Robinson+Cole

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts

February 6, 2015

Melanie A. Bachman Acting Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Notice of Exempt Modification - Facility Modification 599 Matianuck Avenue, Windsor, Connecticut

Dear Ms. Bachman:

Re:

Cellco Partnership d/b/a Verizon Wireless ("Cellco") currently maintains twelve (12) antennas at the top of the existing 100-foot tower at 599 Matianuck Avenue in Windsor (the "Property"). The tower is owned by Crown Castle. Cellco's shared use of this tower was approved by the Council in 1990. Cellco now intends to modify its facility by replacing six (6) of its existing antennas with three (3) model HBXX-6517DS-VTM, 1900 MHz and three (3) model HBXX-6517DS-VTM, 2100 MHz antennas, all at the same level on the tower. Cellco also intends to install six (6) remote radio heads ("RRHs") behind its 1900 MHz and 2100 MHz antennas and one (1) HYBRIFLEXTM antenna cable attached to the outside the monopole tower. Included in Attachment 1 are specifications for Cellco's replacement antennas, RRHs and HYBRIFLEXTM cable.

Please accept this letter as notification pursuant to R.C.S.A. § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent Peter Souza, Town Manager for the Town of Windsor. Please note that the Town of Windsor is the owner of the Property.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

13418729-v1

Robinson+Cole

Melanie A. Bachman February 6, 2015 Page 2

- 1. The proposed modifications will not result in an increase in the height of the existing tower. Cellco's replacement antennas and RRHs will be installed on its existing antenna platform at the top of the 100-foot tower.
- 2. The proposed modifications will not involve any change to ground-mounted equipment and, therefore, will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. A cumulative General Power Density table for Cellco's modified facility is included in <u>Attachment 2</u>.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The tower and its foundation, with certain modifications, can support Cellco's proposed modifications. (*See* Structural Modification Report and Tower Modification Drawings included in Attachment 3).

For the foregoing reasons, Cellco respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Kenneth C. Baldwin

Enclosures Copy to:

Peter Souza, Windsor Town Manager Sandy M. Carter

ATTACHMENT 1

Product Specifications



HBXX-6517DS-VTM

Andrew® Quad Port Teletilt® Antenna, 1710-2180 MHz, 65° horizontal beamwidth, RET compatible



Electrical Specifications

Frequency Band, MHz	1710-1880	1850-1990	1920-2180
Gain by all Beam Tilts, average, dBi	18.5	18.6	18.8
Gain by all Beam Tilts Tolerance, dB	±0.4	±0.3	±0.4
	0 ° 18.4	0 ° 18.4	0 ° 18.7
Gain by Beam Tilt, average, dBi	3 ° 18.7	3 ° 18.7	3° 18.9
	6° 18.4	6 ° 18.5	6 ° 18.6
Beamwidth, Horizontal, degrees	67	66	65
Beamwidth, Horizontal Tolerance, degrees	±2.4	±1.7	±2.9
Beamwidth, Vertical, degrees	5.0	4.7	4.4
Beamwidth, Vertical Tolerance, degrees	±0,3	±0,3	±0.3
Beam Tilt, degrees	0-6	0-6	0-6
USLS, dB	18	19	19
Front-to-Back Total Power at 180° ± 30°, dB	25	26	26
CPR at Boresight, dB	22	23	22
CPR at Sector, dB	10	10	9
Isolation, dB	30	30	30
VSWR Return Loss, dB	1.4 15.6	1.4 15.6	1,4 15.6
PIM, 3rd Order, 2 x 20 W, dBc	-153	-153	-153
Input Power per Port, maximum, watts	350	350	350
Polarization	±45°	±45°	±45°

^{*}Values calculated using NGMN Alliance N-P-BASTA v9.6

Mechanical Specifications

Color | Radome Material Light gray | PVC, UV resistant
Connector Interface | Location | Quantity 7-16 DIN Female | Bottom | 4

Wind Loading, maximum 668.0 N @ 150 km/h 150.2 lbf @ 150 km/h

 Wind Speed, maximum
 241.0 km/h | 149.8 mph

 Antenna Dimensions, L x W x D
 1903.0 mm x 305.0 mm x 166.0 mm | 74.9 in x 12.0 in x 6.5 in

Net Weight 19.5 kg | 43.0 lb Model with factory installed AISG 2.0 RET HBXX-6517DS-A2M



LA6.0.1/13.3

PCS RF MODULES RRH1900 2X60 - HW CHARACTERISTICS

	RRH2x60
RF Output Power	2x60W
Instantaneous Bandwidth	20MHz
Transmitter	2 TX
Receiver 1900 HW version 1900A HW version	2 Branch RX – LA6.0.1 4 Branch RX – LR13.3
Features	AISG 2.0 for RET/TMA
	Internal Smart Bias-T
Power	-48VDC
CPRI Ports	2 CPRI Rate 3 Ports
External Alarms	4 External User Alarms
Monitor Ports	XT
Environmental	GR487 Compliance
RF Connectors	7/16 DIN (top mounted)



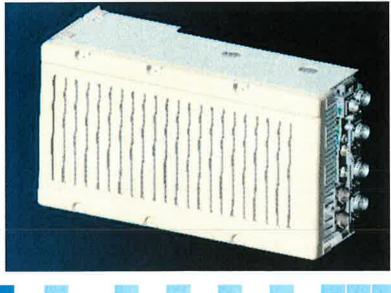




LR14.3

NEW PCS RF MODULES FOR VZW RRH2X60 - HW CHARACTERISTICS

	RRH2x60
RF Output Power	2x60W (4x30W HW Ready)
Instantaneous Bandwidth	60MHz
Target Reliability (Annual Return Rate)	<2%
Receiver	4 Branch Rx
Features	AISG 2.0 for RET/TMA
Power	-48VDC
	Internal Smart Bias-T
CPRI Ports	2 CPRI Rate 5 Ports
External Alarms	4 External User Alarms
Monitor Ports	TX, RX
Environmental	GR487 Compliance
RF Connectors	7/16 DIN (downward facing)
Dimensions	$22''(h) \times 12''(w) \times 9.4''(d)**$
Weight	55lb**



Mcdaca Social Sincks Back not included by the second secon **- Includes solar shield but not mounting brackets (8 lbs.)



ALCATEL-LUCENT WIRELESS PRODUCT DATASHEET

RRH2X60-AWS FOR BAND 4 APPLICATIONS

The Alcatel-Lucent RRH2x60-AWS is a high power, small form factor Remote Radio Head operating in the AWS frequency band (3GPP Band 4) for LTE technology. It is designed with an eco-efficient approach, providing operators with the means to achieve high quality and high capacity coverage with minimum site requirements and efficient operation.



A distributed Node B expands the deployment options by using two components, a Base Band Unit (BBU) containing the digital assets and a separate RRH containing the radiofrequency (RF) elements. This modular design optimizes available space and allows the main components of a Node B to be installed separately, within the same site or several kilometers apart.

The Alcatel-Lucent RRH2x60-AWS is linked to the BBU by an optical-fiber connection carrying downlink and uplink digital radio signals

along with operations, administration and maintenance (OA&M) information.

SUPERIOR RF PERFORMANCE

The Alcatel-Lucent RRH2x60-AWS integrates all the latest technologies. This allows to offer best-in-class characteristics.

It delivers an outstanding 120 watts of total RF power thanks to its two transmit RF paths of 60 W each.

It is ideally suited to support multipleinput multiple-output (MIMO) 2x2 operation.

It includes four RF receivers to natively support 4-way uplink reception diversity. This improves the radio uplink coverage and this can be used to extend the cell radius commensurate with 2x2MIMO 2x60 W for the downlink.

It supports multiple discontinuous LTE carriers within an instantaneous bandwidth of 45 MHz corresponding to the entire AWS B4 spectrum.

The latest generation power amplifiers (PA) used in this product achieve high efficiency (>40%), resulting in improved power consumption figures.

OPTIMIZED TCO

The Alcatel-Lucent RRH2x60-AWS is designed to make available all the benefits of a distributed Node B, with excellent RF characteristics, with low capital expenditures (CAPEX) and low operating expenditures (OPEX).

The Alcatel-Lucent RRH2x60-AWS is a very cost-effective solution to deploy LTE MIMO.

EASY INSTALLATION

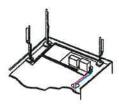
The RRH2x60-AWS includes a reversible mounting bracket which allows for ease of installation behind an antenna, or on a rooftop knee wall while providing easy access to the mid body RF connectors.

The limited space available in some sites may prevent the installation of traditional single-cabinet BTS equipment. However, many of these sites can host an Alcatel-Lucent RRH2x60-AWS installation, providing more flexible site selection and improved network quality along with greatly reduced installation time and costs.

The Alcatel-Lucent RRH2x60-AWS is a zero-footprint solution and is convection cooled without fans for silent operation, simplifying negotiations with site property owners and minimizing environmental impacts.

Installation can easily be done by a single person as the Alcatel–Lucent RRH2x60-AWS is compact and weighs about 20 kg, eliminating the need for a crane to hoist the BTS cabinet to the rooftop. A site can be in operation in less than one day.

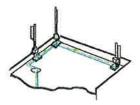
······Alcatel·Lucent 🎻



Macro



RRH for space-constrained cell sites



Distributed

FEATURES

- RRH2x60-AWS integrates two power amplifiers of 60W rating (at each antenna connector)
- Support multiple carriers over the entire 3GPP band 4
- RRH2x60-AWS is optimized for LTE operation
- RRH2x60-AWS is a very compact and lightweight product
- Advanced power management techniques are embedded to provide power savings, such as PA bias control

BENEFITS

- MIMO LTE operation with only one single unit per sector
- Improved uplink coverage with builtin 4-way receive diversity capability
- RRH can be mounted close to the antenna, eliminating nearly all losses in RF cables and thus reducing power consumption by 50% compared to conventional solutions
- Distributed configurations provide easily deployable and cost-effective solutions, near zero footprint and

silent solutions, with minimum impact on the neighborhood, which ease the deployment

 RETA and TMA support without additional hardware thanks to the AISG v2.0 port and the integrated Bias-Tees. Bias-Tees support AISG DC supply and signaling.

TECHNICAL SPECIFICATIONS

Specifications listed are hardware capabilities. Some capabilities depend on support in a specific software release or future release.

Dimensions and weights

 HxWxD: 510x285x186mm (27 I with solar shield)
 Weight: 20 kg (44 lbs)

Electrical Data

- Power Supply: -48V DC (-40.5 to -57V)
- Power Consumption (ETSI average traffic load reference): 250W @2x60W

RF Characteristics

- Frequency band: 1710-1755, UL / 2110-2155 MHz, DL (3GPP band 4)
- Output power: 2x60W at antenna connectors
- · Technology supported: LTE
- Instantaneous bandwidth: 45 MHz
- Rx diversity: 2-way and 4-way uplink reception
- Typical sensitivity without Rx diversity:
 -105 dBm for LTE

Connectivity

- Two CPRI optical ports for daisychaining and up to six RRHs per fiber
- Type of optical fiber: Single-Mode (SM) and Multi-Mode (MM) SFPs
- Optical fiber length: up to 500m using MM fiber, up to 20km using SM fiber
- TMA/RETA: AISG 2.0 (RS485 connector and internal Bias-Tee)
- Six external alarms
- Surge protection for all external ports (DC and RF)

Environmental specifications

- Operating temperature: -40°C to 55°C including solar load
- Operating relative humidity: 8% to 100%
- Environmental Conditions: ETS 300 019-1-4 class 4.1E
- Ingress Protection : IEC 60529 IP65
- Acoustic Noise: Noiseless (natural convection cooling)

Safety and Regulatory Data

- EMC: 3GPP 25113, EN 301 489-1, EN 301 489-23, GR 1089, GR 3108, OET-65
- Safety: IEC60950-1, EN 60825-1, UL, ANSI/NFPA 70, CAN/CSA-C22.2
- Regulatory: FCC Part 15 Class B, CE Mark – European Directive: 2002/95/EC (ROHS); 2002/96/EC (WEEE); 1999/5/EC (R&TTE)
- Health : EN 50385

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HYBRIFLEXTM RRH Hybrid Feeder Cabling Solution, 1-5/8", Single-Mode Fiber

Product Description

RFS' HYBRIFLEX Remote Radio Head (RRH) hybrid feeder cabling solution combines optical fiber and DC power for RRHs in a single lightweight aluminum corrugated cable, making it the world's most innovative solution for RRH deployments.

It was developed to reduce installation complexity and costs at Cellular sites. HYBRIFLEX allows mobile operators deploying an RRH architecture to standardize the RRH installation process and eliminate the need for and cost of cable grounding. HYBRIFLEX combines optical fiber (multi-mode or single-mode) and power in a single corrugated cable. It eliminates the need for junction boxes and can connect multiple RRHs with a single feeder, Standard RFS CELLFLEX® accessories can be used with HYBRIFLEX cable. Both pre-connectorized and on-site options are available.

Feature/Reneins

- a Aluminum corrugated armor with outstanding bending characteristics minimizes installation time and enables mechanical protection and shielding
- Same accessories as 1.5/8" coaxial cable
- Outer conductor grounding Eliminates typical grounding requirements and saves on installation costs
- Lightweight solution and compact design Decreases tower loading
- Robust cabling Eliminates need for expensive cable trays and ducts
- Installation of tight bundled fiber optic cable pairs directly to the RRH Reduces CAPEX and wind load by eliminating need for interconnection
- o Optical fiber and power cables housed in single corrugated cable Saves CAPEX by standardizing RRH cable installation and reducing installation requirements
- Outdoor polyethylene jacket Ensures long-lasting cable protection

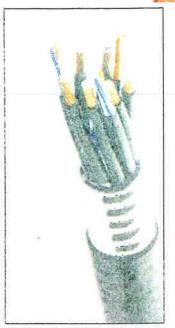


Figure 1: MYBRIFLEX Series

Todastical Specifications

Outer Conductor Armor	Correspond Alamana	(mm (in/)	46.5 (1.83)
Jacket	Corrugated Aluminum		50.3 (1.98)
	Polyethylene, PE	[mm (in)]	
UV-Protection	Individual and External Jacket		Yes
Many of the same of			
Weight, Approximate		[kg/m (lb/fu]	1 9 (1.30)
Minimum Bending Radius	. Single Bending	[mm (in)]	200 (8)
Minimum Bending Radius	Repeated Bending	[mm.lin)]	500 (20)
Recommended/Maximum	Clamp Spacing	(m (ft))	10/12(3.25/4.0)
4 00 7 B Ogodan			
DC-Resistance Outer Cond	luctor Armor	$[\Omega/\text{km}](\Omega/1000\text{fb})$	068 (0.205)
		IO/km (Q/1000ful	2 1 (0 307)
DC-Resistance Power Cab		[Wkm (W1000ft)]	2 1 (0.307)
DC-Resistance Power Cab		[Wkm (W1000ft)]	
DC-Resistance Power Cabi Version		[Ω/km (Ω/1000ft)]	Single-mode OM3
DC-Resistance Power Cab Version Quantity, Fiber Count			Single-mode OM3 16 (8 pairs)
DC-Resistance Power Cab Version Quantity, Fiber Count Core/Clad	le 8 4mm ¹ (8AWG)	(μm)	Single-mode OM3 16 (8 pairs) 50/125
DC-Resistance Power Cab Version Quantity, Fiber Count Core/Clad Primary Coating (Acrylate)	le 8 4mm ¹ (8AWG)	(μπ) (μπ)	Single-mode OM3 16 (8 pairs) 50/125 245
DC-Resistance Power Cab Version Quantity, Fiber Count Core/Clad Primary Coating (Acrylate) Buffer Diameter, Nominal	le 8 4mm²·8AWG)	(µm) (µm)	Single-mode OM3 16 (8 pairs) 50/125 245 900
DC-Resistance Power Cab Version Quantty, Fiber Count Core/Clad Primary Coating (Acrylate, Buffer Diameter, Nominal Secondary Protection, Jack	le 8 4mm² (8AWG)	[µm] [µm] [µm]	Single-mode OM3 16 (8 pairs) 50/125 245 900 2 0 (0 08)
DC-Resistance Power Cabi Version Quantity, Fiber Count Core/Clad Primary Coating (Acrylate, Buffer Diameter, Nominal Secondary Protection, Jack Minimum Bending Radius	le 8 4mm ¹ /8AWG)	(µm) (µm) (µm) (mm (n))	Single-mode OM3 16 (8 pairs) 50/125 245 900 2 0 (9 08) 104 (4.1)
DC-Resistance Power Cab Version Quantity, Fiber Count Core/Clad Primary Coating (Acrylate, Buffer Diameter, Nominal Secondary Protection, Jack Winimum Bending Radius Insertion Loss @ waveleng	th 850nm	(µm) (µm) (µm) (mm (in) (mm (in)) dB/km	Single-mode OM3 16 (8 pairs) 50/125 245 900 2 0 (0 08)
DC-Resistance Power Cabi Version Quantity, Fiber Count Core/Clad Primary Coating (Acrylate, Buffer Diameter, Nominal Secondary Protection, Jack Minimum Bending Radius	th 850nm th 1310nm	(µm) (µm) (µm) (mm (n))	Single-mode OM3 16 (8 pairs) 50/125 245 900 2 0 (9 08) 104 (4 1) 3 0

Size (Power)	[mm (AWG)]	8 4 (8)
Quantity, Wire Count (Power)		16 (3 pairs)
Size (Alarm)	[mm (AWG)]	08(18)
Quantity, Wire Count (Alarm)	1	4 (2 pairs)
Type		UV protected
Strands		19
Primary Jacket Diameter, Nominal	[mm (in,)	6.8 (0.27)
Standards (Meets or exceeds)	======================================	NFPA 130, ICEA 5-95-658
		UL Type XHHVV-2, UL 44
		UL-LS Limited Smoke, UL VW-T
		IEEE-383 (1974), IEEE1202/FT4
		Ro∺S Compliant

Installation Temperature -40 to +65 (-40 to 149) -40 to +65 (-40 to 149) Operation Temperature

* This data is provisional and subject to change

RFS The Clear Choice®

H3153-1-03U3-53113

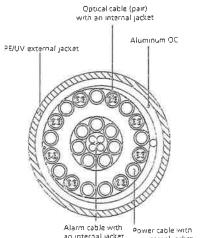


Figure 3: Construction Detail

All information contained in the present darasheel is subject to confirmation at time of ordering

Print Date: 27.5.2012

ATTACHMENT 2

	General	Power	Density					
Site Name: Windsor S								
Tower Height: 100ft								
				CALC. POWER		MAX. PERMISS.	FRACTION	
CARRIER	# OF CHAN.	WATTS ERP	HEIGHT	DENS	FREQ.	EXP.	MPE	Total
*Clearwire	2	153	85	0.0152	2496	1.0000	1.52%	
*Clearwire	1	211	86.5	0.0101	23 GHz	1.0000	1.01%	
*AT&T UMTS	2	200	75	0.0639	880	0.5867	10.90%	
*AT&T UMTS	1	200	75	0.0320	1900	1.0000	3.20%	
*AT&T LTE	71	200	75	0.0320	700	0.4667	6.85%	
*AT&T LTE	7	200	75	0.0320	1900	1.0000	3.20%	
*AT&T LTE	1	200	75	0.0320	2300	1.0000	3.20%	
Verizon PCS	11	463	101	0.1795	1970	1.0000	17.95%	
Verizon Cellular	6	417	101	0.1323	869	0.5793	22.83%	
Verizon AWS	-	1750	101	0.0617	2145	1.0000	6.17%	
Verizon 700	-	1050	101	0.0370	746	0.4973	7.44%	
								84.27%
* Source: Siting Council								

ATTACHMENT 3



Date: November 21, 2014

Timothy Howell Crown Castle 3530 Toringdon Way, Suite 300 Charlotte, NC 28277

Paul J Ford and Company 250 E. Broad Street, Suite 600 Columbus, OH 43215 614-221-6679

Subject:

Structural Modification Report

Carrier Designation:

Verizon Wireless Co-Locate

Carrier Site Number:

Carrier Site Name:

119716

Windsor South

Crown Castle Designation:

Crown Castle BU Number:

Crown Castle Site Name:

806371 HRT 096 943227

Crown Castle JDE Job Number:

311340 965888

Crown Castle Work Order Number: Crown Castle Application Number:

269459 Rev. 0

Engineering Firm Designation:

Paul J Ford and Company Project Number: 37514-2522.001.7700

Site Data:

HRT 96599 MATIANUCK AVE, WINDSOR, Hartford County, CT

Latitude 41° 49' 16.04", Longitude -72° 40' 36.29"

100 Foot - Monopole Tower

Dear Timothy Howell.

Paul J Ford and Company is pleased to submit this "Structural Modification Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 729299, in accordance with application 269459, revision 0.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC4.7: Modified Structure w/ Existing + Reserved + Proposed Equipment Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

Sufficient Capacity

This analysis has been performed in accordance with the TIA/EIA-222-F standard and 2005 CT State Building Code with 2009 amendment based upon a wind speed of 80 mph fastest mile.

All modifications and equipment proposed in this report shall be installed in accordance with the attached drawings for the determined available structural capacity to be effective.

We at Paul J Ford and Company appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:

Corey McCartney, El Structural Designer

tnxTower Report - version 6.1.4.1

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- Table 2 Existing and Reserved Antenna and Cable Information
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- Table 4 Documents Provided
- 3.1) Analysis Method
- 3.2) Assumptions

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Table 6 - Tower Components vs. Capacity

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5) APPENDIX A

tnxTower Output

6) APPENDIX B

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7) APPENDIX C

Additional Calculations

1) INTRODUCTION

This tower is a 100-ft Monopole tower designed by VALMONT in January of 1991. The tower was originally designed for a wind speed of 90 mph per EIA-222-D.

2) ANALYSIS CRITERIA

This analysis has been performed in accordance with the TIA/EIA-222-F standard and 2005 CT State Building Code with 2009 amendment based upon a wind speed of 80 mph fastest mile.

Table 1 - Proposed Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
		3	alcatel lucent	RRH 2x60W-1900MHz			
		3	alcatel lucent	RRH2x60-AWS			
98.0	101.0	6	commscope	HBXX-6517DS-A2M w/ Mount Pipe	1	1-5/8	-
		1	rfs celwave	DB-T1-6Z-8AB-0Z			

Table 2 - Existing and Reserved Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
	104.0	1	gps	GPS_A			
		2	antel	BXA-70063/6CFx2 w/ Mount Pipe	1 18	1/2 1-5/8	1
00.0	404.0	1	antel	BXA-70063/6CFx4 w/ Mount Pipe	10	1-5/0	
98.0	101.0	6	decibel	950G65VTZE-M w/ Mount Pipe	-	-	3
		6	decibel	DB844G65ZAXY w/ Mount Pipe	_	_	1
	98.0	1	tower mounts	Platform Mount [LP 102-1]			
		3	andrew	VHLP2-23			
05.0	05.0	3 -	argus technologies	LLPX310R W/ Mount Pipe	3 6	1/2 5/16	2
85.0	85.0	3	samsung	FDD_R6_RRH		3/10	
		1	tower mounts	Platform Mount [LP 601-1]	2	=	1
		12	cci antennas	HPA-65R-BUU-H8 w/ Mount Pipe			
		3	ericsson	KRF 102 361/1			
		9	ericsson	RRU-11			
		6	ericsson	RRUS 12-B2	2	3/8	
75.0	75.0	6	ericsson	RRUS A2	3	5/16	2
		3	ericsson	RRUS E2 B29	8	3/4	
		3	ericsson	RRUS-32 B30			
		4	raycap	DC6-48-60-18-8F			
		1	tower mounts	Platform Mount [LP 1303-1]			

Notes:

1) 2) 3)

Existing Equipment Reserved Equipment Equipment To Be Removed

Table 3 - Design Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
5:	157	-	-	· =	-	5

3) ANALYSIS PROCEDURE

Table 4 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	FDH, 1463CQ1600, 04/16/14	262194	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	EDP, 19038, 04/26/91	262191	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Valmont, DC0728Z, 01/22/91	2562465	CCISITES
4-PROPOSED TOWER REINFORCEMENT DRAWINGS	PJF, 37514-2522.001.7700, 11/21/14	*	PJF

3.1) Analysis Method

tnxTower (version 6.1.4.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Monopole will be reinforced in conformance with the attached proposed modification drawings.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J Ford and Company should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	100 - 63.0833	Pole	TP23.6275x14.76x0.281	1	-12.51	1098.19	88.1	Pass
L2	63.0833 - 50.8333	Pole	TP26.57x23.6275x0.5355	2	-14.05	1806.47	69.4	Pass
L3	50.8333 - 32	Pole	TP30.5241x24.4982x0.5529	3	-19.56	2249.09	84.8	Pass
L4	32 - 4	Pole	TP37.2405x30.5241x0.5729	4	-26.87	2894.12	86.2	Pass
L5	4 - 0	Pole	TP38.2x37.2405x0.6335	5	-28.10	3438.38	74.9	Pass
						i –	Summary	
	İ					Pole (L1)	88.1	Pass
	i					RATING =	88.1	Pass

Table 6 - Tower Component Stresses vs. Capacity - LC4.7

Notes	Component	Elevation (ft)	% Capacity	Pass / Fai
1	Anchor Rods	0	84.9	Pass
1	Base Plate	0	64.3	Pass
1	Base Foundation Steel	0	99.4	Pass
1, 2	Base Foundation Soil Interaction	0	12.5	Pass

Other than Define the second state of the seco	00.40/
Structure Rating (max from all components) =	99.4%

Notes:

- See additional documentation in "Appendix C Additional Calculations" for calculations supporting the % capacity consumed
- 2) Foundation Analysis Notes: According to the procedures prescribed and agreed to by the Crown Castle Engineering Foundation Committee, held in January 2010, the existing caisson foundation was analyzed using the methodology in the software 'PLS-Caisson' (Version 8.10, or newer, by Power Line Systems, Inc.). Per the methods in PLS-Caisson, the soil reactions of cohesive soils are calculated using 8CD independent of the depth of the soil layer. The depth of soil to be ignored at the top of the caisson is the greater of the geotechnical report's recommendation, the frost depth of the site or half of the caisson diameter.

4.1) Recommendations

1) See attached proposed modification drawings

APPENDIX A

TNXTOWER OUTPUT

Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

- 1) Tower is located in Hartford County, Connecticut.
- 2) Basic wind speed of 80 mph.
- 3) Nominal ice thickness of 1.0000 in.
- 4) Ice thickness is considered to increase with height.
- 5) Ice density of 56.00 pcf.
- 6) A wind speed of 38 mph is used in combination with ice.
- 7) Deflections calculated using a wind speed of 50 mph.
- 8) A non-linear (P-delta) analysis was used.
- 9) Pressures are calculated at each section.
- 10) Stress ratio used in pole design is 1.333.
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- √ Use Code Stress Ratios
- ✓ Use Code Safety Factors Guys
 ✓ Escalate Ice
 Always Use Max Kz
 Use Special Wind Profile
 Include Bolts In Member Capacity
 Leg Bolts Are At Top Of Section
 Secondary Horizontal Braces Leg
 Use Diamond Inner Bracing (4 Sided)
 Add IBC .6D+W Combination

Distribute Leg Loads As Uniform Assume Legs Pinned

- √ Assume Rigid Index Plate
- √ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
- √ Bypass Mast Stability Checks
- √ Use Azimuth Dish Coefficients
- √ Project Wind Area of Appurt.
- Autocalc Torque Arm Areas
 SR Members Have Cut Ends
 Sort Capacity Reports By Component
 Triangulate Diamond Inner Bracing
 Use TIA-222-G Tension Splice
 Capacity Exemption

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

- √ Consider Feedline Torque Include Angle Block Shear Check Poles
- √ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

Tapered Pole Section Geometry

Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft	Sides	<u>In</u>	in	Īn	in	
L1	100.0000- 63.0833	36.9167	0.00	12	14.7600	23.6275	0.2810	1.1240	A572-65 (65 ksi)
L2	63.0833- 50.8333	12.2500	4.17	12	23.6275	26.5700	0.5354	2.1418	Reinf 52.33 ks (52 ksi)
L3	50.8333- 32.0000	23,0000	0.00	12	24.4982	30.5241	0.5529	2.2116	Reinf 52,70 ks (53 ksi)
L4	32.0000- 4.0000	28.0000	0.00	12	30.5241	37.2405	0.5728	2.2914	Reinf 53.50 ks (54 ksi)
L5	4.0000-0.0000	4.0000		12	37.2405	38.2000	0.6335	2.5340	Reinf 56.10 ksi (56 ksi)

Tapered Pole Properties

Section	Tip Dia. in	Area in²	l in⁴	r in	C in	I/C in³	J in⁴	It/Q in²	w in	w/t
L1	15.2807	13.1009	350.5612	5.1835	7.6457	45.8509	710.3320	6.4479	3.2026	11.397
	24.4610	21.1244	1469.6504	8.3581	12.2391	120,0788	2977.9102	10.3968	5.5791	19.854

Section	Tip Dia.	Area	1	r	С	I/C	J	It/Q	w	w/t
	Ĭn	in ²	in⁴	in	in	in³	in⁴	in ²	in	
L2	24,4610	39.8142	2709.8720	8.2670	12.2391	221,4120	5490.9353	19.5953	4.8972	9.146
	27.5073	44.8874	3883.3897	9.3204	13.7633	282.1562	7868,8003	22.0922	5.6858	10,619
L3	26.4926	42.6316	3120,0318	8,5724	12.6901	245,8636	6322.0303	20.9820	5.0837	9.194
	31,6009	53.3599	6118,0008	10.7297	15.8115	386.9336	12396,728	26.2621	6.6987	12,115
							3			
L4	31,6009	55.2474	6325.9958	10.7226	15.8115	400.0883	12818.182	27.1911	6.6452	11.6
							6			
	38.5542	67,6363	11607,339	13.1270	19.2906	601.7099	23519.616	33.2885	8,4452	14,742
			4				4			
L5	38.5542	74.6747	12772.857	13.1053	19.2906	662.1289	25881.272	36.7526	8,2827	13.074
			6				4			
	39.5476	76,6320	13803,752	13.4488	19.7876	697.5961	27970.144	37.7159	8.5398	13.48
			2				3			

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade Adjust. Factor A _f	Adjust. Factor A,	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals
ft	ft^2	in				in	in
L1 100.0000-			1	1	1		
63.0833							
L2 63.0833-			1	1	1		
50.8333							
L3 50.8333-			1	1	1		
32.0000							
L4 32.0000-			1	1	1		
4.0000							
L5 4.0000-			1	1	1		
0.0000							

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg	G///G/G	.,,,,,	ft	, , , , , , , , , , , , , , , , , , , ,		ft²/ft	plf
FSJ4-50B(1/2")	С	No	Inside Pole	98.0000 - 0.0000	1	No Ice	0.0000	0.14
						1/2" Ice	0.0000	0.14
						1" Ice	0.0000	0.14
						2" Ice	0.0000	0.14
						4" Ice	0.0000	0.14
HJ7-50A(1-5/8")	С	No	Inside Pole	98,0000 - 0.0000	18	No Ice	0.0000	1.04
						1/2" Ice	0.0000	1.04
						1" Ice	0.0000	1.04
						2" Ice	0.0000	1.04
						4" Ice	0.0000	1.04
IB158-1-08U8-S8J18(С	No	CaAa (Out Of	98.0000 - 0.0000	1	No Ice	0.1980	1.30
1-5/8)			Face)			1/2" Ice	0.2980	2.81
						1" Ice	0.3980	4.94
						2" Ice	0.5980	11.02
						4" Ice	0.9980	30.52
HB158-1-08U8-	С	No	CaAa (Out Of	98.0000 - 0.0000	2	No Ice	0.0000	1.30
S8J18(1-5/8)			Face)			1/2" Ice	0,0000	2,81
						1" Ice	0.0000	4.94
						2" Ice	0.0000	11.02
****						4" Ice	0.0000	30.52
2" Bundle	С	No	CaAa (Out Of	85.0000 - 0.0000	1	No Ice	0.2000	1.22
			Face)			1/2" Ice	0.3000	2.74
			,			1" Ice	0.4000	4.88
						2" Ice	0.6000	10.99
						4" Ice	1.0000	30.54
2" Bundle	С	No	CaAa (Out Of	85.0000 - 0.0000	2	No Ice	0.0000	1.22
			Face)			1/2" Ice	0.0000	2.74
			,			1" Ice	0.0000	4.88
						2" Ice	0.0000	10.99
						4" Ice	0.0000	30.54
TCB-B01-001 (5/16")	С	No	Inside Pole	85.0000 - 0.0000	6	No Ice	0.0000	0.06
	-			WE	-	1/2" Ice	0.0000	0.06
vTower Bened ve	!	~ 4 4 4						

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Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg	O/IIOIG	1,100	ft	7 707771007		ft²/ft	plf
						1" Ice	0.0000	0.06
						2" Ice	0,0000	0.06
						4" Ice	0.0000	0.06
FSJ4-50B(1/2")	С	No	Inside Pole	85.0000 - 0,0000	3	No Ice	0.0000	0.14
, ,						1/2" Ice	0.0000	0.14
						1" Ice	0.0000	0.14
						2" Ice	0.0000	0.14
						4" Ice	0.0000	0.14

ATCB-B01-060(5/16)	С	No	CaAa (Out Of	75,0000 - 0,0000	3	No Ice	0.0000	0.07
			Face)			1/2" Ice	0.0000	0.57
			•			1" Ice	0.0000	1.68
						2" Ice	0.0000	5.73
						4" Ice	0.0000	21,16
L98B-002-XXX DB(С	No	Inside Pole	75.0000 - 0.0000	2	No Ice	0.0000	0.06
3/8")						1/2" Ice	0.0000	0.06
,						1" Ice	0.0000	0.06
						2" Ice	0.0000	0.06
						4" Ice	0.0000	0.06
WR-VG86ST-BRD(С	No	CaAa (Out Of	75.0000 - 0.0000	8	No Ice	0.0000	0.59
3/4)			Face)			1/2" Ice	0.0000	1.37
,			,			1" Ice	0.0000	2.76
						2" Ice	0.0000	7.37
						4" Ice	0.0000	23.92
1" conduit	С	No	CaAa (Out Of	75.0000 - 0.0000	1	No Ice	0.0000	0.46
			Face)			1/2" Ice	0.0000	0.46
			,			1" Ice	0.0000	0.46
						2" Ice	0.0000	0.46
						4" Ice	0.0000	0.46

1 1/4" Flat	С	No	CaAa (Out Of	35.5000 - 0.0000	1	No Ice	0.2083	0.00
Reinforcement			Face)			1/2" Ice	0.3194	0.00
			,			1" Ice	0.4306	0.00
						2" ice	0.6528	0.00
						4" Ice	1.0972	0.00
1" Flat Reinforcement	С	No	CaAa (Out Of	65.5000 - 35.5000	1	No Ice	0.1667	0.00
			Face)			1/2" Ice	0.2778	0.00
			,			1" Ice	0.3889	0.00
						2" Ice	0.6111	0.00
						4" Ice	1.0556	0.00

Feed Line/Linear Appurtenances Section Areas

Tower Sectio	Tower Elevation	Face	A_R	A_F	C _A A _A In Face	$C_A A_A$ Out Face	Weight
sectio n	ft Elevation		ft ²	ft^2	ft ²	ft ²	K
L1	100.0000-	Α	0.000	0.000	0.000	0.000	0.00
	63.0833	В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	11.700	0.96
L2	63.0833-50.8333	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	6.917	0.40
L3	50.8333-32.0000	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	10.780	0.62
L4	32.0000-4.0000	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	16.977	0.92
L5	4.0000-0.0000	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	2,425	0.13

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	A_R	A_F	C_AA_A	C_AA_A	Weight
Sectio	Elevation	or	Thickness			In Face	Out Face	
n	ft	Leg	in	ft ²	ft ²	ft ²	ft ²	K
L1	100,0000-	Α	1,113	0.000	0.000	0.000	0.000	0.00
	63.0833	В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	24.946	2.03
L2	63,0833-50,8333	Α	1.067	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	15.053	1.01
L3	50.8333-32,0000	Α	1.027	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0,000	0.000	0.00
		С		0.000	0.000	0.000	23,289	1.55
L4	32.0000-4.0000	Α	1.000	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	34.400	2.15
L5	4.0000-0.0000	Α	1.000	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	4.914	0.31

Feed Line Center of Pressure

Section	Elevation	CP_X	CPz	CP _X Ice	CP _z Ice
	ft	in	in	in	in
L1	100.0000-63.0833	-0.3608	0.2083	-0.5996	0.3462
L2	63.0833-50.8333	-0.5776	0.3335	-0.9544	0.5510
L3	50.8333-32.0000	-0.5979	0.3452	-1.0013	0.5781
L4	32.0000-4.0000	-0.6484	0.3744	-1.0681	0.6167
L5	4.0000-0.0000	-0.6603	0.3812	-1.1053	0.6382

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	٥	ft		ft ²	ft ²	K
BXA-70063/6CFx2 w/ Mount Pipe	Α	From Leg	4.0000 0.00 3.00	0.00	98.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	7.9686 8.6091 9.2158 10.4591 13.0655	5.3981 6.5465 7.4089 9.1837 12.9333	0.04 0.10 0.17 0.33 0.79
(2) DB844G65ZAXY w/ Mount Pipe	Α	From Leg	4.0000 0.00 3.00	0.00	98.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	4.9042 5.3460 5.7972 6.7311 8.7345	4.9208 5.5962 6.2837 7.7123 10.8330	0.03 0.08 0.13 0.26 0.62
(2) RRH2x60-AWS	Α	From Leg	4.0000 0.00 3.00	0.00	98.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	3.9569 4.2724 4.5965 5.2705 6.7224	2.1583 2.4414 2.7330 3.3423 4.6645	0.06 0.08 0.11 0.18 0.37
(2) HBXX-6517DS-A2M w/ Mount Pipe	Α	From Leg	4.0000 0.00 3.00	0.00	98.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	8.9758 9.6473 10.2909 11.5946 14.3212	6.9629 8.1817 9.1436 11.0219 15.0267	0.07 0.14 0.21 0.40 0.91
DB-T1-6Z-8AB-0Z	Α	From Leg	4.0000 0.00 3.00	0.00	98,0000	No Ice 1/2" Ice	5.6000 5.9154 6.2395	2.3333 2.5580 2.7914	0.04 0.08 0.12

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C₄A₄ Front	C _A A _A Side	Weight
			Vert ft ft ft	٥	ft		ft²	ft²	К
			п			1" Ice	6.9136	3.2840	0,21
						2" Ice 4" Ice	8.3654	4.3728	0.45
BXA-70063/6CFx4 w/	В	From Leg	4.0000	0.00	98,0000	No Ice	7.9686	5.3981	0.04
Mount Pipe			0,00			1/2"	8.6091	6.5465	0.10
			3.00			Ice 1" Ice	9.2158	7,4089 9,1837	0.17
						2" Ice 4" Ice	10.4591 13.0655	12,9333	0.33 0.79
(2) DB844G65ZAXY w/	В	From Leg	4.0000	0.00	98.0000	No Ice	4.9042	4.9208	0.03
Mount Pipe		r rom Log	0.00	0.00	00.000	1/2"	5.3460	5.5962	0.08
			3.00			lce	5.7972	6,2837	0,13
						1" Ice	6.7311	7.7123	0.26
						2" Ice 4" Ice	8.7345	10.8330	0.62
RRH 2x60W-1900MHz	В	From Leg	4.0000	0.00	98.0000	No Ice	2.1904	1.4056	0.04
			0.00			1/2"	2.3976	1.5867	0.06
			3.00			lce	2.6134	1.7765	0.08
						1" Ice	3.0710	2.1820	0.12
						2" Ice 4" Ice	4.0899	3.0967	0.26
RRH2x60-AWS	В	From Leg	4.0000	0.00	98.0000	No Ice	3.9569	2.1583	0.06
			0.00			1/2"	4.2724	2.4414	0.08
			3.00			lce	4.5965	2.7330	0.11
						1" Ice	5,2705	3.3423	0.18
						2" Ice 4" Ice	6.7224	4.6645	0.37
(2) HBXX-6517DS-A2M w/	В	From Leg	4.0000	0.00	98,0000	No Ice	8.9758	6.9629	0.07
Mount Pipe			0.00			1/2"	9.6473	8.1817	0.14
			3.00			Ice	10.2909	9.1436	0.21
						1" Ice 2" Ice	11.5946 14.3212	11.0219 15.0267	0.40 0.91
BXA-70063/6CFx2 w/	С	From Leg	4.0000	0.00	98.0000	4" Ice No Ice	7.9686	5.3981	0.04
Mount Pipe	C	Fiolii Leg	0.00	0.00	90.0000	1/2"	8.6091	6.5465	0.10
Mount Fipe			3.00			Ice	9.2158	7.4089	0.17
			3.00			1" Ice	10.4591	9.1837	0.17
						2" Ice	13.0655	12.9333	0.33
						4" Ice	15.0055	12.8555	0.79
(2) DB844G65ZAXY w/	С	From Leg	4.0000	0.00	98.0000	No Ice	4.9042	4.9208	0.03
Mount Pipe	•	r rom Log	0.00	0.00	00.0000	1/2"	5.3460	5.5962	0.08
mount ipo			3.00			lce	5.7972	6.2837	0.13
			- 55			1" Ice	6.7311	7.7123	0.26
						2" Ice	8.7345	10.8330	0.62
						4" Ice			
GPS_A	С	From Leg	4.0000	0.00	98.0000	No Ice	0.2975	0.2975	0.00
			0.00			1/2"	0.3739	0.3739	0.00
			6.00			Ice	0.4589	0.4589	0.01
						1" Ice	0.6549	0.6549	0.02
						2" Ice 4" Ice	1.1506	1.1506	0.08
(2) RRH 2x60W-1900MHz	С	From Leg	4.0000	0.00	98.0000	No Ice	2.1904	1.4056	0.04
		J	0.00			1/2"	2.3976	1.5867	0.06
			3.00			Ice	2,6134	1,7765	0.08
						1" Ice	3.0710	2.1820	0.12
						2" Ice 4" Ice	4.0899	3.0967	0.26
(2) HBXX-6517DS-A2M w/	С	From Leg	4.0000	0.00	98.0000	No Ice	8.9758	6.9629	0.07
Mount Pipe		_	0.00			1/2"	9.6473	8.1817	0.14
			3.00			Ice	10.2909	9.1436	0.21
						1" Ice	11.5946	11.0219	0.40
						2" Ice	14.3212	15.0267	0.91
						4" Ice			
Platform Mount [LP 102-1]	С	None		0.00	98.0000	No Ice 1/2"	45.0000 53.2500	45.0000 53.2500	2.84 3.38
						1/2	JJ.2300	JJ.2500	3.30

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			ft ft ft		ft		ft ²	ft ²	К
****						Ice 1" Ice 2" Ice 4" Ice	61.5000 78.0000 111.0000	61.5000 78.0000 111.0000	3.92 5.01 7.20
LLPX310R W/ Mount Pipe	Α	From Leg	4.0000 0.00 0.00	0.00	85.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	4.9623 5.3512 5.7501 6.5777 8.3714	2.8484 3.3668 3.9019 5.0799 7.8368	0.04 0.08 0.12 0.23 0.53
LLPX310R W/ Mount Pipe	В	From Leg	4.0000 0.00 0.00	0,00	85,0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	4.9623 5.3512 5.7501 6.5777 8.3714	2,8484 3,3668 3,9019 5,0799 7,8368	0.04 0.08 0.12 0.23 0.53
LLPX310R W/ Mount Pipe	С	From Leg	4.0000 0.00 0.00	0.00	85,0000	No Ice 1/2" Ice 1" Ice 2" Ice	4.9623 5.3512 5.7501 6.5777 8.3714	2,8484 3,3668 3,9019 5,0799 7,8368	0.04 0.08 0.12 0.23 0.53
FDD_R6_RRH	Α	From Leg	4.0000 0.00 0.00	0.00	85,0000	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	1.7889 1.9715 2.1627 2.5710 3.4914	0.7778 0.9182 1.0673 1.3914 2.1432	0.03 0.04 0.06 0.09 0.20
FDD_R6_RRH	В	From Leg	4.0000 0.00 0.00	0.00	85,0000	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	1.7889 1.9715 2.1627 2.5710 3.4914	0,7778 0,9182 1,0673 1,3914 2,1432	0.03 0.04 0.06 0.09 0.20
FDD_R6_RRH	С	From Leg	4.0000 0.00 0.00	0.00	85.0000	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	1.7889 1.9715 2.1627 2.5710 3.4914	0.7778 0.9182 1.0673 1.3914 2.1432	0.03 0.04 0.06 0.09 0.20
Platform Mount [LP 601-1]	С	None		0.00	85,0000	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	28.4700 33.5900 38.7100 48.9500 69.4300	28.4700 33.5900 38.7100 48.9500 69.4300	1.12 1.51 1.91 2.69 4.26
6' x 2" Mount Pipe	Α	From Leg	4.0000 0.00 0.00	0.00	85.0000	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	1.4250 1.9250 2.2939 3.0596 4.7022	1.4250 1.9250 2.2939 3.0596 4.7022	0.02 0.03 0.05 0.09 0.23
6' x 2" Mount Pipe	В	From Leg	4.0000 0.00 0.00	0.00	85,0000	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	1.4250 1.9250 2.2939 3.0596 4.7022	1.4250 1.9250 2.2939 3.0596 4.7022	0.02 0.03 0.05 0.09 0.23
6' x 2" Mount Pipe	С	From Leg	4.0000 0.00 0.00	0.00	85.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	1,4250 1,9250 2,2939 3,0596 4,7022	1.4250 1.9250 2.2939 3.0596 4.7022	0.02 0.03 0.05 0.09 0.23

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			Vert ft ft ft	•	ft		ft²	ft²	К
(4) HPA-65R-BUU-H8 w/ Mount Pipe	Α	From Leg	4.0000 0.00 0.00	0.00	75,0000	No Ice 1/2" Ice	13,5328 14.3352 15.1425	9.5823 11.0517 12.4963	0.10 0.20 0.30
						1" Ice 2" Ice 4" Ice	16.7076 19.9544	14.7516 19.4621	0.55 1.22
KRF 102 361/1	Α	From Leg	4,0000 0.00 0.00	0.00	75,0000	No Ice 1/2" Ice	2.2619 2.4645 2.6758	0.6306 0.7561 0.8903	0.03 0.04 0.06
						1" Ice 2" Ice 4" Ice	3.1243 4.1251	1.1845 1.8768	0.09 0.21
(3) RRU-11	Α	From Leg	4.0000 0.00 0.00	0.00	75,0000	No Ice 1/2" Ice 1" Ice	1.9116 2.1019 2.3009 2.7248	1.4717 1.6452 1.8274 2.2176	0.04 0.06 0.08 0.12
						2" Ice 4" Ice	3.6763	3.1016	0.25
(2) RRUS 12-B2	Α	From Leg	4.0000 0.00 0.00	0.00	75,0000	No Ice 1/2" Ice 1" Ice 2" Ice	3.6674 3.9238 4.1888 4.7448 5.9604	1.4828 1.6678 1.8614 2.2745 3.2045	0,06 0.08 0.11 0.17 0.34
(2) RRUS A2	Α	From Leg	4.0000 0.00 0.00	0.00	75,0000	4" Ice No Ice 1/2" Ice	2.4107 2.6193 2.8366	0.5424 0.6752 0.8165	0.02 0.03 0.05
			0.00			1" Ice 2" Ice 4" Ice	3.2970 4.3216	1.1252 1.8462	0.09 0.20
RRUS E2 B29	Α	From Leg	4.0000 0.00 0.00	0,00	75.0000	No Ice 1/2" Ice 1" Ice 2" Ice	3.6692 3.9256 4.1907 4.7468 5.9627	1.4875 1.6727 1.8665 2.2800 3.2107	0.06 0.08 0.11 0.17 0.35
RRUS-32 B30	Α	From Leg	4.0000 0.00 0.00	0.00	75,0000	4" Ice No Ice 1/2" Ice 1" Ice	3,8662 4.1506 4.4435 5.0554	2.7616 3.0213 3.2896 3.8522	0.08 0.10 0.14 0.21
DC6-48-60-18-8F	٨	From Leg	4.0000	0.00	75.0000	2" Ice 4" Ice	6.3828 1.4667	5.0811 1.4667	0.41
DC0-40-00-10-01	A	· ·	0.00 0.00	0.00	73.0000	No Ice 1/2" Ice 1" Ice 2" Ice	1.6667 1.8778 2.3333 3.3778	1.6667 1.8778 2.3333 3.3778	0.04 0.06 0.11 0.24
(4) HPA-65R-BUU-H8 w/ Mount Pipe	В	From Leg	4.0000 0.00 0.00	0,00	75,0000	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	13.5328 14.3352 15.1425 16.7076 19.9544	9.5823 11.0517 12.4963 14.7516 19.4621	0.10 0.20 0.30 0.55 1.22
KRF 102 361/1	В	From Leg	4.0000 0.00 0.00	0.00	75.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	2.2619 2.4645 2.6758 3.1243 4.1251	0.6306 0.7561 0.8903 1.1845 1.8768	0.03 0.04 0.06 0.09 0.21
(3) RRU-11	В	From Leg	4.0000 0.00 0.00	0.00	75,0000	No Ice 1/2" Ice 1" Ice	1.9116 2.1019 2.3009 2.7248	1.4717 1.6452 1.8274 2.2176	0.04 0.06 0.08 0.12

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C₄A₄ Front	C _A A _A Side	Weight
			ft ft ft	•	ft		ft ²	ft ²	К
						2" Ice 4" Ice	3.6763	3.1016	0.25
(2) RRUS 12-B2	В	From Leg	4.0000 0.00 0.00	0.00	75.0000	No Ice 1/2" Ice	3.6674 3.9238 4.1888	1.4828 1.6678 1.8614	0.06 0.08 0.11
						1" Ice 2" Ice 4" Ice	4.7448 5 ₋ 9604	2.2745 3.2045	0.17 0.34
(2) RRUS A2	В	From Leg	4.0000 0.00 0.00	0.00	75.0000	No Ice 1/2" Ice	2.4107 2.6193 2.8366	0.5424 0.6752 0.8165	0.02 0.03 0.05
						1" Ice 2" Ice 4" Ice	3.2970 4.3216	1.1252 1.8462	0.09 0.20
RRUS E2 B29	В	From Leg	4.0000 0.00 0.00	0.00	75,0000	No Ice 1/2" Ice 1" Ice 2" Ice	3.6692 3,9256 4.1907 4.7468 5.9627	1.4875 1.6727 1.8665 2.2800 3.2107	0.06 0.08 0.11 0.17 0.35
RRUS-32 B30	В	From Leg	4.0000	0.00	75,0000	4" Ice No Ice	3.8662	2.7616	0.08
			0.00			1/2" Ice 1" Ice 2" Ice 4" Ice	4.1506 4.4435 5.0554 6.3828	3.0213 3.2896 3.8522 5.0811	0.10 0.14 0.21 0.41
(2) DC6-48-60-18-8F	В	From Leg	4.0000 0.00 0.00	0.00	75.0000	No Ice 1/2" Ice 1" Ice 2" Ice	1.4667 1.6667 1.8778 2.3333 3.3778	1,4667 1,6667 1,8778 2,3333 3,3778	0.02 0.04 0.06 0.11 0.24
(4) HPA-65R-BUU-H8 w/ Mount Pipe	С	From Leg	4.0000 0.00 0.00	0.00	75.0000	4" Ice No Ice 1/2" Ice 1" Ice	13.5328 14.3352 15.1425 16.7076	9.5823 11.0517 12.4963 14.7516	0.10 0.20 0.30 0.55
KRF 102 361/1	С	From Leg	4.0000	0.00	75.0000	2" Ice 4" Ice No Ice	19.9544 2.2619	19.4621 0.6306	1.22 0.03
			0.00 0.00			1/2" Ice 1" Ice 2" Ice	2,4645 2.6758 3.1243 4.1251	0.7561 0.8903 1.1845 1.8768	0.04 0.06 0.09 0.21
(3) RRU-11	С	From Leg	4.0000 0.00 0.00	0.00	75.0000	4" Ice No Ice 1/2" Ice 1" Ice	1.9116 2.1019 2.3009 2.7248	1.4717 1.6452 1.8274 2.2176	0.04 0.06 0.08 0.12
(2) RRUS 12-B2	С	From Leg	4.0000 0.00	0.00	75,0000	2" Ice 4" Ice No Ice 1/2"	3.6763 3.6674 3.9238	3.1016 1.4828 1.6678	0.25 0.06 0.08
			0.00			Ice 1" Ice 2" Ice 4" Ice	4.1888 4.7448 5.9604	1.8614 2.2745 3.2045	0.11 0.17 0.34
(2) RRUS A2	С	From Leg	4.0000 0.00 0.00	0.00	75.0000	No Ice 1/2" Ice 1" Ice 2" Ice	2.4107 2.6193 2.8366 3.2970 4.3216	0.5424 0.6752 0.8165 1.1252 1.8462	0.02 0.03 0.05 0.09 0.20
RRUS E2 B29	С	From Leg	4.0000 0.00 0.00	0.00	75.0000	4" Ice No Ice 1/2" Ice	3.6692 3.9256 4.1907	1.4875 1.6727 1.8665	0.06 0.08 0.11

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	٠	ft		ft ²	ft²	K
						1" lce 2" lce 4" lce	4.7468 5.9627	2,2800 3.2107	0.17 0.35
RRUS-32 B30	С	From Leg	4.0000 0.00	0.00	75,0000	No Ice 1/2"	3.8662 4.1506	2.7616 3.0213	0.08 0.10
			0.00			Ice 1" Ice 2" Ice 4" Ice	4.4435 5.0554 6.3828	3.2896 3.8522 5.0811	0.14 0.21 0.41
DC6-48-60-18-8F	С	From Leg	4.0000 0.00 0.00	0.00	75.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	1.4667 1.6667 1.8778 2.3333 3.3778	1.4667 1.6667 1.8778 2.3333 3.3778	0.02 0.04 0.06 0.11 0.24
Platform Mount [LP 1303- 1]	С	None		0.00	75.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	56,8000 70,8000 84,8000 112,8000 168,8000	56.8000 70.8000 84.8000 112.8000 168.8000	2,53 3.38 4.24 5.96 9.38

Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				ft	0	0	ft	ft		ft ²	K
VHLP2-23	Α	Paraboloid w/o	From	4.0000	0.00		85.0000	2.1750	No Ice	3.7200	0.03
		Radome	Leg	0.00					1/2" Ice	4.0100	0.05
				0.00					1" Ice	4.3000	0.07
									2" Ice	4.8800	0.11
									4" Ice	6.0400	0.20
VHLP2-23	В	Paraboloid w/o	From	4.0000	0.00		85.0000	2.1750	No Ice	3.7200	0.03
		Radome	Leg	0.00					1/2" Ice	4.0100	0.05
				0.00					1" Ice	4.3000	0.07
									2" Ice	4.8800	0.11
									4" Ice	6.0400	0.20
VHLP2-23	С	Paraboloid w/o	From	4.0000	0.00		85.0000	2.1750	No Ice	3.7200	0.03
		Radome	Leg	0.00					1/2" Ice	4.0100	0.05
				0.00					1" Ice	4.3000	0.07
									2" ice	4.8800	0.11
									4" Ice	6.0400	0.20

Tower Pressures - No Ice

 $G_H = 1.690$

Section	Z	Kz	q_z	A _G	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation					a				%	In	Out
					С					Face	Face
ft	ft		psf	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
L1 100.0000-	80.4157	1.29	21.08	59.048	Α	0.000	59.048	59.048	100.00	0.000	0.000
63.0833		1			В	0.000	59.048		100.00	0.000	0.000
					С	0.000	59.048		100.00	0.000	11.700
L2 63.0833-	56.8386	1,168	19,14	25.622	Α	0.000	25.622	25.622	100.00	0.000	0.000
50.8333					В	0.000	25.622		100.00	0.000	0.000
					C	0.000	25.622		100.00	0.000	6.917
L3 50.8333-	41,1406	1.065	17.45	44.034	Α	0.000	44.034	44.034	100.00	0.000	0.000
32.0000			ļ I	Į Į	В	0.000	44.034		100.00	0.000	0.000

Section	Z	Kz	q_z	A_{G}	F	A_F	A_R	A _{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation		(a				%	ln	Out
					c					Face	Face
ft	ft		psf	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
					С	0.000	44.034		100,00	0.000	10.780
L4 32.0000-	17.5375	1	16,38	79,059	Α	0.000	79.059	79.059	100.00	0.000	0.000
4,0000					В	0.000	79,059		100,00	0.000	0.000
					С	0.000	79.059		100.00	0,000	16.977
L5 4.0000-	1,9915	1	16.38	12.573	Α	0.000	12.573	12.573	100.00	0.000	0.000
0.0000					В	0.000	12.573		100,00	0,000	0.000
, and the second					С	0.000	12.573		100,00	0.000	2.425

Tower Pressure - With Ice

$G_H = 1.690$

Section	Z	Kz	q_z	tz	A_G	F	A_F	A_R	A _{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation						а				%	In	Out
						С					Face	Face
ft	ft		psf	in	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
L1 100.0000-	80.4157	1.29	4.66	1.1128	65.894	Α	0.000	65.894	65.894	100.00	0.000	0.000
63.0833						В	0.000	65.894		100.00	0.000	0.000
						С	0.000	65.894		100.00	0.000	24.946
L2 63.0833-	56.8386	1.168	4.23	1.0674	27.801	Α	0.000	27.801	27.801	100.00	0.000	0.000
50.8333						В	0.000	27.801		100.00	0.000	0.000
l						С	0.000	27.801		100.00	0.000	15.053
L3 50,8333-	41.1406	1.065	3.85	1.0268	47,384	Α	0,000	47.384	47.384	100.00	0.000	0.000
32.0000						В	0.000	47.384		100.00	0.000	0.000
						C	0.000	47.384		100.00	0.000	23.289
L4 32,0000-	17.5375	1	3.62	1.0000	83.725	Α	0,000	83,725	83,725	100,00	0.000	0.000
4.0000						В	0.000	83.725		100.00	0.000	0.000
						С	0.000	83.725		100.00	0.000	34.400
L5 4,0000-	1.9915	1	3.62	1.0000	13,240	Α	0.000	13.240	13.240	100.00	0.000	0.000
0.0000				× ×	20	В	0.000	13.240		100.00	0,000	0.000
74:						С	0.000	13.240		100.00	0.000	4.914

Tower Pressure - Service

$G_H = 1.690$

Section	Z	Kz	q_z	$A_{\rm G}$	F	A_F	A_R	A _{lea}	Leg	$C_A A_A$	$C_A A_A$
Elevation					а			Ĭ	%	In	Out
					С					Face	Face
ft	ft		psf	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
L1 100.0000-	80.4157	1.29	8.24	59.048	Α	0.000	59.048	59.048	100.00	0.000	0.000
63.0833					В	0.000	59.048		100.00	0.000	0.000
					С	0.000	59.048		100.00	0.000	11.700
L2 63.0833-	56.8386	1.168	7.48	25.622	Α	0.000	25.622	25.622	100.00	0.000	0.000
50.8333					В	0.000	25.622		100.00	0.000	0.000
					С	0.000	25.622		100.00	0.000	6.917
L3 50.8333-	41.1406	1.065	6.82	44.034	Α	0.000	44.034	44,034	100.00	0,000	0.000
32,0000					В	0,000	44.034		100.00	0.000	0.000
					С	0.000	44.034		100.00	0.000	10.780
L4 32,0000-	17,5375	1	6.40	79.059	Α	0.000	79.059	79.059	100.00	0.000	0.000
4.0000					В	0.000	79.059		100.00	0.000	0.000
					С	0.000	79.059		100.00	0.000	16.977
L5 4.0000-	1.9915	1	6.40	12.573	Α	0.000	12.573	12.573	100.00	0.000	0.000
0.0000					В	0.000	12.573		100.00	0.000	0.000
					С	0.000	12.573		100.00	0.000	2.425

Load Combinations

Comb. Description No.

Dead Only Dead+Wind 0 deg - No Ice

Comb.		Description
No.	D - 1/1//- 1 00 1 - 1/- 1	
3	Dead+Wind 30 deg - No Ice	
4	Dead+Wind 60 deg - No Ice	
5	Dead+Wind 90 deg - No Ice	
6	Dead+Wind 120 deg - No Ice	
7	Dead+Wind 150 deg - No Ice	
8	Dead+Wind 180 deg - No Ice	
9	Dead+Wind 210 deg - No Ice	
10	Dead+Wind 240 deg - No Ice	
11 12	Dead+Wind 270 deg - No Ice Dead+Wind 300 deg - No Ice	
13	Dead+Wind 330 deg - No Ice	
14	Dead+lice	
15	Dead+lce Dead+Wind 0 deg+lce	
16	Dead+Wind 30 deg+lce	
17	Dead+Wind 60 deg+lce	
18	Dead+Wind 90 deg+lce	
19	Dead+Wind 120 deg+lce	
20	Dead+Wind 150 deg+lce	
21	Dead+Wind 180 deg+lce	
22	Dead+Wind 210 deg+lce	
23	Dead+Wind 240 deg+lce	
24	Dead+Wind 270 deg+Ice	
25	Dead+Wind 300 deg+lce	
26	Dead+Wind 330 deg+lce	
27	Dead+Wind 0 deg - Service	
28	Dead+Wind 30 deg - Service	
29	Dead+Wind 60 deg - Service	
30	Dead+Wind 90 deg - Service	
31	Dead+Wind 120 deg - Service	
32	Dead+Wind 150 deg - Service	
33	Dead+Wind 180 deg - Service	
34	Dead+Wind 210 deg - Service	
35	Dead+Wind 240 deg - Service	
36	Dead+Wind 270 deg - Service	
37	Dead+Wind 300 deg - Service	
38	Dead+Wind 330 deg - Service	

Maximum Member Forces

Sectio n	Elevation ft	Component Type	Condition	Gov. Load	Force	Major Axis Moment	Minor Axis Moment
No.	"	1,400		Comb.	K	kip-ft	kip-ft
L1	100 - 63.0833	Pole	Max Tension	15	0.00	-0.00	-0.00
			Max. Compression	14	-27.27	0.73	0.11
			Max. Mx	11	-12.55	442.60	3.16
			Max. My	2	-12.51	0.72	451.63
			Max. Vy	11	-20.63	442.60	3.16
			Max. Vx	2	-20.90	0.72	451.63
			Max. Torque	11			-0.59
L2	63.0833 - 50.8333	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-29.36	1.21	-0.16
			Max. Mx	11	-14.08	612.01	4.12
			Max. My	2	-14.05	0.95	623.08
			Max. Vý	11	-21.29	612.01	4.12
			Max. Vx	2	-21.56	0.95	623.08
			Max. Torque	12			-0.48
L3	50.8333 - 32	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-36.64	2.68	-1.00
			Max. Mx	11	-19,57	1124.08	6.81
			Max. My	2	-19.56	1.65	1140.89
			Max. Vy	11	-23.18	1124.08	6.81
			Max. Vx	2	-23.45	1.65	1140.89
			Max. Torque	12			-0.43
L4	32 - 4	Pole	Max Tension	1	0.00	0.00	0.00
			Max, Compression	14	-45.87	4.63	-2.13
			Max. Mx	11	-26.87	1804.55	9.97

Sectio	Elevation	Component	Condition	Gov.	Force	Major Axis	Minor Axis
n	ft	Type		Load		Moment	Moment
No.				Comb.	K	kip-ft	kip-ft
			Max. My	2	-26.87	2.58	1828.09
			Max. Vy	11	-25.47	1804.55	9.97
			Max. Vx	2	-25,73	2.58	1828.09
			Max. Torque	11			-0.36
L5	4 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	- 47.40	4.95	-2.31
			Max. Mx	11	-28,10	1907.14	10.41
			Max. My	2	-28.10	2.71	1931,61
			Max. Vy	11	-25.81	1907.14	10.41
			Max. Vx	2	-26.08	2.71	1931.61
			Max, Torque	4			0.27

Maximum Reactions

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, 2
		Load	K	K	K
		Comb.			
Pole	Max. Vert	23	47.40	6.38	-3.70
	Max. H _x	11	28.11	25.80	0.12
	Max. H _z	2	28.11	0.02	26.07
	Max. M _x	2	1931.61	0,02	26.07
	Max. M _z	5	1905.20	-25.80	0.09
	Max. Torsion	4	0.27	-22.37	13.00
	Min. Vert	1	28.11	0.00	0.00
	Min. H _x	5	28.11	-25.80	0.09
	Min. H₂	8	28.11	-0.02	-26.02
	Min. M _x	8	<i>-</i> 1928.55	-0.02	-26,02
	Min_*M_z	11	-1907.14	25.80	0.12
	Min. Torsion	10	-0.26	22.41	-13.02

Tower Mast Reaction Summary

Load Combination	Vertical	Shear _x	Shearz	Overturning Moment, M _x	Overturning Moment, M ₂	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	28.11	0.00	0.00	0.37	0.95	0.00
Dead+Wind 0 deg - No Ice	28.11	-0.02	-26.07	-1931.61	2.71	-0.10
Dead+Wind 30 deg - No Ice	28.11	12.98	-22.44	-1661.46	- 958.42	-0,21
Dead+Wind 60 deg - No Ice	28.11	22.37	-13,00	-962.23	-1651.59	-0.27
Dead+Wind 90 deg - No Ice	28.11	25.80	-0.09	-6.93	-1905.20	-0.26
Dead+Wind 120 deg - No Ice	28.11	22.42	13.05	967.88	-1656.61	-0.16
Dead+Wind 150 deg - No Ice	28.11	12.83	22.57	1672.98	- 945.77	-0.03
Dead+Wind 180 deg - No Ice	28,11	0.02	26.02	1928.55	-0.77	0.10
Dead+Wind 210 deg - No Ice	28.11	-12.80	22.55	1671.24	944.70	0.20
Dead+Wind 240 deg - No Ice	28.11	-22.41	13.02	964.87	1656.82	0.26
Dead+Wind 270 deg - No Ice	28,11	-25.80	-0.12	-10.41	1907.14	0.26
Dead+Wind 300 deg - No Ice	28.11	-22,39	-13.03	-965.24	1655.26	0.18
Dead+Wind 330 deg - No Ice	28.11	-13.01	-22.46	-1663,20	963.38	0.04
Dead+Ice	47.40	-0.00	0.00	2.31	4.95	0.00
Dead+Wind 0 deg+lce	47.40	-0.00	-7.41	-564.13	5.43	-0.10
Dead+Wind 30 deg+lce	47.40	3.69	-6.38	-485.24	-276.77	-0.10
Dead+Wind 60 deg+lce	47,40	6.37	-3.70	-280.04	-480.54	-0.08
Dead+Wind 90 deg+lce	47.40	7.35	-0.02	0.34	- 555.08	-0.04
Dead+Wind 120 deg+lce	47.40	6.38	3.71	285.93	- 481.83	0.02
Dead+Wind 150 deg+lce	47.40	3.65	6.41	492.74	-273.29	0.07
Dead+Wind 180 deg+lce	47.40	0.00	7.40	567.80	4.62	0.10
Dead+Wind 210 deg+lce	47.40	-3.65	6.41	492.34	282.64	0.10
Dead+Wind 240 deg+lce	47.40	-6.38	3.70	285.23	491.47	0.08
Dead+Wind 270 deg+lce	47.40	- 7.35	-0.03	-0.47	565.12	0.04
Dead+Wind 300 deg+lce	47.40	-6.37	-3.70	-280.73	490.99	-0.02
Dead+Wind 330 deg+lce	47.40	-3.70	-6.39	-485.65	287.51	-0.07
Dead+Wind 0 deg - Service	28.11	-0.01	-10.18	- 754.90	1.65	-0.04
Dead+Wind 30 deg - Service	28.11	5.07	-8.77	-649.28	-374.08	-0,08
Dead+Wind 60 deg - Service	28.11	8.74	-5.08	-375.93	-645.05	-0.11

tnxTower Report - version 6.1.4.1

Load Combination	Vertical	Shear _x	Shear _z	Overturning Moment, M _x	Overturning Moment, M ₂	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 90 deg - Service	28.11	10.08	-0.03	-2.49	-744.19	-0.10
Dead+Wind 120 deg - Service	28.11	8.76	5.10	378,59	-647.02	-0.07
Dead+Wind 150 deg - Service	28.11	5,01	8.81	654.24	-369.14	-0.01
Dead+Wind 180 deg - Service	28.11	0.01	10.16	754.15	0.29	0.04
Dead+Wind 210 deg - Service	28.11	-5,00	8.81	653.55	369.90	0.08
Dead+Wind 240 deg - Service	28.11	-8.75	5.09	377.41	648.28	0.10
Dead+Wind 270 deg - Service	28.11	-10.08	-0.05	-3,85	746.13	0.10
Dead+Wind 300 deg - Service	28.11	-8.74	-5.09	-377.11	647.67	0.07
Dead+Wind 330 deg - Service	28.11	-5.08	-8.77	-649,96	377.20	0.02

Solution Summary

	Sun	n of Applied Force	es		Sum of Reactions				
Load	PX	PY	PZ	PX	PY	PZ	% Erro		
Comb.	K	K	K	K	K	K			
1	0.00	-28.11	0.00	0.00	28,11	0.00	0.000%		
2	-0.02	-28,11	-26.07	0.02	28.11	26.07	0.000%		
3	12.98	-28.11	-22,44	-12.98	28.11	22.44	0.000%		
4	22.37	-28,11	-13,00	-22.37	28.11	13.00	0.000%		
5	25.80	-28,11	-0.09	-25.80	28.11	0.09	0.000%		
6	22.42	-28,11	13.05	-22.42	28.11	-13.05	0.000%		
7	12.83	-28.11	22.57	-12.83	28.11	-22.57	0.000%		
8	0.02	-28.11	26.02	-0.02	28.11	-26.02	0.000%		
9	-12.80	-28.11	22.55	12.80	28.11	-22.55	0.000%		
10	-22.41	-28.11	13.02	22.41	28.11	-13.02	0.000%		
11	-25.80	-28.11	-0.12	25.80	28.11	0.12	0.000%		
12	-22.39	-28.11	-13.03	22.39	28.11	13.03	0.000%		
13	-13.01	-28.11	-22,46	13.01	28.11	22.46	0.000%		
14	0.00	-47.40	0.00	0.00	47.40	-0.00	0.000%		
15	-0.00	-47.40	-7.41	0.00	47.40	7.41	0.000%		
16	3.69	-47.40	-6.38	-3,69	47.40	6.38	0.000%		
17	6.37	-47.40	-3.70	-6.37	47.40	3.70	0.000%		
18	7.35	-47.40	-0.02	-7,35	47.40	0.02	0.000%		
19	6.38	-47.40	3.71	-6,38	47.40	-3.71	0.000%		
20	3.65	-47.40	6.41	-3.65	47.40	-6.41	0.000%		
21	0.00	-47.40	7.40	-0.00	47.40	-7.40	0.000%		
22	-3.65	-47.40	6.41	3.65	47.40	-6.41	0.000%		
23	-6.38	-47.40	3.70	6.38	47.40	-3.70	0.000%		
24	-7.35	-47.40	-0.03	7.35	47.40	0.03	0.000%		
25	-6.37	-47.40	-3.70	6.37	47.40	3.70	0.000%		
26	-3.70	-47.40	-6.39	3.70	47.40	6.39	0.000%		
27	-0.01	- 28.11	-10.18	0.01	28.11	10.18	0.000%		
28	5.07	-28.11	-8.77	-5.07	28.11	8.77	0.000%		
29	8.74	-28.11	-5.08	-8.74	28.11	5.08	0.000%		
30	10.08	- 28.11	-0.03	-10.08	28.11	0.03	0.000%		
31	8.76	-28.11	5.10	-8.76	28.11	-5.10	0.000%		
32	5,01	- 28.11	8.81	-5,01	28.11	-8.81	0.000%		
33	0.01	-28.11	10.16	-0.01	28.11	-10.16	0.000%		
34	-5.00	-28.11	8.81	5.00	28.11	-8.81	0.000%		
35	-8.75	-28.11	5.09	8.75	28.11	-5.09	0.000%		
36	-10.08	-28.11	-0.05	10.08	28.11	0.05	0.000%		
37	-8.74	-28.11	-5.09	8.74	28.11	5.09	0.000%		
38	-5.08	-28.11	-8.77	5.08	28.11	8.77	0.000%		

Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	4	0.0000001	0.00000001
2	Yes	4	0.00000001	0.00008875
3	Yes	5	0.0000001	0.00019737
4	Yes	5	0.00000001	0.00019921
5	Yes	4	0.0000001	0.00021970
6	Yes	5	0.00000001	0.00019682
7	Yes	5	0.0000001	0.00019886
8	Yes	4	0.0000001	0.00009655
9	Yes	5	0.00000001	0.00019733
10	Yes	5	0.0000001	0.00019660
11	Yes	4	0.00000001	0.00024828
12	Yes	5	0.00000001	0.00020091
13	Yes	5	0.0000001	0.00019778
14	Yes	4	0.00000001	0.00000001
15	Yes	4	0,00000001	0.00016280
16	Yes	4	0.0000001	0.00063444
17	Yes	4	0.0000001	0.00065320
18	Yes	4	0.0000001	0.00016153
19	Yes	4	0.00000001	0.00064635
20	Yes	4	0.00000001	0.00064775
21	Yes	4	0.0000001	0.00016279
22	Yes	4	0.00000001	0.00067339
23	Yes	4	0.0000001	0.00065803
24	Yes	4	0.0000001	0.00016473
25	Yes	4	0.0000001	0.00067158
26	Yes	4	0.0000001	0.00066599
27	Yes	4	0.0000001	0.00005192
28	Yes	4	0.0000001	0.00060714
29	Yes	4	0.0000001	0.00061978
30	Yes	4	0.00000001	0.00006392
31	Yes	4	0.00000001	0.00060183
32	Yes	4	0.0000001	0.00061931
33	Yes	4	0.00000001	0.00005210
34	Yes	4	0.00000001	0.00061242
35	Yes	4	0.00000001	0.00060285
36	Yes	4	0.00000001	0.00006574
37	Yes	4	0.00000001	0.00062931
38	Yes	4	0.00000001	0.00060887

Maximum Tower Deflections - Service Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.		à
L1	100 - 63,0833	20.62	27	1.92	0.00
L2	63.0833 -	7.82	27	1.20	0.00
	50.8333				
L3	55 - 32	5.92	27	1.04	0.00
L4	32 - 4	1.91	27	0.59	0.00
L5	4 - 0	0.03	27	0.06	0.00

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	30	0.0	ft
98.0000	BXA-70063/6CFx2 w/ Mount	27	19.84	1.88	0.00	12411
	Pipe					
85.0000	VHLP2-23	27	14.87	1.63	0.00	4137
75.0000	(4) HPA-65R-BUU-H8 w/ Mount	27	11.36	1.43	0.00	2481
	Pipe					

Maximum Tower Deflections	S	- D	esign)	Wind
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Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	100 - 63.0833	52.68	2	4.90	0.01
L2	63.0833 -	20.01	2	3.07	0.00
	50.8333				
L3	55 - 32	15.15	2	2,67	0.00
L4	32 - 4	4.88	2	1.51	0.00
L5	4 - 0	0.07	2	0.16	0.00

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	۰	0	ft
98.0000	BXA-70063/6CFx2 w/ Mount Pipe	2	50.68	4.80	0.01	4919
85.0000	VHLP2-23	2	38.00	4.15	0.01	1638
75.0000	(4) HPA-65R-BUU-H8 w/ Mount Pipe	2	29.04	3.66	0.00	981

Compression Checks

Pole Design Data

Section No.	Elevation	Size	L	L_{u}	KI/r	Fa	Α	Actual P	Allow.	Ratio P
ft		ft	ft		ksi	in ²	K	K	Pa	
L1	100 - 63.0833	TP23.6275x14.76x0.281	36.9167	0.0000	0.0	39.00	21.1244	-12.51	823.85	0.015
L2	63.0833 - 50.8333 (2)	TP26.57x23.6275x0.5355	12.2500	0.0000	0.0	31.40	43.1618	-14.05	1355.19	0.010
L3	50.8333 - 32	TP30.5241x24.4982x0.552	23.0000	0.0000	0.0	31.62	53.3599	-19.56	1687.24	0.012
L4	32 - 4 (4)	TP37.2405x30.5241x0.572	28.0000	0.0000	0.0	32.10	67.6363	-26.87	2171.13	0.012
L5	4 - 0 (5)	TP38.2x37.2405x0.6335	4.0000	0.0000	0.0	33.66	76.6320	-28.10	2579.43	0.011

Pole Bending Design Data

Section No.	Elevation	Size	Actual M _x	Actual f _{bx}	Allow.	Ratio f _{bx}	Actual M _y	Actual f _{by}	Allow. F _{by}	Ratio f _{by}
	ft		kip-ft	ksi	ksi	F _{bx}	kip-ft	ksi	ksi	F_{by}
L1	100 - 63.0833 (1)	TP23.6275x14.76x0.281	451.63	45.13	39.00	1.157	0.00	0.00	39.00	0.000
L2	63.0833 - 50.8333 (2)	TP26.57x23.6275x0.5355	623.08	28.68	31.40	0.914	0.00	0.00	31.40	0.000
L3	50.8333 - 32 (3)	TP30.5241x24.4982x0.55 29	1140.8 9	35.38	31.62	1.119	0.00	0.00	31.62	0.000
L4	32 - 4 (4)	TP37.2405x30,5241x0,57	1828.0 9	36.46	32.10	1.136	0,00	0.00	32.10	0.000
L5	4 - 0 (5)	TP38.2x37.2405x0.6335	1931.6 1	33.23	33.66	0.987	0.00	0.00	33.66	0.000

Pole	Shear	Design	Data

Section No.	Elevation	Size	Actual V	Actual f _v	Allow. F _v	Ratio f _v	Actual T	Actual f _{vt}	Allow. F _{vt}	Ratio f _{vt}
	ft		K	ksi	ksi	$\overline{F_{\nu}}$	kip-ft	ksi	ksi	$\overline{F_{vt}}$
L1	100 - 63.0833 (1)	TP23.6275x14,76x0,281	20.90	0.99	26.00	0.077	0.21	0.01	26.00	0.000
L2	63.0833 - 50.8333 (2)	TP26.57x23.6275x0.5355	21.56	0.50	20,93	0.048	0.18	0.00	20.93	0.000
L3	50.8333 - 32	TP30_5241x24_4982x0.55	23.45	0.44	21.08	0.042	0.08	0.00	21.08	0.000
L4	32 - 4 (4)	TP37.2405x30.5241x0.57	25.73	0.38	21.40	0,036	0.08	0.00	21.40	0.000
L5	4 - 0 (5)	TP38,2x37,2405x0,6335	26.08	0.34	22.44	0.031	0.10	0.00	22.44	0.000

Pole Interaction Design Data

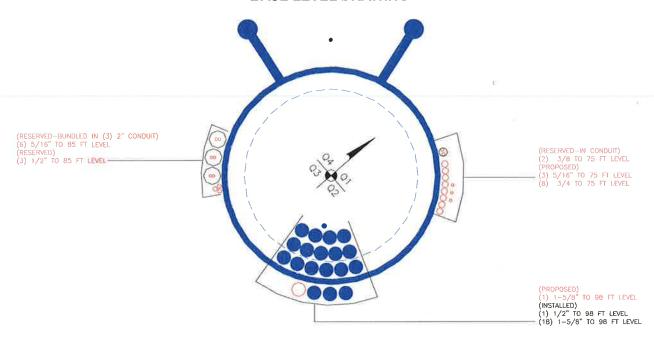
Section No.	Elevation	Ratio P	Ratio f _{bx}		Ratio f _v F _v	Ratio f _{vt}	Comb. Stress	Allow. Stress Ratio	Criteria
	ft	Pa	F_{bx}				Ratio		
L1	100 - 63.0833 (1)	0.015	1.157	0.000	0,077	0.000	1,174	1.333	H1-3+√T 🗸
L2	63,0833 - 50.8333 (2)	0.010	0.914	0.000	0.048	0.000	0.925	1,333	H1-3+VT
L3	50.8333 - 32 (3)	0.012	1.119	0.000	0.042	0.000	1.131	1.333	H1-3+VT
L4	32 - 4 (4)	0.012	1.136	0.000	0.036	0.000	1.148	1.333	H1-3+VT
L5	4 - 0 (5)	0.011	0.987	0.000	0.031	0.000	0.998	1,333	H1-3+VT 🗸

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P _{allow} K	% Capacity	Pass Fail
L1	100 - 63.0833	Pole	TP23.6275x14.76x0.281	1	-12.51	1098.19	88.1	Pass
L2	63.0833 - 50.8333	Pole	TP26,57x23.6275x0.5355	2	- 14.05	1806.47	69.4	Pass
L3	50.8333 - 32	Pole	TP30.5241x24.4982x0.5529	3	-19.56	2249.09	84.8	Pass
L4	32 - 4	Pole	TP37 2405x30.5241x0.5729	4	-26.87	2894.12	86.2	Pass
L5	4 - 0	Pole	TP38.2x37.2405x0.6335	5	-28.10	3438.38	74.9	Pass
							Summary	
						Pole (L1)	88.1	Pass
						RATING =	88.1	Pass

APPENDIX B

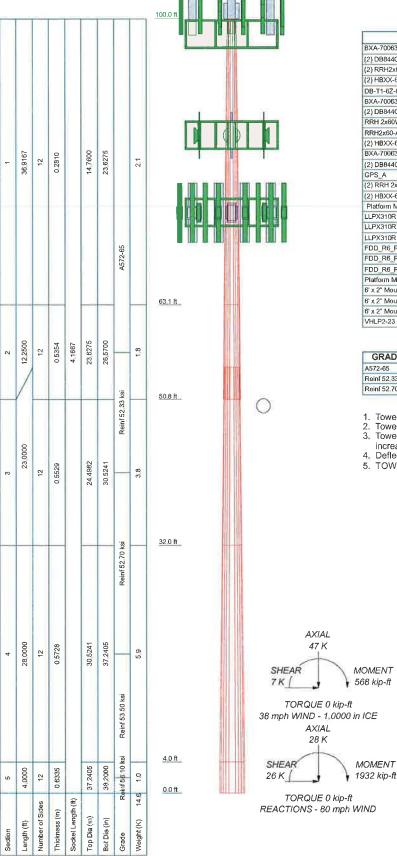
BASE LEVEL DRAWING



APPENDIX C

ADDITIONAL CALCULATIONS

Program Version 6.1.4.1 - 12/17/2013 File:G:/TOWER/375_Crown_Castle/2014/37514-2522 BU 806371/WO 965888 BU 806371 SDD 001/37514-2522.001.7700_Reinforced.eri



DESIGNED APPURTENANCE LOADING

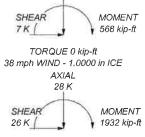
TYPE	ELEVATION	TYPE	ELEVATION	
BXA-70063/6CFx2 w/ Mount Pipe	98	VHLP2-23	85	
(2) DB844G65ZAXY w/ Mount Pipe	98	VHLP2-23	85	
(2) RRH2x60-AWS	98	(2) RRUS 12-B2	75	
(2) HBXX-6517DS-A2M w/ Mount Pipe	98	(2) RRUS A2	75	
DB-T1-6Z-8AB-0Z	98	RRUS E2 B29	75	
BXA-70063/6CFx4 w/ Mount Pipe	98	RRUS-32 B30	75	
(2) DB844G65ZAXY w/ Mount Pipe	98	DC6-48-60-18-8F	75	
RRH 2x60W-1900MHz	98	(4) HPA-65R-BUU-H8 w/ Mount Pipe	75	
RRH2x60-AWS	98	KRF 102 361/1	75	
(2) HBXX-6517DS-A2M w/ Mount Pipe	98	(3) RRU-11	75	
BXA-70063/6CFx2 w/ Mount Pipe	98	(2) RRUS 12-B2	75	
(2) DB844G65ZAXY w/ Mount Pipe	98	(2) RRUS A2	75	
GPS_A	98	RRUS E2 B29	75	
(2) RRH 2x60W-1900MHz	98	RRUS-32 B30	75	
(2) HBXX-6517DS-A2M w/ Mount Pipe	98	(2) DC6-48-60-18-8F	75	
Platform Mount (LP 102-1)	98	(4) HPA-65R-BUU-H8 w/ Mount Pipe	75	
LLPX310R W/ Mount Pipe	85	KRF 102 361/1	75	
LLPX310R W/ Mount Pipe	85	(3) RRU-11	75	
LLPX310R W/ Mount Pipe	85	(2) RRUS 12-B2	75	
FDD_R6_RRH	85	(2) RRUS A2	75	
FDD R6 RRH	85	RRUS E2 B29	75	
FDD_R6_RRH	85	RRUS-32 B30	75	
Platform Mount [LP 601-1]	85	DC6-48-60-18-8F	75	
6' x 2" Mount Pipe	85	Platform Mount [LP 1303-1]	75	
6' x 2" Mount Pipe	85	(4) HPA-65R-BUU-H8 w/ Mount Pipe	75	
6' x 2" Mount Pipe	85	KRF 102 361/1	75	
VHLP2-23	85	(3) RRU-11	75	

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi	Reinf 53 50 ksi	54 ksi	67 ksi
Reinf 52,33 ksi	52 ksi	66 ksi	Reinf 56 10 ksi	56 ksi	71 ksi
Reinf 52 70 ksi	53 ksi	66 ksi			

TOWER DESIGN NOTES

- Tower is located in Hartford County, Connecticut.
 Tower designed for a 80 mph basic wind in accordance with the TIA/EIA-222-F Standard.
 Tower is also designed for a 38 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
 Deflections are based upon a 50 mph wind.
- 5. TOWER RATING: 88.1%



Paul J Ford and Company 250 E. Broad Street Suite 600 Columbus, OH 43215 Phone: 614-221-6679 FAX: 614-448.4105

ob: 100' MP; HRT	096 943227; Windsor, C	CT CT
Project PJF# 37514-252	22.001.7700 (BU# 806371)	
Client: CCI	Drawn by: Corey McCartney	App'd:
Code: TIA/EIA-222-F	Date: 11/24/14	Scale: NTS
Path:		Dwg No. F-1



Job Number: 37514-2522.001.7700 Site Number: 806371

Site Name: HRT 096 943227 Page: By: Date:

CMM 11/24/2014

DRILLED PIER SOIL AND STEEL ANALYSIS - TIA/EIA-222-F

Unfactored Base Reactions from RISA

	Comp. (+)	l ension (-)
Moment, M =	1932.0	k-ft
Shear, V =	26.0	kips
Axial Load, P =	28.0	kips

OTM = 1938.5 0.0 k-ft @ Ground Safety Factors / Load Factors / Pactors

Tower Type =	Monopole DP
ACI Code =	ACI 318-02
Seismic Design Category =	D
Reference Standard =	TIA/EIA-222-F
Use 1.3 Load Factor?	Yes
Load Factor =	1.30

Drilled Pier Parameters

Diameter =	6	ft
Height Above Grade =	0.25	ft
Depth Below Grade =	70	ft
fc' =	3	ksi
εc =	0.003	in/in
		- 20
Mat Etdn Can Width =		ft

Mat Ftdn. Cap Length = Depth Below Grade =

Skin Friction = End Bearing = Concrete Wt. Resist Uplift =

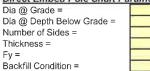
1. Ult. Skin Friction/2.00 + Ult. End Bearing/2.00

Safety Factor Φ Factor 0.75 2.00 0.75 0.75

Steel Parameters

Number of Bars =	24	1
Rebar Size =	#8	İ
Rebar Fy =	60	ksi
Rebar MOE =	29000	ksi
Tie Size =	#4	1
Side Clear Cover to Ties =	3	īn

Direct Embed Pole Shaft Parameters



Load Combinations Checked per TIA/EIA-222-F

+ Effective Soil Wt. - Buoyant Conc. Wt. ≥ Comp. 2. Ult. Skin Friction/2.00 + Buoyant Conc. Wt./1.25 ≥ Uplift 3. Ult. Skin Friction/1.50 + Buoyant Conc. Wt./1.50 ≥ Uplift

Soil Parameters

Soil Lateral Resistance =

3011 Farailleters		
Water Table Depth =	10.00	ft
Depth to Ignore Soil =	5.00	ft
Depth to Full Cohesion =	0	ft
Full Cohesion Starts at?	Ground	

Above Full Cohesion Lateral Resistance = 4(Cohesion)(Dia)(H) Below Full Cohesion Lateral Resistance = 8(Cohesion)(Dia)(H)

Maximum Capacity Ratios

Maximum Soil Ratio = 100.0% Maximum Steel Ratio = 100.0%

Define Soil Layers

Layer	Thickness ft	Unit Weight pcf	Cohesion psf	Friction Angle degrees	Soil Type	Ultimate End Bearing psf	Comp. Ult. Skin Friction psf	Tension Ult. Skin Friction psf	Depth ft
1	5	110	0	30	Sand	0	0		5
2	5	110	0	30	Sand	840	480		10
3	25	.115	300	-0	Clay	0	200		35
4	5	100	0	25	Sand	150	370		40
5	10	105	0	28	Sand	1720	660		50
6	5	110	0	30	Sand	480	1070		55
7	10	105	0	28	Sand	60	740		65
8	4	105	0	28	Sand	0	770		69
9	11	105	00	28	Sand	0	780		70
10									
11									
12									

Soil Results: Overturning

Con moderno, Croma	
Depth to COR =	54.48 ft, from Grade
Bending Moment, M =	3355.06 k-ft, from COR
Resisting Moment, Ma =	34146.04 k-ft, from COR

9.8%

MOMENT RATIO =

OK

Shear, V = 26.00 kips 264.61 kips Resisting Shear, Va =

9.8% SHEAR RATIO =

Soil Results: Compression

Soil Results: Uplift

0.0%	OK
153.6	7 kips
	00 kips
	153.€

Compression, C = Allowable Comp. Cap., Ca = วร

COMPRESSION RATIO =

28.00 kips

224.29 kips

OK

12.5% OK

Steel Results (ACI 318-02):

Minimum Steel Area =	13.57	sg in
Actual Steel Area =	18.96	sq In

Allowable Min Axial, Pa = -787.57 kips, Where Ma = 0 k-ft Allowable Max Axial, Pa = 4588.63 kips, Where Ma = 0 k-ft Axial Load, P = Moment, M = Allowable Moment, Ma =

74.81 kips @ 27.50 ft Below Grade 2329.35 k-ft @ 27.50 ft Below Grade 2146.01 k-ft

SEE ATTACHED L-PILE CALCULATIONS

LPile Plus for Windows, Version 6 (6.0.22)

Analysis of Individual Piles and Drilled Shafts Subjected to Lateral Loading Using the p-y Method

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This program is licensed to:

Paul J Ford and Company Paul J Ford and Company

Files Used for Analysis

Path to file locations: T:\375 Crown Castle\2014\37514-2522 BU 806371\WO 965888 BU 806371 SDD 001\LPile\

Name of input data file: 37514-2522.lp6d
Name of output report file: 37514-2522.lp6o
Name of plot output file: 37514-2522.lp6p
Name of runtime messeage file: 37514-2522.lp6r

Date and Time of Analysis

Date: November 24, 2014 Time: 12:39:04

Problem Title

Project Name: 806371, HRT 096 943227

Job Number: 37514-2522

Client: Crown Castle

Engineer: RH

Description: 100-ft Pole

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes nonlinear bending stiffness and nominal moment capacity with pile response computed using nonlinear EI

Computation Options:

- Only internally-generated p-y curves used in analysis
- Analysis does not use p-y multipliers (individual pile or shaft action only)
- Analysis assumes no shear resistance at pile tip

37514-2522.lp6o

- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix elements
- Output pile response for full length of pile
- Analysis assumes no soil movements acting on pile
- No p-y curves to be computed and output for user-specified depths

Solution Control Parameters:

- Number of pile increments
- 100
- Maximum number of iterations allowed
- 100
- Deflection tolerance for convergence
 Maximum allowable deflection
- = 1,0000E-04 in = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections

= 1

Total Pile Length

70.00 ft

Depth of ground surface below top of pile

- 0.25 ft

Slope angle of ground surface

0.00 deg.

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth	Pile
	X	Diameter
	ft	in
	-	
1	0.00000	72.0000000
2	70.000000	72.0000000

Input Structural Properties:

Pile Section No. 1:

Section Type Section Length Section Diameter Drilled Shaft (Bored Pile)

= 70.000 ft = 72.000 in

Ground Slope and Pile Batter Angles

Ground Slope Angle

0.000 degrees

0.000 radians

Pile Batter Angle

0.000 degrees

0.000 radians

Soil and Rock Layering Information The soil profile is modelled using 7 layers Layer 1 is soft clay, p-y criteria by Matlock, 1970 Distance from top of pile to top of layer 0.250 ft Distance from top of pile to bottom of layer 5.250 ft Layer 2 is sand, p-y criteria by Reese et al., 1974 5.250 ft Distance from top of pile to top of layer 10.250 ft Distance from top of pile to bottom of layer p-y subgrade modulus k for top of soil layer 25.000 lbs/in**3 25.000 lbs/in**3 p-y subgrade modulus k for bottom of layer Layer 3 is soft clay, p-y criteria by Matlock, 1970 10.250 ft Distance from top of pile to top of layer Distance from top of pile to bottom of layer 35.250 ft Layer 4 is sand, p-y criteria by Reese et al., 1974 35.250 ft Distance from top of pile to top of layer Distance from top of pile to bottom of layer 40.250 ft p-y subgrade modulus k for top of soil layer 20.000 lbs/in**3 p-y subgrade modulus k for bottom of layer 20.000 lbs/in**3 Layer 5 is sand, p-y criteria by Reese et al., 1974 Distance from top of pile to top of layer 40.250 ft Distance from top of pile to bottom of layer 50.250 ft 20.000 lbs/in**3 p-y subgrade modulus k for top of soil layer p-y subgrade modulus k for bottom of layer 20.000 lbs/in**3 Layer 6 is sand, p-y criteria by Reese et al., 1974 Distance from top of pile to top of layer 50.250 ft Distance from top of pile to bottom of layer 55.250 ft p-y subgrade modulus k for top of soil layer 60,000 lbs/in**3 60.000 lbs/in**3 p-y subgrade modulus k for bottom of layer Layer 7 is sand, p-y criteria by Reese et al., 1974 Distance from top of pile to top of layer 55.250 ft Distance from top of pile to bottom of layer 85.250 ft p-y subgrade modulus k for top of soil layer 20.000 lbs/in**3 p-y subgrade modulus k for bottom of layer 20,000 lbs/in**3 (Depth of lowest layer extends 15.25 ft below pile tip) Effective Unit Weight of Soil vs. Depth Effective unit weight of soil with depth defined using 14 points

Depth X Eff. Unit Weight

pcf

Point No.

ft

Page 3

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			3/3/17-2322.ipt
1	0.25	110.00000	
2	5.25	110.00000	
3	5.25	110.00000	
4	10.25	110.00000	
5	10.25	53.00000	
6	35.25	53.00000	
7	35.25	38.00000	
8	40.25	38.00000	
9	40.25	43.00000	
10	50.25	43.00000	
11	50.25	48.00000	
12	55.25	48.00000	
13	55.25	43.00000	
14	85.25	43.00000	

Summary of Soil Properties

Laye Ema	ss krm Test Type	Depth Test Prop. Ela	as. Subgr.			,-	RQD	•	.,	Rock
Nur —	n. (p-y Curve Criteria pci) ft	Wt., pcf	psf	Ang., deg.	psi	percent	pci	i psi	
1	Soft Clay	0.250	110.000	1.00E-03	-	-	- (0.00 –		 /
_		5.250 11	0.000 1.0	00E-03		:==	0.00		: 	300
2	Sand (Reese, et al.)	5.250	110.000	0 –	30.000	-	•••	- 25.000) :=:	=
		10.250 11	0.000 -	- 30	.000 –	2=	_	25.000 -		
3	Soft Clay	10.250	53.000	300.000	-	=	- 0.0	03000 -	-	-
		35.250 5	3.000 30	00.000		-	0.030	00 –		
4	Sand (Reese, et al.)	35.250	38.000	D –	25.000	-	-	- 20.000) ==	-
	T. T. T.	40.250 3	8.000 –	25.0	000 –		-	20.000 -	-	
5	Sand (Reese, et al.)	40.250	43.000	0 –	28.000	=	-	- 20.000) =	-
_		50.250 4	3.000 –	28.0	000 –	=	_	20.000 -	_	
6	Sand (Reese, et al.)	50.250	48.000	O –	30.000	-	-	- 60,000) =	-
=		55.250 4	8.000 –	30.0	000 -	=	-	60.000 -	-	
7	Sand (Reese, et al.)	55.250	43.000	0 -	28.000	=	_	- 20.000) =	-
		85.250 4	3.000	28.0	000 –	+62	-	20.000 -	-	

l	oading.	Type		

Static loading criteria were used when computing p-y curves for all analyses.

Number of loads specified = 1

Load Load Condition 1 Condition 2 Axial Thrust

No. Type Force, lbs

1 1 V = 26000.000 lbs M = 23184000.000 in-lbs 28000.000

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applie to pile head

Axial thrust is assumed to be acting axially

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Dimensions and Properties of Drilled Shaft:

Length of Section 70.00000000 ft Shaft Diameter 72.00000000 in Concrete Cover Thickness 3.00000000 in 24 bars Number of Reinforcing Bars 60.00000000 ksi **Yield Stress of Reinforcing Bars** Modulus of Elasticity of Reinforcing Bars 29000. ksi 4071.50407905 sq. in. Gross Area of Shaft Total Area of Reinforcing Steel 18.96000000 sq. in. Area Ratio of Steel Reinforcement 0.47 percent 7.48420249 in Edge-to-Edge Bar Spacing

Axial Structural Capacities:

Nom. Axial Structural Capacity = 0.85 Fc Ac + Fy As = 11471.588 kips
Tensile Load for Cracking of Concrete - -1530.869 kips
Nominal Axial Tensile Capacity - 1137.600 kips

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches
1	1.00000	0.79000	32.50000	0.00000
2	1.00000	0.79000	31.39259	8.41162
3	1.00000	0.79000	28.14583	16.25000
4	1.00000	0.79000	22.98097	22.98097
5	1.00000	0.79000	16.25000	28.14583
6	1.00000	0.79000	8.41162	31.39259
7	1.00000	0.79000	0.00000	32.50000
8	1.00000	0.79000	-8.41162	31.39259
9	1.00000	0.79000	-16.25000	28.14583

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10	1.00000	0.79000	-22.98097	22.98097
11	1.00000	0.79000	-28.14583	16.25000
12	1.00000	0.79000	-31.39259	8.41162
13	1.00000	0.79000	-32.50000	0.00000
14	1.00000	0.79000	-31.39259	-8.41162
15	1.00000	0.79000	-28.14583	-16.25000
16	1.00000	0.79000	-22.98097	-22.98097
17	1.00000	0.79000	-16.25000	-28.14583
18	1.00000	0.79000	-8.41162	-31.39259
19	1.00000	0.79000	0.00000	-32.50000
20	1.00000	0.79000	8.41162	-31.39259
21	1.00000	0.79000	16.25000	-28.14583
22	1.00000	0.79000	22.98097	-22.98097
23	1.00000	0.79000	28.14583	-16.25000
24	1.00000	0.79000	31.39259	-8.41162

Concrete Properties:

Compressive Strength of Concrete	= 3.0000000 ksi
Modulus of Elasticity of Concrete	= 3122.0185778 ksi
Modulus of Rupture of Concrete	= -0.4107919 ksi
Compression Strain at Peak Stress	= 0.0016336
Tensile Strain at Fracture of Concrete	→ -0.0001160
Maximum Coarse Aggregate Size	- 0.7500000 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings - 1

Number	Axial Thrust Force kips
1	28.000

Definitions of Run Messages and Notes:

C = concrete in section has cracked in tension

 Y = stress in reinforcing steel has reached yield stress
 T = tensile strain in reinforcement exceeds 0.005 when compressive strain in concrete is less than 0.003.

Z = depth of tensile zone in concrete section is less than 10 percent of section depth

Bending Stiffness (EI) = Bending Moment / Curvature

Position of neutral axis is computed from compression side of pile

Compressive stresses are positive in sign. Tensile stresses are negative in sign.

Axial Thrust Force = 28.000 kips

Bending Curvature rad/in.	Bendir Mome in-kip	_	iffness	Depth to N Axis in/in	Max Cor Strain in/in		Fens Max Co Stress Stre ksi	ncrete Max S ss Msg	teel Run
0.0000004	17 2118	.368746	0 508408	34990. 40).3703974	0.000016	 58 -0.000013	2 0.060919	0.4834590
0.00000083	33 4224	.482821	7 506937	9386. 38	3.1934538	0.000031	18 -0.000028	2 0.114683	0.9143085
0.00000129	50 6318	.114179.	5 505449	1344. 37	7.4678612	0.000046	58 -0.000043	2 0.167950	9 1.3451600
0.00000160	67 8399	.262378	6 503955	7427. 37	7.1050991	0.000061	8 -0.000058	2 0.220722	25 1.7760131
0.0000020	33 1	0468. 5	02460514	1. 36.88	74687 C	0.0000768	-0.0000732	0.2729980	2.2068678
0.00000250	00 1	2524. 5	00964365	8. 36.74	24035 0	.0000919	-0.0000881	0.3247774	2,6377242
0.0000029	17 1	4568. 4	99467691	9. 36.63	88045 0	0.0001069	-0.0001031	0.3760606	3.0685822
0.00000333	33 1	4568. 4	37034230	4. 17.13	91754 0	.0000571	-0.0001829	0.2019141	-5.2684131 C
0.00000375	50 1	4568. 3	88474871	5. 16.85	59010 0	.0000632	-0.0002068	0.2229062	-5.9577708 C
0.00000410	57 1	4568. 3	49627384	3. 16.62	09959 0	.0000693	-0.0002307	0.2436976	-6.6481297 C
					n				

37514-2522.lp6o 0.0000753 -0.0002547 0.2644238 -7.3383823 C 14568. 3178430767. 16.4295999 0.000004583 -8.0285285 C 0.000005000 14568. 2913561536. 16.2708381 0.0000814 -0.0002786 0.2850845 -8.7191061 C 14568, 2689441418. 16.1337539 0.0000874 -0.0003026 0.3056152 0.000005417 0.3260142 -9,4101333 C 0.0000934 -0.0003266 14568. 2497338460. 16.0135959 0.000005833 0.3463488 -10.1010500 C 14568. 2330849229. 15.9100690 0.0000994 -0.0003506 0.000006250 15.8200566 0.0001055 -0.0003745 0.3666190 -10.7918557 C 0.000006667 14568. 2185171152. -0.0003985 0.3868247 -11.4825501 C 2056631673. 15.7411757 0.0001115 0.000007083 14568. 0.000007500 14568. 1942374357. 15.6715725 0.0001175 -0.0004225 0.4069656 -12.1731330 C 14568. 1840144128. 15.6097838 0.0001236 -0.0004464 0.4270418 -12.8636038 C 0.000007917 0.0001296 -0.0004704 0.4470531 -13.5539622 C 14568. 1748136922. 15.5546390 0.000008333 0.4669994 -14.2442079 C 0.000008750 14568, 1664892306. 15.5051903 0.0001357 -0.0004943 0.0001417 -0.0005183 0.4868464 -14.9346351 C 15.4595542 0.000009167 14568, 1589215383. 15.4169957 0.0001477 -0.0005423 0.5065868 -15.6253099 C 14568. 1520119062. 0.000009583 14568. _ 1456780768. _ 15.3783930 0.0001538 -0.0005662 0.5262630 -16.3158660 C 0.0000100 14568. 1398509537. 15.3432728 0.0001598 -0.0005902 0.5458748 -17.0063030 C 0.0000104 -0.0006141 0.5654223 -17.6966204 C 0.0000108 14568. 1344720709. 15.3112347 0.0001659 0.5849053 -18.3868179 C 15.2819375 0.0001719 -0.0006381 0.0000113 14568. 1294916238. 15.2550887 0.0001780 -0.0006620 0.6043236 -19.0768949 C 0.0000117 14568. 1248669230. 14568. 1205611670. 15.2304364 0.0001840 -0.0006860 0.6236771 -19.7668512 C 0.0000121 -20.4566862 C 0.0001901 -0.0007099 0.6429658 0.0000125 14568. 1165424614. 15.2077621 0.6621894 -21.1463995 C 15.1868754 0.0001962 -0.0007338 14568. 1127830272. 0.0000129 -0.0007578 -21.8359908 C 14568. 1092585576. 15.1676100 0.0002022 0.6813480 0.0000133 15.1498196 0.0002083 -0.0007817 0.7004413 -22.5254594 C 0.0000138 14568. 1059476922. -0.0008056 0.7194692 -23.2148054 C 0.0000142 14568. 1028315836. 15.1333751 0.0002144 15.1181621 0.0002205 -0.0008295 0.7384317 -23.9040276 C 0.0000146 14568. 998935384. 15.1040792 0.0002266 -0.0008534 0.7573286 -24.5931258 C 971187179. 0.0000150 14568. 15.0910356 0.0002327 -0.0008773 0.7761598 -25.2820997 C 944938877. 0.0000154 14568. 0.7949251 -25.9709488 C 0.0000158 14568. 920072064. 15.0789504 0.0002388 -0.0009012 0.0002449 -0.0009251 0.8136244 -26.6596727 C 0.0000163 14568. 896480473. 15.0677508 15.0477527 0.0002571 -0.0009729 0.8508248 -28.0367424 C 852749718. 0.0000171 14568. 15.0305901 0.0002693 -0.0010207 0.8877598 -29.4133058 C 0.0000179 14568. 813086940. 776949743. 15.0158918 0.0002815 -0.0010685 0.9244284 -30.7893588 C 0.0000188 14568. -0.0011162 0.9608296 -32.1648979 C 0.0000196 14568. 743888052. 15.0033500 0.0002938 0.9969624 -33.5399183 C 0.0000204 14568. 713525274. 14.9927071 0.0003061 -0.0011639 14.9837462 0.0003184 -0.0012116 1.0328258 -34.9144166 C 0.0000213 14568. 685543891. -0.0012593 1.0684187 -36.2883889 C 14799. 670136049. 14.9762831 0.0003307 0.0000221 -37.6618310 C 0.0000229 15328. 668861840. 14.9701604 0.0003431 -0.0013069 1.1037401 1.1387888 -39.0347388 C 0.0003554 -0.0013546 0.0000238 15857. 667656806. 14.9652432 14.9614145 0.0003678 -0.0014022 1.1735638 -40.4071082 C 666513783. 0.0000246 16385. 1.2080639 -41,7789350 C 0.0000254 16913. 665426542. 14.9585731 0.0003802 -0.0014498 664389646. 14,9566307 0.0003926 -0.0014974 1.2422881 -43.1502149 C 0.0000263 17440. -0.0015450 1.2762353 -44.5209434 C 0.0000271 17967. 663398322. 14.9555096 0.0004050 -0.0015925 1.3099043 -45.8911163 C 0.0004175 0.0000279 18493. 662448368. 14.9551419 661536068. 14.9554674 0.0004300 -0.0016400 1.3432939 -47.2607289 C 19019. 0.0000288 0.0000296 19544. 660658120. 14.9564329 0.0004425 -0.0016875 1.3764030 -48.6297769 C 1.4092305 0.0004550 -0.0017350 -49.9982555 C 0.0000304 20069. 659811586. 14.9579909 0.0004675 1.4417751 -51.3661601 C 14.9600991 -0.0017825 20594. 658993837. 0.0000313 1.4740356 -52.7334859 C 0.0000321 21117. 658202518. 14.9627200 0.0004801 -0.0018299 14.9658194 0.0004926 -0.0018774 1.5060108 -54.1002282 C 0.0000329 21641. 657435509. 0.0000338 22163. 656690898. 14.9693671 0.0005052 -0.0019248 1.5376994 -55.4663819 C -0.0019722 1.5691004 -56.8319423 C 655966957. 14.9733356 0.0005178 0.0000346 22686. -58.1969041 C 14.9777000 0.0005305 -0.0020195 1.6002122 655262118. 0.0000354 23207. 0.0005431 -0.0020669 1.6310338 -59.5612623 C 0.0000363 23728. 654574957. 14.9824379 -60.0000000 CY 0.0000371 24249. 653904174. 14.9875290 0.0005558 -0.0021142 1.6615638 653248585. 14.9929549 0.0005685 -0.0021615 1.6918008 -60.0000000 CY 0.0000379 24769. 0.0005811 -0.0022089 1.7215444 -60.0000000 CY 652321812. 14.9965548 0.0000387 25277. -0.0022566 1.7500225 -60.0000000 CY 0.0000396 25731. 650056374. 14,9901611 0.0005934 14.9662145 0.0006049 -0.0023051 1.7764914 -60.0000000 CY 0.0000404 26090. 645514580. 1.8026804 -60.0000000 CY 0.0000412 26446. 641103418. 14.9432703 0.0006164 -0.0023536 -0.0024022 1.8282346 -60.0000000 CY 0.0000421 26781. 636371845. 14.9175966 0.0006278 0.0006386-0.0024514 1,8523531 -60,0000000 CY 0.0000429 27052. 630342965. 14.8810188 0.0006494 -0.0025006 1.8759734 -60.0000000 CY 0.0000437 27309. 624202170. 14.8433187 0.0000446 27565. 618285127. 14.8073180 0.0006602 -0.0025498 1.8993769 -60.0000000 CY -60.0000000 CY 0.0006709 -0.0025991 1.9225627 0.0000454 27821. 612579488. 14.7729247 0.0006817 -0.0026483 1.9453881 -60.0000000 CY 607067868. 14.7386423 0.0000462 28077. 0.0000471 28297. 601002335. 14.6976467 0.0006920 -0.0026980 1.9671650 -60,0000000 CY

		55.445.5465		7514-2522.lp			60 0000000 CV
0.0000479	28469.	59413 <i>7</i> 189.	14.6482065	0.0007019	-0.0027481	1.9877058	-60,0000000 CY
0.0000487	28641.	587503119.	14.6006772	0.0007118	-0.0027982	2.0080630	-60.0000000 CY
0.0000496	28812.	581088456.	14.5549635	0.0007217	-0.0028483	2.0282360	-60.0000000 CY
0.0000529	29497.	557416226.	14.3885698	0.0007614	-0.0030486	2.1070744	-60.0000000 CY
0.0000562	30046.	534157192.	14.2172188	0.0007997	-0.0032503	2.1799146	-60.0000000 CY
0.0000596	30472.	511419370.	14.0432597	0.0008367	-0.0034533	2.2472703	-60.0000000 CY
0.0000629	30891.	490987165.	13.8779490	0.0008732	-0.0036568	2.3106567	-60.0000000 CY
0.0000662	31308.	472566398.	13.7310792	0.0009097	-0.0038603	2.3714568	-60.0000000 CY
0.0000696	31603.	454169685.	13.5727462	0.0009444	-0.0040656	2.4266009	-60.0000000 CY
0.0000729	31841.	436682002.	13.4184253	0.0009784	-0.0042716	2.4780453	-60.0000000 CY
0.0000762	32077.	420685117.	13.2756965	0.0010123	-0.0044777	2.5268610	-60.0000000 CY
0.0000796	32308.	405968188.	13.1386262	0.0010456	-0.0046844	2.5725859	-60.0000000 CY
0.0000829	32538.	392418644.	13.0141324	0.0010791	-0.0048909	2.6161572	-60.0000000 CY
0.0000862	32766.	379900860.	12.9007812	0,0011127	-0.0050973	2.6575493	-60.0000000 CY
0.0000896	32968.	368013588.	12.7905569	0.0011458	-0.0053042	2.6960248	-60,0000000 CY
0.0000929	33102.	356252709.	12.6723103	0.0011775	-0.0055125	2.7305813	-60,0000000 CY
0.0000929	33220.	345139481.	12.5560554	0.0011775	-0.0057215	2.7624371	-60.0000000 CY
0.0000996	33333.	334728135.	12.4419144	0.0012390	-0.0059310	2.7917434	-60.0000000 CY
	333436.	324982745.		0.0012596	-0.0059310	2.8192234	-60.0000000 CY
0.0001029			12.3362701		-0.0063497	2.8448561	-60.0000000 CY
0.0001063	33558.	315840494. 307246189.	12.2383378	0.0013003	-0.0065588	2.8686198	-60.0000000 CY
0.0001096	33669.		12.1474290	0.0013312			
0.0001129	33779.	299151151.	12.0629369	0.0013621	-0.0067679	2.8904923	-60.0000000 CY
0.0001163	33888.	291512281.	11.9843249	0.0013932	-0.0069768	2.9104510	-60.0000000 CY
0.0001196	33996.	284291282.	11.9111169	0.0014244	-0.0071856	2.9284728	-60.0000000 CY
0.0001229	34102.	277439502.	11.8385377	0.0014552	-0.0073948	2.9442664	-60.0000000 CY
0.0001263	34205.	270930552.	11.7673244	0.0014856	-0.0076044	2.9579571	-60.0000000 CY
0.0001296	34302.	264713087.	11.6990965	0.0015160	-0.0078140	2.9696889	-60.0000000 CY
0.0001329	34362.	258520192.	11.6224447	0.0015448	-0.0080252	2.9790250	
0.0001363	34414.	252576364.	11.5480367	0.0015734	-0.0082366	2.9865969	-60.0000000 CY
0.0001396	34460.	246878662.	11.4763970	0.0016019	-0.0084481	2.9924601	-60,0000000 CY
0.0001429	34506.	241442260.	11.4088807	0.0016305	-0.0086595	2,9966621	-60,0000000 CY
0.0001462	34551.	236249203.	11.3452170	0.0016592	-0.0088708	2.9991822	-60,0000000 CY
0.0001496	34596.	231283084.	11.2851652	0.0016881	-0.0090819	2.9998621	-60.0000000 CY
0.0001529	34640.	226527247.	11.2286871	0.0017171	-0.0092929	2.9940916	-60.0000000 CY
0.0001562	34683.	221970507.	11.1753106	0.0017461	-0.0095039	2.9964535	-60.0000000 CY
0.0001596	34723.	217587076.	11.1197911	0.0017745	-0.0097155	2.9988933	-60.0000000 CY
0.0001629	34762.	213374247.	11.0651099	0.0018027	-0.0099273	2.9999477	-60.0000000 CY
0.0001662	34800.	209325291.	11.0135487	0.0018310	-0.0101390	2.9962832	-60.0000000 CY
0.0001696	34838.	205432247.	10.9646846	0.0018594	-0.0103506	2.9929159	-60.0000000 CY
0.0001729	34875.	201686842.	10.9182582	0.0018879	-0.0105621	2.9963654	-60.0000000 CY
0.0001762	34912.	198080657.	10.8741397	0.0019166	-0.0107734	2.9986819	-60.0000000 CY
0.0001796	34948.	194605893.	10.8322095	0.0019453	-0.0109847	2.9998507	-60.0000000 CY
0.0001829	34984.	191253980.	10.7925687	0.0019741	-0.0111959	2.9976462	-60.0000000 CY
0.0002029	35188.	173410924.	10.5922454	0.0021493	-0.0124607	2.9990789	60.0000000 CY
0.0002229	35366.	158653322.	10.4371221	0.0023266	-0.0137234	2.9990414	60,0000000 CY
0.0002429	35433.	145865123.	10.2465112	0.0023200	-0.0150010	2.9872583	60.0000000 CY
0.0002429	35487.	134972462.	10.0869532	0.0024530	-0.0162780	2.9994217	60.0000000 CY
0.0002829	35536.	125605402.	9.9570219	0.0028170	-0.0175530	2.9868935	60.0000000 CY
0.0002829	35583.	117467375.	9.8488371	0.0028170	-0.0188266	2.9948273	60.0000000 CY
0.0003029		110322368.	9,7607759	0.0029634	-0.0200981	2.9985234	60.0000000 CY
	35625.	10322366.		0.0031313	-0.0200381	2.9828277	60.0000000 CY
0.0003429	35657.		9.6848053			2.9874128	60.0000000 CY
0.0003629	35686.	98330888.	9.6096316	0.0034875	-0.0226425	2.9978382	60.0000000 CY
0.0003829	35709.	93254363.	9.5515760	0.0036575	-0.0239125		
0.0004029	35728.	88674429.	9.5046155	0.0038296	-0.0251804	2.9957918	60.0000000 CY

Summary of Results for Nominal (Unfactored) Moment Capacity for Section 1

Moment values interpolated at maximum compressive strain = 0.003 or maximum developed moment if pile fails at smaller strains.

Load Axial Thrust Nominal Mom. Cap. Max. Comp. No. kips in-kip Strain 1

0.00300000

Note note that the values of moment capacity in the table above are not factored by a strength reduction factor (phi-factor).

In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are spirals or tied hoops.

The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08, Section 9.3.2.2 or the value required by the design standard being followed.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Horizontal shear force at pile head Applied moment at pile head Axial thrust load on pile head

- 26000.000 lbs
- = 23184000,000 in-lbs
- = 28000.000 lbs

Depth Deflect. Bending Shear Slope Total Bending Soil Res. Soil Spr. Distrib. X y Moment Force S Stress Stiffness p Es*h Lat. Load inches inches in-lbs lbs radians psi* lb-in^2 lb/in lb/inch lb/inch	
0.00 2.0706 23184000, 26000, -0.0123 0.000 6.550E+11 0.000 0.000 0.000	
****	000
	.000
	.000
	.000
	.000
	.000
	.000
	0.000
75.600 1.2436 25164583, 235330.009522 0.000 6.525E+11 -355.7429 2402.9566	0.000
	0.000
92.400 1.0891 25496592. 136080.008869 0.000 6.512E+11 -800.6744 6175.6151	0.000
100.800 1.0160 25584699. 6211.9968 -0.008539 0.000 6.508E+11 -960.2704 7939.6151	0.000
109.200 0.9456 256049712409.0604 -0.008209 0.000 6.507E+11 -1092.3623 9703.6151	0.000
	0.000
126.000 0.8133 25406547183340.007550 0.000 6.517E+11 -301.8749 3118.0436	0.000
134.400 0.7512 25243629208660.007224 0.000 6.524E+11 -301.0672 3366.5429	0.000
142.800 0.6919 25059391233900.006900 0.000 6.527E+11 -299.8069 3639.8498	0.000
151.200	0.000
159.600 0.5814 24627347283960.006261 0.000 6.534E+11 -295.8962 4275.3330	0.000
168.000 0.5301 24379818308700.005946 0.000 6.537E+11 -293.2278 4646.4744	0.000
176.400	0.000
184.800	0.000
193.200 0.3920 23513577381270.005023 0.000 6.549E+11 -281.5867 6034.2205	0.000
201.600 0.3511 23184523404500.004724 0.000 6.553E+11 -271.4246 6494.5343	0.000
210.000 0.3126 22836248426860.004429 0.000 6.558E+11 -261.1354 7016.4185	0.000
218.400 0.2767 22469477448360.004139 0.000 6.563E+11 -250.7088 7612.1656	0.000
226.800	0.000
235,200 0.2119 21683411488700.003574 0.000 6.574E+11 -229.3912 9092.7267	0.000
	0.000
	0.000
	0.000
	0.000
	0.000
	0.000
294.000 0.0560 18462006600150.001780 0.000 6.625E+11 -147.2405 22067. 0	0.000

37514-2522.lp6o 0.0421 17953074. -61196. -0.001549 0.000 6.634E+11 -133.8197 26713. 0.000 302.400 310.800 0.0300 17434647. -62260. -0.001325 0.000 6.644E+11 -119.5685 33456. 0.000 0.0198 16907731. -63199. -0.001108 0.000 6.654E+11 -104.0937 44130. 0.000 319.200 0.0114 16373421. -64000. -0.000899 0.000 6.665E+11 -86.5574 0.000 63784. 336.000 0.004718 15832954. -64634. -0.000696 0.000 6.677E+11 -64.4592 114772. 0.000 344,400 -0.000291 15287892. -64796. -0.000500 0.000 6.690E+11 26.0129 752042. 0.000 352.800 -0.003686 14744620. -64436. -0.000358 0.000 1.329E + 1259.5402 135676. 0.000 361.200 -0.006299 14205528. -63888. -0.000291 $0.000 \ 3.026E + 12$ 71.0668 94770. 0.000 77119. 0.000 5.001E+12 78.7769 369,600 -0.008581 13671441. -63259. -0.000260 0.000 -0.0107 13142907. -62572. -0.000238 0.000 5.005E + 12 84.709066692. 0.000 378,000 386.400 -0.0126 12620345, -61840, -0.000216 0.000 5.009E+12 89.4722 59778. 0.000 -0.0143 12104091. -61072. -0.000195 0.000 5.012E + 12 93.390554865. 0.000 394.800 -0.0159 11594422. -60274. -0.000175 0.000 5.016E+12 96.6601 51216. 0.000 403.200 -0.0172 11091568. -59451. -0.000156 411.600 0.000 5.019E+12 99.4098 48421. 0.000 420.000 -0.0185 10595725. -58606. -0.000138 0.000 5.024E+12 101.7301 46237. 0.000 -0.0196 10107055. -57799. -0.000121 0.0005.027E + 1290.4531 38827. 0.000 428,400 436.800 -0.0205 9624764. -57006. -0.000105 0.000 5.030E+12 98.2697 40238. 0.000 -0.0213 9149403. -56149. -8.885E-05 0.000 5.033E+12 105.7346 41649. 0.000 445.200 0.000 453.600 -0.0220 8681499, -55231.-7.397E-05 0.000 5.037E+12 112.8142 43061. 462,000 -0.0226 8221552, -54256, -5.988E-05 0.000 5.041E+12 119.4793 44472. 0.000 470.400 -0.0230 7770032. -53226, -4.656E-05 0.000 5.043E+12 125.7040 45883. 0.000 -52146. -3.399E-05 0.000 5.046E+12 131.4664 47294. 0.000 478.800 -0.0233 7327379. -51076. -2.216E-05 0.000 5.049E+12 123.1534 43863. 0.000 487.200 -0.0236 6893999. 495.600 -0.0237 6469307. -50022. -1.105E-05 0.000 5.053E+12 127.8593 45275. 0.000 504.000 -0.0238 6053633. -48930, -6.435E-07 0.000 5.056E+12 132.1095 46686. 0.000 -47805. 9.075E-06 512.400 -0.0237 5647279. 0.000 5.058E+12 135.8919 48097. 0.000 0.000 5.061E+12 139.1976 0.000 -0.0236 5250511. -46649, 1.812E-05 49508. 520.800 529.200 -0.0234 4863562. -45468. 2.651E-05 0.000 5.063E+12 142.0208 50919, 0.000 -0,0232 4486633, -44265, 3,427E-05 0.000 5.067E+12 144.3582 52331. 0.000 537,600 546.000 -0.0229 4119888. -43045. 4.140E-05 0.000 5,070E+12 146,2097 53742. 0.000 -0.0225 3763458. -41811. 4.793E-05 0.000 5.071E+12 147.5775 55153. 0.000 554.400 -0.0220 3417440. -40568. 5.388E-05 0.000 5.073E+12 148.4661 56564. 0.000 562,800 -39319. 5.926E-05 -0.0216 3081896. 0.000 5.075E+12 148.8827 57975. 0.000 571.200 -0.0211 2756855. -38068. 6.409E-05 0.000 5.077E+12 148.8363 59387. 0.000 579.600 -36820. 6.839E-05 0.000 5.080E+12 148.3381 60798. 0.000 588.000 -0.0205 2442316. -35578. 7.217E-05 0.000 5.084E+12 147.4014 0.000 -0.0199 2138243. 62209. 596.400 -0.0193 1844569, -33214, 7,546E-05 0.000 5.084E+12 415.4008 180962. 0.000 604.800 -0.0186 1580205. -29744. 7.829E-05 0.000 5.084E+12 410.8617 185196. 0.000 613.200 0.000 5.084E+12 405.1761 189429. -0.0180 1344831. -26317. 8.071E-05 0.000 621.600 0.000 5.084E+12 398.3862 -0.0173 1138046. -22942. 8.276E-05 193663. 0.000 630.000 -0.0166 959371. -19628. 8.449E-05 0.000 5.084E+12 390.5314 197896. 0.000 638.400 -0.0159 808251. -16385. 8.595E-05 -0.0151 684060. -13221. 8.718E-05 -0.0144 586100. -11119. 8.823E-05 -0.0137 497219, -10056. 8.913E-05 0.0005.084E + 12381.6476 202130. 0.000 646,800 655.200 0.000 5.084E+12 371.7661 206364. 0.000 0.000 5.084E+12 128.6787 0.000 75086. 663.600 0.000 5.084E+12 124.3105 76497. 0.000 672.000 680.400 -0.0129 417110, -9031.8668 8.988E-05 0.000 5.084E+12 119.6279 *77*908. 0.000 -0.0121 345442. -8047.9503 9.051E-05 0.000 5.084E+12 114.6379 79319. 0.000 688.800 -0.0114 281862. -7107.2127 9.103E-05 $0.000\ 5.084E + 12\ 109.3472$ 80730. 0.000 697.200 -0.0106 225998. -6212.1540 9.145E-05 0.000 5.084E+12 103.7620 82142. 0.000 705.600 714.000 -0.009841 177455. -5365.2243 9.179E-05 0.000 5.084E+12 97.8880 0.000 83553. 722.400 -0.009069 135819. -4568.8272 9.204E-05 0.000 5.084E+12 91.7304 84964. 0.000 730.800 -0.008295 100655. -3825.3249 9.224E-05 0.000 5.084E+12 85.2940 86375. 0.000 71510. -3137.0423 9.238E-05 0.000 5.084E+12 78.5828 87786. 0.000 739.200 -0.007519 747.600 -0.006743 47910. -2506.2719 9.248E-05 0.000 5.084E+12 71.6006 89198. 0.000 756.000 -0.005966 29361. -1935.2781 9.254E-05 0.000 5.084E+12 64.3503 90609. 0.000 0.000 5.084E+12 56.8344 764,400 -0.005188 15353. -1426.3025 9.258E-05 92020. 0.000 772.800 -0.004410 5355.7019 -981.5677 9.260E-05 0.000 5.084E+12 49.0549 93431. 0.000 781,200 -0,003632 -1180.5914 -603.2821 9.260E-05 0.0005.084E + 1241,0131 94842. 0.000 789.600 -0.002855 -4822.9974 -293.6439 9.260E-05 0.000 5.084E+12 32.7102 0.000 96254. 798.000 -0.002077 -6157,3664 -54.8444 9.259E-05 0.000 5.084E+12 24.1468 97665. 0.000 0.000 5.084E+12 806.400 -0.001299 -5787.9358 110.9287 9.258E-05 99076. 0.000 15.3230 814.800 -0.000522 -4337.3126 201.4885 9.257E-05 0.000 5.084E+12 6.2389 100487. 0.000 823,200 0.000256 -2446,4738 214,6472 9.256E-05 0.000 5.084E+12 -3.1058 101898. 0.000 831.600 0.001034 -774.7808 148.2151 9.256E-05 0.000 5.084E+12 -12.7113 103310. 0.000 0.000 5.084E+12 -22.5780 52360. 0.000 840.000 0.001811 0.000 0.000 9.256E-05

37514-2522.lp6o

* This analysis makes computations of pile response using nonlinear moment-curvature relationships. The above values of total stress are computed for combined axial stress and do not equal the actual stresses in concrete and steel in the range of nonlinear bending.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection = 2.0706211 inches

Computed slope at pile head = -0.0123168 radians

Maximum bending moment = 25604971. inch-lbs

Maximum shear force = -64796. lbs

Depth of maximum bending moment = 109.2000000 inches below pile head

Depth of maximum shear force = 344.4000000 inches below pile head

Number of iterations = 26 Number of zero deflection points = 2

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 - Shear, lbs, and Load 2 - Moment, in-lbs Load Type 2: Load 1 - Shear, lbs, and Load 2 - Slope, radians

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Pile-head Pile-head Load Load Condition 1 Condition 2 Axial Pile-head Maximum Maximum Pile-head Loading Deflection Shear Rotation Case Type V(lbs) or in-lb, rad., Moment No. No. y(inches) or in-lb/rad. lbs inches in-lbs lbs radians 26000. M = 23184000.28000. 2.07062106 25604971. -64796. -0.01231679

The analysis ended normally.

Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material

TIA Rev F

Site Data

BU#: Site Name:

App #:

Pole Manufacturer:

Qty:

Diam:

Rod Material:

Strength (Fu):

Yield (Fy):

Bolt Circle:

Single-Rod B-eff:

Config:

Other

Reactions		
Moment:	1932	ft-kips
Axial:	28	kips
Shear:	26	kips

If No stiffeners, Criteria:

AISC ASD <-Only Applicable to Unstiffened Cases

Anchor	Rod	Results

Maximum Rod Tension: Allowable Tension:

Base Plate Results

Allowable Plate Stress:

Base Plate Stress:

195.0 Kips

Anchor Rod Stress Ratio: 84.9% Pass

Rigid
Service, ASD
Efu*ASIE

	Plate Data	
Diam:	52.05	ir

2.5 Thick: in 60 Grade: ksi 10.24

Stiffener Data (Welding at both sides)

Anchor Rod Data

12

2.25

A615-J

100

75

46.05

in

ksi

ksi

in

in

Base Plate Stress Ratio:

Flexural Check

38.6 ksi 60.0 ksi

165.5 Kips

64.3% Pass

Rigid Service ASD 0.75*Fy*ASIF Y.L. Length: 25.72

Analysis Date: 11/24/2014

n/a

Stiffener Results

Horizontal Weld: n/a Vertical Weld: n/a

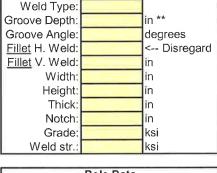
Plate Flex+Shear, fb/Fb+(fv/Fv)^2: n/a Plate Tension+Shear, ft/Ft+(fv/Fv)^2: n/a

Plate Comp. (AISC Bracket):

Pole Results

Pole Punching Shear Check:

n/a



Pole Data							
Diam:	38.2	in					
Thick:	0.344	in					
Grade:	65	ksi					
# of Sides:	12	"0" IF Round					
Fu	80	ksi					
Reinf. Fillet Weld	0	"0" if None					

Stress	Increase Factor
ASIE	1 333





^{* 0 =} none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

^{**} Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

BU NUMBER; SITE NAME BU #806371; HRT 096 943227

APP: 269459 REV. 0; WO: 965888

SITE ADDRESS

HRT 96 599 MATIANUCK AVE WINDSOR, CONNECTICUT 06095 HARTFORD COUNTY

PROJECT NOTES

- 1. DETAILED FIELD INFORMATION REGARDING INTERFERENCES AND/OR EXISTING FIELD CONDITIONS MAY BE AVAILABLE ON CROWN'S CCISITES AND FROM CONTRACTOR'S PRE-MOD MAPPING. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS AND COORDINATE WITH THE AVAILABLE SOURCES OF INFORMATION ABOVE AND WITH THE PROJECT PLANS BEFORE PROCEEDING WITH THE WORK. CONTRACTOR SHALL IMMEDIATELY REPORT ANY AND ALL DISCREPANCIES TO PAUL J. FORD AND COMPANY AND CROWN CASTLE FIELD PERSONNEL BEFORE PROCEFDING WITH THE WORK.
- ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC, 31, 2009.
- ALL STRUCTURAL BOLTS SHALL BE FIELD INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC "SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS", DEC 43, 2009.
- 4. (A.) DTI'S REQUIRED: ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND DETAILS ON SHEET S-3 FOR REQUIREMENTS ON THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.

(B.) EFFECTIVE 5/30/2012: UNTIL FURTHER NOTICE, CROWN CASTLE WILL ACCEPT AJAX BOLTS TIGHTENED USING AISC "TURN-OF-NUT" METHOD. INSTALLERS SHALL FOLLOW CROWN GUIDELINES FOR AISC "TURN-OF-NUT" METHOD AND ALSO PROVIDE COMPLETE INSPECTION DOCUMENTATION IN THE PMI. PRIOR TO STARTING WORK, CONTRACTOR SHALL CONSULT WITH CROWN ENGINEERING TO DETERMINE WHETHER THIS POLICY IS STILL IN PLACE.

(C.) REQUIREMENT EFFECTIVE 04/20/2013, PER CROWN CASTLE DIRECTIVE: ANY AND ALL STRUCTURAL BOLTS THAT ARE TIGHTENED TO THE PRETENSIONED CONDITION USING THE AISC "TURN-OF-NUT" TENSIONING PROCEDURE (NON-TENSION CONTROLLED [NON-TC] BOLTS AND/OR BOLTS WITHOUT DITS INSTALLED) SHALL BE INSPECTED ONSITE BY AN INDEPENDENT THIRD-PARTY BOLT INSPECTOR, AS APPROVED BY CROWN, THIS INSPECTION IS REQUIRED TO BE AN ONSITE FIELD INSPECTION. THE THIRD-PARTY BOLT INSPECTOR SHALL FOLLOW THE PUBLISHED CROWN CASTLE INSPECTION PROCEDURE" IN NON-TC BOLT INSPECTION", DATED APRIL 2013, THE THIRD-PARTY BOLT INSPECTOR SHALL PREPARE A FULLY DOCUMENTED BOLT INSPECTION REPORT, AS SPECIFIED BY CROWN, AND SHALL SUBMIT A COPY OF THE BOLT INSPECTION REPORT TO THE MI INSPECTOR, THE EOR, AND TO CROWN CASTLE.

5. NDE OF THE CIRCUMFERENTIAL WELD OF THE BASE PLATE TO SHAFT CONNECTION IS REQUIRED. SEE CCI DOCUMENTS ENG-SOW-1033 'TOWER BASE PLATE NDE AND ENG-BUL-10051 'NDE REQUIREMENTS FOR MONOPOLE BASE PLATE TO PREVENT CONNECTION FAILURE', NOTIFY THE EOR AND CROWN ENGINEERING IMMEDIATELY IF ANY CRACKS ARE SUSPECTED OR HAVE BEEN IDENTIFIED. THE NDE SHALL INCLUDE ALL EXISTING REINFORCEMENTS THAT HAVE BEEN WELDED TO THE BASE PLATE, ANY FULL PENETRATION WELDING TO THE BASE PLATE REQUIRED AS PART OF THIS ACTIVE REINFORCEMENT DESIGN SHALL BE INCLUDED IN THE NDE SCOPE OF WORK.

PROJECT CONTACTS:

MONOPOLE OWNER:

CROWN CASTLE

3530 TORINGDON WAY SUITE 300 CHARLOTTE, NC 28277

MOD PM: JERRY BRUNO AT JERRY, BRUNO, CONTRACTOR@CROWNCASTLE, COM PH: (781) 970-0059

DESIGN STANDARD

THIS REINFORCEMENT DESIGN IS BASED UPON THE REQUIREMENTS OF THE TIA/EIA-222-F-1996 STRUCTURAL STANDARD FOR ANTENNA SUPPORTING STRUCTURES AND ANTENNAS, USING A DESIGN BASIC WIND SPEED OF 80 MPH (3-SEC GUST) WITH NO ICE, 38 MPH WITH 1 INCH ICE AND 50 MPH SERVICE LOADS,

REFER TO THE POLE DESIGN AND ANTENNA LOADING DOCUMENTED IN THE PJF STRUCTURAL ANALYSIS FOR THIS SITE (PJF#37514-2522.001.7700)

DATED 11-21-2014.

THIS PROJECT INCLUDES THE FOLLOWING REINFORCING ELEMENTS:

SHAFT REINFORCING

FIELD WELDED STIFFENERS

SHEET INDEX					
SHEET NUMBER	DESCRIPTION				
T-1	TITLE SHEET				
S-1	GENERAL NOTES				
S-2	GENERAL NOTES				
S-3	AJAX BOLT DETAIL				
S-4	MONOPOLE PROFILE				
S-5	BASE PLATE DETAILS				
S-6	MI CHECKLIST				



CROWN CASTLE PROJECT: BU #806371; HRT 096 943227; WINDSOR, CONNECTICUT MONOPOLE RETROFIT PROJECT MASTER NOTES DOCUMENT (REV. 2, 1/22/2009)

A. GENERAL NOTES
IT SPALL DE THE RESPONSIBILITY OF THE CONTRACTOR TO FIELD VERIFY ALL EXISTING CONDITIONS AND
DIMENSIONS PRIOR TO FABRICATION AND CONSTRUCTION. THESE DRAWINGS WERE PREPARED FROM
INFORMATION AND DOCUMENTS PROVIDED TO PAUL J. FORD & COMPANY BY CROWN CASTLE. THIS
INFORMATION PROVIDED HAS NOT BEEN FILED VERHIER BY PAUL J. FORD & COMPANY FOR ACCURACY
AND THEREFORE DISCREPANCIES BETWEEN THESE DRAWINGS AND ACTUAL SITE CONDITIONS SHOULD
BE AMTICIPATED. ANY DISCREPANCIES AND/DIOR CHAMPS BETWEEN THE INFORMATION CONTAINED IN
THESE DRAWINGS AND THE ACTUAL VERHIELD SITE CONDITIONS SHALL BE IMMEDIATELY BROUGHT TO
THE ATTENTION OF CROWN CASTLE AND PAUL J. FORD & COMPANY SO THAT ANY CHAMPES AND/OR
ADJUSTMENTS. IF NECESSARY, CAN BE IMADE TO THE DESIGN AND DRAWINGS.
THE EXISTING UNRENPORCED MONOPOLE STRUCTURE DOES NOT HAVE THE STRUCTURAL CAPACITY TO
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CARRY ALL OF THE AMTERNIA AND PLATFORM TO SOME STRUCTURE DISTALL BY ADDITIONAL OR NEW ANTENNA AND
PLATFORM LOADS UNTIL THE MONOPOLE REINFORCING SYSTEMS TO THE THE TAWANINGS OR SPECIFICATIONS

STRUCTURAL CAPACITY TO SAFE MICHAELY THE DAY THE PROMINGS OR SPECIFICATIONS

CARRY ALL OF THE ANTENIA AND PLATFORM LOADS SPONT UT 1—ESE DRAWINGS AT THE REQUIRED MINIMUM ITAGE-222F BASIC WIND SPEEDS. DO NOT INSTALL ANY ADDITIONAL OR NEW ANTENNA AND PLATFORM LOADS UNTIL THE MONOPOLE REINFORCING SYSTEM IS COMPLETELY AND SUCCESSFULLY INSTALLED.

IF MATERIALS, QUANTITIES, STRENGTHS OR SIZES INDICATED BY THE DRAWINGS OR SPECIFICATIONS ARE NOT IN AGREEMENT WITH THESE NOTES, THE BETTER QUALITY AND/OR GREATER QUANTITY, STRENGTH OR SIZE INDICATED, SPECIFICATIONS ARE NOT IN AGREEMENT WITH THESE NOTES, THE BETTER QUALITY AND/OR GREATER QUANTITY, STRENGTH OR SIZE INDICATED, SPECIFICATIONS THE BETTER QUALITY AND/OR GREATER QUANTITY, STRENGTH OR SIZE INDICATED, SPECIFICATIONS THE REINFORCING REPAIR SYSTEM HAS BEEN PROPERLY AND ADEQUARELY COMPLETED. IT IS THE CONTRACTOR'S SOLE RESPONSIBILITY OF INSPERIE ARE FLY AND STATE IT HE INSTALLATION OF THE REINFORCING SCHOLE REPORSIBILITY OF INSPERIE ARE FLY AND STABILITY OF IMMEDIATE THE CONTRACTOR'S SOLE RESPONSIBILITY OF INSPERIE ARE FLY AND STABILITY OF ITHE MITTER OF THE MITTER OF T

B. (SECTION NOT USED)

C. SPECIAL INSPECTION AND TESTING
ALL WORK SHALL BE SUBJECT TO REVIEW AND OBSERVATION BY THE OWNER'S REPRESENTATIVE AND
THE OWNER'S AUTHORIZED INDEPENDENT INSPECTION AND TESTING AGENCY, REFER TO CROWN
CASTLE DOCUMENT END. SOWN-1008 FOR SPECIFICATION.
ANY SUPPORT SERVICES PERFORMED BY THE ENGINEER DURING CONSTRUCTION SHALL BE
DISTINGUISHED FROM CONTINUOUS AND DETAILED INSPECTION SERVICES WHICH ARE FURNISHED BY
OTHERS. THESE SUPPORT SERVICES PERFORMED BY THE ENGINEER ARE PERFORMED SOLELY FOR
THE PURPOSE OF ASSISTING IN OULDITY CONTROL AND IN ACHEVING CONFORMANCE WITH CONTRACT
DOCUMENTS. THEY DO NOT GUARANTEE CONTRACTOR'S PERFORMANCE AND SHALL NOT BE
CONSTRUED AS SUPPERVISION OF CONSTRUCTION.
OBSERVED DISCREPANCIES BETWEEN THE WORK AND THE CONTRACT DOCUMENTS SHALL BE
CORRECTED BY THE CONTRACTOR AND ADDITIONAL COST.
AN INDEPENDENT GUALIFIED INSPECTION/TESTING AGENCY SHALL BE SELECTED, RETAINED AND PAID
PORD BY THE OWNER FOR THE SOLE PURPOSE OF INSPECTION, TESTING, AND
APPROVING ALL WELDING AND FIELD WORK PERFORMED BY THE CONTRACTOR.
(A.) ACCESS TO ANY PLACE WHERE WORK IS BEIND DONE SHALL BE PERMITTED AT ALL TIMES.
(B.) THE INSPECTION AGENCY SHALL SO SCHEDULE THIS WORK AS TO CAUSE A MINIMUM OF
INTERRUPTION TO, AND COORDINATE WITH, THE WORK AND THE CONTRACTOR'S
CONTRACTOR'S RESPONSIBILITY TO COORDINATE THE WORK AS TO CAUSE A MINIMUM OF
INTERRUPTION TO, AND COORDINATE WITH THE WORK AND THE TESTING AGENCY. THE CONTRACTOR'S RESPONSIBILITY TO COORDINATE THE WORK AS TO CAUSE A MINIMUM OF
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SHALL UTILEZ EXPERIENCE, TRAINED MORRAWINGS. THE TESTING AGENCY SHALL INSPECT THE FOLLOWING INSPECTORS
SHALL HILL E

AND COMMENSURATE WITH THE SCOPE AND TYPE OF INSPECTION WORK TO BE PERFORMED.

GENERAL.

(1) PERFORM PERIOD, CON SITE DESERVATION, INSPECTION, VERIFICATION, AND TESTING DURING THE TIME THE CONTRACTOR IS WORKING ON-SITE. AGENCY SHALL MOTIFY OWNER.

MINICIDATELY WHEN FIELD REPOSITELS OF DISCREPANICES OCCUR.

CONCRETE TESTING PER ACT. INDY REQUIRED.

STRUCTURAL STEEL.

(1) CHECK THE STEEL ON THE JOB WITH THE PLANS.

(2) CHECK THE STEEL ON THE JOB WITH THE PLANS.

(3) CHECK THE STEEL MEMBERS FOR DISTORTION, EXCESSIVE RUST, FLAWS AND BURNED HOLES.

(4) INSPECT STEEL MEMBERS FOR DISTORTION, EXCESSIVE RUST, FLAWS AND BURNED HOLES.

(5) CALL, POR LABORATORY TEST REPORTS WHEN IN DOUBT.

(6) CHECK STEEL MEMBERS FOR SIZES, SWEEP AND DIMENSIONAL TOLERANCES.

(7) CHECK FOR SUFFACE PRINSH SPECIFIED, GALVANCED.

(8) CHECK FOR SUFFACE PRINSH SPECIFIED, GALVANCED.

WELDING:

(1.) VERIFY FIELD WELDING PROCEDURES, WELDERS, AND WELDING OPERATORS, NOT DEEMED

(1.) YERRY FIELD WELDING PROCEDURES, WELDERS, AND WELDING OPERATORS, NOT DEEMED PREQUALIFIED, IN ACCORDANCE WITH AWS D.1. (2.) INSPECT FIELD WELDED CONNECTIONS IN ACCORDANCE WITH THE REQUIREMENTS SPECIFIED AND IN ACCORDANCE WITH AWS D.1. (3.) APPROVE FIELD WELDING SEQUENCE. (A.) A PROGRAM OF THE APPROVED SEQUENCES SHALL BE SUBMITTED TO THE OWNER BEFORE WELDING BEGINS. NO CHANGE IN APPROVED SEQUENCES MAY BE MADE WITHOUT PERMISSION FROM THE

WITHOUT PERMISSION FROM THE

(4.) INSPECT WELDED CONNECTIONS AS FOLLOWS AND IN ACCORDANCE WITH AWS D1.1:

(4.) INSPECT WELDED CONNECTIONS AS FOLLOWS AND IN ACCORDANCE WITH AWS D1.1:

(6.) INSPECT WELDING EQUIPMENT FOR CAPACITY, MAINTENANCE AND WORKING CONDITIONS,

(7.) VERIFY SPECIFIED ELECTRODES AND HANDLING AND STORAGE OF ELECTRODES FOR CONFORMANCE TO SPECIFICATIONS.

(8.) VERIFY SPECIFIED ALBORITHMS AND INTERPASS TEMPERATURES FOR CONFORMANCE WITH AWS INSPECT PREHEATING AND INTERPASS TEMPERATURES FOR CONFORMANCE WITH AWS

VISUALLY INSPECT ALL WELDS AND VERIFY THAT QUALITY OF WELDS MEETS THE

REQUIREMENTS OF AWS D1.1.
SPOT TEST AT LEAST ONE FILLET WELD OF EACH MEMBER USING MAGNETIC PARTICLE OR DYE PENETRANT. DYE PENETRANT.
INSPECT FOR SIZE, SPACING, TYPE AND LOCATION AS PER APPROVED PLANS,
VERIFY THAT THE BASE METAL CONFORMS TO THE DRAWINGS.
REVIEW THE REPORTS BY TESTING LABS.
CHECK TO SEE THAT WELDS ARE CLEAR AND FREE FROM SLAG.
INSPECT RUST PROTECTION OF WELDS AS PER SPECIFICATIONS.
CHECK THAT DEFECTIVE WELDS ARE CLEARLY MARKED AND HAVE BEEN ADEQUATELY
REPAIRED.

F. REPORTS:
(1.) COMPILE AND PERIODICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER.

(T) COMPILE AND PERIODICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER.

THE INSPECTION PLAN OUTLINED HEREIN IS INTENDED AS A DESCRIPTION OF GENERAL AND SPECIFIC TIEMS OF CONCERN. IT IS NOT INTENDED TO BE ALL-INCLUSIVE. IT DOES NOT LIMIT THE TESTING AND INSPECTION AGENCY TO THE TESTING INDICATED THE TESTING AND CHECKING MAY BE REQUIRED AND SHOULD BE ANTIOPATED. THE TESTING AND CHECKING MAY BE REQUIRED AND SHOULD BE ANTIOPATED. THE TESTING AND CHECKING MAY BE TO DESCRIPTION OF THE TESTING AND SHOULD BE AND SHOULD BE AND SHOULD BE AND SHOULD BE AND SHOULD BE AND SHOULD BE AND SHOULD BE AND SHOULD BE AND SHOULD BE BROUGHT IMMEDIATELY TO THE OWNER'S ATTENTION. RESOLUTIONS ARE NOT TO BE MADE WITHOUT THE OWNER'S REVIEW AND SPECIFIC WRITTEN CONSENT. THE OWNER RESERVES THE RIGHT TO DETERMINE WHAT IS AN ACCEPTABLE RESOLUTION OF DISCREPANCIES AND PROBLEMS. AFTER ACID HIS PECTION THE TESTING AGENCY WILL PREPARE A WRITTEN ACCEPTANCE OR REJECTION WHICH WILL BE GIVEN TO THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WRITTEN ACTION WILL GIVE THE CONTRACTOR A LIST OF ITEMS TO BE CORRECTED, PRIOR TO CONTINUING CONSTRUCTION, AND/OR LOADING OF STRUCTURAL ITEMS.

RESPONSIBILITY: THE TESTING AGENCY WILL PREVE THE CONTRACTOR'S CONTRACTOR'S CONTRACTOR ON THE STRUCK AND STRUCTURAL ITEMS.

RESPONSIBILITY: THE TESTING AGENCY WILL PREVE THE SOT DE CORRECTED, PRIOR TO CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WRITTEN ACTION WILL GIVE THE CONTRACTOR A LIST OF ITEMS TO BE CORRECTED, PRIOR TO CONTRACTOR AND THE STRUCK AGENCY WILL NOT REPLACE THE CONTRACTOR AND THE SOLD RESPONSIBILITY FOR ANY DEVATIONS FROM THE OFFICIAL CONTRACTOR CONTRACTOR HAS THE SOLD RESONSIBILITY FOR ANY DEVATIONS FROM THE CONTRACTOR HAS THE SOLD RESONSIBILITY FOR ANY DEVATIONS FROM THE CONTRACTOR HAS THE SOLD RESONSIBILITY FOR ANY DEVATIONS FROM THE CONTRACTOR CONTRACTOR HAS THE SOLD RESONSIBILITY FOR ANY DEVATIONS FROM THE CONTRACTOR CONTRACTOR HAS THE SOLD RESONSIBILITY FOR ANY DEVATIONS FROM THE CONTRACTOR CONTRACTOR HAS THE SOLD RESON



BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

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CHECKED BY: C.M.M.	GENERAL NOTES	
APPROVED BY:	0.4	
DATE: 11-21-2014	5-1	

- STRUCTURAL STEEL
 STRUCTURAL STEEL MATERIALS, FABRICATION, DETAILING, AND WORKMANSHIP SHALL CONFORM
 TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:
 BY THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC):

 "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL
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- STRUCTURAL STEEL MATERIALS, FABRICATION, DETAILING, AND WORKMANSHIP SHALL CONFORM TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:

 BY THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (ASSC):

 (A) "SPECIFICATION FOR THE DESIGNA, FABRICATION AND CRECTION OF STRUCTURAL STEEL FOR BUILDINGS."

 (B) "SPECIFICATION FOR THE DESIGNA, FABRICATION AND CRECTION OF STRUCTURAL STEEL FOR BUILDINGS."

 (C) "CODIC OF STANDARD FRACTICE FOR STEEL BUILDINGS AND BRIDGES" (PARAGRAPH 4.2.1 SPECIFICATION OF STRUCTURAL DIDING AND BRIDGES" (PARAGRAPH 4.2.1 SPECIFICATION WEERING FOUNDATION).

 (C) "CODIC OF STANDARD FRACTICE FOR STEEL BUILDINGS AND BRIDGES" (PARAGRAPH 4.2.1 SPECIFICALLY SECULDED).

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 ANY MEDING SOCIOUS.
- FOUNDATION WORK (NOT REQUIRED)

- CAST-IN-PLACE CONCRETE (NOT REQUIRED)
- H. EPOXY GROUTED REINFORCING ANCHOR RODS - (NOT REQUIRED)
- TOUCH UP OF GALVAINZING
 TOUCH UP OF GALVAINZING
 THE CONTRACT OR STRAIL TOUCH UP ANY ANDOR ALL AREAS OF GALVANIZING ON THE EXISTING
 THE CONTRACT OR STRAIL TOUCH UP ANY ANDOR ALL AREAS OF GALVANIZING ON THE EXISTING
 STRUCTURE OR NEW COMPONENTS THAT ARE DAMAGED DIVRING TRANSPORTATION OR RERCTION AND ASSEMBLY AS
 WELL AS ANY AND ALL ABRASIONS, CUTS, FIELD DRILLING, AND ALL FIELD WELDING SHALL BE
 TOUCHED UP WITH TWO (2) COATS OF ZRC-BRAND ZINC-RICH COLD GALVANIZING COMPOUND, FLAN
 HICKNESS PER COAT SHALL BE: WET JOIN MIS, SPRY 1-5 MILLS. APPLY PER ZRC (MANUFACTURER)
 RECOMMENDED PROCEDURES. CONTACT ZRC AT 1-809-831-3275 FOR PRODUCT INFORMATION.
 CONTRACTOR SHALL CLEAN AND PREPARE ALL FIELD WELDS ON GALVANIZED AND PRIME PAINTED
 SUBFACES FOR TOUCH-UP COATING IN ACCORDANCE WITH AWS D1.1. THE OWNERS TESTING
 AGENCY SHALL VERIFY THE PERPARED SURFACE PRIOR TO APPLICATION OF THE TOUCH-UP
 COATING.
 THE OWNERS TESTING AGENCY SHALL TEST AND VERIFY THE COATING THICKNESS AFTER THE
 CONTRACTOR HAS APPLIED THE ZRC COLD GALVANIZING COMPOUND AND IT HAS SUFFICIENTLY
 DRIED, AREAS FOUND TO BE INADEQUATELY COATED, SHALL BE RE-COATED BY THE CONTRACTOR
 AND RE-TESTED BY THE TESTING AGENCY.

- HOT DIP GALVANIZING
 HOT-DIP GALVANIZEAL STRUCTURAL STEEL MEMBERS AND ALL STEEL ACCESSORIES, BOLTS,
 WASHERS, ETC, PER ASTM A123 OR PER ASTM A163, AS APPROPRIATE.
 PROPERLY PREPARE STEEL ITEMS FOR GALVANIZING.
 DRILL OR PUNCH WEEP ANDION DENINGER HOLES AS REQUIRED.
 ALL GALVANIZING SHALL BE DOME AFTER FABRICATION IS COMPLETED AND PRIOR TO FIELD
 INSTALLATION.

- PERPETUAL INSPECTION AND MAINTENANCE BY THE OWNER
 ATTER THE CONTRINCTION HAS SUCCESSFALLY COMMETED THE INSTALLATION OF THE MONOPOLE
 REINFORCING SYSTEM AND THE WORK HAS BEEN ACCEPTED BY THE OWNER. THE OWNER WILL BE
 RESPONSIBLE FOR THE LONG TERM AND PERPETUAL INSPECTION AND MAINTENANCE OF THE POLE
 AND REINFORCING SYSTEM.
 THE MONOPOLE REINFORCING SYSTEM INDICATED IN THESE DOCUMENTS USES REINFORCING
 COMPONENTS THAT INVOLVE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL
 POLE STRUCTURE. THESE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL
 POLE STRUCTURE. THESE FIELD WELDING CONNECTIONS ARE SUBJECT TO CORROSION DAMAGE
 AND DETERIORATION IF THEY ARE NOT PROPERLY MAINTAINED AND COVERED WITH CORROSION
 PREVENTIVE COATING SUCH AS THE ZRG CALVANIZING COMPOUND SPECIFIED PREVIOUSLY. THE
 STRUCTURAL LOAD CARRYING CAPACITY OF THE REINFORCED POLE SYSTEM IS DEPENDENT UPON
 THE INSTALLED SIZE AND QUALITY, MAINTAINED SOUND CONDITION AND STRENGTH OF THESE FIELD
 WELDED CONNECTIONS, ANY CORROSION OF, DAMAGE TO, FATIGUE, FRACTURE, ANDIOR
 DETERIORATION OF THESE WELDS ANDIOR THE CONNECTED COMPONENTS WILL RESULT IN THE
 LOSS OF STRUCTURAL LOAD CARRYING CAPACITY AND MAY LEAD TO FAILURE OF THE
 STRUCTURAL SYSTEM. THEREFORE, IT IS IMPERATIVE THAT THE OWNER REQULARLY INSPECTS,
 MAINTAINS, AND REPAIRS AS NECESSARY, ALL OF THESE WELDS, CONNECTIONS, AND
 COMPONENTS FOR THE LIFE OF THE STRUCTURE.

 THE COWNER SHALL REFER TO TIMEIA-222-F-1996, SECTION 14 AND ANNEX E FOR RECOMMENDATIONS
 FOR MAINTENANCE AND INSPECTION. THE REQUENCY OF THE INSPECTION AND MAINTENANCE
 INTERVALS IS TO BE DETERMINED BY THE OWNER BASED UPON ACTUAL SITE AND ENVIRONMENTAL
 CONDITIONS, PAUL J. FORD COMPONENTS OF THE STRUCTURAL SYSTEM BE PERFORMED
 YEARLY AND ONE AS PREQUENTLY AS CONDITIONS WARRANTA. ACCORDING TO TIME THE ADDITIONS
 OF MAINTENANCE AND INSPECTION. THE RECOMMENDED THAT AT COMPLETE AND THOROUGH
 INSPECTION OF THE ENTIRE REINFORCED MONOPOLE STRUCTURAL SYSTEM BE PERFORMED
 YEARLY AND ONE AS PREQUENTLY AS CONDITIONS WARRANTA. ACCORDING TO TATELE AND

AJAX BOLT NOTE SHEET: REV. 1.5, 5-12-2014

NOTES: 1 ALL

- 1, ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
- 2. ALL STRUCTURAL BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS' DEC. 31, 2009.
- 3. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND DETAIL BELOW FOR THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
- 4. ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS, DTI'S SHALL BE THE SQUIRTER® STYLE, MADE TO ASTM F959 LATEST REVISION; AND HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A HARDNESS OF RC 38 OR HIGHER.

NOTES FOR AJAX M20 'ONE-SIDE BOLTS WITH DIRECT TENSION INDICATORS (DTIS):

DTI'S REQUIRED: DTI'S SHALL BE "SELF-INDICATING" SQUIRTER® STYLE DTI'S MADE WITH RED DURABLE SQUIRT MEDIA EMBEDDED IN THEM, INSPECTED BY MEANS OF THE VISUAL EJECTION OF SILICONE AS THE DTI PROTRUSIONS COMPRESS. SQUIRTER® DTI'S SHALL BE CALIBRATED PER MANUFACTURER'S INSTRUCTIONS PRIOR TO USE.

THE DIRECT TENSION INDICATOR (DTI) WASHERS SHALL BE THE "SQUIRTER® STYLE" AS MANUFACTURED BY APPLIED BOLTING TECHNOLOGY PRODUCTS' INC.:

.PART NUMBER: 2DTIM208MGAFSIF

DESCRIPTION: P.C. 8.8 DTI SQUIRTER WASHER WITH RED DURABLE SQUIRT MEDIA DESIGNED SPECIFICALLY FOR THE AJAX M20 ONESIDE BOLT, FINISH SHALL BE ZINC GALVANIZED AS PROVIDED BY THE DTI MANUFACTURER.

DISTRIBUTOR CONTACT DETAILS:

ALLFASTENERS 15401 COMMERCE PARK DR. BROOKPARK, OHIO 44142 PHONE: 440-232-6060

E-MAIL: SALES@ALLFASTENERS.COM

DTI: USE DIRECT TENSION INDICATOR (DTI) WASHERS COMPATIBLE WITH 20 MM (M20) NOMINAL A325 BOLTS FOR THE AJAX M20 BOLTS. DTI'S SHALL NOT BE HOT-DIP GALVANIZED. DTI'S SHALL BE MECHANICALLY GALVANIZED (MG) BY THE COLD MECHANICAL PROCESS ONLY AS PROVIDED BY THE DTI MANUFACTURER.

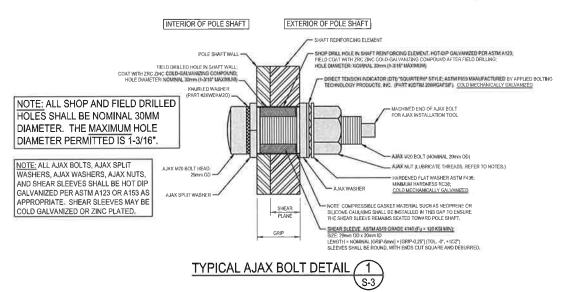
HARDENED WASHERS REQUIRED: USE A HARDENED WASHER FOR A 20 MM (M20) NOMINAL BOLT BETWEEN THE TOP OF THE DIRECT TENSION INDICATOR (DTI) WASHER AND THE NUT OF THE AJAX MZO BOLTS, HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A MINIMUM HARDNESS OF RC 38 OR HIGHER. THE HARDENED WASHERS SHALL BE MECHANICALLY GALVANIZED BY THE COLD MECHANICAL PROCESS. ALTERNATIVELY, CORRECTLY MADE HOT DIP GALVANIZED BY THE COLD MECHANICAL PROCESS. ALTERNATIVELY, CORRECTLY MADE HOT DIP GALVANIZED BY THE WASHERS HAVING A MINIMUM HARDNESS OF RC 38 CAN BE USED; CONTRACTOR SHALL PROVIDE DOCUMENTATION OF WASHER SPECIFICATION AND HARDNESS.

NUT LUBRICATION REQUIRED: PROPERLY LUBRICATE THE THREADS OF THE NUT OF THE AJAX BOLT SO THAT IT CAN BE PROPERLY TIGHTENED WITHOUT GALLING AND/OR LOCKING UP ON THE BOLT THREADS, CONTRACTOR SHALL FOLLOW DTI MANUFACTURER INSTRUCTIONS FOR PROPER LUBRICATION AND TIGHTENING.

NOTE: COMPLETELY COMPRESSED DTI'S SHOWING NO VISIBLE REMAINING GAP ARE ACCEPTABLE. DTI WASHERS SHALL BE PLACED DIRECTLY AGAINST THE OUTER AJAX WASHER WITH THE DTI BUMPS FACING AWAY FROM THE AJAX WASHER. PLACE A HARDENED WASHER BETWEEN THE DTI AND THE AJAX NUT. THE DTI BUMPS SHALL BEAR AGAINST THE UNDERSIDE OF A HARDENED FLAT WASHER. NEVER DIRECTLY AGAINST THE NUT.

CONTRACTOR SHALL FOLLOW DTI MANUFACTURER'S INSTRUCTIONS FOR INSTALLATION, LUBRICATION, TIGHTENING AND INSPECTION.

INSPECTION REQUIRED: ALL AJAX BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2008, BY A QUALIFIED BOLT INSPECTOR. DURING INSTALLATION, THE BOLT INSPECTOR SHALL VERIFY AND DOCUMENT: THE SHOP-DRILLED AND FIELD-DRILLED HOLE SIZES, THE INSTALLATION OF THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S TENSIONING PROCEDURE. IN ADDITION, ALL AJAX BOLTS AND DTI'S SHALL BE VISUALLY INSPECTED ACCORDING TO THE DTI MANUFACTURER'S INSTRUCTIONS. THE BOLT INSPECTOR SHALL PROVIDE COMPLETE PHOTO DOCUMENTATION OF ALL BOLTS AFTER TIGHTENING CLEARLY SHOWING THE CONDITION OF THE DTI'S.

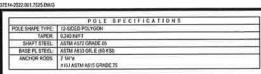




BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT: 37514-2522.001.7700

DRAWN BY:
LM.
CHECKED BY:
C.M.M.
APPROVED BY:
11-21-2014

S-3



SHAFT SECTION LENGTH SECTION (FT)		PLATE THICKNESS	LAP SPLICE	DIAMETER ACROSS FLATS (IN)		
SECTION	ME11	(IN)	001	@ 10P	@ BOTTON	
1	49.166	0.2810	50.00	14,760	26,570	
2	55.00	0.3440	20,00	25.007	38,200	

CONTRACTOR SHALL PROVIDE AS IM AND SHIM PLATES SELOW SUP JOINTS. THE SHIM PLATES SHALL BE INJUCTED BETWEEN THE MENY SHAFT REIN-PORCEMENT AND THE EXISTING PLUE SHAFT FROM THE SUP JOINT TO THE NEW SHAFT REIN-PORCEMENT SHALL SE PLATE LOCATION AND A EXTRA LOON SHALLS SHAW SHALL BE PLACED DETWEEN THE NEW UPPER AND LOWER SHIFT REINFORCEMENT FLATES AT THE SHAFT REINFORCEMENT SPLOET SHAFT REINFORCEMENT SHAFT RE

MODIFICATIONS:

- (A) INSTALL NEW TRANSITION STIFFENERS AT BASE PLATE, SEE SHEET S-5,
- B INSTALL NEW SHAFT REINFORCING, SEE CHART,

				NEW COLF	AT PLATE (6	5 KSI RENFOR	CING SCHED	ULE			
BOTTOM ELEVATION	TOP ELEVATION	FLAT #/ DEGREE SEPARATION	ELEMENT	ELEMENT LENGTH	ELEMENT QUANTITY	APPROXIMATE AJAX BOLTS PER ELEMENT	APPROXIMATE TOTAL AJAX BOLT QUANTITY	SOLTS BOLTS BOTTON	TERMINATION BOLTS (TOP)	MAIDMUM INTERMEDIATE BOLT SPACING	TOTAL STEEL WEIGHT
0.07	201/01	73.694192	OCLAFF MEDISTS	30.7	3	- 6	130	ji .	14	621	2003:BS
20.0	10.7	F2 FEAFED	COLALD (KOLDIN)	30.0	- 9)	34	***	#3	61	H.	11.8 LES
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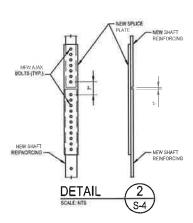
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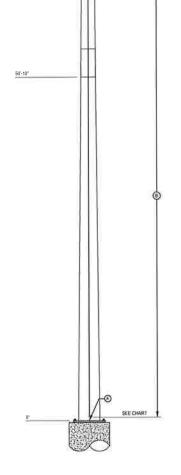
			SPLICE	PLATE INSTAL	LATION CHAP	17		
ELEVATION	FLAT PLATE THICKNESS	FLAT PLATE WIDTH	FLAT PLATE LENGTH	FLAT PLATE QUANTITY	WELD LENGTH MER SIDE	TOTAL WELD LENGTH	AJAK BOLTSPER SPLICE*	TOTAL STEEL
20 F	110	2.10	8.7	3	- 7	- F		541.55
						-		4.24190.1

BOLTS INCLUDED IN THE TOTAL QUANTITY LISTED IN THE FLAT PLATE INSTALLATION CHART,

	- 1	VEW SHIM CHA	RT	
DUNITITY SHEW	QUANTITY	SHMWDTH	SHIPLENGTH	HOLE
5	3	0.065	(40)	(1141)

SHIMS ARE FOR BIDDING PURPOSED ONLY, FINAL SHIM REQUIREMENTS TO BE DETERMINED BY CONTRACTOR DURING FABRICATION.

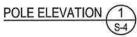




SEE CHART

98'-0"

85'-0" C/L MOUNT

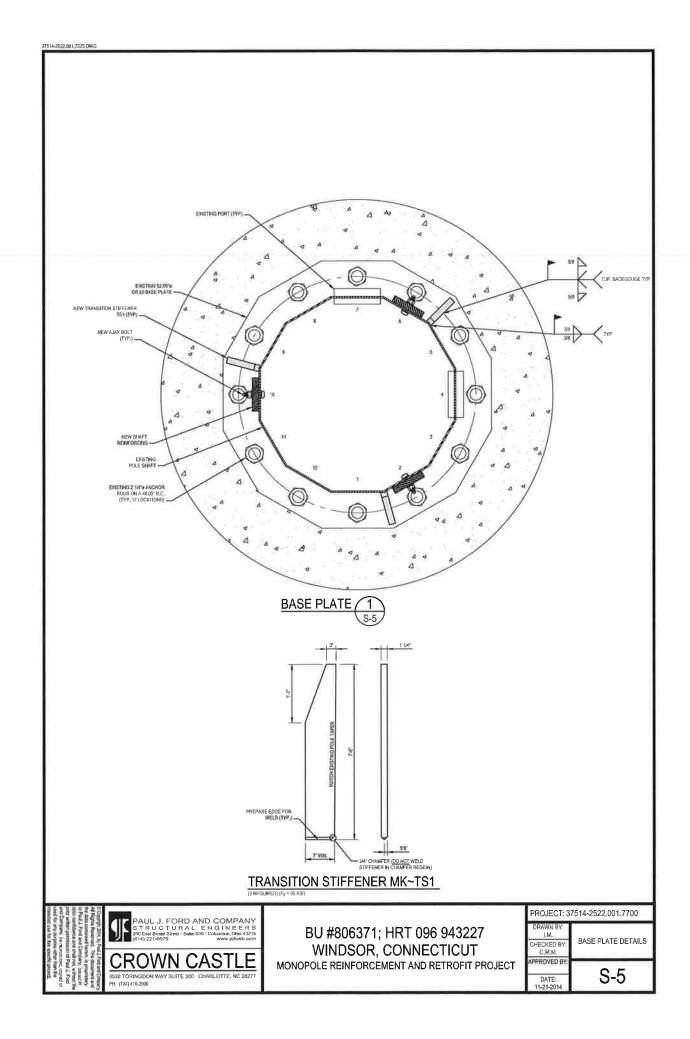


PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 East Broad Street * Sutile 500 * Columbus, Oho 43215 (514) 221-8679

CROWN CASTLE

BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT: 37514-2522.001.7700 LM-MONOPOLE PROFILE CHECKED B C.M,M,

S-4 DATE: 11-21-201



CREATION

III AND A THE AND THE AND A REVIEW A VISUAL HISPECTION OF TOWER MODIFICATIONS AND A REVIEW OF CONSTRUCTION HISPECTIONS OF THE AND A REVIEW OF CONSTRUCTION HISPECTIONS OF THE AND A REVIEW OF CONSTRUCTION HAS CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS IMMELY THE OD

THE M IS TO COVERM NISTALLATION CONFIGURATION AND WORMMARSHIP ONLY MAD IS NOT A REVIEW OF THE MODERCATION DESIGN ISSUE, NOR DOES THE WINESECTOR TAKE OWNERSHIP OF THE MODIFICATION DESIGN. OWNERSHIP OF THE STRUCTURAL MODERCATION DESIGN EFFECTIVENESS AND INTEGRITY RESIDES WITH THE BEST AT LET INTEREST.

ALL WIS SHALL BE CONDUCTED BY A CROWN ENGINEERING VENDOR (ABY) OR ENGINEERING SERVICE VENDOR (ABSV) THAT IS APPROVED TO PERFORMELEVATED WORL FOR CROWN: SEE ENGIBUL-1017) LIST OF AFPROVED MY VENDORS.

TO ENSURE THAT THE REQUIREMENTS OF THE MILADE MET, IT IS VITAL THAT THE GENERAL CONTRACTOR (GC) AND THE MILNOFECTION BEGIN COMMUNICATING AND CONSIDERATING AS SOOTING A PIOT RECEIPED. IT IS EXPECTED THAT EXCHARATIVELE PROJECTIVE MISSAGNING OUT TO THE OTHER PARTY IF COMMETA BOORMATIONS ROTI EXCHAIN CONTRACT FOR TOTAL OTHER CONTRACT (POC.)

REFER TO ENSISOW/10007 MODIFICATION WISPECTION SOW FOR FURTHER DETAILS AND REGULEMENTS

MINSPECTOR
THE MINSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A POIFOR THE MITGLAT A MANAGEMENT.

- REWEWTHE REQUIREMENTS OF THE MI CHECKLIST
 WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT CAUSITE INSPECTIONS. INCLUDING FOUNDATION INSPECTIONS.

GENERAL CONTRACTOR
THE OLD REQUIRED TO CONTACT THE MILINSPECTOR AS BOON AS RECEIVING A POINCY THE MODIFICATION INSTALLATION OR TURNEY
PROJECTION, AT A MARKAN

- REMEM THE REQUIREMENTS OF THE MI CHECKLIST
 WORK WITH THE MI REPECTOR TO GENELOR A SCHEDULE TO CORDUCT ON SITE INSPECTIONS INCLUDING FOUNDATION INSPECTIONS
 SETTER CARGENERAND ALL IMPRECIONS AND TESTING RECOVERABITS.

THE GC SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IM ACCORDANCE WITH THE REQUIREMENTS OF THE MICHECKUST AND DENG-50W-10007

RECOMMENDATIONS THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO BRIMINGE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO BRIMINGE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING

- IT IS SUGGESTED THAT THE GC PROVIDE A MINIMAL OF SPUSINESS DAYS NOTICE PREFERABLE ID TO THE MINISPECTOR AS TO WHEN THE SIST WILL BE REDOY FOR THE MIT OB ECONOMITED.

 THE GO AGAIN INSPECTOR CORDINATE CLOSES IT HEROCHARD THE ENTIRE PROJECT.

 WHEN PASSIBLE IT IS PREFERRED TO HAVE THE GO AND MINISPECTOR ON SITE SMULT/INSOURLY FOR ANY GUY WHE TENSION IN OR REFLICIATION DOPENATIONS.

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CANCELLATION OR DELAYS IN SCHEDULED MI

FINE OF AND WINSPECTION ARREST ON ADMIT ON WHICH THE MI WILL BE CONDUCTED, AND BITHER PARTY CAUCELS ON DELAYS, CROWN
SHALL AND BE REPONSIBLE FOR AN TWO COSTS FEES LOSS OF DEPOSITS ANDION OTHER FERMITIES RELATED TO THE CAUCELLATICS OR
DELAY INCLURED BY STHAED PARTY FOR ANY TIME (FO TRAVEL AND LODGING, COSTS OF KEEPING EQUERABITION SHE ETC.) IF CROWN
CONTROLTS DIRECTLY FOR A THARD PARTY M. EXCEPTIONS MAY BE MADE III, THE EVENT FINT THE DELAY CANCELLATION IS CAUSED BY
WEATHER OR OTHER CONDITIONS THAT WAY COMPROMISE THE SAFETY OF THE PARTIES INVOLVED.

CORRECTION OF FAILING MS.
THE MCO STATE WHICH CASHING MICE OF ALL THE MICE ALL MILE THE GC SHALL WORK WITH CROWN TO COORDINATE A FEMEDIATION.

- CORRECT FALING ISSUES TO COUNTY WITH THE SPECIFICATIONS CONTAINED IN THE ORIGINAL CONTRACT DOCUMENTS AND
 CORROMATE A SUPPLEMENT WI.
 OR WITH CROWITS APPROVAL. THE GC MAY WORK WITH THE ECT TO RE ANALYZE THE MODIFICATION REINFORCEMENT USING THE
 ASPAIL TO ORDITION.

M VERFICATION INSPECTIONS
CONTROL SEASON TO CONDUCT A MILYER PICATION INSPECTION TO VERFY THE ACCURACY AND COMPLETENESS OF PREVIOUS CONDUCTED MILYER CONTROL ON TOWER MODIFICATION PROJECTS

LL VERRICATION INSPECTIONS SHALL BE HELD TO THE SAVE SPECIFICATIONS AND REQUIREMENTS IN THE CONTRACT DOCUMENTS AND IN COORDANCE WITH ENS SOM-10007

- FRE CONSTRUCTION GENERAL SITE CONDITION
 PROTOGRAPHS DUANTS THE RESPONDENT MODIFICATION CONSTRUCTION/SECTION AND INSPECTION
 RAW MATERIAL CENTRAL DETAILS
 PROTOGS OF ALL CRITICAL DETAILS
 FOLOMATION NOCINCATIONS
 WELD PREPARATION
 BULL INSTALLATION AND TORQUE
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 SIES COLINIS REPARA
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HOTOS OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED INADEQUATE

THIS IS NOT A COMPLETE LIST OF REQUIRED PHOTOS. FLEASE REFER TO ENG SOW 1960?

	MI CHECKLIST
CONSTRUCTION INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY EOR)	REPORT ITEM
	PRE-CONSTRUCTION
Х	MI CHECKLIST DRAWINGS
х	EOR REVIEW
x	FABRICATION INSPECTION
NA	FABRICATOR CERTIFIED WELD INSPECTION
X	MATERIAL TEST REPORT (MTR)
NA	#ABRICATOR NDE INSPECTION
х	NDE REPORT OF MONOPOLE BASE PLATE (AS REQUIRED)
x	PACKING SLIPS
DOITIONAL TESTING AND INSPECTIONS:	
	CONSTRUCTION
х	CONSTRUCTION INSPECTIONS
NA.	FOUNDATION INSPECTIONS
NA	CONCRETE COMP. STRENGTH AND SLUMP TESTS
NA	POST INSTALLED ANCHOR ROD VERIFICATION
NA	BASE PLATE GROUT VERIFICATION
Х	CONTRACTOR'S CERTIFIED WELD INSPECTION
NA	EARTHWORK LIFT AND DENSITY
×	ON SITE COLD GALVANIZING VERIFICATION
NA .	GUY WIRE TENSION REPORT
х	GC AS-BUILT DOCUMENTS
x	INSPECTION OF AJAX BOLTS AND DTI'S PER REQUIREMENTS ON SHEET S-3
NA.	MICROPLERIOCK ANCHOR INSTALLER'S DRILLING AND INSTALLATION LOGS AS DAYGO DOCUMENTS
NA.	REFER TO MICROPILE/ROCK ANCHOR NOTES FOR SPECIAL PISPECTION AND TESTING REQUIREMENTS.
DDITIONAL TESTING AND INSPECTIONS:	430000000000000000000000000000000000000
	POST-CONSTRUCTION
×	MI INSPECTOR REDLINE OR RECORD DRAWING(S)
NA.	POST INSTALLED ANCHOR ROD PULL-OUT TESTING
N/	
	PHOTOGRAPHS

MOTE: X DENOTES A DOCUMENT RECEDED FOR THE PHILIPPORT NA DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE PMILIPPORT

PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 200 East Bood Street * Salle 800 * Columbus. Oho 40216 (2014) 221-8079 **CROWN CASTLE**

BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

PROJECT: 37514-2522,001,7700				
DRAWN BY:				
CHECKED BY: C.M.M.	MI CHECKLIST			
APPROVED BY:	0.6			
DATE: 11-21-2014	5-6			

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

BU NUMBER; SITE NAME BU #806371; HRT 096 943227

APP: 269459 REV. 0; WO: 965888

SITE ADDRESS

HRT 96 599 MATIANUCK AVE WINDSOR, CONNECTICUT 06095 HARTFORD COUNTY

PROJECT NOTES

- DETAILED FIELD INFORMATION REGARDING INTERFERENCES AND/OR EXISTING FIELD CONDITIONS MAY BE AVAILABLE ON CROWN'S CCISITES AND FROM CONTRACTOR'S PRE-MOD MAPPING, IT IS THE CONTRACTOR'S RESPONSIBILITY TO FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS AND COORDINATE WITH THE AVAILABLE SOURCES OF INFORMATION ABOVE AND WITH THE PROJECT PLANS BEFORE PROCEEDING WITH THE WORK, CONTRACTOR SHALL IMMEDIATELY REPORT ANY AND ALL DISCREPANCIES TO PAUL J. FORD AND COMPANY AND CROWN CASTLE FIELD PERSONNEL BEFORE PROCEEDING WITH THE WORK.
- ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
- ALL STRUCTURAL BOLTS SHALL BE FIELD INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS',
- (A.) DTI'S REQUIRED: ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND DETAILS ON SHEET S-3 FOR REQUIREMENTS ON THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
 - (B.) EFFECTIVE 5/30/2012: UNTIL FURTHER NOTICE, CROWN CASTLE WILL ACCEPT AJAX BOLTS TIGHTENED USING AISC "TURN-OF-NUT" METHOD, INSTALLERS SHALL FOLLOW CROWN GUIDELINES FOR AISC "TURN-OF-NUT" METHOD AND ALSO PROVIDE COMPLETE INSPECTION DOCUMENTATION IN THE PMI. PRIOR TO STARTING WORK, CONTRACTOR SHALL CONSULT WITH CROWN ENGINEERING TO DETERMINE WHETHER THIS POLICY IS STILL IN PLACE.
 - (C.) REQUIREMENT EFFECTIVE 04/20/2013, PER CROWN CASTLE DIRECTIVE: ANY AND ALL STRUCTURAL BOLTS THAT ARE TIGHTENED TO THE PRETENSIONED CONDITION USING THE AISC "TURN-OF-NUT" TENSIONING PROCEDURE (NON-TENSION CONTROLLED [NON-TC] BOLTS AND/OR BOLTS WITHOUT DTI'S INSTALLED) SHALL BE INSPECTED ONSITE BY AN INDEPENDENT THIRD-PARTY BOLT INSPECTOR, AS APPROVED BY CROWN, THIS INSPECTION IS REQUIRED TO BE AN ONSITE FIELD INSPECTION. THE THIRD-PARTY BOLT INSPECTOR SHALL FOLLOW THE PUBLISHED CROWN CASTLE INSPECTION PROCEDURE "MI NON-TC BOLT INSPECTION", DATED APRIL 2013. THE THIRD-PARTY BOLT INSPECTOR SHALL PREPARE A FULLY DOCUMENTED BOLT INSPECTION REPORT. AS SPECIFIED BY CROWN. AND SHALL SUBMIT A COPY OF THE BOLT INSPECTION REPORT TO THE MI INSPECTOR, THE EOR, AND TO CROWN CASTLE.
- NDE OF THE CIRCUMFERENTIAL WELD OF THE BASE PLATE TO SHAFT CONNECTION IS REQUIRED. SEE CCI DOCUMENTS ENG-SOW-1033 'TOWER BASE PLATE NDE AND ENG-BUL-10051 'NDE REQUIREMENTS FOR MONOPOLE BASE PLATE TO PREVENT CONNECTION FAILURE', NOTIFY THE EOR AND CROWN ENGINEERING IMMEDIATELY IF ANY CRACKS ARE SUSPECTED OR HAVE BEEN IDENTIFIED. THE NDE SHALL INCLUDE ALL EXISTING REINFORCEMENTS THAT HAVE BEEN WELDED TO THE BASE PLATE. ANY FULL PENETRATION WELDING TO THE BASE PLATE REQUIRED AS PART OF THIS ACTIVE REINFORCEMENT DESIGN SHALL BE INCLUDED IN THE NDE SCOPE OF WORK.

PROJECT CONTACTS:

MONOPOLE OWNER:

3530 TORINGDON WAY SUITE 300 CHARLOTTE, NC 28277

MOD PM: JERRY BRUNO AT JERRY, BRUNO, CONTRACTOR@CROWNCASTLE, COM PH: (781) 970-0069

DESIGN STANDARD

THIS REINFORCEMENT DESIGN IS BASED UPON THE REQUIREMENTS OF THE TIA/EIA-222-F-1996 STRUCTURAL STANDARD FOR ANTENNA SUPPORTING STRUCTURES AND ANTENNAS, USING A DESIGN BASIC WIND SPEED OF 80 MPH (3-SEC GUST) WITH NO ICE, 38 MPH WITH 1 INCH ICE AND 50 MPH SERVICE LOADS.

REFER TO THE POLE DESIGN AND ANTENNA LOADING DOCUMENTED IN THE PJF STRUCTURAL ANALYSIS FOR THIS SITE (PJF#37514-2522,001,7700), DATED 11-21-2014.

THIS PROJECT INCLUDES THE FOLLOWING **REINFORCING ELEMENTS:**

SHAFT REINFORCING

EIELD WEI DED STIFFENERS

SHEET INDEX			
SHEET NUMBER	DESCRIPTION		
T-1	TITLE SHEET		
S-1	GENERAL NOTES		
S-2	GENERAL NOTES		
S-3	AJAX BOLT DETAIL		
S-4	MONOPOLE PROFILE		
S-5	BASE PLATE DETAILS		
S-6	MI CHECKLIST		



CROWN CASTLE PROJECT: BU #806371; HRT 096 943227; WINDSOR, CONNECTICUT MONOPOLE RETROFIT PROJECT MASTER NOTES DOCUMENT (REV. 2, 1/22/2009)

A. GENERAL NOTES
IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS PRIOR TO FABRICATION AND CONSTRUCTION. THESE DRAWINGS WERE PREPARED FROM INFORMATION AND DOCUMENTS PROVIDED TO PAUL J., FORD & COMPANY BY CROWIN CASTLE. THIS INFORMATION OF ROVIDED HAS NOT BEEN FIELD VERHIED BY PAUL J., FORD & COMPANY FOR ACCURACY AND THEREFORE DISCREPANCIES BETWEEN THESE DRAWINGS AND ACTUAL SITE CONDITIONS SHOULD BE ANTICIPATED. ANY DISCREPANCIES BETWEEN THE INFORMATION CONTAINED IN THESE DRAWINGS AND THE ACTUAL VERFIELD SITE CONDITIONS SHALL BE IMMEDIATELY BROUGHT TO THE ATTENTION OF CROWIN CASTLE AND PAUL J., FORD & COMPANY SO THAT ANY CHANGES AND/OR ADJUSTMENTS, IF NECESSARY, CAN BE MADE TO THE DESIGN AND DRAWINGS.
THE EXISTING UNKENFORCED MONDPOLE STRUCTURE DOES NOT HAVE THE STRUCTURAL CAPACITY TO CARRY ALL OF THE ANTENNA AND PLATFORM LOADS SFOWN ON THESE DRAWINGS AT THE REQUIRED MINIMUM THEAL 222.F BASIC WIND SPECES. DO NOT INSTALL ANY ADDITIONAL OR NEW ANTENNA AND PLATFORM LOADS STOWN ON THESE DRAWINGS AT THE REQUIRED MINIMUM THEAL 222.F BASIC WIND SPECES. DO NOT INSTALL ANY ADDITIONAL OR NEW ANTENNA AND PLATFORM LOADS STOWN ON THESE DRAWINGS AT THE REQUIRED MINIMUM THEAL 222.F BASIC WIND SPECES. DO NOT INSTALL ANY ADDITIONAL OR NEW ANTENNA AND PLATFORM LOADS STOWN ON THESE DRAWINGS AT THE REQUIRED MINIMUM THEAL 222.F BASIC WIND SPECES. DO NOT INSTALL ANY ADDITIONAL OR NEW ANTENNA AND PLATFORM LOADS STOWN ON THESE DRAWINGS AT THE REQUIRED MINIMUM THEAL 222.F BASIC WIND SPECES.

THE EXISTING UNREINFORCED MONOPICLE STRUCTURE DUES NOT HAVE HE SINCL LIVAR, CAPACITY ID CARRY ALLO OF THE ANTENNA AND PLATFORM LONG SHOWN ORTH-SEE DEAMINGS AT THE REQUIRED MINIMUM TAKEIA-222-F BASIC WIND SPEEDS. DO NOT INSTALL ANY ADDITIONAL OR NEW ANTENNA AND PLATFORM LONG STRUCTURE WAS AND PLATFORM LONG STRUCTURE. AND PLATFORM LONG STRUCTURE WAS AND PLATFORM LONG STRUCTURE. AND PLATFORM LONG STRUCTURE WAS AND PLATFORM LONG STRUCTURE. AND PLATFORM LONG STRUCTURE WAS AND PLATFORM LONG STRUCTURE. AND PLATFORM LONG STRUCTURE STRUCTURE IS DESIGNED TO BE SELF-SUPPORTING BE PROVIDED. THIS STRUCTURE IS DESIGNED TO BE SELF-SUPPORTING AND STABLE AFTER THE INSTALLATION OF THE REINFORCING REPAIR SYSTEM HAS BEEN PROPERLY AND ADEQUATELY COMPLETED. IT IS THE CONTRACTOR'S SOLE RESPONSIBILITY OF INSURE THE SAFETY AND STABILITY OF THE MONOPOLE AND ITS COMPONENT PARTS DURING FIELD MODIFICATIONS. THIS INSURED THE SECRESIAN SYSTEM HAS BEEN PROPERLY AND ADEQUATELY COMPLETED. IT IS THE CONTRACTOR'S SOLE RESPONSIBILITY OF INSURE THE SAFETY AND STABILITY OF THE MONOPOLE AND ITS COMPONENT PARTS DURING FIELD MODIFICATIONS. THIS INSCLUDES, BUT IS NOT LIMITED TO, THE ADDITION OF WHATEVER TEMPORARY BRACKING, GUYS OR TIE DOWNS THAT MAY BE INCESSARY. SUCH MATERIAL SHALL BE REMOVED AND SHALL REMAIN THE PROPERTY OF THE CONTRACTOR AFTER THE COMPLETION OF THE PROVIDE. THE MODIFICATION OF THE PROVIDE. THE CONTRACTOR SHALL FOLLOW ALC TROWN CASTLE CUTTING, WELDING, FIRE PREVENTION AND SAFETY GUIDELINES. THE CONTRACTOR SHALL FOLLOW ALC TROWN CASTLE CUTTING WELDING, AND SAFETY GUIDELINES. THE CONTRACTOR SHALL FOLLOW ALC TROWN CASTLE CUTTING WAS AND SHALL BE SUBJECTIVED. THE CONTRACTOR SHALL FOLLOW ALC TROWN CASTLE CUTTING WAS AND ADDITIONATION OF THE CONTRACTOR SHALL FOLLOW AND SHALL BE SUBJECT ON THE CONTRACTOR SHALL FOLLOW AND SHALL BE SUBJECT OF THE CONTRACTOR SHALL FOLLOW AND SHALL B

B. (SECTION NOT USED)

C. SPECIAL INSPECTION AND TESTING
ALL WORK SHALL BE SUBJECT TO REVIEW AND OBSERVATION BY THE OWNER'S REPRESENTATIVE AND
THE OWNER'S AUTHORIZED INDEPENDENT INSPECTION AND TESTING AGENCY, REFER TO CROWN
CASTLE DOCUMENT BENGSOW-1006 FOR SPECIFICATION.
ANY SUPPORT SERVICES PERFORMED BY THE ENGINEER DURING CONSTRUCTION SHALL BE
DISTINGUISHED FROM CONTINUOUS AND DETAILE DI INSPECTION SERVICES WHICH ARE FURNISHED BY
OTHERS. THESE SUPPORT SERVICES PERFORMED BY THE ENGINEER ARE PERFORMED SOLELY FOR
THE PURPOSE OF ASSISTING IN OUALITY CONTROL AND IN ACHIEVING COMFORMANCE WITH CONTRACT
DOCUMENTS. THEY DO NOT GUARANTEE CONTRACTOR'S PERFORMANCE AND SHALL NOT BE
CONSTRUED AS SUPERVISION OF CONSTRUCTION.
OBSERVED DISCREPANCIES BETWEEN THE WORK AND THE CONTRACT DOCUMENTS SHALL BE
CORRECTED BY THE CONTRACTOR'S AND ADDITIONAL COST.
AN INDEPENDENT QUALIFIED INSPECTION/TESTING AGENCY SHALL BE SELECTED, RETAINED AND PAID
POR BY THE OWNER FOR THE SOLE PURPOSE OF INSPECTION, TESTING, TO COUMENTING, AND
APPROVING ALL WELDING AND FIELD WORK PERFORMED BY THE CONTRACTOR.

(A.) ACCESS TO ANY PLACE WHERE WORK IS BEING DONE SHALL BE PERMITTED AT ALL TIMES,
INTERRYPTION TO, AND COORDINATE WITH, THE YORK KIND SHOWS AS TO CAUSE A MINIMUM OF
INTERRYPTION TO, AND COORDINATE WITH, THE HOWER AND ACCESS TO ANY PLACE WHERE WORK IS BEING DONE SHALL BE PERMITTED AT ALL TIMES,

(B.) THE INSPECTION AGENCY SHALL SO SCHEDULE THIS WORK AS TO CAUSE A MINIMUM OF
INTERRYPTION TO, AND COORDINATE WITH, THE TWORK IN PROFISE SIT IS THE
CONTRACTOR'S RESPONSIBILITY TO COORDINATE THE WORK SCHEDULE WITH THE TESTING
AGENCY, THE CONTRACTOR'S THE STING AGENCY SHALL HIS PROFILE THE FOLLOWING
SERVICES FOR THE OWNER, THE TESTING AGENCY SHALL HIS PERFORM THE FOLLOWING
SERVICES FOR THE OWNER, THE TESTING AGENCY SHALL HIS PERFORM THE FOLLOWING
SERVICES FOR THE OWNER, THE TESTING AGENCY SHALL HIS PERFORMED WHITH THE THE SING AGENCY SHALL HIS PERFORMED THE FOLLOWING
SERVICES FOR THE OWNER, THE TESTING AGENCY SHALL HIS PROFILE THE FOLLOWING INSPECTORS INCLUDING AWAS CERTIFIED WE AND COMMENSURATE WITH THE SCOPE AND TYPE OF INSPECTION WORK TO BE PERFORMED.

A SENERAL.

(1.) PHEFORM PERIODIC CHASTIE OBSERVATION, INSPECTION, VERRICATION, AND TESTING DURING (1.) PHEFORM PERIODIC CHASTIE OBSERVATION, INSPECTION, VERRICATION, AND TESTING DURING (1.) PHEFORM PERIODIC CHASTIC OBSERVATION, INSPECTION, VERRICATION, AND TESTING DURING INMEDIATELY WHEN FIELD PROBLEMS OR DISCREPANCIES OCCUR.

B. FOUNDATIONS CONCRETE AND SOL, PERPARATION—IN OTREGURED)

STRUCTURAL STEEL

(1.) CHECK THE STEEL ON THE JOB WITH THE PLANS.

(2.) CHECK MILL CERTIFICATIONS.

(3.) CHECK MILL CERTIFICATIONS.

(4.) INSPECT STEEL MEMBERS FOR DOLTS FOR CONFORMANCE WITH DRAWINGS.

(5.) CALL FOR LABORATORY TEST REPORTS WHEN IN DOUBT.

(6.) CHECK STEEL MEMBERS FOR DISCRESSIVE PRUST, FLAWS AND BURNED HOLES.

(7.) CHECK STEEL MEMBERS FOR DISCRESSIVE PRUST, FLAWS AND BURNED HOLES.

(8.) CHECK STEEL MEMBERS FOR DISCRESSIVE PRUST, FLAWS AND BURNED HOLES.

(9.) CHECK STEEL MEMBERS FOR DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST, TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN OF THE MUST WHEN DISCRESSIVE PRUST TOWN

(3) CHECK FOR SURFACE FINISH SPECIFIED, GALVANAZEV,
(8) CHECK BOLT TIGHTENING ACCORDING TO AISC "TURN OF THE NUT" METHOD.

WELDING.

(1) VERIFY FIELD WELDING PROCEDURES, WELDERS, AND WELDING OPERATORS, MOT DEEMED PREDUALFIELD. IN ACCORDANCE WITH AWS D1.1.

(2) INSPECT FIELD WELDED CONNECTIONS IN ACCORDANCE WITH THE REQUIREMENTS SPECIFIED AND IN ACCORDANCE WITH AWS D1.1.

(3) APPROYER SECURING SEQUENCE.

(4) A PROGRAM OF THE APPROVED SEQUENCES SHALL BE SUBMITTED TO THE OWNER BEFORE WELDING SEGUENCE.

(4) INSPECT WELDING SEGUENCE.

(4) INSPECT WELDING SEGUENCE SOLLOWS AND IN ACCORDANCE WITH AWS D1.1:

(A) INSPECT WELDING ECURPAENT FOR CAPACITY, MAINTENANCE AND WORKING CONDITIONS.

(6) VERIFY SPECIFIED ELECTRODES AND HANDLING AND STORAGE OF ELECTRODES FOR CONFORMANCE OF SPECIFICATIONS.

(C) INSPECT PREHEATING AND INTERPASS TEMPERATURES FOR CONFORMANCE WITH AWS D1.1.

(D) VISUALLY INSPECT ALL WELDS AND VERIFY THAT QUALITY OF WELDS MEETS THE REQUIREMENTS OF AWS D1.1.

(E) SPOT TEST AT LEAST ONE FILLET WELD OF EACH MEMBER USING MAGNETIC PARTICLE OR DIFFERENT THE REPORTS BY TESTING LACE AND ALL OF THE PROPROVED PLANS.

(G) VERIFY THAT THE BASE METAL CONFORMS TO THE DRAWINGS.

(H) REVIEW THE REPORTS BY TESTING LACE AND FREE FROM SLAG.

(I) INSPECT THE DEFORT SET THE LIB AND FREE FROM SLAG.

(I) INSPECT THE PROTECTION OF WELDS AND FREE FROM SLAG.

(II) INSPECT THE DEFORT SET OF THE LIB AND THE PROW SLAG.

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(III) INSPECT THE THE CALL OF THE AND THE PROW SLAG.

(III) INSPECT THE THE CALL OF THE AND THE PROW SLAG.

(IVERTIFY

UNEED TO SEE ITHAT WELLDS AND CLEAN AND PREE PROM STORY INSPECT ROST PROTECTION OF WELDS AS PER SPECIFICATIONS.
CHECK THAT DEFECTIVE WELDS ARE CLEARLY MARKED AND HAVE BEEN ADEQUATELY REPAIRED.

F, REPORTS:
(1.) COMPILE AND PERIODICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER,

(1,1 COMPILE AND PERIODICALLY SUBMIT DALLY INSPECTION REPORTS TO THE OWNER.

6. THE INSPECTION PLAN OUTLINED HEREIN IS INTENDED AS A DESCRIPTION OF GENERAL AND SPECIFIC TIEMS OF CONCERN, IT IS NOT INTENDED TO BE ALL-INCLUSIVE, IT DOES NOT LIMIT THE TESTING AND INSPECTION AGENCY TO THE ITEMS LISTED, ADDITIONAL TESTING, INSPECTION, AND CHECKING MAY BE REQUIRED AND SHOULD BE ANTICIPATED. THE TESTING AGENCY SHALL USE THEIR PROFESSIONAL JUDGMENT AND KNOWLEDGE OF THE JOB SITE CONDITIONS AND THE CONTRACTORS PERFORMANCH TO SEED WHAT OTHER ITEMS REQUIRED. ADDITIONED, AND THE CONTRACTORS PERFORMANCH TO SEED WHAT OTHER ITEMS REQUIRED. ADDITIONED, AND THE CONTRACTORS PERFORMANCH TO SEED WHAT OTHER ITEMS REGISTED AND DISCREDE. AND DISCREDANCES AND PROFESSIONAL BE BROUGHT IMMEDIATELY TO THE OWNERS ATTENTION. RESOLUTIONS ARE NOT TO BE MADE WITHOUT THE OWNER'S REVIEW AND SPECIFIC WITHIN THE CONTRACTOR. AND TO SEED WITHOUT THE OWNER'S REVIEW AND SPECIFIC WITHIN CONTRACTOR AND FILED AS DAILY REPORTS TO THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WITHITEN ACCEPTANCE OR REJECTION WHICH WILL BE GIVEN TO THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WITHIT AND ACTION WHICH WILL SHOW THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WITHITEN ACCEPTANCE OR REJECTION WHICH WILL BE GIVEN TO THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WITHITEN ACCEPTANCE OR REJECTION WHICH WILL SET STANDAY OF OWNER. THIS WITHIT AND ACTION WILL GIVE THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WITHIT AND ACTION WILL GIVE THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WITHIT AND ACTION AND ADDRESS TO THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS STATUTORY OBLIGATIONS. THE CONTRACTOR HAS THE SOLE RESPONSIBILITY FOR ANY DEVARDOUS FROM THE CONTRACTOR AND THE STRING AGENCY WILL NOT REPLACE THE CONTRACTOR'S QUALITY CONTROL PERSONNEL.



BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

	PROJECT: 37514-2522.001.7700		
	DRAWN BY:	GENERAL NOTES	
	CHECKED BY: C.M.M.		
	APPROVED BY:	0.4	
	DATE: 11-21-2014	5-1	

STRUCTURAL STEEL
STRUCTURAL STEEL MATERIALS, FABRICATION, DETAILING, AND WORKMANSHIP SHALL CONFORM
TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:
BY THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (ASS):
(A.) SPECIFICATION FOOT THE DESIGN, PASRICATION AND ENECTION OF STRUCTURAL STEEL

10.

STRUCTURAL STEEL MATERIALS, FABRICATION, DETAILING, AND WORKMANSHIP SHALL CONFORM TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:

BY THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC):

(A.) "SPECIFICATION FOR THE DESION, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS."

(B.) "SPECIFICATION FOR THE DESION, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS."

(C.) "SECFICIATION FOR TRUCTURAL JOINTS USING ASTM A325 OR A490 BOLTS," AS APPROVED BY THE RESEARCH COUNCIL ON STRUCTURAL CONNECTIONS OF THE CONTROL OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE AMERICAN WELDING SOCIETY (WS):

(C.) "STRUCTURAL WELDING COCE STEEL BUILDINGS AND BRIDGES" (PARAGRAPH 4.2.1 SECRETICALLY EXCLUDED).

BY THE AMERICAN WELDING SOCIETY (WS):

(A.) "STRUCTURAL WELDING COCE STEEL BUILDINGS AND BRIDGES" (PARAGRAPH 4.2.1 SECRETICAL STEEL OF THE AMERICAN WELDING SOCIETY (WS):

(A.) "STRUCTURAL STEEL BY COLOR OF STEEL BUILDINGS AND BRIDGES" (PARAGRAPH 4.2.1 SECRETICAL STEEL OF THE AMERICAN WELDING SOCIETY (WS):

(A.) "STRUCTURAL STRUCTURAL BOTS, INCLUDING THE AMAY MOD BOLTS WITH SHEAR SLEEVES, ACCORDING TO THE REQUIREMENTS OF THE AISC TURN OF THE AUT" METHOD. TIGHTEN BOLTS 1/3 TURN PAST THE SHILD STRUCT CONDITION AS DEFINED BY AISC.

WELDED CONNECTIONS SHALL CONFORM TO THE LATEST REVISED COOP OF THE AMERICAN WELDING SOCIETY, ANY BOT, ALL WELD ELECTRODES SHALL BE EBOXX UNLESS NOTED OTHERWISE ON THE DRAWINGS.

ALL WELDED CONNECTIONS SHALL BE MADE BY WELDERS CERTIFIED BY AWS, CONTRACTOR SHALL SUBMIT WELDERS CERTIFICATION AND QUALIFICATION DOCUMENTATION TO THE OWNERS TESTING AGENCY OF REVIEW AND APPROVAL PRIOR TO CONSTRUCTION.

STRUCTURAL STEEL PLATES SHALL CONFORM TO CONSTRUCTION.

STRUCTURAL STEEL PLATES SHALL CONFORM TO CONSTRUCTION.

STRUCTURAL STEEL PLATES SHALL CONFORM TO CONSTRUCTION.

STRUCTURAL STEEL PLATES SHALL BE PREPARED AS REQUIRED FOR FIELD WELDING FOR THE METADOL OF THE PLATES SHALL BE CONFORMED TO THE RESEARCH OF THE PLATES SHALL BE CONFO

(C.)

Ē. BASE PLATE GROUT - [NOT REQUIRED]

FOUNDATION WORK - (NOT REQUIRED)

CAST-IN-PLACE CONCRETE - (NOT REQUIRED)

Н, EPOXY GROUTED REINFORCING ANCHOR RODS - (NOT REQUIRED)

G.

TOUCH UP OF GALVAINZING
THE CONTRACTOR SHALL TOUCH UP ANY ANDIOR ALL AREAS OF GALVANIZING ON THE EXISTING
THE CONTRACTOR SHALL TOUCH UP ANY ANDIOR ALL AREAS OF GALVANIZING ON THE EXISTING
STRUCTURE OR NEW COMPONENTS THAT ARE DAMAGED DIRING REPORT OF STRUCTURE OR NEW COMPONENTS THAT ARE DAMAGED DRI ARRADED DIRING CONSTRUCTION
GALVANIZED SURFACES DAMAGED DIRING TRANSPORTATION OR ERECTION AND ASSEMBLY AS
WELL AS ANY AND ALL ABRASIONS, CUTS, FIELD DRILLING, AND ALL FIELD WELDING SHALL BE
TOUCHED UP WITH TWO (2) COATS OF ZRC-BRAND ZINC-RICH COLD GALVANIZING COMPOUND, FLAN
HICKNESS PER COAT SHALL BE: WET 3.0 MIS. SPM 1.5 BILLS. APPLY PER ZRC (MANUFACTURER)
RECOMMENDED PROCEDURES. CONTACT ZRC AT 1-800-831-3275 FOR PRODUCT INFORMATION.
CONTRACTOR SHALL CLEAR AND PREPARE ALL FIELD WELDS ON GALVANIZED AND PRIME PAINTED
SUBFACES FOR TOUCH-UP COATING IN ACCORDANCE WITH AWS D.1.1. THE OWNERS TESTING
AGENCY SHALL VERRY THE PREPARED SURFACE PRIOR TO APPLICATION OF THE TOUCH-UP
COATING.
THE OWNERS TESTING AGENCY SHALL TEST AND VERIFY THE COATING THICKNESS AFTER THE
CONTRACTOR HAS APPLIED THE ZRC COLD GALVANIZING COMPOUND AND IT HAS SUFFICIENTLY
DRIED. AREAS FOUND TO BE IMADEQUATELY COATED, SHALL BE RE-COATED BY THE CONTRACTOR
AND RE-TESTED BY THE TESTING AGENCY.

HOT DIP GALVANIZING
HOT-DIP GALVANIZE ALL
STRUCTURAL STEEL MEMBERS AND ALL STEEL ACCESSORIES, BOLTS,
WASHERS, ETC, PER ASTM A123 OR PER ASTM A153, AS APPROPRIATE,
PROPERLY PREPARE STEEL ITEMS FOR GALVANIZING,
DRILL OR PUNCH WEEP AND/OR DRAINAGE HOLES AS REQUIRED.
ALL GALVANIZING SHALL BE DONE AFTER FABRICATION IS COMPLETED AND PRIOR TO FIELD
MISTALLATION.

INSTALLATION,

PERPETUAL INSPECTION AND MAINTENANCE BY THE OWNER

AFTER THE CONTRACTOR HAS SUCCESSFULLY COMPLETED THE INSTALLATION OF THE MONOPOLE

REINFORCING SYSTEM AND THE WORK HAS BEEN ACCEPTED BY THE OWNER, THE OWNER WILL BE

RESPONSIBLE FOR THE LONG TERM AND PERPETUAL INSPECTION AND MAINTENANCE OF THE POLE

AND REINFORCING SYSTEM.

THE MONOPOLE REINFORCING SYSTEM MOICATED IN THESE DOCUMENTS USES REINFORCING

COMPONENTS THAT INVOLVE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL

POLE STRUCTURE. THESE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL

POLE STRUCTURE. THESE FIELD WELDING CONNECTIONS ARE SUBJECT TO CORROSION DAMAGE

AND DETERIORATION IF THEY ARE NOT PROPERLY MAINTAINED AND COVERED WITH CORROSION

PREVENTIVE COATING SUCH AS THE ZRG GALVANIZING COMPOUND SPECIFIED PREVIOUSLY. THE

STRUCTURAL LOAD CARRYING CAPACITY OF THE REINFORCED POLE SYSTEM IS DEPENDENT UPON

THE INSTALLED SIZE AND QUALITY, MAINTAINED SOUND CONDITION AND STRENGTH OF THESE FIELD

WELDED CONNECTIONS. ANY CORROSION OF, DAMAGE TO, FATIGUE, FRACTURE, ANDIOR

DETERIORATION OF THESE WELDS ANDIOR THE CONNECTED COMPONENTS WILL RESULT IN THE

LOSS OF STRUCTURAL LOAD CARRYING CAPACITY AND MAY LEAD TO FAILURE OF THE

STRUCTURAL SYSTEM. THEREFORE, IT IS IMPERATIVE THAT THE OWNER REQULARLY INSPECTS,

MAINTAINS, AND REPAIRS AS NECESSARY, ALL OF THESE WELDS, CONNECTIONS, AND

COMPONENTS FOR THE LIFE OF THE STRUCTURE.

THE OWNER SHALL REFER TO TIMELA 2222-F-1996, SECTION 14 AND ANNEX E FOR RECOMMENDATIONS

FOR MAINTENANCE AND INSPECTION. THE FREQUENCY OF THE INSPECTION AND MAINTENANCE

INTERVALS IS TO BE DETERMINED BY THE OWNER BASED UPON ACTUAL SITE AND ENVIRONMENTAL

CONDITIONS, PAUL J. FORD & COMPANY RECOMMENDS THAT A COMPETER AND ENVIRONMENTAL

CONDITIONS, PAUL J. FORD & COMPANY RECOMMENDS THAT A COMPETER AND ENVIRONMENTAL

CONDITIONS, PAUL J. FORD & COMPANY RECOMMENDED THAT THE OWNER BEFORD TO THE THE SEVERE

WIND AND/OR ICE STORMS OR OTHER EXTREME LOADING CONDITIONS'

SECTION 14.1, NOTE 1: "IT IS RECOMMENDED TH



PH: (724) 416-2000

BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

PROJECT: 37514-2522.001.7700 GENERAL NOTES CHECKED BY C.M.M. PROVED B

AJAX BOLT NOTE SHEET: REV. 1.5, 5-12-2014

NOTES:

- 1. ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
 - 2. ALL STRUCTURAL BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS' DEC. 31, 2009.
 - 3. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND DETAIL BELOW FOR THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
 - 4. ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. DTI'S SHALL BE THE SQUIRTER® STYLE, MADE TO ASTM F959 LATEST REVISION; AND HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A HARDNESS OF RC 38 OR HIGHER.

NOTES FOR AJAX M20 'ONE-SIDE BOLTS WITH DIRECT TENSION INDICATORS (DTI'S):

DTI'S REQUIRED: DTI'S SHALL BE "SELF-INDICATING" SQUIRTER® STYLE DTI'S MADE WITH RED DURABLE SQUIRT MEDIA EMBEDDED IN THEM, INSPECTED BY MEANS OF THE VISUAL EJECTION OF SILICONE AS THE DTI PROTRUSIONS COMPRESS. SQUIRTER® DTI'S SHALL BE CALIBRATED PER MANUFACTURER'S INSTRUCTIONS PRIOR TO USE.

THE DIRECT TENSION INDICATOR (DTI) WASHERS SHALL BE THE "SQUIRTER® STYLE" AS MANUFACTURED BY APPLIED BOLTING TECHNOLOGY PRODUCTS' INC.:

PART NUMBER: 2DTIM208MGAFSIF

DESCRIPTION; P.C. 8.8 DTI SQUIRTER WASHER WITH RED DURABLE SQUIRT MEDIA DESIGNED SPECIFICALLY FOR THE AJAX M20 ONESIDE BOLT. FINISH SHALL BE ZINC GALVANIZED AS PROVIDED BY THE DTI MANUFACTURER.

DISTRIBUTOR CONTACT DETAILS:

ALLFASTENERS 15401 COMMERCE PARK DR. BROOKPARK, OHIO 44142 PHONE: 440-232-6060

E-MAIL: SALES@ALLFASTENERS,COM

DTI; USE DIRECT TENSION INDICATOR (DTI) WASHERS COMPATIBLE WITH 20 MM (M20) NOMINAL A325 BOLTS FOR THE AJAX M20 BOLTS. DTI'S SHALL NOT BE HOT-DIP GALVANIZED. DTI'S SHALL BE MECHANICALLY GALVANIZED (MG) BY THE COLD MECHANICAL PROCESS ONLY AS PROVIDED BY THE DTI MANUFACTURER.

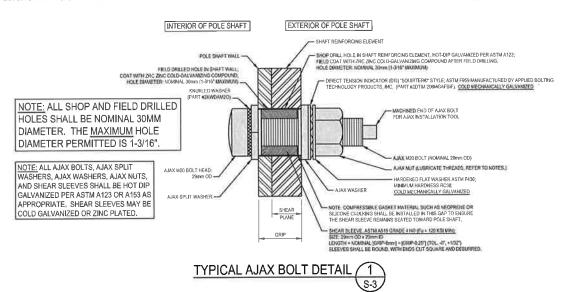
HARDENED WASHERS REQUIRED: USE A HARDENED WASHER FOR A 20 MM (M20) NOMINAL BOLT BETWEEN THE TOP OF THE DIRECT TENSION INDICATOR (DTI) WASHER AND THE NUT OF THE AJAX M20 BOLTS. HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A MINIMUM HARDNESS OF RC 38 OR HIGHER. THE HARDENED WASHERS SHALL BE MECHANICALLY GALVANIZED BY THE COLD MECHANICAL PROCESS. ALTERNATIVELY, CORRECTLY MADE HOT DIP GALVANIZED HARDENED FLAT WASHERS HAVING A MINIMUM HARDNESS OF RC 38 CAN BE USED; CONTRACTOR SHALL PROVIDE DOCUMENTATION OF WASHER SPECIFICATION AND HARDNESS.

NUT LUBRICATION REQUIRED: PROPERLY LUBRICATE THE THREADS OF THE NUT OF THE AJAX BOLT SO THAT IT CAN BE PROPERLY TIGHTENED WITHOUT GALLING AND/OR LOCKING UP ON THE BOLT THREADS, CONTRACTOR SHALL FOLLOW DTI MANUFACTURER INSTRUCTIONS FOR PROPER LUBRICATION AND TIGHTENING.

NOTE: COMPLETELY COMPRESSED DTI'S SHOWING NO VISIBLE REMAINING GAP ARE ACCEPTABLE. DTI WASHERS SHALL BE PLACED DIRECTLY AGAINST THE OUTER AJAX WASHER WITH THE DTI BUMPS FACING AWAY FROM THE AJAX WASHER. PLACE A HARDENED WASHER BETWEEN THE DTI AND THE AJAX NUT. THE DTI BUMPS SHALL BEAR AGAINST THE UNDERSIDE OF A HARDENED FLAT WASHER, NEVER DIRECTLY AGAINST THE NUT.

CONTRACTOR SHALL FOLLOW DTI MANUFACTURER'S INSTRUCTIONS FOR INSTALLATION, LUBRICATION, TIGHTENING AND INSPECTION.

INSPECTION REQUIRED: ALL AJAX BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009, BY A QUALIFIED BOLT INSPECTOR. DURING INSTALLATION, THE BOLT INSPECTOR SHALL VERIFY AND DOCUMENT: THE SHOP-DRILLED AND FIELD-DRILLED HOLE SIZES; THE INSTALLATION OF THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S TENSIONING PROCEDURE. IN ADDITION, ALL AJAX BOLTS AND DTI'S SHALL BE VISUALLY INSPECTED ACCORDING TO THE DTI MANUFACTURER'S INSTRUCTIONS. THE BOLT INSPECTOR SHALL PROVIDE COMPLETE PHOTO DOCUMENTATION OF ALL BOLTS AFTER TIGHTENING CLEARLY SHOWING THE CONDITION OF THE DTI'S,

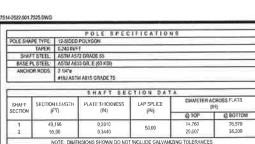




BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT: 37514-2522.001.7700

DRAWN BY:
I.M.
CHECKED BY:
C.M.M.
APPROVED BY:
DATE:
11-21-2014

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CONTRACTOR SHALL PROVIDE ASTM AND SHIM PLATES BELOW SUP JOINTS, THE SHIM PLATES SHALL BE PLACED BETWEEN THE NEW SHART REINFORCEMENT AND THE EXISTING POLE SHAFT FROM THE SUB JOINT TO THE NEW SHAFT REINFORCEMENT SHULE PLATE LOCATION AND A EXTRA LONG "SPLICE SHIM" SHALL BE PLACED BETWEEN THE NEW UPPER AND LOWER SHAFT REINFORCEMENT FLATES AT THE SHAFT REINFORCEMENT SHALE BETWEEN THE SHAFT REINFORCEMENT SHAF

MODIFICATIONS:

(A) INSTALL NEW TRANSITION STIFFENERS AT BASE PLATE, SEE SHEET S-5.

B INSTALL NEW SHAFT REINFORCING SEE CHART

				NEW CCIFE	AT PLATE (S	S KSARENFOR	RCING SCHED	ULE			
BOTTON	TOP ELEVATION	FLATO: DEGREE SEPARATION	ELEMENT	ELEMENT LENGTH	ELEMENT QUANTITY	APPROXIMATE AJAX BOLTS PER ELEMENT	APPROXIMATE TOTAL AJAX BOLT QUANTITY	TERMINATION BOLTS BOTTOM	TERMINATION BOLTS (TOP)	MAXIMUM INTERMEDIATE BOLT SPACING	TOTAL STEEL WEIGHT
\$150	W.F.	12 FEB (10	0010509 0010509	26.07	0	- 6	126	H.	14	, IA,	243,65
2.5	861.91	12/04/19	001AFF 00143638	37 (*	3.	35	618	10	89	#	1016181
						_	281				ATTIVES.

HOTES

LI AND BS 15 ART TO DE DESCRIPTION AND OSSES SOMEWED PROCEDURES WITH MACKING STEEL SAME.

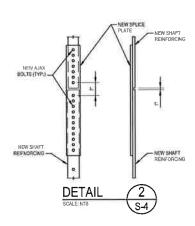
21 ALS BELL SHAP SENDE OF SAME WAZED FROM ARCOCKING SOME AND THAN TOWN A FEBRUAR LEAST FROM A STEEL SHAP GROWN WAZED FROM A STEEL SHAP AND STEEL SHAP GROWN WAZED FROM A STEEL SHAP AND STAN AND STAN

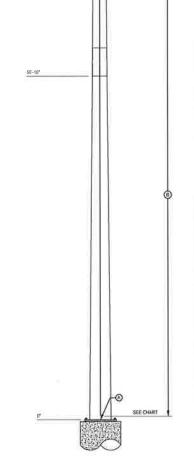
SPLICE PLATE INSTALLATION CHART								
ELEVA1IÓN	THICKNESS		FLAT PLATE LENGTH	PLAT PLATE	WELD LENGTH PER SIDE	TOTAL WELD LENGTH	AJAX BOLTS PER SPLICE*	TOTAL STEEL
20.7	112	413"	1 F		- 0	.7	- 11	548189
				-	-	- 22		430190

* BOLTS INCLUDED IN THE TOTAL QUANTITY LISTED IN THE FLAT PLATE INSTALLATION CHART.

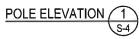
		NEW SHIM CHA	NT.	
PIE, 2HIR	QUANTITY	BHOW WOTH	SHIM LENGTH	DIAMETER
3.		100	- 40	8.540

SHIMS ARE FOR BIDDING PURPOSED ONLY, FINAL SHIM REQUIREMENTS TO BE DETERMINED BY CONTRACTOR DURING FABRICATION,





SEE CIVART



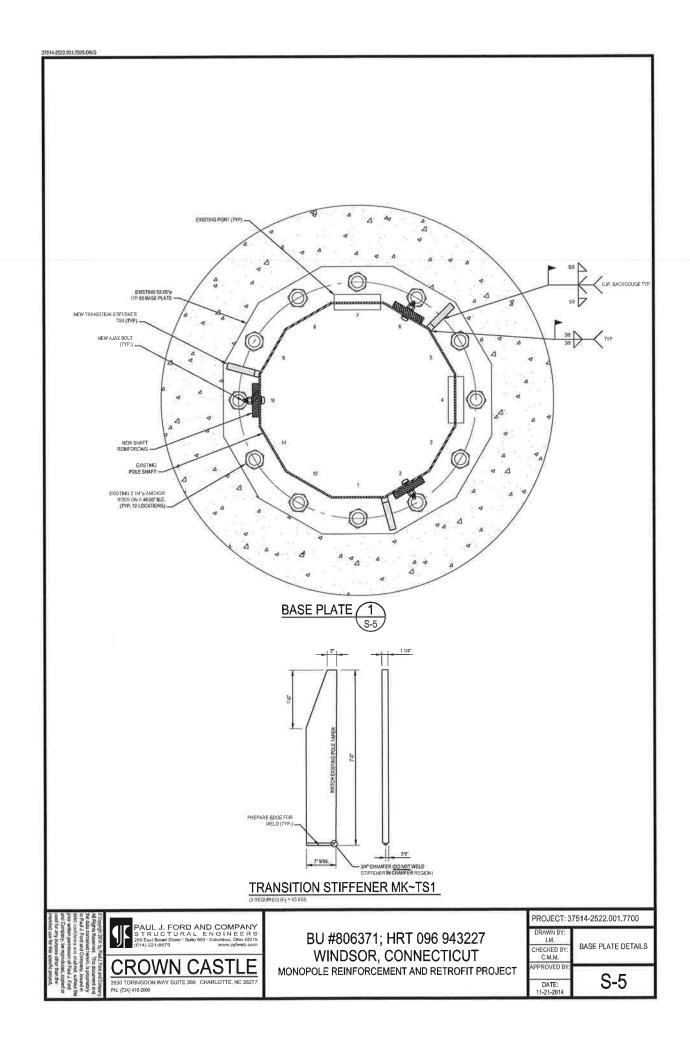
PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 Easl Broad Street * Suste 600 * Columbus: Orio 43215 (614) 221-6679 www.pjf/web.com **CROWN CASTLE**

WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

BU #806371; HRT 096 943227

PROJECT: 37514-2522.001.7700 LM. MONOPOLE PROFILE CHECKED BY

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MEDIAL TO MEPECTION IMPLY A VISUAL INSPECTION OF TOWER MEDIFICATIONS AND A REVIEW OF CONSTRUCTION INSPECTIONS O OTHER REPORTS TO ELEVIEW THE INSTALLATIC WAS CONSTRUCTED IN ACCIDENCE WITH THE CONTRACT DOCUMENTS INVALLY THE OPENCIATION FLOWINGS AS DESIGNED OF THE EMPLECEMENT RECORDS (1959).

THE MILISTO CONFIRM INSTALLATION CONFIDURATION AND WORKMANSHIP ONLY AND IS HOT A REVIEW OF THE MODIFICATION DESIGN TISBER, DISP DOES THE MILISPECTION TAKE OWNERSHIP OF THE UDDIFICATION DESIGN. OWNERSHIP OF THE STRUCTURAL MUDIFICATION DESIGN EPPECTURES AND INTERPRITY RESIDES WITH THE DEGRAFAL TURNED.

ALL MIS SMALL BE CONDUCTED BY A CROWN ERIGNEERING VENDOR (ASV) OR ENGNEERING SERVICE VENDOR (ASSV) THAT IS APPROVED TO PEPFORM ELEVATED WORK FOR CROWN. SEE END BUL/10/13/UST OF AFPROVED MI VENDORS

TO ENSURE THAT THE REQUIREMENTS OF THE MURCHEST, IT IS VITAL THAT THE CENERAL CONTRACTOR (GC) AND THE MUNSPECTOR BEGIN COMMUNICATING AND CONDINATING AS SOON AS A POT IS RECEIVED. IT IS EXPECTED THAT EACH PARTY WILL BE PROMITIVE IN REACHING OUT TO THE OTHER PARTY. IF CONTRACT REPORTATION IN AT MANUAL CONTRACT YOR'S CONTRACT (PCC).

REFER TO ENG-SOW-10007 MODIFICATION INSPECTION SOW FOR FURTHER DETAILS AND REQUIREMENTS.

MINSPECTOR THE MINSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A POPOR THE MINTO, AT A MINIMUM

- REVIEW THE PROUREMENTS OF THE MI CHECKLIST
 WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT CHISITE INSPECTIONS. INCLUDING FOUNDATION INSPECTIONS.

THE MINISPECTOR IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (SCI INSPECTION AND TEST REPORTS, REMIEWING THE DOCUMENTS FOR ADHERENCE TO THE CONTRACT DOCUMENTS, CONDUCTING THE IN MELD INSPECTIONS, AND SUBMITTING THE MIREPORT

GENERAL CONTRACTOR
THE BUTS PROGRED TO CONTACT THE MI INSPECTOR AS SOON AS RECEIVING A PO FOR THE MODIFICATION BISTALLATION OR TURKKEY
PRODUCT TO A TAX MINEMAL

TO A THE MINEMAL TO A THE MINEMAL THE MINEMAL TO A THE MODIFICATION OF THE MODIFICATION OF THE MODIFICATION OF THE MINEMAL THE MINEMA

- REVIEW THE REQUIREMENTS OF THE MICHECKUST.
 WORK WITH THE MI MERCENDATION CONTROL TO CONTROL TO CONDUCT ON SITE MERPECTIONS INCLUDING FOUNDATION ASPECTIONS.
 SETTER (NORTHWAND ALL INFECTION AND TESTIONS REQUIREMENTS.

HEIGG SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IN ACCORDANCE WITH THE REQUIREMENTS OF THE MI MEDKUST AN DEM 3-SOWN 0007

RECOMMENDATIONS THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING

- It is suggested that the CC provide a minutal of 5 suspess days notice preferrable to to them inspector as to when the site will be ready for them it due conducted. The site will be ready for them it due conducted. The conductivity is entire project.

 The CS also inspector cookinate closely the projection of the project.

 WHEN PASSIBLE IT IS PREFERRED TO HAVE THE CO AND MINISPECTOR ON-SITE SINULTANEOUSLY FOR AIM GUY VIAVE TENSIONAND OF PROTECTIONS FROM TO CONDUCTING THE FOUNDATION HIS PRECIONS TO ALLOW FOUNDATION AND MINISPECTORS, TO COMPANIE WITH OR SITE WAY TO AND THE MINISPECTOR SITE WITH OR WAY TO AND THE MINISPECTOR ON SITE BURNED THE MINISPECTOR OF THE MINISPECTOR SITE WITH A MINISPECTOR THE OWN OF ADAPTION OF CONSIDERABLE THE MINISPECTOR THE OWN OF ADAPTION OF CONSIDERABLE THE MINISPECTOR THE OWN OF ADAPTION OF CONSIDERABLE THE MINISPECTOR THE OWN OF ADAPTION OF CONSIDERABLE THE MINISPECTOR THE OWN OF ADAPTION OF CONSIDERABLE THE MINISPECTOR THE OWN OF ADAPTION OF CONSIDERABLE THE MINISPECTOR THE MINISPECTOR IS CONSIDERABLE.

CANCELLATION OR DELAYS IN SCHEDULED MI IF THE OR AND MINISPECTIOR GROWED OR ADMIT OR WHICH THE MI WILL BE CONDUCTED, AND EITHER PARTY CANCELS OR DELAYS, CROWN SWILL NOT BE REPONSIEL FOR AN TWO COSTS FERS LIGIS OF DEPOSITS AND COLORISE FERMILIES RELATED TO THE CANCELLATION OR DELAY MICHAEL BY CENTER PARTY FOR ANY TWO LIGIS OF TRAVEL AND LODGINGS COSTS OF VERFINE EQUIPMENT ON-SITE, ETC.) IF CROWN CONTROLTS BIRECTLY FOR A THIRD PARTY M. EXCEPTIONS MAY BE IMADE IN THE EVENT THAT THE DELAYCANCELLATION IS CAUSED BY WEATHER OR OF THER DOWNSHOWS THAT MAY COMPROMISE THE SKETLY OF THE PARTIES MODIFIED.

- CORRECT FALING ISSUES TO COUPLY WITH THE SPECIFICATIONS CONTAINED IN THE ORIGINAL CONTRACT DOCUMENTS AND
- A SUPPLEMENT IM WAS APPROVAL. THE GO MAY WORK WITH THE EOR TO RE-ALVALYZE THE MODIFICATION/REINFORCEMENT USING THE PROPERTY OF THE GO MAY WORK WITH THE EOR TO RE-ALVALYZE THE MODIFICATION/REINFORCEMENT USING THE

MINERICATION INSPECTIONS.

TO CHOOSE IT AND CONDUCT A MINERICATION INSPECTION TO VERIEV THE ACCURACY AND COMPLETENESS OF PREVIOUS COMPLETED WITH INSPECTIONS) ON TOWER MIDDIFICATION PROJECTS.

PHOTOGRAPHS
BETWEEN THE GO AND THE MITHSPECTOR THE FOLLOWING PHOTOGRAPHS, AT A MINNUM, ARE TO BE TAKEN AND INCLUDED IN THE MITHSPECTOR.
BETWEEN THE GO AND THE MITHSPECTOR THE FOLLOWING PHOTOGRAPHS, AT A MINNUM, ARE TO BE TAKEN AND INCLUDED IN THE MITHSPECTOR.

- PRE-CONSTRUCTION GENERAL SITE CONDITION
 PROTOGRAPHS DURNS THE RENDORCEMENT MODIFICATION CONSTRUCTION SECTION AND INSPECTION
 RAW MATERIALS
 PROTOG OF ALL CRITICAL DETAILS
 FOLKDATION MODIFICATIONS
 WELD PREPARTION
 BOLT INSTALLATION ALD TORCISE
 FRAM, INSTALLED CONDITION
 SURFACE COATING REPAR
 POST CONSTRUCTION PROTOGRAPHS
 FINAL INSPELIO CONDITION
 SURFACE COATING REPAR
 POST CONSTRUCTION PROTOGRAPHS
 FINAL INSPELIO CONDITION

PHOTOS OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED INADEQUATE

IS IS NOT A COMPLETE JIST OF REQUIRED PHOTOS. PLEASE REFER TO ENG-SOW-10007

	MI CHECKLIST
CONSTRUCTION:INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY EOR)	REPORT ITEM
	PRE-CONSTRUCTION
X	MI CHECKLIST DRAWINGS
Х	ÉDR RÉVIEW
х	FABRICATION INSPECTION
NA NA	FABRICATOR CERTIFIED WELD INSPECTION
х	MATERIAL TEST REPORT (MTR)
NA NA	FABRICATOR NDE INSPECTION
Х	NDE REPORT OF MONOPOLE BASE PLATE (AS REQUIRED)
Х	PACKING SLIPS
	CONSTRUCTION
X	CONSTRUCTION INSPECTIONS
NA NA	FOUNDATION INSPECTIONS
NA	CONCRETE COMP. STRENGTH AND SLUMP TESTS
NA NA	POST INSTALLED ANCHOR ROD VERIFICATION
NA	BASE PLATE GROUT VERIFICATION
X	CONTRACTOR'S CERTIFIED WELD INSPECTION
NÁ	EARTHWORK: LIFT AND DENSITY
X	DN SITE COLD GALVANIZING VERIFICATION
NA NA	BUY WIRE TENSION REPORT
X	GC AS-BUILT DOCUMENTS
X	INSPECTION OF AJAX BOLTS AND DTIS PER REQUIREMENTS ON SHEET S-3
NA	MICROPLERIOCK ANCHOR INSTALLERS DRILLING AND INSTALLATION LOGS AND DAYOC DOCUMENTS
NA	REFER TO MICROSE, ERROCK ANCHOR NOTES FOR SPECIAL INSPECTION AND TESTING REQUIREMENTS.
ADDITIONAL TESTING AND INSPECTIONS:	distribution of the second sec
	POST-CONSTRUCTION
Х	MI INSPECTOR REDLINE OR RECORD DRAWING(S)
NA NA	POST INSTALLED ANCHOR ROD PULL-OUT TESTING
Pes	

MOTE: X DENOTES A DOCUMENT MEEDED FOR THE FMI REPORT NA DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE FMI REPORT

PAUL J, FORD AND COMPANY STRUCTURAL ENGINEERS 250 East Broad Steet - Surbe 600 + Columbus, Oth 4215 is www.plymb.com **CROWN CASTLE** PH: (724) 416-2000

BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT: 37514-2522-001-7700 LM. MI CHECKLIST CHECKED BY C.M.M. PROVED B S-6

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

BU #806371; HRT 096 943227 BU NUMBER; SITE NAME

APP: 269459 REV. 0; WO: 965888

SITE ADDRESS

ҮТИООЭ ПЯОЭТЯАН MINDSOR, CONNECTICUT 06095 HRT 96 599 MATIANUCK AVE

PROJECT CONTACTS:

3530 TORINGDON WAY SUITE 300 CHARLOTTE, NC 28277 CROWN CASTLE MONOPOLE OWNER:

6900-026 (T8Z) 3Hd MOD PAT JERRY BRUNO AT JERRY, BRUNO, CONTRACTOR @ CROWNCASTLE, COM

DESIGN STANDARD

THE TAYOUR NOT UNAUNAL STANDONNES SELECTION AND THE TAYOUR AND THE THIS REINFORCEMENT DESIGN IS BASED UPON THE REQUIREMENTS OF

20 MPH SERVICE LOADS. SPEED OF 80 MPH (3-SEC GUST) WITH NO ICE, 38 MPH WITH 1 INCH ICE AND SUPPORTING STRUCTURES AND ANTENNAS, USING A DESIGN BASIC WIND

THE PJF STRUCTURAL ANALYSIS FOR THIS SITE (PJF#37614-2622.001.7700) REFER TO THE POLE DESIGN AND ANTENNA LOADING DOCUMENTED IN

REINFORCING ELEMENTS: THIS PROJECT INCLUDES THE FOLLOWING

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	STIFFENERS	ELD WELDED

SHEET INDEX			
DESCRIPTION	SHEET NUMBER		
TITLE SHEET	l-T		
GENERAL NOTES	1-8		
GENERAL NOTES	Z-S		
AJAX BOLT DETAIL	£-S		
MONOPOLE PROFILE	₹ \$		
BASE PLATE DETAILS	g-S		
WI CHECKLIST	9-8		
INI OUTONCIOL	0-0		

PROJECT NOTES

- PROCEEDING WITH THE WORK, IL FORD AND COMPANY AND CROWN CASTLE FIELD PERSONNEL BEFORE CONTRACTOR SHALL IMMEDIATELY REPORT ANY AND ALL DISCREPANCIES TO WORK. OF INFORMATION ABOVE AND WITH THE PROJECT PLANS BEFORE PROCEEDING WITH THE CONDITIONS MAY BE AVAILABLE ON CROWN'S CCISITES AND FROM CONTRACTOR'S PRESPONSIBILITY TO FIELD VERIEY ALL EXISTING CONDITIONS AND DIMERSISIONS AND COORDINGTE WITH THE AVAILABLE SOURCES DETAILED FIELD INFORMATION REGARDING INTERFERENCES AND/OR EXISTING FIELD
- STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS", DEC. 31, 2009, CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC "SPECIFICATION FOR ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED
- OF THE AISC "SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS" ALL STRUCTURAL BOLTS SHALL BE FIELD INSPECTED ACCORDING TO THE REQUIREMENTS
- (TID) WASHERS WITH THE ALAX M20 BOLTS. DETAILS ON SHEET 5-3 FOR REQUIREMENTS ON THE USE OF DIRECT TENSION INDICATOR SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) VIASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND REVER (DTI'S) AND HARDENED WASHERS. ALL ALAX M20 BOLTS WITH SHERR SLEEVES DITIS REQUIRED: ALL ALAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION

BOLTS TIGHTERED USING AIGC TURK-DENUTY NETHOD, INSTALLERS SHALL FOLLOW CROWN GUIDELINES FOR AIGC TURK-DENUTY METHOD AND ALSO PROVIDE COMPLETE INSPECTION DOCUMENTATION IN THE PMI. PRIOR TO STRATING WORK, CONTRACTOR SHALL CONSULT WITH CROWN ENGINEERING TO DETERMINE WHETHER THIS FOLICY IS EFFECTIVE 5/30/2012: UNTIL FURTHER NOTICE, CROWN CASTLE WILL ACCEPT AJAX

EOR, AND TO CROWN CASTLE. AND SHALL SUBMIT A COPY OF THE BOLT INSPECTION REPORT TO THE MI INSPECTOR, THE NON-TC BOLT INSPECTION", DATED APRIL 2013, THE THIRD-PARTY BOLT INSPECTOR SHALL NON-TC BOLT INSPECTOR SHALL INSPECTOR SHALL FOLLOW THE PUBLISHED CROWN CASTLE INSPECTION PROCEDURE "MI INSPECTION IS REQUIRED TO BE AN ONSITE FIELD INSPECTION. THE THIRD-PARTY BOLT BOLTS AND/OR BOLTS WITHOUT DITS INSTALLED) SHALL BE INSPECTED ONSITE BY AN INDEPENDENT THIRD-PARTY BOLT INSPECTOR, AS APPROVED BY CROWN, THIS PROPERTY THIRD-PARTY BOLT. AISC "TURN-OF-NUT" TENSIONING PROCEDURE (NON-TENSION CONTROLLED [NON-TC] STRUCTURAL BOLTS THAT ARE TIGHTENED TO THE PRETENSIONED CONDITION USING THE C.) REQUIREMENT EFFECTIVE 04/20/2013, PER CROWN CASTLE DIRECTIVE: ANY AND ALL

REINFORCEMENT DESIGN SHALL BE INCLUDED IN THE NDE SCOPE OF WORK CRACKS ARE SUSPECTED OR HAVE BEEN IDENTIFIED, THE NDE SHALL INCLUDE ALL EXISTING REINFORCEMENTS THAT HAVE BEEN WELDED TO THE BASE PLATE, ANY FULL PENETRATION WELDING TO THE BASE PLATE REQUIRED AS PART OF THIS ACTIVE ENG-BUL-10031 'NDE REQUIREMENTS FOR MONOPOLE BASE PLATE TO PREVENT CONNECTION FAILURE, NOTIFY THE EOR AND CROWN ENGINEERING IMMEDIATELY IF RNY REQUIRED SEE CCI DOCUMENTS ENG-SOW-1033 'TOWER BASE PLATE NOF AND NDE OF THE CIRCUMFERENTIAL WELD OF THE BASE PLATE TO SHAFT CONNECTION IS



PROJECT: 37514-2522,001,7700

1-1 -116 CWW СНЕСКЕР ВА TITLE SHEET W

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT WINDSOR, CONNECTICUT BU #806371; HRT 096 943227

PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS

CROWN CASTLE



CROWN CASTLE PROJECT: 8U #806371; HRT 096 943227; WINDSOR, CONNECTICUT MONOPOLE RETROFIT PROJECT MASTER NOTES DOCUMENT (REV. 2, 1/22/2009)

ROWN CASTLE PROJECT: 8U 80/8371; HRT 0/89 94327; WRDSOR, CONNECTICUT (ONCPOLE RETROFIT PROJECT MASTER NOTES DCCLIMENT (REV. 2, 1/22/2009)

A. GEMERAL NOTES

I. STAILE DE TIEL RESPONSIBILITY OF THE CONTRACTOR TO FIELD VERFEY ALL EXISTING CONDITIONS AND DIMENSIONS PRIOR TO FABRICATION AND COLUMENTS PROVIDED TO PAUL. I. FORD A COMPANY BY CROWN CASTLE. THIS INFORMATION PROVIDED HAS NOT BEEN FIELD VERFED BY FAUL. I. FORD A COMPANY FOR ACCURACY AND THEREFORE DISCREPANCIES RETWEEN THESE DEMANNES AND ACCURACY AND THEREFORE DISCREPANCIES RETWEEN THESE DEMANNES AND ACCURACY AND THEREFORE DISCREPANCIES AND CONTRACTS THE PROGRAMMEN SECONDITIONS SHOULD BE ANTICIPATED. ANY DISCREPANCIES AND CONTRACTS THE DESPONSIBLE THE INFORMATION COSTANGED IN HIS DEMANNES AND THE ACTUAL VERRIENDED SITE COMPILITIONS AND THE DESPONSIBLE THE PROGRAMMEN SHOULD BE ANTICIPATED. ANY DISCREPANCIES AND CONTRACTS THE DESPONSIBLE THE PROGRAMMEN CONTRACTS TO THE SECONDITION OF THE PROGRAMMEN AND THE ACTUAL VERRIENDED SITE COMPILITION OF THE PROGRAMMEN AND THE ACTUAL VERRIENDED SITE COMPILITION OF THE PROGRAMMEN AND THE ACTUAL VERRIENDED SITE COMPILITION OF THE PROGRAMMEN AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND THE ACCURACY AND ACCURACY AND THE ACCURACY AND THE ACCURACY AND ACCUR

B. (SECTION NOT USED)

C. SPECIAL INSPECTION AND TESTING
ALL WORK SHALL BE SUBJECT TO REVIEW AND DISSERVATION BY THE OWNER'S REPRESENTATIVE AND
THE OWNER'S AUTHORIZED INDEPENDENT INSPECTION AND TESTING AGENCY. REFER TO CROWN
CASTLE DOCUMENT BIOLSOW-1006 FOR SPECIFICATION.
ANY SUPPORT SERVICES PERFORMED BY THE ENGINEER DURING CONSTRUCTION SHALL BE
DISTINGUISHED FROM CONTINUOUS AND DETAILED INSPECTION SERVICES WHICH ARE FURNISHED BY
OTHERS. THESES SUPPORTS SERVICES PERFORMED BY THE ENGINEER AND FERD ASSISTING IN QUALITY CONTROL, AND IN ACHEVING COMPORATIVE SOLELY FOR
THE PURPOSE OF ASSISTING IN QUALITY CONTROL, AND IN ACHEVING COMPORATIVE SOLELY FOR
THE PURPOSE OF ASSISTING IN QUALITY CONTROL, AND IN ACHEVING COMPORATIVE BY CONTRACTOR
OSCINGLINES THEY DO NOT QUARANTEE CONTRACTORS A REPROGRAMOR WITH CONTRACT
OCCURRECTED BY THE CONTRACTOR AT IOA ASSISTING
OSSERVED DESCREPANCES BETWEEN THE WORK AS THE CONTRACT DOCUMENTS SHALL BE
CORRECTED BY THE CONTRACTOR AT IOA ASSISTING
ORDINARY THE CONTRACTOR AT IOA ASSISTING
AND ASSISTING OF THE CONTRACTOR AT IOA ASSISTING
AND ASSISTING ASSISTING ASSISTING
ASSISTING AND FELD WORK PERFORMED BY THE CONTRACTOR.
AND ASSISTING AND FELD WORK PERFORMED BY THE CONTRACTOR.

(A) ACCESS TO ANY PLACE WHERE YORK SEEDILE THIS WORK AS TO CAUSE A MINIMAL OF BEITTENED AND ALL THESE
BY THE INSPECTION AS DECENDANCE WHILE ADDRESS AS ASSISTING
AGENCY. THE CONTRACTOR SHALL ALLOW FOR ADEQUATE THE AND ACCIDENT WITH THE TESTING
AGENCY. THE CONTRACTOR SHALL ALLOW FOR ADEQUATE THE AND ACCOMPANY TO PERFORM THEIR DUTIES.

THE INSPECTION AS DESTING AGENCY SHALL AS A MINIMAL OF BEITTEN AS ADEAUNCE WITH THE CONTRACTOR'S RESPONSIBILITY TO COORDINATE THE WORK SCHEDULE WITH THE FESTING AGENCY. THE CONTRACTOR'S RESPONSIBILITY TO COORDINATE THE WORK SCHEDULE WITH THE FESTING AGENCY TO PERFORM THEIR DUTIES.

THE INSPECTION AS DESTING AGENCY SHALL AS AND ADDRESS AS A THE TESTING AGENCY SHALL AS A MINIMAL OF BEITTENED AS ADDRESS AS A STATE OF THE ADDRESS AS A STATE OF THE ADDRESS AS A STATE OF THE ADDRESS AS A STATE OF THE ADDRESS AS A STA

(2) CHECK FOR SURFACE FINES SPECIFED, GALVANZEO.
(E) CHECK BOLT TIGHTENING ACCORDING TO JASC TURK OF THE MUT METHOD.

E WELDING:
(1) VEREPY FIELD WELDING PROCEDURES, WELDERS, AND WELDING OPERATORS, NOT DEEVED PREQUARIED, SI ACCORDANCE WITH ANS 01.1.
(2) INSPECT FIELD WELDING PROCEDURES. WELDERS, AND WELDING OPERATORS, NOT DEEVED AND IN ACCORDANCE WITH ANS 01.1.
(3) APPROVED FIELD WELDING SEGONS, NO CHANGE IN APPROVED SEQUENCES MAY BE MADE WITHOUT FERMASION FROM THE WITHOUT FERMASION FERMAS

DYS PENETRANT.

NSPECT FOR SUZE SPACING, TYPE AND LOCATION AS PER APPROVED PLAYS, VERNY THAT THE BASE METAL. CONFORMS TO THE DRAWNOS. REVIEW THE REPORTS BY TESTING LABS.
CHECK TO SEE THAT WELDS ARE CLEAN AND FREE FROM SLAG.
INSPECT RUST PROTECTION OF WELDS AS PER SPECTFOATIONS.
CHECK THAT DEFECTIVE WELDS ARE CLEANLY MARKED AND HAVE BEEN ADEQUATELY REPARED.

F. REPORTS: (1.) COMPILE AND PERICOICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER

(T) COMPILE AND PERCOICALY SUBMIT DALLY INSPECTION REPORTS TO THE OWNER.

THE INSPECTION PLAN OUTLINED HERBIN IS INTENDED AS A DESCRIPTION OF GENERAL AND SPECIFIC TIERS OF CONCERN. IT IS NOT INTENDED TO BE ALLANCUERVE. IT DOES NOT LIMIT THE TESTING AND INSPECTION AGENCY TO THE ITEMS LISTED. ADDITIONAL TESTING, INSPECTION, AND CHECKING MAY BE REQUIRED AND SHOULD BE MINIOPATED. THE TESTING ABONCY SHALL USE THEIR PROPERSIONAL JUDGMENT AND KNOWLEDGE OF THE JOS SHE CONDITIONS AND THE CONTRACTORS PERFORMANCE TO DECIDE WHAT OTHER TERMS REQUIRED ACCITIONAL ATTENDO. THE TESTING AGENCY SUDGMENT AND KNOWLEDGE OF THE JOS SHE CONDITIONS AND THE CONTRACTORS PERFORMANCE AND ADDITIONAL THE SHOWLED AND SPECIFICALLY COVERED, ANY DISCREPANCES AND PROBLEDS SHALL BE THE CONCERN SHALL BE SHOWLED AND SPECIFIC WHITTIED LONGEST. THE CONCERN BENEFIX THE RIGHT BOOK TO THE CONTRACTORS OF THE CONCERN BENEFIX AND SPECIFIC WHITTIED CONCERN. THE CONCERN BENEFIX THE FIRST THE CONCERN BENEFIX AND SPECIFIC WHITTIED CONCERN. THE CONTRACTOR OF THE CONTRACTOR AND FLED AS DAMY REPORTS TO THE OWNER. THIS STEED CONTRACTOR WILL GIVE THE CONTRACTOR A LIST OF THEMS TO BE CONSECTED, PRIOR TO CONTRIBUTE CONSTRUCTION, AND DET LOOKING TO STRUCTURAL ITEMS.

RESPONSIBILITY. THE TESTING AGENCY WILL REPORT SO THE CONSECTED, PRIOR TO CONTRIBUTIONS. THE CONTRACTOR ALST OF THE SYS TO BE CONSECTED, PRIOR TO CONTRIBUTE CONSTRUCTION. THE CONTRACTOR ALST OF THE SYS TO BE CONSTRUCTIVE. OR STATUTORY ORIGINATIONS. THE CONTRACTOR HAS THE SIXE RESPONSIBILITY FOR ANY DEVATIONS FROM THE CONTRACTOR'S CONTRACTOR AND THE STRING AGENCY WILL NOT REPLACE THE CONTRACTOR'S CONTRACTOR. PERSONNEL.





BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT: 37514-2522.001.7700

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DRAWN BY:		
CHECKED BY: C.M.M.	GENERAL NOTES	
DATE:	S-1	

- STRUCTURAL STEEL
 STRUCTURAL STEEL MATERIALS, FABRICATION, DETAILING, AND WORKMANSHIP SHALL CONFORM
 TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:
 BY THE AMERICAN INSTITUTE OF STREEL CONSTRUCTION (ASS);
 [A] SPECIFICATION FART THE IDESIGN, FABRICATION FAID ERECTION OF STRUCTURAL STEEL

- 10. 11.
- (A)
- STRUCTURAL STEEL MATERIALS, PARRICATION, DETAILING, AND WORKMANSHIP SHALL CONFORM TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:

 BY THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC):

 AND SECRETARY OF THE DESIGN, PARRICATION AND ERECTION OF STRUCTURAL STEEL

 FOR BUILDINGS:

 (A) "SPECIFICATION FOR STRUCTURAL JOINTS USING ASTM AZS OR A450 BOLTS," AS

 APPROVED BY THE RESEARCH COUNCIL ON STRUCTURAL CONNECTIONS OF THE

 ENGINEERING FOUNDATION:

 (C) "CODE OF STANDARD FRACTICE FOR STEEL BUILDINGS AND BRIDGES' (PARAGRAPH 4.2.1

 STRUCTURAL WELDING BOLT / AWS:

 AT STRUCTURAL WELDING AND NAN-DESTRUCTURE TESTING'

 BY THE AMERICAN WELDING BOLTS AND NAN-DESTRUCTURE TESTING'

 AND VALERIAL OR WORKMANSHE WHICH IS DESCRIPED TO BE DEFECTIVE OR INCONSISTENT WITH

 HE CONTINUED TO COUNTING IS SHALL BE CORRECTIVE TO BE DEFECTIVE OR INCONSISTENT WITH

 HE CONTINUED TO COUNTING AS SHALL BE CORRECTIVE TO BE DEFECTIVE OR INCONSISTENT WITH

 HE CONTINUED TO COUNTING AS SHALL BE CORRECTION, MODIFIED, OR REPLACED AT THE

 CONTINUED TO THE REQUIREMENTS OF THE AISC TURN OF THE KUT METHOD. TIGHTEN BOLTS 19

 THEN HE SHALL STRUCTURAL BOLTS. INCLUDING THE ALIAN MAD BOLTS WITH SHEAR SLEEPES,

 ACCORDING TO THE REQUIREMENTS OF THE AISC TURN OF THE KUT METHOD. TIGHTEN BOLTS 19

 THEN HE SHALL BELT OWNERS. THE SHALL OWNERS AND THE AISC TURN OF THE KUT METHOD. TIGHTEN BOLTS 19

 THEN HE SHALL BELT OWNERS AND SEEMED BY AND.

 WELDING SOCIETY, AND SOLT, ALL WELD ELECTRODES SHALL BE BOXX, UNITES STOTED

 OTHERWISE ON THE DRAWMANS.

 ALL WELDED CONNECTIONS SHALL BE MADE BY WELDERS CERTIFIED BY AWS. CONTRACTOR SHALL

 SUBJIT WELDERS CERTIFICATION AND QUALIFICATION DOCUMENTATION TO THE OWNERS TESTING

 ABELT OF REVIEW AND APPROVAL PREFOR TO CONSTITUTION.

 STRUCTURAL STEEL PLATES SHALL CONFORM TO ASTM ASTZ GRADE BY FY 56 KSI MIN, UNLESS

 ONTED OTHERWISE ON THE DRAWWASE.

 ALL WELDED CONNECTIONS SHALL BE MADE BY WELDERS CERTIFIED BY AWS. CONTRACTOR SHALL

 SUBJIT WELD SHALL BE VISUALLY INSPECTED BY THE CONTRACTOR SHALL BOOT AND THE TESTING AFFORM.

 THE WORE
- BASE PLATE GROUT (NOT REQUIRED)
- FOUNDATION WORK (NOT REQUIRED)

- CAST-IN-PLACE CONCRETE (NOT REQUIRED)
- EPOXY GROUTED REINFORCING ANCHOR RODS (NOT REQUIRED)
- TOUCH UP OF GALVANIZION
 THE CONTRACTOR AND THE PERPARED VIOLENT TO THE EXISTING
 THE CONTRACTOR SHALL TOUCH UP ANY ANDIOR ALL AREAS OF GALVANIZING ON THE EXISTING
 THE CONTRACTOR ON THE CONTRACTOR
 THE CONTRACTOR SHALL CERE
 TOUCHED UP WITH TWO (2) COATS OF PRO-BRAND CINC-RICH COLD GALVANIZING COMPOUND. FILM
 THICKINESS PER COAT SHALL ES WE TAN ON INLS DRY 15 AMB. S. APPLY PER ZRC (MANUFACTURER RECOMMENDED PROCEDURES. CONTRACT DRG THE TOWN THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PERPARED SHALL FILE OF WELLOS ON GALVANIZED AND PRIME PAINTED
 SURFACES FOR TOUCH-UP COATING IN ACCORDANCE WITH AWAS DI.1. THE OWNERS TESTING
 AGENCY SHALL VERIFY THE PREPARED SHATE AND VERIFY THE COATING. THE COUNTRACTOR HAS APPLIED THE ZRC COLD GALVANIZING COMPOUND AND IT HAS SUFFICIENTLY
 THE OWNERS TESTING AGENCY SHALL TEST AND VERIFY THE COATING THICKNESS AFTER THE
 CONTRACTOR HAS APPLIED THE ZRC COLD GALVANIZING COMPOUND AND IT HAS SUFFICIENTLY
 RIPE OF THE CONTRACTOR HAS APPLIED THE ZSTING AGENCY.

- HOT DIP GALVANIZAM HOTOIP GALVANIZZ ALL STRUCTURAL STEEL MENBERS AND ALL STEEL ACCESSORIES, BOLTS, WASHERS, ET O. PER ASTM A122 OR PER ASTM A153, AS APPROPRIATE, PROPERLY PREPARE STEEL TEMS FOR GALVANIZING DRILL OR PUNOT WEEP ANDOR POMITAGE HOLES AS REQUIRED. ALL GALVANIZING SHALL BE DONE AFTER FABRICATION IS COMPLETED AND PRIOR TO FIELD INSTALLATION.
- PERPETUAL INSPECTION AND MAINTENANCE BY THE OWNER
 AFTER THE CONTRACTOR HAS SUCCESSFULLY COMPLETED THE INSTALLATION OF THE MONCPOLE
- PERPETUAL MISPECTION AND MAINTENANCE BY TIPE OWNER
 AFTER THE CONTRACTOR HAS SUCCESSFULLY COMPLETED THE INSTALLATION OF THE MONCPOLE
 REINFORCING SYSTEM AND THE WORK HAS BEEN ACCEPTED BY THE OWNER. THE OWNER WILL BE
 RESPONSIBLE FOR THE LONG TERM AND PERPETUAL INSPECTION AND MAINTENANCE OF THE FOLE
 AND REINFORCING SYSTEM.
 THE MONOPOLE REINFORCING SYSTEM MOLCATED IN THESE DOCUMENTS USES REINFORCING
 COMPONENTS THAT INVOLVE FIELD WELDING STEEL MEMBERS TO THE EXISTING GAL WANZED STEEL
 POLE STRUCTURE. THESE FIELD WELDING ONNECTIONS ARE SUBJECT TO CORROSION DAMAGE
 AND DETERORATION IF THEY ARE NOT PROPERLY MAINTAINED AND COVERED WITH CORROSION
 PREVENTING COATING SUCH AS THE ZOR GALVANIZING COMPOUND SPECIFIED PREVIOUSLY. THE
 STRUCTURAL LOAD CARRYING CAPACITY OF THE REINFORCED POLE SYSTEM IS DEPENDENT UPON
 THE INSTALLED SIZE AND QUALITY, MAINTAINED SOUND CONDITION AND STRENGTH OF THESE FIELD
 WELDED CONNECTIONS ANY CORROSION OF, DAMAGE TO, FATIGUE, FRACTURE, ANDIOR
 DETERIORATION OF THESE WELDS ANDORD THE COMMECTED COMPONENTS WILL RESULT IN THE
 LOSS OF STRUCTURAL LOAD CARRYING CAPACITY AND MAY LEAD TO FAILURE OF THE
 STRUCTURAL SYSTEM. THEREFORE, IT IS IMPERATIVE THAT THE OWNER REQUILARLY INSPECTS,
 MAINTAINS, AND REPAIRS AS NECESSARY, ALL OF THESE WELDS, CONNECTIONS, AND
 COMPONENTS FOR THE LIFE OF THE STRUCTURE.

 THE OWNER SHALL REFER TO TAKELA 222.F-1996, SECTION 14 AND ANNEX E FOR RECOMMENDATIONS
 FOR MAINTENANCE AND INSPECTION, THE FREQUENCY OF THE INSPECTION AND MAINTENANCE
 INTERVALS IS TO BE DETERMINED BY THE OWNER BASED UPON ACTUAL STE AND ENVIRONMENTAL
 CONDITIONS. PAUL J. FORD COMPANY PRECOMMENDS THAT A COMPILETE AND THOROUGH
 MSPECTION OF THE ENTIRE REINFORCED MONOPOLE STRUCTURAL SYSTEM BE PERFORMED
 YEARLY ANDOR AS FREQUENTLY AS CONDITIONS WARRAIT. ACCORDING TO TITMELA 222.F-1996
 SECTION 14.1, NOTE 1: TI IS RECOMMENDED THAT THE STRUCTURAL SYSTEM BE PERFORMED
 YEARLY ANDOR AS FREQUENTLY AS CONDITIONS WARRAIT. ACCORDING TO TOTALL 222.F-1996
 SECTION 14.1, NOTE 1: TI IS RECOMMENDED THAT THE STRUCTURE BE INSPECTED AFTER SEVER



PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 220 East Board Street - Suite 400 - Coultmodu, Druk 4315 9141 221-4678

CROWN CASTLE 3530 TORINGDON WAY SUITE 300 CHARLOTTE, NG 2827

BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

PROJECT: 37514-2522.001,7700

DRAWN BY **GENERAL NOTES** HECKED BY C.M.M.

THE

AJAX BOLT NOTE SHEET: REV. 1.5, 5-12-2014

NOTES

- 1. ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
- 2, ALL STRUCTURAL BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS, DEC. 31, 2009.
- 3. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND DETAIL BELOW FOR THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
- 4. ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. DTI'S SHALL BE THE SQUIRTER® STYLE, MADE TO ASTM F959 LATEST REVISION; AND HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A HARDNESS OF RC 38 OR HIGHER.

NOTES FOR AJAX M20 'ONE-SIDE BOLTS WITH DIRECT TENSION INDICATORS (DTI'S):

DTI'S REQUIRED: DTI'S SHALL BE "SELF-INDICATING" SQUIRTER® STYLE DTI'S MADE WITH RED DURABLE SQUIRT MEDIA EMBEDDED IN THEM, INSPECTED BY MEANS OF THE VISUAL EJECTION OF SILICONE AS THE DTI PROTRUSIONS COMPRESS. SQUIRTER® DTI'S SHALL BE CALIBRATED PER MANUFACTURER'S INSTRUCTIONS PRIOR TO USE.

THE DIRECT TENSION INDICATOR (DTI) WASHERS SHALL BE THE "SQUIRTER® STYLE" AS MANUFACTURED BY APPLIED BOLTING TECHNOLOGY PRODUCTS' INC.:

PART NUMBER: 2DTIM208MGAFSIF

DESCRIPTION: P.C. 8.8 DTI SQUIRTER WASHER WITH RED DURABLE SQUIRT MEDIA DESIGNED SPECIFICALLY FOR THE AJAX M20 ONESIDE BOLT. FINISH SHALL BE ZINC GALVANIZED AS PROVIDED BY THE DTI MANUFACTURER.

DISTRIBUTOR CONTACT DETAILS:

ALLFASTENERS

15401 COMMERCE PARK DR. BROOKPARK, OHIO 44142 PHONE: 440-232-6060

E-MAIL: SALES@ALLFASTENERS.COM

DTI: USE DIRECT TENSION INDICATOR (DTI) WASHERS COMPATIBLE WITH 20 MM (M20) NOMINAL A325 BOLTS FOR THE AJAX M20 BOLTS, DTI'S SHALL NOT BE HOT-DIP GALVANIZED DTI'S SHALL BE MECHANICALLY GALVANIZED (MG) BY THE COLD MECHANICAL PROCESS ONLY AS PROVIDED BY THE DTI MANUFACTURER.

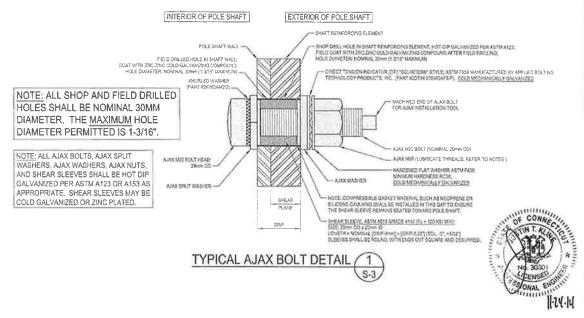
HARDENED WASHERS REQUIRED: USE A HARDENED WASHER FOR A 20 MM (M20) NOMINAL BOLT BETWEEN THE TOP OF THE DIRECT TENSION INDICATOR (DTI) WASHER AND THE NUT OF THE MAX M20 BOLTS. HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A MINIMUM HARDNESS OF RC 38 OR HIGHER. THE HARDENED WASHERS SHALL BE MECHANICALLY GALVANIZED BY THE COLD MECHANICAL PROCESS. ALTERNATIVELY, CORRECTLY MADE HOT DIP GALVANIZED HARDENED FLAT WASHERS HAVING A MINIMUM HARDNESS OF RC 38 CAN BE USED; CONTRACTOR SHALL PROVIDE DOCUMENTATION OF WASHER SPECIFICATION AND HARDNESS.

NUT LUBRICATION REQUIRED: PROPERLY LUBRICATE THE THREADS OF THE NUT OF THE AJAX BOLT SO THAT IT CAN BE PROPERLY TIGHTENED WITHOUT GALLING ANC/OR LOCKING UP ON THE BOLT THREADS, CONTRACTOR SHALL FOLLOW DTI MANUFACTURER INSTRUCTIONS FOR PROPER LUBRICATION AND TIGHTENING.

NOTE: COMPLETELY COMPRESSED DTI'S SHOWING NO VISIBLE REMAINING GAP ARE ACCEPTABLE. DTI WASHERS SHALL BE PLACED DIRECTLY AGAINST THE OUTER AJAX WASHER NOTH THE DTI BUMPS FACING AWAY FROM THE AJAX WASHER. NEVER HARDENED WASHER BETWEEN THE DTI AND THE AJAX NUT. THE DTI BUMPS SHALL BEAR AGAINST THE UNDERSIDE OF A HARDENED FLAT WASHER. NEVER DIRECTLY AGAINST THE NUT.

CONTRACTOR SHALL FOLLOW DTI MANUFACTURER'S INSTRUCTIONS FOR INSTALLATION, LUBRICATION, TIGHTENING AND INSPECTION.

INSPECTION REQUIRED: ALL AJAX BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AJSC SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS, DEC. 31, 2009, BY A QUALIFIED BOLT INSPECTOR. DURING INSTALLATION, THE BOLT INSPECTOR SHALL VERIFY AND DOCUMENT: THE SHOP-DRILLED AND FIELD-DRILLED HOLE SIZES; THE INSTALLATION OF THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S TENSIONING PROCEDURE. IN ADDITION, ALL AJAX BOLTS AND DTIS SHALL BE VISUALLY INSPECTED ACCORDING TO THE DTI MANUFACTURER'S INSTRUCTIONS. THE BOLT INSPECTOR SHALL PROVIDE COMPLETE PHOTO DOCUMENTATION OF ALL BOLTS AFTER TIGHTENING CLEARLY SHOWING THE CONDITION OF THE DTI'S.



Objected 2014 by Park 1 in and Objected and All Hights Records 1 the document and Market Records 2 the document and Market Records 2 the document and Market Records 2 the Park 1 fines and Document, Parad 1 in the Cold (unreference and Objected), Parad 1 in the Cold (unreference and Objected), Parad 1 in the Cold (unreference and Objected), Parad 1 in Fall 1 in Fall 1 in Fall 2 in Fal



BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

PROJECT:	37514-2522.00	1.7700
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DRAWN BY:	
CHECKED BY: C.M.N.	AJAX BOLT DETAIL
APPROVED BY. DATE:	S-3



SHAFT	SECTION LENGTH	PLATE THICKNESS	LAP SPLICE	DIAMETER ACROSS FLATS [N]		
SECTION	37.0	(18)	1919	12 TOF	@ 507T0V	
1	49,168 55.00	0.2810	50 00	14 760 25 007	26 570 38,200	

CONTRUCTOR SHALL PROVIDE ASTM AND SHIM PLATES BELOW BLP., CONTR. THE SHAM PLATES SHALL BE FRACED BETWEEN HE NOW SHAFT FRANCHOLDSON AND THE SYSTEMS FOLE SHAFT FRACED HE BLP. JOHN TO THE NATH ALMAST BENCHESTERS SHALL BLATE LOCATION AND A EXTRA LOCATION STRICE SHAP SHALL BE FRANCED BETWEEN THE NEW LOPPER AND LOCATE SHAFT RESHOUGHEST FLATES AT THE SHAFT RESHOUGHEST SHALLS SHAFT LOCATION AND ALL DESHARTONS HE SHAFT SHAFT AS RESHOUGHEST.

(A) INSTALL NEW TRANSITION STIFFENERS AT BASE PLATE. SEE SHEET S-5.

(8) NSTALL NEW SHAFT REINFORCING SEE CHART

				MESA COLLE	ATPLATED	5 KSI) REINFOR					
EOFTON HOIT AVELE	TOP ELEVATION	FLAT DI DEGREE SEPARATION	FLEMENT	ELEMENT LENGTH	GUANTITY	APPROENATE AJAX BOLTS PER ELEMENT	APPROXIMATE TOTAL ALAX BOLT QUANTITY	BOLTS (BOTYCM)	TERMINATION BOLTS(TOP)	MAXIMUM INTERMEDIATE BOLT SPACING	TOTAL STEEL WEIGHT
0°-6°	35-8"	F2, F8 5 F10	CCLAFP. 36512535	35'-0"	1	45	135	1114	14	192	2903 LHS
35-7	E5.7	F2. F5 & F10	06010030	30.0	3	79	314	10	19	392	1833 LBS

NOTES:

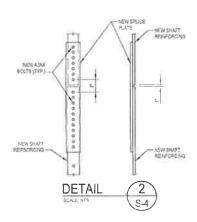
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 2) ALL STEEL SHALL SE HOT O'D GILVINGZED INTER FARRICATION IN ACCORDINGZEMEN HATTO MOST ALL NEWST FERNARIA ALL NEWST FERNARIA COLD
 GILVINGZED AS FOLLODE APPLY ANDINLI DET WO COLTS DE ZOCARMOD ZNC, PICH COLD OLIVINAZIA O COLPOLAD, FLU THODRESS PRE COLF SHALL SE VIST 3.0 M LS. DRY
 1/ALL RELADGECTS APPLY PER ZING UNIMIZACTURED) RECONDURENCED PROCEDURES. CONTINCE ZERC AT 1400-401-7215 FOR PRODUCT INFORMATION.
 2) ALL RELADGECNOS GIALL SE AST MARTO ROLL
 4) MICH 25 SHALL SE SENCE NO DISCRETE. TERMINACION MELOS SHALL SE SIF FILLST WELDS.
 5) FICH SES FOR MARCHES AND SECTION AND SERVE SOMO MILLES SAND SOME AND SECTION AND SEC

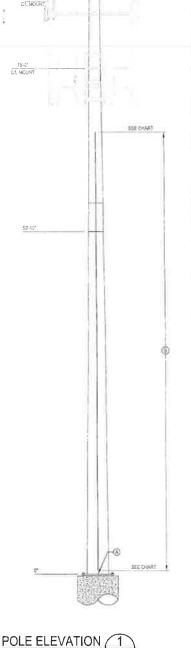
					LATION CHAP			
ELEVATION	FLAT FLATE TRICKNESS		FLAT PLATE. LENGTH	PLAT PLATE QUANTITY	PER SIDE	LENGTH	SPLICE*	TOTAL STEEL WEIGHT
35.7	1458*	612	E-3*	3	00	(F)	:24	\$834,85
						6		140195

* BOLTS INCLUDED IN THE TOTAL QUARTITY LISTED IN THE FLAT PLATE INSTALLATION CHART,

	N.	EW SHIM CHA	RT	
DANULLA DANULL	YTITHAUD YTITHAUD	SHI'N WADTH	SHIM LENGTH	DIAMETER CLAMETER
- 1	1		- 4"	1.14



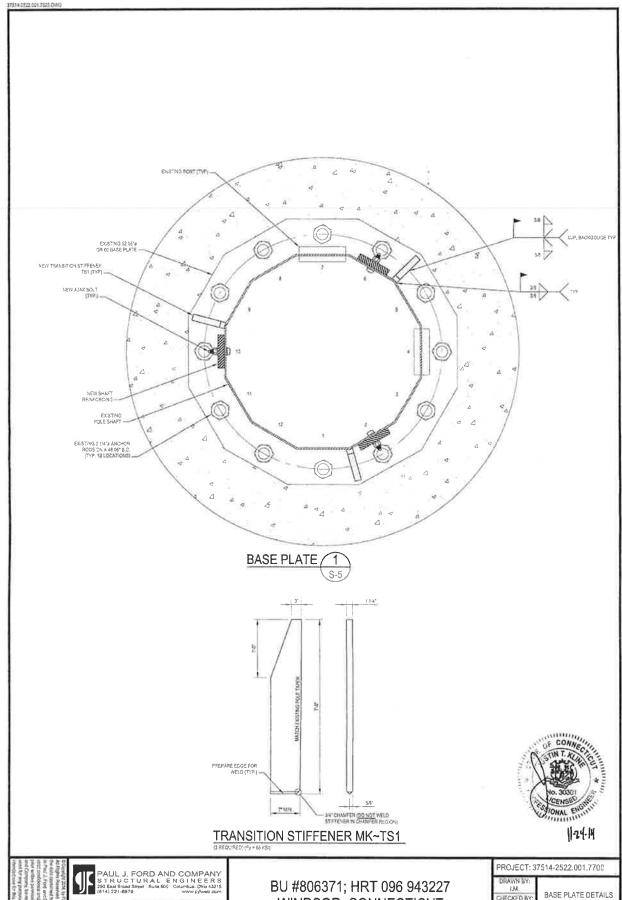








BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT: 37514-2522.001.7700 MONOPOLE PROFILE CHECKED BY APPROVED B **S-4** DATE:



PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 Eaal Bradel Street State ECC Columbia, Otho 42:15 www.pythous.page 15.12 ECC Columbia, Otho 42:15

CROWN CASTLE
3530 TORINGDON WAY SUITE 350 CHARLOTTE, NC 28277
PPE [774]416-2000

WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT DRAWN BY: I.M. CHECKED BY C.M.M. DATE:

S-5

MODIFICATION INSPECTION NOTES

GENERAL.
THE MODIFICATION INSPECTION (MJ) IS A VISUAL INSPECTION OF TOWER MODIFICATIONS AND A REVIEW OF CONSTRUCTION INSPECTIONS AND DIMER REPORTS TO DISSIRE THE ASSTALLATION WAS CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, INAMELY THE MODIFICATION DRAWINGS, AS DESIGNED BY THE ENGINEER OF PECORD, (COP).

THE MIS TO CONTROL NISTALIATION CONFIGURATION AND WORMANISH POINT MID SHOT A REVIEW OF THE MODIFICATION DESIGN TISSLE, MICROSES THE MEMPRETOR TAKE CONTRIBUTE OF THE MICRIPACTION DESIGN. CONTRIBUTE OF THE STRUCTURAL MODIFICATION DESIGN REPECTIVENESS AND INTEGRITY RESIDES WITH THE SER AT ALL TWEE.

ALL MTS SHALL BE CONDUCTED BY A CROWN ENGINEERING VENDOR (AEV) OR ENGINEERING SERVICE VENDOR (AESV) THAT IS APPROVED TO PERFORM REPVATED MORK FOR CROWN. SEE ENG-BUL-19173 UST OF APPROVED MI VENDORS.

TO ENSURE THAT THE REQUIREMENTS OF THE MEARS WET, IT IS VITAL THAT THE OBJECTAL CONTRACTOR (OC) AND THE MEASPECTOR BEGIN COMMAIN, INCLINING AND COORDINATING AS SOOK AS A POLS RECEIVED. IT IS EXPECTED THAT EXCHEMITM WILL BE PROJECTED IN PERCHAPMENT WILL BE PROJECTED IN PERCHAPMENT AND ADDRESS OF PROJECT PROJ.

REFER TO ENG-SOW-10007: MODIFICATION INSPECTION SOW FOR FURTHER DETAILS AND REQUIREMENTS.

 $\underline{\text{MINSPECTOR}}$ THE MINSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A POIFOR THE MITO, AT A MINVALLE

REVIEW THE REQUIREMENTS OF THE MICHECKLIST
 WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS

DENERAL CONTRACTOR
THE OC IS REQUIRED TO CONTACT THE MEINSPECTOR AS SOON AS RECEIVING A PO FOR THE MODIFICATION INSTALLATION OR TURNARY.
PROJECT TO, A MUNICIPAL.

REVIEW THE REQUIREMENTS OF THE MICHEOLIST
 WORK WITH THE MISPECTOR TO DEVICE A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS. INCLUDING FOUNDATION INSPECTIONS.
 BETTER INDEPSTATION ALL PRINCETON AND TESTING REQUIREMENTS

THE GC SHALL PERFORM AND RECORD THE TEST AND ASPECTION RESULTS IN ACCORDANCE WITH THE REQUIREMENTS OF THE MI CHECKLIST AND ENG-SOMH DOT.

RECONVENDATIONS THE FOLLOWING RECONMENDATIONS AND BUSINESTRANG OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTANCES OF DELIVERING

- THE SECRET THAT THE DIPPROVIDE A MENALULY OF 5 BUSINESS DAYS NOTICE, PREZERVABLE 12, TO THE MILESPECTOR AS TO WHEN THE SET WILL BE REJULY FOR THE METO BE CONDUCTED.

 THE SET WILL BE REJULY FOR THE METO BE CONDUCTED.

 THE SET WILL BE REJULY FOR THE METO BE CONDUCTED.

 THE GA ADM WAS MERCETOR COORDINATE CLOSELY THROUGHOUT THE ENTRE PROJECT.

 WHEN POSSIBLE, IT IS PRETENDED TO HAVE THE CO. AND MET MESPECTOR CANSITE SMALLTANEOUSLY FOR ANY OUT WIRE TENSORING OR RE-TENSORING OR PRETENDED.

 THAY SE EXEMPTION TO SATIAL ALL TOWER MODIFICATIONS PROPE TO CONDUCTION THE POLICIATION INSPECTIONS TO ALLOW POLICIATION FOR METAPORT OF THE POLICIATION METAPORT OF THE METAPORT OF THE POLICIATION AND HISPECTORY TO COMMENTE OF THE WIRE THE METAPORT OF THE METAPORT OF THE POLICIATION FOR THE WIRE THE METAPORT OF THE POLICIATION FOR THE WIRE THE METAPORT OF THE POLICIATION FOR THE WIRE THE METAPORT OF THE POLICIATION FOR THE WIRE THE WIRE THE WIRE THE WIRE THE WIRE THE WIRE THE WIRE THE WIRE THE WIRE THE WIRE THE WIRE THE WIRE THE WIRE CAREFULLY TO ENSURE ALL CONSTRUCTION FAULTES ARE AT THERE DISPOSAL WHEN THE ME ASSPECTOR BOOK SITE.

CANCEL LATION OF BY ANY METERS AS ME.

IF THE GO AND IN A ROPECTOR AREAS TO A DATE ON WHICH THE ME WILL BE CONDUCTED, AND ETHER PARTY CANCELS OR DELAYS, CROWN
SHALL NOT BE RESPONSIBLE FOR MY COSTS, PESS, LOSS OF DEPOSITS A MODOR OTHER PROMITTES BEATED TO THE CANCELLATION ON
DELAY MOURRED BY ETHER PARTY FOR MAY THAN ELO TEAMEL AND LOCKING, COSTS OF REPORT GLOUPSHOTH, CONSTITE CITY, DEPOSITS ON CONTRACTS OR SECTLY FOR A THIRD PARTY ME, DECEPTIONS MAY BE MADE IN THE EYEMT THAT THE DELAY/CANCELLATION IS CAUSED BY
WRATHER OR OF THE PROMISONS THAT MAY COMPROMISE THE SUPPLY OF THE PARTERS WORLD THE PROMISON THAT ANY COMPROMISE THE METER OF THE PARTERS WORLD THE PROMISE AND THE METERS AND THE PROMISE OF THE PARTERS WORLD CONTRACT.

<u>CORRECTION OF FALLING MIS</u> IF THE WODSTCATION INSTALLATION WOULD FAA THE MI ("FAALED MID), THE GC BHALL WORK WITH CROWN TO COORDINATE A REMEDIATION.

- CORRECT FALING ISSUES TO COMPLY WITH THE SPECIFICATIONS CONTAINED IN THE OPIGINAL CONTRACT DOCUMENTS AND
 COORDINATE A SUPPLIBERT MI.
 OR, MITH CONDING SUPPRIVAL, THE GC MAY WORK WITH THE EOR TO RE-MALYZE THE MODIFICATION REINFORCEMENT USING THE
 AS-BULT CONDITION.

IN VERTICATION RESERVES THE RIGHT TO CONDUCT A IN VERHICATION INSPECTION TO VERLEY THE ACCURACY AND COMPLETENESS OF PREVIOUSLY COMPLETED ME INFERTION IS ON TOWARD MODIFICATION FROM CO.

ALL YERDYCATION INSPECTIONS SHALL BE HELD TO THE SAME SPECIFICATIONS AND REQUIREMENTS IN THE CONTRACT DOCUMENTS AND IN ACCORDANCE WITH ENG-SOW-1007.

ERFICATION INSPECTION MAY BE CONDUCTED BY AN INDEPENDENT AEVAESY FRIM AFTER A MIQUECATION PROJECT IS COMPLETED, AS MAKED BY THE DATE OF AN ACCEPTED <u>IPASSANG MI</u>T OR <u>PASS AS NOTED MI</u>T REPORT FOR THE ORIGINAL PROJECT.

PHOTOGRAPHS BETWEEN THE BC AND THE MI INSPECTOR THE FOLLOWING PHOTOGRAPHS, AT A MINIMUM, ARE TO BE TAKEN AND INCLUDED IN THE MI

- PRE-CONSTRUCTION GENERAL SITE DON
 PROTOGRAPHS GUERN A BE RENTONCE
 RAYMATERIAS
 PRIOTOS OF ALL CENTROL DETAILS
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 WILLD PREPARATION
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 SOLT INSTALLED CONDITION
 SURFACE CONTINUE DEPAIR
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HOTO'S OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED INADEQUATE

THIS IS NOT A COMPLETE LIST OF REQUIRED PHOTOS, PLEASE REFER TO ENG-SOW-1000?

CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY EOR)	REPORT (TEV				
	PRE-CONSTRUCTION				
X	NI CHECKLIST DRAWINGS				
x	EOR REVIEW				
X	ABRICATION INSPECTION				
NA	FASRICATOR CERTIFIED WELD HISPECTION				
х	MATERIAL TEST REPORT (WTR)				
NA.	FABRICATOR NDE INSPECTION				
×	NDE REPORT OF MONOPOLE BASE PLATE (AS RECURRED)				
X	PACICING SUP6				
COTTONAL TESTING AND INSPECTIONS					
,	CONSTRUCTION				
Х	CONSTRUCTION INSPECTIONS				
NA	FOUNDATION INSPECTIONS				
NA.	CONCRETE COMP, STRENGTH AND SLUMP TESTS				
NA.	POST INSTALLED ANCHOR ROD VERIFICATION				
NA NA	BASE PLATE DROUT VERLICATION				
×	CONTRACTOR'S CERTIFIED WELD INSPECTION				
NA	EARTHWORK LET AND DESIGNY				
×	ON SITE COLD GALVANIZING VERIFICATION				
NA.	GUY WIRE TENSION REPORT				
×	OC AS-BUILT DOCUMENTS				
×	INSPECTION OF A JAX BOLTS AND OTTS PER REQUIREMENTS (A SHEET \$-3)				
NA	MICROPEERSON AND FOR NETALLER'S DRILLING AND HIGH ALLATION LOSS AND DAGGO DOCUMENTS				
NA,	REFER TO MOROPLE NOW ANGHOR NOTES FOR SPECIAL INSPECTION AND THISTING REQUIREMENTS.				
CONTIONAL TESTING AND INSPECTIONS					
	POST-CONSTRUCTION				
x	MI INSPECTOR REDUME OR RECORD DRAWING(9)				
NA.	POST INSTALLED ANCHOR ROD PULL-OUT TESTING				
	PHOTOGRAPHS				

NOTE: X DENUTES A DOCUMENT NEEDED FOR THE PMI REPORT NA DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE PMI REPORT



PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 305 East Brood Street: - Quie 600 - Columbia, One 422-55 (2014) 221-6679 **CROWN CASTLE**

BU #806371; HRT 096 943227 WINDSOR, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT: 37514-2522.001.7700

MICHECKLIST CHECKED BY C.M.M. PROVED BY TIP S-6