



Together with Nextel

10 Industrial Ave, Suite 3  
Mahwah, NJ 07430  
Phone: (845)499-4712  
Jennifer Notaro  
Real Estate Consultant

August 22, 2014

**Hand Delivered**

Ms. Melanie A. Bachman  
Acting Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

CC to Property Owner  
Connecticut State Police  
1111 Country Club Road  
Middletown, CT 06457

RE: Sprint Spectrum L.P. notice of intent to modify an existing telecommunications facility located at 46 Fernwood Lane Wilton, CT 06897. Known to Sprint Spectrum L.P. as site CT03XC360.

Dear Ms. Bachman:

In order to accommodate technological changes, implement Code Division Multiple Access (“CDMA”) and/or Long Term Evolution (“LTE”) capabilities, and enhance system performance in the state of Connecticut, Sprint Spectrum L.P. plans to modify the equipment configurations at many of its existing cell sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and its attachments is being sent to the chief elected official of the municipality in which affected cell site is located.

CDMA employs Spread-Spectrum technology and special coding scheme to allow multiple users to be multiplexed over the same physical channel.

LTE is a new high-performance air interface for cellular mobile communications. It is designed to increase the capacity and speed of mobile telephone networks.

Attached is a summary of the planned modifications, including power density calculations reflecting the change in Sprint's operations at the site. Also included is documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration.

The changes to the facility do not constitute modification as defined Connecticut General Statutes ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed or altered. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for the R.C.S.A. Section 16-50j-72(b)(2).

1. The height of the overall structure will not be affected.
2. The proposed changes will not extend the site boundaries. There will be no effect on the site compound.
3. The proposed changes will not increase the noise level at the existing facility by 6 decibels or more.
4. Radio Frequency power density may increase due to the use of one or more CDMA transmissions. Moreover, LTE will utilize additional radio frequencies newly licensed by the FCC for cellular mobile communications. However, the changes will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site.

For the foregoing reasons Sprint Spectrum L.P. respectfully submits that the proposed changes at the referenced site constitute exempt modifications under R.C.S.A. Section 16-50j-72(b)(2).

Please feel free to call me at (845)-499-4712 or email [JNotaro@Transcendwireless.com](mailto:JNotaro@Transcendwireless.com) with questions concerning this matter.  
Thank you for your consideration.

Sincerely,

Jennifer Notaro  
Real Estate Consultant

RADIO FREQUENCY FCC REGULATORY COMPLIANCE  
MAXIMUM PERMISSIBLE EXPOSURE (MPE) ASSESSMENT

Sprint Existing Facility

Site ID: CT03XC360

CTS

46 Fernwood Lane  
Wilton, CT 06897

**July 11, 2014**

**EBI Project Number: 62143782**

July 11, 2014

Sprint  
Attn: RF Engineering Manager  
1 International Boulevard, Suite 800  
Mahwah, NJ 07495

Re: Radio Frequency Maximum Permissible Exposure (MPE) Assessment for Site:  
**CT03XC360 - CTS**

**Site Total: 11.87% - MPE% in full compliance**

EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at 46 Fernwood Lane, Wilton, CT, for the purpose of determining whether the radio frequency (RF) exposure levels from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limit for the cellular band (850 MHz Band) is approximately  $567 \mu\text{W}/\text{cm}^2$ , and the general population exposure limit for the 1900 MHz and 2500 MHz bands is  $1000 \mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## **CALCULATIONS**

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at 46 Fernwood Lane, Wilton, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. All calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

- 1) 3 channels in the 1900 MHz Band were considered for each sector of the proposed installation.
- 2) 1 channel in the 800 MHz Band was considered for each sector of the proposed installation
- 3) 2 channels in the 2500 MHz Band were considered for each sector of the proposed installation.
- 4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

- 6) The antennas used in this modeling are the RFS APXVSPP18-C-A20 and the RFS APXVTM14-C-I20. This is based on feedback from the carrier with regards to anticipated antenna selection. The RFS APXVSPP18-C-A20 has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz. The RFS APXVTM14-C-I20 has a 15.9 dBd gain value at its main lobe at 2500 MHz. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 7) The antenna mounting height centerline for the proposed antennas is **106 feet** above ground level (AGL).
- 8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits

Site ID	CT03XC360 - CTS
Site Address	46 Fernwood Lane, Wilton, CT, 06897
Site Type	Self Support Tower

**Sector 1**

Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain (10 db reduction)	Antenna Height (ft)	analysis height	Cable Size	Cable Loss (dB)	Additional Loss (dB)	ERP	Power Density Percentage
1a	RFS	APXVSP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	3	60	5.9	106	100	1/2 "	0.5	0	208.04	0.75%
1a	RFS	APXVSP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	3.4	106	100	1/2 "	0.5	0	39.00	0.25%
1B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	106	100	1/2 "	0.5	0	138.69	0.88%
Sector total Power Density Value:																1.87%

**Sector 2**

Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain (10 db reduction)	Antenna Height (ft)	analysis height	Cable Size	Cable Loss (dB)	Additional Loss (dB)	ERP	Power Density Percentage
2a	RFS	APXVSP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	3	60	5.9	106	100	1/2 "	0.5	0	208.04	0.75%
2a	RFS	APXVSP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	3.4	106	100	1/2 "	0.5	0	39.00	0.25%
2B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	106	100	1/2 "	0.5	0	138.69	0.88%
Sector total Power Density Value:																1.87%

**Sector 3**

Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain (10 db reduction)	Antenna Height (ft)	analysis height	Cable Size	Cable Loss (dB)	Additional Loss (dB)	ERP	Power Density Percentage
3a	RFS	APXVSP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	3	60	5.9	106	100	1/2 "	0.5	0	208.04	0.75%
3a	RFS	APXVSP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	3.4	106	100	1/2 "	0.5	0	39.00	0.25%
3B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	106	100	1/2 "	0.5	0	138.69	0.88%
Sector total Power Density Value:																1.87%

Site Composite MPE %	
Carrier	MPE %
Sprint	5.62%
Field Measurements for all additional systems on site	6.25%
<b>Total Site MPE %</b>	<b>11.87%</b>

## Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public Maximum Permissible Exposure (MPE) to radio frequency energy.

The anticipated Maximum Composite contributions from the Sprint facility are **5.62% (1.87% from sector 1, 1.87% from sector 2 and 1.87% from sector 3)** of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **11.87%** of the allowable FCC established general public limit sampled at 6 feet above ground level. This total composite site value is based upon MPE values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.



**Scott Heffernan**  
RF Engineering Director

**EBI Consulting**  
21 B Street  
Burlington, MA 01803

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# DETAILED STRUCTURAL ANALYSIS AND EVALUATION OF AN EXISTING 180' SELF- SUPPORTING LATTICE TOWER FOR NEW ANTENNA ARRANGEMENT

**Sprint Site #:** CT03XC360  
**Site Name:** Connecticut State Police Tower #31  
**Address:** 46 Fenwood Lane  
Wilton, Connecticut

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*prepared for*



**1 International Blvd.  
Suite 800  
Mahwah, NJ. 07495**

*prepared by*



**URS CORPORATION  
500 ENTERPRISE DRIVE, SUITE 3B  
ROCKY HILL, CT 06067  
TEL. 860-529-8882**

**36928700.00000  
TWS-015**

**May 16, 2014**

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1. EXECUTIVE SUMMARY

This report summarizes the structural analysis and evaluation of the 180' self-supporting lattice tower located at 46 Fenwood Lane in Wilton, Connecticut. The analysis was conducted in accordance with the 2005 Connecticut State Building Code, the TIA/EIA-222-F standard and additional requirements of the Connecticut State Police for wind velocity of 90 mph concurrent with 1/2" ice design wind load. The antenna loading considered in the analysis consists of all existing and proposed antennas, transmission lines, and ancillary items as outlined in the Introduction Section of this report. The proposed Sprint installation is as follows:

Antenna and Mount	Carrier	Antenna Center Elevation
<b>Install:</b>		
(3) RFS APXVTM14-C-20 Panel Antennas		
(3) TD-RRH-8x20-25 RRH Units		
(1) Junction Box	<b>Sprint</b>	<b>@ 106'</b>
(27) 8' Jumper cables	<b>(Proposed)</b>	
(3) 8' Comscope AISG Cables		
(1) ALU Fiber Optic Cable		

The result of the analysis indicates that the existing tower, foundation and anchor bolts have sufficient capacity to support the proposed loading conditions without modification. The tower structure, foundation and anchor bolts are considered structurally adequate for the proposed antenna loading with the wind load classification specified above.

The tower deflection (sway) is 0.7097 degrees, and the tower rotation (twist) is 0.0349 degrees with a wind velocity of 90 mph concurrent with 0.5" ice. **The tower deflection and rotation are within the Connecticut State Police specification of 0.75 degrees for combined deflection (sway) and rotation (twist).**

The above analysis is based upon completion of tower foundation modifications required for T-mobile antenna loadings, per URS Corporation structural analysis and reinforcement design, project number HPC-070 (Rev. 1), signed and sealed April 11, 2014. If this foundation modification has not been constructed, notify the engineer in writing immediately.

**1. EXECUTIVE SUMMARY - *continued***

This analysis is based on:

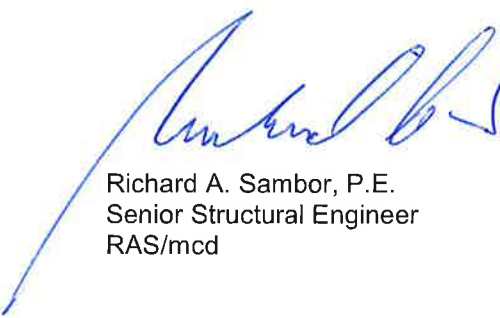
- 1) The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- 2) Tower geometry and structural member sizes utilized in the preparation of this report obtained from the manufacturers original design documents prepared by Bayar and Associates dated July 1990.
- 3) Sprint antennas taken from CT Police Sites Flat File, dated April 22, 2014.
- 4) Antenna inventory provided by the Connecticut State Police via email on February 8, 2014.
- 5) Previous structural analysis and reinforcement design performed by URS Corporation, project number HPC-070 (Rev 1), signed and sealed April 11, 2014.
- 6) Antenna and mount configuration as specified on the following page of this report.

This report is only valid as per the assumptions and data utilized in this report for antenna inventory, mounts and associated cables. The user of this report shall field verify the assumption of the antenna and mount configuration. Notify the engineer in writing immediately if any of the information in this report is found to be other than specified.

If you should have any questions, please call.

Sincerely,

**URS Corporation AES**

  
Richard A. Sambor, P.E.  
Senior Structural Engineer  
RAS/mcd





## 2. INTRODUCTION

The subject tower is located at 46 Fenwood Lane in Wilton, Connecticut. The structure is a 180' four sided self-supporting lattice tower designed by Bayar and Associates.

The inventory is summarized in the table below:

<b>Antenna Type</b>	<b>Carrier</b>	<b>Mount</b>	<b>Mount Elevation</b>	<b>Cable</b>
(3) 6' Dishes (Wind Load)	CSP 69 to 71 (reserved)	Leg Mounted	180'	N/A
(2) Scala OGT9-806 (2) TX/RX 101-83B-09 (1) 7' Omni	CSP 1 to 4,6 (existing)	(3) 4' Stand-Off	180'	(4) 1-5/8" (1) 7/8"
(1) 10' Dipole (1) TX/RX TMA	CSP 7 & 67 (existing)	Pipe Mounted	180'	(1) 7/8" (1) 1/2"
(1) 6' Dishes	CSP – 59 (existing)	(1) Pipe Mounts	180'	(1) WEP65
(2) 6' Dishes	CSP 5 & 36 (existing)	(2) Pipe Mounts	176'	(2) WEP65
(1) 8-Bay Dipole	FCP – 12 (existing)	6' Standoff	170'	(1) 7/8"
(1) 5' Omni	CSP – 10 (existing)	6' Standoff	170'	(1) 7/8"
(1) 3' Omni	CAP – 25 (existing)	Leg Mounted	169'	(1) 7/8"
(6) Powerwave 7770 (6) LGP21401 TMAs	AT&T (existing)	(3) T-Frames	163'	(12) 1-5/8"
(3) Powerwave P-65-16-XLH-RR (6) Ericsson RRU (12) LGP21901 Diplexers (3) Powerwave TT19-08BP111-001 TMAs (1) RAYCAP Surge Protector	AT&T (existing)	Shared with Above	163'	(1) 3" Flex Conduit with Fiber & DC Cables
(3) TX/RX 101-83B-08-T5 (1) TX/RX TMA	CSP 63 to 66 (existing)	Leg Mounted	160'	(3) 1-5/8" (1) 1/2"
(1) DB636	NEU – 57 (existing)	4' Standoff	150'	(1) 7/8"
(1) 3' Yagi	WTR – 28 (existing)	6' Standoff	145'	(1) 7/8"
(1) 6' Dish	CSP – 35 (existing)	Pipe Mounted	130'	(1) WEP65
(3) Ericsson AIR21 B2A B4P Panel Antennas (3) Ericsson AIR21 B4A/B2P Panel Antennas (3) (UMTS) TMA Units (3) (LTE) TMA Units	T-Mobile (Existing)	(3) Antenna Mounts	122'	(6) 1 1/4" (6) 1-1/4" (2) Fiber Optic Cables
(2) DB586-Y (one inverted and one upright)	NEU 30 & 31 (existing)	6' Standoff	120'	(2) 7/8"

<i>Antenna Type</i>	<i>Carrier</i>	<i>Mount</i>	<i>Mount Elevation</i>	<i>Cable</i>
(1) Celwave PD-128 (1) 17' Omni	WPD 33 & 55 (existing)	6' Standoff	120'	(2) 7/8"
(1) Celwave PD-128	CSP – 8 (existing)	Leg Mounted	120'	(1) 7/8"
(1) ASP-711	WTR – 29 (existing)	Leg Mounted	116'	(1) 7/8"
(1) Decibel DB-222	DHS – 9 (existing)	Leg Mounted	112'	(1) 7/8"
<b>(3) RFS APXVTM14-C-20 Panel Antennas</b> <b>(3) TD-RRH-8x20-25 RRH Units</b> <b>(1) Junction Box</b>	<b>Sprint</b> <b>(Proposed)</b>	<i>See Below Mount</i>	<b>106'</b>	<b>(27) 8' Jumper cables</b> <b>(3) 8' Comscope AISG Cables</b> <b>(1) ALU Fiber Optic Cable</b>
(3) APXVSP18-C (6) ALU RRH	Sprint (existing)	(3) 10' Frame (existing)	106'	(3) RFS Hybriflex Cables
(1) BCD806-09NE	CSP – 62 (existing)	Leg Mounted	101'	(1) 1-5/8"
(1) 4' Grid Dish	CSP – 11 (existing)	Pipe Mounted	100'	(1) 7/8"
(1) 15' Omni	DEA – 32 (existing)	4' Standoff	100'	(1) 7/8"
(1) 20' 4-Bay Dipole	USS – 26 (existing)	3' Standoff	85'	(1) 7/8"
(1) Ice Shield for 6' Grid Dish Below	CSP (existing)	4' Standoff	80'	N/A
(1) 6' Grid Dish	CSP – 13 (existing)	Pipe Mounted	75'	(1) 1/2"
(1) GPS	Sprint (existing)	3' Standoff	56'	(1) 1/2"
(1) DB-803 Omni	CSP – 68 (existing)	3' Stand-Off	47'	(1) 1/2"

This structural analysis of the communications tower was performed by URS Corporation, AES (URS) for Sprint. The purpose of this analysis was to analyze the existing tower for its existing and proposed antenna loads. This analysis was conducted to evaluate rotation (twist), deflection (sway) and stress on the tower, and the effect of forces to the foundation of the tower resulting from existing and proposed antenna arrangements.

### 3. ANALYSIS METHODOLOGY AND LOADING CONDITIONS

The structural analysis was done in accordance with the 2005 Connecticut State Building Code, TIA/EIA-222-F - Structural Standard for Steel Antenna Towers and Antenna Supporting Structures, and the American Institute of Steel Construction (AISC) Manual of Steel Construction - Allowable Stress Design (ASD).

The analysis was conducted using TNX Tower 6.0.0.8. Two load conditions were evaluated as shown below which were compared to allowable stresses according to AISC and TIA/EIA.

Load Condition 1 = 90 mph (fastest mile) Wind Load + Tower Dead Load

Load Condition 2 = 90 mph (fastest mile) Wind Load (with ice) + Ice Load + Tower Dead Load

The TIA/EIA standard permits a one-third increase in allowable stresses for towers and monopoles less than 700 feet tall. For the purposes of this analysis, in computing the load capacity the allowable stresses of the tower members were increased by one-third.

#### 4. FINDINGS AND EVALUATION

The combined axial and bending stresses on the tower structure were evaluated to compare with the allowable stress in accordance with AISC. The results of the analysis indicate that the calculated stresses under the proposed loading are within the allowable stresses for the tower structure, foundation and anchor bolts.

The tower deflection and rotation are within the Connecticut State Police specification of 0.75 degrees for deflection (sway) and rotation (twist).

##### Tower Base Reactions:

Description	Current
Pier Compression (kips)	453
Pier Uplift (kips)	404
Overall Overturning (kip-ft)	10769
Overall Shear (kips)	99
Shear per Leg (kips)	43

##### Controlling Tower Component Stress vs. Capacity Summary:

Component / (Section No.)	Critical Component Size	Controlling Elevation	Stress (% capacity)	Pass/Fail
Leg (T19)	L8x8x1 1/8"	0' – 10'	99.3	Pass
Diagonal (T12)	L3 1/2X3X1/4	80'-90'	84.8	Pass
Horizontal (T19)	2L2 1/2x2 1/2x1/4	0'-10'	53.5	Pass
Secondary Horizontal (T18)	L3 1/2x3 1/2x1/4	10'-20'	86.9	Pass
Top Girt (T3)	L2x2x3/16	159.049'-163.573'	12.9	Pass
Redund Horz 1 Bracing (T19)	L2 1/2x2 1/2x3/16	0'-10'	44.4	Pass
Redund Diag 1 Bracing (T19)	L2 1/2x2 1/2x3/16	0'-10'	73.3	Pass
Redund Hip 1 Bracing (T19)	L2 1/2x2 1/2x3/16	0'-10'	0.3	Pass
Redund Sub Horz Bracing (T19)	L3x3x5/16	0'-10'	68.4	Pass
Inner Bracing (T19)	2L2x2 1/2x3/16	0'-10'	3.5	Pass
Anchor Bolts	(4) 2-1/2" dia. A36 bolts	N/A	88	Pass

##### Foundation Summary:

Component	Required / Allowable	Computed	% Capacity	Pass/Fail
Overturning Moment Factor of Safety	2.0 min	2.30	87.0	Pass
Foundation Bearing Pressure	3.4 ksf max	2.4679 ksf	72.6	Pass

##### Tower Twist & Sway at Top:

Description	Current	Total Allowable
Tower Twist (degrees)	0.0349	---
Tower Sway (degrees)	0.7097	
Total Deflection (degrees)	0.7446	0.75

## 5. CONCLUSIONS

The result of the analysis indicates that the existing tower, foundation and anchor bolts have sufficient capacity to support the proposed loading conditions without modification. The tower structure, foundation and anchor bolts are considered structurally adequate for the proposed antenna loading with the wind load classification specified above. The tower deflection (sway) is 0.7097 degrees, and the tower rotation (twist) is 0.0349 degrees with a wind velocity of 90 mph concurrent with 0.5" ice. **The tower deflection and rotation are within the Connecticut State Police specification of 0.75 degrees for combined deflection (sway) and rotation (twist).**

The above analysis is based upon completion of tower foundation modifications required for T-mobile antenna loadings, per URS Corporation structural analysis and reinforcement design, project number HPC-070 (Rev. 1), signed and sealed April 11, 2014. If this foundation modification has not been constructed, notify the engineer in writing immediately.

### Limitations/Assumptions:

This report is based on the following:

1. Tower inventory as listed in this report.
2. Tower is properly installed and maintained.
3. All members are as specified in the original design documents and are in good condition.
4. All required members are in place and all previous modifications have been performed.
5. All bolts are in place and are properly tightened.
6. Tower is in plumb condition.
7. All member protective coatings are in good condition.
8. All tower members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.
9. Foundations were properly constructed to support original design loads as specified in the original design documents.

URS is not responsible for any modifications completed prior to or hereafter in which URS is not or was not directly involved. Modifications include but are not limited to:

- A. Adding antennas
- B. Removing/replacing antennas
- C. Adding coaxial cables

URS hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations, and conclusions are based upon information contained and set forth herein. If you are aware of any information which conflicts with that which is contained herein, or you are aware of any defects arising from original design, material, fabrication, or erection deficiencies, you should disregard this report and immediately contact URS. URS disclaims all liability for any representation, recommendation, or conclusion not expressly stated herein.

After the Contractor has successfully completed the installation and the work has been accepted, the owner will be responsible for the ongoing and periodic inspection and maintenance of the tower.

The owner shall refer to TIA/EIA-222-F for recommendations for maintenance and inspection. The frequency of the inspection and maintenance intervals is to be determined by the owner based upon actual site and environmental conditions. It is recommended that a complete and thorough inspection of the entire tower structural system be performed at least yearly and more frequently as conditions warrant. According to TIA/EIA-222-F section 14.1, Note 1: It is recommended that the structure be inspected after severe wind and/or ice storms or other extreme loading condition.

## **6.) DRAWINGS AND DATA**

## TNX TOWER INPUT / OUTPUT SUMMARY

DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
6 Standoff (CSP)	180	DB636-A (NEU - 57)	150
3" Dia x 15' Omni (CSP - 1)	180	6 Standoff (CSP)	145
3" Yagi (WTR - 28)	180	3" Yagi (WTR - 28)	145
6 Standoff (CSP)	180	6 Standoff (CSP)	145
OGT9-806 (CSP - 6)	180	6 Standoff (CSP)	145
3" Dia x 15' Omni (CSP - 3)	180	6 Standoff (CSP)	143
6 Standoff (CSP)	180	106"x4" Pipe Mount (CSP)	133
7 Whip (CSP - 4)	180	3 Standoff (CSP)	132
106"x4" Pipe Mount (CSP)	180	PA6-65AC (CSP - 35)	130
10' Dipole (CSP - 7)	180	LeBlanc 10' Standoff (1) (CSP)	126
TMA (CSP - 67)	180	EUSF-10-U (T-Mobile)	122
PA6-65AC (CSP - 69)	180	EUSF-10-U (T-Mobile)	122
PA6-65AC (CSP - 70)	180	EUSF-10-U (T-Mobile)	122
PA6-65AC (CSP - 71)	180	(2) AIR B2AB4P (T-Mobile)	122
PA6-65AC (CSP - 69)	180	(2) AIR B2AB4P (T-Mobile)	122
106"x4" Pipe Mount (CSP)	176	(2) TMA (T-Mobile)	122
106"x4" Pipe Mount (CSP)	176	(2) TMA (T-Mobile)	122
106"x4" Pipe Mount (CSP)	176	(2) TMA (T-Mobile)	122
PA6-65AC (CSP - 5)	176	(2) TMA (T-Mobile)	120
PA6-65AC (CSP - 36)	176	Rehm 6 Side-Arm(1) (NU - 3031)	120
106"x4" Pipe Mount (CSP)	176	3" Dia x 15' Omni (WPD - 55)	120
6 Standoff (CSP)	172	PD128-1 (CSP - 8)	120
6 Standoff (CSP)	172	PD128-1 (WPD - 33)	120
20' 6 Bay D-Pole (FCP - 12)	170	(2) DB596Y (NU - 3031)	120
4 Omni (CSP - 10)	170	ASPT11 (WTR - 28)	116
4 Omni (CAP - 25)	169	3 Standoff (CSP)	115
7770 (ATT)	163	6 Standoff (CSP)	115
(2) LGP 219mm (ATT)	163	6 Standoff (CSP)	112
TT19-08BP11-001 TMA (ATT)	163	106"x4" Pipe Mount (CSP)	112
P65-16-XLHRR (ATT)	163	DB222 DHS - 9)	112
(2) RRU (ATT)	163	12' Wireless Frame (Sprint)	106
Raycap DC5-46-60-16-8F DC Power Surge Protection (ATT)	163	12' Wireless Frame (Sprint)	106
7770 (ATT)	163	12' Wireless Frame (Sprint)	106
(2) LGP 219mm (ATT)	163	APXVSP18-C (Sprint)	106
(2) LGP 219mm (ATT)	163	APXVSP18-C (Sprint)	106
(2) LFG21401 TMA (ATT)	163	APXVSP18-C (Sprint)	106
(2) LFG21401 TMA (ATT)	163	APXVSP18-C (Sprint)	106
(2) LGP 219mm (ATT)	163	APXVSP18-C (Sprint)	106
(2) LGP 219mm (ATT)	163	APXVSP18-C (Sprint)	106
TT19-08BP11-001 TMA (ATT)	163	APXVSP18-C (Sprint)	106
P65-16-XLHRR (ATT)	163	APXVSP18-C (Sprint)	106
(2) RRU (ATT)	163	TD-RRH8x20-25 (Sprint)	106
T-Frame (ATT)	163	TD-RRH8x20-25 (Sprint)	106
T-Frame (ATT)	163	TD-RRH8x20-25 (Sprint)	106
7770 (ATT)	163	Jurisdiction box (Sprint)	106
(2) LGP 219mm (ATT)	163	APXVSP18-C (Sprint)	106
(2) LFG21401 TMA (ATT)	163	APXVSP18-C (Sprint)	106
7770 (ATT)	163	(2) ALU RRR (Sprint)	106
(2) LGP 219mm (ATT)	163	(2) ALU RRR (Sprint)	106
TT19-08BP11-001 TMA (ATT)	163	(2) ALU RRR (Sprint)	106
P65-16-XLHRR (ATT)	163	LeBlanc 10' Standoff (1) (CSP)	101
(2) RRU (ATT)	163	SC479-HFLDF (CSP - 62)	101
T-Frame (ATT)	163	4' Grid Dish (CSP - 11)	100
T-Frame (ATT)	163	3' Dia x 15' Omni (DEA - 32)	100
7770 (ATT)	163	3 Standoff (CSP)	88
(2) LGP 219mm (ATT)	163	3 Standoff (CSP)	85
(2) LFG21401 TMA (ATT)	163	20' 4 Bay Dipole (USS - 26)	85
T-Frame (ATT)	163	6" Ice Shield (CSP)	80
(2) LGP 219mm (ATT)	163	106"x4" Pipe Mount (CSP)	76
3" Dia x 15' Omni (CSP - 63)	160	6" Grid Dish (CSP - 13)	75
3" Dia x 15' Omni (CSP - 64)	160	3 Standoff (Sprint)	56
3" Dia x 15' Omni (CSP - 65)	160	GPS (Sprint)	56
TMA (CSP - 66)	160	3 Standoff (CSP)	47
2" Dia 10' Omni (CSP)	150	DB903U-L-Y (CSP - 68)	47

MARK	SIZE	MARK	SIZE
A	L2x2x3/16		

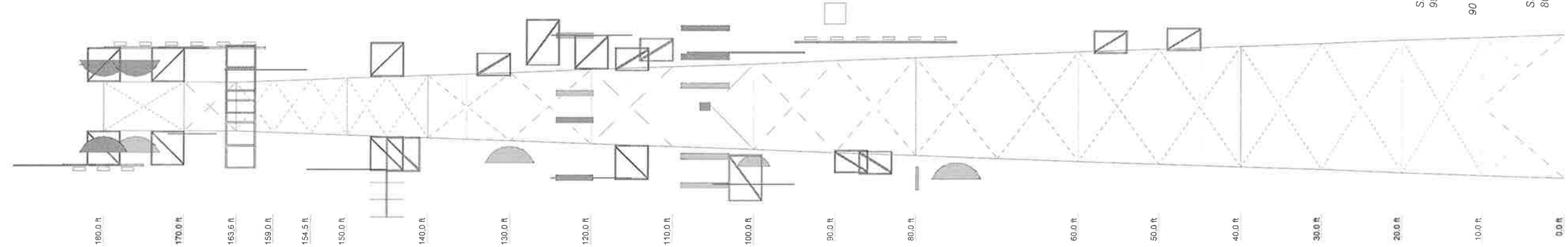
GRADE	Fy	GRADE	Fy
A36	36 ksi	A36	36 ksi

MARK	SIZE	MARK	SIZE
A	L2x2x3/16		

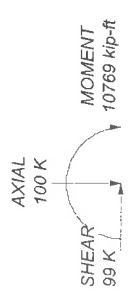
GRADE	Fu	GRADE	Fy	Fu
A36	58 ksi	A36	36 ksi	58 ksi

GRADE	Fu	GRADE	Fy	Fu
A36	58 ksi	A36	36 ksi	58 ksi

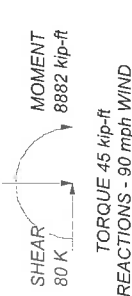
- TOWER DESIGN NOTES**
1. Tower designed for a 90 mph basic wind in accordance with the TIA/EIA-222-F Standard.
  2. Tower is also designed for a 90 mph basic wind with 0.50 in ice.
  3. Deflections are based upon a 90 mph wind.
  4. TOWER RATING: 99.3%



MAX. CORNER REACTIONS AT BASE:  
 DOWN: 453 K  
 UPLIFT: -404 K  
 SHEAR: 43 K



TORQUE 75 kip-ft  
 90 mph WIND - 0.5000 in ICE



TORQUE 45 kip-ft  
 REACTIONS - 90 mph WIND

**URS Corporation**  
 500 Enterprise Drive, Suite 3B  
 Rocky Hill, CT 06067  
 Phone: 860-529-8882  
 FAX: 860-529-3991

Job: **180' Lattice Tower - CSP**  
 Project: **Wilton, Connecticut (TWS-015)**  
 Client: **Sprint**  
 Code: **TIA/EIA-222-F**  
 Path: **W:\Projects\180' Lattice Tower\180' Lattice Tower.dwg**

App'd: **MCD**  
 Drawn by: **MCD**  
 Date: **05/14/14**  
 Scale: **NTS**  
 Dwg No: **E-1**



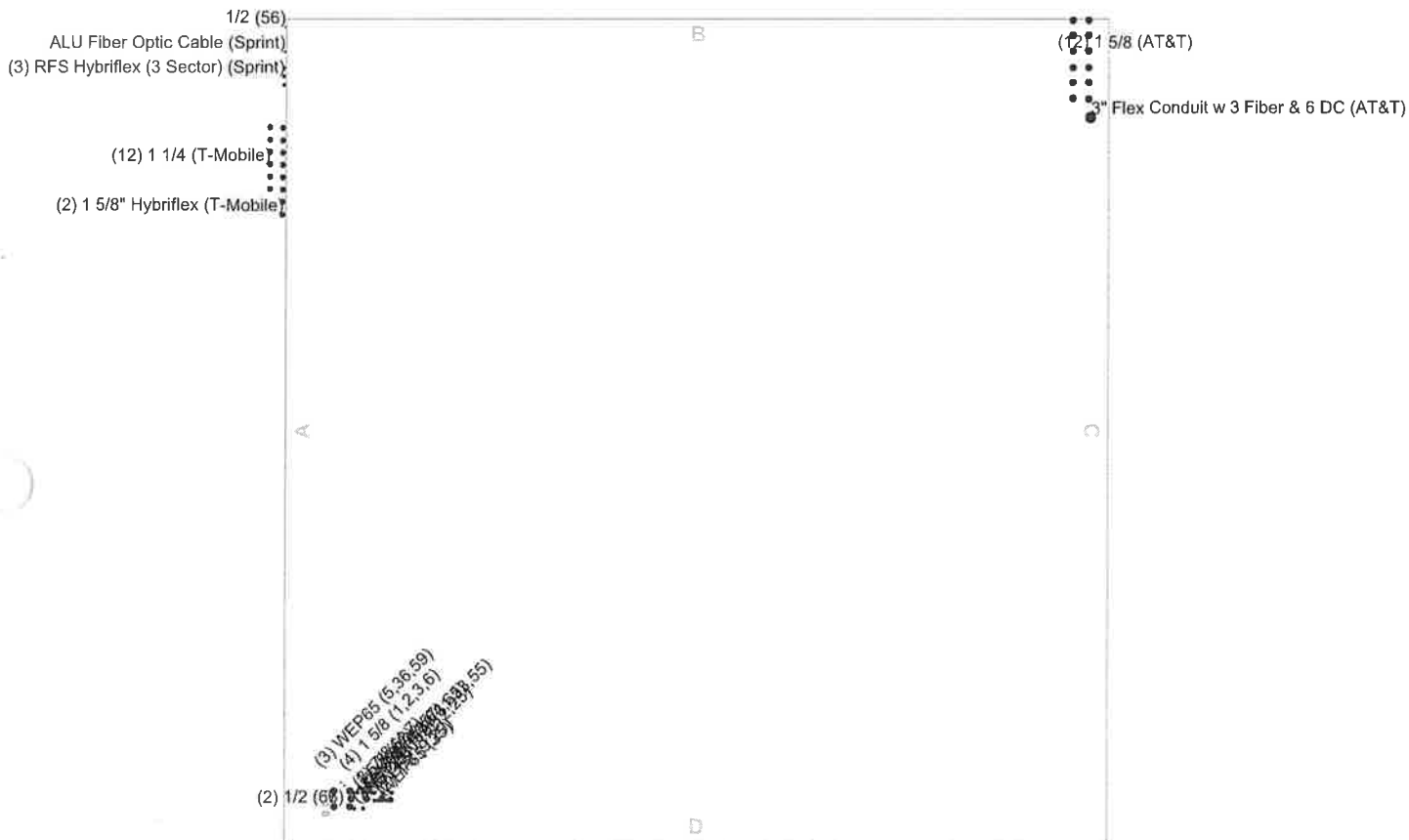
# TNX TOWER FEEDLINE DISTRIBUTION



# TNX TOWER FEEDLINE PLAN

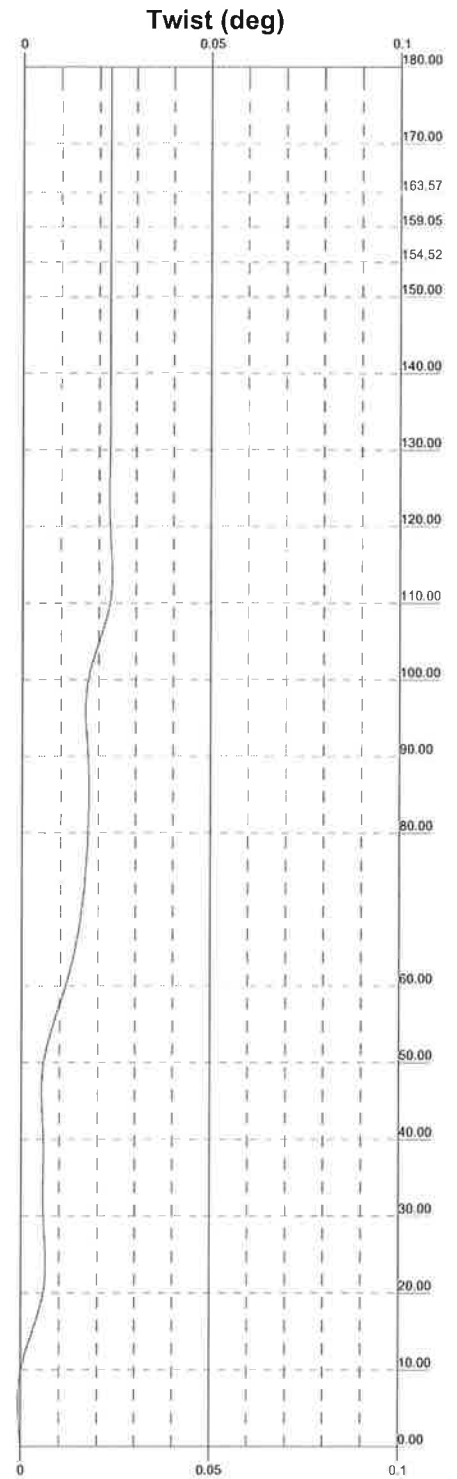
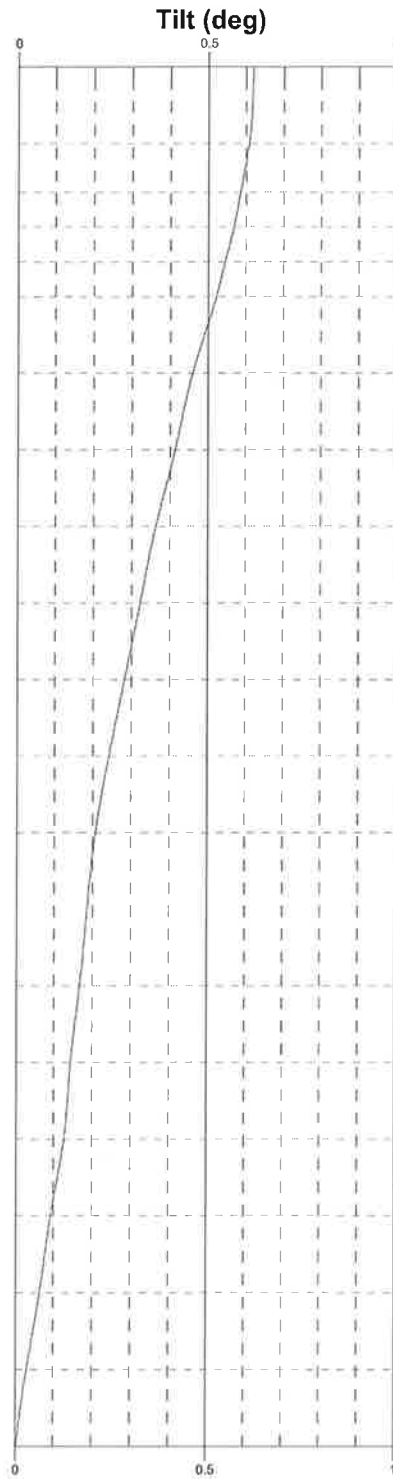
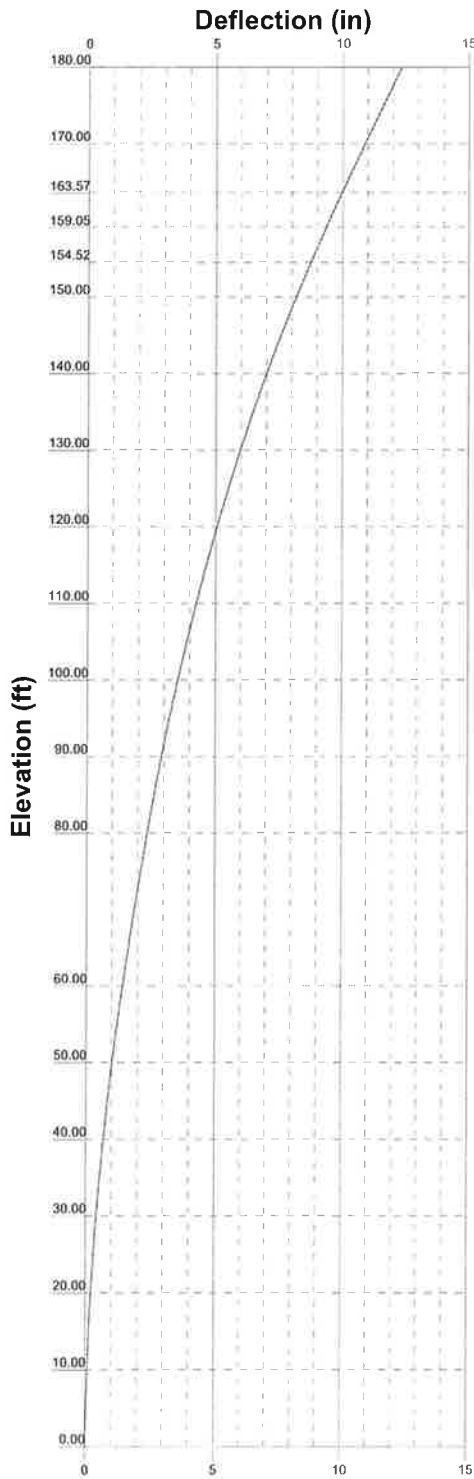
# Feedline Plan

Round      Flat      App In Face      App Out Face



<b>URS Corporation</b>			<b>Job: 180' Lattice Tower - CSP</b>		
500 Enterprise Drive, Suite 3B			Project: <b>Wilton, Connecticut (TWS-015)</b>		
Rocky Hill, CT 06067			Client: <b>Sprint</b>	Drawn by: <b>MCD</b>	App'd:
Phone: 860-529-8882			Code: <b>TIA/EIA-222-F</b>	Date: <b>05/14/14</b>	Scale: <b>NTS</b>
FAX: 860-529-3991			Path:		Dwg No. <b>E-7</b>
W:\Temp\land Works\TWS\1682700-TWS015\Wilton\051414\Feed\180' Lattice Wilton CSP.dwg					

## TNX TOWER DEFLECTION, TILT AND TWIST



<p><b>URS Corporation</b>                  500 Enterprise Drive, Suite 3B                  Rocky Hill, CT 06067                  Phone: 860-529-8882                  FAX: 860-529-3991</p>	<p><b>Job: 180' Lattice Tower - CSP</b></p>		
	<p>Project: <b>Wilton, Connecticut (TWS-015)</b></p>		
	Client: Sprint	Drawn by: MCD	App'd:
	Code: TIA/EIA-222-F	Date: 05/14/14	Scale: NTS
	Path: \\filerepo\w\w\w\TWS\3818700_11\0515_0000\GEN\Figs\180' Lattice Tower CSP.dwg	Dwg No. E-5	

## DETAILED OUTPUT

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 1 of 63
	<b>Project</b> Wilton, Connecticut (TWS-015)	<b>Date</b> 11:06:21 05/14/14
	<b>Client</b> Sprint	<b>Designed by</b> MCD

## Tower Input Data

The main tower is a 4x free standing tower with an overall height of 180.00 ft above the ground line.  
The base of the tower is set at an elevation of 0.00 ft above the ground line.  
The face width of the tower is 6.00 ft at the top and 17.73 ft at the base.  
This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

- Basic wind speed of 90 mph.
- Nominal ice thickness of 0.5000 in.
- Ice density of 56 pcf.
- A wind speed of 90 mph is used in combination with ice.
- Temperature drop of 50 °F.
- Deflections calculated using a wind speed of 90 mph.
- A non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- Stress ratio used in tower member design is 1.333.
- Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

## Options

- |  |  |  |
|--|--|--|
| <ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>√ Include Bolts In Member Capacity</li> <li>√ Leg Bolts Are At Top Of Section</li> <li>√ Secondary Horizontal Braces Leg</li> <li>√ Use Diamond Inner Bracing (4 Sided)</li> <li>Add IBC .6D+W Combination</li> </ul> | <ul style="list-style-type: none"> <li>Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>√ Use Clear Spans For KL/r</li> <li>Retension Guys To Initial Tension</li> <li>Bypass Mast Stability Checks</li> <li>Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <li>Autocalc Torque Arm Areas</li> <li>SR Members Have Cut Ends</li> <li>√ Sort Capacity Reports By Component</li> <li>√ Triangulate Diamond Inner Bracing</li> </ul> | <ul style="list-style-type: none"> <li>Treat Feedline Bundles As Cylinder</li> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>√ Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>√ All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feedline Torque</li> <li>Include Angle Block Shear Check</li> <li style="text-align: center;"><b>Poles</b></li> <li>Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> </ul> |
|--|--|--|





<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	3 of 63
	<b>Project</b>	Wilton, Connecticut (TWS-015)	<b>Date</b>	11:06:21 05/14/14
	<b>Client</b>	Sprint	<b>Designed by</b>	MCD

Tower Section	Tower Elevation ft	Diagonal Spacing ft	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset in	Bottom Girt Offset in
T1	180.00-170.00	10.00	X Brace	No	Yes	0.0000	0.0000
T2	170.00-163.57	6.43	X Brace	No	No	0.0000	0.0000
T3	163.57-159.05	4.52	X Brace	No	No	0.0000	0.0000
T4	159.05-154.52	4.52	X Brace	No	No	0.0000	0.0000
T5	154.52-150.00	4.52	X Brace	No	No	0.0000	0.0000
T6	150.00-140.00	5.00	X Brace	No	No	0.0000	0.0000
T7	140.00-130.00	10.00	X Brace	No	Yes	0.0000	0.0000
T8	130.00-120.00	10.00	X Brace	No	Yes	0.0000	0.0000
T9	120.00-110.00	10.00	X Brace	No	Yes	0.0000	0.0000
T10	110.00-100.00	10.00	X Brace	No	Yes	0.0000	0.0000
T11	100.00-90.00	10.00	X Brace	No	Yes	0.0000	0.0000
T12	90.00-80.00	10.00	X Brace	No	Yes	0.0000	0.0000
T13	80.00-60.00	10.00	X Brace	No	Yes	0.0000	0.0000
T14	60.00-50.00	10.00	X Brace	No	Yes	0.0000	0.0000
T15	50.00-40.00	10.00	X Brace	No	Yes	0.0000	0.0000
T16	40.00-30.00	10.00	X Brace	No	Yes	0.0000	0.0000
T17	30.00-20.00	10.00	X Brace	No	Yes	0.0000	0.0000
T18	20.00-10.00	10.00	X Brace	No	Yes	0.0000	0.0000
T19	10.00-0.00	10.00	K1 Down	No	Yes	0.0000	0.0000

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 180.00-170.00	Single Angle	L3 1/2x3 1/2x3/8	A36 (36 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T2 170.00-163.57	Single Angle	L5x5x5/16	A36 (36 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T3 163.57-159.05	Single Angle	L5x5x5/16	A36 (36 ksi)	Single Angle	L2x2x3/16	A36 (36 ksi)
T4 159.05-154.52	Single Angle	L5x5x5/16	A36 (36 ksi)	Single Angle	L2 1/2x2x3/16	A36 (36 ksi)
T5 154.52-150.00	Single Angle	L5x5x5/16	A36 (36 ksi)	Single Angle	L2 1/2x2x3/16	A36 (36 ksi)
T6 150.00-140.00	Single Angle	L5x5x3/8	A36 (36 ksi)	Single Angle	L2 1/2x2x3/16	A36 (36 ksi)
T7 140.00-130.00	Single Angle	L6x6x1/2	A36 (36 ksi)	Single Angle	L3x2 1/2x1/4	A36 (36 ksi)
T8 130.00-120.00	Single Angle	L6x6x1/2	A36 (36 ksi)	Single Angle	L3x3x1/4	A36 (36 ksi)
T9 120.00-110.00	Single Angle	L6x6x3/4	A36 (36 ksi)	Single Angle	L3x3x1/4	A36 (36 ksi)
T10 110.00-100.00	Single Angle	L6x6x3/4	A36 (36 ksi)	Single Angle	L3 1/2x3x1/4	A36 (36 ksi)
T11 100.00-90.00	Single Angle	L8x8x3/4	A36 (36 ksi)	Single Angle	L3 1/2x3x1/4	A36 (36 ksi)
T12 90.00-80.00	Single Angle	L8x8x3/4	A36 (36 ksi)	Single Angle	L3 1/2x3x1/4	A36 (36 ksi)
T13 80.00-60.00	Arbitrary Shape	L8x8x1 w/ 1/2x7 Plates	A36 (36 ksi)	Double Angle	2L2 1/2x2x3/16	A36 (36 ksi)
T14 60.00-50.00	Arbitrary Shape	L8x8x1-1/8 w/ 1/2x7 Plates	A36 (36 ksi)	Double Angle	2L2 1/2x2x3/16	A36 (36 ksi)
T15 50.00-40.00	Arbitrary Shape	L8x8x1-1/8 w/ 1/2x7 Plates	A36 (36 ksi)	Double Angle	2L2 1/2x2x3/8	A36 (36 ksi)
T16 40.00-30.00	Single Angle	L8x8x1 1/8	A36 (36 ksi)	Double Angle	2L2 1/2x2x3/8	A36 (36 ksi)

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	4 of 63
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Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T17 30.00-20.00	Single Angle	L8x8x1 1/8	A36 (36 ksi)	Double Angle	2L2 1/2x2x3/8	A36 (36 ksi)
T18 20.00-10.00	Single Angle	L8x8x1 1/8	A36 (36 ksi)	Double Angle	2L2 1/2x2x3/8	A36 (36 ksi)
T19 10.00-0.00	Single Angle	L8x8x1 1/8	A36 (36 ksi)	Double Angle	2L2 1/2x2 1/2x1/4	A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 180.00-170.00	Single Angle	L2x2x3/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T2 170.00-163.57	Single Angle	L2x2x3/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T3 163.57-159.05	Single Angle	L2x2x3/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T6 150.00-140.00	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T7 140.00-130.00	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T13 80.00-60.00	Single Angle	L2 1/2x2 1/2x1/4	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T16 40.00-30.00	Double Angle	2L2x2x3/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T1 180.00-170.00	1	Single Angle	L2x2x3/16	A36 (36 ksi)	Double Angle		A36 (36 ksi)
T9 120.00-110.00	1	Single Angle	L2x2x3/16	A36 (36 ksi)	Single Angle	L2 1/2x2 1/2x1/4	A36 (36 ksi)
T11 100.00-90.00	None	Single Angle		A36 (36 ksi)	Single Angle	L2 1/2x2 1/2x1/4	A36 (36 ksi)
T14 60.00-50.00	None	Single Angle		A36 (36 ksi)	Double Angle	2L2x2x3/16	A36 (36 ksi)
T18 20.00-10.00	None	Single Angle		A36 (36 ksi)	Double Angle	2L2x2x3/16	A36 (36 ksi)
T19 10.00-0.00	None	Single Angle		A36 (36 ksi)	Double Angle	2L2 1/2x2 1/2x1/4	A36 (36 ksi)

### Tower Section Geometry (cont'd)

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	5 of 63
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Tower Elevation	Secondary Horizontal Type	Secondary Horizontal Size	Secondary Horizontal Grade	Inner Bracing Type	Inner Bracing Size	Inner Bracing Grade
<i>ft</i>						
T1 180.00-170.00	Single Angle	L2x2x3/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T7 140.00-130.00	Equal Angle	L2x2x1/4	A36 (36 ksi)	Single Angle	L2x2x3/16	A36 (36 ksi)
T8 130.00-120.00	Single Angle	L2x2x1/4	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T9 120.00-110.00	Single Angle	L2x2x3/16	A36 (36 ksi)	Single Angle	L2 1/2x2x3/16	A36 (36 ksi)
T10 110.00-100.00	Single Angle	L2x2x1/4	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T11 100.00-90.00	Single Angle		A36 (36 ksi)	Single Angle	L2 1/2x2x3/16	A36 (36 ksi)
T12 90.00-80.00	Single Angle	L2 1/2x2 1/2x1/4	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T13 80.00-60.00	Equal Angle		A36 (36 ksi)	Double Angle	2L2x2x3/16	A36 (36 ksi)
T14 60.00-50.00	Single Angle		A36 (36 ksi)	Double Angle	2L2x2x3/16	A36 (36 ksi)
T15 50.00-40.00	Single Angle	L3 1/2x3 1/2x1/4	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T16 40.00-30.00	Single Angle	L3 1/2x3 1/2x1/4	A36 (36 ksi)	Double Angle	2L2x2x3/16	A36 (36 ksi)
T17 30.00-20.00	Single Angle	L3 1/2x3 1/2x1/4	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T18 20.00-10.00	Single Angle	L3 1/2x3 1/2x1/4	A36 (36 ksi)	Double Angle	2L2x2 1/2x3/16	A36 (36 ksi)
T19 10.00-0.00	Single Angle		A36 (36 ksi)	Double Angle	2L2x2 1/2x3/16	A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation	Redundant Bracing Grade	Redundant Type	Redundant Size	K Factor
<i>ft</i>				
T19 10.00-0.00	A36 (36 ksi)	Horizontal (1) Diagonal (1) Sub-Horizontal Hip (1)	Single Angle Single Angle L3x3x5/16 L2 1/2x2 1/2x3/16	1 1 1 1

### Tower Section Geometry (cont'd)

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_f$	Adjust. Factor $A_e$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals
<i>ft</i>	<i>ft<sup>2</sup></i>	<i>in</i>					<i>in</i>	<i>in</i>
T1 180.00-170.00	0.00	0.0000	A36 (36 ksi)	1	1	1.02	24.0000	24.0000
T2 170.00-163.57	0.00	0.0000	A36 (36 ksi)	1	1	1.02	24.0000	24.0000







<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 9 of 63
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Tower Elevation <i>ft</i>	Connection Offsets							
	Diagonal				K-Bracing			
	Vert. Top	Horiz. Top	Vert. Bot.	Horiz. Bot.	Vert. Top	Horiz. Top	Vert. Bot.	Horiz. Bot.
	in	in	in	in	in	in	in	in
T11	0.0000	3.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000
100.00-90.00								
T12	0.0000	3.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000
90.00-80.00								
T13	0.0000	3.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000
80.00-60.00								
T14	0.0000	3.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000
60.00-50.00								
T15	0.0000	3.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000
50.00-40.00								
T16	0.0000	3.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000
40.00-30.00								
T17	0.0000	3.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000
30.00-20.00								
T18	0.0000	3.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000
20.00-10.00								
T19 10.00-0.00	0.0000	3.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000

### Tower Section Geometry (cont'd)

Tower Elevation <i>ft</i>	Leg Connection Type	Leg Bolt Size <i>in</i>	Leg No.	Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
				Bolt Size <i>in</i>	No.	Bolt Size <i>in</i>	No.	Bolt Size <i>in</i>	No.	Bolt Size <i>in</i>	No.	Bolt Size <i>in</i>	No.	Bolt Size <i>in</i>	No.
T1	Flange	0.7500	0	0.6250	2	0.6250	2	0.6250	0	0.6250	2	0.6250	0	0.6250	2
180.00-170.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T2	Flange	0.7500	0	0.6250	2	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0
170.00-163.57		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T3	Flange	0.7500	0	0.6250	2	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0
163.57-159.05		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T4	Flange	0.7500	0	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
159.05-154.52		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T5	Flange	0.7500	0	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
154.52-150.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T6	Flange	0.7500	0	0.6250	2	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0
150.00-140.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T7	Flange	0.7500	0	0.6250	2	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0
140.00-130.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T8	Flange	0.7500	0	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	2
130.00-120.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T9	Flange	0.7500	0	0.6250	2	0.6250	0	0.6250	0	0.6250	2	0.6250	2	0.6250	2
120.00-110.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T10	Flange	0.7500	0	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	2
110.00-100.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T11	Flange	0.7500	0	0.6250	2	0.6250	0	0.6250	0	0.6250	2	0.6250	2	0.6250	0
100.00-90.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T12	Flange	0.7500	0	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	2
90.00-80.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	
T13	Flange	0.7500	0	0.6250	2	0.6250	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0
80.00-60.00		A325X		A325X		A325X		A325N		A325X		A325X		A325X	



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Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T14 60,00-50,00	Flange	0.7500 A325X	0	0.6250 A325X	2	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325X	2	0.6250 A325X	0
T15 50,00-40,00	Flange	0.7500 A325X	0	0.6250 A325X	2	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325X	0	0.6250 A325X	0	0.6250 A325X	2
T16 40,00-30,00	Flange	0.7500 A325X	0	0.6250 A325X	2	0.6250 A325X	2	0.0000 A325N	0	0.6250 A325X	0	0.6250 A325X	0	0.6250 A325X	2
T17 30,00-20,00	Flange	0.7500 A325X	0	0.6250 A325X	2	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325X	0	0.6250 A325X	0	0.6250 A325X	2
T18 20,00-10,00	Flange	0.7500 A325X	0	0.6250 A325X	2	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325X	2	0.6250 A325X	2
T19 10,00-0,00	Flange	0.7500 A325X	0	0.6250 A325X	2	0.6250 A325X	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325X	2	0.6250 A325X	0

**Feed Line/Linear Appurtenances - Entered As Round Or Flat**

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
1 1/4 (T-Mobile)	A	Yes	Ar (CfAe)	126.00 - 6.00	0.0000	0.33	12	6	1.5500	1.5500		0.66
WEP65 (5,36,59)	D	Yes	Af (CfAe)	180.00 - 6.00	-12.0000	0.45	3	1	1.5836	1.5836	5.1284	0.53
WEP65 (35)	D	Yes	Ar (CfAe)	130.00 - 6.00	-10.0000	0.37	1	1	1.5836	1.5836		0.53
1/2 (67)	D	No	Ar (Leg)	180.00 - 6.00	0.0000	0.1	2	1	0.5800	0.5800		0.25
1/2 (66)	D	No	Ar (Leg)	160.00 - 6.00	0.0000	0.1	2	1	0.5800	0.5800		0.25
7/8 (9,29)	D	Yes	Ar (CfAe)	116.00 - 6.00	-10.0000	0.38	2	2	1.1100	1.1100		0.54
1/2 (13)	D	Yes	Ar (CfAe)	75.00 - 6.00	-10.0000	0.39	1	1	0.5800	0.5800		0.25
7/8 (26)	D	Yes	Ar (CfAe)	85.00 - 6.00	-10.0000	0.39	1	1	1.1100	1.1100		0.54
1/2 (68)	D	Yes	Ar (CfAe)	47.00 - 6.00	-10.0000	0.4	1	1	0.5800	0.5800		0.25
1/2 (56)	A	Yes	Ar (CfAe)	56.00 - 6.00	0.0000	0.49	1	1	0.5800	0.5800		0.25
1 5/8 (1,2,3,6)	D	Yes	Ar (CfAe)	180.00 - 6.00	-12.0000	0.43	4	2	1.9800	1.9800		1.04
7/8 (4,7)	D	Yes	Ar (CfAe)	180.00 - 6.00	-12.0000	0.41	2	2	1.1100	1.1100		0.54
7/8 (28,57)	D	Yes	Ar (CfAe)	150.00 - 6.00	-12.0000	0.4	2	2	1.1100	1.1100		0.54
7/8 (8,30,31,33,55)	D	Yes	Ar (CfAe)	120.00 - 6.00	-12.0000	0.39	5	5	1.1100	1.1100		0.54
1 5/8 (62)	D	Yes	Ar (CfAe)	101.00 - 6.00	-12.0000	0.4	1	1	1.9800	1.9800		1.04
7/8 (10,12,25)	D	Yes	Ar (CfAe)	170.00 - 6.00	-12.0000	0.38	3	3	1.1100	1.1100		0.54
7/8 (11,32)	D	Yes	Ar (CfAe)	100.00 - 6.00	-8.0000	0.41	2	2	1.1100	1.1100		0.54
1 5/8	D	Yes	Ar (CfAe)	160.00 - 6.00	-10.0000	0.4	3	3	1.9800	1.9800		1.04

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Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
(63,64,65) 1 5/8 (AT&T) 3" Flex Conduit w 3 Fiber & 6 DC (AT&T)	C	Yes	Ar (CfAe)	163.00 - 6.00	-8.0000	-0.45	12	6	1,9800	1,9800		1.04
RFS Hybriflex (3 Sector) (Sprint)	C	Yes	Ar (CfAe)	163.00 - 6.00	-3.0000	-0.38	1	1	3,0000	3,0000		3.00
1 5/8" Hybriflex (T-Mobile)	A	Yes	Ar (CfAe)	106.00 - 6.00	0.0000	0.43	3	3	1,0900	1,0900		0.37
ALU Fiber Optic Cable (Sprint)	A	Yes	Ar (CfAe)	126.00 - 6.00	0.0000	0.27	2	2	1,6250	1,6250		0.21
	A	Yes	Ar (CfAe)	126.00 - 6.00	0.0000	0.46	1	1	0,7000	0,7000		0.12

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight K
T1	180.00-170.00	A	0.483	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.00
		D	5.633	1.320	0.000	0.000	0.07
T2	170.00-163.57	A	0.311	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.00
		D	5.404	0.848	0.000	0.000	0.06
T3	163.57-159.05	A	0.265	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	4.900	0.000	0.000	0.000	0.06
		D	4.321	0.597	0.000	0.000	0.04
T4	159.05-154.52	A	0.437	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	5.610	0.000	0.000	0.000	0.07
		D	6.262	0.597	0.000	0.000	0.06
T5	154.52-150.00	A	0.437	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	5.610	0.000	0.000	0.000	0.07
		D	6.262	0.597	0.000	0.000	0.06
T6	150.00-140.00	A	0.967	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
		D	15.692	1.320	0.000	0.000	0.14
T7	140.00-130.00	A	0.967	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
		D	15.692	1.320	0.000	0.000	0.14
T8	130.00-120.00	A	7.592	0.000	0.000	0.000	0.05
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
		D	17.011	1.320	0.000	0.000	0.14
T9	120.00-110.00	A	12.008	0.000	0.000	0.000	0.08
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15

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Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
T10	110.00-100.00	D	22.746	1.320	0.000	0.000	0.18
		A	13.643	0.000	0.000	0.000	0.09
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
T11	100.00-90.00	D	23.651	1.320	0.000	0.000	0.18
		A	14.733	0.000	0.000	0.000	0.10
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
T12	90.00-80.00	D	26.986	1.320	0.000	0.000	0.20
		A	14.733	0.000	0.000	0.000	0.10
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
T13	80.00-60.00	D	27.449	1.320	0.000	0.000	0.20
		A	29.467	0.000	0.000	0.000	0.19
		B	0.000	0.000	0.000	0.000	0.00
		C	24.800	0.000	0.000	0.000	0.31
T14	60.00-50.00	D	56.548	2.639	0.000	0.000	0.42
		A	15.023	0.000	0.000	0.000	0.10
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
T15	50.00-40.00	D	28.395	1.320	0.000	0.000	0.21
		A	15.217	0.000	0.000	0.000	0.10
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
T16	40.00-30.00	D	28.733	1.320	0.000	0.000	0.21
		A	15.217	0.000	0.000	0.000	0.10
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
T17	30.00-20.00	D	28.878	1.320	0.000	0.000	0.21
		A	15.217	0.000	0.000	0.000	0.10
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
T18	20.00-10.00	D	28.878	1.320	0.000	0.000	0.21
		A	15.217	0.000	0.000	0.000	0.10
		B	0.000	0.000	0.000	0.000	0.00
		C	12.400	0.000	0.000	0.000	0.15
T19	10.00-0.00	D	28.878	1.320	0.000	0.000	0.21
		A	6.087	0.000	0.000	0.000	0.04
		B	0.000	0.000	0.000	0.000	0.00
		C	4.960	0.000	0.000	0.000	0.06
		D	11.551	0.528	0.000	0.00	0.08

**Feed Line/Linear Appurtenances Section Areas - With Ice**

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
T1	180.00-170.00	A	0.500	1.317	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.00
		D		9.800	1.875	0.000	0.000	0.21
T2	170.00-163.57	A	0.500	0.846	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.00
		D		9.689	1.205	0.000	0.000	0.16
T3	163.57-159.05	A	0.500	0.721	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		7.205	0.000	0.000	0.000	0.14

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Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
T4	159.05-154.52	D	0.500	7.654	0.848	0.000	0.000	0.12
		A		1.191	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		8.249	0.000	0.000	0.000	0.16
T5	154.52-150.00	D	0.500	10.787	0.848	0.000	0.000	0.16
		A		1.191	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		8.249	0.000	0.000	0.000	0.16
T6	150.00-140.00	D	0.500	10.787	0.848	0.000	0.000	0.16
		A		2.633	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T7	140.00-130.00	D	0.500	27.358	1.875	0.000	0.000	0.38
		A		2.633	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T8	130.00-120.00	D	0.500	27.358	1.875	0.000	0.000	0.38
		A		13.758	0.000	0.000	0.000	0.16
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T9	120.00-110.00	D	0.500	29.511	1.875	0.000	0.000	0.40
		A		21.175	0.000	0.000	0.000	0.27
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T10	110.00-100.00	D	0.500	40.413	1.875	0.000	0.000	0.49
		A		24.310	0.000	0.000	0.000	0.29
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T11	100.00-90.00	D	0.500	42.068	1.875	0.000	0.000	0.51
		A		26.400	0.000	0.000	0.000	0.31
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T12	90.00-80.00	D	0.500	47.820	1.875	0.000	0.000	0.56
		A		26.400	0.000	0.000	0.000	0.31
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T13	80.00-60.00	D	0.500	48.699	1.875	0.000	0.000	0.57
		A		52.800	0.000	0.000	0.000	0.62
		B		0.000	0.000	0.000	0.000	0.00
		C		36.467	0.000	0.000	0.000	0.72
T14	60.00-50.00	D	0.500	101.131	3.750	0.000	0.000	1.16
		A		27.190	0.000	0.000	0.000	0.31
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T15	50.00-40.00	D	0.500	50.895	1.875	0.000	0.000	0.58
		A		27.717	0.000	0.000	0.000	0.32
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T16	40.00-30.00	D	0.500	51.816	1.875	0.000	0.000	0.59
		A		27.717	0.000	0.000	0.000	0.32
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T17	30.00-20.00	D	0.500	52.211	1.875	0.000	0.000	0.59
		A		27.717	0.000	0.000	0.000	0.32
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
T18	20.00-10.00	D	0.500	52.211	1.875	0.000	0.000	0.59
		A		27.717	0.000	0.000	0.000	0.32
		B		0.000	0.000	0.000	0.000	0.00
		C		18.233	0.000	0.000	0.000	0.36
		D		52.211	1.875	0.000	0.000	0.59

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	14 of 63
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Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
T19	10.00-0.00	A	0.500	11.087	0.000	0.000	0.000	0.13
		B		0.000	0.000	0.000	0.000	0.00
		C		7.293	0.000	0.000	0.000	0.14
		D		20.885	0.750	0.000	0.000	0.24

### Feed Line Shielding

Section	Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_R$ Ice ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$A_F$ Ice ft <sup>2</sup>
T1	180.00-170.00	A	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000
		C	0.000	0.000	0.000	0.000
		D	0.000	0.522	0.740	1.216
T2	170.00-163.57	A	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000
		C	0.000	0.000	0.000	0.000
		D	0.000	0.521	0.719	1.237
T3	163.57-159.05	A	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000
		C	0.000	0.462	0.628	0.924
		D	0.000	0.507	0.597	1.014
T4	159.05-154.52	A	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000
		C	0.000	0.370	0.630	0.926
		D	0.000	0.475	0.721	1.187
T5	154.52-150.00	A	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000
		C	0.000	0.365	0.620	0.912
		D	0.000	0.467	0.710	1.168
T6	150.00-140.00	A	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000
		C	0.000	0.888	1.509	2.219
		D	0.000	1.309	1.953	3.271
T7	140.00-130.00	A	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000
		C	0.000	0.788	1.453	2.137
		D	0.000	1.162	1.880	3.150
T8	130.00-120.00	A	0.000	0.374	0.613	1.029
		B	0.000	0.000	0.000	0.000
		C	0.000	0.613	1.147	1.686
		D	0.000	0.976	1.606	2.685
T9	120.00-110.00	A	0.000	0.758	1.216	2.042
		B	0.000	0.000	0.000	0.000
		C	0.000	0.745	1.366	2.008
		D	0.000	1.632	2.544	4.398
T10	110.00-100.00	A	0.000	0.686	1.247	2.132
		B	0.000	0.000	0.000	0.000
		C	0.000	0.577	1.219	1.793
		D	0.000	1.317	2.360	4.089
T11	100.00-90.00	A	0.000	0.735	1.376	2.375
		B	0.000	0.000	0.000	0.000
		C	0.000	0.564	1.239	1.822
		D	0.000	1.464	2.732	4.730
T12	90.00-80.00	A	0.000	0.720	1.346	2.323
		B	0.000	0.000	0.000	0.000
		C	0.000	0.553	1.212	1.782

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 15 of 63
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	<b>Client</b> Sprint	<b>Designed by</b> MCD

Section	Elevation	Face	$A_R$	$A_{R_{Ice}}$	$A_F$	$A_{F_{Ice}}$
	ft		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>
T13	80.00-60.00	D	0.000	1.461	2.717	4.713
		A	0.000	1.206	1.747	3.016
		B	0.000	0.000	0.000	0.000
		C	0.000	0.925	1.573	2.314
T14	60.00-50.00	D	0.000	2.542	3.633	6.356
		A	0.000	0.710	0.958	1.673
		B	0.000	0.000	0.000	0.000
		C	0.000	0.527	0.845	1.242
T15	50.00-40.00	D	0.000	1.458	1.959	3.435
		A	0.000	0.717	1.137	2.001
		B	0.000	0.000	0.000	0.000
		C	0.000	0.521	0.989	1.455
T16	40.00-30.00	D	0.000	1.467	2.320	4.095
		A	0.000	0.918	1.364	2.400
		B	0.000	0.000	0.000	0.000
		C	0.000	0.667	1.186	1.745
T17	30.00-20.00	D	0.000	1.894	2.797	4.950
		A	0.000	0.703	1.117	1.965
		B	0.000	0.000	0.000	0.000
		C	0.000	0.511	0.972	1.429
T18	20.00-10.00	D	0.000	1.449	2.290	4.053
		A	0.000	0.906	1.346	2.369
		B	0.000	0.000	0.000	0.000
		C	0.000	0.658	1.171	1.722
T19	10.00-0.00	D	0.000	1.868	2.760	4.885
		A	0.000	0.425	0.604	1.064
		B	0.000	0.000	0.000	0.000
		C	0.000	0.309	0.526	0.773
		D	0.000	0.878	1.240	2.194

### Feed Line Center of Pressure

Section	Elevation	$CP_x$	$CP_z$	$CP_x$	$CP_z$
	ft	in	in	Ice in	Ice in
T1	180.00-170.00	-3.3826	2.7685	-3.8531	3.1934
T2	170.00-163.57	-3.6578	3.0306	-4.4392	3.7152
T3	163.57-159.05	-0.0465	-0.7044	-0.6833	-0.1357
T4	159.05-154.52	-0.8855	0.0638	-1.7348	0.8176
T5	154.52-150.00	-0.8792	0.1478	-1.7609	0.9417
T6	150.00-140.00	-1.4265	0.8104	-2.4720	1.7730
T7	140.00-130.00	-1.3634	0.9668	-2.4818	2.0106
T8	130.00-120.00	-4.9685	-0.2959	-6.7865	0.5263
T9	120.00-110.00	-8.1539	0.5717	-10.4982	1.7164
T10	110.00-100.00	-9.7412	0.4492	-12.7005	1.5964
T11	100.00-90.00	-10.4376	1.2946	-13.8446	2.5397
T12	90.00-80.00	-11.0751	1.6543	-14.6978	3.0477
T13	80.00-60.00	-13.4332	2.5084	-17.6794	4.3543
T14	60.00-50.00	-14.1222	2.6899	-18.5584	4.5244
T15	50.00-40.00	-14.0874	2.8092	-18.8530	4.7382
T16	40.00-30.00	-13.9195	2.9324	-18.3797	4.8481
T17	30.00-20.00	-15.4507	3.3467	-20.6102	5.5396
T18	20.00-10.00	-14.7660	3.2923	-19.5210	5.3704
T19	10.00-0.00	-7.1714	1.6290	-9.8467	2.7506

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	16 of 63
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## Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz	Lateral					
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
6' Standoff (CSP)	B	From Leg	3.00	0.0000	180.00	No Ice	4.97	4.97	0.07
			0.00			1/2" Ice	6.12	6.12	0.13
			0.00						
OGT9-806 (CSP - 1)	B	From Leg	6.00	0.0000	180.00	No Ice	2.15	2.15	0.02
			0.00			1/2" Ice	3.25	3.25	0.03
			0.00						
3" Dia x 15' Omni (CSP - 2)	D	From Leg	6.00	0.0000	180.00	No Ice	4.50	4.50	0.04
			0.00			1/2" Ice	6.00	6.00	0.07
			6.00						
6' Standoff (CSP)	D	From Leg	3.00	0.0000	180.00	No Ice	4.97	4.97	0.07
			0.00			1/2" Ice	6.12	6.12	0.13
			0.00						
OGT9-806 (CSP - 6)	B	From Leg	6.00	0.0000	180.00	No Ice	2.15	2.15	0.02
			0.00			1/2" Ice	3.25	3.25	0.03
			0.00						
3" Dia x 15' Omni (CSP - 3)	D	From Leg	6.00	0.0000	180.00	No Ice	4.50	4.50	0.04
			0.00			1/2" Ice	6.00	6.00	0.07
			6.00						
6' Standoff (CSP)	C	From Leg	3.00	0.0000	180.00	No Ice	4.97	4.97	0.07
			0.00			1/2" Ice	6.12	6.12	0.13
			0.00						
7' Whip (CSP - 4)	C	From Leg	3.00	0.0000	180.00	No Ice	1.74	1.74	0.04
			0.00			1/2" Ice	2.60	2.60	0.05
			0.00						
10'6"x4" Pipe Mount (CSP)	A	From Leg	0.50	0.0000	180.00	No Ice	4.72	4.72	0.11
			0.00			1/2" Ice	5.62	5.62	0.15
			0.00						
10' Dipole (CSP - 7)	A	From Leg	6.00	0.0000	180.00	No Ice	4.00	4.00	0.05
			0.00			1/2" Ice	6.00	6.00	0.07
			0.00						
TMA (CSP - 67)	C	From Leg	2.00	0.0000	180.00	No Ice	1.06	0.45	0.02
			0.00			1/2" Ice	1.21	0.57	0.03
			0.00						
10'6"x4" Pipe Mount (CSP)	A	From Leg	0.50	0.0000	176.00	No Ice	4.72	4.72	0.11
			0.00			1/2" Ice	5.62	5.62	0.15
			0.00						
10'6"x4" Pipe Mount (CSP)	B	From Leg	0.50	0.0000	176.00	No Ice	4.72	4.72	0.11
			0.00			1/2" Ice	5.62	5.62	0.15
			0.00						
10'6"x4" Pipe Mount (CSP)	C	From Leg	0.50	0.0000	176.00	No Ice	4.72	4.72	0.11
			0.00			1/2" Ice	5.62	5.62	0.15
			0.00						
10'6"x4" Pipe Mount (CSP)	D	From Leg	0.50	0.0000	176.00	No Ice	4.72	4.72	0.11
			0.00			1/2" Ice	5.62	5.62	0.15
			0.00						
6' Standoff (CSP)	D	From Leg	3.00	0.0000	172.00	No Ice	4.97	4.97	0.07
			0.00			1/2" Ice	6.12	6.12	0.13
			0.00						
6' Standoff (CSP)	C	From Leg	3.00	0.0000	172.00	No Ice	4.97	4.97	0.07
			0.00			1/2" Ice	6.12	6.12	0.13
			0.00						
20' 8 Bay Di-Pole	B	From Leg	6.00	0.0000	170.00	No Ice	4.00	4.00	0.06

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	<b>Client</b> Sprint	<b>Designed by</b> MCD

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz	Lateral					
(FCP - 12)			0.00			1/2" Ice	6.00	6.00	0.10
4' Omni (CSP - 10)	C	From Leg	0.00		0.0000	170.00	No Ice	0.53	0.03
			0.00				1/2" Ice	0.80	0.10
4' Omni (CAP - 25)	D	From Leg	0.50		0.0000	169.00	No Ice	0.53	0.03
			0.00				1/2" Ice	0.80	0.10
T-Frame (AT&T)	A	From Leg	0.50		0.0000	163.00	No Ice	10.20	0.40
			0.00				1/2" Ice	16.20	0.60
T-Frame (AT&T)	B	From Leg	0.50		0.0000	163.00	No Ice	10.20	0.40
			0.00				1/2" Ice	16.20	0.60
T-Frame (AT&T)	C	From Leg	0.50		0.0000	163.00	No Ice	10.20	0.40
			0.00				1/2" Ice	16.20	0.60
7770 (AT&T)	A	From Face	2.00		0.0000	163.00	No Ice	10.03	0.02
			4.00				1/2" Ice	10.61	0.07
(2) LGP 219nn (AT&T)	A	From Face	2.00		0.0000	163.00	No Ice	0.23	0.01
			4.00				1/2" Ice	0.30	0.01
(2) LPG21401 TMA (AT&T)	A	From Face	2.00		0.0000	163.00	No Ice	0.95	0.02
			4.00				1/2" Ice	1.09	0.02
7770 (AT&T)	A	From Face	0.50		0.0000	163.00	No Ice	10.03	0.02
			-4.00				1/2" Ice	10.61	0.07
(2) LGP 219nn (AT&T)	A	From Face	0.50		0.0000	163.00	No Ice	0.23	0.01
			-4.00				1/2" Ice	0.30	0.01
TT19-08BP111-001 TMA (AT&T)	A	From Face	0.50		0.0000	163.00	No Ice	0.64	0.02
			-4.00				1/2" Ice	0.76	0.02
P65-16-XLH-RR (AT&T)	A	From Face	1.50		0.0000	163.00	No Ice	8.40	0.06
			0.00				1/2" Ice	8.95	0.11
(2) RRU (AT&T)	A	From Leg	1.50		0.0000	163.00	No Ice	3.79	0.06
			0.00				1/2" Ice	4.16	0.08
Raycap DC6-48-60-18-8F DC Power Surge Protection (AT&T)	A	From Leg	0.50		0.0000	163.00	No Ice	1.27	0.05
			0.00				1/2" Ice	1.46	0.07
7770 (AT&T)	B	From Face	0.50		0.0000	163.00	No Ice	10.03	0.02
			4.00				1/2" Ice	10.61	0.07
(2) LGP 219nn (AT&T)	B	From Face	0.50		0.0000	163.00	No Ice	0.23	0.01
			4.00				1/2" Ice	0.30	0.01
(2) LPG21401 TMA (AT&T)	B	From Face	0.50		0.0000	163.00	No Ice	0.95	0.02
			4.00				1/2" Ice	1.09	0.02
7770 (AT&T)	B	From Face	0.50		0.0000	163.00	No Ice	10.03	0.02
			-4.00				1/2" Ice	10.61	0.07
(2) LGP 219nn	B	From Face	0.50		0.0000	163.00	No Ice	0.23	0.01



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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz	Vert					
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
(AT&T)			-4.00			1/2" Ice	0.30	0.17	0.01
			0.00						
TT19-08BP111-001 TMA	B	From Face	0.50		0.0000	163.00	No Ice	0.64	0.02
(AT&T)			-4.00			1/2" Ice	0.76	0.62	0.02
			0.00						
P65-16-XLH-RR	B	From Face	0.50		0.0000	163.00	No Ice	8.40	0.06
(AT&T)			0.00			1/2" Ice	8.95	5.15	0.11
			0.00						
(2) RRU	B	From Leg	0.50		0.0000	163.00	No Ice	3.79	0.06
(AT&T)			0.00			1/2" Ice	4.16	1.23	0.08
			0.00						
7770	C	From Face	0.50		0.0000	163.00	No Ice	10.03	0.02
(AT&T)			4.00			1/2" Ice	10.61	6.15	0.07
			0.00						
(2) LGP 219nn	C	From Face	0.50		0.0000	163.00	No Ice	0.23	0.01
(AT&T)			4.00			1/2" Ice	0.30	0.17	0.01
			0.00						
(2) LPG21401 TMA	C	From Face	0.50		0.0000	163.00	No Ice	0.95	0.02
(AT&T)			4.00			1/2" Ice	1.09	0.48	0.02
			0.00						
7770	C	From Face	4.00		0.0000	163.00	No Ice	10.03	0.02
(AT&T)			-4.00			1/2" Ice	10.61	6.15	0.07
			0.00						
(2) LGP 219nn	C	From Face	4.00		0.0000	163.00	No Ice	0.23	0.01
(AT&T)			-4.00			1/2" Ice	0.30	0.17	0.01
			0.00						
TT19-08BP111-001 TMA	C	From Face	4.00		0.0000	163.00	No Ice	0.64	0.02
(AT&T)			-4.00			1/2" Ice	0.76	0.62	0.02
			0.00						
P65-16-XLH-RR	C	From Face	2.00		0.0000	163.00	No Ice	8.40	0.06
(AT&T)			0.00			1/2" Ice	8.95	5.15	0.11
			0.00						
(2) RRU	C	From Leg	2.00		0.0000	163.00	No Ice	3.79	0.06
(AT&T)			0.00			1/2" Ice	4.16	1.23	0.08
			0.00						
3" Dia x 15' Omni	C	From Leg	2.00		0.0000	160.00	No Ice	4.50	0.04
(CSP - 63)			0.00			1/2" Ice	6.00	6.00	0.07
			0.00						
3" Dia x 15' Omni	C	From Leg	2.00		0.0000	160.00	No Ice	4.50	0.04
(CSP - 64)			0.00			1/2" Ice	6.00	6.00	0.07
			0.00						
3" Dia x 15' Omni	C	From Leg	2.00		0.0000	160.00	No Ice	4.50	0.04
(CSP - 65)			0.00			1/2" Ice	6.00	6.00	0.07
			0.00						
TMA	C	From Leg	2.00		0.0000	160.00	No Ice	1.06	0.02
(CSP - 66)			0.00			1/2" Ice	1.21	0.57	0.03
			0.00						
2" Dia 10' Omni	D	From Leg	6.00		0.0000	150.00	No Ice	2.00	0.03
(CSP)			0.00			1/2" Ice	3.02	3.02	0.04
			0.00						
DB636-A	D	From Leg	6.00		0.0000	150.00	No Ice	2.78	0.03
(NEU - 57)			0.00			1/2" Ice	3.96	3.96	0.05
			0.00						
6' Standoff	A	From Leg	3.00		0.0000	145.00	No Ice	4.97	0.07
(CSP)			0.00			1/2" Ice	6.12	6.12	0.13
			0.00						
3' Yagi	A	From Leg	6.00		0.0000	145.00	No Ice	2.08	0.03

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	19 of 63
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	<b>Client</b>	Sprint	<b>Designed by</b>	MCD

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz	Lateral					
			ft	ft					
(WTR - 28)			0.00			1/2" Ice	3.79	3.79	0.05
6' Standoff (CSP)	C	From Leg	0.00		0.0000	No Ice	4.97	4.97	0.07
			0.00			1/2" Ice	6.12	6.12	0.13
6' Standoff (CSP)	D	From Leg	0.00		0.0000	No Ice	4.97	4.97	0.07
			0.00			1/2" Ice	6.12	6.12	0.13
6' Standoff (CSP)	A	From Leg	0.00		0.0000	No Ice	4.97	4.97	0.07
			0.00			1/2" Ice	6.12	6.12	0.13
10'6"x4" Pipe Mount (CSP)	A	From Leg	0.50		0.0000	No Ice	4.72	4.72	0.11
			0.00			1/2" Ice	5.62	5.62	0.15
3' Stand-off (CSP)	C	From Leg	0.00		0.0000	No Ice	1.00	2.00	0.05
			0.00			1/2" Ice	1.20	2.70	0.07
LeBlanc 10' Standoff (1) (CSP)	C	From Leg	0.00		0.0000	No Ice	17.00	17.00	0.55
			0.00			1/2" Ice	22.00	22.00	0.75
3" Dia x 15' Omni (WPD - 55)	D	From Leg	0.00		0.0000	No Ice	4.50	4.50	0.04
			0.00			1/2" Ice	6.00	6.00	0.07
PD128-1 (CSP - 8)	C	From Leg	0.00		0.0000	No Ice	1.00	1.00	0.01
			0.00			1/2" Ice	1.80	1.80	0.02
PD128-1 (WPD - 33)	D	From Leg	0.00		0.0000	No Ice	1.00	1.00	0.01
			0.00			1/2" Ice	1.80	1.80	0.02
(2) DB586-Y (NU - 30&31)	C	From Leg	0.00		0.0000	No Ice	1.01	1.01	0.01
			0.00			1/2" Ice	1.28	1.28	0.02
Rohn 6' Side-Arm(1) (NU - 30&31)	C	From Leg	0.00		0.0000	No Ice	10.60	10.60	0.14
			0.00			1/2" Ice	15.40	15.40	0.21
ASP711 (WTR - 29)	A	From Leg	0.00		0.0000	No Ice	2.34	2.34	0.01
			0.00			1/2" Ice	3.64	3.64	0.02
6' Standoff (CSP)	D	From Leg	0.00		0.0000	No Ice	4.97	4.97	0.07
			0.00			1/2" Ice	6.12	6.12	0.13
3' Stand-off (CSP)	C	From Leg	0.00		0.0000	No Ice	1.00	2.00	0.05
			0.00			1/2" Ice	1.20	2.70	0.07
6' Stand-off (CSP)	B	From Leg	0.00		0.0000	No Ice	1.20	4.50	0.07
			0.00			1/2" Ice	1.40	5.50	0.13
10'6"x4" Pipe Mount (CSP)	C	From Leg	0.00		0.0000	No Ice	4.72	4.72	0.11
			0.00			1/2" Ice	5.62	5.62	0.15
DB222 (DHS - 9)	B	From Leg	0.00		0.0000	No Ice	1.60	1.60	0.02
			0.00			1/2" Ice	2.88	2.88	0.02
12' Wireless Frame (Sprint)	A	From Leg	0.00		0.0000	No Ice	11.07	11.07	0.24
			0.00			1/2" Ice	15.53	15.53	0.35
12' Wireless Frame	B	From Leg	0.00		0.0000	No Ice	11.07	11.07	0.24

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	20 of 63
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	<b>Client</b>	Sprint	<b>Designed by</b>	MCD

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
(Sprint)			0.00 0,00			1/2" Ice 15.53	15.53	0.35
12' Wireless Frame (Sprint)	C	From Leg	1.00 0,00	0.0000	106.00	No Ice 1/2" Ice 11.07 15.53	11.07 15.53	0.24 0.35
APXVSP18-C (Sprint)	A	From Leg	1.50 -5,00 0,00	0.0000	106,00	No Ice 1/2" Ice 8,26 8,81	5,28 5,74	0,06 0,11
APXVSP18-C (Sprint)	B	From Leg	1.50 -5,00 0,00	0.0000	106,00	No Ice 1/2" Ice 8,26 8,81	5,28 5,74	0,06 0,11
APXVSP18-C (Sprint)	C	From Leg	1.50 -5,00 0,00	0.0000	106,00	No Ice 1/2" Ice 8,26 8,81	5,28 5,74	0,06 0,11
(2) ALU RRH (Sprint)	A	From Leg	1.50 0,00 0,00	0.0000	106,00	No Ice 1/2" Ice 2,25 2,45	1,23 1,39	0,05 0,07
(2) ALU RRH (Sprint)	B	From Leg	1.50 0,00 0,00	0.0000	106,00	No Ice 1/2" Ice 2,25 2,45	1,23 1,39	0,05 0,07
(2) ALU RRH (Sprint)	C	From Leg	1.50 0,00 0,00	0.0000	106,00	No Ice 1/2" Ice 2,25 2,45	1,23 1,39	0,05 0,07
LeBlanc 10' Standoff (1) (CSP)	A	From Leg	5,00 0,00 0,00	0,0000	101,00	No Ice 1/2" Ice 17,00 22,00	17,00 22,00	0,55 0,75
SC479-HF1LDF (CSP - 62)	C	From Leg	2,00 0,00 0,00	0,0000	101,00	No Ice 1/2" Ice 5,06 6,54	5,06 6,54	0,03 0,07
3" Dia x 15' Omni (DEA - 32)	D	From Leg	6,00 0,00 0,00	0,0000	100,00	No Ice 1/2" Ice 4,50 6,00	4,50 6,00	0,04 0,07
3' Stand-off (CSP)	D	From Leg	1,50 0,00 0,00	0,0000	88,00	No Ice 1/2" Ice 1,00 1,20	2,00 2,70	0,05 0,07
3' Stand-off (CSP)	D	From Leg	1,50 0,00 0,00	0,0000	85,00	No Ice 1/2" Ice 1,00 1,20	2,00 2,70	0,05 0,07
20' 4-Bay Dipole (USS - 26)	C	From Leg	3,00 0,00 0,00	0,0000	85,00	No Ice 1/2" Ice 4,00 6,00	4,00 6,00	0,06 0,10
6' Ice Shield (CSP)	A	From Leg	4,00 0,00 0,00	0,0000	80,00	No Ice 1/2" Ice 2,60 3,00	2,60 3,00	0,13 0,15
10'6"x4" Pipe Mount (CSP)	A	From Leg	0,50 0,00 0,00	0,0000	76,00	No Ice 1/2" Ice 4,72 5,62	4,72 5,62	0,11 0,15
3' Stand-off (Sprint)	B	From Leg	1,50 0,00 0,00	0,0000	56,00	No Ice 1/2" Ice 1,00 1,20	2,00 2,70	0,05 0,07
GPS (Sprint)	B	From Leg	3,00 0,00 0,00	0,0000	56,00	No Ice 1/2" Ice 1,00 1,50	1,00 1,50	0,01 0,01
3' Stand-off (CSP)	B	From Leg	1,50 0,00 0,00	0,0000	47,00	No Ice 1/2" Ice 1,00 1,20	2,00 2,70	0,05 0,07
DB803M-Y	B	From Leg	3,00	0,0000	47,00	No Ice	0,50	0,00

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight	
			Horz	Vert						
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K	
(CSP - 68)			0.00			1/2" Ice	0.68	0.68	0.01	
EUSF10-U (T-Mobile)	A	From Leg	0.50	0.00	0.0000	122.00	No Ice	8.91	3.67	0.41
			0.00			1/2" Ice	12.66	5.24	0.51	
EUSF10-U (T-Mobile)	D	From Leg	0.50	0.00	0.0000	122.00	No Ice	8.91	3.67	0.41
			0.00			1/2" Ice	12.66	5.24	0.51	
EUSF10-U (T-Mobile)	B	From Leg	0.50	0.00	0.0000	122.00	No Ice	8.91	3.67	0.41
			0.00			1/2" Ice	12.66	5.24	0.51	
(2) AIR B2A/B4P (T-Mobile)	A	From Leg	1.00	0.00	0.0000	122.00	No Ice	6.42	4.22	0.08
			0.00			1/2" Ice	6.86	4.64	0.12	
(2) AIR B2A/B4P (T-Mobile)	B	From Leg	1.00	0.00	0.0000	122.00	No Ice	6.42	4.22	0.08
			0.00			1/2" Ice	6.86	4.64	0.12	
(2) AIR B2A/B4P (T-Mobile)	D	From Leg	1.00	0.00	0.0000	122.00	No Ice	6.42	4.22	0.08
			0.00			1/2" Ice	6.86	4.64	0.12	
(2) TMA (T-Mobile)	A	From Leg	1.00	0.00	0.0000	122.00	No Ice	1.00	1.00	0.01
			0.00			1/2" Ice	1.50	1.50	0.02	
(2) TMA (T-Mobile)	B	From Leg	1.00	0.00	0.0000	122.00	No Ice	1.00	1.00	0.01
			0.00			1/2" Ice	1.50	1.50	0.02	
(2) TMA (T-Mobile)	D	From Leg	1.00	0.00	0.0000	122.00	No Ice	1.00	1.00	0.01
			0.00			1/2" Ice	1.50	1.50	0.02	
APXVTM14-C-1 20 (Sprint)	A	From Leg	1.50	0.00	0.0000	106.00	No Ice	6.90	4.34	0.07
			0.00			1/2" Ice	7.35	4.74	0.11	
APXVTM14-C-1 20 (Sprint)	B	From Leg	1.50	0.00	0.0000	106.00	No Ice	6.90	4.34	0.07
			0.00			1/2" Ice	7.35	4.74	0.11	
APXVTM14-C-1 20 (Sprint)	C	From Leg	1.50	0.00	0.0000	106.00	No Ice	6.90	4.34	0.07
			0.00			1/2" Ice	7.35	4.74	0.11	
TD-RRH8x20-25 (Sprint)	A	From Leg	1.50	0.00	0.0000	106.00	No Ice	4.32	1.41	0.07
			0.00			1/2" Ice	4.60	1.61	0.09	
TD-RRH8x20-25 (Sprint)	B	From Leg	1.50	0.00	0.0000	106.00	No Ice	4.32	1.41	0.07
			0.00			1/2" Ice	4.60	1.61	0.09	
TD-RRH8x20-25 (Sprint)	C	From Leg	1.50	0.00	0.0000	106.00	No Ice	4.32	1.41	0.07
			0.00			1/2" Ice	4.60	1.61	0.09	
junction box (Sprint)	A	None			0.0000	106.00	No Ice	1.87	1.40	0.05
						1/2" Ice	2.05	1.57	0.06	

## Dishes

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	22 of 63
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Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight		
				Horz	Vert								
				ft	°	°	ft	ft	ft <sup>2</sup>	K			
PA6-65AC (CSP - 69)	A	Paraboloid w/o Radome	From Leg	1.00	Worst	180.00	6.00	No Ice	28.27	0.09			
				0.00							1/2" Ice	29.05	0.24
				0.00									
PA6-65AC (CSP - 70)	B	Paraboloid w/o Radome	From Leg	1.00	Worst	180.00	6.00	No Ice	28.27	0.09			
				0.00							1/2" Ice	29.05	0.24
				0.00									
PA6-65AC (CSP - 71)	C	Paraboloid w/o Radome	From Leg	1.00	Worst	180.00	6.00	No Ice	28.27	0.09			
				0.00							1/2" Ice	29.05	0.24
				0.00									
4' Grid Dish (CSP - 11)	A	Grid	From Leg	1.00	Worst	100.00	4.00	No Ice	12.57	0.08			
				0.00							1/2" Ice	13.10	0.15
				0.00									
6' Grid Dish (CSP - 13)	A	Grid	From Leg	1.00	Worst	75.00	6.00	No Ice	28.27	0.13			
				0.00							1/2" Ice	29.07	0.28
				0.00									
PA6-65AC (CSP - 5)	A	Paraboloid w/o Radome	From Leg	1.00	Worst	176.00	6.00	No Ice	28.27	0.09			
				0.00							1/2" Ice	29.05	0.24
				0.00									
PA6-65AC (CSP - 36)	C	Paraboloid w/o Radome	From Leg	1.00	Worst	176.00	6.00	No Ice	28.27	0.09			
				0.00							1/2" Ice	29.05	0.24
				0.00									
PA6-65AC (CSP - 59)	D	Paraboloid w/o Radome	From Leg	1.00	Worst	180.00	6.00	No Ice	28.27	0.09			
				0.00							1/2" Ice	29.05	0.24
				0.00									
PA6-65AC (CSP - 35)	A	Paraboloid w/o Radome	From Leg	1.00	Worst	130.00	6.00	No Ice	28.27	0.09			
				0.00							1/2" Ice	29.05	0.24
				0.00									

### Tower Pressures - No Ice

$$G_H = 1.121$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>In</sub> Face	C <sub>A</sub> A <sub>Out</sub> Face
ft	ft		psf	ft <sup>2</sup>	c	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	%	ft <sup>2</sup>	ft <sup>2</sup>
T1 180.00-170.00	175.00	1,611	33	61.674	A	12.491	0.483	5.833	44.96	0.000	0.000
					B	12.491	0.000		46.70	0.000	0.000
					C	12.491	0.000		46.70	0.000	0.000
					D	13.071	5.633		31.19	0.000	0.000
T2 170.00-163.57	166.79	1,589	33	40.022	A	9.832	0.311	5.356	52.81	0.000	0.000
					B	9.832	0.000		54.47	0.000	0.000
					C	9.832	0.000		54.47	0.000	0.000
					D	9.961	5.404		34.86	0.000	0.000
T3 163.57-159.05	161.31	1,574	33	28.908	A	7.122	0.265	3.775	51.11	0.000	0.000
					B	7.122	0.000		53.00	0.000	0.000
					C	6.494	4.900		33.13	0.000	0.000
					D	7.123	4.321		32.99	0.000	0.000
T4 159.05-154.52	156.79	1,561	32	30.376	A	6.903	0.437	3.775	51.43	0.000	0.000
					B	6.903	0.000		54.69	0.000	0.000
					C	6.273	5.610		31.77	0.000	0.000
					D	6.779	6.262		28.95	0.000	0.000
T5 154.52-150.00	152.26	1,548	32	31.844	A	7.011	0.437	3.775	50.68	0.000	0.000
					B	7.011	0.000		53.84	0.000	0.000

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	23 of 63
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	<b>Client</b>	Sprint	<b>Designed by</b>	MCD

Section Elevation	z	K <sub>z</sub>	q <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T6 150.00-140.00	145.00	1.526	32	75.634	C	6.391	5.610	8.344		0.000	0.000
					D	6.898	6.262			0.000	0.000
					A	16.767	0.967			0.000	0.000
					B	16.767	0.000			0.000	0.000
					C	15.258	12.400			0.000	0.000
T7 140.00-130.00	135.00	1.496	31	83.296	D	16.134	15.692	10.013		0.000	0.000
					A	19.051	0.967			0.000	0.000
					B	19.051	0.000			0.000	0.000
					C	17.598	12.400			0.000	0.000
					D	18.490	15.692			0.000	0.000
T8 130.00-120.00	125.00	1.463	30	90.466	A	17.265	7.592	10.013		0.000	0.000
					B	17.878	0.000			0.000	0.000
					C	16.731	12.400			0.000	0.000
					D	17.591	17.011			0.000	0.000
					A	18.812	12.008			0.000	0.000
T9 120.00-110.00	115.00	1.429	30	97.774	B	20.028	0.000	10.013		0.000	0.000
					C	18.662	12.400			0.000	0.000
					D	18.804	22.746			0.000	0.000
					A	18.510	13.643			0.000	0.000
					B	19.757	0.000			0.000	0.000
T10 110.00-100.00	105.00	1.392	29	104.945	C	18.538	12.400	10.013		0.000	0.000
					D	18.716	23.651			0.000	0.000
					A	22.496	14.733			0.000	0.000
					B	23.872	0.000			0.000	0.000
					C	22.633	12.400			0.000	0.000
T11 100.00-90.00	95.00	1.353	28	112.984	D	22.460	26.986	13.350		0.000	0.000
					A	23.020	14.733			0.000	0.000
					B	24.365	0.000			0.000	0.000
					C	23.153	12.400			0.000	0.000
					D	22.968	27.449			0.000	0.000
T12 90.00-80.00	85.00	1.31	27	120.155	A	13.769	57.836	28.370		0.000	0.000
					B	15.516	28.370			0.000	0.000
					C	13.943	53.170			0.000	0.000
					D	14.523	84.917			0.000	0.000
					A	8.092	29.208			0.000	0.000
T13 80.00-60.00	70.00	1.24	26	263.233	B	9.050	14.185	14.185		0.000	0.000
					C	8.205	26.585			0.000	0.000
					D	8.411	42.580			0.000	0.000
					A	10.055	29.402			0.000	0.000
					B	11.192	14.185			0.000	0.000
T14 60.00-50.00	55.00	1.157	24	142.444	C	10.202	26.585	14.185		0.000	0.000
					D	10.191	42.918			0.000	0.000
					A	26.004	15.217			0.000	0.000
					B	27.367	0.000			0.000	0.000
					C	26.181	12.400			0.000	0.000
T15 50.00-40.00	45.00	1.093	23	149.614	D	25.890	28.878	13.350		0.000	0.000
					A	24.350	15.217			0.000	0.000
					B	25.467	0.000			0.000	0.000
					C	24.495	12.400			0.000	0.000
					D	24.496	28.878			0.000	0.000
T16 40.00-30.00	35.00	1.017	21	156.196	A	27.188	15.217	13.350		0.000	0.000
					B	28.533	0.000			0.000	0.000
					C	27.362	12.400			0.000	0.000
					D	27.093	28.878			0.000	0.000
					A	29.084	6.087			0.000	0.000
T17 30.00-20.00	25.00	1	21	163.366	B	29.688	0.000	13.350		0.000	0.000
					C	29.162	4.960			0.000	0.000
					D	28.976	11.551			0.000	0.000
					A	27.188	15.217			0.000	0.000
					B	28.533	0.000			0.000	0.000
T18 20.00-10.00	15.00	1	21	170.539	C	27.362	12.400	13.350		0.000	0.000
					D	27.093	28.878			0.000	0.000
					A	29.084	6.087			0.000	0.000
					B	29.688	0.000			0.000	0.000
					C	29.162	4.960			0.000	0.000
T19 10.00-0.00	5.00	1	21	177.715	D	28.976	11.551	13.350		0.000	0.000

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 24 of 63
	<b>Project</b> Wilton, Connecticut (TWS-015)	<b>Date</b> 11:06:21 05/14/14
	<b>Client</b> Sprint	<b>Designed by</b> MCD

**Tower Pressure - With Ice**

$G_H = 1.121$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	t <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face
ft	ft		psf	in	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
T1 180.00-170.00	175.00	1.611	33	0.5000	62.507	A	12.491	5.837	7.500	40.92	0.000	0.000
						B	12.491	4.520	44.09	0.000	0.000	
						C	12.491	4.520	44.09	0.000	0.000	
						D	13.151	13.798	27.83	0.000	0.000	
T2 170.00-163.57	166.79	1.589	33	0.5000	40.557	A	9.832	3.803	6.427	47.14	0.000	0.000
						B	9.832	2.957	50.26	0.000	0.000	
						C	9.832	2.957	50.26	0.000	0.000	
						D	9.800	12.124	29.31	0.000	0.000	
T3 163.57-159.05	161.31	1.574	33	0.5000	29.285	A	7.122	3.150	4.530	44.10	0.000	0.000
						B	7.122	2.429	47.43	0.000	0.000	
						C	6.198	9.171	29.47	0.000	0.000	
						D	6.957	9.576	27.40	0.000	0.000	
T4 159.05-154.52	156.79	1.561	32	0.5000	30.753	A	6.903	3.197	4.530	44.85	0.000	0.000
						B	6.903	2.006	50.85	0.000	0.000	
						C	5.976	9.885	28.56	0.000	0.000	
						D	6.564	12.318	23.99	0.000	0.000	
T5 154.52-150.00	152.26	1.548	32	0.5000	32.221	A	7.011	3.241	4.530	44.19	0.000	0.000
						B	7.011	2.050	50.00	0.000	0.000	
						C	6.099	9.934	28.25	0.000	0.000	
						D	6.691	12.369	23.77	0.000	0.000	
T6 150.00-140.00	145.00	1.526	32	0.5000	76.467	A	16.767	7.671	10.013	40.97	0.000	0.000
						B	16.767	5.038	45.92	0.000	0.000	
						C	14.548	22.384	27.11	0.000	0.000	
						D	15.371	31.088	21.55	0.000	0.000	
T7 140.00-130.00	135.00	1.496	31	0.5000	84.129	A	19.051	7.625	11.682	43.79	0.000	0.000
						B	19.051	4.992	48.59	0.000	0.000	
						C	16.914	22.437	29.69	0.000	0.000	
						D	17.776	31.188	23.86	0.000	0.000	
T8 130.00-120.00	125.00	1.463	30	0.5000	91.300	A	16.849	17.904	11.682	33.61	0.000	0.000
						B	17.878	4.520	52.16	0.000	0.000	
						C	16.191	22.140	30.48	0.000	0.000	
						D	17.068	33.055	23.31	0.000	0.000	
T9 120.00-110.00	115.00	1.429	30	0.5000	98.608	A	17.986	25.793	11.682	26.68	0.000	0.000
						B	20.028	5.376	45.98	0.000	0.000	
						C	18.020	22.864	28.57	0.000	0.000	
						D	17.505	44.157	18.94	0.000	0.000	
T10 110.00-100.00	105.00	1.392	29	0.5000	105.778	A	17.625	28.422	11.682	25.37	0.000	0.000
						B	19.757	4.799	47.57	0.000	0.000	
						C	17.964	22.455	28.90	0.000	0.000	
						D	17.543	45.550	18.52	0.000	0.000	
T11 100.00-90.00	95.00	1.353	28	0.5000	113.818	A	21.497	30.579	15.019	28.84	0.000	0.000
						B	23.872	4.914	52.17	0.000	0.000	
						C	22.050	22.584	33.65	0.000	0.000	
						D	21.017	51.270	20.78	0.000	0.000	
T12 90.00-80.00	85.00	1.31	27	0.5000	120.989	A	22.043	30.757	15.019	28.45	0.000	0.000
						B	24.365	5.077	51.01	0.000	0.000	
						C	22.583	22.758	33.13	0.000	0.000	
						D	21.528	52.314	20.34	0.000	0.000	
T13 80.00-60.00	70.00	1.24	26	0.5000	264.901	A	12.500	89.507	31.707	31.08	0.000	0.000
						B	15.516	37.914	59.34	0.000	0.000	
						C	13.202	73.455	36.59	0.000	0.000	
						D	12.911	136.503	21.22	0.000	0.000	
T14 60.00-50.00	55.00	1.157	24	0.5000	143.277	A	7.377	46.165	15.854	29.61	0.000	0.000

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	25 of 63
	<b>Project</b>	Wilton, Connecticut (TWS-015)	<b>Date</b>	11:06:21 05/14/14
	<b>Client</b>	Sprint	<b>Designed by</b>	MCD

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub> psf	t <sub>z</sub> in	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
T15 50.00-40.00	45.00	1.093	23	0.5000	150.448	B	9.050	19.686		55.17	0.000	0.000
						C	7.807	37.392		35.08	0.000	0.000
						D	7.490	69.122		20.69	0.000	0.000
						A	9.191	46.871	15.854	28.28	0.000	0.000
T16 40.00-30.00	35.00	1.017	21	0.5000	157.030	B	11.192	19.871		51.04	0.000	0.000
						C	9.737	37.583		33.50	0.000	0.000
						D	8.972	70.220		20.02	0.000	0.000
						A	24.967	33.825	15.019	25.55	0.000	0.000
T17 30.00-20.00	25.00	1	21	0.5000	164.200	B	27.367	7.027		43.67	0.000	0.000
						C	25.623	24.592		29.91	0.000	0.000
						D	24.293	57.344		18.40	0.000	0.000
						A	23.501	33.021	15.019	26.57	0.000	0.000
T18 20.00-10.00	15.00	1	21	0.5000	171.373	B	25.467	6.007		47.72	0.000	0.000
						C	24.038	23.729		31.44	0.000	0.000
						D	23.289	56.769		18.76	0.000	0.000
						A	26.165	34.281	15.019	24.85	0.000	0.000
T19 10.00-0.00	5.00	1	21	0.5000	178.549	B	28.533	7.470		41.72	0.000	0.000
						C	26.811	25.045		28.96	0.000	0.000
						D	25.523	57.813		18.02	0.000	0.000
						A	28.624	18.717	15.019	31.73	0.000	0.000
						B	29.688	8.056		39.79	0.000	0.000
						C	28.915	15.040		34.17	0.000	0.000
						D	28.244	28.063		26.67	0.000	0.000

### Tower Pressure - Service

$$G_H = 1.121$$

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub> psf	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
T1 180.00-170.00	175.00	1.611	33	61.674	A	12.491	0.483	5.833	44.96	0.000	0.000
					B	12.491	0.000		46.70	0.000	0.000
					C	12.491	0.000		46.70	0.000	0.000
					D	13.071	5.633		31.19	0.000	0.000
T2 170.00-163.57	166.79	1.589	33	40.022	A	9.832	0.311	5.356	52.81	0.000	0.000
					B	9.832	0.000		54.47	0.000	0.000
					C	9.832	0.000		54.47	0.000	0.000
					D	9.961	5.404		34.86	0.000	0.000
T3 163.57-159.05	161.31	1.574	33	28.908	A	7.122	0.265	3.775	51.11	0.000	0.000
					B	7.122	0.000		53.00	0.000	0.000
					C	6.494	4.900		33.13	0.000	0.000
					D	7.123	4.321		32.99	0.000	0.000
T4 159.05-154.52	156.79	1.561	32	30.376	A	6.903	0.437	3.775	51.43	0.000	0.000
					B	6.903	0.000		54.69	0.000	0.000
					C	6.273	5.610		31.77	0.000	0.000
					D	6.779	6.262		28.95	0.000	0.000
T5 154.52-150.00	152.26	1.548	32	31.844	A	7.011	0.437	3.775	50.68	0.000	0.000
					B	7.011	0.000		53.84	0.000	0.000
					C	6.391	5.610		31.46	0.000	0.000
					D	6.898	6.262		28.68	0.000	0.000
T6 150.00-140.00	145.00	1.526	32	75.634	A	16.767	0.967	8.344	47.05	0.000	0.000
					B	16.767	0.000		49.76	0.000	0.000
					C	15.258	12.400		30.17	0.000	0.000



<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 26 of 63
	<b>Project</b> Wilton, Connecticut (TWS-015)	<b>Date</b> 11:06:21 05/14/14
	<b>Client</b> Sprint	<b>Designed by</b> MCD

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>s</sub> In Face	C <sub>A</sub> A <sub>s</sub> Out Face
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
T7 140.00-130.00	135.00	1.496	31	83.296	D	16.134	15.692	10.013	26.22	0.000	0.000
					A	19.051	0.967		50.02	0.000	0.000
					B	19.051	0.000		52.56	0.000	0.000
					C	17.598	12.400		33.38	0.000	0.000
T8 130.00-120.00	125.00	1.463	30	90.466	D	18.490	15.692	10.013	29.29	0.000	0.000
					A	17.265	7.592		40.28	0.000	0.000
					B	17.878	0.000		56.01	0.000	0.000
					C	16.731	12.400		34.37	0.000	0.000
T9 120.00-110.00	115.00	1.429	30	97.774	D	17.591	17.011	10.013	28.94	0.000	0.000
					A	18.812	12.008		32.49	0.000	0.000
					B	20.028	0.000		49.99	0.000	0.000
					C	18.662	12.400		32.23	0.000	0.000
T10 110.00-100.00	105.00	1.392	29	104.945	D	18.804	22.746	10.013	24.10	0.000	0.000
					A	18.510	13.643		31.14	0.000	0.000
					B	19.757	0.000		50.68	0.000	0.000
					C	18.538	12.400		32.36	0.000	0.000
T11 100.00-90.00	95.00	1.353	28	112.984	D	18.716	23.651	13.350	23.63	0.000	0.000
					A	22.496	14.733		35.86	0.000	0.000
					B	23.872	0.000		55.93	0.000	0.000
					C	22.633	12.400		38.11	0.000	0.000
T12 90.00-80.00	85.00	1.31	27	120.155	D	22.460	26.986	13.350	27.00	0.000	0.000
					A	23.020	14.733		35.36	0.000	0.000
					B	24.365	0.000		54.79	0.000	0.000
					C	23.153	12.400		37.55	0.000	0.000
T13 80.00-60.00	70.00	1.24	26	263.233	D	22.968	27.449	28.370	26.48	0.000	0.000
					A	13.769	57.836		39.62	0.000	0.000
					B	15.516	28.370		64.64	0.000	0.000
					C	13.943	53.170		42.27	0.000	0.000
T14 60.00-50.00	55.00	1.157	24	142.444	D	14.523	84.917	14.185	28.53	0.000	0.000
					A	8.092	29.208		38.03	0.000	0.000
					B	9.050	14.185		61.05	0.000	0.000
					C	8.205	26.585		40.77	0.000	0.000
T15 50.00-40.00	45.00	1.093	23	149.614	D	8.411	42.580	14.185	27.82	0.000	0.000
					A	10.055	29.402		35.95	0.000	0.000
					B	11.192	14.185		55.90	0.000	0.000
					C	10.202	26.585		38.56	0.000	0.000
T16 40.00-30.00	35.00	1.017	21	156.196	D	10.191	42.918	13.350	26.71	0.000	0.000
					A	26.004	15.217		32.39	0.000	0.000
					B	27.367	0.000		48.78	0.000	0.000
					C	26.181	12.400		34.60	0.000	0.000
T17 30.00-20.00	25.00	1	21	163.366	D	25.890	28.878	13.350	24.38	0.000	0.000
					A	24.350	15.217		33.74	0.000	0.000
					B	25.467	0.000		52.42	0.000	0.000
					C	24.495	12.400		36.18	0.000	0.000
T18 20.00-10.00	15.00	1	21	170.539	D	24.496	28.878	13.350	25.01	0.000	0.000
					A	27.188	15.217		31.48	0.000	0.000
					B	28.533	0.000		46.79	0.000	0.000
					C	27.362	12.400		33.58	0.000	0.000
T19 10.00-0.00	5.00	1	21	177.715	D	27.093	28.878	13.350	23.85	0.000	0.000
					A	29.084	6.087		37.96	0.000	0.000
					B	29.688	0.000		44.97	0.000	0.000
					C	29.162	4.960		39.13	0.000	0.000
					D	28.976	11.551		32.94	0.000	0.000

**Tower Forces - No Ice - Wind Normal To Face**

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	27 of 63
	<b>Project</b>	Wilton, Connecticut (TWS-015)	<b>Date</b>	11:06:21 05/14/14
	<b>Client</b>	Sprint	<b>Designed by</b>	MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K	e						ft <sup>2</sup>	K	plf	
T1 180.00-170.00	0.07	0.75	A	0.21	2.936	0.593	1	1	12.778	1.60	159.73	D
			B	0.203	2.969	0.591	1	1	12.491			
			C	0.203	2.969	0.591	1	1	12.491			
			D	0.303	2.579	0.617	1	1	16.547			
T2 170.00-163.57	0.06	0.54	A	0.253	2.762	0.603	1	1	10.019	1.15	179.59	D
			B	0.246	2.792	0.601	1	1	9.832			
			C	0.246	2.792	0.601	1	1	9.832			
			D	0.384	2.324	0.645	1	1	13.448			
T3 163.57-159.05	0.11	0.39	A	0.256	2.754	0.603	1	1	7.282	0.83	183.94	D
			B	0.246	2.789	0.601	1	1	7.122			
			C	0.394	2.296	0.649	1	1	9.675			
			D	0.396	2.291	0.65	1	1	9.931			
T4 159.05-154.52	0.13	0.36	A	0.242	2.808	0.6	1	1	7.165	0.87	193.31	D
			B	0.227	2.866	0.596	1	1	6.903			
			C	0.391	2.304	0.648	1	1	9.908			
			D	0.429	2.204	0.664	1	1	10.937			
T5 154.52-150.00	0.13	0.37	A	0.234	2.839	0.598	1	1	7.273	0.89	196.59	D
			B	0.22	2.895	0.595	1	1	7.011			
			C	0.377	2.345	0.642	1	1	9.995			
			D	0.413	2.245	0.657	1	1	11.014			
T6 150.00-140.00	0.29	0.97	A	0.234	2.837	0.598	1	1	17.345	2.09	209.20	D
			B	0.222	2.889	0.595	1	1	16.767			
			C	0.366	2.377	0.638	1	1	23.172			
			D	0.421	2.226	0.66	1	1	26.495			
T7 140.00-130.00	0.29	1.53	A	0.24	2.813	0.599	1	1	19.630	2.25	225.35	D
			B	0.229	2.86	0.597	1	1	19.051			
			C	0.36	2.394	0.636	1	1	25.486			
			D	0.41	2.252	0.656	1	1	28.782			
T8 130.00-120.00	0.35	1.43	A	0.275	2.681	0.609	1	1	21.884	2.26	226.11	D
			B	0.198	2.99	0.59	1	1	17.878			
			C	0.322	2.515	0.623	1	1	24.454			
			D	0.382	2.328	0.645	1	1	28.557			
T9 120.00-110.00	0.41	2.05	A	0.315	2.538	0.621	1	1	26.265	2.49	249.07	D
			B	0.205	2.959	0.591	1	1	20.028			
			C	0.318	2.529	0.621	1	1	26.369			
			D	0.425	2.215	0.662	1	1	33.864			
T10 110.00-100.00	0.43	1.91	A	0.306	2.568	0.618	1	1	26.940	2.51	250.90	D
			B	0.188	3.031	0.588	1	1	19.757			
			C	0.295	2.608	0.614	1	1	26.155			
			D	0.404	2.27	0.653	1	1	34.163			
T11 100.00-90.00	0.45	2.50	A	0.33	2.49	0.625	1	1	31.710	2.78	277.95	D
			B	0.211	2.932	0.593	1	1	23.872			
			C	0.31	2.555	0.619	1	1	30.309			
			D	0.438	2.184	0.668	1	1	40.478			
T12 90.00-80.00	0.45	2.43	A	0.314	2.541	0.62	1	1	32.160	2.79	278.82	D
			B	0.203	2.968	0.591	1	1	24.365			
			C	0.296	2.604	0.615	1	1	30.775			
			D	0.42	2.229	0.66	1	1	41.078			
T13 80.00-60.00	0.92	7.96	A	0.272	2.691	0.608	1	1	48.919	4.66	233.17	D
			B	0.167	3.128	0.584	1	1	32.089			
			C	0.255	2.756	0.603	1	1	46.012			
			D	0.378	2.342	0.643	1	1	69.106			
T14 60.00-50.00	0.46	4.57	A	0.262	2.729	0.605	1	1	25.762	2.29	228.96	D
			B	0.163	3.144	0.584	1	1	17.328			
			C	0.244	2.798	0.6	1	1	24.167			
			D	0.358	2.401	0.635	1	1	35.464			
T15 50.00-40.00	0.46	5.12	A	0.264	2.722	0.605	1	1	27.857	2.29	228.95	D
			B	0.17	3.114	0.585	1	1	19.485			
			C	0.246	2.791	0.601	1	1	26.175			
			D	0.355	2.41	0.634	1	1	37.412			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	28 of 63
	<b>Project</b>	Wilton, Connecticut (TWS-015)	<b>Date</b>	11:06:21 05/14/14
	<b>Client</b>	Sprint	<b>Designed by</b>	MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K	e						ft <sup>2</sup>	K	plf	
T16 40.00-30.00	0.46	4.78	A	0.264	2.722	0.606	1	1	35.218	2.53	252.92	D
			B	0.175	3.089	0.586	1	1	27.367			
			C	0.247	2.787	0.601	1	1	33.635			
			D	0.351	2.423	0.633	1	1	44.161			
T17 30.00-20.00	0.46	4.27	A	0.242	2.806	0.6	1	1	33.479	2.47	247.05	D
			B	0.156	3.177	0.582	1	1	25.467			
			C	0.226	2.872	0.596	1	1	31.886			
			D	0.327	2.499	0.624	1	1	42.529			
T18 20.00-10.00	0.46	5.02	A	0.249	2.78	0.602	1	1	36.341	2.62	261.71	D
			B	0.167	3.125	0.584	1	1	28.533			
			C	0.233	2.842	0.598	1	1	34.774			
			D	0.328	2.494	0.625	1	1	45.139			
T19 10.00-0.00	0.19	4.70	A	0.198	2.989	0.59	1	1	32.675	2.39	238.63	D
			B	0.167	3.126	0.584	1	1	29.688			
			C	0.192	3.015	0.589	1	1	32.083			
			D	0.228	2.863	0.597	1	1	35.867			
Sum Weight:	6.59	51.64					OTM	3576.82 kip-ft	41.77			

### Tower Forces - No Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K	e						ft <sup>2</sup>	K	plf	
T1 180.00-170.00	0.07	0.75	A	0.21	2.936	0.593	1.158	1.158	14.794	1.92	191.67	D
			B	0.203	2.969	0.591	1.152	1.152	14.389			
			C	0.203	2.969	0.591	1.152	1.152	14.389			
			D	0.303	2.579	0.617	1.2	1.2	19.856			
T2 170.00-163.57	0.06	0.54	A	0.253	2.762	0.603	1.19	1.19	11.923	1.39	215.51	D
			B	0.246	2.792	0.601	1.184	1.184	11.643			
			C	0.246	2.792	0.601	1.184	1.184	11.643			
			D	0.384	2.324	0.645	1.2	1.2	16.138			
T3 163.57-159.05	0.11	0.39	A	0.256	2.754	0.603	1.192	1.192	8.677	1.00	220.73	D
			B	0.246	2.789	0.601	1.185	1.185	8.438			
			C	0.394	2.296	0.649	1.2	1.2	11.610			
			D	0.396	2.291	0.65	1.2	1.2	11.917			
T4 159.05-154.52	0.13	0.36	A	0.242	2.808	0.6	1.181	1.181	8.463	1.05	231.97	D
			B	0.227	2.866	0.596	1.17	1.17	8.079			
			C	0.391	2.304	0.648	1.2	1.2	11.890			
			D	0.429	2.204	0.664	1.2	1.2	13.124			
T5 154.52-150.00	0.13	0.37	A	0.234	2.839	0.598	1.175	1.175	8.549	1.07	235.91	D
			B	0.22	2.895	0.595	1.165	1.165	8.169			
			C	0.377	2.345	0.642	1.2	1.2	11.994			
			D	0.413	2.245	0.657	1.2	1.2	13.216			
T6 150.00-140.00	0.29	0.97	A	0.234	2.837	0.598	1.176	1.176	20.395	2.51	251.04	D
			B	0.222	2.889	0.595	1.166	1.166	19.555			
			C	0.366	2.377	0.638	1.2	1.2	27.806			
			D	0.421	2.226	0.66	1.2	1.2	31.794			
T7 140.00-130.00	0.29	1.53	A	0.24	2.813	0.599	1.18	1.18	23.169	2.70	270.42	D
			B	0.229	2.86	0.597	1.172	1.172	22.319			
			C	0.36	2.394	0.636	1.2	1.2	30.583			
			D	0.41	2.252	0.656	1.2	1.2	34.539			
T8 130.00-120.00	0.35	1.43	A	0.275	2.681	0.609	1.2	1.2	26.261	2.71	271.33	D
			B	0.198	2.99	0.59	1.148	1.148	20.527			
			C	0.322	2.515	0.623	1.2	1.2	29.345			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	29 of 63
	<b>Project</b>	Wilton, Connecticut (TWS-015)	<b>Date</b>	11:06:21 05/14/14
	<b>Client</b>	Sprint	<b>Designed by</b>	MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T9 120.00-110.00	0.41	2.05	D	0.382	2.328	0.645	1.2	1.2	34.268	2.99	298.88	D
			A	0.315	2.538	0.621	1.2	1.2	31.518			
			B	0.205	2.959	0.591	1.154	1.154	23.105			
			C	0.318	2.529	0.621	1.2	1.2	31.642			
T10 110.00-100.00	0.43	1.91	D	0.425	2.215	0.662	1.2	1.2	40.637	3.01	301.07	D
			A	0.306	2.568	0.618	1.2	1.2	32.328			
			B	0.188	3.031	0.588	1.141	1.141	22.546			
			C	0.295	2.608	0.614	1.2	1.2	31.386			
T11 100.00-90.00	0.45	2.50	D	0.404	2.27	0.653	1.2	1.2	40.996	3.34	333.54	D
			A	0.33	2.49	0.625	1.2	1.2	38.052			
			B	0.211	2.932	0.593	1.158	1.158	27.655			
			C	0.31	2.555	0.619	1.2	1.2	36.371			
T12 90.00-80.00	0.45	2.43	D	0.438	2.184	0.668	1.2	1.2	48.574	3.35	334.59	D
			A	0.314	2.541	0.62	1.2	1.2	38.592			
			B	0.203	2.968	0.591	1.152	1.152	28.071			
			C	0.296	2.604	0.615	1.2	1.2	36.930			
T13 80.00-60.00	0.92	7.96	D	0.42	2.229	0.66	1.2	1.2	49.294	5.60	279.80	D
			A	0.272	2.691	0.608	1.2	1.2	58.702			
			B	0.167	3.128	0.584	1.125	1.125	36.101			
			C	0.255	2.756	0.603	1.191	1.191	54.810			
T14 60.00-50.00	0.46	4.57	D	0.378	2.342	0.643	1.2	1.2	82.927	2.75	274.75	D
			A	0.262	2.729	0.605	1.196	1.196	30.822			
			B	0.163	3.144	0.584	1.122	1.122	19.447			
			C	0.244	2.798	0.6	1.183	1.183	28.594			
T15 50.00-40.00	0.46	5.12	D	0.358	2.401	0.635	1.2	1.2	42.556	2.75	274.74	D
			A	0.264	2.722	0.605	1.198	1.198	33.366			
			B	0.17	3.114	0.585	1.127	1.127	21.964			
			C	0.246	2.791	0.601	1.184	1.184	31.002			
T16 40.00-30.00	0.46	4.78	D	0.355	2.41	0.634	1.2	1.2	44.895	3.04	303.50	D
			A	0.264	2.722	0.606	1.198	1.198	42.188			
			B	0.175	3.089	0.586	1.131	1.131	30.964			
			C	0.247	2.787	0.601	1.185	1.185	39.866			
T17 30.00-20.00	0.46	4.27	D	0.351	2.423	0.633	1.2	1.2	52.993	2.96	296.46	D
			A	0.242	2.806	0.6	1.182	1.182	39.560			
			B	0.156	3.177	0.582	1.117	1.117	28.444			
			C	0.226	2.872	0.596	1.169	1.169	37.287			
T18 20.00-10.00	0.46	5.02	D	0.327	2.499	0.624	1.2	1.2	51.034	3.14	314.05	D
			A	0.249	2.78	0.602	1.186	1.186	43.118			
			B	0.167	3.125	0.584	1.125	1.125	32.114			
			C	0.233	2.842	0.598	1.175	1.175	40.855			
T19 10.00-0.00	0.19	4.70	D	0.328	2.494	0.625	1.2	1.2	54.167	2.79	279.44	D
			A	0.198	2.989	0.59	1.148	1.148	37.524			
			B	0.167	3.126	0.584	1.125	1.125	33.408			
			C	0.192	3.015	0.589	1.144	1.144	36.702			
Sum Weight:	6.59	51.64	D	0.228	2.863	0.597	1.171	OTM	4291.84 kip-ft	50.05		

### Tower Forces - With Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 180.00-170.00	0.21	1.18	A	0.293	2.614	0.614	1	1	16.074	1.84	183.84	D
			B	0.272	2.691	0.608	1	1	15.239			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 30 of 63
	<b>Project</b> Wilton, Connecticut (TWS-015)	<b>Date</b> 11:06:21 05/14/14
	<b>Client</b> Sprint	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K	e						ft <sup>2</sup>	K	plf	
T2 170.00-163.57	0.16	0.86	C	0.272	2.691	0.608	1	1	15.239	1.35	210.60	D
			D	0.431	2.2	0.665	1	1	22.324			
			A	0.336	2.469	0.628	1	1	12.219			
			B	0.315	2.537	0.621	1	1	11.667			
			C	0.315	2.537	0.621	1	1	11.667			
T3 163.57-159.05	0.27	0.63	D	0.541	1.979	0.719	1	1	18.518	0.99	219.57	D
			A	0.351	2.423	0.633	1	1	9.115			
			B	0.326	2.501	0.624	1	1	8.638			
			C	0.525	2.005	0.71	1	1	12.714			
			D	0.565	1.944	0.733	1	1	13.971			
T4 159.05-154.52	0.32	0.56	A	0.328	2.494	0.625	1	1	8.901	1.09	241.19	D
			B	0.29	2.627	0.613	1	1	8.132			
			C	0.516	2.021	0.706	1	1	12.952			
			D	0.614	1.885	0.762	1	1	15.954			
			A	0.318	2.528	0.622	1	1	9.026			
T5 154.52-150.00	0.32	0.57	B	0.281	2.657	0.61	1	1	8.262	1.10	242.18	D
			C	0.498	2.055	0.696	1	1	13.016			
			D	0.592	1.91	0.748	1	1	15.949			
			A	0.32	2.523	0.622	1	1	21.539			
			B	0.285	2.643	0.611	1	1	19.848			
T6 150.00-140.00	0.74	1.49	C	0.483	2.084	0.689	1	1	29.969	2.61	261.39	D
			D	0.608	1.892	0.758	1	1	38.943			
			A	0.317	2.531	0.621	1	1	23.788			
			B	0.286	2.641	0.612	1	1	22.104			
			C	0.468	2.115	0.682	1	1	32.207			
T7 140.00-130.00	0.74	2.18	D	0.582	1.921	0.743	1	1	40.941	2.73	273.40	D
			A	0.381	2.334	0.644	1	1	28.377			
			B	0.245	2.793	0.601	1	1	20.592			
			C	0.42	2.228	0.66	1	1	30.801			
			D	0.549	1.967	0.724	1	1	40.990			
T8 130.00-120.00	0.92	1.98	A	0.444	2.169	0.671	1	1	35.281	2.74	274.10	D
			B	0.258	2.745	0.604	1	1	23.274			
			C	0.415	2.241	0.658	1	1	33.057			
			D	0.625	1.875	0.769	1	1	51.480			
			A	0.435	2.19	0.667	1	1	36.573			
T9 120.00-110.00	1.12	2.78	B	0.232	2.846	0.597	1	1	22.624	3.19	318.89	D
			C	0.382	2.33	0.644	1	1	32.435			
			D	0.596	1.904	0.751	1	1	51.771			
			A	0.458	2.138	0.677	1	1	42.192			
			B	0.253	2.764	0.603	1	1	26.833			
T10 110.00-100.00	1.16	2.52	C	0.392	2.301	0.648	1	1	36.694	3.57	356.68	D
			D	0.635	1.866	0.776	1	1	60.788			
			A	0.436	2.187	0.667	1	1	42.561			
			B	0.243	2.801	0.6	1	1	27.413			
			C	0.375	2.351	0.642	1	1	37.185			
T11 100.00-90.00	1.23	3.28	D	0.61	1.889	0.76	1	1	61.285	6.32	316.21	D
			A	0.385	2.321	0.646	1	1	70.289			
			B	0.202	2.973	0.591	1	1	37.914			
			C	0.327	2.498	0.625	1	1	59.081			
			D	0.564	1.945	0.732	1	1	112.865			
T12 90.00-80.00	1.23	3.15	A	0.374	2.354	0.641	1	1	36.979	3.05	304.72	D
			B	0.201	2.978	0.591	1	1	20.674			
			C	0.315	2.537	0.621	1	1	31.018			
			D	0.535	1.989	0.716	1	1	56.969			
			A	0.373	2.357	0.641	1	1	39.226			
T13 80.00-60.00	2.50	9.49	B	0.206	2.952	0.592	1	1	22.950	3.00	299.66	D
			C	0.315	2.54	0.62	1	1	33.056			
			D	0.526	2.003	0.711	1	1	58.919			
			A	0.374	2.352	0.641	1	1	46.666			
			B	0.219	2.9	0.594	1	1	31.544			
T14 60.00-50.00	1.26	5.52	C	0.315	2.537	0.621	1	1	31.018	3.09	308.84	D
			D	0.526	2.003	0.711	1	1	58.919			
			A	0.374	2.352	0.641	1	1	46.666			
			B	0.219	2.9	0.594	1	1	31.544			
			C	0.315	2.537	0.621	1	1	31.018			
T15 50.00-40.00	1.27	5.97	D	0.535	1.989	0.716	1	1	56.969	3.00	299.66	D
			A	0.373	2.357	0.641	1	1	39.226			
			B	0.206	2.952	0.592	1	1	22.950			
			C	0.315	2.54	0.62	1	1	33.056			
			D	0.526	2.003	0.711	1	1	58.919			
T16 40.00-30.00	1.27	5.99	A	0.374	2.352	0.641	1	1	46.666	3.09	308.84	D
			B	0.219	2.9	0.594	1	1	31.544			
			C	0.315	2.537	0.621	1	1	31.018			
			D	0.535	1.989	0.716	1	1	56.969			
			A	0.373	2.357	0.641	1	1	39.226			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	31 of 63
	<b>Project</b>	Wilton, Connecticut (TWS-015)	<b>Date</b>	11:06:21 05/14/14
	<b>Client</b>	Sprint	<b>Designed by</b>	MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K	e						ft <sup>2</sup>	K	plf	
T17 30.00-20.00	1.27	5.18	C	0.32	2.522	0.622	1	1	40,923	3.01	301.46	D
			D	0.52	2.014	0.708	1	1	64,883			
			A	0.344	2.443	0.63	1	1	44,319			
			B	0.192	3.016	0.589	1	1	29,003			
			C	0.291	2.622	0.613	1	1	38,588			
T18 20.00-10.00	1.27	6.32	D	0.488	2.074	0.691	1	1	62,529	3.16	315.92	D
			A	0.353	2.417	0.633	1	1	47,880			
			B	0.21	2.937	0.593	1	1	32,959			
			C	0.303	2.581	0.617	1	1	42,256			
			D	0.486	2,077	0.691	1	1	65,449			
T19 10.00-0.00	0.51	6.11	A	0.265	2.717	0.606	1	1	39,964	2.69	269.28	D
			B	0.211	2.932	0.593	1	1	34,463			
			C	0.246	2.79	0.601	1	1	37,952			
			D	0.315	2,537	0.621	1	1	45,663			
Sum Weight:	17.73	65.76						OTM	4467.74 kip-ft	52.27		

### Tower Forces - With Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K	e						ft <sup>2</sup>	K	plf	
T1 180.00-170.00	0.21	1.18	A	0.293	2.614	0.614	1.2	1.2	19,289	2.21	220.61	D
			B	0.272	2.691	0.608	1.2	1.2	18,286			
			C	0.272	2.691	0.608	1.2	1.2	18,286			
			D	0.431	2.2	0.665	1.2	1.2	26,789			
T2 170.00-163.57	0.16	0.86	A	0.336	2.469	0.628	1.2	1.2	14,662	1.62	252.72	D
			B	0.315	2.537	0.621	1.2	1.2	14,001			
			C	0.315	2.537	0.621	1.2	1.2	14,001			
			D	0.541	1,979	0.719	1.2	1.2	22,222			
T3 163.57-159.05	0.27	0.63	A	0.351	2,423	0.633	1.2	1.2	10,938	1.19	263.48	D
			B	0.326	2.501	0.624	1.2	1.2	10,366			
			C	0.525	2.005	0.71	1.2	1.2	15,257			
			D	0.565	1,944	0.733	1.2	1.2	16,766			
T4 159.05-154.52	0.32	0.56	A	0.328	2,494	0.625	1.2	1.2	10,681	1.31	289.43	D
			B	0.29	2,627	0.613	1.2	1.2	9,758			
			C	0.516	2,021	0.706	1.2	1.2	15,542			
			D	0.614	1,885	0.762	1.2	1.2	19,145			
T5 154.52-150.00	0.32	0.57	A	0.318	2,528	0.622	1.2	1.2	10,831	1.31	290.61	D
			B	0.281	2,657	0.61	1.2	1.2	9,915			
			C	0.498	2,055	0.696	1.2	1.2	15,620			
			D	0.592	1,91	0.748	1.2	1.2	19,139			
T6 150.00-140.00	0.74	1.49	A	0.32	2,523	0.622	1.2	1.2	25,847	3.14	313.67	D
			B	0.285	2,643	0.611	1.2	1.2	23,817			
			C	0.483	2,084	0.689	1.2	1.2	35,963			
			D	0.608	1,892	0.758	1.2	1.2	46,732			
T7 140.00-130.00	0.74	2.18	A	0.317	2,531	0.621	1.2	1.2	28,546	3.28	328.08	D
			B	0.286	2,641	0.612	1.2	1.2	26,525			
			C	0.468	2,115	0.682	1.2	1.2	38,648			
			D	0.582	1,921	0.743	1.2	1.2	49,130			
T8 130.00-120.00	0.92	1.98	A	0.381	2,334	0.644	1.2	1.2	34,052	3.29	328.92	D
			B	0.245	2,793	0.601	1.184	1.184	24,381			
			C	0.42	2,228	0.66	1.2	1.2	36,962			
			D	0.549	1,967	0.724	1.2	1.2	49,188			
T9	1.12	2.78	A	0.444	2,169	0.671	1.2	1.2	42,337	3.85	384.54	D

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 32 of 63
	<b>Project</b> Wilton, Connecticut (TWS-015)	<b>Date</b> 11:06:21 05/14/14
	<b>Client</b> Sprint	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
120.00-110.00			B	0.258	2.745	0.604	1.193	1.193	27.771			
			C	0.415	2.241	0.658	1.2	1.2	39.668			
			D	0.625	1.875	0.769	1.2	1.2	61.776			
T10	1.16	2.52	A	0.435	2.19	0.667	1.2	1.2	43.888	3.83	382.67	D
110.00-100.00			B	0.232	2.846	0.597	1.174	1.174	26.563			
			C	0.382	2.33	0.644	1.2	1.2	38.922			
			D	0.596	1.904	0.751	1.2	1.2	62.125			
T11	1.23	3.28	A	0.458	2.138	0.677	1.2	1.2	50.631	4.28	428.02	D
100.00-90.00			B	0.253	2.764	0.603	1.19	1.19	31.923			
			C	0.392	2.301	0.648	1.2	1.2	44.033			
			D	0.635	1.866	0.776	1.2	1.2	72.945			
T12	1.23	3.15	A	0.436	2.187	0.667	1.2	1.2	51.073	4.23	423.12	D
90.00-80.00			B	0.243	2.801	0.6	1.183	1.183	32.416			
			C	0.375	2.351	0.642	1.2	1.2	44.622			
			D	0.61	1.889	0.76	1.2	1.2	73.542			
T13	2.50	9.49	A	0.385	2.321	0.646	1.2	1.2	84.346	7.59	379.45	D
80.00-60.00			B	0.202	2.973	0.591	1.151	1.151	43.649			
			C	0.327	2.498	0.625	1.2	1.2	70.897			
			D	0.564	1.945	0.732	1.2	1.2	135.438			
T14	1.26	5.52	A	0.374	2.354	0.641	1.2	1.2	44.374	3.66	365.67	D
60.00-50.00			B	0.201	2.978	0.591	1.15	1.15	23.784			
			C	0.315	2.537	0.621	1.2	1.2	37.222			
			D	0.535	1.989	0.716	1.2	1.2	68.363			
T15	1.27	5.97	A	0.373	2.357	0.641	1.2	1.2	47.071	3.60	359.60	D
50.00-40.00			B	0.206	2.952	0.592	1.155	1.155	26.504			
			C	0.315	2.54	0.62	1.2	1.2	39.667			
			D	0.526	2.003	0.711	1.2	1.2	70.703			
T16	1.27	5.99	A	0.374	2.352	0.641	1.2	1.2	55.999	3.71	370.61	D
40.00-30.00			B	0.219	2.9	0.594	1.164	1.164	36.726			
			C	0.32	2.522	0.622	1.2	1.2	49.108			
			D	0.52	2.014	0.708	1.2	1.2	77.860			
T17	1.27	5.18	A	0.344	2.443	0.63	1.2	1.2	53.182	3.62	361.75	D
30.00-20.00			B	0.192	3.016	0.589	1.144	1.144	33.172			
			C	0.291	2.622	0.613	1.2	1.2	46.306			
			D	0.488	2.074	0.691	1.2	1.2	75.035			
T18	1.27	6.32	A	0.353	2.417	0.633	1.2	1.2	57.456	3.79	379.11	D
20.00-10.00			B	0.21	2.937	0.593	1.158	1.158	38.152			
			C	0.303	2.581	0.617	1.2	1.2	50.708			
			D	0.486	2.077	0.691	1.2	1.2	78.539			
T19	0.51	6.11	A	0.265	2.717	0.606	1.199	1.199	47.911	3.23	323.13	D
10.00-0.00			B	0.211	2.932	0.593	1.159	1.159	39.927			
			C	0.246	2.79	0.601	1.185	1.185	44.960			
			D	0.315	2.537	0.621	1.2	1.2	54.796			
Sum Weight:	17.73	65.76						OTM	5361.29	62.72		

### Tower Forces - Service - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.07	0.75	A	0.21	2.936	0.593	1	1	12.778	1.60	159.73	D
180.00-170.00			B	0.203	2.969	0.591	1	1	12.491			
			C	0.203	2.969	0.591	1	1	12.491			
			D	0.303	2.579	0.617	1	1	16.547			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 33 of 63
	<b>Project</b> Wilton, Connecticut (TWS-015)	<b>Date</b> 11:06:21 05/14/14
	<b>Client</b> Sprint	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl, Face
ft	K	K							ft <sup>2</sup>	K	plf	
T2 170.00-163.57	0.06	0.54	A	0.253	2.762	0.603	1	1	10.019	1.15	179.59	D
			B	0.246	2.792	0.601	1	1	9.832			
			C	0.246	2.792	0.601	1	1	9.832			
			D	0.384	2.324	0.645	1	1	13.448			
T3 163.57-159.05	0.11	0.39	A	0.256	2.754	0.603	1	1	7.282	0.83	183.94	D
			B	0.246	2.789	0.601	1	1	7.122			
			C	0.394	2.296	0.649	1	1	9.675			
			D	0.396	2.291	0.65	1	1	9.931			
T4 159.05-154.52	0.13	0.36	A	0.242	2.808	0.6	1	1	7.165	0.87	193.31	D
			B	0.227	2.866	0.596	1	1	6.903			
			C	0.391	2.304	0.648	1	1	9.908			
			D	0.429	2.204	0.664	1	1	10.937			
T5 154.52-150.00	0.13	0.37	A	0.234	2.839	0.598	1	1	7.273	0.89	196.59	D
			B	0.22	2.895	0.595	1	1	7.011			
			C	0.377	2.345	0.642	1	1	9.995			
			D	0.413	2.245	0.657	1	1	11.014			
T6 150.00-140.00	0.29	0.97	A	0.234	2.837	0.598	1	1	17.345	2.09	209.20	D
			B	0.222	2.889	0.595	1	1	16.767			
			C	0.366	2.377	0.638	1	1	23.172			
			D	0.421	2.226	0.66	1	1	26.495			
T7 140.00-130.00	0.29	1.53	A	0.24	2.813	0.599	1	1	19.630	2.25	225.35	D
			B	0.229	2.86	0.597	1	1	19.051			
			C	0.36	2.394	0.636	1	1	25.486			
			D	0.41	2.252	0.656	1	1	28.782			
T8 130.00-120.00	0.35	1.43	A	0.275	2.681	0.609	1	1	21.884	2.26	226.11	D
			B	0.198	2.99	0.59	1	1	17.878			
			C	0.322	2.515	0.623	1	1	24.454			
			D	0.382	2.328	0.645	1	1	28.557			
T9 120.00-110.00	0.41	2.05	A	0.315	2.538	0.621	1	1	26.265	2.49	249.07	D
			B	0.205	2.959	0.591	1	1	20.028			
			C	0.318	2.529	0.621	1	1	26.369			
			D	0.425	2.215	0.662	1	1	33.864			
T10 110.00-100.00	0.43	1.91	A	0.306	2.568	0.618	1	1	26.940	2.51	250.90	D
			B	0.188	3.031	0.588	1	1	19.757			
			C	0.295	2.608	0.614	1	1	26.155			
			D	0.404	2.27	0.653	1	1	34.163			
T11 100.00-90.00	0.45	2.50	A	0.33	2.49	0.625	1	1	31.710	2.78	277.95	D
			B	0.211	2.932	0.593	1	1	23.872			
			C	0.31	2.555	0.619	1	1	30.309			
			D	0.438	2.184	0.668	1	1	40.478			
T12 90.00-80.00	0.45	2.43	A	0.314	2.541	0.62	1	1	32.160	2.79	278.82	D
			B	0.203	2.968	0.591	1	1	24.365			
			C	0.296	2.604	0.615	1	1	30.775			
			D	0.42	2.229	0.66	1	1	41.078			
T13 80.00-60.00	0.92	7.96	A	0.272	2.691	0.608	1	1	48.919	4.66	233.17	D
			B	0.167	3.128	0.584	1	1	32.089			
			C	0.255	2.756	0.603	1	1	46.012			
			D	0.378	2.342	0.643	1	1	69.106			
T14 60.00-50.00	0.46	4.57	A	0.262	2.729	0.605	1	1	25.762	2.29	228.96	D
			B	0.163	3.144	0.584	1	1	17.328			
			C	0.244	2.798	0.6	1	1	24.167			
			D	0.358	2.401	0.635	1	1	35.464			
T15 50.00-40.00	0.46	5.12	A	0.264	2.722	0.605	1	1	27.857	2.29	228.95	D
			B	0.17	3.114	0.585	1	1	19.485			
			C	0.246	2.791	0.601	1	1	26.175			
			D	0.355	2.41	0.634	1	1	37.412			
T16 40.00-30.00	0.46	4.78	A	0.264	2.722	0.606	1	1	35.218	2.53	252.92	D
			B	0.175	3.089	0.586	1	1	27.367			
			C	0.247	2.787	0.601	1	1	33.635			
			D	0.351	2.423	0.633	1	1	44.161			



<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 34 of 63
	<b>Project</b> Wilton, Connecticut (TWS-015)	<b>Date</b> 11:06:21 05/14/14
	<b>Client</b> Sprint	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T17 30.00-20.00	0.46	4.27	A	0.242	2.806	0.6	1	1	33.479	2.47	247.05	D
			B	0.156	3.177	0.582	1	1	25.467			
			C	0.226	2.872	0.596	1	1	31.886			
			D	0.327	2.499	0.624	1	1	42.529			
T18 20.00-10.00	0.46	5.02	A	0.249	2.78	0.602	1	1	36.341	2.62	261.71	D
			B	0.167	3.125	0.584	1	1	28.533			
			C	0.233	2.842	0.598	1	1	34.774			
			D	0.328	2.494	0.625	1	1	45.139			
T19 10.00-0.00	0.19	4.70	A	0.198	2.989	0.59	1	1	32.675	2.39	238.63	D
			B	0.167	3.126	0.584	1	1	29.688			
			C	0.192	3.015	0.589	1	1	32.083			
			D	0.228	2.863	0.597	1	1	35.867			
Sum Weight:	6.59	51.64						OTM	3576.82 kip-ft	41.77		

**Tower Forces - Service - Wind 45 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 180.00-170.00	0.07	0.75	A	0.21	2.936	0.593	1.158	1.158	14.794	1.92	191.67	D
			B	0.203	2.969	0.591	1.152	1.152	14.389			
			C	0.203	2.969	0.591	1.152	1.152	14.389			
			D	0.303	2.579	0.617	1.2	1.2	19.856			
T2 170.00-163.57	0.06	0.54	A	0.253	2.762	0.603	1.19	1.19	11.923	1.39	215.51	D
			B	0.246	2.792	0.601	1.184	1.184	11.643			
			C	0.246	2.792	0.601	1.184	1.184	11.643			
			D	0.384	2.324	0.645	1.2	1.2	16.138			
T3 163.57-159.05	0.11	0.39	A	0.256	2.754	0.603	1.192	1.192	8.677	1.00	220.73	D
			B	0.246	2.789	0.601	1.185	1.185	8.438			
			C	0.394	2.296	0.649	1.2	1.2	11.610			
			D	0.396	2.291	0.65	1.2	1.2	11.917			
T4 159.05-154.52	0.13	0.36	A	0.242	2.808	0.6	1.181	1.181	8.463	1.05	231.97	D
			B	0.227	2.866	0.596	1.17	1.17	8.079			
			C	0.391	2.304	0.648	1.2	1.2	11.890			
			D	0.429	2.204	0.664	1.2	1.2	13.124			
T5 154.52-150.00	0.13	0.37	A	0.234	2.839	0.598	1.175	1.175	8.549	1.07	235.91	D
			B	0.22	2.895	0.595	1.165	1.165	8.169			
			C	0.377	2.345	0.642	1.2	1.2	11.994			
			D	0.413	2.245	0.657	1.2	1.2	13.216			
T6 150.00-140.00	0.29	0.97	A	0.234	2.837	0.598	1.176	1.176	20.395	2.51	251.04	D
			B	0.222	2.889	0.595	1.166	1.166	19.555			
			C	0.366	2.377	0.638	1.2	1.2	27.806			
			D	0.421	2.226	0.66	1.2	1.2	31.794			
T7 140.00-130.00	0.29	1.53	A	0.24	2.813	0.599	1.18	1.18	23.169	2.70	270.42	D
			B	0.229	2.86	0.597	1.172	1.172	22.319			
			C	0.36	2.394	0.636	1.2	1.2	30.583			
			D	0.41	2.252	0.656	1.2	1.2	34.539			
T8 130.00-120.00	0.35	1.43	A	0.275	2.681	0.609	1.2	1.2	26.261	2.71	271.33	D
			B	0.198	2.99	0.59	1.148	1.148	20.527			
			C	0.322	2.515	0.623	1.2	1.2	29.345			
			D	0.382	2.328	0.645	1.2	1.2	34.268			
T9 120.00-110.00	0.41	2.05	A	0.315	2.538	0.621	1.2	1.2	31.518	2.99	298.88	D
			B	0.205	2.959	0.591	1.154	1.154	23.105			
			C	0.318	2.529	0.621	1.2	1.2	31.642			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	35 of 63
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Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T10 110.00-100.00	0.43	1.91	D	0.425	2.215	0.662	1.2	1.2	40.637	3.01	301.07	D
			A	0.306	2.568	0.618	1.2	1.2	32.328			
			B	0.188	3.031	0.588	1.141	1.141	22.546			
			C	0.295	2.608	0.614	1.2	1.2	31.386			
T11 100.00-90.00	0.45	2.50	D	0.404	2.27	0.653	1.2	1.2	40.996	3.34	333.54	D
			A	0.33	2.49	0.625	1.2	1.2	38.052			
			B	0.211	2.932	0.593	1.158	1.158	27.655			
			C	0.31	2.555	0.619	1.2	1.2	36.371			
T12 90.00-80.00	0.45	2.43	D	0.438	2.184	0.668	1.2	1.2	48.574	3.35	334.59	D
			A	0.314	2.541	0.62	1.2	1.2	38.592			
			B	0.203	2.968	0.591	1.152	1.152	28.071			
			C	0.296	2.604	0.615	1.2	1.2	36.930			
T13 80.00-60.00	0.92	7.96	D	0.42	2.229	0.66	1.2	1.2	49.294	5.60	279.80	D
			A	0.272	2.691	0.608	1.2	1.2	58.702			
			B	0.167	3.128	0.584	1.125	1.125	36.101			
			C	0.255	2.756	0.603	1.191	1.191	54.810			
T14 60.00-50.00	0.46	4.57	D	0.378	2.342	0.643	1.2	1.2	82.927	2.75	274.75	D
			A	0.262	2.729	0.605	1.196	1.196	30.822			
			B	0.163	3.144	0.584	1.122	1.122	19.447			
			C	0.244	2.798	0.6	1.183	1.183	28.594			
T15 50.00-40.00	0.46	5.12	D	0.358	2.401	0.635	1.2	1.2	42.556	2.75	274.74	D
			A	0.264	2.722	0.605	1.198	1.198	33.366			
			B	0.17	3.114	0.585	1.127	1.127	21.964			
			C	0.246	2.791	0.601	1.184	1.184	31.002			
T16 40.00-30.00	0.46	4.78	D	0.355	2.41	0.634	1.2	1.2	44.895	3.04	303.50	D
			A	0.264	2.722	0.606	1.198	1.198	42.188			
			B	0.175	3.089	0.586	1.131	1.131	30.964			
			C	0.247	2.787	0.601	1.185	1.185	39.866			
T17 30.00-20.00	0.46	4.27	D	0.351	2.423	0.633	1.2	1.2	52.993	2.96	296.46	D
			A	0.242	2.806	0.6	1.182	1.182	39.560			
			B	0.156	3.177	0.582	1.117	1.117	28.444			
			C	0.226	2.872	0.596	1.169	1.169	37.287			
T18 20.00-10.00	0.46	5.02	D	0.327	2.499	0.624	1.2	1.2	51.034	3.14	314.05	D
			A	0.249	2.78	0.602	1.186	1.186	43.118			
			B	0.167	3.125	0.584	1.125	1.125	32.114			
			C	0.233	2.842	0.598	1.175	1.175	40.855			
T19 10.00-0.00	0.19	4.70	D	0.328	2.494	0.625	1.2	1.2	54.167	2.79	279.44	D
			A	0.198	2.989	0.59	1.148	1.148	37.524			
			B	0.167	3.126	0.584	1.125	1.125	33.408			
			C	0.192	3.015	0.589	1.144	1.144	36.702			
Sum Weight:	6.59	51.64										
								OTM	4291.84 kip-ft	50.05		

### Force Totals

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, M <sub>x</sub> kip-ft	Sum of Overturning Moments, M <sub>z</sub> kip-ft	Sum of Torques kip-ft
Leg Weight	30.80					
Bracing Weight	20.84					
Total Member Self-Weight	51.64					
Total Weight	68.76			-11.13	10.48	
Wind 0 deg - No Ice		-0.21	-71.45	-8070.12	35.04	-42.38
Wind 30 deg - No Ice		39.95	-68.94	-7597.36	-4398.04	-45.44

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Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, M <sub>x</sub> kip-ft	Sum of Overturning Moments, M <sub>y</sub> kip-ft	Sum of Torques kip-ft
Wind 45 deg - No Ice		56.60	-56.23	-6197.92	-6236.82	-38.98
Wind 60 deg - No Ice		69.40	-39.68	-4376.86	-7649.86	-29.88
Wind 90 deg - No Ice		71.97	0.21	13.43	-8134.08	-7.53
Wind 120 deg - No Ice		69.61	40.05	4397.15	-7674.42	18.95
Wind 135 deg - No Ice		56.90	56.53	6210.40	-6271.55	30.07
Wind 150 deg - No Ice		40.31	69.15	7599.67	-4440.58	39.13
Wind 180 deg - No Ice		0.21	71.45	8047.86	-14.09	42.38
Wind 210 deg - No Ice		-39.95	68.94	7575.10	4418.99	45.44
Wind 225 deg - No Ice		-56.60	56.23	6175.66	6257.77	38.98
Wind 240 deg - No Ice		-69.40	39.68	4354.60	7670.81	29.88
Wind 270 deg - No Ice		-71.97	-0.21	-35.69	8155.03	7.53
Wind 300 deg - No Ice		-69.61	-40.05	-4419.41	7695.37	-18.95
Wind 315 deg - No Ice		-56.90	-56.53	-6232.66	6292.51	-30.07
Wind 330 deg - No Ice		-40.31	-69.15	-7621.93	4461.54	-39.13
Member Ice	14.12					
Total Weight Ice	100.21			-14.38	37.97	
Wind 0 deg - Ice		-0.21	-88.06	-9747.26	60.97	-72.15
Wind 30 deg - Ice		49.35	-85.21	-9205.64	-5299.03	-74.88
Wind 45 deg - Ice		69.89	-69.51	-7512.14	-7521.59	-62.89
Wind 60 deg - Ice		85.68	-49.08	-5307.68	-9228.98	-46.60
Wind 90 deg - Ice		88.60	0.21	8.61	-9782.31	-8.61
Wind 120 deg - Ice		85.89	49.44	5318.74	-9251.98	36.49
Wind 135 deg - Ice		70.19	69.81	7515.89	-7554.11	54.63
Wind 150 deg - Ice		49.71	85.42	9199.87	-5338.86	69.04
Wind 180 deg - Ice		0.21	88.06	9718.49	14.98	72.15
Wind 210 deg - Ice		-49.35	85.21	9176.87	5374.97	74.88
Wind 225 deg - Ice		-69.89	69.51	7483.37	7597.53	62.89
Wind 240 deg - Ice		-85.68	49.08	5278.91	9304.92	46.60
Wind 270 deg - Ice		-88.60	-0.21	-37.38	9858.26	8.61
Wind 300 deg - Ice		-85.89	-49.44	-5347.51	9327.92	-36.49
Wind 315 deg - Ice		-70.19	-69.81	-7544.66	7630.06	-54.63
Wind 330 deg - Ice		-49.71	-85.42	-9228.64	5414.80	-69.04
Total Weight	68.76			-11.13	10.48	
Wind 0 deg - Service		-0.21	-71.45	-8067.82	25.54	-42.38
Wind 30 deg - Service		39.95	-68.94	-7595.06	-4407.54	-45.44
Wind 45 deg - Service		56.60	-56.23	-6195.62	-6246.32	-38.98
Wind 60 deg - Service		69.40	-39.68	-4374.56	-7659.36	-29.88
Wind 90 deg - Service		71.97	0.21	15.74	-8143.58	-7.53
Wind 120 deg - Service		69.61	40.05	4399.45	-7683.92	18.95
Wind 135 deg - Service		56.90	56.53	6212.70	-6281.06	30.07
Wind 150 deg - Service		40.31	69.15	7601.97	-4450.09	39.13
Wind 180 deg - Service		0.21	71.45	8050.16	-23.59	42.38
Wind 210 deg - Service		-39.95	68.94	7577.41	4409.49	45.44
Wind 225 deg - Service		-56.60	56.23	6177.97	6248.27	38.98
Wind 240 deg - Service		-69.40	39.68	4356.91	7661.31	29.88
Wind 270 deg - Service		-71.97	-0.21	-33.39	8145.53	7.53
Wind 300 deg - Service		-69.61	-40.05	-4417.10	7685.87	-18.95
Wind 315 deg - Service		-56.90	-56.53	-6230.36	6283.01	-30.07
Wind 330 deg - Service		-40.31	-69.15	-7619.62	4452.03	-39.13

### Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice

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Comb. No.	Description
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 45 deg - No Ice
5	Dead+Wind 60 deg - No Ice
6	Dead+Wind 90 deg - No Ice
7	Dead+Wind 120 deg - No Ice
8	Dead+Wind 135 deg - No Ice
9	Dead+Wind 150 deg - No Ice
10	Dead+Wind 180 deg - No Ice
11	Dead+Wind 210 deg - No Ice
12	Dead+Wind 225 deg - No Ice
13	Dead+Wind 240 deg - No Ice
14	Dead+Wind 270 deg - No Ice
15	Dead+Wind 300 deg - No Ice
16	Dead+Wind 315 deg - No Ice
17	Dead+Wind 330 deg - No Ice
18	Dead+Ice+Temp
19	Dead+Wind 0 deg+Ice+Temp
20	Dead+Wind 30 deg+Ice+Temp
21	Dead+Wind 45 deg+Ice+Temp
22	Dead+Wind 60 deg+Ice+Temp
23	Dead+Wind 90 deg+Ice+Temp
24	Dead+Wind 120 deg+Ice+Temp
25	Dead+Wind 135 deg+Ice+Temp
26	Dead+Wind 150 deg+Ice+Temp
27	Dead+Wind 180 deg+Ice+Temp
28	Dead+Wind 210 deg+Ice+Temp
29	Dead+Wind 225 deg+Ice+Temp
30	Dead+Wind 240 deg+Ice+Temp
31	Dead+Wind 270 deg+Ice+Temp
32	Dead+Wind 300 deg+Ice+Temp
33	Dead+Wind 315 deg+Ice+Temp
34	Dead+Wind 330 deg+Ice+Temp
35	Dead+Wind 0 deg - Service
36	Dead+Wind 30 deg - Service
37	Dead+Wind 45 deg - Service
38	Dead+Wind 60 deg - Service
39	Dead+Wind 90 deg - Service
40	Dead+Wind 120 deg - Service
41	Dead+Wind 135 deg - Service
42	Dead+Wind 150 deg - Service
43	Dead+Wind 180 deg - Service
44	Dead+Wind 210 deg - Service
45	Dead+Wind 225 deg - Service
46	Dead+Wind 240 deg - Service
47	Dead+Wind 270 deg - Service
48	Dead+Wind 300 deg - Service
49	Dead+Wind 315 deg - Service
50	Dead+Wind 330 deg - Service

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T1	180 - 170	Leg	Max Tension	21	6.70	-0.86	-0.83
			Max. Compression	29	-6.92	-0.99	-1.14
			Max. Mx	34	1.14	3.29	-2.58
			Max. My	24	1.15	-2.62	3.33
			Max. Vy	27	-2.81	1.25	-0.33

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft		
T2	170 - 163.573	Diagonal	Max. Vx	19	-2.81	-0.32	1.25		
			Max Tension	27	5.71	0.00	0.00		
			Max. Compression	19	-6.55	0.00	0.00		
			Max. Mx	29	4.56	0.02	-0.00		
			Max. My	17	4.23	0.01	0.00		
			Max. Vy	29	0.01	0.02	-0.00		
		Secondary Horizontal	Max. Vx	17	0.00	0.00	0.00		
			Max Tension	23	0.78	0.00	0.00		
			Max. Compression	23	-0.80	0.00	0.00		
			Max. Mx	18	0.01	-0.02	0.00		
			Max. My	26	0.39	0.00	0.00		
			Max. Vy	18	0.01	0.00	0.00		
		Top Girt	Max. Vx	26	-0.00	0.00	0.00		
			Max Tension	27	0.51	0.00	0.00		
			Max. Compression	14	-0.12	0.00	0.00		
			Max. Mx	18	0.12	-0.02	0.00		
			Max. My	34	0.03	0.00	0.00		
			Max. Vy	18	0.01	0.00	0.00		
		Leg		Max. Vx	Max. Vx	34	-0.00	0.00	0.00
					Max Tension	29	19.66	-0.68	-0.82
				Max. Compression	Max. Compression	29	-21.37	-1.00	-1.05
					Max. Mx	31	-15.04	1.44	-0.40
				Max. My	Max. My	23	-14.89	-0.40	1.44
Max. Vy	27				0.35	1.34	-0.30		
Diagonal				Max. Vx	Max. Vx	19	0.35	-0.30	1.34
					Max Tension	32	6.52	0.00	0.00
				Max. Compression	Max. Compression	24	-7.13	0.00	0.00
					Max. Mx	25	5.84	0.03	-0.00
		Max. My	Max. My	15	4.23	0.00	0.00		
			Max. Vy	25	0.01	0.03	-0.00		
Top Girt		Max. Vx	Max. Vx	15	-0.00	0.00	0.00		
			Max Tension	27	1.25	0.00	0.00		
		Max. Compression	Max. Compression	10	-0.73	0.00	0.00		
			Max. Mx	18	0.34	-0.02	0.00		
		Max. My	Max. My	28	-0.09	0.00	0.00		
			Max. Vy	18	0.01	0.00	0.00		
T3	163.573 - 159.049	Leg	Max. Vx	28	-0.00	0.00	0.00		
			Max Tension	25	32.78	-0.65	-0.65		
			Max. Compression	Max. Compression	25	-36.54	-1.05	-1.10	
				Max. Mx	31	-25.51	1.74	-0.06	
				Max. My	23	-26.00	-0.04	1.74	
		Max. Vy	Max. Vy	23	1.06	-0.69	-0.23		
			Max. Vx	31	1.08	-0.23	-0.69		
			Max Tension	31	5.69	0.00	0.00		
		Diagonal		Max. Compression	Max. Compression	31	-5.90	0.00	0.00
					Max. Mx	24	3.20	0.02	0.00
				Max. My	Max. My	19	-5.74	-0.00	-0.01
					Max. Vy	24	0.01	0.02	0.00
				Max. Vx	19	0.00	0.00	0.00	
Top Girt		Max Tension	Max Tension	27	1.52	0.00	0.00		
			Max. Compression	14	-0.90	0.00	0.00		
		Max. Mx	Max. Mx	18	0.25	-0.02	0.00		
			Max. My	28	-0.44	0.00	0.00		
		Max. Vy	18	0.01	0.00	0.00			
T4	159.049 - 154.524	Leg	Max. Vx	28	0.00	0.00	0.00		
			Max Tension	25	43.19	-0.39	-0.42		
		Max. Compression	Max. Compression	25	-48.73	-0.53	-0.51		
			Max. Mx	30	8.90	1.33	-0.96		

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
			Max. My	24	9.36	-0.96	1.33
			Max. Vy	34	-0.41	1.30	-0.95
			Max. Vx	24	-0.41	-0.96	1.33
		Diagonal	Max Tension	27	6.46	0.00	0.00
			Max. Compression	19	-6.15	0.00	0.00
			Max. Mx	24	2.68	0.04	0.00
			Max. My	27	-6.10	-0.01	0.01
			Max. Vy	24	0.02	0.04	0.00
			Max. Vx	27	-0.00	0.00	0.00
T5	154.524 - 150	Leg	Max Tension	25	52.82	-0.66	-0.61
			Max. Compression	25	-58.08	-0.91	-0.92
			Max. Mx	20	-55.82	-1.01	-0.74
			Max. My	30	-55.44	-0.74	-1.02
			Max. Vy	20	0.41	-1.01	-0.74
			Max. Vx	30	0.42	-0.74	-1.02
		Diagonal	Max Tension	31	6.02	0.00	0.00
			Max. Compression	31	-6.40	0.00	0.00
			Max. Mx	24	2.36	0.05	-0.00
			Max. My	27	-5.98	-0.01	0.01
			Max. Vy	24	-0.02	0.05	-0.00
			Max. Vx	27	-0.00	-0.01	0.01
T6	150 - 140	Leg	Max Tension	25	74.80	-0.68	-0.71
			Max. Compression	25	-81.08	-0.89	-0.79
			Max. Mx	30	14.11	1.66	-1.23
			Max. My	24	14.35	-1.24	1.67
			Max. Vy	30	-0.56	1.66	-1.23
			Max. Vx	24	-0.57	-1.24	1.67
		Diagonal	Max Tension	31	6.75	0.00	0.00
			Max. Compression	31	-6.84	0.00	0.00
			Max. Mx	24	3.07	0.07	-0.00
			Max. My	23	-6.30	-0.02	-0.01
			Max. Vy	24	-0.02	0.07	-0.00
			Max. Vx	23	0.00	0.00	0.00
		Top Girt	Max Tension	23	1.05	0.00	0.00
			Max. Compression	6	-0.91	0.00	0.00
			Max. Mx	27	1.04	-0.03	0.00
			Max. My	28	-0.38	0.00	0.00
			Max. Vy	27	0.02	0.00	0.00
			Max. Vx	28	-0.00	0.00	0.00
T7	140 - 130	Leg	Max Tension	25	89.59	-1.01	-1.02
			Max. Compression	25	-97.27	-0.22	-0.07
			Max. Mx	29	-3.77	4.88	-4.73
			Max. My	21	-5.06	-4.73	4.88
			Max. Vy	33	-1.03	4.79	-4.66
			Max. Vx	25	-1.03	-4.65	4.79
		Diagonal	Max Tension	31	8.96	0.00	0.00
			Max. Compression	24	-9.13	0.00	0.00
			Max. Mx	24	5.77	0.13	-0.00
			Max. My	23	-9.03	-0.03	-0.05
			Max. Vy	24	0.03	0.13	-0.00
			Max. Vx	23	0.01	0.00	0.00
		Secondary Horizontal	Max Tension	25	1.46	0.00	0.00
			Max. Compression	25	-1.46	0.00	0.00
			Max. Mx	27	-0.82	-0.04	0.00
			Max. My	28	0.42	0.00	0.00
			Max. Vy	27	0.02	0.00	0.00
			Max. Vx	28	0.00	0.00	0.00
		Top Girt	Max Tension	32	0.90	0.00	0.00
			Max. Compression	31	-0.92	-0.09	0.00
			Max. Mx	19	-0.90	-0.12	0.00

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	180' Lattice Tower - CSP	<b>Page</b>	40 of 63
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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T8	130 - 120	Inner Bracing	Max. My	19	-0.90	-0.12	0.01	
			Max. Vy	19	-0.04	0.00	0.00	
			Max. Vx	19	-0.00	0.00	0.00	
			Max Tension	33	0.17	0.00	0.00	
			Max. Compression	33	-0.17	0.00	0.00	
			Max. Mx	18	0.00	-0.03	0.00	
		Leg	Max. My	31	-0.00	0.00	0.00	
			Max. Vy	18	0.02	0.00	0.00	
			Max. Vx	31	-0.00	0.00	0.00	
			Max Tension	25	110.86	0.90	0.89	
			Max. Compression	25	-120.84	-1.03	-0.73	
			Max. Mx	30	-115.14	3.17	1.83	
			Max. My	20	-114.83	1.83	3.16	
			Max. Vy	20	1.33	2.20	-0.88	
			Max. Vx	30	1.34	-0.86	2.25	
			Diagonal	Max Tension	30	10.53	0.00	0.00
				Max. Compression	22	-10.76	0.00	0.00
				Max. Mx	24	3.84	0.17	-0.02
				Max. My	23	-10.10	-0.03	0.06
			Secondary Horizontal	Max. Vy	24	-0.04	0.17	-0.02
Max. Vx	23	-0.01		-0.03	0.06			
Max Tension	25	1.81		0.00	0.00			
Max. Compression	25	-1.81		0.00	0.00			
Max. Mx	27	-1.38		-0.05	0.00			
Max. My	28	0.52		0.00	0.00			
Max. Vy	27	-0.02		0.00	0.00			
Max. Vx	28	0.00		0.00	0.00			
T9	120 - 110	Leg		Max Tension	25	133.20	-1.87	-1.85
				Max. Compression	25	-146.56	-0.42	-0.40
			Max. Mx	21	-5.82	5.80	-5.61	
			Max. My	29	-7.73	-5.61	5.80	
			Max. Vy	33	-1.27	5.75	-5.56	
			Max. Vx	25	-1.27	-5.58	5.76	
		Diagonal	Max Tension	32	11.02	0.00	0.00	
			Max. Compression	24	-11.24	0.00	0.00	
			Max. Mx	24	7.19	0.12	-0.00	
			Max. My	23	-10.99	-0.02	-0.06	
		Horizontal	Max. Vy	24	0.04	0.12	-0.00	
			Max. Vx	23	0.01	0.00	0.00	
			Max Tension	23	0.97	0.00	0.00	
			Max. Compression	23	-1.16	-0.15	0.01	
			Max. Mx	27	-1.14	-0.20	0.01	
			Max. My	19	-1.12	-0.20	0.01	
			Max. Vy	27	-0.06	0.00	0.00	
			Max. Vx	19	-0.00	0.00	0.00	
Secondary Horizontal	Max Tension		25	2.20	0.00	0.00		
	Max. Compression		25	-2.20	0.00	0.00		
Inner Bracing	Max. Mx		27	-1.17	-0.05	0.00		
	Max. My		28	0.63	0.00	0.00		
	Max. Vy	27	-0.02	0.00	0.00			
	Max. Vx	28	-0.00	0.00	0.00			
	Max Tension	25	0.11	0.00	0.00			
	Max. Compression	25	-0.11	0.00	0.00			
	Max. Mx	18	0.00	-0.05	0.00			
	Max. My	31	-0.00	0.00	0.00			
	Max. Vy	18	0.02	0.00	0.00			
	Max. Vx	31	-0.00	0.00	0.00			
T10	110 - 100	Leg	Max Tension	25	157.46	-2.01	-2.30	
			Max. Compression	33	-173.77	-2.02	-1.75	

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft		
T11	100 - 90	Diagonal	Max. Mx	23	-117.68	3.77	-0.06		
			Max. My	31	-117.99	-0.01	3.66		
			Max. Vy	34	1.43	-1.18	-0.55		
			Max. Vx	24	1.45	-0.60	-1.14		
			Max Tension	26	12.31	0.00	0.00		
			Max. Compression	34	-12.55	0.00	0.00		
			Max. Mx	24	4.90	0.21	-0.01		
			Max. My	31	-12.17	-0.03	0.04		
			Max. Vy	24	-0.05	0.21	-0.01		
			Max. Vx	27	0.01	-0.03	-0.04		
			Max Tension	33	2.61	0.00	0.00		
			Max. Compression	33	-2.61	0.00	0.00		
		Secondary Horizontal	Max. Mx	27	-1.49	-0.07	0.00		
			Max. My	28	0.75	0.00	0.00		
			Max. Vy	27	0.03	0.00	0.00		
			Max. Vx	28	0.00	0.00	0.00		
			Max Tension	33	183.09	-1.79	-1.39		
			Max. Compression	33	-202.52	-0.52	-0.90		
			Leg	Max. Mx	34	38.58	6.53	-5.68	
				Max. My	24	40.91	-5.69	6.55	
				Max. Vy	34	-1.01	6.53	-5.68	
				Max. Vx	24	-1.00	-5.69	6.55	
				Max Tension	27	12.96	0.00	0.00	
				Max. Compression	27	-13.16	0.00	0.00	
		Diagonal		Max. Mx	32	7.36	0.15	0.00	
				Max. My	19	-13.07	-0.02	0.05	
				Max. Vy	32	0.04	0.15	0.00	
				Max. Vx	19	-0.01	0.00	0.00	
				Horizontal	Max Tension	23	1.55	0.00	0.00
					Max. Compression	23	-1.65	-0.21	0.01
			Max. Mx		19	-1.61	-0.29	0.01	
			Max. My		19	-1.60	-0.29	0.01	
			Max. Vy		19	-0.07	0.00	0.00	
Max. Vx	19		-0.00		0.00	0.00			
Inner Bracing	Max Tension		25	0.12	0.00	0.00			
	Max. Compression		25	-0.12	0.00	0.00			
	Max. Mx	18	0.00	-0.07	0.00				
	Max. My	31	-0.00	0.00	0.00				
	Max. Vy	18	0.03	0.00	0.00				
	Max. Vx	31	-0.00	0.00	0.00				
T12	90 - 80	Leg	Max Tension	33	209.04	-1.95	-2.17		
			Max. Compression	33	-230.26	-1.08	-1.20		
			Max. Mx	31	-155.62	3.86	-0.31		
			Max. My	23	-155.62	-0.28	3.84		
			Max. Vy	30	1.27	-2.53	-1.75		
			Max. Vx	20	1.26	-1.83	-2.44		
		Diagonal	Max Tension	27	13.70	0.00	0.00		
			Max. Compression	27	-13.97	0.00	0.00		
			Max. Mx	34	5.61	0.18	0.01		
			Max. My	19	-12.49	-0.01	0.03		
			Max. Vy	34	-0.05	0.18	0.01		
			Max. Vx	19	-0.01	-0.01	0.03		
		Secondary Horizontal	Max Tension	33	3.46	0.00	0.00		
			Max. Compression	33	-3.46	0.00	0.00		
			Max. Mx	27	-1.54	-0.11	0.00		
			Max. My	28	0.98	0.00	0.00		
			Max. Vy	27	0.04	0.00	0.00		
			Max. Vx	28	-0.00	0.00	0.00		
T13	80 - 60	Leg	Max Tension	33	260.62	0.77	0.22		



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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
			Max. Compression	33	-287.22	7.03	-0.04
			Max. Mx	33	-287.22	7.03	-0.04
			Max. My	21	-12.56	-1.27	6.85
			Max. Vy	25	-1.09	7.02	-0.41
			Max. Vx	21	-1.46	-1.27	6.85
		Diagonal	Max Tension	27	14.25	0.00	0.00
			Max. Compression	27	-14.93	0.00	0.00
			Max. Mx	34	6.15	-0.09	-0.01
			Max. My	19	-13.72	-0.03	-0.03
			Max. Vy	34	0.04	-0.09	-0.01
			Max. Vx	19	0.01	0.00	0.00
		Top Girt	Max Tension	26	1.08	0.00	0.00
			Max. Compression	30	-0.87	-0.34	0.01
			Max. Mx	27	-0.72	-0.48	0.02
			Max. My	19	-0.72	-0.48	0.02
			Max. Vy	27	-0.10	0.00	0.00
			Max. Vx	19	-0.00	0.00	0.00
		Inner Bracing	Max Tension	25	0.16	0.00	0.00
			Max. Compression	25	-0.16	0.00	0.00
			Max. Mx	18	0.00	0.14	0.00
			Max. My	31	0.00	0.00	-0.00
			Max. Vy	18	0.05	0.00	0.00
			Max. Vx	31	-0.00	0.00	0.00
T14	60 - 50	Leg	Max Tension	33	283.24	0.67	-0.43
			Max. Compression	33	-314.06	-0.34	0.51
			Max. Mx	25	279.90	-4.34	0.15
			Max. My	21	-15.56	-2.25	9.12
			Max. Vy	25	0.64	-4.34	0.15
			Max. Vx	21	-1.48	-2.25	9.12
		Diagonal	Max Tension	20	14.12	0.00	0.00
			Max. Compression	28	-14.48	0.00	0.00
			Max. Mx	32	7.66	-0.08	-0.01
			Max. My	28	-14.43	-0.03	0.03
			Max. Vy	33	-0.04	-0.08	-0.01
			Max. Vx	19	0.00	0.00	0.00
		Horizontal	Max Tension	19	2.52	0.00	0.00
			Max. Compression	14	-1.35	0.34	-0.02
			Max. Mx	19	-0.64	0.66	-0.04
			Max. My	27	-0.63	0.66	-0.04
			Max. Vy	19	0.12	0.00	0.00
			Max. Vx	27	0.01	0.00	0.00
		Inner Bracing	Max Tension	33	0.15	0.00	0.00
			Max. Compression	33	-0.15	0.00	0.00
			Max. Mx	18	0.00	0.17	0.00
			Max. My	31	0.00	0.00	-0.00
			Max. Vy	18	-0.05	0.00	0.00
			Max. Vx	31	0.00	0.00	0.00
T15	50 - 40	Leg	Max Tension	33	307.24	0.13	0.43
			Max. Compression	33	-339.75	2.16	-0.20
			Max. Mx	33	-339.22	5.92	0.07
			Max. My	33	-18.52	1.22	5.77
			Max. Vy	33	-2.20	5.92	0.07
			Max. Vx	33	-1.58	1.22	5.77
		Diagonal	Max Tension	20	14.31	0.00	0.00
			Max. Compression	28	-15.89	0.00	0.00
			Max. Mx	34	4.74	-0.16	-0.02
			Max. My	20	6.51	-0.15	-0.02
			Max. Vy	32	-0.07	-0.16	0.02
			Max. Vx	20	-0.00	0.00	0.00
		Secondary Horizontal	Max Tension	33	5.10	0.00	0.00

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T16	40 - 30	Leg	Max. Compression	33	-5.10	0.00	0.00	
			Max. Mx	27	-2.06	-0.24	0.00	
			Max. My	28	1.46	0.00	0.01	
			Max. Vy	27	0.06	0.00	0.00	
			Max. Vx	28	0.00	0.00	0.00	
			Max Tension	33	327.83	-2.83	-1.91	
			Max. Compression	33	-365.07	2.28	1.56	
			Max. Mx	20	-107.92	7.70	-5.86	
			Max. My	26	-106.61	-5.88	7.69	
			Max. Vy	20	-1.82	7.70	-5.86	
			Max. Vx	26	-1.82	-5.88	7.69	
			Diagonal	Max Tension	20	15.27	0.00	0.00
		Max. Compression		28	-16.23	0.00	0.00	
		Max. Mx		33	11.46	-0.17	-0.02	
		Max. My		22	-15.94	-0.04	-0.05	
		Max. Vy		33	-0.07	-0.17	-0.02	
		Max. Vx		22	0.01	0.00	0.00	
		Secondary Horizontal		Max Tension	33	5.48	0.00	0.00
				Max. Compression	33	-5.48	0.00	0.00
			Max. Mx	27	-2.01	-0.26	0.00	
			Max. My	28	1.58	0.00	0.01	
		Top Girt	Max. Vy	27	-0.07	0.00	0.00	
			Max. Vx	28	-0.00	0.00	0.00	
			Max Tension	34	3.04	0.00	0.00	
			Max. Compression	14	-1.25	0.43	-0.03	
			Max. Mx	19	-0.01	0.73	-0.04	
			Max. My	19	-0.01	0.73	-0.04	
			Max. Vy	19	0.13	0.00	0.00	
Max. Vx	19		0.01	0.00	0.00			
Inner Bracing	Max Tension	33	0.20	0.00	0.00			
	Max. Compression	33	-0.20	0.00	0.00			
	Max. Mx	18	0.00	0.21	0.00			
	Max. My	31	0.00	0.00	-0.00			
	Max. Vy	18	-0.06	0.00	0.00			
	Max. Vx	33	-0.00	0.00	0.00			
	T17	30 - 20	Leg	Max Tension	33	351.40	-2.57	-3.23
				Max. Compression	33	-392.79	0.22	0.39
Max. Mx				27	-259.11	6.54	0.56	
Max. My				19	-258.88	0.52	6.56	
Max. Vy				26	2.09	-3.70	-3.34	
Max. Vx				20	2.10	-3.31	-3.71	
Diagonal			Max Tension	20	14.87	0.00	0.00	
			Max. Compression	28	-14.94	0.00	0.00	
			Max. Mx	34	6.02	-0.20	-0.02	
			Max. My	20	6.88	-0.19	-0.02	
			Max. Vy	33	-0.07	-0.19	0.02	
			Max. Vx	20	-0.00	0.00	0.00	
Secondary Horizontal	Max Tension	33	5.90	0.00	0.00			
	Max. Compression	33	-5.90	0.00	0.00			
T18	20 - 10	Leg	Max. Mx	27	-2.59	-0.28	0.00	
			Max. My	28	1.71	0.00	0.01	
			Max. Vy	27	0.07	0.00	0.00	
			Max. Vx	28	0.00	0.00	0.00	
			Max Tension	33	372.69	-3.58	-2.72	
			Max. Compression	33	-411.29	0.72	0.50	
		Diagonal	Max. Mx	25	-18.91	-4.50	4.10	
			Max. My	21	-19.77	4.08	-4.48	
			Max. Vy	34	-1.40	2.47	1.79	
			Max. Vx	28	-1.40	1.77	2.47	

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T19	10 - 0	Diagonal	Max Tension	20	14.90	0.00	0.00	
			Max. Compression	22	-20.29	0.00	0.00	
			Max. Mx	33	11.25	-0.18	-0.02	
			Max. My	19	-9.71	-0.10	-0.06	
			Max. Vy	34	-0.08	-0.18	-0.02	
			Max. Vx	19	0.01	0.00	0.00	
		Horizontal	Max Tension	19	6.08	0.00	0.00	
			Max. Compression	14	-1.12	0.57	-0.03	
			Max. Mx	19	0.97	0.79	-0.05	
			Max. My	19	0.98	0.79	-0.05	
			Max. Vy	19	-0.13	0.00	0.00	
			Max. Vx	19	-0.01	0.00	0.00	
		Secondary Horizontal	Max Tension	33	6.17	0.00	0.00	
			Max. Compression	33	-6.17	0.00	0.00	
			Max. Mx	18	0.31	-0.31	0.00	
			Max. My	28	1.77	0.00	0.01	
			Max. Vy	18	-0.07	0.00	0.00	
			Max. Vx	28	-0.00	0.00	0.00	
		Inner Bracing	Max Tension	32	0.08	0.00	0.00	
			Max. Compression	32	-0.06	0.00	0.00	
			Max. Mx	18	0.00	0.29	0.00	
			Max. My	33	0.06	0.00	0.00	
			Max. Vy	18	-0.07	0.00	0.00	
			Max. Vx	33	-0.00	0.00	0.00	
		Leg	Max Tension	33	369.65	-2.08	-2.32	
			Max. Compression	33	-426.59	0.00	-0.00	
			Max. Mx	27	-282.98	4.25	-0.33	
			Max. My	19	-282.60	-0.35	4.26	
			Max. Vy	34	1.52	-3.81	-3.41	
			Max. Vx	28	1.52	-3.36	-3.83	
			Diagonal	Max Tension	20	26.83	-0.04	-0.00
				Max. Compression	28	-21.38	0.00	0.00
				Max. Mx	3	13.15	-0.06	0.03
				Max. My	34	-21.22	0.01	-0.09
				Max. Vy	20	0.03	-0.06	-0.00
				Max. Vx	34	-0.02	0.00	0.00
		Horizontal	Max Tension	28	16.90	0.00	0.00	
			Max. Compression	20	-16.66	-0.06	0.02	
			Max. Mx	31	7.51	-0.14	-0.03	
			Max. My	27	-5.17	-0.04	0.03	
			Max. Vy	31	-0.07	-0.14	-0.03	
			Max. Vx	27	-0.01	-0.04	0.03	
Redund Horz 1 Bracing	Max Tension	33	6.40	0.00	0.00			
	Max. Compression	33	-6.40	0.00	0.00			
	Max. Mx	28	6.16	-0.01	0.00			
	Max. My	28	-1.17	0.00	0.00			
	Max. Vy	28	0.01	0.00	0.00			
	Max. Vx	28	0.00	0.00	0.00			
Redund Diag 1 Bracing	Max Tension	19	10.47	0.00	0.00			
	Max. Compression	14	-6.38	0.00	0.00			
	Max. Mx	34	4.70	-0.02	0.00			
	Max. My	20	10.42	0.00	-0.00			
	Max. Vy	34	0.01	0.00	0.00			
	Max. Vx	20	0.00	0.00	0.00			
Redund Hip 1 Bracing	Max Tension	19	0.01	0.00	0.00			
	Max. Compression	16	-0.03	0.00	0.00			
	Max. Mx	18	0.01	-0.02	0.00			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 45 of 63
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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
		Redund Sub Horz Bracing	Max. Vy	18	0.02	0.00	0.00
			Max Tension	19	12.84	0.00	0.00
		Inner Bracing	Max. Compression	14	-7.43	0.00	0.00
			Max. Mx	18	4.30	-0.09	0.00
			Max. My	18	4.30	0.00	0.00
			Max. Vy	18	0.04	0.00	0.00
			Max. Vx	18	0.00	0.00	0.00
			Max Tension	33	0.17	0.00	0.00
			Max. Compression	33	-0.20	0.00	0.00
			Max. Mx	18	-0.00	0.32	0.00
			Max. My	31	0.00	0.00	-0.00
			Max. Vy	18	-0.07	0.00	0.00
		Max. Vx	31	0.00	0.00	0.00	

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg D	Max. Vert	29	450.73	26.55	-28.40
	Max. H <sub>x</sub>	30	436.73	27.41	-25.67
	Max. H <sub>z</sub>	20	-384.87	-26.24	31.55
	Min. Vert	21	-399.86	-29.07	30.76
	Min. H <sub>x</sub>	22	-385.77	-29.96	27.91
	Min. H <sub>z</sub>	28	435.82	23.84	-29.14
Leg C	Max. Vert	25	450.42	-28.31	-26.76
	Max. H <sub>x</sub>	32	-389.70	31.27	26.97
	Max. H <sub>z</sub>	34	-388.80	28.42	29.72
	Min. Vert	33	-403.85	30.88	29.33
	Min. H <sub>x</sub>	24	436.36	-28.67	-24.51
	Min. H <sub>z</sub>	26	435.45	-25.98	-27.14
Leg B	Max. Vert	21	449.39	-28.35	26.53
	Max. H <sub>x</sub>	30	-387.10	31.26	-26.70
	Max. H <sub>z</sub>	20	434.49	-25.98	26.95
	Min. Vert	29	-401.19	30.83	-29.08
	Min. H <sub>x</sub>	22	435.40	-28.75	24.25
	Min. H <sub>z</sub>	28	-386.21	28.33	-29.52
Leg A	Max. Vert	33	453.37	26.83	28.40
	Max. H <sub>x</sub>	32	439.32	27.71	25.65
	Max. H <sub>z</sub>	34	438.41	24.09	29.17
	Min. Vert	25	-400.88	-29.27	-30.77
	Min. H <sub>x</sub>	24	-386.74	-30.18	-27.89
	Min. H <sub>z</sub>	26	-385.84	-26.41	-31.58

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	68.76	0.00	0.00	-11.13	10.48	0.00
Dead+Wind 0 deg - No Ice	68.76	-0.21	-71.45	-8077.54	35.16	-42.39
Dead+Wind 30 deg - No Ice	68.76	39.95	-68.94	-7603.64	-4401.62	-45.47

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Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>y</sub>	Overturning Moment, M <sub>x</sub>	Overturning Moment, M <sub>y</sub>	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 45 deg - No Ice	68.76	56.60	-56.23	-6203.05	-6241.96	-39.03
Dead+Wind 60 deg - No Ice	68.76	69.40	-39.68	-4380.49	-7656.20	-29.93
Dead+Wind 90 deg - No Ice	68.76	71.97	0.21	13.45	-8141.64	-7.58
Dead+Wind 120 deg - No Ice	68.76	69.61	40.05	4400.80	-7680.81	18.91
Dead+Wind 135 deg - No Ice	68.76	56.90	56.53	6215.54	-6276.77	30.05
Dead+Wind 150 deg - No Ice	68.76	40.31	69.15	7605.95	-4444.26	39.13
Dead+Wind 180 deg - No Ice	68.76	0.21	71.45	8055.23	-14.06	42.39
Dead+Wind 210 deg - No Ice	68.76	-39.95	68.94	7581.26	4422.74	45.48
Dead+Wind 225 deg - No Ice	68.76	-56.60	56.23	6180.66	6263.02	39.03
Dead+Wind 240 deg - No Ice	68.76	-69.40	39.68	4358.11	7677.23	29.93
Dead+Wind 270 deg - No Ice	68.76	-71.97	-0.21	-35.77	8162.62	7.58
Dead+Wind 300 deg - No Ice	68.76	-69.61	-40.05	-4423.05	7701.83	-18.92
Dead+Wind 315 deg - No Ice	68.76	-56.90	-56.53	-6237.77	6297.81	-30.04
Dead+Wind 330 deg - No Ice	68.76	-40.31	-69.15	-7628.17	4465.35	-39.12
Dead+Ice+Temp	100.21	0.00	0.00	-14.41	38.01	0.00
Dead+Wind 0 deg+Ice+Temp	100.21	-0.21	-88.06	-9763.79	61.21	-72.23
Dead+Wind 30 deg+Ice+Temp	100.21	49.35	-85.21	-9220.06	-5307.22	-75.00
Dead+Wind 45 deg+Ice+Temp	100.21	69.89	-69.51	-7523.92	-7533.31	-63.00
Dead+Wind 60 deg+Ice+Temp	100.21	85.68	-49.08	-5316.02	-9243.43	-46.71
Dead+Wind 90 deg+Ice+Temp	100.21	88.60	0.21	8.64	-9799.00	-8.67
Dead+Wind 120 deg+Ice+Temp	100.21	85.89	49.44	5327.13	-9266.47	36.49
Dead+Wind 135 deg+Ice+Temp	100.21	70.19	69.81	7527.70	-7565.90	54.65
Dead+Wind 150 deg+Ice+Temp	100.21	49.71	85.42	9214.27	-5347.14	69.10
Dead+Wind 180 deg+Ice+Temp	100.21	0.21	88.06	9734.95	15.11	72.24
Dead+Wind 210 deg+Ice+Temp	100.21	-49.35	85.21	9191.08	5383.54	74.99
Dead+Wind 225 deg+Ice+Temp	100.21	-69.89	69.51	7494.92	7609.54	63.00
Dead+Wind 240 deg+Ice+Temp	100.21	-85.68	49.08	5287.04	9319.58	46.70
Dead+Wind 270 deg+Ice+Temp	100.21	-88.60	-0.21	-37.48	9875.08	8.67
Dead+Wind 300 deg+Ice+Temp	100.21	-85.89	-49.44	-5355.81	9342.63	-36.47
Dead+Wind 315 deg+Ice+Temp	100.21	-70.19	-69.81	-7556.36	7642.15	-54.64
Dead+Wind 330 deg+Ice+Temp	100.21	-49.71	-85.42	-9242.97	5423.48	-69.08
Dead+Wind 0 deg - Service	68.76	-0.21	-71.45	-8077.54	35.16	-42.39
Dead+Wind 30 deg - Service	68.76	39.95	-68.94	-7603.64	-4401.62	-45.47
Dead+Wind 45 deg - Service	68.76	56.60	-56.23	-6203.05	-6241.96	-39.03
Dead+Wind 60 deg - Service	68.76	69.40	-39.68	-4380.49	-7656.20	-29.93
Dead+Wind 90 deg - Service	68.76	71.97	0.21	13.45	-8141.64	-7.58
Dead+Wind 120 deg - Service	68.76	69.61	40.05	4400.80	-7680.81	18.91
Dead+Wind 135 deg - Service	68.76	56.90	56.53	6215.54	-6276.77	30.05
Dead+Wind 150 deg - Service	68.76	40.31	69.15	7605.95	-4444.26	39.13
Dead+Wind 180 deg - Service	68.76	0.21	71.45	8055.23	-14.06	42.39
Dead+Wind 210 deg - Service	68.76	-39.95	68.94	7581.26	4422.74	45.48
Dead+Wind 225 deg - Service	68.76	-56.60	56.23	6180.66	6263.02	39.03
Dead+Wind 240 deg - Service	68.76	-69.40	39.68	4358.11	7677.23	29.93
Dead+Wind 270 deg - Service	68.76	-71.97	-0.21	-35.77	8162.62	7.58
Dead+Wind 300 deg - Service	68.76	-69.61	-40.05	-4423.05	7701.83	-18.92
Dead+Wind 315 deg - Service	68.76	-56.90	-56.53	-6237.77	6297.81	-30.04
Dead+Wind 330 deg - Service	68.76	-40.31	-69.15	-7628.17	4465.35	-39.12

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-68.76	0.00	-0.00	68.76	0.00	0.000%
2	-0.21	-68.76	-71.45	0.21	68.76	71.45	0.000%
3	39.95	-68.76	-68.94	-39.95	68.76	68.94	0.000%
4	56.60	-68.76	-56.23	-56.60	68.76	56.23	0.000%
5	69.40	-68.76	-39.68	-69.40	68.76	39.68	0.000%

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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
6	71.97	-68.76	0.21	-71.97	68.76	-0.21	0.000%
7	69.61	-68.76	40.05	-69.61	68.76	-40.05	0.000%
8	56.90	-68.76	56.53	-56.90	68.76	-56.53	0.000%
9	40.31	-68.76	69.15	-40.31	68.76	-69.15	0.000%
10	0.21	-68.76	71.45	-0.21	68.76	-71.45	0.000%
11	-39.95	-68.76	68.94	39.95	68.76	-68.94	0.000%
12	-56.60	-68.76	56.23	56.60	68.76	-56.23	0.000%
13	-69.40	-68.76	39.68	69.40	68.76	-39.68	0.000%
14	-71.97	-68.76	-0.21	71.97	68.76	0.21	0.000%
15	-69.61	-68.76	-40.05	69.61	68.76	40.05	0.000%
16	-56.90	-68.76	-56.53	56.90	68.76	56.53	0.000%
17	-40.31	-68.76	-69.15	40.31	68.76	69.15	0.000%
18	0.00	-100.21	0.00	-0.00	100.21	-0.00	0.000%
19	-0.21	-100.21	-88.06	0.21	100.21	88.06	0.000%
20	49.35	-100.21	-85.21	-49.35	100.21	85.21	0.000%
21	69.89	-100.21	-69.51	-69.89	100.21	69.51	0.001%
22	85.68	-100.21	-49.08	-85.68	100.21	49.08	0.000%
23	88.60	-100.21	0.21	-88.60	100.21	-0.21	0.000%
24	85.89	-100.21	49.44	-85.89	100.21	-49.44	0.000%
25	70.19	-100.21	69.81	-70.19	100.21	-69.81	0.001%
26	49.71	-100.21	85.42	-49.71	100.21	-85.42	0.000%
27	0.21	-100.21	88.06	-0.21	100.21	-88.06	0.000%
28	-49.35	-100.21	85.21	49.35	100.21	-85.21	0.001%
29	-69.89	-100.21	69.51	69.89	100.21	-69.51	0.001%
30	-85.68	-100.21	49.08	85.68	100.21	-49.08	0.000%
31	-88.60	-100.21	-0.21	88.60	100.21	0.21	0.000%
32	-85.89	-100.21	-49.44	85.89	100.21	49.44	0.000%
33	-70.19	-100.21	-69.81	70.19	100.21	69.81	0.001%
34	-49.71	-100.21	-85.42	49.71	100.21	85.42	0.001%
35	-0.21	-68.76	-71.45	0.21	68.76	71.45	0.000%
36	39.95	-68.76	-68.94	-39.95	68.76	68.94	0.000%
37	56.60	-68.76	-56.23	-56.60	68.76	56.23	0.000%
38	69.40	-68.76	-39.68	-69.40	68.76	39.68	0.000%
39	71.97	-68.76	0.21	-71.97	68.76	-0.21	0.000%
40	69.61	-68.76	40.05	-69.61	68.76	-40.05	0.000%
41	56.90	-68.76	56.53	-56.90	68.76	-56.53	0.000%
42	40.31	-68.76	69.15	-40.31	68.76	-69.15	0.000%
43	0.21	-68.76	71.45	-0.21	68.76	-71.45	0.000%
44	-39.95	-68.76	68.94	39.95	68.76	-68.94	0.000%
45	-56.60	-68.76	56.23	56.60	68.76	-56.23	0.000%
46	-69.40	-68.76	39.68	69.40	68.76	-39.68	0.000%
47	-71.97	-68.76	-0.21	71.97	68.76	0.21	0.000%
48	-69.61	-68.76	-40.05	69.61	68.76	40.05	0.000%
49	-56.90	-68.76	-56.53	56.90	68.76	56.53	0.000%
50	-40.31	-68.76	-69.15	40.31	68.76	69.15	0.000%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00080087
2	Yes	6	0.00070591	0.00026647
3	Yes	5	0.00082153	0.00034561
4	Yes	5	0.00052442	0.00026055
5	Yes	5	0.00086647	0.00029255
6	Yes	6	0.00078687	0.00021839

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7	Yes	5	0.00087492	0.00029386
8	Yes	5	0.00052947	0.00026231
9	Yes	5	0.00081949	0.00034597
10	Yes	6	0.00069777	0.00026444
11	Yes	5	0.00081313	0.00034477
12	Yes	5	0.00052482	0.00026137
13	Yes	5	0.00087674	0.00029421
14	Yes	6	0.00079667	0.00022016
15	Yes	5	0.00088301	0.00029585
16	Yes	5	0.00053515	0.00026346
17	Yes	5	0.00082756	0.00034717
18	Yes	5	0.00000001	0.00054990
19	Yes	7	0.00099477	0.00038415
20	Yes	6	0.00092845	0.00040174
21	Yes	6	0.00083428	0.00035581
22	Yes	9	0.00079693	0.00024253
23	Yes	11	0.00087677	0.00024619
24	Yes	9	0.00080773	0.00024525
25	Yes	6	0.00084303	0.00035816
26	Yes	6	0.00092392	0.00040076
27	Yes	7	0.00098060	0.00038024
28	Yes	6	0.00091711	0.00039848
29	Yes	6	0.00085704	0.00036109
30	Yes	9	0.00083981	0.00025285
31	Yes	11	0.00093018	0.00025842
32	Yes	9	0.00084808	0.00025471
33	Yes	6	0.00086805	0.00036460
34	Yes	6	0.00093467	0.00040365
35	Yes	6	0.00070591	0.00026647
36	Yes	5	0.00082153	0.00034561
37	Yes	5	0.00052442	0.00026055
38	Yes	5	0.00086647	0.00029255
39	Yes	6	0.00078687	0.00021839
40	Yes	5	0.00087492	0.00029386
41	Yes	5	0.00052947	0.00026231
42	Yes	5	0.00081949	0.00034597
43	Yes	6	0.00069777	0.00026444
44	Yes	5	0.00081313	0.00034477
45	Yes	5	0.00052482	0.00026137
46	Yes	5	0.00087674	0.00029421
47	Yes	6	0.00079667	0.00022016
48	Yes	5	0.00088301	0.00029585
49	Yes	5	0.00053515	0.00026346
50	Yes	5	0.00082756	0.00034717

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 170	12.325	48	0.6165	0.0227
T2	170 - 163.573	10.870	48	0.6053	0.0212
T3	163.573 - 159.049	9.959	48	0.5870	0.0215
T4	159.049 - 154.524	9.334	48	0.5699	0.0217
T5	154.524 - 150	8.734	48	0.5469	0.0229
T6	150 - 140	8.161	48	0.5203	0.0239
T7	140 - 130	6.996	48	0.4586	0.0250
T8	130 - 120	5.971	48	0.4114	0.0248
T9	120 - 110	5.059	48	0.3610	0.0224
T10	110 - 100	4.250	48	0.3204	0.0211

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Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T11	100 - 90	3.533	48	0.2781	0.0199
T12	90 - 80	2.902	48	0.2424	0.0175
T13	80 - 60	2.349	48	0.2061	0.0153
T14	60 - 50	1.416	48	0.1659	0.0101
T15	50 - 40	1.017	48	0.1460	0.0076
T16	40 - 30	0.689	48	0.1252	0.0063
T17	30 - 20	0.417	48	0.0940	0.0050
T18	20 - 10	0.213	48	0.0626	0.0037
T19	10 - 0	0.076	40	0.0307	0.0024

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
180.00	PA6-65AC	48	12.325	0.6165	0.0227	40708
176.00	PA6-65AC	48	11.740	0.6137	0.0218	40708
172.00	6' Standoff	48	11.158	0.6090	0.0213	26063
170.00	20' 8 Bay Di-Pole	48	10.870	0.6053	0.0212	22252
169.00	4' Omni	48	10.726	0.6031	0.0212	21256
163.00	T-Frame	48	9.879	0.5850	0.0215	15392
160.00	3" Dia x 15' Omni	48	9.464	0.5739	0.0216	11105
150.00	2" Dia 10' Omni	48	8.161	0.5203	0.0239	8594
145.00	6' Standoff	48	7.561	0.4885	0.0245	8353
143.00	6' Standoff	48	7.331	0.4760	0.0247	8270
133.00	10'6"x4" Pipe Mount	48	6.266	0.4253	0.0251	10120
132.00	3' Stand-off	48	6.167	0.4207	0.0250	10444
130.00	PA6-65AC	48	5.971	0.4114	0.0248	10983
126.00	LeBlanc 10' Standoff (1)	48	5.594	0.3912	0.0239	11315
122.00	EUSF10-U	48	5.233	0.3706	0.0229	11312
120.00	3" Dia x 15' Omni	48	5.059	0.3610	0.0224	11416
116.00	ASP711	48	4.723	0.3440	0.0218	12015
115.00	6' Standoff	48	4.642	0.3401	0.0216	12218
112.00	6' Stand-off	48	4.404	0.3284	0.0213	12809
106.00	12' Wireless Frame	48	3.952	0.3034	0.0207	13356
101.00	LeBlanc 10' Standoff (1)	48	3.600	0.2821	0.0201	13569
100.00	4' Grid Dish	48	3.533	0.2781	0.0199	13656
88.00	3' Stand-off	48	2.786	0.2350	0.0171	16256
85.00	3' Stand-off	48	2.617	0.2236	0.0164	16998
80.00	6' Ice Shield	48	2.349	0.2061	0.0153	18550
76.00	10'6"x4" Pipe Mount	48	2.146	0.1952	0.0144	20641
75.00	6' Grid Dish	48	2.097	0.1928	0.0142	21294
56.00	3' Stand-off	48	1.250	0.1581	0.0090	22444
47.00	3' Stand-off	48	0.911	0.1403	0.0071	15906

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 170	14.496	32	0.7097	0.0349
T2	170 - 163.573	12.824	32	0.6975	0.0316



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Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T3	163.573 - 159.049	11.776	32	0.6777	0.0319
T4	159.049 - 154.524	11.055	32	0.6594	0.0323
T5	154.524 - 150	10.360	32	0.6342	0.0339
T6	150 - 140	9.695	32	0.6048	0.0352
T7	140 - 130	8.338	32	0.5360	0.0366
T8	130 - 120	7.138	32	0.4827	0.0362
T9	120 - 110	6.066	32	0.4255	0.0339
T10	110 - 100	5.111	32	0.3791	0.0328
T11	100 - 90	4.260	32	0.3304	0.0316
T12	90 - 80	3.509	32	0.2890	0.0283
T13	80 - 60	2.846	32	0.2466	0.0253
T14	60 - 50	1.722	32	0.1994	0.0169
T15	50 - 40	1.237	32	0.1758	0.0126
T16	40 - 30	0.840	32	0.1510	0.0104
T17	30 - 20	0.511	32	0.1135	0.0082
T18	20 - 10	0.262	32	0.0756	0.0061
T19	10 - 0	0.094	24	0.0372	0.0040

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
180.00	PA6-65AC	32	14.496	0.7097	0.0349	37045
176.00	PA6-65AC	32	13.824	0.7067	0.0334	37045
172.00	6' Standoff	32	13.155	0.7015	0.0318	23764
170.00	20' 8 Bay Di-Pole	32	12.824	0.6975	0.0316	20473
169.00	4' Omni	32	12.659	0.6950	0.0316	19745
163.00	T-Frame	32	11.683	0.6756	0.0319	14941
160.00	3" Dia x 15' Omni	32	11.204	0.6637	0.0321	10305
150.00	2" Dia 10' Omni	32	9.695	0.6048	0.0352	7773
145.00	6' Standoff	32	8.997	0.5694	0.0361	7496
143.00	6' Standoff	32	8.729	0.5555	0.0363	7392
133.00	10'6"x4" Pipe Mount	32	7.484	0.4985	0.0366	8909
132.00	3' Stand-off	32	7.367	0.4933	0.0365	9182
130.00	PA6-65AC	32	7.138	0.4827	0.0362	9644
126.00	LeBlanc 10' Standoff (1)	32	6.695	0.4598	0.0353	9983
122.00	EUSF10-U	32	6.271	0.4364	0.0343	10053
120.00	3" Dia x 15' Omni	32	6.066	0.4255	0.0339	10158
116.00	ASP711	32	5.671	0.4061	0.0333	10628
115.00	6' Standoff	32	5.575	0.4016	0.0332	10781
112.00	6' Stand-off	32	5.293	0.3882	0.0329	11220
106.00	12' Wireless Frame	32	4.758	0.3595	0.0325	11708
101.00	LeBlanc 10' Standoff (1)	32	4.341	0.3350	0.0318	11957
100.00	4' Grid Dish	32	4.260	0.3304	0.0316	12031
88.00	3' Stand-off	32	3.370	0.2803	0.0277	13962
85.00	3' Stand-off	32	3.167	0.2671	0.0268	14666
80.00	6' Ice Shield	32	2.846	0.2466	0.0253	16143
76.00	10'6"x4" Pipe Mount	32	2.602	0.2338	0.0239	17989
75.00	6' Grid Dish	32	2.543	0.2311	0.0235	18556
56.00	3' Stand-off	32	1.520	0.1902	0.0150	18683
47.00	3' Stand-off	32	1.109	0.1690	0.0118	13069

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### Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load / Allowable	Allowable Ratio	Criteria
T1	180	Diagonal	A325X	0.6250	2	3.27	8.16	0.401	1.333	Member Bearing
		Secondary Horizontal	A325X	0.6250	2	0.40	8.16	0.049	1.333	Member Bearing
		Top Girt	A325X	0.6250	2	0.25	8.16	0.031	1.333	Member Bearing
T2	170	Diagonal	A325X	0.6250	2	3.56	8.16	0.437	1.333	Member Bearing
		Top Girt	A325X	0.6250	2	0.63	8.16	0.077	1.333	Member Bearing
T3	163.573	Diagonal	A325X	0.6250	2	2.95	8.16	0.361	1.333	Member Bearing
		Top Girt	A325X	0.6250	2	0.76	8.16	0.093	1.333	Member Bearing
T4	159.049	Diagonal	A325X	0.6250	2	3.23	8.16	0.396	1.333	Member Bearing
T5	154.524	Diagonal	A325X	0.6250	2	3.20	8.16	0.392	1.333	Member Bearing
T6	150	Diagonal	A325X	0.6250	2	3.42	8.16	0.420	1.333	Member Bearing
		Top Girt	A325X	0.6250	2	0.53	8.16	0.065	1.333	Member Bearing
T7	140	Diagonal	A325X	0.6250	2	4.57	9.20	0.496	1.333	Bolt Shear
		Top Girt	A325X	0.6250	2	0.46	8.16	0.056	1.333	Member Bearing
T8	130	Diagonal	A325X	0.6250	2	5.38	9.20	0.585	1.333	Bolt Shear
		Secondary Horizontal	A325X	0.6250	2	0.91	9.20	0.099	1.333	Bolt Shear
T9	120	Diagonal	A325X	0.6250	2	5.62	9.20	0.610	1.333	Bolt Shear
		Horizontal	A325X	0.6250	2	0.58	9.20	0.063	1.333	Bolt Shear
		Secondary Horizontal	A325X	0.6250	2	1.10	8.16	0.135	1.333	Member Bearing
T10	110	Diagonal	A325X	0.6250	2	6.27	9.20	0.682	1.333	Bolt Shear
		Secondary Horizontal	A325X	0.6250	2	1.30	9.20	0.142	1.333	Bolt Shear
T11	100	Diagonal	A325X	0.6250	2	6.58	9.20	0.715	1.333	Bolt Shear
		Horizontal	A325X	0.6250	2	0.82	9.20	0.089	1.333	Bolt Shear
T12	90	Diagonal	A325X	0.6250	2	6.99	9.20	0.759	1.333	Bolt Shear
		Secondary Horizontal	A325X	0.6250	2	1.73	9.20	0.188	1.333	Bolt Shear
T13	80	Diagonal	A325X	0.6250	2	7.46	16.31	0.458	1.333	Member Bearing
		Top Girt	A325X	0.6250	2	0.54	9.20	0.059	1.333	Bolt Shear
T14	60	Diagonal	A325X	0.6250	2	7.24	16.31	0.444	1.333	Member Bearing
		Horizontal	A325X	0.6250	2	1.26	16.31	0.077	1.333	Member Bearing
T15	50	Diagonal	A325X	0.6250	2	7.95	18.41	0.432	1.333	Bolt Shear
		Secondary Horizontal	A325X	0.6250	2	2.55	9.20	0.277	1.333	Bolt Shear
T16	40	Diagonal	A325X	0.6250	2	8.11	18.41	0.441	1.333	Bolt Shear
		Secondary Horizontal	A325X	0.6250	2	2.74	9.20	0.298	1.333	Bolt Shear
		Top Girt	A325X	0.6250	2	1.52	16.31	0.093	1.333	Member Bearing
T17	30	Diagonal	A325X	0.6250	2	7.47	18.41	0.406	1.333	Bolt Shear
		Secondary Horizontal	A325X	0.6250	2	2.95	9.20	0.320	1.333	Bolt Shear

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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
T18	20	Diagonal	A325X	0.6250	2	10.14	18.41	0.551 ✓	1.333	Bolt Shear
		Horizontal	A325X	0.6250	2	3.04	16.31	0.186 ✓	1.333	Member Bearing
		Secondary Horizontal	A325X	0.6250	2	3.09	9.20	0.335 ✓	1.333	Bolt Shear
T19	10	Diagonal	A325X	0.6250	2	13.41	18.41	0.729 ✓	1.333	Bolt Shear
		Horizontal	A325X	0.6250	2	8.45	18.41	0.459 ✓	1.333	Bolt Shear

**Compression Checks**

**Leg Design Data (Compression)**

Section No.	Elevation ft	Size	L ft	L <sub>n</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	180 - 170	L3 1/2x3 1/2x3/8	10.00	5.00	87.3 K=1.00	14.519	2.4800	-6.92	36.01	0.192 ✓
T2	170 - 163.573	L5x5x5/16	6.43	6.43	77.6 K=1.00	15.232	3.0300	-21.37	46.15	0.463 ✓
T3	163.573 - 159.049	L5x5x5/16	4.53	4.53	54.7 K=1.00	17.404	3.0300	-36.54	52.74	0.693 ✓
T4	159.049 - 154.524	L5x5x5/16	4.53	4.53	54.7 K=1.00	17.404	3.0300	-48.73	52.74	0.924 ✓
T5	154.524 - 150	L5x5x5/16	4.53	4.53	54.7 K=1.00	17.404	3.0300	-58.08	52.74	1.101 ✓
T6	150 - 140	L5x5x3/8	10.01	5.01	60.7 K=1.00	17.364	3.6100	-81.08	62.68	1.293 ✓
T7	140 - 130	L6x6x1/2	10.01	5.23	53.2 K=1.00	18.066	5.7500	-97.27	103.88	0.936 ✓
T8	130 - 120	L6x6x1/2	10.01	5.21	53.0 K=1.00	18.083	5.7500	-120.85	103.98	1.162 ✓
T9	120 - 110	L6x6x3/4	10.01	5.20	53.3 K=1.00	18.057	8.4400	-146.56	152.40	0.962 ✓
T10	110 - 100	L6x6x3/4	10.01	5.18	53.2 K=1.00	18.069	8.4400	-173.77	152.50	1.139 ✓
T11	100 - 90	L8x8x3/4	10.01	10.01	76.0 K=1.00	15.789	11.4000	-202.51	180.00	1.125 ✓
T12	90 - 80	L8x8x3/4	10.01	5.16	39.2 K=1.00	19.253	11.4000	-230.26	219.49	1.049 ✓
T13	80 - 60	L8x8x1 w/ 1/2x7 Plates	20.03	10.01	48.3 K=1.00	18.499	22.0000	-287.22	406.97	0.706 ✓
T14	60 - 50	L8x8x1-1/8 w/ 1/2x7 Plates	10.01	10.01	48.6 K=1.00	18.477	23.7340	-314.06	438.54	0.716 ✓
T15	50 - 40	L8x8x1-1/8 w/ 1/2x7 Plates	10.01	5.13	24.9 K=1.00	20.291	23.7340	-339.75	481.58	0.705 ✓
T16	40 - 30	L8x8x1 1/8	10.01	5.12	39.4	19.236	16.7000	-365.07	321.24	1.136 ✓

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P/P <sub>a</sub>
					K=1.00					
T17	30 - 20	L8x8x1 1/8	10.01	5.12	39.4	19,239	16.7000	-392.79	321.29	1.223
					K=1.00					
T18	20 - 10	L8x8x1 1/8	10.01	5.11	39.3	19,242	16.7000	-411.29	321.34	1.280
					K=1.00					
T19	10 - 0	L8x8x1 1/8	10.01	5.01	38.5	19,307	16.7000	-426.58	322.43	1.323
					K=1.00					

### Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P/P <sub>a</sub>
T1	180 - 170	L2 1/2x2 1/2x3/16	11.41	5.49	130.1	8,827	0.9020	-6.55	7.96	0.823
					K=0.98					
T2	170 - 163.573	L2 1/2x2 1/2x3/16	8.46	4.02	103.0	12,592	0.9020	-7.13	11.36	0.628
					K=1.06					
T3	163.573 - 159.049	L2x2x3/16	7.25	3.51	110.1	11,658	0.7150	-5.90	8.34	0.707
					K=1.03					
T4	159.049 - 154.524	L2 1/2x2x3/16	7.51	3.63	106.6	12,128	0.8090	-6.15	9.81	0.627
					K=1.04					
T5	154.524 - 150	L2 1/2x2x3/16	7.77	3.76	109.3	11,766	0.8090	-6.40	9.52	0.672
					K=1.03					
T6	150 - 140	L2 1/2x2x3/16	8.61	4.20	118.4	10,505	0.8090	-6.84	8.50	0.805
					K=1.00					
T7	140 - 130	L3x2 1/2x1/4	12.53	6.33	138.3	7,810	1.3100	-9.13	10.23	0.893
					K=0.96					
T8	130 - 120	L3x3x1/4	12.98	6.54	129.6	8,886	1.4400	-10.76	12.80	0.841
					K=0.98					
T9	120 - 110	L3x3x1/4	13.45	6.76	133.1	8,432	1.4400	-11.24	12.14	0.925
					K=0.97					
T10	110 - 100	L3 1/2x3x1/4	13.94	7.00	130.0	8,832	1.5600	-12.55	13.78	0.911
					K=0.98					
T11	100 - 90	L3 1/2x3x1/4	14.44	7.25	133.6	8,366	1.5600	-13.16	13.05	1.008
					K=0.97					
T12	90 - 80	L3 1/2x3x1/4	14.97	7.50	137.3	7,920	1.5600	-13.97	12.36	1.131
					K=0.96					
T13	80 - 60	2L2 1/2x2x3/16	16.07	8.04	122.1	9,977	1.6200	-14.93	16.16	0.924
					K=1.00					
T14	60 - 50	2L2 1/2x2x3/16	16.63	8.32	126.4	9,352	1.6200	-14.48	15.15	0.956
					K=1.00					
T15	50 - 40	2L2 1/2x2x3/8	17.21	8.60	131.0	8,696	3.0900	-15.89	26.87	0.592
					K=0.97					
T16	40 - 30	2L2 1/2x2x3/8	17.80	8.90	134.5	8,254	3.0900	-16.23	25.50	0.636
					K=0.97					
T17	30 - 20	2L2 1/2x2x3/8	18.40	9.19	138.0	7,837	3.0900	-14.94	24.22	0.617
					K=0.96					
T18	20 - 10	2L2 1/2x2x3/8	19.00	9.49	141.6	7,446	3.0900	-20.29	23.01	0.882
					K=0.95					
T19	10 - 0	2L2 1/2x2 1/2x1/4	13.37	6.47	110.5	11,606	2.3800	-21.38	27.62	0.774

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
K=1.09										✓

### Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T9	120 - 110	L2 1/2x2 1/2x1/4	9.12	4.10	110.1 K=1.10	11.660	1.1900	-1.16	13.88	0.084
T11	100 - 90	L2 1/2x2 1/2x1/4	10.56	4.82	118.8 K=1.01	10.447	1.1900	-1.65	12.43	0.132
T14	60 - 50	2L2x2x3/16	13.43	6.15	119.8 K=1.00	10.316	1.4300	-1.35	14.75	0.091
T18	20 - 10	2L2x2x3/16	16.29	7.60	141.2 K=0.96	7.486	1.4300	-1.12	10.70	0.104
T19	10 - 0	2L2 1/2x2 1/2x1/4	17.01	7.96	123.2 K=0.99	9.813	2.3800	-16.66	23.35	0.713

### Secondary Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	180 - 170	L2x2x3/16	6.00	5.28	141.5 K=0.88	7.454	0.7150	-0.80	5.33	0.151
T7	140 - 130	L2x2x1/4	8.03	7.53	192.1 K=0.83	4.048	0.9380	-1.46	3.80	0.384
T8	130 - 120	L2x2x1/4	8.75	7.82	198.2 K=0.83	3.802	0.9380	-1.81	3.57	0.509
T9	120 - 110	L2x2x3/16	9.47	8.54	211.7 K=0.81	3.331	0.7150	-2.20	2.38	0.924
T10	110 - 100	L2x2x1/4	10.19	9.26	228.0 K=0.80	2.873	0.9380	-2.61	2.69	0.968
T12	90 - 80	L2 1/2x2 1/2x1/4	11.62	10.53	209.8 K=0.82	3.392	1.1900	-3.46	4.04	0.856
T15	50 - 40	L3 1/2x3 1/2x1/4	14.49	13.36	191.8 K=0.83	4.061	1.6900	-5.10	6.86	0.743
T16	40 - 30	L3 1/2x3 1/2x1/4	15.21	14.12	200.8 K=0.82	3.705	1.6900	-5.48	6.26	0.875
T17	30 - 20	L3 1/2x3 1/2x1/4	15.93	14.83	209.2 K=0.82	3.412	1.6900	-5.90	5.77	1.022
T18	20 - 10	L3 1/2x3 1/2x1/4	16.65	15.55	217.6 K=0.81	3.154	1.6900	-6.17	5.33	1.158

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**Top Girt Design Data (Compression)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	180 - 170	L2x2x3/16	6.00	5.28	145.1 K=0.90	7.091	0.7150	-0.12	5.07	0.024
T2	170 - 163.573	L2x2x3/16	6.00	5.28	145.1 K=0.90	7.091	0.7150	-0.73	5.07	0.144
T3	163.573 - 159.049	L2x2x3/16	6.00	5.16	142.8 K=0.91	7.325	0.7150	-0.90	5.24	0.172
T6	150 - 140	L2 1/2x2 1/2x3/16	6.97	6.13	137.6 K=0.93	7.889	0.9020	-0.91	7.12	0.127
T7	140 - 130	L2 1/2x2 1/2x3/16	7.69	3.42	101.5 K=1.22	12.788	0.9020	-0.92	11.53	0.080
T13	80 - 60	L2 1/2x2 1/2x1/4	11.99	5.45	130.1 K=0.98	8.825	1.1900	-0.87	10.50	0.083
T16	40 - 30	2L2x2x3/16	14.86	6.86	130.3 K=0.98	8.795	1.4300	-1.25	12.58	0.099

**Redundant Horizontal (1) Design Data (Compression)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T19	10 - 0	L2 1/2x2 1/2x3/16	4.25	3.92	107.5 K=1.13	12.004	0.9020	-6.40	10.83	0.591

**Redundant Diagonal (1) Design Data (Compression)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T19	10 - 0	L2 1/2x2 1/2x3/16	6.45	5.92	143.6 K=1.00	7.239	0.9020	-6.38	6.53	0.977

**Redundant Hip (1) Design Data (Compression)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T19	10 - 0	L2 1/2x2 1/2x3/16	6.01	6.01	145.8 K=1.00	7.024	0.9020	-0.03	6.34	0.005

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**Redundant Sub-Horizontal Design Data (Compression)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T19	10 - 0	L3x3x5/16	8.86	8.86	180.6 K=1.00	4.578	1,7800	-7.43	8.15	0.911 ✓

**Inner Bracing Design Data (Compression)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T7	140 - 130	L2x2x3/16	5.44	5.44	165.6 K=1.00	5.444	0.7150	-0.17	3.89	0.044 ✓
T9	120 - 110	L2 1/2x2x3/16	6.45	6.45	181.3 K=1.00	4.542	0.8090	-0.11	3.67	0.031 ✓
T11	100 - 90	L2 1/2x2x3/16	7.47	7.47	209.8 K=1.00	3.392	0.8090	-0.12	2.74	0.044 ✓
T13	80 - 60	2L2x2x3/16	8.48	8.48	164.9 K=1.00	5.490	1.4300	-0.16	7.85	0.020 ✓
T14	60 - 50	2L2x2x3/16	9.49	9.49	184.6 K=1.00	4.380	1.4300	-0.15	6.26	0.024 ✓
T16	40 - 30	2L2x2x3/16	10.51	10.51	204.4 K=1.00	3.575	1.4300	-0.20	5.11	0.038 ✓
T18	20 - 10	2L2x2 1/2x3/16	11.52	11.52	230.4 K=1.00	2.812	1.6200	-0.06	4.56	0.013 ✓
T19	10 - 0	2L2x2 1/2x3/16	12.03	12.03	240.6 K=1.00	2.580	1.6200	-0.20	4.18	0.047 ✓

**Tension Checks**

**Leg Design Data (Tension)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T1	180 - 170	L3 1/2x3 1/2x3/8	10.00	5.00	56.1	21,600	2.4800	6.70	53.57	0.125 ✓
T2	170 - 163.573	L5x5x5/16	6.43	6.43	49.1	21,600	3.0300	19.66	65.45	0.300 ✓
T3	163.573 - 159.049	L5x5x5/16	4.53	4.53	34.6	21,600	3.0300	32.78	65.45	0.501 ✓
T4	159.049 - 154.524	L5x5x5/16	4.53	4.53	34.6	21,600	3.0300	43.19	65.45	0.660 ✓
T5	154.524 - 150	L5x5x5/16	4.53	4.53	34.6	21,600	3.0300	52.82	65.45	0.807 ✓
T6	150 - 140	L5x5x3/8	10.01	5.01	38.5	21,600	3.6100	74.65	77.98	0.957 ✓

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T7	140 - 130	L6x6x1/2	10.01	5.23	33.7	21.600	5.7500	89.59	124.20	0.721
T8	130 - 120	L6x6x1/2	10.01	5.21	33.6	21.600	5.7500	110.86	124.20	0.893
T9	120 - 110	L6x6x3/4	10.01	5.20	34.1	21.600	8.4400	133.20	182.30	0.731
T10	110 - 100	L6x6x3/4	10.01	5.18	34.0	21.600	8.4400	157.46	182.30	0.864
T11	100 - 90	L8x8x3/4	10.01	10.01	48.6	21.600	11.4000	183.09	246.24	0.744
T12	90 - 80	L8x8x3/4	10.01	5.16	25.1	21.600	11.4000	209.04	246.24	0.849
T13	80 - 60	L8x8x1 w/ 1/2x7 Plates	20.03	10.01	48.3	21.600	22.0000	260.62	475.20	0.548
T14	60 - 50	L8x8x1-1/8 w/ 1/2x7 Plates	10.01	10.01	48.6	21.600	23.7340	283.25	512.65	0.553
T15	50 - 40	L8x8x1-1/8 w/ 1/2x7 Plates	10.01	5.13	24.9	21.600	23.7340	307.24	512.65	0.599
T16	40 - 30	L8x8x1 1/8	10.01	5.12	25.4	21.600	16.7000	327.83	360.72	0.909
T17	30 - 20	L8x8x1 1/8	10.01	5.12	25.4	21.600	16.7000	351.40	360.72	0.974
T18	20 - 10	L8x8x1 1/8	10.01	5.11	25.4	21.600	16.7000	372.69	360.72	1.033
T19	10 - 0	L8x8x1 1/8	10.01	5.01	24.8	21.600	16.7000	369.65	360.72	1.025

### Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	180 - 170	L2 1/2x2 1/2x3/16	11.41	5.49	88.0	29.000	0.5710	5.71	16.56	0.345
T2	170 - 163.573	L2 1/2x2 1/2x3/16	8.46	4.02	65.2	29.000	0.5710	6.52	16.56	0.393
T3	163.573 - 159.049	L2x2x3/16	7.25	3.51	72.4	29.000	0.4308	5.69	12.49	0.455
T4	159.049 - 154.524	L2 1/2x2x3/16	7.51	3.63	77.0	29.000	0.5013	6.46	14.54	0.445
T5	154.524 - 150	L2 1/2x2x3/16	7.77	3.76	79.6	29.000	0.5013	6.02	14.54	0.414
T6	150 - 140	L2 1/2x2x3/16	8.61	4.20	88.2	29.000	0.5013	6.75	14.54	0.464
T7	140 - 130	L3x2 1/2x1/4	12.53	6.33	104.5	29.000	0.8419	8.96	24.41	0.367
T8	130 - 120	L3x3x1/4	12.98	6.54	87.2	29.000	0.9394	10.53	27.24	0.386
T9	120 - 110	L3x3x1/4	13.45	6.76	90.0	29.000	0.9394	11.02	27.24	0.404



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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T10	110 - 100	L3 1/2x3x1/4	13.94	7.00	94.8	29.000	1.0294	12.31	29.85	0.412
T11	100 - 90	L3 1/2x3x1/4	14.44	7.25	98.1	29.000	1.0294	12.96	29.85	0.434
T12	90 - 80	L3 1/2x3x1/4	14.97	7.50	101.4	29.000	1.0294	13.70	29.85	0.459
T13	80 - 60	2L2 1/2x2x3/16	16.07	8.04	125.4	29.000	1.0041	14.25	29.12	0.489
T14	60 - 50	2L2 1/2x2x3/16	16.63	8.32	129.6	29.000	1.0041	14.12	29.12	0.485
T15	50 - 40	2L2 1/2x2x3/8	17.21	8.60	137.8	29.000	1.8956	14.31	54.97	0.260
T16	40 - 30	2L2 1/2x2x3/8	17.80	8.90	142.3	29.000	1.8956	15.27	54.97	0.278
T17	30 - 20	2L2 1/2x2x3/8	18.40	9.19	147.0	29.000	1.8956	14.87	54.97	0.271
T18	20 - 10	2L2 1/2x2x3/8	19.00	9.49	151.6	29.000	1.8956	14.90	54.97	0.271
T19	10 - 0	2L2 1/2x2 1/2x1/4	13.37	6.47	104.3	29.000	1.5037	26.83	43.61	0.615

### Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T9	120 - 110	L2 1/2x2 1/2x1/4	9.12	4.10	67.3	29.000	0.7519	0.97	21.80	0.045
T11	100 - 90	L2 1/2x2 1/2x1/4	10.56	4.82	78.5	29.000	0.7519	1.55	21.80	0.071
T14	60 - 50	2L2x2x3/16	13.43	6.15	123.7	29.000	0.8616	2.52	24.99	0.101
T18	20 - 10	2L2x2x3/16	16.29	7.60	152.0	29.000	0.8616	6.08	24.99	0.243
T19	10 - 0	2L2 1/2x2 1/2x1/4	17.01	7.96	127.5	29.000	1.5037	16.90	43.61	0.388

### Secondary Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	180 - 170	L2x2x3/16	6.00	5.28	111.0	29.000	0.4308	0.78	12.49	0.063
T7	140 - 130	L2x2x1/4	8.03	7.53	148.4	21.600	0.9380	1.46	20.26	0.072

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P/P <sub>a</sub>
T8	130 - 120	L2x2x1/4	8.75	7.82	162.6	29.000	0.5629	1.81	16.32	0.111
T9	120 - 110	L2x2x3/16	9.47	8.54	174.4	29.000	0.4308	2.20	12.49	0.176
T10	110 - 100	L2x2x1/4	10.19	9.26	190.9	29.000	0.5629	2.61	16.32	0.160
T12	90 - 80	L2 1/2x2 1/2x1/4	11.62	10.53	171.0	29.000	0.7519	3.46	21.80	0.159
T15	50 - 40	L3 1/2x3 1/2x1/4	14.49	13.36	151.8	29.000	1.1269	5.10	32.68	0.156
T16	40 - 30	L3 1/2x3 1/2x1/4	15.21	14.12	160.1	29.000	1.1269	5.48	32.68	0.168
T17	30 - 20	L3 1/2x3 1/2x1/4	15.93	14.83	168.0	29.000	1.1269	5.90	32.68	0.180
T18	20 - 10	L3 1/2x3 1/2x1/4	16.65	15.55	175.9	29.000	1.1269	6.17	32.68	0.189

### Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P/P <sub>a</sub>
T1	180 - 170	L2x2x3/16	6.00	5.28	111.0	29.000	0.4308	0.51	12.49	0.040
T2	170 - 163.573	L2x2x3/16	6.00	5.28	111.0	29.000	0.4308	1.25	12.49	0.100
T3	163.573 - 159.049	L2x2x3/16	6.00	5.16	108.6	29.000	0.4308	1.52	12.49	0.122
T6	150 - 140	L2 1/2x2 1/2x3/16	6.97	6.13	101.1	29.000	0.5710	1.05	16.56	0.064
T7	140 - 130	L2 1/2x2 1/2x3/16	7.69	3.42	56.1	29.000	0.5710	0.90	16.56	0.054
T13	80 - 60	L2 1/2x2 1/2x1/4	11.99	5.45	88.4	29.000	0.7519	1.08	21.80	0.050
T16	40 - 30	2L2x2x3/16	14.86	6.86	137.6	29.000	0.8616	3.04	24.99	0.122

### Redundant Horizontal (1) Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P/P <sub>a</sub>
T19	10 - 0	L2 1/2x2 1/2x3/16	4.25	3.92	60.5	21.600	0.9020	6.40	19.48	0.329

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### Redundant Diagonal (1) Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T19	10 - 0	L2 1/2x2 1/2x3/16	6.45	5.92	91.4	21.600	0.9020	10.47	19.48	0.537 ✓

### Redundant Hip (1) Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T19	10 - 0	L2 1/2x2 1/2x3/16	6.01	6.01	92.8	21.600	0.9020	0.01	19.48	0.000 ✓

\* DL controls

### Redundant Sub-Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T19	10 - 0	L3x3x5/16	8.86	8.86	115.4	21.600	1.7800	12.84	38.45	0.334 ✓

### Inner Bracing Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T7	140 - 130	L2x2x3/16	5.44	5.44	105.8	21.600	0.7150	0.17	15.44	0.011 ✓
T9	120 - 110	L2 1/2x2x3/16	6.45	6.45	129.1	21.600	0.8090	0.11	17.47	0.006 ✓
T11	100 - 90	L2 1/2x2x3/16	7.47	7.47	149.4	21.600	0.8090	0.12	17.47	0.007 ✓
T13	80 - 60	2L2x2x3/16	8.48	8.48	164.9	21.600	1.4300	0.16	30.89	0.005 ✓
T14	60 - 50	2L2x2x3/16	9.49	9.49	184.6	21.600	1.4300	0.15	30.89	0.005 ✓
T16	40 - 30	2L2x2x3/16	10.51	10.51	204.4	21.600	1.4300	0.20	30.89	0.007 ✓
T18	20 - 10	2L2x2 1/2x3/16	11.52	11.52	230.4	21.600	1.6200	0.08	34.99	0.002 ✓
T19	10 - 0	2L2x2 1/2x3/16	12.03	12.03	240.6	21.600	1.6200	0.17	34.99	0.005 ✓

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
										✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
T1	180 - 170	Leg	L3 1/2x3 1/2x3/8	1	-6.92	48.00	14.4	Pass
T2	170 - 163.573	Leg	L5x5x5/16	21	-21.37	61.52	34.7	Pass
T3	163.573 - 159.049	Leg	L5x5x5/16	38	-36.54	70.30	52.0	Pass
T4	159.049 - 154.524	Leg	L5x5x5/16	54	-48.73	70.30	69.3	Pass
T5	154.524 - 150	Leg	L5x5x5/16	66	-58.08	70.30	82.6	Pass
T6	150 - 140	Leg	L5x5x3/8	78	-81.08	83.56	97.0	Pass
T7	140 - 130	Leg	L6x6x1/2	102	-97.27	138.47	70.2	Pass
T8	130 - 120	Leg	L6x6x1/2	127	-120.85	138.60	87.2	Pass
T9	120 - 110	Leg	L6x6x3/4	143	-146.56	203.15	72.1	Pass
T10	110 - 100	Leg	L6x6x3/4	170	-173.77	203.29	85.5	Pass
T11	100 - 90	Leg	L8x8x3/4	186	-202.51	239.94	84.4	Pass
T12	90 - 80	Leg	L8x8x3/4	207	-230.26	292.58	78.7	Pass
T13	80 - 60	Leg	L8x8x1 w/ 1/2x7 Plates	223	-287.22	542.49	52.9	Pass
T14	60 - 50	Leg	L8x8x1-1/8 w/ 1/2x7 Plates	252	-314.06	584.58	53.7	Pass
T15	50 - 40	Leg	L8x8x1-1/8 w/ 1/2x7 Plates	273	-339.75	641.95	52.9	Pass
T16	40 - 30	Leg	L8x8x1 1/8	289	-365.07	428.21	85.3	Pass
T17	30 - 20	Leg	L8x8x1 1/8	314	-392.79	428.28	91.7	Pass
T18	20 - 10	Leg	L8x8x1 1/8	330	-411.29	428.35	96.0	Pass
T19	10 - 0	Leg	L8x8x1 1/8	355	-426.58	429.80	99.3	Pass
T1	180 - 170	Diagonal	L2 1/2x2 1/2x3/16	15	-6.55	10.61	61.7	Pass
T2	170 - 163.573	Diagonal	L2 1/2x2 1/2x3/16	30	-7.13	15.14	47.1	Pass
T3	163.573 - 159.049	Diagonal	L2x2x3/16	50	-5.90	11.11	53.1	Pass
T4	159.049 - 154.524	Diagonal	L2 1/2x2x3/16	60	-6.15	13.08	47.0	Pass
T5	154.524 - 150	Diagonal	L2 1/2x2x3/16	69	-6.40	12.69	50.4	Pass
T6	150 - 140	Diagonal	L2 1/2x2x3/16	85	-6.84	11.33	60.4	Pass
T7	140 - 130	Diagonal	L3x2 1/2x1/4	115	-9.13	13.64	67.0	Pass
T8	130 - 120	Diagonal	L3x3x1/4	134	-10.76	17.06	63.1	Pass
T9	120 - 110	Diagonal	L3x3x1/4	156	-11.24	16.19	69.4	Pass
T10	110 - 100	Diagonal	L3 1/2x3x1/4	177	-12.55	18.37	68.3	Pass
T11	100 - 90	Diagonal	L3 1/2x3x1/4	203	-13.16	17.40	75.6	Pass
T12	90 - 80	Diagonal	L3 1/2x3x1/4	215	-13.97	16.47	84.8	Pass
T13	80 - 60	Diagonal	2L2 1/2x2x3/16	240	-14.93	21.54	69.3	Pass
T14	60 - 50	Diagonal	2L2 1/2x2x3/16	269	-14.48	20.20	71.7	Pass
T15	50 - 40	Diagonal	2L2 1/2x2x3/8	281	-15.89	35.82	44.4	Pass
T16	40 - 30	Diagonal	2L2 1/2x2x3/8	306	-16.23	34.00	47.7	Pass
T17	30 - 20	Diagonal	2L2 1/2x2x3/8	322	-14.94	32.28	46.3	Pass
T18	20 - 10	Diagonal	2L2 1/2x2x3/8	344	-20.29	30.67	66.1	Pass
T19	10 - 0	Diagonal	2L2 1/2x2 1/2x1/4	386	-21.38	36.82	58.1	Pass
T9	120 - 110	Horizontal	L2 1/2x2 1/2x1/4	149	-1.16	18.50	6.3	Pass
T11	100 - 90	Horizontal	L2 1/2x2 1/2x1/4	190	-1.65	16.57	9.9	Pass
T14	60 - 50	Horizontal	2L2x2x3/16	255	2.52	33.31	7.6	Pass
T18	20 - 10	Horizontal	2L2x2x3/16	333	6.08	33.31	18.2	Pass
T19	10 - 0	Horizontal	2L2 1/2x2 1/2x1/4	382	-16.66	31.13	53.5	Pass
T1	180 - 170	Secondary Horizontal	L2x2x3/16	20	-0.80	7.10	11.3	Pass
T7	140 - 130	Secondary Horizontal	L2x2x1/4	122	-1.46	5.06	28.8	Pass
T8	130 - 120	Secondary Horizontal	L2x2x1/4	138	-1.81	4.75	38.2	Pass

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> 180' Lattice Tower - CSP	<b>Page</b> 62 of 63
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	<b>Client</b> Sprint	<b>Designed by</b> MCD

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail	
T9	120 - 110	Secondary Horizontal	L2x2x3/16	163	-2.20	3.17	69.3	Pass	
T10	110 - 100	Secondary Horizontal	L2x2x1/4	181	-2.61	3.59	72.6	Pass	
T12	90 - 80	Secondary Horizontal	L2 1/2x2 1/2x1/4	219	-3.46	5.38	64.2	Pass	
T15	50 - 40	Secondary Horizontal	L3 1/2x3 1/2x1/4	284	-5.10	9.15	55.7	Pass	
T16	40 - 30	Secondary Horizontal	L3 1/2x3 1/2x1/4	309	-5.48	8.35	65.7	Pass	
T17	30 - 20	Secondary Horizontal	L3 1/2x3 1/2x1/4	325	-5.90	7.69	76.7	Pass	
T18	20 - 10	Secondary Horizontal	L3 1/2x3 1/2x1/4	350	-6.17	7.11	86.9	Pass	
T1	180 - 170	Top Girt	L2x2x3/16	5	0.51	16.65	3.0	Pass	
T2	170 - 163.573	Top Girt	L2x2x3/16	27	-0.73	6.76	10.8	Pass	
T3	163.573 - 159.049	Top Girt	L2x2x3/16	42	-0.90	6.98	12.9	Pass	
T6	150 - 140	Top Girt	L2 1/2x2 1/2x3/16	84	-0.91	9.49	9.5	Pass	
T7	140 - 130	Top Girt	L2 1/2x2 1/2x3/16	106	-0.92	15.38	6.0	Pass	
T13	80 - 60	Top Girt	L2 1/2x2 1/2x1/4	225	-0.87	14.00	6.2	Pass	
T16	40 - 30	Top Girt	2L2x2x3/16	292	3.04	33.31	9.1	Pass	
T19	10 - 0	Redund Horz 1 Bracing	L2 1/2x2 1/2x3/16	378	-6.40	14.43	44.4	Pass	
T19	10 - 0	Redund Diag 1 Bracing	L2 1/2x2 1/2x3/16	385	-6.38	8.70	73.3	Pass	
T19	10 - 0	Redund Hip 1 Bracing	L2 1/2x2 1/2x3/16	372	-0.03	8.44	0.3	Pass	
T19	10 - 0	Redund Sub Horz Bracing	L3x3x5/16	389	-7.43	10.86	68.4	Pass	
T7	140 - 130	Inner Bracing	L2x2x3/16	112	-0.17	5.19	3.3	Pass	
T9	120 - 110	Inner Bracing	L2 1/2x2x3/16	151	-0.11	4.90	2.3	Pass	
T11	100 - 90	Inner Bracing	L2 1/2x2x3/16	192	-0.12	3.66	3.3	Pass	
T13	80 - 60	Inner Bracing	2L2x2x3/16	229	-0.16	10.46	1.5	Pass	
T14	60 - 50	Inner Bracing	2L2x2x3/16	258	-0.15	8.35	1.8	Pass	
T16	40 - 30	Inner Bracing	2L2x2x3/16	297	-0.20	6.82	2.9	Pass	
T18	20 - 10	Inner Bracing	2L2x2 1/2x3/16	336	-0.06	6.07	1.0	Pass	
T19	10 - 0	Inner Bracing	2L2x2 1/2x3/16	395	-0.20	5.57	3.5	Pass	
							Summary		
							Leg (T19)	99.3	Pass
							Diagonal (T12)	84.8	Pass
							Horizontal (T19)	53.5	Pass
							Secondary Horizontal (T18)	86.9	Pass
							Top Girt (T3)	12.9	Pass
							Redund Horz 1 Bracing (T19)	44.4	Pass
							Redund Diag 1 Bracing (T19)	73.3	Pass
							Redund Hip 1 Bracing (T19)	0.3	Pass
							Redund Sub Horz Bracing (T19)	68.4	Pass
							Inner Bracing (T19)	3.5	Pass
							Bolt Checks	56.9	Pass

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	<b>Client</b> Sprint	<b>Designed by</b> MCD

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
<b>RATING =</b>							<b>99.3</b>	<b>Pass</b>

# ANCHOR BOLT EVALUATION

Job	<u>180' Self-Supporting Lattice Tower - Wilton, CT</u>	Project No.	<u>TWS-015</u>	Sheet	<u>1</u>	of	<u>3</u>
Description	<u>Anchor Bolt Evaluation</u>	Computed by	<u>MCD</u>	Date	<u>05/14/14</u>		
		Checked by	<u>                    </u>	Date	<u>                    </u>		

## ANCHOR BOLT ANALYSIS

### Input Data

#### Max Pier Reactions:

Uplift:	<u>Uplift := 404 kips</u>	<i>user input</i>
Shear:	<u>Shear := 43 kips</u>	<i>user input</i>
Compression:	<u>Compression := 453 kips</u>	<i>user input</i>

#### Anchor Bolt Data:

Use ASTM A36

Number of Anchor Bolts = N	<u>N := 4</u>	<i>user input</i>
Bolt Ultimate Strength:	<u>F<sub>u</sub> := 58 ksi</u>	<i>user input</i>
Bolt Yield Strength:	<u>F<sub>y</sub> := 36 ksi</u>	<i>user input</i>
Bolt Modulus:	<u>E := 29000 ksi</u>	<i>user input</i>
Thickness of Anchor Bolts	<u>D := 2.5 in</u>	<i>user input</i>
Threads per Inch:	<u>n := 4</u>	<i>user input</i>
Coefficient of Friction:	<u>μ := 0.55</u>	<i>user input</i> (for baseplate with grout ASCE 10-97)



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Description	Anchor Bolt Evaluation	Computed by	MCD	Date	05/14/14		
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## Anchor Bolt Area:

Gross Area of Bolt:

$$A_g := \frac{\pi}{4} \cdot D^2 \qquad A_g = 4.909 \text{ in}^2$$

Net Area of Bolt:

$$A_n := \frac{\pi}{4} \cdot \left( D - \frac{0.9743 \cdot \text{in}}{n} \right)^2 \qquad A_n = 3.999 \text{ in}^2$$

## Check Tensile Forces:

Maximum Tensile Force (Gross Area):

$$\text{AllowableTension} := 1.33 \cdot (0.33 \cdot A_g \cdot F_u) \qquad \text{AllowableTension} = 125.0 \text{ kips}$$

Note: 1.33 increase allowed per TIA/EIA

Maximum Tensile Force (Net Area):

$$F_{\text{net.area}} := 1.33 \cdot (0.60 \cdot A_n \cdot F_y) \qquad F_{\text{net.area}} = 114.9 \text{ kips}$$

Note: 1.33 increase allowed per TIA/EIA

Applied Tension:

$$\text{MaxTension} := \frac{\text{Uplift}}{N} \qquad \text{MaxTension} = 101.0 \text{ kips}$$

Check Stresses:

$$\frac{\text{MaxTension}}{F_{\text{net.area}}} = 0.88$$

$$\text{Condition1} := \text{if} \left( \frac{\text{MaxTension}}{F_{\text{net.area}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition1 = "OK"

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## Check Anchor Bolt Area:

Based on the ASCE 10-97 Design of Latticed Steel Transmission Structures

Required Area:

$$A_{s1} := \frac{\text{Uplift}}{F_y} + \frac{\text{Shear}}{\mu \cdot 0.85 \cdot F_y} \quad A_{s1} = 13.8 \cdot \text{in}^2$$

$$A_{s2} := \left| \frac{\text{Shear} - (0.3 \cdot \text{Compression})}{\mu \cdot 0.85 \cdot F_y} \right| \quad A_{s2} = 5.5 \cdot \text{in}^2$$

Provided Area:

$$A_{\text{provided}} := A_n \cdot N \quad A_{\text{provided}} = 16.0 \cdot \text{in}^2$$

$$\text{Condition2} := \text{if} \left( \frac{A_{s1}}{A_{\text{provided}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right) \quad \frac{A_{s1}}{A_{\text{provided}}} = 0.86$$

Condition2 = "OK"

$$\text{Condition3} := \text{if} \left( \frac{A_{s2}}{A_{\text{provided}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right) \quad \frac{A_{s2}}{A_{\text{provided}}} = 0.35$$

Condition3 = "OK"

# FOUNDATION ANALYSIS

Job	180' Self-Supporting Lattice Tower - Wilton, CT	Project No.	TWS-015	Sheet	1 of 10
Description	Foundation Analysis	Computed by	MCD	Date	5/14/14
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## FOOTING WITH FOUR CONCRETE PIERS

### INPUT DATA

#### TOWER FORCES:

Moment Caused by Tower	$M_t := 10769 \cdot \text{kip} \cdot \text{ft}$
Shear at Base of Tower	$S_t := 99 \text{kip}$
Max Compressive Force	$C_t := 453 \text{kip}$
Max Uplift	$U_t := 404 \text{kip}$
Max Pier Shear	$S_p := 43 \text{kip}$
Height of Tower	$H_t := 180 \cdot \text{ft}$
Width of Tower at Base	$W_t := 17.729 \cdot \text{ft}$
Weight of Tower	$WT_t := 1 \cdot \text{kip}$

#### FOOTING DIMENSIONS:

Width of Footing	$W_f := 37 \cdot \text{ft} + 0 \text{ft}$
Overall Depth of Footing	$D_f := 9.5 \text{ft}$
Length of Pier	$L_p := 6.5 \cdot \text{ft} - 0 \text{ft}$
Extension of Pier Above Grade	$L_{pag} := 1.0 \text{ft}$
Square Dimension of Pier	$d_p := 4.0 \text{ft}$
Thickness of Footing	$T_f := 3.0 \text{ft} + 0 \text{ft}$
Reinforcement Cover:	$Cvr := 3 \text{in}$
Ftg. Edge To Pier CL:	$X_t := 8.635 \text{ft}$

NOTE: Weight of Tower is incorporated into the other loads listed above and is therefore set equal to one for programming.

#### MATERIAL PROPERTIES:

Compressive Strength of Concrete	$f_c := 3000 \cdot \text{psi}$	Unit Weight of Soil	$\gamma_s := 100 \text{pcf}$
Yield Strength of Steel Reinforcement	$f_y := 60000 \cdot \text{psi}$	Unit Weight of Concrete	$\gamma_c := 150 \cdot \text{pcf}$
Internal Friction Angle of Soil	$\phi_s := 30 \cdot \text{deg}$	Depth to Neglect	$n := 1.5 \text{ft}$
Allowable Bearing Capacity	$q_s := 3400 \cdot \text{psf}$	Cohesion of Clay Type Soil	$c_{\text{all}} := 0 \cdot \text{ksf}$
Stability Factor of Safety	$FS_{\text{req}} := 2.0$	Note: Use 0 for Sandy Soil	

Coefficient of Lateral Soil Pressure  $K_p := \frac{1 + \sin(\phi_s)}{1 - \sin(\phi_s)}$   $K_p = 3$

What is Position of Center of Tower with respect to Center of Pad?   
 1=Offset      2=Not Offset      Pos<sub>tower</sub> := 1

#### PIER REINFORCEMENT:

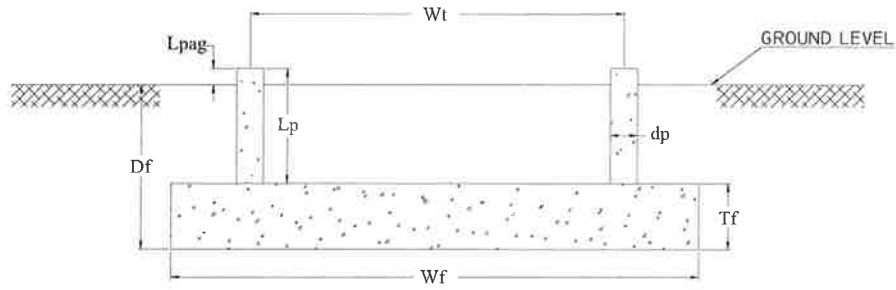
Bar Size	$BS_{\text{pier}} := 9$	Bar Diameter	$d_{\text{bpier}} := 1.128 \cdot \text{in}$
Number of Bars	$NB_{\text{pier}} := 24$	Bar Area	$A_{\text{bpier}} := 1.00 \cdot \text{in}^2$

#### PAD REINFORCEMENT:

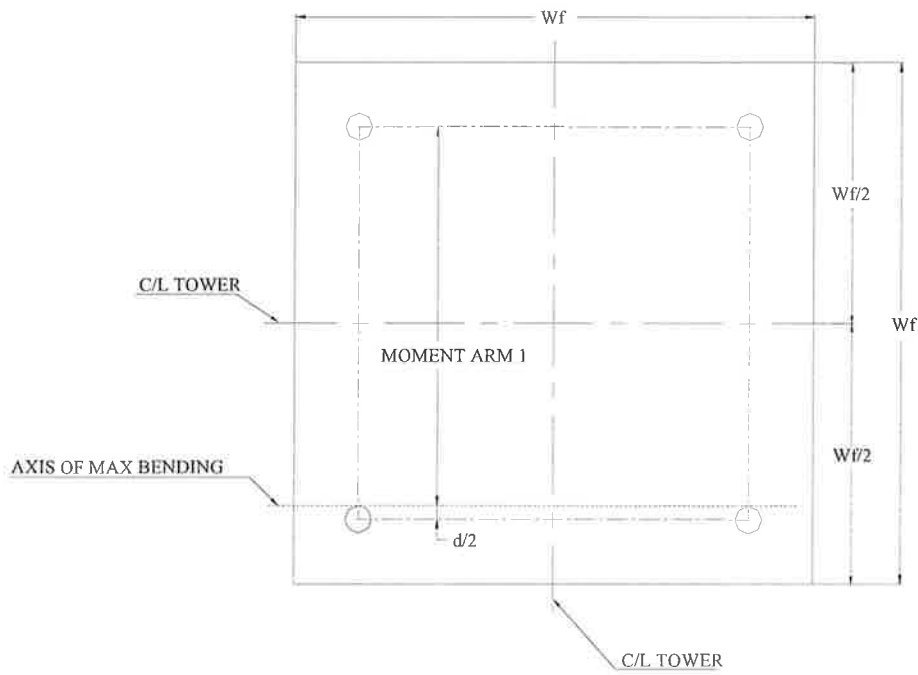
Bar Size	$BS_{\text{pad}} := 9$	Bar Diameter	$d_{\text{bpad}} := 1.128 \cdot \text{in}$
Number of Bars	$NB_{\text{pad}} := 42$	Bar Area	$A_{\text{bpad}} := 1.00 \cdot \text{in}^2$

Job 180' Self-Supporting Lattice Tower - Wilton, CTProject No. TWS-015Sheet 2 of 10Description Foundation AnalysisComputed by MCDDate 5/14/14Checked by     Date     

## Typical Footing Plan and Elevation:



## ELEVATION



## PLAN

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## STABILITY OF FOOTING

### Passive Pressure:

Pressure at Neglect:  $P_{pn} := K_p \cdot \gamma_s \cdot n + c \cdot 2 \cdot \sqrt{K_p}$   $P_{pn} = 0.45 \cdot \text{ksf}$

Pressure at Footing Top:  $P_{pt} := K_p \cdot \gamma_s \cdot (D_f - T_f) + c \cdot 2 \cdot \sqrt{K_p}$   $P_{pt} = 1.95 \cdot \text{ksf}$

Pressure at Top:  $P_{top} := \text{if}[n < (D_f - T_f), P_{pt}, P_{pn}]$   $P_{top} = 1.95 \cdot \text{ksf}$

Pressure at Bottom:  $P_{bot} := K_p \cdot \gamma_s \cdot D_f + c \cdot 2 \cdot \sqrt{K_p}$   $P_{bot} = 2.85 \cdot \text{ksf}$

Average Pressure:  $P_{ave} := \frac{P_{top} + P_{bot}}{2}$   $P_{ave} = 2.4 \cdot \text{ksf}$

### Soil Shear:

Effective Soil Depth:  $T_{pp} := \text{if}[n < (D_f - T_f), T_f, (D_f - n)]$   $T_{pp} = 3 \cdot \text{ft}$

Area of Resistance:  $A_{pp} := W_f \cdot T_{pp}$   $A_{pp} = 111 \cdot \text{ft}^2$

Shear Resistance:  $S_u := P_{ave} \cdot A_{pp}$   $S_u = 266.4 \cdot \text{kip}$

### Stabilizing Dead Load:

Weight of Concrete Pad:  $WT_c := (W_f^2 \cdot T_f) \cdot \gamma_c$   $WT_c = 616.05 \cdot \text{kip}$

Weight of Soil above Footing:  $\text{Depth} := \begin{cases} D_f - n - T_f & \text{if } n < (D_f - T_f) \\ 0 & \text{otherwise} \end{cases}$   $\text{Depth} = 5 \cdot \text{ft}$

$WT_{s1} := W_f^2 \cdot \text{Depth} \cdot \gamma_s$   $WT_{s1} = 684.5 \cdot \text{kip}$

Weight of Soil Wedge at Back Face:  $WT_{s2} := \left[ \frac{(D_f - n)^2 \cdot \tan(\phi_s)}{2} \cdot W_f \right] \cdot \gamma_s$   $WT_{s2} = 68.3583 \cdot \text{kip}$

Distance to center of Tower Leg from Edge of Footing:  $X_{t1} := \frac{W_f}{2} - \frac{W_t}{2}$   $X_{t2} := \frac{W_f}{2} - \frac{W_t}{2}$   $X_{tw} := \text{if}(\text{Pos}_{tower} = 1, X_{t1}, X_{t2})$

Additional Offset of Footing:  $X_{off1} := \frac{W_f}{2} - \left( \frac{W_t \cdot \cos(30 \cdot \text{deg})}{3} + X_t \right)$   $X_{off2} := 0$

$X_{off} := \text{if}(\text{Pos}_{tower} = 1, X_{off1}, X_{off2})$   $X_{off} = 10.6354 \cdot \text{ft}$

### Stability Analysis:

Resisting Moment:  $M_r := (WT_c + WT_{s1}) \cdot \frac{W_f}{2} + WT_t \left( \frac{W_f}{2} - X_{off} \right) + S_u \cdot \frac{T_{pp}}{3} + WT_{s2} \cdot \left( W_f + \frac{T_{pp} \cdot \tan(\phi_s)}{3} \right)$

$M_r = 26903.1623 \cdot \text{kip} \cdot \text{ft}$

Overturing Moment:  $M_{ot} := M_t + S_t \cdot (L_p + T_f) + WT_t \cdot X_{off}$   $M_{ot} = 11720.1354 \cdot \text{kip} \cdot \text{ft}$

Factor of Safety:  $FS := \frac{M_r}{M_{ot}}$   $FS = 2.3$

$\text{SafetyCheck} := \text{if}(FS > FS_{req}, \text{"Okay"}, \text{"No Good"})$   $\text{SafetyCheck} = \text{"Okay"}$

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## BEARING PRESSURES

### Loading Eccentricity:

Total Axial Load:  $LOAD_{tot} := WT_c + WT_{s1} + WT_t$   $LOAD_{tot} = 1301.55 \cdot \text{kip}$

Total Moment:  $M_{tot} := M_t + S_f(L_p + T_f) + WT_t$   $M_{tot} = 11710.5 \cdot \text{kip} \cdot \text{ft}$

Eccentricity:  $e := \frac{M_{tot}}{LOAD_{tot}}$   $e = 8.9973 \cdot \text{ft}$

Dist. From Ftg. CL to Kern Edge:  $X_k := \frac{W_f}{6}$   $X_k = 6.1667 \cdot \text{ft}$

### Calculate Soil Pressures:

Maximum Contact Pressure:

$$P_{max} := \begin{cases} \frac{LOAD_{tot}}{W_f^2} \cdot \left(1 + \frac{6 \cdot e}{W_f}\right) & \text{if } e \leq X_k \\ \frac{2 \cdot LOAD_{tot}}{3 \cdot W_f \cdot \left(\frac{W_f}{2} - e\right)} & \text{otherwise} \end{cases}$$

$P_{max} = 2.4679 \cdot \text{ksf}$

Minimum Contact Pressure:

$$P_{min} := \begin{cases} \frac{LOAD_{tot}}{W_f^2} \cdot \left(1 - \frac{6 \cdot e}{W_f}\right) & \text{if } e \leq X_k \\ 0 \text{ksf} & \text{otherwise} \end{cases}$$

$P_{min} = 0 \cdot \text{ksf}$

Length of Applied Pressure:

$$X_p := \begin{cases} W_f & \text{if } e \leq X_k \\ 3 \cdot \left(\frac{W_f}{2} - e\right) & \text{otherwise} \end{cases}$$

$X_p = 28.508 \cdot \text{ft}$

Pressure Slope:

$$m_p := \frac{P_{max} - P_{min}}{X_p}$$

$m_p = 0.0866 \cdot \text{ksf}$

### Soil Bearing Pressure Check:

BearingStatus := if( $P_{max} < q_s$ , "Okay", "No Good")

BearingStatus = "Okay"

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## Concrete Bearing Capacity (ACI 10.17):

$$(ACI 9.3.2.2) \quad \phi_c := 0.75$$

$$P_b := \phi_c \cdot 0.85 \cdot f_c \cdot \frac{d_p^2 \cdot \pi}{4} \quad P_b = 3460.7785 \cdot \text{kip}$$

$$\text{BearingCheck} := \text{if}(P_b > C_t, \text{"Okay"}, \text{"No Good"}) \quad \text{BearingCheck} = \text{"Okay"}$$

## SHEAR STRENGTH OF CONCRETE

### Beam (One-Way) Shear Action (ACI 11.3.1.1):

$$\text{Load Factor: (EIA 3.1.1)} \quad LF := \text{if}\left[H_t \leq 700 \cdot \text{ft}, 1.3, \text{if}\left[H_t \geq 1200, 1.7, 1.3 + \left(\frac{H_t - 700}{1200 - 700}\right) \cdot 0.4\right]\right] \quad LF = 1.3$$

$$\text{"d" Distance:} \quad d := T_f - C_{vr} - .5 \cdot \text{in} \quad d = 32.5 \cdot \text{in}$$

$$\text{Factored Pressure at "d" Distance:} \quad P_d := LF \cdot \left[ P_{\max} - \left( X_t - \frac{d_p}{2} - d \right) \cdot m_p \right] \quad P_d = 2.6537 \cdot \text{ksf}$$

$$\text{Factored Pressure at Edge:} \quad P_{\text{edge}} := LF \cdot P_{\max} \quad P_{\text{edge}} = 3.2082 \cdot \text{ksf}$$

$$\text{Average Pressure:} \quad P_{\text{ave}} := \frac{P_d + P_{\text{edge}}}{2} \quad P_{\text{ave}} = 2.931 \cdot \text{ksf}$$

$$\text{Capacity Reduction Factor: (ACI 9.3.2.3)} \quad \phi_{\text{shear}} := .85$$

$$\text{Applied Shear Force:} \quad V_{\text{req}} := \frac{P_{\text{ave}} \cdot (X_t - 0.5 \cdot d_p - d) \cdot W_f}{\phi_c} \quad V_{\text{req}} = 628.6289 \cdot \text{kip}$$

$$\text{Available Shear: (ACI 11.3.1.1)} \quad V_{\text{Avail}} := 2 \cdot \sqrt{f_c \cdot \text{psi}} \cdot W_f \cdot d \quad V_{\text{Avail}} = 1580.7273 \cdot \text{kip}$$

$$\text{Check Capacity:} \quad \text{BeamShearCheck} := \text{if}(V_{\text{req}} < V_{\text{Avail}}, \text{"Okay"}, \text{"No Good"})$$

$$\text{BeamShearCheck} = \text{"Okay"}$$



Job	180' Self-Supporting Lattice Tower - Wilton, CT	Project No.	TWS-015	Sheet	6 of 10
Description	Foundation Analysis	Computed by	MCD	Date	5/14/14
		Checked by		Date	

## Punching (Two-Way) Shear Action (ACI 11.12.2.1):

Critical Perimeter:	$b_o := 4(d_p + d)$	$b_o = 26.8333 \cdot \text{ft}$
Capacity Reduction Factor: (ACI 9.3.2.3)	$\phi_{max} := .85$	$C_t = 453 \cdot \text{kip}$
Factored Maximum Punching Shear Force	$FL := \frac{LF \cdot C_t}{\phi_c}$	$FL = 692.8235 \cdot \text{kip}$
Available Shear:	$V_{Avail} := 4 \cdot \sqrt{f_c \text{ psi}} \cdot b_o \cdot d$	$V_{Avail} = 2292.7666 \cdot \text{kip}$
Check Capacity:	PunchingShearCheck := if( $V_{req} < V_{Avail}$ , "Okay", "No Good")	
	PunchingShearCheck = "Okay"	

## **BENDING**

### Maximim Bending Moment:

Distance From Edge of FTG To Face of Pier:	$X_b := \frac{W_f}{2} - e - \frac{d_p}{2}$	$X_b = 7.5027 \cdot \text{ft}$
---	--	--------------------------------

### Moment Due To Overturning:

Factored Pressure at "d" Distance:	$P_{face} := LF \cdot (P_{max} - X_b \cdot m_p)$	$P_{face} = 2.3639 \cdot \text{ksf}$
Factored Pressure at Edge:	$P_{edge} := LF \cdot P_{max}$	$P_{edge} = 3.2082 \cdot \text{ksf}$
Moment Due To Rectangular Loading:	$M_1 := (P_{face} \cdot X_b \cdot W_f) \cdot \left(\frac{1}{2} \cdot X_b\right)$	$M_1 = 2461.674 \cdot \text{kip} \cdot \text{ft}$
Moment Due to Triangular Loading:	$M_2 := \left[\frac{1}{2} \cdot X_b \cdot (P_{edge} - P_{face})\right] \cdot \left(\frac{2}{3} \cdot X_b\right)$	$M_2 = 15.8425 \cdot \text{kip} \cdot \text{ft}$
Sum Moments:	$M_{tot} := M_1 + M_2$	$M_{ot} = 2477.5165 \cdot \text{kip} \cdot \text{ft}$

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### Moment Due To Uplift:

Pier Forces:  $M_{nT} := LF \cdot \left[ U_t \cdot \left( W_f - 2 \cdot X_b - \frac{d}{2} - d \right) + S_t \cdot (D_f + L_{pag}) \right]$   $M_{nT} = 10769.3407 \cdot \text{kip} \cdot \text{ft}$

Concrete Resistance:  $M_{nS} := \frac{1}{2} \cdot (W_f - X_b - d_p)^2 \cdot (T_f \cdot W_f) \cdot \gamma_s$   $M_{nS} = 3608.1373 \cdot \text{kip} \cdot \text{ft}$

Soil Resistance:  $M_{nC} := \frac{1}{2} \cdot (W_f - X_b - d_p)^2 \cdot (T_f \cdot W_f) \cdot \gamma_c$   $M_{nC} = 5412.2059 \cdot \text{kip} \cdot \text{ft}$

Sum Moments  $M_{uplift} := M_{nT} - M_{nS} - M_{nC}$   $M_{uplift} = 1748.9976 \cdot \text{kips} \cdot \text{ft}$

### Select Controlling Moment:

$$M_u := \begin{cases} M_{ot} & \text{if } M_{ot} \geq M_{uplift} \\ M_{uplift} & \text{otherwise} \end{cases}$$

$M_u = 2477.5165 \cdot \text{kips} \cdot \text{ft}$

Strength Reduction Factor:  
(ACI 9.3.2.2)  $\phi_m := .90$

Design Moment:  $M_n := \frac{M_u}{\phi_m}$   $M_n = 2752.7961 \cdot \text{kips} \cdot \text{ft}$

### Size Reinforcing Steel:

Effective Width:  $b_{eff} := W_f$   $b_{eff} = 444 \cdot \text{in}$

Stress Block:  $a := d \cdot \left( 1 - \sqrt{1 - 2.3529 \cdot \frac{M_n}{f_c \cdot b_{eff} \cdot d^2}} \right)$   $a = 0.9105 \cdot \text{in}$

Steel Req'd For Bending:  $A_s := \frac{M_n}{f_y \cdot \left( d - \frac{a}{2} \right)}$   $A_s = 17.1809 \cdot \text{in}^2$

Reinforcement Ratio:  $\rho := \frac{A_s}{b_{eff} \cdot d}$   $\rho = 0.0012$

Steel Req'd For Temperature and Shrinkage:  
(ACI 7.12.2.1b)  $\rho_{sh} := \text{if}(f_y \geq 60000 \cdot \text{psi}, 0.0018, 0.0020)$   $\rho_{sh} = 0.0018$

$A_s := \text{if}(\rho \geq \rho_{sh}, A_s, \rho_{sh} \cdot b_{eff} \cdot d)$   $A_s = 25.974 \cdot \text{in}^2$

$A_{s_{prov}} := A_{bpad} \cdot NB_{pad}$   $A_{s_{prov}} = 42 \cdot \text{in}^2$

Check Provided Steel:  $\text{PadReinforcement} := \text{if}(A_{s_{prov}} > A_s, \text{"Okay"}, \text{"No Good"})$   
 $\text{PadReinforcement} = \text{"Okay"}$

Job	180' Self-Supporting Lattice Tower - Wilton, CT	Project No.	TWS-015	Sheet	8 of 10
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## DEVELOPMENT LENGTH OF PAD REINFORCEMENT

### TENSION (ACI 12.2.3)

Bar Spacing:  $B_{sPad} := \frac{W_f - 2 \cdot C_{vr} - NB_{pad} \cdot d_{bpad}}{NB_{pad} - 1}$   $B_{sPad} = 9.5274 \cdot \text{in}$

Development Length Factors:

Reinforcement Location Factor	$\alpha := 1.0$
Coating Factor	$\beta := 1.0$
Concrete strength Factor	$\lambda := 1.0$
Reinforcement Size Factor	$\gamma := 1.0$

Spacing or Cover Dimension:  $c := \text{if} \left( C_{vr} < \frac{B_{sPad}}{2}, C_{vr}, \frac{B_{sPad}}{2} \right)$   $c = 3 \cdot \text{in}$

Transverse Reinforcement Index: As allowed by ACI 12.2.4  $k_{tr} := 0$

$$L_{dbt} := \frac{3}{40} \cdot \frac{f_y}{\sqrt{f_c \text{ psi}}} \cdot \frac{\alpha \cdot \beta \cdot \gamma \cdot \lambda}{c + k_{tr}} \cdot d_{bpad}$$

$L_{dbt} = 34.8457 \cdot \text{in}$   
 $L_{dbmin} := 12 \cdot \text{in}$

Minimum Development Length: (ACI 12.2.1)  $L_{dbtCheck} := \text{if}(L_{dbt} \geq L_{dbmin}, \text{"Use L.dbt"}, \text{"Use L.dbmin"})$   $L_{dbtCheck} = \text{"Use L.dbt"}$

Available Length in Pad:  $L_{Pad} := \frac{W_f}{2} - \frac{W_t}{2} - C_{vr}$   $L_{Pad} = 112.626 \cdot \text{in}$

$L_{padTension} := \text{if}(L_{Pad} > L_{dbt}, \text{"Okay"}, \text{"No Good"})$   $L_{padTension} = \text{"Okay"}$

### REINFORCEMENT IN PIER

Pier Area:  $A_p := \frac{\pi \cdot d_p^2}{4}$   $A_p = 1809.5574 \cdot \text{in}^2$

(ACI 10.8.4 and 10.9.1)  $A_{smin} := 0.01 \cdot 0.5 \cdot A_p$   $A_{smin} = 9.0478 \cdot \text{in}^2$

$A_{sprov} := NB_{pier} \cdot A_{bpier}$   $A_{sprov} = 24 \cdot \text{in}^2$

SteelAreaCheck :=  $\text{if}(A_{sprov} > A_{smin}, \text{"Okay"}, \text{"No Good"})$   $\text{SteelAreaCheck} = \text{"Okay"}$

NOTE: Anchor Bolts are not accounted for in reinforcement calculation and will provide additional reinforcement to satisfy minimum requirement of steel.

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		Checked by		Date	

Bar Spacing In Pier:  $B_{sPier} := \frac{d_p \cdot \pi}{NB_{pier}} - d_{bpier}$   $B_{sPier} = 5.1552 \text{ in}$

Diameter of Reinforcement Cage:  $Diam_{cage} := d_p - 2 \cdot C_{vr}$   $Diam_{cage} = 42 \text{ in}$

Maximum Moment in Pier:  $M_p := (S_p \cdot L_p) \cdot LF$   $M_p = 4360 \text{ kips-in}$

Pier Check evaluated from outside program and results are listed below;

(defined variables)  $(f_c \ f_y \ c1 \ Spiral) = (3 \ 60 \ 4 \ 0)$

The required input is column diameter in inches, number of reinforcing bars, bar size number, factored axial load in kips and moment in kip inches:  $(D \ N_{\text{bar}} \ n_{\text{bar}} \ P_u \ M_{xu}) := (48 \ 24 \ 9 \ 144 \ 16045)$

Clears any previous output:  $(\phi P_n \ \phi M_{xn} \ f_{sp} \ \rho) := (0 \ 0 \ 0 \ 0)$

$$(\phi P_n \ \phi M_{xn} \ f_{sp} \ \rho) := \phi P'_n (D, N, n, P_u, M_{xu})^T$$

The Output is given as useable axial load in kips, moment capacity in kip inches, splicing stress in ksi, and reinforcement ratio:  $(\phi P_n \ \phi M_{xn} \ f_{sp} \ \rho) = (208.5987 \ 23242.8205 \ -60 \ 0.0133)$

Column size and reinforcement may be changed to match capacity to the applied load.

AxialLoadCheck := if( $\phi P_n \geq P_u$ , "Okay", "No Good") AxialLoadCheck = "Okay"

BendingCheck := if( $\phi M_{xn} \geq M_{xu}$ , "Okay", "No Good") BendingCheck = "Okay"

Job	180' Self-Supporting Lattice Tower - Wilton, CT	Project No.	TWS-015	Sheet	10 of 10
Description	Foundation Analysis	Computed by	MCD	Date	5/14/14
		Checked by		Date	

## DEVELOPMENT LENGTH OF PIER REINFORCEMENT

### TENSION (ACI 12.2.3)

Spacing and Cover:  $C_{vr} = 3 \cdot \text{in}$   $B_{sPier} = 5.1552 \cdot \text{in}$

Factors for development:

Reinforcement Location Factor	$\alpha := 1.0$
Coating Factor	$\beta := 1.0$
Concrete strength Factor	$\lambda := 1.0$
Reinforcement Size Factor	$\gamma := 1.0$

Spacing or Cover Dimension:  $c := \text{if} \left( C_{vr} < \frac{B_{sPier}}{2}, C_{vr}, \frac{B_{sPier}}{2} \right) c = 2.5776 \cdot \text{in}$

Transverse Reinforcement: As allowed by ACI 12.2.4  $k_{tr} := 0$

$$L_{dbt} := \frac{3}{40} \cdot \frac{f_y}{\sqrt{f_c \text{ psi}}} \cdot \frac{\alpha \cdot \beta \cdot \gamma \cdot \lambda}{c + k_{tr}} \cdot d_{bpier} \quad L_{dbt} = 40.5561 \cdot \text{in}$$

Minimum Development Length: (ACI 12.2.1)

$$L_{dbmin} := 12 \cdot \text{in}$$

$$L_{dbtCheck} := \text{if} (L_{dbt} \geq L_{dbmin}, \text{"Use L.dbt"}, \text{"Use L.dbmin"}) \quad L_{dbtCheck} = \text{"Use L.dbt"}$$

### COMPRESSION: (ACI 12.3.2)

$$L_{dbc1} := \frac{.02 \cdot d_{bpier} \cdot f_y}{\sqrt{f_c \text{ psi}}} \quad L_{dbc1} = 24.7132 \cdot \text{in}$$

$$L_{dbmin} := 0.0003 \cdot \frac{\text{in}^2}{\text{lb}} \cdot (d_{bpier} \cdot f_y) \quad L_{dbmin} = 20.304 \cdot \text{in}$$

$$L_{dbc} := \text{if} (L_{dbc1} \geq L_{dbmin}, L_{dbc1}, L_{dbmin}) \quad L_{dbc} = 24.7132 \cdot \text{in}$$

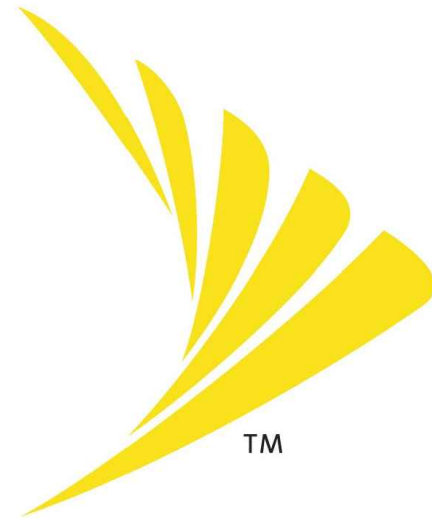
Available Length in Pier:  $L_{pier} := L_p - 3 \cdot \text{in}$   $L_{pier} = 75 \cdot \text{in}$

Available Length in Pad:  $L_{pad} := T_f - 3 \cdot \text{in}$   $L_{pad} = 33 \cdot \text{in}$

Available Length:  $L_{total} := L_{pad} + L_{pier}$   $L_{total} = 108 \cdot \text{in}$

$$L_{tension} := \text{if} (L_{total} > L_{dbt}, \text{"Okay"}, \text{"No Good"}) \quad L_{tension} = \text{"Okay"}$$

$$L_{compression} := \text{if} (L_{total} > L_{dbc}, \text{"Okay"}, \text{"No Good"}) \quad L_{compression} = \text{"Okay"}$$



PROJECT: 2.5 EQUIPMENT DEPLOYMENT  
 SITE NAME: CTS  
 SITE CASCADE: CT03XC360-E  
 SITE ADDRESS: 46 FERNWOOD LANE  
 WILTON, CT 06897  
 SITE TYPE: 180'-0" SELF SUPPORT  
 TOWER



6580 SPRINT PARKWAY  
 OVERLAND PARK, KANSAS 66251



1120 Dallas Street, Sauk City, WI 53583  
 Phone: 608-643-4100 Fax: 608-643-7999  
 www.Ramaker.com



48 SPRUCE STREET  
 OAKLAND, NJ 07346

Certification & Seal:  
 I hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the laws of the State of Connecticut.



Signature: *James R. Skowronski* Date: 8/08/2014

MARK	DATE	DESCRIPTION
A	08/08/14	FINAL CONSTRUCTION DRAWINGS
ISSUE PHASE	FINAL	DATE ISSUED 08/08/2014

PROJECT TITLE:  
 CTS  
 CT03XC360-A

PROJECT INFORMATION:  
 46 FERNWOOD LANE  
 WILTON, CT 06897  
 FAIRFIELD COUNTY

SHEET TITLE:  
 TITLE SHEET

SCALE: NONE

PROJECT NUMBER: 28731  
 SHEET NUMBER: T-1

**SITE INFORMATION**

**PROPERTY OWNER:**  
 THE STATE OF CONNECTICUT DEPARTMENT OF PUBLIC SAFETY DIVISION OF STATE POLICE  
 1111 COUNTY CLUB ROAD  
 MIDDLETOWN, CT 06457

**SITE ADDRESS:**  
 46 FERNWOOD LANE  
 WILTON, CT 06897  
 FAIRFIELD COUNTY

**GEOGRAPHIC COORDINATES:**  
 LATITUDE: 41° 10' 20.7798" (41.1724393 N)  
 LONGITUDE: 73° 26' 3.6954" (-73.4343597 W)

**ZONING JURISDICTION:**  
 THE CONNECTICUT SITING COUNCIL  
 10 FRANKLIN SQUARE  
 NEW BRITAIN, CT 06051

**ZONING DISTRICT:**  
 CSC APPROVED

**POWER COMPANY:**  
 NORTHEAST UTILITIES (CONNECTICUT LIGHT & POWER)  
 PH.: (800) 286-2000

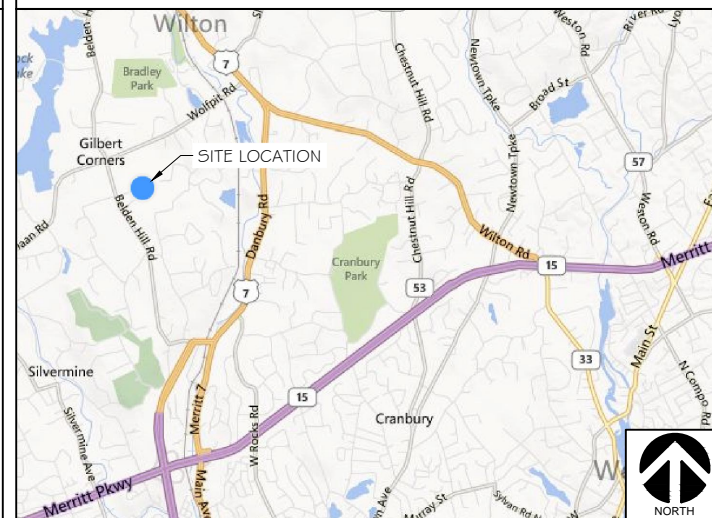
**AAV PROVIDER:**  
 FIBERTECH  
 PH.: (866) 697-5100

**SPRINT CONSTRUCTION MANAGER:**  
 NAME: GARY WOOD  
 PHONE: (860) 940-9168  
 E-MAIL: gary.wood@sprint.com

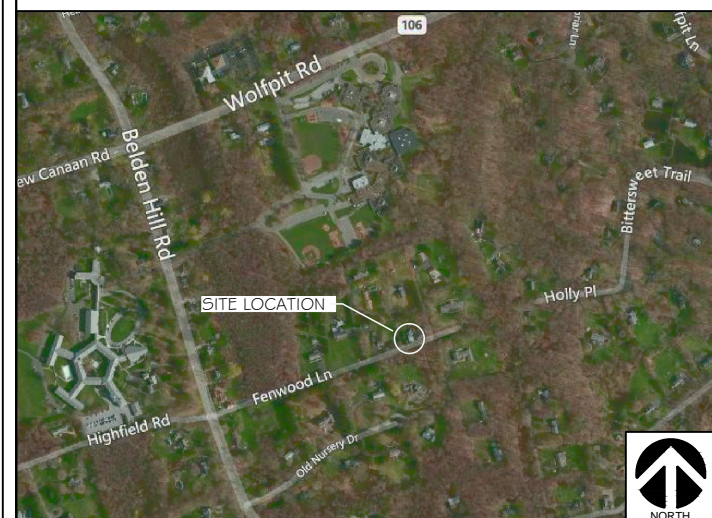
**EQUIPMENT SUPPLIER:**  
 ALCATEL-LUCENT  
 600-700 MOUNTAIN AVENUE  
 MURRAY HILL, NJ 07974  
 PH.: (908) 508-8080

**PLANS PREPARED BY:**  
 RAMAKER & ASSOCIATES, INC.  
 CONTACT: KEITH BOHNSACK, PROJECT MANAGER  
 PH.: (608) 643-4100  
 EMAIL: kbohnsack@ramaker.com

**AREA MAP**



**LOCATION MAP**



**PROJECT DESCRIPTION**

- INSTALL NEW 2.5 EQUIPMENT IN EXISTING BTS CABINET  
 \*(1) RECTIFIER SHELF AND (3) RECTIFIERS  
 \*(1) BASE BAND UNIT
- INSTALL (2) NEW BATTERY STRINGS IN EXISTING BATTERY CABINET
- INSTALL (3) PANEL ANTENNAS
- INSTALL (3) RRH'S ON TOWER
- INSTALL (2) FIBER CABLES AND (3) FIBER JUMPERS
- INSTALL (27) ANTENNA / RRH JUMPERS

**APPLICABLE CODES**

\* ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALLED IN ACCORDANCE WITH THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE CODES.

- INTERNATIONAL BUILDING CODE
- ANSI/TIA-222 STRUCTURAL STANDARD FOR ANTENNA STRUCTURES
- NFPA 780 - LIGHTNING PROTECTION CODE
- NATIONAL ELECTRIC CODE





**SECTION 01 100 - SCOPE OF WORK**

**THE WORK:**  
THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE CONSTRUCTION DRAWINGS AND ASSOCIATED OUTLINE SPECIFICATIONS AND THE SITE SPECIFIC WORK ORDER, DESCRIBE THE WORK TO BE PERFORMED BY THIS CONSTRUCTION CONTRACTOR (SUPPLIER).

**RELATED DOCUMENTS:**

- A. THE REQUIREMENTS OF EACH SECTION OF THIS SPECIFICATION APPLY TO ALL SECTIONS, INDIVIDUALLY AND COLLECTIVELY.
- B. RELATED DOCUMENTS: THE CONTRACTOR SHALL COMPLY WITH THE MOST CURRENT VERSION OF THE FOLLOWING SUPPLEMENTAL REQUIREMENTS FOR INSTALLATION AND TESTING.
  - 1. EN-201 2-001 : (FIBER OPTIC, DC CABLE, AND DC CIRCUIT BREAKER TAGGING STANDARDS)
  - 2. TS-0200 - (TRANSMISSION ANTENNA LINE ACCEPTANCE STANDARDS)
  - 3. EL-0568: (FIBER TESTING POLICY)
  - 4. NP-312-201 : (EXTERIOR GROUNDING SYSTEM TESTING)
  - 5. NP-760-500: ETHERNET, MICROWAVE, TESTING AND ACCEPTANCE

**PRECEDENCE:**

SHOULD CONFLICTS OCCUR BETWEEN THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES AND THE CONSTRUCTION DRAWINGS, INFORMATION ON THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE. NOTIFY SPRINT CONSTRUCTION MANAGER IF THIS OCCURS.

**NATIONALLY RECOGNIZED CODES AND STANDARDS:**

- THE WORK SHALL COMPLY WITH APPLICABLE NATIONAL AND LOCAL CODES AND STANDARDS, LATEST EDITION, AND PORTIONS THEREOF, INCLUDED BUT NOT LIMITED TO THE FOLLOWING:
- A. GR-63-CORE NEBS REQUIREMENTS: PHYSICAL PROTECTION
  - B. GR-78-CORE GENERIC REQUIREMENTS FOR THE PHYSICAL DESIGN AND MANUFACTURE OF TELECOMMUNICATIONS EQUIPMENT.
  - C. GR-1089 CORE, ELECTROMAGNETIC COMPATIBILITY AND ELECTRICAL SAFETY -GENERIC CRITERIA FOR NETWORK TELECOMMUNICATIONS EQUIPMENT.
  - D. NATIONAL FIRE PROTECTION ASSOCIATION CODES AND STANDARDS (NFPA) INCLUDING NFPA 70 (NATIONAL ELECTRICAL CODE - "NEC") AND NFPA 101 (LIFE SAFETY CODE).
  - E. AMERICAN SOCIETY FOR TESTING OF MATERIALS (ASTM)
  - F. INSTITUTE OF ELECTRONIC AND ELECTRICAL ENGINEERS (IEEE)
  - G. AMERICAN CONCRETE INSTITUTE (ACI)
  - H. AMERICAN WIRE PRODUCERS ASSOCIATION (AWPA)
  - I. CONCRETE REINFORCING STEEL INSTITUTE (CRSI)
  - J. AMERICAN ASSOCIATION OF STATE HIGHWAY AND TRANSPORTATION OFFICIALS (AASHTO)
  - K. PORTLAND CEMENT ASSOCIATION (PCA)
  - L. NATIONAL CONCRETE MASONRY ASSOCIATION (NCMA)
  - M. BRICK INDUSTRY ASSOCIATION (BIA)
  - N. AMERICAN WELDING SOCIETY (AWS)
  - O. NATIONAL ROOFING CONTRACTORS ASSOCIATION (NRCA)
  - P. SHEET METAL AND AIR CONDITIONING CONTRACTORS' NATIONAL ASSOCIATION (SMACNA)
  - Q. DOOR AND HARDWARE INSTITUTE (DHI)
  - R. OCCUPATIONAL SAFETY AND HEALTH ACT (OSHA)
  - 5. APPLICABLE BUILDING CODES INCLUDING UNIFORM BUILDING CODE, SOUTHERN BUILDING CODE, BOCA, AND THE INTERNATIONAL BUILDING CODE.

**DEFINITIONS:**

- A. WORK: THE SUM OF TASKS AND RESPONSIBILITIES IDENTIFIED IN THE CONTRACT DOCUMENTS.
- B. COMPANY: "SPRINT"; SPRINT NEXTEL CORPORATION AND ITS OPERATING ENTITIES.
- C. ENGINEER: SYNONYMOUS WITH ARCHITECT & ENGINEER AND "A&E". THE DESIGN PROFESSIONAL HAVING PROFESSIONAL RESPONSIBILITY FOR DESIGN OF THE PROJECT.
- D. CONTRACTOR: CONSTRUCTION CONTRACTOR, SUPPLIER, CONSTRUCTION VENDOR; INDIVIDUAL OR ENTITY WHO AFTER EXECUTION OF A CONTRACT IS BOUND TO ACCOMPLISH THE WORK.
- E. THIRD PARTY VENDOR OR AGENCY: A VENDOR OR AGENCY ENGAGED SEPARATELY BY THE COMPANY, A&E, OR CONTRACTOR TO PROVIDE MATERIALS OR TO ACCOMPLISH SPECIFIC TASKS RELATED TO BUT NOT INCLUDED IN THE WORK.
- F. CONSTRUCTION MANAGER - ALL PROJECTS RELATED COMMUNICATION TO FLOW THROUGH SPRINT REPRESENTATIVE IN CHARGE OF PROJECT.

**SITE FAMILIARITY:**

CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING HIMSELF WITH ALL CONTRACT DOCUMENTS, FIELD CONDITIONS AND DIMENSIONS PRIOR TO PROCEEDING WITH CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE SPRINT CONSTRUCTION MANAGER PRIOR TO THE COMMENCEMENT OF WORK. NO COMPENSATION WILL BE AWARDED BASED ON CLAIM OF LACK OF KNOWLEDGE OR FIELD CONDITIONS.

**POINT OF CONTACT:**

COMMUNICATION BETWEEN SPRINT AND THE CONTRACTOR SHALL FLOW THROUGH THE SINGLE SPRINT CONSTRUCTION MANAGER APPOINTED TO MANAGE THE PROJECT FOR SPRINT.

**ON-SITE SUPERVISION:**

THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE RESPONSIBLE FOR CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. THE CONTRACTOR SHALL EMPLOY A COMPETENT SUPERINTENDENT WHO SHALL BE IN ATTENDANCE AT THE SITE AT ALL TIMES DURING PERFORMANCE OF THE WORK.

**DRAWINGS REQUIRED AT JOBSITE:**

- THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A FULL SET OF THE CONSTRUCTION DRAWINGS FOR WIRELESS SITES AND THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES AT THE JOBSITE FROM MOBILIZATION THROUGH CONSTRUCTION COMPLETION.
- A. THE JOBSITE DRAWINGS SHALL BE CLEARLY MARKED DAILY IN RED PENCIL WITH ANY CHANGES IN CONSTRUCTION OVER WHAT IS DEPICTED IN THE DOCUMENTS. AT CONSTRUCTION COMPLETION, THIS JOBSITE MARKUP SET SHALL BE DELIVERED TO THE COMPANY OR COMPANY'S DESIGNATED REPRESENTATIVE TO BE FORWARDED TO THE COMPANY'S A&E VENDOR FOR PRODUCTION OF "AS-BUILT" DRAWINGS.
  - B. DIMENSIONS SHOWN ARE TO FINISH SURFACES UNLESS NOTED OTHERWISE. SPACING BETWEEN EQUIPMENT IS THE REQUIRED CLEARANCE. SHOULD THERE BE ANY QUESTIONS REGARDING THE CONTRACT DOCUMENTS, EXISTING CONDITIONS AND/OR DESIGN INTENT, THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING A CLARIFICATION FROM THE SPRINT CONSTRUCTION MANAGER PRIOR TO PROCEEDING WITH THE WORK.

**USE OF JOB SITE:**

THE CONTRACTOR SHALL CONFINE ALL CONSTRUCTION AND RELATED OPERATIONS INCLUDING STAGING AND STORAGE OF MATERIALS AND EQUIPMENT, PARKING, TEMPORARY FACILITIES, AND WASTE STORAGE TO THE LEASE PARCEL UNLESS OTHERWISE PERMITTED BY THE CONTRACT DOCUMENTS.

**UTILITY SERVICES:**

WHERE NECESSARY TO CUT EXISTING PIPES, ELECTRICAL WIRES, CONDUITS, CABLES, ETC., OF UTILITY SERVICES, OR OF FIRE PROTECTION OR COMMUNICATIONS SYSTEMS, THEY SHALL BE CUT AND CAPPED AT SUITABLE PLACES OR WHERE SHOWN. ALL SUCH ACTIONS SHALL BE COORDINATED WITH THE UTILITY COMPANY INVOLVED:

**PERMITS/FEES:**

WHEN REQUIRED THAT A PERMIT OR CONNECTION FEE BE PAID TO A PUBLIC UTILITY PROVIDER FOR NEW SERVICE TO THE CONSTRUCTION PROJECT, PAYMENT OF SUCH FEE SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR.

**CONTRACTOR:**

CONTRACTOR SHALL TAKE ALL MEASURES AND PROVIDE ALL MATERIAL NECESSARY FOR PROTECTING EXISTING EQUIPMENT AND PROPERTY.

**USE OF ELECTRONIC PROJECT MANAGEMENT SYSTEMS:**

CONTRACTOR WILL UTILIZE ITS BEST EFFORTS TO WORK WITH SPRINT ELECTRONIC PROJECT MANAGEMENT SYSTEMS. CONTRACTOR UNDERSTANDS THAT SUFFICIENT INTERNET ACCESS, EQUIVALENT TO "BROADBAND" OR BETTER, IS REQUIRED TO TIMELY AND EFFECTIVELY UTILIZE SPRINT DATA AND DOCUMENT MANAGEMENT SYSTEMS AND AGREES TO MAINTAIN APPROPRIATE CONNECTIONS FOR CONTRACTOR'S STAFF AND OFFICES THAT ARE COMPATIBLE WITH SPRINT DATA AND DOCUMENT MANAGEMENT SYSTEMS

**TEMPORARY UTILITIES AND FACILITIES:**

THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TEMPORARY UTILITIES AND FACILITIES NECESSARY EXCEPT AS OTHERWISE INDICATED IN THE CONSTRUCTION DOCUMENTS. TEMPORARY UTILITIES AND FACILITIES INCLUDE POTABLE WATER, HEAT, HVAC, ELECTRICITY, SANITARY FACILITIES, WASTE DISPOSAL FACILITIES, AND TELEPHONE/COMMUNICATION SERVICES. PROVIDE TEMPORARY UTILITIES AND FACILITIES IN ACCORDANCE WITH OSHA AND THE AUTHORITY HAVING JURISDICTION. CONTRACTOR MAY UTILIZE THE COMPANY ELECTRICAL SERVICE IN THE COMPLETION OF THE WORK WHEN IT BECOMES AVAILABLE. USE OF THE LESSOR'S OR SITE OWNER'S UTILITIES OR FACILITIES IS EXPRESSLY FORBIDDEN EXCEPT AS OTHERWISE ALLOWED IN THE CONTRACT DOCUMENTS.

**ACCESS TO WORK:**

THE CONTRACTOR SHALL PROVIDE ACCESS TO THE JOB SITE FOR AUTHORIZED COMPANY PERSONNEL AND AUTHORIZED REPRESENTATIVES OF THE ARCHITECT/ENGINEER DURING ALL PHASES OF THE WORK.

**DIMENSIONS:**

VERIFY DIMENSIONS INDICATED ON DRAWINGS WITH FIELD DIMENSIONS BEFORE FABRICATION OR ORDERING OF MATERIALS. DO NOT SCALE DRAWINGS.

**EXISTING CONDITIONS:**

NOTIFY THE SPRINT CONSTRUCTION MANAGER OF EXISTING CONDITIONS DIFFERING FROM THOSE INDICATED ON THE DRAWINGS. DO NOT REMOVE OR ALTER STRUCTURAL COMPONENTS WITHOUT PRIOR WRITTEN APPROVAL FROM THE ARCHITECT AND ENGINEER.

**SECTION 01 200 - COMPANY FURNISHED MATERIAL AND EQUIPMENT**

**FURNISHED MATERIALS:**

COMPANY FURNISHED MATERIALS AND EQUIPMENT TO BE INSTALLED BY THE CONTRACTOR (OFIC) IS IDENTIFIED ON THE RF DATA SHEET IN THE CONSTRUCTION DOCUMENTS.

**RECEIPT OF MATERIAL AND EQUIPMENT:**

A. THE CONTRACTOR IS RESPONSIBLE FOR SPRINT PROVIDED MATERIAL AND EQUIPMENT AND UPON RECEIPT SHALL:

- 1. ACCEPT DELIVERIES AS SHIPPED AND TAKE RECEIPT.
  - 2. VERIFY COMPLETENESS AND CONDITION OF ALL DELIVERIES.
  - 3. TAKE RESPONSIBILITY FOR EQUIPMENT AND PROVIDE INSURANCE PROTECTION AS REQUIRED IN AGREEMENT.
- B. RECORD ANY DEFECTS OR DAMAGES AND WITHIN TWENTY-FOUR HOURS AFTER RECEIPT, REPORT TO SPRINT OR ITS DESIGNATED PROJECT REPRESENTATIVE OF SUCH.
- C. PROVIDE SECURE AND NECESSARY WEATHER PROTECTED WAREHOUSING.
- D. COORDINATE SAFE AND SECURE TRANSPORTATION OF MATERIAL AND EQUIPMENT, DELIVERING AND OFF-LOADING FROM CONTRACTOR'S WAREHOUSE TO SITE.

**DELIVERABLES:**

- A. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.
- B. IF APPLICABLE, COMPLETE LOST/STOLEN/DAMAGED DOCUMENTATION REPORT AS NECESSARY IN ACCORDANCE WITH COMPANY PRACTICE, AND AS DIRECTED BY COMPANY.

**SECTION 01 300 - CELL SITE CONSTRUCTION**

**NOTICE TO PROCEED:**

- A. NO WORK SHALL COMMENCE PRIOR TO COMPANY'S ISSUANCE OF THE WORK ORDER.
- B. UPON RECEIVING NOTICE TO PROCEED, CONTRACTOR SHALL FULLY PERFORM ALL WORK NECESSARY TO PROVIDE SPRINT WITH AN OPERATIONAL WIRELESS FACILITY.

**GENERAL REQUIREMENTS FOR CONSTRUCTION:**

- A. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH. AT THE COMPLETION OF THE WORK, CONTRACTOR SHALL REMOVE FROM THE SITE ALL REMAINING RUBBISH, IMPLEMENTS, TEMPORARY FACILITIES, AND SURPLUS MATERIALS.
- B. EQUIPMENT ROOMS SHALL AT ALL TIMES BE MAINTAINED "BROOM CLEAN" AND CLEAR OF DEBRIS.
- C. CONTRACTOR SHALL TAKE ALL REASONABLE PRECAUTIONS TO DISCOVER AND LOCATE ANY HAZARDOUS CONDITION.
  - 1. IN THE EVENT CONTRACTOR ENCOUNTERS ANY HAZARDOUS CONDITION WHICH HAS NOT BEEN ABATED OR OTHERWISE MITIGATED, CONTRACTOR AND ALL OTHER PERSONS SHALL IMMEDIATELY STOP WORK IN THE AFFECTED AREA AND NOTIFY COMPANY IN WRITING. THE WORK IN THE AFFECTED AREA SHALL NOT BE RESUMED EXCEPT BY WRITTEN NOTIFICATION BY COMPANY.
  - 2. CONTRACTOR AGREES TO USE CARE WHILE ON THE SITE AND SHALL NOT TAKE ANY ACTION THAT WILL OR MAY RESULT IN OR CAUSE THE HAZARDOUS CONDITION TO BE FURTHER RELEASED IN THE ENVIRONMENT, OR TO FURTHER EXPOSE INDIVIDUALS TO THE HAZARD.
- D. CONTRACTOR'S ACTIVITIES SHALL BE RESTRICTED TO THE PROJECT LIMITS. SHOULD AREAS OUTSIDE THE PROJECT LIMITS BE AFFECTED BY CONTRACTOR'S ACTIVITIES, CONTRACTOR SHALL IMMEDIATELY RETURN THEM TO ORIGINAL CONDITION

**FUNCTIONAL REQUIREMENTS:**

- A. THE ACTIVITIES DESCRIBED IN THIS PARAGRAPH REPRESENT MINIMUM ACTIONS AND PROCESSES REQUIRED TO SUCCESSFULLY COMPLETE THE WORK. CONTRACTOR SHALL TAKE ALL ACTIONS AS NECESSARY TO SUCCESSFULLY COMPLETE THE CONSTRUCTION OF A FULLY FUNCTIONING WIRELESS FACILITY AT THE SITE IN ACCORDANCE WITH COMPANY PROCESSES.
- B. SUBMIT SPECIFIC DOCUMENTATION AS INDICATED HEREIN, AND OBTAIN REQUIRED APPROVALS WHILE THE WORK IS BEING PERFORMED.
- C. MANAGE AND CONDUCT ALL FIELD CONSTRUCTION SERVICE RELATED ACTIVITIES
- D. PROVIDE CONSTRUCTION ACTIVITIES TO THE EXTENT REQUIRED BY THE CONTRACT DOCUMENTS, INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
  - 1. PERFORM ANY REQUIRED SITE ENVIRONMENTAL MITIGATION.
  - 2. PREPARE GROUND SITES; PROVIDE DE-GRUBBING; AND ROUGH AND FINAL GRADING, AND COMPOUND SURFACE TREATMENTS.
  - 3. MANAGE AND CONDUCT ALL ACTIVITIES FOR INSTALLATION OF UTILITIES INCLUDING ELECTRICAL AND BACKHAUL (FIBER, COPPER, OR MICROWAVE).
  - 4. INSTALL UNDERGROUND FACILITIES INCLUDING UNDERGROUND POWER AND COMMUNICATIONS CONDUITS, AND UNDERGROUND GROUNDING SYSTEM.
  - 5. INSTALL ABOVE GROUND GROUNDING SYSTEMS, CONDUIT AND BOXES.
  - 6. PROVIDE NEW HVAC INSTALLATIONS AND MODIFICATIONS.
  - 7. INSTALL "H-FRAMES", CABINETS AND PADS AND PLATFORMS AS INDICATED.
  - 8. INSTALL ROADS, ACCESS WAYS, CURBS AND DRAINS AS INDICATED.
  - 9. ACCOMPLISH REQUIRED MODIFICATION OF EXISTING FACILITIES.

10. PROVIDE ANTENNA SUPPORT STRUCTURE FOUNDATIONS.

- 11. PROVIDE SLABS AND EQUIPMENT PLATFORMS.
- 12. INSTALL COMPOUND FENCING, SIGHT SHIELDING, LANDSCAPING AND ACCESS BARRIERS.
- 13. PERFORM INSPECTION AND MATERIAL TESTING AS REQUIRED HEREINAFTER.
- 14. CONDUCT SITE RESISTANCE TO EARTH TESTING AS REQUIRED HEREINAFTER.
- 15. INSTALL FIXED GENERATOR SETS AND OTHER STANDBY POWER SOLUTIONS.
- 16. INSTALL TOWERS, ANTENNA SUPPORT STRUCTURES AND PLATFORMS ON EXISTING TOWERS AS REQUIRED.
- 17. INSTALL CELL SITE RADIOS, MICROWAVE, GPS, COAXIAL MAINLINE, ANTENNAS, CROSS BAND COUPLERS, TOWER TOP AMPLIFIERS, LOW NOISE AMPLIFIERS AND RELATED EQUIPMENT.
- 18. CONDUCT ALL REQUIRED TESTS AND INSPECTIONS
- 19. PERFORM, DOCUMENT, AND CLOSE OUT ALL JURISDICTIONAL PERMITTING REQUIREMENTS AND ANY CONSTRUCTION CONTROL DOCUMENTS THAT MAY BE REQUIRED BY GOVERNMENT AGENCIES AND LANDLORDS.
- 20. PERFORM ALL ADDITIONAL WORK AS IDENTIFIED IN SCOPE OF SERVICES ATTACHED TO THE SUPPLIER AGREEMENT FOR THIS PROJECT. THIS WORK MAY INCLUDE COMMISSIONING, INTEGRATION, SPECIAL WAREHOUSING, REVERSE LOGISTICS ACTIVITIES, ETC. PERFORM COMMISSIONING AND INTEGRATION ACTIVITIES PER APPLICABLE MOPS.

**DELIVERABLES:**

- A. THE CONTRACTOR SHALL PROVIDE ALL REQUIRED TEST REPORTS AND DOCUMENTATION INCLUDED BUT NOT LIMITED TO THE FOLLOWING:
  - 1. PRODUCT SPECIFICATIONS FOR MATERIALS OR SPECIAL CONSTRUCTION IF REQUESTED BY SPRINT
  - 2. ACTUALIZE ALL CONSTRUCTION RELATED MILESTONES IN SITERRA AND COMPLETE ALL ON-LINE FORMS AND COMPLETE DOCUMENT UP-LOADS. UPLOAD ALL REQUIRED CLOSEOUT DOCUMENTS AND FINAL SITE PHOTOS
  - 3. SCANABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT LEFT ON SITE INSIDE BASE OF MAIN RF CABINET IN A PROTECTIVE POUCH.
  - 4. ALL REQUIRED TEST REPORTS.
  - 5. REQUIRED CLOSEOUT DOCUMENTATION INCLUDING BUT NOT LIMITED TO:
    - a. ALL JURISDICTIONAL PERMITTING AND OCCUPANCY INFORMATION
    - b. PDF SCAN OF REDLINES PRODUCED IN THE FIELD
    - c. ELECTRONIC AS-BUILT DRAWINGS IN AUTOCAD AND PDF FORMATS
    - d. LIEN WAIVERS
    - e. FINAL PAYMENT APPLICATION
    - f. REQUIRED FINAL CONSTRUCTION PHOTOS
    - g. CONSTRUCTION AND COMMISSIONING CHECKLIST COMPLETE WITH NO DEFICIENT ITEMS
    - h. LISTS OF SUBCONTRACTORS
- B. PROVIDE ADDITIONAL DOCUMENTATION INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING. DOCUMENTATION SHALL BE FORWARDED IN ORIGINAL FORMAT AND/OR UPLOADED INTO SMS.
  - 1. ALL CORRESPONDENCE AND PRELIMINARY CONSTRUCTION REPORTS.
  - 2. PROJECT PROGRESS REPORTS.
  - 3. PRE-CONSTRUCTION MEETING NOTES.

**SECTION 01 400 - TESTS, INSPECTIONS, SUBMITTALS, AND PROJECT CLOSEOUT**

**TESTS AND INSPECTIONS:**

- A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL CONSTRUCTION TESTS, INSPECTIONS AND PROJECT DOCUMENTATION.
- B. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
  - 1. COAX SWEEPS AND FIBER TESTS PER TS-0200 (CURRENT VERSION) ANTENNA LINE ACCEPTANCE STANDARDS
  - 2. POST CONSTRUCTION HEIGHT VERIFICATION, AZIMUTH AND DOWNTILT USING ELECTRONIC COMMERCIAL MADE-FOR-THE-PURPOSE ANTENNA ALIGNMENT TOOL.
  - 3. CONCRETE BREAK TESTS
  - 4. SITE RESISTANCE TO EARTH TEST
  - 5. STRUCTURAL BACKFILL COMPACTION TESTS
  - 6. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF TESTING.
  - 7. ADDITIONAL TESTING AS REQUIRED ELSEWHERE IN THIS SPECIFICATION.

**SUBMITTALS:**

- A. THE WORK IN ALL ASPECTS SHALL COMPLY WITH THE CONSTRUCTION DRAWINGS AND THESE SPECIFICATIONS.
- B. UPLOAD THE FOLLOWING TO SITERRA AS APPLICABLE INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
  - 1. CONCRETE MIX-DESIGNS FOR TOWER FOUNDATIONS, ANCHORS PIERS, AND CONCRETE PAVING.
  - 2. CONCRETE BREAK TESTS AS SPECIFIED HEREIN.
  - 3. CHEMICAL GROUNDING SYSTEM .
  - 4. REINFORCEMENT CERTIFICATIONS
  - 5. STRUCTURAL BACKFILL TEST RESULTS
  - 6. SWEEP AND FIBER TESTS
  - 7. ANTENNA AZIMUTH AND DOWN-TILT VERIFICATION
  - 8. POST CONSTRUCTION HEIGHT VERIFICATION
  - 9. ADDITIONAL SUBMITTALS MAY BE REQUIRED FOR SPECIAL CONSTRUCTION OR MINOR MATERIALS
- C. ALTERNATES: AT THE COMPANY'S REQUEST, ANY ALTERNATIVES TO THE MATERIALS OR METHODS SPECIFIED SHALL BE SUBMITTED TO SPRINT'S CONSTRUCTION MANAGER FOR APPROVAL PRIOR TO BEING SHIPPED TO SITE. SPRINT WILL REVIEW AND APPROVE ONLY THOSE REQUESTS MADE IN WRITING. NO VERBAL APPROVALS WILL BE CONSIDERED. SUBMITTAL FOR APPROVAL SHALL INCLUDE A STATEMENT OF COST REDUCTION PROPOSED FOR USE OF ALTERNATE PRODUCT.

**TESTING BY THIRD PARTY AGENCY:**

- A. EMPLOY AN AGENCY OF ENGINEERS AND SCIENTISTS WHO IS REGULARLY ENGAGED IN FIELD AND LABORATORY TESTING AND ANALYSIS. AGENCY SHALL HAVE BEEN IN BUSINESS A MINIMUM OF FIVE YEARS, AND BE LICENSED AS PROFESSIONAL ENGINEERS IN THE STATE WHERE THE PROJECT IS LOCATED. AGENCY IS SUBJECT TO APPROVAL BY COMPANY.
  - 1. AGENCY MUST HAVE A THOROUGH UNDERSTANDING OF LOCAL AVAILABLE MATERIALS, INCLUDING THE SOIL, ROCK, AND GROUNDWATER CONDITIONS.
  - 2. AGENCY IS TO BE FAMILIAR WITH THE APPLICABLE REQUIREMENTS FOR THE TESTS TO BE DONE, EQUIPMENT TO BE USED, AND ASSOCIATED HEALTH AND SAFETY ISSUES.
  - 3. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASHTO, AND OTHER METHODS IS NEEDED.
- B. REQUIRED THIRD PARTY TESTS:
  - 1. SITE RESISTANCE TO EARTH TEST PER NP-312-201
  - 2. CONCRETE CYLINDER BREAK TESTS FOR TOWER PIER AND ANCHORS PER NATIONALLY RECOGNIZED STANDARDS
  - 3. STRUCTURAL SOILS COMPACTION TESTS PER NATIONALLY RECOGNIZED STANDARDS
  - 4. REBAR PLACEMENT VERIFICATION WITH REPORT
  - 5. TESTING TENSION STUDY FOR ROCK ANCHORS
  - 6. ALL THIRD PARTY TESTS AS REQUIRED BY LOCAL JURISDICTION
- C. REQUIRED TESTS BY CONTRACTOR
  - 1. COAX SWEEP TESTS PER SPRINT STANDARD TS-0200
  - 2. FIBER TESTS PER SPRINT STANDARD EL-0568
  - 3. MICROWAVE LINK TESTS PER NP-760-500
  - 4. ANTENNA AZIMUTHS AND DOWN TILT USING ELECTRONIC ALIGNMENT TOOL PER ANTENNA INSTALLATION SPECIFICATION HEREIN.



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**Certification & Seal:**  
I hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the laws of the State of Connecticut.



Signature: *James R. Skowronski* Date: 8/08/2014


MARK	DATE	DESCRIPTION
A	08/08/14	FINAL CONSTRUCTION DRAWINGS

ISSUE PHASE FINAL DATE ISSUED 08/08/2014

PROJECT TITLE:

CTS  
CT03XC360-A

PROJECT INFORMATION:  
4G FERNWOOD LANE  
WILTON, CT 06897  
FAIRFIELD COUNTY

SHEET TITLE:

SPRINT SPECIFICATIONS

SCALE: NONE

PROJECT NUMBER	28731
SHEET NUMBER	SP-1



5. POST CONSTRUCTION HEIGHT VERIFICATION AS REQUIRED HERewith IN THE TOWER INSTALLATION SPECIFICATIONS.
  6. ASPHALT ROADWAY COMPACTED THICKNESS, SURFACE SMOOTHNESS, AND COMPACTED DENSITY TESTING AS SPECIFIED HERewith IN THE ASPHALT PAVING SPECIFICATIONS.
  7. FIELD QUALITY CONTROL TESTING AS SPECIFIED HERewith IN THE CONCRETE PAVING SPECIFICATIONS.
  8. TESTING REQUIRED HERewith UNDER SPECIFICATIONS FOR AGGREGATE BASE FOR ROADWAYS
  9. ALL OTHER TESTS REQUIRED BY LOCAL JURISDICTION
- D. INSPECTIONS BY COMPANY: THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN INSPECTION ACTIVITIES, FINAL ACCEPTANCE / PUNCH WALK REVIEW, AND/OR AS A RESULT OF TESTING
- E. SPRINT RESERVES THE RIGHT TO INSPECT THE CONSTRUCTION SITE AT ANY TIME VIA SITE WALKS AND/OR PHOTO REVIEWS. CONTRACTOR SHALL GIVE SPRINT 24 HOURS NOTICE PRIOR TO THE COMMENCEMENT OF THE FOLLOWING CONSTRUCTION ACTIVITIES AND PHOTOGRAPHS OF THE IN-PROGRESS WORK.
1. GROUNDING SYSTEM AND BURIED UTILITIES INSTALLATION PRIOR TO EARTH CONCEALMENT DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
  2. FORMING FOR CONCRETE AND REBAR PLACEMENT PRIOR TO POUR DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
  3. COMPACTION OF BACKFILL MATERIALS, AGGREGATE BASE FOR ROADS, PADS, AND ANCHORS, ASPHALT PAVING, AND SHAFT BACKFILL FOR CONCRETE AND WOOD POLES, BY INDEPENDENT THIRD PARTY AGENCY.
  4. PRE AND POST CONSTRUCTION ROOFTOP AND STRUCTURAL INSPECTIONS ON EXISTING FACILITIES. PRIOR TO CONSTRUCTION ACTIVITIES AND AFTER CONSTRUCTION IS COMPLETE. PROVIDE PHOTOGRAPHIC DOCUMENTATION OF ROOF, FLASHINGS, AND PARAPETS, BOTH BEFORE AND AFTER CONSTRUCTION IS COMPLETE.
  5. TOWER ERECTION SECTION STACKING AND PLATFORM ATTACHMENT DOCUMENTED BY DIGITAL PHOTOGRAPHS BY THIRD PARTY AGENCY.
  6. TOWER TOP AND INACCESSIBLE EQUIPMENT (RRUS, ANTENNAS, AND CABLING): PROVIDE PHOTOS OF THE BACKS OF ALL ANTENNAS, RRUS, COMBINERS, FILTERS, FIBER AND DC CABLING, CABLE COLOR CODING, EQUIPMENT GROUNDING AND CONNECTOR WATER PROOFING INCLUDING NAME PLATE AND SERIAL NUMBER FOR ALL SERIALIZED EQUIPMENT.

**PROJECT CLOSEOUT:**

- A. FINAL ACCEPTANCE PUNCH WALK AND INSPECTION: AS IDENTIFIED IN THE SCOPE OF SERVICES, SPRINT WILL CONDUCT A FINAL PUNCH WALK OR FINAL DESK TOP PHOTO REVIEW (SITE MODIFICATIONS). PUNCH WALKS MUST BE SCHEDULED IN ADVANCE AS REQUIRED. AT THE PUNCH WALK / REVIEW, SPRINT MAY IDENTIFY CRITICAL DEFICIENCIES WHICH MUST BE CORRECTED PRIOR TO PUTTING SITE ON AIR. MINOR DEFICIENCIES MUST BE CORRECTED WITHIN 30 DAYS EXCEPT AS OTHERWISE REQUIRED. VERIFICATIONS OF CORRECTIONS MAY BE MADE BY COMPANY DURING A REPEAT SITE WALK OR DESK TOP PHOTO REVIEW AT COMPANY'S SOLE DISCRETION.
- B. CLOSEOUT DOCUMENTATION: ALL CLOSEOUT DOCUMENTATION AND PHOTOGRAPHS SHALL BE UPLOADED PRIOR TO FINAL ACCEPTANCE. SPRINT WILL REVIEW CLOSEOUT DOCUMENTATION FOR PRESENCE AND CONTENT. CLOSEOUT DOCUMENTATION SHALL INCLUDE BUT IS NOT LIMITED TO THE FOLLOWING AS APPLICABLE:
1. COAX SWEEP TESTS:
  2. FIBER TESTS:
  3. JURISDICTION FINAL INSPECTION DOCUMENTATION
  4. REINFORCEMENT CERTIFICATION (MILL CERTIFICATION)
  5. CONCRETE MIX DESIGN AND PRODUCT DATA (TOWER FOUNDATION)
  6. LIEN WAIVERS AND RELEASES.
  7. POST -CONSTRUCTION HEIGHT VERIFICATION
  8. JURISDICTION CERTIFICATE OF OCCUPANCY
  9. ELECTRONIC ANTENNA AZIMUTH AND DOWN TILT VERIFICATION
  10. STRUCTURAL BACKFILL TEST RESULTS (IF APPLICABLE)
  11. CELL SITE UTILITY SETUP
  12. AS-BUILT REDLINE CONSTRUCTION DRAWINGS (PDF SCAN OF FIELD MARKS)
  13. AS-BUILT CONSTRUCTION DRAWINGS IN DWG AND PDF FORMATS
  14. LIST OF SUB CONTRACTORS
  15. APPROVED PERMITTING DOCUMENTS
  16. FINAL SITE PHOTOS UP-LOADED TO SITERRA. INCLUDE THE FOLLOWING AS APPLICABLE:
    - a. TOWER, ANTENNAS, RRUS, AND MAINLINE: INSPECTION AND PHOTOGRAPHS OF SECTION STACKING; INSPECTION AND PHOTOGRAPHS OF PLATFORM COMPONENT ATTACHMENT POINTS; PHOTOGRAPHS OF TOWER TOP GROUNDING; PHOTOS OF TOWER COAX/CABLE LINE COLOR CODING AT THE TOP AND AT GROUND LEVEL; INSPECTION AND PHOTOGRAPHS OF OPERATIONAL OF TOWER LIGHTING, AND PLACEMENT OF FAA REGISTRATION SIGN; PHOTOGRAPHS SHOWING ADDITIONAL GROUNDING POINTS FOR TOWERS GREATER THAN 200 FEET.; PHOTOS OF ANTENNA GROUND BAR, EQUIPMENT GROUND BAR, AND MASTER GROUND BAR; PHOTOS OF GPS ANTENNA(S); PHOTOS OF EACH SECTOR OF ANTENNAS; ONE PHOTOGRAPH LOOKING AT THE SECTOR AND ONE FROM BEHIND SHOWING THE PROJECTED COVERAGE AREA; PHOTOS OF COAX WEATHERPROOFING - TOP AND BOTTOM; PHOTOS OF COAX GROUNDING--TOP AND BOTTOM; PHOTOS OF ANTENNA AND MAST GROUNDING; PHOTOS OF COAX CABLE ENTRY INTO SHELTER; PHOTOS OF PLATFORM MECHANICAL CONNECTIONS TO TOWER/MONOPOLE.
    - b. ROOF TOPS: PRE-CONSTRUCTION AND POST-CONSTRUCTION VISUAL INSPECTION AND PHOTOGRAPHS OF THE ROOF AND INTERIOR TO DETERMINE AND DOCUMENT CONDITIONS; ROOF TOP CONSTRUCTION INSPECTIONS AS REQUIRED BY THE JURISDICTION; PHOTOGRAPHS OF CABLE TRAY AND/OR ICE BRIDGE; PHOTOGRAPHS OF DOGHOUSE/CABLE EXIT FROM ROOF;
    - c. SITE LAYOUT - PHOTOGRAPHS OF THE OVERALL COMPOUND, INCLUDING EQUIPMENT PLATFORM FROM ALL FOUR CORNERS.
    - d. FINISHED UTILITIES: CLOSE-UP PHOTOGRAPHS OF THE PPC BREAKER PANEL; CLOSE-UP PHOTOGRAPH OF THE INSIDE OF THE TELCO PANEL AND NIU; CLOSE-UP PHOTOGRAPH OF THE POWER METER AND DISCONNECT; PHOTOS OF POWER AND TELCO ENTRANCE TO COMPANY ENCLOSURE; PHOTOGRAPHS AT METER BOX AND/OR FACILITY DISTRIBUTION PANEL.

**PROJECT PHOTOGRAPHS:**

- A. PROVIDE PROJECT CLOSEOUT GENERAL ARRANGEMENT PHOTOS OF ALL NEW WORK. THE FOLLOWING LIST REPRESENTS MINIMUM REQUIREMENTS AND MINIMUM QUANTITY. ADDITIONAL PHOTOS MAY BE REQUIRED TO ADEQUATELY DOCUMENT THE WORK.
1. ASR AND RF MPE SIGNAGE (IF NOT IN PLACE, SUPPLIER NOTIFIES EMS FIELD REPRESENTATIVE)
  2. BACK OF ANTENNAS AND RRUS (1 EACH SECTOR)
  3. BACK OF ANTENNAS AND RRUS (1 EACH SECTOR) CLOSE UP SHOWING WEATHERPROOFING AND GROUNDING (AS REQUIRED). CLOSE-UP OF BACK SIDE OF EACH PERMANENT RRU SHOWING SERIAL NUMBER/BAR CODE.
  4. VIEW (1 EACH SECTOR) ALONG THE AZIMUTH AND TILT OF THE ANTENNAS
  5. TOP OF TOWER FROM GROUND, 1 EACH SECTOR
  6. MAINLINE HYBRID CABLE ROUTE DOWN TOWER SHOWING FASTENERS AND SUPPORT
  7. MAINLINE/HYBRID CABLE ROUTE ALONG ICE BRIDGE OR IN CABLE TRAY SHOWING FASTENERS AND SUPPORT
  8. GROUND MOUNTED RRU RACKS (FRONT AND BACK)
  9. FRONT, SIDE AND BACK ELEVATIONS OF ALL GROUND CABINETS
  10. VIEW OF COMPOUND FROM A DISTANCE
  11. VIEW OF EACH GROUND CABINET (POWER, RF, FIBER SPOOL, PPC POWER, PPC TELCO WITH DOOR OPEN)
  12. BACKHAUL FIBER MEET-ME POINT AND CONDUIT ROUTE (MICROWAVE INSTALLATION IF NOT FIBER)
  13. AAV NETWORK INTERFACE DEVICE OR MICROWAVE RADIO INSTALLATION

**DEFICIENCY CORRECTIONS:**

CONTRACTOR IS RESPONSIBLE FOR ALL CORRECTIONS TO DEFICIENCIES IDENTIFIED THROUGH TESTING, REVIEW OF SUBMITTALS, INSPECTIONS AND CLOSEOUT REVIEWS.

**SECTION 01 500 - PROJECT REPORTING**

**WEEKLY REPORTS:**

- A. CONTRACTOR SHALL REPORT TO SPRINT AT MINIMUM ON A WEEKLY BASIS VIA SITERRA BY UPDATING ALL APPLICABLE POST END KEEPING MILESTONES WITH ACTUAL AND FORECASTED COMPLETION DATES.
- B. ADDITIONAL REQUIREMENTS FOR REPORTING MAY BE IDENTIFIED ELSEWHERE OR REQUIRED BY THE SCOPE OF SERVICES OR SPRINTS LOCAL MARKET CONSTRUCTION MANAGER. THIS INFORMATION WILL PROVIDE A BASIS FOR PROGRESS MONITORING AND PAYMENT.

**PROJECT CONFERENCE CALLS:**

SPRINT MAY HOLD PERIODIC PROJECT CONFERENCE CALLS. CONTRACTOR WILL BE REQUIRED TO COMMUNICATE SITE STATUS, MILESTONE COMPLETIONS AND UPCOMING MILESTONE PROJECTIONS, AND ANSWER ANY OTHER SITE STATUS QUESTIONS AS NECESSARY.

**FINAL PROJECT ACCEPTANCE:** PRIOR TO SPRINTS FINAL PROJECT ACCEPTANCE. ALL REQUIRED MILESTONE ACTUALS MUST BE UPDATED IN SITERRA AND ALL REQUIRED REPORTING TASKS MUST BE COMPLETE.

**SECTION 11 700 - ANTENNA ASSEMBLY, REMOTE RADIO UNITS AND CABLE INSTALLATION**

**SUMMARY:**

THIS SECTION SPECIFIES INSTALLATION OF ANTENNAS, RRUS, AND CABLE EQUIPMENT, INSTALLATION, AND TESTING OF COAXIAL FIBER CABLE.

**ANTENNAS AND RRUS:**

THE NUMBER AND TYPE OF ANTENNAS AND RRUS TO BE INSTALLED IS DETAILED ON THE CONSTRUCTION DRAWINGS.

**HYBRID CABLE:**

HYBRID CABLE WILL BE DC/FIBER AND FURNISHED FOR INSTALLATION AT EACH SITE. CABLE SHALL BE INSTALLED PER THE CONSTRUCTION DRAWINGS AND THE APPLICABLE MANUFACTURER'S REQUIREMENTS.

**JUMPERS AND CONNECTORS:**

FURNISH AND INSTALL 1/2" COAX JUMPER CABLES BETWEEN THE RRUS AND ANTENNAS. JUMPERS SHALL BE TYPE LDF 4, FLC 12-50, CR 540, OR FXL 540. SUPER-FLEX CABLES ARE NOT ACCEPTABLE. JUMPERS BETWEEN THE RRUS AND ANTENNAS OR TOWER TOP AMPLIFIERS SHALL CONSIST OF 1/2 INCH FOAM DIELECTRIC, OUTDOOR RATED COAXIAL CABLE, MIN. LENGTH FOR JUMPER SHALL BE 10'-0".

**REMOTE ELECTRICAL TILT (RET) CABLES:**

**MISCELLANEOUS:**

INSTALL SPLITTERS, COMBINERS, FILTERS PER RF DATA SHEET, FURNISHED BY SPRINT.

**ANTENNA INSTALLATION:**

THE CONTRACTOR SHALL ASSEMBLE ALL ANTENNAS ONSITE IN ACCORDANCE WITH THE INSTRUCTIONS SUPPLIED BY THE MANUFACTURER. ANTENNA HEIGHT, AZIMUTH, AND FEED ORIENTATION INFORMATION SHALL BE A DESIGNATED ON THE CONSTRUCTION DRAWINGS.

A. THE CONTRACTOR SHALL POSITION THE ANTENNA ON TOWER PIPE MOUNTS SO THAT THE BOTTOM STRUT IS LEVEL. THE PIPE MOUNTS SHALL BE PLUMB TO WITHIN 1 DEGREE.

B. ANTENNA MOUNTING REQUIREMENTS: PROVIDE ANTENNA MOUNTING HARDWARE AS INDICATED ON THE DRAWINGS.

**HYBRID CABLE INSTALLATION:**

A. THE CONTRACTOR SHALL ROUTE, TEST, AND INSTALL ALL CABLES AS INDICATED ON THE CONSTRUCTION DRAWINGS AND IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.

B. THE INSTALLED RADIUS OF THE CABLES SHALL NOT BE LESS THAN THE MANUFACTURER'S SPECIFICATIONS FOR BENDING RADII.

C. EXTREME CARE SHALL BE TAKEN TO AVOID DAMAGE TO THE CABLES DURING HANDLING AND INSTALLATION.

1. FASTENING MAIN HYBRID CABLES: ALL CABLES SHALL BE INSTALLED INSIDE MONOPOLE WITH CABLE SUPPORT GRIPS AS REQUIRED BY THE MANUFACTURER.
2. FASTENING INDIVIDUAL FIBER AND DC CABLES ABOVE BREAKOUT ENCLOSURE (MEDUSA), WITHIN THE MMBS CABINET AND ANY INTERMEDIATE DISTRIBUTION BOXES:
  - a. FIBER: SUPPORT FIBER BUNDLES USING 1/2" VELCRO STRAPS OF THE REQUIRED LENGTH AT 18" O.C. STRAPS SHALL BE UV, OIL AND WATER RESISTANT AND SUITABLE FOR INDUSTRIAL INSTALLATIONS AS MANUFACTURED BY TEXTOL OR APPROVED EQUAL.
  - b. DC: SUPPORT DC BUNDLES WITH ZIP TIES OF THE ADEQUATE LENGTH. ZIP TIES TO BE UV STABILIZED, BLACK NYLON, WITH TENSILE STRENGTH AT 12,000 PSI AS MANUFACTURED BY NELCO PRODUCTS OR EQUAL.
3. FASTENING JUMPERS: SECURE JUMPERS TO THE SIDE ARMS OR HEAD FRAMES USING STAINLESS STEEL TIE WRAPS OR STAINLESS STEEL BUTTERFLY CLIPS.
4. CABLE INSTALLATION:
  - a. INSPECT CABLE PRIOR TO USE FOR SHIPPING DAMAGE, NOTIFY THE CONSTRUCTION MANAGER.
  - b. CABLE ROUTING: CABLE INSTALLATION SHALL BE PLANNED TO ENSURE THAT THE LINES WILL BE PROPERLY ROUTED IN THE CABLE ENVELOP AS INDICATED ON THE DRAWINGS. AVOID TWISTING AND CROSSOVERS.
  - c. HOIST CABLE USING PROPER HOISTING GRIPS. DO NOT EXCEED MANUFACTURER'S RECOMMENDED MAXIMUM BEND RADIUS.
5. GROUNDING OF TRANSMISSION LINES: ALL TRANSMISSION LINES SHALL BE GROUNDED AS INDICATED ON DRAWINGS.
6. HYBRID CABLE COLOR CODING: ALL COLOR CODING SHALL BE AS REQUIRED IN TS 0200 (CURRENT VERSION).
7. HYBRID CABLE LABELING: INDIVIDUAL HYBRID AND DC BUNDLES SHALL BE LABELED ALPHA-NUMERICALLY ACCORDING TO SPRINT CELL SITE ENGINEERING NOTICE - EN 2012-001, REV 1

**WEATHERPROOFING EXTERIOR CONNECTORS AND HYBRID CABLE GROUND KITS:**

A. ALL FIBER & COAX CONNECTORS AND GROUND KITS SHALL BE WEATHERPROOFED.

B. WEATHERPROOFED USING ONE OF THE FOLLOWING METHODS. ALL INSTALLATIONS MUST BE DONE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS AND INDUSTRY BEST PRACTICES.

1. COLD SHRINK: ENCOMPASS CONNECTOR IN COLD SHRINK TUBING AND PROVIDE A DOUBLE WRAP OF 2" ELECTRICAL TAPE EXTENDING 2" BEYOND TUBING. PROVIDE 3M COLD SHRINK CX5 SERIES OR EQUAL.
2. SELF-AMALGAMATING TAPE: CLEAN SURFACES. APPLY A DOUBLE WRAP OF SELF-AMALGAMATING TAPE 2" BEYOND CONNECTOR. APPLY A SECOND WRAP OF SELF-AMALGAMATING TAPE IN OPPOSITE DIRECTION. APPLY DOUBLE WRAP OF 2" WIDE ELECTRICAL TAPE EXTENDING 2" BEYOND THE SELF-AMALGAMATING TAPE.
3. 3M SLIM LOCK CLOSURE 716: SUBSTITUTIONS WILL NOT BE ALLOWED.
4. OPEN FLAME ON JOB SITE IS NOT ACCEPTABLE

**SECTION 11 800 - INSTALLATION OF MULTIMODAL BASE STATIONS (MMBS) AND RELATED EQUIPMENT**

**SUMMARY:**

A. THIS SECTION SPECIFIES MMBS CABINETS, POWER CABINETS, AND INTERNAL EQUIPMENT INCLUDING BY NOT LIMITED TO RECTIFIERS, POWER DISTRIBUTION UNITS, BASE BAND UNITS, SURGE ARRESTORS, BATTERIES, AND SIMILAR EQUIPMENT FURNISHED BY THE COMPANY FOR INSTALLATION BY THE CONTRACTOR (OFCI).

B. CONTRACTOR SHALL PROVIDE AND INSTALL ALL MISCELLANEOUS MATERIALS AND PROVIDE ALL LABOR REQUIRED FOR INSTALLATION EQUIPMENT IN EXISTING CABINET OR NEW CABINET AS SHOWN ON DRAWINGS AND AS REQUIRED BY THE APPLICABLE INSTALLATION MOPS.

C. COMPLY WITH MANUFACTURER'S INSTALLATION AND START-UP REQUIREMENTS.

**DC CIRCUIT BREAKER LABELING**

A. NEW DC CIRCUIT IS REQUIRED IN MMBS CABINET SHALL BE CLEARLY IDENTIFIED AS TO RRU BEING SERVICED.

**SECTION 26 100 - BASIC ELECTRICAL REQUIREMENTS**

**SUMMARY:**

THIS SECTION SPECIFIES BASIC ELECTRICAL REQUIREMENTS FOR SYSTEMS AND COMPONENTS

**QUALITY ASSURANCE:**

A. ALL EQUIPMENT FURNISHED UNDER DIVISION 26 SHALL CARRY UL LABELS AND LISTINGS WHERE SUCH LABELS AND LISTINGS ARE AVAILABLE IN THE INDUSTRY.

B. MANUFACTURERS OF EQUIPMENT SHALL HAVE A MINIMUM OF THREE YEARS EXPERIENCE WITH THEIR EQUIPMENT INSTALLED AND OPERATING IN THE FIELD IN A USE SIMILAR TO THE PROPOSED USE FOR THIS PROJECT.

C. MATERIALS AND EQUIPMENT: ALL MATERIALS AND EQUIPMENT SPECIFIED IN DIVISION 26 OF THE SAME TYPE SHALL BE OF THE SAME MANUFACTURER AND SHALL BE NEW, OF THE BEST QUALITY AND DESIGN, AND FREE FROM DEFECTS.

**SUPPORTING DEVICES:**

A. MANUFACTURED STRUCTURAL SUPPORT MATERIALS: SUBJECT TO COMPLIANCE WITH REQUIREMENTS, PROVIDE PRODUCTS BY THE FOLLOWING:

1. ALLIED TUBE AND CONDUIT.
2. B-LINE SYSTEM.
3. UNISTRUT DIVERSIFIED PRODUCTS.
4. THOMAS & BETTS.

B. FASTENERS: TYPES, MATERIALS, AND CONSTRUCTION FEATURES AS FOLLOWS:

1. EXPANSION ANCHORS: CARBON STEEL WEDGE OR SLEEVE TYPE.
2. POWER-DRIVEN THREADED STUDS: HEAT-TREATED STEEL, DESIGNED SPECIFICALLY FOR THE INTENDED SERVICE.
3. FASTEN BY MEANS OF WOOD SCREWS ON WOOD.
4. TOGGLE BOLTS ON HOLLOW MASONRY UNITS.
5. CONCRETE INSERTS OR EXPANSION BOLTS ON CONCRETE OR SOLID MASONRY.
6. MACHINE SCREWS, WELDED THREADED STUDS, OR SPRING-TENSION CLAMPS ON STEEL.
7. EXPLOSIVE DEVICES FOR ATTACHING HANGERS TO STRUCTURE SHALL NOT BE PERMITTED.
8. DO NOT WELD CONDUIT, PIPE STRAPS, OR ITEMS OTHER THAN THREADED STUDS TO STEEL STRUCTURES.
9. IN PARTITIONS OF LIGHT STEEL CONSTRUCTION, USE SHEET METAL SCREWS.



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Signature: *James R. Skowronski* Date: 8/08/2014


MARK	DATE	DESCRIPTION
A	08/08/14	FINAL CONSTRUCTION DRAWINGS

ISSUE PHASE: FINAL DATE ISSUED: 08/08/2014

PROJECT TITLE:

CTS  
CT03XC360-A

PROJECT INFORMATION:  
46 FERNWOOD LANE  
WILTON, CT 06897  
FAIRFIELD COUNTY

SHEET TITLE:  
SPRINT SPECIFICATIONS

SCALE: NONE

PROJECT NUMBER	28731
SHEET NUMBER	SP-2



SUPPORTING DEVICES:

- A. INSTALL SUPPORTING DEVICES TO FASTEN ELECTRICAL COMPONENTS SECURELY AND PERMANENTLY IN ACCORDANCE WITH NEC.
- B. COORDINATE WITH THE BUILDING STRUCTURAL SYSTEM AND WITH OTHER TRADES.
- C. UNLESS OTHERWISE INDICATED ON THE DRAWINGS, FASTEN ELECTRICAL ITEMS AND THEIR SUPPORTING HARDWARE SECURELY TO THE STRUCTURE IN ACCORDANCE WITH THE FOLLOWING:
  - 1. ENSURE THAT THE LOAD APPLIED BY ANY FASTENER DOES NOT EXCEED 25 PERCENT OF THE PROOF TEST LOAD.
  - 2. USE VIBRATION AND SHOCK-RESISTANT FASTENERS FOR ATTACHMENTS TO CONCRETE SLABS.

ELECTRICAL IDENTIFICATION:

- A. UPDATE AND PROVIDE TYPED CIRCUIT BREAKER SCHEDULES IN THE MOUNTING BRACKET, INSIDE DOORS OF AC PANEL BOARDS WITH ANY CHANGES MADE TO THE AC SYSTEM.
- B. BRANCH CIRCUITS FEEDING AVIATION OBSTRUCTION LIGHTING EQUIPMENT SHALL BE CLEARLY IDENTIFIED AS SUCH AT THE BRANCH CIRCUIT PANELBOARD.

SECTION 26 200 - ELECTRICAL MATERIALS AND EQUIPMENT

- A. RIGID GALVANIZED STEEL (RGS) CONDUIT SHALL BE USED FOR EXTERIOR LOCATIONS ABOVE GROUND AND IN UNFINISHED INTERIOR LOCATIONS AND FOR UNDERGROUND RUNS. RIGID CONDUIT AND FITTINGS SHALL BE STEEL, COATED WITH ZINC EXTERIOR AND INTERIOR BY THE HOT DIP GALVANIZING PROCESS. CONDUIT SHALL BE PRODUCED TO ANSI SPECIFICATIONS C80.1, FEDERAL SPECIFICATION WW-C-581 AND SHALL BE LISTED WITH THE UNDERWRITERS' LABORATORIES. FITTINGS SHALL BE THREADED - SET SCREW OR COMPRESSION FITTINGS WILL NOT BE ACCEPTABLE. RGS CONDUITS SHALL BE MANUFACTURED BY ALLIED, REPUBLIC OR WHEATLAND.
- B. UNDERGROUND CONDUIT IN CONCRETE SHALL BE POLYVINYLCHLORIDE (PVC) SUITABLE FOR DIRECT BURIAL AS APPLICABLE. JOINTS SHALL BE BELLED, AND FLUSH SOLVENT WELDED IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS. CONDUIT SHALL BE CARLON ELECTRICAL PRODUCTS OR APPROVED EQUAL.
- C. TRANSITIONS BETWEEN PVC AND RIGID (RGS) SHALL BE MADE WITH PVC COATED METALLIC LONG SWEEP RADIUS ELBOWS.
- D. EMT OR RIGID GALVANIZED STEEL CONDUIT MAY BE USED IN FINISHED SPACES CONCEALED IN WALLS AND CEILINGS. EMT SHALL BE MILD STEEL, ELECTRICALLY WELDED, ELECTRO-GALVANIZED OR HOT-DIPPED GALVANIZED AND PRODUCED TO ANSI SPECIFICATION C80.3, FEDERAL SPECIFICATION WW-C-563, AND SHALL BE UL LISTED. EMT SHALL BE MANUFACTURED BY ALLIED, REPUBLIC OR WHEATLAND, OR APPROVED EQUAL. FITTINGS SHALL BE METALLIC COMPRESSION. SET SCREW CONNECTIONS SHALL NOT BE ACCEPTABLE.
- E. LIQUID TIGHT FLEXIBLE METALLIC CONDUIT SHALL BE USED FOR FINAL CONNECTION TO EQUIPMENT. FITTINGS SHALL BE METALLIC GLAND TYPE COMPRESSION FITTINGS, MAINTAINING THE INTEGRITY OF CONDUIT SYSTEM. SET SCREW CONNECTIONS SHALL NOT BE ACCEPTABLE. MAXIMUM LENGTH OF FLEXIBLE CONDUIT SHALL NOT EXCEED 6-FEET. LFMC SHALL BE PROTECTED AND SUPPORTED AS REQUIRED BY NEC. MANUFACTURERS OF FLEXIBLE CONDUITS SHALL BE CAROL, ANACONDA METAL HOSE OR UNIVERSAL METAL HOSE, OR APPROVED EQUAL.
- F. MINIMUM SIZE CONDUIT SHALL BE 3/4 INCH (21 MM).

HUBS AND BOXES:

- A. AT ENTRANCES TO CABINETS OR OTHER EQUIPMENT NOT HAVING INTEGRAL THREADED HUBS PROVIDE METALLIC THREADED HUBS OF THE SIZE AND CONFIGURATION REQUIRED. HUB SHALL INCLUDE LOCKNUT AND NEOPRENE O-RING SEAL. PROVIDE IMPACT RESISTANT 105 DEGREE C PLASTIC BUSHINGS TO PROTECT CABLE INSULATION.
- B. CABLE TERMINATION FITTINGS FOR CONDUIT
  - 1. CABLE TERMINATORS FOR RGS CONDUITS SHALL BE TYPE CRC BY O-Z/GEDNEY OR EQUAL BY ROXTEC.
  - 2. CABLE TERMINATORS FOR LFMC SHALL BE ETCO - CL2075; OR MADE FOR THE PURPOSE PRODUCTS BY ROXTEC.
- C. EXTERIOR PULL BOXES AND PULL BOXES IN INTERIOR INDUSTRIAL AREAS SHALL BE PLATED CAST ALLOY, HEAVY DUTY, WEATHERPROOF, DUST PROOF, WITH GASKET, PLATED IRON ALLOY COVER AND STAINLESS STEEL COVER SCREWS, CROUSE-HINDS WAB SERIES OR EQUAL.
- D. CONDUIT OUTLET BODIES SHALL BE PLATED CAST ALLOY WITH SIMILAR GASKET COVERS. OUTLET BODIES SHALL BE OF THE CONFIGURATION AND SIZE SUITABLE FOR THE APPLICATION. PROVIDE CROUSE-HINDS FORM 8 OR EQUAL.
- E. MANUFACTURER FOR BOXES AND COVERS SHALL BE HOFFMAN, SQUARE "D", CROUSE-HINDS, COOPER, ADALET, APPLETON, O-Z GEDNEY, RACO, OR APPROVED EQUAL.

SUPPLEMENTAL GROUNDING SYSTEM:

- A. FURNISH AND INSTALL A SUPPLEMENTAL GROUNDING SYSTEM TO THE EXTENT INDICATED ON THE DRAWINGS. SUPPORT SYSTEM WITH NON-MAGNETIC STAINLESS STEEL CLIPS WITH RUBBER GROMMETS. GROUNDING CONNECTORS SHALL BE TINNED COPPER WIRE, SIZES AS INDICATED ON THE DRAWINGS. PROVIDE STRANDED OR SOLID BARE OR INSULATED CONDUCTORS EXCEPT AS OTHERWISE NOTED.
- B. SUPPLEMENTAL GROUNDING SYSTEM: ALL CONNECTIONS TO BE MADE WITH CAD WELDS, EXCEPT AT EQUIPMENT USE LUGS OR OTHER AVAILABLE GROUNDING MEANS AS REQUIRED BY MANUFACTURER; AT GROUND BARS USE TWO HOLE SPADES WITH NO-OX.
- C. STOLEN GROUND-BARS: IN THE EVENT OF STOLEN GROUND BARS, CONTACT SPRINT CM FOR REPLACEMENT INSTRUCTION USING THREADED ROD KITS.

EXISTING STRUCTURE:

- A. EXISTING EXPOSED WIRING AND ALL EXPOSED OUTLETS, RECEPTACLES, SWITCHES, DEVICES, BOXES, AND OTHER EQUIPMENT THAT ARE NOT TO BE UTILIZED IN THE COMPLETED PROJECT SHALL BE REMOVED OR DE-ENERGIZED AND CAPPED IN THE WALL, CEILING, OR FLOOR SO THAT THEY ARE CONCEALED AND SAFE. WALL, CEILING, OR FLOOR SHALL BE PATCHED TO MATCH THE ADJACENT CONSTRUCTION.

CONDUIT AND CONDUCTOR INSTALLATION:

- A. CONDUITS SHALL BE FASTENED SECURELY IN PLACE WITH APPROVED NON-PERFORATED STRAPS AND HANGERS. EXPLOSIVE DEVICES FOR ATTACHING HANGERS TO STRUCTURE WILL NOT BE PERMITTED. CLOSELY FOLLOW THE LINES OF THE STRUCTURE, MAINTAIN CLOSE PROXIMITY TO THE STRUCTURE AND KEEP CONDUITS IN TIGHT ENVELOPES. CHANGES IN DIRECTION TO ROUTE AROUND OBSTACLES SHALL BE MADE WITH CONDUIT OUTLET BODIES. CONDUIT SHALL BE INSTALLED IN A NEAT AND WORKMANLIKE MANNER, PARALLEL AND PERPENDICULAR TO STRUCTURE WALL AND CEILING LINES. ALL CONDUIT SHALL BE FISHED TO CLEAR OBSTRUCTIONS. ENDS OF CONDUITS SHALL BE TEMPORARILY CAPPED TO PREVENT CONCRETE, PLASTER OR DIRT FROM ENTERING. CONDUITS SHALL BE RIGIDLY CLAMPED TO BOXES BY GALVANIZED MALLEABLE IRON BUSHING ON INSIDE AND GALVANIZED MALLEABLE IRON LOCKNUT ON OUTSIDE AND INSIDE.
- B. CONDUCTORS SHALL BE PULLED IN ACCORDANCE WITH ACCEPTED GOOD PRACTICE.



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*James R. Skowronski* Signature: \_\_\_\_\_ Date: 8/08/2014


A	08/08/14	FINAL CONSTRUCTION DRAWINGS
MARK	DATE	DESCRIPTION

ISSUE PHASE FINAL DATE ISSUED 08/08/2014

PROJECT TITLE:  
 CTS  
 CT03XC360-A

PROJECT INFORMATION:  
 46 FERNWOOD LANE  
 WILTON, CT 06897  
 FAIRFIELD COUNTY

SHEET TITLE:  
 SPRINT SPECIFICATIONS

SCALE: NONE

PROJECT NUMBER	28731
SHEET NUMBER	SP-3



**Sprint**

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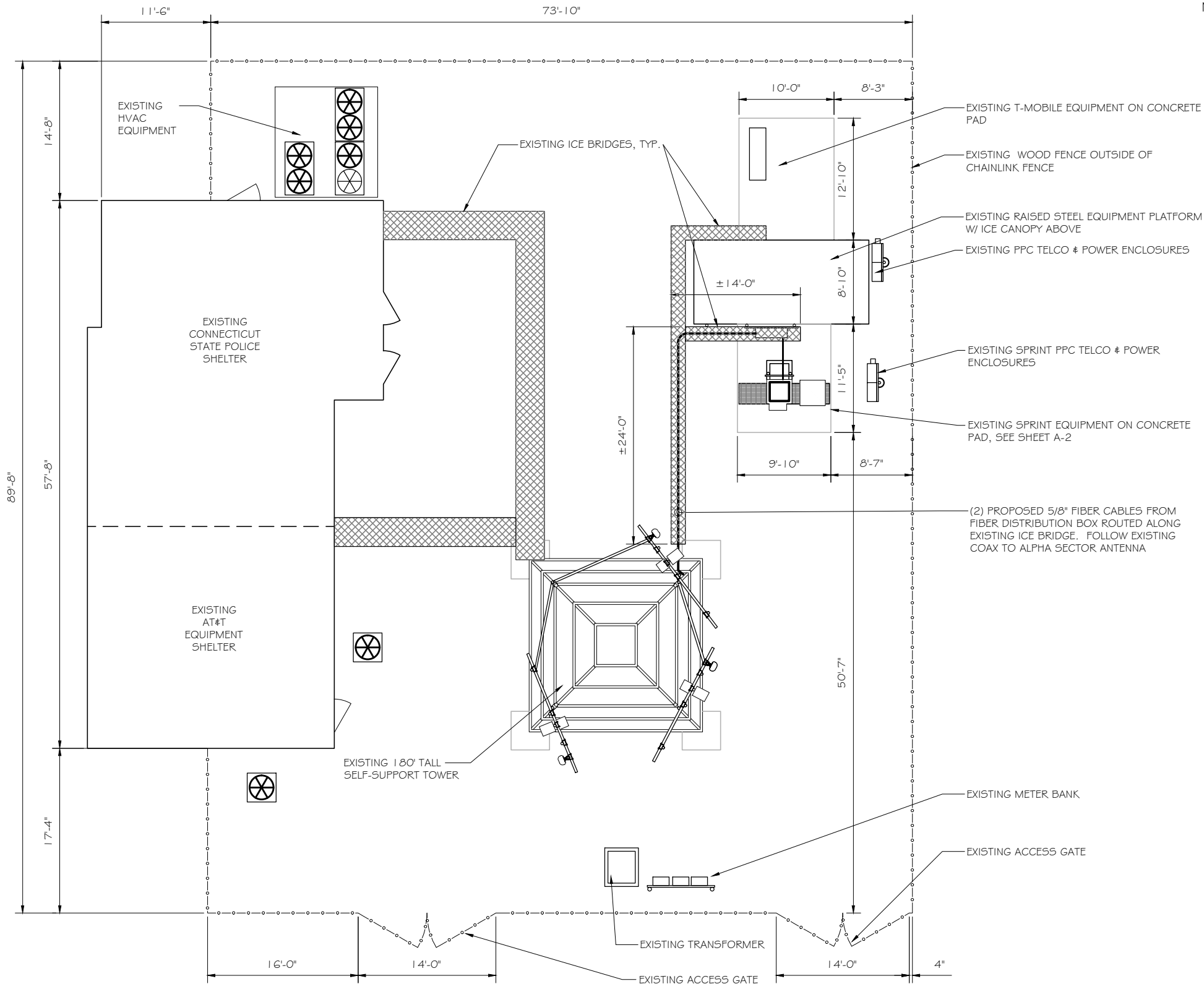


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**SITE PLAN**  
 SCALE: 1" = 12.5'

MARK	DATE	DESCRIPTION
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ISSUE	FINAL	DATE ISSUED 08/08/2014

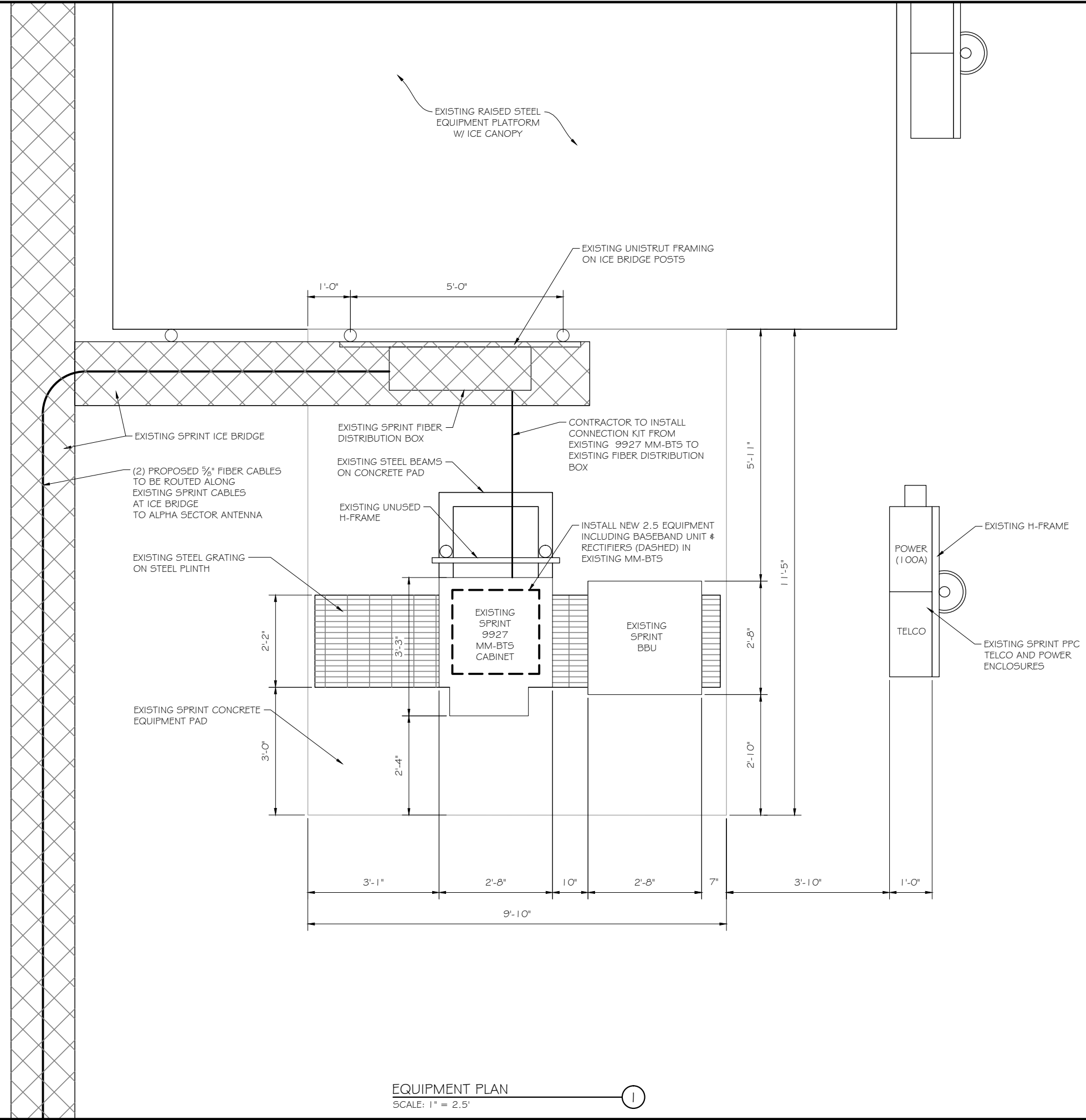
PROJECT TITLE:  
**CTS  
 CT03XC360-A**

PROJECT INFORMATION:  
 46 FERNWOOD LANE  
 WILTON, CT 06897  
 FAIRFIELD COUNTY

SHEET TITLE:  
**SITE PLAN**

11" x 17" - 1" = 12.5'  
 22" x 34" - 1" = 6.25'

PROJECT NUMBER: **28731**  
 SHEET NUMBER: **A-1**



**EQUIPMENT PLAN**  
 SCALE: 1" = 2.5'



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PROJECT TITLE:

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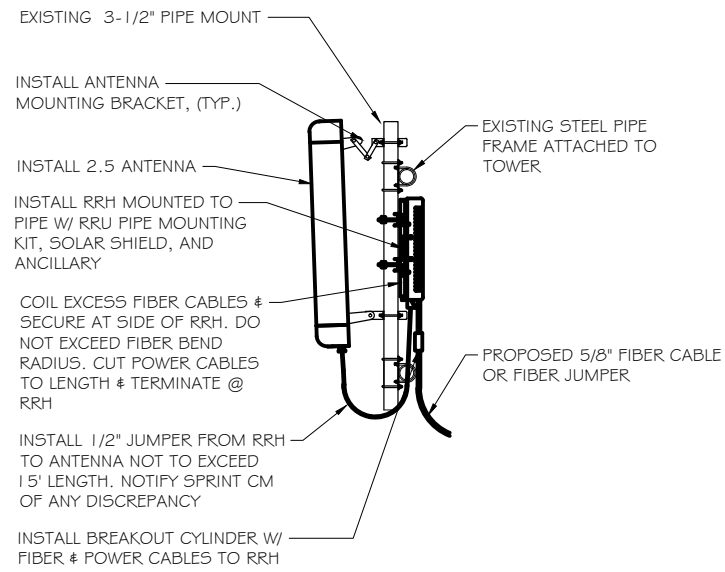
PROJECT INFORMATION:  
 46 FERNWOOD LANE  
 WILTON, CT 06897  
 FAIRFIELD COUNTY

SHEET TITLE:  
**EQUIPMENT PLAN**

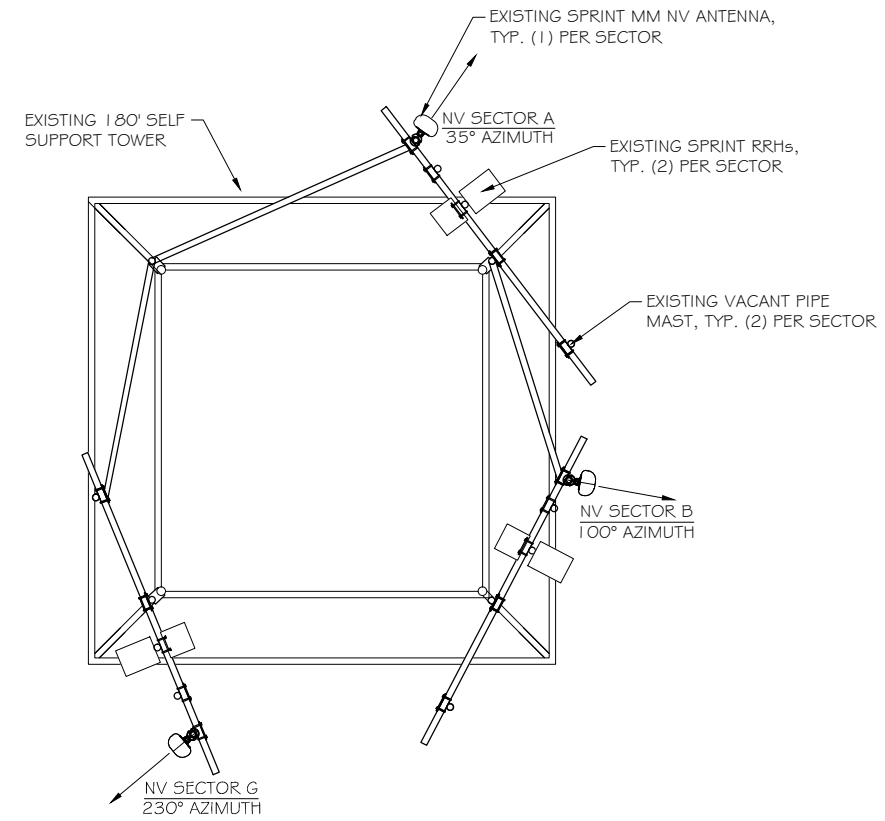
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11" x 17" - 1" = 2.5'  
 22" x 34" - 1" = 1.25'

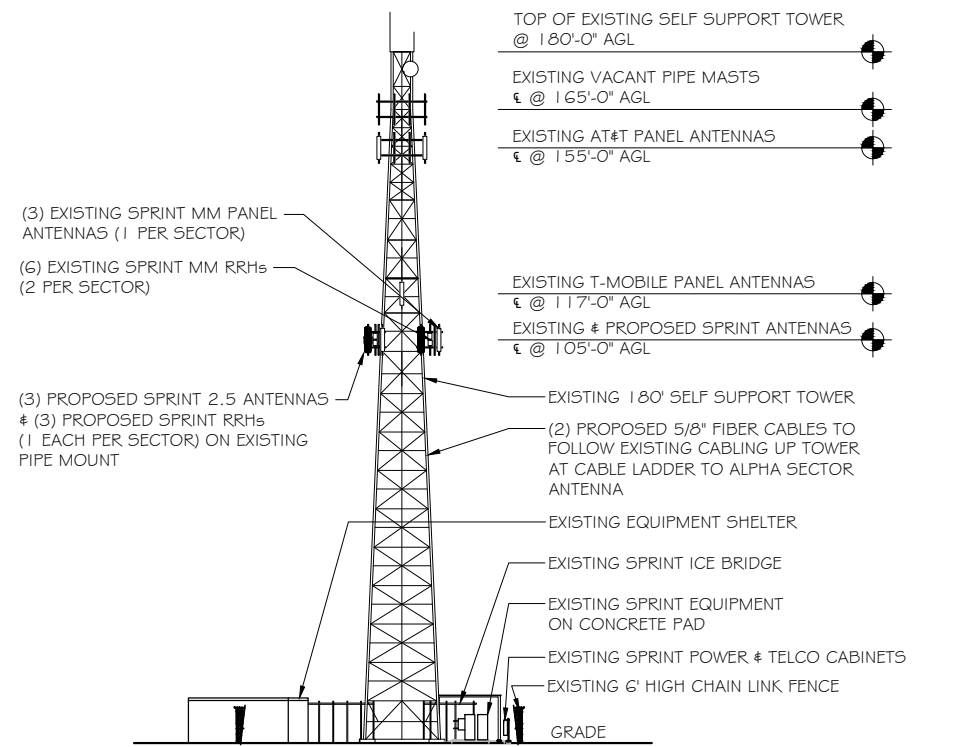
PROJECT NUMBER	28731
SHEET NUMBER	A-2



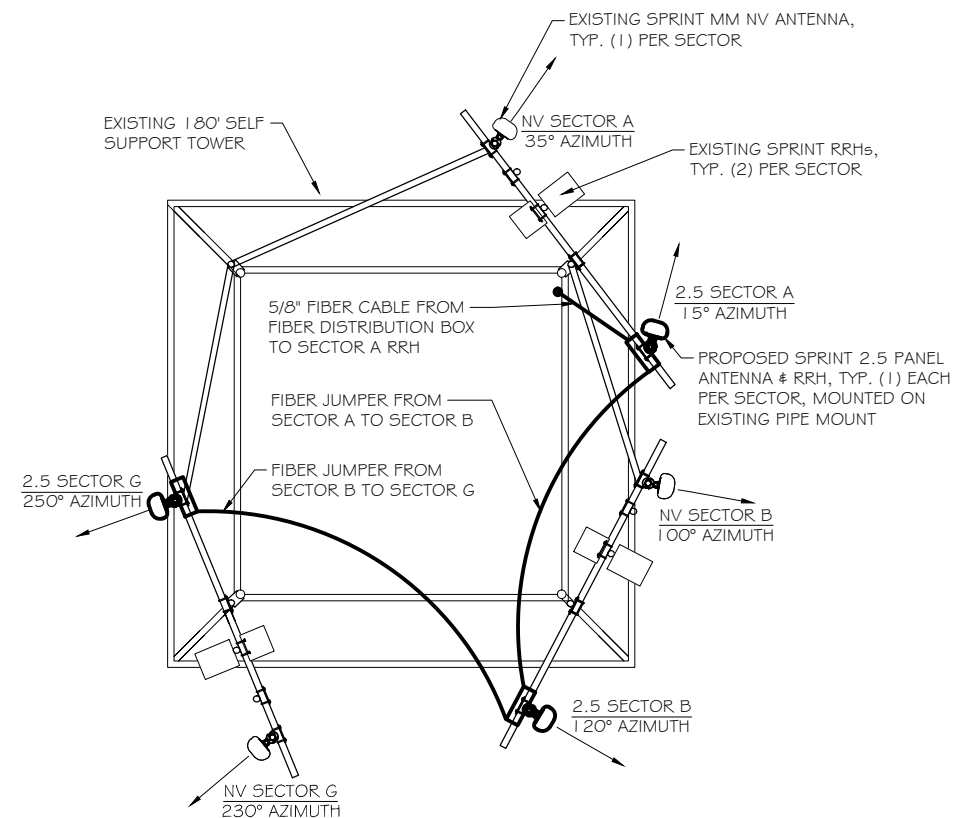
ANTENNA & RRH MOUNTING DETAILS  
 SCALE: NTS



EXISTING ANTENNA ARRAY  
 SCALE: NTS



BUILDING ELEVATION  
 SCALE: 1" = 50'



PROPOSED ANTENNA ARRAY  
 SCALE: NTS



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 46 FERNWOOD LANE  
 WILTON, CT 06897  
 FAIRFIELD COUNTY

SHEET TITLE:  
**BUILDING ELEVATIONS &  
 ANTENNA DETAILS**

SCALE:  
 AS NOTED

PROJECT NUMBER: 28731  
 SHEET NUMBER: A-3





**RFDS Sheet**

**General Site Information**

Site ID	CT03XC360	Equipment Vendor	Alcatel-Lucent
Market	Southern Connecticut	Latitude	41.1724393
Region	Northeast	Longitude	-73.4343597
MLA	N/A	LL SITE ID	N/A
Structure Type	Lattice Tower		
BTS Type			

Solution ID		Siterra SR Equipment type		Incremental Power Draw needed by added Equipment	
		Equipment Vendor	Alcatel-Lucent		N/A

**Base Equipment**

BBU Kit	ALU BBU Kit	Top Hat	None
BBU Kit Qty	1	Top Hat Qty	N/A
Growth Cabinet	None	Top Hat Dimensions	N/A
Growth Cabinet Qty	N/A	Top Hat Weight (lbs)	N/A
Growth Cabinet Dimensions	N/A		
Growth Cabinet Weight	N/A		

**RF Path Information**

RRH	TD-RRH8x20-25
RRH Qty	3
RRH Dimensions	25.4"x17.5"x5.7"
RRH Weight. lbs.	66
RRH Mount Weight. Lbs.	TBD
Power and Fiber Cable	ALU Fiber Only
Cable Qty	2
Weight per foot. Lbs.	0.242
Diameter. Inches.	0.73
Length Ft.	175' (calculated as antenna height plus 20%)
Coax Jumper	TBD
Coax Jumper Qty	27
Coax Jumper Length. Feet.	8
Coax Jumper Weight	TBD
Coax Jumper Diameter. Inches	0.5
AISG Cable	Commscope ATCB-B01-006
AISG Cable Qty	3
AISG Diameter. Inches.	0.315
AISG Cable length.	8
Weight of entire AISG cable. Lbs.	1.3

**Antenna Sector Information**

	Sector 1	Sector 2	Sector 3
Antenna make/model	RFS APXVTM14-C-120	RFS APXVTM14-C-120	RFS APXVTM14-C-120
Antenna qty	1	1	1
Antenna Dimensions. Inches	56.3"x12.6"x7.9"	56.3"x12.6"x7.9"	56.3"x12.6"x7.9"
Antenna Weight. Lbs	54	54	54
Antenna Mounting Kit Weight. Lbs.	11	11	11
CL Height	105	105	105
Antenna Azimuth	15	120	250
Antenna Mechanical Downtilt	0	0	0
Antenna etilt	-2	-2	-2

\*RFDS SHEET WAS GENERATED BY RAMAKER & ASSOCIATES FROM PLAN OF RECORD (POR) PROVIDED BY SPRINT. CONTRACTOR SHALL VERIFY AND OBTAIN FINAL RFDS FROM SPRINT CONSTRUCTION MANAGER PRIOR TO CONSTRUCTION.



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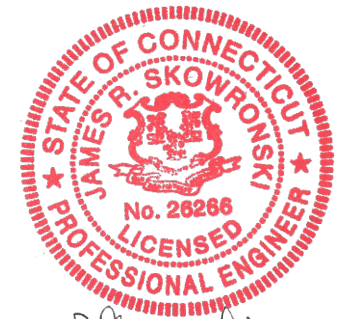


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**NOTES:**

- GENERAL CONTRACTOR TO FIELD VERIFY AZIMUTH AND C/L HEIGHT AND MECHANICAL DOWNTILT. IF DIFFERENT THAN CALLED OUT BELOW, HALT ANTENNA WORK FOR ONE HOUR, CALL SPRINT RF ENGINEER (OR MANAGER IF RF ENGINEER DOES NOT ANSWER, BUT STILL LEAVE A MESSAGE TO RF ENGINEER) USING CONTACT INFORMATION ABOVE FOR FURTHER INSTRUCTIONS. IF SPRINT DOES NOT RESPOND WITHIN ONE HOUR, PLACE 2.5GHZ ANTENNA AT SAME C/L HEIGHT AS 1.9GHZ ANTENNA AND EMAIL CORRECT C/L HEIGHT AND AZIMUTH TO SPRINT RF ENGINEER. UPDATE AS-BUILT DRAWING WITH CORRECT C/L HEIGHT. ALSO EMAIL CORRECT 1.9GHZ AND 800MHZ ANTENNA C/L HEIGHT, AZIMUTH AND MECHANICAL DOWNTILT TO RF ENGINEER.
- AISG TESTS TO VERIFY OPERATION IS TO BE PERFORMED AFTER FINAL INSTALLATION OF ANTENNAS AND AISG CABLES HAVE BEEN CONNECTED. VERIFY OPERATION OF ALL EXISTING SPRINT AISG EQUIPMENT INCLUDING 800MHZ, 1.9GHZ AND 2.5GHZ. TEST TO INCLUDE COMPLETE DOWNTILT, AZIMUTH (IF APPLICABLE) AND BEAMWIDTH SWINGS (IF APPLICABLE). DOCUMENT AISG TEST RESULTS IN COAX SWEEP TEST SPREADSHEET.
- GENERAL CONTRACTOR MUST ENSURE THAT NO OBJECT IS LOCATED WITHIN 45 DEGREES OF LEFT AND RIGHT OF FRONT OF ANTENNA OR 7 DEGREES UP AND DOWN FROM CENTER OF ANTENNA. IF THIS IS NOT POSSIBLE, CONTACT RF ENGINEER FOR FURTHER INSTRUCTION. IN ADDITION, 2.5GHZ ANTENNA IS NOT TO BE PLACED IN FRONT OF ANY OTHER ANTENNA USING THE SAME 45 DEGREE RULE. THIS INCLUDES SPRINT AND NON-SPRINT ANTENNAS.
- 2.5GHZ ANTENNA MUST BE AT LEAST 6" FROM 1.9GHZ ANTENNA, 30" FROM 800MHZ ANTENNA AND 30" FROM DUAL BAND 1.9GHZ AND 800MHZ ANTENNA.
- GENERAL CONTRACTOR IS REQUIRED TO USE A DIGITAL ALIGNMENT TOOL TO SET AZIMUTH, ROLL AND DOWNTILT. AZIMUTH ACCURACY IS TO BE WITHIN 1 DEGREE. DOWNTILT AND ROLL (LEFT TO RIGHT TILT) IS TO BE WITHIN 0.1 DEGREES. IF FOR SOME REASON THIS ACCURACY CANNOT BE ACHIEVED, UPDATE AS-BUILT DRAWINGS AND EMAIL SPRINT RF ENGINEER WITH AS-BUILT SETTINGS. USE 3Z RF ALIGNMENT TOOL OR EQUIVALENT TOOL.

MARK	DATE	DESCRIPTION
A	08/08/14	FINAL CONSTRUCTION DRAWINGS

ISSUE	FINAL	DATE	08/08/2014
PHASE		ISSUED	

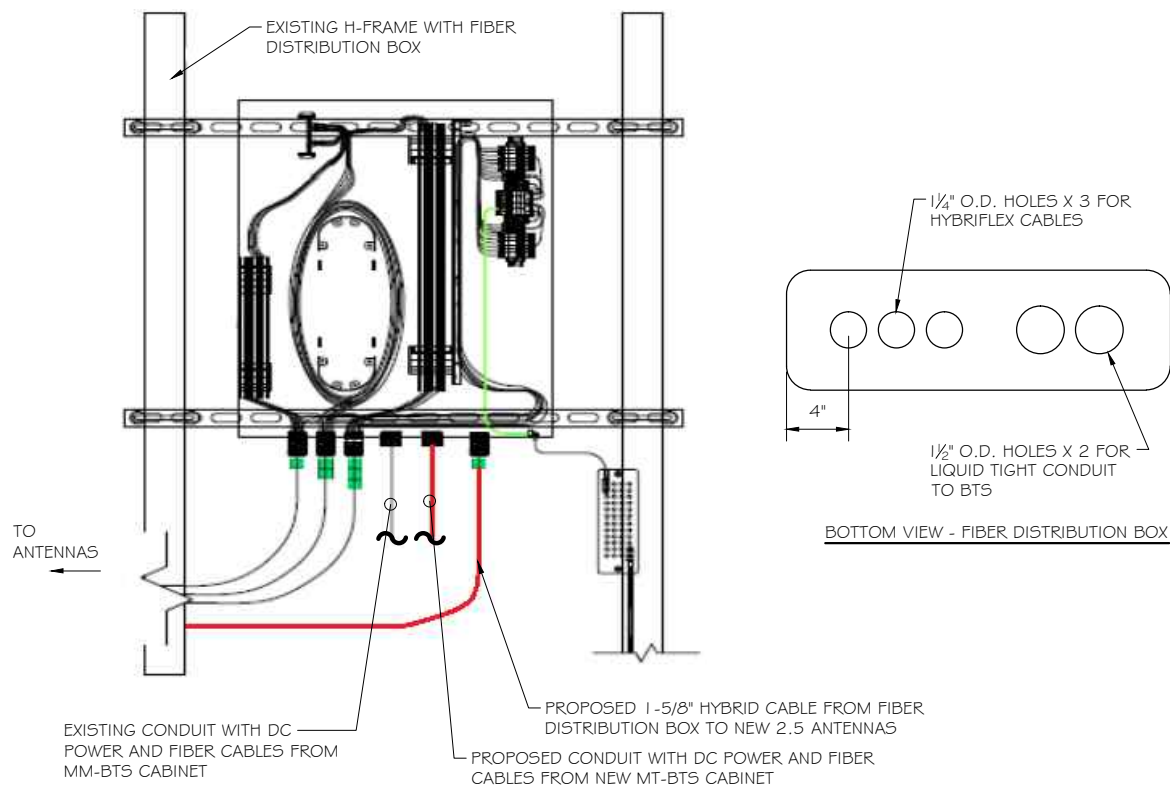
PROJECT TITLE:  
 CTS  
 CT03XC360-A

PROJECT INFORMATION:  
 46 FERNWOOD LANE  
 WILTON, CT 06897  
 FAIRFIELD COUNTY

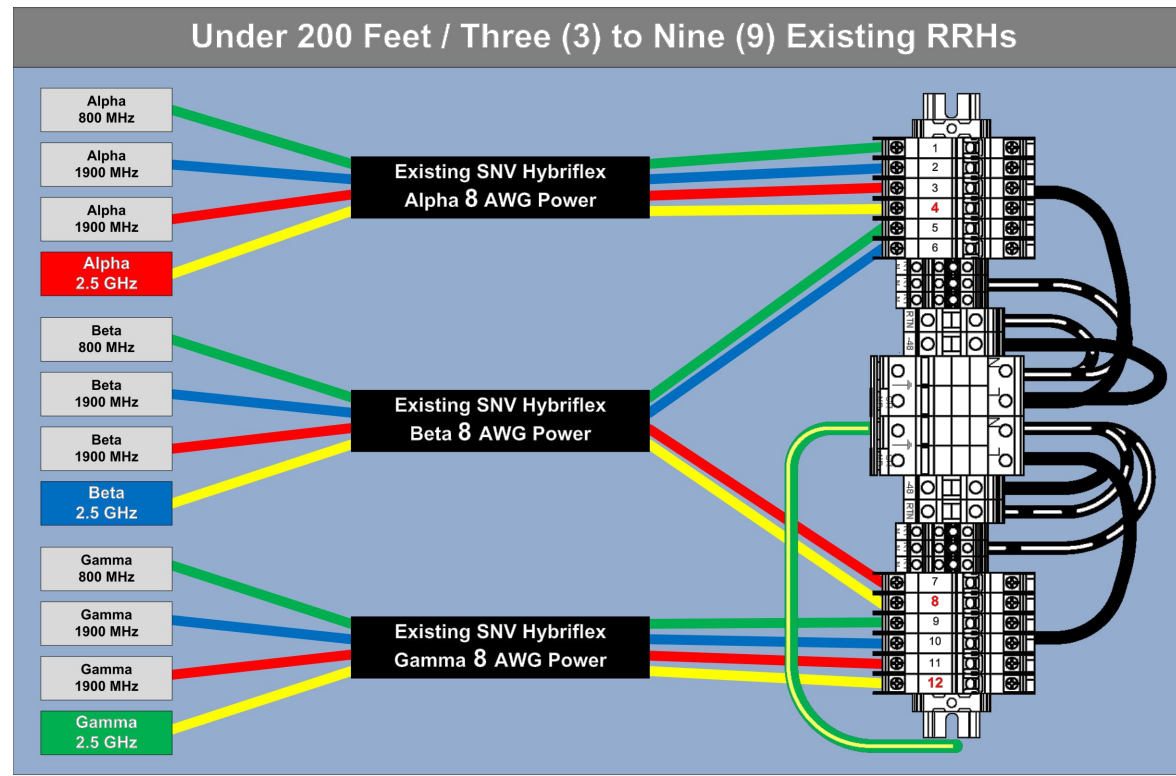
SHEET TITLE:  
 RF DATA SHEET

SCALE:  
 AS NOTED

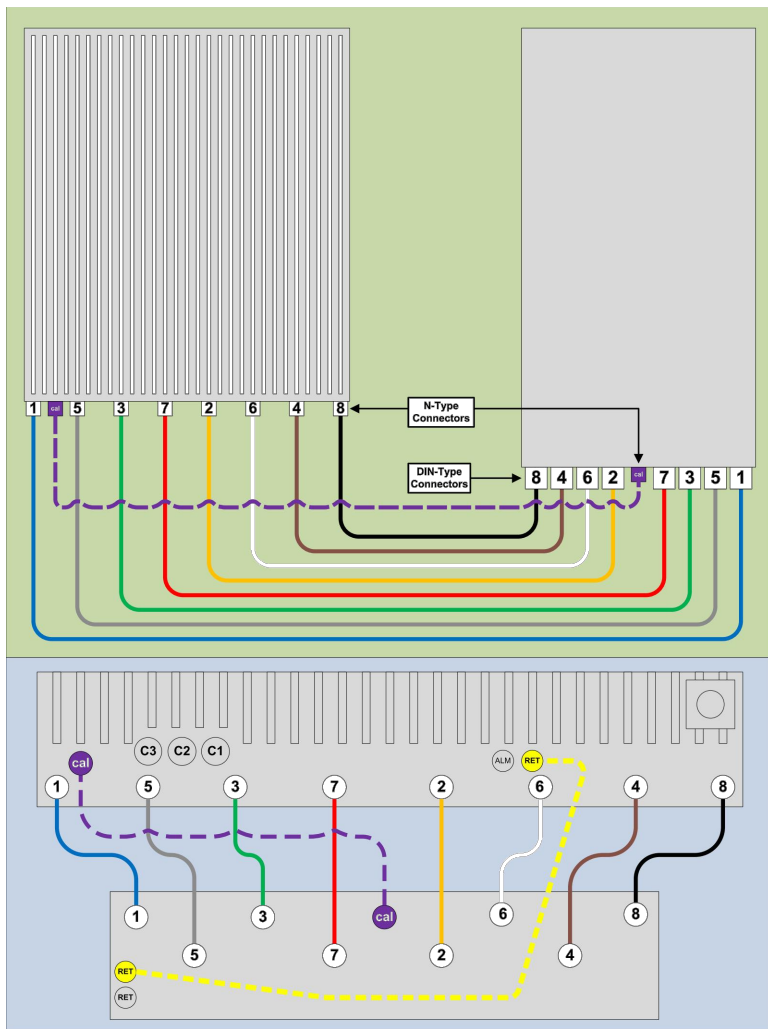
PROJECT NUMBER: 28731  
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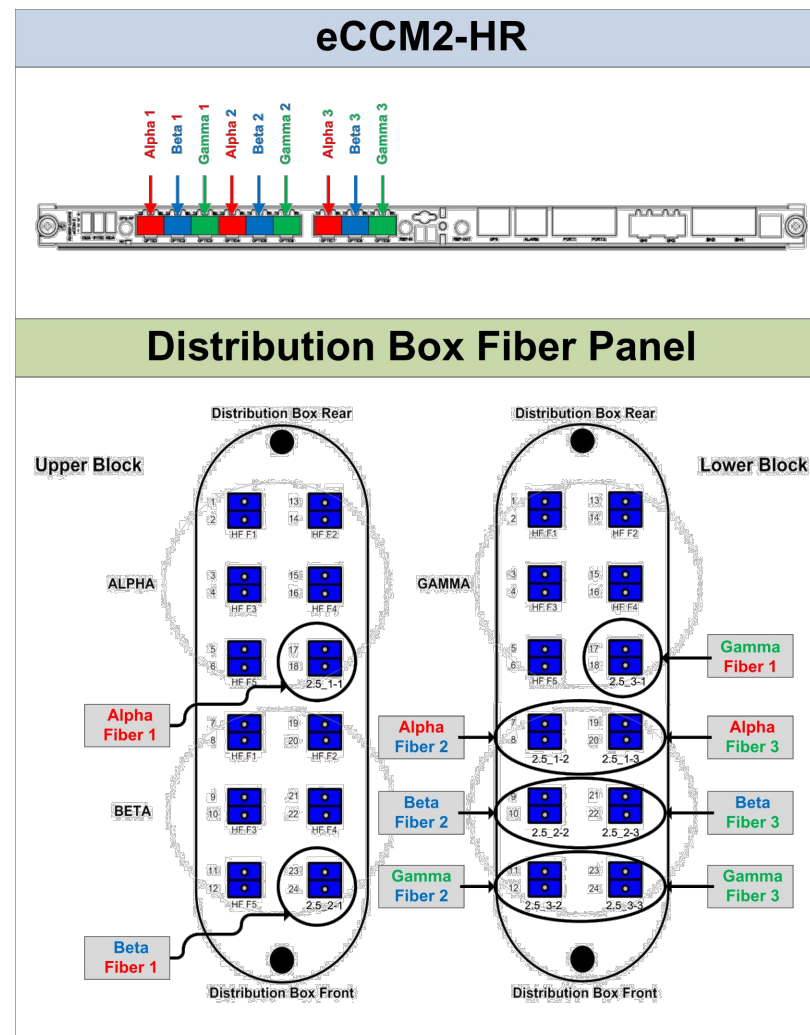
TYPICAL FIBER DISTRIBUTION BOX DETAIL  
 SCALE: NTS



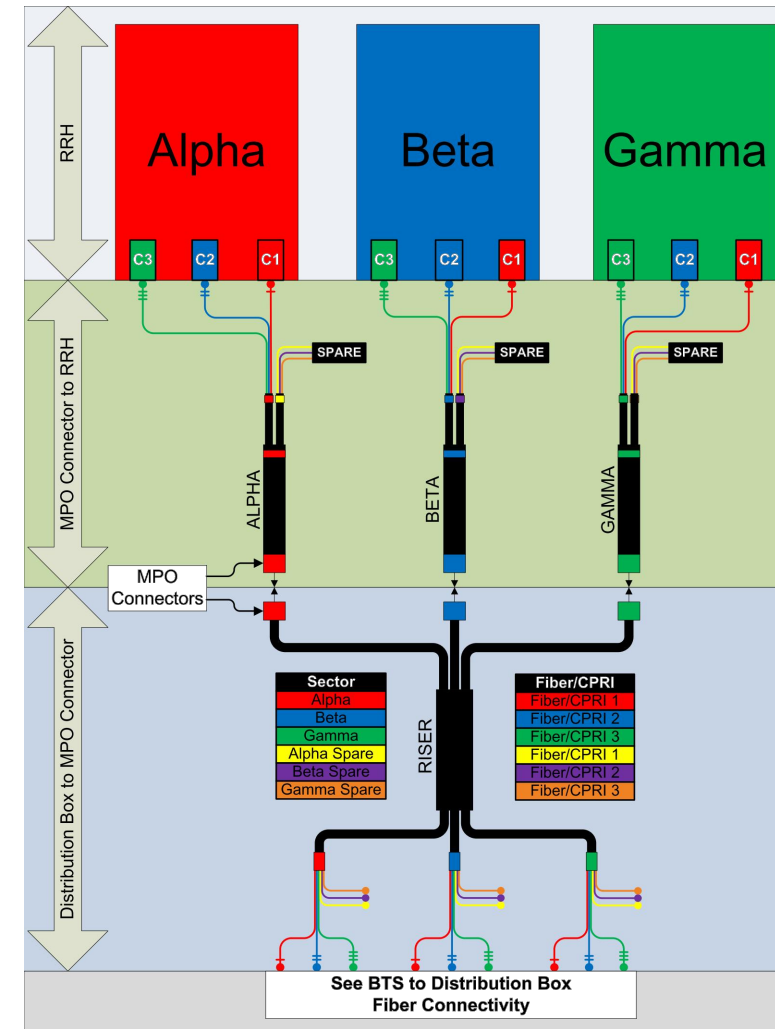
RRH TO DISTRIBUTION BOX POWER CONNECTIVITY DETAIL  
 SCALE: NTS



8T8R DETAIL  
 SCALE: NTS



BTS TO DISTRIBUTION BOX FIBER CONNECTIVITY DETAIL  
 SCALE: NTS



RRH TO DISTRIBUTION BOX FIBER CONNECTIVITY DETAIL  
 SCALE: NTS



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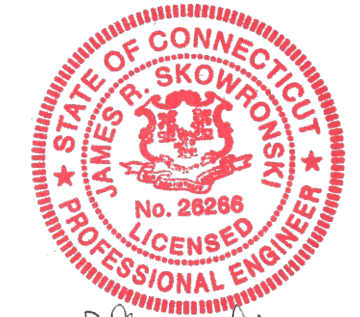


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FIBER PLUMBING DIAGRAM

SCALE:  
 AS NOTED

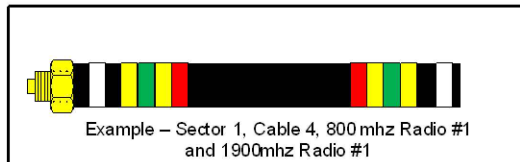
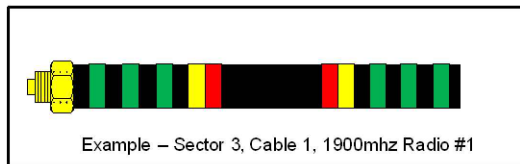
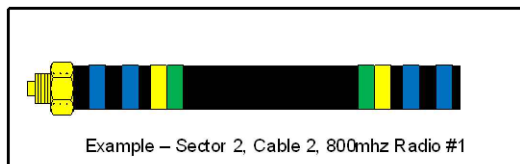
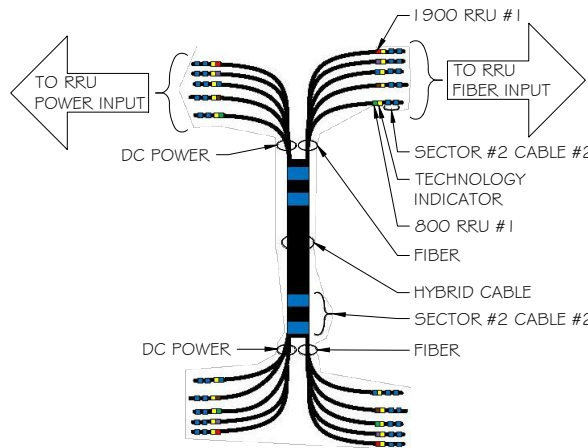
PROJECT NUMBER: 28731  
 SHEET NUMBER: A-5



2.5 FREQUENCY	INDICATOR		ID
2500 -1	YEL	WHT	GRN
2500 -2	YEL	WHT	RED
2500 -3	YEL	WHT	BRN
2500 -4	YEL	WHT	BLU
2500 -5	YEL	WHT	SLT
2500 -6	YEL	WHT	ORG
2500 -7	YEL	WHT	WHT
2500 -8	YEL	WHT	PPL

NV FREQUENCY	INDICATOR	ID
800-1	YEL	GRN
1900-1	YEL	RED
1900-2	YEL	BRN
1900-3	YEL	BLU
1900-4	YEL	SLT
800-1	YEL	ORG
RESERVED	YEL	WHT
RESERVED	YEL	PPL

Sector	Cable	First Ring	Second Ring	Third Ring
<b>1 Alpha</b>	<b>1</b>	Green	No Tape	No Tape
<b>1</b>	<b>2</b>	Blue	No Tape	No Tape
<b>1</b>	<b>3</b>	Brown	No Tape	No Tape
<b>1</b>	<b>4</b>	White	No Tape	No Tape
<b>1</b>	<b>5</b>	Red	No Tape	No Tape
<b>1</b>	<b>6</b>	Grey	No Tape	No Tape
<b>1</b>	<b>7</b>	Purple	No Tape	No Tape
<b>1</b>	<b>8</b>	Orange	No Tape	No Tape
<b>2 Beta</b>	<b>1</b>	Green	Green	No Tape
<b>2</b>	<b>2</b>	Blue	Blue	No Tape
<b>2</b>	<b>3</b>	Brown	Brown	No Tape
<b>2</b>	<b>4</b>	White	White	No Tape
<b>2</b>	<b>5</b>	Red	Red	No Tape
<b>2</b>	<b>6</b>	Grey	Grey	No Tape
<b>2</b>	<b>7</b>	Purple	Purple	No Tape
<b>2</b>	<b>8</b>	Orange	Orange	No Tape
<b>3 Gamma</b>	<b>1</b>	Green	Green	Green
<b>3</b>	<b>2</b>	Blue	Blue	Blue
<b>3</b>	<b>3</b>	Brown	Brown	Brown
<b>3</b>	<b>4</b>	White	White	White
<b>3</b>	<b>5</b>	Red	Red	Red
<b>3</b>	<b>6</b>	Grey	Grey	Grey
<b>3</b>	<b>7</b>	Purple	Purple	Purple
<b>3</b>	<b>8</b>	Orange	Orange	Orange



COLOR CODING CHARTS  
SCALE: NTS

CABLE MARKING NOTES

- ALL CABLES SHALL BE MARKED WITH 2" WIDE, UV STABILIZED, UL APPROVED TAPE.
- THE FIRST RING SHALL BE CLOSEST TO THE END OF THE CABLE AND SPACED APPROXIMATELY 2" FROM THE END CONNECTOR, WEATHERPROOFING, OR BREAKOUT UNIT. THERE SHALL BE 1" SPACE BETWEEN EACH RING.
- A 2" GAP SHALL SEPARATE THE CABLE COLOR CODE FROM THE FREQUENCY COLOR CODE. THE 2" COLOR RINGS FOR THE FREQUENCY CODE SHALL BE PLACED NEXT TO EACH OTHER WITH NO SPACES.
- THE 2" COLORED TAPE(S) SHALL BE WRAPPED A MINIMUM OF 3 TIMES AROUND THE INDIVIDUAL CABLES, AND THE TAPE SHALL BE KEPT IN THE SAME LOCATION AS MUCH AS POSSIBLE.
- SITES WITH MORE THAN FOUR (4) SECTORS WILL REQUIRE ADDITIONAL RINGS FOR EACH SECTOR, FOLLOWING THE PATTERN. HIGH CAPACITY SITES WILL USE THE SECOND CABLE IDENTIFIED BY BLUE BANDS OF TAPE
- HYBRID FIBER CABLE SHALL BE SECTOR IDENTIFIED INSIDE THE CABINET ON FREQUENCY BUNDLES, ON THE SEALTITE, ON THE MAIN LINE UPON EXIT OF SEALTITE, AND BEFORE AND AFTER THE BREAKOUT UNIT (MEDUSA), AS WELL AS BEFORE AND AFTER ANY ENTRANCE OR EXIT.
- HFC "MAIN TRUNK" WILL NOT BE MARKED WITH THE FREQUENCY CODES, AS IT CONTAINS ALL FREQUENCIES.
- INDIVIDUAL POWER PAIRS AND FIBER BUNDLES SHALL BE LABELED WITH BOTH THE CABLE AND FREQUENCY.



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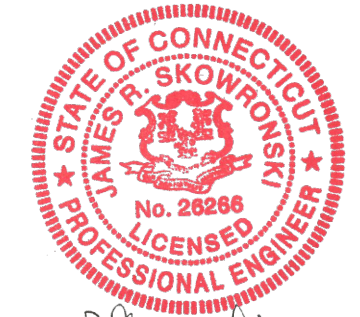


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**CTS  
CT03XC360-A**

PROJECT INFORMATION:  
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WILTON, CT 06897  
FAIRFIELD COUNTY

SHEET TITLE:  
**CABLE COLOR CODING**

SCALE:  
AS NOTED

PROJECT NUMBER: 28731  
SHEET NUMBER: A-6

HYBRID CABLE DC CONDUCTOR SIZE GUIDELINE  
 MANUF:RFS

CABLE	LENGTH	DC CONDUCTOR	CABLE DIAMETER
*Fiber Only	Varies	Use NV Hybriflex	5/8"
Hybriflex	<200'	8 AWG	1-1/4"
Hybriflex	225-300'	6 AWG	1-1/4"
Hybriflex	325-375'	4 AWG	1-1/4"

RFS HYBRIFLEX RISER CABLE SCHEDULE

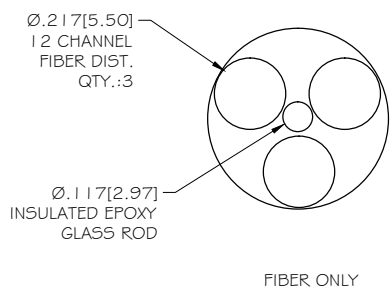
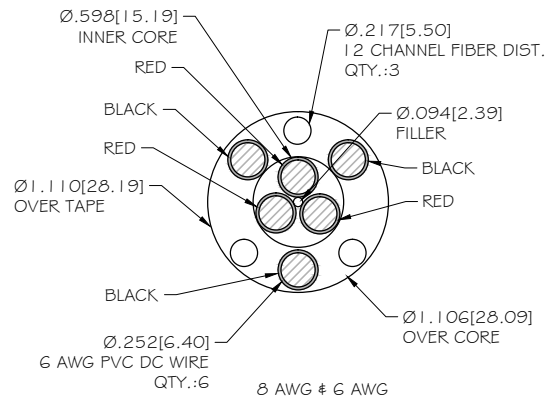
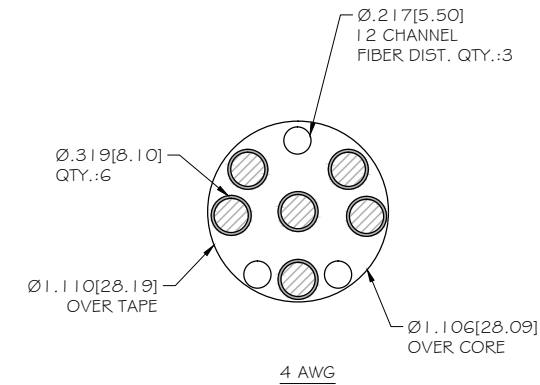
FIBER ONLY (EXISTING DC POWER)	Hybrid cable	
	MN:HB058-M12-050F 12x multi-mode fiber pairs, Top:Outdoor protected connectors, Bottom:LC Connectors, 5/8 cable, 50 ft	50 ft
	MN:HB058-M12-075F	75 ft
	MN:HB058-M12-100F	100 ft
	MN:HB058-M12-125F	125 ft
	MN:HB058-M12-150F	150 ft
	*MN:HB058-M12-175F	175 ft
	MN:HB058-M12-200F	200 ft
8 AWG Power	Hybrid cable	
	MN:HB114-08U3M12-050F 3x 8 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC connectors. 1 1/4 cable, 50 ft	50 ft
	MN:HB114-08U3M12-075F	75 ft
	MN:HB114-08U3M12-100F	100 ft
	MN:HB114-08U3M12-125F	125 ft
	MN:HB114-08U3M12-150F	150 ft
	MN:HB114-08U3M12-175F	175 ft
	MN:HB114-08U3M12-200F	200 ft
6 AWG Power	Hybrid cable	
	MN:HB114-13U3M12-225F 3x 6 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC connectors. 1 1/4 cable, 225 ft	225 ft
	MN:HB114-13U3M12-250F	250 ft
	MN:HB114-13U3M12-275F	275 ft
	MN:HB114-13U3M12-300F	300 ft
4 AWG Power	Hybrid cable	
	MN:HB114-21U3M12-325F 3x 4 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC connectors. 1 1/4 cable, 325 ft	325 ft
	MN:HB114-21U3M12-350F	350 ft
	MN:HB114-21U3M12-375F	375 ft

RFS HYBRIFLEX JUMPER CABLE SCHEDULE

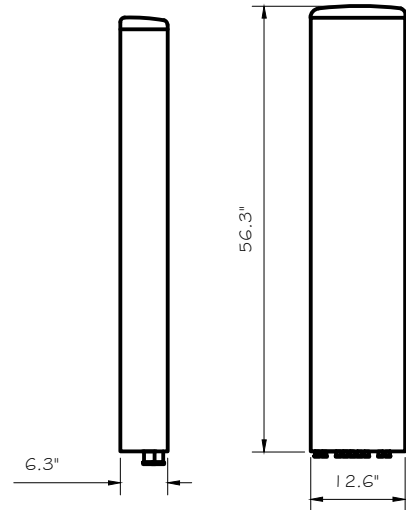
FIBER ONLY	Hybrid Jumper cable	
	MN:HBF012-M3-5F1 5 ft, 3x multi-mode fiber pairs, Outdoor & LC connectors, 1/2 cable	5 ft
	MN:HBF012-M3-10F1	10 ft
	*MN:HBF012-M3-15F1	15 ft
	MN:HBF012-M3-20F1	20 ft
	MN:HBF012-M3-30F1	30 ft
8 AWG POWER	Hybrid Jumper cable	
	MN:HBF058-08U1M3-5F1 5 ft, 1x 8 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC connectors, 5/8 cable	5 ft
	MN:HBF058-08U1M3-10F1	10 ft
	MN:HBF058-08U1M3-15F1	15 ft
	SPECIAL INSTALLATION NOTE: JUMPERS FROM 2.5 RRH TO 2.5 ANTENNA SHALL NOT EXCEED 15' NOTIFY SPRINT CM OF ANY DISCREPANCY	
6 AWG POWER	Hybrid Jumper cable	
	MN:HBF058-13U1M3-5F1 5 ft, 1x 6 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC connectors, 5/8 cable	5 ft
	MN:HBF058-13U1M3-10F1	10 ft
	MN:HBF058-13U1M3-15F1	15 ft
	SPECIAL INSTALLATION NOTE: JUMPERS FROM 2.5 RRH TO 2.5 ANTENNA SHALL NOT EXCEED 15' NOTIFY SPRINT CM OF ANY DISCREPANCY	
4 AWG POWER	Hybrid Jumper cable	
	MN:HBF078-21U1M3-5F1 5 ft, 1x 4 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC connectors, 7/8 cable	5 ft
	MN:HBF078-21U1M3-10F1	10 ft
	MN:HBF078-21U1M3-15F1	15 ft
	SPECIAL INSTALLATION NOTE: JUMPERS FROM 2.5 RRH TO 2.5 ANTENNA SHALL NOT EXCEED 15' NOTIFY SPRINT CM OF ANY DISCREPANCY	

\*NOTE: SPRINT CM TO CONFIRM HYBRID/FIBER RISER CABLE & HYBRID/FIBER JUMPER CABLE MODEL NUMBERS BEFORE PREPARING BOM.

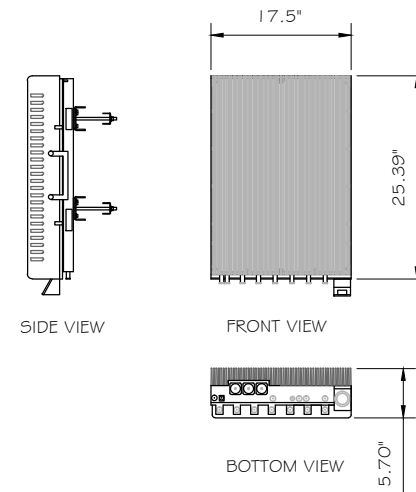
FIBER CABLE CROSS SECTION & DATA  
 SCALE: NTS



DIMENSIONS, HxWxD: 56.3" x 12.6" x 6.3"  
 WEIGHT, WITHOUT PRE-MOUNTED BRACKETS: 55.12 lbs  
 CONNECTOR: (9) MINI-DIN FEMALE/BOTTOM



2.5 ANTENNA DETAIL  
 SCALE: NTS



ALCATEL-LUCENT: TD-RRH8x20

HxWxD = (25.3" x 17.5" x 5.7")

WEIGHT = 66.13 lbs.

2.5 RRH DETAIL  
 SCALE: NTS



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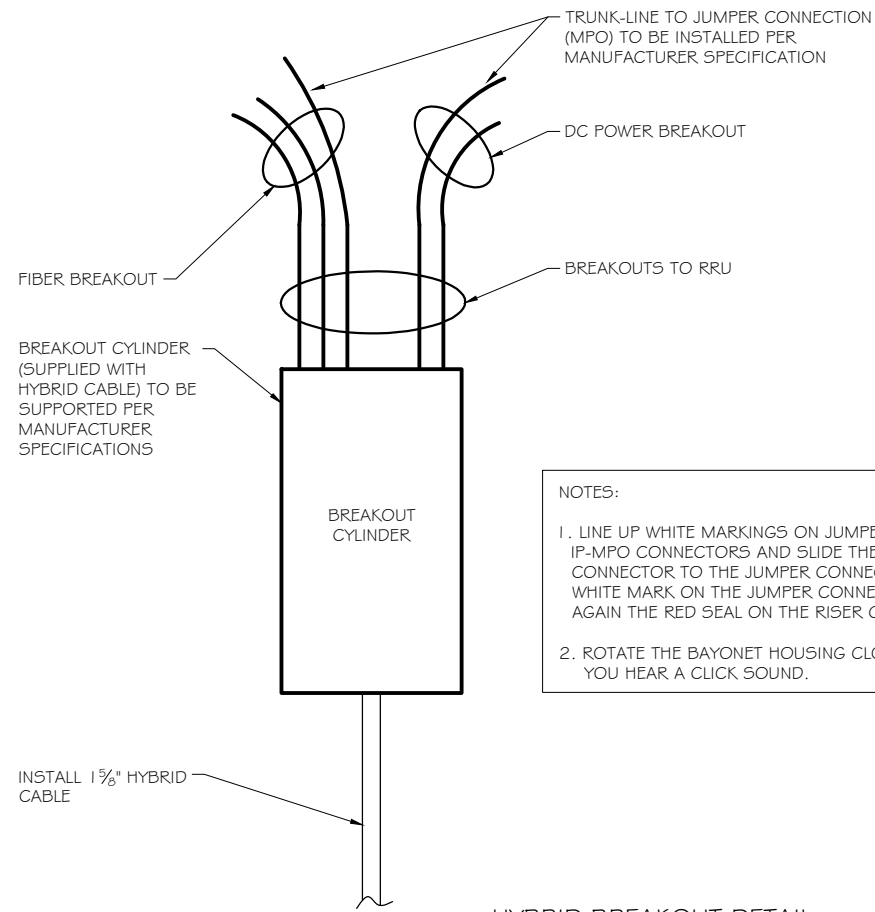
PROJECT INFORMATION:  
 46 FERNWOOD LANE  
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SHEET TITLE:  
 ANTENNA & HYBRID CABLE  
 DETAILS

SCALE:  
 AS NOTED

PROJECT NUMBER: 28731  
 SHEET NUMBER: A-7

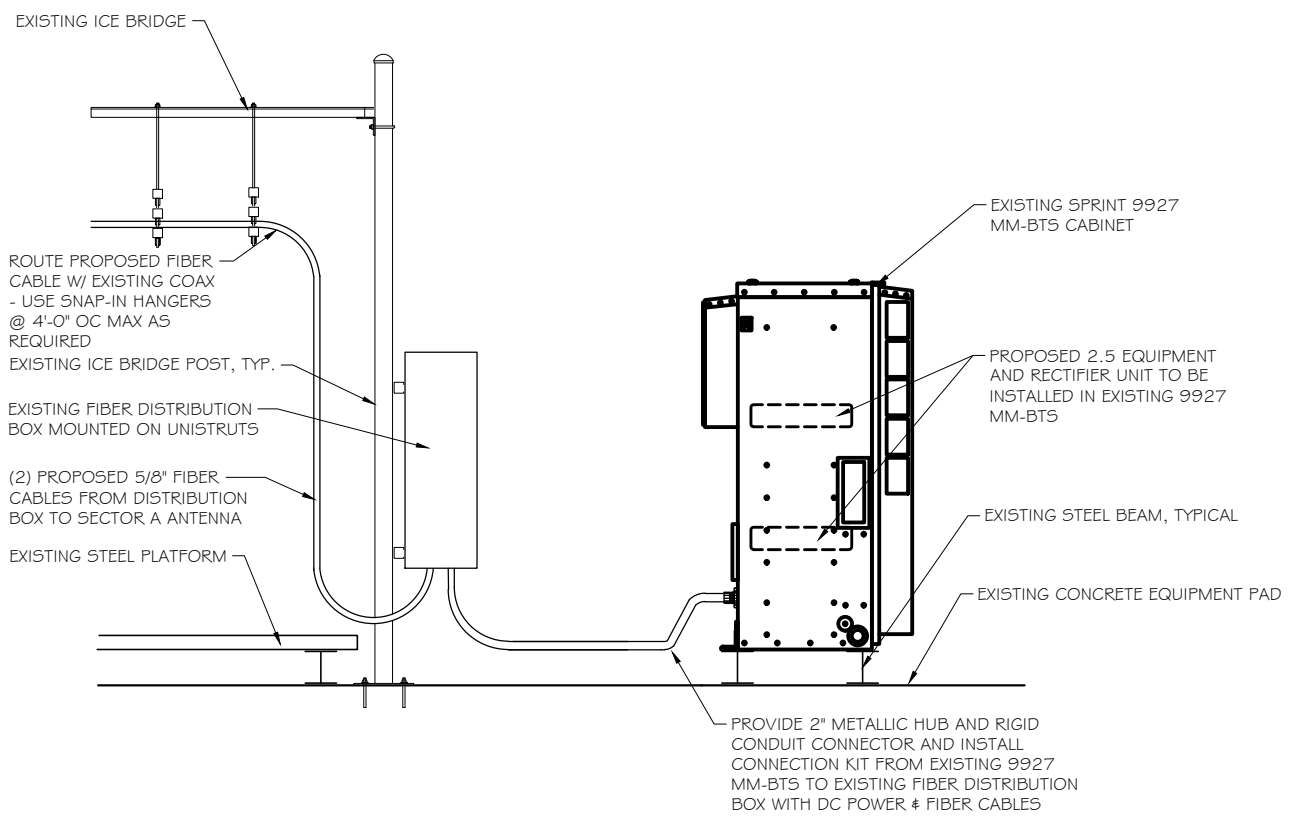




NOTES:

1. LINE UP WHITE MARKINGS ON JUMPER AND RISER IP-MPO CONNECTORS AND SLIDE THE RISER CONNECTOR TO THE JUMPER CONNECTOR. PUSH THE WHITE MARK ON THE JUMPER CONNECTOR FLUSH AGAIN THE RED SEAL ON THE RISER CONNECTOR.
2. ROTATE THE BAYONET HOUSING CLOCKWISE UNTIL YOU HEAR A CLICK SOUND.

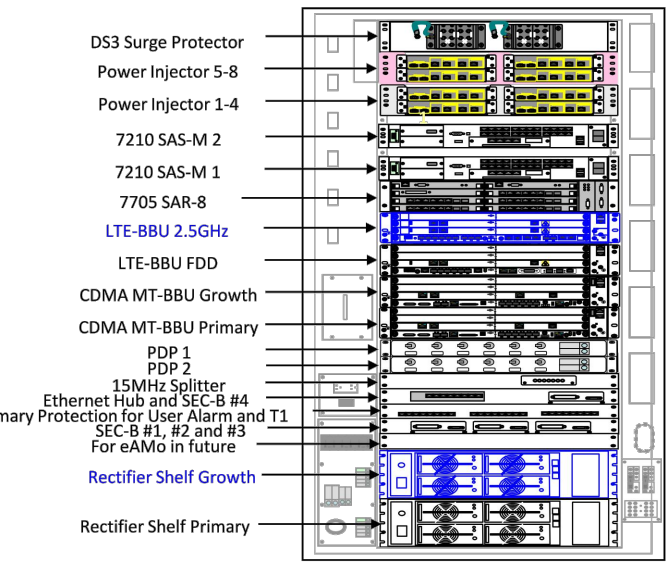
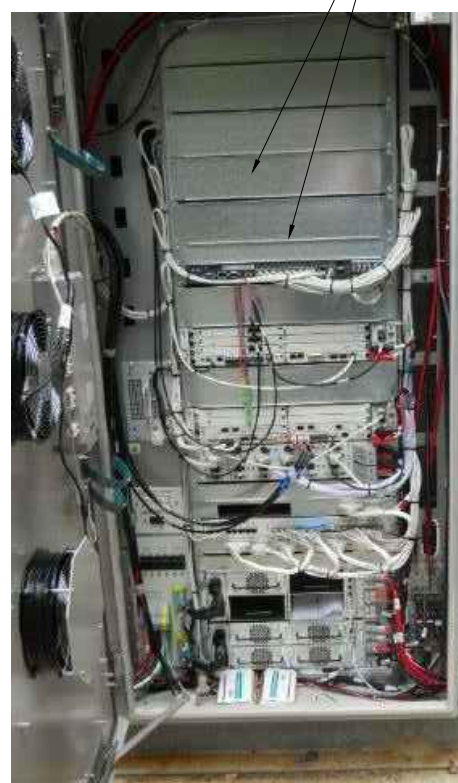
HYBRID BREAKOUT DETAIL ①  
 SCALE: NTS



CABLE ROUTE FROM CABINET ②  
 SCALE: NTS



EXISTING BBU CABINET ③  
 SCALE: NTS



EXISTING MMBS CABINET ④  
 SCALE: NTS



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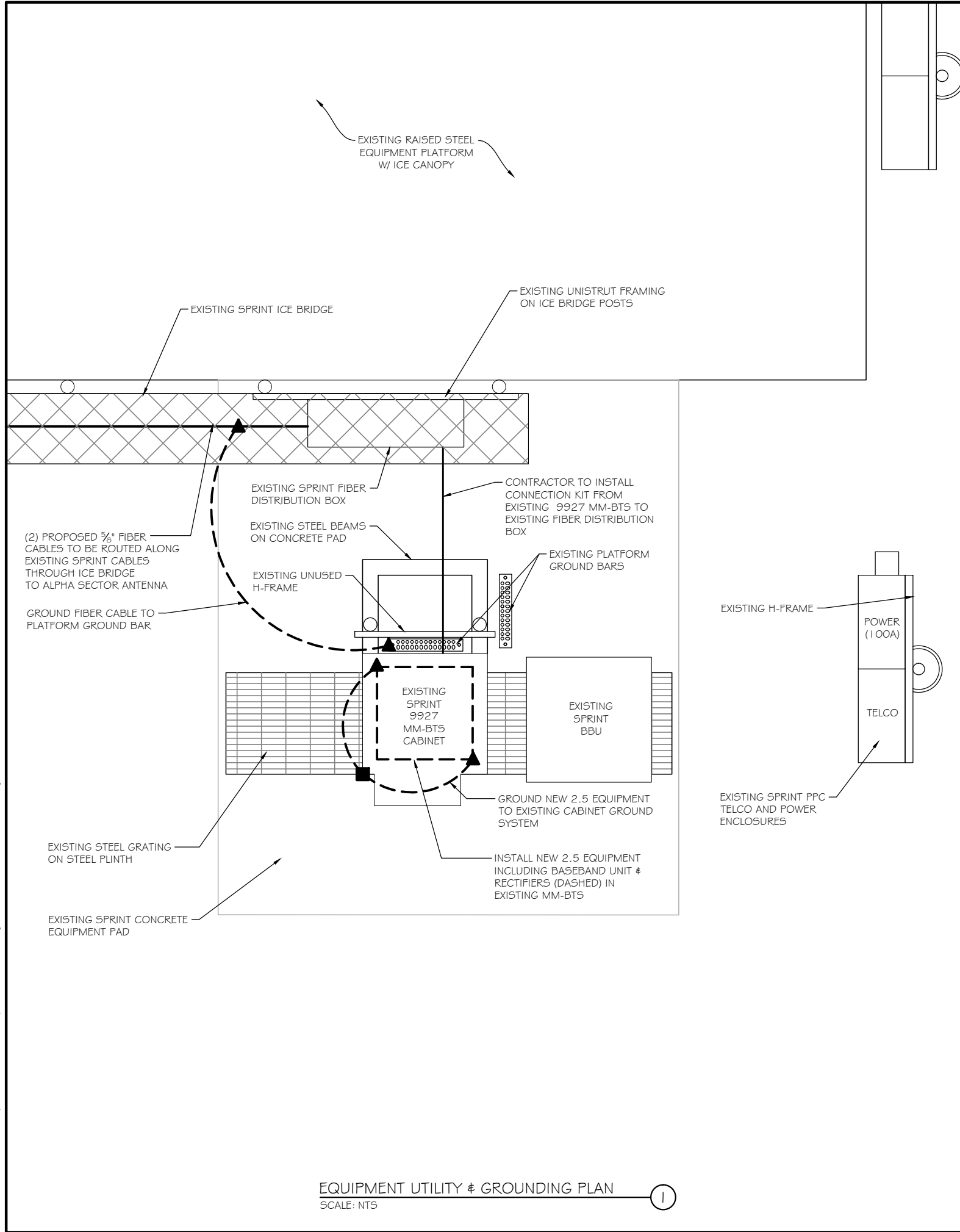
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 CTS  
 CT03XC360-A

PROJECT INFORMATION:  
 4G FERNWOOD LANE  
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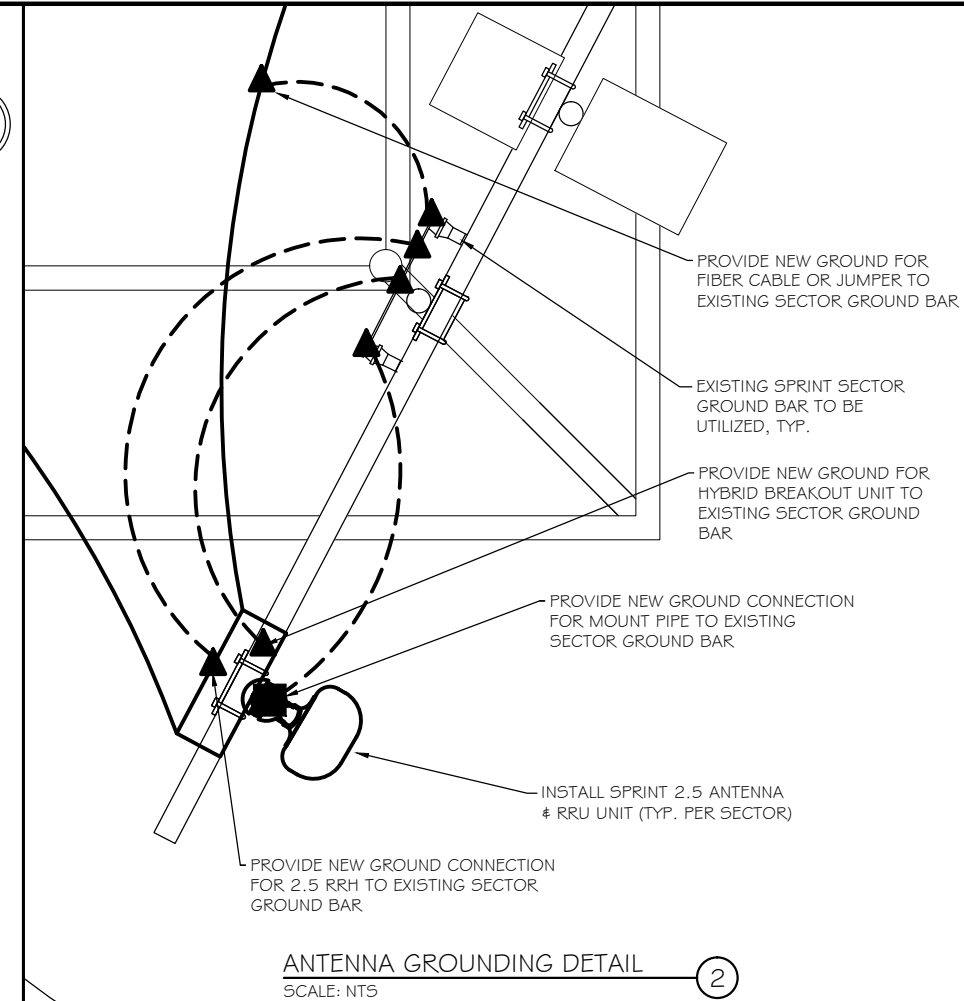
SHEET TITLE:  
 EQUIPMENT DETAILS

SCALE:  
 AS NOTED

PROJECT NUMBER: 28731  
 SHEET NUMBER: A-8



EQUIPMENT UTILITY & GROUNDING PLAN  
 SCALE: NTS



ANTENNA GROUNDING DETAIL  
 SCALE: NTS

- GROUNDING NOTES:**
- CONTRACTOR TO ENSURE PROPER SEQUENCING OF GROUNDING AND UNDERGROUND CONDUIT INSTALLATION TO PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM AND/OR DAMAGE TO THE CONDUIT.
  - ALL EXTERIOR GROUND CONDUCTORS SHALL BE #2 AWG SOLID TINNED COPPER UNLESS NOTED OTHERWISE.
  - ALL GROUND CONNECTIONS BELOW GRADE SHALL BE EXOTHERMIC (CADWELD).
  - ALL GROUND CONNECTIONS ABOVE GRADE AND/OR INTERIOR SHALL BE COMPRESSION TYPE, TWO-HOLE LUGS OR DOUBLE-CRIMP "C" TAPS.
  - CONTACT AREAS WHERE CONNECTIONS ARE MADE SHALL BE PREPARED TO A BARE BRIGHT FINISH AND COATED WITH AN ANTI-OXIDATION MATERIAL BEFORE CONNECTIONS ARE MADE.
  - MAXIMUM RESISTANCE OF THE COMPLETED GROUND SYSTEM SHALL NOT EXCEED 5 OHMS.
  - WHERE GROUNDING CONNECTIONS ARE MADE TO PAINTED METAL SURFACES, PAINT SHALL BE REMOVED TO BARE METAL TO ENSURE PROPER CONTACT AND RESTORED/PAINTED TO ORIGINAL FINISH.
  - GROUND DEPTH SHALL BE 30" MINIMUM BELOW FINISHED GRADE, OR 6" BELOW FROST LINE, WHICHEVER IS GREATER.

**LEGEND:**

---	EXISTING GROUND CABLE
---	PROPOSED GROUND CABLE
▲	MECHANICAL CONNECTION
■	EXOTHERMIC CONNECTION
—E—E—E—E—E—	PROPOSED ELECTRIC



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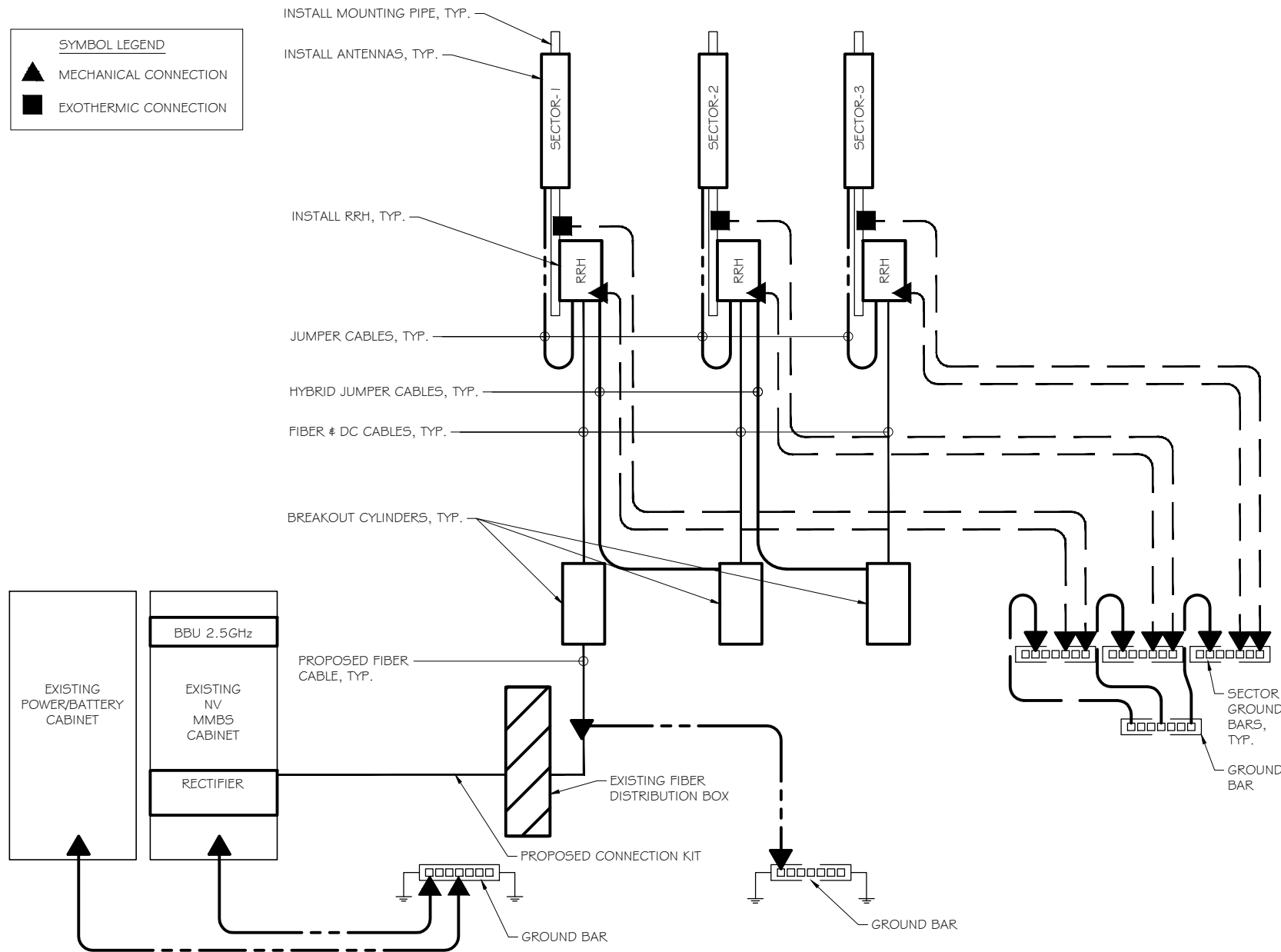
SHEET TITLE:  
 EQUIPMENT UTILITY &  
 GROUNDING PLAN

SCALE:  
 AS NOTED

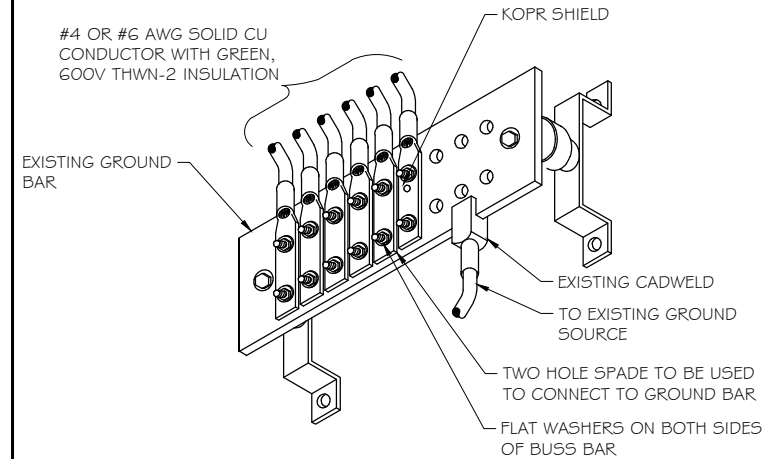
PROJECT NUMBER: 28731  
 SHEET NUMBER: E-1

**SYMBOL LEGEND**

▲	MECHANICAL CONNECTION
■	EXOTHERMIC CONNECTION

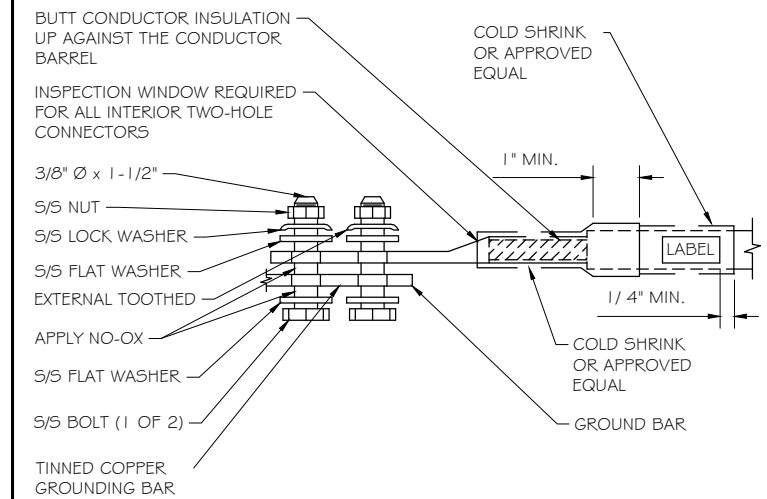


**GROUNDING RISER DIAGRAM**  
 SCALE: NTS



- NOTES:**
1. APPLY NO-OX TO LUG AND GROUND BAR CONTACT SURFACE. DO NOT COAT INLINE LUG.
  2. IF STOLEN GROUND BARS ARE ENCOUNTERED, CONTACT SPRINT CM FOR REPLACEMENT THREADED ROD KIT.

**GROUNDING CONDUCTOR INSTALLATION**  
 SCALE: NTS



**TWO-HOLE LUG**  
 SCALE: NTS



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A	08/08/14	FINAL CONSTRUCTION DRAWINGS

ISSUE PHASE: FINAL DATE ISSUED: 08/08/2014

PROJECT TITLE:  
**CTS  
 CT03XC360-A**

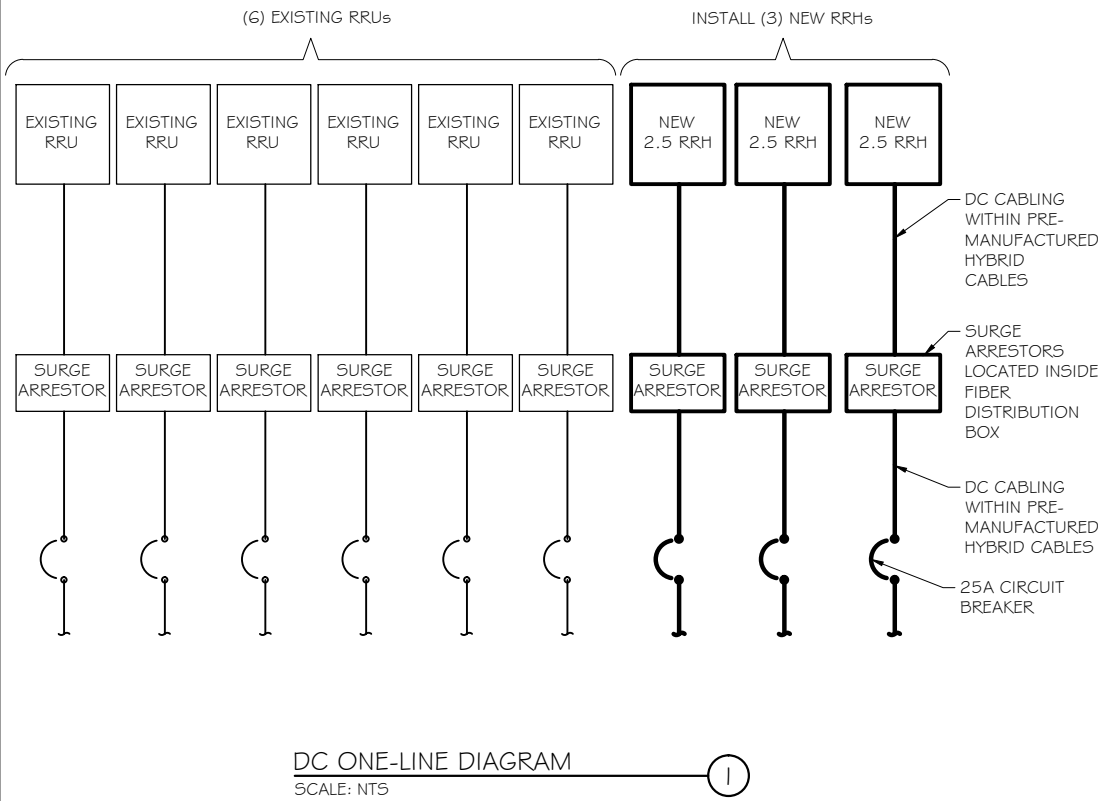
PROJECT INFORMATION:  
 46 FERNWOOD LANE  
 WILTON, CT 06897  
 FAIRFIELD COUNTY

SHEET TITLE:  
**GROUNDING DETAILS**

SCALE:  
 AS NOTED

PROJECT NUMBER: 28731  
 SHEET NUMBER: E-2





### A/C PANEL SCHEDULE

VOLTAGE:	240V/1 20	PANEL STATUS:	EXISTING	N TO GROUND BOND:	YES
MAIN BREAKER:	100 AMP	MODEL NUMBER:	TBD	INTERNAL TVSS:	YES
MOUNT:	GROUND	PHASE:	1	WIRE:	3
ENCLOSURE TYPE:	NEMA 3R	BUSS RATING:	200 AMP	GROUND BAR:	YES
		NEUTRAL BAR:	YES		

CKT	DESCRIPTION	BREAKER AMPS	BREAKER POLES	BREAKER STATUS	PHASE A VA	PHASE B VA	BREAKER STATUS	BREAKER POLES	BREAKER AMPS	DESCRIPTION	CKT
1	BLANK (UNUSED)	-	-	-						SURGE PROTECTOR	7
2	MMBTS	100	2	ON			ON	2	60	TOWER LIGHT	8
3	BLANK (UNUSED)	-	-	-			ON	1	20	NOT LABELED	9
4	GEN CHARGER	20	1	ON			ON	1	20	GFI	10
5	FAN	10	1	ON			-	-	-	BLANK (UNUSED)	11
6											12

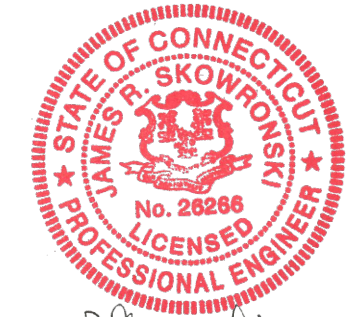
AC PANEL SCHEDULE  
 SCALE: NTS

**Sprint**  
 6580 SPRINT PARKWAY  
 OVERLAND PARK, KANSAS 66251

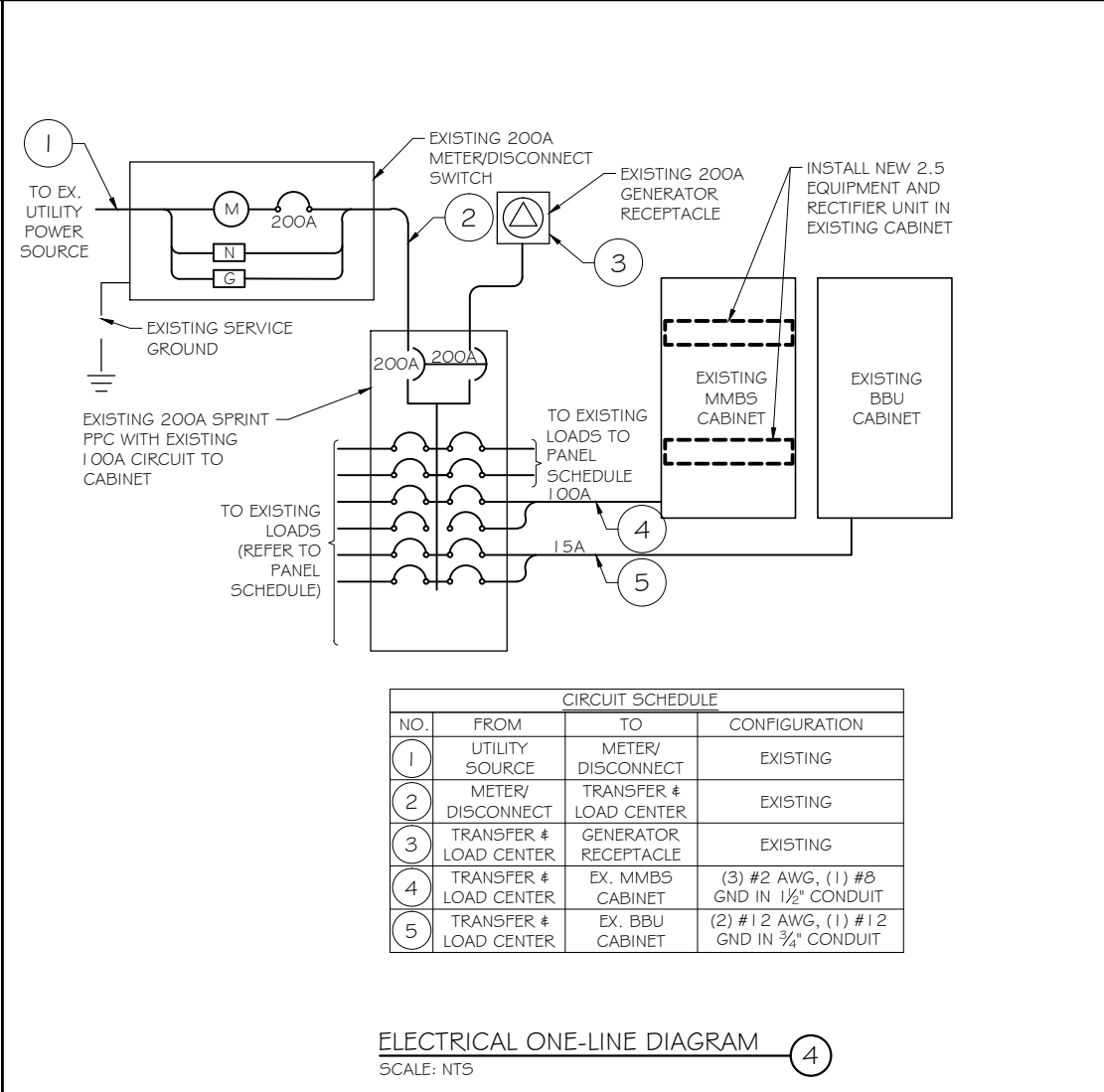
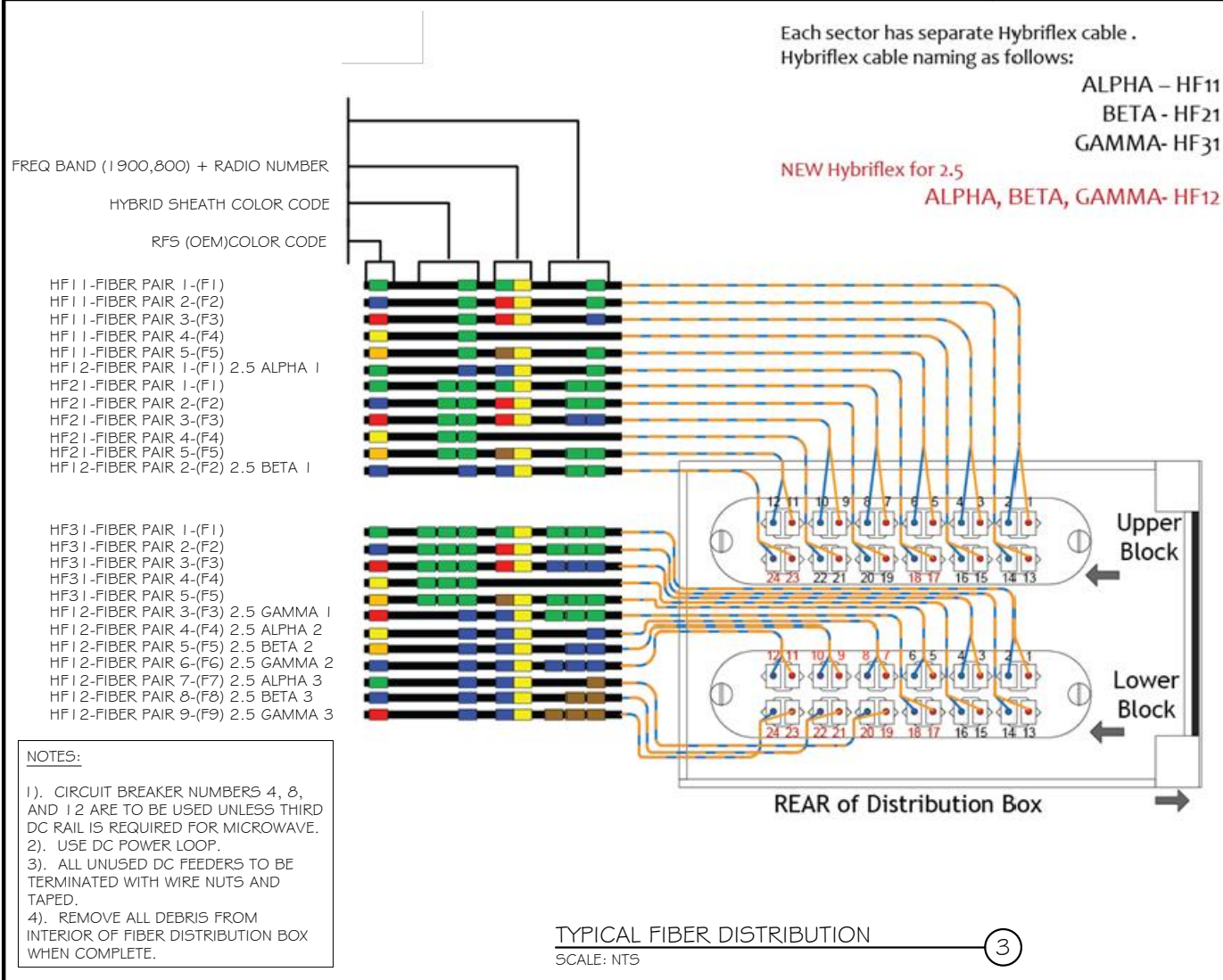
**RAMAKER & ASSOCIATES, INC.**  
 1120 Dallas Street, Sauk City, WI 53583  
 Phone: 608-643-4100 Fax: 608-643-7999  
 www.Ramaker.com

**Transcend Wireless**  
 48 SPRUCE STREET  
 OAKLAND, NJ 07346

Certification & Seal:  
 I hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the laws of the State of Connecticut.



Signature: *James R. Skowronski* Date: 8/08/2014



MARK	DATE	DESCRIPTION
A	08/08/14	FINAL CONSTRUCTION DRAWINGS
ISSUE PHASE	FINAL	DATE ISSUED 08/08/2014
PROJECT TITLE: CTS CT03XC360-A		
PROJECT INFORMATION: 4G FERNWOOD LANE WILTON, CT 06897 FAIRFIELD COUNTY		
SHEET TITLE: DC POWER DETAILS & PANEL SCHEDULES		
SCALE:	AS NOTED	
PROJECT NUMBER	28731	
SHEET NUMBER	E-3	