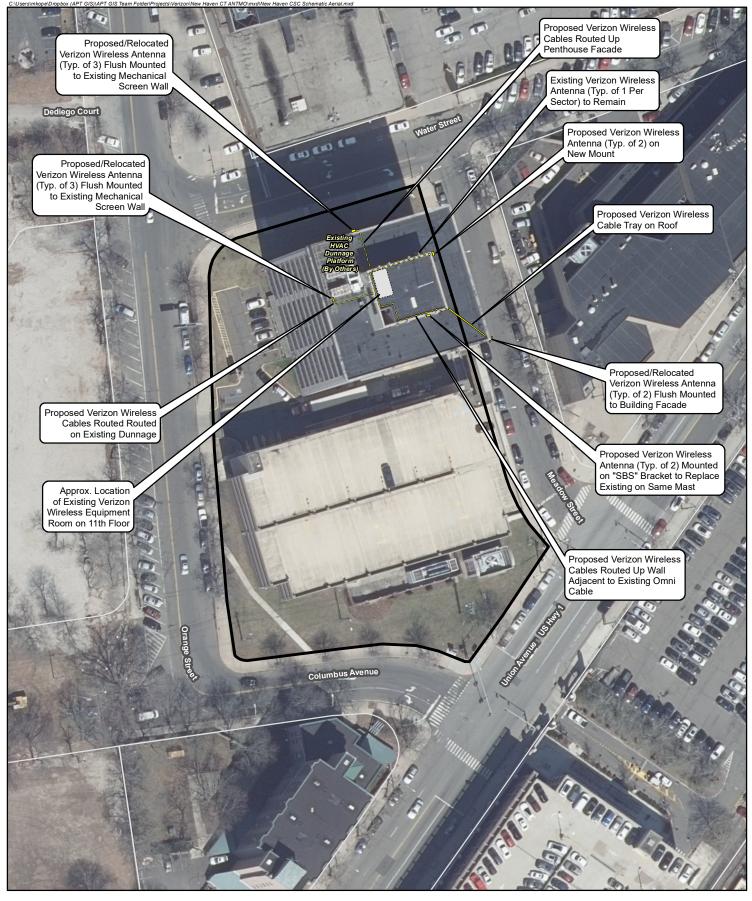
Site Vicinity Map

Feet

**Proposed Wireless Telecommunications Facility** New Haven CT 54 Meadow Street New Haven, Connecticut

verizon<sup>4</sup>





#### Legend

Proposed/Relocated Verizon Wireless Equipment Subject Property

- Existing Verizon Wireless Cable
   Existing Verizon Wireless Equipment to Remain
- Existing Verizon Wireless Equipment Room

Subject Property
Approximate Parcel Boundary



### Site Schematic

Proposed Wireless Telecommunications Facility New Haven CT 54 Meadow Street New Haven, Connecticut

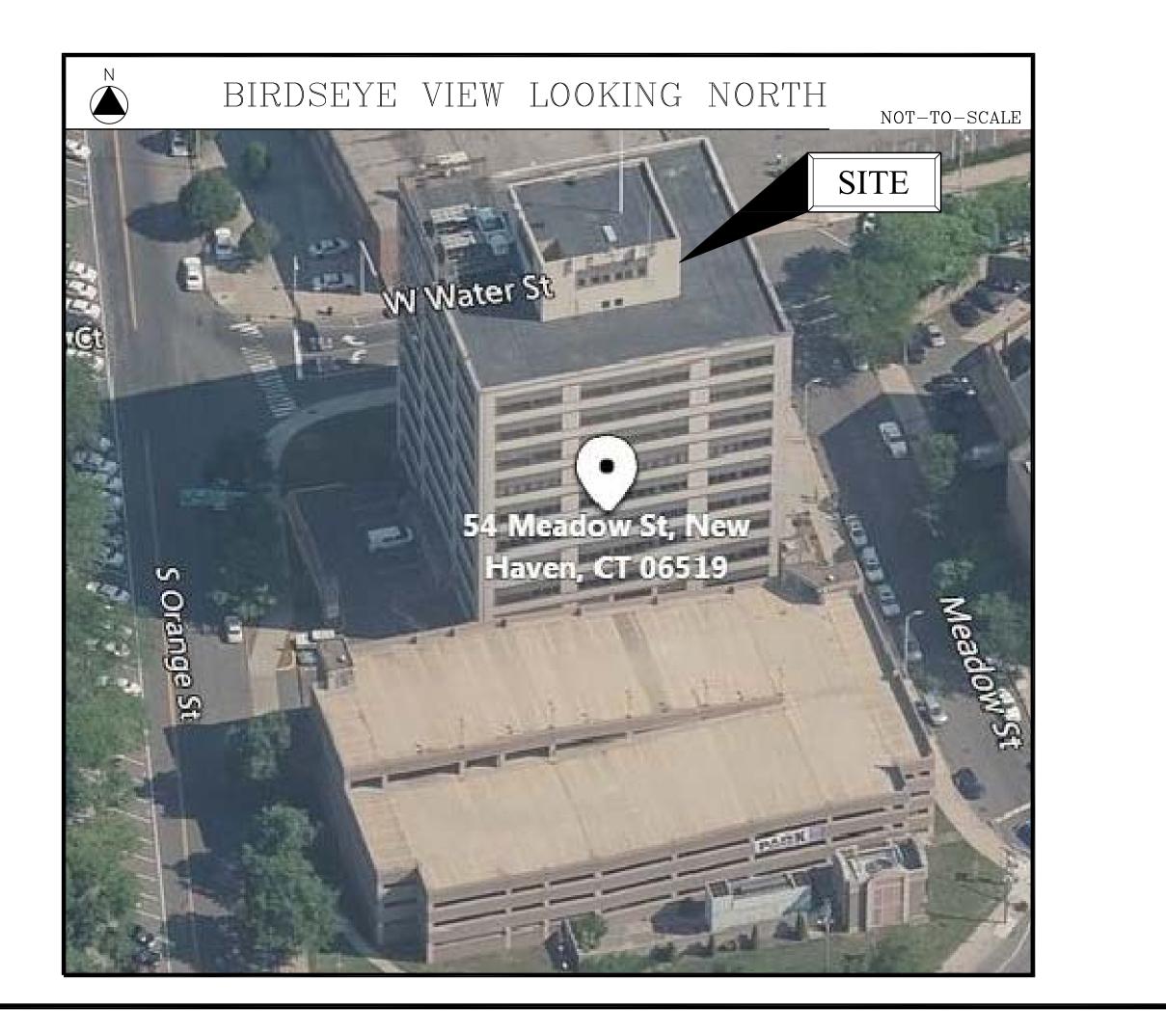
verizon

ALL-POINTS TECHNOLOGY CORPORATION



## **ATTACHMENT 2**

# SITE NAME: NEW HAVEN CT



## PROJECT DESCRIPTION

REPLACEMENT & RELOCATION OF SEVERAL EXISTING VERIZON PANEL ANTENNAS CURRENTLY ACADE MOUNTED TO THE CENTRAL ROOFTOP PENTHOUSE. THE TOTAL ANTENNA QUANTITY WILL NCREASE FROM (12) TO (15) PANEL ANTENNAS. NEW ANTENNAS LOCATIONS INCLUDE FLUSH MOUNTS ON AN EXISTING MECHANICAL SCREEN

WALL AND THE BUILDING FACADE. SEVERAL ANTENNAS TO REMAIN ON PENTHOUSE FACADE. ACCESSORY EQUIPMENT (RRH'S, CABLE BOXES, ETC.) SHALL ALSO BE REPLACED AND RELOCATED WITH THEIR ASSOCIATED ANTENNA SECTORS.



# 54 MEADOW ST. NEW HAVEN, CT 06519



C-3

C-4

20 J	JECT SUMMARY
	NEW HAVEN CT
	54 MEADOW ST. NEW HAVEN, CT 06519
	GATEWAY PARTNERS LLC C/O LEXINGTON PROPERTY MGMT. 30 LEWIS ST. HARTFORD, CT 06103
	MCM SITE # CT-520
	238/ 0106/ 00101-00106
	41° 17' 59.543" N 72° 55' 35.570" W
	CELLCO PARTNERSHIP d.b.a. VERIZON WIRELESS 20 ALEXANDER DR. WALLINGFORD, CT 06492
S	ARLINDO NETO - CONSTRUCTION ALEKSEY TYURIN - LEASING
RY	KENNETH C. BALDWIN, ESQ. ROBINSON & COLE, LLP (860) 275-8345

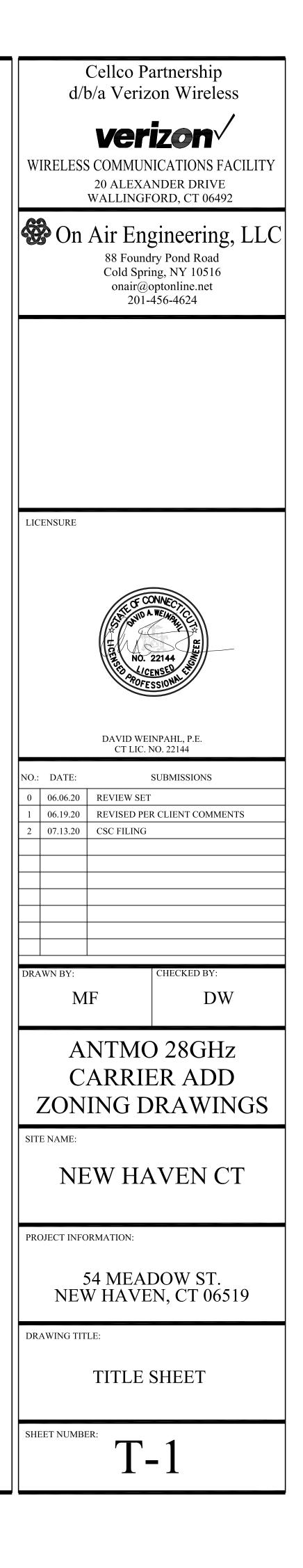
## DRAWING SCHEDULE

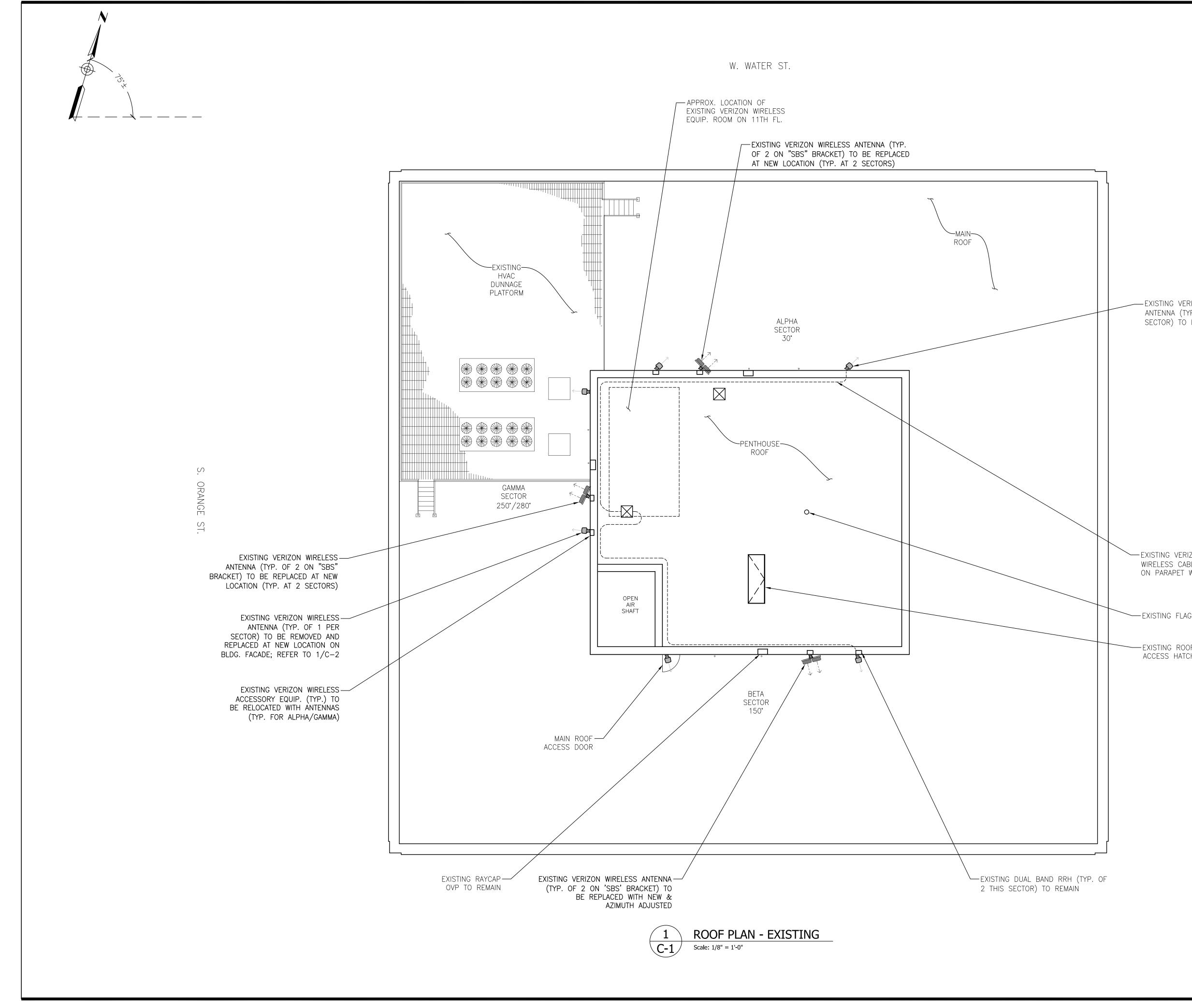
SHEET DESCRIPTION

ROOF PLAN - EXISTING

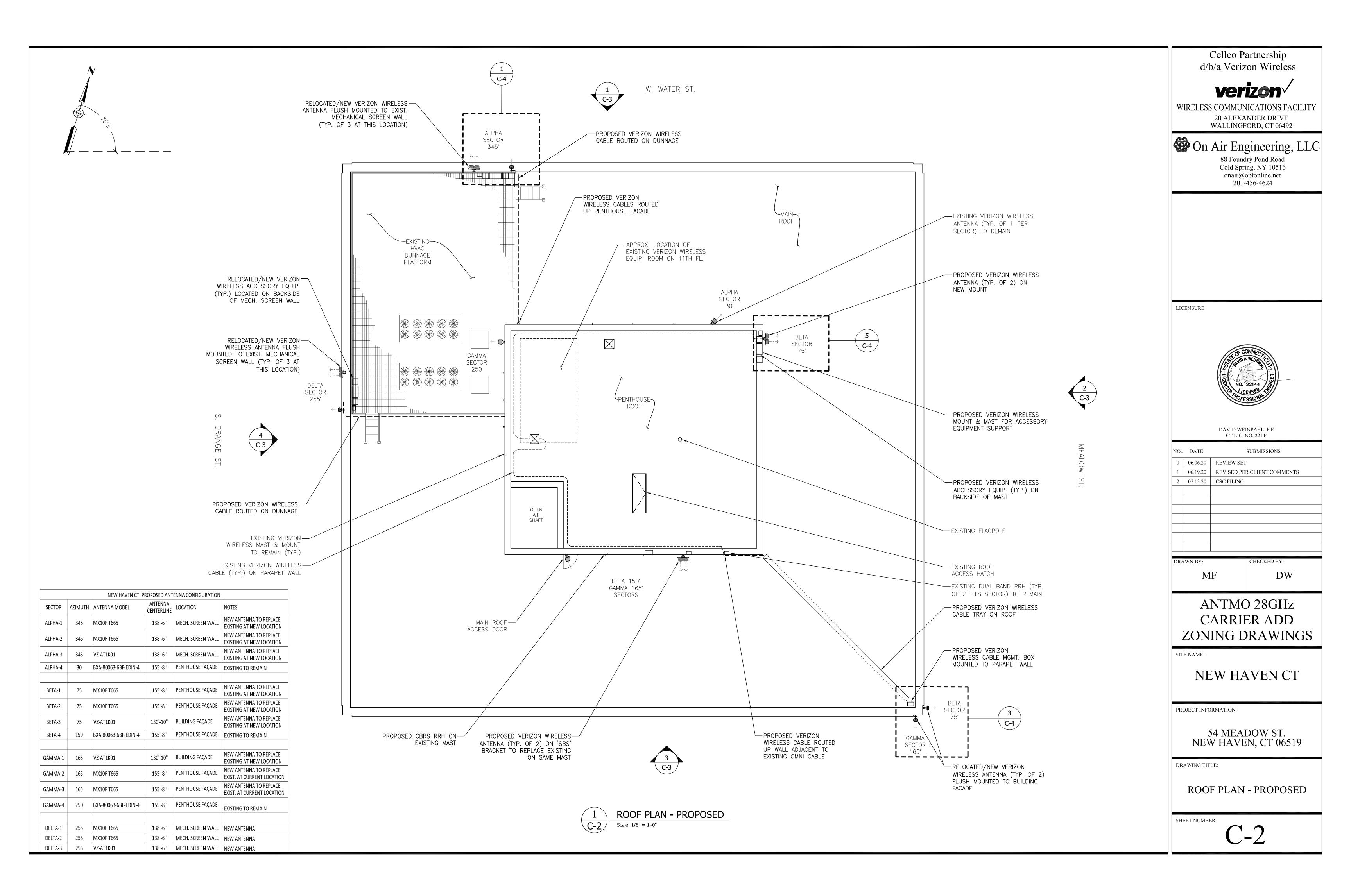
ELEVATIONS

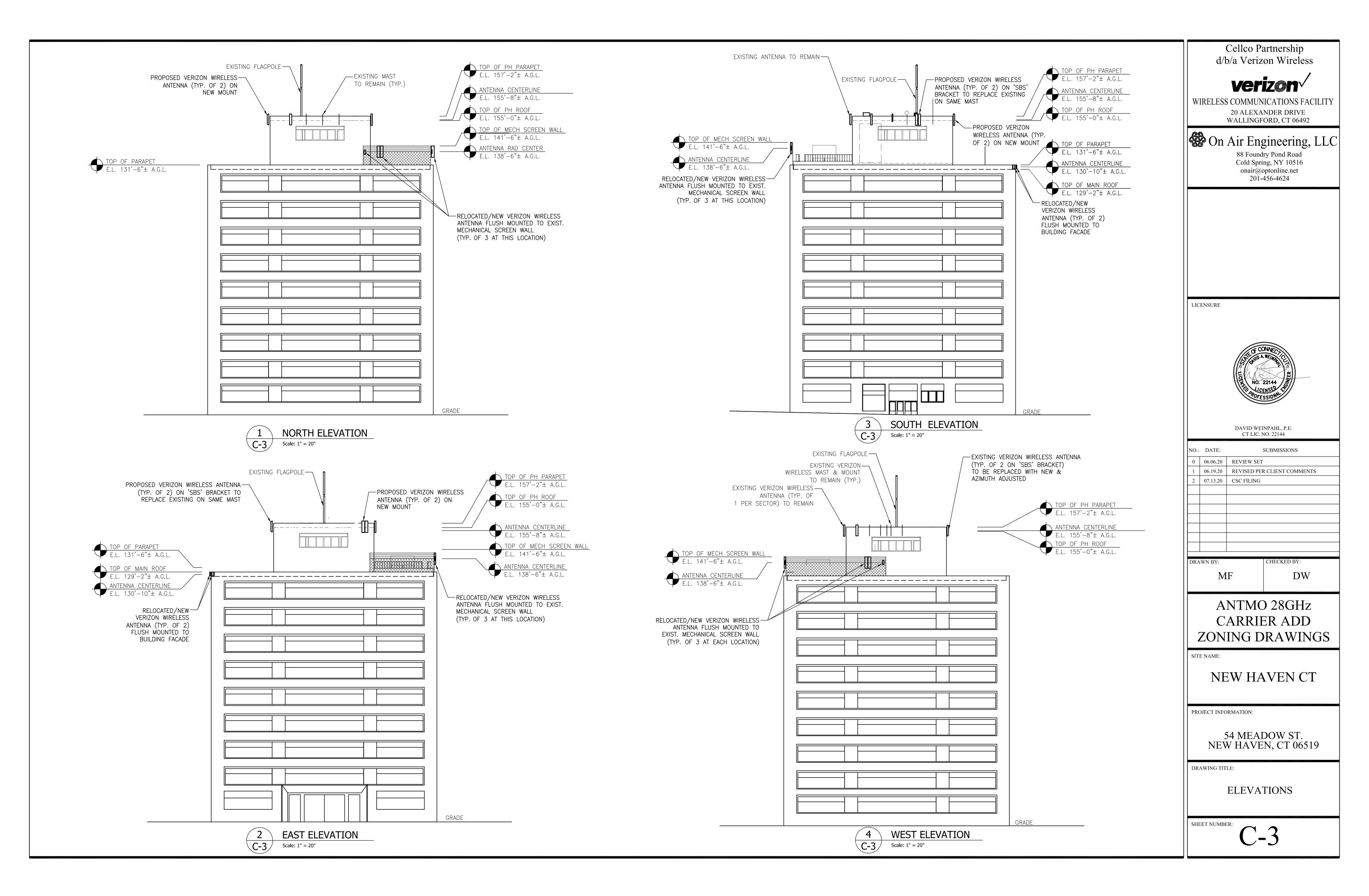
ANTENNA PLANS & SECTIONS

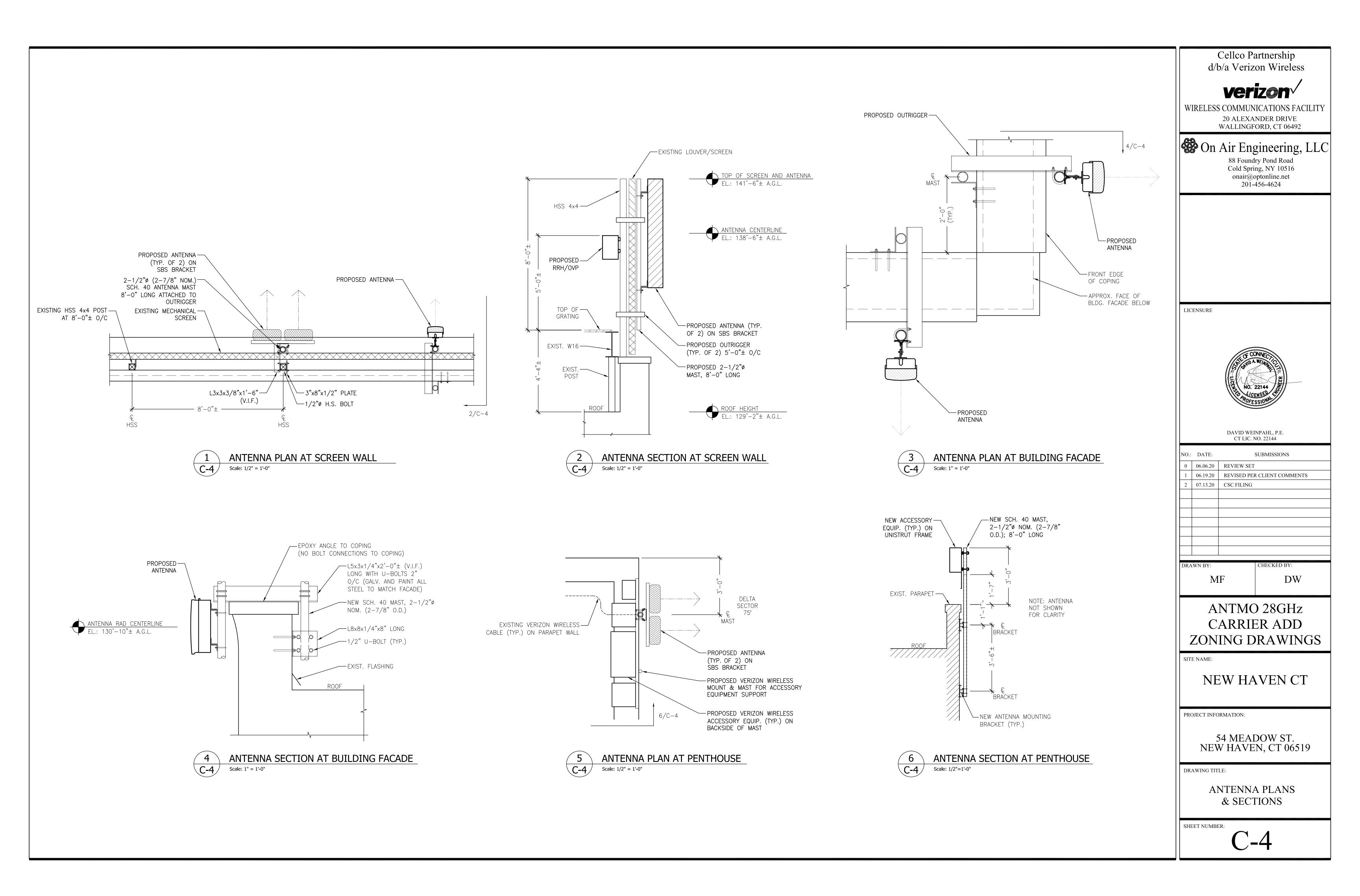




				artnership zon Wireless
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		Se On	88 Found Cold Spr onair@	gineering, LLC dry Pond Road ing, NY 10516 optonline.net -456-4624
RIZON WIRELESS 'P. OF 1 PER REMAIN		LICENSURE		
				22144 ENSED SSIONAL INPAHL, P.E.
ZON BLE (TYP.)	MEADOW ST.	NO.:       DATE:         0       06.06.20         1       06.19.20         2       07.13.20	REVIEW SET	NO. 22144 SUBMISSIONS C R CLIENT COMMENTS
WALL				
GPOLE				CHECKED BY:
)F CH		DRAWN BY:	IF	DW
		C	ARRI	D 28GHz ER ADD DRAWINGS
		SITE NAME:	EW HA	AVEN CT
		PROJECT INFO	DRMATION:	
				DOW ST. En, CT 06519
		DRAWING TIT		- EXISTING
		SHEET NUMBI	ER: C-	-1







## **ATTACHMENT 3**



## **MX10FIT665-xx**

## NWAV™ X-Pol Ten-Port Antenna

## X-Pol Ten-Port 6 ft, 65° Form in Tighter with Smart Bias Ts, 698-4200 MHz:

2 ports 698-894 MHz, 4 ports 1695-2180 MHz, and 4 ports 3400-4200 MHz

- Excellent passive intermodulation (PIM) performance reduces harmful interference.
- Fully integrated (iRETs) with independent RET control for low band and mid band
- FET configured with internal RET for high band & ease of future network optimization.
- · SON-Ready array spacing supports beamforming capabilities
- Suitable for 3G, 4G, and 5G interface technologies
- Integrated Smart Bias-Ts reduce leasing costs
- · Optimized form factor for reduced wind loading



Electrical specification (minimum/maximum)	Port	s 1, 2		Ports 3, 4, 5, 6	5
Frequency bands, MHz	698-798	824-894	1695-1880	1850-1990	1920-2180
Polarization	± 4	45°	± 45°		
Average gain over all tilts, dBi	14.4	14.8	17.8	18.1	18.2
Horizontal beamwidth (HBW), degrees <sup>1</sup>	66.0	57.0	63.0	63.0	58.0
Front-to-back ratio, co-polar power @180°± 30°, dB	>22	>22.0	>25.0	>25.0	>25.0
X-Pol discrimination (CPR) at boresight, dB	>17.0	>15.6	>23	>18	>18
Vertical beamwidth (VBW), degrees <sup>1</sup>	13.5	12.0	6.0	5.5	5.4
Electrical downtilt (EDT) range, degrees	2-14		0-9		
First upper side lobe (USLS) suppression, dB <sup>1</sup>	≤-17.0	≤-16.0	≤-17.0	≤-16.0	≤-16.0
Cross-polar isolation, port-to-port, dB <sup>1</sup>	25	25	25	25	25
Max VSWR / return loss, dB	1.5:1 / -14.0 1.5:1 / -14.0				
Max passive intermodulation (PIM), 2x20W carrier, dBc	-153 -153				
Max input power per any port, watts	300		250		
Total composite power all ports (1-10), watts	1500				

<sup>1</sup> Typical value over frequency and tilt

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MX10FIT665-xx

## PRELIMINARY

## NWAV™ X-Pol Ten-Port Antenna

Electrical specification (minimum/maximum)	Ports 7, 8, 9, 10			
Frequency bands, MHz	3400-3550	3550-3700	3700-3950	3950-4200
Polarization	± 45°			
Average gain over all tilts, dBi	13.6	13.8	14.0	14.2
Horizontal beamwidth (HBW), degrees	65	62	60	58
Front-to-back ratio, co-polar power @180°± 30°, dB	>23	>23	>23	>22
Vertical beamwidth (VBW), degrees <sup>1</sup>	20	19.6	19.3	18.5
Electrical downtilt (EDT) range, degrees	2-12 orderable in 1 deg increments			its
First upper side lobe (USLS) suppression, dB <sup>1</sup>	≤-15 ≤-15 ≤-15 ≤-15			≤-15
Cross-polar isolation, port-to-port, dB <sup>1</sup>	25	25	25	25
Max VSWR / return loss, dB	1.5:1 / -14.0			
Max input power per any port, watts	150			
Total composite power all ports (1-10), watts	1500			

<sup>1</sup> Typical value over frequency and tilt

\* For ports 7-10, the electrical downtilt is FET configured with internal RET, where the required electrical downtilt is defined at the time of order per the ordering information below.

Ordering information				
Antenna model	Description			
	6F X- Pol 10 Port FIT 65º 2-14º/ 0-9º/ 2-12º, 4.3-10 & SBTs			
MX10FIT665-xx (xx represents the FET in one degree increments for 3.4-4.2 GHz)	xx=02 thru 12 for each 1 degree tilt 3.4-4.2 GHz Examples MX10FIT665-02 – 2deg, MX10FIT665-09 – 9deg, MX10FIT665-12- 12deg			
Optional accessories				
AISG cables	M/F cables for AISG connections			
PCU-1000 RET controller	Stand-alone controller for RET control and configurations			
91900314-02	Dual Mount Bracket (see 91900314 bracket document for details)			



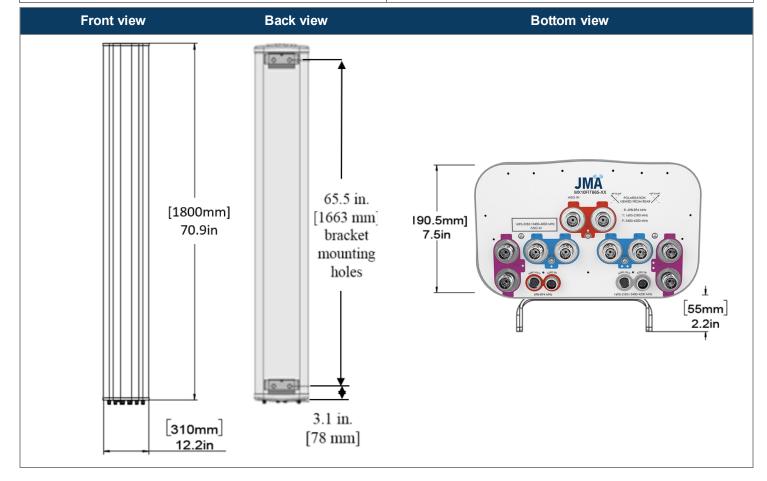
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**MX10FIT665-xx** 

## NWAV™ X-Pol Ten-Port Antenna

PRELIMINARY

Mechanical specifications	
Dimensions height/width/depth, inches (mm)	70.9/ 12.2/ 7.5 (1800/ 309.9/ 190.5)
Shipping dimensions length/width/height, inches (mm)	76/20/14.5 (1930/508/368)
No. of RF input ports, connector type, and location	10 x 4.3-10 female, bottom
RF connector torque	96 lbf·in (10.85 N·m or 8 lbf·ft)
Net antenna weight, lb (kg)	53.4 (24.3)
Shipping weight, Ib (kg)	97.5 (44.3)
Antenna mounting and downtilt kit included with antenna	91900318
Net weight of the mounting and downtilt kit, lb (kg)	20.3 (9.2)
Range of mechanical up/down tilt	-2° to 12°
Rated wind survival speed, mph (km/h)	150 (241)
Frontal, lateral, and rear wind loading @ 150 km/h, lbf (N)	74.1 (330), 26.1 (116), 69.8 (311)
Equivalent flat plate @ 100 mph and Cd=2, sq ft	1.49



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MX10FIT665-xx

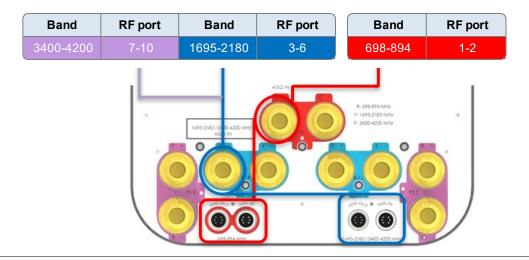
## PRELIMINARY

## NWAV™ X-Pol Ten-Port Antenna

Remote electrical tilt (RET 1000) information	
RET location	Integrated into antenna
RET interface connector type	8-pin AISG connector per IEC 60130-9 or RF port bias-t
RET connector torque	Min 0.5 N $\cdot m$ to max 1.0 N $\cdot m$ (hand pressure & finger tight)
RET interface connector quantity	2 pairs of AISG male/female connectors and 2 RF port bias-ts
RET interface connector location	Bottom of the antenna
Total no. of internal RETs 698-894 MHz	1
Total no. of internal RETs 1695-2180 MHz	1
Total no. of internal RETs 3400-4200 MHz	1
RET input operating voltage, vdc	10-30
RET max power consumption, idle state, W	≤ 2.0
RET max power consumption, normal operating conditions, W	≤ 13.0
RET communication protocol	AISG 2.0 / 3GPP

## **RET and RF connector topology**

Each RET device can be controlled either via the designated external AISG connector or RF smart bias-t port as shown below:



Note: The RET Device for 3400-4200 MHz is connected via the 1695-2180 Port 3 Bias T port or 1695-2180/3400-4200 MHz AISG ports.

Array topology		
5 sets of radiating arrays	Band	RF port
R1: 698-894 MHz	698-894	1-2
B1: 1695-2180 MHz B2: 1695-2180 MHz	1695-2180	3-4
P1: 3400-4200 MHz P2: 3400-4200 MHz	1695-2180	5-6
1 2. 3400-4200 Will2	3400-4200	7-8
	3400-4200	9-10

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## SAMSUNG

## Dual-Band Radio Unit 700/850MHz (B13/B5) RFV01U-D2A

Samsung's RFV01U-D2A is a compact remote Radio Unit (RU) designed for deployments that require flexibility in installation and rapid onlining, without compromising on coverage, capacity or operational expenses.



The RFV01U-D2A RU targets dual-band support across Band 13 (700MHz) and Band 5 (850MHz), making it an ideal product for broad coverage footprints across multiple common low-end, long-range frequencies.

The RU handles all Radio Frequency (RF) processing in a single, compact unit, and is designed to interface via CPRI with Samsung's CDU baseband offerings, in both distributedand central-RAN configurations.

In addition to its minimal footprint and ease of installation, the RU is also designed to reduce cost of ownership through its integrated spectrum analyzer, which allows for remote RF monitoring, greatly reducing the need for on-site maintenance visits.

Features and Benefits

- Dual-band support for broad frequency coverage
- Minimal footprint reduces site costs
- Rapid, easy installation
- Flexibly deployable in any location
- Remote RF monitoring capability
- Convection cooled, silent operation

Key Technical Specifications

Duplex Type: FDD Operating Frequencies: B13: DL(746-756MHz)/UL(777-787MHz) B5: DL(869-894MHz)/UL(824-849MHz) Instantaneous Bandwidth: 10MHz(B13) + 25MHz(B5) RF Chain: 4T4R/2T4R/2T2R Output Power: Total 320W DU-RU Interface: CPRI (10Gbps) Dimensions: 380 x 380 x 207mm (29.9L) Weight: 31.9kg Input Power: -48V DC Operating Temp.: -40 - 55°(w/o solar load) Cooling: Natural convection

## SAMSUNG

## Dual-Band Radio Unit AWS/PCS (B66/B2) RFV01U-D1A

Samsung's RFV01U-D1A is a compact remote Radio Unit (RU) designed for deployments that require flexibility in installation and rapid onlining, without compromising on coverage, capacity or operational expenses.



The RFV01U-D1A RU targets dual-band support across Band 66 (AWS) and Band 2 (PCS), making it an ideal product for broad coverage footprints across multiple common mid-range frequencies.

The RU handles all Radio Frequency (RF) processing in a single, compact unit, and is designed to interface via CPRI with Samsung's CDU baseband offerings, in both distributed-and central-RAN configurations.

In addition to its minimal footprint and ease of installation, the RU is also designed to reduce cost of ownership through its integrated spectrum analyzer, which allows for remote RF monitoring, greatly reducing the need for on-site maintenance visits.

Features and Benefits

- Dual-band support for broad frequency coverage
- Minimal footprint reduces site costs
- Rapid, easy installation
- Flexibly deployable in any location
- Remote RF monitoring capability
- Convection cooled, silent operation
- Built-in Broadcast Auxiliary Services (BAS) filter ensures compliant AWS operation without impacting footprint

Key Technical Specifications

Duplex Type: FDD Operating Frequencies: B66: DL(2,110-2,180MHz)/UL(1,710-1,780MHz) B2: DL(1,930-1,990MHz)/UL(1,850-1,910MHz) Instantaneous Bandwidth: 70MHz(B66) + 60MHz(B2) RF Chain: 4T4R/2T4R/2T2R Output Power: Total 320W DU-RU Interface: CPRI (10Gbps) Dimensions: 380 x 380 x 255mm (36.8L) Weight: 38.3kg Input Power: -48V DC Operating Temp.: -40 -  $55^{\circ}$ (w/o solar load) Cooling: Natural convection

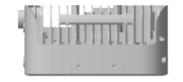
## **Specifications**

The table below outlines the main specifications of the AU:

### Table 1. Specifications

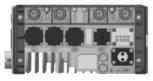
ltem		AT1K01		
Technology		5G NR		
Operating F	requency	27.5 to 28.35 GHz		
RF Chain		1024 TR/unit		
Antenna	Configuration	1024 AE (4T4R)		
Array	Element	256 AE (16H16V)/path, 1024 AE/unit		
	Gain	28 dBi/path		
IBW/OBW	•	850/800 MHz		
Channel Ba	ndwidth/Capacity	100 MHz Max 8CC (50/200/400 MHz will be supported in ES2, SVR19A: 100 MHz)		
RF Output F	Power	26 dBm/path, 32 dBm/unit		
Input Voltag	е	-48 V DC (-36 to -58 V DC) or 100 to 240 V AC		
Input Current		10.9 A @ -48 V DC 4.3 A @ 100 to 240 V AC		
LED		Total: 1 EA Powered, Operational, Fail (3 Status w/different colors)		
Operational	Temperature	-40~55°C (with solar load)		
Humidity		TBD		
IP rating		IP65		
EMC		FCC Title 47 CFR Part 15 Subpart B		
Safety		UL 60950 or 62368		
Installation		Pole/Wall/Tower mounting		
Dimension (W × D × H)		<ul> <li>9.57 in. (243 mm) × 6.89 in. (175 mm) × 16.81 in. (427 mm) •(@without cover)</li> <li>9.57 in. (243 mm) × 6.89 in. (175 mm) × 19.4 in. (493 mm) (@with</li> </ul>		
		cover & GPS Port)		
Volume		< 18.16 L		
Weight		< 33.07 lb (15.8 kg)		

## [CBRS RRH] Spec.









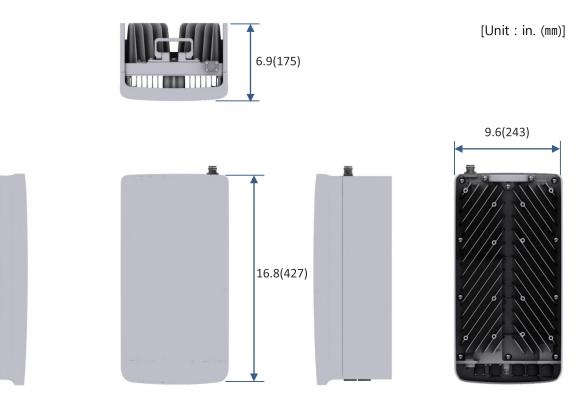
Current Size: 216 x 307 x 105.5 mm (6.99L) (8.5 x 12.1 x 4.1 inch., excluding Port Guard) Design is subject to minor change

Item	Specification		
Band	Band 48 (3.5 GHz)		
Frequency	3550~3700 MHz		
IBW	150 MHz		
OBW	80 MHz		
# of Carriers	5/10/15/20 MHz x 4 carriers		
RF Chain	4TX / 4RX		
RF Output Power	4 path x 5 W (Total: 20 W = 43 dBm)		
& EIRP	(EIRP: 47 dBm / 10 MHz)		
RX Sensitivity	Typical : -101.5 dBm @ 1 Rx (3GPP 36.104, Wide Area)		
Modulation	256-QAM support (1024-QAM with 1~2dB power back-off)		
Input Power	-48 VDC (-38 to -57 VDC, 1 SKU),		
Input Power	with clip-on AC-DC converter (Option)		
Power Consumption	About 160 Watt @ 100% RF load, typical conditions		
Volume	Under 7L (w/o Antenna), Under 9.6L (with antenna)		
Weight	Under 8.0 kg (18.64 lb) (w/o Antenna), Under 10.5 Kg (with a		
Operating Temperature	-40°C (-40°F) ~ 55°C (131°F) (W/o solar load)		
Cooling	Natural convection		
Unwanted Emission	3GPP 36.104 Category A		
Onwanted Emission	[B48] : FCC 47 CFR 96.41 e)		
Optic Interface	20km, 2 ports (9.8Gbps x 2), SFP, single mode, duplex or Bi-Di		
CPRI Cascade	Not supported		
# of Antenna Port	4		
External Alarm (UDA)	4		
RET	AISG 2.2		
TMA & built-in Bias-T I//F	Not supported		
and PIM cancellation			
Mounting Options	Pole, wall, tower, back to back, side by side (for external ant),		
Mounting Options	3 RRH with Clip-on Antenna on the pole		
Antenna Type	Integrated (Clip-on) antenna (Option),		
Antenna Type	External antenna (Option)		
NB-IoT	Not Supported (HW Resource reserved		
	for 1 Guard Band NB-IoT per LTE carrier)		
Spectrum Analyzer	TX/RX Support		
External Alarm (UDA)	4		
5G NR	Support with S/W upgrade		
XRAN	Support with S/W upgrade		

## 5G NR AU (AT1K01) Product Specifications

	28GHz	39GHz	
Integrated AU			
Operating frequency	26.5 ~ 29. 5GHz	37 ~ 40GHz	
IBW/OBW	850MHz/800MHz	1.4GHz/800MHz	
EIRP	60dBm	59dBm	
Antenna Gain	25dBi	24dBi	
Tx/Rx	4T4R		
Antenna Elements	1,024		
Beam Scan Range	120Н / 4	.0V	
Size/Weight	9.6 x 16.8 x 6.9 in (18.1	L) / 15.0Kg (33lbs)	
Input Power	-48VDC / 100 ^	~ 240VAC	
Power Consumption	362W	,	
Midhaul (gNB-CU Interface)	10G Optic x 2 ports		
Installation	Outdoor Pole/Wall Mount		
Clock Synchronization	GPS and IEEE 1588v2		
Operating Temperature	-40 deg C to +55 deg C with solar load		
Cooling	Natural Convection		

## Appearance





量

## **ATTACHMENT 4**

## On Air Engineering, LLC

88 Foundry Pond Road Cold Spring, NY 10516 onair@optonline.net

July 13, 2020

Mr. Aleksey Tyurin Verizon Wireless 20 Alexander Drive Wallingford, CT 06492

Re: New Haven CT - Structural Assessment Letter – ANTMO 28GHz Carrier Add/Sector Add MCM Site # CT-520; 54 Meadow St., New Haven, CT

Dear Aleksey:

This letter serves as a Structural Assessment for the proposed Cellco Partnership (d/b/a Verizon Wireless) antenna modification on the above referenced building.

Verizon Wireless is proposing to modify their existing 3-sector antenna configuration with a 4-sector configuration by replacing existing antennas, adding new antennas and relocating several antennas on the structure. The proposed antenna locations are detailed in Zoning Drawings prepared by our office dated July 13, 2020. Verizon's equipment room is located on the 11th floor inside the building.

Verizon's existing (12) panel antennas are all flush mounted to the central penthouse façade, extending approx. 18" above the parapet wall. The proposed re-configuration will maintain (7) antenna positions on the penthouse, some of which are being relocated to new mounts on the eastern penthouse facade. Verizon's other (5) antennas will be replaced and relocated to the existing mechanical HVAC screen wall framing in the northwest corner of the roof and supplemented with a sixth antenna, all flush mounted to that structure. Lastly, two additional antennas are proposed in southeast corner of the building, mounted to the inside parapet wall and extending over the top to achieve a "flush mount" appearance. Verizon's existing RRH's and OVP's will also be replaced, relocated and supplemented with new equipment as part of the modification, which will yield a total of (15) panel antennas upon completion.

The building structural components have been evaluated for this proposed modification, including the new antenna mounts and we have determined that they are capable of supporting the proposed loading, as per the attached structural calculations.

In conclusion, the proposed Verizon Wireless modification will not negatively impact the structural integrity of the host building and will be installed in accordance with the 2018 Connecticut State Building Code, adopted model codes (as amended) and all referenced standards, including TIA-222-G. Our findings are based on the assumption that the hosting structure and all structural members and appurtenances were properly designed, detailed, fabricated, installed and have been properly maintained since erection. Should you have any questions, please do not hesitate to contact our office.

Very touly yours, David A. Weimpahl, P.E. CT License No. 22144 Managing Partner On Air Engineering, LLC DW:dw

enclosure

## STRUCTURAL CALCULATIONS

FOR

VERIZON SITE NAME: NEW HAVEN CT 54 MEADOW ST NEW HAVEN, CT

> DAVID A. WEINPAHL, P.E. ON AIR ENGINEERING, LLC 88 FOUNDRY POND ROAD COLD SPRING, NY 10516

PAUL C. BECK, P.E.

LICENSE NO. (CT) 12949 PRESIDENT

PBA ENGINEERING, P.C. 12 KULICK ROAD FAIRFIELD, NEW JERSEY 07004-3363 PHONE: (973) 276-1700 FAX: (973) 276-9766

## STRUCTURAL ENGINEERS PROJECT NO. N-545 DATE: 6/15/2020 TOTAL NO. PAGES ATTACHED: 17

(APPENDIX N) MUNICIPALITY - SPECIFIC STRUCTURAL DESIGN PARAMETERS Wind Design Parameters												
							Wind D	esign P	aramet	ers		
pality	Snow ad	Spe Accele	Spectral Wind Speeds, Vult Wind Sp			ninal Des Speeds (mph)		Del Regi	Wind-Borne Debris Regions <sup>1</sup>			
Municipality	Ground Snow Load	S₅	S <sub>1</sub>	Risk Cat.l	Risk Cat.II	Risk Cat III-IV	Risk Cat. I	Risk Cat. II	Risk Cat. III-IV	Risk Cat. II & III except Occup I-2	Risk Cat III Occup I-2 & Risk Cat. IV	Hurricane-Prone Regions
New Haven	30	0.186	0.062	115	125	135	89	97	105		Type C	Yes
Newington	30	0.182	0.064	115	125	135	89	97	105			
New London	30	0.161	0.058	125	135	145	97	105	112	Туре В	Type A	Yes
New Milford	35	0.198	0.066	105	115	125	81	89	97			
Newtown	30	0.208	0.066	110	120	130	85	93	101			Yes
Norfolk	40	0.175	0.065	105	115	125	81	89	97			
North	30	0.179	0.061	120	130	140	93	101	108			Yes
Branford												
North Canaan	40	0.173	0.065	105	115	120	81	89	93			
North Haven	30	0.184	0.062	115	125	135	89	97	105			Yes
North Stonington	30	0.163	0.059	125	135	145	97	105	112		Type A	Yes
Norwalk	30	0.232	0.067	110	120	130	85	93	101			Yes
Norwich	30	0.168	0.060	125	135	145	97	105	112		Type A	Yes
Old Lyme	30	0.164	0.059	125	135	145	97	105	112	Туре В	Type A	Yes
Old Saybrook	30	0.164	0.059	125	135	145	97	105	112	Type B	Type A	Yes
Orange	30	0.192	0.063	115	125	135	89	97	105			Yes
Oxford	30	0.196	0.064	110	125	130	85	97	101			Yes
Plainfield	35	0.170	0.061	125	135	145	97	105	112		Type A	Yes
Plainville	35	0.184	0.064	115	125	135	89	97	105			Yes
Plymouth	35	0.186	0.064	110	120	130	85	93	101			Yes
Pomfret	40	0.172	0.063	120	130	140	93	101	108			Yes
Portland	30	0.180	0.063	115	130	135	89	101	105			Yes
Preston	30	0.167	0.060	125	135	145	97	105	112		Type A	Yes
Prospect	30	0.188	0.064	115	125	135	89	97	105			Yes
Putnam	40	0.172	0.063	120	130	140	93	101	108			Yes
Redding	30	0.220	0.067	110	120	130	85	93	101			Yes
Ridgefield	30	0.230	0.068	110	120	125	85	93	97			Yes
Rocky Hill	30	0.181	0.063	115	125	135	89	97	105			Yes
Roxbury	35	0.197	0.065	110	120	125	85	93	97			Yes
Salem	30	0.170	0.060	120	135	140	93	105	108		Туре А	Yes
Salisbury	40	0.173	0.065	105	115	120	81	89	93			X
Scotland	30	0.172	0.061	120	130	140	93	101	108			Yes
Seymour	30	0.194	0.064	115	125	135	89	97	105			Yes
Sharon	40	0.179	0.065	105	115	120	81	89	93			Ver
Shelton	30	0.199	0.064	115	125	135	89	97	105			Yes
Sherman	35	0.202	0.066	105	115	120	81	89	93			Vac
Simsbury	35	0.179	0.064	110	120	130	85	93	101			Yes
Somers	35 35	0.174	0.064	115	125	135	89 85	97 93	105 101			Yes Yes
Southbury	35 30	0.198	0.065	110 115	120 125	<u>130</u> 135		93 97	101			
Southington	30	0.185	0.064	115	125	135	89 89	97 97	105			Yes Yes
South Windsor	30	0.170	0.064	115	120	135	09	97	105			res

#### MecaWind v2333

Software Developer: Meca Enterprises Inc., www.meca.biz, Copyright © 2018

Calculations Prepared by: Date: Jun 12, 2020

FileLocation : U:\Mike\N-Jobs\N-545\N-545.wnd

#### Basic Wind Parameters

Wind Load Standard	= ASCE 7-16	Exposure Category	= B
Wind Design Speed	= 125.0 mph	Risk Category	= II
Structure Type	= Other	Other Structure Type	= Solid Sign
General Wind Settings			
<pre>Incl_LF = Include ASD Load</pre>	Factor of 0.6	in Pressures	= False
DynType = Dynamic Type of S	tructure		= Rigid
NF = Natural Frequency	of Structure	(Mode 1)	= 1.000 Hz
Zg = Altitude (Ground	Elevation) abov	ve Sea Level	= 0.000 ft
Bdist = Base Elevation of	Structure		= 0.000 ft
Reacs = Show the Base Rea	ctions in the d	output	= False
MWFRSType = MWFRS Method Sele	ected		= Ch 27 Pt 1
Topographic Factor per Fig 26			
Topo = Topographic Featu			= None
Kzt = Topographic Facto	r		= 1.000
Solid Sign Inputs	1 4 1 5 0 0 5		
		B : Horizontal Width of Sigr	
		s : Vertical Height of Sign	
e : Solidity Ratio	= 1.000	Att: Attached to Wall	= False
European Constants nor Wahle	26 11 1.		
Exposure Constants per Table		Za. Const from Moble 26 1	1- 1200 000 5-

## Alpha:Const from Table 26.11-1= 7.000Zg:Const from Table 26.11-1= 1200.000 ftAt:Const from Table 26.11-1= 0.143Bt:Const from Table 26.11-1= 0.840Am:Const from Table 26.11-1= 0.250Bm:Const from Table 26.11-1= 0.450C:Const from Table 26.11-1= 0.300Eps:Const from Table 26.11-1= 0.333

#### Gust Factor Calculation:

Gust Factor Category I Rigid Structures - Simplified Method	
G1 = For Rigid Structures (Nat. Freq.>1 Hz) use 0.85	= 0.85
Gust Factor Category II Rigid Structures - Complete Analysis	
Zm = 0.6 * Ht	= 84.900 ft
$Izm = Cc * (33 / Zm) ^ 0.167$	= 0.256
Lzm = L * (Zm / 33) ^ Epsilon	= 438.478
$Q = (1 / (1 + 0.63 * ((B + Ht) / Lzm)^{0.63}))^{0.5}$	= 0.873
G2 = 0.925*((1+1.7*1zm*3.4*Q)/(1+1.7*3.4*1zm))	= 0.855
Gust Factor Used in Analysis	
G = Lessor Of G1 Or G2	= 0.850

### Main Wind Force Resisting System (MWFRS) Calculations for Solid Sign per Ch 29:

LF	= Load Factor based upon STRENGTH Design	= 1.00
hs	= Overall height of structure	= 141.500 ft
h	= Mean Roof Height above grade	= 141.500 ft
Kh	= 15 ft [4.572 m] < Z <zg>(2.01*(Z/zg)^(2/Alpha) {Table 26.10-1</zg>	}= 1.091
Kzt	= Topographic Factor is 1 since no Topographic feature specified	= 1.000
Kd	= Wind Directionality Factor per Table 26.6-1	= 0.85
qh	= (0.00256 * Kh * Kzt * Kd * Ke * V^2) * LF	= 37.10 psf
MWFRS Pre	essures on Solid Sign per Fig 29.3-1:	
<b>MWFRS Pre</b> R	essures on Solid Sign per Fig 29.3-1: = Reduction factor to account for openings: (1-(1-e)^1.5)	= 1.000
		= 1.000 = 1.000
R	= Reduction factor to account for openings: (1-(1-e)^1.5)	
R Rc	<pre>= Reduction factor to account for openings: (1-(1-e)^1.5) = Reduction factor for Case C not applicable since s/h &lt;= 0.8</pre>	= 1.000
R Rc As	<pre>= Reduction factor to account for openings: (1-(1-e)^1.5) = Reduction factor for Case C not applicable since s/h &lt;= 0.8 = Gross Area of Sign: B * s</pre>	= 1.000 = 24.00 sq ft
R Rc As B/s	<pre>= Reduction factor to account for openings: (1-(1-e)^1.5) = Reduction factor for Case C not applicable since s/h &lt;= 0.8 = Gross Area of Sign: B * s = Aspect Ratio: B / s</pre>	= 1.000 = 24.00 sq ft = 0.375

Case A: F	Resultant force acts normal to face through geometric center = Design Wind force: qh * G * Cf * As * R	= 1400 lb
Case B:	Resultant force acts normal to face at a distance from the geometri center toward the windward edge equal to 0.2 times the average widt	
Dx	= Force Offset from Center toward windward edge: 0.2 * B	= 0.600 ft
F	= Design Wind force: qh * G * Cf * As * R	= 1400 lb
Case C:	Since $B/s < 2$ then Case C need not be considered	





Project Title: Engineer: Project ID: Project Descr:

> Fy : Steel Yield : E: Modulus :

35.0 ksi 29,000.0 ksi

Design OK

Service loads entered. Load Factors will be applied for calculations.

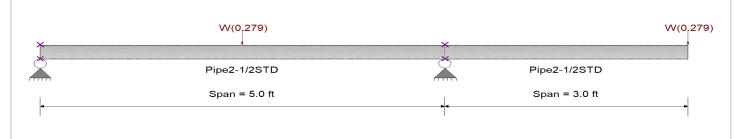
## Steel Beam File: N-545.ec6 Software copyright ENERCALC, INC. 1983-2020, Build:12.20.3.25 Lic. # : KW-06000304 PBA ENGINEERING, P.C. DESCRIPTION: New Antenna Pipe Mast

### **CODE REFERENCES**

Calculations per AISC 360-16, IBC 2018, CBC 2019, ASCE 7-16 Load Combination Set : ASCE 7-16

### **Material Properties**

Analysis Method :	Allowable Strength Design
Beam Bracing :	Completely Unbraced
Bending Axis :	Major Axis Bending



### **Applied Loads**

Beam self weight NOT internally calculated and added Load(s) for Span Number 1 Point Load : W = 0.2790 k @ 2.50 ft

Load(s) for Span Number 2 Point Load : W = 0.2790 k @ 3.0 ft

## **DESIGN SUMMARY**

DEGICIN COMMANY			Boolgii Oik
Maximum Bending Stress Ratio =	0.210:1	Maximum Shear Stress Ratio =	<b>0.018</b> : 1
Section used for this span	Pipe2-1/2STD	Section used for this span	Pipe2-1/2STD
Ma : Applied	0.502 k-ft	Va : Applied	0.1841 k
Mn / Omega : Allowable	2.393 k-ft	Vn/Omega : Allowable	10.123 k
Load Combination	+D+0.60W+H	Load Combination	+D+0.60W+H
Location of maximum on span	5.000ft	Location of maximum on span	2.520 ft
Span # where maximum occurs	Span # 1	Span # where maximum occurs	Span # 1
Maximum Deflection			
Max Downward Transient Deflection	0.221 in Ratio		
Max Upward Transient Deflection	-0.028 in Ratio	<b>=</b> 2,161 >=180.	
Max Downward Total Deflection	0.133 in Ratio		
Max Upward Total Deflection	-0.017 in Ratio	<b>=</b> 3602 >=180.	

### **Maximum Forces & Stresses for Load Combinations**

Load Combination		Max Stres	s Ratios		9	Summary of Mo	oment Valu	ies			Summa	ary of Sh	ear Values
Segment Length	Span #	М	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
+D+H													
Dsgn. L = 5.00 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L = $3.00 \text{ ft}$	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+L+H													
Dsgn. L = 5.00 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L = $3.00 \text{ ft}$	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+Lr+H													
Dsgn. L = 5.00 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L = $3.00 \text{ ft}$	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+S+H													
Dsgn. L = 5.00 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L = $3.00 \text{ ft}$	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+0.750Lr+0.750L+H													
Dsgn. L = 5.00 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L = $3.00 \text{ ft}$	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+0.750L+0.750S+H													
Dsgn. L = 5.00 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L = $3.00 \text{ ft}$	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+0.60W+H													

## **Steel Beam** Lic. # : KW-06000304

File: N-545.ec6 Software copyright ENERCALC, INC. 1983-2020, Build:12.20.3.25 PBA ENGINEERING, P.C.

## DESCRIPTION: New Antenna Pipe Mast

Load Combination		Max Stres	ss Ratios		S	Summary of M	oment Valu	es			Summ	ary of Sh	ear Values
Segment Length	Span #	М	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
Dsgn. L = 5.00 ft	1	0.210	0.018		-0.50	0.50	4.00	2.39	2.72	1.00	0.18	16.91	10.12
Dsgn. L = 3.00 ft	2	0.210	0.017		-0.50	0.50	4.00	2.39	1.00	1.00	0.17	16.91	10.12
+D+0.750Lr+0.750L+0.450\	W+H												
Dsgn. L = 5.00 ft	1	0.157	0.014		-0.38	0.38	4.00			1.00	0.14	16.91	10.12
Dsgn. L = $3.00 \text{ ft}$	2	0.157	0.012		-0.38	0.38	4.00	2.39	1.00	1.00	0.13	16.91	10.12
+D+0.750L+0.750S+0.450V													
Dsgn. L = $5.00 \text{ ft}$	1	0.157	0.014		-0.38	0.38	4.00			1.00	0.14	16.91	10.12
Dsgn. L = $3.00$ ft	2	0.157	0.012		-0.38	0.38	4.00	2.39	1.00	1.00	0.13	16.91	10.12
+0.60D+0.60W+0.60H	1	0.010	0.010		0.50	0.50	4.00	2.20	0 70	1 00	0.10	1/ 01	10.10
Dsgn. L = $5.00 \text{ ft}$	1 2	0.210 0.210	0.018 0.017		-0.50 -0.50	0.50	4.00 4.00			1.00 1.00	0.18 0.17	16.91 16.91	10.12 10.12
Dsgn. L = 3.00 ft +D+0.70E+0.60H	Z	0.210	0.017		-0.50	0.50	4.00	2.39	1.00	1.00	0.17	10.91	10.12
Dsgn. L = 5.00 ft	1		0.000				4.00	2.39	1 00	1.00	-0.00	16.91	10.12
Dsgn. L = $3.00 \text{ ft}$	2		0.000				4.00			1.00	-0.00	16.91	10.12
+D+0.750L+0.750S+0.5250			0.000				4.00	2.57	1.00	1.00	0.00	10.71	10.12
Dsqn. L = 5.00 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L = 3.00 ft	2		0.000				4.00			1.00	-0.00	16.91	10.12
+0.60D+0.70E+H													
Dsgn. L = 5.00 ft	1		0.000				4.00			1.00	-0.00	16.91	10.12
Dsgn. L = 3.00 ft	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Overall Maximu	m Defle	ctions											
Load Combination		Span	Max. "-" Defl	Location	in Span	Load Com	bination			Max	(. "+" Defl	Locatio	n in Span
		1	0.0000		0.000	W Only					-0.0278		3.380
W Only		2	0.2211		3.000						0.0000		3.380
Vertical Reactio	ns				Support	notation : Far	left is #1			Values i	n KIPS		
Load Combination		Support 1	Support 2	Support	3								
Overall MAXimum		-0.028	0.586										
Overall MINimum		-0.013	0.264										
+D+0.60W+H		-0.017	0.352										
+D+0.750Lr+0.750L+0.4	450W+H	-0.013	0.264										
+D+0.750L+0.750S+0.4	50W+H	-0.013	0.264										
+0.60D+0.60W+0.60H		-0.017	0.352										
W Only		-0.028	0.586										
H Only													

Project Title: Engineer: Project ID: Project Descr:

Steel Beam		File: N-545.ec6 Software copyright ENERCALC, INC. 1983-2020, Build:12.20.3.25
Lic. # : KW-06000304		PBA ENGINEERING, P.C
DESCRIPTION: Existing Screen Verticals		
CODE REFERENCES		
Calculations per AISC 360-16, IBC 2018, CBC 2019	9, ASCE 7-16	
Load Combination Set : ASCE 7-16		
Material Properties		
Analysis Method : Allowable Strength Design		Fy: Steel Yield: 46.0 ksi
Beam Bracing : Completely Unbraced		E: Modulus : 29,000.0 ksi
Bending Axis : Major Axis Bending		
W(-0.028)	\\/(0.1113)	W(0,586)
★ ★ ★	W(0.1113)	\$ •
$\widehat{1}$		
HSS4x4x1/4	HSS4x4x	:1/4
Span = 1.330 ft	Span = 8.	.0 ft
<b>▲ • • •</b> •		•
Applied Loads	Service	loads entered. Load Factors will be applied for calculations.
Beam self weight NOT internally calculated and added		

Loads on all spans... Uniform Load on ALL spans : W = 0.01855 ksf, Tributary Width = 6.0 ft

Load(s) for Span Number 2 Point Load : W = -0.0280 k @ 0.250 ft

Point Load : W = 0.5860 k @ 5.0 ft

## **DESIGN SUMMARY**

DESIGN SUMMARY			Design OK
Maximum Bending Stress Ratio =	<b>0.361</b> : 1	Maximum Shear Stress Ratio =	0.117:1
Section used for this span	<b>HSS4x4x1/4</b>	Section used for this span	HSS4x4x1/4
Ma : Applied	3.891 k-ft	Va : Applied	2.970 k
Mn / Omega : Allowable	10.765 k-ft	Vn/Omega : Allowable	25.423 k
Load Combination	+D+0.60W+H	Load Combination	+D+0.60W+H
Location of maximum on span	1.330ft	Location of maximum on span	1.330 ft
Span # where maximum occurs	Span # 1	Span # where maximum occurs	Span # 1
Maximum Deflection Max Downward Transient Deflection Max Upward Transient Deflection Max Downward Total Deflection Max Upward Total Deflection	0.963 in Ratio -0.006 in Ratio 0.578 in Ratio -0.003 in Ratio	0 = 2,841 >=180. 0 = 332 >=180.	

### **Maximum Forces & Stresses for Load Combinations**

Load Combination		Max Stres	s Ratios		S	Summary of M	oment Valu	ies			Summa	ary of Sh	ear Values
Segment Length	Span #	М	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
+D+H													
Dsgn. L = 1.33 ft	1		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
Dsgn. L = 8.00 ft	2		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
+D+L+H													
Dsgn. L = 1.33 ft	1		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
Dsgn. L = 8.00 ft	2		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
+D+Lr+H													
Dsgn. L = 1.33 ft	1		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
Dsgn. L = 8.00 ft	2		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
+D+S+H													
Dsgn. L = 1.33 ft	1		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
Dsgn. L = 8.00 ft	2		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
+D+0.750Lr+0.750L+H													
Dsgn. L = 1.33 ft	1		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
Dsgn. L = 8.00 ft	2		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
+D+0.750L+0.750S+H													

## **Steel Beam** Lic. # : KW-06000304

W Only

H Only

-4.802

6.398

File: N-545.ec6 Software copyright ENERCALC, INC. 1983-2020, Build:12.20.3.25 PBA ENGINEERING, P.C.

## DESCRIPTION: Existing Screen Verticals

Load Combination		Max Stress Ratios		Summary of Moment Values							Summary of Shear Values		
Segment Length	Span #	М	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
Dsqn. L = 1.33 ft	1		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
Dsgn. L = 8.00 ft	2		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
+D+0.60W+H													
Dsgn. L = 1.33 ft	1	0.361	0.117		-3.89	3.89	17.98	10.77	1.67	1.00	2.97	42.46	25.42
Dsgn. L = 8.00 ft	2	0.361	0.034		-3.89	3.89	17.98	10.77	1.00	1.00	0.87	42.46	25.42
+D+0.750Lr+0.750L+0.450	DW+H												
Dsgn. L = 1.33 ft	1	0.271	0.088		-2.92	2.92	17.98			1.00	2.23	42.46	25.42
Dsgn. L = 8.00 ft	2	0.271	0.026		-2.92	2.92	17.98	10.77	1.00	1.00	0.65	42.46	25.42
+D+0.750L+0.750S+0.450	W+H												
Dsgn. L = 1.33 ft	1	0.271	0.088		-2.92	2.92	17.98			1.00	2.23	42.46	
Dsgn. L = 8.00 ft	2	0.271	0.026		-2.92	2.92	17.98	10.77	1.00	1.00	0.65	42.46	25.42
+0.60D+0.60W+0.60H													
Dsgn. L = 1.33 ft	1	0.361	0.117		-3.89	3.89	17.98	10.77		1.00	2.97	42.46	
Dsgn. L = 8.00 ft	2	0.361	0.034		-3.89	3.89	17.98	10.77	1.00	1.00	0.87	42.46	25.42
+D+0.70E+0.60H													
Dsgn. L = 1.33 ft	1		0.000				17.98			1.00	-0.00	42.46	
Dsgn. L = 8.00 ft	2		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
+D+0.750L+0.750S+0.525													
Dsgn. L = 1.33 ft	1		0.000				17.98			1.00	-0.00	42.46	
Dsgn. L = $8.00 \text{ ft}$	2		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
+0.60D+0.70E+H			0.000				47.00	40.77	4 00	4 00	0.00	10.17	05.40
Dsgn. L = $1.33$ ft	1		0.000				17.98			1.00	-0.00	42.46	
Dsgn. L = 8.00 ft	2		0.000				17.98	10.77	1.00	1.00	-0.00	42.46	25.42
Overall Maximu	Im Defle	ctions											
Load Combination		Span	Max. "-" Defl	Location in Span		Load Combination				Max. "+" Defl		Location in Span	
		1	0.0000		0.000	W Only					-0.0056		0.771
W Only		2	0.9626		8.000						0.0000		0.771
Vertical Reactions				Support notation : Far left is #1					Values in KIPS				
Load Combination		Support 1	Support 2	Suppor	t 3								
Overall MAXimum		-4.802	6.398										
Overall MINimum		-2.161	2.879										
+D+0.60W+H		-2.881	3.839										
+D+0.750Lr+0.750L+0.450W+H		-2.161	2.879										
+D+0.750L+0.750S+0.450W+H		-2.161	2.879										
+0.60D+0.60W+0.60H		-2.881	3.839										
+0.00D+0.00W+0.00H		-2.001	3.037										

Project Title: Engineer: Project ID: Project Descr:

#### File: N-545.ec6 **Steel Beam** Software copyright ENERCALC, INC. 1983-2020, Build:12.20.3.25 Lic. # : KW-06000304 PBA ENGINEERING, P.C. DESCRIPTION: Facade Mount Vertical **CODE REFERENCES** Calculations per AISC 360-16, IBC 2018, CBC 2019, ASCE 7-16 Load Combination Set : ASCE 7-16 **Material Properties** Fy : Steel Yield : E: Modulus : Analysis Method : Allowable Strength Design 35.0 ksi Beam Bracing : Completely Unbraced 29,000.0 ksi Bending Axis : Major Axis Bending W(0.1) ₽ oe2-1/2ST Pipe2-1/2STD Span = 0.250 ft Span = 2.0 ft **Applied Loads** Service loads entered. Load Factors will be applied for calculations. Beam self weight NOT internally calculated and added Load(s) for Span Number 2 Point Load : W = 0.10 k @ 2.0 ft

DESIGN SUMMARY			Design OK
Maximum Bending Stress Ratio =	0.050:1	Maximum Shear Stress Ratio =	<b>0.047</b> : 1
Section used for this span	Pipe2-1/2STD	Section used for this span	Pipe2-1/2STD
Ma : Applied	0.120 k-ft	Va : Applied	0.480 k
Mn / Omega : Allowable	2.393 k-ft	Vn/Omega : Allowable	10.123 k
Load Combination Location of maximum on span Span # where maximum occurs	+D+0.60W+H 0.250ft Span # 1	Load Combination Location of maximum on span Span # where maximum occurs	+D+0.60W+H 0.000 ft Span # 1
Maximum Deflection Max Downward Transient Deflection Max Upward Transient Deflection Max Downward Total Deflection Max Upward Total Deflection	0.012 in Rat 0.000 in Rat 0.007 in Rat -0.000 in Rat	tio = 0 < 180.0	

### **Maximum Forces & Stresses for Load Combinations**

Load Combina	ition		Max Stress	Ratios		S	ummary of Mo	oment Valu	les			Summa	ary of Sh	ear Values
Segment	Length S	pan #	М	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
+D+H														
Dsgn. L =	0.25 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L =	2.00 ft	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+L+H														
Dsgn. L =	0.25 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L =	2.00 ft	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+Lr+H														
Dsgn. L =	0.25 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L =	2.00 ft	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+S+H														
Dsgn. L =	0.25 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L =	2.00 ft	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+0.750Lr+0.	.750L+H													
Dsgn. L =	0.25 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L =	2.00 ft	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+0.750L+0.7	750S+H													
Dsgn. L =	0.25 ft	1		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
Dsgn. L =	2.00 ft	2		0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
+D+0.60W+H														
Dsgn. L =	0.25 ft	1	0.050	0.047		-0.12	0.12	4.00	2.39	1.67	1.00	0.48	16.91	10.12
Dsgn. L =	2.00 ft	2	0.050	0.006		-0.12	0.12	4.00	2.39	1.00	1.00	0.06	16.91	10.12
+D+0.750Lr+0.	.750L+0.450W+H													
Dsgn. L =	0.25 ft	1	0.038	0.036		-0.09	0.09	4.00	2.39	1.67	1.00	0.36	16.91	10.12

## **Steel Beam** Lic. # : KW-06000304

#### File: N-545.ec6 Software copyright ENERCALC, INC. 1983-2020, Build:12.20.3.25 PBA ENGINEERING, P.C.

DESCRIPTION: Facade Mount Vertical

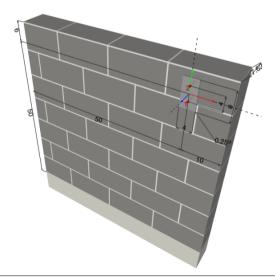
			Summary of N		03			Junn	iary 01 511	ear Values
V V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
38 0.004		-0.09	0.09	4.00	2.39	1.00	1.00	0.05	16.91	10.12
		-0.09	0.09	4.00	2.39			0.36	16.91	
38 0.004		-0.09	0.09	4.00	2.39	1.00	1.00	0.05	16.91	10.12
50 0.006		-0.12	0.12	4.00	2.39	1.00	1.00	0.06	16.91	10.12
0.000					0.00	4 00	1 00	0.00	4 / 04	10.10
0.000				4.00	2.39	1.00	1.00	-0.00	16.91	10.12
0.000				1.00	2.20	1 00	1 00	0.00	14 01	10.12
0.000				4.00	2.39	1.00	1.00	-0.00	10.91	10.12
0.000				1.00	2 30	1 00	1 00	-0.00	16 01	10.12
0.000				4.00				-0.00	16.91	
Max. "-" D	efl Locatio	on in Span	Load Com	bination			Ma	x. "+" Defl	Locatio	n in Span
0.000	0	0.000	W Only					-0.0000		0.145
0.012	3	2.000	- 1					0.0000		0.145
		Support	notation : Far	left is #1			Values i	in KIPS		
1 Support	2 Suppo	ort 3								<u> </u>
0 0.90	0									
0 0.40	5									
0 0.54	0									
	5									
5 0.70	-									
	338         0.004           338         0.036           338         0.004           338         0.004           338         0.004           338         0.004           350         0.047           350         0.006           0.000         0.000           0.000         0	Display         Display <thdisplay< th=""> <thdisplay< th=""> <thd< td=""><td>038         0.004         -0.09           038         0.036         -0.09           038         0.004         -0.09           038         0.004         -0.09           038         0.004         -0.09           050         0.047         -0.12           0.000         0.000         -0.12           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.0123         2.000         Support           1         Support 2         Support 3           00         0.900         0.405           00         0.405         0.405           00         0.540         0.540</td><td>0.004         -0.09         0.09           038         0.004         -0.09         0.09           038         0.036         -0.09         0.09           038         0.004         -0.09         0.09           038         0.004         -0.09         0.09           050         0.047         -0.12         0.12           0.000         -0.12         0.12         0.12           0.000         0.000         0.000         0.000           0.000         0.000         0.000         0.000           0.000         0.000         0.000         W Only           0.0123         2.000         Support notation : Far           1         Support 2         Support 3         Suport 3           00         0.900         0.405         30         0.540           50         0.405         30         0.540         30         0.540</td><td>0.004         -0.09         0.09         4.00           038         0.036         -0.09         0.09         4.00           038         0.004         -0.09         0.09         4.00           038         0.004         -0.09         0.09         4.00           050         0.047         -0.12         0.12         4.00           050         0.006         -0.12         0.12         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         0.000         W Only         4.00           0.000         0.000         W Only         4.00           0.0123         2.000         Support notation : Far left is #1           1         Support 2         Support 3         50           00         0.405         50</td><td>Number         Number         Number&lt;</td><td>Max         Max         Max<td>0.004         -0.09         0.09         4.00         2.39         1.00         1.00           038         0.036         -0.09         0.09         4.00         2.39         1.67         1.00           038         0.004         -0.09         0.09         4.00         2.39         1.67         1.00           038         0.004         -0.12         0.12         4.00         2.39         1.67         1.00           050         0.047         -0.12         0.12         4.00         2.39         1.67         1.00           050         0.006         -0.12         0.12         4.00         2.39         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         0.000         W Only         2.39         1.00         1.00           0.000</td><td>No. 1         No. 1         <th< td=""><td>Normality         Normality         <t< td=""></t<></td></th<></td></td></thd<></thdisplay<></thdisplay<>	038         0.004         -0.09           038         0.036         -0.09           038         0.004         -0.09           038         0.004         -0.09           038         0.004         -0.09           050         0.047         -0.12           0.000         0.000         -0.12           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.000         0.000         0.000           0.0123         2.000         Support           1         Support 2         Support 3           00         0.900         0.405           00         0.405         0.405           00         0.540         0.540	0.004         -0.09         0.09           038         0.004         -0.09         0.09           038         0.036         -0.09         0.09           038         0.004         -0.09         0.09           038         0.004         -0.09         0.09           050         0.047         -0.12         0.12           0.000         -0.12         0.12         0.12           0.000         0.000         0.000         0.000           0.000         0.000         0.000         0.000           0.000         0.000         0.000         W Only           0.0123         2.000         Support notation : Far           1         Support 2         Support 3         Suport 3           00         0.900         0.405         30         0.540           50         0.405         30         0.540         30         0.540	0.004         -0.09         0.09         4.00           038         0.036         -0.09         0.09         4.00           038         0.004         -0.09         0.09         4.00           038         0.004         -0.09         0.09         4.00           050         0.047         -0.12         0.12         4.00           050         0.006         -0.12         0.12         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         4.00         4.00         4.00           0.000         0.000         W Only         4.00           0.000         0.000         W Only         4.00           0.0123         2.000         Support notation : Far left is #1           1         Support 2         Support 3         50           00         0.405         50	Number         Number<	Max         Max <td>0.004         -0.09         0.09         4.00         2.39         1.00         1.00           038         0.036         -0.09         0.09         4.00         2.39         1.67         1.00           038         0.004         -0.09         0.09         4.00         2.39         1.67         1.00           038         0.004         -0.12         0.12         4.00         2.39         1.67         1.00           050         0.047         -0.12         0.12         4.00         2.39         1.67         1.00           050         0.006         -0.12         0.12         4.00         2.39         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         0.000         W Only         2.39         1.00         1.00           0.000</td> <td>No. 1         No. 1         <th< td=""><td>Normality         Normality         <t< td=""></t<></td></th<></td>	0.004         -0.09         0.09         4.00         2.39         1.00         1.00           038         0.036         -0.09         0.09         4.00         2.39         1.67         1.00           038         0.004         -0.09         0.09         4.00         2.39         1.67         1.00           038         0.004         -0.12         0.12         4.00         2.39         1.67         1.00           050         0.047         -0.12         0.12         4.00         2.39         1.67         1.00           050         0.006         -0.12         0.12         4.00         2.39         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         4.00         2.39         1.00         1.00         1.00         1.00           0.000         0.000         W Only         2.39         1.00         1.00           0.000	No. 1         No. 1 <th< td=""><td>Normality         Normality         <t< td=""></t<></td></th<>	Normality         Normality <t< td=""></t<>



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Company:		Page:	1
Address: Phone I Fax:	1	Specifier: E-Mail:	
Design:	l Masonry - Jun 12, 2020	Date:	6/12/2020
Fastening point:			
Specifier's comments:			
1 Input data			·
Anchor type and diameter:	HY 270 + threaded rod 5.8 1	/2, HIT-SC 18x50	
Item number:	385422 HAS 5.8 1/2"x3-1/8" ( 270 (adhesive) / 360485 HIT-3		
Effective embedment depth:	h <sub>ef</sub> = 2.000 in.		
Material:	5.8		
Evaluation Service Report:	ESR-4143		
Issued I Valid:	1/1/2020   1/1/2021		
Proof:	Design Method ASD Masonry		
Stand-off installation:	e <sub>b</sub> = 0.000 in. (no stand-off); t	= 0.250 in.	
Anchor plate <sup>R</sup> :	l <sub>x</sub> x l <sub>y</sub> x t = 4.000 in. x 8.000 in	x 0.250 in.; (Recommended plate thickness: n	ot calculated)
Profile:	no profile		
Base material:	Hollow CMU, L x W x H: 16.00	00 in. x 8.000 in. x 8.000 in.;	
	Joints: vertical: 0.375 in.; horiz	zontal: 0.375 in.	
	Base material temperature: 68	3°F	
Installation:	Face installation		
Seismic loads	no		

 $^{\rm R}$  - The anchor calculation is based on a rigid anchor plate assumption.

## Geometry [in.]



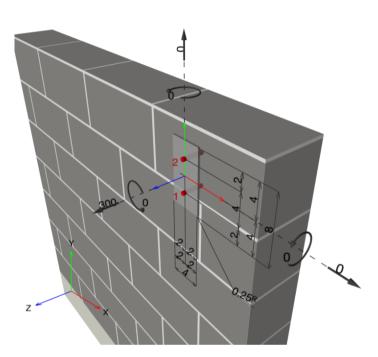
Input data and results must be checked for conformity with the existing conditions and for plausibility! PROFIS Engineering ( c ) 2003-2020 Hilti AG, FL-9494 Schaan Hilti is a registered Trademark of Hilti AG, Schaan



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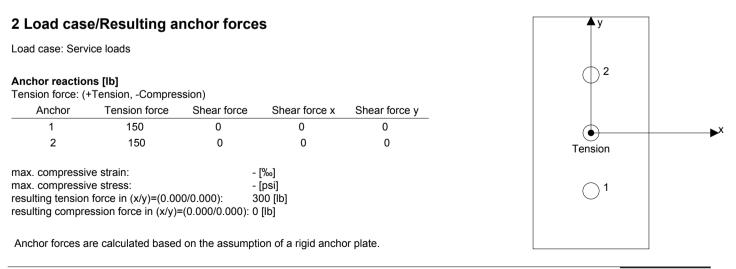
Company:		Page:	2
Address:		Specifier:	
Phone I Fax:		E-Mail:	
Design: Fastening point:	Masonry - Jun 12, 2020	Date:	6/12/2020

#### Geometry [in.] & Loading [lb, in.lb]



#### 1.1 Design results

Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	$N = 300; V_x = 0; V_y = 0;$	no	46
		$M_x = 0; M_y = 0; M_z = 0;$		



Input data and results must be checked for conformity with the existing conditions and for plausibility! PROFIS Engineering ( c ) 2003-2020 Hilti AG, FL-9494 Schaan Hilti is a registered Trademark of Hilti AG, Schaan



Company:		Page:	3
Address:		Specifier:	
Phone I Fax:		E-Mail:	
Design:	Masonry - Jun 12, 2020	Date:	6/12/2020
Fastening point:			

## 3 Tension load (Most utilized anchor 1)

	Load P <sub>s</sub> [lb]	Capacity P <sub>t</sub> [lb]	Utilization $\beta_{P} = P_{s}/P_{t}$ [%]	Status
Steel strength	150	4,700	4	OK
Bond strength	150	330	46	OK

#### 3.1 Steel strength

P <sub>ts</sub> = ESR Value	refer to ICC-ES ESR-4143
$P_{t,s} \ge P_s$	

#### Results

P <sub>t,s</sub> [lb]	P <sub>s</sub> [lb]
4,700	150

### 3.2 Bond strength

P <sub>t,b,Base</sub>	。= ESR Value	refer to ICC-ES ESR-4143
$P_{t,b}$	$= P_{t,b,Base} \cdot f_{red,E} \cdot f_{red,s} \cdot f_{red,Temp}$	
P <sub>t,b</sub>	≥ P <sub>s</sub>	

#### Variables

c <sub>min</sub> [in.]	c <sub>cr</sub> [in.]	s <sub>min</sub> [in.]	s <sub>cr</sub> [in.]	Temperature [°F]		
4.000	-	4.000	-	68		
Results						
P <sub>t,b</sub> [lb]	P <sub>t,b,Base</sub> [lb]	P <sub>s</sub> [lb]	$f_{red,E}$	$f_{red,S}$	f <sub>red,Temp</sub>	f <sub>red,TwoInOne</sub>
330	330	150	1.000	1.000	1.000	1.000



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Company:		Page:	4
Address:		Specifier:	
Phone I Fax:		E-Mail:	
Design: Fastening point:	Masonry - Jun 12, 2020	Date:	6/12/2020

## 4 Shear load (Most utilized anchor 1)

	Load V <sub>s</sub> [lb]	Capacity V <sub>t</sub> [lb]	Utilization $\beta_V = V_s/V_t$ [%]	Status
Overall strength	N/A	N/A	N/A	N/A

## 5 Warnings

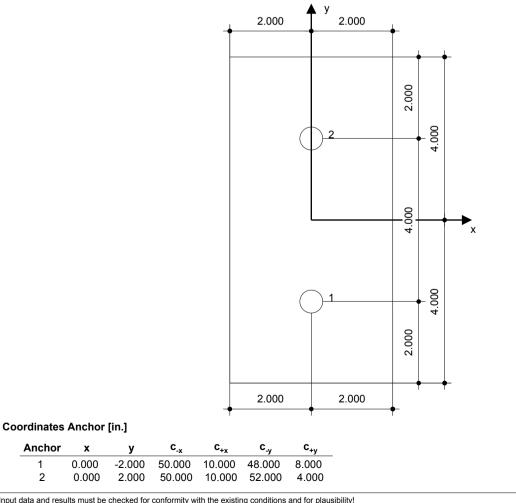
- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2018, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered - the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Refer to the manufacturer's product literature for cleaning and installation instructions.
- For additional information about ACI 318 strength design provisions, please go to https://submittals.us.hilti.com/PROFISAnchorDesignGuide/
- The min. sizes of the bricks, the masonry compressive strength, the type / strength of the mortar and the grout (in case of fully grouted CMU walls) has to fulfill the requirements given in the relevant ESR-approval or in the PTG.
- Only the local load transfer from the anchor(s) to the wall is considered, a further load transfer in the wall is not covered by PROFIS!
- Wall is assumed as being perfectly aligned vertically checking required(!): Noncompliance can lead to significantly different distribution of forces and higher tension loads than those calculated by PROFIS. Masonry wall must not have any damages (neither visible nor not visible)! While installation, the positioning of the anchors needs to be maintained as in the design phase i.e. either relative to the brick or relative to the mortar joints.
- The effect of the joints on the compressive stress distribution on the plate / bricks was not taken into consideration.
- If no significant resistance is felt over the entire depth of the hole when drilling (e.g. in unfilled butt joints), the anchor should not be set at this position or the area should be assessed and reinforced. Hilti recommends the anchoring in masonry always with sieve sleeve. Anchors can only be installed without sieve sleeves in solid bricks when it is guaranteed that it has not any hole or void.
- The accessories and installation remarks listed on this report are for the information of the user only. In any case, the instructions for use provided with the product have to be followed to ensure a proper installation.
- The compliance with current standards (e.g. 2015, 2012, 2009 and 2006 IBC) is the responsibility of the user.
- · Drilling method (hammer, rotary) to be in accordance with the approval!
- · Masonry needs to be built in a regular way in accordance with state-of the art guidelines!
- · Warnings/Notes OST in Masonry HNA!

## Fastening meets the design criteria!



Company: Address:		Page: Specifier:	5
Phone I Fax:	I	E-Mail:	
Design: Fastening point:	Masonry - Jun 12, 2020	Date:	6/12/2020
6 Installation da	ta		
		Anchor type and diameter: HY 270	) + threaded rod 5.8 1/2,
		HIT-SC 18x50	
Profile: no profile		Item number: 385422 HAS 5.8 1/2"x3-1/8" (element) / 2194247 HIT-HY 270 (adhesive) / 360485 HIT-SC 18x50	
		(sieve sleeve)	
Hole diameter in the fixture: $d_f = 0.563$ in.		Installation torque: 54 in.lb	
Plate thickness (input): 0.250 in.		Hole diameter in the base material: 0.688 in.	
		Hole depth in the base material: 2	.375 in.
Drilling method: Drilled	in rotary mode	Minimum thickness of the base ma	aterial: 7.625 in.

Hilti HIT-V threaded rod with HIT-HY 270 injection mortar and 1 HIT-SC 18x50 sieve sleeve(s) with 2 in embedment h\_ef, 1/2, Steel galvanized, Rotary drilled installation per ESR-4143



Input data and results must be checked for conformity with the existing conditions and for plausibility! PROFIS Engineering ( c ) 2003-2020 Hilti AG, FL-9494 Schaan Hilti is a registered Trademark of Hilti AG, Schaan

1

2



www.hilti.com			
Company:		Page:	6
Address:		Specifier:	
Phone I Fax:		E-Mail:	
Design:	Masonry - Jun 12, 2020	Date:	6/12/2020
Fastening point:			

## 7 Remarks; Your Cooperation Duties

- Any and all information and data contained in the Software concern solely the use of Hilti products and are based on the principles, formulas and security regulations in accordance with Hilti's technical directions and operating, mounting and assembly instructions, etc., that must be strictly complied with by the user. All figures contained therein are average figures, and therefore use-specific tests are to be conducted prior to using the relevant Hilti product. The results of the calculations carried out by means of the Software are based essentially on the data you put in. Therefore, you bear the sole responsibility for the absence of errors, the completeness and the relevance of the data to be put in by you. Moreover, you bear sole responsibility for having the results of the calculation checked and cleared by an expert, particularly with regard to compliance with applicable norms and permits, prior to using them for your specific facility. The Software serves only as an aid to interpret norms and permits without any guarantee as to the absence of errors, the correctness and the relevance of the results or suitability for a specific application.
- You must take all necessary and reasonable steps to prevent or limit damage caused by the Software. In particular, you must arrange for the
  regular backup of programs and data and, if applicable, carry out the updates of the Software offered by Hilti on a regular basis. If you do not use
  the AutoUpdate function of the Software, you must ensure that you are using the current and thus up-to-date version of the Software in each
  case by carrying out manual updates via the Hilti Website. Hilti will not be liable for consequences, such as the recovery of lost or damaged data
  or programs, arising from a culpable breach of duty by you.

## **ATTACHMENT 5**

# Photo Documentation & Simulations



## NEW HAVEN CT 54 MEADOW STREET NEW HAVEN, CT 06519

Prepared in July 2020 by: All-Points Technology Corporation, P.C. 567 Vauxhall Street Extension – Suite 311 Waterford, CT 06385

Prepared for Verizon Wireless



## **VISUAL ASSESSMENT & PHOTO-SIMULATIONS**

Cellco Partnership, d/b/a Verizon Wireless is seeking approval for the modification of an existing wireless communications facility (the "Facility") at 54 Meadow Street in New Haven, Connecticut. At the request of Verizon Wireless, All-Points Technology Corporation, P.C. ("APT") completed this assessment and prepared computer-generated photo-simulations depicting the Facility.

## **Project Undertaking**

The proposed modifications to the Facility would take place on the rooftop of an existing multistory building (the "Host Building"). Currently, Verizon Wireless maintains twelve (12) antennas and various appurtenances on the building's penthouse. Verizon Wireless plans to replace nine (9) antennas, leave three (3) existing antennas as is, and install three (3) new antennas for a total of fifteen (15) antennas. Of the nine (9) antennas being replaced, seven (7) will be relocated to positions on the building façade, penthouse façade, and an existing mechanical screen wall on the rooftop.

The building rooftop extends to a height of approximately 129' 2" above ground level ("AGL"). A parapet wall extends to a height of approximately 131' 6" AGL. The penthouse rooftop extends to a height of approximately 155' AGL with a parapet extending to approximately 157' 2" AGL. Please refer to the Site Drawings prepared by On Air Engineering, LLC, Rev. 2 dated July 13, 2020, and provided under separate cover, for details regarding the proposed installation.

## Field Reconnaissance

APT completed field reconnaissance in the vicinity of the Facility to record existing conditions, inventory visible and non-visible locations, and provide photographic documentation from publicly accessible areas. The field reconnaissance was completed on July 8, 2020. Weather conditions were favorable for the in-field activity with partly cloudy skies.

## **Photographic Documentation and Simulations**

During the field reconnaissance, APT obtained photo-documentation of representative locations where the Host Building was visible. At each photo location, the geographic coordinates of the camera's position were logged using global positioning system ("GPS") technology. Photographs were taken with a Canon EOS 6D digital camera body<sup>1</sup> and Canon EF 24 to 105 millimeter ("mm") zoom lens. APT typically uses a standard focal length of 50mm to present a consistent

<sup>&</sup>lt;sup>1</sup> The Canon EOS 6D is a full-framed camera which includes a lens receptor of the same size as the film used in 35mm cameras. As such, the images produced are comparable to those taken with a conventional 35mm camera.

field of view. On occasion, photos are taken at lower focal lengths to provide a greater depth of field and to provide context to the scene by including surrounding features within the photograph. During this evaluation, one (1) photograph was taken at a 24mm focal length as noted in the table (Table 1 - Photo Locations) on the following pages.

Photographic simulations were generated to portray scaled renderings of the proposed Facility from all eight (8) locations presented herein where the Facility may be recognizable. Using field data, Site plan information and 3-dimensional (3D) modeling software, spatially referenced models of the Facility were generated and merged. The geographic coordinates obtained in the field for the photograph locations were incorporated into the model to produce virtual camera positions within the spatial 3D model. Photo-simulations were then created using a combination of renderings generated in the 3D model and photo-rendering software programs, which were ultimately composited and merged with the existing conditions photographs (using Photoshop image editing software). The scale of the subjects in the photograph (the Host Building) and the corresponding simulation (the Facility) is proportional to their surroundings.

For presentation purposes in this report, the photographs were produced in an approximate 7inch by 10.5-inch format. When reproducing the images in this format size, we believe it is important to present the largest view while providing key contextual landscape elements (existing developments, street signs, utility poles, etc.) so that the viewer can determine the proportionate scale of each object within the scene. Photographs presented in the attachment at the end of this report include documentation of existing conditions, identification of antennas proposed for removal/relocation, identification of relocated/new antennas, and photosimulations of the modified Facility. The photo-simulations are intended to provide the reader with a general understanding of the different view characteristics associated with the Facility from various locations. Photographs were taken from publicly-accessible areas and unobstructed view lines were chosen wherever possible.

The table on the following page summarizes the photographs and simulations presented in the attachment to this report, and includes a description of each location, view orientation, and distance from where the photo was taken relative to the proposed Facility. The photo locations are depicted on the photolog provided as an attachment to this report.

## **Table 1 – Photo Locations**

Photo	Location	Orientation	Distance to Site
1	Orange Street at George Street	South	± 0.23 Mile
2	Church Street South	Southeast	± 0.18 Mile
3	Cedar Street	Northeast	± 0.32 Mile
4	Union Avenue	Northeast	± 0.22 Mile
5	Church Street	Northwest	± 0.44 Mile
6	Food Terminal Plaza	Northwest	± 0.41 Mile
7	Brewery Street	Northwest	± 0.32 Mile
8	Union Avenue	West	± 309 Feet

## Conclusions

As presented on the attached photo-simulations, views of the Facility would change slightly with the proposed modifications. The Host Building currently has multiple antennas and equipment mounted on the penthouse façade. The modifications as proposed by Verizon Wireless do not increase visibility of the Facility, nor do they detract from the general characteristics of the Host Building, as is.

## Limitations

This analysis may not account for all visible locations, as it is based on the combination of computer modeling, incorporating aerial photographs, and in-field observations from publicly-accessible locations. No access to private properties was provided to APT personnel. This analysis does not claim to depict the only areas, or all locations, where visibility may occur; it is intended to provide a representation of those areas where the Facility is likely to be seen.

The photo-simulations provide a representation of the Facility under similar settings as those encountered during the field review and reconnaissance. Views of the Facility can change throughout the seasons and the time of day, and are dependent on weather and other atmospheric conditions (e.g., haze, fog, clouds); the location, angle and intensity of the sun; and the specific viewer location. Weather conditions on the day of the field review included variable winds and sunny skies.

## ATTACHMENTS



Legend Site Photographic Location

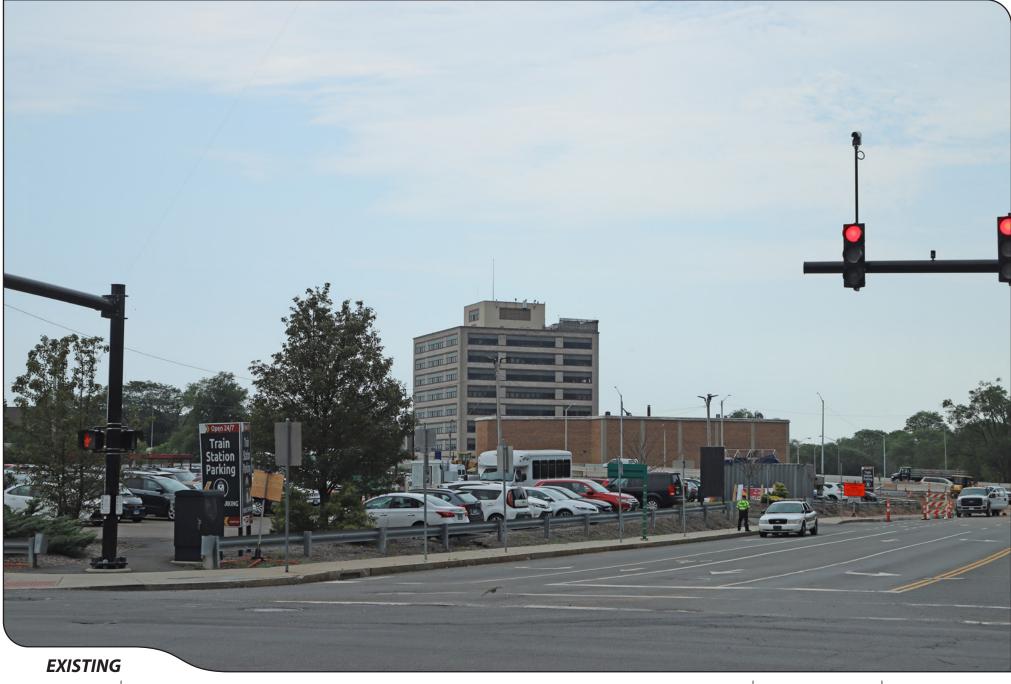


1 inch = 600 feet 300

600







РНОТО	LOCATION	ORIENTATION	DISTANCE TO SITE
1	ORANGE STREET AT GEORGE STREET	SOUTH	+/- 0.23 MILE















РНОТО	LOCATION	ORIENTATION	DISTANCE TO SITE
1	ORANGE STREET AT GEORGE STREET	SOUTH	+/- 0.23 MILE







**CHURCH STREET SOUTH** 

2

ALL-POINTS TECHNOLOGY CORPORATION

SOUTHEAST



+/- 0.18 MILE





















ΡΗΟΤΟ

3





DISTANCE TO SITE

+/- 0.32 MILE















РНОТО	LOCATION	ORIENTATION	DISTANCE TO SITE
3	CEDAR STREET	NORTHEAST	+/- 0.32 MILE







4	UNION AVENUE
РНОТО	LOCATION





















PHOTO	LOCATION	ORIENTATION	DISTANCE TO SITE
4	UNION AVENUE	NORTHEAST	+/- 0.22 MILE







LOCATION

**CHURCH STREET EXTENSION** 

NORTHWEST	+/- 0.44 MILE
ORIENTATION	DISTANCE TO SITE





ΡΗΟΤΟ 5



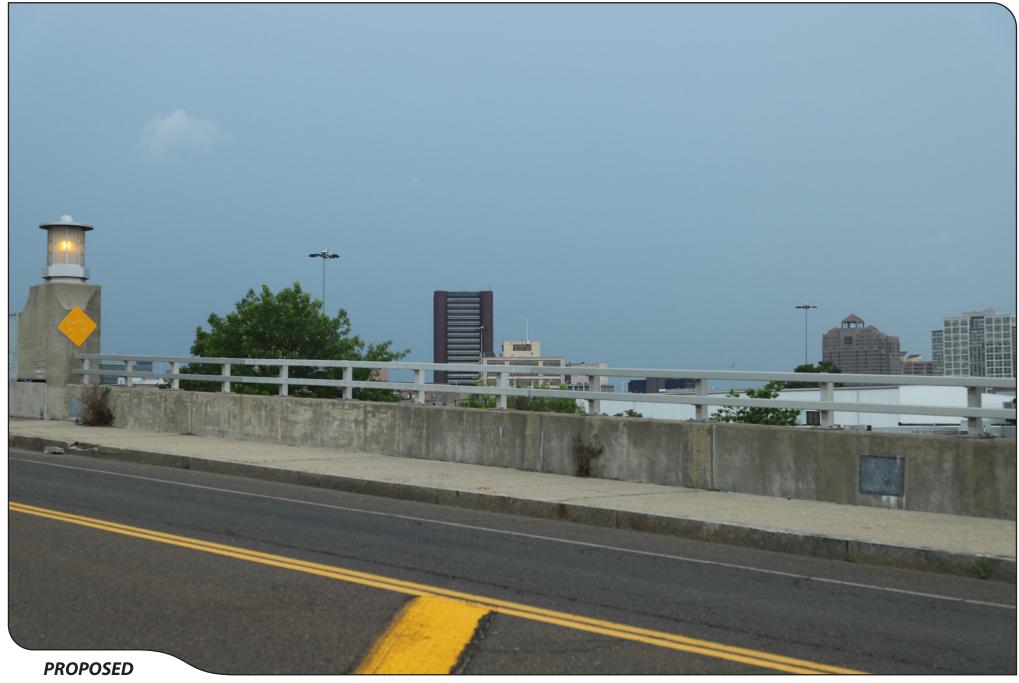












рното	LOCATION	ORIENTATION	DISTANCE TO SITE
5	CHURCH STREET EXTENSION	NORTHWEST	+/- 0.44 MILE

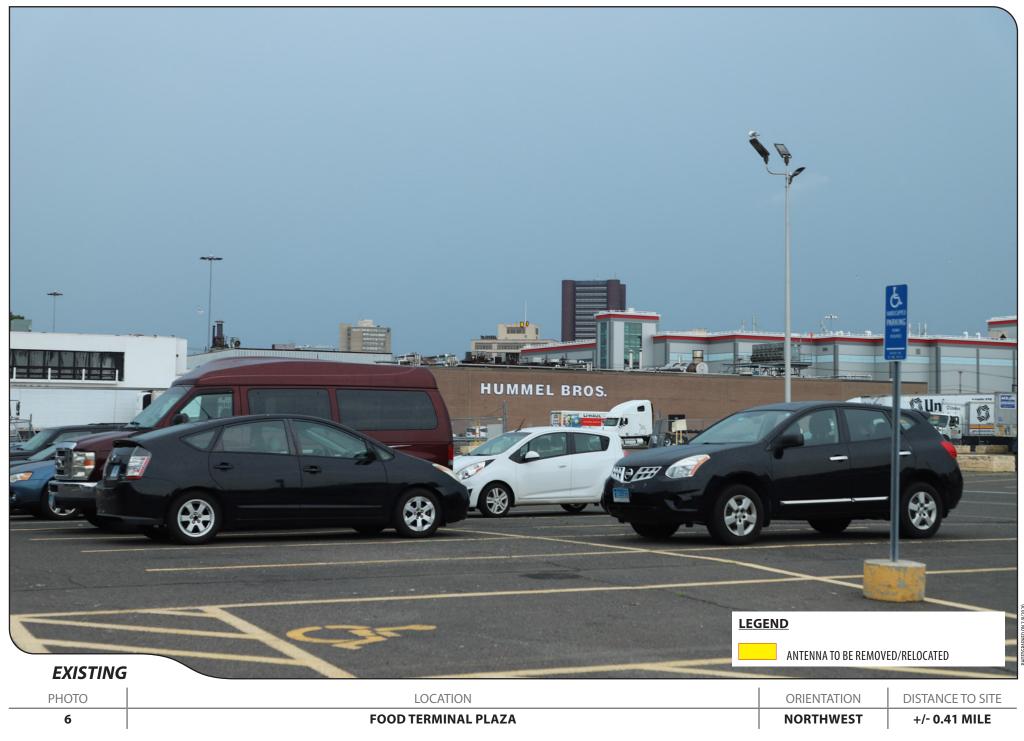
























рното	LOCATION	ORIENTATION	DISTANCE TO SITE
6	FOOD TERMINAL PLAZA	NORTHWEST	+/- 0.41 MILE

























PHOTO	LOCATION	ORIENTATION	DISTANCE TO SITE
7	BREWERY STREET	NORTHWEST	+/- 0.32 MILE

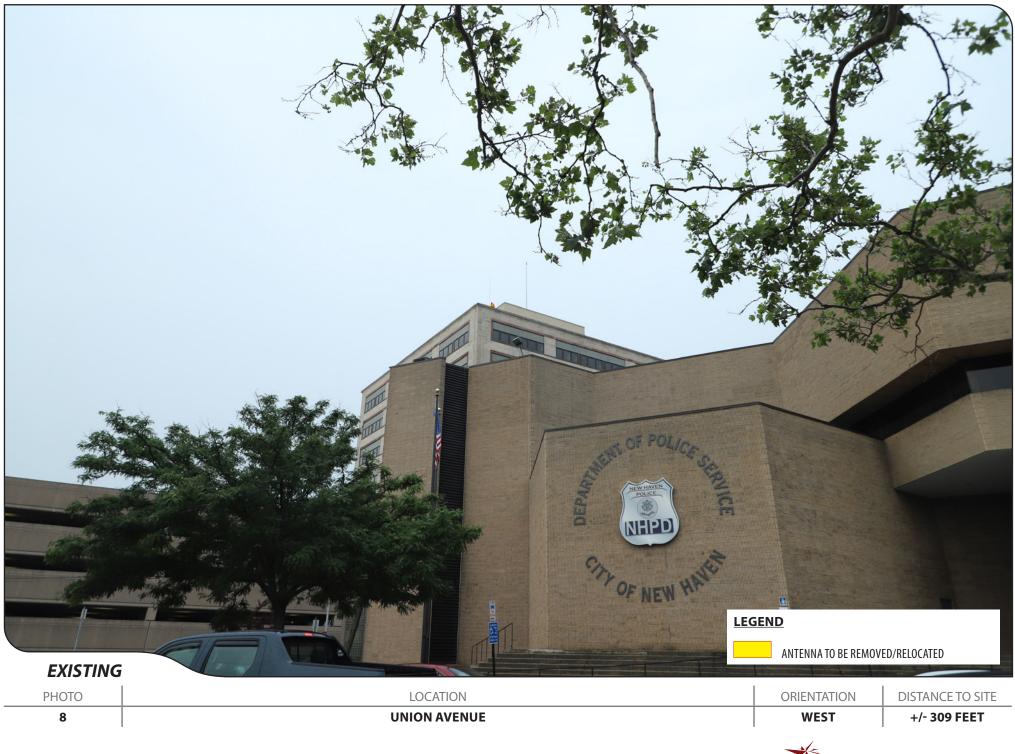












verizon

ALL-POINTS TECHNOLOGY CORPORATION









LOCATION	ONILINIATION	DISTANCE TO SITE
UNION AVENUE	WEST	+/- 309 FEET
•		





# **ATTACHMENT 6**

Site Name: New Haven CT Cumulative Power Density

Operator	Operating Frequency	Number of Trans.	ERP Per Trans.	Total ERP	Distance to Target	Calculated Power Density	Maximum Permissible Exposure*	Fraction of MPE		
	(MHz)		(watts)	(watts)	(feet)	(mW/cm^2)	(mW/cm^2)	(%)		
VZW 700	746	4	556	2,224	136	0.0432	0.497333333	8.69%		
VZW Cellular	869	2	354	708	155	0.0106	0.579333333	1.83%		
VZW Cellular	880	4	556	2,224	136	0.0432	0.586666667	7.37%		
VZW PCS	1,970	4	1,303	5,213	136	0.1013	1.0	10.13%		
VZW AWS	2,145	4	1,396	5,585	136	0.1086	1.0	10.86%		
VZW CBRS	3,550	4	51	204	136	0.0040	1.0	0.40%		
VZW 28GHz	27,600	1	610	610	136	0.0119	1.0	1.19%		
Total Percentage of Maximum Permissible Exposure										

**Total Percentage of Maximum Permissible Exposure** 

40.47%

\*Guidelines adopted by the FCC on August 1, 1996, 47 CFR Section 1.13101 based on NCRP Report 86, 1986 and generally on ANSI/IEEE C95.1-1992

MHz = Megahertz

mW/cm<sup>2</sup> = milliwatts per square centimeter

ERP = Effective Radiated Power

Absolute worst case maximum values used, including the following assumptions:

1. closest accessible point is distance from antenna to base of pole;

2. continuous transmission from all available channels at full power for indefinite time period; and,

3. all RF energy is assumed to be directed solely to the base of the pole.

# **ATTACHMENT 7**

# Federal Aviation Regulations Part 77 Sub-Part C Obstruction Analysis Report

Verizon Wireless Ziad Cheiban 20 Alexander Drive Wallingford, CT 06492

E-mail: ziad.cheiban@verizonwireless.com Phone: 8604717860 Fax:

Site Identification:	MCM_CT-520
Nearest City:	New Haven, CT

Site Information (Coordinate Datum - NAD83)

Latitude: Longitude:	41° - 17' - 59.54 72° - 55' - 35.57	
Ground Elev Structure He		11 feet AMSL 60 feet AGL
Overall Heig	<b>ht:</b> 1	71 feet AMSL

FAA Number:NullAirspace Study #:2020-APS-3708-OE

Analyzed on: 5/22/2020. Using Airspace® 20.5.463. Airspace® Data Date: 5/15/2020

This Airspace Analysis was completed under all obstacle evaluation rules specified in Federal Aviation Regulations (FAR) Part 77 sub-Part C.

Approved,

Bella B Harris, Airspace Technician Federal Airways and Airspace® 1423 S. Patrick Dr. Satellite Beach, FL 32935 (321)777-1266 Clyde J Pittman, Aerospace Engineer

Date Printed: 05-22-2020

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Site ID Number: MCM\_CT-520

## **AERONAUTICAL RECOMMENDATIONS**

Notice to the FAA is not required at the analyzed height and location.

TERPS® analysis has been completed for the proposed site. **The maximum allowable** height identified is 363 feet AMSL based upon HVN VFR Traffic Pattern Airspace.

The proposed structure does not penetrate obstruction standards. An aeronautical analysis by the Federal Aviation Administration would likely find no adverse aeronautical impact. An extended study will not be required. The maximum not to exceed height to avoid an extended study by the FAA is 213 feet AMSL based upon HVN FAR 77.17(a)(2) VFR Transitional Surface.

Marking and Lighting are not normally required for structures 200 feet or less. However, it may become a requirement based upon the outcome of the aeronautical study conducted by the FAA. It will then become part of the determination and a requirement of the determination.

No adverse impact to low altitude federal airways are identified.

No impact to VFR Traffic Pattern Airspace.

No Potential FCC Licensed AM Broadcast Station interference identified.

No impact to an Air Navigation Facility has been identified.

Date Printed: 05-22-2020

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Site ID Number: MCM\_CT-520

## LANDING FACILITY INFORMATION

The nearest public use landing facility to the proposed location is: TWEED-NEW HAVE (Ident: HVN)

The distance to the nearest runway of this landing facility is 14983 feet or 2.8 statute miles. The true bearing is 140.12° to this landing facility.

Private landing facilities are exempt from review by the FAA under FAR Part 77. However, locating near a private landing facility may affect aircraft operations during take-off and landing.

The nearest private landing facility is: 1CT2: YALE The proposed structure is located 3220 feet or .6 statute miles. The true bearing to this landing facility is 301 degrees.

The proposed structure is within 3 nautical miles (3.45 statute miles) of a private landing facility. This landing facility and supporters are likely to resist this proposal during the local zoning board hearing.

## FAA NOTICE REQUIREMENTS

#### Notice to the FAA is not required because the proposed structure

1) is less than 200 feet above ground level [FAR Part 77.9(a)].

- 2) does not exceed runway slope criteria [FAR Part 77.9(b)].
- 3) is not a traverse way (road) [FAR 77.9(c)].
- 4) is not within a protected instrument procedure area [FAR 77.9 IFR].
- 5) is not on airport property [FAR 77.9(d)].
- 6) is not near an air navigation facility [FAR 77.9 IFR].

Date Printed: 05-22-2020

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Site ID Number: MCM\_CT-520

## AERONAUTICAL IMPACT

### FAR Part 77 Subpart-C Obstruction Standards

The proposed structure would not violate or exceed obstruction standards as defined by FAR Part 77.17(a)(1), 77.17(a)(2) and 77.19.

## Terminal Instrument Procedure Standards - FAR Part 77.17(a)(3)

No adverse impact with a US Terminal Approach or Departure Procedure has been identified.

## Minimum Obstacle Clearance Altitude (MOCA) - FAR Part 77.17(a)(4)

The proposed structure is not located within a low altitude airway area or will not impact aircraft using any airway.

## VFR Traffic Pattern Airspace

The proposed structure is not located within a VFR Traffic Pattern Airspace or is below the allowable height. It will not impact aircraft circling to land.

#### FCC Licensed AM Broadcast Station Proof-of-Performance

The proposed structure is not located within the specified range of an FCC Licensed AM radio and will not require Proof-of-Performance analysis.

Date Printed: 05-22-2020

Federal Airways & Airspace \* Summary Report: Alteration Of Existing Structure \* Non-Antenna Structure Airspace User: File: 2020-APS-3708-OE Location: New Haven, CT Latitude: 41°-17'-59.54" Longitude: 72°-55'-35.57" SITE ELEVATION AMSL.....11 ft. STRUCTURE HEIGHT.....160 ft. OVERALL HEIGHT AMSL.....171 ft. NOTICE CRITERIA FAR 77.9(a): NNR (DNE 200 ft AGL) FAR 77.9(b): NR (Exceeds Notice Slope, Maximum: 162 ft.) NNR See below regarding Notice Criteria Exemption under 77.9(e)(4). FAR 77.9(c): NNR (Not a Traverse Way) FAR 77.9: NNR FAR 77.9 IFR Straight-In Notice Criteria for HVN FAR 77.9: NNR FAR 77.9 IFR Straight-In Notice Criteria for BDR FAR 77.9(d): NNR (Off Airport Construction) NR = Notice Required NNR = Notice Not Required PNR = Possible Notice Required (depends upon actual IFR procedure) For new construction review Air Navigation Facilities at bottom

of this report. If the proposed construction is an alteration to an existing structure,

notice requirements may be superceded by the item exemptions listed below.

The location and analysis were based upon an existing structure. However, no existing aeronautical study number was identified. If the 'existing' structure penetrates an obstruction surface defined by CFR 77.17, 77.19, 77.21 or 77.23 (see below) it is strongly recommended the FAA be notified of the 'existing' structure to determine obstruction marking or lighting requirements. It is not uncommon for the FAA to issue a Determination of No Hazard (DNH) for an existing structure and modify the airspace to accommodate the structure, should that be required. If the FAA issues a DNH enter the aeronautical study number (ASN) in the space provided on the Airspace Analysis Window Form and re-run Airspace.

No frequencies were identified in this alteration are included in the FAA's Co-Location Policy published in the Federal Register November 15, 2007. Therefore, application of the Co-Location Policy notice exemption rule can not be applied.

Title 14 CFR Part 77.9(e), Notice Criteria Exception: The location and analysis were based upon an existing structure with the alteration limited to the addition of an antenna with a height no greater than 20 feet. Title 14 CFR Part 77.9(e)(4) exempts the requirement for notice to the FAA; "Any antenna structure of 20 feet or less in height except one that would increase the height of another antenna structure." If the addition of an antenna of 20 feet or less to an existing structure increase the height of the structure to exceed 200 feet AGL or penetrate an obstruction surface defined by Title 14 CFR 77.17, 77.19, 77.21 or 77.23 notice is recommended. This will allow the FAA to determine the level of obstruction lighting required and any aeronautical impacts, if any, to aircraft operations. Notice of an existing structure almost always receives a No Hazard Determination. Please see Summary Report below plus the Airport and Part 77 Reports for application of the above listed CFRs. OBSTRUCTION STANDARDS FAR 77.17(a)(1): DNE 499 ft AGL FAR 77.17(a)(2): DNE - Airport Surface FAR 77.19(a) (2): DNE - Allport Sufface FAR 77.19(a): DNE - Horizontal Surface FAR 77.19(b): DNE - Conical Surface FAR 77.19(c): DNE - Primary Surface FAR 77.19(d): DNE - Approach Surface FAR 77.19(e): DNE - Approach Transitional Surface FAR 77.19(e): DNE - Abeam Transitional Surface VFR TRAFFIC PATTERN AIRSPACE FOR: HVN: TWEED-NEW HAVEN Type: A RD: 14983.55 RE: 12.6 FAR77.17(a)(1):DNEFAR77.17(a)(2):DNE DNE - Height No Greater Than 200 feet AGL. VFR Horizontal Surface: DNE VFR Conical Surface: DNE DNE VFR Primary Surface: VFR Approach Surface: DNE VFR Transitional Surface: DNE The structure is within VFR - Traffic Pattern Airspace Climb/Descent Area. Structures exceeding the greater of 350' AAE, 77.17(a)(2), or VFR horizontal and conical surfaces will receive a hazard determination from the FAA. Maximum AMSL of Climb/Descent Area is 363 feet. VFR TRAFFIC PATTERN AIRSPACE FOR: BDR: IGOR I SIKORSKY MEMORIAL Type: A RD: 72131.77 RE: 6.5 FAR 77.17(a)(1):DNEFAR 77.17(a)(2):DNE - Greater Than 5.99 NM.VFR Horizontal Surface:DNE VFR Conical Surface: DNE VFR Primary Surface: DNE VFR Primary Surface: VFR Approach Surface: DNE VFR Transitional Surface: DNE TERPS DEPARTURE PROCEDURE (FAA Order 8260.3, Volume 4) FAR 77.17(a)(3) Departure Surface Criteria (40:1) DNE Departure Surface MINIMUM OBSTACLE CLEARANCE ALTITUDE (MOCA) FAR 77.17(a)(4) MOCA Altitude Enroute Criteria The Maximum Height Permitted is 500 ft AMSL PRIVATE LANDING FACILITIES BEARING RANGE DELTA ARP FAA To FACIL IN NM ELEVATION IFR FACTL IDENT TYP NAME 1CT2 HEL YALE NEW HAVEN HOSPITAL 300.93 .53 -48 No Impact to Private Landing Facility Structure 48 ft below heliport. CT40 HEL BOB THOMAS FORD 5.74 4.21 +91 No Impact to Private Landing Facility Structure is beyond notice limit by 20580 feet. CT84 HEL PARTYKA CHEVROLET 10.38 4.5 +121 No Impact to Private Landing Facility Structure is beyond notice limit by 22342 feet. AIR NAVIGATION ELECTRONIC FACILITIES STDIST DELTAGRND APCHEAT FREQ VECTOR (ft)ELEVA ST LOCATIONANGLE BEAR FAC IDNT TYPE 

 HVN
 LOCALIZER
 I
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 +154
 CT RWY 02 TWEED-NEW
 .61

 HVN
 ATCT
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 +80
 CT TWEED-NEW HAVEN
 .27

 JWE
 NDB
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 36
 300.55
 59247
 -400
 CT CLERA
 -.39

 MAD
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 110.4
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 CT MADISON
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 16

CCC	VOR/DME	R	117.2	165.42	139419	+86	NY	CALVERTON	.04
KOKX	RADAR WXL	I		173.79	159182	-24	NY	NEW YORK	01
HFD	VOR/DME	R	114.9	39.76	162031	-678	CT	HARTFORD	24
QVH	RADAR ARSR	I	1326.9	156.82	167033	-180	NY	RIVERHEAD	06
CMK	VOR/DME	R	116.6	267.49	180089	-523	NY	CARMEL	17
ISP	RADAR	I	2735.	194.47	185780	-11	NY	LONG ISLAND MacAR	0.00
FOK	TACAN	R	111.0	154.33	186959	+121	NY	SUFFOLK CO	.04
DPK	VOR/DME	R	117.7	209.21	212362	+48	NY	DEER PARK	.01
HPN	RADAR	I	2735.	248.88	232364	-339	NY	WESTCHESTER COUNT	08
BDL	RADAR	I		15.92	242105	-65	СТ	BRADLEY INTL	02

CFR Title 47, §1.30000-§1.30004 AM STUDY NOT REQUIRED: Structure is near a licensed AM radio station. However, Movement Method Proof is not required because only antenna structures fall within the jurisdiction of the FCC. Please review AM Station Report for details.

Airspace<sup>®</sup> Summary Version 20.5.565

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05-22-2020 14:12:20

F.A.R. 77 OBSTRUCTION ANALYSIS FILE: 2020-APS-3708-OE LATITUDE: 41°-17'-59.54" LONGITUDE: 72°-55'-35.57" SITE ELEVATION AMSL..... 11 ft. 160 ft. STRUCTURE HEIGHT..... 160 ft. OVERALL HEIGHT AMSL..... 171 ft. 77.17(a)(1) A height more than 499 ft. Above Ground Level (AGL). THE MAXIMUM ALLOWABLE HEIGHT IS:..... 510 ft. AMSL THE GROUND ELEVATION AT THE SITE IS:... 11 ft. AMSL THE OVERALL CASE ELEVATION IS:..... 171 ft. AMSL THE CASE IS BELOW THE ALLOWABLE BY:.... 339 ft. BEGIN AIRPORT ANALYSIS FOR HVN 77.17(a)(2) A height AGL or airport elevation, whichever is higher. BECAUSE: Proposed height does not exceed 200 feet Above Ground Level. THE REFERENCE AIRPORT IDENT IS:.... HVN THE AIRPORT ELEVATION IS:..... 13 ft. AMSL

THE DISTANCE FROM THE CASE TO ARP IS:.. 2.8126 NAUTICAL MILES THE BEARING AIRPORT TO CASE IS:..... 320.115 DEGREES THE CASE HEIGHT AGL IS:..... 160 ft. ALLOWABLE HEIGHT..... 213 ft. AMSL

\* BEGIN RUNWAY ANALYSIS \* \*\*\*\*\*\*\*\*\*\*

RUNWAY 02/20

#### EXISTING RUNWAY 02/20

77.19(d) A height exceeding an approach surface of RUNWAY 20.

The FAA has defined this runway as a non-utility runway. It has a non-precision approach. The obstacle surface extends 10,000 feet (34:1 Slope) symmetrically centered along the runway centerline extended. Please review the US Terminal Procedures volume associated with this airport. If a procedure for this airport and/or runway exist use Terps® Professional software to determine the height limits (if any) the procedure will have on the proposed structure. Non-precision instrument procedures can extend 10 NM from the runway and a circling approach to the airport or runway can extend out up to 4.5 NM from every runway end.

RUNWAY 14/32 EXISTING RUNWAY 14/32

77.19(c) A height exceeding runway primary surface.

NOT WITHIN SPECIFIED RUNWAY PRIMARY SURFACE

77.19(d) A height exceeding an approach surface of RUNWAY 14.

The FAA has defined this runway as a non-utility runway. It has a visual approach. The obstacle surface extends 5000 feet (20:1 Slope) symmetrically centered along the runway centerline extended. This airport may have a circling approach. Please review the US Terminal Procedures volume associated with this airport. If a procedure for this airport and/or this runway exist use Terps<sup>®</sup> Professional software to determine the height limits (if any) the procedure will have on the proposed structure. A circling approach to the airport or any runway can extend out up to 4.5 NM from every runway end.

#### 

77.17(a)(2) A height AGL or airport elevation, whichever is higher.

BECAUSE: Location studied is further than 5.99 nm. from ARP.

77.19(a) A height exceeding a horizontal surface 150 ft. above airport elevation within a radius of >> BDR <<.

NOT WITHIN SPECIFIED HORIZONTAL SURFACE AREA

77.19(b) A height exceeding a conical surface (a slope outward 4000 ft. from the horizontal surface at 20/1 ratio).

NOT WITHIN SPECIFIED CONICAL SURFACE AREA

RUNWAY 06/24 EXISTING RUNWAY 06/24

77.19(c) A height exceeding runway primary surface.

77.19(d) A height exceeding an approach surface of RUNWAY 24.

THE BEARING TO THE CASE FROM THE THRESHOLD IS..... 47.451 degrees THE NORMAL BEARING TO THE CENTERLINE IS..... 135 degrees THE CENTERLINE OUTBOUND TRUE BEARING IS..... 45 degrees THE ABEAM DISTANCE TO CENTERLINE FROM CASE IS..... 3070.97 ft. \*

CASE MEETS ANGULAR CRITERIA BUT IS LOCATED GREATER THAN 50,000 ft. FROM THE START OF ANY APPROACH TYPE, OUT BY 21872.7 feet

RUNWAY 11/29 EXISTING RUNWAY 11/29

77.19(d) A height exceeding an approach surface of RUNWAY 29. THE BEARING TO THE CASE FROM THE THRESHOLD IS..... 46.656 degrees THE NORMAL BEARING TO THE CENTERLINE IS..... 187.83 degrees

The FAA has defined this runway as a non-utility runway. It has a non-precision approach. The obstacle surface extends 10,000 feet (34:1 Slope) symmetrically centered along the runway centerline extended. Please review the US Terminal Procedures volume associated with this airport. If a procedure for this airport and/or runway exist use Terps<sup>®</sup> Professional software to determine the height limits (if any) the procedure will have on the proposed structure. Non-precision instrument procedures can extend 10 NM from the runway and a circling approach to the airport or runway can extend out up to 4.5 NM from every runway end.

Airspace Data Version: 2020.5.463

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05-22-2020 12:40:38

File: 2020-APS-3708-OE

OVERALL ELEVATION (AMSL): 171 LATITUDE: 41°-17'-59.54" LONGITUDE: 72°-55'-35.57"

FACIL			BEARING	DISTANCE	DELTA ARP	FAR
IDENT	TYP	NAME	To FACIL	IN N.M.	ELEVATION	P77
HVN	AIR	TWEED-NEW HAVEN	140.12	2.812	+158.4	YES

This facility has at least one runway over 3,200 feet in length.

Your structure DNE FAR 77.9(a) but EXCEEDS FAR 77.9(b) Notice Criteria for this airport. You must notify the Federal Aviation Administration using a FAA Form 7460-1 a minimum of 45 days prior to your construction start date. As a minimum, please review reports for FAR Part 77 Obstruction Surfaces, Air Navigation and Communication facilities.

EXCEEDS FAR 77.9(b)(2) Notice Criteria by: 9 feet.

You are 14983 feet from the nearest runway threshold and the threshold elevation is 13 feet. Please review runway analysis for remaining airport surfaces.

This airport has both Circling and Straight-In Instrument Procedures. Please review published US Terminal (TERPS®) Approach Procedures for this landing facility.

DNE FAR 77.9 IFR Notice Criteria for HVN

Category 'D' Circling Approach Area extends 3.78 NM from each runway.

FACIL			BEARING	DISTANCE	DELTA ARP	FAR
IDENT	TYP	NAME	To FACIL	IN N.M.	ELEVATION	P77
BDR	AIR	IGOR I SIKORSKY MEMORIAL	227.75	12.193	+162.5	YES

This facility has at least one runway over 3,200 feet in length.

Your structure DNE FAR 77.9(a) or 77.9(b) Notice Criteria for this airport. However, you may EXCEED other Notice Standards. As a minimum, please review reports for FAR Part 77 Obstruction Surfaces, Air Navigation and Communication facilities.

You are 72131 feet from the nearest runway threshold and the threshold elevation is 7 feet. Please review runway analysis for remaining airport surfaces.

This airport has both Circling and Straight-In Instrument Procedures. Please review published US Terminal (TERPS®) Approach Procedures for this landing facility.

DNE 77.9 IFR Notice Criteria BDR

Category 'D' Circling Approach Area extends 3.78 NM from each runway.

THE NEAREST AIRPORT TO CASE COORDINATES IS: HVN

TWEED-NEW HAVEN is an Airport type landing facility and is associated with the city of NEW HAVEN, CT. The facility is eligible for Study

under FAR Part 77 sub-Part C.

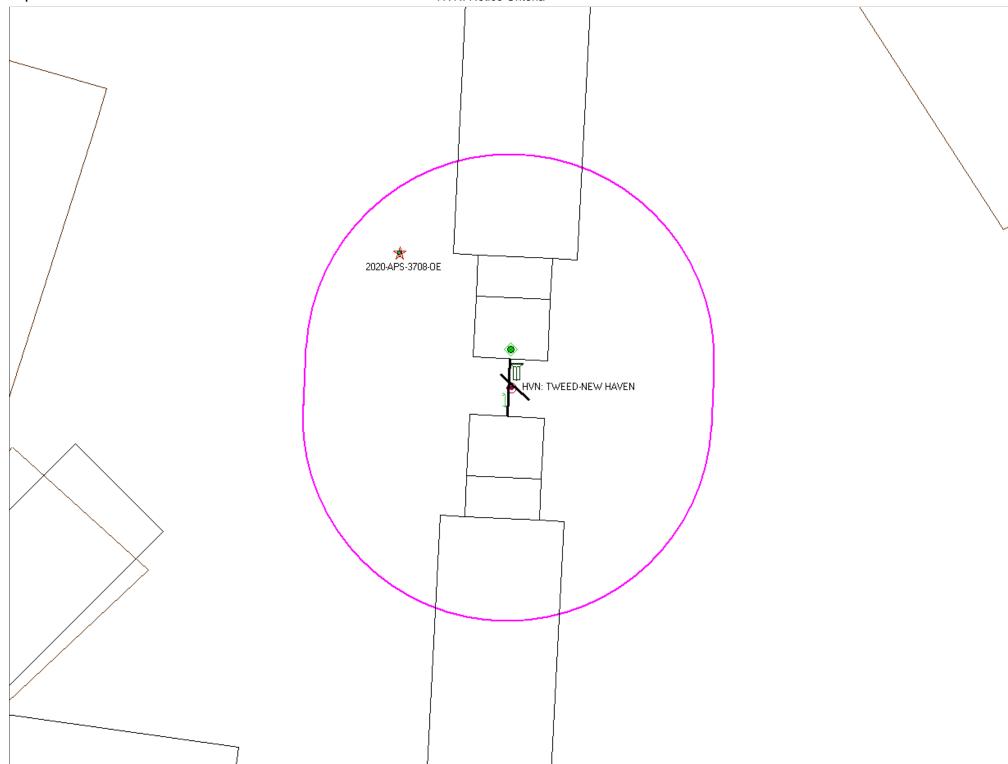
Its Reference Point (ARP) elevation is: 12.6 feet AMSL and you are locating 17089 feet from this landing facility.

Airspace<sup>®</sup> State Data Version 2020.5.463

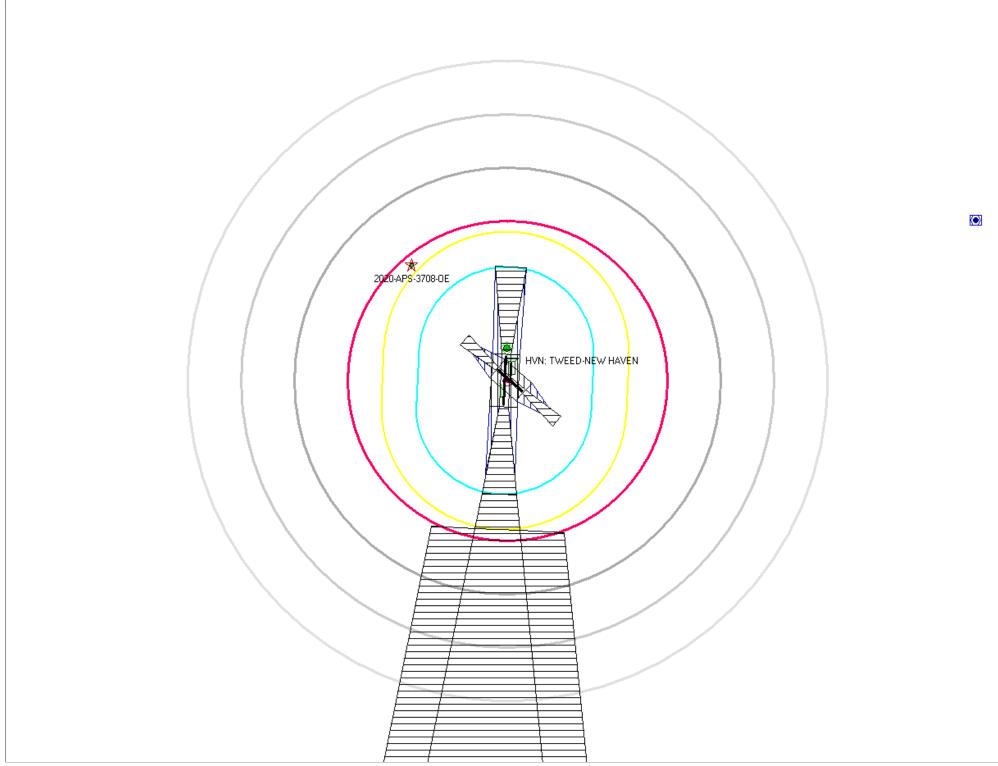
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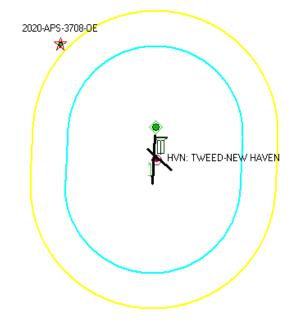
05-22-2020 12:40:37

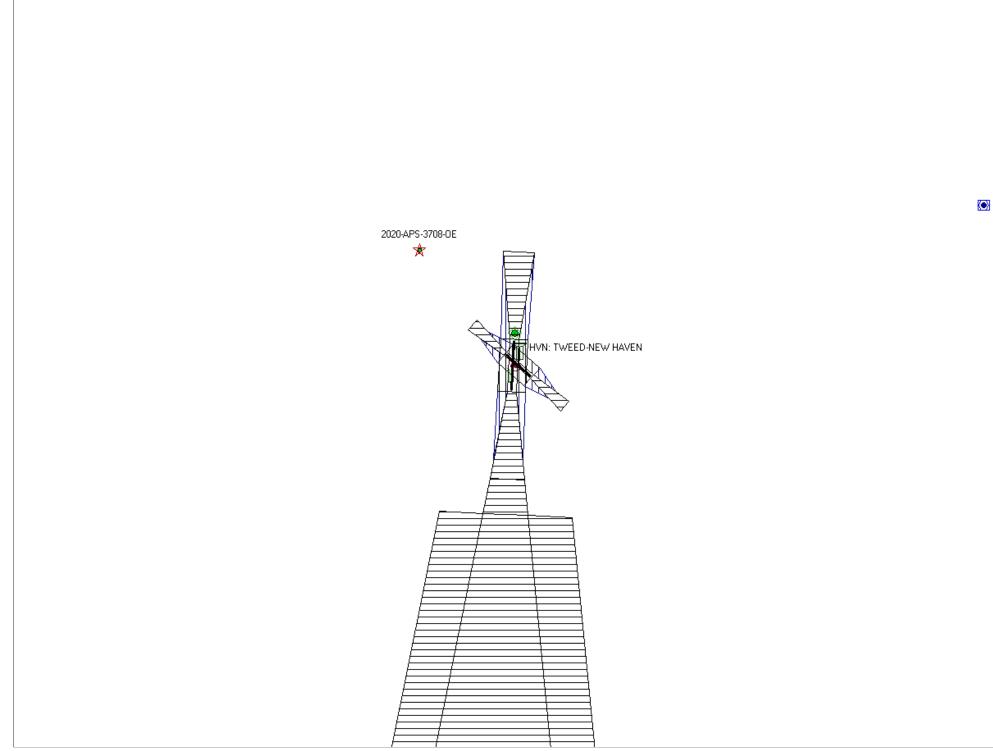


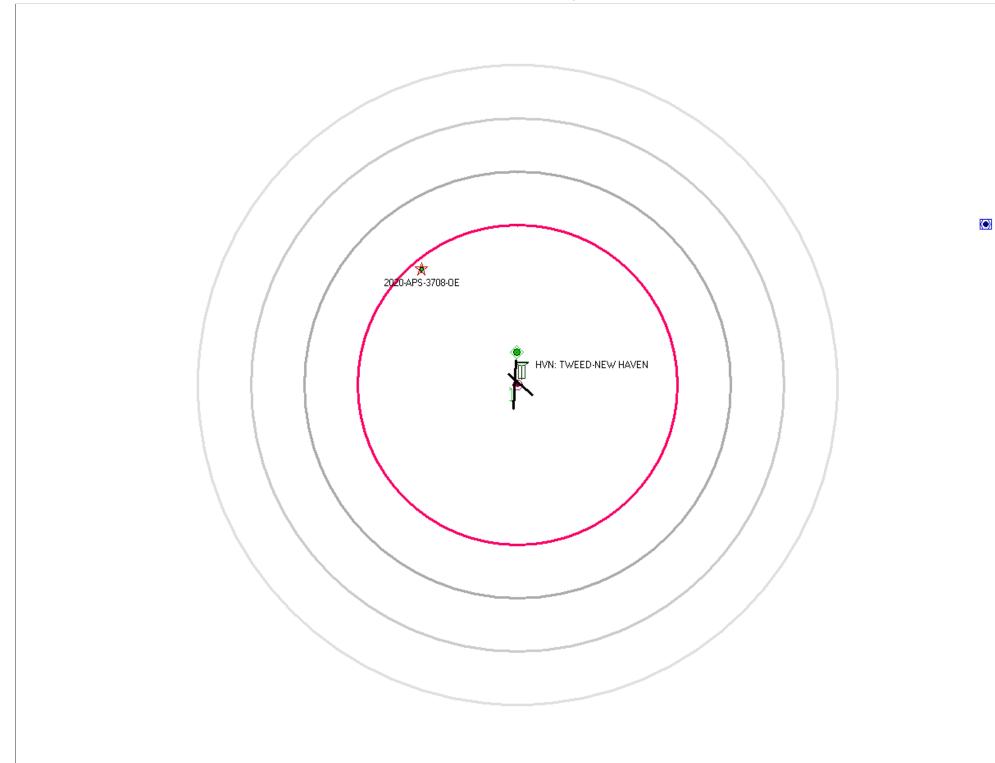


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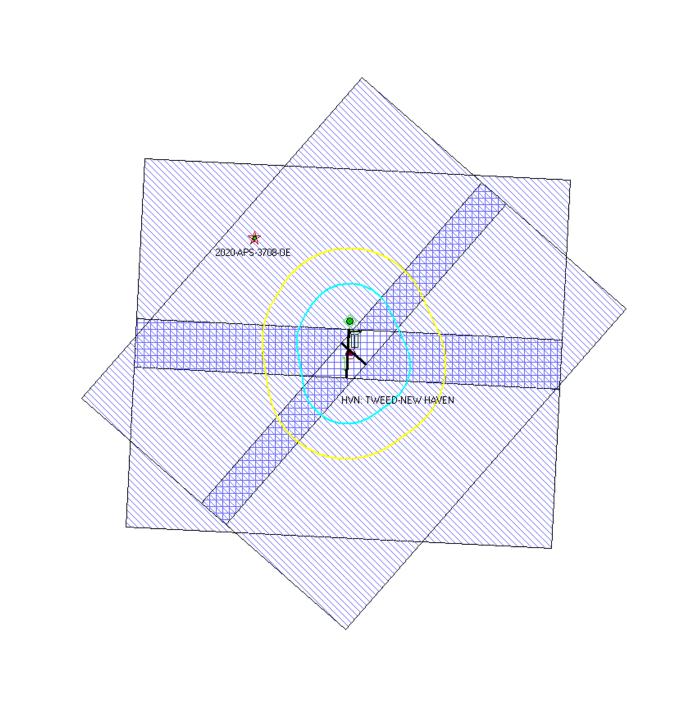


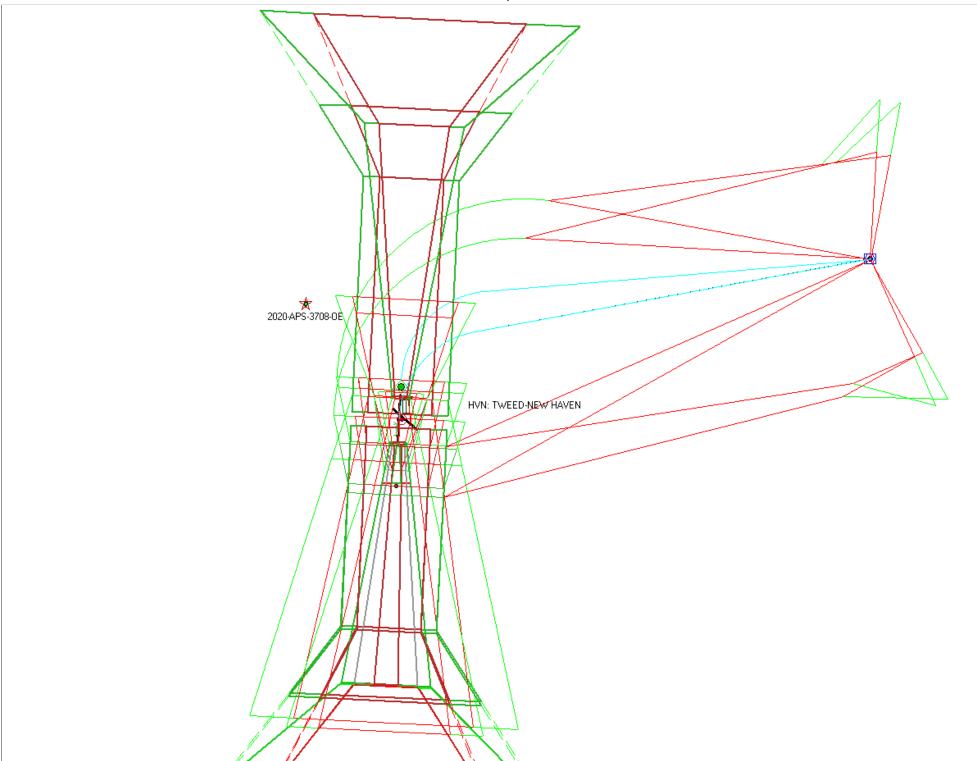


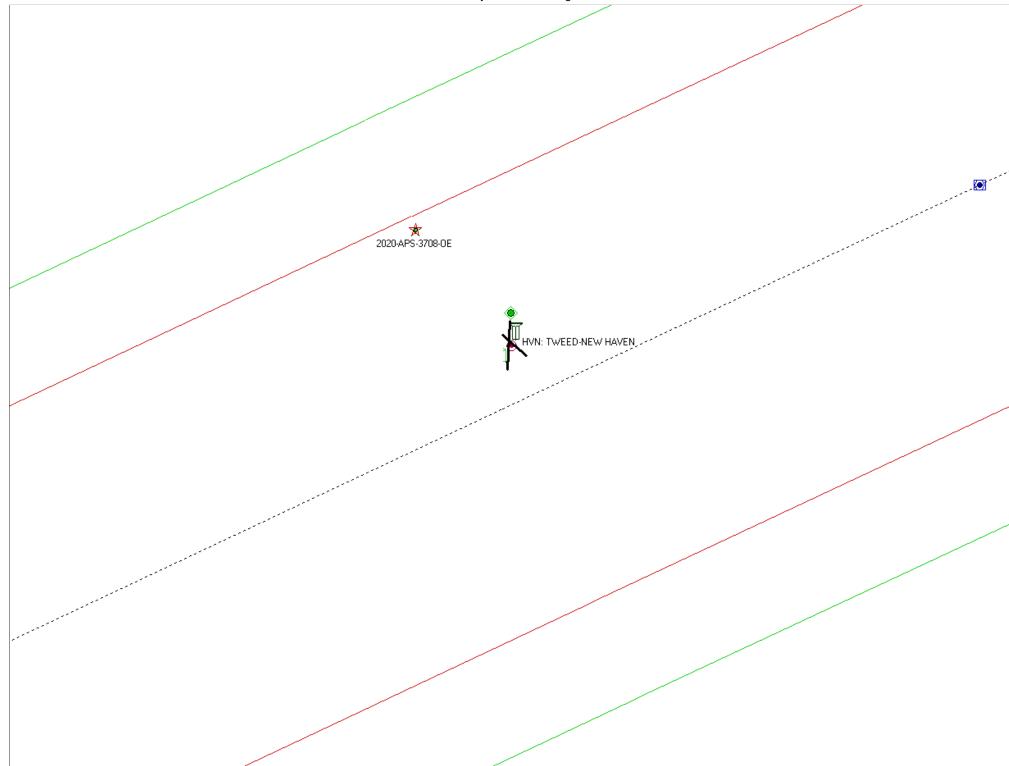




 $\langle \circ \rangle$ 







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FILE: 2020-APS-3708-OE

LATITUDE: 41 - 17 - 59.54 LONGITUDE: 72 - 55 - 35.57

SITE ELEVATION AMSL..... 11 ft. STRUCTURE HEIGHT..... 160 ft. OVERALL HEIGHT AMSL..... 171 ft.

> FAR 77.17(a)(4) - EN ROUTE CRITERIA MINIMUM OBSTACLE CLEARANCE ALTITUDE (MOCA)

### LOW ALTITUDE AIRWAY

AIRWAY	SEQUENCE	LATITUDE	LONGITUDE	MEA	LENGTH (NM)
V188	140	41-19-35.11N	073-16-59.58W	3000	20.09
V188	150	41-23-33.74N	072-50-50.56W	3000	

Minimum Obstacle Clearance Altitude (MOCA) is: 3000 AMSL.

Proposed structure is between the above points along Airway V188. The Abeam distance from the course centerline is 4.74 NM. The proposed structure is within the width of the secondary area of this airway. The width of the primary area is 8 NM and the width of the secondary is 2 NM.

The maximum allowable height permitted by the secondary area MOCA of this airway at this location is 2684 feet AMSL.

LOW ALTITUDE AIRWAY

AIRWAY	SEQUENCE	LATITUDE	LONGITUDE	MEA	LENGTH (NM)
V229 V229	210 220	41-17-58.03N 41-23-33.74N	072-57-32.8W 072-50-50.56W	2000 2000	7.53
VZZ9	220	41-23-33.74N	072-50-50.56W	2000	

Minimum Obstacle Clearance Altitude (MOCA) is: 2000 AMSL.

Proposed structure is between the above points along Airway V229. The Abeam distance from the course centerline is 1.07 NM. The proposed structure is within the width of the primary area of this airway. The width of the primary area of this airway is 8 NM. The minimum en route altitude (MEA) for this airway segment Is 2000 feet AMSL. Any Height above 1000 feet AMSL will not be approved. Your proposed structure must remain below this value.

#### LOW ALTITUDE AIRWAY

AIRWAY	SEQUENCE	LATITUDE	LONGITUDE	MEA	LENGTH (NM)
V374	80	41-13-59.78N	073-11-37.93W	2500	17.54
V374	90	41-11-08.77N	072-48-41.98W	2500	

Minimum Obstacle Clearance Altitude (MOCA) is: 2500 AMSL.

Proposed structure is between the above points along Airway V374. The Abeam distance from the course centerline is 5.9 NM. The proposed structure is within the width of the secondary area of this airway. The width of the primary area is 8 NM and the width of the secondary is 2 NM.

The maximum allowable height permitted by the secondary area MOCA of this airway at this location is 2474 feet AMSL.

LOW ALTITUDE AIRWAY

AIRWAY	SEQUENCE	LATITUDE	LONGITUDE	MEA	LENGTH (NM)
V475	60	41-09-38.495N	073-07-28.188W	2000	11.72
V475	70	41-14-38.04N	072-53-25.59W	2000	

Minimum Obstacle Clearance Altitude (MOCA) is: 1500 AMSL.

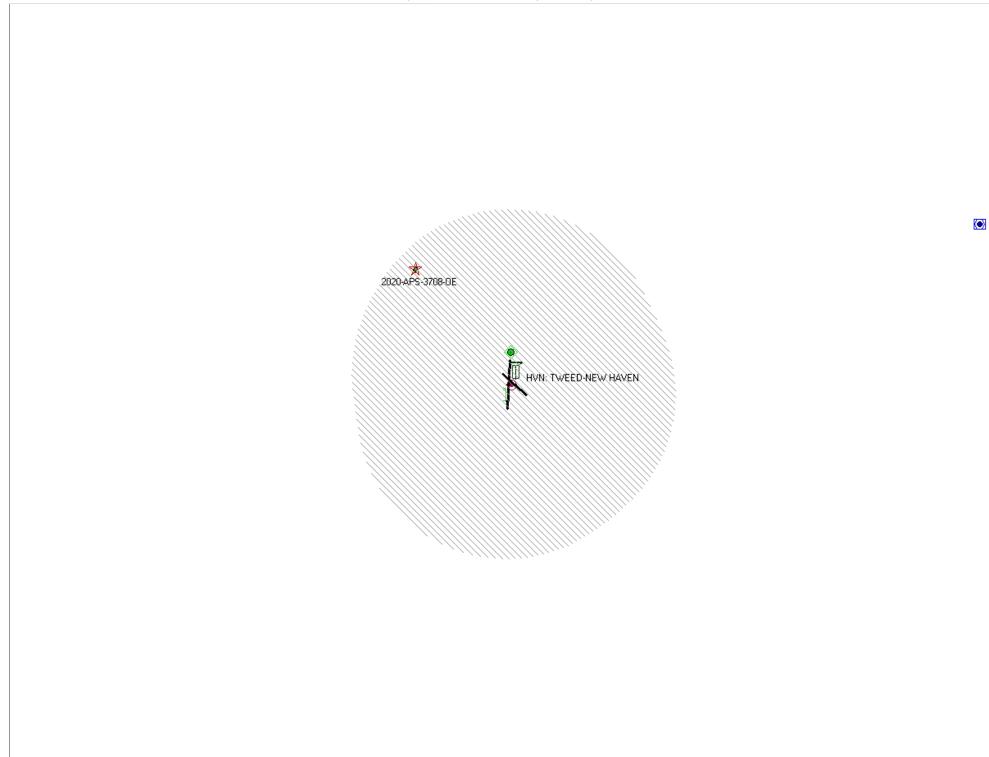
Proposed structure is between the above points along Airway V475. The Abeam distance from the course centerline is 3.73 NM. The proposed structure is within the width of the primary area of this airway. The width of the primary area of this airway is 8 NM. The minimum en route altitude (MEA) for this airway segment Is 2000 feet AMSL. Any Height above 500 feet AMSL will not be approved. Your proposed structure must remain below this value.

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05-22-2020 12:40:42

The mathematical algorithms used by this program are derived directly from Federal Aviation Regulations Part 77, sub-part C.



### Circling Approach Area Analysis

\*\*\* 2020-APS-3708-OE \*\*\*

### TWEED-NEW HAVEN

Date: 05-22-2020 Time: 13:17:25

#### STUDY OBJECT DATA

Study Latitude: 41° 17' 59.54" N Study Longitude: 72° 55' 35.57" W Ground Elevation: 11' AMSL ft. AGL Height: 160' AGL ft. Overall Elevation: 171' AMSL ft.

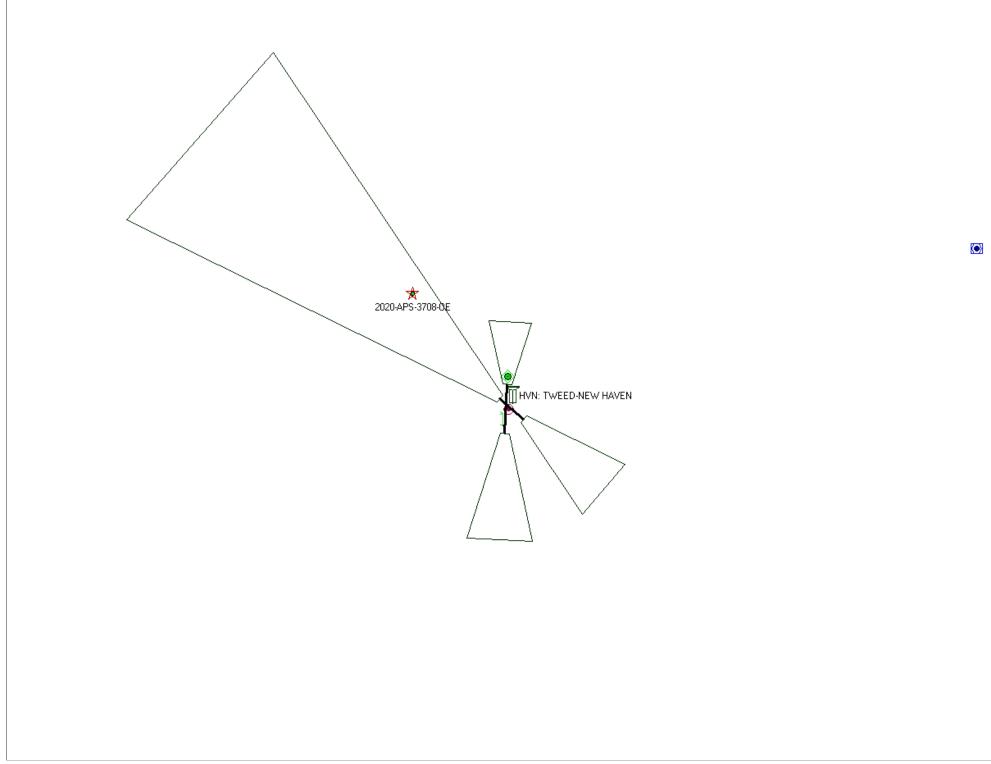
### INSTRUMENT APPROACH PROCEDURE (IAP) ANALYSIS

Distance: 14984 ft. Aircraft Category: C Circling MDA: 780 Vkias: 140 knots Vktas: 145.7757 knots Bank Angle: 20° Straight Segment: 0.5 NM Expanded CAA: True Turn Radius: 2.8 NM

Maximum AMSL: 480

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The mathematical algorithms used by this program are derived directly from Federal Aviation Administration (FAA) Orders on Instrument Flight Procedures.



### Departure Runway 32

### \*\*\* 2020-APS-3708-OE \*\*\*

**TWEED-NEW HAVEN - Runway: 32** Date: 05-27-2020 Time: 09:54:32

#### STUDY OBJECT DATA

Study Latitude: 41° 17' 59.54" N Study Longitude: 72° 55' 35.57" W Ground Elevation: 11' AMSL ft. AGL Height: 160' AGL ft. Overall Elevation: 171' AMSL ft.

INSTRUMENT DEPARTURE ANALYSIS

Initial Climb Area (ICA): DNE ICA Diverse Departure A Inside Diverse A - Max Hgt: 899 ft Diverse Departure B Not in Diverse B - DNE Diverse B

The above analysis is in accordance with FAA Order 8260.3B Change 26. This analysis used a 465 ft/NM climb gradient (CG) and an Obstacle Clearance Surface (OCS) that provides 111 feet of obstacle clearance at 1 NM from the Departure End of Runway (DER). Some runways have published climb gradients greater than 200 ft/NM. A specified climb gradient greater than standard (200 ft/NM) is sometimes necessary to allow acceptable obstacle clearance. Should your location exceed the value indicated above you may need to determine if there is a published CG and conduct additional calculations to determine if the CG will provide proper clearance for your proposed structure.

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The mathematical algorithms used by this program are derived directly from Federal Aviation Administration (FAA) Orders on Instrument Flight Procedures.

### TERPS ANALYSIS SUMMARY

\*\*\* 2020-APS-3708-OE \*\*\*

### STUDY OBJECT DATA

Study Latitude:	41° 17' 59.54"
Study Longitude:	72° 55' 35.57"
Ground Elevation:	11' AMSL
AGL Height:	160' AGL
Overall Elevation:	171' AMSL
AIRSPACE/TERPS LIMIT	: 363' AMSL VFR TRAFFIC PATTERN AIRSPACE

#### HVN IAP RWY 02 ILS19 Amdt 18 10000 HVN IAP RWY 02 LOC19 Amdt 18 10000 HVN IAP RWY 02 LPV Amdt 1 10000 HVN IAP RWY 02 VNAV Amdt 1 10000 HVN IAP RWY 02 LNAV Amdt 1 10000 HVN IAP RWY 20X LOC19 Oriq-1DR 10000 HVN IAP RWY 20X LNAV 10000 Oriq -1DR HVN MRP LOW ALTITUDE AIRWAY V475 500 HVN CIR CATEGORY C EXPANDED 480 HVN DEP RUNWAY 02 DIVERSE A 712 HVN DEP RUNWAY 32 899 DIVERSE A HVN VFR TRAFFIC PATTERN AIRSPACE CATEGORY D CLIMB/DESCEND AREA 363 HVN VFR TRANSITIONAL SURFACE 77.17(A)(2) 213

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## POINT ELEVATION DATA

## SRTM GROUND ELEVATION DATA North American Datum 1983 North American Vertical Datum 1988 - NAVD88

### 2020-APS-3708-OE MCM\_CT-520

Latitude:	41° - 17' - 59.54" N	Decimal Degrees: 41.2998722222222°
Longitude:	72° - 55' - 35.57" W	Decimal Degrees: 72.9265472222222°

## **Ground Elevation: 8.18 Feet AMSL**

This certifies the Digital Elevation Model (DEM) value for the specified latitude/longitude point was obtained from the SRTM Endeavour radar mission of February 2000. NASA has released the finished version edited by the National Intelligence Agency. The elevation value meets vertical accuracy criteria as specified by FAA Order 8260.19C, Appendix 2, Obstacle Accuracy Standards, Codes And Sources, paragraph 101 for Code 'C'. The elevation value for the specified latitude/longitude is accurate to within ±20 feet vertically.

Date Printed: 05-21-2020

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# **ATTACHMENT 8**

### KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

August 26, 2020

Via Certificate of Mailing

Justin Elicker, Mayor City of New Haven 165 Church Street, 2<sup>nd</sup> Floor New Haven, CT 06510

## Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to its Existing Wireless Telecommunications Facility at 54 Meadow Street, New Haven, Connecticut

Dear Mayor Elicker:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval to make certain modifications to its existing telecommunications facility on the roof of the building at 54 Meadow Street in New Haven (the "Property").

The modifications will consist of removing certain antennas and installing newer model antennas and remote radio heads at various locations on the roof. The existing facility is under the exclusive jurisdiction of the Connecticut Siting Council by virtue of its April 1, 1991 approval of Docket No. 140.

A copy of the full Petition is attached for your review. Landowners whose parcels are considered to abut the Property were also sent notice of this filing along with a copy of the Petition.

Please contact me if you have any questions regarding this proposal.

Sincerely,

Kunig mm

Kenneth C. Baldwin

Attachment

Boston | Hartford | New York | Providence | Stamford | Albany | Los Angeles | Miami | New London | rc.com

### KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

August 26, 2020

Via Certificate of Mailing

Aicha Woods, Director of City Plan City of New Haven 165 Church Street, 5<sup>th</sup> Floor New Haven, CT 06510

## Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to its Existing Wireless Telecommunications Facility at 54 Meadow Street, New Haven, Connecticut

Dear Ms. Woods:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval to make certain modifications to its existing telecommunications facility on the roof of the building at 54 Meadow Street in New Haven (the "Property").

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A copy of the full Petition is attached for your review. Landowners whose parcels are considered to abut the Property were also sent notice of this filing along with a copy of the Petition.

Please contact me if you have any questions regarding this proposal.

Sincerely,

Kuniel mm

Kenneth C. Baldwin

Attachment

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### KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

August 26, 2020

Via Certificate of Mailing

Gateway Partners LLC c/o Lexington Property Management 30 Lewis Street Hartford, CT 06103

## Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to its Existing Wireless Telecommunications Facility at 54 Meadow Street, New Haven, Connecticut

Dear Sir or Madam:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval to make certain modifications to its existing telecommunications facility on the roof of the building at 54 Meadow Street in New Haven (the "Property").

The modifications will consist of removing certain antennas and installing newer model antennas and remote radio heads at various locations on the roof. The existing facility is under the exclusive jurisdiction of the Connecticut Siting Council by virtue of its April 1, 1991 approval of Docket No. 140.

A copy of the full Petition is attached for your review. Landowners whose parcels are considered to abut the Property were also sent notice of this filing along with a copy of the Petition.

Please contact me if you have any questions regarding this proposal.

Sincerely,

Kuniel mm

Kenneth C. Baldwin

Attachment

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### KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

August 26, 2020

### Via Certificate of Mailing

MCM Holdings LLC 40 Woodland Street Hartford, CT 06105

### Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to its Existing Wireless Telecommunications Facility at 54 Meadow Street, New Haven, Connecticut

Dear Sir or Madam:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval to make certain modifications to its existing telecommunications facility on the roof of the building at 54 Meadow Street in New Haven (the "Property").

The modifications will consist of removing certain antennas and installing newer model antennas and remote radio heads at various locations on the roof. The existing facility is under the exclusive jurisdiction of the Connecticut Siting Council by virtue of its April 1, 1991 approval of Docket No. 140.

A copy of the full Petition is attached for your review. Landowners whose parcels are considered to abut the Property were also sent notice of this filing along with a copy of the Petition.

Please contact me if you have any questions regarding this proposal.

Sincerely,

Kenneth C. Baldwin

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Attachment

# **ATTACHMENT 9**

### KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

August 26, 2020

### Via Certificate of Mailing

«Owners\_and\_Mailing\_Address»

## Re: Petition for Declaratory Ruling Filed with the Connecticut Siting Council for Modifications to an Existing Wireless Telecommunications Facility at 54 Meadow Street, New Haven, Connecticut

Dear «Salutation»:

This firm represents Cellco Partnership d/b/a Verizon Wireless ("Cellco"). Today, Cellco filed a Petition for Declaratory Ruling ("Petition") with the Connecticut Siting Council ("Council") seeking approval to make certain modifications to its existing telecommunications facility on the roof of the building at 54 Meadow Street in New Haven (the "Property").

The modifications will consist of removing certain antennas and installing newer model antennas and remote radio heads at various locations on the roof. The existing facility is under the exclusive jurisdiction of the Connecticut Siting Council by virtue of its April 1, 1991 approval of Docket No. 140. A copy of the full Petition is attached for your review.

This notice is being sent to you because you are listed on the City Assessor's records as an owner of land that abuts the Property. If you have any questions regarding the Petition, the Council's process for reviewing the Petition or the details of the filing itself, please feel free to contact me at the number listed above. You may also contact the Council directly at 860-827-2935.

Sincerely,

Kunie BMM

Kenneth C. Baldwin

Attachment

21048844-v1

## CELLCO PARTNERSHIP D/B/A VERIZON WIRELESS

## **ABUTTING PROPERTY OWNERS**

## 54 MEADOWN STREET NEW HAVEN, CONNECTICUT

	Property Address	Owner's and Mailing Address
1.	78 Meadow Street	Knights of Columbus 1 Columbus Plaza New Haven, CT 06510
2.	1 Union Avenue	City of New Haven 1 Union Avenue New Haven, CT 06519
3.	170 Union Avenue	State of Connecticut PO Box 317546 Newington, CT 06131
4.	49 Union Avenue	City of New Haven Housing Authority 360 Orange Street New Haven, CT 06511
5.	86 South Orange Street	Church Street New Haven LLC 2150 Washington Street Newton, MA 02462
6.	90 South Orange Street	City of New Haven 165 Church Street New Haven, CT 06511