



**Centek Engineering, Inc.**  
3-2 North Branford Road  
Branford, Connecticut 06405  
Phone: (203) 488-0580  
Fax: (203) 488-8587

**Steven L. Levine**  
Real Estate Consultant

**HAND DELIVERED**

April 18, 2016

Attorney Melanie Bachman  
Acting Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, Connecticut 06051

**Notice of Exempt Modification: Existing Telecommunications Facility at Garden Circle  
(Farmdale Drive), Waterbury**

Dear Ms. Bachman:

In order to accommodate technological changes, implement Uniform Mobile Telecommunications System ("UMTS") and/or Long Term Evolution ("LTE") capabilities, and enhance system performance in the State of Connecticut, New Cingular Wireless PCS, LLC ("AT&T") plans to modify the equipment configurations at many of its existing cell sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, copies of this letter are being sent to the chief elected official of the municipality in which the affected cell site is located, the property owner of record, and the tower owner or operator.

UMTS technology offers services to mobile computer and phone users anywhere in the world. Based on the Global System for Mobile ("GSM") communication standard, UMTS is the planned worldwide standard for mobile users. UMTS, fully implemented, gives computer and phone users high-speed access to the Internet as they travel. They have the same capabilities even when they roam, through both terrestrial wireless and satellite transmissions.

LTE is a high-performance air interface for cellular mobile communications. It is designed to increase the capacity and speed of mobile telephone networks.

Attached is a summary of the planned modifications, including power density calculations reflecting the change in AT&T's operations at the site. Also included is documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration.

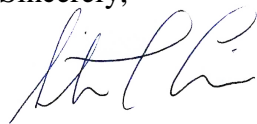
The changes to the facility do not constitute modifications as defined in Connecticut General Statutes ("C.G.S.") Section 16-50i(d) because the general physical and environmental characteristics of the site will not be significantly changed or altered. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in R.C.S.A. Section 16-50j-72(b)(2).

1. The height of the overall structure will not increase.
2. The proposed changes will not extend the site boundaries.
3. The proposed changes will not increase the noise level at the site boundary by six decibels or more, or to levels that exceed state and local criteria.
4. The changes will not add radio frequency sending or receiving capability which increases the total radio frequency electromagnetic radiation power density measured at the site boundary to or above the standards adopted by the Federal Communications Commission pursuant to Section 704 of the Telecommunications Act of 1996, as amended, and the State Department of Energy and Environmental Protection, pursuant to Section 22a-162 of the Connecticut General Statutes.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The proposed changes will not impair the structural integrity of the facility, as determined in a certification provided by a professional engineer licensed in Connecticut.

For the foregoing reasons, AT&T respectfully submits that the proposed changes at the referenced site constitute exempt modifications under R.C.S.A. Section 16-50j-72(b)(2).

Please feel free to call me at (860) 830-0380 with questions concerning this matter. Thank you for your consideration.

Sincerely,



Steven L. Levine  
Real Estate Consultant

cc: TownCEO – Mayor Neil M. O'Leary, City of Waterbury  
Property Owner of Record – AT&T  
Tower Owner / Operator – American Tower Corporation (by email)

Attachments

**NEW CINGULAR WIRELESS PCS, LLC**  
**Equipment Modification**

Garden Circle (Farmdale Drive), Waterbury, CT

Site Number 1005

Prior Decisions: Docket 44.5

EM's 4/89, 3/94, 8/02, 7/07, 5/12, 6/13, 5/14, 6/15

**Tower Owner/Manager:** American Tower

**Property Owner:** AT&T

**Original Permitting:** The Garden Circle (Farmdale Drive), Waterbury site was approved by the Council in 1984 in Docket 44.5, the tower not to exceed 167 feet in height. Please refer to the attached Decision & Order. Proposed equipment modifications will not violate any of the approval conditions.

**Lease Area:** The Garden Circle (Farmdale Drive), Waterbury site was approved by the Council in Docket 44.5 with a 70 ft x 70 ft lease area. (See attached site plan from Docket 44.5 Application.) Subsequently, on 3/30/94 the Council approved an exempt modification expanding the lease and fenced areas to 70 ft x 100 ft, as shown in the current construction drawings ("CD's"; attached) to accommodate colocation by Verizon. No further changes have been made to the site's lease and fenced areas. Since all proposed equipment modifications will occur either on the existing tower structure or within AT&T's existing equipment shelter, the proposed modifications will not extend either the lease area or the overall site boundaries.

**Equipment configuration:** 155 ft. Guyed Monopole

**Current and/or approved:** Equipment platform @ 150 ft  
Three PowerWave 7770 antennas @ 153 ft c.l.  
Three CCI OPA-65R-LCUU-H6 antennas @ 153 ft c.l.  
Three CCI OPA-65R-LCUU-H8 antennas @ 153 ft c.l.  
Twelve TMA's @ 153 ft  
Nine remote radio heads @ 153 ft  
Two Raycap DC6-48-60-18-8F surge arrestors @ 153 ft  
Twelve lines 1¼ inch coax  
Two fiber and four DC control cables  
Equipment shelter  
Diesel generator on concrete pad

**Proposed modifications:** Remove two CCI OPA-65R-LCUU-H6 antennas.  
Remove one CCI OPA-65R-LCUU-H8 antenna.  
Remove three RRUS-11 remote radio heads.  
Install two CCI TPA-65R-LCUUUU-H8 antennas @ 153 ft c.l.  
Install one Quintel QS66512-3 antenna @ 153 ft c.l.  
Install three RRUS-32 remote radio heads @ 153 ft c.l.

## Power Density:

Worst-case calculations with 10 dB reduction for existing wireless operations at the site indicate a radio frequency electromagnetic radiation power density, measured at six feet above ground level beside the tower, of approximately 3.8 % of the standard adopted by the FCC. As depicted in the second table below, the total radio frequency electromagnetic radiation power density following proposed modifications would be approximately 5.3 % of the standard.

### Existing

Company	Frequency (MHz)	Centerline Ht (feet)	Number of Channels	Power Per Channel (Watts)	Power Density (mW/cm <sup>2</sup> )	Standard Limits (mW/cm <sup>2</sup> )	Percent of Limit
Other Users *							2.63
AT&T LTE †	740	154	1	500	0.0082	0.4933	0.17
AT&T LTE †	880	154	1	500	0.0082	0.5867	0.14
AT&T LTE †	1900	154	1	500	0.0082	1.0000	0.08
AT&T LTE †	2300	154	1	500	0.0082	1.0000	0.08
AT&T UMTS †	880	154	3	500	0.0246	0.5867	0.42
AT&T UMTS †	1900	154	1	500	0.0082	1.0000	0.08
AT&T GSM †	880	154	1	296	0.0049	0.5867	0.08
AT&T GSM †	1900	154	1	427	0.0070	1.0000	0.07
<b>Total</b>							<b>3.76%</b>

\* Per CSC records.

† Source of AT&T Data is EM-CING-151-150605.

### Proposed

Company	Frequency (MHz)	Antenna (Total for all sectors)	Centerline Ht (feet)	Number of Channels	Power Per Channel (Watts)	Power Density (mW/cm <sup>2</sup> )	Standard Limits (mW/cm <sup>2</sup> )	Percent of Limit
Other Users *								2.63
AT&T LTE	740	CCI TPA 2 antennas  Quintel 1 antenna	153	2	1476	0.0491	0.4933	1.00
AT&T LTE	1900	CCI TPA 2 antennas  Quintel 1 antenna	153	2	2421	0.0806	1.0000	0.81
AT&T LTE	2300	CCI OPA H8 2 antennas  CCI OPA H6 1 antenna	153	2	1146	0.0381	1.0000	0.38
AT&T UMTS	880	PW 7770 3 antennas	153	3	261	0.0130	0.5867	0.22
AT&T UMTS	1900	PW 7770 3 antennas	153	2	424	0.0141	1.0000	0.14
AT&T GSM	880	CCI OPA H8 2 antennas  CCI OPA H6 1 antenna	153	1	261	0.0043	0.5867	0.07
<b>Total</b>								<b>5.25%</b>

\* Per CSC records

**Structural information:**

The attached structural analysis (American Tower Corp., 4/12/16) demonstrates that the tower and foundation are adequate to accommodate the proposed equipment modifications.

## Docket 44 Excerpt

### DOCKET NO. 44

AN APPLICATION SUBMITTED BY THE SOUTHERN : CONNECTICUT SITING  
NEW ENGLAND TELEPHONE COMPANY FOR A  
CERTIFICATE OF ENVIRONMENTAL COMPATIBILITY : COUNCIL  
AND PUBLIC NEED FOR THE CONSTRUCTION,  
MAINTENANCE AND OPERATION OF FACILITIES TO  
PROVIDE CELLULAR SERVICE IN NEW HAVEN COUNTY : July 24, 1984

### D E C I S I O N A N D O R D E R

Pursuant to the foregoing opinion, the Council hereby directs that a certificate of environmental compatibility and public need as required by section 16-50k of the General Statutes of Connecticut, revisions of 1958, revised to 1983, as amended, be issued to the Southern New England Telephone Company for the construction, operation, and maintenance of a telecommunications tower and associated equipment to provide cellular service at each of the following sites:

Jasudowich tract, Brushy Plain Road, Branford, Connecticut;  
Town of Guilford tract, Tanner Marsh Road, Guilford, Connecticut;  
Bridgeport Avenue, Milford, Connecticut;  
Quagliaro tract, Farmdale Drive, Waterbury, Connecticut;  
Pease Road, Woodbridge, Connecticut; and  
Dwight Street, North Haven, Connecticut.

The facilities shall be constructed, operated, and maintained as specified in the Council's record on this matter, and subject to the following conditions:

1. The towers including antennas shall be no taller than necessary to provide the proposed service and in no event shall exceed
  - a) 167' at the Branford site,
  - b) 167' at the Guilford site,
  - c) 117' at the Milford site,
  - d) 167' at the Waterbury site,
  - e) 167' at the Woodbridge site,
  - f) 167' at the North Haven site;
2. A fence not lower than eight feet shall surround each tower and its associated equipment;

3. The applicant or its successor shall notify the Council if and when directional antennas or any other equipment is added to any of these facilities;
4. The applicant or its successor shall permit, in accordance with representations made by it during the proceeding, public or private entities to share space on the facilities, for due consideration received, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing;
5. Unless necessary to comply with condition number six, below, no lights shall be installed on any of these towers;
6. The facilities shall be constructed in accordance with all applicable federal, state, and municipal laws and regulations;
7. The applicant shall submit a development and management plan (D&M) for the Branford, Milford, Woodbridge, and North Haven sites pursuant to sections 16-50j-85 through 16-50j-87 of the regulations of state agencies, except that irrelevant items in section 16-50j-86 need only be identified as such. The D&M plans shall include appropriate evergreen screening of the sites, erosion control measures, reseeding plans, and tree removal plans. The applicant shall comply with the reporting requirements of section 16-50j-87 for all sites;
8. Construction activities shall take place during daylight working hours;
9. This decision and order shall be void and the towers and associated equipment approved herein shall be dismantled and removed, or reapplication for any new use shall be made to the Connecticut

Siting Council before any such new use is made, if the towers do not provide or permanently cease to provide cellular service following completion of construction;

10. This decision and order shall be void if all construction authorized is not completed within three years of the issuance of this decision.

Pursuant to section 16-50p of the General Statutes, we hereby direct that a copy of the opinion and decision and order be served on each person listed below. A notice of the issuance shall be published in the Hartford Courant, New Haven Register, and the Waterbury Republican.

The parties to this proceeding are

The Southern New England Telephone Company (Applicant)  
Room 314  
227 Church Street  
New Haven, Connecticut 06506

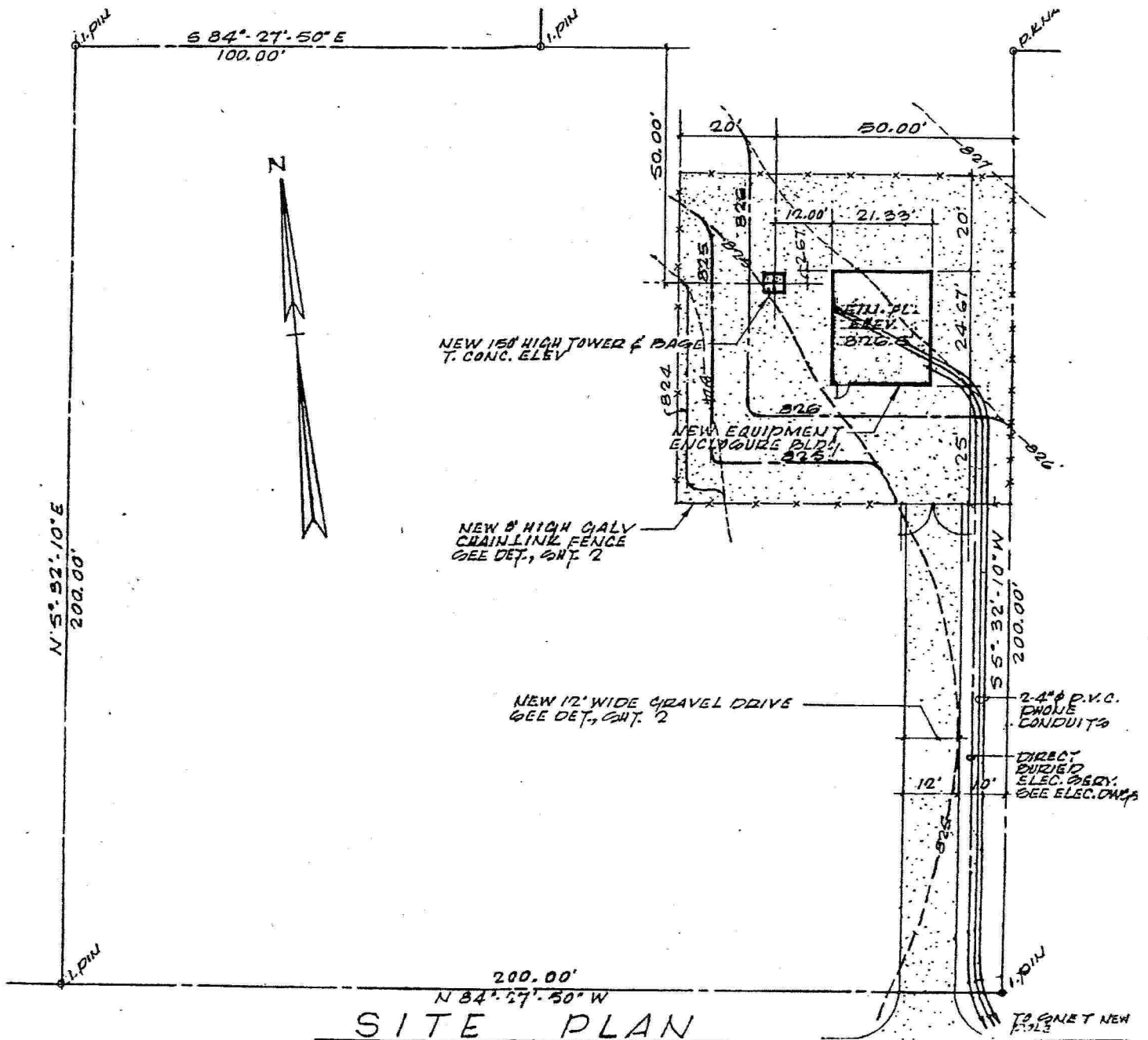
ATTENTION: Mr. Peter J. Tyrrell (its attorney)  
Senior Attorney

Town of Hamden represented by:  
Peter F. Villano, Mayor  
Shirley Gonzales, Town Planner  
Mr. Hugh Manke, Esquire  
Office of the Town Attorney  
Memorial Town Hall  
2372 Whitney Avenue  
Hamden, Connecticut 06518

Inland Wetlands Agency represented by:  
Town of Woodbridge  
Robert J. Klancko  
Chairman  
Town Hall  
11 Meeting House Lane  
Woodbridge, Connecticut 06525



Connecticut Siting Council Application  
Southern New England Telephone Company



SITE PLAN

TO SHEET NEW  
P. 12

**PROJECT INFORMATION**

SCOPE OF WORK: REMOVE & RELOCATE (1) EXISTING ANTENNA PER SECTOR, REMOVE & RELOCATE (1) EXISTING RRUS PER SECTOR

SITE ADDRESS: FARMDALE DRIVE  
WATERBURY, CT 06704

LATITUDE: 41° 34' 14.4" (NAD 83)\*  
LONGITUDE: 73° 01' 3.3" (NAD 83)\*

\*PER AT&T EXISTING PLANS

JURISDICTION: CONNECTICUT SITING COUNCIL

CURRENT USE: TELECOMMUNICATIONS FACILITY  
PROPOSED USE: TELECOMMUNICATIONS FACILITY

NAME OF APPLICANT: AT&T MOBILITY  
500 ENTERPRISE DRIVE,  
SUITE 3A  
ROCKY HILL, CT 06067

TOWER OWNER: AMERICAN TOWER  
TOWER NUMBER: 302476

**DRAWING INDEX**

TITLE SHEET	REV
T01	4
G01	4
A01	4
A02	4
A03	4
E01	4

THIS DOCUMENT WAS DEVELOPED TO REFLECT A SPECIFIC SITE AND ITS SITE CONDITIONS AND IS NOT TO BE USED FOR ANOTHER SITE OR WHEN OTHER CONDITIONS PERTAIN. REUSE OF THIS DOCUMENT IS AT THE SOLE RISK OF THE USER.

**STRUCTURAL NOTE:**

1. AS REQUIRED THE TIA/EIA 222F - STANDARD, SAI COMMUNICATIONS, INC. SHALL PROVIDE A STRUCTURAL ANALYSIS OF THE TOWER PREPARED BY A LICENSED CONNECTICUT STRUCTURAL ENGINEER CERTIFYING THAT, THE EXISTING TOWER AND ANY REQUIRED IMPROVEMENTS AND REINFORCEMENTS HAVE SUFFICIENT CAPACITY TO SUPPORT ALL EXISTING AND PROPOSED ANTENNAS, CABLES, SUPPORTS AND APPURTENANCES AND COMPLIES WITH THE CURRENT CONNECTICUT STATE BUILDING CODE AND EIA/TIA CRITERIA. THE CONTRACTOR IS RESPONSIBLE TO CONFIRM THAT ANY IMPROVEMENTS AND REINFORCEMENTS REQUIRED BY THE STRUCTURAL ANALYSIS CERTIFICATION ARE PROPERLY INSTALLED PRIOR TO THE ADDITION OF ANTENNAS, CABLES, SUPPORTS AND APPURTENANCES PROPOSED ON THESE DRAWINGS OR OTHERWISE NOTED IN THE STRUCTURAL ANALYSIS.

**CONTACT INFORMATION**

CONTACT	COMPANY	PHONE NO.
ENGINEERING:	DEWBERRY	(973) 576-8653
SAC:	SAI	(978) 807-2700
CONST.:	SAI	(978) 979-7638



**Dewberry**  
Dewberry Engineers, Inc.  
600 PARSONSPANY ROAD  
SUITE 301  
PARSONSPANY, NJ 07054  
PHONE: 973.738.9400  
FAX: 973.738.9710



**SAI**  
27 NORTHWESTERN DRIVE  
SALEM, NH 03079

**WOLCOTT WEST  
SITE NO. CT1005**  
FARMDALE DRIVE  
WATERBURY, CT 06704



500 ENTERPRISE DRIVE,  
SUITE 3A  
ROCKY HILL, CT 06067

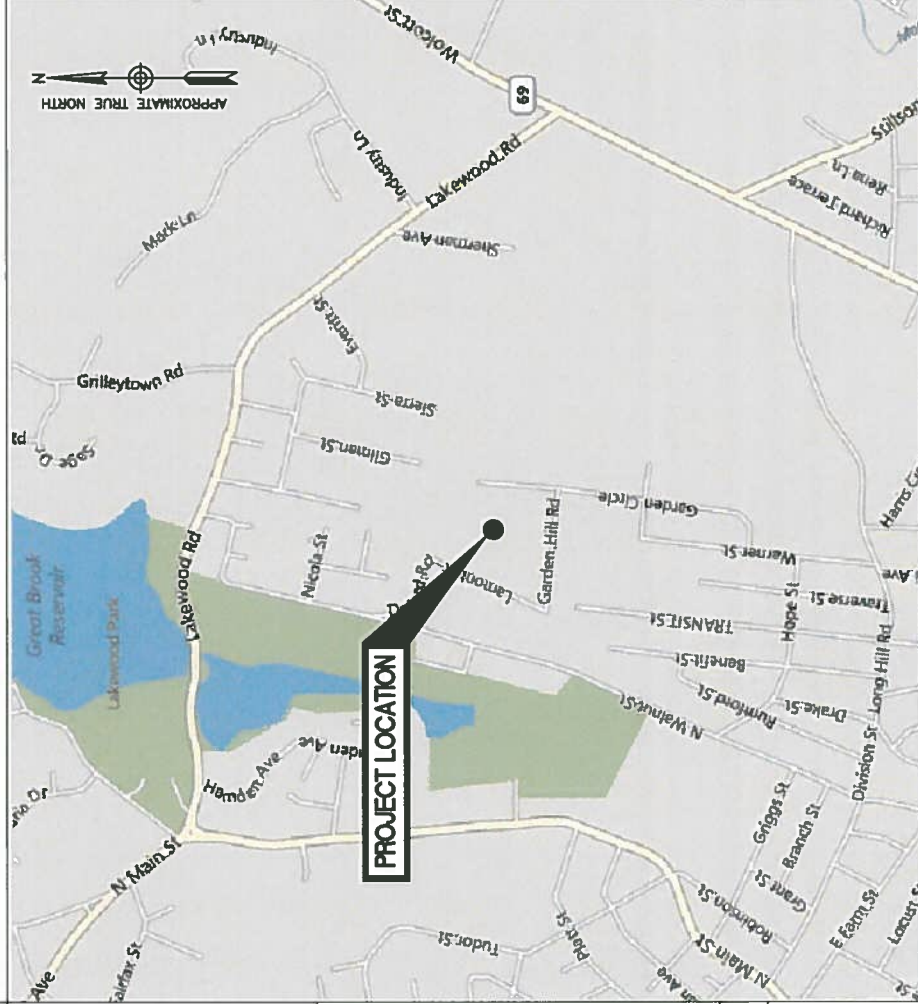


**at&t**

**SITE NAME: WOLCOTT WEST  
SITE NUMBER: CT1005**

**VICINITY MAP**

**DIRECTIONS:** (FROM ROCKY HILL, CT) HEAD NORTHEAST ON ENTERPRISE DR TOWARD CAPITOL BLVD. 0.3 MILES TURN LEFT ONTO CAPITOL BLVD. 0.2 MILES TURN LEFT ONTO WEST ST. 0.3 MILES MERGE ONTO I-81 S VIA RAMP ON THE LEFT TOWARD NEW HAVEN. 9.0 MILES MERGE ONTO I-81 W VIA EXIT 18 TOWARD MERIDEN/WATERBURY. 7.9 MILES MERGE ONTO I-84 W VIA EXIT 1 ON THE LEFT TOWARD WATERBURY/DANBURY. 7.4 MILES TAKE THE UNION ST EXIT TOWARD DOWNTOWN WATERBURY. STAY STRAIGHT TO GO ONTO BRASS MILL DR. BRASS MILL DR BECOMES WELTON ST. 0.1 MILES TURN RIGHT ONTO WALNUT ST. 0.8 MILES TURN RIGHT ONTO DELFORD RD. DELFORD RD BECOMES LAMONT ST. 0.1 MILES TURN LEFT ONTO GARDEN HILL RD. TURN LEFT ONTO GARDEN HILL CIRCLE. TURN LEFT ONTO FARMDALE DR. SITE IS ON THE RIGHT.



**APPLICABLE BUILDING CODES AND STANDARDS**

CONTRACTOR'S WORK SHALL COMPLY WITH PROJECT STANDARD NOTES, SYMBOLS AND DETAILS (SEE DRAWING INDEX FOR STANDARD NOTES AND DETAILS INCLUDED WITH TYPICAL DRAWING PACKAGE). CONTRACTOR WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.

BUILDING CODE:  
CONNECTICUT STATE BUILDING CODE (2005) & ALL SUBSEQUENT AMENDMENTS

ELECTRICAL CODE:  
NATIONAL ELECTRICAL CODE (NEC 2005)

CONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS.  
AMERICAN CONCRETE INSTITUTE (ACI) 318, BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE  
AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC), MANUAL OF STEEL CONSTRUCTION, ASD, NINTH EDITION

TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-F, STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWER AND ANTENNA SUPPORTING STRUCTURES:

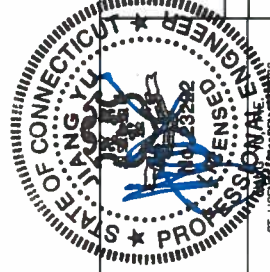
TIA 607, COMMERCIAL BUILDING GROUNDING AND BONDING REQUIREMENTS FOR TELECOMMUNICATIONS INSTITUTE FOR ELECTRICAL AND ELECTRONICS ENGINEERS (IEEE) 81, GUIDE FOR MEASURING EARTH RESISTIVITY, GROUND IMPEDANCE, AND EARTH SURFACE POTENTIALS OF A GROUND SYSTEM  
IEEE 1100 (1999) RECOMMENDED PRACTICE FOR POWERING AND GROUNDING OF ELECTRONIC EQUIPMENT

IEEE C62.41, RECOMMENDED PRACTICES ON SURGE VOLTAGES IN LOW VOLTAGE AC POWER CIRCUITS (FOR LOCATION CATEGORY "C3" AND "HIGH SYSTEM EXPOSURE")

TELCORDIA GR-1503, COAXIAL CABLE CONNECTIONS

ANSI T1.311, FOR TELECOM - DC POWER SYSTEMS - TELECOM, ENVIRONMENTAL PROTECTION

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.



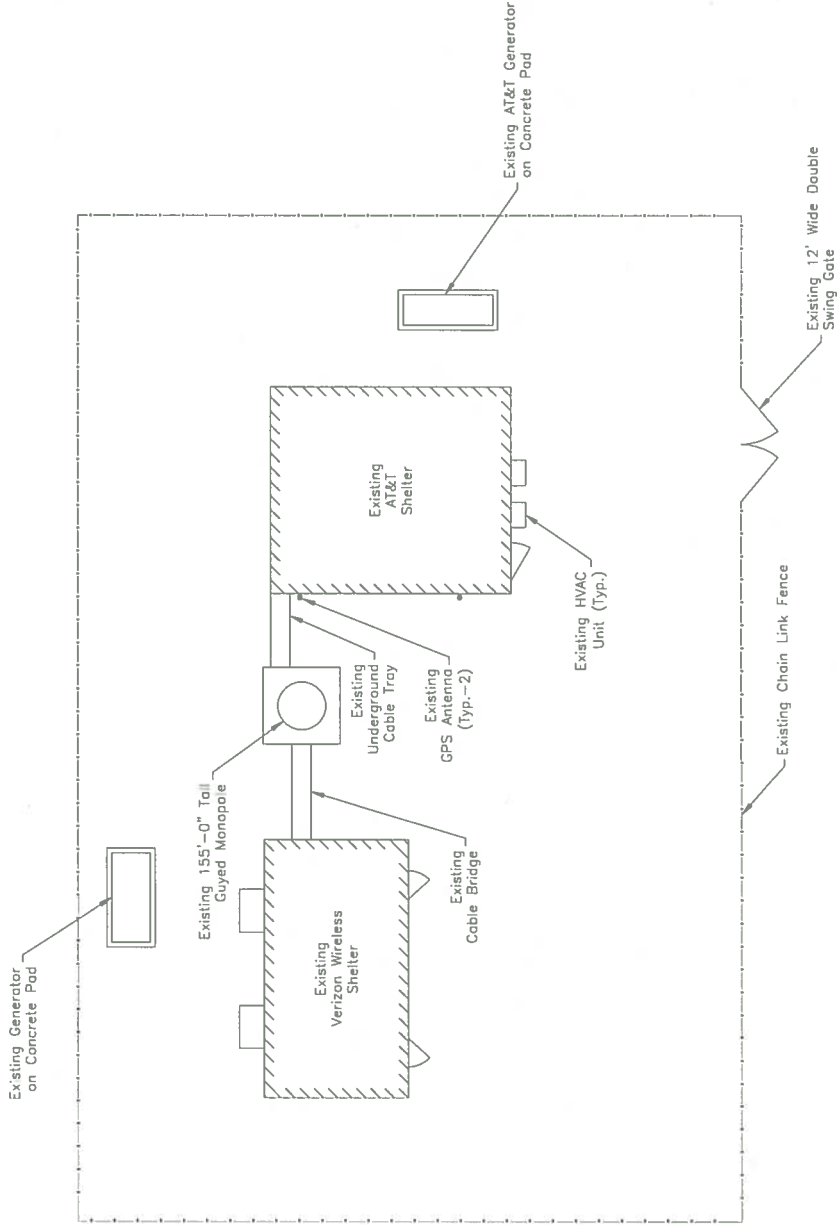
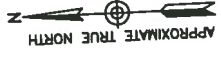
NO.	DATE	REVISIONS	DESIGNED BY:	BSH	DRAWN BY:	RSA
4	04/07/16	FINAL				
3	03/18/16	REVISED PER RF DESIGN				
2	04/27/15	REVISED PER COMMENTS				
1	03/18/15	REVISED PER COMMENTS				
0	04/29/14	ISSUED FOR CONSTRUCTION				
			BY	CHK	APP'D	

TITLE SHEET

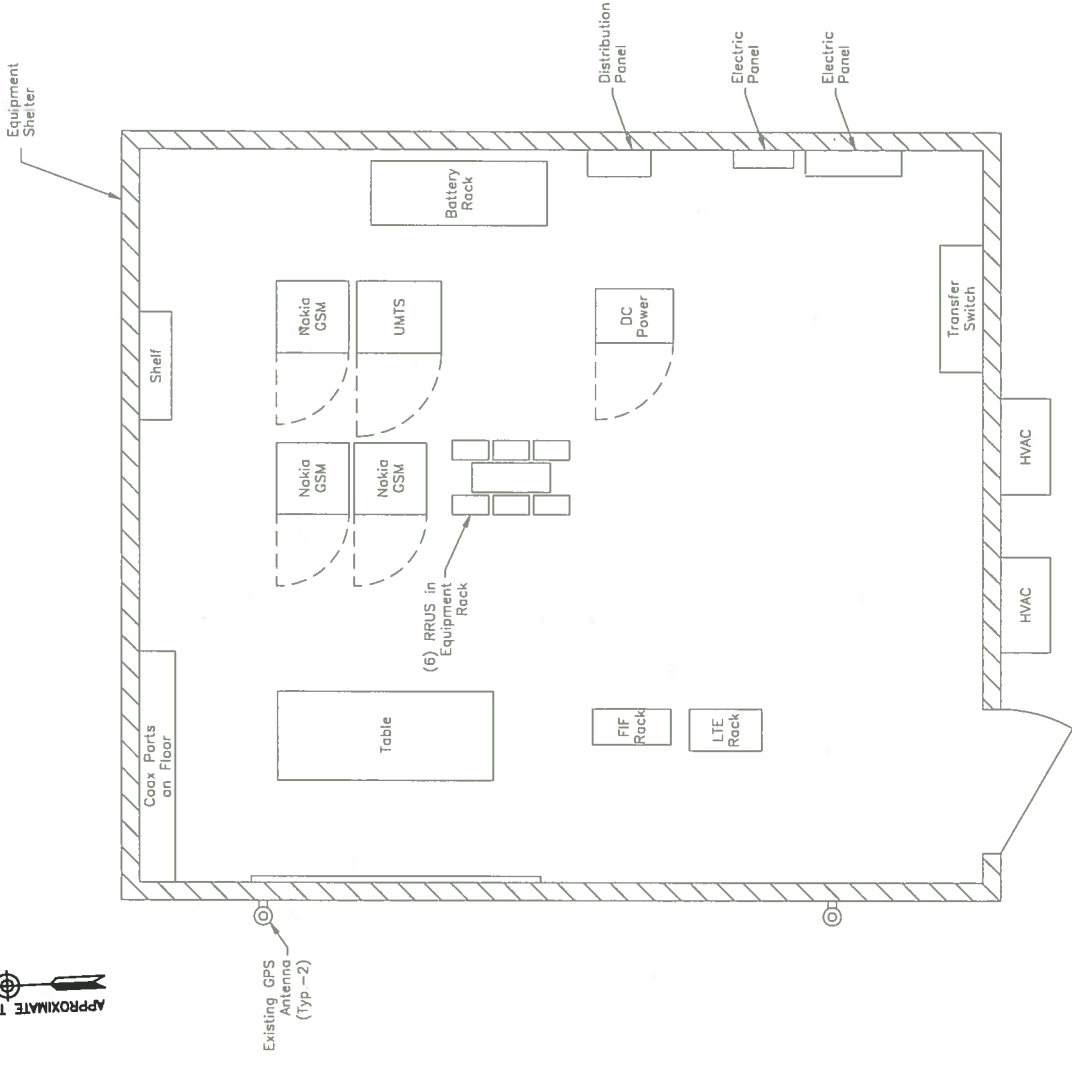
DEWBERRY NO. 50055106/50065666

DRAWING NUMBER T01

REV 4



**SITE PLAN**  
SCALE: 1"=20' FOR 11'x17'  
1"=10' FOR 22'x34'



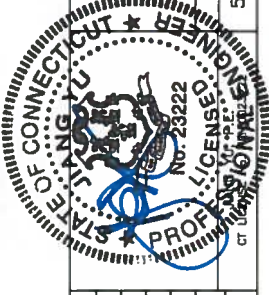
**SHELTER LAYOUT DETAIL**

SCALE: 3/16"=1' FOR 11'x17'  
3/8"=1' FOR 22'x34'



**NOTES:**

1. NORTH SHOWN AS APPROXIMATE.
2. MOUNT ALL ANTENNAS, COAX, SURGE ARRESTORS, RRU'S, ETC. IN ACCORDANCE WITH STRUCTURAL ANALYSIS BY OTHERS.
3. NOT ALL INFORMATION SHOWN FOR CLARITY.



**Dewberry**  
Dewberry Engineers, Inc.  
600 PASSIPPANY ROAD  
SUITE 301  
PASSIPPANY, NJ 07654  
PHONE: 973.739.8400  
FAX: 973.739.8710



27 NORTHWESTERN DRIVE  
SALEM, NH 03079

**WOLCOTT WEST**  
SITE NO. CT1005  
FARMDALE DRIVE  
WATERBURY, CT 06704



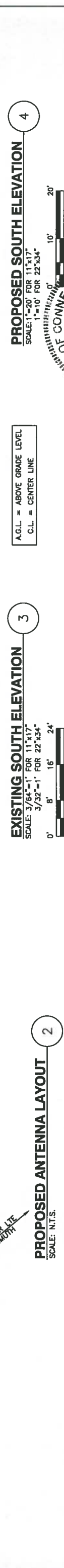
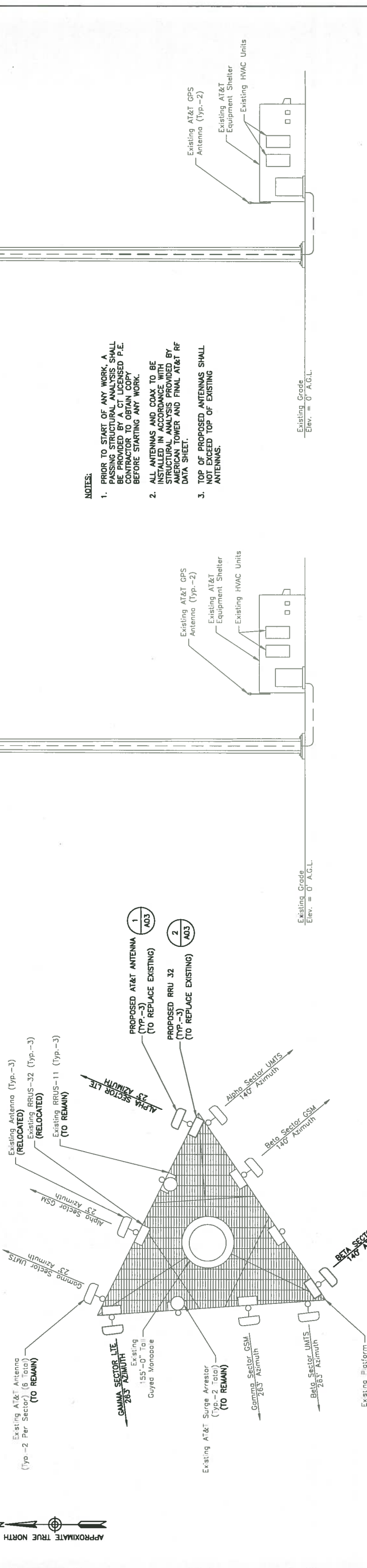
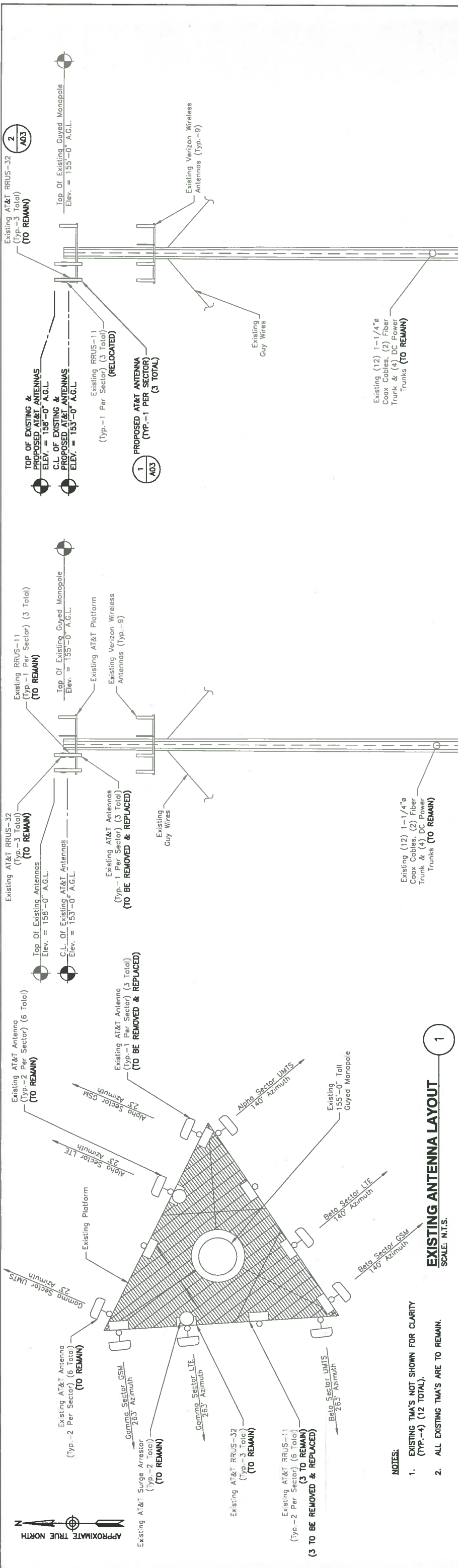
500 ENTERPRISE DRIVE,  
SUITE 3A  
ROCKY HILL, CT 06067

NO.	DATE	REVISIONS	BY	CHK	APP'D	SCALE	AS SHOWN	DESIGNED BY	BSH	DRAWN BY	RSA
4	04/07/16	FINAL									
3	03/18/16	REVISED PER RF DESIGN	RSA	MCD	GHN						
2	04/27/15	REVISED PER COMMENTS	RSA	PD	GHN						
1	03/18/15	REVISED PER COMMENTS	RSA	PD	GHN						
0	04/29/14	ISSUED FOR CONSTRUCTION	RSA	BSH	GHN						

SITE PLAN & SHELTER LAYOUT

REV	DRAWING NUMBER	REV
4	AO1	4

DEWBERRY NO. 50055106/50065666  
CT DEWBERRY ENGINEERS, INC.



**NOTES:**

- EXISTING TMA'S NOT SHOWN FOR CLARITY (TYP.-4) (12 TOTAL).
- ALL EXISTING TMA'S ARE TO REMAIN.

**NOTES:**

- PRIOR TO START OF ANY WORK, A PASSING STRUCTURAL ANALYSIS SHALL BE PROVIDED BY A CT LICENSED P.E. CONTRACTOR TO OBTAIN COPY BEFORE STARTING ANY WORK.
- ALL ANTENNAS AND COAX TO BE INSTALLED IN ACCORDANCE WITH STRUCTURAL ANALYSIS PROVIDED BY AMERICAN TOWER AND FINAL AT&T RF DATA SHEET.
- TOP OF PROPOSED ANTENNAS SHALL NOT EXCEED TOP OF EXISTING ANTENNAS.

**LEGEND:**  
 A.G.L. = ABOVE GRADE LEVEL  
 C.L. = CENTER LINE

**SCALE:** 1"=20' FOR 11"x17"  
 1"=10' FOR 22"x34"

**PROPOSED SOUTH ELEVATION 4**

**EXISTING SOUTH ELEVATION 3**

**PROPOSED ANTENNA LAYOUT 2**

**EXISTING ANTENNA LAYOUT 1**

**at&t**  
 500 ENTERPRISE DRIVE,  
 SUITE 3A  
 ROCKY HILL, CT 06067

**SAI**  
 27 NORTHWESTERN DRIVE  
 SALEM, NH 03079

**Dewberry**  
 Dewberry Engineers Inc.  
 600 PARSIPPANY ROAD  
 SUITE 301  
 PARSIPPANY, NJ 07654  
 PHONE: 973.739.9400  
 FAX: 973.739.8710

**WOLCOTT WEST  
 SITE NO. CT1005**  
 FARMDALE DRIVE  
 WATERBURY, CT 06704

NO.	DATE	REVISIONS	BY	CHK	APP'D	SCALE:	AS SHOWN	DESIGNED BY:	BSH	DRAWN BY:	RSA
4	04/07/16	FINAL	RSA	MCD	CHN						
3	03/18/16	REVISED PER RF DESIGN	RSA	MCD	CHN						
2	04/27/15	REVISED PER COMMENTS	RSA	PD	CHN						
1	03/18/15	REVISED PER COMMENTS	RSA	PD	CHN						
0	04/29/14	ISSUED FOR CONSTRUCTION	RSA	BSH	CHN						

ANTENNA LAYOUTS & ELEVATIONS

DWBERRY NO. 50055106/50065666 DRAWING NUMBER A02 REV 4

JUANG YU, P.E. PROFESSIONAL ENGINEER STATE OF CONNECTICUT LICENSE NO. 13222



**AMERICAN TOWER®**  
CORPORATION

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## Structural Analysis Report

**Structure** : 150 ft Guyed Monopole  
**ATC Site Name** : Wtbr - Waterbury, CT  
**ATC Site Number** : 302476  
**Engineering Number** : 65649522  
**Proposed Carrier** : AT&T Mobility  
**Carrier Site Name** : Waterbury  
**Carrier Site Number** : CT1005/FA#10034976  
**Site Location** : Farmdale Drive  
Waterbury, CT 06704-2833  
41.570667,-73.017600  
**County** : New Haven  
**Date** : April 12, 2016  
**Max Usage** : 80%  
**Result** : Pass

Prepared By:  
Sarah W. Frye, E.I.  
Structural Engineer I

**COA: F-6274**



## Introduction

The purpose of this report is to summarize results of a structural analysis performed on the 150 ft guyed monopole to reflect the change in loading by AT&T Mobility.

## Supporting Documents

<b>Tower Drawings</b>	SpectraSite Site #CT-0012, Rev 1, dated November 18, 2004
<b>Foundation Drawing</b>	Girard & Co. Engineers Job #38926, dated July 10, 1984

## Analysis

The tower was analyzed using tnxTower version 6.1 analysis software. This program considers an elastic three-dimensional model and second-order effects per ANSI/EIA-222.

<b>Basic Wind Speed:</b>	95 mph (3-Second Gust)
<b>Basic Wind Speed w/ Ice:</b>	50 mph (3-Second Gust) w/ 3/4" radial ice concurrent
<b>Code:</b>	ANSI/TIA-222-G / 2003 IBC w/ 2005 CT Supplement & 2009 CT Amendment
<b>Structure Class:</b>	II
<b>Exposure Category:</b>	B
<b>Topographic Category:</b>	1
<b>Crest Height:</b>	0 ft

## Conclusion

Based on the analysis results, the structure meets the requirements per the applicable codes listed above. The tower and foundation can support the equipment as described in this report.

If you have any questions or require additional information, please contact American Tower via email at [Engineering@americantower.com](mailto:Engineering@americantower.com). Please include the American Tower site name, site number, and engineering number in the subject line for any questions.



**Existing and Reserved Equipment**

Elevation <sup>1</sup> (ft)		Qty	Antenna	Mount Type	Lines	Carrier	
Mount	RAD						
154.0	154.0	6	CCI DTMABP7819VG12A	Platform w/ Handrails	(12) 1 1/4" Coax (2) 0.78" 8 AWG 6 (1) 0.39" Fiber Trunk	AT&T Mobility	
		2	Raycap DC6-48-60-18-8F				
		6	ADC DD1900				
		3	Ericsson RRUS 32				
		3	Ericsson RRUS 11 B5				
		3	Ericsson RRUS-32				
		3	Powerwave 7770.00				
		1	CCI OPA-65R-LCUU-H6				
		2	CCI OPA-65R-LCUU-H8				
129.0	129.0	6	RFS FD9R6004/2C-3L	Low Profile Platform	(15) 1 5/8" Coax (2) 1 5/8" Hybriflex	Verizon	
		3	Andrew DB948F85E-M				
		3	Antel BXA-80063-4CF-EDIN-X				
		1	Commscope LNX-4514DS-A1M				
		4	Commscope SBNHH-1D65B				
		2	Commscope LNX-6514DS-A1M				
		2	Commscope SBNHH-1D45B				
	126.0	126.0	3				Alcatel-Lucent RRH2X60-1900
			3				Alcatel-Lucent RRH2x60 700
			3				Alcatel-Lucent RRH4x45-B66 w/o Solar Shield
			1				RFS DB-T1-6Z-8AB-OZ

**Equipment to be Removed**

Elevation <sup>1</sup> (ft)		Qty	Antenna	Mount Type	Lines	Carrier
Mount	RAD					
154.0	154.0	1	CCI OPA-65R-LCUU-H8	-	-	AT&T Mobility
		2	CCI OPA-65R-LCUU-H6			
		3	Ericsson RRUS E2 B29			

**Proposed Equipment**

Elevation <sup>1</sup> (ft)		Qty	Antenna	Mount Type	Lines	Carrier
Mount	RAD					
154.0	154.0	1	Quintel QS66512-3	Platform w/ Handrails	(4) 0.78" 8 AWG 6 (1) 0.39" Fiber Trunk	AT&T Mobility
		2	CCI TPA-65R-LCUUUU-H8			

<sup>1</sup>Mount elevation is defined as height above bottom of steel structure to the bottom of mount, RAD elevation is defined as center of antenna above ground level (AGL).

Install proposed coax outside the pole shaft. Stacking is not allowed.

**Structure Usages**

Structural Component	Controlling Usage	Pass/Fail
Anchor Bolts	16%	Pass
Shaft	80%	Pass
Base Plate	10%	Pass
Flanges	52%	Pass
Guys	65%	Pass

**Foundations**

Reaction Component	Analysis Reactions
Moment (Kips-Ft)	244.8
Axial (Kips)	75.3
Shear (Kips)	5.8
Anchor Uplift (Kips)	22.3
Anchor Shear (Kips)	21.3

The structure base reactions resulting from this analysis were found to be acceptable through analysis based on geotechnical and foundation information, therefore no modification or reinforcement of the foundation will be required. Foundations include a factor of safety of 2 or greater.

**Deflection, Twist and Sway\***

Antenna Elevation (ft)	Antenna	Carrier	Deflection (in)	Sway (Rotation) (°)	Twist (°)
154.0	Quintel QS66512-3	AT&T Mobility	5.003	0.792	0.012
	CCI TPA-65R-LCUUUU-H8				

\*Deflection, Twist and Sway was evaluated considering a design wind speed of 60 mph (3-Second Gust) per ANSI/TIA-222-G.





## **Standard Conditions**

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessary limited, to:

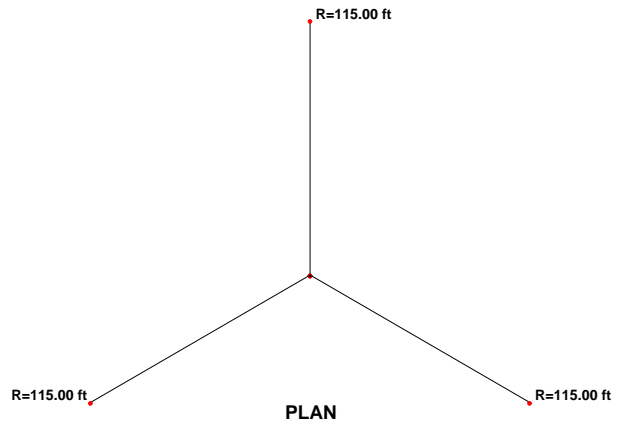
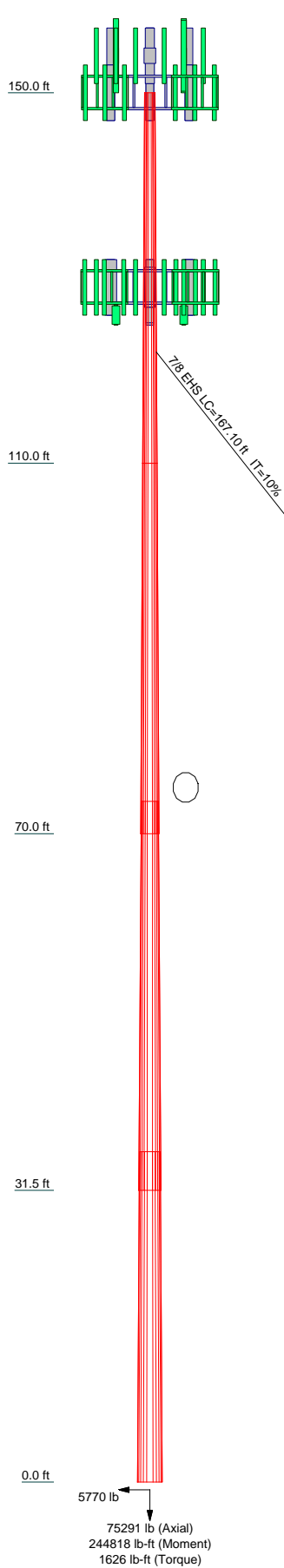
- Information supplied by the client regarding the structure itself, antenna, mounts and feed line loading on the structure and its components, or other relevant information.
- Information from drawings in the possession of American Tower Corporation, or generated by field inspections or measurements of the structure.

It is the responsibility of the client to ensure that the information provided to ATC Tower Services LLC and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and that their capacity has not significantly changed from the "as new" condition.

Unless explicitly agreed by both the client and American Tower Corporation, all services will be performed in accordance with the current revision of ANSI/TIA -222. The design basic wind speed will be determined based on the minimum basic wind speed as prescribed in ANSI/TIA-222. Although every effort is taken to ensure that the loading considered is adequate to meet the requirements of all applicable regulatory entities, we can provide no assurance to meet any other local and state codes or requirements. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement.

All services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. ATC Tower Services LLC is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

Section	1	2	3	4
Length (ft)	40.00	40.00	42.00	35.67
Number of Sides	12	12	12	12
Thickness (in)	0.1875	0.2500	0.3125	0.3750
Socket Length (ft)		3.50	4.17	
Top Dia (in)	15.0000	21.2500	26.5635	31.8255
Bot Dia (in)	21.2500	27.6100	33.1000	37.3800
Grade		A572-65		
Weight (lb)	1474.1	2649.4	4244.5	5016.1



**DESIGNED APPURTENANCE LOADING**

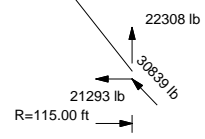
TYPE	ELEVATION	TYPE	ELEVATION
7770.00	150	Flat Platform w/ Handrails	129
7770.00	150	(2) FD9R6004/2C-3L (3.1 lbs)	129
7770.00	150	(2) FD9R6004/2C-3L (3.1 lbs)	129
DC6-48-60-18-8F	150	(2) FD9R6004/2C-3L (3.1 lbs)	129
DC6-48-60-18-8F	150	RRH2x60-1900	129
(2) DTMABP7819VG12A	150	RRH2x60-1900	129
(2) DTMABP7819VG12A	150	RRH2x60 700	129
(2) DTMABP7819VG12A	150	RRH2x60 700	129
(2) DD1900	150	RRH2x60 700	129
(2) DD1900	150	RRH2x60 700	129
(2) DD1900	150	RRH4x45-B66 w/o Solar Shield	129
RRUS-32	150	RRH4x45-B66 w/o Solar Shield	129
RRUS-32	150	RRH4x45-B66 w/o Solar Shield	129
RRUS-32	150	DB948F85E-M	129
OPA-65R-LCUU-H6	150	DB948F85E-M	129
OPA-65R-LCUU-H8 (92.7")	150	DB948F85E-M	129
OPA-65R-LCUU-H8 (92.7")	150	BXA-80063-4CF-EDIN-X	129
RRUS 32	150	BXA-80063-4CF-EDIN-X	129
RRUS 32	150	BXA-80063-4CF-EDIN-X	129
RRUS 32	150	DB-T1-6Z-8AB-0Z	129
RRUS 11 B5	150	DB-T1-6Z-8AB-0Z	129
RRUS 11 B5	150	LNx-4514DS-A1M	129
RRUS 11 B5	150	(2) SBNHH-1D45B	129
QS66512-3 (112 lbs.)	150	(2) SBNHH-1D65B	129
TPA-65R-LCUUUU-H8	150	(2) SBNHH-1D65B	129
TPA-65R-LCUUUU-H8	150	LNx-6514DS-A1M	129
Flat Platform w/ Handrails	150		

**MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

**TOWER DESIGN NOTES**

1. Tower is located in New Haven County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 95 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: 80%



ALL REACTIONS ARE FACTORED

<b>American Tower Corporation</b> 3500 Regency Parkway, Suite 100 Cary, North Carolina 27518 Phone: FAX:	Job: <b>302476 - Wtbr-Waterbury, CT</b>		
	Project: <b>65649522</b>		
	Client: AT&T Mobility	Drawn by: sarah.frye	App'd:
	Code: TIA-222-G	Date: 04/12/16	Scale: NTS
	Path: U:\TNX\Wtbr - Waterbury, CT (302476)\656495 AT&T Mobility\656495_212_tnx\302476-656495_2.dwg		Dwg No. E-1



**Centek Engineering, Inc.**  
3-2 North Branford Road  
Branford, Connecticut 06405  
Phone: (203) 488-0580  
Fax: (203) 488-8587

**Steven L. Levine**  
Real Estate Consultant

April 18, 2016

Honorable Neil M. O'Leary, Mayor  
City of Waterbury  
City Hall, 235 Grand Street  
Waterbury, CT 06702

**Notice of Exempt Modification: Existing Telecommunications Facility at Garden Circle  
(Farmdale Drive), Waterbury**

Dear Mayor O'Leary:

In order to accommodate technological changes, implement Uniform Mobile Telecommunications System ("UMTS") and Long Term Evolution ("LTE") capabilities, and enhance system performance in the State of Connecticut, New Cingular Wireless PCS, LLC ("AT&T") will be changing its equipment configuration at certain cell sites.

As required by Regulations of Connecticut State Agencies ("R.C.S.A.") Section 16-50j-73, the Connecticut Siting Council has been notified of the changes and will review AT&T's proposal. Please accept this letter as notification under Section 16-50j-73 of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2).

The enclosed Notice fully sets forth the AT&T proposal. However, if you have any questions or require any further information on the plans for the site or the Siting Council's procedures, please contact the undersigned at 860-830-0380 or Ms. Melanie Bachman, Acting Executive Director, Connecticut Siting Council at (860) 827-2935.

Sincerely,

A handwritten signature in black ink, appearing to read "S. Levine".

Steven L. Levine  
Real Estate Consultant

Enclosure



**AMERICAN TOWER®**  
CORPORATION

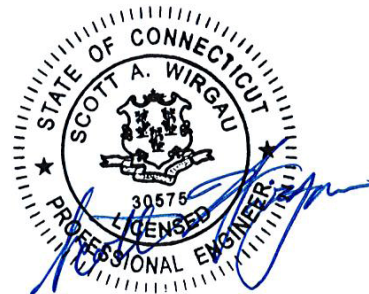
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## Structural Analysis Report

**Structure** : 150 ft Guyed Monopole  
**ATC Site Name** : Wtbr - Waterbury, CT  
**ATC Site Number** : 302476  
**Engineering Number** : 65649522  
**Proposed Carrier** : AT&T Mobility  
**Carrier Site Name** : Waterbury  
**Carrier Site Number** : CT1005/FA#10034976  
**Site Location** : Farmdale Drive  
Waterbury, CT 06704-2833  
41.570667,-73.017600  
**County** : New Haven  
**Date** : April 12, 2016  
**Max Usage** : 80%  
**Result** : Pass

Reviewed by:  
Scott Wirgau, PE  
Structural Team Leader

Prepared By:  
Sarah W. Frye, E.I.  
Structural Engineer I



Apr 14 2016 11:34 AM

COA: F-6274



**Table of Contents**

Introduction ..... 1

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Analysis ..... 1

Conclusion ..... 1

Existing and Reserved Equipment ..... 2

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Foundations ..... 3

Deflection, Twist, and Sway ..... 3

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Calculations ..... Attached



## Introduction

The purpose of this report is to summarize results of a structural analysis performed on the 150 ft guyed monopole to reflect the change in loading by AT&T Mobility.

## Supporting Documents

<b>Tower Drawings</b>	SpectraSite Site #CT-0012, Rev 1, dated November 18, 2004
<b>Foundation Drawing</b>	Girard & Co. Engineers Job #38926, dated July 10, 1984

## Analysis

The tower was analyzed using tnxTower version 6.1 analysis software. This program considers an elastic three-dimensional model and second-order effects per ANSI/EIA-222.

<b>Basic Wind Speed:</b>	95 mph (3-Second Gust)
<b>Basic Wind Speed w/ Ice:</b>	50 mph (3-Second Gust) w/ 3/4" radial ice concurrent
<b>Code:</b>	ANSI/TIA-222-G / 2003 IBC w/ 2005 CT Supplement & 2009 CT Amendment
<b>Structure Class:</b>	II
<b>Exposure Category:</b>	B
<b>Topographic Category:</b>	1
<b>Crest Height:</b>	0 ft

## Conclusion

Based on the analysis results, the structure meets the requirements per the applicable codes listed above. The tower and foundation can support the equipment as described in this report.

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		3	Ericsson RRUS-32				
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		4	Commscope SBNHH-1D65B				
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			3				Alcatel-Lucent RRH4x45-B66 w/o Solar Shield
			1				RFS DB-T1-6Z-8AB-OZ

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The structure base reactions resulting from this analysis were found to be acceptable through analysis based on geotechnical and foundation information, therefore no modification or reinforcement of the foundation will be required. Foundations include a factor of safety of 2 or greater.

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Antenna Elevation (ft)	Antenna	Carrier	Deflection (in)	Sway (Rotation) (°)	Twist (°)
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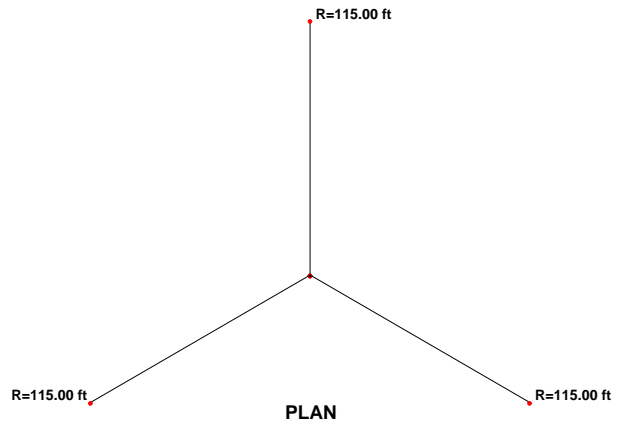
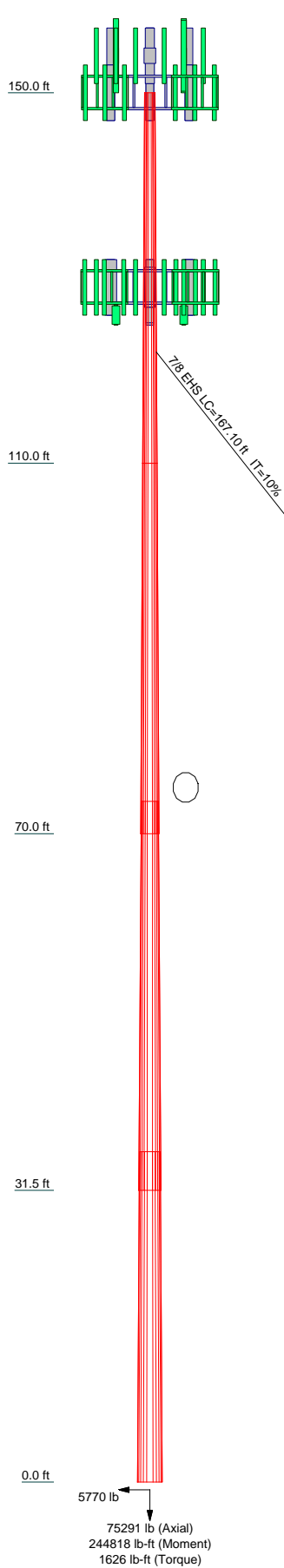
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Bot Dia (in)	21.2500	27.6100	33.1000	37.3800
Grade		A572-65		
Weight (lb)	1474.1	2649.4	4244.5	5016.1



**DESIGNED APPURTENANCE LOADING**

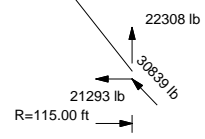
TYPE	ELEVATION	TYPE	ELEVATION
7770.00	150	Flat Platform w/ Handrails	129
7770.00	150	(2) FD9R6004/2C-3L (3.1 lbs)	129
7770.00	150	(2) FD9R6004/2C-3L (3.1 lbs)	129
DC6-48-60-18-8F	150	(2) FD9R6004/2C-3L (3.1 lbs)	129
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(2) DTMABP7819VG12A	150	RRH2x60-1900	129
(2) DTMABP7819VG12A	150	RRH2x60-1900	129
(2) DTMABP7819VG12A	150	RRH2x60 700	129
(2) DD1900	150	RRH2x60 700	129
(2) DD1900	150	RRH2x60 700	129
(2) DD1900	150	RRH4x45-B66 w/o Solar Shield	129
RRUS-32	150	RRH4x45-B66 w/o Solar Shield	129
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OPA-65R-LCUU-H8 (92.7")	150	DB948F85E-M	129
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RRUS 32	150	BXA-80063-4CF-EDIN-X	129
RRUS 32	150	BXA-80063-4CF-EDIN-X	129
RRUS 32	150	DB-T1-6Z-8AB-0Z	129
RRUS 11 B5	150	DB-T1-6Z-8AB-0Z	129
RRUS 11 B5	150	LNx-4514DS-A1M	129
RRUS 11 B5	150	(2) SBNHH-1D45B	129
QS66512-3 (112 lbs.)	150	(2) SBNHH-1D65B	129
TPA-65R-LCUUUU-H8	150	(2) SBNHH-1D65B	129
TPA-65R-LCUUUU-H8	150	LNx-6514DS-A1M	129
Flat Platform w/ Handrails	150		

**MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

**TOWER DESIGN NOTES**

1. Tower is located in New Haven County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 95 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: 80%



ALL REACTIONS ARE FACTORED

<b>American Tower Corporation</b> 3500 Regency Parkway, Suite 100 Cary, North Carolina 27518 Phone: FAX:	Job: <b>302476 - Wtbr-Waterbury, CT</b>		
	Project: <b>65649522</b>		
	Client: AT&T Mobility	Drawn by: sarah.frye	App'd:
	Code: TIA-222-G	Date: 04/12/16	Scale: NTS
	Path: U:\TNX\Wtbr - Waterbury, CT (302476)\656495 AT&T Mobility\656495_212_tmx\302476-656495_2.dwg		Dwg No. E-1

<b>tnxTower</b>  <b>American Tower Corporation</b> 3500 Regency Parkway, Suite 100 Cary, North Carolina 27518 Phone: FAX:	<b>Job</b>	302476 - Wtbr-Waterbury, CT	<b>Page</b>	1 of 22
	<b>Project</b>	65649522	<b>Date</b>	17:36:20 04/12/16
	<b>Client</b>	AT&T Mobility	<b>Designed by</b>	sarah.frye

<b>tnxTower</b>  <b>American Tower Corporation</b> 3500 Regency Parkway, Suite 100 Cary, North Carolina 27518 Phone: FAX:	<b>Job</b>	302476 - Wtbr-Waterbury, CT	<b>Page</b>	2 of 22
	<b>Project</b>	65649522	<b>Date</b>	17:36:20 04/12/16
	<b>Client</b>	AT&T Mobility	<b>Designed by</b>	sarah.frye

### Tower Input Data

There is a pole section.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in New Haven County, Connecticut.

Basic wind speed of 95 mph.

Structure Class II.

Exposure Category B.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 0.7500 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.

Safety factor used in guy design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

### Options

<ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>√ Include Bolts In Member Capacity</li> <li>Leg Bolts Are At Top Of Section</li> <li>√ Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>SR Members Have Cut Ends</li> <li>SR Members Are Concentric</li> </ul>	<ul style="list-style-type: none"> <li>Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>√ Use Clear Spans For KL/r</li> <li>√ Retension Guys To Initial Tension</li> <li>Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <li>√ Autocalc Torque Arm Areas</li> <li>Add IBC .6D+W Combination</li> <li>√ Sort Capacity Reports By Component</li> <li>Triangulate Diamond Inner Bracing</li> <li>Treat Feed Line Bundles As Cylinder</li> </ul>	<ul style="list-style-type: none"> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>√ Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>√ SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feed Line Torque</li> <li>√ Include Angle Block Shear Check</li> <li>Use TIA-222-G Bracing Resist. Exemption</li> <li>Use TIA-222-G Tension Splice Exemption</li> <li>√ Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> </ul>
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### Tapered Pole Section Geometry

Section	Elevation	Section Length	Splice Length	Number of Sides	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft		in	in	in	in	
L1	150.00-110.00	40.00	0.00	12	15.0000	21.2500	0.1875	4.0000	A572-65 (65 ksi)
L2	110.00-70.00	40.00	3.50	12	21.2500	27.6100	0.2500	4.0000	A572-65 (65 ksi)

Section	Elevation	Section Length	Splice Length	Number of Sides	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft		in	in	in	in	
L3	70.00-31.50	42.00	4.17	12	26.5535	33.1000	0.3125	4.0000	A572-65 (65 ksi)
L4	31.50-0.00	35.67		12	31.8255	37.3800	0.3750	4.0000	A572-65 (65 ksi)

### Tapered Pole Properties

Section	Tip Dia.	Area	I	r	C	I/C	J	Iv/Q	w	w/t
	in	in <sup>2</sup>	in <sup>4</sup>	in	in	in <sup>3</sup>	in <sup>2</sup>	in <sup>2</sup>	in	
L1	15.5291	8.9430	250.4541	5.3029	7.7700	32.2335	507.4880	4.4015	3.5175	18.76
	21.9996	12.7165	720.0669	7.5404	11.0075	65.4160	1459.0508	6.2587	5.1925	27.693
L2	21.9996	16.9050	951.5678	7.5180	11.0075	86.4472	1928.1342	8.3201	5.0250	20.1
	28.5840	22.0248	2104.4088	9.7949	14.3020	147.1411	4264.1028	10.8399	6.7295	26.918
L3	28.0550	26.4050	2320.7747	9.3943	13.7547	168.7258	4702.5188	12.9957	6.2788	20.092
	34.2676	32.9924	4527.0653	11.7379	17.1458	264.0335	9173.0615	16.2379	8.0333	25.707
L4	33.6200	37.9765	4794.6345	11.2593	16.4856	290.8376	9715.2293	18.6909	7.5242	20.065
	38.6986	44.6835	7810.0590	13.2478	19.3628	403.3530	15825.2970	21.9919	9.0128	24.034

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Spacing Diagonals	Double Angle Spacing Horizontals	Double Angle Spacing Redundants
ft	ft <sup>2</sup>	in					in	in	in
L1				1	1	1			
150.00-110.00									
L2				1	1	1			
110.00-70.00									
L3				1	1	1			
70.00-31.50									
L4				1	1	1			
31.50-0.00									

### Guy Data

Guy Elevation	Guy Grade	Guy Size	Initial Tension	%	Guy Modulus	Guy Weight	L <sub>o</sub>	Anchor Radius	Anchor Azimuth Adj.	Anchor Elevation	End Fitting Efficiency
ft			lb		ksi	plf	ft	ft	°	ft	%
122	EHS	A	7/8	10%	19000	1.581	166.95	115.00	0.0000	0.00	100%
		B	7/8	10%	19000	1.581	166.95	115.00	0.0000	0.00	100%
		C	7/8	10%	19000	1.581	166.95	115.00	0.0000	0.00	100%

### Guy Data(cont'd)

Guy Elevation	Mount Type	Torque-Arm Spread	Torque-Arm Leg Angle	Torque-Arm Style	Torque-Arm Grade	Torque-Arm Type	Torque-Arm Size
ft		ft	°				
122	Corner						

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### Guy Data (cont'd)

Guy Elevation ft	Diagonal Grade	Diagonal Type	Upper Diagonal Size	Lower Diagonal Size	Is Strap	Pull-Off Grade	Pull-Off Type	Pull-Off Size
122.00	A572-50 (50 ksi)	Solid Round			No	A572-50 (50 ksi)	Solid Round	1 1/4

### Guy Data (cont'd)

Guy Elevation ft	Cable Weight A lb	Cable Weight B lb	Cable Weight C lb	Cable Weight D lb	Tower Intercept A ft	Tower Intercept B ft	Tower Intercept C ft	Tower Intercept D ft
122	263.95	263.95	263.95		2.73	2.73	2.73	
					2.9 sec/pulse	2.9 sec/pulse	2.9 sec/pulse	

### Guy Data (cont'd)

Guy Elevation ft	Calc K Single Angles	Calc K Solid Rounds	Torque Arm		Pull Off		Diagonal	
			K <sub>x</sub>	K <sub>y</sub>	K <sub>x</sub>	K <sub>y</sub>	K <sub>x</sub>	K <sub>y</sub>
122	No	No			1	1	1	1

### Guy Data (cont'd)

Guy Elevation ft	Torque-Arm				Pull Off				Diagonal			
	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U
122	0.6250	0	0.0000	0.75	0.6250	0	0.0000	0.75	0.6250	0	0.0000	0.75
	A325N				A325N				A325N			

### Guy Pressures

Guy Elevation ft	Guy Location	z ft	q <sub>c</sub> psf	q <sub>i</sub> Ice psf	Ice Thickness in
122	A	61.00	19	5	1.5950
	B	61.00	19	5	1.5950
	C	61.00	19	5	1.5950

### Guy-Tensioning Information

Temperature At Time Of Tensioning																	
Guy Elevation ft	H ft	V ft	0 F		20 F		40 F		60 F		80 F		100 F		120 F		
			Initial Tension lb	Intercept ft	Initial Tension lb	Intercept ft	Initial Tension lb	Intercept ft	Initial Tension lb	Intercept ft	Initial Tension lb	Intercept ft	Initial Tension lb	Intercept ft			
122	A	114.19	122.00	9507	2.30	8992	2.43	8479	2.57	7970	2.73	7465	2.92	6966	3.12	6473	3.36
	B	114.19	122.00	9507	2.30	8992	2.43	8479	2.57	7970	2.73	7465	2.92	6966	3.12	6473	3.36
	C	114.19	122.00	9507	2.30	8992	2.43	8479	2.57	7970	2.73	7465	2.92	6966	3.12	6473	3.36

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Sector	Component Type	Placement ft	Total Number	Number Per Row	Start/End Position	Width or Diameter in	Perimeter in	Weight plf
0.78" (19.7 mm) 8 AWG 6	A	Surface Ar (CaAa)	150.00 - 7.00	2	2	-0.200 0.200	0.7800		0.59
0.39" (10mm) Fiber Trunk	A	Surface Ar (CaAa)	150.00 - 7.00	1	1	0.200 0.250	0.3900		0.07
***									
1 5/8" Coax	C	Surface Ar (CaAa)	129.00 - 7.00	15	8	-0.250 0.250	1.9800		0.82
1 5/8" Hybriflex	C	Surface Ar (CaAa)	129.00 - 7.00	2	2	0.250 0.300	1.9800		1.30
***									

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	C <sub>A</sub> A <sub>A</sub> ft <sup>2</sup>	Weight plf
1 1/4" Coax	A	No	Inside Pole	150.00 - 7.00	12	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.63
0.39" (10mm) Fiber Trunk	A	No	Inside Pole	150.00 - 7.00	1	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.07
0.78" (19.7 mm) 8 AWG 6	A	No	Inside Pole	150.00 - 7.00	4	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.59
***							
***							

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight lb
L1	150.00-110.00	A	0.000	0.000	7.800	0.000	449.60
		B	0.000	0.000	0.000	0.000	0.00

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Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight lb
L2	110.00-70.00	C	0.000	0.000	37.620	0.000	283.10
		A	0.000	0.000	7.800	0.000	449.60
		B	0.000	0.000	0.000	0.000	0.00
L3	70.00-31.50	C	0.000	0.000	79.200	0.000	596.00
		A	0.000	0.000	7.507	0.000	432.74
		B	0.000	0.000	0.000	0.000	0.00
L4	31.50-0.00	C	0.000	0.000	76.230	0.000	573.65
		A	0.000	0.000	4.777	0.000	275.38
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	48.510	0.000	365.05

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>no Ice</sub>	K <sub>Ice</sub>
L1	12	1 5/8" Hybriflex	129.00	1.0000	1.0000
			110.00 - 129.00		
L2	4	0.78" (19.7 mm) 8 AWG 6	70.00 - 110.00	1.0000	1.0000
			0.39" (10mm) Fiber Trunk		
L2	11	1 5/8" Coax	70.00 - 110.00	1.0000	1.0000
			1 5/8" Hybriflex		
L3	4	0.78" (19.7 mm) 8 AWG 6	31.50 - 70.00	1.0000	1.0000
			0.39" (10mm) Fiber Trunk		
L3	11	1 5/8" Coax	31.50 - 70.00	1.0000	1.0000
			1 5/8" Hybriflex		
L3	12	1 5/8" Hybriflex	31.50 - 70.00	1.0000	1.0000

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight lb
L1	150.00-110.00	A	1.719	0.000	0.000	40.305	0.000	880.52
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	63.357	0.000	1112.86
L2	110.00-70.00	A	1.657	0.000	0.000	39.191	0.000	855.06
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	132.146	0.000	2277.18
L3	70.00-31.50	A	1.566	0.000	0.000	37.722	0.000	822.99
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	127.190	0.000	2191.78
L4	31.50-0.00	A	1.390	0.000	0.000	22.994	0.000	501.46
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	79.816	0.000	1336.01

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horiz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>A</sub> A <sub>A</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Side ft <sup>2</sup>	Weight lb	
7770.00	A	From Centroid-Le	5.00	0.0000	150.00	No Ice	5.51	2.93	35.00
			0.00			1/2" Ice	5.86	3.26	67.63
			4.00			1" Ice	6.21	3.61	105.06
7770.00	B	From Centroid-Le	5.00	0.0000	150.00	No Ice	5.51	2.93	35.00
			0.00			1/2" Ice	5.86	3.26	67.63
			4.00			1" Ice	6.21	3.61	105.06
7770.00	C	From Centroid-Le	5.00	0.0000	150.00	No Ice	5.51	2.93	35.00
			0.00			1/2" Ice	5.86	3.26	67.63
			4.00			1" Ice	6.21	3.61	105.06
DC6-48-60-18-8F	B	From Centroid-Le	5.00	0.0000	150.00	No Ice	1.11	1.47	31.80
			0.00			1/2" Ice	1.67	1.67	49.52
			4.00			1" Ice	1.88	1.88	69.72
DC6-48-60-18-8F	C	From Centroid-Le	5.00	0.0000	150.00	No Ice	1.11	1.47	31.80
			0.00			1/2" Ice	1.67	1.67	49.52
			4.00			1" Ice	1.88	1.88	69.72
(2)DTMABP7819VG12A	A	From Centroid-Le	5.00	0.0000	150.00	No Ice	0.97	0.39	19.20
			0.00			1/2" Ice	0.00	0.49	26.49
			3.00			1" Ice	1.43	0.60	35.63
(2)DTMABP7819VG12A	B	From Centroid-Le	5.00	0.0000	150.00	No Ice	0.97	0.39	19.20
			0.00			1/2" Ice	0.00	0.49	26.49
			3.00			1" Ice	1.43	0.60	35.63
(2)DTMABP7819VG12A	C	From Centroid-Le	5.00	0.0000	150.00	No Ice	0.97	0.39	19.20
			0.00			1/2" Ice	0.00	0.49	26.49
			3.00			1" Ice	1.43	0.60	35.63
(2)DD1900	A	From Centroid-Le	5.00	0.0000	150.00	No Ice	1.09	0.30	12.10
			0.00			1/2" Ice	1.43	0.40	19.21
			3.00			1" Ice	1.59	0.51	28.18
(2)DD1900	B	From Centroid-Le	5.00	0.0000	150.00	No Ice	1.09	0.30	12.10
			0.00			1/2" Ice	1.43	0.40	19.21
			3.00			1" Ice	1.59	0.51	28.18
(2)DD1900	C	From Centroid-Le	5.00	0.0000	150.00	No Ice	1.09	0.30	12.10
			0.00			1/2" Ice	1.43	0.40	19.21
			3.00			1" Ice	1.59	0.51	28.18
RRUS-32	A	From	5.00	0.0000	150.00	No Ice	3.31	2.76	77.00

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>x</sub> in	CP <sub>z</sub> in	CP <sub>x</sub> Ice in	CP <sub>z</sub> Ice in
L1	150.00-110.00	-0.2397	0.8892	-0.4297	0.5193
L2	110.00-70.00	-0.2810	1.4875	-0.4615	1.0691
L3	70.00-31.50	-0.3075	1.6031	-0.5329	1.2113
L4	31.50-0.00	-0.2755	1.4244	-0.5171	1.1966

### Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>no Ice</sub>	K <sub>Ice</sub>
L1	4	0.78" (19.7 mm) 8 AWG 6	110.00 - 150.00	1.0000	1.0000
			110.00 - 150.00		
L1	6	0.39" (10mm) Fiber Trunk	110.00 - 150.00	1.0000	1.0000
			110.00 - 150.00		
L1	11	1 5/8" Coax	110.00 -	1.0000	1.0000



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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	C <sub>v</sub> A <sub>A</sub> Front	C <sub>v</sub> A <sub>A</sub> Side	Weight
			ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	lb
(2) SBNHH-1D45B	A	From Centroid-Le	5.00 0.00 0.00	0.0000	129.00	No Ice 1/2" Ice 1" Ice	11.40 11.87 12.35	61.70 127.29 199.37
(2) SBNHH-1D65B	B	From Centroid-Le	5.00 0.00 0.00	0.0000	129.00	No Ice 1/2" Ice 1" Ice	8.17 8.62 9.07	50.70 101.21 157.85
(2) SBNHH-1D65B	C	From Centroid-Le	5.00 0.00 0.00	0.0000	129.00	No Ice 1/2" Ice 1" Ice	8.17 8.62 9.07	50.70 101.21 157.85
LNX-6514DS-A1M	B	From Centroid-Le	5.00 0.00 0.00	0.0000	129.00	No Ice 1/2" Ice 1" Ice	8.17 8.62 9.07	38.80 89.31 145.95

\*\*\*

Section Elevation	z	K <sub>Z</sub>	q <sub>e</sub>	t <sub>Z</sub>	A <sub>G</sub>	F <sub>a</sub> c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>v</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>v</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	in	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	%	ft <sup>2</sup>	ft <sup>2</sup>
L3 70.00-31.50	50.64	0.814	5	1.5656	110.610	B C A	0.000 0.000 0.000	95.355 95.355 110.610	110.610	100.00 100.00 100.00	0.000 132.146 37.722	0.000 0.000 0.000
L4 31.50-0.00	15.38	0.7	4	1.3898	103.138	B C A B C	0.000 0.000 0.000 0.000 0.000	110.610 110.610 103.138 103.138 103.138	103.138	100.00 100.00 100.00 100.00 100.00	0.000 0.000 22.994 0.000 79.816	0.000 0.000 0.000 0.000 0.000

### Tower Pressure - Service

$G_H = 1.100$

Section Elevation	z	K <sub>Z</sub>	q <sub>e</sub>	A <sub>G</sub>	F <sub>a</sub> c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>v</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>v</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	%	ft <sup>2</sup>	ft <sup>2</sup>
L1 150.00-110.00	129.07	1.063	8	62.548	A B C	0.000 0.000 0.000	62.548 62.548 62.548	62.548	100.00 100.00 100.00	7.800 0.000 37.620	0.000 0.000 0.000
L2 110.00-70.00	89.45	0.957	7	84.306	A B C	0.000 0.000 0.000	84.306 84.306 84.306	84.306	100.00 100.00 100.00	7.800 0.000 79.200	0.000 0.000 0.000
L3 70.00-31.50	50.64	0.814	6	99.976	A B C	0.000 0.000 0.000	99.976 99.976 99.976	99.976	100.00 100.00 100.00	7.507 0.000 76.230	0.000 0.000 0.000
L4 31.50-0.00	15.38	0.7	5	94.918	A B C	0.000 0.000 0.000	94.918 94.918 94.918	94.918	100.00 100.00 100.00	4.777 0.000 48.510	0.000 0.000 0.000

### Tower Pressures - No Ice

$G_H = 1.100$

Section Elevation	z	K <sub>Z</sub>	q <sub>e</sub>	A <sub>G</sub>	F <sub>a</sub> c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>v</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>v</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	%	ft <sup>2</sup>	ft <sup>2</sup>
L1 150.00-110.00	129.07	1.063	23	62.548	A B C	0.000 0.000 0.000	62.548 62.548 62.548	62.548	100.00 100.00 100.00	7.800 0.000 37.620	0.000 0.000 0.000
L2 110.00-70.00	89.45	0.957	21	84.306	A B C	0.000 0.000 0.000	84.306 84.306 84.306	84.306	100.00 100.00 100.00	7.800 0.000 79.200	0.000 0.000 0.000
L3 70.00-31.50	50.64	0.814	18	99.976	A B C	0.000 0.000 0.000	99.976 99.976 99.976	99.976	100.00 100.00 100.00	7.507 0.000 76.230	0.000 0.000 0.000
L4 31.50-0.00	15.38	0.7	15	94.918	A B C	0.000 0.000 0.000	94.918 94.918 94.918	94.918	100.00 100.00 100.00	4.777 0.000 48.510	0.000 0.000 0.000

### Tower Pressure - With Ice

$G_H = 1.100$

Section Elevation	z	K <sub>Z</sub>	q <sub>e</sub>	t <sub>Z</sub>	A <sub>G</sub>	F <sub>a</sub> c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>v</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>v</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	in	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	%	ft <sup>2</sup>	ft <sup>2</sup>
L1 150.00-110.00	129.07	1.063	6	1.7192	74.009	A B C	0.000 0.000 0.000	74.009 74.009 74.009	74.009	100.00 100.00 100.00	40.305 0.000 63.357	0.000 0.000 0.000
L2 110.00-70.00	89.45	0.957	6	1.6573	95.355	A	0.000	95.355	95.355	100.00	39.191	0.000

### Tower Forces - No Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F <sub>a</sub> c e	e	C <sub>F</sub>	q <sub>e</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb	e			psf			ft <sup>2</sup>	lb	plf	
L1 150.00-110.00	732.70	1474.06	A B C	1 1 1	1.151 1.176 1	23	1 1 1	1 1 1	62.548 62.548 62.548	1885.07	47.13	B
L2 110.00-70.00	1045.60	2649.40	A B C	1 1 1	1.2 1.2 1	21	1 1 1	1 1 1	84.306 84.306 84.306	3017.62	75.44	A
L3 70.00-31.50	1006.39	4244.46	A B C	1 1 1	1.2 1.187 1	18	1 1 1	1 1 1	99.976 99.976 99.976	2340.81	60.80	A
L4 31.50-0.00	640.43	5016.11	A B C	1 1 1	1.083 1.026 1	15	1 1 1	1 1 1	94.918 94.918 94.918	1737.81	55.17	A
Sum Weight:	3425.12	13384.03								8981.31		

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	<b>Client</b> AT&T Mobility	<b>Designed by</b> sarah.frye

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**Tower Forces - No Ice - Wind 60 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>e</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
L1 150.00-110.00	732.70	1474.06	A B C	1 1 1	1 1.151 1.176	23	1 1 1	1 1 1	62.548 62.548 62.548	1885.07	47.13	C
L2 110.00-70.00	1045.60	2649.40	A B C	1 1 1	1 1.2 1.2	21	1 1 1	1 1 1	84.306 84.306 84.306	3017.62	75.44	B
L3 70.00-31.50	1006.39	4244.46	A B C	1 1 1	1 1.2 1.187	18	1 1 1	1 1 1	99.976 99.976 99.976	2340.81	60.80	B
L4 31.50-0.00	640.43	5016.11	A B C	1 1 1	1 1.083 1.026	15	1 1 1	1 1 1	94.918 94.918 94.918	1737.81	55.17	B
Sum Weight:	3425.12	13384.03								8981.31		

**Tower Forces - No Ice - Wind 90 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>e</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
L1 150.00-110.00	732.70	1474.06	A B C	1 1 1	1 1 1.001	23	1 1 1	1 1 1	62.548 62.548 62.548	1604.66	40.12	C
L2 110.00-70.00	1045.60	2649.40	A B C	1 1 1	1 1 1.17	21	1 1 1	1 1 1	84.306 84.306 84.306	2273.91	56.85	C
L3 70.00-31.50	1006.39	4244.46	A B C	1 1 1	1 1 1.081	18	1 1 1	1 1 1	99.976 99.976 99.976	2109.15	54.78	C
L4 31.50-0.00	640.43	5016.11	A B C	1 1 1	1 1 1	15	1 1 1	1 1 1	94.918 94.918 94.918	1604.17	50.93	C
Sum Weight:	3425.12	13384.03								7591.90		

**Tower Forces - With Ice - Wind Normal To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>e</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
L1 150.00-110.00	1993.39	3182.88	A B C	1 1 1	1.2 1.2 1.2	6	1 1 1	1 1 1	74.009 74.009 74.009	887.06	22.18	B

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>e</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
L2 110.00-70.00	3132.23	4814.95	A B C	1 1 1	1.2 1.2 1.2	6	1 1 1	1 1 1	95.355 95.355 95.355	1050.79	26.27	B
L3 70.00-31.50	3014.78	6634.54	A B C	1 1 1	1.2 1.2 1.2	5	1 1 1	1 1 1	110.610 110.610 110.610	977.94	25.40	B
L4 31.50-0.00	1837.48	7006.97	A B C	1 1 1	1.2 1.2 1.2	4	1 1 1	1 1 1	103.138 103.138 103.138	579.42	18.39	C
Sum Weight:	9977.87	21639.34								3495.20		

**Tower Forces - With Ice - Wind 60 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>e</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
L1 150.00-110.00	1993.39	3182.88	A B C	1 1 1	1.2 1.2 1.2	6	1 1 1	1 1 1	74.009 74.009 74.009	887.06	22.18	C
L2 110.00-70.00	3132.23	4814.95	A B C	1 1 1	1.2 1.2 1.2	6	1 1 1	1 1 1	95.355 95.355 95.355	1050.79	26.27	C
L3 70.00-31.50	3014.78	6634.54	A B C	1 1 1	1.2 1.2 1.2	5	1 1 1	1 1 1	110.610 110.610 110.610	977.94	25.40	C
L4 31.50-0.00	1837.48	7006.97	A B C	1 1 1	1.2 1.2 1.2	4	1 1 1	1 1 1	103.138 103.138 103.138	579.42	18.39	C
Sum Weight:	9977.87	21639.34								3495.20		

**Tower Forces - With Ice - Wind 90 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>e</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
L1 150.00-110.00	1993.39	3182.88	A B C	1 1 1	1.2 1.2 1.2	6	1 1 1	1 1 1	74.009 74.009 74.009	799.52	19.99	A
L2 110.00-70.00	3132.23	4814.95	A B C	1 1 1	1.2 1.2 1.2	6	1 1 1	1 1 1	95.355 95.355 95.355	952.69	23.82	C
L3 70.00-31.50	3014.78	6634.54	A B C	1 1 1	1.2 1.2 1.2	5	1 1 1	1 1 1	110.610 110.610 110.610	898.04	23.33	C
L4 31.50-0.00	1837.48	7006.97	A B C	1 1 1	1.2 1.2 1.2	4	1 1 1	1 1 1	103.138 103.138 103.138	579.42	18.39	C



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Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>c</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
Sum Weight:	9977.87	21639.34								3229.68		

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>c</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
L1 150.00-110.00	732.70	1474.06	A	1	1	8	1	1	62.548	572.71	14.32	C
			B	1	1		1	1	62.548			
			C	1	1.001		1	1	62.548			
L2 110.00-70.00	1045.60	2649.40	A	1	1	7	1	1	84.306	811.57	20.29	C
			B	1	1		1	1	84.306			
			C	1	1.17		1	1	84.306			
L3 70.00-31.50	1006.39	4244.46	A	1	1	6	1	1	99.976	752.76	19.55	C
			B	1	1.187		1	1	99.976			
			C	1	1		1	1	99.976			
L4 31.50-0.00	640.43	5016.11	A	1	1.083	5	1	1	94.918	572.53	18.18	C
			B	1	1.026		1	1	94.918			
			C	1	1		1	1	94.918			
Sum Weight:	3425.12	13384.03								2709.57		

**Tower Forces - Service - Wind Normal To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>c</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
L1 150.00-110.00	732.70	1474.06	A	1	1.151	8	1	1	62.548	672.79	16.82	B
			B	1	1.176		1	1	62.548			
			C	1	1		1	1	62.548			
L2 110.00-70.00	1045.60	2649.40	A	1	1.2	7	1	1	84.306	1077.00	26.92	A
			B	1	1.2		1	1	84.306			
			C	1	1		1	1	84.306			
L3 70.00-31.50	1006.39	4244.46	A	1	1.2	6	1	1	99.976	835.44	21.70	A
			B	1	1.187		1	1	99.976			
			C	1	1		1	1	99.976			
L4 31.50-0.00	640.43	5016.11	A	1	1.083	5	1	1	94.918	620.23	19.69	A
			B	1	1.026		1	1	94.918			
			C	1	1		1	1	94.918			
Sum Weight:	3425.12	13384.03								3205.46		

**Force Totals (Does not include forces on guys)**

Load Case	Vertical Forces	Sum of Forces X	Sum of Forces Z	Sum of Torques
	lb	lb	lb	lb-ft
Leg Weight	13384.03			
Bracing Weight	0.00			
Total Member Self-Weight	13384.03			
Guy Weight	791.86			
Total Weight	24063.41			
Wind 0 deg - No Ice		-23.06	-13331.51	450.45
Wind 30 deg - No Ice		6629.75	-11533.89	733.56
Wind 60 deg - No Ice		12438.11	-7183.86	820.12
Wind 90 deg - No Ice		13789.02	23.06	686.92
Wind 120 deg - No Ice		13122.41	7605.57	1011.87
Wind 150 deg - No Ice		6669.70	11556.96	-46.64
Wind 180 deg - No Ice		23.06	13331.51	-450.45
Wind 210 deg - No Ice		-6629.75	11533.89	-733.56
Wind 240 deg - No Ice		-12438.11	7183.86	-820.12
Wind 270 deg - No Ice		-13789.02	-23.06	-686.92
Wind 300 deg - No Ice		-13122.41	-7605.57	-1011.87
Wind 330 deg - No Ice		-6669.70	-11556.96	46.64
Member Ice				
Guy Ice	8255.31			
Total Weight Ice	2410.85			
Total Weight	51242.82			
Wind 0 deg - Ice		-6.38	-5003.74	160.93
Wind 30 deg - Ice		2675.98	-4647.90	263.02
Wind 60 deg - Ice		5048.29	-2914.75	294.63
Wind 90 deg - Ice		5398.58	6.38	247.30
Wind 120 deg - Ice		4931.38	2854.62	292.05
Wind 150 deg - Ice		2503.58	4336.55	-15.72
Wind 180 deg - Ice		6.38	5003.74	-160.93
Wind 210 deg - Ice		-2675.98	4647.90	-263.02
Wind 240 deg - Ice		-5048.29	2914.75	-294.63
Wind 270 deg - Ice		-5398.58	-6.38	-247.30
Wind 300 deg - Ice		-4931.38	-2854.62	-292.05
Wind 330 deg - Ice		-2503.58	-4336.55	15.72
Total Weight	24063.41			
Wind 0 deg - Service		-8.23	-4758.06	160.77

**Tower Forces - Service - Wind 60 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	q <sub>c</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	plf	
L1 150.00-110.00	732.70	1474.06	A	1	1	8	1	1	62.548	672.79	16.82	C
			B	1	1.151		1	1	62.548			
			C	1	1.176		1	1	62.548			
L2 110.00-70.00	1045.60	2649.40	A	1	1	7	1	1	84.306	1077.00	26.92	B
			B	1	1.2		1	1	84.306			
			C	1	1.2		1	1	84.306			
L3 70.00-31.50	1006.39	4244.46	A	1	1	6	1	1	99.976	835.44	21.70	B
			B	1	1.2		1	1	99.976			
			C	1	1.187		1	1	99.976			
L4 31.50-0.00	640.43	5016.11	A	1	1	5	1	1	94.918	620.23	19.69	B
			B	1	1.083		1	1	94.918			
			C	1	1.026		1	1	94.918			
Sum Weight:	3425.12	13384.03								3205.46		

**Tower Forces - Service - Wind 90 To Face**

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Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Torques lb-ft
Wind 30 deg - Service		2366.18	-4116.48	261.81
Wind 60 deg - Service		4439.20	-2563.94	292.70
Wind 90 deg - Service		4921.35	8.23	245.17
Wind 120 deg - Service		4683.43	2714.45	131.94
Wind 150 deg - Service		2380.44	4124.72	-16.65
Wind 180 deg - Service		8.23	4758.06	-160.77
Wind 210 deg - Service		-2366.18	4116.48	-261.81
Wind 240 deg - Service		-4439.20	2563.94	-292.70
Wind 270 deg - Service		-4921.35	-8.23	-245.17
Wind 300 deg - Service		-4683.43	-2714.45	-131.94
Wind 330 deg - Service		-2380.44	-4124.72	16.65

### Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy
3	1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy
4	1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy
5	1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy
6	1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy
7	1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy
8	1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy
9	1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy
10	1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy
11	1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy
12	1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy
13	1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy
14	1.2 Dead+1.0 Ice+1.0 Temp+Guy
15	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy
16	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy
17	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy
18	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy
19	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy
20	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy
21	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy
22	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy
23	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy
24	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy
25	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy
26	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy
27	Dead+Wind 0 deg - Service+Guy
28	Dead+Wind 30 deg - Service+Guy
29	Dead+Wind 60 deg - Service+Guy
30	Dead+Wind 90 deg - Service+Guy
31	Dead+Wind 120 deg - Service+Guy
32	Dead+Wind 150 deg - Service+Guy
33	Dead+Wind 180 deg - Service+Guy
34	Dead+Wind 210 deg - Service+Guy
35	Dead+Wind 240 deg - Service+Guy
36	Dead+Wind 270 deg - Service+Guy
37	Dead+Wind 300 deg - Service+Guy
38	Dead+Wind 330 deg - Service+Guy

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment lb-ft	Minor Axis Moment lb-ft
L1	150 - 110	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	6	-51355.66	-132300.42	-75450.64
			Max. Mx	5	-9106.88	-220946.76	-1307.64
			Max. My	2	-9070.54	77.09	218044.68
			Max. Vy	5	11980.96	-220946.76	-1307.64
			Max. Vx	2	-12057.76	77.09	218044.68
			Max. Torque	4			-1318.15
			Bottom Tension	7	30401.83		
			Top Tension	7	30592.71		
			Top Cable Vert	7	22425.97		
		Top Cable Norm	7	20808.40			
		Top Cable Tan	7	8.95			
		Bot Cable Vert	7	-21993.38			
		Bot Cable Norm	7	20988.58			
		Bot Cable Tan	7	204.11			
		Bottom Tension	12	30838.56			
		Top Tension	12	31030.09			
		Top Cable Vert	12	22747.90			
		Top Cable Norm	12	21104.49			
		Top Cable Tan	12	0.01			
L2	110 - 70	Pole	Bot Cable Vert	12	-22307.58		
			Bot Cable Norm	12	21292.92		
			Bot Cable Tan	12	0.01		
			Bottom Tension	5	30786.22		
			Top Tension	5	30977.07		
			Top Cable Vert	5	22704.87		
			Top Cable Norm	5	21072.92		
			Top Cable Tan	5	13.18		
			Bot Cable Vert	5	-22272.27		
			Bot Cable Norm	5	21253.09		
Bot Cable Tan	5	208.34					
L3	70 - 31.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	6	-55268.52	-43035.92	-24620.42
			Max. Mx	5	-45304.61	-153640.34	-5439.93
			Max. My	2	-48476.77	53.96	159297.96
			Max. Vy	12	4673.72	120516.95	68357.20
			Max. Vx	8	-4359.79	-465.54	-147891.34
			Max. Torque	12			1529.68
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	23	-63889.39	9360.73	-5190.70
			Max. Mx	6	-61284.96	-78071.05	-45853.04
Max. My	2	-58440.54	100.14	63408.68			
Max. Vy	6	2462.83	-78071.05	-45853.04			
Max. Vx	8	-1651.48	-460.94	-24036.21			
Max. Torque	12			1626.35			
L4	31.5 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	23	-75291.45	37883.44	-20784.46
			Max. Mx	6	-68770.39	-211324.35	-123602.71
			Max. My	2	-65919.04	98.39	164753.84
			Max. Vy	6	5005.00	-211324.35	-123602.71
			Max. Vx	2	-4244.86	98.39	164753.84
Max. Torque	12			1626.35			

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### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal, X lb	Horizontal, Z lb	
Mast	Max. Vert	23	75291.45	1049.30	-530.21	
	Max. H <sub>x</sub>	12	55061.69	4769.40	2799.67	
	Max. H <sub>y</sub>	2	65919.04	-3.62	4244.86	
	Max. M <sub>x</sub>	2	164753.84	-3.62	4244.86	
	Max. M <sub>y</sub>	6	211324.38	-4997.36	-2884.03	
	Max. Torsion	12	1626.34	4769.40	2799.67	
	Min. Vert	1	41333.94	-0.51	19.27	
	Min. H <sub>x</sub>	6	68771.14	-4997.36	-2884.03	
	Min. H <sub>y</sub>	8	53994.38	-1.31	-3955.05	
	Min. M <sub>x</sub>	6	-123602.66	-4997.36	-2884.03	
	Min. M <sub>y</sub>	10	-177700.46	4353.73	-2516.38	
	Min. Torsion	6	-1579.99	-4997.36	-2884.03	
	Guy C @ 115 ft Elev 0 ft Azimuth 240 deg	Max. Vert	10	-158.94	-86.73	50.07
	Guy B @ 115 ft Elev 0 ft Azimuth 120 deg	Max. H <sub>x</sub>	10	-158.94	-86.73	50.07
Max. H <sub>y</sub>		3	-21866.87	-17971.44	10609.72	
Min. Vert		5	-22272.27	-18509.89	10446.12	
Min. H <sub>x</sub>		5	-22272.27	-18509.89	10446.12	
Min. H <sub>y</sub>		10	-158.94	-86.73	50.07	
Guy A @ 115 ft Elev 0 ft Azimuth 0 deg	Max. Vert	6	-154.57	83.28	48.08	
	Max. H <sub>x</sub>	11	-22276.88	18513.34	10448.85	
	Max. H <sub>y</sub>	13	-21948.41	18038.00	10649.03	
	Min. Vert	12	-22307.58	18440.20	10646.47	
	Min. H <sub>x</sub>	6	-154.57	83.28	48.08	
Guy A @ 115 ft Elev 0 ft Azimuth 0 deg	Min. H <sub>y</sub>	6	-154.57	83.28	48.08	
	Max. Vert	2	-166.87	0.00	-107.39	
	Max. H <sub>x</sub>	10	-19373.11	341.18	-18454.17	
	Max. H <sub>y</sub>	2	-166.87	0.00	-107.39	
	Min. Vert	7	-21993.38	-204.11	-20988.58	
Guy A @ 115 ft Elev 0 ft Azimuth 0 deg	Min. H <sub>x</sub>	6	-19949.52	-351.57	-19000.00	
	Min. H <sub>y</sub>	7	-21993.38	-204.11	-20988.58	

### Tower Mast Reaction Summary

Load Combination	Vertical lb	Shear <sub>x</sub> lb	Shear <sub>y</sub> lb	Overtuning Moment, M <sub>x</sub> lb-ft	Overtuning Moment, M <sub>y</sub> lb-ft	Torque lb-ft
Dead Only	41333.94	0.51	-19.27	-32.74	149.50	-0.00
1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy	65919.04	3.62	-4244.86	-164753.84	98.39	704.29
1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy	62111.93	1897.57	-3692.45	-139228.14	-42344.41	1220.92
1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy	54619.16	4136.87	-2432.73	-71498.01	-122129.20	1310.14
1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy	62749.44	4574.51	151.92	32642.74	-164838.16	1030.08
1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy	68771.14	4997.36	2884.03	123602.66	-211324.38	1579.99
1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy	62289.58	2193.28	3470.35	107830.59	-97326.14	-41.15

Load Combination	Vertical lb	Shear <sub>x</sub> lb	Shear <sub>y</sub> lb	Overtuning Moment, M <sub>x</sub> lb-ft	Overtuning Moment, M <sub>y</sub> lb-ft	Torque lb-ft
No Ice+1.0 Guy						
1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy	53994.38	1.31	3955.05	105764.31	-330.57	-705.43
1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy	62140.04	-2195.10	3472.94	107674.88	97303.68	-1178.05
1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy	67671.99	-4353.73	2516.38	104046.53	177700.46	-1263.43
1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy	62675.32	-4572.89	156.94	32620.10	164994.28	-1031.90
1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy	55061.69	-4769.40	-2799.67	-89884.29	153227.35	-1626.34
1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy	62187.52	-1891.11	-3690.66	-139448.62	42567.56	-0.17
1.2 Dead+1.0 Ice+1.0 Temp+Guy	73959.30	2.17	-80.76	-658.64	1000.61	0.40
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy	74956.10	2.96	-931.76	-23997.54	1036.72	154.47
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy	74914.61	466.65	-894.16	-25974.74	-13136.21	296.66
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy	74864.54	1047.52	-689.22	-21218.30	-34232.18	306.10
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy	74900.11	1110.66	-81.98	-653.71	-34338.84	232.43
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy	75219.89	1033.62	517.76	19942.33	-34345.56	308.14
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy	74861.38	421.09	653.15	19168.48	-10052.63	27.95
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy	74753.88	2.06	767.72	22222.42	1030.81	-153.68
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy	74976.69	-463.32	730.24	24434.70	15588.99	-294.10
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy	75291.45	-1049.30	530.21	20784.46	37883.44	-303.79
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy	74901.16	-1105.67	-81.06	-656.95	36410.36	-231.74
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy	74831.02	-1023.38	-677.69	-20564.16	35154.33	-308.81
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy	74807.24	-417.66	-815.27	-20370.93	12379.50	-28.88
Dead+Wind 0 deg - Service+Guy	41439.80	0.99	-902.36	-20892.41	147.56	159.16
Dead+Wind 30 deg - Service+Guy	41423.56	437.74	-784.25	-18078.73	-10028.71	269.15
Dead+Wind 60 deg - Service+Guy	41425.37	918.98	-555.50	-14633.75	-24525.72	291.93
Dead+Wind 90 deg - Service+Guy	41429.14	979.96	-20.77	-137.15	-25261.34	235.93
Dead+Wind 120 deg - Service+Guy	41467.95	1059.96	597.04	18406.72	-31251.56	131.32
Dead+Wind 150 deg - Service+Guy	41425.82	435.61	745.14	18055.36	-9862.56	-7.93
Dead+Wind 180 deg - Service+Guy	41417.88	-0.14	863.97	20884.45	168.54	-159.05
Dead+Wind 210 deg - Service+Guy	41425.11	-435.74	745.71	18066.00	10196.71	-267.58
Dead+Wind 240 deg - Service+Guy	41456.27	-917.73	516.08	14518.89	24812.70	-290.46
Dead+Wind 270 deg - Service+Guy	41429.12	-979.11	-19.64	-116.25	25578.65	-236.02
Dead+Wind 300 deg - Service+Guy	41432.32	-1059.29	-636.35	-18503.67	31565.69	-132.80

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Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>y</sub>	Overtuning Moment, M <sub>x</sub>	Overtuning Moment, M <sub>y</sub>	Torque
	lb	lb	lb	lb-ft	lb-ft	lb-ft
Dead+Wind 330 deg - Service+Guy	41424.28	-435.91	-783.69	-18069.24	10327.14	6.49

### Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX lb	PY lb	PZ lb	PX lb	PY lb	PZ lb	
1	0.00	-24063.39	0.00	0.01	24063.31	0.03	0.000%
2	-36.90	-28768.37	-22322.74	36.90	28768.32	22321.71	0.003%
3	11103.32	-28717.70	-19312.85	-11103.30	28717.67	19312.14	0.002%
4	20760.37	-28667.04	-11990.34	-20760.18	28667.03	11990.39	0.000%
5	23053.89	-28717.71	36.90	-23053.25	28717.67	-36.57	0.002%
6	21855.23	-28768.37	12665.08	-21854.23	28768.30	-12664.50	0.003%
7	11167.24	-28717.71	19349.75	-11166.64	28717.67	-19349.38	0.002%
8	36.90	-28667.04	22322.74	-36.80	28667.03	-22322.62	0.000%
9	-11103.32	-28717.71	19312.85	11102.73	28717.67	-19312.48	0.002%
10	-20760.37	-28768.37	11990.34	20759.40	28768.31	-11989.79	0.003%
11	-23053.89	-28717.70	-36.90	23053.25	28717.67	37.24	0.002%
12	-21855.23	-28667.04	-12665.08	21855.11	28667.03	12665.01	0.000%
13	-11167.24	-28717.70	-19349.75	11167.22	28717.67	19349.05	0.002%
14	0.00	-56377.70	0.00	0.05	56377.70	0.23	0.000%
15	-6.38	-56418.46	-5801.90	6.38	56418.45	5801.44	0.001%
16	3074.71	-56377.70	-5338.52	-3074.68	56377.70	5338.16	0.001%
17	5739.52	-56336.95	-3313.84	-5738.66	56336.93	3313.47	0.002%
18	6196.04	-56377.70	6.38	-6195.71	56377.70	-6.21	0.001%
19	5622.61	-56418.46	3253.70	-5622.08	56418.44	-3253.39	0.001%
20	2902.31	-56377.70	5027.17	-2902.03	56377.70	-5026.97	0.001%
21	6.38	-56336.95	5801.90	-6.36	56336.92	-5800.95	0.002%
22	-3074.71	-56377.70	5338.52	3074.38	56377.69	-5338.30	0.001%
23	-5739.52	-56418.46	3313.84	5738.96	56418.44	-3313.51	0.001%
24	-6196.04	-56377.70	-6.38	6195.71	56377.70	6.54	0.001%
25	-5622.61	-56336.95	-3253.70	5621.78	56336.93	3253.33	0.002%
26	-2902.31	-56377.70	-5027.17	2902.28	56377.70	5026.86	0.001%
27	-8.23	-24074.70	-4979.41	8.23	24074.69	4979.32	0.000%
28	2476.76	-24063.39	-4308.01	-2476.75	24063.39	4307.95	0.000%
29	4630.90	-24052.09	-2674.62	-4630.86	24052.09	2674.60	0.000%
30	5142.51	-24063.39	8.23	-5142.43	24063.39	-8.21	0.000%
31	4875.13	-24074.70	2825.13	-4875.02	24074.69	-2825.07	0.001%
32	2491.02	-24063.39	4316.24	-2490.96	24063.39	-4316.20	0.000%
33	8.23	-24052.09	4979.41	-8.23	24052.09	-4979.37	0.000%
34	-2476.76	-24063.39	4308.01	2476.71	24063.39	-4307.97	0.000%
35	-4630.90	-24074.70	2674.62	4630.80	24074.69	-2674.56	0.000%
36	-5142.51	-24063.39	-8.23	5142.43	24063.39	8.26	0.000%
37	-4875.13	-24052.09	-2825.13	4875.08	24052.09	2825.10	0.000%
38	-2491.02	-24063.39	-4316.24	2491.00	24063.39	4316.18	0.000%

3	Yes	7	0.00000001	0.00035143
4	Yes	6	0.00000001	0.00025191
5	Yes	7	0.00000001	0.00024677
6	Yes	7	0.00010497	0.00049049
7	Yes	7	0.00000001	0.00029492
8	Yes	6	0.00000001	0.00012316
9	Yes	7	0.00000001	0.00033033
10	Yes	7	0.00000001	0.00051231
11	Yes	7	0.00000001	0.00024438
12	Yes	6	0.00000001	0.00024495
13	Yes	7	0.00000001	0.00026720
14	Yes	4	0.00000001	0.00005920
15	Yes	6	0.00000001	0.00009244
16	Yes	6	0.00000001	0.00009240
17	Yes	5	0.00077524	0.00036737
18	Yes	6	0.00000001	0.00008623
19	Yes	6	0.00000001	0.00012513
20	Yes	6	0.00000001	0.00009163
21	Yes	5	0.00083867	0.00037857
22	Yes	6	0.00000001	0.00009811
23	Yes	6	0.00000001	0.00013336
24	Yes	6	0.00000001	0.00008397
25	Yes	5	0.00076779	0.00034409
26	Yes	6	0.00000001	0.00008183
27	Yes	5	0.00000001	0.00006884
28	Yes	5	0.00000001	0.00008628
29	Yes	5	0.00000001	0.00007544
30	Yes	5	0.00000001	0.00007858
31	Yes	5	0.00000001	0.00007267
32	Yes	5	0.00000001	0.00005479
33	Yes	5	0.00000001	0.00006138
34	Yes	5	0.00000001	0.00007397
35	Yes	5	0.00000001	0.00010017
36	Yes	5	0.00000001	0.00007792
37	Yes	5	0.00000001	0.00005119
38	Yes	5	0.00000001	0.00005532

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	150 - 110	5.003	35	0.7924	0.0119
L2	110 - 70	0.803	31	0.1573	0.0046
L3	73.5 - 31.5	0.366	37	0.0285	0.0018
L4	35.667 - 0	0.132	37	0.0285	0.0006

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
150.00	7770.00	35	5.003	0.7924	0.0119	24743
129.00	Flat Platform w/ Handrails	31	2.393	0.4121	0.0077	5891
122.00	Guy	31	1.689	0.3059	0.0064	4418

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00017263
2	Yes	7	0.00000001	0.00026465

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### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	150 - 110	32.565	6	4.1475	0.0582
L2	110 - 70	8.966	6	1.1956	0.0208
L3	73.5 - 31.5	3.734	6	0.4300	0.0097
L4	35.667 - 0	1.025	6	0.2435	0.0031

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
150.00	7770.00	6	32.565	4.1475	0.0582	5227
129.00	Flat Platform w/ Handrails	6	18.348	2.3990	0.0345	1243
122.00	Guy	6	14.330	1.8946	0.0289	931

### Guy Design Data

Section No.	Elevation ft	Size	Initial Tension lb	Breaking Load lb	Actual T <sub>u</sub> lb	Allowable φT <sub>u</sub> lb	Required S.F.	Actual S.F.
L1	122.00 (A) (7)	7/8 EHS	7970.00	79699.84	30592.70	47820.00	1.000	1.563
	122.00 (B) (6)	7/8 EHS	7970.00	79699.84	31030.10	47820.00	1.000	1.541
	122.00 (C) (5)	7/8 EHS	7970.00	79699.84	30977.10	47820.00	1.000	1.544

### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L	L <sub>u</sub>	KU/r	A	P <sub>u</sub>	φP <sub>u</sub>	Ratio P <sub>u</sub> φP <sub>u</sub>
L1	150 - 110 (1)	TP21.25x15x0.1875	40.00	28.00	48.9	11.5845	-50657.70	615724.00	0.082
L2	110 - 70 (2)	TP27.61x21.25x0.25	40.00	122.00	194.7	16.9050	-50335.40	100711.00	0.500
L3	70 - 31.5 (3)	TP33.1x26.5535x0.3125	42.00	122.00	152.7	26.9540	-55106.50	261264.00	0.211
L4	31.5 - 0 (4)	TP37.38x31.8255x0.375	35.67	122.00	110.5	44.6835	-68770.40	826594.00	0.083

### Pole Bending Design Data

Section No.	Elevation ft	Size	M <sub>ux</sub>	φM <sub>ux</sub>	Ratio	M <sub>uy</sub>	φM <sub>uy</sub>	Ratio
			lb-ft	lb-ft	$\frac{M_{ux}}{\phi M_{ux}}$	lb-ft	lb-ft	$\frac{M_{uy}}{\phi M_{uy}}$
L1	150 - 110 (1)	TP21.25x15x0.1875	208078.33	315006.67	0.661	0.00	315006.67	0.000
L2	110 - 70 (2)	TP27.61x21.25x0.25	159306.67	531001.67	0.300	0.00	531001.67	0.000
L3	70 - 31.5 (3)	TP33.1x26.5535x0.3125	54238.58	1080200.00	0.050	0.00	1080200.00	0.000
L4	31.5 - 0 (4)	TP37.38x31.8255x0.375	244817.50	2374800.00	0.103	0.00	2374800.00	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V <sub>v</sub>	φV <sub>v</sub>	Ratio	Actual T <sub>u</sub>	φT <sub>u</sub>	Ratio
			lb	lb	$\frac{V_v}{\phi V_v}$	lb-ft	lb-ft	$\frac{T_u}{\phi T_u}$
L1	150 - 110 (1)	TP21.25x15x0.1875	4749.97	403664.00	0.012	554.96	638735.00	0.001
L2	110 - 70 (2)	TP27.61x21.25x0.25	4030.33	623034.00	0.006	1264.23	1076708.33	0.001
L3	70 - 31.5 (3)	TP33.1x26.5535x0.3125	959.34	993388.00	0.001	1263.48	2190300.00	0.001
L4	31.5 - 0 (4)	TP37.38x31.8255x0.375	5778.71	1578480.00	0.004	1579.98	4815341.67	0.000

### Pole Interaction Design Data

Section No.	Elevation ft	Ratio P <sub>u</sub>	Ratio M <sub>ux</sub>	Ratio M <sub>uy</sub>	Ratio V <sub>v</sub>	Ratio T <sub>u</sub>	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
		$\frac{P_u}{\phi P_u}$	$\frac{M_{ux}}{\phi M_{ux}}$	$\frac{M_{uy}}{\phi M_{uy}}$	$\frac{V_v}{\phi V_v}$	$\frac{T_u}{\phi T_u}$			
L1	150 - 110 (1)	0.082	0.661	0.000	0.012	0.001	0.743	1.000	4.8.2
L2	110 - 70 (2)	0.500	0.300	0.000	0.006	0.001	0.800	1.000	4.8.2
L3	70 - 31.5 (3)	0.211	0.050	0.000	0.001	0.001	0.261	1.000	4.8.2
L4	31.5 - 0 (4)	0.083	0.103	0.000	0.004	0.000	0.186	1.000	4.8.2

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	φP <sub>allow</sub> lb	% Capacity	Pass Fail	
L1	150 - 110	Pole	TP21.25x15x0.1875	1	-50657.70	615724.00	74.3	Pass	
L2	110 - 70	Pole	TP27.61x21.25x0.25	2	-50335.40	100711.00	80.0	Pass	
L3	70 - 31.5	Pole	TP33.1x26.5535x0.3125	3	-55106.50	261264.00	26.1	Pass	
L4	31.5 - 0	Pole	TP37.38x31.8255x0.375	4	-68770.40	826594.00	18.6	Pass	
L1	150 - 110	Guy A@122	7/8	7	30592.70	47820.00	64.0	Pass	
L1	150 - 110	Guy B@122	7/8	6	31030.10	47820.00	64.9	Pass	
L1	150 - 110	Guy C@122	7/8	5	30977.10	47820.00	64.8	Pass	
Summary									
							Pole (L2)	80.0	Pass
							Guy A (L1)	64.0	Pass
							Guy B (L1)	64.9	Pass
							Guy C (L1)	64.8	Pass
							<b>RATING =</b>	<b>80.0</b>	<b>Pass</b>

<b>Base/Flange Plate</b>	Plate Type	<b>Baseplate</b>
	Pole Diameter	37.38 in
	Pole Thickness	0.375 in
	Plate Length	44 in
	Plate Thickness	2.5 in
	Plate Fy	60 ksi
	Weld Length	0.3125 in
	$\phi_s$ Resistance	1382.37 k-in
	Applied	137.75 k-in
<b>Stiffeners</b>	#	0

Code Rev. **G**

Date 4/12/2016  
 Engineer SWF  
 Site # 302476  
 Carrier AT&T Mobility

Moment 244.8 k-ft  
 Axial 75.3 k

<b>Bolts</b>	#	8
	Bolt Circle	44 in
	(R)adial / (S)quare	S
	Bolt Gap	6 in
	Diameter	2.25 in
	Hole Diameter	2.75 in
	Type	A615-75
	Fy	75 ksi
	Fu	100 ksi
	$\phi_s$ Resistance	259.82 k
Applied	42.45 k	
<b>Reinforcement</b>	#	0
<b>Extra Bolts</b>	#	0

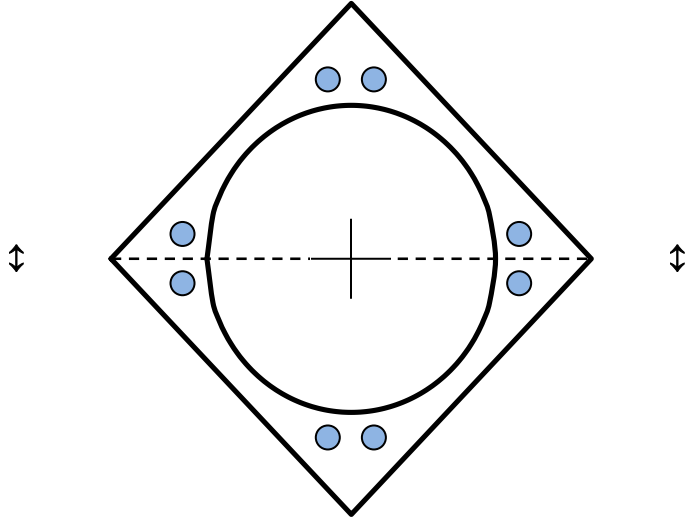


Plate Stress Ratio:  
**0.10** (Pass)

Bolt Stress Ratio:  
**0.16** (Pass)

<b>Base/Flange Plate</b>	Plate Type	<b>Flange @ 110.0 ft</b>
	Pole Diameter	21.267 in
	Pole Thickness	0.1875 in
	Plate Diameter	28.5 in
	Plate Thickness	1 in
	Plate Fy	60 ksi
	Weld Length	0.3125 in
	Allowable	75.16 k-in
	Applied	38.37 k-in
	<b>Stiffeners</b>	#

Code Rev. **G**

Date **4/12/2016**  
 Engineer **SWF**  
 Site # **302476**  
 Carrier **AT&T Mobility**

Moment **208.1 k-ft**  
 Axial **50.7 k**

Required Flange Thickness:  
**0.71 in** OK

<b>Bolts</b>	#	<b>12</b>
	Bolt Circle	25.75 in
	(R)adial / (S)quare	R
	Diameter	1 in
	Hole Diameter	1.125 in
	Type	A325
	Fy	92 ksi
	Fu	120 ksi
	Allowable	54.52 k
	Applied	28.08 k
<b>Reinforcement</b>	#	0
<b>Extra Bolts</b>	#	0

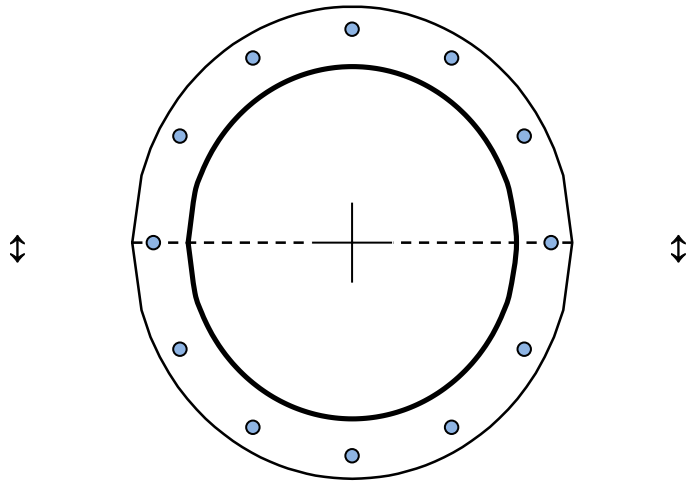
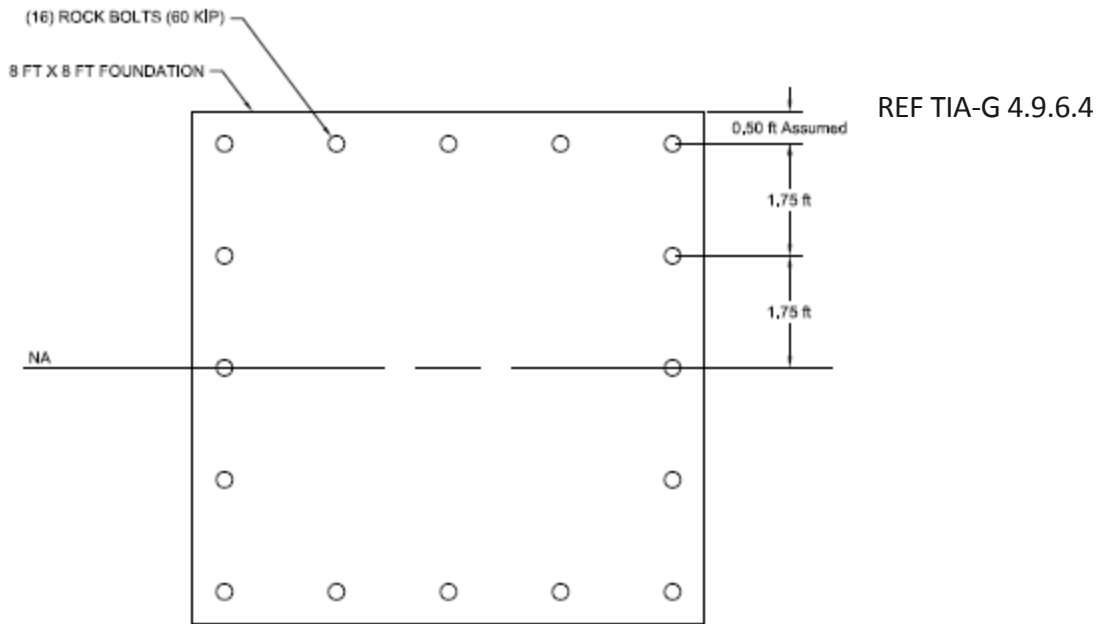
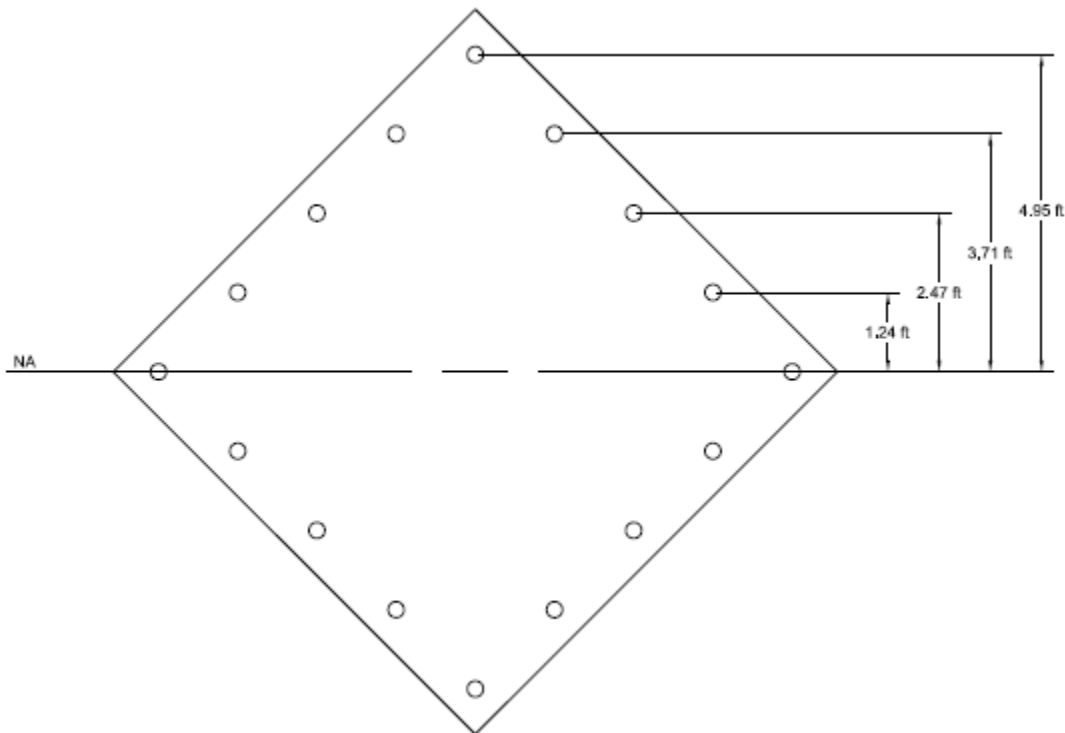


Plate Stress Ratio:  
**0.51** (Pass)

Bolt Stress Ratio:  
**0.52** (Pass)



$$OTM = 60 K[(5 * 3.5 \text{ ft}) + (2 * 1.75 \text{ ft})] * 0.9 = 1134.0 \text{ kft}$$



$$OTM = 60 K[4.95 \text{ ft} + (2 * 3.71 \text{ ft}) + (2 * 2.47 \text{ ft}) + (2 * 1.24 \text{ ft})] * 0.9 = 1068.7 \text{ kft}$$





Tower Number 302476  
Eng. Number 65649522  
April 12, 2016

### CONTROLLING USAGE

$$244.8kft/1068.6 kft = 0.23 \text{ OK}$$

### COMBINED SHEAR & TENSION

$$V_{total} = 5.8 k \quad V_{ub} = 5.4 k/16 \text{ bolts} = 0.36 k$$

$$T_{ub} = T_{applied} = 4.71 k \text{ (from Baseplate Spreadsheet)}$$

$$\left(\frac{V_{ub}}{\phi R_{nv}}\right)^2 + \left(\frac{T_{ub}}{\phi R_{nt}}\right)^2 = \left(\frac{0.36 k}{0.75(0.45 * 60 k)}\right)^2 + \left(\frac{4.71 k}{0.75(60 k)}\right)^2 = 0.01$$

$$0.01 < 1.0 \text{ OK}$$

### GUY ANCHOR ROD CHECK

$$\left. \begin{array}{l} T = 22.3 k \\ V = 21.3 k \end{array} \right\} \text{ Guy Anchor Reactions}$$

$$T_{ub} = T_{applied} = \sqrt{(22.3 k)^2 + (21.3 k)^2} = 30.8 k$$

1.5" Diameter Anchor Rod

A36 Grade Assumed

$$A_{nt} = 1.405 \text{ in}^2$$

$$\frac{T_{ub}}{\phi R_{nt}} = \frac{30.8 k}{0.5(58 \text{ ksi} * 1.405 \text{ in}^2)} = 0.76$$

$$0.76 < 1.0 \text{ OK}$$