## Transcend Wireless

June 26, 2019

Members of the Siting Council
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

RE: Notice of Exempt Modification
75 Wells Road, Wethersfield, CT 06109
Latitude: 41.7058800000
Longitude: -72.66333000000
T-Mobile Site\#: CTHA506A - L600

Dear Ms. Bachman:

T-Mobile currently maintains six (6) antennas at the 95 -foot level of the existing 101-foot monopole at 75 Wells Road, Wethersfield, CT. The 101-foot monopole is owned and operated by Everest Infrastructure Partners. The property is owned by Frontier Communications. T-Mobile now intends to remove three (3) of its existing antennas and add six (6) new $600 / 700 / 1900 / 2100 \mathrm{MHz}$ antennas. The new antennas will be installed at the same 95 -foot level of the tower.

## Planned Modifications:

Tower:

Remove
N/A

Remove and Replace:
(3) AIR 21 B4A/B12P (Remove) - (3) AIR 32 KRD901146-1 B66A B2A Antenna (Replace) 1900/2100 MHz
(3) RRUS11B12 (Remove) - Radio 4449 B71+B12 (Replace)

Install New:
(3) APXVAARR24_43-U-NA20 Antenna $600 / 700 \mathrm{MHz}$
(3) 1-3/8" Hybrid Cables

Handrail Kit on Antenna Mounts

Existing to Remain:
(3) AIR 21 KRC1180121_B2P/B4A Antenna 2100 MHz
(2) 1-3/8" Hybrid Cable

This facility has been approved by the Council in Petition No. 1012 dated 12/1/2011. This modification complies with this approval. Please see the enclosed.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies§ 16-SOj-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.SA. § 16-SOj-73, a copy of this letter is being sent to Mayor-Amy Bello, Elected Official, and Peter Gillespie, Director of Planning \& Economic Development for the Town of Wethersfield, as well as the tower owner and property owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S;A. § 16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

## Kyle Richers

Transcend Wireless
Cell: 908-447-4716
Email: krichers@transcendwireless.com

## Attachments

cc: Amy Bello - Town of Wethersfield Mayor
Peter Gillespie- Town of Wethersfield Director of Planning \& Economic Development
Everest Infrastructure Partners - Tower Owner
Frontier Communications- Property Owner

## From:

Sent:
To:
Subject:

UPS Quantum View [pkginfo@ups.com](mailto:pkginfo@ups.com)
Wednesday, June 26, 2019 9:05 AM
krichers@transcendwireless.com
UPS Ship Notification, Reference Number 1: CTHA506A CSC ZO

## $\times$

## You have a package coming.

Scheduled Delivery Date: Thursday, 06/27/2019

This message was sent to you at the request of TRANSCEND WIRELESS to notify you that the shipment information below has been transmitted to UPS. The physical package may or may not have actually been tendered to UPS for shipment. To verify the actual transit status of your shipment, click on the tracking link below.

## Shipment Details

| From: | TRANSCEND WIRELESS |
| :---: | :---: |
| Tracking Number: | 1ZV257424292677964 |
| Ship To: | Peter Gillespie <br> Town of Wethersfield 505 Silas Deane Highway <br> WETHERSFIELD, CT 061092216 US |
| UPS Service: | UPS GROUND |
| Number of Packages: | 1 |
| Scheduled Delivery: | 06/27/2019 |
| Signature Required: | A signature is required for package delivery |
| Weight: | 1.0 LBS |
| Reference Number 1: | CTHA506A CSC ZO |
|  |  |
| x Download the UPS mobile app |  |

## From:

Sent:
To:
Subject:

UPS Quantum View [pkginfo@ups.com](mailto:pkginfo@ups.com)
Wednesday, June 26, 2019 9:08 AM
krichers@transcendwireless.com
UPS Ship Notification, Reference Number 1: CTHA506A CSC EO

## $\times$

## You have a package coming.

Scheduled Delivery Date: Thursday, 06/27/2019

This message was sent to you at the request of TRANSCEND WIRELESS to notify you that the shipment information below has been transmitted to UPS. The physical package may or may not have actually been tendered to UPS for shipment. To verify the actual transit status of your shipment, click on the tracking link below.

## Shipment Details

| From: | TRANSCEND WIRELESS |
| :---: | :---: |
| Tracking Number: | 1ZV257424293867971 |
| Ship To: | Amy Bello <br> Town of Wethersfield Mayor's Office 505 Silas Deane Highway WETHERSFIELD, CT 061092216 US |
| UPS Service: | UPS GROUND |
| Number of Packages: | 1 |
| Scheduled Delivery: | 06/27/2019 |
| Signature Required: | A signature is required for package delivery |
| Weight: | 1.0 LBS |
| Reference Number 1: | CTHA506A CSC EO |
|  |  |
| Download the UPS mobile app |  |

## From:

Sent:
To:
Subject:

UPS Quantum View [pkginfo@ups.com](mailto:pkginfo@ups.com)
Wednesday, June 26, 2019 9:11 AM
krichers@transcendwireless.com
UPS Ship Notification, Reference Number 1: CTHA506A CSC PO

## $\times$

## You have a package coming.

Scheduled Delivery Date: Thursday, 06/27/2019

This message was sent to you at the request of TRANSCEND WIRELESS to notify you that the shipment information below has been transmitted to UPS. The physical package may or may not have actually been tendered to UPS for shipment. To verify the actual transit status of your shipment, click on the tracking link below.

## Shipment Details

| From: | TRANSCEND WIRELESS |
| :---: | :---: |
| Tracking Number: | 1ZV257424291061988 |
| Ship To: | Frontier Communications 401 Merritt 7 <br> NORWALK, CT 068511000 US |
| UPS Service: | UPS GROUND |
| Number of Packages: | 1 |
| Scheduled Delivery: | 06/27/2019 |
| Signature Required: | A signature is required for package delivery |
| Weight: | 1.0 LBS |
| Reference Number 1: | CTHA506A CSC PO |
|  | $\square$ |
| $x$ Download the UPS mobile app |  |

## From:

Sent:
To:
Subject:

UPS Quantum View [pkginfo@ups.com](mailto:pkginfo@ups.com)
Wednesday, June 26, 2019 9:15 AM
krichers@transcendwireless.com
UPS Ship Notification, Reference Number 1: CTHA506A CSC TO

## x

## You have a package coming.

Scheduled Delivery Date: Friday, 06/28/2019

This message was sent to you at the request of TRANSCEND WIRELESS to notify you that the shipment information below has been transmitted to UPS. The physical package may or may not have actually been tendered to UPS for shipment. To verify the actual transit status of your shipment, click on the tracking link below.

## Shipment Details

| From: | TRANSCEND WIRELESS |
| :---: | :---: |
| Tracking Number: | 1ZV257424290859995 |
| Ship To: | Everest Infrastructure Partners 1435 Bedford Avenue Suite 108 PITTSBURGH, PA 152193675 US |
| UPS Service: | UPS GROUND |
| Number of Packages: | 1 |
| Scheduled Delivery: | 06/28/2019 |
| Signature Required: | A signature is required for package delivery |
| Weight: | 1.0 LBS |
| Reference Number 1: | CTHA506A CSC TO |
|  | $\square$ |
| x Download the UPS mobile app |  |

The Assessor's office is responsible for the maintenance of records on the ownership of properties. Assessments are computed at 70\% of the estimated market value of real property at the time of the last revaluation which was 2018.


Information on the Property Records for the Municipality of Wethersfield was last updated on 5/22/2019.

## Parcel Information

| Location: | 75 WELLS RD | Property Use: | Industrial | Primary Use: | Utility Building |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Unique ID: | 205069 | Map Block <br> Lot: | 205069 | Acres: | 0.90 |
| 490 Acres: | 0.00 | Zone: | SRD/A | Volume / | Page: |

## Value Information

|  | Appraised Value | Assessed Value |
| :--- | :--- | :--- |
| Land | 371,250 | 259,870 |
| Buildings | 435,101 | 304,570 |
| Detached Outbuildings | 686,169 | 480,320 |
| Total | $1,492,520$ | $1,044,760$ |

## Owner's Information

| Owner's Data |
| :---: | :---: |
| SOUTHERN N E TELEPHONE CO |
| C/O FRONTIER COMMUNICATIONS |
| 401 MERRITT 7 |
| TAX DEPT |

Building 1


| Category: | Industrial | Use: | Utility Building | GLA: | 14,497 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Stories: | 2.00 | Construction: | Masonry | Year Built: | 1939 |


| Heating: | Hot Water | Fuel: | Oil | Cooling <br> Percent: | 100 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Siding: | Brick/Pre-Finish Metal | Roof Material: | Tar and Gravel | Beds/Units: | 0 |

## Special Features

## Attached Components

| Type: | Year Built: | Area: |
| :--- | :--- | :--- |
| Unfinished Area | 1939 | 2,160 |

## Detached Outbuildings

| Type: | Year Built: | Length: | Width: | Area: |
| :--- | :--- | :--- | :--- | :--- |
| PreCastConCel | 2003 | 200.00 | 0.00 | 200 |
| Paving | 1999 | 0.00 | 0.00 | 2,400 |
| Cell Tower | 2000 | 0.00 | 0.00 | 1 |

Owner History-Sales

| Owner Name | Volume | Page | Sale Date | Deed Type | Valid Sale | Sale Price |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| SOUTHERN N E TELEPHONE CO | 0121 | 0472 | $11 / 30 / 1946$ |  | No | \$0 |

## Building Permits

| Permit <br> Number | Permit Type | Date <br> Opened | Date <br> Closed | Permit <br> Status | Reason |
| :--- | :--- | :--- | :--- | :--- | :--- |
| B-17-502 | Miscellaneous | $10 / 11 / 2018$ |  | Closed | CELL TOWER WORK (AT\&T) |


| Permit <br> Number | Permit Type | Date Opened | Date <br> Closed | Permit <br> Status | Reason |
| :---: | :---: | :---: | :---: | :---: | :---: |
| B-16-545 | Comm <br> Renovations | 11/08/2016 |  | Permit Issued | REMOVE 3 ANTENNA AND REPL WITH 3 NEWER MODELS. ADD 2 NEW RRUS PER SECTOR FOR 6 TOTAL. ADD 1 DC6 S |
| B-16-552 | Comm <br> Renovations | 11/04/2016 |  | Permit Issued | REPL EXISTING 6201 CABINET W/ NEW 6131 CABINET. ADD 6 NEW COAX LINES \& 1 NEW HYBRID. REPL 3 EXIST |
| E-15-251 | Electrical | 07/20/2015 |  | Permit <br> Issued | INSTALL NEW 200 AMP METER \& NEW ELECTRICAL FOR TMOBILE CABINET W/ PIPING \& FIBER |
| E-15-284 | Electrical | 07/20/2015 |  | Permit Issued | INSTALL SURFACE MOUNT FEED IN RIGID PIPE FROM METER TO NEW PPC CABINET |
| B-15-26 | Comm <br> Renovations | 03/05/2015 |  | Permit <br> Issued | 16x10 CONCRETE PAD, ANTENNA T ANN MOUNTING TO EXISTING TOWER. 16 NEW ANTENNAS, 8' HIGH ICE BRIDGE, |
| E-13-8 | Electrical | 01/14/2013 |  | Permit <br> Issued | INSTALL NEW 200 AMP PANEL ON EXISTING METER CAN |
| M-10-24 | HVAC | 07/28/2010 |  | Permit Issued | Replace existing a/c split sys. \& ductwork |
| B-10-119 | Other | 07/08/2010 |  | Permit <br> Issued | Instsall reinforcement to existing 101.5' monopole tower. |
| MP-0199 | HVAC | 12/23/2009 |  | Permit <br> Issued | Install 3 split a/c systems \& ducts on roof |
| EP-0227 | Electrical | 09/10/2009 |  | Permit <br> Issued | Wiring for new ac and controls |
| MP-0075 | HVAC | 06/03/2009 |  | Permit <br> Issued | Replace air cond. unit |
| BP06840 | Comm <br> Renovations | 12/28/2006 |  | Permit Issued | Change Cellular antennas |
| BP03629 | Comm <br> Renovations | 10/10/2003 |  | Permit <br> Issued | Foundation for generator |
| EP03344 | Electrical | 10/03/2003 |  | Permit <br> Issued | Install generator |
| MP03041 | HVAC | 04/29/2003 |  | Permit <br> Issued | Install 2 A/C units |
| EP03086 | Electrical | 04/11/2003 |  | Permit Issued | Wire $A / C-2 n d f l$ |


| Permit <br> Number | Permit Type | Date Opened | Date Closed | Permit <br> Status | Reason |
| :---: | :---: | :---: | :---: | :---: | :---: |
| EP03066 | Electrical | 03/17/2003 |  | Permit Issued | Wire A/C per plan |
| BP0356 | Comm <br> Renovations | 02/12/2003 |  | Permit Issued | Revamp 1st fl |
| MP02202 | HVAC | 12/31/2002 |  | Permit Issued | A/C-computer rm |
| BP02824 | Comm <br> Renovations | 12/05/2002 |  | Permit Issued | Partial demolition-CMU unit |
| BP02626 | Comm <br> Renovations | 09/23/2002 |  | Permit Issued | 6X10.4 concrete pad \& antennas |
| MP01030 | HVAC | 02/12/2001 |  | Permit Issued | Trane A/C |
| EP000415 | Electrical | 11/15/2000 |  | Permit Issued | 1200 amp service |
| EP000416 | Electrical | 11/15/2000 |  | Permit Issued | Repl tank level system |
| EP000246 | Electrical | 06/29/2000 |  | Permit Issued | Telecom Install |
| MP990137 | HVAC | 09/09/1999 |  | Permit Issued | INSTALL AIR HANDLER \& COOLING UNIT |
| EP990184 | Electrical | 06/25/1999 |  | Permit Issued |  |
| BP990306 | Comm <br> Renovations | 06/21/1999 |  | Permit Issued |  |
| 8737 | Comm <br> Renovations | 10/26/1998 |  | Permit Issued |  |

Information Published With Permission From The Assessor


Petition No. 1012<br>MetroPCS<br>75 Wells Road, Wethersfield, Connecticut<br>Staff Report<br>December 1, 2011

On October 26, 2011, the Connecticut Siting Council (Council) received a petition (Petition) from MetroPCS for a declaratory ruling that no Certificate of Environmental Compatibility and Public Need is required for the proposed modifications to an existing telecommunications facility at 75 Wells Road in Wethersfield. Specifically, MetroPCS seeks to co-locate on an existing 104-foot tall monopole owned by New Cingular Wireless PCS LLC (AT\&T). The existing tower, located adjacent to the east side of an existing building, currently supports AT\&T. T-Mobile and Verizon have existing leases for tower space but have not located on the tower to date.

MetroPCS seeks to install six panel antennas on $t$-arms at the 75 -foot level of the tower. The tower and foundation would require modifications to support the new equipment.

MetroPCS would install three equipment cabinets adjacent to the existing fenced compound area. The ground equipment would require MetroPCS to expand the existing compound and lease area to the south. The new fenced area would extend 17 feet to the south, then angle 12 feet to the west, terminating at the existing building. The new fence would match the existing. Three new plantings would be installed along the east side of the new fenced area to screen views from Wells Road and Savage Road. Staff recommends one additional evergreen planting along the south side of the compound extension to provide further screening.

There are no wetlands at the site. One evergreen shrub would be removed. The addition of new plantings along the fence line of the compound expansion area would mitigate views of the compound from the south and east. Evergreens along the east side and north side of the existing compound would remain. The maximum worst-case power density including AT\&T's existing and T-Mobile's and Verizon's proposed equipment, would be 53 percent of the applicable limit.


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## GENERAL NOTES:

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14. SHHP Commectons Stall be weloed or hich strenth botieo.











## Rigorous Structural Analysis Report

## T- "Mobile

# T-Mobile - Wethersfield Site \#CTHA506A Owner: Everest Infrastructure - Wethersfield CO Site Wethersfield, Connecticut 

May 13, 2019

MEI Project ID: CT04861M-19V1

MALOUF ENGINEERING INTL.,INC.


STRUCTURAL CONSULTANTS

ACEC
mexiside

May 13, 2019

Mr. Kyle Richers
Transcend Wireless
Mahwah, NJ 04730

RIGOROUS STRUCTURAL ANALYSIS

| Structure/Make/Model: | 101 ft Monopole | Not Known / 18-Sided |
| :--- | :--- | :--- |
| Client/Site Name/\#: | Transcend Wireless \|T-Mobile | Wethersfield \#CTHA506A |
| Owner/Site Name/\#: | Everest Infrastructure | Wethersfield CO |
| MEI Project ID: | CT04861M-19V1 |  |
| Location: | 75 Wells Rd | Hartford County |
|  | Wethersfield, Connecticut 06109 | FCC \#1200438 |
|  | LAT | $41-42-21.2 \mathrm{~N}$ |

## EXECUTIVE SUMMARY:

Malouf Engineering $I^{\prime} \dagger^{\prime} \mathrm{I}(\mathrm{MEI})$, as requested, has performed a rigorous structural analysis of the above-mentioned structure to assess the impact of the changed condition as noted in Table 1.

Based on the stress analysis performed, the existing structure is in conformance with the Int'I Building Code (IBC) / ANSI/TIA-222-G Standard for the loading considered under the criteria listed and referenced in the report sections - tower rated at $99.5 \%$ - Base Plate.

The installation of the proposed changed condifion as noted in Table 1 is structurally acceptable. Please refer to Appendix 1 for Schematic Lines Layout.

MEI appreciates the opportunity of providing our continuing professional services to you. If you have any questions or need further assistance on this or other projects, please contact us.

Respectfully submitted,
Malouf Engineering Int'l, Inc.

Analysis performed by:

Luan Nguyen, PE
Sr. Project Engineer


972-783-2578 ext. 106 mmalouf@maloufengineering.com


5/13/2019

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## 1. INTRODUCTION \& SCOPE

A rigorous structural analysis was performed by Malouf Engineering Int'I (MEI), as requested and authorized by Mr. Kyle Richers, Transcend Wireless, on behalf of T-Mobile, to determine the acceptance of the proposed changed conditions in conformance with the IBC / ANSI/TIA-222-G Standard, "Structural Standard for Antenna Supporting Structures and Antennas".

The scope of this independent analysis is to determine the overall stability and the adequacy of structural members, foundations, and member connections, as available and stated. This analysis considers the structure to have been properly installed and maintained with no structural defects. Installation procedures and related loading are not within the scope of this analysis and should be performed and evaluated by a competent person of the erection contractor.

The different report sections detail the applicable information used in this evaluation, relating to the tower data, the appurtenances configuration and the wind and ice loading considered.

## 2. SOURCE OF DATA

The following information has been used in this evaluation as source data that accurately represent the existing structure and the related appurtenances:

|  | Source | Information | Reference |
| :---: | :---: | :---: | :---: |
| Structure |  |  |  |
| Tower | MEI Records | Previous Structural Analysis | ID CT04861M-19V0 Dated 03/26/2019 |
| Foundation | MEI Records | Previous Structural Analysis | ID CT04861M-19V0 Dated 03/26/2019 |
| Material Grade | Not available from supplied documents-Assumed based on typical towers of this type-refer to Appendix |  |  |
| Current Appurtenances |  |  |  |
|  | MEI Records | Previous Structural Analysis | ID CT04861M-19V0 Dated 03/26/2019 |
| CHANGED CONDITION |  |  |  |
|  | Transcend Wireless Mr. Kyle Richers | T-Mobile Collocation Application | Dated 04/30/2019 |

## Background Information:

Based on available information, the following is known regarding this structure:

| Designer / FAbricator | Not Known / 18-Sided |
| :--- | :--- |
| Original Design Criteria | TIA/EIA 222-Unknown |
| Prior Structural Modifications | As per GPD Group base plate and anchor rod <br> modifications Job \#2009264.50 dated 06/12/2009; <br> pole shaft modifications by others as per B+T <br> mapping report dated 07/17/2014 - considered <br> properly installed. |

## 3. ANALYSIS CRITERIA

The structural analysis performed used the following criteria:

| CODE / STANDARD | 2018 CT Building Code / 2015 Int'I Building Code / ANSI/TIA-222-G-4 Standard |  |
| :--- | :--- | :--- |
| LOADING CASES | Full Wind: | 129 Mph ultimate gust [equiv. $100 \mathrm{Mph}(3-$-sec gust)] w/No Radial Ice** |
|  | Iced Case: | $40 \mathrm{Mph}+1.25 "$ Radial Ice |
|  | Service: | 60 Mph |
|  | Seismic: | $\mathrm{S}_{\mathrm{s}}=0.181 / \mathrm{S}_{1}=0.064$ / Site Class: D - Stiff Soil |
| StRUCTURE CRITERIA | Risk Category (Structural Class): 2 |  |
|  | Exposure Category: 'B' - Topographic Category: 1 |  |

## Appurtenances Configuration

The following appurtenances configuration is denoted by the summation of Tables 1 \& 2:
Table 1: Tenant with Changed Condition Appurtenances Configuration

| Elev <br> (ft) | Tenant | Ants Qty | Appurtenance Model / Description | Mount Description | Lines Qty | Line size \& Location |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 95 | T-Mobile | 3 | AIR32 KRD901146-1 B66A B2A Panel Antennas | [Existing Mount] w/ New Handrail Kit | 4 | 1-5/8 HybridFiber cables (I) |
|  |  | 3 | APXVAARR24_43-U-NA20 Panel Antennas |  |  |  |
|  |  | 3 | Radio 4449 B71/B12 Boxes |  |  |  |
| Appurtenances to Remain |  |  |  |  |  |  |
| 95 | T-Mobile | 3 | AIR21 KRC118023 B2P B4A Panel Antennas | (3) 12.5 ft . L.P. T-Arm Mounts (SiteProl RMV12-3XX) | $\begin{aligned} & 6 \\ & 1 \end{aligned}$ | $\begin{aligned} & \hline 7 / 8^{\prime \prime} \\ & \text { 1-5/8 Hybrid- } \\ & \text { Cable - (I) } \\ & \hline \end{aligned}$ |
| Appurtenances to be Removed |  |  |  |  |  |  |
| 95 | T-Mobile | 3 | AlR21 B4A B12P Panel Antennas |  |  |  |
|  |  | 3 | RRUS-11 B12 Boxes |  |  |  |

## Table 2: Remaining Tenants Current and Reserved/Future Appurtenances

| Elev <br> (ft) | Tenant | Ants Qły | Appurtenance Model / Description | Mount Description | Lines Qty | Line size \& Location |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 101 |  | 1 | 5' Lightning Rod |  | 1 | 1/2" - (I) |
|  |  | 1 | Beacon/Strobe |  |  |  |
| 103.5 | AT\&T [New] | 3 | HPA-65R-BUU-H6 Panel Antennas | (3) SiteProl RRU Dual Swivel Mounts \#RRUDSM (2/sector) |  | [Existing Lines] |
|  |  | 3 | RRUS-32 B66 Boxes |  |  |  |
| 103.5 | AT\&T | 3 | QS66512-3 Panel Antennas | Top Platform w/ Rails (\& Ladder) | $\begin{aligned} & 12 \\ & 2 \\ & 4 \\ & 1 \end{aligned}$ | 1-5/8" <br> 5/8" Fiber <br> 3/4" DC Power <br> ATCB-BO1-xxx <br> Homerun <br> Cable-(I/E) |
|  |  | 3 | 7770.00 Panels Panel Antennas |  |  |  |
|  |  | 3 | RRUS-11 Boxes |  |  |  |
|  |  | 3 | RRUS-32 Boxes |  |  |  |
|  |  | 3 | RRUS-32 B2 Boxes |  |  |  |
|  |  | 2 | Raycap DC6 (Squid) Suppressors |  |  |  |
|  |  | 6 | LGP21401 TMA'S |  |  |  |
|  |  | 6 | TPX-070821 Triplexers |  |  |  |
| 46.5 |  | 1 | GPS Antenna | 18" $\pm$. Standoff Arm Mount |  | 3/8"-(E) |
| 37 |  | 1 | GPS Antenna | 18 " $\pm$ Standoff Arm Mount |  | 3/8"-(E) |

## Notes:

1. ${ }^{* *}$ As per 2015 IBC for ultimate $3-\mathrm{sec}$ gust wind speed converted to nominal 3 -sec gust wind speed as per Sect. 1609.3.1 as required to be used in ANSI/TIA-222-G Standard per exception 5 of Sect. 1609.1.1.
2. All elevations are measured from tower base.
3. Please note appurtenances not listed above are to be removed/not present as per data supplied.
4. (I) = Internal; (E) = External; (FZ) = Within Face Zone; (OFZ) = Outside Face Zone - as per TIA-222-G.
5. The above appurtenances represent MEl's understanding of the appurtenances configuration. If different than above, the analysis is invalid. Please contact MEl if any discrepancies are found.

## 4. ANALYSIS PROCEDURE

The subject structure is analyzed for feasibility of the installation of the proposed changed condition previously noted. The data records furnished were reviewed and a computer stress analysis was performed in accordance with the TIA-222 Standard provisions and with the agreed scope of work terms and the results of this analysis are reported.

## Analysis Program

The computer program used to model the structure is a rigorous Finite Element Analysis program, tnxTower (ver. 8.05), a commercially available program by Tower Numerics Inc. The latticed structures members are modeled using beam/truss and cable members and the pole members using tubular beam elements. The structural parameters and geometry of the members are included in the model. The dead and temperature loads and the wind loads are internally calculated by the program for the different wind directions and then applied as external loads on the structure. Any applicable exemptions, as per Section 15.6 of the TIA-222-G Standard for existing structures originally designed in accordance with a previous revision of the TIA-222 Standard, have been taken.

## Assumptions

This engineering study is based on the theoretical capacity of the members and is not a condition assessment of the structure. This analysis is based on information supplied, and therefore, its results are based on and as accurate as that supplied data. MEI has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural stress analysis:

- This existing tower is assumed, for the purpose of this analysis, to have been properly maintained and to be in good condition with no structural defects and with no deterioration to its member capacities ('asnew' condition).
- The tower member sizes and configuration are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated.
- The appurtenances configuration is as supplied and/or as stated in the report. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
- Some assumptions are made regarding antennas and mounts sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type \& industry practice.
- Mounts/Platforms are considered adequate to support the loading. No actual analysis of the platform/mount itself is performed, with the analysis being limited to analyzing the structure.
- The soil parameters are as per data supplied or as assumed and stated in the calculations. Refer to the Appendix. If no data is available, the foundation system is assumed to support the structure with its new reactions.
- All welds and connections are assumed to develop at least the member capacity, unless determined otherwise and explicitly stated in this report.
- All prior structural modifications, if any, are assumed to be as per data supplied/available, and to have been properly installed and to be fully effective.

If any of the above assumptions are not valid or have been made in error, this analysis results may be invalided, MEI should be contacted to review any contradictory information to determine its effect.

## 5. ANALYSIS RESULTS

The results of the structural stress analysis based on data available and with the previous listed criteria, indicated the following:

Note: The Wind loading controls over the Seismic loading as per TIA Section 2.7.
Table 3: $\quad$ Stress Analysis Results

| Component Type | Maximum <br> Stress Ratio | Controlling Elev. (ft) / <br> Component | Pass/Fail | Comment |
| :--- | :---: | :---: | :---: | :---: |
| POLE | $95.0 \%$ | $88-61.25$ | Pass |  |
| BASE PLATE | $99.5 \%$ | Bending | Pass |  |
| ANCHOR RODS | $60.7 \%$ | Tension | Pass |  |
| FOUNDATION | $95.0 \%$ | Moment | Pass |  |

## Table 4: Serviceability Requirements

|  | Maximum Value | TIA Requirement (10dB) | Pass/Fail | Comment |
| :--- | :---: | :---: | :---: | :---: |
| TwIST/SWAY | 2.0805 Deg. | 4 Deg. from Vert. or <br> Horiz. Axis | Pass |  |
| HORIZONTAL <br> DISPLACEMENT | 22.233 In./ <br> $1.79 \%$ of Ht. | $3.0 \%$ of Height | Pass |  |

## Notes:

1. The Maximum Stress Ratio is the percentage that the maximum load in the member is relative to the allowable load as determined by Code requirements.
2. Refer to the Appendix 1 for more details on the member loads.
3. A maximum stress ratio between $100 \%$ and $105 \%$ may be considered as Acceptable according to industry standard practice.

## 6. FINDINGS \& RECOMMENDATIONS

- Based on the rigorous stress analysis results, the subject structure is rated at $\mathbf{9 9 . 5 \%}$ of its support capacity (controlling component: Base Plate) with the proposed changed condition considered. Please refer to Table 3 and to Appendix 1 for more details of the analysis results.
- Based on the stress analysis performed, the existing structure is in conformance with the IBC / ANSI/TIA 222-G Standard for the loading considered under the criteria listed and referenced in the report sections.
- The installation of the proposed changed condition as noted in Table 1 is structurally acceptable. Please refer to Appendix 1 for Schematic Lines Layout.
- This structure is at its support capacity for the appurtenances and loading criteria considered. Therefore, no changes to the configuration considered should be made without performing a new proper evaluation.

Rigging and temporary supports required for the erection/modification shall be determined, documented, furnished and installed by the erector/contractor accounting for the loads imposed on the structure due to the proposed construction method.

## 7. REPORT DISCLAIMER

The engineering services rendered by Malouf Engineering International, Inc. ('MEI') in connection with this Structural Analysis are limited to a computer analysis of the tower structure, size and capacity of its members. MEI does not analyze the fabrication, including welding and connection capacities, except as included in this Report.
The analysis performed, and the conclusions contained herein are based on the assumption that the tower has been properly installed and maintained, including, but not limited to the following:

1. Proper alignment and plumbness.
2. Correct guy tensions, as applicable.
3. Correct bolt tightness or slip jacking of sleeved connections.
4. No significant deterioration or damage to any structural component.

Furthermore, the information and conclusions contained in this Report were determined by application of the current "state-of-the-art" engineering and analysis procedures and formulae. Malouf Engineering INTERNATIONAL, INC. assumes no obligation to revise any of the information or conclusions contained in this Report in the event that such engineering and analysis procedures and formulae are hereafter modified or revised. In addition, under no circumstances will Malouf Engineering International, Inc. have any obligation or responsibility whatsoever for or on account of consequential or incidental damages sustained by any person, firm or organization as a result of any information or conclusions contained in the Report, and the maximum liability of Malouf Engineering International, Inc., if any, pursuant to this Report shall be limited to the total funds actually received by Malouf Engineering International, Inc. for preparation of this Report.

Customer has requested Malouf Engineering International, Inc. to prepare and submit to Customer an engineering analysis with respect to the Subject Tower and has further requested Malouf Engineering INTERNATIONAL, INC. to make appropriate recommendations regarding suggested structural modifications and changes to the Subject Tower. In making such request of Malouf Engineering International, Inc., Customer has informed Malouf Engineering International, Inc. that Customer will make a determination as to whether or not to implement any of the changes or modifications which may be suggested by Malouf Engineering International, Inc. and that Customer will have any such changes or modifications made by riggers, erectors and other subcontractors of Customer's choice. Malouf Engineering International, Inc. shall have the right to rely upon the accuracy of the information supplied by the customer and shall not be held responsible for the Customer's misrepresentation or omission of relevant fact whether intentional or otherwise.

Customer hereby agrees and acknowledges that Malouf Engineering International, Inc. shall have no liability whatsoever to Customer or to others for any work or services performed by any persons other than Malouf Engineering International, Inc. in connection with the implementation of services including but not limited to any services rendered for Customer or for others by riggers, erectors or other subcontractors. Customer acknowledges and agrees that any riggers, erectors or subcontractors retained or employed by Customer shall be solely responsible to Customer and to others for the quality of work performed by them and that Malouf Engineering international, Inc. shall have no liability or responsibility whatsoever as a result of any negligence or breach of contract by any such rigger, erector or subcontractor and that Customer and rigger, erector, or subcontractor will provide Malouf Engineering International, Inc. with a Certificate of Insurance naming Malouf Engineering International, Inc. as additional insured.

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## APPENDIX 1 - ANALYSIS PRINTOUT \& GRAPHICS



3 2
61.3 ft
DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :--- | :--- | :--- | :--- |
| QS66512-3 w/ Pipe Mount (ATI / E) | 103.5 | Top Platform w/ Rails ( Ladder) (ATI/ | 103.5 |
| QS66512-3 w/ Pipe Mount (ATI / E) | 103.5 | E) |  |

## TOWER DESIGN NOTES

1. Tower is located in Hartford County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 100 mph basic wind in accordance with the TIA-222-G Standard
4. Tower is also designed for a 40 mph basic wind with 1.25 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: $99.5 \%$

## ALL REACTIONS <br> ARE FACTORED


TORQUE 0 kip-ft 40 mph WIND - 1.2500 in ICE

TORQUE 0 kip-ft REACTIONS - 100 mph WIND

Malouf Engineering Int'l, Inc. 17950 Preston Road, Suite \#720

Dallas, TX 75252
Phone: (972) 783-2578
FAX: (972) 783-2583
Job: 101 ft MP / Wethersfield Site \#CTHA506A

| Project: CTO4861M-19V1 |
| :--- |
| Client: Transcend Wireless / T-Mobile |
| Drawn by: |
| Code: |
| Path: |
| TIA-222-G |
| Pate: |






| tnxTower | Job | 101 ft MP \| Wethersfield Site \#CTHA506A | $\begin{array}{ll} \text { Page } \\ & 1 \text { of } 5 \end{array}$ |
| :---: | :---: | :---: | :---: |
| Malouf Engineering Int'l, Inc. <br> 17950 Preston Road, Suite \#720 <br> Dallas, TX 75252 <br> Phone: (972) 783-2578 <br> FAX: (972) 783-2583 | Project | CT04861M-19V1 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 12:41:16 05/13/19 } \end{array}$ |
|  | Client | Transcend Wireless / T-Mobile | Designed by LNguyen |

## Tower Input Data

The tower is a monopole.
This tower is designed using the TIA-222-G standard.
The following design criteria apply:
Tower is located in Hartford County, Connecticut.
Basic wind speed of 100 mph .
Structure Class II.
Exposure Category B.
Topographic Category 1.
Crest Height 0.00 ft .
Nominal ice thickness of 1.2500 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf.
A wind speed of 40 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Placement | Total <br> Number |
| :---: | :---: | :---: |
|  | $f t$ |  |
| 3/4" DC Power Cable | $101.00-$ | 2 |
| (AT\&T / E) | 0.00 |  |
| ATCB-B01-xxx | $101.00-$ | 1 |
| Homerun Cable | 62.00 |  |
| (AT\&T / E) |  |  |


| Description | Placement | Total <br> Number |
| :---: | :---: | :---: |
| $3 / 8$ (Shielded) | $46.50-0.00$ | 1 |
| (E) | $37.00-0.00$ | 1 |
| $3 / 8$ (Shielded) |  |  |
| (E) |  |  |

## Feed Line/Linear Appurtenances - Entered As Area

| Description | Placement | Total <br> Number |
| :---: | :---: | :---: |
| Safety Line 3/8 <br> (E) | $101.00-0.00$ | 1 |
| Step Bolts <br> (E) <br> $1 / 2$ | $101.00-0.00$ | 1 |
| (E (Lighting)) <br> $15 / 8$ | $101.00-0.00$ | 1 |
| (AT\&T / E) <br> 5/8" Fiber Cable <br> (AT\&T / E) | $101.00-0.00$ | 12 |
| 3/4" DC Power <br> Cable | $101.00-0.00-0.00$ | 2 |
| (AT\&T / E) <br> ATCB-B01-xxx <br> Homerun Cable <br> (AT\&T / E) | $62.00-0.00$ | 2 |
| 1 5/8 (Hybrid-Fiber) |  |  |


| Description | Placement | Total <br> Number |
| :---: | :---: | :---: |
| (T-Mobile / E) <br> $15 / 8$ (Hybrid-Fiber) <br> (T-Mobile / P) <br> $7 / 8$ | $95.00-0.00$ | 4 |
| (T-Mobile / E) <br> MP303 <br> (Mods) | $95.00-0.00$ | 6 |
| MP303 <br> (Mods) | $62.00-47.00$ | 1 |
| MP304 <br> (Mods) | $45.50-0.00-47.00$ | 1 |
| MP304 <br> (Mods) | $45.50-0.00$ | 1 |


| tnxTower | $101 \mathrm{ft} \mathrm{MP} \mathrm{\mid} \mathrm{Wethersfield} \mathrm{Site} \mathrm{\# CTHA506A}$ |  | $\text { Page } 2 \text { of } 5$ |
| :---: | :---: | :---: | :---: |
| Malouf Engineering Int'l, Inc. 17950 Preston Road, Suite \#720 | Project | CT04861M-19V1 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 12:41:16 05/13/19 } \end{array}$ |
| Dallas, TX 75252 <br> Phone: (972) 783-2578 <br> FAX: (972) 783-2583 | Client | Transcend Wireless / T-Mobile | Designed by LNguyen |

## Discrete Tower Loads

| Description | Placement | Weight | Description | Placement <br> $f t$ | Weight <br> K |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | K |  |  |  |
| 5' Lightning Rod <br> (E) | 101.00 | 0.00 | $\begin{gathered} \text { RRUS-32 B2 } \\ (\text { AT\&T / E) } \end{gathered}$ | 103.50 | 0.05 |
|  |  | 0.01 |  |  | 0.07 |
|  |  | 0.01 |  |  | 0.10 |
|  |  | 0.03 |  |  | 0.16 |
| Beacon/Strobe <br> (E) | 101.00 | 0.06 | RRUS-32 B2 <br> (AT\&T / E) | 103.50 | 0.05 |
|  |  | 0.09 |  |  | 0.07 |
|  |  | 0.12 |  |  | 0.10 |
|  |  | 0.20 |  |  | 0.16 |
| QS66512-3 w/ Pipe Mount (AT\&T / E) | 103.50 | 0.16 | RRUS-32 B2 <br> (AT\&T / E) | 103.50 | 0.05 |
|  |  | 0.23 |  |  | 0.07 |
|  |  | 0.32 |  |  | 0.10 |
|  |  | 0.52 |  |  | 0.16 |
| QS66512-3 w/ Pipe Mount <br> (AT\&T / E) | 103.50 | 0.16 | $\begin{aligned} & \text { RRUS-32 } \\ & (\mathrm{AT} \& \mathrm{~T} / \mathrm{E}) \end{aligned}$ | 103.50 | 0.08 |
|  |  | 0.23 |  |  | 0.10 |
|  |  | 0.32 |  |  | 0.14 |
|  |  | 0.52 |  |  | 0.21 |
| QS66512-3 w/ Pipe Mount (AT\&T / E) | 103.50 | 0.16 | $\begin{aligned} & \text { RRUS-32 } \\ & \text { (AT\&T / E) } \end{aligned}$ | 103.50 | 0.08 |
|  |  | 0.23 |  |  | 0.10 |
|  |  | 0.32 |  |  | 0.14 |
|  |  | 0.52 |  |  | 0.21 |
| 7770.00 Panels w/ Pipe <br> Mount <br> (AT\&T / E) | 103.50 | 0.04 | $\begin{aligned} & \text { RRUS-32 } \\ & \text { (AT\&T / E) } \end{aligned}$ | 103.50 | 0.08 |
|  |  | 0.09 |  |  | 0.10 |
|  |  | 0.15 |  |  | 0.14 |
|  |  | 0.29 |  |  | 0.21 |
| 7770.00 Panels w/ Pipe <br> Mount <br> (AT\&T / E) | 103.50 | 0.04 | (2) LGP21401 TMA'S <br> (AT\&T / E) | 103.50 | 0.02 |
|  |  | 0.09 |  |  | 0.03 |
|  |  | 0.15 |  |  | 0.04 |
|  |  | 0.29 |  |  | 0.06 |
| 7770.00 Panels w/ Pipe Mount (AT\&T / E) | 103.50 | 0.04 | (2) LGP21401 TMA'S <br> (AT\&T / E) | 103.50 | 0.02 |
|  |  | 0.09 |  |  | 0.03 |
|  |  | 0.15 |  |  | 0.04 |
|  |  | 0.29 |  |  | 0.06 |
| HPA-65R-BUU-H6 w/ Pipe <br> Mounts (AT\&T / New) | 103.50 | 0.09 | (2) LGP21401 TMA'S <br> (AT\&T / E) | 103.50 | 0.02 |
|  |  | 0.17 |  |  | 0.03 |
|  |  | 0.26 |  |  | 0.04 |
|  |  | 0.48 |  |  | 0.06 |
| HPA-65R-BUU-H6 w/ Pipe <br> Mounts (AT\&T / New) | 103.50 | 0.09 | (2) TPX-070821 Triplexer (AT\&T / E) | 103.50 | 0.01 |
|  |  | 0.17 |  |  | 0.01 |
|  |  | 0.26 |  |  | 0.02 |
|  |  | 0.48 |  |  | 0.03 |
| HPA-65R-BUU-H6 w/ Pipe <br> Mounts <br> (AT\&T / New) | 103.50 | 0.09 | (2) TPX-070821 Triplexer (AT\&T / E) | 103.50 | 0.01 |
|  |  | 0.17 |  |  | 0.01 |
|  |  | 0.26 |  |  | 0.02 |
|  |  | 0.48 |  |  | 0.03 |
| RRUS-11 (AT\&T) <br> (AT\&T / E) | 103.50 | 0.06 | (2) TPX-070821 Triplexer (AT\&T / E) | 103.50 | 0.01 |
|  |  | 0.08 |  |  | 0.01 |
|  |  | 0.11 |  |  | 0.02 |
|  |  | 0.18 |  |  | 0.03 |
| RRUS-11 (AT\&T) <br> (AT\&T / E) | 103.50 | 0.06 | Raycap DC6 (Squid) | 103.50 | 0.02 |
|  |  | 0.08 | Suppressor |  | 0.04 |
|  |  | 0.11 | (AT\&T / E) |  | 0.05 |
|  |  | 0.18 |  |  | 0.10 |
| RRUS-11 (AT\&T) (AT\&T / E) | 103.50 | 0.06 | Raycap DC6 (Squid) | 103.50 | 0.02 |
|  |  | 0.08 | Suppressor |  | 0.04 |
|  |  | 0.11 | (AT\&T / E) |  | 0.05 |
|  |  | 0.18 |  |  | 0.10 |


| tnxTower | $101 \mathrm{ft} \mathrm{MP} \mathrm{\mid} \mathrm{Wethersfield} \mathrm{Site} \mathrm{\# CTHA506A}$ |  | Page 3 of 5 |
| :---: | :---: | :---: | :---: |
| Malouf Engineering Int'l, Inc. 17950 Preston Road, Suite \#720 Dallas, TX 75252 Phone: (972) 783-2578 FAX: (972) 783-2583 | Project | CT04861M-19V1 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 12:41:16 05/13/19 } \end{array}$ |
|  | Client | Transcend Wireless / T-Mobile | Designed by LNguyen |

Description Placement Weight

| Description | Placement | Weight |
| :---: | :---: | :---: |
|  | $f t$ | K |
| APXVAARR24_43-U-NA20 w/ Pipe Mount (T-Mobile / P) | 95.00 | 0.18 |
|  |  | 0.32 |
|  |  | 0.46 |
|  |  | 0.78 |
| APXVAARR24_43-U-NA20 <br> w/ Pipe Mount <br> (T-Mobile / P) | 95.00 | 0.18 |
|  |  | 0.32 |
|  |  | 0.46 |
|  |  | 0.78 |
| RADIO 4449-B71 + B12 <br> (T-Mobile / P) | 95.00 | 0.07 |
|  |  | 0.09 |
|  |  | 0.11 |
|  |  | 0.15 |
| RADIO 4449-B71 + B12 <br> (T-Mobile / P) | 95.00 | 0.07 |
|  |  | 0.09 |
|  |  | 0.11 |
|  |  | 0.15 |
| RADIO 4449 - B71 + B12 (T-Mobile / P) | 95.00 | 0.07 |
|  |  | 0.09 |
|  |  | 0.11 |
|  |  | 0.15 |
| 12.5 ft L. P. T-Arm Mount (SiteProl RMV12-3XX) w/ New Handrail Kit (T-Mobile / E) | 95.00 | 0.40 |
|  |  | 0.60 |
|  |  | 0.80 |
|  |  | 1.20 |
| 12.5 ft L. P. T-Arm Mount (SitePro1 RMV12-3XX) w/ | 95.00 | 0.40 |
|  |  | 0.60 |
| New Handrail Kit(T-Mobile / E) |  | 0.80 |
|  |  | 1.20 |
| 12.5 ft . L.P. T-Arm Mount (SitePro1 RMV12-3XX) w/ | 95.00 | 0.40 |
|  |  | 0.60 |
| New Handrail Kit |  | 0.80 |
| (T-Mobile / E) |  | 1.20 |
| GPS <br> (E) | 46.50 | 0.00 |
|  |  | 0.01 |
|  |  | 0.01 |
|  |  | 0.01 |
| 18" Approx. Standoff Arm <br> (E) | 46.50 | 0.03 |
|  |  | 0.04 |
|  |  | 0.06 |
|  |  | 0.09 |
| GPS <br> (E) | 37.00 | 0.00 |
|  |  | 0.00 |
|  |  | 0.01 |
|  |  | 0.01 |
| 18" Approx. Standoff Arm <br> (E) | 37.00 | 0.03 |
|  |  | 0.05 |
|  |  | 0.07 |
|  |  | 0.11 |


|  | $f t$ | K |
| :---: | :---: | :---: |
| RRUS-32 B66 (AT\&T / New) | 103.50 | 0.06 |
|  |  | 0.08 |
|  |  | 0.11 |
|  |  | 0.16 |
| RRUS-32 B66 (AT\&T / New) | 103.50 | 0.06 |
|  |  | 0.08 |
|  |  | 0.11 |
|  |  | 0.16 |
| RRUS-32 B66 (AT\&T / New) | 103.50 | 0.06 |
|  |  | 0.08 |
|  |  | 0.11 |
|  |  | 0.16 |
| SitePro1 RRU Dual Swivel Mount (AT\&T / New) | 103.50 | 0.04 |
|  |  | 0.07 |
|  |  | 0.10 |
|  |  | 0.16 |
| SitePro1 RRU Dual Swivel Mount (AT\&T / New) | 103.50 | 0.04 |
|  |  | 0.07 |
|  |  | 0.10 |
|  |  | 0.16 |
| SiteProl RRU Dual Swivel Mount (AT\&T / New) | 103.50 | 0.04 |
|  |  | 0.07 |
|  |  | 0.10 |
|  |  | 0.16 |
|  <br> Ladder) <br> (AT\&T / E) | 103.50 | 2.00 |
|  |  | 3.15 |
|  |  | 4.30 |
|  |  | 6.60 |
| AIR21 KRC118023 B2P B4A <br> w/ Pipe Mount <br> (T-Mobile / E) | 95.00 | 0.13 |
|  |  | 0.18 |
|  |  | 0.25 |
|  |  | 0.40 |
| AIR21 KRC118023 B2P B4A <br> w/ Pipe Mount <br> (T-Mobile / E) | 95.00 | 0.13 |
|  |  | 0.18 |
|  |  | 0.25 |
|  |  | 0.40 |
| AIR21 KRC118023 B2P B4A <br> w/ Pipe Mount (T-Mobile / E) | 95.00 | 0.13 |
|  |  | 0.18 |
|  |  | 0.25 |
|  |  | 0.40 |
| AIR32 KRD901146-1 B66A B2A Panel Antenna w/ Pipe | 95.00 | 0.17 |
|  |  | 0.23 |
| B2A Panel Antenna w/ Pipe Mount |  | 0.30 |
| (T-Mobile / P) |  | 0.46 |
| AIR32 KRD901146-1 B66A B2A Panel Antenna w/ Pipe | 95.00 | 0.17 |
|  |  | 0.23 |
| B2A Panel Antenna w/ Pipe Mount |  | 0.30 |
| (T-Mobile / P) |  | 0.46 |
| AIR32 KRD901146-1 B66A | 95.00 | 0.17 |
| B2A Panel Antenna w/ Pipe |  | 0.23 |
| Mount |  | 0.30 |
| (T-Mobile / P) |  | 0.46 |
| APXVAARR24_43-U-NA20 | 95.00 | 0.18 |
| w/ Pipe Mount |  | 0.32 |
| (T-Mobile / P) |  | 0.46 |
|  |  | 0.78 |



|  |  |  | Max | n React |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Condition | Gov. Load Comb | Vertical K | $\begin{gathered} \text { Horizontal, } X \\ K \end{gathered}$ | $\begin{gathered} \text { Horizontal, } Z \\ K \end{gathered}$ |
| Pole | Max. Vert | 26 | 59.03 | -0.00 | -0.00 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 21 | 16.94 | 16.58 | -0.02 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 3 | 16.94 | -0.02 | 16.73 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 2 | 1313.41 | -0.02 | 16.73 |
|  | Max. $\mathrm{M}_{\mathrm{z}}$ | 8 | 1308.13 | -16.58 | 0.02 |
|  | Max. Torsion | 6 | 0.25 | -14.48 | 8.38 |
|  | Min. Vert | 3 | 16.94 | -0.02 | 16.73 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 9 | 16.94 | -16.58 | 0.02 |
|  | $\text { Min. } \mathrm{H}_{\mathrm{z}}$ | 15 | $16.94$ | 0.02 | -16.73 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 14 | -1313.06 | 0.02 | -16.73 |
|  | Min. $\mathrm{M}_{\mathrm{z}}$ | 20 | -1308.28 | 16.58 | -0.02 |
|  | Min. Torsion | 18 | -0.25 | 14.48 | -8.38 |

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | o |
| :---: | :---: | :---: | :---: | :---: | :---: |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation | Appurtenance | Gov. <br> Load | Deflection | Tilt | Twist | Radius of <br> Curvature |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  | Comb. | in | $\circ$ | $\circ$ | $\circ$ |
| 103.50 |  | 40 | 22.233 | 2.0805 | 0.0011 | 6815 |
| 101.00 | QS66512-3 w/ Pipe Mount | 5' Lightning Rod | 40 | 22.233 | 2.0805 | 0.0011 |
| 95.00 | AIR21 KRC118023 B2P B4A w/ | 40 | 19.646 | 2.0281 | 0.0009 | 6815 |
|  | Pipe Mount |  |  |  | 5680 |  |
| 46.50 | GPS | 40 | 4.463 | 0.8926 | 0.0003 |  |
| 37.00 | GPS | 40 | 2.827 | 0.7313 | 0.0002 | 3460 |


| tnxTower | $101 \mathrm{ft} \mathrm{MP} \mathrm{\mid} \mathrm{Wethersfield} \mathrm{Site} \mathrm{\# CTHA506A}$ |  | $\begin{array}{ll} \hline \text { Page } \\ & \\ \end{array}$ |
| :---: | :---: | :---: | :---: |
| Malouf Engineering Int'l, Inc. 17950 Preston Road, Suite \#720 | Project | CT04861M-19V1 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 12:41:16 05/13/19 } \end{array}$ |
| Dallas, TX 75252 <br> Phone: (972) 783-2578 <br> FAX: (972) 783-2583 | Client | Transcend Wireless / T-Mobile | Designed by LNguyen |

## Base Plate Design Data

| Plate <br> Thickness | Number of Anchor Bolts | Anchor Bolt Size | Actual | Actual | Actual | Actual | Controlling Condition | Critical Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Allowable | Allowable | Allowable | Allowable |  |  |
|  |  |  | Ratio | Ratio | Ratio | Ratio |  |  |
|  |  |  | Bolt | Concrete | Plate | Stiffener |  |  |
|  |  |  | Tension | Stress | Stress | Stress |  |  |
|  |  |  | K | ksi | ksi | ksi |  |  |
| in |  | in |  |  |  |  |  |  |
| 3.7000 | 8 | 1.7500 | 131.36 | 3.064 | 44.763 |  | Plate | 0.99 |
|  |  |  | 216.48 | 4.080 | 45.000 |  |  | V |
|  |  |  | 0.61 | 0.75 | 0.99 |  |  |  |

## Section Capacity Table

| Section No. | $\begin{gathered} \text { Elevation } \\ f t \end{gathered}$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} \phi P_{\text {allow }} \\ K \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 101-88 | Pole | TP16.36x14.64x0.1875 | 1 | -7.15 | 701.90 | 45.3 | Pass |
| L2 | 88-61.25 | Pole | TP19.7689x15.6873x0.25 | 2 | -10.32 | 1150.70 | 95.0 | Pass |
| L3 | 61.25-56.25 | Pole | TP20.4726x19.7689x0.250* | 3 | -11.07 | 1717.72 | 71.0 | Pass |
| L4 | 56.25-51.75 | Pole | TP21.1059x20.4726x0.250* | 4 | -11.75 | 1754.20 | 75.0 | Pass |
| L5 | 51.75-46.25 | Pole | TP21.88x21.1059x0.250* | 5 | -12.17 | 1764.42 | 77.9 | Pass |
| L6 | 46.25-40 | Pole | TP22.28x20.725x0.3125* | 6 | -14.13 | 2370.46 | 68.2 | Pass |
| L7 | 40-35 | Pole | TP22.995x22.28x0.3125* | 7 | -15.14 | 2419.54 | 71.0 | Pass |
| L8 | 35-30 | Pole | TP23.71x22.995x0.3125* | 8 | -16.13 | 2466.74 | 73.8 | Pass |
| L9 | 30-25 | Pole | TP24.425x23.71x0.3125* | 9 | -17.15 | 2517.17 | 76.2 | Pass |
| L10 | 25-20 | Pole | TP25.14x24.425x0.3125* | 10 | -18.19 | 2566.02 | 78.6 | Pass |
| L11 | 20-15 | Pole | TP25.855x25.14x0.3125* | 11 | -19.25 | 2613.31 | 80.8 | Pass |
| L12 | 15-10 | Pole | TP26.57x25.855x0.3125* | 12 | -20.33 | 2664.61 | 82.7 | Pass |
| L13 | 10-5 | Pole | TP27.285x26.57x0.3125* | 13 | -21.44 | 2714.66 | 84.5 | Pass |
| L14 | 5-0 | Pole | TP28x27.285x0.3125* | 14 | -22.57 | 2763.46 | 86.3 | Pass |
|  |  |  |  |  |  | Summary |  |  |
|  |  |  |  |  |  | Pole (L2) | 95.0 | Pass |
|  |  |  |  |  |  | Base Plate | 99.5 | Pass |
|  |  |  |  |  |  | RATING = | 99.5 | Pass |

*Modified w/ MP304 \& MP303 Channels

Program Version 8.0.5.0-11/28/2018 File:D:/MEIProjects/19 DATA/MNP/CT04861M-19V1/CT04861M-19V1.eri

## APPENDIX 2 - SOURCE / CHANGED CONDITION

Tower Equipment
List ALL equipment components installed on the tower or ground space area, including mounting apparatus, ice bridges, etc.

| Tower Equipment |  |  |  | Equipment Status (mark with "x") |  |  | Equipment Dimensions |  |  |  | Azimuths | Equip. Centerline |  | Lines |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Component Type (Ant. type, RRU, mount, etc.) | Manufacturer | Model | \# Units | Exist | New | $\begin{array}{\|c\|} \hline \text { To be } \\ \text { Remo } \\ \text { ved } \end{array}$ | Height (inches) | Width (inches) | Depth (inches) | Weight (lbs) | Degrees (a/b/c) | AGL (ft) | $\begin{gathered} \text { Leg } \\ \text { (e.g. NE) } \end{gathered}$ | Type | \# Units | Size |
| Antenna | Ericsson | AIR 21 KRC118023 B2P_B4A | 3 | X |  |  | 56.0 | 12.0 | 8.0 | 91.0 | 20/150/255 | $9^{95}$ |  | Coax | 6 | 7/8" |
| Antenna | Ericsson | AIR 21 B4A/B12P | 3 |  |  | X | 57.0 | 14.8 | 9.5 | 124.0 | 20/150/255 | $95^{\prime}$ |  |  |  |  |
| Antenna | Ericsson | AIR 32 KRD901146-1_B66A_B2A | 3 |  | x |  | 56.5 | 12.9 | 8.7 | 132.2 | 20/150/255 | $95^{\prime}$ |  | Hybrid | 5 | 1-5/8" |
| Antenna | RFS | APXVAARR24_43-U-NA20 | 3 |  | X |  | 95.9 | 24.0 | 8.7 | 128.0 | 20/150/255 | 95' |  |  |  |  |
| RRU | Ericsson | Radio 4449 B71B12 | 3 |  | X |  | 14.9 | 13.2 | 9.3 | 74.0 | 20/150/255 | $95^{\prime}$ |  |  |  |  |
| RRU | Ericsson | RRUS11B12 | 3 |  |  | x | 19.7 | 17.0 | 7.2 | 50.7 | 20/150/255 | $95^{\prime}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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## Ground Equipment Equipment

| Ground Equipment |  |  |  | Equipment Status (mark with "x") |  |  | Equipment Dimensions |  |  |  | Equipment Details |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Component | Manufacturer | Model | Quantity | Existing | New | To be <br> Remov ed | Height (inches) | Width (inches) | Depth (inches) | Weight (lbs) | (e.g. generator KWs, battery type, operating requirements, etc.) |
|  |  |  |  |  |  |  |  |  |  |  |  |
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## Structural Analysis Report

Antenna Mount Analysis
T-Mobile Site \#: CTHA506A

75 Wells Road Wethersfield, CT

Centek Project No. 19027.22

Date: May 03, 2019

Max Stress Ratio $=90.8 \%$


Prepared for:
T-Mobile USA 35 Griffin Road Bloomfield, CT 06002

## Table of Contents

## SECTION 1 - REPORT

- ANTENNA AND APPURTENANCE SUMMARY
- STRUCTURE LOADING
- CONCLUSION


## SECTION 2 - CALCULATIONS

- WIND LOAD ON APPURTENANCES
- RISA3D OUTPUT REPORT

SECTION 3 - REFERENCE MATERIALS (NOT INCLUDED WITHIN REPORT)

- RF DATA SHEET, DATED 04/13/2019


## Centered on Solutions" ${ }^{\text {"" }}$

May 03, 2019
Mr. Dan Reid
Transcend Wireless
10 Industrial Ave
M ahwah, NJ 07430
Re: Structural Letter ~Antenna Mount
T-Mobile - Site Ref: CTHA506A
75 Wells Road Wethersfield, CT 06109

Centek Project No. 19027.22

Dear Mr. Reid,

Centek Engineering, Inc. has reviewed the T-M obile antenna installation at the above referenced site. The purpose of the review is to determine the structural adequacy of the existing three (3) 12-ft T-frames with proposed handrails (SitePro P/N: HRK12-U). The review considered the effects of wind load, dead load and ice load in accordance with the 2015 International Building Code as modified by the 2018 Connecticut State Building Code (CTBC) including ASCE 7-10 and ANSI/TIA-222-G Structural Standards for Steel Antenna Towers and Supporting Structures.
The loads considered in this analysis consist of the following:

## - T-Mobile:

T-Arms: Three (3) Ericsson AIR21 KRC118023-1_B2P_B4A panel antennas, three (3) Ericsson AIR32KRD901146-1_B66A_B2A panel antennas ,three (3) RFS APXVAARR24_43-U-NA20 panel antennas and (3) Ericsson 4449 B71 B12 remote radio units mounted on three (3) T-Arms with a RAD center elevation of $95 \mathrm{ft}+/-\mathrm{AG}$ L. (Proposed handrail SitePro P/N: HRK12-U to be installed)

The antenna mount was analyzed per the requirements of the 2015 International Building Code as modified by the 2018 Connecticut State Building Code considering a nominal design wind speed of 97 mph for Wethersfield as required in Appendix N of the 2018 Connecticut State Building Code.

A structural analysis of tower and foundation needs to be completed prior to any work.
Based on our review of the installation, it is our opinion that the subject antenna mount has sufficient capacity to support the aforementioned antenna configuration. If there are any questions regarding this matter, please feel free to call.


Structural Engineer


Prepared by:


Fernando J. Palacios
Engineer

CENTEK Engineering, Inc.
Structural Analysis - Mount Analysis
T-Mobile Site Ref. ~ CTHA506A
Wethersfield, CT
May 03, 2019

## Section2-Calculations

## Development of Design Heights, Exposure Coefficients,

## and Velocity Pressures Per TIA-222-G

## Wind Speeds

| Basic Wind Speed | $\mathrm{V}:=97$ | mph |
| ---: | :--- | :--- |
| Basic Wind Speed with Ice | $\mathrm{V}_{\mathrm{i}}:=50$ | mph |

Input
Structure Type =
Structure Category =
Structure Type:= Pole
(User Input)

Exposure Category =
SC:=11 ph
(User Input - 2018 CSBC Appendix N)
(User Input per Annex B of TIA-222-G)

| Structure Type = | Structure_Type:= Pole |  | (User Input) |
| :---: | :---: | :---: | :---: |
| Structure Category = | SC: $=11$ |  | (User Input) |
| Exposure Category = | Exp : = C |  | (User Input) |
| Structure Height = | $\mathrm{h}:=103.5$ | ft | (User Input) |
| Height to Center of Antennas = | $\mathrm{z}:=95$ | ft | (User Input) |
| Radial Ice Thickness = | $\mathrm{t}_{\mathrm{i}}:=1$ | in | (User Input per Annex B of TIA-222-G) |
| Radial Ice Density = | Id := 56.00 | pcf | (User Input) |
| Topograpic Factor = | $\mathrm{K}_{\text {zt }}:=1.0$ |  | (User Input) |
|  | $\mathrm{K}_{\mathrm{a}}:=1.0$ |  | (User Input) |
| Gust Response Factor = | $\mathrm{G}_{\mathrm{H}}=1.1$ |  | (User Input) |

## Output

Wind Direction Probability Factor $=$

$$
\mathrm{K}_{\mathrm{iz}}:=\left(\frac{\mathrm{z}}{33}\right)^{0.1}=1.112
$$

Velocity Pressure Coefficient Antennas =

Velocity Pressure w/o Ice Antennas =

Velocity Pressure with Ice Antennas =

$$
\mathrm{t}_{\mathrm{iz}}:=2.0 \cdot \mathrm{t}_{\mathrm{i}} \cdot \mathrm{I}_{\text {ice }} \cdot \mathrm{K}_{\mathrm{iz}} \cdot \mathrm{~K}_{\mathrm{zt}}^{0.35}=2.223
$$

$\mathrm{K}_{\mathrm{d}}: \left.=\|$| if Structure_Type $=$ Pole |
| :--- |
| $\\| 0.95$ |
| if Structure_Type $=$ Lattice |
| $\\| 0.85$ | \right\rvert\,$=0.95$

I Wind $: \left.=\| \begin{gathered}\text { if } \mathrm{SC}=1 \\ \| \mathrm{S} \\ \| .87 \\ \text { if } \mathrm{SC}=2 \\ \| \\ \| 1.00 \\ \text { if } \mathrm{SC}=3 \\ \| 1.15\end{gathered} \right\rvert\,=1$
I Wind_w_Ice: $=\left|\begin{array}{c}\text { if } \mathrm{SC}=1 \\ \| \\ 0 \\ \text { if } \mathrm{SC}=2 \\ \| 1.00 \\ \text { if } \mathrm{SC}=3 \\ \| 1.00\end{array}\right|=1$
$I_{\text {ice }}: \left.=\| \begin{gathered}\text { if } S C=1 \\ \| 0 \\ \text { if } S C=2 \\ \| 1.00 \\ \text { if } S C=3 \\ \| 1.25\end{gathered} \right\rvert\,=1$

$$
\mathrm{KZ}:=2.01 \cdot\left(\left(\frac{\mathrm{z}}{\mathrm{zg}}\right)\right)^{\bar{\alpha}}=1.252
$$

$$
q z:=0.00256 \cdot K_{d} \cdot K z \cdot V^{2} \cdot I_{\text {Wind }}=28.65
$$

$q Z_{i c e}:=0.00256 \cdot K_{d} \cdot K z \cdot V_{i}{ }^{2} \cdot I_{\text {Wind }}=7.612 \mathrm{psf}$

## Location:

Rev. 0: 05/03/19

Wethersfield, CT
Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.22

## Development of Wind \& Ice Load on Antennas

## Antenna Data:

| Antenna Model $=$ | RFS APXVAARR24_43-U-NA20 |  |  |
| ---: | :--- | ---: | ---: |
| Antenna Shape $=$ | Flat | (User Input) |  |
| Antenna Height $=$ | $\mathrm{L}_{\text {ant }}:=95.9$ | in | (User Input) |
| Antenna Width $=$ | $\mathrm{W}_{\text {ant }}:=19.7$ | in | (User Input) |
| Antenna Thickness $=$ | $\mathrm{T}_{\text {ant }}:=8.7$ | in | (User Input) |
| Antenna Weight $=$ | $\mathrm{WT}_{\text {ant }}:=133.4$ | Ibs | (User Input) |

## Wind Load (without ice)

| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\text {antF }}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{W}_{\mathrm{ant}}}{144}=13.1$ | sf |
| :--- | :--- | :--- |
| Total Antenna Wind Force Front $=$ | $\mathrm{F}_{\mathrm{ant}}:=\mathrm{qZ} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\mathrm{ant}} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\mathrm{antF}}=540$ | lbs |
| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\mathrm{ants}}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{T}_{\mathrm{ant}}}{144}=5.8$ | sf |
| Total Antenna Wind Force Side $=$ | $\mathrm{F}_{\mathrm{ant}}:=\mathrm{qZ} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\mathrm{ant}} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\mathrm{ants}}=238$ | lbs |

## Wind Load (with ice)

| Surface Area for One Antenna w/ Ice = | $\mathrm{SA}_{\text {ICEantF }}:=\frac{\left(\mathrm{L}_{\mathrm{ant}}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=16.8$ | sf |
| :---: | :---: | :---: |
| Total Antenna Wind Force w/ Ice Front = | $\mathrm{Fi}_{\text {ant }}:=\mathrm{qz} \mathrm{i}_{\text {ice }} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca} \mathrm{ant} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICEantF }}=184$ | lbs |
| Surface Area for One Antenna w/ Ice = | $\mathrm{SA}_{\text {ICEants }}:=\frac{\left(\mathrm{L}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=9.2$ | sf |
| Total Antenna Wind Force w/ Ice Side = | $\mathrm{Fi}_{\text {ant }}:=\mathrm{qz} \mathrm{ice} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca} \mathrm{a}_{\text {ant }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICEantS }}=100$ | lbs |

## Gravity Load (without ice)

Weight of All Antennas =
$W T_{\text {ant }} \cdot N_{\text {ant }}=133$
lbs

## Gravity Loads (ice only)

Volume of Each Antenna =
$\mathrm{V}_{\text {ant }}:=\mathrm{L}_{\text {ant }} \cdot \mathrm{W}_{\text {ant }} \cdot \mathrm{T}_{\text {ant }}=2 \cdot 10^{4} \quad \mathrm{cu}$ in

Volume of Ice on Each Antenna =
$\mathrm{V}_{\text {ice }}:=\left(\mathrm{L}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)-\mathrm{V}_{\text {ant }}=2 \cdot 10^{4}$
cu in
Weight of Ice on Each Antenna =

Weight of Ice on All Antennas =
$W_{\text {ICEant }}:=\frac{V_{\text {ice }}}{1728} \cdot I d=500$
$W_{\text {ICEant }} \cdot N_{\text {ant }}=500$

Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.22

## Development of Wind \& Ice Load on Antennas

## Antenna Data:

| Antenna Model $=$ | Ericsson AIR 32 KRD901146-1_B66A_B2A |  |  |
| ---: | :--- | ---: | ---: |
| Antenna Shape $=$ | Flat | in(User Input) <br> (User Input) |  |
| Antenna Height $=$ | $\mathrm{L}_{\text {ant }}:=56.6$ | in | (User Input) |
| Antenna Width $=$ | $\mathrm{W}_{\text {ant }}:=12.9$ | in | (User Input) |
| Antenna Thickness $=$ | $\mathrm{T}_{\text {ant }}:=8.7$ | lbs | (User Input) |
| Antenna Weight $=$ | $\mathrm{WT}_{\text {ant }}:=133$ |  | (User Input) |

## Wind Load (without ice)

| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\mathrm{antF}}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{W}_{\mathrm{ant}}}{144}=5.1$ | sf |
| :--- | :--- | :--- |
| Total Antenna Wind Force Front $=$ | $\mathrm{F}_{\mathrm{ant}}:=\mathrm{qZ} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\mathrm{ant}} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\mathrm{antF}}=205$ | lbs |
| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\text {ants }}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{T}_{\mathrm{ant}}}{144}=3.4$ | sf |

## Wind Load (with ice)

| Surface Area for One Antenna w/ Ice $=$ | $\mathrm{SA}_{\text {ICEantF }}:=\frac{\left(\mathrm{L}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=7.4$ | sf |
| :--- | :--- | :--- |
| Total Antenna Wind Force $\mathrm{w} /$ Ice Front $=$ | $\mathrm{Fi}_{\text {ant }}:=\mathrm{qZ}_{\mathrm{ice}} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {ant }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICE antF }}=79$ | lbs |
| Surface Area for One Antenna w/ Ice $=$ | $\mathrm{SA}_{\text {ICEants }}:=\frac{\left(\mathrm{L}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{i}}\right)}{144}=5.6$ | sf |
| Total Antenna Wind Force $\mathrm{w} /$ Ice Side $=$ | $\mathrm{Fi}_{\text {ant }}:=\mathrm{qz}_{\mathrm{ice}} \cdot \mathrm{G}_{H} \cdot \mathrm{Ca}_{\text {ant }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICEants }}=60$ | lbs |

## Gravity Load (without ice)

| Weight of All Antennas = | W $\mathrm{T}_{\text {ant }} \cdot \mathrm{N}_{\text {ant }}=133$ | Ibs |
| :---: | :---: | :---: |
| Gravity Loads (ice only) |  |  |
| Volume of Each Antenna = | $\mathrm{V}_{\text {ant }}:=\mathrm{L}_{\text {ant }} \cdot \mathrm{W}_{\text {ant }} \cdot \mathrm{T}_{\text {ant }}=6352$ | cu in |
| Volume of Ice on Each Antenna = | $\mathrm{V}_{\text {ice }}=\left(\mathrm{L}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {ant }}\right.$ | $\mathrm{V}_{\text {ant }}=7568$ |
| Weight of Ice on Each Antenna = | $W_{\text {ICEant }}:=\frac{V_{\text {ice }}}{1728} \cdot I d=245$ | lbs |
| Weight of Ice on All Antennas = | $\mathrm{W}_{\text {ICEant }} \cdot \mathrm{N}_{\text {ant }}=245$ | lbs |

Rev. 0: 05/03/19

Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.22

## Development of Wind \& Ice Load on Antennas

## Antenna Data:

| Antenna Model = | Ericsson - AIR21 KRC118023-1_B2P_B4A |  |  |
| :---: | :---: | :---: | :---: |
| Antenna Shape = | Flat |  | (User Input) |
| Antenna Height = | $\mathrm{L}_{\text {ant }}:=55.9$ | in | (User Input) |
| Antenna Width = | $\mathrm{W}_{\text {ant }}:=12.1$ | in | (User Input) |
| Antenna Thickness = | $\mathrm{T}_{\text {ant }}:=7.9$ | in | (User Input) |
| Antenna Weight = | $W T_{\text {ant }}:=91.5$ | lbs | (User Input) |
| Number of Antennas = | $\mathrm{Nant}:=1$ |  | (User Input) |
| Antenna Aspect Ratio = | $\mathrm{Ar}_{\mathrm{ant}}:=\frac{\mathrm{L}_{\mathrm{ant}}}{\mathrm{~W}_{\mathrm{ant}}}=4.6$ |  |  |
| Antenna Force Coefficient $=$ | $\mathrm{Ca}_{\text {ant }}=1.29$ |  |  |

## Wind Load (without ice)

| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\text {antF }}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{W}_{\mathrm{ant}}}{144}=4.7$ | sf |
| :--- | :--- | :--- |
| Total Antenna Wind Force Front $=$ | $\mathrm{F}_{\mathrm{ant}}:=\mathrm{qZ} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\mathrm{ant}} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {antF }}=192$ | lbs |
| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\mathrm{ants}}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{T}_{\mathrm{ant}}}{144}=3.1$ | sf |
| Total Antenna Wind Force Side $=$ | $\mathrm{F}_{\mathrm{ant}}:=\mathrm{qZ} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\mathrm{ant}} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ants }}=125$ | lbs |

## Wind Load (with ice)

| Surface Area for One Antenna w/ Ice = | $S A_{\text {ICE antF }}:=\frac{\left(\mathrm{L}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=6.9$ | sf |
| :---: | :---: | :---: |
| Total Antenna Wind Force w/ Ice Front = | $\mathrm{Fi}_{\text {ant }}:=\mathrm{qZ} \mathrm{ice} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {ant }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICEantF }}=75$ | lbs |
| Surface Area for One Antenna w/ Ice = | $\mathrm{SA}_{1 \mathrm{CE} \text { ants }}:=\frac{\left(\mathrm{L}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=5.2$ | sf |
| Total Antenna Wind Force w/ Ice Side = | $\mathrm{Fi}_{\text {ant }}:=\mathrm{q} \mathrm{Z}_{\text {ice }} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{C} \mathrm{a}_{\text {ant }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICEants }}=56$ | lbs |

Gravity Load (without ice)


Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.22

## Development of Wind \& Ice Load on RRUS's

RRUS Data:

RRUS Model = RRUS Shape = RRUS Height = RRUS Width = RRUS Thickness = RRUS Weight = Number of RRUS's =

RRUS Aspect Ratio $=\quad \operatorname{Ar}_{\text {RRUS }}:=\frac{L_{\text {RRUS }}}{W_{\text {RRUS }}}=1.1$
RRUS Force Coefficient =

## Wind Load (without ice)

Surface Area for One RRUS
Total RRUS Wind Force =

Surface Area for One RRUS =
Total RRUS Wind Force =
Ericsson 4449 B71B12

| Flat |  |
| :--- | :--- |
| $L_{\text {RRUS }}:=14.9$ | in |
| $W_{\text {RRUS }}:=13.2$ | in |
| $T_{\text {RRUS }}:=10.4$ | in |
| $W_{\text {RRUS }}:=74$ | lbs |
| $N_{\text {RRUS }}:=1$ |  |
| Ar $_{\text {RRUS }}:=\frac{L_{\text {RRUS }}}{W_{\text {RRUS }}}=1.1$ |  |

$C a_{\text {RRUS }}=1.2$
$\mathrm{SA}_{\text {RRUSF }}:=\frac{\mathrm{L}_{\text {RRUS }} \cdot \mathrm{W}_{\text {RRUS }}}{144}=1.4 \quad \mathrm{sf}$
$\mathrm{F}_{\text {RRUS }}:=\mathrm{qz} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {RRUSF }}=52 \mathrm{lbs}$
$\mathrm{SA}_{\text {RRUSS }}:=\frac{\mathrm{L}_{\text {RRUS }} \cdot \mathrm{T}_{\text {RRUS }}}{144}=1.1 \quad \mathrm{sf}$
$\mathrm{F}_{\text {RRUS }}:=\mathrm{qz} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {RRUSS }}=41 \quad \mathrm{lbs}$

## Wind Load (with ice)

Surface Area for One RRUS w/ Ice =

Total RRUS Wind Force w/ Ice =

Surface Area for One RRUS w/ Ice =

Total RRUS Wind Force w/ Ice =
$\mathrm{SA}_{\text {ICERRUSF }}:=\frac{\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=2.4 \mathrm{sf}$
$\mathrm{Fi}_{\text {RRUS }}:=\mathrm{qZ} \mathrm{Z}_{\mathrm{ie}} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot S \mathrm{I}_{\text {ICERRUSF }}=24 \quad \mathrm{lbs}$
$\mathrm{SA}_{\text {ICERRUSS }}:=\frac{\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=2 \quad \mathrm{sf}$
$\mathrm{Fi}_{\text {RRUS }}:=\mathrm{qZ} \mathrm{Z}_{\mathrm{ie}} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{C} \mathrm{a}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA} \mathrm{I}_{\text {ICERRUSS }}=20 \quad \mathrm{lbs}$

## Gravity Load (without ice)

Weight of All RRUSs $=\quad W_{\text {RRUS }} \cdot N_{\text {RRUS }}=74 \quad$ lbs
Gravity Loads (ice only)
Volume of Each RRUS $=\quad V_{\text {RRUS }}:=L_{\text {RRUS }} \cdot W_{\text {RRUS }} \cdot T_{\text {RRUS }}=2045 \quad c u$ in

Volume of Ice on Each RRUS
$\mathrm{V}_{\text {ice }}:=\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)-\mathrm{V}_{\text {RRUS }}=3023$
cu in
Weight of Ice on Each RRUS $=\quad W_{\text {ICERRUS }}:=\frac{V_{\text {ice }}}{1728} \cdot 1 \mathrm{~d}=98 \quad$ Ibs

Weight of Ice on All RRUSs =
$W_{\text {ICERRUS }} \cdot N_{\text {RRUS }}=98$
lbs


| Centek | CTHA506A - Mount Member Framing |  |
| :---: | :---: | :---: |
| FJP |  | May 3, 2019 at 12:28 PM |
| 19027.22 |  | CTHA506A_AMA.r3d |

Model Name

## (Global) Model Settings

| Display Sections for Member Calcs | 5 |
| :---: | :---: |
| Max Internal Sections for Member Calcs | 97 |
| Include Shear Deformation? | Yes |
| Increase Nailing Capacity for Wind? | Yes |
| Include Warping? | Yes |
| Trans Load Btwn Intersecting Wood Wall? | Yes |
| Area Load Mesh (in^2) | 144 |
| Merge Tolerance (in) | . 12 |
| P-Delta Analysis Tolerance | 0.50\% |
| Include P-Delta for Walls? | Yes |
| Automatically Iterate Stiffness for Walls? | Yes |
| Max Iterations for Wall Stiffness | 3 |
| Gravity Acceleration (ft/sec^2) | 32.2 |
| Wall Mesh Size (in) | 12 |
| Eigensolution Convergence Tol. (1.E-) | 4 |
| Vertical Axis | Y |
| Global Member Orientation Plane | XZ |
| Static Solver | Sparse Accelerated |
| Dynamic Solver | Accelerated Solver |
| Hot Rolled Steel Code | AISC 14th(360-10): LRFD |
| Adjust Stiffness? | Yes(Iterative) |
| RISAConnection Code | AISC 14th(360-10): ASD |
| Cold Formed Steel Code | AISI S100-10: ASD |
| Wood Code | AWC NDS-12: ASD |
| Wood Temperature | < 100F |
| Concrete Code | ACI 318-11 |
| Masonry Code | ACI 530-11: ASD |
| Aluminum Code | AA ADM1-10: ASD - Building |
| Stainless Steel Code | AISC 14th(360-10): ASD |
| Adjust Stiffness? | Yes(Iterative) |
| Number of Shear Regions | 4 |
| Region Spacing Increment (in) | 4 |
| Biaxial Column Method | Exact Integration |
| Parme Beta Factor (PCA) | . 65 |
| Concrete Stress Block | Rectangular |
| Use Cracked Sections? | Yes |
| Use Cracked Sections Slab? | No |
| Bad Framing Warnings? | No |
| Unused Force Warnings? | Yes |
| Min 1 Bar Diam. Spacing? | No |
| Concrete Rebar Set | REBAR_SET_ASTMA615 |
| Min \% Steel for Column | 1 |
| Max \% Steel for Column | 8 |

Model Name
(Global) Model Settings, Continued

| Seismic Code | ASCE 7-10 |
| :---: | :---: |
| Seismic Base Elevation (ft) | Not Entered |
| Add Base Weight? | Yes |
| Ct X | . 02 |
| Ct Z | . 02 |
| T X (sec) | Not Entered |
| T Z (sec) | Not Entered |
| R X | 3 |
| R Z | 3 |
| Ct Exp. X | . 75 |
| Ct Exp. Z | . 75 |
| SD1 | 1 |
| SDS | 1 |
| S1 | 1 |
| TL (sec) | 5 |
| Risk Cat | I or II |
| Drift Cat | Other |
| Om Z | 1 |
| Om X | 1 |
| Cd Z | 1 |
| Cd X | 1 |
| Rho Z | 1 |
| Rho X | 1 |
|  |  |
| Footing Overturning Safety Factor | 1 |
| Optimize for OTM/Sliding | No |
| Check Concrete Bearing | No |
| Footing Concrete Weight (k/ft^3) | 150.001 |
| Footing Concrete f'c (ksi) | 4 |
| Footing Concrete Ec (ksi) | 3644 |
| Lambda | 1 |
| Footing Steel fy (ksi) | 60 |
| Minimum Steel | 0.0018 |
| Maximum Steel | 0.0075 |
| Footing Top Bar | \#3 |
| Footing Top Bar Cover (in) | 2 |
| Footing Bottom Bar | \#3 |
| Footing Bottom Bar Cover (in) | 3.5 |
| Pedestal Bar | \#3 |
| Pedestal Bar Cover (in) | 1.5 |
| Pedestal Ties | \#3 |

Hot Rolled Steel Properties

|  | Label | E [ksi] | G [ksi] | Nu | Therm ( $\backslash 1$ | Density[k/ft^3] | Yield[ksi] | Ry | Fu[ksi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A36 Gr. 36 | 29000 | 11154 | . 3 | . 65 | 49 | 36 | 1.5 | 58 | 1.2 |
| 2 | A572 Gr. 50 | 29000 | 11154 | . 3 | . 65 | 49 | 50 | 1.1 | 58 | 1.2 |
| 3 | A992 | 29000 | 11154 | . 3 | . 65 | 49 | 50 | 1.1 | 58 | 1.2 |
| 4 | A500 Gr. 42 | 29000 | 11154 | . 3 | . 65 | 49 | 42 | 1.3 | 58 | 1.1 |
| 5 | A500 Gr. 46 | 29000 | 11154 | . 3 | . 65 | . 49 | 46 | 1.2 | 58 | 1.1 |
| 6 | A53 Grade B | 29000 | 11154 | . 3 | . 65 | 49 | 35 | 1.5 | 58 | 1.2 |

## Hot Rolled Steel Section Sets

| Label |  | Shape | Type | Design List | Material | Design ... A [in2] |  | lyy [in4] Izz [in4] |  | J [in4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | (E)Outrigger | HSS4X4X4 | Beam | Tube | A500 Gr. 46 | Typical | 3.37 | 7.8 | 7.8 | 12.8 |
| 2 | (E) Horz | PIPE 3.0 | Beam | Pipe | A53 Grade B | Typical | 2.07 | 2.85 | 2.85 | 5.69 |
| 3 | (E) Antenna Mast | PIPE_2.0 | Column | Pipe | A53 Grade B | Typical | 1.02 | 627 | 627 | 1.25 |
| 4 | (E) Vert | PIPE 4.0 | Column | Pipe | A53 Grade B | Typical | 2.96 | 6.82 | 6.82 | 13.6 |
| 5 | (P) Antenna Mast | PIPE_2.0 | Column | Pipe | A53 Grade B | Typical | 1.02 | . 627 | . 627 | 1.25 |
| 6 | (P) Handrails | PIPE 2.0 | Column | Pipe | A53 Grade B | Typical | 1.02 | . 627 | . 627 | 1.25 |
| 7 | (P) Handrail Co... | L2.5x2.5x4 | Column | Pipe | A36 Gr. 36 | Typical | 1.19 | . 692 | . 692 | . 026 |

## Hot Rolled Steel Design Parameters

|  | Label | Shape | Length[ft] | Lbyy[ft] | Lbzz[ft] | Lcomp top[ft] | Lcomp bot[ft] | L-torqu. | Kyy | Kzz | Cb | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | (E)Outrigger | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 2 | M2 | (E) Vert | 1.5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 3 | M3 | (E) Horz | 12.5 | Segment | 6 | Lbyy | 6 | 6 |  |  |  | Lateral |
| 4 | M4 | (E) Antenna.. | 8 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 5 | M5 | (E) Antenna.. | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 6 | M6 | (E) Antenna.. | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 7 | M7 | (E)Outrigger | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 8 | M8 | (E) Vert | 1.5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 9 | M9 | (E) Horz | 12.5 | Segment | 6 | Lbyy | 6 | 6 |  |  |  | Lateral |
| 10 | M10 | (E) Antenna.. | 8 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 11 | M11 | (E) Antenna.. | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 12 | M12 | (E) Antenna.. | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 13 | M13 | (E)Outrigger | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 14 | M14 | (E) Vert | 1.5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 15 | M15 | (E) Horz | 12.5 | Segment | 6 | Lbyy | 6 | 6 |  |  |  | Lateral |
| 16 | M16 | (E) Antenna.. | 8 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 17 | M17 | (E) Antenna.. | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 18 | M18 | (E) Antenna.. | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 19 | M19 | (P) Handrails | 12.5 | Segment |  | Lbyy |  |  |  |  |  | Lateral |
| 20 | M20 | (P) Handrails | 12.5 | Segment |  | Lbyy |  |  |  |  |  | Lateral |
| 21 | M21 | (P) Handrails | 12.5 | Segment |  | Lbyy |  |  |  |  |  | Lateral |
| 22 | M22 | (P) Handrail.. | 926 | Segment |  | Lbyy |  |  |  |  |  | Lateral |
| 23 | M23 | (P) Handrail.. | . 926 | Segment |  | Lbyy |  |  |  |  |  | Lateral |
| 24 | M24 | (P) Handrail.. | . 926 | Segment |  | Lbyy |  |  |  |  |  | Lateral |

## Member Primary Data

|  | Label | I Joint | $J$ Joint | K Joint | Rotate(d.. | Section/Shape | Type | Design List | Material | Design Rul... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | N1 | N2 |  |  | (E)Outrigger | Beam | Tube | A500 Gr... | Typical |
| 2 | M2 | N3 | N4 |  |  | (E) Vert | Column | Pipe | A53 Gra... | Typical |
| 3 | M3 | N6 | N5 |  |  | (E) Horz | Beam | Pipe | A53 Gra... | Typical |
| 4 | M4 | N12 | N10 |  |  | (E) Antenna Mast | Column | Pipe | A53 Gra... | Typical |
| 5 | M5 | N11 | N9 |  |  | (E) Antenna Mast | Column | Pipe | A53 Gra... | Typical |
| 6 | M6 | N15 | N14 |  |  | (E) Antenna Mast | Column | Pipe | A53 Gra... | Typical |
| 7 | M7 | N17 | N18 |  |  | (E)Outrigger | Beam | Tube | A500 Gr... | Typical |
| 8 | M8 | N19 | N20 |  |  | (E) Vert | Column | Pipe | A53 Gra... | Typical |
| 9 | M9 | N22 | N21 |  |  | (E) Horz | Beam | Pipe | A53 Gra... | Typical |
| 10 | M10 | N28 | N26 |  |  | (E) Antenna Mast | Column | Pipe | A53 Gra... | Typical |
| 11 | M11 | N27 | N25 |  |  | (E) Antenna Mast | Column | Pipe | A53 Gra.. | Typical |

Member Primary Data (Continued)

|  | Label | I Joint | $J$ Joint | K Joint | Rotate(d.. | Section/Shape | Type | Design List | Material | Design Rul.. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | M12 | N31 | N30 |  |  | (E) Antenna Mast | Column | Pipe | A53 Gra... | Typical |
| 13 | M13 | N32 | N33 |  |  | (E)Outrigger | Beam | Tube | A500 Gr... | Typical |
| 14 | M14 | N34 | N35 |  |  | (E) Vert | Column | Pipe | A53 Gra... | Typical |
| 15 | M15 | N37 | N36 |  |  | (E) Horz | Beam | Pipe | A53 Gra... | Typical |
| 16 | M16 | N43 | N41 |  |  | (E) Antenna Mast | Column | Pipe | A53 Gra... | Typical |
| 17 | M17 | N42 | N40 |  |  | (E) Antenna Mast | Column | Pipe | A53 Gra... | Typical |
| 18 | M18 | N46 | N45 |  |  | (E) Antenna Mast | Column | Pipe | A53 Gra... | Typical |
| 19 | M19 | N48 | N47 |  |  | (P) Handrails | Column | Pipe | A53 Gra... | Typical |
| 20 | M20 | N57 | N58 |  |  | (P) Handrails | Column | Pipe | A53 Gra... | Typical |
| 21 | M21 | N53 | N52 |  |  | (P) Handrails | Column | Pipe | A53 Gra... | Typical |
| 22 | M22 | N50 | N59 |  | 180 | (P) Handrail Connector | Column | Pipe | A36 Gr. 36 | Typical |
| 23 | M23 | N49 | N55 |  | 90 | (P) Handrail Connector | Column | Pipe | A36 Gr. 36 | Typical |
| 24 | M24 | N60 | N54 |  | 180 | (P) Handrail Connector | Column | Pipe | A36 Gr. 36 | Typical |

Joint Coordinates and Temperatures

|  | Label | $\mathrm{X}[\mathrm{ft}]$ | Y [ft] | Z [ft] | Temp [F] | Detach From Dia... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | 0 | 0 | 0.854167 | 0 |  |
| 2 | N2 | 0 | 0 | 3.854167 | 0 |  |
| 3 | N3 | 0 | . 75 | 3.854167 | 0 |  |
| 4 | N4 | 0 | -. 75 | 3.854167 | 0 |  |
| 5 | N5 | 6.25 | 0 | 3.854167 | 0 |  |
| 6 | N6 | -6.25 | 0 | 3.854167 | 0 |  |
| 7 | N7 | 5.75 | 0 | 3.854167 | 0 |  |
| 8 | N8 | -5.75 | 0 | 3.854167 | 0 |  |
| 9 | N9 | 5.75 | -3 | 3.854167 | 0 |  |
| 10 | N10 | -5.75 | -4 | 3.854167 | 0 |  |
| 11 | N11 | 5.75 | 3 | 3.854167 | 0 |  |
| 12 | N12 | -5.75 | 4 | 3.854167 | 0 |  |
| 13 | N13 | 1.583333 | 0 | 3.854167 | 0 |  |
| 14 | N14 | 1.583333 | -3 | 3.854167 | 0 |  |
| 15 | N15 | 1.583333 | 3 | 3.854167 | 0 |  |
| 16 | N16 | 0 | 0 | 0 | 0 |  |
| 17 | N17 | 0.73973 | 0 | -0.427083 | 0 |  |
| 18 | N18 | 3.337806 | 0 | -1.927083 | 0 |  |
| 19 | N19 | 3.337806 | 75 | -1.927083 | 0 |  |
| 20 | N20 | 3.337806 | -. 75 | -1.927083 | 0 |  |
| 21 | N21 | 0.212806 | 0 | -7.339742 | 0 |  |
| 22 | N22 | 6.462806 | 0 | 3.485575 | 0 |  |
| 23 | N23 | 0.462806 | 0 | -6.906729 | 0 |  |
| 24 | N24 | 6.212806 | 0 | 3.052563 | 0 |  |
| 25 | N25 | 0.462806 | -3 | -6.906729 | 0 |  |
| 26 | N26 | 6.212806 | -4 | 3.052563 | 0 |  |
| 27 | N27 | 0.462806 | 3 | -6.906729 | 0 |  |
| 28 | N28 | 6.212806 | 4 | 3.052563 | 0 |  |
| 29 | N29 | 2.54614 | 0 | -3.29829 | 0 |  |
| 30 | N30 | 2.54614 | -3 | -3.29829 | 0 |  |
| 31 | N31 | 2.54614 | 3 | -3.29829 | 0 |  |
| 32 | N32 | -0.73973 | 0 | -0.427083 | 0 |  |
| 33 | N33 | -3.337806 | 0 | -1.927083 | 0 |  |
| 34 | N34 | -3.337806 | 75 | -1.927083 | 0 |  |


| Company | $:$Centek <br> Designer <br> Job Number <br> ANEMETSCHEK COMPANY <br> Model Name |
| :--- | :--- |

Joint Coordinates and Temperatures (Continued)

|  | Label | X [ft] | $\mathrm{Y}[\mathrm{ft}]$ | Z [ft] | Temp [F] | Detach From Dia... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 35 | N35 | -3.337806 | -. 75 | -1.927083 | 0 |  |
| 36 | N36 | -6.462806 | 0 | 3.485575 | 0 |  |
| 37 | N37 | -0.212806 | 0 | -7.339742 | 0 |  |
| 38 | N38 | -6.212806 | 0 | 3.052563 | 0 |  |
| 39 | N39 | -0.462806 | 0 | -6.906729 | 0 |  |
| 40 | N40 | -6.212806 | -3 | 3.052563 | 0 |  |
| 41 | N41 | -0.462806 | -4 | -6.906729 | 0 |  |
| 42 | N42 | -6.212806 | 3 | 3.052563 | 0 |  |
| 43 | N43 | -0.462806 | 4 | -6.906729 | 0 |  |
| 44 | N44 | -4.129473 | 0 | -0.555876 | 0 |  |
| 45 | N45 | -4.129473 | -3 | -0.555876 | 0 |  |
| 46 | N46 | -4.129473 | 3 | -0.555876 | 0 |  |
| 47 | N47 | 6.25 | 2.5 | 3.854167 | 0 |  |
| 48 | N48 | -6.25 | 2.5 | 3.854167 | 0 |  |
| 49 | N49 | 5.75 | 2.5 | 3.854167 | 0 |  |
| 50 | N50 | -5.75 | 2.5 | 3.854167 | 0 |  |
| 51 | N51 | 1.583333 | 2.5 | 3.854167 | 0 |  |
| 52 | N52 | 0.212806 | 2.5 | -7.339742 | 0 |  |
| 53 | N53 | 6.462806 | 2.5 | 3.485575 | 0 |  |
| 54 | N54 | 0.462806 | 2.5 | -6.906729 | 0 |  |
| 55 | N55 | 6.212806 | 2.5 | 3.052563 | 0 |  |
| 56 | N56 | 2.54614 | 2.5 | -3.29829 | 0 |  |
| 57 | N57 | -6.462806 | 2.5 | 3.485575 | 0 |  |
| 58 | N58 | -0.212806 | 2.5 | -7.339742 | 0 |  |
| 59 | N59 | -6.212806 | 2.5 | 3.052563 | 0 |  |
| 60 | N60 | -0.462806 | 2.5 | -6.906729 | 0 |  |
| 61 | N61 | -4.129473 | 2.5 | -0.555876 | 0 |  |
| 62 | N63 | 0 | 0 | 2.854167 | 0 |  |
| 63 | N65 | -2.471781 | 0 | -1.427083 | 0 |  |
| 64 | N67 | 2.471781 | 0 | -1.427083 | 0 |  |

Joint Boundary Conditions

|  | Joint Label | X [k/in] | Y [k/in] | Z [k/in] | X Rot.[k-ft/rad] | Y Rot.[k-ft/rad] | Z Rot.[k-ft/rad] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 2 | N17 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 3 | N32 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 4 | N63 |  |  |  |  |  |  |
| 5 | N65 |  |  |  |  |  |  |
| 6 | N67 |  |  |  |  |  |  |

Member Point Loads (BLC 2 : Dead Load)

| Member Label |  | Direction |  | Magnitude[k, $\mathrm{k}-\mathrm{ft}]$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M | Y | -.067 | Location[ft, \%] |
| 2 | M 10 | Y | -.067 | .5 |
| 3 | M 16 | Y | -.067 | .5 |
| 4 | M 4 | Y | -.067 | .5 |
| 5 | M 10 | Y | -.067 | 7.5 |
| 6 | M 16 | Y | -.067 | 7.5 |
| 7 | M 6 | -.067 | .5 |  |

Member Point Loads (BLC 2 : Dead Load) (Continued)

| Member Label | Direction |  | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 8 | M12 | Y | -.067 | .5 |
| 9 | M18 | Y | -.067 | .5 |
| 10 | M6 | Y | -.067 | 5.5 |
| 11 | M12 | Y | -.067 | 5.5 |
| 12 | M18 | Y | -.067 | 5.5 |
| 13 | M5 | Y | -.046 | .5 |
| 14 | M11 | Y | -.046 | .5 |
| 15 | M17 | Y | -.046 | .5 |
| 16 | M1 | Y | -.046 | 5.5 |
| 17 | M17 | Y | -.046 | 5.5 |
| 18 | M4 | Y | -.046 | 5.5 |
| 19 | M10 | Y | -.074 | 3 |
| 20 | M16 | Y | -.074 | 3 |
| 21 |  |  | -.074 | 3 |

Member Point Loads (BLC 3 : Ice Load)

| Member Labe |  | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M4 | Y | -. 25 | . 5 |
| 2 | M10 | Y | -. 25 | . 5 |
| 3 | M16 | Y | -. 25 | . 5 |
| 4 | M4 | Y | -. 25 | 7.5 |
| 5 | M10 | Y | -. 25 | 7.5 |
| 6 | M16 | Y | -. 25 | 7.5 |
| 7 | M6 | Y | -. 123 | . 5 |
| 8 | M12 | Y | -. 123 | . 5 |
| 9 | M18 | Y | -. 123 | . 5 |
| 10 | M6 | Y | -. 123 | 5.5 |
| 11 | M12 | Y | -. 123 | 5.5 |
| 12 | M18 | Y | -. 123 | 5.5 |
| 13 | M5 | Y | -. 113 | . 5 |
| 14 | M11 | Y | -. 113 | . 5 |
| 15 | M17 | Y | -. 113 | . 5 |
| 16 | M5 | Y | -. 113 | 5.5 |
| 17 | M11 | Y | -. 113 | 5.5 |
| 18 | M17 | Y | -. 113 | 5.5 |
| 19 | M4 | Y | -. 098 | 3 |
| 20 | M10 | Y | -. 098 | 3 |
| 21 | M16 | Y | -. 098 | 3 |

Member Point Loads (BLC 4 : Wind with Ice X)

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M4 | X | . 05 | . 5 |
| 2 | M4 | X | . 05 | 7.5 |
| 3 | M10 | X | . 092 | . 5 |
| 4 | M16 | X | . 092 | . 5 |
| 5 | M10 | X | . 092 | 7.5 |
| 6 | M16 | X | . 092 | 7.5 |
| 7 | M6 | X | . 03 | . 5 |
| 8 | M6 | X | . 03 | 5.5 |
| 9 | M12 | X | . 04 | . 5 |
| 10 | M18 | X | . 04 | . 5 |


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| :--- | :--- |

Member Point Loads (BLC 4 : Wind with Ice X) (Continued)

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 11 | M12 | X | . 04 | 5.5 |
| 12 | M18 | X | . 04 | 5.5 |
| 13 | M5 | X | . 028 | . 5 |
| 14 | M5 | X | . 028 | 5.5 |
| 15 | M11 | X | . 038 | . 5 |
| 16 | M17 | X | . 038 | . 5 |
| 17 | M11 | X | . 038 | 5.5 |
| 18 | M17 | X | . 038 | 5.5 |
| 19 | M4 | X | . 02 | 3 |

Member Point Loads (BLC 5 : Wind X)

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M4 | X | . 119 | . 5 |
| 2 | M4 | X | . 119 | 7.5 |
| 3 | M10 | X | . 27 | . 5 |
| 4 | M16 | X | . 27 | . 5 |
| 5 | M10 | X | . 27 | 7.5 |
| 6 | M16 | X | . 27 | 7.5 |
| 7 | M6 | X | . 069 | . 5 |
| 8 | M6 | X | . 069 | 5.5 |
| 9 | M12 | X | . 103 | . 5 |
| 10 | M18 | X | . 103 | . 5 |
| 11 | M12 | X | . 103 | 5.5 |
| 12 | M18 | X | . 103 | 5.5 |
| 13 | M5 | X | . 063 | . 5 |
| 14 | M5 | X | . 063 | 5.5 |
| 15 | M11 | X | . 096 | . 5 |
| 16 | M17 | X | . 096 | 5 |
| 17 | M11 | X | . 096 | 5.5 |
| 18 | M17 | X | . 096 | 5.5 |
| 19 | M4 | X | . 041 | 3 |

Member Point Loads (BLC 6 : Wind with Ice Z)

| Member Labe |  | Directio | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M4 | Z | . 092 | . 5 |
| 2 | M4 | Z | . 092 | 7.5 |
| 3 | M10 | Z | . 05 | . 5 |
| 4 | M16 | Z | . 05 | . 5 |
| 5 | M10 | Z | . 05 | 7.5 |
| 6 | M16 | Z | . 05 | 7.5 |
| 7 | M6 | Z | . 04 | . 5 |
| 8 | M6 | Z | . 04 | 5.5 |
| 9 | M12 | Z | . 03 | . 5 |
| 10 | M18 | Z | . 03 | . 5 |
| 11 | M12 | Z | . 03 | 5.5 |
| 12 | M18 | Z | . 03 | 5.5 |
| 13 | M5 | Z | . 038 | . 5 |
| 14 | M5 | Z | . 038 | 5.5 |
| 15 | M11 | Z | . 028 | . 5 |
| 16 | M17 | Z | . 028 | . 5 |
| 17 | M11 | Z | . 028 | 5.5 |

Member Point Loads (BLC 6 : Wind with Ice Z) (Continued)

| Member Label |  | Direction |  | Magnitude $[k, k-f t]$ |
| :---: | :---: | :---: | :---: | :---: |
| 18 | M17 | Z | .028 | 5.5 |
| 19 | M10 | $Z$ | .02 | 3 |
| 20 | M16 | Z | .02 | 3 |

Member Point Loads (BLC 7 : Wind Z)

| Member Label |  | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M4 | Z | . 27 | . 5 |
| 2 | M4 | Z | . 27 | 7.5 |
| 3 | M10 | Z | . 119 | . 5 |
| 4 | M16 | Z | . 119 | . 5 |
| 5 | M10 | Z | . 119 | 7.5 |
| 6 | M16 | Z | . 119 | 7.5 |
| 7 | M6 | Z | . 103 | . 5 |
| 8 | M6 | Z | . 103 | 5.5 |
| 9 | M12 | Z | . 069 | . 5 |
| 10 | M18 | Z | . 069 | . 5 |
| 11 | M12 | Z | . 069 | 5.5 |
| 12 | M18 | Z | . 069 | 5.5 |
| 13 | M5 | Z | . 096 | . 5 |
| 14 | M5 | Z | . 096 | 5.5 |
| 15 | M11 | Z | . 063 | . 5 |
| 16 | M17 | Z | . 063 | . 5 |
| 17 | M11 | Z | . 063 | 5.5 |
| 18 | M17 | Z | . 063 | 5.5 |
| 19 | M10 | Z | . 041 | 3 |
| 20 | M16 | Z | . 041 | 3 |

## Member Distributed Loads (BLC 4 : Wind with Ice X)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/.. | Start Location [ft,\%] | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M20 | X | . 002 | . 002 | 0 | 0 |
| 2 | M21 | X | . 002 | . 002 | 0 | 0 |
| 3 | M22 | X | . 002 | . 002 | 0 | 0 |
| 4 | M23 | X | . 002 | . 002 | 0 | 0 |
| 5 | M15 | X | . 002 | . 002 | 0 | 0 |
| 6 | M9 | X | . 002 | . 002 | 0 | 0 |
| 7 | M2 | X | . 003 | . 003 | 0 | 0 |
| 8 | M8 | X | . 003 | . 003 | 0 | 0 |
| 9 | M14 | X | . 003 | . 003 | 0 | 0 |
| 10 | M1 | X | . 003 | . 003 | 0 | 0 |
| 11 | M7 | X | . 003 | . 003 | 0 | 0 |
| 12 | M13 | X | . 003 | . 003 | 0 | 0 |

Member Distributed Loads (BLC 5 : Wind X)

| Member Label |  |  |  |  |  |  |  |  | Direction |  | Start Magnitude[k/ft,F,ksf] |  | End Magnitude[k/..Start Location[ft,\%] End Location $[\mathrm{ft}, \%]$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M 20 | X | .006 | .006 | 0 | 0 |  |  |  |  |  |  |  |  |
| 2 | M 21 | X | .006 | .006 | 0 | 0 |  |  |  |  |  |  |  |  |
| 3 | M 22 | X | .006 | .006 | 0 | 0 |  |  |  |  |  |  |  |  |
| 4 | M 23 | X | .006 | .006 | 0 | 0 |  |  |  |  |  |  |  |  |
| 5 | M 15 | X | .008 | .008 | 0 | 0 |  |  |  |  |  |  |  |  |


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| :--- | :--- |

## Member Distributed Loads (BLC 5 : Wind X) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/.. | Start Location[ft,\%] | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | M9 | X | . 008 | . 008 | 0 | 0 |
| 7 | M2 | X | . 011 | . 011 | 0 | 0 |
| 8 | M8 | X | . 011 | . 011 | 0 | 0 |
| 9 | M14 | X | . 011 | . 011 | 0 | 0 |
| 10 | M1 | X | . 01 | . 01 | 0 | 0 |
| 11 | M7 | X | . 01 | . 01 | 0 | 0 |
| 12 | M13 | X | . 01 | . 01 | 0 | 0 |

## Member Distributed Loads (BLC 6 : Wind with Ice Z)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/... | Start Location[ft,\%] | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | . 002 | . 002 | 0 | 0 |
| 2 | M20 | Z | . 002 | . 002 | 0 | 0 |
| 3 | M21 | Z | . 002 | . 002 | 0 | 0 |
| 4 | M22 | Z | . 002 | . 002 | 0 | 0 |
| 5 | M23 | Z | . 002 | . 002 | 0 | 0 |
| 6 | M24 | Z | . 002 | . 002 | 0 | 0 |
| 7 | M15 | Z | . 002 | . 002 | 0 | 0 |
| 8 | M9 | Z | . 002 | . 002 | 0 | 0 |
| 9 | M3 | Z | . 002 | . 002 | 0 | 0 |
| 10 | M2 | Z | . 003 | . 003 | 0 | 0 |
| 11 | M8 | Z | . 003 | . 003 | 0 | 0 |
| 12 | M14 | Z | . 003 | . 003 | 0 | 0 |
| 13 | M7 | Z | . 003 | . 003 | 0 | 0 |
| 14 | M13 | Z | . 003 | . 003 | 0 | 0 |

## Member Distributed Loads (BLC 7 : Wind Z)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/.. | Start Location[ft,\%] | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | . 006 | . 006 | 0 | 0 |
| 2 | M24 | Z | . 006 | . 006 | 0 | 0 |
| 3 | M20 | Z | . 006 | . 006 | 0 | 0 |
| 4 | M21 | Z | . 006 | . 006 | 0 | 0 |
| 5 | M22 | Z | . 006 | . 006 | 0 | 0 |
| 6 | M23 | Z | . 006 | . 006 | 0 | 0 |
| 7 | M15 | Z | . 008 | . 008 | 0 | 0 |
| 8 | M9 | Z | . 008 | . 008 | 0 | 0 |
| 9 | M3 | Z | . 008 | . 008 | 0 | 0 |
| 10 | M2 | Z | . 011 | . 011 | 0 | 0 |
| 11 | M8 | Z | . 011 | . 011 | 0 | 0 |
| 12 | M14 | Z | . 011 | . 011 | 0 | 0 |
| 13 | M7 | Z | . 01 | . 01 | 0 | 0 |
| 14 | M13 | Z | . 01 | . 01 | 0 | 0 |

## Basic Load Cases

| BLC Description |  | Category | X Gravity Y Gravity Z Gravity |  |  | Joint | Point | Distribu. | .Area(M... | Surface... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Self Weight | None |  | -1 |  |  |  |  |  |  |
| 2 | Dead Load | None |  |  |  |  | 21 |  |  |  |
| 3 | Ice Load | None |  |  |  |  | 21 |  |  |  |
| 4 | Wind with Ice $X$ | None |  |  |  |  | 19 | 12 |  |  |
| 5 | Wind X | None |  |  |  |  | 19 | 12 |  |  |

## Basic Load Cases (Continued)

|  | BLC Description | Category | X Gravity | Y Gravity | Z Gravity | Joint | Point | Distribu | .Area(M.. | Surface... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | Wind with Ice Z | None |  |  |  |  | 20 | 14 |  |  |
| 7 | Wind Z | None |  |  |  |  | 20 | 14 |  |  |

## Load Combinations

Description

| 1 | $1.2 \mathrm{D}+1.6 \mathrm{~W}(\mathrm{X}$-dire... | Y |
| :---: | :---: | :---: |
| 2 | $0.9 \mathrm{D}+1.6 \mathrm{~W}(\mathrm{X}$ dire... | Y |
| 3 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} .$. |  |
| 4 | $1.2 \mathrm{D}+1.6 \mathrm{~W}(\mathrm{Z}$-direc... | Y |
| 5 | $0.9 \mathrm{D}+1.6 \mathrm{~W}(\mathrm{Z}$-direc.. | Y |
| 6 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} .$. |  |

Solve PDel...S...B...Fa... BLC Fa... BLC Fa... BLC Fa...BLC Fa...B...Fa...BLC Fa...B...Fa...B...Fa...B...Fa... | Yes | Y |  | 1 | 1.2 | 2 | 1.2 | 5 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

## Envelope Joint Reactions

| Joint |  |  | X [k] | LC | Y [k] | LC | Z [k] | LC | MX [k-ft] | LC | MY [k-ft] | LC | MZ [k-ft] | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | max | . 043 | 6 | 1.961 | 6 | . 15 | 3 | -1.415 | 5 | -. 121 | 6 | 492 | 1 |
| 2 |  | min | -1.481 | 2 | . 556 | 2 | -1.188 | 5 | -5.118 | 3 | -3.403 | 1 | -. 129 | 5 |
| 3 | N17 | max | . 031 | 6 | 1.958 | 3 | -. 225 | 3 | 2.639 | 6 | 3.071 | 5 | 4.423 | 6 |
| 4 |  | min | -1.572 | 2 | . 508 | 5 | -1.473 | 4 | 43 | 2 | . 576 | 3 | 1.463 | 5 |
| 5 | N32 | max | . 298 | 5 | 1.853 | 6 | . 463 | 2 | 2.504 | 3 | 3.163 | 2 | -1.395 | 5 |
| 6 |  | min | -1.642 | 1 | . 388 | 2 | -1.653 | 4 | . 196 | 5 | -3.902 | 4 | -4.595 | 3 |
| 7 | Totals: | max | 0 | 6 | 5.687 | 6 | 0 | 3 |  |  |  |  |  |  |
| 8 |  | min | -4.679 | 1 | 1.858 | 2 | -4.298 | 4 |  |  |  |  |  |  |

## Envelope Joint Displacements

| Joint |  |  | X [in] | LC | Y [in] | LC | Z [in] | LC | X Rotation [rad] | LC Y Rotatio... LC Z Rotatio... LC |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | max | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 |
| 2 |  | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 |
| 3 | N2 | max | . 086 | 1 | -. 023 | 5 | 0 | 5 | 5.53e-03 | 3 | $2.893 \mathrm{e}-03$ | 1 | $3.908 \mathrm{e}-04$ | 5 |
| 4 |  | min | . 007 | 6 | -. 143 | 3 | 0 | 3 | $9.834 \mathrm{e}-05$ | 5 | $4.427 \mathrm{e}-04$ | 6 | -1.489e-03 | 1 |
| 5 | N3 | max | . 1 | 1 | -. 023 | 5 | . 05 | 3 | 5.53e-03 | 3 | 2.893e-03 | 1 | $3.908 \mathrm{e}-04$ | 5 |
| 6 |  | min | . 01 | 6 | -. 143 | 3 | . 001 | 5 | $9.944 \mathrm{e}-05$ | 5 | $4.427 \mathrm{e}-04$ | 6 | -1.49e-03 | 1 |
| 7 | N4 | max | . 073 | 1 | -. 023 | 5 | 0 | 5 | 5.53e-03 | 3 | 2.893e-03 | 1 | $3.908 \mathrm{e}-04$ | 5 |
| 8 |  | min | . 004 | 6 | -. 143 | 3 | -. 05 | 3 | $9.724 \mathrm{e}-05$ | 5 | $4.427 \mathrm{e}-04$ | 6 | -1.487e-03 | 1 |
| 9 | N5 | max | . 087 | 1 | -. 181 | 5 | . 298 | 5 | $3.394 \mathrm{e}-03$ | 1 | 2.045e-03 | 3 | -2.104e-03 | 5 |
| 10 |  | min | . 006 | 6 | -. 602 | 3 | -. 133 | 3 | -3.378e-03 | 5 | -5.357e-03 | 5 | -6.169e-03 | 3 |
| 11 | N6 | max | . 087 | 1 | -. 057 | 2 | . 689 | 5 | $3.874 \mathrm{e}-03$ | 3 | 1.169e-02 | 5 | $6.18 \mathrm{e}-03$ | 6 |
| 12 |  | min | . 008 | 6 | -. 636 | 6 | -. 009 | 3 | -1.46e-02 | 5 | -5.886e-04 | 1 | 1.722e-04 | 2 |
| 13 | N7 | max | . 087 | 1 | -. 169 | 5 | . 266 | 5 | $3.394 \mathrm{e}-03$ | 1 | $2.045 \mathrm{e}-03$ | 3 | -2.104e-03 | 5 |
| 14 |  | min | . 006 | 6 | -. 565 | 3 | -. 12 | 3 | -3.378e-03 | 5 | -5.356e-03 | 5 | -6.168e-03 | 3 |
| 15 | N8 | max | . 087 | 1 | -. 056 | 2 | . 618 | 5 | $3.874 \mathrm{e}-03$ | 3 | 1.169e-02 | 5 | $6.18 \mathrm{e}-03$ | 6 |
| 16 |  | min | . 008 | 6 | -. 598 | 6 | -. 006 | 3 | -1.46e-02 | 5 | -5.886e-04 | 1 | $1.719 \mathrm{e}-04$ | 2 |
| 17 | N9 | max | -. 01 | 2 | -. 169 | 5 | . 512 | 5 | 3.389e-03 | 1 | $2.045 \mathrm{e}-03$ | 3 | -1.832e-03 | 2 |
| 18 |  | min | -. 192 | 6 | -. 566 | 3 | -. 227 | 3 | -8.122e-03 | 5 | -5.356e-03 | 5 | -5.509e-03 | 6 |
| 19 | N10 | max | . 514 | 1 | -. 056 | 2 | 2.21 | 5 | 3.821e-03 | 3 | 1.169e-02 | 5 | 1.222e-02 | 1 |
| 20 |  | min | . 199 | 5 | -. 599 | 6 | -. 19 | 3 | -4.069e-02 | 5 | -5.886e-04 | 1 | $3.673 \mathrm{e}-03$ | 5 |
| 21 | N11 | max | . 312 | 1 | -. 169 | 5 | . 182 | 5 | 4.586e-03 | 2 | $2.128 \mathrm{e}-03$ | 3 | -1.517e-03 | 5 |
| 22 |  | min | . 048 | 5 | -. 566 | 3 | -. 078 | 3 | -1.765e-03 | 4 | -1.539e-03 | 5 | -6.15e-03 | 1 |

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## Envelope Joint Displacements (Continued)

| Joint |  |  | X [in] | LC | Y [in] | LC | Z [in] | LC | X Rotation [rad] | LC | $\begin{aligned} & \text { Y Rotatio... L } \\ & \hline 3.295 e-03 \end{aligned}$ | $$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 23 | N12 | max | . 42 |  | -. 056 | 2 | . 328 | 4 | 3.136e-03 |  |  |  |  |  |
| 24 |  | min | . 053 | 5 | -. 599 | 6 | -. 099 | 2 | -2.997e-03 | 2 | 5.224e-04 | 2 | -8.342e-03 | 1 |
| 25 | N13 | max | . 086 | 1 | -. 043 | 5 | . 025 | 5 | $4.314 \mathrm{e}-03$ | 3 | 1.738e-03 | 1 | -1.853e-03 | 5 |
| 26 |  | min | . 007 | 6 | -. 215 | 3 | -. 044 | 1 | -5.882e-04 | 5 | -2.944e-03 | 5 | -5.574e-03 | 3 |
| 27 | N14 | max | . 032 | 2 | -. 043 | 5 | . 18 | 5 | $4.294 \mathrm{e}-03$ | 3 | 1.738e-03 | 1 | -5.65e-04 | 2 |
| 28 |  | min | -. 176 | 6 | -. 216 | 3 | -. 181 | 3 | -5.68e-03 | 5 | -2.944e-03 | 5 | -5.068e-03 | 6 |
| 29 | N15 | max | . 301 | 1 | -. 043 | 5 | . 139 | 4 | $3.449 \mathrm{e}-03$ | 4 | 1.79e-03 | 3 | -2.921e-05 | 5 |
| 30 |  | min | . 039 | 5 | -. 216 | 3 | . 019 | 2 | $1.633 \mathrm{e}-03$ | 3 | -6.203e-04 | 5 | -4.498e-03 | 1 |
| 31 | N16 | max | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 |
| 32 |  | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 |
| 33 | N17 | max | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 |
| 34 |  | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 |
| 35 | N18 | max | . 038 | 5 | -. 029 | 2 | . 066 | 5 | $8.041 \mathrm{e}-04$ | 2 | -2.432e-04 | 3 | -9.541e-04 | 2 |
| 36 |  | min | . 006 | 3 | -. 145 | 6 | . 01 | 3 | -3.009e-03 | 6 | -2.44e-03 | 5 | -4.765e-03 | 6 |
| 37 | N19 | max | . 06 | 4 | -. 029 | 2 | . 07 | 2 | $8.041 \mathrm{e}-04$ | 2 | -2.432e-04 | 3 | -9.552e-04 | 2 |
| 38 |  | min | . 045 | 2 | -. 145 | 6 | -. 014 | 3 | -3.008e-03 | 6 | -2.44e-03 | 5 | -4.765-03 | 6 |
| 39 | N20 | max | . 028 | 2 | -. 029 | 2 | . 071 | 4 | $8.041 \mathrm{e}-04$ | 2 | -2.432e-04 | 3 | -9.53e-04 | 2 |
| 40 |  | min | -. 035 | 6 | -. 145 | 6 | . 035 | 3 | -3.009e-03 | 6 | -2.44e-03 | 5 | -4.765e-03 | 6 |
| 41 | N21 | max | . 408 | 2 | . 039 | 5 | . 153 | 4 | $2.476 \mathrm{e}-03$ | 2 | 4.026e-03 | 4 | 3.191e-03 | 1 |
| 42 |  | min | -. 119 | 6 | -. 531 | 3 | -. 151 | 2 | -5.261e-03 | 6 | -6.364e-03 | 2 | -6.962e-04 | 5 |
| 43 | N22 | max | . 413 | 2 | -. 204 | 5 | . 197 | 4 | $8.425 \mathrm{e}-03$ | 1 | 8.482e-03 | 2 | 7.966e-03 | 2 |
| 44 |  | min | -. 189 | 4 | -. 638 | 3 | -. 155 | 2 | -1.553e-03 | 5 | -3.626e-03 | 4 | -7.841e-03 | 6 |
| 45 | N23 | max | . 375 | 2 | . 029 | 5 | . 141 | 4 | $2.476 \mathrm{e}-03$ | 2 | 4.025e-03 | 4 | 3.191e-03 | 1 |
| 46 |  | min | -. 104 | 6 | -. 501 | 3 | -. 132 | 2 | -5.261e-03 | 6 | -6.364e-03 | 2 | -6.963e-04 | 5 |
| 47 | N24 | max | . 369 | 2 | -. 193 | 5 | . 186 | 4 | $8.425 \mathrm{e}-03$ | 1 | 8.481e-03 | 2 | 7.967e-03 | 2 |
| 48 |  | min | -. 17 | 4 | -. 601 | 3 | -. 129 | 2 | -1.553e-03 | 5 | -3.625--03 | 4 | -7.841e-03 | 6 |
| 49 | N25 | max | . 614 | 2 | . 029 | 5 | . 29 | 6 | $2.473 \mathrm{e}-03$ | 2 | 4.025e-03 | 4 | 7.932e-03 | 1 |
| 50 |  | min | -. 117 | 4 | -. 502 | 3 | -. 221 | 2 | -6.104e-03 | 6 | -6.364e-03 | 2 | -6.955e-04 | 5 |
| 51 | N26 | max | 1.643 | 2 | -. 193 | 5 | . 653 | 5 | $8.393 \mathrm{e}-03$ | 1 | 8.481e-03 | 2 | 3.408e-02 | 2 |
| 52 |  | min | -. 512 | 4 | -. 602 | 3 | -. 532 | 1 | -1.307e-02 | 5 | -3.625e-03 | 4 | -7.734e-03 | 6 |
| 53 | N27 | max | . 305 | 2 | . 029 | 5 | . 295 | 5 | $4.317 \mathrm{e}-03$ | 5 | 3.188e-03 | 4 | 3.267e-03 | 3 |
| 54 |  | min | -. 136 | 6 | -. 501 | 3 | -. 015 | 3 | -1.821e-03 | 3 | -2.033e-03 | 2 | 9.898e-04 | 5 |
| 55 | N28 | max | . 349 | 1 | -. 193 | 5 | . 237 | 5 | $4.256 \mathrm{e}-03$ | 2 | 9.985e-04 | 3 | -2.62e-03 | 3 |
| 56 |  | min | . 115 | 6 | -. 602 | 3 | -. 137 | 3 | -3.178e-03 | 6 | -1.03e-03 | 5 | -6.705e-03 | 4 |
| 57 | N29 | max | . 104 | 2 | -. 022 | 2 | . 062 | 4 | $4.211 \mathrm{e}-04$ | 5 | 1.386e-03 | 6 | 4.776e-04 | 2 |
| 58 |  | min | -. 002 | 6 | -. 202 | 6 | . 009 | 3 | -5.976e-03 | 6 | -5.161e-03 | 2 | -1.34e-03 | 4 |
| 59 | N30 | max | . 255 | 2 | -. 022 | 2 | . 258 | 6 | $3.731 \mathrm{e}-04$ | 2 | 1.386e-03 | 6 | 5.569e-03 | 2 |
| 60 |  | min | -. 049 | 6 | -. 203 | 6 | . 011 | 2 | -6.872e-03 | 6 | -5.161e-03 | 2 | -1.337e-03 | 4 |
| 61 | N31 | max | . 239 | 1 | -. 022 | 2 | . 209 | 5 | $3.643 \mathrm{e}-03$ | 5 | 2.222e-03 | 6 | 4.397e-04 | 5 |
| 62 |  | min | . 034 | 6 | -. 203 | 6 | -. 068 | 3 | -1.409e-03 | 3 | -2.035e-03 | 2 | $-3.525 \mathrm{e}-03$ | 1 |
| 63 | N32 | max | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 6 |
| 64 |  | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 |
| 65 | N33 | max | . 044 | 2 | -. 039 | 5 | . 09 | 4 | $5.624 \mathrm{e}-04$ | 5 | 3.726e-03 | 4 | 5.316e-03 | 3 |
| 66 |  | min | -. 052 | 4 | -. 149 | 3 | -. 075 | 2 | -2.619e-03 | 3 | -3.223e-03 | 2 | 2.218e-03 | 5 |
| 67 | N34 | max | . 018 | 2 | -. 039 | 5 | . 095 | 5 | $5.635 \mathrm{e}-04$ | 5 | 3.726e-03 | 4 | 5.316e-03 | 3 |
| 68 |  | min | -. 076 | 4 | -. 149 | 3 | -. 092 | 1 | -2.619e-03 | 3 | -3.223e-03 | 2 | 2.218e-03 | 5 |
| 69 | N35 | max | . 074 | 1 | -. 039 | 5 | . 087 | 4 | $5.613 \mathrm{e}-04$ | 5 | 3.726e-03 | 4 | 5.316e-03 | 3 |
| 70 |  | min | -. 031 | 5 | -. 149 | 3 | -. 059 | 2 | -2.619e-03 | 3 | -3.223e-03 | 2 | 2.218e-03 | 5 |
| 71 | N36 | max | . 278 | 1 | -. 048 | 2 | . 264 | 4 | $3.739 \mathrm{e}-03$ | 6 | 5.805e-03 | 1 | 5.884e-03 | 4 |
| 72 |  | min | . 148 | 6 | -. 599 | 6 | . 054 | 2 | -2.218e-03 | 2 | 2.939e-03 | 6 | 2.469e-03 | 2 |
| 73 | N37 | max | . 654 | 1 | . 017 | 5 | . 278 | 1 | -2.518e-04 | 5 | -1.169e-03 | 6 | 1.485e-02 | 1 |
| 74 |  | min | . 023 | 5 | -. 58 | 3 | . 048 | 6 | -8.287e-03 | 3 | -1.118e-02 | 1 | 1.527e-03 | 6 |

Centek

FJP
19027.22

CTHA506A - Mount

May 3, 2019
12:26 PM
Checked By: CAG

## Envelope Joint Displacements (Continued)

|  | Joint |  | X [in] | LC | Y [in] | LC | Z [in] | LC | X Rotation [r | LC | R |  | R Rotatio. | L |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 75 | N38 | max | . 248 | 1 | -. 052 | 2 | . 251 | 4 | $3.738 \mathrm{e}-03$ | 6 | 5.804e-03 | 1 | 5.883e-03 | 4 |
| 76 |  | min | 132 | 6 | -. 562 | 6 | . 037 | 2 | -2.219e-03 | 2 | 2.939e-03 | 6 | $2.468 \mathrm{e}-03$ | 2 |
| 77 | N39 | max | . 596 | 1 | . 011 | 5 | . 244 | 1 | -2.515e-04 | 5 | -1.169e-03 | 6 | $1.485 \mathrm{e}-02$ | 1 |
| 78 |  | min | . 008 | 5 | -. 549 | 3 | . 045 | 6 | -8.287e-03 | 3 | -1.118e-02 | 1 | $1.527 \mathrm{e}-03$ | 6 |
| 79 | N40 | max | . 478 | 1 | -. 052 | 2 | . 236 | 5 | 2.86e-03 | 6 | 5.804e-03 | 1 | $7.705 \mathrm{e}-03$ | 1 |
| 80 |  | min | . 34 | 6 | -. 562 | 6 | -. 035 | 3 | -2.216e-03 | 2 | 2.939e-03 | 6 | 5.382e-03 | 5 |
| 81 | N41 | max | 2.199 | 1 | . 011 | 5 | . 629 | 1 | -7.322e-03 | 2 | -1.169e-03 | 6 | $4.091 \mathrm{e}-02$ | 1 |
| 82 |  | min | . 094 | 6 | -. 55 | 3 | 46 | 3 | -1.245e-02 | 4 | -1.118e-02 | 1 | $1.507 \mathrm{e}-03$ | 6 |
| 83 | N42 | max | . 266 | 1 | -. 052 | 2 | . 38 | 4 | $4.233 \mathrm{e}-03$ | 6 | 2.996e-03 | 1 | 6.537e-03 | 4 |
| 84 |  | min | -. 017 | 5 | -. 562 | 6 | -. 045 | 2 | -1.373e-03 | 2 | $1.541 \mathrm{e}-03$ | 5 | -1.622e-03 | 2 |
| 85 | N43 | max | . 279 | 2 | . 011 | 5 | . 435 | 4 | $8.121 \mathrm{e}-03$ | 4 | 8.834e-04 | 4 | $4.611 \mathrm{e}-03$ | 6 |
| 86 |  | min | -. 202 | 6 | -. 55 | 3 | -. 119 | 2 | -6.584e-03 | 2 | -3.374e-03 | 2 | $1.869 \mathrm{e}-03$ | 2 |
| 87 | N44 | max | . 041 | 1 | -. 069 | 2 | . 131 | 4 | $2.64 \mathrm{e}-03$ | 4 | 4.596e-03 | 4 | 6.542e-03 | 6 |
| 88 |  | min | . 015 | 6 | -. 215 | 6 | -. 077 | 2 | -1.473e-03 | 2 | 1.712e-03 | 3 | 2.225e-03 | 2 |
| 89 | N45 | max | . 278 | 3 | -. 069 | 2 | . 131 | 5 | $1.818 \mathrm{e}-03$ | 3 | 4.596e-03 | 4 | 7.948e-03 | 1 |
| 90 |  | min | 143 | 5 | -. 216 | 6 | -. 07 | 3 | -1.471e-03 | 2 | $1.712 \mathrm{e}-03$ | 3 | $3.464 \mathrm{e}-03$ | 5 |
| 91 | N46 | max | . 135 | 2 | -. 069 | 2 | . 323 | 4 | $4.28 \mathrm{e}-03$ | 4 | 2.22e-03 | 4 | $2.153 \mathrm{e}-03$ | 6 |
| 92 |  | min | -. 105 | 6 | -. 216 | 6 | -. 115 | 2 | $1.431 \mathrm{e}-04$ | 2 | 1.284e-03 | 2 | -2.951e-03 | 2 |
| 93 | N47 | max | . 275 | 1 | -. 178 | 5 | . 201 | 5 | $4.586 \mathrm{e}-03$ | 2 | 2.128e-03 | 3 | -1.518e-03 | 5 |
| 94 |  | min | . 038 | 5 | -. 595 | 3 | -. 091 | 3 | -1.765e-03 | 4 | -1.541e-03 | 5 | -6.151e-03 | 1 |
| 95 | N48 | max | . 273 | 1 | -. 013 | 2 | . 37 | 4 | $2.675 \mathrm{e}-03$ | 6 | 3.297e-03 | 4 | -8.064e-04 | 5 |
| 96 |  | min | . 038 | 5 | -. 584 | 6 | -. 042 | 2 | -3.248e-03 | 5 | 5.224e-04 | 2 | -7.395e-03 | 1 |
| 97 | N49 | max | . 275 | 1 | -. 169 | 5 | . 192 | 5 | $4.586 \mathrm{e}-03$ | 2 | $2.128 \mathrm{e}-03$ | 3 | -1.517e-03 | 5 |
| 98 |  | min | . 038 | 5 | -. 566 | 3 | -. 078 | 3 | -1.765e-03 | 4 | -1.539e-03 | 5 | -6.15e-03 | 1 |
| 99 | N50 | max | . 273 | 1 | -. 056 | 2 | . 35 | 4 | $2.675 \mathrm{e}-03$ | 6 | 3.295e-03 | 4 | -8.07e-04 | 5 |
| 100 |  | min | . 038 | 5 | -. 599 | 6 | -. 045 | 2 | -3.248e-03 | 5 | $5.224 \mathrm{e}-04$ | 2 | -7.396e-03 | 1 |
| 101 | N51 | max | . 274 | 1 | -. 043 | 5 | . 118 | 4 | $3.449 \mathrm{e}-03$ | 4 | $1.79 \mathrm{e}-03$ | 3 | -2.921e-05 | 5 |
| 102 |  | min | . 039 | 5 | -. 216 | 3 | . 009 | 2 | $1.633 \mathrm{e}-03$ | 3 | -6.203e-04 | 5 | -4.498e-03 | 1 |
| 103 | N52 | max | . 331 | 2 | . 048 | 5 | . 278 | 5 | $4.316 \mathrm{e}-03$ | 5 | 3.189e-03 | 4 | 3.267e-03 | 3 |
| 104 |  | min | -. 134 | 6 | -. 521 | 3 | . 001 | 3 | -1.822e-03 | 3 | -2.035e-03 | 2 | 9.901e-04 | 5 |
| 105 | N53 | max | . 285 | 1 | -. 22 | 5 | . 201 | 5 | $4.255 \mathrm{e}-03$ | 2 | 9.988e-04 | 3 | -1.996e-03 | 2 |
| 106 |  | min | . 043 | 5 | -. 593 | 3 | -. 089 | 3 | -3.418e-03 | 6 | -1.031e-03 | 5 | -6.702e-03 | 4 |
| 107 | N54 | max | . 32 | 2 | . 029 | 5 | . 269 | 5 | $4.317 \mathrm{e}-03$ | 5 | 3.188e-03 | 4 | 3.267e-03 | 3 |
| 108 |  | min | -. 119 | 6 | -. 501 | 3 | -. 004 | 3 | -1.821e-03 | 3 | -2.033e-03 | 2 | 9.898e-04 | 5 |
| 109 | N55 | max | . 28 | 1 | -. 193 | 5 | . 198 | 5 | $4.255 \mathrm{e}-03$ | 2 | $9.985 \mathrm{e}-04$ | 3 | -1.995e-03 | 2 |
| 110 |  | min | . 048 | 5 | -. 602 | 3 | -. 086 | 3 | -3.419e-03 | 6 | -1.03e-03 | 5 | -6.702e-03 | 4 |
| 111 | N56 | max | . 217 | 1 | -. 022 | 2 | . 187 | 5 | $3.643 \mathrm{e}-03$ | 5 | 2.222e-03 | 6 | 4.397e-04 | 5 |
| 112 |  | min | . 032 | 6 | -. 203 | 6 | -. 06 | 3 | -1.409e-03 | 3 | -2.035e-03 | 2 | -3.525e-03 | 1 |
| 113 | N57 | max | . 273 | 1 | -. 04 | 2 | . 366 | 4 | $4.233 \mathrm{e}-03$ | 6 | $2.998 \mathrm{e}-03$ | 1 | 6.537e-03 | 4 |
| 114 |  | min | . 029 | 5 | -. 592 | 6 | -. 029 | 2 | -1.373e-03 | 2 | 1.542e-03 | 5 | -1.622e-03 | 2 |
| 115 | N58 | max | . 338 | 2 | . 055 | 5 | . 289 | 4 | $7.174 \mathrm{e}-03$ | 4 | 8.824e-04 | 4 | $4.96 \mathrm{e}-03$ | 3 |
| 116 |  | min | -. 123 | 6 | -. 54 | 3 | . 006 | 3 | -6.582e-03 | 2 | -3.376e-03 | 2 | $2.15 \mathrm{e}-03$ | 5 |
| 117 | N59 | max | . 257 | 1 | -. 052 | 2 | . 361 | 4 | $4.233 \mathrm{e}-03$ | 6 | 2.996e-03 | 1 | 6.537e-03 | 4 |
| 118 |  | min | . 021 | 5 | -. 562 | 6 | -. 037 | 2 | -1.373e-03 | 2 | $1.541 \mathrm{e}-03$ | 5 | -1.622e-03 | 2 |
| 119 | N60 | max | . 32 | 2 | . 011 | 5 | . 292 | 4 | $7.175 \mathrm{e}-03$ | 4 | 8.834e-04 | 4 | 4.961e-03 | 3 |
| 120 |  | min | -. 119 | 6 | -. 549 | 3 | 0 | 2 | -6.582e-03 | 2 | -3.374e-03 | 2 | $2.151 \mathrm{e}-03$ | 5 |
| 121 | N61 | max | . 118 | 2 | -. 069 | 2 | . 297 | 4 | $4.28 \mathrm{e}-03$ | 4 | 2.22e-03 | 4 | $2.153 \mathrm{e}-03$ | 6 |
| 122 |  | min | -. 093 | 6 | -. 216 | 6 | -. 116 | 2 | $1.431 \mathrm{e}-04$ | 2 | 1.284e-03 | 2 | -2.951e-03 | 2 |
| 123 | N63 | max | . 048 | 1 | -. 017 | 5 | 0 | 5 | $5.166 \mathrm{e}-03$ | 3 | 3.083e-03 | 1 | 2.605e-04 | 5 |
| 124 |  | min | . 003 | 6 | -. 076 | 3 | 0 | 3 | $7.89 \mathrm{e}-04$ | 5 | $2.608 \mathrm{e}-04$ | 6 | -9.923e-04 | 1 |
| 125 | N65 | max | . 024 | 2 | -. 02 | 5 | . 049 | 4 | $2.135 \mathrm{e}-04$ | 5 | 3.72e-03 | 4 | 4.803e-03 | 3 |
| 126 |  | min | -. 028 | 4 | -. 079 | 3 | -. 04 | 2 | -2.473e-03 | 3 | -3.107e-03 | 2 | $1.759 \mathrm{e}-03$ | 5 |

## Envelope Joint Displacements (Continued)

| Joint |  |  | X [in] | LC | Y [in] | LC | Z [in] | LC | X Rotation [rad] | LC Y Rotatio... LC Z Rotatio... LC |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 127 | N67 | max | . 021 | 5 | -. 019 | 2 | . 037 | 5 | 1.797e-04 | 2 | -4.13e-04 | 3 | -1.253e-03 | 2 |
| 128 |  | min | . 004 | 3 | -. 077 | 6 | . 006 | 3 | -2.743e-03 | 6 | -2.707e-03 | 5 | -4.453e-03 | 6 |

## Envelope AISC 14th(360-10): LRFD Steel Code Checks

| Member |  | Shape | Code Check | Lo.. | LC | She. | Lo |  | phi* ${ }^{\text {P }}$ | phi*P |  | phi* | Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M4 | PIPE_2.0 | . 908 | 4 | 4 | . 242 | 1.5 |  | 514.916 | 32.13 | 1.872 | 1.872 | ... $\mathrm{H} 1-.$. |
| 2 | M10 | PIPE 2.0 | . 831 | 4 | 1 | . 221 | 1.5 |  | 214.916 | 32.13 | 1.872 | 1.872 | .. $\mathrm{H} 1-\ldots$ |
| 3 | M16 | PIPE_2.0 | . 817 | 4 | 2 | . 228 | 1.5 |  | 114.916 | 32.13 | 1.872 | 1.872 | H1-. |
| 4 | M3 | PIPE 3.0 | . 513 | 6.25 | 4 | . 271 | 6.25 |  | 453.7766 | 65.205 | 5.749 | 5.749 | 1 H3-6 |
| 5 | M9 | PIPE 3.0 | . 439 | 6.25 | 1 | . 217 | 6.25 |  | 153.7766 | 65.205 | 5.749 | 5.749 | 1 H1-... |
| 6 | M15 | PIPE 3.0 | . 424 | 6.25 | 6 | . 237 | 6.25 |  | 153.7766 | 65.205 | 5.749 | 5.749 | $1 \mathrm{H} 1-$ |
| 7 | M18 | PIPE_2.0 | . 423 | 3 | 1 | . 099 | . 5 |  | 520.867 | 32.13 | 1.872 | 1.872 | H1-. |
| 8 | M11 | PIPE 2.0 | . 421 | 3 | 3 | . 150 | . 5 |  | 120.867 | 32.13 | 1.872 | 1.872 | . $\mathrm{H} 1-$ |
| 9 | M12 | PIPE_2.0 | . 419 | 3 | 1 | . 124 | . 5 |  | 120.867 | 32.13 | 1.872 | 1.872 | ... $\mathrm{H} 1-.$. |
| 10 | M17 | PIPE 2.0 | . 398 | 3 | 3 | . 092 | . 5 |  | 120.867 | 32.13 | 1.872 | 1.872 | . $\mathrm{H} 1-\ldots$ |
| 11 | M5 | PIPE_2.0 | . 388 | 3 | 6 | . 118 | . 5 |  | 420.867 | 32.13 | 1.872 | 1.872 | . $\mathrm{H} 1-\ldots$ |
| 12 | M13 | HSS4X4X4 | . 373 | 0 | 6 | . 081 | 0 | z 4 | 4 134.... | 139.... | 16.181 | 16.181 | .. $\mathrm{H} 1-\ldots$ |
| 13 | M1 | HSS4X4X4 | . 371 | 0 | 3 | . 075 | 0 | z 1 | 1 134.... | 139.... | 16.181 | 16.181 | ... $\mathrm{H} 1-.$. |
| 14 | M7 | HSS4X4X4 | . 364 | 0 | 6 | . 061 | 0 | z 2 | $2134 . .$. | 139.... | 16.181 | 16.181 | .. $\mathrm{H} 1-$ |
| 15 | M21 | PIPE_2.0 | . 346 | 7.9.. | 3 | . 117 | 7.9.. | 1 | 16.295 | 32.13 | 1.872 | 1.872 | ... $\mathrm{H} 1-.$. |
| 16 | M19 | PIPE 2.0 | . 335 | 7.9... | 6 | . 090 | 7.9.. | 4 | 46.295 | 32.13 | 1.872 | 1.872 | ... $\mathrm{H} 1-.$. |
| 17 | M20 | PIPE 2.0 | . 331 | 4.5... | 3 | . 083 | 4.6.. | 1 | 16.295 | 32.13 | 1.872 | 1.872 | .. $\mathrm{H} 1-\ldots$ |
| 18 | M22 | L2.5x2.5x4 | . 321 | 0 | 5 | . 149 | . 926 | z 4 | 437.4933 | 38.556 | 1.114 | 2.537 | . H 2 -1 |
| 19 | M23 | L2.5x2.5x4 | . 310 | . 926 | 2 | . 089 | . 926 | y 5 | 537.4933 | 38.556 | 1.114 | 2.537 | H2-1 |
| 20 | M24 | L2.5x2.5x4 | . 308 | 0 | 1 | . 161 | 0 | z 2 | 237.4933 | 38.556 | 1.114 | 2.537 | . H 2 -1 |
| 21 | M6 | PIPE_2.0 | . 295 | 3 | 5 | . 086 | . 5 |  | 420.867 | 32.13 | 1.872 | 1.872 | H1- |
| 22 | M2 | PIPE 4.0 | . 001 | . 75 | 1 | . 000 | 75 |  | 192.571 | 93.24 | 10.631 | 10.631 | ... $\mathrm{H} 1-.$. |
| 23 | M8 | PIPE_4.0 | . 001 | . 75 | 1 | . 000 | 75 |  | 192.571 | 93.24 | 10.631 | 10.631 | ... $\mathrm{H} 1-\ldots$ |
| 24 | M14 | PIPE 4.0 | . 001 | . 75 | 4 | . 000 | 75 |  | 592.571 | 93.24 | 10.631 | 10.631 | $1 \mathrm{H} 1-.$. |



| Centek | CTHA506A - Mount Unity Check |  |
| :---: | :---: | :---: |
| FJP |  | May 3, 2019 at 12:27 PM |
| 19027.22 |  | CTHA506A_AMA.r3d |

# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

T-Mobile Existing Facility
Site ID: CTHA506A
AT\&T Wethersfield Monopole 75 Wells Road
Wethersfield, Connecticut 06I09
May 29, 2019
EBI Project Number: 6219001818

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general <br> population allowable <br> limit: | $\mathbf{1 5 . 7 9 \%}$ |

environmental | engineering | due diligence

May 29, 2019
T-Mobile
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, Connecticut 06002

Emissions Analysis for Site: CTHA506A - AT\&T Wethersfield Monopole

EBI Consulting was directed to analyze the proposed T-Mobile facility located at 75 Wells Road in Wethersfield, Connecticut for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-Oland ANSI/IEEE Std C95.I. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR I.I307(b)(I) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately $400 \mu \mathrm{~W} / \mathrm{cm}^{2}$ and $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, respectively. The general population exposure limit for the $1900 \mathrm{MHz}(\mathrm{PCS}), 2100 \mathrm{MHz}(\mathrm{AWS})$ and II GHz frequency bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.
environmental | engineering | due diligence

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 75 Wells Road in Wethersfield, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top a 6 -foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 2 LTE channels ( 600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
2) 2 LTE channels ( 700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
3) 2 LTE channels (PCS Band - 1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
4) 2 UMTS channels (AWS Band - 2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
5) 2 LTE channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
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6) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-0I recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
7) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
8) The antennas used in this modeling are the Ericsson AIR 21 for the 2100 MHz channel(s), the Ericsson AIR 32 for the $1900 \mathrm{MHz} / 2100 \mathrm{MHz}$ channel(s), the RFS APXVAARR24_43-UNA20 for the $600 \mathrm{MHz} / 700 \mathrm{MHz}$ channel(s) in Sector A, the Ericsson AIR 21 for the 2100 MHz channel(s), the Ericsson AIR 32 for the $1900 \mathrm{MHz} / 2100 \mathrm{MHz}$ channel(s), the RFS APXVAARR24_43-U-NA20 for the $600 \mathrm{MHz} / 700 \mathrm{MHz}$ channel(s) in Sector B, the Ericsson AIR 21 for the 2100 MHz channel(s), the Ericsson AIR 32 for the $1900 \mathrm{MHz} / 2100 \mathrm{MHz}$ channel(s), the RFS APXVAARR24_43-U-NA20 for the $600 \mathrm{MHz} / 700 \mathrm{MHz}$ channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
9) The antenna mounting height centerline of the proposed antennas is 95 feet above ground level (AGL).
10) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
11) All calculations were done with respect to uncontrolled / general population threshold limits.

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## T-Mobile Site Inventory and Power Data

| Sector: | A | Sector: | B | Sector: | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna \#: | I | Antenna \#: | I | Antenna \#: | I |
| Make / Model: | Ericsson AIR 21 | Make / Model: | Ericsson AIR 21 | Make / Model: | Ericsson AIR 21 |
| Frequency Bands: | 2100 MHz | Frequency Bands: | 2100 MHz | Frequency Bands: | 2100 MHz |
| Gain: | 15.35 dBd | Gain: | 15.35 dBd | Gain: | 15.35 dBd |
| Height (AGL): | 95 feet | Height (AGL): | 95 feet | Height (AGL): | 95 feet |
| Channel Count: | 2 | Channel Count: | 2 | Channel Count: | 2 |
| Total TX Power (W): | 60 Watts | Total TX Power (W): | 60 Watts | Total TX Power (W): | 60 Watts |
| ERP (W): | 2,056.61 | ERP (W): | 2,056.61 | ERP (W): | 2,056.61 |
| Antenna AI MPE \%: | 0.82\% | Antenna BI MPE \%: | 0.82\% | Antenna CI MPE \%: | 0.82\% |
| Antenna \#: | 2 | Antenna \#: | 2 | Antenna \#: | 2 |
| Make / Model: | Ericsson AIR 32 | Make / Model: | Ericsson AIR 32 | Make / Model: | Ericsson AIR 32 |
| Frequency Bands: | $1900 \mathrm{MHz} / 2100 \mathrm{MHz}$ | Frequency Bands: | $1900 \mathrm{MHz} / 2100 \mathrm{MHz}$ | Frequency Bands: | $1900 \mathrm{MHz} / 2100 \mathrm{MHz}$ |
| Gain: | $15.35 \mathrm{dBd} / 15.85 \mathrm{dBd}$ | Gain: | 15.35 dBd / 15.85 dBd | Gain: | $15.35 \mathrm{dBd} / 15.85 \mathrm{dBd}$ |
| Height (AGL): | 95 feet | Height (AGL): | 95 feet | Height (AGL): | 95 feet |
| Channel Count: | 4 | Channel Count: | 4 | Channel Count: | 4 |
| Total TX Power (W): | 240 Watts | Total TX Power (W): | 240 Watts | Total TX Power (W): | 240 Watts |
| ERP (W): | 8,728.3 I | ERP (W): | 8,728.3 I | ERP (W): | 8,728.3 I |
| Antenna A2 MPE \%: | 3.48\% | Antenna B2 MPE \%: | 3.48\% | Antenna C2 MPE \%: | 3.48\% |
| Antenna \#: | 3 | Antenna \#: | 3 | Antenna \#: | 3 |
| Make / Model: | RFS APXVAARR24_43-UNA20 | Make / Model: | RFS APXVAARR24_43-U- <br> NA20 | Make / Model: | RFS APXVAARR24_43-UNA20 |
| Frequency Bands: | $600 \mathrm{MHz} / 700 \mathrm{MHz}$ | Frequency Bands: | $600 \mathrm{MHz} / 700 \mathrm{MHz}$ | Frequency Bands: | $600 \mathrm{MHz} / 700 \mathrm{MHz}$ |
| Gain: | 12.95 dBd / 13.35 dBd | Gain: | 12.95 dBd / 13.35 dBd | Gain: | 12.95 dBd / 13.35 dBd |
| Height (AGL): | 95 feet | Height (AGL): | 95 feet | Height (AGL): | 95 feet |
| Channel Count: | 4 | Channel Count: | 4 | Channel Count: | 4 |
| Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts |
| ERP (W): | 2,481.08 | ERP (W): | 2,481.08 | ERP (W): | 2,481.08 |
| Antenna A3 MPE \%: | 2.29\% | Antenna B3 MPE \%: | 2.29\% | Antenna C3 MPE \%: | 2.29\% |

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| Site Composite MPE \% |  |
| :---: | :---: |
| Carrier | MPE \% |
| T-Mobile (Max at Sector A): | $6.58 \%$ |
| AT\&T | $9.21 \%$ |
| Site Total MPE \% : | $15.79 \%$ |


| T-Mobile Sector A Total: | $6.58 \%$ |  |
| ---: | :--- | :---: |
| T-Mobile Sector B Total: | $6.58 \%$ |  |
| T-Mobile Sector C Total: | $6.58 \%$ |  |
| Site Total: |  |  |
| $15.79 \%$ |  |  |

## T-Mobile Maximum MPE Power Values (Sector A)

| T-Mobile Frequency Band / Technology (Sector A) | \# Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Frequency (MHz) | Allowable MPE ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Calculated \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T-Mobile 2100 MHz UMTS | 2 | 1028.30 | 95.0 | 8.19 | 2100 MHz UMTS | 1000 | 0.82\% |
| T-Mobile 1900 MHz LTE | 2 | 2056.61 | 95.0 | 16.39 | 1900 MHz LTE | 1000 | 1.64\% |
| T-Mobile 2100 MHz LTE | 2 | 2307.55 | 95.0 | 18.38 | 2100 MHz LTE | 1000 | 1.84\% |
| T-Mobile 600 MHz LTE | 2 | 591.73 | 95.0 | 4.71 | 600 MHz LTE | 400 | 1.18\% |
| T-Mobile 700 MHz LTE | 2 | 648.82 | 95.0 | 5.17 | 700 MHz LTE | 467 | I.II\% |
|  |  |  |  |  |  | Total: | 6.58\% |

- NOTE: Totals may vary by approximately $0.01 \%$ due to summation of remainders in calculations.
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## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| T-Mobile Sector | Power Density Value (\%) |
| :---: | :---: |
| Sector A: | $6.58 \%$ |
| Sector B: | $6.58 \%$ |
| Sector C: | $6.58 \%$ |
| T-Mobile Maximum <br> MPE \% (Sector A): | $6.58 \%$ |
| Site Total: |  |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{I 5 . 7 9 \%}$ of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.

