

# STATE OF CONNECTICUT

## CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: [siting.council@ct.gov](mailto:siting.council@ct.gov)

[www.ct.gov/csc](http://www.ct.gov/csc)

### VIA ELECTRONIC MAIL

August 9, 2018

Ryan Bailey  
Charles Cherundolo Consulting  
1280 Route 46 West, Suite 9  
Parsippany, NJ 07054

RE: **EM-SPRINT-166-180803** – Sprint notice of intent to modify an existing telecommunications facility located at 164 Country Road, rear, Wolcott, Connecticut.

Dear Mr. Bailey:

The Connecticut Siting Council (Council) is in receipt of your correspondence of August 9, 2018 submitted in response to the Council's August 7, 2018 notification of an incomplete request for exempt modification with regard to the above-referenced matter.

The submission renders the request for exempt modification complete and the Council will process the request in accordance with the Federal Communications Commission 60-day timeframe.

Thank you for your attention and cooperation.

Sincerely,

Melanie A. Bachman  
Executive Director

MAB/emr



## **Robidoux, Evan**

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**From:** Ryan Bailey <ryan@mackenzierealtyconsulting.com>  
**Sent:** Thursday, August 09, 2018 7:58 AM  
**To:** Robidoux, Evan  
**Cc:** CSC-DL Siting Council; Ryan Bailey  
**Subject:** RE: Council Incomplete for EM-SPRINT-166-180803-CountryRoadRear-Wolcott  
**Attachments:** CT60XC956 CSC filing .pdf

Attached please find a revised submission. I have updated the cover letter to show the property owner was sent the package as well as provided the proof of mailing. Please let me know if you need anything else.

Thank you

Ryan Bailey  
Mackenzie Realty Consulting  
3B Prospect Pl  
Madison NJ 07940  
856-625-1596  
973-215-2940 Fax  
[ryan@mackenzierealtyconsulting.com](mailto:ryan@mackenzierealtyconsulting.com)

**From:** Robidoux, Evan <Evan.Robidoux@ct.gov>  
**Sent:** Wednesday, August 8, 2018 10:13 AM  
**To:** Ryan Bailey <ryan@mackenzierealtyconsulting.com>  
**Cc:** CSC-DL Siting Council <Siting.Council@ct.gov>  
**Subject:** Council Incomplete for EM-SPRINT-166-180803-CountryRoadRear-Wolcott

Please see the attached correspondence.

Evan Robidoux  
Clerk Typist  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051



1280 Route 46 West, Suite 9, Parsippany NJ, 07054

Melanie Bachman  
Executive Director  
CT Siting Council  
10 Franklin Square  
New Britain, CT 06051

Re: Notice of Exempt Modification Application  
164 Country Rd, Rear, Wolcott, CT

Latitude: N41.5782  
Longitude: W72.9566

Dear Ms. Bachman:

Sprint currently maintains 3 existing panel antennas and 3 remote radio units at the 200'9" centerline level of the existing lattice tower. Sprint proposes to add 3 panel antennas and 6 remote radio unit at the 200'9" centerline on the tower. Sprint further proposes to add 1 hybrid cable and 30 Antenna to RRH jumper cables. Sprint is performing a new high-performance upgrade for cellular mobile communications. It is designed to increase the capacity and speed of mobile telephone networks.

Please accept this letter as notification to the Council, pursuant to R.C.S.A. Section 16-50j-73, for construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter is being sent to Mayor Thomas G. Dunn of the Town of Wolcott as well as David Kalinowski, Zoning Inspector for the Town of Wolcott and Insite Towers, owner of the tower as well as Mark Proul, property owner.

Attached is a summary of the planned modifications, including power density calculations reflecting the change in Sprint's operations at the site. Also included is documentation of the structural sufficiency of the tower with proposed modifications to accommodate the revised antenna configuration as well as the latest CSC decision, tax sheet and tax map.

### **Existing Facility**

CSC Summary Statement – CT60XC956 – 164 County Rd, Wolcott CT 06088

The Communications Tower facility is located at 164 Country Rd, Wolcott CT and is owned by Insite Tower, the Site coordinates are: N41.5762 W72.9566.

The existing facility consists of a 350' Lattice Tower. Sprint currently operates wireless communications equipment on a platform on a concrete slab at the facility and has 3 antennas and 3 RRU's mounted on at centerline of 200'9" feet.

## **Statutory Considerations**

The planned modifications to the facility fall within the activities explicitly provided for in R.C.S.A. 16-50j-72(b)(2)

1. The height of the overall structure will be unaffected.
2. The proposed changes will not require an extension of the property boundaries.
3. The proposed additions will not increase the noise level at the existing facility by six decibels or more, or to levels that exceed state and/or local criteria
4. The changes will not increase the calculated “worst case” power density for the combined operations at the site to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Sprint respectfully submits that the proposed changes at the referenced site constitute exempt modifications under R.C.S.A Section §16-50j-72(b)(2).

Respectfully submitted,

Ryan G Bailey  
Charles Cherundolo Consulting  
856-625-1596  
[ryan@mackenzierealtyconsulting.com](mailto:ryan@mackenzierealtyconsulting.com)

Additional Recipients:

Mayor Thomas G. Dunn for the Town of Wolcott– Via FedEx  
David Kalinowski, Zoning Officer for the Town of Wolcott - Via FedEx  
Insite Towers, owner of the tower – Via FedEx

Mark Proul, property owner – Via FedEx



# Sprint



PROJECT: MIMO UPGRADE  
 SITE NAME: COX COMMUNICATIONS TOWER  
 SITE CASCADE: CT60XC956  
 SITE ADDRESS: 164 COUNTY ROAD REAR  
 WOLCOTT, CT 06716  
 SITE TYPE: GUYED TOWER  
 MARKET: SOUTHERN CONNECTICUT

PLANS PREPARED FOR:

6580 Sprint Parkway  
 Overland Park, Kansas 66251

PLANS PREPARED BY:

FROM ZERO TO INFINIGY  
 the solutions are endless

1033 Watervliet Shaker Rd  
 Albany, NY 12205  
 Office # (518) 690-0790  
 JOB NUMBER 528-102

ENGINEERING LICENSE:

DRAWING NOTICE:

THESE DOCUMENTS ARE CONFIDENTIAL AND ARE THE SOLE PROPERTY OF SPRINT AND MAY NOT BE REPRODUCED, DISSEMINATED OR REDISTRIBUTED WITHOUT THE EXPRESS WRITTEN CONSENT OF SPRINT.

REVISIONS:	DESCRIPTION	DATE	BY	REV
REVISED/ISSUED FOR PERMIT		05/13/18	BMM	2
REVISED/ISSUED FOR PERMIT		04/24/18	BMM	1
ISSUED FOR PERMIT		11/10/17	ASW	0

SITE NAME:  
**COX COMMUNICATIONS TOWER**

SITE CASCADE:  
**CT60XC956**

SITE ADDRESS:  
 164 COUNTY ROAD REAR  
 WOLCOTT, CT 06716

SHEET DESCRIPTION:  
**TITLE SHEET & PROJECT DATA**

SHEET NUMBER:  
**T-1**

SITE INFORMATION	AREA MAP	PROJECT DESCRIPTION	DRAWING INDEX																																										
<p><b>TOWER OWNER:</b>            COXCOM, INC. COX ENTERPRISES            1400 LAKE HEARN DR, NE            ATLANTA, GA 30319</p> <p><b>LATITUDE (NAD83):</b>            41° 34' 34.3992" N            41.578222'</p> <p><b>LONGITUDE (NAD83):</b>            72° 57' 24.1092" W            -72.956697'</p> <p><b>COUNTY:</b>            NEW HAVEN</p> <p><b>ZONING JURISDICTION:</b>            TOWN OF WOLCOTT</p> <p><b>ZONING DISTRICT:</b>            TBD</p> <p><b>POWER COMPANY:</b>            CL&amp;P            (203) 597-4246</p> <p><b>AAV PROVIDER:</b>            AT&amp;T            (800) 246-2020</p> <p><b>SPRINT CM:</b>            JESSE ROSENTHAL            (862) 226-9768</p>		<p>SPRINT PROPOSES TO MODIFY AN EXISTING UNMANNED TELECOMMUNICATIONS FACILITY.</p> <ul style="list-style-type: none"> <li>INSTALL (1) 9927 EQUIPMENT CABINET IN EXISTING LEASE SPACE</li> <li>REMOVE (3) PANEL ANTENNAS</li> <li>INSTALL (6) PANEL ANTENNAS</li> <li>INSTALL (3) RRUS-800 TO TOWER</li> <li>INSTALL (30) JUMPER CABLES</li> <li>INSTALL (1) HYBRID CABLE</li> </ul> <p>THESE PLANS HAVE BEEN DEVELOPED FOR THE MODIFICATION OF AN EXISTING UNMANNED TELECOMMUNICATIONS FACILITY OWNED OR LEASED BY SPRINT IN ACCORDANCE WITH THE SCOPE OF WORK PROVIDED BY SPRINT. INFINIGY HAS INCORPORATED THIS SCOPE OF WORK IN THE PLANS. THESE PLANS ARE NOT FOR CONSTRUCTION UNLESS ACCOMPANIED BY A PASSING STRUCTURAL STABILITY ANALYSIS PREPARED BY A LICENSED STRUCTURAL ENGINEER. STRUCTURAL ANALYSIS MUST INCLUDE BOTH TOWER AND MOUNT.</p>	<table border="1"> <thead> <tr> <th>SHEET NO.</th> <th>SHEET TITLE</th> <th>REV.</th> </tr> </thead> <tbody> <tr> <td>T-1</td> <td>TITLE SHEET &amp; PROJECT DATA</td> <td>2</td> </tr> <tr> <td>SP-1</td> <td>SPRINT SPECIFICATIONS</td> <td>2</td> </tr> <tr> <td>SP-2</td> <td>SPRINT SPECIFICATIONS</td> <td>2</td> </tr> <tr> <td>SP-3</td> <td>SPRINT SPECIFICATIONS</td> <td>2</td> </tr> <tr> <td>A-1</td> <td>SITE PLAN</td> <td>2</td> </tr> <tr> <td>A-2</td> <td>TOWER ELEVATION</td> <td>2</td> </tr> <tr> <td>A-3</td> <td>ANTENNA LAYOUT &amp; MOUNTING DETAILS</td> <td>2</td> </tr> <tr> <td>A-4</td> <td>COLOR CODING AND NOTES</td> <td>2</td> </tr> <tr> <td>A-5</td> <td>EQUIPMENT &amp; MOUNTING DETAILS</td> <td>2</td> </tr> <tr> <td>A-6</td> <td>CIVIL DETAILS</td> <td>2</td> </tr> <tr> <td>A-7</td> <td>PLUMBING DIAGRAM</td> <td>2</td> </tr> <tr> <td>E-1</td> <td>ELECTRICAL &amp; GROUNDING PLAN</td> <td>2</td> </tr> <tr> <td>E-2</td> <td>ELECTRICAL &amp; GROUNDING DETAILS</td> <td>2</td> </tr> </tbody> </table>	SHEET NO.	SHEET TITLE	REV.	T-1	TITLE SHEET & PROJECT DATA	2	SP-1	SPRINT SPECIFICATIONS	2	SP-2	SPRINT SPECIFICATIONS	2	SP-3	SPRINT SPECIFICATIONS	2	A-1	SITE PLAN	2	A-2	TOWER ELEVATION	2	A-3	ANTENNA LAYOUT & MOUNTING DETAILS	2	A-4	COLOR CODING AND NOTES	2	A-5	EQUIPMENT & MOUNTING DETAILS	2	A-6	CIVIL DETAILS	2	A-7	PLUMBING DIAGRAM	2	E-1	ELECTRICAL & GROUNDING PLAN	2	E-2	ELECTRICAL & GROUNDING DETAILS	2
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	<p><b>LOCATION MAP</b></p>	<p><b>APPLICABLE CODES</b></p> <p>ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALL IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE CODES.</p> <ol style="list-style-type: none"> <li>INTERNATIONAL BUILDING CODE (2012 IBC)</li> <li>TIA-EIA-222-G OR LATEST EDITION</li> <li>NFPA 780 - LIGHTNING PROTECTION CODE</li> <li>2011 NATIONAL ELECTRIC CODE OR LATEST EDITION</li> <li>ANY OTHER NATIONAL OR LOCAL APPLICABLE CODES, MOST RECENT EDITIONS</li> <li>CT BUILDING CODE</li> <li>LOCAL BUILDING CODE</li> <li>CITY/COUNTY ORDINANCES</li> </ol>																																											





THESE OUTLINE SPECIFICATIONS IN CONJUNCTION WITH THE SPRINT STANDARD CONSTRUCTION SPECIFICATIONS, INCLUDING CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

**SECTION 01 100 – SCOPE OF WORK**

**PART 1 – GENERAL**

- 1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE SPRINT CONSTRUCTION STANDARDS FOR WIRELESS SITES, CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.
- 1.2 RELATED DOCUMENTS:
  - A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
  - B. SPRINT 'STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES' ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.
- 1.3 PRECEDENCE: SHOULD CONFLICTS OCCUR BETWEEN THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES INCLUDING THE STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES AND THE CONSTRUCTION DRAWINGS, INFORMATION ON THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE. NOTIFY SPRINT CONSTRUCTION MANAGER IF THIS OCCURS.
- 1.4 NATIONALLY RECOGNIZED CODES AND STANDARDS:
  - A. THE WORK SHALL COMPLY WITH APPLICABLE NATIONAL AND LOCAL CODES AND STANDARDS, LATEST EDITION, AND PORTIONS THEREOF, INCLUDED BUT NOT LIMITED TO THE FOLLOWING:
    - 1. GR-63-CORE NEBS REQUIREMENTS: PHYSICAL PROTECTION
    - 5. GR-78-CORE GENERIC REQUIREMENTS FOR THE PHYSICAL DESIGN AND MANUFACTURE OF TELECOMMUNICATIONS EQUIPMENT.
    - 3. GR-1089 CORE, ELECTROMAGNETIC COMPATIBILITY AND ELECTRICAL SAFETY –GENERIC CRITERIA FOR NETWORK TELECOMMUNICATIONS EQUIPMENT.
    - 4. NATIONAL FIRE PROTECTION ASSOCIATION CODES AND STANDARDS (NFPA) INCLUDING NFPA 70 (NATIONAL ELECTRICAL CODE – 'NEC') AND NFPA 101 (LIFE SAFETY CODE).
    - 5. AMERICAN SOCIETY FOR TESTING OF MATERIALS (ASTM)
    - 6. INSTITUTE OF ELECTRONIC AND ELECTRICAL ENGINEERS (IEEE)
    - 7. AMERICAN CONCRETE INSTITUTE (ACI)
    - 8. AMERICAN WIRE PRODUCERS ASSOCIATION (AWPA)
    - 9. CONCRETE REINFORCING STEEL INSTITUTE (CRSI)
    - 10. AMERICAN ASSOCIATION OF STATE HIGHWAY AND TRANSPORTATION OFFICIALS (AASHTO)
    - 11. PORTLAND CEMENT ASSOCIATION (PCA)
    - 12. NATIONAL CONCRETE MASONRY ASSOCIATION (NCMA)
    - 13. BRICK INDUSTRY ASSOCIATION (BIA)
    - 14. AMERICAN WELDING SOCIETY (AWS)
    - 15. NATIONAL ROOFING CONTRACTORS ASSOCIATION (NRCA)
    - 16. SHEET METAL AND AIR CONDITIONING CONTRACTORS' NATIONAL ASSOCIATION (SMACNA)
    - 17. DOOR AND HARDWARE INSTITUTE (DHI)
    - 18. OCCUPATIONAL SAFETY AND HEALTH ACT (OSHA)
    - 19. APPLICABLE BUILDING CODES INCLUDING UNIFORM BUILDING CODE, SOUTHERN BUILDING CODE, BOCA, AND THE INTERNATIONAL BUILDING CODE.
- 1.5 DEFINITIONS:
  - A. WORK: THE SUM OF TASKS AND RESPONSIBILITIES IDENTIFIED IN THE CONTRACT DOCUMENTS.
  - B. COMPANY: SPRINT CORPORATION
  - C. ENGINEER: SYNONYMOUS WITH ARCHITECT & ENGINEER AND 'A&E'. THE DESIGN PROFESSIONAL HAVING PROFESSIONAL RESPONSIBILITY FOR DESIGN OF THE PROJECT.
  - D. CONTRACTOR: CONSTRUCTION CONTRACTOR; CONSTRUCTION VENDOR; INDIVIDUAL OR ENTITY WHO AFTER EXECUTION OF A CONTRACT IS BOUND TO ACCOMPLISH THE WORK.
  - E. THIRD PARTY VENDOR OR AGENCY: A VENDOR OR AGENCY ENGAGED SEPARATELY BY THE COMPANY, A&E, OR CONTRACTOR TO PROVIDE MATERIALS OR TO ACCOMPLISH SPECIFIC TASKS RELATED TO BUT NOT INCLUDED IN THE WORK.
  - F. OFCI: OWNER FURNISHED, CONTRACTOR INSTALLED EQUIPMENT.
  - G. CONSTRUCTION MANAGER – ALL PROJECTS RELATED COMMUNICATION TO FLOW THROUGH SPRINT REPRESENTATIVE IN CHARGE OF PROJECT...

- 1.6 SITE FAMILIARITY: CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING HIMSELF WITH ALL CONTRACT DOCUMENTS, FIELD CONDITIONS AND DIMENSIONS PRIOR TO PROCEEDING WITH CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE SPRINT CONSTRUCTION MANAGER PRIOR TO THE COMMENCEMENT OF WORK. NO COMPENSATION WILL BE AWARDED BASED ON CLAIM OF LACK OF KNOWLEDGE OR FIELD CONDITIONS.
- 1.7 POINT OF CONTACT: COMMUNICATION BETWEEN SPRINT AND THE CONTRACTOR SHALL FLOW THROUGH THE SINGLE SPRINT CONSTRUCTION MANAGER APPOINTED TO MANAGE THE PROJECT FOR SPRINT.
- 1.8 ON-SITE SUPERVISION: THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE RESPONSIBLE FOR CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. THE CONTRACTOR SHALL EMPLOY A COMPETENT SUPERINTENDENT WHO SHALL BE IN ATTENDANCE AT THE SITE AT ALL TIMES DURING PERFORMANCE OF THE WORK.
- 1.9 DRAWINGS, SPECIFICATIONS AND DETAILS REQUIRED AT JOBSITE: THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A FULL SET OF THE CONSTRUCTION DRAWINGS, STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES AND THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES AT THE JOBSITE FROM MOBILIZATION THROUGH CONSTRUCTION COMPLETION.
  - A. THE JOBSITE DRAWINGS, SPECIFICATIONS AND DETAILS SHALL BE CLEARLY MARKED DAILY IN RED PENCIL WITH ANY CHANGES IN CONSTRUCTION OVER WHAT IS DEPICTED IN THE DOCUMENTS. AT CONSTRUCTION COMPLETION, THIS JOBSITE MARKUP SET SHALL BE DELIVERED TO THE COMPANY OR COMPANY'S DESIGNATED REPRESENTATIVE TO BE FORWARDED TO THE COMPANY'S A&E VENDOR FOR PRODUCTION OF 'AS-BUILT' DRAWINGS.
  - B. DETAILS ARE INTENDED TO SHOW DESIGN INTENT. MODIFICATIONS MAY BE REQUIRED TO SUIT JOB DIMENSIONS OR CONDITIONS, AND SUCH MODIFICATIONS SHALL BE INCLUDED AS PART OF THE WORK. CONTRACTOR SHALL NOTIFY SPRINT CONSTRUCTION MANAGER OF ANY VARIATIONS PRIOR TO PROCEEDING WITH THE WORK.
  - C. DIMENSIONS SHOWN ARE TO FINISH SURFACES UNLESS NOTED OTHERWISE. SPACING BETWEEN EQUIPMENT IS THE REQUIRED CLEARANCE. SHOULD THERE BE ANY QUESTIONS REGARDING THE CONTRACT DOCUMENTS, EXISTING CONDITIONS AND/OR DESIGN INTENT, THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING A CLARIFICATION FROM THE SPRINT CONSTRUCTION MANAGER PRIOR TO PROCEEDING WITH THE WORK.
- 1.10 USE OF JOB SITE: THE CONTRACTOR SHALL CONFINE ALL CONSTRUCTION AND RELATED OPERATIONS INCLUDING STAGING AND STORAGE OF MATERIALS AND EQUIPMENT, PARKING, TEMPORARY FACILITIES, AND WASTE STORAGE TO THE LEASE PARCEL UNLESS OTHERWISE PERMITTED BY THE CONTRACT DOCUMENTS.
- 1.11 UTILITIES SERVICES: WHERE NECESSARY TO CUT EXISTING PIPES, ELECTRICAL WIRES, CONDUITS, CABLES, ETC., OF UTILITY SERVICES, OR OF FIRE PROTECTION OR COMMUNICATIONS SYSTEMS, THEY SHALL BE CUT AND CAPPED AT SUITABLE PLACES OR WHERE SHOWN. ALL SUCH ACTIONS SHALL BE COORDINATED WITH THE UTILITY COMPANY INVOLVED:
- 1.12 PERMITS / FEES: WHEN REQUIRED THAT A PERMIT OR CONNECTION FEE BE PAID TO A PUBLIC UTILITY PROVIDER FOR NEW SERVICE TO THE CONSTRUCTION PROJECT, PAYMENT OF SUCH FEE SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR.
- 1.13 CONTRACTOR SHALL TAKE ALL MEASURES AND PROVIDE ALL MATERIAL NECESSARY FOR PROTECTING EXISTING EQUIPMENT AND PROPERTY.
- 1.14 METHODS OF PROCEDURE (MOPS) FOR CONSTRUCTION: CONTRACTOR SHALL PERFORM WORK AS DESCRIBED IN THE FOLLOWING INSTALLATION AND COMMISSIONING MOPS.
 

NOTE: IN SHORT-FORM SPECIFICATIONS ON THE DRAWINGS, A/E TO INSERT LIST OF APPLICABLE MOPS INCLUDING EN-2012-001, EN-2013-002, EL-0568, AND TS-0193
- 1.15 USE OF ELECTRONIC PROJECT MANAGEMENT SYSTEMS:

**PART 2 – PRODUCTS (NOT USED)**

**PART 3 – EXECUTION**

- 3.1 TEMPORARY UTILITIES AND FACILITIES: THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TEMPORARY UTILITIES AND FACILITIES NECESSARY EXCEPT AS OTHERWISE INDICATED IN THE CONSTRUCTION DOCUMENTS. TEMPORARY UTILITIES AND FACILITIES INCLUDE POTABLE WATER, HEAT, HVAC, ELECTRICITY, SANITARY FACILITIES, WASTE DISPOSAL FACILITIES, AND TELEPHONE/COMMUNICATION SERVICES. PROVIDE TEMPORARY UTILITIES AND FACILITIES IN ACCORDANCE WITH OSHA AND THE AUTHORITY HAVING JURISDICTION. CONTRACTOR MAY UTILIZE THE COMPANY ELECTRICAL SERVICE IN THE COMPLETION OF THE WORK WHEN IT BECOMES AVAILABLE. USE OF THE LESSORS OR SITE OWNER'S UTILITIES OR FACILITIES IS EXPRESSLY FORBIDDEN EXCEPT AS OTHERWISE ALLOWED IN THE CONTRACT DOCUMENTS.
- 3.2 ACCESS TO WORK: THE CONTRACTOR SHALL PROVIDE ACCESS TO THE JOB SITE FOR AUTHORIZED COMPANY PERSONNEL AND AUTHORIZED REPRESENTATIVES OF THE ARCHITECT/ENGINEER DURING ALL PHASES OF THE WORK.
- 3.3 TESTING: REQUIREMENTS FOR TESTING BY THIS CONTRACTOR SHALL BE AS INDICATED HEREWITH, ON THE CONSTRUCTION DRAWINGS, AND IN THE INDIVIDUAL SECTIONS OF THESE SPECIFICATIONS. SHOULD COMPANY CHOOSE TO ENGAGE ANY THIRD-PARTY TO CONDUCT ADDITIONAL TESTING, THE CONTRACTOR SHALL COOPERATE WITH AND PROVIDE A WORK AREA FOR COMPANY'S TEST AGENCY.
- 3.4 DIMENSIONS: VERIFY DIMENSIONS INDICATED ON DRAWINGS WITH FIELD DIMENSIONS BEFORE FABRICATION OR ORDERING OF MATERIALS. DO NOT SCALE DRAWINGS.

3.5 EXISTING CONDITIONS: NOTIFY THE SPRINT CONSTRUCTION MANAGER OF EXISTING CONDITIONS DIFFERING FROM THOSE INDICATED ON THE DRAWINGS. DO NOT REMOVE OR ALTER STRUCTURAL COMPONENTS WITHOUT PRIOR WRITTEN APPROVAL FROM THE ARCHITECT AND ENGINEER.

**SECTION 01 200 – COMPANY FURNISHED MATERIAL AND EQUIPMENT**

**PART 1 – GENERAL**

- 1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.
- 1.2 RELATED DOCUMENTS:
  - A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
  - B. SPRINT 'STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES' ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.

**PART 2 – PRODUCTS (NOT USED)**

**PART 3 – EXECUTION**

- 3.1 RECEIPT OF MATERIAL AND EQUIPMENT:
  - A. A COMPANY FURNISHED MATERIAL AND EQUIPMENT IS IDENTIFIED ON THE RF DATA SHEET IN THE CONSTRUCTION DOCUMENTS.
  - B. THE CONTRACTOR IS RESPONSIBLE FOR SPRINT PROVIDED MATERIAL AND EQUIPMENT AND UPON RECEIPT SHALL:
    - 1. ACCEPT DELIVERIES AS SHIPPED AND TAKE RECEIPT.
    - 2. VERIFY COMPLETENESS AND CONDITION OF ALL DELIVERIES.
    - 3. TAKE RESPONSIBILITY FOR EQUIPMENT AND PROVIDE INSURANCE PROTECTION AS REQUIRED IN AGREEMENT.
    - 4. RECORD ANY DEFECTS OR DAMAGES AND WITHIN TWENTY-FOUR HOURS AFTER RECEIPT, REPORT TO SPRINT OR ITS DESIGNATED PROJECT REPRESENTATIVE OF SUCH.
    - 5. PROVIDE SECURE AND NECESSARY WEATHER PROTECTED WAREHOUSING.
    - 6. COORDINATE SAFE AND SECURE TRANSPORTATION OF MATERIAL AND EQUIPMENT, DELIVERING AND OFF-LOADING FROM CONTRACTOR'S WAREHOUSE TO SITE.
- 3.2 DELIVERABLES:
  - A. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.
  - B. IF APPLICABLE, COMPLETE LOST/STOLEN/DAMAGED DOCUMENTATION REPORT AS NECESSARY IN ACCORDANCE WITH COMPANY PRACTICE, AND AS DIRECTED BY COMPANY.
  - C. UPLOAD DOCUMENTATION INTO SPRINT SITE MANAGEMENT SYSTEM (SMS) AND/OR PROVIDE HARD COPY DOCUMENTATION AS REQUESTED.

**SECTION 01 300 – CELL SITE CONSTRUCTION CO.**

**PART 1 – GENERAL**

- 1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.
- 1.2 RELATED DOCUMENTS:
  - A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
  - B. SPRINT 'STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES' ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.
- 1.3 NOTICE TO PROCEED
  - A. NO WORK SHALL COMMENCE PRIOR TO COMPANY'S WRITTEN NOTICE TO PROCEED AND THE ISSUANCE OF THE WORK ORDER.
  - B. UPON RECEIVING NOTICE TO PROCEED, CONTRACTOR SHALL FULLY PERFORM ALL WORK NECESSARY TO PROVIDE SPRINT WITH AN OPERATIONAL WIRELESS FACILITY.

**PART 2 – PRODUCTS (NOT USED)**

**PART 3 – EXECUTION**

- 3.1 FUNCTIONAL REQUIREMENTS:
  - A. THE ACTIVITIES DESCRIBED IN THIS PARAGRAPH REPRESENT MINIMUM ACTIONS AND PROCESSES REQUIRED TO SUCCESSFULLY COMPLETE THE WORK. THE ACTIVITIES DESCRIBED ARE NOT EXHAUSTIVE, AND CONTRACTOR SHALL TAKE ANY AND ALL ACTIONS AS NECESSARY TO SUCCESSFULLY COMPLETE THE CONSTRUCTION OF A FULLY FUNCTIONING WIRELESS FACILITY AT THE SITE IN ACCORDANCE WITH COMPANY PROCESSES.
  - B. SUBMIT SPECIFIC DOCUMENTATION AS INDICATED HEREIN, AND OBTAIN REQUIRED APPROVALS WHILE THE WORK IS BEING PERFORMED.
  - C. MANAGE AND CONDUCT ALL FIELD CONSTRUCTION SERVICE RELATED ACTIVITIES
  - D. PROVIDE CONSTRUCTION ACTIVITIES TO THE EXTENT REQUIRED BY THE CONTRACT DOCUMENTS, INCLUDING BUT NOT LIMITED TO THE FOLLOWING:

PLANS PREPARED FOR:



PLANS PREPARED BY:



ENGINEERING LICENSE:



DRAWING NOTICE:

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ISSUED FOR PERMIT	11/10/17	ASW	0

SITE NAME:

**COX COMMUNICATIONS TOWER**

SITE CASCADE:

**CT60XC956**

SITE ADDRESS:

164 COUNTY ROAD REAR  
WOLCOTT, CT 06716

SHEET DESCRIPTION:

**SPRINT SPECIFICATIONS**

SHEET NUMBER:

**SP-1**



**CONTINUE FROM SP-1**

1. PERFORM ANY REQUIRED SITE ENVIRONMENTAL MITIGATION.
2. PREPARE GROUND SITES; PROVIDE DE-GRUBBING; AND ROUGH AND FINAL GRADING, AND COMPOUND SURFACE TREATMENTS.
3. MANAGE AND CONDUCT ALL ACTIVITIES FOR INSTALLATION OF UTILITIES INCLUDING ELECTRICAL AND TELCO BACKHAUL.
4. INSTALL UNDERGROUND FACILITIES INCLUDING UNDERGROUND POWER AND COMMUNICATIONS CONDUITS, AND UNDERGROUND GROUNDING SYSTEM.
5. INSTALL ABOVE GROUND GROUNDING SYSTEMS.
6. PROVIDE NEW HVAC INSTALLATIONS AND MODIFICATIONS.
7. INSTALL "H-FRAMES", CABINETS AND SHELTERS AS INDICATED.
8. INSTALL ROADS, ACCESS WAYS, CURBS AND DRAINS AS INDICATED.
9. ACCOMPLISH REQUIRED MODIFICATION OF EXISTING FACILITIES.
10. PROVIDE ANTENNA SUPPORT STRUCTURE FOUNDATIONS.
11. PROVIDE SLABS AND EQUIPMENT PLATFORMS.
12. INSTALL COMPOUND FENCING, SIGHT SHIELDING, LANDSCAPING AND ACCESS BARRIERS.
13. PERFORM INSPECTION AND MATERIAL TESTING AS REQUIRED HEREINAFTER.
14. CONDUCT SITE RESISTANCE TO EARTH TESTING AS REQUIRED HEREINAFTER
15. INSTALL FIXED GENERATOR SETS AND OTHER STANDBY POWER SOLUTIONS.
16. INSTALL TOWERS, ANTENNA SUPPORT STRUCTURES AND PLATFORMS ON EXISTING TOWERS AS REQUIRED.
17. INSTALL CELL SITE RADIOS, MICROWAVE, GPS, COAXIAL MAINLINE, ANTENNAS, CROSS BAND COUPLERS, TOWER TOP AMPLIFIERS, LOW NOISE AMPLIFIERS AND RELATED EQUIPMENT.
18. PERFORM, DOCUMENT, AND CLOSE OUT ANY CONSTRUCTION CONTROL DOCUMENTS THAT MAY BE REQUIRED BY GOVERNMENT AGENCIES AND LANDLORDS.
19. PERFORM ANTENNA AND COAX SWEEP TESTING AND MAKE ANY AND ALL NECESSARY CORRECTIONS.
20. REMAIN ON SITE MOBILIZED THROUGHOUT HAND-OFF AND INTEGRATION TO ASSIST AS NEEDED UNTIL SITE IS DEEMED SUBSTANTIALLY COMPLETE AND PLACED "ON AIR."

**3.2 GENERAL REQUIREMENTS FOR CIVIL CONSTRUCTION:**

- A. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH. AT THE COMPLETION OF THE WORK, CONTRACTOR SHALL REMOVE FROM THE SITE ALL REMAINING RUBBISH, IMPLEMENTS, TEMPORARY FACILITIES, AND SURPLUS MATERIALS.
- B. EQUIPMENT ROOMS SHALL AT ALL TIMES BE MAINTAINED "BROOM CLEAN" AND CLEAR OF DEBRIS.
- C. CONTRACTOR SHALL TAKE ALL REASONABLE PRECAUTIONS TO DISCOVER AND LOCATE ANY HAZARDOUS CONDITION.
  1. IN THE EVENT CONTRACTOR ENCOUNTERS ANY HAZARDOUS CONDITION WHICH HAS NOT BEEN ABATED OR OTHERWISE MITIGATED, CONTRACTOR AND ALL OTHER PERSONS SHALL IMMEDIATELY STOP WORK IN THE AFFECTED AREA AND NOTIFY COMPANY IN WRITING. THE WORK IN THE AFFECTED AREA SHALL NOT BE RESUMED EXCEPT BY WRITTEN NOTIFICATION BY COMPANY.
  2. CONTRACTOR AGREES TO USE CARE WHILE ON THE SITE AND SHALL NOT TAKE ANY ACTION THAT WILL OR MAY RESULT IN OR CAUSE THE HAZARDOUS CONDITION TO BE FURTHER RELEASED IN THE ENVIRONMENT, OR TO FURTHER EXPOSE INDIVIDUALS TO THE HAZARD.
- D. CONTRACTOR'S ACTIVITIES SHALL BE RESTRICTED TO THE PROJECT LIMITS. SHOULD AREAS OUTSIDE THE PROJECT LIMITS BE AFFECTED BY CONTRACTOR'S ACTIVITIES, CONTRACTOR SHALL IMMEDIATELY RETURN THEM TO ORIGINAL CONDITION
- E. CONDUCT TESTING AS REQUIRED HEREIN.

**3.3 DELIVERABLES:**

- A. CONTRACTOR SHALL REVIEW, APPROVE, AND SUBMIT TO SPRINT SHOP DRAWINGS, PRODUCT DATA, SAMPLES, AND SIMILAR SUBMITTALS AS REQUIRED HEREINAFTER
- B. PROVIDE DOCUMENTATION INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING. DOCUMENTATION SHALL BE FORWARDED IN ORIGINAL FORMAT AND/OR UPLOADED INTO SMS.
  1. ALL CORRESPONDENCE AND PRELIMINARY CONSTRUCTION REPORTS.
  2. PROJECT PROGRESS REPORTS.
  3. CIVIL CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
  4. ELECTRICAL SERVICE COMPLETION DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).

5. LINES AND ANTENNA INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
6. POWER INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
7. TELCO READY DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
8. PPC (OR SHELTER) INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
9. TOWER CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
10. TOWER CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
11. BTS AND RADIO EQUIPMENT DELIVERED AT SITE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
12. NETWORK OPERATIONS HANDOFF CHECKLIST (HOC WALK) COMPLETE (UPLOAD FORM IN SMS)
13. CIVIL CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
14. SITE CONSTRUCTION PROGRESS PHOTOS UNLOADED INTO SMS.

**SECTION 01 400 - SUBMITTALS & TESTS**

**PART 1 - GENERAL**

- 1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.
- 1.2 RELATED DOCUMENTS:
  - A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
  - B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HERewith.
- 1.3 SUBMITTALS:
  - A. THE WORK IN ALL ASPECTS SHALL COMPLY WITH THE CONSTRUCTION DRAWINGS AND THESE SPECIFICATIONS.
  - B. SUBMIT THE FOLLOWING TO COMPANY REPRESENTATIVE FOR APPROVAL.
    1. CONCRETE MIX-DESIGNS FOR TOWER FOUNDATIONS, ANCHORS PIERS, AND CONCRETE PAVING.
    2. CONCRETE BREAK TESTS AS SPECIFIED HEREIN.
    3. SPECIAL FINISHES FOR INTERIOR SPACES, IF ANY.
    4. ALL EQUIPMENT AND MATERIALS SO IDENTIFIED ON THE CONSTRUCTION DRAWINGS.
    5. CHEMICAL GROUNDING DESIGN
  - D. ALTERNATES: AT THE COMPANY'S REQUEST, ANY ALTERNATIVES TO THE MATERIALS OR METHODS SPECIFIED SHALL BE SUBMITTED TO SPRINT'S CONSTRUCTION MANAGER FOR APPROVAL PRIOR TO BEING SHIPPED TO SITE. SPRINT WILL REVIEW AND APPROVE ONLY THOSE REQUESTS MADE IN WRITING. NO VERBAL APPROVALS WILL BE CONSIDERED. SUBMITTAL FOR APPROVAL SHALL INCLUDE A STATEMENT OF COST REDUCTION PROPOSED FOR USE OF ALTERNATE PRODUCT.

**1.4 TESTS AND INSPECTIONS:**

- A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL CONSTRUCTION TESTS, INSPECTIONS AND PROJECT DOCUMENTATION.
- B. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
  1. COAX SWEEPS AND FIBER TESTS PER TS-0200 REV 4 ANTENNA LINE ACCEPTANCE STANDARDS.
  2. AGL, AZIMUTH AND DOWNTILT USING ELECTRONIC COMMERCIAL MADE-FOR-THE-PURPOSE ANTENNA ALIGNMENT TOOL.
  3. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF TESTING.
- C. REQUIRED CLOSEOUT DOCUMENTATION INCLUDES, BUT IS NOT LIMITED TO THE FOLLOWING:
  1. AZIMUTH, DOWNTILT, AGL - UPLOAD REPORT FROM ANTENNA ALIGNMENT TOOL TO SITERRA TASK 465. INSTALLED AZIMUTH, DOWNTILT, AND AGL MUST CONFORM TO THE RF DATA SHEETS. SWEEP AND FIBER TESTS
  2. SCANABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT
  3. ALL AVAILABLE JURISDICTIONAL INFORMATION
  4. PDF SCAN OF REDLINES PRODUCED IN FIELD

5. ELECTRONIC AS-BUILT DRAWINGS IN AUTOCAD AND PDF FORMATS. ANY FIELD CHANGE MUST BE REFLECTED BY MODIFYING THE PLANS, ELEVATIONS, AND DETAILS IN THE DRAWING SETS. GENERAL NOTES INDICATING MODIFICATIONS WILL NOT BE ACCEPTED. CHANGES SHALL BE HIGHLIGHTED AS "CLOUDS" IDENTIFIED AS THE "AS-BUILT" CONDITION.
6. LIEN WAIVERS
7. FINAL PAYMENT APPLICATION
8. REQUIRED FINAL CONSTRUCTION PHOTOS
9. CONSTRUCTION AND COMMISSIONING CHECKLIST COMPLETE WITH NO DEFICIENT ITEMS
10. ALL POST NTP TASKS INCLUDING DOCUMENT UPLOADS COMPLETED IN SITERRA (SPRINTS DOCUMENT REPOSITORY OF RECORD).

- 1.5 COMMISSIONING: PERFORM ALL COMMISSIONING AS REQUIRED BY APPLICABLE MOPs
- 1.6 INTEGRATION: PERFORM ALL INTEGRATION ACTIVITIES AS REQUIRED BY APPLICABLE MOPs

**PART 2 - PRODUCTS (NOT USED)**

**PART 3 - EXECUTION**

**3.1 REQUIREMENTS FOR TESTING:**

**A. THIRD PARTY TESTING AGENCY:**

1. WHEN THE USE OF A THIRD PARTY INDEPENDENT TESTING AGENCY IS REQUIRED, THE AGENCY THAT IS SELECTED MUST PERFORM SUCH WORK ON A REGULAR BASIS IN THE STATE WHERE THE PROJECT IS LOCATED AND HAVE A THOROUGH UNDERSTANDING OF LOCAL AVAILABLE MATERIALS, INCLUDING THE SOIL, ROCK, AND GROUNDWATER CONDITIONS.
2. THE THIRD PARTY TESTING AGENCY IS TO BE FAMILIAR WITH THE APPLICABLE REQUIREMENTS FOR THE TESTS TO BE DONE, EQUIPMENT TO BE USED, AND ASSOCIATED HEALTH AND SAFETY ISSUES.
3. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASJTO, AND OTHER METHODS IS NEEDED.
4. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASJTO, AND OTHER METHODS IS NEEDED.

**3.2 REQUIRED TESTS:**

- A. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
  1. CONCRETE CYLINDER BREAK TESTS FOR THE TOWER AND ANCHOR FOUNDATIONS AS SPECIFIED IN SECTION: PORTLAND CEMENT CONCRETE PAVING.
  2. ASPHALT ROADWAY COMPACTED THICKNESS, SURFACE SMOOTHNESS, AND COMPACTED DENSITY TESTING AS SPECIFIED IN SECTION: HOT MIX ASPHALT PAVING.
  3. FIELD QUALITY CONTROL TESTING AS SPECIFIED IN SECTION: PORTLAND CEMENT CONCRETE PAVING.
  4. TESTING REQUIRED UNDER SECTION: AGGREGATE BASE FOR ACCESS ROADS, PADS AND ANCHOR LOCATIONS
  5. STRUCTURAL BACKFILL COMPACTION TESTS FOR THE TOWER FOUNDATION.
  6. SITE RESISTANCE TO EARTH TESTING PER EXHIBIT: CELL SITE GROUNDING SYSTEM DESIGN.
  7. ANTENNA AND COAX SWEEP TESTS PER EXHIBIT: ANTENNA TRANSMISSION LINE ACCEPTANCE STANDARDS.
  8. GROUNDING AT ANTENNA MASTS FOR GPS AND ANTENNAS
  9. ALL OTHER TESTS REQUIRED BY COMPANY OR JURISDICTION.

**3.3 REQUIRED INSPECTIONS**

- A. SCHEDULE INSPECTIONS WITH COMPANY REPRESENTATIVE.
- B. CONDUCT INSPECTIONS INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
  1. GROUNDING SYSTEM INSTALLATION PRIOR TO EARTH CONCEALMENT DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
  2. FORMING FOR CONCRETE AND REBAR PLACEMENT PRIOR TO POUR DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
  3. COMPACTION OF BACKFILL MATERIALS; AGGREGATE BASE FOR ROADS, PADS, AND ANCHORS; ASPHALT PAVING; AND SHAFT BACKFILL FOR CONCRETE AND WOOD POLES, BY INDEPENDENT THIRD PARTY AGENCY.
  4. PRE- AND POST-CONSTRUCTION ROOFTOP AND STRUCTURAL INSPECTIONS ON EXISTING FACILITIES.
  5. TOWER ERECTION SECTION STACKING AND PLATFORM ATTACHMENT DOCUMENTED BY DIGITAL PHOTOGRAPHS BY THIRD PARTY AGENCY.
  6. ANTENNA AZIMUTH , DOWN TILT AND PER SUNLIGHT TOOL SUNSIGHT INSTRUMENTS - ANTENNALIGN ALIGNMENT TOOL (AAT)

PLANS PREPARED FOR:



PLANS PREPARED BY:



ENGINEERING LICENSE:



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ISSUED FOR PERMIT	11/10/17	ASW	0

SITE NAME:

**COX COMMUNICATIONS TOWER**

SITE CASCADE:

**CT60XC956**

SITE ADDRESS:

164 COUNTY ROAD REAR  
WOLCOTT, CT 06716

SHEET DESCRIPTION:

**SPRINT SPECIFICATIONS**

SHEET NUMBER:

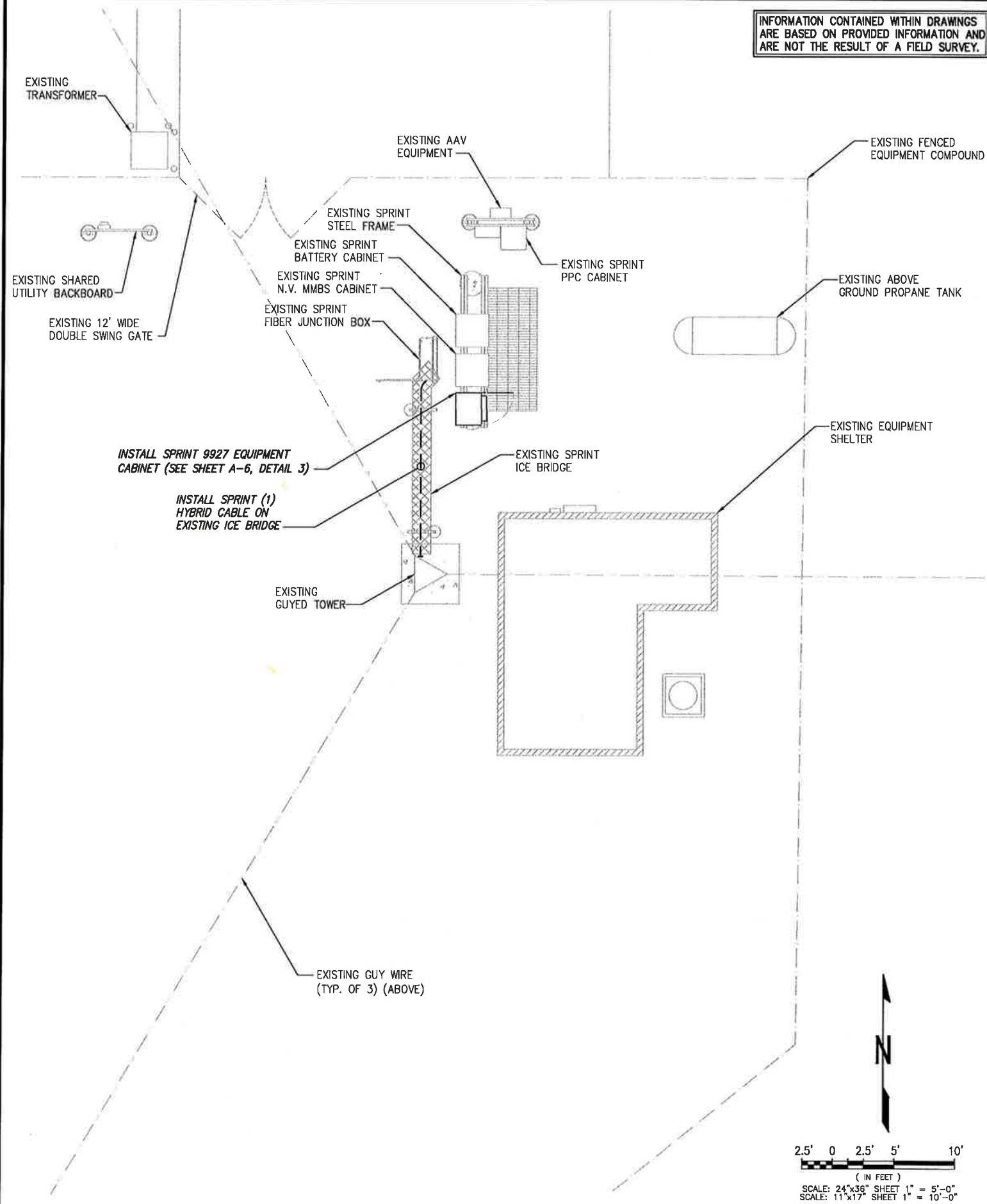
**SP-2**







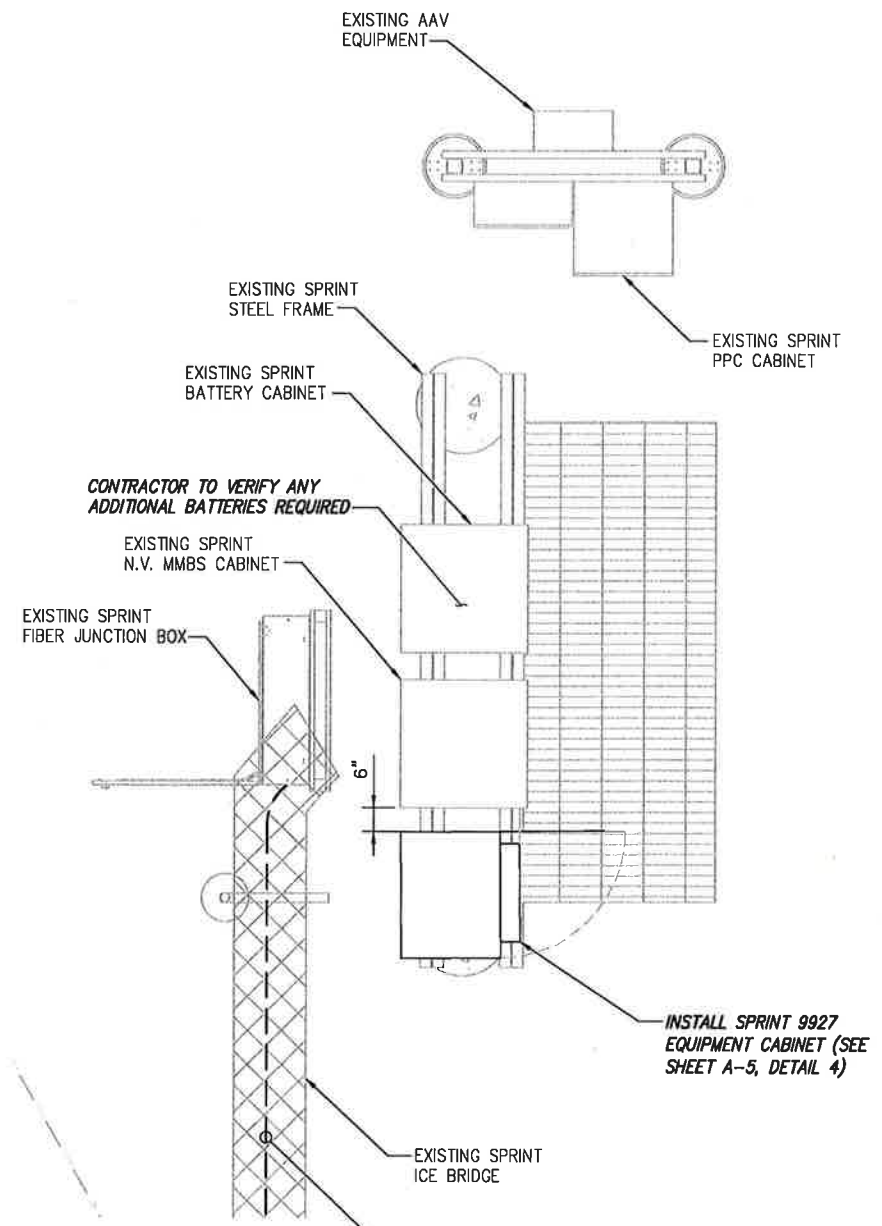
INFORMATION CONTAINED WITHIN DRAWINGS ARE BASED ON PROVIDED INFORMATION AND ARE NOT THE RESULT OF A FIELD SURVEY.



2.5' 0 2.5' 5' 10'  
( IN FEET )  
SCALE: 24"x36" SHEET 1" = 5'-0"  
SCALE: 11"x17" SHEET 1" = 10'-0"

OVERALL SITE PLAN

SCALE: AS NOTED 1



1' 0 1' 2' 4'  
( IN FEET )  
SCALE: 24"x36" SHEET 1" = 2'-0"  
SCALE: 11"x17" SHEET 1" = 4'-0"

SPRINT EQUIPMENT PLAN

SCALE: AS NOTED 2

PLANS PREPARED FOR:

6580 Sprint Parkway  
Overland Park, Kansas 66251

PLANS PREPARED BY:

FROM ZERO TO INFINIGY  
the solutions are endless

1033 Watervliet Shaker Rd  
Albany, NY 12205  
Office # (518) 690-0790  
JOB NUMBER 528-102

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WOLCOTT, CT 06716

SHEET DESCRIPTION:

**SITE PLAN**

SHEET NUMBER:

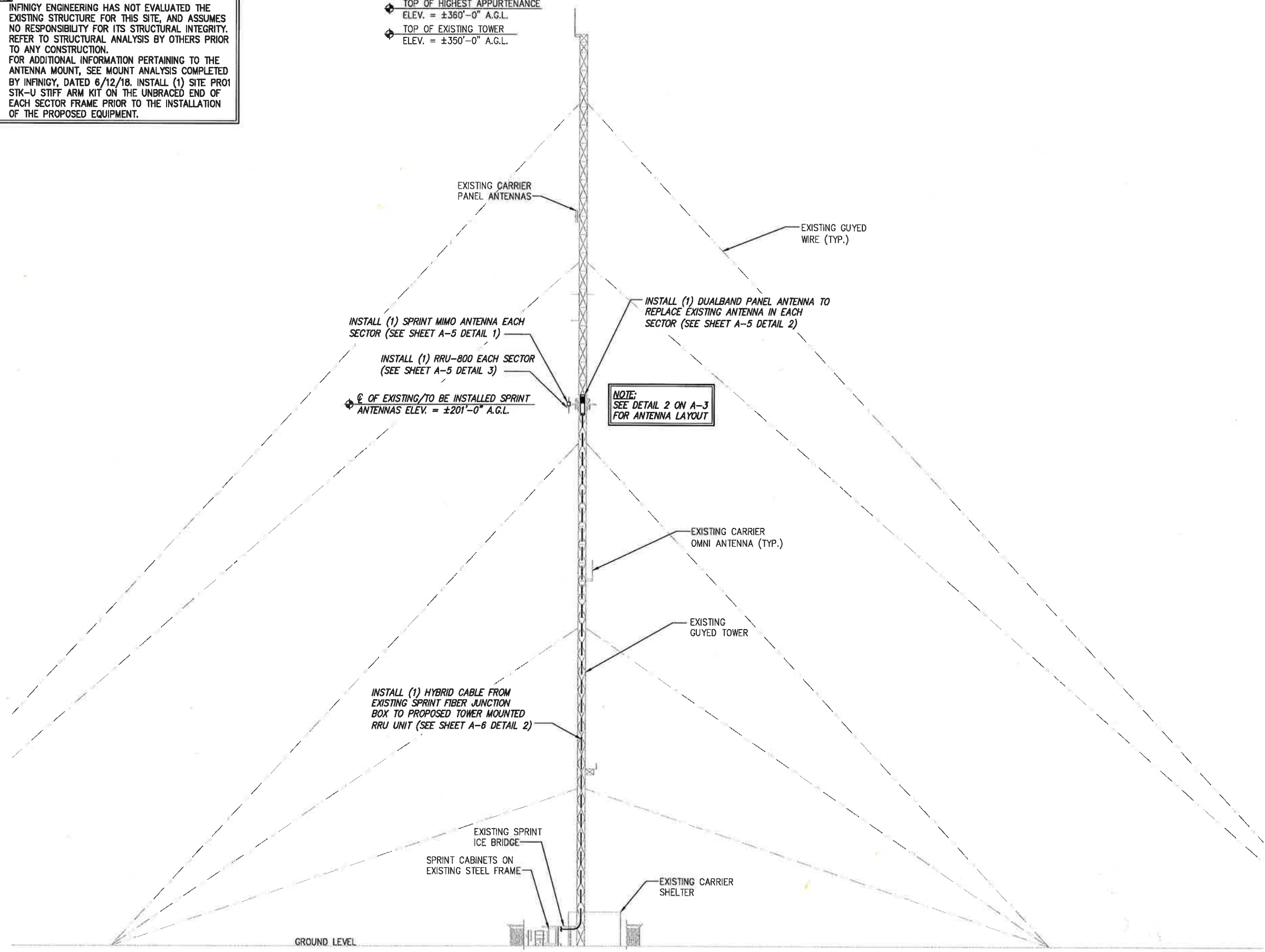
**A-1**

**NOTE:**

- INFINIGY ENGINEERING HAS NOT EVALUATED THE EXISTING STRUCTURE FOR THIS SITE, AND ASSUMES NO RESPONSIBILITY FOR ITS STRUCTURAL INTEGRITY. REFER TO STRUCTURAL ANALYSIS BY OTHERS PRIOR TO ANY CONSTRUCTION.
- FOR ADDITIONAL INFORMATION PERTAINING TO THE ANTENNA MOUNT, SEE MOUNT ANALYSIS COMPLETED BY INFINIGY, DATED 6/12/18. INSTALL (1) SITE PRO1 STK-U STIFF ARM KIT ON THE UNBRACED END OF EACH SECTOR FRAME PRIOR TO THE INSTALLATION OF THE PROPOSED EQUIPMENT.

◆ TOP OF HIGHEST APPURTENANCE  
ELEV. = ±360'-0" A.G.L.

◆ TOP OF EXISTING TOWER  
ELEV. = ±350'-0" A.G.L.



PLANS PREPARED FOR:

6580 Sprint Parkway  
Overland Park, Kansas 66251

PLANS PREPARED BY:

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ISSUED FOR PERMIT	11/10/17	ASW	0

SITE NAME:  
**COX COMMUNICATIONS TOWER**

SITE CASCADE:  
**CT60XC956**

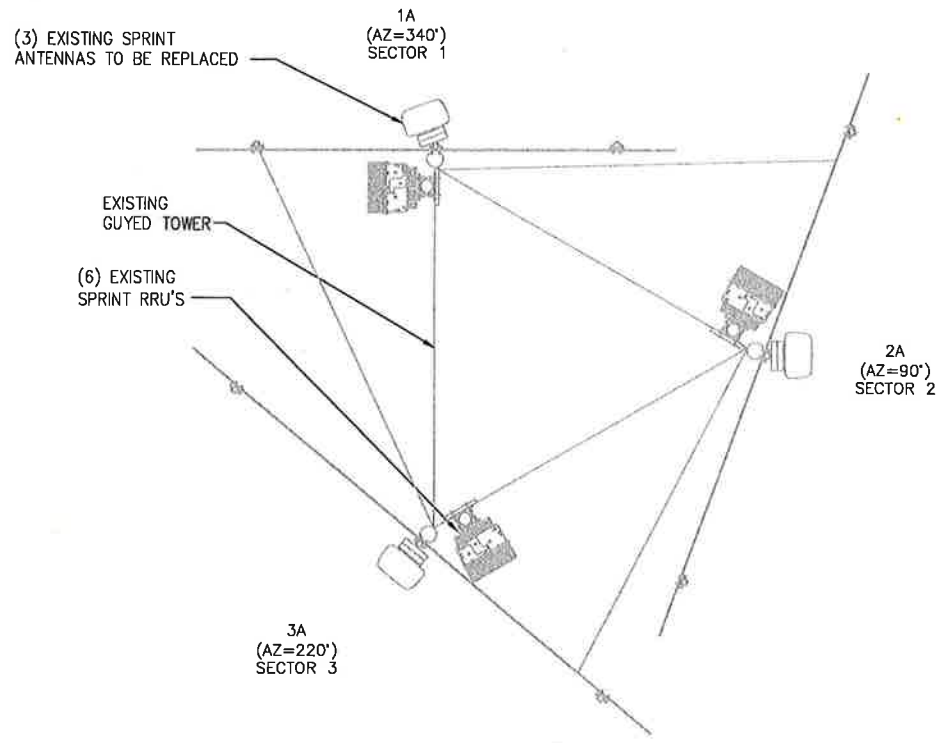
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**164 COUNTY ROAD REAR  
WOLCOTT, CT 06716**

SHEET DESCRIPTION:  
**TOWER ELEVATION**

SHEET NUMBER:  
**A-2**

**TOWER ELEVATION**



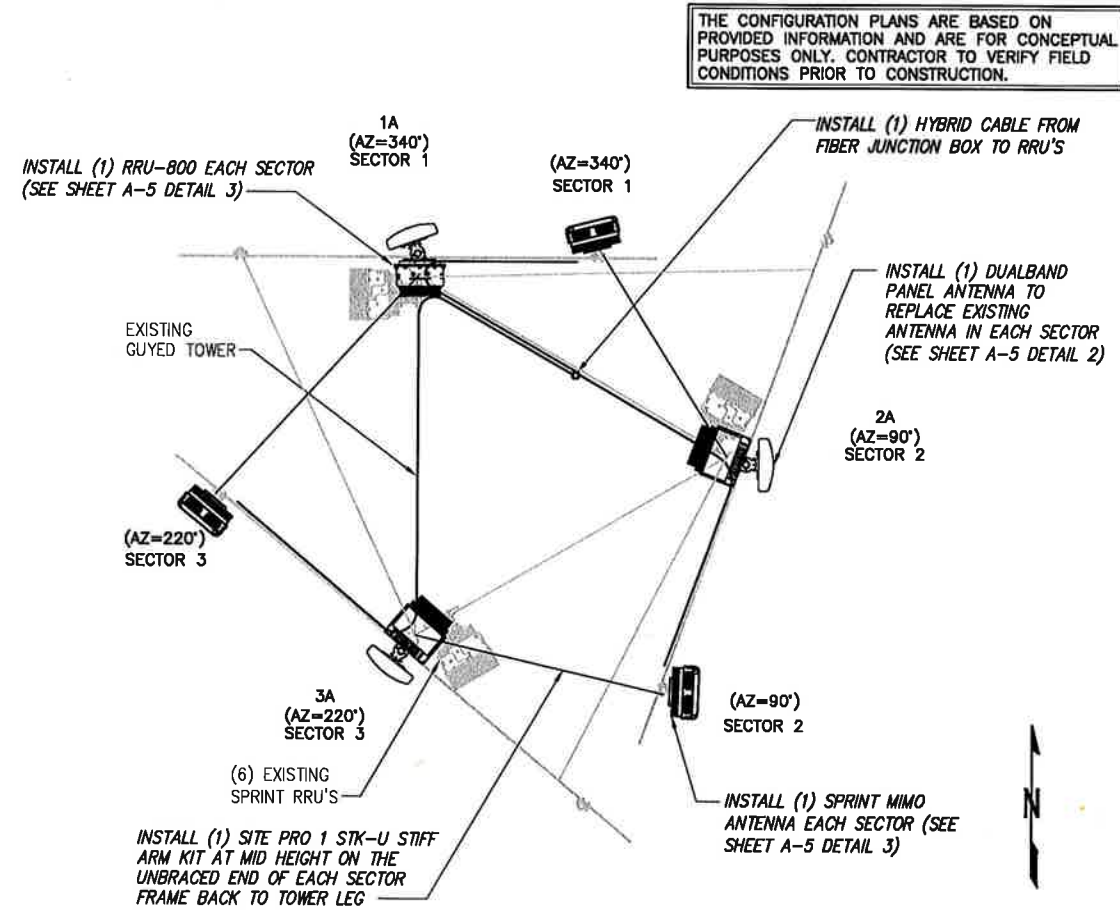


0° = TRUE NORTH

EXISTING ANTENNA & RRU LAYOUT

NO SCALE

1

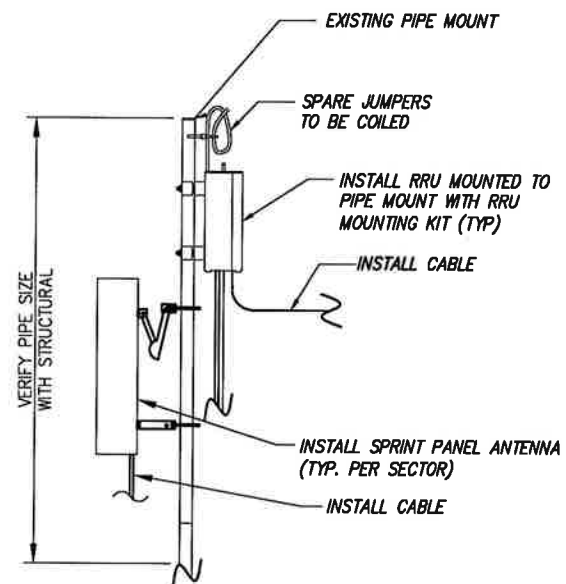


0° = TRUE NORTH

FINAL ANTENNA LAYOUT

NO SCALE

2



**NOTE:**  
CONTRACTOR TO POSITION RRU ON MOUNT BEHIND ANTENNA SUCH THAT THE RRU DOES NOT INTERFERE WITH THE EXISTING MOUNTING HARDWARE.

**NOTE:**  
THE DIAGRAM IS FOR CONCEPTUAL PURPOSES ONLY. CONTRACTOR IS TO REFER TO PASSING STRUCTURAL ANALYSIS FOR ANTENNA AND RRU MOUNTING DETAILS

DETAIL NOT USED

NO SCALE

3

TYPICAL ANTENNA & RRU MOUNTING DETAILS

NO SCALE

4

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Overland Park, Kansas 66251

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**CT60XC956**

SITE ADDRESS:  
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WOLCOTT, CT 06716

SHEET DESCRIPTION:  
**ANTENNA LAYOUT & MOUNTING DETAILS**

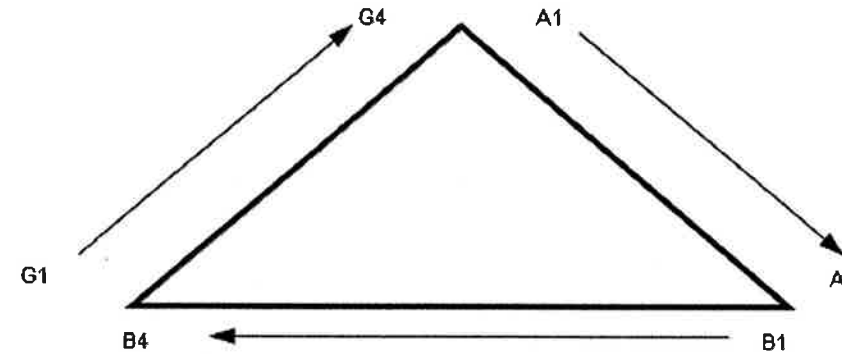
SHEET NUMBER:  
**A-3**

NV CABLES			
BAND	INDICATOR	PORT	COLOR
800-1	YEL GRN	NV-1	GRN
1900-1	YEL RED	NV-2	BLU
1900-2	YEL BRN	NV-3	BRN
1900-3	YEL BLU	NV-4	WHT
1900-4	YEL SLT	NV-5	RED
800-2	YEL ORG	NV-6	SLT
SPARE	YEL WHT	NV-7	PPL
2500	YEL PPL	NV-8	ORG

HYBRID	
HYBRID	COLOR
1	GRN
2	BLU
3	BRN
4	WHT
5	RED
6	SLT
7	PPL
8	ORG

2.5 Band		
2500 Radio 1	COLOR	
YEL WHT	GRN	GRN
YEL WHT	BLU	BLU
YEL WHT	BRN	BRN
YEL WHT	WHT	WHT
YEL WHT	RED	RED
YEL WHT	SLT	SLT
YEL WHT	PPL	PPL
YEL WHT	ORG	ORG

Figure 1: Antenna Orientation



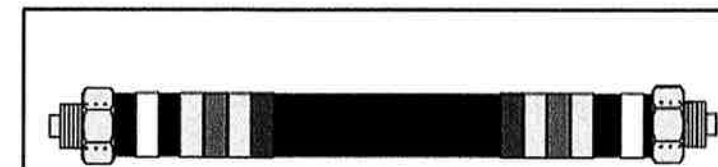
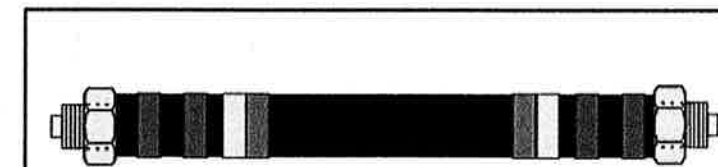
NOTES:

- ALL CABLES SHALL BE MARKED WITH 2" WIDE, UV STABILIZED, UL APPROVED TAPE.
- THE FIRST RING SHALL BE CLOSEST TO THE END OF THE CABLE AND SPACED APPROXIMATELY 2" FROM THE END CONNECTOR, WEATHERPROOFING, OR BREAK-OUT CYLINDER. THERE SHALL BE A 1" SPACE BETWEEN EACH RING FOR THE CABLE IDENTIFIER, AND NO SPACES BETWEEN THE FREQUENCY BANDS.
- A 2" GAP SHALL SEPARATE THE CABLE COLOR CODE FROM THE FREQUENCY COLOR CODE. THE 2" COLOR RINGS FOR THE FREQUENCY CODE SHALL BE PLACED NEXT TO EACH OTHER WITH NO SPACES.
- THE 2" COLORED TAPE(S) SHALL EACH BE WRAPPED A MINIMUM OF 3 TIMES AROUND THE INDIVIDUAL CABLES, AND THE TAPE SHALL BE KEPT IN THE SAME LOCATION AS MUCH AS POSSIBLE.
- SITES WITH MORE THAN FOUR (4) SECTORS WILL REQUIRE ADDITIONAL RINGS FOR EACH SECTOR, FOLLOWING THE PATTERN. HIGH CAPACITY SITES WILL USE THE NEXT COLOR IN THE SEQUENCE FOR ADDITIONAL CABLES IN EACH SECTOR.
- HYBRID FIBER CABLE SHALL BE SECTOR IDENTIFIED INSIDE THE CABINET ON FREQUENCY BUNDLES, ON THE SEALTITE, ON THE MAIN LINE UPON EXIT OF SEALTITE, AND BEFORE AND AFTER THE BREAKOUT UNIT (MEDUSA), AS WELL AS BEFORE AND AFTER ANY ENTRANCE OR EXIT.
- HFC "MAIN TRUNK" WILL NOT BE MARKED WITH THE FREQUENCY CODES, AS IT CONTAINS ALL FREQUENCIES.
- INDIVIDUAL POWER PAIRS AND FIBER BUNDLES SHALL BE LABELED WITH BOTH THE CABLE AND FREQUENCY.

Sector	Cable	First Ring	Second Ring	Third Ring
1 Alpha	1	Green	No Tape	No Tape
1	2	Red	No Tape	No Tape
1	3	Brown	No Tape	No Tape
1	4	White	No Tape	No Tape
1	5	Blue	No Tape	No Tape
1	6	Grey	No Tape	No Tape
1	7	Purple	No Tape	No Tape
1	8	Orange	No Tape	No Tape
2 Beta	1	Green	Green	No Tape
2	2	Red	Red	No Tape
2	3	Brown	Brown	No Tape
2	4	White	White	No Tape
2	5	Blue	Blue	No Tape
2	6	Grey	Grey	No Tape
2	7	Purple	Purple	No Tape
2	8	Orange	Orange	No Tape
3 Gamma	1	Green	Green	Green
3	2	Red	Red	Red
3	3	Brown	Brown	Brown
3	4	White	White	White
3	5	Blue	Blue	Blue
3	6	Grey	Grey	Grey
3	7	Purple	Purple	Purple
3	8	Orange	Orange	Orange

NV FREQUENCY	INDICATOR	ID
800-1	YEL GRN	GRN
1900-1	YEL RED	BLU
1900-2	YEL BRN	BRN
1900-3	YEL BLU	BLU
1900-4	YEL SLT	SLT
800-1	YEL ORG	ORG
RESERVED	YEL WHT	WHT
RESERVED	YEL PPL	PPL

2.5 FREQUENCY	INDICATOR		ID
2500 -1	YEL	WHT	GRN
2500 -2	YEL	WHT	BLU
2500 -3	YEL	WHT	BRN
2500 -4	YEL	WHT	BLU
2500 -5	YEL	WHT	SLT
2500 -6	YEL	WHT	ORG
2500 -7	YEL	WHT	WHT
2500 -8	YEL	WHT	PPL



PLANS PREPARED FOR:

6580 Sprint Parkway  
Overland Park, Kansas 66251

PLANS PREPARED BY:

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ISSUED FOR PERMIT	11/10/17	ASW	0

SITE NAME:

**COX COMMUNICATIONS TOWER**

SITE CASCADE:

**CT60XC956**

SITE ADDRESS:

164 COUNTY ROAD REAR  
WOLCOTT, CT 06716

SHEET DESCRIPTION:

**COLOR CODING AND NOTES**

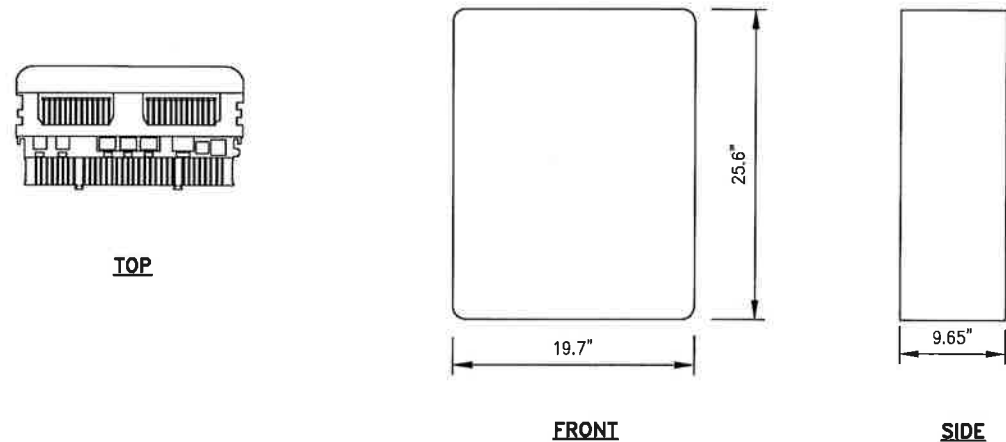
SHEET NUMBER:

**A-4**



**ANTENNA: NOKIA AAHC**

RADOME MATERIAL: FIBERGLASS  
 RADOME COLOR: LIGHT GREY  
 DIMENSIONS, HxWxD.in(mim): 25.6"x19.7"x9.65" (651x501x245mm)  
 WEIGHT: 103.6 lbs



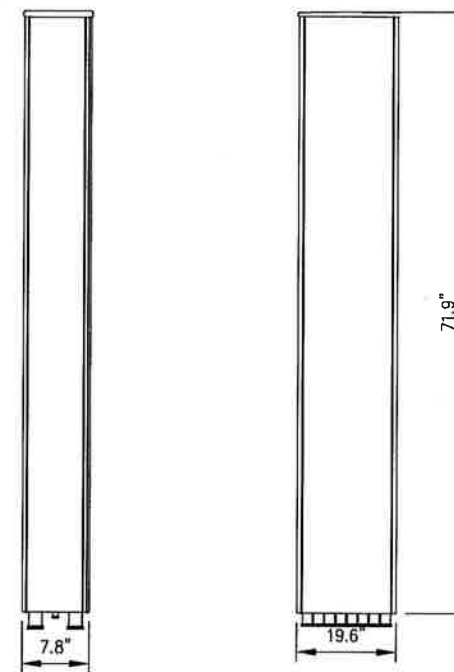
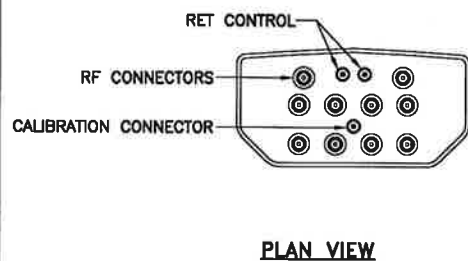
**NOKIA ANTENNA DETAIL**

NO SCALE

1

**ANTENNA COMMSCOPE NNVV-65B-R4**

RADOME MATERIAL: FIBERGLASS  
 RADOME COLOR: LIGHT GREY  
 DIMENSIONS, HxWxD.in(mim): 71.9"x19.6"x7.8" (1826x498x198mm)  
 WEIGHT: 77.4 lbs  
 CONNECTORS: (2) 7/16" DIN FEMALE  
 (8) 4.1/9.5 DIN FEMALE

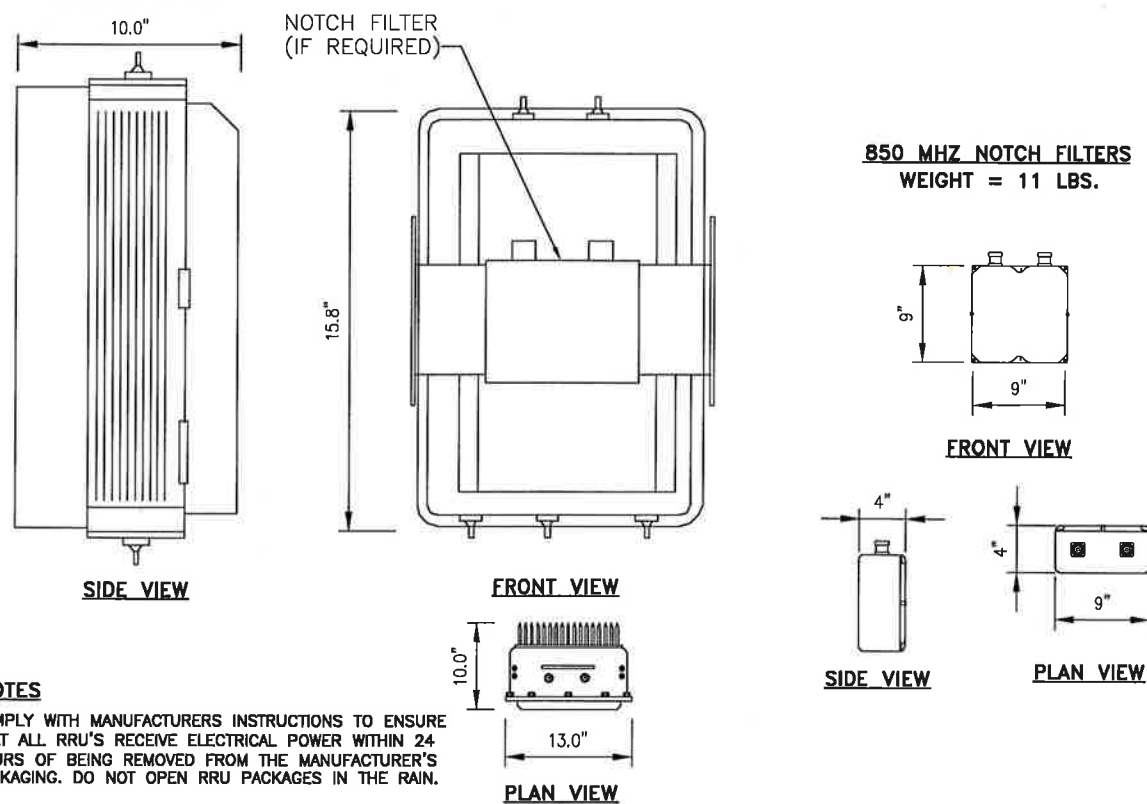


**DUALBAND ANTENNA**

NO SCALE

2

**RRU: ALCATEL LUCENT RRH 800 MHz 2x50W**  
 COLOR: LIGHT GREY  
 WEIGHT: 53 LBS.



**NOTES**  
 COMPLY WITH MANUFACTURERS INSTRUCTIONS TO ENSURE THAT ALL RRU'S RECEIVE ELECTRICAL POWER WITHIN 24 HOURS OF BEING REMOVED FROM THE MANUFACTURER'S PACKAGING. DO NOT OPEN RRU PACKAGES IN THE RAIN.

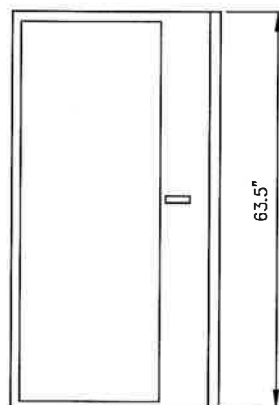
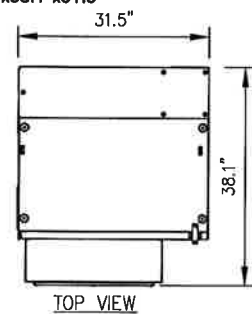
**800 RRU DETAIL**

NO SCALE

3

**ALU MODEL 9927**

DIMENSIONS, HxWxD: 65.5"x38.1"x31.5"



**DESIGN CRITERIA:**

2009 INTERNATIONAL BUILDING CODE W/ STATE MODIFICATION

WIND SPEED (ASCE-7-05)	90 MPH
EXPOSURE B	
IMPORTANCE FACTOR	1.0
SEISMIC SITE CLASS	D
S <sub>s</sub> =0.152 S <sub>1</sub> =0.050	
SEISMIC IMPORTANCE FACTOR	1.0
SEISMIC DESIGN CATEGORY	B
9927 MM BTS CABINET WEIGHT:	594 LBS.

**MATERIAL SPECIFICATIONS**

C-, M-, AND ANGLE SHAPES:	ASTM A36
HIGH-STRENGTH BOLTS:	ASTM A325SC OR (A325N)
STRUCTURAL WF SHAPES:	ASTM A572-GR50
TUBE STEEL & PIPE COLUMNS:	ASTM A500, GRADE B
WELDING ELECTRODES:	E70XX
W - SHAPES:	ASTM A992, GRADE 50
U-BOLTS:	ASTM A36

**BTS CABINET DETAIL**

NO SCALE

4

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PLANS PREPARED BY:



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SITE NAME:  
**COX COMMUNICATIONS TOWER**

SITE CASCADE:  
**CT60XC956**

SITE ADDRESS:  
 164 COUNTY ROAD REAR  
 WOLCOTT, CT 06716

SHEET DESCRIPTION:  
**EQUIPMENT & MOUNTING DETAILS**

SHEET NUMBER:  
**A-5**

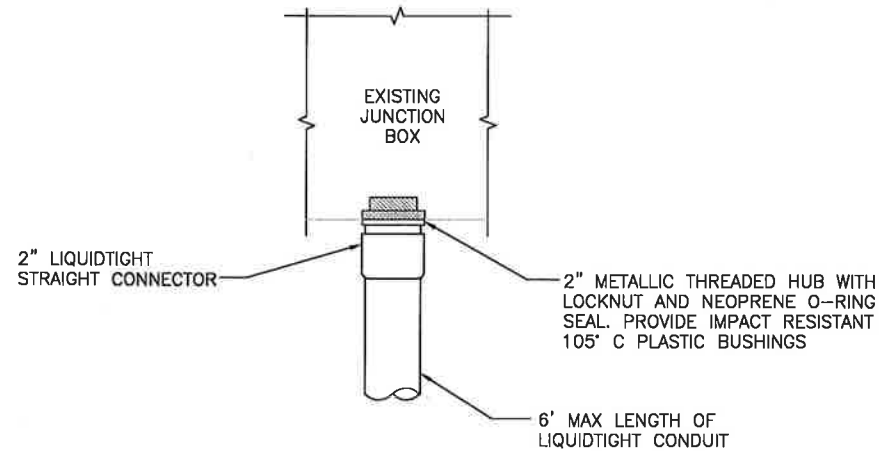
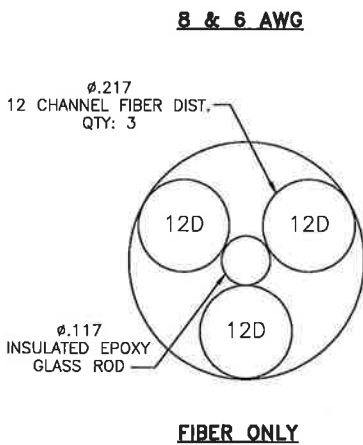
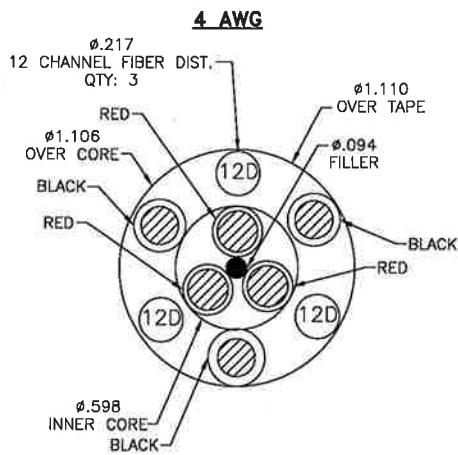
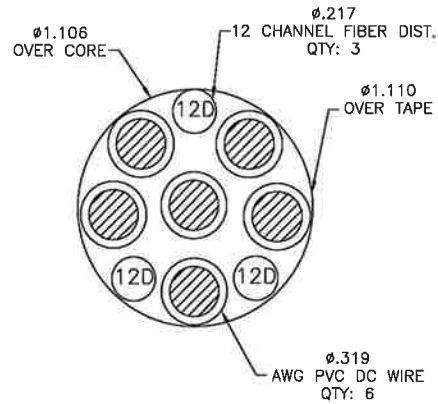
**RFS HYBRIFLEX RISER CABLE SCHEDULE**

Fiber Only (Existing DC Power)	Hybrid cable MN: HB058-M12-050F 12x multi-mode fiber pairs, Top: Outdoor protected connectors, Bottom: LC Connectors, 5/8 cable, 50 ft	50 ft
	MN: HB058-M12-075F	75 ft
	MN: HB058-M12-100F	100 ft
	MN: HB058-M12-125F	125 ft
	MN: HB058-M12-150F	150 ft
	MN: HB058-M12-175F	175 ft
	MN: HB058-M12-200F	200 ft
8 AWG Power	Hybrid cable MN: HB114-08U3M12-050F 3x 8 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 50 ft	50 ft
	MN: HB114-08U3M12-075F	75 ft
	MN: HB114-08U3M12-100F	100 ft
	MN: HB114-08U3M12-125F	125 ft
	MN: HB114-08U3M12-150F	150 ft
	MN: HB114-08U3M12-175F	175 ft
	MN: HB114-08U3M12-200F	200 ft
6 AWG Power	Hybrid cable MN: HB114-13U3M12-225F 3x 6 AWG power pair, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 225 ft	225 ft
	MN: HB114-13U3M12-250F	250 ft
	MN: HB114-13U3M12-275F	275 ft
4 AWG Power	Hybrid cable MN: HB114-21U3M12-325F 3x 4 AWG power pair, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 325 ft	325 ft
	MN: HB114-21U3M12-350F	350 ft
	MN: HB114-21U3M12-375F	375 ft

**RFS HYBRIFLEX JUMPER CABLE SCHEDULE**

Fiber Only	Hybrid Jumper cable MN: HBF012-M3-5F1 5 ft, 3x multi-mode fiber pairs, Outdoor & LC connectors, 1/2 cable	5 ft
	MN: HBF012-M3-10F1	10 ft
	MN: HBF012-M3-15F1	15 ft
	MN: HBF012-M3-20F1	20 ft
	MN: HBF012-M3-25F1	25 ft
	MN: HBF012-M3-30F1	30 ft
8 AWG Power	Hybrid Jumper cable MN: HBF058-08U1M3-5F1 5 ft, 1x 8 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 5/8 cable	5 ft
	MN: HBF058-08U1M3-10F1	10 ft
	MN: HBF058-08U1M3-15F1	15 ft
	MN: HBF058-08U1M3-20F1	20 ft
	MN: HBF058-08U1M3-25F1	25 ft
	MN: HBF058-08U1M3-30F1	30 ft
6 AWG Power	Hybrid Jumper cable MN: HBF058-13U1M3-5F1 5 ft, 1x 6 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 5/8 cable	5 ft
	MN: HBF058-13U1M3-10F1	10 ft
	MN: HBF058-13U1M3-15F1	15 ft
	MN: HBF058-13U1M3-20F1	20 ft
	MN: HBF058-13U1M3-25F1	25 ft
	MN: HBF058-13U1M3-30F1	30 ft
4 AWG Power	Hybrid Jumper cable MN: HBF078-21U1M3-5F1 5 ft, 1x 4 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 7/8 cable	5 ft
	MN: HBF078-21U1M3-10F1	10 ft
	MN: HBF078-21U1M3-15F1	15 ft
	MN: HBF078-21U1M3-20F1	20 ft
	MN: HBF078-21U1M3-25F1	25 ft
	MN: HBF078-21U1M3-30F1	30 ft

**NOTE:**  
SPRINT CM TO CONFIRM HYBRID OR FIBER RISER CABLE AND HYBRID OR FIBER JUMPER CABLE MODEL NUMBERS IF HYBRID CABLES ARE REQUIRED BEFORE PREPARING BOM.



**FIBER JUNCTION BOX PENETRATION**

NO SCALE

2

**2.5 CABLE CROSS SECTION DATA**

NO SCALE

1

NO SCALE

3

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Overland Park, Kansas 66251

PLANS PREPARED BY:

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ISSUED FOR PERMIT	11/10/17	ASW	0

SITE NAME:  
**COX COMMUNICATIONS TOWER**

SITE CASCADE:  
**CT60XC956**

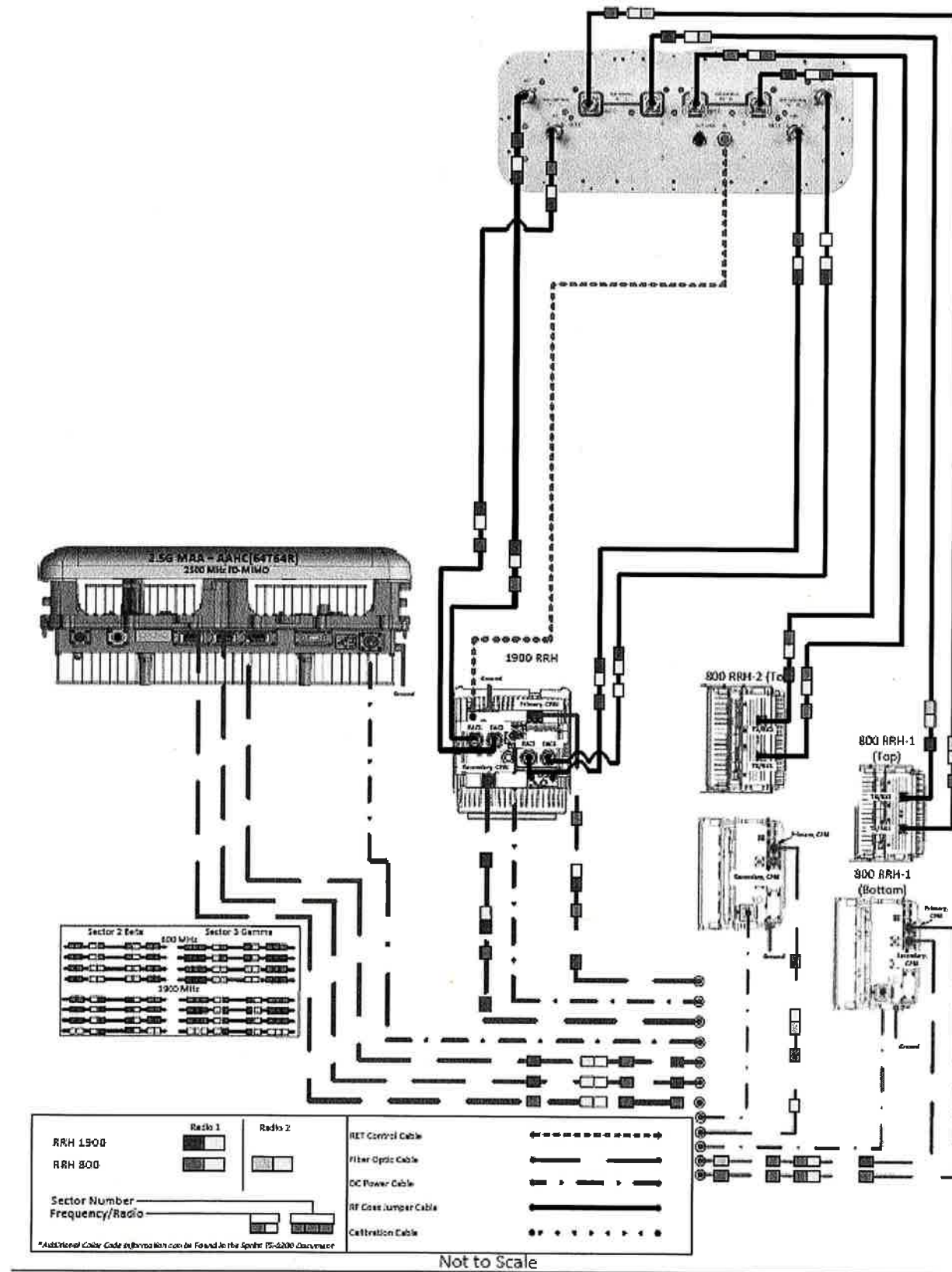
SITE ADDRESS:  
164 COUNTY ROAD REAR  
WOLCOTT, CT 06716

SHEET DESCRIPTION:  
**CIVIL DETAILS**

SHEET NUMBER:  
**A-6**



ALU 21-MIMO NNVV-65B-R4 wo Filters



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**Sprint**

6580 Sprint Parkway  
Overland Park, Kansas 66251

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**COX COMMUNICATIONS TOWER**

SITE CASCADE:

**CT60XC956**

SITE ADDRESS:

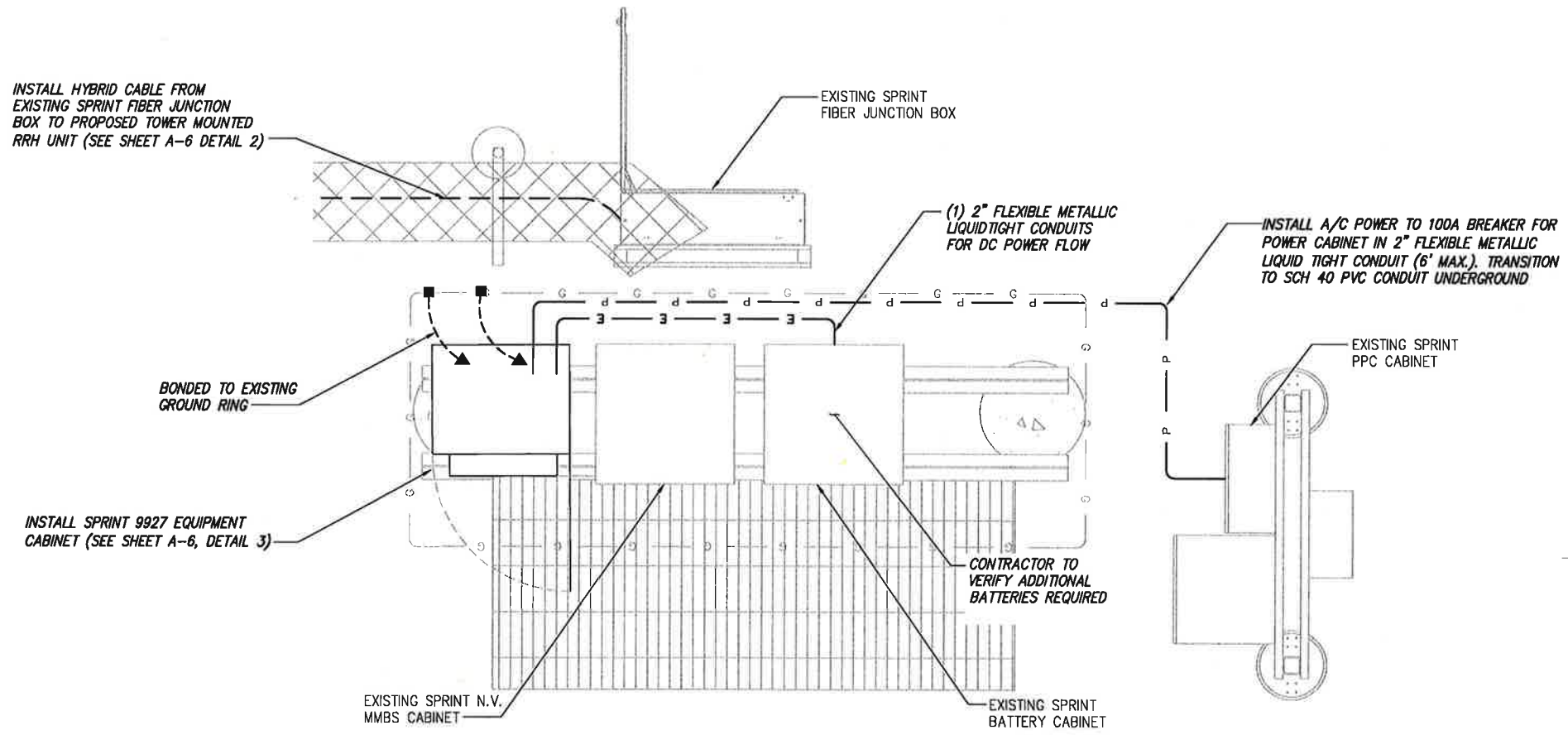
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SHEET DESCRIPTION:

**PLUMBING DIAGRAM**

SHEET NUMBER:

**A-7**

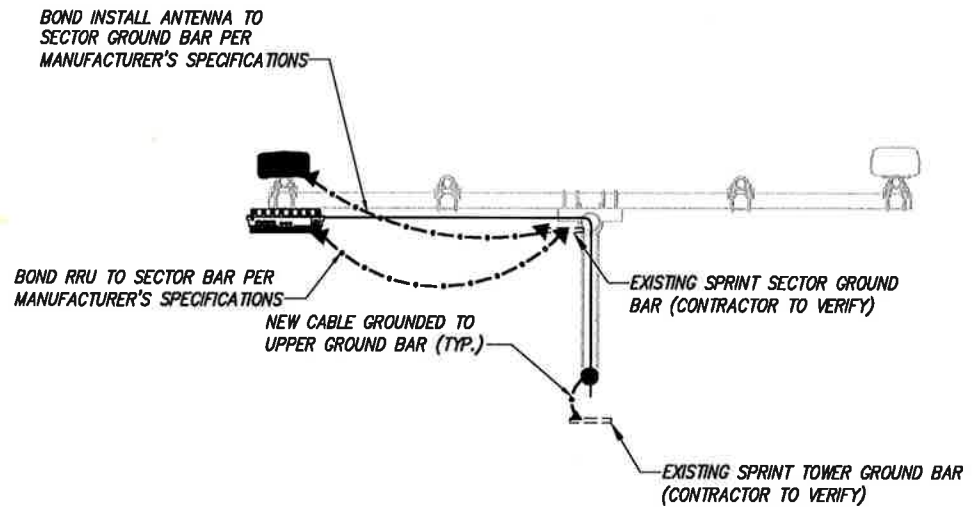


**NOTE:**  
 CONTRACTOR IS TO ENSURE THE  
 INSTALLATION INSTRUCTIONS FOR  
 EACH CABINET ARE FOLLOWED  
 AND THAT THE MANUFACTURER'S  
 REQUIREMENTS ARE MET.

- LEGEND:**
- G — EXISTING GROUND RING
  - CADWELD CONNECTION (EXOTHERMIC WELD)
  - ▲ MECHANICAL CONNECTION
  - ⊗ GROUND ROD
  - CABLE GROUND KIT

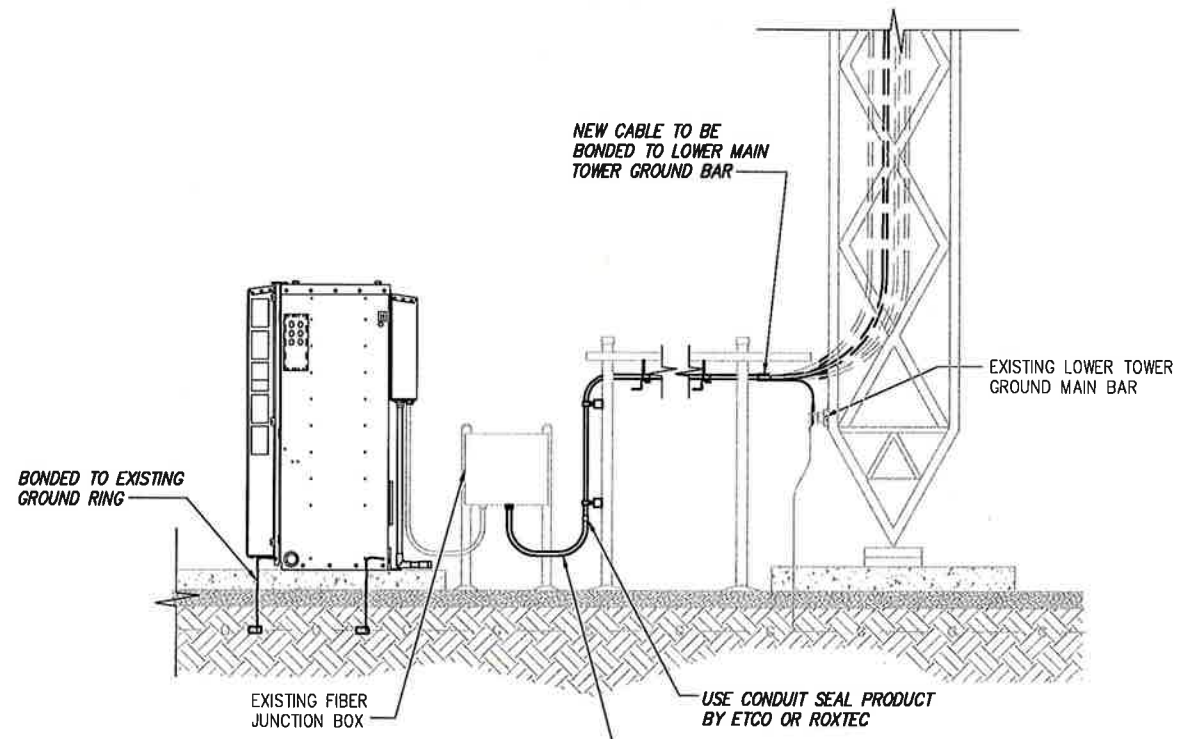
**ELECTRICAL AND GROUNDING PLAN**

NO SCALE 1



**TYPICAL ANTENNA GROUNDING PLAN**

NO SCALE 2



**NOTE:**  
 DEPICTION IS FOR CONCEPTUAL  
 PURPOSES ONLY. CONTRACTOR IS TO  
 FIELD VERIFY PRIOR TO CONSTRUCTION

**TYPICAL EQUIPMENT GROUNDING PLAN (ELEVATION)**

NO SCALE 3

PLANS PREPARED FOR:

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PLANS PREPARED BY:

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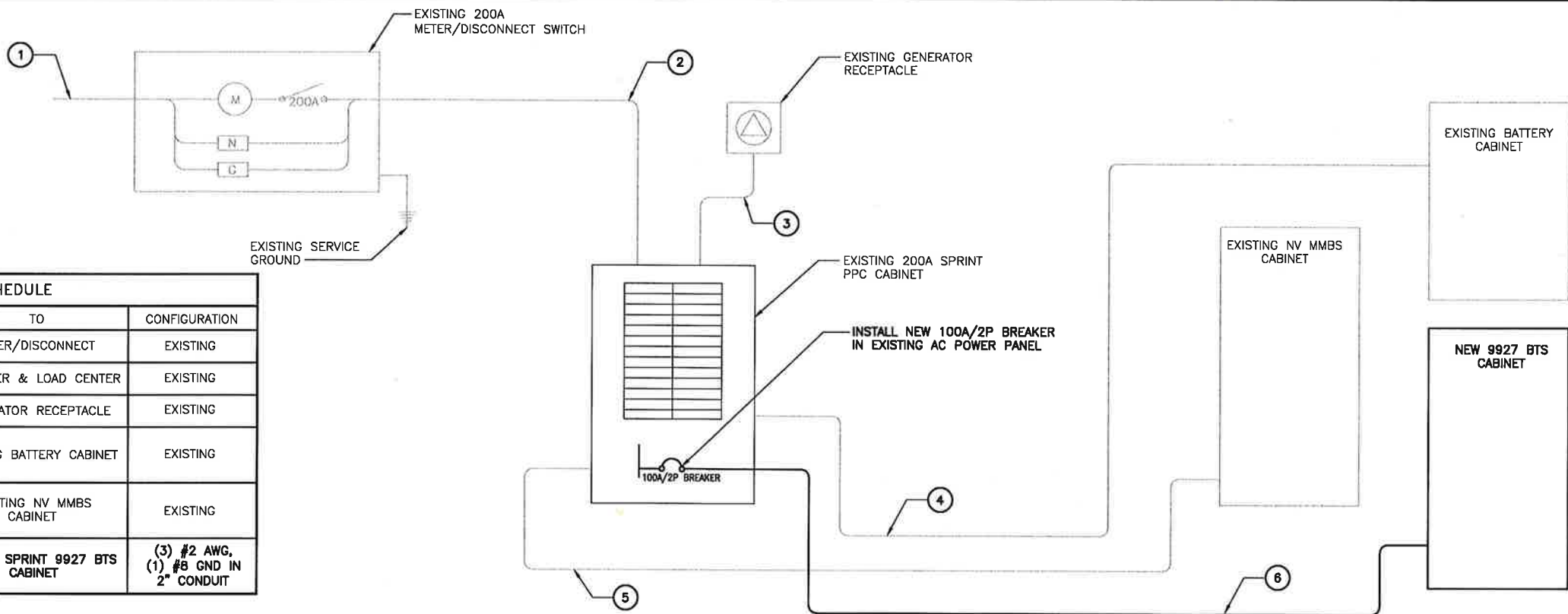
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SHEET DESCRIPTION:  
**ELECTRICAL & GROUNDING PLAN**

SHEET NUMBER:  
**E-1**



**NOTES**  
GC SHALL REFERENCE ALL SPECS FOR "CONNECTING THE POWER SUPPLY" OF THE NEW INSTALLATION DOCUMENTS, FOR ALL CONNECTION SPECIFICATIONS.



CIRCUIT SCHEDULE			
NO	FROM	TO	CONFIGURATION
①	UTILITY SOURCE	METER/DISCONNECT	EXISTING
②	METER/DISCONNECT	TRANSFER & LOAD CENTER	EXISTING
③	TRANSFER & LOAD CENTER	GENERATOR RECEPTACLE	EXISTING
④	TRANSFER & LOAD CENTER	EXISTING BATTERY CABINET	EXISTING
⑤	TRANSFER & LOAD CENTER	EXISTING NV MMBS CABINET	EXISTING
⑥	TRANSFER & LOAD CENTER	INSTALL SPRINT 9927 BTS CABINET	(3) #2 AWG, (1) #8 GND IN 2" CONDUIT

ELECTRICAL ONE-LINE DIAGRAM

NO SCALE 1

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6580 Sprint Parkway  
Overland Park, Kansas 66251

PLANS PREPARED BY:  
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Albany, NY 12205  
Office # (518) 690-0790  
JOB NUMBER 528-102

**Cherundolo Consulting**

ENGINEERING LICENSE:  
  
JOHN S. STEVEN  
PROFESSIONAL ENGINEER  
No. 24706  
JUN 24 2018

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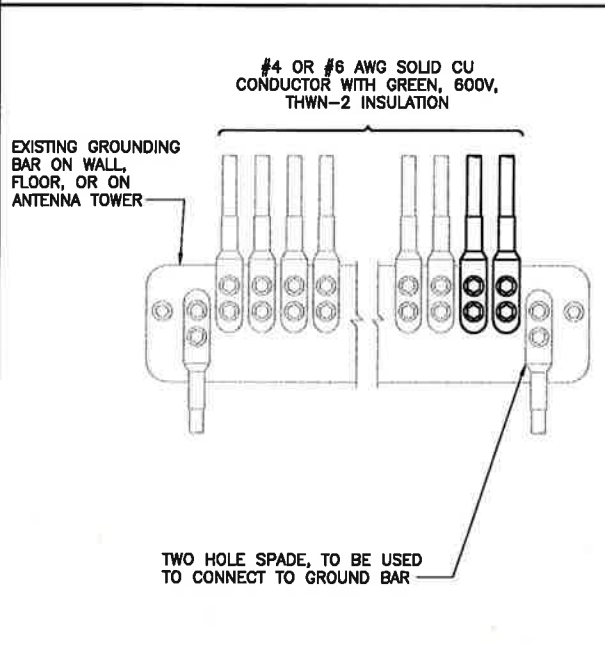
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SITE CASCADE:  
**CT60XC956**

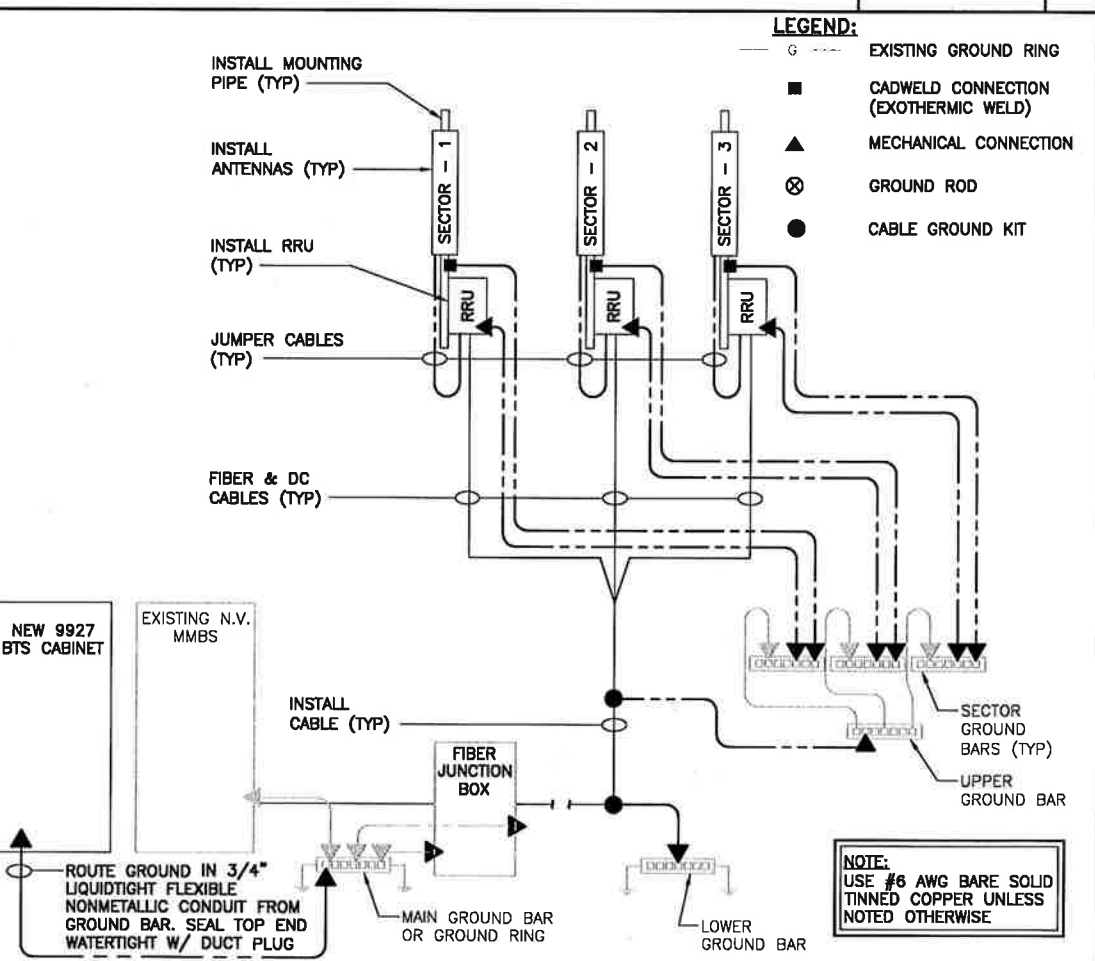
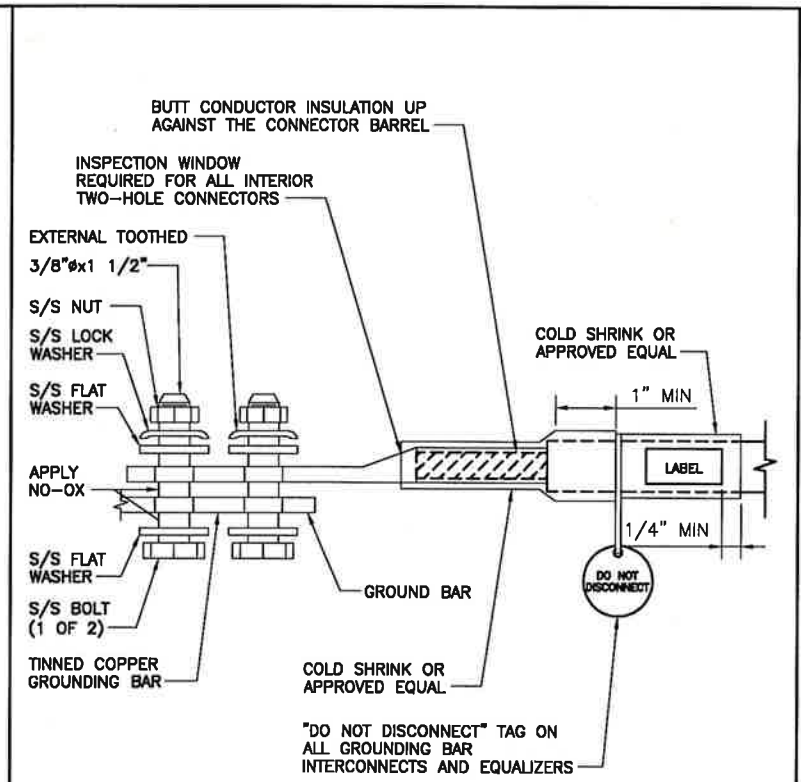
SITE ADDRESS:  
164 COUNTY ROAD REAR  
WOLCOTT, CT 06716

SHEET DESCRIPTION:  
**ELECTRICAL & GROUNDING DETAILS**

SHEET NUMBER:  
**E-2**



**NOTES**  
1. APPLY NO-OX TO LUG AND BAR CONTACT SURFACE. DO NOT COAT INLINE LUG.  
2. IF STOLEN GROUND BARS ARE ENCOUNTERED, CONTACT SPRINT CM FOR REPLACEMENT THREADED ROD KIT.



INSTALLATION OF GROUNDING CONDUCTOR TO GROUNDING BAR

NO SCALE 2

TWO HOLE LUG

NO SCALE 3

NO SCALE 4



## Structural Analysis Report

**Structure** : 347 foot Guyed Tower  
**Insite Site Name** : Wolcott  
**Insite Site Number** : CT900  
**Proposed Carrier** : Sprint  
**Carrier Site Name** : Cox Communications Tower  
**Carrier Site Number** : CT60XC956  
**Site Location** : 164 County Road Rear  
Wolcott, CT 06716  
41.5762, -72.9561  
**Date** : June 20, 2018  
**Max Member Stress Level** : 100%  
**Result** : PASS



06/20/2018

Prepared by:  
Bennett & Pless, Inc.  
B&P Job No.: 18313.020



Atlanta | Boca Raton | Charlotte | Chattanooga

750 Park of Commerce Drive, Suite 200, Boca Raton, FL 33487 | T: 561 282 2676 F: 561 989 0277

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**Table of Contents**

**Introduction .....1**

**Existing Structural Information .....1**

**Final Proposed Equipment Loading for Sprint .....1**

**Design Criteria .....2**

**Analysis Results .....2**

**Assumptions .....2**

**Conclusions .....3**

**Standard Conditions .....4**

**Disclaimer of Warranties .....4**

**Calculations..... Attached**

**Collocation Application ..... Attached**

## Introduction

We have completed our structural analysis of the proposed equipment installation on the foregoing tower to determine its ability to support the new loads proposed by Sprint. The objective of the analysis was to determine if the tower meets the current structural codes and standards with the proposed equipment installation.

## Existing Structural Information

The following documents for the existing structure were made available for our structural analysis.

<b>Tower Information</b>	Structural Components, LLC Post Mod SA Job No. 140257 dated May 6, 2014 Tectonic Modification Dwgs Project No. 2850.CT956 dated July 25, 2006
<b>Foundation Information</b>	Tectonic Modification Dwgs Project No. 2850.CT956 dated July 25, 2006
<b>Geotechnical Information</b>	Geotechnical information was not available at the time of analysis.
<b>Existing Equipment Information</b>	Structural Components, LLC Post Mod SA Job No. 140257 dated May 6, 2014 Sprint Colocation Application dated May 15, 2018 LoJack Colocation Application dated June 1, 2018
<b>Tower Reinforcement Information</b>	Tower has been previously reinforced. Tectonic Modification Dwgs Project No. 2850.CT956 dated July 25, 2006

## Final Proposed Equipment Loading for Sprint

The following proposed loading was obtained from the Insite Collocation Application:

Antenna/Equipment				Coax		
Mount	RAD	Qty.	Antenna	Type	Qty.	Size/Type
201.0	-	3	12' Sector Mount	Mount	3 3 1	1 1/4" Hybrid <b>1 1/4" Hybrid</b> 1/2" Fiber
	201.0	<b>3</b>	<b>CommScope NNVV-65B-R4</b>	<b>Panel</b>		
		<b>3</b>	<b>Nokia AAHC</b>	<b>Panel</b>		
		<b>3</b>	<b>ALU 1900 MHz RRH</b>	<b>RRH</b>		
		<b>6</b>	<b>ALU 800 2x50W</b>	<b>RRH</b>		
		3	ALU Notch Filter (800MHz)*	Filter		
		1	PCTEL GPS-TMG-HR-26NCM	GPS		

Note: All Equipment shown in bold is proposed.

\*Note: Equipment is reserved.



## Design Criteria

The tower was analyzed using tnxTower (Version 8.0.1.0) tower analysis software using the following design criteria.

<b>State/County</b>	Connecticut / Haven
<b>State Building Code</b>	2012 IBC
<b>TIA/EIA Standard Code</b>	TIA-222-G
<b>Basic Wind Speed</b>	121 MPH ( $V_{ult}$ )/94 MPH ( $V_{asd}$ )
<b>Basic Wind Speed w/ Ice</b>	50 MPH/ 0.75" Ice
<b>Steel Grade</b>	50 ksi legs, 36 ksi all others, A325X bolts
<b>Exposure Category</b>	C
<b>Topographic Category (height)</b>	1 (0.0 ft)
<b>Importance Factor</b>	1.0

## Analysis Results

Based on the foregoing information, our structural analysis determined that **the existing tower is structurally capable of supporting the proposed equipment loads without further modification.** The existing tower base and the anchor foundations have also been evaluated. The tower base and the anchor foundation reactions resulting from the proposed installation are less than the modification design reactions and as such the existing tower base and the anchor foundations are considered to be structurally capable of supporting the proposed equipment loads.

## Assumptions

The below assumptions are true, complete and accurate.

1. The existing tower has been maintained to manufacturer's specifications and is in good condition.
2. Foundations are considered to have been properly designed for the original design loads.
3. All member connections are considered to have been designed to meet the load carrying capacity of the connected member.
4. Antenna mount loads have been estimated based on generally accepted industry standards.
5. The mounts for the proposed antennas have been analyzed and designed by others.
6. See additional assumptions contained in the report attached.
7. Tower is within acceptable engineering tolerance at 105%.
8. Foundations are within acceptable engineering tolerance at 110%.

## Conclusions

The existing tower and foundation described above **does have sufficient capacity** to support the proposed loading based on the governing Building Code. The existing tower base and anchor foundations also acceptable.

We appreciate the opportunity of providing our continuing professional services to you. If you have any questions or need further assistance, please call us anytime at 561-288-1187.

Sincerely,

Analysis by:

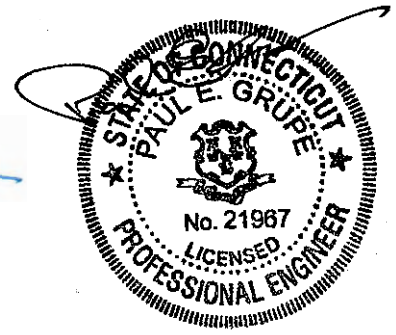


Chunhui Song, P.E.  
Design Engineer

Reviewed by:



Paul Grupe, P.E.  
Vice President



06/20/2018



## **Standard Conditions**

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but not necessarily limited, to:

- Information supplied by the client regarding the structure itself, the antenna and transmission line loading on the structure and its components, or relevant information.
- Information from drawings in possession of Bennett & Pless Inc., or generated by field inspections or measurements of the structure.

It is the responsibility of the client to ensure that the information provided to Bennett & Pless Inc. and used in the performance of our engineering services is correct and complete. In the absence of information contrary, we consider that all structures were constructed in accordance with the drawings and specifications and are in an uncorroded condition and have not deteriorated; and we, therefore consider that their capacity has not significantly changed from the original design condition.

All services will be performed to the codes and standards specified by the client, and we do not imply to meet any other code and standard requirements unless explicitly agreed to in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes and standards, the client shall specify the exact requirements. In the absence of information to the contrary, all work will be performed in accordance with the revision of ANSI/TIA/EIA-222 requested.

All services are performed, results obtained and recommendations made in accordance with the generally accepted engineering principles and practices. Bennett & Pless Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

## **Disclaimer of Warranties**

Bennett & Pless Inc. makes no warranties, expressed or implied, in connection with this report, and disclaims any liability arising from the ability of the existing structure to support the design loads for which it was originally designed. Bennett & Pless Inc. will not be responsible whatsoever for or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of Bennett & Pless Inc. pursuant to this report will be limited to the total fee received for preparation of this report.

# Attachment 1: Calculations

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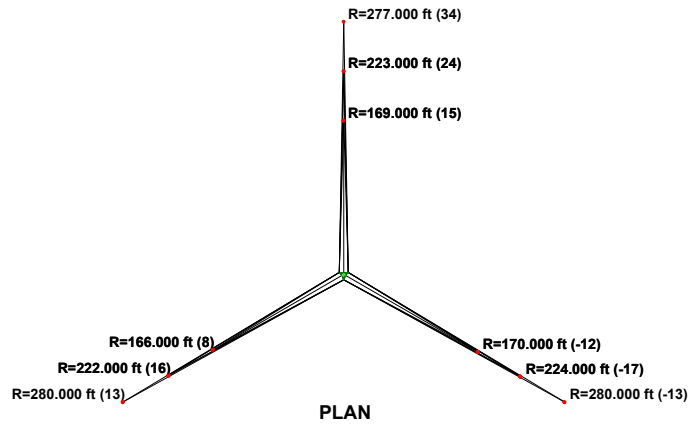
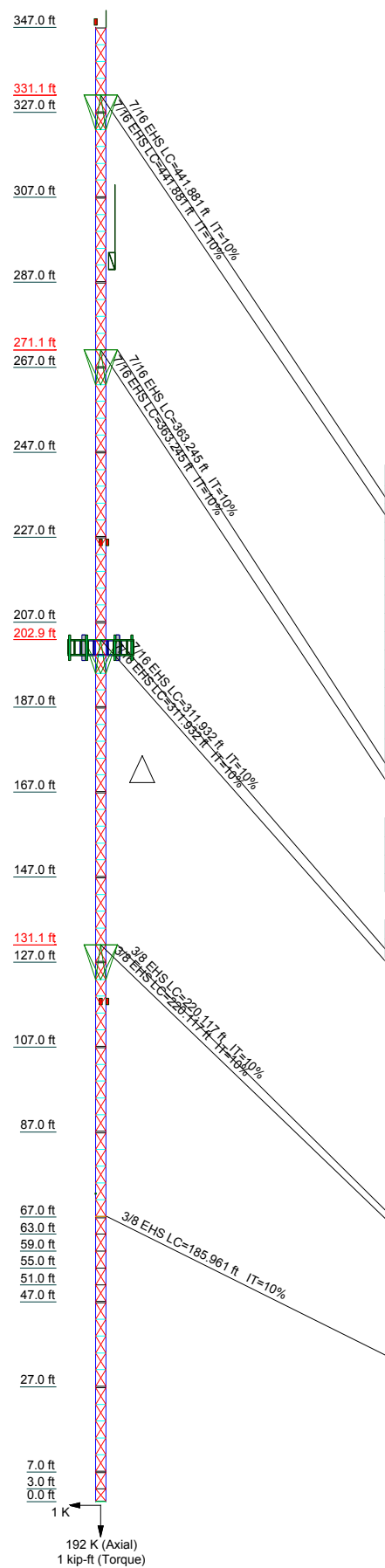
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Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11	T12	T13	T14	T15	T16	T17	T18	T19	T20	T21	T22	T23
Legs	P2.5 STD w/ SP HSS 3.5x.3																						
Leg Grade	A572-50																						
Diagonals	SR 3/4																						
Diagonal Grade	A36																						
Top Girts	L2x1 1/2x3/16																						
Bottom Girts	L2x1 1/2x3/16																						
Horizontals	L2x1 1/2x3/16																						
Top Guy Pull-Offs	N.A.																						
Face Width (ft)	3																						
# Panels @ (ft)	70 @ 3.93333																						
Weight (K)	14.3	2.02	0.9	0.9	0.2	0.2	0.2	0.2	0.1	0.1	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	1.4



**DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
5' Lightning Rod	347	(2) 800MHz 2X50W RRH W/FILTER (Sprint)	201
Beacon (.035k 2.250CAAA)	347	Alcatel Lucent 1900 MHz (Sprint)	201
Telewave ANT150F6-L (Lojack)	300	Alcatel Lucent 1900 MHz (Sprint)	201
4' Stand off (Lojack)	300	Alcatel Lucent 1900 MHz (Sprint)	201
Beacon (10lbs 0.5CaAa)	225	Alcatel Lucent 1900 MHz (Sprint)	201
Beacon (10lbs 0.5CaAa)	225	800 EXTERNAL NOTCH FILTER (Sprint)	201
Commscope NNVV-65B-R4 (Sprint)	201	800 EXTERNAL NOTCH FILTER (Sprint)	201
Commscope NNVV-65B-R4 (Sprint)	201	800 EXTERNAL NOTCH FILTER (Sprint)	201
Commscope NNVV-65B-R4 (Sprint)	201	800 EXTERNAL NOTCH FILTER (Sprint)	201
Nokia AAHC (Sprint)	201	SM 407-3 (Sprint)	201
Nokia AAHC (Sprint)	201	Beacon (10lbs 0.5CaAa)	117
Nokia AAHC (Sprint)	201	Beacon (10lbs 0.5CaAa)	117
(2) 800MHz 2X50W RRH W/FILTER (Sprint)	201	PCTEL GPS-TMG-HR-26NCM (.0006, .277CAAA) (Sprint)	70
(2) 800MHz 2X50W RRH W/FILTER (Sprint)	201		

**SYMBOL LIST**

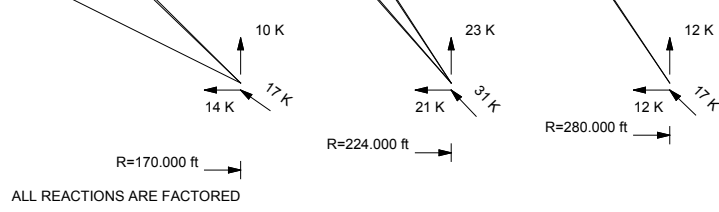
MARK	SIZE	MARK	SIZE
A	N.A.	D	1 @ 3.83333
B	L2x1 1/2x3/16	E	1 @ 2.83333
C	1 @ 3.86333		

**MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A36	36 ksi	58 ksi

**TOWER DESIGN NOTES**

1. Tower is located in New Haven County, Connecticut.
2. Tower designed for Exposure C to the TIA-222-G Standard.
3. Tower designed for a 94 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.000 ft
8. TOWER RATING: 100%



<p><b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Experience Structural Expertise Phone: 678.990.8700 FAX: 678.990.8701</p>	<p>Job: <b>CT900 Wolcott</b></p>
	<p>Project: <b>Guyed Tower Structural Analysis</b></p>
	<p>Client: <b>Insite</b>      Drawn by: <b>Chunhui Song</b>      App'd:</p>
	<p>Code: <b>TIA-222-G</b>      Date: <b>06/19/18</b>      Scale: <b>NTS</b></p>
	<p>Path: _____      Dwg No. <b>E-1</b></p>

<p><b>tnxTower</b></p> <p><b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701</p>	<p><b>Job</b></p> <p>CT900 Wolcott</p>	<p><b>Page</b></p> <p>1 of 62</p>
	<p><b>Project</b></p> <p>Guyed Tower Structural Analysis</p>	<p><b>Date</b></p> <p>17:19:08 06/19/18</p>
	<p><b>Client</b></p> <p>Insite</p>	<p><b>Designed by</b></p> <p>Chunhui Song</p>

## Tower Input Data

The main tower is a 3x guyed tower with an overall height of 347.000 ft above the ground line.

The base of the tower is set at an elevation of 0.000 ft above the ground line.

The face width of the tower is 3.000 ft at the top and 3.000 ft at the base.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in New Haven County, Connecticut.

Basic wind speed of 94 mph.

Structure Class II.

Exposure Category C.

Topographic Category 1.

Crest Height 0.000 ft.

Nominal ice thickness of 0.7500 in.

Ice thickness is considered to increase with height.

Ice density of 56.000 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50.000 °F.

Deflections calculated using a wind speed of 60 mph.

Tension only take-up is 0.0313 in.

Pressures are calculated at each section.

Safety factor used in guy design is 1.

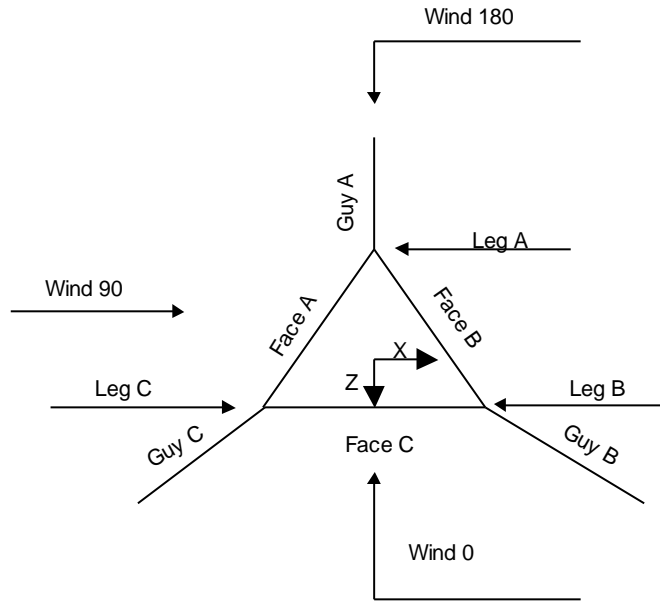
Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

- |  |  |   |
|--|--|---|
| <ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>√ Include Bolts In Member Capacity</li> <li>√ Leg Bolts Are At Top Of Section</li> <li>Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>√ SR Members Have Cut Ends</li> <li>SR Members Are Concentric</li> </ul> | <ul style="list-style-type: none"> <li>√ Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>√ Use Clear Spans For KL/r</li> <li>√ Retension Guys To Initial Tension</li> <li>√ Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <li>√ Autocalc Torque Arm Areas</li> <li>Add IBC .6D+W Combination</li> <li>√ Sort Capacity Reports By Component</li> <li>Triangulate Diamond Inner Bracing</li> <li>Treat Feed Line Bundles As Cylinder</li> </ul> | <ul style="list-style-type: none"> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>√ Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feed Line Torque</li> <li>Include Angle Block Shear Check</li> <li>Use TIA-222-G Bracing Resist. Exemption</li> <li>Use TIA-222-G Tension Splice Exemption</li> <li style="text-align: center;">Poles</li> <li>Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> <li>Pole Without Linear Attachments</li> <li>Pole With Shroud Or No Appurtenances</li> <li>Outside and Inside Corner Radii Are Known</li> </ul> |
|--|--|---|

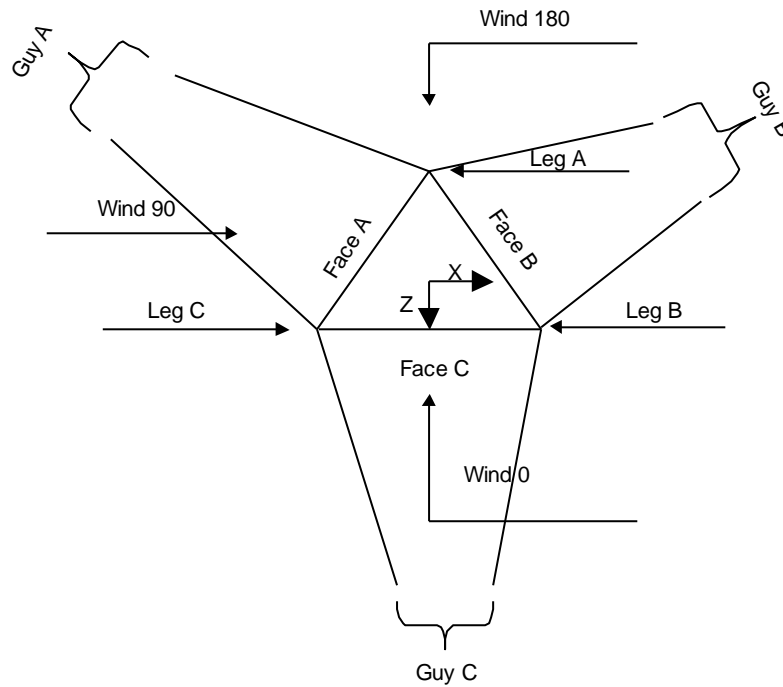
<b>Job</b>	CT900 Wolcott	<b>Page</b>	2 of 62
<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song



**Corner & Starmount Guyed Tower**



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	<b>Project</b> Guyed Tower Structural Analysis	<b>Date</b> 17:19:08 06/19/18
	<b>Client</b> Insite	<b>Designed by</b> Chunhui Song



**Face Guyed**

## Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T1	347.000-327.000			3.000	1	20.000
T2	327.000-307.000			3.000	1	20.000
T3	307.000-287.000			3.000	1	20.000
T4	287.000-267.000			3.000	1	20.000
T5	267.000-247.000			3.000	1	20.000
T6	247.000-227.000			3.000	1	20.000
T7	227.000-207.000			3.000	1	20.000
T8	207.000-187.000			3.000	1	20.000
T9	187.000-167.000			3.000	1	20.000
T10	167.000-147.000			3.000	1	20.000
T11	147.000-127.000			3.000	1	20.000
T12	127.000-107.000			3.000	1	20.000
T13	107.000-87.000			3.000	1	20.000
T14	87.000-67.000			3.000	1	20.000
T15	67.000-62.970			3.000	1	4.030
T16	62.970-58.990			3.000	1	3.980

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	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T17	58.990-55.010			3.000	1	3.980
T18	55.010-51.030			3.000	1	3.980
T19	51.030-47.000			3.000	1	4.030
T20	47.000-27.000			3.000	1	20.000
T21	27.000-7.000			3.000	1	20.000
T22	7.000-3.000			3.000	1	4.000
T23	3.000-0.000			3.000	1	3.000

### Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	347.000-327.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T2	327.000-307.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T3	307.000-287.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T4	287.000-267.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T5	267.000-247.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T6	247.000-227.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T7	227.000-207.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T8	207.000-187.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T9	187.000-167.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T10	167.000-147.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T11	147.000-127.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T12	127.000-107.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T13	107.000-87.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T14	87.000-67.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T15	67.000-62.970	3.863	TX Brace	No	Yes	2.0000	0.0000
T16	62.970-58.990	3.980	TX Brace	No	Yes	0.0000	0.0000
T17	58.990-55.010	3.980	TX Brace	No	Yes	0.0000	0.0000
T18	55.010-51.030	3.980	TX Brace	No	Yes	0.0000	0.0000
T19	51.030-47.000	3.863	TX Brace	No	Yes	0.0000	2.0000
T20	47.000-27.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T21	27.000-7.000	3.933	TX Brace	No	Yes	2.0000	2.0000
T22	7.000-3.000	3.833	TX Brace	No	Yes	2.0000	0.0000
T23	3.000-0.000	2.833	TX Brace	No	Yes	0.0000	2.0000

### Tower Section Geometry (cont'd)

Tower Elevation	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
ft						
T1 347.000-327.000	Pipe	P2.5 STD	A572-50 (50 ksi)	Solid Round	7/8	A36 (36 ksi)
T2 327.000-307.000	Pipe	P2.5 STD	A572-50 (50 ksi)	Solid Round	5/8	A36 (36 ksi)
T3 307.000-287.000	Pipe	P2.5 STD	A572-50 (50 ksi)	Solid Round	5/8	A36 (36 ksi)
T4 287.000-267.000	Pipe	P2.5 STD	A572-50 (50 ksi)	Solid Round	7/8	A36 (36 ksi)
T5	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36

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	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
267.000-247.000			(50 ksi)			(36 ksi)
T6	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36
247.000-227.000			(50 ksi)			(36 ksi)
T7	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36
227.000-207.000			(50 ksi)			(36 ksi)
T8	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36
207.000-187.000			(50 ksi)			(36 ksi)
T9	Pipe	P2.5 STD	A572-50	Solid Round	3/4	A36
187.000-167.000			(50 ksi)			(36 ksi)
T10	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36
167.000-147.000			(50 ksi)			(36 ksi)
T11	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36
147.000-127.000			(50 ksi)			(36 ksi)
T12	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36
127.000-107.000			(50 ksi)			(36 ksi)
T13	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36
107.000-87.000			(50 ksi)			(36 ksi)
T14	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36
87.000-67.000			(50 ksi)			(36 ksi)
T15	Pipe	P2.5 STD	A572-50	Solid Round	5/8	A36
67.000-62.970			(50 ksi)			(36 ksi)
T16	Arbitrary Shape	P2.5 STD w/ SP HSS 3.5x.3	A572-50	Solid Round	5/8	A36
62.970-58.990			(50 ksi)			(36 ksi)
T17	Arbitrary Shape	P2.5 STD w/ SP HSS 3.5x.3	A572-50	Solid Round	5/8	A36
58.990-55.010			(50 ksi)			(36 ksi)
T18	Arbitrary Shape	P2.5 STD w/ SP HSS 3.5x.3	A572-50	Solid Round	5/8	A36
55.010-51.030			(50 ksi)			(36 ksi)
T19	Arbitrary Shape	P2.5 STD w/ SP HSS 3.5x.3	A572-50	Solid Round	5/8	A36
51.030-47.000			(50 ksi)			(36 ksi)
T20	Arbitrary Shape	P2.5 STD w/ SP HSS 3.5x.3	A572-50	Solid Round	5/8	A36
47.000-27.000			(50 ksi)			(36 ksi)
T21 27.000-7.000	Arbitrary Shape	P2.5 STD w/ SP HSS 3.5x.3	A572-50	Solid Round	5/8	A36
			(50 ksi)			(36 ksi)
T22 7.000-3.000	Arbitrary Shape	P2.5 STD w/ SP HSS 3.5x.3	A572-50	Solid Round	5/8	A36
			(50 ksi)			(36 ksi)
T23 3.000-0.000	Arbitrary Shape	P2.5 STD w/ SP HSS 3.5x.3	A572-50	Solid Round	5/8	A36
			(50 ksi)			(36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1	Single Angle	L2x2x1/4	A36	Single Angle	L2x2x1/4	A36
347.000-327.000			(36 ksi)			(36 ksi)
T2	Single Angle	L2x1 1/2x3/16	A36	Single Angle	L2x1 1/2x3/16	A36
327.000-307.000			(36 ksi)			(36 ksi)
T3	Single Angle	L2x1 1/2x3/16	A36	Single Angle	L2x1 1/2x3/16	A36
307.000-287.000			(36 ksi)			(36 ksi)
T4	Single Angle	L2x2x1/4	A36	Single Angle	L2x2x1/4	A36
287.000-267.000			(36 ksi)			(36 ksi)
T5	Single Angle	L2x1 1/2x3/16	A36	Single Angle	L2x1 1/2x3/16	A36
267.000-247.000			(36 ksi)			(36 ksi)
T6	Single Angle	L2x1 1/2x3/16	A36	Single Angle	L2x1 1/2x3/16	A36
247.000-227.000			(36 ksi)			(36 ksi)
T7	Single Angle	L2x1 1/2x3/16	A36	Single Angle	L2x1 1/2x3/16	A36



<p style="text-align: center;"><b>tnxTower</b></p> <p style="text-align: center;"><b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701</p>	<p style="text-align: center;"><b>Job</b></p> <p style="text-align: center;">CT900 Wolcott</p>	<p style="text-align: center;"><b>Page</b></p> <p style="text-align: center;">6 of 62</p>
	<p style="text-align: center;"><b>Project</b></p> <p style="text-align: center;">Guyed Tower Structural Analysis</p>	<p style="text-align: center;"><b>Date</b></p> <p style="text-align: center;">17:19:08 06/19/18</p>
	<p style="text-align: center;"><b>Client</b></p> <p style="text-align: center;">Insite</p>	<p style="text-align: center;"><b>Designed by</b></p> <p style="text-align: center;">Chunhui Song</p>

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
227.000-207.000 T8	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
207.000-187.000 T9	Single Angle	L2x1 1/2x1/4	(36 ksi) A36	Single Angle	L2x1 1/2x1/4	(36 ksi) A36
187.000-167.000 T10	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
167.000-147.000 T11	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
147.000-127.000 T12	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
127.000-107.000 T13	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
107.000-87.000 T14	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
87.000-67.000 T15	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
67.000-62.970 T16	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
62.970-58.990 T17	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
58.990-55.010 T18	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
55.010-51.030 T19	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
51.030-47.000 T20	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
47.000-27.000 T21	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
27.000-7.000 T22	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
7.000-3.000 T23	Single Angle	L2x1 1/2x3/16	(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36

### Tower Section Geometry (cont'd)

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
347.000-327.000 T1	None	Flat Bar		(36 ksi) A36	Single Angle	L2x2x1/4	(36 ksi) A36
327.000-307.000 T2	None	Flat Bar		(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
307.000-287.000 T3	None	Flat Bar		(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
287.000-267.000 T4	None	Flat Bar		(36 ksi) A36	Single Angle	L2x2x1/4	(36 ksi) A36
267.000-247.000 T5	None	Flat Bar		(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
247.000-227.000 T6	None	Flat Bar		(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
227.000-207.000 T7	None	Flat Bar		(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36
207.000-187.000 T8	None	Flat Bar		(36 ksi) A36	Single Angle	L2x1 1/2x3/16	(36 ksi) A36

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	<p style="text-align: center;"><b>Project</b></p> <p style="text-align: center;">Guyed Tower Structural Analysis</p>	<p style="text-align: center;"><b>Date</b></p> <p style="text-align: center;">17:19:08 06/19/18</p>
	<p style="text-align: center;"><b>Client</b></p> <p style="text-align: center;">Insite</p>	<p style="text-align: center;"><b>Designed by</b></p> <p style="text-align: center;">Chunhui Song</p>

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T9 187.000-167.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x1/4	A36 (36 ksi)
T10 167.000-147.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T11 147.000-127.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T12 127.000-107.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T13 107.000-87.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T14 87.000-67.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T15 67.000-62.970	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T16 62.970-58.990	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T17 58.990-55.010	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T18 55.010-51.030	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T19 51.030-47.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T20 47.000-27.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T21 27.000-7.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T22 7.000-3.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)
T23 3.000-0.000	None	Flat Bar		A36 (36 ksi)	Single Angle	L2x1 1/2x3/16	A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
T1 347.000-327.000	0.000	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T2 327.000-307.000	0.000	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T3 307.000-287.000	0.000	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T4 287.000-267.000	0.000	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T5 267.000-247.000	0.000	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T6 247.000-227.000	0.000	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000





<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	9 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Tower Elevation	Calc K Single Angles	Calc K Solid Rounds	K Factors <sup>1</sup>								
			Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace	
				X Y	X Y	X Y	X Y	X Y	X Y	X Y	
327.000-307.000				1	1	1	1	1	1	1	1
T3	Yes	Yes	1	1	1	1	1	1	1	1	1
307.000-287.000				1	1	1	1	1	1	1	1
T4	Yes	Yes	1	1	1	1	1	1	1	1	1
287.000-267.000				1	1	1	1	1	1	1	1
T5	Yes	Yes	1	1	1	1	1	1	1	1	1
267.000-247.000				1	1	1	1	1	1	1	1
T6	Yes	Yes	1	1	1	1	1	1	1	1	1
247.000-227.000				1	1	1	1	1	1	1	1
T7	Yes	Yes	1	1	1	1	1	1	1	1	1
227.000-207.000				1	1	1	1	1	1	1	1
T8	Yes	Yes	1	1	1	1	1	1	1	1	1
207.000-187.000				1	1	1	1	1	1	1	1
T9	Yes	Yes	1	1	1	1	1	1	1	1	1
187.000-167.000				1	1	1	1	1	1	1	1
T10	Yes	Yes	1	1	1	1	1	1	1	1	1
167.000-147.000				1	1	1	1	1	1	1	1
T11	Yes	Yes	1	1	1	1	1	1	1	1	1
147.000-127.000				1	1	1	1	1	1	1	1
T12	Yes	Yes	1	1	1	1	1	1	1	1	1
127.000-107.000				1	1	1	1	1	1	1	1
T13	Yes	Yes	1	1	1	1	1	1	1	1	1
107.000-87.000				1	1	1	1	1	1	1	1
T14	Yes	Yes	1	1	1	1	1	1	1	1	1
87.000-67.000				1	1	1	1	1	1	1	1
T15	Yes	Yes	1	1	1	1	1	1	1	1	1
67.000-62.970				1	1	1	1	1	1	1	1
T16	Yes	Yes	1	1	1	1	1	1	1	1	1
62.970-58.990				1	1	1	1	1	1	1	1
T17	Yes	Yes	1	1	1	1	1	1	1	1	1
58.990-55.010				1	1	1	1	1	1	1	1
T18	Yes	Yes	1	1	1	1	1	1	1	1	1
55.010-51.030				1	1	1	1	1	1	1	1
T19	Yes	Yes	1	1	1	1	1	1	1	1	1
51.030-47.000				1	1	1	1	1	1	1	1
T20	Yes	Yes	1	1	1	1	1	1	1	1	1
47.000-27.000				1	1	1	1	1	1	1	1
T21	Yes	Yes	1	1	1	1	1	1	1	1	1
27.000-7.000				1	1	1	1	1	1	1	1
T22	Yes	Yes	1	1	1	1	1	1	1	1	1
7.000-3.000				1	1	1	1	1	1	1	1
T23	Yes	Yes	1	1	1	1	1	1	1	1	1
3.000-0.000				1	1	1	1	1	1	1	1

<sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.







<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	12 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T12 127.000-107.000	Flange	0.6250 A325X	3	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T13 107.000-87.000	Flange	0.6250 A325X	3	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T14 87.000-67.000	Flange	0.6250 A325X	3	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T15 67.000-62.970	Flange	0.6250 A325X	3	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T16 62.970-58.990	Flange	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T17 58.990-55.010	Flange	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T18 55.010-51.030	Flange	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T19 51.030-47.000	Flange	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T20 47.000-27.000	Flange	0.6250 A325X	3	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T21 27.000-7.000	Flange	0.6250 A325X	3	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T22 7.000-3.000	Flange	0.6250 A325X	3	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T23 3.000-0.000	Flange	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0

### Guy Data

Guy Elevation ft	Guy Grade	Guy Size	Initial Tension K	%	Guy Modulus ksi	Guy Weight plf	$L_u$ ft	Anchor Radius ft	Anchor Azimuth Adj. °	Anchor Elevation ft	End Fitting Efficiency %	
331.1	EHS	A	7/16	2.080	10%	21000.000	0.399	404.000	277.000	0.0000	34.000	100%
		B	7/16	2.080	10%	21000.000	0.399	441.539	280.000	0.0000	-13.000	100%
		C	7/16	2.080	10%	21000.000	0.399	421.624	280.000	0.0000	13.000	100%
271.1	EHS	A	7/16	2.080	10%	21000.000	0.399	330.736	223.000	0.0000	24.000	100%
		B	7/16	2.080	10%	21000.000	0.399	362.952	224.000	0.0000	-17.000	100%
		C	7/16	2.080	10%	21000.000	0.399	336.093	222.000	0.0000	16.000	100%
202.9	EHS	A	7/16	2.080	10%	21000.000	0.399	283.515	223.000	0.0000	24.000	100%
		B	7/16	2.080	10%	21000.000	0.399	311.682	224.000	0.0000	-17.000	100%
		C	7/16	2.080	10%	21000.000	0.399	287.860	222.000	0.0000	16.000	100%
131.1	EHS	A	3/8	1.540	10%	21000.000	0.273	202.597	169.000	0.0000	15.000	100%
		B	3/8	1.540	10%	21000.000	0.273	219.918	170.000	0.0000	-12.000	100%
		C	3/8	1.540	10%	21000.000	0.273	204.281	166.000	0.0000	8.000	100%
67.1667	EHS	A	3/8	1.540	10%	21000.000	0.273	175.057	169.000	0.0000	15.000	100%
		B	3/8	1.540	10%	21000.000	0.273	185.794	170.000	0.0000	-12.000	100%
		C	3/8	1.540	10%	21000.000	0.273	174.442	166.000	0.0000	8.000	100%

### Guy Data(cont'd)

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	13 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Guy Elevation ft	Mount Type	Torque-Arm Spread ft	Torque-Arm Leg Angle °	Torque-Arm Style	Torque-Arm Grade	Torque-Arm Type	Torque-Arm Size
331.1	Torque Arm	9.760	56.1600	Bat Ear	A36 (36 ksi)	Equal Angle	L3x3x5/16
271.1	Torque Arm	9.760	56.1600	Bat Ear	A36 (36 ksi)	Equal Angle	L3x3x5/16
202.9	Torque Arm	9.760	56.1600	Bat Ear	A36 (36 ksi)	Equal Angle	L3x3x5/16
131.1	Torque Arm	9.760	56.1600	Bat Ear	A36 (36 ksi)	Equal Angle	L3x3x5/16
67.1667	Corner						

### Guy Data (cont'd)

Guy Elevation ft	Diagonal Grade	Diagonal Type	Upper Diagonal Size	Lower Diagonal Size	Is Strap.	Pull-Off Grade	Pull-Off Type	Pull-Off Size
331.100	A572-50 (50 ksi)	Solid Round				A572-50 (50 ksi)	Single Angle	
271.100	A572-50 (50 ksi)	Solid Round				A572-50 (50 ksi)	Single Angle	
202.900	A572-50 (50 ksi)	Solid Round				A572-50 (50 ksi)	Single Angle	
131.100	A572-50 (50 ksi)	Solid Round				A572-50 (50 ksi)	Single Angle	
67.167	A572-50 (50 ksi)	Solid Round			Yes	A36 (36 ksi)	Flat Bar	3x3/8

### Guy Data (cont'd)

Guy Elevation ft	Cable Weight A K	Cable Weight B K	Cable Weight C K	Cable Weight D K	Tower Intercept A ft	Tower Intercept B ft	Tower Intercept C ft	Tower Intercept D ft
331.1	0.161	0.176	0.168		15.238	18.122	16.564	
271.1	0.132	0.145	0.134		6.7 sec/pulse 10.259	7.4 sec/pulse 12.308	7.0 sec/pulse 10.586	
202.9	0.113	0.124	0.115		5.5 sec/pulse 7.587	6.1 sec/pulse 9.135	5.6 sec/pulse 7.816	
131.1	0.055	0.060	0.056		4.8 sec/pulse 3.605	5.2 sec/pulse 4.237	4.8 sec/pulse 3.663	
67.1667	0.048	0.051	0.048		3.3 sec/pulse 2.706	3.6 sec/pulse 3.041	3.3 sec/pulse 2.686	
					2.8 sec/pulse	3.0 sec/pulse	2.8 sec/pulse	

### Guy Data (cont'd)

Torque Arm      Pull Off      Diagonal

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	14 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Guy Elevation ft	Calc K Single Angles	Calc K Solid Rounds	K <sub>x</sub>	K <sub>y</sub>	K <sub>x</sub>	K <sub>y</sub>	K <sub>x</sub>	K <sub>y</sub>
331.1	No	No	1	1	1	1	1	1
271.1	No	No	1	1	1	1	1	1
202.9	No	No	1	1	1	1	1	1
131.1	No	No	1	1	1	1	1	1
67.1667	No	No			1	1	1	1

### Guy Data (cont'd)

Guy Elevation ft	Torque-Arm				Pull Off				Diagonal			
	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U
331.1	0.0000 A325N	0	0.0000	1	0.6250 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75
271.1	0.0000 A325N	0	0.0000	1	0.6250 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75
202.9	0.0000 A325N	0	0.0000	1	0.6250 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75
131.1	0.0000 A325N	0	0.0000	1	0.6250 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75
67.1667	0.6250 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75

### Guy Pressures

Guy Elevation ft	Guy Location	z ft	q <sub>z</sub> ksf	q <sub>z</sub> Ice ksf	Ice Thickness in
331.1	A	182.550	0.028	0.008	1.7798
	B	159.050	0.027	0.008	1.7555
	C	172.050	0.027	0.008	1.7693
271.1	A	147.550	0.026	0.007	1.7423
	B	127.050	0.026	0.007	1.7165
	C	143.550	0.026	0.007	1.7376
202.9	A	113.450	0.025	0.007	1.6972
	B	92.950	0.024	0.007	1.6637
	C	109.450	0.025	0.007	1.6911
131.1	A	73.050	0.023	0.006	1.6241
	B	59.550	0.022	0.006	1.5912
	C	69.550	0.023	0.006	1.6161
67.1667	A	41.083	0.020	0.006	1.5332
	B	27.583	0.019	0.005	1.4733
	C	37.583	0.020	0.006	1.5196

### Guy-Tensioning Information

Temperature At Time Of Tensioning

0 F      20 F      40 F      60 F      80 F      100 F      120 F



<p><b>tnxTower</b></p> <p><b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701</p>	<p><b>Job</b></p> <p>CT900 Wolcott</p>	<p><b>Page</b></p> <p>15 of 62</p>
	<p><b>Project</b></p> <p>Guyed Tower Structural Analysis</p>	<p><b>Date</b></p> <p>17:19:08 06/19/18</p>
	<p><b>Client</b></p> <p>Insite</p>	<p><b>Designed by</b></p> <p>Chunhui Song</p>

Guy Elevation		H	V	Initial Tension	Intercept	Initial Tension	Intercept	Initial Tension	Intercept	Initial Tension	Intercept	Initial Tension	Intercept	Initial Tension	Intercept	Initial Tension	Intercept
ft		ft	ft	K	ft	K	ft	K	ft	K	ft	K	ft	K	ft	K	ft
331.1	A	274.23	297.10	2.445	13.01	2.320	13.70	2.198	14.44	2.080	15.24	1.965	16.10	1.855	17.03	1.750	18.03
	B	277.23	344.10	2.390	15.83	2.284	16.54	2.181	17.31	2.080	18.12	1.982	18.99	1.887	19.92	1.795	20.90
	C	277.23	318.10	2.420	14.29	2.304	14.99	2.191	15.75	2.080	16.56	1.973	17.44	1.869	18.38	1.770	19.37
271.1	A	220.24	247.10	2.453	8.73	2.326	9.19	2.202	9.70	2.080	10.26	1.961	10.87	1.845	11.53	1.734	12.26
	B	221.24	288.10	2.391	10.74	2.286	11.23	2.182	11.75	2.080	12.31	1.980	12.91	1.883	13.56	1.788	14.27
	C	219.24	255.10	2.438	9.06	2.316	9.53	2.197	10.03	2.080	10.59	1.966	11.19	1.854	11.84	1.747	12.56
202.9	A	220.24	178.90	2.590	6.11	2.416	6.55	2.246	7.03	2.080	7.59	1.920	8.21	1.766	8.91	1.620	9.70
	B	221.24	219.90	2.504	7.61	2.360	8.07	2.218	8.57	2.080	9.13	1.945	9.75	1.815	10.44	1.690	11.19
	C	219.24	186.90	2.570	6.34	2.403	6.78	2.240	7.27	2.080	7.82	1.925	8.43	1.777	9.13	1.632	9.92
131.1	A	166.25	116.10	1.954	2.85	1.815	3.06	1.676	3.31	1.540	3.60	1.406	3.94	1.276	4.34	1.150	4.81
	B	167.25	143.10	1.895	3.45	1.775	3.68	1.657	3.94	1.540	4.24	1.425	4.58	1.312	4.96	1.203	5.41
	C	163.26	123.10	1.934	2.92	1.801	3.14	1.670	3.38	1.540	3.66	1.413	3.99	1.288	4.37	1.168	4.82
67.1667	A	167.27	52.17	2.104	1.98	1.913	2.18	1.725	2.42	1.540	2.71	1.360	3.06	1.186	3.51	1.024	4.06
	B	168.27	79.17	2.046	2.29	1.875	2.50	1.706	2.75	1.540	3.04	1.378	3.40	1.221	3.83	1.072	4.36
	C	164.27	59.17	2.089	1.98	1.903	2.17	1.720	2.41	1.540	2.69	1.364	3.03	1.195	3.46	1.035	3.99

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement	Face Offset	Lateral Offset	#	# Per Row	Clear Spacing	Width or Diameter	Perimeter	Weight
				ft	in	(Frac FW)			in	in	in	klf
7/8" Coax	B	No	Ar (CaAa)	347.000 - 6.000	0.0000	-0.25	1	1	0.5000	1.1000		0.000
1 1/4" Hybriflex (Sprint)	B	No	Ar (CaAa)	210.000 - 6.000	0.0000	0.25	3	3	0.5000	1.5500		0.001
1 1/4" Hybriflex (Sprint)	B	No	Ar (CaAa)	210.000 - 6.000	0.5000	0.25	3	3	0.5000	1.5500		0.001
1/2" Coax (Sprint)	B	No	Ar (CaAa)	70.000 - 6.000	0.0000	0.15	1	1	0.5000	0.5800		0.000
7/8" Coax (Lojack)	B	No	Ar (CaAa)	300.000 - 6.000	0.0000	0.15	1	1	0.5000	1.1000		0.000

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation	Face	A <sub>R</sub>	A <sub>F</sub>	C <sub>AA</sub> In Face	C <sub>AA</sub> Out Face	Weight
	ft		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	K
T1	347.000-327.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	2.200	0.000	0.002
		C	0.000	0.000	0.000	0.000	0.000
T2	327.000-307.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	2.200	0.000	0.002
		C	0.000	0.000	0.000	0.000	0.000
T3	307.000-287.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	3.630	0.000	0.003
		C	0.000	0.000	0.000	0.000	0.000
T4	287.000-267.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	4.400	0.000	0.004
		C	0.000	0.000	0.000	0.000	0.000
T5	267.000-247.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	4.400	0.000	0.004
		C	0.000	0.000	0.000	0.000	0.000
T6	247.000-227.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	4.400	0.000	0.004
		C	0.000	0.000	0.000	0.000	0.000
T7	227.000-207.000	A	0.000	0.000	0.000	0.000	0.000

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	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
		B	0.000	0.000	7.190	0.000	0.016
		C	0.000	0.000	0.000	0.000	0.000
T8	207.000-187.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	23.000	0.000	0.083
		C	0.000	0.000	0.000	0.000	0.000
T9	187.000-167.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	23.000	0.000	0.083
		C	0.000	0.000	0.000	0.000	0.000
T10	167.000-147.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	23.000	0.000	0.083
		C	0.000	0.000	0.000	0.000	0.000
T11	147.000-127.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	23.000	0.000	0.083
		C	0.000	0.000	0.000	0.000	0.000
T12	127.000-107.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	23.000	0.000	0.083
		C	0.000	0.000	0.000	0.000	0.000
T13	107.000-87.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	23.000	0.000	0.083
		C	0.000	0.000	0.000	0.000	0.000
T14	87.000-67.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	23.174	0.000	0.084
		C	0.000	0.000	0.000	0.000	0.000
T15	67.000-62.970	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	4.868	0.000	0.018
		C	0.000	0.000	0.000	0.000	0.000
T16	62.970-58.990	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	4.808	0.000	0.018
		C	0.000	0.000	0.000	0.000	0.000
T17	58.990-55.010	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	4.808	0.000	0.018
		C	0.000	0.000	0.000	0.000	0.000
T18	55.010-51.030	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	4.808	0.000	0.018
		C	0.000	0.000	0.000	0.000	0.000
T19	51.030-47.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	4.868	0.000	0.018
		C	0.000	0.000	0.000	0.000	0.000
T20	47.000-27.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	24.160	0.000	0.088
		C	0.000	0.000	0.000	0.000	0.000
T21	27.000-7.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	24.160	0.000	0.088
		C	0.000	0.000	0.000	0.000	0.000
T22	7.000-3.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	1.208	0.000	0.004
		C	0.000	0.000	0.000	0.000	0.000
T23	3.000-0.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000	0.000
		C	0.000	0.000	0.000	0.000	0.000

**Feed Line/Linear Appurtenances Section Areas - With Ice**

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
T1	347.000-327.000	A	1.892	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	9.769	0.000	0.140

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	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
T2	327.000-307.000	C		0.000	0.000	0.000	0.000	0.000
		A	1.881	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	9.723	0.000	0.139
		C		0.000	0.000	0.000	0.000	0.000
T3	307.000-287.000	A	1.869	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	15.963	0.000	0.227
		C		0.000	0.000	0.000	0.000	0.000
T4	287.000-267.000	A	1.856	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	19.245	0.000	0.272
		C		0.000	0.000	0.000	0.000	0.000
T5	267.000-247.000	A	1.842	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	19.134	0.000	0.269
		C		0.000	0.000	0.000	0.000	0.000
T6	247.000-227.000	A	1.827	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	19.015	0.000	0.265
		C		0.000	0.000	0.000	0.000	0.000
T7	227.000-207.000	A	1.811	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	26.849	0.000	0.359
		C		0.000	0.000	0.000	0.000	0.000
T8	207.000-187.000	A	1.793	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	71.593	0.000	0.899
		C		0.000	0.000	0.000	0.000	0.000
T9	187.000-167.000	A	1.774	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	71.181	0.000	0.887
		C		0.000	0.000	0.000	0.000	0.000
T10	167.000-147.000	A	1.753	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	70.724	0.000	0.874
		C		0.000	0.000	0.000	0.000	0.000
T11	147.000-127.000	A	1.729	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	70.212	0.000	0.860
		C		0.000	0.000	0.000	0.000	0.000
T12	127.000-107.000	A	1.702	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	69.628	0.000	0.844
		C		0.000	0.000	0.000	0.000	0.000
T13	107.000-87.000	A	1.671	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	68.946	0.000	0.826
		C		0.000	0.000	0.000	0.000	0.000
T14	87.000-67.000	A	1.633	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	69.277	0.000	0.818
		C		0.000	0.000	0.000	0.000	0.000
T15	67.000-62.970	A	1.605	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	15.135	0.000	0.177
		C		0.000	0.000	0.000	0.000	0.000
T16	62.970-58.990	A	1.595	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	14.896	0.000	0.173
		C		0.000	0.000	0.000	0.000	0.000
T17	58.990-55.010	A	1.584	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	14.841	0.000	0.172
		C		0.000	0.000	0.000	0.000	0.000
T18	55.010-51.030	A	1.573	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	14.783	0.000	0.171
		C		0.000	0.000	0.000	0.000	0.000
T19	51.030-47.000	A	1.561	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	14.906	0.000	0.171
		C		0.000	0.000	0.000	0.000	0.000
T20	47.000-27.000	A	1.517	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	72.869	0.000	0.821
		C		0.000	0.000	0.000	0.000	0.000
T21	27.000-7.000	A	1.404	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	69.975	0.000	0.750
		C		0.000	0.000	0.000	0.000	0.000

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	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
T22	7.000-3.000	A	1.242	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	3.293	0.000	0.033
		C		0.000	0.000	0.000	0.000	0.000
T23	3.000-0.000	A	1.101	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	0.000	0.000	0.000
		C		0.000	0.000	0.000	0.000	0.000

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>x</sub> in	CP <sub>z</sub> in	CP <sub>x</sub> Ice in	CP <sub>z</sub> Ice in
T1	347.000-327.000	4.9763	-13.2654	4.9763	-13.2654
T2	327.000-307.000	4.9763	-13.2654	4.9763	-13.2654
T3	307.000-287.000	7.8127	-8.3527	7.8127	-8.3527
T4	287.000-267.000	8.5763	-7.0300	8.5763	-7.0300
T5	267.000-247.000	8.5763	-7.0300	8.5763	-7.0300
T6	247.000-227.000	8.5763	-7.0300	8.5763	-7.0300
T7	227.000-207.000	10.3490	-3.4928	9.7239	-4.7813
T8	207.000-187.000	12.9075	0.3417	12.1892	-0.7719
T9	187.000-167.000	12.9075	0.3417	12.1919	-0.7650
T10	167.000-147.000	12.9075	0.3417	12.1949	-0.7572
T11	147.000-127.000	12.9075	0.3417	12.1984	-0.7484
T12	127.000-107.000	12.9075	0.3417	12.2024	-0.7382
T13	107.000-87.000	12.9075	0.3417	12.2071	-0.7261
T14	87.000-67.000	12.8980	0.3342	12.2067	-0.7102
T15	67.000-62.970	12.8473	0.2934	12.1799	-0.6959
T16	62.970-58.990	12.8473	0.2934	12.1813	-0.6923
T17	58.990-55.010	12.8473	0.2934	12.1829	-0.6885
T18	55.010-51.030	12.8473	0.2934	12.1846	-0.6843
T19	51.030-47.000	12.8473	0.2934	12.1864	-0.6798
T20	47.000-27.000	12.8473	0.2934	12.1929	-0.6637
T21	27.000-7.000	12.8473	0.2934	12.2112	-0.6191
T22	7.000-3.000	12.8473	0.2934	12.2407	-0.5486
T23	3.000-0.000	0.0000	0.0000	0.0000	0.0000

### Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>a</sub> No Ice	K <sub>a</sub> Ice
T1	1	7/8" Coax	327.00 - 347.00	0.6000	0.3269
T2	1	7/8" Coax	307.00 - 327.00	0.6000	0.3426
T3	1	7/8" Coax	287.00 - 307.00	0.6000	0.3452
T3	10	7/8" Coax	287.00 - 300.00	0.6000	0.3452
T4	1	7/8" Coax	267.00 - 287.00	0.6000	0.3345
T4	10	7/8" Coax	267.00 -	0.6000	0.3345



**tnxTower**

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<b>Job</b>	CT900 Wolcott	<b>Page</b>	19 of 62
<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	$K_a$ No Ice	$K_a$ Ice
			287.00		
T5	1	7/8" Coax	247.00 - 267.00	0.6000	0.3508
T5	10	7/8" Coax	247.00 - 267.00	0.6000	0.3508
T6	1	7/8" Coax	227.00 - 247.00	0.6000	0.3539
T6	10	7/8" Coax	227.00 - 247.00	0.6000	0.3539
T7	1	7/8" Coax	207.00 - 227.00	0.6000	0.3573
T7	2	1 1/4" Hybriflex	207.00 - 210.00	0.6000	0.3573
T7	3	1 1/4" Hybriflex	207.00 - 210.00	0.6000	0.3573
T7	10	7/8" Coax	207.00 - 227.00	0.6000	0.3573
T8	1	7/8" Coax	187.00 - 207.00	0.6000	0.3609
T8	2	1 1/4" Hybriflex	187.00 - 207.00	0.6000	0.3609
T8	3	1 1/4" Hybriflex	187.00 - 207.00	0.6000	0.3609
T8	10	7/8" Coax	187.00 - 207.00	0.6000	0.3609
T9	1	7/8" Coax	167.00 - 187.00	0.6000	0.3582
T9	2	1 1/4" Hybriflex	167.00 - 187.00	0.6000	0.3582
T9	3	1 1/4" Hybriflex	167.00 - 187.00	0.6000	0.3582
T9	10	7/8" Coax	167.00 - 187.00	0.6000	0.3582
T10	1	7/8" Coax	147.00 - 167.00	0.6000	0.3694
T10	2	1 1/4" Hybriflex	147.00 - 167.00	0.6000	0.3694
T10	3	1 1/4" Hybriflex	147.00 - 167.00	0.6000	0.3694
T10	10	7/8" Coax	147.00 - 167.00	0.6000	0.3694
T11	1	7/8" Coax	127.00 - 147.00	0.6000	0.3744
T11	2	1 1/4" Hybriflex	127.00 - 147.00	0.6000	0.3744
T11	3	1 1/4" Hybriflex	127.00 - 147.00	0.6000	0.3744
T11	10	7/8" Coax	127.00 - 147.00	0.6000	0.3744
T12	1	7/8" Coax	107.00 - 127.00	0.6000	0.3802
T12	2	1 1/4" Hybriflex	107.00 - 127.00	0.6000	0.3802
T12	3	1 1/4" Hybriflex	107.00 - 127.00	0.6000	0.3802
T12	10	7/8" Coax	107.00 - 127.00	0.6000	0.3802
T13	1	7/8" Coax	87.00 - 107.00	0.6000	0.3869
T13	2	1 1/4" Hybriflex	87.00 - 107.00	0.6000	0.3869
T13	3	1 1/4" Hybriflex	87.00 - 107.00	0.6000	0.3869
T13	10	7/8" Coax	87.00 - 107.00	0.6000	0.3869
T14	1	7/8" Coax	67.00 - 87.00	0.6000	0.3745

<p><b>tnxTower</b></p> <p><b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701</p>	<p><b>Job</b></p> <p>CT900 Wolcott</p>	<p><b>Page</b></p> <p>20 of 62</p>
	<p><b>Project</b></p> <p>Guyed Tower Structural Analysis</p>	<p><b>Date</b></p> <p>17:19:08 06/19/18</p>
	<p><b>Client</b></p> <p>Insite</p>	<p><b>Designed by</b></p> <p>Chunhui Song</p>

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	$K_a$ No Ice	$K_a$ Ice
T14	2	1 1/4" Hybriflex	67.00 - 87.00	0.6000	0.3745
T14	3	1 1/4" Hybriflex	67.00 - 87.00	0.6000	0.3745
T14	9	1/2" Coax	67.00 - 70.00	0.6000	0.3745
T14	10	7/8" Coax	67.00 - 87.00	0.6000	0.3745
T15	1	7/8" Coax	62.97 - 67.00	0.6000	0.4225
T15	2	1 1/4" Hybriflex	62.97 - 67.00	0.6000	0.4225
T15	3	1 1/4" Hybriflex	62.97 - 67.00	0.6000	0.4225
T15	9	1/2" Coax	62.97 - 67.00	0.6000	0.4225
T15	10	7/8" Coax	62.97 - 67.00	0.6000	0.4225
T16	1	7/8" Coax	58.99 - 62.97	0.6000	0.4524
T16	2	1 1/4" Hybriflex	58.99 - 62.97	0.6000	0.4524
T16	3	1 1/4" Hybriflex	58.99 - 62.97	0.6000	0.4524
T16	9	1/2" Coax	58.99 - 62.97	0.6000	0.4524
T16	10	7/8" Coax	58.99 - 62.97	0.6000	0.4524
T17	1	7/8" Coax	55.01 - 58.99	0.6000	0.4578
T17	2	1 1/4" Hybriflex	55.01 - 58.99	0.6000	0.4578
T17	3	1 1/4" Hybriflex	55.01 - 58.99	0.6000	0.4578
T17	9	1/2" Coax	55.01 - 58.99	0.6000	0.4578
T17	10	7/8" Coax	55.01 - 58.99	0.6000	0.4578
T18	1	7/8" Coax	51.03 - 55.01	0.6000	0.4598
T18	2	1 1/4" Hybriflex	51.03 - 55.01	0.6000	0.4598
T18	3	1 1/4" Hybriflex	51.03 - 55.01	0.6000	0.4598
T18	9	1/2" Coax	51.03 - 55.01	0.6000	0.4598
T18	10	7/8" Coax	51.03 - 55.01	0.6000	0.4598
T19	1	7/8" Coax	47.00 - 51.03	0.6000	0.3889
T19	2	1 1/4" Hybriflex	47.00 - 51.03	0.6000	0.3889
T19	3	1 1/4" Hybriflex	47.00 - 51.03	0.6000	0.3889
T19	9	1/2" Coax	47.00 - 51.03	0.6000	0.3889
T19	10	7/8" Coax	47.00 - 51.03	0.6000	0.3889
T20	1	7/8" Coax	27.00 - 47.00	0.6000	0.4563
T20	2	1 1/4" Hybriflex	27.00 - 47.00	0.6000	0.4563
T20	3	1 1/4" Hybriflex	27.00 - 47.00	0.6000	0.4563
T20	9	1/2" Coax	27.00 - 47.00	0.6000	0.4563
T20	10	7/8" Coax	27.00 - 47.00	0.6000	0.4563
T21	1	7/8" Coax	7.00 - 27.00	0.6000	0.4768
T21	2	1 1/4" Hybriflex	7.00 - 27.00	0.6000	0.4768
T21	3	1 1/4" Hybriflex	7.00 - 27.00	0.6000	0.4768
T21	9	1/2" Coax	7.00 - 27.00	0.6000	0.4768
T21	10	7/8" Coax	7.00 - 27.00	0.6000	0.4768
T22	1	7/8" Coax	6.00 - 7.00	0.6000	0.5232
T22	2	1 1/4" Hybriflex	6.00 - 7.00	0.6000	0.5232
T22	3	1 1/4" Hybriflex	6.00 - 7.00	0.6000	0.5232
T22	9	1/2" Coax	6.00 - 7.00	0.6000	0.5232
T22	10	7/8" Coax	6.00 - 7.00	0.6000	0.5232

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	$C_{AA}$ Front	$C_{AA}$ Side	Weight	
			ft ft ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K	
5' Lightning Rod	B	From Leg	0.000	0.0000	347.000	No Ice	0.500	0.500	0.015

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	21 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	CAAA Front	CAAA Side	Weight
			Horz	Vert					
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
			0.000			1/2" Ice	1.017	1.017	0.020
			2.000			1" Ice	1.426	1.426	0.028
Beacon (.035k 2.250CAAA)	C	From Leg	0.000	0.0000	347.000	No Ice	2.250	2.250	0.035
			0.000			1/2" Ice	2.500	2.500	0.450
			0.500			1" Ice	2.750	2.750	0.865
Beacon (10lbs 0.5CaAa)	A	From Leg	0.500	0.0000	225.000	No Ice	0.500	0.500	0.005
			0.000			1/2" Ice	0.700	0.700	0.006
			0.000			1" Ice	0.900	0.900	0.008
Beacon (10lbs 0.5CaAa)	B	From Leg	0.500	0.0000	225.000	No Ice	0.500	0.500	0.005
			0.000			1/2" Ice	0.700	0.700	0.006
			0.000			1" Ice	0.900	0.900	0.008
Beacon (10lbs 0.5CaAa)	A	From Leg	0.500	0.0000	117.000	No Ice	0.500	0.500	0.005
			0.000			1/2" Ice	0.700	0.700	0.006
			0.000			1" Ice	0.900	0.900	0.008
Beacon (10lbs 0.5CaAa)	B	From Leg	0.500	0.0000	117.000	No Ice	0.500	0.500	0.005
			0.000			1/2" Ice	0.700	0.700	0.006
			0.000			1" Ice	0.900	0.900	0.008
***									
Telewave ANT150F6-L (Lojack)	B	From Leg	2.000	0.0000	300.000	No Ice	5.592	5.592	0.043
			0.000			1/2" Ice	7.656	7.656	0.084
			0.000			1" Ice	9.738	9.738	0.137
4' Stand off (Lojack)	B	From Leg	0.000	0.0000	300.000	No Ice	0.700	0.700	0.010
			0.000			1/2" Ice	0.900	0.900	0.013
			2.000			1" Ice	1.100	1.100	0.016
***									
Commscope NNVV-65B-R4 (Sprint)	A	From Leg	4.000	0.0000	201.000	No Ice	12.271	5.750	0.077
			0.000			1/2" Ice	12.766	6.207	0.150
			0.000			1" Ice	13.268	6.671	0.228
Commscope NNVV-65B-R4 (Sprint)	B	From Leg	4.000	0.0000	201.000	No Ice	12.271	5.750	0.077
			0.000			1/2" Ice	12.766	6.207	0.150
			0.000			1" Ice	13.268	6.671	0.228
Commscope NNVV-65B-R4 (Sprint)	C	From Leg	4.000	0.0000	201.000	No Ice	12.271	5.750	0.077
			0.000			1/2" Ice	12.766	6.207	0.150
			0.000			1" Ice	13.268	6.671	0.228
Nokia AAHC (Sprint)	A	From Leg	4.000	0.0000	201.000	No Ice	4.212	2.073	0.104
			0.000			1/2" Ice	4.468	2.265	0.136
			0.000			1" Ice	4.731	2.468	0.172
Nokia AAHC (Sprint)	B	From Leg	4.000	0.0000	201.000	No Ice	4.212	2.073	0.104
			0.000			1/2" Ice	4.468	2.265	0.136
			0.000			1" Ice	4.731	2.468	0.172
Nokia AAHC (Sprint)	C	From Leg	4.000	0.0000	201.000	No Ice	4.212	2.073	0.104
			0.000			1/2" Ice	4.468	2.265	0.136
			0.000			1" Ice	4.731	2.468	0.172
(2) 800MHz 2X50W RRH W/FILTER (Sprint)	A	From Leg	3.000	0.0000	201.000	No Ice	2.058	1.932	0.064
			0.000			1/2" Ice	2.240	2.109	0.086
			0.000			1" Ice	2.429	2.293	0.111
(2) 800MHz 2X50W RRH W/FILTER (Sprint)	B	From Leg	3.000	0.0000	201.000	No Ice	2.058	1.932	0.064
			0.000			1/2" Ice	2.240	2.109	0.086
			0.000			1" Ice	2.429	2.293	0.111
(2) 800MHz 2X50W RRH W/FILTER (Sprint)	C	From Leg	3.000	0.0000	201.000	No Ice	2.058	1.932	0.064
			0.000			1/2" Ice	2.240	2.109	0.086
			0.000			1" Ice	2.429	2.293	0.111
Alcatel Lucent 1900 MHz (Sprint)	A	From Leg	3.000	0.0000	201.000	No Ice	1.706	1.286	0.053
			0.000			1/2" Ice	1.870	1.432	0.070
			0.000			1" Ice	2.041	1.585	0.090
Alcatel Lucent 1900 MHz (Sprint)	B	From Leg	3.000	0.0000	201.000	No Ice	1.706	1.286	0.053
			0.000			1/2" Ice	1.870	1.432	0.070

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	22 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight	
			Horz	Lateral						Vert
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K	
Alcatel Lucent 1900 MHz (Sprint)	C	From Leg	0.000		0.0000	201.000	1" Ice	2.041	1.585	0.090
			3.000				No Ice	1.706	1.286	0.053
			0.000				1/2" Ice	1.870	1.432	0.070
			0.000				1" Ice	2.041	1.585	0.090
800 EXTERNAL NOTCH FILTER (Sprint)	A	From Leg	3.000		0.0000	201.000	No Ice	0.660	0.321	0.011
			0.000				1/2" Ice	0.763	0.398	0.017
			0.000				1" Ice	0.873	0.483	0.024
800 EXTERNAL NOTCH FILTER (Sprint)	B	From Leg	3.000		0.0000	201.000	No Ice	0.660	0.321	0.011
			0.000				1/2" Ice	0.763	0.398	0.017
			0.000				1" Ice	0.873	0.483	0.024
800 EXTERNAL NOTCH FILTER (Sprint)	C	From Leg	3.000		0.0000	201.000	No Ice	0.660	0.321	0.011
			0.000				1/2" Ice	0.763	0.398	0.017
			0.000				1" Ice	0.873	0.483	0.024
			0.000				1" Ice	0.873	0.483	0.024
SM 407-3 (Sprint)	C	From Leg	0.000		0.0000	201.000	No Ice	20.490	20.490	0.956
			0.000				1/2" Ice	30.390	30.390	1.376
			0.000				1" Ice	40.290	40.290	1.796
PCTEL GPS-TMG-HR-26NCM (.0006, .277CAA) (Sprint)	C	From Leg	0.000		0.0000	70.000	No Ice	0.237	0.139	0.001
			0.000				1/2" Ice	0.304	0.189	0.004
			2.500				1" Ice	0.378	0.245	0.008

## Tower Pressures - No Ice

$$G_H = 0.850$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>AA</sub> In Face	C <sub>AA</sub> Out Face
ft	ft		ksf	ft <sup>2</sup>	c	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
T1 347.000-327.000	337.000	1.634	0.031	64.792	A	2.760	12.902	9.583	61.19	0.000	0.000
					B	2.760	12.902	61.19	2.200	0.000	
					C	2.760	12.902	61.19	0.000	0.000	
T2 327.000-307.000	317.000	1.614	0.031	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954	65.13	2.200	0.000	
					C	2.760	11.954	65.13	0.000	0.000	
T3 307.000-287.000	297.000	1.592	0.031	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954	65.13	3.630	0.000	
					C	2.760	11.954	65.13	0.000	0.000	
T4 287.000-267.000	277.000	1.568	0.030	64.792	A	2.760	12.902	9.583	61.19	0.000	0.000
					B	2.760	12.902	61.19	4.400	0.000	
					C	2.760	12.902	61.19	0.000	0.000	
T5 267.000-247.000	257.000	1.544	0.030	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954	65.13	4.400	0.000	
					C	2.760	11.954	65.13	0.000	0.000	
T6 247.000-227.000	237.000	1.518	0.029	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954	65.13	4.400	0.000	
					C	2.760	11.954	65.13	0.000	0.000	
T7 227.000-207.000	217.000	1.49	0.029	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954	65.13	7.190	0.000	
					C	2.760	11.954	65.13	0.000	0.000	



<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b> CT900 Wolcott	<b>Page</b> 23 of 62
	<b>Project</b> Guyed Tower Structural Analysis	<b>Date</b> 17:19:08 06/19/18
	<b>Client</b> Insite	<b>Designed by</b> Chunhui Song

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub> ksf	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>
T8 207.000-187.000	197.000	1.46	0.028	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954		65.13	23.000	0.000
					C	2.760	11.954		65.13	0.000	0.000
T9 187.000-167.000	177.000	1.427	0.027	64.792	A	2.760	12.428	9.583	63.10	0.000	0.000
					B	2.760	12.428		63.10	23.000	0.000
					C	2.760	12.428		63.10	0.000	0.000
T10 167.000-147.000	157.000	1.392	0.027	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954		65.13	23.000	0.000
					C	2.760	11.954		65.13	0.000	0.000
T11 147.000-127.000	137.000	1.352	0.026	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954		65.13	23.000	0.000
					C	2.760	11.954		65.13	0.000	0.000
T12 127.000-107.000	117.000	1.308	0.025	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954		65.13	23.000	0.000
					C	2.760	11.954		65.13	0.000	0.000
T13 107.000-87.000	97.000	1.258	0.024	64.792	A	2.760	11.954	9.583	65.13	0.000	0.000
					B	2.760	11.954		65.13	23.000	0.000
					C	2.760	11.954		65.13	0.000	0.000
T14 87.000-67.000	77.000	1.198	0.023	64.792	A	3.451	11.954	9.583	62.21	0.000	0.000
					B	3.451	11.954		62.21	23.174	0.000
					C	3.451	11.954		62.21	0.000	0.000
T15 67.000-62.970	64.985	1.156	0.022	13.056	A	0.460	2.400	1.931	67.52	0.000	0.000
					B	0.460	2.400		67.52	4.868	0.000
					C	0.460	2.400		67.52	0.000	0.000
T16 62.970-58.990	60.980	1.14	0.022	13.213	A	2.782	0.473	2.322	71.33	0.000	0.000
					B	2.782	0.473		71.33	4.808	0.000
					C	2.782	0.473		71.33	0.000	0.000
T17 58.990-55.010	57.000	1.124	0.022	13.213	A	2.773	0.469	2.322	71.62	0.000	0.000
					B	2.773	0.469		71.62	4.808	0.000
					C	2.773	0.469		71.62	0.000	0.000
T18 55.010-51.030	53.020	1.107	0.021	13.213	A	2.773	0.469	2.322	71.62	0.000	0.000
					B	2.773	0.469		71.62	4.808	0.000
					C	2.773	0.469		71.62	0.000	0.000
T19 51.030-47.000	49.015	1.089	0.021	13.379	A	3.254	0.460	2.351	63.30	0.000	0.000
					B	3.254	0.460		63.30	4.868	0.000
					C	3.254	0.460		63.30	0.000	0.000
T20 47.000-27.000	37.000	1.027	0.020	66.397	A	14.375	2.326	11.667	69.86	0.000	0.000
					B	14.375	2.326		69.86	24.160	0.000
					C	14.375	2.326		69.86	0.000	0.000
T21 27.000-7.000	17.000	0.872	0.017	66.397	A	14.375	2.326	11.667	69.86	0.000	0.000
					B	14.375	2.326		69.86	24.160	0.000
					C	14.375	2.326		69.86	0.000	0.000
T22 7.000-3.000	5.000	0.85	0.016	13.279	A	2.785	0.458	2.333	71.96	0.000	0.000
					B	2.785	0.458		71.96	1.208	0.000
					C	2.785	0.458		71.96	0.000	0.000
T23 3.000-0.000	1.500	0.85	0.016	9.960	A	2.653	0.388	1.750	57.55	0.000	0.000
					B	2.653	0.388		57.55	0.000	0.000
					C	2.653	0.388		57.55	0.000	0.000

### Tower Pressure - With Ice

$$G_H = 0.850$$

<b>Job</b>	CT900 Wolcott	<b>Page</b>	24 of 62
<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation ft	z ft	Kz	qz ksf	tz in	AG ft <sup>2</sup>	F a c e	AF ft <sup>2</sup>	AR ft <sup>2</sup>	Aleg ft <sup>2</sup>	Leg %	CAAA In Face ft <sup>2</sup>	CAAA Out Face ft <sup>2</sup>	
T1 347.000-327.000	337.000	1.634	0.009	1.8924	71.100	A	2.760	45.098	22.199	46.39	0.000	0.000	
						B	2.760	45.098			9.769	0.000	
						C	2.760	45.098			46.39	0.000	0.000
T2 327.000-307.000	317.000	1.614	0.009	1.8808	71.061	A	2.760	43.953	22.122	47.36	0.000	0.000	
						B	2.760	43.953			47.36	9.723	0.000
						C	2.760	43.953			47.36	0.000	0.000
T3 307.000-287.000	297.000	1.592	0.009	1.8686	71.020	A	2.760	43.745	22.041	47.39	0.000	0.000	
						B	2.760	43.745			47.39	15.963	0.000
						C	2.760	43.745			47.39	0.000	0.000
T4 287.000-267.000	277.000	1.568	0.009	1.8556	70.977	A	2.760	44.473	21.954	46.48	0.000	0.000	
						B	2.760	44.473			46.48	19.245	0.000
						C	2.760	44.473			46.48	0.000	0.000
T5 267.000-247.000	257.000	1.544	0.008	1.8418	70.931	A	2.760	43.289	21.862	47.47	0.000	0.000	
						B	2.760	43.289			47.47	19.134	0.000
						C	2.760	43.289			47.47	0.000	0.000
T6 247.000-227.000	237.000	1.518	0.008	1.8269	70.881	A	2.760	43.036	21.763	47.52	0.000	0.000	
						B	2.760	43.036			47.52	19.015	0.000
						C	2.760	43.036			47.52	0.000	0.000
T7 227.000-207.000	217.000	1.49	0.008	1.8109	70.828	A	2.760	42.763	21.656	47.57	0.000	0.000	
						B	2.760	42.763			47.57	26.849	0.000
						C	2.760	42.763			47.57	0.000	0.000
T8 207.000-187.000	197.000	1.46	0.008	1.7934	70.770	A	2.760	42.466	21.540	47.63	0.000	0.000	
						B	2.760	42.466			47.63	71.593	0.000
						C	2.760	42.466			47.63	0.000	0.000
T9 187.000-167.000	177.000	1.427	0.008	1.7743	70.706	A	2.760	42.616	21.412	47.19	0.000	0.000	
						B	2.760	42.616			47.19	71.181	0.000
						C	2.760	42.616			47.19	0.000	0.000
T10 167.000-147.000	157.000	1.392	0.008	1.7532	70.636	A	2.760	41.782	21.271	47.76	0.000	0.000	
						B	2.760	41.782			47.76	70.724	0.000
						C	2.760	41.782			47.76	0.000	0.000
T11 147.000-127.000	137.000	1.352	0.007	1.7295	70.557	A	2.760	41.378	21.113	47.83	0.000	0.000	
						B	2.760	41.378			47.83	70.212	0.000
						C	2.760	41.378			47.83	0.000	0.000
T12 127.000-107.000	117.000	1.308	0.007	1.7024	70.466	A	2.760	40.917	20.933	47.92	0.000	0.000	
						B	2.760	40.917			47.92	69.628	0.000
						C	2.760	40.917			47.92	0.000	0.000
T13 107.000-87.000	97.000	1.258	0.007	1.6708	70.361	A	2.760	40.379	20.722	48.03	0.000	0.000	
						B	2.760	40.379			48.03	68.946	0.000
						C	2.760	40.379			48.03	0.000	0.000
T14 87.000-67.000	77.000	1.198	0.007	1.6326	70.234	A	3.451	40.482	20.468	46.59	0.000	0.000	
						B	3.451	40.482			46.59	69.277	0.000
						C	3.451	40.482			46.59	0.000	0.000
T15 67.000-62.970	64.985	1.156	0.006	1.6052	14.134	A	0.460	7.703	4.087	50.07	0.000	0.000	
						B	0.460	7.703			50.07	15.135	0.000
						C	0.460	7.703			50.07	0.000	0.000
T16 62.970-58.990	60.980	1.14	0.006	1.5950	14.271	A	4.192	3.622	3.732	47.76	0.000	0.000	
						B	4.192	3.622			47.76	14.896	0.000
						C	4.192	3.622			47.76	0.000	0.000
T17 58.990-55.010	57.000	1.124	0.006	1.5843	14.264	A	4.174	3.560	3.723	48.14	0.000	0.000	
						B	4.174	3.560			48.14	14.841	0.000
						C	4.174	3.560			48.14	0.000	0.000
T18 55.010-51.030	53.020	1.107	0.006	1.5728	14.256	A	4.164	3.538	3.713	48.21	0.000	0.000	
						B	4.164	3.538			48.21	14.783	0.000
						C	4.164	3.538			48.21	0.000	0.000
T19 51.030-47.000	49.015	1.089	0.006	1.5605	14.427	A	4.651	4.166	3.748	42.51	0.000	0.000	
						B	4.651	4.166			42.51	14.906	0.000
						C	4.651	4.166			42.51	0.000	0.000
T20 47.000-27.000	37.000	1.027	0.006	1.5173	71.455	A	21.118	17.728	18.410	47.39	0.000	0.000	
						B	21.118	17.728			47.39	72.869	0.000
						C	21.118	17.728			47.39	0.000	0.000

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	25 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation ft	z ft	Kz	qz ksf	tz in	AG ft <sup>2</sup>	F a c e ft <sup>2</sup>	AF ft <sup>2</sup>	AR ft <sup>2</sup>	Aleg ft <sup>2</sup>	Leg %	CAAA In Face ft <sup>2</sup>	CAAA Out Face ft <sup>2</sup>
T21 27.000-7.000	17.000	0.872	0.005	1.4037	71.076	A 20.614	20.614	16.576	17.905	48.15	0.000	0.000
						B 20.614	20.614	16.576		48.15	69.975	0.000
						C 20.614	20.614	16.576		48.15	0.000	0.000
T22 7.000-3.000	5.000	0.85	0.005	1.2420	14.107	A 3.889	3.889	2.838	3.437	51.10	0.000	0.000
						B 3.889	3.889	2.838		51.10	3.293	0.000
						C 3.889	3.889	2.838		51.10	0.000	0.000
T23 3.000-0.000	1.500	0.85	0.005	1.1012	10.510	A 3.387	3.387	2.750	2.484	40.48	0.000	0.000
						B 3.387	3.387	2.750		40.48	0.000	0.000
						C 3.387	3.387	2.750		40.48	0.000	0.000

### Tower Pressure - Service

$$G_H = 0.850$$

Section Elevation ft	z ft	Kz	qz ksf	AG ft <sup>2</sup>	F a c e ft <sup>2</sup>	AF ft <sup>2</sup>	AR ft <sup>2</sup>	Aleg ft <sup>2</sup>	Leg %	CAAA In Face ft <sup>2</sup>	CAAA Out Face ft <sup>2</sup>
T1 347.000-327.000	337.000	1.634	0.013	64.792	A 2.760	2.760	12.902	9.583	61.19	0.000	0.000
					B 2.760	2.760	12.902		61.19	2.200	0.000
					C 2.760	2.760	12.902		61.19	0.000	0.000
T2 327.000-307.000	317.000	1.614	0.013	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000
					B 2.760	2.760	11.954		65.13	2.200	0.000
					C 2.760	2.760	11.954		65.13	0.000	0.000
T3 307.000-287.000	297.000	1.592	0.012	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000
					B 2.760	2.760	11.954		65.13	3.630	0.000
					C 2.760	2.760	11.954		65.13	0.000	0.000
T4 287.000-267.000	277.000	1.568	0.012	64.792	A 2.760	2.760	12.902	9.583	61.19	0.000	0.000
					B 2.760	2.760	12.902		61.19	4.400	0.000
					C 2.760	2.760	12.902		61.19	0.000	0.000
T5 267.000-247.000	257.000	1.544	0.012	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000
					B 2.760	2.760	11.954		65.13	4.400	0.000
					C 2.760	2.760	11.954		65.13	0.000	0.000
T6 247.000-227.000	237.000	1.518	0.012	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000
					B 2.760	2.760	11.954		65.13	4.400	0.000
					C 2.760	2.760	11.954		65.13	0.000	0.000
T7 227.000-207.000	217.000	1.49	0.012	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000
					B 2.760	2.760	11.954		65.13	7.190	0.000
					C 2.760	2.760	11.954		65.13	0.000	0.000
T8 207.000-187.000	197.000	1.46	0.011	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000
					B 2.760	2.760	11.954		65.13	23.000	0.000
					C 2.760	2.760	11.954		65.13	0.000	0.000
T9 187.000-167.000	177.000	1.427	0.011	64.792	A 2.760	2.760	12.428	9.583	63.10	0.000	0.000
					B 2.760	2.760	12.428		63.10	23.000	0.000
					C 2.760	2.760	12.428		63.10	0.000	0.000
T10 167.000-147.000	157.000	1.392	0.011	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000
					B 2.760	2.760	11.954		65.13	23.000	0.000
					C 2.760	2.760	11.954		65.13	0.000	0.000
T11 147.000-127.000	137.000	1.352	0.011	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000
					B 2.760	2.760	11.954		65.13	23.000	0.000
					C 2.760	2.760	11.954		65.13	0.000	0.000
T12 127.000-107.000	117.000	1.308	0.010	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000
					B 2.760	2.760	11.954		65.13	23.000	0.000
					C 2.760	2.760	11.954		65.13	0.000	0.000
T13 97.000	97.000	1.258	0.010	64.792	A 2.760	2.760	11.954	9.583	65.13	0.000	0.000

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	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub> ksf	A <sub>G</sub> ft <sup>2</sup>	F <sub>a</sub> c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>
107.000-87.000					B	2.760	11.954		65.13	23.000	0.000
0					C	2.760	11.954		65.13	0.000	0.000
T14	77.000	1.198	0.009	64.792	A	3.451	11.954	9.583	62.21	0.000	0.000
87.000-67.000					B	3.451	11.954		62.21	23.174	0.000
					C	3.451	11.954		62.21	0.000	0.000
T15	64.985	1.156	0.009	13.056	A	0.460	2.400	1.931	67.52	0.000	0.000
67.000-62.970					B	0.460	2.400		67.52	4.868	0.000
					C	0.460	2.400		67.52	0.000	0.000
T16	60.980	1.14	0.009	13.213	A	2.782	0.473	2.322	71.33	0.000	0.000
62.970-58.990					B	2.782	0.473		71.33	4.808	0.000
					C	2.782	0.473		71.33	0.000	0.000
T17	57.000	1.124	0.009	13.213	A	2.773	0.469	2.322	71.62	0.000	0.000
58.990-55.010					B	2.773	0.469		71.62	4.808	0.000
					C	2.773	0.469		71.62	0.000	0.000
T18	53.020	1.107	0.009	13.213	A	2.773	0.469	2.322	71.62	0.000	0.000
55.010-51.030					B	2.773	0.469		71.62	4.808	0.000
					C	2.773	0.469		71.62	0.000	0.000
T19	49.015	1.089	0.009	13.379	A	3.254	0.460	2.351	63.30	0.000	0.000
51.030-47.000					B	3.254	0.460		63.30	4.868	0.000
					C	3.254	0.460		63.30	0.000	0.000
T20	37.000	1.027	0.008	66.397	A	14.375	2.326	11.667	69.86	0.000	0.000
47.000-27.000					B	14.375	2.326		69.86	24.160	0.000
					C	14.375	2.326		69.86	0.000	0.000
T21	17.000	0.872	0.007	66.397	A	14.375	2.326	11.667	69.86	0.000	0.000
27.000-7.000					B	14.375	2.326		69.86	24.160	0.000
					C	14.375	2.326		69.86	0.000	0.000
T22	5.000	0.85	0.007	13.279	A	2.785	0.458	2.333	71.96	0.000	0.000
7.000-3.000					B	2.785	0.458		71.96	1.208	0.000
					C	2.785	0.458		71.96	0.000	0.000
T23	1.500	0.85	0.007	9.960	A	2.653	0.388	1.750	57.55	0.000	0.000
3.000-0.000					B	2.653	0.388		57.55	0.000	0.000
					C	2.653	0.388		57.55	0.000	0.000

### Tower Forces - No Ice - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F <sub>a</sub> c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
T1	0.002	0.824	A	0.242	2.463	0.031	1	1	10.283	0.712	0.036	C
347.000-327.000		TA 0.531	B	0.242	2.463		1	1	10.283			
			C	0.242	2.463		1	1	10.283			
T2	0.002	0.617	A	0.227	2.508	0.031	1	1	9.691	0.676	0.034	C
327.000-307.000			B	0.227	2.508		1	1	9.691			
			C	0.227	2.508		1	1	9.691			
T3	0.003	0.617	A	0.227	2.508	0.031	1	1	9.691	0.689	0.034	C
307.000-287.000			B	0.227	2.508		1	1	9.691			
			C	0.227	2.508		1	1	9.691			
T4	0.004	0.824	A	0.242	2.463	0.030	1	1	10.283	0.717	0.036	C
287.000-267.000		TA 0.531	B	0.242	2.463		1	1	10.283			
			C	0.242	2.463		1	1	10.283			
T5	0.004	0.617	A	0.227	2.508	0.030	1	1	9.691	0.680	0.034	C
267.000-247.000			B	0.227	2.508		1	1	9.691			
			C	0.227	2.508		1	1	9.691			
T6	0.004	0.617	A	0.227	2.508	0.029	1	1	9.691	0.668	0.033	C
247.000-227.000			B	0.227	2.508		1	1	9.691			
			C	0.227	2.508		1	1	9.691			



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	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K				ksf			ft <sup>2</sup>	K	klf	
T7 227.000-207.000	0.016	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.029	1 1 1	1 1 1	9.691 9.691 9.691	0.697	0.035	B
T8 207.000-187.000	0.083	0.617 TA 0.520	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.028	1 1 1	1 1 1	9.691 9.691 9.691	0.909	0.045	B
T9 187.000-167.000	0.083	0.720	A B C	0.234 0.234 0.234	2.485 2.485 2.485	0.027	1 1 1	1 1 1	9.986 9.986 9.986	0.901	0.045	B
T10 167.000-147.000	0.083	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.027	1 1 1	1 1 1	9.691 9.691 9.691	0.867	0.043	B
T11 147.000-127.000	0.083	0.617 TA 0.531	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.026	1 1 1	1 1 1	9.691 9.691 9.691	0.842	0.042	B
T12 127.000-107.000	0.083	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.025	1 1 1	1 1 1	9.691 9.691 9.691	0.815	0.041	B
T13 107.000-87.000	0.083	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.024	1 1 1	1 1 1	9.691 9.691 9.691	0.783	0.039	B
T14 87.000-67.000	0.084	0.651	A B C	0.238 0.238 0.238	2.475 2.475 2.475	0.023	1 1 1	1 1 1	10.409 10.409 10.409	0.776	0.039	B
T15 67.000-62.970	0.018	0.120	A B C	0.219 0.219 0.219	2.534 2.534 2.534	0.022	1 1 1	1 1 1	1.847 1.847 1.847	0.144	0.036	B
T16 62.970-58.990	0.018	0.177	A B C	0.246 0.246 0.246	2.449 2.449 2.449	0.022	1 1 1	1 1 1	3.058 3.058 3.058	0.193	0.049	B
T17 58.990-55.010	0.018	0.177	A B C	0.245 0.245 0.245	2.452 2.452 2.452	0.022	1 1 1	1 1 1	3.047 3.047 3.047	0.190	0.048	B
T18 55.010-51.030	0.018	0.177	A B C	0.245 0.245 0.245	2.452 2.452 2.452	0.021	1 1 1	1 1 1	3.047 3.047 3.047	0.187	0.047	B
T19 51.030-47.000	0.018	0.197	A B C	0.278 0.278 0.278	2.357 2.357 2.357	0.021	1 1 1	1 1 1	3.526 3.526 3.526	0.200	0.050	B
T20 47.000-27.000	0.088	0.904	A B C	0.252 0.252 0.252	2.433 2.433 2.433	0.020	1 1 1	1 1 1	15.737 15.737 15.737	0.886	0.044	B
T21 27.000-7.000	0.088	0.904	A B C	0.252 0.252 0.252	2.433 2.433 2.433	0.017	1 1 1	1 1 1	15.737 15.737 15.737	0.752	0.038	B
T22 7.000-3.000	0.004	0.177	A B C	0.244 0.244 0.244	2.455 2.455 2.455	0.016	1 1 1	1 1 1	3.052 3.052 3.052	0.114	0.029	B
T23 3.000-0.000	0.000	0.159	A B C	0.305 0.305 0.305	2.282 2.282 2.282	0.016	1 1 1	1 1 1	2.886 2.886 2.886	0.091	0.030	C
Sum Weight:	0.887	14.292								13.488		

**Tower Forces - No Ice - Wind 60 To Face**

<b>Job</b>	CT900 Wolcott	<b>Page</b>	28 of 62
<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K				ksf			ft <sup>2</sup>	K	klf	
T1 347.000-327.000	0.002	0.824 TA 0.531	A B C	0.242 0.242 0.242	2.463 2.463 2.463	0.031	0.8 0.8 0.8	1 1 1	9.731 9.731 9.731	0.675	0.034	C
T2 327.000-307.000	0.002	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.031	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.639	0.032	C
T3 307.000-287.000	0.003	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.031	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.653	0.033	C
T4 287.000-267.000	0.004	0.824 TA 0.531	A B C	0.242 0.242 0.242	2.463 2.463 2.463	0.030	0.8 0.8 0.8	1 1 1	9.731 9.731 9.731	0.682	0.034	C
T5 267.000-247.000	0.004	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.030	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.645	0.032	C
T6 247.000-227.000	0.004	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.029	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.634	0.032	C
T7 227.000-207.000	0.016	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.029	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.663	0.033	C
T8 207.000-187.000	0.083	0.617 TA 0.520	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.028	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.876	0.044	C
T9 187.000-167.000	0.083	0.720	A B C	0.234 0.234 0.234	2.485 2.485 2.485	0.027	0.8 0.8 0.8	1 1 1	9.433 9.433 9.433	0.869	0.043	C
T10 167.000-147.000	0.083	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.027	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.835	0.042	C
T11 147.000-127.000	0.083	0.617 TA 0.531	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.026	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.812	0.041	C
T12 127.000-107.000	0.083	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.025	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.785	0.039	C
T13 107.000-87.000	0.083	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.024	0.8 0.8 0.8	1 1 1	9.139 9.139 9.139	0.755	0.038	C
T14 87.000-67.000	0.084	0.651	A B C	0.238 0.238 0.238	2.475 2.475 2.475	0.023	0.8 0.8 0.8	1 1 1	9.719 9.719 9.719	0.743	0.037	C
T15 67.000-62.970	0.018	0.120	A B C	0.219 0.219 0.219	2.534 2.534 2.534	0.022	0.8 0.8 0.8	1 1 1	1.755 1.755 1.755	0.139	0.035	C
T16 62.970-58.990	0.018	0.177	A B C	0.246 0.246 0.246	2.449 2.449 2.449	0.022	0.8 0.8 0.8	1 1 1	2.502 2.502 2.502	0.168	0.042	C
T17 58.990-55.010	0.018	0.177	A B C	0.245 0.245 0.245	2.452 2.452 2.452	0.022	0.8 0.8 0.8	1 1 1	2.492 2.492 2.492	0.165	0.042	C
T18 55.010-51.030	0.018	0.177	A B C	0.245 0.245 0.245	2.452 2.452 2.452	0.021	0.8 0.8 0.8	1 1 1	2.492 2.492 2.492	0.163	0.041	C
T19 51.030-47.000	0.018	0.197	A B C	0.278 0.278 0.278	2.357 2.357 2.357	0.021	0.8 0.8 0.8	1 1 1	2.875 2.875 2.875	0.173	0.043	C
T20 47.000-27.000	0.088	0.904	A B C	0.252 0.252 0.252	2.433 2.433 2.433	0.020	0.8 0.8 0.8	1 1 1	12.862 12.862 12.862	0.768	0.038	C

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b> CT900 Wolcott	<b>Page</b> 29 of 62
	<b>Project</b> Guyed Tower Structural Analysis	<b>Date</b> 17:19:08 06/19/18
	<b>Client</b> Insite	<b>Designed by</b> Chunhui Song

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
T21 27.000-7.000	0.088	0.904	A	0.252	2.433	0.017	0.8	1	12.862	0.652	0.033	C
			B	0.252	2.433		0.8	1	12.862			
			C	0.252	2.433		0.8	1	12.862			
T22 7.000-3.000	0.004	0.177	A	0.244	2.455	0.016	0.8	1	2.495	0.095	0.024	C
			B	0.244	2.455		0.8	1	2.495			
			C	0.244	2.455		0.8	1	2.495			
T23 3.000-0.000	0.000	0.159	A	0.305	2.282	0.016	0.8	1	2.355	0.075	0.025	C
			B	0.305	2.282		0.8	1	2.355			
			C	0.305	2.282		0.8	1	2.355			
Sum Weight:	0.887	14.292								12.664		

### Tower Forces - No Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
T1 347.000-327.000	0.002	0.824	A	0.242	2.463	0.031	0.85	1	9.869	0.684	0.034	C
		TA 0.531	B	0.242	2.463		0.85	1	9.869			
			C	0.242	2.463		0.85	1	9.869			
T2 327.000-307.000	0.002	0.617	A	0.227	2.508	0.031	0.85	1	9.277	0.648	0.032	C
			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T3 307.000-287.000	0.003	0.617	A	0.227	2.508	0.031	0.85	1	9.277	0.662	0.033	C
			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T4 287.000-267.000	0.004	0.824	A	0.242	2.463	0.030	0.85	1	9.869	0.691	0.035	C
		TA 0.531	B	0.242	2.463		0.85	1	9.869			
			C	0.242	2.463		0.85	1	9.869			
T5 267.000-247.000	0.004	0.617	A	0.227	2.508	0.030	0.85	1	9.277	0.654	0.033	C
			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T6 247.000-227.000	0.004	0.617	A	0.227	2.508	0.029	0.85	1	9.277	0.643	0.032	C
			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T7 227.000-207.000	0.016	0.617	A	0.227	2.508	0.029	0.85	1	9.277	0.672	0.034	C
			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T8 207.000-187.000	0.083	0.617	A	0.227	2.508	0.028	0.85	1	9.277	0.884	0.044	C
		TA 0.520	B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T9 187.000-167.000	0.083	0.720	A	0.234	2.485	0.027	0.85	1	9.571	0.877	0.044	C
			B	0.234	2.485		0.85	1	9.571			
			C	0.234	2.485		0.85	1	9.571			
T10 167.000-147.000	0.083	0.617	A	0.227	2.508	0.027	0.85	1	9.277	0.843	0.042	C
			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T11 147.000-127.000	0.083	0.617	A	0.227	2.508	0.026	0.85	1	9.277	0.819	0.041	C
		TA 0.531	B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T12 127.000-107.000	0.083	0.617	A	0.227	2.508	0.025	0.85	1	9.277	0.792	0.040	C
			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T13	0.083	0.617	A	0.227	2.508	0.024	0.85	1	9.277	0.762	0.038	C

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	30 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
107.000-87.000			B	0.227	2.508		0.85	1	9.277			
0			C	0.227	2.508		0.85	1	9.277			
T14	0.084	0.651	A	0.238	2.475	0.023	0.85	1	9.891	0.751	0.038	C
87.000-67.000			B	0.238	2.475		0.85	1	9.891			
			C	0.238	2.475		0.85	1	9.891			
T15	0.018	0.120	A	0.219	2.534	0.022	0.85	1	1.778	0.140	0.035	C
67.000-62.970			B	0.219	2.534		0.85	1	1.778			
			C	0.219	2.534		0.85	1	1.778			
T16	0.018	0.177	A	0.246	2.449	0.022	0.85	1	2.641	0.174	0.044	C
62.970-58.990			B	0.246	2.449		0.85	1	2.641			
			C	0.246	2.449		0.85	1	2.641			
T17	0.018	0.177	A	0.245	2.452	0.022	0.85	1	2.631	0.172	0.043	C
58.990-55.010			B	0.245	2.452		0.85	1	2.631			
			C	0.245	2.452		0.85	1	2.631			
T18	0.018	0.177	A	0.245	2.452	0.021	0.85	1	2.631	0.169	0.042	C
55.010-51.030			B	0.245	2.452		0.85	1	2.631			
			C	0.245	2.452		0.85	1	2.631			
T19	0.018	0.197	A	0.278	2.357	0.021	0.85	1	3.038	0.179	0.045	C
51.030-47.000			B	0.278	2.357		0.85	1	3.038			
			C	0.278	2.357		0.85	1	3.038			
T20	0.088	0.904	A	0.252	2.433	0.020	0.85	1	13.580	0.798	0.040	C
47.000-27.000			B	0.252	2.433		0.85	1	13.580			
			C	0.252	2.433		0.85	1	13.580			
T21	0.088	0.904	A	0.252	2.433	0.017	0.85	1	13.580	0.677	0.034	C
27.000-7.000			B	0.252	2.433		0.85	1	13.580			
			C	0.252	2.433		0.85	1	13.580			
T22	0.004	0.177	A	0.244	2.455	0.016	0.85	1	2.634	0.100	0.025	C
7.000-3.000			B	0.244	2.455		0.85	1	2.634			
			C	0.244	2.455		0.85	1	2.634			
T23	0.000	0.159	A	0.305	2.282	0.016	0.85	1	2.488	0.079	0.026	C
3.000-0.000			B	0.305	2.282		0.85	1	2.488			
			C	0.305	2.282		0.85	1	2.488			
Sum Weight:	0.887	14.292								12.870		

### Tower Forces - With Ice - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
T1	0.140	3.024	A	0.673	1.777	0.009	1	1	38.488	0.541	0.027	C
347.000-327.000		TA 1.773	B	0.673	1.777		1	1	38.488			
			C	0.673	1.777		1	1	38.488			
T2	0.139	2.671	A	0.657	1.78	0.009	1	1	37.107	0.518	0.026	C
327.000-307.000			B	0.657	1.78		1	1	37.107			
			C	0.657	1.78		1	1	37.107			
T3	0.227	2.650	A	0.655	1.78	0.009	1	1	36.868	0.524	0.026	C
307.000-287.000			B	0.655	1.78		1	1	36.868			
			C	0.655	1.78		1	1	36.868			
T4	0.272	2.960	A	0.665	1.778	0.009	1	1	37.758	0.534	0.027	C
287.000-267.000		TA 1.742	B	0.665	1.778		1	1	37.758			
			C	0.665	1.778		1	1	37.758			
T5	0.269	2.605	A	0.649	1.782	0.008	1	1	36.348	0.510	0.026	C
267.000-247.000			B	0.649	1.782		1	1	36.348			



<b>Job</b>	CT900 Wolcott	<b>Page</b>	31 of 62
<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K				ksf			ft <sup>2</sup>	K	klf	
00			C	0.649	1.782		1	1	36.348			
T6	0.265	2.580	A	0.646	1.783	0.008	1	1	36.062	0.498	0.025	C
247.000-227.0			B	0.646	1.783		1	1	36.062			
00			C	0.646	1.783		1	1	36.062			
T7	0.359	2.554	A	0.643	1.784	0.008	1	1	35.755	0.503	0.025	B
227.000-207.0			B	0.643	1.784		1	1	35.755			
00			C	0.643	1.784		1	1	35.755			
T8	0.899	2.525	A	0.639	1.785	0.008	1	1	35.422	0.585	0.029	B
207.000-187.0		TA 1.657	B	0.639	1.785		1	1	35.422			
00			C	0.639	1.785		1	1	35.422			
T9	0.887	2.637	A	0.642	1.784	0.008	1	1	35.613	0.572	0.029	B
187.000-167.0			B	0.642	1.784		1	1	35.613			
00			C	0.642	1.784		1	1	35.613			
T10	0.874	2.460	A	0.631	1.788	0.008	1	1	34.661	0.552	0.028	B
167.000-147.0			B	0.631	1.788		1	1	34.661			
00			C	0.631	1.788		1	1	34.661			
T11	0.860	2.422	A	0.626	1.79	0.007	1	1	34.217	0.532	0.027	B
147.000-127.0		TA 1.636	B	0.626	1.79		1	1	34.217			
00			C	0.626	1.79		1	1	34.217			
T12	0.844	2.379	A	0.62	1.793	0.007	1	1	33.714	0.511	0.026	B
127.000-107.0			B	0.62	1.793		1	1	33.714			
00			C	0.62	1.793		1	1	33.714			
T13	0.826	2.329	A	0.613	1.796	0.007	1	1	33.131	0.487	0.024	B
107.000-87.00			B	0.613	1.796		1	1	33.131			
0			C	0.613	1.796		1	1	33.131			
T14	0.818	2.388	A	0.626	1.79	0.007	1	1	34.224	0.470	0.024	B
87.000-67.000			B	0.626	1.79		1	1	34.224			
00			C	0.626	1.79		1	1	34.224			
T15	0.177	0.427	A	0.578	1.82	0.006	1	1	6.081	0.091	0.022	B
67.000-62.970			B	0.578	1.82		1	1	6.081			
00			C	0.578	1.82		1	1	6.081			
T16	0.173	0.378	A	0.548	1.846	0.006	1	1	6.771	0.099	0.025	B
62.970-58.990			B	0.548	1.846		1	1	6.771			
00			C	0.548	1.846		1	1	6.771			
T17	0.172	0.376	A	0.542	1.851	0.006	1	1	6.697	0.097	0.024	B
58.990-55.010			B	0.542	1.851		1	1	6.697			
00			C	0.542	1.851		1	1	6.697			
T18	0.171	0.373	A	0.54	1.853	0.006	1	1	6.667	0.095	0.024	B
55.010-51.030			B	0.54	1.853		1	1	6.667			
00			C	0.54	1.853		1	1	6.667			
T19	0.171	0.458	A	0.611	1.798	0.006	1	1	7.779	0.097	0.024	B
51.030-47.000			B	0.611	1.798		1	1	7.779			
00			C	0.611	1.798		1	1	7.779			
T20	0.821	1.895	A	0.544	1.85	0.006	1	1	33.697	0.441	0.022	B
47.000-27.000			B	0.544	1.85		1	1	33.697			
00			C	0.544	1.85		1	1	33.697			
T21	0.750	1.782	A	0.523	1.872	0.005	1	1	32.181	0.367	0.018	B
27.000-7.000			B	0.523	1.872		1	1	32.181			
00			C	0.523	1.872		1	1	32.181			
T22	0.033	0.310	A	0.477	1.932	0.005	1	1	5.798	0.050	0.013	B
7.000-3.000			B	0.477	1.932		1	1	5.798			
00			C	0.477	1.932		1	1	5.798			
T23	0.000	0.304	A	0.584	1.815	0.005	1	1	5.404	0.039	0.013	C
3.000-0.000			B	0.584	1.815		1	1	5.404			
00			C	0.584	1.815		1	1	5.404			
Sum Weight:	10.147	49.295								8.713		

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	32 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

### Tower Forces - With Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K				ksf			ft <sup>2</sup>	K	klf	
T1 347.000-327.000	0.140	3.024 TA 1.773	A B C	0.673 0.673 0.673	1.777 1.777 1.777	0.009	0.8 0.8 0.8	1 1 1	37.936 37.936 37.936	0.534	0.027	C
T2 327.000-307.000	0.139	2.671	A B C	0.657 0.657 0.657	1.78 1.78 1.78	0.009	0.8 0.8 0.8	1 1 1	36.554 36.554 36.554	0.510	0.026	C
T3 307.000-287.000	0.227	2.650	A B C	0.655 0.655 0.655	1.78 1.78 1.78	0.009	0.8 0.8 0.8	1 1 1	36.316 36.316 36.316	0.516	0.026	C
T4 287.000-267.000	0.272	2.960 TA 1.742	A B C	0.665 0.665 0.665	1.778 1.778 1.778	0.009	0.8 0.8 0.8	1 1 1	37.206 37.206 37.206	0.526	0.026	C
T5 267.000-247.000	0.269	2.605	A B C	0.649 0.649 0.649	1.782 1.782 1.782	0.008	0.8 0.8 0.8	1 1 1	35.796 35.796 35.796	0.503	0.025	C
T6 247.000-227.000	0.265	2.580	A B C	0.646 0.646 0.646	1.783 1.783 1.783	0.008	0.8 0.8 0.8	1 1 1	35.510 35.510 35.510	0.491	0.025	C
T7 227.000-207.000	0.359	2.554	A B C	0.643 0.643 0.643	1.784 1.784 1.784	0.008	0.8 0.8 0.8	1 1 1	35.203 35.203 35.203	0.496	0.025	C
T8 207.000-187.000	0.899	2.525 TA 1.657	A B C	0.639 0.639 0.639	1.785 1.785 1.785	0.008	0.8 0.8 0.8	1 1 1	34.870 34.870 34.870	0.578	0.029	C
T9 187.000-167.000	0.887	2.637	A B C	0.642 0.642 0.642	1.784 1.784 1.784	0.008	0.8 0.8 0.8	1 1 1	35.061 35.061 35.061	0.566	0.028	C
T10 167.000-147.000	0.874	2.460	A B C	0.631 0.631 0.631	1.788 1.788 1.788	0.008	0.8 0.8 0.8	1 1 1	34.109 34.109 34.109	0.545	0.027	C
T11 147.000-127.000	0.860	2.422 TA 1.636	A B C	0.626 0.626 0.626	1.79 1.79 1.79	0.007	0.8 0.8 0.8	1 1 1	33.665 33.665 33.665	0.526	0.026	C
T12 127.000-107.000	0.844	2.379	A B C	0.62 0.62 0.62	1.793 1.793 1.793	0.007	0.8 0.8 0.8	1 1 1	33.162 33.162 33.162	0.505	0.025	C
T13 107.000-87.000	0.826	2.329	A B C	0.613 0.613 0.613	1.796 1.796 1.796	0.007	0.8 0.8 0.8	1 1 1	32.579 32.579 32.579	0.481	0.024	C
T14 87.000-67.000	0.818	2.388	A B C	0.626 0.626 0.626	1.79 1.79 1.79	0.007	0.8 0.8 0.8	1 1 1	33.534 33.534 33.534	0.464	0.023	C
T15 67.000-62.970	0.177	0.427	A B C	0.578 0.578 0.578	1.82 1.82 1.82	0.006	0.8 0.8 0.8	1 1 1	5.989 5.989 5.989	0.090	0.022	C
T16 62.970-58.990	0.173	0.378	A B C	0.548 0.548 0.548	1.846 1.846 1.846	0.006	0.8 0.8 0.8	1 1 1	5.932 5.932 5.932	0.090	0.023	C
T17 58.990-55.010	0.172	0.376	A B C	0.542 0.542 0.542	1.851 1.851 1.851	0.006	0.8 0.8 0.8	1 1 1	5.862 5.862 5.862	0.089	0.022	C
T18 55.010-51.030	0.171	0.373	A B C	0.54 0.54 0.54	1.853 1.853 1.853	0.006	0.8 0.8 0.8	1 1 1	5.834 5.834 5.834	0.087	0.022	C
T19	0.171	0.458	A	0.611	1.798	0.006	0.8	1	6.849	0.089	0.022	C

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	33 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
51.030-47.000			B	0.611	1.798		0.8	1	6.849			
			C	0.611	1.798		0.8	1	6.849			
T20	0.821	1.895	A	0.544	1.85	0.006	0.8	1	29.473	0.404	0.020	C
47.000-27.000			B	0.544	1.85		0.8	1	29.473			
			C	0.544	1.85		0.8	1	29.473			
T21	0.750	1.782	A	0.523	1.872	0.005	0.8	1	28.058	0.336	0.017	C
27.000-7.000			B	0.523	1.872		0.8	1	28.058			
			C	0.523	1.872		0.8	1	28.058			
T22	0.033	0.310	A	0.477	1.932	0.005	0.8	1	5.020	0.044	0.011	C
7.000-3.000			B	0.477	1.932		0.8	1	5.020			
			C	0.477	1.932		0.8	1	5.020			
T23	0.000	0.304	A	0.584	1.815	0.005	0.8	1	4.727	0.034	0.011	C
3.000-0.000			B	0.584	1.815		0.8	1	4.727			
			C	0.584	1.815		0.8	1	4.727			
Sum Weight:	10.147	49.295								8.507		

### Tower Forces - With Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
T1	0.140	3.024	A	0.673	1.777	0.009	0.85	1	38.074	0.535	0.027	C
347.000-327.000		TA 1.773	B	0.673	1.777		0.85	1	38.074			
			C	0.673	1.777		0.85	1	38.074			
T2	0.139	2.671	A	0.657	1.78	0.009	0.85	1	36.692	0.512	0.026	C
327.000-307.000			B	0.657	1.78		0.85	1	36.692			
			C	0.657	1.78		0.85	1	36.692			
T3	0.227	2.650	A	0.655	1.78	0.009	0.85	1	36.454	0.518	0.026	C
307.000-287.000			B	0.655	1.78		0.85	1	36.454			
			C	0.655	1.78		0.85	1	36.454			
T4	0.272	2.960	A	0.665	1.778	0.009	0.85	1	37.344	0.528	0.026	C
287.000-267.000		TA 1.742	B	0.665	1.778		0.85	1	37.344			
			C	0.665	1.778		0.85	1	37.344			
T5	0.269	2.605	A	0.649	1.782	0.008	0.85	1	35.934	0.505	0.025	C
267.000-247.000			B	0.649	1.782		0.85	1	35.934			
			C	0.649	1.782		0.85	1	35.934			
T6	0.265	2.580	A	0.646	1.783	0.008	0.85	1	35.648	0.493	0.025	C
247.000-227.000			B	0.646	1.783		0.85	1	35.648			
			C	0.646	1.783		0.85	1	35.648			
T7	0.359	2.554	A	0.643	1.784	0.008	0.85	1	35.341	0.496	0.025	C
227.000-207.000			B	0.643	1.784		0.85	1	35.341			
			C	0.643	1.784		0.85	1	35.341			
T8	0.899	2.525	A	0.639	1.785	0.008	0.85	1	35.008	0.568	0.028	C
207.000-187.000		TA 1.657	B	0.639	1.785		0.85	1	35.008			
			C	0.639	1.785		0.85	1	35.008			
T9	0.887	2.637	A	0.642	1.784	0.008	0.85	1	35.199	0.555	0.028	C
187.000-167.000			B	0.642	1.784		0.85	1	35.199			
			C	0.642	1.784		0.85	1	35.199			
T10	0.874	2.460	A	0.631	1.788	0.008	0.85	1	34.247	0.535	0.027	C
167.000-147.000			B	0.631	1.788		0.85	1	34.247			
			C	0.631	1.788		0.85	1	34.247			
T11	0.860	2.422	A	0.626	1.79	0.007	0.85	1	33.803	0.516	0.026	C
147.000-127.000		TA 1.636	B	0.626	1.79		0.85	1	33.803			

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	34 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K				ksf			ft <sup>2</sup>	K	klf	
00			C	0.626	1.79		0.85	1	33.803			
T12	0.844	2.379	A	0.62	1.793	0.007	0.85	1	33.300	0.495	0.025	C
127.000-107.000			B	0.62	1.793		0.85	1	33.300			
00			C	0.62	1.793		0.85	1	33.300			
T13	0.826	2.329	A	0.613	1.796	0.007	0.85	1	32.717	0.471	0.024	C
107.000-87.000			B	0.613	1.796		0.85	1	32.717			
0			C	0.613	1.796		0.85	1	32.717			
T14	0.818	2.388	A	0.626	1.79	0.007	0.85	1	33.706	0.455	0.023	C
87.000-67.000			B	0.626	1.79		0.85	1	33.706			
			C	0.626	1.79		0.85	1	33.706			
T15	0.177	0.427	A	0.578	1.82	0.006	0.85	1	6.012	0.088	0.022	C
67.000-62.970			B	0.578	1.82		0.85	1	6.012			
			C	0.578	1.82		0.85	1	6.012			
T16	0.173	0.378	A	0.548	1.846	0.006	0.85	1	6.142	0.090	0.023	C
62.970-58.990			B	0.548	1.846		0.85	1	6.142			
			C	0.548	1.846		0.85	1	6.142			
T17	0.172	0.376	A	0.542	1.851	0.006	0.85	1	6.071	0.089	0.022	C
58.990-55.010			B	0.542	1.851		0.85	1	6.071			
			C	0.542	1.851		0.85	1	6.071			
T18	0.171	0.373	A	0.54	1.853	0.006	0.85	1	6.042	0.087	0.022	C
55.010-51.030			B	0.54	1.853		0.85	1	6.042			
			C	0.54	1.853		0.85	1	6.042			
T19	0.171	0.458	A	0.611	1.798	0.006	0.85	1	7.081	0.089	0.022	C
51.030-47.000			B	0.611	1.798		0.85	1	7.081			
			C	0.611	1.798		0.85	1	7.081			
T20	0.821	1.895	A	0.544	1.85	0.006	0.85	1	30.529	0.403	0.020	C
47.000-27.000			B	0.544	1.85		0.85	1	30.529			
			C	0.544	1.85		0.85	1	30.529			
T21	0.750	1.782	A	0.523	1.872	0.005	0.85	1	29.089	0.334	0.017	C
27.000-7.000			B	0.523	1.872		0.85	1	29.089			
			C	0.523	1.872		0.85	1	29.089			
T22	0.033	0.310	A	0.477	1.932	0.005	0.85	1	5.215	0.045	0.011	C
7.000-3.000			B	0.477	1.932		0.85	1	5.215			
			C	0.477	1.932		0.85	1	5.215			
T23	0.000	0.304	A	0.584	1.815	0.005	0.85	1	4.896	0.035	0.012	C
3.000-0.000			B	0.584	1.815		0.85	1	4.896			
			C	0.584	1.815		0.85	1	4.896			
Sum Weight:	10.147	49.295								8.441		

### Tower Forces - Service - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K				ksf			ft <sup>2</sup>	K	klf	
T1	0.002	0.824	A	0.242	2.463	0.013	1	1	10.283	0.290	0.014	C
347.000-327.000		TA 0.531	B	0.242	2.463		1	1	10.283			
00			C	0.242	2.463		1	1	10.283			
T2	0.002	0.617	A	0.227	2.508	0.013	1	1	9.691	0.275	0.014	C
327.000-307.000			B	0.227	2.508		1	1	9.691			
00			C	0.227	2.508		1	1	9.691			
T3	0.003	0.617	A	0.227	2.508	0.012	1	1	9.691	0.281	0.014	C
307.000-287.000			B	0.227	2.508		1	1	9.691			
00			C	0.227	2.508		1	1	9.691			

<b>Job</b>	CT900 Wolcott	<b>Page</b>	35 of 62
<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K				ksf			ft <sup>2</sup>	K	klf	
T4 287.000-267.000	0.004	0.824 TA 0.531	A B C	0.242 0.242 0.242	2.463 2.463 2.463	0.012	1 1 1	1 1 1	10.283 10.283 10.283	0.292	0.015	C
T5 267.000-247.000	0.004	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.012	1 1 1	1 1 1	9.691 9.691 9.691	0.277	0.014	C
T6 247.000-227.000	0.004	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.012	1 1 1	1 1 1	9.691 9.691 9.691	0.272	0.014	C
T7 227.000-207.000	0.016	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.012	1 1 1	1 1 1	9.691 9.691 9.691	0.284	0.014	B
T8 207.000-187.000	0.083	0.617 TA 0.520	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.011	1 1 1	1 1 1	9.691 9.691 9.691	0.370	0.019	B
T9 187.000-167.000	0.083	0.720	A B C	0.234 0.234 0.234	2.485 2.485 2.485	0.011	1 1 1	1 1 1	9.986 9.986 9.986	0.367	0.018	B
T10 167.000-147.000	0.083	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.011	1 1 1	1 1 1	9.691 9.691 9.691	0.353	0.018	B
T11 147.000-127.000	0.083	0.617 TA 0.531	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.011	1 1 1	1 1 1	9.691 9.691 9.691	0.343	0.017	B
T12 127.000-107.000	0.083	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.010	1 1 1	1 1 1	9.691 9.691 9.691	0.332	0.017	B
T13 107.000-87.000	0.083	0.617	A B C	0.227 0.227 0.227	2.508 2.508 2.508	0.010	1 1 1	1 1 1	9.691 9.691 9.691	0.319	0.016	B
T14 87.000-67.000	0.084	0.651	A B C	0.238 0.238 0.238	2.475 2.475 2.475	0.009	1 1 1	1 1 1	10.409 10.409 10.409	0.316	0.016	B
T15 67.000-62.970	0.018	0.120	A B C	0.219 0.219 0.219	2.534 2.534 2.534	0.009	1 1 1	1 1 1	1.847 1.847 1.847	0.059	0.015	B
T16 62.970-58.990	0.018	0.177	A B C	0.246 0.246 0.246	2.449 2.449 2.449	0.009	1 1 1	1 1 1	3.058 3.058 3.058	0.079	0.020	B
T17 58.990-55.010	0.018	0.177	A B C	0.245 0.245 0.245	2.452 2.452 2.452	0.009	1 1 1	1 1 1	3.047 3.047 3.047	0.078	0.019	B
T18 55.010-51.030	0.018	0.177	A B C	0.245 0.245 0.245	2.452 2.452 2.452	0.009	1 1 1	1 1 1	3.047 3.047 3.047	0.076	0.019	B
T19 51.030-47.000	0.018	0.197	A B C	0.278 0.278 0.278	2.357 2.357 2.357	0.009	1 1 1	1 1 1	3.526 3.526 3.526	0.081	0.020	B
T20 47.000-27.000	0.088	0.904	A B C	0.252 0.252 0.252	2.433 2.433 2.433	0.008	1 1 1	1 1 1	15.737 15.737 15.737	0.361	0.018	B
T21 27.000-7.000	0.088	0.904	A B C	0.252 0.252 0.252	2.433 2.433 2.433	0.007	1 1 1	1 1 1	15.737 15.737 15.737	0.306	0.015	B
T22 7.000-3.000	0.004	0.177	A B C	0.244 0.244 0.244	2.455 2.455 2.455	0.007	1 1 1	1 1 1	3.052 3.052 3.052	0.047	0.012	B
T23 3.000-0.000	0.000	0.159	A B C	0.305 0.305 0.305	2.282 2.282 2.282	0.007	1 1 1	1 1 1	2.886 2.886 2.886	0.037	0.012	C



<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	36 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K				ksf			ft <sup>2</sup>	K	klf	
Sum Weight:	0.887	14.292								5.495		

### Tower Forces - Service - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K				ksf			ft <sup>2</sup>	K	klf	
T1	0.002	0.824	A	0.242	2.463	0.013	0.8	1	9.731	0.275	0.014	C
347.000-327.000		TA 0.531	B	0.242	2.463		0.8	1	9.731			
			C	0.242	2.463		0.8	1	9.731			
T2	0.002	0.617	A	0.227	2.508	0.013	0.8	1	9.139	0.260	0.013	C
327.000-307.000			B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T3	0.003	0.617	A	0.227	2.508	0.012	0.8	1	9.139	0.266	0.013	C
307.000-287.000			B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T4	0.004	0.824	A	0.242	2.463	0.012	0.8	1	9.731	0.278	0.014	C
287.000-267.000		TA 0.531	B	0.242	2.463		0.8	1	9.731			
			C	0.242	2.463		0.8	1	9.731			
T5	0.004	0.617	A	0.227	2.508	0.012	0.8	1	9.139	0.263	0.013	C
267.000-247.000			B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T6	0.004	0.617	A	0.227	2.508	0.012	0.8	1	9.139	0.258	0.013	C
247.000-227.000			B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T7	0.016	0.617	A	0.227	2.508	0.012	0.8	1	9.139	0.270	0.014	C
227.000-207.000			B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T8	0.083	0.617	A	0.227	2.508	0.011	0.8	1	9.139	0.357	0.018	C
207.000-187.000		TA 0.520	B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T9	0.083	0.720	A	0.234	2.485	0.011	0.8	1	9.433	0.354	0.018	C
187.000-167.000			B	0.234	2.485		0.8	1	9.433			
			C	0.234	2.485		0.8	1	9.433			
T10	0.083	0.617	A	0.227	2.508	0.011	0.8	1	9.139	0.340	0.017	C
167.000-147.000			B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T11	0.083	0.617	A	0.227	2.508	0.011	0.8	1	9.139	0.331	0.017	C
147.000-127.000		TA 0.531	B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T12	0.083	0.617	A	0.227	2.508	0.010	0.8	1	9.139	0.320	0.016	C
127.000-107.000			B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T13	0.083	0.617	A	0.227	2.508	0.010	0.8	1	9.139	0.307	0.015	C
107.000-87.000			B	0.227	2.508		0.8	1	9.139			
			C	0.227	2.508		0.8	1	9.139			
T14	0.084	0.651	A	0.238	2.475	0.009	0.8	1	9.719	0.303	0.015	C
87.000-67.000			B	0.238	2.475		0.8	1	9.719			
			C	0.238	2.475		0.8	1	9.719			
T15	0.018	0.120	A	0.219	2.534	0.009	0.8	1	1.755	0.057	0.014	C
67.000-62.970			B	0.219	2.534		0.8	1	1.755			
			C	0.219	2.534		0.8	1	1.755			
T16	0.018	0.177	A	0.246	2.449	0.009	0.8	1	2.502	0.068	0.017	C

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	37 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
62.970-58.990			B	0.246	2.449		0.8	1	2.502			
			C	0.246	2.449		0.8	1	2.502			
T17	0.018	0.177	A	0.245	2.452	0.009	0.8	1	2.492	0.067	0.017	C
58.990-55.010			B	0.245	2.452		0.8	1	2.492			
			C	0.245	2.452		0.8	1	2.492			
T18	0.018	0.177	A	0.245	2.452	0.009	0.8	1	2.492	0.066	0.017	C
55.010-51.030			B	0.245	2.452		0.8	1	2.492			
			C	0.245	2.452		0.8	1	2.492			
T19	0.018	0.197	A	0.278	2.357	0.009	0.8	1	2.875	0.070	0.017	C
51.030-47.000			B	0.278	2.357		0.8	1	2.875			
			C	0.278	2.357		0.8	1	2.875			
T20	0.088	0.904	A	0.252	2.433	0.008	0.8	1	12.862	0.313	0.016	C
47.000-27.000			B	0.252	2.433		0.8	1	12.862			
			C	0.252	2.433		0.8	1	12.862			
T21	0.088	0.904	A	0.252	2.433	0.007	0.8	1	12.862	0.266	0.013	C
27.000-7.000			B	0.252	2.433		0.8	1	12.862			
			C	0.252	2.433		0.8	1	12.862			
T22	0.004	0.177	A	0.244	2.455	0.007	0.8	1	2.495	0.039	0.010	C
7.000-3.000			B	0.244	2.455		0.8	1	2.495			
			C	0.244	2.455		0.8	1	2.495			
T23	0.000	0.159	A	0.305	2.282	0.007	0.8	1	2.355	0.030	0.010	C
3.000-0.000			B	0.305	2.282		0.8	1	2.355			
			C	0.305	2.282		0.8	1	2.355			
Sum Weight:	0.887	14.292								5.159		

### Tower Forces - Service - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
T1	0.002	0.824	A	0.242	2.463	0.013	0.85	1	9.869	0.279	0.014	C
347.000-327.000		TA 0.531	B	0.242	2.463		0.85	1	9.869			
			C	0.242	2.463		0.85	1	9.869			
T2	0.002	0.617	A	0.227	2.508	0.013	0.85	1	9.277	0.264	0.013	C
327.000-307.000			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T3	0.003	0.617	A	0.227	2.508	0.012	0.85	1	9.277	0.270	0.013	C
307.000-287.000			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T4	0.004	0.824	A	0.242	2.463	0.012	0.85	1	9.869	0.281	0.014	C
287.000-267.000		TA 0.531	B	0.242	2.463		0.85	1	9.869			
			C	0.242	2.463		0.85	1	9.869			
T5	0.004	0.617	A	0.227	2.508	0.012	0.85	1	9.277	0.266	0.013	C
267.000-247.000			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T6	0.004	0.617	A	0.227	2.508	0.012	0.85	1	9.277	0.262	0.013	C
247.000-227.000			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T7	0.016	0.617	A	0.227	2.508	0.012	0.85	1	9.277	0.274	0.014	C
227.000-207.000			B	0.227	2.508		0.85	1	9.277			
			C	0.227	2.508		0.85	1	9.277			
T8	0.083	0.617	A	0.227	2.508	0.011	0.85	1	9.277	0.360	0.018	C
207.000-187.000		TA 0.520	B	0.227	2.508		0.85	1	9.277			

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	38 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	q <sub>z</sub> ksf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
00			C	0.227	2.508		0.85	1	9.277			
T9	0.083	0.720	A	0.234	2.485	0.011	0.85	1	9.571	0.357	0.018	C
187.000-167.0			B	0.234	2.485		0.85	1	9.571			
00			C	0.234	2.485		0.85	1	9.571			
T10	0.083	0.617	A	0.227	2.508	0.011	0.85	1	9.277	0.343	0.017	C
167.000-147.0			B	0.227	2.508		0.85	1	9.277			
00			C	0.227	2.508		0.85	1	9.277			
T11	0.083	0.617	A	0.227	2.508	0.011	0.85	1	9.277	0.334	0.017	C
147.000-127.0		TA 0.531	B	0.227	2.508		0.85	1	9.277			
00			C	0.227	2.508		0.85	1	9.277			
T12	0.083	0.617	A	0.227	2.508	0.010	0.85	1	9.277	0.323	0.016	C
127.000-107.0			B	0.227	2.508		0.85	1	9.277			
00			C	0.227	2.508		0.85	1	9.277			
T13	0.083	0.617	A	0.227	2.508	0.010	0.85	1	9.277	0.310	0.016	C
107.000-87.00			B	0.227	2.508		0.85	1	9.277			
0			C	0.227	2.508		0.85	1	9.277			
T14	0.084	0.651	A	0.238	2.475	0.009	0.85	1	9.891	0.306	0.015	C
87.000-67.000			B	0.238	2.475		0.85	1	9.891			
			C	0.238	2.475		0.85	1	9.891			
T15	0.018	0.120	A	0.219	2.534	0.009	0.85	1	1.778	0.057	0.014	C
67.000-62.970			B	0.219	2.534		0.85	1	1.778			
			C	0.219	2.534		0.85	1	1.778			
T16	0.018	0.177	A	0.246	2.449	0.009	0.85	1	2.641	0.071	0.018	C
62.970-58.990			B	0.246	2.449		0.85	1	2.641			
			C	0.246	2.449		0.85	1	2.641			
T17	0.018	0.177	A	0.245	2.452	0.009	0.85	1	2.631	0.070	0.018	C
58.990-55.010			B	0.245	2.452		0.85	1	2.631			
			C	0.245	2.452		0.85	1	2.631			
T18	0.018	0.177	A	0.245	2.452	0.009	0.85	1	2.631	0.069	0.017	C
55.010-51.030			B	0.245	2.452		0.85	1	2.631			
			C	0.245	2.452		0.85	1	2.631			
T19	0.018	0.197	A	0.278	2.357	0.009	0.85	1	3.038	0.073	0.018	C
51.030-47.000			B	0.278	2.357		0.85	1	3.038			
			C	0.278	2.357		0.85	1	3.038			
T20	0.088	0.904	A	0.252	2.433	0.008	0.85	1	13.580	0.325	0.016	C
47.000-27.000			B	0.252	2.433		0.85	1	13.580			
			C	0.252	2.433		0.85	1	13.580			
T21	0.088	0.904	A	0.252	2.433	0.007	0.85	1	13.580	0.276	0.014	C
27.000-7.000			B	0.252	2.433		0.85	1	13.580			
			C	0.252	2.433		0.85	1	13.580			
T22	0.004	0.177	A	0.244	2.455	0.007	0.85	1	2.634	0.041	0.010	C
7.000-3.000			B	0.244	2.455		0.85	1	2.634			
			C	0.244	2.455		0.85	1	2.634			
T23	0.000	0.159	A	0.305	2.282	0.007	0.85	1	2.488	0.032	0.011	C
3.000-0.000			B	0.305	2.282		0.85	1	2.488			
			C	0.305	2.282		0.85	1	2.488			
Sum Weight:	0.887	14.292								5.243		

### Force Totals (Does not include forces on guys)

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Torques kip-ft

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	39 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Torques kip-ft
Leg Weight	6.940			
Bracing Weight	7.352			
Total Member Self-Weight	14.292			
Guy Weight	3.026			
Total Weight	20.404			
Wind 0 deg - No Ice		0.001	-18.054	2.328
Wind 30 deg - No Ice		9.075	-15.717	3.039
Wind 60 deg - No Ice		15.539	-8.971	2.082
Wind 90 deg - No Ice		18.148	-0.001	0.567
Wind 120 deg - No Ice		15.636	9.027	-0.780
Wind 150 deg - No Ice		8.399	14.548	-1.188
Wind 180 deg - No Ice		-0.001	17.230	-2.328
Wind 210 deg - No Ice		-9.075	15.717	-3.039
Wind 240 deg - No Ice		-16.253	9.384	-2.082
Wind 270 deg - No Ice		-18.148	0.001	-0.567
Wind 300 deg - No Ice		-14.922	-8.614	0.780
Wind 330 deg - No Ice		-8.399	-14.548	1.188
Member Ice	35.003			
Guy Ice	35.980			
Total Weight Ice	106.210			
Wind 0 deg - Ice		0.000	-10.884	1.102
Wind 30 deg - Ice		5.483	-9.496	1.336
Wind 60 deg - Ice		9.553	-5.516	1.017
Wind 90 deg - Ice		10.965	-0.000	0.273
Wind 120 deg - Ice		9.426	5.442	-0.350
Wind 150 deg - Ice		5.306	9.190	-0.726
Wind 180 deg - Ice		-0.000	10.678	-1.102
Wind 210 deg - Ice		-5.483	9.496	-1.336
Wind 240 deg - Ice		-9.732	5.619	-1.017
Wind 270 deg - Ice		-10.965	0.000	-0.273
Wind 300 deg - Ice		-9.247	-5.339	0.350
Wind 330 deg - Ice		-5.306	-9.190	0.726
Total Weight	20.404			
Wind 0 deg - Service		0.000	-7.356	0.948
Wind 30 deg - Service		3.697	-6.403	1.238
Wind 60 deg - Service		6.331	-3.655	0.848
Wind 90 deg - Service		7.394	-0.000	0.231
Wind 120 deg - Service		6.370	3.678	-0.318
Wind 150 deg - Service		3.422	5.927	-0.484
Wind 180 deg - Service		-0.000	7.020	-0.948
Wind 210 deg - Service		-3.697	6.403	-1.238
Wind 240 deg - Service		-6.622	3.823	-0.848
Wind 270 deg - Service		-7.394	0.000	-0.231
Wind 300 deg - Service		-6.079	-3.510	0.318
Wind 330 deg - Service		-3.422	-5.927	0.484

## Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy
3	1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy
4	1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy

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	<p><b>Project</b></p> <p style="text-align: center;">Guyed Tower Structural Analysis</p>	<p><b>Date</b></p> <p style="text-align: center;">17:19:08 06/19/18</p>
	<p><b>Client</b></p> <p style="text-align: center;">Insite</p>	<p><b>Designed by</b></p> <p style="text-align: center;">Chunhui Song</p>

Comb. No.	Description
5	1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy
6	1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy
7	1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy
8	1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy
9	1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy
10	1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy
11	1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy
12	1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy
13	1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy
14	1.2 Dead+1.0 Ice+1.0 Temp+Guy
15	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy
16	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy
17	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy
18	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy
19	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy
20	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy
21	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy
22	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy
23	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy
24	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy
25	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy
26	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy
27	Dead+Wind 0 deg - Service+Guy
28	Dead+Wind 30 deg - Service+Guy
29	Dead+Wind 60 deg - Service+Guy
30	Dead+Wind 90 deg - Service+Guy
31	Dead+Wind 120 deg - Service+Guy
32	Dead+Wind 150 deg - Service+Guy
33	Dead+Wind 180 deg - Service+Guy
34	Dead+Wind 210 deg - Service+Guy
35	Dead+Wind 240 deg - Service+Guy
36	Dead+Wind 270 deg - Service+Guy
37	Dead+Wind 300 deg - Service+Guy
38	Dead+Wind 330 deg - Service+Guy

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Guy C @ 280 ft Elev 13 ft Azimuth 240 deg	Max. Vert	10	-2.156	-1.305	0.755
	Max. H <sub>x</sub>	10	-2.156	-1.305	0.755
	Max. H <sub>z</sub>	16	-10.266	-9.800	6.157
	Min. Vert	17	-10.655	-10.355	5.986
	Min. H <sub>x</sub>	17	-10.655	-10.355	5.986
	Min. H <sub>z</sub>	10	-2.156	-1.305	0.755
Guy B @ 280 ft Elev -13 ft Azimuth 120 deg	Max. Vert	6	-2.569	1.438	0.831
	Max. H <sub>x</sub>	25	-11.606	10.388	5.999
	Max. H <sub>z</sub>	26	-11.195	9.819	6.185
	Min. Vert	25	-11.606	10.388	5.999
	Min. H <sub>x</sub>	6	-2.569	1.438	0.831
	Min. H <sub>z</sub>	6	-2.569	1.438	0.831
Guy A @ 277 ft Elev 34 ft Azimuth 0 deg	Max. Vert	2	-1.864	0.001	-1.380



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	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Guy C @ 222 ft Elev 16 ft Azimuth 240 deg	Max. H <sub>x</sub>	24	-7.649	1.041	-8.923
	Max. H <sub>z</sub>	2	-1.864	0.001	-1.380
	Min. Vert	21	-10.092	0.004	-11.996
	Min. H <sub>x</sub>	18	-7.655	-1.032	-8.928
	Min. H <sub>z</sub>	21	-10.092	0.004	-11.996
	Max. Vert	10	-1.838	-1.121	0.649
	Guy B @ 224 ft Elev -17 ft Azimuth 120 deg	Max. H <sub>x</sub>	10	-1.838	-1.121
Max. H <sub>z</sub>		16	-17.468	-18.370	11.287
Min. Vert		4	-20.585	-18.901	10.905
Min. H <sub>x</sub>		17	-18.305	-19.423	11.228
Min. H <sub>z</sub>		10	-1.838	-1.121	0.649
Max. Vert		6	-2.722	1.528	0.883
Guy A @ 223 ft Elev 24 ft Azimuth 0 deg		Max. H <sub>x</sub>	25	-20.990	19.421
	Max. H <sub>z</sub>	26	-20.110	18.377	11.330
	Min. Vert	12	-22.690	18.331	10.583
	Min. H <sub>x</sub>	6	-2.722	1.528	0.883
	Min. H <sub>z</sub>	6	-2.722	1.528	0.883
	Max. Vert	2	-1.654	0.001	-1.206
	Guy C @ 166 ft Elev 8 ft Azimuth 240 deg	Max. H <sub>x</sub>	24	-12.297	1.469
Max. H <sub>z</sub>		2	-1.654	0.001	-1.206
Min. Vert		8	-19.605	-0.005	-21.635
Min. H <sub>x</sub>		18	-12.370	-1.451	-15.995
Min. H <sub>z</sub>		21	-17.358	0.009	-22.276
Max. Vert		10	-0.195	-0.217	0.125
Guy B @ 170 ft Elev -12 ft Azimuth 120 deg		Max. H <sub>x</sub>	10	-0.195	-0.217
	Max. H <sub>z</sub>	3	-8.325	-12.035	7.125
	Min. Vert	5	-8.424	-12.312	6.929
	Min. H <sub>x</sub>	5	-8.424	-12.312	6.929
	Min. H <sub>z</sub>	10	-0.195	-0.217	0.125
	Max. Vert	6	-0.345	0.299	0.173
	Guy A @ 169 ft Elev 15 ft Azimuth 0 deg	Max. H <sub>x</sub>	11	-9.858	12.319
Max. H <sub>z</sub>		11	-9.858	12.319	6.919
Min. Vert		11	-9.858	12.319	6.919
Min. H <sub>x</sub>		6	-0.345	0.299	0.173
Min. H <sub>z</sub>		6	-0.345	0.299	0.173
Max. Vert		2	-0.153	0.000	-0.244
Mast		Max. H <sub>x</sub>	24	-4.366	0.562
	Max. H <sub>z</sub>	2	-0.153	0.000	-0.244
	Min. Vert	9	-7.592	0.148	-13.939
	Min. H <sub>x</sub>	18	-4.400	-0.556	-10.028
	Min. H <sub>z</sub>	9	-7.592	0.148	-13.939
	Max. Vert	15	192.430	-0.025	-0.217
	Max. H <sub>x</sub>	11	92.297	1.024	0.107
	Max. H <sub>z</sub>	2	92.552	-0.032	1.128
	Max. M <sub>x</sub>	1	0.000	0.005	-0.001
	Max. M <sub>z</sub>	1	0.000	0.005	-0.001
	Max. Torsion	9	1.465	0.448	-1.072
	Min. Vert	1	54.109	0.005	-0.001
	Min. H <sub>x</sub>	5	90.522	-1.115	0.111

<p style="text-align: center;"><b>tnxTower</b></p> <p style="text-align: center;"><b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701</p>	<b>Job</b>	CT900 Wolcott	<b>Page</b>	42 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
	Min. H <sub>z</sub>	8	86.800	0.021	-1.151
	Min. M <sub>x</sub>	1	0.000	0.005	-0.001
	Min. M <sub>z</sub>	1	0.000	0.005	-0.001
	Min. Torsion	3	-1.472	-0.678	0.883

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	54.109	-0.005	0.001	0.000	0.000	-0.000
1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy	92.552	0.032	-1.128	0.000	0.000	1.153
1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy	90.953	0.678	-0.883	0.000	0.000	1.472
1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy	87.976	1.022	-0.607	0.000	0.000	0.852
1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy	90.522	1.115	-0.111	0.000	0.000	-0.009
1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy	90.896	1.032	0.619	0.000	0.000	-0.540
1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy	88.168	0.429	0.954	0.000	0.000	-0.593
1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy	86.800	-0.021	1.151	0.000	0.000	-1.150
1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy	90.107	-0.448	1.072	0.000	0.000	-1.465
1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy	93.446	-0.998	0.641	0.000	0.000	-0.853
1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy	92.297	-1.024	-0.107	0.000	0.000	-0.015
1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy	88.855	-0.915	-0.512	0.000	0.000	0.590
1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy	90.296	-0.548	-0.760	0.000	0.000	0.620
1.2 Dead+1.0 Ice+1.0 Temp+Guy	184.703	0.014	0.096	0.000	0.000	0.003
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy	192.430	0.025	0.217	0.000	0.000	0.435
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy	191.093	-0.014	0.194	0.000	0.000	0.559
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy	189.784	-0.036	0.146	0.000	0.000	0.254
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy	188.918	-0.031	0.118	0.000	0.000	-0.145
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy	188.631	-0.019	0.084	0.000	0.000	-0.226
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy	188.381	0.019	0.050	0.000	0.000	-0.218
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy	188.809	0.017	0.031	0.000	0.000	-0.405
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy	189.826	0.045	0.039	0.000	0.000	-0.560
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy	191.183	0.122	0.045	0.000	0.000	-0.293
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy	191.192	0.105	0.129	0.000	0.000	0.137

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	43 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy	191.332	0.106	0.158	0.000	0.000	0.241
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy	191.867	0.080	0.176	0.000	0.000	0.234
Dead+Wind 0 deg - Service+Guy	56.105	-0.002	-0.431	0.000	0.000	0.276
Dead+Wind 30 deg - Service+Guy	56.380	0.188	-0.343	0.000	0.000	0.349
Dead+Wind 60 deg - Service+Guy	56.642	0.314	-0.184	0.000	0.000	0.201
Dead+Wind 90 deg - Service+Guy	56.247	0.387	0.006	0.000	0.000	-0.002
Dead+Wind 120 deg - Service+Guy	55.881	0.366	0.217	0.000	0.000	-0.136
Dead+Wind 150 deg - Service+Guy	56.190	0.171	0.302	0.000	0.000	-0.152
Dead+Wind 180 deg - Service+Guy	56.525	-0.006	0.349	0.000	0.000	-0.276
Dead+Wind 210 deg - Service+Guy	56.235	-0.205	0.343	0.000	0.000	-0.348
Dead+Wind 240 deg - Service+Guy	55.942	-0.398	0.233	0.000	0.000	-0.199
Dead+Wind 270 deg - Service+Guy	56.231	-0.394	0.010	0.000	0.000	0.003
Dead+Wind 300 deg - Service+Guy	56.575	-0.298	-0.169	0.000	0.000	0.137
Dead+Wind 330 deg - Service+Guy	56.298	-0.169	-0.301	0.000	0.000	0.151

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.000	-20.403	0.000	-0.001	20.403	-0.001	0.007%
2	-0.052	-24.423	-36.746	0.051	24.423	36.742	0.009%
3	18.433	-23.922	-31.897	-18.435	23.921	31.891	0.016%
4	31.745	-23.412	-18.236	-31.749	23.412	18.231	0.014%
5	37.022	-23.784	0.026	-37.016	23.784	-0.019	0.020%
6	31.948	-24.174	18.413	-31.940	24.174	-18.408	0.022%
7	17.435	-23.741	30.117	-17.431	23.741	-30.117	0.009%
8	0.052	-23.334	35.426	-0.053	23.334	-35.427	0.004%
9	-18.433	-23.836	31.897	18.427	23.835	-31.896	0.012%
10	-32.888	-24.345	18.896	32.880	24.345	-18.892	0.020%
11	-37.022	-23.973	-0.026	37.018	23.973	0.030	0.015%
12	-30.806	-23.583	-17.753	30.814	23.583	17.744	0.029%
13	-17.435	-24.016	-30.117	17.435	24.016	30.114	0.009%
14	0.000	-109.680	0.000	0.000	109.680	-0.000	0.000%
15	-0.098	-110.526	-23.381	0.099	110.526	23.368	0.011%
16	11.704	-109.741	-20.220	-11.707	109.740	20.185	0.032%
17	20.521	-108.945	-11.677	-20.521	108.945	11.676	0.001%
18	23.703	-109.553	0.054	-23.700	109.553	-0.050	0.005%
19	20.490	-110.184	11.773	-20.485	110.184	-11.769	0.006%
20	11.688	-109.491	20.083	-11.684	109.491	-20.082	0.004%
21	0.098	-108.833	23.175	-0.097	108.833	-23.175	0.001%
22	-11.704	-109.619	20.220	11.685	109.618	-20.211	0.018%
23	-20.699	-110.415	11.781	20.669	110.414	-11.759	0.033%
24	-23.703	-109.807	-0.054	23.698	109.807	0.059	0.007%

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	44 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
25	-20.312	-109.175	-11.670	20.309	109.175	11.667	0.004%
26	-11.688	-109.868	-20.083	11.689	109.868	20.076	0.007%
27	-0.013	-20.542	-9.357	0.013	20.542	9.355	0.010%
28	4.694	-20.414	-8.122	-4.693	20.414	8.120	0.010%
29	8.084	-20.284	-4.644	-8.083	20.284	4.643	0.004%
30	9.427	-20.379	0.007	-9.426	20.379	-0.007	0.007%
31	8.135	-20.478	4.689	-8.133	20.478	-4.687	0.012%
32	4.440	-20.368	7.669	-4.439	20.368	-7.668	0.005%
33	0.013	-20.264	9.021	-0.014	20.264	-9.019	0.007%
34	-4.694	-20.392	8.122	4.692	20.392	-8.121	0.009%
35	-8.375	-20.522	4.812	8.372	20.522	-4.811	0.010%
36	-9.427	-20.427	-0.007	9.426	20.427	0.006	0.006%
37	-7.844	-20.328	-4.521	7.843	20.328	4.520	0.009%
38	-4.440	-20.438	-7.669	4.438	20.438	7.668	0.006%

## Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	12	0.00000001	0.00004231
2	Yes	24	0.00009336	0.00005096
3	Yes	23	0.00013635	0.00006349
4	Yes	18	0.00013726	0.00004400
5	Yes	21	0.00011886	0.00005482
6	Yes	21	0.00013632	0.00007203
7	Yes	21	0.00013384	0.00005715
8	Yes	18	0.00009788	0.00003575
9	Yes	23	0.00011266	0.00005183
10	Yes	23	0.00011503	0.00006586
11	Yes	23	0.00009761	0.00005362
12	Yes	16	0.00010644	0.00003672
13	Yes	23	0.00012975	0.00006760
14	Yes	24	0.00015000	0.00008858
15	Yes	22	0.00014795	0.00004426
16	Yes	18	0.00015000	0.00011156
17	Yes	19	0.00010144	0.00002003
18	Yes	22	0.00010502	0.00003104
19	Yes	22	0.00013828	0.00003779
20	Yes	21	0.00014208	0.00003124
21	Yes	19	0.00011050	0.00002343
22	Yes	18	0.00015000	0.00007402
23	Yes	19	0.00015000	0.00012087
24	Yes	21	0.00010667	0.00003146
25	Yes	19	0.00010241	0.00003048
26	Yes	21	0.00010610	0.00002938
27	Yes	12	0.00000001	0.00003790
28	Yes	12	0.00000001	0.00005215
29	Yes	13	0.00000001	0.00002357
30	Yes	12	0.00000001	0.00004216
31	Yes	11	0.00000001	0.00005361
32	Yes	12	0.00000001	0.00003640
33	Yes	12	0.00000001	0.00004262
34	Yes	12	0.00000001	0.00004475
35	Yes	12	0.00000001	0.00003803
36	Yes	13	0.00000001	0.00003324
37	Yes	13	0.00000001	0.00004854

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	45 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

38                      Yes                      13                      0.00000001                      0.00003313

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	347 - 327	2.498	37	0.0929	0.0513
T2	327 - 307	2.709	37	0.0974	0.0519
T3	307 - 287	2.885	37	0.0715	0.0597
T4	287 - 267	2.922	37	0.0453	0.0541
T5	267 - 247	2.923	37	0.0526	0.0481
T6	247 - 227	2.932	37	0.0312	0.0467
T7	227 - 207	2.811	37	0.0402	0.0442
T8	207 - 187	2.615	37	0.0403	0.0395
T9	187 - 167	2.488	37	0.0380	0.0470
T10	167 - 147	2.265	37	0.0681	0.0564
T11	147 - 127	1.933	37	0.0785	0.0569
T12	127 - 107	1.658	37	0.0408	0.0490
T13	107 - 87	1.554	36	0.0344	0.0659
T14	87 - 67	1.406	36	0.0502	0.0767
T15	67 - 62.97	1.177	36	0.0557	0.0762
T16	62.97 - 58.99	1.133	36	0.0562	0.0746
T17	58.99 - 55.01	1.089	36	0.0578	0.0727
T18	55.01 - 51.03	1.044	35	0.0603	0.0704
T19	51.03 - 47	0.998	35	0.0637	0.0676
T20	47 - 27	0.948	35	0.0678	0.0642
T21	27 - 7	0.621	35	0.0928	0.0420
T22	7 - 3	0.173	35	0.1134	0.0108
T23	3 - 0	0.074	35	0.1150	0.0035

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
347.000	5' Lightning Rod	37	2.498	0.0929	0.0513	275466
331.100	Guy	37	2.666	0.0986	0.0509	86737
300.000	Telewave ANT150F6-L	37	2.912	0.0593	0.0591	33300
271.100	Guy	37	2.921	0.0519	0.0489	64372
225.000	Beacon (10lbs 0.5CaAa)	37	2.792	0.0418	0.0436	50595
202.900	Guy	37	2.586	0.0382	0.0400	41849
201.000	Commscope NNVV-65B-R4	37	2.574	0.0373	0.0405	58363
131.100	Guy	37	1.701	0.0482	0.0490	23995
117.000	Beacon (10lbs 0.5CaAa)	36	1.590	0.0323	0.0556	75403
70.000	PCTEL GPS-TMG-HR-26NCM (.0006, .277CAAA)	36	1.211	0.0555	0.0771	75581
67.167	Guy	36	1.179	0.0557	0.0763	82007

### Maximum Tower Deflections - Design Wind



<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	46 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	347 - 327	16.335	12	0.4214	0.3420
T2	327 - 307	16.685	12	0.4291	0.3442
T3	307 - 287	17.035	11	0.3632	0.3716
T4	287 - 267	17.453	11	0.2996	0.3452
T5	267 - 247	17.877	10	0.2980	0.3196
T6	247 - 227	18.402	10	0.2392	0.3036
T7	227 - 207	18.265	10	0.2622	0.2805
T8	207 - 187	17.664	10	0.2563	0.2484
T9	187 - 167	17.194	10	0.2644	0.2733
T10	167 - 147	16.201	10	0.3945	0.3068
T11	147 - 127	14.603	10	0.4415	0.3036
T12	127 - 107	13.116	10	0.3004	0.2680
T13	107 - 87	12.182	10	0.2730	0.3238
T14	87 - 67	10.873	10	0.3807	0.3525
T15	67 - 62.97	9.027	10	0.4716	0.3365
T16	62.97 - 58.99	8.639	10	0.4856	0.3280
T17	58.99 - 55.01	8.242	10	0.4984	0.3185
T18	55.01 - 51.03	7.830	10	0.5153	0.3070
T19	51.03 - 47	7.401	10	0.5357	0.2942
T20	47 - 27	6.946	10	0.5592	0.2786
T21	27 - 7	4.333	10	0.6905	0.1803
T22	7 - 3	1.177	10	0.7820	0.0460
T23	3 - 0	0.504	10	0.7886	0.0149

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
347.000	5' Lightning Rod	12	16.335	0.4214	0.3420	10187
331.100	Guy	12	16.613	0.4349	0.3406	3205
300.000	Telewave ANT150F6-L	11	17.236	0.3350	0.3675	5309
271.100	Guy	10	17.747	0.3010	0.3236	7985
225.000	Beacon (10lbs 0.5CaAa)	10	18.214	0.2665	0.2768	9373
202.900	Guy	10	17.565	0.2485	0.2489	9687
201.000	Commscope NNVV-65B-R4	10	17.524	0.2474	0.2503	12965
131.100	Guy	10	13.370	0.3289	0.2694	5913
117.000	Beacon (10lbs 0.5CaAa)	10	12.629	0.2648	0.2896	16501
70.000	PCTEL GPS-TMG-HR-26NCM (.0006, .277CAAA)	10	9.315	0.4604	0.3417	9473
67.167	Guy	10	9.043	0.4710	0.3369	14096

### Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria	
T2	327	Leg	A325X	0.6250	3	0.371	20.709	0.018	✓	1	Bolt Tension
T3	307	Leg	A325X	0.6250	3	2.579	20.709	0.125	✓	1	Bolt Tension
T4	287	Leg	A325X	0.6250	3	2.353	20.709	0.114	✓	1	Bolt Tension

<p><b>tnxTower</b></p> <p><b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701</p>	<b>Job</b>	CT900 Wolcott	<b>Page</b>	47 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria	
T5	267	Leg	A325X	0.6250	3	2.133	20.709	0.103	✓	1	Bolt Tension
T6	247	Leg	A325X	0.6250	3	4.276	20.709	0.207	✓	1	Bolt Tension
T7	227	Leg	A325X	0.6250	3	3.983	20.709	0.192	✓	1	Bolt Tension
T8	207	Leg	A325X	0.6250	3	3.974	20.709	0.192	✓	1	Bolt Tension
T9	187	Leg	A325X	0.6250	3	5.474	20.709	0.264	✓	1	Bolt Tension
T10	167	Leg	A325X	0.6250	3	5.596	20.709	0.270	✓	1	Bolt Tension
T11	147	Leg	A325X	0.6250	3	5.564	20.709	0.269	✓	1	Bolt Tension
T12	127	Leg	A325X	0.6250	3	6.126	20.709	0.296	✓	1	Bolt Tension
T13	107	Leg	A325X	0.6250	3	6.660	20.709	0.322	✓	1	Bolt Tension
T14	87	Leg	A325X	0.6250	3	6.923	20.709	0.334	✓	1	Bolt Tension
T15	67	Leg	A325X	0.6250	3	7.074	20.709	0.342	✓	1	Bolt Tension
T20	47	Leg	A325X	0.6250	3	7.506	20.709	0.362	✓	1	Bolt Tension
T21	27	Leg	A325X	0.6250	3	7.615	20.709	0.368	✓	1	Bolt Tension
T22	7	Leg	A325X	0.6250	3	7.293	20.709	0.352	✓	1	Bolt Tension

### Guy Design Data

Section No.	Elevation ft	Size	Initial Tension K	Breaking Load K	Actual $T_u$ K	Allowable $\phi T_n$ K	Required S.F.	Actual S.F.
T1	331.100 (A) (919)	7/16 EHS	2.080	20.800	9.391	12.480	1.000	1.329 ✓
	331.100 (A) (920)	7/16 EHS	2.080	20.800	9.373	12.480	1.000	1.331 ✓
	331.100 (B) (913)	7/16 EHS	2.080	20.800	10.090	12.480	1.000	1.237 ✓
	331.100 (B) (914)	7/16 EHS	2.080	20.800	10.095	12.480	1.000	1.236 ✓
	331.100 (C) (907)	7/16 EHS	2.080	20.800	9.640	12.480	1.000	1.295 ✓
	331.100 (C) (908)	7/16 EHS	2.080	20.800	9.652	12.480	1.000	1.293 ✓
T4	271.100 (A) (937)	7/16 EHS	2.080	20.800	8.399	12.480	1.000	1.486 ✓
	271.100 (A) (938)	7/16 EHS	2.080	20.800	8.383	12.480	1.000	1.489 ✓
	271.100 (B) (931)	7/16 EHS	2.080	20.800	9.159	12.480	1.000	1.363 ✓
	271.100 (B) (932)	7/16 EHS	2.080	20.800	9.160	12.480	1.000	1.362 ✓
	271.100 (C) (925)	7/16 EHS	2.080	20.800	8.571	12.480	1.000	1.456 ✓
	271.100 (C) (926)	7/16 EHS	2.080	20.800	8.588	12.480	1.000	1.453 ✓
T8	202.900 (A) (955)	7/16 EHS	2.080	20.800	7.874	12.480	1.000	1.585 ✓
	202.900 (A)	7/16 EHS	2.080	20.800	7.862	12.480	1.000	1.587 ✓

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	48 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	Initial Tension K	Breaking Load K	Actual $T_u$ K	Allowable $\phi T_n$ K	Required S.F.	Actual S.F.
	(956)							
	202.900 (B) (949)	7/16 EHS	2.080	20.800	8.662	12.480	1.000	1.441 ✓
	202.900 (B) (950)	7/16 EHS	2.080	20.800	8.656	12.480	1.000	1.442 ✓
	202.900 (C) (943)	7/16 EHS	2.080	20.800	8.090	12.480	1.000	1.543 ✓
	202.900 (C) (944)	7/16 EHS	2.080	20.800	8.113	12.480	1.000	1.538 ✓
T11	131.100 (A) (973)	3/8 EHS	1.540	15.400	5.542	9.240	1.000	1.667 ✓
	131.100 (A) (974)	3/8 EHS	1.540	15.400	5.358	9.240	1.000	1.724 ✓
	131.100 (B) (967)	3/8 EHS	1.540	15.400	5.981	9.240	1.000	1.545 ✓
	131.100 (B) (968)	3/8 EHS	1.540	15.400	5.906	9.240	1.000	1.564 ✓
	131.100 (C) (961)	3/8 EHS	1.540	15.400	5.621	9.240	1.000	1.644 ✓
	131.100 (C) (962)	3/8 EHS	1.540	15.400	5.698	9.240	1.000	1.622 ✓
T14	67.167 (A) (984)	3/8 EHS	1.540	15.400	5.212	9.240	1.000	1.773 ✓
	67.167 (B) (983)	3/8 EHS	1.540	15.400	5.571	9.240	1.000	1.659 ✓
	67.167 (C) (979)	3/8 EHS	1.540	15.400	5.372	9.240	1.000	1.720 ✓

### Compression Checks

### Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	$L_u$ ft	$Kl/r$	A $in^2$	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T1	347 - 327	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-14.029	63.956	0.219 <sup>1</sup> ✓
T2	327 - 307	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-27.402	63.956	0.428 <sup>1</sup> ✓
T3	307 - 287	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-27.612	63.956	0.432 <sup>1</sup> ✓
T4	287 - 267	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-27.734	63.956	0.434 <sup>1</sup> ✓
T5	267 - 247	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-40.705	63.956	0.636 <sup>1</sup> ✓
T6	247 - 227	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-40.683	63.956	0.636 <sup>1</sup> ✓
T7	227 - 207	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-37.643	63.956	0.589 <sup>1</sup> ✓
T8	207 - 187	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-49.552	63.956	0.775 <sup>1</sup> ✓

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	49 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T9	187 - 167	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-50.778	63.956	0.794 <sup>1</sup> ✓
T10	167 - 147	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-50.652	63.956	0.792 <sup>1</sup> ✓
T11	147 - 127	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-57.221	63.956	0.895 <sup>1</sup> ✓
T12	127 - 107	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-59.842	63.956	0.936 <sup>1</sup> ✓
T13	107 - 87	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-62.332	63.956	0.975 <sup>1</sup> ✓
T14	87 - 67	P2.5 STD	20.000	3.933	49.8 K=1.00	1.7040	-62.491	63.956	0.977 <sup>1</sup> ✓
T15	67 - 62.97	P2.5 STD	4.030	3.863	48.9 K=1.00	1.7040	-64.370	64.367	1.000 <sup>1</sup> ✗
T16	62.97 - 58.99	4.8.1 (1.00 CR) - 716 P2.5 STD w/ SP HSS 3.5x.3	3.980	3.980	52.4 K=1.00	3.1100	-67.014	114.522	0.585 <sup>1</sup> ✓
T17	58.99 - 55.01	P2.5 STD w/ SP HSS 3.5x.3	3.980	3.980	52.4 K=1.00	3.1100	-67.674	114.522	0.591 <sup>1</sup> ✓
T18	55.01 - 51.03	P2.5 STD w/ SP HSS 3.5x.3	3.980	3.980	52.4 K=1.00	3.1100	-68.504	114.522	0.598 <sup>1</sup> ✓
T19	51.03 - 47	P2.5 STD w/ SP HSS 3.5x.3	4.030	3.863	50.8 K=1.00	3.1100	-69.533	115.856	0.600 <sup>1</sup> ✓
T20	47 - 27	P2.5 STD w/ SP HSS 3.5x.3	20.000	3.933	51.8 K=1.00	3.1100	-70.684	115.058	0.614 <sup>1</sup> ✓
T21	27 - 7	P2.5 STD w/ SP HSS 3.5x.3	20.000	3.933	51.8 K=1.00	3.1100	-70.467	115.058	0.612 <sup>1</sup> ✓
T22	7 - 3	P2.5 STD w/ SP HSS 3.5x.3	4.000	3.833	50.4 K=1.00	3.1100	-67.230	116.195	0.579 <sup>1</sup> ✓
T23	3 - 0	P2.5 STD w/ SP HSS 3.5x.3	3.000	2.833	37.3 K=1.00	3.1100	-68.844	126.427	0.545 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	347 - 327	L2x2x1/4	3.000	2.760	102.4 K=1.21	0.9380	-10.657	17.506	0.609 <sup>1</sup> ✓
T2	327 - 307	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-5.217	10.466	0.499 <sup>1</sup> ✓
T3	307 - 287	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-4.790	10.466	0.458 <sup>1</sup> ✓
T4	287 - 267	L2x2x1/4	3.000	2.760	102.4 K=1.21	0.9380	-10.434	17.506	0.596 <sup>1</sup> ✓
T5	267 - 247	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-4.475	10.466	0.428 <sup>1</sup> ✓

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	50 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T6	247 - 227	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-4.021	10.466	0.384 <sup>1</sup> ✓
T7	227 - 207	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-3.722	10.466	0.356 <sup>1</sup> ✓
T8	207 - 187	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-8.622	10.466	0.824 <sup>1</sup> ✓
T9	187 - 167	L2x1 1/2x1/4	3.000	2.760	111.8 K=1.08	0.8125	-4.465	13.629	0.328 <sup>1</sup> ✓
T10	167 - 147	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-3.157	10.466	0.302 <sup>1</sup> ✓
T11	147 - 127	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-8.555	10.466	0.817 <sup>1</sup> ✓
T12	127 - 107	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-3.281	10.466	0.314 <sup>1</sup> ✓
T13	107 - 87	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.662	10.466	0.254 <sup>1</sup> ✓
T14	87 - 67	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.567	10.466	0.245 <sup>1</sup> ✓
T20	47 - 27	L2x1 1/2x3/16	3.000	2.708	110.5 K=1.09	0.6211	-4.053	10.585	0.383 <sup>1</sup> ✓
T21	27 - 7	L2x1 1/2x3/16	3.000	2.708	110.5 K=1.09	0.6211	-3.985	10.585	0.377 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	347 - 327	L2x2x1/4	3.000	2.760	102.4 K=1.21	0.9380	-4.293	17.506	0.245 <sup>1</sup> ✓
T2	327 - 307	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.600	10.466	0.248 <sup>1</sup> ✓
T3	307 - 287	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.475	10.466	0.236 <sup>1</sup> ✓
T4	287 - 267	L2x2x1/4	3.000	2.760	102.4 K=1.21	0.9380	-3.898	17.506	0.223 <sup>1</sup> ✓
T5	267 - 247	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.282	10.466	0.218 <sup>1</sup> ✓
T6	247 - 227	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.065	10.466	0.197 <sup>1</sup> ✓
T7	227 - 207	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.031	10.466	0.194 <sup>1</sup> ✓
T8	207 - 187	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-1.873	10.466	0.179 <sup>1</sup> ✓
T9	187 - 167	L2x1 1/2x1/4	3.000	2.760	111.8 K=1.08	0.8125	-2.190	13.629	0.161 <sup>1</sup> ✓
T10	167 - 147	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-1.736	10.466	0.166 <sup>1</sup> ✓



<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	51 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T11	147 - 127	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-1.505	10.466	0.144 <sup>1</sup> ✓
T12	127 - 107	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-1.725	10.466	0.165 <sup>1</sup> ✓
T13	107 - 87	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-1.301	10.466	0.124 <sup>*1</sup> ✓
T14	87 - 67	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-1.381	10.466	0.132 <sup>1</sup> ✓
T15	67 - 62.97	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-1.060	10.466	0.101 <sup>*1</sup> ✓
T16	62.97 - 58.99	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-3.057	10.466	0.292 <sup>1</sup> ✓
T17	58.99 - 55.01	L2x1 1/2x3/16	3.000	2.708	110.5 K=1.09	0.6211	-3.709	10.585	0.350 <sup>1</sup> ✓
T18	55.01 - 51.03	L2x1 1/2x3/16	3.000	2.708	110.5 K=1.09	0.6211	-3.752	10.585	0.354 <sup>1</sup> ✓
T19	51.03 - 47	L2x1 1/2x3/16	3.000	2.708	110.5 K=1.09	0.6211	-3.973	10.585	0.375 <sup>1</sup> ✓
T20	47 - 27	L2x1 1/2x3/16	3.000	2.708	110.5 K=1.09	0.6211	-2.007	10.585	0.190 <sup>1</sup> ✓
T21	27 - 7	L2x1 1/2x3/16	3.000	2.708	110.5 K=1.09	0.6211	-2.107	10.585	0.199 <sup>1</sup> ✓
T22	7 - 3	L2x1 1/2x3/16	3.000	2.708	110.5 K=1.09	0.6211	-2.131	10.585	0.201 <sup>1</sup> ✓
T23	3 - 0	L2x1 1/2x3/16	3.000	2.708	110.5 K=1.09	0.6211	-5.060	10.585	0.478 <sup>1</sup> ✓

\* DL controls

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Bottom Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	347 - 327	L2x2x1/4	3.000	2.760	102.4 K=1.21	0.9380	-4.637	17.506	0.265 <sup>1</sup> ✓
T2	327 - 307	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.453	10.466	0.234 <sup>1</sup> ✓
T3	307 - 287	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.284	10.466	0.218 <sup>1</sup> ✓
T4	287 - 267	L2x2x1/4	3.000	2.760	102.4 K=1.21	0.9380	-3.903	17.506	0.223 <sup>1</sup> ✓
T5	267 - 247	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-2.072	10.466	0.198 <sup>1</sup> ✓
T6	247 - 227	L2x1 1/2x3/16	3.000	2.760	111.4 K=1.08	0.6211	-1.897	10.466	0.181 <sup>1</sup> ✓
T7	227 - 207	L2x1 1/2x3/16	3.000	2.760	111.4	0.6211	-1.968	10.466	0.188 <sup>1</sup> ✓

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	52 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	KL/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T8	207 - 187	L2x1 1/2x3/16	3.000	2.760	K=1.08 111.4	0.6211	-1.759	10.466	0.168 <sup>1</sup> ✓
T9	187 - 167	L2x1 1/2x1/4	3.000	2.760	K=1.08 111.8	0.8125	-2.178	13.629	0.160 <sup>1</sup> ✓
T10	167 - 147	L2x1 1/2x3/16	3.000	2.760	K=1.08 111.4	0.6211	-1.578	10.466	0.151 <sup>1</sup> ✓
T11	147 - 127	L2x1 1/2x3/16	3.000	2.760	K=1.08 111.4	0.6211	-1.451	10.466	0.139 <sup>1</sup> ✓
T12	127 - 107	L2x1 1/2x3/16	3.000	2.760	K=1.08 111.4	0.6211	-1.385	10.466	0.132 <sup>1</sup> ✓
T13	107 - 87	L2x1 1/2x3/16	3.000	2.760	K=1.08 111.4	0.6211	-1.313	10.466	0.125 <sup>1</sup> ✓
T14	87 - 67	L2x1 1/2x3/16	3.000	2.760	K=1.08 111.4	0.6211	-0.400	10.466	0.038 <sup>1</sup> ✓
T19	51.03 - 47	L2x1 1/2x3/16	3.000	2.708	K=1.09 110.5	0.6211	-2.177	10.585	0.206 <sup>1</sup> ✓
T20	47 - 27	L2x1 1/2x3/16	3.000	2.708	K=1.09 110.5	0.6211	-2.039	10.585	0.193 <sup>1</sup> ✓
T21	27 - 7	L2x1 1/2x3/16	3.000	2.708	K=1.09 110.5	0.6211	-1.813	10.585	0.171 <sup>1</sup> ✓
T23	3 - 0	L2x1 1/2x3/16	3.000	2.708	K=1.09 110.5	0.6211	-0.423	10.585	0.040 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Top Guy Pull-Off Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	KL/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T14	87 - 67	3x3/8	3.000	2.760	K=1.00 306.0	1.1250	-0.725	2.714	0.267 <sup>1</sup> ✓
KL/R > 200 (C) - 981									

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Torque-Arm Top Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	KL/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T4	287 - 267 (927)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-0.213	34.278	0.006 <sup>1</sup> ✓
T4	287 - 267 (928)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-0.227	34.278	0.007 <sup>1</sup> ✓
T4	287 - 267 (934)	L3x3x5/16	4.999	4.879	99.4	1.7800	-0.102	34.278	0.003 <sup>1</sup> ✓

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	53 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T4	287 - 267 (940)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-0.019	34.278	0.001 <sup>1</sup> ✓
T8	207 - 187 (945)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-1.744	34.278	0.051 <sup>1</sup> ✓
T8	207 - 187 (946)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-1.859	34.278	0.054 <sup>1</sup> ✓
T8	207 - 187 (951)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-1.296	34.278	0.038 <sup>1</sup> ✓
T8	207 - 187 (952)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-1.600	34.278	0.047 <sup>1</sup> ✓
T8	207 - 187 (957)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-1.155	34.278	0.034 <sup>1</sup> ✓
T8	207 - 187 (958)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-1.486	34.278	0.043 <sup>1</sup> ✓
T11	147 - 127 (963)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-2.567	34.278	0.075 <sup>1</sup> ✓
T11	147 - 127 (964)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-2.671	34.278	0.078 <sup>1</sup> ✓
T11	147 - 127 (969)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-2.452	34.278	0.072 <sup>1</sup> ✓
T11	147 - 127 (970)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-2.529	34.278	0.074 <sup>1</sup> ✓
T11	147 - 127 (975)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-2.184	34.278	0.064 <sup>1</sup> ✓
T11	147 - 127 (976)	L3x3x5/16	4.999	4.879	K=1.00 99.4	1.7800	-2.308	34.278	0.067 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Torque-Arm Bottom Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	347 - 327 (911)	L3x3x5/16	9.604	9.374	K=1.00 191.0	1.7800	-9.559	11.026	0.867 <sup>1</sup> ✓
T1	347 - 327 (912)	L3x3x5/16	9.604	9.374	K=1.00 191.0	1.7800	-9.040	11.026	0.820 <sup>1</sup> ✓
T1	347 - 327 (917)	L3x3x5/16	9.604	9.374	K=1.00 191.0	1.7800	-9.921	11.026	0.900 <sup>1</sup> ✓
T1	347 - 327 (918)	L3x3x5/16	9.604	9.374	K=1.00 191.0	1.7800	-9.753	11.026	0.885 <sup>1</sup> ✓
T1	347 - 327 (923)	L3x3x5/16	9.604	9.374	K=1.00 191.0	1.7800	-10.009	11.026	0.908 <sup>1</sup> ✓
T1	347 - 327 (924)	L3x3x5/16	9.604	9.374	K=1.00 191.0	1.7800	-9.320	11.026	0.845 <sup>1</sup> ✓
T4	287 - 267 (929)	L3x3x5/16	9.604	9.374	K=1.00 191.0	1.7800	-8.295	11.026	0.752 <sup>1</sup> ✓

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	54 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T4	287 - 267 (930)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-8.220	11.026	0.746 <sup>1</sup>
T4	287 - 267 (935)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-9.201	11.026	0.834 <sup>1</sup>
T4	287 - 267 (936)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-8.408	11.026	0.763 <sup>1</sup>
T4	287 - 267 (941)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-9.119	11.026	0.827 <sup>1</sup>
T4	287 - 267 (942)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-8.249	11.026	0.748 <sup>1</sup>
T8	207 - 187 (947)	L3x3x5/16	9.321	9.097	185.3 K=1.00	1.7800	-7.446	11.706	0.636 <sup>1</sup>
T8	207 - 187 (948)	L3x3x5/16	9.321	9.097	185.3 K=1.00	1.7800	-7.174	11.706	0.613 <sup>1</sup>
T8	207 - 187 (953)	L3x3x5/16	9.321	9.097	185.3 K=1.00	1.7800	-8.465	11.706	0.723 <sup>1</sup>
T8	207 - 187 (954)	L3x3x5/16	9.321	9.097	185.3 K=1.00	1.7800	-7.773	11.706	0.664 <sup>1</sup>
T8	207 - 187 (959)	L3x3x5/16	9.321	9.097	185.3 K=1.00	1.7800	-8.040	11.706	0.687 <sup>1</sup>
T8	207 - 187 (960)	L3x3x5/16	9.321	9.097	185.3 K=1.00	1.7800	-7.187	11.706	0.614 <sup>1</sup>
T11	147 - 127 (965)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-5.194	11.026	0.471 <sup>1</sup>
T11	147 - 127 (966)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-4.786	11.026	0.434 <sup>1</sup>
T11	147 - 127 (971)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-5.521	11.026	0.501 <sup>1</sup>
T11	147 - 127 (972)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-5.242	11.026	0.475 <sup>1</sup>
T11	147 - 127 (977)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-5.498	11.026	0.499 <sup>1</sup>
T11	147 - 127 (978)	L3x3x5/16	9.604	9.374	191.0 K=1.00	1.7800	-4.822	11.026	0.437 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	347 - 327	P2.5 STD	20.000	0.167	2.1	1.7040	0.755	76.682	0.010 <sup>1</sup>
T2	327 - 307	P2.5 STD	20.000	0.167	2.1	1.7040	5.079	76.682	0.066 <sup>1</sup>

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	55 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T3	307 - 287	P2.5 STD	20.000	0.167	2.1	1.7040	5.078	76.682	0.066 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	347 - 327	7/8	4.947	4.552	249.7	0.6013	8.685	19.483	0.446 <sup>1</sup> ✓
T2	327 - 307	5/8	4.947	4.552	349.6	0.3068	4.990	9.940	0.502 <sup>1</sup> ✓
T3	307 - 287	5/8	4.947	4.552	349.6	0.3068	4.464	9.940	0.449 <sup>1</sup> ✓
T4	287 - 267	7/8	4.947	4.552	249.7	0.6013	8.053	19.483	0.413 <sup>1</sup> ✓
T5	267 - 247	5/8	4.947	4.552	349.6	0.3068	4.740	9.940	0.477 <sup>1</sup> ✓
T6	247 - 227	5/8	4.947	4.552	349.6	0.3068	3.707	9.940	0.373 <sup>1</sup> ✓
T7	227 - 207	5/8	4.947	4.552	349.6	0.3068	4.343	9.940	0.437 <sup>1</sup> ✓
T8	207 - 187	5/8	4.947	4.552	349.6	0.3068	5.301	9.940	0.533 <sup>1</sup> ✓
T9	187 - 167	3/4	4.947	4.552	291.3	0.4418	4.001	14.314	0.280 <sup>1</sup> ✓
T10	167 - 147	5/8	4.947	4.552	349.6	0.3068	3.589	9.940	0.361 <sup>1</sup> ✓
T11	147 - 127	5/8	4.947	4.552	349.6	0.3068	4.512	9.940	0.454 <sup>1</sup> ✓
T12	127 - 107	5/8	4.947	4.552	349.6	0.3068	3.879	9.940	0.390 <sup>1</sup> ✓
T13	107 - 87	5/8	4.947	4.552	349.6	0.3068	2.554	9.940	0.257 <sup>1</sup> ✓
T14	87 - 67	5/8	4.947	4.552	349.6	0.3068	2.738	9.940	0.275 <sup>1</sup> ✓
T15	67 - 62.97	5/8	4.891	4.501	345.7	0.3068	3.209	9.940	0.323 <sup>1</sup> ✓
T16	62.97 - 58.99	5/8	4.984	4.543	348.9	0.3068	4.146	9.940	0.417 <sup>1</sup> ✓
T17	58.99 - 55.01	5/8	4.984	4.499	345.6	0.3068	3.977	9.940	0.400 <sup>1</sup> ✓
T18	55.01 - 51.03	5/8	4.984	4.499	345.6	0.3068	3.808	9.940	0.383 <sup>1</sup> ✓
T19	51.03 - 47	5/8	4.891	4.416	339.1	0.3068	3.946	9.940	0.397 <sup>1</sup> ✓
T20	47 - 27	5/8	4.947	4.466	343.0	0.3068	3.850	9.940	0.387 <sup>1</sup> ✓



<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	56 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T21	27 - 7	5/8	4.947	4.466	343.0	0.3068	4.345	9.940	0.437 <sup>1</sup> ✓
T22	7 - 3	5/8	4.868	4.394	337.5	0.3068	4.380	9.940	0.441 <sup>1</sup> ✓
T23	3 - 0	5/8	4.126	3.725	286.1	0.3068	5.454	9.940	0.549 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	347 - 327	L2x2x1/4	3.000	2.760	54.4	0.9380	0.243	30.391	0.008 <sup>1</sup> ✓
T2	327 - 307	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.475	20.123	0.024 <sup>1</sup> ✓
T3	307 - 287	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.478	20.123	0.024 <sup>1</sup> ✓
T4	287 - 267	L2x2x1/4	3.000	2.760	54.4	0.9380	0.480	30.391	0.016 <sup>1</sup> ✓
T5	267 - 247	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.705	20.123	0.035 <sup>1</sup> ✓
T6	247 - 227	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.705	20.123	0.035 <sup>1</sup> ✓
T7	227 - 207	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.652	20.123	0.032 <sup>1</sup> ✓
T8	207 - 187	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	3.628	20.123	0.180 <sup>1</sup> ✓
T9	187 - 167	L2x1 1/2x1/4	3.000	2.760	76.7	0.8125	0.879	26.325	0.033 <sup>1</sup> ✓
T10	167 - 147	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.877	20.123	0.044 <sup>1</sup> ✓
T11	147 - 127	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	4.002	20.123	0.199 <sup>1</sup> ✓
T12	127 - 107	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	1.036	20.123	0.052 <sup>1</sup> ✓
T13	107 - 87	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	1.080	20.123	0.054 <sup>1</sup> ✓
T14	87 - 67	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	1.082	20.123	0.054 <sup>1</sup> ✓
T20	47 - 27	L2x1 1/2x3/16	3.000	2.708	73.9	0.6211	1.224	20.123	0.061 <sup>1</sup> ✓
T21	27 - 7	L2x1 1/2x3/16	3.000	2.708	73.9	0.6211	1.221	20.123	0.061 <sup>1</sup> ✓

<p><b>tnxTower</b></p> <p><b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701</p>	<p><b>Job</b></p> <p>CT900 Wolcott</p>	<p><b>Page</b></p> <p>57 of 62</p>
	<p><b>Project</b></p> <p>Guyed Tower Structural Analysis</p>	<p><b>Date</b></p> <p>17:19:08 06/19/18</p>
	<p><b>Client</b></p> <p>Insite</p>	<p><b>Designed by</b></p> <p>Chunhui Song</p>

<sup>1</sup>  $P_u / \phi P_n$  controls

**Top Girt Design Data (Tension)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T10	167 - 147	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.029	20.123	0.001 <sup>1</sup>
T11	147 - 127	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.058	20.123	0.003 <sup>1</sup>
T12	127 - 107	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.071	20.123	0.004 <sup>1</sup>
T13	107 - 87	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.019	20.123	0.001 <sup>1</sup>
T14	87 - 67	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.029	20.123	0.001 <sup>1</sup>
T15	67 - 62.97	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.137	20.123	0.007 <sup>1</sup>

<sup>1</sup>  $P_u / \phi P_n$  controls

**Bottom Girt Design Data (Tension)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T8	207 - 187	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.002	20.123	0.000 <sup>1</sup>
T10	167 - 147	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.080	20.123	0.004 <sup>1</sup>
T11	147 - 127	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.028	20.123	0.001 <sup>1</sup>
T12	127 - 107	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.039	20.123	0.002 <sup>1</sup>
T13	107 - 87	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.008	20.123	0.000 <sup>1</sup>
T14	87 - 67	L2x1 1/2x3/16	3.000	2.760	75.4	0.6211	0.897	20.123	0.045 <sup>1</sup>
T23	3 - 0	L2x1 1/2x3/16	3.000	2.708	73.9	0.6211	0.374	20.123	0.019 <sup>1</sup>

<sup>1</sup>  $P_u / \phi P_n$  controls

**Top Guy Pull-Off Design Data (Tension)**

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	58 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T14	87 - 67	3x3/8	3.000	2.760	306.0	1.1250	1.624	36.450	0.045 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Torque-Arm Top Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	347 - 327 (909)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.607	57.672	0.132 <sup>1</sup> ✓
T1	347 - 327 (910)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.318	57.672	0.127 <sup>1</sup> ✓
T1	347 - 327 (915)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.627	57.672	0.132 <sup>1</sup> ✓
T1	347 - 327 (916)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.601	57.672	0.132 <sup>1</sup> ✓
T1	347 - 327 (921)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.723	57.672	0.134 <sup>1</sup> ✓
T1	347 - 327 (922)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.423	57.672	0.129 <sup>1</sup> ✓
T4	287 - 267 (927)	L3x3x5/16	4.999	4.879	63.5	1.7800	6.926	57.672	0.120 <sup>1</sup> ✓
T4	287 - 267 (928)	L3x3x5/16	4.999	4.879	63.5	1.7800	6.952	57.672	0.121 <sup>1</sup> ✓
T4	287 - 267 (933)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.258	57.672	0.126 <sup>1</sup> ✓
T4	287 - 267 (934)	L3x3x5/16	4.999	4.879	63.5	1.7800	6.952	57.672	0.121 <sup>1</sup> ✓
T4	287 - 267 (939)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.202	57.672	0.125 <sup>1</sup> ✓
T4	287 - 267 (940)	L3x3x5/16	4.999	4.879	63.5	1.7800	6.923	57.672	0.120 <sup>1</sup> ✓
T8	207 - 187 (945)	L3x3x5/16	4.999	4.879	63.5	1.7800	8.422	57.672	0.146 <sup>1</sup> ✓
T8	207 - 187 (946)	L3x3x5/16	4.999	4.879	63.5	1.7800	8.381	57.672	0.145 <sup>1</sup> ✓
T8	207 - 187 (951)	L3x3x5/16	4.999	4.879	63.5	1.7800	8.656	57.672	0.150 <sup>1</sup> ✓
T8	207 - 187 (952)	L3x3x5/16	4.999	4.879	63.5	1.7800	8.522	57.672	0.148 <sup>1</sup> ✓
T8	207 - 187 (957)	L3x3x5/16	4.999	4.879	63.5	1.7800	8.260	57.672	0.143 <sup>1</sup> ✓
T8	207 - 187 (958)	L3x3x5/16	4.999	4.879	63.5	1.7800	8.042	57.672	0.139 <sup>1</sup> ✓
T11	147 - 127 (963)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.104	57.672	0.123 <sup>1</sup> ✓
T11	147 - 127 (964)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.110	57.672	0.123 <sup>1</sup> ✓

<b>tnxTower</b>  <b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701	<b>Job</b>	CT900 Wolcott	<b>Page</b>	59 of 62
	<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
	<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T11	147 - 127 (969)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.309	57.672	0.127 <sup>1</sup> ✓
T11	147 - 127 (970)	L3x3x5/16	4.999	4.879	63.5	1.7800	7.424	57.672	0.129 <sup>1</sup> ✓
T11	147 - 127 (975)	L3x3x5/16	4.999	4.879	63.5	1.7800	6.544	57.672	0.113 <sup>1</sup> ✓
T11	147 - 127 (976)	L3x3x5/16	4.999	4.879	63.5	1.7800	6.645	57.672	0.115 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Torque-Arm Bottom Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T8	207 - 187 (947)	L3x3x5/16	9.321	9.097	118.4	1.7800	1.139	57.672	0.020 <sup>1</sup> ✓
T8	207 - 187 (948)	L3x3x5/16	9.321	9.097	118.4	1.7800	1.072	57.672	0.019 <sup>1</sup> ✓
T8	207 - 187 (953)	L3x3x5/16	9.321	9.097	118.4	1.7800	0.777	57.672	0.013 <sup>1</sup> ✓
T8	207 - 187 (954)	L3x3x5/16	9.321	9.097	118.4	1.7800	1.117	57.672	0.019 <sup>1</sup> ✓
T8	207 - 187 (959)	L3x3x5/16	9.321	9.097	118.4	1.7800	0.966	57.672	0.017 <sup>1</sup> ✓
T8	207 - 187 (960)	L3x3x5/16	9.321	9.097	118.4	1.7800	1.177	57.672	0.020 <sup>1</sup> ✓
T11	147 - 127 (965)	L3x3x5/16	9.604	9.374	122.0	1.7800	0.140	57.672	0.002 <sup>1</sup> ✓
T11	147 - 127 (972)	L3x3x5/16	9.604	9.374	122.0	1.7800	0.095	57.672	0.002 <sup>1</sup> ✓
T11	147 - 127 (977)	L3x3x5/16	9.604	9.374	122.0	1.7800	0.008	57.672	0.000 <sup>1</sup> ✓
T11	147 - 127 (978)	L3x3x5/16	9.604	9.374	122.0	1.7800	0.042	57.672	0.001 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	φP <sub>allow</sub> K	% Capacity	Pass Fail
T1	347 - 327	Leg	P2.5 STD	1	-14.029	63.956	21.9	Pass
T2	327 - 307	Leg	P2.5 STD	53	-27.402	63.956	42.8	Pass
T3	307 - 287	Leg	P2.5 STD	104	-27.612	63.956	43.2	Pass

<b>Job</b>	CT900 Wolcott	<b>Page</b>	60 of 62
<b>Project</b>	Guyed Tower Structural Analysis	<b>Date</b>	17:19:08 06/19/18
<b>Client</b>	Insite	<b>Designed by</b>	Chunhui Song

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail
T4	287 - 267	Leg	P2.5 STD	155	-27.734	63.956	43.4	Pass
T5	267 - 247	Leg	P2.5 STD	206	-40.705	63.956	63.6	Pass
T6	247 - 227	Leg	P2.5 STD	257	-40.683	63.956	63.6	Pass
T7	227 - 207	Leg	P2.5 STD	308	-37.643	63.956	58.9	Pass
T8	207 - 187	Leg	P2.5 STD	359	-49.552	63.956	77.5	Pass
T9	187 - 167	Leg	P2.5 STD	409	-50.778	63.956	79.4	Pass
T10	167 - 147	Leg	P2.5 STD	460	-50.652	63.956	79.2	Pass
T11	147 - 127	Leg	P2.5 STD	511	-57.221	63.956	89.5	Pass
T12	127 - 107	Leg	P2.5 STD	562	-59.842	63.956	93.6	Pass
T13	107 - 87	Leg	P2.5 STD	614	-62.332	63.956	97.5	Pass
T14	87 - 67	Leg	P2.5 STD	665	-62.491	63.956	97.7	Pass
T15	67 - 62.97	Leg	P2.5 STD	716	-64.370	64.367	100.0	Pass
T16	62.97 - 58.99	Leg	P2.5 STD w/ SP HSS 3.5x.3	728	-67.014	114.522	58.5	Pass
T17	58.99 - 55.01	Leg	P2.5 STD w/ SP HSS 3.5x.3	740	-67.674	114.522	59.1	Pass
T18	55.01 - 51.03	Leg	P2.5 STD w/ SP HSS 3.5x.3	752	-68.504	114.522	59.8	Pass
T19	51.03 - 47	Leg	P2.5 STD w/ SP HSS 3.5x.3	764	-69.533	115.856	60.0	Pass
T20	47 - 27	Leg	P2.5 STD w/ SP HSS 3.5x.3	779	-70.684	115.058	61.4	Pass
T21	27 - 7	Leg	P2.5 STD w/ SP HSS 3.5x.3	830	-70.467	115.058	61.2	Pass
T22	7 - 3	Leg	P2.5 STD w/ SP HSS 3.5x.3	881	-67.230	116.195	57.9	Pass
T23	3 - 0	Leg	P2.5 STD w/ SP HSS 3.5x.3	893	-68.844	126.427	54.5	Pass
T1	347 - 327	Diagonal	7/8	13	8.685	19.483	44.6	Pass
T2	327 - 307	Diagonal	5/8	100	4.990	9.940	50.2	Pass
T3	307 - 287	Diagonal	5/8	113	4.464	9.940	44.9	Pass
T4	287 - 267	Diagonal	7/8	167	8.053	19.483	41.3	Pass
T5	267 - 247	Diagonal	5/8	254	4.740	9.940	47.7	Pass
T6	247 - 227	Diagonal	5/8	267	3.707	9.940	37.3	Pass
T7	227 - 207	Diagonal	5/8	318	4.343	9.940	43.7	Pass
T8	207 - 187	Diagonal	5/8	394	5.301	9.940	53.3	Pass
T9	187 - 167	Diagonal	3/4	457	4.001	14.314	28.0	Pass
T10	167 - 147	Diagonal	5/8	470	3.589	9.940	36.1	Pass
T11	147 - 127	Diagonal	5/8	520	4.512	9.940	45.4	Pass
T12	127 - 107	Diagonal	5/8	607	3.879	9.940	39.0	Pass
T13	107 - 87	Diagonal	5/8	661	2.554	9.940	25.7	Pass
T14	87 - 67	Diagonal	5/8	673	2.738	9.940	27.5	Pass
T15	67 - 62.97	Diagonal	5/8	726	3.209	9.940	32.3	Pass
T16	62.97 - 58.99	Diagonal	5/8	738	4.146	9.940	41.7	Pass
T17	58.99 - 55.01	Diagonal	5/8	750	3.977	9.940	40.0	Pass
T18	55.01 - 51.03	Diagonal	5/8	762	3.808	9.940	38.3	Pass
T19	51.03 - 47	Diagonal	5/8	777	3.946	9.940	39.7	Pass
T20	47 - 27	Diagonal	5/8	788	3.850	9.940	38.7	Pass
T21	27 - 7	Diagonal	5/8	840	4.345	9.940	43.7	Pass
T22	7 - 3	Diagonal	5/8	888	4.380	9.940	44.1	Pass
T23	3 - 0	Diagonal	5/8	903	5.454	9.940	54.9	Pass
T1	347 - 327	Horizontal	L2x2x1/4	16	-10.657	17.506	60.9	Pass
T2	327 - 307	Horizontal	L2x1 1/2x3/16	96	-5.217	10.466	49.9	Pass
T3	307 - 287	Horizontal	L2x1 1/2x3/16	147	-4.790	10.466	45.8	Pass
T4	287 - 267	Horizontal	L2x2x1/4	170	-10.434	17.506	59.6	Pass
T5	267 - 247	Horizontal	L2x1 1/2x3/16	249	-4.475	10.466	42.8	Pass
T6	247 - 227	Horizontal	L2x1 1/2x3/16	300	-4.021	10.466	38.4	Pass
T7	227 - 207	Horizontal	L2x1 1/2x3/16	351	-3.722	10.466	35.6	Pass
T8	207 - 187	Horizontal	L2x1 1/2x3/16	401	-8.622	10.466	82.4	Pass
T9	187 - 167	Horizontal	L2x1 1/2x1/4	452	-4.465	13.629	32.8	Pass
T10	167 - 147	Horizontal	L2x1 1/2x3/16	503	-3.157	10.466	30.2	Pass
T11	147 - 127	Horizontal	L2x1 1/2x3/16	527	-8.555	10.466	81.7	Pass
T12	127 - 107	Horizontal	L2x1 1/2x3/16	605	-3.281	10.466	31.4	Pass
T13	107 - 87	Horizontal	L2x1 1/2x3/16	629	-2.662	10.466	25.4	Pass
T14	87 - 67	Horizontal	L2x1 1/2x3/16	707	-2.567	10.466	24.5	Pass
T20	47 - 27	Horizontal	L2x1 1/2x3/16	794	-4.053	10.585	38.3	Pass
T21	27 - 7	Horizontal	L2x1 1/2x3/16	872	-3.985	10.585	37.7	Pass
T1	347 - 327	Top Girt	L2x2x1/4	5	-4.293	17.506	24.5	Pass
T2	327 - 307	Top Girt	L2x1 1/2x3/16	55	-2.600	10.466	24.8	Pass

<p><b>tnxTower</b></p> <p><b>Bennett and Pless</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: 678.990.8700 FAX: 678.990.8701</p>	<p><b>Job</b></p> <p>CT900 Wolcott</p>	<p><b>Page</b></p> <p>61 of 62</p>
	<p><b>Project</b></p> <p>Guyed Tower Structural Analysis</p>	<p><b>Date</b></p> <p>17:19:08 06/19/18</p>
	<p><b>Client</b></p> <p>Insite</p>	<p><b>Designed by</b></p> <p>Chunhui Song</p>

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail
T3	307 - 287	Top Girt	L2x1 1/2x3/16	108	-2.475	10.466	23.6	Pass
T4	287 - 267	Top Girt	L2x2x1/4	159	-3.898	17.506	22.3	Pass
T5	267 - 247	Top Girt	L2x1 1/2x3/16	210	-2.282	10.466	21.8	Pass
T6	247 - 227	Top Girt	L2x1 1/2x3/16	261	-2.065	10.466	19.7	Pass
T7	227 - 207	Top Girt	L2x1 1/2x3/16	312	-2.031	10.466	19.4	Pass
T8	207 - 187	Top Girt	L2x1 1/2x3/16	363	-1.873	10.466	17.9	Pass
T9	187 - 167	Top Girt	L2x1 1/2x1/4	414	-2.190	13.629	16.1	Pass
T10	167 - 147	Top Girt	L2x1 1/2x3/16	464	-1.736	10.466	16.6	Pass
T11	147 - 127	Top Girt	L2x1 1/2x3/16	515	-1.505	10.466	14.4	Pass
T12	127 - 107	Top Girt	L2x1 1/2x3/16	565	-1.725	10.466	16.5	Pass
T13	107 - 87	Top Girt	L2x1 1/2x3/16	618	-1.301	10.466	12.4	Pass
T14	87 - 67	Top Girt	L2x1 1/2x3/16	668	-1.381	10.466	13.2	Pass
T15	67 - 62.97	Top Girt	L2x1 1/2x3/16	720	-1.060	10.466	10.1	Pass
T16	62.97 - 58.99	Top Girt	L2x1 1/2x3/16	730	-3.057	10.466	29.2	Pass
T17	58.99 - 55.01	Top Girt	L2x1 1/2x3/16	742	-3.709	10.585	35.0	Pass
T18	55.01 - 51.03	Top Girt	L2x1 1/2x3/16	754	-3.752	10.585	35.4	Pass
T19	51.03 - 47	Top Girt	L2x1 1/2x3/16	767	-3.973	10.585	37.5	Pass
T20	47 - 27	Top Girt	L2x1 1/2x3/16	781	-2.007	10.585	19.0	Pass
T21	27 - 7	Top Girt	L2x1 1/2x3/16	833	-2.107	10.585	19.9	Pass
T22	7 - 3	Top Girt	L2x1 1/2x3/16	884	-2.131	10.585	20.1	Pass
T23	3 - 0	Top Girt	L2x1 1/2x3/16	895	-5.060	10.585	47.8	Pass
T1	347 - 327	Bottom Girt	L2x2x1/4	9	-4.637	17.506	26.5	Pass
T2	327 - 307	Bottom Girt	L2x1 1/2x3/16	60	-2.453	10.466	23.4	Pass
T3	307 - 287	Bottom Girt	L2x1 1/2x3/16	111	-2.284	10.466	21.8	Pass
T4	287 - 267	Bottom Girt	L2x2x1/4	162	-3.903	17.506	22.3	Pass
T5	267 - 247	Bottom Girt	L2x1 1/2x3/16	213	-2.072	10.466	19.8	Pass
T6	247 - 227	Bottom Girt	L2x1 1/2x3/16	264	-1.897	10.466	18.1	Pass
T7	227 - 207	Bottom Girt	L2x1 1/2x3/16	315	-1.968	10.466	18.8	Pass
T8	207 - 187	Bottom Girt	L2x1 1/2x3/16	365	-1.759	10.466	16.8	Pass
T9	187 - 167	Bottom Girt	L2x1 1/2x1/4	416	-2.178	13.629	16.0	Pass
T10	167 - 147	Bottom Girt	L2x1 1/2x3/16	468	-1.578	10.466	15.1	Pass
T11	147 - 127	Bottom Girt	L2x1 1/2x3/16	518	-1.451	10.466	13.9	Pass
T12	127 - 107	Bottom Girt	L2x1 1/2x3/16	569	-1.385	10.466	13.2	Pass
T13	107 - 87	Bottom Girt	L2x1 1/2x3/16	620	-1.313	10.466	12.5	Pass
T14	87 - 67	Bottom Girt	L2x1 1/2x3/16	671	0.897	20.123	4.5	Pass
T19	51.03 - 47	Bottom Girt	L2x1 1/2x3/16	770	-2.177	10.585	20.6	Pass
T20	47 - 27	Bottom Girt	L2x1 1/2x3/16	785	-2.039	10.585	19.3	Pass
T21	27 - 7	Bottom Girt	L2x1 1/2x3/16	836	-1.813	10.585	17.1	Pass
T23	3 - 0	Bottom Girt	L2x1 1/2x3/16	898	-0.423	10.585	4.0	Pass
T1	347 - 327	Guy A@331.1	7/16	919	9.391	12.480	75.2	Pass
T4	287 - 267	Guy A@271.1	7/16	937	8.399	12.480	67.3	Pass
T8	207 - 187	Guy A@202.9	7/16	955	7.874	12.480	63.1	Pass
T11	147 - 127	Guy A@131.1	3/8	973	5.542	9.240	60.0	Pass
T14	87 - 67	Guy A@67.1667	3/8	984	5.212	9.240	56.4	Pass
T1	347 - 327	Guy B@331.1	7/16	914	10.095	12.480	80.9	Pass
T4	287 - 267	Guy B@271.1	7/16	932	9.160	12.480	73.4	Pass
T8	207 - 187	Guy B@202.9	7/16	949	8.662	12.480	69.4	Pass
T11	147 - 127	Guy B@131.1	3/8	967	5.981	9.240	64.7	Pass
T14	87 - 67	Guy B@67.1667	3/8	983	5.571	9.240	60.3	Pass
T1	347 - 327	Guy C@331.1	7/16	908	9.652	12.480	77.3	Pass
T4	287 - 267	Guy C@271.1	7/16	926	8.588	12.480	68.8	Pass
T8	207 - 187	Guy C@202.9	7/16	944	8.113	12.480	65.0	Pass
T11	147 - 127	Guy C@131.1	3/8	962	5.698	9.240	61.7	Pass
T14	87 - 67	Guy C@67.1667	3/8	979	5.372	9.240	58.1	Pass
T14	87 - 67	Top Guy	3x3/8	981	-0.725	2.714	26.7	Pass
		Pull-Off@67.1667						
T1	347 - 327	Torque Arm Top@331.1	L3x3x5/16	921	7.723	57.672	13.4	Pass
T4	287 - 267	Torque Arm Top@271.1	L3x3x5/16	933	7.258	57.672	12.6	Pass
T8	207 - 187	Torque Arm	L3x3x5/16	951	8.656	57.672	15.0	Pass





Attachment 2:  
Collocation Application


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**WORKSHEET 1 OF 2 (COMPLETE BOTH WORKSHEET TABS)**

		<h2>CUSTOMER APPLICATION</h2>		A Site Application Fee to be paid upon submission of this Customer Application.
		DATE SUBMITTED:		
<b>CUSTOMER INFORMATION</b>				
COMPANY NAME:	Sprint	PHONE:	800-357-7641	
ENTITY Type: i.e. Inc., LLP	LP	FAX:		
STATE of Inc.	Delaware	SERVICE (PCS, SMR):	PCS (CDMA and EVDO), 4G	
<b>CUSTOMER ADDRESSES</b>				
COMPANY Address:	6391 Sprint Parkway	CITY/STATE:	Overland Park, Kansas	ZIP : 66251
BILLING Address:	Sprint/Nextel Property Services	CITY/STATE:	Overland Park, Kansas	ZIP : 66251-2650
NOTICE Address 1:	same as billing address	CITY/STATE:		ZIP :
NOTICE Address 2:	Sprint/Nextel Law Department	CITY/STATE:	Overland Park, Kansas	ZIP : 66251-2020
<b>CUSTOMER CONTACTS</b>				
PRIMARY CONTACT:	Ryan Bailey	PHONE:	856-625-1596	
TITLE:	Site Acq	E-MAIL Address:	ryan@mackenzierealtyconsulting.com	
SIGNATORY NAME:	TBD	PHONE:		
TITLE:		E-MAIL Address:		
EMERGENCY CONTACT:	NOCC	PHONE:	888-859-1400 or 866-400-6040	
TITLE:		E-MAIL Address:		
TECHNICAL/OPS:		PHONE:		
TITLE:		E-MAIL Address:		
RF ENGINEER:		PHONE:		
TITLE:		E-MAIL Address:		
BILLING CONTACT:	Landlord Solutions	PHONE:	800-357-7641	
TITLE:		E-MAIL Address:		
LEGAL CONTACT:		PHONE:		
TITLE:		E-MAIL Address:		
<b>SITE INFORMATION</b>				
CUSTOMER Site # / Name:	Cox Communications Tower / CT60XC956	INSITE Site # and Name:	CT900 Wolcott	
SITE LATITUDE:	41° 34' 34.3"	SITE LONGITUDE:	-72° 57' 22"	
SITE ADDRESS:	164 County Road Rear	CITY:	Wolcott	
STATE:	CT	ZIP:	6716	
		STRUCTURE TYPE:	Guyed Tower	
<b>USE THIS SECTION TO PROVIDE A DESCRIPTION OF COLOCATION OR MODIFICATION REQUEST</b>				
Replacing (3) antennas with (6) new antennas, replacing(3) 1900 RRH with (3) new 1900 RRH, adding (6) new 800 RRH (lease allows 3 of different model) adding (3) Hybrid cables				
<b>USE THIS SECTION TO LIST EQUIPMENT TO BE REMOVED</b>				
(3) APXV/TM-14-C-I20 antennas (3) 1900 4X45 65MHz (1900 MHz) RRH. Note: Installed antenna model does not match lease rights. 800 RRH and Notch Filters are not currently installed.				
<b>APPLICATION PREPARED BY</b>				
NAME:	Ryan Bailey	PHONE:	856-625-1596	
COMPANY:		ADDRESS:	3-B Prospect PLm Madison NJ 07940	
TITLE:		E-MAIL Address:	ryan@mackenzierealtyconsulting.com	

**EXHIBIT  
Equipment**

Site Name and #: **CT900 Wolcott**

Licensee Name: **Sprint**

The mounting method and exact location of the space and equipment listed herein shall be subject to InSite's approval.

SYSTEM REQUIREMENTS						
POWER provided by:	Utility Company direct			TELCO provided by:	Fiber	
Power Requirements:	Amps:	200	Volts:	120/240	No. of Outlets:	None
Generator Provided by:	N/A	Make:	N/A	Model:	N/A	Fuel Type: N/A Capacity: N/A
Batteries:	Quantity:	One (1) Cabinet	Make:	Commscope	Model:	60EC
SPACE REQUIREMENTS & RADIO INVENTORY						
Type of Space Required:	Ground:	Yes	Floor:	No	Total Square Feet:	375 sq. ft.
Dimensions of Equipment Floor/Ground Space:			15' x 25'		Equipment Height:	76"
Dimensions of Generator Ground Space:			N/A		Dimensions of Fuel Tank Ground Space:	N/A
No. of Transmitters (Tx):	1 BTS for both TX and RX	Transmitter Make/Model:	MODCELL 4.0		Transmitter Power Output	N/A
No. of Receivers (Rx):	1 BTS for both TX and RX	Receiver Make/Model:	MODCELL 4.0		Transmitter ERP:	300
Cabinet also contains:						
EQUIPMENT LOADING DESCRIPTION (FINAL CONFIGURATION)						
	Sector 1	Sector 2	Sector 3	DISH(ES)	OTHER	
Antenna Type (1):	Panel	Panel	Panel	GPS	N/A	
# of Antennas (1)/ Sector:	One (1)	One (1)	One (1)	One (1)	None	
Tx, Rx or Both:	Both	Both	Both	Receive	N/A	
Antenna Manufacturer (1):	CommScope	CommScope	CommScope	PCTEL	N/A	
Antenna Model (1):	NNVV-65B-R4	NNVV-65B-R4	NNVV-65B-R4	GPS-TMG-HR-26NCM	N/A	
Antenna Dimensions (1):	72" x 19.6" x 7.8"	72" x 19.6" x 7.8"	72" x 19.6" x 7.8"	5' x 3.2"	N/A	
Antenna Weight (1):	77 lbs	77 lbs	77 lbs	.6 lbs	N/A	
Antenna RAD Ctr (1):	201 ft	201 ft	201 ft	70 ft	N/A	
Antenna Type (2):	Panel	Panel	Panel	N/A	N/A	
# of Antennas (2)/ Sector:	One (1)	One (1)	One (1)	None	None	
Tx, Rx or Both:	Both	Both	Both	N/A	N/A	
Antenna Manufacturer (2):	Nokia	Nokia	Nokia	N/A	N/A	
Antenna Model (2):	AAHC	AAHC	AAHC	N/A	N/A	
Antenna Dimensions (2):	25.6" x 19.7" x 9.64"	25.6" x 19.7" x 9.64"	25.6" x 19.7" x 9.64"	N/A	N/A	
Antenna Weight (2):	104 lbs	104 lbs	104 lbs	N/A	N/A	
Antenna RAD Ctr (2):	201 ft	201 ft	201 ft	N/A	N/A	
# of RRU/RRHs/ Sector (1):	One (1)	One (1)	One (1)			
RRU/RRH Manufacturer (1):	ALU	ALU	ALU			
RRU/RRH Model (1):	1900 MHz RRH	1900 MHz RRH	1900 MHz RRH			
RRU/RRH Dimensions (1):	25.1" x 11.1" x 10.1"	25.1" x 11.1" x 10.1"	25.1" x 11.1" x 10.1"			
RRU/RRH Weight (1):	60 lbs	60 lbs	60 lbs			
RRU/RRH RAD Ctr (1):	201 ft	201 ft	201 ft			
# of RRU/RRHs/ Sector (2):	Two (2)	Two (2)	Two (2)			
RRU/RRH Manufacturer (2):	ALU	ALU	ALU			
RRU/RRH Model (2):	800 2x50W	800 2x50W	800 2x50W			
RRU/RRH Dimension (2):	16" x 13" x 10"	16" x 13" x 10"	16" x 13" x 10"			
RRU/RRH Weight (2):	69 lbs	69 lbs	69 lbs			
RRU/RRH RAD Ctr (2):	201 ft	201 ft	201 ft			
# of Filters/ Sector (1):	One (1) Reserved	One (1) Reserved	One (1) Reserved			
Filter Manufacturer (1):	ALU	ALU	ALU			
Filter Model (1):	Notch Filter (800MHz)	Notch Filter (800MHz)	Notch Filter (800MHz)			
Filter Dimensions (1):	8.9" x 10" x 4.3"	8.9" x 10" x 4.3"	8.9" x 10" x 4.3"			
Filter Weight (1):	9.45 lbs	9.45 lbs	9.45 lbs			
Filter RAD Ctr (1):	201 ft	201 ft	201 ft			
# of TMAs/ Sector:	None	None	None			
# of Diplexers/ Sector:	None	None	None			
# of Surge Suppressors/Sctr:	None	None	None			
OTHER:	None	None	None			
Transmit Frequencies:	851-869; 1950-1965; 1990-1995; 2496-2690 MHz			N/A	N/A	
Receive Frequencies:	806-824; 1870-1885; 1910-1915; 2496-2690 MHz			1575.42 MHz	N/A	
# of Lines:	Two (2)	Two (2)	Two (2)	One (1)	None	
Line Size:	1-1/4" Hybrid	1-1/4" Hybrid	1-1/4" Hybrid	1/2" (for GPS)	N/A	
Mount Type:	Sector Frame	Sector Frame	Sector Frame	Standoff Mount	N/A	
Mount Size:	Twelve Feet (12')	Twelve Feet (12')	Twelve Feet (12')	N/A	N/A	

RADIO FREQUENCY EMISSIONS ANALYSIS REPORT  
EVALUATION OF HUMAN EXPOSURE POTENTIAL  
TO NON-IONIZING EMISSIONS

SPRINT Existing Facility

Site ID: CT60XC956

Cox Communications Tower (Wolcott)  
164 County Road Rear  
Wolcott, CT 06716

**July 3, 2018**

**EBI Project Number: 6218004752**

Site Compliance Summary	
Compliance Status:	<b>COMPLIANT</b>
Site total MPE% of FCC general population allowable limit:	<b>1.59 %</b>

July 3, 2018

SPRINT

Attn: RF Engineering Manager  
1 International Boulevard, Suite 800  
Mahwah, NJ 07495

Emissions Analysis for Site: **CT60XC956 – Cox Communications Tower (Wolcott)**

EBI Consulting was directed to analyze the proposed SPRINT facility located at **164 County Road Rear, Wolcott, CT**, for the purpose of determining whether the emissions from the Proposed SPRINT Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

General population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limits for the 850 MHz Band is approximately  $567 \mu\text{W}/\text{cm}^2$ . The general population exposure limit for the 1900 MHz (PCS) and 2500 MHz (BRS) bands is  $1000 \mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## **CALCULATIONS**

Calculations were done for the proposed SPRINT Wireless antenna facility located at **164 County Road Rear, Wolcott, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since SPRINT is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 1 CDMA channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 20 Watts per Channel.
- 2) 2 LTE channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 50 Watts per Channel.
- 3) 5 CDMA channels (1900 MHz (PCS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 16 Watts per Channel.
- 4) 2 LTE channels (1900 MHz (PCS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 5) 8 LTE channels (2500 MHz (BRS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 20 Watts per Channel.

- 6) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 7) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 8) The antennas used in this modeling are the **Commscope NNVV-65B-R4 and the Nokia AAHC** for transmission in the 850 MHz, 1900 MHz (PCS) and 2500 MHz (BRS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 9) The antenna mounting height centerlines of the proposed antennas are **201 feet** above ground level (AGL) for **Sector A**, **201 feet** above ground level (AGL) for **Sector B** and **201 feet** above ground level (AGL) for Sector C.
- 10) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general population threshold limits.





## SPRINT Site Inventory and Power Data by Antenna

Sector:	A	Sector:	B	Sector:	C
Antenna #:	<b>1</b>	Antenna #:	<b>1</b>	Antenna #:	<b>1</b>
Make / Model:	Commscope NNVV-65B-R4	Make / Model:	Commscope NNVV-65B-R4	Make / Model:	Commscope NNVV-65B-R4
Gain:	12.75 / 15.05 dBd	Gain:	12.75 / 15.05 dBd	Gain:	12.75 / 15.05 dBd
Height (AGL):	<b>201 feet</b>	Height (AGL):	<b>201 feet</b>	Height (AGL):	<b>201 feet</b>
Frequency Bands	850 MHz / 1900 MHz (PCS)	Frequency Bands	850 MHz / 1900 MHz (PCS)	Frequency Bands	850 MHz / 1900 MHz (PCS)
Channel Count	10	Channel Count	10	Channel Count	10
Total TX Power(W):	280 Watts	Total TX Power(W):	280 Watts	Total TX Power(W):	280 Watts
ERP (W):	7,378.61	ERP (W):	7,378.61	ERP (W):	7,378.61
Antenna A1 MPE%	<b>0.86 %</b>	Antenna B1 MPE%	<b>0.86 %</b>	Antenna C1 MPE%	<b>0.86 %</b>
Antenna #:	<b>2</b>	Antenna #:	<b>2</b>	Antenna #:	<b>2</b>
Make / Model:	Nokia AAHC	Make / Model:	Nokia AAHC	Make / Model:	Nokia AAHC
Gain:	15.05 dBd	Gain:	15.05 dBd	Gain:	15.05 dBd
Height (AGL):	<b>201 feet</b>	Height (AGL):	<b>201 feet</b>	Height (AGL):	<b>201 feet</b>
Frequency Bands	2500 MHz (BRS)	Frequency Bands	2500 MHz (BRS)	Frequency Bands	2500 MHz (BRS)
Channel Count	8	Channel Count	8	Channel Count	8
Total TX Power(W):	160 Watts	Total TX Power(W):	160 Watts	Total TX Power(W):	160 Watts
ERP (W):	5,118.23	ERP (W):	5,118.23	ERP (W):	5,118.23
Antenna A2 MPE%	<b>0.48 %</b>	Antenna B2 MPE%	<b>0.48 %</b>	Antenna C2 MPE%	<b>0.48 %</b>

Site Composite MPE%	
Carrier	MPE%
SPRINT – Max per sector	<b>1.34 %</b>
Cox Communications	0.07 %
Clearwire	0.05 %
T-Mobile	0.13 %
<b>Site Total MPE %:</b>	<b>1.59 %</b>

SPRINT Sector A Total:	1.34 %
SPRINT Sector B Total:	1.34 %
SPRINT Sector C Total:	1.34 %
<b>Site Total:</b>	<b>1.59 %</b>

SPRINT _ Frequency Band / Technology Max Power Values (Per Sector)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ( $\mu\text{W}/\text{cm}^2$ )	Frequency (MHz)	Allowable MPE ( $\mu\text{W}/\text{cm}^2$ )	Calculated % MPE
Sprint 850 MHz CDMA	1	376.73	201	0.36	850 MHz	567	0.06%
Sprint 850 MHz LTE	2	941.82	201	1.78	850 MHz	567	0.32%
Sprint 1900 MHz (PCS) CDMA	5	511.82	201	2.42	1900 MHz (PCS)	1000	0.24%
Sprint 1900 MHz (PCS) LTE	2	1,279.56	201	2.42	1900 MHz (PCS)	1000	0.24%
Sprint 2500 MHz (BRS) LTE	8	639.78	201	4.84	2500 MHz (BRS)	1000	0.48%
						<b>Total:</b>	<b>1.34%</b>

## Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the SPRINT facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

SPRINT Sector	Power Density Value (%)
Sector A:	1.34 %
Sector B:	1.34 %
Sector C:	1.34 %
SPRINT Maximum Total (per sector):	1.34 %
Site Total:	1.59 %
Site Compliance Status:	<b>COMPLIANT</b>

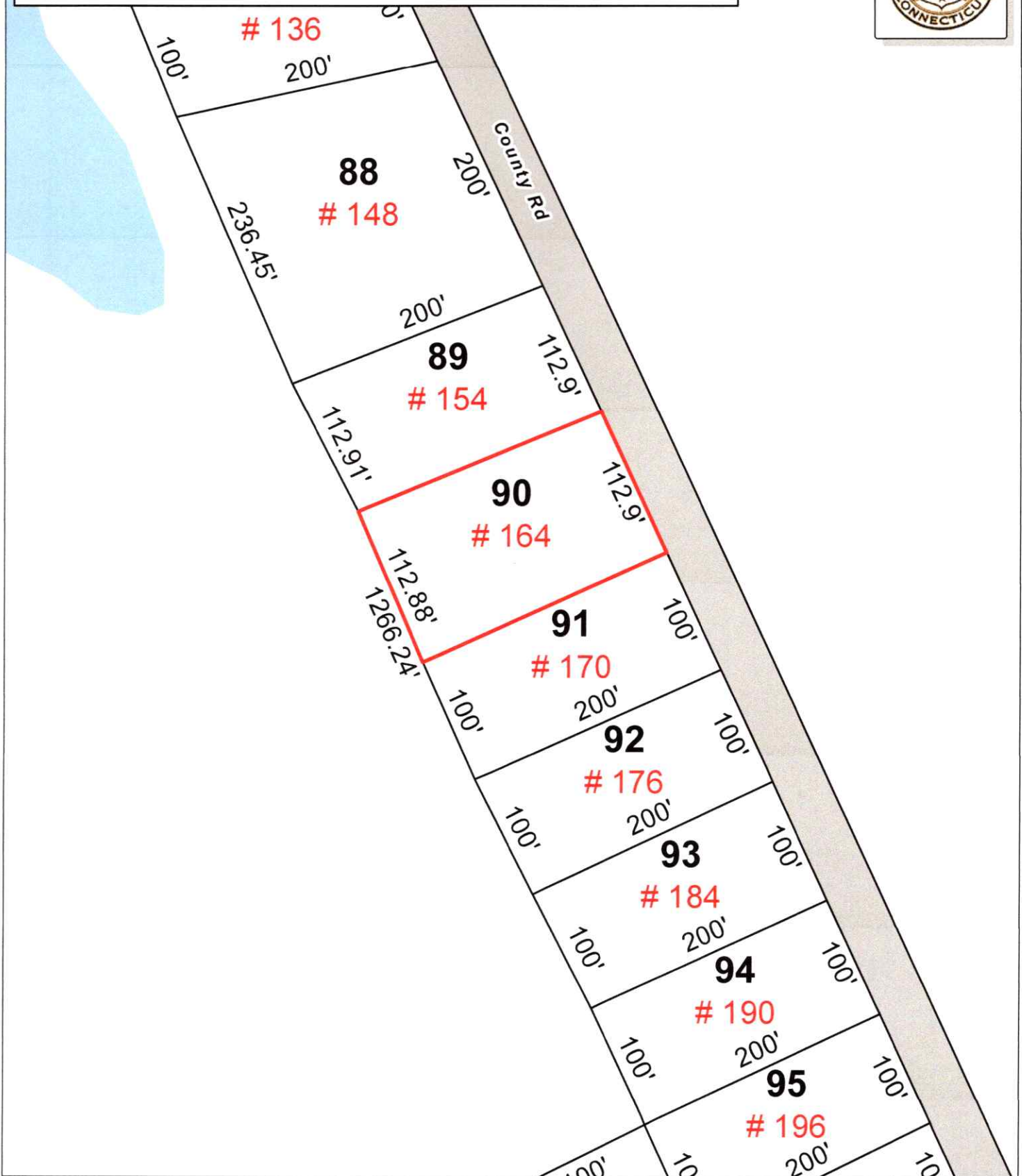
The anticipated composite MPE value for this site assuming all carriers present is **1.59 %** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

# Town of Wolcott, Connecticut - Assessment Parcel Map

Parcel: F0188700

Address: 164 COUNTY RD

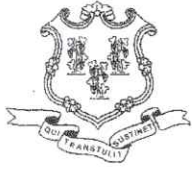


Approximate Scale: 1 inch = 100 feet

Map Produced Feb 2018

Disclaimer: This map is for informational purposes only. All information is subject to verification by any user. The Town of Wolcott and its mapping contractors assume no legal responsibility for the information contained herein.





STATE OF CONNECTICUT  
CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051  
Phone: (860) 827-2935 Fax: (860) 827-2950  
E-Mail: [siting.council@ct.gov](mailto:siting.council@ct.gov)  
[www.ct.gov/csc](http://www.ct.gov/csc)

July 18, 2014

Paul F. Sagristano  
Vertical Development LLC  
20 Commercial Street  
Branford, CT 06405

RE: **EM-SPRINT-166-140627** – Sprint Nextel Corporation notice of intent to modify an existing telecommunications facility located at 164 County Road, Wolcott, Connecticut.

Dear Mr. Sagristano:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies with the following conditions:

- Any deviation from the proposed modification as specified in this notice and supporting materials with the Council shall render this acknowledgement invalid;
- Any material changes to this modification as proposed shall require the filing of a new notice with the Council;
- Within 45 days after completion of construction, the Council shall be notified in writing that construction has been completed;
- Any nonfunctioning antenna and associated antenna mounting equipment on this facility owned and operated by Sprint shall be removed within 60 days of the date the antenna ceased to function.
- The validity of this action shall expire one year from the date of this letter; and
- The applicant may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration.

The proposed modifications including the placement of all necessary equipment and shelters within the tower compound are to be implemented as specified here and in your notice dated June 27, 2014. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site by any dimension, increase noise levels at the tower site boundary by six decibels or more, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standards adopted by the Federal Communications Commission pursuant to Section 704 of the Telecommunications Act of 1996 and by the state Department of Energy and Environmental Protection pursuant to Connecticut General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below state and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such



notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Thank you for your attention and cooperation.

Very truly yours,



Melanie A. Bachman  
Acting Executive Director

MAB/RDM/cm

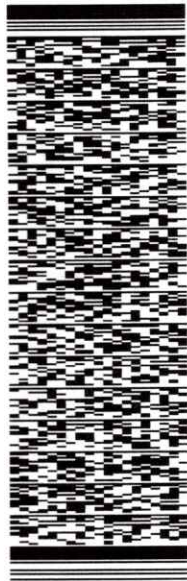
c: The Honorable Thomas G. Dunn, Mayor, Town of Wolcott  
David Kalinowski, Zoning Enforcement Officer, Town of Wolcott  
Mark Proul

ORIGIN ID: LKKA (856) 625-1596  
RYAN BILLEY  
CHARLES CHERUNDOLO CONSULTING  
3 PROSPECT PL  
B  
MADISON, NJ 07940  
UNITED STATES US

SHIP DATE: 30 JUL 18  
ACTWGT: 1.00 LB  
CAD: 11040787/MET4040  
BILL SENDER

TO  
**MAYOR THOMAS G DUNN**  
**TOWN OF WOLCOTT**  
**10 KENEA AVE**

**WOLCOTT CT 06716**  
(203) 879-8100 REF: CT60XC956 CSC FILING  
INV: DEPT:  
PO:



J182018072201uv

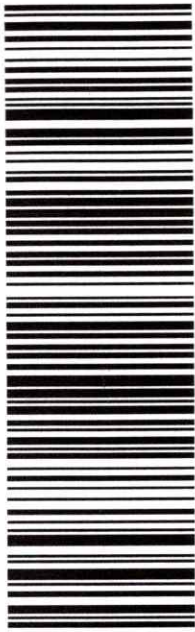
552J1/3309/DCA5

TRK#  
0201 **7728 5406 0896**

**THU - 02 AUG 4:30P**  
**EXPRESS SAVER**

**K7 BNHA**

06716  
CT-US BDL



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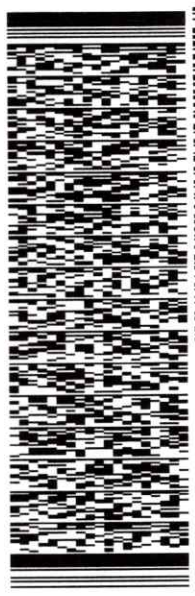
Use of this system constitutes your agreement to the service conditions in the current FedEx Service Guide, available on fedex.com. FedEx will not be responsible for any claim in excess of \$100 per package, whether the result of loss, damage, delay, non-delivery, misdelivery, or misinformation, unless you declare a higher value, pay an additional charge, document your actual loss and file a timely claim. Limitations found in the current FedEx Service Guide apply. Your right to recover from FedEx for any loss, including intrinsic value of the package, loss of sales, income interest, profit, attorney's fees, costs, and other forms of damage whether direct, incidental, consequential, or special is limited to the greater of \$100 or the authorized declared value. Recovery cannot exceed actual documented loss. Maximum for items of extraordinary value is \$1,000, e.g. jewelry, precious metals, negotiable instruments and other items listed in our ServiceGuide. Written claims must be filed within strict time limits, see current FedEx Service Guide.

ORIGIN: IDL:KKA (856) 625-1596  
RYAN BILLET  
CHARLES CHERUNDOLO CONSULTING  
3 PROSPECT PL  
B  
MADISON, NJ 07940  
UNITED STATES US

SHIP DATE: 30 JUL 18  
ACTWGT: 1.00 LB  
CAD: 111040781IN/NET4040  
BILL SENDER

TO DAVID KALNOWSKI  
TOWN OF WOLCOTT  
10 KENEA AVE

WOLCOTT CT 06716  
(203) 879-8100 REF: CT80XC956 CSC: FLING  
INV. PO. DEPT.



TRK# 7728 5406 9356 THU - 02 AUG 4:30P  
0201 EXPRESS SAVER

K7 BNHA 06716  
CT-US BDL

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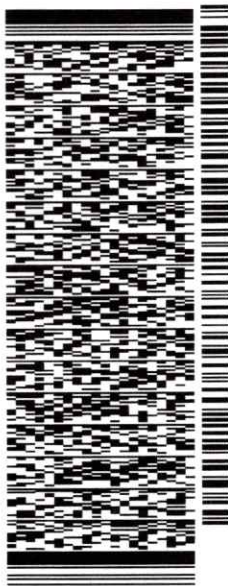
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RYAN BAILEY  
CHARLES CHERUNDOLO CONSULTING  
3 PROSPECT PL  
B MADISON, NJ 07940  
UNITED STATES US

SHP DATE: 30 JUL 18  
ACTWGT: 1.00 LB  
CAD: 11040781/NET4040  
BILL SENDER

TO NANCY TERRY  
INSITE TOWERS  
1199 NORTH FAIRFAX ST  
SUITE 700  
ALEXANDRIA VA 22314  
(540) 588-3150  
REF: CT6DX0956 CSC:FLING  
INV. DEPT:  
P.O.

552J11/3309/DCA5



TRK# 7728 5408 4963  
0201

THU - 02 AUG 4:30P  
EXPRESS SAVER

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22314  
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VA-US



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STEVIE SOFMAN  
CHARLES-CHERUNDOLLO CONSULTING  
1280 ROUTE 46 WEST  
SUITE 9  
PARSHIPANY, NJ 07054  
UNITED STATES US

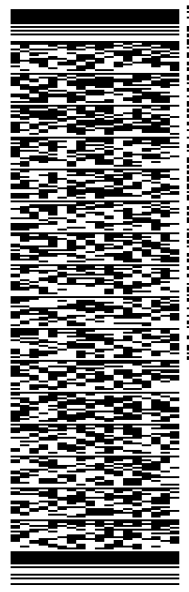
SHIP DATE: 09AUG18  
ACT WGT: 1.00 LB  
CAD: 111040787/MET4040  
BILL SENDER

TO MARK PROUL

164 COUNTRY RD

WOLCOTT CT 06716

(203) 758-6895 REF: CSC FILING CT60XC956  
INVT  
PO. DEPT.

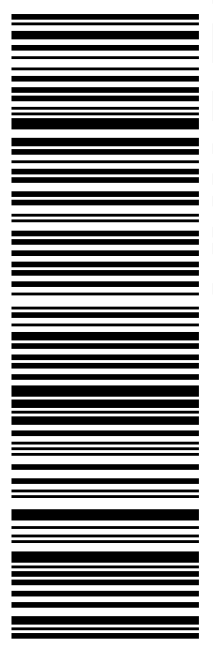


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0201

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06716  
BDL  
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