



September 13, 2018

Melanie A. Bachman Acting Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

**RE:** Notice of Exempt Modification for T-Mobile Crown Site BU: 829013

T-Mobile Site ID: CT11178D

467 South Quaker Lane, West Hartford, CT 06110 Latitude: 41.74882000 / Longitude: -72.3132000

Dear Ms. Bachman:

T-Mobile currently maintains (9) existing antennas at the 120' level of the existing 119' monopole at 467 South Quaker Lane in West Hartford, CT (also known as 457 South Quaker Lane and 471 South Quaker Lane). The tower is owned by Crown Castle. The property is owned by Church of St. Mark the Evangelist Corp. T-Mobile now intends to replace (6) existing antennas (6) new panel antennas, Swap out (3) RRU's and add (1) Hybrid fiber cable. T-Mobile will also be adding a handrail kit to their antenna platform as well as radio componentry to their existing radio cabinet.

This facility was approved by the Town of West Hartford on March 31, 2000. This approval came with conditions that would not be violated by this modification. Enclosed is a copy of the original approval.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b) (2). In accordance with R.S.C.A. § 16-50j-73, a copy of this letter is being sent to Shari Cantor, Mayor of the Town of West Hartford, Mark McGovern, Director of Community Development for the Town of West Hartford, as well as the property owner, and Crown Castle is the tower owner.

- 1. The proposed modifications will not result in an increase in the height of the existing tower.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.

### Page 2

- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: William Stone.

### Sincerely,

William Stone Real Estate Specialist 3 Corporate Park Drive, Suite 101 Clifton Park, NY 12065 518-373-3543 William.stone@crowncastle.com

### Attachments:

Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes

Tab 2: Exhibit-2: Structural Modification Report

Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)

cc:

Mayor Shari Cantor Town of West Hartford 50 South Main Street West Hartford, CT 06107

Mark McGovern
Director of Community Development
Town of West Hartford
50 South Main Street
West Hartford, CT 06107

Church of St Marks the Evangelist Corp 1088 NEW BRITAIN AVENUE WEST HARTFORD, CT 06110-2426



- 1. Use the 'Print' button on this page to print your label to your laser or inkjet printer.
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# TOWN PLAN AND ZONING COMMISSION

### **CERTIFIED MAIL**

March 10, 2000

Dennis Brown
Ominipoint Communications, Inc.
100 Filley Street
Bloomfield, CT 06002

SUBJECT: 457 South Quaker Lane – SUP #893

Dear Mr. Brown:

At its regular meeting of March 6, 2000 the West Hartford Town Plan and Zoning Commission gave consideration to the following item:

457 South Quaker Lane – St. Mark's Church – Application (SUP #893) of the Archdiocese of Hartford, R.O., Omnipoint Communications, Inc., Dennis Brown of Omnipoint and Agent for Special Use Permit application. Omnipoint Communications, Inc. proposes to erect a 120 foot tall telecommunications monopole behind St. Mark's Rectory and abutting the right-of-way for Interstate 84. The 120 foot monopole would provide location for Omnipoint antenna and co-location for two other carriers. At the base of the monopole would be an equipment box the size of two filing cabinets. The site would be surrounded by a chain link fenced area, 50' x 50', with security gate and landscape buffering. (Submitted for TPZ receipt on February 7, 2000. Suggest required public hearing be scheduled for March 6, 2000. Required TPZ public hearing scheduled for March 6, 2000.)

R-6 ZONE

After a review of the application and its related exhibits and after consideration of staff technical comments and the public hearing record, the TPZ acted by <u>majority vote</u> (Motion/Kearns; Second/Kappes) (Kappes seated for Wirth) to **CONDITIONALLY** APPROVE the subject application. During its discussions and deliberations on this matter, the Commission made the following findings:

1. The landscape plan shall be revised to substitute the proposed hemlocks with Austrian Pines. The landscape plan shall provide the number, type and size of all proposed plantings.

As required by Section 177.16.7D(4) Telecommunication towers and antennas of the West Hartford Code of Ordinances the applicant shall make payment to the "Town Abandonment Fund". The applicant shall provide to the Town of West Hartford a statement setting forth the estimated cost of construction for the approved antennas, ancillary facilities and supporting structure, together with a payment equal to 5% of the estimated cost of the



TOWN OF WEST HARTFORD 50 SOUTH MAIN STREET WEST HARTFORD, CONNECTICUT 06107-2431 (860) 523-3123 FAX: (860) 523-3200



construction. The payment shall be deposited to the Tower Abandonment Fund.

3. The proposed Special Use Permit will comply with the finding requirements of Section 177-42A(5a & 5b) of the West Hartford Code of Ordinances.

You should now contact the Planning Staff to discuss the submission requirements for your plans. A ten dollar (\$10) filing fee is required to file a notice of approval on the West Hartford Land Records. My staff will happy to assist you in completing these requirements. The TPZ approval is not final until the legal requirements for filing are completed. The effective date of approval is March 31, 2000.

If you have questions, please feel free to call the Planning Staff at 523-3123.

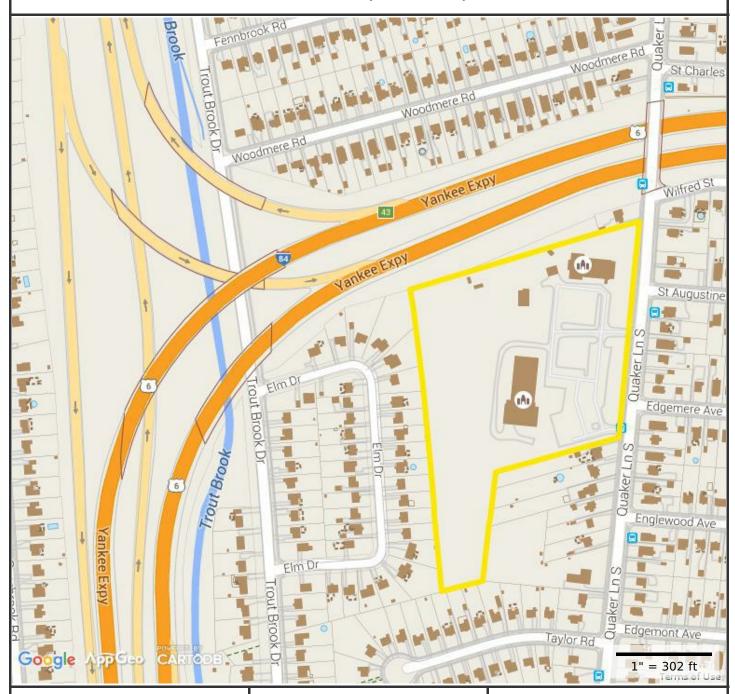
Very truly yours,

Donald R. Foster
Town Planner

C: Ronald Van Winkle, Director of Community Kevin O'Connor, Corporation Counsel Norma Cronin, Town Clerk William Farrell, Town Engineer Subject TPZ File

457Soqkr-Mar00

## CT111178 parcel map



### **Property Information**

Property

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Location Owner 471 SOUTH QUAKER LANE CHURCH OF ST MARK THE EVANGELIST CORP



## MAP FOR REFERENCE ONLY NOT A LEGAL DOCUMENT

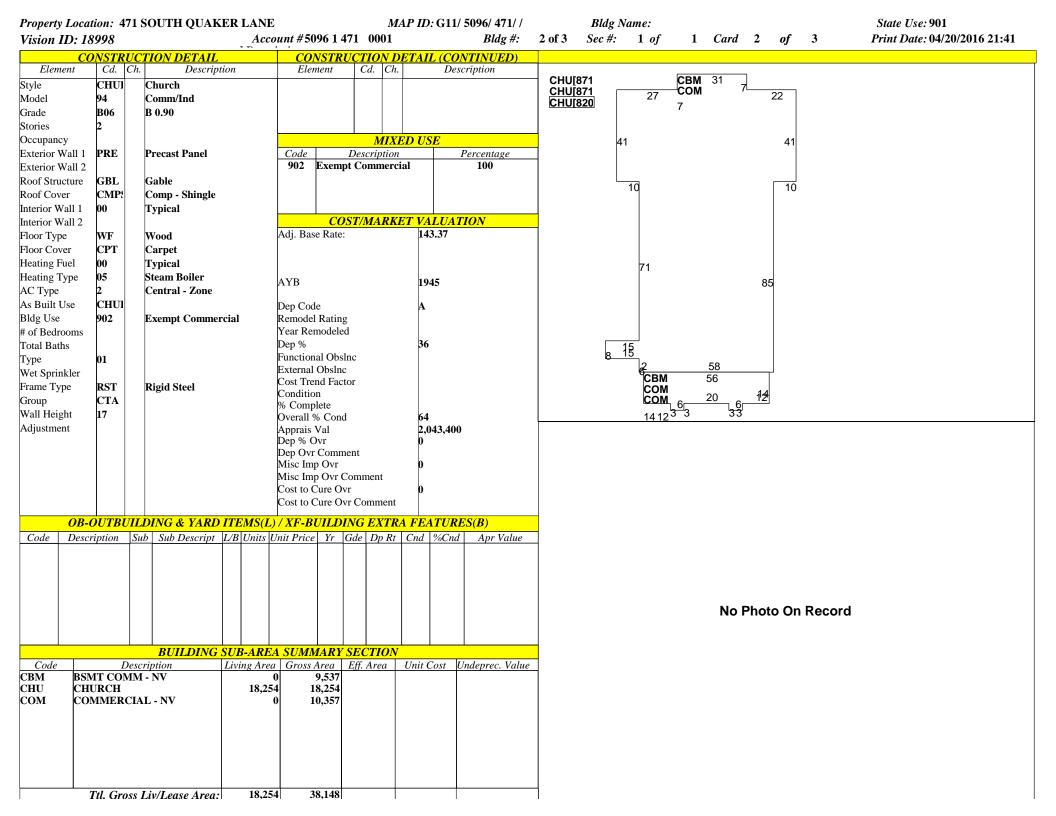
Town of West Hartford, CT makes no claims and no warranties, expressed or implied, concerning the validity or accuracy of the GIS data presented on this map.

Parcels updated 5/22/2015 Properties updated Daily

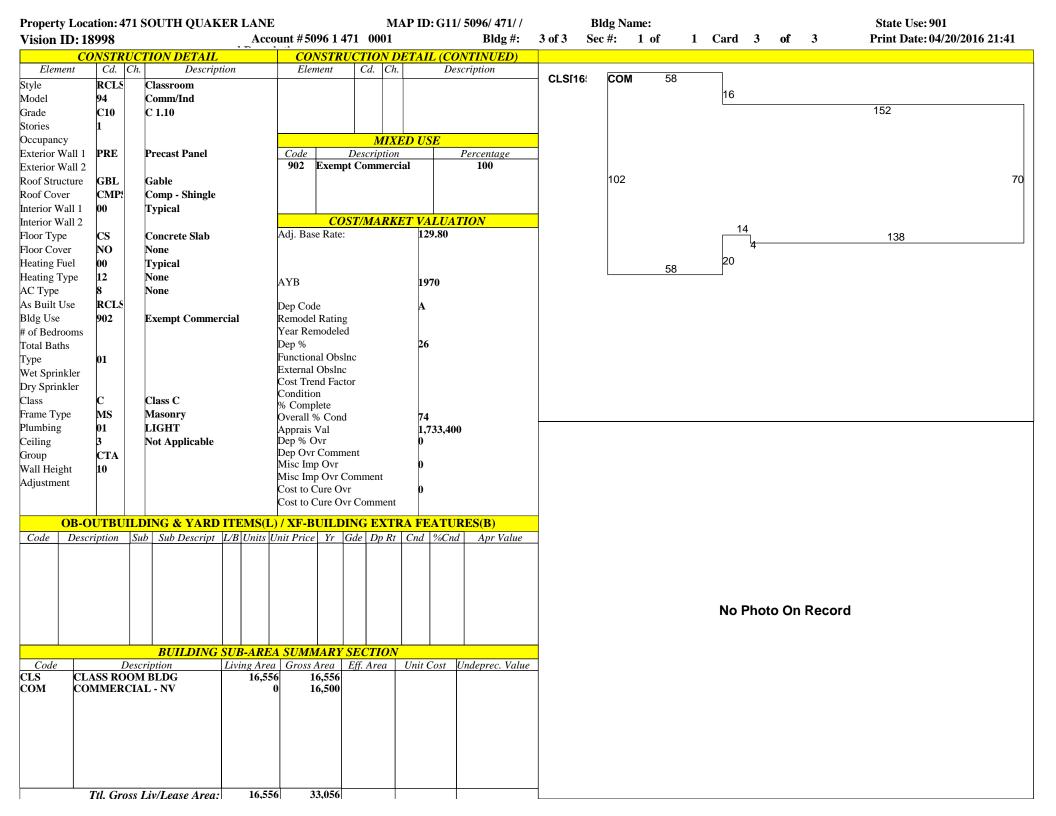
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Property Location: 471 SOUTH QUAKER LANE MAP ID: G11/5096/471// Bldg Name: State Use: 901 Vision ID: 18998 Account #5096 1 471 0001 Bldg #: 1 of 3 Sec #: 1 of 1 *Card* 1 Print Date: 04/20/2016 21:41 CONSTRUCTION DETAIL CONSTRUCTION DETAIL (CONTINUED) Element Cd. Ch. Description Element Cd. Ch. Description Style Colonial **FBLA** вмт 21 Model Residential Int Condition Typical 2AU C05 C 1.10 Grade Attic Access 12 5 Stories Dormer LF Occupancy **MIXED USE** Exterior Wall 1 Brick Code Description Percentage 20 100 901 Exempt Res 15 Exterior Wall 2 Roof Structure Typical Roof Cover Typical Interior Wall 1 Typical Interior Wall 2 COST/MARKET VALUATION Adj. Base Rate: 92.17 25 Interior Flr 1 Typical Interior Flr 2 Heat Fuel Oil Heat Type Forced Air AYB 1945 Yes AC Type # of Bedrooms 34 Dep Code Full Bthrms Remodel Rating 1945 Year Remodeled Half Baths Dep % Extra Fixtures Functional Obslnc Total Rooms External Obslnc Bath Style Typical Cost Trend Factor Kitchen Style Typical 35 Condition Extra Kitchens % Complete Overall % Cond 276,000 Fireplaces Apprais Val Dep % Ovr Prefab Fpl(s) Dep Ovr Comment Bsmt Egress Misc Imp Ovr Foundation Conc Per Piers Misc Imp Ovr Comment None Bsmt Garage(s) Cost to Cure Ovr Fin Bsmt/RRm Cost to Cure Ovr Comment Bsmt Rec Rm OB-OUTBUILDING & YARD ITEMS(L) / XF-BUILDING EXTRA FEATURES(B) Code Sub Sub Descript L/B Units Unit Price Yr Gde Dp Rt Cnd %Cnd Apr Value Description 1970 C 1945 C 1945 C CCP9 50 64 64 83 Canopy-wood 6.75 100 56 7A A5 Garage - 1.0 Sto Garage - 1.0 Sto Enclosed Porch 918 9,600 CRG4 26.14 26.14 52.87 A5 247 3,800 CRG4 RP4 1986 C 1,400 **BUILDING SUB-AREA SUMMARY SECTION** Unit Cost Undeprec. Value Code Description Living Area | Gross Area | Eff. Area 2 STORY U UNFIN ATT 2AU 1,790 3,580 BMT BSMT UNFIN RES 1,790 **SOUTH QUAKER LN 455** Ttl. Gross Liv/Lease Area: 3,580 3,580

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# WEST HARTFORD-I-84-X43

T-MOBILE SITE NUMBER:

CT11178D

CROWN CASTLE BU NUMBER/APPLICATION NUMBER: 829013/433326

## 67D92M CONFIGURATION

467 SOUTH QUAKER LANE WEST HARTFORD, CT 06110

EXISTING 119'-0" MONOPOLE

SHEET #

T-1

C-1

C-2

C-4

C-5E-1

G-1

SP-2

Kibbe St

Flatbush Ave

TITLE SHEET

OVERALL SITE PLAN

PLUMBING DIAGRAM

ONE-LINE DIAGRAM

**SPECIFICATIONS** 

**SPECIFICATIONS** 

ENLARGED SITE PLAN

# **PROJECT SUMMARY**

SITE TYPE: EXISTING EQUIPMENT UPGRADE

SITE ADDRESS: 467 SOUTH QUAKER LANE WEST HARTFORD, CT 06110

JURISDICTION: HARTFORD COUNTY

41.74882000° N LONGITUDE: 72.73132000° W

TOWER OWNER CROWN CASTLE

3200 HORIZON DRIVE, SUITE 150 KING OF PRUSSIA, PA 19406

CONTACT: JASON SMITH

(610) 635-3225

CUSTOMER/APPLICANT: T-MOBILE

4 SYLVAN WAY PARSIPPANY, NJ 07054

(973) 397-4800

OCCUPANCY TYPE:

A.D.A. COMPLIANCE: FACILITY IS UNMANNED AND NOT

FOR HUMAN HABITATION

### **CONTACT INFORMATION**

A&E FIRM: B+T GROUP

1717 S. BOULDER AVENUE TULSA, OK 74119

CONTACT:

DUSTIN SPEARS

ELECTRIC PROVIDER:

TELCO

-T--Mobile-

REMOVE (6) EXISTING ANTENNAS.

- REMOVE (2) EXISTING DUS41.
- INSTALL (6) NEW ANTENNAS AT 120'-0".
- INSTALL (3) NEW RRUs.
- ANTENNAS.
- INSTALL (1) HANDRAIL RÉINFORCEMENT KIT ON EXISTING

## **DO NOT SCALE DRAWINGS**

Kane St

Caya Ave

Westphal St

Boulanger Ave

Levesque Ave

Foley S

Layton St

Mozart St

St Augustine St

Edgemere Ave

Englewood Ave

Edgement Ave

Sidney Ave

Hampton Ave

Flatbush Ave

ALL DRAWINGS CONTAINED HEREIN ARE FORMATTED FOR 11X17. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.

> SEE SHEETS SP-1 & SP-2 FOR ADDITIONAL CONSTRUCTION NOTES

## A/E DOCUMENT REVIEW STATUS

**DRAWING INDEX** 

SHEET DESCRIPTION

TOWER ELEVATION & ANTENNA ORIENTATION

ANTENNA, RRU & TMA SCHEDULE

GROUNDING PLAN AND DETAILS

		TITLE	:	SIGNATURE	DATE
	T-MOBILE	R.E. MGR.:			
	T-MOBILE	R.F. MGR.:			
	T-MOBILE	NetOps:			
	T-MOBILE	CONST. MGR.:			
	INTERCONN	IECT:			
	T-MOBILE	SITE DEV. MGR.:			
	PROPERTY	OWNER:			
٦	PLANNING:				
	1 100	CEDTED: WITH OR	NO COMMENT	CONSTRUCTION N	MY DROCEED

I ACCEPTED: WITH OR NO COMMENTS, CONSTRUCTION MAY PROCEE! NOT ACCEPTED: RESOLVE COMMENTS AND RESUBMIT

ACCEPTANCE DOES NOT CONSTITUTE APPROVAL OF DESIGN, CALCULATIONS, ANALYSIS, TEST METHODS OF MATERIALS DEVELOPED OR SELECTED BY THE SUBCONTRACTOR AND DOES NOT RELIEVE SUBCONTRACTOR FROM FULL COMPLIANCE WITH CONTRACTUAL OBLIGATIONS.

CALL CONNECTICUT ONE CALL



(800) 922-4455 **CALL 3 WORKING DAYS** BEFORE YOU DIG!





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REV.#

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127044.001.01

EXISTING MONOPOLE

**ISSUED FOR:** REV DATE DRWN DESCRIPTION A 8/9/18 FWP PRELIMINARY REVIEW 0 9/6/18 FWP CONSTRUCTION

> B&T ENGINEERING, INC. Expires 2/10/19



SHEET NUMBER:

REVISION

**CODE COMPLIANCE** 

ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALLED IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE CODES:

BUILDING/DWELLING IBC 2012 MECHANICAL IMC 2012 **ELECTRICAL** 

## PROJECT DESCRIPTION

RIGHT ONTO LOCAL ROAD(S) AND ARRIVE AT WEST HARTFORD.

Rumford-St

**LOCATION MAP** 

White Ave

NO SCALE

**DRIVING DIRECTIONS** 

DEPART BRADLEY INTERNATIONAL AIRPORT ON TERMINAL RD. ROAD NAME CHANGES TO BRADLEY FIELD CONNECTOR. ROAD

NAME CHANGES TO CT-20 [BRADLEY FIELD CONNECTOR]. TAKE RAMP (RIGHT) ONTO I-91 [RICHARD P HORAN MEMORIAL HWY]. AT EXIT 32A-32B, TURN RIGHT ONTO RAMP. TAKE RAMP (LEFT) ONTO I-84 [US-6]. AT EXIT 42, TURN LEFT ONTO RAMP. KEEP LEFT TO STAY ON RAMP. TURN LEFT ONTO TROUT BROOK DR. TURN RIGHT ONTO WOODMERE RD. TURN

Boulevard &

-Meadowbrook Rd

THE PROPOSED PROJECT INCLUDES:

- REMOVE (3) EXISTING RRUs.
- RELOCATE (3) EXISTING ANTENNAS.
- INSTALL (1) ADDITIONAL 1 5/8" HYBRID CABLE FOR NEW
- INSTALL (1) BB5216 & (3) XMU.





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: 829013

WEST HARTFORD-I-84-X43 467 SOUTH QUAKER LANE WEST HARTFORD, CT 06110

EXISTING MONOPOLE

PROJECT NO: 127044.001.01 CHECKED BY: RPS

ISSUED FOR:									
REV DATE DRWN DESCRIPTION									
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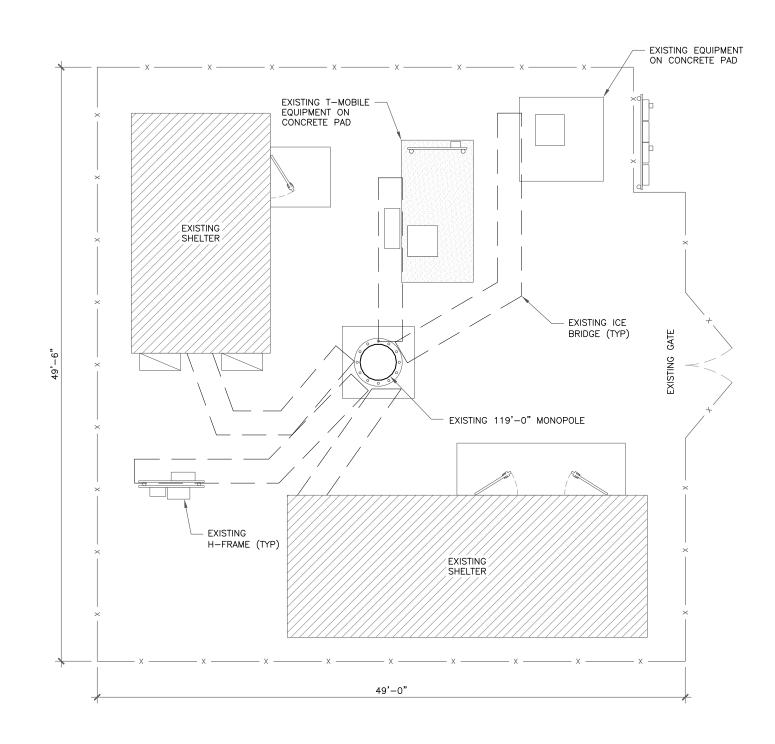
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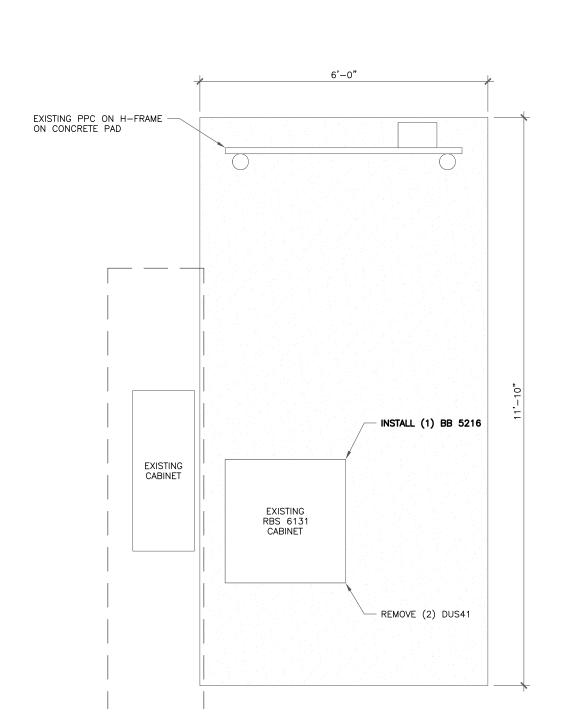
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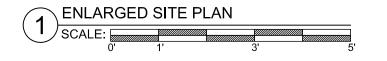
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WEST HARTFORD-I-84-X43 467 SOUTH QUAKER LANE WEST HARTFORD, CT 06110 PROJECT NO: 127044.001.01

EXISTING MONOPOLE

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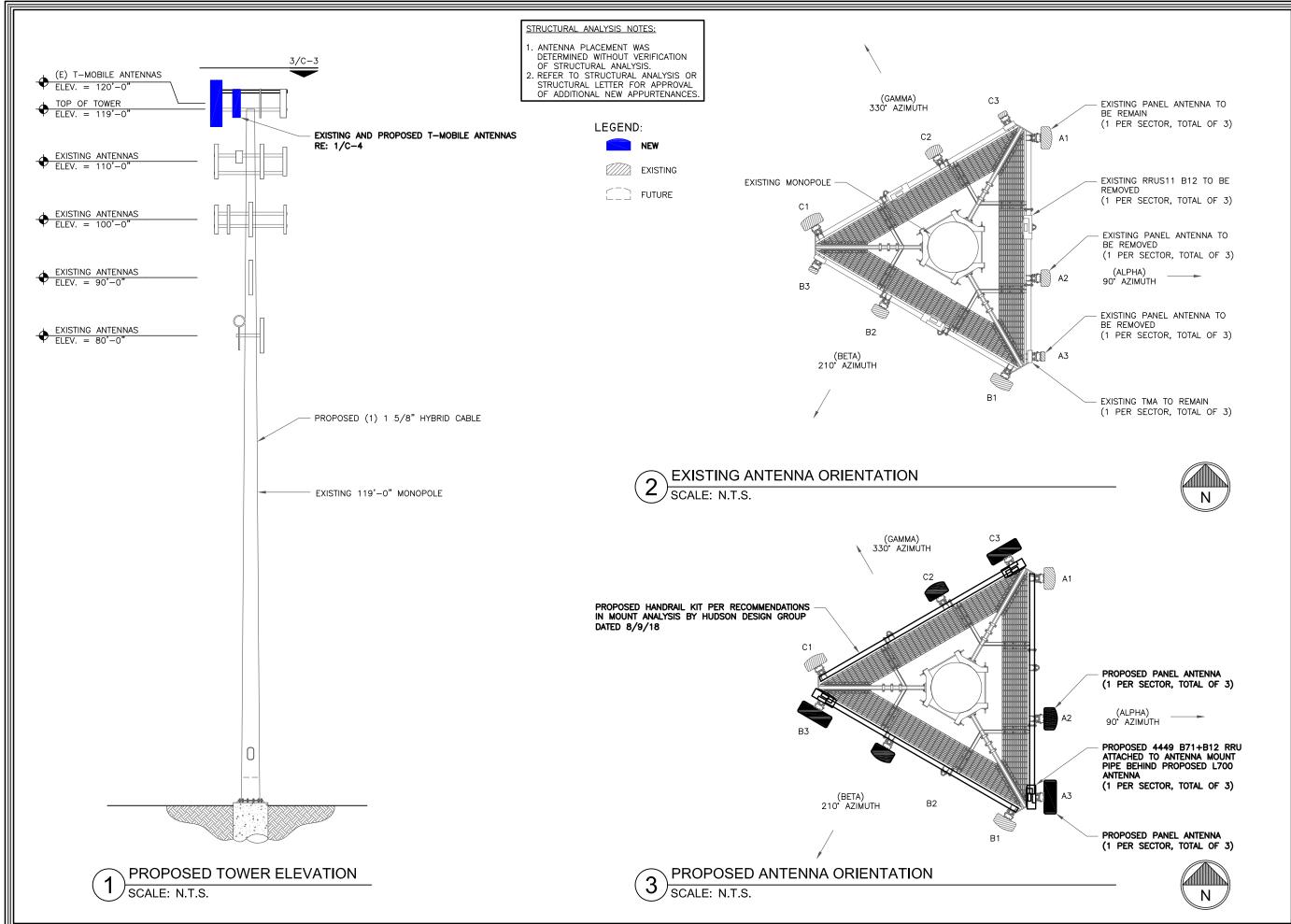
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REVISION





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CT11178D BU #: 829013

PROJECT NO: 127044.001.01 CHECKED BY: RPS

WEST HARTFORD-I-84-X43

467 SOUTH QUAKER LANE WEST HARTFORD, CT 06110

EXISTING MONOPOLE

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B&T ENGINEERING, INC. PEC.0001564 Expires 2/10/19



UNLESS THEY ARE ACTING UNDER THE DIRECTIO OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT.

C-3

	ANTENNA AND COAXIAL CABLE SCHEDULE									
		1	ANTE	INNA AND	COANIAL CABL	E SCHEDULE				
SECTOR MARK	ANTENNA MODEL	AZIMUTH	MECH TILT	ELEC. TILT	ANTENNA CENTERLINE	SECTOR	TMA/RRU	CABLE	JUMPER TYPE	CABLE LENGTH
A-1 L1900/G1900	ERICSSON AIR32 KRD901146-1_B66A_B2A	90°	0°	0°	120'-0"	LEFT ALPHA	0/0	HYBRID CABLES (2) 1-5/8" COAX	1/2" COAX	140'
A-2 L2100	ERICSSON AIR3246 B66	90°	o	o	120'-0"	CENTER ALPHA	0/0	(2) 1-5/8" COAX	1/2" COAX	140'
A-3 U2100/ L700/L600	APXVAARR24_43-U-NA20	90°	o	O.	120'-0"	RIGHT ALPHA	1/1	(2) HYBRID CABLES	DC/FIBER	140'
B-1 L1900/G1900	ERICSSON AIR32 KRD901146-1_B66A_B2A	210°	0,	0,	120'-0"	LEFT BETA	0/0	(1) 1-5/8" COAX	1/2" COAX	140'
B-2 L2100	ERICSSON AIR3246 B66	210°	o	O.	120'-0"	CENTER BETA	0/0	_	_	_
B-3 U2100/ L700/L600	APXVAARR24_43-U-NA20	210°	o	0°	120'-0"	RIGHT BETA	1/1	(2) 1-5/8" COAX	1/2" COAX	140'
C-1 L1900/G1900	ERICSSON AIR32 KRD901146-1_B66A_B2A	330°	0,	0,	120'-0"	LEFT GAMMA	0/0	(2) 1-5/8" COAX	1/2" COAX	140'
C-2 L2100	ERICSSON AIR3246 B66	330°	o	o	120'-0"	CENTER GAMMA	0/0	(2) 1-5/8" COAX	1/2" COAX	140'
C-3 U2100/ L700/L600	APXVAARR24_43-U-NA20	330*	o	O.	120'-0"	RIGHT GAMMA	1/1	_	_	_

### EQUIPMENT NOTES:

- 1. THE HYBRID CABLE LENGTH SHOWN IS ONLY AN ESTIMATE AND SHOULD NOT BE USED FOR ORDERING MATERIALS. CONFIRM THE REQUIRED HYBRID CABLE LENGTH WITH T-MOBILE PROIR TO ORDERING OR INSTALLATION.
- 2. THE CONTRACTOR SHALL TEST THE OPTICAL FIBER AFTER INSTALLATION IN ACCORDANCE WITH T-MOBILE STANDARDS AND SUPPLY THE RESULTS TO T-MOBILE.
- 3. THE CONTRACTOR SHALL CONFIRM THE TOWER TOP EQUIPMENT LIST ABOVE WITH THE FINAL T-MOBILE RFDS PRIOR TO INSTALLATION.
- 4. ALL EXISTING AND PROPOSED ANTENNA CABLES SHALL BE COLOR CODED PER T-MOBILE STANDARDS.
- 5. REFER TO EQUIPMENT MANUFACTURER'S SPECIFICATION SHEETS FOR ADDITIONAL INFORMATION NOT LISTED ABOVE.

67D92M CONFIGURATION TOWER LOADING SUMMARY									
EXISTING QUANTITY	REMOVE QUANTITY	EQUIPMENT TYPE	ADD QUANTITY	TOTAL QUANTITY					
9	6	PANEL ANTENNA	6	9					
3	3	RRUs	3	3					
3	0	TMA	0	3					



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WEST HARTFORD-I-84-X43 467 SOUTH QUAKER LANE WEST HARTFORD, CT 06110

EXISTING MONOPOLE

PROJECT NO: 127044.001.01 CHECKED BY: RPS

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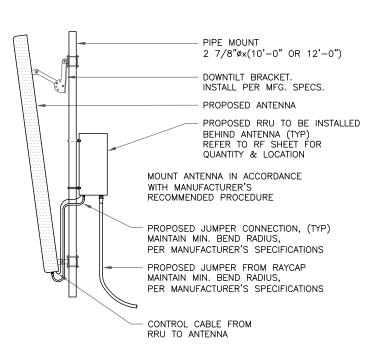
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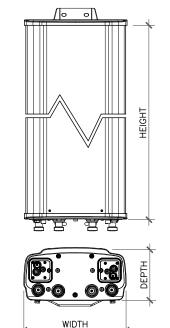
REVISION

AT TIME OF CONSTRUCTION, CONTRACTOR TO VERIFY AZIMUTHS OF EXISTING ANTENNAS. IF DIFFERENT FROM RFDS, PLEASE NOTIFY THE RF ENGINEER AND CONSTRUCTION MANAGER WITH ACTUAL AZIMUTHS TO ENSURE T-MOBILE'S DATABASE IS ACCURATE AND UP-TO-DATE.

## ANTENNA, RRU & TMA SCHEDULE

SCALE: N.T.S.

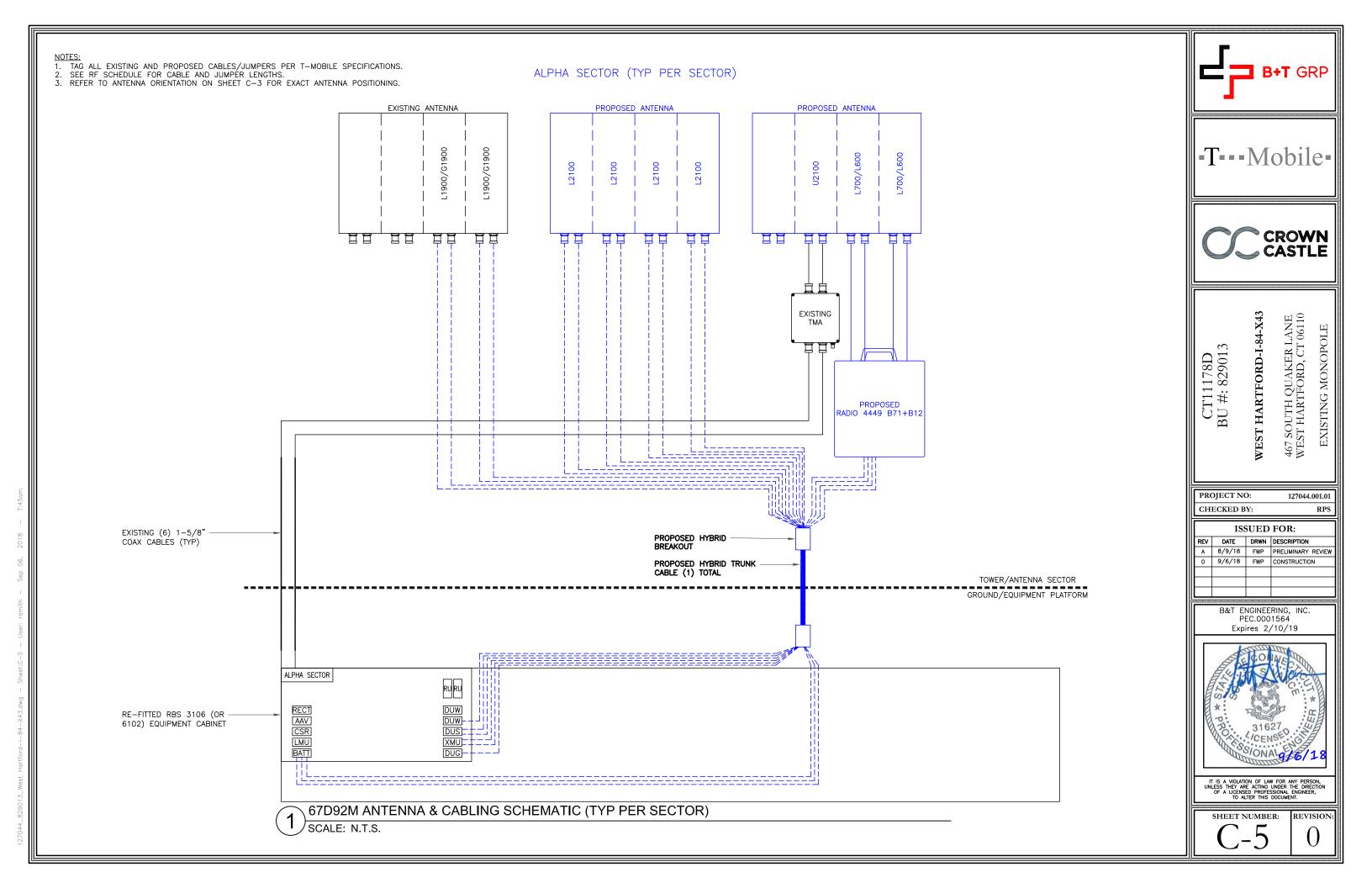


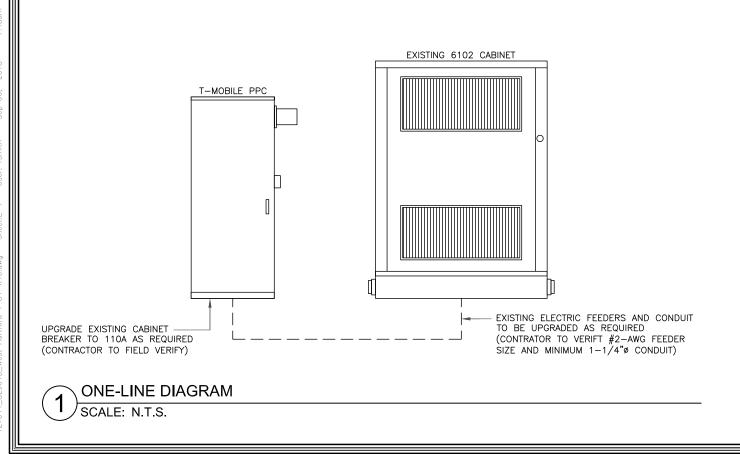


ANTENNA	DIMENSIC	NS (INC	HES)	
MODEL	HEIGHT	WIDTH	DEPTH	WEIGHT
APXVARR24_43-U-NA20	95.9"	24"	8.7"	128 lbs
AIR3246 B66	58.1"	15.75"	9.4"	50.7 lbs

- NOTES:
  1. VERIFY ANTENNA DIMENSIONS WITH MANUFACTURER.
  2. ANTENNA MOUNTING KIT FOR 2 TO 4.5 O.D. MAST
- (RFS, MODEL #APM40-2) (QTY. 2)

  3. LOCKING TILT MOUNT KIT 0-13 DEGREES DOWNTILT
- 4. VERIFY FINAL ANTENNA MODEL WITH CURRENT VERSION OF THE RFDS.







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WEST HARTFORD-I-84-X43 467 SOUTH QUAKER LANE WEST HARTFORD, CT 06110 EXISTING MONOPOLE PROJECT NO: 127044.001.01

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SHEET NUMBER:

REVISION

PROVIDE LABOR, MATERIALS AND EQUIPMENT, ETC. REQUIRED TO COMPLETE THE INSTALLATION SHOWN ON THE DRAWINGS.

2. CODE AND STANDARDS

INSTALLATION SHALL COMPLY WITH APPLICABLE LAWS AND ORDINANCES, UTILITY COMPANY REGULATIONS AND APPLICABLE REQUIREMENTS OF THE LATEST EDITIONS OF THE:

A. NFC- NATIONAL FIRE CODES

UL- UNDERWRITERS LABORATORY

C. NEC- NATIONAL ELECTRIC CODE

D. NEMA- NATIONAL ELECTRIC MANUFACTURERS ASSOCIATION

OSHA- OCCUPATIONAL SAFETY AND HEALTH ACT

IBC- INTERNATIONAL BUILDING CODE

PERMITS:

OBTAIN AND PAY FOR REQUIRED PERMITS, LICENSES, FEES, INSPECTIONS, ETC.

4. COORDINATION:

COORDINATE WORK WITH OTHER TRADES.

SUBMIT BROCHURE FOR APPROVAL ON SERVICE DISCONNECTING MEANS AND OTHER MAJOR SYSTEM COMPONENTS.

**FXISTING SERVICES** 

DO NOT INTERRUPT EXISTING SERVICES WITHOUT WRITTEN PERMISSION OF THE OWNER.

CONNECT ELECTRICALLY OPERATED EQUIPMENT.

RECORD DRAWINGS

MAINTAIN A RECORD OF ALL CHANGES & SUBSTITUTIONS BETWEEN WORK AS SPECIFIED AND INSTALLED. RECORD CHANGED ON A CLEAN SET ON CONTRACT DOCUMENTS WHICH SHALL BE TURNED OVER TO THE CONSTRUCTION MANAGER UPON COMPLETION OF THE

9. IDENTIFICATION:

IDENTIFY SERVICE DISCONNECTING MEAN WITH PERMANENT NAMEPLATE.

10. GUARANTEE/WARRANTY

GUARANTEE INSTALLATION TO BE FREE OF DEFECTS, SHORTS, GROUNDS, ETC, FOR A PERIOD OF ONE YEAR. FURNISH WARRANTY SO THE DEFECTIVE MATERIAL AND/OR WORKMANSHIP WILL BE REPAIRED IMMEDIATELY UPON NOTIFICATION AT NO COST TO THE OWNER

PROVIDE CUTTING REQUIRED TO DO THE WORK. DO NOT CUT MAJOR STRUCTURAL ELEMENTS WITHOUT APPROVAL. PATCHING SHALL BE OF QUALITY EQUAL TO AND OF MATCHING APPEARANCE WITH EXISTING CONSTRUCTION.

12. DITCHING & BACKFILL:

PROVIDE FOR ALL UNDERGROUND INSTALLED CONDUIT AND/OR CABLES.

13. RACEWAYS

UNDERGROUND CONDUIT SHALL BE SCHEDULE 40 PVC CONDUIT (MEET NEMA TC2-1990). EXPOSED CONDUIT SHALL BE RIGID GALVANIZED STEEL CONDUIT BEFORE RISING ABOVE GRADE. PLUG AND CAP EACH END OF SPARE AND EMPTY CONDUITS AND PROVIDE TWO SEPARATE PULL STRINGS - 200 LB. TEST POLYETHYLENE CORD. ALL CONDUIT BENDS SHALL BE A MINIMUM OF 24" RADIUS. RGS CONDUITS, WHEN SPECIFIED, SHALL MEET UL-6 FOR GALVANIZED STEEL. ALL FITTINGS SHALL BE SUITABLE FOR USE WITH THREADED RIGID CONDUIT.

14. SUPPORTS:

AS REQUIRED BY THE NEC.

15. CONDUCTORS

USE 98% CONDUCTIVITY COPPER WITH TYPE XHHW-2 INSULATION, 600V COLOR CODED. USE SOLID CONDUCTORS FOR WIRE UP TO AND INCLUDING #8 AWG. USE STRANDED CONDUCTORS FOR WIRE ABOVE #8 AWG.

16. CONNECTORS FOR POWER CONDUCTORS:

USE PRESSURE TYPE INSULATED TWIST-ON CONNECTORS FOR #10 AWG AND SMALLER. USE SOLDERLESS MECHANICAL TERMINAL LUGS FOR #8 AWG AND LARGER.

240/120V, SINGLE PHASE, 3 WIRE CONNECTION AVAILABLE FROM UTILITY COMPANY. COORDINATE AND PAY ALL FEES.

18. TELEPHONE SERVICE:

PROVIDE EMPTY CONDUITS WITH PULL WIRES AS INDICATED ON DRAWINGS.

19. UTILITY FRAME METER CENTER:

(AS REQUIRED) PROVIDED BY OWNER, INSTALLED BY CONTRACTOR. THE ELECTRICAL DESIGN IN THESE DRAWINGS IS BASED ON A MFTFR CFNTER CONFIGURED AS FOLLOWS:

- A. A NEMA 3R ENCLOSURE, MOUNTED ON THE FRONT SIDE OF AN EQUIPMENT FRAME INCORPORATING 120/240V, 200A METER SOCKETS AND CIRCUIT BREAKER HOUSINGS. EACH METER/CIRCUIT BREAKER COMBINATION SHALL PROVIDE SERVICE TO ONE (1) CARRIER (OR TOWER LIGHTING, AS REQUIRED). METERS ARE TO BE PROVIDED BY LOCAL POWER COMPANY.
- B. TOWERS REQUIRING FAA LIGHTING SHALL BE ALLOCATED ONE METER SOCKET AND CIRCUIT BREAKER HOUSING IN THE METER BANK, CIRCUIT BREAKER TO BE SIZED AS REQUIRED FOR TOWER LIGHTING EQUIPMENT. METER IS TO BE PROVIDED BY LOCAL POWER

20. UTILITY FRAME TELCO CABINET:

PROVIDED BY OWNER, INSTALLED BY CONTRACTOR. THE ELECTRICAL DESIGN ON THESE DRAWINGS IS BASED ON A TELCO CABINET

- A. A NEMA 3R ENCLOSURE SHALL INCLUDE A 3/4" THICK PLYWOOD BACKBOARD SIZED TO FIT CABINET. A PRE-WIRED 20A, 120V, GFCI DUPLEX RECEPTACLE, SURGE PROTECTORS AND A GROUND BAR. TELCO CABINET SHALL BE MOUNTED TO THE UTILITY
- B. THE TELEPHONE CABINET SHALL ACCOMMODATE ALL TELEPHONE LINES (PROPOSED AND FUTURE) AND CONNECTIONS FOR THEM.

21. POWER CABINET:

PROVIDED BY OWNER, INSTALLED BY CONTRACTOR. THE ELECTRICAL DESIGN ON THESE DRAWINGS IS BASED ON A POWER CABINET

- A. A NEMA 3R ENCLOSURE SHALL INCLUDE A 120/240V, 1 PHASE, 200A MAIN BREAKER LOAD CENTER. POWER CABINET SHALL BE MOUNTED TO THE EQUIPMENT SLED SERVICE FRAME. SURGE PROTECTION AND A 20A/120V WEATHERPROOF GFCI RECEPTACLE SHALL ALSO BE MOUNTED TO THE EQUIPMENT SERVICE SLED FRAME
- B. LOAD CENTER SHALL HAVE A DOOR TO ALLOW ACCESS TO INTERNAL COMPONENTS.
- C. PROVIDE A GROUND WIRE SIZED PER NEC IN ALL CIRCUITS OVER 20 AMPS AND IN ALL CIRCUIT RUNS IN PVC.

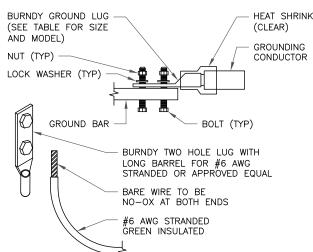
PROVIDED BY OWNER, INSTALLED BY CONTRACTOR. THE ELECTRIDAL DESIGN ON THESE DRAWINGS IS BASED ON A TELCO CABINET AS FOLLOWS:

- A. A NEMA 3R ENCLOSURE SHALL INCLUDE A 3/4" THICK PLYWOOD BACKBOARD SIZED TO FIT A CABINET. A PRE-WIRED 20A, 120V, GFCI DUPLEX RECEPTACLE (IF REQUIRED), SURGE PROTECTORS AND A GROUND BAR. TELCO CABINET SHALL BE MOUNTED TO THE EQUIPMENT SLED SERVICE FRAME.
- B. THE TELEPHONE COMPANY SHALL ACCOMMODATE ALL TELEPHONE LINE (PROPOSED AND FUTURE) AND CONNECTIONS FOR THEM.

WIRE SIZE	BURNDY LUG	BOLT SIZE
#6 AWG GREEN INSULATED	YA6C-2TC38	3/8" - 16 NC S 2 BOLT
#2 AWG SOLID TINNED	YA3C-2TC38	3/8" - 16 NC S 2 BOLT
#2 AWG STRANDED	YA2C-2TC38	3/8" - 16 NC S 2 BOLT
#2/0 AWG STRANDED	YA26-2TC38	3/8" - 16 NC S 2 BOLT
#4/0 AWG STRANDED	YA28-2N	1/2" - 16 NC S 2 BOLT

#### NOTES:

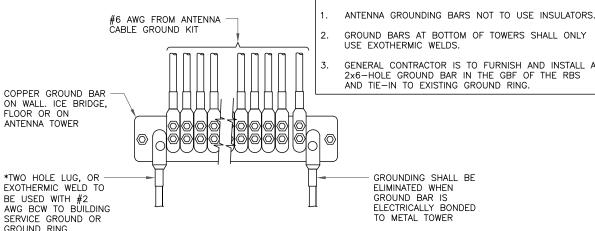
- ALL HARDWARE BOLTS, NUTS, LOCK WASHERS SHALL BE STAINLESS STEEL. ALL HARDWARE ARE TO BE AS FOLLOWS: BOLT, FLAT WASHER GROUND BAR, GROUND LUG, FLAT WASHER AND NUT.
- 2. COPPER SHIELD, ANTIOX, CR NO-OX OR APPROVED EQUAL SHALL BE PLACE WHERE ALL DISSIMILAR METALS CONNECT
- ALL LUGS ARE TO BE INSTALLED PER MANUFACTURER'S SPECIFICATIONS.





GROUNDWIRE INSTALLATION

SCALE: N.T.S.



NOTES:

- GROUND BARS AT BOTTOM OF TOWERS SHALL ONLY USE EXOTHERMIC WELDS.
- GENERAL CONTRACTOR IS TO FURNISH AND INSTALL A 2x6-HOLE GROUND BAR IN THE GBF OF THE RBS AND TIE-IN TO EXISTING GROUND RING.



SHEET NUMBER:

REVISION

CROWN CASTLE

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LANE 7 06110 7 SOUTH QUAKER I EST HARTFORD, CT 1178D 82901 1111 #:8 467 WES

EXISTING MONOPOLE

PROIECT NO 127044.001.01

**ISSUED FOR:** REV DATE DRWN DESCRIPTION A 8/9/18 FWP PRELIMINARY REVIEW 0 9/6/18 FWP CONSTRUCTION

> B&T ENGINEERING, INC. PEC.0001564 Expires 2/10/19

IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT.

#### 1.1 INTENT:

- A. THESE SPECIFICATIONS AND CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE DONE AND THE MATERIALS TO BE FURNISHED FOR CONSTRUCTION. PLANS ARE NOT TO BE SCALED.
- B. THE DRAWINGS AND SPECIFICATIONS ARE INTENDED TO BE FULLY EXPLANATORY AND SUPPLEMENTARY, HOWEVER, SHOULD ANYTHING BE SHOWN, INDICATED OR SPECIFIED ON ONE AND NOT THE OTHER, IT SHALL BE DONE THE SAME AS IF SHOWN, INDICATED OR SPECIFIED IN BOTH.
- C. THE INTENTION OF DOCUMENTS IS TO INCLUDE ALL LABOR AND MATERIALS REASONABLY NECESSARY FOR THE PROPER EXECUTION AND COMPLETION OF THE WORK AS STIPULATED IN THE CONTRACT.
- D. CONFLICTS: THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFICATION OF ALL MEASUREMENTS AT THE SITE BEFORE ORDERING MATERIAL OR DOING ANY WORK. NO COMPENSATION SHALL BE ALLOWED DUE TO DIFFERENCE BETWEEN ACTUAL DIMENSIONS AND THOSE ON THE DOCUMENTS. ANY DISCREPANCY SHALL BE REPORTED TO THE OWNER OR HIS AGENT FOR CONSIDERATION.

#### 1.2 LICENSING REQUIREMENTS:

THE CONTRACTOR IS RESPONSIBLE FOR PROCUREMENT AND MAINTAINING OF ALL APPLICABLE LICENSES AND BONDS.

#### 1.3 STORAGE

ALL MATERIALS MUST BE STORED IN A LEVEL AND DRY FASHION THAT DOES NOT OBSTRUCT THE FLOW OF OTHER WORK. ANY STORAGE METHOD MUST MEET ALL RECOMMENDATIONS OF THE ASSOCIATED MANUFACTURER.

#### 1.4 CLEAN UP:

THE CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATION OF WASTE MATERIALS OR RUBBISH AT ALL TIMES. TRASH MUST BE REMOVED DAILY.

#### 1.5 QUALITY ASSURANCE:

ALL WORK SHALL BE IN ACCORDANCE WITH APPLICABLE LOCAL, STATE AND FEDERAL REGULATIONS.

PART 2 PRODUCTS - NOT APPLICABLE TO THIS SECTION

PART 3 EXECUTION - NOT APPLICABLE TO THIS SECTION

ELECTRICAL

### PART 1 GENERAL

1.1 GENERAL CONDITIONS:

- A. THE CONTRACTOR SHALL INSPECT THE SITE WHERE THIS WORK IS TO BE PERFORMED
- AND FULLY FAMILIARIZE HIMSELF WITH ALL CONDITIONS RELATED TO THIS PROJECT.

  3. THE CONTRACTOR SHALL OBTAIN AND PAY FOR ALL PERMITS AND LICENSES AND SHALL MAKE ALL DEPOSITS AND PAY ALL FEES REQUIRED FOR THE PERFORMANCE OF WORK UNDER THIS SECTION.

**SECTION 16000:** 

C. DRAWINGS SHOW THE GENERAL ARRANGEMENT OF ALL SYSTEMS AND COMPONENTS COVERED UNDER THIS SECTION. THE CONTRACTOR SHALL VERIFY ALL DIMENSIONS. DRAWINGS SHALL NOT BE SCALED TO DETERMINE DIMENSIONS.

#### 1.2 LAWS, REGULATIONS, ORDINANCES, STATUTES AND CODES

A. ALL WORK SHALL BE INSTALLED IN ACCORDANCE WITH THE NATIONAL ELECTRICAL CODE, AND ALL APPLICABLE LOCAL LAWS, REGULATIONS, ORDINANCES, STATUTES AND CODES.

#### 1.3 REFERENCES:

- A. THE PUBLICATIONS LISTED BELOW FORM PART OF THIS SPECIFICATION. EACH PUBLICATION SHALL BE THE LATEST REVISION AND ADDENDUM IN EFFECT ON THE DATE OF THIS SPECIFICATION IS ISSUED FOR CONSTRUCTION UNLESS OTHERWISE NOTED. EXCEPT AS MODIFIED BY THE REQUIREMENTS SPECIFIED HEREIN OR THE DETAILS OF THE DRAWINGS, WORK INCLUDED IN THIS SPECIFICATION SHALL CONFIRM TO THE APPLICABLE PROVISIONS OF THESE PUBLICATIONS.
- 1. ANSI/IEEE (AMERICAN NATIONAL STANDARDS INSTITUTE)
- 2. IEEE (INSTITUTE OF ELECTRICAL AND ELECTRONICS ENGINEERS)
- 3. ASTM (AMERICAN SOCIETY FOR TESTING AND MATERIALS)
- 4. ICFA (INSULATED CABLE ENGINEERS ASSOCIATION)
- 5. NEMA (NATIONAL ELECTRICAL MANUFACTURER'S ASSOCIATION)
- 6. NFPA (NATIONAL FIRE PROTECTION ASSOCIATION)
- 7. OSHA (OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION)
- 8. UL (UNDERWRITERS LABORATORIES, INC.)

### 1.4 SCOPE OF WORK:

- A. WORK UNDER THIS SECTION SHALL CONSIST OF FURNISHING ALL LABOR, MATERIAL AND ASSOCIATED SERVICES REQUIRED TO COMPLETELY CONSTRUCT AND LEAVE READY FOR OPERATION SYSTEMS AS SHOWN ON THE DRAWINGS AND HEREIN DESCRIBED.
- B. ALL ELECTRICAL EQUIPMENT UNDER THIS CONTRACT SHALL BE PROPERLY TESTED, ADJUSTED AND ALIGNED BY THE CONTRACTOR.
- C. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL EXCAVATING, DRAINING, TRENCHES, BACKFILLING, AND REMOVAL AND EXCESS DIRT.
- D. THE CONTRACTOR SHALL FURNISH TO THE OWNER, CERTIFICATES OF FINAL INSPECTION AND APPROVAL FROM THE INSPECTION AUTHORITIES HAVING JURISDICTION.

### PART 2 PRODUCTS

#### 2.1 GENERAL:

- A. ALL ITEMS OF MATERIALS AND EQUIPMENT SHALL BE NEW, FREE FROM DEFECTS AND OF THE BEST QUALITY NORMALLY USED FOR THE PURPOSE IN GOOD COMMERCIAL PRACTICE.
- B. ALL MATERIALS AND EQUIPMENT SHALL BE ACCEPTABLE TO THE AUTHORITY HAVING JURISDICTION AS SUITABLE FOR THE USE INTENDED.
- C. ALL EQUIPMENT SHALL BEAR THE UNDERWRITERS LABORATORIES LABEL OF APPROVAL, AND SHALL CONFORM TO THE REQUIREMENTS OF THE NATIONAL ELECTRICAL CODE.
- D. ALL OVERCURRENT DEVICES SHALL HAVE AN INTERRUPTING RATING EQUAL TO OR GREATER THAN THE SHORT CIRCUIT CURRENT TO WHICH THEY ARE SUBJECTED, 10,000 AIC MINIMUM. VERIFY AVAILABLE SHORT CIRCUIT CURRENT DOES NOT EXCEED THE RATING OF ELECTRICAL EQUIPMENT.

#### 2.2 MATERIALS AND EQUIPMENT:

#### A. CONDUIT:

- RIGID GALVANIZED STEEL CONDUIT (RGS) SHALL BE HOT-DIP GALVANIZED INSIDE AND OUTSIDE INCLUDING ENDS AND THREADS AND ENAMELED OR LACQUERED INSIDE IN ADDITION TO GALVANIZING.
- FLEXIBLE METAL CONDUIT SHALL BE GALVANIZED, ZINC—COATED STEEL, PVC COATED FOR OUTDOOR APPLICATIONS.
- CONDUIT CLAMPS, STRAPS AND SUPPORTS SHALL BE STEEL OR MALLEABLE IRON. ALL FITTINGS SHALL BE COMPRESSION TYPE AND WATERTIGHT.
- 4. NON-METALLIC CONDUIT FITTINGS SHALL BE SCHEDULE 40 PVC, HEAVY-WALL RIGID WITH SOLVENT-CEMENT-TYPE JOINTS AS RECOMMENDED BY THE MANUFACTURER

#### B. WIRE AND CABLE:

- 1. WIRE AND CABLE SHALL BE FLAME—RETARDANT, MOISTURE AND HEAT RESISTANT THERMOPLASTIC, SINGLE CONDUCTOR, COPPER, TYPE THHN/THWN, 600 VOLT, SIZES AS INDICATED, #12 AWG MINIMUM.
- 2. #10 AWG AND SMALLER CONDUCTORS SHALL BE SOLID AND #8 AWG AND LARGER CONDUCTORS SHALL BE STRANDED.
- 3. SOLDERLESS, PRESSURE—TYPE CONNECTORS CONSTRUCTED OF HIGH—STRENGTH, NON—CORRODIBLE, TIN—PLATED COPPER DESIGNED TO FURNISH HIGH—PULLOUT STRENGTH AND HIGH CONDUCTIVITY JOINTS SHALL BE USED.
- 4. SUPPORT GRIPS SHALL BE SINGLE WEAVE, CLOSED MESH, HIGH-GRADE, NON-MAGNETIC, TIN-COATED BRONZE, CAPABLE OF SUPPORTING TEN TIMES THE CABLE DEAD WEIGHT, HUBBELL KELLEMS OR APPROVED EQUAL.

#### C. DISCONNECT SWITCHES:

 DISCONNECT SWITCHES SHALL BE HEAVY DUTY, DEAD—FRONT, QUICK—MAKE, QUICK—BREAK, EXTERNALLY OPERABLE, HANDLE LOCKABLE AND INTERLOCKED WITH COVER IN CLOSED POSITION, RATING AS INDICATED, UL LABELED FURNISHED IN NEMA 3R ENCLOSURE, SQUARE D CLASS 3110 OR APPROVED EQUAL.

#### D. SYSTEM GROUNDING:

- GROUNDING CONDUCTOR SHALL BE BARE, SOLID TINNED COPPER, SIZE AS INDICATED, EXCEPT ABOVE GROUND GROUNDING CONDUCTORS SHALL BE INSULATED.
- 2. GROUND BUSSES SHALL BE BARE ANNEALED COPPER BARS OF RECTANGULAR CROSS SECTION.
- 3. CONNECTORS SHALL BE HIGH-CONDUCTIVITY, HEAVY DUTY, LISTED AND LABELED AS GROUNDING CONNECTORS FOR THE MATERIALS USED. USE TWO-HOLE COMPRESSION LUGS WITH HEAT SHRINK FOR MECHANICAL CONNECTIONS.
- 4. EXOTHERMIC WELDED CONNECTIONS SHALL BE PROVIDED IN KIT FORM AND SELECTED FOR THE SPECIFIC TYPES, SIZES, AND COMBINATIONS OF CONDUCTORS AND OTHER ITEMS TO BE CONNECTED.
- 5. GROUND RODS SHALL BE COPPER—CLAD STEEL WITH HIGH—STRENGTH STEEL CORE AND ELECTROLYTIC—GRADE COPPER OUTER SHEATH, MOLTEN WELDED TO CORE, 3/4"x10'-0".

#### E. OTHER MATERIALS:

 THE CONTRACTOR SHALL PROVIDE OTHER MATERIALS, THOUGH NOT SPECIFICALLY DESCRIBED, WHICH ARE REQUIRED FOR A COMPLETELY OPERATIONAL SYSTEM AND PROPER INSTALLATION OF THE WORK.



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CT11178D BU #: 829013 467 SOUTH QUAKER LANE WEST HARTFORD, CT 06110

EXISTING MONOPOLE

PROJECT NO: 127044.001.01
CHECKED BY: RPS

HARTFORD-I-84-

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Ш	REV	DATE	DRWN	DESCRIPTION					
Ш	Α	8/9/18	FWP	PRELIMINARY REVIEW					
Ш	0	9/6/18	FWP	CONSTRUCTION					
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#### 3.1 GENERAL:

- A. ALL MATERIALS AND EQUIPMENT SHALL BE INSTALLED IN STRICT ACCORDANCE W/ THE MANUFACTURER'S RECOMMENDATION
- EQUIPMENT SHALL BE TIGHTLY COVER AND PROTECTED AGAINST DIRT OR WATER, AND AGAINST CHEMICAL OR MECHANICAL INJURY DURING INSTALLATION AND CONSTRUCTION PERIODS.

#### LABOR AND WORK:

- A. ALL LABOR FOR THE INSTALLATION OF MATERIALS AND EQUIPMENT FURNISHED FOR THE ELECTRICAL SYSTEM SHALL BE DONE BY EXPERIENCED MECHANICS OF THE
- ALL ELECTRICAL EQUIPMENT FURNISHED SHALL BE ADJUSTED, ALIGNED AND TESTED BY THE CONTRACTOR AS REQUIRED TO PRODUCE THE INTENDED PERFORMANCE.
- UPON COMPLETION OF THE WORK, THE CONTRACTOR SHALL THOROUGHLY CLEAN ALL EXPOSED EQUIPMENT, REMOVE ALL LABELS AND ANY DEBRIS, CRATING OR CARTONS AND LEAVE THE INSTALLATION FINISHED AND READY FOR OPERATION.

#### COORDINATION:

THE CONTRACTOR SHALL COORDINATE THE INSTALLATION OF ELECTRICAL ITEMS WITH THE OWNER-FURNISHED EQUIPMENT DELIVERY SCHEDULE TO PREVENT UNNECESSARY DELAYS IN THE TOTAL WORK.

#### 3.4 INSTALLATION:

#### A. CONDUIT

- ALL ELECTRICAL WIRING SHALL BE INSTALLED IN CONDUIT AS HEREIN SPECIFIED. NO CONDUIT OR TUBING OF LESS THAN 3/4 INCH NOMINAL SIZE
- 2. PROVIDE RGS CONDUIT FOR ALL EXPOSED, EXTERIOR CONDUIT.
- PROVIDE SCHEDULE 40 PVC OR RGS CONDUIT BELOW GRADE, 1" MINIMUM, UNLESS NOTED OTHERWISE. ALL 90 DEGREE BENDS TO ABOVE GRADE SHALL BE RGS, MINIMUM BURIAL DEPTH SHALL BE 30" CLEAR TO TOP OF CONDUIT, UNLESS NOTED OTHERWISE.
- 4. USE GALVANIZED FLEXIBLE STEEL CONDUIT WHERE DIRECT CONNECTION IS NOT DESIRABLE FOR REASONS EQUIPMENT MOVEMENT, VIBRATION OR FOR EASE OF MAINTENANCE. USE LIQUIDTIGHT, PVC COATED FLEXIBLE METAL CONDUIT FOR OUTDOOR APPLICATIONS.
- INSTALL GALVANIZED FLEXIBLE STEEL CONDUIT AT ALL POINTS OF CONNECTION TO EQUIPMENT MOUNTED ON SUPPORTS TO ALLOW FOR EXPANSION AND
- A RUN OF CONDUIT BETWEEN BOXES OR FITTINGS SHALL NOT CONTAIN MORE THE EQUIVALENT OF FOUR QURATER-BENDS INCLUDING THOSE BENDS LOCATED IMMEDIATELY AT THE BOX OR FITTING. THE RADIUS OF BENDS SHALL NEVER BE SHORTER THAN THAT OF THE CORRESPONDING TRADE ELBOW.
- 7. WHERE CONDUIT HAS TO BE CUT IN THE FIELD, IT SHALL BE CUT SQUARE WITH A PIPE CUTTER USING CUTTING KNIVES.
- ALL CONDUITS SHALL BE SWABBED CLEAN BY PULLING AN APPROPRIATE SIZE MANDREL THROUGH THE CONDUIT BEFORE INSTALLATION OF WIRE OR CABLE. CLEAR ALL BLOCKAGES AND REMOVE BURRS, DIRT AND DEBRIS.
- INSTALL MULE TAPE IN ALL EMPTY CONDUIT IDENTIFY PULL STRINGS AT EACH FND WITH ITS DESTINATION.
- 10. PROVIDE INSULATED GROUNDING BUSHINGS OR ALL CONDUITS STUBBED INTO EQUIPMENT ENCLOSURES OR STUBBED OUT FOR FUTURE USE BY OTHERS.
- 11. CONTRACTOR IS RESPONSIBLE FOR PROTECTING ALL CONDUITS DURING CONSTRUCTION. TEMPORARY OPENINGS IN THE CONDUIT SYSTEM SHALL BE PLUGGED OR CAPPED TO PREVENT ENTRANCE OF MOISTURE OR FOREIGN MATTER. CONTRACTOR SHALL REPLACE ANY CONDUIT CONTAINING FOREIGN MATERIALS THAT CANNOT BE REMOVED
- 12. INSTALL 3" RED METALLIC LOCATOR TAPE 12" ABOVE ALL UNDERGROUND CONDUIT AND WIRE.
- 13. CONDUITS SHALL BE INSTALLED IN SUCH A MANNER AS TO INSURE AGAINST COLLECTION OF TRAPPED CONDENSATION.

#### WIRE AND CABLE:

1. ALL POWER WIRING SHALL BE COLOR CODED AS FOLLOWS

DESCRIPTION	120/270V	208Y/120V	480Y/277V
PHASE A	BLACK	BLACK	BROWN
PHASE B	RED	RED	ORANGE
PHASE C		BLUE	YELLOW
NEUTRAL	WHITE	WHITE	GRAY
GROUND	GREEN	GREEN	GREEN

- SPLICES SHALL BE MADE ONLY AT OUTLETS, JUNCTION BOXES OR ACCESSIBLE RACEWAYS WITH PRESSURE-TYPE CONNECTORS
- PULLING LUBRICANT SHALL BE SOAPSTONE POWDER, POWDERED TALC OR A COMMERCIAL PULLING COMPOUND. NO SOAP SUDS, SOAP FLAKES, OIL OR GREASE SHALL BE USED, AS THESE MAY BE HARMFUL TO CABLE INSULATION. CONTRACTOR SHALL USE NYLON OR HEMP ROPE FOR PULLING CABLE TO AVOID SCORING THE CONDUIT.
- 4. CABLES SHALL BE NEATLY TRAINED, WITHOUT INTERLACING, AND BE OF SUFFICIENT LENGTH IN ALL BOXES, EQUIPMENT. ETC. TO PERMIT MAKING A NEAT ARRANGEMENT. CABLES SHALL BE SECURED IN A MANNER TO AVOID TENSION ON CONDUCTORS OR TERMINALS AND SHALL BE PROTECTED FROM MECHANICAL INJURY AND FROM MOISTURE. SHARP BENDS OVER CONDUIT BUSHINGS ARE PROHIBITED. DAMAGED CABLES SHALL BE REMOVED AND REPLACE AT THE CONTRACTOR'S EXPENSE.

#### C DISCONNECT SWITCHES:

1. INSTALL DISCONNECT SWITCHED LEVEL AND PLUMB. CONNECT TO WIRING SYSTEM AND GROUND AS INDICATED.

#### D GROUNDING:

- 1. ALL METALLIC PARTS OF ELECTRICAL EQUIPMENT WHICH DO NOT CARRY CURRENT SHALL BE GROUNDED IN ACCORDANCE WITH THE REQUIREMENTS OF ARTICLE 250 OF THE NATIONAL ELECTRIC CODE.
- PROVIDE ELECTRICAL GROUNDING AND BONDING SYSTEMS INDICATED WITH ASSEMBLY OF MATERIALS, INCLUDING GROUNDING ELECTRODES, BONDING JUMPERS AND ADDITIONAL ACCESSORIES AS REQUIRED FOR A COMPLETE
- 3. ROUTE GROUNDING CONNECTIONS AND CONDUCTORS TO GROUND IN THE SHORTEST AND STRAIGHTEST PATHS POSSIBLE TO MINIMIZE TRANSIENT VOLTAGE
- 4. TIGHTEN GROUNDING AND BONDING CONNECTORS, INCLUDING SCREWS AND BOLTS, IN ACCORDANCE WITH MANUFACTURER'S PUBLISHED TORQUE TIGHTENING VALUES FOR CONNECTORS AND BOLTS. WHERE MANUFACTURE'S TORQUING REQUIREMENTS ARE NOT AVAILABLE. TIGHTEN CONNECTIONS TO COMPLY WITH TIGHTENING TORQUE VALUES SPECIFIED IN UL 486A TO ASSURE PERMANENT AND EFFECTIVE GROUNDING.
- 5. ALL UNDERGROUND GROUNDING CONNECTIONS SHALL BE MADE BY THE EXOTHERMIC WELD PROCESS AND INSTALL IN ACCORDANCE WITH THE MANUFACTURER'S INSTRUCTION.
- 6. ALL GROUND CONNECTIONS SHALL BE INSPECTED FOR TIGHTNESS. EXOTHERMIC—WELDED CONNECTIONS SHALL BE APPROVED BY THE CONSTRUCTION INSPECTOR BEFORE BEING PERMANENTLY CONCEALED.
- APPLY CORROSION-RESISTANT FINISH TO FIELD CONNECTION AND PLACES WHERE FACTORY APPLIED PROTECTIVE COATING HAVE BEEN DESTROYED. USE COPPER-BASED "NO-OX" OR APPROVED EQUAL.
- A SEPARATE, CONTINUOUS, INSULATED EQUIPMENT GROUNDING CONDUCTOR SHALL BE INSTALLED IN ALL FEEDER AND BRACH CIRCUITS.
- 9. BOND ALL INSULATED GROUNDING BUSHINGS WITH A BARE #6 AWG GROUNDING CONDUCTOR TO A GROUND BUS OR GROUNDING LUG IN ENCLOSURE.
- 10. DIRECT BURIED GROUND CONDUCTORS SHALL BE INSTALLED AT A NOMINAL DEPTH OF 30" BELOW GRADE, UNLESS NOTED OTHERWISE.
- 11. ALL GROUNDING CONDUCTORS EMBEDDED IN OR PENETRATING CONCRETE SHALL BE INSULATED OR INSTALLED IN PVC CONDUIT.
- 12. INSTALL ELECTROLYTIC GROUNDING SYSTEM IN STRICT ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS. REMOVE SEALING TAPE FROM LEACHING AND BREATHER HOLES. INSTALL PROTECTIVE BOX FLUSH WITH GRADE.
- 13. DRIVE GROUND RODS UNTIL TOPS ARE 30" BELOW FINAL GRADE
- 14. GROUNDING CONDUCTOR TO EQUIP[MENT GROUND LUGS:
  - BOLTED TO EQUIPMENT HOUSING WITH STAINLESS STEEL BOLTS AND LOCK
  - ALL EQUIPMENT TO BE GROUNDED SHALL BE FREE OF PAINT OR ANY OTHER MATERIAL COVERING BARE METAL AT THE POINT OF CONNECTION.

### 3.5 ACCEPTANCE TESTING:

- PROVIDE PERSONNEL AND EQUIPMENT, MAKE REQUIRED TESTS AND SUBMIT TEST REPORTS UPON COMPLETE OF TESTS.
- WHEN MATERIAL AND/OR WORKMANSHIP IS FOUND NOT TO COMPLY WITH THE SPECIFIED REQUIREMENTS, THE NON—COMPLYING ITEMS SHALL BE REMOVED FROM THE JOBSITE AND REPLACED WITH THE ITEMS COMPLYING WITH THE SPECIFIED REQUIREMENTS PROMPTLY AFTER RECEIPT OF NOTICE OF SUCH NON-COMPLIANCE.

#### A. TEST PROCEDURES:

- ALL FEEDERS SHALL HAVE THEIR INSULATION TESTED AFTER INSTALLATION, BUT BEFORE CONNECTION TO DEVICES. THE CONDUCTORS SHALL TEST FREE FROM SHORT CIRCUITS AND GROUNDS. TESTING SHALL BE FOR ONE MINUTE, USING 1000V DC. INVESTIGATE ANY VALUES LESS THAN 50 MEGOHMS.
- PRIOR TO ENERGIZING CIRCUITRY, TEST WIRING DEVICES FOR ELECTRICAL CONTINUITY AND PROPER POLARITY CONNECTIONS.
- MEASURE AND RECORD VOLTAGES BETWEEN PHASES AN BETWEEN PHASE WIRE AND NEUTRALS. SUBMIT A REPORT OF MAXIMUM AND MINIMUM VOLTAGES.
- PERFORM GROUND TEST TO MEASURE GROUND RESISTANCE OF GROUNDING SYSTEM USING THE IEEE STANDARD 3-POINT "FALL -OF-POTENTIAL" METHOD. PROVIDE PLOTTED TEST VALUES AND LOCATION SKETCH. NOTIFY THE ENGINEER IMMEDIATELY IF MEASURED VALUE IS OVER 5 OHMS.

END OF SECTION

FND OF SPECIFICATION



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T111 #: 8

EXISTING MONOPOLE 77 SOUTH QUAKER EST HARTFORD, CJ 467 WE

LANE r 06110

PROIECT NO 127044.001.01

HARTFORD-I-84

ISSUED FOR:								
REV	DATE	DRWN	DESCRIPTION					
Α	8/9/18	FWP	PRELIMINARY REVIEW					
0 9/6/18		FWP	CONSTRUCTION					

B&T ENGINEERING, INC. PEC.0001564 Expires 2/10/19



SHEET NUMBER:

REVISION

Date: July 2, 2018

Heather Simeone Crown Castle

3530 Toringdon Way, Suite 300

Charlotte, NC 28277

**Subject:** Structural Analysis Report

Carrier Designation: T-Mobile Co-Locate

Carrier Site Number: CT11178D

Carrier Site Name: West Hartford/I-84/X43

Tower Engineering Professionals

326 Tryon Road

(919) 661-6351

Raleigh, NC 27603

Crown Castle BU Number: 829013

Crown Castle Site Name: West Hartford/I-84/X43

Crown Castle JDE Job Number: 496734 Crown Castle Work Order Number: 1591903 Crown Castle Order Number: 433326 Rev. 6

Engineering Firm Designation: TEP Project Number: 25680.161675

Site Data: 467 South Quaker Lane (Church of St. Mark),

West Hartford, Hartford County, CT 06110

Latitude 41°44′55.59″, Longitude -72°43′52.86″

119 Foot - Monopole Tower

Dear Heather Simeone,

Tower Engineering Professionals is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 1211828, in accordance with order 433326, revision 6.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Existing/Reserved + Proposed Equipment

Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

**Sufficient Capacity** 

This analysis has been performed in accordance with the 2016 <u>Connecticut State Building Code</u> (2012 <u>International Building Code</u>) based upon an ultimate 3-second gust wind speed of 125 mph converted to a nominal 3-second gust wind speed of 97 mph per Section 1609.3.1 and Appendix N as required for use in the TIA-222-G Standard per Exception #5 of Section 1609.1.1. Exposure Category C and Risk Category II were used in this analysis.

All modifications and equipment proposed in this report shall be installed in accordance with the appurtenances listed in Tables 1 and 2 and the attached drawing for the determined available structural capacity to be effective.

We at *Tower Engineering Professionals* appreciate the opportunity of providing our continuing professional services to you and *Crown Castle*. If you have any questions or need further assistance on this or any other projects please give us a call.

Structural analysis prepared by: Alex Bramhall, E.I. / AAS

Respectfully submitted by:

Aaron T. Rucker, P.E.



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tnxTower Output

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### 1) INTRODUCTION

This tower is a 119-ft monopole tower designed by Pirod, Inc. in May of 2000. The tower was originally designed for a wind speed of 80 mph per EIA/TIA-222-F for the appurtenances listed in Table 3. The tower has been modified multiple times in the past to accommodate additional loading. TEP visited the site in July of 2014 to perform a rebar mapping. All information provided to TEP was assumed to be accurate and complete.

### 2) ANALYSIS CRITERIA

The analysis has been performed in accordance with the ANSI/TIA-222-G-2-2009 Structural Standard for Antenna Supporting Structures and Antennas – Addendum 2 using a nominal 3-second gust wind speed of 97 mph with no ice, 40 mph with 1.0 inch ice thickness, and 60 mph under service loads with the following design criteria:

Type of Analysis: Rigorous Structural Analysis

Classification of Structure: Class II

Exposure Category: Exposure C

Topographic Category: Category 1

Earthquake Category: Not Considered

Earthquake effects may be ignored per this standard for site locations where Ss does not exceed 1.0.

(Hartford County Max Ss = 0.28).

Table 1 - Proposed Antenna and Cable Information

Mounting Level (ft)	Flevation	Number of Antennas	Antenna Manufacturer		Number of Feed Lines		Note											
		3	RFS Celwave	APXVAARR24_43-U-NA20 w/ Mount Pipe														
100.0	120.0	120.0	120.0	120.0	120.0	120.0	3	Ericsson	AIR 3246 B66 w/ Mount Pipe	_	1 1/0	_						
120.0							120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0	120.0
		3	Ericsson	Radio 4449 B12/B71														
		1	Tower Mounts	Handrail Kit														

Notes:

Table 2 - Existing/Reserved Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note			
		3	Commscope	LNX-6515DS-VTM w/ Mount Pipe		1-5/8 7/8	3			
	120.0	3	Ericsson	AIR 21 B2A B4P w/ Mount Pipe	1					
120.0		3	Ericsson	RRUS 11 B12						
					3	Ericsson	AIR -32 B2A/B66AA w/ Mount Pipe	10	4.5/0	
					3 Ericsson		KRY 112 144/1	12	1-5/8	1
		1 Tower Mounts		Platform Mount [LP 403-1]						
115.0	115.0	1	Andrew	drew VHLP2-18		1/2	1			
113.0	115.0	1	Tower Mounts	Side Arm Mount [SO 102-3]	<b>'</b>	1/2	1			

<sup>1)</sup> See "Appendix B - Base Level Drawing" for assumed feed line configuration.

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note						
		3	Powerwave Tech.	7770.00 w/ Mount Pipe									
		2	KMW Comm.	AM-X-CD-16-65-00T-RET w/ Mount Pipe									
		2	Quintel Tech.	QS66512-3 w/ Mount Pipe									
		1	Andrew	SBNH-1D6565C w/ Mount Pipe									
			1	CCI Antennas	TPA-65R-LCUUUU-H8 w/ Mount Pipe								
		6	CCI Antennas	TPX-070821	12 2	1-5/8 3/4							
110.0	110.0	6	Powerwave Tech.	7020.00	2	7/16	1						
		6	Powerwave Tech.	LGP21401	2	3/8							
		3	Ericsson	RRUS 11									
		3	Ericsson	RRUS 32									
		3	Ericsson	RRUS 32 B2									
		3	Powerwave Tech. 1001983										
		2	Raycap DC6-48-60-18-8F										
		1	1 Tower Mounts Miscellaneous [NA 507-1]										
		1	Tower Mounts	Platform Mount [LP 712-1]									
		3	Amphenol	BXA-80063-4BF-EDIN-X w/ Mount Pipe									
								2	Andrew	LNX-6514DS-T4M w/ Mount Pipe			
				1	Antel	BXA-70063-6CF-EDIN-0 w/ Mount Pipe	12	1-5/8	1				
100.0	100.0	1	RFS Celwave	DB-T1-6Z-8AB-0Z	SZ-8AB-0Z								
100.0	100.0	1	Tower Mounts	Platform Mount [LP 403-1]									
		6	Commscope	SBNHH-1D65B w/ Mount Pipe									
		3	Alcatel Lucent	RRH2x60-700									
		3	Alcatel Lucent	RRH2x60-AWS	2	1-5/8	2						
		3	Alcatel Lucent	RRH2X60-PCS									
		1	RFS Celwave	DB-T1-6Z-8AB-0Z									
90.0	90.0 3 Kathrein 742 213 w/ Mount Pipe		742 213 w/ Mount Pipe	6	1-5/8	4							
	83.0	1	Andrew	VHLP2-23									
	03.0	1	Clearwire	CW Junction Box	3	5/8							
80.0		3	Argus Tech.	LLPX310R w/ Mount Pipe	3	1/2 1/4	1						
33.0	81.0	3	Samsung Telecomm.	Wimax Dap Head	1	5/16	'						
	80.0	1	Tower Mounts	Tower Mounts Side Arm Mount [SO 101-3]									

### Notes:

- Existing equipment Reserved equipment 1) 2) 3) 4)
- Existing equipment to be removed; not considered in this analysis Abandoned equipment; considered in this analysis

Mounting Level (ft)	Elevetion	Number of Antennas	Antenna Manufacturer	I Antenna Model		Feed Line Size (in)
120.0	120.0	12	Generic	1'x4' Panels	12	1-5/8
110.0	110.0	12	Generic	1'x4' Panels	12	1-5/8
100.0	100.0	12	Generic	1'x4' Panels	12	1-5/8

### 3) ANALYSIS PROCEDURE

**Table 4 - Documents Provided** 

Document	Remarks	Reference	Source
Supplemental Geotechnical Report	Tower Engineering Professionals	3636697	CCISites
Tower Foundation Drawings	Pirod, Inc.	3636698	CCISites
Rebar Mapping	Tower Engineering Professionals	3636698	CCISites
Tower Manufacturer Drawings	Pirod, Inc.	3525378	CCISites
Tower Reinforcement Drawings	Natcomm Consulting Engineers, Inc.	3525386	CCISites
Post-Modification Inspection	Natcomm Consulting Engineers, Inc.	3974228	CCISites
Tower Reinforcement Drawings	Tower Engineering Professionals	5650111	CCISites
Post-Modification Inspection	SGS Towers, Inc.	5852136	CCISites

### 3.1) Analysis Method

tnxTower (version 7.0.5.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

RISA-3D, a commercially available analysis software package, was used to model and analyze the foundation. Selected output from the analysis is included in Appendix C.

### 3.2) Assumptions

- 1) The tower and foundation were built in accordance with the manufacturer's specifications.
- 2) The tower and foundation have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2, and "Appendix B Base Level Drawing".
- 4) All tower components are in sufficient condition to carry their full design capacity.
- 5) Serviceability with respect to antenna twist, tilt, roll, or lateral translation, is not checked and is left to the carrier or tower owner to ensure conformance. See Table 7.
- 6) All antenna mounts and mounting hardware are structurally sufficient to carry the full design capacity requirements of appurtenance wind area and weight as provided by the original manufacturer specifications. It is the carrier's responsibility to ensure compliance to the structural limitations of the existing and/or proposed antenna mounts. TEP did not analyze antennas supporting mounts as part of this structural analysis report.

This analysis may be affected if any assumptions are not valid or have been made in error. Tower Engineering Professionals should be notified to determine the effect on the structural integrity of the tower.

### 4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (lb)	ΦP <sub>allow</sub> (Ib)	% Capacity	Pass / Fail
L1	119.083 - 101.083	Pole	TP26x22.13x0.25	1	-8929.87	1479480.00	23.1	Pass
L2	101.083 - 66.5	Pole	TP34.063x24.873x0.313	2	-18889.40	2387960.00	58.7	Pass
L3	66.5 - 32.8333	Pole	TP41.75x32.498x0.375	3	-27587.90	3492730.00	64.1	Pass
L4	32.8333 - 0	Pole	TP49.063x39.849x0.375	4	-39470.60	3984000.00	74.9	Pass
						Summary		
						Pole (L4)	74.9	Pass
						Rating =	74.9	Pass

Table 6 - Tower Component Stresses vs. Capacity - LC7

Notes	Component	ent Elevation (ft) % Capacity		Pass / Fail	
1	Slip Splice Connection	101.1	25.0	Pass	
1	Slip Splice Connection	66.5	62.9	Pass	
1	Slip Splice Connection	32.8	69.5	Pass	
1	Anchor Rods	-	85.1	Pass	
1	Base Plate	-	69.4	Pass	
1	Base Foundation Soil Interaction	-	78.9	Pass	
1	Base Foundation Structural	-	58.2	Pass	
1	Rock Anchors	-	88.7	Pass	

Structure Rating (max from all components) =	88.7%
--	-------

Notes:

Table 7 - Dish Twist/Sway Results for 60 mph Service Wind Speed

Elevation	I I I I I I I I I I I I I I I I I I I	Beam Deflection					
(ft)		Deflection (in)	Tilt (deg)	Twist (deg)			
115.0	Andrew VHLP2-18	14.708	1.119	0.020			

### 4.1) Recommendations

- 1) If the load differs from that described in Tables 1 and 2 of this report, "Appendix B Base Level Drawing" or the provisions of this analysis are found to be invalid, another structural analysis should be performed.
- 2) The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

<sup>1)</sup> See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the % capacity listed.

# APPENDIX A TNXTOWER OUTPUT

Section 4		2	-
Length (ft) 37.50	37.50	37.50	18.00
Number of Sides 18	18	18	18
Thickness (in) 0.375	0.375	0.313	0.250
Socket Length (ft)	4.67	3.83	2.92
Top Dia (in) 39.849	32.498	24.873	22.130
Bot Dia (in) 49.063	41.750	34.063	26.000
Grade	A572-65		
Weight (lb) 17124.1 6695.0	5581.5	3690.1	1157.5
0.0 ft	66.5 ft		119.1 ft_
ALL REACTIONS ARE FACTORED  AXIAL 91495 lb  SHEAR 6775 lb  TORQUE 1216 lb-ft 40 mph WIND - 1.000 in ICE AXIAL 39493 lb  SHEAR 31149 lb  TORQUE 9435 lb-ft REACTIONS - 97 mph WIND			

### **DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
AIR -32 B2A/B66AA w/ Mount Pipe	120	1001983	110
AIR -32 B2A/B66AA w/ Mount Pipe	120	1001983	110
AIR -32 B2A/B66AA w/ Mount Pipe	120	1001983	110
KRY 112 144/1	120	DC6-48-60-18-8F	110
KRY 112 144/1	120	DC6-48-60-18-8F	110
KRY 112 144/1	120	2.4" Dia x 6-ft Mount Pipe	110
APXVAARR24 43-U-NA20 w/ Mount Pipe	120	2.4" Dia x 6-ft Mount Pipe	110
APXVAARR24 43-U-NA20 w/ Mount Pipe	120	2.4" Dia x 6-ft Mount Pipe	110
APXVAARR24 43-U-NA20 w/ Mount Pipe	120	2.4" Dia x 6-ft Mount Pipe	110
AIR 3246 B66 w/ Mount Pipe	120	2.4" Dia x 6-ft Mount Pipe	110
AIR 3246 B66 w/ Mount Pipe	120	2.4" Dia x 6-ft Mount Pipe	110
AIR 3246 B66 w/ Mount Pipe	120	Platform Mount [LP 712-1]	110
RADIO 4449 B12/B71	120	Miscellaneous [NA 507-1]	110
RADIO 4449 B12/B71	120	7770.00 w/ Mount Pipe	110
BADIO 4449 B12/B71	120	BXA-80063-4BF-EDIN-X w/ Mount Pipe	100
KRY 112 144/2	120	BXA-80063-4BF-EDIN-X w/ Mount Pipe	100
KRY 112 144/2	120	BXA-70063-4BF-EDIN-X W/ Mount Pipe	100
KRY 112 144/2	120	LNX-6514DS-T4M w/ Mount Pipe	100
2.4" Dia x 6-ft Mount Pipe	120	LNX-6514DS-T4M w/ Mount Pipe	100
2.4" Dia x 6-ft Mount Pipe	120	DB-T1-6Z-8AB-0Z	100
2.4" Dia x 6-ft Mount Pipe	120	(2) SBNHH-1D65B w/ Mount Pipe	100
2.4" Dia x 8.5-ft Mount Pipe	120	(2) SBNHH-1D65B w/ Mount Pipe	100
Platform Mount [LP 404-1] (w/ Handrail Kit)	120	(2) SBNHH-1D65B w/ Mount Pipe	100
	-	1 1	100
2.4" Dia x 6-ft Mount Pipe	115	RRH2x60-700	
Side Arm Mount [SO 102-3] VHI P2-18	115	RRH2x60-700 RRH2x60-700	100
7770.00 w/ Mount Pipe	115	RRH2x60-AWS	100
7770.00 w/ Mount Pipe	110	RRH2x60-AWS	100
·	-	RRH2x60-AWS	
AM-X-CD-16-65-00T-RET w/ Mount Pipe	110	RRH2X60-PCS	100
AM-X-CD-16-65-00T-RET w/ Mount Pipe	110	RRH2X60-PCS	100
QS66512-3 w/ Mount Pipe QS66512-3 w/ Mount Pipe	110	RRH2X60-PCS	100
<u>'</u>	-		
SBNH-1D6565C w/ Mount Pipe	110	DB-T1-6Z-8AB-0Z	100
TPA-65R-LCUUUU-H8 w/ Mount Pipe	110	Platform Mount [LP 403-1]	100
(2) LGP21401	110	BXA-80063-4BF-EDIN-X w/ Mount Pipe	100
(2) LGP21401	110	2'x3' Ice Shield 2'x3' Ice Shield	97
(2) LGP21401	110		95
(2) TPX-070821	110	742 213 w/ Mount Pipe	90
(2) TPX-070821	110	742 213 w/ Mount Pipe	90
(2) TPX-070821	110	742 213 w/ Mount Pipe	90
(2) 7020.00	110	LLPX310R w/ Mount Pipe	80
(2) 7020.00	110	LLPX310R w/ Mount Pipe	80
(2) 7020.00	110	WIMAX DAP HEAD	80
RRUS 32	110	WIMAX DAP HEAD	80
RRUS 32	110	WIMAX DAP HEAD	80
RRUS 32	110	CW JUNCTION BOX	80
RRUS 32 B2	110	2.4" Dia x 6-ft Mount Pipe	80
RRUS 32 B2	110	2.4" Dia x 6-ft Mount Pipe	80
RRUS 32 B2	110	2.4" Dia x 6-ft Mount Pipe	80
RRUS 11	110	Side Arm Mount [SO 101-3]	80
RRUS 11	110	LLPX310R w/ Mount Pipe	80
RRUS 11	110	VHLP2-23	80

### **MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

### **TOWER DESIGN NOTES**

- TOWER DESIGN NOTES

  1. Tower is located in Hartford County, Connecticut.
  2. Tower designed for Exposure C to the TIA-222-G Standard.
  3. Tower designed for a 97 mph basic wind in accordance with the TIA-222-G Standard.
  4. Tower is also designed for a 40 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
  5. Deflections are based upon a 60 mph wind.
  6. Tower Structure Class II.
  7. Topographic Category 1 with Crest Height of 0.00 ft
  8. TOWER RATING: 74.9%

Scale: NTS
Dwg No. E-1

4	Tower Engineering Professionals	Job: West Hartford/I-84/	X43 (BU 829013)
A CONTRACTOR OF THE CONTRACTOR	326 Tryon Road	Project: TEP No. 25680.16167	5
	Raleigh, NC 27603	Client: Crown Castle	Drawn by: AAS
Tower Engineering Professionals	Phone: (919) 661-6351	Code: TIA-222-G	Date: 07/02/18
		Path: CULTURAL SANDERS DE LA PROGRACIÓ DE SA PROGRACIÁ CON P. 167557 J 161637	5 809013 WEST HARFFORDI-BOXES SOLUTION Analysis on Fower 809013 LCT in

### *tnxTower*

Tower Engineering Professionals

326 Tryon Road Raleigh, NC 27603 Phone: (919) 661-6351 FAX: (919) 661-6350

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	West Hartford/I-84/X43 (BU 829013)	1 of 19
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## **Tower Input Data**

There is a pole section.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in Hartford County, Connecticut.

Basic wind speed of 97 mph.

Structure Class II.

Exposure Category C.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 1.000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 40 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## **Options**

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

√ Use Code Stress Ratios

✓ Use Code Safety Factors - Guys
 Escalate Ice
 Always Use Max Kz
 Use Special Wind Profile
 Include Bolts In Member Capacity
 Leg Bolts Are At Top Of Section
 Secondary Horizontal Braces Leg
 Use Diamond Inner Bracing (4 Sided)
 SR Members Have Cut Ends

SR Members Are Concentric

Distribute Leg Loads As Uniform Assume Legs Pinned

√ Assume Rigid Index Plate

- √ Use Clear Spans For Wind Area
   Use Clear Spans For KL/r
   Retension Guys To Initial Tension
- √ Bypass Mast Stability Checks
- √ Use Azimuth Dish Coefficients
- Project Wind Area of Appurt.
   Autocalc Torque Arm Areas
   Add IBC .6D+W Combination
- √ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder

Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

 √ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-G Bracing Resist. Exemption Use TIA-222-G Tension Splice Exemption Poles

 ✓ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

## **Tapered Pole Section Geometry**

Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft	Sides	in	in	in	in	
L1	119.08-101.08	18.00	2.917	18	22.130	26.000	0.250	1.000	A572-65
									(65 ksi)
L2	101.08-66.50	37.50	3.833	18	24.873	34.063	0.313	1.250	A572-65
									(65 ksi)

## *tnxTower*

### Tower Engineering Professionals

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Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L3	66.50-32.83	37.50	4.667	18	32.498	41.750	0.375	1.500	A572-65
L4	32.83-0.00	37.50		18	39.849	49.063	0.375	1.500	(65 ksi) A572-65 (65 ksi)

## **Tapered Pole Properties**

Section	Tip Dia.	Area	I	r	С	I/C	J	It/Q	w	w/t
	in	$in^2$	$in^4$	in	in	$in^3$	$in^4$	$in^2$	in	
L1	22.471	17.362	1050.090	7.767	11.242	93.407	2101.561	8.683	3.455	13.82
	26.401	20.433	1711.654	9.141	13.208	129.592	3425.561	10.218	4.136	16.544
L2	25.982	24.361	1856.528	8.719	12.635	146.930	3715.500	12.183	3.828	12.248
	34.588	33.476	4817.433	11.981	17.304	278.404	9641.206	16.741	5.445	17.424
L3	33.960	38.235	4984.583	11.404	16.509	301.930	9975.725	19.121	5.060	13.492
	42.394	49.247	10650.982	14.688	21.209	502.192	21315.979	24.628	6.688	17.835
L4	41.628	46.984	9249.061	14.013	20.243	456.899	18510.293	23.496	6.353	16.942
	49.819	57.950	17355.138	17.284	24.924	696.329	34733.112	28.981	7.975	21.267

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade A	djust. Factor $A_f$	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals	Double Angle Stitch Bolt Spacing Redundants
ft	ft <sup>2</sup>	in					in	in	in
L1				1	1	1			
119.08-101.08									
L2				1	1	1			
101.08-66.50									
L3 66.50-32.83				1	1	1			
L4 32.83-0.00				1	1	1			

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Sector	Component Type	Placement	Total Number	Number Per Row	Start/End Position	Width or Diameter	Perimeter	Weight
		Туре	ft	rumber	1 er Row	1 Ostilon	in	in	plf
Safety Line 3/8	В	Surface Ar	119.00 - 0.00	1	1	0.250 0.250	0.375		0.220
Rung 5/8" SR (12.5"w, 16"s)	В	(CaAa) Surface Ar (CaAa)	119.00 - 0.00	1	1	0.250 0.250 0.250	0.488		0.816
LDF7-50A(1-5/8) (1 TBR)	A	Surface Ar (CaAa)	119.08 - 0.00	2	2	0.500 0.500	1.980		0.820
EC4-50(1/2")	В	Surface Ar (CaAa)	115.00 - 80.00	1	1	0.250 0.250	0.630		0.160
LDF7-50A(1-5/8") (1E + 2R) *** 90' ***	С	Surface Ar (CaAa)	100.00 - 0.00	3	3	0.000 0.000	1.980		0.820
LDF7-50A(1-5/8") (Abandoned)	A	Surface Ar (CaAa)	90.00 - 0.00	6	6	-0.250 -0.250	1.980		0.820
2" Flexible Conduit	В	Surface Ar (CaAa)	80.00 - 0.00	2	2	0.250 0.250	2.000		0.340

# Tower Engineering Professionals

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## Feed Line/Linear Appurtenances - Entered As Area

Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg		71	ft			ft²/ft	plf
**120**				,				
LDF7-50A(1-5/8)	Α	No	Inside Pole	119.08 - 0.00	10	No Ice	0.00	0.820
						1/2" Ice	0.00	0.820
						1" Ice	0.00	0.820
MLC HYBRID	Α	No	CaAa (Out Of	119.08 - 0.00	2	No Ice	0.00	0.983
SPOWER/12FIBER(1-1/			Face)			1/2" Ice	0.00	2.205
2)			,			1" Ice	0.00	4.038
*** 110' ***								
LDF7-50A(1-5/8")	C	No	Inside Pole	110.00 - 0.00	12	No Ice	0.00	0.820
,						1/2" Ice	0.00	0.820
						1" Ice	0.00	0.820
WR-VG102ST-BRDA(	C	No	Inside Pole	110.00 - 0.00	2	No Ice	0.00	0.201
7/16")	_	110	1113146 1 016	110.00	-	1/2" Ice	0.00	0.201
(In Conduit)						1" Ice	0.00	0.201
FB-L98B-002-XXX(3/8)	C	No	Inside Pole	110.00 - 0.00	1	No Ice	0.00	0.065
(In Conduit)	_	110	1113146 1 016	110.00	•	1/2" Ice	0.00	0.065
(iii conduit)						1" Ice	0.00	0.065
3" Flexible Conduit	C	No	Inside Pole	110.00 - 0.00	1	No Ice	0.00	1.040
3 Tiexible Collumn	C	110	mside i oie	110.00 0.00		1/2" Ice	0.00	1.040
						1" Ice	0.00	1.040
WR-VG86ST-BRD(3/4)	C	No	Inside Pole	110.00 - 0.00	2	No Ice	0.00	0.584
WIC 1 G00051 BRD(5/4)	C	110	mside i oie	110.00 0.00	2	1/2" Ice	0.00	0.584
						1" Ice	0.00	0.584
FB-L98B-034-XXX(3/8)	C	No	Inside Pole	110.00 - 0.00	1	No Ice	0.00	0.057
D-L/0D-034-AAA(3/0)	C	140	mside i oic	110.00 - 0.00	1	1/2" Ice	0.00	0.057
						1" Ice	0.00	0.057
*** 115' ***						1 100	0.00	0.037
EC4-50(1/2")	В	No	CaAa (Out Of	80.00 - 0.00	1	No Ice	0.00	0.160
EC 1 30(1/2 )		110	Face)	00.00 0.00	•	1/2" Ice	0.00	0.850
			r acc)			1" Ice	0.00	2.151
*** 100' ***						1 100	0.00	2.131
LDF7-50A(1-5/8")	C	No	Inside Pole	100.00 - 0.00	11	No Ice	0.00	0.820
EDI / 30/1(1 3/0 )	C	110	mside i oie	100.00 0.00	11	1/2" Ice	0.00	0.820
						1" Ice	0.00	0.820
*** 80' ***						1 100	0.00	0.020
FSJ1-50A(1/4")	В	No	Inside Pole	80.00 - 0.00	3	No Ice	0.00	0.045
(In Conduit)		110	mside i ore	00.00 0.00	5	1/2" Ice	0.00	0.045
(III Conduit)						1" Ice	0.00	0.045
HJ4.5-50(5/8")	В	No	Inside Pole	80.00 - 0.00	3	No Ice	0.00	0.400
(In Conduit)	ь	140	mside i oic	00.00 - 0.00	3	1/2" Ice	0.00	0.400
(III Conduit)						1" Ice	0.00	0.400
9207(5/16")	В	No	Inside Pole	80.00 - 0.00	1	No Ice	0.00	0.400
(In Conduit)	Б	INO	HISIUC FOIC	00.00 - 0.00	1	1/2" Ice	0.00	0.600
(III Conduit)						1/2 Ice 1" Ice	0.00	0.600
FSJ4-50B(1/2")	В	No	CaAa (Out Of	80.00 - 0.00	3	No Ice	0.00	0.000
F3J4-30D(1/2 )	D	INO	Face)	00.00 - 0.00	3	1/2" Ice	0.00	0.140
			race)			1/2 Ice 1" Ice	0.00	1.997
***						1 100	0.00	1.99/

## Feed Line/Linear Appurtenances Section Areas

# Tower Engineering Professionals 326 Tryon Road

326 Tryon Road Raleigh, NC 27603 Phone: (919) 661-6351 FAX: (919) 661-6350

Job	West Hartford/I-84/X43 (BU 829013)	<b>Page</b> 4 of 19
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Client	Crown Castle	Designed by AAS

Tower	Tower	Face	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	lb
L1	119.08-101.08	A	0.000	0.000	7.128	0.000	212.53
		В	0.000	0.000	2.423	0.000	20.79
		C	0.000	0.000	0.000	0.000	112.10
L2	101.08-66.50	A	0.000	0.000	41.613	0.000	523.95
		В	0.000	0.000	9.713	0.000	82.33
		C	0.000	0.000	19.899	0.000	819.34
L3	66.50-32.83	A	0.000	0.000	53.328	0.000	563.14
		В	0.000	0.000	16.372	0.000	142.44
		C	0.000	0.000	19.998	0.000	809.73
L4	32.83-0.00	A	0.000	0.000	52.008	0.000	549.20
		В	0.000	0.000	15.967	0.000	138.92
		C	0.000	0.000	19.503	0.000	789.69

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness			In Face	Out Face	
	ft	Leg	in	ft <sup>2</sup>	ft <sup>2</sup>	$ft^2$	ft <sup>2</sup>	lb
L1	119.08-101.08	A	2.256	0.000	0.000	19.060	0.000	883.21
		В		0.000	0.000	24.866	0.000	396.79
		C		0.000	0.000	0.000	0.000	112.10
L2	101.08-66.50	A	2.194	0.000	0.000	84.769	0.000	2533.41
		В		0.000	0.000	59.388	0.000	1418.86
		C		0.000	0.000	43.764	0.000	1465.00
L3	66.50-32.83	A	2.082	0.000	0.000	103.587	0.000	2760.14
		В		0.000	0.000	67.743	0.000	2167.57
		C		0.000	0.000	43.461	0.000	1435.82
L4	32.83-0.00	A	1.864	0.000	0.000	99.192	0.000	2534.89
		В		0.000	0.000	63.686	0.000	1920.84
		C		0.000	0.000	41.470	0.000	1361.01

### **Feed Line Center of Pressure**

Se	ection	Elevation	$CP_X$	$CP_Z$	$CP_X$	$CP_Z$
					Ice	Ice
		ft	in	in	in	in
	L1	119.08-101.08	0.162	-0.502	0.753	-0.609
	L2	101.08-66.50	-0.482	0.158	0.082	0.078
	L3	66.50-32.83	-0.597	0.168	-0.022	0.093
	L4	32.83-0.00	-0.639	0.180	-0.042	0.108

### **Shielding Factor Ka**

ı	Tower	Feed Line	Description	Feed Line	$K_a$	$K_a$
	Section	Record No.		Segment Elev.	No Ice	Ice
	L1	1	Safety Line 3/8	101.08 -	1.0000	1.0000
			•	119.00		
	L1	2	Rung 5/8" SR (12.5"w, 16"s)	101.08 -	1.0000	1.0000

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	Crown Castle	AAS

Tower	Feed Line	Description	Feed Line	$K_a$	$K_a$
Section	Record No.		Segment Elev.	No Ice	Ice
			119.00		
L1	5	LDF7-50A(1-5/8)	101.08 -	1.0000	1.0000
			119.08		
L1	18	EC4-50(1/2")	101.08 -	1.0000	1.0000
			115.00		
L1	21	LDF7-50A(1-5/8")	101.08 -	1.0000	1.0000
			100.00		
L1	24	LDF7-50A(1-5/8")	101.08 - 90.00	1.0000	1.0000
L1	29	2" Flexible Conduit	101.08 - 80.00	1.0000	1.0000
L2	1	Safety Line 3/8	66.50 - 101.08	1.0000	1.0000
L2	2	Rung 5/8" SR (12.5"w, 16"s)	66.50 - 101.08	1.0000	1.0000
L2	5	LDF7-50A(1-5/8)	66.50 - 101.08	1.0000	1.0000
L2	21	LDF7-50A(1-5/8")	66.50 - 100.00	1.0000	1.0000
L2	24	LDF7-50A(1-5/8")	66.50 - 90.00	1.0000	1.0000
L2	29	2" Flexible Conduit	66.50 - 80.00	1.0000	1.0000
L3	1	Safety Line 3/8	32.83 - 66.50	1.0000	1.0000
L3	2	Rung 5/8" SR (12.5"w, 16"s)	32.83 - 66.50	1.0000	1.0000
L3	5	LDF7-50A(1-5/8)	32.83 - 66.50	1.0000	1.0000
L3	21	LDF7-50A(1-5/8")	32.83 - 66.50	1.0000	1.0000
L3	24	LDF7-50A(1-5/8")	32.83 - 66.50	1.0000	1.0000
L3	29	2" Flexible Conduit	32.83 - 66.50	1.0000	1.0000

Discrete	e Tower	l nade
		Luuus

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weight
			ft ft	0	ft		ft <sup>2</sup>	ft <sup>2</sup>	lb
*** 120' ***			ft						
AIR -32 B2A/B66AA w/ Mount Pipe	A	From Centroid-Fa ce	4.00 7.000 0.000	30.000	120.00	No Ice 1/2" Ice 1" Ice	6.75 7.20 7.65	6.07 6.87 7.58	153.07 214.04 281.89
AIR -32 B2A/B66AA w/ Mount Pipe	В	From Centroid-Fa	4.00 -7.000 0.000	30.000	120.00	No Ice 1/2" Ice 1" Ice	6.75 7.20 7.65	6.07 6.87 7.58	153.07 214.04 281.89
AIR -32 B2A/B66AA w/ Mount Pipe	C	From Centroid-Fa	4.00 -7.000 0.000	30.000	120.00	No Ice 1/2" Ice 1" Ice	7.03 6.75 7.20 7.65	6.07 6.87 7.58	153.07 214.04 281.89
KRY 112 144/1	A	From Centroid-Fa	4.00 2.500 0.000	30.000	120.00	No Ice 1/2" Ice 1" Ice	0.35 0.43 0.51	0.16 0.22 0.28	11.02 14.12 18.44
KRY 112 144/1	В	From Centroid-Fa	4.00 2.500 0.000	30.000	120.00	No Ice 1/2" Ice 1" Ice	0.35 0.43 0.51	0.16 0.22 0.28	11.02 14.12 18.44
KRY 112 144/1	С	From Centroid-Fa ce	4.00 7.000 0.000	30.000	120.00	No Ice 1/2" Ice 1" Ice	0.35 0.43 0.51	0.16 0.22 0.28	11.02 14.12 18.44
APXVAARR24_43-U-NA20 w/ Mount Pipe	A	From Centroid-Fa	4.00 -7.000 0.000	30.000	120.00	No Ice 1/2" Ice 1" Ice	20.48 21.23 21.99	11.02 12.55 14.10	160.82 297.10 444.18
APXVAARR24_43-U-NA20 w/ Mount Pipe	В	From Centroid-Fa	4.00 7.000	30.000	120.00	No Ice 1/2" Ice	20.48 21.23	11.02 12.55	160.82 297.10

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Client	Crown Castle	Designed by AAS

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Vert ft ft ft	o	ft		ft <sup>2</sup>	ft <sup>2</sup>	lb
		ce	0.000			1" Ice	21.99	14.10	444.18
APXVAARR24_43-U-NA20	C	From	4.00	30.000	120.00	No Ice	20.48	11.02	160.82
w/ Mount Pipe		Centroid-Fa	2.500			1/2" Ice	21.23	12.55	297.10
		ce	0.000			1" Ice	21.99	14.10	444.18
AIR 3246 B66 w/ Mount Pipe	Α	From	4.00	30.000	120.00	No Ice	8.18	6.56	201.32
		Centroid-Fa	2.500			1/2" Ice	8.66	7.39	271.57
AIR 3246 B66 w/ Mount Pipe	В	ce From	0.000 4.00	30.000	120.00	1" Ice No Ice	9.12 8.18	8.13 6.56	349.05 201.32
AIR 3240 Boo w/ Mount Fipe	ь	Centroid-Fa	2.500	30.000	120.00	1/2" Ice	8.66	7.39	271.57
		ce centroid-ra	0.000			1" Ice	9.12	8.13	349.05
AIR 3246 B66 w/ Mount Pipe	C	From	4.00	30.000	120.00	No Ice	8.18	6.56	201.32
THE 32 TO BOO WI WOULD TIPE	Č	Centroid-Fa	7.000	50.000	120.00	1/2" Ice	8.66	7.39	271.57
		ce	0.000			1" Ice	9.12	8.13	349.05
RADIO 4449 B12/B71	Α	From	4.00	30.000	120.00	No Ice	1.65	1.30	75.00
		Centroid-Fa	-7.000			1/2" Ice	1.81	1.44	92.20
		ce	0.000			1" Ice	1.98	1.60	112.11
RADIO 4449 B12/B71	В	From	4.00	30.000	120.00	No Ice	1.65	1.30	75.00
		Centroid-Fa	7.000			1/2" Ice	1.81	1.44	92.20
		ce	0.000			1" Ice	1.98	1.60	112.11
RADIO 4449 B12/B71	C	From	4.00	30.000	120.00	No Ice	1.65	1.30	75.00
		Centroid-Fa	2.500			1/2" Ice	1.81	1.44	92.20
		ce	0.000			1" Ice	1.98	1.60	112.11
KRY 112 144/2	Α	From	4.00	30.000	120.00	No Ice	0.48	0.23	9.70
		Centroid-Fa	-7.000			1/2" Ice	0.57	0.30	13.78
WDW 110 144/0	ъ	ce	0.000	20.000	120.00	1" Ice	0.66	0.38	19.25
KRY 112 144/2	В	From	4.00	30.000	120.00	No Ice	0.48	0.23	9.70
		Centroid-Fa	-7.000			1/2" Ice	0.57	0.30	13.78
KRY 112 144/2	C	ce From	0.000 4.00	30.000	120.00	1" Ice No Ice	0.66 0.48	0.38 0.23	19.25 9.70
KK1 112 144/2	C	Centroid-Fa	-7.000	30.000	120.00	1/2" Ice	0.48	0.23	13.78
		ce centroid-ra	0.000			1" Ice	0.66	0.38	19.25
2.4" Dia x 6-ft Mount Pipe	A	From	4.00	0.000	120.00	No Ice	1.43	1.43	21.96
2.4 Dia x o it Would i ipe	71	Centroid-Fa	-2.500	0.000	120.00	1/2" Ice	1.93	1.93	32.81
		ce	0.000			1" Ice	2.30	2.30	47.71
2.4" Dia x 6-ft Mount Pipe	В	From	4.00	0.000	120.00	No Ice	1.43	1.43	21.96
		Centroid-Fa	-2.500			1/2" Ice	1.93	1.93	32.81
		ce	0.000			1" Ice	2.30	2.30	47.71
2.4" Dia x 6-ft Mount Pipe	C	From	4.00	0.000	120.00	No Ice	1.43	1.43	21.96
		Centroid-Fa	-2.500			1/2" Ice	1.93	1.93	32.81
		ce	0.000			1" Ice	2.30	2.30	47.71
2.4" Dia x 8.5-ft Mount Pipe	В	From Leg	1.00	0.000	120.00	No Ice	2.02	2.02	25.93
			0.000			1/2" Ice	2.90	2.90	41.14
	_		3.000			1" Ice	3.71	3.71	61.95
Platform Mount [LP 404-1]	C	None		0.000	120.00	No Ice	32.79	32.79	2043.00
(w/ Handrail Kit)						1/2" Ice	44.63	44.63	2475.48
ቀቀቀ <b>1</b> 1 <i>ሮ</i> ! ቀቀቀ						1" Ice	56.47	56.47	2907.96
*** 115' ***	C	Erom I aa	0.50	0.000	115.00	No Ice	1.42	1 42	21.06
2.4" Dia x 6-ft Mount Pipe	C	From Leg	0.50 0.000	0.000	115.00	No Ice 1/2" Ice	1.43 1.93	1.43 1.93	21.96 32.81
			0.000			1" Ice	2.30	2.30	47.71
Side Arm Mount [SO 102-3]	C	None	0.000	0.000	115.00	No Ice	3.00	3.00	81.00
5.de / Hill Moulit [50 102-5]	C	TOHE		0.000	113.00	1/2" Ice	3.48	3.48	111.00
						1" Ice	3.96	3.96	141.00
*** 110' ***						- 100	0	,0	- /1.00
7770.00 w/ Mount Pipe	Α	From	4.00	30.000	110.00	No Ice	5.75	4.25	55.38
1		Centroid-Fa	-6.000			1/2" Ice	6.18	5.01	102.81
		ce	0.000			1" Ice	6.61	5.71	156.64

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Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_AA_A$ Front	$C_A A_A$ Side	Weigh
	Leg		Lateral Vert						
			ft	0	ft		$ft^2$	ft <sup>2</sup>	lb
			ft ft						
7770.00 w/ Mount Pipe	В	From	4.00	20.000	110.00	No Ice	5.75	4.25	55.38
*		Centroid-Fa	-6.000			1/2" Ice	6.18	5.01	102.8
	_	ce	0.000			1" Ice	6.61	5.71	156.6
7770.00 w/ Mount Pipe	C	From	4.00	30.000	110.00	No Ice	5.75	4.25	55.38
		Centroid-Fa	-6.000 0.000			1/2" Ice 1" Ice	6.18	5.01 5.71	102.8
AM-X-CD-16-65-00T-RET	A	ce From	4.00	30.000	110.00	No Ice	6.61 8.26	6.30	156.6 74.05
w/ Mount Pipe	А	Centroid-Fa	-2.000	30.000	110.00	1/2" Ice	8.82	7.48	139.0
w/ Mount i ipe		ce	0.000			1" Ice	9.35	8.37	211.9
AM-X-CD-16-65-00T-RET	C	From	4.00	30.000	110.00	No Ice	8.26	6.30	74.05
w/ Mount Pipe		Centroid-Fa	-2.000			1/2" Ice	8.82	7.48	139.0
•		ce	0.000			1" Ice	9.35	8.37	211.9
QS66512-3 w/ Mount Pipe	A	From	4.00	30.000	110.00	No Ice	8.37	8.46	130.5
		Centroid-Fa	6.000			1/2" Ice	8.93	9.66	206.2
		ce	0.000			1" Ice	9.46	10.55	290.0
QS66512-3 w/ Mount Pipe	C	From	4.00	30.000	110.00	No Ice	8.37	8.46	130.5
		Centroid-Fa	6.000			1/2" Ice	8.93	9.66	206.2
SBNH-1D6565C w/ Mount	В	ce From	0.000 4.00	20.000	110.00	1" Ice No Ice	9.46 11.69	10.55 9.85	290.0 99.25
Pipe	ь	Centroid-Fa	-2.000	20.000	110.00	1/2" Ice	12.42	11.38	189.0
Tipe		ce centroid-i a	0.000			1" Ice	13.16	12.94	288.8
ΓPA-65R-LCUUUU-H8 w/	В	From	4.00	20.000	110.00	No Ice	13.54	10.96	114.4
Mount Pipe		Centroid-Fa	6.000			1/2" Ice	14.24	12.49	217.6
1		ce	0.000			1" Ice	14.95	14.04	330.9
(2) LGP21401	A	From	4.00	30.000	110.00	No Ice	1.10	0.21	14.10
		Centroid-Fa	-6.000			1/2" Ice	1.24	0.27	21.20
		ce	0.000			1" Ice	1.38	0.35	30.32
(2) LGP21401	В	From	4.00	20.000	110.00	No Ice	1.10	0.21	14.10
		Centroid-Fa	-6.000			1/2" Ice	1.24	0.27	21.20
(2) I CD21401	C	ce	0.000 4.00	20,000	110.00	1" Ice No Ice	1.38 1.10	0.35 0.21	30.32
(2) LGP21401	C	From Centroid-Fa	-6.000	30.000	110.00	1/2" Ice	1.10	0.21	14.10 21.20
		ce centroid-ra	0.000			1" Ice	1.38	0.27	30.32
(2) TPX-070821	A	From	4.00	30.000	110.00	No Ice	0.47	0.10	7.50
(2) 1111 0, 0021		Centroid-Fa	6.000	20.000	110.00	1/2" Ice	0.56	0.15	10.95
		ce	0.000			1" Ice	0.66	0.20	15.73
(2) TPX-070821	В	From	4.00	20.000	110.00	No Ice	0.47	0.10	7.50
		Centroid-Fa	6.000			1/2" Ice	0.56	0.15	10.93
		ce	0.000			1" Ice	0.66	0.20	15.73
(2) TPX-070821	C	From	4.00	30.000	110.00	No Ice	0.47	0.10	7.50
		Centroid-Fa	6.000			1/2" Ice	0.56	0.15	10.9
(2) 7020 00		ce	0.000	20,000	110.00	1" Ice	0.66	0.20	15.73
(2) 7020.00	A	From Centroid-Fa	4.00 6.000	30.000	110.00	No Ice 1/2" Ice	0.10 0.15	0.17 0.24	2.20 5.16
		ce ce	0.000			1" Ice	0.13	0.24	9.33
(2) 7020.00	В	From	4.00	20.000	110.00	No Ice	0.10	0.17	2.20
(2) 7020.00	ь	Centroid-Fa	6.000	20.000	110.00	1/2" Ice	0.15	0.24	5.16
		ce	0.000			1" Ice	0.20	0.31	9.33
(2) 7020.00	C	From	4.00	30.000	110.00	No Ice	0.10	0.17	2.20
• •		Centroid-Fa	6.000			1/2" Ice	0.15	0.24	5.16
		ce	0.000			1" Ice	0.20	0.31	9.33
RRUS 32	Α	From	4.00	30.000	110.00	No Ice	2.86	1.78	55.12
		Centroid-Fa	2.000			1/2" Ice	3.08	1.97	77.39
DDIIG 22	-	ce	0.000	20.000	110.00	1" Ice	3.32	2.17	102.9
RRUS 32	В	From	4.00	20.000	110.00	No Ice	2.86	1.78	55.12
		Centroid-Fa	2.000			1/2" Ice	3.08	1.97	77.39

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Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_AA_A$ Front	$C_AA_A$ Side	Weigh
	Leg		Vert						
			ft ft	٥	ft		ft <sup>2</sup>	ft <sup>2</sup>	lb
DDIIG 22			ft	20.000	110.00	N. T	2.06	1.70	55.10
RRUS 32	C	From	4.00 2.000	30.000	110.00	No Ice	2.86	1.78	55.12
		Centroid-Fa ce	0.000			1/2" Ice 1" Ice	3.08 3.32	1.97 2.17	77.39 102.9
RRUS 32 B2	Α	From	4.00	30.000	110.00	No Ice	2.73	1.67	52.90
KK03 32 B2	А	Centroid-Fa	2.000	30.000	110.00	1/2" Ice	2.95	1.86	73.96
		ce	0.000			1" Ice	3.18	2.05	98.21
RRUS 32 B2	В	From	4.00	20.000	110.00	No Ice	2.73	1.67	52.90
14(05 02 52	2	Centroid-Fa	2.000	20.000	110.00	1/2" Ice	2.95	1.86	73.90
		ce	0.000			1" Ice	3.18	2.05	98.2
RRUS 32 B2	C	From	4.00	30.000	110.00	No Ice	2.73	1.67	52.90
		Centroid-Fa	2.000			1/2" Ice	2.95	1.86	73.90
		ce	0.000			1" Ice	3.18	2.05	98.21
RRUS 11	A	From	4.00	30.000	110.00	No Ice	2.79	1.19	50.70
		Centroid-Fa	-2.000			1/2" Ice	3.00	1.34	71.5
		ce	0.000			1" Ice	3.21	1.50	95.48
RRUS 11	В	From	4.00	20.000	110.00	No Ice	2.79	1.19	50.70
		Centroid-Fa	-2.000			1/2" Ice	3.00	1.34	71.5
		ce	0.000			1" Ice	3.21	1.50	95.48
RRUS 11	C	From	4.00	30.000	110.00	No Ice	2.79	1.19	50.70
		Centroid-Fa	-2.000			1/2" Ice	3.00	1.34	71.5
1001002		ce	0.000	20.000	110.00	1" Ice	3.21	1.50	95.48
1001983	A	From	4.00	30.000	110.00	No Ice	0.18	0.08	2.00
		Centroid-Fa	6.000			1/2" Ice 1" Ice	0.23 0.30	0.13	3.59
1001983	В	ce From	0.000 4.00	20.000	110.00	No Ice	0.30	0.18 0.08	6.10 2.00
1001983	ь	Centroid-Fa	6.000	20.000	110.00	1/2" Ice	0.18	0.08	3.59
		ce centroid-ra	0.000			1" Ice	0.23	0.13	6.10
1001983	C	From	4.00	30.000	110.00	No Ice	0.18	0.08	2.00
1001703	C	Centroid-Fa	6.000	50.000	110.00	1/2" Ice	0.23	0.13	3.59
		ce	0.000			1" Ice	0.30	0.18	6.10
DC6-48-60-18-8F	В	From	4.00	20.000	110.00	No Ice	1.21	1.21	32.80
		Centroid-Fa	6.000			1/2" Ice	1.89	1.89	54.70
		ce	0.000			1" Ice	2.11	2.11	79.58
DC6-48-60-18-8F	В	From	4.00	20.000	110.00	No Ice	1.21	1.21	32.80
		Centroid-Fa	-6.000			1/2" Ice	1.89	1.89	54.70
		ce	0.000			1" Ice	2.11	2.11	79.5
.4" Dia x 6-ft Mount Pipe	A	From	4.00	0.000	110.00	No Ice	1.43	1.43	21.90
		Centroid-Fa	2.000			1/2" Ice	1.93	1.93	32.8
411 D' ( C 3 4 . D'	ъ.	ce	0.000	0.000	110.00	1" Ice	2.30	2.30	47.7
.4" Dia x 6-ft Mount Pipe	В	From	4.00	0.000	110.00	No Ice	1.43	1.43	21.90
		Centroid-Fa	2.000			1/2" Ice 1" Ice	1.93	1.93	32.8
.4" Dia x 6-ft Mount Pipe	С	ce From	0.000 4.00	0.000	110.00	No Ice	2.30 1.43	2.30 1.43	47.7 21.9
.4 Dia x 0-it Mount Fipe	C	Centroid-Fa	2.000	0.000	110.00	1/2" Ice	1.43	1.43	32.8
		ce ce	0.000			1" Ice	2.30	2.30	47.7
.4" Dia x 6-ft Mount Pipe	A	From	4.00	0.000	110.00	No Ice	0.00	1.43	21.90
.4 Dia x o it Would Tipe	7.1	Centroid-Fa	-6.000	0.000	110.00	1/2" Ice	0.00	1.93	37.8
		ce	0.000			1" Ice	0.00	2.31	55.50
.4" Dia x 6-ft Mount Pipe	В	From	4.00	0.000	110.00	No Ice	0.00	1.43	21.90
T-		Centroid-Fa	-6.000			1/2" Ice	0.00	1.93	37.8
		ce	0.000			1" Ice	0.00	2.31	55.50
.4" Dia x 6-ft Mount Pipe	C	From	4.00	0.000	110.00	No Ice	0.00	1.43	21.90
•		Centroid-Fa	-6.000			1/2" Ice	0.00	1.93	37.8
		ce	0.000			1" Ice	0.00	2.31	55.50
latform Mount [LP 712-1]	C	None		0.000	110.00	No Ice	24.53	24.53	1335.0
						1/2" Ice	29.94	29.94	1645.5
						1" Ice	35.35	35.35	1956.

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Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Vert ft ft ft	0	ft		ft²	ft <sup>2</sup>	lb
Miscellaneous [NA 507-1]	С	None	J.	0.000	110.00	No Ice 1/2" Ice 1" Ice	4.80 6.70 8.60	4.80 6.70 8.60	245.00 294.00 343.00
**100**						1 100	0.00	0.00	2.2.00
BXA-80063-4BF-EDIN-X w/ Mount Pipe	A	From Centroid-Fa	4.00 7.000	0.000	100.00	No Ice 1/2" Ice	4.62 4.99	3.47 4.04	29.82 70.14
000/0 /PE /	_	ce	0.000	0.000	100.00	1" Ice	5.36	4.63	116.05
BXA-80063-4BF-EDIN-X w/ Mount Pipe	В	From Centroid-Fa ce	4.00 7.000 0.000	0.000	100.00	No Ice 1/2" Ice 1" Ice	4.62 4.99 5.36	3.47 4.04 4.63	29.82 70.14 116.05
BXA-80063-4BF-EDIN-X w/	С	From	4.00	0.000	100.00	No Ice	4.62	3.47	29.82
Mount Pipe	C	Centroid-Fa	7.000 0.000	0.000	100.00	1/2" Ice 1" Ice	4.99 5.36	4.04 4.63	70.14 116.05
BXA-70063-6CF-EDIN-0 w/	A	From	4.00	0.000	100.00	No Ice	7.81	5.80	42.25
Mount Pipe		Centroid-Fa ce	-2.500 0.000			1/2" Ice 1" Ice	8.36 8.87	6.95 7.82	103.01 171.49
LNX-6514DS-T4M w/	В	From	4.00	0.000	100.00	No Ice	8.44	7.42	79.33
Mount Pipe		Centroid-Fa	-2.500			1/2" Ice	8.98	8.45	151.64
TANK (51 IDG TIA) (		ce	0.000	0.000	100.00	1" Ice	9.51	9.34	232.88
LNX-6514DS-T4M w/	C	From Centroid-Fa	4.00	0.000	100.00	No Ice 1/2" Ice	8.44 8.98	7.42	79.33 151.6
Mount Pipe		ce ce	-2.500 0.000			1" Ice	8.98 9.51	8.45 9.34	232.88
DB-T1-6Z-8AB-0Z	C	From	4.00	0.000	100.00	No Ice	4.80	2.00	44.00
		Centroid-Fa	2.500			1/2" Ice	5.07	2.19	80.13
		ce	0.000			1" Ice	5.35	2.39	120.22
(2) SBNHH-1D65B w/	A	From	4.00	0.000	100.00	No Ice	8.29	7.00	76.26
Mount Pipe		Centroid-Fa	-2.500			1/2" Ice	8.85	8.19	144.6
(2) SBNHH-1D65B w/	В	ce From	0.000 4.00	0.000	100.00	1" Ice No Ice	9.37 8.29	9.08 7.00	221.00 76.26
Mount Pipe	ь	Centroid-Fa	-2.500	0.000	100.00	1/2" Ice	8.85	8.19	144.6
1110 <b>u</b> 111 1 1 pc		ce	0.000			1" Ice	9.37	9.08	221.00
(2) SBNHH-1D65B w/	C	From	4.00	0.000	100.00	No Ice	8.29	7.00	76.26
Mount Pipe		Centroid-Fa	-2.500			1/2" Ice	8.85	8.19	144.68
DD112 (0.700		ce	0.000	0.000	100.00	1" Ice	9.37	9.08	221.00
RRH2x60-700	A	From Centroid-Fa	4.00 -2.500	0.000	100.00	No Ice 1/2" Ice	3.50 3.76	1.82 2.05	60.00 82.72
		ce ce	0.000			1" Ice	4.03	2.03	109.0
RRH2x60-700	В	From	4.00	0.000	100.00	No Ice	3.50	1.82	60.00
		Centroid-Fa	-2.500			1/2" Ice	3.76	2.05	82.72
		ce	0.000			1" Ice	4.03	2.29	109.0
RRH2x60-700	C	From	4.00	0.000	100.00	No Ice	3.50	1.82	60.00
		Centroid-Fa	-2.500			1/2" Ice 1" Ice	3.76	2.05 2.29	82.72
RRH2x60-AWS	A	ce From	0.000 4.00	0.000	100.00	No Ice	4.03 3.50	1.82	109.00 60.00
RRIIZX00 AWS	71	Centroid-Fa	2.500	0.000	100.00	1/2" Ice	3.76	2.05	82.72
		ce	0.000			1" Ice	4.03	2.29	109.0
RRH2x60-AWS	В	From	4.00	0.000	100.00	No Ice	3.50	1.82	60.00
		Centroid-Fa	2.500			1/2" Ice	3.76	2.05	82.72
DDIIOCO AMO	C	ce	0.000	0.000	100.00	1" Ice	4.03	2.29	109.00
RRH2x60-AWS	C	From Centroid-Fa	4.00 2.500	0.000	100.00	No Ice 1/2" Ice	3.50 3.76	1.82 2.05	60.00 82.72
		ce ce	0.000			1" Ice	4.03	2.03	109.0
RRH2X60-PCS	A	From	4.00	0.000	100.00	No Ice	2.20	1.72	55.00
		Centroid-Fa	-7.000			1/2" Ice	2.39	1.90	75.35
		ce	0.000			1" Ice	2.59	2.09	98.71
RRH2X60-PCS	В	From	4.00	0.000	100.00	No Ice	2.20	1.72	55.00
		Centroid-Fa	-7.000			1/2" Ice	2.39	1.90	75.35

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Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
	Ü		Vert ft ft ft	o	ft		ft²	ft <sup>2</sup>	lb
		ce	0.000			1" Ice	2.59	2.09	98.71
RRH2X60-PCS	C	From Centroid-Fa	4.00 -7.000	0.000	100.00	No Ice 1/2" Ice	2.20 2.39	1.72 1.90	55.00 75.35
		ce	0.000			1" Ice	2.59	2.09	98.71
DB-T1-6Z-8AB-0Z	A	From	4.00	0.000	100.00	No Ice	4.80	2.00	44.00
		Centroid-Fa	-2.500			1/2" Ice	5.07	2.19	80.13
DI 10 15 15 100 11		ce	0.000	0.000	100.00	1" Ice	5.35	2.39	120.22
Platform Mount [LP 403-1]	C	None		0.000	100.00	No Ice	18.85	18.85	1500.00
						1/2" Ice	24.30	24.30	1796.56
*** 90' ***						1" Ice	29.75	29.75	2093.12
742 213 w/ Mount Pipe	Α	From Leg	0.50	30.000	90.00	No Ice	5.37	4.62	48.92
7-12 213 W/ Would Tipe	7.	Trom Leg	0.000	50.000	70.00	1/2" Ice	5.95	6.00	93.54
			0.000			1" Ice	6.50	6.98	145.83
742 213 w/ Mount Pipe	В	From Leg	0.50	0.000	90.00	No Ice	5.37	4.62	48.92
			0.000			1/2" Ice	5.95	6.00	93.54
			0.000			1" Ice	6.50	6.98	145.83
742 213 w/ Mount Pipe	C	From Leg	0.50	-10.000	90.00	No Ice	5.37	4.62	48.92
			0.000			1/2" Ice	5.95	6.00	93.54
			0.000			1" Ice	6.50	6.98	145.83
2'x3' Ice Shield	C	From Leg	0.50	-10.000	95.00	No Ice	0.72	1.18	72.00
			0.000			1/2" Ice	0.99	1.61	132.00
			0.000			1" Ice	1.26	2.04	192.00
2'x3' Ice Shield	C	From Leg	0.50	-10.000	97.00	No Ice	0.72	1.18	72.00
			0.000			1/2" Ice	0.99	1.61	132.00
*** 80' ***			0.000			1" Ice	1.26	2.04	192.00
LLPX310R w/ Mount Pipe	Α	From Leg	1.00	30.000	80.00	No Ice	4.45	2.87	43.87
LLI X310K w/ Would 1 lpc	А	110III Leg	-2.000	30.000	80.00	1/2" Ice	4.79	3.40	80.95
			1.000			1" Ice	5.13	3.94	123.32
LLPX310R w/ Mount Pipe	В	From Leg	1.00	30.000	80.00	No Ice	4.45	2.87	43.87
ZZZ TZG TOTE W MIGUIN T IPE	2	Trom 20g	-2.000	20.000	00.00	1/2" Ice	4.79	3.40	80.95
			1.000			1" Ice	5.13	3.94	123.32
LLPX310R w/ Mount Pipe	C	From Leg	1.00	30.000	80.00	No Ice	4.45	2.87	43.87
		Č	-2.000			1/2" Ice	4.79	3.40	80.95
			1.000			1" Ice	5.13	3.94	123.32
WIMAX DAP HEAD	A	From Leg	1.00	30.000	80.00	No Ice	1.55	0.68	33.00
			-2.000			1/2" Ice	1.70	0.80	44.58
			1.000			1" Ice	1.87	0.92	58.46
WIMAX DAP HEAD	В	From Leg	1.00	30.000	80.00	No Ice	1.55	0.68	33.00
			-2.000			1/2" Ice	1.70	0.80	44.58
			1.000			1" Ice	1.87	0.92	58.46
WIMAX DAP HEAD	C	From Leg	1.00	30.000	80.00	No Ice	1.55	0.68	33.00
			-2.000			1/2" Ice	1.70	0.80	44.58
a			1.000	20.000	00.00	1" Ice	1.87	0.92	58.46
CW JUNCTION BOX	Α	From Leg	0.50	30.000	80.00	No Ice	1.20	0.60	0.00
			0.000			1/2" Ice 1" Ice	1.34	0.70	10.34
2.4" Dia x 6-ft Mount Pipe	Α	From Leg	3.000 1.00	0.000	80.00	No Ice	1.48 1.43	0.81 1.43	22.81 21.96
2.4 Dia x 0-11 Mount Pipe	А	rioni Leg	2.000	0.000	00.00	1/2" Ice	1.43	1.43	32.81
			0.000			1/2 Ice 1" Ice	2.30	2.30	32.81 47.71
2.4" Dia x 6-ft Mount Pipe	В	From Leg	1.00	0.000	80.00	No Ice	1.43	1.43	21.96
2.4 Dia x 0-it Would i ipe	ь	1 Tom Leg	2.000	0.000	00.00	1/2" Ice	1.43	1.43	32.81
			0.000			1" Ice	2.30	2.30	47.71
2.4" Dia x 6-ft Mount Pipe	C	From Leg	1.00	0.000	80.00	No Ice	1.43	1.43	21.96
2 Dia A O It Mount I ipc	C	Trom Log	2.000	0.000	00.00	1/2" Ice	1.93	1.93	32.81
			2.000			1,2 100	1.//	1.//	J2.01

# Tower Engineering

Professionals 326 Tryon Road Raleigh, NC 27603 Phone: (919) 661-6351 FAX: (919) 661-6350

Job	West Hartford/I-84/X43 (BU 829013)	<b>Page</b> 11 of 19
Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	$C_AA_A$ Side	Weight
			ft ft ft	0	ft		ft <sup>2</sup>	ft <sup>2</sup>	lb
Side Arm Mount [SO 101-3]	С	None	J.	0.000	80.00	No Ice 1/2" Ice 1" Ice	7.50 8.90 10.30	7.50 8.90 10.30	252.00 333.00 414.00
***						1 100	10.50	10.50	111.00

					Dis	shes					
Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				Vert ft	0	0	ft	ft		ft <sup>2</sup>	lb
*** 115' ***											
VHLP2-18	C	Paraboloid	From	1.00	0.000		115.00	2.00	No Ice	3.14	31.00
		w/Shroud (HP)	Leg	0.000					1/2" Ice	3.41	49.00
				0.000					1" Ice	3.68	66.00
*** 80' ***											
VHLP2-23	A	Paraboloid	From	1.00	-30.000		80.00	2.18	No Ice	3.73	30.00
		w/Shroud (HP)	Leg	2.000					1/2" Ice	4.02	50.00
				3.000					1" Ice	4.31	70.00
***											

### **Load Combinations**

Comb.	Description
No.	· · · · · · · · · · · · · · · · · · ·
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice

Tower Engineering Professionals 326 Tryon Road Raleigh, NC 27603 Phone: (919) 661-6351 FAX: (919) 661-6350

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Comb.	Description
No.	
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

### **Maximum Member Forces**

Section No.	Elevation ft	Component Type	Condition	Gov. Load	Axial	Major Axis Moment	Minor Axis Moment
1,0.	J	1,770		Comb.	lb	lb-ft	lb-ft
L1	119.083 - 101.083	Pole	Max Tension	26	0.00	-0.03	0.45
			Max. Compression	26	-27572.54	-478.06	-6159.50
			Max. Mx	20	-8931.82	170584.38	-1460.12
			Max. My	14	-8945.14	1409.46	-170299.56
			Max. Vy	8	15310.97	-170296.78	941.71
			Max. Vx	2	-15168.97	-1567.91	168593.14
			Max. Torque	22			9402.19
L2	101.083 - 66.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-54632.25	1083.64	-7413.96
			Max. Mx	8	-18889.43	-930676.17	1921.81
			Max. My	14	-18904.59	4141.51	-926590.21
			Max. Vy	8	25906.70	-930676.17	1921.81
			Max. Vx	14	25749.56	4141.51	-926590.21
			Max. Torque	22			10082.86
L3	66.5 - 32.8333	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-70976.54	4.18	-7619.83
			Max. Mx	8	-27587.87	-1826420.6 1	917.58
			Max. My	14	-27590.01	4911.76	-1819347.9 0
			Max. Vy	8	28600.06	-1826420.6 1	917.58
			Max. Vx	14	28607.51	4911.76	-1819347.9 0

### Tower Engineering Professionals

326 Tryon Road Raleigh, NC 27603 Phone: (919) 661-6351 FAX: (919) 661-6350

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Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

Section No.	Elevation ft	Component Type	Condition	Gov. Load	Axial	Major Axis Moment	Minor Axis Moment
	J	71		Comb.	lb	lb-ft	lb-ft
			Max. Torque	22			9468.20
L4	32.8333 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-91494.80	-1306.30	-7471.21
			Max. Mx	8	-39470.62	-2947865.6	-64.55
						9	
			Max. My	14	-39470.59	5696.45	-2943216.9 5
			Max. Vy	8	31085.57	-2947865.6 9	-64.55
			Max. Vx	14	31178.05	5696.45	-2943216.9 5
			Max. Torque	22			9444.44

### **Maximum Reactions**

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, Z
		Load	lb	lb	lb
		Comb.			
Pole	Max. Vert	33	91494.80	-11.43	-6774.82
	Max. H <sub>x</sub>	20	39493.42	31005.24	-2.83
	Max. H <sub>z</sub>	2	39493.42	-66.65	31112.85
	Max. M <sub>x</sub>	2	2938326.03	-66.65	31112.85
	Max. M <sub>z</sub>	8	2947865.69	-31056.60	-28.14
	Max. Torsion	22	9435.35	26609.55	15331.90
	Min. Vert	23	29620.07	26609.55	15331.90
	Min. H <sub>x</sub>	8	39493.42	-31056.60	-28.14
	Min. H <sub>z</sub>	14	39493.42	13.46	-31149.12
	Min. M <sub>x</sub>	14	-2943216.95	13.46	-31149.12
	Min. M <sub>z</sub>	20	-2944625.06	31005.24	-2.83
	Min. Torsion	10	-9286.96	-26669.69	-15337.39

## **Tower Mast Reaction Summary**

Load	Vertical	$Shear_x$	$Shear_z$	Overturning	Overturning	Torque
Combination				Moment, $M_x$	Moment, $M_z$	
	lb	lb	lb	lb-ft	lb-ft	lb-ft
Dead Only	32911.18	-0.00	0.00	829.57	1015.40	-0.00
1.2 Dead+1.6 Wind 0 deg - No	39493.42	66.65	-31112.85	-2938326.03	-9104.25	-3916.03
Ice						
0.9 Dead+1.6 Wind 0 deg - No	29620.07	66.65	-31112.85	-2910427.56	-9302.02	-3911.07
Ice						
1.2 Dead+1.6 Wind 30 deg - No	39493.42	15399.83	-26643.38	-2530574.93	-1465781.66	964.68
Ice						
0.9 Dead+1.6 Wind 30 deg - No	29620.07	15399.83	-26643.38	-2506516.62	-1451985.02	959.71
Ice						
1.2 Dead+1.6 Wind 60 deg - No	39493.42	26647.37	-15408.46	-1464371.28	-2533506.25	5488.67
Ice						
0.9 Dead+1.6 Wind 60 deg - No	29620.07	26647.37	-15408.46	-1450545.32	-2509456.40	5475.04
Ice						
1.2 Dead+1.6 Wind 90 deg - No	39493.42	31056.60	28.14	62.69	-2947865.69	8398.17
Ice						
0.9 Dead+1.6 Wind 90 deg - No	29620.07	31056.60	28.14	-160.30	-2919873.65	8379.44
Ice						

Job		Page
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Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

Load Combination	Vertical	Shearx	Shear <sub>z</sub>	Overturning Moment, M <sub>x</sub>	Overturning Moment, M <sub>z</sub>	Torque
	lb	lb	lb	lb-ft	lb-ft	lb-ft
1.2 Dead+1.6 Wind 120 deg -	39493.42	26669.69	15337.39	1454039.50	-2533922.75	9286.96
No Ice 0.9 Dead+1.6 Wind 120 deg - No Ice	29620.07	26669.69	15337.39	1439838.83	-2509867.90	9268.37
1.2 Dead+1.6 Wind 150 deg - No Ice	39493.42	15355.79	26633.95	2529606.68	-1456222.56	7689.85
0.9 Dead+1.6 Wind 150 deg - No Ice	29620.07	15355.79	26633.95	2505044.05	-1442539.85	7676.38
1.2 Dead+1.6 Wind 180 deg - No Ice	39493.42	-13.46	31149.12	2943216.95	5695.61	3799.30
0.9 Dead+1.6 Wind 180 deg - No Ice	29620.07	-13.46	31149.12	2914741.53	5306.75	3794.43
1.2 Dead+1.6 Wind 210 deg - No Ice	39493.42	-15335.86	26644.77	2531803.51	1461798.00	-1129.55
0.9 Dead+1.6 Wind 210 deg - No Ice	29620.07	-15335.86	26644.77	2507205.97	1447397.32	-1124.56
1.2 Dead+1.6 Wind 240 deg - No Ice	39493.42	-26632.24	15353.55	1461017.72	2533608.98	-5373.41
0.9 Dead+1.6 Wind 240 deg - No Ice	29620.07	-26632.24	15353.55	1446704.16	2508916.22	-5359.83
1.2 Dead+1.6 Wind 270 deg - No Ice	39493.42	-31005.24	2.83	4132.83	2944625.06	-8474.09
0.9 Dead+1.6 Wind 270 deg - No Ice	29620.07	-31005.24	2.83	3820.56	2916030.20	-8455.51
1.2 Dead+1.6 Wind 300 deg - No Ice	39493.42	-26609.55	-15331.90	-1452595.76	2530308.50	-9435.35
0.9 Dead+1.6 Wind 300 deg - No Ice 1.2 Dead+1.6 Wind 330 deg -	29620.07 39493.42	-26609.55 -15364.52	-15331.90 -26576.96	-1438905.09 -2522072.21	2505668.92 1460477.01	-9416.87 -7819.65
No Ice 0.9 Dead+1.6 Wind 330 deg -	29620.07	-15364.52	-26576.96	-2498100.56	1446136.42	-7819.03
No Ice 1.2 Dead+1.0 Ice+1.0 Temp	91494.80	-0.00	0.03	7471.21	-1306.30	-0.81
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	91494.80	-3.66	-6769.67	-635181.67	-1469.68	-327.05
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	91494.80	2957.95	-5142.55	-503319.53	-295622.34	328.18
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	91494.80	5132.88	-2964.99	-287089.75	-511560.11	881.78
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	91494.80	6124.27	17.37	8933.04	-608383.28	1180.78
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	91494.80	5149.65	2977.91	302969.15	-513114.07	1192.40
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	91494.80	2974.77	5154.71	519582.96	-296685.06	887.89
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	91494.80	11.43	6774.82	650841.09	-2106.49	310.42
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	91494.80	-2948.67	5142.63	518406.48	291959.03	-352.41
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	91494.80	-5130.56	2957.07	301499.85	508506.82	-866.76
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	91494.80	-6116.75	-13.00	6630.30	604823.00	-1194.03
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 330	91494.80 91494.80	-5140.94 -2976.16	-2977.25 -5146.48	-287836.37 -503492.90	509517.48 294334.55	-1216.32 -907.93
deg+1.0 Ice+1.0 Temp Dead+Wind 0 deg - Service	32911.18	14.26	-6656.93	-624825.76	-1146.38	-907.93 -845.04
Dead+Wind 30 deg - Service	32911.18	3294.96	-5700.64	-538020.78	-311228.03	208.23
Dead+Wind 60 deg - Service	32911.18	5701.50	-3296.81	-311057.88	-538513.53	1184.38
Dead+Wind 90 deg - Service	32911.18	6644.90	6.02	676.11	-626724.85	1812.52

# Tower Engineering

Professionals 326 Tryon Road Raleigh, NC 27603 Phone: (919) 661-6351 FAX: (919) 661-6350

Job	West Hartford/I-84/X43 (BU 829013)	<b>Page</b> 15 of 19
Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

Load Combination	Vertical	$Shear_x$	$Shear_z$	Overturning Moment, $M_x$	Overturning Moment, $M_z$	Torque
	lb	lb	lb	lb-ft	lb-ft	lb-ft
Dead+Wind 120 deg - Service	32911.18	5706.27	3281.60	310173.81	-538588.10	2004.26
Dead+Wind 150 deg - Service	32911.18	3285.54	5698.62	539113.23	-309182.65	1660.69
Dead+Wind 180 deg - Service	32911.18	-2.88	6664.70	627165.72	1999.74	821.45
Dead+Wind 210 deg - Service	32911.18	-3281.27	5700.94	539579.59	311944.34	-242.95
Dead+Wind 240 deg - Service	32911.18	-5698.26	3285.06	311652.93	540094.33	-1159.89
Dead+Wind 270 deg - Service	32911.18	-6633.91	0.61	1538.37	627600.47	-1830.13
Dead+Wind 300 deg - Service	32911.18	-5693.40	-3280.43	-308545.24	539397.98	-2037.55
Dead+Wind 330 deg - Service	32911.18	-3287.41	-5686.43	-536200.10	311673.52	-1688.35

## **Solution Summary**

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		Sur	n of Applied Forces	5		Sum of Reaction	ıs	
1	Load		PY		PX	PY		% Error
2 66.65	Comb.							
3 66.65	1	0.00	-32911.18	0.00	0.00	32911.18	-0.00	0.000%
4 15399.83 39493.42 -26643.38 1-5399.83 39493.42 26643.38 0.000%   5 15399.83 -29620.07 -26643.38 1-5399.83 39493.42 15408.46 0.000%   6 26647.37 39493.42 -15408.46 -26647.37 39493.42 15408.46 0.000%   7 26647.37 -29620.07 -15408.46 -26647.37 39493.42 15408.46 0.000%   8 31056.60 -39493.42 28.14 -31056.60 39493.42 -28.14 0.000%   9 31056.60 -29620.07 28.14 -31056.60 29620.07 -28.14 0.000%   10 26669.69 -39493.42 15337.39 -26669.69 39493.42 -15337.39 0.000%   11 26669.69 -29620.07 15337.39 -26669.69 92620.07 -15337.39 0.000%   12 15355.79 -39493.42 5633.95 -15355.79 39493.42 -26633.95 0.000%   13 15355.79 -29620.07 26633.95 -15355.79 39493.42 -26633.95 0.000%   14 -15.46 -39493.42 31149.12 13.46 39493.42 -3663.95 0.000%   15 -15.46 -29620.07 13149.12 13.46 39493.42 -26644.77 0.000%   16 -15335.86 -39493.42 26644.77 15335.86 39493.42 -26644.77 0.000%   18 -26632.24 -39493.42 15353.55 26632.24 39493.42 -26644.77 0.000%   18 -26632.24 -39493.42 15333.55 26632.24 39493.42 -25833.55 0.000%   19 -26632.24 -29620.07 15335.55 26632.24 39493.42 -2.83 0.000%   20 -31005.24 -39493.42 15333.55 26632.24 39493.42 -2.83 0.000%   21 -31005.24 -39493.42 15331.90 26609.55 39493.42 -2.83 0.000%   22 -26609.55 -39493.42 -26576.96 15364.52 39493.42 -2.83 0.000%   23 -26609.55 -39493.42 -26576.96 15364.52 39493.42 -2.83 0.000%   24 -15364.52 -39493.42 -26576.96 15364.52 29620.07 -26576.96 0.000%   25 -13364.52 -29620.07 -26576.96 15364.52 29620.07 2576.96 0.000%   26 -0.00 -91494.80 -6769.54 3.66 91494.80 6769.67 0.000%   26 -0.00 -91494.80 -5142.44 -2957.95 91494.80 -477.79 0.000%   27 -3.66 -91494.80 -5142.44 -2957.95 91494.80 -477.79 0.000%   30 -6124.14 -91494.80 -5142.44 -2957.95 91494.80 -5142.55 0.000%   31 -1434 -91494.80 -5142.44 -2957.95 91494.80 -5142.55 0.000%   31 -1434 -91494.80 -5142.44 -2957.95 91494.80 -5142.55 0.000%   32 -2974.71 -91494.80 -5142.44 -2957.95 91494.80 -5142.55 0.000%   33 -1436 -91494.80 -5142.44 -2957.95 91494.80 -5142.55 0.000%   34 -2948.61 -91494.80 -5142.44 -2957.95 91494.80 -5142.63 0.000%   35	2		-39493.42	-31112.85	-66.65	39493.42	31112.85	0.000%
5         15399.83         29620.07         -26643.38         -15399.83         29620.07         26643.38         0.000%           6         26647.37         -39493.42         -15408.46         -26647.37         29620.07         15408.46         0.000%           8         31056.60         -39493.42         28.14         -31056.60         39493.42         -28.14         0.000%           10         26669.69         -39493.42         15337.39         -26669.69         39493.42         -15337.39         0.000%           11         26669.69         -39493.42         15337.39         -26669.69         39493.42         -15337.39         0.000%           12         15355.79         -39493.42         16337.59         -26669.69         29620.07         -15337.39         0.000%           12         15355.79         -39493.42         26633.95         -15355.79         39493.42         -26633.95         0.000%           13         15355.79         -29620.07         26633.95         -15355.79         39493.42         -3149.12         0.000%           15         -13.46         -39493.42         -1419.12         0.000%         16         -15335.86         -39493.42         -15449.12         0.000%	3	66.65	-29620.07	-31112.85	-66.65	29620.07	31112.85	0.000%
6 26647.37	4	15399.83	-39493.42	-26643.38	-15399.83	39493.42	26643.38	0.000%
7	5	15399.83	-29620.07	-26643.38	-15399.83	29620.07	26643.38	0.000%
8 31056.60	6	26647.37	-39493.42	-15408.46	-26647.37	39493.42	15408.46	0.000%
9 31056.60	7	26647.37	-29620.07	-15408.46	-26647.37	29620.07	15408.46	0.000%
10	8	31056.60	-39493.42	28.14	-31056.60	39493.42	-28.14	0.000%
10         26669.69         -39493.42         15337.39         -26669.69         39493.42         -15337.39         0.000%           11         26669.69         -29620.07         15337.39         -26669.69         29620.07         -15337.39         0.000%           12         15355.79         -39493.42         26633.95         -15355.79         39493.42         -26633.95         0.000%           14         -13.46         -39493.42         31149.12         13.46         39493.42         -31149.12         0.000%           15         -13.46         -29620.07         31149.12         13.46         39493.42         -26644.77         0.000%           16         -15335.86         -39493.42         26644.77         15335.86         39493.42         -26644.77         0.000%           18         -26632.24         -39493.42         15355.55         26632.24         39493.42         -15353.55         0.000%           19         -26632.24         -29620.07         15353.55         26632.24         39493.42         -2533.55         0.000%           20         -31005.24         -29620.07         2.83         31005.24         29620.07         -2.83         0.000%           22         -26609.55 <td< td=""><td>9</td><td>31056.60</td><td>-29620.07</td><td>28.14</td><td>-31056.60</td><td>29620.07</td><td>-28.14</td><td>0.000%</td></td<>	9	31056.60	-29620.07	28.14	-31056.60	29620.07	-28.14	0.000%
11         26669.69         -29620.07         15337.39         -26669.69         29620.07         -15335.79         0.000%           12         15355.79         -39493.42         26633.95         -15355.79         39493.42         -26633.95         0.000%           14         -13.46         -39493.42         31149.12         13.46         39493.42         -31149.12         0.000%           15         -13.46         -29620.07         31149.12         13.46         29620.07         -31149.12         0.000%           16         -15335.86         -39493.42         26644.77         15335.86         39493.42         -26644.77         0.000%           17         -15335.86         -29620.07         26644.77         15335.86         39493.42         -26644.77         0.000%           18         -26632.24         -39493.42         15353.55         26632.24         39493.42         -15353.55         0.000%           20         -31005.24         -29620.07         15353.55         26632.24         39493.42         -2.83         0.000%           21         -31005.24         -29620.07         2.83         31005.24         29620.07         -2.83         0.000%           22         -26609.55         -3	10	26669.69	-39493.42		-26669.69	39493.42	-15337.39	0.000%
13         15355.79         -29620.07         26633.95         -15355.79         29620.07         -26633.95         0.000%           14         -13.46         -39493.42         31149.12         13.46         39493.42         -31149.12         0.000%           15         -13.46         -29620.07         31149.12         13.46         29620.07         -31149.12         0.000%           16         -15335.86         -39493.42         26644.77         15335.86         39493.42         -26644.77         0.000%           17         -15335.86         -29620.07         26644.77         15335.86         29620.07         -26644.77         0.000%           18         -26632.24         -39493.42         15353.55         26632.24         29620.07         -15353.55         0.000%           20         -31005.24         -39493.42         2.83         31005.24         39493.42         -2.83         0.000%           21         -31005.24         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           22         -26609.55         -39493.42         -15331.90         26009.55         39493.42         15331.90         0.000%           23         -26609.55 <t< td=""><td></td><td>26669.69</td><td>-29620.07</td><td>15337.39</td><td>-26669.69</td><td></td><td>-15337.39</td><td></td></t<>		26669.69	-29620.07	15337.39	-26669.69		-15337.39	
13         15355.79         -29620.07         26633.95         -15355.79         29620.07         -26633.95         0.000%           14         -13.46         -39493.42         31149.12         13.46         39493.42         -31149.12         0.000%           15         -13.46         -29620.07         31149.12         13.46         29620.07         -31149.12         0.000%           16         -15335.86         -39493.42         26644.77         15335.86         39493.42         -26644.77         0.000%           17         -15335.86         -29620.07         26644.77         15335.86         29620.07         -26644.77         0.000%           18         -26632.24         -39493.42         15353.55         26632.24         29620.07         -15353.55         0.000%           20         -31005.24         -39493.42         2.83         31005.24         39493.42         -2.83         0.000%           21         -31005.24         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           22         -26609.55         -39493.42         -15331.90         26009.55         39493.42         15331.90         0.000%           23         -26609.55 <t< td=""><td>12</td><td>15355.79</td><td>-39493.42</td><td>26633.95</td><td>-15355.79</td><td>39493.42</td><td>-26633.95</td><td>0.000%</td></t<>	12	15355.79	-39493.42	26633.95	-15355.79	39493.42	-26633.95	0.000%
14         -13.46         -39493.42         31149.12         13.46         29620.07         -31149.12         0.000%           15         -13.46         -29620.07         31149.12         13.46         29620.07         -31149.12         0.000%           16         -15335.86         -39493.42         26644.77         15335.86         29620.07         -26644.77         0.000%           18         -26632.24         -39493.42         15353.55         26632.24         29620.07         -15353.55         0.000%           20         -31005.24         -29620.07         15353.55         26632.24         29620.07         -15353.55         0.000%           20         -31005.24         -39493.42         2.83         31005.24         39493.42         2.83         0.000%           21         -31005.24         -29620.07         2.83         31005.24         29620.07         -283         0.000%           23         -26609.55         -39493.42         -15331.90         26609.55         39493.42         26576.96         0.00           24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.00           25         -15364.52         -39493.42 <td></td> <td>15355.79</td> <td>-29620.07</td> <td>26633.95</td> <td>-15355.79</td> <td>29620.07</td> <td>-26633.95</td> <td>0.000%</td>		15355.79	-29620.07	26633.95	-15355.79	29620.07	-26633.95	0.000%
15         -13.46         -29620.07         31149.12         13.46         29620.07         -31149.12         0.000%           16         -15335.86         -39493.42         26644.77         15335.86         39493.42         -26644.77         0.000%           18         -26632.24         -39493.42         15353.55         26632.24         39493.42         -15353.55         0.000%           19         -26632.24         -29620.07         15353.55         26632.24         29620.07         -15353.55         0.000%           20         -31005.24         -39493.42         2.83         31005.24         39493.42         -2.83         0.000%           21         -31005.24         -29620.07         2.83         31005.24         29620.07         -2.83         0.000%           22         -26609.55         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           23         -26609.55         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.00           24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.00           25         -15364.52         -396	14	-13.46		31149.12	13.46	39493.42	-31149.12	0.000%
16         -15335.86         -39493.42         26644.77         15335.86         39493.42         -26644.77         0.000%           17         -15335.86         -29620.07         26644.77         15335.86         29620.07         -26644.77         0.000%           18         -26632.24         -39493.42         15353.55         26632.24         39493.42         -15353.55         0.000%           20         -31005.24         -39493.42         2.83         31005.24         39493.42         -2.83         0.000%           21         -31005.24         -29620.07         2.83         31005.24         39493.42         -2.83         0.000%           22         -26609.55         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           23         -26609.55         -29620.07         -15331.90         26609.55         39493.42         15331.90         0.000%           24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.000%           25         -15364.52         -2962.007         -26576.96         15364.52         39493.42         26576.96         0.000%           26         0.00 <td< td=""><td></td><td></td><td>-29620.07</td><td></td><td></td><td></td><td></td><td></td></td<>			-29620.07					
17         -15335.86         -29620.07         26644.77         15335.86         29620.07         -26644.77         0.000%           18         -26632.24         -39493.42         15353.55         26632.24         29620.07         -15353.55         0.000%           20         -31005.24         -39493.42         2.83         31005.24         39493.42         -2.83         0.000%           21         -31005.24         -29620.07         2.83         31005.24         29620.07         -2.83         0.000%           22         -26609.55         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           23         -26609.55         -29620.07         -15331.90         26609.55         39493.42         15331.90         0.000%           24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.000           25         -15364.52         -29620.07         -26576.96         15364.52         39493.42         26576.96         0.000           26         0.00         -91494.80         0.00         0.00         91494.80         6769.67         0.000%           27         -3.66         -91494.80								
18         -26632.24         -39493.42         15353.55         26632.24         39493.42         -15353.55         0.000%           19         -26632.24         -29620.07         15353.55         26632.24         29620.07         -15353.55         0.000%           20         -31005.24         -39493.42         2.83         31005.24         39493.42         -2.83         0.000%           21         -31005.24         -29620.07         2.83         31005.24         29620.07         -2.83         0.000%           22         -26609.55         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           23         -26609.55         -29620.07         -15331.90         26609.55         29620.07         15331.90         0.000%           24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.000%           25         -15364.52         -29620.07         -26576.96         15364.52         29620.07         26576.96         0.000%           26         0.00         -91494.80         -6769.54         3.66         91494.80         -6769.54         3.66         91494.80         -676.67         0.000%								
19         -26632.24         -29620.07         15353.55         26632.24         29620.07         -15353.55         0.000%           20         -31005.24         -39493.42         2.83         31005.24         39493.42         -2.83         0.000%           21         -31005.24         -29620.07         2.83         31005.24         29620.07         -2.83         0.000%           22         -26609.55         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           23         -26609.55         -29620.07         -15331.90         26609.55         29620.07         15331.90         0.000%           24         -15364.52         -39493.42         -26576.96         15364.52         29620.07         26576.96         0.000%           25         -15364.52         -29620.07         -26576.96         15364.52         29620.07         26576.96         0.000%           26         0.00         -91494.80         0.00         0.00         91494.80         6769.54         3.66         91494.80         6769.67         0.000%           28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%								
20         -31005.24         -39493.42         2.83         31005.24         39493.42         -2.83         0.000%           21         -31005.24         -29620.07         2.83         31005.24         29620.07         -2.83         0.000%           22         -26609.55         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           23         -26609.55         -29620.07         -15331.90         26609.55         29620.07         15331.90         0.000%           24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.000%           25         -15364.52         -29620.07         -26576.96         15364.52         29620.07         26576.96         0.000%           26         0.00         -91494.80         0.00         0.00         91494.80         -0.03         0.000%           27         -3.66         -91494.80         -5142.44         -2957.95         91494.80         6769.67         0.000%           28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%           30         6124.14         -91494.80								
21         -31005.24         -29620.07         2.83         31005.24         29620.07         -2.83         0.000%           22         -26609.55         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           23         -26609.55         -29620.07         -15331.90         26609.55         29620.07         15331.90         0.000%           24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.000%           25         -15364.52         -29620.07         -26576.96         15364.52         29620.07         26576.96         0.000%           26         0.00         -91494.80         0.00         0.00         91494.80         -0.03         0.000%           27         -3.66         -91494.80         -6769.54         3.66         91494.80         5142.55         0.000%           28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%           30         6124.14         -91494.80         17.37         -6124.27         91494.80         2974.71         91494.80         -17.37         0.000%           31         5								
22         -26609.55         -39493.42         -15331.90         26609.55         39493.42         15331.90         0.000%           23         -26609.55         -29620.07         -15331.90         26609.55         29620.07         15331.90         0.000%           24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.000           25         -15364.52         -29620.07         -26576.96         15364.52         29620.07         26576.96         0.000%           26         0.00         -91494.80         0.00         0.00         91494.80         -0.03         0.000%           27         -3.66         -91494.80         -6769.54         3.66         91494.80         6769.67         0.000%           28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%           30         6124.14         -91494.80         -2944.73         -6124.27         91494.80         -17.37         0.000%           31         5149.54         -91494.80         2977.84         -5149.65         91494.80         -2977.91         0.000%           32         2974.71         -91494.80								
23         -26609.55         -29620.07         -15331.90         26609.55         29620.07         15331.90         0.000%           24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.000%           25         -15364.52         -29620.07         -26576.96         15364.52         29620.07         26576.96         0.000%           26         0.00         -91494.80         0.00         0.00         91494.80         -0.03         0.000%           27         -3.66         -91494.80         -6769.54         3.66         91494.80         6769.67         0.000%           28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%           29         5132.77         -91494.80         -2964.93         -5132.88         91494.80         2964.99         0.000%           30         6124.14         -91494.80         2977.84         -5149.65         91494.80         -17.37         0.000%           31         5149.54         -91494.80         5154.59         -2974.77         91494.80         -5154.71         0.000%           32         2974.71         -91494.80 <t< td=""><td>22</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	22							
24         -15364.52         -39493.42         -26576.96         15364.52         39493.42         26576.96         0.000%           25         -15364.52         -29620.07         -26576.96         15364.52         29620.07         26576.96         0.000%           26         0.00         -91494.80         0.00         0.00         91494.80         -0.03         0.000%           27         -3.66         -91494.80         -6769.54         3.66         91494.80         6769.67         0.000%           28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%           29         5132.77         -91494.80         -2964.93         -5132.88         91494.80         2964.99         0.000%           30         6124.14         -91494.80         17.37         -6124.27         91494.80         -17.37         0.000%           31         5149.54         -91494.80         2977.84         -5149.65         91494.80         -5154.71         0.000%           32         2974.71         -91494.80         5142.51         2948.67         91494.80         -5142.43         0.000%           34         -2948.61         -91494.80         5142								
25         -15364.52         -29620.07         -26576.96         15364.52         29620.07         26576.96         0.000%           26         0.00         -91494.80         0.00         0.00         91494.80         -0.03         0.000%           27         -3.66         -91494.80         -6769.54         3.66         91494.80         6769.67         0.000%           28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%           30         6124.14         -91494.80         17.37         -6124.27         91494.80         2964.99         0.000%           31         5149.54         -91494.80         2977.84         -5149.65         91494.80         -2977.91         0.000%           32         2974.71         -91494.80         5154.59         -2974.77         91494.80         -5154.71         0.000%           33         11.43         -91494.80         6774.67         -11.43         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -2977.19 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
26         0.00         -91494.80         0.00         0.00         91494.80         -0.03         0.000%           27         -3.66         -91494.80         -6769.54         3.66         91494.80         6769.67         0.000%           28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%           29         5132.77         -91494.80         -2964.93         -5132.88         91494.80         2964.99         0.000%           30         6124.14         -91494.80         17.37         -6124.27         91494.80         -17.37         0.000%           31         5149.54         -91494.80         2977.84         -5149.65         91494.80         -2977.91         0.000%           32         2974.71         -91494.80         5154.59         -2974.77         91494.80         -5154.71         0.000%           34         -2948.61         -91494.80         5142.51         2948.67         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00								
27         -3.66         -91494.80         -6769.54         3.66         91494.80         6769.67         0.000%           28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%           29         5132.77         -91494.80         -2964.93         -5132.88         91494.80         2964.99         0.000%           30         6124.14         -91494.80         17.37         -6124.27         91494.80         -17.37         0.000%           31         5149.54         -91494.80         2977.84         -5149.65         91494.80         -2977.91         0.000%           32         2974.71         -91494.80         5154.59         -2974.77         91494.80         -5154.71         0.000%           34         -2948.61         -91494.80         5142.51         2948.67         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00         6116.75         91494.80         13.00         0.000%           37         -5140.83         -91494.80         -2								
28         2957.88         -91494.80         -5142.44         -2957.95         91494.80         5142.55         0.000%           29         5132.77         -91494.80         -2964.93         -5132.88         91494.80         2964.99         0.000%           30         6124.14         -91494.80         17.37         -6124.27         91494.80         -17.37         0.000%           31         5149.54         -91494.80         2977.84         -5149.65         91494.80         -2977.91         0.000%           32         2974.71         -91494.80         5154.59         -2974.77         91494.80         -5154.71         0.000%           33         11.43         -91494.80         6774.67         -11.43         91494.80         -6774.82         0.000%           34         -2948.61         -91494.80         5142.51         2948.67         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00         6116.75         91494.80         2977.25         0.000%           37         -5140.83         -91494.80 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>								
29         5132.77         -91494.80         -2964.93         -5132.88         91494.80         2964.99         0.000%           30         6124.14         -91494.80         17.37         -6124.27         91494.80         -17.37         0.000%           31         5149.54         -91494.80         2977.84         -5149.65         91494.80         -2977.91         0.000%           32         2974.71         -91494.80         5154.59         -2974.77         91494.80         -5154.71         0.000%           33         11.43         -91494.80         6774.67         -11.43         91494.80         -6774.82         0.000%           34         -2948.61         -91494.80         5142.51         2948.67         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00         6116.75         91494.80         13.00         0.000%           37         -5140.83         -91494.80         -2977.19         5140.94         91494.80         2977.25         0.000%           38         -2976.10         -91494.80								
30         6124.14         -91494.80         17.37         -6124.27         91494.80         -17.37         0.000%           31         5149.54         -91494.80         2977.84         -5149.65         91494.80         -2977.91         0.000%           32         2974.71         -91494.80         5154.59         -2974.77         91494.80         -5154.71         0.000%           33         11.43         -91494.80         6774.67         -11.43         91494.80         -6774.82         0.000%           34         -2948.61         -91494.80         5142.51         2948.67         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00         6116.75         91494.80         13.00         0.000%           37         -5140.83         -91494.80         -2977.19         5140.94         91494.80         2977.25         0.000%           38         -2976.10         -91494.80         -5146.37         2976.16         91494.80         5146.48         0.000%           39         14.26         -32911.18         -66								
31         5149.54         -91494.80         2977.84         -5149.65         91494.80         -2977.91         0.000%           32         2974.71         -91494.80         5154.59         -2974.77         91494.80         -5154.71         0.000%           33         11.43         -91494.80         6774.67         -11.43         91494.80         -6774.82         0.000%           34         -2948.61         -91494.80         5142.51         2948.67         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00         6116.75         91494.80         13.00         0.000%           37         -5140.83         -91494.80         -2977.19         5140.94         91494.80         2977.25         0.000%           38         -2976.10         -91494.80         -5146.37         2976.16         91494.80         5146.48         0.000%           39         14.26         -32911.18         -6656.93         -14.26         32911.18         5700.64         -3294.96         32911.18         5700.64         0.000%								
32         2974.71         -91494.80         5154.59         -2974.77         91494.80         -5154.71         0.000%           33         11.43         -91494.80         6774.67         -11.43         91494.80         -6774.82         0.000%           34         -2948.61         -91494.80         5142.51         2948.67         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00         6116.75         91494.80         13.00         0.000%           37         -5140.83         -91494.80         -2977.19         5140.94         91494.80         2977.25         0.000%           38         -2976.10         -91494.80         -5146.37         2976.16         91494.80         5146.48         0.000%           39         14.26         -32911.18         -6656.93         -14.26         32911.18         6656.93         0.000%           40         3294.96         -32911.18         -5700.64         -3294.96         32911.18         5700.64         0.000%           41         5701.49         -32911.18         -								
33         11.43         -91494.80         6774.67         -11.43         91494.80         -6774.82         0.000%           34         -2948.61         -91494.80         5142.51         2948.67         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00         6116.75         91494.80         13.00         0.000%           37         -5140.83         -91494.80         -2977.19         5140.94         91494.80         2977.25         0.000%           38         -2976.10         -91494.80         -5146.37         2976.16         91494.80         5146.48         0.000%           39         14.26         -32911.18         -6656.93         -14.26         32911.18         6656.93         0.000%           40         3294.96         -32911.18         -5700.64         -3294.96         32911.18         5700.64         0.000%           41         5701.49         -32911.18         -3296.81         -5701.50         32911.18         3296.81         0.000%           42         6644.90         -32911.18         6								
34         -2948.61         -91494.80         5142.51         2948.67         91494.80         -5142.63         0.000%           35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00         6116.75         91494.80         13.00         0.000%           37         -5140.83         -91494.80         -2977.19         5140.94         91494.80         2977.25         0.000%           38         -2976.10         -91494.80         -5146.37         2976.16         91494.80         5146.48         0.000%           39         14.26         -32911.18         -6656.93         -14.26         32911.18         6656.93         0.000%           40         3294.96         -32911.18         -5700.64         -3294.96         32911.18         5700.64         0.000%           41         5701.49         -32911.18         -3296.81         -5701.50         32911.18         3296.81         0.000%           42         6644.90         -32911.18         6.02         -6644.90         32911.18         -3281.60         0.000%           43         5706.27         -32911.18								
35         -5130.45         -91494.80         2957.00         5130.56         91494.80         -2957.07         0.000%           36         -6116.62         -91494.80         -13.00         6116.75         91494.80         13.00         0.000%           37         -5140.83         -91494.80         -2977.19         5140.94         91494.80         2977.25         0.000%           38         -2976.10         -91494.80         -5146.37         2976.16         91494.80         5146.48         0.000%           39         14.26         -32911.18         -6656.93         -14.26         32911.18         6656.93         0.000%           40         3294.96         -32911.18         -5700.64         -3294.96         32911.18         5700.64         0.000%           41         5701.49         -32911.18         -3296.81         -5701.50         32911.18         3296.81         0.000%           42         6644.90         -32911.18         6.02         -6644.90         32911.18         -3281.60         0.000%           43         5706.27         -32911.18         3281.60         -5706.27         32911.18         -3281.60         0.000%								
36     -6116.62     -91494.80     -13.00     6116.75     91494.80     13.00     0.000%       37     -5140.83     -91494.80     -2977.19     5140.94     91494.80     2977.25     0.000%       38     -2976.10     -91494.80     -5146.37     2976.16     91494.80     5146.48     0.000%       39     14.26     -32911.18     -6656.93     -14.26     32911.18     6656.93     0.000%       40     3294.96     -32911.18     -5700.64     -3294.96     32911.18     5700.64     0.000%       41     5701.49     -32911.18     -3296.81     -5701.50     32911.18     3296.81     0.000%       42     6644.90     -32911.18     6.02     -6644.90     32911.18     -6.02     0.000%       43     5706.27     -32911.18     3281.60     -5706.27     32911.18     -3281.60     0.000%	35							
37     -5140.83     -91494.80     -2977.19     5140.94     91494.80     2977.25     0.000%       38     -2976.10     -91494.80     -5146.37     2976.16     91494.80     5146.48     0.000%       39     14.26     -32911.18     -6656.93     -14.26     32911.18     6656.93     0.000%       40     3294.96     -32911.18     -5700.64     -3294.96     32911.18     5700.64     0.000%       41     5701.49     -32911.18     -3296.81     -5701.50     32911.18     3296.81     0.000%       42     6644.90     -32911.18     6.02     -6644.90     32911.18     -6.02     0.000%       43     5706.27     -32911.18     3281.60     -5706.27     32911.18     -3281.60     0.000%								
38     -2976.10     -91494.80     -5146.37     2976.16     91494.80     5146.48     0.000%       39     14.26     -32911.18     -6656.93     -14.26     32911.18     6656.93     0.000%       40     3294.96     -32911.18     -5700.64     -3294.96     32911.18     5700.64     0.000%       41     5701.49     -32911.18     -3296.81     -5701.50     32911.18     3296.81     0.000%       42     6644.90     -32911.18     6.02     -6644.90     32911.18     -6.02     0.000%       43     5706.27     -32911.18     3281.60     -5706.27     32911.18     -3281.60     0.000%								
39     14.26     -32911.18     -6656.93     -14.26     32911.18     6656.93     0.000%       40     3294.96     -32911.18     -5700.64     -3294.96     32911.18     5700.64     0.000%       41     5701.49     -32911.18     -3296.81     -5701.50     32911.18     3296.81     0.000%       42     6644.90     -32911.18     6.02     -6644.90     32911.18     -6.02     0.000%       43     5706.27     -32911.18     3281.60     -5706.27     32911.18     -3281.60     0.000%								
40     3294.96     -32911.18     -5700.64     -3294.96     32911.18     5700.64     0.000%       41     5701.49     -32911.18     -3296.81     -5701.50     32911.18     3296.81     0.000%       42     6644.90     -32911.18     6.02     -6644.90     32911.18     -6.02     0.000%       43     5706.27     -32911.18     3281.60     -5706.27     32911.18     -3281.60     0.000%								
41     5701.49     -32911.18     -3296.81     -5701.50     32911.18     3296.81     0.000%       42     6644.90     -32911.18     6.02     -6644.90     32911.18     -6.02     0.000%       43     5706.27     -32911.18     3281.60     -5706.27     32911.18     -3281.60     0.000%								
42 6644.90 -32911.18 6.02 -6644.90 32911.18 -6.02 0.000% 43 5706.27 -32911.18 3281.60 -5706.27 32911.18 -3281.60 0.000%								
43 5706.27 -32911.18 3281.60 -5706.27 32911.18 -3281.60 0.000%								
++ J20J.J+ -J2711.10 J070.02 -J20J.J4 J2711.10 -J070.02 0.000%								
	44	3203.34	-34911.10	3030.02	-3203.34	34711.10	-3070.02	0.000 /0

# Tower Engineering Professionals

326 Tryon Road Raleigh, NC 27603 Phone: (919) 661-6351 FAX: (919) 661-6350

Job	Wast Lightford/L04/V40 (DLL000040)	<b>Page</b> 16 of 19
	West Hartford/I-84/X43 (BU 829013)	10 01 19
Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

	Sui	n of Applied Forces	7		Sum of Reaction	s	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	lb	lb	lb	lb	lb	lb	
45	-2.88	-32911.18	6664.69	2.88	32911.18	-6664.70	0.000%
46	-3281.27	-32911.18	5700.94	3281.27	32911.18	-5700.94	0.000%
47	-5698.26	-32911.18	3285.06	5698.26	32911.18	-3285.06	0.000%
48	-6633.91	-32911.18	0.61	6633.91	32911.18	-0.61	0.000%
49	-5693.40	-32911.18	-3280.43	5693.40	32911.18	3280.43	0.000%
50	-3287.41	-32911.18	-5686.43	3287.41	32911.18	5686.43	0.000%

### **Non-Linear Convergence Results**

Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	5	0.00000001	0.00020954
3	Yes	5	0.00000001	0.00009444
4	Yes	6	0.00000001	0.00005463
5	Yes	5	0.00000001	0.00054761
6	Yes	6	0.00000001	0.00004738
7	Yes	5	0.00000001	0.00047384
8	Yes	5	0.00000001	0.00047176
9	Yes	5	0.00000001	0.00021214
10	Yes	6	0.00000001	0.00006993
11	Yes	5	0.00000001	0.00070681
12	Yes	6	0.00000001	0.00004567
13	Yes	5	0.00000001	0.00045740
14	Yes	5	0.00000001	0.00022921
15	Yes	5	0.00000001	0.00010301
16	Yes	6	0.00000001	0.00005213
17	Yes	5	0.00000001	0.00052104
18	Yes	6	0.00000001	0.00006245
19	Yes	5	0.00000001	0.00062816
20	Yes	5	0.00000001	0.00048445
21	Yes	5	0.00000001	0.00021779
22	Yes	6	0.00000001	0.00004502
23	Yes	5	0.00000001	0.00045221
24	Yes	6	0.00000001	0.00006653
25	Yes	5	0.00000001	0.00067177
26	Yes	4	0.00000001	0.00010287
27	Yes	5	0.00000001	0.00047272
28	Yes	5	0.00000001	0.00054062
29	Yes	5	0.00000001	0.00053297
30	Yes	5	0.00000001	0.00033237
31	Yes	5	0.00000001	0.00060466
32	Yes	5	0.00000001	0.00056711
33	Yes	5	0.00000001	0.00030711
34	Yes	5	0.00000001	0.00056701
35	Yes	5	0.00000001	0.00059183
36	Yes	5	0.0000001	0.00039183
37	Yes	5	0.0000001	0.00053986
38	Yes	5	0.0000001	0.00055963
39	Yes	4	0.0000001	0.00033903
40	Yes	4	0.0000001	0.00029430
40	Yes	4	0.0000001	0.00044439
41	Yes	4	0.0000001	0.00042273
42	Yes	4	0.0000001	0.00063219
43 44	Yes Yes	4	0.00000001	0.00095525
		4		
45	Yes	4	0.00000001	0.00030035

tnx	Tower	Job	West Hartford/I-	.84/X43 (BU 829013)	<b>Page</b> 17 of 19	
Tower Engineering Professionals 326 Tryon Road		Project	TEP No.	25680.161675	Date 13:54:52 07/02/1	
Raleis Phone:	gh, NC 27603 (919) 661-6351 919) 661-6350	Client	Cro	Designed by AAS		
46	Yes	4	0.00000001	0.00039345		
47	Yes	4	0.00000001	0.00037343		
48	Yes	4	0.00000001	0.00064085		
49	Yes	4	0.00000001	0.00062252		
50	Yes	4	0.00000001	0.00084592		

		Maximum	Tower	Deflection	s - Service Wind
Section	Elevation	Horz.	Gov.	Tilt	Twist
No.	210 rumon	Deflection	Load	1000	1,,,,,,
	ft	in	Comb.	0	•
L1	119.083 - 101.083	15.672	48	1.129	0.022
L2	104 - 66.5	12.163	48	1.078	0.014
L3	70.3333 - 32.8333	5.558	48	0.748	0.005
L4	37.5 - 0	1.587	48	0.390	0.002

	Critical Deflections and Radius of Curvature - Service Wind									
Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature				
ft		Comb.	in	0	0	ft				
120.00	AIR -32 B2A/B66AA w/ Mount Pipe	48	15.672	1.129	0.022	24799				
115.00	VHLP2-18	48	14.708	1.119	0.020	24799				
110.00	7770.00 w/ Mount Pipe	48	13.538	1.104	0.017	13651				
100.00	BXA-80063-4BF-EDIN-X w/ Mount Pipe	48	11.273	1.053	0.012	7678				
97.00	2'x3' Ice Shield	48	10.622	1.031	0.011	7312				
95.00	2'x3' Ice Shield	48	10.196	1.014	0.010	7089				
90.00	742 213 w/ Mount Pipe	48	9.160	0.967	0.009	6585				
83.00	VHLP2-23	48	7.787	0.893	0.007	5987				
80.00	LLPX310R w/ Mount Pipe	48	7.228	0.860	0.007	5762				

		Maximum	Tower I	Deflection	s - Desig
tion	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	119.083 - 101.083	73.546	8	5.293	0.103
L2	104 - 66.5	57.104	8	5.061	0.064
L3	70.3333 - 32.8333	26.114	8	3.513	0.024
L4	37.5 - 0	7.458	8	1.831	0.009

### Critical Deflections and Radius of Curvature - Design Wind

### Tower Engineering Professionals

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Job		Page
	West Hartford/I-84/X43 (BU 829013)	18 of 19
Project	TEP No. 25680.161675	Date 13:54:52 07/02/18
Client	Crown Castle	Designed by AAS

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	0	0	ft
120.00	AIR -32 B2A/B66AA w/ Mount	8	73.546	5.293	0.103	5475
	Pipe					
115.00	VHLP2-18	8	69.031	5.248	0.092	5475
110.00	7770.00 w/ Mount Pipe	8	63.548	5.181	0.079	3013
100.00	BXA-80063-4BF-EDIN-X w/	8	52.933	4.945	0.056	1686
	Mount Pipe					
97.00	2'x3' Ice Shield	8	49.879	4.839	0.051	1601
95.00	2'x3' Ice Shield	8	47.880	4.762	0.048	1550
90.00	742 213 w/ Mount Pipe	8	43.022	4.544	0.041	1433
83.00	VHLP2-23	8	36.580	4.198	0.034	1295
80.00	LLPX310R w/ Mount Pipe	8	33.956	4.039	0.031	1244

### Compression Checks

### **Pole Design Data**

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
110.	ft		ft	ft		$in^2$	lb	lb	$\frac{I_u}{\phi P_n}$
L1	119.083 - 101.083 (1)	TP26x22.13x0.25	18.00	0.00	0.0	19.935	-8929.87	1479480.00	0.006
L2	101.083 - 66.5 (2)	TP34.063x24.873x0.313	37.50	0.00	0.0	32.544	-18889.40	2387960.00	0.008
L3	66.5 - 32.8333	TP41.75x32.498x0.375	37.50	0.00	0.0	47.876	-27587.90	3492730.00	0.008
L4	32.8333 - 0 (4)	TP49.063x39.849x0.375	37.50	0.00	0.0	57.950	-39470.60	3984000.00	0.010

### Pole Bending Design Data

Section No.	Elevation	Size	$M_{ux}$	$\phi M_{nx}$	Ratio M <sub>ux</sub>	$M_{uy}$	$\phi M_{ny}$	Ratio M <sub>uy</sub>
1,0.	ft		lb-ft	lb-ft	$\phi M_{nx}$	lb-ft	lb-ft	$\phi M_{ny}$
L1	119.083 - 101.083 (1)	TP26x22.13x0.25	171465.83	762729.17	0.225	0.00	762729.17	0.000
L2	101.083 - 66.5	TP34.063x24.873x0.313	930675.00	1608483.33	0.579	0.00	1608483.33	0.000
L3	66.5 - 32.8333	TP41.75x32.498x0.375	1826425.00	2884758.33	0.633	0.00	2884758.33	0.000
L4	32.8333 - 0 (4)	TP49.063x39.849x0.375	2947866.67	3989300.00	0.739	0.00	3989300.00	0.000

Pole	Shear	Design	Data
	<b>UU</b>	_00.9	_ ~ ~

Section	Elevation	Size	Actual	$\phi V_n$	Ratio	Actual	$\phi T_n$	Ratio
No.			$V_u$		$V_u$	$T_u$	·	$T_u$
	ft		lb	lb	$\phi V_n$	lb-ft	lb-ft	$\phi T_n$
L1	119.083 -	TP26x22.13x0.25	15338.90	739739.00	0.021	5493.46	1527325.00	0.004

#### Tower Engineering Professionals

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Section No.	Elevation	Size	Actual $V_u$	$\phi V_n$	Ratio $V_u$	Actual T <sub>u</sub>	$\phi T_n$	Ratio T <sub>u</sub>
	ft		lb	lb	$\phi V_n$	lb-ft	lb-ft	$\phi T_n$
	101.083 (1)							
L2	101.083 - 66.5	TP34.063x24.873x0.313	25906.70	1193980.00	0.022	8431.33	3220900.00	0.003
	(2)							
L3	66.5 - 32.8333	TP41.75x32.498x0.375	28600.10	1746370.00	0.016	8408.58	5776566.67	0.001
	(3)							
L4	32.8333 - 0 (4)	TP49.063x39.849x0.375	31085.60	1992000.00	0.016	8398.17	7988358.00	0.001

### **Pole Interaction Design Data**

Section No.	Elevation	Ratio P <sub>u</sub>	Ratio M <sub>ux</sub>	Ratio M <sub>uy</sub>	Ratio $V_u$	Ratio T <sub>u</sub>	Comb. Stress	Allow. Stress	Criteria
	ft	$\phi P_n$	$\phi M_{nx}$	$\phi M_{ny}$	$\phi V_n$	$\phi T_n$	Ratio	Ratio	
L1	119.083 - 101.083 (1)	0.006	0.225	0.000	0.021	0.004	0.231	1.000	4.8.2
L2	101.083 - 66.5 (2)	0.008	0.579	0.000	0.022	0.003	0.587	1.000	4.8.2
L3	66.5 - 32.8333 (3)	0.008	0.633	0.000	0.016	0.001	0.641	1.000	4.8.2
L4	32.8333 - 0 (4)	0.010	0.739	0.000	0.016	0.001	0.749	1.000	4.8.2

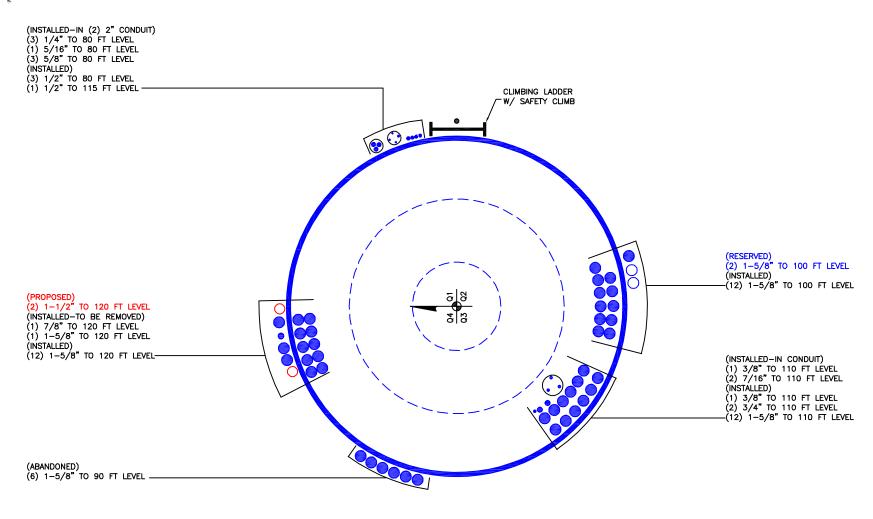
### **Section Capacity Table**

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	øP <sub>allow</sub> lb	% Capacity	Pass Fail
L1	119.083 - 101.083	Pole	TP26x22.13x0.25	1	-8929.87	1479480.00	23.1	Pass
L2	101.083 - 66.5	Pole	TP34.063x24.873x0.313	2	-18889.40	2387960.00	58.7	Pass
L3	66.5 - 32.8333	Pole	TP41.75x32.498x0.375	3	-27587.90	3492730.00	64.1	Pass
L4	32.8333 - 0	Pole	TP49.063x39.849x0.375	4	-39470.60	3984000.00	74.9	Pass
							Summary	
						Pole (L4)	74.9	Pass
						Rating =	74.9	Pass

 $Program\ Version\ 7.0.5.1\ -\ 2/1/2016\ File: C:/Users/ashah/Desktop/Work\ in\ Progress/Crown\ SA\ Reviews/ADB/P-147557\_L-161675\_829013\_WEST\ HARTFORDI-84X43\_Structural\ Analysis/tnxTower/829013\_LC7.eri$ 

# APPENDIX B BASE LEVEL DRAWING





# APPENDIX C ADDITIONAL CALCULATIONS



#### West Hartford/I-84/X43 (BU 829013)

TEP #:

Check:

25680.161675

Analysis:

ADB AAS

7/2/2018 7/2/2018

#### 18-Sided, Tubular Polygon Tower Section

Reaction Input				
Elevation:	101.1	ft		
Moment:	171.47	kip-ft		
Axial:	8.93	kip		
Shear:	15.34	kip		
Torsion:	5.49	kip-ft		

**Section Properties** Diameter: 26.00 in Thickness: 0.2500 in No. of Sides: 18 Flat Width: 4.14 in 20.43 in<sup>2</sup> Area: **Material Properties** 

ksi

ksi

F<sub>y</sub>: 65 E: 29000

Actual Slip-Splice Length: 35.00 in

Required Slip-Splice Length: 38.25 in (per TIA-222-G 4.9.7.1)

Check Bending

**S:** 131.67 in<sup>3</sup>

**F**'<sub>y</sub>: 71.47 ksi

(reduced to account for actual slip-splice length per TIA-222-G 13.3.5)

0.9\*F'<sub>v</sub> \*S  $φM_n$ : 705.73 kip-ft 24.3% **PASS** 

**Check Axial** 

**ΦP**<sub>n</sub>: 1314.18 kip

PASS

0.9\*F'<sub>y</sub> \*A<sub>g</sub>

**Check Shear** 

**φV**<sub>n</sub>: 657.09 kip

2.3% **PASS** 

0.9\*0.5\*F'<sub>y</sub> \*A<sub>g</sub>

**Check Torsion** 

J: 3423.31 in<sup>4</sup>

c: 13.00 in

**φT**<sub>n</sub>: 1411.46 kip-ft

0.9\*F'<sub>y</sub> \*(J/c)

Interaction:

25.0% PASS

0.4% **PASS** 

 $(P_u/\varphi P_n) + (M_u/\varphi M_n) + [(V_u/\varphi V_n) + T_u/\varphi T_n)]^2$ 



#### West Hartford/I-84/X43 (BU 829013)

TEP #:

25680.161675

Analysis:

Check:

ADB AAS

7/2/2018 7/2/2018

#### 18-Sided, Tubular Polygon Tower Section

Reaction Input				
Elevation:	66.5	ft		
Moment:	930.68	kip-ft		
Axial:	18.89	kip		
Shear:	25.91	kip		
Torsion:	8.43	kip-ft		

**Section Properties** Diameter: 34.06 in Thickness: 0.3125 in No. of Sides: 18 Flat Width: 5.46 in 33.47 in<sup>2</sup> Area: **Material Properties** F<sub>y</sub>: 65 ksi

29000

ksi

Actual Slip-Splice Length: 46.00 in

Required Slip-Splice Length: 50.16 in (per TIA-222-G 4.9.7.1)

Check Bending

**S**: 282.86 in<sup>3</sup>

**F'<sub>v</sub>:** 70.82 ksi

(reduced to account for actual slip-splice length per TIA-222-G 13.3.5)

E:

0.9\*F'<sub>v</sub> \*S **φM**<sub>n</sub>: 1502.33 kip-ft 61.9% **PASS** 

**Check Axial** 

**ΦP**<sub>n</sub>: 2133.50 kip

0.9% PASS

PASS

 $0.9*F'_{v}*A_{q}$ 

**Check Shear** 

**φV**<sub>n</sub>: 1066.75 kip 2.4% 0.9\*0.5\*F'<sub>y</sub> \*A<sub>g</sub>

**Check Torsion** 

**J**: 9634.87 in<sup>4</sup>

c: 17.03 in

 $\phi T_n$ : 3004.67 kip-ft 0.3% PASS 0.9\*F'<sub>y</sub> \*(J/c)

Interaction:

62.9% PASS

 $(P_u/\varphi P_n) + (M_u/\varphi M_n) + [(V_u/\varphi V_n) + T_u/\varphi T_n)]^2$ 



#### West Hartford/I-84/X43 (BU 829013)

AAS

25680.161675 TEP#:

Analysis: ADB

Check:

7/2/2018 7/2/2018

#### 18-Sided, Tubular Polygon Tower Section

Reaction Input				
Elevation:	32.8	ft		
Moment:	1826.43	kip-ft		
Axial:	27.59	kip		
Shear:	28.60	kip		
Torsion:	8.41	kip-ft		

**Section Properties** Diameter: 41.75 in Thickness: 0.3750 in No. of Sides: 18 Flat Width: 6.70 in in<sup>2</sup> 49.24 Area: **Material Properties**  $\mathbf{F}_{\mathbf{y}}$ : 65 ksi

29000

ksi

E:

Actual Slip-Splice Length: 56.00

Required Slip-Splice Length:

61.50 in (per TIA-222-G 4.9.7.1)

**Check Bending** 

S: 510.23 in<sup>3</sup>

F'<sub>y</sub>: 69.60 (reduced to account for actual slip-splice length per TIA-222-G 13.3.5) ksi

0.9\*F'<sub>v</sub> \*S **φM**<sub>n</sub>: 2663.44 kip-ft 68.6% **PASS** 

**Check Axial** 

**ΦP**<sub>n</sub>: 3084.76 kip 0.9% PASS  $0.9*F'_y*A_g$ 

**Check Shear** 

 $0.9*0.5*F'_y*A_g$ **φV**<sub>n</sub>: 1542.38 kip 1.9% PASS

**Check Torsion** 

**J**: 21302.0 in<sup>4</sup>

c: 20.88 in

**ΦT**<sub>n</sub>: 5326.87 kip-ft 0.2% **PASS** 0.9\*F'<sub>y</sub>\*(J/c)

Interaction: 69.5% PASS  $(P_u/\phi P_n) + (M_u/\phi M_n) + [(V_u/\phi V_n) + T_u/\phi T_n)]^2$ 

### Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material

**TIA Rev G** Assumption: Clear space between bottom of leveling nut and top of concrete **not** exceeding (1)\*(Rod Diameter)

#### Site Data

BU#: 829013

Site Name: West Hartford/I-84/X43

App #: 433326 Rev. 6

Pole Manufacturer: Other

Anchor Rod Data				
Qty:	33			
Diam:	1.25	in		
Rod Material:	Other			
Strength (Fu):	125	ksi		
Yield (Fy):	105	ksi		
Bolt Circle:	54	in		

Plate Data				
Diam:	58	in		
Thick:	1.5	in		
Grade:	50	ksi		
Single-Rod B-eff:	4.72	in		

Stiffener Da	Stiffener Data (Welding at both sides)					
Config:	1	*				
Weld Type:	Fillet					
Groove Depth:		< Disregard				
Groove Angle:		< Disregard				
Fillet H. Weld:	0.5	in				
Fillet V. Weld:	0.25	in				
Width:	4	in				
Height:	12	in				
Thick:	0.75	in				
Notch:	0.5	in				
Grade:	36	ksi				
Weld str.:	70	ksi				

Pole Data				
Diam:	49.0625	in		
Thick:	0.375	in		
Grade:	65	ksi		
# of Sides:	18	"0" IF Round		
Fu	80	ksi		
Reinf. Fillet Weld	0	"0" if None		

Reactions					
Mu:	2947.87	ft-kips			
Axial, Pu:	39.49	kips			
Shear, Vu:	31.15	kips			
Eta Factor, η	0.5	TIA G (Fig. 4-4)			

If N	lo stiffeners	Criteria:	AISC L RED	<-Only Applcable to Unstiffened Cases
11 18	10 31111611613,	Ontena.	AISO LI II D	C-Only Applicable to Onstillened Cases

#### **Anchor Rod Results**

Max Rod (Cu+ Vu/ $\dot{\eta}$ ): 82.5 Kips Allowable Axial,  $\Phi$ \*Fu\*Anet: 96.9 Kips Anchor Rod Stress Ratio: 85.1% Pass

	Stiffened
	AISC LRFD
I	φ*Tn

Base Plate ResultsFlexural CheckBase Plate Stress:27.5 ksiAllowable Plate Stress:45.0 ksiBase Plate Stress Ratio:61.1% Pass

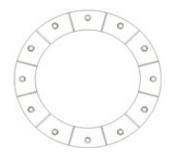
Stiffened				
AISC LRFD				
φ*Fy				
Y.L. Length:				
N/A, Roark				

#### **Stiffener Results**

Horizontal Weld: 69.3% Pass
Vertical Weld: 46.2% Pass
Plate Flex+Shear, fb/Fb+(fv/Fv)^2: 19.7% Pass
Plate Tension+Shear, ft/Ft+(fv/Fv)^2 69.4% Pass
Plate Comp. (AISC Bracket): 67.9% Pass

#### **Pole Results**

Pole Punching Shear Check: 9.3% Pass



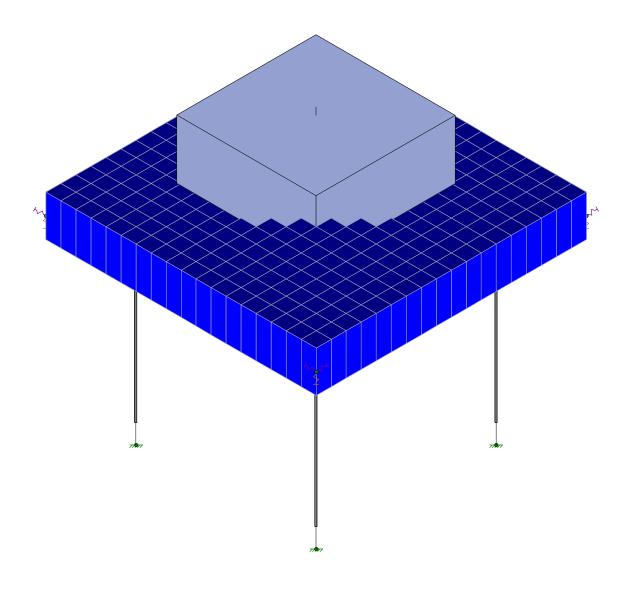


Analysis Date: 7/2/2018

<sup>\* 0 =</sup> none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

<sup>\*\*</sup> Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

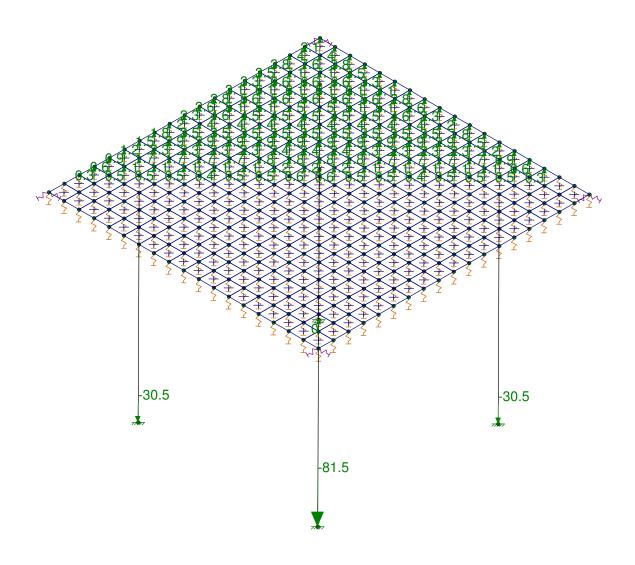




### **Envelope Only Solution**

Crown Castle		SK - 1	
ADB	West Hartford/I-84/X43 (BU 829013)	July 2, 2018 at 4:01 PM	
TEP No. 25680.161675		829013.02S_Foundation.r3d	





### Y-direction Reaction Units are k and k-ft

Crown Castle		SK - 2
ADB	West Hartford/I-84/X43 (BU 829013)	July 2, 2018 at 4:08 PM
TEP No. 25680.161675		829013.02S_Foundation.r3d



Company

: Crown Castle

: ADB

Job Number : TEP No. 25680.161675

Model Name : West Hartford/I-84/X43 (BU 829013)

July 2, 2018 4:08 PM

Checked By: AAS

#### **Concrete Properties**

	Label	E [ksi]	G [ksi]	Nu	Therm (\1E	.Density[lb/f	f'c[ksi]	Lambda	Flex Steel[	Shear Stee
1	Conc3000NW	3156	1372	.15	.6	145	3	1	60	60
2	Conc3500NW	3409	1482	.15	.6	145	3.5	1	60	60
3	Conc4000NW	3644	1584	.15	.6	145	4	1	60	60
4	Conc3000LW	2085	907	.15	.6	109.999	3	.75	60	60
5	Conc3500LW	2252	979	.15	.6	109.999	3.5	.75	60	60
6	Conc4000LW	2408	1047	.15	.6	109.999	4	.75	60	60

### **Member Primary Data**

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M1	N8	N12			1" WF Rock	Column	None	A722	Typical
2	M2	N7	N11			1" WF Rock	Column	None	A722	Typical
3	M3	N6	N10			1" WF Rock	Column	None	A722	Typical
4	M4	N5	N9			1" WF Rock	Column	None	A722	Typical
5	M5	TL1	N367			CRECT102X1	Column	Rectangular	Conc3000	Typical
6	M6	N367	TOWER			6' rigid offset	Column	None	RIGID	Typical

### Joint Loads and Enforced Displacements (BLC 1 : Dead)

	Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/f
1	TL1	L	Υ	-32.9

#### Joint Loads and Enforced Displacements (BLC 2 : Wind 0)

	Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/f
1	TL1	L	X	19.5
2	TL1		Mz	-1842.4

### Joint Loads and Enforced Displacements (BLC 3 : Wind 90)

	Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/f
1	TL1	L	Z	19.5
2	TL1	L	Mx	1842.4

#### Joint Loads and Enforced Displacements (BLC 4: Wind 45)

	Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/f
1	TL1	L	Χ	13.8
2	TL1	L	Mz	-1302.8
3	TL1	L	Z	13.8
4	TL1	L	Mx	1302.8

#### **Basic Load Cases**

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed	Area(Me	Surface(P
1	Dead	DL		-1		1				324
2	Wind 0	WL				2				
3	Wind 90	WL				2				
4	Wind 45	WL				4				
5	Prestress	None						4		



: Crown Castle : ADB

Company Designer Job Number

: TEP No. 25680.161675

Model Name : West Hartford/I-84/X43 (BU 829013)

July 2, 2018 4:08 PM

Checked By: AAS

### **Load Combinations**

	Description	So	P	S	BLC	Fac	BLC	Fac	.BLC	Fac	BLC	Fac	.BLC	Fac	.BLC	Fac	BLC	Fac	.BLC	Fac	.BLC	Fac	.BLC	Fac
1	1.2D+1.6Wind 0	Yes	Υ		1	1.2	2	1.6	5	1														
2	1.2D+1.6Wind 90	Yes	Υ		1	1.2	3	1.6	5	1														
3	1.2D+1.6Wind 45	Yes	Υ		1	1.2	4	1.6	5	1														
4	0.9D+1.6Wind 0	Yes	Υ		1	.9	2	1.6	5	1														
5	0.9D+1.6Wind 90	Yes	Υ		1	.9	3	1.6	5	1														
6	0.9D+1.6Wind 45	Yes	Υ		1	.9	4	1.6	5	1														
7	Prestress	Yes	Υ		5	1																		

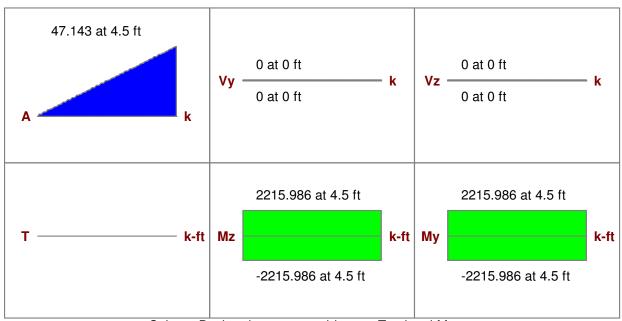
Column: M5

Shape: CRECT102X102 Concrete Stress Block: Rectangular

Material: Conc3000NW Cracked Sections Used: Yes Length: 4.5 ft Cracked 'I' Factor: .70

I Joint: TL1 Effective 'I': 6.31419e+6 in^4
J Joint: N367 Effective 'I': PCA Load Contour

Code Check: **0.570 (LC 1)**Report Based On 97 Sections



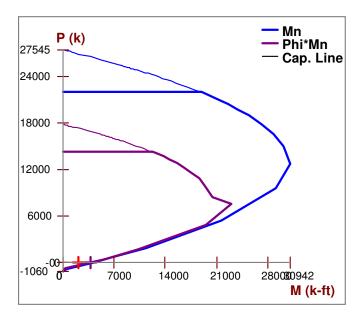
Column Design does not consider any Torsional Moments

#### Warning: Exact Integration selected but PCA method used Custom rebar layout does not meet min steel (As,min) per Global Parameters

#### ACI 318-11 Code Check

Gov LC	7	Bending Check Location	0.570 4.5 ft	Shear Check Location	0.000 (y) 0 ft
Gov Pu phi*Pn Phi eff.	0 k .9	Gov Muy Gov Muz phi*Mnoy phi*Mnoz	2215.986 k-ft 0 k-ft 9 k-ft	Gov Vuy Gov Vuz phi*Vny phi*Vnz	0 k 0 k 1111.305 k 1111.305 k
Tension Bar Fy Shear Bar Fy F'c Flex. Rebar Set Flex. Bars Shear Bars	60 ksi 60 ksi 3 ksi ASTM A615 9 #6 , 9 #6 #4 @6in	Concrete Weight  \( \lambda \)  E_Concrete  Shear Rebar Set  , 11 #6 , 11 #6	145 lb/ft^3 1 3156 ksi ASTM A615	Sway yy Sway zz Thres. Torsior	No No 917.543k-ft(LC:1)

#### **Column Interaction Diagram**



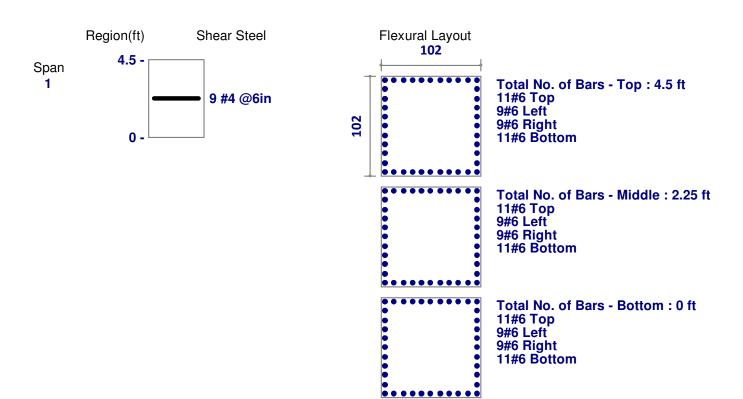
**Span Information** 

Column Steel

**Axial Span Results** 

**Bending Span Results** 

**Rebar Detailing** 



### Monopole on Mat Foundation with Rock Anchors - TIA-222-G

#### Site Data

Site Name: West Hartford/I-84/X43

CCI Number: BU 829013 TEP Job Number: 25680.161675

Mat and Pie	r Properties	
Mat Width	16.5	ft
Mat Length	16.5	ft
Mat Thickness	2.5	ft
Pier Type	Square	
Pier Width/Diam.	8.5	ft
Pier Height	4.5	ft

Soil Properties					
q <sub>allow</sub>	10.8	ksf			
FS	2.0				
Subgrade Mod.	390	kcf			
Rock Weight	160	pcf			
Rock Cone Angle	30	deg			

Rock Ancho	or Properties	
Type of Bar	WilliamsF	orm150
Bar Size	1.00	in
Net Area	0.85	in <sup>2</sup>
Ultimate Stress, Fu	150.0	ksi
Yield Stress, Fy	120.0	ksi
Bar Diameter	1.000	in
Steel/Grout Bond <sup>1</sup>	230	psi
Grout/Rock Allow Bond	50	psi
FS	2	
Drilled Shaft Diam.	3.75	in

<sup>&</sup>lt;sup>1</sup> Ultimate Bond Values

Factored Reactions from TNX					
Axial	39.493	k			
Shear	31.149	k			
Moment	2947.866	k-ft			

#### **Mat Foundation Results**

Bearing Stress	12.8	ksf
Bearing Capacity, $\phi q_{allow}$	16.3	ksf
% Capacity	78.9%	<b>Pass</b>

#### **Mat and Pier Structural Results**

Bending Moment	670.2	kft
Flexural Capacity,	1151.3	kft
% Capacity	58.2%	Pass

#### **Rock Anchor Steel Results**

Max Tension Force	81.5	k
Anchor Capacity, $\phi$ Pn	91.8	k
% Capacity	88.7%	<b>Pass</b>

#### **Rock Anchor Pullout Results**

Req. Bond Length, ld	12.5	ft
Req. Cone Height, h	12.2	ft
Total Req. Embedment	19.3	ft
Pullout Capacity, phiTn	97.9	k
% Capacity	83.2%	Pass



**Drilled Caisson Tool - Pier** 

Moment:

Axial (uplift):

Shear:

Axial (download):

Results Summary: LC1 LC2
Soil Interaction: N/A N/A
Foundation Structural: 34.3% 7.2%

West Hartford/I-84/X43 (BU 829013) TEP #: 25680.161675

Analysis:

Check:

ADB 7/2/2018 AAS 7/2/2018

Code Revisions: TIA-222-G ACI 318-11

LC1

872.05

39.49

31.15

kip-ft kip

kip

kip

LC2

192.08

91.50

6.78

Tower Type: Monopole

	Shaft Information	on
Diameter:	6.00	ft
Projection:	0.50	ft
Caisson Length:	4.50	ft
f'c:	3.000	ksi
Мах єс:	0.003	in/in

#### Cage 1 Reinforcement

Tie Bar Size: (fy = 60.0 ksi)4 **Clear Cover to Tie:** 3.00 in (Cage  $\emptyset$  = 63.87in) Tie Bar Spacing: 6.00 **Vertical Bar Size:** 9 **Vertical Bar Quantity:** 18 (ρ =0.442%) 60.0 ksi fy: 29,000 E: ksi



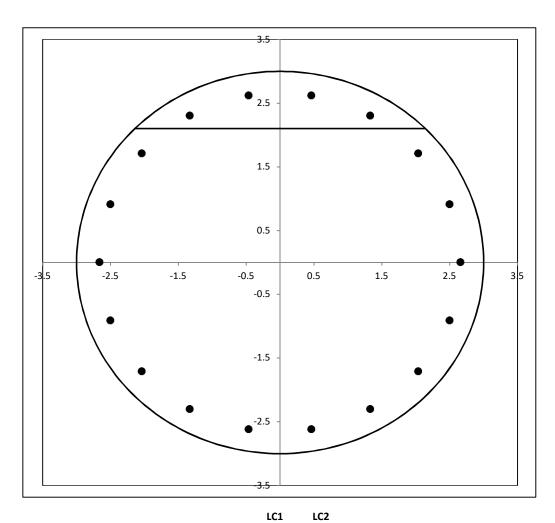
**Reinforcement Capacity** 

TEP #:

25680.161675

 Analysis:
 ADB
 7/2/2018

 Check:
 AAS
 7/2/2018



Vu = 31.1 6.8 kip
Vc = 448.2 451.0 kip
fy,tie = 60.0 Vs = 269.8 269.8 kip
$$\phi Vn = 538.5 540.6 \text{ kip}$$
Capacity = 5.8% 1.3%
PASS PASS

LC1 LC2
Mu = 872.1 192.1 kip-ft
$$\phi Mn = 2541.8 2655.4 \text{ kip-ft}$$
Capacity = 34.3% 7.2%

PASS

PASS

Date: May 9, 2018

2000 Corporate Drive

Canonsburg, PA 15317

Charles McGuirt Crown Castle

(724) 416-2000



Hudson Design Group LLC 45 Beechwood Drive N. Andover, MA 01845 (978) 557-5553

Subject: **Mount Structural Analysis** 

Carrier Designation: T-Mobile Equipment Change-Out

> Carrier Site Number: CT11178D

Carrier Site Name:

WEST HARTFORD/I-84/X43

Crown Castle Designation: Crown Castle BU Number:

829013

Crown Castle Site Name: WEST HARTFORD/I-84/X43

**Crown Castle JDE Number:** 496734 **Crown Castle PO Number:** 1181203 **Crown Castle Application Number:** 433326 Rev. 1

Engineering Firm Designation:

**Crown Castle Report Designation:** 

3712509

Site Data:

Structure Information:

467 South Quaker Lane, West Hartford, CT, 06110 Latitude: 41° 44' 55.59" Longitude: -72° 43' 52.86"

120 ft Monopole

**Tower Height & Type:** Mount Elevation:

120 ft

Mount Width & Type:

14 ft Platform

Dear Charles McGuirt,

Hudson Design Group LLC (HDG) is pleased to submit this "Mount Structural Analysis Report" to determine the structural integrity of T-Mobile's antenna mounting system with the proposed appurtenance and equipment addition on the abovementioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tieoff point for fall protection or rigging is not part of this document.

Based upon our analysis, we have determined the adequacy of the antenna mounting system that will support the existing and proposed loading to be:

Platform Mount (Single)

Insufficient

This analysis has been performed in accordance with the 2012 International Building Code and the TIA-222-G based on a basic wind speed of 105 mph as required for use in the TIA-222-G Standard Annex B. Exposure Category B with a maximum topographic factor, Kzt, of 1.0 and Risk Category II were used in this analysis.

We at HDG appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects, please give us a call.

Mount structural analysis prepared by: HDG Respectfully Submitted by:

Michael Cabral

Structural Dept. Head

Daniel P. Hamm, P.E.

Principal

May 9, 2018 CCI BU No: 829013 Page 2

#### **TABLE OF CONTENTS**

#### 1) INTRODUCTION

#### 2) ANALYSIS CRITERIA

- Table 1 Proposed Equipment Loading Information
- Table 2 Existing and Reserved Equipment Loading Information

#### 3) ANALYSIS PROCEDURE

- Table 3 Documents Provided
- 3.1) Analysis Method
- 3.2) Assumptions

#### 4) ANALYSIS RESULTS

- Table 4 Mount Component Stresses vs. Capacity
- 4.1) Recommendations

#### 5) APPENDIX A

Wire Frame and Rendered Models

#### 6) APPENDIX B

**RAM Elements Input Calculations** 

#### 7) APPENDIX C

RAM Elements Analysis Output

#### 8) APPENDIX D

**Additional Calculations** 

May 9, 2018 CCI BU No: 829013 Page 3

#### 1) INTRODUCTION

This mount is a 14' low profile platform. No original structural design documents or fabrication drawings were available for the existing mounts. A mount mapping was not performed at this site. HDG performed a visual assessment using field photographs and mount mapping data from similar mounts to perform this analysis. The mount is installed at an elevation of 120 ft on the 120 ft Monopole.

#### 2) ANALYSIS CRITERIA

The mount structural analysis was conducted in accordance with the requirements of TIA-222-G, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a basic wind speed of 105 mph with no ice, 50 mph with a 2.28 inch escalated ice thickness, Exposure Category B and Topographic category 1 with a crest height of 0 ft. In addition, the mounts have been analyzed for various live loading conditions consisting of a 250 pound man live load applied individually at the midpoint and cantilevered ends of horizontal members as well as a 500 pound man live load applied individually at mount pipe locations using a 3-second gust wind speed of 30 mph.

Table 1 - Proposed Equipment Loading Information

Mount Centerline (ft)	Antenna Centerline (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Proposed Mount Type	Note
120	120	3	RFS/Celwave	APXVAARR24_43-U-NA20	-	1,2
120	120	3	Ericsson	4449 B12/B71 RRH		1,2

Notes:

Proposed Equipment

2) Existing Mount to Remain

Table 2 - Existing and Reserved Equipment Loading Information

Mount Centerline (ft)		Number of Antennas	Antenna Manufacturer	Antenna Model	Existing Mount Type	Note
120	120	6	Ericsson	AIR 32 B2a/B66Aa	14' Platform	1
	120	3	Ericsson	KRY 112 144/1 TMA	14' Platform	1

Notes:

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided							
Document	Remarks	Reference	Source				
RFDS	T-Mobile	-	ON FILE				

<sup>1)</sup> Existing Equipment

# 3.1) Analysis Method

RAM Elements (Version 14.0.1), a commercially available analysis software package, was used to create a three-dimensional model of the antenna mounting system and calculate member stresses for various loading cases.

## 3.2) Assumptions

- 1) The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specifications.
- 2) The configuration of antennas, mounts, and other appurtenances are as specified in Table 1 and 2 and the referenced drawings.
- 3) All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
- Steel grades have been assumed as follows, unless noted otherwise:

Channel, Solid Round, Angle, Plate HSS (Square, Rectangular) Pipe

**Connection Bolts** 

ASTM A36 (GR 36)

ASTM A500 (GR B)

**ASTM A53 (GR 53)** 

ASTM A325

This analysis may be affected if any assumptions are not valid or have been made in error. Crown Castle should be notified to determine the effect on the structural integrity of the antenna mounting system.

#### 4) ANALYSIS RESULTS

Table 4(a) - Mount Component Stresses vs. Capacity (Platform Mount, Alpha Sector)

Notes	Component	Member No.	Centerline (ft)	% Capacity	Pass / Fail
1	Face Horizontal	84	152	169	Fail
1	Standoff Members	36	152	171	Fail
2	Mount-to-Tower Connection	=	152	84	Pass

Table 4(b) - Mount Component Stresses vs. Capacity (Platform Mount, Beta Sector)

Notes	Component	Beam No.	Centerline (ft)	% Capacity	Pass / Fail
1	Face Horizontal	84	152	169	Fail
1	Standoff Members	36	152	171	Fail
2	Mount-to-Tower Connection	14	152	84	Pass

Table 4(c) - Mount Component Stresses vs. Capacity (Platform Mount, Gamma Sector)

Notes	Component	Beam No.	Centerline (ft)	% Capacity	Pass / Fail
1	Face Horizontal	84	152	169	Fail
1	Standoff Members	36	152	171	Fail
2	Mount-to-Tower Connection	7=	152	84	Pass

Structure Rating (max from all components) =	181%
Structure Rating (max from all components) –	101%

#### Notes:

- See additional documentation in "Appendix C Analysis Output" for calculations supporting the % Capacity 1) consumed.
- 2) See additional documentation in "Appendix D - Additional Calculations" for calculations supporting the % capacity consumed.

## 4.1) Recommendations

The Mount has insufficient capacity to support the proposed loading. We recommend installing a handrail reinforcement kit.

May 9, 2018 CCI BU No: 829013 Page 5

# APPENDIX A WIRE FRAME AND RENDERED MODELS



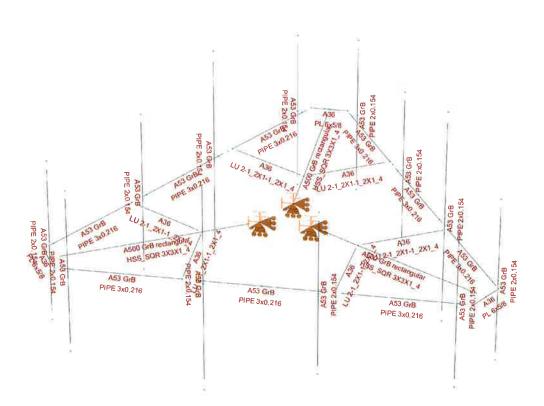
Current Date: 5/9/2018 2:19 PM
Units system: English
File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\CROWN CASTLE\829013\829013.etz\







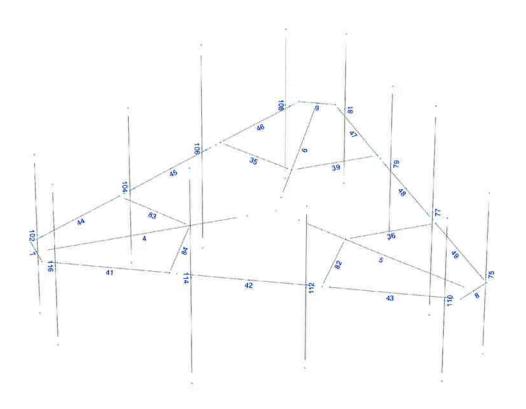
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Units system: English
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# APPENDIX B RAM ELEMENTS INPUT CALCULATIONS

Date:

5/9/2018

Project Name: WEST HARTFORD/I-84/X43

Project Number: 829013

Designed By: BD Checked By: MSC



## 2.6.5.2 Velocity Pressure Coeff:

$$K_z$$
= 2.01  $(z/z_g)^{2/\alpha}$ 

120 (ft) Z=

 $Z_g =$ 

1200 (ft)

K<sub>z</sub>=

1.041

7.0 α=

 $Kzmin \le Kz \le 2.01$ 

## Table 2-4

Exposure	Z <sub>g</sub>	α	K <sub>zmin</sub>	K <sub>e</sub>
В	1200 ft	7.0	0.70	0.9
С	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

## 2.6.6.4 Topographic Factor:

## Table 2-5

Topo. Category	K <sub>t</sub>	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} = [1 + (K_e K_t/K_h)]^2$$

$$K_h = e^{-(f*z/H)}$$

# Kzt= #DIV/0! (If Category 1 then K zt =1.0)

#DIV/0! K<sub>h</sub>=

K<sub>e</sub>=

0 (from Table 2-4)

 $K_t =$ 

0 (from Table 2-5)

f=

0 (from Table 2-5)

Category= 1

120 z=

H=

0 (Ht. of the crest above surrounding terrain)

 $K_{zt} =$ 1.00

 $K_{iz} =$ 1.14 (from Sec. 2.6.8)

# 2.6.8 Design Ice Thickness

Max Ice Thickness =

1.00 in  $t_i =$ 

 $t_{iz} = 2.0*t_i*I*K_{iz}*(Kzt)^{0.35}$ 

t<sub>iz</sub> = 2.28 in Date:

5/9/2018

Project Name: WEST HARTFORD/I-84/X43

Project Number: 829013

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#### 2.6.7 Gust Effect Factor

# 2.6.7.1 Self Supporting Lattice Structures

Gh = 1.0 Latticed Structures > 600 ft

Gh = 0.85 Latticed Structures 450 ft or less

Gh = 0.85 + 0.15 [h/150 - 3.0]

h= ht. of structure

h=

120

Gh= 0.85

2.6.7.2 Guyed Masts

Gh=

2.6.7.3 Pole Structures

Gh= 1.1

2.6.9 Appurtenances

Gh= 1.0

# 2.6.7.4 Structures Supported on Other Structures

(Cantilivered tubular or latticed spines, pole, structures on buildings (ht.: width ratio > 5)

Gh=

1.35

Gh=

1.00

0.85

## 2.6.9.2 Design Wind Force on Appurtenances

F= qz\*Gh\*(EPA)A

 $q_z = 0.00256*K_z*K_{zt}*K_d*V_{max}^2*I$ 

 $K_z = 1.041$ 

 $K_{zt} =$ 

q<sub>z</sub>=

27.91 6.33

2.28

K<sub>d</sub>= 0.95

q<sub>z (ice)</sub>= q<sub>z (30)</sub>=

 $V_{max} =$ 

105 mph

V<sub>max (ice)</sub>=

50 mph

V<sub>30</sub>=

30 mph

- 30

1.0

1.0

#### Table 2-2

Structure Type	Wind Direction Probability Factor, Kd
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95

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Project Name: WEST HARTFORD/I-84/X43

Project Number: 829013

Designed By: BD Checked By: MSC



## Determine Ca:

Table 2-8

	For	ce Coefficients (Ca) for Ap	purtenances	
	Member Type	Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
	member type	Ca	Ca	Ca
	Flat	1.2	1.4	2.0
Round	C < 32	0.7	0.0	4.2
	(Subcritical)	0.7	0.8	1.2
Ī	32 ≤ C ≤ 64	. 0.495	0.415	-1.0
	(Transitional)	3.76/(C <sup>0.485</sup> )	3.37/(C <sup>0,415</sup> )	38.4/(C <sup>-1.0</sup> )
	C > 64	0.5	0.5	0.5
	(Supercritical)	0.5	0.6	0.6

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.

(Aspect ratio is independent of the spacing between support points of a linear appurtenance,

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness =	2.28	in	Angle =	0 (deg)		Equival	ent Angle =	180 (deg)	
<u>Appurtenances</u>	<u>Height</u>	Width	<u>Depth</u>	Flat Area	Aspect Ratio	<u>Ca</u>	Force (lbs)	Force (lbs) (w/ lce)	Force (lbs) (30 mph)
APXVAARR24_43-U-NA20 Antenna	95.9	24.0	8.7	15.98	4.00	1.27	565	160	46
AIR 32 B2a/B66Aa Antenna	. 56.6	12.9	8.7	5.07	4.39	1.28	182	60	15
4449 B12/B71 RRH	15.0	13.2	9.3	1.38	1.14	1.20	46	18	4
KRY 112 144/1 TMA	6.9	6.1	2.8	0.29	1.13	1.20	10	6	1
2" Pipe	2.4	12.0		0.20	0.20	1.20	7	6	1
3" Pipe	3.5	12.0		0.29	0.29	1.20	10	7	1
L2-1/2x1-1/2	2.5	12.0		0.21	0.21	2.00	12	10	1
HSS 3x3	3.0	12.0		0.25	0.25	2.00	14	11	1

**Date:** 5/9/2018

Project Name: WEST HARTFORD/i-84/X43

Project Number: 629013
Designed By: BD Checked By: MSC



					ID LOADS							
Angle = 30	(deg)		Ice Thick	ness =	2.28	in.			Equivale	ent Angle =	210	(deg)
WIND LOADS WITH NO ICE:												
Appurtenances	Height	Width	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Aspect Ratio	Aspect Ratio	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
APXVAARR24_43-U-NA20 Antenna	95,9	24.0	8.7	15.98	5.79	4.00	11.02	1.27	1,53	565	248	486
AIR 32 B2a/B66Aa Antenna	56.6	12.9	8.7	5.07	3.42	4.39	6.51	1.28	1.38	182	132	169
4449 B12/B71 RRH	15.0	13.2	9.3	1.38	0.97	1.14	1.61	1.20	1.20	46	32	43
KRY 112 144/1 TMA	6.9	6.1	2.8	0.29	0.13	1.13	2.46	1.20	1.20	10	4	8
WIND LOADS WITH ICE:												
APXVAARR24_43-U-NA20 Antenna	100.5	28,6	13.3	19.92	9.24	3.52	7.58	1.25	1.42	157	83	139
AIR 32 B2a/B66Aa Antenna	61.2	17.5	13.3	7.41	5.63	3.50	4.61	1.24	1,29	58	46	55
4449 B12/B71 RRH	19.6	17.8	13.9	2.41	1.88	1,10	1,41	1,20	1,20	18	14	17
KRY 112 144/1 TMA	11.5	10.7	7.4	0.85	0.58	1,08	1,56	1.20	1.20	6	4	6
WIND LOADS AT 30 MPH:												
APXVAARR24_43-U-NA20 Antenna	95.9	24.0	8,7	15.98	5.79	4.00	11.02	1.27	1,53	46	20	40
AIR 32 B2a/B66Aa Antenna	56.6	12.9	8.7	5.07	3.42	4.39	6,51	1.28	1,38	15	11	14
4449 B12/B71 RRH	15.0	13.2	9.3	1.38	0.97	1.14	1,61	1,20	1,20	4	3	3
KRY 112 144/1 TMA	6.9	6.1	2.8	0.29	0.13	1.13	2.46	1.20	1.20	1	0	1

Date:

5/9/2018

Project Name: WEST HARTFORD/I-84/X43

Project Number: 829013

Designed By: BD Checked By: MSC



WIND LOADS Angle = 60 (deg) Ice Thickness = 2.28 in. Equivalent Angle = 240 (deg) WIND LOADS WITH NO ICE: Appurtenances <u>Height</u> Width Depth Flat Area Flat Area Ca Ca Force (lbs) Force (lbs) Force (lbs) Ratio Ratio (side) (side) (normal) (side) (normal) (normal) (angle) (normal) (side) APXVAARR24\_43-U-NA20 Antenna 95.9 24.0 15.98 5.79 4.00 11.02 1.27 1.53 565 248 327 AIR 32 BZa/B66Aa Antenna 56.6 12.9 5.07 3.42 4.39 6.51 1.28 1.38 182 132 144 4449 B12/B71 RRH 15.0 13.2 1.38 0.97 1.20 1.20 46 32 36 9.3 1,14 1,61 0.13 10 6 KRY 112 144/1 TMA 6.9 6.1 2,8 0.29 1,13 2,46 1,20 1,20 4 WIND LOADS WITH ICE: 19.92 9.24 102 APXVAARR24\_43-U-NA20 Antenna 100.5 28.6 3.52 7.58 1.25 1.42 157 83 13.3 AIR 32 B2a/B66Aa Antenna 61.2 17.5 13.3 7.41 5.63 3.50 4.61 1.24 1.29 58 46 49 15 4449 B12/B71 RRH 19.6 17.8 13.9 2.41 1.88 1,10 1.41 1.20 1.20 18 14 KRY 112 144/1 TMA 11.5 10.7 7.4 0.85 0.58 1.08 1.56 1,20 1,20 6 5 WIND LOADS AT 30 MPH: APXVAARR24\_43-U-NA20 Antenna 95.9 24.0 15.98 5.79 4.00 11.02 1.27 1.53 46 20 27 3.42 15 12 AIR 32 B2a/B66Aa Antenna 56.6 12.9 5.07 4.39 6.51 1.28 1.38 11 8.7 1.38 0.97 3 4449 B12/B71 RRH 1.20 3 15.0 13.2 9.3 1.14 1.61 1.20 KRY 112 144/1 TMA 6.9 6.1 2.8 0.29 0.13 1.13 2.46 1.20 1,20 1 0 0

Date:

5/9/2018

Project Name: WEST HARTFORD/I-84/X43

Project Number: 829013

Designed By: BD Checked By: MSC



WIND LOADS Ice Thickness = 2.28 in. Equivalent Angle = 270 (deg) Angle = 90 (deg) WIND LOADS WITH NO ICE: Height Width Flat Area Flat Area Ca Force (lbs) Force (lbs) Force (lbs) Appurtenances Depth Ratio Ratio Ca (side) (normal) (side) (normal) (side) (normal) (side) (normal) (angle) 248 15.98 5.79 565 248 APXVAARR24\_43-U-NA20 Antenna 95.9 24.0 8.7 4.00 11.02 1.27 1.53 132 AIR 32 B2a/B66Aa Antenna 56.6 12.9 8.7 5.07 3.42 4.39 6.51 1.28 1.38 182 132 4449 B12/B71 RRH 9.3 1.38 0.97 1.20 1.20 46 32 32 15.0 13.2 1.14 1,61 0.13 10 4 KRY 112 144/1 TMA 0.29 6.9 6.1 2.8 1,13 2.46 1,20 1.20 WIND LOADS WITH ICE: 13.3 19.92 9.24 3.52 7.58 1.25 1.42 157 83 APXVAARR24\_43-U-NA20 Antenna 100.5 28.6 7.41 46 AIR 32 B2a/B66Aa Antenna 61.2 17.5 13.3 5.63 3.50 4.61 1.24 1.29 58 46 14 2.41 1.88 18 4449 B12/B71 RRH 19.6 17.8 13.9 1,10 1.41 1.20 1.20 14 KRY 112 144/1 TMA 11.5 10.7 0.85 0.58 1.20 1.20 6 4 WIND LOADS AT 30 MPH: 20 APXVAARR24\_43-U-NA20 Antenna 95.9 24.0 8.7 15.98 5.79 4.00 11.02 1.27 1.53 46 20 AIR 32 B2a/B66Aa Antenna 56.6 12.9 8.7 5.07 3.42 4.39 6.51 1.28 1.38 15 11 11 1.38 4 3 4449 B12/B71 RRH 15.0 13.2 9.3 0.97 1.14 1.61 1.20 1,20 0.13 1 0 KRY 112 144/1 TMA 6.9 6.1 2.8 0.29 1.13 2.46 1.20 1.20 0

Dale:

5/9/2018

Project Name: WEST HARTFORD/I-84/X43

Project Number: 829013

Designed By: BD Checked By: MSC



WIND LOADS Angle = 120 (deg) Ice Thickness = 2.28 in. Equivalent Angle = 300 (deg) WIND LOADS WITH NO ICE: Appurtenances Height Width Depth Flat Area Flat Area Ratio Force (lbs) Force (lbs) Force (lbs) Ca Ca Ratio (normal) (normal) (side) (normal) (side) (side) (normal) (side) (angle) APXVAARR24\_43-U-NA20 Antenna 95.9 24.0 8.7 15.98 5.79 4.00 11.02 1,27 1.53 565 248 327 AIR 32 B2a/B66Aa Antenna 5.07 3.42 56.6 12.9 8.7 4.39 6.51 1.28 1.38 182 132 144 4449 B12/B71 RRH 15.0 1.38 0.97 1.14 46 36 13.2 9.3 1,61 1.20 1.20 32 KRY 112 144/1 TMA 6.9 0.29 0.13 1.13 10 6 6.1 2.8 2.46 1.20 1.20 4 WIND LOADS WITH ICE: APXVAARR24\_43-U-NA20 Antenna 19.92 9.24 3.52 100.5 28.6 13.3 7.58 1.25 1.42 157 83 102 AIR 32 B2a/B66Aa Antenna 61.2 17.5 13.3 7.41 5.63 3.50 4,61 1,24 1.29 58 46 49 4449 B12/B71 RRH 19.6 17.8 2.41 1.88 1,10 1.41 1.20 1.20 18 15 KRY 112 144/1 TMA 11.5 10.7 0.85 0.58 1.08 5 1.56 1.20 1.20 WIND LOADS AT 30 MPH: APXVAARR24\_43-U-NA20 Antenna 95.9 24.0 15.98 5.79 4.00 46 20 27 8.7 1.27 11.02 1.53 AIR 32 B2a/B66Aa Antenna 5.07 3.42 4.39 15 11 12 56.6 12.9 8.7 6.51 1,28 1.38 4449 B12/B71 RRH 1.38 0.97 1.14 4 3 15.0 13.2 9.3 1.61 1.20 1.20 3 KRY 112 144/1 TMA 0.29 0.13 1.13 1 0 6.9 6.1 2.8 2.46 1.20 1-20 0

**Dale:** 5/9/2018

Project Name: WEST HARTFORD/I-84/X43

Project Number: 829013
Designed By: BD Checked By: MSC



Angle = 150	(deg)		Ice Thick	ness =	2.28	In.		- 1	Equiva	lent Angle =	330	(deg)
ringia 250	(408)		ICC TIMES		2.20				cquive	ient Angle -	330	(GCE)
WIND LOADS WITH NO ICE:												
Appurtenances	<u>Height</u>	Width	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	<u>Ca</u> (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs (angle)
APXVAARR24_43-U-NA20 Antenna	95.9	24.0	8.7	15.98	5.79	4.00	11.02	1.27	1,53	565	248	486
AIR 32 B2a/B66Aa Antenna	56.6	12.9	8.7	5.07	3.42	4.39	6.51	1.28	1.38	182	132	169
4449 B12/B71 RRH	15.0	13.2	9.3	1.38	0.97	1.14	1.61	1.20	1.20	46	32	43
KRY 112 144/1 TMA	6.9	6.1	2.8	0.29	0.13	1.13	2.46	1.20	1.20	10	4	8
WIND LOADS WITH ICE:												
APXVAARR24_43-U-NA20 Antenna	100.5	28.6	13.3	19.92	9,24	3.52	7.58	1.25	1.42	157	\$3	139
AIR 32 B2a/B66Aa Antenna	61,2	17.5	13.3	7.41	5.63	3,50	4.61	1.24	1.29	58	46	55
4449 B12/B71 RRH	19.6	18.2	13.9	2.47	1.88	1.07	1.41	1.20	1.20	19	14	18
KRY 112 144/1 TMA	11.5	16.3	7.4	1.30	0.58	0.70	1.56	1.20	1.20	10	4	8
WIND LOADS AT 30 MPH:												
APXVAARR24_43-U-NA20 Antenna	95.9	24.0	8.7	15.98	5.79	4.00	11.02	1.27	1.53	46	20	40
AIR 32 B2a/B66Aa Antenna	56.6	12.9	8.7	5.07	3.42	4.39	6.51	1.28	1.38	15	11	14
4449 B12/B71 RRH	15.0	13.2	9.3	1.38	0.97	1.14	1.61	1.20	1.20	4	3	3

**Date:** 5/9/2018

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#### **ICE WEIGHT CALCULATIONS**

Thickness of ice:

1 in.

Density of ice:

56 pcf

## APXVAARR24\_43-U-NA20 Antenna

Weight of ice based on total radial SF area:

Height (in):

95.9

Width (in):

24.0

Depth (in):

8.7

Total weight of ice on object:

234 lbs

Weight of object:

128 lbs

Combined weight of ice and object:

362 lbs

#### 4449 B12/B71 RRH

Weight of ice based on total radial SF area:

Height (in):

15.0

Width (in):

13.2

Depth (in):

9.3

Total weight of ice on object:

35 lbs

Weight of object:

74 lbs

Combined weight of ice and object:

109 lbs

# 2" pipe

Per foot weight of ice:

diameter (in):

2.38

Per foot weight of ice on object:

4 plf

#### HSS 3x3

Weight of ice based on total radial SF area:

Height (in):

3

Width (in):

3

Per foot weight of ice on object:

6 plf

# PL 6x5/8

Weight of ice based on total radial SF area:

Height (in):

6

Width (in):

0.625

Per foot weight of ice on object:

7 plf

# AIR 32 B2a/B66Aa Antenna

Weight of ice based on total radial SF area:

Height (in):

56.6

Width (in):

12.9

Depth (in):

8.7

Total weight of ice on object:

97 lbs

Weight of object:

133 lbs

Combined weight of ice and object:

230 lbs

# KRY 112 144/1 TMA

Weight of ice based on total radial SF area:

Height (in):

6.9

Width (in):

6.1

Depth (in):

2.8

Total weight of ice on object:

7 lbs

Weight of object:

11 lbs

Combined weight of ice and object:

18 lbs

# 3" Pipe

Per foot weight of ice:

diameter (in):

3.5

Per foot weight of ice on object:

5 plf

# L2-1/2x1-1/2x1/4 Angles

Weight of ice based on total radial SF area:

Thickness (in):

0.25

Height (in):

2.5

Width (in):

1.5

Per foot weight of ice on object:

5 plf



Current Date: 5/9/2018 2:20 PM

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File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\CROWN CASTLE\829013\829013.etz\

# **Load data**

**GLOSSARY** 

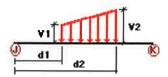
Comb

: Indicates if load condition is a load combination

## **Load Conditions**

Condition	Description	Comb.	Category
DL	Dead Load	No	DL
W0	Wind Load 0/60/120 deg	No	WIND
W30	Wind Load 30/90/150 deg	No	WIND
Di	Ice Load	No	LL
Wi0	Ice Wind Load 0/60/120 deg	No	WIND
Wi30	Ice Wind Load 30/90/150 deg	No	WIND
WL0	WL 30 mph 0/60/120 deg	No	WIND
WL30	WL 30 mph 30/90/150 deg	No	WIND
LL1	250 lb Live Load Center of Mount	No	LL
LL2	250 lb Live Load End of Mount	No	LL
LLa1	500 lb Live Load Antenna 1	No	LL
LLa3	500 lb Live Load Antenna 3	No	LL
LLa4	500 lb Live Load Antenna 4	No	LL
W180	-W0	Yes	
W210	-W30	Yes	
Wi180	-Wi0	Yes	
Wi210	-Wi30	Yes	
WL180	-WL0	Yes	
WL210	-WL30	Yes	

# **Distributed force on members**

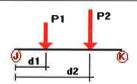


Condition	Member	Dir1	<b>Val1</b> [Kip/ft]	<b>Val2</b> [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
DL	41	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	42	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	43	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	44	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	45	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	46	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	47	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	48	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	49	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
W0	4	Z	-0.014	-0.014	0.00	Yes	100.00	Yes

	_							
	5	Z	-0.014	-0.014	0.00	Yes	100.00	Yes
	35	Z	-0.012	-0.012	0.00	Yes	100.00	Yes
	36	Z	-0.012	-0.012	0.00	Yes	100.00	Yes
	39	Z	-0.012	-0.012	0.00	Yes	100.00	Yes
	41	Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	42	Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	43	Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	44	Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	45	Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	46	Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	47	Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	48	Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	49	Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	75	Z	-0.007	-0.007	0.00	Yes	100.00	Yes
	77	Z	-0.007	-0.007	0.00	Yes	100.00	Yes
	79	Z	-0.007	-0.007	0.00	Yes	100.00	Yes
	81	Z	-0.007	-0.007	0.00	Yes	100.00	Yes
	83	Z	-0.012	-0.012	0.00	Yes	100.00	Yes
	102	Z	-0.007	-0.007	0.00	Yes	100.00	Yes
	104	Z	-0.007	-0.007	0.00	Yes	100.00	Yes
	106	Z	-0.007	-0.007	0.00	Yes	100.00	Yes
	108	Z	-0.007	-0.007	0.00	Yes	100.00	Yes
W30	4	X	-0.014	-0.014	0.00	Yes	100.00	Yes
	5	×	-0.014	-0.014	0.00	Yes	100.00	Yes
	6	×	-0.014	-0.014	0.00	Yes	100.00	Yes
	35	×	-0.012	-0.012	0.00	Yes	100.00	Yes
	36	×	-0.012	-0.012	0.00	Yes	100.00	Yes
	39	×	-0.012	-0.012	0.00	Yes	100.00	Yes
	44	×	-0.01	-0.01	0.00	Yes	100.00	Yes
	45	×	-0.01	-0.01	0.00	Yes	100.00	Yes
	46	×	-0.01	-0.01	0.00	Yes	100.00	Yes
	47	×	-0.01	-0.01	0.00	Yes	100.00	Yes
	48	×	-0.01	-0.01	0.00	Yes	100.00	Yes
	49	×	-0.01	-0.01	0.00	Yes	100.00	Yes
	75	×	-0.007	-0.007	0.00	Yes	100.00	Yes
	77	×	-0.007	-0.007	0.00	Yes	100.00	Yes
	79	×	-0.007	-0.007	0.00	Yes	100.00	Yes
	81	×	-0.007	-0.007	0.00	Yes	100.00	Yes
	82	×	-0.012	-0.012	0.00	Yes	100.00	Yes
	83	×	-0.012	-0.012	0.00	Yes	100.00	Yes
	84	×	-0.012	-0.012	0.00	Yes	100.00	Yes
	102	X	-0.007	-0.007	0.00	Yes	100.00	Yes
	104	×	-0.007	-0.007	0.00	Yes	100.00	Yes
	106	×	-0.007	-0.007	0.00	Yes	100.00	Yes
	108	×	-0.007	-0.007	0.00	Yes	100.00	Yes
	110	X	-0.007	-0.007	0.00	Yes	100.00	Yes
	112	×	-0.007	-0.007	0.00	Yes	100.00	Yes
	114	X	-0.007	-0.007	0.00	Yes	100.00	Yes
	116	×	-0.007	-0.007	0.00	Yes	100.00	Yes
Di	4	Y	-0.006	-0.006	0.00	Yes	100.00	Yes
	5	Υ	-0.006	-0.006	0.00	Yes	100.00	Yes
	6	Y	-0.006	-0.006	0.00	Yes	100.00	Yes
	7	Y	-0.007	-0.007	0.00	Yes	100.00	Yes
	8	Y	-0.007	-0.007	0.00	Yes	100.00	Yes
	9	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	35	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
	36	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	39	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	41	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	42	Ý	-0.005	-0.005	0.00	Yes	100.00	Yes
		17.	0.000	0.000	0.00	. 55	100.00	1 00

43	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
44	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
45	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
46	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
47	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
48	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
49	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
75	* Y	-0.004	-0.004	0.00	Yes	100.00	Yes
77	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
79	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
81	Y	-0.004	-0.004	0.00	Yes	100.00	Yes
82	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
83	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
84	Υ	-0.005	-0.005	0.00	Yes	100.00	Yes
102	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
104	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
106	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
108	Y	-0.004	-0.004	0.00	Yes	100.00	Yes
110	Y	-0.004	-0.004	0.00	Yes	100.00	Yes
112	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
114	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
116	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes

# **Concentrated forces on members**



Condition	Member	Dir1	<b>Value1</b> [Kip]	Dist1 [ft]	%
		********	0.007		<del>egistere</del>
DL	75	У	-0.067	0.64	No
		У	-0.067	5.36	No
		У	-0.011	2.00	No
	77	У	-0.064	0.00	No
		У	-0.064	8.00	No
	79	у	-0.074	2.00	No
	81	у	-0.067	0.64	No
		у	-0.067	5.36	No
		у	-0.011	2.00	No
	102	y	-0.067	0.64	No
		y	-0.067	5.36	No
		у	-0.011	2.00	No
	104	у	-0.074	2.00	No
	106	у	-0.064	0.00	No
		у	-0.064	8.00	No
	108	у	-0.067	0.64	No
		у	-0.067	5.36	No
		у	-0.011	2.00	No
	110	y	-0.067	0.64	No
		ý	-0.067	5.36	No
		y	-0.011	2.00	No
	112	y	-0.074	2.00	No
	114	y	-0.064	0.00	No
		7	0.001	0.00	140

		У	-0.064	8.00	No
	116	У	-0.067	0.64	No
		у	-0.067	5.36	No
		У	-0.011	2.00	No
W0	75	z	-0.072	0.64	No
		z	-0.072	5.36	No
	77	Z	-0.164	0.00	No
		Z	-0.164	8.00	No
	79	z	-0.036	2.00	No
	81	Z	-0.072	0.64	No
		z	-0.072	5.36	No
	102	z	-0.072	0.64	No
		Z	-0.072	5.36	No
	104	z	-0.036	2.00	No
	106	z	-0.164	0.00	No
		z	-0.164	8.00	No
	108	Z	-0.072	0.64	No
		z	-0.072	5.36	No
	110	z	-0.091	0.64	No
		z	-0.091	5.36	No
	112	z	-0.046	2.00	No
	114	z	-0.283	0.00	No
		z	-0.283	8.00	No
	116	z	-0.091	0.64	No
		z	-0.091	5.36	No
W30	75	×	-0.085	0.64	No
		x	-0.085	5.36	No
		×	-0.008	2.00	No
	77	×	-0.243	0.00	No
		×	-0.243	8.00	No
	79	x	-0.043	2.00	No
	81	×	-0.085	0.64	No
		×	-0.085	5.36	No
		×	-0.008	2.00	No
	102	x	-0.085	0.64	No
		×	-0.085	5.36	No
		×	-0.008	2.00	No
	104	x	-0.043	2.00	No
	106	x	-0.243	0.00	No
		×	-0.243	8.00	No
	108	×	-0.085	0.64	No
		×	-0.085	5.36	No
		x	-0.008	2.00	No
	110	x	-0.066	0.64	No
		×	-0.066	5.36	No
		×	-0.004	2.00	No
	112	×	-0.032	2.00	No
	114	×	-0.124	0.00	No
		×	-0.124	8.00	No
	116	×	-0.066	0.64	No
		×	-0.066	5.36	No
		x	-0.004	2.00	No
Di	75	y	-0.049	0.64	No
	. •	y	-0.049	5.36	No
		y	-0.007	2.00	No
	77	y	-0.117	0.00	No
	.,	y	-0.117	8.00	No
	79	y	-0.035	2.00	No
	81	y	-0.049	0.64	No
	O I		-0.049	5.36	No
		У	-0.0+3	5.50	NO

		У	-0.007	2.00	No
	102	У	-0.049	0.64	No
		у	-0.049	5.36	No
		ý	-0.007	2.00	No
	104		-0.035	2.00	No
		У			
	106	У	-0.117	0.00	No
		У	-0.117	8.00	No
	108	У	-0.049	0.64	No
		У	-0.049	5.36	No
		y	-0.007	2.00	No
	110	у	-0.049	0.64	No
		ý	-0.049	5.36	No
			-0.007	2.00	No
	110	У			
	112	У	-0.035	2.00	No
	114	У	-0.117	0.00	No
		У	-0.117	8.00	No
	116	У	-0.049	0.64	No
		У	-0.049	5.36	No
		у	-0.007	2.00	No
Wi0	75	z	-0.025	0.64	No
	, -	z	-0.025	5.36	No
	77				
	11	Z	-0.051	0.00	No
		Z	-0.051	8.00	No
	79	Z	-0.015	2.00	No
	81	Z	-0.025	0.64	No
		Z	-0.025	5.36	No
	102	Z	-0.025	0.64	No
		Z	-0.025	5.36	No
	104	z	-0.015	2.00	No
	106	z	-0.051	0.00	No
		z	-0.051	8.00	No
	108				
	100	Z	-0.025	0.64	No
	440	Z	-0.025	5.36	No
	110	Z	-0.03	0.64	No
		Z	-0.03	5.36	No
	112	Z	-0.018	2.00	No
	114	Z	-0.08	0.00	No
		Z	-0.08	8.00	No
	116	Z	-0.03	0.64	No
		Z	-0.03	5.36	No
Wi30	75	x	-0.028	0.64	No
		x	-0.028	5.36	No
			-0.006	2.00	No
	77	x			
	7.7	×	-0.07	0.00	No
		×	-0.07	8.00	No
	79	X	-0.017	2.00	No
	81	×	-0.028	0.64	No
		×	-0.028	5.36	No
		X	-0.006	2.00	No
	102	×	-0.028	0.64	No
		×	-0.028	5.36	No
		×	-0.006	2.00	No
	104		-0.017	2.00	No
		×			
	106	X	-0.07	0.00	No
		×	-0.07	8.00	No
	108	×	-0.028	0.64	No
		×	-0.028	5.36	No
		x	-0.006	2.00	No
	110	×	-0.023	0.64	No
		×	-0.023	5.36	No
		100			

		x	-0.004	2.00	No
	112	×	-0.014	2.00	No
	114	×	-0.042	0.00	No
		×	-0.042	8.00	No
	116	x	-0.023	0.64	No
		×	-0.023	5.36	No
		×	-0.004	2.00	No
WL0	75	z	-0.006	0.64	No
		z	-0.006	5.36	No
	77	Z	-0.014	0.00	No
		z	-0.014	8.00	No
	79	z	-0.003	2.00	No
	81	Z	-0.006	0.64	No
		Z	-0.006	5.36	No
	102	z	-0.006	0.64	No
		Z	-0.006	5.36	No
	104	Z	-0.003	2.00	No
	106	z	-0.014	0.00	No
		Z	-0.014	8.00	No
	108	Z	-0.006	0.64	No
		z	-0.006	5.36	No
	110	Z	-0.008	0.64	No
		Z	-0.008	5.36	No
	112	Z	-0.004	2.00	No
	114	Z	-0.023	0.00	No
		z	-0.023	8.00	No
	116	Z	-0.008	0.64	No
		Z	-0.008	5.36	No
WL30	75	×	-0.007	0.64	No
		×	-0.007	5.36	No
		x	-0.001	2.00	No
	77	×	-0.02	0.00	No
		×	-0.02	8.00	No
	79	×	-0.003	2.00	No
	81	X	-0.007	0.64	No
		X	-0.007	5.36	No
		x	-0.001	2.00	No
	102	X	-0.007	0.64	No
		×	-0.007	5.36	No
		×	-0.001	2.00	No
	104	×	-0.003	2.00	No
	106	×	-0.02	0.00	No
		×	-0.02	8.00	No
	108	×	-0.007	0.64	No
		×	-0.007	5.36	No
	440	×	-0.001	2.00	No
	110	×	-0.006	0.64	No
		×	-0.006	5.36	No
	440	×	-0.001	2.00	No
	112	×	-0.003	2.00	No
	114	X	-0.01	0.00	No
	440	×	-0.01	8.00	No
	116	×	-0.006	0.64	No
		×	-0.006	5.36	No
11.4	40	×	-0.001	2.00	No
LL1	42	У	-0.25	2.40	No
LL2	43	У	-0.25	4.50	No
LLa1	81	У	-0.50	3.00	No
	102	У	-0.50	3.00	No
	110	У	-0.50	3.00	No

LLa3	77	у	-0.50	4.00	No
	106	У	-0.50	4.00	No
	114	У	-0.50	4.00	No
LLa4	75	У	-0.50	3.00	No
	108	у	-0.50	3,00	No
	116	У	-0.50	3.00	No

# Self weight multipliers for load conditions

		- <u>-</u>	Self weigh	nt multiplie	г
Condition	Description	Comb.	MultX	MultY	MultZ
DL	Dead Load	No	0.00	-1.00	0.00
W0	Wind Load 0/60/120 deg	No	0.00	0.00	0.00
W30	Wind Load 30/90/150 deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
Wi0	Ice Wind Load 0/60/120 deg	No	0.00	0.00	0.00
Wi30	Ice Wind Load 30/90/150 deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0/60/120 deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30/90/150 deg	No	0.00	0.00	0.00
LL1	250 lb Live Load Center of Mount	No	0.00	0.00	0.00
LL2	250 lb Live Load End of Mount	No	0.00	0.00	0.00
LLa1	500 lb Live Load Antenna 1	No	0.00	0.00	0.00
LLa3	500 lb Live Load Antenna 3	No	0.00	0.00	0.00
LLa4	500 lb Live Load Antenna 4	No	0.00	0.00	0.00
W180	-W0	Yes	0.00	0.00	0.00
W210	-W30	Yes	0.00	0.00	0.00
Wi180	-Wi0	Yes	0.00	0.00	0.00
Wi210	-Wi30	Yes	0.00	0.00	0.00
WL180	-WL0	Yes	0.00	0.00	0.00
WL210	-WL30	Yes	0.00	0.00	0.00

# Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
DL	0.00	0.00	0.00
W0	0.00	0.00	0.00
W30	0.00	0.00	0.00
Di	0.00	0.00	0.00
Wi0	0.00	0.00	0.00
Wi30	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
LL1	0.00	0.00	0.00
LL2	0.00	0.00	0.00
LLa1	0.00	0.00	0.00
LLa3	0.00	0.00	0.00
LLa4	0.00	0.00	0.00
W180	0.00	0.00	0.00
W210	0.00	0.00	0.00
Wi180	0.00	0.00	0.00

Wi210	0.00	0.00	0.00
WL180	0.00	0.00	0.00
WL210	0.00	0.00	0.00

9



Current Date: 5/9/2018 2:20 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\CROWN CASTLE\829013\829013.etz\

# **Geometry data**

**GLOSSARY** 

Cb22, Cb33 : Moment gradient coefficients

Cm22, Cm33 Coefficients applied to bending term in interaction formula Tapered member section depth at J end of member d0 DJX Rigid end offset distance measured from J node in axis X DJY Rigid end offset distance measured from J node in axis Y DJZ Rigid end offset distance measured from J node in axis Z DKX Rigid end offset distance measured from K node in axis X DKY Rigid end offset distance measured from K node in axis Y DKZ : Rigid end offset distance measured from K node in axis Z : Tapered member section depth at K end of member dL

Ig factor : Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members

K22 : Effective length factor about axis 2
K33 : Effective length factor about axis 3

L22 : Member length for calculation of axial capacity
L33 : Member length for calculation of axial capacity

LB pos : Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg : Lateral unbraced length of the compression flange in the negative side of local axis 2

RX : Rotation about X
RY : Rotation about Y
RZ : Rotation about Z

TO 11 = Tension only member 0 = Normal member

TX : Translation in X
TY : Translation in Y
TZ : Translation in Z

## **Nodes**

Node	<b>X</b> [ft]	<b>Y</b> [ft]	<b>Z</b> [ft]	Rigid Floor
1	0.00	0.00	0.00	0
3	4.1136	0.00	-2.375	0
4	0.6761	0.00	-8.3289	0
5	7.5511	0.00	3.5789	1° 0
24	-4.1136	0.00	-2.375	0
25	-7.5511	0.00	3.5789	0
26	-0.6761	0.00	-8.3289	0
31	0.00	0.00	4.75	0
32	6.875	0.00	4.75	0
33	-6.875	0.00	4.75	0
42	-1.85E-06	0.00	-8.3289	0
45	-7.2131	0.00	4.1645	0
46	7.2131	0.00	4.1645	0
47	-0.866	0.00	0.50	0
48	0.866	0.00	0.50	0
49	0.00	0.00	-1.00	0
152	5.3011	0.00	-0.3182	0
153	2.9261	0.00	-4.4318	0
158	-2.9261	0.00	-4.4318	0
159	-5.3011	0.00	-0.3182	0
160	2.375	0.00	4.75	0
161	-2.375	0.00	4.75	0

168	5.4261	0.00	-0.1017	0
169	2.8011	0.00	-4.6483	0
174	-2.8011	0.00	-4.6483	0
175	-5.4261	0.00	-0.1017	0
176	-2.625	0.00	4.75	0
177	2.625	0.00	4.75	0
178	2.625	0.00	1.5155	0
181	3.86E-06	0.00	-3.0311	0
182	-2.625	0.00	1.5155	0
231	7.3011	0.00	3.1459	0
232	7.4743	0.00	3.0459	0
233	7.4743	-3.00	3.0459	0
234	7.4743	3.00	3.0459	0
235	5.0511	0.00	-0.7512	0
236	5.2243	-4.00	-0.8512	0
237	5.2243	0.00	-0.8512	0
238	5.2243	4.00	-0.8512	0
239	3.1761	0.00	-3.9988	0
240	3.3493	0.00	-4.0988	0
241	3.3493	-3.00	-4.0988	0
242	3.3493	3.00	-4.0988	0
243	0.9261	0.00	-7.8959	0
244	1.0993	3.00	-7.9959	0
245	1.0993	0.00	-7.9959	0
246	1.0993	-3.00	-7.9959	0
279	-7.3011	0.00	3.1459	0
280	-7.4743	3.00	3.0459	0
281	-7.4743	0.00	3.0459	0
282	-7.4743	-3.00	3.0459	0
283	-5.0511	0.00	-0.7512	0
284	-5.2243	0.00	-0.8512	-0
285	-5.2243	-3.00	-0.8512	0
286	-5.2243	3.00	-0.8512	0
287	-3.1761	0.00	-3.9988	0
288	-3.3493	-4.00	-4.0988	0
289	-3.3493	0.00	-4.0988	0
290	-3.3493	4.00	-4.0988	0
291	-0.9261	0.00	-7.8959	0
292	-1.0993	0.00	-7.9959	0
293	-1.0993	-3.00	-7.9959	0
294	-1.0993	3.00	-7.9959	0
295	6.375	0.00	4.75	0
296	6.375	3.00	4.95	0
297	6.375	0.00	4.95	0
298	6.375	-3.00	4.95	0
299	1.875	0.00	4.75	0
300	1.875	0.00	4.95	0
301	1.875	-3.00	4.95	0
302	1.875	3.00	4.95	0
303	-1.875	0.00	4.75	0
304	-1.875	-4.00	4.95	0
305	-1.875	0.00	4.95	0
306	-1.875	4.00	4.95	0
307	-6.375	0.00	4.75	0
308	-6.375	0.00	4.95	0
309	-6.375	-3.00	4.95	0
310	-6.375	3.00	4.95	0
				******

# Restraints

TX	TY	TZ	RX	RY	RZ
<del></del>	1	1	1	1	1
1	1	1	1	1	1
1	1	1	1	1	1
					TX TY TZ RX RY  1 1 1 1 1 1 1 1 1 1 1 1 1 1

# Members

Member	NJ	NK	Description	Section	Material	<b>d0</b> [in]	<b>dL</b> (in)	lg factor
4	45	47	************************	HSS_SQR 3X3X1_4	A500 GrB rectangular		0.00	0.00
5	48	46		HSS_SQR 3X3X1_4	A500 GrB rectangular	0.00	0.00	0.00
6	49	42		HSS_SQR 3X3X1_4	A500 GrB rectangular	0.00	0.00	0.00
7	33	25		PL 6x5/8	A36	0.00	0.00	0.00
8	32	5		PL 6x5/8	A36	0.00	0.00	0.00
9	4	26		PL 6x5/8	A36	0.00	0.00	0.00
35	181	174		LU 2-1_2X1-1_2X1_4	A36	0.00	0.00	0.00
36	178	168		LU 2-1_2X1-1_2X1_4	A36	0.00	0.00	0.00
39	169	181		LU 2-1_2X1-1_2X1_4	A36	0.00	0.00	0.00
41	33	161		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
42	161	160		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
43	160	32		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
44	25	159		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
45	159	158		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
46	158	26		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
47	4	153		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
48	153	152		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
49	152	5		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
75	234	233		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
77	238	236		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
79	242	241		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
81	244	246		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
82	160	178		LU 2-1_2X1-1_2X1_4	A36	0.00	0.00	0.00
83	175	182		LU 2-1_2X1-1_2X1_4	A36	0.00	0.00	0.00
84	182	176		LU 2-1_2X1-1_2X1_4	A36	0.00	0.00	0.00
102	280	282		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
104	286	285		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
106	290	288		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
108	294	293		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
110	296	298		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
112	302	301		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
114	306	304		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
116	310	309		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

# Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
75	0.00	2	-0.50	0.00	-0.866
77	0.00	2	-0.50	0.00	-0.866
79	0.00	2	-0.50	0.00	-0.866
81	0.00	2	-0.50	0.00	-0.866
102	0.00	2	-0.50	0.00	0.866
104	0.00	2	-0.50	0.00	0.866

106	0.00	2	-0.50	0.00	0.866
108	0.00	2	-0.50	0.00	0.866

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# APPENDIX C RAM ELEMENTS ANALYSIS OUTPUT



Current Date: 5/9/2018 2:20 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\CROWN CASTLE\829013\829013.etz\

# **Steel Code Check**

## Report: Summary - For all selected load conditions

## Load conditions to be included in design :

LC1=1.2DL+1.6W0

LC2=1.2DL+1.6W30

LC3=1.2DL-1.6W0

LC4=1.2DL-1.6W30

LC5=0.9DL+1.6W0

LC6=0.9DL+1.6W30

LC7=0.9DL-1.6W0

LC8=0.9DL-1.6W30

LC9=1.2DL+Di+Wi0

LC9-1.2DE1D11VIO

LC10=1.2DL+Di+Wi30

LC11=1.2DL+Di-Wi0

LC12=1.2DL+Di-Wi30

LC13=1.2DL

LC14=0.9DL

LC15=1.2DL+1.5LL1

LC16=1.2DL+1.5LL2

LC17=1.2DL+WL0+1.5LLa1

LC18=1.2DL+WL30+1.5LLa1

LC19=1.2DL-WL0+1.5LLa1

LC20=1.2DL-WL30+1.5LLa1

LC25=1.2DL+WL0+1.5LLa3

LC26=1.2DL+WL30+1.5LLa3

LC27=1.2DL-WL0+1.5LLa3

LC28=1.2DL-WL30+1.5LLa3 LC29=1.2DL+WL0+1.5LLa4

LC30=1.2DL+WL30+1.5LLa4

LC31=1.2DL-WL0+1.5LLa4

LC32=1.2DL-WL30+1.5LLa4

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	HSS_SQR 3X3X1_4	4	LC1 at 100.00%	1.04	N.G.	****************
			LC10 at 100.00%	1.25	N.G.	
			LC11 at 100.00%	1.28	N.G.	
			LC12 at 100.00%	1.23	N.G.	
			LC13 at 100.00%	0.74	OK	
			LC14 at 100.00%	0.56	OK	
			LC15 at 100.00%	0.87	OK	
			LC16 at 100.00%	0.72	OK	
			LC17 at 100.00%	1.35	N.G.	
			LC18 at 100.00%	1.34	N.G.	
			LC19 at 100.00%	1.35	N.G.	Eq. H1-1b
			LC2 at 100.00%	0.82	OK	
			LC20 at 100.00%	1.34	N.G.	
			LC25 at 100.00%	1.20	N.G.	
			LC26 at 100.00%	1.20	N.G.	
			LC27 at 100.00%	1.21	N.G.	
			LC28 at 100.00%	1.19	N.G.	
			LC29 at 100.00%	1.35	N.G.	
			LC3 at 100.00%	1.05	N.G.	
			LC30 at 100.00%	1.34	N.G.	
			LC31 at 100.00%	1.35	N.G.	

	LC32 at 100.00% LC4 at 100.00% LC5 at 100.00% LC6 at 100.00% LC7 at 100.00% LC8 at 100.00%	1.34 0.80 0.85 0.63 0.86 0.61 1.27	N.G. OK OK OK OK OK N.G.	
5	LC1 at 0.00% LC10 at 0.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC18 at 0.00% LC20 at 0.00% LC20 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC3 at 0.00% LC3 at 0.00% LC3 at 0.00% LC30 at 0.00%	0.93 1.24 1.26 1.25 0.74 0.56 0.88 1.12 1.35 1.34 1.35 0.80 1.34 1.20 1.19 1.20 1.20 1.35 0.95 1.34 1.35	OK N.G. N.G. N.G. OK OK OK N.G. N.G. N.G. N.G. N.G. N.G. N.G. N.G	Eq. H1-1b
	LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00% LC9 at 0.00%	1.34 0.83 0.75 0.62 0.76 0.64 1.25	N.G. OK OK OK OK OK N.G.	
6	LC1 at 0.00% LC10 at 0.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC16 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC20 at 0.00%	0.81 1.29 1.24 1.29 0.75 0.56 0.70 0.70 1.35 1.36 1.34 1.21 1.36 1.20 1.21 1.20 1.21 1.35 0.76	OK N.G. N.G. OK OK OK OK N.G. N.G. N.G. N.G. N.G. N.G. N.G. N.G	Fa H1-1h
	LC3 at 0.00% LC30 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00%	1.36 1.34 1.36 1.20 0.62 1.02 0.57 1.02	N.G. N.G. N.G. N.G. OK N.G. OK N.G.	Eq. H1-1b

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LU 2-1\_2X1-1\_2X1\_4

	LC13 at 100.00%	0.90	ОК	
	LC14 at 100.00%	0.67	OK	
	LC15 at 100.00%	0.86	OK	
	LC16 at 100.00%	0.93	OK	
	LC17 at 100.00%	1.44	N.G.	
	LC18 at 100.00%	1.45	N.G.	
	LC19 at 100.00%	1.44	N.G.	
	LC2 at 100.00%	1.06	N.G.	
	LC20 at 100.00%	1.44	N.G.	
	LC25 at 100.00%	1.58	N.G.	
	LC26 at 100.00%	1.58	N.G.	Eg. H2-1
	LC27 at 100.00%	1.58	N.G.	
	LC28 at 100.00%	1.58	N.G.	
	LC29 at 100.00%	1.47	N.G.	
	LC3 at 100.00%	1.00	OK	
	LC30 at 100.00%	1.47	N.G.	
	LC31 at 100.00%	1.47	N.G.	*
	LC32 at 100.00%	1.47	N.G.	
	LC4 at 100.00%	0.85	OK	
	LC5 at 100.00%	0.64	ΟK	
	LC6 at 100.00%	0.83	OK	
	LC7 at 100.00%	0.78	OK	
	LC8 at 100.00%	0.62	OK	
	LC9 at 100.00%	1.50	N.G.	
82	LC1 at 100.00%	1.10	N.G.	
	LC10 at 100.00%	1.51	N.G.	
	LC11 at 100.00%	1.51	N.G.	
	LC12 at 100.00%	1.54	N.G.	
	LC13 at 100.00%	0.91	OK	
	LC14 at 100.00%	0.68	OK	
	LC15 at 100.00%	1.26	N.G.	
	LC16 at 100.00%	1.17	N.G.	
	LC17 at 100.00%	1.47	N.G.	
	LC18 at 100.00%	1.46	N.G.	
	LC19 at 100.00%	1.46	N.G.	
	LC2 at 100.00%	0.86	OK	
	LC20 at 100.00%	1.47	N.G.	
	LC25 at 100.00%	1.62	N.G.	
	LC26 at 100.00%	1.61	N.G.	
	LC27 at 100.00%	1.61	N.G.	
	LC28 at 100.00%	1.62	N.G.	Eq. H2-1
	LC29 at 100.00%	1.49	N.G.	
	LC3 at 100.00%	0.80	OK	
	LC30 at 100.00%	1.48	N.G.	
	LC31 at 100.00%	1.49	N.G.	
	LC32 at 100.00%	1.50	N.G.	
	LC4 at 100.00%	1.02	N.G.	
	LC5 at 100.00%	0.87	OK	
	LC6 at 100.00%	0.63	OK	
	LC7 at 100.00%	0.57	OK	
	LC8 at 100.00% LC9 at 100.00%	0.80 1.55	OK N.G.	
		1.00	N.G.	
83	LC1 at 100.00%	0.82	OK	
	LC10 at 100.00%	1.49	N.G.	
	LC11 at 100.00%	1.52	N.G.	
	LC12 at 100.00%	1.52	N.G.	
	LC13 at 100.00%	0.90	OK	
	LC14 at 100.00%	0.67	OK	
	LC15 at 100.00%	0.96	OK	
	LC16 at 100.00%	0.86	OK	
	LC17 at 100.00%	1.44	N.G.	
	LC18 at 100.00%	1.44	N.G.	

		LC19 at 100.00%	1.45	N.G.	
		LC2 at 100.00%	0.75	OK	
		LC20 at 100.00%	1.45	N.G.	
		LC25 at 100.00%	1.58	N.G.	
		LC26 at 100.00%	1.58	N.G.	
		LC27 at 100.00%	1.59	N.G.	Eq. H2-1
		LC28 at 100.00%	1.59	N.G.	·
		LC29 at 100.00%		N.G.	
			1.46		
		LC3 at 100.00%	0.99	OK	
		LC30 at 100.00%	1.46	N.G.	
		LC31 at 100.00%	1.47	N.G.	
		LC32 at 100.00%	1.47	N.G.	
		LC4 at 100.00%	1.12	N.G.	
		LC5 at 100.00%	0.59	OK	
		LC6 at 100.00%	0.52	OK	
		LC7 at 100.00%	0.77	OK	
		LC8 at 100.00%	0.89	OK	
		LC9 at 100.00%	1.48	N.G.	•
				1000000000000	
	84	LC1 at 0.00%	1.18	N.G.	
		LC10 at 0.00%	1.54	N.G.	
		LC11 at 0.00%	1.52	N.G.	
		LC12 at 0.00%	1.52	N.G.	
		LC13 at 0.00%	0.90	OK	
		LC14 at 0.00%	0.67	OK	
		LC15 at 0.00%	1.24	N.G.	
		LC16 at 0.00%	0.97	OK	
		LC17 at 0.00%	1.47	N.G.	
		LC18 at 0.00%	1.47	N.G.	
		LC19 at 0.00%	1.46	N.G.	
		LC2 at 0.00%	0.98	OK	
		LC20 at 0.00%	1.46	N.G.	
		LC25 at 0.00%	1.69	N.G.	Eq. H2-1
		LC26 at 0.00%	1.69	N.G.	Eq. H2-1
					Lq.,112-1
		LC27 at 0.00%	1.68	N.G.	
		LC28 at 0.00%	1.68	N.G.	
		LC29 at 0.00%	1.45	N.G.	
		LC3 at 0.00%	0.81	ÓΚ	
		LC30 at 0.00%	1.45	N.G.	
		LC31 at 0.00%	1.44	N.G.	
		LC32 at 0.00%	1.44	N.G.	
		LC4 at 0.00%	0.89	OK	
		LC5 at 0.00%	0.96	OK	
		LC6 at 0.00%	0.76	OK	
		LC7 at 0.00%	0.59	OK	
		LC8 at 0.00%	0.66	OK	
		LC9 at 0.00%	1.56	N.G.	
PIPE 2x0.154	75	LC1 at 50.00%	0.36	ОК	
·		LC10 at 46.88%	0.08	OK	
		LC10 at 40.86%			
			0.07	OK	
		LC12 at 46.88%	0.08	OK	
		LC13 at 46.88%	0.01	OK	
		LC14 at 46.88%	0.01	OK	
		LC15 at 46.88%	0.01	OK	
		LC16 at 46.88%	0.01	OK	
		LC17 at 50.00%	0.02	OK	
		LC18 at 46.88%	0.02	OK	
		LC19 at 50.00%	0.02	OK	
		LC2 at 50.00%	0.41	OK	
		LC20 at 46.88%	0.02	OK	
		LC25 at 50.00%	0.02	OK	
		LC26 at 46.88%	0.02	OK	
		LC27 at 50.00%	0.02	OK	
		_3 2. 3. 3. 3. 7.			

	LC28 at 46.88% LC29 at 50.00% LC3 at 50.00% LC30 at 46.88% LC31 at 50.00% LC32 at 46.88% LC4 at 50.00% LC5 at 50.00% LC6 at 50.00% LC7 at 50.00% LC8 at 50.00%	0.02 0.02 0.36 0.02 0.02 0.02 0.41 0.36 0.41 0.36 0.41 0.07	OK OK OK OK OK OK OK OK	Eq. H1-1b
77	LC1 at 50.00%	1.25	N.G.	***************************************
	LC10 at 50.00%	0.31	OK	
	LC11 at 50.00% LC12 at 50.00%	0.23 0.31	OK	
	LC12 at 50.00%	0.31	OK OK	
	LC14 at 46.88%	0.01	OK	
	LC15 at 46.88%	0.01	ОК	
	LC16 at 46.88%	0.01	OK	
	LC17 at 50.00%	0.06	OK	
	LC18 at 50.00%	0.09	OK	
	LC19 at 50.00% LC2 at 50.00%	0.06 1. <mark>8</mark> 1	OK N.G.	
	LC20 at 50.00%	0.09	OK	
	LC25 at 50.00%	0.06	OK	
	LC26 at 50.00%	0.09	OK	
	LC27 at 50.00%	0.06	OK	
	LC28 at 50.00%	0.09	OK	
	LC29 at 50.00% LC3 at 50.00%	0.06 1.25	OK N.G.	
	LC30 at 50.00%	0.09	OK	
	LC31 at 50.00%	0.06	OK	
	LC32 at 50.00%	0.09	OK	
	LC4 at 50.00%	1.81	N.G.	Eq. H1-1b
	LC5 at 50.00%	1.25	N.G.	
	LC6 at 50.00%	1.81	N.G.	
	LC7 at 50.00% LC8 at 50.00%	1.25 1.81	N.G. N.G.	
	LC9 at 50.00%	0.23	OK	
	01000-10000-1000-1000-1	oopenanga uenga po		
79	LC1 at 46.88%	0.10	OK	
	LC10 at 46.88% LC11 at 46.88%	0.02 0.01	OK OK	
	LC12 at 46.88%	0.02	OK OK	
	LC13 at 46.88%	0.01	OK	
	LC14 at 46.88%	0.01	OK	
	LC15 at 46.88%	0.01	OK	
	LC16 at 46.88%	0.01	OK	
	LC17 at 46.88% LC18 at 46.88%	0.01	OK	
	LC19 at 46.88%	0.01 0.01	OK OK	
	LC2 at 46.88%	0.11	oĸ	Eq. H1-1b
	LC20 at 46.88%	0.01	OK	
	LC25 at 46.88%	0.01	OK	
	LC26 at 46.88%	0.01	OK	
	LC27 at 46.88%	0.01	OK	
	LC28 at 46.88%	0.01	OK	
	LC29 at 46.88% LC3 at 46.88%	0.01 0.10	OK OK	
	LC30 at 46.88%	0.10	OK OK	
	LC31 at 46.88%	0.01	ОК	
	LC32 at 46.88%	0.01	OK	

	LC4 at 46.88%	0.11	OK	
	LC5 at 46.88%	0.10	OK	
	LC6 at 46.88%	0.11	OK	
	LC7 at 46.88%	0.10	OK	
	LC8 at 46.88%	0.11	OK	
	LC9 at 46.88%	0.01	OK	
81	LC1 at 50.00%	0.36	OK	ISSER VICE DE L'ARTINITATE DE CARACTER DE CARACTER DE L'ARTINE DE
•	LC10 at 46.88%	0.08	OK	
	LC11 at 50.00%	0.07	OK	
	LC12 at 46.88%	0.08	OK	
	LC13 at 46.88%	0.01	OK	
	LC14 at 46.88%	0.01	OK	
	LC15 at 46.88%	0.01	OK	
	LC16 at 46.88%	0.01	OK	
	LC17 at 50.00%	0.02	OK	
	LC18 at 46.88%	0.02	OK	
	LC19 at 50.00%	0.02	OK	
	LC2 at 50.00%	0.41	OK	Eq. H1-1b
	LC20 at 46.88%	0.02	OK	
	LC25 at 50.00%	0.02	OK	
	LC26 at 46.88% LC27 at 50.00%	0.02 0.02	OK OK	
	LC28 at 46.88%	0.02	OK OK	
	LC29 at 50.00%	0.02	OK OK	
	LC3 at 50.00%	0.36	OK	
	LC30 at 46.88%	0.02	OK	
	LC31 at 50.00%	0.02	OK	
	LC32 at 46.88%	0.02	OK	
	LC4 at 50.00%	0.41	OK	
	LC5 at 50.00%	0.36	OK	
	LC6 at 50.00%	0.41	OK	
	LC7 at 50.00%	0.36	OK	
	LC8 at 50.00%	0.41	OK	
	LC9 at 50.00%	0.07	OK	
102	LC1 at 50.00%	0.36	OK	
	LC10 at 46.88%	0.08	OK	
		0.08 0.07	OK OK	
	LC10 at 46.88%			
	LC10 at 46.88% LC11 at 50.00%	0.07	OK	
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88%	0.07 0.08 0.01 0.01	OK OK OK	
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88%	0.07 0.08 0.01 0.01 0.01	OK OK OK OK	
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88%	0.07 0.08 0.01 0.01 0.01 0.01	OK OK OK OK OK	
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.01 0.02	OK OK OK OK OK OK	
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88%	0.07 0.08 0.01 0.01 0.01 0.01 0.02 0.02	OK OK OK OK OK OK OK	
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.01 0.02 0.02	OK OK OK OK OK OK OK	Fa H1.1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.01 0.02 0.02 0.02 <b>0.41</b>	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.41 0.02	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00% LC26 at 46.88%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00% LC26 at 46.88% LC27 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00% LC26 at 46.88% LC27 at 50.00% LC26 at 46.88%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00% LC26 at 46.88% LC27 at 50.00% LC28 at 46.88% LC27 at 50.00% LC28 at 46.88% LC29 at 50.00% LC30 at 46.88% LC29 at 50.00% LC30 at 46.88%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00% LC26 at 46.88% LC27 at 50.00% LC28 at 46.88% LC27 at 50.00% LC30 at 46.88% LC27 at 50.00% LC30 at 46.88% LC21 at 50.00% LC30 at 46.88% LC31 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00% LC26 at 46.88% LC27 at 50.00% LC28 at 46.88% LC29 at 50.00% LC30 at 46.88% LC31 at 50.00% LC30 at 46.88% LC31 at 50.00% LC30 at 46.88% LC31 at 50.00% LC32 at 46.88%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00% LC26 at 46.88% LC27 at 50.00% LC28 at 46.88% LC29 at 50.00% LC30 at 46.88% LC31 at 50.00% LC30 at 46.88% LC40 at 46.88% LC31 at 50.00% LC31 at 50.00% LC32 at 46.88% LC31 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00% LC26 at 46.88% LC27 at 50.00% LC28 at 46.88% LC29 at 50.00% LC30 at 46.88% LC40 at 46.88% LC30 at 46.88% LC40 at 50.00% LC30 at 46.88% LC31 at 50.00% LC31 at 50.00% LC32 at 46.88% LC4 at 50.00% LC5 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC27 at 50.00% LC26 at 46.88% LC27 at 50.00% LC28 at 46.88% LC29 at 50.00% LC30 at 46.88% LC4 at 50.00% LC30 at 46.88% LC4 at 50.00% LC31 at 50.00% LC32 at 46.88% LC4 at 50.00% LC5 at 50.00% LC5 at 50.00% LC5 at 50.00% LC5 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC27 at 50.00% LC26 at 46.88% LC27 at 50.00% LC28 at 46.88% LC29 at 50.00% LC30 at 46.88% LC4 at 50.00% LC30 at 46.88% LC4 at 50.00% LC31 at 50.00% LC32 at 46.88% LC4 at 50.00% LC5 at 50.00% LC6 at 50.00% LC6 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC27 at 50.00% LC26 at 46.88% LC27 at 50.00% LC28 at 46.88% LC29 at 50.00% LC30 at 46.88% LC4 at 50.00% LC30 at 46.88% LC4 at 50.00% LC31 at 50.00% LC32 at 46.88% LC4 at 50.00% LC5 at 50.00% LC5 at 50.00% LC5 at 50.00% LC5 at 50.00%	0.07 0.08 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

104	LC1 at 46.88%	0.10	OK	
104		0.10		
	LC10 at 46.88%	0.02	OK	
	LC11 at 46.88%	0.01	OK	
	LC12 at 46.88%	0.02	OK	
	LC13 at 46.88%	0.01	OK	
	LC14 at 46.88%	0.01	OK	
	LC15 at 46.88%	0.01	OK	
	LC16 at 46.88%	0.01	OK	
	LC17 at 46.88%	0.01	OK	
	LC18 at 46.88%		ok	
		0.01		
	LC19 at 46.88%	0.01	OK	
	LC2 at 46.88%	0.11	OK	
	LC20 at 46.88%	0.01	OK	
	LC25 at 46.88%	0.01	OK	
	LC26 at 46.88%	0.01	OK	
	LC27 at 46.88%	0.01	OK	
	LC28 at 46.88%	0.01	OK	
	LC29 at 46.88%	0.01	QΚ	
	LC3 at 46.88%	0.10	OK	
	LC30 at 46.88%		OK	
		0.01		
	LC31 at 46.88%	0.01	OK	
	LC32 at 46.88%	0.01	OK	
	LC4 at 46.88%	0.11	OK	Eg. H1-1b
	LC5 at 46.88%	0.10	OK	·
	LC6 at 46.88%	0.11	OK	
	LC7 at 46.88%	0.10	OK	
	LC8 at 46.88%	0.11	OK	
	LC9 at 46.88%	0.01	OK	
106	LC1 at 50.00%	1.25	N.G.	
	LC10 at 50.00%	0.31	OK	
	LC11 at 50.00%	0.23	OK	
	LC12 at 50.00%	0.31	OK	
	LC13 at 46.88%	0.01	OK	
	LC14 at 46.88%	0.01	OK	
			OK	
	LC15 at 46.88%	0.01		
	LC16 at 46.88%	0.01	OK	
	LC17 at 50.00%	0.06	OK	
	LC18 at 50.00%	0.09	OK	
	LC19 at 50.00%	0.06	OK	
	LC2 at 50.00%	1.81	N.G.	Eq. H1-1b
				Eq. 111-10
	LC20 at 50.00%	0.09	OK	
	LC25 at 50.00%	0.06	OK	
	LC26 at 50.00%	0.09	OK	
	LC27 at 50.00%	0.06	OK	
	LC28 at 50.00%	0.09	OK	
	LC29 at 50.00%	0.06	OK	
	LC3 at 50.00%	1.25	N.G.	
	LC30 at 50.00%	0.09	OK	
	LC31 at 50.00%	0.06	OK	
	LC32 at 50.00%	0.09	OK	
	LC4 at 50.00%	1.81	N.G.	
	LC5 at 50.00%	1.25	N.G.	
	LC6 at 50.00%	1.81	N.G.	
	LC7 at 50.00%	1.25	N.G.	
	LC8 at 50.00%	1.81	N.G.	
	LC9 at 50.00%	0.23	OK	
	LOG at 30.00 /0	U.Z3		over servicement av av complete vegat a contract the execute but even
108	LC1 at 50.00%	0.36	OK	
	LC10 at 46.88%	0.08	OK	
	LC11 at 50.00%	0.07	OK	
	LC12 at 46.88%	0.08	OK	
	LC13 at 46.88%	0.01	OK	
	LO 13 at 40.00 /0	0.01	OI.	

	LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 50.00% LC18 at 46.88% LC19 at 50.00% LC2 at 50.00% LC20 at 46.88% LC25 at 50.00% LC26 at 46.88% LC27 at 50.00% LC30 at 46.88% LC27 at 50.00% LC30 at 46.88% LC29 at 50.00% LC30 at 46.88% LC31 at 50.00% LC31 at 50.00% LC31 at 50.00% LC32 at 46.88% LC4 at 50.00% LC5 at 50.00% LC5 at 50.00% LC5 at 50.00% LC6 at 50.00% LC7 at 50.00% LC9 at 50.00%	0.01 0.01 0.02 0.02 0.02 0.02 0.02 0.02	OK O	Eq. H1-1b
110	LC1 at 50.00% LC10 at 46.88% LC11 at 50.00% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 46.88% LC19 at 46.88% LC19 at 46.88% LC2 at 50.00% LC20 at 46.88% LC25 at 46.88% LC25 at 46.88% LC27 at 46.88% LC27 at 46.88% LC29 at 46.88% LC29 at 46.88% LC29 at 46.88% LC20 at 46.88% LC27 at 46.88% LC27 at 46.88% LC27 at 46.88% LC3 at 50.00% LC30 at 46.88% LC31 at 46.88% LC31 at 46.88% LC32 at 50.00% LC30 at 50.00% LC5 at 50.00% LC6 at 50.00% LC7 at 50.00% LC9 at 50.00%	0.28 0.05 0.06 0.05 0.01 0.01 0.01 0.02 0.02 0.01 0.02 0.04 0.02 0.04 0.02 0.04 0.02 0.04	OK           OK	Eq. H1-1b
112	LC1 at 46.88% LC10 at 46.88% LC11 at 46.88% LC12 at 46.88% LC13 at 46.88% LC14 at 46.88% LC15 at 46.88% LC16 at 46.88% LC17 at 46.88% LC17 at 46.88% LC19 at 46.88%	0.05 0.01 0.02 0.01 0.01 0.01 0.01 0.01 0.01	OK	1.001.001.001.001.001.001.001.001.001.0

	LC2 at 46.88%	0.07	ок	Eq. H1-1b
	LC20 at 46.88%	0.01	OK	24
	LC25 at 46.88%	0.01	OK	
	LC26 at 46.88%	0.01	OK	
	LC27 at 46.88%	0.01	ок	
	LC28 at 46.88%	0.01	OK	
	LC29 at 46.88%	0.01	OK	
	LC3 at 46.88%	0.05	OK	
	LC30 at 46.88%	0.01	OK	
	LC31 at 46.88%	0.01	OK	
	LC32 at 46.88%	0.01	OK	
	LC4 at 46.88%	0.07	OK	
	LC5 at 46.88%	0.05	OK	
	LC6 at 46.88%	0.07	ok	
	LC7 at 46.88%	0.05	OK	
	LC8 at 46.88%	0.07	OK	
	LC9 at 46.88%	0.02	OK	
114	LC1 at 50.00%	1.46	N.G.	Eq. H1-1b
	LC10 at 50.00%	0.14	OK	
	LC11 at 50.00%	0.26	OK	
	LC12 at 50.00%	0.14	OK	
	LC13 at 46.88%	0.01	OK	
	LC14 at 46.88%	0.01	OK	
	LC15 at 46.88%	0.01	OK	
	LC16 at 46.88%	0.01	OK	
	LC17 at 50.00%	0.08	OK	
	LC18 at 46.88%	0.03	OK	
	LC19 at 50.00%	0.08	OK	
	LC2 at 50.00%	0.71	OK	
	LC20 at 46.88%	0.03	OK	
	LC25 at 50.00%	0.08	OK	
	LC26 at 46.88%	0.03	OK	
	LC27 at 50.00%	0.08	OK	
	LC28 at 46.88%	0.03	OK	
	LC29 at 50.00%	0.08	OK	
	LC3 at 50.00%	1.46	N.G.	
	LC30 at 46.88%	0.03	OK	
	LC31 at 50.00%	0.08	OK	
	LC32 at 46.88%	0.03	OK	
	LC4 at 50.00%	0.71	OK	
	LC5 at 50.00%	1.46	N.G.	
	LC6 at 50.00%	0.71	OK	
	LC7 at 50.00%	1.46	N.G.	
	LC8 at 50.00%	0.71	OK	
	LC9 at 50.00%	0.26	OK	
116	LC1 at 50.00%	0.28	 ОК	***************************************
110	LC10 at 46.88%	0.05	OK	
	LC11 at 50.00%	0.06	OK	
	LC12 at 46.88%	0.05	OK	
	LC13 at 46.88%	0.01	OK	
	LC14 at 46.88%	0.01	OK	
	LC15 at 46.88%	0.01	OK	
	LC16 at 46.88%	0.01	OK	
	LC17 at 46.88%	0.02	OK	
	LC18 at 46.88%	0.01	OK	
	LC19 at 46.88%	0.02	OK	
	LC2 at 50.00%	0.24	OK OK	
	LC20 at 46.88%	0.01	OK	
	LC25 at 46.88%	0.02	OK	
	LC26 at 46.88%	0.02	OK	
	LC27 at 46.88%	0.02	OK	
	LC28 at 46.88%	0.01	OK	

		LC29 at 46.88% LC3 at 50.00% LC30 at 46.88% LC31 at 46.88% LC32 at 46.88% LC4 at 50.00% LC5 at 50.00% LC6 at 50.00% LC7 at 50.00% LC8 at 50.00%	0.02 0.28 0.01 0.02 0.01 0.24 0.28 0.24 0.28 0.24 0.06	OK	Eq. H1-1b
PIPE 3x0.216	41	LC1 at 93.75%	0.31	OK	
		LC10 at 93.75%	0.38	OK	
		LC11 at 93.75%	0.38	OK	
		LC12 at 93.75%	0.37	OK	
		LC13 at 93.75%	0.22	OK	
		LC14 at 93.75%	0.17	OK	
		LC15 at 0.00%	0.21	OK	
		LC16 at 93.75%	0.28	OK	
		LC17 at 93.75%	0.60	OK	
		LC18 at 93.75% LC19 at 93.75%	0.60	ок <b>ок</b>	Ea 42.6
		LC2 at 93.75%	<b>0.60</b> 0.37	OK	Eq. H3-6
		LC20 at 93.75%	0.60	OK OK	
		LC25 at 0.00%	0.40	OK	
		LC26 at 0.00%	0.40	OK	Eq. H3-6
		LC27 at 0.00%	0.40	OK	24.710 0
		LC28 at 0.00%	0.40	OK	
		LC29 at 95.83%	0.47	OK	
		LC3 at 93.75%	0.34	OK	
		LC30 at 93.75%	0.48	OK	
		LC31 at 93.75%	0.48	OK	
		LC32 at 95.83%	0.47	OK	
		LC4 at 95.83%	0.37	OK	
		LC5 at 93.75%	0.26	OK	
		LC6 at 93.75%	0.31	OK	
		LC7 at 93.75%	0.29	OK	
		LC8 at 95.83%	0.32	OK	
		LC9 at 93.75%	0.37	OK	
	42	LC1 at 100.00%	0.32	ок	
		LC10 at 100.00%	0.41	OK	
		LC11 at 100.00%	0.38	OK	
		LC12 at 100.00%	0.39	OK	
		LC13 at 100.00%	0.23	OK	
		LC14 at 100.00%	0.18	OK	
		LC15 at 100.00%	0.20	OK	
		LC16 at 100.00%	0.32	OK	
		LC17 at 0.00% LC18 at 0.00%	0.52	OK	
		LC19 at 0.00%	0.51 0.51	OK OK	
		LC2 at 100.00%	0.39	OK	
		LC20 at 0.00%	0.52	OK	Eq. H1-1b
		LC25 at 100.00%	0.37	OK	=4
		LC26 at 100.00%	0.37	OK	
		LC27 at 100.00%	0.36	OK	
		LC28 at 100.00%	0.36	OK	
		LC29 at 100.00%	0.55	OK	
		LC3 at 100.00%	0.31	OK	
		LC30 at 100.00%	0.55	OK	Eq. H1-1b
		LC31 at 100.00%	0.54	OK	
		LC32 at 100.00%	0.54	OK	
		LC4 at 100.00%	0.37	OK	

	LC5 at 100.00% LC6 at 100.00% LC7 at 100.00% LC8 at 100.00% LC9 at 100.00%	0.26 0.33 0.25 0.32 0.40	OK OK OK OK	
43	LC1 at 0.00% LC10 at 0.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC20 at 0.00% LC25 at 0.00% LC26 at 0.00%	0.31 0.46 0.47 0.46 0.25 0.19 0.22 0.34 0.51 0.50 0.51 0.37 0.51 0.46 0.46	OK OK OK OK OK OK OK OK	
	LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC3 at 0.00% LC30 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00% LC9 at 0.00%	0.46 0.46 0.63 0.34 0.63 0.63 0.63 0.26 0.31 0.28 0.32 0.46	OK OK OK OK OK OK OK OK OK OK	Eq. H3-6
44	LC1 at 93.75% LC10 at 93.75% LC11 at 93.75% LC12 at 93.75% LC13 at 93.75% LC14 at 93.75% LC15 at 93.75% LC16 at 93.75% LC17 at 93.75% LC19 at 93.75% LC19 at 93.75% LC20 at 93.75% LC20 at 93.75% LC25 at 93.75% LC26 at 93.75% LC27 at 93.75% LC27 at 93.75% LC28 at 93.75% LC29 at 93.75%	0.25 0.46 0.46 0.24 0.18 0.29 0.24 0.49 0.49 0.49 0.49 0.46 0.46 0.46 0.46 0.62 0.24	OK O	
	LC30 at 93.75% LC31 at 93.75% LC32 at 93.75% LC4 at 12.50% LC5 at 95.83% LC6 at 12.50% LC7 at 93.75% LC8 at 12.50% LC9 at 93.75%	0.62 0.62 0.62 0.29 0.19 0.26 0.18 0.25 0.46	OK OK OK OK OK OK OK OK	Eq. H3-6

45	LC1 at 100.00% LC10 at 0.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC18 at 100.00% LC19 at 100.00% LC20 at 100.00% LC20 at 100.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC21 at 100.00% LC20 at 100.00% LC21 at 100.00% LC21 at 100.00% LC22 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC31 at 100.00% LC4 at 100.00% LC5 at 100.00% LC5 at 100.00% LC6 at 100.00% LC9 at 0.00%	0.27 0.38 0.38 0.39 0.23 0.17 0.27 0.22 0.51 0.51 0.52 0.28 0.52 0.36 0.35 0.35 0.35 0.36 0.54 0.28 0.53 0.54 0.28 0.53 0.54 0.28 0.53 0.54 0.28 0.53 0.54 0.28 0.53 0.54 0.28 0.53 0.54 0.28 0.53 0.54 0.28 0.53 0.54 0.28 0.53 0.54 0.28 0.53	OK O	Eq. H1-1b
46	LC1 at 6.25% LC10 at 6.25% LC11 at 6.25% LC11 at 6.25% LC12 at 6.25% LC13 at 6.25% LC15 at 6.25% LC16 at 6.25% LC16 at 6.25% LC19 at 6.25% LC2 at 6.25% LC2 at 6.25% LC2 at 6.25% LC20 at 6.25% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC28 at 100.00% LC29 at 6.25% LC3 at 4.17% LC30 at 6.25% LC31 at 6.25% LC31 at 6.25% LC31 at 6.25% LC32 at 4.17% LC4 at 4.17% LC5 at 6.25% LC5 at 6.25% LC7 at 4.17% LC5 at 6.25% LC6 at 6.25% LC7 at 4.17% LC8 at 6.25% LC9 at 6.25% LC9 at 6.25% LC9 at 6.25%	0.33 0.38 0.37 0.37 0.22 0.17 0.23 0.21 0.60 0.60 0.60 0.37 0.60 0.40 0.40 0.40 0.40 0.47 0.31 0.48 0.47 0.37 0.31 0.48 0.47 0.31 0.48 0.47 0.31 0.48 0.47 0.31 0.48 0.47 0.31 0.48 0.47 0.31 0.31 0.31 0.31 0.31 0.31 0.31 0.31	0K 0	Eq. H3-6
47	LC1 at 93.75% LC10 at 93.75% LC11 at 93.75% LC12 at 93.75% LC13 at 93.75% LC14 at 93.75%	0.34 0.46 0.46 0.46 0.24 0.18	OK OK OK OK OK OK	

	LC15 at 93.75% LC16 at 93.75% LC17 at 93.75% LC18 at 95.83% LC19 at 93.75% LC2 at 95.83% LC20 at 93.75% LC25 at 93.75% LC26 at 93.75% LC27 at 93.75% LC29 at 93.75% LC3 at 95.83% LC30 at 93.75% LC3 at 95.83% LC30 at 93.75% LC31 at 93.75% LC31 at 93.75% LC32 at 93.75% LC32 at 93.75% LC4 at 93.75% LC5 at 93.75% LC5 at 93.75% LC5 at 93.75% LC6 at 95.83% LC7 at 95.83% LC7 at 95.83% LC8 at 93.75% LC8 at 93.75%	0.25 0.30 0.49 0.49 0.49 0.37 0.50 0.46 0.46 0.46 0.62 0.33 0.62 0.62 0.39 0.27 0.31 0.27 0.32 0.46	OK	Eq. H3-6
48	LC1 at 0.00% LC10 at 0.00% LC11 at 0.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC20 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC3 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00%	0.30 0.40 0.39 0.37 0.23 0.17 0.25 0.32 0.52 0.51 0.34 0.51 0.35 0.36 0.36 0.35 0.36 0.35 0.53 0.53 0.53 0.54 0.54 0.54 0.53 0.54 0.54 0.54 0.54 0.54 0.54 0.53 0.54 0.54 0.55 0.56 0.57	OK O	Eq. H1-1b
49	LC9 at 0.00%	0.37 0.24 0.37 0.38 0.22 0.17 0.27 0.34 0.60 0.60 0.60 0.29	OK	

		LC20 at 6.25%	0.60	OK	Eq. H3-6
		LC25 at 100.00%	0.40	OK	• •
		LC26 at 100.00%	0.40	OK	
		LC27 at 100.00%	0.40	OK	<b>=</b> 440.0
		LC28 at 100.00%	0.40	OK	Eq. H3-6
		LC29 at 6.25%	0.47	OK	
		LC3 at 6.25%	0.23	OK	
		LC30 at 6.25%	0.47	OK	
		LC31 at 6.25%	0.47	ОК	
		LC32 at 6.25%		OK	
			0.47		
		LC4 at 87.50%	0.30	OK	
		LC5 at 0.00%	0.19	OK	
		LC6 at 87.50%	0.25	OK	
		LC7 at 0.00%	0.18	OK	
		LC8 at 87.50%	0.26	OK	
		LC9 at 6.25%	0.37	OK	
PL 6x5/8	7	LC1 at 0.00%	0.51	 OK	***************************************
		LC10 at 0.00%	0.59	OK	
		LC11 at 0.00%	0.58	OK	
		LC12 at 0.00%	0.58	OK	
		LC13 at 0.00%	0.34	OK	
		LC14 at 0.00%	0.26	OK	
		LC15 at 0.00%	0.44	OK	
		LC16 at 50.00%	0.36	OK	
		LC17 at 0.00%	0.60	OK	
		LC18 at 0.00%	0.60	OK	
		LC19 at 0.00%	0.60	OK	=
		LC2 at 50.00%	0.63	OK	Eq. H3-6
		LC20 at 0.00%	0.60	OK	
		LC25 at 0.00%	0.66	OK	
		LC26 at 0.00%	0.66	ок	Eq. H3-1
		LC27 at 0.00%	0.66	OK	_4
		LC28 at 0.00%	0.66	OK	
		LC29 at 50.00%	0.60	OK	
		LC3 at 0.00%	0.52	OK	
		LC30 at 50.00%	0.60	OK	
		LC31 at 50.00%	0.60	OK	
		LC32 at 50.00%	0.60	OK	
		LC4 at 50.00%	0.63	OK	Eq. H3-6
		LC5 at 0.00%		OK	Eq. 115-0
			0.44		
		LC6 at 50.00%	0.55	OK	
		LC7 at 0.00%	0.44	OK	
		LC8 at 50.00%	0.55	OK	
		LC9 at 0.00%	0.59	OK	
	8	LC1 at 0.00%	0.52	ок	***************************************
		LC10 at 53.13%	0.59	OK	
		LC11 at 53.13%	0.59	OK	
		LC12 at 53.13%	0.59	OK	
		LC13 at 53.13%	0.35	OK	
		LC14 at 53.13%	0.26	OK	
		LC15 at 0.00%	0.45	OK	
		LC16 at 53.13%	0.49	ok	
		LC17 at 53.13%	0.60	OK	
		LC18 at 53.13%	0.60	OK	
		LC19 at 53.13%	0.60	OK	
		LC2 at 100.00%	0.62	OK	Eq. H3-6
					Eq. 113-0
		LC20 at 53.13%	0.60	OK	
		LC25 at 53.13%	0.66	OK	
		LC26 at 53.13%	0.66	OK	
		LC27 at 53.13%	0.66	ok	Eq. H3-1
		LC28 at 53.13%	0.66	OK	
		LC29 at 0.00%	0.60	OK	

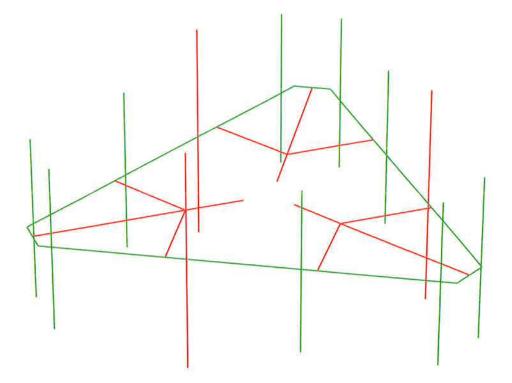
	LC3 at 0.00% LC30 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 100.00% LC5 at 0.00% LC6 at 100.00% LC7 at 0.00% LC7 at 100.00% LC8 at 100.00%	0.52 0.60 0.60 0.60 0.63 0.44 0.54 0.55	OK OK OK OK OK OK OK	Eq. H3-6
9	LC1 at 50.00%	0.58	OK	Eg. H3-6
•	LC10 at 53.13%	0.58	OK	Eq. 110 0
	LC11 at 53.13%	0.59	OK	
	LC12 at 53.13%	0.59	ОК	
	LC13 at 53.13%	0.35	ОК	
	LC14 at 53.13%	0.26	OK	
	LC15 at 53.13%	0.33	OK	
	LC16 at 53.13%	0.35	OK	
	LC17 at 53.13%	0.60	OK	
	LC18 at 53.13%	0.60	OK	
	LC19 at 53.13%	0.60	OK	
	LC2 at 0.00%	0.37	OK	
	LC20 at 53.13%	0.60	OK	
	LC25 at 53.13%	0.67	OK	
	LC26 at 53.13%	0.66	OK	
	LC27 at 53.13%	0.66	OK	F- 110.4
	LC28 at 53.13%	0.67	OK	Eq. H3-1
	LC29 at 0.00%	0.60	OK	
	LC3 at 50.00%	0.57	OK	
	LC30 at 0.00%	0.60	OK	
	LC31 at 0.00% LC32 at 0.00%	0.60	OK OK	
	LC32 at 0.00%	0.60 0.37	OK	
	LC5 at 50.00%	0.50	OK	
	LC6 at 0.00%	0.30	OK OK	
	LC7 at 50.00%	0.49	OK	
	LC8 at 100.00%	0.30	OK	
	LC9 at 53.13%	0.59	OK	



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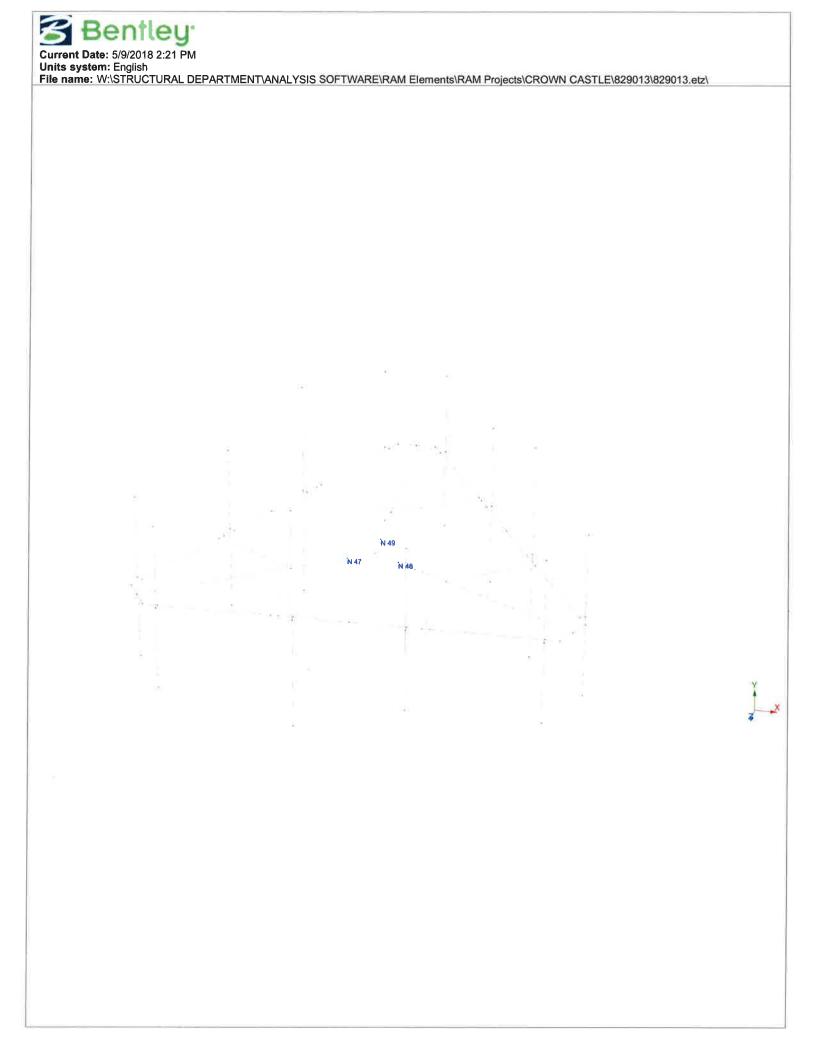






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# APPENDIX D ADDITIONAL CALCUATIONS





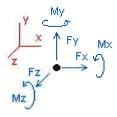
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## **Analysis result**

#### Reactions



Direction of positive forces and moments

		Forces [Kip]		Moments [Kip*ft]			
Node	FX	FY	FZ	MX	MY	MZ	
Condition	W180=-W0				ach mar colos hamanas decenies. Colos peas.		
47	0.50297	0.00514	-1.06564	-0.02992	-1.01771	-0.01324	
48	-0.42075	0.00381	-0.75428	-0.02727	0.66658	0.01250	
49	-0.08222	-0.00894	-1.59704	-0.04740	0.09619	0.00189	
SUM	0.00000	0.00000	-3.41696	-0.10459	-0.25494	0.00115	
Condition	W210=-W30						
47	-1.24933	-0.00930	0.69502	0.01274	0.15544	0.05675	
48	-1.48069	0.01007	-0.55777	-0.00999	-0.16851	0.05893	
49	-0.95380	-0.00077	-0.13725	-0.00159	1.64044	0.02555	
SUM	-3.68381	0.00000	0.00000	0.00116	1.62737	0.14123	
Condition	Wi180=-Wi0						
47	0.11186	0.00219	-0.23738	-0.01135	-0.22724	-0.00628	
48	-0.08820	0.00168	-0.15300	-0.01039	0.13352	0.00603	
49	-0.02366	-0.00387	-0.34162	-0.02045	0.02819	0.00069	
SUM	0.00000	0.00000	-0.73200	-0.04219	-0.06554	0.00044	
Condition	Wi210=-Wi30						
47	-0.25968	-0.00512	0.15351	0.00902	0.03594	0.02888	
48	-0.32267	0.00540	-0.11651	-0.00805	-0.05178	0.02968	
49	-0.17764	-0.00028	-0.03700	-0.00054	0.30638	0.01233	
SUM	-0.76000	0.00000	0.00000	0.00042	0.29054	0.07089	
Condition	WL180=-WL0						
47	0.02878	0.00045	-0.06483	-0.00246	-0.06319	-0.00126	
48	-0.02200	0.00033	-0.03964	-0.00225	0.03495	0.00120	
49	-0.00678	-0.00078	-0.08753	-0.00413	0.00801	0.00015	
SUM	0.00000	0.00000	-0.19200	-0.00883	-0.02022	0.00010	

	WL210=-WL30					
47	-0.06383	-0.00096	0.04017	0.00166	0.01352	0.00540
48	-0.08296	0.00102	-0.02916	-0.00145	-0.01289	0.00568
49	-0.04821	-0.00006	-0.01101	-0.00012	0.08331	0.00221
SUM	-0.19500	0.00000	0.00000	0.00008	0.08394	0.01329
Condition	LC1=1.2DL+1.6W0					
47	-0.70338	1.08656	1.64637	-2.09206	1.62820	-3.66900
48	0.57199	1.09765	1.14874	-2.09440	-1.06677	3.67284
49	0.13139	1.11309	2.67203	4.35415	-0.15332	-0.01490
SUM	0.00000	3.29730	5.46714	0.16770	0.40812	-0.01106
Condition	LC2=1.2DL+1.6W30					
47	2.10030	1.10965	-1.17068	-2.16031	-0.24884	-3.78098
48	2.26789	1.08763	0.83432	-2.12205	0.26937	3.59855
49	1.52591	1.10002	0.33635	4.28086	-2.62411	-0.05275
SUM	5.89410	3.29730	0.00000	-0.00149	-2.60358	-0.23519
Condition	LC3=1.2DL-1.6W0					
47	0.90613	1.10299	-1.76366	-2.18779	-1.62847	-3.71136
48	-0.77441	1.10983	-1.26497	-2.18166	1.06628	3.71284
49	-0.13172	1.08448	-2.43851	4.20247	0.15450	-0.00885
SUM	0.00000	3.29730	-5.46714	-0.16698	-0.40769	-0.00737
Condition	LC4=1.2DL-1.6W30					
47	-1.89754	1.07990	1.05338	-2.11954	0.24857	-3.59938
48	-2.47031	1.11984	-0.95055	-2.15401	-0.26986	3.78713
49	-1.52624	1.09755	-0.10283	4.27576	2.62530	0.02900
SUM	-5.89410	3.29730	0.00000	0.00221	2.60401	0.21675
Condition	LC5=0.9DL+1.6W0					
47	-0.72872	0.81287	1.66103	-1.55708	1.62824	-2.74646
48	0.59729	0.82171	1.16327	-1.55989	-1.06671	2.74963
49	0.13143	0.83839	2.64284	3.28458	-0.15347	-0.01193
SUM	0.00000	2.47297	5.46714	0.16761	0.40806	-0.00875
Condition	LC6=0.9DL+1.6W30					
47	2.07496	0.83596	-1.15601	-1.62533	-0.24881	-2.85844
48	2.29319	0.81170	0.84885	-1.58754	0.26943	2.67534
49	1.52595	0.82532	0.30716	3.21128	-2.62426	-0.04978
SUM	5.89410	2.47297	0.00000	-0.00158	-2.60364	-0.23288
Condition	LC7=0.9DL-1.6W0					
47	0.88079	0.82930	-1.74900	-1.65281	-1.62844	-2.78882
48	-0.74911	0.83389	-1.25044	-1.64715	1.06634	2.78963
49	-0.13168	0.80978	-2.46770	3.13289	0.15435	-0.00588
SUM	0.00000	2.47297	-5.46714	-0.16707	-0.40775	-0.00507

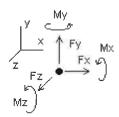
Condition	I C9=0 0DL 4 6W20					
47	LC8=0.9DL-1.6W30 -1.92289	0.80621	1.06805	-1.58456	0.24861	-2.67684
48	-2.44501	0.84391	-0.93602	-1.61951	-0.26980	2.8639
49	-1.52620	0.82286	-0.13202	3.20619	2.62515	0.03197
SUM	-5.89410	2.47297	0.00000	0.00212	2.60395	0.21906
Condition	LC9=1.2DL+Di+Wi0					
47	0.05875	1.82725	0.13849	-3.55446	0.22719	-6.09264
48	-0.08228	1.84270	0.05531	-3.50897	-0.13381	6.12160
49	0.02353	1.84000	0.53820	7.10614	-0.02699	-0.04570
SUM	0.00000	5.50995	0.73200	0.04271	0.06639	-0.01674
Condition	LC10=1.2DL+Di+Wi3	80				
47	0.43029	1.83456	-0.25240	-3.57482	-0.03599	-6.12781
48	0.15219	1.83898	0.01882	-3.51131	0.05149	6.09795
49	0.17752	1.83641	0.23358	7.08623	-0.30519	-0.05733
SUM	0.76000	5.50995	0.00000	0.00010	-0.28968	-0.08719
Condition	LC11=1.2DL+Di-Wi0					
47	0.28247	1.83163	-0.33627	-3.57715	-0.22729	-6.10521
48	-0.25869	1.84607	-0.25068	-3.52976	0.13323	6.13365
49	-0.02379	1.83225	-0.14504	7.06523	0.02938	-0.04431
SUM	0.00000	5.50995	-0.73200	-0.04167	-0.06468	-0.01587
Condition	LC12=1.2DL+Di-Wi3	0				
47	-0.08907	1.82432	0.05462	-3.55678	0.03589	-6.07005
48	-0.49316	1.84979	-0.21420	-3.52742	-0.05207	6.15731
49 	-0.17777 	1.83584	0.15958	7.08514	0.30757	-0.03268
SUM	-0.76000	5.50995	0.00000	0.00094	0.29139	0.05458
Condition	LC13=1.2DL					
47	0.10138	1.09478	-0.05865	-2.13993	-0.00013	-3.69018
48	-0.10121	1.10374	-0.05811	-2.13803	-0.00024	3.69284
49 	-0.00017	1.09878	0.11676	4.27831	0.00059	-0.01188
SUM	0.00000	3.29730	0.00000	0.00036	0.00021	-0.00922
Condition	LC14=0.9DL					
47	0.07603	0.82108	-0.04398	-1.60494	-0.00010	-2.76764
48	-0.07591	0.82780	-0.04359	-1.60352	-0.00018	2.76963
49	-0.00012	0.82409	0.08757	3.20873	0.00044	-0.00891
SUM	0.00000	2.47297	0.00000	0.00027	0.00016	-0.00691
	LC15=1.2DL+1.5LL1					
47	0.11676	1.30503	-0.06728	-2.75852	0.01232	-4.18314
48	-0.11650	1.31965	-0.06664	-2.76893	-0.01292	4.19012
49 	-0.00026	1.04761	0.13392	4.01082	0.00077	-0.01172
SUM	0.00000	3.67230	0.00000	-1.51664	0.00016	-0.00475

Condition L	.C16=1.2DL+1.5LL	_2				
47	0.11067	1.07599	-0.06747	-2.21660	0.00065	-3.47296
48	-0.10807	1.54342	-0.06244	-3.31229	0.00018	5.52983
49	-0.00260	1.05289	0.12991	4.00433	-0.00037	0.11498
SUM	0.00000	3.67230	0.00000	-1.52455	0.00046	2.17186
Condition L	.C17=1.2DL+WL0+	+1.5LLa1				
47	0.13305	1.84171	-0.02875	-3.72180	0.06283	-6.71915
48	-0.13947	1.85629	-0.05311	-3.97453	-0.03529	6.57613
49	0.00643	1.84929	0.27386	7.70592	-0.00713	0.12894
SUM	0.00000	5.54730	0.19200	0.00959	0.02042	-0.01408
Condition L	C18=1.2DL+WL30	)+1.5LLa1				
47	0.22565	1.84312	-0.13375	-3.72592	-0.01388	-6.72581
48	-0.07851	1.85560	-0.06359	-3.97532	0.01255	6.57166
49	0.04786	1.84857	0.19735	7.70192	-0.08242	0.12688
SUM	0.19500	5.54730	0.00000	0.00068	-0.08375	-0.02727
Condition L	C19=1.2DL-WL0+	1.5LLa1				
47	0.19060	1.84261	-0.15842	-3.72672	-0.06354	-6.72167
48	-0.18347	1.85695	-0.13239	-3.97902	0.03462	6.57854
49	-0.00713	1.84774	0.09881	7.69766	0.00890	0.12925
SUM	0.00000	5.54730	-0.19200	-0.00807	-0.02003	-0.01388
Condition L	C20=1.2DL-WL30	+1.5LLa1				
47	0.09799	1.84120	-0.05341	-3.72260	0.01317	-6.71501
48	-0.24443	1.85764	-0.12191	-3.97823	-0.01322	6.58301
49	-0.04856	1.84846	0.17532	7.70167	0.08419	0.13130
SUM	-0.19500	5.54730	0.00000	0.00084	0.08413	-0.00070
Condition L	C25=1.2DL+WL0+	1.5LLa3				
47	0.15803	1.84054	-0.04409	-3.52458	0.06370	-5.85990
48	-0.16516	1.85735	-0.06694	-3.33367	-0.03487	5.97522
49	0.00713	1.84940	0.30303	6.86768	-0.00604	-0.13133
SUM	0.00000	5.54730	0.19200	0.00943	0.02279	-0.01602
Condition Lo	C26=1.2DL+WL30	+1.5LLa3				
47	0.25064	1.84195	-0.14910	-3.52869	-0.01301	-5.86655
48	-0.10421	1.85667	-0.07742	-3.33446	0.01297	5.97074
49	0.04857	1.84868	0.22652	6.86367	-0.08133	-0.13339
SUM	0.19500	5.54730	0.00000	0.00052	-0.08137	-0.02920
Condition Le	C27=1.2DL-WL0+1	I.5LLa3				
47	0.21558	1.84144	-0.17376	-3.52949	-0.06268	-5.86241
48	-0.20916	1.85802	-0.14622	-3.33816	0.03504	5.97762
49 	-0.00642	1.84785	0.12798	6.85942	0.00999	-0.13103
SUM	0.00000	5.54730	-0.19200	-0.00823	-0.01766	-0.01582

Condition	LC28=1.2DL-WL30-	+1.5LLa3				
47	0.12298	1.84003	-0.06876	-3.52538	0.01403	-5.85576
48	-0.27012	1.85870	-0.13574	-3.33737	-0.01280	5.98210
49	-0.04786	1.84857	0.20450	6.86343	0.08528	-0.12897
SUM	-0.19500	5.54730	0.00000	0.00068	0.08651	-0.00263
Condition	LC29=1.2DL+WL0+	-1.5LLa4				
47	0.13295	1.84176	-0.02866	-3.96587	0.06298	-6.57759
48	-0.13950	1.85613	-0.05317	-3.73121	-0.03531	6.71694
49	0.00655	1.84940	0.27384	7.70650	-0.00720	-0.15325
SUM	0.00000	5.54730	0.19200	0.00943	0.02048	-0.01390
Condition	LC30=1.2DL+WL30	+1.5LLa4				
47	0.22556	1.84317	-0.13367	-3.96999	-0.01373	-6.58425
48	-0.07854	1.85545	-0.06365	-3.73200	0.01254	6.71246
49	0.04798	1.84868	0.19732	7.70250	-0.08249	-0.15531
SUM	0.19500	5.54730	0.00000	0.00051	-0.08369	-0.02709
Condition	LC31=1.2DL-WL0+	1.5LLa4				
47	0.19050	1.84265	-0.15833	-3.97079	-0.06340	-6.58011
48	-0.18349	1.85679	-0.13245	-3.73570	0.03460	6.71934
49	-0.00701	1.84785	0.09878	7.69825	0.00883	-0.15294
SUM	0.00000	5.54730	-0.19200	-0.00824	-0.01997	-0.01370
Condition	LC32=1.2DL-WL30+	+1.5LLa4				
47	0.09789	1.84125	-0.05333	-3.96667	0.01331	-6.57345
48	-0.24445	1.85748	-0.12197	-3.73491	-0.01324	6.72382
49	-0.04844	1.84857	0.17530	7.70225	0.08412	-0.15088
SUM	-0.19500	5.54730	0.00000	0.00068	0.08419	-0.00052

### **Envelope for nodal reactions**

Note.- Ic is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for

W180=-W0

W210=-W30

Wi180=-Wi0

Wi210=-Wi30

WL180=-WL0

WL210=-WL30

LC1=1.2DL+1.6W0

LC2=1.2DL+1.6W30

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LC3=1.2DL-1.6W0 LC4=1.2DL-1.6W30 LC5=0.9DL+1.6W0 LC6=0.9DL+1.6W30 LC7=0.9DL-1.6W0 LC8=0.9DL-1.6W30 LC9=1.2DL+Di+Wi0 LC10=1.2DL+Di+Wi30 LC11=1.2DL+Di-Wi0 LC12=1.2DL+Di-Wi30 LC13=1.2DL LC14=0.9DL LC15=1.2DL+1.5LL1 LC16=1.2DL+1.5LL2 LC17=1.2DL+WL0+1.5LLa1 LC18=1.2DL+WL30+1.5LLa1 LC19=1.2DL-WL0+1.5LLa1 LC20=1.2DL-WL30+1.5LLa1 LC25=1.2DL+WL0+1.5LLa3 LC26=1.2DL+WL30+1.5LLa3 LC27=1.2DL-WL0+1.5LLa3 LC28=1.2DL-WL30+1.5LLa3 LC29=1.2DL+WL0+1.5LLa4 LC30=1.2DL+WL30+1.5LLa4 LC31=1.2DL-WL0+1.5LLa4

LC32=1.2DL-WL30+1.5LLa4

		Forces					Moments						
Node		Fx [Kip]	łc	<b>Fy</b> [Kip]	Ic	<b>Fz</b> [Kip]	lc	Mx [Kip*ft]	lc	<b>My</b> [Kip*ft]	lc	<b>Mz</b> [Kip*ft]	lc
47	Max	2.100	LC2	1.843	LC30	1.661	LC5	0.01274	W210	1.62824	LC5	0.05675	W210
	Min	-1.923	LC8	-0.009	W210	-1.764	LC3	-3.97079	LC31	-1.62847	LC3	-6.72581	LC18
48	Max	2.293	LC6	1.859	LC28	1.163	LC5	-0.00145	WL210	1.06634	LC7	6.72382	LC32
	Min	-2.470	LC4	0.000	WL180	-1.265	LC3	-3.97902	LC19	-1.06677	LC1	0.00120	WL180
49	Max	1.526	LC6	1.849	LC29	2.672	LC1	7.70650	LC29	2.62530	LC4	0.13130	LC20
	Min	-1.526	LC4	-0.009	W180	-2.468	LC7	-0.04740	W180	-2.62426	LC6	-0.15531	LC30

Date: 5/9/2018

Project Name: WEST HARTFORD/I-84/X43

Project Number: 829013

Designed By: BD Checked By: MSC



## **CHECK CONNECTION CAPACITY (Worse Case)**

**Reference:** AISC Steel Construction Manual 9th Edition (ASD)

**Bolt Type =** 

Threaded Rod

**Bolt Diameter =** 

1/2 in.

Steel Grade =

A36

Allowable Tensile Load =

F<sub>Tall</sub> = 3750 lbs.

Allowable Shear Load =

F<sub>Vall</sub>= 1940 lbs.

**WIND FORCES** 

Reaction

**F** = 2672 lbs.

**GRAVITY LOADS** 

Ice and Equipment

1859 lbs.

No. of Supports =

1

No. of Bolts / Support =

2

Tension Design Load /Bolts =

 $f_t$ = 1336.00 lbs.

3750 lbs. Therefore, OK!

Shear Design Load / Bolts=

 $f_v$ = 929.50 lbs. < 1940 lbs. Therefore, OK!

**CHECK COMBINED TENSION AND SHEAR** 

 $f_{t}/F_{T}$ 

 $f_v/F_v$ 

**≤** 1.0

0.356

0.479

= 0.835

< 1.0 Therefore, OK!



## RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

## T-Mobile Existing Facility

Site ID: CT11178D

West Hartford/I-84/X43
467 South Quaker Lane (Church of St. Mark)
West Hartford, CT 06110
July 25, 2018

EBI Project Number: 6218005237

Site Compliance Summary					
Compliance Status:	COMPLIANT				
Site total MPE% of					
FCC general	19.95 %				
population	13.33 /0				
allowable limit:					



July 25, 2018

T-Mobile USA Attn: Jason Overbey, RF Manager 35 Griffin Road South Bloomfield, CT 06002

Emissions Analysis for Site: CT11178D - West Hartford/I-84/X43

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **467 South Quaker** Lane (Church, West Hartford, CT, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu$ W/cm<sup>2</sup>). The number of  $\mu$ W/cm<sup>2</sup> calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu$ W/cm²). The general population exposure limits for the 600 MHz and 700 MHz Band are approximately 400  $\mu$ W/cm² and 467  $\mu$ W/cm² respectively. The general population exposure limit for the 1900 MHz (PCS) and 2100 MHz (AWS) bands is 1000  $\mu$ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

#### **CALCULATIONS**

Calculations were done for the proposed T-Mobile Wireless antenna facility located at **467 South Quaker Lane, West Hartford, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 GSM channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) 2 UMTS channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 3) 2 LTE channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 4) 4 LTE channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 5) 2 LTE channels (600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 6) 2 LTE channels (700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.



- 7) 1 microwave backhaul channel (10GHz) was considered for the proposed facility. This channel has a transmit power of 1 Watt.
- 8) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 9) For the following calculations the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 10) The antennas used in this modeling are the **Ericsson AIR3246 B66, Ericsson AIR32 B66A/B2A** and the **RFS APXVAARR24\_43-U-NA20** for 600 MHz, 700 MHz, 1900 MHz
  (PCS) and 2100 MHz (AWS) channels. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 11) The antenna mounting height centerline of the proposed antennas is **120 feet** above ground level (AGL).
- 12) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
- 13) All calculations were done with respect to uncontrolled / general population threshold limits.



### **T-Mobile Site Inventory and Power Data**

Sector:	A	Sector:	В	Sector:	С
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	Ericsson AIR3246 B66	Make / Model:	Ericsson AIR3246 B66	Make / Model:	Ericsson AIR3246 B66
Gain:	15.9 dBd	Gain:	15.9 dBd	Gain:	15.9 dBd
Height (AGL):	120	Height (AGL):	120	Height (AGL):	120
Frequency Bands	2100 MHz (AWS)	Frequency Bands	2100 MHz (AWS)	Frequency Bands	2100 MHz (AWS)
Channel Count	4	Channel Count	4	Channel Count	4
Total TX Power(W):	240	Total TX Power(W):	240	Total TX Power(W):	240
ERP (W):	9,337.08	ERP (W):	9,337.08	ERP (W):	9,337.08
Antenna A1 MPE%	2.58	Antenna B1 MPE%	2.58	Antenna C1 MPE%	2.58
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	Ericsson AIR32 B66A/B2A	Make / Model:	Ericsson AIR32 B66A/B2A	Make / Model:	Ericsson AIR32 B66A/B2A
Gain:	15.9 dBd	Gain:	15.9 dBd	Gain:	15.9 dBd
Height (AGL):	120	Height (AGL):	120	Height (AGL):	120
Frequency Bands	1900 MHz (PCS)	Frequency Bands	1900 MHz (PCS)	Frequency Bands	1900 MHz (PCS)
Channel Count	4	Channel Count	4	Channel Count	4
Total TX Power(W):	180	Total TX Power(W):	180	Total TX Power(W):	180
ERP (W):	7,002.81	ERP (W):	7,002.81	ERP (W):	7,002.81
Antenna A2 MPE%	1.94	Antenna B2 MPE%	1.94	Antenna C2 MPE%	1.94
Antenna #:	3	Antenna #:	3	Antenna #:	3
Make / Model:	RFS APXVAARR24_43-U- NA20	Make / Model:	RFS APXVAARR24_43-U- NA20	Make / Model:	RFS APXVAARR24_43-U- NA20
Gain:	16.35 / 12.95 / 13.35 dBd	Gain:	16.35 / 12.95 / 13.35 dBd	Gain:	16.35 / 12.95 / 13.35 dBd
Height (AGL):	120	Height (AGL):	120	Height (AGL):	120
Frequency Bands	2100 MHz / 600 MHz / 700 MHz	Frequency Bands	2100 MHz / 600 MHz / 700 MHz	Frequency Bands	2100 MHz / 600 MHz / 700 MHz
Channel Count	6	Channel Count	6	Channel Count	6
Total TX Power(W):	180	Total TX Power(W):	180	Total TX Power(W):	180
ERP (W):	5,070.20	ERP (W):	5,070.20	ERP (W):	5,070.20
Antenna A3 MPE%	2.30	Antenna B3 MPE%	2.30	Antenna C3 MPE%	2.30

Site Composite MPE%						
Carrier	MPE%					
T-Mobile (Per Sector Max)	6.82 %					
AT&T	4.96					
Clearwire	0.34					
Verizon Wireless	7.83					
Site Total MPE %:	19.95 %					

T-Mobile Sector A Total:	6.82 %		
T-Mobile Sector B Total:	6.82 %		
T-Mobile Sector C Total:	6.82 %		
Site Total:	19.95 %		



## **T-Mobile Max Power Values (Per Sector)**

T-Mobile _Max Power Values (Per Sector)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (µW/cm²)	Frequency (MHz)	Allowable MPE (µW/cm²)	Calculated % MPE
					AWS - 2100		
T-Mobile AWS - 2100 MHz LTE	4	2,334.27	120	25.83	MHz	1000.00	2.57%
					PCS - 1900		
T-Mobile PCS - 1900 MHz LTE	2	2,334.27	120	12.91	MHz	1000.00	1.29%
					PCS - 1900		
T-Mobile PCS - 1900 MHz GSM	2	1,167.14	120	6.46	MHz	1000.00	0.65%
T-Mobile AWS - 2100 MHz UMTS	2	1,294.56	120	7.16	AWS - 2100 MHz	1000.00	0.72%
T-Mobile 600 MHz LTE	2	591.73	120	3.27	600 MHz	400.00	0.82%
T-Mobile 700 MHz LTE	2	648.82	120	3.59	700 MHz	467.00	0.77%
						Total:	6.82 %

21 B Street Burlington, MA 01803 Tel: (781) 273.2500 Fax: (781) 273.3311



## **Summary**

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)
Sector A:	6.82 %
Sector B:	6.82 %
Sector C:	6.82 %
T-Mobile Maximum	6.82 %
MPE % (Per Sector):	0.82 %
Site Total:	19.95 %
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **19.95%** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.