Adam Wolfrey, Consultant
c/o New Cingular Wireless, PCS LLC(AT\&T)
Centerline Communications LLC
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Raynham, MA 02767
Phone: 508-667-3100
awolfrey@clinellc.com

## 5/17/2017

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## RE: Tower of Sharing Application // Site Number: CT1304

136 Wright Road Torrington, CT 06757 (Site Name: Torrington Wright Road)
N 41.82733 // W-73.170519

Dear Ms. Bachman:

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[^9]Adam Wolfrey, Consultant
c/o New Cingular Wireless, PCS LLC(AT\&T)
Centerline Communications LLC
95 Ryan Drive, Suite 1
Raynham, MA 02767
Phone: 508-667-3100
awolfrey@clinellc.com

## 5/17/2017

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## RE: Tower of Sharing Application // Site Number: CT1304

136 Wright Road Torrington, CT 06757 (Site Name: Torrington Wright Road)
N 41.82733 // W-73.170519

Dear Ms. Bachman:

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# Radio Frequency Emissions Analysis Report 

AT\&T Existing Facility
Site ID: CT1304
Torrington Wright Road
136 Wright Road
Torrington, CT 6757

## April 28, 2017

Centerline Communications Project Number: 950012-001

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general <br> population <br> allowable limit: | $\mathbf{4 . 9 1} \%$ |

April 28, 2017
AT\&T Mobility - New England
Attn: John Benedetto, RF Manager
550 Cochituate Road
Suite 550-13\&14
Framingham, MA 06040

## Emissions Analysis for Site: CT1304 - Torrington Wright Road

Centerline Communications, LLC ("Centerline") was directed to analyze the proposed AT\&T facility located at $\mathbf{1 3 6}$ Wright Road, Torrington, CT, for the purpose of determining whether the emissions from the Proposed AT\&T Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$. The general population exposure limits for the 700 and 850 MHz Bands are approximately $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$ and $567 \mu \mathrm{~W} / \mathrm{cm}^{2}$ respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 2300 MHz (WCS) bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were performed for the proposed AT\&T Wireless antenna facility located at $\mathbf{1 3 6}$ Wright Road, Torrington, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since AT\&T is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was focused at the base of the tower. For this report the sample point is the top of a 6 -foot person standing at the base of the tower.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in Table 1:

| Technology | Frequency Band | Channel Count | Transmit Power per <br> Channel (W) |
| :---: | :---: | :---: | :---: |
| LTE | 700 MHz | 2 | 60 |
| LTE | $1900 \mathrm{MHz}(\mathrm{PCS})$ | 2 | 60 |

Table 1: Channel Data Table

The following antennas listed in Table 2 were used in the modeling for transmission in the 700 MHz and 1900 MHz (PCS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

| Sector | Antenna <br> Number | Antenna Make / Model | Antenna <br> Centerline <br> $(\mathrm{ft})$ |
| :---: | :---: | :---: | :---: |
| A | 1 | CCI HPA-65R-BUU-H8 | 128 |
| A | 2 | CCI HPA-65R-BUU-H8 (Future) | 128 |
| A | 3 | CCI HPA-65R-BUU-H8 (Future) | 128 |
| A | 4 | CCI HPA-65R-BUU-H8 (Future) | 128 |
| B | 1 | CCI HPA-65R-BUU-H8 | 128 |
| B | 2 | CCI HPA-65R-BUU-H8 (Future) | 128 |
| B | 3 | CCI HPA-65R-BUU-H8 (Future) | 128 |
| B | 4 | CCI HPA-65R-BUU-H8 (Future) | 128 |
| C | 1 | CCI HPA-65R-BUU-H8 | 128 |
| C | 2 | CCI HPA-65R-BUU-H8 (Future) | 128 |
| C | 3 | CCI HPA-65R-BUU-H8 (Future) | 128 |
| C | 4 | CCI HPA-65R-BUU-H8 (Future) | 128 |

Table 2: Antenna Data

All calculations were done with respect to uncontrolled / general population threshold limits.

## RESULTS

Per the calculations completed for the proposed AT\&T configurations Table 3 shows resulting emissions power levels and percentages of the FCC's allowable general population limit.

| Antenna ID | Antenna Make / Model | Frequency Bands | Antenna Gain <br> (dBd) | Channel Count | Total TX Power (W) | ERP (W) | MPE \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna A1 | $\begin{gathered} \text { CCI } \\ \text { HPA-65R-BUU-H8 } \end{gathered}$ | $\begin{gathered} 700 \mathrm{MHz} \text { / } \\ 1900 \mathrm{MHz} \text { (PCS) } \end{gathered}$ | 13.15 / 14.95 | 4 | 240 | 6,229.75 | 2.19 |
| Antenna A2 | $\begin{gathered} \text { CCI } \\ \text { HPA-65R-BUU-H8 } \end{gathered}$ | Future Antenna | N/A | N/A | N/A | N/A | N/A |
| Antenna A3 | $\begin{gathered} \text { CCI } \\ \text { HPA-65R-BUU-H8 } \end{gathered}$ | Future Antenna | N/A | N/A | N/A | N/A | N/A |
| Antenna A4 | HPA-65R-BUU-H8 | Future Antenna | N/A | N/A | N/A | N/A | N/A |
| Sector A Composite MPE\% |  |  |  |  |  |  | 2.19 |
| Antenna B1 | $\begin{gathered} \text { CCI } \\ \text { HPA-65R-BUU-H8 } \end{gathered}$ | $\begin{gathered} 700 \mathrm{MHz} \text { / } \\ 1900 \mathrm{MHz} \text { (PCS) } \\ \hline \end{gathered}$ | 13.15 / 14.95 | 4 | 240 | 6,229.75 | 2.19 |
| Antenna B2 | $\begin{gathered} \text { CCI } \\ \text { HPA-65R-BUU-H8 } \end{gathered}$ | Future Antenna | N/A | N/A | N/A | N/A | N/A |
| $\begin{aligned} & \text { Antenna } \\ & \text { B3 } \end{aligned}$ | $\begin{gathered} \text { CCI } \\ \text { HPA-65R-BUU-H8 } \end{gathered}$ | Future Antenna | N/A | N/A | N/A | N/A | N/A |
| Antenna B4 | HPA-65R-BUU-H8 | Future Antenna | N/A | N/A | N/A | N/A | N/A |
| Sector B Composite MPE\% |  |  |  |  |  |  | 2.19 |
| Antenna C1 | $\begin{gathered} \text { CCI } \\ \text { HPA-65R-BUU-H8 } \end{gathered}$ | $\begin{gathered} 700 \mathrm{MHz} / \\ 1900 \mathrm{MHz} \text { (PCS) } \end{gathered}$ |  | 4 | 240 | 6,229.75 | 2.19 |
| Antenna | $\begin{gathered} \text { CCI } \\ \text { HPA-65R-BUU-H8 } \end{gathered}$ | Future Antenna | N/A | N/A | N/A | N/A | N/A |
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| $\begin{gathered} \text { Antenna } \\ \text { C } 4 \\ \hline \end{gathered}$ | $\begin{gathered} \text { CCI } \\ \text { HPA-65R-BUU-H8 } \end{gathered}$ | Future Antenna | N/A | N/A | N/A | N/A | N/A |
| Sector C Composite MPE\% |  |  |  |  |  |  | 2.19 |

Table 3: AT\&T Emissions Levels

The Following table (table 4) shows all additional carriers on site and their MPE\% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum AT\&T MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, all three sectors have the same configuration yielding the same results on all three sectors. Table 5 below shows a summary for each AT\&T Sector as well as the composite MPE value for the site.

| Site Composite MPE \% |  |
| :---: | :---: |
| Carrier | MPE \% |
| AT\&T - Max Sector Value | $\mathbf{2 . 1 9} \%$ |
| Verizon Wireless | $2.10 \%$ |
| Sprint | $0.62 \%$ |
| Site Total MPE \%: | $\mathbf{4 . 9 1} \%$ |

Table 4: All Carrier MPE Contributions

| AT\&T Sector A Total: | $2.19 \%$ |
| ---: | :---: |
| AT\&T Sector B Total: | $2.19 \%$ |
| AT\&T Sector C Total: | $2.19 \%$ |
| Site Total: |  |

Table 5: Site MPE Summary

FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. Table 6 below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated AT\&T sector(s). For this site, all three sectors have the same configuration yielding the same results on all three sectors.

| AT\&T _Max Power Values per Frequency Band / Technology (All Sectors) | \# Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Frequency (MHz) | Allowable MPE ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Calculated \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AT\&T 700 MHz LTE | 2 | 1,239.23 | 128 | 5.99 | 700 MHz | 467 | 1.28\% |
| AT\&T 1900 MHz (PCS) LTE | 2 | 1,875.65 | 128 | 9.06 | 1900 MHz (PCS) | 1000 | 0.91\% |
|  |  |  |  |  |  |  |  |

Table 6: AT\&T Maximum Sector MPE Power Values

## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the AT\&T facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| AT\&T Sector | Power Density Value (\%) |
| ---: | :--- |
| Sector A: | $2.19 \%$ |
| Sector B: | $2.19 \%$ |
| Sector C: | $2.19 \%$ |
| AT\&T Maximum Total <br> (per sector): | $2.19 \%$ |
|  |  |
| Site Total: | $4.91 \%$ |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $4.91 \%$ of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


## Scott Heffernan

RF Engineering Director
Centerline Communications, LLC
95 Ryan Drive, Suite 1
Raynham, MA 02767













4. THE SCOPE OF MORR SHAL MCLUDE FURNSHMG AL


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 6. HE Contacion stal obia Auliorzaion To proced
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## ELECTRICAL AND GROUNDING NOTES



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30. DURING CONSTRUCTION. PER FCC MANDATE, ENHANCED EMERGENC
(E911) SERVCE IS REOURED TO MEE NATONWIDE STANDAROS 31. For wielss coumucanon syirus pracc omers

 Specifications.
32. APPLICABLE BULDING CODES

UBBCONTRACTOR'S WORK SHALL COMPIY WTH ALL APPLCABLE
AATONL, STATE, ANO LOCAL COOES AS ADOPTED BY THE LOCAL
 BULDING COOE:
009 ITIERNATONAL BULDING CODE

SUBCONTRACTOR'S WORK SHALL COMPLY WTH THE LATEST EDTION OF
THE FOLOWNGG STANDARD:
AMERCAN CONCRETE NSTITUTE (ACI) 318 ; BULDING CODE
REQUREMENS FOR STRUCTURAL CONCRIE;
MERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC)
MANUAL OF STEEL CONSTRUCTION, ASD, NNTH EDTION;
IEECOMMUNICATONS INOUSTRY ASSOOCATION (TAA) 222-6,
STRUCTURAL STANOARDS FOR STELL
ANTENNA TOWER AND ANTENNA SUPPORTNG STRUCTURES: REFER
TO ELECTRRCAL DRAWINGS FOR SPECIFCC ELECTRICAL STANDAROS.



15. USE \#6 COPPER STRANDED WRE WIH GREEN COLOR
ISSUATION FOR ABOVE GRADE GROUNOING (UNESSS OTHE
 DRAWING. 16. ALL GROUND CONNECTIONS TO BE BURNOY HYGROUND
COMPRSSION TPE CONECTORS OR CAOWELD EXOHHERMCC WELD. COMPRESSION TPE CONNECTORS OR CADWELD EXOTHERMC WED
OO NOT ALLOW EARE COPPER WRE TO BE N CONTACT WTH
GALVAIZE STEEL. Galvanzed Steel.

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\begin{aligned}
& \begin{array}{l}
\text { 17. ROUTE GROUNDNG CONOUCTORS ALONG THE SHORTEST AND } \\
\text { STRAIGHIEST PATH POSSIBEE, EXCETT AS OTHERWIS INDCAIED. }
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 18. CONNECTONS TO GROUNO BARS SHAL BE MADE WTH TWO
HOLECOPRESIIN TPE OPPER LUGS. APPLY OXIE INHBTING
COMPOUND TO ALL LOCATINS. 19. BoND ANIENNA MOUNTING BRACKETS, COAXAL CABLE GROUND
KIS, AND ALLA TO EGB PLACED NEAR THE ANIENNA LOCATION. 20. APPLY OXIDE INHIBIING COMPOUND TO ALL COMPRESSION
TTPE GROUND CONNECTONS. 21. CONTRACTOR SHAL PROODE AND INSTAL OMNN DIRECTONA
EEECTRONC MAREER SYSTEM (EMS) BALS OVER EACH GROUND ROD AND BONOING POINT BETWEEN EXISTING TOWER/ (E)
MONOPOLE GROUNONG RING ANO EQUIPMENT GROUNONG RING.

23.CONTRACTOR SHAL CONDUCT ANTENNA, COAX, AND LNA


11. ALL EQUPMENT LOCATED OUTSIDE SHALL HAVE NEMA $3 R$ ENCLOSURE. 12. PPC SUPPLLED BY PROUECT OWNER.
 14. GROUND COAXAL CABLE SHIEDS MIMMUM AT BOTH ENOS USING
MANUFACTURERS COAX CABLE GROUNDING KITS SUPPLED BY PROUECT


## ABBREVIATIONS

| AGL | above grade level | g.c. | general contractor | RF | RADIO FREQUENCY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| awg | american wire gauge | м ${ }^{\text {cb }}$ | master ground bus |  |  |
| bcw | bare copper wire | MIN | minimum | TBD | to be determined |
| втS | base transceiver station | (P) | PROPOSED/NEW | TBR | to be removed |
| (E) | Existing | N.t.s. | not to Scale | TBRR | TO BE REMOVED |
| EG | EQUIPMENT GROUND | REF | Reference |  |  |
| EGR | Equipment ground ring | REQ | Required | TrP | trpical |




## SITE NUMBER: CT1304







| CADVANCED <br> ENGINEERING GROUP, P.C <br> Civil Engineering - Site Development - Surveying - Telecommunication 500 North Broadway | CENTERLINE <br> CENTERLINE COMMUNICATIONS 5 RYAN DRIVE, SUITE RAYNHAM, MA 02767 | SITE NUMBER: CT1304 <br> SITE NAME: TORRINGTON WRIGHT ROAD <br> 136 WRIGHT ROAD <br> TORRINGTON, CT 06757 <br> LITCHFIELD COUNTY | at\&t <br> 550 COCHITUATE ROAD, SUITE 13, FRAMINGHAM, MA 01701-4681 | No. | оптE | Rensions | Br | वнкк | DETAILS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\bigcirc$ | 03/01/17 | ISSUED For Renew |  | Mrc |  |  |
|  |  |  |  |  | 03/16/717 | Rension |  | MRC, |  |  |
|  |  |  |  |  | -405/7 |  |  | mac |  |  |
|  |  |  |  |  |  |  |  |  | SHEET No. | A-4 |





## Subject:

Carrier Designation:

Crown Castle Designation:

Engineering Firm Designation:
Site Data:

Structural Analysis Report
AT\&T Mobility Co-Locate
Carrier Site Number:
Carrier Site Name:
Crown Castle BU Number:
Crown Castle Site Name:
Crown Castle JDE Job Number:
Crown Castle Work Order Number:
Crown Castle Application Number:
B+T Group Project Number:

CT1304
Torrington Wright Road
876373
Long Eddy / Wright Property 427346
1381942
378332 Rev. 2
89028.006.01

136 Wright Rd., Torrington, Litchfield County, CT Latitude $41^{\circ} 49^{\prime} 38.34^{\prime \prime}$, Longitude -73 ${ }^{\circ} 10^{\prime} 13.97{ }^{\prime \prime}$
148 Foot - Monopole Tower
Dear Charles McGuirt,
$B+T$ Group is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 1016487, in accordance with application 378332, revision 2.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

```
LC5: Existing + SLA Equipment + Proposed Equipment
Note: See Table 1 and Table 2 for the proposed and existing loading, respectively.
```


## Sufficient Capacity

This analysis has been performed in accordance with the 2016 Connecticut State Building Code based upon an ultimate 3 -second gust wind speed of 120 mph converted to a nominal 3 -second gust wind speed of 93 mph per Section 1609.3 and Appendix N as required for use in the TIA-222-G Standard per Exception \#5 of Section 1609.1.1. Exposure Category B and Risk Category II were used in this analysis.

All equipment proposed in this report shall be installed in accordance with the attached drawings for the determined available structural capacity to be effective.

We at $B+T$ Group appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:
B+T Engineering, Inc.


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Table 4 - Documents Provided
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## 5) APPENDIX A

tnxTower Output

## 6) APPENDIX B

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7) APPENDIX C

Additional Calculations

## 1) INTRODUCTION

This tower is a 148 ft . Monopole tower designed by Summit manufacturing in June of 2000. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-F.This tower has been modified by B+T Group in February of 2014 and those modifications are incorporated in our Analysis.

## 2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA-222-G Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a 3-second gust wind speed of 93 mph with no ice, 40 mph with 0.75 inch ice thickness and 60 mph under service loads, exposure category B with topographic category 1 and crest height of 0 feet.

Table 1 - Proposed Antenna and Cable Information

| Mounting Level (ft) | Center Line Elevation (ft) | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 128.0 | 128.0 | 3 | CCI Antennas | HPA-65R-BUU-H8 | 51 | $\begin{aligned} & 3 / 4 \\ & 3 / 8 \end{aligned}$ | -- |
|  |  | 9 | Ericsson | RRU-11 |  |  |  |
|  |  | 2 | Raycap | DC6-48-60-18-8F |  |  |  |
|  |  | 1 | -- | Sector Mount [SM 406-3] |  |  |  |

Table 2 - Existing Antenna and Cable Information

| Mounting Level (ft) | Center Line Elevation (ft) | $\begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 149.0 | 149.0 | 3 | Alcatel Lucent | TME-1900MHz RRH (65MHz) | -- | -- | 1 |
|  |  | 3 | Alcatel Lucent | TME-800MHZ RRH |  |  |  |
|  |  | 1 | -- | Pipe Mount [PM 601-3] |  |  |  |
| 148.0 | 149.0 | 3 | Alcatel Lucent | 800 EXTERNAL NOTCH FILTER | 3 | 1-1/4 | 1 |
|  |  | 9 | Rfs Celwave | ACU-A20-N |  |  |  |
|  |  | 3 | Rfs Celwave | APXVSPP18-C-A20 |  |  |  |
|  | 148.0 | 1 | -- | Platform Mount [LP 712-1] |  |  |  |
| 138.0 | 138.0 | 1 | Antel | BXA-171063-8BF-2 | 18 | 1-5/8 | 1 |
|  |  | 2 | Antel | BXA-171085-8BF-EDIN-2 |  |  |  |
|  |  | 3 | Antel | BXA-70063-6CF-2 |  |  |  |
|  |  | 2 | Antel | LPA-80063/6CF |  |  |  |
|  |  | 4 | Antel | LPA-80080/6CF |  |  |  |
|  |  | 1 | -- | Platform Mount [LP 712-1] |  |  |  |
| 128.0 | 128.0 | 12 | CCI Antennas | HPA-65R-BUU-H8 | $\begin{aligned} & 8 \\ & 3 \\ & 2 \end{aligned}$ | $\begin{gathered} 3 / 4 \\ 5 / 16 \\ 3 / 8 \end{gathered}$ | 2 |
|  |  | 3 | Ericsson | KRF 102 361/1 |  |  |  |
|  |  | 9 | Ericsson | RRU-11 |  |  |  |
|  |  | 6 | Ericsson | RRUS 12-B2 |  |  |  |
|  |  | 6 | Ericsson | RRUS A2 |  |  |  |
|  |  | 3 | Ericsson | RRUS E2 B29 |  |  |  |
|  |  | 3 | Ericsson | RRUS-32 B30 |  |  |  |


| Mounting Level (ft) | Center Line Elevation (ft) | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 4 | Raycap | DC6-48-60-18-8F |  |  |  |
| 79.0 | 84.0 | 1 | Rfs Celwave | PD1109E | 1 | 1/2 | 1 |
|  | 79.0 | 1 | -- | Side Arm Mount [SO 701-1] |  |  |  |
| 45.0 | 45.0 | 1 | Gps | GPS_A | 1 | 1/2 | 1 |
|  |  | 1 | -- | Side Arm Mount [SO 701-1] |  |  |  |
| 13.0 | 13.0 | 1 | Gps | GPS_A | 1 | 1/2 | 1 |
|  |  | 1 | -- | Side Arm Mount [SO 701-1] |  |  |  |

Notes:

1) Existing Equipment
2) SLA Equipment; Considered in This Analysis

Table 3 - Design Antenna and Cable Information

| Mounting Level (ft) | Center Line Elevation (ft) | $\begin{array}{\|c} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array}$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 148 | 148 | 12 | Dapa | 48000 PCS Panel | -- | -- |
|  |  | 1 | Generic | 14' LP Platform |  |  |
| 140 | 140 | 12 | Dapa | 48000 PCS Panel | -- | -- |
|  |  | 1 | Generic | 14' LP Platform |  |  |
| 130 | 130 | 12 | Dapa | 48000 PCS Panel | -- | -- |
|  |  | 1 | Generic | 14' LP Platform |  |  |
| 120 | 120 | 12 | Dapa | 48000 PCS Panel | -- | -- |
|  |  | 1 | Generic | 14' LP Platform |  |  |
| 76 | 76 | 1 | Generic | GPS Antenna | -- | -- |
|  |  | 1 | Generic | GPS Stand-on Mount |  |  |

## 3) ANALYSIS PROCEDURE

Table 4 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| Online Application | AT\&T Mobility Co-locate, Revision\# 2 | 378332 | CCI Sites |
| Tower Manufacturer Drawing | Summit, Date: 06/23/2000 | 1631601 | CCI Sites |
| Tower Modification Drawing | B+T Group, Project No. 89028.003.01 | 4491592 | CCI Sites |
| Post Modification Inspection | TEP, Project No. 52429.14747 | 5215998 | CCI Sites |
| Foundation Drawing | Summit, Job No. 10185 | 1634518 | CCI Sites |
| Geotech Report | Clerence Welti Assoc., Inc., Date: 05/12/2000 | 1531964 | CCI Sites |
| Antenna Configuration | Crown CAD Package | Date: $03 / 06 / 2017$ | CCI Sites |

## 3.1) Analysis Method

tnxTower (version 7.0.5.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases.
Selected output from the analysis is included in Appendix A.

## 3.2) Assumptions

1) Tower and structures were built in accordance with the manufacturer's specifications.
2) The tower and structures have been maintained in accordance with the manufacturer's specification.
3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
4) Mount areas and weights are assumed based on photographs provided.

This analysis may be affected if any assumptions are not valid or have been made in error. $\mathrm{B}+\mathrm{T}$ Group should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

| Section <br> No. | Elevation (ft) | Component <br> Type | Size | Critical <br> Element | P (K) | SF*P_allow <br> (K) | \% <br> Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $148-116.5$ | Pole | TP29.48x24x0.219 | 1 | -11.599 | 1273.620 | 35.3 | Pass |
| L2 | $116.5-98.5$ | Pole | TP32.175x28.39x0.25 | 2 | -14.888 | 1751.620 | 58.2 | Pass |
| L3 | $98.5-80.25$ | Pole | TP35.35x32.175x0.434 | 3 | -17.904 | 2235.790 | 60.3 | Pass |
| L4 | $80.25-70.5$ | Pole | TP36.547x34.067x0.487 | 4 | -22.445 | 2653.470 | 63.4 | Pass |
| L5 | $70.5-39.75$ | Pole | TP41.9x36.547x0.591 | 5 | -30.635 | 3874.320 | 56.6 | Pass |
| L6 | $39.75-31.75$ | Pole | TP42.666x40.361x0.643 | 6 | -37.154 | 4394.700 | 56.3 | Pass |
| L7 | $31.75-17.75$ | Pole | TP45.102x42.666x0.626 | 7 | -42.513 | 4539.090 | 59.7 | Pass |
| L8 | $17.75-14.25$ | Pole | TP45.711x45.102x0.728 | 8 | -44.114 | 4902.000 | 56.7 | Pass |
| L9 | $14.25-0$ | Pole | TP48.19x45.711x0.619 | 9 | -50.195 | 4669.620 | 64.0 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Pole (L9) | 64.0 | Pass |
|  |  |  |  |  |  | Rating = | 64.0 | Pass |

Table 6 - Tower Component Stresses vs. Capacity - LC5

| Notes | Component | Elevation (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Anchor Rod Bracket | Base | 77.4 | Pass |
| 1 | Anchor Rods | Base | 50.9 | Pass |
| 1 | Base Plate | Base | 49.5 | Pass |
| 1 | Base Foundation(Structure) | Base | 48.7 | Pass |
| 1 | Base Foundation (Soil Interaction) | Base | 76.9 | Pass |
|  |  |  |  |  |

Notes:

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity consumed.

## 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the final load configuration. No modifications are required at this time.

APPENDIX A
TNXTOWER OUTPUT
148.0 ft



DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| Top Hat (E) | 149.5 | (3) RRU-11 (P) | 128 |
| TME-1900MHz RRH (65MHz) (E) | 149 | (3) RRU-11 (P) | 128 |
| TME-1900MHz RRH ( 65 MHz ) (E) | 149 | (2) DC6-48-60-18-8F (P) | 128 |
| TME-1900MHz RRH (65MHz) (E) | 149 | (4) HPA-65R-BUU-H8 w/ Mount Pipe (ATI--SLA) | 128 |
| TME-800MHZ RRH (E) | 149 |  |  |
| TME-800MHZ RRH (E) | 149 | (4) HPA-65R-BUU-H8 w/ Mount Pipe (SLA) | 128 |
| TME-800MHZ RRH (E) | 149 |  |  |
| Pipe Mount [PM 601-3] (E) | 149 | (4) HPA-65R-BUU-H8 w/ Mount Pipe (SLA) | 128 |
| APXVSPP18-C-A20 w/ Mount Pipe (E) | 148 | RRUS E2 B29 (SLA) | 128 |
| APXVSPP18-C-A20 w/ Mount Pipe (E) | 148 | RRUS E2 B29 (SLA) | 128 |
| APXVSPP18-C-A20 w/ Mount Pipe (E) | 148 | RRUS E2 B29 (SLA) | 128 |
| (3) ACU-A20-N (E) | 148 | (3) RRU-11 (SLA) | 128 |
| (3) ACU-A20-N (E) | 148 | (3) RRU-11 (SLA) | 128 |
| (3) ACU-A20-N (E) | 148 | (3) RRU-11 (SLA) | 128 |
| 800 EXTERNAL NOTCH FILTER (E) | 148 | RRUS-32 B30 (SLA) | 128 |
| 800 EXTERNAL NOTCH FILTER (E) | 148 | RRUS-32 B30 (SLA) | 128 |
| 800 EXTERNAL NOTCH FILTER (E) | 148 | RRUS-32 B30 (SLA) | 128 |
| (2) $6^{\prime} \times 2$ 2" Mount Pipe (E) | 148 | DC6-48-60-18-8F (SLA) | 128 |
| (2) 6' $\times 2$ " Mount Pipe (E) | 148 | (2) DC6-48-60-18-8F (SLA) | 128 |
| (2) 6' $\times 2$ ' Mount Pipe (E) | 148 | DC6-48-60-18-8F (SLA) | 128 |
| Platform Mount [LP 712-1] (E-12'/TIA) | 148 | (2) RRUS 12-B2 (SLA) | 128 |
| BXA-70063-6CF-2 w/ Mount Pipe (E) | 138 | (2) RRUS 12-B2 (SLA) | 128 |
| BXA-70063-6CF-2 w/ Mount Pipe (E) | 138 | (2) RRUS 12-B2 (SLA) | 128 |
| BXA-70063-6CF-2 w/ Mount Pipe (E) | 138 | (2) RRUS A2 (SLA) | 128 |
| BXA-171085-8BF-EDIN-2 w/ Mount Pipe (E) | 138 | (2) RRUS A2 (SLA) | 128 |
| BXA-171085-8BF-EDIN-2 w/ Mount | 138 | (2) RRUS A2 (SLA) | 128 |
| Pipe (E) |  | KRF 102 361/1 (SLA) | 128 |
| BXA-171063-8BF-2 w/ Mount Pipe (E) | 138 | KRF 102 361/1 (SLA) | 128 |
| (2) LPA-80063/6CF w/ Mount Pipe (E) | 138 | KRF 102 361/1 (SLA) | 128 |
| (2) LPA-80080/6CF w/ Mount Pipe (E) | 138 | Sector Mount [SM 406-3] (P) | 128 |
| (2) LPA-80080/6CF w/ Mount Pipe (E) | 138 | PD1109E (E) | 79 |
| Platform Mount [LP 712-1] (E) | 138 | Side Arm Mount [SO 701-1] (E) | 79 |
| HPA-65R-BUU-H8 w/ Mount Pipe | 128 | GPS_A (E) | 45 |
| (ATI--P) |  | Side Arm Mount [SO 701-1] (E) | 45 |
| HPA-65R-BUU-H8 w/ Mount Pipe (P) | 128 | GPS_A (E-CL/TIA) | 13 |
| HPA-65R-BUU-H8 w/ Mount Pipe (P) | 128 | Side Arm Mount [SO 701-1] (E-Mount Ht./TIA) | 13 |
| (3) RRU-11 (P) | 128 |  |  |

## MATERIAL STRENGTH

| GRADE |  |  |  |  |  |  |  | Fy | Fu | GRADE | Fy | Fu |
| :--- | :--- | :--- | :---: | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A607-60 | 60 ksi | 75 ksi | 44.81049 ksi | 45 ksi | 60 ksi |  |  |  |  |  |  |  |
| A607-65 | 65 ksi | 80 ksi | 44.910822 ksi | 45 ksi | 60 ksi |  |  |  |  |  |  |  |
| 41.599417 ksi | 42 ksi | 57 ksi | 41.277494 ksi | 41 ksi | 56 ksi |  |  |  |  |  |  |  |
| 41.661197 ksi | 42 ksi | 57 ksi | 43.725232 ksi | 44 ksi | 59 ksi |  |  |  |  |  |  |  |
| 44.711572 ksi | 45 ksi | 60 ksi |  |  |  |  |  |  |  |  |  |  |

## TOWER DESIGN NOTES

1. Tower is located in Litchfield County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 93 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 40 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
ALL REACTIO^5. Deflections are based upon a 60 mph wind.
ARE FACTORE6. Tower Structure Class II.
5. Topographic Category 1 with Crest Height of 0.000 ft
6. TOWER RATING: $64 \%$


TORQUE 0 kip-ft
40 mph WIND - 0.750 in ICE

## AXIAL 50 K


$25 \mathrm{~K} \longrightarrow \quad, 2859 \mathrm{kip}-\mathrm{ft}$
TORQUE 1 kip-ft REACTIONS - 93 mph WIND

| B+T Group  <br> F 1717 S.Boulder, Suite 300 <br> Tulsa, OK 74119  <br> Phone: (918) 587-4630  <br>  FAX: (918) 295-0265 |  | Tob: 89028.006 .01 - LONG EDDY WRIGHT PROPERTY, CT (BU\# 87637 ( ${ }^{\text {Project: }}$ |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  | Client: Crown Castle | Drawn by: Pavan Pai | App'd: |
|  |  | Code: TIA-222-G | Date: 03/23/17 | Scale: NTS |
|  |  | Path: |  | Dwg No. E-1 |







Twist (deg)


| B+T Group |  |
| :---: | :---: |
| B + T GRP | 1717 S.Boulder, Suite 300 |
| Tulsa, OK 74119 |  |

Tulsa, OK 74119 Phone: (918) 587-4630
FAX: (918) 295-0265
$\qquad$
$\qquad$ Flat $\qquad$ App In Face $\qquad$ App Out Face $\qquad$ Truss Leg


| $\sqrt{B+T}$ | B+T Group <br> 1717 S.Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Pob: 89028.006.01 - LONG EDDY WRIGHT PROPERTY, CT (BU\# 87637 |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  | Client: Crown Castle | Drawn by: Pavan Pai | App'd: |
|  |  | Code: TIA-222-G | Date: 03/23/17 | Scale: NTS |
|  |  | Path: |  | Dwg No. E-7 |



## Tower Input Data

There is a pole section.
This tower is designed using the TIA-222-G standard.
The following design criteria apply:
Tower is located in Litchfield County, Connecticut.
Basic wind speed of 93 mph .
Structure Class II.
Exposure Category B.
Topographic Category 1.
Crest Height 0.000 ft .
Nominal ice thickness of 0.750 in.
Ice thickness is considered to increase with height.
Ice density of 56.000 pcf.
A wind speed of 40 mph is used in combination with ice.
Temperature drop of $50.000^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

[^15]Distribute Leg Loads As Uniform Assume Legs Pinned
$\sqrt{ }$ Assume Rigid Index Plate
$\sqrt{ }$ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
$\sqrt{ }$ Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder

Use ASCE 10 X-Brace Ly Rules
Calculate Redundant Bracing Forces
Ignore Redundant Members in FEA
SR Leg Bolts Resist Compression
All Leg Panels Have Same Allowable
Offset Girt At Foundation
$\sqrt{ }$ Consider Feed Line Torque
Include Angle Block Shear Check
Use TIA-222-G Bracing Resist. Exemption
Use TIA-222-G Tension Splice Exemption Poles
$\sqrt{ }$ Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets

## Tapered Pole Section Geometry

| Section | Elevation <br> $f t$ | Section Length $f t$ | Splice Length ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend <br> Radius <br> in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 148.000-116.50 | 31.500 | 3.750 | 18 | 24.000 | 29.480 | 0.219 | 0.875 | A607-60 |
|  | 0 |  |  |  |  |  |  |  | (60 ksi) |
| L2 | 116.500-98.500 | 21.750 | 0.000 | 18 | 28.390 | 32.175 | 0.250 | 1.000 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |



| Section | Elevation <br> $f t$ | Section Length $f t$ | Splice Length <br> ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L3 | 98.500-80.250 | 18.250 | 4.500 | 18 | 32.175 | 35.350 | 0.434 | 1.736 | $\begin{aligned} & \text { 41.599417ksi } \\ & (42 \mathrm{ksi}) \end{aligned}$ |
| L4 | 80.250-70.500 | 14.250 | 0.000 | 18 | 34.067 | 36.547 | 0.487 | 1.947 | $\begin{aligned} & \text { 41.661197ksi } \\ & (42 \mathrm{ksi}) \end{aligned}$ |
| L5 | 70.500-39.750 | 30.750 | 5.250 | 18 | 36.547 | 41.900 | 0.591 | 2.365 | $\begin{aligned} & 44.711572 \mathrm{ksi} \\ & (45 \mathrm{ksi}) \end{aligned}$ |
| L6 | 39.750-31.750 | 13.250 | 0.000 | 18 | 40.361 | 42.666 | 0.643 | 2.573 | $\begin{aligned} & 44.81049 \mathrm{ksi} \\ & (45 \mathrm{ksi}) \end{aligned}$ |
| L7 | 31.750-17.750 | 14.000 | 0.000 | 18 | 42.666 | 45.102 | 0.626 | 2.506 | $\begin{aligned} & 44.910822 \mathrm{ksi} \\ & (45 \mathrm{ksi}) \end{aligned}$ |
| L8 | 17.750-14.250 | 3.500 | 0.000 | 18 | 45.102 | 45.711 | 0.728 | 2.911 | $\begin{aligned} & \text { 41.277494ksi } \\ & (41 \mathrm{ksi}) \end{aligned}$ |
| L9 | 14.250-0.000 | 14.250 |  | 18 | 45.711 | 48.190 | 0.619 | 2.475 | $\begin{aligned} & 43.725232 \mathrm{ksi} \\ & (44 \mathrm{ksi}) \end{aligned}$ |

Tapered Pole Properties

| Section | Tip Dia. <br> in | Area <br> $i n^{2}$ | $I$ <br> $i n^{4}$ | $r$ <br> in | $C$ <br> in | $I / C$ <br> $i n^{3}$ | $J$ <br> $i n^{4}$ | $I t / Q$ <br> $i n^{2}$ | $w$ <br> in |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 24.370 | 16.512 | 1179.768 | 8.442 | 12.192 | 96.766 | 2361.088 | 8.257 | 3.839 | 17.55 |
|  | 29.935 | 20.316 | 2197.713 | 10.388 | 14.976 | 146.751 | 4398.319 | 10.160 | 4.803 |  |
| L2 | 29.491 | 22.329 | 2233.892 | 9.990 | 14.422 | 154.893 | 4470.723 | 11.167 | 4.557 | 18.227 |
|  | 32.671 | 25.332 | 3261.812 | 11.333 | 16.345 | 199.564 | 6527.916 | 12.668 | 5.223 | 20.891 |
| L3 | 32.671 | 43.726 | 5565.479 | 11.268 | 16.345 | 340.507 | 11138.281 | 21.867 | 4.899 | 11.287 |
|  | 35.895 | 48.100 | 7408.540 | 12.395 | 17.958 | 412.553 | 14826.827 | 24.055 | 5.458 | 12.575 |
| L4 | 35.388 | 51.890 | 7392.471 | 11.921 | 17.306 | 427.161 | 14794.670 | 25.950 | 5.139 | 10.555 |
|  | 37.111 | 55.723 | 9154.622 | 12.802 | 18.566 | 493.082 | 18321.290 | 27.867 | 5.575 | 11.452 |
| L5 | 37.111 | 67.480 | 11022.014 | 12.764 | 18.566 | 593.663 | 22058.531 | 33.747 | 5.392 | 9.119 |
|  | 42.546 | 77.526 | 16713.430 | 14.665 | 21.285 | 785.214 | 33448.852 | 38.770 | 6.334 | 10.712 |
| L6 | 41.911 | 81.096 | 16162.580 | 14.100 | 20.503 | 788.285 | 32346.427 | 40.556 | 5.971 | 9.282 |
|  | 43.325 | 85.803 | 19143.219 | 14.918 | 21.674 | 883.214 | 38311.628 | 42.910 | 6.377 | 9.913 |
| L7 | 43.325 | 83.582 | 18662.634 | 14.924 | 21.674 | 861.042 | 37349.825 | 41.799 | 6.407 | 10.228 |
|  | 45.798 | 88.424 | 22097.930 | 15.789 | 22.912 | 964.478 | 44224.937 | 44.221 | 6.836 | 10.913 |
| L8 | 45.798 | 102.493 | 25497.284 | 15.753 | 22.912 | 1112.845 | 51028.117 | 51.256 | 6.657 | 9.148 |
|  | 46.416 | 103.899 | 26561.387 | 15.969 | 23.221 | 1143.846 | 53157.724 | 51.960 | 6.764 | 9.295 |
| L9 | 46.416 | 88.564 | 22750.786 | 16.008 | 23.221 | 979.745 | 45531.507 | 44.291 | 6.956 | 11.241 |
|  | 48.933 | 93.434 | 26713.350 | 16.888 | 24.481 | 1091.208 | 53461.849 | 46.726 | 7.392 | 11.946 |


| Tower Elevation <br> ft | Gusset Area (per face) | Gusset Thickness in | Gusset Grade | Adjust. Factor $A_{f}$ | Adjust. <br> Factor <br> $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 |  |  |  | 1 | 1 | 1 |  |  |  |
| 148.000-116.5 |  |  |  |  |  |  |  |  |  |
| 00 |  |  |  |  |  |  |  |  |  |
| L2 |  |  |  | 1 | 1 | 1 |  |  |  |
| 116.500-98.50 |  |  |  |  |  |  |  |  |  |
| 0 |  |  |  |  |  |  |  |  |  |
| L3 |  |  |  | 1 | 1 | 0.962717 |  |  |  |
| 98.500-80.250 |  |  |  |  |  |  |  |  |  |
| L4 |  |  |  | 1 | 1 | 0.968696 |  |  |  |
| 80.250-70.500 |  |  |  |  |  |  |  |  |  |
| L5 |  |  |  | 1 | 1 | 0.953422 |  |  |  |
| 70.500-39.750 |  |  |  |  |  |  |  |  |  |



| Tower Elevation <br> ft | Gusset <br> Area (per face) <br> $f t^{2}$ | Gusset Thickness in | Gusset Grade | Adjust. Factor $A_{f}$ | Adjust. <br> Factor <br> $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L6 |  |  |  | 1 | 1 | 0.958861 |  |  |  |
| 39.750-31.750 |  |  |  |  |  |  |  |  |  |
| L7 |  |  |  | 1 | 1 | 0.963264 |  |  |  |
| 31.750-17.750 |  |  |  |  |  |  |  |  |  |
| L8 |  |  |  | 1 | 1 | 0.983373 |  |  |  |
| 17.750-14.250 |  |  |  |  |  |  |  |  |  |
| L9 |  |  |  | 1 | 1 | 1.01129 |  |  |  |
| 14.250-0.000 |  |  |  |  |  |  |  |  |  |

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Sector | Component <br> Type | Placement | Total <br> Number | Number <br> Per Row | Start/End <br> Position | Width or <br> Diameter <br> in | Perimeter |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## Feed Line/Linear Appurtenances - Entered As Area



| Description | Face or Leg | Allow Shield | Component Type | $f t$ | Total <br> Number |  | $C_{A} A_{A}$ <br> $f t^{2} / f t$ | Weight <br> klf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { HB114-1-0813U4-M5J(1 } \\ -1 / 4) \end{gathered}$ | A | No | Inside Pole | 148.000-0.000 | 3 | No Ice | 0.000 | 0.001 |
|  |  |  |  |  |  | 1/2" Ice | 0.000 | 0.001 |
| (E) |  |  |  |  |  | $1{ }^{1 \prime}$ Ice | 0.000 | 0.001 |
| LDF7-50A(1-5/8) | B | No | Inside Pole | 138.000-0.000 | 12 | No Ice | 0.000 | 0.001 |
| (E) |  |  |  |  |  | 1/2" Ice | 0.000 | 0.001 |
|  |  |  |  |  |  | 1 " Ice | 0.000 | 0.001 |
| **/>** |  |  |  |  |  |  |  |  |
| L98B-002-XXX_DB(3/8 | C | No | Inside Pole | 128.000-0.000 | 1 | No Ice | 0.000 | 0.000 |
| ) |  |  |  |  |  | 1/2" Ice | 0.000 | 0.000 |
| (P) |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.000 | 0.000 |
| WR-VG86ST-BRD(3/4) | C | No | Inside Pole | 128.000-0.000 | 5 | No Ice | 0.000 | 0.001 |
| (P) |  |  |  |  |  | 1/2" Ice | 0.000 | 0.001 |
|  |  |  |  |  |  | $1{ }^{1 \prime}$ Ice | 0.000 | 0.001 |
| ATCB-B01-060(5/16) | C | No | Inside Pole | 128.000-0.000 | 3 | No Ice | 0.000 | 0.000 |
| (SLA) |  |  |  |  |  | 1/2" Ice | 0.000 | 0.000 |
|  |  |  |  |  |  | 1" Ice | 0.000 | 0.000 |
| L98B-002-XXX_DB(3/8 | C | No | Inside Pole | 128.000-0.000 | 2 | No Ice | 0.000 | 0.000 |
| ) |  |  |  |  |  | 1/2" Ice | 0.000 | 0.000 |
| (SLA) |  |  |  |  |  | $1^{\prime \prime}$ Ice | 0.000 | 0.000 |
| WR-VG86ST-BRD(3/4) | C | No | Inside Pole | 128.000-0.000 | 8 | No Ice | 0.000 | 0.001 |
| (SLA) |  |  |  |  |  | 1/2" Ice | 0.000 | 0.001 |
|  |  |  |  |  |  | $1{ }^{1 \prime}$ Ice | 0.000 | 0.001 |
| **/>** |  |  |  |  |  |  |  |  |
| LDF4-50A(1/2) | C | No | Inside Pole | 79.000-0.000 | 1 | No Ice | 0.000 | 0.000 |
| (E) |  |  |  |  |  | 1/2" Ice | 0.000 | 0.000 |
|  |  |  |  |  |  | $1{ }^{1 \prime}$ Ice | 0.000 | 0.000 |
| **/>** |  |  |  |  |  |  |  |  |
| LDF4-50A(1/2) | B | No | Inside Pole | 13.000-0.000 | 1 | No Ice | 0.000 | 0.000 |
| (E-Ht./TIA) |  |  |  |  |  | 1/2" Ice | 0.000 | 0.000 |
|  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.000 | 0.000 |
| **/>** |  |  |  |  |  |  |  |  |

## Feed Line/Linear Appurtenances Section Areas

| Tower Section | Tower Elevation $f t$ | Face | $A_{R}$ $f t^{2}$ | $A_{F}$ $f t^{2}$ | $C_{A} A_{A}$ In Face $f t^{2}$ | $C_{A} A_{A}$ <br> Out Face $f t^{2}$ | Weight K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 148.000-116.500 | A | 0.000 | 0.000 | 1.181 | 0.000 | 0.120 |
|  |  | B | 0.000 | 0.000 | 25.542 | 0.000 | 0.317 |
|  |  | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.092 |
| L2 | 116.500-98.500 | A | 0.000 | 0.000 | 0.675 | 0.000 | 0.069 |
|  |  | B | 0.000 | 0.000 | 21.384 | 0.000 | 0.266 |
|  |  | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.144 |
| L3 | 98.500-80.250 | A | 0.000 | 0.000 | 18.934 | 0.000 | 0.070 |
|  |  | B | 0.000 | 0.000 | 39.931 | 0.000 | 0.269 |
|  |  | C | 0.000 | 0.000 | 18.250 | 0.000 | 0.146 |
| L4 | 80.250-70.500 | A | 0.000 | 0.000 | 10.116 | 0.000 | 0.037 |
|  |  | B | 0.000 | 0.000 | 21.333 | 0.000 | 0.144 |
|  |  | C | 0.000 | 0.000 | 9.750 | 0.000 | 0.079 |
| L5 | 70.500-39.750 | A | 0.000 | 0.000 | 45.046 | 0.000 | 0.118 |
|  |  | B | 0.000 | 0.000 | 80.094 | 0.000 | 0.454 |
|  |  | C | 0.000 | 0.000 | 43.563 | 0.000 | 0.250 |
| L6 | 39.750-31.750 | A | 0.000 | 0.000 | 12.137 | 0.000 | 0.032 |
|  |  | B | 0.000 | 0.000 | 20.837 | 0.000 | 0.118 |
|  |  | C | 0.000 | 0.000 | 11.333 | 0.000 | 0.065 |
| L7 | 31.750-17.750 | A | 0.000 | 0.000 | 21.240 | 0.000 | 0.056 |
|  |  | B | 0.000 | 0.000 | 36.465 | 0.000 | 0.207 |
|  |  | C | 0.000 | 0.000 | 19.833 | 0.000 | 0.114 |



| Tower <br> Section | Tower <br> Elevation <br> $f t$ | Face | $A_{R}$ | $A_{F}$ | $C_{A} A_{A}$ <br> In Face | $C_{A} A_{A}$ <br> Out Face | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t^{2}$ | ${f t^{2}}^{f t^{2}}$ | $t^{2}$ | K |  |
| L8 | $17.750-14.250$ | A | 0.000 | 0.000 | 9.102 | 0.000 | 0.014 |
|  |  | B | 0.000 | 0.000 | 12.908 | 0.000 | 0.052 |
|  |  | C | 0.000 | 0.000 | 4.958 | 0.000 | 0.028 |
| L9 | $14.250-0.000$ | A | 0.000 | 0.000 | 16.870 | 0.000 | 0.057 |
|  |  | B | 0.000 | 0.000 | 52.554 | 0.000 | 0.212 |
|  |  | C | 0.000 | 0.000 | 20.188 | 0.000 | 0.116 |

Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower Section | Tower Elevation ft | Face or Leg | Ice Thickness in | $A_{R}$ $f t^{2}$ | $A_{F}$ $f t^{2}$ | $C_{A} A_{A}$ In Face $f t^{2}$ | $\begin{gathered} C_{A} A_{A} \\ \text { Out Face } \\ {f t^{2}}^{2} \end{gathered}$ | Weight K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 148.000-116.500 | A | 1.723 | 0.000 | 0.000 | 12.035 | 0.000 | 0.259 |
|  |  | B |  | 0.000 | 0.000 | 41.188 | 0.000 | 0.805 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.092 |
| L2 | 116.500-98.500 | A | 1.688 | 0.000 | 0.000 | 6.877 | 0.000 | 0.148 |
|  |  | B |  | 0.000 | 0.000 | 34.483 | 0.000 | 0.674 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.144 |
| L3 | 98.500-80.250 | A | 1.657 | 0.000 | 0.000 | 31.030 | 0.000 | 0.383 |
|  |  | B |  | 0.000 | 0.000 | 58.958 | 0.000 | 0.905 |
|  |  | C |  | 0.000 | 0.000 | 24.298 | 0.000 | 0.384 |
| L4 | 80.250-70.500 | A | 1.629 | 0.000 | 0.000 | 16.577 | 0.000 | 0.205 |
|  |  | B |  | 0.000 | 0.000 | 31.498 | 0.000 | 0.483 |
|  |  | C |  | 0.000 | 0.000 | 12.981 | 0.000 | 0.207 |
| L5 | 70.500-39.750 | A | 1.579 | 0.000 | 0.000 | 66.124 | 0.000 | 0.738 |
|  |  | B |  | 0.000 | 0.000 | 111.074 | 0.000 | 1.570 |
|  |  | C |  | 0.000 | 0.000 | 53.272 | 0.000 | 0.731 |
| L6 | 39.750-31.750 | A | 1.512 | 0.000 | 0.000 | 19.716 | 0.000 | 0.221 |
|  |  | B |  | 0.000 | 0.000 | 28.897 | 0.000 | 0.408 |
|  |  | C |  | 0.000 | 0.000 | 13.860 | 0.000 | 0.190 |
| L7 | 31.750-17.750 | A | 1.457 | 0.000 | 0.000 | 33.480 | 0.000 | 0.352 |
|  |  | B |  | 0.000 | 0.000 | 49.803 | 0.000 | 0.671 |
|  |  | C |  | 0.000 | 0.000 | 23.913 | 0.000 | 0.312 |
| L8 | 17.750-14.250 | A | 1.395 | 0.000 | 0.000 | 12.976 | 0.000 | 0.123 |
|  |  | B |  | 0.000 | 0.000 | 17.090 | 0.000 | 0.202 |
|  |  | C |  | 0.000 | 0.000 | 5.935 | 0.000 | 0.076 |
| L9 | 14.250-0.000 | A | 1.286 | 0.000 | 0.000 | 27.778 | 0.000 | 0.282 |
|  |  | B |  | 0.000 | 0.000 | 65.256 | 0.000 | 0.768 |
|  |  | C |  | 0.000 | 0.000 | 20.497 | 0.000 | 0.290 |

Feed Line Center of Pressure

| Section | Elevation | $C P_{X}$ | $C P_{Z}$ | $C P_{X}$ <br> Ice <br> in | $C P_{Z}$ <br> Ice <br> in |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | in | in | -0.942 |  |
| L1 | $148.000-116.500$ | 0.397 | -0.863 | 0.193 | -1.212 |
| L2 | $116.500-98.500$ | 0.538 | -1.134 | 0.354 | -0.766 |
| L3 | $98.500-80.250$ | 0.318 | -0.670 | 0.227 | -0.795 |
| L4 | $80.250-70.500$ | 0.327 | -0.690 | 0.235 | -0.753 |
| L5 | $70.500-39.750$ | 0.288 | -0.622 | 0.198 | -0.780 |
| L6 | $39.750-31.750$ | 0.267 | -0.645 | 0.067 | -0.802 |
| L7 | $31.750-17.750$ | 0.274 | -0.662 | 0.085 | -1.198 |
| L8 | $17.750-14.250$ | 0.227 | -1.095 | 0.078 | -1.092 |
| L9 | $14.250-0.000$ | 0.984 | -0.857 | 0.699 |  |



## Shielding Factor Ka

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{gathered} \hline K_{a} \\ \text { Ice } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 3 | LDF7-50A(1-5/8) | $\begin{array}{r} 116.50- \\ 138.00 \end{array}$ | 1.0000 | 1.0000 |
| L1 | 32 | Safety Line 3/8 | $116.50-$ 148.00 | 1.0000 | 1.0000 |
| L3 | 3 | LDF7-50A(1-5/8) | 80.25-98.50 | 1.0000 | 1.0000 |
| L3 | 25 | CCI 6" x 1" Plate | 80.25-98.50 | 1.0000 | 1.0000 |
| L3 | 26 | CCI 6" x 1" Plate | 80.25-98.50 | 1.0000 | 1.0000 |
| L3 | 27 | CCI 6" x 1" Plate | 80.25-98.50 | 1.0000 | 1.0000 |
| L3 | 32 | Safety Line 3/8 | 80.25-98.50 | 1.0000 | 1.0000 |
| L5 | 3 | LDF7-50A(1-5/8) | 39.75-70.50 | 1.0000 | 1.0000 |
| L5 | 14 | LDF4-50A(1/2) | 39.75-45.00 | 1.0000 | 1.0000 |
| L5 | 21 | CCI $8.5{ }^{\prime \prime}$ x $1.25{ }^{\prime \prime}$ Plate | 39.75-70.50 | 1.0000 | 1.0000 |
| L5 | 22 | CCI $8.5{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 39.75-70.50 | 1.0000 | 1.0000 |
| L5 | 23 | CCI $8.5{ }^{\prime \prime}$ x $1.25{ }^{\prime \prime}$ Plate | 39.75-70.50 | 1.0000 | 1.0000 |
| L5 | 32 | Safety Line 3/8 | 39.75-70.50 | 1.0000 | 1.0000 |
| L7 | 3 | LDF7-50A(1-5/8) | 17.75-31.75 | 1.0000 | 1.0000 |
| L7 | 14 | LDF4-50A(1/2) | 17.75-31.75 | 1.0000 | 1.0000 |
| L7 | 21 | CCI $8.5{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 17.75-31.75 | 1.0000 | 1.0000 |
| L7 | 22 | CCI $8.55^{\prime \prime}$ x $1.25{ }^{\prime \prime}$ Plate | 17.75-31.75 | 1.0000 | 1.0000 |
| L7 | 23 | CCI $8.5{ }^{\prime \prime}$ x 1.25" Plate | 17.75-31.75 | 1.0000 | 1.0000 |
| L7 | 32 | Safety Line 3/8 | 17.75-31.75 | 1.0000 | 1.0000 |
| L8 | 3 | LDF7-50A(1-5/8) | 14.25-17.75 | 1.0000 | 1.0000 |
| L8 | 14 | LDF4-50A(1/2) | 14.25-17.75 | 1.0000 | 1.0000 |
| L8 | 21 | CCI $8.5{ }^{\prime \prime}$ x $1.25{ }^{\prime \prime}$ Plate | 14.25-17.75 | 1.0000 | 1.0000 |
| L8 | 22 | CCI $8.5{ }^{\prime \prime}$ x $1.25{ }^{\prime \prime}$ Plate | 14.25-17.75 | 1.0000 | 1.0000 |
| L8 | 23 | CCI $8.5{ }^{\prime \prime}$ x $1.25{ }^{\prime \prime}$ Plate | 14.25-17.75 | 1.0000 | 1.0000 |
| L8 | 29 | CCI 6.5" x $1.25{ }^{\prime \prime}$ Plate | 14.25-17.75 | 1.0000 | 1.0000 |
| L8 | 30 | CCI $6.5{ }^{\prime \prime}$ x $1.25{ }^{\prime \prime}$ Plate | 14.25-17.75 | 1.0000 | 1.0000 |
| L8 | 32 | Safety Line 3/8 | 14.25-17.75 | 1.0000 | 1.0000 |
| L9 | 3 | LDF7-50A(1-5/8) | 0.00-14.25 | 1.0000 | 1.0000 |
| L9 | 14 | LDF4-50A(1/2) | 0.00-14.25 | 1.0000 | 1.0000 |
| L9 | 18 | CCI $8.5{ }^{\prime \prime}$ x $1.25{ }^{\prime \prime}$ Plate | 0.00-14.25 | 1.0000 | 1.0000 |
| L9 | 19 | CCI $8.55^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 0.00-14.25 | 1.0000 | 1.0000 |
| L9 | 29 | CCI $6.55^{\prime \prime}$ x $1.25{ }^{\prime \prime}$ Plate | 0.00-14.25 | 1.0000 | 1.0000 |
| L9 | 30 | CCI 6.5" x 1.25" Plate | 0.00-14.25 | 1.0000 | 1.0000 |
| L9 | 32 | Safety Line 3/8 | 0.00-14.25 | 1.0000 | 1.0000 |

## Discrete Tower Loads

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> $f t$ <br> $f t$ | Azimuth Adjustment | Placement |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Side <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Top Hat | C | None |  | 0.000 | 149.500 | No Ice | 3.000 | 3.000 | 0.081 |





\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& Azimuth Adjustment \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& | $C_{A} A_{A}$ |
| :--- |
| Side |
| $f t^{2}$ | \& Weight <br>


\hline \multirow{4}{*}{| (2) 6' x 2" Mount Pipe |
| :--- |
| (E) |} \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& 1.000 \& \multirow{4}{*}{0.000} \& \multirow{4}{*}{148.000} \& 1" Ice \& 2.294 \& 2.294 \& 0.048 <br>

\hline \& \& \& 4.000 \& \& \& No Ice \& 1.425 \& 1.425 \& 0.022 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.925 \& 1.925 \& 0.033 <br>
\hline \& \& \& 1.000 \& \& \& 1" Ice \& 2.294 \& 2.294 \& 0.048 <br>
\hline \multirow[t]{3}{*}{Platform Mount [LP 712-1] (E-12'/TIA)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{None} \& \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{148.000} \& No Ice \& 24.530 \& 24.530 \& 1.335 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 29.940 \& 29.940 \& 1.646 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 35.350 \& 35.350 \& 1.956 <br>
\hline **/>** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{BXA-70063-6CF-2 w/ Mount Pipe (E)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 7.806 \& 5.801 \& 0.042 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 8.357 \& 6.953 \& 0.103 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 8.872 \& 7.819 \& 0.171 <br>
\hline \multirow[t]{3}{*}{BXA-70063-6CF-2 w/ Mount Pipe (E)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 7.806 \& 5.801 \& 0.042 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 8.357 \& 6.953 \& 0.103 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.872 \& 7.819 \& 0.171 <br>
\hline \multirow[t]{3}{*}{BXA-70063-6CF-2 w/ Mount Pipe (E)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 7.806 \& 5.801 \& 0.042 <br>
\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 8.357 \& 6.953 \& 0.103 <br>
\hline \& \& \& 0.000 \& \& \& 1 " Ice \& 8.872 \& 7.819 \& 0.171 <br>

\hline \multirow[t]{3}{*}{| BXA-171085-8BF-EDIN-2 w/ Mount Pipe |
| :--- |
| (E) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 3.179 \& 3.353 \& 0.029 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.555 \& 3.971 \& 0.061 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.930 \& 4.595 \& 0.099 <br>
\hline \multirow[t]{3}{*}{BXA-171085-8BF-EDIN-2 w/ Mount Pipe (E)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 3.179 \& 3.353 \& 0.029 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.555 \& 3.971 \& 0.061 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 3.930 \& 4.595 \& 0.099 <br>

\hline \multirow[t]{3}{*}{| BXA-171063-8BF-2 w/ Mount Pipe |
| :--- |
| (E) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 3.179 \& 3.353 \& 0.029 <br>

\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 3.555 \& 3.971 \& 0.061 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 3.930 \& 4.595 \& 0.099 <br>
\hline \multirow[t]{3}{*}{(2) LPA-80063/6CF w/ Mount Pipe (E)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 9.831 \& 10.215 \& 0.052 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 10.400 \& 11.384 \& 0.145 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 10.933 \& 12.269 \& 0.246 <br>
\hline \multirow[t]{2}{*}{(2) LPA-80080/6CF w/ Mount Pipe} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 4.564 \& 10.259 \& 0.046 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 5.105 \& 11.427 \& 0.113 <br>
\hline (E) \& \& \& 0.000 \& \& \& 1 " Ice \& 5.612 \& 12.312 \& 0.187 <br>
\hline \multirow[t]{3}{*}{(2) LPA-80080/6CF w/ Mount Pipe (E)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 4.564 \& 10.259 \& 0.046 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 5.105 \& 11.427 \& 0.113 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 5.612 \& 12.312 \& 0.187 <br>

\hline \multirow[t]{3}{*}{| Platform Mount [LP 712-1] |
| :--- |
| (E) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{None} \& \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{138.000} \& No Ice \& 24.530 \& 24.530 \& 1.335 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 29.940 \& 29.940 \& 1.646 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 35.350 \& 35.350 \& 1.956 <br>
\hline **/>** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{2}{*}{HPA-65R-BUU-H8 w/
Mount Pipe} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 13.213 \& 9.582 \& 0.100 <br>
\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 13.899 \& 11.052 \& 0.196 <br>
\hline (AT\&T--P) \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 14.587 \& 12.496 \& 0.303 <br>
\hline \multirow[t]{2}{*}{HPA-65R-BUU-H8 w/ Mount Pipe} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 13.213 \& 9.582 \& 0.100 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 13.899 \& 11.052 \& 0.196 <br>
\hline (P) \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 14.587 \& 12.496 \& 0.303 <br>
\hline \multirow[t]{2}{*}{HPA-65R-BUU-H8 w/ Mount Pipe} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 13.213 \& 9.582 \& 0.100 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 13.899 \& 11.052 \& 0.196 <br>
\hline (P) \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 14.587 \& 12.496 \& 0.303 <br>

\hline \multirow[t]{3}{*}{| (3) RRU-11 |
| :--- |
| (P) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 1.639 \& 1.262 \& 0.044 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.802 \& 1.410 \& 0.060 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 1.972 \& 1.566 \& 0.078 <br>

\hline \multirow[t]{3}{*}{| (3) RRU-11 |
| :--- |
| (P) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 1.639 \& 1.262 \& 0.044 <br>

\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 1.802 \& 1.410 \& 0.060 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 1.972 \& 1.566 \& 0.078 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { (3) RRU-11 } \\
& \text { (P) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 1.639 \& 1.262 \& 0.044 <br>

\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 1.802 \& 1.410 \& 0.060 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 1.972 \& 1.566 \& 0.078 <br>
\hline
\end{tabular}



\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
ft \\
ft \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$ Side

$$
f t^{2}
$$ \& Weight <br>

\hline \multirow[t]{3}{*}{| (2) DC6-48-60-18-8F |
| :--- |
| (P) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 0.917 \& 0.917 \& 0.019 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.458 \& 1.458 \& 0.037 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.643 \& 1.643 \& 0.057 <br>

\hline \multirow[t]{4}{*}{| (4) HPA-65R-BUU-H8 w/ Mount Pipe (AT\&T--SLA) |
| :--- |
| (4) HPA-65R-BUU-H8 w/ |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 13.213 \& 9.582 \& 0.100 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 13.899 \& 11.052 \& 0.196 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 14.587 \& 12.496 \& 0.303 <br>
\hline \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 13.213 \& 9.582 \& 0.100 <br>
\hline \multirow[t]{2}{*}{(4) HPA-65R-BUU-H8 w/ Mount Pipe (SLA)} \& \& \& 0.000 \& \& \& 1/2" Ice \& 13.899 \& 11.052 \& 0.196 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 14.587 \& 12.496 \& 0.303 <br>
\hline (4) HPA-65R-BUU-H8 w/ \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 13.213 \& 9.582 \& 0.100 <br>
\hline Mount Pipe \& \& \& 0.000 \& \& \& 1/2" Ice \& 13.899 \& 11.052 \& 0.196 <br>
\hline (SLA) \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 14.587 \& 12.496 \& 0.303 <br>
\hline \multirow[t]{3}{*}{RRUS E2 B29 (SLA)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 3.145 \& 1.285 \& 0.060 <br>
\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 3.365 \& 1.438 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 3.592 \& 1.600 \& 0.110 <br>
\hline \multirow[t]{3}{*}{RRUS E2 B29 (SLA)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 3.145 \& 1.285 \& 0.060 <br>
\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 3.365 \& 1.438 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 3.592 \& 1.600 \& 0.110 <br>
\hline \multirow[t]{3}{*}{RRUS E2 B29 (SLA)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 3.145 \& 1.285 \& 0.060 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.365 \& 1.438 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 3.592 \& 1.600 \& 0.110 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { (3) RRU-11 } \\
& \text { (SLA) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 1.639 \& 1.262 \& 0.044 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.802 \& 1.410 \& 0.060 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.972 \& 1.566 \& 0.078 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { (3) RRU-11 } \\
& \text { (SLA) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 1.639 \& 1.262 \& 0.044 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.802 \& 1.410 \& 0.060 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 1.972 \& 1.566 \& 0.078 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { (3) RRU-11 } \\
& \text { (SLA) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 1.639 \& 1.262 \& 0.044 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.802 \& 1.410 \& 0.060 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.972 \& 1.566 \& 0.078 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { RRUS-32 B30 } \\
& \text { (SLA) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 3.314 \& 2.424 \& 0.077 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.558 \& 2.638 \& 0.105 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.809 \& 2.860 \& 0.136 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { RRUS-32 B30 } \\
& \text { (SLA) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 3.314 \& 2.424 \& 0.077 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.558 \& 2.638 \& 0.105 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 3.809 \& 2.860 \& 0.136 <br>

\hline \multirow[t]{3}{*}{$$
\begin{gathered}
\text { RRUS-32 B30 } \\
\text { (SLA) }
\end{gathered}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 3.314 \& 2.424 \& 0.077 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.558 \& 2.638 \& 0.105 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.809 \& 2.860 \& 0.136 <br>

\hline \multirow[t]{3}{*}{$$
\begin{gathered}
\text { DC6-48-60-18-8F } \\
\text { (SLA) }
\end{gathered}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 0.917 \& 0.917 \& 0.019 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.458 \& 1.458 \& 0.037 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.643 \& 1.643 \& 0.057 <br>
\hline \multirow[t]{3}{*}{(2)

$$
\begin{aligned}
& \text { DC6-48-60-18-8F } \\
& \text { (SLA) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 0.917 \& 0.917 \& 0.019 <br>

\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 1.458 \& 1.458 \& 0.037 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 1.643 \& 1.643 \& 0.057 <br>

\hline \multirow[t]{3}{*}{$$
\begin{gathered}
\text { DC6-48-60-18-8F } \\
\text { (SLA) }
\end{gathered}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 0.917 \& 0.917 \& 0.019 <br>

\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 1.458 \& 1.458 \& 0.037 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.643 \& 1.643 \& 0.057 <br>
\hline \multirow[t]{3}{*}{(2) RRUS 12-B2 (SLA)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 3.143 \& 1.282 \& 0.058 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.363 \& 1.434 \& 0.081 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.590 \& 1.595 \& 0.108 <br>
\hline \multirow[t]{3}{*}{(2) RRUS 12-B2 (SLA)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 3.143 \& 1.282 \& 0.058 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.363 \& 1.434 \& 0.081 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.590 \& 1.595 \& 0.108 <br>
\hline \multirow[t]{3}{*}{(2) RRUS 12-B2 (SLA)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& \multirow[t]{3}{*}{0.000} \& \multirow[t]{3}{*}{128.000} \& No Ice \& 3.143 \& 1.282 \& 0.058 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.363 \& 1.434 \& 0.081 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.590 \& 1.595 \& 0.108 <br>
\hline
\end{tabular}



\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face \\
or Leg
\end{tabular} \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
ft \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$ Side $f t^{2}$ \& Weight <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { (2) RRUS A2 } \\
& \text { (SLA) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& 0.000 \& 128.000 \& No Ice \& 2.066 \& 0.498 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.245 \& 0.607 \& 0.035 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.431 \& 0.724 \& 0.050 <br>
\hline \multirow[t]{3}{*}{(2) RRUS A2 (SLA)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& 0.000 \& 128.000 \& No Ice \& 2.066 \& 0.498 \& 0.022 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.245 \& 0.607 \& 0.035 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 2.431 \& 0.724 \& 0.050 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { (2) RRUS A2 } \\
& \text { (SLA) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& 0.000 \& 128.000 \& No Ice \& 2.066 \& 0.498 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.245 \& 0.607 \& 0.035 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 2.431 \& 0.724 \& 0.050 <br>

\hline \multirow[t]{3}{*}{$$
\begin{gathered}
\text { KRF } 102361 / 1 \\
\text { (SLA) }
\end{gathered}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& 0.000 \& 128.000 \& No Ice \& 1.939 \& 0.552 \& 0.026 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.112 \& 0.655 \& 0.039 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 2.294 \& 0.766 \& 0.055 <br>
\hline \multirow[t]{3}{*}{KRF 102 361/1 (SLA)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& 0.000 \& 128.000 \& No Ice \& 1.939 \& 0.552 \& 0.026 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.112 \& 0.655 \& 0.039 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 2.294 \& 0.766 \& 0.055 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { KRF } 102 \text { 361/1 } \\
& \text { (SLA) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.000 \& 0.000 \& 128.000 \& No Ice \& 1.939 \& 0.552 \& 0.026 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.112 \& 0.655 \& 0.039 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 2.294 \& 0.766 \& 0.055 <br>

\hline \multirow[t]{3}{*}{| Sector Mount [SM 406-3] |
| :--- |
| (P) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{None} \& \& 0.000 \& 128.000 \& No Ice \& 19.830 \& 19.830 \& 0.923 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 29.410 \& 29.410 \& 1.326 <br>
\hline \& \& \& \& \& \& 1 I' Ice \& 38.990 \& 38.990 \& 1.729 <br>
\hline **/>** \& \& \& \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{| PD1109E |
| :--- |
| (E) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.000 \& 0.000 \& 79.000 \& No Ice \& 2.854 \& 2.854 \& 0.017 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.924 \& 3.924 \& 0.038 <br>
\hline \& \& \& 5.000 \& \& \& $1{ }^{1 \prime}$ Ice \& 5.010 \& 5.010 \& 0.066 <br>

\hline \multirow[t]{3}{*}{| Side Arm Mount [SO 701-1] |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 1.500 \& 0.000 \& 79.000 \& No Ice \& 0.850 \& 1.670 \& 0.065 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.140 \& 2.340 \& 0.079 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.430 \& 3.010 \& 0.093 <br>
\hline \multicolumn{8}{|l|}{**/>** 30.010} \& \& <br>

\hline \multirow[t]{3}{*}{| GPS A |
| :--- |
| (E) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.000 \& 0.000 \& 45.000 \& No Ice \& 0.255 \& 0.255 \& 0.001 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 0.320 \& 0.320 \& 0.005 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 0.393 \& 0.393 \& 0.010 <br>

\hline \multirow[t]{3}{*}{| Side Arm Mount [SO 701-1] |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 1.500 \& 0.000 \& 45.000 \& No Ice \& 0.850 \& 1.670 \& 0.065 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.140 \& 2.340 \& 0.079 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.430 \& 3.010 \& 0.093 <br>
\hline **/>** \& \& \& \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{$$
\begin{gathered}
\text { GPS_A } \\
(\mathrm{E}-\mathrm{CL} / \mathrm{TIA})
\end{gathered}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.000 \& 0.000 \& 13.000 \& No Ice \& 0.255 \& 0.255 \& 0.001 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 0.320 \& 0.320 \& 0.005 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 0.393 \& 0.393 \& 0.010 <br>
\hline \multirow[t]{3}{*}{Side Arm Mount [SO 701-1] (E-Mount Ht./TIA)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 1.500 \& 0.000 \& 13.000 \& No Ice \& 0.850 \& 1.670 \& 0.065 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.140 \& 2.340 \& 0.079 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 1.430 \& 3.010 \& 0.093 <br>
\hline
\end{tabular}

## Load Combinations

| Comb. |  | Description |
| :---: | :--- | :--- |
| No. |  |  |
| 1 | Dead Only |  |
| 2 | 1.2 Dead +1.6 Wind 0 deg - No Ice |  |
| 3 | 0.9 Dead+1.6 Wind 0 deg - No Ice |  |
| 4 | 1.2 Dead+1.6 Wind 30 deg - No Ice |  |



| Comb. No. | Description |
| :---: | :---: |
| 5 | 0.9 Dead+1.6 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.6 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.6 Wind 60 deg - No Ice |
| 8 | 1.2 Dead+1.6 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.6 Wind 90 deg - No Ice |
| 10 | 1.2 Dead+1.6 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.6 Wind 120 deg - No Ice |
| 12 | 1.2 Dead+1.6 Wind 150 deg - No Ice |
| 13 | 0.9 Dead+1.6 Wind 150 deg - No Ice |
| 14 | 1.2 Dead+1.6 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.6 Wind 180 deg - No Ice |
| 16 | 1.2 Dead+1.6 Wind 210 deg - No Ice |
| 17 | 0.9 Dead+1.6 Wind 210 deg - No Ice |
| 18 | 1.2 Dead+1.6 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.6 Wind 240 deg - No Ice |
| 20 | 1.2 Dead+1.6 Wind 270 deg - No Ice |
| 21 | 0.9 Dead+1.6 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.6 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.6 Wind 300 deg - No Ice |
| 24 | 1.2 Dead+1.6 Wind 330 deg - No Ice |
| 25 | 0.9 Dead+1.6 Wind 330 deg - No Ice |
| 26 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 27 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |
| 28 | 1.2 Dead+1.0 Wind $30 \mathrm{deg}+$ 1.0 Ice+1.0 Temp |
| 29 | 1.2 Dead+1.0 Wind $60 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 30 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp |
| 32 | 1.2 Dead+1.0 Wind $150 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 33 | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp |
| 34 | 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp |
| 35 | 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp |
| 36 | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp |
| 37 | 1.2 Dead+1.0 Wind $300 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 38 | 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp |
| 39 | Dead+Wind 0 deg - Service |
| 40 | Dead+Wind 30 deg - Service |
| 41 | Dead+Wind 60 deg - Service |
| 42 | Dead+Wind 90 deg - Service |
| 43 | Dead+Wind 120 deg - Service |
| 44 | Dead+Wind 150 deg - Service |
| 45 | Dead+Wind 180 deg - Service |
| 46 | Dead+Wind 210 deg - Service |
| 47 | Dead+Wind 240 deg - Service |
| 48 | Dead+Wind 270 deg - Service |
| 49 | Dead+Wind 300 deg - Service |
| 50 | Dead+Wind 330 deg - Service |

## Maximum Member Forces

| Section | Elevation | Component <br> Type | $f t$ |  | Condition | Gov. <br> Load | Axial |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Major Axis <br> Moment <br> kip-ft | Minor Axis <br> Moment <br> kip-ft |  |  |
| L1 | $148-116.5$ | Pole | Max Tension | 26 | 0.000 | 0.000 | -0.000 |
|  |  |  | Max. Compression | 26 | -32.760 | -1.511 | 0.991 |
|  |  |  | Max. Mx | 8 | -11.647 | -252.029 | 0.042 |
|  |  |  | Max. My | 2 | -11.599 | -0.347 | 257.981 |
|  |  |  | Max. Vy | 8 | 17.439 | -252.029 | 0.042 |
|  |  |  | Max. Vx | 2 | -17.795 | -0.347 | 257.981 |
|  |  |  | Max. Torque | 5 |  | -0.445 |  |


| tnxTower <br> B+T Group <br> 1717 S.Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{array}{\|l} \begin{array}{l} \text { Job } \\ 89028.006 .01 ~-~ L O N G ~ E D D Y ~ W R I G H T ~ P R O P E R T Y, ~ C T ~(B U \# ~ \\ 876373) \end{array} \\ \hline \end{array}$ |  | $\begin{aligned} & \text { Page } \\ & \\ & \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | Date $15: 42: 42 \text { 03/23/17 }$ |
|  | Client | Crown Castle | Designed by Pavan Pai |


| Section No. | Elevation $f t$ | Component Type | Condition | Gov. Load Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L2 | 116.5-98.5 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -38.087 | -1.831 | 1.844 |
|  |  |  | Max. Mx | 8 | -14.926 | -646.215 | 0.197 |
|  |  |  | Max. My | 2 | -14.888 | -0.429 | 659.990 |
|  |  |  | Max. Vy | 8 | 18.773 | -646.215 | 0.197 |
|  |  |  | Max. Vx | 2 | -19.129 | -0.429 | 659.990 |
|  |  |  | Max. Torque | 5 |  |  | -0.445 |
| L3 | 98.5-80.25 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -42.869 | -2.044 | 2.434 |
|  |  |  | Max. Mx | 8 | -17.936 | -910.422 | 0.314 |
|  |  |  | Max. My | 2 | -17.904 | -0.485 | 929.142 |
|  |  |  | Max. Vy | 8 | 19.665 | -910.422 | 0.314 |
|  |  |  | Max. Vx | 2 | -20.021 | -0.485 | 929.142 |
|  |  |  | Max. Torque | 5 |  |  | -0.445 |
| L4 | 80.25-70.5 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -49.763 | -2.266 | 3.954 |
|  |  |  | Max. Mx | 8 | -22.471 | -1199.785 | 0.735 |
|  |  |  | Max. My | 2 | -22.445 | -0.543 | 1223.724 |
|  |  |  | Max. Vy | 8 | 20.798 | -1199.785 | 0.735 |
|  |  |  | Max. Vx | 2 | -21.126 | -0.543 | 1223.724 |
|  |  |  | Max. Torque | 10 |  |  | 0.522 |
| L5 | 70.5-39.75 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -61.560 | -2.606 | 5.042 |
|  |  |  | Max. Mx | 8 | -30.651 | -1750.176 | 0.977 |
|  |  |  | Max. My | 2 | -30.635 | -0.653 | 1782.567 |
|  |  |  | Max. Vy | 8 | 22.350 | -1750.176 | 0.977 |
|  |  |  | Max. Vx | 2 | -22.675 | -0.653 | 1782.567 |
|  |  |  | Max. Torque | 10 |  |  | 0.521 |
| L6 | 39.75-31.75 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -70.498 | -2.320 | 5.381 |
|  |  |  | Max. Mx | 8 | -37.167 | -2052.173 | 0.844 |
|  |  |  | Max. My | 2 | -37.154 | -0.355 | 2089.189 |
|  |  |  | Max. Vy | 8 | 23.173 | -2052.173 | $0.844$ |
|  |  |  | Max. Vx | 2 | -23.509 | $-0.355$ | 2089.189 |
|  |  |  | Max. Torque | 11 |  |  | 0.351 |
| L7 | 31.75-17.75 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -77.786 | -2.430 | 5.991 |
|  |  |  | Max. Mx | 8 | -42.520 | -2381.016 | 0.844 |
|  |  |  | Max. My | 2 | -42.513 | -0.271 | 2422.784 |
|  |  |  | Max. Vy | 8 | 23.815 | -2381.016 | 0.844 |
|  |  |  | Max. Vx | 2 | -24.147 | -0.271 | 2422.784 |
|  |  |  | Max. Torque | 11 |  |  | 0.351 |
| L8 | 17.75-14.25 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -79.937 | -2.460 | 6.220 |
|  |  |  | Max. Mx | 8 | -44.120 | -2464.640 | 0.845 |
|  |  |  | Max. My | 2 | -44.114 | -0.250 | 2507.588 |
|  |  |  | Max. Vy | 8 | 23.985 | -2464.640 | 0.845 |
|  |  |  | Max. Vx | 2 | -24.316 | -0.250 | 2507.588 |
|  |  |  | Max. Torque | 11 |  |  | 0.351 |
| L9 | 14.25-0 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -87.931 | -2.889 | 7.410 |
|  |  |  | Max. Mx | 8 | -50.195 | -2811.416 | 1.122 |
|  |  |  | Max. My | 2 | -50.195 | -0.168 | 2859.116 |
|  |  |  | Max. Vy | 8 | 24.655 | -2811.416 | 1.122 |
|  |  |  | Max. Vx | 2 | -24.959 | -0.168 | 2859.116 |
|  |  |  | Max. Torque | 11 |  |  | 0.507 |



## Maximum Reactions

| Location | Condition | Gov. Load Comb. | Vertical K | $\begin{gathered} \text { Horizontal, } X \\ K \end{gathered}$ | $\begin{gathered} \text { Horizontal, Z } \\ K \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pole | Max. Vert | 26 | 87.931 | -0.000 | 0.000 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 20 | 50.202 | 24.642 | 0.010 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 2 | 50.202 | 0.010 | 24.946 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 2 | 2859.116 | 0.010 | 24.946 |
|  | Max. $\mathrm{M}_{\mathrm{z}}$ | 8 | 2811.416 | -24.642 | -0.010 |
|  | Max. Torsion | 11 | 0.507 | -21.346 | -12.482 |
|  | Min. Vert | 19 | 37.651 | 21.335 | -12.464 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 8 | 50.202 | -24.642 | -0.010 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 14 | 50.202 | -0.010 | -24.946 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 14 | -2855.932 | -0.010 | -24.946 |
|  | Min. $\mathrm{M}_{\mathrm{z}}$ | 20 | -2810.135 | 24.642 | 0.010 |
|  | Min. Torsion | 23 | -0.505 | 21.346 | 12.482 |

## Tower Mast Reaction Summary

| Load Combination | Vertical K | Shear $_{x}$ K | Shear $_{z}$ K | Overturning <br> Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | $\begin{gathered} \text { Torque } \\ \text { kip-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 41.835 | 0.000 | 0.000 | -1.288 | -0.507 | 0.000 |
| 1.2 Dead+1.6 Wind 0 deg - No | 50.202 | -0.010 | -24.946 | -2859.116 | -0.168 | 0.206 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 0 deg - No | 37.651 | 0.021 | -24.946 | -2833.060 | -0.019 | 0.209 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 30 deg - No | 50.202 | 12.312 | -21.598 | -2476.071 | -1405.588 | -0.054 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 30 deg - No | 37.651 | 12.312 | -21.598 | -2453.447 | -1392.828 | -0.050 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 60 deg - No | 50.202 | 21.335 | -12.464 | -1429.985 | -2434.593 | -0.299 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 60 deg - No | 37.651 | 21.335 | -12.464 | -1416.751 | -2412.612 | -0.297 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 90 deg - No | 50.202 | 24.642 | 0.010 | -1.122 | -2811.416 | -0.465 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 90 deg - No | 37.651 | 24.642 | 0.010 | -0.716 | -2786.063 | -0.464 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 120 deg - | 50.202 | 21.346 | 12.482 | 1427.616 | -2435.066 | -0.506 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 120 deg - | 37.651 | 21.346 | 12.482 | 1415.194 | -2413.083 | -0.507 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 150 deg - | 50.202 | 12.330 | 21.609 | 2473.358 | -1406.406 | -0.411 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 150 deg - | 37.651 | 12.330 | 21.609 | 2451.547 | -1393.644 | -0.413 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 180 deg - | 50.202 | 0.010 | 24.946 | 2855.932 | -1.112 | -0.206 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 180 deg - | 37.651 | 0.010 | 24.946 | 2830.690 | -0.944 | -0.209 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 210 deg - | 50.202 | -12.312 | 21.598 | 2472.886 | 1404.309 | 0.055 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 210 deg - | 37.651 | -12.312 | 21.598 | 2451.077 | 1391.882 | 0.052 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 240 deg - | 50.202 | -21.335 | 12.464 | 1426.798 | 2433.313 | 0.301 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 240 deg - | 37.651 | -21.335 | 12.464 | 1414.379 | 2411.666 | 0.298 |


| tnxTower | Job <br> 89028.006.01 - LONG EDDY WRIGHT PROPERTY, CT (BU\# 876373) |  | $\begin{aligned} & \text { Page } \\ & \\ & \\ & 14 \text { of } 19 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| B+T Group <br> 1717 S.Boulder, Suite 300 | Project |  | Date $15: 42: 42 \text { 03/23/17 }$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by Pavan Pai |


| Load Combination | Vertical <br> K | Shear $_{x}$ K | Shear <br> K | Overturning <br> Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 270 deg - | 50.202 | -24.642 | -0.010 | -2.066 | 2810.135 | 0.465 |
| No Ice <br> 0.9 Dead+1.6 Wind 270 deg - | 37.651 | -24.642 |  |  | 2785.115 |  |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 300 deg - | 50.202 | -21.346 | -12.482 | -1430.803 | 2433.784 | 0.505 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 300 deg - | 37.651 | -21.346 | -12.482 | -1417.565 | 2412.134 | 0.505 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.6 Wind 330 deg - No Ice | 50.202 | -12.330 | -21.609 | -2476.543 | 1405.124 | 0.410 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.6 Wind 330 deg - | 37.651 | -12.330 | -21.609 | -2453.917 | 1392.696 | 0.412 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Ice+1.0 Temp | 87.931 | 0.000 | -0.000 | -7.410 | -2.889 | -0.000 |
| 1.2 Dead+1.0 Wind 0 deg +1.0 | 87.931 | -0.003 | -4.877 | -570.548 | -2.832 | 0.045 |
| Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 30 deg+1.0 | 87.931 | 2.421 | -4.222 | -495.059 | -281.599 | -0.022 |
| Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind $60 \mathrm{deg}+1.0$ | 87.931 | 4.196 | -2.436 | -288.956 | -485.707 | -0.082 |
| Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 90 deg+1.0 | 87.931 | 4.847 | 0.003 | -7.463 | -560.465 | -0.121 |
| Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp | 87.931 | 4.199 | 2.441 | 273.994 | -485.842 | -0.127 |
| 1.2 Dead+1.0 Wind 150 | 87.931 | 2.426 | 4.225 | 479.998 | -281.833 | -0.099 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 180 | 87.931 | 0.003 | 4.877 | 555.352 | -3.102 | -0.045 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 210 | 87.931 | -2.421 | 4.222 | 479.864 | 275.666 | 0.021 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 240 | 87.931 | -4.196 | 2.436 | 273.760 | 479.774 | 0.082 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 270 | 87.931 | -4.847 | -0.003 | -7.733 | 554.532 | 0.121 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 300 | 87.931 | -4.199 | -2.441 | -289.190 | 479.909 | 0.127 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 330 | 87.931 | -2.426 | -4.225 | -495.195 | 275.899 | 0.099 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| Dead+Wind 0 deg - Service | 41.835 | -0.002 | -5.806 | -662.984 | -0.422 | 0.049 |
| Dead+Wind 30 deg - Service | 41.835 | 2.866 | -5.027 | -574.283 | -325.847 | -0.012 |
| Dead+Wind 60 deg - Service | 41.835 | 4.966 | -2.901 | -332.058 | -564.105 | -0.069 |
| Dead+Wind 90 deg - Service | 41.835 | 5.736 | 0.002 | -1.213 | -651.353 | -0.108 |
| Dead+Wind 120 deg - Service | 41.835 | 4.968 | 2.905 | 329.604 | -564.214 | -0.118 |
| Dead+Wind 150 deg - Service | 41.835 | 2.870 | 5.030 | 571.748 | -326.037 | -0.096 |
| Dead+Wind 180 deg - Service | 41.835 | 0.002 | 5.806 | 660.339 | -0.641 | -0.049 |
| Dead+Wind 210 deg - Service | 41.835 | -2.866 | 5.027 | 571.639 | 324.784 | 0.012 |
| Dead+Wind 240 deg - Service | 41.835 | -4.966 | 2.901 | 329.414 | 563.042 | 0.069 |
| Dead+Wind 270 deg - Service | 41.835 | -5.736 | -0.002 | -1.432 | 650.291 | 0.108 |
| Dead+Wind 300 deg - Service | 41.835 | -4.968 | -2.905 | -332.248 | 563.152 | 0.118 |
| Dead+Wind 330 deg - Service | 41.835 | -2.870 | -5.030 | -574.393 | 324.974 | 0.096 |

Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | $P Y$ | $P Z$ | $P X$ | $P Y$ | $P Z$ | \% Error |
| Comb. | $K$ | $K$ | $K$ | $K$ | $K$ | $K$ |  |
| 1 | 0.000 | -41.835 | 0.000 | 0.000 | 41.835 | 0.000 | $0.000 \%$ |
| 2 | -0.010 | -50.202 | -24.945 | 0.010 | 50.202 | 24.946 | $0.000 \%$ |



|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | PX | PY | PZ | PX | PY | PZ |  |
| Comb. | K | K | K | K | K | K |  |
| 3 | -0.010 | -37.651 | -24.945 | -0.021 | 37.651 | 24.946 | 0.068\% |
| 4 | 12.312 | -50.202 | -21.598 | -12.312 | 50.202 | 21.598 | 0.000\% |
| 5 | 12.312 | -37.651 | -21.598 | -12.312 | 37.651 | 21.598 | 0.000\% |
| 6 | 21.335 | -50.202 | -12.464 | -21.335 | 50.202 | 12.464 | 0.000\% |
| 7 | 21.335 | -37.651 | -12.464 | -21.335 | 37.651 | 12.464 | 0.000\% |
| 8 | 24.642 | -50.202 | 0.010 | -24.642 | 50.202 | -0.010 | 0.000\% |
| 9 | 24.642 | -37.651 | 0.010 | -24.642 | 37.651 | -0.010 | 0.000\% |
| 10 | 21.346 | -50.202 | 12.482 | -21.346 | 50.202 | -12.482 | 0.000\% |
| 11 | 21.346 | -37.651 | 12.482 | -21.346 | 37.651 | -12.482 | 0.000\% |
| 12 | 12.330 | -50.202 | 21.609 | -12.330 | 50.202 | -21.609 | 0.000\% |
| 13 | 12.330 | -37.651 | 21.609 | -12.330 | 37.651 | -21.609 | 0.000\% |
| 14 | 0.010 | -50.202 | 24.945 | -0.010 | 50.202 | -24.946 | 0.000\% |
| 15 | 0.010 | -37.651 | 24.945 | -0.010 | 37.651 | -24.946 | 0.000\% |
| 16 | -12.312 | -50.202 | 21.598 | 12.312 | 50.202 | -21.598 | 0.000\% |
| 17 | -12.312 | -37.651 | 21.598 | 12.312 | 37.651 | -21.598 | 0.000\% |
| 18 | -21.335 | -50.202 | 12.464 | 21.335 | 50.202 | -12.464 | 0.000\% |
| 19 | -21.335 | -37.651 | 12.464 | 21.335 | 37.651 | -12.464 | 0.000\% |
| 20 | -24.642 | -50.202 | -0.010 | 24.642 | 50.202 | 0.010 | 0.000\% |
| 21 | -24.642 | -37.651 | -0.010 | 24.642 | 37.651 | 0.010 | 0.000\% |
| 22 | -21.346 | -50.202 | -12.482 | 21.346 | 50.202 | 12.482 | 0.000\% |
| 23 | -21.346 | -37.651 | -12.482 | 21.346 | 37.651 | 12.482 | 0.000\% |
| 24 | -12.330 | -50.202 | -21.609 | 12.330 | 50.202 | 21.609 | 0.000\% |
| 25 | -12.330 | -37.651 | -21.609 | 12.330 | 37.651 | 21.609 | 0.000\% |
| 26 | 0.000 | -87.931 | 0.000 | -0.000 | 87.931 | 0.000 | 0.000\% |
| 27 | -0.003 | -87.931 | -4.876 | 0.003 | 87.931 | 4.877 | 0.000\% |
| 28 | 2.421 | -87.931 | -4.222 | -2.421 | 87.931 | 4.222 | 0.000\% |
| 29 | 4.196 | -87.931 | -2.436 | -4.196 | 87.931 | 2.436 | 0.000\% |
| 30 | 4.847 | -87.931 | 0.003 | -4.847 | 87.931 | -0.003 | 0.000\% |
| 31 | 4.199 | -87.931 | 2.441 | -4.199 | 87.931 | -2.441 | 0.000\% |
| 32 | 2.426 | -87.931 | 4.225 | -2.426 | 87.931 | -4.225 | 0.000\% |
| 33 | 0.003 | -87.931 | 4.876 | -0.003 | 87.931 | -4.877 | 0.000\% |
| 34 | -2.421 | -87.931 | 4.222 | 2.421 | 87.931 | -4.222 | 0.000\% |
| 35 | -4.196 | -87.931 | 2.436 | 4.196 | 87.931 | -2.436 | 0.000\% |
| 36 | -4.847 | -87.931 | -0.003 | 4.847 | 87.931 | 0.003 | 0.000\% |
| 37 | -4.199 | -87.931 | -2.441 | 4.199 | 87.931 | 2.441 | 0.000\% |
| 38 | -2.426 | -87.931 | -4.225 | 2.426 | 87.931 | 4.225 | 0.000\% |
| 39 | -0.002 | -41.835 | -5.806 | 0.002 | 41.835 | 5.806 | 0.000\% |
| 40 | 2.866 | -41.835 | -5.027 | -2.866 | 41.835 | 5.027 | 0.000\% |
| 41 | 4.966 | -41.835 | -2.901 | -4.966 | 41.835 | 2.901 | 0.000\% |
| 42 | 5.736 | -41.835 | 0.002 | -5.736 | 41.835 | -0.002 | 0.000\% |
| 43 | 4.968 | -41.835 | 2.905 | -4.968 | 41.835 | -2.905 | 0.000\% |
| 44 | 2.870 | -41.835 | 5.030 | -2.870 | 41.835 | -5.030 | 0.000\% |
| 45 | 0.002 | -41.835 | 5.806 | -0.002 | 41.835 | -5.806 | 0.000\% |
| 46 | -2.866 | -41.835 | 5.027 | 2.866 | 41.835 | -5.027 | 0.000\% |
| 47 | -4.966 | -41.835 | 2.901 | 4.966 | 41.835 | -2.901 | 0.000\% |
| 48 | -5.736 | -41.835 | -0.002 | 5.736 | 41.835 | 0.002 | 0.000\% |
| 49 | -4.968 | -41.835 | -2.905 | 4.968 | 41.835 | 2.905 | 0.000\% |
| 50 | -2.870 | -41.835 | -5.030 | 2.870 | 41.835 | 5.030 | 0.000\% |

## Non-Linear Convergence Results

| Load <br> Combination | Converged? | Number <br> of Cycles | Displacement <br> Tolerance | Force <br> Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 4 | 0.00000001 | 0.00000001 |
| 2 | Yes | 4 | 0.00000001 | 0.00043366 |
| 3 | Yes | 4 | 0.00000001 | 0.00031730 |


| tnxTower <br> B+T Group <br> 1717 S.Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{array}{\|l} \begin{array}{l} \text { Job } \\ 89028.006 .01 ~-~ L O N G ~ E D D Y ~ W R I G H T ~ P R O P E R T Y, ~ C T ~(B U \# ~ \\ 876373) \end{array} \\ \hline \end{array}$ |  | $\begin{array}{ll} \hline \text { Page } \\ & \\ & \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | Date $15: 42: 42 \text { 03/23/17 }$ |
|  | Client | Crown Castle | Designed by Pavan Pai |


| 4 | Yes | 5 | 0.00000001 | 0.00079841 |
| :---: | :---: | :---: | :---: | :---: |
| 5 | Yes | 5 | 0.00000001 | 0.00037024 |
| 6 | Yes | 5 | 0.00000001 | 0.00078828 |
| 7 | Yes | 5 | 0.00000001 | 0.00036582 |
| 8 | Yes | 4 | 0.00000001 | 0.00035762 |
| 9 | Yes | 4 | 0.00000001 | 0.00018818 |
| 10 | Yes | 5 | 0.00000001 | 0.00078296 |
| 11 | Yes | 5 | 0.00000001 | 0.00036344 |
| 12 | Yes | 5 | 0.00000001 | 0.00079958 |
| 13 | Yes | 5 | 0.00000001 | 0.00037101 |
| 14 | Yes | 4 | 0.00000001 | 0.00043782 |
| 15 | Yes | 4 | 0.00000001 | 0.00025066 |
| 16 | Yes | 5 | 0.00000001 | 0.00078717 |
| 17 | Yes | 5 | 0.00000001 | 0.00036502 |
| 18 | Yes | 5 | 0.00000001 | 0.00078769 |
| 19 | Yes | 5 | 0.00000001 | 0.00036605 |
| 20 | Yes | 4 | 0.00000001 | 0.00036007 |
| 21 | Yes | 4 | 0.00000001 | 0.00019020 |
| 22 | Yes | 5 | 0.00000001 | 0.00079337 |
| 23 | Yes | 5 | 0.00000001 | 0.00036856 |
| 24 | Yes | 5 | 0.00000001 | 0.00078635 |
| 25 | Yes | 5 | 0.00000001 | 0.00036438 |
| 26 | Yes | 4 | 0.00000001 | 0.00007774 |
| 27 | Yes | 5 | 0.00000001 | 0.00052012 |
| 28 | Yes | 5 | 0.00000001 | 0.00055675 |
| 29 | Yes | 5 | 0.00000001 | 0.00055319 |
| 30 | Yes | 5 | 0.00000001 | 0.00051132 |
| 31 | Yes | 5 | 0.00000001 | 0.00054205 |
| 32 | Yes | 5 | 0.00000001 | 0.00054236 |
| 33 | Yes | 5 | 0.00000001 | 0.00050513 |
| 34 | Yes | 5 | 0.00000001 | 0.00053536 |
| 35 | Yes | 5 | 0.00000001 | 0.00053336 |
| 36 | Yes | 5 | 0.00000001 | 0.00050221 |
| 37 | Yes | 5 | 0.00000001 | 0.00054469 |
| 38 | Yes | 5 | 0.00000001 | 0.00054991 |
| 39 | Yes | 4 | 0.00000001 | 0.00006861 |
| 40 | Yes | 4 | 0.00000001 | 0.00031988 |
| 41 | Yes | 4 | 0.00000001 | 0.00031133 |
| 42 | Yes | 4 | 0.00000001 | 0.00006590 |
| 43 | Yes | 4 | 0.00000001 | 0.00030492 |
| 44 | Yes | 4 | 0.00000001 | 0.00032079 |
| 45 | Yes | 4 | 0.00000001 | 0.00006840 |
| 46 | Yes | 4 | 0.00000001 | 0.00030614 |
| 47 | Yes | 4 | 0.00000001 | 0.00030974 |
| 48 | Yes | 4 | 0.00000001 | 0.00006572 |
| 49 | Yes | 4 | 0.00000001 | 0.00031661 |
| 50 | Yes | 4 | 0.00000001 | 0.00030565 |

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | o |
| :---: | :---: | :---: | :---: | :---: | :---: |


| tnxTower | Job <br> 89028.006.01 - LONG EDDY WRIGHT PROPERTY, CT (BU\# 876373) |  | $\begin{aligned} & \text { Page } \\ & \\ & \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| B+T Group <br> 1717 S.Boulder, Suite 300 | Project |  | Date $15: 42: 42 \text { 03/23/17 }$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by Pavan Pai |


| Section <br> No. | Elevation | Horz. <br> Deflection | Gov. <br> Load | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | in | Comb. | $\circ$ | $\circ$ |
| L8 | $17.75-14.25$ | 0.235 | 39 | 0.124 | 0.000 |
| L9 | $14.25-0$ | 0.152 | 39 | 0.102 | 0.000 |
|  |  |  |  |  |  |



## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | $\circ$ |
| :---: | :---: | :---: | :---: | :---: | :---: |

## Critical Deflections and Radius of Curvature - Design Wind

| Elevation | Appurtenance | Gov. <br> Load | Deflection | Tilt | Twist | Radius of <br> Curvature |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  | Comb. | in | $\circ$ | $\circ$ | ot |
| 149.500 |  | Top Hat | 2 | 72.472 | 4.433 | 0.003 |
| 149.000 | TME-1900MHz RRH (65MHz) | 2 | 72.472 | 4.433 | 0.003 | 10743 |
| 148.000 | APXVSPP18-C-A20 w/ Mount Pipe | 2 | 72.472 | 4.433 | 0.003 | 10743 |
| 138.000 | BXA-70063-6CF-2 w/ Mount Pipe | 2 | 63.199 | 4.371 | 0.002 | 10743 |
| 128.000 | HPA-65R-BUU-H8 w/ Mount Pipe | 2 | 54.152 | 4.236 | 5371 |  |
| 79.000 | PD1109E | 2 | 19.746 | 2.399 | 0.002 | 2684 |
| 45.000 | GPS_A | 2 | 6.464 | 1.310 | 0.001 | 1896 |
| 13.000 | GPS_A | 2 | 0.551 | 0.406 | 0.000 | 2204 |

## Compression Checks



## Pole Design Data

| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | $A$ | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | in ${ }^{2}$ | K | K | $\phi P_{n}$ |
| L1 | 148-116.5 (1) | TP29.48x24x0.219 | 31.500 | 0.000 | 0.0 | 19.864 | -11.599 | 1273.620 | 0.009 |
| L2 | 116.5-98.5 (2) | TP32.175x28.39x0.25 | 21.750 | 0.000 | 0.0 | 25.332 | -14.888 | 1751.620 | 0.008 |
| L3 | 98.5-80.25 (3) | TP35.35x $32.175 \times 0.434$ | 18.250 | 0.000 | 0.0 | 47.022 | -17.904 | 2235.790 | 0.008 |
| L4 | 80.25-70.5 (4) | TP36.547x34.067x0.487 | 14.250 | 0.000 | 0.0 | 55.723 | -22.445 | 2653.470 | 0.008 |
| L5 | 70.5-39.75 (5) | TP41.9x36.547x0.591 | 30.750 | 0.000 | 0.0 | 75.811 | -30.635 | 3874.320 | 0.008 |
| L6 | $39.75-31.75$ <br> (6) | TP42.666x40.361x0.643 | 13.250 | 0.000 | 0.0 | 85.803 | -37.154 | 4394.700 | 0.008 |
| L7 | $31.75-17.75$ <br> (7) | TP45.102x42.666x0.626 | 14.000 | 0.000 | 0.0 | 88.424 | -42.513 | 4539.090 | 0.009 |
| L8 | $17.75-14.25$ <br> (8) | TP45.711x45.102x0.728 | 3.500 | 0.000 | 0.0 | 103.899 | -44.114 | 4902.000 | 0.009 |
| L9 | 14.25-0 (9) | TP48.19x45.711x0.619 | 14.250 | 0.000 | 0.0 | 93.434 | -50.195 | 4669.620 | 0.011 |

## Pole Bending Design Data

| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | $\begin{gathered} \text { Ratio } \\ M_{u x} \\ \hline \end{gathered}$ | $M_{u y}$ | $\phi M_{n y}$ | $\begin{gathered} \text { Ratio } \\ M_{u y} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  |  | kip-ft | kip-ft | $\phi M_{n x}$ | kip-ft | kip-ft | $\phi M_{n y}$ |
| L1 | 148-116.5 (1) | TP29.48x24x0.219 | 257.981 | 749.418 | 0.344 | 0.000 | 749.418 | 0.000 |
| L2 | 116.5-98.5 (2) | TP32.175x28.39x0.25 | 659.991 | 1149.925 | 0.574 | 0.000 | 1149.925 | 0.000 |
| L3 | 98.5-80.25 (3) | TP35.35x32.175x0.434 | 929.142 | 1561.742 | 0.595 | 0.000 | 1561.742 | 0.000 |
| L4 | 80.25-70.5 (4) | TP36.547x34.067x0.487 | 1223.725 | 1956.667 | 0.625 | 0.000 | 1956.667 | 0.000 |
| L5 | 70.5-39.75 (5) | TP41.9x36.547x0.591 | 1782.567 | 3196.708 | 0.558 | 0.000 | 3196.708 | 0.000 |
| L6 | $39.75-31.75$ <br> (6) | TP42.666x40.361x0.643 | 2089.192 | 3769.733 | 0.554 | 0.000 | 3769.733 | 0.000 |
| L7 | $31.75-17.75$ <br> (7) | TP45.102x42.666x0.626 | 2422.783 | 4125.800 | 0.587 | 0.000 | 4125.800 | 0.000 |
| L8 | $17.75-14.25$ <br> (8) | TP45.711x45.102x0.728 | 2507.592 | 4497.242 | 0.558 | 0.000 | 4497.242 | 0.000 |
| L9 | 14.25-0 (9) | TP48.19x45.711x0.619 | 2859.117 | 4544.692 | 0.629 | 0.000 | 4544.692 | 0.000 |

## Pole Shear Design Data

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | Ratio $V_{u}$ | Actual $T_{u}$ | $\phi T_{n}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $K$ | K | $\phi V_{n}$ | kip-ft | kip-ft | $\phi T_{n}$ |
| L1 | 148-116.5 (1) | TP29.48x24x0.219 | 17.795 | 636.808 | 0.028 | 0.377 | 1500.667 | 0.000 |
| L2 | 116.5-98.5 (2) | TP32.175x28.39x0.25 | 19.129 | 875.812 | 0.022 | 0.377 | 2302.667 | 0.000 |
| L3 | 98.5-80.25 (3) | TP35.35x32.175x0.434 | 20.021 | 1117.890 | 0.018 | 0.377 | 3127.308 | 0.000 |
| L4 | 80.25-70.5 (4) | TP36.547x34.067x0.487 | 21.126 | 1326.740 | 0.016 | 0.376 | 3918.117 | 0.000 |
| L5 | 70.5-39.75 (5) | TP41.9x36.547x0.591 | 22.675 | 1937.160 | 0.012 | 0.376 | 6401.233 | 0.000 |
| L6 | $39.75-31.75$ <br> (6) | TP42.666x40.361x0.643 | 23.509 | 2188.250 | 0.011 | 0.206 | 7548.691 | 0.000 |
| L7 | $31.75-17.75$ <br> (7) | TP45.102x42.666x0.626 | 24.147 | 2260.670 | 0.011 | 0.206 | 8261.700 | 0.000 |
| L8 | $17.75-14.25$ <br> (8) | TP45.711x45.102x0.728 | 24.316 | 2439.940 | 0.010 | 0.206 | 9005.500 | 0.000 |
| L9 | 14.25-0 (9) | TP48.19x45.711x0.619 | 24.959 | 2326.120 | 0.011 | 0.206 | 9100.500 | 0.000 |



| Section <br> No. | Elevation | Size | $\begin{gathered} \text { Actual } \\ V_{u} \\ K \end{gathered}$ | $\phi V_{n}$ | $\begin{gathered} \hline \text { Ratio } \\ V_{u} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Actual } \\ T_{u} \\ \text { kip-ft } \end{gathered}$ | $\begin{gathered} \phi T_{n} \\ k i p-f t \end{gathered}$ | $\begin{gathered} \hline \text { Ratio } \\ T_{u} \\ \hline \phi T_{n} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  |  | K | $\phi V_{n}$ |  |  |  |

Pole Interaction Design Data

| Section No. | Elevation | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ | Ratio $M_{u x}$ | Ratio $M_{u y}$ | $\begin{gathered} \text { Ratio } \\ V_{u} \\ \hline \end{gathered}$ | Ratio $T_{u}$ | Comb. Stress | Allow. Stress | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $\phi P_{n}$ | $\phi M_{n X}$ | $\phi M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ | Ratio | Ratio |  |
| L1 | 148-116.5 (1) | 0.009 | 0.344 | 0.000 | 0.028 | 0.000 | $0.354$ | 1.000 | 4.8.2 |
| L2 | 116.5-98.5 (2) | 0.008 | 0.574 | 0.000 | 0.022 | 0.000 |  | 1.000 | 4.8.2 |
| L3 | 98.5-80.25 (3) | 0.008 | 0.595 | 0.000 | 0.018 | 0.000 | $0.603$ | 1.000 | 4.8.2 |
| L4 | 80.25-70.5 (4) | 0.008 | 0.625 | 0.000 | 0.016 | 0.000 | $0.634$ | 1.000 | 4.8.2 |
| L5 | 70.5-39.75 (5) | 0.008 | 0.558 | 0.000 | 0.012 | 0.000 | $0.566$ | 1.000 | 4.8.2 |
| L6 | $39.75-31.75$ <br> (6) | 0.008 | 0.554 | 0.000 | 0.011 | 0.000 | $0.563$ | 1.000 | 4.8.2 |
| L7 | $31.75-17.75$ <br> (7) | 0.009 | 0.587 | 0.000 | 0.011 | 0.000 | $0.597$ | 1.000 | 4.8.2 |
| L8 | $17.75-14.25$ <br> (8) | 0.009 | 0.558 | 0.000 | 0.010 | 0.000 | $0.567$ | 1.000 | 4.8.2 |
| L9 | 14.25-0 (9) | 0.011 | 0.629 | 0.000 | 0.011 | 0.000 | $0.640$ | 1.000 | 4.8.2 |

## Section Capacity Table

| Section No. | Elevation $f t$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} ø P_{\text {allow }} \\ K \end{gathered}$ | \% Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 148-116.5 | Pole | TP29.48x24x0.219 | 1 | -11.599 | 1273.620 | ** | ** |
| L2 | 116.5-98.5 | Pole | TP32.175x28.39x0.25 | 2 | -14.888 | 1751.620 | ** | ** |
| L3 | 98.5-80.25 | Pole | TP35.35x32.175x0.434 | 3 | -17.904 | 2235.790 | ** | ** |
| L4 | 80.25-70.5 | Pole | TP36.547x34.067x0.487 | 4 | -22.445 | 2653.470 | ** | ** |
| L5 | 70.5-39.75 | Pole | TP41.9x36.547x0.591 | 5 | -30.635 | 3874.320 | ** | ** |
| L6 | 39.75-31.75 | Pole | TP42.666x40.361x0.643 | 6 | -37.154 | 4394.700 | ** | ** |
| L7 | 31.75-17.75 | Pole | TP45.102x42.666x0.626 | 7 | -42.513 | 4539.090 | ** | ** |
| L8 | 17.75-14.25 | Pole | TP45.711x45.102x0.728 | 8 | -44.114 | 4902.000 | ** | ** |
| L9 | 14.25-0 | Pole | TP48.19x45.711x0.619 | 9 | -50.195 | 4669.620 | ** | ** |
|  |  |  |  |  |  | Pole (L9) <br> RATING = | $\begin{gathered} \text { Summary }_{* *} \\ * * \end{gathered}$ | ** |

**Check Additional Calculations

Program Version 7.0.5.1

APPENDIX B

## BASE LEVEL DRAWING

(INSTALLED)
(1) $1 / 2^{n}$ TO 16 FT LEVEL
(18) $1-5 / 8^{\prime \prime}$ TO 138 FT LEVEL
(INSTALLED)
(1) $1 / 2^{\prime \prime}$ TO 45 FT LEVEL
(3) $1-1 / 4$ " TO 148 FT LEVEL


BUSINESS UNIT: 876373

APPENDIX C
ADDITIONAL CALCULATIONS


Rein1



Rein3

| Bottom | Top | Qty | Model | Position | T or T\&C |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 |  |  |  | F | T\&C |
|  |  |  |  |  | F | T\&C |
|  |  |  |  |  | F | T\&C |
|  |  |  |  |  | F | T\&C |
|  |  |  |  |  | F | T\&C |
|  |  |  |  |  | F | T\&C |
|  |  |  |  |  | F | T\&C |
|  |  |  |  |  | F | T\&C |
|  |  |  |  |  | F | T\&C |



## Anchor Rod Information for TIA/EIA-222-F and TIA-222-G-2



| Original Anchor Rod Data |  |
| :---: | :---: |
| Quantity: | 16 |
| Diameter: | 2.25 |
| Material: | A615 GR 75 |
| Bolt Circle: | 55.0 |
| Bolt Spacing: | 6 |
| Bolt Group Area: | 63.62 |
| Bolt Group MOIx: | 24055 |


|  |  |  |
| :---: | :---: | :---: |
| Quantity: $\quad$ First Added Anchor Rod Data |  |  |
| Diameter: | 2.25 | in |
| Material: | A193 B7 |  |
| Bolt Circle: | 62.0 | in |
| Bolt Group Area: | 11.93 | in ${ }^{2}$ |
| Bolt Group MOIx: | 5732 | in ${ }^{4}$ |
| Reactions Seen by First Added AR Group |  |  |
| Moment: | 550.1 | kip-ft |
| Axial: | 0.0 | kip |
| Shear: | 0.0 | kip |
| First Added AR Capacity Check |  |  |
| Combined Load: | 134.2 | kip |
| Allowable load: | 324.8 | kip |
| AR Capacity: | 41.3\% | Pass |




| Design Information |  |
| :---: | :---: |
| TIA Code: | G |
| ASIF: | 1.000 |
| Failure: | 105\% |
| eta Factor: | 0.50 |


| Third Added Anchor Rod Data |  |  |
| :---: | :---: | :---: |
| Quantity: <br> Diameter: <br> Material: <br> Bolt Circle: |  | in |
|  |  |  |
|  |  |  |
|  |  |  |
| Bolt Group Area: | 0.00 | in ${ }^{2}$ |
| Bolt Group MOIx: | 0 | in ${ }^{4}$ |
| Reactions Seen by Second Added AR Group |  |  |
| Moment: | 0.0 | kip-ft |
| Axial: | 0.0 | kip |
| Shear: | 0.0 | kip |
| Second Added AR Capacity Check |  |  |
| Combined Load: | 0.0 | kip |
| Allowable load: | 0.0 | kip |
| AR Capacity: | 0.0\% |  |

Square, Stiffened / Unstiffened Base Plate, Any Rod Material - Rev. F /C
Assumptions: 1) Rod groups at corners. Total \# rods divisible by 4. Maximum total \# of rods = 48 (12 per Corner).
2) Rod Spacing $=$ Straight Center-to-Center distance between any (2) adjacent rods (same corner)
3) Clear space between bottom of leveling nut and top of concrete not exceeding (1)*(Rod Diameter)

| Site Data |  |  |
| :---: | :---: | :---: |
| BU\#: 876373 |  |  |
| Site Name: LONG EDDY - WRIGHT P <br> App \#: 378332 Revision \# 2 |  |  |
|  |  |  |
| Anchor Rod Data |  |  |
| Eta Factor, $\eta$ | 0.5 | TIA G (Fig. 4-4) |
| Qty: Diam: <br> Rod Material: <br> Yield, Fy: <br> Strength, Fu: <br> Bolt Circle: | 16 |  |
|  | 2.25 | in |
|  | A615-J |  |
|  | 75 | ksi |
|  | 100 | ksi |
|  | 55 | in |
| Anchor Spacing: | 6 | in |


| Base Reactions |  |  |
| ---: | :---: | :--- |
| TIA Revision: | G |  |
| Factored Moment, Mu: | 2308.97098 | ft-kips |
| Factored Axial, Pu: | 50.1951 |  |
| kips |  |  |
| Factored Shear, Vu: | 24.959102 | kips |


| Anchor Rod Results |  |
| :--- | :---: |
| TIA G --> Max Rod (Cu+ Vu/n): | 132.2 Kips |
| Axial Design Strength, $\Phi^{*} F$ AAnet: $^{\text {Anchor Rod Stress Ratio: }}$ | 260.0 Kips |
| Anch | $50.8 \%$ Pass |


| Plate Data |  |  |
| ---: | :---: | :--- |
| W=Side: | 54 | in |
| Thick: | 2.75 | in |
| Grade: | 55 | ksi |
| Clip Distance: | 6 | in |


| Base Plate Results | Flexural Check |
| :--- | :---: |
| Base Plate Stress: | 24.5 ksi |
| PL Design Bending Strength, $\Phi^{*}$ Fy: | 49.5 ksi |
| Base Plate Stress Ratio: | $49.5 \%$ Pass |


| Stiffener Data (Welding at both sides) |  |  |
| :---: | :---: | :---: |
| Configuration: | Unstiffened |  |
| Weld Type: |  | ** |
| Groove Depth: |  | in ** |
| Groove Angle: |  | degrees |
| Fillet H. Weld: |  | <-- Disregard |
| Fillet V. Weld: |  | in |
| Width: |  | in |
| Height: |  | in |
| Thick: |  | in |
| Notch: |  | in |
| Grade: |  | ksi |
| Weld str.: |  | ksi |


| Pole Data |  |  |  |
| ---: | :---: | :--- | :---: |
| Diam: | 48.19 | in |  |
| Thick: | 0.375 | in |  |
| Grade: | 65 | ksi |  |
| \# of Sides: | 18 | "0" IF Round |  |

N/A - Unstiffened
Stiffener Results

| Horizontal Weld | N/A |
| :---: | :---: |
| Vertical Weld: | N/A |
| Plate Flex+Shear, $\mathrm{fb} / \mathrm{Fb}+(\mathrm{fv} / \mathrm{Fv})^{\wedge} 2$ : | N/A |
| Plate Tension+Shear, $\mathrm{ft} / \mathrm{Ft}+(\mathrm{fv} / \mathrm{Fv})^{\wedge} 2$ : | N/A |
| Plate Comp. (AISC Bracket): | N/A |
| Pole Results |  |
| Pole Punching Shear Check: | N/A |



[^16]| $\frac{\text { Proj. Number }}{\text { Proj. Name }}$ | $\frac{89028.006 .01}{\text { LONG EDDY / WRIGT PROI }}$ |
| :--- | :--- |
| $\underline{\text { Code }}$ |  |


| Previously Added Anchor Rods |  |
| ---: | ---: |
| Diameter | 2.25 in |
| Grade | A193 Gr B7 |
| Quantity | 3 |
| Bolt Circle | 62 in |


| Existing Mfg Anchor Rods |  |
| ---: | ---: |
| Diameter | 2.25 in |
| Quantity | 16 |
| Bolt Circle | 55 |
|  | in |


| Summary Output |  |
| :--- | :---: |
| - Anchor Rod Bracket Checks |  |
| Tube Stress: | $36.8 \%$ |
| Max. Weld Stress: | $77.4 \%$ |
|  |  |


| Analysis Criteria |  |
| ---: | ---: |
| Load for Calcs? | Current Load |
| Current Load | 134.2 kips |
| Capacity | 325 kips |

Tower Properties

| $\mathrm{Fy}_{\text {pole }}=$ | 60 |
| :---: | :---: |
| $\mathrm{Fu}_{\text {pole }}=$ | 75 |
| $\mathrm{Fy}_{\text {base }}=$ | 55 |
| $\mathrm{Fu}_{\text {base }}=$ | 75 |

## Foundation Properties

| Type | Pad |
| :---: | :---: |
| Pad Thickness | 3.5 |
| $\mathrm{f}_{\mathrm{c}}$ | 3000 |
| Clear Cover | 3 |
| Pad Width | 24.5 |
|  | 10 |
|  | 18 |
|  |  |
|  |  |

## Anchor Rod Bracket Properties

## Gusset Properties

| Thickness | 1.25 | inch |
| :---: | :---: | :---: |
| Pole to Tube CL | 6.8125 | inch |
| Height | 54 | inch |
| Width at Tube | 4.5625 | inch |
| $F y_{\text {plate }}=$ | 65 | ksi |
| $F u_{\text {plate }}=$ | 80 | ksi |
| Gap = | 0 | inch |
| Notch $=$ | 0.75 | inch |

Pipe/Tube Properties

| Size | 4 XXS Pipe |  |
| :---: | :---: | :---: |
| $\mathrm{L}_{\text {pipe }}=$ | 14 | inch |
| Length Above Gusset |  | 3 inch |
| $F_{\text {ypipe }}=$ | 50 | ksi |
| $\mathrm{D}_{\text {pipe }}=$ | 4.5 | inch |
| $\mathrm{t}_{\text {pipe }}=$ | 0.674 | inch |
| $\mathrm{A}_{\text {pipe }}=$ | 8.101300374 | inch $^{2}$ |
| $\mathrm{I}_{\text {pipe }}=$ | 15.28366215 | inch $^{4}$ |
| $\mathrm{r}_{\text {pipe }}=$ | 1.373524299 | inch |

## Weld Properties

| $\mathrm{F}_{\text {EXX }}=$ | $70 \mathrm{ksi} \quad$ Weld Material Grade |
| :--- | :--- |
| Load Angle | 45 degrees |


| $l$ | - Bracket to Tube Weld |  |
| :--- | ---: | :--- |
| Double Bevel+Fillet |  |  |

- Bracket to Pole Weld

| Weld Type | Double Fillet |  |
| :--- | ---: | :--- |
| $D_{\text {vpole }}=$ | 6 | Vertical fillet weld size in sixteenths |
| $H=$ | 54 inch | Height of vertical weld from base plate |

- Gusset to Base Plate Weld

| Weld Type | Double Bevel+Fillet |  |
| :--- | :---: | :--- |
| Bevel Depth | 0.5 inch | Bevel depth in inches |
|  | 8 | Fillet weld size in sixteenths |
| Fillet Size | 8 |  |

Additional Variables

| $C_{1}=$ | 1.00 |  |
| :--- | ---: | :--- |
| $\mathrm{k}_{\mathrm{rt}}=$ | 0 | Electrode Strength Coefficient |
| $\Psi_{\mathrm{t}}=$ | 1 | Transverse Reinforcement Index: |
|  |  | Rebar Location Factor: |


| PROJ ECT | 876373 - LONG EDDY / WRI GHT PROPERTY, CT |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SUBJ ECT | Foundation Analysis |  |  |  |  |
| DATE | 03-23-17 | PAGE | 1 | OF | 1 |

Monopole Pad \& Pier Foundation Analysis

Design Loads:

Shear:
Moment:
Tower Height:
Tower Weight:

Pad \& Pier Dimensions / Properties:

Pole Diameter at Base:
Bearing Depth:
Pad Width:
Neglected Depth:
Thickness:
Pier Diameter:
Pier Height Above Grade:
BP Dist. Above Pier:
Clear Cover:
Pier Rebar Size:
Pier Rebar Quanity:
Pad Rebar Size:
Pad Rebar Quanity:
Pier Tie Size:
Tie Quanity:
Rebar Yield Strength:
Concrete Strength:
Concrete Unit Weight:




### 24.5 FT

Elevation Overview


## Summary of Results

| Req'd Pier Diam. | No Good! |
| :--- | :---: |
| Overturning | $76.9 \%$ |
| Shear Capacity | $29.6 \%$ |
| Bearing | $21.6 \%$ |
| Pad Shear - 1-way | $30.7 \%$ |
|  |  |
| Pad Moment Capacity | $48.7 \%$ |


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[^15]:    Consider Moments - Legs
    Consider Moments - Horizontals
    Consider Moments - Diagonals
    Use Moment Magnification
    $\sqrt{ }$ Use Code Stress Ratios
    $\sqrt{ }$ Use Code Safety Factors - Guys Escalate Ice
    Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric

[^16]:    ** Note: for complete joint penetration groove welds the groove depth must be exactly $1 / 2$ the stiffener thickness for calculation purposes

