

May 24, 2023

Melanie A. Bachman, Esq.
Executive Director/Staff Attorney
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Re: Request of Cellco Partnership d/b/a Verizon Wireless for an Order to Approve the Shared Use of an Existing Tower at 780 Prospect Hill Road, Windsor, Connecticut

Dear Attorney Bachman:

Pursuant to Connecticut General Statutes (“C.G.S.”) §16-50aa, as amended, Cellco Partnership d/b/a Verizon Wireless (“Cellco”) hereby requests an order from the Siting Council (“Council”) to approve the shared use of an existing telecommunications tower located on a 5.71-acre parcel at 780 Prospect Hill Road in Windsor (the “Property”). The Property is owned by The Ferraina Company LLC. The tower is owned by Tarpon Towers (“Tarpon”). Cellco identifies this site as its “Windsor 4 Facility”. The existing 135-foot monopole tower was approved by the Siting Council (“Council”) in June of 2021 (Docket No. 496). A copy of the Council’s Docket 496 Decision and Order is included in Attachment 1.

Cellco requests that the Council find that the proposed shared use of the existing tower satisfies the criteria of C.G.S § 16-50aa and issue an order approving this request. A copy of this filing is being sent to Windsor’s Mayor, Donald Trinks and Town Planner, Eric Barz.

Background

Cellco is licensed by the Federal Communications Commission (“FCC”) to provide wireless services throughout the State of Connecticut. Cellco and Tarpon have agreed to the proposed shared use of the Prospect Hill Road tower pursuant to mutually acceptable terms and conditions. Likewise, Tarpon and Cellco have agreed to the proposed installation of equipment

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on the ground near the base of the tower. Tarpon has authorized Cellco to apply for all necessary permits and approvals that may be required to share the existing tower. (See Attachment 2).

Cellco proposes to install nine (9) antennas and nine (9) remote radio heads (“RRHs”) on an antenna platform at a centerline height of 105 feet above ground level (“AGL”). Cellco will also install two equipment cabinets and a 50-kW diesel-fueled backup generator on a concrete pad on the ground near the base of the tower. Included in Attachment 3 are Cellco’s project plans showing the location of Cellco’s proposed site improvements. Attachment 4 contains specifications for Cellco’s proposed antennas, RRHs and backup generator.

C.G.S. § 16-50aa(c)(1) provides that, upon written request for approval of a proposed shared use, “if the council finds that the proposed shared use of the facility is technically, legally, environmentally and economically feasible and meets public safety concerns, the council shall issue an order approving such shared use.” Cellco respectfully submits that the shared use of the tower satisfies these criteria.

A. Technical Feasibility. The existing tower is structurally capable of supporting Cellco’s antennas, RRHs, antenna platform and related equipment. The proposed shared use of this tower is, therefore, technically feasible. A Structural Analysis (“SA”) dated May 9, 2023 prepared by Michael F. Plahovinsak, P.E. confirms that the tower can support Cellco’s proposed antennas and related equipment. Likewise, an Antenna Mount Analysis (“MA”) dated April 13, 2023 also confirms that the proposed antenna and RRH mounting system can support Cellco’s proposed shared use. Copies of the SA and MA are included in Attachment 5.

B. Legal Feasibility. Under C.G.S. § 16-50aa, the Council has been authorized to issue orders approving the shared use of an existing tower, such as the existing Prospect Hill Road tower. This authority complements the Council’s prior-existing authority under C.G.S. § 16-50p to issue orders approving the construction of new towers that are subject to the Council’s jurisdiction. In addition, § 16-50x(a) directs the Council to “give such consideration to other state laws and municipal regulations as it shall deem appropriate” in ruling on requests for the shared use of existing tower facilities. Under the statutory authority vested in the Council, an order by the Council approving the requested shared use would permit the Applicant to obtain a building permit for the proposed installations.

C. Environmental Feasibility. The proposed shared use of the existing tower would have minimal environmental effects, for the following reasons:

1. The proposed installation of nine (9) antennas and nine (9) RRHs on an

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antenna platform at a height of 105 feet AGL on the existing 135-foot tower would have an insignificant incremental visual impact on the area around the Property. As mentioned above, all of Cellco's equipment will be located within a fenced facility compound near the base of the tower. Cellco's shared use of the existing tower would, therefore, not cause any significant change or alteration in the physical or environmental characteristics of the existing facility.

2. Noise associated with Cellco's proposed facility will comply with State and local noise standards. Noise associated with the backup generator is exempt from state and local noise standards.
3. Operation of Cellco's antennas at this site would not exceed the RF emissions standards adopted by the Federal Communications Commission ("FCC"). Included in Attachment 6 of this filing is a Calculated Radio Frequency Emissions Report that demonstrates that the modified facility will operate well within the FCC's safety standards.
4. Under ordinary operating conditions, the proposed installation would not require the use of any water or sanitary facilities and would not generate air emissions or discharges to water bodies or sanitary facilities. After construction is complete the proposed installations would not generate any increased traffic to the facility other than periodic maintenance visits to the cell site.

The proposed shared use of the existing tower would, therefore, have a minimal environmental effect, and is environmentally feasible.

D. Economic Feasibility. As previously mentioned, Cellco has entered into an agreement with Tarpon for the shared use of the existing tower subject to mutually agreeable terms. The proposed tower sharing is, therefore, economically feasible.

E. Public Safety Concerns. As discussed above, the tower and antenna mounts are structurally capable of supporting Cellco's antennas, antenna mounting frame, RRHs and all related equipment. Cellco is not aware of any public safety concerns relative to the proposed sharing of the existing Prospect Hill Road tower. In fact, the provision of new and improved wireless service through Cellco's shared use of the existing tower would enhance the safety and welfare of area residents and members of the general public traveling through the Town of

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Windsor.

A Certificate of Mailing verifying that a copy of this filing was sent to the municipal officials, the Property owner, and Tarpon, the tower owner is included in Attachment 7.

Conclusion

For the reasons discussed above, the proposed shared use of the existing tower at the Property satisfies the criteria stated in C.G.S. § 16-50aa and advances the General Assembly's and the Council's goal of preventing the unnecessary proliferation of towers in Connecticut. The Applicant, therefore, respectfully requests that the Council issue an order approving the proposed shared use.

Thank you for your consideration of this matter.

Very truly yours,



Kenneth C. Baldwin

Enclosures

Copy to:

Donald Trinks, Mayor
Eric Barz, Town Planner
The Ferraina Company LLC, Property Owner
Brett Buggeln, Tarpon Towers
Tim Parks, Verizon Wireless

ATTACHMENT 1

DOCKET NO. 496 – Tarpon Towers II, LLC application for a } Connecticut
Certificate of Environmental Compatibility and Public Need for }
the construction, maintenance, and operation of a } Siting
telecommunications facility located at 800 Prospect Hill Road, }
Windsor, Connecticut. } Council

June 3, 2021

Decision and Order

Pursuant to Connecticut General Statutes §16-50p, and the foregoing Findings of Fact and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the construction, maintenance, and operation of a telecommunications facility, including effects on the natural environment, ecological balance, public health and safety, scenic, historic, and recreational values, agriculture, forests and parks, air and water purity, and fish, aquaculture and wildlife are not disproportionate, either alone or cumulatively with other effects, when compared to need, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application, and therefore directs that a Certificate of Environmental Compatibility and Public Need, as provided by General Statutes §16-50k, be issued to Tarpon Towers II, LLC, hereinafter referred to as the Certificate Holder, for a telecommunications facility located at 800 Prospect Hill Road, Windsor, Connecticut.

Unless otherwise approved by the Council, the facility shall be constructed, operated, and maintained substantially as specified in the Council's record in this matter, and subject to the following conditions:

1. The tower shall be constructed as a monopole at a height of 135 feet above ground level to provide the proposed wireless services, sufficient to accommodate the antennas of T-Mobile Northeast LLC, and other entities, both public and private. The height of the tower may be extended after the date of this Decision and Order pursuant to regulations of the Federal Communications Commission.
2. The Certificate Holder shall prepare a Development and Management (D&M) Plan for this site in compliance with Sections 16-50j-75 through 16-50j-77 of the Regulations of Connecticut State Agencies. The D&M Plan shall be submitted to and approved by the Council prior to the commencement of facility construction and shall include:
 - a) a certified letter from a wireless telecommunications carrier with a firm commitment to install associated wireless equipment at the facility upon completion of construction;
 - b) final site plan(s) for development of the facility that employ the governing standard in the State of Connecticut for tower design in accordance with the currently adopted International Building Code and include specifications for the tower, tower foundation, antennas and equipment compound including, but not limited to, fence design, landscaping, ground equipment, access road, utility installation and emergency backup power;
 - c) the tower shall be designed with a yield point to ensure that the tower setback radius remains within the boundaries of the subject property;
 - d) construction plans for site clearing, grading, landscaping, water drainage and stormwater control, and erosion and sedimentation controls consistent with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control, as amended; and
 - e) construction schedule including hours and days of the week for construction activities.

3. Prior to the commencement of operation, the Certificate Holder shall provide the Council worst-case modeling of the electromagnetic radio frequency power density of all proposed entities' antennas at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin No. 65, August 1997. The Certificate Holder shall ensure a recalculated report of the electromagnetic radio frequency power density be submitted to the Council if and when circumstances in operation cause a change in power density above the levels calculated and provided pursuant to this Decision and Order.
4. Upon the establishment of any new federal radio frequency standards applicable to frequencies of this facility, the facility granted herein shall be brought into compliance with such standards.
5. The Certificate Holder shall provide the Council with a copy of necessary permits from any other state or federal agency with concurrent jurisdiction prior to the commencement of construction.
6. The Certificate Holder shall permit public or private entities to share space on the proposed tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
7. Unless otherwise approved by the Council, if the facility authorized herein is not fully constructed with at least one fully operational wireless telecommunications carrier providing wireless service within eighteen months from the date of the mailing of the Council's Findings of Fact, Opinion, and Decision and Order (collectively called "Final Decision"), this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapply for any continued or new use to the Council before any such use is made. The time between the filing and resolution of any appeals of the Council's Final Decision shall not be counted in calculating this deadline. Authority to monitor and modify this schedule, as necessary, is delegated to the Executive Director. The Certificate Holder shall provide written notice to the Executive Director of any schedule changes as soon as is practicable.
8. Any request for extension of the time period referred to in Condition 7 shall be filed with the Council not later than 60 days prior to the expiration date of this Certificate and shall be served on all parties and intervenors, as listed in the service list, and the Town Windsor.
9. If the facility ceases to provide wireless services for a period of one year, this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapply for any continued or new use to the Council within 90 days from the one year period of cessation of service. The Certificate Holder may submit a written request to the Council for an extension of the 90 day period not later than 60 days prior to the expiration of the 90 day period.
10. Any nonfunctioning antenna, and associated antenna mounting equipment, on this facility shall be removed within 60 days of the date the antenna ceased to function.
11. In accordance with Section 16-50j-77 of the Regulations of Connecticut State Agencies, the Certificate Holder shall provide the Council with written notice two weeks prior to the commencement of site construction activities. In addition, the Certificate Holder shall provide the Council with written notice of the completion of site construction, and the commencement of site operation.

12. The Certificate Holder shall remit timely payments associated with annual assessments and invoices submitted by the Council for expenses attributable to the facility under Conn. Gen. Stat. §16-50v.
13. This Certificate may be transferred in accordance with Conn. Gen. Stat. §16-50k(b), provided both the Certificate Holder/transferor and the transferee are current with payments to the Council for their respective annual assessments and invoices under Conn. Gen. Stat. §16-50v. In addition, both the Certificate Holder/transferor and the transferee shall provide the Council a written agreement as to the entity responsible for any quarterly assessment charges under Conn. Gen. Stat. §16-50v(b)(2) that may be associated with this facility. If construction has not been completed in accordance with Condition 7 of this Decision and Order at the time the Certificate is requested to be transferred, a certified letter from a wireless telecommunications carrier with a firm commitment to install associated wireless equipment at the facility upon completion of construction shall also be provided.
14. The Certificate Holder shall maintain the facility and associated equipment, including but not limited to, the tower, tower foundation, antennas, equipment compound, radio equipment, access road, utility line and landscaping in a reasonable physical and operational condition that is consistent with this Decision and Order and a Development and Management Plan to be approved by the Council.
15. If the Certificate Holder is a wholly-owned subsidiary of a corporation or other entity and is sold/transferred to another corporation or other entity, the Council shall be notified of such sale and/or transfer and of any change in contact information for the individual or representative responsible for management and operations of the Certificate Holder within 30 days of the sale and/or transfer.
16. This Certificate may be surrendered by the Certificate Holder upon written notification and acknowledgment by the Council.

We hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed in the Service List, dated February 25, 2021, and notice of issuance published in the Hartford Courant.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section 16-50j-17 of the Regulations of Connecticut State Agencies.

ATTACHMENT 2



May 3, 2023

Andrew Candiello
Principal Engineer-RE/Regulatory
Cellco Partnership d/b/a Verizon Wireless
20 Alexander Drive
Wallingford, CT 06492

Re: Letter of Authorization – **Tarpon Towers II, LLC with site address of 780 / 810 Prospect Hill, Windsor, CT 06095** grants Cellco Partnership d/b/a Verizon Wireless authority to install equipment.

Dear Mr. Candiello:

I, Brett Buggeln, COO of Tarpon Towers II, LLC, hereby authorizes Cellco Partnership d/b/a Verizon Wireless and/or its authorized agents, to file for all necessary permit and approval applications for the installation of antennas and related equipment at an existing telecommunications facility in Bloomfield, CT.

Sincerely,

A handwritten signature in black ink, appearing to read "Brett Buggeln", is written over a faint, larger version of the signature.

Brett Buggeln
Chief Operating Officer
Tarpon Towers II, LLC

ATTACHMENT 3

SUPPORTING DOCUMENTS

RADIO FREQUENCY (RF) DESIGN DATE: 4/4/23
 ANTENNA MOUNT STRUCTURAL ANALYSIS DATE: 4/13/23
 ANTENNA SUPPORT STRUCTURE (135'± MONOPOLE) STRUCTURAL ANALYSIS DATE: 5/9/23 (BY OTHERS)



20 ALEXANDER DRIVE, 2nd FLOOR, WALLINGFORD, CT 06492

WINDSOR 4 CT
780 PROSPECT HILL ROAD
WINDSOR, CT 06095

PROJECT TYPE: WIRELESS TELECOMMUNICATIONS
COLLOCATION ON EXISTING 135'± MONOPOLE

CLIENT:

ARCHITECT/ENGINEER:

 R.K. EXECUTIVE CENTRE
 201 BOSTON POST ROAD WEST
 SUITE 101
 MARLBOROUGH, MA 01752
 (508) 481-7400
 www.chappellengineering.com

SEAL:

 ENGINEER/LAND SURVEYOR DATE

SITE INFORMATION:

PARENT PARCEL OWNER: THE FERRAINA COMPANY LLC.
 810 PROSPECT HILL ROAD
 WINDSOR, CT 06095

TOWER OWNER: TARPON TOWERS II, LLC.
 8916 77TH TERRACE EAST, SUITE 103
 LAKEWOOD RANCH, FL 34202
 (941) 757-5010

TOWER OWNER ID: CT1209 (WINDSOR)

APPLICANT: CELLCO PARTNERSHIP
 (d/b/a VERIZON WIRELESS)
 20 ALEXANDER DRIVE
 WALLINGFORD, CT 06492

SITE ADDRESS: 780 PROSPECT HILL ROAD
 WINDSOR, CT 06095

COUNTY: HARTFORD COUNTY, CT

SITE CONTROL POINT: CENTER OF EXISTING MONOPOLE
 N 41°-52'-58.47" (41.882908°) (NAD '83)
 W 72°-42'-29.14" (72.708084°) (NAD '83)

JURISDICTION: CONNECTICUT SITING COUNCIL

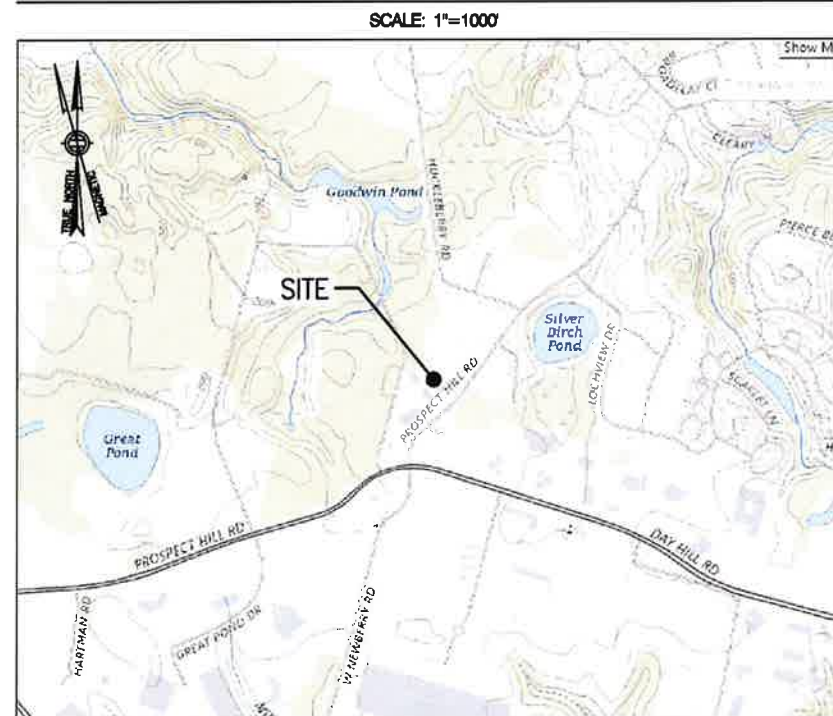
TAX ID PARCEL NUMBER: MAP 17 BLOCK 135 LOT 1

ARCHITECT / ENGINEER: CHAPPELL ENGINEERING ASSOCIATES, LLC
 201 BOSTON POST ROAD WEST, SUITE 101
 MARLBOROUGH, MA 01752

POWER COMPANY: EVERSOURCE ENERGY
 247 STATION DRIVE, SE 210
 WESTWOOD, MA 02090
 (781) 441-3610

TELEPHONE COMPANY: VERIZON
 185 FRANKLIN STREET
 BOSTON, MA 02107
 (800) 941-9900

VICINITY MAP



DRIVING DIRECTIONS

FROM WALLINGFORD, TAKE I-91 NORTH. TAKE EXIT 37 FOR CT-305/BLOOMFIELD AVENUE TOWARD WINDSOR CENTER. USE LEFT 2 LANES TO TURN LEFT ONTO CT-305 W/BLOOMFIELD AVENUE. TURN RIGHT ONTO MARSHALL PHELPS ROAD. USE THE LEFT 2 LANES TO TURN LEFT ONTO DAY HILL ROAD. TURN RIGHT ONTO PROSPECT HILL ROAD. THE SITE WILL BE ON THE RIGHT HAND SIDE.

SHEET INDEX

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A03	NORTHEAST AND SOUTHWEST EQUIPMENT COMPOUND ELEVATIONS	2
S01	ICE SHIELD FRAMING PLAN & STRUCTURAL DETAILS	2
RF01	ANTENNA MOUNTING PLAN AND DETAILS	2
RF02	ANTENNA DETAILS AND ANCILLARY EQUIPMENT SPECIFICATIONS	2
RF03	RF BILL OF MATERIALS AND RF CABLE PLUMBING DIAGRAM	2
RF04	RF COLOR CODE SPECIFICATIONS	2
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E02	EQUIPMENT COMPOUND UTILITY PLAN & DETAILS	2
E03	ELECTRICAL DIAGRAMS & DETAILS	2
E04	SCHEMATIC GROUNDING PLAN & DETAILS	2
E05	GROUNDING DETAILS	2

GENERAL NOTES

- CONTRACTOR SHALL VERIFY ALL PLANS, EXISTING DIMENSIONS, AND CONDITIONS ON JOB SITE. CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ARCHITECT/ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK. FAILURE TO NOTIFY THE ARCHITECT/ENGINEER PLACES THE RESPONSIBILITY ON THE CONTRACTOR TO CORRECT THE DISCREPANCIES AT THE CONTRACTOR'S EXPENSE.
- NEW CONSTRUCTION SHALL CONFORM TO ALL APPLICABLE CODES AND ORDINANCES.
 - BUILDING CODE: 2022 CONNECTICUT STATE BUILDING CODE
 - ELECTRICAL CODE: 2017 NATIONAL ELECTRICAL CODE
 - STRUCTURAL CODE: TIA/EIA-222-H STRUCTURAL STANDARDS FOR ANTENNA SUPPORTING STRUCTURES AND ANTENNAS.

AT LEAST 72 HOURS PRIOR TO DIGGING, THE CONTRACTOR IS REQUIRED TO CALL DIG SAFE AT 811



DO NOT SCALE DRAWINGS

ALL PLANS, EXISTING DIMENSIONS AND CONDITIONS AT THE PROPOSED PROJECT SITE SHALL BE VERIFIED IN THE FIELD DURING THE CONSTRUCTION PHASE. THE PROJECT OWNER'S REPRESENTATIVE SHALL BE NOTIFIED IN WRITING OF ANY DISCREPANCIES IMMEDIATELY PRIOR TO PROCEEDING WITH THE PROPOSED WORK AFFECTED BY SUCH DISCREPANCIES. IN THE EVENT OF LACK OF SUCH NOTIFICATION, SUCH DISCREPANCIES SHALL BECOME THE RESPONSIBILITY OF THE PREVAILING CONTRACTOR RESPONSIBLE FOR CONSTRUCTION.

PROJECT DESCRIPTION

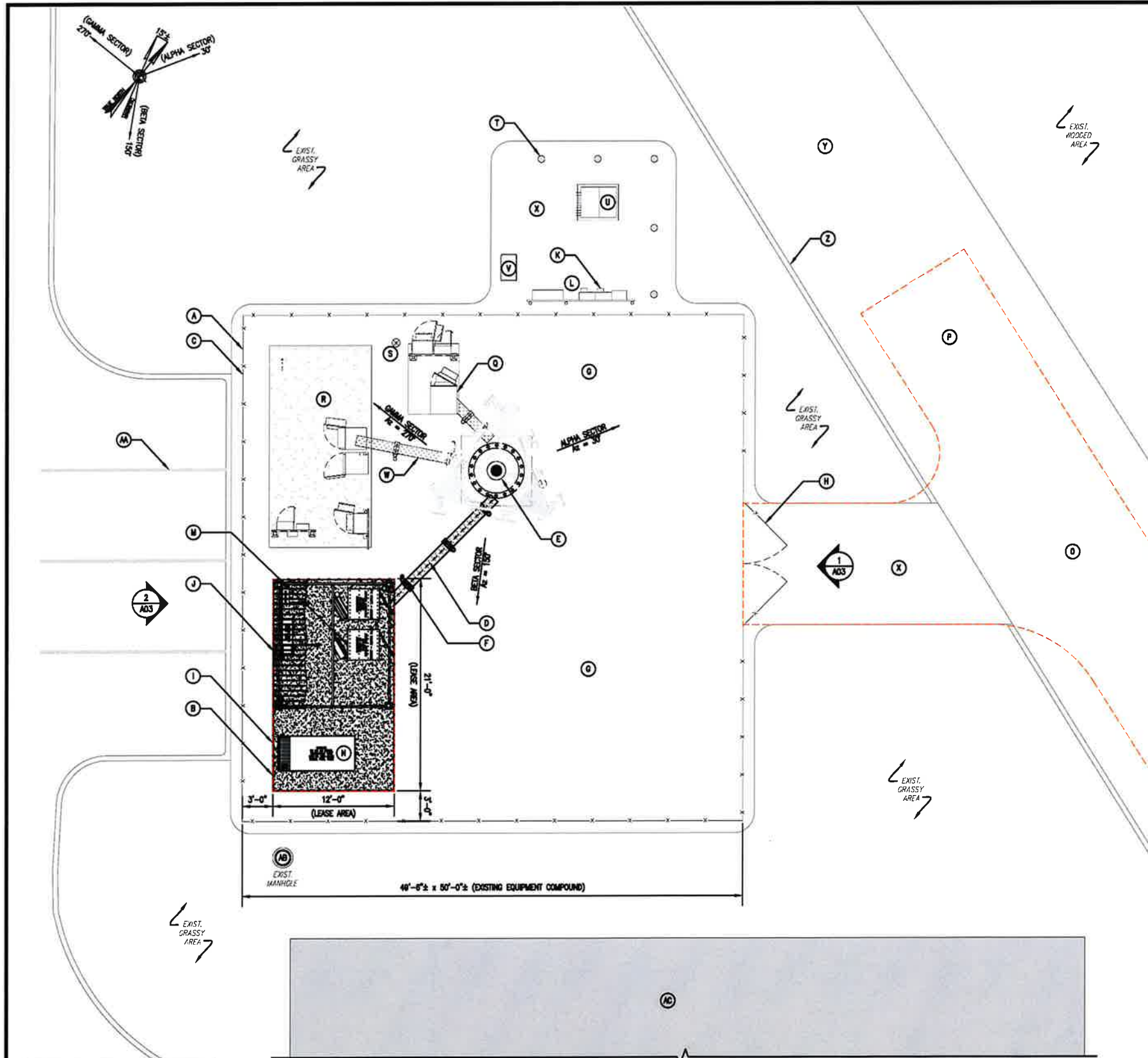
- THIS IS AN UNMANNED AND RESTRICTED ACCESS EQUIPMENT INSTALLATION AND WILL BE USED FOR THE TRANSMISSION OF RADIO SIGNAL FOR THE PURPOSE OF PROVIDING PUBLIC WIRELESS TELECOMMUNICATIONS SERVICE.
- THIS FACILITY WILL CONSUME NO UNRECOVERABLE ENERGY.
- NO POTABLE WATER SUPPLY IS TO BE PROVIDED AT THIS LOCATION.
- NO WASTE WATER WILL BE GENERATED AT THIS LOCATION.
- NO SOLID WASTE WILL BE GENERATED AT THIS LOCATION.

PROJECT NAME:
WINDSOR 4 CT
 780 PROSPECT HILL ROAD
 WINDSOR, CT 06095

DRAWING TITLE:
 TITLE SHEET

DRAWING NO.:
T01

SCALE:	DESIGNED BY: HMC	VZW PROJECT CODE:
AS SHOWN	DRAWN BY: HMC	20230415008
CIA PROJECT NO:	CHECKED BY: GCS	VZW PROJECT NO:
98210.416	ORIGINAL ISSUE DATE:	18069214
	4/28/23	MDG LOCATION ID:
		5000207278



LEGEND	
ITEM	DESCRIPTION
A	EXIST. 45'-6" x 50'-0" (2,475 S.F.) EQUIPMENT COMPOUND (TARPOON TOWERS II, LLC. SITE #CT1209 "WINDSOR")
B	LIMITS OF VERIZON'S PROP. 12'-0" x 21'-0" (252 S.F.) LEASE AREA/EQUIPMENT PAD (TYP.)
C	EXIST. 7'-9" CHAIN-LINK FENCE SURROUNDING EXIST. 49'-6" x 50'-0" (2,475 S.F.) EQUIPMENT COMPOUND (TYP.)
3 AD2	PROP. VERIZON (2)-LOW INDUCTANCE #12 HYBRID SIGNAL CABLES ROUTED ALONG PROP. OVERHEAD CABLE ICE BRIDGE (TYP.) FROM VERIZON'S PROP. EQUIPMENT PAD TO EXIST. MONOPOLE AS SHOWN.
E	EXIST. 135' MONOPOLE
3 RF01	PROP. VERIZON GPS ANTENNA MOUNTED TO PROP. OVERHEAD CABLE ICE BRIDGE. TOP OF GPS ANTENNA SHALL BE MOUNTED 2'-0" ABOVE TOP OF ICE BRIDGE.
G	EXIST. GRAVEL COVER WITHIN EXIST. COMPOUND
H	EXIST. 12' DOUBLE LEAF GATE
8 S01	PROP. VERIZON 12'-0" x 21'-0" (252 S.F.) REINFORCED CONCRETE EQUIPMENT PAD
1-4 S01	PROP. VERIZON 12'-0" x 11'-10" (148 S.F.) METAL DECK ICE SHIELD (SHOWN TRANSPARENT FOR CLARITY) ABOVE PROP. EQUIPMENT
K	EXIST. VACANT METER SOCKET AND DISCONNECT BREAKER W/DOORCUT TO BE UTILIZED FOR VERIZON'S PROP. 200A ELECTRIC SERVICE TO PROP. EQUIPMENT INSTALLATION.
L	EXIST. 200A 1Φ-3W 120/240 VAC ELECTRIC METER BANK
1.2 AD2	PROP. VERIZON EQUIPMENT CABINET MOUNTED TO PROP. 12'-0" x 21'-0" (252 S.F.) REINFORCED CONCRETE EQUIPMENT PAD (TYP.)
1 ED1	PROP. VERIZON 50 KW BACK-UP DIESEL GENERATOR MOUNTED TO PROP. 12'-0" x 21'-0" (252 S.F.) REINFORCED CONCRETE PAD
D	PROP. VERIZON 12' WIDE ACCESS EASEMENT (OVER EXIST. PAVED DRIVEWAY/TRIWELED HWY) FROM EXIST. PUBLIC RIGHT-OF-WAY (PROSPECT HILL ROAD), TO EXIST. EQUIPMENT COMPOUND (TO BE UTILIZED BY VERIZON FOR ACCESS TO VERIZON'S PROP. INSTALLATION). SEE SHEET C01 FOR CONTINUATION TO PROSPECT HILL ROAD.
P	PROP. VERIZON 12' x 20' PARKING SPACE OR TURN-AROUND AREA
Q	EXIST. DISH WIRELESS EQUIPMENT CABINET ON EXIST. 5'-0" x 7'-0" (35 S.F.) STEEL EQUIPMENT PLATFORM
R	EXIST. T-MOBILE EQUIPMENT CABINET ON EXIST. 10'-0" x 20'-0" (200 S.F.) CONCRETE PAD (TYP.)
S	EXIST. GROUND TEST WELL
T	EXIST. BOLLARD (TYP.)
U	EXIST. ELECTRIC TRANSFORMER ON EXIST. CONCRETE PAD/Vault
V	EXIST. TELCO HANDHOLE
W	EXIST. OVERHEAD CABLE ICE BRIDGE OF OTHERS (TYP.)
X	EXIST. GRAVEL COVER
Y	EXIST. PAVED ACCESS ROAD
Z	EXIST. ASPHALT CURB (TYP.)
MA	EXIST. PARKING STRIPE (TYP.)
MB	EXIST. MANHOLE
MC	EXIST. BUILDING #B00

CLIENT:

ARCHITECT/ENGINEER:

 R.K. EXECUTIVE CENTRE
 201 BOSTON POST ROAD WEST
 SUITE 101
 MARLBOROUGH, MA 01752
 (508) 481-7400
 www.chappellengineering.com

SEAL:

 ENGINEER/LAND SURVEYOR _____ DATE _____

DRAWING SCALE NOTE:
 THESE DRAWINGS HAVE BEEN PREPARED IN ACH D (24"x36") FORMAT. AS SUCH, THE WRITTEN SCALES SHOWN ON ANY REPRODUCTIONS OF A CONSTRUCTION SET SHALL BE REPRODUCED EXACTLY. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED. WHERE IN CONFLICT, DIMENSIONS SHALL SUPERSEDE WRITTEN SCALES.
 IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT.

REVISIONS		
NO.	DESCRIPTION	DATE
0	ISSUED FOR REVIEW	4/26/23
1	ISSUED FOR CONSTRUCTION (FINAL)	4/26/23
2	REVISED PER (5/9/23) TSA	5/16/23

PROJECT NAME:
WINDSOR 4 CT
 780 PROSPECT HILL ROAD
 WINDSOR, CT 06095

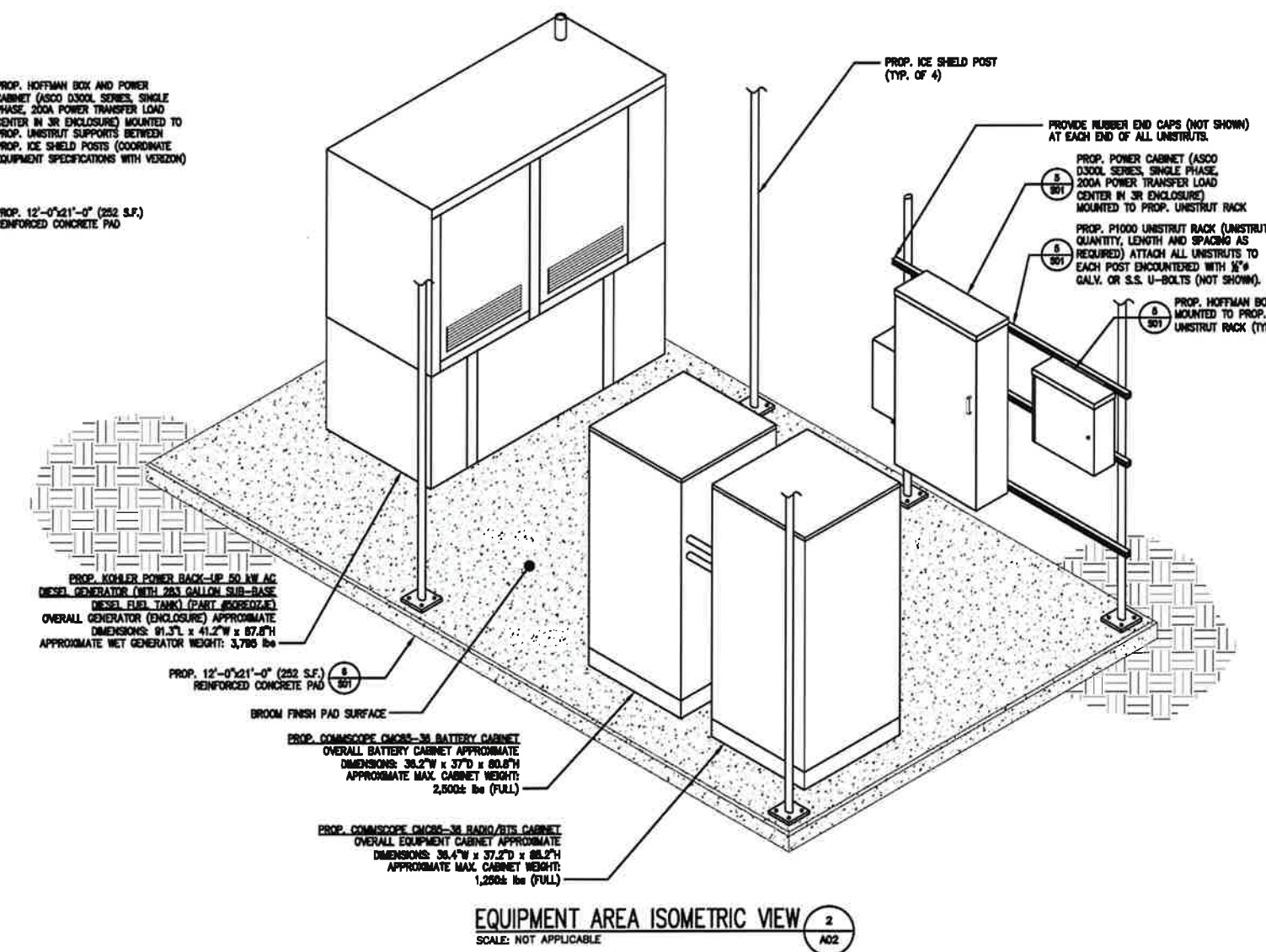
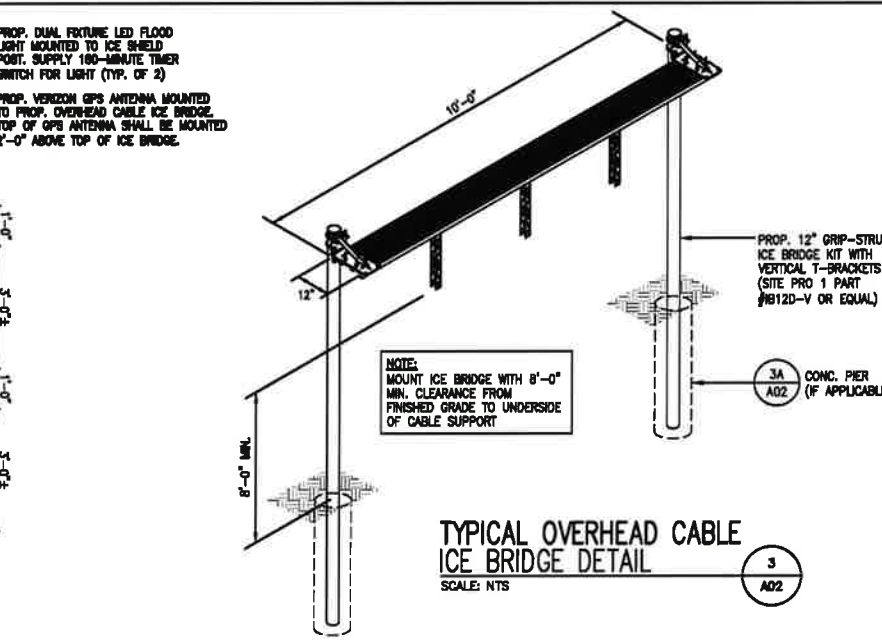
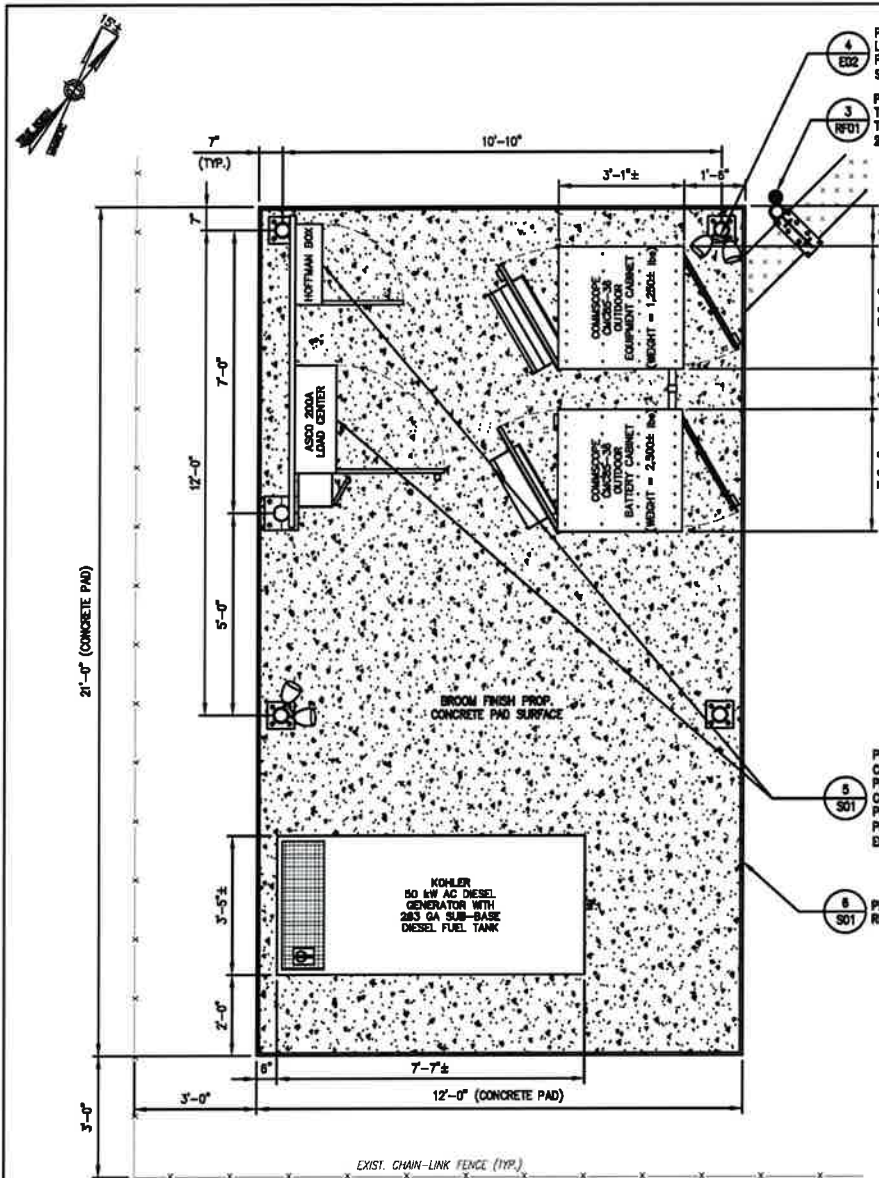
DRAWING TITLE:
EQUIPMENT COMPOUND PLAN

DRAWING NO:
A01

SCALE: 3/16" = 1'-0"	DESIGNED BY: MIC DRAWN BY: MIC CHECKED BY: GEB	VIZ PROJECT CODE: 2023241628 VIZ PROJECT NO.: 1899214
PER 1A SURVEY OF OTHERS	DATE: 4/26/23	MOD. LOCATION ID: 5000207278

● SITE CONTROL POINT:
 CENTER OF EXISTING MONOPOLE
 N 41°-52'-58.47" (41.862908°) (NAD 83)
 W 72°-42'-29.14" (72.708094°) (NAD 83)
 GROUND ELEVATION - 174.0' AMSL (NAVD '88)
 PER 1A SURVEY OF OTHERS

EQUIPMENT COMPOUND PLAN 1
 SCALE: 3/16" = 1'-0"



CLIENT:
verizon
Business Support Services

ARCHITECT/ENGINEER:
CHAPPELL ENGINEERING ASSOCIATES, LLC
Civil Structural Land Surveying
R.K. EXECUTIVE CENTRE
201 BOSTON POST ROAD WEST
SUITE 101
MARLBOROUGH, MA 01752
(508) 481-7400
www.chappellengineering.com

SEAL:

ENGINEER/LAND SURVEYOR DATE

DRAWING SCALE NOTE:
THESE DRAWINGS HAVE BEEN PREPARED IN ARCH D (DWG) FORMAT. AS SUCH, THE WRITTEN SCALES SHOWN ON ANY REPRODUCTIONS OF A CONVENTIONAL SIZE SHALL BE RENDERED NULL. ALL DIM SCALES MAY BE USED REGARDLESS OF REPRODUCTION SIZE. WHERE IN CONFLICT, DIM SCALES SHALL SUPERSEDE WRITTEN SCALES.
IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT.

REVISIONS

NO.	DESCRIPTION	DATE
0	ISSUED FOR REVIEW	4/28/23
1	ISSUED FOR CONSTRUCTION (FINAL)	4/28/23
2	REVISED PER (5/9/23) TSA	5/18/23

PROJECT NAME:
WINDSOR 4 CT
780 PROSPECT HILL ROAD
WINDSOR, CT 06095

DRAWING TITLE:
EQUIPMENT AREA PLAN & DETAILS

DRAWING NO.:
A02

SCALE:	DESIGNED BY:	VIEW PROJECT CODE:
AS SHOWN	MMB	20230415025
	CHKD BY:	VIEW PROJECT NO.:
	MMB	19999214
06210.418	ORIGINAL ISSUE DATE:	MDG LOCATION ID:
	4/28/23	500020727B

REVISIONS

NO.	DESCRIPTION	DATE
0	ISSUED FOR REVIEW	4/28/23
1	ISSUED FOR CONSTRUCTION (FINAL)	4/28/23
2	REVISED PER (5/9/23) TSA	5/16/23

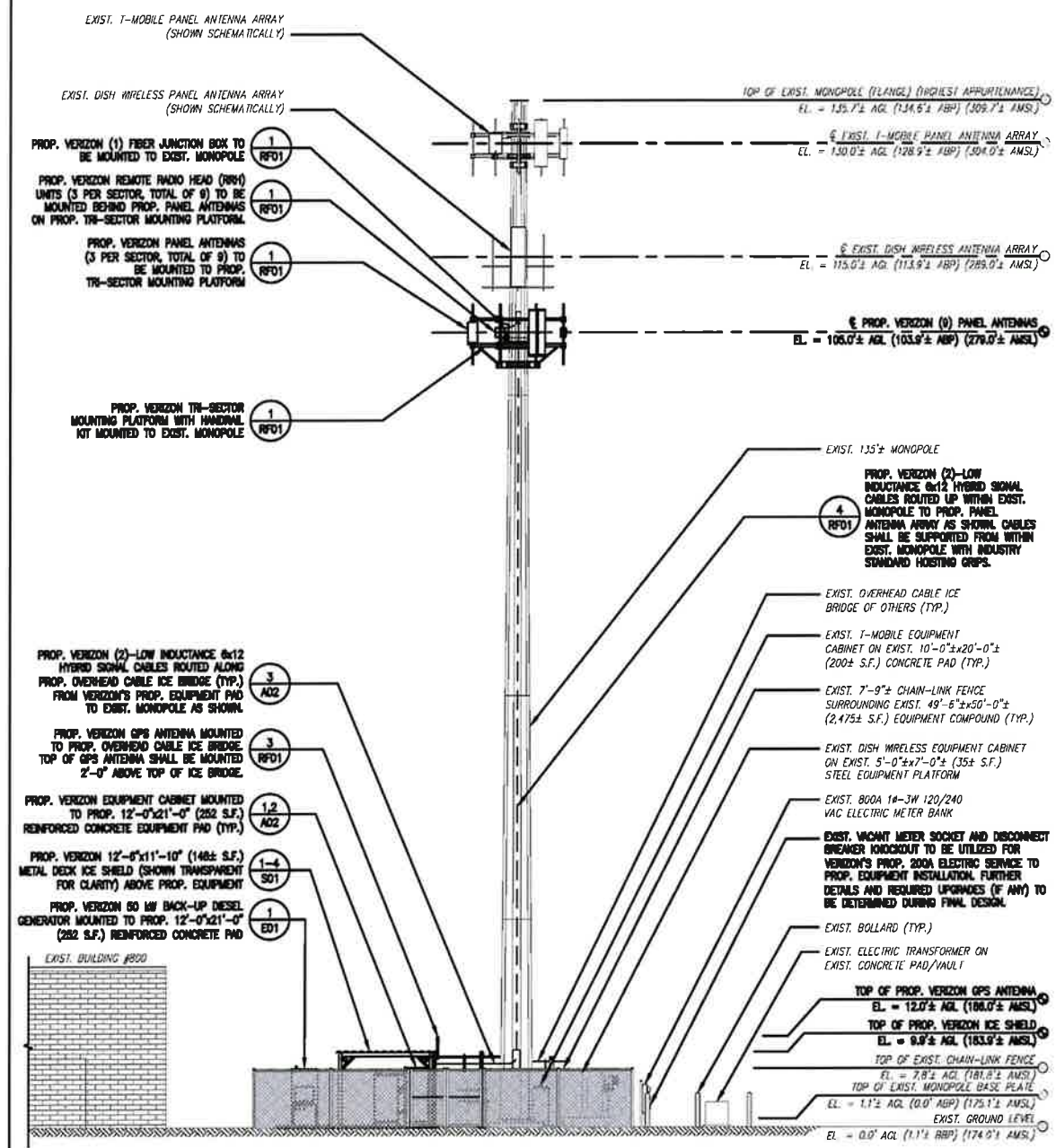
PROJECT NAME:
WINDSOR 4 CT
 780 PROSPECT HILL ROAD
 WINDSOR, CT 06095

DRAWING TITLE:
**NORTHEAST AND
 SOUTHWEST EQUIPMENT
 COMPOUND ELEVATIONS**

DRAWING NO.:
A03

SCALE: 1" = 10'	DESIGNED BY: HMC	VIEW PROJECT CODE: 00232415636
DATE PROJECT NO.: 06210.416	CHECKED BY: GRS	VIEW PROJECT NO.: 10009214
	ORIGINAL ISSUE DATE: 4/28/23	MOI LOCATION ID: 5000207278

NOTE:
 MONOPOLE AND APPURTENANCES SHOWN
 SCHEMATICALLY OR NOT SHOWN FOR CLARITY.

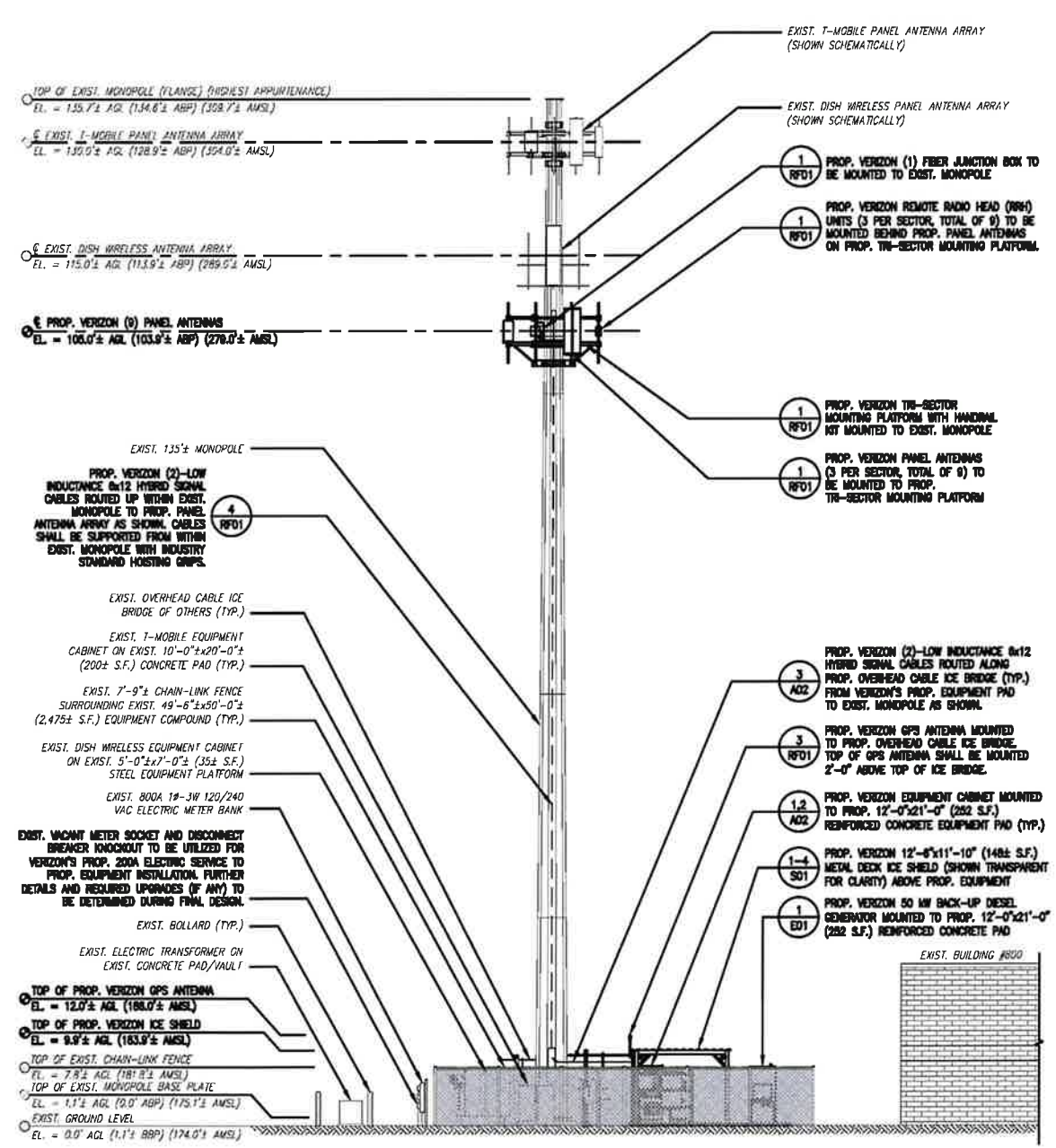


NORTHEAST EQUIPMENT COMPOUND ELEVATION 1
 SCALE: 1" = 10'
 0 5' 10' 20' 30'

LEGEND

AGL	ABOVE GROUND LEVEL
ABP	ABOVE MONOPOLE BASE PLATE
BBP	BELOW MONOPOLE BASE PLATE
AMSL	ABOVE MEAN SEA LEVEL

NOTE:
 MONOPOLE AND APPURTENANCES SHOWN
 SCHEMATICALLY OR NOT SHOWN FOR CLARITY.



SOUTHWEST EQUIPMENT COMPOUND ELEVATION 2
 SCALE: 1" = 10'
 0 5' 10' 20' 30'



ARCHITECT/ENGINEER:
CHAPPELL ENGINEERING ASSOCIATES, LLC
 Civil Structural Land Surveying
 R.K. EXECUTIVE CENTRE
 201 BOSTON POST ROAD WEST
 SUITE 101
 MARLBOROUGH, MA 01752
 (508) 481-7400
 www.chappellengineering.com

SEAL:

 ENGINEER/LAND SURVEYOR DATE

DRAWING SCALE NOTE:
 THESE DRAWINGS HAVE BEEN PREPARED IN ARCH D (24"X36") FORMAT. AS SUCH, THE WRITTEN SCALES SHOWN ON ANY REPRODUCTIONS OF A CONSTRUCTION SET SHALL BE REFERENCED IN ALL. ALL WRITTEN SCALES MAY BE USED REGARDLESS OF REPRODUCTION SIZE. WHERE IN CONFLICT, WRITTEN SCALES SHALL SUPERSEDE WRITTEN SCALES.
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REVISIONS

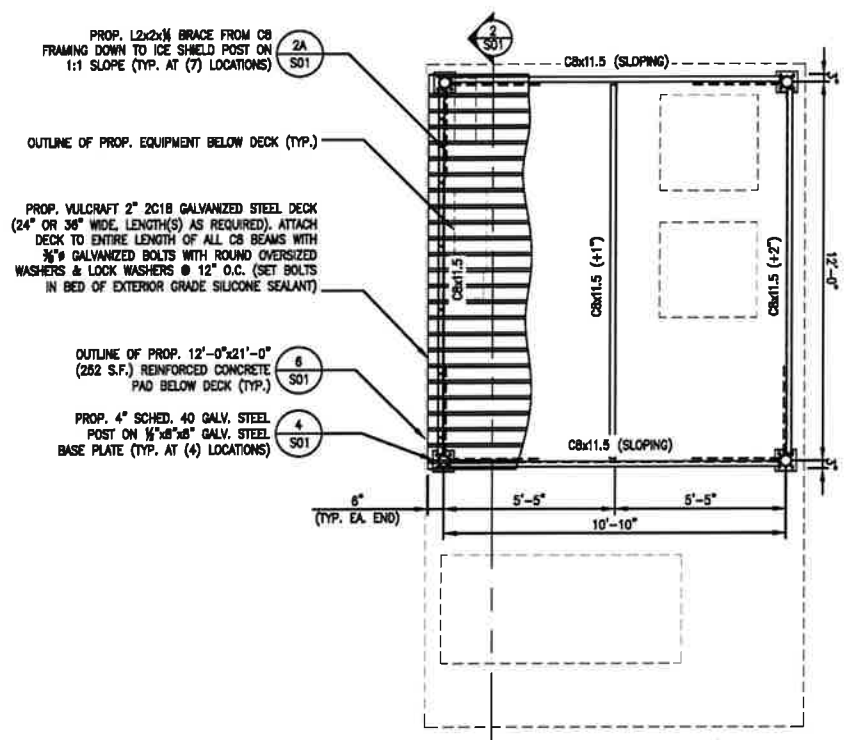
NO.	DESCRIPTION	DATE
0	ISSUED FOR REVIEW	4/28/23
1	ISSUED FOR CONSTRUCTION (FINAL)	4/28/23
2	REVISED PER (5/8/23) TSA	5/16/23

PROJECT NAME:
WINDSOR 4 CT
 780 PROSPECT HILL ROAD
 WINDSOR, CT 06095

DRAWING TITLE:
ICE SHIELD FRAMING PLAN & STRUCTURAL DETAILS

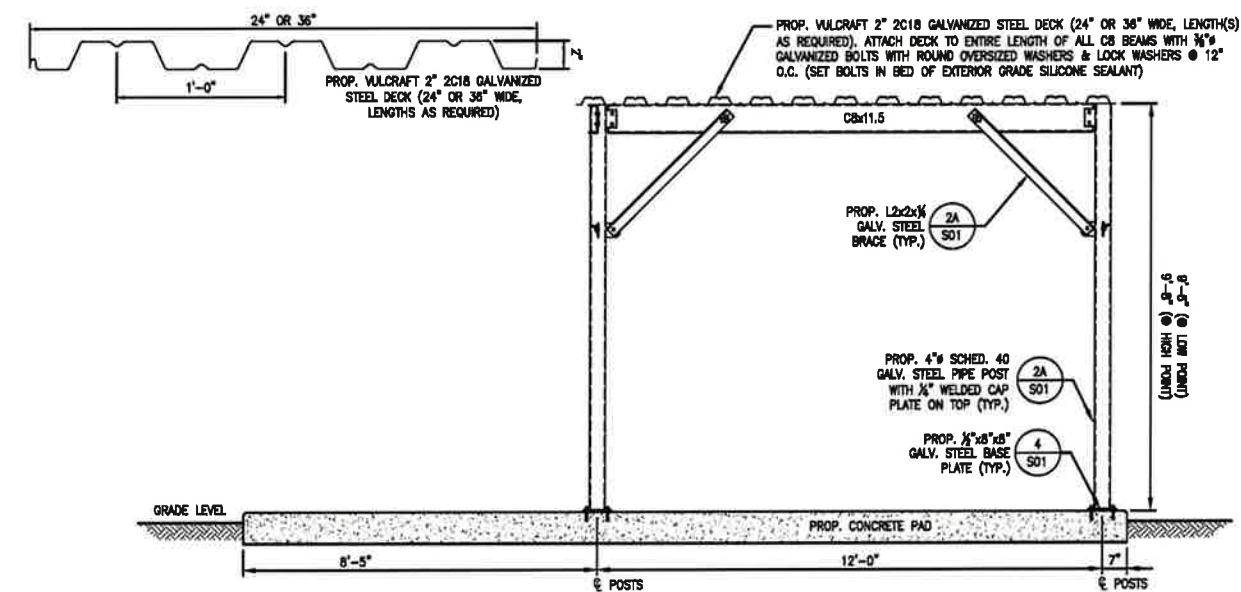
DRAWING NO.:
S01

SCALE: AS SHOWN	DESIGNED BY: MNC	VIEW PROJECT CODE: 2023-115028
OWNER: VERIZON	CHECKED BY: GMS	VIEW PROJECT NO.: 1899214
DATE: 4/28/23	DATE: 4/28/23	NO. LOCATION ID: 5000207278

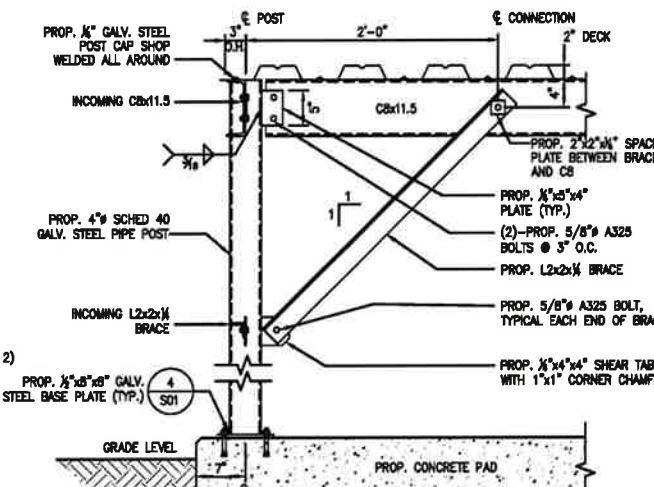


FRAMING PLAN NOTES:
 1.) ALL STEEL SHALL BE INSTALLED LEVEL UNLESS OTHERWISE NOTED.
 2.) TOP OF NEW STEEL ELEVATION SHALL BE HELD 9'-0" ABOVE EQUIPMENT PAD SURFACE UNLESS OTHERWISE NOTED THUS (±X") INDICATING DISTANCE ABOVE OR BELOW TOP OF STEEL REFERENCE ELEVATION.

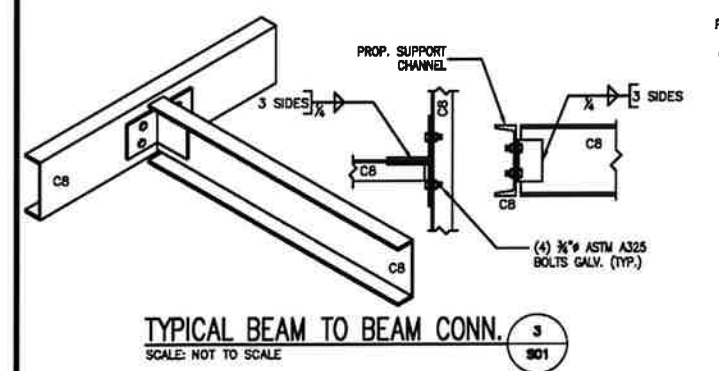
ICE SHIELD FRAMING PLAN (1)
 SCALE: 3/8" = 1'-0"
 NORTH



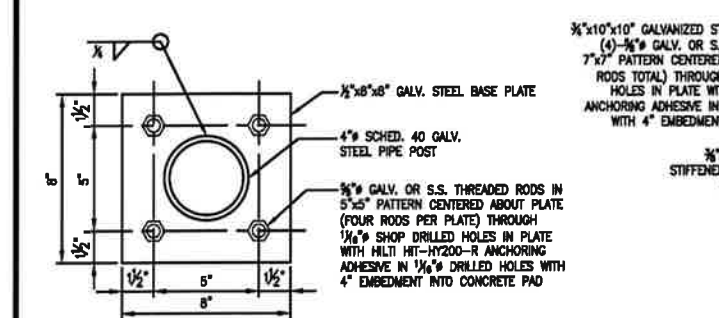
ICE SHIELD SECTION (2)
 SCALE: 1/2" = 1'-0"



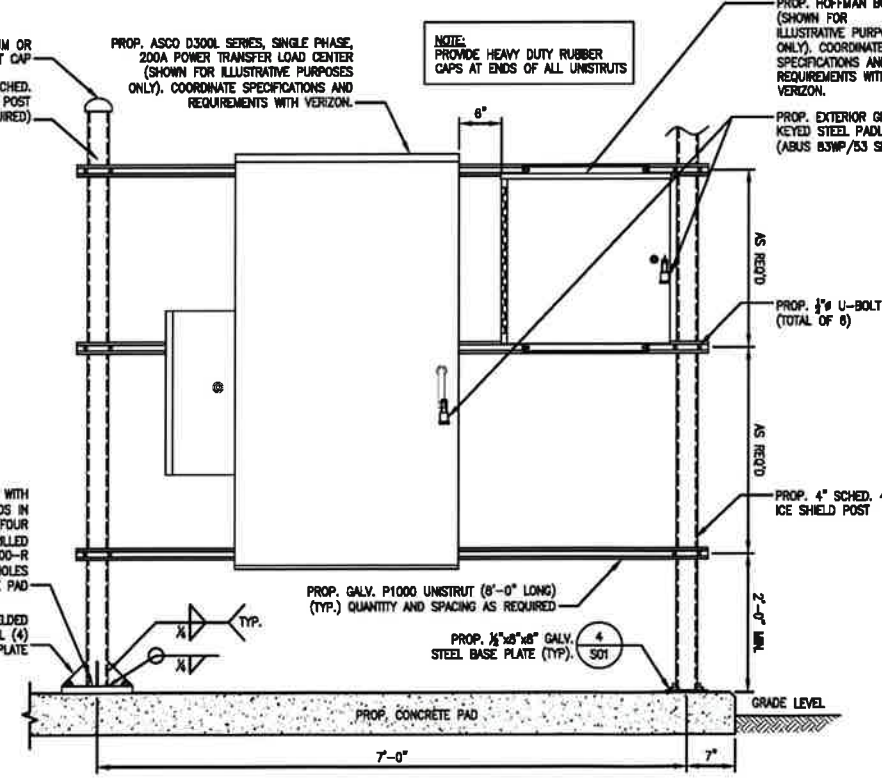
TYPICAL ICE SHIELD POST DETAIL (2A)
 SCALE: 1" = 1'-0"



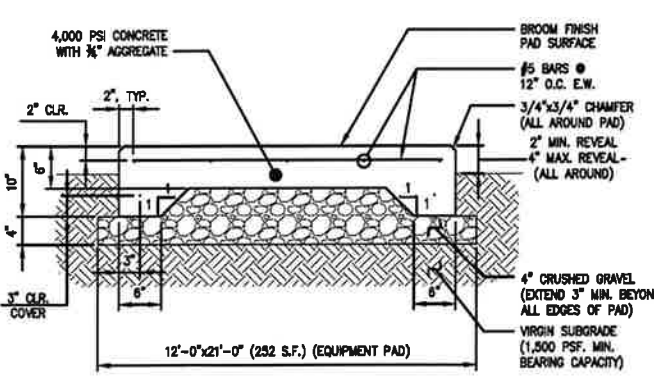
TYPICAL BEAM TO BEAM CONN. (3)
 SCALE: NOT TO SCALE



TYPICAL ICE SHIELD POST BASE PLATE (4)
 SCALE: NONE




UNISTRUT RACK DETAIL (5)
 SCALE: N.T.S.



REINFORCED CONCRETE PAD DETAIL (6)
 SCALE: NONE

CLIENT:
verizon
Solutions | Service | Support

ARCHITECT/ENGINEER:
CHAPPELL ENGINEERING ASSOCIATES, LLC
Civil, Structural, Land Surveying
R.K. EXECUTIVE CENTRE
201 BOSTON POST ROAD WEST
SUITE 101
MARLBOROUGH, MA 01752
(508) 481-7400
www.chappellengineering.com

SEAL:

ENGINEER/LAND SURVEYOR DATE

DRAWING SCALE NOTE:
THESE DRAWINGS HAVE BEEN PREPARED IN ACH D (A) (30" X 42") FORM. AS SUCH, THE WRITTEN SCALES SHOWN ON ANY REPRODUCTIONS OF A COMMERCIAL SIZE SHALL BE RENDERED INVALID. ALL DIMENSIONS SHALL BE USED UNLESS OTHERWISE SPECIFIED. WHERE IN CONFLICT, DIMENSIONS SHALL SUPERSEDE WRITTEN SCALES.
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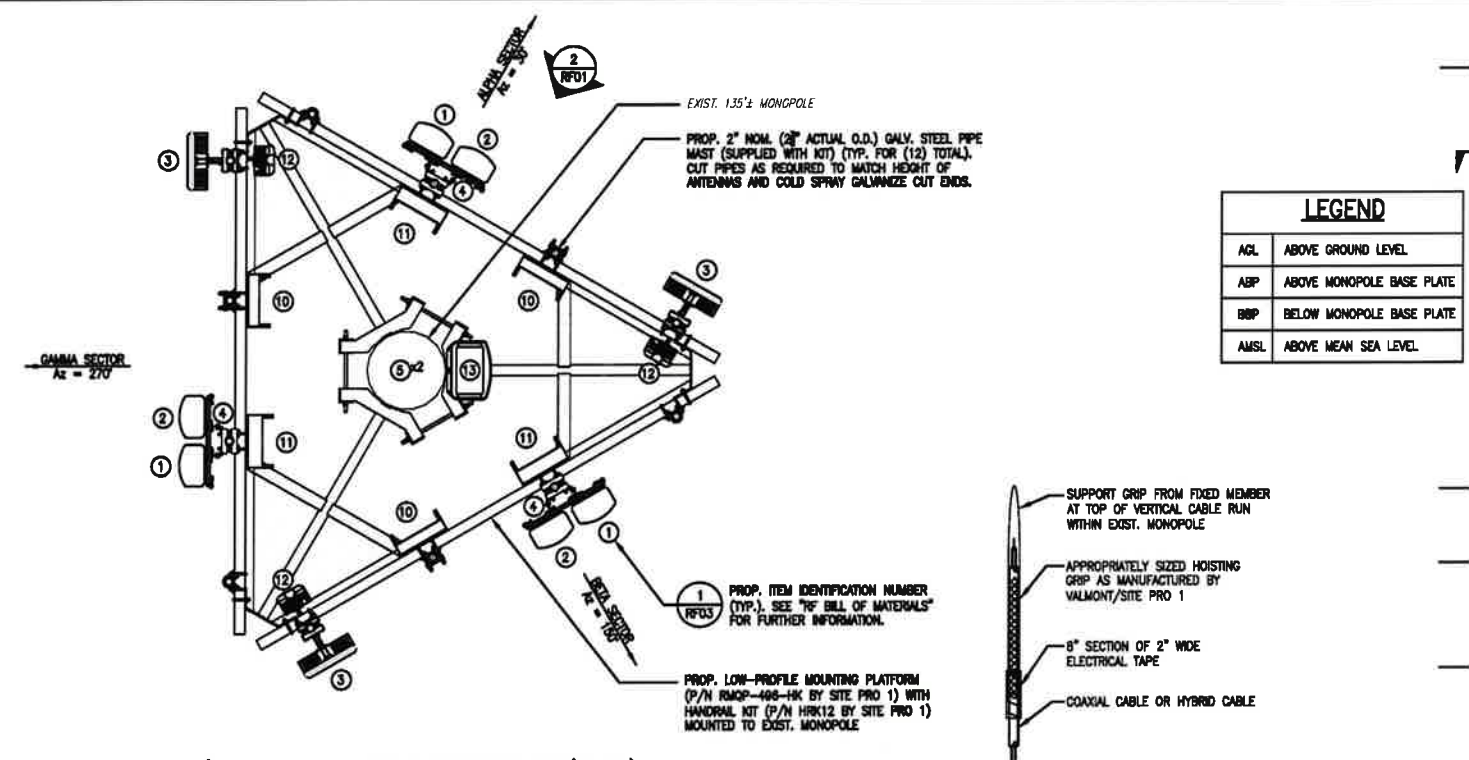
REVISIONS		
NO.	DESCRIPTION	DATE
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1	ISSUED FOR CONSTRUCTION (FINAL)	4/28/23
2	REVISED PER (5/9/23) TSA	5/16/23

PROJECT NAME:
WINDSOR 4 CT
780 PROSPECT HILL ROAD
WINDSOR, CT 06095

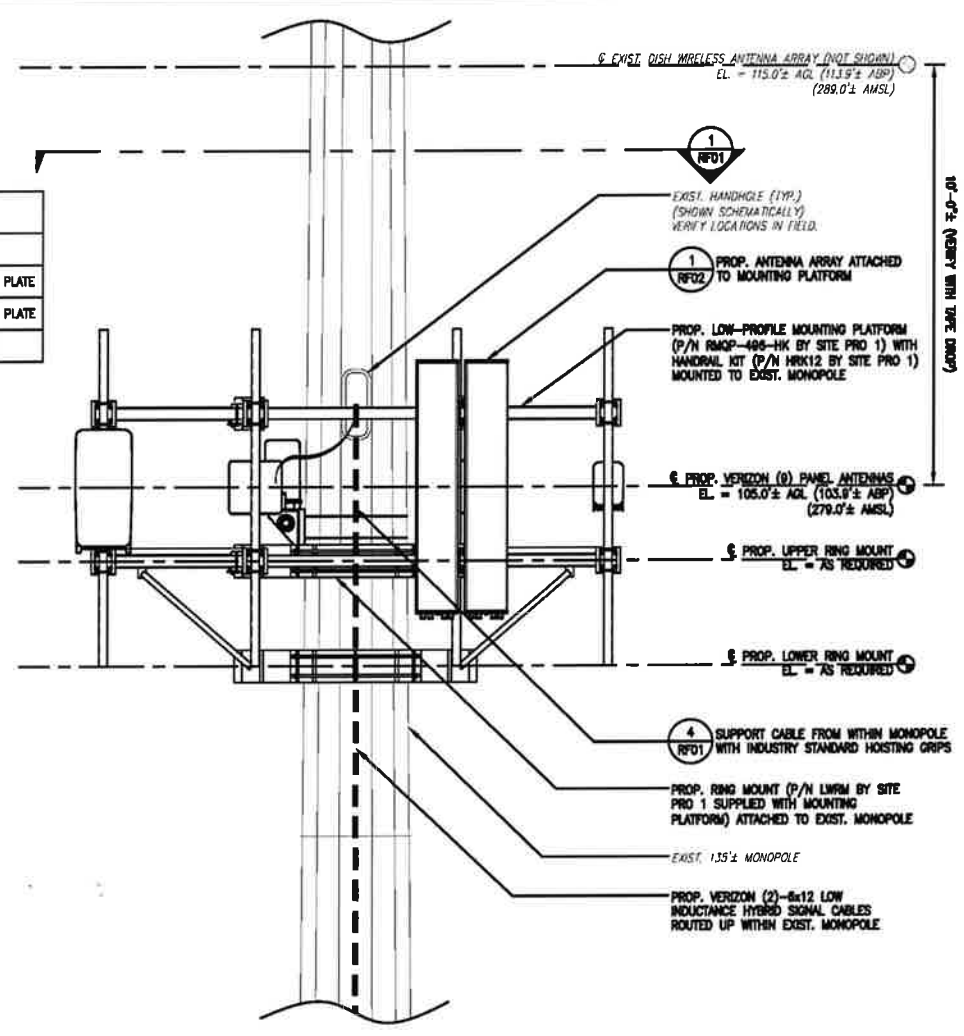
DRAWING TITLE:
ANTENNA MOUNTING PLAN AND DETAILS

DRAWING NO.:
RF01

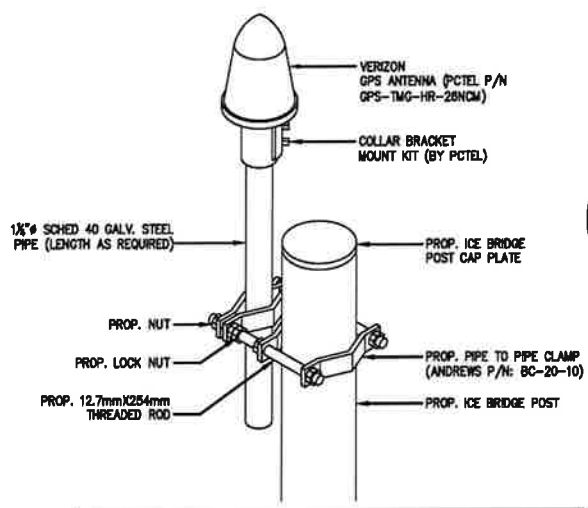
SCALE: AS SHOWN	DESIGNED BY: MRC CHECKED BY: GCB	VIEW PROJECT CODE: 20230415028
CEA PROJECT NO.: 08210.416	ORIGINAL ISSUE DATE: 4/28/23	VIEW PROJECT NO.: 16099214
		MDG LOCATION ID: 5000202728



(MONOPOLE PLAN VIEW AT ELEVATION 105.0'± AGL)
ANTENNA MOUNTING PLAN
SCALE: 1/2" = 1'-0"
RF01

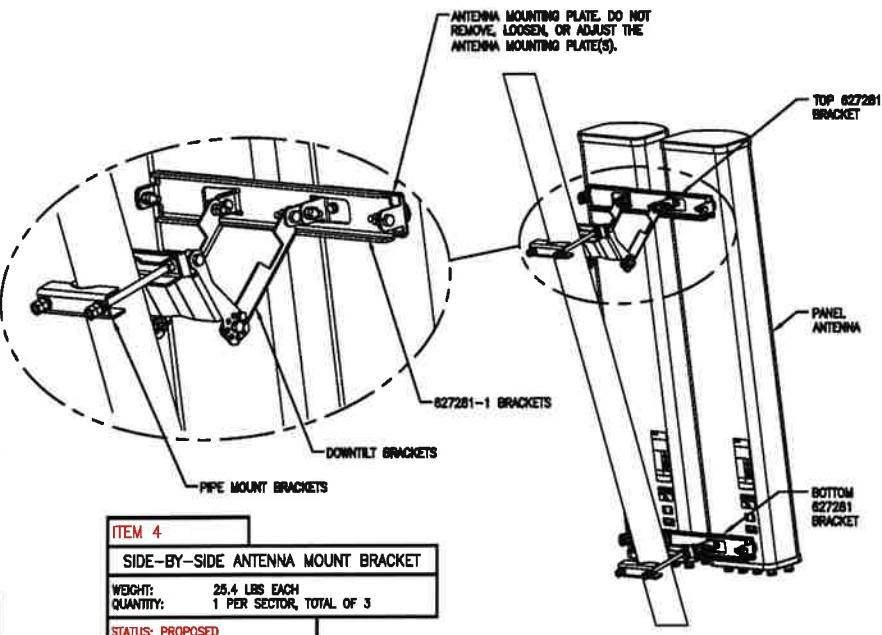


ANTENNA MOUNTING PLATFORM MOUNTING DETAIL
SCALE: 1/2" = 1'-0"
RF01



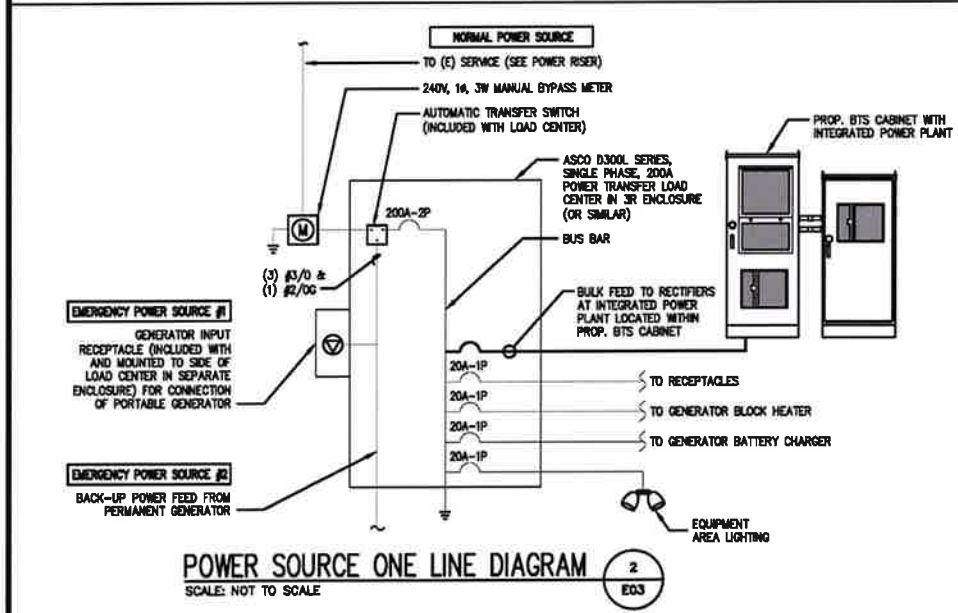
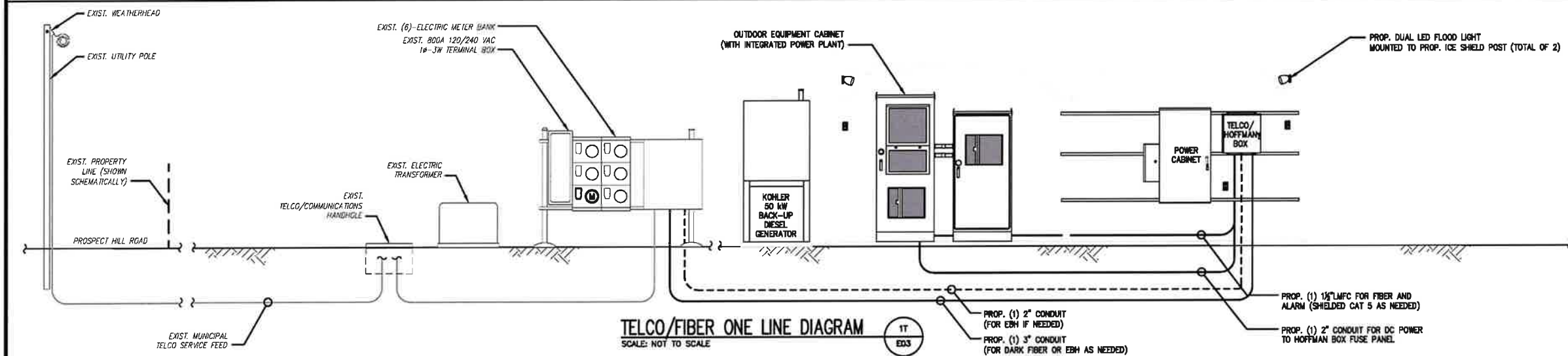
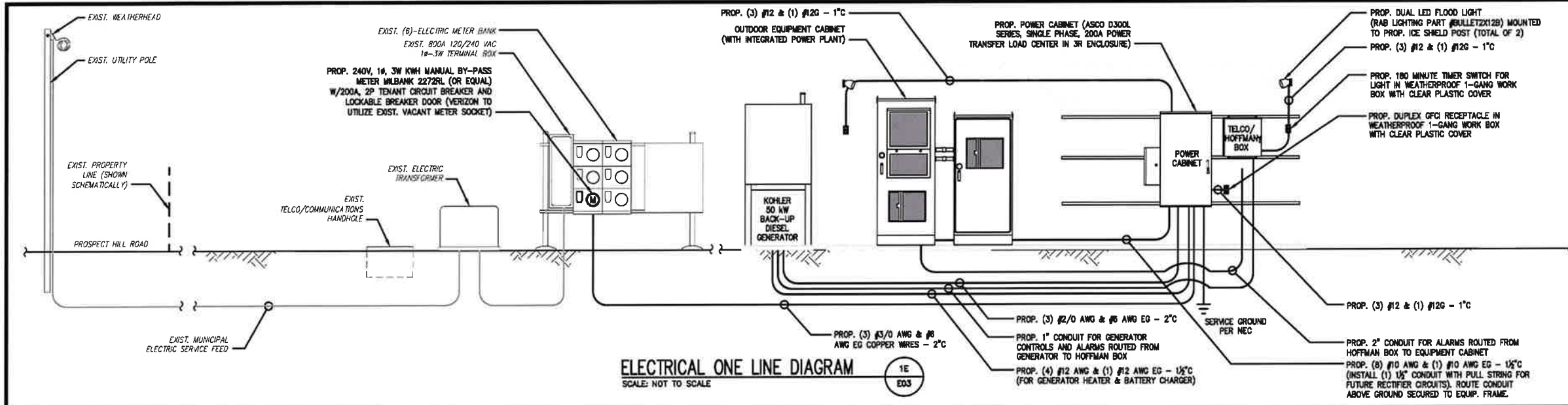
NOTE:
THE GPS ANTENNA MOUNT IS DESIGNED TO FASTEN TO A STANDARD 1"-1.5" DIAMETER GALVANIZED STEEL OR STAINLESS STEEL PIPE. THE PIPE MUST NOT BE THREADED AT THE ANTENNA MOUNT END. THE PIPE SHALL BE CUT TO THE REQUIRED LENGTH USING A HAND OR ROTARY PIPE CUTTER TO ASSURE A SMOOTH AND PERPENDICULAR CUT. THE CUT PIPE END SHALL BE DEBURRED AND SMOOTH IN ORDER TO SEAL AGAINST THE NEOPRENE GASKET ATTACHED TO THE ANTENNA MOUNT.

GPS ANTENNA MOUNTING DETAIL
SCALE: N.T.S.
RF01



ITEM 4
SIDE-BY-SIDE ANTENNA MOUNT BRACKET
WEIGHT: 25.4 LBS EACH
QUANTITY: 1 PER SECTOR, TOTAL OF 3
STATUS: PROPOSED

MOUNT ANTENNA IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDED PROCEDURE
TYPICAL SIDE-BY-SIDE ANTENNA MOUNT KIT (COMMSCOPE PART #BSAMNT-SBS-1-2)
SCALE: NOT TO SCALE
RF01



ELECTRICAL PANEL SCHEDULE 65,000 A.L.C. NEAR 3R

CKT #	DESCRIPTION	AMP	AMP	DESCRIPTION	CKT #
1	RECTIFIER #1	30	30	FUTURE RECTIFIER	2
3					4
5	RECTIFIER #2	30	30	FUTURE RECTIFIER	6
7					8
9	RECTIFIER #3	30	20	PAD LIGHTING	10
11				BLANK	12
13				BLANK	14
15	RECTIFIER #4	30		BLANK	16
17	GFCI RECEPTACLE/LIGHT	20		BLANK	18
18	GENERATOR BLOCK HEATER	20		BLANK	20
21	GENERATOR BATTERY CHARGER	20		BLANK	22
23	BLANK	-	-	BLANK	24
25	BLANK	-	-	BLANK	26
27	BLANK	-	-	BLANK	28
29	BLANK	-	-	BLANK	30

- ONE-LINE DIAGRAM NOTES:**
- 1) PROVIDE WEATHER TIGHT SEAL CONNECTORS ON ALL CONNECTIONS INSIDE AND OUT.
 - 2) COORDINATE ANY FURTHER MISCELLANEOUS WIRING AND CONDUIT REQUIREMENTS WITH VERIZON WIRELESS AND ELECTRIC COMPANY.
 - 3) ALL CONDUIT ROUTING SHOWN ON THESE DIAGRAMS IS SCHEMATIC IN NATURE AND INTENDED TO CONVEY GENERAL INTENT ONLY.
 - 4) ALL PROPOSED UTILITY DESIGN ELEMENTS SHOWN ARE SUBJECT TO CHANGE BASED ON FINAL DESIGN TO BE PROVIDED BY UTILITY PROVIDERS AND VERIZON WIRELESS. CONTRACTOR SHALL OBTAIN A COPY OF THE FINAL UTILITY DESIGN BY UTILITY COMPANY PRIOR TO COMMENCEMENT OF WORK.

UTILITY CONTACTS

ELECTRICAL: EVERSOURCE ENERGY
247 STATION DRIVE, SE 210
WESTWOOD, MA 02090
(781) 441-3610

TELEPHONE: VERIZON
185 FRANKLIN STREET
BOSTON, MA 02107
(800) 941-8800

MAKE ALL CONNECTIONS AS PER UTILITY COMPANY'S REQUIREMENTS.

CLIENT:
verizon
Wireless by Verizon Mobility

ARCHITECT/ENGINEER:
CHAPPELL ENGINEERING ASSOCIATES, LLC
Civil Structural Land Surveying

R.K. EXECUTIVE CENTRE
201 BOSTON POST ROAD WEST
SUITE 101
MARLBOROUGH, MA 01752
(508) 481-7400
www.chappellengineering.com

SEAL:

ENGINEER/LAND SURVEYOR _____ **DATE** _____

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REVISIONS

NO.	DESCRIPTION	DATE
0	ISSUED FOR REVIEW	4/26/23
1	ISSUED FOR CONSTRUCTION (FINAL)	4/26/23
2	REVISED PER (5/9/23) TSA	5/16/23

PROJECT NAME:
WINDSOR 4 CT
780 PROSPECT HILL ROAD
WINDSOR, CT 06095

DRAWING TITLE:
ELECTRICAL DIAGRAMS & DETAILS

DRAWING NO.:
E03

SCALE: AS SHOWN	DESIGNED BY: MHC	VIEW PROJECT CODE: 20230119028
CHECKED BY: GSB	CHECKED BY: GSB	NEW PROJECT NO.: 18999214
DATE: 4/26/23	DATE: 4/26/23	MOI LOCATION ID: 9000207278

ELECTRICAL PANEL SCHEDULE 3
SCALE: NTS



ARCHITECT/ENGINEER:
CHAPPELL ENGINEERING ASSOCIATES, LLC
Civil-Structural-Land Surveying
 R.K. EXECUTIVE CENTRE
 201 BOSTON POST ROAD WEST
 SUITE 101
 MARLBOROUGH, MA 01752
 (508) 481-7400
 www.chappellengineering.com

SEAL:

ENGINEER/LAND SURVEYOR DATE

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REVISIONS

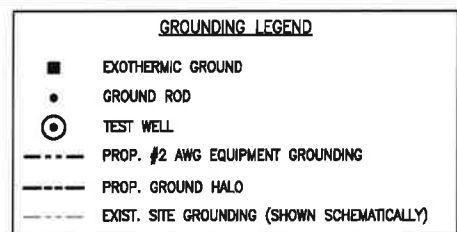
NO.	DESCRIPTION	DATE
0	ISSUED FOR REVIEW	4/26/23
1	ISSUED FOR CONSTRUCTION (FINAL)	4/26/23
2	REVISED PER (5/9/23) TSA	5/16/23

PROJECT NAME:
WINDSOR 4 CT
 780 PROSPECT HILL ROAD
 WINDSOR, CT 06095

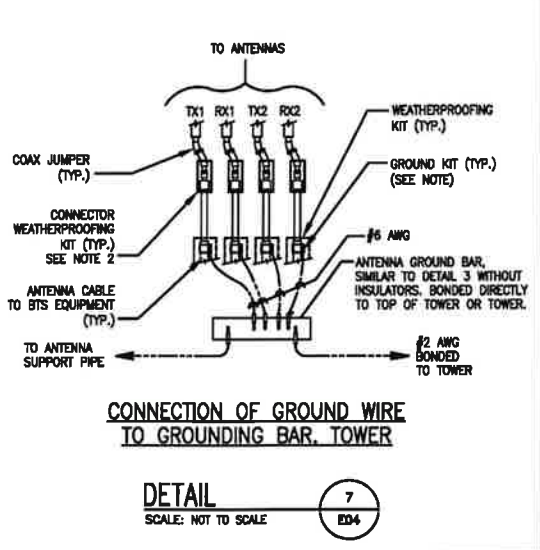
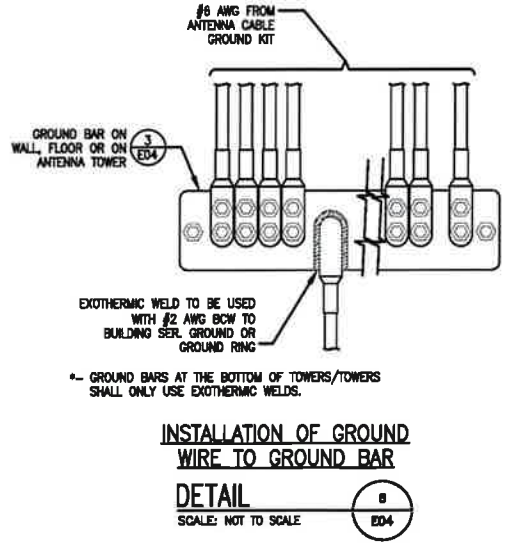
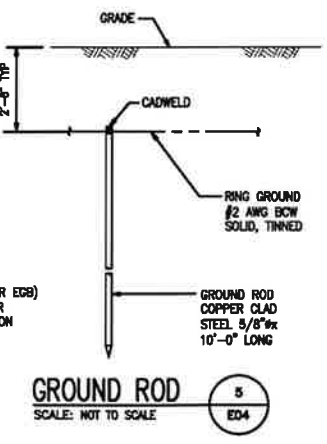
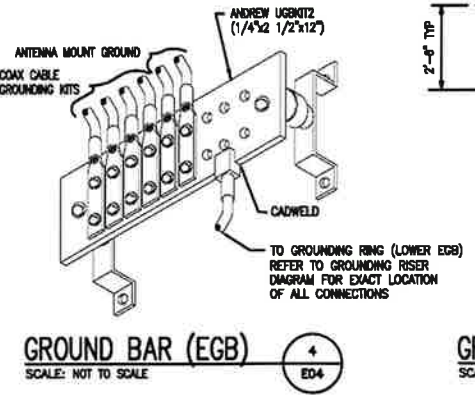
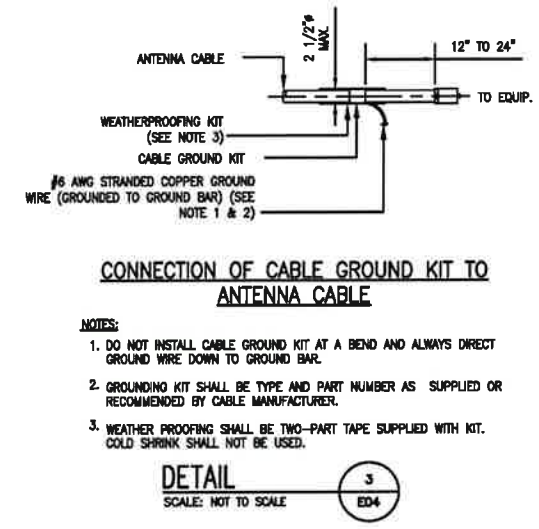
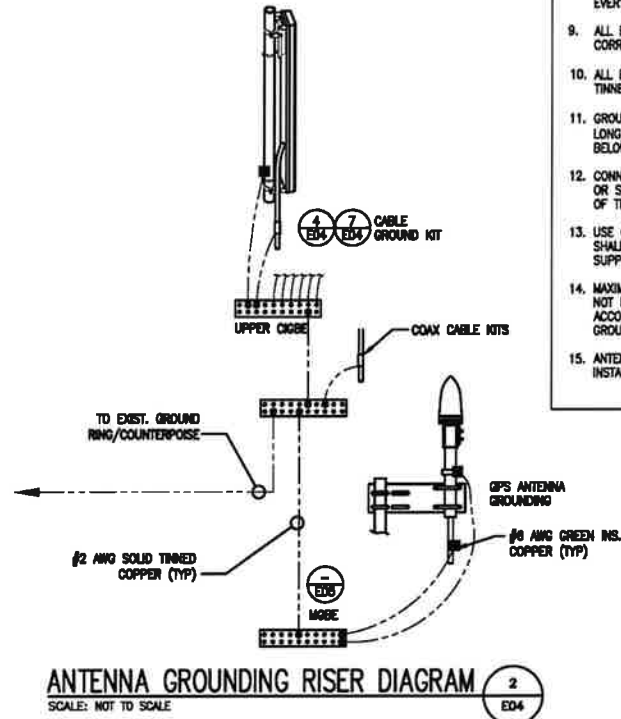
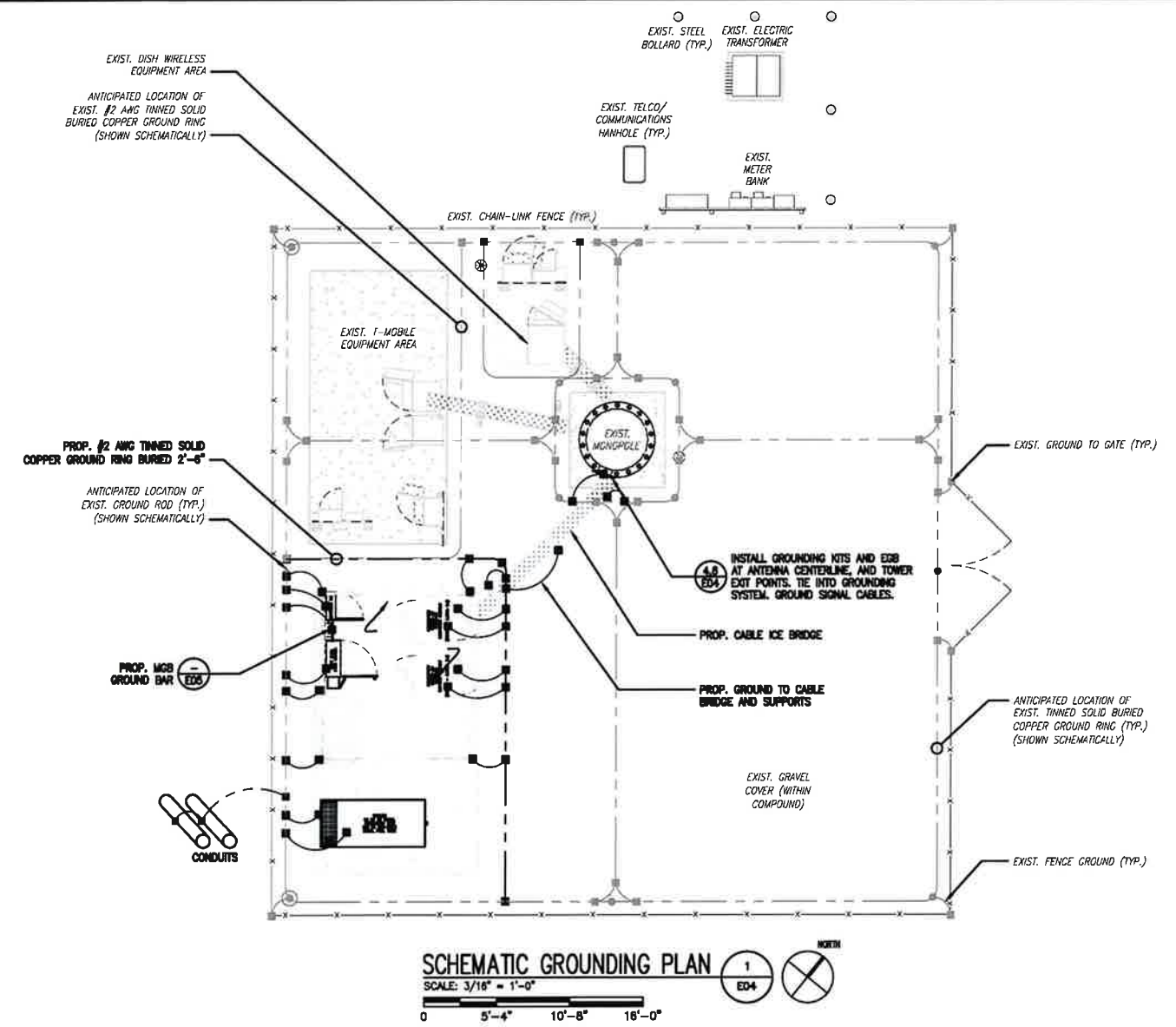
DRAWING TITLE:
SCHEMATIC GROUNDING PLAN & DETAILS

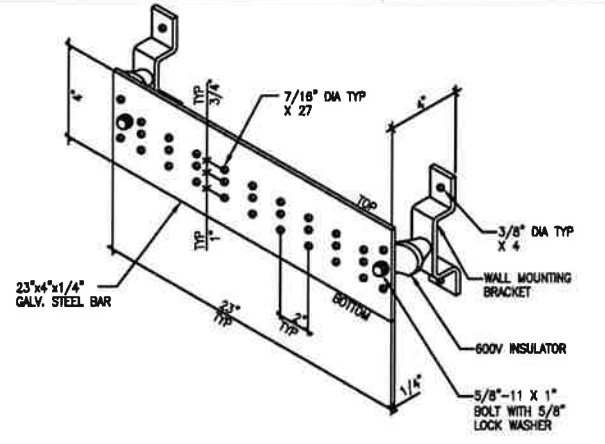
DRAWING NO.:
E04

SCALE: AS SHOWN	DESIGNED BY: MRC DRAWN BY: MRC CHECKED BY: GMS	VDR PROJECT CODE: 20232415628 VDR PROJECT NO. 18895214
SEA PROJECT NO.: 98210.418	ORIGINAL ISSUE DATE: 4/28/23	MDG LOCATION EX: 5000207278



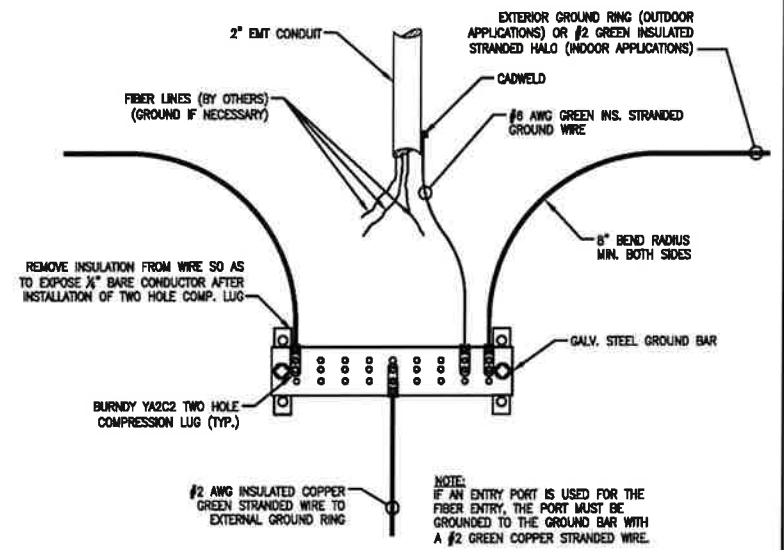
- ELECTRICAL AND GROUNDING NOTES:**
- ELECTRICAL**
- ALL ELECTRICAL WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS AND ALL APPLICABLE LOCAL CODES.
 - CONDUIT ROUTINGS ARE SCHEMATIC. SUBCONTRACTOR SHALL INSTALL CONDUITS SO THAT ACCESS TO EQUIPMENT IS NOT BLOCKED.
 - SERVICE TO EQUIP. SHALL BE 120/240 VAC, 200 AMP, 1ϕ, 60 Hz.
 - THE SUBCONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENCING GROUNDING AND UNDERGROUND CONDUIT INSTALLATION AS TO PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO THE CONDUIT.
- GROUNDING**
- COMPRESSION GROUND CONNECTIONS MAY BE REPLACED BY EXOTHERMIC (CADWELD) CONNECTIONS.
 - ALL GROUND CONNECTIONS BELOW GRADE SHALL BE EXOTHERMIC (CADWELD).
 - ALL GROUND CONNECTIONS ABOVE GRADE (INTERIOR & EXTERIOR) SHALL BE FORMED USING HIGH PRESS CRIMPS.
 - ALL EXOTHERMIC CONNECTIONS TO THE GROUND RODS SHALL START AT THE TOP & HAVE A VERTICAL SEPARATION OF 8" FOR EVERY ADDITIONAL CONNECTION.
 - ALL EXTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERIAL.
 - ALL EXTERIOR GROUND CONDUCTORS SHALL BE #2 AWG SOLID TINNED COPPER UNLESS OTHERWISE INDICATED.
 - GROUND RODS SHALL BE COPPER CLAD STEEL, 5/8" 10-FT. LONG, AND SHALL BE DRIVEN VERTICALLY WITH THEIR TOPS 48" BELOW FINAL GRADE.
 - CONNECTIONS TO THE GROUND BUS SHALL NOT BE DOUBLED UP OR STACKED. BACK TO BACK CONNECTIONS ON OPPOSITE SIDES OF THE GROUND BUS ARE PERMITTED.
 - USE OF 90° BENDS IN THE PROTECTION GROUNDING CONDUCTORS SHALL BE AVOIDED WHEN 45° BENDS CAN BE ADEQUATELY SUPPORTED.
 - MAXIMUM RESISTANCE OF THE COMPLETED GROUND SYSTEM SHALL NOT EXCEED 5 OHMS. TESTING SHALL BE PERFORMED IN ACCORDANCE WITH PROJECT SPECIFICATION FOR FACILITY GROUNDING, USING FALL OF POTENTIAL METHOD.
 - ANTENNA GROUND KITS SHALL BE FURNISHED BY VERIZON AND INSTALLED BY CONTRACTOR.



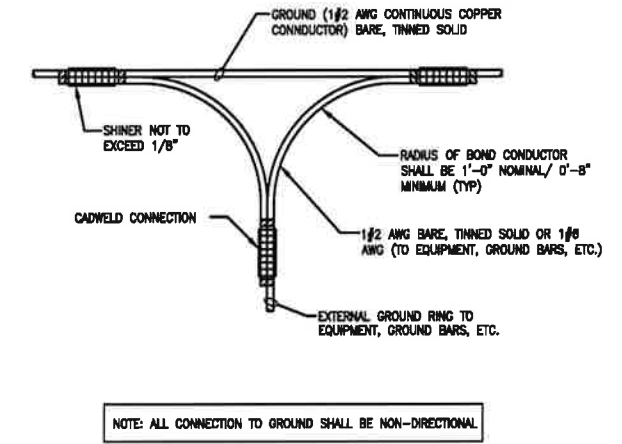


1. **SURFACE PREPARATION:** ALL CONNECTIONS MADE TO BARE METAL ALL PAINTED SURFACES SHALL BE MADE BARE TO ENSURE PROPER CONTACT. NO WASHERS SHALL BE ALLOWED BETWEEN THE ITEMS BEING GROUNDED. ALL CONNECTIONS SHALL HAVE AN ANTI-OXIDANT AGENT APPLIED PRIOR TO INSTALLATION.
 2. **BUSSES PREPARATION:** ALL GALV. STEEL BUSSES SHALL BE CLEANED, POLISHED AND AN ANTI-OXIDANT APPLIED. NO FINGERPRINTS OR DISCOLORED STEEL WILL BE PERMITTED.
 3. **TERMINATIONS:** ALL EQUIPMENT TERMINATIONS SHALL BE MADE WITH A BURNDY TWO HOLE COMPRESSION LUG WITH 10-24x3/4" LONG S.S. SCREWS, NUTS AND LOCK WASHERS. ALL BUSS TERMINATIONS SHALL BE MADE WITH A CAD-WELD OR BURNDY YC2C2 2 HOLE COMPRESSION LUG OR EQUAL. ALL INTERIOR HALO ATTACHMENTS SHALL BE MADE USING A BURNDY YC2C2 COMPRESSION LUG.

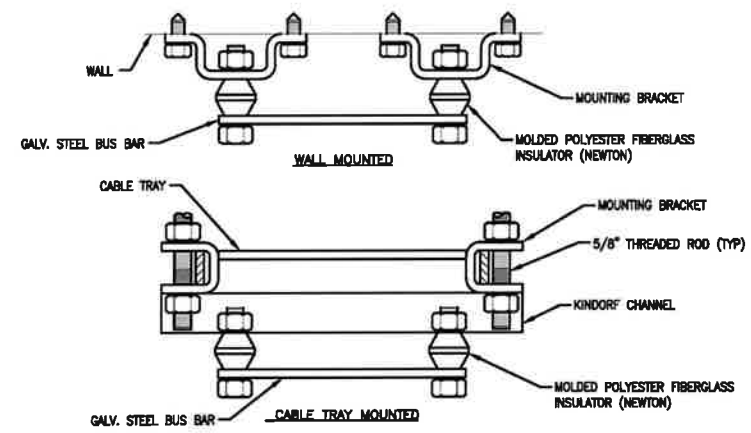
TYP. INTERIOR & EXTERIOR GROUND BAR
SCALE: N.T.S.



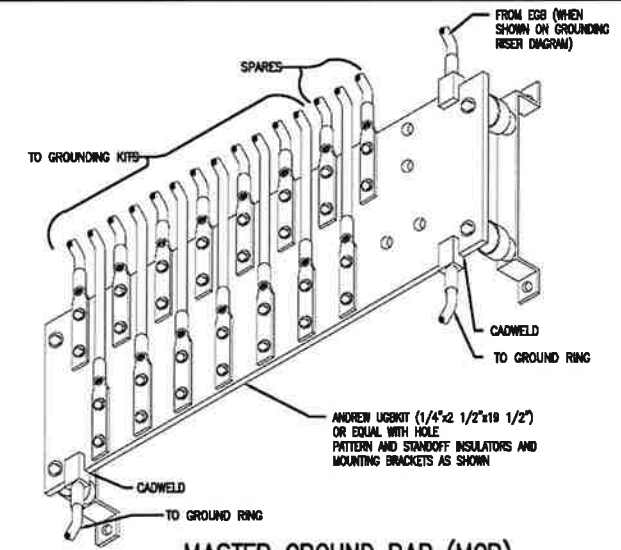
INTERIOR GROUNDING AT TELCO ENTRY
SCALE: N.T.S.



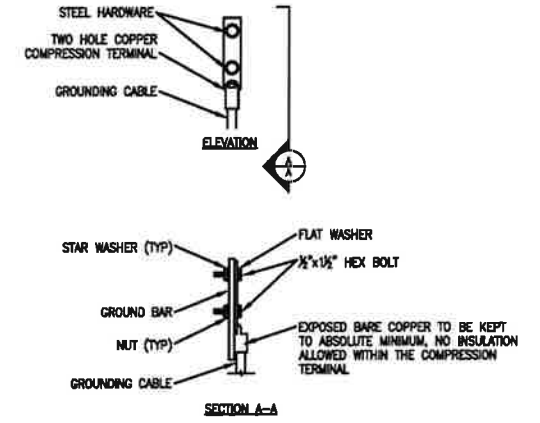
NON-DIRECTIONAL SPLICE
SCALE: N.T.S.



BUS BAR MOUNTING
SCALE: N.T.S.

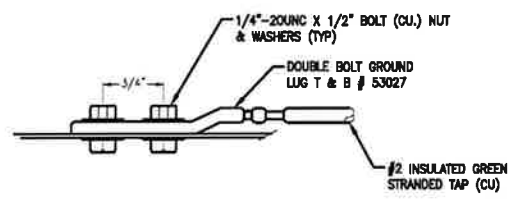


MASTER GROUND BAR (MGB)
SCALE: NOT TO SCALE

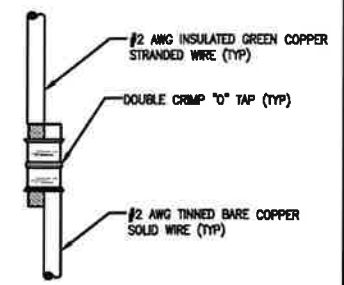


NOTE:
1. "DOUBLING UP" OR "STACKING" OF CONNECTION IS NOT PERMITTED.
2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATIONS.

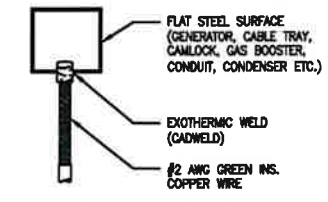
TYPICAL GROUND BAR CONNECTION DETAIL
SCALE: N.T.S.



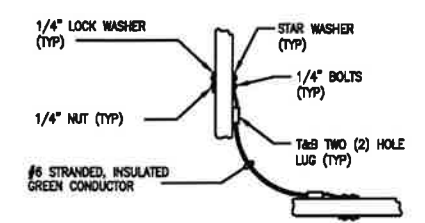
TYPICAL EQUIPMENT GROUND CONNECTION
SCALE: N.T.S.



TYPICAL GROUND CONNECTION SPLICE DETAIL
SCALE: N.T.S.



TYP. CADWELD #2 GREEN TO FLAT STEEL SURFACE
SCALE: NOT TO SCALE



CABLE TRAY GROUNDING
SCALE: N.T.S.

CLIENT:
verizon
Verizon Wireless

ARCHITECT/ENGINEER:
CHAPPELL ENGINEERING ASSOCIATES, LLC
Civil Structural Land Surveying
R.K. EXECUTIVE CENTRE
201 BOSTON POST ROAD WEST
SUITE 101
MARLBOROUGH, MA 01752
(508) 481-7400
www.chappellengineering.com

SEAL:

ENGINEER/LAND SURVEYOR DATE

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THESE DRAWINGS HAVE BEEN PREPARED IN ARCH D (DWG) FORMAT. AS SUCH, THE WRITTEN SCALES SHOWN ON ANY REPRODUCTIONS OF A COMMERCIAL SIZE SHALL BE OBSERVED. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED. WHERE IN CONFLICT, DIMENSIONS SHALL SUPERSEDE WRITTEN SCALES.
IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT.

REVISIONS		
NO.	DESCRIPTION	DATE
0	ISSUED FOR REVIEW	4/28/23
1	ISSUED FOR CONSTRUCTION (FINAL)	4/28/23
2	REVISED PER (5/9/23) TSA	5/16/23

PROJECT NAME:
WINDSOR 4 CT
780 PROSPECT HILL ROAD
WINDSOR, CT 06095

DRAWING TITLE:
GROUNDING DETAILS

DRAWING NO.:
E05

SCALE: AS SHOWN	DESIGNED BY: MHC CHECKED BY: GRS	VDR PROJECT CODE: 20230415028 VDR PROJECT NO.: 10000214
DATE PROJECT NO.: 08210.416	ORIGINAL ISSUE DATE: 4/28/23	MDG LOCATION ID: 5000207278

ATTACHMENT 4

NHH-65B-R2B



6-port sector antenna, 2x 698–896 and 4x 1695–2360 MHz, 65° HPBW, 2x RET. Both high bands share the same electrical tilt.

- Interleaved dipole technology providing for attractive, low wind load mechanical package
- Internal SBT on low and high band allow remote RET control from the radio over the RF jumper cable
- Separate RS-485 RET input/output for low and high band
- One RET for low band and one RET for both high bands to ensure same tilt level for 4x Rx or 4x MIMO

General Specifications

Antenna Type	Sector
Band	Multiband
Color	Light gray
Grounding Type	RF connector body grounded to reflector and mounting bracket
Performance Note	Outdoor usage Wind loading figures are validated by wind tunnel measurements described in white paper WP-112534-EN
Radome Material	Fiberglass, UV resistant
Radiator Material	Low loss circuit board
Reflector Material	Aluminum
RF Connector Interface	4.3-10 Female
RF Connector Location	Bottom
RF Connector Quantity, high band	4
RF Connector Quantity, low band	2
RF Connector Quantity, total	6

Remote Electrical Tilt (RET) Information

RET Interface	8-pin DIN Female 8-pin DIN Male
RET Interface, quantity	2 female 2 male
Input Voltage	10–30 Vdc
Internal Bias Tee	Port 1 Port 3
Internal RET	High band (1) Low band (1)
Power Consumption, idle state, maximum	2 W
Power Consumption, normal conditions, maximum	13 W

NHH-65B-R2B

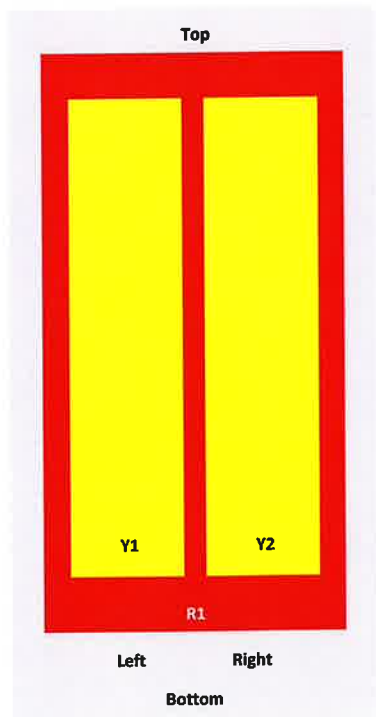
Protocol 3GPP/AISG 2.0 (Single RET)

Dimensions

Width 301 mm | 11.85 in
Depth 180 mm | 7.087 in
Length 1828 mm | 71.969 in
Net Weight, without mounting kit 19.8 kg | 43.651 lb

Array Layout

NHH



Array	Freq. (MHz)	Comps	RET (SBET)	AISG: RET UID
R1	698-896	1-2	1	AN*****1
Y1	1695-2360	3-4	2	AN*****2
Y2	1695-2360	5-6		

View from the front of the antenna
 (Sizes of colored boxes are not true depictions of array sizes)

Electrical Specifications

Impedance 50 ohm
Operating Frequency Band 1695 – 2360 MHz | 698 – 896 MHz

NHH-65B-R2B

Polarization	±45°
Total Input Power, maximum	900 W @ 50 °C

Electrical Specifications

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2200	2300–2360
Gain, dBi	14.9	15	17.7	17.9	18.4	18.7
Beamwidth, Horizontal, degrees	65	60	71	69	64	57
Beamwidth, Vertical, degrees	12.4	11.2	5.7	5.2	4.9	4.6
Beam Tilt, degrees	0–14	0–14	0–7	0–7	0–7	0–7
USLS (First Lobe), dB	13	14	18	18	19	18
Front-to-Back Ratio at 180°, dB	30	29	31	30	29	31
Isolation, Cross Polarization, dB	25	25	25	25	25	25
Isolation, Inter-band, dB	30	30	30	30	30	30
VSWR Return loss, dB	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0
PIM, 3rd Order, 2 x 20 W, dBc	-153	-153	-153	-153	-153	-153
Input Power per Port at 50°C, maximum, watts	300	300	300	300	300	300

Electrical Specifications, BASTA

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2200	2300–2360
Gain by all Beam Tilts, average, dBi	14.5	14.5	17.3	17.7	18.1	18.5
Gain by all Beam Tilts Tolerance, dB	±0.6	±1.1	±0.4	±0.4	±0.5	±0.3
Gain by Beam Tilt, average, dBi	0° 14.4 7° 14.6 14° 14.3	0° 14.7 7° 14.7 14° 14.1	0° 17.2 4° 17.3 7° 17.3	0° 17.6 4° 17.7 7° 17.7	0° 18.0 4° 18.2 7° 18.1	0° 18.3 4° 18.5 7° 18.6
Beamwidth, Horizontal Tolerance, degrees	±2	±2.1	±3	±4.1	±6.5	±2.9
Beamwidth, Vertical Tolerance, degrees	±0.7	±0.7	±0.3	±0.2	±0.3	±0.2
USLS, beampeak to 20° above beampeak, dB	13	14	16	16	17	15
Front-to-Back Total Power at 180° ± 30°, dB	23	22	27	27	25	25
CPR at Boresight, dB	22	21	23	23	22	19

NHH-65B-R2B

CPR at Sector, dB	10	7	16	13	11	4
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Mechanical Specifications

Effective Projective Area (EPA), frontal	0.26 m ² 2.799 ft ²
Effective Projective Area (EPA), lateral	0.22 m ² 2.368 ft ²
Wind Loading @ Velocity, frontal	278.0 N @ 150 km/h (62.5 lbf @ 150 km/h)
Wind Loading @ Velocity, lateral	230.0 N @ 150 km/h (51.7 lbf @ 150 km/h)
Wind Loading @ Velocity, maximum	537.0 N @ 150 km/h (120.7 lbf @ 150 km/h)
Wind Loading @ Velocity, rear	282.0 N @ 150 km/h (63.4 lbf @ 150 km/h)
Wind Speed, maximum	241 km/h 149.75 mph

Packaging and Weights

Width, packed	409 mm 16.102 in
Depth, packed	299 mm 11.772 in
Length, packed	1952 mm 76.85 in
Weight, gross	32.3 kg 71.209 lb

Regulatory Compliance/Certifications

Agency	Classification
CHINA-ROHS	Below maximum concentration value
ISO 9001:2015	Designed, manufactured and/or distributed under this quality management system
ROHS	Compliant



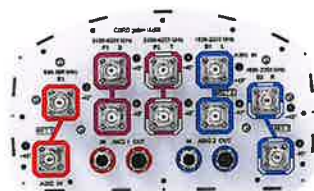
Included Products

BSAMNT-3	– Wide Profile Antenna Downtilt Mounting Kit for 2.4 - 4.5 in (60 - 115 mm) OD round members. Kit contains one scissor top bracket set and one bottom bracket set.
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* Footnotes

Performance Note	Severe environmental conditions may degrade optimum performance
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NHHSS-65B-R2BT4



10-port sector antenna, 2x 698–896, 4x 1695–2200 and 4x 3100–4200 MHz, 65° HPBW, 2x RETs and 2x SBTs. Both high bands share the same electrical tilt.

- Perfect antenna to add 3.5GHz CBRS to macro sites
- Low band and mid band performance mirrors the performance of existing NHH hex port antennas
- Interleaved dipole technology providing for attractive, low wind load mechanical package
- Internal SBT on low and high band allow remote RET control from the radio over the RF jumper cable
- One LB RET and one HB RET. Both high bands are controlled by one RET to ensure same tilt level for 4x MIMO

General Specifications

Antenna Type	Sector
Band	Multiband
Color	Light gray
Grounding Type	RF connector inner conductor and body grounded to reflector and mounting bracket
Performance Note	Outdoor usage
Radome Material	Fiberglass, UV resistant
Radiator Material	Low loss circuit board
Reflector Material	Aluminum
RF Connector Interface	4.3-10 Female
RF Connector Location	Bottom
RF Connector Quantity, high band	4
RF Connector Quantity, mid band	4
RF Connector Quantity, low band	2
RF Connector Quantity, total	10

Remote Electrical Tilt (RET) Information

RET Hardware	CommRET v2
RET Interface	4x 8 pin connector as per IEC 60130-9 Daisy chain in: Male / Daisy chain out: Female Pin3: RS485A(AISG_B), Pin5: RS485B(AISG_A), Pin6: DC 10~30V, Pin7: DC_ Return

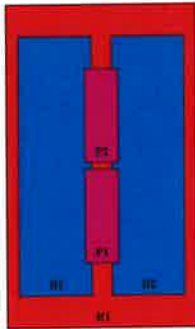
NHHSS-65B-R2BT4

RET Interface, quantity	2 female 2 male
Input Voltage	10–30 Vdc
Internal RET	High band (1) Low band (1)
Power Consumption, active state, maximum	10 W
Power Consumption, idle state, maximum	2 W
Protocol	3GPP/AISG 2.0 (Single RET)

Dimensions

Width	301 mm 11.85 in
Depth	181 mm 7.126 in
Length	1828 mm 71.969 in
Net Weight, without mounting kit	23.1 kg 50.927 lb

Array Layout

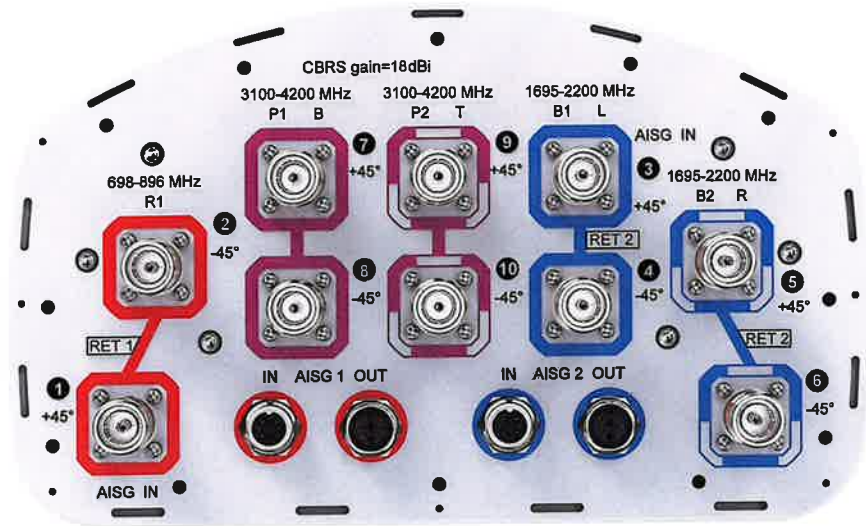


Array ID	Frequency (MHz)	RF Connector	RET (SRET)	AISG No.	AISG RET UID
R1	698-896	1 - 2	1	AISG1	CPxxxxxxxxxxxxxxxxR1
B1	1695-2200	3 - 4	2	AISG2	CPxxxxxxxxxxxxxxxxB1
B2	1695-2200	5 - 6			
R1	3100-4200	7 - 8	N/A	NA	N/A
R2	3100-4200	9 - 10	N/A	NA	N/A

(Sizes of colored boxes are not true depictions of array sizes)

Port Configuration

NHHSS-65B-R2BT4



Electrical Specifications

Impedance	50 ohm
Operating Frequency Band	1695 – 2200 MHz 3100 – 4200 MHz 698 – 896 MHz
Polarization	±45°
Total Input Power, maximum	1,000 W @ 50 °C

Electrical Specifications

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2200	3100–3550	3550–3700	3700–4200
Gain, dBi	14.8	15.2	17.4	17.8	18	17.7	17.3	17.9
Beamwidth, Horizontal, degrees	65	62	66	61	64	54	64	60
Beamwidth, Vertical, degrees	13	11.6	5.5	5.2	4.9	5.7	5.3	4.9
Beam Tilt, degrees	0–14	0–14	0–7	0–7	0–7	4	4	4
USLS (First Lobe), dB	15	15	16	18	18	16	17	18
Front-to-Back Ratio at 180°, dB	26	29	31	28	27	30	33	29
Isolation, Cross Polarization, dB	25	25	25	25	25	25	25	25
Isolation, Inter-band, dB	25	25	25	25	25	28	28	28
VSWR Return loss, dB	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0
PIM, 3rd Order, 2 x 20 W, dBc	-153	-153	-153	-153	-153	-140	-140	-140

NHHSS-65B-R2BT4

Input Power per Port at 50°C, maximum, watts	300	300	300	300	300	100	100	100
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Electrical Specifications, BASTA

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2200	3100–3550	3550–3700	3700–4200
Gain by all Beam Tilts, average, dBi	14.6	14.8	17	17.5	17.7	17.3	17	17.2
Gain by all Beam Tilts Tolerance, dB	±0.4	±0.4	±0.6	±0.3	±0.4	±0.6	±0.7	±0.8
Gain by Beam Tilt, average, dBi	0° 14.6 7° 14.6 14° 14.4	0° 15.0 7° 14.9 14° 14.5	0° 16.9 3° 17.0 7° 16.8	0° 17.4 3° 17.5 7° 17.4	0° 17.5 3° 17.8 7° 17.6			
Beamwidth, Horizontal Tolerance, degrees	±1.7	±1.3	±7.2	±3.1	±6.2	±10	±6.7	±10.5
Beamwidth, Vertical Tolerance, degrees	±0.8	±0.8	±0.2	±0.2	±0.4	±0.4	±0.3	±0.4
USLS, beampeak to 20° above beampeak, dB	18	16	14	15	17	14		
Front-to-Back Total Power at 180° ± 30°, dB	22	25	25	25	24	26	25	24
CPR at Boresight, dB	24	17	16	21	19	15	17	14
CPR at Sector, dB	12	6	11	10	8	8	9	7

Mechanical Specifications

Wind Loading @ Velocity, frontal	278.0 N @ 150 km/h (62.5 lbf @ 150 km/h)
Wind Loading @ Velocity, lateral	230.0 N @ 150 km/h (51.7 lbf @ 150 km/h)
Wind Loading @ Velocity, maximum	537.0 N @ 150 km/h (120.7 lbf @ 150 km/h)
Wind Loading @ Velocity, rear	287.0 N @ 150 km/h (64.5 lbf @ 150 km/h)
Wind Speed, maximum	241 km/h 149.75 mph

Packaging and Weights

Width, packed	1973 mm 77.677 in
Depth, packed	441 mm 17.362 in
Length, packed	337 mm 13.268 in
Weight, gross	35.1 kg 77.382 lb

Regulatory Compliance/Certifications

Agency	Classification
CHINA-ROHS	Above maximum concentration value

NHHSS-65B-R2BT4

ROHS

Compliant/Exempted



Included Products

BSAMNT-3

- Wide Profile Antenna Downtilt Mounting Kit for 2.4 - 4.5 in (60 - 115 mm) OD round members. Kit contains one scissor top bracket set and one bottom bracket set.

* Footnotes

Performance Note

Severe environmental conditions may degrade optimum performance

SAMSUNG

SAMSUNG C-Band 64T64R Massive MIMO Radio

for High Capacity and Wide Coverage

Samsung C-Band 64T64R Massive MIMO Radio enables mobile operators to increase coverage range, boost data speeds and ultimately offer enriched 5G experiences to users in the U.S..

Model Code : MT6407-77A



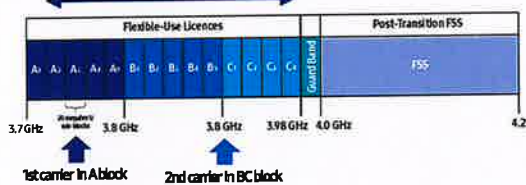
Points of Differentiation

Wide Bandwidth

With capability to support up to 2 CC carrier configuration, Samsung C-Band massive MIMO Radio supports 200 MHz bandwidth in the C-Band spectrum.

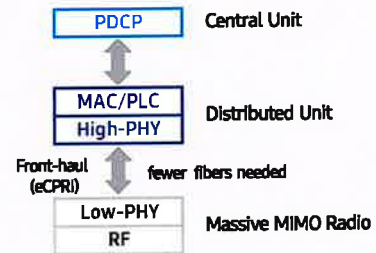
Samsung C-Band massive MIMO Radio covers the entire C-Band 280 MHz spectrum, so it can meet the operator's needs in current A block and future B/C blocks

C-Band spectrum supported by Massive MIMO Radio



Future Proof Product

Samsung C-Band 64T64R Massive MIMO radio supports not only CPRI but also eCPRI as front-haul interface. It enables operators can cut down on OPEX/CAPEX by reducing front-haul bandwidth through low layer split and using ethernet based higher efficient line.



Enhanced Performance

C-Band massive MIMO Radio creates sharp beams and extends networks' coverage on the critical mid-band spectrum using a large number of antenna elements and high output power to boost data speeds.

This helps operators reduce their CAPEX as they now need less products to cover the same area than before.

Furthermore, as C-Band massive MIMO Radio supports MU-MIMO (Multi-user MIMO), it enables to increase user throughput by minimizing interference.



Well Matched Design

Samsung C-Band Massive MIMO radio utilizes 64 antennas, supports up to 280MHz bandwidth, and delivers a 200W output power. Despite the above advanced performance, the Radio has a compact size of 50.9L and 79.4lbs. This makes it easy to install the Radio.

It is designed to look solid and compact, with a low profile appearance so that, when installed, harmonizes well with the surrounding environment.



Technical Specifications

Item	Specification
Tech	NR
Band	n77
Frequency Band	3700 - 3980 MHz
EIRP	78.5dBm (53.0 dBm+25.5 dBi)
IBW/OBW	280 MHz / 200 MHz
Installation	Pole/Wall
Size/Weight	16.06 x 35.06 x 5.51 inch (50.86L) / 79.4 lbs

SAMSUNG



About Samsung Electronics Co., Ltd.

Samsung inspires the world and shapes the future with transformative ideas and technologies. The company is redefining the worlds of TVs, smartphones, wearable devices, tablets, digital appliances, network systems, and memory, system LSI, foundry and LED solutions.

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SAMSUNG

AWS/PCS MACRO RADIO

DUAL-BAND AND HIGH POWER FOR MACRO COVERAGE

Samsung's future proof dual-band radio is designed to help effectively increase the coverage areas in wireless networks. This AWS/PCS 4T4R dual-band radio has 4Tx/4Rx to 2Tx/2Rx RF chains options and a total output power of 320W, making it ideal for macro sites.

Model Code RF4439d-25A



Homepage
[samsungnetworks.com](https://www.samsungnetworks.com)

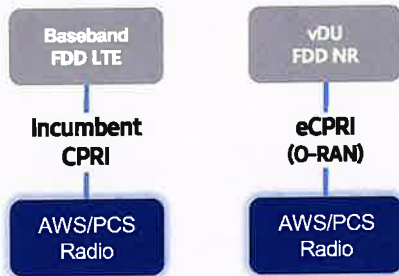


Youtube
www.youtube.com/samsung5g

Points of Differentiation

Continuous Migration

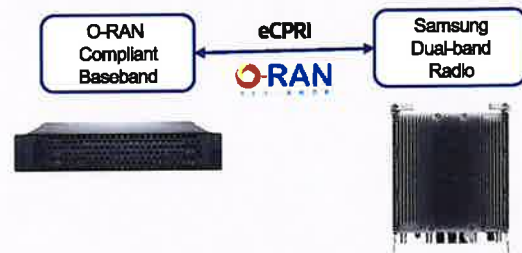
Samsung's AWS/PCS macro radio can support each incumbent CPRI interface as well as advanced eCPRI interfaces. This feature provides installable options for both legacy LTE networks and added NR networks.



O-RAN Compliant

A standardized O-RAN radio can help in implementing cost-effective networks, which are capable of sending more data without compromising additional investments.

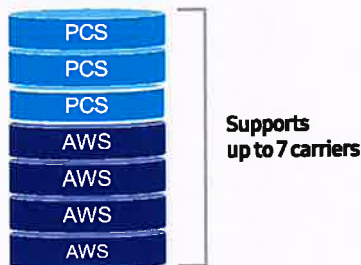
Samsung's state-of-the-art O-RAN technology will help accelerate the effort toward constructing a solid O-RAN ecosystem.



Optimum Spectrum Utilization

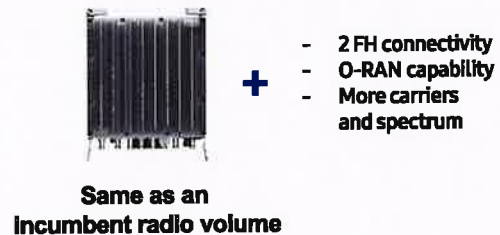
The number of required carriers varies according to site (region). Supporting many carriers is essential for using all frequencies that the operator has available.

The new AWS/PCS dual-band radio can support up to 3 carriers in the PCS (1.9GHz) band and 4 carriers in the AWS (2.1GHz) band, respectively.



Brand New Features in a Compact Size

Samsung's AWS/PCS macro radio offers several features, such as dual connectivity for baseband for both CDU and vDU, O-RAN capability, more carriers and an enlarged PCS spectrum, combined into an incumbent radio volume of 36.8L.



Technical Specifications

Item	Specification
Tech	LTE/NR
Brand	B25(PCS), B66(AWS)
Frequency Band	DL: 1930 – 1995MHz, UL: 1850 – 1915MHz DL: 2110 – 2200MHz, UL: 1710 – 1780MHz
RF Power	(B25) 4 × 40W or 2 × 60W (B66) 4 × 60W or 2 × 80W
IBW/OBW	(B25) 65MHz / 30MHz (B66) DL 90MHz, UL 70MHz / 60MHz
Installation	Pole, Wall
Size/Weight	14.96 x 14.96 x 10.04inch (36.8L) / 74.7lb

SAMSUNG

700/850MHZ MACRO RADIO

DUAL-BAND AND HIGH POWER FOR MACRO COVERAGE

Samsung's future proof dual-band radio is designed to help effectively increase the coverage areas in wireless networks. This 700/850MHz 4T4R dual-band radio has 4Tx/4Rx to 2Tx/2Rx RF chains options and a total output power of 320W, making it ideal for macro sites.

Model Code RF4440d-13A



Homepage
samsungnetworks.com

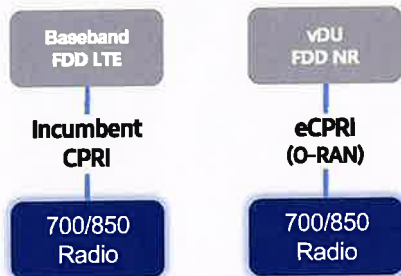


Youtube
www.youtube.com/samsung5g

Points of Differentiation

Continuous Migration

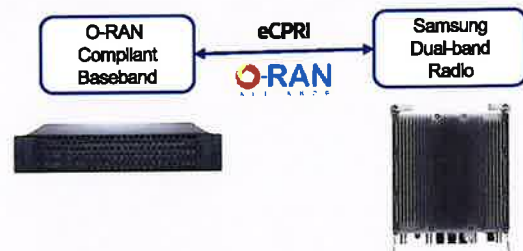
Samsung's 700/850MHz macro radio can support each incumbent CPRI interface as well as an advanced eCPRI interface. This feature provides installable options for both legacy LTE networks and added NR networks.



O-RAN Compliant

A standardized O-RAN radio can help when implementing cost-effective networks because it is capable of sending more data without compromising additional investments.

Samsung's state-of-the-art O-RAN technology will help accelerate the effort toward constructing a solid O-RAN ecosystem.



Optimum Spectrum Utilization

The number of required carriers varies according to site (region). The ability to support many carriers is essential for using all frequencies that the operator has available.

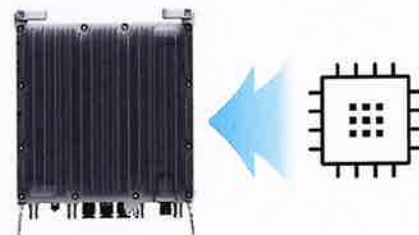
The new 700/850MHz dual-band radio can support up to 2 carriers in the B13 (700MHz) band and 3 carriers in the B5 (850MHz) band, respectively.



Secured Integrity

Access to sensitive data is allowed only to authorized software.

The Samsung radio's CPU can protect root of trust, which is credential information to verify SW integrity, and secure storage provides access control to sensitive data by using dedicated hardware (TPM).



Technical Specifications

Item	Specification
Tech	LTE / NR
Brand	B13(700MHz), B5(850MHz)
Frequency Band	DL: 746 – 756MHz, UL: 777 – 787MHz DL: 869 – 894MHz, UL: 824 – 849MHz
RF Power	(B13) 4 × 40W or 2 × 60W (B5) 4 × 40W or 2 × 60W
IBW/OBW	(B13) 10MHz / 10MHz (B5) 25MHz / 25MHz
Installation	Pole, Wall
Size/ Weight	14.96 x 14.96 x 9.05inch (33.2L) / 70.33 lb

Specifications

The table below outlines the main specifications of the RRH.

Table 1. Specifications

Item	RT4401-48A
Air Technology	LTE
Band	Band 48 (3.5 GHz)
Operating Frequency (MHz)	3550 to 3700
RF Chain	4TX/4RX
Input Power	-48 V DC (-38 to -57 V DC, 1 SKU), with clip-on AC-DC converter (Option)
Dimension (W × D × H) (mm)	8.55 in. (217.4) × 4.15 in. (105.5) × 13.91 in. (353.5) * RRH only 11.39 in. (289.4) × 5.45 in. (138.5) × 16.16 in. (410.5) * with Clip-on antenna, AC-DC power unit
Cooling	Natural convection
Unwanted Emission	3GPP 36.104 Category A [B48]: FCC 47 CFR 96.41 e)
Spectrum Analyzer	TX/RX Support
Antenna Type	Integrated (Clip-on) antenna (Option), External antenna (Option)
Operating Humidity	5 to 100 [%] (RH), condensing, not to exceed 30 g/m ³ absolute humidity
Altitude	-60 to 1,800 m
Earthquake	Telcordia Earthquake Risk Zone4 (Telcordia GR-63-CORE)
Vibration in Use Transportation Vibration	Office Vibration Transportation Vibration
Noise	Fanless (natural convection cooling)
Wind Resistance	Telcordia GR-487-CORE, Section 3.34
EMC	FCC Title 47, CFR Part 96
Safety	UL 60950-1 2nd ED

Item	RT4401-48A
	UL 62368-1 UL 60950-22
RF	FCC Title 47, CFR Part 96

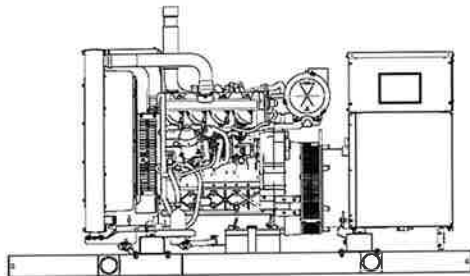
The table below outlines the AC/DC power unit specifications of the RRH system.



**Tier 3 EPA-Certified for Stationary
Emergency Applications**

Ratings Range

		60 Hz
Standby:	kW	44- 52
	kVA	44- 65
Prime:	kW	40- 47
	kVA	40- 58



Model with TM Engine shown

Generator Set Ratings

Alternator	Voltage	Ph	Hz	130°C Rise Standby Rating		105°C Rise Prime Rating	
				kW/kVA	Amps	kW/kVA	Amps
4P7BX	120/208	3	60	51/63	176	46/57	159
	127/220	3	60	51/63	167	46/57	150
	120/240	3	60	49/61	147	44/55	132
	120/240	1	60	44/44	183	40/40	166
	139/240	3	60	51/63	153	46/57	138
	220/380	3	60	49/61	93	45/56	85
	277/480	3	60	51/63	76	46/57	69
	347/600	3	60	51/63	61	46/57	55
4P8X	120/208	3	60	52/65	180	47/58	163
	127/220	3	60	52/65	170	47/58	154
	120/240	3	60	50/62	150	45/56	135
	120/240	1	60	50/50	208	45/45	187
	139/240	3	60	52/65	156	47/58	141
	220/380	3	60	52/65	98	47/58	89
	277/480	3	60	52/65	78	47/58	70
	347/600	3	60	52/65	62	47/58	56
4P10X	120/208	3	60	52/65	180	47/58	163
	127/220	3	60	52/65	170	47/58	154
	120/240	3	60	50/62	150	45/56	135
	120/240	1	60	50/50	208	45/45	187
	139/240	3	60	52/65	156	47/58	141
	220/380	3	60	52/65	98	47/58	89
4Q7BX	120/240	1	60	48/48	200	43/43	179
	4Q8X	120/240	1	60	50/50	208	45/45
4Q10X	120/240	1	60	50/50	208	45/45	187

Standard Features

- Kohler Co. provides one-source responsibility for the generating system and accessories.
- The generator set and its components are prototype-tested, factory-built, and production-tested.
- The 60 Hz generator set offers a UL 2200 listing.
- The generator set accepts rated load in one step.
- The 60 Hz generator set meets NFPA 110, Level 1, when equipped with the necessary accessories and installed per NFPA standards.
- The generator set engine is certified to meet the Environmental Protection Agency (EPA) emergency stationary emissions requirements.
- A one-year limited warranty covers all generator set systems and components. Two- and five-year extended limited warranties are also available.
- Alternator features:
 - The unique Fast-Response® X excitation system delivers excellent voltage response and short-circuit capability using a rare-earth, permanent magnet (PM)-excited alternator.
 - The brushless, rotating-field alternator has broadrange reconnectability.
- Other features:
 - Kohler designed controllers for one-source system integration and remote communication. See Controllers on page 3.
 - The low coolant level shutdown prevents overheating (standard on radiator models only).
 - Integral vibration isolation eliminates the need for under-unit vibration spring isolators.
 - The generator set for 49-state applications is equipped with the KDI 3404 TM engine. The generator set that is CARB compliant/California South Coast Air Quality Management District (SCAQMD) pre-certified is equipped with the KDI 3404 TCR engine.

RATINGS: All three-phase units are rated at 0.8 power factor. All single-phase units are rated at 1.0 power factor. Standby Ratings: Standby rating is applicable to varying loads for the duration of a power outage. There is no overload capability for this rating. Prime Power Ratings: At varying load, the number of generator set operating hours is unlimited. A 10% overload capacity is available for one hour in twelve. Ratings are in accordance with ISO-8528-1 and ISO-3046-1. For limited running time and continuous ratings, consult the factory. Obtain the technical information bulletin (TIB-101) for ratings guidelines, complete ratings definitions, and site condition derates. The generator set manufacturer reserves the right to change the design or specifications without notice and without any obligation or liability whatsoever.

Alternator Specifications

Specifications	Alternator
Manufacturer	Kohler
Type	4-Pole, Rotating-Field
Exciter type	Brushless, Rare-Earth Permanent Magnet
Leads: quantity, type	12, Reconnectable
	4, 110- 120/220- 240 V
Voltage regulator	Solid State, Volts/Hz
Insulation:	NEMA MG1
Material	Class H
Temperature rise	130°C, Standby
Bearing: quantity, type	1, Sealed
Coupling	Flexible Disc
Amortisseur windings	Full
Voltage regulation, no-load to full-load	Controller Dependent
One-step load acceptance	100% of Rating
Unbalanced load capability	100% of Rated Standby Current

- NEMA MG1, IEEE, and ANSI standards compliance for temperature rise and motor starting.
- Sustained short-circuit current of up to 300% of the rated current for up to 10 seconds.
- Sustained short-circuit current enabling downstream circuit breakers to trip without collapsing the alternator field.
- Self-ventilated and dripproof construction.
- Windings are vacuum-impregnated with epoxy varnish for dependability and long life.
- Superior voltage waveform from a two-thirds pitch stator and skewed rotor.

Specifications	Alternator
Peak motor starting kVA:	(35% dip for voltages below)
480 V 4P7BX (12 lead)	180
480 V 4P8X (12 lead)	261
480 V 4P10X (12 lead)	275
240 V 4Q7BX (4 lead)	113
240 V 4Q8X (4 lead)	121
240 V 4Q10X (4 lead)	144

Application Data

Engine

Engine Specifications	49-State Engine	California SCAQMD
Manufacturer	Kohler Diesel	
	KDI	KDI
Engine model	3404TM	3404TCR
Engine type	4-Cycle, Turbocharged	
Cylinder arrangement	4 Inline	
Displacement, L (cu. in.)	3.4 (207)	
Bore and stroke, mm (in.)	96 x 116 (3.28 x 4.57)	
Compression ratio	18.5:1	17.0:1
Piston speed, m/min. (ft./min.)	418 (1371)	510 (1673)
Main bearings: quantity, type	5, Replaceable Insert	
Rated rpm	1800	
Max. power at rated rpm, kWm (BHP)	64 (86)	70 (94)
Cylinder head material	Cast Iron	
Crankshaft material	Cast Iron	
Valve material:		
Intake	Chromium-Silicon Steel	
Exhaust	Chromium Steel	
Governor: type, make/model	Mech. (or Electronic *)	Electronic
	Droop, 5%	
	(or Isochr. *)	Isochronous
Frequency regulation, no-load to full-load	±0.5%	±0.28%
Frequency regulation, steady state	Fixed	
Frequency	Dry	
Air cleaner type, all models		
* Requires available electronic governor option		

Exhaust

Exhaust System	49-State Engine	California SCAQMD
Exhaust manifold type	Dry	
Exhaust flow at rated kW, m ³ /min. (cfm)	8.8 (310)	
Exhaust temperature at rated kW, dry exhaust, °C (°F)	490 (914)	471 (880)
Minimum/maximum allowable back pressure, kPa (in. Hg)	6 (1.8)/ 9 (2.7)	8 (2.4)/ 13.5 (4.0)
Exhaust outlet size at engine hookup, mm (in.)	63.5 (2.5)	

Engine Electrical

Engine Electrical System	49-State Engine	California SCAQMD
Battery charging alternator:		
Ground (negative/positive)	Negative	
Volts (DC)	12	
Ampere rating	90	
Starter motor rated voltage (DC)	12	
Battery, recommended cold cranking amps (CCA):		
Quantity, CCA rating	One, 650	
Battery voltage (DC)	12	

Fuel

Fuel System	49-State Engine	California SCAQMD
Fuel supply line, min. ID, mm (in.)	8.0 (0.31)	
Fuel return line, min. ID, mm (in.)	6.0 (0.25)	
Max. lift, engine-driven fuel pump, m (ft.)	6.0 (20.0)	3.7 (12.1)
Max. fuel flow, Lph (gph)	46 (12.2)	87.4 (23.1)
Max. return line restriction, kPa (in. Hg)	20 (5.9)	17.7 (5.2)
Fuel filter		
Prefilter	74 Microns	
Primary/Water Separator	5 Microns @ 98% Efficiency	5 Microns @ 95% Efficiency
Recommended fuel	#2 Ultra Low Sulfur Diesel	

Lubrication

Lubricating System	49-State Engine	California SCAQMD
Type	Full Pressure	
Oil pan capacity, L (qt.) §	15.3 (16.2)	
Oil pan capacity with filter, L (qt.) §	15.6 (16.5)	
Oil filter: quantity, type §	1, Cartridge	
Oil cooler	Water-Cooled	
§ Kohler recommends the use of Kohler Genuine oil and filters.		

Application Data

Cooling

Radiator System	49-State Engine	California SCAQMD
Ambient temperature, °C (°F) *	50 (122)	
Engine jacket water capacity, L (gal.)	4.5 (1.19)	
Radiator system capacity, including engine, L (gal.)	12.3 (3.2)	
Engine jacket water flow, Lpm (gpm)	125 (33)	120 (32)
Heat rejected to cooling water at rated kW, dry exhaust, kW (Btu/min.)	37.8 (2207)	41.3 (2352)
Heat rejected to air charge cooler at rated kW, dry exhaust, kW (Btu/min.)	12 (682)	8.4(477)
Water pump type	Centrifugal	
Fan diameter, including blades, mm (in.)	597 (23.5)	
Fan, kWm (HP)	1.8 (2.3)	
Max. restriction of cooling air, intake and discharge side of radiator, kPa (in. H ₂ O)	0.125 (0.5)	

* Enclosure reduces ambient temperature capability by 5°C (9°F).

Operation Requirements

Air Requirements	49-State Engine	California SCAQMD
Radiator-cooled cooling air, m ³ /min. (scfm) †	96.3 (3400)	
Combustion air, m ³ /min. (cfm)	4.8 (170)	4.0 (140)
Heat rejected to ambient air:		
Engine, kW (Btu/min.)	13.2 (750)	
Alternator, kW (Btu/min.)	7.6 (435)	
Max. air intake restriction, kPa (in. Hg)	5.2 (1.54)	4.2 (1.24)

† Air density = 1.20 kg/m³ (0.075 lbm/ft³)

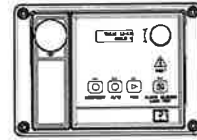
Fuel Consumption	49-State Engine	
Diesel, Lph (gph) at % load	Standby Rating	
100%	17.4	(4.6)
75%	13.2	(3.5)
50%	9.1	(2.4)
25%	5.3	(1.4)

Fuel Consumption	49-State Engine	
Diesel, Lph (gph) at % load	Prime Rating	
100%	16.1	(4.2)
75%	12.1	(3.2)
50%	8.3	(2.2)
25%	4.9	(1.3)

Fuel Consumption	Calif. SCAQMD Engine	
Diesel, Lph (gph) at % load	Standby Rating	
100%	15.2	(4.0)
75%	11.6	(3.1)
50%	8.0	(2.1)
25%	4.6	(1.2)

Fuel Consumption	Calif. SCAQMD Engine	
Diesel, Lph (gph) at % load	Prime Rating	
100%	12.3	(3.2)
75%	10.6	(2.8)
50%	6.6	(1.7)
25%	4.1	(1.1)

Controllers

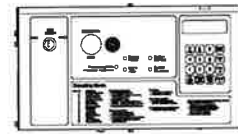


APM402 Controller

Provides advanced control, system monitoring, and system diagnostics for optimum performance and compatibility.

- Digital display and menu control provide easy local data access
- Measurements are selectable in metric or English units
- Remote communication thru a PC via network or serial configuration
- Controller supports Modbus® protocol
- Integrated hybrid voltage regulator with ±0.5% regulation
- Built-in alternator thermal overload protection
- NFPA 110 Level 1 capability

Refer to G6-161 for additional controller features and accessories.



(Available with the 49-State generator set only.)

Decision-Maker® 550 Controller

Provides advanced control, system monitoring, and system diagnostics with remote monitoring capabilities.

- Digital display and keypad provide easy local data access
- Measurements are selectable in metric or English units
- Remote communication thru a PC via network or modem configuration
- Controller supports Modbus® protocol
- Integrated voltage regulator with ±0.25% regulation
- Built-in alternator thermal overload protection
- NFPA 110 Level 1 capability

Refer to G6-46 for additional controller features and accessories.

Modbus® is a registered trademark of Schneider Electric.

Additional Standard Features

- Air Cleaner, Heavy Duty
- Alternator Protection
- Battery Rack and Cables
- Open Crankcase Ventilation
- Oil Drain and Coolant Drain with Hose Barb
- Oil Drain Extension (with narrow skid and enclosure models only)
- Operation and Installation Literature
- Radiator Drain Extension (with enclosure models only)
- Stainless Steel Fasteners on Enclosure (with enclosure models only)

Available Options

Approvals and Listings

- CSA Certified
- IBC Seismic Certification
- UL2200 Listing

Enclosed Unit

- Sound Enclosure (with enclosed critical silencer)
- Weather Enclosure (with enclosed critical silencer)
- Stainless Steel Latches and Hinges

Open Unit

- Exhaust Silencer, Critical (kit: PA-324470)
- Flexible Exhaust Connector, Stainless Steel

Fuel System

- Flexible Fuel Lines
- Fuel Pressure Gauge (Available with 49-state engine only)
- Subbase Fuel Tanks

Controller

- 15-Relay Dry Contact (SCAQMD engine with APM402 controller only)
- Common Failure Relay (550 controller only)
- Communication Products and PC Software (550 controller only)
- Customer Connection (550 controller only)
- Dry Contact (isolated alarm) (550 controller only)
- Two Input/Five Output Module (49-state engine with APM402 controller only)
- Key Switch (SCAQMD engine with APM402 controller only)
- Manual Speed Adjust (requires Electronic Governor or SCAQMD engine)
- Remote Annunciator Panel
- Remote Emergency Stop
- Run Relay

Cooling System

- Block Heater (1000 W, 110-120 V)
Required for ambient temperatures below 0°C (32°F).
- Radiator Duct Flange

Electrical System

- Alternator Strip Heater
- Battery
- Battery Charger, Equalize/Float Type
- Battery Heater
- Electronic Governor
- Line Circuit Breaker (NEMA type 1 enclosure)
- Line Circuit Breaker with Shunt Trip (NEMA type 1 enclosure)

Miscellaneous

- Air Cleaner Restriction Indicator
- Engine Fluids Added
- Rated Power Factor Testing
- Rodent Guards

Literature

- General Maintenance
- NFPA 110
- Overhaul
- Production

Warranty

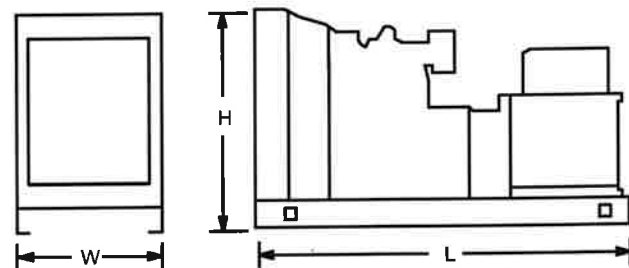
- 2-Year Basic Limited Warranty
- 5-Year Basic Limited Warranty
- 5-Year Comprehensive Limited Warranty

Other Options

- _____
- _____
- _____
- _____
- _____

Dimensions and Weights

Overall Size, L x W x H, mm (in.):
 Wide Skid: 2300 x 1040 x 1133 (90.6 x 41.0 x 44.6)
 Narrow Skid: 1875 x 780 x 1067 (73.8 x 30.7 x 42.0)
 Weight (radiator model), wet, kg (lb.): 802 (1769)



NOTE: This drawing is provided for reference only and should not be used for planning installation. Contact your local distributor for more detailed information.

DISTRIBUTED BY:

ATTACHMENT 5

Structural Analysis 135-ft Monopole

Prepared For:
Tarpon Towers II, LLC
8916 77th Terrace East, Suite 103
Lakewood Ranch, FL 34202

MFP Project #94122-009

Site Location:
CT1209 Windsor
780 Prospect Hill Road
Windsor, Hartford County, CT
Hartford Co., CT
Lat/Long: 41°52'58.5", -72°42'29.2"

Analysis Type:
TIA-222-H
Structure Rating - 45.6% (Foundation) Passing

May 9, 2023

Michael Plahovinsak Member Paraprofessionals
30725.29113428 class



5.9.2023

Michael F. Plahovinsak, P.E.
18301 State Route 161 W, Plain City, OH 43064
614-398-6250 - mike@mfpeng.com

Project Summary:

I have completed a structural analysis of the existing monopole for the following new configuration:

- 105' – Verizon:
 - (3) Commscope NHH-65B-R2B + (3) NHHSS-65B-R2BT4 Antennas
 - (3) Samsung MT6407-77A Antennas
 - (3) Samsung RF4439d-25A + (3) RF4440d-13A RRH's
 - (3) Samsung CBRS RRH-RT4401-48A
 - (1) Raycap RVZDC-6627-PF-48
 - (2) 1 5/8" Hybrid
 - SitePro RMQP-496-HK Mount

The pole has been analyzed in accordance with the requirements of the International Building Code per IBC section 3108, and the recommendations of the Telecommunications Industry Association "Structural Standard for Steel Antenna Supporting Structures" **TIA-222-H**.

This analysis may be considered a "Rigorous Structural Analysis" as defined in TIA-222-H.

As indicated in the conclusions of this analysis, I have determined that the existing pole and foundation have *sufficient capacity* to support the existing, reserved and proposed antenna loads as detailed herein. Based on the results of my analysis, structural modifications are not required at this time.

Source of Data:

Resource	Source	Job Number	Date
Pole and Foundation Drawings	Michael F. Plahovinsak, PE	23521-150	06/11/21
Geotechnical Report	Wolti Geotechnical	N/A	04/13/21
Erection Book	TAPP	TP-19977	06/15/21

Michael F. Plahovinsak, P.E. - Since 2011

mike@mfpeng.com

Analysis Criteria:

2022 Connecticut Building Code
 Structural Standards for Steel Antenna Supporting Structures **TIA-222-H**

- TIA-222-H Wind Speed 116 mph
- TIA-222-H Wind w/ 1 ½" Ice 50 mph (3-Sec Gust)
- Operational Wind Speed 60 mph (3-Sec Gust)

Risk Category	Exposure Category	Topographic Category
II (I = 1.0)	C	I

Appurtenance Listing:

Status	Elev.	Antenna / Mounting	Coax	Owner
Existing	130'	(3) Ericsson AIR3246 B66 Antennas (3) RFS APXVAARR24_43-U-NA20 Antennas (3) RFS APX16DWV16DWVSEA20 Antennas (3) Ericsson 4415 B66A + (3) 4449 B71+B12 + (3) 4415 B25 RRH's (1) Commscope VHLP1-23-CR4B Dish Platform Mount	(4) 6x12 HCS	T-Mobile
Existing*	115'	(3) JMA MX08FRO665-20_V0F Antennas (3) Fujitsu TA08025-B604 + (3) Fujitsu TA08025-B605 RRH's (1) Raycap RDIDC-9181-PF-48 Valmont SNP8HR-396 Mount	(1) 1.65" Hybrid	Dish Wireless
Proposed	105'	(3) Commscope NHH-65B-R2B + (3) NHHSS-65B-R2BT4 Antennas (3) Samsung MT6407-77A Antennas (3) Samsung RF4439d-25A + (3) RF4440d-13A RRH's (3) Samsung CBRs RRH-RT4401-48A (1) Raycap RVZDC-6627-PF-48 SitePro RMQP-496-HK Mount	(2) 1 5/8" Hybrid	Verizon

* Analysis is based on a leased wind area of 11,000 in². The 11,000 in² is greater than the proposed actual equipment wind area.

All antenna lines assumed internally mounted, not exposed to the wind.

Michael F. Plahovinsak, P.E. - Since 2011

mike@mfpeng.com

Foundation Analysis:

The existing monopole foundation design was analyzed in conjunction with site specific geotechnical report. The existing foundation has sufficient capacity to support the pole with the proposed antenna configuration.

Conclusion:

I have completed a structural analysis of the existing monopole and foundation in accordance with the project specifics outlined above. My analysis indicates that the existing monopole and foundation are structurally adequate when considering the existing plus proposed loading. Please refer to the attached calculations for an itemized listing of all member stress ratios. The existing pole is safe and adequate to support the proposed loads, and no structural reinforcing is required to support the above loading.

Recommendations:

As a part of routine maintenance, I recommend periodic inspection of the pole and foundation structure for signs of fatigue or corrosion.

If you have any questions about the contents of this structural report or require any additional information, please feel free to contact my office.

Sincerely,

Michael F. Plahovinsak, P.E.



mike@mfpeng.com - 614.398-6250

Michael F. Plahovinsak, P.E. - Since 2011

mike@mfpeng.com

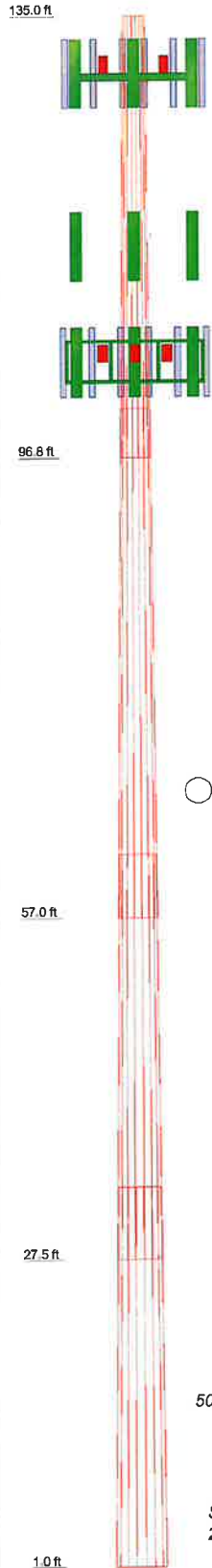
**Standard Conditions for Providing Structural Consulting
Services on Existing Structures**

1. The following standard conditions are a general overview of key issues regarding the work product supplied.
2. If the existing conditions are not as represented in this structural report or attached sketches, I should be contacted to evaluate the significance of the deviation and revise the structural assessment accordingly.
3. The structural analysis has been performed assuming that the structure is in "like new" condition. No allowance was made for excessive corrosion, damaged or missing structural members, loose bolts, etc. If there are any known deficiencies in the structure that potentially compromise structural integrity, I should be made aware of the deficiencies. If I am aware of a deficiency that exists in a structure at the time of my analysis, a general explanation of the structural concern due to the deficiency will be included in the structural report, but the deficiency will not be reflected in capacity calculations.
4. The structural analysis provided is an assessment of the primary load carrying capacity of the structure. I provide a limited scope of service in that I have not verified the capacity of every weld, plate, connection detail, etc. In most cases, structural fabrication details are unknown at the time of my analysis, and the detailed field measurement of this information is beyond the scope of my services. In instances where I have not performed connection capacity calculations, it is assumed that existing manufactured connections develop the full capacity of the primary members being connected.
5. The structural integrity of the existing foundation system can only be verified if exact foundation sizes and soils conditions are known. I will not accept any responsibility for the adequacy of the existing foundations unless this site-specific data is supplied.
6. Miscellaneous items such as antenna mounts, coax supports, etc. have not been designed, detailed, or specified as part of my work. It is assumed that material of adequate size and strength will be purchased from a reputable component manufacturer. The attached report and sketches are schematic in nature and should not be used to fabricate or purchase hardware and accessories to be attached to the structure. I recommend field measurement of the structure before fabricating or purchasing new hardware and accessories. I am not responsible for proper fit and clearance of hardware and accessory items in the field.
7. The structural analysis has been performed considering minimum code requirements or recommendations. If alternate wind, ice, or deflection criteria are to be considered, then I shall be made aware of the alternate criteria.

Michael F. Plahovinsak, P.E. - Since 2011

mike@mfpeng.com

Section	1	2	3	4
Length (ft)	38.25	44.00	35.00	32.75
Number of Sides	18	18	18	18
Thickness (in)	0.1875	0.3750	0.4375	0.5000
Socket Length (ft)	4.25	5.50	6.25	7.00
Top Dia (in)	22.0000	29.4907	37.6474	43.4235
Bot Dia (in)	30.8489	39.9898	45.7444	51.0000
Grade	2.0	6.1	6.8	8.3
Weight (K)				23.2



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
Ericsson AIR 3246 B66 (T-Mobile)	130	Commscope NHHSS-65B-R2BT4 w/ mount pipe (Verizon)	105
RFS - APXVAARR24_43-U-NA20 (T-Mobile)	130	Samsung MT6407-77A w/ mount pipe (Verizon)	105
RFS APX16VDWV-16DWVS (T-Mobile)	130	Commscope NHH-65B-R2B (Verizon)	105
Ericsson AIR 3246 B66 (T-Mobile)	130	Commscope NHHSS-65B-R2BT4 w/ mount pipe (Verizon)	105
RFS - APXVAARR24_43-U-NA20 (T-Mobile)	130	Samsung MT6407-77A w/ mount pipe (Verizon)	105
RFS APX16VDWV-16DWVS (T-Mobile)	130	Commscope NHH-65B-R2B (Verizon)	105
Ericsson AIR 3246 B66 (T-Mobile)	130	Commscope NHHSS-65B-R2BT4 w/ mount pipe (Verizon)	105
RFS - APXVAARR24_43-U-NA20 (T-Mobile)	130	Samsung MT6407-77A w/ mount pipe (Verizon)	105
RFS APX16VDWV-16DWVS (T-Mobile)	130	(3) Samsung RF4439d-25A (Verizon)	105
(3) Ericsson 4415 B66A (T-Mobile)	130	(3) Samsung RF4440d-13A (Verizon)	105
(3) Ericsson 4449 B12+B71 (T-Mobile)	130	(3) Samsung CBR5 RRR-RT4401-48A (Verizon)	105
(3) Ericsson 4415 B25 (T-Mobile)	130	Raycap RVZDC-6627-PF-48 (Verizon)	105
12' Platform w/ Handrail (T-Mobile)	130	SitePro RMQP-496-HK Mount (Verizon)	105
Commscope VHLP1-23 (T-Mobile)	130	Commscope NHH-65B-R2B (Verizon)	105
Antennas + Equipment (EPA 11,000 in2 / 2,000 lbs) (Dish)	115		

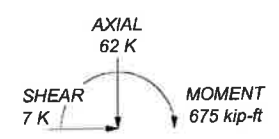
MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

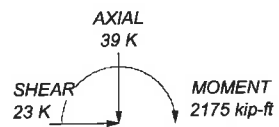
TOWER DESIGN NOTES

1. Tower is located in Hartford County, Connecticut.
2. Tower designed for Exposure C to the TIA-222-H Standard.
3. Tower designed for a 116 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 50 mph basic wind with 1.50 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: 39.9%

ALL REACTIONS ARE FACTORED



TORQUE 0 kip-ft
50 mph WIND - 1.5000 in ICE



TORQUE 0 kip-ft
REACTIONS - 116 mph WIND

Michael Plahovinsak, P.E. Job: **135' Monopole - MFP #94122-009**

18301 State Route 161
Plain City, OH 43064
Phone: 614-398-6250
FAX: mike@mfpeng.com

Project: **CT1209 Windsor**
Client: **Tarpon Towers**
Code: **TIA-222-H**
Path: C:\Users\jpc\Documents\MFP Engineering\135' Monopole\135' Monopole\135' Monopole.dwg

Drawn by: **JC**
Date: **05/09/23**
Scale: **NTS**
Dwg No: **E-1**

tnxTower Michael Plahovinsak, P.E. 18301 State Route 161 Plain City, OH 43064 Phone: 614-398-6250 FAX: mike@mfpeng.com	Job 135' Monopole - MFP #94122-009	Page 1 of 8
	Project CT1209 Windsor	Date 09:43:56 05/09/23
	Client Tarpon Towers	Designed by JC

Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower is located in Hartford County, Connecticut.

Tower base elevation above sea level: 175.00 ft.

Basic wind speed of 116 mph.

Risk Category II.

Exposure Category C.

Simplified Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Category: 1.

Crest Height: 0.00 ft.

Nominal ice thickness of 1.5000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	135.00-96.75	38.25	4.25	18	22.0000	30.8489	0.1875	0.7500	A572-65 (65 ksi)
L2	96.75-57.00	44.00	5.50	18	29.4907	39.6698	0.3750	1.5000	A572-65 (65 ksi)
L3	57.00-27.50	35.00	6.25	18	37.6474	45.7444	0.4375	1.7500	A572-65 (65 ksi)
L4	27.50-1.00	32.75		18	43.4235	51.0000	0.5000	2.0000	A572-65 (65 ksi)

Tapered Pole Properties

Section	Tip Dia. in	Area in ²	I in ⁴	r in	C in	I/C in ³	J in ⁴	I/Q in ²	w in	w/t
L1	22.3105	12.9812	780.3007	7.7434	11.1760	69.8193	1561.6281	6.4918	3.5420	18.891
	31.2958	18.2474	2167.3087	10.8848	15.6712	138.2986	4337.4693	9.1254	5.0994	27.197
L2	30.8861	34.6549	3711.5567	10.3361	14.9813	247.7466	7427.9971	17.3308	4.5304	12.081
	40.2239	46.7706	9123.8911	13.9496	20.1522	452.7481	18259.7876	23.3897	6.3219	16.858
L3	39.4527	51.6706	9038.5241	13.2095	19.1249	472.6057	18088.9412	25.8402	5.8559	13.385
	46.3826	62.9143	16316.0700	16.0840	23.2382	702.1241	32653.6091	31.4631	7.2810	16.642
L4	45.4845	68.1196	15856.2313	15.2378	22.0591	718.8055	31733.3266	34.0663	6.7625	13.525
	51.7096	80.1435	25821.9188	17.9275	25.9080	996.6774	51677.8148	40.0794	8.0960	16.192

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Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A_f	Adjust. Factor A_r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
ft	ft ²	in							
L1 135.00-96.75				1	1	1			
L2 96.75-57.00				1	1	1			
L3 57.00-27.50				1	1	1			
L4 27.50-1.00				1	1	1			

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Total Number	$C_A A_A$ ft ² /ft	Weight plf
1 1/4" (T-Mobile)	C	No	Yes	Inside Pole	130.00 - 1.00	4	No Ice	0.66
							1/2" Ice	0.66
							1" Ice	0.66
							2" Ice	0.66
1.65" (Dish)	C	No	Yes	Inside Pole	115.00 - 1.00	1	No Ice	0.92
							1/2" Ice	0.92
							1" Ice	0.92
							2" Ice	0.92
1 5/8" (Verizon)	C	No	Yes	Inside Pole	105.00 - 1.00	2	No Ice	0.92
							1/2" Ice	0.92
							1" Ice	0.92
							2" Ice	0.92

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A_R ft ²	A_F ft ²	$C_A A_A$ In Face ft ²	$C_A A_A$ Out Face ft ²	Weight K
L1	135.00-96.75	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.12
L2	96.75-57.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.21
L3	57.00-27.50	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.16
L4	27.50-1.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.14

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A_R ft ²	A_F ft ²	$C_A A_A$ In Face ft ²	$C_A A_A$ Out Face ft ²	Weight K
L1	135.00-96.75	A	1.699	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.12
L2	96.75-57.00	A	1.631	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.21

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Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
L3	57.00-27.50	A	1.536	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.16
L4	27.50-1.00	A	1.376	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.14

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C _{AA} Front ft ²	C _{AA} Side ft ²	Weight K	
Ericsson AIR 3246 B66 (T-Mobile)	A	From Face	3.00 0.00 0.00	0.0000	130.00	No Ice	8.04	6.41	0.24
						1/2" Ice	8.45	7.09	0.31
						1" Ice	8.87	7.78	0.38
						2" Ice	9.72	9.21	0.56
RFS - APXVAARR24_43-U-NA20 (T-Mobile)	A	From Face	3.00 0.00 0.00	0.0000	130.00	No Ice	20.24	10.79	0.16
						1/2" Ice	20.89	12.21	0.29
						1" Ice	21.55	13.49	0.44
						2" Ice	22.88	15.72	0.76
RFS APX16VDWV-16DWVS (T-Mobile)	A	From Face	3.00 0.00 0.00	0.0000	130.00	No Ice	6.67	3.34	0.06
						1/2" Ice	7.06	3.99	0.11
						1" Ice	7.47	4.64	0.16
						2" Ice	8.30	6.01	0.29
Ericsson AIR 3246 B66 (T-Mobile)	B	From Face	3.00 0.00 0.00	0.0000	130.00	No Ice	8.04	6.41	0.24
						1/2" Ice	8.45	7.09	0.31
						1" Ice	8.87	7.78	0.38
						2" Ice	9.72	9.21	0.56
RFS - APXVAARR24_43-U-NA20 (T-Mobile)	B	From Face	3.00 0.00 0.00	0.0000	130.00	No Ice	20.24	10.79	0.16
						1/2" Ice	20.89	12.21	0.29
						1" Ice	21.55	13.49	0.44
						2" Ice	22.88	15.72	0.76
RFS APX16VDWV-16DWVS (T-Mobile)	B	From Face	3.00 0.00 0.00	0.0000	130.00	No Ice	6.67	3.34	0.06
						1/2" Ice	7.06	3.99	0.11
						1" Ice	7.47	4.64	0.16
						2" Ice	8.30	6.01	0.29
Ericsson AIR 3246 B66 (T-Mobile)	C	From Face	3.00 0.00 0.00	0.0000	130.00	No Ice	8.04	6.41	0.24
						1/2" Ice	8.45	7.09	0.31
						1" Ice	8.87	7.78	0.38
						2" Ice	9.72	9.21	0.56
RFS - APXVAARR24_43-U-NA20 (T-Mobile)	C	From Face	3.00 0.00 0.00	0.0000	130.00	No Ice	20.24	10.79	0.16
						1/2" Ice	20.89	12.21	0.29
						1" Ice	21.55	13.49	0.44
						2" Ice	22.88	15.72	0.76
RFS APX16VDWV-16DWVS (T-Mobile)	C	From Face	3.00 0.00 0.00	0.0000	130.00	No Ice	6.67	3.34	0.06
						1/2" Ice	7.06	3.99	0.11
						1" Ice	7.47	4.64	0.16
						2" Ice	8.30	6.01	0.29
(3) Ericsson 4415 B66A (T-Mobile)	A	From Face	2.00 0.00 0.00	0.0000	130.00	No Ice	1.64	0.68	0.05
						1/2" Ice	1.80	0.79	0.06
						1" Ice	1.97	0.91	0.07
						2" Ice	2.32	1.18	0.11
(3) Ericsson 4449 B12+B71 (T-Mobile)	B	From Face	2.00 0.00 0.00	0.0000	130.00	No Ice	1.64	1.02	0.07
						1/2" Ice	1.80	1.15	0.09
						1" Ice	1.97	1.29	0.11

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment	Placement ft	C _{AA} Front ft ²	C _{AA} Side ft ²	Weight K	
(3) Ericsson 4415 B25 (T-Mobile)	C	From Face	2.00 0.00 0.00	0.0000	130.00	2" Ice	2.32	1.58	0.15
						No Ice	1.64	0.68	0.05
						1/2" Ice	1.80	0.79	0.06
						1" Ice	1.97	0.91	0.07
12' Platform w/ Handrail (T-Mobile)	C	None		0.0000	130.00	2" Ice	2.32	1.18	0.11
						No Ice	30.00	30.00	1.80
						1/2" Ice	35.00	35.00	2.60
						1" Ice	40.00	40.00	3.40
** Antennas + Equipment (EPA 11,000 in2 / 2,000 lbs) (Dish) **	C	None		0.0000	115.00	No Ice	76.39	76.39	2.00
						1/2" Ice	81.39	81.39	2.50
						1" Ice	86.39	86.39	3.00
						2" Ice	96.39	96.39	4.00
** Commscope NHH-65B-R2B (Verizon)	A	From Face	3.00 0.00 0.00	0.0000	105.00	No Ice	8.08	6.77	0.07
						1/2" Ice	8.53	7.72	0.13
						1" Ice	9.00	8.55	0.21
						2" Ice	9.95	10.26	0.38
Commscope NHHSS-65B-R2BT4 w/ mount pipe (Verizon)	A	From Face	3.00 0.00 0.00	0.0000	105.00	No Ice	8.05	6.78	0.07
						1/2" Ice	8.50	7.73	0.14
						1" Ice	8.97	8.56	0.21
						2" Ice	9.91	10.27	0.39
Samsung MT6407-77A w/ mount pipe (Verizon)	A	From Face	3.00 0.00 0.00	0.0000	105.00	No Ice	4.71	2.42	0.09
						1/2" Ice	5.00	2.83	0.13
						1" Ice	5.30	3.26	0.17
						2" Ice	5.92	4.16	0.27
Commscope NHH-65B-R2B (Verizon)	B	From Face	3.00 0.00 0.00	0.0000	105.00	No Ice	8.08	6.77	0.07
						1/2" Ice	8.53	7.72	0.13
						1" Ice	9.00	8.55	0.21
						2" Ice	9.95	10.26	0.38
Commscope NHHSS-65B-R2BT4 w/ mount pipe (Verizon)	B	From Face	3.00 0.00 0.00	0.0000	105.00	No Ice	8.05	6.78	0.07
						1/2" Ice	8.50	7.73	0.14
						1" Ice	8.97	8.56	0.21
						2" Ice	9.91	10.27	0.39
Samsung MT6407-77A w/ mount pipe (Verizon)	B	From Face	3.00 0.00 0.00	0.0000	105.00	No Ice	4.71	2.42	0.09
						1/2" Ice	5.00	2.83	0.13
						1" Ice	5.30	3.26	0.17
						2" Ice	5.92	4.16	0.27
Commscope NHH-65B-R2B (Verizon)	C	From Face	3.00 0.00 0.00	0.0000	105.00	No Ice	8.08	6.77	0.07
						1/2" Ice	8.53	7.72	0.13
						1" Ice	9.00	8.55	0.21
						2" Ice	9.95	10.26	0.38
Commscope NHHSS-65B-R2BT4 w/ mount pipe (Verizon)	C	From Face	3.00 0.00 0.00	0.0000	105.00	No Ice	8.05	6.78	0.07
						1/2" Ice	8.50	7.73	0.14
						1" Ice	8.97	8.56	0.21
						2" Ice	9.91	10.27	0.39
Samsung MT6407-77A w/ mount pipe (Verizon)	C	From Face	3.00 0.00 0.00	0.0000	105.00	No Ice	4.71	2.42	0.09
						1/2" Ice	5.00	2.83	0.13
						1" Ice	5.30	3.26	0.17
						2" Ice	5.92	4.16	0.27
(3) Samsung RF4439d-25A (Verizon)	A	From Face	2.00 0.00 0.00	0.0000	105.00	No Ice	1.88	1.25	0.08
						1/2" Ice	2.05	1.39	0.10
						1" Ice	2.22	1.54	0.12
						2" Ice	2.60	1.86	0.18
(3) Samsung RF4440d-13A	B	From Face	2.00	0.0000	105.00	No Ice	1.88	1.01	0.07

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight	
			ft ft ft	°	ft	ft ²	ft ²	K	
(Verizon)			0.00 0.00		1/2" Ice 1" Ice 2" Ice	2.05 2.22 2.60	1.14 1.28 1.59	0.09 0.11 0.15	
(3) Samsung CBRS RRH-RT4401-48A (Verizon)	C	From Face	2.00 0.00 0.00	0.0000	105.00	No Ice 1/2" Ice 1" Ice 2" Ice	0.99 1.12 1.26 1.55	0.50 0.60 0.70 0.94	0.02 0.03 0.04 0.06
Raycap RVZDC-6627-PF-48 (Verizon)	A	From Face	2.00 0.00 0.00	0.0000	105.00	No Ice 1/2" Ice 1" Ice 2" Ice	4.06 4.32 4.58 5.14	3.10 3.34 3.58 4.09	0.03 0.07 0.11 0.20
SitePro RMQP-496-HK Mount (Verizon)	C	None		0.0000	105.00	No Ice 1/2" Ice 1" Ice 2" Ice	30.00 35.00 40.00 50.00	30.00 35.00 40.00 50.00	2.00 2.20 2.40 2.80

Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight	
				ft ft ft	°	°	ft	ft	ft ²	K	
Commscope VHLP1-23 (T-Mobile)	C	Paraboloid w/Radome	From Face	1.00 0.00 0.00	0.0000		130.00	1.00	No Ice 1/2" Ice 1" Ice 2" Ice	0.79 0.92 1.06 1.33	0.02 0.02 0.03 0.04

Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.0 Wind 0 deg - No Ice
3	0.9 Dead+1.0 Wind 0 deg - No Ice
4	1.2 Dead+1.0 Wind 90 deg - No Ice
5	0.9 Dead+1.0 Wind 90 deg - No Ice
6	1.2 Dead+1.0 Wind 180 deg - No Ice
7	0.9 Dead+1.0 Wind 180 deg - No Ice
8	1.2 Dead+1.0 Ice+1.0 Temp
9	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
10	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
11	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
12	Dead+Wind 0 deg - Service
13	Dead+Wind 90 deg - Service
14	Dead+Wind 180 deg - Service

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Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	135 - 96.75	Pole	Max Tension	2	0.00	-0.00	-0.00
			Max. Compression	8	-26.24	0.34	1.43
			Max. Mx	4	-12.31	-257.94	0.37
			Max. My	2	-12.31	0.54	259.62
			Max. Vy	4	15.32	-257.94	0.37
			Max. Vx	2	-15.31	0.54	259.62
			Max. Torque	5			0.43
			Max Tension	1	0.00	0.00	0.00
L2	96.75 - 57	Pole	Max. Compression	8	-36.17	0.34	1.43
			Max. Mx	4	-19.34	-904.17	-0.25
			Max. My	2	-19.33	1.39	905.58
			Max. Vy	4	18.28	-904.17	-0.25
			Max. Vx	2	-18.28	1.39	905.58
			Max. Torque	5			0.43
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	8	-46.80	0.34	1.43
L3	57 - 27.5	Pole	Max. Mx	4	-27.37	-1462.71	-0.72
			Max. My	2	-27.37	2.01	1463.91
			Max. Vy	4	20.54	-1462.71	-0.72
			Max. Vx	2	-20.54	2.01	1463.91
			Max. Torque	5			0.43
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	8	-61.77	0.34	1.43
			Max. Mx	4	-39.34	-2174.17	-1.25
L4	27.5 - 1	Pole	Max. My	2	-39.34	2.71	2175.13
			Max. Vy	4	22.81	-2174.17	-1.25
			Max. Vx	2	-22.80	2.71	2175.13
			Max. Torque	5			0.42

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	135 - 96.75	11.199	12	0.7341	0.0001
L2	101 - 57	6.251	12	0.6011	0.0003
L3	62.5 - 27.5	2.302	12	0.3558	0.0001
L4	33.75 - 1	0.652	12	0.1779	0.0000

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
130.00	Commscope VHLP1-23	12	10.432	0.7176	0.0005	56811
115.00	Antennas + Equipment (EPA 11,000 in2 / 2,000 lbs)	12	8.182	0.6641	0.0004	14203
105.00	Commscope NHH-65B-R2B	12	6.779	0.6209	0.0004	9470

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Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	135 - 96.75	46.919	2	3.0756	0.0006
L2	101 - 57	26.198	2	2.5185	0.0011
L3	62.5 - 27.5	9.647	2	1.4914	0.0004
L4	33.75 - 1	2.734	2	0.7459	0.0002

Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
130.00	Commscope VHLP1-23	2	43.706	3.0065	0.0020	13646
115.00	Antennas + Equipment (EPA 11,000 in2 / 2,000 lbs)	2	34.285	2.7822	0.0019	3410
105.00	Commscope NHH-65B-R2B	2	28.410	2.6015	0.0017	2273

Pole Design Data

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio P _u φP _n
L1	135 - 96.75 (1)	TP30.8489x22x0.1875	38.25	0.00	0.0	17.6622	-12.31	1033.24	0.012
L2	96.75 - 57 (2)	TP39.6698x29.4907x0.375	44.00	0.00	0.0	45.2561	-19.34	2647.48	0.007
L3	57 - 27.5 (3)	TP45.7444x37.6474x0.4375	35.00	0.00	0.0	60.9065	-27.37	3563.03	0.008
L4	27.5 - 1 (4)	TP51x43.4235x0.5	32.75	0.00	0.0	80.1435	-39.34	4688.40	0.008

Pole Bending Design Data

Section No.	Elevation ft	Size	M _{ux} kip-ft	φM _{ux} kip-ft	Ratio M _{ux} φM _{ux}	M _{vy} kip-ft	φM _{vy} kip-ft	Ratio M _{vy} φM _{vy}
L1	135 - 96.75 (1)	TP30.8489x22x0.1875	259.62	674.89	0.385	0.00	674.89	0.000
L2	96.75 - 57 (2)	TP39.6698x29.4907x0.375	905.58	2582.00	0.351	0.00	2582.00	0.000
L3	57 - 27.5 (3)	TP45.7444x37.6474x0.4375	1463.92	4019.69	0.364	0.00	4019.69	0.000
L4	27.5 - 1 (4)	TP51x43.4235x0.5	2175.13	6078.80	0.358	0.00	6078.80	0.000

Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V _u K	φV _n K	Ratio V _u φV _n	Actual T _u kip-ft	φT _n kip-ft	Ratio T _u φT _n
L1	135 - 96.75 (1)	TP30.8489x22x0.1875	15.31	309.97	0.049	0.28	805.64	0.000
L2	96.75 - 57 (2)	TP39.6698x29.4907x0.375	18.28	794.25	0.023	0.28	2644.68	0.000
L3	57 - 27.5 (3)	TP45.7444x37.6474x0.4375	20.54	1068.91	0.019	0.28	4105.82	0.000
L4	27.5 - 1 (4)	TP51x43.4235x0.5	22.80	1406.52	0.016	0.28	6220.37	0.000

tnxTower Michael Plahovinsak, P.E. 18301 State Route 161 Plain City, OH 43064 Phone: 614-398-6250 FAX: mike@mfpeng.com	Job 135' Monopole - MFP #94122-009	Page 8 of 8
	Project CT1209 Windsor	Date 09:43:56 05/09/23
	Client Tarpon Towers	Designed by JC

Pole Interaction Design Data

Section No.	Elevation ft	Ratio P_u ϕP_n	Ratio M_{ux} ϕM_{nx}	Ratio M_{uy} ϕM_{ny}	Ratio V_u ϕV_n	Ratio T_u ϕT_n	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	135 - 96.75 (1)	0.012	0.385	0.000	0.049	0.000	0.399	1.000	4.8.2 ✓
L2	96.75 - 57 (2)	0.007	0.351	0.000	0.023	0.000	0.359	1.000	4.8.2 ✓
L3	57 - 27.5 (3)	0.008	0.364	0.000	0.019	0.000	0.372	1.000	4.8.2 ✓
L4	27.5 - 1 (4)	0.008	0.358	0.000	0.016	0.000	0.366	1.000	4.8.2 ✓

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	ϕP_{allow} K	% Capacity	Pass Fail	
L1	135 - 96.75	Pole	TP30.8489x22x0.1875	1	-12.31	1033.24	39.9	Pass	
L2	96.75 - 57	Pole	TP39.6698x29.4907x0.375	2	-19.34	2647.48	35.9	Pass	
L3	57 - 27.5	Pole	TP45.7444x37.6474x0.4375	3	-27.37	3563.03	37.2	Pass	
L4	27.5 - 1	Pole	TP51x43.4235x0.5	4	-39.34	4688.40	36.6	Pass	
							Summary		
							Pole (L1)	39.9	Pass
							RATING =	39.9	Pass

Michael F. Plahovinsak, P.E. 18301 State Route 161 W Plain City, OH 43064 Phone: 614-398-6250 email: mike@mpeng.com	Job 135-ft monopole - MFP #94122-009	Page BP & AB Calc
	Project CT1209 Windsor	Date 5/9/2023
	Client Tarpon Towers	Designed by Mike

Anchor Rod and Base Plate Calculation

TIA-222-H

Factored Base Reactions:	Pole Shape:	Anchor Rods:	Base Plate:
Moment: 2175 ft-kips	18-Sided	(18) 2.25 in. A615 GR. 75	2.5 in. x 64.5 in. Round
Shear: 23 kips	Pole Dia. (D_p):	Anchor Rods Evenly Spaced	fy = 50 ksi
Axial: 39 kips	51.00 in	On a 58.5 in Bolt Circle	

Anchor Rod Calculation According to TIA-222-H section 4.9.9

$\phi_t, \phi_v = 0.75$ TIA 4.9.6
 $I_{bolts} = 7700.06 \text{ in}^2$ Moment of Inertia
 $P_u = 101 \text{ kips}$ Compr Force
 $V_u = 1.3 \text{ kips}$ Shear Force
 $R_{nt} = 325.00 \text{ kips}$ Nominal Tensile Strength
 $R_{nv} = 198.80 \text{ kips}$ (0.5 x fu x ag)
Stress Rating = 42.5% Satisfies TIA-H 4.9.9

Base Plate Calculation According to TIA-222-H

$\phi = 0.90$ TIA 4.7
 $M_{PL} = 235.6 \text{ in-kip}$ Plate Moment
 $L = 8.9 \text{ in}$ Section Length
 $Z = 13.9$ Plastic Section Modulus
 $M_p = 695.4 \text{ in-kip}$ Plastic Moment
 $\phi M_n = 625.9 \text{ in-kip}$ Factored Resistance

Calculated Moment vs Factored Resistance
 $235.62 \text{ in-kip} \leq 626 \text{ in-kip}$

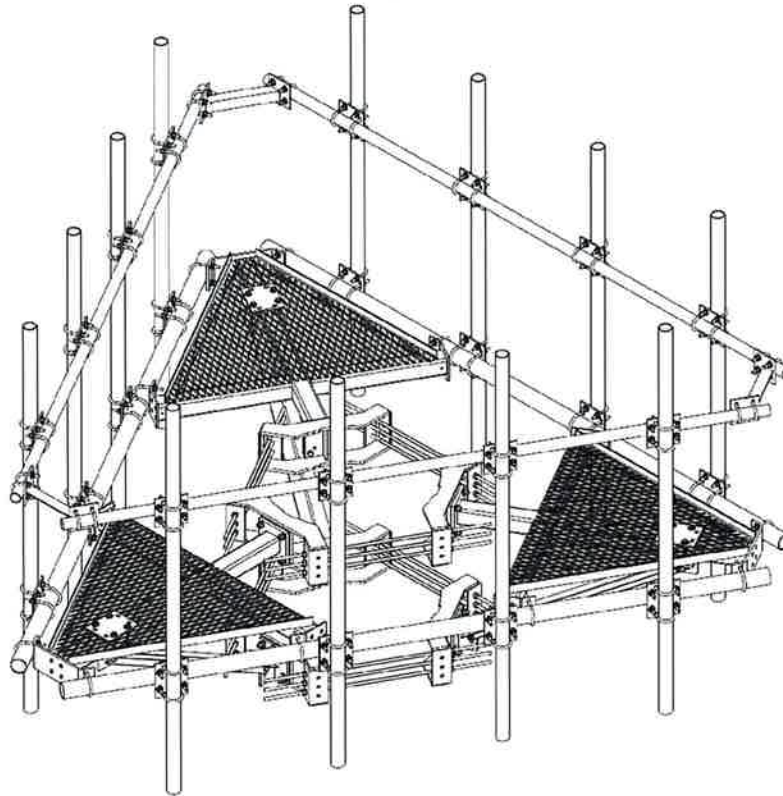
Stress Rating = 37.6%

Anchor Rods Are Adequate	42.5% <input checked="" type="checkbox"/>
Base Plate is Adequate	37.6% <input checked="" type="checkbox"/>



20 Alexander Drive, 2nd Floor
Wallingford, CT 06492

ANTENNA MOUNT ANALYSIS
WINDSOR 4 CT



Address:

780 PROSPECT HILL ROAD
WINDSOR, CT 06095

LOCATION CODE: 470880

Date:

APRIL 13, 2023 (REVISION 0)



April 13, 2023



20 Alexander Drive
2nd Floor
Wallingford, CT 06492

RE:

Applicant Site Name: Windsor 4 CT
Location Code: 470880
Site Address: 780 Prospect Hill Road, Windsor, CT 06095

To whom it may concern:

Chappell Engineering Associates, LLC has performed a structural analysis of the proposed Verizon braced low-profile antenna mounting platform being proposed at the existing 135' +/- monopole located at the above-referenced address at approximately 105 ft AGL to analyze the effect of the proposed Verizon antenna installation on the subject platform. Our analysis has been performed in accordance with the 2022 Connecticut State Building Code (2021 International Building Code) with Connecticut Amendments.

The proposed antenna support structure will consist of one (1) low-profile antenna frame supporting twelve (12) individual antenna pipes mounts. Our analysis has considered the following total major equipment loads indicated on the antenna design summary (included in this report) to be installed on the proposed low-profile antenna frame:

Appurtenance	Size (HxWxD)(in)	Weight	Location	Status
(3) NHH-65B-R2B Panel Antennas	72.0x11.9x7.1	43.7lbs	Face of Mount	Proposed
(3) NHHSS-65B-R2BT4 Panel Antennas	72.0x11.9x7.1	48.1lbs	Face of Mount	Proposed
(3) Samsung MT6407-77A Panel Antennas	35.2x16.1x5.6	88lbs	Face of Mount	Proposed
(3) Samsung RF4440d-13A B5/B13	15.0x15.0x9.0	71lbs	Face of Mount	Proposed
(3) Samsung RF4439d-25A B2/B66A	15.0x15.0x10.0	75lbs	Face of Mount	Proposed
(3) RT4401-48A RRH	13.9x8.6x4.2	18.6lbs	Face of Mount	Proposed
(1) Fiber Junction Box	29.6x16.5x12.6	32lbs	Face of Mount	Proposed

The proposed antennas and ancillary hardware are shown on the enclosed Lease Exhibit.

We have modeled the entire low-profile antenna frame under both wind and wind/ice loads. Our analysis and results are included in this report.

Based upon our analysis of the antenna mounts being proposed, **we consider the proposed RMQP-496-HK low-profile mounting frame assembly has adequate capacity** to support the proposed antenna configuration as shown. **The maximum percentage stress capacity as determined by our analysis are the antenna mounting pipes supporting the combined dual-mount antennas with a capacity of 48%.** Our analysis assumes the proposed antenna mounting platform will be properly installed and maintained according to manufacturers' recommendations.

If you have any questions regarding this matter, please do not hesitate to call.

Very truly yours,

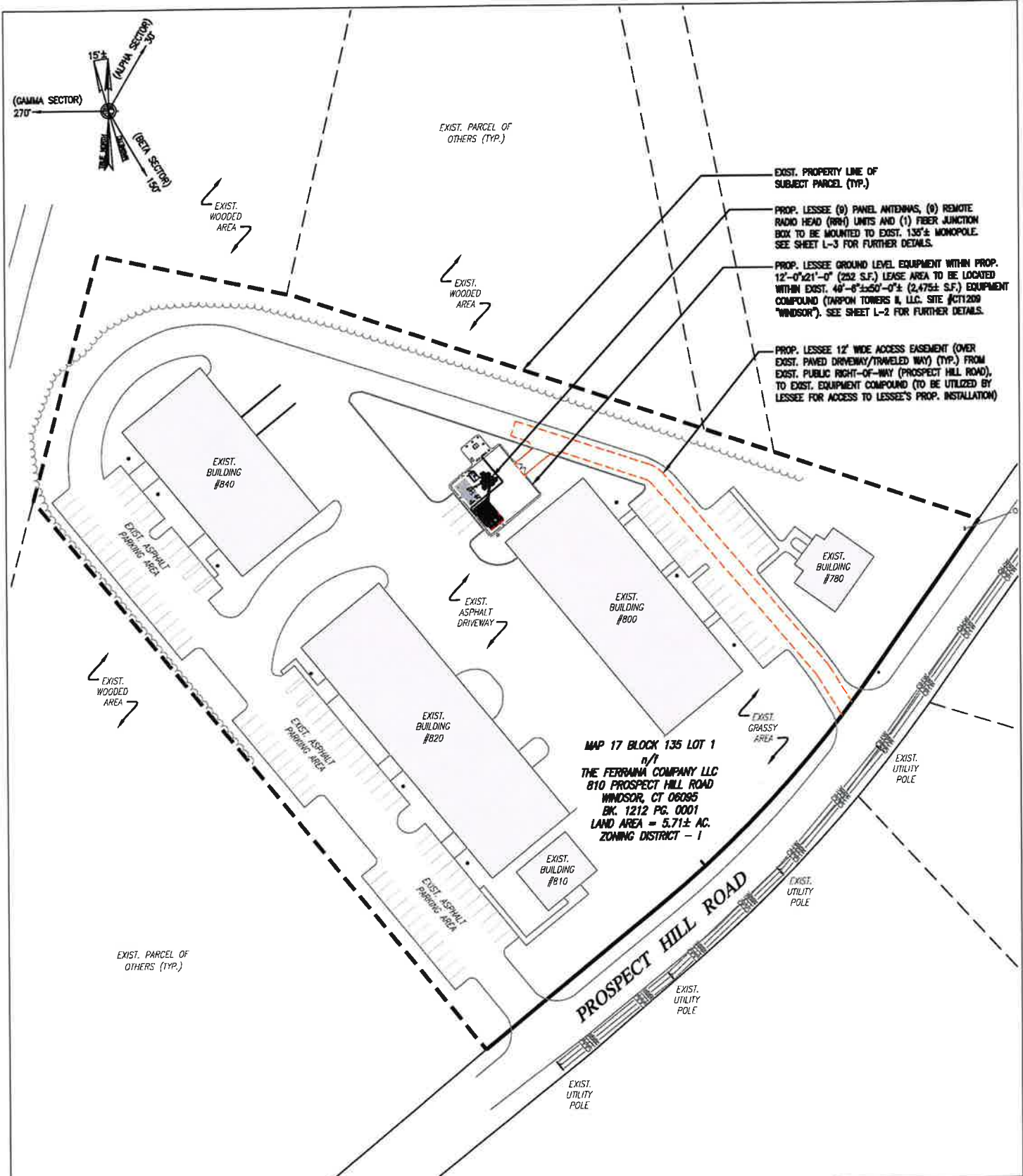
CHAPPELL ENGINEERING ASSOCIATES, LLC



Clement J Salek, P.E.
CJS/cjs



Appendix A – Lease Exhibit



PROPERTY PLAN 1
SCALE: 1" = 100' L-1

DRAWING SCALE NOTE:
THESE DRAWINGS HAVE BEEN PREPARED IN LETTER (8 1/2"x11") FORMAT. AS SUCH, THE WRITTEN SCALES SHOWN ON ANY REPRODUCTIONS OF A CONSTRUCTION SIZE SHALL BE REVISED TO MATCH ALL DIM SCALES MAY BE USED. REGARDLESS OF REPRODUCTION SIZE, WHERE IN CONFLICT, DIM SCALES SHALL SUPERSEDE WRITTEN SCALES.

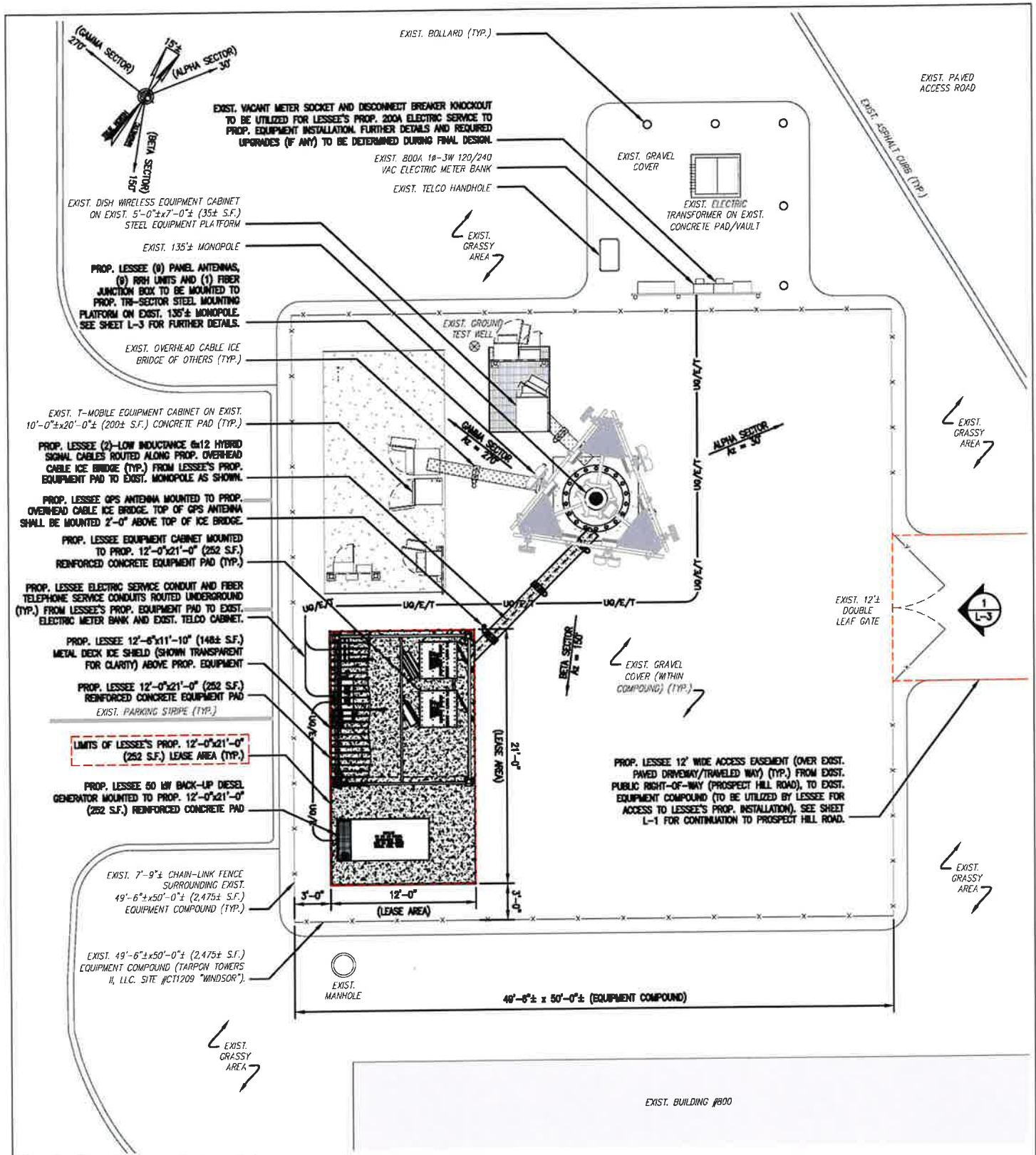
C CHAPPELL
ENGINEERING
ASSOCIATES, LLC
Civil · Structural · Land Surveying

NO.	DATE	REVISIONS	BY	CHK	APP'D
2	4/5/23	REVISED RRH COUNT	NWC	GRS	GRS
1	4/5/23	REVISED ELEVATIONS	NWC	GRS	GRS
0	2/7/23	ISSUED FOR REVIEW	NWC	GRS	GRS

NO. DATE REVISIONS BY CHK APP'D
SCALE: 1" = 100' DESIGNED BY: GRS DRAWN BY: NWC

WINDSOR 4 CT
780 PROSPECT HILL ROAD
WINDSOR, CT 06085
LEASE EXHIBIT
NOT FOR CONSTRUCTION

LEASE AREA				
PROJECT NO.	DRAWING NAME	DATE	LOC. CODE	REV
EQUIPMENT LEASE AREA: 12'-0"x21'-0" (252 S.F.)				
TOTAL = 252 S.F.				
PR210.416	L-1	4/5/23	470680	2



● **SITE CONTROL POINT:**
 CENTER OF EXISTING MONOPOLE
 N 41°-52'-58.47" (41.882908°) (NAD '83)
 W 72°-42'-29.14" (72.708094°) (NAD '83)
 GROUND ELEVATION - 174.0' AMSL (NAVD '88)

PER 1A SURVEY OF OTHERS

EQUIPMENT COMPOUND PLAN 1
 SCALE: 3/32" = 1'-0"

DRAWING SCALE NOTE:
 THESE DRAWINGS HAVE BEEN PREPARED IN LETTER (8 1/2"x11") FORMAT. AS SUCH, THE WRITTEN SCALES SHOWN ON ANY REPRODUCTIONS OF A CONCORDATORY SIZE SHALL BE FOLLOWS. ALL DIM. SCALES MAY BE USED. NOTWITHSTANDING OF REPRODUCTION SIZE, WHERE IN CONFLICT, DIM. SCALES SHALL SUPERSEDE WRITTEN SCALES.

CHAPPELL ENGINEERING ASSOCIATES, LLC
 Civil · Structural · Land Surveying

NO.	DATE	REVISIONS	BY	CHK	APP'D
2	4/5/23	REVISED RISH COUNT	NWC	GRS	GRS
1	4/5/23	REVISED ELEVATIONS	NWC	GRS	GRS
0	2/7/23	ISSUED FOR REVIEW	NWC	GRS	GRS

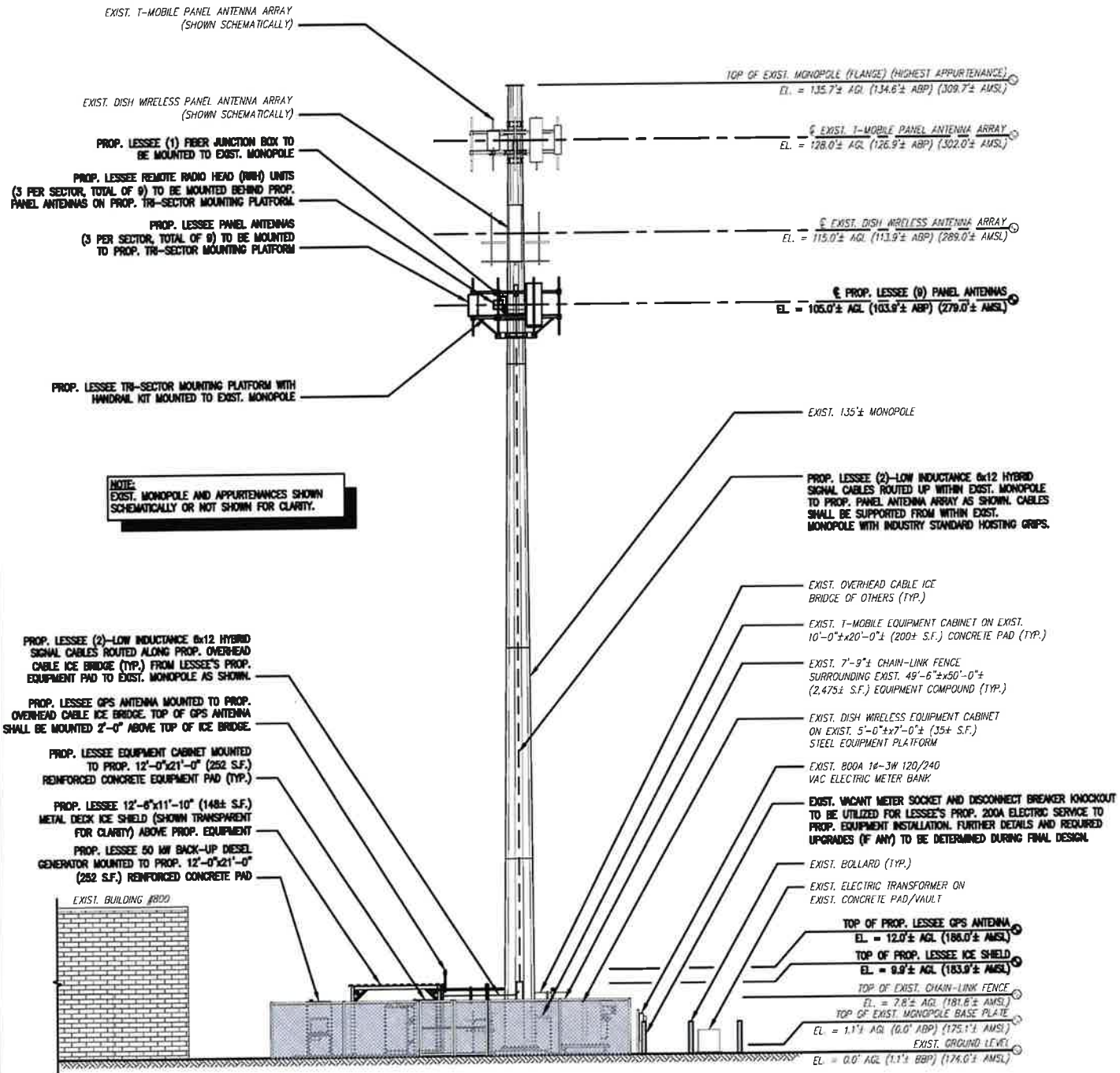
SCALE: 3/32" = 1'-0" DESIGNED BY: GRS DRAWN BY: NWC

WINDSOR 4 CT
 780 PROSPECT HILL ROAD
 WINDSOR, CT 06095

LEASE EXHIBIT
 NOT FOR CONSTRUCTION

LEASE AREA			
EQUIPMENT LEASE AREA: 12'-0"x21'-0" (252 S.F.)			
TOTAL = 252 S.F.			
PROJECT NO.	DRAWING NAME	DATE	LOC. CODE REV
06210.416	L-2	4/5/23	470880 2

LEGEND	
AGL	ABOVE GROUND LEVEL
ABP	ABOVE MONOPOLE BASE PLATE
BBP	BELOW MONOPOLE BASE PLATE
AMSL	ABOVE MEAN SEA LEVEL



NORTHEAST EQUIPMENT COMPOUND ELEVATION 1

SCALE: 1" = 20'

DRAWING SCALE NOTE:
THESE DRAWINGS HAVE BEEN PREPARED IN LETTER (8 1/2"x11") FORMAT. AS SUCH, THE WRITTEN SCALES SHOWN ON ANY REPRODUCTION OF A CONFLICTORY SIZE SHALL BE RENDERED INVALID. ALL DIM. SCALES MAY BE USED REGARDLESS OF REPRODUCTION SIZE. WHERE IN CONFLICT, DIM. SCALES SHALL SUPERSEDE WRITTEN SCALES.

C CHAPPELL
ENGINEERING
ASSOCIATES, LLC
Civil · Structural · Land Surveying

NO.	DATE	REVISIONS	BY	CHK	APP'D
2	4/5/23	REVISED RRH COUNT	NWC	GRS	GRS
1	4/5/23	REVISED ELEVATIONS	NWC	GRS	GRS
0	2/7/23	ISSUED FOR REVIEW	NWC	GRS	GRS

DESIGNED BY: GRS DRAWN BY: NWC

WINDSOR 4 CT

780 PROSPECT HILL ROAD
WINDSOR, CT 06095

LEASE EXHIBIT
NOT FOR CONSTRUCTION

LEASE AREA			
EQUIPMENT LEASE AREA: 12'-0"x21'-0" (252 S.F.)			
TOTAL = 252 S.F.			
PROJECT NO.	DRAWING NAME	DATE	LOC. CODE
06210.418	L-3	4/5/23	470080
REV	2		

Appendix B – Mount Analysis

Windsor 4 CT Mount Analysis

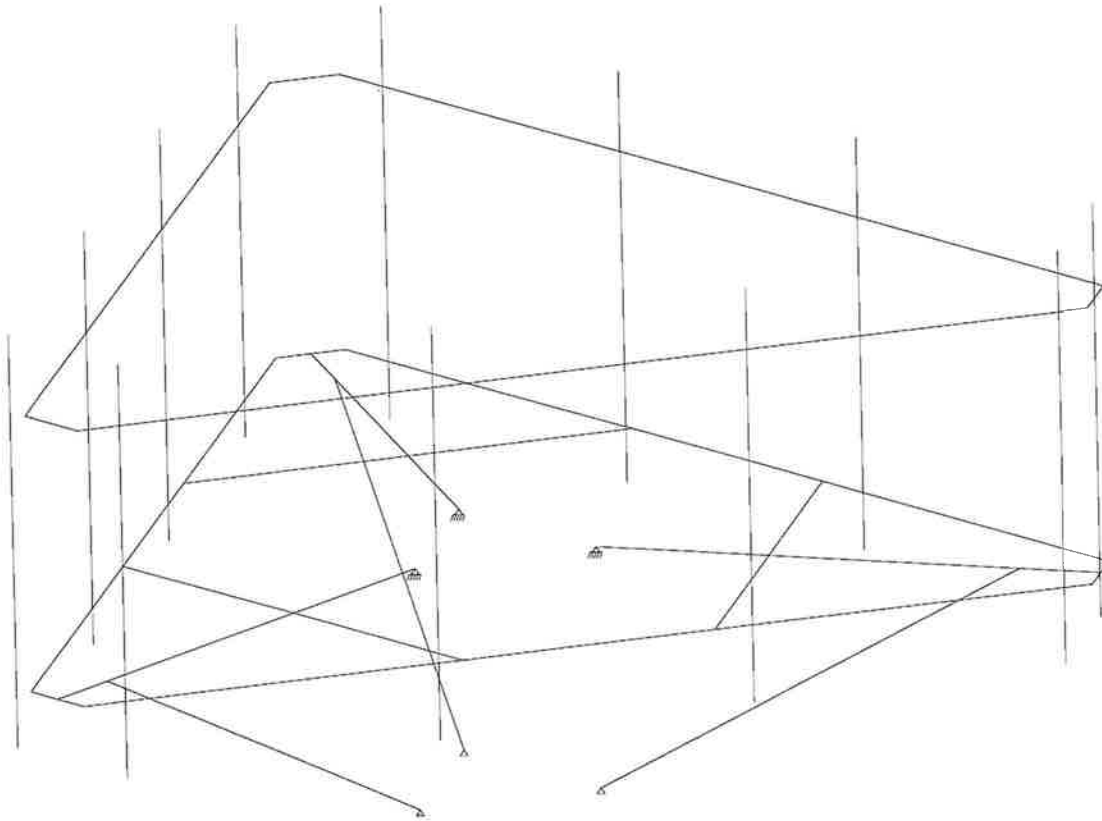
View: Steel Beam Design



SCALE = 1:30

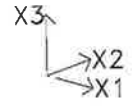
UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

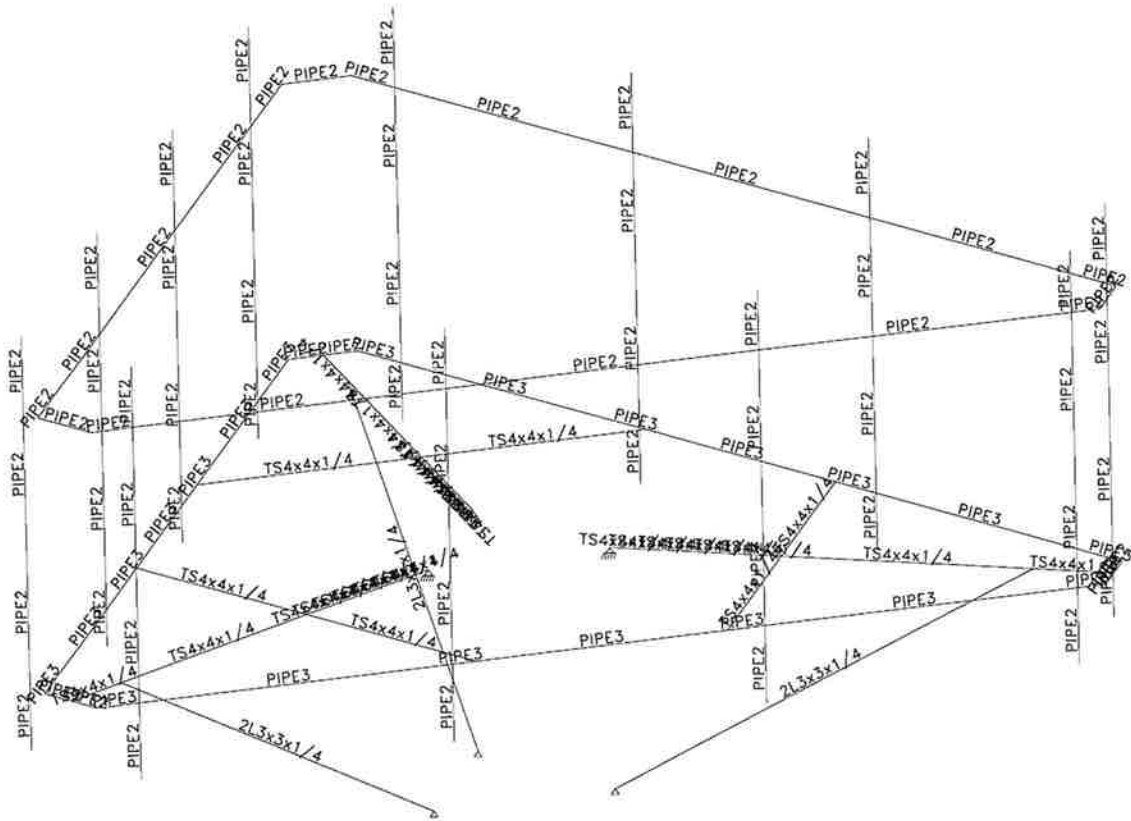
View: Steel Beam Design



SCALE = 1:30

UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

Page: 1
Date: 4/10/23

Prepared by:

Load no. 1: Front No Ice (units - kips ft.)

/ JOINT LOADS
 / BEAM LOADS
 / JOINT LOADS
 / BEAM LOADS
 / JOINT LOADS
 / BEAM LOADS
 / JOINT LOADS
 / JOINT LOADS
 / JOINT LOADS
 / JOINT LOADS
 / JOINT LOADS
 FX2 0.073 FX3 -0.045 N 70 26
 FX2 0.025 FX3 -0.045 N 84 54 76 38
 FX2 0.047 FX3 -0.023 N 132
 FX2 0.047 FX3 -0.023 N 133 135
 FX2 0.22 FX3 -0.045 N 28 27
 FX2 0.143 FX3 -0.045 N 48 47 64 63
 FX2 0.57 FX3 -0.084 N 126 131 127 136 125 134
 / END

FORCE SUMMATION

FX1=0. kip
 FX2=4.819 kip
 FX3=-1.113 kip

Load no. 2: Side No Ice (units - kips ft.)

/ JOINT LOADS
 / BEAM LOADS
 / JOINT LOADS
 / BEAM LOADS
 / JOINT LOADS
 / BEAM LOADS
 / JOINT LOADS
 / BEAM LOADS
 / JOINT LOADS
 / JOINT LOADS
 / JOINT LOADS
 / JOINT LOADS
 FX1 0.025 FX3 -0.044 N 70 26 76 38 84 54
 FX1 0.047 FX3 -0.023 N 132 135 133
 FX1 0.143 FX3 -0.045 N 28 27 48 47 64 63
 FX1 0.057 FX3 -0.084 N 126 127 125
 FX1 0.057 FX3 -0.084 N 131 136 134
 / END

FORCE SUMMATION

FX1=1.491 kip
 FX2=0. kip
 FX3=-1.107 kip

Windsor 4 CT Mount Analysis

Page: 2
Date: 4/10/23

Prepared by:

Load no. 3: Front Ice (units - kips ft.)

/ JOINT LOADS
/ BEAM LOADS
/ JOINT LOADS
/ BEAM LOADS
/ JOINT LOADS

/ JOINT LOADS
/ BEAM LOADS
/ JOINT LOADS
/ JOINT LOADS
/ JOINT LOADS

FX2 0.021 FX3 -0.075 N 70 26
FX2 0.01 FX3 -0.075 N 76 38 84 54
FX2 0.016 FX3 -0.049 N 132 135 133
FX2 0.065 FX3 -0.156 N 28 27 48 47 64 63
FX2 0.02 FX3 -0.123 N 126 127 125 134 131 136

/END

FORCE SUMMATION

FX1=0. kip
FX2=0.64 kip
FX3=-2.271 kip

Load no. 4: Side Ice (units - kips ft.)

/ JOINT LOADS
/ BEAM LOADS
/ JOINT LOADS
/ BEAM LOADS
/ JOINT LOADS

/ BEAM LOADS
/ JOINT LOADS
/ JOINT LOADS
/ JOINT LOADS

FX1 0.01 FX3 -0.075 N 70 26 38 76 84 54
FX1 0.01 FX3 -0.049 N 132 135 133
FX1 0.048 FX3 -0.156 N 28 27 48 47 64 63
FX1 0.014 FX3 -0.123 N 126 127 125 134 131 136

/END

FORCE SUMMATION

FX1=0.462 kip
FX2=0. kip
FX3=-2.271 kip

Windsor 4 CT Mount Analysis

Page: 3
Date: 4/10/23

Prepared by:

Load no. 5: Selfweight (units - kips ft.)

/ BEAM LOADS
 SELF X3 -1. B 1 TO 138 142 TO 150
 / GLOBAL LOADS
 / GLOBAL LOADS
 / GLOBAL LOADS
 DIST FX3 -0.003 PLANE -7.25 4.763 0. -1.805 4.763 0. -5.028 -0.818
 0. PT -0.5 0.866 BEAMS
 DIST FX3 -0.003 PLANE 1.805 4.763 0. 7.25 4.763 0. 7.75 3.897 0. PT
 3.223 5.581 BEAMS
 DIST FX3 -0.003 PLANE -3.222 -3.945 0. 3.222 -3.945 0. 0.5 -8.66
 0. PT 2.722 4.715 BEAMS
 / END

FORCE SUMMATION

FX1=0. kip
 FX2=0. kip
 FX3=-1.4597 kip

Load no. 6: Front Frame Ice (units - kips ft.)

/ BEAM LOADS
 DIST GL FX2 -0.002 B 1 4 5 13 TO 35 BY 2 49 TO 51 55 56 63 64 66 71 TO 74
 76 TO 81 83 TO 88 90 TO 115 117 133 TO 135 142 TO 150
 / END

FORCE SUMMATION

FX1=0. kip
 FX2=-0.3127 kip
 FX3=0. kip

Load no. 7: Side Frame Ice (units - kips ft.)

/ BEAM LOADS
 / BEAM LOADS
 DIST GL FX1 -0.002 B 4 5 13 TO 35 BY 2 50 51 63 64 66 71 72 TO 78 BY 2
 79 TO 81 83 TO 88 90 91 93 94 TO 100 BY 2 101 TO 115 117 133 TO 135
 142 TO 150
 / END

FORCE SUMMATION

FX1=-0.2564 kip
 FX2=0. kip
 FX3=0. kip

Windsor 4 CT Mount Analysis

Page: 4
Date: 4/10/23

Prepared by:

Load no. 8: Front Frame No Ice (units - kips ft.)

/ BEAM LOADS
/ BEAM LOADS
DIST GL FX2 -0.005 B 1 4 5 13 TO 35 BY 2 49 TO 51 55 56 63 64 66 71 TO 74
76 TO 81 83 TO 88 90 TO 115 117 133 TO 135 142 TO 150
/ END

FORCE SUMMATION

FX1=0. kip
FX2=-0.7817 kip
FX3=0. kip

Load no. 9: Side Frame No Ice (units - kips ft.)

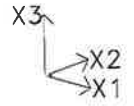
/ BEAM LOADS
/ BEAM LOADS
/ BEAM LOADS
DIST GL FX1 -0.005 B 4 5 13 TO 35 BY 2 50 51 63 64 66 71 72 TO 78 BY 2
79 TO 81 83 TO 88 90 91 93 94 TO 100 BY 2 101 TO 115 117 133 TO 135
142 TO 150
/ END STATIC

FORCE SUMMATION

FX1=-0.6411 kip
FX2=0. kip
FX3=0. kip

Windsor 4 CT Mount Analysis

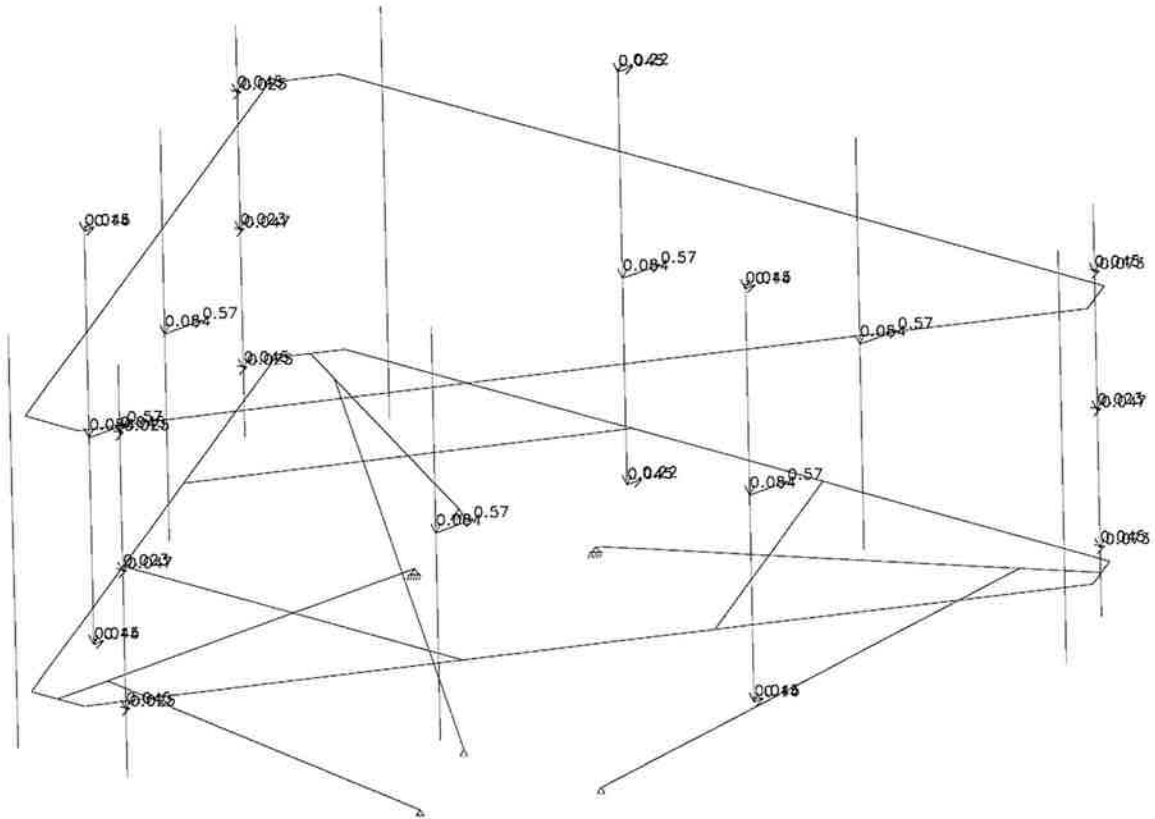
Load 1: Front No Ice
View: Steel Beam Design



SCALE = 1:30

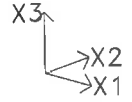
UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

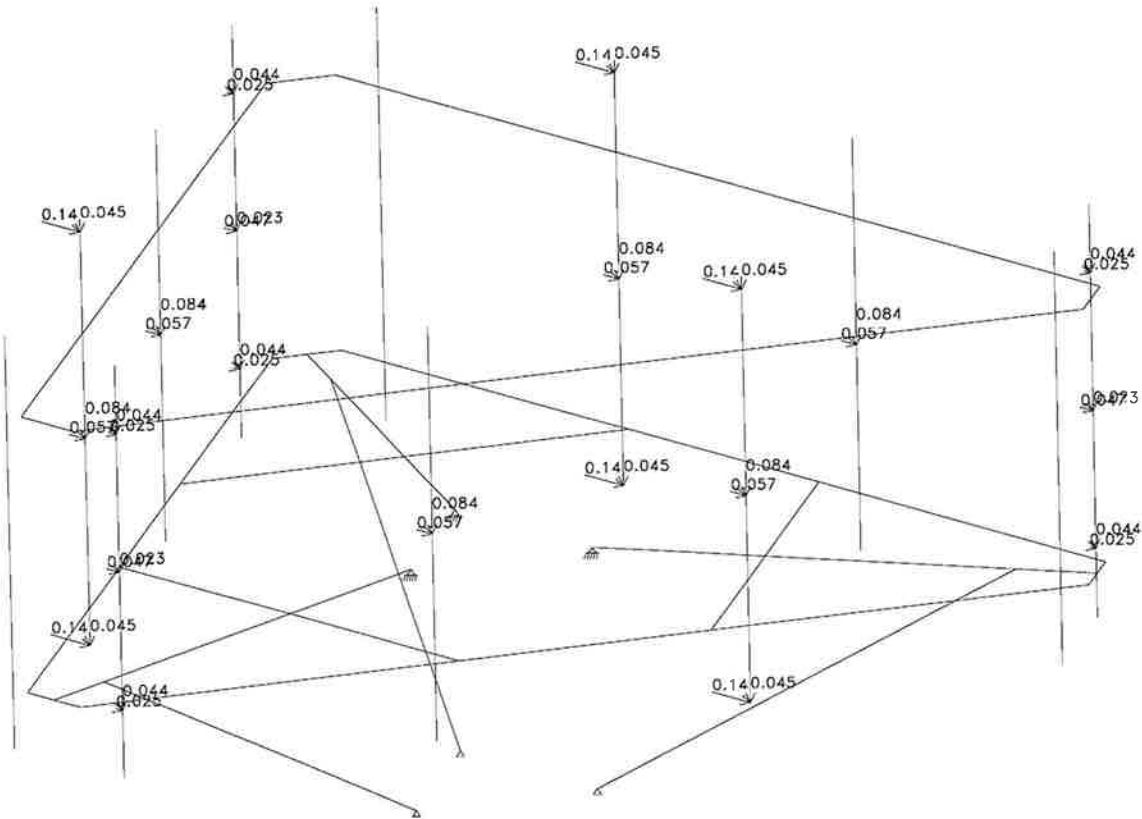
Load 2: Side No Ice
View: Steel Beam Design



SCALE = 1:30

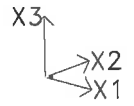
UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

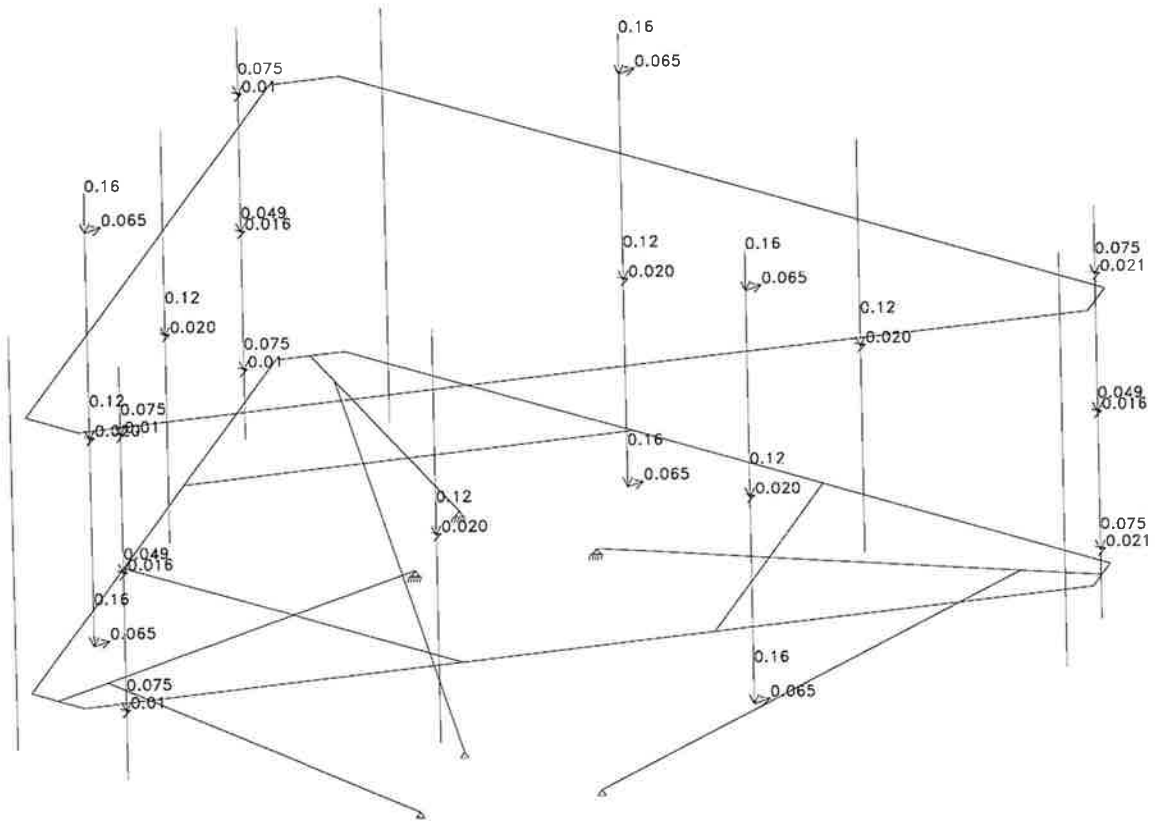
Load 3: Front Ice
View: Steel Beam Design



SCALE = 1:30

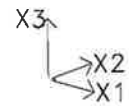
UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

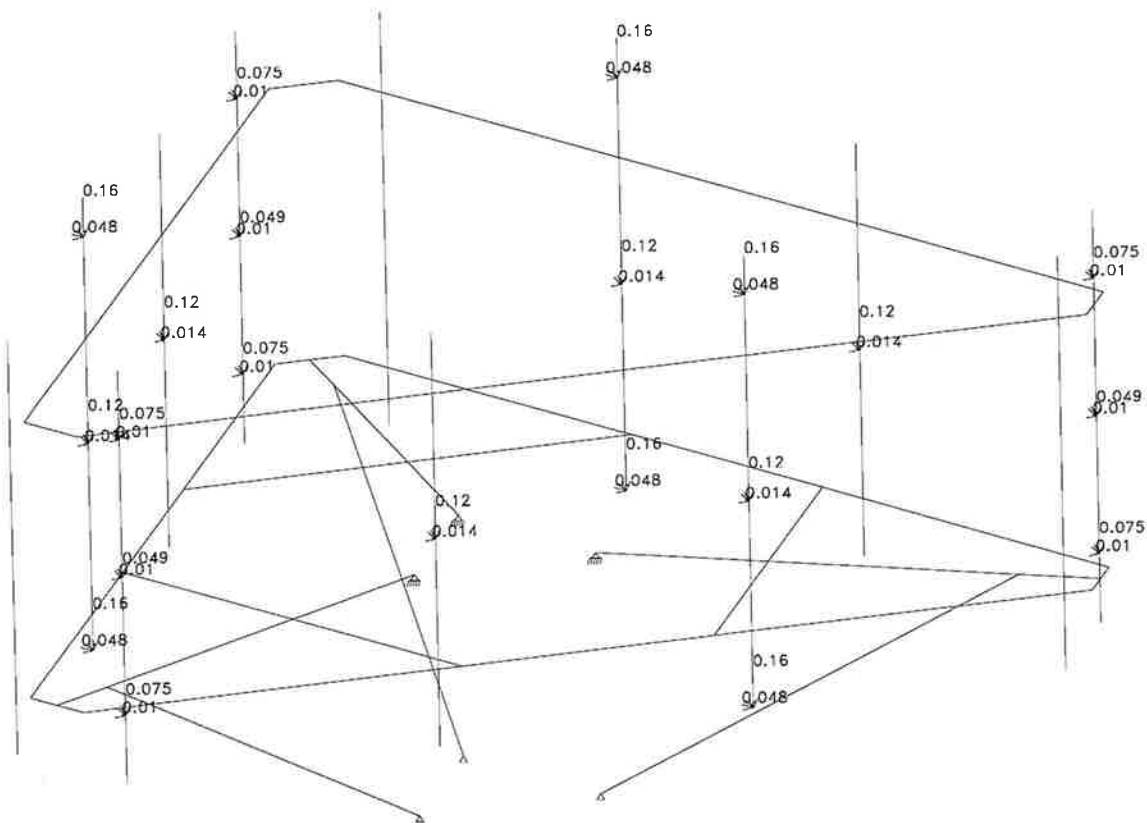
Load 4: Side Ice
View: Steel Beam Design



SCALE = 1:30

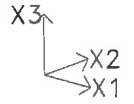
UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

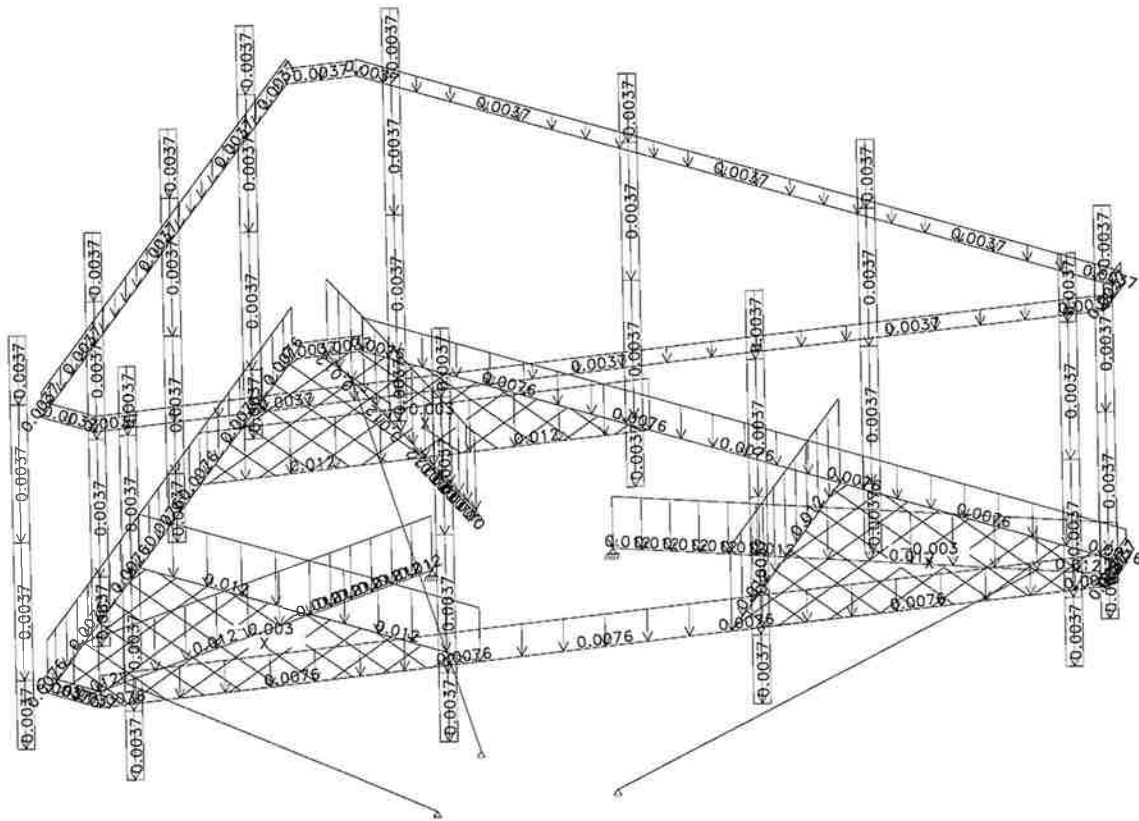
Load 5: Selfweight
View: Steel Beam Design



SCALE = 1:30

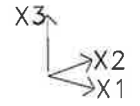
UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

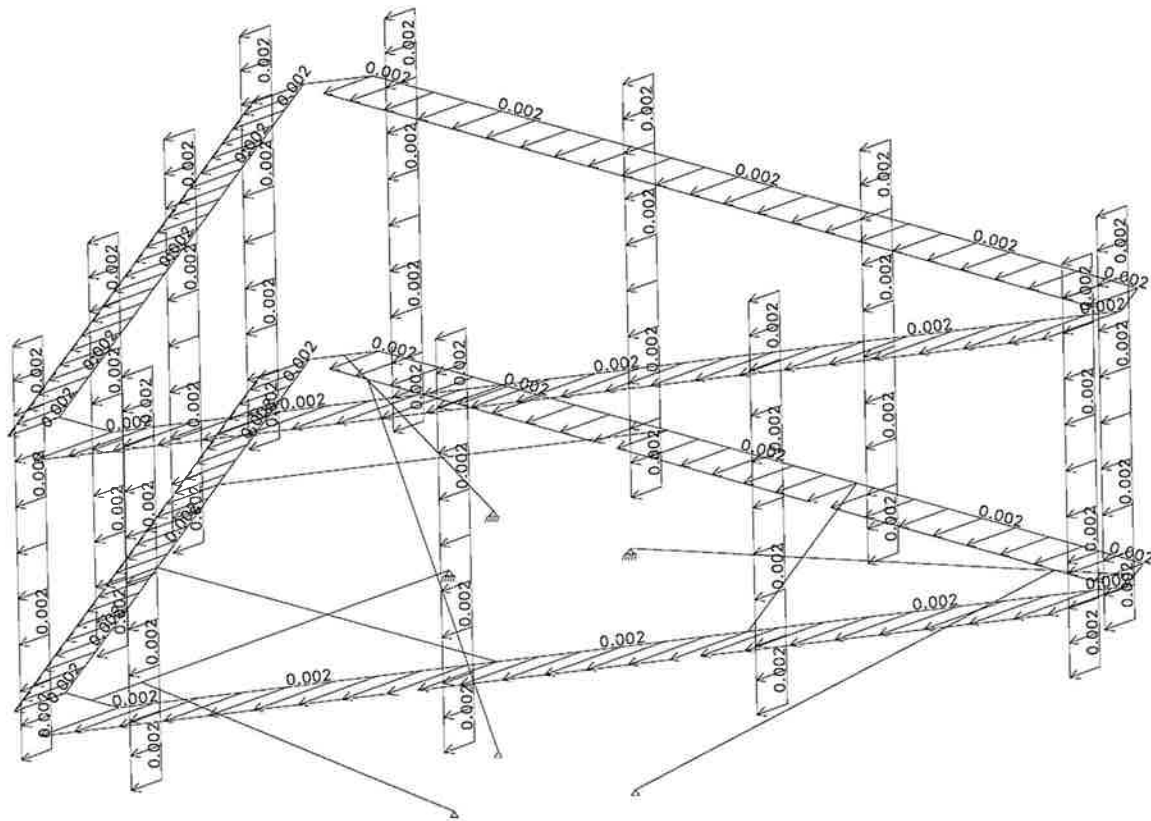
Load 6: Front Frame Ice
View: Steel Beam Design



SCALE = 1:30

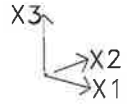
UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

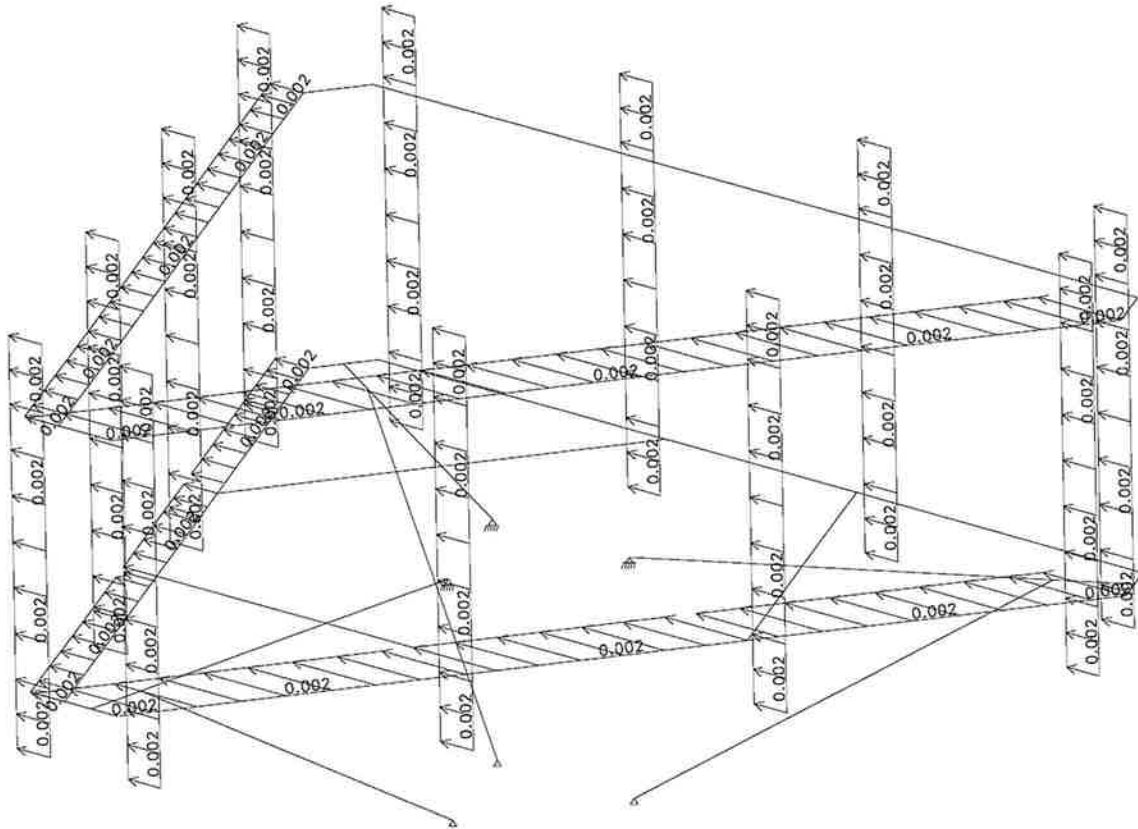
Load 7: Side Frame Ice
View: Steel Beam Design



SCALE = 1:30

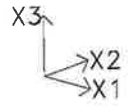
UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

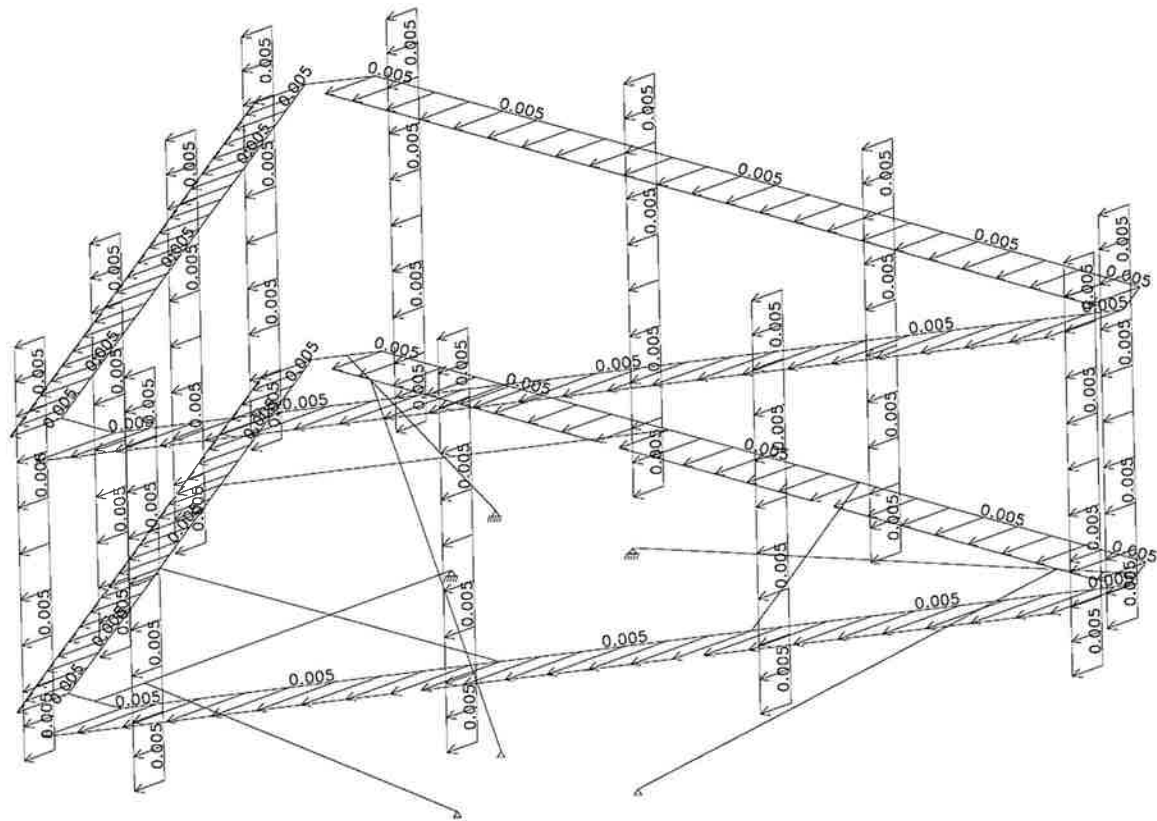
Load 8: Front Frame No Ice
View: Steel Beam Design



SCALE = 1:30

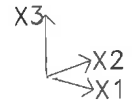
UNITS: kip ft

DATE: 4/10/23



Windsor 4 CT Mount Analysis

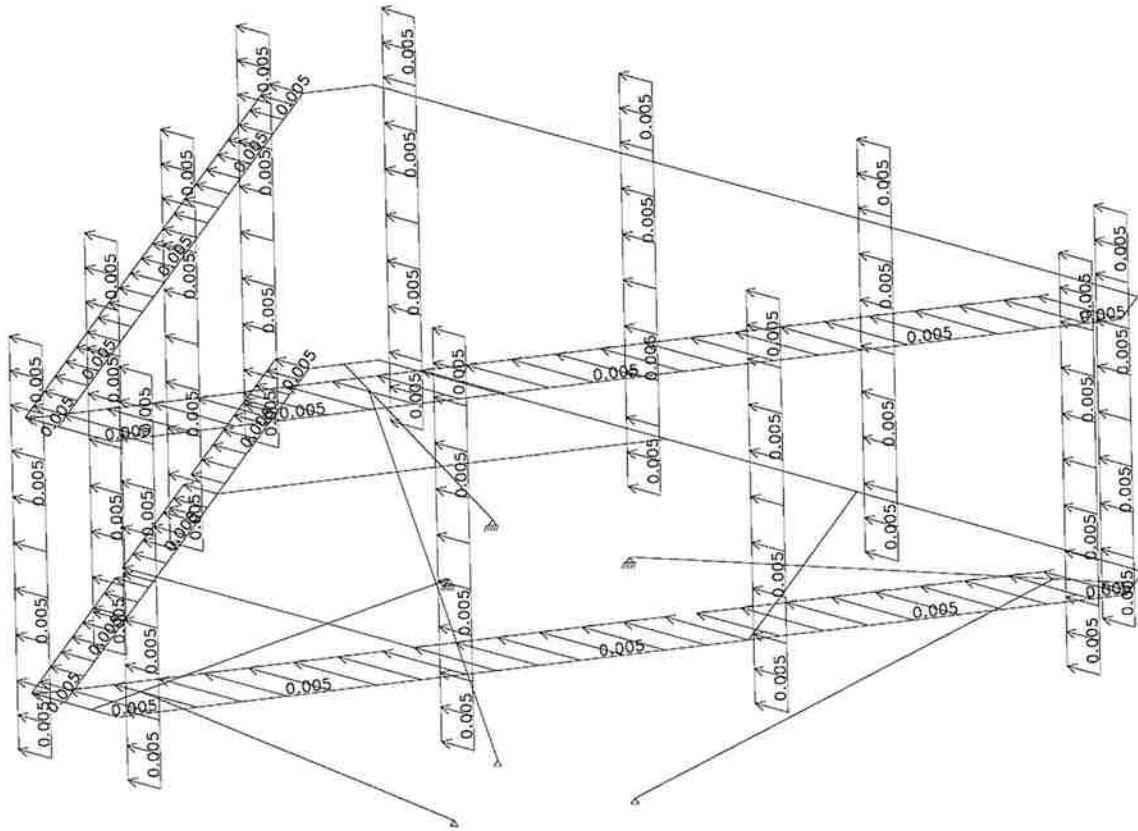
Load 9: Side Frame No Ice
View: Steel Beam Design



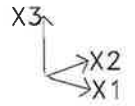
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UNITS: kip ft

DATE: 4/10/23

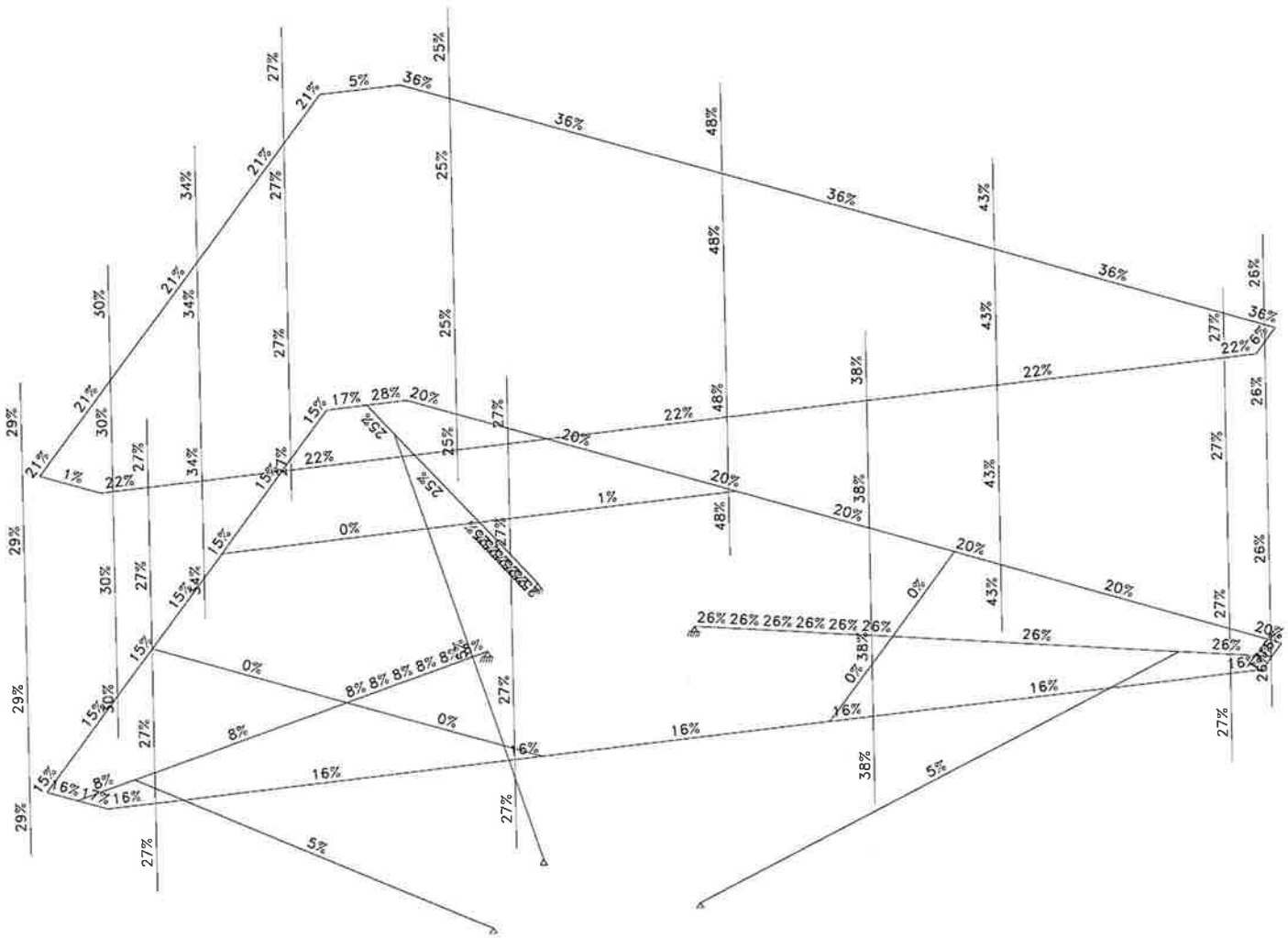


Windsor 4 CT Mount Analysis



SCALE = 1:24

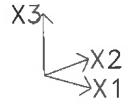
DATE: 4/10/23



Actual/allowable Moment+Axial

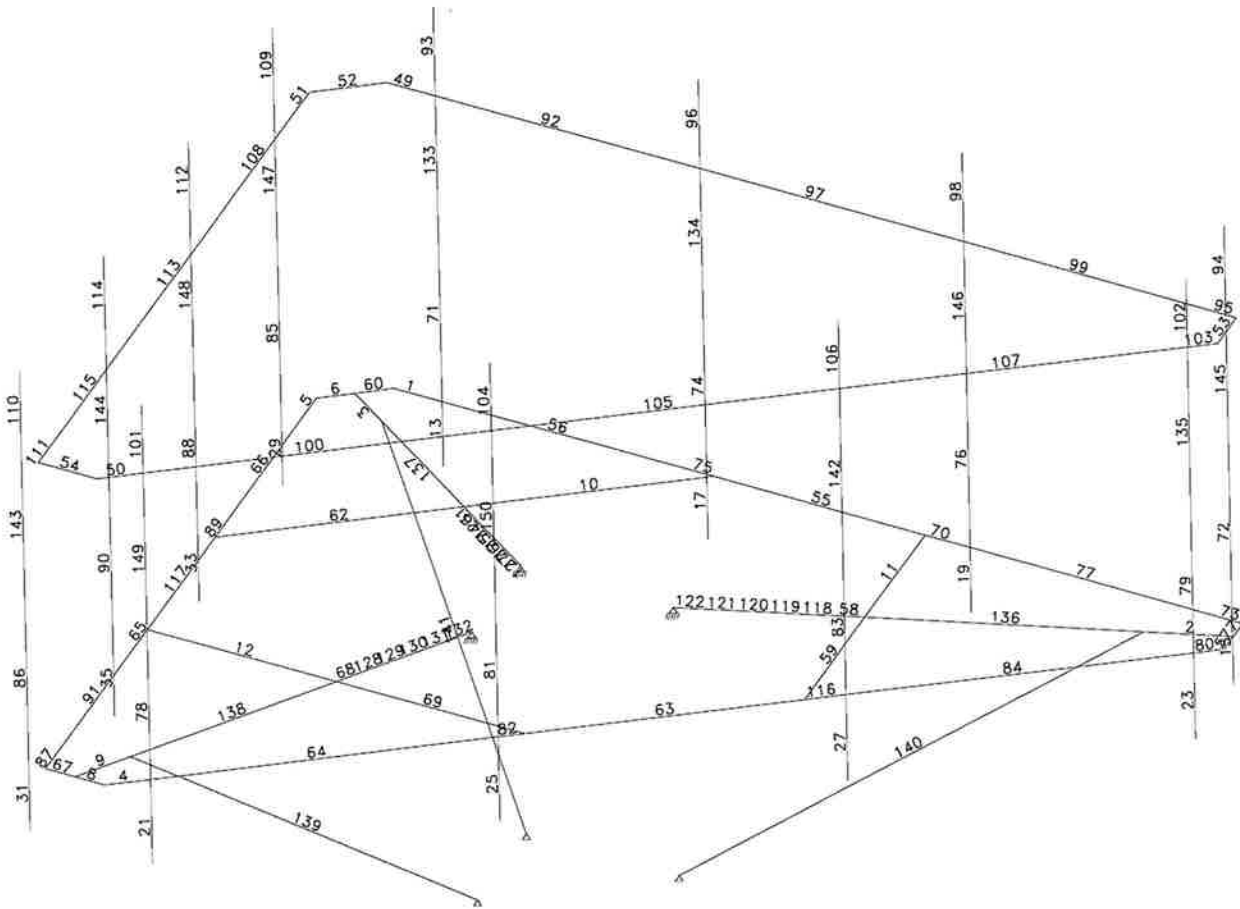
Windsor 4 CT Mount Analysis

View: Steel Beam Design



SCALE = 1:27

DATE: 4/10/23



Windsor 4 CT Mount Analysis

Code: AISC-LRFD

Prepared by:

Date: 4/10/23

Results Summary Table

Beam	Section	Com	Defl L	Slen	CAPACITY					Combined Axial+Mom	
					Axial	Dir Shear	Mom	LTB			
1	PIPE 3	1	518	150	0.01	MJ 0.02 MI 0.02	0.13 0.07	0.13 0.00	0.20		
2	TS 4x4x1/4	1	2962	57	0.02	MJ 0.03 MI 0.03	0.08 0.19	0.08 0.00	0.26		
3	TS 4x4x1/4	1	3294	57	0.02	MJ 0.03 MI 0.03	0.08 0.18	0.08 0.00	0.25		
6	PIPE 2	1	7444	8	-0.01	MJ 0.04 MI 0.01	0.13 0.04	0.13 0.00	0.17		
7	PIPE 2	3	9999	8	0.00	MJ 0.04 MI 0.01	0.13 0.03	0.13 0.00	0.16		
8	PIPE 2	1	9999	8	0.01	MJ 0.04 MI 0.04	0.12 0.13	0.12 0.00	0.17		
9	TS 4x4x1/4	4	3861	46	-0.01	MJ 0.03 MI 0.00	0.07 0.03	0.07 0.00	0.08		
10	TS 4x4x1/4	3	9999	26	0.01	MI 0.00	0.00	0.00	0.01		
11	TS 4x4x1/4	4	9999	26	0.00	MI 0.00	0.00	0.00	0.00		
12	TS 4x4x1/4	1	9999	26	0.00	MI 0.00	0.00	0.00	0.00		
49	PIPE 2	1	403	201	-0.06	MJ 0.02 MI 0.01	0.16 0.17	0.16 0.00	0.36	***	
52	PIPE 2	1	9999	15	0.00	MJ 0.02	0.05	0.05	0.05		
53	PIPE 2	1	9999	15	0.00	MJ 0.02	0.06	0.06	0.06		
54	PIPE 2	2	9999	15	0.00	MJ 0.00	0.01	0.01	0.01		
57	PIPE 2	1	6219	8	0.00	MJ 0.03 MI 0.01	0.14 0.03	0.14 0.00	0.17		
59	TS 4x4x1/4	1	9999	26	0.00	MI 0.00	0.00	0.00	0.00		
60	PIPE 2	1	4173	8	-0.01	MJ 0.04 MI 0.01	0.24 0.04	0.24 0.00	0.28		
62	TS 4x4x1/4	1	9999	26	0.00	MI 0.00	0.00	0.00	0.00		
67	PIPE 2	1	9999	8	0.01	MJ 0.03 MI 0.04	0.10 0.13	0.10 0.00	0.16		
69	TS 4x4x1/4	1	9999	26	0.00	MI 0.00	0.00	0.00	0.00		
80	PIPE 3	4	643	150	0.01	MJ 0.02 MI 0.01	0.13 0.05	0.13 0.00	0.16		
87	PIPE 3	4	645	150	0.01	MJ 0.02 MI 0.01	0.13 0.04	0.13 0.00	0.15		
93	PIPE 2	1	177	88	-0.02	MJ 0.01 MI 0.00	0.20 0.04	0.20 0.00	0.25	***	
94	PIPE 2	1	157	88	-0.02	MJ 0.01 MI 0.00	0.19 0.07	0.19 0.00	0.26	***	
96	PIPE 2	1	87	69	0.00	MJ 0.01 MI 0.03	0.13 0.36	0.13 0.00	0.48	***	
98	PIPE 2	1	92	91	0.00	MJ 0.01 MI 0.03	0.13 0.29	0.13 0.00	0.43	***	
101	PIPE 2	1	427	86	-0.01	MJ 0.01 MI 0.01	0.13 0.13	0.13 0.00	0.27		
102	PIPE 2	1	193	91	-0.01	MJ 0.01 MI 0.02	0.08 0.25	0.08 0.00	0.27	***	
103	PIPE 2	4	680	205	-0.05	MJ 0.02 MI 0.01	0.15 0.06	0.15 0.00	0.22	***	
104	PIPE 2	1	225	68	0.00	MJ 0.01 MI 0.03	0.08 0.24	0.08 0.00	0.27	***	
106	PIPE 2	1	175	69	0.00	MJ 0.01 MI 0.03	0.09 0.31	0.09 0.00	0.38	***	
109	PIPE 2	1	227	91	-0.01	MJ 0.01 MI 0.02	0.07 0.24	0.07 0.00	0.27	***	
110	PIPE 2	1	411	87	-0.01	MJ 0.01 MI 0.01	0.13 0.15	0.13 0.00	0.29		
111	PIPE 2	3	686	209	-0.06	MJ 0.02 MI 0.01	0.15 0.05	0.15 0.00	0.21	***	
112	PIPE 2	1	195	66	0.00	MJ 0.00 MI 0.03	0.05 0.29	0.05 0.00	0.34	***	
114	PIPE 2	1	214	74	0.00	MJ 0.01 MI 0.03	0.11 0.25	0.11 0.00	0.30	***	

Windsor 4 CT Mount Analysis	Code: AISC-LRFD
Prepared by:	Date: 4/10/23

Results Summary Table

Beam	Section	Com	Defl		CAPACITY					Combined Axial+Mom
			L/	Slen	Axial	Dir	Shear	Mom	LTB	
139	2L 3x3x1/4	4	9999	91	-0.05	MI	0.00	0.00	0.00	0.05
140	2L 3x3x1/4	4	9999	90	-0.05	MI	0.00	0.00	0.00	0.05
141	2L 3x3x1/4	3	9999	90	-0.05	MI	0.00	0.00	0.00	0.05

Windsor 4 CT Mount Analysis

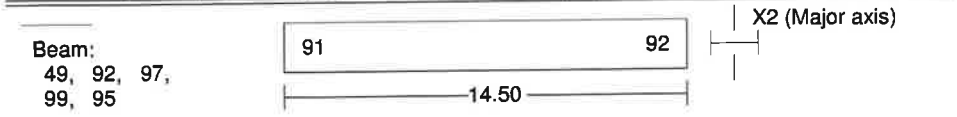
Code: AISC-LRFD

Prepared by:

Date: 4/10/23

Detailed Results Table for Beam 49 - 95

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



- | | |
|----------------------|--|
| CONSTRAINTS | DESIGN DATA |
| - Sections : Check | - Kx = 1.00 - Ky = 1.00 |
| - Steel Grade: A500C | - Allow. Slend. : 200 (compr.) 300 (tens.) |
| | - Allowable Deflection : 1/240 |
| | - Tension Area Reduction Factor : 1.00 |
| | - Building type : Unbraced |

Section: PIPE 2

ix = 0.67 ly = 0.67in4 Zx = 0.76 Zy = 0.76in3 Area = 1.07
 D = 2.37 t = 0.15in
 J = 1.33 Cw = 0.00in6

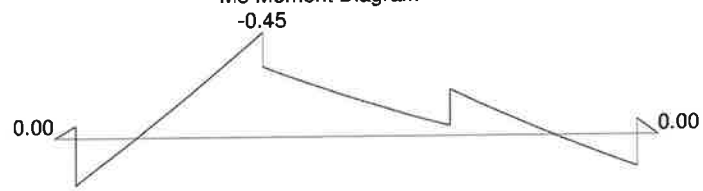
DESIGN COMBINATION = 1

M2 Moment Diagram



Max. AXIAL Force = 0.08 (tens.), -0.25 (compr.) Max. SHEAR Force = 0.34

M3 Moment Diagram



Max. AXIAL Force = 0.08 (tens.), -0.25 (compr.) Max. SHEAR Force = 0.16

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact
 d/t= 15.46 < 45.0 71.7 (Fy= 46.0 R= 0.005)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V2 Shear (F2-1)	$Vu/(.9*Vn) < 1.00$ $Vn=0.6*Fy*Av$	Av = 0.64	Vu = 0.16 Vn = 17.81	0.01
M3 Moment (A-F1-1) without LTB	$M / 0.9Mn < 1.00$	Z = 0.76	M = 0.45 Mn = 2.92	0.17
V3 Shear (F2-1)	$Vu/(.9*Vn) < 1.00$ $Vn=0.6*Fy*Av$	Av = 0.64	Vu = 0.34 Vn = 17.81	0.02

Windsor 4 CT Mount Analysis

Code: AISC-LRFD

Prepared by:

Date: 4/10/23

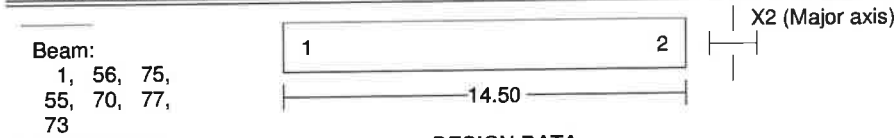
Detailed Results Table for Beam 49 - 95

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M2 Moment (A-F1-1) without LTB	$\frac{M}{0.9M_n} < 1.00$	Z = 0.76	M = 0.41 Mn = 2.92	0.16
Deflection	$\frac{\text{defl.}}{L / 240} < 1.00$		defl = 0.43143	0.60
Axial Force (E2-1)	$\frac{P_u}{0.85A_g F_{cr}} < 1.00$	(kL/r)x = 192 (kL/r)y = 192 $\lambda_c = 2.43$	Pu = 0.25 Ag = 1.07 Fcr = 6.83	0.04
Combined Forces (compress.) (H1-1b)	$\frac{P_u}{2\phi P_n} + \frac{M_{ux}}{\phi M_{nx}} + \frac{M_{uy}}{\phi M_{ny}} < 1.00$	Cmx = 1.00 Cmy = 1.00 Pex = 8.38 Pey = 8.38	Mux = 0.42 Muy = 0.47 B1x = 1.03 B1y = 1.03	0.36

Detailed Results Table for Beam 1 - 73

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



CONSTRAINTS

- Sections : Check
- Steel Grade: A500C

DESIGN DATA

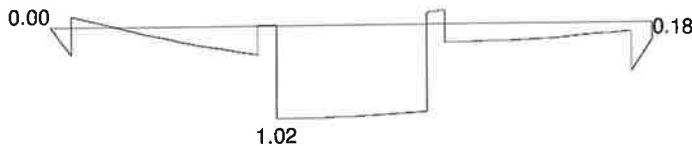
- Kx = 1.00 - Ky = 1.00
- Allow. Slend. : 200 (compr.) 300 (tens.)
- Allowable Deflection : 1/240
- Tension Area Reduction Factor : 1.00
- Building type : Unbraced

Section: PIPE 3

Ix = 3.02 Iy = 3.02in4 Zx = 2.33 Zy = 2.33in3 Area = 2.23
 D = 3.50 t = 0.22in
 J = 6.03 Cw = 0.00in6

DESIGN COMBINATION = 1

M2 Moment Diagram



Max. AXIAL Force = 0.47 (tens.), -0.30 (compr.) Max. SHEAR Force = 0.70

Windsor 4 CT Mount Analysis

Code: AISC-LRFD

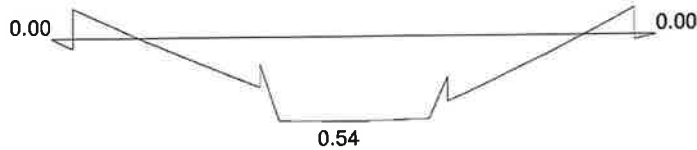
Prepared by:

Date: 4/10/23

Detailed Results Table for Beam 1 - 73

Moments: kips*foot, Forces: kips, Stresses: ksi, Section prop.: inch

M3 Moment Diagram



Max. AXIAL Force = 0.47 (tens.), -0.30 (compr.) Max. SHEAR Force = 0.82

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact
 d/t= 16.16 < 45.0 71.7 (Fy= 46.0 R = -0.005)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V2 Shear (F2-1)	$\frac{Vu}{.9*Vn} < 1.00$ $Vn = 0.6*Fy*Av$	Av = 1.34	Vu = 0.82 Vn = 36.95	0.02
M3 Moment (A-F1-1) without LTB	$\frac{M}{0.9Mn} < 1.00$	Z = 2.33	M = 0.54 Mn = 8.95	0.07
V3 Shear (F2-1)	$\frac{Vu}{.9*Vn} < 1.00$ $Vn = 0.6*Fy*Av$	Av = 1.34	Vu = 0.70 Vn = 36.95	0.02
M2 Moment (A-F1-1) without LTB	$\frac{M}{0.9Mn} < 1.00$	Z = 2.33	M = 1.02 Mn = 8.95	0.13
Deflection	$\frac{\text{defl.}}{L / 240} < 1.00$		defl = 0.33567	0.46
Axial Force (D1-1)	$\frac{Pu}{0.90AgFy} < 1.00$	(kL/r)x = 61 (kL/r)y = 61	Pu = 0.47 Ag = 2.23 Fy = 46.00	0.01
Combined Forces (compress.) (H1-1b)	$\frac{Pu}{2\phi Pn} + \frac{Mux}{\phi Mn_x} + \frac{Muy}{\phi Mn_y} < 1.00$	Cmx = 1.00 Cmy = 1.00 Pex = 172.22 Pey = 172.22	Mux = 1.02 Muy = 0.54 B1x = 1.00 B1y = 1.00	0.20

Windsor 4 CT Mount Analysis

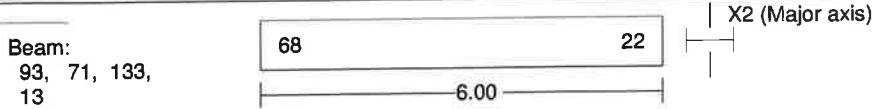
Code: AISC-LRFD

Prepared by:

Date: 4/10/23

Detailed Results Table for Beam 93 - 13

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



CONSTRAINTS

- Sections : Check
- Steel Grade: A500C

DESIGN DATA

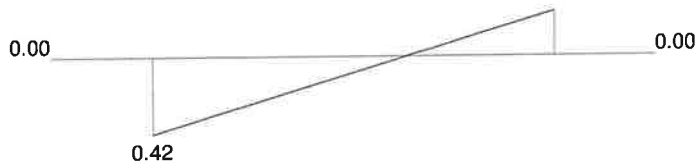
- Kx = 1.00 - Ky = 1.00
- Allow. Slend. : 200 (compr.) 300 (tens.)
- Allowable Deflection : 1/240
- Tension Area Reduction Factor : 1.00
- Building type : Unbraced

Section: PIPE 2

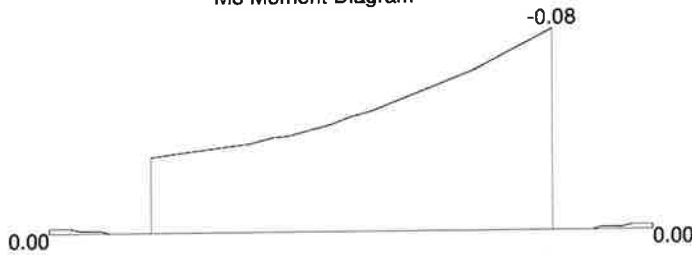
Ix = 0.67 Iy = 0.67in4 Zx = 0.76 Zy = 0.76in3 Area = 1.07
D = 2.37 t = 0.15in
J = 1.33 Cw = 0.00in6

DESIGN COMBINATION = 1

M2 Moment Diagram



Max. AXIAL Force = 0.00 (tens.), -0.47 (compr.) Max. SHEAR Force = 0.16
M3 Moment Diagram



Max. AXIAL Force = 0.00 (tens.), -0.47 (compr.) Max. SHEAR Force = 0.02

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact
d/t= 15.46 < 45.0 71.7 (Fy= 46.0 R = 0.010)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M3 Moment (A-F1-1) without LTB	$\frac{M}{0.9M_n} < 1.00$	Z = 0.76	M = 0.08 Mn = 2.92	0.03
V3 Shear (F2-1)	$\frac{V_u}{V_n} < 1.00$ Vn=0.6*Fy*Av	Av = 0.64	Vu = 0.16 Vn = 17.81	0.01
M2 Moment (A-F1-1) without LTB	$\frac{M}{0.9M_n} < 1.00$	Z = 0.76	M = 0.42 Mn = 2.92	0.16

Windsor 4 CT Mount Analysis

Code: AISC-LRFD

Prepared by:

Date: 4/10/23

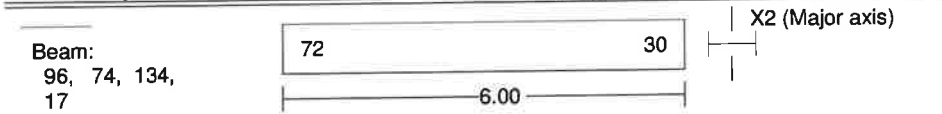
Detailed Results Table for Beam 93 - 13

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
Deflection	$\frac{\text{defl.}}{L / 240} < 1.00$		defl = 0.40660	1.36
Axial Force (E2-1)	$\frac{P_u}{0.85A_g F_{cr}} < 1.00$	(kL/r) _x = 88 (kL/r) _y = 88 $\lambda_c = 1.11$	P _u = 0.47 A _g = 1.07 F _{cr} = 27.37	0.02
Combined Forces (compress.) (H1-1b)	$\frac{P_u}{2\phi P_n} + \frac{M_{ux}}{\phi M_{nx}} + \frac{M_{uy}}{\phi M_{ny}} < 1.00$	C _{mx} = 1.00 C _{my} = 1.00 P _{ex} = 39.88 P _{ey} = 39.88	M _{ux} = 0.42 M _{uy} = 0.08 B _{1x} = 1.01 B _{1y} = 1.01	0.20

Detailed Results Table for Beam 96 - 17

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



CONSTRAINTS

- Sections : Check
- Steel Grade: A500C

DESIGN DATA

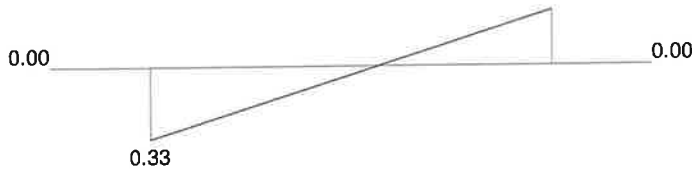
- K_x = 1.00 - K_y = 1.00
- Allow. Slend. : 200 (compr.) 300 (tens.)
- Allowable Deflection : 1/240
- Tension Area Reduction Factor : 1.00
- Building type : Unbraced

Section: PIPE 2

I_x = 0.67 I_y = 0.67in⁴ Z_x = 0.76 Z_y = 0.76in³ Area = 1.07
 D = 2.37 t = 0.15in
 J = 1.33 C_w = 0.00in⁶

DESIGN COMBINATION = 1

M2 Moment Diagram



Max. AXIAL Force = 0.09 (tens.), -0.05 (compr.) Max. SHEAR Force = 0.15

Windsor 4 CT Mount Analysis

Code: AISC-LRFD

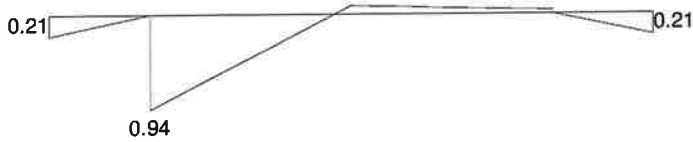
Prepared by:

Date: 4/10/23

Detailed Results Table for Beam 96 - 17

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

M3 Moment Diagram



Max. AXIAL Force = 0.09 (tens.), -0.05 (compr.) Max. SHEAR Force = 0.52

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact
 d/t= 15.46 < 45.0 71.7 (Fy= 46.0 R = -0.002)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V2 Shear (F2-1)	$V_u / (0.9 V_n) < 1.00$ $V_n = 0.6 F_y A_v$	$A_v = 0.64$	$V_u = 0.52$ $V_n = 17.81$	0.03
M3 Moment (A-F1-1) without LTB	$M / (0.9 M_n) < 1.00$	$Z = 0.76$	$M = 0.94$ $M_n = 2.92$	0.36
V3 Shear (F2-1)	$V_u / (0.9 V_n) < 1.00$ $V_n = 0.6 F_y A_v$	$A_v = 0.64$	$V_u = 0.15$ $V_n = 17.81$	0.01
M2 Moment (A-F1-1) without LTB	$M / (0.9 M_n) < 1.00$	$Z = 0.76$	$M = 0.33$ $M_n = 2.92$	0.13
Deflection	$defl. / (L / 240) < 1.00$		$defl = 0.82553$	2.75
Axial Force (D1-1)	$P_u / (0.90 A_g F_y) < 1.00$	$(kL/r)_x = 31$ $(kL/r)_y = 31$	$P_u = 0.09$ $A_g = 1.07$ $F_y = 46.00$	0.00
Combined Forces (compress.) (H1-1b)	$P_u / (2 \phi P_n) + \phi M_{nx} / \phi M_{ny} < 1.00$	$C_{mx} = 1.00$ $C_{my} = 1.00$ $P_{ex} = 321.36$ $P_{ey} = 321.36$	$M_{ux} = 0.33$ $M_{uy} = 0.94$ $B_{1x} = 1.00$ $B_{1y} = 1.00$	0.48

Windsor 4 CT Mount Analysis

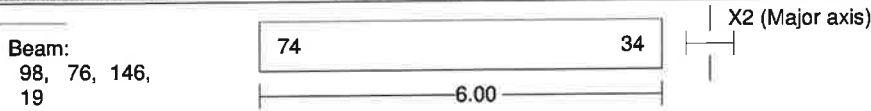
Code: AISC-LRFD

Prepared by:

Date: 4/10/23

Detailed Results Table for Beam 98 - 19

Moments: kips*foot, Forces: kips, Stresses: ksi, Section prop.: inch



CONSTRAINTS

- Sections : Check
- Steel Grade: A500C

DESIGN DATA

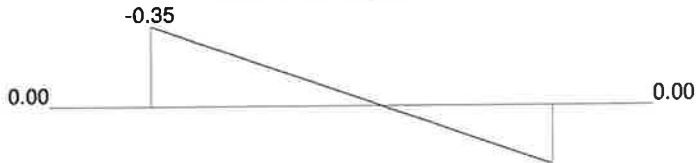
- Kx = 1.00 - Ky = 1.00
- Allow. Slend. : 200 (compr.) 300 (tens.)
- Allowable Deflection : 1/240
- Tension Area Reduction Factor : 1.00
- Building type : Unbraced

Section: PIPE 2

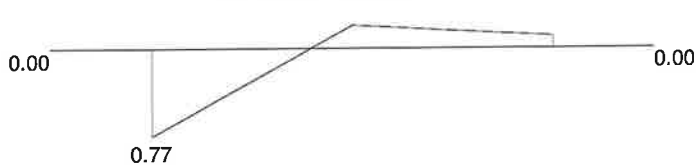
$I_x = 0.67$ $I_y = 0.67$ in⁴ $Z_x = 0.76$ $Z_y = 0.76$ in³ Area = 1.07
 D = 2.37 t = 0.15in
 J = 1.33 Cw = 0.00in⁶

DESIGN COMBINATION = 1

M2 Moment Diagram



Max. AXIAL Force = 0.15 (tens.), 0.00 (compr.) Max. SHEAR Force = 0.15
 M3 Moment Diagram



Max. AXIAL Force = 0.15 (tens.), 0.00 (compr.) Max. SHEAR Force = 0.49

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact
 $d/t = 15.46 < 45.0$ 71.7 (Fy= 46.0 R = -0.003)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V2 Shear (F2-1)	$V_u / (.9 * V_n) < 1.00$ $V_n = 0.6 * F_y * A_v$	$A_v = 0.64$	$V_u = 0.49$ $V_n = 17.81$	0.03
M3 Moment (A-F1-1) without LTB	$M / (0.9 * M_n) < 1.00$	$Z = 0.76$	$M = 0.77$ $M_n = 2.92$	0.29
V3 Shear (F2-1)	$V_u / (.9 * V_n) < 1.00$ $V_n = 0.6 * F_y * A_v$	$A_v = 0.64$	$V_u = 0.15$ $V_n = 17.81$	0.01

Windsor 4 CT Mount Analysis	Code: AISC-LRFD
Prepared by:	Date: 4/10/23

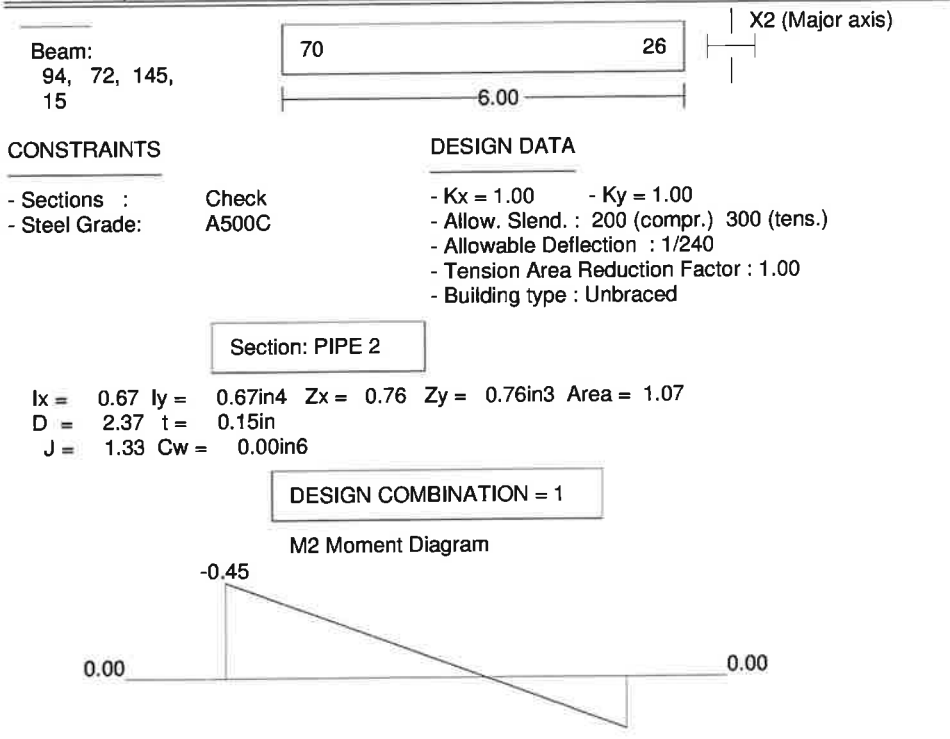
Detailed Results Table for Beam 98 - 19

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M2 Moment (A-F1-1) without LTB	$\frac{M}{0.9M_n} < 1.00$	Z = 0.76	M = 0.35 Mn = 2.92	0.13
Deflection	$\frac{\text{defl.}}{L / 240} < 1.00$		defl = 0.78578	2.62
Axial Force (D1-1)	$\frac{P_u}{0.90A_g F_y} < 1.00$	(kL/r)x =91 (kL/r)y =91	Pu = 0.15 Ag = 1.07 Fy = 46.00	0.00
Combined Forces (compress.) (H1-1b)	$\frac{P_u}{2\phi P_n} + \frac{M_{ux}}{\phi M_{nx}} + \frac{M_{uy}}{\phi M_{ny}} < 1.00$	Cmx = 1.00 Cmy = 1.00 Pex = 37.29 Pey = 37.29	Mux = 0.35 Muy = 0.77 B1x = 1.00 B1y = 1.00	0.43

Detailed Results Table for Beam 94 - 15

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



Windsor 4 CT Mount Analysis

Code: AISC-LRFD

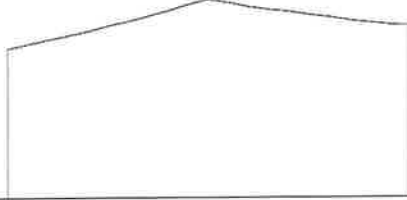
Prepared by:

Date: 4/10/23

Detailed Results Table for Beam 94 - 15

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

M3 Moment Diagram
-0.19



0.00 0.00

Max. AXIAL Force = 0.00 (tens.), -0.60 (compr.) Max. SHEAR Force = 0.03

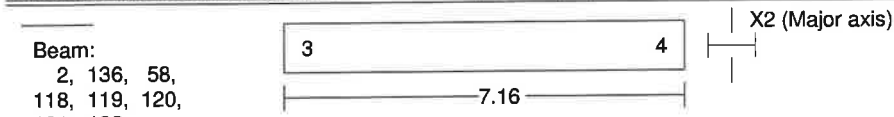
SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact
d/t= 15.46 < 45.0 71.7 (Fy= 46.0 R = 0.012)

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M3 Moment (A-F1-1) without LTB	$\frac{M}{0.9M_n} < 1.00$	Z = 0.76	M = 0.19 Mn = 2.92	0.07
V3 Shear (F2-1)	$\frac{V_u}{V_n} < 1.00$ $V_n = 0.6 \cdot F_y \cdot A_v$	Av = 0.64	Vu = 0.17 Vn = 17.81	0.01
M2 Moment (A-F1-1) without LTB	$\frac{M}{0.9M_n} < 1.00$	Z = 0.76	M = 0.45 Mn = 2.92	0.17
Deflection	$\frac{\text{defl.}}{L / 240} < 1.00$		defl = 0.45714	1.52
Axial Force (E2-1)	$\frac{P_u}{0.85A_g F_{cr}} < 1.00$	(kL/r)x = 88 (kL/r)y = 88 $\lambda_c = 1.11$	Pu = 0.60 Ag = 1.07 Fcr = 27.37	0.02
Combined Forces (compress.) (H1-1b)	$\frac{P_u}{2\phi P_n} + \frac{M_{ux}}{\phi M_{nx}} + \frac{M_{uy}}{\phi M_{ny}} < 1.00$	Cmx = 1.00 Cmy = 1.00 Pex = 39.88 Pey = 39.88	Mux = 0.45 Muy = 0.19 B1x = 1.02 B1y = 1.02	0.26

Detailed Results Table for Beam 2 - 122

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch



CONSTRAINTS

- Sections : Check
- Steel Grade: A500B

DESIGN DATA

- Kx = 1.00 - Ky = 1.00
- Allow. Slend. : 200 (compr.) 300 (tens.)
- Allowable Deflection : 1/240
- Tension Area Reduction Factor : 1.00
- Building type : Unbraced

Windsor 4 CT Mount Analysis

Code: AISC-LRFD

Prepared by:

Date: 4/10/23

Detailed Results Table for Beam 2 - 122

Moments: kips*foot, Forces: kips, Stresses: ksi, Section prop.: inch

INTERMEDIATE SUPPORTS

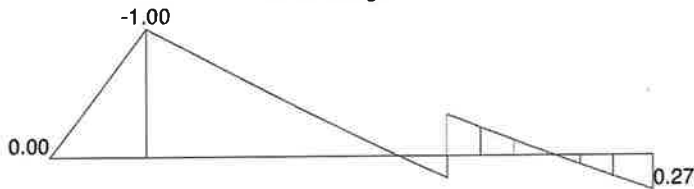
L =	1.17	4.71	5.12	5.50	5.92	6.29	6.71
Lat.-Tors.							
Compress.	X	X	X	X	X	X	X

Section: TS 4x4x1/4

$I_x = 8.22$ $I_y = 8.22$ $I_n = 4.97$ $Z_x = 4.97$ $Z_y = 4.97$ $I_p = 3.59$
 $h = 4.00$ $b = 4.00$ $t = 0.25$
 $J = 13.50$ $C_w = 0.00$

DESIGN COMBINATION = 1

M2 Moment Diagram

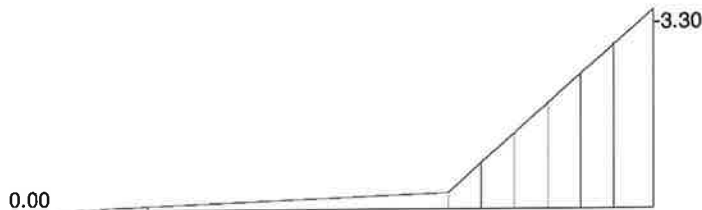


Moments at Intermediate Supports:

-0.99 0.17 -0.13 0.07
 -0.22 -0.02 0.16

Max. AXIAL Force = 2.38 (tens.) Max. SHEAR Force = 0.87

M3 Moment Diagram



Moments at Intermediate Supports:

-0.07 -0.27 -1.24 -2.22
 -0.78 -1.76 -2.74

Max. AXIAL Force = 2.38 (tens.) Max. SHEAR Force = 1.24

SECTION CLASSIFICATION: *** COMPACT ***

Limiting Ratios: Compact Non-Compact
 $d/t = 13.13 < 35.2$ 35.2 ($F_y = 46.0$ $R = -0.014$)
 $b/t = 13.13 < 28.1$ 35.2

DESIGN	EQUATION	FACTORS	VALUES	RESULT
V2 Shear (F2-1)	$V_u / (.9 * V_n) < 1.00$ $V_n = 0.6 * F_y * A_v$	$A_v = 1.79$	$V_u = 1.24$ $V_n = 49.60$	0.03
M3 Moment (A-F1-1) without LTB	$M / (0.9 * M_n) < 1.00$	$Z = 4.97$	$M = 3.30$ $M_n = 19.07$	0.19
V3 Shear (F2-1)	$V_u / (.9 * V_n) < 1.00$ $V_n = 0.6 * F_y * A_v$	$A_v = 1.79$	$V_u = 0.87$ $V_n = 49.60$	0.02

Windsor 4 CT Mount Analysis

Code: AISC-LRFD

Prepared by:

Date: 4/10/23

Detailed Results Table for Beam 2 - 122

Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch

DESIGN	EQUATION	FACTORS	VALUES	RESULT
M2 Moment (A-F1-1) without LTB	$\frac{M}{0.9M_n} < 1.00$	Z = 4.97	M = 1.00 Mn = 19.07	0.06
Deflection	$\frac{\text{defl.}}{L / 240} < 1.00$		defl = 0.02900	0.08
Axial Force (D1-1)	$\frac{P_u}{0.90A_g F_y} < 1.00$	(kL/r) _x = 28 (kL/r) _y = 57	Pu = 2.38 Ag = 3.59 Fy = 46.00	0.02
Lateral Torsional Buckling	$\frac{M}{0.9M_n} < 1.00$ Critical Segment from 0.00 to 7.16 on -z flange Segment End Moments: 0.00 and 0.27	Lb = 7.16 Lp = 14.40	M = 1.00 Mn = 19.07	0.06
Combined Forces (tension) (H1-1b)	$\frac{P_u}{2\phi P_n} + \frac{M_{ux}}{\phi M_{nx}} + \frac{M_{uy}}{\phi M_{ny}} < 1.00$		Mux = 1.00 Muy = 3.30	0.26

ATTACHMENT 6



C Squared Systems, LLC
65 Dartmouth Drive
Auburn, NH 03032
(603) 644-2800

support@csquaredsystems.com

Calculated Radio Frequency Emissions Report



Windsor 4

780 Prospect Hill Road, Windsor, CT 06095

May 23, 2023

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1. Introduction

The purpose of this report is to investigate compliance with applicable FCC regulations for the proposed installation of Verizon's antenna arrays to be mounted at 105' AGL on an existing monopole located at 780 Prospect Hill Road in Windsor, CT. The coordinates of the monopole tower are 41° 52' 58.476" N, 72° 42' 29.196" W.

Verizon is proposing the following:

- 1) Install nine (9) multi-band antennas, three (3) per sector to support its commercial LTE network.

This report considers the planned antenna configuration for Verizon¹ and the existing antennas for DISH² and T-Mobile³ to derive the resulting % MPE of its proposed installation.

2. FCC Guidelines for Evaluating RF Radiation Exposure Limits

In 1985, the FCC established rules to regulate radio frequency (RF) exposure from FCC licensed antenna facilities. In 1996, the FCC updated these rules, which were further amended in August 1997 by OET Bulletin 65 Edition 97-01. These new rules include Maximum Permissible Exposure (MPE) limits for transmitters operating between 300 kHz and 100 GHz. The FCC MPE limits are based upon those recommended by the National Council on Radiation Protection and Measurements (NCRP), developed by the Institute of Electrical and Electronics Engineers, Inc., (IEEE) and adopted by the American National Standards Institute (ANSI).

The FCC general population/uncontrolled limits set the maximum exposure to which most people may be subjected. General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

Public exposure to radio frequencies is regulated and enforced in units of milliwatts per square centimeter (mW/cm²). The general population exposure limits for the various frequency ranges are defined in the attached "FCC Limits for Maximum Permissible Exposure (MPE)" in Attachment C of this report.

Higher exposure limits are permitted under the occupational/controlled exposure category, but only for persons who are exposed as a consequence of their employment and who have been made fully aware of the potential for exposure, and they must be able to exercise control over their exposure. General population/uncontrolled limits are five times more stringent than the levels that are acceptable for occupational, or radio frequency trained individuals. Attachment C contains excerpts from OET Bulletin 65 and defines the Maximum Exposure Limit.

Finally, it should be noted that the MPE limits adopted by the FCC for both general population/uncontrolled exposure and for occupational/controlled exposure incorporate a substantial margin of safety and have been established to be well below levels generally accepted as having the potential to cause adverse health effects.

¹ As referenced to Verizon's Radio Frequency Design Sheet updated 4/4/2023.

² As referenced to Dish's Radio Frequency Emissions Analysis Report by Fox Hill Telecom, dated 1/11/2022.

³ As referenced to Connecticut Siting Council, Tower Share Application – 780 Prospect Hill Road, Windsor CT, Dated 1/31/2022

3. RF Exposure Prediction Methods

The emission field calculation results displayed in the following figures were generated using the following formula as outlined in FCC bulletin OET 65:

$$\text{Power Density} = \left(\frac{1.6^2 \times 1.64 \times \text{ERP}}{4\pi \times R^2} \right) \times \text{Off Beam Loss}$$

Where:

EIRP = Effective Isotropic Radiated Power

R = Radial Distance = $\sqrt{(H^2 + V^2)}$

H = Horizontal Distance from antenna in meters

V = Vertical Distance from radiation center of antenna in meters

Off Beam Loss is determined by the selected antenna patterns

Ground reflection factor of 1.6

These calculations assume that the antennas are operating at 100 percent capacity, that all antenna channels are transmitting simultaneously, and that the radio transmitters are operating at full power. Obstructions (trees, buildings, etc.) that would normally attenuate the signal are not taken into account. The calculations assume even terrain in the area of study and do not take into account actual terrain elevations which could attenuate the signal. As a result, the predicted signal levels reported below are much higher than the actual signal levels will be from the final installations.

4. Antenna Inventory

Table 1 below outlines Verizon’s proposed antenna configuration for the site. The associated data sheets and antenna patterns for these specific antenna models are included in Attachments C.

Operator	Sector / Call Sign	TX Freq (MHz)	Power at Antenna (Watts)	Ant Gain (dBi)	Power EIRP (Watts)	Antenna Model	Beam Width	Mech. Tilt	Length (ft)	Antenna Centerline Height (ft)
Verizon	Alpha / 30°	700	160	14.9	4944	NHH-65B-R2B	65	0	5.99	105
		850	160	15	5060		60			
		1900	160	17.9	9866		69			
		2100	240	18.4	16604		64			
		3500	20	17.7	1178	NHHSS-65B-R2BT4	54	0	5.99	105
		3700	200	25.5	70963	MT6407-77A	-	0	2.92	105
	Beta / 150°	700	160	14.9	4944	NHH-65B-R2B	65	0	5.99	105
		850	160	15	5060		60			
		1900	160	17.9	9866		69			
		2100	240	18.4	16604		64			
		3500	20	17.7	1178	NHHSS-65B-R2BT4	54	0	5.99	105
		3700	200	25.5	70963	MT6407-77A	-	0	2.92	105
	Gamma / 270°	700	160	14.9	4944	NHH-65B-R2B	65	0	5.99	105
		850	160	15	5060		60			
		1900	160	17.9	9866		69			
		2100	240	18.4	16604		64			
		3500	20	17.7	1178	NHHSS-65B-R2BT4	54	0	5.99	105
		3700	200	25.5	70963	MT6407-77A	-	0	2.92	105

Table 1: Proposed Antenna Inventory^{4 5}

⁴ Antenna heights are in reference to Verizon’s Radio Frequency Design Sheet updated 4/26/2023.

⁵ Transmit power assumes 0 dB of cable loss.

5. Calculation Results

The calculated power density results are shown in Figure 1 below. For completeness, the calculations for this analysis range from 0 feet horizontal distance (directly below the antennas) to a value of 3,000 feet horizontal distance from the site. In addition to the other worst-case scenario considerations that were previously mentioned, the power density calculations to each horizontal distance point away from the antennas was completed using a local maximum off beam antenna gain (within ± 5 degrees of the true mathematical angle) to incorporate a realistic worst-case scenario.

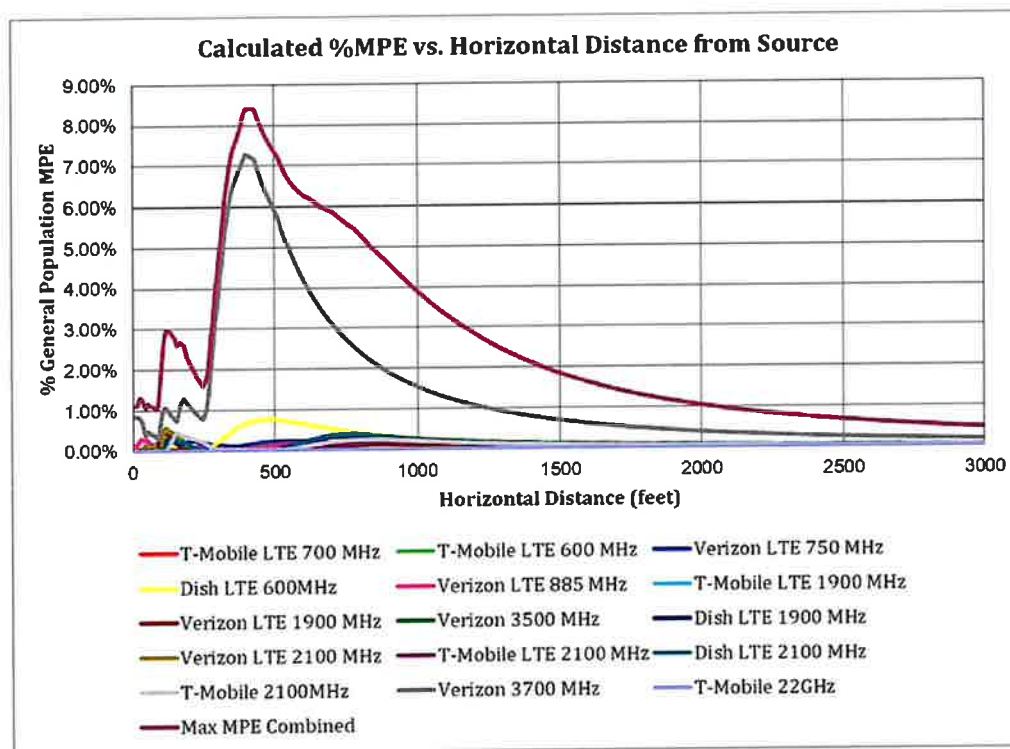


Figure 1: Graph of General Population % MPE vs. Distance

The highest percent of MPE (8.39% of the General Population limit) is calculated to occur at a horizontal distance of 410 feet from antennas. Please note that the percent of MPE calculations close to the site take into account off beam loss, which is determined from the vertical pattern of the antennas used. Therefore, RF power density levels may increase as the distance from the site increases. At distances of approximately 1500 feet and beyond, one would now be in the main beam of the antenna pattern and off beam loss is no longer considered. Beyond this point, RF levels become calculated solely on distance from the site and the percent of MPE decreases significantly as distance from the site increases.

Table 2 below lists percent of MPE values as well as the associated parameters that were included in the calculations. The highest percent of MPE value was calculated to occur at a horizontal distance of 410 feet from the site (reference Figure 1).

As stated in Section 3, all calculations assume that the antennas are operating at 100 percent capacity, that all antenna channels are transmitting simultaneously, and that the radio transmitters are operating at full power. Obstructions (trees, buildings etc.) that would normally attenuate the signal are not taken into account. In addition, a six foot height offset was considered in this analysis to account for average human height. As a result, the predicted signal levels are significantly higher than the actual signal levels will be from the final configuration. The results presented in Figure 1 and Table 2 assume level ground elevation from the base of the tower out to the horizontal distances calculated.

Carrier	Number of Transmitters	Power out of Base Station Per Transmitter (Watts)	Antenna Height (Feet)	Distance to the Base of Antennas (Feet)	Power Density (mW/cm ²)	Limit (mW/cm ²)	% MPE
Dish LTE 1900 MHz	1	160.0	115.0	410	0.000199	1.000	0.02%
Dish LTE 2100 MHz	1	160.0	115.0	410	0.000145	1.000	0.01%
Dish LTE 600MHz	1	246.0	115.0	410	0.002855	0.400	0.71%
T-Mobile 2100MHz	1	160.0	130.0	410	0.000258	1.000	0.03%
T-Mobile 22GHz	1	1.0	130.0	410	0.000002	1.000	0.00%
T-Mobile LTE 1900 MHz	1	160.0	130.0	410	0.000046	1.000	0.00%
T-Mobile LTE 2100 MHz	1	160.0	130.0	410	0.000036	1.000	0.00%
T-Mobile LTE 600 MHz	1	160.0	130.0	410	0.000120	0.400	0.03%
T-Mobile LTE 700 MHz	1	160.0	130.0	410	0.000188	0.467	0.04%
Verizon 3500 MHz	1	20.0	105.0	410	0.000276	1.000	0.03%
Verizon 3700 MHz	1	200.0	105.0	410	0.072386	1.000	7.24%
Verizon LTE 1900 MHz	1	160.0	105.0	410	0.000185	1.000	0.02%
Verizon LTE 2100 MHz	1	240.0	105.0	410	0.000271	1.000	0.03%
Verizon LTE 750 MHz	1	160.0	105.0	410	0.000779	0.500	0.16%
Verizon LTE 885 MHz	1	160.0	105.0	410	0.000398	0.567	0.07%
Total							8.39%

Table 2: Maximum Percent of General Population Exposure Values

6. Conclusion

The above analysis verifies that RF exposure levels from the site with Verizon's proposed antenna configuration will be well below the maximum permissible levels as outlined by the FCC in the OET Bulletin 65 Ed. 97-01. Using the conservative calculation methods and parameters detailed above, the maximum cumulative percent of MPE in consideration of all transmitters is calculated to be **8.39% of the FCC limit (General Population/Uncontrolled)**. This maximum cumulative percent of MPE value is calculated to occur 410 feet away from the site.

7. Statement of Certification

I certify to the best of my knowledge that the statements in this report are true and accurate. The calculations follow guidelines set forth in ANSI/IEEE Std. C95.3, ANSI/IEEE Std. C95.1 and FCC OET Bulletin 65 Edition 97-01.



Report Prepared By:

Ram Acharya
RF Engineer 1
C Squared Systems, LLC

May 22, 2023

Date



Reviewed/Approved By:

Martin J. Lavin
Senior RF Engineer
C Squared Systems, LLC

May 23, 2023

Date

Attachment A: References

OET Bulletin 65 - Edition 97-01 - August 1997 Federal Communications Commission Office of Engineering & Technology

IEEE C95.1-2005, IEEE Standard Safety Levels With Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz IEEE-SA Standards Board

IEEE C95.3-2002 (R2008), IEEE Recommended Practice for Measurements and Computations of Radio Frequency Electromagnetic Fields With Respect to Human Exposure to Such Fields, 100 kHz-300 GHz IEEE-SA Standards Board

Verizon's Radio Frequency Design Sheet updated 10/21/2022

AT&T's filing, Connecticut Siting Council Notice of Exempt Modification – Antenna Add - 780 Prospect Hill Road (aka 1 Service Road) Windsor, CT, dated 9/23/2022

As referenced to Dish Wireless LLC's filing, Connecticut Siting Council Tower Share Application – 780 Prospect Hill Road, Windsor, CT, dated 11/19/2021

T-Mobile's filing, Connecticut Siting Council Notice of Exempt Modification – 780 Prospect Hill Road, Windsor, CT, dated 10/1/2020

Attachment B: FCC Limits for Maximum Permissible Exposure (MPE)

(A) Limits for Occupational/Controlled Exposure⁶

Frequency Range (MHz)	Electric Field Strength (E) (V/m)	Magnetic Field Strength (E) (A/m)	Power Density (S) (mW/cm ²)	Averaging Time E ² , H ² or S (minutes)
0.3-3.0	614	1.63	(100)*	6
3.0-30	1842/f	4.89/f	(900/f ²)*	6
30-300	61.4	0.163	1.0	6
300-1500	-	-	f/300	6
1500-100,000	-	-	5	6

(B) Limits for General Population/Uncontrolled Exposure⁷

Frequency Range (MHz)	Electric Field Strength (E) (V/m)	Magnetic Field Strength (E) (A/m)	Power Density (S) (mW/cm ²)	Averaging Time E ² , H ² or S (minutes)
0.3-1.34	614	1.63	(100)*	30
1.34-30	824/f	2.19/f	(180/f ²)*	30
30-300	27.5	0.073	0.2	30
300-1500	-	-	f/1500	30
1500-100,000	-	-	1.0	30

f = frequency in MHz * Plane-wave equivalent power density

Table 3: FCC Limits for Maximum Permissible Exposure

⁶ Occupational/controlled limits apply in situations in which persons are exposed as a consequence of their employment provided those persons are fully aware of the potential for exposure and can exercise control over their exposure. Limits for occupational/controlled exposure also apply in situations when an individual is transient through a location where occupational/controlled limits apply provided he or she is made aware of the potential for exposure.

⁷ General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

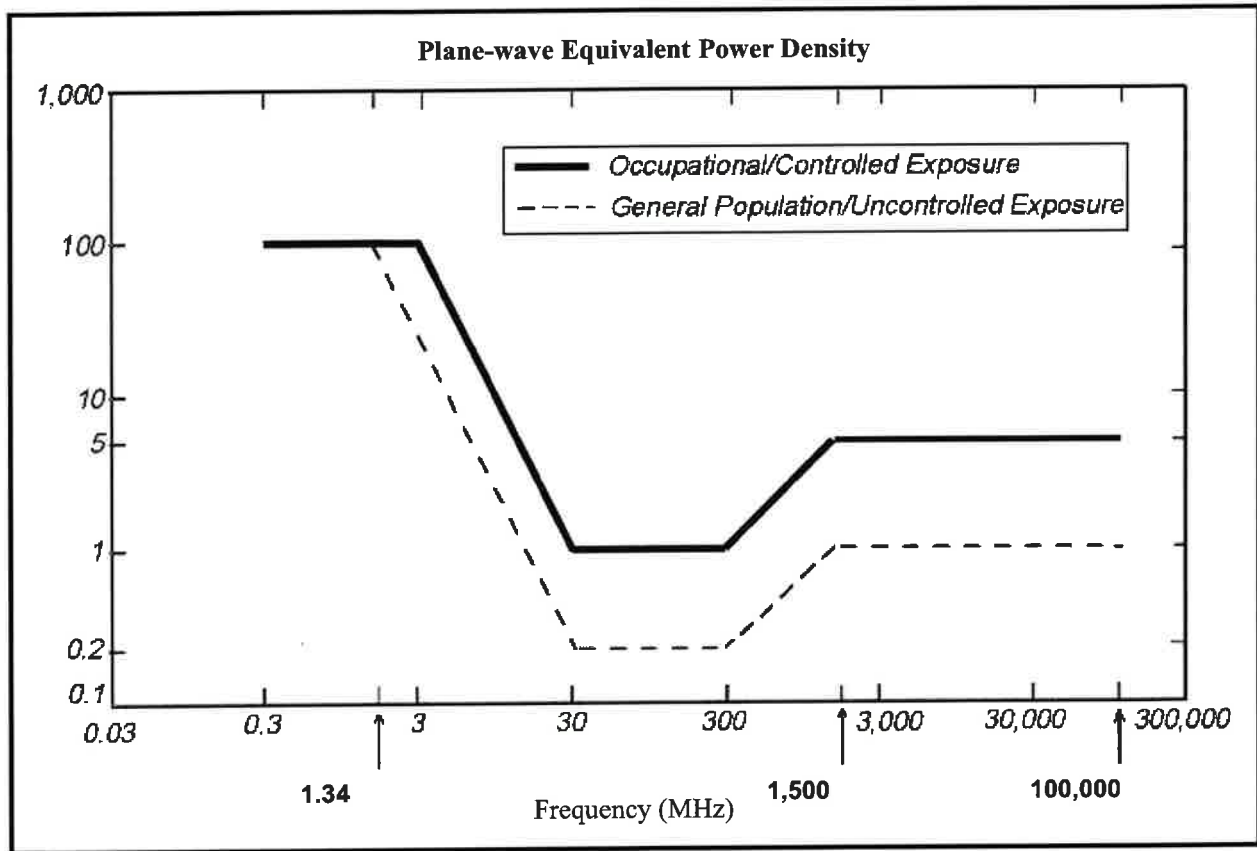
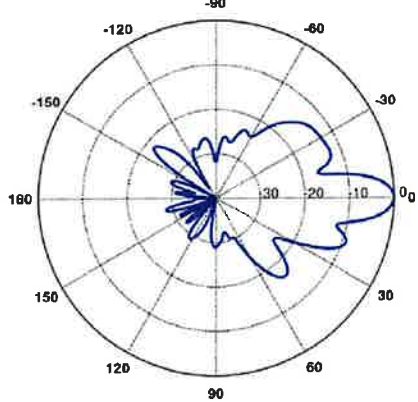
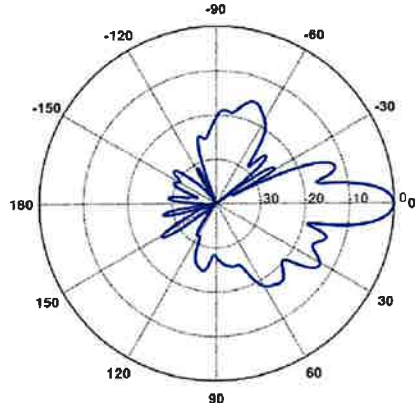
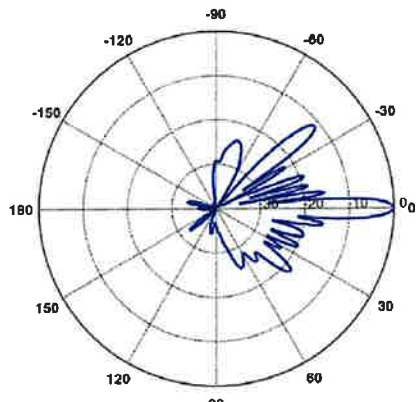


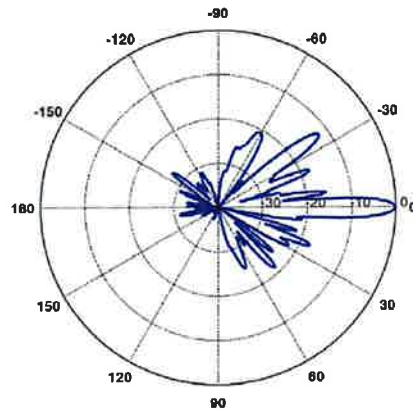
Figure 2: Graph of FCC Limits for Maximum Permissible Exposure (MPE)

Attachment C: Verizon Antenna Model Data Sheets and Electrical Patterns

<p>750 MHz</p> <p>Manufacturer: COMMSCOPE Model #: NHH-65B-R2B Frequency Band: 698-806 MHz Gain: 14.9 dBi Vertical Beamwidth: 12.4° Horizontal Beamwidth: 65° Polarization: ±45° Dimensions (L x W x D): 71.9" x 7.1" x 11.85"</p>	 <p>A polar plot showing the radiation pattern for the 750 MHz antenna. The plot is circular with concentric grid lines representing gain levels. The main lobe is centered at 0 degrees and extends to approximately 30 dB. The pattern shows a broad horizontal beamwidth and a narrow vertical beamwidth.</p>
<p>885 MHz</p> <p>Manufacturer: COMMSCOPE Model #: NHH-65B-R2B Frequency Band: 806-896 MHz Gain: 15 dBi Vertical Beamwidth: 11.2° Horizontal Beamwidth: 65° Polarization: ±45° Dimensions (L x W x D): 71.9" x 7.1" x 11.85"</p>	 <p>A polar plot showing the radiation pattern for the 885 MHz antenna. The plot is circular with concentric grid lines representing gain levels. The main lobe is centered at 0 degrees and extends to approximately 30 dB. The pattern shows a broad horizontal beamwidth and a narrow vertical beamwidth.</p>
<p>1900 MHz</p> <p>Manufacturer: COMMSCOPE Model #: NHH-65B-R2B Frequency Band: 1850-1990 MHz Gain: 17.9 dBi Vertical Beamwidth: 5.2° Horizontal Beamwidth: 69° Polarization: ±45° Dimensions (L x W x D): 71.9" x 7.1" x 11.85"</p>	 <p>A polar plot showing the radiation pattern for the 1900 MHz antenna. The plot is circular with concentric grid lines representing gain levels. The main lobe is centered at 0 degrees and extends to approximately 30 dB. The pattern shows a very narrow vertical beamwidth and a wide horizontal beamwidth.</p>

2100 MHz



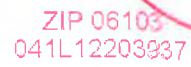


Manufacturer: COMMSCOPE
Model #: NHH-65B-R2B
Frequency Band: 1920-2200 MHz
Gain: 18.4 dBi
Vertical Beamwidth: 4.9°
Horizontal Beamwidth: 64°
Polarization: ±45°
Dimensions (L x W x D): 71.9" x 7.1" x 11.85"



ATTACHMENT 7



Certificate of Mailing — Firm

Name and Address of Sender Kenneth C. Baldwin, Esq. Robinson & Cole LLP 280 Trumbull Street Hartford, CT 06103	TOTAL NO. of Pieces Listed by Sender 4	TOTAL NO. of Pieces Received at Post Office™ 4	Affix Stamp Here <i>Postmark with Date of Receipt.</i> <div style="text-align: right;">    </div> <div style="text-align: right; margin-top: 20px;">  </div>
Postmaster, per (name of receiving employee) 			

USPS® Tracking Number Firm-specific Identifier	Address (Name, Street, City, State, and ZIP Code™)	Postage	Fee	Special Handling	Parcel Airlift
1.	Donald Trinks, Mayor Town of Windsor 275 Broad Street Windsor, CT 06095				
2.	Eric Barz, Town Planner Town of Windsor 275 Broad Street Windsor, CT 06095				
3.	The Ferraina Company LLC 810 Prospect Hill Road Windsor, CT 06095				
4.	Tarpon Towers Attn: Brett Buggeln 8916 77 th Terrace East, Suite 103 Lakewood Ranch, FL 34202				
5.					
6.					