

## Structural Analysis Report For a 120-ft Monopole Tower

Hartford 9 CT  
Site No.: 468180  
Fuze#: 16232035  
250 Silas Deane Highway  
Wethersfield, CT 06109  
Hartford County

Prepared for:

**Verizon Wireless**  
118 Flanders Road  
Westborough, MA 01581-3956

December 30, 2020

Prepared by:

**Dewberry Engineers Inc.**  
99 Summer Street, Suite 700  
Boston, MA 02110  
Dewberry Project Number: 50121823

Tower Controlling Member	% Capacity	Result
Tower Components	92.7	Sufficient
Base Plate	34.9	Sufficient
Anchor Bolts	64.8	Sufficient
Foundation	-	Sufficient

Tower/Foundation Previously Reinforced?	YES <input checked="" type="checkbox"/> / NO <input type="checkbox"/>
Previous Reinforcement Verified?	YES <input checked="" type="checkbox"/> / NO <input type="checkbox"/> Date: <b>07/26/19</b>
Additional Reinforcement Required?	YES <input type="checkbox"/> / NO <input checked="" type="checkbox"/>

Prepared by:



Brandon Kelsey  
Structural Project Engineer

Checked by:



Deep Patel  
Structural Project Engineer

Approved by:



Benjamin Revette, P.E.  
Associate Vice President

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## 1.0 INTRODUCTION AND PROJECT SUMMARY

The objective of this report is to assess the proposed installation of new antennas and support equipment on an existing 120 ft. steel monopole located in Wethersfield, CT. This report is limited to the analysis of the tower only. The telecommunication upgrade is proposed by Verizon Wireless. For the Antenna mount modification please refer to the Mount Modification Report by Maser Consulting dated December 16, 2020.

Please refer to the appendices for the structural analysis package regarding the structural analysis.

## 2.0 CODES, STANDARDS, AND REFERENCES

The structural analysis was completed according to the provisions of the following Codes and standards:

- *2018 Connecticut State Building Code – Amendments to IBC 2015*
- *International Building Code (IBC) 2015*, International Code Council
- ASCE 7-10 Minimum design Loads for Buildings and Other Structures, American Society of Civil Engineers
- *TIA-222-G-4, Structural Standard for Antenna Supporting Structures and Antennas*
- *Steel Construction Manual 14<sup>th</sup> Ed*, American Institute of Steel Construction

The analysis was in compliance with the minimum requirements as specified by TIA-222-G for the County of Hartford, CT under the following load parameters:

<b>Risk Category:</b>	II	
<b>Exposure Category:</b>	C	IBC 2015
<b>Design Ultimate Wind Speed</b>	125 mph	2018 CT Bld. Code Appendix N
<b>Design Basic Wind Speed</b>	97 mph	Except. #5, Sect. 1609.3.1, Eqn. 16-33, IBC 15
<b>Design Ice Wind Speed:</b>	50 mph	ASCE 7-10 Hazard Tool
<b>Design Ice Thickness:</b>	1.00 in.	ASCE 7-10 Hazard Tool
<b>Serviceability Wind Speed:</b>	60 mph	Sect. 2.8.3, TIA Rev G

The tower geometry, member sizes, existing antenna loading, and foundation design loading were referenced from the following reports, all of which can be found in Appendix B:

- Structural Analysis Report by CENTEK Engineering dated November 14, 2016
- Structural Analysis Report (Rev 3) by Dewberry Engineers Inc. dated November 21, 2019
- Radio Frequency Design Sheet (RFDS name: Hartford 9 CT) by Verizon Wireless dated October 8, 2020.
- Site Visit by Dewberry Engineers on October 20, 2020
- Post-Mod Antenna Mount Analysis Report by Maser Consulting dated December 16, 2020

### 3.0 EXISTING AND PROPOSED TOWER LOADING

#### 3.1 Existing (includes Reserved, if applicable) Antenna and Cable information:

Mounting Elevation (ft)	Center Line Elevation (ft)	Carrier	QTY.	APPURTENANCES DESCRIPTION	FEEDLINE
117	123	Public Safety	2	DB809-XC Omni (Reserve)	(2) 7/8"
110	110	Public Safety	1	2' Dish	(2) 1/2"
			2	1' Dish (Reserve)	(6) 7/8"
			2	2' Dish (Reserve)	
105	106	Metro PCS	6	Air21	(1) 1-5/8"
	105		3	4' Standoff T-Arm	
90	92	VZW	3	B2/B66A RRH	(12) 1-5/8" (1)* Hybriflex
	90		1*	OVP Box	
			6**	BXA 80063 6CF	
			6	SBNHH-1D65B	
			3	BSAMNT-SBS-1-2	
			3	B5/B13 RRH	
90	3***	4' Standoff T-Arm			
54	63	Public Safety	1	PD1142	(5) 1/2"
	56.5		1	5'x1" Omni	
			1	DB404	
	52		2	DB583	
	54		3	4' Side Mount Standoff	

\* To be removed  
 \*\* 3 To be removed  
 \*\*\* To be modified

#### 3.2 Proposed Antenna Loading and Cable information:

Mounting Elevation (ft)	Center Line Elevation (ft)	Carrier	QTY.	APPURTENANCES DESCRIPTION	FEEDLINE
90	92	VZW	2	6-OVP	(2) Hybriflex
	90		3	Licensed Sub 6 Ant. w/ integrated VZS01 RRH	

### 3.3 Final Appurtenance Loading Configuration on Tower:

Mounting Elevation (ft)	Center Line Elevation (ft)	Carrier	QTY.	APPURTENANCES DESCRIPTION	FEEDLINE
90	92	VZW	3	B2/B66A RRH	(12) 1-5/8" (2) Hybriflex
			2	6-OVP	
	90		3	BXA 80063 6CF	
			3	Licensed Sub 6 Ant. w/ integrated VZS01 RRH	
			6	SBNHH-1D65B	
			3	BSAMNT-SBS-1-2	
			3	B5/B13 RRH	
	88		3	B5/B13 RRH	
	90		3	Modified 4' T-Boom	

### 3.4 Method:

tnxTower, a commercially available engineering software program, was used to create a three dimensional model of the tower members and calculate primary member stresses under various loading conditions. Selected output from the analysis is included in Appendix A.

## 4.0 TOWER ANALYSIS RESULTS SUMMARY

### 4.1 Tower Structure Results

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	$\phi P_{allow}$ lb	% Capacity	Pass Fail
L1	120 - 89.75	Pole	TP21.287x16x0.188	1	-3270.95	892475.00	28.6	Pass
L2	89.75 - 70	Pole	TP24.3628x20.4443x0.188	2	-9899.60	995069.00	83.4	Pass
L3	70 - 44.417	Pole	TP28.8342x24.3628x0.275	3	-12805.00	1804540.00	77.0	Pass
L4	44.417 - 35	Pole	TP29.93x27.6579x0.275	4	-15011.70	1885590.00	92.7	Pass
L5	35 - 0	Pole	TP36.0472x29.93x0.364	5	-22025.80	3062890.00	84.8	Pass
Summary								
Pole (L4)							92.7	Pass
<b>RATING =</b>							<b>92.7</b>	<b>Pass</b>

Table above displays the summary of the ratio (as the percentage) of force in the member to their capacities. Values greater than 100% indicate the maximum force in the member exceeds its capacity.

*\*Note: Capacities up to 105% are considered acceptable (where applicable)*

### 4.2 Foundation results

The foundation reactions are summarized below:

Tower Component	Condition	Utilization	Pass/Fail
Base Plate	Bending (kip-ft)	34.9%	Pass
Anchor Bolts	Tensile (kip)	64.8%	Pass
Foundation	Overturning Moment (kip-ft)	1.19 F.S.	Pass

*\*Note: A foundation-soil interaction of 110% or less is within engineering tolerances for foundations and is considered acceptable.*

## 5.0 CONCLUSIONS AND COMMENTARY

After analysis, it was determined that the existing tower structure and foundation **is adequate** to support the proposed forces as a result of the telecommunication upgrade.

This engineering analysis is based upon the theoretical capacity of the structure. It is not a condition assessment of the tower and its foundation. Dewberry Engineers Inc. reserves the right to add to or modify this report if more information becomes available. The conclusions reached by Dewberry Engineers Inc. in this report are only applicable to the previously mentioned existing structural elements supporting the proposed wireless telecommunications installation. The results of this report are based on the assumption that existing structural elements have been installed per the original design documents, have been well maintained and are uncompromised. This report does not imply that a thorough inspection of the existing structure has been performed. Any deviation of the support condition, loading, location, placement, equipment configuration, etc, will require Dewberry Engineers Inc. to generate an additional structural analysis.

## 6.0 ASSUMPTIONS

This structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. Dewberry Engineers Inc. has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analyzing the tower only.
5. The soil parameters are as per data supplied or as assumed and stated in the calculations.
6. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
7. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
8. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
9. All prior structural modifications are assumed to be as per data supplied/ available and to have been properly installed.
10. Loading interpreted from photos is accurate to  $\pm 5'$  AGL, antenna size accurate to  $\pm 3.3$  sf, and coax equal to the number of existing antennas without reserves

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and Dewberry Engineering Inc. should be allowed to review any new information to determine its effect on the structural integrity of the tower.

## 7.0 DISCLAIMER OF WARRANTIES

If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by Dewberry Engineers Inc. in connection with this Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. All tower components have been assumed to only resist dead loads when no other loads are applied. No allowance was made for any damaged, bent, missing, loose or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

This analysis is limited to the designated maximum wind and seismic conditions per the governing tower standards and code. Wind forces resulting in tower vibrations near the structure's resonant frequencies were not considered in this analysis and are outside the scope of this analysis. Lateral loading from any dynamic response was not evaluated under a time-domain based fatigue analysis.

Dewberry Engineers Inc. does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. Dewberry Engineers Inc. provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to calculate the structural integrity for the existing tower under existing and proposed loadings.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the code specified amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing condition, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from Dewberry Engineering Inc., but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

Towers are designed to carry gravity, wind, and ice loads. All members, legs, diagonals, struts, and redundant members provide structural stability to the tower with little redundancy. Absence or removal of a member can trigger catastrophic failure unless a substitute is provided before any removal. Legs carry axial loads and derive their strength from shorter unbraced lengths by the presence of redundant members and their connections to the diagonals with bolts or welds. If the bolts or welds are removed without providing any substitute to the frame, the leg is subjected to a higher unbraced length that immediately reduces its load carrying capacity. If a diagonal is also removed in addition to the connection, the unbraced length of the leg is greatly increased, jeopardizing its load carrying capacity. Failure of one leg can result in a tower collapse because there is no redundancy. Redundant members and diagonals are critical to the stability of the tower.

Client: Verizon Wireless  
Site Name: Hartford 9 CT  
Date: December 30, 2020

Dewberry Engineers Inc. makes no warranties, expresses and/or implied in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. Dewberry will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of Dewberry pursuant to this report will be limited to the total fee received for preparation of this report.



## **APPENDIX A**

### **tnxTOWER OUTPUT FOR PROPOSED LOADING**

## DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
DB809K-XC	117	B2/B66A RRH	90
DB809K-XC	117	B5/B13 RRH	90
6' Long 2-3/8" Mast Pipe	110	Licensed Sub 6 5G w/ radio _mast pipe	90
6' Long 2-3/8" Mast Pipe	110	DB-T1-6Z-12AB-OZ OVP	90
6' Long 2-3/8" Mast Pipe	110	(2) 4' T-Boom (7' Face)	90
2' Diameter Dish w/o Radome	110	BXA-80063-6CF w/ mast pipe	90
2' Diameter Dish w/o Radome	110	(2) SBNHH-1D65B SBS-1-2	90
2' Diameter Dish w/o Radome	110	B2/B66A RRH	90
1' Dish w/o Radome	110	B5/B13 RRH	90
1' Dish w/o Radome	110	Licensed Sub 6 5G w/ radio _mast pipe	90
Ericsson Air 21 B2A w/ mast pipe	105	(2) 4' T-Boom (7' Face)	90
4' T-Arm (7' Face)	105	BXA-80063-6CF w/ mast pipe	90
Ericsson Air 21 B2A w/ mast pipe	105	(2) SBNHH-1D65B SBS-1-2	90
Ericsson Air 21 B2A w/ mast pipe	105	B2/B66A RRH	90
4' T-Arm (7' Face)	105	B5/B13 RRH	90
Ericsson Air 21 B2A w/ mast pipe	105	DB404 4-bay Dipole	54
Ericsson Air 21 B2A w/ mast pipe	105	Pirod 4' Side Mount Standoff	54
4' T-Arm (7' Face)	105	5' Omni	54
Ericsson Air 21 B2A w/ mast pipe	105	Pirod 4' Side Mount Standoff	54
Licensed Sub 6 5G w/ radio _mast pipe	90	PD1142-1	54
DB-T1-6Z-12AB-OZ OVP	90	DB583	54
(2) 4' T-Boom (7' Face)	90	Pirod 4' Side Mount Standoff	54
BXA-80063-6CF w/ mast pipe	90	DB583	54
(2) SBNHH-1D65B SBS-1-2	90		

## MATERIAL STRENGTH

GRADE	F <sub>y</sub>	F <sub>u</sub>	GRADE	F <sub>y</sub>	F <sub>u</sub>
A572-65	65 ksi	80 ksi			

## TOWER DESIGN NOTES

1. Tower designed for Exposure C to the TIA-222-G Standard.
2. Tower designed for a 97 mph basic wind in accordance with the TIA-222-G Standard.
3. Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 60 mph wind.
5. Tower Structure Class II.
6. Topographic Category 1 with Crest Height of 0.00 ft
7. TOWER RATING: 92.7%

120.0 ft

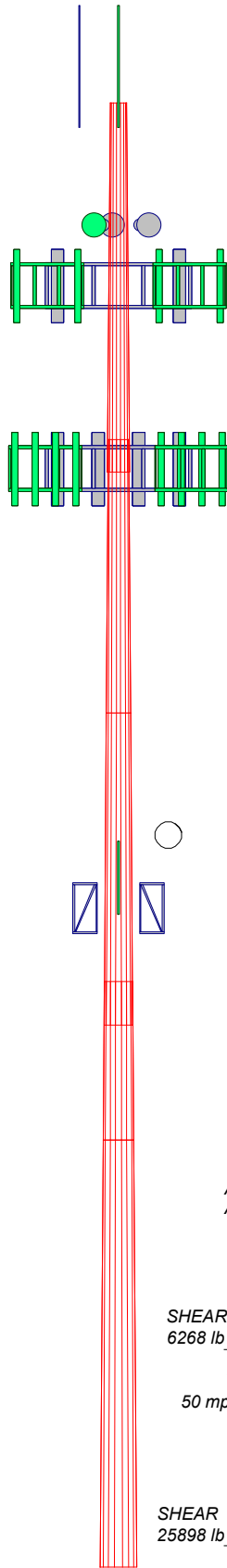
89.8 ft

70.0 ft

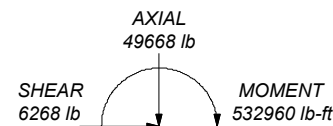
44.4 ft

35.0 ft

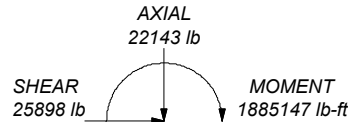
0.0 ft



ALL REACTIONS  
ARE FACTORED



TORQUE 749 lb-ft  
50 mph WIND - 1.0000 in ICE



TORQUE 3952 lb-ft  
REACTIONS - 97 mph WIND

Section	1	2	3	4	5
Length (ft)	30.25	22.42	25.58	13.00	35.00
Number of Sides	18	18	18	18	18
Thickness (in)	0.1880	0.1880	0.2750	0.2750	0.3640
Socket Length (ft)	2.67		3.58		
Top Dia (in)	16.0000	20.4443	24.3628	27.6579	29.9300
Bot Dia (in)	21.2870	24.3628	28.6342	29.9300	36.0472
Grade			A572-65		
Weight (lb)	1133.6	1011.3	2000.2	1101.2	4489.1

**Dewberry Engineers Inc.**  
99 Summer Street, Suite 700  
Boston, MA 02110  
Phone: (617) 531-0744  
FAX:

Job: <b>Hartford 9 CT</b>		
Project: <b>50002925 / 50114613</b>		
Client: VZW	Drawn by: bkelsey	App'd:
Code: TIA-222-G	Date: 12/30/20	Scale: NTS
Path:		Dwg No. E-1

# Feed Line Plan 35'

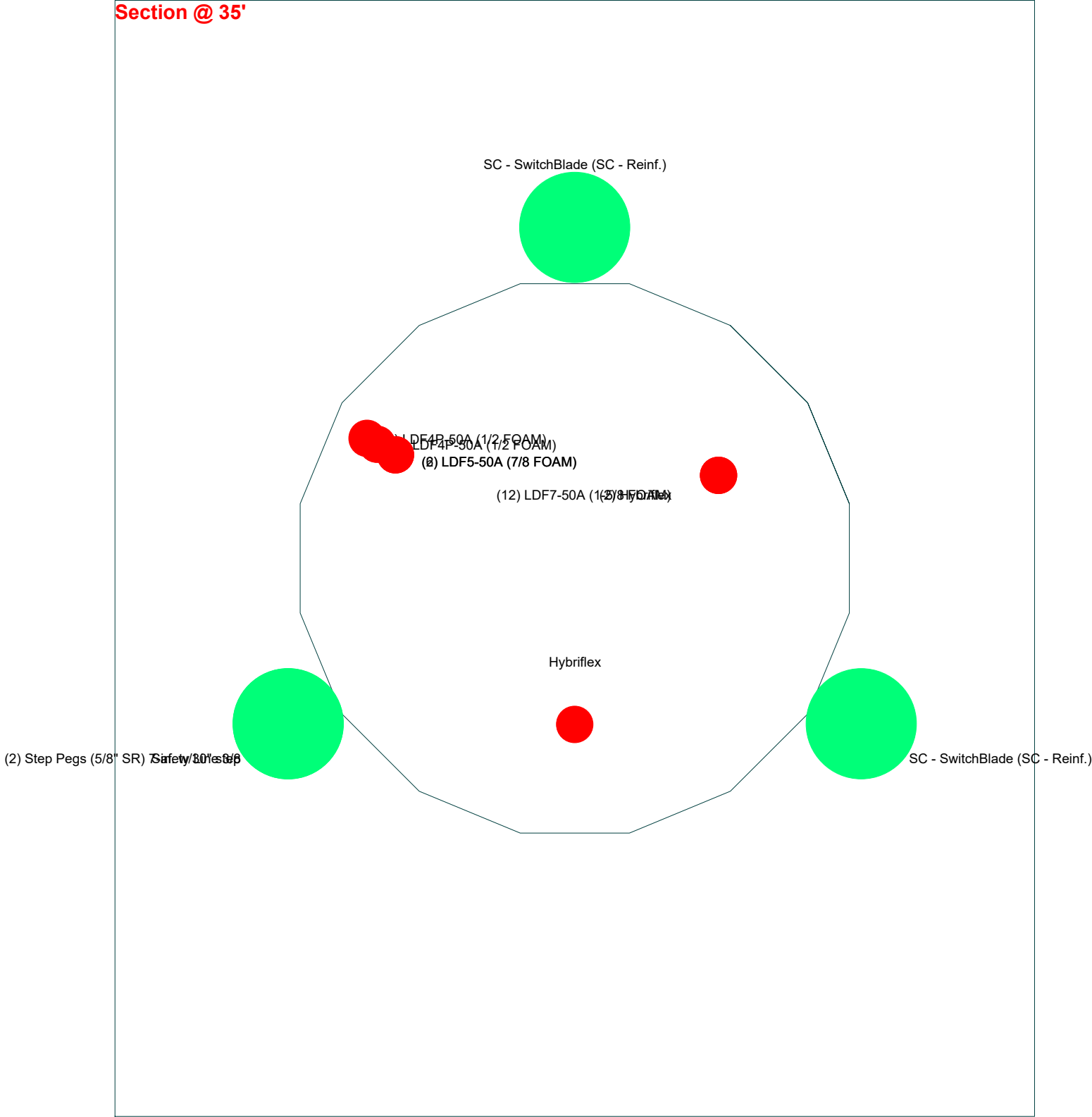
Round

Flat

App In Face

App Out Face

## Section @ 35'



<b>Dewberry Engineers Inc.</b> 99 Summer Street, Suite 700 Boston, MA 02110 Phone: (617) 531-0744 FAX:		Job: <b>Hartford 9 CT</b>	
		Project: <b>50002925 / 50114613</b>	
Client: VZW	Drawn by: bkelsey	App'd:	
Code: TIA-222-G	Date: 12/30/20	Scale: NTS	
Path:	Dwg No. E-7		

<b>tnxTower</b>  <b>Dewberry Engineers Inc.</b> 99 Summer Street, Suite 700 Boston, MA 02110 Phone: (617) 531-0744 FAX:	<b>Job</b> Hartford 9 CT	<b>Page</b> 1 of 22
	<b>Project</b> 50002925 / 50114613	<b>Date</b> 12:48:35 12/30/20
	<b>Client</b> VZW	<b>Designed by</b> bkelsey

## Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).

Basic wind speed of 97 mph.

Structure Class II.

Exposure Category C.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	120.00-89.75	30.25	2.67	18	16.0000	21.2870	0.1880	0.7520	A572-65 (65 ksi)
L2	89.75-70.00	22.42	0.00	18	20.4443	24.3628	0.1880	0.7520	A572-65 (65 ksi)
L3	70.00-44.42	25.58	3.58	18	24.3628	28.8342	0.2750	1.1000	A572-65 (65 ksi)
L4	44.42-35.00	13.00	0.00	18	27.6579	29.9300	0.2750	1.1000	A572-65 (65 ksi)
L5	35.00-0.00	35.00		18	29.9300	36.0472	0.3640	1.4560	A572-65 (65 ksi)

## Tapered Pole Properties

Section	Tip Dia. in	Area in <sup>2</sup>	I in <sup>4</sup>	r in	C in	I/C in <sup>3</sup>	J in <sup>4</sup>	I <sub>t</sub> /Q in <sup>2</sup>	w in	w/t
L1	16.2178	9.4352	298.0318	5.6133	8.1280	36.6673	596.4558	4.7185	2.4851	13.219
	21.5864	12.5900	708.0890	7.4901	10.8138	65.4802	1417.1097	6.2962	3.4156	18.168
L2	21.2046	12.0872	626.5930	7.1910	10.3857	60.3321	1254.0105	6.0448	3.2673	17.379
	24.7097	14.4254	1065.1069	8.5821	12.3763	86.0600	2131.6153	7.2141	3.9570	21.048
L3	24.6963	21.0251	1541.2419	8.5512	12.3763	124.5315	3084.5118	10.5145	3.8039	13.832
	29.2365	24.9279	2568.6995	10.1385	14.6478	175.3648	5140.7791	12.4663	4.5908	16.694
L4	28.6781	23.9012	2264.2116	9.7209	14.0502	161.1512	4531.4024	11.9529	4.3838	15.941

<b>tnxTower</b>  <b>Dewberry Engineers Inc.</b> 99 Summer Street, Suite 700 Boston, MA 02110 Phone: (617) 531-0744 FAX:	<b>Job</b> Hartford 9 CT	<b>Page</b> 2 of 22
	<b>Project</b> 50002925 / 50114613	<b>Date</b> 12:48:35 12/30/20
	<b>Client</b> VZW	<b>Designed by</b> bkelsey

Section	Tip Dia. in	Area in <sup>2</sup>	I in <sup>4</sup>	r in	C in	I/C in <sup>3</sup>	J in <sup>4</sup>	I/Q in <sup>2</sup>	w in	w/t
L5	30.3493	25.8844	2875.8902	10.5275	15.2045	189.1478	5755.5646	12.9447	4.7837	17.395
	30.3356	34.1587	3772.4625	10.4959	15.2045	248.1156	7549.8888	17.0826	4.6270	12.712
	36.5472	41.2261	6631.9001	12.6675	18.3120	362.1616	13272.5267	20.6170	5.7037	15.669

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals	Double Angle Stitch Bolt Spacing Redundants
ft	ft <sup>2</sup>	in					in	in	in
L1 120.00-89.75				1	1	1			
L2 89.75-70.00				1	1	1			
L3 70.00-44.42				1	1	1			
L4 44.42-35.00				1	1	1			
L5 35.00-0.00				1	1	1			

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	C <sub>A</sub> A <sub>A</sub> ft <sup>2</sup> /ft	Weight plf		
LDF4P-50A (1/2 FOAM)	A	No	No	Inside Pole	110.00 - 4.00	0.0000	0	2	No	0.00	0.15	
									Ice	0.00	0.15	
									1/2"	0.00	0.15	
									Ice			
LDF4P-50A (1/2 FOAM)	A	No	No	Inside Pole	55.00 - 4.00	0.0000	0	5	1" Ice	No	0.00	0.15
									Ice	0.00	0.15	
									1/2"	0.00	0.15	
									Ice			
***** Hybriflex	C	No	No	Inside Pole	105.00 - 7.00	0.0000	0	1	No	0.00	0.82	
									Ice	0.00	0.82	
									1/2"	0.00	0.82	
									Ice			
***** Hybriflex	B	No	No	Inside Pole	90.00 - 4.00	0.0000	0	2	1" Ice	No	0.00	0.82
									Ice	0.00	0.82	
									1/2"	0.00	0.82	
									Ice			
LDF7-50A (1-5/8 FOAM)	B	No	No	Inside Pole	90.00 - 4.00	0.0000	0	12	1" Ice	No	0.00	0.82
									Ice	0.00	0.82	
									1/2"	0.00	0.82	
									Ice			
***** Safety Line 3/8	C	No	No	CaAa (Out Of Face)	120.00 - 4.00	4.0000	0	1	No	0.04	0.22	
									Ice	0.14	0.75	
									1/2"	0.24	1.28	
									Ice			
Step Pegs (5/8" SR) 7-in.	C	No	No	CaAa (Out Of Face)	120.00 - 12.00	4.0000	0	2	1" Ice	No	0.30	0.49
									Ice	0.14	1.01	

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Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#		C <sub>A</sub> A <sub>A</sub> ft <sup>2</sup> /ft	Weight plf
w/30" step									1/2" Ice 1" Ice	0.23	1.53
*****											
LDF5-50A (7/8 FOAM)	A	No	No	Inside Pole	117.00 - 4.00	0.0000	0	2	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.00	0.33 0.33 0.33
LDF5-50A (7/8 FOAM)	A	No	No	Inside Pole	110.00 - 4.00	0.0000	0	6	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.00	0.33 0.33 0.33
*****											
SC - SwitchBlade (SC - Reinf.)	A	No	No	CaAa (Out Of Face)	35.00 - 0.00	0.0000	0	1	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.00	0.00 0.00 0.00
SC - SwitchBlade (SC - Reinf.)	B	No	No	CaAa (Out Of Face)	70.00 - 0.00	0.0000	0	1	No Ice 1/2" Ice 1" Ice	0.35 0.45 0.55	0.00 0.00 0.00

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight lb
L1	120.00-89.75	A	0.000	0.000	0.000	0.000	64.16
		B	0.000	0.000	0.000	0.000	2.87
		C	0.000	0.000	0.000	19.284	48.81
L2	89.75-70.00	A	0.000	0.000	0.000	0.000	58.06
		B	0.000	0.000	0.000	0.000	226.73
		C	0.000	0.000	0.000	12.591	39.90
L3	70.00-44.42	A	0.000	0.000	0.000	0.000	83.15
		B	0.000	0.000	0.000	8.954	293.69
		C	0.000	0.000	0.000	16.309	51.68
L4	44.42-35.00	A	0.000	0.000	0.000	0.000	34.75
		B	0.000	0.000	0.000	3.296	108.11
		C	0.000	0.000	0.000	6.003	19.02
L5	35.00-0.00	A	0.000	0.000	0.000	0.000	114.39
		B	0.000	0.000	0.000	12.250	355.88
		C	0.000	0.000	0.000	14.962	52.32

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight lb
L1	120.00-89.75	A	2.244	0.000	0.000	0.000	0.000	64.16
		B		0.000	0.000	0.000	0.000	2.87

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Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight lb
L2	89.75-70.00	C	2.184	0.000	0.000	0.000	14.710	261.94
		A		0.000	0.000	0.000	0.000	58.06
		B		0.000	0.000	0.000	0.000	226.73
L3	70.00-44.42	C	2.112	0.000	0.000	0.000	9.604	179.05
		A		0.000	0.000	0.000	0.000	83.15
		B		0.000	0.000	0.000	19.759	293.69
L4	44.42-35.00	C	2.037	0.000	0.000	0.000	11.764	221.32
		A		0.000	0.000	0.000	0.000	34.75
		B		0.000	0.000	0.000	7.273	108.11
L5	35.00-0.00	C	1.877	0.000	0.000	0.000	4.330	81.47
		A		0.000	0.000	0.000	0.000	114.39
		B		0.000	0.000	0.000	25.386	355.88
		C		0.000	0.000	0.000	14.103	203.77

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>x</sub> in	CP <sub>z</sub> in	CP <sub>x</sub> Ice in	CP <sub>z</sub> Ice in
L1	120.00-89.75	-2.0360	1.1755	-1.3895	0.8022
L2	89.75-70.00	-2.1304	1.2300	-1.4808	0.8549
L3	70.00-44.42	-0.8988	1.7824	0.8272	1.8831
L4	44.42-35.00	-0.9199	1.8243	0.8579	1.9531
L5	35.00-0.00	-0.2239	1.5300	0.9649	1.9108

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>A</sub> A <sub>A</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Side ft <sup>2</sup>	Weight lb
DB809K-XC	A	From Face	3.00	0.0000	117.00	No Ice	3.66	30.00
			0.00			1/2" Ice	4.91	56.00
			6.00			1" Ice	6.18	91.00
DB809K-XC	C	From Face	3.00	0.0000	117.00	No Ice	3.66	30.00
			0.00			1/2" Ice	4.91	56.00
			6.00			1" Ice	6.18	91.00
6' Long 2-3/8" Mast Pipe	A	None	0.0000	0.0000	110.00	No Ice	1.43	21.96
						1/2" Ice	1.92	32.79
						1" Ice	2.29	47.67
6' Long 2-3/8" Mast Pipe	B	None	0.0000	0.0000	110.00	No Ice	1.43	21.96
						1/2" Ice	1.92	32.79
						1" Ice	2.29	47.67
6' Long 2-3/8" Mast Pipe	C	None	0.0000	0.0000	110.00	No Ice	1.43	21.96
						1/2" Ice	1.92	32.79
						1" Ice	2.29	47.67

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz Lateral	Vert					
*****									
4' T-Arm (7' Face)	A	From Face	2.00	0.0000	105.00	No Ice	5.00	5.00	500.00
			0.00			1/2" Ice	8.00	8.00	750.00
			0.00			1" Ice	11.00	11.00	1000.00
Ericsson Air 21 B2A w/ mast pipe	A	From Face	4.00	0.0000	105.00	No Ice	6.26	5.64	104.90
			-3.50			1/2" Ice	6.74	6.49	161.79
			1.00			1" Ice	7.20	7.21	225.40
Ericsson Air 21 B2A w/ mast pipe	A	From Face	4.00	0.0000	105.00	No Ice	6.26	5.64	104.90
			3.50			1/2" Ice	6.74	6.49	161.79
			1.00			1" Ice	7.20	7.21	225.40
4' T-Arm (7' Face)	B	From Face	2.00	0.0000	105.00	No Ice	5.00	5.00	500.00
			0.00			1/2" Ice	8.00	8.00	750.00
			0.00			1" Ice	11.00	11.00	1000.00
Ericsson Air 21 B2A w/ mast pipe	B	From Face	4.00	0.0000	105.00	No Ice	6.26	5.64	104.90
			-3.50			1/2" Ice	6.74	6.49	161.79
			1.00			1" Ice	7.20	7.21	225.40
Ericsson Air 21 B2A w/ mast pipe	B	From Face	4.00	0.0000	105.00	No Ice	6.26	5.64	104.90
			3.50			1/2" Ice	6.74	6.49	161.79
			1.00			1" Ice	7.20	7.21	225.40
4' T-Arm (7' Face)	C	From Face	2.00	0.0000	105.00	No Ice	5.00	5.00	500.00
			0.00			1/2" Ice	8.00	8.00	750.00
			0.00			1" Ice	11.00	11.00	1000.00
Ericsson Air 21 B2A w/ mast pipe	C	From Face	4.00	0.0000	105.00	No Ice	6.26	5.64	104.90
			-3.50			1/2" Ice	6.74	6.49	161.79
			1.00			1" Ice	7.20	7.21	225.40
Ericsson Air 21 B2A w/ mast pipe	C	From Face	4.00	0.0000	105.00	No Ice	6.26	5.64	104.90
			3.50			1/2" Ice	6.74	6.49	161.79
			1.00			1" Ice	7.20	7.21	225.40
*****									
(2) 4' T-Boom (7' Face)	A	From Face	2.00	0.0000	90.00	No Ice	5.00	5.00	500.00
			0.00			1/2" Ice	8.00	8.00	750.00
			0.00			1" Ice	11.00	11.00	1000.00
BXA-80063-6CF w/ mast pipe	A	From Face	4.00	0.0000	90.00	No Ice	7.60	5.19	36.80
			-3.50			1/2" Ice	8.05	6.12	93.34
			0.00			1" Ice	8.51	6.93	157.38
(2) SBNHH-1D65B SBS-1-2	A	From Face	4.00	0.0000	90.00	No Ice	14.76	6.85	128.50
			-1.25			1/2" Ice	15.28	7.81	226.26
			0.00			1" Ice	15.81	8.64	332.62
B2/B66A RRH	A	From Face	4.00	0.0000	90.00	No Ice	1.88	1.25	97.50
			1.25			1/2" Ice	2.05	1.39	115.84
			2.00			1" Ice	2.22	1.54	136.97
B5/B13 RRH	A	From Face	4.00	0.0000	90.00	No Ice	1.88	1.01	82.00
			1.25			1/2" Ice	2.05	1.14	98.43
			-2.00			1" Ice	2.22	1.28	117.53
Licensed Sub 6 5G w/ radio & mast pipe	A	From Face	4.00	0.0000	90.00	No Ice	7.30	4.30	166.74
			3.50			1/2" Ice	7.79	4.93	225.67
			0.00			1" Ice	8.29	5.57	291.64
DB-T1-6Z-12AB-OZ OVP	A	From Face	0.50	0.0000	90.00	No Ice	2.82	1.85	26.00
			0.00			1/2" Ice	3.04	2.03	51.02
			2.00			1" Ice	3.25	2.22	79.31
(2) 4' T-Boom (7' Face)	B	From Face	2.00	0.0000	90.00	No Ice	5.00	5.00	500.00
			0.00			1/2" Ice	8.00	8.00	750.00
			0.00			1" Ice	11.00	11.00	1000.00
BXA-80063-6CF w/ mast pipe	B	From Face	4.00	0.0000	90.00	No Ice	7.60	5.19	36.80
			-3.50			1/2" Ice	8.05	6.12	93.34
			0.00			1" Ice	8.51	6.93	157.38
(2) SBNHH-1D65B SBS-1-2	B	From Face	4.00	0.0000	90.00	No Ice	14.76	6.85	128.50



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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight			
			Horz Lateral	Vert						ft	ft	ft
				-1.25					1/2" Ice	15.28	7.81	226.26
				0.00					1" Ice	15.81	8.64	332.62
B2/B66A RRH	B	From Face	4.00	0.0000	90.00				No Ice	1.88	1.25	97.50
			1.25						1/2" Ice	2.05	1.39	115.84
			2.00						1" Ice	2.22	1.54	136.97
B5/B13 RRH	B	From Face	4.00	0.0000	90.00				No Ice	1.88	1.01	82.00
			1.25						1/2" Ice	2.05	1.14	98.43
			-2.00						1" Ice	2.22	1.28	117.53
Licensed Sub 6 5G w/ radio & mast pipe	B	From Face	4.00	0.0000	90.00				No Ice	7.30	4.30	166.74
			3.50						1/2" Ice	7.79	4.93	225.67
			0.00						1" Ice	8.29	5.57	291.64
DB-T1-6Z-12AB-OZ OVP	B	From Face	0.50	0.0000	90.00				No Ice	2.82	1.85	26.00
			0.00						1/2" Ice	3.04	2.03	51.02
			2.00						1" Ice	3.25	2.22	79.31
(2) 4' T-Boom (7' Face)	C	From Face	2.00	0.0000	90.00				No Ice	5.00	5.00	500.00
			0.00						1/2" Ice	8.00	8.00	750.00
			0.00						1" Ice	11.00	11.00	1000.00
BXA-80063-6CF w/ mast pipe	C	From Face	4.00	0.0000	90.00				No Ice	7.60	5.19	36.80
			-3.50						1/2" Ice	8.05	6.12	93.34
			0.00						1" Ice	8.51	6.93	157.38
(2) SBNHH-1D65B SBS-1-2	C	From Face	4.00	0.0000	90.00				No Ice	14.76	6.85	128.50
			-1.25						1/2" Ice	15.28	7.81	226.26
			0.00						1" Ice	15.81	8.64	332.62
B2/B66A RRH	C	From Face	4.00	0.0000	90.00				No Ice	1.88	1.25	97.50
			1.25						1/2" Ice	2.05	1.39	115.84
			2.00						1" Ice	2.22	1.54	136.97
B5/B13 RRH	C	From Face	4.00	0.0000	90.00				No Ice	1.88	1.01	82.00
			1.25						1/2" Ice	2.05	1.14	98.43
			-2.00						1" Ice	2.22	1.28	117.53
Licensed Sub 6 5G w/ radio & mast pipe	C	From Face	4.00	0.0000	90.00				No Ice	7.30	4.30	166.74
			3.50						1/2" Ice	7.79	4.93	225.67
			0.00						1" Ice	8.29	5.57	291.64
*****												
Pirot 4' Side Mount Standoff	A	From Face	2.00	0.0000	54.00				No Ice	2.72	2.72	50.00
			0.00						1/2" Ice	4.91	4.91	89.00
			0.00						1" Ice	7.10	7.10	128.00
PD1142-1	A	From Face	4.00	0.0000	54.00				No Ice	1.32	1.32	10.00
			0.00						1/2" Ice	3.21	3.21	24.00
			9.00						1" Ice	5.12	5.12	49.00
DB583	A	From Face	4.00	0.0000	54.00				No Ice	0.54	0.54	6.20
			0.00						1/2" Ice	0.71	0.71	12.00
			-2.00						1" Ice	0.89	0.89	19.00
Pirot 4' Side Mount Standoff	B	From Face	2.00	0.0000	54.00				No Ice	2.72	2.72	50.00
			0.00						1/2" Ice	4.91	4.91	89.00
			0.00						1" Ice	7.10	7.10	128.00
DB583	B	From Face	4.00	0.0000	54.00				No Ice	0.54	0.54	6.20
			0.00						1/2" Ice	0.71	0.71	12.00
			-2.00						1" Ice	0.89	0.89	19.00
DB404 4-bay Dipole	B	From Face	4.00	0.0000	54.00				No Ice	1.14	1.14	14.00
			0.00						1/2" Ice	2.05	2.05	18.20
			2.50						1" Ice	2.96	2.96	22.40
Pirot 4' Side Mount Standoff	C	From Face	2.00	0.0000	54.00				No Ice	2.72	2.72	50.00
			0.00						1/2" Ice	4.91	4.91	89.00
			0.00						1" Ice	7.10	7.10	128.00
5' Omni	C	From Face	4.00	0.0000	54.00				No Ice	1.58	1.58	10.00
			0.00						1/2" Ice	2.40	2.40	20.00
			2.50						1" Ice	3.22	3.22	30.00

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### Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight
				Horz Lateral	Vert						
				ft	°	°	ft	ft	ft <sup>2</sup>	lb	
2' Diameter Dish w/o Radome	C	Paraboloid w/o Radome	From Face	1.00	0.0000		110.00	2.00	No Ice	3.14	35.00
				2.00				1/2" Ice	3.41	52.50	
				0.00				1" Ice	3.68	70.01	
2' Diameter Dish w/o Radome	A	Paraboloid w/o Radome	From Face	1.00	0.0000		110.00	2.00	No Ice	3.14	35.00
				2.00				1/2" Ice	3.41	52.50	
				0.00				1" Ice	3.68	70.01	
2' Diameter Dish w/o Radome	B	Paraboloid w/o Radome	From Face	1.00	0.0000		110.00	2.00	No Ice	3.14	35.00
				2.00				1/2" Ice	3.41	52.50	
				0.00				1" Ice	3.68	70.01	
1' Dish w/o Radome	A	Paraboloid w/o Radome	From Face	1.00	0.0000		110.00	1.00	No Ice	0.79	10.00
				0.50				1/2" Ice	0.92	20.00	
				0.00				1" Ice	1.06	30.00	
1' Dish w/o Radome	B	Paraboloid w/o Radome	From Face	1.00	0.0000		110.00	1.00	No Ice	0.79	10.00
				0.50				1/2" Ice	0.92	20.00	
				0.00				1" Ice	1.06	30.00	

### Tower Pressures - No Ice

$G_H = 1.100$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face
ft	ft		psf	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
L1 120.00-89.75	104.27	1.277	29	47.649	A	0.000	47.649	47.649	100.00	0.000	0.000
					B	0.000	47.649	100.00	0.000	0.000	
					C	0.000	47.649	100.00	0.000	19.284	
L2 89.75-70.00	79.62	1.206	28	37.784	A	0.000	37.784	37.784	100.00	0.000	0.000
					B	0.000	37.784	100.00	0.000	0.000	
					C	0.000	37.784	100.00	0.000	12.591	
L3 70.00-44.42	56.85	1.124	26	57.490	A	0.000	57.490	57.490	100.00	0.000	0.000
					B	0.000	57.490	100.00	0.000	8.954	
					C	0.000	57.490	100.00	0.000	16.309	
L4 44.42-35.00	39.66	1.042	24	23.161	A	0.000	23.161	23.161	100.00	0.000	0.000
					B	0.000	23.161	100.00	0.000	3.296	
					C	0.000	23.161	100.00	0.000	6.003	
L5 35.00-0.00	17.46	0.876	21	97.537	A	0.000	97.537	97.537	100.00	0.000	0.000
					B	0.000	97.537	100.00	0.000	12.250	
					C	0.000	97.537	100.00	0.000	14.962	

### Tower Pressure - With Ice

$G_H = 1.100$

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	<b>Client</b> VZW	<b>Designed by</b> bkelsey

Section Elevation <i>ft</i>	<i>z</i> <i>ft</i>	<i>K<sub>Z</sub></i>	<i>q<sub>z</sub></i> <i>psf</i>	<i>t<sub>Z</sub></i> <i>in</i>	<i>A<sub>G</sub></i> <i>ft<sup>2</sup></i>	<i>F<sub>a</sub></i> <i>c</i> <i>e</i>	<i>A<sub>F</sub></i> <i>ft<sup>2</sup></i>	<i>A<sub>R</sub></i> <i>ft<sup>2</sup></i>	<i>A<sub>leg</sub></i> <i>ft<sup>2</sup></i>	<i>Leg</i> <i>%</i>	<i>C<sub>AA</sub></i> <i>In</i> <i>Face</i> <i>ft<sup>2</sup></i>	<i>C<sub>AA</sub></i> <i>Out</i> <i>Face</i> <i>ft<sup>2</sup></i>
L1 120.00-89.75	104.27	1.277	8	2.2439	58.962	A	0.000	58.962	58.962	100.00	0.000	0.000
						B	0.000	58.962	100.00	0.000	0.000	
						C	0.000	58.962	100.00	0.000	14.710	
L2 89.75-70.00	79.62	1.206	7	2.1842	45.170	A	0.000	45.170	45.170	100.00	0.000	0.000
						B	0.000	45.170	100.00	0.000	0.000	
						C	0.000	45.170	100.00	0.000	9.604	
L3 70.00-44.42	56.85	1.124	7	2.1118	66.494	A	0.000	66.494	66.494	100.00	0.000	0.000
						B	0.000	66.494	100.00	0.000	19.759	
						C	0.000	66.494	100.00	0.000	11.764	
L4 44.42-35.00	39.66	1.042	6	2.0371	26.475	A	0.000	26.475	26.475	100.00	0.000	0.000
						B	0.000	26.475	100.00	0.000	7.273	
						C	0.000	26.475	100.00	0.000	4.330	
L5 35.00-0.00	17.46	0.876	5	1.8767	108.485	A	0.000	108.485	108.485	100.00	0.000	0.000
						B	0.000	108.485	100.00	0.000	25.386	
						C	0.000	108.485	100.00	0.000	14.103	

### Tower Pressure - Service

$G_H = 1.100$

Section Elevation <i>ft</i>	<i>z</i> <i>ft</i>	<i>K<sub>Z</sub></i>	<i>q<sub>z</sub></i> <i>psf</i>	<i>A<sub>G</sub></i> <i>ft<sup>2</sup></i>	<i>F<sub>a</sub></i> <i>c</i> <i>e</i>	<i>A<sub>F</sub></i> <i>ft<sup>2</sup></i>	<i>A<sub>R</sub></i> <i>ft<sup>2</sup></i>	<i>A<sub>leg</sub></i> <i>ft<sup>2</sup></i>	<i>Leg</i> <i>%</i>	<i>C<sub>AA</sub></i> <i>In</i> <i>Face</i> <i>ft<sup>2</sup></i>	<i>C<sub>AA</sub></i> <i>Out</i> <i>Face</i> <i>ft<sup>2</sup></i>
L1 120.00-89.75	104.27	1.277	10	47.649	A	0.000	47.649	47.649	100.00	0.000	0.000
					B	0.000	47.649	100.00	0.000	0.000	
					C	0.000	47.649	100.00	0.000	19.284	
L2 89.75-70.00	79.62	1.206	9	37.784	A	0.000	37.784	37.784	100.00	0.000	0.000
					B	0.000	37.784	100.00	0.000	0.000	
					C	0.000	37.784	100.00	0.000	12.591	
L3 70.00-44.42	56.85	1.124	9	57.490	A	0.000	57.490	57.490	100.00	0.000	0.000
					B	0.000	57.490	100.00	0.000	8.954	
					C	0.000	57.490	100.00	0.000	16.309	
L4 44.42-35.00	39.66	1.042	8	23.161	A	0.000	23.161	23.161	100.00	0.000	0.000
					B	0.000	23.161	100.00	0.000	3.296	
					C	0.000	23.161	100.00	0.000	6.003	
L5 35.00-0.00	17.46	0.876	7	97.537	A	0.000	97.537	97.537	100.00	0.000	0.000
					B	0.000	97.537	100.00	0.000	12.250	
					C	0.000	97.537	100.00	0.000	14.962	

### Tower Forces - No Ice - Wind Normal To Face

Section Elevation <i>ft</i>	<i>Add</i> <i>Weight</i> <i>lb</i>	<i>Self</i> <i>Weight</i> <i>lb</i>	<i>F<sub>a</sub></i> <i>c</i> <i>e</i>	<i>e</i>	<i>C<sub>F</sub></i>	<i>q<sub>z</sub></i> <i>psf</i>	<i>D<sub>F</sub></i>	<i>D<sub>R</sub></i>	<i>A<sub>E</sub></i> <i>ft<sup>2</sup></i>	<i>F</i> <i>lb</i>	<i>w</i> <i>plf</i>	<i>Ctrl.</i> <i>Face</i>
L1 120.00-89.75	115.83	1133.58	A	1	1.2	29	1	1	47.649	2455.80	81.18	C
			B	1	1.2	1	1	47.649				
			C	1	1.2	1	1	47.649				
L2 89.75-70.00	324.69	1011.33	A	1	1.2	28	1	1	37.784	1759.06	89.07	C
			B	1	1.2	1	1	37.784				
			C	1	1.2	1	1	37.784				

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Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L3 70.00-44.42	428.52	2000.18	C	1	1.2		1	1	37.784			
			A	1	1.2	26	1	1	57.490	2665.97	104.21	C
			B	1	1.2		1	1	57.490			
			C	1	1.2		1	1	57.490			
L4 44.42-35.00	161.88	1101.17	A	1	1.2	24	1	1	23.161	972.61	103.28	C
			B	1	1.2		1	1	23.161			
			C	1	1.2		1	1	23.161			
L5 35.00-0.00	522.59	4489.08	A	1	1.2	21	1	1	97.537	3266.37	93.32	C
			B	1	1.2		1	1	97.537			
			C	1	1.2		1	1	97.537			
Sum Weight:	1553.51	9735.34						OTM	643314.72 lb-ft	11119.81		

**Tower Forces - No Ice - Wind 60 To Face**

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L1 120.00-89.75	115.83	1133.58	A	1	1.2	29	1	1	47.649	2455.80	81.18	C
			B	1	1.2		1	1	47.649			
			C	1	1.2		1	1	47.649			
L2 89.75-70.00	324.69	1011.33	A	1	1.2	28	1	1	37.784	1759.06	89.07	C
			B	1	1.2		1	1	37.784			
			C	1	1.2		1	1	37.784			
L3 70.00-44.42	428.52	2000.18	A	1	1.2	26	1	1	57.490	2665.97	104.21	C
			B	1	1.2		1	1	57.490			
			C	1	1.2		1	1	57.490			
L4 44.42-35.00	161.88	1101.17	A	1	1.2	24	1	1	23.161	972.61	103.28	C
			B	1	1.2		1	1	23.161			
			C	1	1.2		1	1	23.161			
L5 35.00-0.00	522.59	4489.08	A	1	1.2	21	1	1	97.537	3266.37	93.32	C
			B	1	1.2		1	1	97.537			
			C	1	1.2		1	1	97.537			
Sum Weight:	1553.51	9735.34						OTM	643314.72 lb-ft	11119.81		

**Tower Forces - No Ice - Wind 90 To Face**

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L1 120.00-89.75	115.83	1133.58	A	1	1.2	29	1	1	47.649	2455.80	81.18	C
			B	1	1.2		1	1	47.649			
			C	1	1.2		1	1	47.649			
L2 89.75-70.00	324.69	1011.33	A	1	1.2	28	1	1	37.784	1759.06	89.07	C
			B	1	1.2		1	1	37.784			
			C	1	1.2		1	1	37.784			

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Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L3 70.00-44.42	428.52	2000.18	A	1	1.2	26	1	1	57.490	2665.97	104.21	C
			B	1	1.2		1	1	57.490			
			C	1	1.2		1	1	57.490			
L4 44.42-35.00	161.88	1101.17	A	1	1.2	24	1	1	23.161	972.61	103.28	C
			B	1	1.2		1	1	23.161			
			C	1	1.2		1	1	23.161			
L5 35.00-0.00	522.59	4489.08	A	1	1.2	21	1	1	97.537	3266.37	93.32	C
			B	1	1.2		1	1	97.537			
			C	1	1.2		1	1	97.537			
Sum Weight:	1553.51	9735.34						OTM	643314.72 lb-ft	11119.81		

### Tower Forces - With Ice - Wind Normal To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L1 120.00-89.75	328.96	2883.58	A	1	1.2	8	1	1	58.962	729.32	24.11	C
			B	1	1.2		1	1	58.962			
			C	1	1.2		1	1	58.962			
L2 89.75-70.00	463.84	2332.94	A	1	1.2	7	1	1	44.973	512.90	25.97	C
			B	1	1.2		1	1	44.973			
			C	1	1.2		1	1	44.973			
L3 70.00-44.42	598.16	3914.76	A	1	1.2	7	1	1	66.494	836.61	32.70	C
			B	1	1.2		1	1	66.494			
			C	1	1.2		1	1	66.494			
L4 44.42-35.00	224.32	1838.63	A	1	1.2	6	1	1	26.358	301.21	31.99	C
			B	1	1.2		1	1	26.358			
			C	1	1.2		1	1	26.358			
L5 35.00-0.00	674.04	7315.80	A	1	1.2	5	1	1	108.485	1020.77	29.16	C
			B	1	1.2		1	1	108.485			
			C	1	1.2		1	1	108.485			
Sum Weight:	2289.33	18285.71						OTM	194221.55 lb-ft	3400.82		

### Tower Forces - With Ice - Wind 60 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L1 120.00-89.75	328.96	2883.58	A	1	1.2	8	1	1	58.962	729.32	24.11	C
			B	1	1.2		1	1	58.962			
			C	1	1.2		1	1	58.962			
L2 89.75-70.00	463.84	2332.94	A	1	1.2	7	1	1	44.973	512.90	25.97	C
			B	1	1.2		1	1	44.973			
			C	1	1.2		1	1	44.973			
L3 70.00-44.42	598.16	3914.76	A	1	1.2	7	1	1	66.494	836.61	32.70	C

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Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
70.00-44.42			B	1	1.2		1	1	66.494			
			C	1	1.2		1	1	66.494			
L4 44.42-35.00	224.32	1838.63	A	1	1.2	6	1	1	26.358	301.21	31.99	C
			B	1	1.2		1	1	26.358			
			C	1	1.2		1	1	26.358			
L5 35.00-0.00	674.04	7315.80	A	1	1.2	5	1	1	108.485	1020.77	29.16	C
			B	1	1.2		1	1	108.485			
			C	1	1.2		1	1	108.485			
Sum Weight:	2289.33	18285.71						OTM	194221.55 lb-ft	3400.82		

### Tower Forces - With Ice - Wind 90 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L1 120.00-89.75	328.96	2883.58	A	1	1.2	8	1	1	58.962	729.32	24.11	C
			B	1	1.2		1	1	58.962			
			C	1	1.2		1	1	58.962			
L2 89.75-70.00	463.84	2332.94	A	1	1.2	7	1	1	44.973	512.90	25.97	C
			B	1	1.2		1	1	44.973			
			C	1	1.2		1	1	44.973			
L3 70.00-44.42	598.16	3914.76	A	1	1.2	7	1	1	66.494	836.61	32.70	C
			B	1	1.2		1	1	66.494			
			C	1	1.2		1	1	66.494			
L4 44.42-35.00	224.32	1838.63	A	1	1.2	6	1	1	26.358	301.21	31.99	C
			B	1	1.2		1	1	26.358			
			C	1	1.2		1	1	26.358			
L5 35.00-0.00	674.04	7315.80	A	1	1.2	5	1	1	108.485	1020.77	29.16	C
			B	1	1.2		1	1	108.485			
			C	1	1.2		1	1	108.485			
Sum Weight:	2289.33	18285.71						OTM	194221.55 lb-ft	3400.82		

### Tower Forces - Service - Wind Normal To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L1 120.00-89.75	115.83	1133.58	A	1	1.2	10	1	1	47.649	840.71	27.79	C
			B	1	1.2		1	1	47.649			
			C	1	1.2		1	1	47.649			
L2 89.75-70.00	324.69	1011.33	A	1	1.2	9	1	1	37.784	602.19	30.49	C
			B	1	1.2		1	1	37.784			
			C	1	1.2		1	1	37.784			
L3 70.00-44.42	428.52	2000.18	A	1	1.2	9	1	1	57.490	912.66	35.67	C
			B	1	1.2		1	1	57.490			

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Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L4 44.42-35.00	161.88	1101.17	C	1	1.2	8	1	1	57.490	332.96	35.36	C
			A	1	1.2		1	1	23.161			
			B	1	1.2		1	1	23.161			
L5 35.00-0.00	522.59	4489.08	C	1	1.2	7	1	1	23.161	1118.20	31.95	C
			A	1	1.2		1	1	97.537			
			B	1	1.2		1	1	97.537			
Sum Weight:	1553.51	9735.34	C	1	1.2		1	1	97.537			
								OTM	220230.69 lb-ft	3806.73		

### Tower Forces - Service - Wind 60 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L1 120.00-89.75	115.83	1133.58	A	1	1.2	10	1	1	47.649	840.71	27.79	C
			B	1	1.2		1	1	47.649			
			C	1	1.2		1	1	47.649			
L2 89.75-70.00	324.69	1011.33	A	1	1.2	9	1	1	37.784	602.19	30.49	C
			B	1	1.2		1	1	37.784			
			C	1	1.2		1	1	37.784			
L3 70.00-44.42	428.52	2000.18	A	1	1.2	9	1	1	57.490	912.66	35.67	C
			B	1	1.2		1	1	57.490			
			C	1	1.2		1	1	57.490			
L4 44.42-35.00	161.88	1101.17	A	1	1.2	8	1	1	23.161	332.96	35.36	C
			B	1	1.2		1	1	23.161			
			C	1	1.2		1	1	23.161			
L5 35.00-0.00	522.59	4489.08	A	1	1.2	7	1	1	97.537	1118.20	31.95	C
			B	1	1.2		1	1	97.537			
			C	1	1.2		1	1	97.537			
Sum Weight:	1553.51	9735.34	C	1	1.2		1	1	97.537			
								OTM	220230.69 lb-ft	3806.73		

### Tower Forces - Service - Wind 90 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L1 120.00-89.75	115.83	1133.58	A	1	1.2	10	1	1	47.649	840.71	27.79	C
			B	1	1.2		1	1	47.649			
			C	1	1.2		1	1	47.649			
L2 89.75-70.00	324.69	1011.33	A	1	1.2	9	1	1	37.784	602.19	30.49	C
			B	1	1.2		1	1	37.784			
			C	1	1.2		1	1	37.784			
L3 70.00-44.42	428.52	2000.18	A	1	1.2	9	1	1	57.490	912.66	35.67	C
			B	1	1.2		1	1	57.490			
			C	1	1.2		1	1	57.490			

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Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F lb	w plf	Ctrl. Face
L4 44.42-35.00	161.88	1101.17	A	1	1.2	8	1	1	23.161	332.96	35.36	C
			B	1	1.2		1	1	23.161			
			C	1	1.2		1	1	23.161			
L5 35.00-0.00	522.59	4489.08	A	1	1.2	7	1	1	97.537	1118.20	31.95	C
			B	1	1.2		1	1	97.537			
			C	1	1.2		1	1	97.537			
Sum Weight:	1553.51	9735.34						OTM	220230.69 lb-ft	3806.73		

### Force Totals

Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Overturning Moments, M <sub>x</sub> lb-ft	Sum of Overturning Moments, M <sub>z</sub> lb-ft	Sum of Torques lb-ft
Leg Weight	9735.34					
Bracing Weight	0.00					
Total Member Self-Weight	9735.34			28.62	192.18	
Total Weight	18452.15			28.62	192.18	
Wind 0 deg - No Ice		0.00	-16113.22	-1119762.26	192.18	-1592.16
Wind 30 deg - No Ice		7988.00	-13969.32	-971373.40	-551936.24	-672.70
Wind 60 deg - No Ice		14039.59	-8054.84	-559671.49	-978559.16	105.01
Wind 90 deg - No Ice		16135.41	97.76	10782.32	-1121600.51	1345.00
Wind 120 deg - No Ice		13998.32	8064.79	560823.25	-974019.62	1884.71
Wind 150 deg - No Ice		8147.01	13891.32	962850.45	-569427.96	1827.61
Wind 180 deg - No Ice		0.00	16167.24	1125761.81	192.18	973.93
Wind 210 deg - No Ice		-8147.01	13891.32	962850.45	569812.31	371.54
Wind 240 deg - No Ice		-13998.32	8064.79	560823.25	974403.98	-698.80
Wind 270 deg - No Ice		-16135.41	97.76	10782.32	1121984.87	-1679.21
Wind 300 deg - No Ice		-14039.59	-8054.84	-559671.49	978943.52	-2509.51
Wind 330 deg - No Ice		-7988.00	-13969.32	-971373.40	552320.60	-2174.20
Member Ice	8550.37					
Total Weight Ice	45517.94			249.90	1396.81	
Wind 0 deg - Ice		0.00	-6239.95	-458570.96	1396.81	-417.25
Wind 30 deg - Ice		3093.97	-5409.28	-397686.52	-225086.49	-156.82
Wind 60 deg - Ice		5437.53	-3117.44	-228881.38	-399533.01	24.65
Wind 90 deg - Ice		6249.01	37.96	4425.71	-458289.06	381.14
Wind 120 deg - Ice		5421.04	3123.82	230083.85	-397719.08	509.84
Wind 150 deg - Ice		3154.86	5380.62	395034.23	-231784.97	467.87
Wind 180 deg - Ice		0.00	6261.99	461495.25	1396.81	186.69
Wind 210 deg - Ice		-3154.86	5380.62	395034.23	234578.60	47.39
Wind 240 deg - Ice		-5421.04	3123.82	230083.85	400512.71	-243.70
Wind 270 deg - Ice		-6249.01	37.96	4425.71	461082.69	-506.14
Wind 300 deg - Ice		-5437.53	-3117.44	-228881.38	402326.64	-743.49
Wind 330 deg - Ice		-3093.97	-5409.28	-397686.52	227880.12	-598.71
Total Weight	18452.15			28.62	192.18	
Wind 0 deg - Service		0.00	-5516.16	-383386.46	73.05	-545.05
Wind 30 deg - Service		2734.59	-4782.22	-332587.40	-188941.16	-230.29
Wind 60 deg - Service		4806.28	-2757.47	-191646.44	-334990.14	35.95
Wind 90 deg - Service		5523.75	33.47	3641.23	-383958.54	460.45
Wind 120 deg - Service		4792.15	2760.88	191940.82	-333436.08	645.21
Wind 150 deg - Service		2789.03	4755.52	329569.77	-194929.22	625.66
Wind 180 deg - Service		0.00	5534.65	385340.42	73.05	333.41
Wind 210 deg - Service		-2789.03	4755.52	329569.77	195075.33	127.19



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Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Overturning Moments, $M_x$ lb-ft	Sum of Overturning Moments, $M_z$ lb-ft	Sum of Torques lb-ft
Wind 240 deg - Service		-4792.15	2760.88	191940.82	333582.19	-239.23
Wind 270 deg - Service		-5523.75	33.47	3641.23	384104.65	-574.86
Wind 300 deg - Service		-4806.28	-2757.47	-191646.44	335136.25	-859.10
Wind 330 deg - Service		-2734.59	-4782.22	-332587.40	189087.26	-744.31

## Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service

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Comb. No.	Description
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment lb-ft	Minor Axis Moment lb-ft
L1	120 - 89.75	Pole	Max Tension	33	0.01	-0.30	0.67
			Max. Compression	26	-22165.70	356.76	45.53
			Max. Mx	20	-3290.00	105127.84	-2817.40
			Max. My	14	-3273.04	110.51	-106652.72
			Max. Vy	8	8982.93	-65480.08	-1677.44
			Max. Vx	14	9006.16	54.87	-66424.02
L2	89.75 - 70	Pole	Max. Torque	22			1942.83
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-32185.10	947.87	-152.90
			Max. Mx	20	-9937.48	403701.17	-6671.36
			Max. My	14	-9925.14	133.77	-406436.77
			Max. Vy	20	-15407.84	403701.17	-6671.36
L3	70 - 44.417	Pole	Max. Vx	14	15463.27	133.77	-406436.77
			Max. Torque	22			2403.46
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-37354.63	1350.76	-102.69
			Max. Mx	20	-12859.71	783354.04	-10359.66
			Max. My	14	-12850.73	160.50	-787256.12
L4	44.417 - 35	Pole	Max. Vy	20	-19339.90	783354.04	-10359.66
			Max. Vx	14	19394.42	160.50	-787256.12
			Max. Torque	23			2974.65
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-40675.44	1458.24	-164.79
			Max. Mx	20	-15075.70	1048404.52	-12532.85
L5	35 - 0	Pole	Max. My	14	-15069.08	185.31	-1053003.14
			Max. Vy	20	-21373.37	1048404.52	-12532.85
			Max. Vx	14	21427.18	185.31	-1053003.14
			Max. Torque	23			3337.05
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-49667.63	1674.68	-289.97
			Max. Mx	20	-22110.68	1875650.13	-18177.61
			Max. My	14	-22110.51	228.10	-1882068.38
			Max. Vy	20	-25843.98	1875650.13	-18177.61
			Max. Vx	14	25895.01	228.10	-1882068.38
			Max. Torque	23			3952.40

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal, X lb	Horizontal, Z lb
Pole	Max. Vert	37	49667.63	5437.60	3117.47

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Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal, X lb	Horizontal, Z lb
	Max. H <sub>x</sub>	20	22142.58	25816.66	-156.42
	Max. H <sub>z</sub>	2	22142.58	0.00	25781.16
	Max. M <sub>x</sub>	2	1872032.34	0.00	25781.16
	Max. M <sub>z</sub>	8	1875158.42	-25816.66	-156.42
	Max. Torsion	23	3952.42	22463.34	12887.74
	Min. Vert	23	16606.93	22463.34	12887.74
	Min. H <sub>x</sub>	8	22142.58	-25816.66	-156.42
	Min. H <sub>z</sub>	14	22142.58	0.00	-25867.59
	Min. M <sub>x</sub>	14	-1882068.38	0.00	-25867.59
	Min. M <sub>z</sub>	20	-1875650.14	25816.66	-156.42
	Min. Torsion	11	-2972.76	-22397.31	-12903.66

### Tower Mast Reaction Summary

Load Combination	Vertical lb	Shear <sub>x</sub> lb	Shear <sub>z</sub> lb	Overturning Moment, M <sub>x</sub> lb-ft	Overturning Moment, M <sub>z</sub> lb-ft	Torque lb-ft
Dead Only	18452.15	0.00	0.00	28.62	192.18	0.00
1.2 Dead+1.6 Wind 0 deg - No Ice	22142.58	-0.00	-25781.16	-1872032.34	209.77	-2504.81
0.9 Dead+1.6 Wind 0 deg - No Ice	16606.93	-0.00	-25781.16	-1849841.41	154.70	-2504.21
1.2 Dead+1.6 Wind 30 deg - No Ice	22142.58	12780.80	-22350.91	-1624003.69	-922685.73	-1051.65
0.9 Dead+1.6 Wind 30 deg - No Ice	16606.93	12780.80	-22350.91	-1604746.58	-911842.66	-1050.78
1.2 Dead+1.6 Wind 60 deg - No Ice	22142.58	22463.34	-12887.74	-935613.50	-1636092.48	180.66
0.9 Dead+1.6 Wind 60 deg - No Ice	16606.93	22463.34	-12887.74	-924532.35	-1616716.59	181.00
1.2 Dead+1.6 Wind 90 deg - No Ice	22142.58	25816.66	156.42	18186.45	-1875158.42	2127.25
0.9 Dead+1.6 Wind 90 deg - No Ice	16606.93	25816.66	156.42	17913.21	-1852981.84	2127.69
1.2 Dead+1.6 Wind 120 deg - No Ice	22142.58	22397.31	12903.66	937536.01	-1628473.06	2972.62
0.9 Dead+1.6 Wind 120 deg - No Ice	16606.93	22397.31	12903.66	926412.91	-1609205.03	2972.76
1.2 Dead+1.6 Wind 150 deg - No Ice	22142.58	13035.22	22226.11	1609555.44	-952244.91	2880.78
0.9 Dead+1.6 Wind 150 deg - No Ice	16606.93	13035.22	22226.11	1590497.14	-940961.16	2880.37
1.2 Dead+1.6 Wind 180 deg - No Ice	22142.58	-0.00	25867.59	1882068.38	227.53	1539.74
0.9 Dead+1.6 Wind 180 deg - No Ice	16606.93	-0.00	25867.59	1859714.44	167.53	1538.26
1.2 Dead+1.6 Wind 210 deg - No Ice	22142.58	-13035.22	22226.11	1609579.15	952696.84	586.10
0.9 Dead+1.6 Wind 210 deg - No Ice	16606.93	-13035.22	22226.11	1590514.29	941294.00	584.73
1.2 Dead+1.6 Wind 240 deg - No Ice	22142.58	-22397.31	12903.66	937557.15	1628952.46	-1102.07
0.9 Dead+1.6 Wind 240 deg - No Ice	16606.93	-22397.31	12903.66	926428.21	1609557.74	-1103.37
1.2 Dead+1.6 Wind 270 deg - No Ice	22142.58	-25816.66	156.42	18176.65	1875650.14	-2648.41
0.9 Dead+1.6 Wind 270 deg - No Ice	16606.93	-25816.66	156.42	17906.14	1853343.47	-2649.42

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Load Combination	Vertical lb	Shear <sub>x</sub> lb	Shear <sub>z</sub> lb	Overturning Moment, M <sub>x</sub> lb-ft	Overturning Moment, M <sub>z</sub> lb-ft	Torque lb-ft
No Ice						
1.2 Dead+1.6 Wind 300 deg - No Ice	22142.58	-22463.34	-12887.74	-935665.72	1636554.15	-3951.44
0.9 Dead+1.6 Wind 300 deg - No Ice	16606.93	-22463.34	-12887.74	-924570.09	1617056.50	-3952.42
1.2 Dead+1.6 Wind 330 deg - No Ice	22142.58	-12780.80	-22350.91	-1624035.57	923120.94	-3426.65
0.9 Dead+1.6 Wind 330 deg - No Ice	16606.93	-12780.80	-22350.91	-1604769.63	912163.42	-3426.61
1.2 Dead+1.0 Ice+1.0 Temp	49667.63	-0.01	0.00	289.97	1674.68	-0.00
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	49667.63	-0.00	-6240.02	-527754.33	1772.94	-429.12
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	49667.63	3094.00	-5409.34	-457702.88	-258766.51	-166.66
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	49667.63	5437.55	-3117.44	-263395.69	-459777.56	19.36
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	49667.63	6249.09	37.96	5262.29	-527287.21	381.50
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	49667.63	5421.06	3123.83	264836.98	-457625.18	516.12
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	49667.63	3154.90	5380.69	454565.16	-266726.31	478.59
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	49667.63	-0.00	6262.06	531241.31	1777.16	199.21
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	49667.63	-3154.87	5380.63	454579.03	270284.77	57.53
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	49667.63	-5421.06	3123.83	264840.41	461182.66	-237.70
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	49667.63	-6249.09	37.96	5259.86	530846.64	-505.83
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	49667.63	-5437.60	-3117.47	-263400.94	463320.75	-749.28
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp	49667.63	-3093.97	-5409.29	-457718.93	262320.88	-609.40
Dead+Wind 0 deg - Service	18452.15	-0.00	-5516.16	-398390.91	203.69	-546.23
Dead+Wind 30 deg - Service	18452.15	2734.59	-4782.22	-345601.74	-196214.12	-231.18
Dead+Wind 60 deg - Service	18452.15	4806.28	-2757.47	-199110.49	-348062.56	35.56
Dead+Wind 90 deg - Service	18452.15	5523.76	33.47	3893.38	-398929.96	460.42
Dead+Wind 120 deg - Service	18452.15	4792.15	2760.88	199563.75	-346432.31	645.71
Dead+Wind 150 deg - Service	18452.15	2789.03	4755.52	342578.98	-202499.37	626.69
Dead+Wind 180 deg - Service	18452.15	-0.00	5534.65	400585.85	204.36	334.83
Dead+Wind 210 deg - Service	18452.15	-2789.03	4755.52	342579.88	202907.97	128.37
Dead+Wind 240 deg - Service	18452.15	-4792.15	2760.88	199564.55	346841.96	-238.41
Dead+Wind 270 deg - Service	18452.15	-5523.76	33.47	3893.01	399340.08	-574.65
Dead+Wind 300 deg - Service	18452.15	-4806.28	-2757.47	-199112.48	348471.54	-859.55
Dead+Wind 330 deg - Service	18452.15	-2734.59	-4782.22	-345602.96	196622.09	-745.42

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX lb	PY lb	PZ lb	PX lb	PY lb	PZ lb	
1	0.00	-18452.15	0.00	0.00	18452.15	0.00	0.000%
2	0.00	-22142.58	-25781.16	0.00	22142.58	25781.16	0.000%
3	0.00	-16606.93	-25781.16	0.00	16606.93	25781.16	0.000%
4	12780.80	-22142.58	-22350.91	-12780.80	22142.58	22350.91	0.000%
5	12780.80	-16606.93	-22350.91	-12780.80	16606.93	22350.91	0.000%
6	22463.34	-22142.58	-12887.74	-22463.34	22142.58	12887.74	0.000%

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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX lb	PY lb	PZ lb	PX lb	PY lb	PZ lb	
7	22463.34	-16606.93	-12887.74	-22463.34	16606.93	12887.74	0.000%
8	25816.66	-22142.58	156.42	-25816.66	22142.58	-156.42	0.000%
9	25816.66	-16606.93	156.42	-25816.66	16606.93	-156.42	0.000%
10	22397.31	-22142.58	12903.66	-22397.31	22142.58	-12903.66	0.000%
11	22397.31	-16606.93	12903.66	-22397.31	16606.93	-12903.66	0.000%
12	13035.22	-22142.58	22226.11	-13035.22	22142.58	-22226.11	0.000%
13	13035.22	-16606.93	22226.11	-13035.22	16606.93	-22226.11	0.000%
14	0.00	-22142.58	25867.59	0.00	22142.58	-25867.59	0.000%
15	0.00	-16606.93	25867.59	0.00	16606.93	-25867.59	0.000%
16	-13035.22	-22142.58	22226.11	13035.22	22142.58	-22226.11	0.000%
17	-13035.22	-16606.93	22226.11	13035.22	16606.93	-22226.11	0.000%
18	-22397.31	-22142.58	12903.66	22397.31	22142.58	-12903.66	0.000%
19	-22397.31	-16606.93	12903.66	22397.31	16606.93	-12903.66	0.000%
20	-25816.66	-22142.58	156.42	25816.66	22142.58	-156.42	0.000%
21	-25816.66	-16606.93	156.42	25816.66	16606.93	-156.42	0.000%
22	-22463.34	-22142.58	-12887.74	22463.34	22142.58	12887.74	0.000%
23	-22463.34	-16606.93	-12887.74	22463.34	16606.93	12887.74	0.000%
24	-12780.80	-22142.58	-22350.91	12780.80	22142.58	22350.91	0.000%
25	-12780.80	-16606.93	-22350.91	12780.80	16606.93	22350.91	0.000%
26	0.00	-49667.63	0.00	0.01	49667.63	-0.00	0.000%
27	0.00	-49667.63	-6239.95	0.00	49667.63	6240.02	0.000%
28	3093.97	-49667.63	-5409.28	-3094.00	49667.63	5409.34	0.000%
29	5437.53	-49667.63	-3117.44	-5437.55	49667.63	3117.44	0.000%
30	6249.01	-49667.63	37.96	-6249.09	49667.63	-37.96	0.000%
31	5421.04	-49667.63	3123.82	-5421.06	49667.63	-3123.83	0.000%
32	3154.86	-49667.63	5380.62	-3154.90	49667.63	-5380.69	0.000%
33	0.00	-49667.63	6261.99	0.00	49667.63	-6262.06	0.000%
34	-3154.86	-49667.63	5380.62	3154.87	49667.63	-5380.63	0.000%
35	-5421.04	-49667.63	3123.82	5421.06	49667.63	-3123.83	0.000%
36	-6249.01	-49667.63	37.96	6249.09	49667.63	-37.96	0.000%
37	-5437.53	-49667.63	-3117.44	5437.60	49667.63	3117.47	0.000%
38	-3093.97	-49667.63	-5409.28	3093.97	49667.63	5409.29	0.000%
39	0.00	-18452.15	-5516.16	0.00	18452.15	5516.16	0.000%
40	2734.59	-18452.15	-4782.22	-2734.59	18452.15	4782.22	0.000%
41	4806.28	-18452.15	-2757.47	-4806.28	18452.15	2757.47	0.000%
42	5523.75	-18452.15	33.47	-5523.76	18452.15	-33.47	0.000%
43	4792.15	-18452.15	2760.88	-4792.15	18452.15	-2760.88	0.000%
44	2789.03	-18452.15	4755.52	-2789.03	18452.15	-4755.52	0.000%
45	0.00	-18452.15	5534.65	0.00	18452.15	-5534.65	0.000%
46	-2789.03	-18452.15	4755.52	2789.03	18452.15	-4755.52	0.000%
47	-4792.15	-18452.15	2760.88	4792.15	18452.15	-2760.88	0.000%
48	-5523.75	-18452.15	33.47	5523.76	18452.15	-33.47	0.000%
49	-4806.28	-18452.15	-2757.47	4806.28	18452.15	2757.47	0.000%
50	-2734.59	-18452.15	-4782.22	2734.59	18452.15	4782.22	0.000%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	5	0.00000001	0.00059212
3	Yes	5	0.00000001	0.00024931
4	Yes	6	0.00000001	0.00032631
5	Yes	6	0.00000001	0.00008792
6	Yes	6	0.00000001	0.00034873
7	Yes	6	0.00000001	0.00009433

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8	Yes	5	0.00000001	0.00049825
9	Yes	5	0.00000001	0.00020710
10	Yes	6	0.00000001	0.00036238
11	Yes	6	0.00000001	0.00009906
12	Yes	6	0.00000001	0.00032377
13	Yes	6	0.00000001	0.00008600
14	Yes	5	0.00000001	0.00031967
15	Yes	5	0.00000001	0.00013383
16	Yes	6	0.00000001	0.00034971
17	Yes	6	0.00000001	0.00009471
18	Yes	6	0.00000001	0.00034628
19	Yes	6	0.00000001	0.00009366
20	Yes	5	0.00000001	0.00064452
21	Yes	5	0.00000001	0.00026878
22	Yes	6	0.00000001	0.00031650
23	Yes	6	0.00000001	0.00008351
24	Yes	6	0.00000001	0.00036826
25	Yes	6	0.00000001	0.00010185
26	Yes	4	0.00000001	0.00008007
27	Yes	6	0.00000001	0.00052333
28	Yes	6	0.00000001	0.00095243
29	Yes	7	0.00000001	0.00018530
30	Yes	6	0.00000001	0.00051354
31	Yes	7	0.00000001	0.00018791
32	Yes	6	0.00000001	0.00097071
33	Yes	6	0.00000001	0.00051893
34	Yes	7	0.00000001	0.00018825
35	Yes	7	0.00000001	0.00018644
36	Yes	6	0.00000001	0.00052292
37	Yes	6	0.00000001	0.00097862
38	Yes	7	0.00000001	0.00018956
39	Yes	4	0.00000001	0.00075044
40	Yes	5	0.00000001	0.00009894
41	Yes	5	0.00000001	0.00011788
42	Yes	4	0.00000001	0.00045110
43	Yes	5	0.00000001	0.00013207
44	Yes	5	0.00000001	0.00010045
45	Yes	4	0.00000001	0.00042873
46	Yes	5	0.00000001	0.00011910
47	Yes	5	0.00000001	0.00011572
48	Yes	4	0.00000001	0.00062522
49	Yes	5	0.00000001	0.00009906
50	Yes	5	0.00000001	0.00013897

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	120 - 89.75	25.739	49	1.7244	0.0104
L2	92.42 - 70	15.950	49	1.6180	0.0068
L3	70 - 44.417	9.081	49	1.2453	0.0041
L4	48 - 35	4.231	49	0.8458	0.0023
L5	35 - 0	2.217	49	0.6031	0.0015

### Critical Deflections and Radius of Curvature - Service Wind

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Elevation	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
117.00	DB809K-XC	49	24.649	1.7236	0.0150	34948
110.00	2' Diameter Dish w/o Radome	49	22.114	1.7175	0.0135	17474
105.00	4' T-Arm (7' Face)	49	20.323	1.7050	0.0125	11649
90.00	(2) 4' T-Boom (7' Face)	49	15.139	1.5888	0.0093	5493
54.00	Pirod 4' Side Mount Standoff	49	5.373	0.9551	0.0037	3367

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	120 - 89.75	120.592	22	8.1036	0.0499
L2	92.42 - 70	74.819	22	7.6088	0.0328
L3	70 - 44.417	42.639	22	5.8577	0.0191
L4	48 - 35	19.879	22	3.9777	0.0107
L5	35 - 0	10.416	22	2.8358	0.0069

### Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
117.00	DB809K-XC	22	115.494	8.1007	0.0683	7774
110.00	2' Diameter Dish w/o Radome	22	103.647	8.0733	0.0616	3885
105.00	4' T-Arm (7' Face)	22	95.274	8.0159	0.0567	2588
90.00	(2) 4' T-Boom (7' Face)	22	71.023	7.4718	0.0423	1213
54.00	Pirod 4' Side Mount Standoff	22	25.241	4.4920	0.0168	725

### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> lb	φP <sub>n</sub> lb	Ratio P <sub>u</sub> /φP <sub>n</sub>
L1	120 - 89.75 (1)	TP21.287x16x0.188	30.25	0.00	0.0	12.3116	-3271.09	892475.00	0.004
L2	89.75 - 70 (2)	TP24.3628x20.4443x0.188	22.42	0.00	0.0	14.4254	-9919.00	995069.00	0.010
L3	70 - 44.417 (3)	TP28.8342x24.3628x0.275	25.58	0.00	0.0	24.3813	-12846.10	1804540.00	0.007
L4	44.417 - 35 (4)	TP29.93x27.6579x0.275	13.00	0.00	0.0	25.8844	-15065.60	1885590.00	0.008
L5	35 - 0 (5)	TP36.0472x29.93x0.364	35.00	0.00	0.0	41.2261	-22110.40	3062890.00	0.007

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### Pole Bending Design Data

Section No.	Elevation ft	Size	$M_{ux}$ lb-ft	$\phi M_{nx}$ lb-ft	Ratio $\frac{M_{ux}}{\phi M_{nx}}$	$M_{uy}$ lb-ft	$\phi M_{ny}$ lb-ft	Ratio $\frac{M_{uy}}{\phi M_{ny}}$
L1	120 - 89.75 (1)	TP21.287x16x0.188	106708.33	378179.17	0.282	0.00	378179.17	0.000
L2	89.75 - 70 (2)	TP24.3628x20.4443x0.188	407262.50	494703.33	0.823	0.00	494703.33	0.000
L3	70 - 44.417 (3)	TP28.8342x24.3628x0.275	788840.83	1034475.00	0.763	0.00	1034475.00	0.000
L4	44.417 - 35 (4)	TP29.93x27.6579x0.275	1055000.00	1148233.33	0.919	0.00	1148233.33	0.000
L5	35 - 0 (5)	TP36.0472x29.93x0.364	1885150.00	2242233.33	0.841	0.00	2242233.33	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual $V_u$ lb	$\phi V_n$ lb	Ratio $\frac{V_u}{\phi V_n}$	Actual $T_u$ lb-ft	$\phi T_n$ lb-ft	Ratio $\frac{T_u}{\phi T_n}$
L1	120 - 89.75 (1)	TP21.287x16x0.188	7261.62	446237.00	0.016	1942.83	758324.17	0.003
L2	89.75 - 70 (2)	TP24.3628x20.4443x0.188	15495.60	497535.00	0.031	2403.46	991783.33	0.002
L3	70 - 44.417 (3)	TP28.8342x24.3628x0.275	19426.40	902268.00	0.022	2974.29	2074550.00	0.001
L4	44.417 - 35 (4)	TP29.93x27.6579x0.275	21458.80	942795.00	0.023	3336.39	2302483.33	0.001
L5	35 - 0 (5)	TP36.0472x29.93x0.364	25925.20	1531450.00	0.017	3951.42	4496850.00	0.001

### Pole Interaction Design Data

Section No.	Elevation ft	Ratio $\frac{P_u}{\phi P_n}$	Ratio $\frac{M_{ux}}{\phi M_{nx}}$	Ratio $\frac{M_{uy}}{\phi M_{ny}}$	Ratio $\frac{V_u}{\phi V_n}$	Ratio $\frac{T_u}{\phi T_n}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	120 - 89.75 (1)	0.004	0.282	0.000	0.016	0.003	0.286	1.000	4.8.2 ✓
L2	89.75 - 70 (2)	0.010	0.823	0.000	0.031	0.002	0.834	1.000	4.8.2 ✓
L3	70 - 44.417 (3)	0.007	0.763	0.000	0.022	0.001	0.770	1.000	4.8.2 ✓
L4	44.417 - 35 (4)	0.008	0.919	0.000	0.023	0.001	0.927	1.000	4.8.2 ✓
L5	35 - 0 (5)	0.007	0.841	0.000	0.017	0.001	0.848	1.000	4.8.2 ✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	$\phi P_{allow}$ lb	% Capacity	Pass Fail
L1	120 - 89.75	Pole	TP21.287x16x0.188	1	-3271.09	892475.00	28.6	Pass
L2	89.75 - 70	Pole	TP24.3628x20.4443x0.188	2	-9919.00	995069.00	83.4	Pass



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Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	$\phi P_{allow}$ lb	% Capacity	Pass Fail	
L3	70 - 44.417	Pole	TP28.8342x24.3628x0.275	3	-12846.10	1804540.00	77.0	Pass	
L4	44.417 - 35	Pole	TP29.93x27.6579x0.275	4	-15065.60	1885590.00	92.7	Pass	
L5	35 - 0	Pole	TP36.0472x29.93x0.364	5	-22110.40	3062890.00	84.8	Pass	
							Summary		
							Pole (L4)	92.7	Pass
							<b>RATING =</b>	<b>92.7</b>	<b>Pass</b>

**(Hartford 9 CT) - Anchor Bolt & Base Plate**

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 -TIA 222 Rev G

Site Name: Hartford 9 CT

**Monopole Anchor Bolt & Base Plate Check**

	LRFD Loads	
Global Axial Force (1.2DL), $P_L$ =	22.1 kips	(TNX Tower MTO)
Global Shear Force (1.6WL), $S_L$ =	25.9 kips	(TNX Tower MTO)
Global Moment (1.6WL), $M_L$ =	1885.1 kip-ft	(TNX Tower MTO)

**Existing Anchor Bolt Data:**

Number of Anchor Bolts, $N$ =	6
Diameter of Bolt Circle, $d_{bc}$ =	41.50 in
Bolt "Column" Distance, $l$ =	3.50 in
Bolt Ultimate Strength, $F_u$ =	100 ksi
Bolt Yield Strength, $F_y$ =	75 ksi
Bolt Modulus of Elasticity, $E$ =	29000 ksi
Diameter of Anchor Bolt Circle, $d_{ab}$ =	2.25 in
Threads per Inch, $n$ =	4.5
Top of Concrete to Bolt Leveling Nut, $l_{ar}$ =	2.00 in

**Reinforcement Anchor Bolt Data:**

Number of Anchor Bolts, $N_o$ =	6
Diameter of Bolt Circle, $d_{bco}$ =	50.38 in
Bolt "Column" Distance, $l_o$ =	3.00 in
Bolt Ultimate Strength, $F_{uo}$ =	100 ksi
Bolt Yield Strength, $F_{yo}$ =	75 ksi
Bolt Modulus of Elasticity, $E_o$ =	29000 ksi
Diameter of Anchor Bolt Circle, $d_{abo}$ =	2.75 in
Threads per Inch, $n_o$ =	4

**Base Plate Data:**

Plate Yield Strength, $F_{ybp}$ =	50 ksi	Base Plate Diameter, $d_{bp}$ =	47.50 in
Base Plate Thickness, $t_{bp}$ =	2.25 in	Monopole Outside Diameter, $d_{mp}$ =	36.00 in
$\gamma$ =	0.5	per TIA-222-G Section 4.9.9 (detail type d)	

**Geometry:**

**Distance from Bolts to Centroid of Monopole:**

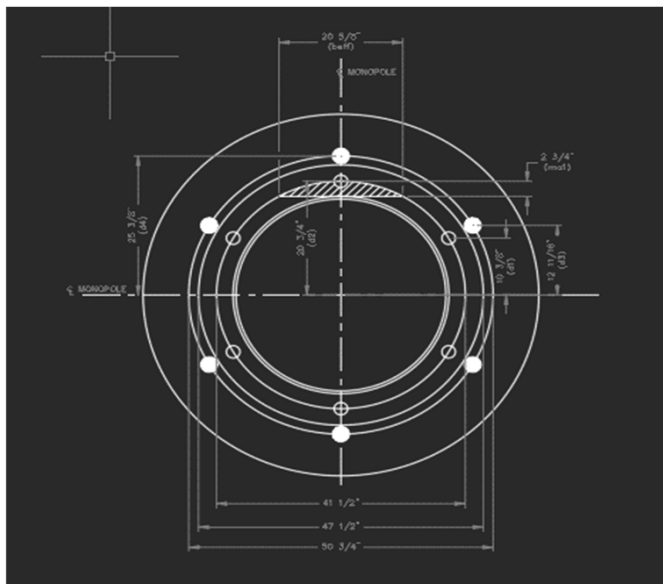
$d_1$ =	10.38 in
$d_2$ =	20.75 in
$d_3$ =	12.69 in
$d_4$ =	25.38 in

**Critical Distances for Bending in Plate:**

$m_{a1}$ =	2.75 in
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**Effective Width of Base Plate (Bending):**

$b_{eff}$ =	20.63 in
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**Analysis of Inner Anchor Bolts:**

$$\begin{aligned} \text{Total Polar Moment of Inertia, } I_p &= d_1^2 * 4 + d_2^2 * 2 + d_3^2 * 4 + d_4^2 * 2 \\ &= 3224.54 \text{ in}^2 \\ \text{Gross Area of Inner Bolts, } A_{gi} &= \pi / 4 * d_{ab}^2 \\ &= 3.98 \text{ in}^2 \\ \text{Net Area of Inner Bolts, } A_{ni} &= \pi / 4 * (d_{ab} - 0.9743 / n)^2 \quad \text{per TIA-222-G Section 4.9.9 (detail type d)} \\ &= 3.25 \text{ in}^2 \\ \text{Net Diameter of Inner Bolts, } d_{ni} &= 2 * \sqrt{A_{ni} / \pi} \\ &= 2.03 \text{ in} \\ \text{Radius of Gyration of Inner Bolts, } r_i &= d_{ni} / 4 \\ &= 0.51 \text{ in} \\ \text{Section Modulus of Inner Bolts, } S_{xi} &= \pi * d_{ni}^3 / 32 \\ &= 0.83 \text{ in}^3 \\ \text{Plastic Modulus of Inner Bolts, } Z_{xi} &= d_{ni}^3 / 6 \\ &= 1.40 \text{ in}^3 \end{aligned}$$

**Anchor Bolt Tension Force Check:**

$$\begin{aligned} \text{Maximum Tensile Force, } T_{MAX} &= M_L * d_2 / l_p - P_L / N \\ &= 141.9 \text{ kips} \\ \text{Maximum Compressive Force, } P_u &= M_L * d_2 / l_p + P_L / N \\ &= 149.3 \text{ kips} \\ \text{Maximum Shear Force, } V_u &= S_L / N \\ &= 4.3 \text{ kips} \end{aligned}$$

**Tensile Check:**

$$\begin{aligned} \text{Design Tensile Strength, } \phi R_{nt} &= 0.75 * F_u * A_{ni} \\ &= 243.6 \text{ kips} \\ \text{Tensile Capacity of Bolt} &= (P_u + V_u / \eta) / \phi R_{nt} \\ &= 64.8\% \leq 100\% \quad \text{OK!} \end{aligned}$$

**Shear Check:**

$$\begin{aligned} \text{Design Shear Strength, } \phi R_{nv} &= 0.75 * 0.45 * F_u * A_{gi} \\ &= 134.2 \text{ kips} \\ \text{Shear Capacity of Bolt} &= V_u / \phi R_{nv} \\ &= 3.2\% \leq 100\% \quad \text{OK!} \end{aligned}$$

**Flexure Check:**

$$\begin{aligned} \text{Design Flexure Strength, } \phi R_{nm} &= 0.9 * F_y * Z_{xi} \\ &= 94.6 \text{ kip-ft} \\ M_u &= \text{if } l_{ar} < d_{ab}, 0; \text{ otherwise, } 0.65 * l_{ar} * V_u \\ &= 0.0 \text{ kip-ft} \\ \text{Flexure Capacity of Bolt} &= M_u / \phi R_{nm} \\ &= 0.0\% \leq 100\% \quad \text{OK!} \end{aligned}$$

**Combined Check:**

$$\begin{aligned} \text{Capacity of Bolt} &= (V_u / \phi R_{nv})^2 + (P_u / \phi R_{nt} + M_u / \phi R_{nm})^2 \\ &= 37.6\% \leq 100\% \quad \text{OK!} \end{aligned}$$

**Analysis of Outer Anchor Bolts:**

$$\begin{aligned} \text{Total Polar Moment of Inertia, } I_p &= d_1^2 * 4 + d_2^2 * 2 + d_3^2 * 4 + d_4^2 * 2 \\ &= 3224.54 \text{ in}^2 \\ \text{Gross Area of Outer Bolts, } A_{go} &= \pi / 4 * d_{abo}^2 \\ &= 5.94 \text{ in}^2 \\ \text{Net Area of Outer Bolts, } A_{no} &= \pi / 4 * (d_{abo} - 0.9743 / n_o)^2 \quad \text{per TIA-222-G Section 4.9.9 (detail type d)} \\ &= 4.93 \text{ in}^2 \\ \text{Net Diameter of Outer Bolts, } d_{no} &= 2 * \sqrt{A_{no} / \sqrt{\pi}} \\ &= 2.51 \text{ in} \\ \text{Radius of Gyration of Outer Bolts, } r_o &= d_{no} / 4 \\ &= 0.63 \text{ in} \\ \text{Section Modulus of Outer Bolts, } S_{xo} &= \pi * d_{no}^3 / 32 \\ &= 1.55 \text{ in}^3 \\ \text{Plastic Modulus of Outer Bolts, } Z_{xo} &= d_{no}^3 / 6 \\ &= 2.62 \text{ in}^3 \end{aligned}$$

**Anchor Bolt Tension Force Check:**

$$\begin{aligned} \text{Maximum Tensile Force, } T_{MAX} &= M_L * d_4 / l_p - P_L / N_o \\ &= 174.4 \text{ kips} \\ \text{Maximum Compressive Force, } P_u &= M_L * d_4 / l_p + P_L / N_o \\ &= 181.7 \text{ kips} \\ \text{Maximum Shear Force, } V_u &= S_L / N_o \\ &= 4.3 \text{ kips} \end{aligned}$$

**Tensile Check:**

$$\begin{aligned} \text{Design Tensile Strength, } \phi R_{nt} &= 0.8 * F_{uo} * A_{no} \\ &= 394.7 \text{ kips} \\ \text{Tensile Capacity of Bolt} &= (P_u + V_u / \eta) / \phi R_{nt} \\ &= 48.2\% \leq 100\% \quad \text{OK!} \end{aligned}$$

**Shear Check:**

$$\begin{aligned} \text{Design Shear Strength, } \phi R_{nv} &= 0.75 * 0.45 * F_{uo} * A_{go} \\ &= 200.5 \text{ kips} \\ \text{Shear Capacity of Bolt} &= V_u / \phi R_{nv} \\ &= 2.2\% \leq 100\% \quad \text{OK!} \end{aligned}$$

**Flexure Check:**

$$\begin{aligned} \text{Design Flexure Strength, } \phi R_{nm} &= 0.9 * F_{yo} * Z_{xo} \\ &= 177.1 \text{ kip-ft} \\ M_u &= \text{if } l_{ar} < d_{abo}, 0; \text{ otherwise, } 0.65 * l_{ar} * V_u \\ &= 0.0 \text{ kip-ft} \\ \text{Flexure Capacity of Bolt} &= M_u / \phi R_{nm} \\ &= 0.0\% \leq 100\% \quad \text{OK!} \end{aligned}$$

**Combined Check:**

$$\begin{aligned} \text{Capacity of Bolt} &= (V_u / \phi R_{nv})^2 + (P_u / \phi R_{nt} + M_u / \phi R_{nm})^2 \\ &= 21.2\% \quad \text{OK!} \end{aligned}$$

**Base Plate Analysis:**

$$\begin{aligned} \text{Force from Bolts, } C_1 &= M_L * d_2 / l_p + P_L / N_o \\ &= 149.3 \text{ kips} \\ \text{Applied Bending Stress in Plate, } f_{bp} &= 4 * C_1 * m_{a1} / (b_{eff} + t_{bp}^2) \\ &= 15.7 \text{ ksi} \\ \text{Allowable Bending Stress in Plate, } F_{bp} &= 0.9 * F_{ybp} \\ &= 45.0 \text{ ksi} \\ \text{Capacity of Base Plate} &= f_{bp} / F_{bp} \\ &= 34.9\% \leq 100\% \quad \text{OK!} \end{aligned}$$

**(Hartford 9 CT) - Foundation**

\\capecod\projects\50121487\50121823 - Hartford 9 CT\Engineering\Structural\Rev 0\Calcs\50110171 - Monopole Anchor Bolts, Base Plate and Foundation Check.xlsx  
 -TIA 222 Rev G

Site Name: Hartford 9 CT

**Monopole Foundation Check**

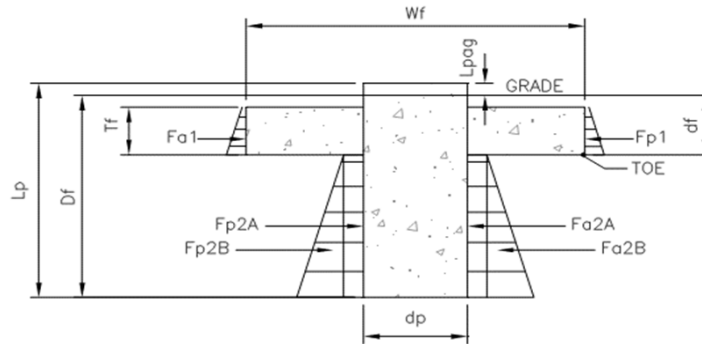
	LRFD Loads	
Global Axial Force (1.2DL), $P_L$ =	22.1 kips	(TNX Tower MTO)
Global Shear Force (1.6WL), $S_L$ =	25.9 kips	(TNX Tower MTO)
Global Moment (1.6WL), $M_L$ =	1885.1 kip-ft	(TNX Tower MTO)

**Tower & Monopole Data:**

Monopole Height, $H_t$ =	120.00 ft	Footing Thickness, $T_f$ =	2.00 ft
Depth of Footing, $D_f$ =	19.00 ft	Footing Width, $W_f$ =	14.50 ft
Pier Length, $L_p$ =	19.50 ft	Water Depth, $d_{water}$ =	0.00 ft
Pier Extension Above Grade, $L_{pag}$ =	0.50 ft	Distance from Grade to Bottom of Pad, $d_f$ =	4.00 ft
Cassion Diameter, $d_p$ =	5.50 ft		

**Material Properties:**

Unit Weight of Concrete, $\gamma_c$ =	150 psf	Internal Friction Angle of Soil, $\phi_{s1}$ =	33 °	(mat)
Unit Weight of Soil, $\gamma_{s1}$ =	120 psf	Internal Friction Angle of Soil, $\phi_{s2}$ =	33 °	(below mat)
Unit Weight of Soil, $\gamma_{s2}$ =	58 psf	Ultimate Soil Bearing Capacity, $q_s$ =	8000 psf	
Concrete Compressive Strength, $f_c$ =	3000 psi	Depth to Neglect Foundation Bouyancy, $n$ =	0.00 ft	(if applicable)
Steel Reinforcement Yield Strength, $f_y$ =	60000 psi	Cohesion of Clay Type Soil, $c$ =	0 ksf	(0 for Sandy Soil)
Anchor Bolt Yield Strength, $f_{ya}$ =	75000 psi	Seismic Zone Factor, $z$ =	2	(UBC-1997, Fig. 23-2)



**Coefficient of Lateral Soil Factors:**

$$\begin{aligned}
 k_{p1} &= (1 + \sin(\phi_{s1}) / (1 - \sin(\phi_{s1})) \\
 &= 3.39 \\
 k_{p2} &= (1 + \sin(\phi_{s2}) / (1 - \sin(\phi_{s2})) \\
 &= 3.39
 \end{aligned}$$

$$\begin{aligned}
 k_{a1} &= (1 - \sin(\phi_{s1}) / (1 + \sin(\phi_{s1})) \\
 &= 0.29 \\
 k_{a2} &= (1 - \sin(\phi_{s2}) / (1 + \sin(\phi_{s2})) \\
 &= 0.29
 \end{aligned}$$

**Footing Stability Check:**

$$\begin{aligned} \text{Passive Pressure 1, } P_{p1top} &= k_{p1} * \gamma_{s1} * (d_f - T_f) \\ &= 0.814 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Passive Pressure 1, } P_{p1ave} &= (P_{p1top} + P_{p1bot}) / 2 \\ &= 1.221 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Active Pressure 1, } P_{a1top} &= k_{a1} * \gamma_{s1} * (d_f - T_f) \\ &= 0.071 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Active Pressure 1, } P_{a1ave} &= (P_{a1top} + P_{a1bot}) / 2 \\ &= 0.106 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Area of Pressure 1, } A_{p1} &= T_f * W_f \\ &= 29.0 \text{ ft}^2 \end{aligned}$$

$$\begin{aligned} \text{Passive Force 1, } F_{p1} &= P_{p1ave} * A_{p1} \\ &= 35.4 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Ultimate Shear 1, } S_{u1} &= F_{p1} - F_{a1} \\ &= 32.3 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Passive Pressure 2, } P_{p2top} &= k_{p2} * \gamma_{s2} * d_f \\ &= 0.787 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Active Pressure 2, } P_{a2top} &= k_{a2} * \gamma_{s2} * d_f \\ &= 0.068 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Area of Pressure 2, } A_{p2} &= (D_f - d_f) * d_p \\ &= 82.5 \text{ ft}^2 \end{aligned}$$

$$\begin{aligned} \text{Passive Force 2, } F_{p2T} &= P_{p2top} * A_{p2} \\ &= 64.9 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Active Force 2, } F_{a2T} &= P_{a2top} * A_{p2} \\ &= 5.6 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Ultimate Shear 2, } S_{u2T} &= F_{p2T} - F_{a2T} \\ &= 59.3 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Concrete Mat Weight, } W_{mat} &= (W_f^2 - d_p^2 * \pi / 4) * T_f * \gamma_c \\ &= 55.9 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Soil Above Mat Weight, } W_{s1} &= (W_f^2 - d_p^2 * \pi / 4) * (d_f - T_f) * \gamma_{s1} \\ &= 44.8 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Total Weight, } W_{tot} &= 0.9 * (W_{mat} + W_{cas} + P_L) + 0.75W_{s1} \\ &= 166.4 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Overturning Moment, } M_{ot} &= M_L + S_L * (d_f + L_{pag}) \\ &= 2001.7 \text{ kip-ft} \end{aligned}$$

$$\begin{aligned} \text{Resisting Moment, } M_r &= W_{tot} * W_f / 2 + 0.75 * (S_{u1} * T_f / 3 + S_{u2T} * (D_f - d_f) / 2 + S_{u2B} * 2 * (D_f - d_f) / 3) \\ &= 2389.4 \text{ kip-ft} \end{aligned}$$

$$\begin{aligned} \text{Factor of Safety, } FS &= M_r / M_{ot} \\ &= 1.19 > 1.00 \end{aligned}$$

$$\begin{aligned} \text{Passive Pressure 1, } P_{p1bot} &= k_{p1} * \gamma_{s1} * d_f \\ &= 1.628 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Active Pressure 1, } P_{a1bot} &= k_{a1} * \gamma_{s1} * d_f \\ &= 0.142 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Active Force 1, } F_{a1} &= P_{a1ave} * A_{p1} \\ &= 3.1 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Passive Pressure 2, } P_{p2bot} &= k_{p2} * \gamma_{s2} * D_f \\ &= 3.738 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Active Pressure 2, } P_{a2bot} &= k_{a2} * \gamma_{s2} * D_f \\ &= 0.325 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Passive Force 2, } F_{p2B} &= 0.5 * (P_{p2bot} - P_{p2top}) * A_{p2} \\ &= 121.7 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Active Force 2, } F_{a2B} &= 0.5 * (P_{a2bot} - P_{a2top}) * A_{p2} \\ &= 10.6 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Ultimate Shear 2, } S_{u2B} &= F_{p2B} - F_{a2B} \\ &= 111.2 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Concrete Cassion Weight, } W_{cas} &= (d_p^2 * \pi / 4) * L_p * \gamma_c \\ &= 69.5 \text{ kips} \end{aligned}$$

**Footing Stability Check:**

$$\begin{aligned} \text{Area of Mat, } A_{mat} &= W_f^2 - d_p^2 * \pi / 4 \\ &= 186.5 \text{ ft}^2 \end{aligned}$$

$$\begin{aligned} \text{Axial Force, } P_{mat} &= W_{mat} + W_{s1} \\ &= 100.7 \text{ kips} \end{aligned}$$

$$\begin{aligned} \text{Cassion Resisting Moment Capacity, } M_{cap} &= S_{u2T} * (D_f - d_f) / 2 + S_{u2B} * 2 * (D_f - d_f) / 3 \\ &= 1556.2 \text{ kip-ft} \end{aligned}$$

$$\begin{aligned} \text{Matt Residual Moment Capacity, } M_{mat} &= (M_L - M_{cap}) + S_L * (d_f + L_{pag}) \geq 0 \\ &= 445.5 \text{ kip-ft} \end{aligned}$$

$$\begin{aligned} \text{Maximum Matt Pressure, } p_{MAX} &= P_{mat} / A_{mat} + M_{mat} / S_{mat} \\ &= 1.446 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Minimum Matt Pressure, } p_{MIN} &= P_{mat} / A_{mat} - M_{mat} / S_{mat} \\ &= -0.366 \text{ ksf} \end{aligned}$$

$$\begin{aligned} \text{Section Modulus of Mat, } S_{mat} &= W_f^3 / 6 - d_p^3 * \pi / 32 \\ &= 491.8 \text{ ft}^3 \end{aligned}$$

$$\begin{aligned} &\leq 0.75q_s \\ &\leq 6.000 \text{ ksf} \end{aligned} \quad \text{OK!}$$

$$\begin{aligned} &\leq 0.75q_s \\ &\leq 6.000 \text{ ksf} \end{aligned} \quad \text{OK!}$$

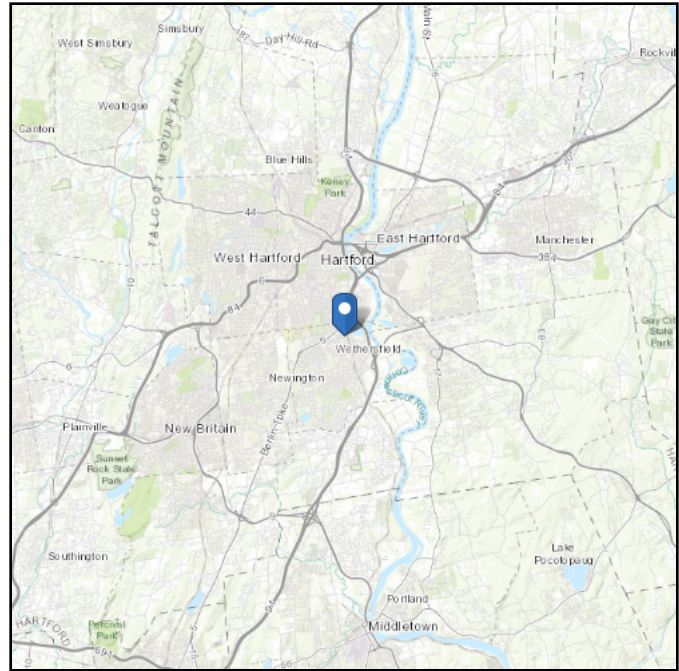
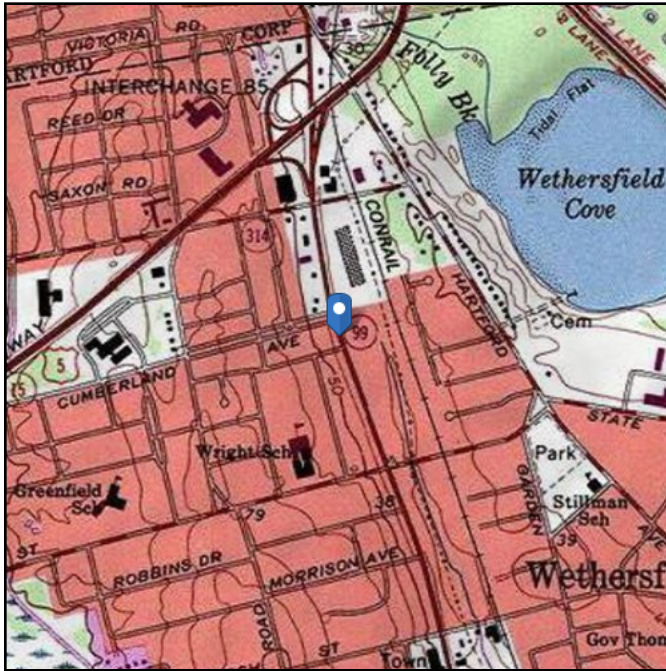
**APPENDIX B**  
**REFERENCE MATERIAL**

# ASCE 7 Hazards Report

**Address:**  
250 Silas Deane Hwy  
Wethersfield, Connecticut  
06109

**Standard:** ASCE/SEI 7-10  
**Risk Category:** II  
**Soil Class:**

**Elevation:** 36.77 ft (NAVD 88)  
**Latitude:** 41.720291  
**Longitude:** -72.667228



## Ice

### Results:

Ice Thickness: 1.00 in.  
Concurrent Temperature: 5 F  
Gust Speed: 50 mph

**Data Source:** Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8

**Date Accessed:** Mon Jul 29 2019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.



The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided “as is” and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.



NORTHEAST > North East > New England > New England West > **HARTFORD 9 CT**

Brauer, Mark - mark.brauer2@verizonwireless.com - 10/8/2020 10:30:18

### Project Details

<b>Carrier Aggregation:</b> false
<b>MPT Id:</b>
<b>eCIP-0:</b> false
<b>Project Name:</b> 5G L-Sub6 - Carrier Add
<b>FUZE Project ID:</b> 16232035
<b>Designed Sector Carrier 4G:</b> 13
<b>Designed Sector Carrier 5G:</b> N/A
<b>Additional Sector Carrier 4G:</b> N/A
<b>Additional Sector Carrier 5G:</b> N/A
<b>SiteTraker Project Id:</b>
<b>FP Solution Type &amp; Tech Type: ;</b>
<b>RFDS Project Scope:</b> Sub 6 add Update 10/08/2020 per Andrew Leone: Added: (2) 6-OVP (2) LI 6x12 Hybrid cables Removed: (1) 6-OVP (1) 6x12 hybrid cable
<b>Suffix:</b>

### Location Information

<b>Site ID:</b> 674932
<b>E-NodeB ID:</b> 068620
<b>PSLC:</b> 468180
<b>Switch Name:</b> Windsor 1
<b>Tower Owner:</b>
<b>Tower Type:</b> Monopole
<b>Site Type:</b> MACRO
<b>Street Address:</b> 250 Silas Deane Highway
<b>City:</b> Wethersfield
<b>State:</b> CT
<b>Zip Code:</b> 06109
<b>County:</b> Hartford
<b>Latitude:</b> 41.720597 / 41° 43' 14.1492" N
<b>Longitude:</b> -72.666044 / 72° 39' 57.7584" W

## Antenna Summary

<b>Added</b>																			
700	850	1900	AWS	AWS3	28 GHz	31 GHz	39 GHz	CBRS	LAA	L-Sub6	Make	Model	Centerline	Tip Height	Azimuth	RET	4xRx	Inst. Type	Quantity
											TBD	nL-Sub6 Antenna	90	93	30(0001) 180(0002) 300(0003)	false	false	PHYSICAL	3
<b>Removed</b>																			
700	850	1900	AWS	AWS3	28 GHz	31 GHz	39 GHz	CBRS	LAA	L-Sub6	Make	Model	Centerline	Tip Height	Azimuth	RET	4xRx	Inst. Type	Quantity
											Antel	BXA-80063/6CF	90	93	30(D1) 180(D2) 300(D3)	false	false	PHYSICAL	3
<b>Retained</b>																			
700	850	1900	AWS	AWS3	28 GHz	31 GHz	39 GHz	CBRS	LAA	L-Sub6	Make	Model	Centerline	Tip Height	Azimuth	RET	4xRx	Inst. Type	Quantity
LTE	LTE	LTE	LTE								ANDREW	SBNHH-1D65B	90	93	30(D1) 180(D2) 300(D3)	true	true	PHYSICAL	3
	CDMA										ANTEL	BXA-80063/6CF (181901)	90	93	30(D1) 180(D2) 300(D3)	false	false	PHYSICAL	3

Added: 3
Removed: 3
Retained: 6

## Equipment Summary

<b>Added</b>																		
Equipment Type	Location	700	850	1900	AWS	AWS3	28 GHz	31 GHz	39 GHz	CBRS	LAA	L-Sub6	Make	Model	Cable Length	Cable Size	Install Type	Quantity
RRU	Tower												Samsung	VZS01			PHYSICAL	3
Hybrid Cable	Tower													6x12 LI			PHYSICAL	2
OVP Box	Tower													OVP-6			PHYSICAL	2
<b>Removed</b>																		
Equipment Type	Location	700	850	1900	AWS	AWS3	28 GHz	31 GHz	39 GHz	CBRS	LAA	L-Sub6	Make	Model	Cable Length	Cable Size	Install Type	Quantity
Hybrid Cable	Tower													6x12			PHYSICAL	1
OVP Box	Tower													OVP-6			PHYSICAL	1
<b>Retained</b>																		
Equipment Type	Location	700	850	1900	AWS	AWS3	28 GHz	31 GHz	39 GHz	CBRS	LAA	L-Sub6	Make	Model	Cable Length	Cable Size	Install Type	Quantity
RRU	Tower			LTE	LTE								Samsung	B2/B66A RRH-BR049 (RFV01U-D1A)			PHYSICAL	3
RRU	Tower	LTE	LTE										Samsung	B5/B13 RRH-BR04C (RFV01U-D2A)			PHYSICAL	3
Coaxial Cables	Tower																PHYSICAL	6

## Service Info

1900 MHZ LTE				5GLS		
	0000			5GLS		
Sector	D1	D2	D3	D1	D2	D3
Azimuth	30	180	300	30	180	300
Cell / ENode B ID	068620	068620	068620	068620	068620	068620
Antenna Model	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B
Antenna Make	ANDREW	ANDREW	ANDREW	ANDREW	ANDREW	ANDREW
Antenna Centerline(Ft)	90	90	90	90	90	90
Mechanical Down-Tilt(Deg.)	0	0	0	0	0	0
Electrical Down-Tilt	2	2	1	2	2	1
Tip Height	93	93	93	93	93	93
Regulatory Power	290.31	290.31	289.24	290.31	290.31	289.24
TMA Make						
TMA Model						
RRU Make	Samsung	Samsung	Samsung	Samsung	Samsung	Samsung
RRU Model	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)
Number of Tx, Rx Lines	4,4	4,4	4,4	4,4	4,4	4,4
Position						
Transmitter Id	3431029	3431030	3431031	7476631	7476632	7476633
Source	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API
2100 MHZ LTE				5GLS		
	0000			5GLS		
Sector	D1	D2	D3	D1	D2	D3
Azimuth	30	180	300	30	180	300
Cell / ENode B ID	068620	068620	068620	068620	068620	068620
Antenna Model	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B
Antenna Make	ANDREW	ANDREW	ANDREW	ANDREW	ANDREW	ANDREW
Antenna Centerline(Ft)	90	90	90	90	90	90
Mechanical Down-Tilt(Deg.)	0	0	0	0	0	0
Electrical Down-Tilt	2	2	1	2	2	1
Tip Height	93	93	93	93	93	93
Regulatory Power	142.44	142.44	143.23	142.44	142.44	143.23
TMA Make						
TMA Model						
RRU Make	Samsung	Samsung	Samsung	Samsung	Samsung	Samsung
RRU Model	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)	B2/B66A RRH-BR049 (RFV01U-D1A)
Number of Tx, Rx Lines	4,4	4,4	4,4	4,4	4,4	4,4
Position						
Transmitter Id	3430965	3430967	3430969	7476626	7476628	7476630
Source	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API
850 MHZ CDMA				5GLS		
	0000			5GLS		
Sector	D1	D2	D3	D1	D2	D3
Azimuth	30	180	300	30	180	300
Cell / ENode B ID						
Antenna Model	BXA-80063/6CF (181901)	BXA-80063/6CF (181901)	BXA-80063/6CF (181901)	BXA-80063/6CF (181901)	BXA-80063/6CF (181901)	BXA-80063/6CF (181901)
Antenna Make	ANTEL	ANTEL	ANTEL	ANTEL	ANTEL	ANTEL
Antenna Centerline(Ft)	90	90	90	90	90	90
Mechanical Down-Tilt(Deg.)	3	0	3	3	0	3
Electrical Down-Tilt	0	0	0	0	0	0
Tip Height	93	93	93	93	93	93
Regulatory Power	497.74	497.74	497.74	497.74	497.74	497.74
TMA Make						
TMA Model						
RRU Make						
RRU Model						
Number of Tx, Rx Lines						
Position						
Transmitter Id						
Source	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API

850 MHZ LTE				5GLS					
	0000			5GLS					
Sector	D1	D2	D3	D1	D2	D3			
Azimuth	30	180	300	30	180	300			
Cell / ENode B ID	068620	068620	068620	068620	068620	068620			
Antenna Model	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B			
Antenna Make	ANDREW	ANDREW	ANDREW	ANDREW	ANDREW	ANDREW			
Antenna Centerline(Ft)	90	90	90	90	90	90			
Mechanical Down-Tilt(Deg.)	0	0	0	0	0	0			
Electrical Down-Tilt	5	3	3	5	3	3			
Tip Height	93	93	93	93	93	93			
Regulatory Power	329.75	328.54	328.54	328.97	327.76	327.76			
TMA Make									
TMA Model									
RRU Make	Samsung	Samsung	Samsung	Samsung	Samsung	Samsung			
RRU Model	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)			
Number of Tx, Rx Lines	4,4	4,4	4,4	4,4	4,4	4,4			
Position									
Transmitter Id	3431032	3431033	3431034	7476634	7476635	7476636			
Source	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API			
700 MHZ LTE				5GLS					
	0000			5GLS					
Sector	D1	D2	D3	D1	D2	D3			
Azimuth	30	180	300	30	180	300			
Cell / ENode B ID	068620	068620	068620	068620	068620	068620			
Antenna Model	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B	SBNHH-1D65B			
Antenna Make	ANDREW	ANDREW	ANDREW	ANDREW	ANDREW	ANDREW			
Antenna Centerline(Ft)	90	90	90	90	90	90			
Mechanical Down-Tilt(Deg.)	0	0	0	0	0	0			
Electrical Down-Tilt	5	3	3	5	3	3			
Tip Height	93	93	93	93	93	93			
Regulatory Power	77.44	76.99	76.99	77.44	76.99	76.99			
TMA Make									
TMA Model									
RRU Make	Samsung	Samsung	Samsung	Samsung	Samsung	Samsung			
RRU Model	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)	B5/B13 RRH-BR04C (RFV01U-D2A)			
Number of Tx, Rx Lines	4,4	4,4	4,4	4,4	4,4	4,4			
Position									
Transmitter Id	3430964	3430966	3430968	7476625	7476627	7476629			
Source	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API	ATOLL_API			
nL-Sub6				5GLS					
Sector	0001			0002			0003		
Azimuth	30			180			300		
Cell / ENode B ID	0068620			0068620			0068620		
Antenna Model	nL-Sub6 Antenna			nL-Sub6 Antenna			nL-Sub6 Antenna		
Antenna Make	TBD			TBD			TBD		
Antenna Centerline(Ft)	90			90			90		
Mechanical Down-Tilt(Deg.)	0			0			0		
Electrical Down-Tilt	3			3			3		
Tip Height	93			93			93		
Regulatory Power	142.44			142.44			143.23		
TMA Make									
TMA Model									
RRU Make	Samsung			Samsung			Samsung		
RRU Model	VZS01			VZS01			VZS01		
Number of Tx, Rx Lines	4,4			4,4			4,4		
Position									
Transmitter Id	7476685			7476686			7476687		
Source	ATOLL_API			ATOLL_API			ATOLL_API		

Service Comments

### Callsigns Per Antenna

Sector	Antenna Make	Antenna Mode	Ant CL Height AGL	Tip Height	Azimuth (TN)	Electrical Tilt	Mechanical Tilt	Gain	Beamwidth	Regulatory Power	Callsigns						
											700	850	1900	2100	28 GHz	31 GHz	39 GHz
D1	ANDREW	SBNHH-1D65B	90	93	30	2	0	16.139	61.5	142.44				WQGA906 WQGB276			
D3	ANTEL	BXA-80063/6CF (181901)	90	93	300	0	3	14.5	61.25	368.13		KNKA404					
D2	ANDREW	SBNHH-1D65B	90	93	180	2	0	16.221001	53	290.31			KNLH251 WPOJ730				
D1	ANDREW	SBNHH-1D65B	90	93	30	5	0	12.632	69.25	77.44	WQJQ689						
D2	ANDREW	SBNHH-1D65B	90	93	180	3	0	12.607	69	76.99	WQJQ689						
D3	ANDREW	SBNHH-1D65B	90	93	300	3	0	13.335	66	327.76		KNKA404					
D3	ANDREW	SBNHH-1D65B	90	93	300	1	0	16.163	61	143.23				WQGA906 WQGB276			
D3	ANDREW	SBNHH-1D65B	90	93	300	3	0	12.607	69	76.99	WQJQ689						
D2	ANDREW	SBNHH-1D65B	90	93	180	2	0	16.139	61.5	142.44				WQGA906 WQGB276			
D2	ANTEL	BXA-80063/6CF (181901)	90	93	180	0	0	14.5	61.25	368.13		KNKA404					
D1	ANDREW	SBNHH-1D65B	90	93	30	5	0	13.351	64.5	328.97		KNKA404					
D3	ANDREW	SBNHH-1D65B	90	93	300	1	0	16.205	52.75	289.24			KNLH251 WPOJ730				
D2	ANTEL	BXA-80063/6CF (181901)	90	93	180	0	0	14.5	61.25	497.74		KNKA404					
D1	ANDREW	SBNHH-1D65B	90	93	30	2	0	16.221001	53	290.31			KNLH251 WPOJ730				
D1	ANTEL	BXA-80063/6CF (181901)	90	93	30	0	3	14.5	61.25	368.13		KNKA404					
D1	ANTEL	BXA-80063/6CF (181901)	90	93	30	0	3	14.5	61.25	497.74		KNKA404					
D3	ANTEL	BXA-80063/6CF (181901)	90	93	300	0	3	14.5	61.25	497.74		KNKA404					
D2	ANDREW	SBNHH-1D65B	90	93	180	3	0	13.335	66	327.76		KNKA404					

## Callsigns

Callsign	Market	Radio Code	Market Number	Block	State	County	Licensee Name	Wholly Owned	Total MHZ	Freq Range 1	Freq Range 2	Freq Range 3	Freq Range 4	Regulatory Power	Threshold (W)	POPs/Sq Mi	Status	Action	Approved for Insvc
WQJQ689	Northeast	WU	REA001	C	CT	Hartford	Cellco Partnership	Yes	22.000	746.000-757.000	776.000-787.000	.000-.000	.000-.000	77.44	1000	1216.19	Active	retained	Yes
KNKA404	Hartford-New Britain-Bristol, CT	CL	CMA032	A	CT	Hartford	Cellco Partnership	Yes	25.000	824.000-835.000	869.000-880.000	845.000-846.500	890.000-891.500	497.74	500	1216.19	Active	added	Yes
WPOJ730	Hartford, CT	CW	BTA184	C	CT	Hartford	Cellco Partnership	Yes	15.000	1895.000-1902.500	1975.000-1982.500	.000-.000	.000-.000	290.31	1640	1216.19	Active	retained	Yes
KNLH251	Hartford, CT	CW	BTA184	F	CT	Hartford	Cellco Partnership	Yes	10.000	1890.000-1895.000	1970.000-1975.000	.000-.000	.000-.000	290.31	1640	1216.19	Active	retained	Yes
WQGB276	Hartford-New Britain-Bristol, CT	AW	CMA032	A	CT	Hartford	Cellco Partnership	Yes	20.000	1710.000-1720.000	2110.000-2120.000	.000-.000	.000-.000	143.23	1640	1216.19	Active	retained	Yes
WQGA906	New York-No. New Jer.-Long Island, NY-NJ-CT-PA-MA-	AW	BEA010	B	CT	Hartford	Cellco Partnership	Yes	20.000	1720.000-1730.000	2120.000-2130.000	.000-.000	.000-.000	143.23	1640	1216.19	Active	retained	Yes
WPOH943	Hartford, CT	LD	BTA184	A	CT	Hartford	Cellco Partnership	Yes	300.000	29100.000-29250.000	31075.000-31225.000	.000-.000	.000-.000			1216.19	Active		No
WPLM398	Hartford, CT	LD	BTA184	B	CT	Hartford	Cellco Partnership	Yes	150.000	31000.000-31075.000	31225.000-31300.000	.000-.000	.000-.000			1216.19	Active		No
WRBA708	Hartford, CT	UU	BTA184	L1	CT	Hartford	Cellco Partnership	Yes	325.000	27500.000-27600.000	27700.000-27925.000	.000-.000	.000-.000			1216.19	Active		Yes
WRBA709	Hartford, CT	UU	BTA184	L2	CT	Hartford	Cellco Partnership	Yes	325.000	27925.000-28050.000	28150.000-28350.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD609	New York, NY	UU	PEA001	M1	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	37600.000-37700.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD610	New York, NY	UU	PEA001	M10	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	38500.000-38600.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD611	New York, NY	UU	PEA001	M2	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	37700.000-37800.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD612	New York, NY	UU	PEA001	M3	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	37800.000-37900.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD613	New York, NY	UU	PEA001	M4	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	37900.000-38000.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD614	New York, NY	UU	PEA001	M5	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	38000.000-38100.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD615	New York, NY	UU	PEA001	M6	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	38100.000-38200.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD616	New York, NY	UU	PEA001	M7	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	38200.000-38300.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes



WRHD617	New York, NY	UU	PEA001	M8	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	38300.000-38400.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD618	New York, NY	UU	PEA001	M9	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	38400.000-38500.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes
WRHD619	New York, NY	UU	PEA001	N1	CT	Hartford	Straight Path Spectrum, LLC	Yes	100.000	38600.000-38700.000	.000-.000	.000-.000	.000-.000			1216.19	Active		No
WRDG500	New York, NY	UU	PEA001	S2	CT	Hartford	Cellco Partnership	Yes	400.000	37800.000-38200.000	.000-.000	.000-.000	.000-.000			1216.19	Active		Yes

