

October 27, 2021

Members of the Siting Council Connecticut Siting Council Ten Franklin Square New Britain, CT 06051

RE: Tower Share Application 109 Schofield Road, Willington CT 06279

Latitude: 41.9222611 N Longitude: -72.293650 W

Site# BOBDL00147A\_Dish\_Willington\_TS\_Zoning

Dear Ms. Bachman:

This letter and attachments are submitted on behalf of Dish Wireless LLC. Dish Wireless LLC plans to install antennas and related equipment to the tower site located at 109 Schofield Road, Willington, Connecticut 06279

**Northeast Site Solutions** 

4 Angela's Way, Burlington CT 06013 denise@northeastsitesolutions.com

Denise Sabo

Dish Wireless LLC proposes to install three (3) 600/19005G MHz antenna and six (6) RRUs, at the 145-foot level of the existing 149 foot guyed tower, one (1) Fiber cable will also be installed. Dish Wireless LLC equipment cabinets will be placed within 7x5 lease area. Included are plans by Infinigy, stamped October 22, 2021, Exhibit C. Also included is a structural analysis prepared by Aerosmith Engineering, dated April 21, 2021, confirming that the existing tower is structurally capable of supporting the proposed equipment. Attached as Exhibit D. This facility was approved by the Connecticut Siting Council, Docket No. 429, on February 7, 2013. Please see attached Exhibit A.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies 16-50aa, of Dish Wireless LLC intent to share a telecommunications facility pursuant to R.C.S.A. 16-50j-88. In accordance with R.C.S.A., a copy of this letter is being sent to First Selectman Erika Wiecenski for the Town of Willington, Michael D'Amato, Zoning Agent, Planning & Zoning Commission for the Town of Willington, as well as the property owner Joseph J. Mottes Co. and Tarpon Towers II, LLC tower owner.

The planned modifications of the facility fall squarely within those activities explicitly provided for in R.C.S.A. 16-50j-89.

- 1. The proposed modifications will not result in an increase in the height of the existing structure. The top of the tower is 149-feet; Dish Wireless LLC proposed antennas will be located at a center line height of 145-feet.
- 2. The proposed modification will not result in the increase of the site boundary as depicted on the attached site plan.
- 3. The proposed modification will not increase the noise levels at the facility by six decibels or more, or to levels that exceed local and state criteria. The incremental effect of the proposed changes will be negligent.



4.The operation of the proposed antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard. As indicated in the attached power density calculations, the combined site operations will result in a total density of 1.42% as evidenced by Exhibit F.

Connecticut General Statutes 16-50-aa indicates that the Council must approve the shared use of a telecommunications facility provided it finds the shared use is technically, legally, environmentally, and economically feasible and meets public safety concerns. As demonstrated in this letter, Dish Wireless LLC respectfully indicates that the shared use of this facility satisfies these criteria.

A. Technical Feasibility. The existing monopole has been deemed structurally capable of supporting Dish Wireless LLC proposed loading. The structural analysis is included in Exhibit D.

B. Legal Feasibility. As referenced above, C.G.S. 16-50aa has been authorized to issue orders approving the shared use of an existing tower such as this support tower in Willington. Under the authority granted to the Council, an order of the Council approving the requested shared use would permit Dish Wireless LLC to obtain a building permit for the proposed installation. Further, a letter of Authorization is included as Exhibit G, authorizing Dish Wireless LLC to file this application for shared use.

C. Environmental Feasibility. The proposed shared use of this facility would have a minimal environmental impact. The installation of Dish Wireless LLC equipment at the 145-foot level of the existing 149-foot tower would have an insignificant visual impact on the area around the tower. Dish Wireless LLC ground equipment would be installed within the existing facility compound. Dish Wireless LLC shared use would therefore not cause any significant alteration in the physical or environmental characteristics of the existing site. Additionally, as evidenced by Exhibit F, the proposed antennas would not increase radio frequency emissions to a level at or above the Federal Communications Commission safety standard.

D. Economic Feasibility. Dish Wireless LLC will be entering into an agreement with the owner of this facility to mutually agreeable terms. As previously mentioned, the Letter of Authorization has been provided by the owner to assist Dish Wireless LLC with this tower share application.

E. Public Safety Concerns. As discussed above, the tower is structurally capable of supporting Dish Wireless LLC proposed loading. Dish Wireless LLC is not aware of any public safety concerns relative to the proposed sharing of the existing tower. Dish Wireless LLC intentions of providing new and improved wireless service through the shared use of this facility is expected to enhance the safety and welfare of local residents and individuals traveling through Willington.

Sincerely,

Deníse Sabo

Denise Sabo

Mobile: 203-435-3640 Fax: 413-521-0558

Office: Angela's Way, Burlington CT 06013 Email: denise@northeastsitesolutions.com



Attachments

Cc: First Selectman Erika Wiecenski Town of Willington 40 Old Farms Road Willington, CT 06279

Michael D'Amato, Zoning Agent Town of Willington 40 Old Farms Road Willington, CT 06279

Joseph J. Mottes Co P.O. Box 535 Willington, CT 06270

Tarpon Tower II, LLC, Tower Owner

# Exhibit A

**Original Facility Approval** 

DOCKET NO. 429 - New Cingular Wireless PCS, LLC }

(AT&T) application for a Certificate of Environmental Compatibility and Public Need for the construction, } maintenance, and operation of a telecommunications facility located at one of two sites: Willington Tax Assessor Parcel ID } #M23-P62 Tolland Turnpike, Willington, Connecticut; or Willington Tax Assessor Parcel ID #M18-19 Old South Willington Road, Willington, Connecticut.

#### **Findings of Fact**

#### Introduction

- 1. New Cingular Wireless PCS, LLC (AT&T), in accordance with provisions of Connecticut General Statutes (CGS) § 16-50g et. seq., applied to the Connecticut Siting Council (Council) on July 24, 2012 for the construction, maintenance, and operation of a telecommunications facility at one of two proposed locations in the Town of Willington (Town), Connecticut. (AT&T 1, pp. 1)
- 2. AT&T's Candidate A site would be located off of Tolland Turnpike and would include a 160-foot monopole tower. AT&T's Candidate B site would be located off of Old South Willington Road and would include a 190-foot monopole tower. (AT&T 1, p. 2)
- 3. AT&T is a Delaware limited liability company with an office at 500 Enterprise Drive, Rocky Hill, Connecticut. AT&T is licensed by the Federal Communications Commission (FCC) to construct and operate a personal wireless services system. (AT&T 1, p. 3)
- 4. The party in this proceeding is the applicant. Robert and Marissa Golden are intervenors. (Transcript, October 11, 2012, 3:00 p.m. [Tr. 1], pp. 4, 9)
- 5. The purpose of the proposed facility would be to provide service along Tolland Turnpike (State Route 74), Willington Hill Road (Route 320), Ruby Road, and surrounding areas in the Town of Willington. (AT&T 1, p. 1)
- 6. AT&T originally submitted a Certificate application for these two locations on May 19, 2011. AT&T subsequently withdrew the application without prejudice. (AT&T 1, p. 23)
- 7. Pursuant to CGS § 16-50*l*(b), AT&T published public notice of its intent to submit this application on July 17 and July 18, 2012 in the Willimantic Chronicle. (AT&T 1, p. 4, Attachment 7; AT&T 2 Affidavit of Publication, dated September 5, 2012)
- 8. Pursuant to CGS § 16-50*l*(b), AT&T sent, via certified mail, notices of its intent to file an application with the Council to each person appearing of record as owner of property abutting the properties on which the two candidate sites are located. (AT&T 1, p. 4; Attachment 7)

- 9. Of 33 notice letters sent to abutting property owners, AT&T received 19 return receipts and confirmed the delivery of another nine letters through the U.S. Postal Service website's Track and Confirm tool. Five notice letters were re-sent via first class mail to the abutting property owners from whom receipts were not received. (AT&T 3, A1)
- 10. Pursuant to CGS § 16-50*l* (b), AT&T provided copies of its application to all federal, state and local officials and agencies listed therein. (AT&T 1, p. 4; Attachment 6)
- 11. AT&T posted signs at each of the two candidate sites on September 28, 2012. The signs gave the date of the public hearing and contact information for the Council. (AT&T 6 Affidavit of Sign Posting)
- 12. The Council and its staff conducted an inspection of the proposed sites on October 11, 2012, beginning at 1:30 p.m. The applicant attempted to fly a balloon at each of the two sites to simulate the heights of the proposed towers but gusty wind conditions resulted in several lost balloons and made it difficult for the balloons to fly at the intended heights. (Tr. 1, pp. 32-33)
- 13. Pursuant to CGS § 16-50m, the Council, after giving due notice thereof, held a public hearing on October 11, 2012, beginning at 3:00 p.m. and continuing at 7:00 p.m. in the Old Senior Center Room in the Willington Town Office Building at 40 Old Farms Road in Willington, Connecticut. (Tr. 1, p. 3 ff.)
- 14. On November 29, 2012, the Council ruled that cross examination of late filed exhibits was not necessary and closed the evidentiary record. (Council Memorandum from Linda Roberts to Parties and Intervenors, dated November 30, 2012)

# **State Agency Comment**

- 15. Pursuant to CGS § 16-50j(h), on August 13, 2012, the Council solicited comments on this application from the following state agencies: Department of Agriculture, Department of Energy & Environmental Protection (DEEP), Department of Public Health, Council on Environmental Quality, Public Utilities Regulatory Authority, Office of Policy and Management, Department of Economic and Community Development, the Department of Transportation (ConnDOT), and the Department of Emergency Management and Homeland Security. (CSC Hearing Package dated August 13, 2012)
- 16. ConnDOT submitted comments in which it stated that AT&T would need a Highway Encroachment Permit should it need to do any work within the right-of-way of Route 74 (Tolland Turnpike) for the Candidate A site. ConnDOT had no comment on the Candidate B site. (ConnDOT Comment Letter, August 24, 2012)
- 17. The Council did not receive comments from any of the other state agencies. (Record)

# **Municipal Consultation**

- 18. AT&T first contacted the Town about its interest in the two candidate sites on October 4, 2010 when it submitted to the Town a Technical Report that provided details about the two sites. (AT&T 1, p. 22)
- 19. After some discussions with AT&T, the First Selectman and Town staff indicated a preference for the proposed Candidate A Site (off of Tolland Turnpike) because the 160-foot tower at this location appeared to minimally impact the Willington Green and this location was in an existing gravel mining operation near other commercial ventures. (AT&T 1, p. 23; Docket 418 Application, p. 8)
- 20. The Candidate B Site was less preferred by Town officials due to its proximity to residential homes and Old Willington Road, a local dirt road of rural nature. Town officials also noted that should Candidate B become the preferred site they would want AT&T to consider utilizing an alternate route across an existing driveway for access rather than building an entirely new gravel access drive. (AT&T 1, p. 23)
- 21. AT&T contacted the Town again on May 31, 2012 to indicate that it was going to re-apply for a facility at one of the two potential sites. (AT&T 1, p. 23; Attachment 6)
- 22. In response to AT&T's notice of the re-submittal of its application, the Town stated that no further consultation was necessary and added that it requested that the Council add an "ultimate height" stipulation that would limit the height of the tower at its preferred Candidate A site to the proposed 160 feet. (AT&T 1, Attachment 6 Letter of Willington First Selectman dated July 10, 2012)
- 23. AT&T would offer space on its proposed tower for public safety users at no cost. (Transcript, October 11, 2012, 7:00 p.m. [Tr. 2], p. 27)

#### **Public Need for Service**

- 24. In 1996, the United States Congress recognized a nationwide need for high quality wireless telecommunications services, including cellular telephone service. Through the Federal Telecommunications Act of 1996, Congress seeks to promote competition, encourage technical innovations, and foster lower prices for telecommunications services. (Council Administrative Notice Item No. 4 Telecommunications Act of 1996; AT&T 1, p. 5)
- 25. In issuing cellular licenses, the Federal government has preempted the determination of public need for cellular service by the states, and has established design standards to ensure technical integrity and nationwide compatibility among all systems. (Council Administrative Notice Item No. 4 Telecommunications Act of 1996)
- 26. The Telecommunications Act of 1996 prohibits local and state bodies from discriminating among providers of functionally equivalent services. (Council Administrative Notice Item No. 4 Telecommunications Act of 1996)

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- 27. The Telecommunications Act of 1996 prohibits any state or local entity from regulating telecommunications towers on the basis of the environmental effects, which include human health effects, of radio frequency emissions to the extent that such towers and equipment comply with FCC's regulations concerning such emissions. This Act also blocks the Council from prohibiting or acting with the effect of prohibiting the provision of personal wireless service. (Council Administrative Notice Item No. 4 Telecommunications Act of 1996)
- 28. The Wireless Communications and Public Safety Act of 1999 (911 Act) was enacted by Congress to promote and enhance public safety by making 9-1-1 the universal emergency assistance number, by furthering deployment of wireless 9-1-1 capabilities, and by encouraging construction and operation of seamless ubiquitous and reliable networks for wireless services. (Council Administrative Notice Item No. 6 Wireless Communications and Public Safety Act of 1999, as amended)
- 29. AT&T would provide "Enhanced 911" services from the proposed facility as required by the 911 Act. (AT&T 1, p. 9)
- 30. The Tolland County Mutual Aid Fire Service, one of the largest regional 911 centers in the State of Connecticut, would be interested in locating antennas on the proposed tower, preferably at the Candidate A site. (Tr. 2, pp. 14-15)
- 31. Approximately 70 percent of the 40,000 911 calls received annually by the Tolland County Mutual Aid Fire Service are made from wireless devices. (Tr. 2, p. 15)
- 32. In December 2009, President Barack Obama recognized cell phone towers as critical infrastructure vital to the United States. The Department of Homeland Security, in collaboration with other Federal stakeholders, State, local, and tribal governments, and private sector partners, has developed the National Infrastructure Protection Plan (NIPP) to establish a framework for securing our resources and maintaining their resilience from all hazards during an event or emergency. (Council Administrative Notice Item No. 10 -Barack Obama Presidential Proclamation 8460, Critical Infrastructure Protection)
- 33. In 2009, the U.S. Congress directed the FCC to develop a national broadband plan to ensure that every American would have access to broadband capability whether by wire or wireless. As a result of this directive, the FCC produced a plan entitled, "Connecting America: The National Broadband Plan." The goal of this plan was to: Advance consumer welfare, civic participation, public safety and homeland security, community development, healthcare delivery, energy independence and efficiency, education, employee training, private sector investment, entrepreneurial activity, job creation and economic growth, and other national purposes. (AT&T 1, p. 6)
- 34. Pursuant to the tower sharing policy of the State of Connecticut under C.G.S. §16-50aa, if the Council finds that a request for shared use of a facility by a municipality or other person, firm, corporation or public agency is technically, legally, environmentally and economically feasible, and the Council finds that the request for shared use of a facility meets public safety concerns, the Council shall issue an order approving such shared use to avoid the unnecessary proliferation of towers in the state. (Conn. Gen. Stat. §16-50aa)

# **Existing and Proposed Wireless Coverage**

- 35. Within the area to be covered from the proposed facility, AT&T is licensed to operate within the Cellular B-Band; the D-Block, E-Block, A3 Block and C1 Block at the 1900 MHz PCS frequencies; and the Lower C Block, the Lower E Block, and the Lower B Block within the 700 MHz frequency range. (AT&T 3, A9)
- 36. AT&T's design criteria for satisfactory coverage are -74 dBm for in-building coverage and -82 dBm for in-vehicle coverage. These criteria are the same for each of the different frequencies utilized by AT&T. (AT&T 3, A11)
- 37. AT&T's existing signal strengths in the area that would be covered from the proposed site(s) range from -82 dBm to less than -100 dBm. (AT&T 3, A12)
- 38. AT&T experiences a coverage gap of 2.17 miles on Route 74 (Tolland Turnpike) and a gap of 2.6 miles on Route 320 (Willington Hill Road). (AT&T 1, Attachment 2 Radio Frequency Analysis Report, p. 2)
- 39. The distances that the proposed sites would allow AT&T to cover on its target roads are indicated in the following table.

Road	Distance Covered from Candidate A	Distance Covered from Candidate B
Route 74, Tolland Turnpike	1.46 miles	0.86 miles
Route 320, Willington Hill Road	1.93 miles	1.93 miles

(AT&T 3, A14)

- 40. The Candidate A site would provide unique incremental coverage on Tolland Turnpike of approximately 0.25 miles west of State Route 320 and 0.35 miles east of State Route 320. This incremental coverage would enable AT&T to provide continuous coverage on close to 2.5 miles along Tolland Turnpike. (AT&T 1, Attachment 1, p. 4)
- 41. AT&T could achieve a majority of its coverage objectives from Candidate B, but each of the remaining coverage gaps on Route 74 west of Route 320 and on Route 74 east of Route 320 would likely require another site to provide adequate coverage. (AT&T 1, Attachment 2 Radio Frequency Analysis Report, p. 5)
- 42. The incremental coverage that would result from each site is listed in the table below.

Signal Level	Sq. Mi. covered from Candidate A	Sq. Mi. covered from Candidate B
In-building (-74 dBm)	7.49	6.22
In-vehicle (-82 dBm)	6.11	4.88

(AT&T 3, A15; Tr. 1, p. 30-31)

43. From either proposed facility, AT&T's antennas would hand off signals to the adjacent sites identified in the table below.

Site Location	Distance and Direction from Candidate A	Distance and Direction From Candidate B
5 Barbara Road, Tolland	3.6 miles, W	3.4 miles, W
1298 Storrs Road, Mansfield	4.3 miles, S	3.5 miles, S
426 River Road, Willington	1.5 miles, NW	2.0 miles, NW
1725 Stafford Road, Mansfield	3.4 miles, SW	2.6 miles, SW
99 Knowlton Hill Road, Ashford	4.0 miles, SE	3.8 miles, SE
20 Seles Road, Ashford	4.5 miles, E	4.7 miles, E
497 Middle Turnpike, Mansfield	3.5 miles, S	2.6 miles, S

(AT&T 7, Attachments 3 and 4)

- 44. The lowest feasible height at which AT&T could fulfill its coverage objectives from the Candidate A site is 157 feet above ground level. From the Candidate B site, it is 187 feet above ground level. (AT&T 3, A16)
- 45. The Candidate A site would provide better coverage and is AT&T's preferred site. (AT&T 1, p. 13)
- 46. The Candidate B site would allow AT&T to achieve a majority of its coverage objectives, but a remaining coverage gap on Tolland Turnpike east of Route 320 would likely require an additional site. (AT&T 1, Attachment 1, p. 5)

#### **Site Selection**

- 47. AT&T established a search ring for a site in this vicinity on December 17, 2008. The search ring was centered at 41° 51' 59.1" north latitude and 72° 16' 26.4" west longitude and was approximately one mile in diameter. (AT&T 3, A2)
- 48. There are 16 existing telecommunications towers and a church steeple located within approximately four miles of AT&T's search area. AT&T has antennas on eight of these facilities, but none of these facilities would be able to provide the service needed in the area that AT&T is seeking to cover. The existing facilities are listed in the following table.

Owner	Approx. Height	Location	AT&T at site	Distance from Candidate A	Direction from Candidate A
Willington Hill FD	75'	24 Old Farms Rd, Willington	No	.5 mi.	SE
Federated Churches of Willington	50'	236 Tolland Tpk, Willington	No	.2 mi.	Е
State of CT	75'	Jared Sparks Road, Willington	No	.4 mi.	NE

(table continued on next page)

Owner	Approx. Height	Location	AT&T at site	Distance from Candidate A	Direction from Candidate A
Verizon	140'	Cosgrove Road,	No	1.3 mi.	N
		Willington			
Willington FD	110'	126 River Road,	Yes	1.5 mi.	NW
		Willington			
Cordless Data	170'	Turnpike Road,	Yes	3.6 mi.	N
		Willington			
DPS	120'	Tolland Stage Rd,	No	2.9 mi.	W
		Tolland			
American	150'	5 Barbara Road,	Yes	3.6 mi.	W
Tower		Tolland			
Town of	170'	1725 Stafford Rd,	Yes	3.4 mi.	SW
Mansfield		Mansfield			
AT&T	120'	497 Middle Tpk,	Yes	3.5 mi.	S
		Mansfield			
UConn tower	80' – 320'	North Eagleville	Yes	4.3 mi.	S
farm		Road, Mansfield			
SBA	150'	Knowlton Hill Rd,	Yes	4.0 mi.	SE
		Ashford			
Ray Baker	190'	20 Seles Road,	Yes	4.5 mi.	Е
		Ashford			
North Atlantic	149'	155 Schofield Rd,	No	3.5 mi.	NW
Towers		Willington			

(AT&T 1, Attachment 2 – Existing Tower/Cell Site Listing)

- 49. AT&T investigated a total of nine properties as possible locations. These properties and the determinations of their suitability are listed below.
  - a. Tolland Turnpike This is the Candidate A property. It is approximately 47.7 acres.
  - b. <u>180 Tolland Turnpike</u> This is a 128.5-acre parcel. A facility on this property would interfere with an ongoing gravel operation.
  - c. Old South Willington Road This is a 170-acre parcel, which is the site of the proposed Candidate B facility.
  - d. <u>236 Tolland Turnpike</u> This is the Federated Churches of Willington property. The church steeple at this location was rejected by AT&T's radio frequency engineers.
  - e. <u>24 Old Farms Road</u> This is a .84-acre parcel owned by the Willington Hill Fire Department. There is an existing 75-foot tower, but it is too short for AT&T's needs. There is limited ground space for a tower replacement, and there is less natural screening on this property. With a tower on this property, AT&T would require a second tower to achieve coverage comparable to the proposed facility sites.
  - f. <u>74 Willington Hill Road</u> This is a 25.3-acre parcel that was rejected by AT&T's radio frequency engineers.

- g. <u>49 Hancock Road</u> This is a 49.85-acre parcel that was rejected by AT&T's radio frequency engineers.
- h. <u>Luchon Road</u> This is a 3.26-acre parcel owned by the Town of Willington. It was rejected by AT&T's radio frequency engineers. Furthermore, a facility on this property would likely impact on-site wetlands.
- i. <u>Jared Sparks Road</u> This is a 20-acre parcel owned by the Town of Willington. It was rejected by AT&T's radio frequency engineers.

(AT&T 1, Attachment 2)

- 50. In addition to the nine sites identified in the preceding finding of fact, AT&T also reviewed a site at 343 Daleville Road in Willington, which was the subject of the Council's Docket No. 400. AT&T's radio frequency engineers determined that the Daleville Road site would not satisfy the coverage needs it is seeking to satisfy from the proposed sites. (AT&T 4, A1)
- 51. Repeaters, microcell transmitters, distributed antenna systems (DAS) and other types of transmitting technologies would not be practicable or feasible means for AT&T's provision of service in the area surrounding the proposed facility. These technologies are better suited for specifically defined areas where new coverage is necessary, such as commercial buildings, shopping malls, and tunnels. (AT&T 1, p. 11)

# **Facility Description**

#### Candidate A

- 52. The Candidate A site is located on a 47.7-acre parcel on Tolland Turnpike. It is owned by Lawrence Becker. There is an active gravel pit on the property. (AT&T 1, p. 13; Tr. 1, p. 17)
- 53. Mr. Becker also owns the Candidate Site B. He prefers that the facility be located at the Candidate A site. (Tr. 2, pp. 8-9)
- 54. The Candidate A property is zoned R-80, a single-family residential zoning district requiring a minimum lot size of 80,000 square feet. Wireless telecommunications facilities are permitted in R-80 zones with a Special Permit. (AT&T 1, p. 14; AT&T Bulk Filing Zoning Regulations for the Town of Willington)
- 55. The Candidate A site would be located in the northerly portion of the Becker property. AT&T would lease a 100-foot by 100-foot parcel, within which it would erect a 160-foot monopole tower inside a 40-foot by 80-foot equipment compound enclosed by an eight-foot high chain link fence. AT&T's ground equipment would be installed inside a 12-foot by 20-foot equipment shelter (AT&T 1, p. 13; Attachment 3A Drawings C01 and Compound Plan)

- 56. For backup power, AT&T would utilize a 50 kW diesel generator. AT&T would also have a battery backup in order avoid a "re-boot" condition during the generator start-up delay period. The typical run time of the generator before it requires refueling is 48 hours. (AT&T 3, A17; Tr. 1, p. 73)
- 57. The generator would be designed with secondary containment capable of retaining 110 percent of the oil fill. (Tr. 1, p. 32)
- 58. The proposed tower would be located at 41° 52' 32.4" North latitude and 72° 16' 9.7" West longitude. Its elevation at ground level would be approximately 768 feet above mean sea level. (AT&T 1, Attachment 3 Site A: Site Evaluation Report)
- 59. AT&T's proposed tower would be designed in accordance with American National Standards Institute EIA/TIA-222-G "Structural Standards for Steel Antenna Towers and Antenna Support Structures" and the 2003 International Building Code with 2005 Connecticut Amendment. The foundation design would be based on existing soil conditions. The diameter of the tower would be approximately four and one-half feet at its base and two feet at its top. (AT&T 1, Attachment 3 Candidate A Tolland Turnpike: Facilities and Equipment Specification)
- 60. AT&T would initially install nine multi-band antennas on a low profile platform at a centerline height of 157 feet above ground level (agl). (AT&T 1, Attachment 3 Candidate A Tolland Turnpike: Facilities and Equipment Specification; Tr. 1, p. 14)
- 61. The tower would be designed to accommodate three other carriers, in addition to AT&T. (AT&T 1, Attachment 3 Candidate A Tolland Turnpike: Facilities and Equipment Specification; Tr. 1, p. 28)
- 62. Development of the Candidate A site would require 111 cubic yards of cut and 151 cubic yards of fill. (AT&T 3, A5)
- 63. Vehicular access to the facility would be provided over an existing drive for a distance of 331 feet and then over a new gravel access drive that would be 581 feet long and 12 feet wide. (AT&T 1, Attachment 3 Candidate A: General Facility Description)
- 64. Underground electric and telephone utilities would be extended to the site from an existing offsite utility pole along the edge of the access drive. (AT&T 1, Attachment 3 Candidate A: General Facility Description; Attachment 3A Drawing Sheet C02)
- 65. AT&T does not anticipate the need for blasting. If ledge is encountered, mechanical means would be the preferred method of removal. (AT&T 3, A6)
- 66. The setback radius of the proposed tower would be contained within the host property. (AT&T 1, Attachment 3A Drawing Sheet C02)
- 67. There are six residences within 1,000 feet of the Candidate A site. (AT&T 1, Attachment 3A)
- 68. The nearest residence to the Candidate A site is located 445 feet to the northwest at 202 Tolland Turnpike. It is owned by Jean Paul Landry. (AT&T 1, Attachment 3A)

- 69. Land uses within one-quarter mile of the proposed facility include a sand and gravel mining operation, a cemetery, and commercial and residential properties. (AT&T 1, Attachment 3 Site A: Site Evaluation Report)
- 70. The estimated cost of the proposed facility is:

Tower and foundation	\$ 90,000
Site development costs	45,000
Utility installation	27,360
Facility installation	93,000
Antennas and equipment	<u>250,000</u>
Total cost	\$505,360

(AT&T 1, p. 23)

#### Candidate B

- 71. The Candidate B site is located on a 170-acre parcel on Old South Willington Road. It is owned by Lawrence Becker. A portion of the gravel pit on the Candidate A property spills onto this property. (AT&T 1, p. 14; Tr. 1, p. 17)
- 72. The Candidate B property is zoned R-80, a single-family residential zoning district requiring a minimum lot size of 80,000 square feet. Wireless telecommunications facilities are permitted in R-80 zones with a Special Permit. (AT&T 1, p. 15; AT&T Bulk Filing Zoning Regulations for the Town of Willington)
- 73. The Candidate B site would be located in the southerly portion of this property. AT&T would lease a 100-foot by 100-foot parcel, within which it would erect a 190-foot monopole tower inside a 75-foot by 75-foot equipment compound enclosed by an eight-foot high chain link fence. AT&T's ground equipment would be installed inside a 12-foot by 20-foot equipment shelter. (AT&T 1, p. 14; Attachment 4A Drawings C01 and Compound Plan)
- 74. For backup power, AT&T would utilize a 50 kW diesel generator. AT&T would also have a battery backup in order avoid a "re-boot" condition during the generator start-up delay period. The typical run time of the generator before it requires refueling is 48 hours. (AT&T 3, A17; Tr. 1, p. 73)
- 75. The generator would be designed with secondary containment capable of retaining 110 percent of the oil fill. (Tr. 1, p. 32)
- 76. The proposed tower would be located at 41° 51′ 48.3″ North latitude and 72° 16′ 28.3″ West longitude. Its elevation at ground level would be approximately 682 feet above mean sea level. (AT&T 1, Attachment 4 Site B: Site Evaluation Report)
- 77. AT&T's proposed tower would be designed in accordance with American National Standards Institute EIA/TIA-222-G "Structural Standards for Steel Antenna Towers and Antenna Support Structures" and the 2003 International Building Code with 2005 Connecticut Amendment. The foundation design would be based on existing soil conditions. The diameter of the tower would be approximately four and one-half feet at its base and two feet at its top. (AT&T 1, Attachment 4 Candidate B: Facilities and Equipment Specification)

- 78. AT&T would initially install nine multi-band antennas on a low profile platform at a centerline height of 187 feet agl. (AT&T 1, Attachment 4 Candidate B: Facilities and Equipment Specification; Attachment 4A Drawing Sheet Tower Elevation; Tr. 1, p. 14)
- 79. The tower would be designed to accommodate three other carriers, in addition to AT&T. (AT&T 1, Attachment 4 Candidate B: Facilities and Equipment Specification; Tr. 1, p. 28)
- 80. Development of the Candidate B site would require 590 cubic yards of cut and 286 cubic yards of fill. (AT&T 3, A5)
- 81. Vehicular access to the Candidate B site would be over a new gravel access drive from Old South Willington Road that would be 958 feet long and 12 feet wide. (AT&T 1, Attachment 4 Candidate B: General Facility Description)
- 82. Underground electric and telephone utilities would be extended from a proposed riser utility pole to the Candidate B site within the easement for the access drive. (AT&T 1, Attachment 4 Candidate B: General Facility Description; Attachment 4A Drawing Sheets C01 and Compound Plan)
- 83. AT&T does not anticipate the need for blasting. If ledge is encountered, mechanical means would be the preferred method of removal. (AT&T 3, A6)
- 84. The setback radius of the proposed tower would be contained within the host property. (AT&T 1, Attachment 4A Drawing Sheet C02B)
- 85. There are eight residences within 1,000 feet of the Candidate B site. (AT&T 1, Attachment 4A)
- 86. The nearest residence to the Candidate B site is located 550 feet to the southwest at 52 Old South Willington Road. It is owned by Robert and Marissa Golden. (AT&T 1, Attachment 4A)
- 87. Land uses within one-quarter mile of the proposed facility include a sand and gravel mining operation, and commercial and residential properties. (AT&T 1, Attachment 4 Site B: Site Evaluation Report)
- 88. The estimated cost of the proposed facility is:

Tower and foundation	\$ 90,000
Site development costs	47,900
Utility installation	28,740
Facility installation	93,000
Antennas and equipment	<u>250,000</u>
Total cost	\$509,640

(AT&T 1, p. 23)

# **Environmental Considerations**

#### Candidate A

- 89. The State Historic Preservation Office (SHPO) initially expressed concerns about potentially adverse effects on visual resources of a 160-foot tower at the Candidate A site. However, this conclusion was based on an understanding that a nearby historic cemetery was located on the south side of Tolland Turnpike instead of on the north side, where it is actually located. AT&T requested SHPO to reconsider its proposal given the proximity and visibility of other existing utility infrastructure in the vicinity of the cemetery. (AT&T 1, p. 17; Attachment 3 Candidate A Tolland Turnpike: Environmental Assessment Statement, II. Scenic, Natural, Historic & Recreational Values)
- 90. SHPO issued a later opinion based on revisions AT&T made to its originally proposed Candidate A Site. This SHPO opinion concluded that AT&T's revised proposal would have no adverse effect if the project were designed to be as unobtrusive as possible and, if not in use for six months, the tower and all related equipment would be removed. (Council Administrative Notice #51: SHPO letter dated November 28, 2012)
- 91. After reviewing the viewshed analysis, the Willington Planning and Zoning Commission concluded that the tower at the Candidate A site would have a miniscule impact on the town's historic district. (AT&T 1, Attachment 6 Memorandum from Willington Planning and Zoning Commission, dated November 10, 2010)
- 92. A facility at the Candidate A site would not impact any extant populations of Federal or State Endangered, Threatened or Special Concern Species. (AT&T 1, Attachment 3D Letter from DEEP, dated July 11, 2012)
- 93. Both proposed sites are located within the Willimantic Reservoir Public Water Supply Watershed of the Mansfield Hollow Reservoir. AT&T would adopt measures recommended by the Drinking Water Section of the Connecticut Department of Public Health to protect this water supply area. (AT&T 1, Attachment 5, Public Water Supply Assessment)
- 94. A facility at the Candidate A site would comply with the recommended guidelines of the US Fish and Wildlife Service for minimizing the potential for telecommunications towers to impact bird species. (AT&T 3, A7)
- 95. The Candidate A site is not located within an Important Bird Area (IBA) as designated by the National Audubon Society. The nearest IBA is located approximately 5.2 miles to the east. (AT&T 3, A8)
- 96. There is an isolated forested wetland system on the property, the nearest point of which is located approximately 47 feet from the proposed access drive to the Candidate A site. (AT&T 1, p. 22; Attachment 5 Wetland Investigation)
- 97. A drainage swale on the property is 33 feet at its nearest point from the proposed access road for Candidate A. (Tr. 1, p. 29)

- 98. AT&T would establish and maintain appropriate soil erosion and sedimentation control measures, in accordance with the 2002 <u>Connecticut Guidelines for Soil Erosion and Sediment Control</u> established by the Connecticut Council for Soil and Water Conservation, in cooperation with the Connecticut Department of Energy and Environmental Protection, throughout the construction period of the proposed facility. (AT&T 1, p. 22)
- 99. With erosion controls in place, the proposed facility at the Candidate A site should have no impact on any wetlands or watercourses. (NAT 1, p. 22; Attachment 5 Wetland Investigation)
- 100. The development of the Candidate A site would require the clearing of 55 trees with a diameter at breast height of six inches or greater. (AT&T 3, A18)
- 101. The proposed facility would not constitute an obstruction or hazard to air navigation and, therefore, would not require any obstruction marking or lighting. (AT&T 1, pp. 18-19; Attachment 3C)
- 102. The cumulative worst-case maximum power density from the radio frequency emissions from the operation of AT&T's proposed antennas at the Candidate A site would be 5.2% of the standard for Maximum Permissible Exposure, as adopted by the FCC, at the base of the proposed tower. This calculation was based on methodology prescribed by the FCC Office of Engineering and Technology Bulletin No. 65E, Edition 97-01 (August 1997) that assumes all antennas would be pointed at the base of the tower and all channels would be operating simultaneously, which creates the highest possible power density levels. Under normal operation, the antennas would be oriented outward, directing radio frequency emissions away from the tower, thus resulting in significantly lower power density levels in areas around the tower. (AT&T 1, Attachment 3C C Squared Systems RF Power Density Calculation)

# Candidate B

- 103. According to the SHPO, the proposed facility at the Candidate B site would have no adverse effect. (AT&T 1, p. 17; Attachment 4D Letter stamped by State Historic Preservation Office)
- 104. A facility at the Candidate B site would not impact any extant populations of Federal or State Endangered, Threatened or Special Concern Species. (AT&T 1, Attachment 4D – Letter from DEEP, dated July 11, 2012)
- 105. A facility at the Candidate B site would comply with the recommended guidelines of the US Fish and Wildlife Service for minimizing the potential for telecommunications towers to impact bird species. (AT&T 3, A7)
- 106. The Candidate B site is not located within an Important Bird Area (IBA) as designated by the National Audubon Society. The nearest IBA is located approximately 5.2 miles to the east. (AT&T 3, A8)
- 107. The access drive AT&T has proposed for the Candidate B site would pass approximately 100 feet from a wetland system. There is also a drainage culvert that is 79 feet at its nearest point to the access drive proposed for Candidate B. (AT&T 1, p. 22; Tr. 1, pp. 29-30)

Docket 429: Willington Findings of Fact Page 14

- 108. AT&T would establish and maintain appropriate soil erosion and sedimentation control measures, in accordance with the 2002 <u>Connecticut Guidelines for Soil Erosion and Sediment Control</u> established by the Connecticut Council for Soil and Water Conservation, in cooperation with the Connecticut Department of Energy and Environmental Protection, throughout the construction period of the proposed facility. (AT&T 1, p. 22)
- 109. With erosion controls in place, the proposed facility at the Candidate B site should have no impact on any wetlands or watercourses. (NAT 1, p. 22; Attachment 5 Wetland Investigation)
- 110. The development of the Candidate B site would require the clearing of 115 trees with a diameter at breast height of six inches or greater. (AT&T 1, Attachment 4A, Tree Inventory)
- 111. The proposed facility would not constitute an obstruction or hazard to air navigation and, therefore, would not require any obstruction marking or lighting. (AT&T 1, pp. 18-19; Attachment 4C)
- 112. The cumulative worst-case maximum power density from the radio frequency emissions from the operation of AT&T's proposed antennas at the Candidate B site would be 3.62% of the standard for Maximum Permissible Exposure, as adopted by the FCC, at the base of the proposed tower. This calculation was based on methodology prescribed by the FCC Office of Engineering and Technology Bulletin No. 65E, Edition 97-01 (August 1997) that assumes all antennas would be pointed at the base of the tower and all channels would be operating simultaneously, which creates the highest possible power density levels. Under normal operation, the antennas would be oriented outward, directing radio frequency emissions away from the tower, thus resulting in significantly lower power density levels in areas around the tower. (AT&T 1, Attachment 4C C Squared Systems RF Power Density Calculation)

#### **Visibility**

#### Candidate A

- 113. The proposed 160-foot tower at the Candidate A site would be visible on a year-round basis from approximately 71.7 acres within a two-mile radius of the site. (AT&T 1, Attachment 3B Visual Analysis Report)
- 114. From the Willington Historic District, the proposed 160-foot tower at the Candidate A site would appear to clip the treetops from the highest point on the town green and a larger portion of the tower would be visible through the trees on a seasonal basis. (Tr. 1, p. 16)
- 115. The proposed tower would be visible year round from Willington Hill Cemetery and Old West Cemetery. (AT&T 1, Attachment 3B Visual Analysis Report)
- 116. The proposed tower would be visible on a seasonal basis from approximately 16.3 acres within a two-mile radius of the Candidate A site. (AT&T 1, Attachment 3B Visual Analysis Report)

117. The table below lists the distances along which the proposed tower would be visible year-round from nearby streets and the number of residences within these stretches of roadway which would have year-round views of the tower.

Name of Street	Distance Visible	Number of residential properties with potential year round views
Glass Factory Road	1,150'	1
Willington Hill Road (State Route 320)	285'	0
Tolland Turnpike (State Route 74)	370', 670', 1,635'	10

(AT&T 1, Attachment 3B – Visual Analysis Report)

118. The table below lists the distances along which the proposed tower would be seasonally visible from nearby streets and the number of residences within these stretches of roadway that would have seasonal views of the tower.

Name of Street	Distance Visible	Number of residential properties with potential year-round views
Old Farms Road	1,500'	6
Jared Sparks Road	465'	0
Common Road	575'	0
Tolland Turnpike (State Route 74)	705'	0

(AT&T 1, Attachment 3B – Visual Analysis Report)

- 119. The proposed tower would be seasonally visible from the Willington Common Historic District, St. Jude Church and Rectory, and two town-designated historic properties on Old Farms Road. (AT&T 1, Attachment 3B Visual Analysis Report)
- 120. The visibility of the proposed tower at Candidate A site from different vantage points in the surrounding vicinity is summarized in the following table. The vantage points listed are identified by their corresponding number in the Visual Analysis Report contained in Attachment 3B of AT&T's application.

Location	<u>Visibility</u>	Approx. Portion of (160') Tower	Approx. Distance and Direction to Tower
		Visible	
1 – Willington Hill Cemetery	Year-round	35'	1,410 feet, SE
2 – Old West Cemetery	Year-round	20'	1,600 feet, SE
3 – Tolland Turnpike	Year-round	75'	1,525 feet, SE
4 – Tolland Turnpike	Year-round	105'	7,090 feet, E

(Table continued on next page)

Location	<u>Visibility</u>	Approx. Portion of (160') Tower	Approx. Distance and Direction to Tower
		<u>Visible</u>	
5 – Tolland Turnpike	Year-round	80'	5,700 feet, E
6 – Koller Road	None	n/a	4,060 feet, E
7 – Glass Factory Road	Year-round	10'	6,990 feet, E
8 – Old Farms Road	Seasonal	30'	4,550 feet, NW
9 – Green of Willington Common	Seasonal	75'	1,510 feet, W
Historic District			
10 – Hiram Rider House (Willington	Seasonal	10'	1,430 feet, W
Common Historic District)			
11 – Daniel Glazier Tavern (Willington	Seasonal	10'	1,030 feet, W
Common Historic District)			
12 – Old Baptist Parsonage (Willington	Seasonal	30'	1,365 feet, SW
Common Historic District)			
13 – Old Congregational Church	Seasonal	60'	1,550 feet, W
(Willington Common Historic District)			
14 – Crossgrove Road	None	n/a	5,480 feet, SW

(AT&T 1, Attachment 3B – Visual Analysis Report)

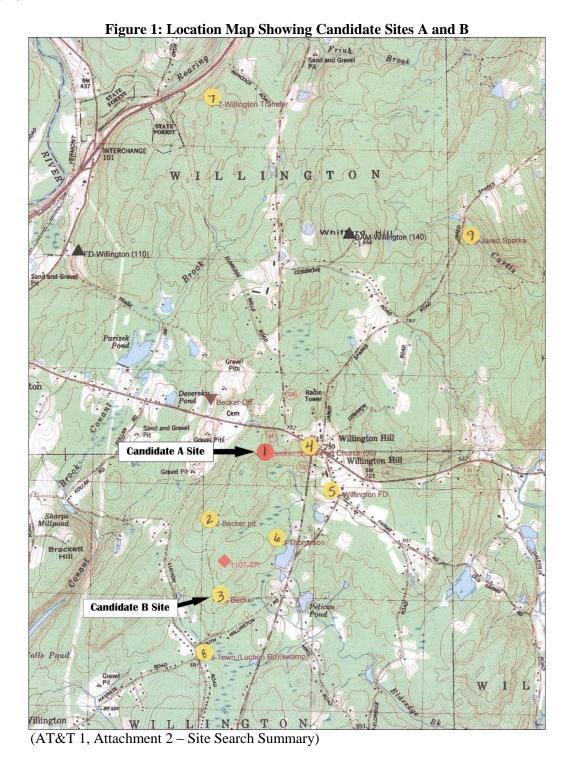
#### Candidate B

- 121. The proposed 190-foot tower at the Candidate B site would be visible on a year-round basis from approximately 20 acres within a two-mile radius of the site. Most of this acreage occurs over open water on undeveloped land, part of a large wetland area south of the site, and open land located to the northeast. (AT&T 1, Attachment 4B Visual Analysis Report)
- 122. Approximately six residential properties, within a two-mile radius of the site, would have at least partial year-round views of the tower at this location. Two of these properties are located along Route 320. One property is along Mirtl Road. One property is located along Luchon Road. One property is located along Glass Factory Road. One property is located along Lindsey Lane. (AT&T 1, Attachment 4B Visual Analysis Report)
- 123. The proposed Candidate B tower would be visible on a seasonal basis from approximately 18 acres within a two-mile radius of its proposed location. (AT&T 1, Attachment 4B Visual Analysis Report)
- 124. Approximately three residential properties within a two-mile radius would have seasonal views of the tower at the Candidate B site. One of these properties is located along Route 320; one property is located along Luchon Road; and one property is located off of Old South Willington Road. (AT&T 1, Attachment 4B Visual Analysis Report)

125. The visibility of the proposed tower at Candidate B site from different vantage points in the surrounding vicinity is summarized in the following table. The vantage points listed are identified by their corresponding number in the Visual Analysis Report contained in Attachment 4B of AT&T's application.

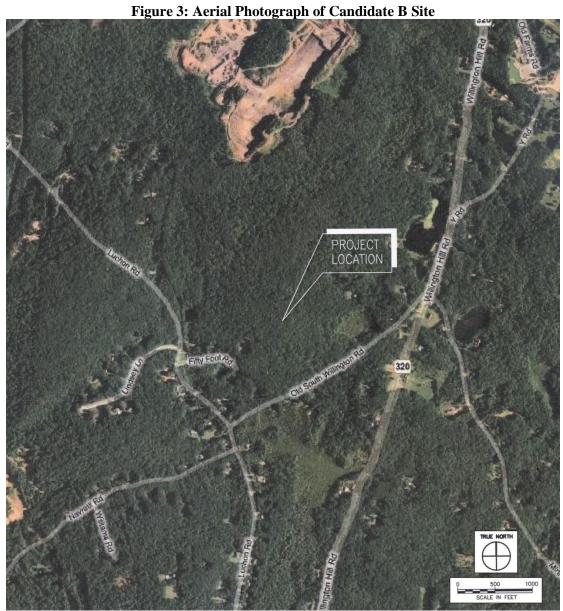
Location	Visibility	Approx. Portion of (190') Tower Visible	Approx. Distance and Direction to Tower
1 – Intersection of Y Road and Route 320	Year-round	10'	2,640 feet, SW
2 – Tolland Turnpike	None	n/a	5,170 feet, S
3 – Willington Town Green	None	n/a	5,330 feet, S
4 – Willington Town Hall parking lot	None	n/a	4,750 feet, SW
5 – Willington Center School parking lot	None	n/a	4,700 feet, SW
6 – Lindsey Lane cul-de-sac	None	n/a	4,700 feet, NE
7 – #4 Lindsey Lane	Year-round	50'	1,850 feet, E
8 – 87 Luchon Road	None	n/a	1,530 feet, E
9 – Willington Woods Senior Housing – Old Farms Road	None	n/a	4,700 feet, SW
10 – Willington Hill Cemetery	None	n/a	5,540 feet, S

(AT&T 1, Attachment 4B – Visual Analysis Report)

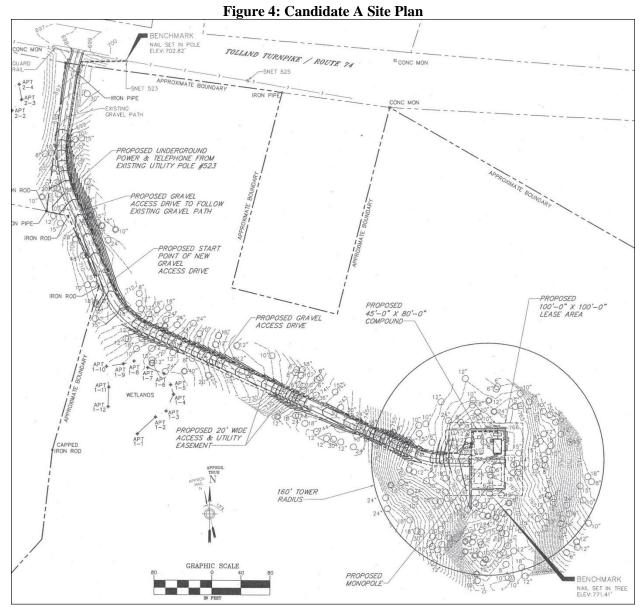




(AT&T 1, Attachment 3 – Candidate A: General Facility Description)



(AT&T 1, Attachment 4 – Candidate B: General Facility Description)



(AT&T 1, Attachment 3A, Sheet CO2, Site Access Map)

Figure 5: Candidate B Site Plan

(AT&T 1, Attachment 4A – Sheets C02A and C02B)

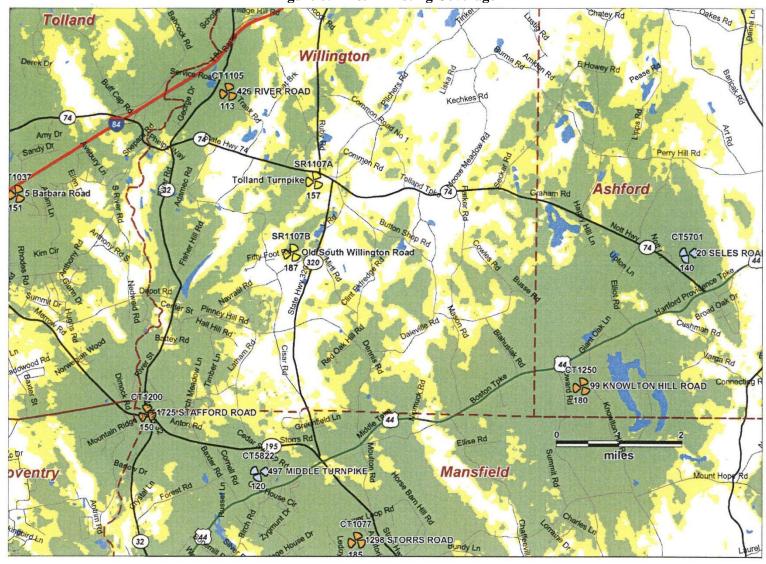


Figure 6: AT&T Existing Coverage

(AT&T 7, Updated RF Information – Radio Frequency Analysis Report, p. 10)

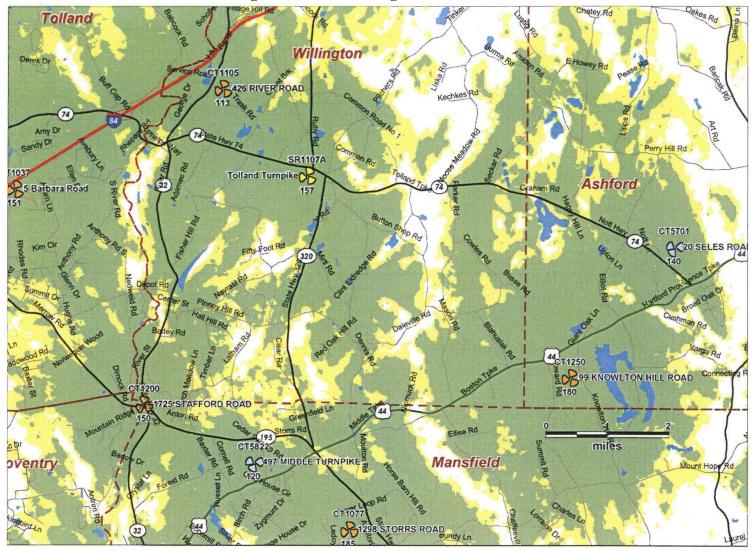


Figure 7: AT&T Coverage with Candidate A

(AT&T 7, Updated RF Information – Radio Frequency Analysis Report, p. 11)

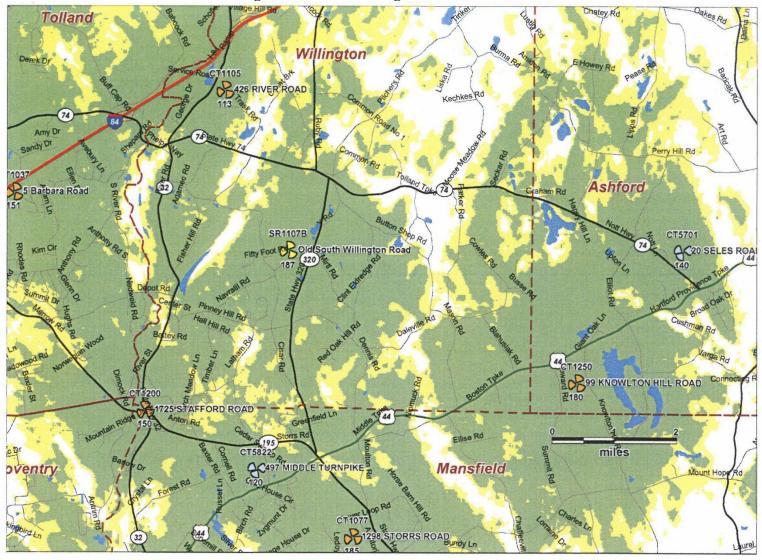


Figure 8: AT&T Coverage with Candidate B

(AT&T 7, Updated RF Information – Radio Frequency Analysis Report, p. 12)

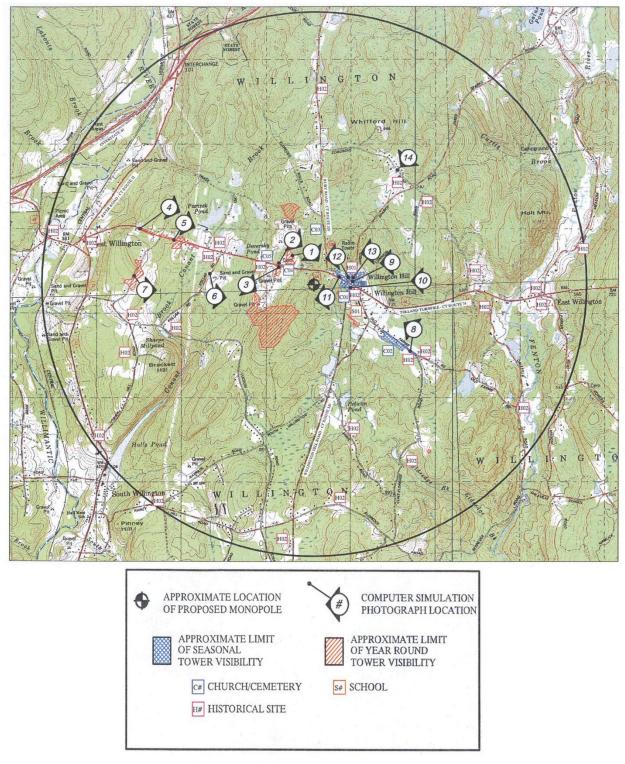


Figure 9: Candidate A 2-Mile Viewshed Analysis Map

(AT&T 1, Attachment 3B – Visual Analysis Report)

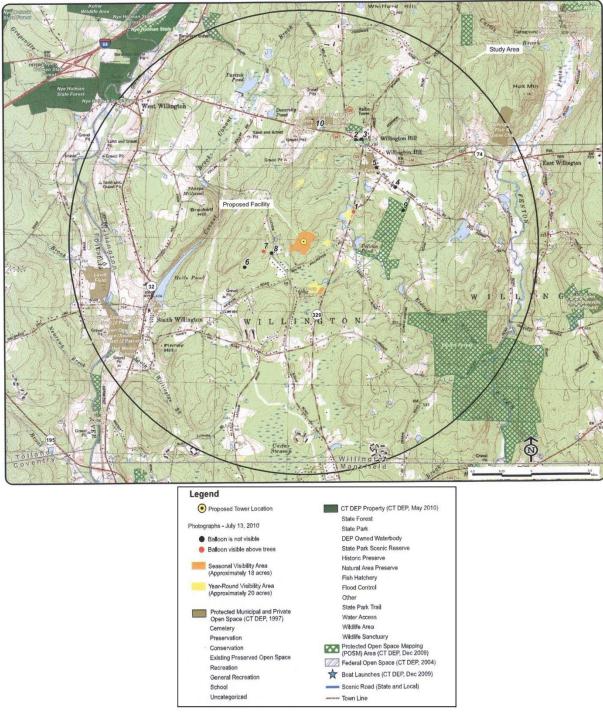


Figure 10: Candidate B 2-Mile Viewshed Analysis

(AT&T 1, Attachment 4B, Visual Resource Evaluation Report)

# Exhibit B

# **Property Card**

Please see attached Statutory Form Warranty Deed transferring ownership from Diane Becker to Tarpon Towers I, LLC dated September 13, 2021 and recorded on September 28, 2021, Book 228, Page 396-397

# **109 SCHOFIELD RD**

Location 109 SCHOFIELD RD Mblu 47//009-0A//

Acct# 00192000 Owner SCHOFIELD, CAROL E

**Assessment** \$214,260 **Appraisal** \$312,170

PID 4301 Building Count 1

#### **Current Value**

Appraisal			
Valuation Year	Improvements	Land	Total
2018	\$255,280	\$56,890	\$312,170
Assessment			
Valuation Year	Improvements	Land	Total
2018	\$178,700	\$35,560	\$214,260

# Owner of Record

Owner

SCHOFIELD, CAROL E Sale Price \$0

Co-Owner Certificate

Address 109 SCHOFIELD RD Book & Page 86/399

WILLINGTON, CT 06279 Sale Date 08/15/2014

# **Building Information**

# **Building 1: Section 1**

Year Built: 1987
Living Area: 2,499
Replacement Cost: \$290,092
Building Percent Good: 88

Replacement Cost

Less Depreciation: \$255,280

Building Attributes			
Field Description			
Style	Modern/Contemp		
Model	Residential		
Grade:	Good		
Stories:	1.5		
Occupancy	1		

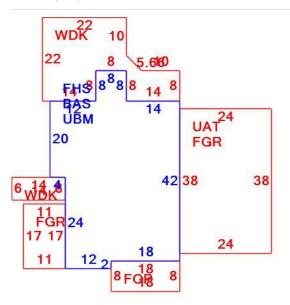
Exterior Wall 1	Clapboard
Exterior Wall 2	
Roof Structure:	Gable or Hip
Roof Cover	Asphalt
Interior Wall 1	Drywall/Sheet
Interior Wall 2	
Interior FIr 1	Average
Interior FIr 2	
Heat Fuel	Oil
Heat Type:	Hot Water
AC Type:	None
Total Bedrooms:	4 Bedrooms
Total Bthrms:	2
Total Half Baths:	0
Total Xtra Fixtrs:	2
Total Rooms:	6
Bath Style:	
Kitchen Style:	
Fireplaces	1
Bsmt Garage	None

# **Building Photo**



(http://images.vgsi.com/photos/WillingtonCTPhotos//00\00\01\24.jpg)

# **Building Layout**



(ParcelSketch.ashx?pid=4301&bid=4301)

Building Sub-Areas (sq ft)			<u>Legend</u>
Code	Description	Gross Area	Living Area
BAS	First Floor	1,428	1,428
FHS	Half Story, Finished	1,428	1,071
FGR	Garage	1,099	0
FOP	Open Porch	144	0
UAT	Unfinished Attic	912	0
UBM	Unfinished Basement	1,428	0
WDK	Wood Deck	624	0
		7,063	2,499

# **Extra Features**

Extra Features	<u>Legend</u>
No Data for Extra Features	

# Land

Land Use		Land Line Valuation	
Use Code	1010	Size (Acres)	7.4
Description	Single Fam MDL-01	Frontage	
Zone	R80	Depth	
Neighborhood	110	Assessed Value	\$35,560
Alt Land Appr	No	Appraised Value	\$56,890
Category			

# Outbuildings

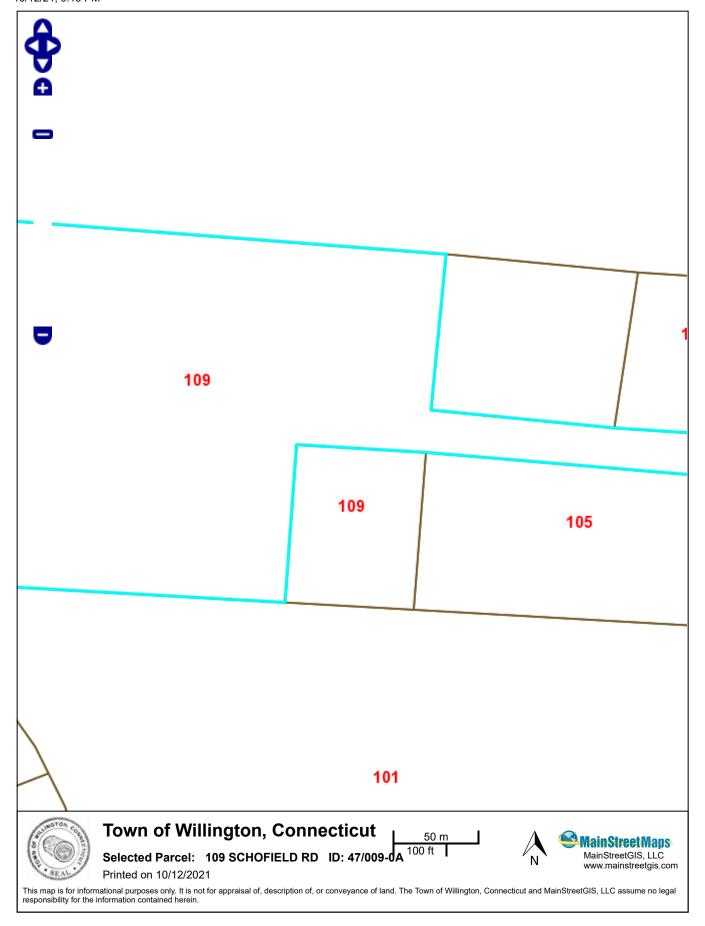
Outbuildings	Legend
No Data for Outbuildings	

# **Valuation History**

Appraisal			
Valuation Year	Improvements	Land	Total
2019	\$255,280	\$56,890	\$312,170

Assessment			
Valuation Year	Improvements	Land	Total
2019	\$178,700	\$35,560	\$214,260

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Book: 228 Page: 396 Page: 1 of 2



After Recording, return to:

AFTER RECORDING, PLEASE RETURN TO: Fidelity National Title Group 7130 Glen Forest Dr., Ste. 300 Richmond, VA 23226 Attn:

### STATUTORY FORM WARRANTY DEED

DIANE BECKER, of the Town of Willington, County of Tolland and State of Connecticut, for the consideration of Two Hundred Fifty Thousand and no/100 Dollars (\$250,000.00), grants to TARPON TOWERS II, LLC, a Florida limited liability company, with WARRANTY COVENANTS, a certain piece or parcel of land situated in the Town of Willington, County of Tolland and State of Connecticut, known as 109 Schofield Road, and being more particularly described in Schedule A attached hereto and made a part hereof.

Said premises are conveyed subject to the following:

- 1. Real estate taxes on the List of October 1, 2018 and thereafter, which the Grantee herein assumes and agrees to pay as part consideration for this transfer.
- 2. Any and all provisions of any ordinance, municipal regulation, or public or private law.
- 3. Any declarations, restrictions, covenants, and easements of record.
- 4. Any state of facts an accurate survey or personal inspection of the property might reveal.

Being the same premises acquired by the grantor herein by virtue of a Warranty Deed from The Joseph J. Mottes Company, dated December 7, 2017 and recorded December 8, 2017 in Volume 216 at Page 1087 of the Willington Land Records.

Signed this 15th day of September, 2021.

Witnessed by:

STATE OF CONNECTICUT

) ss. Glastonbury

September /5, 2021

COUNTY OF HARTFORD

The foregoing instrument was acknowledged before me this \_/s day of September, 2021, by Diane Becker, as her free act and deed.

**CONVEYANCE TAX RECEIVED** 

TOWN \$ (25.10 STATE \$ -

**ROBIN CAMPBELL** TOWN CLERK OF WILLINGTON

Commissioner of the Superior Court

Book: 228 Page: 396 Page: 2 of 2

# SCHEDULE A Property Description

A certain piece or parcel of land situated in the Town of Willington, County of Tolland and State of Connecticut, bounded and described as follows, to wit:

BEGINNING at an iron pin at the Northeast corner of the premises herein described, said point being the Northwest corner of premises now or formerly, of Edward R. and Marian N. Dell, and situated in the Southerly line of a 50 foot right of way; thence N. 70° 09'10" W. One Hundred Eighty-nine and 20/100 (189.20) feet in the Southerly line of an extension of said right of way, to an iron pin; thence S. 19° 50'50" W. Two Hundred Thirty-one and 11/100 (231.11) feet along other land of George L. Schofield, Jr. and Rose Schofield to an iron pin at land now or formerly of Stuart S. Schofield; thence S. 70° 42' E. One Hundred Eighty-nine and 21/100 (189.21) feet along land now or formerly of said Stuart S. Schofield to an iron pin; thence N. 19° 50' 50" E. Two Hundred Twenty-nine and 30/100 (229.30) feet along land of said Dells to an iron pin which is point and place of beginning.

TOGETHER WITH the use of a right of way fifty (50) feet wide extending from the Westerly side of Schofield Road to the Westerly boundary of the herein conveyed land.

AND BEING the same property conveyed to The Joseph J. Mottes Company from George L. Schofield, Jr. and Rose Schofield by Warranty Deed dated September 16, 1968 and recorded October 05, 1968 in Deed Book 49, Page 192; AND FURTHER CONVEYED to Diane Becker from The Joseph J. Mottes Company by Quit Claim Deed dated December 07, 2017 and recorded December 08, 2017 in Deed Book 216, Page 1087.

RECEIVED SEP 28 2021

Received for Record at Willington, Ct On 09/29/2021 At 2:09:06 pm

# Exhibit C

**Construction Drawings** 

# dish wireless.

DISH WIRELESS, LLC. SITE ID:

### **BOBDL00147A**

DISH WIRELESS, LLC. SITE ADDRESS:

# 109 SCHOFIELD ROAD **WILLINGTON, CT 06279**

### CONNECTICUT CODE COMPLIANCE

ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALLED IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE CODES:

2018 CT STATE BUILDING CODE/2015 IBC W/ CT AMENDMENTS 2018 CT STATE BUILDING CODE/2015 IMC W/ CT AMENDMENTS 2018 CT STATE BUILDING CODE/2017 NEC W/ CT AMENDMENTS MECHANICAL

	SHEET INDEX
SHEET NO.	SHEET TITLE
T-1	TITLE SHEET
	ALEDALI AND ENLADOED OFF DIAM
A-1	OVERALL AND ENLARGED SITE PLAN
A-2 A-3	ELEVATION, ANTENNA LAYOUT AND SCHEDULE
A-3	EQUIPMENT PLATFORM AND H-FRAME DETAILS
A-4	EQUIPMENT DETAILS
A-5	EQUIPMENT DETAILS
A-6	EQUIPMENT DETAILS
E-1	ELECTRICAL/FIBER ROUTE PLAN AND NOTES
E-2	ELECTRICAL DETAILS
E-3	ELECTRICAL ONE-LINE, FAULT CALCS & PANEL SCHEDULE
G-1	GROUNDING PLANS AND NOTES
G-2	GROUNDING DETAILS
G-3	GROUNDING DETAILS
RF-1	RF CABLE COLOR CODE
RF-2	RF PLUMBING DIAGRAM
GN-1	LEGEND AND ABBREVIATIONS
GN-2	GENERAL NOTES
GN-3	GENERAL NOTES
GN-4	GENERAL NOTES

### SCOPE OF WORK

THIS IS NOT AN ALL INCLUSIVE LIST. CONTRACTOR SHALL UTILIZE SPECIFIED EQUIPMENT PART OR ENGINEER APPROVED EQUIVALENT. CONTRACTOR SHALL VERIFY ALL NEEDED EQUIPMENT TO PROVIDE A FUNCTIONAL SITE. THE PROJECT GENERALLY CONSISTS OF THE FOLLOWING:

- TOWER SCOPE OF WORK:

   INSTALL (3) PROPOSED PANEL ANTENNAS (1 PER SECTOR)

   INSTALL (3) PROPOSED ANTENNA MOUNTS (1 PER SECTOR)
- INSTALL PROPOSED JUMPERS
  INSTALL (6) PROPOSED RRUS (2 PER SECTOR)
- INSTALL (1) PROPOSED OVER VOLTAGE PROTECTION DEVICE (OVP) INSTALL (1) PROPOSED HYBRID CABLE

- INSTALL (1) PROPOSED METAL PLATFORM
  INSTALL (1) PROPOSED ICE BRIDGE
- INSTALL (1) PROPOSED PPC CARINET
- INSTALL (1) PROPOSED EQUIPMENT CABINET
- PROPOSED POWER CONDUIT INSTALL (1) PROPOSED TELCO CONDUIT
- INSTALL (1) PROPOSED TELCO-FIBER BOX
- INSTALL (1) PROPOSED GPS LINIT
- INSTALL (1) PROPOSED SAFETY SWITCH (IF REQUIRED)
- INSTALL (1) PROPOSED CIENA BOX (IF REQUIRED)
  EXISTING METER SOCKET ON EXISTING UTILITY POLE TO BE UTILIZED

### SITE PHOTO





UNDERGROUND SERVICE ALERT CBYD 811 UTILITY NOTIFICATION CENTER OF CONNECTICUT (800) 922-4455 WWW.CBYD.COM

CALL 2 WORKING DAYS UTILITY NOTIFICATION PRIOR TO CONSTRUCTION

### **GENERAL NOTES**

THE FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION. A TECHNICIAN WILL VISIT THE SITE AS REQUIRED FOR ROUTINE MAINTENANCE. THE PROJECT WILL NOT RESULT IN ANY SIGNIFICANT DISTURBANCE OR EFFECT ON DRAINAGE. NO SANITARY SEWER SERVICE, POTABLE WATER, OR TRASH DISPOSAL IS REQUIRED AND NO COMMERCIAL SIGNAGE IS PROPOSED.

#### 11"x17" PLOT WILL BE HALF SCALE UNLESS OTHERWISE NOTED

CONTRACTOR SHALL VERIFY ALL PLANS, EXISTING DIMENSIONS, AND CONDITIONS ON THE JOB SITE, AND SHALL IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK.

#### PROPERTY OWNER: TARPON TOWER DISH WIRELESS, LLC. ADDRESS: 109 SCHOFIELD ROAD 5701 SOUTH SANTA FE DRIVE WILLINGTON, CT 06279 LITTLETON, CO 80120 TOWER TYPE: GUYED TOWER TOWER CO SITE ID: TOWER OWNER: TARPON TOWER 905 E MARTIN LUTHER KING JR DR, TOWER APP NUMBER: TARPON SPRINGS, FL 34689 COUNTY: TOLLAND SITE DESIGNER: 1033 WATERVLIET SHAKER RD LATITUDE (NAD 83): 41° 55' 20.14" N 41.922261 N ALBANY, NY 12205 LONGITUDE (NAD 83): -72° 17' 37.14" W (518) 690-0790 -72.293650 W SITE ACQUISITION: TIMOTHY SLOAN ZONING JURISDICTION: CITY OF TOLLAND (303) 706-4606 ZONING DISTRICT: CONSTRUCTION MANAGER: JAVIER SOTO PARCEL NUMBER: 4301 (617) 839-6514 BOSSENER CHARLES OCCUPANCY GROUP: RF ENGINEER: (917) 567-9837 CONSTRUCTION TYPE: POWER COMPANY: EVERSOURCE TELEPHONE COMPANY: AT&T

PROJECT DIRECTORY

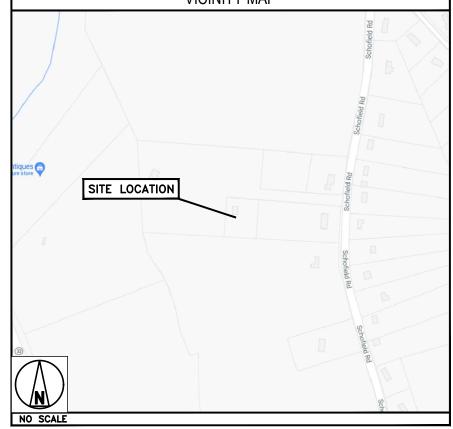
### **DIRECTIONS**

#### DIRECTIONS FROM SIMSBURY AIRPORT:

SITE INFORMATION

DEPART AND HEAD TOWARD WOLCOTT RD, TURN RIGHT ONTO WOLCOTT RD, BEAR RIGHT ONTO FLOYDVILLE RD, BEAR RIGHT ONTO CT-189 / HARTFORD AVE, TAKE THE RAMP ON THE RIGHT FOR CT-187 SOUTH AND HEAD TOWARD BLOOMFIELD / HARTFORD, CONTINUE ON DAY HILL RD, TAKE THE RAMP ON THE RIGHT FOR I-91 SOUTH AND HEAD TOWARD HARTFORD, AT EXIT 35A, HEAD RIGHT ON THE RAMP FOR I-291 TOWARD MANCHESTER, TAKE THE RAMP ON THE LEFT FOR I-84 EAST AND HEAD TOWARD BOSTON, AT EXIT 70, HEAD RIGHT ON THE RAMP FOR CT-32 TOWARD STAFFORD SPRINGS, TURN LEFT ONTO CT-32 / RIVER RD TOWARD STAFFORD SPRINGS, TURN RIGHT ONTO SCHOFIELD RD, ARRIVE AT 109 SCHOFIELD ROAD WILLINGTON, CT 06279

### **VICINITY MAP**





5701 SOUTH SANTA FF DRIVE LITTLETON, CO 80120



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2039-Z5555C

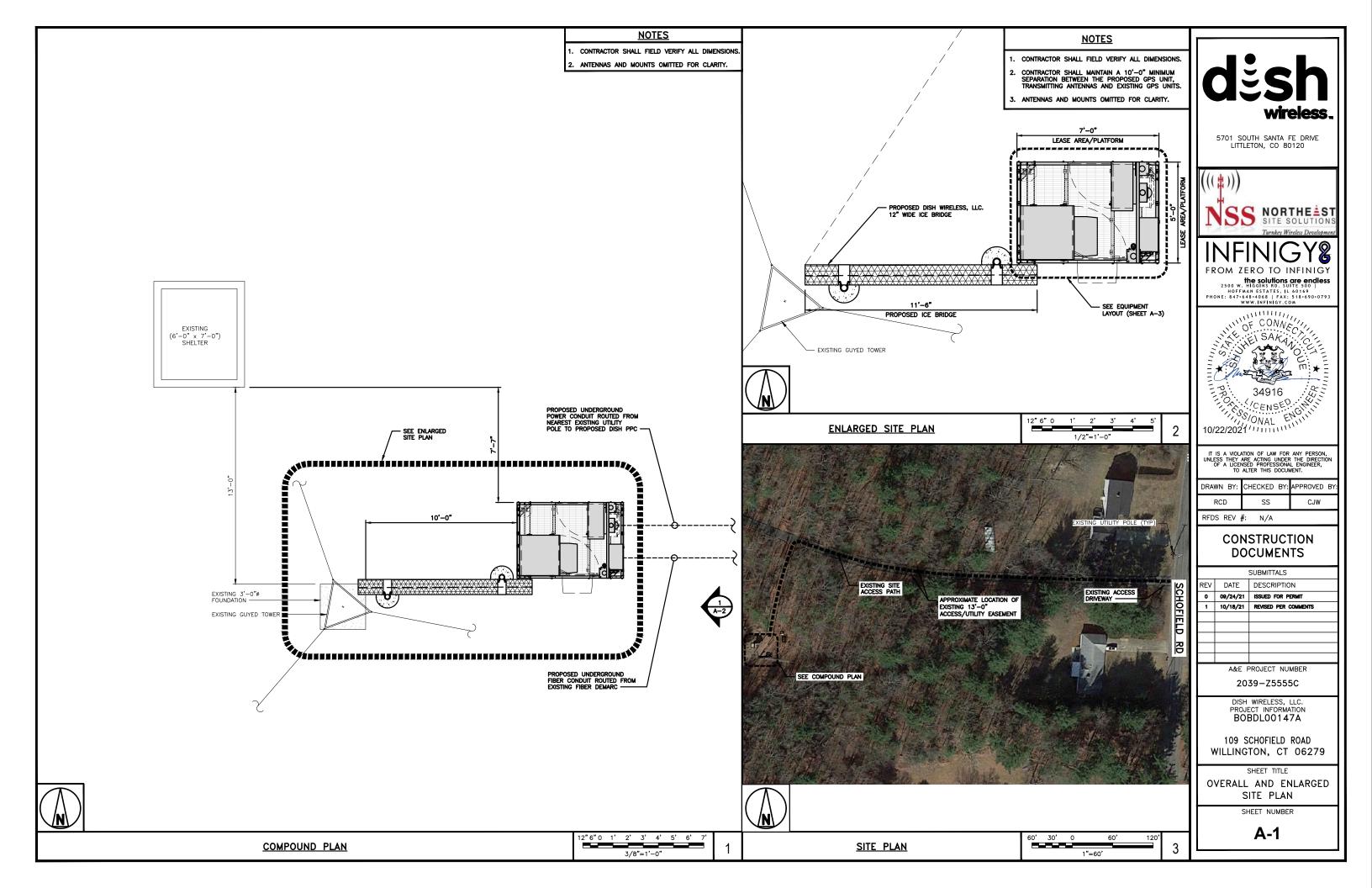
DISH WIRELESS, LLC. BOBDLO0147A

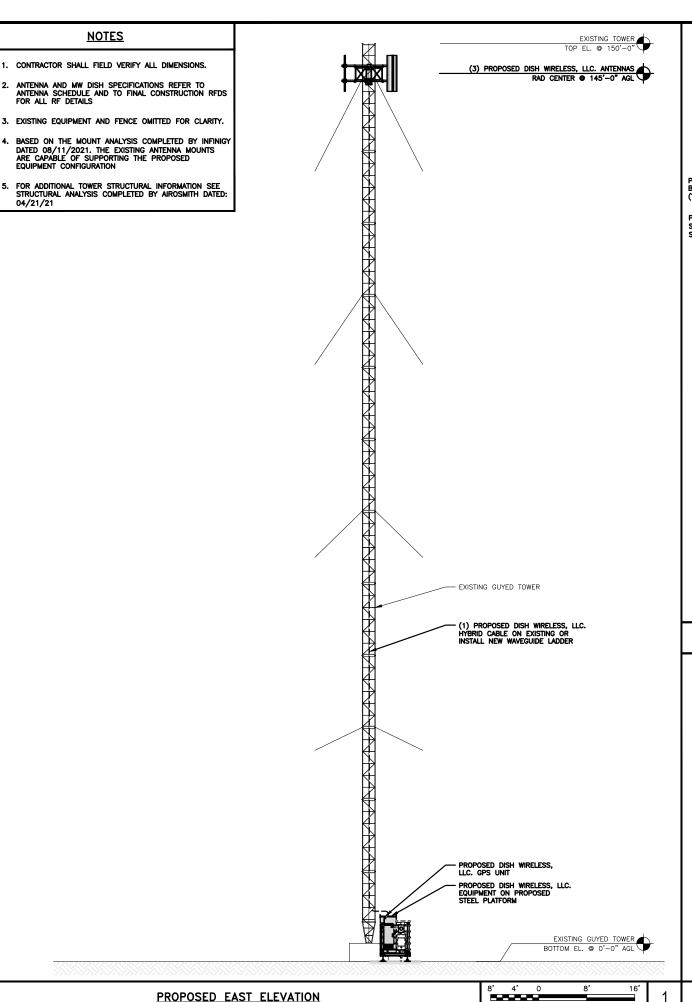
109 SCHOFIELD ROAD WILLINGTON, CT 06279

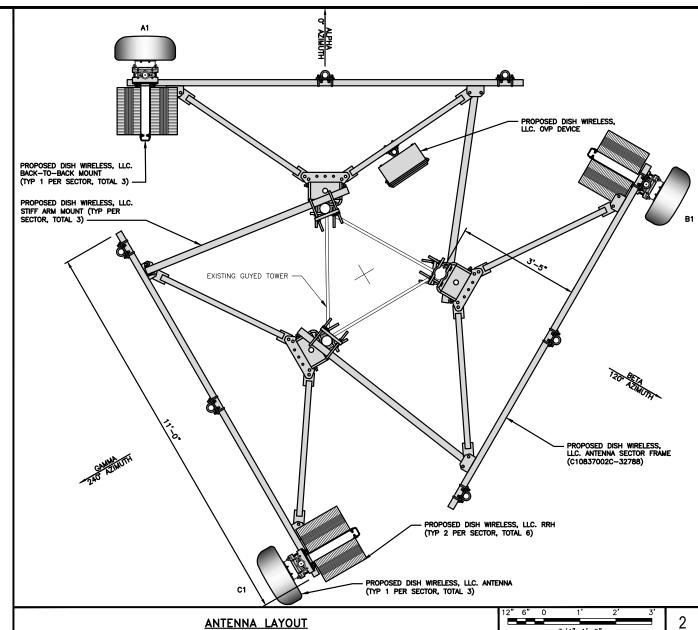
> SHEET TITLE TITLE SHEET

SHEET NUMBER

T-1







			AN	TENNA				TRANSMISSION CABLE
SECTOR	TOR POSITION	EXISTING OR PROPOSED	MANUFACTURER — MODEL NUMBER	TECHNOLOGY	SIZE (HxW)	AZMUITH	RAD CENTER	FEED LINE TYPE AND LENGTH
ALPHA	A1	PROPOSED	JMA WIRELESS - MX08FR0665-21	5G	72.0" × 20.0"	O.	145'-0"	(1) HIGH-CAPACITY
BETA	B1	PROPOSED	JMA WIRELESS - MX08FR0665-21	5G	72.0" × 20.0"	120°	145'-0"	HYBRID CABLE (165' LONG)
GAMMA	C1	PROPOSED	JMA WIRELESS — MX08FR0665—21	5G	72.0" × 20.0"	240°	145'-0"	(100 2010)

#### NOTES

1/8"=1'-0"

1. CONTRACTOR TO REFER TO FINAL CONSTRUCTION RFDS FOR ALL RF DETAILS.

2. ANTENNA OR RRH MODELS MAY CHANGE DUE TO EQUIPMENT AVAILABILITY. ALL EQUIPMENT CHANGES MUST BE APPROVED AND REMAIN IN COMPLIANCE WITH THE PROPOSED DESIGN AND STRUCTURAL ANALYSES.

		RRH			
SECTOR	POSITION	MANUFACTURER — MODEL NUMBER	TECHNOLOGY	1.	
ALPHA	A1	FUJITSU - TA08025-B604	5G	2.	
ALFIIA	A1	FUJITSU - TA08025-B605	5G		
BETA	B1	FUJITSU - TA08025-B604	5G		
BLIA	B1	FUJITSU - TA08025-B605	5G		
04144	C1	FUJITSU - TA08025-B604	5G		
GAMMA	C1	FUJITSU - TA08025-B605	5G		

- CONTRACTOR TO REFER TO FINAL CONSTRUCTION RFDS FOR ALL RF DETAILS.
- ANTENNA AND RRH MODELS MAY CHANGE DUE TO EQUIPMENT AVAILABILITY. ALL EQUIPMENT CHANGES MUST BE APPROVED AND REMAIN IN COMPLIANCE WITH THE PROPOSED DESIGN AND STRUCTURAL ANALYSES.

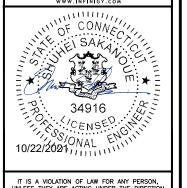
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109 SCHOFIELD ROAD WILLINGTON, CT 06279

SHEET TITLE

ELEVATION, ANTENNA LAYOUT AND SCHEDULE

SHEET NUMBER

**A-2** 

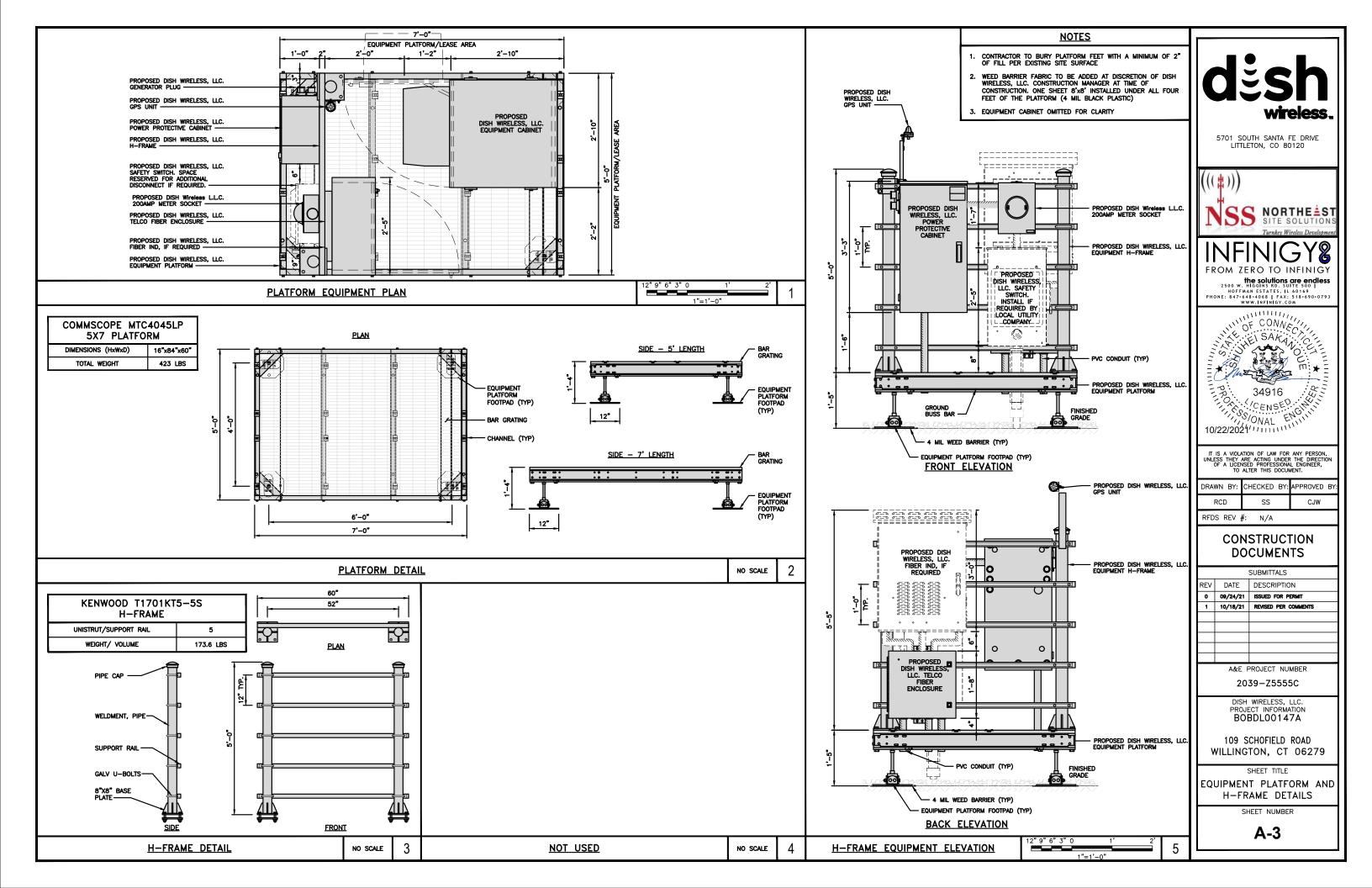
ANTENNA SCHEDULE

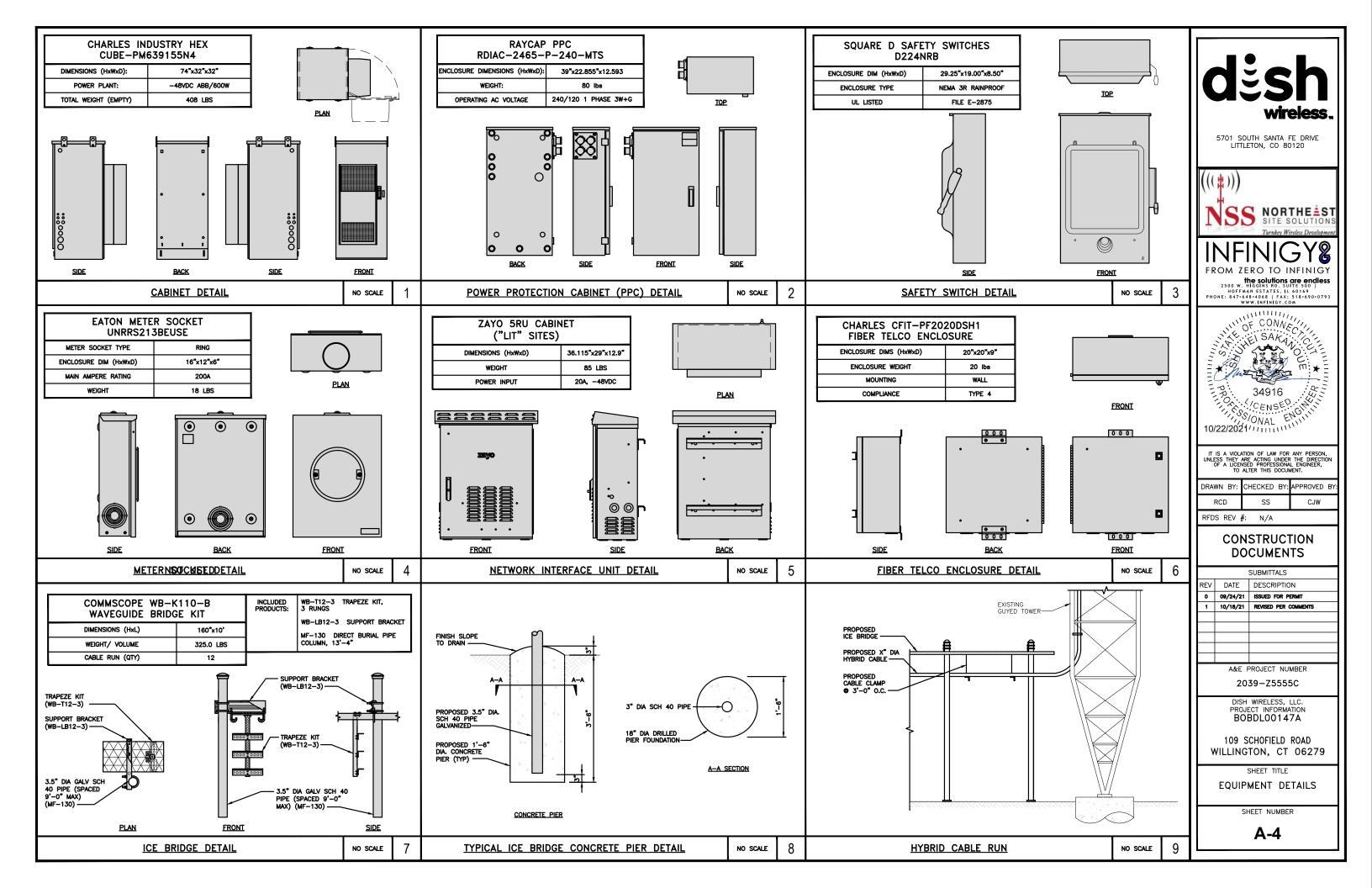
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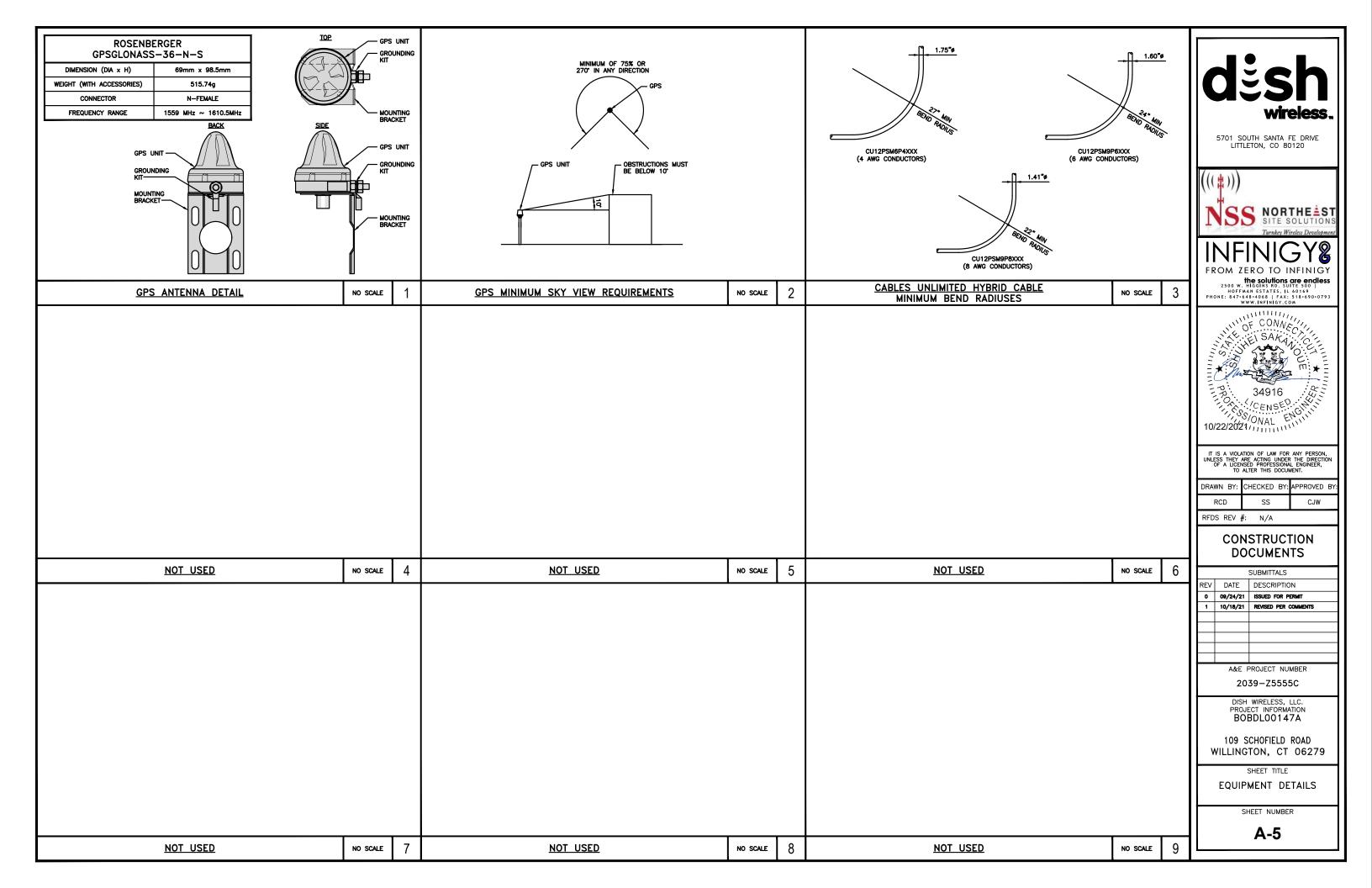
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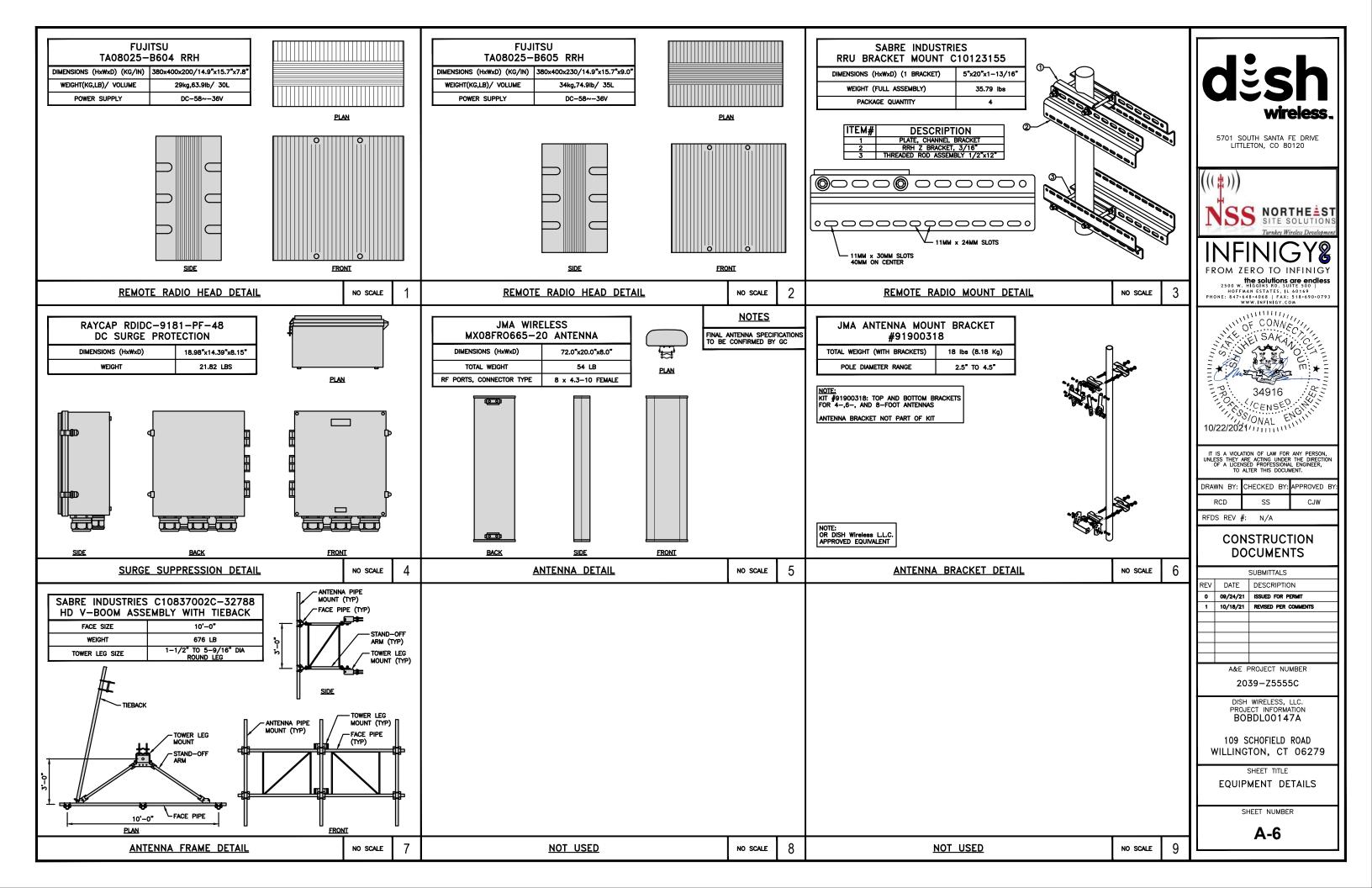
3/4"=1'-0"

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#### **NOTES**

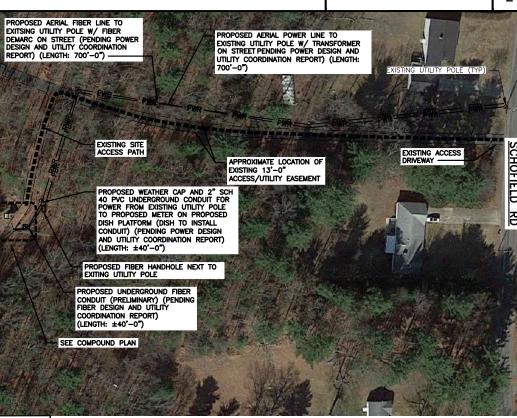
- CONTRACTOR SHALL FIELD VERIFY ALL PROPOSED UNDERGROUND UTILITY CONDUIT ROUTE.
- ANTENNAS AND MOUNTS OMITTED FOR CLARITY.

DC POWER WIRING SHALL BE COLOR CODED AT EACH END FOR IDENTIFYING +24V AND -48V CONDUCTORS. RED MARKINGS SHALL IDENTIFY +24V AND BLUE MARKINGS SHALL IDENTIFY -48V.

- CONTRACTOR SHALL INSPECT THE EXISTING CONDITIONS PRIOR TO SUBMITTING A BID. ANY QUESTIONS ARISING DURING THE BID PERIOD IN REGARDS TO THE CONTRACTOR'S FUNCTIONS, THE SCOPE OF WORK, OR ANY OTHER ISSUE RELATED TO THIS PROJECT SHALL BE BROUGHT UP DURING THE BID PERIOD WITH THE PROJECT MANAGER FOR CLARIFICATION, NOT AFTER THE CONTRACT HAS BEEN AWARDED.
- ALL ELECTRICAL WORK SHALL BE DONE IN ACCORDANCE WITH CURRENT NATIONAL ELECTRICAL CODES AND ALL STATE AND LOCAL CODES, LAWS, AND ORDINANCES. PROVIDE ALL COMPONENTS AND WIRING SIZES AS REQUIRED TO MEET NEC STANDARDS.
- 3. LOCATION OF EQUIPMENT, CONDUIT AND DEVICES SHOWN ON THE DRAWINGS ARE APPROXIMATE AND SHALL BE COORDINATED WITH FIELD CONDITIONS PRIOR TO CONSTRUCTION.
- CONDUIT ROUGH—IN SHALL BE COORDINATED WITH THE MECHANICAL EQUIPMENT TO AVOID LOCATION CONFLICTS.
  VERIFY WITH THE MECHANICAL EQUIPMENT CONTRACTOR AND COMPLY AS REQUIRED.
- 5. CONTRACTOR SHALL PROVIDE ALL BREAKERS, CONDUITS AND CIRCUITS AS REQUIRED FOR A COMPLETE SYSTEM.
- 6. CONTRACTOR SHALL PROVIDE PULL BOXES AND JUNCTION BOXES AS REQUIRED BY THE NEC ARTICLE 314.
- 7. CONTRACTOR SHALL PROVIDE ALL STRAIN RELIEF AND CABLE SUPPORTS FOR ALL CABLE ASSEMBLIES. INSTALLATION SHALL BE IN ACCORDANCE WITH MANUFACTURER'S SPECIFICATIONS AND RECOMMENDATIONS.
- 8. ALL DISCONNECTS AND CONTROLLING DEVICES SHALL BE PROVIDED WITH ENGRAVED PHENOLIC NAMEPLATES INDICATING EQUIPMENT CONTROLLED, BRANCH CIRCUITS INSTALLED ON, AND PANEL FIELD LOCATIONS FED FROM.
- INSTALL AN EQUIPMENT GROUNDING CONDUCTOR IN ALL CONDUITS PER THE SPECIFICATIONS AND NEC 250.
  THE EQUIPMENT GROUNDING CONDUCTORS SHALL BE BONDED AT ALL JUNCTION BOXES, PULL BOXES, AND ALL
  DISCONNECT SWITCHES, AND EQUIPMENT CABINETS.
- 10. ALL NEW MATERIAL SHALL HAVE A U.L. LABEL.
- 11. PANEL SCHEDULE LOADING AND CIRCUIT ARRANGEMENTS REFLECT POST-CONSTRUCTION EQUIPMENT.
- 12. CONTRACTOR SHALL BE RESPONSIBLE FOR AS-BUILT PANEL SCHEDULE AND SITE DRAWINGS.
- 13. FIBER ROUTE IS PRELIMINARY, FINAL FIBER ROUTE TO BE DETERMINED ONCE UCR (UTILITY COORDINATION REPORT) HAS BEEN FINALIZED.

EXISTING UTILITY POLE W/ METERS -PROPOSED FIBER HANDHOLE NEXT TO EXITING UTILITY POLE (6'-0" x 7'-0") SHELTER PROPOSED WEATHER CAP AND 2" SCH 40 PVC UNDERGROUND CONDUIT FOR POWER FROM EXISTING UTILITY POLE TO PROPOSED METER ON PROPOSED DISH PLATFORM (DISH TO INSTALL CONDUIT) (PENDING POWER DESIGN AND UTILITY COORDINATION REPORT)
(LENGTH: ±40'-0") 10'-0" EXISTING 3'-0"¢
FOUNDATION — EXISTING GUYED TOWER PROPOSED 2" SCH 40 PVC CONDUIT FOR FIBER FROM PROPOSED HANDLHOLE TO DISH H-FRAME PENDING POWER DESIGN AND UTILITY COORDINATION REPORT) (LENGTH: 40'-0")

**ELECTRICAL NOTES** 





1"=60

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	RCD		S	S	CJ	w
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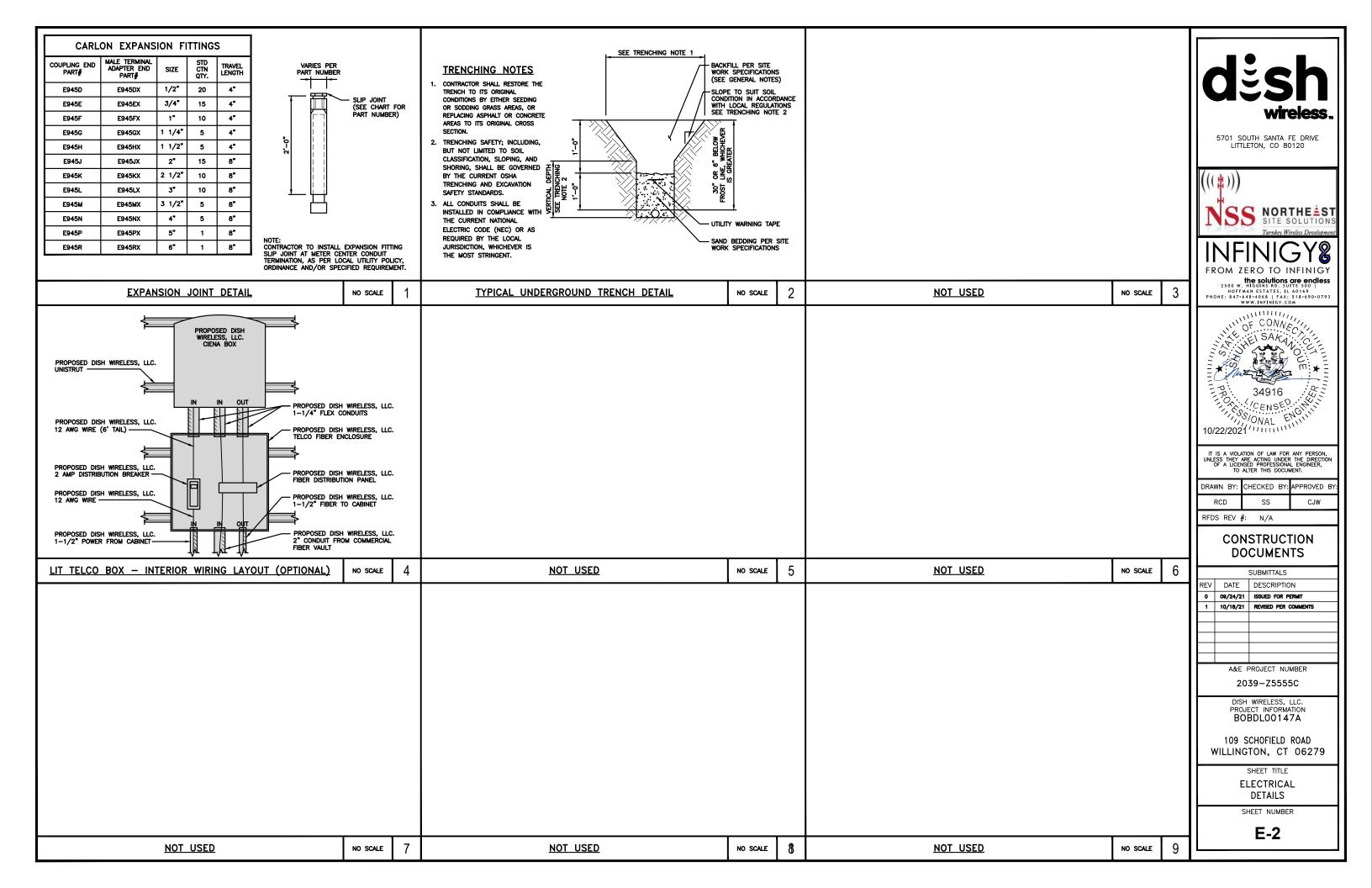
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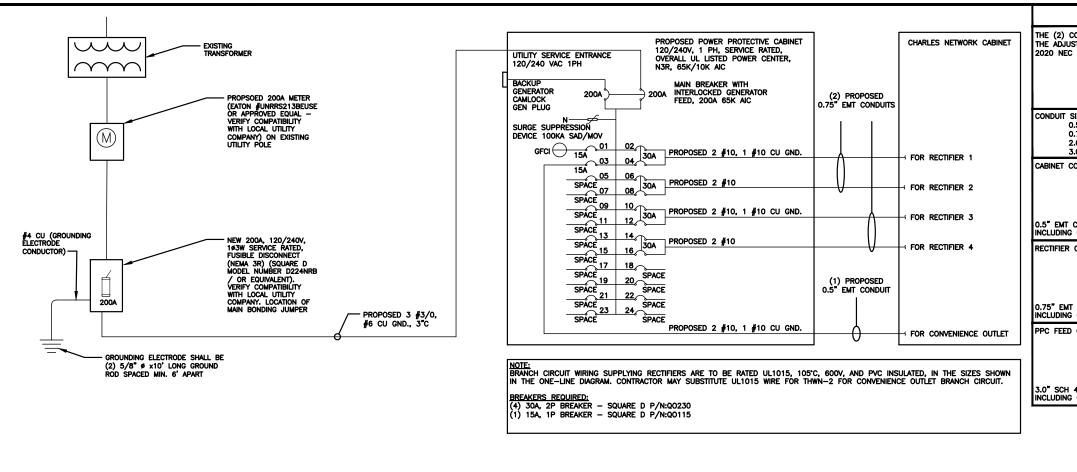
ELECTRICAL/FIBER ROUTE PLAN AND NOTES

SHEET NUMBER

E-1

2"6"0 1' 2' 3' 4' 5' 6' 3/8"=1'-0"





2

NO SCALE

### **NOTES**

THE (2) CONDUITS WITH (4) CURRENT CARRYING CONDUCTORS EACH, SHALL APPLY THE ADJUSTMENT FACTOR OF 80% PER 2014/17 NEC TABLE 310.15(B)(3)(a) OR 2020 NEC TABLE 310.15(C)(1) FOR UL1015 WIRE.

> #12 FOR 15A-20A/1P BREAKER: 0.8 x 30A = 24.0A #10 FOR 25A-30A/2P BREAKER: 0.8 x 40A = 32.0A #8 FOR 35A-40A/2P BREAKER: 0.8 x 55A = 44.0A #8 FOR 35A-40A/2P BREAKER: 0.8 x 55A = 44.0A #6 FOR 45A-60A/2P BREAKER: 0.8 x 75A = 60.0A

CONDUIT SIZING: AT 40% FILL PER NEC CHAPTER 9, TABLE 4, ARTICLE 358. 0.5" CONDUIT - 0.122 SQ. IN AREA 0.75" CONDUIT - 0.213 SQ. IN AREA

2.0" CONDUIT - 1.316 SQ. IN AREA 3.0" CONDUIT - 2.907 SQ. IN AREA

CABINET CONVENIENCE OUTLET CONDUCTORS (1 CONDUIT): USING THWN-2, CU.

#10 - 0.0211 SQ. IN X 2 = 0.0422 SQ. IN #10 - 0.0211 SQ. IN X 1 = 0.0211 SQ. IN <GROUND = 0.0633 SQ. IN

O.5" EMT CONDUIT IS ADEQUATE TO HANDLE THE TOTAL OF (3) WIRES, INCLUDING GROUND WIRE, AS INDICATED ABOVE.

RECTIFIER CONDUCTORS (2 CONDUITS): USING UL1015, CU.

#10 - 0.0266 SQ. IN X 4 = 0.1064 SQ. IN #10 - 0.0082 SQ. IN X 1 = 0.0082 SQ. IN <BARE GROUND TOTAL

= 0.1146 SQ. IN

0.75" EMT CONDUIT IS ADEQUATE TO HANDLE THE TOTAL OF (5) WIRES, INCLUDING GROUND WIRE, AS INDICATED ABOVE.

PPC FEED CONDUCTORS (1 CONDUIT): USING THWN, CU.

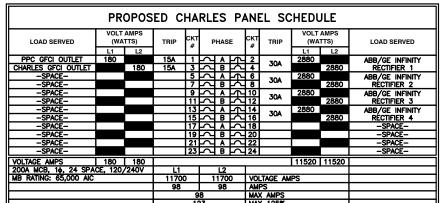
3/0 - 0.2679 SQ. IN X 3 = 0.8037 SQ. IN #6 - 0.0507 SQ. IN X 1 = 0.0507 SQ. IN <GROUND

TOTAL = 0.8544 SQ. IN

3.0" SCH 40 PVC CONDUIT IS ADEQUATE TO HANDLE THE TOTAL OF (4) WIRES, INCLUDING GROUND WIRE, AS INDICATED ABOVE.

PPC ONE-LINE DIAGRAM NO SCALE

NOT USED



PANEL SCHEDULE

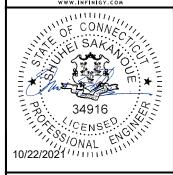


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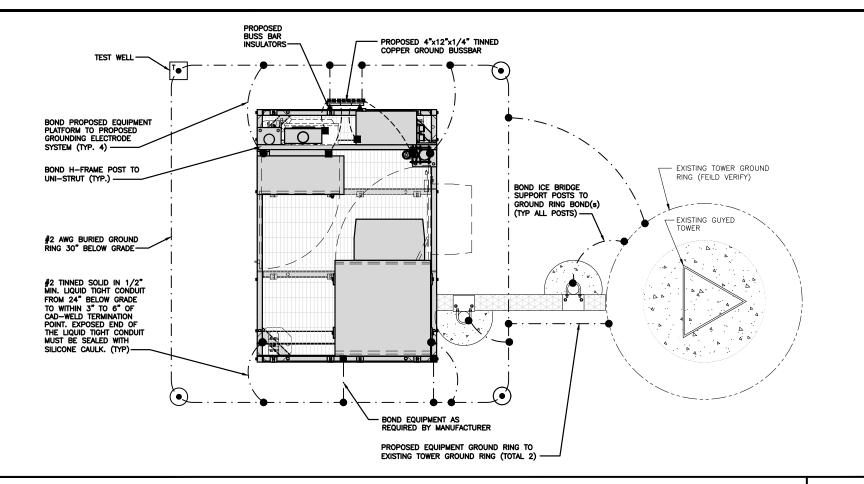
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ELECTRICAL ONE-LINE, FAULT CALCS & PANEL SCHEDULE

SHEET NUMBER

NO SCALE

E-3

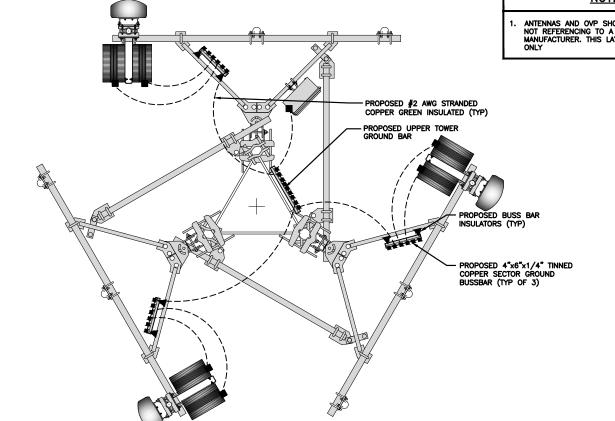


TYPICAL EQUIPMENT GROUNDING PLAN

NO SCALE

### <u>NOTES</u>

ANTENNAS AND OVP SHOWN ARE GENERIC AND NOT REFERENCING TO A SPECIFIC MANUFACTURER. THIS LAYOUT IS FOR REFERENCE ONLY



EXOTHERMIC CONNECTION

GROUND ROD

■ MECHANICAL CONNECTION

TEST GROUND ROD WITH INSPECTION SLEEVE

---- #2 AWG STRANDED & INSULATED

- · - - #2 AWG SOLID COPPER TINNED

GROUND BUS BAR

#### **GROUNDING LEGEND**

- GROUNDING IS SHOWN DIAGRAMMATICALLY ONLY.
- CONTRACTOR SHALL GROUND ALL EQUIPMENT AS A COMPLETE SYSTEM. GROUNDING SHALL BE IN COMPLIANCE WITH NEC SECTION 250 AND DISH WIRELESS, LLC. GROUNDING AND BONDING REQUIREMENTS AND MANUFACTURER'S SPECIFICATIONS.
- 3. ALL GROUND CONDUCTORS SHALL BE COPPER; NO ALUMINUM CONDUCTORS SHALL BE USED.

#### **GROUNDING KEY NOTES**

- (A) EXTERIOR GROUND RING: #2 AWG SOLID COPPER, BURIED AT A DEPTH OF AT LEAST 30 INCHES BELOW GRADE, OR 6 INCHES BELOW THE FROST LINE AND APPROXIMATELY 24 INCHES FROM THE EXTERIOR WALL OR FOOTING.
- B TOWER GROUND RING: THE GROUND RING SYSTEM SHALL BE INSTALLED AROUND AN ANTENNA TOWER'S LEGS, AND/OR GUY ANCHORS. WHERE SEPARATE SYSTEMS HAVE BEEN BROWNER FOR THE FORMAL PROPERTY. AND/OR GUY ANCHORS. WHERE SEPARATE SYSTEMS HAVE BEEN PROVIDED FOR THE TOWER AND THE BUILDING, AT LEAST TWO BONDS SHALL BE MADE BETWEEN THE TOWER RING GROUND SYSTEM AND THE BUILDING RING GROUND SYSTEM USING MINIMUM #2 AWG SOLID COPPER CONDUCTORS.
- © Interior ground ring: #2 awg stranded green insulated copper conductor extended around the perimeter of the equipment area. All non-telecommunications related metallic objects found within a site shall be grounded to the interior ground ring with #6 awg stranded green
- D BOND TO INTERIOR GROUND RING: #2 AWG SOLID TINNED COPPER WIRE PRIMARY BONDS SHALL BE PROVIDED AT LEAST AT FOUR POINTS ON THE INTERIOR GROUND RING, LOCATED AT THE CORNERS OF THE
- (E) GROUND ROD: UL LISTED COPPER CLAD STEEL. MINIMUM 1/2" DIAMETER BY EIGHT FEET LONG. GROUND RODS SHALL BE INSTALLED WITH INSPECTION SLEEVES. GROUND RODS SHALL BE DRIVEN TO THE DEPTH OF GROUND RING CONDUCTOR.
- F CELL REFERENCE GROUND BAR: POINT OF GROUND REFERENCE FOR ALL COMMUNICATIONS EQUIPMENT FRAMES. ALL BONDS ARE MADE WITH #2 AWG UNLESS NOTED OTHERWISE STRANDED GREEN INSULATED COPPER CONDUCTORS. BOND TO GROUND RING WITH (2) #2 SOLID TINNED COPPER CONDUCTORS.
- G HATCH PLATE GROUND BAR: BOND TO THE INTERIOR GROUND RING WITH TWO #2 AWG STRANDED GREEN INSULATED COPPER CONDUCTORS. WHEN A HATCH-PLATE AND A CELL REFERENCE GROUND BAR ARE BOTH PRESENT, THE CRGB MUST BE CONNECTED TO THE HATCH-PLATE AND TO THE INTERIOR GROUND RING USING (2) TWO #2 AWG STRANDED GREEN INSULATED COPPER CONDUCTORS EACH.
- (H) EXTERIOR CABLE ENTRY PORT GROUND BARS; LOCATED AT THE ENTRANCE TO THE CELL SITE BUILDING, BOND TO GROUND RING WITH A #2 AWG SOLID TINNED COPPER CONDUCTORS WITH AN EXOTHERMIC WELD AND INSPECTION SLEEVE.
- J TELCO GROUND BAR: BOND TO BOTH CELL REFERENCE GROUND BAR OR EXTERIOR GROUND RING.
- K FRAME BONDING: THE BONDING POINT FOR TELECOM EQUIPMENT FRAMES SHALL BE THE GROUND BUS THAT IS NOT ISOLATED FROM THE EQUIPMENTS METAL FRAMEWORK.
- INTERIOR UNIT BONDS: METAL FRAMES, CABINETS AND INDIVIDUAL METALLIC UNITS LOCATED WITH THE AREA OF THE INTERIOR GROUND RING REQUIRE A #6 AWG STRANDED GREEN INSULATED COPPER BOND TO THE
- M FENCE AND GATE GROUNDING: METAL FENCES WITHIN 7 FEET OF THE EXTERIOR GROUND RING OR OBJECTS BONDED TO THE EXTERIOR GROUND RING SHALL BE BONDED TO THE GROUND RING WITH A #2 AWG SOLID TINNED COPPER CONDUCTOR AT AN INTERVAL NOT EXCEEDING 25 FEET. BONDS SHALL BE MADE AT EACH
- $\underbrace{ \text{N} \ \ }_{\text{N}} \ \underbrace{ \text{exterior unit bonds: Metallic objects, external to or mounted to the building, shall be bonded to the exterior ground ring. Using $\#2$ tinned solid copper wire }$
- (P) ICE BRIDGE SUPPORTS: EACH ICE BRIDGE LEG SHALL BE BONDED TO THE GROUND RING WITH #2 AWG BARE TINNED COPPER CONDUCTOR. PROVIDE EXOTHERMIC WELDS AT BOTH THE ICE BRIDGE LEG AND BURIED
- Q DURING ALL DC POWER SYSTEM CHANGES INCLUDING DC SYSTEM CHANGE OUTS, RECTIFIER REPLACEMENTS OR ADDITIONS, BREAKER DISTRIBUTION CHANGES, BATTERY ADDITIONS, BATTERY REPLACEMENTS AND INSTALLATIONS OR CHANGES TO DC CONVERTER SYSTEMS IT SHALL BE REQUIRED THAT SERVICE CONTRACTORS VERIFY ALL DC POWER SYSTEMS ARE EQUIPPED WITH A MASTER DC SYSTEM RETURN GROUND CONDUCTOR FROM THE DC POWER SYSTEM COMMON RETURN BUS DIRECTLY CONNECTED TO THE CELL SITE PEFERDENCE CROUND BAR
- (R) TOWER TOP COLLECTOR BUSS BAR IS TO BE MECHANICALLY BONDED TO PROPOSED ANTENNA MOUNT COLLAR. REFER TO DISH WIRELESS, LLC. GROUNDING NOTES.

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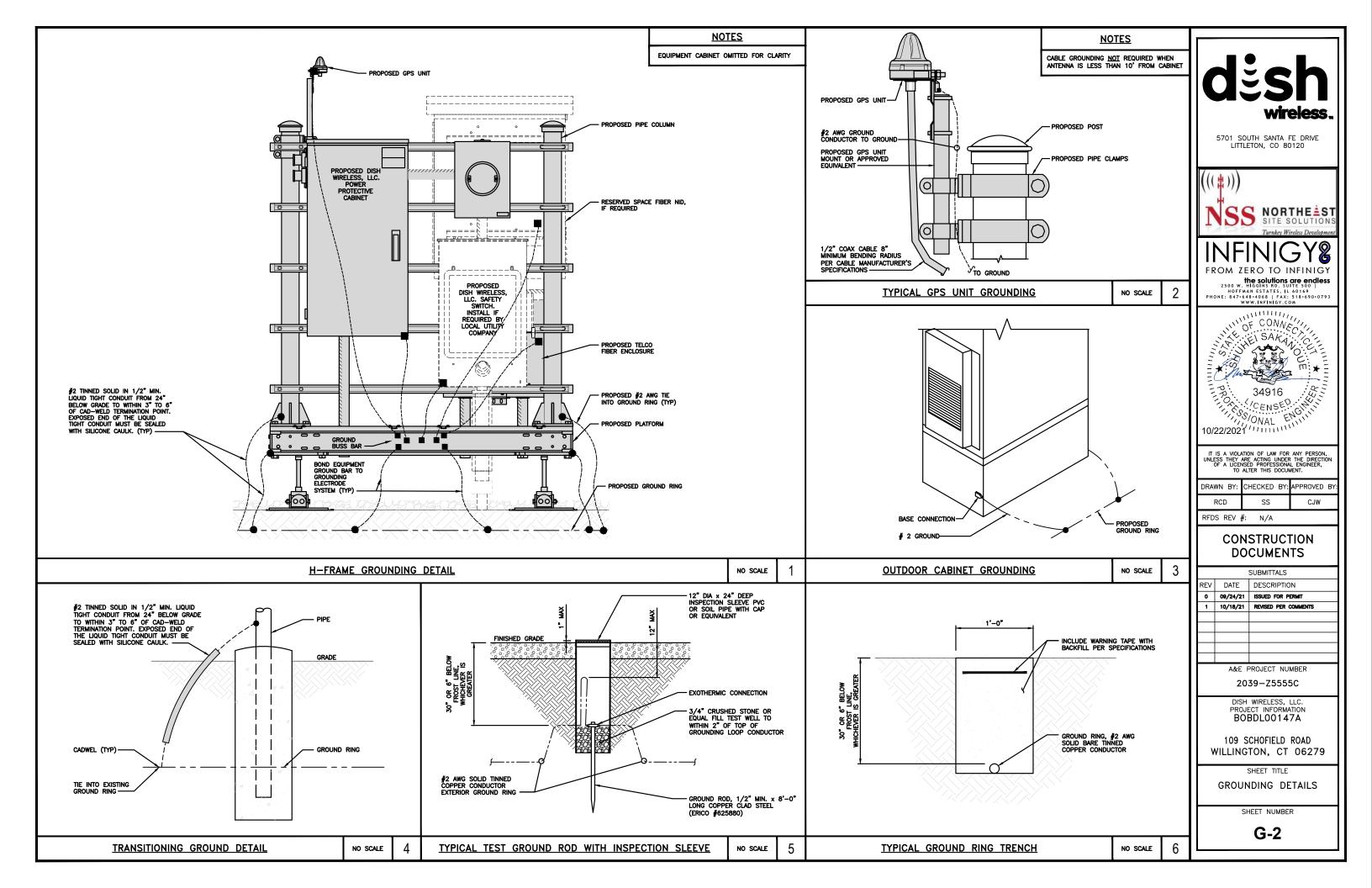
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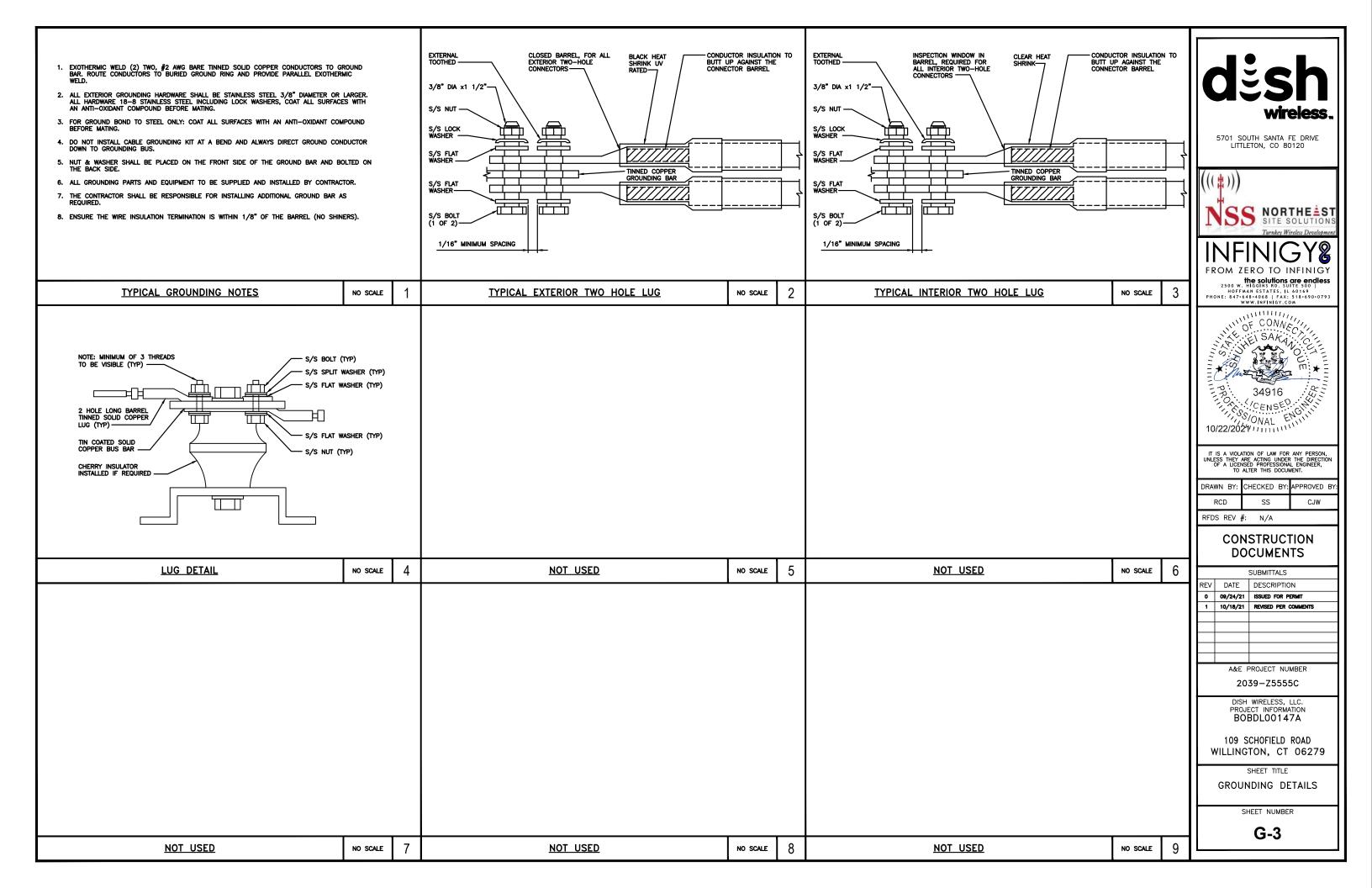
GROUNDING PLANS AND NOTES

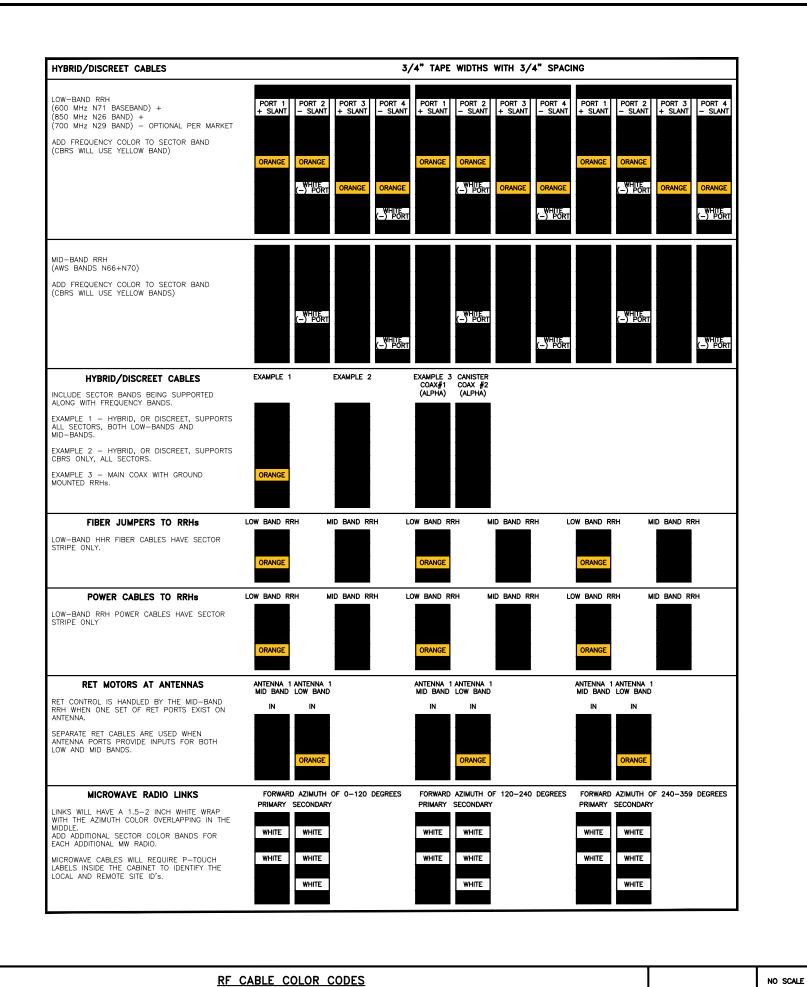
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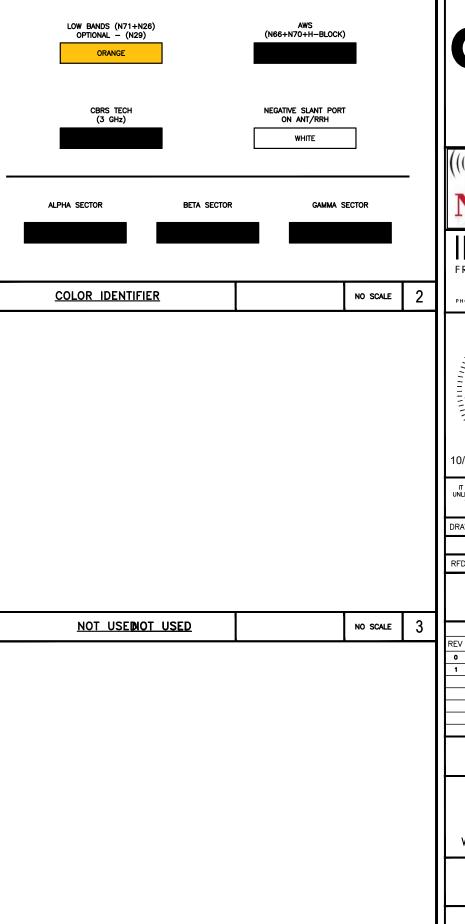
G-1

**GROUNDING KEY NOTES** 









NOT USEINOT USED

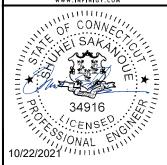
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RCD	SS	CJW

RFDS REV #: N/A

# CONSTRUCTION DOCUMENTS

	SUBMITTALS				
REV	DATE	DESCRIPTION			
0	09/24/21	ISSUED FOR PERMIT			
1	10/18/21	REVISED PER COMMENTS			
	∧ & e E = E	DECT NUMBER			

A&E PROJECT NUMBER

2039-Z5555C

DISH WIRELESS, LLC. PROJECT INFORMATION BOBDLO0147A

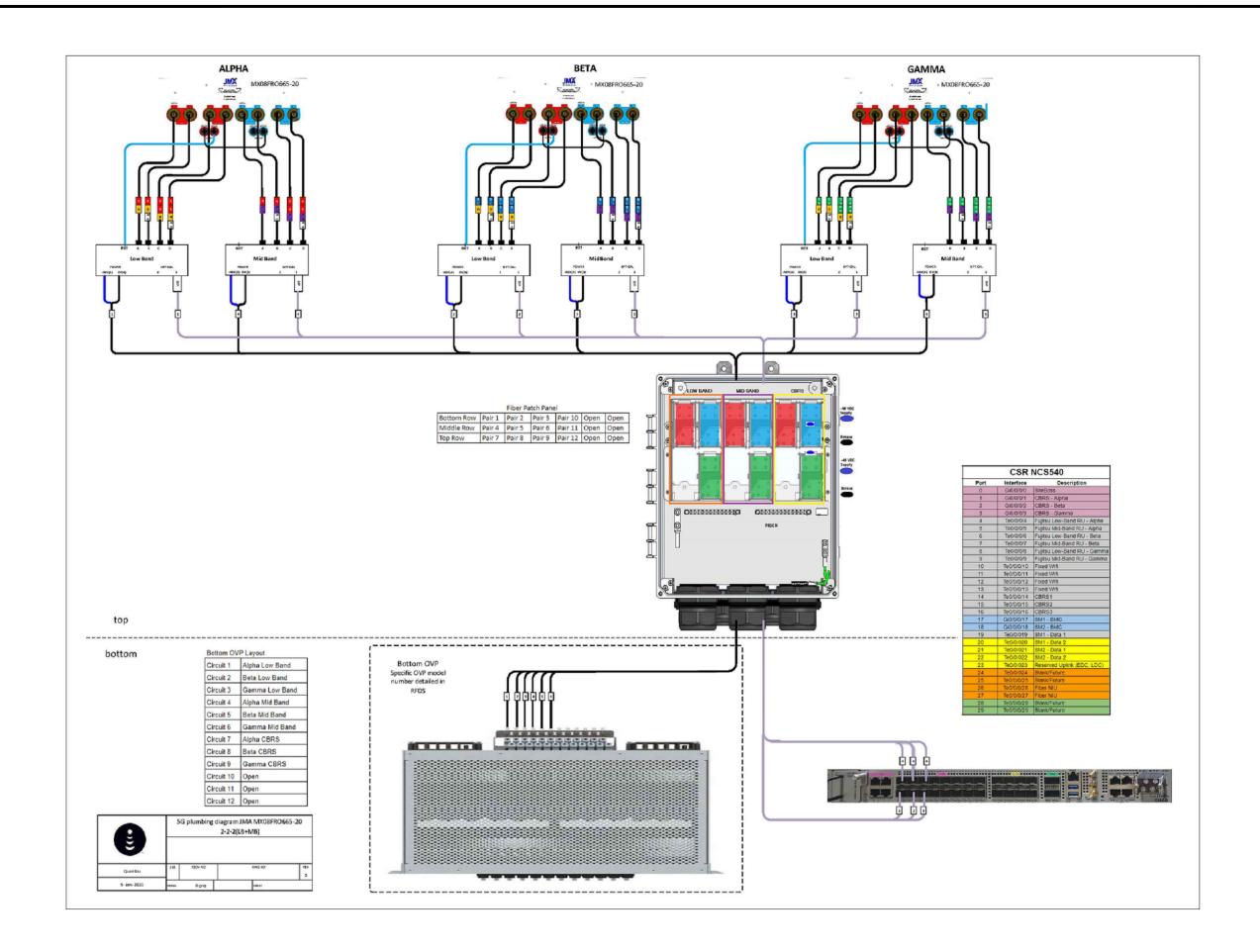
109 SCHOFIELD ROAD WILLINGTON, CT 06279

SHEET TITLE **RF** 

SHEET NUMBER

NO SCALE

RF-1





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RCI	)	SS		CJW	

RFDS REV #: N/A

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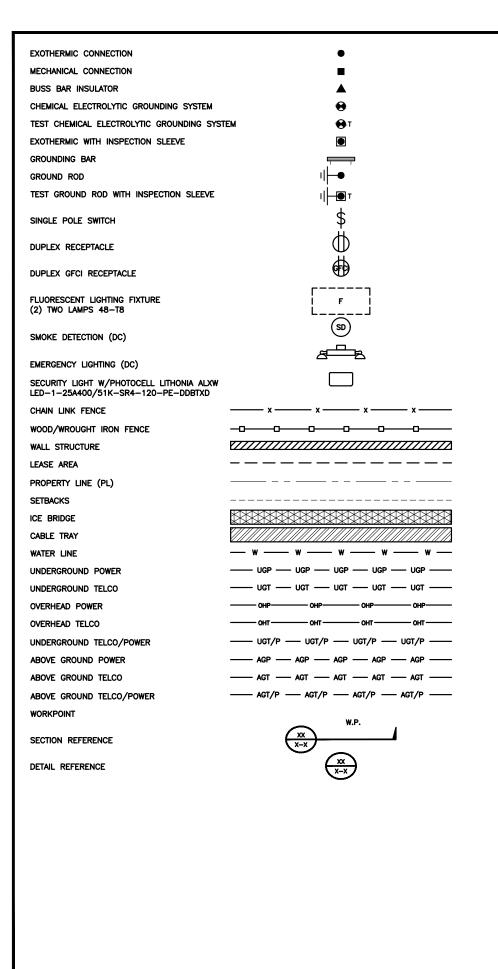
109 SCHOFIELD ROAD WILLINGTON, CT 06279

SHEET TITLE

RF
PLUMBING DIAGRAM

SHEET NUMBER

RF-2



AB	ANCHOR BOLT	IN	INCH
ABV	ABOVE	INT	INTERIOR
AC	ALTERNATING CURRENT	LB(S)	POUND(S)
ADDL	ADDITIONAL		* *
AFF	ABOVE FINISHED FLOOR	LF	LINEAR FEET
		LTE	LONG TERM EVOLUTION
AFG	ABOVE FINISHED GRADE	MAS	MASONRY
AGL	ABOVE GROUND LEVEL	MAX	MAXIMUM
AIC	AMPERAGE INTERRUPTION CAPACITY	MB	MACHINE BOLT
ALUM	ALUMINUM	MECH	MECHANICAL
ALT	ALTERNATE	MFR	MANUFACTURER
ANT	ANTENNA	MGB	MASTER GROUND BAR
APPROX	APPROXIMATE	MIN	MINIMUM
ARCH	ARCHITECTURAL	MISC	MISCELLANEOUS
ATS	AUTOMATIC TRANSFER SWITCH	MTL	METAL
AWG	AMERICAN WIRE GAUGE		
		MTS	MANUAL TRANSFER SWITCH
BATT	BATTERY	MW	MICROWAVE
BLDG	BUILDING	NEC	NATIONAL ELECTRIC CODE
BLK	BLOCK	NM	NEWTON METERS
BLKG	BLOCKING	NO.	NUMBER
BM	BEAM	#	NUMBER
BTC	BARE TINNED COPPER CONDUCTOR	NTS	NOT TO SCALE
BOF	BOTTOM OF FOOTING	oc	ON-CENTER
CAB	CABINET		
CANT	CANTILEVERED	OSHA	OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION
		OPNG	OPENING
CHG	CHARGING	P/C	PRECAST CONCRETE
CLG	CEILING	PCS	PERSONAL COMMUNICATION SERVICES
CLR	CLEAR	PCU	PRIMARY CONTROL UNIT
COL	COLUMN	PRC	PRIMARY RADIO CABINET
COMM	COMMON	PP	POLARIZING PRESERVING
CONC	CONCRETE		
CONSTR	CONSTRUCTION	PSF	POUNDS PER SQUARE FOOT
DBL	DOUBLE	PSI	POUNDS PER SQUARE INCH
DC	DIRECT CURRENT	PT	PRESSURE TREATED
		PWR	POWER CABINET
DEPT	DEPARTMENT	QTY	QUANTITY
DF	DOUGLAS FIR	RAD	RADIUS
DIA	DIAMETER	RECT	RECTIFIER
DIAG	DIAGONAL	REF	REFERENCE
DIM	DIMENSION	REINF	
DWG	DRAWING		REINFORCEMENT
DWL	DOWEL	REQ'D	REQUIRED
EA	EACH	RET	REMOTE ELECTRIC TILT
EC	ELECTRICAL CONDUCTOR	RF	RADIO FREQUENCY
		RMC	RIGID METALLIC CONDUIT
EL.	ELEVATION	RRH	REMOTE RADIO HEAD
ELEC	ELECTRICAL	RRU	REMOTE RADIO UNIT
EMT	ELECTRICAL METALLIC TUBING	RWY	RACEWAY
ENG	ENGINEER		
EQ	EQUAL	SCH	SCHEDULE
EXP	EXPANSION	SHT	SHEET
EXT	EXTERIOR	SIAD	SMART INTEGRATED ACCESS DEVICE
EW	EACH WAY	SIM	SIMILAR
FAB	FABRICATION	SPEC	SPECIFICATION
		SQ	SQUARE
FF FO	FINISH FLOOR	SS	STAINLESS STEEL
FG	FINISH GRADE	STD	STANDARD
FIF	FACILITY INTERFACE FRAME	STL	STEEL
FIN	FINISH(ED)	TEMP	TEMPORARY
FLR	FLOOR	THK	THICKNESS
FDN	FOUNDATION	TMA	TOWER MOUNTED AMPLIFIER
FOC			CONTRACT AND INCIDENT AMERICAN
	FACE OF CONCRETE		
FOM		TN	TOE NAIL
FOM FOS	FACE OF MASONRY	TN TOA	TOE NAIL TOP OF ANTENNA
FOS	FACE OF MASONRY FACE OF STUD	TN	TOE NAIL
FOS FOW	FACE OF MASONRY FACE OF STUD FACE OF WALL	TN TOA	TOE NAIL TOP OF ANTENNA
FOS FOW FS	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE	TN TOA TOC	TOE NAIL TOP OF ANTENNA TOP OF CURB
FOS FOW FS FT	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT	TN TOA TOC TOF TOP	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET)
FOS FOW FS FT FTG	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE	TN TOA TOC TOF TOP TOS	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL
FOS FOW FS FT	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT	TN TOA TOC TOF TOP TOS TOW	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL
FOS FOW FS FT FTG	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING	TN TOA TOC TOF TOP TOS TOW TVSS	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION
FOS FOW FS FT FTG GA	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE	TN TOA TOC TOF TOP TOS TOW TVSS TYP	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL
FOS FOW FS FT FTG GA GEN GFCI	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND
FOS FOW FS FT FTG GA GEN GFCI GLB	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM	TN TOA TOC TOF TOP TOS TOW TVSS TYP	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL
FOS FOW FS FT FTG GA GEN GFCI GLB GLV	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS GND	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM GROUND	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL UNO UMTS	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS GND GSM	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM GROUND GLOBAL SYSTEM FOR MOBILE	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL UNO UMTS UPS	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM UNITERRUPTIBLE POWER SYSTEM (DC POWER PLANT)
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS GND	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM GROUND	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL UNO UMTS UPS VIF	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM UNITERRUPTIBLE POWER SYSTEM (DC POWER PLANT) VERIFIED IN FIELD
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS GND GSM	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM GROUND GLOBAL SYSTEM FOR MOBILE	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL UNO UMTS UPS VIF W	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM UNITERRUPTIBLE POWER SYSTEM (DC POWER PLANT) VERIFIED IN FIELD WIDE
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS GND GSM HDG	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM GROUND GLOBAL SYSTEM FOR MOBILE HOT DIPPED GALVANIZED	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL UNO UMTS UPS VIF	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM UNITERRUPTIBLE POWER SYSTEM (DC POWER PLANT) VERIFIED IN FIELD
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS GND GSM HDG HDR	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM GROUND GLOBAL SYSTEM FOR MOBILE HOT DIPPED GALVANIZED HEADER	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL UNO UMTS UPS VIF W	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM UNITERRUPTIBLE POWER SYSTEM (DC POWER PLANT) VERIFIED IN FIELD WIDE
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS GND GSM HDG HDR HGR HVAC	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM GROUND GLOBAL SYSTEM FOR MOBILE HOT DIPPED GALVANIZED HEADER HANGER HEAT/VENTILATION/AIR CONDITIONING	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL UNO UMTS UPS VIF W	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM UNITERRUPTIBLE POWER SYSTEM (DC POWER PLANT) VERIFIED IN FIELD WIDE WITH
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS GND GSM HDG HDR HGR HVAC HT	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM GROUND GLOBAL SYSTEM FOR MOBILE HOT DIPPED GALVANIZED HEADER HANGER HEAT/VENTILATION/AIR CONDITIONING HEIGHT	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL UNO UMTS UPS VIF W W/ WD	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM UNITERRUPTIBLE POWER SYSTEM (DC POWER PLANT) VERIFIED IN FIELD WIDE WITH WOOD
FOS FOW FS FT FTG GA GEN GFCI GLB GLV GPS GND GSM HDG HDR HGR HVAC	FACE OF MASONRY FACE OF STUD FACE OF WALL FINISH SURFACE FOOT FOOTING GAUGE GENERATOR GROUND FAULT CIRCUIT INTERRUPTER GLUE LAMINATED BEAM GALVANIZED GLOBAL POSITIONING SYSTEM GROUND GLOBAL SYSTEM FOR MOBILE HOT DIPPED GALVANIZED HEADER HANGER HEAT/VENTILATION/AIR CONDITIONING	TN TOA TOC TOF TOP TOS TOW TVSS TYP UG UL UNO UMTS UPS VIF W W/ WD	TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM UNITERRUPTIBLE POWER SYSTEM (DC POWER PLANT) VERIFIED IN FIELD WIDE WITH WOOD WEATHERPROOF



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RFDS REV #: N/A

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A&E PROJECT NUMBER

2039-Z5555C

DISH WIRELESS, LLC. PROJECT INFORMATION BOBDLO0147A

109 SCHOFIELD ROAD WILLINGTON, CT 06279

SHEET TITLE

LEGEND AND ABBREVIATIONS

SHEET NUMBER

GN-1

#### SITE ACTIVITY REQUIREMENTS:

- 1. NOTICE TO PROCEED NO WORK SHALL COMMENCE PRIOR TO CONTRACTOR RECEIVING A WRITTEN NOTICE TO PROCEED (NTP) AND THE ISSUANCE OF A PURCHASE ORDER. PRIOR TO ACCESSING/ENTERING THE SITE YOU MUST CONTACT THE DISH WIRELESS, LLC, AND TOWER OWNER NOC & THE DISH WIRELESS, LLC, AND TOWER OWNER CONSTRUCTION MANAGER.
- 2. "LOOK UP" DISH WIRELESS, LLC. AND TOWER OWNER SAFETY CLIMB REQUIREMENT:

THE INTEGRITY OF THE SAFETY CLIMB AND ALL COMPONENTS OF THE CLIMBING FACILITY SHALL BE CONSIDERED DURING ALL STAGES OF DESIGN, INSTALLATION, AND INSPECTION. TOWER MODIFICATION, MOUNT REINFORCEMENTS, AND/OR EQUIPMENT INSTALLATIONS SHALL NOT COMPROMISE THE INTEGRITY OR FUNCTIONAL USE OF THE SAFETY CLIMB OR ANY COMPONENTS OF THE CLIMBING FACILITY ON THE STRUCTURE. THIS SHALL INCLUDE, BUT NOT BE LIMITED TO: PINCHING OF THE WIRE ROPE, BENDING OF THE WIRE ROPE FROM ITS SUPPORTS, DIRECT CONTACT OR CLOSE PROXIMITY TO THE WIRE ROPE WHICH MAY CAUSE FRICTIONAL WEAR, IMPACT TO THE ANCHORAGE POINTS IN ANY WAY, OR TO IMPEDE/BLOCK ITS INTENDED USE. ANY COMPROMISED SAFETY CLIMB, INCLUDING EXISTING CONDITIONS MUST BE TAGGED OUT AND REPORTED TO YOUR DISH WIRELESS, LLC. AND DISH WIRELESS, LLC. AND TOWER OWNER POC OR CALL THE NOC TO GENERATE A SAFETY CLIMB MAINTENANCE AND CONTRACTOR NOTICE TICKET.

- 3. PRIOR TO THE START OF CONSTRUCTION, ALL REQUIRED JURISDICTIONAL PERMITS SHALL BE OBTAINED. THIS INCLUDES, BUT IS NOT LIMITED TO, BUILDING, ELECTRICAL, MECHANICAL, FIRE, FLOOD ZONE, ENVIRONMENTAL, AND ZONING. AFTER ONSITE ACTIVITIES AND CONSTRUCTION ARE COMPLETED, ALL REQUIRED PERMITS SHALL BE SATISFIED AND CLOSED OUT ACCORDING TO LOCAL JURISDICTIONAL REQUIREMENTS.
- 4. ALL CONSTRUCTION MEANS AND METHODS; INCLUDING BUT NOT LIMITED TO, ERECTION PLANS, RIGGING PLANS, CLIMBING PLANS, AND RESCUE PLANS SHALL BE THE RESPONSIBILITY OF THE GENERAL CONTRACTOR RESPONSIBLE FOR THE EXECUTION OF THE WORK CONTAINED HEREIN, AND SHALL MEET ANSI/ASSE A10.48 (LATEST EDITION); FEDERAL, STATE, AND LOCAL REGULATIONS; AND ANY APPLICABLE INDUSTRY CONSENSUS STANDARDS RELATED TO THE CONSTRUCTION ACTIVITIES BEING PERFORMED. ALL RIGGING PLANS SHALL ADHERE TO ANSI/ASSE A10.48 (LATEST EDITION) AND DISH WIRELESS, LLC. AND TOWER OWNER STANDARDS, INCLUDING THE REQUIRED INVOLVEMENT OF A QUALIFIED ENGINEER FOR CLASS IV CONSTRUCTION, TO CERTIFY THE SUPPORTING STRUCTURE(S) IN ACCORDANCE WITH ANSI/TIA-322 (LATEST EDITION).
- 5. ALL SITE WORK TO COMPLY WITH DISH WIRELESS, LLC. AND TOWER OWNER INSTALLATION STANDARDS FOR CONSTRUCTION ACTIVITIES ON DISH WIRELESS, LLC. AND TOWER OWNER TOWER SITE AND LATEST VERSION OF ANSI/TIA-1019-A-2012 "STANDARD FOR INSTALLATION, ALTERATION, AND MAINTENANCE OF ANTENNA SUPPORTING STRUCTURES AND ANTENNAS."
- 6. IF THE SPECIFIED EQUIPMENT CAN NOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION FOR APPROVAL BY DISH WIRELESS, LLC. AND TOWER OWNER PRIOR TO PROCEEDING WITH ANY SUCH CHANGE OF INSTALLATION.
- 7. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS AND ORDINANCES. CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
- 8. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- 9. THE CONTRACTOR SHALL CONTACT UTILITY LOCATING SERVICES INCLUDING PRIVATE LOCATES SERVICES PRIOR TO THE START OF CONSTRUCTION.
- 10. ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SHALL BE RELOCATED AS DIRECTED BY CONTRACTOR. EXTREME CAUTION SHOULD BE USED BY THE CONTRACTOR WHEN EXCAVATING OR DRILLING PIERS AROUND OR NEAR UTILITIES. CONTRACTOR SHALL PROVIDE SAFETY TRAINING FOR THE WORKING CREW. THIS WILL INCLUDE BUT NOT BE LIMITED TO A) FALL PROTECTION B) CONFINED SPACE C) ELECTRICAL SAFETY D) TRENCHING AND EXCAVATION E) CONSTRUCTION SAFETY PROCEDURES.
- 11. ALL SITE WORK SHALL BE AS INDICATED ON THE STAMPED CONSTRUCTION DRAWINGS AND DISH PROJECT SPECIFICATIONS, LATEST APPROVED REVISION.
- 12. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH AT THE COMPLETION OF THE WORK. IF NECESSARY, RUBBISH, STUMPS, DEBRIS, STICKS, STONES AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.
- 13. ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES, WHICH INTERFERE WITH THE EXECUTION OF THE WORK, SHALL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, SUBJECT TO THE APPROVAL OF DISH WIRELESS, LLC. AND TOWER OWNER, AND/OR LOCAL UTILITIES.
- 14. THE CONTRACTOR SHALL PROVIDE SITE SIGNAGE IN ACCORDANCE WITH THE TECHNICAL SPECIFICATION FOR SITE SIGNAGE REQUIRED BY LOCAL JURISDICTION AND SIGNAGE REQUIRED ON INDIVIDUAL PIECES OF EQUIPMENT, ROOMS, AND SHELTERS.
- 15. THE SITE SHALL BE GRADED TO CAUSE SURFACE WATER TO FLOW AWAY FROM THE CARRIER'S EQUIPMENT AND TOWER AREAS.
- 16. THE SUB GRADE SHALL BE COMPACTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE APPLICATION.
- 17. THE AREAS OF THE OWNERS PROPERTY DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUIPMENT OR DRIVEWAY, SHALL BE GRADED TO A UNIFORM SLOPE, AND STABILIZED TO PREVENT EROSION AS SPECIFIED ON THE CONSTRUCTION DRAWINGS AND/OR PROJECT SPECIFICATIONS.
- 18. CONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES, IF REQUIRED DURING CONSTRUCTION, SHALL BE IN CONFORMANCE WITH THE LOCAL GUIDELINES FOR EROSION AND SEDIMENT CONTROL.
- 19. THE CONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT CONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
- 20. CONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS AND RADIOS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
- 21. CONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION, TRASH AND DEBRIS SHOULD BE REMOVED FROM SITE ON A DAILY BASIS.
- 22. NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OR EMBANKMENT.

#### GENERAL NOTES:

1.FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:

CONTRACTOR:GENERAL CONTRACTOR RESPONSIBLE FOR CONSTRUCTION

CARRIER:DISH WIRELESS, LLC.

TOWER OWNER:TOWER OWNER

- 2. THESE DRAWINGS HAVE BEEN PREPARED USING STANDARDS OF PROFESSIONAL CARE AND COMPLETENESS NORMALLY EXERCISED UNDER SIMILAR CIRCUMSTANCES BY REPUTABLE ENGINEERS IN THIS OR SIMILAR LOCALITIES. IT IS ASSUMED THAT THE WORK DEPICTED WILL BE PERFORMED BY AN EXPERIENCED CONTRACTOR AND/OR WORKPEOPLE WHO HAVE A WORKING KNOWLEDGE OF THE APPLICABLE CODE STANDARDS AND REQUIREMENTS AND OF INDUSTRY ACCEPTED STANDARD GOOD PRACTICE. AS NOT EVERY CONDITION OR ELEMENT IS (OR CAN BE) EXPLICITLY SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL USE INDUSTRY ACCEPTED STANDARD GOOD PRACTICE FOR MISCELLANEOUS WORK NOT EXPLICITLY SHOWN.
- 3. THESE DRAWINGS REPRESENT THE FINISHED STRUCTURE. THEY DO NOT INDICATE THE MEANS OR METHODS OF CONSTRUCTION. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR THE CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES. THE CONTRACTOR SHALL PROVIDE ALL MEASURES NECESSARY FOR PROTECTION OF LIFE AND PROPERTY DURING CONSTRUCTION. SUCH MEASURES SHALL INCLUDE, BUT NOT BE LIMITED TO, BRACING, FORMWORK, SHORING, ETC. SITE VISITS BY THE ENGINEER OR HIS REPRESENTATIVE WILL NOT INCLUDE INSPECTION OF THESE ITEMS AND IS FOR STRUCTURAL OBSERVATION OF THE FINISHED STRUCTURE ONLY.
- 4. NOTES AND DETAILS IN THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE OVER GENERAL NOTES AND TYPICAL DETAILS. WHERE NO DETAILS ARE SHOWN, CONSTRUCTION SHALL CONFORM TO SIMILAR WORK ON THE PROJECT, AND/OR AS PROVIDED FOR IN THE CONTRACT DOCUMENTS. WHERE DISCREPANCIES OCCUR BETWEEN PLANS, DETAILS, GENERAL NOTES, AND SPECIFICATIONS, THE GREATER, MORE STRICT REQUIREMENTS, SHALL GOVERN. IF FURTHER CLARIFICATION IS REQUIRED CONTACT THE ENGINEER OF RECORD.
- 5. SUBSTANTIAL EFFORT HAS BEEN MADE TO PROVIDE ACCURATE DIMENSIONS AND MEASUREMENTS ON THE DRAWINGS TO ASSIST IN THE FABRICATION AND/OR PLACEMENT OF CONSTRUCTION ELEMENTS BUT IT IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO FIELD VERIFY THE DIMENSIONS, MEASUREMENTS, AND/OR CLEARANCES SHOWN IN THE CONSTRUCTION DRAWINGS PRIOR TO FABRICATION OR CUTTING OF ANY NEW OR EXISTING CONSTRUCTION ELEMENTS. IF IT IS DETERMINED THAT THERE ARE DISCREPANCIES AND/OR CONFLICTS WITH THE CONSTRUCTION DRAWINGS THE ENGINEER OF RECORD IS TO BE NOTIFIED AS SOON AS POSSIBLE.
- 6. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING CONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CARRIER POC AND TOWER OWNER.
- 7. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS AND ORDINANCES. CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
- 8. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
- 9. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- 10. IF THE SPECIFIED EQUIPMENT CAN NOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION FOR APPROVAL BY THE CARRIER AND TOWER OWNER PRIOR TO PROCEEDING WITH ANY SUCH CHANGE OF INSTALLATION
- 11. CONTRACTOR IS TO PERFORM A SITE INVESTIGATION, BEFORE SUBMITTING BIDS, TO DETERMINE THE BEST ROUTING OF ALL CONDUITS FOR POWER, AND TELCO AND FOR GROUNDING CABLES AS SHOWN IN THE POWER, TELCO, AND GROUNDING PLAN DRAWINGS.
- 12. THE CONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT CONTRACTOR'S EXPENSE TO THE SATISFACTION OF DISH WIRELESS, LLC. AND TOWER OWNER
- 13. CONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
- 14. CONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION. TRASH AND DEBRIS SHOULD BE REMOVED FROM SITE ON A DAILY BASIS.



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DRAWN	BY:	CHECKED	BY:	APPROVED	BY:
RCE	)	SS		CJW	

RFDS REV #: N/A

# CONSTRUCTION DOCUMENTS

	SUBMITTALS				
REV	DATE	DESCRIPTION			
0	09/24/21	ISSUED FOR PERMIT			
1	10/18/21	REVISED PER COMMENTS			
	A&E F	PROJECT NUMBER			

A&E PROJECT NUMBER

2039-Z5555C

DISH WIRELESS, LLC.
PROJECT INFORMATION
BOBDL00147A

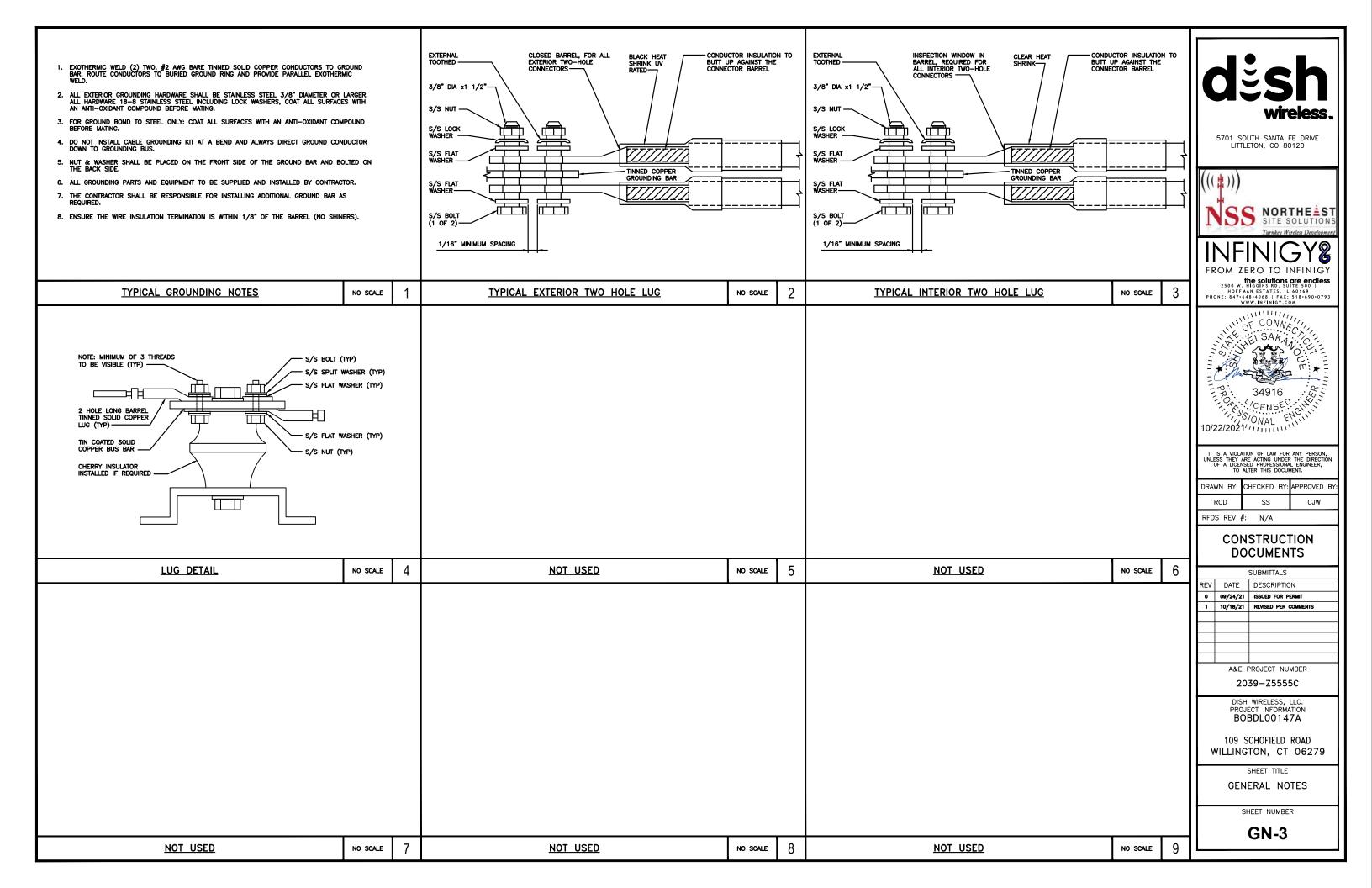
109 SCHOFIELD ROAD WILLINGTON, CT 06279

SHEET TITLE

GENERAL NOTES

SHEET NUMBER

GN-2



#### **GROUNDING NOTES:**

- 1. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION AND AC POWER GES'S) SHALL BE BONDED TOGETHER AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
- 2. THE CONTRACTOR SHALL PERFORM IEEE FALL—OF—POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR GROUND ELECTRODE SYSTEMS, THE CONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
- 3. THE CONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENCING GROUNDING AND UNDERGROUND CONDUIT INSTALLATION AS TO PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO THE CONDUIT AND PROVIDE TESTING RESULTS.
- 4. METAL CONDUIT AND TRAY SHALL BE GROUNDED AND MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH #6 COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
- 5. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.
- 6. EACH CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, #6 STRANDED COPPER OR LARGER FOR INDOOR BTS; #2 BARE SOLID TINNED COPPER FOR OUTDOOR BTS.
- 7. CONNECTIONS TO THE GROUND BUS SHALL NOT BE DOUBLED UP OR STACKED BACK TO BACK CONNECTIONS ON OPPOSITE SIDE OF THE GROUND BUS ARE PERMITTED.
- 8. ALL EXTERIOR GROUND CONDUCTORS BETWEEN EQUIPMENT/GROUND BARS AND THE GROUND RING SHALL BE #2 SOLID TINNED COPPER UNLESS OTHERWISE INDICATED.
- 9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
- 10. USE OF 90° BENDS IN THE PROTECTION GROUNDING CONDUCTORS SHALL BE AVOIDED WHEN 45° BENDS CAN BE ADEQUATELY SUPPORTED.
- 11. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
- 12. ALL GROUND CONNECTIONS ABOVE GRADE (INTERIOR AND EXTERIOR) SHALL BE FORMED USING HIGH PRESS CRIMPS.
- 13. COMPRESSION GROUND CONNECTIONS MAY BE REPLACED BY EXOTHERMIC WELD CONNECTIONS.
- 14. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR
- 15. APPROVED ANTIOXIDANT COATINGS (i.e. CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
- 16. ALL EXTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERIAL.
- 17. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
- 18. BOND ALL METALLIC OBJECTS WITHIN 6 ft OF MAIN GROUND RING WITH (1) #2 BARE SOLID TINNED COPPER GROUND CONDUCTOR.
- 19. GROUND CONDUCTORS USED FOR THE FACILITY GROUNDING AND LIGHTNING PROTECTION SYSTEMS SHALL NOT BE ROUTED THROUGH METALLIC OBJECTS THAT FORM A RING AROUND THE CONDUCTOR, SUCH AS METALLIC CONDUITS, METAL SUPPORT CLIPS OR SLEEVES THROUGH WALLS OR FLOORS. WHEN IT IS REQUIRED TO BE HOUSED IN CONDUIT TO MEET CODE REQUIREMENTS OR LOCAL CONDITIONS, NON-METALLIC MATERIAL SUCH AS PVC CONDUIT SHALL BE USED. WHERE USE OF METAL CONDUIT IS UNAVOIDABLE (i.e., NONMETALLIC CONDUIT PROHIBITED BY LOCAL CODE) THE GROUND CONDUCTOR SHALL BE BONDED TO EACH END OF THE METAL CONDUIT.
- 20. ALL GROUNDS THAT TRANSITION FROM BELOW GRADE TO ABOVE GRADE MUST BE #2 BARE SOLID TINNED COPPER IN 3/4" NON-METALLIC, FLEXIBLE CONDUIT FROM 24" BELOW GRADE TO WITHIN 3" TO 6" OF CAD-WELD TERMINATION POINT. THE EXPOSED END OF THE CONDUIT MUST BE SEALED WITH SILICONE CAULK. (ADD TRANSITIONING GROUND STANDARD DETAIL AS WELL).
- 21. BUILDINGS WHERE THE MAIN GROUNDING CONDUCTORS ARE REQUIRED TO BE ROUTED TO GRADE, THE CONTRACTOR SHALL ROUTE TWO GROUNDING CONDUCTORS FROM THE ROOFTOP, TOWERS, AND WATER TOWERS GROUNDING RING, TO THE EXISTING GROUNDING SYSTEM, THE GROUNDING CONDUCTORS SHALL NOT BE SMALLER THAN 2/O COPPER. ROOFTOP GROUNDING RING SHALL BE BONDED TO THE EXISTING GROUNDING SYSTEM, THE BUILDING STEEL COLUMNS, LIGHTNING PROTECTION SYSTEM, AND BUILDING MAIN WATER LINE (FERROUS OR NONFERROUS METAL PIPING ONLY). DO NOT ATTACH GROUNDING TO FIRE SPRINKLER SYSTEM PIPES.



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DRAWN BY:	CHECKED	ы:	APPROVED	В1:
RCD	SS		CJW	

RFDS REV #: N/A

# CONSTRUCTION DOCUMENTS

	SUBMITTALS				
REV	DATE	DESCRIPTION			
0	09/24/21	ISSUED FOR PERMIT			
1	10/18/21	REVISED PER COMMENTS			
	∧ &c = 1	DECT NUMBER			

A&E PROJECT NUMBER

2039-Z5555C

DISH WIRELESS, LLC. PROJECT INFORMATION BOBDL00147A

109 SCHOFIELD ROAD WILLINGTON, CT 06279

SHEET TITLE

GENERAL NOTES

SHEET NUMBER

GN-4

# Exhibit D

# **Structural Analysis Report**



### **Structural Analysis Report**

### April 21, 2021

Tarpon Site Name:	Willington
Tarpon Site ID:	CT1010
Dish Network Site ID:	BOHVN00147A
Airosmith Project ID:	Tarpon ENG 2020
	109 Schofield Road
Site Location	Willington, CT 06279
	Tolland County
Applicable Code	2018 CT State Building Code / 2015 IBC
Applicable Design Standard	ANSI/TIA-222-H
Structure	149' Guyed Tower
Demand-Capacity Ratio (CSR)	36.2%
Overall Result	Pass

### PREPARED FOR:





APPROVED BY: Joseph R. Johnston, P.E. CT License #: PEN.0029460





### Table of Contents

1.0 Scope	2
2.0 Supporting Documentation	
3.0 Analysis Code Requirements	
4.0 Existing & Reserved Loading	
5.0 To Be Removed Loading	
6.0 Proposed Loading	
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8.0 Results and Conclusions	3
9.0 Assumptions & Limitations	5



### 1.0 Scope

Airosmith Engineering has been requested to perform a structural analysis on the existing 149 ft Guyed Tower for Dish Network's proposed install. The structure was analyzed using tnxTower Version 8.0.7 analysis software. Selected output from the analysis is included in this report.

The proposed Dish Network install consists of installing (1) new platform mount, (3) new panel antennas, (6) new radio units, (1) new surge suppressor, and (1) new hybrid line.

### 2.0 Supporting Documentation

Collocation Application	Dish Network App, dated 3/8/2021
Tower Design Drawings	Sabre Job #35784, dated 10/19/2010
Foundation Design Drawings	Sabre Job #35784, dated 10/28/2010
Geotechnical Report	Welti Geotechnical, dated 9/24/2018

### 3.0 Analysis Code Requirements

Wind Speed	125 mph (3-Second Gust)
Wind Speed with Ice	50 mph (3-Second Gust) w/ 1.5" ice
Design Standard	ANSI/TIA-222-H
Adopted IBC	2018 CT State Building Code / 2015 IBC
Risk Category	
Exposure Category	В
Topographic Factor Procedure	Method 1, Category 1
Crest Height	0 ft.
HSML (ft.)	785.0 ft.



4.0 Existing & Reserved Loading

RAD					
Center	Qty.	Appurtenance	Mount Type	Lines	Carrier
(ft.)					
No loading considered to be removed					

5.0 To Be Removed Loading

RAD Center (ft.)	Qty.	Appurtenance	Mount Type	Lines	Carrier
No loading considered to be removed					

6.0 Proposed Loading

RAD					
Center	Qty.	Appurtenance*	Mount Type	Lines	Carrier
(ft.)					
	3	JMA Wireless MX08FRO665 -20_V0F			
145.0	3	Fujitsu TA08025-B604	Platform w/	(1) 1.65"	Dish
145.0	3	Fujitsu TA08025-B605	Handrails	Hybrid	Network
	1	Generic Junction Box			

<sup>\*</sup>The results of this analysis considers Dish Networks full 11,000 in<sup>2</sup> MLA loading

7.0 Final Configuration

	, to this combandion				
RAD					
Center	Qty.	Appurtenance*	Mount Type	Lines	Carrier
(ft.)					
	3	JMA Wireless MX08FRO665 -20_V0F			
145.0	3	Fujitsu TA08025-B604	Platform w/	(1) 1.65"	Dish
145.0	3	Fujitsu TA08025-B605	Handrails	Hybrid	Network
	1	Generic Junction Box			

<sup>\*</sup>The results of this analysis considers Dish Networks full 11,000 in<sup>2</sup> MLA loading

Coax lines can be installed on any tower face.



### 8.0 Results and Conclusions

Upon reviewing the results of this analysis, it is our opinion that the existing structure meets the specified code requirements. The 149' guyed tower structure and foundation are considered acceptable to support the final loading configuration as listed within in this report. The controlling structure and foundation usages are displayed in the tables below:

### Structure Usages

Component	Controlling Usage*
Legs	29.7%
Diagonals	28.7%
Guy Wires	36.2%

<sup>\*</sup>Listed usage is for the controlling component. Refer to the appendix for detailed results on each individual member

### Foundation Usages

Component	Design Reaction	Analysis Reaction	Usage
Base Axial (kips)	182.5	54.2	29.7%
Anchor Uplift (kips)	36.4	12.5	34.3%
Anchor Shear (kips)	34.2	11.2	32.8%

The tower foundation is acceptable in comparison to original design reactions.

We appreciate the opportunity to be of service on this project. If you have any questions, require additional information, or actual conditions differ from those as detailed in this report, please contact me via the information below:

Brad Davenport, P.E. engineering@airosmithdevelopment.com



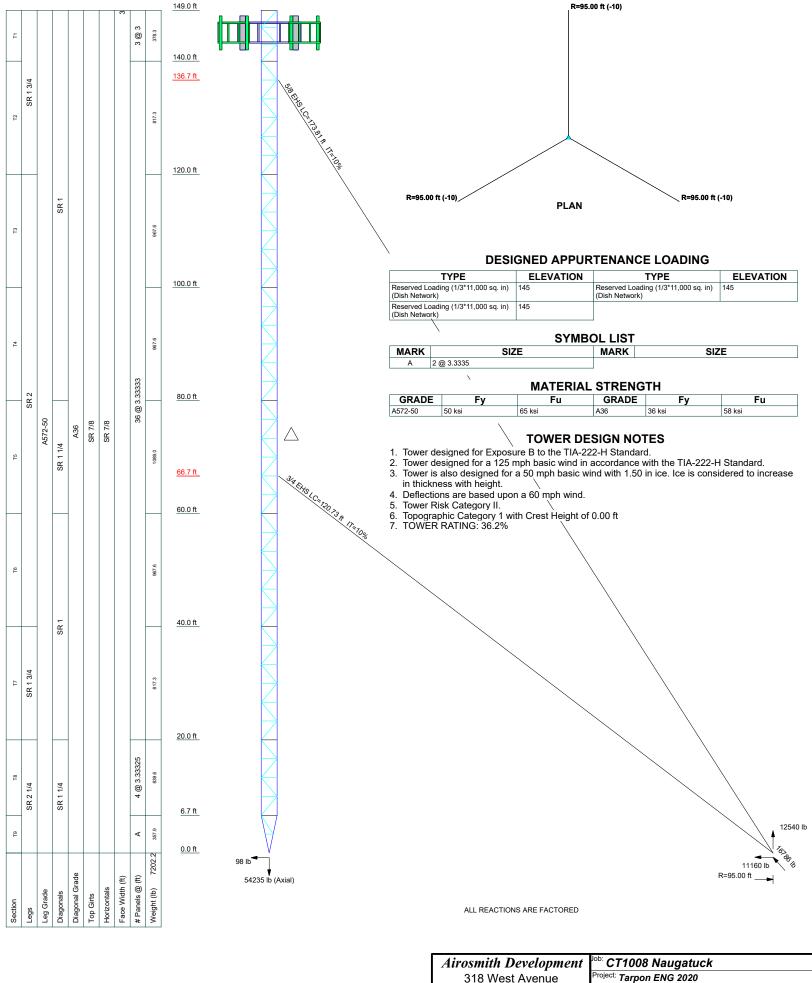
### 9.0 Assumptions & Limitations

The following assumptions have been made for this analysis:

- Structural calculations are completed assuming all information provided to Airosmith Development is accurate and applicable to this site.
- The existing structures were designed, manufactured, and constructed in accordance with the applicable codes and standards in effect at that time
- The existing structures have been properly maintained in accordance with industry standards.
- All structural and foundation elements, unless otherwise noted, are in good condition, and are capable of supporting their original design capacity.
- Steel grades have been assumed as follows, unless otherwise noted

Channel, Solid Round, Angle & Plate
 HSS (Rectangular)
 HSS (Pipe)
 Threaded Rods
 ASTM A36 Gr. 36
 ASTM A53 Gr. B
 ASTM A36 Gr. 36

• Calculation-specific assumptions are as noted in the attached appendix



Airosmith Development	Job: CT1008 Naugatuck	
318 West Avenue	Project: Tarpon ENG 2020	
Saratoga Springs, NY 12866	Client: Tarpon Towers Drawn by: BDavenport	App'd:
Phone: (518) 307-8700	Code: TIA-222-H Date: 04/21/21	Scale: NTS
	Path: C:\Users\bdavenport\Desktop\CT1010 Willington.eri	Dwg No. E-

4 6	
thv	Tower

### Airosmith Development

318 West Avenue Saratoga Springs, NY 12866 Phone: (518) 307-8700 FAX:

Job		Page
	CT1008 Naugatuck	1 of 17
Project		Date
	Tarpon ENG 2020	15:41:38 04/21/21
Client	Tarpon Towers	Designed by BDavenport

### **Tower Input Data**

The main tower is a 3x guyed tower with an overall height of 149.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 3.00 ft at the top and tapered at the base.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower base elevation above sea level: 785.00 ft.

Basic wind speed of 125 mph.

Risk Category II.

Exposure Category B.

Simplified Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Category: 1.

Crest Height: 0.00 ft.

Nominal ice thickness of 1.5000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

Pressures are calculated at each section.

Safety factor used in guy design is 1.

Tower analysis based on target reliabilities in accordance with Annex S.

Load Modification Factors used:  $K_{es}(F_w) = 0.95$ ,  $K_{es}(t_i) = 0.85$ .

Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

### **Options**

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- √ Use Code Stress Ratios
- √ Use Code Safety Factors Guys Escalate Ice Always Use Max Kz

Use Special Wind Profile

- √ Include Bolts In Member Capacity Leg Bolts Are At Top Of Section
- √ Secondary Horizontal Braces Leg
   Use Diamond Inner Bracing (4 Sided)
   SR Members Have Cut Ends
   SR Members Are Concentric

- Distribute Leg Loads As Uniform Assume Legs Pinned
- √ Assume Rigid Index Plate
- √ Use Clear Spans For Wind Area
- √ Use Clear Spans For KL/r
- √ Retension Guys To Initial Tension Bypass Mast Stability Checks
- √ Use Azimuth Dish Coefficients
- √ Project Wind Area of Appurt.
- ✓ Autocalc Torque Arm Areas Add IBC .6D+W Combination
- √ Sort Capacity Reports By Component
- √ Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

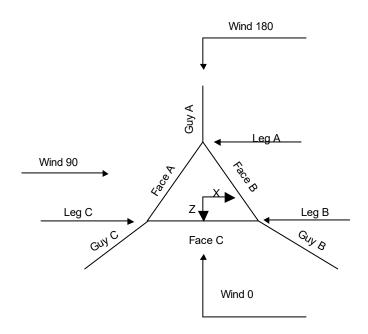
- Use ASCE 10 X-Brace Ly Rules
- √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation
- √ Consider Feed Line Torque
- ✓ Include Angle Block Shear Check
   Use TIA-222-H Bracing Resist. Exemption
   Use TIA-222-H Tension Splice Exemption
   Poles
- √ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

4	7
tnvi	'ower
	UIVE

Airosmith Development 318 West Avenue

318 West Avenue Saratoga Springs, NY 12866 Phone: (518) 307-8700 FAX:

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	CT1008 Naugatuck	2 of 17
Project		Date
	Tarpon ENG 2020	15:41:38 04/21/21
Client	Tarpon Towers	Designed by BDavenport



**Corner & Starmount Guyed Tower** 

	Tower Section Geometry						
-	Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of	Section Length
	section	Lievation	Database		,, iain	Sections	Lengin
		ft			ft		ft
	T1	149.00-140.00			3.00	1	9.00
	T2	140.00-120.00			3.00	1	20.00
	Т3	120.00-100.00			3.00	1	20.00
	T4	100.00-80.00			3.00	1	20.00
	T5	80.00-60.00			3.00	1	20.00
	Т6	60.00-40.00			3.00	1	20.00
	T7	40.00-20.00			3.00	1	20.00
	T8	20.00-6.67			3.00	1	13.33
	Т9	6.67-0.00			3.00	1	6.67

	Tower Section Geometry (cont a)						
Tower	Tower	Diagonal	Bracing	Has	Has	Top Girt	Bottom Girt
Section	Elevation	Spacing	Туре	K Brace End	Horizontals	Offset	Offset
	ft	ft		Panels		in	in
T1	149.00-140.00	3.00	K Brace Left	No	Yes	0.0000	0.0000

tnx7	<i>ower</i>

### Airosmith Development 318 West Avenue

318 West Avenue Saratoga Springs, NY 12866 Phone: (518) 307-8700 FAX:

Job		Page
	CT1008 Naugatuck	3 of 17
Project		Date
	Tarpon ENG 2020	15:41:38 04/21/21
Client	Tarpon Towers	Designed by BDavenport

Tower	Tower	Diagonal	Bracing	Has	Has	Top Girt	Bottom Girt
Section	Elevation	Spacing	Туре	K Brace	Horizontals	Offset	Offset
				End			
	ft	ft		Panels		in	in
T2	140.00-120.00	3.33	K Brace Left	No	Yes	0.0000	0.0000
T3	120.00-100.00	3.33	K Brace Left	No	Yes	0.0000	0.0000
T4	100.00-80.00	3.33	K Brace Left	No	Yes	0.0000	0.0000
T5	80.00-60.00	3.33	K Brace Left	No	Yes	0.0000	0.0000
T6	60.00-40.00	3.33	K Brace Left	No	Yes	0.0000	0.0000
T7	40.00-20.00	3.33	K Brace Left	No	Yes	0.0000	0.0000
T8	20.00-6.67	3.33	K Brace Left	No	Yes	0.0000	0.0000
Т9	6.67-0.00	3.33	K Brace Left	No	Yes	0.0000	0.0000

# **Tower Section Geometry** (cont'd)

Tower	Leg	Leg	Leg	Diagonal	Diagonal	Diagonal
Elevation	Туре	Size	Grade	Туре	Size	Grade
ft						
T1 149.00-140.00	Solid Round	1 3/4	A572-50	Solid Round	1	A36
			(50 ksi)			(36 ksi)
T2 140.00-120.00	Solid Round	1 3/4	A572-50	Solid Round	1	A36
			(50 ksi)			(36 ksi)
T3 120.00-100.00	Solid Round	2	A572-50	Solid Round	1	A36
			(50 ksi)			(36 ksi)
T4 100.00-80.00	Solid Round	2	A572-50	Solid Round	1	A36
			(50 ksi)			(36 ksi)
T5 80.00-60.00	Solid Round	2	A572-50	Solid Round	1 1/4	A36
			(50 ksi)			(36 ksi)
T6 60.00-40.00	Solid Round	2	A572-50	Solid Round	1	A36
			(50 ksi)			(36 ksi)
T7 40.00-20.00	Solid Round	1 3/4	A572-50	Solid Round	1	A36
			(50 ksi)			(36 ksi)
T8 20.00-6.67	Solid Round	2 1/4	A572-50	Solid Round	1 1/4	A36
			(50 ksi)			(36 ksi)
T9 6.67-0.00	Solid Round	2 1/4	A572-50	Solid Round	1 1/4	A36
			(50 ksi)			(36 ksi)

# **Tower Section Geometry** (cont'd)

Tower	Top Girt	Top Girt	Top Girt	Bottom Girt	Bottom Girt	Bottom Girt
Elevation ft	Туре	Size	Grade	Туре	Size	Grade
T1 149.00-140.00	Solid Round	7/8	A36	Flat Bar		A36
			(36 ksi)			(36 ksi)
T2 140.00-120.00	Solid Round	7/8	A36	Flat Bar		A36
			(36 ksi)			(36 ksi)
T3 120.00-100.00	Solid Round	7/8	A36	Flat Bar		A36
			(36 ksi)			(36 ksi)
T4 100.00-80.00	Solid Round	7/8	A36	Flat Bar		A36
			(36 ksi)			(36 ksi)
T5 80.00-60.00	Solid Round	7/8	A36	Flat Bar		A36
			(36 ksi)			(36 ksi)
T6 60.00-40.00	Solid Round	7/8	A36	Flat Bar		A36
			(36 ksi)			(36 ksi)
T7 40.00-20.00	Solid Round	7/8	A36	Flat Bar		A36
			(36 ksi)			(36 ksi)

tnx <sub>T</sub>	<i>ower</i>

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Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T8 20.00-6.67	Solid Round	7/8	A36	Flat Bar		A36
			(36 ksi)			(36 ksi)
T9 6.67-0.00	Solid Round	7/8	A36	Flat Bar		A36
			(36 ksi)			(36 ksi)

# **Tower Section Geometry** (cont'd)

Tower	No.	Mid Girt	Mid Girt	Mid Girt	Horizontal	Horizontal	Horizontal
Elevation	of	Туре	Size	Grade	Туре	Size	Grade
	Mid						
ft	Girts						
Γ1 149.00-140.00	None	Flat Bar		A36	Solid Round	7/8	A36
				(36 ksi)			(36 ksi)
Γ2 140.00-120.00	None	Flat Bar		A36	Solid Round	7/8	A36
				(36 ksi)			(36 ksi)
Γ3 120.00-100.00	None	Flat Bar		A36	Solid Round	7/8	A36
				(36 ksi)			(36 ksi)
T4 100.00-80.00	None	Flat Bar		A36	Solid Round	7/8	A36
				(36 ksi)			(36 ksi)
T5 80.00-60.00	None	Flat Bar		A36	Solid Round	7/8	A36
				(36 ksi)			(36 ksi)
T6 60.00-40.00	None	Flat Bar		A36	Solid Round	7/8	A36
				(36 ksi)			(36 ksi)
T7 40.00-20.00	None	Flat Bar		A36	Solid Round	7/8	A36
				(36 ksi)			(36 ksi)
T8 20.00-6.67	None	Flat Bar		A36	Solid Round	7/8	A36
				(36 ksi)			(36 ksi)
T9 6.67-0.00	None	Flat Bar		A36	Solid Round	7/8	A36
				(36 ksi)			(36 ksi)

### **Tower Section Geometry** (cont'd)

Tower	Gusset	Gusset	Gusset Grade	Adjust. Factor	Adjust.	Weight Mult.	Double Angle	0	0
Elevation	Area	Thickness		$A_f$	Factor		Stitch Bolt	Stitch Bolt	Stitch Bolt
	(per face)				$A_r$		Spacing	Spacing	Spacing
							Diagonals	Horizontals	Redundants
ft	ft <sup>2</sup>	in					in	in	in
T1	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
149.00-140.00			(36 ksi)						
T2	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
140.00-120.00			(36 ksi)						
T3	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
120.00-100.00			(36 ksi)						
T4	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
100.00-80.00			(36 ksi)						
T5 80.00-60.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						
T6 60.00-40.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						
T7 40.00-20.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						

tnx <sub>T</sub>	<i>ower</i>

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Tower	Gusset	Gusset	Gusset Grade	Adjust. Factor	Adjust.	Weight Mult.	Double Angle	Double Angle	Double Angle
Elevation	Area	Thickness		$A_f$	Factor		Stitch Bolt	Stitch Bolt	Stitch Bolt
	(per face)				$A_r$		Spacing	Spacing	Spacing
							Diagonals	Horizontals	Redundants
ft	ft <sup>2</sup>	in					in	in	in
T8 20.00-6.67	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						
T9 6.67-0.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						

# Tower Section Geometry (cont'd)

		_				K Fa	ctors <sup>1</sup>			
Tower Elevation	Calc K	Calc K	Legs	X Brace	K Brace	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
	Single	Solid		Diags X	Diags X	X	X	X	V	X
ft	Angles	Rounds		A V	A V	X Y	X Y	X Y	X $Y$	Y
T1	No	Yes	1	1	1	1	1	1	1	1
149.00-140.00	110	1 03	1	1	1	1	1	1	1	1
T2	No	Yes	1	1	1	1	1	1	1	1
140.00-120.00				1	1	1	1	1	1	1
Т3	No	Yes	1	1	1	1	1	1	1	1
120.00-100.00				1	1	1	1	1	1	1
T4	No	Yes	1	1	1	1	1	1	1	1
100.00-80.00				1	1	1	1	1	1	1
T5	No	Yes	1	1	1	1	1	1	1	1
80.00-60.00				1	1	1	1	1	1	1
T6	No	Yes	1	1	1	1	1	1	1	1
60.00-40.00				1	1	1	1	1	1	1
T7	No	Yes	1	1	1	1	1	1	1	1
40.00-20.00				1	1	1	1	1	1	1
T8 20.00-6.67	No	Yes	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1
T9 6.67-0.00	No	Yes	1	1	1	1	1	1	1	1
12.7				1	1	1	1	1	1	1

<sup>&</sup>lt;sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

### **Tower Section Geometry** (cont'd)

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 149.00-140.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 140.00-120.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 120.00-100.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 100.00-80.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

### tnxTower

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Tower Elevation	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
ft	Net Width	U	Net Width	U	Net Width	U	Net	U	Net	U	Net	U	Net	$\overline{U}$
		U		U		U		U		U		U		U
	Deduct		Deduct		Deduct		Width		Width		Width		Width	
	in		in		in		Deduct		Deduct		Deduct		Deduct	
							in		in		in		in	
T5 80.00-60.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T6 60.00-40.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T7 40.00-20.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T8 20.00-6.67	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T9 6.67-0.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

Guy	Data
-----	------

Guy Elevation	Guy Grade		Guy Size	Initial Tension	%	Guy Modulus	Guy Weight	$L_u$	Anchor Radius	Anchor Azimuth	Anchor Elevation	End Fitting
ft				lb		ksi	plf	ft	ft	$\underset{\circ}{Adj}$ .	ft	Efficiency %
136.667	EHS	A	5/8	4240.00	10%	21000	0.813	173.66	95.00	0.0000	-10.00	100%
		В	5/8	4240.00	10%	21000	0.813	173.66	95.00	0.0000	-10.00	100%
		C	5/8	4240.00	10%	21000	0.813	173.66	95.00	0.0000	-10.00	100%
66.6667	EHS	Α	3/4	5830.00	10%	19000	1.155	120.62	95.00	0.0000	-10.00	100%
		В	3/4	5830.00	10%	19000	1.155	120.62	95.00	0.0000	-10.00	100%
		C	3/4	5830.00	10%	19000	1.155	120.62	95.00	0.0000	-10.00	100%

# Guy Data(cont'd)

Guy Elevation ft	Mount Type	Torque-Arm Spread	Torque-Arm Leg Angle	Torque-Arm Style	Torque-Arm Grade	Torque-Arm Type	Torque-Arm Size
		ft	0				
136.667	Corner						
66.6667	Corner						

# Guy Data (cont'd)

Guy Elevation ft	Diagonal Grade	Diagonal Type	Upper Diagonal Size	Lower Diagonal Size	Is Strap.	Pull-Off Grade	Pull-Off Type	Pull-Off Size
136.67	A572-50	Solid Round				A572-50	Solid Round	
	(50 ksi)					(50 ksi)		
66.67	A572-50	Solid Round				A572-50	Solid Round	
	(50 ksi)					(50 ksi)		

# Guy Data (cont'd)

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Guy	Cable	Cable	Cable	Cable	Tower	Tower	Tower	Tower
Elevation	Weight	Weight	Weight	Weight	Intercept	Intercept	Intercept	Intercept
	A	B	C	D	A	B	C	D
ft	lb	lb	lb	lb	ft	ft	ft	ft
136.667	141.19	141.19	141.19		2.85	2.85	2.85	
					2.9 sec/pulse	2.9 sec/pulse	2.9 sec/pulse	
66.6667	139.32	139.32	139.32		1.43	1.43	1.43	
					2.1 sec/pulse	2.1 sec/pulse	2.1 sec/pulse	

# Guy Data (cont'd)

			Torqu	Torque Arm		l Off	Diagonal	
Guy	Calc	Calc	$K_x$	$K_{y}$	$K_x$	$K_{y}$	$K_x$	$K_{y}$
Elevation	K	K		•		·		•
ft	Single	Solid						
	Angles	Rounds						
136.667	No	No			1	1	1	1
66.6667	No	No			1	1	1	1

# Guy Data (cont'd)

		Torqı	ıe-Arm		Pull Off			Diagonal				
Guy	Bolt Size	Number	Net Width	U	Bolt Size	Number	Net Width	U	Bolt Size	Number	Net Width	U
Elevation	in		Deduct		in		Deduct		in		Deduct	
ft			in				in				in	
136.667	0.6250	0	0.0000	0.75	0.6250	0	0.0000	0.75	0.6250	0	0.0000	0.75
	A325N				A325N				A325N			
66.6667	0.6250	0	0.0000	0.75	0.6250	0	0.0000	0.75	0.6250	0	0.0000	0.75
	A325N				A325N				A325N			

#### **Guy Pressures**

Guy Elevation	Guy Location	Z	$q_z$	$q_z$ $Ice$	Ice Thickness
ft		ft	psf	psf	in
136.667	A	63.33	27	4	1.3609
	В	63.33	27	4	1.3609
	C	63.33	27	4	1.3609
66.6667	A	28.33	22	4	1.2557
	В	28.33	22	4	1.2557
	C	28.33	22	4	1.2557

# Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Total Number	Number Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
1.65" Hybird	C	No	No	Ar (CaAa)	145.00 - 0.00	1	1	1.6250	1.6500		1.00

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# Feed Line/Linear Appurtenances Section Areas

Tower	Tower	Face	$A_R$	$A_F$	$C_AA_A$	$C_A A_A$	Weight
Section	Elevation		_	_	In Face	Out Face	
	ft		ft²	ft <sup>2</sup>	_ft²	ft <sup>2</sup>	lb
T1	149.00-140.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.825	0.000	5.00
T2	140.00-120.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	3.300	0.000	20.00
T3	120.00-100.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	3.300	0.000	20.00
T4	100.00-80.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	3.300	0.000	20.00
T5	80.00-60.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	3.300	0.000	20.00
T6	60.00-40.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	3.300	0.000	20.00
T7	40.00-20.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	3.300	0.000	20.00
T8	20.00-6.67	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	2.200	0.000	13.33
T9	6.67-0.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	1.100	0.000	6.67

# Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness			In Face	Out Face	
	ft	Leg	in	$ft^2$	$ft^2$	$ft^2$	$ft^2$	lb
T1	149.00-140.00	A	1.478	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	2.303	0.000	33.24
T2	140.00-120.00	A	1.462	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	9.149	0.000	131.21
T3	120.00-100.00	A	1.438	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	9.053	0.000	128.52
T4	100.00-80.00	A	1.410	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	8.938	0.000	125.38
T5	80.00-60.00	A	1.375	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	8.798	0.000	121.59
T6	60.00-40.00	A	1.329	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	8.616	0.000	116.75
T7	40.00-20.00	A	1.263	0.000	0.000	0.000	0.000	0.00

tnx <sub>T</sub>	<i>ower</i>

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Tower Section	Tower Elevation	Face or	Ice Thickness	$A_R$	$A_F$	$C_AA_A$ In Face	$C_AA_A$ Out Face	Weight
	ft	Leg	in	$ft^2$	ft²	ft²	ft²	lb
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	8.352	0.000	109.89
T8	20.00-6.67	A	1.165	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	5.305	0.000	66.72
T9	6.67-0.00	A	1.014	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	2.452	0.000	28.66

# **Feed Line Center of Pressure**

Section	Elevation	$CP_X$	$CP_Z$	$CP_X$	$CP_Z$
				Ice	Ice
	ft	in	in	in	in
T1	149.00-140.00	0.0000	0.7722	0.0000	0.7382
T2	140.00-120.00	0.0000	1.3433	0.0000	1.3374
T3	120.00-100.00	0.0000	1.2620	0.0000	1.3022
T4	100.00-80.00	0.0000	1.2620	0.0000	1.3125
T5	80.00-60.00	0.0000	1.2155	0.0000	1.2897
T6	60.00-40.00	0.0000	1.2620	0.0000	1.3409
T7	40.00-20.00	0.0000	1.3433	0.0000	1.4048
T8	20.00-6.67	0.0000	1.1508	0.0000	1.3129
T9	6.67-0.00	0.0000	1.0416	0.0000	0.8716

# **Shielding Factor Ka**

Tower	Feed Line	Description	Feed Line	$K_a$	$K_a$
Section	Record No.		Segment Elev.	No Ice	Ice
T1	1	1.65" Hybird	140.00 -	0.6000	0.5485
			145.00		
T2	1	1.65" Hybird	120.00 -	0.6000	0.5666
			140.00		
T3	1	1.65" Hybird	100.00 -	0.6000	0.5629
			120.00		
T4	1	1.65" Hybird	80.00 - 100.00	0.6000	0.5681
T5	1	1.65" Hybird	60.00 - 80.00	0.6000	0.5666
T6	1	1.65" Hybird	40.00 - 60.00	0.6000	0.5827
T7	1	1.65" Hybird	20.00 - 40.00	0.6000	0.6000
T8	1	1.65" Hybird	6.67 - 20.00	0.6000	0.5964
T9	1	1.65" Hybird	0.00 - 6.67	0.6000	0.4433

# **Discrete Tower Loads**

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	C₄A₄ Side	Weight
			ft ft ft	0	ft		ft²	ft²	lb
Reserved Loading	A	From Face	4.00	0.0000	145.00	No Ice	25.46	25.46	1200.00
(1/3*11,000 sq. in)			0.00			1/2" Ice	26.83	26.83	1560.0
(Dish Network)			0.00			1" Ice	28.21	28.21	1920.0
` ′						2" Ice	31.24	31.24	2640.0
Reserved Loading	В	From Face	4.00	0.0000	145.00	No Ice	25.46	25.46	1200.0
(1/3*11,000 sq. in)			0.00			1/2" Ice	26.83	26.83	1560.0
(Dish Network)			0.00			1" Ice	28.21	28.21	1920.0
`						2" Ice	31.24	31.24	2640.0
Reserved Loading	C	From Face	4.00	0.0000	145.00	No Ice	25.46	25.46	1200.0
(1/3*11,000 sq. in)			0.00			1/2" Ice	26.83	26.83	1560.0
(Dish Network)			0.00			1" Ice	28.21	28.21	1920.0
,						2" Ice	31.24	31.24	2640.0

# **Load Combinations**

Comb.	Description
No.	<u> </u>
1	Dead Only
2	1.2 Dead+1.0 Wind 0 deg - No Ice+1.0 Guy
3	1.2 Dead+1.0 Wind 30 deg - No Ice+1.0 Guy
4	1.2 Dead+1.0 Wind 60 deg - No Ice+1.0 Guy
5	1.2 Dead+1.0 Wind 90 deg - No Ice+1.0 Guy
6	1.2 Dead+1.0 Wind 120 deg - No Ice+1.0 Guy
7	1.2 Dead+1.0 Wind 150 deg - No Ice+1.0 Guy
8	1.2 Dead+1.0 Wind 180 deg - No Ice+1.0 Guy
9	1.2 Dead+1.0 Wind 210 deg - No Ice+1.0 Guy
10	1.2 Dead+1.0 Wind 240 deg - No Ice+1.0 Guy
11	1.2 Dead+1.0 Wind 270 deg - No Ice+1.0 Guy
12	1.2 Dead+1.0 Wind 300 deg - No Ice+1.0 Guy
13	1.2 Dead+1.0 Wind 330 deg - No Ice+1.0 Guy
14	1.2 Dead+1.0 Ice+1.0 Temp+Guy
15	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy
16	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy
17	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy
18	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy
19	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy
20	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy
21	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy
22	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy
23	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy
24	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy
25	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy
26	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy
27	Dead+Wind 0 deg - Service+Guy
28	Dead+Wind 30 deg - Service+Guy
29	Dead+Wind 60 deg - Service+Guy
30	Dead+Wind 90 deg - Service+Guy
31	Dead+Wind 120 deg - Service+Guy
32	Dead+Wind 150 deg - Service+Guy
33	Dead+Wind 180 deg - Service+Guy
34	Dead+Wind 210 deg - Service+Guy

tnx <sub>T</sub>	<i>ower</i>

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Comb.	Description
No.	
35	Dead+Wind 240 deg - Service+Guy
36	Dead+Wind 270 deg - Service+Guy
37	Dead+Wind 300 deg - Service+Guy
38	Dead+Wind 330 deg - Service+Guy

#### **Maximum Tower Deflections - Service Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
T1	149 - 140	0.908	33	0.0579	0.0957
T2	140 - 120	0.797	33	0.0565	0.0945
T3	120 - 100	0.580	33	0.0482	0.1063
T4	100 - 80	0.386	33	0.0441	0.1068
T5	80 - 60	0.214	37	0.0354	0.1067
T6	60 - 40	0.099	37	0.0185	0.1068
T7	40 - 20	0.048	37	0.0088	0.1084
T8	20 - 6.667	0.023	27	0.0054	0.1095
T9	6.667 - 0	0.008	27	0.0055	0.1005

#### Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
145.00	Reserved Loading (1/3*11,000 sq.	33	0.858	0.0575	0.0955	145726
	in)					
136.67	Guy	33	0.758	0.0555	0.0943	92836
66.67	Guy	37	0.129	0.0240	0.1068	66385

# **Maximum Tower Deflections - Design Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
T1	149 - 140	4.825	6	0.3134	0.3975
T2	140 - 120	4.224	6	0.3078	0.3959
T3	120 - 100	3.020	6	0.2695	0.4090
T4	100 - 80	1.938	10	0.2426	0.4109
T5	80 - 60	1.004	10	0.1903	0.4100
T6	60 - 40	0.440	12	0.0986	0.4101
T7	40 - 20	0.195	12	0.0416	0.4160
T8	20 - 6.667	0.084	12	0.0210	0.4196
T9	6.667 - 0	0.028	12	0.0202	0.4099

# **Critical Deflections and Radius of Curvature - Design Wind**

tnxTower	tnx	To	wei
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T9

6.667 - 0

2 1/4

6.89

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Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	0	0	ft
145.00	Reserved Loading (1/3*11,000 sq.	6	4.555	0.3117	0.3971	35707
	in)					
136.67	Guy	6	4.010	0.3031	0.3943	22320
66.67	Guy	12	0.587	0.1286	0.4097	12297

				Guy De	sign Dat	ta		
Section No.	Elevation ft	Size	Initial Tension lb	Breaking Load lb	Actual T <sub>u</sub> lb	Allowable $\phi T_n$ $lb$	Required S.F.	Actual S.F.
T2	136.67 (A) (297)	5/8 EHS	4240.00	42399.99	9192.33	25440.00	1.000	2.768
	136.67 (B) (296)	5/8 EHS	4240.00	42399.99	9197.02	25440.00	1.000	2.766
	136.67 (C) (295)	5/8 EHS	4240.00	42399.99	9196.95	25440.00	1.000	2.766
T5	66.67 (A) (300)	3/4 EHS	5830.00	58299.91	8600.65	34980.00	1.000	4.067
	66.67 (B) (299)	3/4 EHS	5830.00	58299.91	8601.58	34980.00	1.000	4.067
	66.67 (C) (298)	3/4 EHS	5830.00	58299.91	8601.65	34980.00	1.000	4.067

# Compression Checks

Leg Design Data (Compression)

0.156 <sup>1</sup>

120569.00

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	Mast Stability	$P_u$	$\phi P_n$	$Ratio$ $P_u$
	ft		ft	ft		$in^2$	Index	lb	lb	$\phi P_n$
T1	149 - 140	1 3/4	9.00	3.00	82.3 K=1.00	2.4053	1.00	-4834.51	65973.80	0.073 1
T2	140 - 120	1 3/4	20.00	3.33	91.4 K=1.00	2.4053	1.00	-10275.80	58740.50	0.175 1
T3	120 - 100	2	20.00	3.33	80.0 K=1.00	3.1416	1.00	-11228.40	88538.90	0.127 1
T4	100 - 80	2	20.00	3.33	80.0 K=1.00	3.1416	1.00	-16570.80	88538.90	0.187 1
T5	80 - 60	2	20.00	3.33	80.0 K=1.00	3.1416	1.00	-24545.40	88538.90	0.277 1
T6	60 - 40	2	20.00	3.33	80.0 K=1.00	3.1416	1.00	-22053.30	88538.90	0.249 1
T7	40 - 20	1 3/4	20.00	3.33	91.4 K=1.00	2.4053	1.00	-17452.00	58740.50	0.297 1
T8	20 - 6.667	2 1/4	13.33	3.33	71.1 K=1.00	3.9761	1.00	-17914.20	123623.00	0.145 <sup>1</sup>

3.44 73.5 3.9761

1.00

-18850.70

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Section No.	Elevation	Size	L	$L_u$	Kl/r	A	Mast Stability	$P_u$	$\phi P_n$	Ratio
NO.	ft		ft	ft		$in^2$	Stability Index	lb	lb	$\frac{P_u}{\phi P_n}$
					K=1.00					~

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

# **Diagonal Design Data (Compression)**

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	149 - 140	1	4.24	4.04	135.6 K=0.70	0.7854	-2471.73	9646.34	0.256
T2	140 - 120	1	4.48	4.27	143.4 K=0.70	0.7854	-2475.60	8633.74	0.287 1
T3	120 - 100	1	4.48	4.24	142.3 K=0.70	0.7854	-468.08	8761.17	0.053
T4	100 - 80	1	4.48	4.24	142.3 K=0.70	0.7854	-932.43	8761.17	0.106
T5	80 - 60	1 1/4	4.48	4.24	113.8 K=0.70	1.2272	-1189.42	20096.40	0.059
Т6	60 - 40	1	4.48	4.24	142.3 K=0.70	0.7854	-1097.45	8761.17	0.125
T7	40 - 20	1	4.48	4.27	143.4 K=0.70	0.7854	-719.24	8633.74	0.083
Т8	20 - 6.667	1 1/4	4.48	4.20	113.0 K=0.70	1.2272	-437.67	20298.70	0.022
Т9	6.667 - 0	1 1/4	4.05	3.71	99.8 K=0.70	1.2272	-302.09	23528.10	0.013

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

# **Horizontal Design Data (Compression)**

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	$Ratio$ $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	149 - 140	7/8	3.00	2.85	109.6 K=0.70	0.6013	-682.32	10351.80	0.066 1
T2	140 - 120	7/8	3.00	2.85	109.6 K=0.70	0.6013	-177.98	10351.80	0.017 1
Т3	120 - 100	7/8	3.00	2.83	108.8 K=0.70	0.6013	-194.48	10447.40	0.019 1
T4	100 - 80	7/8	3.00	2.83	108.8 K=0.70	0.6013	-287.01	10447.40	0.027 1
T5	80 - 60	7/8	3.00	2.83	108.8 K=0.70	0.6013	-425.14	10447.40	0.041 1
T6	60 - 40	7/8	3.00	2.83	108.8 K=0.70	0.6013	-381.97	10447.40	0.037 1

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Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	$Ratio$ $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T7	40 - 20	7/8	3.00	2.85	109.6 K=0.70	0.6013	-302.28	10351.80	0.029 1
Т8	20 - 6.667	7/8	3.00	2.81	108.0 K=0.70	0.6013	-310.28	10543.30	0.029 1
Т9	6.667 - 0	7/8	1.50	1.31	79.2 K=1.10	0.6013	-334.53	14003.60	0.024 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

	Top Girt Design Data (Compression)											
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio			
110.	ft		ft	ft		$in^2$	lb	lb	$\frac{1}{\phi P_n}$			
T1	149 - 140	7/8	3.00	2.85	109.6 K=0.70	0.6013	-52.35	10351.80	0.005 1			
T2	140 - 120	7/8	3.00	2.85	109.6 K=0.70	0.6013	-44.34	10351.80	0.004 1			

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

#### Tension Checks

	Leg Design Data (Tension)								
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	149 - 140	1 3/4	9.00	3.00	82.3	2.4053	1707.63	108238.00	0.016 1
T2	140 - 120	1 3/4	20.00	3.33	91.4	2.4053	4735.82	108238.00	0.044 1
T4	100 - 80	2	20.00	3.33	80.0	3.1416	1228.54	141372.00	0.009 1
T5	80 - 60	2	20.00	3.33	80.0	3.1416	5730.82	141372.00	0.041 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

# **Diagonal Design Data (Tension)**

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Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	149 - 140	1	4.24	4.04	193.7	0.7854	2455.41	25446.90	0.096 1
T2	140 - 120	1	4.48	4.27	204.8	0.7854	2453.63	25446.90	0.096 1
Т3	120 - 100	1	4.48	4.24	203.3	0.7854	326.50	25446.90	0.013 1
T4	100 - 80	1	4.48	4.24	203.3	0.7854	780.44	25446.90	0.031 1
T5	80 - 60	1 1/4	4.48	4.24	162.6	1.2272	1076.03	39760.80	0.027 1
Т6	60 - 40	1	4.48	4.24	203.3	0.7854	868.07	25446.90	0.034 1
T7	40 - 20	1	4.48	4.27	204.8	0.7854	520.65	25446.90	0.020 1
Т8	20 - 6.667	1 1/4	4.48	4.20	161.4	1.2272	173.60	39760.80	0.004 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
110.	ft		ft	ft		$in^2$	lb	lb	$\frac{1}{\phi P_n}$
T1	149 - 140	7/8	3.00	2.85	156.6	0.6013	688.95	19482.80	0.035 1
T2	140 - 120	7/8	3.00	2.85	156.6	0.6013	2764.66	19482.80	0.142 1
Т3	120 - 100	7/8	3.00	2.83	155.4	0.6013	194.48	19482.80	0.010 1
T4	100 - 80	7/8	3.00	2.83	155.4	0.6013	287.01	19482.80	0.015 1
T5	80 - 60	7/8	3.00	2.83	155.4	0.6013	3803.71	19482.80	0.195 1
T6	60 - 40	7/8	3.00	2.83	155.4	0.6013	381.97	19482.80	0.020 1
T7	40 - 20	7/8	3.00	2.85	156.6	0.6013	302.28	19482.80	0.016 1
Т8	20 - 6.667	7/8	3.00	2.81	154.3	0.6013	310.28	19482.80	0.016 1
Т9	6.667 - 0	7/8	1.50	1.31	72.0	0.6013	334.53	19482.80	0.017 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

# Top Girt Design Data (Tension)

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Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	149 - 140	7/8	3.00	2.85	156.6	0.6013	54.19	19482.80	0.003 1
T2	140 - 120	7/8	3.00	2.85	156.6	0.6013	62.30	19482.80	0.003 1
Т3	120 - 100	7/8	3.00	2.83	155.4	0.6013	69.34	19482.80	0.004 1
T4	100 - 80	7/8	3.00	2.83	155.4	0.6013	78.01	19482.80	0.004 1
T5	80 - 60	7/8	3.00	2.83	155.4	0.6013	83.35	19482.80	0.004 1
Т6	60 - 40	7/8	3.00	2.83	155.4	0.6013	104.51	19482.80	0.005 1
T7	40 - 20	7/8	3.00	2.85	156.6	0.6013	104.48	19482.80	0.005 1
Т8	20 - 6.667	7/8	3.00	2.81	154.3	0.6013	117.51	19482.80	0.006 1
Т9	6.667 - 0	7/8	3.00	2.81	154.3	0.6013	2808.57	19482.80	0.144 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

# **Section Capacity Table**

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	$ otag P_{allow} \\ lb $	% Capacity	Pass Fail
T1	149 - 140	Leg	1 3/4	2	-4834.51	65973.80	7.3	Pass
T2	140 - 120	Leg	1 3/4	22	-10275.80	58740.50	17.5	Pass
T3	120 - 100	Leg	2	61	-11228.40	88538.90	12.7	Pass
T4	100 - 80	Leg	2	101	-16570.80	88538.90	18.7	Pass
T5	80 - 60	Leg	2	140	-24545.40	88538.90	27.7	Pass
T6	60 - 40	Leg	2	179	-22053.30	88538.90	24.9	Pass
T7	40 - 20	Leg	1 3/4	218	-17452.00	58740.50	29.7	Pass
T8	20 - 6.667	Leg	2 1/4	257	-17914.20	123623.00	14.5	Pass
T9	6.667 - 0	Leg	2 1/4	283	-18850.70	120569.00	15.6	Pass
T1	149 - 140	Diagonal	1	7	-2471.73	9646.34	25.6	Pass
T2	140 - 120	Diagonal	1	58	-2475.60	8633.74	28.7	Pass
T3	120 - 100	Diagonal	1	69	-468.08	8761.17	5.3	Pass
T4	100 - 80	Diagonal	1	106	-932.43	8761.17	10.6	Pass
T5	80 - 60	Diagonal	1 1/4	157	-1189.42	20096.40	5.9	Pass
T6	60 - 40	Diagonal	1	214	-1097.45	8761.17	12.5	Pass
T7	40 - 20	Diagonal	1	253	-719.24	8633.74	8.3	Pass
T8	20 - 6.667	Diagonal	1 1/4	280	-437.67	20298.70	2.2	Pass
T9	6.667 - 0	Diagonal	1 1/4	293	-302.09	23528.10	1.3	Pass
T1	149 - 140	Horizontal	7/8	16	-682.32	10351.80	6.6	Pass
T2	140 - 120	Horizontal	7/8	55	2764.66	19482.80	14.2	Pass
T3	120 - 100	Horizontal	7/8	72	-194.48	10447.40	1.9	Pass
T4	100 - 80	Horizontal	7/8	109	-287.01	10447.40	2.7	Pass
T5	80 - 60	Horizontal	7/8	154	3803.71	19482.80	19.5	Pass
T6	60 - 40	Horizontal	7/8	193	-381.97	10447.40	3.7	Pass
T7	40 - 20	Horizontal	7/8	227	-302.28	10351.80	2.9	Pass
T8	20 - 6.667	Horizontal	7/8	266	-310.28	10543.30	2.9	Pass
T9	6.667 - 0	Horizontal	7/8	289	-334.53	14003.60	2.4	Pass

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Section	Elevation	Component	Size	Critical	P	$ olimits P_{allow} $	%	Pass
No.	ft	Туре		Element	lb	lb	Capacity	Fail
T1	149 - 140	Top Girt	7/8	5	-52.35	10351.80	0.5	Pass
T2	140 - 120	Top Girt	7/8	26	-44.34	10351.80	0.4	Pass
T3	120 - 100	Top Girt	7/8	64	69.34	19482.80	0.4	Pass
T4	100 - 80	Top Girt	7/8	103	78.01	19482.80	0.4	Pass
T5	80 - 60	Top Girt	7/8	142	83.35	19482.80	0.4	Pass
T6	60 - 40	Top Girt	7/8	181	104.51	19482.80	0.5	Pass
T7	40 - 20	Top Girt	7/8	220	104.48	19482.80	0.5	Pass
T8	20 - 6.667	Top Girt	7/8	259	117.51	19482.80	0.6	Pass
T9	6.667 - 0	Top Girt	7/8	288	2808.57	19482.80	14.4	Pass
T2	140 - 120	Guy A@136.667	5/8	297	9192.33	25440.00	36.1	Pass
T5	80 - 60	Guy A@66.6667	3/4	300	8600.65	34980.00	24.6	Pass
T2	140 - 120	Guy B@136.667	5/8	296	9197.02	25440.00	36.2	Pass
T5	80 - 60	Guy B@66.6667	3/4	299	8601.58	34980.00	24.6	Pass
T2	140 - 120	Guy C@136.667	5/8	295	9196.95	25440.00	36.2	Pass
T5	80 - 60	Guy C@66.6667	3/4	298	8601.65	34980.00	24.6	Pass
		, .					Summary	
						Leg (T7)	29.7	Pass
						Diagonal (T2)	28.7	Pass
						Horizontal	19.5	Pass
						(T5)		
						Top Girt (T9)	14.4	Pass
						Guy A (T2)	36.1	Pass
						Guy B (T2)	36.2	Pass
						Guy C (T2)	36.2	Pass
						RATING =	36.2	Pass

 $Program\ Version\ 8.0.7.5-8/3/2020\ File: C:/Users/bdavenport/Desktop/CT1010\ Willington.eri$ 

# Exhibit E

**Mount Analysis** 



1033 WATERVLIET SHAKER RD, ALBANY, NY 12205

# **Mount Analysis Report**

October 25, 2021

Dish Wireless Site Number	BOBDL00147A
Infinigy Job Number	2039-Z5555C
Client	Northeast Site Solutions
Carrier	Dish Wireless
	109 Schofield Road,
Site Location	Willington, CT 06249
Site Location	41.9223 N NAD83
	72.2936 W NAD83
Mount Centerline EL.	145 ft
Mount Classification	Sector Frame
Structural Usage Ratio	19%
Overall Result	Pass

Upon reviewing the results of this analysis, it is our opinion that the structure meets the specified TIA and ASCE code requirements. The proposed antenna mounts for the proposed carrier are therefore deemed **adequate** to support the final loading configuration as listed in this report.



Dmitriy Albul, P.E. Engineering Consultant to Infinigy

#### Mount Analysis Report

#### October 25, 2021

# **Contents**

Introduction	3
Supporting Documentation	3
Analysis Code Requirements	3
Conclusion	3
Final Configuration Loading	4
Structure Usages	4
Assumptions and Limitations	4
Calculations	Appended

BOBDL00147A Page | 2

October 25, 2021

#### **Introduction**

Infinigy Engineering has been requested to perform a mount analysis of proposed antenna mount from the Dish Wireless equipment. All supporting documents have been obtained from the client and are assumed to be accurate and applicable to this site. The mount was analyzed using RISA-3D Version 19.0. analysis software.

#### **Supporting Documentation**

<b>Mount Details</b>	Mount Specification Sabre Industries C10837002C-32788
<b>Construction Drawings</b>	Infinigy Engineering PLLC, Job No. 2039-Z5555C, dated April 29, 2021
RF Design Sheet	Dish Wireless, dated February 15, 2021

#### **Analysis Code Requirements**

Wind Speed	125 mph (3-second Gust, V <sub>ult</sub> .)
Wind Speed w/ ice	50 mph (3-Second Gust) w/ 1" ice
TIA Revision	ANSI/TIA-222-G
Adopted IBC	2018 Connecticut State Building Code (2015 IBC)
Structure Class	II
Exposure Category	В
Topographic Method	Method 2
Topographic Category	1
Spectral Response	Ss=0.174, S <sub>1</sub> =0.063
Site Class	D – Stiff Soil
HMSL	808.17 ft.

#### **Conclusion**

Upon reviewing the results of this analysis, it is our opinion that the structure meets the specified TIA code requirements. The proposed antenna mounts are therefore deemed adequate to support the final loading configuration as listed in this report.

If you have any questions, require additional information, or actual conditions differ from those as detailed in this report please contact me via the information below:

Dmitriy Albul, P.E. Professional Engineer | Engineering Consultant to Infinigy 1033 Watervliet Shaker Road, Albany, NY 12205 (O) (518) 690-0790 | (M) (518) 669-4428 www.infinigy.com

BOBDL00147A Page | 3

#### October 25, 2021

#### **Final Configuration Loading**

Mount	Rad.	Vert.	Horiz.			Carrier
CL	HT	O/S	O/S	Qty	Qty Appurtenance	
(ft)	(ft)	(ft)	(ft)*			
			5	3	JMA MX08FRO665-20_VOF	
145.0	1450		5	3	Fujitsu TA08025-B605	Dish
145.0	145.0	-	5	3	Fujitsu TA08025-B604	Wireless
			ı	1	Raycap RDIDC-9181-PF-48	

<sup>\*</sup>Horizontal Offset is defined as the distance from the left most edge of the mount face horizontal when viewed facing the tower.

#### **Structure Usages**

Plates	13%	Pass
Arms	4%	Pass
Mount Pipes	19%	Pass
Stabilizer	4%	Pass
Bracing	7%	Pass
Connections	15%	Pass
Rating	<u>19%</u>	Pass

#### **Assumptions and Limitations**

Our structural calculations are completed assuming all information provided to Infinigy Engineering is accurate and applicable to this site. For the purposes of calculations, we assume an overall structure condition of "like new" and all members and connections to be free of corrosion and/or structural defects. The structure owner and/or contractor shall verify the structure's condition prior to installation of any proposed equipment. If actual conditions differ from those described in this report Infinigy Engineering should be notified immediately to complete a revised evaluation.

Our evaluation is completed using standard TIA, AISC, ACI, and ASCE methods and procedures. Our structural results are proprietary and should not be used by others as their own. Infinigy Engineering is not responsible for decisions made by others that are or are not based on our supplied assumptions and conclusions.

This report is an evaluation of the proposed carriers mount structure only and does not reflect adequacy of the existing tower, other mounts, or coax mounting attachments. These elements are assumed to be adequate for the purposes of this analysis and are assumed to have been installed per their manufacturer requirements.

BOBDL00147A Page | 4

# **INFINIGY8**

#### FROM ZERO TO INFINIGY

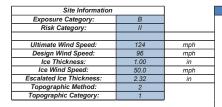
#### the solutions are endless

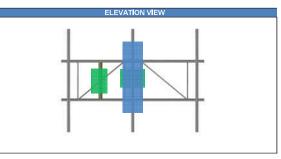
Date:	10/25/2021
Site Name:	BOBDL00147A
Project Engineer:	DVA
Project No:	2039-Z5555C
Customer:	Northeast Site Solutions
Carrier:	Dish Wireless

Building Code:	2015	
ASCE Standard:	ASCE 7-10	
TIA Standard:	G	
Mount Type:	Sector Frame	
	Proposed	
Mount Centerline:	145	ft
Superstructure Height:	N/A	ft
Structure Type:	Tower	

Factors						
Gh:	1.000					
K <sub>zmin</sub> :	0.700					
K <sub>z</sub> :	1.099					
K <sub>d</sub> :	0.950					
K <sub>zt</sub> :	1.000					
Ка:	0.900					
I wind:	1.000					
l ice:	1.000					

q <sub>z</sub> :	24.66	psf
Surface Wind Pressure:	0.00	psf





	PLAN VIEW
	PLAN VIEW
+	

Service Wind:	30.0	mph
Lm (man live load) =	500.0	<b>l</b> b
Lv (man live load) =	250.0	<b>I</b> b

#### Table 1. Equipment Specifications and Wind Pressure

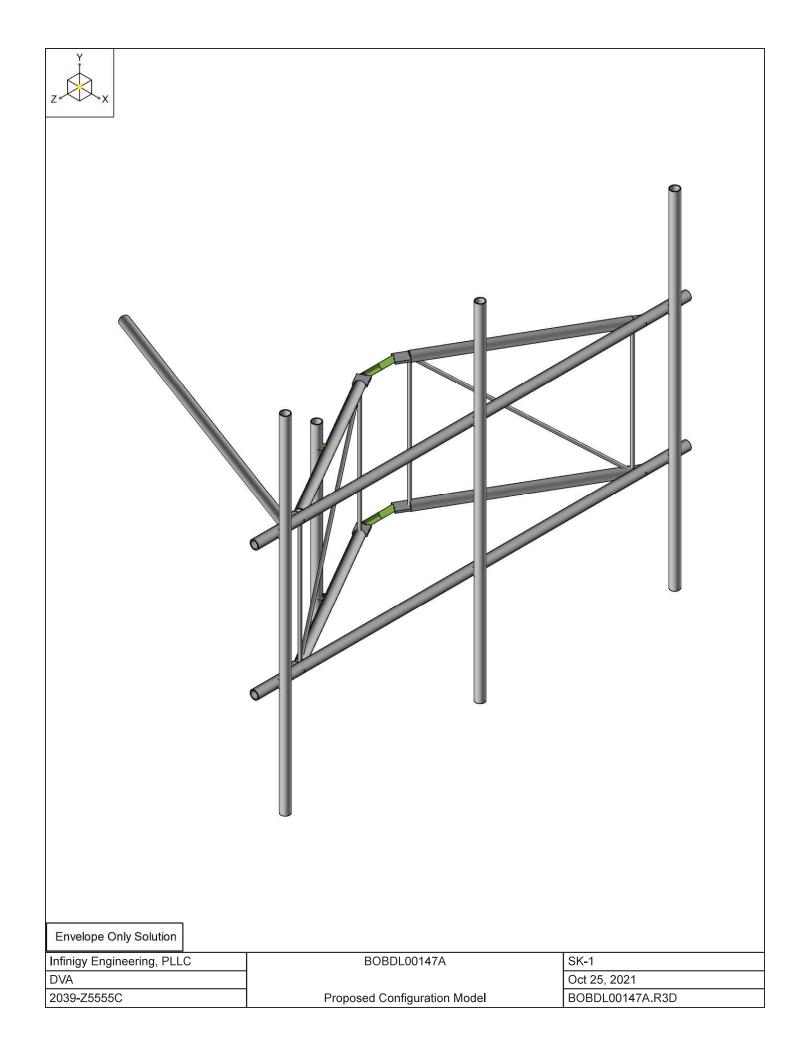
	Manufacturer	Model	Elevation	Pipe Label	Weight (lb)	Height (in)	Width (in)	Depth (in)	EPA <sub>N</sub>	EPA <sub>T</sub>	EPA N w/ ice	EPA T w/ ice	q z:	q z ice:	q z live:
	JMA WIRELESS	MX08FRO665-20	145	30	64.50	72.8	20	8	8.01	3.21	9.08	4.15	24.66	6.68	2.41
	FUJ <b>I</b> TSU	TA08025-B605	145	30	74.95	14.96	15.75	9.06	1.85	1.09	3.14	2.15	24.66	6.68	2.41
	FUJ <b>I</b> TSU	TA08025-B604	145	30	63.93	14.96	15.75	7.87	1.85	0.96	3.14	1.97	24.66	6.68	2.41
Γ	RAYCAP	RDIDC-9181-PF-48	145	37	21.85	16	14	8	1.77	1.05	3.04	2.10	24.66	6.68	2.41

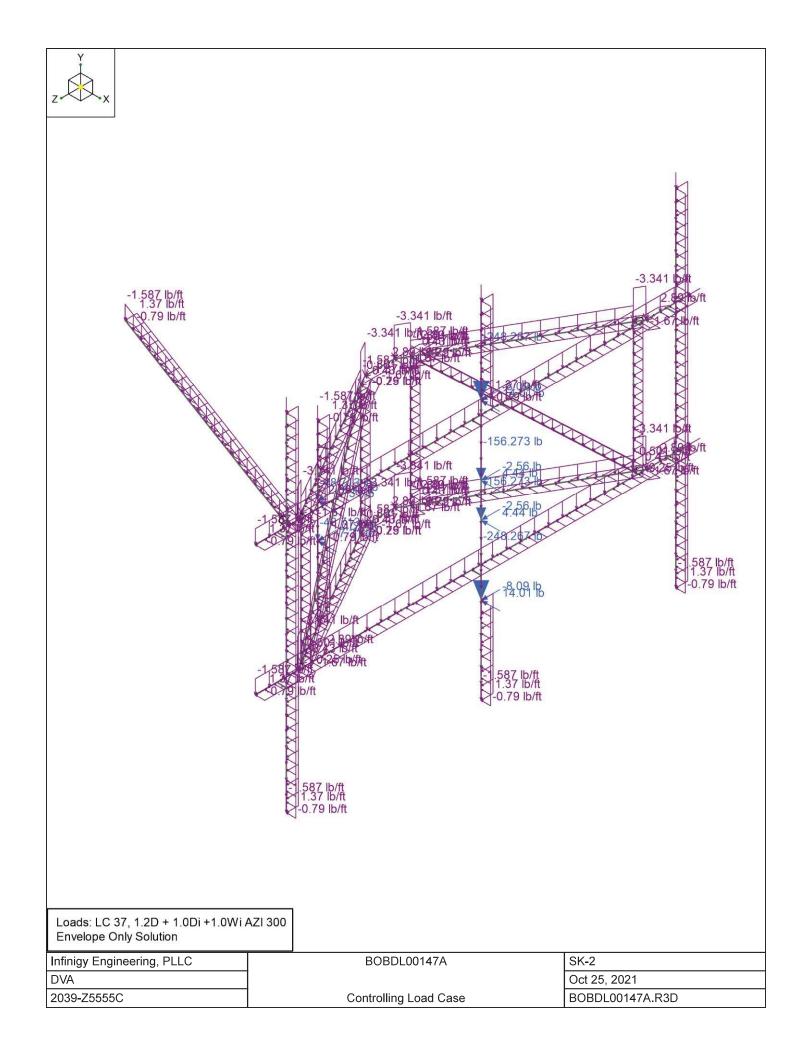
Table 2. Equipment Wind and Seismic Loads

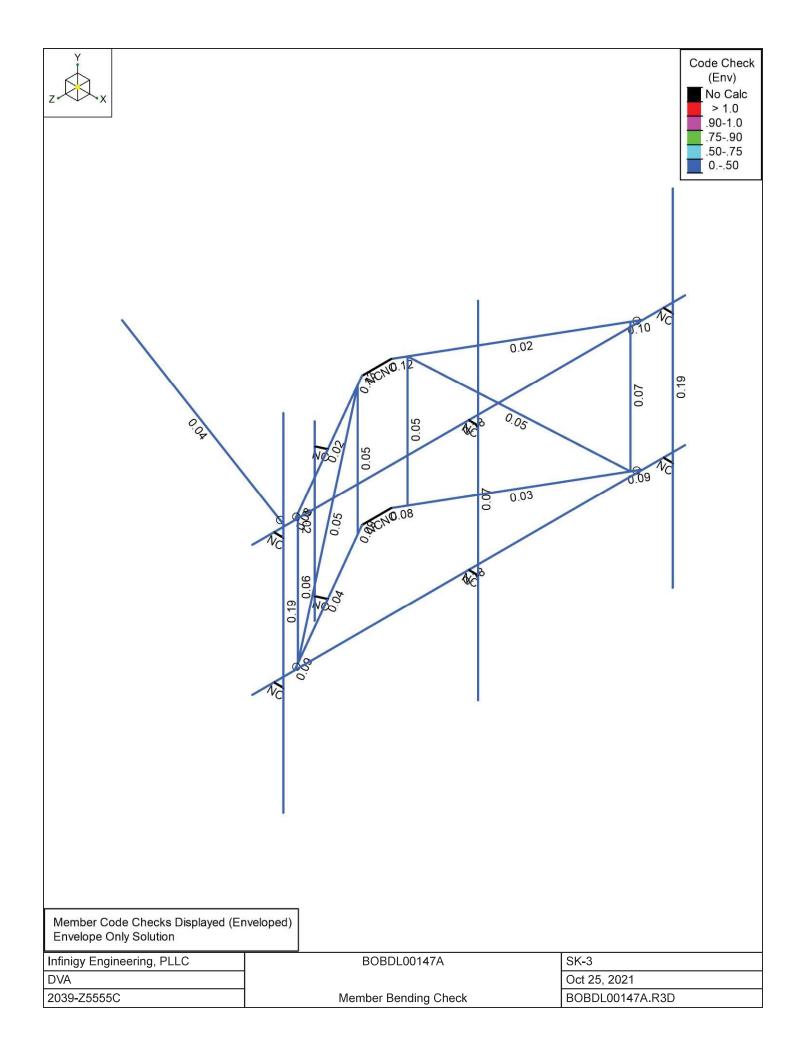
Manufacturer	Model	Wind Lo	Wind Load ( $F_A$ ), ID Wind Load Ice Case ( $F_A$ ), ID			Wind Load	Seismic		
JMA WIRELESS	MX08FRO665-20	178	71	55	25	419	17	7	0.0
FUJ <b>I</b> TSU	TA08025-B605	41	24	19	13	74	4	2	0.0
FUJ <b>I</b> TSU	TA08025-B604	41	21	19	12	72	4	2	0.0
RAYCAP	RDIDC-9181-PF-48	39	23	18	13	71	4	2	0.0

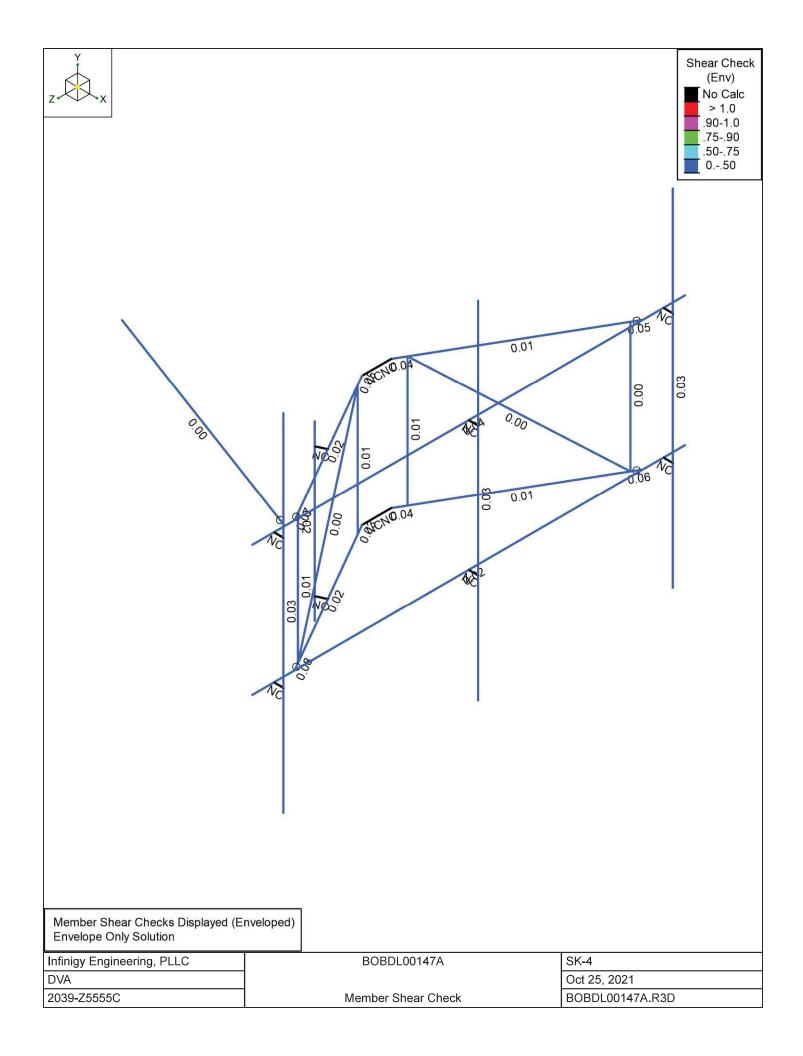
Table 3. Member Capacities

Member Name	Member Shape	Wind load	Wind Load	Weight Ice	Bending Check	Chang Chank	Total	Controlling
wember name	меттьег зпаре	r Snape (plf) Ice	Ice (plf)	(plf)	bending Check	Silear Check	Capacity	Capacity
Mount Pipes	PIPE_2.0	5.86	1.59	1.69	19%	3%	19%	
Stabilizer	PIPE_2.0	5.86	1.59	1.69	4%	0%	4%	
Bracing	0.75" SR	1.85	0.50	1.30	7%	1%	7%	19%
Arms	PIPE_2.0X	5,86	1.59	1.69	4%	2%	4%	15%
Frame Rails	PIPE_2.0X	5,86	1.59	1.69	18%	4%	18%	
Plates	3"x.5"	12,33	3.34	1.84	13%	8%	13%	











the solutions are endless

Company Designer

: Infinigy Engineering, PLLC

: DVA

Job Number : 2039-Z5555C Model Name: BOBDL00147A 10/25/2021 7:56:25 PM

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#### Model Settings

#### Solution

Members

Number of Reported Sections	5
Number of Internal Sections	100
Member Area Load Mesh Size (in²)	144
Consider Shear Deformation	Yes
Consider Torsional Warping	Yes

#### Wall Panels

Approximate Mesh Size (in)	12
Transfer Forces Between Intersecting Wood Walls	Yes
Increase Wood Wall Nailing Capacity for Wind Loads	Yes
Include P-Delta for Walls	Yes
Optimize Masonry and Wood Walls	Yes
Maximum Number of Iterations	3

#### **Processor Core Utilization**

Single	No
Multiple (Optimum)	Yes
Maximum	No

#### Axis

Vertical Global Axis

Global Axis corresponding to vertical direction		Υ		
	Convert Existing Data	Yes		

#### **Default Member Orientation**

Default Global Plane for z-axis	XZ
---------------------------------	----

#### Plate Axis

Plate Legal Axis Orientation	Nodel
I Plate Local Axis Orientation	Nodal

#### Codes

Hot Rolled Steel	AISC 14th (360-10): LRFD
Stiffness Adjustment	Yes (Iterative)
Notional Annex	None
Connections	AISC 14th (360-10): LRFD
Cold Formed Steel	AISI S100-12: LRFD
Stiffness Adjustment	Yes (Iterative)
Wood	AWC NDS-12: ASD
Temperature	< 100F
Concrete	ACI 318-11
Masonry	ACI 530-11: Strength
Aluminum	AA ADM1-10: LRFD
Structure Type	Building
Stiffness Adjustment	Yes (Iterative)
Stainless	AISC 14th (360-10): LRFD
Stiffness Adjustment	Yes (Iterative)

#### Concrete

Column Design

Analysis Methodology	Exact Integration Method
Parme Beta Factor	0.65

Compression Stress Block	Rectangular Stress Block
Analyze using Cracked Sections	Yes
Leave room for horizontal rebar splices (2*d bar spacing)	No



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Company

: Infinigy Engineering, PLLC

Designer : DVA

Job Number: 2039-Z5555C Model Name: BOBDL00147A 10/25/2021 7:56:25 PM Checked By : \_\_\_\_\_

#### the solutions are endless Model Settings (Continued) List forces which were ignored for design in the Detail Report Yes Rebar Column Min Steel 1 Column Max Steel 8 Rebar Material Spec ASTM A615 Warn if beam-column framing arrangement is not understood No Shear Reinforcement Number of Shear Regions 4 Region 2 & 3 Spacing Increase Increment (in) 4 Seismic RISA-3D Seismic Load Options Code **ASCE 7-10** Risk Category I or II Drift Cat Other Base Elevation (ft) Include the weight of the structure in base shear calcs Yes Site Parameters S<sub>1</sub> (g) SD<sub>1</sub> (g) 1 SD<sub>s</sub> (g) 5 T<sub>L</sub> (sec) Structure Characteristics TZ (sec) TX (sec) $C_tX$ 0.02 C<sub>t</sub>Exp. Z 0.75 C<sub>t</sub>Exp. X 0.75 3 RX 3 $\Omega_0 Z$ 1 $\Omega_0 X$ 1 $C_dZ$ 4 4

1



Company Designer

: Infinigy Engineering, PLLC

: DVA

Job Number : 2039-Z5555C Model Name: BOBDL00147A 10/25/2021 7:56:25 PM

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#### Member Primary Data

	Label	l Node	J Node	Rotate(deg)	Section/Shape	Туре	Design List	Material	Design Rule
1	M1	N1	N3		RIGID	None	None	RIGID	Typical
2	M2	N5	N8		Arms	Beam	Pipe	A500 Gr.C	Typical
3	M3	N2	N4		RIGID	None	None	RIGID	Typical
4	M4	N6	N7		Arms	Beam	Pipe	A500 Gr.C	Typical
5	M5	N8	N7		Bracing	VBrace	BAR	A572 Gr.50	Typical
6	M6	N5	N6		Bracing	VBrace	BAR	A572 Gr.50	Typical
7	M7	N6	N8		Bracing	VBrace	BAR	A572 Gr.50	Typical
8	M8	N1	N9		RIGID	None	None	RIGID	Typical
9	M9	N2	N10		RIGID	None	None	RIGID	Typical
10	M10	N16	N12		Frame Rails	Beam	Pipe	A500 Gr.C	Typical
11	M11	N15	N11		Frame Rails	Beam	Pipe	A500 Gr.C	Typical
12	M12	N7	N19	90	Plates	Beam	BAR	A572 Gr.50	Typical
13	M13	N8	N20	90	Plates	Beam	BAR	A572 Gr.50	Typical
14	M14	N4	N6	90	Plates	Beam	BAR	A572 Gr.50	Typical
15	M15	N3	N5	90	Plates	Beam	BAR	A572 Gr.50	Typical
16	M16	N21	N24		Arms	Beam	Pipe	A500 Gr.C	Typical
17	M17	N22	N23		Arms	Beam	Pipe	A500 Gr.C	Typical
18	M18	N24	N23		Bracing	VBrace	BAR	A572 Gr.50	Typical
19	M19	N21	N22		Bracing	VBrace	BAR	A572 Gr.50	Typical
20	M20	N22	N24		Bracing	VBrace	BAR	A572 Gr.50	Typical
21	M21	N23	N25	90	Plates	Beam	BAR	A572 Gr.50	Typical
22	M22	N24	N26	90	Plates	Beam	BAR	A572 Gr.50	Typical
23	M23	N10	N22	90	Plates	Beam	BAR	A572 Gr.50	Typical
24	M24	N9	N21	90	Plates	Beam	BAR	A572 Gr.50	Typical
25	M25	N28	N27		Stabilizer	HBrace	Pipe	A53 Gr.B	Typical
26	M26	N32	N30		RIGID	None	None	RIGID	Typical
27	M27	N29	N31		RIGID	None	None	RIGID	Typical
28	M28	N37	N38		Mount Pipes	Column	Pipe	A53 Gr.B	Typical
29	M29	N41	N42		Mount Pipes	Column	Pipe	A53 Gr.B	Typical
30	M30	N45	N46		Mount Pipes	Column	Pipe	A53 Gr.B	Typical
31	M31	N17	N39		RIGID	None	None	RIGID	Typical
32	M32	N18	N40		RIGID	None	None	RIGID	Typical
33	M33	N34	N44		RIGID	None	None	RIGID	Typical
34	M34	N33	N43		RIGID	None	None	RIGID	Typical
35	M35	N14	N36		RIGID	None	None	RIGID	Typical
36	M36	N13	N35		RIGID	None	None	RIGID	Typical
37	M37	N47	N48		Mount Pipes	Column	Pipe	A53 Gr.B	Typical

#### Material Take-Off

	Material	Size Pieces		Length[in]	Weight[K]	
1	General Members					
2	RIGID		12	37.3	0	
3	Total General		12	37.3	0	
4						
5	Hot Rolled Steel					
6	A500 Gr.C	PIPE_2.0X	6	421	0.18	
7	A53 Gr.B	PIPE_2.0	5	413	0.119	
8	A572 Gr.50	0.75" SR	6	259.6	0.033	
9	A572 Gr.50	3"x.5"	8	23.2	0.01	
10	Total HR Steel		25	1116.9	0.342	

#### Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rule	Area [in²]	lyy [in⁴]	Izz [in⁴]	J [in⁴]
1	Mount Pipes	PIPE_2.0	Column	Pipe	A53 Gr.B	Typical	1.02	0.627	0.627	1.25
2	Stabilizer	PIPE_2.0	HBrace	Pipe	A53 Gr.B	Typical	1.02	0.627	0.627	1.25
3	Bracing	0.75" SR	VBrace	BAR	A572 Gr.50	Typical	0.442	0.016	0.016	0.031
4	Arms	PIPE_2.0X	Beam	Pipe	A500 Gr.C	Typical	1.4	0.827	0.827	1.65



Company : Infinigy Engineering, PLLC Designer : DVA

Job Number : 2039-Z5555C Model Name: BOBDL00147A 10/25/2021 7:56:25 PM

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#### Hot Rolled Steel Section Sets (Continued)

	Label	Shape	Type	Design List	Material	Design Rule	Area [in²]	lyy [in⁴]	Izz [in⁴]	J [in⁴]
5	Frame Rails	PIPE_2.0X	Beam	Pipe	A500 Gr.C	Typical	1.4	0.827	0.827	1.65
6	Plates	3"x.5"	Beam	BAR	A572 Gr.50	Typical	1.5	0.031	1.125	0.112

#### Basic Load Cases

	BLC Description	Category	Y Gravity	Point	Distributed
1	Self Weight	DĽ	-1	8	
2	Wind Load AZI 0	WLX		16	78
3	Wind Load AZI 30	None		16	78
4	Wind Load AZI 60	None		16	78
5	Wind Load AZI 90	WLZ		16	78
6	Wind Load AZI 120	None		16	78
7	Wind Load AZI 150	None		16	78
8	Wind Load AZI 180	None		16	78
9	Wind Load AZI 210	None		16	78
10	Wind Load AZI 240	None		16	78
11	Wind Load AZI 270	None		16	78
12	Wind Load AZI 300	None		16	78
13	Wind Load AZI 330	None		16	78
14	Ice Weight	OL1		8	37
15	Ice Wind Load AZI 0	OL2		16	78
16	Ice Wind Load AZI 30	None		16	78
17	Ice Wind Load AZI 60	None		16	78
18	Ice Wind Load AZI 90	OL3		16	78
19	Ice Wind Load AZI 120	None		16	78
20	Ice Wind Load AZI 150	None		16	78
21	Ice Wind Load AZI 180	None		16	78
22	Ice Wind Load AZI 210	None		16	78
23	Ice Wind Load AZI 240	None		16	78
24	Ice Wind Load AZI 270	None		16	78
25	Ice Wind Load AZI 300	None		16	78
26	Ice Wind Load AZI 330	None		16	78
29	Service Live Loads	LL			
30	Maintenance Load 1	LL		1	
31	Maintenance Load 2	LL		1	
32	Maintenance Load 3	LL		1	
33	Maintenance Load 4	LL		1	
34	Maintenance Load 5	LL		1	
35	Maintenance Load 6	LL		1	

#### **Load Combinations**

	Description	Solve	PDelta	BLC	Factor	BLC	Factor	BLC	Factor
1	1.4DL	Yes	Y	1	1.4				
2	1.2DL + 1.6WL AZI 0	Yes	Y	1	1.2	2	1.6		
3	1.2DL + 1.6WL AZI 30	Yes	Y	1	1.2	3	1.6		
4	1.2DL + 1.6WL AZI 60	Yes	Υ	1	1.2	4	1.6		
5	1.2DL + 1.6WL AZI 90	Yes	Υ	1	1.2	5	1.6		
6	1.2DL + 1.6WL AZI 120	Yes	Υ	1	1.2	6	1.6		
7	1.2DL + 1.6WL AZI 150	Yes	Υ	1	1.2	7	1.6		
8	1.2DL + 1.6WL AZI 180	Yes	Υ	1	1.2	8	1.6		
9	1.2DL + 1.6WL AZI 210	Yes	Υ	1	1.2	9	1.6		
10	1.2DL + 1.6WL AZI 240	Yes	Υ	1	1.2	10	1.6		
11	1.2DL + 1.6WL AZI 270	Yes	Υ	1	1.2	11	1.6		
12	1.2DL + 1.6WL AZI 300	Yes	Υ	1	1.2	12	1.6		
13	1.2DL + 1.6WL AZI 330	Yes	Υ	1	1.2	13	1.6		
14	0.9DL + 1.6WL AZI 0	Yes	Y	1	0.9	2	1.6		
15	0.9DL + 1.6WL AZI 30	Yes	Υ	1	0.9	3	1.6		
16	0.9DL + 1.6WL AZI 60	Yes	Υ	1	0.9	4	1.6		



Company Designer : Infinigy Engineering, PLLC

: DVA

Job Number : 2039-Z5555C Model Name: BOBDL00147A 10/25/2021 7:56:25 PM

Checked By : \_\_\_

#### **Load Combinations (Continued)**

	oad Combinations (Continued)								
	Description	Solve	PDelta	BLC	Factor	BLC	Factor	BLC	Factor
17	0.9DL + 1.6WL AZI 90	Yes	Y	1	0.9	5	1.6		
18	0.9DL + 1.6WL AZI 120	Yes	Ý	1	0.9	6	1.6		
19	0.9DL + 1.6WL AZI 150	Yes	Y	1	0.9	7	1.6		
20	0.9DL + 1.6WL AZI 180	Yes	Y	1	0.9	8	1.6		
21	0.9DL + 1.6WL AZI 100	Yes	Y	1	0.9	9	1.6		
22	0.9DL + 1.6WL AZI 240	Yes	Y	1	0.9	10	1.6		
23	0.9DL + 1.6WL AZI 270	Yes	Y	1	0.9	11	1.6		
						12			
24	0.9DL + 1.6WL AZI 300	Yes	Y	1	0.9		1.6		
25	0.9DL + 1.6WL AZI 330	Yes	Y	1	0.9	13	1.6		
26	1.2D + 1.0Di	Yes	Y	1	1.2	14	1	4.5	
27	1.2D + 1.0Di +1.0Wi AZI 0	Yes	Υ	1	1.2	14	1	15	1
28	1.2D + 1.0Di +1.0Wi AZI 30	Yes	Υ	1	1.2	14	1	16	1
29	1.2D + 1.0Di +1.0Wi AZI 60	Yes	Υ	1	1.2	14	1	17	1
30	1.2D + 1.0Di +1.0Wi AZI 90	Yes	Υ	1	1.2	14	1	18	1
31	1.2D + 1.0Di +1.0Wi AZI 120	Yes	Υ	1	1.2	14	1	19	1
32	1.2D + 1.0Di +1.0Wi AZI 150	Yes	Y	1	1.2	14	1	20	1
33	1.2D + 1.0Di +1.0Wi AZI 180	Yes	Υ	1	1.2	14	1	21	1
34	1.2D + 1.0Di +1.0Wi AZI 210	Yes	Y	1	1.2	14	1	22	1
35	1.2D + 1.0Di +1.0Wi AZI 240	Yes	Υ	1	1.2	14	1	23	1
36	1.2D + 1.0Di +1.0Wi AZI 270	Yes	Υ	1	1.2	14	1	24	1
37	1.2D + 1.0Di +1.0Wi AZI 300	Yes	Y	1	1.2	14	1	25	1
38	1.2D + 1.0Di +1.0Wi AZI 330	Yes	Y	1	1.2	14	1	26	1
39	(1.2 + 0.2Sds)DL + 1.0E AZI 0	Yes	Y	1	1.2	27	1	28	
40	(1.2 + 0.2Sds)DL + 1.0E AZI 30	Yes	Y	1	1.2	27	0.866	28	0.5
41	(1.2 + 0.2Sds)DL + 1.0E AZI 60	Yes	Y	1	1.2	27	0.5	28	0.866
42	(1.2 + 0.2Sds)DL + 1.0E AZI 90	Yes	Y	1	1.2	27	0.5	28	1
43		Yes	Y	1	1.2	27	0.5	28	0.866
	(1.2 + 0.2Sds)DL + 1.0E AZI 120		Y		1.2		-0.5	28	
44	(1.2 + 0.2Sds)DL + 1.0E AZI 150	Yes	Y	1		27	-0.866		0.5
45	(1.2 + 0.2Sds)DL + 1.0E AZI 180	Yes		1	1.2	27	-1	28	0.5
46	(1.2 + 0.2Sds)DL + 1.0E AZI 210	Yes	Y	1	1.2	27	-0.866	28	-0.5
47	(1.2 + 0.2Sds)DL + 1.0E AZI 240	Yes	Y	1	1.2	27	-0.5	28	-0.866
48	(1.2 + 0.2Sds)DL + 1.0E AZI 270	Yes	Y	1	1.2	27		28	-1
49	(1.2 + 0.2Sds)DL + 1.0E AZI 300	Yes	Υ	1	1.2	27	0.5	28	-0.866
50	(1.2 + 0.2Sds)DL + 1.0E AZI 330	Yes	Υ	1	1.2	27	0.866	28	-0.5
51	(0.9 - 0.2Sds)DL + 1.0E AZI 0	Yes	Υ	1	0.9	27	1	28	
52	(0.9 - 0.2Sds)DL + 1.0E AZI 30	Yes	Υ	1	0.9	27	0.866	28	0.5
53	(0.9 - 0.2Sds)DL + 1.0E AZI 60	Yes	Υ	1	0.9	27	0.5	28	0.866
54	(0.9 - 0.2Sds)DL + 1.0E AZI 90	Yes	Υ	1	0.9	27		28	1
55	(0.9 - 0.2Sds)DL + 1.0E AZI 120	Yes	Υ	1	0.9	27	-0.5	28	0.866
56	(0.9 - 0.2Sds)DL + 1.0E AZI 150	Yes	Υ	1	0.9	27	-0.866	28	0.5
57	(0.9 - 0.2Sds)DL + 1.0E AZI 180	Yes	Υ	1	0.9	27	-1	28	
58	(0.9 - 0.2Sds)DL + 1.0E AZI 210	Yes	Υ	1	0.9	27	-0.866	28	-0.5
59	(0.9 - 0.2Sds)DL + 1.0E AZI 240	Yes	Y	1	0.9	27	-0.5	28	-0.866
60	(0.9 - 0.2Sds)DL + 1.0E AZI 270	Yes	Ý	1	0.9	27		28	-1
61	(0.9 - 0.2Sds)DL + 1.0E AZI 300	Yes	Y	1	0.9	27	0.5	28	-0.866
62	(0.9 - 0.2Sds)DL + 1.0E AZI 330	Yes	Y	1	0.9	27	0.866	28	-0.5
63	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 0	Yes	Y	1	1	2	0.008	29	1.5
64	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 30	Yes	Y	1	1	3	0.098	29	1.5
65	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 60	Yes	Y	1	1	4	0.098	29	1.5
66	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 90	Yes	Y	1	1	5	0.098	29	1.5
			Y						
67	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 120	Yes		1	1	6	0.098	29	1.5
68	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 150	Yes	Y	1	1	7	0.098	29	1.5
69	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 180	Yes	Y	1	1	8	0.098	29	1.5
70	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 210	Yes	Y	1	1	9	0.098	29	1.5
71	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 240	Yes	Υ	1	1	10	0.098	29	1.5
72	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 270	Yes	Υ	1	1	11	0.098	29	1.5
73	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 300	Yes	Υ	1	1	12	0.098	29	1.5
74	1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 330	Yes	Υ	1	1	13	0.098	29	1.5



Company : Infinigy Engineering, PLLC Designer : DVA

Job Number : 2039-Z5555C Model Name: BOBDL00147A 10/25/2021 7:56:25 PM Checked By : \_\_\_

#### Load Combinations (Continued)

	oad Combinations (Continued)								
	Description	Solve	PDelta	BLC	Factor	BLC	Factor	BLC	Factor
75	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 0	Yes	Y	1	1.2	34	1.5	2	0.156
76	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 30	Yes	Y	1	1.2	34	1.5	3	0.156
77	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 60	Yes	Y	1	1.2	34	1.5	4	0.156
78	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 90	Yes	Y	1	1.2	34	1.5	5	0.156
79	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 120	Yes	Y	1	1.2	34	1.5	6	0.156
80	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 150	Yes	Y	1	1.2	34	1.5	7	0.156
81	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 180	Yes	Υ	1	1.2	34	1.5	8	0.156
82	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 210	Yes	Υ	1	1.2	34	1.5	9	0.156
83	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 240	Yes	Υ	1	1.2	34	1.5	10	0.156
84	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 270	Yes	Y	1	1.2	34	1.5	11	0.156
85	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 300	Yes	Υ	1	1.2	34	1.5	12	0.156
86	1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 330	Yes	Υ	1	1.2	34	1.5	13	0.156
87	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 0	Yes	Y	1	1.2	35	1.5	2	0.156
88	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 30	Yes	Y	1	1.2	35	1.5	3	0.156
89	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 60	Yes	Y	1	1.2	35	1.5	4	0.156
90		Yes	Y	1	1.2	35	1.5	5	0.156
	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 90								
91	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 120	Yes	Y	1	1.2	35	1.5	6	0.156
92	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 150	Yes	Y	1	1.2	35	1.5	7	0.156
93	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 180	Yes	Υ	1	1.2	35	1.5	8	0.156
94	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 210	Yes	Υ	1	1.2	35	1.5	9	0.156
95	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 240	Yes	Υ	1	1.2	35	1.5	10	0.156
96	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 270	Yes	Y	1	1.2	35	1.5	11	0.156
97	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 300	Yes	Υ	1	1.2	35	1.5	12	0.156
98	1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 330	Yes	Y	1	1.2	35	1.5	13	0.156
99	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 0	Yes	Υ	1	1.2	36	1.5	2	0.156
100	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 30	Yes	Υ	1	1.2	36	1.5	3	0.156
101	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 60	Yes	Y	1	1.2	36	1.5	4	0.156
102	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 90	Yes	Y	1	1.2	36	1.5	5	0.156
103	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 120	Yes	Y	1	1.2	36	1.5	6	0.156
103	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 150	Yes	Y	1	1.2	36	1.5	7	0.156
105	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 180	Yes	Y	1	1.2	36	1.5	8	0.156
		Yes	Y		1.2	36	1.5		
106	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 210			1				9	0.156
107	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 240	Yes	Y	1	1.2	36	1.5	10	0.156
108	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 270	Yes	Y	1	1.2	36	1.5	11	0.156
109	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 300	Yes	Y	1	1.2	36	1.5	12	0.156
110	1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 330	Yes	Υ	1	1.2	36	1.5	13	0.156
111	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 0	Yes	Υ	1	1.2	37	1.5	2	0.156
112	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 30	Yes	Υ	1	1.2	37	1.5	3	0.156
113	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 60	Yes	Υ	1	1.2	37	1.5	4	0.156
114	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 90	Yes	Υ	1	1.2	37	1.5	5	0.156
115	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 120	Yes	Υ	1	1.2	37	1.5	6	0.156
116	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 150	Yes	Υ	1	1.2	37	1.5	7	0.156
117	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 180	Yes	Y	1	1.2	37	1.5	8	0.156
118	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 210	Yes	Y	1	1.2	37	1.5	9	0.156
119	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 240	Yes	Y	1	1.2	37	1.5	10	0.156
120	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 240	Yes	Y	1	1.2	37	1.5	11	0.156
121	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 300	Yes	Y	1	1.2	37	1.5	12	0.156
	1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 330		Y						0.156
122		Yes		1	1.2	37	1.5	13	
123	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 0	Yes	Y	1	1.2	38	1.5	2	0.156
124	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 30	Yes	Y	1	1.2	38	1.5	3	0.156
125	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 60	Yes	Υ	1	1.2	38	1.5	4	0.156
126	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 90	Yes	Υ	1	1.2	38	1.5	5	0.156
127	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 120	Yes	Υ	1	1.2	38	1.5	6	0.156
128	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 150	Yes	Υ	1	1.2	38	1.5	7	0.156
129	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 180	Yes	Y	1	1.2	38	1.5	8	0.156
130	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 210	Yes	Y	1	1.2	38	1.5	9	0.156
131	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 240	Yes	Υ	1	1.2	38	1.5	10	0.156
132	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 270	Yes	Ý	1	1.2	38	1.5	11	0.156
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Company : Infinigy Engineering, PLLC

Company : Infini Designer : DVA

Job Number : 2039-Z5555C Model Name : BOBDL00147A 10/25/2021 7:56:25 PM Checked By :

#### Load Combinations (Continued)

	Description	Solve	PDelta	BLC	Factor	BLC	Factor	BLC	Factor
133	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 300	Yes	Υ	1	1.2	38	1.5	12	0.156
134	1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 330	Yes	Υ	1	1.2	38	1.5	13	0.156
135	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 0	Yes	Υ	1	1.2	39	1.5	2	0.156
136	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 30	Yes	Υ	1	1.2	39	1.5	3	0.156
137	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 60	Yes	Υ	1	1.2	39	1.5	4	0.156
138	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 90	Yes	Υ	1	1.2	39	1.5	5	0.156
139	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 120	Yes	Υ	1	1.2	39	1.5	6	0.156
140	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 150	Yes	Υ	1	1.2	39	1.5	7	0.156
141	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 180	Yes	Υ	1	1.2	39	1.5	8	0.156
142	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 210	Yes	Υ	1	1.2	39	1.5	9	0.156
143	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 240	Yes	Υ	1	1.2	39	1.5	10	0.156
144	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 270	Yes	Υ	1	1.2	39	1.5	11	0.156
145	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 300	Yes	Υ	1	1.2	39	1.5	12	0.156
146	1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 330	Yes	Y	1	1.2	39	1.5	13	0.156

#### **Envelope Node Reactions**

	Node Label		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-in]	LC	MY [lb-in]	LC	MZ [lb-in]	LC
1	N2	max	345.594	15	874.41	31	575.416	91	1259.215	97	0	146	1120.071	38
2		min	-1056.274	9	296.526	24	-654.29	12	-856.58	6	0	1	277.953	19
3	N1	max	1010.376	27	554.981	37	370.964	6	806.156	95	0	146	811.734	35
4		min	-216.27	20	190.38	18	-553.536	97	-519.862	4	0	1	225.489	16
5	N28	max	482.897	24	18.468	31	149.231	24	0	146	0	146	0	146
6		min	-487.258	18	9.982	24	-150.729	18	0	1	0	1	0	1
7	Totals:	max	1103.253	14	1444.078	37	765.315	6						
8		min	-1103.253	8	510.183	18	-826.492	24						

#### Envelope AISC 14TH (360-10): LRFD Member Steel Code Checks

	Membei	Shape	Code Check	<pre><loc[in]lc< pre=""></loc[in]lc<></pre>	Shear Check	Loc[in]	DirL	_Ср	hi*Pnc [ <b>l</b> b]	phi*Pnt [lb]	phi*Mn y-y [lb-in]	phi*Mn z-z [lb-in]	Cb Eqn
1	M28	PIPE_2.0	0.192	66 37	0.032	30	3	31/1	14916.096	32130	22459.5	22459.5	3 H1-1b
2	M29	PIPE_2.0	0.19	66 31	0.034	30	3	37 1	14916.096	32130	22459.5	22459.5	2.126 H1-1b
3	M11	PIPE_2.0X		60 34	0.04	10	1	12 1	12974.268	57960	39909.6	39909.6	1.908 H1-1b
4	M10	PIPE_2.0X	0.175	60 38	0.024	12.5	2	29 1	12974.268	57960	39909.6	39909.6	1.893 H1-1b
5	M23	3"x.5"	0.129	0 32	0.051	0	y 1	12 6	64929.826	67500	8460	50625	1.179 H1-1b
6	M14	3"x.5"	0.116	0 88	0.039	0.38	у	6 6	64929.826	67500	8460	50625	1.036 H1-1b
7	M12	3"x.5"	0.101	0 98	0.053	2.5	y 3	32 6	6023.816	67500	8460	50625	1.672 H1-1b
8	M22	3"x.5"	0.093	0 32	0.083	2.5	у 3	386	6023.816	67500	8460	50625	1.149 H1-1b
9	M24	3"x.5"	0.092	0 38	0.032	0.38	y 1	106	64929.826	67500	8460	50625	1.186 H1-1b
10	M13	3"x.5"	0.089	0 34	0.056	2.5	y 2	296	6023.816	67500	8460	50625	1.62 H1-1b
11	M21	3"x.5"	0.082	0 29	0.074	2.5	y 3	346	6023.816	67500	8460	50625	1.667 H1-1b
12	M15	3"x.5"	0.081	0 95	0.037	3.313	y 3	31/6	64929.826	67500	8460	50625	1.033 H1-1b
13	M30	PIPE_2.0	0.07	66 12	0.026	66	1	13 1	14916.096	32130	22459.5	22459.5	2.609 H1-1b
14	M5	0.75" SR	0.068	0 98	0.005	36		6	5691.919	19890	3072	3072	2.077H1-1b*
15	M18	0.75" SR	0.06	0 28	0.006	36		6	5691.919	19890	3072	3072	2.275H1-1b*
16	M6	0.75" SR	0.049	0 95	0.006	0	1	12	5691.919	19890	3072	3072	2.348H1-1b*
17	M7	0.75" SR	0.049	57.82438	0.003	57.824	1	12 ;	2206.248	19890	3072	3072	2.623 H1-1b
18	M20	0.75" SR	0.048	57.82429	0.003	57.824		4 :	2206.248	19890	3072	3072	2.184 H1-1b
19	M19	0.75" SR	0.046	0 29	0.006	0	1	12	5691.919	19890	3072	3072	2.254H1-1b*
20	M25	PIPE_2.0	0.041	38.498 12	0.003	76.996		6 1	19612.716	32130	22459.5	22459.5	1.136 H1-1b
21	M16	PIPE_2.0X	0.036	22.625 28	0.017	45.25	3	37 4	15905.544	57960	39909.6	39909.6	1.465 H1-1b
22	M2	PIPE_2.0X	0.027	45.25 98	0.009	45.25	3	314	15905.544	57960	39909.6	39909.6	2.533 H1-1b
23	M17	PIPE_2.0X	0.024	0 6	0.015	45.25	3	344	15905.544	57960	39909.6	39909.6	1.408 H1-1b
24	M37	PIPE_2.0	0.022	42 4	0.021	6	1	122	26521.424	32130	22459.5	22459.5	2.148 H1-1b
25	M4	PIPE_2.0X	0.021	45.25 95	0.01	45.25	3	31/4	15905.544	57960	39909.6	39909.6	2.42 H1-1b



### FROM ZERO TO INFINIGY

#### the solutions are endless

#### **BOLT CONNECTION CALCULATION**

#### **BOLT PROPERTIES**

Date:	10/25/2021
Site:	BOBDL00147A
Engineer:	DVA
Job No:	2039-Z5555C
Connection Location:	Mount to Tower

Bolt Capacity Equation	TIA-222-G
Connection Type	Steel
Bolt Size, <b>d</b>	1/2
Threads per Inch, <b>n</b>	13
Steel Grade	A307
Bolt Ultimate Tensile Stress, <b>F</b> <sub>u</sub>	60
Threads Exclusion	N
Shear Plane	1

Net Bolt Cross-Sectional Area,  $\mathbf{An}$  Gross Bolt Cross-Sectional Area,  $\mathbf{Ag}$  Tensile Steel Strength (per bolt),  $\mathbf{\phi R}_{nt}$  Shear Steel Strength (per bolt),  $\mathbf{\phi R}_{nv}$ 

0.142	in <sup>2</sup>
0.196	in <sup>2</sup>
6385	lbs
3976	lbs

in

ksi



# FROM ZERO TO INFINIGY the solutions are endless

# BOLT CONNECTION CALCULATION BOLT GROUP CHECK

10/25/2021 BOBDL00147A DVA 2039-25555C Mount to Tower
---

**Bolt Group Pattern** 

	70	Loads Properties			
Controlling LC:	31				
Load Point Number:	N2				
X-Coordinate (in.)	4.00				
Y-Coordinate (in.)	2.00				
Z-Coordinate (in.)	2.00				
Shear Load, Px (lbs)	-22.000	0	0	0	0
Shear Load, Py (lbs)	-874.000	0	0	0	0
Axial Load, Pz (lbs)	863,000	0	0	0	0
Moment, Mx (Ib-in)	1078,000	0	0	0	0
Moment, My (Ib-in)	000'0	0	0	0	0
Moment, Mz (Ib-in)	269,000	0	0	0	0

Memt	Member Properties	
	X	٨
Start Coordinates:	0.0	0.0
Dimentions:	8.0	4.0

•					
	4				
		Bolt Coo	Bolt Coordinates	Bol	Bolt Loads
No.	Bolt Type	Xo (in)	Yo (in)	Axial (Ibs)	Shear
_	Main Type	1.00	1.00	-494.42	162.
2	Main Type	2.00	3.00	925.92	276.
က	Main Type	1.00	3.0	918.58	161.
4	Main Tyne	2 00	10	-487 08	277

Number of Bolts

Max. Capacity

Combined

Steel Bolt Usage Shear 4.1%

Tension

14.5% %0.0

Shear (Ibs) 162.71 276.52 161.41

6.0

4.0

2.0

0.0

\*

3.5 3.0 3.0 2.5 2.0 1.0 0.5

14.5% 14.4%

4.1% 14.5% 14.4% 7.0%

7.0%

%0:0

277.28

erties:	. <b>Ľ</b>	.⊑	in.^2	in.^2	in ^2	
<b>Bolt Group Properties:</b>	4.00	2.00	7.07	0.79	7.85	
	Xc =	Yc =	C.y =	II X O	c.xy =	

Bolt Group:	sql	sql	sql	lb-in	lb-in	. <u>c</u>
Loads at Center of Gravity of Bolt Group:	863.00	-22.00	-874.00	2826.00	-44.00	00 692
Loads at Ce	Pz =	Px =	Py =	M×=	My =	M2 =

Total Capacity of Bolt Group:

14.5%

å

# Exhibit F

**Power Density/RF Emissions Report** 



# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

Dish Wireless Existing Facility

Site ID: BOBDL00147A

BOBDL00147A 109 Schofield Road Willington, Connecticut 06279

October 6, 2021

EBI Project Number: 6221005579

Site Comp	liance Summary
Compliance Status:	COMPLIANT
Site total MPE% of FCC general population allowable limit:	1.42%



October 6, 2021

Dish Wireless

Emissions Analysis for Site: BOBDL00147A - BOBDL00147A

EBI Consulting was directed to analyze the proposed Dish Wireless facility located at 109 Schofield Road in Willington, Connecticut for the purpose of determining whether the emissions from the Proposed Dish Wireless Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu$ W/cm²). The number of  $\mu$ W/cm² calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu$ W/cm²). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately 400  $\mu$ W/cm² and 467  $\mu$ W/cm², respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 11 GHz frequency bands is 1000  $\mu$ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure.



Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

#### CALCULATIONS

Calculations were done for the proposed Dish Wireless antenna facility located at 109 Schofield Road in Willington, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since Dish Wireless is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 20 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 4 n7l channels (600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) 4 n70 channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 3) 4 n66 channels (AWS Band 2190 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 5) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 20 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative



estimate as gain reductions for these particular antennas are typically much higher in this direction.

- 6) The antennas used in this modeling are the JMA MX08FRO665-21 for the 600 MHz / 1900 MHz / 2190 MHz channel(s) in Sector A, the JMA MX08FRO665-21 for the 600 MHz / 1900 MHz / 2190 MHz channel(s) in Sector B, the JMA MX08FRO665-21 for the 600 MHz / 1900 MHz / 2190 MHz channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 20 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 7) The antenna mounting height centerline of the proposed antennas is 135 feet above ground level (AGL).
- 8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
- 9) Emissions from additional carriers were not included because there were no other carriers listed in the Connecticut Siting Council active database.
- 10) All calculations were done with respect to uncontrolled / general population threshold limits.



# **Dish Wireless Site Inventory and Power Data**

Sector:	Α	Sector:	В	Sector:	С
Antenna #:	I	Antenna #:	I	Antenna #:	I
Make / Model:	JMA MX08FRO665- 21	Make / Model:	JMA MX08FRO665- 21	Make / Model:	JMA MX08FRO665- 21
Frequency Bands:	600 MHz / 1900 MHz / 2190 MHz	Frequency Bands:	600 MHz / 1900 MHz / 2190 MHz	Frequency Bands:	600 MHz / 1900 MHz / 2190 MHz
Gain:	17.45 dBd / 22.65 dBd / 22.65 dBd	Gain:	17.45 dBd / 22.65 dBd / 22.65 dBd	Gain:	17.45 dBd / 22.65 dBd / 22.65 dBd
Height (AGL):	135 feet	Height (AGL):	135 feet	Height (AGL):	135 feet
Channel Count:	12	Channel Count:	12	Channel Count:	12
Total TX Power (W):	440 Watts	Total TX Power (W):	440 Watts	Total TX Power (W):	440 Watts
ERP (W):	5,236.31	ERP (W):	5,236.31	ERP (W):	5,236.31
Antenna A1 MPE %:	1.42%	Antenna B1 MPE %:	1.42%	Antenna C1 MPE %:	1.42%

Site Composite MPE %	
Carrier	MPE %
Dish Wireless (Max at Sector A):	1.42%
no additional carriers	N/A
Site Total MPE % :	1.42%

Dish Wireless MPE % Per Sector					
Dish Wireless Sector A Total:	1.42%				
Dish Wireless Sector B Total: 1.42%					
Dish Wireless Sector C Total: 1.42%					
·					
Site Total MPE % : 1.42%					

Dish	Wirele	ess Maxir	num	MPE Pow	er Values (S	ector A)	
Dish Wireless Frequency Band / Technology (Sector A)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (µW/cm²)	Frequency (MHz)	Allowable MPE (μW/cm²)	Calculated % MPE
Dish Wireless 600 MHz n71	4	223.68	135.0	1.93	600 MHz n71	400	0.48%
Dish Wireless 1900 MHz n70	4	542.70	135.0	4.69	1900 MHz n70	1000	0.47%
Dish Wireless 2190 MHz n66	4	542.70	135.0	4.69	2190 MHz n66	1000	0.47%
	•					Total:	1.42%

<sup>•</sup> NOTE: Totals may vary by approximately 0.01% due to summation of remainders in calculations.



#### **Summary**

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the Dish Wireless facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

Dish Wireless Sector	Power Density Value (%)		
Sector A:	1.42%		
Sector B:	1.42%		
Sector C:	1.42%		
Dish Wireless Maximum MPE % (Sector A):	1.42%		
Site Total:	1.42%		
Site Compliance Status:	COMPLIANT		

The anticipated composite MPE value for this site assuming all carriers present is **1.42%** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

# Exhibit G

# **Letter of Authorization**



October 26, 2021

CT - CONNECTICUT SITING COUNCIL

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

#### Re: TARPON TOWERS II, LLC - LETTER OF AUTHORIZATION

Tower Share Application, Tarpon Towers II, LLC Telecommunications Site at: 109 SCHOFIELD ROAD, WILLINGTON, TOLLAND COUNTY, CONNECTICUT 06279

Tarpon Towers II, LLC ("Tarpon") hereby authorizes DISH Wireless LLC, including their Agent, to act as our Agent in the processing of all zoning applications, building permits and approvals through the CT - CONNECTICUT SITING COUNCIL for the existing wireless communications site described below:

Tarpon ID/Name: CT1010 Willington

Customer Site ID: BOBDL00147A / TAR- Schofield Road

Site Address: 109 SCHOFIELD ROAD, WILLINGTON, TOLLAND COUNTY,

**CONNECTICUT -06279** 

Tarpon Towers II, LLC

Name: Brett Buggeln

Title: COO

Date: October 26, 2021

# Exhibit H

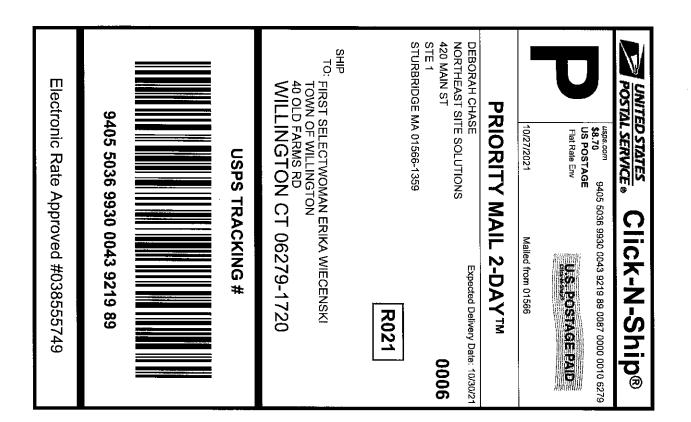
**Recipient Mailings** 

# 60000L00147A



UNIONVILLE 24 MILL ST UNIONVILLE, CT 06085-9998 (800)275-8777

10/27/2021	(800)2/5-0	111	02:01 PM
Product	Qty	Unit Price	Price
Prepaid Mail Bradenton, Weight: 0 1 Acceptance Wed 10, Tracking #	b 2.uu oz		\$0.00 30
Weight: 0 Acceptance Wed 10	1 CT 06279 1b 11.80 o Date: 0/27/2021 1: 5036 9930 0		\$0.00 09
Weight: 0 Acceptanc Wed 1	1 n, CT 06279 lb 11.70 e Date: 0/27/2021 #: 5036 9930 (	OZ	\$0.00 88
Weight: ( Acceptand Wed Tracking 9405	10/27/2021 #: 5036 9930	0043 921	
Grand Total:			\$0,00





#### Instructions

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Trans. #: Print Date: Ship Date: Expected

Delivery Date:

546869888 10/26/2021 10/27/2021 10/30/2021 Priority Mail® Postage: \$8.70
Total: \$8.70

From: DEBORAH CHASE

NORTHEAST SITE SOLUTIONS

420 MAIN ST

STE 1

STURBRIDGE MA 01566-1359

To: FIRST SELECTWOMAN ERIKA WIECENSKI

TOWN OF WILLINGTON 40 OLD FARMS RD

WILLINGTON CT 06279-1720

\* Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date.

**UNITED STATES**POSTAL SERVICE
Thank you for shipping with the United States Postal Service!
Check the status of your shipment on the USPS Tracking® page at usps.com





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#### Click-N-Ship® Label Record

# USPS TRACKING # : 9405 5036 9930 0043 9219 96

Trans. #: Print Date: Ship Date: Expected

Delivery Date:

546869888 10/26/2021 10/27/2021 10/30/2021 Priority Mail® Postage:

\$8.70 \$8.70

From:

DEBORAH CHASE

NORTHEAST SITE SOLUTIONS

420 MAIN ST

STE 1

STURBRIDGE MA 01566-1359

To:

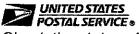
MICHAEL D'AMATO

ZONING AGENT- TOWN OF WILLINGTON

40 OLD FARMS RD

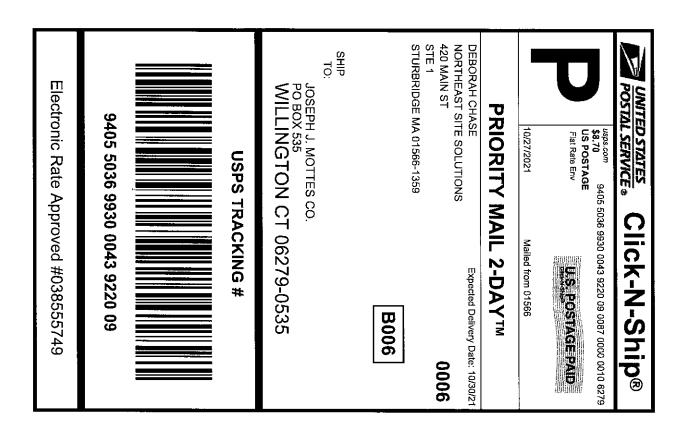
WILLINGTON CT 06279-1720

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- 5. Mail your package on the "Ship Date" you selected when creating this label.

#### Click-N-Ship® Label Record

# USPS TRACKING #: 9405 5036 9930 0043 9220 09

Trans. #: Print Date: Ship Date: Expected

Delivery Date:

546869888 10/26/2021 10/27/2021 10/30/2021 Priority Mail® Postage:

\$8.70

From:

DEBORAH CHASE

NORTHEAST SITE SOLUTIONS

420 MAIN ST

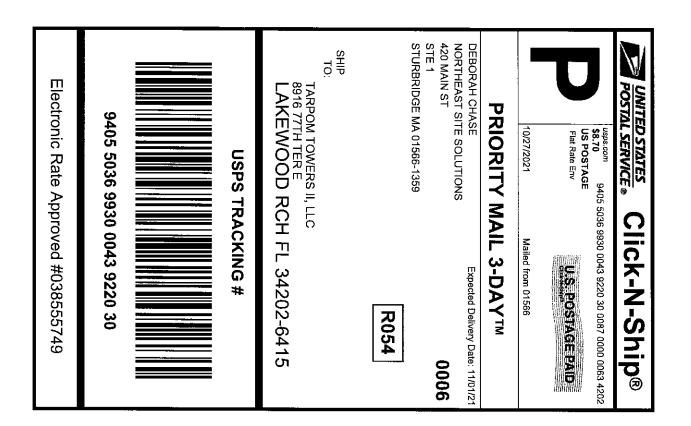
STE 1 STURBRIDGE MA 01566-1359

0.010110001000100

To: JOSEPH J. MOTTES CO. PO BOX 535

WILLINGTON CT 06279-0535

\* Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date.





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- 5. Mail your package on the "Ship Date" you selected when creating this label.

#### Click-N-Ship® Label Record

#### **USPS TRACKING #:** 9405 5036 9930 0043 9220 30

Trans. #: Print Date: Ship Date: Expected

Delivery Date:

546869888 10/26/2021 10/27/2021 11/01/2021 Priority Mail® Postage: \$8.70 \$8.70 Total:

From: DEBORAH CHASE

NORTHEAST SITE SOLUTIONS

420 MAIN ST

STE 1

STURBRIDGE MA 01566-1359

TARPOM TOWERS II, LLC

8916 77TH TER F

LAKEWOOD RCH FL 34202-6415

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