



56 Prospect Street,
P.O. Box 270
Hartford, CT 06103

Kathleen M. Shanley
Manager – Transmission Siting
Tel: (860) 728-4527

January 28, 2021

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

**RE: Notice of Exempt Modification
Eversource Site # ES-051 Thompson
97 Mountain Hill Road, Thompson, CT 06255
Latitude: 41-59-11.76 N / Longitude: 71-54-49.11 W**

Dear Ms. Bachman:

The Connecticut Light and Power Company doing business as Eversource Energy (“Eversource”) currently maintains multiple antennas mounted at various heights on an existing 180-foot self-support tower located at 97 Mountain Hill Road in Thompson. See [Attachment A](#), Parcel Map and Property Card. The tower and property are owned by the State of Connecticut Department of Emergency Services and Public Protection (“DESPP”). Eversource and DESPP have entered into an agreement allowing the modification of Eversource’s equipment on the DESPP tower. See [Attachment B](#), Letter of Authorization. Eversource plans to install two 4-foot 3-inch tall omni-directional antennas to be mounted at 131 feet and 154 feet above ground level (“AGL”) and two 7/8-inch diameter coaxial cables. Two existing antennas and associated coaxial cables will be removed. The antennas will be mounted to the existing tower on new 4-foot stand-off mounts. See [Attachment C](#), Mount Analysis. There will be no other changes to the area of the fenced compound, the tower or the existing antennas and equipment currently mounted on the tower. The tower and existing and proposed equipment are depicted on [Attachment D](#), Construction Drawings, dated December 16, 2020 and [Attachment E](#), Structural Analysis, dated November 25, 2020. The Connecticut Siting Council approved this tower under Docket No. 157 in March 1993.

The proposed installation is part of Eversource’s program to update the current obsolete analog voice radio communications system to a modern digital voice communications system. The new system will enable the highest level of voice communications under all operating conditions, including during critical emergency and storm restoration activities. The new radio system will also provide for remote control of distribution safety equipment.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies (“R.C.S.A.”) §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this notice is being delivered to Amy

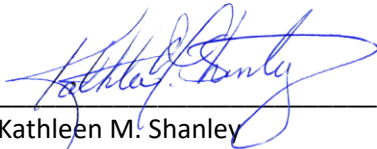
St. Onge, First Selectman for the Town of Thompson and Tyra Penn-Gesek, Director of Planning and Development for the Town of Thompson via private carrier. Proof of delivery is attached. See Attachment F, Proof of Delivery of Notice.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2):

1. There will be no change to the height of the existing tower.
2. The proposed modifications will not require an extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the new antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard as shown in the attached Radio Frequency Emissions Report, dated December 18, 2020 (Attachment G – Power Density Report)¹.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Eversource respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2). One original copy of this notice is enclosed.

Communications regarding this Notice of Exempt Modification should be directed to Kathleen Shanley at (860) 728-4527.

By: 
Kathleen M. Shanley
Manager – Transmission Siting

cc: Honorable Amy St. Onge, First Selectman, Town of Thompson
Tyra Penn-Gesek, Director of Planning and Development, Town of Thompson
DESPP

Attachments

- A. Parcel Map and Property Card
- B. Letter of Authorization
- C. Mount Analysis
- D. Construction Drawings
- E. Structural Analysis
- F. Proof of Delivery of Notice
- G. Power Density Report

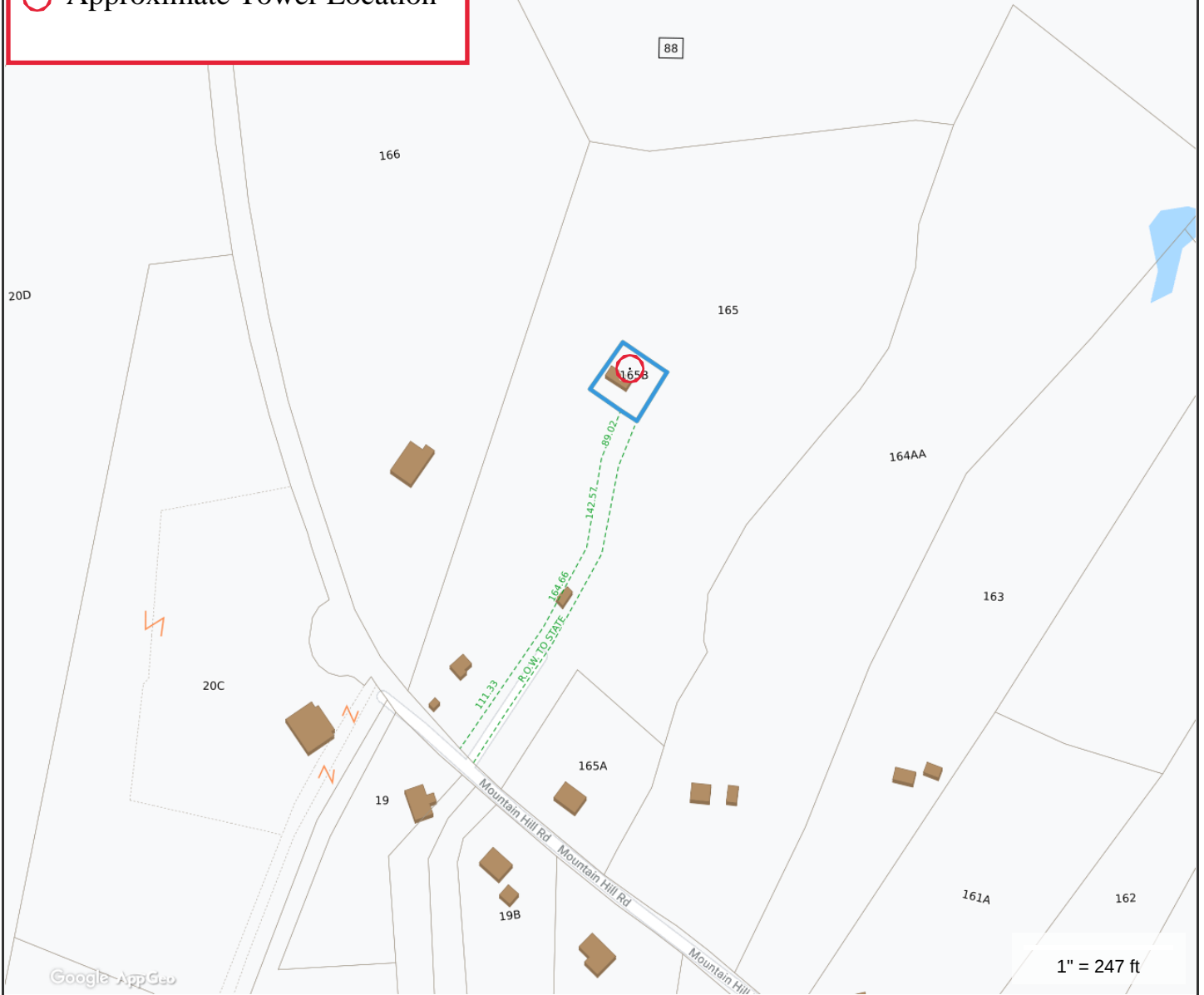
¹ Any receive-only antennas are not included in the Power Density Report, as they are irrelevant in terms of the % MPE calculations.

ATTACHMENT A – PARCEL MAP AND PROPERTY CARD

ES-051 Thompson

Legend

 Approximate Tower Location



Property Information

Property ID 104520
Location 97 MOUNTAIN HILL RD
Owner CONNECTICUT STATE OF DPS



**MAP FOR REFERENCE ONLY
NOT A LEGAL DOCUMENT**

Town of Thompson, CT makes no claims and no warranties, expressed or implied, concerning the validity or accuracy of the GIS data presented on this map.

Geometry updated April 1, 2018
Data updated April 1, 2018

Property Location: 97 MOUNTAIN HILL RD

MAP ID: 42/ 88/ 165/B /

Bldg Name:

State Use: 9010

Vision ID: 848

Account #001730

Bldg #: 1 of 1

Sec #: 1 of 1 Card 1 of 1

Print Date: 12/02/2019 11:40

CURRENT OWNER		TOPO.	UTILITIES	STRT./ROAD	LOCATION	CURRENT ASSESSMENT					
CONNECTICUT STATE OF DEPT PUBLIC SAFETY 165 CAPITOL AVE				1 Paved	2 Secondary St.	Description	Code	Appraised Value	Assessed Value	6140 THOMPSON, CT	
HARTFORD, CT 06106 Additional Owners:						EX COM LN	21	200,000	140,000		
						EX CM OTB	25	239,200	167,500	VISION	
SUPPLEMENTAL DATA											
Other ID:				DV LOT #		Total					
SIDE N-28		SEWER NO									
CENSUS TR 09002		BAA									
FLOOD PLN NO		CALLBACK:									
ACCOUNT # 5268		DM Result 848									
DV MAP # 1120		ASSOC PID#									
GIS ID:											

RECORD OF OWNERSHIP		BK-VOL/PAGE	SALE DATE	q/u	v/i	SALE PRICE	V.C.	PREVIOUS ASSESSMENTS (HISTORY)								
CONNECTICUT STATE OF		0248/0073	11/27/1989	U		0		Yr.	Code	Assessed Value	Yr.	Code	Assessed Value	Yr.	Code	Assessed Value
								2018	21	140,000	2017	21	140,000	2016	21	140,000
								2018	25	167,900	2017	25	167,900	2016	25	167,900
								Total:		307,900	Total:		307,900	Total:		307,900

EXEMPTIONS				OTHER ASSESSMENTS				This signature acknowledges a visit by a Data Collector or Assessor												
Year	Type	Description	Amount	Code	Description	Number	Amount	Comm. Int.												
Total:																				

ASSESSING NEIGHBORHOOD					APPRAISED VALUE SUMMARY											
NBHD/ SUB	NBHD Name	Street Index Name	Tracing	Batch												
0001/A				DM1												
NOTES					Appraised Bldg. Value (Card) 0											
180' TRIPOLE TOWER POLICE RADIO LEASE TO N. E. UTILITIES SHED ON LAND OF N/V LEASE IS RECIPROCAL FOR SPACE ONLY					Appraised XF (B) Value (Bldg) 0											
					Appraised OB (L) Value (Bldg) 239,200											
					Appraised Land Value (Bldg) 200,000											
					Special Land Value 0											
					Total Appraised Parcel Value 439,200											
					Valuation Method: C											
					Adjustment: 0											
					Net Total Appraised Parcel Value 439,200											

BUILDING PERMIT RECORD										VISIT/ CHANGE HISTORY					
Permit ID	Issue Date	Type	Description	Amount	Insp. Date	% Comp.	Date Comp.	Comments	Date	Type	IS	ID	Cd.	Purpose/Result	
									10/01/2019			V	53	FIELD REVIEW	
									05/03/2019			RH	14	Vacant Land/Oby	
									01/14/2009			MM	14	Vacant Land/Oby	
									01/14/2000			NS	00	Measur+Listed	

LAND LINE VALUATION SECTION																			
B #	Use Code	Use Description	Zone	D	Front	Depth	Units	Unit Price	I. Factor	S.A.	C. Factor	ST. Idx	Adj.	Notes- Adj	Special Pricing	S Adj	Adj. Unit Price	Land Value	
															Spec Use	Spec Calc	Fact		
1	9010	STATE	RA80				0.23	AC	0.00	1.0000	0		0.00				.00	0.00	0
1	9010	STATE	RA80				1.00	BL	200,000.00	1.0000	0		0.00				1.00	200,000.00	200,000

Total Card Land Units: 0.23 AC Parcel Total Land Area: 0.23 AC Total Land Value: 200,000

CONSTRUCTION DETAIL				CONSTRUCTION DETAIL (CONTINUED)			
Element	Cd.	Ch.	Description	Element	Cd.	Ch.	Description
Model	00		Vacant				
MIXED USE							
	Code		Description				Percentage
	9010		STATE				100
COST/MARKET VALUATION							
	Adj. Base Rate:						0.00
							0
	Net Other Adj:						0.00
	Replace Cost						0
	AYB						
	Dep Code						
	Remodel Rating						
	Year Remodeled						
	Dep %						
	Functional Obslnc						
	External Obslnc						
	Cost Trend Factor					1	
	Condition						
	% Complete						
	Overall % Cond						
	Apprais Val						
	Dep % Ovr						0
	Dep Ovr Comment						
	Misc Imp Ovr						0
	Misc Imp Ovr Comment						
	Cost to Cure Ovr						0
	Cost to Cure Ovr Comment						

OB-OUTBUILDING & YARD ITEMS(L) / XF-BUILDING EXTRA FEATURES(B)

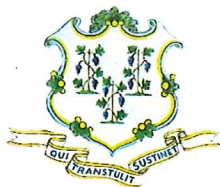
Code	Description	Sub	Sub Descript	L/B	Units	Unit Price	Yr	Gde	Dp Rt	Cnd	%Cnd	Apr Value
CB1	PRECAST CO			L	756	125.00	2000		0		90	85,100
FN9	W/O TOP RL-4			L	370	25.00	2000		0		90	8,300
TWR2	MONOPOLE			L	180	900.00	2000		0		90	145,800

No Photo On Record

BUILDING SUB-AREA SUMMARY SECTION

Code	Description	Living Area	Gross Area	Eff. Area	Unit Cost	Undeprec. Value
<p>Ttl. Gross Liv/Lease Area: 0 0 0</p>						

ATTACHMENT B – LETTER OF AUTHORIZATION



STATE OF CONNECTICUT
DEPARTMENT OF EMERGENCY SERVICES AND PUBLIC PROTECTION

April 7, 2020

Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Re: **Letter of Authorization** – Co-location on Connecticut State Police tower
Property address: 97 Mt. Hill Road, Thompson, CT
Latitude: 41 98'-65" Longitude: 71 54' 49.16"

To Whom It May Concern:

Eversource Energy (Eversource) has an Agreement with the Connecticut Department of Emergency Services and Public Protection (DESPP) to co-locate its communications equipment on the DESPP tower located at 97 Mt. Hill Road, Thompson, Connecticut.

Eversource shall be required by the terms of the agreement to seek and obtain all necessary permits and approvals. As a duly authorized representative of the DESPP, permission is hereby granted to Eversource and agents thereof, for the purpose of consummating any applications necessary to gain the required approvals from the State of Connecticut.

Any fees or charges associated with all applications or permits and any conditions placed on the applicant shall be the sole responsibility of Eversource.

Yours truly,

Brian Benito
Planning Specialist
State Of Connecticut
Department of Emergency Services and Public Protection
CTS Unit
860-685-8297
brian.benito@ct.gov

*1111 Country Club Road
Middletown, CT 06457
Phone: (860) 685-8280/Fax: (860) 685-8345
An Affirmative Action/Equal Employment Opportunity Employer*

ATTACHMENT C – MOUNT ANALYSIS

December 2, 2020

MOUNT EVALUATION LETTER

Site Number: 848
Site Name: THOMPSON CSP
Site Data: 97 Mountain Hill Road
 Thompson, CT 06255
Latitude: 41° 59' 11.76"
Longitude: -71° 54' 49.11"

Black & Veatch Corporation is pleased to submit this "Mount Evaluation Letter" to determine the structural integrity of antenna mounting system on the above-mentioned site. The purpose of this evaluation is to determine the capacity of the system in supporting the final loading in the attached "Loading Summary".

Based on our evaluation we have determined the proposed antenna mounting system to be: **SUFFICIENT**

Structure Rating (max from all components) =	17.1%
---	-------

Proposed Mounting System
SitePro 1 (USF-4U) 48" Ultimate Universal Stand-off Frame

This analysis analyzes the worst-case scenario for the proposed USF-4U Stand-off Frame. All levels are deemed sufficient. The proposed mounting system will be capable of supporting the proposed equipment, under the following conditions:

- Contractor shall be responsible for the means and methods of construction.
- Contractor shall inspect the condition of all existing and proposed structural members, all relevant members and connections and report any deficiencies to the engineer prior to installation of any new antennas and other equipment.

The scope of this evaluation pertains only to the proposed antenna mounting system and does not include examination of the loads imparted by the antenna mounting system to the existing tower and its structural components. This document was prepared based on information provided to Black & Veatch. If existing conditions do not reflect those represented, this analysis is no longer valid.

Please contact Josh Riley in our Overland Park Office at 913-458-2522 if you have any questions or comments.

Sincerely,
 Black & Veatch Corporation

Prepared By: JooHwan Jung
 Submitted By: Josh Riley, P.E.

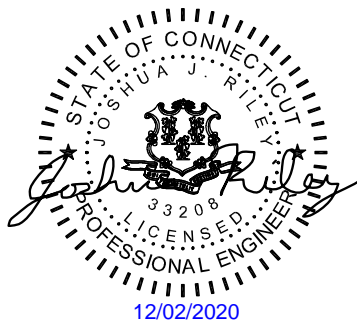




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2. ANALYSIS CRITERIA SUMMARY
3. REFERENCES
4. ASSUMPTIONS
5. RESULTS SUMMARY

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APPENDIX 2: RISA PRINTOUTS

APPENDIX 3: ATTACHMENTS



1. LOADING SUMMARY

Appurtenance								
Carrier	Position	Sector	Antenna RAD Center (ft)	Mount Centerline (ft)	Qty	Type	Manufacturer	Model
Eversource	1	-	157	154	1	Omni	Telewave	ANT220F2
Eversource	1	-	134	131	1	Omni	Telewave	ANT220F2

This analysis analyzes the worst-case scenario for the proposed USF-4U Stand-off Frame. All levels are deemed sufficient.



2. ANALYSIS CRITERIA SUMMARY

ANALYSIS CRITERIA	
STANDARD	TIA-222-H
WIND SPEED	Ultimate of 140 mph
WIND SPEED WITH ICE	50 mph with 2" radial ice thickness
EXPOSURE CATEGORY	B
RISK CATEGORY	III
TOPO CATEGORY	Hill
CREST HEIGHT	110 ft

3. REFERENCES

- American Institute of Steel Construction, AISC 15th Edition
- Telecommunications Industry Association Standard, TIA-222-H & 2018 Connecticut State Building Code
- Antenna Mount Assembly Drawing (Model: USF-4U) by SitePro 1, dated 02/16/2011

4. ASSUMPTIONS

This analysis may be affected if any assumptions are not valid or have been made in error. Black & Veatch should be notified to determine the effect on the structural integrity of the antenna mounting system.

- The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specifications.
- The configuration of antennas, mounts, and other appurtenances are as specified in the Loading Summary and the referenced drawings.
- All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
- Sector frame center line: located equidistant between top & bottom boom; Platform center line: located at the base perimeter of platform, unless otherwise specified.
- Steel grades have been assumed as follows, unless noted otherwise:

Channel, Solid Round, Angle, Plate	ASTM A36 (GR 36)
HSS (Rectangular)	ASTM 500 (GR B-46)
Pipe	ASTM A53 (GR B-35)
Connection Bolts	ASTM A325



5. RESULTS SUMMARY

Name	Bending Stress Ratio		Shear Stress Ratio	
Arm: HSS3X3X3/16	13.0%	Pass	2.8%	Pass
Bracing: Pipe 2.0 Std	17.1%	Pass	2.2%	Pass
Mount Pipe: Pipe 3.0 Std	8.6%	Pass	3.8%	Pass

*Von Mises SR = (Max Von Mises Value From RISA-3D)/(0.9*Fy)

**Capacity rating per TIA-222-H Section 15.5.



BLACK & VEATCH

November 30, 2020

THOMPSON CSP

**APPENDIX 1:
MOUNT ANALYSIS REPORT**



BLACK & VEATCH

Client: Eversource
Site Name: THOMPSON CSP (848)

Computed By: Joochan Jung

Date: 11/30/2020

Verified By: JW

Title: MOUNT ANALYSIS REPORT

Date: 11/30/2020

Dead and Live Loads

Maintenance Live Load: $L_V = 250$ lb

Installation Live Load: $L_M = 0$ lb

Appurtenance Dead Loads	
Name	Weight (lb)
ANT220F2	11



Member Wind Loading

Exposure Category = B
 Risk Category = III
 Topographic Category = 1
 Basic Wind Speed, V = 140 mph
 Height Above Ground, z = 157 ft
 Crest Height, H = 110 ft
 Velocity Pressure Coefficient, K_z = 1.12
 Topographic Factor, K_{zt} = 1.06
 Wind Directionality Factor, K_d = 0.95
 Shielding Factor, K_a = 0.90
 Ground Elevation Factor, K_e = 1.000
 Wind Velocity Pressure, q_z = 56.59 psf
 Gust Effect Factor, G_h = 1.00

Equations

$$K_z = 2.01 (z / z_g)^{2/\alpha}$$

$$K_h = e^{(f \cdot z / H)}$$

$$K_{zt} = [1 + K_c K_t / K_h]^2$$

$$K_e = e^{-0.0005z^2}$$

$$q_z = 0.00256 K_z K_{zt} K_e K_d V^2$$

$$F_A = q_z G_h (EPA)$$

$$F_M = q_z G_h C_f D_p$$

TIA-222-H

2.6.5.2

2.6.6.2.1

2.6.6.2.1

2.6.8

2.6.11.6

2.6.11.2

2.6.11.2

Member Wind Loads

Name	Depth (ft)	Width (ft)	C_f	D_p (ft)	F_M (lb)
Arm: HSS3X3X3/16	0.25	0.25	2	0.25	28.29
Bracing: Pipe 2.0 Std	0.20		1.2	0.20	13.44
Mount Pipe: Pipe 3.0 Std	0.29		1.2	0.29	19.81



Client: Eversource
 Site Name: THOMPSON CSP (848)

Computed By: JooHwan Jung

Date: 11/30/2020

Verified By: JW

BLACK & VEATCH

Title: MOUNT ANALYSIS REPORT

Date: 11/30/2020

Appurtenance Ice Dead Loading

Exposure Category = B
 Risk Category = III
 Topographic Category = 1
 Height Above Ground, z = 157 ft
 Crest Height, H = 110 ft
 Design Ice Thickness, T_i = 2.00 in
 Importance Factor, I = 1.15
 Topographic Factor, K_{zt} = 1.06
 Height Escalation Factor, K_{iz} = 1.17
 Factored Ice Thickness, T_{iz} = 2.74 in
 Grating Ice Dead Load, D_{Gice} = 12.79 psf

Equations

$$K_h = e^{(f \cdot z / H)}$$

$$K_{zt} = [1 + K_c K_t / K_h]^2$$

$$K_{iz} = (z/33)^{u \cdot 10}$$

$$T_{iz} = T_i I K_{iz} (K_{zt})^{u \cdot 30}$$

$$DL_{ice} = [(H_{ice} * D_{ice} * W_{ice}) - (H * W * D)] * 56pcf$$

TIA-222-H

2.6.6.2.1

2.6.6.2.1

2.6.10

2.6.10

Appurtenance Ice Dead Loads

Name	Height w/ ice (ft)	Width w/ice (ft)	Depth w/ ice (ft)	V_{ice} (ft ³)	DL_{ice} (lb)
ANT220F2	4.71	0.69	0.69	1.99	111.48



BLACK & VEATCH

Client: Eversource
 Site Name: THOMPSON CSP (848)

Computed By: JooHwan Jung

Date: 11/30/2020

Verified By: JW

Title: MOUNT ANALYSIS REPORT

Date: 11/30/2020

Member Ice Dead Loading

Exposure Category = B
 Risk Category = III
 Topographic Category = 1
 Height Above Ground, z = 157 ft
 Crest Height, H = 110 ft
 Design Ice Thickness, T_i = 2.00 in
 Importance Factor, I = 1.15
 Topographic Factor, K_{zt} = 1.06
 Height Escalation Factor, K_{iz} = 1.17
 Factored Ice Thickness, T_{iz} = 2.74 in
 Grating Ice Dead Load, D_{Gice} = 12.79 psf

Equations

$$K_h = e^{(f \cdot z / H)}$$

$$K_{zt} = [1 + K_c K_t / K_h]^2$$

$$K_{iz} = (z/33)^{0.10}$$

$$T_{iz} = T_i I K_{iz} (K_{zt})^{0.35}$$

$$A_{iz} = \pi \cdot T_{iz} \cdot (D_c + T_{iz})$$

$$DL_{ice} = A_{iz} \cdot 56 \text{pcf}$$

TIA-222-H

2.6.6.2.1

2.6.6.2.1

2.6.10

2.6.10

2.6.10

Member Ice Dead Loads

Name	Depth w/ ice (ft)	Width w/ ice (ft)	Dc (ft)	Aiz (ft ²)	DL _{ice} (lb/ft)
Arm: HSS3X3X3/16	0.71	0.71	0.35	0.42	23.38
Bracing: Pipe 2.0 Std	0.65		0.20	0.31	17.12
Mount Pipe: Pipe 3.0 Std	0.75		0.29	0.37	20.89



Client: Eversource
 Site Name: THOMPSON CSP (848)

Computed By: Joochan Jung

Date: 11/30/2020

Verified By: JW

BLACK & VEATCH

Title: MOUNT ANALYSIS REPORT

Date: 11/30/2020

Member Ice Wind Loading

Exposure Category = B
 Risk Category = III
 Topographic Category = 1
 Ice Wind Speed, V_{ice} = 50 mph
 Height Above Ground, z = 157 ft
 Crest Height, H = 110 ft
 Velocity Pressure Coefficient, K_z = 1.12 psf
 Topographic Factor, K_{zt} = 1.06
 Wind Directionality Factor, K_d = 0.95
 Shielding Factor, K_a = 0.90
 Ground Elevation Factory, K_e = 1.000
 Ice Wind Velocity Pressure, $q_{z(ice)}$ = 7.218
 Factored Ice Thickness, T_{iz} = 2.74 in
 Gust Effect Factor, G_h = 1

Equations

$K_z = 2.01 (z / z_g)^{2/\alpha}$

$K_h = e^{(f \cdot z / H)}$

$K_{zt} = [1 + K_c K_t / K_h]^2$

$K_e = e^{-0.00003z^2}$

$q_z = 0.00256 K_z K_{zt} K_e K_d V^2$

$F_{A(ice)} = q_{z(ice)} G_h (EPA)_{A(ice)}$

$F_{M(ice)} = q_{z(ice)} G_h C_f D_{p(ice)}$

TIA-222-H

2.6.5.2

2.6.6.2.1

2.6.6.2.1

2.6.8

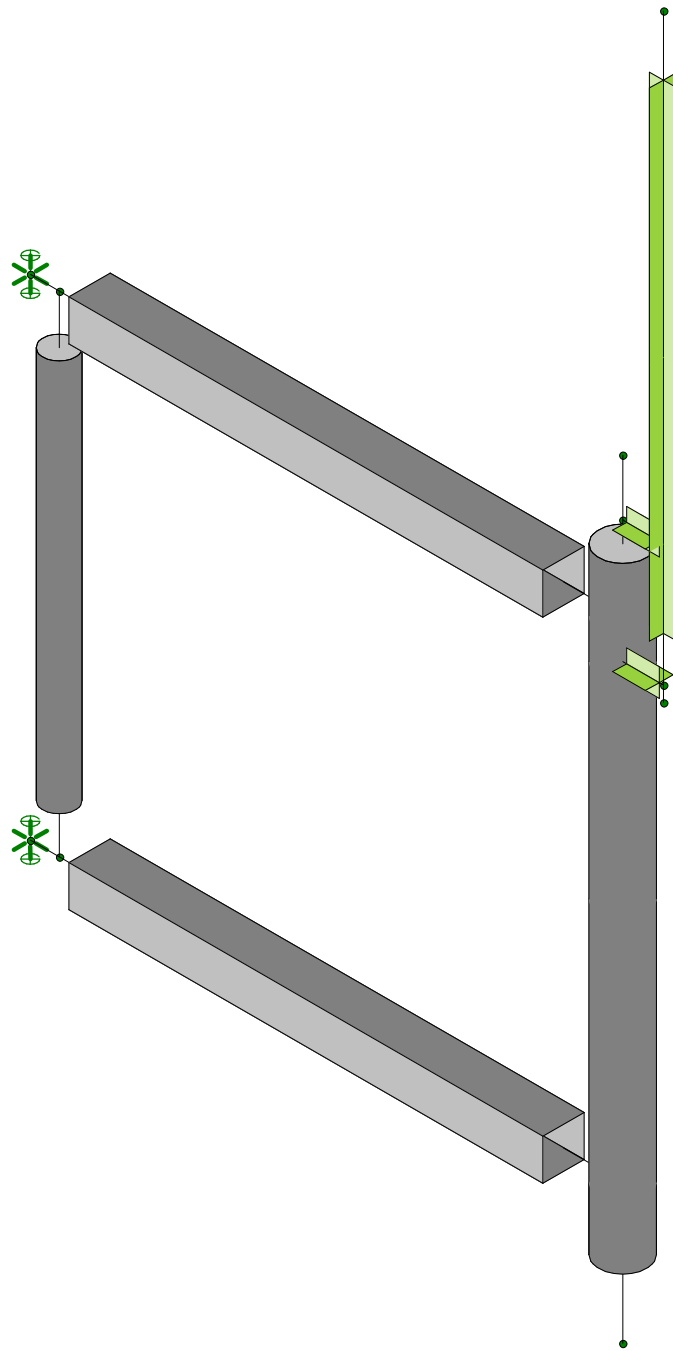
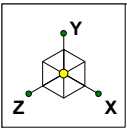
2.6.11.6

2.6.11.2

2.6.11.2

Member Ice Wind Loads					
Name	Depth w/ Ice (ft)	Width w/ Ice (ft)	C_f	$D_{p(ice)}$ (ft)	$F_{M(ice)}$ (lb/ft)
Arm: HSS3X3X3/16	0.71	0.71	2	0.71	10.20
Bracing: Pipe 2.0 Std	0.65		1.2	0.65	5.67
Mount Pipe: Pipe 3.0 Std	0.75		1.2	0.75	6.48

**APPENDIX 2:
RISA PRINTOUTS**

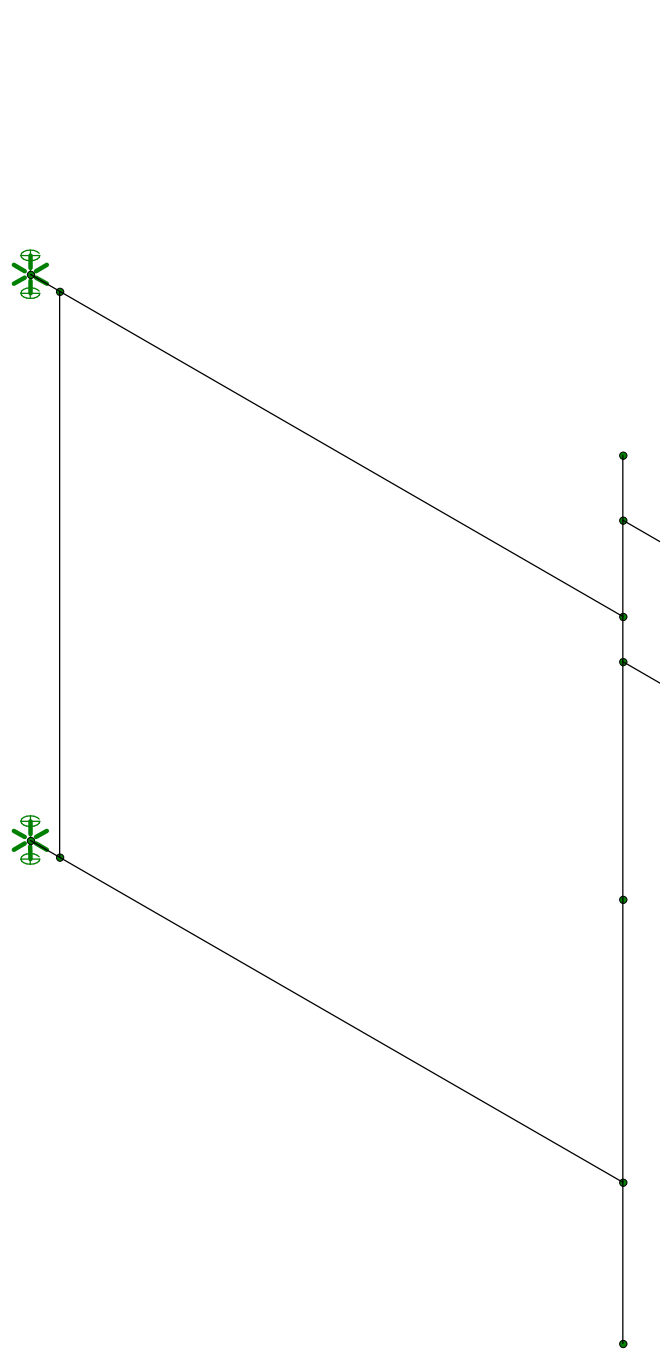
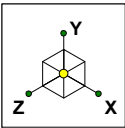


Envelope Only Solution

Black & Veatch
JooHwan Jung
405025.2021.2200

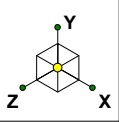
THOMPSONCSP USF-4U Model

SK - 1
Dec 1, 2020 at 11:29 AM
THOMPSONCSP USF-4U Model.r3d

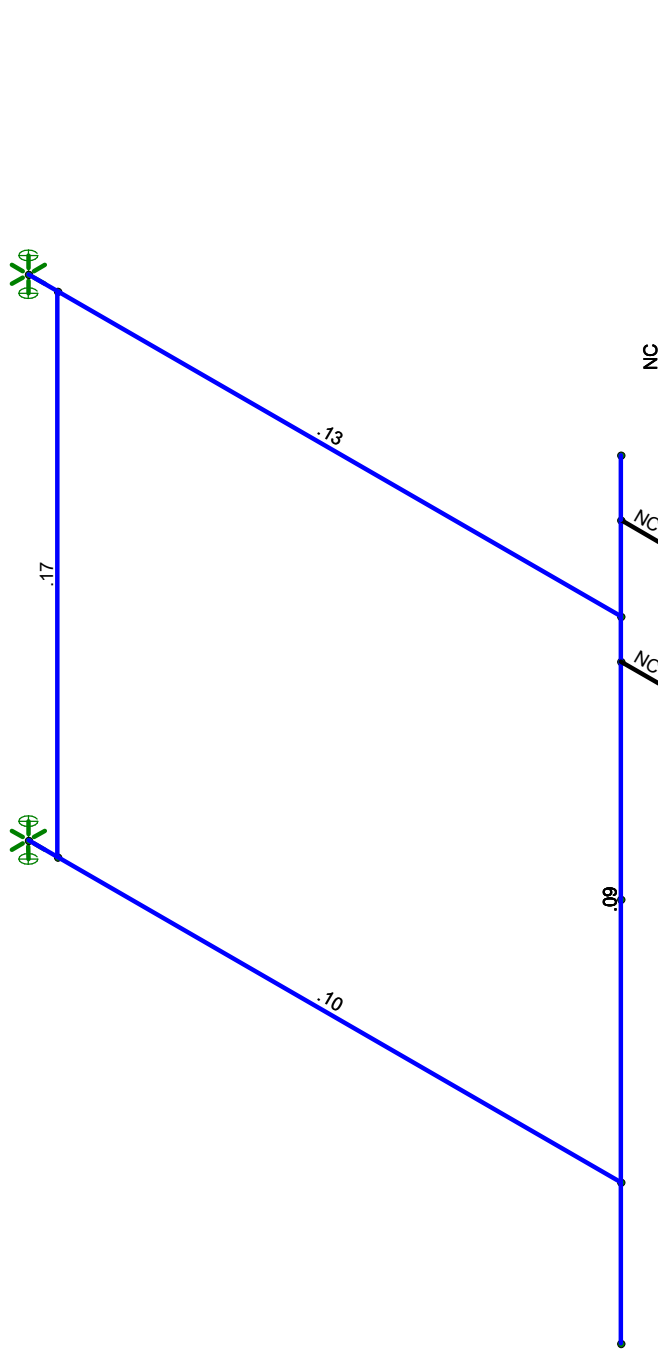


Envelope Only Solution

Black & Veatch	THOMPSONCSP USF-4U Model	SK - 2
Joochan Jung		Dec 1, 2020 at 11:29 AM
405025.2021.2200		THOMPSONCSP USF-4U Model.r3d

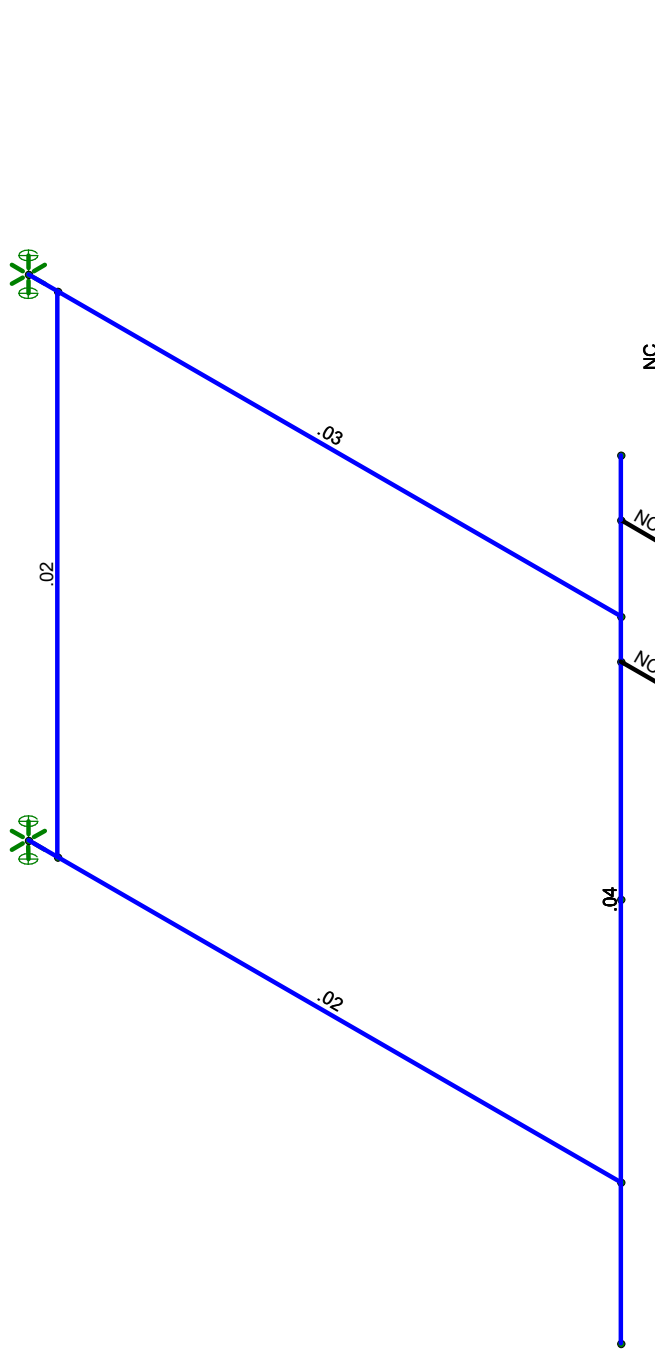
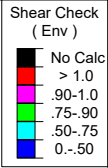
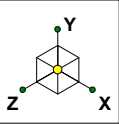


Code Check (Env)	
No Calc	
> 1.0	
.90-1.0	
.75-.90	
.50-.75	
0.-.50	



Member Code Checks Displayed (Enveloped)
Envelope Only Solution

Black & Veatch	THOMPSONCSP USF-4U Model	SK - 3
JooHwan Jung		Dec 1, 2020 at 11:29 AM
405025.2021.2200		THOMPSONCSP USF-4U Model.r3d

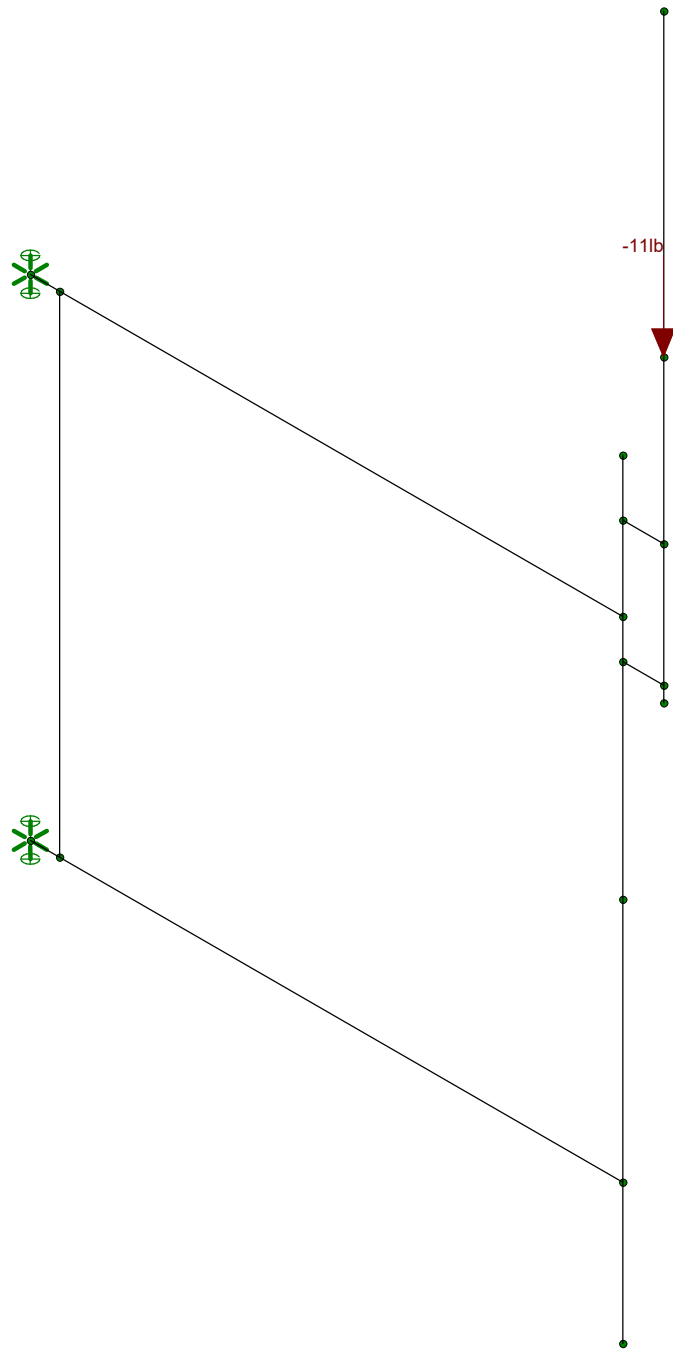
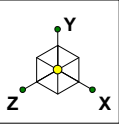


Member Shear Checks Displayed (Enveloped)
Envelope Only Solution

Black & Veatch
JooHwan Jung
405025.2021.2200

THOMPSONCSP USF-4U Model

SK - 4
Dec 1, 2020 at 11:29 AM
THOMPSONCSP USF-4U Model.r3d



Loads: BLC 1, DL
Envelope Only Solution

Black & Veatch
Joochan Jung
405025.2021.2200

THOMPSONCSP USF-4U Model

SK - 5
Dec 1, 2020 at 11:29 AM
THOMPSONCSP USF-4U Model.r3d

(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (in/sec^2)	386.4
Wall Mesh Size (in)	24
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver

Hot Rolled Steel Code	AISC 15th(360-16): LRFD
Adjust Stiffness?	Yes(Iterative)
RISACONNECTION CODE	None
Cold Formed Steel Code	None
Wood Code	None
Wood Temperature	< 100F
Concrete Code	None
Masonry Code	None
Aluminum Code	None - Building
Stainless Steel Code	None

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parame Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR SET ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

(Global) Model Settings, Continued

Seismic Code	ASCE 7-16
Seismic Base Elevation (in)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
R X	3
R Z	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	I or II
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	4
Cd X	4
Rho Z	1
Rho X	1

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (/1...	Density[k/ft^3]	Yield[ksi]	Ry	Fu[ksi]	Rt
1	A992	29000	11154	.3	.65	.49	50	1.1	65	1.1
2	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
3	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	65	1.1
4	A500 Gr.B RND	29000	11154	.3	.65	.527	42	1.4	58	1.3
5	A500 Gr.B Rect	29000	11154	.3	.65	.527	46	1.4	58	1.3
6	A53 Gr.B	29000	11154	.3	.65	.49	35	1.6	60	1.2
7	A1085	29000	11154	.3	.65	.49	50	1.4	65	1.3

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design ...	A [in2]	Iyy [in4]	Izz [in4]	J [in4]
1	Arm	HSS3X3X3	Beam	SquareTube	A53 Gr.B	Typical	1.89	2.46	2.46	4.03
2	Bracing	PIPE_2.0	Column	Pipe	A53 Gr.B	Typical	1.02	.627	.627	1.25
3	Mount Pipe	PIPE_3.0	Column	Pipe	A53 Gr.B	Typical	2.07	2.85	2.85	5.69

General Material Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (/1E5 F)	Density[k/ft^3]
1	gen_Conc3NW	3155	1372	.15	.6	.145
2	gen_Conc4NW	3644	1584	.15	.6	.145
3	gen_Conc3LW	2085	906	.15	.6	.11
4	gen_Conc4LW	2408	1047	.15	.6	.11
5	gen_Alum	10100	4077	.3	1.29	.173
6	gen_Steel	29000	11154	.3	.65	.49
7	gen_Plywood	1800	38	0	.3	.035
8	RIGID	1e+6		.3	0	0

Joint Boundary Conditions

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
1	N1	Reaction	Reaction	Reaction		Reaction	
2	N3	Reaction	Reaction	Reaction		Reaction	

Member Primary Data

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M1	N1	N2			Arm	Beam	SquareTube	A53 Gr.B	Typical
2	M2	N3	N4			Arm	Beam	SquareTube	A53 Gr.B	Typical
3	M3	N5	N6			Bracing	Column	Pipe	A53 Gr.B	Typical
4	M4	N7	N8			Mount Pipe	Column	Pipe	A53 Gr.B	Typical
5	M5	N9	N10			RIGID	None	None	RIGID	Typical
6	M6	N12	N13			RIGID	None	None	RIGID	Typical
7	M7	N15	N14			RIGID	None	None	RIGID	Typical

Member Advanced Data

	Label	I Release	J Release	I Offset[in]	J Offset[in]	T/C Only	Physical	Defl Rat...	Analysis ...	Inactive	Seismic...
1	M1						Yes				None
2	M2						Yes				None
3	M3						Yes	** NA **			None
4	M4						Yes	** NA **			None
5	M5						Yes	** NA **			None
6	M6						Yes	** NA **			None
7	M7						Yes	** NA **			None

Hot Rolled Steel Design Parameters

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in]	L-torqu...	Kyy	Kzz	Cb	Function
1	M1	Arm	43.5			Lbyy						Lateral
2	M2	Arm	43.5			Lbyy						Lateral
3	M3	Bracing	36									Lateral
4	M4	Mount Pipe	56.5									Lateral

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed Area(Me...	Surface(...
1	DL	DL		-1		1			
2	Maintenance LL - LV	LL				1			
3	Installation LL - LM	LL				1			
4	Wind - 0 Deg (X)	WL				1		4	
5	Wind - 30 Deg (X)	WL				1		4	
6	Wind - 60 Deg (X)	WL				1		4	
7	Wind - 90 Deg (X)	WL				1		4	
8	Wind - 120 Deg (X)	WL				1		4	
9	Wind - 150 Deg (X)	WL				1		4	
10	Wind - 180 Deg (X)	WL				1		4	
11	Wind - 210 Deg (X)	WL				1		4	
12	Wind - 240 Deg (X)	WL				1		4	
13	Wind - 270 Deg (X)	WL				1		4	
14	Wind - 300 Deg (X)	WL				1		4	
15	Wind - 330 Deg (X)	WL				1		4	
16	Wind - 0 Deg (Z)	WL				1		4	
17	Wind - 30 Deg (Z)	WL				1		4	
18	Wind - 60 Deg (Z)	WL				1		4	



Basic Load Cases (Continued)

BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed Area(Me... Surface(...
19 Wind - 90 Deg (Z)	WL				1		4
20 Wind - 120 Deg (Z)	WL				1		4
21 Wind - 150 Deg (Z)	WL				1		4
22 Wind - 180 Deg (Z)	WL				1		4
23 Wind - 210 Deg (Z)	WL				1		4
24 Wind - 240 Deg (Z)	WL				1		4
25 Wind - 270 Deg (Z)	WL				1		4
26 Wind - 300 Deg (Z)	WL				1		4
27 Wind - 330 Deg (Z)	WL				1		4
28 Ice DL	DL				1		4
29 Ice Wind - 0 Deg (X)	WL				1		4
30 Ice Wind - 30 Deg (X)	WL				1		4
31 Ice Wind - 60 Deg (X)	WL				1		4
32 Ice Wind - 90 Deg (X)	WL				1		4
33 Ice Wind - 120 Deg (X)	WL				1		4
34 Ice Wind - 150 Deg (X)	WL				1		4
35 Ice Wind - 180 Deg (X)	WL				1		4
36 Ice Wind - 210 Deg (X)	WL				1		4
37 Ice Wind - 240 Deg (X)	WL				1		4
38 Ice Wind - 270 Deg (X)	WL				1		4
39 Ice Wind - 300 Deg (X)	WL				1		4
40 Ice Wind - 330 Deg (X)	WL				1		4
41 Ice Wind - 0 Deg (Z)	WL				1		4
42 Ice Wind - 30 Deg (Z)	WL				1		4
43 Ice Wind - 60 Deg (Z)	WL				1		4
44 Ice Wind - 90 Deg (Z)	WL				1		4
45 Ice Wind - 120 Deg (Z)	WL				1		4
46 Ice Wind - 150 Deg (Z)	WL				1		4
47 Ice Wind - 180 Deg (Z)	WL				1		4
48 Ice Wind - 210 Deg (Z)	WL				1		4
49 Ice Wind - 240 Deg (Z)	WL				1		4
50 Ice Wind - 270 Deg (Z)	WL				1		4
51 Ice Wind - 300 Deg (Z)	WL				1		4
52 Ice Wind - 330 Deg (Z)	WL				1		4

Load Combinations

Description	S...PDe...	SRSS	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1 WIND LOAD COMBOS (140 MPH)																		
2 1.2DL + WL (0 DEG)	Y...	Y		1	1.2	4	1	16	1									
3 1.2DL + WL (30 DEG)	Y...	Y		1	1.2	5	1	17	1									
4 1.2DL + WL (60 DEG)	Y...	Y		1	1.2	6	1	18	1									
5 1.2DL + WL (90 DEG)	Y...	Y		1	1.2	7	1	19	1									
6 1.2DL + WL (120 DEG)	Y...	Y		1	1.2	8	1	20	1									
7 1.2DL + WL (150 DEG)	Y...	Y		1	1.2	9	1	21	1									
8 1.2DL + WL (180 DEG)	Y...	Y		1	1.2	10	1	22	1									
9 1.2DL + WL (210 DEG)	Y...	Y		1	1.2	11	1	23	1									
10 1.2DL + WL (240 DEG)	Y...	Y		1	1.2	12	1	24	1									
11 1.2DL + WL (270 DEG)	Y...	Y		1	1.2	13	1	25	1									
12 1.2DL + WL (300 DEG)	Y...	Y		1	1.2	14	1	26	1									
13 1.2DL + WL (330 DEG)	Y...	Y		1	1.2	15	1	27	1									
14																		
15 MOUNT LOAD COMBOS (30 MPH)																		
16 1.4DL	Y...	Y		1	1.4													
17 1.2DL + 1.5LV	Y...	Y		1	1.2	2	1.5											
18 1.2DL + 1.5LM + WL (0 DEG)	Y...	Y		1	1.2	3	1.5	4	.046	16	.046							



Load Combinations (Continued)

	Description	S...	PDe...	SRSS	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	
19	1.2DL + 1.5LM + WL (30 DEG)	Y...	Y		1	1.2	3	1.5	5	.046	17	.046										
20	1.2DL + 1.5LM + WL (60 DEG)	Y...	Y		1	1.2	3	1.5	6	.046	18	.046										
21	1.2DL + 1.5LM + WL (90 DEG)	Y...	Y		1	1.2	3	1.5	7	.046	19	.046										
22	1.2DL + 1.5LM + WL (120 DEG)	Y...	Y		1	1.2	3	1.5	8	.046	20	.046										
23	1.2DL + 1.5LM + WL (150 DEG)	Y...	Y		1	1.2	3	1.5	9	.046	21	.046										
24	1.2DL + 1.5LM + WL (180 DEG)	Y...	Y		1	1.2	3	1.5	10	.046	22	.046										
25	1.2DL + 1.5LM + WL (210 DEG)	Y...	Y		1	1.2	3	1.5	11	.046	23	.046										
26	1.2DL + 1.5LM + WL (240 DEG)	Y...	Y		1	1.2	3	1.5	12	.046	24	.046										
27	1.2DL + 1.5LM + WL (270 DEG)	Y...	Y		1	1.2	3	1.5	13	.046	25	.046										
28	1.2DL + 1.5LM + WL (300 DEG)	Y...	Y		1	1.2	3	1.5	14	.046	26	.046										
29	1.2DL + 1.5LM + WL (330 DEG)	Y...	Y		1	1.2	3	1.5	15	.046	27	.046										
30																						
31	ICE LOAD COMBOS (2", 50 MPH)																					
32	1.2DL + Ice DL + Ice WL (0 DEG)	Y...	Y		1	1.2	28	1	29	1	41	1										
33	1.2DL + Ice DL + Ice WL (30 DEG)	Y...	Y		1	1.2	28	1	30	1	42	1										
34	1.2DL + Ice DL + Ice WL (60 DEG)	Y...	Y		1	1.2	28	1	31	1	43	1										
35	1.2DL + Ice DL + Ice WL (90 DEG)	Y...	Y		1	1.2	28	1	32	1	44	1										
36	1.2DL + Ice DL + Ice WL (120 DEG)	Y...	Y		1	1.2	28	1	33	1	45	1										
37	1.2DL + Ice DL + Ice WL (150 DEG)	Y...	Y		1	1.2	28	1	34	1	46	1										
38	1.2DL + Ice DL + Ice WL (180 DEG)	Y...	Y		1	1.2	28	1	35	1	47	1										
39	1.2DL + Ice DL + Ice WL (210 DEG)	Y...	Y		1	1.2	28	1	36	1	48	1										
40	1.2DL + Ice DL + Ice WL (240 DEG)	Y...	Y		1	1.2	28	1	37	1	49	1										
41	1.2DL + Ice DL + Ice WL (270 DEG)	Y...	Y		1	1.2	28	1	38	1	50	1										
42	1.2DL + Ice DL + Ice WL (300 DEG)	Y...	Y		1	1.2	28	1	39	1	51	1										
43	1.2DL + Ice DL + Ice WL (330 DEG)	Y...	Y		1	1.2	28	1	40	1	52	1										
44																						

Envelope Joint Reactions

Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-ft]	LC	MY [lb-ft]	LC	MZ [lb-ft]	LC	
1	N1	max	202.383	2	291.863	38	302.166	5	0	43	667.538	11	0	43
2		min	-559.263	38	2.819	2	-302.166	11	0	2	-667.538	5	0	2
3	N3	max	552.813	17	295.242	32	125.067	5	0	43	392.418	11	0	43
4		min	-25.514	8	5.454	8	-125.067	11	0	2	-392.418	5	0	2
5	Totals:	max	427.235	2	552.076	38	427.233	5						
6		min	-427.235	8	121.444	2	-427.233	11						

Envelope AISC 15th(360-16): LRFD Steel Code Checks

Member	Shape	Code Check	Loc[in]	LC	Shear..	Loc[...]	Dir	LC	phi*Pn...	phi*Pnt...	phi*Mn...	phi*Mn...Cb	Eqn	
1	M1	HSS3X3X3	.130	0	11	.028	2.266	z	11	55265....	59535	5171.25	5171.25	2...H1-1b
2	M2	HSS3X3X3	.099	43.5	17	.018	0	y	32	55265....	59535	5171.25	5171.25	2...H1-1b
3	M3	PIPE 2.0	.171	0	17	.022	0		17	28843....	32130	1871.6...	1871.6...	2...H1-1b
4	M4	PIPE 3.0	.086	45.906	17	.038	10.5...		17	57908....	65205	5748.75	5748.75	1...H1-1b

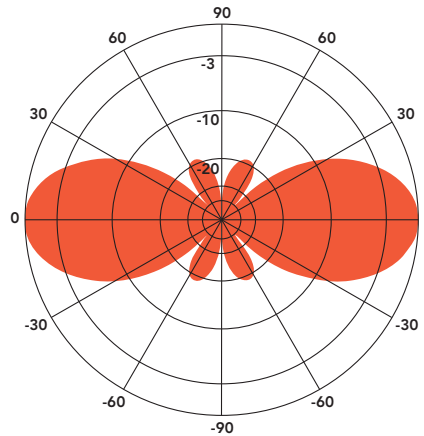
**APPENDIX 3:
ATTACHMENTS**

ANT220F2DIN FIBERGLASS COLLINEAR ANTENNA 2.5 dBd

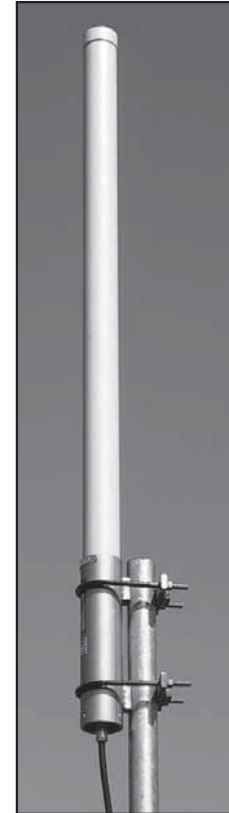
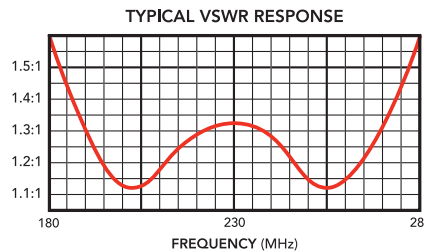
The Telewave ANT220F2 is an extremely rugged collinear antenna, with moderate gain and wide vertical beamwidth. This compact antenna produces 2.5 dBd gain, and is designed for operation in all environmental conditions. The antenna is constructed with brass and copper elements, with a path to ground potential for lightning impulse protection. The ANT220F2 is an excellent choice for wireless PTC systems in urban or rural areas.

All junctions are fully soldered to prevent RF intermodulation, and each antenna is completely protected within a rugged, high-tech radome to ensure survivability in the worst environments. The "Cool Blue" radome provides maximum protection from corrosive gases, ultraviolet radiation, icing, salt spray, acid rain, and wind blown abrasives.

The ANT220F2 includes the ANTC485 dual clamp set for mounting to a 1.5" to 3" O.D. support pipe, and a 24" removable RG-213 DIN-Male jumper.



ANT220F2 - 230 MHz
Vertical Plane
Gain = 2.58 dBd

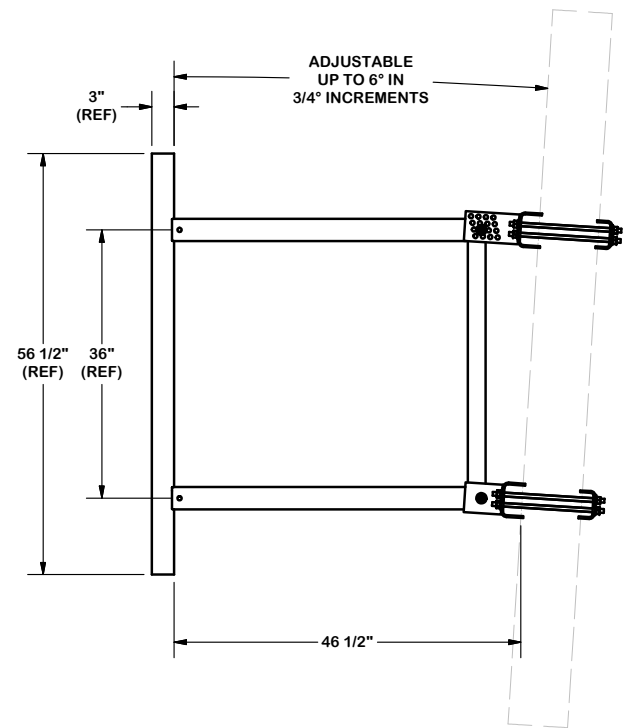
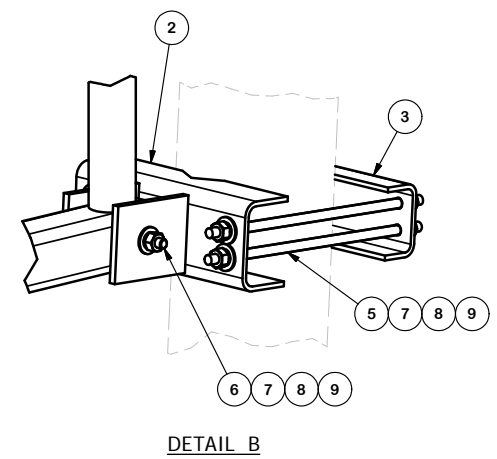
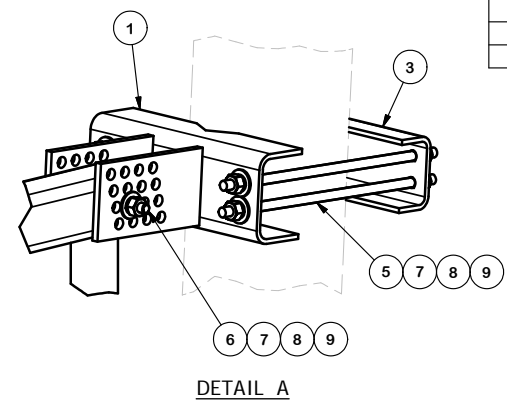
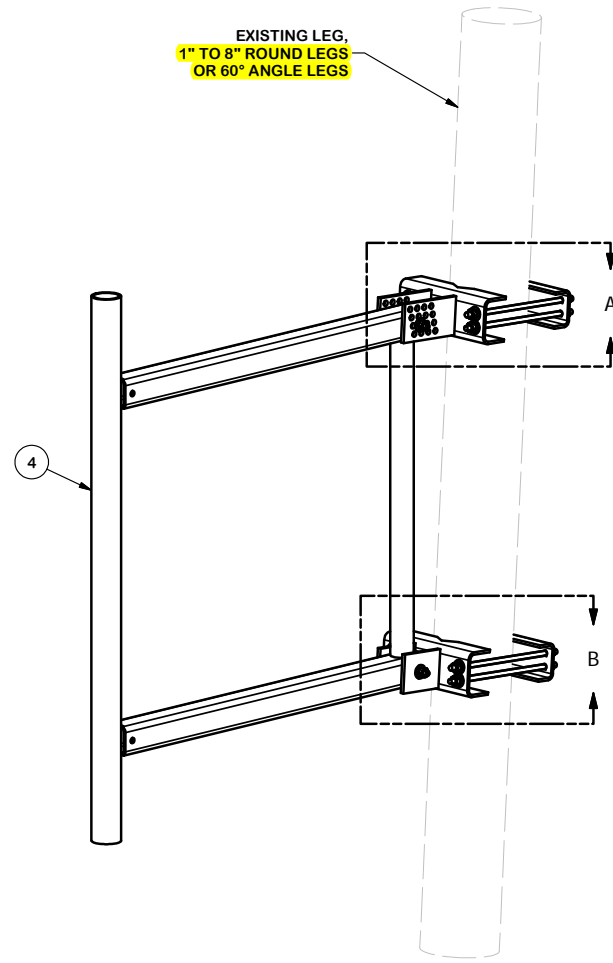


ONE SITE PRO 1 P/N DCP12K CLAMP SET REQUIRED.

SPECIFICATIONS			
Frequency (continuous)	195-260 MHz	Dimensions (L x base diam.) in.	51 x 2.75
Gain	2.5 dBd	Tower weight (antenna + clamps)	11 lb.
Power rating (typ.)	500 watts	Shipping weight	14 lb.
Impedance	50 ohms	Wind rating / with 0.5" ice	200 / 150 MPH
VSWR	1.5:1 or less	Maximum exposed area	1.1 ft. ²
Pattern	Omnidirectional	Lateral thrust at 100 MPH	44 lb.
Vertical beamwidth	38°	Bending moment at top clamp	47 ft. lb.
Termination	7-16 DIN-F	(100 MPH, 40 PSF flat plate equiv.)	

TOWER/MAST SIZE AT PROPOSED ANTENNA ATTACHMENT = 5.0"± DIAMETER.

PARTS LIST						
ITEM	QTY	PART NO.	PART DESCRIPTION	LENGTH	UNIT WT.	NET WT.
1	1	CFM	UPPER GATE FOOT WELDMENT		13.90	13.90
2	1	CFS	LOWER GATE FOOT WELDMENT		12.72	12.72
3	2	GBB	GATE BACKING BAR		4.53	9.06
4	1	4PBG	48" PIPE MOUNT STANDOFF ARM		113.96	113.96
5	8	G12R-12	1/2" x 12" GALV. THREADED ROD		0.67	5.35
5	8	G12R-15	1/2" x 15" GALV. THREADED ROD		0.84	6.69
6	2	A1205	1/2" x 5" A325 HDG BOLT		0.34	0.69
7	18	G12FW	1/2" HDG USS FLATWASHER		0.03	0.61
8	18	G12LW	1/2" HDG LOCKWASHER		0.01	0.25
9	18	G12NUT	1/2" HDG HEAVY 2H HEX NUT		0.07	1.29
					TOTAL WT. #	164.53

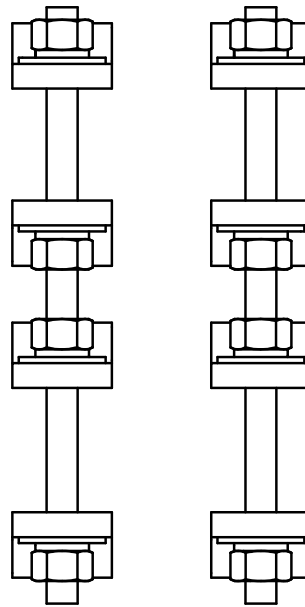
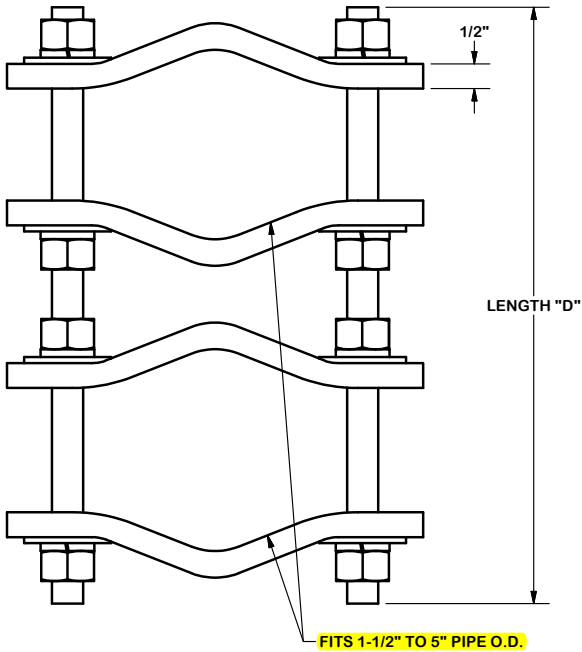
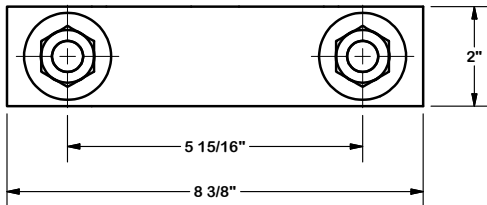
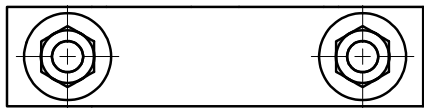


TOLERANCE NOTES
 TOLERANCES ON DIMENSIONS, UNLESS OTHERWISE NOTED ARE:
 SAWED, SHEARED AND GAS CUT EDGES ($\pm 0.030"$)
 DRILLED AND GAS CUT HOLES ($\pm 0.030"$) - NO CONING OF HOLES
 LASER CUT EDGES AND HOLES ($\pm 0.010"$) - NO CONING OF HOLES
 BENDS ARE $\pm 1/2$ DEGREE
 ALL OTHER MACHINING ($\pm 0.030"$)
 ALL OTHER ASSEMBLY ($\pm 0.060"$)

PROPRIETARY NOTE:
 THE DATA AND TECHNIQUES CONTAINED IN THIS DRAWING ARE PROPRIETARY INFORMATION OF VALMONT INDUSTRIES AND CONSIDERED A TRADE SECRET. ANY USE OR DISCLOSURE WITHOUT THE CONSENT OF VALMONT INDUSTRIES IS STRICTLY PROHIBITED.

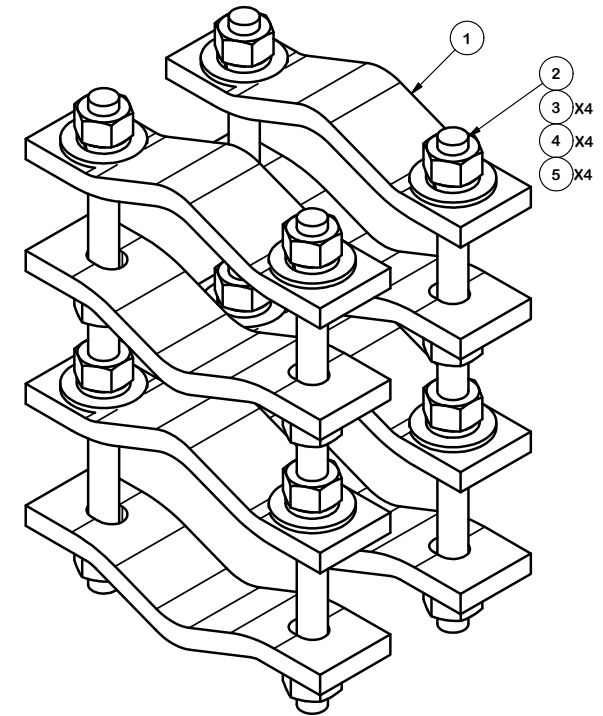
DESCRIPTION 48" ULTIMATE UNIVERSAL STANDOFF FRAME		
CPD NO.	DRAWN BY RCH	ENG. APPROVAL
CLASS 81	SUB 01	CHECKED BY BMC
DRAWING USAGE CUSTOMER		DATE 2/16/2011

<p>Engineering Support Team: 1-888-753-7446</p> <p>A valmont COMPANY</p>	Locations: New York, NY Atlanta, GA Los Angeles, CA Plymouth, IN Salem, OR Dallas, TX
	PART NO. USF-4U DWG. NO. USF-4U



PARTS LIST						
ITEM	QTY	PART NO.	PART DESCRIPTION	LENGTH	UNIT WT.	NET WT.
1	8	DCP	CLAMP HALF, 1/2" THICK, 8-3/8"		2.40	19.20
2	B	C	5/8" THREADED ROD	D	E	F
3	16	G58NUT	5/8" HDG HEAVY 2H HEX NUT		0.13	2.08
4	16	G58LW	5/8" HDG LOCKWASHER		0.03	0.42
5	16	G58FW	5/8" HDG USS FLATWASHER		0.07	1.13

VARIABLE PARTS TABLE						
ASSEMBLY "A"	QTY "B"	PART "C"	LENGTH "D"	UNIT WT. "E"	NET WT. "F"	TOTAL WEIGHT
DCP12K	4	G58R-12	12"	1.05	4.18	27.01
DCP18K	4	G58R-18	18"	1.57	6.27	29.10



TOLERANCE NOTES

TOLERANCES ON DIMENSIONS, UNLESS OTHERWISE NOTED ARE:
 SAWED, SHEARED AND GAS CUT EDGES ($\pm 0.030"$)
 DRILLED AND GAS CUT HOLES ($\pm 0.030"$) - NO CONING OF HOLES
 LASER CUT EDGES AND HOLES ($\pm 0.010"$) - NO CONING OF HOLES
 BENDS ARE $\pm 1/2$ DEGREE
 ALL OTHER MACHINING ($\pm 0.030"$)
 ALL OTHER ASSEMBLY ($\pm 0.060"$)

PROPRIETARY NOTE:
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DESCRIPTION
PIPE TO PIPE CLAMP SET
 1-1/2" TO 5" PIPE
 1/2" THICK CLAMP

SITE PRO 1
 Engineering Support Team:
 1-888-753-7446

Locations:
 New York, NY
 Atlanta, GA
 Los Angeles, CA
 Plymouth, IN
 Salem, OR
 Dallas, TX

CPD NO.	DRAWN BY	ENG. APPROVAL
	KC8 8/21/2012	
CLASS	DRAWING USAGE	CHECKED BY
81	CUSTOMER	CEK 1/22/2013

PART NO.	SEE ASSEMBLY "A"
DWG. NO.	DCPxxK

ATTACHMENT D – CONSTRUCTION DRAWINGS



THOMPSON CSP

97 MOUNTAIN HILL ROAD

THOMPSON, CT 06255

EVERSOURCE
ENERGY

107 SELDEN STREET
BERLIN, CT 06037
PHONE: (800) 286-2000



BLACK & VEATCH

6800 W 115TH ST, SUITE 2292
OVERLAND PARK, KS 66211
PHONE: (913) 458-2522

PROJECT SUMMARY

- THE GENERAL SCOPE OF WORK CONSISTS OF THE FOLLOWING:
1. INSTALL (2) NEW OMNI/WHIP ANTENNAS, (1) AT ELEVATION 159'-1 1/2"± AGL AND (1) AT ELEVATION 136'-1 1/2"± AGL
 2. REMOVE (2) EXISTING ANTENNAS AND THEIR ASSOCIATED COAX, (1) AT ELEVATION 127'-0"± AGL AND (1) AT ELEVATION 47'-0"± AGL
 3. INSTALL (1) NEW RACK WITH DMR EQUIPMENT IN EXISTING TELECOM ROOM

GOVERNING CODES

2018 CONNECTICUT STATE BUILDING CODE (2015 IBC BASIS)
2017 NATIONAL ELECTRIC CODE
TIA-222-H

GENERAL NOTES

THE FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION. A TECHNICIAN WILL VISIT THE SITE AS REQUIRED FOR ROUTINE MAINTENANCE. THE PROJECT WILL NOT RESULT IN ANY SIGNIFICANT DISTURBANCE OR EFFECT ON DRAINAGE; NO SANITARY SEWER SERVICE, POTABLE WATER, OR TRASH DISPOSAL IS REQUIRED AND NO COMMERCIAL SIGNAGE IS PROPOSED.

SITE INFORMATION

SITE NAME: THOMPSON CSP
SITE ID NUMBER: #848
SITE ADDRESS: 97 MOUNTAIN HILL ROAD
THOMPSON, CT 06255
MAP: 42
BLOCK: 88
LOT: 165
ZONE: RAB0
LATITUDE: 41° 59' 11.76" N
LONGITUDE: 71° 54' 49.11" W
ELEVATION: 558'± AMSL
FEMA/FIRM DESIGNATION: C
ACREAGE: 0.23± AC (BOOK: 0248, PAGE: 0073)

CONTACT INFORMATION

APPLICANTS:
EVERSOURCE ENERGY
107 SELDEN STREET
BERLIN, CT 06037
POWER PROVIDER:
EVERSOURCE ENERGY
(800) 286-2000
PROPERTY OWNER:
CONNECTICUT STATE POLICE
165 CAPITOL AVE
HARTFORD, CT 06106
TELCO PROVIDER:
FRONTIER
(800) 921-8102
EVERSOURCE ENERGY
PROJECT MANAGER:
NIKOLL PRECI
(860) 655-3079
CALL BEFORE YOU DIG:
(800) 922-4455

LOCATION MAP



NO SCALE

DESIGN TYPE

SITE UPGRADE
SELF-SUPPORT TOWER

DRAWING INDEX

SHEET NO:	SHEET TITLE
T-1	TITLE SHEET
C-1	SITE PLAN
C-2	TOWER ELEVATION
G-1	GROUNDING DETAILS
N-1	NOTES & SPECIFICATIONS
N-2	NOTES & SPECIFICATIONS
N-3	NOTES & SPECIFICATIONS

DO NOT SCALE DRAWINGS

SUBCONTRACTOR SHALL VERIFY ALL PLANS & EXISTING DIMENSIONS & CONDITIONS ON THE JOB SITE & SHALL IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME

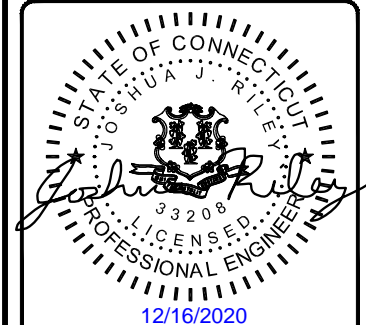


UNDERGROUND SERVICE ALERT
UTILITIES PROTECTION CENTER, INC.
811

48 HOURS BEFORE YOU DIG

PROJECT NO: 405025
DRAWN BY: TYW
CHECKED BY: TH

REV	DATE	DESCRIPTION
0	12/16/20	ISSUED FOR FILING



IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT.

THOMPSON CSP
97 MOUNTAIN HILL ROAD
THOMPSON, CT 06255

SHEET TITLE
TITLE SHEET

SHEET NUMBER
T-1

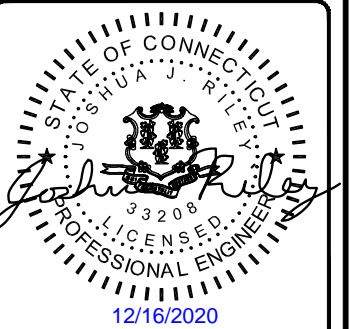


PROJECT NO: 405025

DRAWN BY: TYW

CHECKED BY: TH

REV	DATE	DESCRIPTION
0	12/16/20	ISSUED FOR FILING

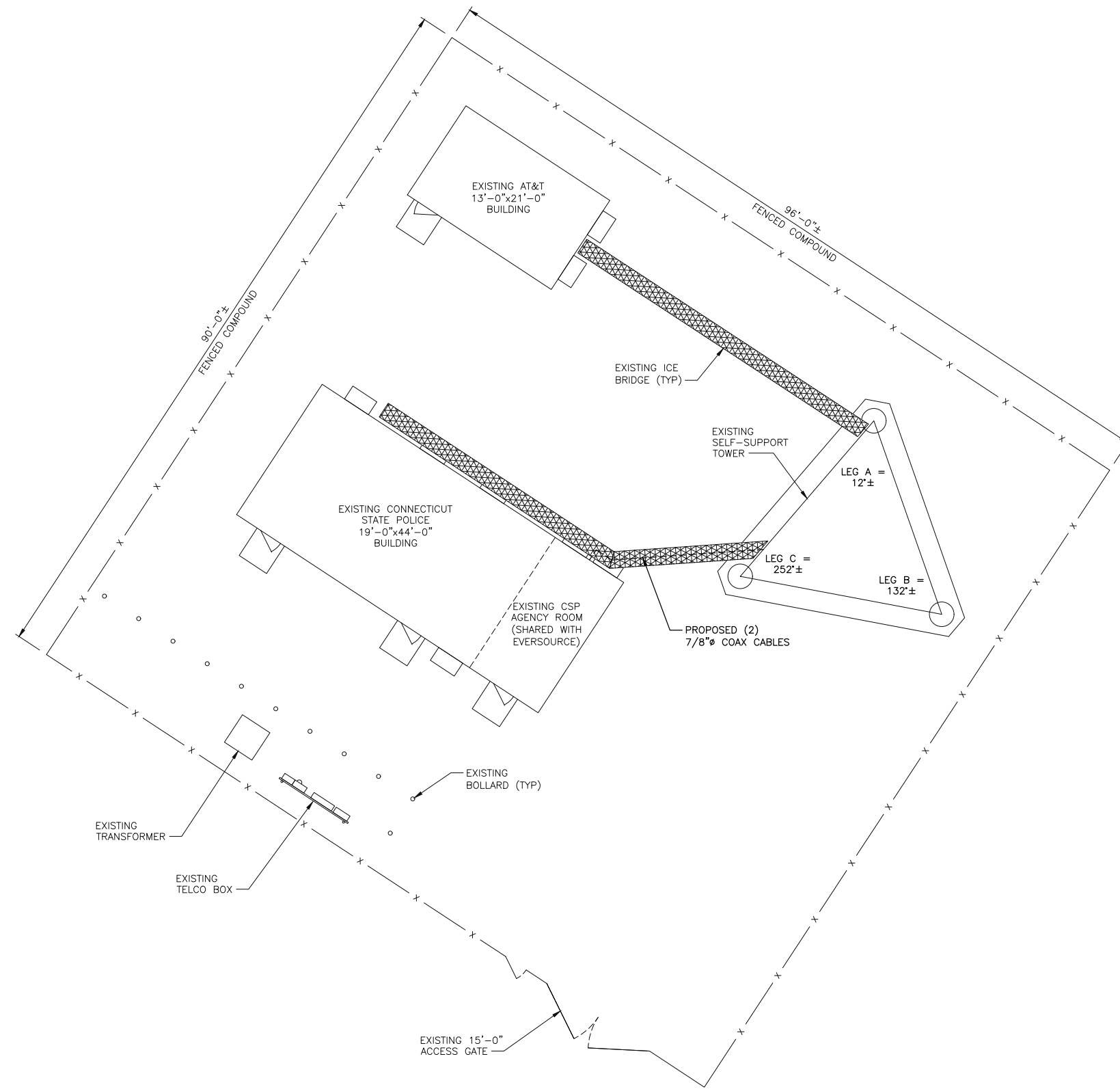


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THOMPSON CSP
97 MOUNTAIN HILL ROAD
THOMPSON, CT 06255

SHEET TITLE
SITE PLAN

SHEET NUMBER
C-1



SITE PLAN
NO SCALE



TOP OF EXISTING ANTENNA (NON-EVERSOURCE)
ELEVATION 195'-0"± AGL

TOP OF EXISTING ANTENNA (NON-EVERSOURCE)
ELEVATION 182'-0"± AGL
TOP OF EXISTING TOWER
ELEVATION 180'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 167'-0"± AGL

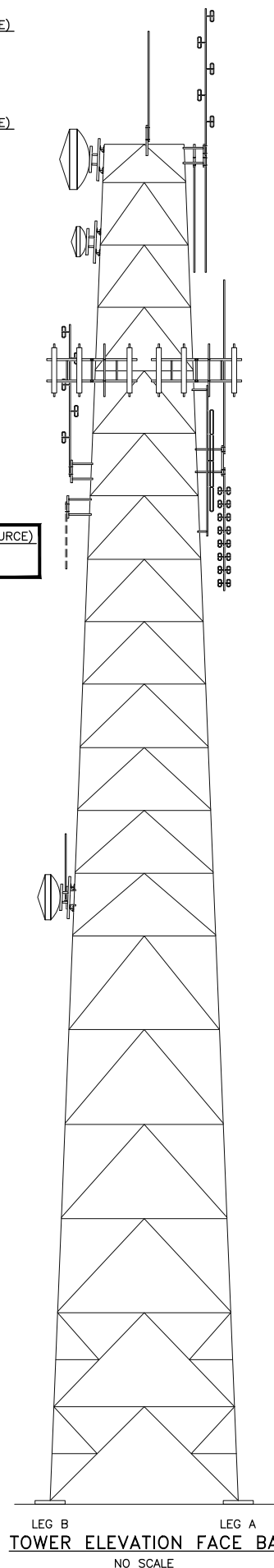
EXISTING ANTENNAS (NON-EVERSOURCE)
RAD CL ELEVATION 149'-0"± AGL
EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 146'-0"± AGL

EXISTING ABANDONED ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 127'-0"± AGL
(ANTENNA AND COAX TO BE REMOVED)

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 87'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 80'-0"± AGL

EXISTING GRADE
ELEVATION 558'-0"± AMSL



LEG B LEG A
TOWER ELEVATION FACE BA
NO SCALE

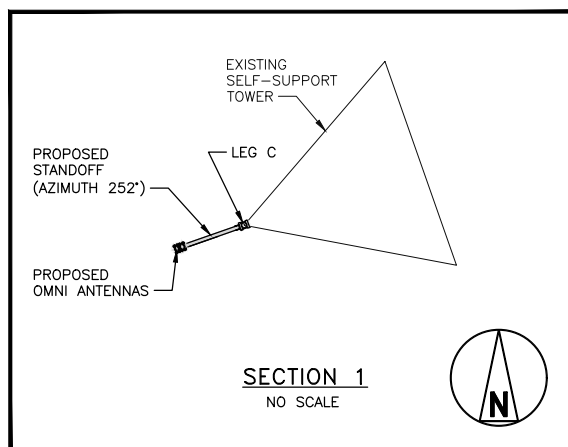
TOP OF EXISTING ANTENNA (NON-EVERSOURCE)
ELEVATION 198'-0"± AGL

EXISTING ANTENNAS (NON-EVERSOURCE)
RAD CL ELEVATION 170'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 151'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 138'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 127'-0"± AGL



SECTION 1
NO SCALE

TOP OF EXISTING ANTENNA (NON-EVERSOURCE)
ELEVATION 198'-0"± AGL

TOP OF EXISTING TOWER
ELEVATION 180'-0"± AGL

EXISTING ANTENNAS (NON-EVERSOURCE)
RAD CL ELEVATION 170'-0"± AGL

TOP OF PROPOSED EVERSOURCE
OMNI / WHIP ANTENNA
ELEVATION 159'-1 1/2" AGL
RX RAD CL ELEVATION 157'-0" AGL
(ANTENNA MECHANICAL LENGTH 4'-3")

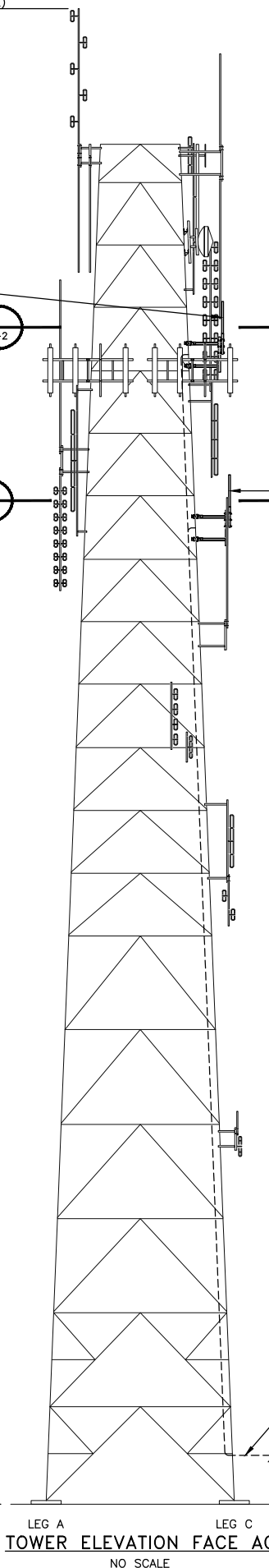
EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 151'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 138'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 127'-0"± AGL

198'-0"± AGL
TOTAL HEIGHT WITH APPURTENANCES

EXISTING GRADE
ELEVATION 558'-0"± AMSL



LEG A LEG C
TOWER ELEVATION FACE AC
NO SCALE

TOP OF EXISTING ANTENNA (NON-EVERSOURCE)
ELEVATION 192'-0"± AGL

TOP OF EXISTING ANTENNA (NON-EVERSOURCE)
ELEVATION 181'-0"± AGL
TOP OF EXISTING ANTENNA (NON-EVERSOURCE)
ELEVATION 180'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 170'-0"± AGL
EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 169'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 158'-0"± AGL

EXISTING ANTENNAS (NON-EVERSOURCE)
RAD CL ELEVATION 149'-0"± AGL
EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 147'-0"± AGL

TOP OF PROPOSED EVERSOURCE
OMNI / WHIP ANTENNA
ELEVATION 136'-1 1/2" AGL
TX RAD CL ELEVATION 134'-0" AGL
(ANTENNA MECHANICAL LENGTH 4'-3")

EXISTING EVERSOURCE ANTENNA
RAD CL ELEVATION 125'-0"± AGL

EXISTING EVERSOURCE ANTENNA
RAD CL ELEVATION 104'-0"± AGL
EXISTING EVERSOURCE ANTENNA
RAD CL ELEVATION 100'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 87'-6"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 79'-0"± AGL

EXISTING ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 50'-0"± AGL

EXISTING ABANDONED ANTENNA (NON-EVERSOURCE)
RAD CL ELEVATION 47'-0"± AGL
(ANTENNA AND COAX TO BE REMOVED)

PROPOSED (2) 7/8"Ø
COAX CABLES ROUTED TO
PROPOSED ANTENNAS

EVERSOURCE
ENERGY

107 SELDEN STREET
BERLIN, CT 06037
PHONE: (800) 286-2000



BLACK & VEATCH

6800 W 115TH ST, SUITE 2292
OVERLAND PARK, KS 66211
PHONE: (913) 458-2522

PROJECT NO:	405025
DRAWN BY:	TYW
CHECKED BY:	TH

REV	DATE	DESCRIPTION
0	12/16/20	ISSUED FOR FILING



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UNLESS THEY ARE ACTING UNDER THE DIRECTION
OF A LICENSED PROFESSIONAL ENGINEER,
TO ALTER THIS DOCUMENT.

THOMPSON CSP
97 MOUNTAIN HILL ROAD
THOMPSON, CT 06255

SHEET TITLE
TOWER ELEVATION &
ANTENNA EQUIPMENT

SHEET NUMBER
C-2

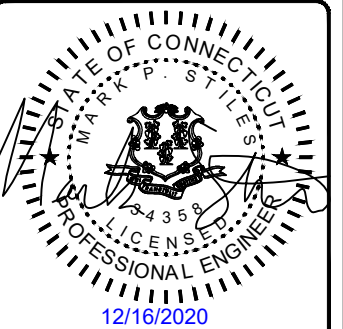


PROJECT NO: 405025

DRAWN BY: TYW

CHECKED BY: TH

REV	DATE	DESCRIPTION
0	12/16/20	ISSUED FOR FILING

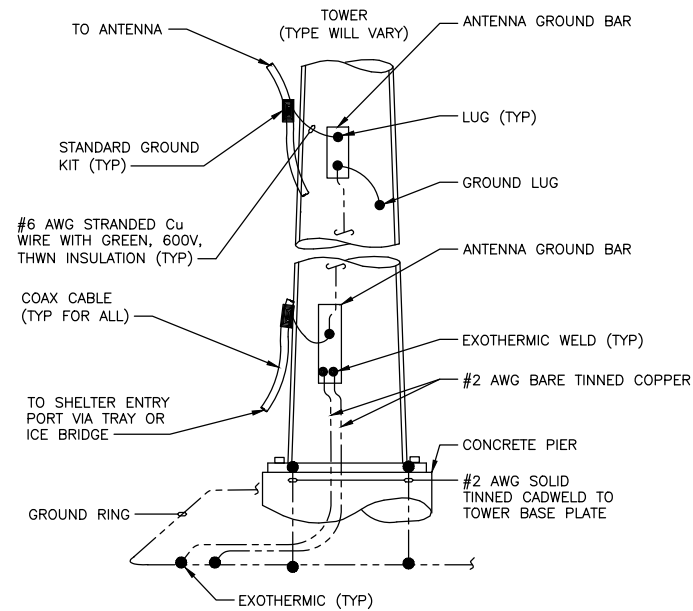


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THOMPSON CSP
97 MOUNTAIN HILL ROAD
THOMPSON, CT 06255

SHEET TITLE
**GROUNDING
DETAILS**

SHEET NUMBER
G-1

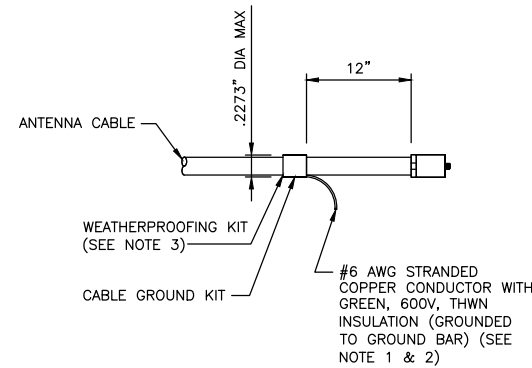


NOTE

1. NUMBER OF GROUND BARS MAY VARY DEPENDING ON THE TYPE OF TOWER, ANTENNA LOCATION AND CONNECTION ORIENTATION. PROVIDE AS REQUIRED.

ANTENNA CABLE GROUNDING

NO SCALE

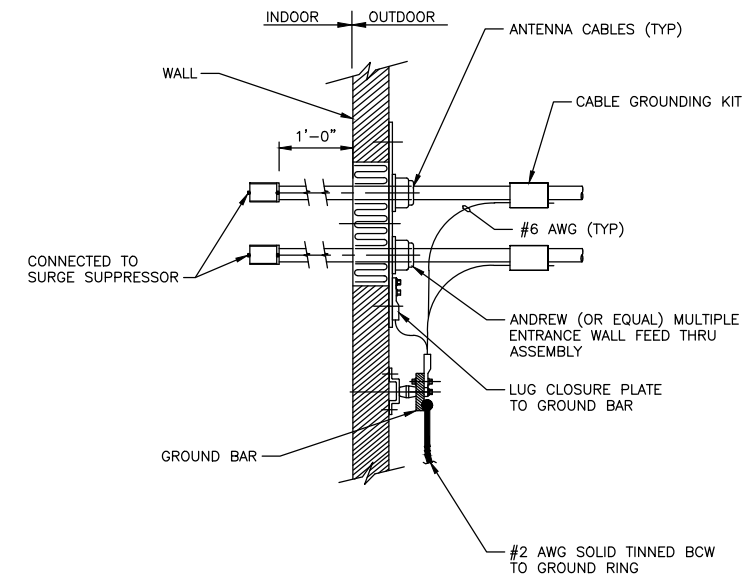


NOTES

- DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO GROUND BAR.
- GROUNDING KIT SHALL BE TYPE AND PART NUMBER AS SUPPLIED OR RECOMMENDED BY CABLE MANUFACTURER.
- WEATHER PROOFING SHALL BE TYPE AND PART NUMBER AS SUPPLIED OR RECOMMENDED BY CABLE MANUFACTURER.

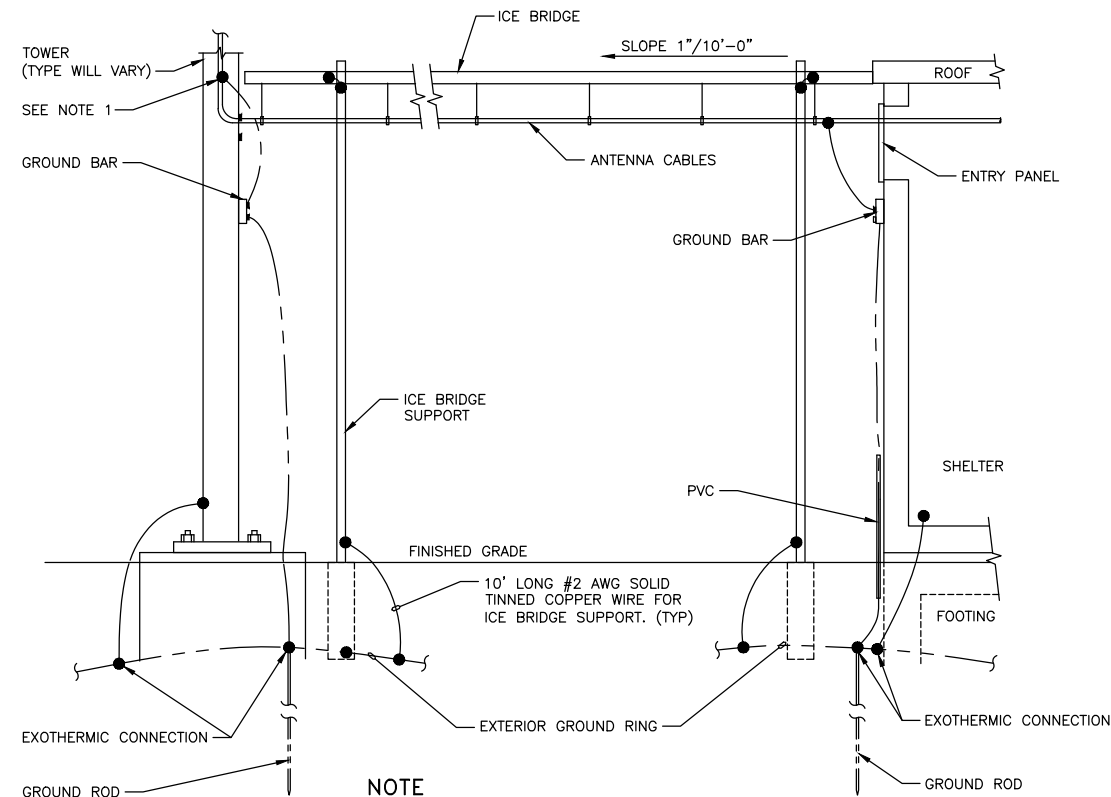
CONNECTION OF CABLE GROUND KIT TO ANTENNA CABLE

NO SCALE



CABLE INSTALLATION WITH WALL FEED THRU ASSEMBLY

NO SCALE



NOTE

1. PROVIDE GROUND KIT 6" BEFORE TURN

ICE BRIDGE AND ANTENNA CABLE DETAIL

NO SCALE

SYMBOLS

●	EXOTHERMIC CONNECTION
■	COMPRESSION CONNECTION
⊕	5/8"Øx10-0" COPPER CLAD STEEL GROUND ROD.
⊕	TEST GROUND ROD WITH INSPECTION SLEEVE
---	GROUNDING CONDUCTOR
Ⓐ	KEY NOTES
— X — X — X — X — X —	CHAINLINK FENCE
— □ — □ — □ — □ — □ —	WOOD FENCE
---	LEASE AREA
▨	ICE BRIDGE
▧	CABLE TRAY
— G — G — G — G — G —	GAS LINE
— E/T — E/T — E/T — E/T —	UNDERGROUND ELECTRICAL/TELCO
— E/C — E/C — E/C — E/C —	UNDERGROUND ELECTRICAL/CONTROL
— E — E — E — E — E —	UNDERGROUND ELECTRICAL
— T — T — T — T — T —	UNDERGROUND TELCO
---	PROPERTY LINE (PL)

ABBREVIATIONS

AC	ALTERNATING CURRENT	MGB	MASTER GROUNDING BAR
AIC	AMPERAGE INTERRUPTION CAPACITY	MIN	MINIMUM
ANI	AUXILIARY NETWORK INTERFACE	MW	MICROWAVE
ATM	ASYNCHRONOUS TRANSFER MODE	MTS	MANUAL TRANSFER SWITCH
ATS	AUTOMATIC TRANSFER SWITCH	NEC	NATIONAL ELECTRICAL CODE
AWG	AMERICAN WIRE GAUGE	OC	ON CENTER
AWS	ADVANCED WIRELESS SERVICES	PP	POLARIZING PRESERVING
BATT	BATTERY	PCU	PRIMARY CONTROL UNIT
BBU	BASEBAND UNIT	PDU	PROTOCOL DATA UNIT
BTC	BARE TINNED COPPER CONDUCTOR	PWR	POWER
BTS	BASE TRANSCEIVER STATION	RECT	RECTIFIER
CCU	CLIMATE CONTROL UNIT	RET	REMOTE ELECTRICAL TILT
CDMA	CODE DIVISION MULTIPLE ACCESS	RMC	RIGID METALLIC CONDUIT
CHG	CHARGING	RF	RADIO FREQUENCY
CLU	CLIMATE UNIT	RUC	RACK USER COMMISSIONING
COMM	COMMON	RRH	REMOTE RADIO HEAD
DC	DIRECT CURRENT	RRU	REMOTE RADIO UNIT
DIA	DIAMETER	RWY	RACEWAY
DWG	DRAWING	SFP	SMALL FORM-FACTOR PLUGGABLE
EC	ELECTRICAL CONDUCTOR	SIAD	SMART INTEGRATED ACCESS DEVICE
EMT	ELECTRICAL METALLIC TUBING	SSC	SITE SOLUTIONS CABINET
FIF	FACILITY INTERFACE FRAME	T1	1544KBPS DIGITAL LINE
GEN	GENERATOR	TDMA	TIME-DIVISION MULTIPLE ACCESS
GPS	GLOBAL POSITIONING SYSTEM	TMA	TOWER MOUNT AMPLIFIER
GSM	GLOBAL SYSTEM FOR MOBILE	TVSS	TRANSIENT VOLTAGE SUPPRESSION SYSTEM
HVAC	HEAT/VENTILATION/AIR CONDITIONING	TYP	TYPICAL
ICF	INTERCONNECTION FRAME	UMTS	UNIVERSAL MOBILE TELECOMMUNICATION SYSTEM
IGR	INTERIOR GROUNDING RING (HALO)	UPS	UNINTERRUPTIBLE POWER SUPPLY (DC POWER PLANT)
LTE	LONG TERM EVOLUTION		

EVERSOURCE ENERGY

107 SELDEN STREET
BERLIN, CT 06037
PHONE: (800) 286-2000

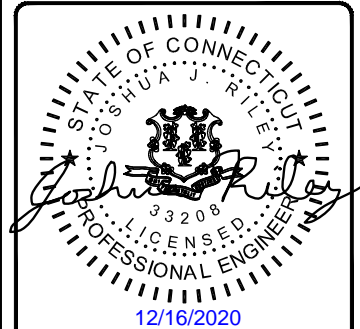


BLACK & VEATCH

6800 W 115TH ST, SUITE 2292
OVERLAND PARK, KS 66211
PHONE: (913) 458-2522

PROJECT NO:	405025
DRAWN BY:	TYW
CHECKED BY:	TH

REV	DATE	DESCRIPTION
0	12/16/20	ISSUED FOR FILING



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THOMPSON CSP
97 MOUNTAIN HILL ROAD
THOMPSON, CT 06255

SHEET TITLE
NOTES & SPECIFICATIONS

SHEET NUMBER
N-3

REFERENCE CUTSHEETS

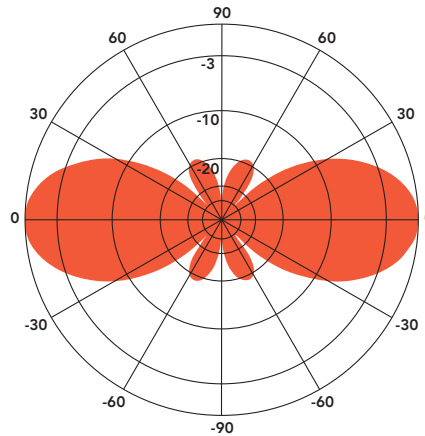
ANT220F2DIN

FIBERGLASS COLLINEAR ANTENNA 2.5 dBd

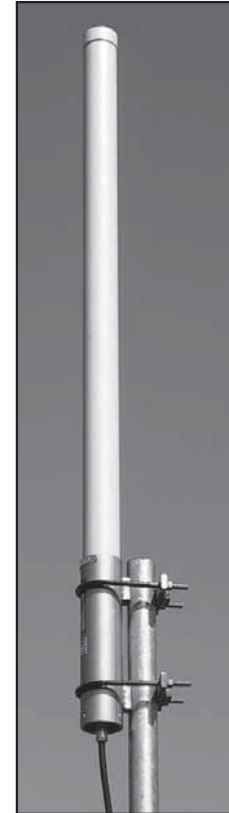
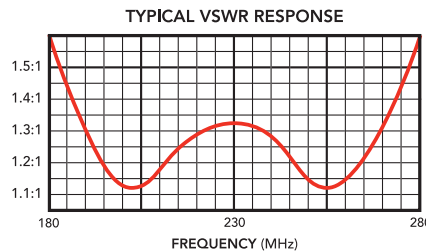
The Telewave ANT220F2 is an extremely rugged collinear antenna, with moderate gain and wide vertical beamwidth. This compact antenna produces 2.5 dBd gain, and is designed for operation in all environmental conditions. The antenna is constructed with brass and copper elements, with a path to ground potential for lightning impulse protection. The ANT220F2 is an excellent choice for wireless PTC systems in urban or rural areas.

All junctions are fully soldered to prevent RF intermodulation, and each antenna is completely protected within a rugged, high-tech radome to ensure survivability in the worst environments. The "Cool Blue" radome provides maximum protection from corrosive gases, ultraviolet radiation, icing, salt spray, acid rain, and wind blown abrasives.

The ANT220F2 includes the ANTC485 dual clamp set for mounting to a 1.5" to 3" O.D. support pipe, and a 24" removable RG-213 DIN-Male jumper.



ANT220F2 - 230 MHz
Vertical Plane
Gain = 2.58 dBd

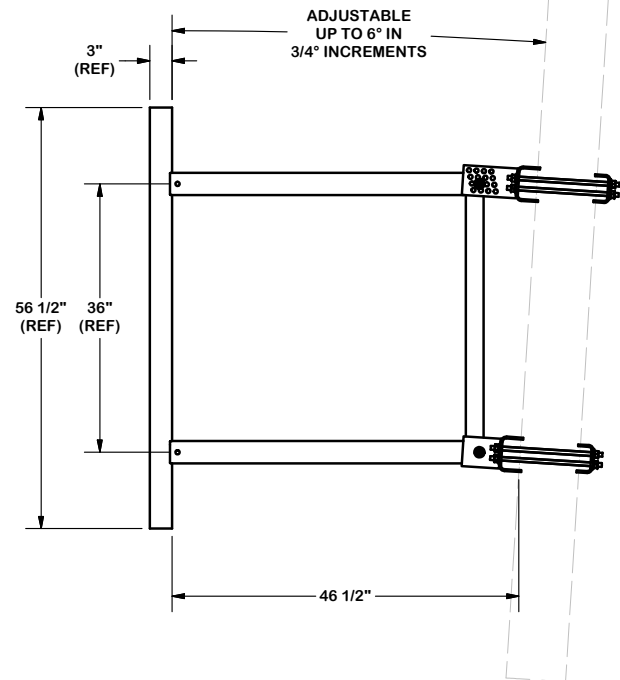
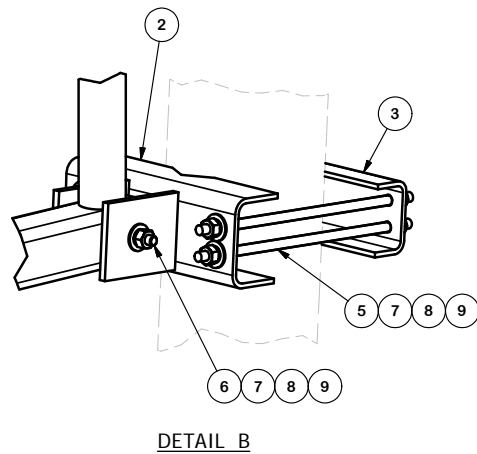
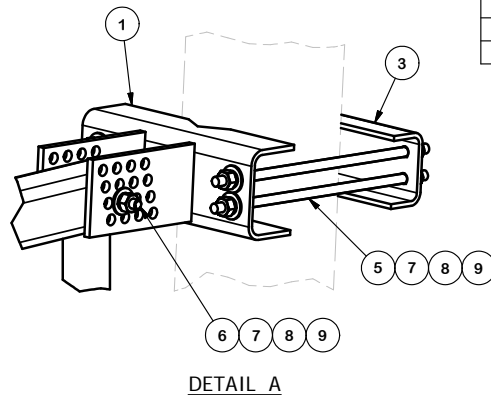
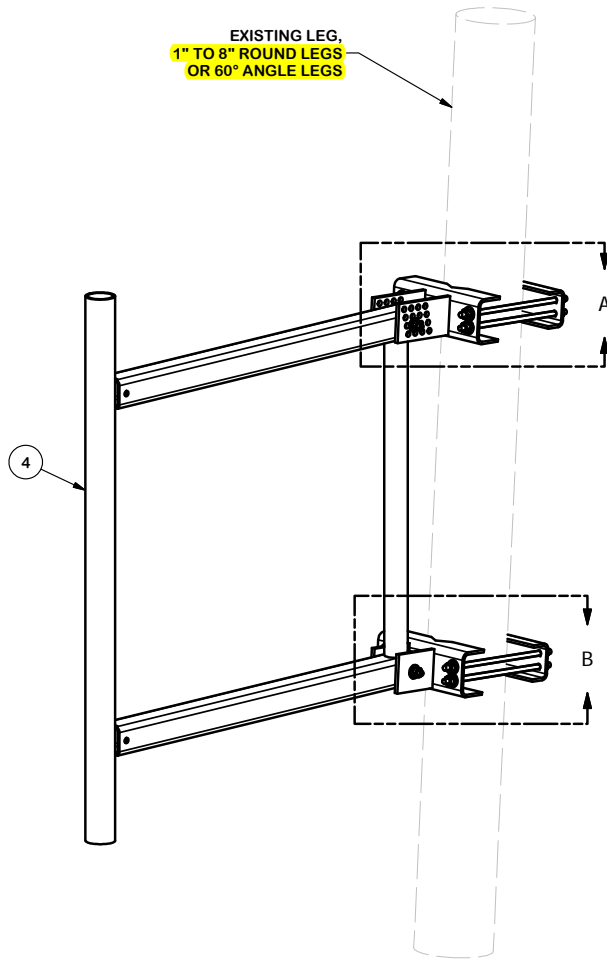


ONE SITE PRO 1 P/N DCP12K CLAMP SET REQUIRED.

SPECIFICATIONS			
Frequency (continuous)	195-260 MHz	Dimensions (L x base diam.) in.	51 x 2.75
Gain	2.5 dBd	Tower weight (antenna + clamps)	11 lb.
Power rating (typ.)	500 watts	Shipping weight	14 lb.
Impedance	50 ohms	Wind rating / with 0.5" ice	200 / 150 MPH
VSWR	1.5:1 or less	Maximum exposed area	1.1 ft. ²
Pattern	Omnidirectional	Lateral thrust at 100 MPH	44 lb.
Vertical beamwidth	38°	Bending moment at top clamp	47 ft. lb.
Termination	7-16 DIN-F	(100 MPH, 40 PSF flat plate equiv.)	

TOWER/MAST SIZE AT PROPOSED ANTENNA ATTACHMENT = 5.0"± DIAMETER.

EXISTING LEG,
1" TO 8" ROUND LEGS
OR 60° ANGLE LEGS



PARTS LIST						
ITEM	QTY	PART NO.	PART DESCRIPTION	LENGTH	UNIT WT.	NET WT.
1	1	CFM	UPPER GATE FOOT WELDMENT		13.90	13.90
2	1	CFS	LOWER GATE FOOT WELDMENT		12.72	12.72
3	2	GBB	GATE BACKING BAR		4.53	9.06
4	1	4PBG	48" PIPE MOUNT STANDOFF ARM		113.96	113.96
5	8	G12R-12	1/2" x 12" GALV. THREADED ROD		0.67	5.35
5	8	G12R-15	1/2" x 15" GALV. THREADED ROD		0.84	6.69
6	2	A1205	1/2" x 5" A325 HDG BOLT		0.34	0.69
7	18	G12FW	1/2" HDG USS FLATWASHER		0.03	0.61
8	18	G12LW	1/2" HDG LOCKWASHER		0.01	0.25
9	18	G12NUT	1/2" HDG HEAVY 2H HEX NUT		0.07	1.29
					TOTAL WT. #	164.53

TOLERANCE NOTES

TOLERANCES ON DIMENSIONS, UNLESS OTHERWISE NOTED ARE:
 SAWED, SHEARED AND GAS CUT EDGES ($\pm 0.030"$)
 DRILLED AND GAS CUT HOLES ($\pm 0.030"$) - NO CONING OF HOLES
 LASER CUT EDGES AND HOLES ($\pm 0.010"$) - NO CONING OF HOLES
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DESCRIPTION

48" ULTIMATE UNIVERSAL
STANDOFF FRAME

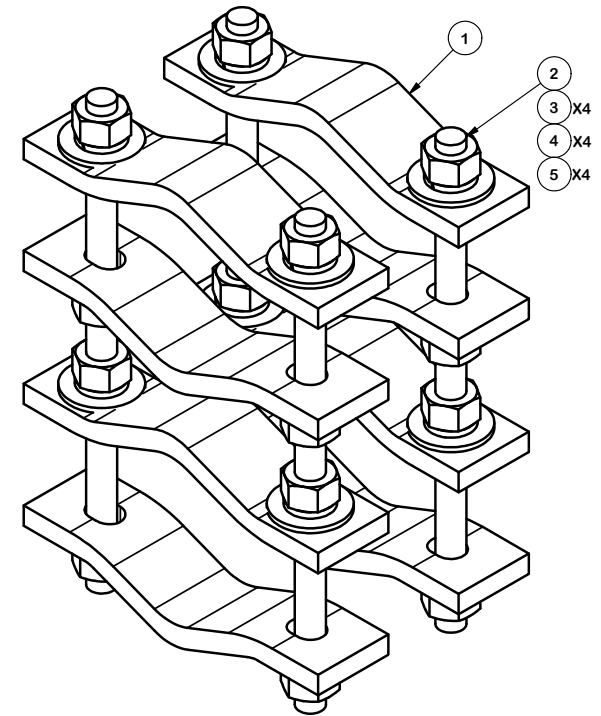
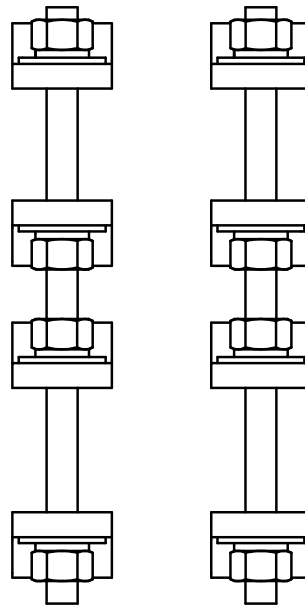
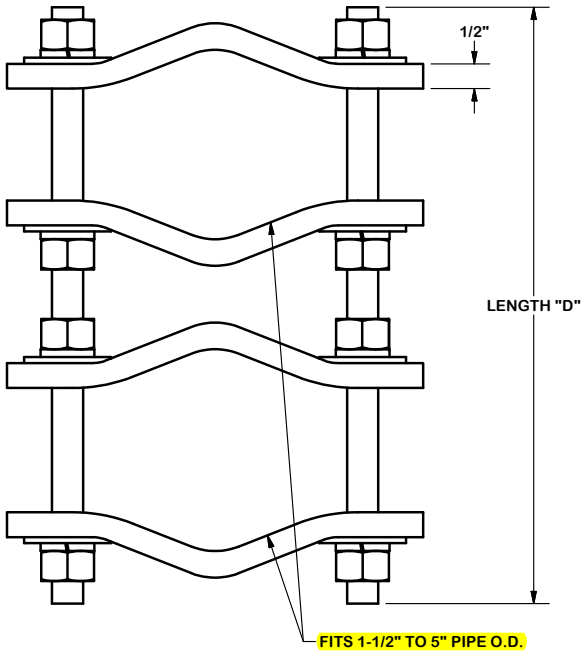
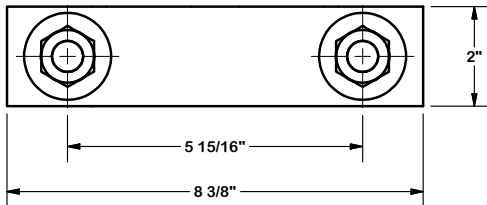
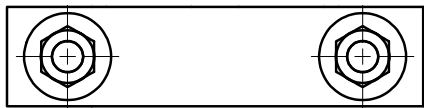


Engineering
Support Team:
1-888-753-7446

Locations:
New York, NY
Atlanta, GA
Los Angeles, CA
Plymouth, IN
Salem, OR
Dallas, TX

CPD NO.	DRAWN BY RCH	ENG. APPROVAL
CLASS 81	SUB 01	CHECKED BY BMC
DRAWING USAGE CUSTOMER		DATE 2/16/2011

PART NO.	USF-4U	PAGE
DWG. NO.	USF-4U	1 OF 1



PARTS LIST						
ITEM	QTY	PART NO.	PART DESCRIPTION	LENGTH	UNIT WT.	NET WT.
1	8	DCP	CLAMP HALF, 1/2" THICK, 8-3/8"		2.40	19.20
2	B	C	5/8" THREADED ROD	D	E	F
3	16	G58NUT	5/8" HDG HEAVY 2H HEX NUT		0.13	2.08
4	16	G58LW	5/8" HDG LOCKWASHER		0.03	0.42
5	16	G58FW	5/8" HDG USS FLATWASHER		0.07	1.13

VARIABLE PARTS TABLE						
ASSEMBLY "A"	QTY "B"	PART "C"	LENGTH "D"	UNIT WT. "E"	NET WT. "F"	TOTAL WEIGHT
DCP12K	4	G58R-12	12"	1.05	4.18	27.01
DCP18K	4	G58R-18	18"	1.57	6.27	29.10

TOLERANCE NOTES

TOLERANCES ON DIMENSIONS, UNLESS OTHERWISE NOTED ARE:
 SAWED, SHEARED AND GAS CUT EDGES ($\pm 0.030"$)
 DRILLED AND GAS CUT HOLES ($\pm 0.030"$) - NO CONING OF HOLES
 LASER CUT EDGES AND HOLES ($\pm 0.010"$) - NO CONING OF HOLES
 BENDS ARE $\pm 1/2$ DEGREE
 ALL OTHER MACHINING ($\pm 0.030"$)
 ALL OTHER ASSEMBLY ($\pm 0.060"$)

PROPRIETARY NOTE:
 THE DATA AND TECHNIQUES CONTAINED IN THIS DRAWING ARE PROPRIETARY INFORMATION OF VALMONT INDUSTRIES AND CONSIDERED A TRADE SECRET. ANY USE OR DISCLOSURE WITHOUT THE CONSENT OF VALMONT INDUSTRIES IS STRICTLY PROHIBITED.

DESCRIPTION
PIPE TO PIPE CLAMP SET
 1-1/2" TO 5" PIPE
 1/2" THICK CLAMP

SITE PRO 1
 Engineering Support Team:
 1-888-753-7446

Locations:
 New York, NY
 Atlanta, GA
 Los Angeles, CA
 Plymouth, IN
 Salem, OR
 Dallas, TX

CPD NO.	DRAWN BY	ENG. APPROVAL
	KC8 8/21/2012	
CLASS	DRAWING USAGE	CHECKED BY
81	CUSTOMER	CEK 1/22/2013

PART NO.	SEE ASSEMBLY "A"
DWG. NO.	DCPxxK

ATTACHMENT E – STRUCTURAL ANALYSIS

DETAILED STRUCTURAL ANALYSIS AND MODIFICATION OF AN EXISTING 180' SELF SUPPORTING LATTICE TOWER AND EXISTING FOUNDATION FOR PROPOSED ANTENNA ARRANGEMENT



Site ID : CSP #62 Thompson
Site Address: 97 Mountain Hill Road
Thompson, Connecticut

60619086 CSP#62
EVS-017 Revision 3 (b.2)

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- 2. INTRODUCTION**
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 - REINFORCEMENT DRAWINGS**
 - TNX TOWER INPUT / OUTPUT SUMMARY**
 - TNX TOWER FEEDLINE DISTRIBUTION CHART**
 - TNX TOWER FEEDLINE PLAN**
 - TNX TOWER DEFLECTION, TILT, AND TWIST**
 - TNX TOWER DETAILED OUTPUT**
 - ANCHOR BOLT ANALYSIS**
 - FOUNDATION ANALYSIS**

1. EXECUTIVE SUMMARY

This report summarizes the structural analysis and modification of the existing 180' self-supporting lattice tower structure located at 97 Mountain Hill Road, Thompson, Connecticut.

The structural analysis was conducted in accordance with the 2018 Connecticut State Building Code which include the TIA-222-H¹ Standard, 2015 International Building Code, the 2018 Connecticut State Building Code Amendments, the AISC² Load Resistance Factor Design (LRFD), the ASCE 7³ design Code, and the Department of Emergency Services and Public Protection (DESPP) / Connecticut State Police (CSP) design requirements.

The antenna loading considered in the analysis consists of all the existing antennas, transmission lines and ancillary items as outlined in the Introduction Section of this report.

The proposed Eversource antenna upgrades are listed below:

Proposed Antenna and Mount	Carrier	Antenna Center Elevation
Remove:		
(1) Decibel DB-212 Dipole (CSP-23)	CSP	47'
(1) Amphenol BCD806-09NE Inverted Whip (CSP-38)	CSP	127'
Install:		
(1) Telewave ANT220F2 Omni Antenna (Antenna Centerline Install @ 134')		
(1) SitePro USF-4U (Mount Centerline Install @ 131')		
(1) RFS LCF78-50JA-A7 Cellflex Coaxial Cable	Eversource (Proposed)	131'-157'
(1) Telewave ANT220F2 Omni Antenna (Antenna Centerline Install @ 157')		
(1) SitePro USF-4U (Mount Centerline Install @ 154')		
(1) RFS LCF78-50JA-A7 Cellflex Coaxial Cable		

The results of the structural analysis indicated the existing tower structure did not have enough capacity for the proposed loading conditions above. The tower structure requires modifications shown on SK-1 through SK-2. **Once the modifications indicated on sheets SK-1 through SK-2 are performed, the modified structure is considered structurally adequate with the wind load specification specified above with the existing and proposed antenna loading herein. The controlling structural capacity for all tower and foundation components for the proposed antenna loading after modifications are installed is 87.6%.**

1. TIA = Telecommunications Industry Association Structural Standard for Antenna Supporting Structures and Antennas (Version H)

2. AISC = American Institute of Steel Construction (15th Edition)

3. ASCE 7 = American Society of Civil Engineers Standard 7 (2016 Edition)

1. EXECUTIVE SUMMARY *(continued)*:

This analysis is based on:

- 1) The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- 2) Tower geometry, member sizes and foundation taken from original construction documents prepared by Stainless, Inc. project number 358815 dated October 31, 1995.
- 3) Previous structural analysis performed by URS Corporation on behalf of Northeast Utilities System, project number NU1-045 \ 36922408 signed and sealed March 14, 2013.
- 4) Geotechnical Study for Evaluation (for CSP#62) performed by Welti Geotechnical, P.C. dated March 26, 2018.
- 5) Proposed Antenna Radio Frequency Data Sheet (RFDS) from Smartlink on behalf of AT&T, dated May 5, 2019, obtained via e-mail dated November 20, 2019.
- 6) Existing tower antenna inventory obtained via tower climb performed by Eastern Communications, Inc. obtained via e-mail dated January 28, 2020.
- 7) Existing antenna inventory as specified in Section 2 and 6 of this report, provided by the CT State Police, obtained via e-mail dated October 11, 2017, with a follow up inventory update e-mail dated February 4, 2020.
- 8) Proposed Eversource inventory obtained via email dated February 10, 2020.
- 9) Previous structural analysis performed by AECOM on behalf of Eversource, project 60619086/EVS-017 Rev. 1 (a), signed and sealed September 22, 2020.
- 10) Previous structural analysis performed by AECOM on behalf of Eversource, project 60619086/EVS-017 Rev. 1 (b.1), signed and sealed September 22, 2020.
- 11) Previous structural analysis performed by AECOM on behalf of Eversource, project 60619086/EVS-017 Rev. 2 (b.1), dated October 27, 2020.
- 12) Antenna inventory as specified in Sections 2 and 6 of this report.
- 13) Coaxial cable orientation as specified in Section 6 of this report.

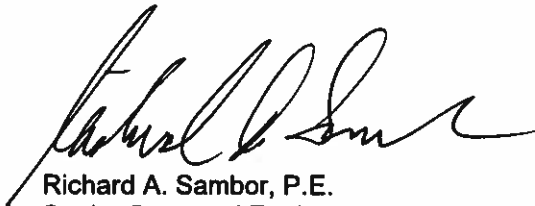
1. **EXECUTIVE SUMMARY *(continued)*:**

This report is only valid as per the assumptions and data utilized in this report for antenna inventory, mounts and associated cables. The user of this report shall field verify the antenna, cabling and mount configuration used, as well as the physical condition of the tower members, connections and foundations. Notify the engineer in writing immediately if any of the information in this report is found to be other than specified.

If you should have any questions, please contact Michael Egan at (860) 263-5817.

Sincerely,

AECOM,



Richard A. Sambor, P.E.
Senior Structural Engineer
RAS/cmc



2. INTRODUCTION

The subject tower is located at 97 Mountain Hill Road in Thompson, Connecticut. The structure is a self-supporting three-legged 180' steel tapered lattice tower manufactured by Stainless Incorporated.

The structural analysis was conducted in accordance with the following:

- 2018 International Building Code (compliant with the TIA-222-H design loads)
- 2015 International Building Code with 2018 Connecticut State Building Code Amendments for an ultimate wind speed of 140 mph (3-second gust)
- 2016 AISC Load Resistance Factor Design (LRFD)
- 2016 ASCE 7 Minimum Design Loads for Buildings and Other Structures for the ice thickness referenced in the TIA-222-H Standard

The inventory together with the proposed Eversource antenna arrangement is summarized in the table below:

Antenna Type	Carrier	Mount	Centerline Elevation	Cable
(1) 4' Lightning Rod	Tower (existing)	(1) 15' Pipe Mounted to Top of Tower	197'	n/a
(1) PD440-2 Dipole Antenna	HGT-30 CSP-19 (existing)	(2) 4' Side Arm Mounts @ 175'	181'	(1) 7/8" coax cable
(1) OGT9-840 Omni Antenna	HGT-29 CSP-5 (existing)	Mount Shared with HGT-28 (below)	181'	(1) 1-5/8" coax cable
(1) 10 Foot Dish with Radome	HGT-27 CSP-1 (existing)	Pipe Mounted to Tower Leg	178'	(1) WEP65 Elliptical Cable
(1) DB225-A 2 Element Dipole	HGT-31 CSP-17 (existing)	Mounted to Tower Leg	177'	(1) 1/2" coax cable
(1) (Inverted) OGT9-840 Omni Antenna	HGT-24 CSP-6 (existing)	(1) 4' Side Arm Mount (Shared with HGT-24, 25, 26 / CSP 4, 6) @ 175'	177'	(1) 1-5/8" coax cable (1) 0.4" (dia) cable
(1) (inverted) OGT9-840 Omni Antenna	HGT-25 CSP-4 (existing)	(1) 4' Side Arm Mount (Shared with HGT-24, 25, 26 / CSP 4, 6) @ 175'	177'	(1) 1-5/8" coax cable
(1) DB-B1-6C-8AB-0Z Distribution Box	HGT-26 CSP (existing)	(1) 4' Side Arm Mount (Shared with HGT-24, 25, 26 / CSP 4, 6) @ 175'	177'	(1) 1-5/8 " coax cable (1) 1/2" (dia) cable

Antenna Type	Carrier	Mount	Centerline Elevation	Cable
(1) SE4192-SWBP4LDF (Dxx-E6461) Panel Antenna (1) 432E-83I-01T TTA Unit (2) (inverted) SC479-HF1LDF Omni Antennas (centerline Elevation appx 168')	CSP Troop D (existing)	(1) USF-2U Side Arm Mount Frame @ 175'	175'	(2) AVA7-50 1-5/8" Low Density Coaxial Cable (1) 1/2" coax cable
(1) (inverted) OGT9-840 Omni Antenna	HGT-28 CSP-7 (existing)	(2) 4' Side Arm Mounts	175'	(1) 1-5/8" coax cable
(1) 8 Foot Dish with Radome	HGT-23 CSP-3 (existing)	Pipe Mounted to Tower Leg	169'	(1) EW63 Elliptical Cable
(1) 8 Foot Dish with Radome	HGT-22 CSP-2 (existing)	Pipe Mounted to Tower Leg	168'	(1) EW63 Elliptical Cable
(1) Telewave ANT220F2 Omni Antenna	Eversource (Proposed)	(1) SitePro USF-4U (Mount Centerline Install @ 154')	157'	(1) 7/8"
(6) Powerwave 7770 Panel (2) KMW AM-X-CD-17-65-00T-RET Panel Antennas (Alpha & Gamma Sectors) (1) KMW AM-X-CD-16-65-00T-RET Panel Antennas (Beta Sector) (3) RRUS-11 RRH Units (3) Ericsson RRUS-12 RRH Units (1) DC6-48-60-18-8F Surge Protector (6) Powerwave LGP21401 TMA Units	AT&T HGT (existing)	(3) 13' Lightweight T-Arms (Valmont P/N 800942)	150'	(12) 1 5/8" coax cables (1) 3" Flex conduit containing (1) F.O. Cable and (2) DC Cables
(1) 8-Bay Dipole Antenna	HGT-17 CSP-20 (existing)	<i>Shared with Below Mount</i>	148'	(1) 7/8" coax cable
(1) PD200 Omni Antenna	HGT-15 CSP-9 (existing)	<i>Shared with below mount HGT-14/CSP#11</i>	140'	(1) 7/8" coax cable

Antenna Type	Carrier	Mount	Centerline Elevation	Cable
(1) 12' Dipole Antenna	HGT-11 CSP (existing)	4' Side Arm Mount	138'	(1) 0.4" (dia) Cable
(1) DB 420 (inverted) Dipole Antenna	HGT-16 CSP-12 (existing)	4' Side Arm Mount	138'	(1) 7/8" coax cable
(1) DB224-A 4-Bay Dipole Antenna	HGT-13 CSP (existing)	1' Side Arm Mount	138'	(1) 7/8" coax cable
(1) (inverted) 20' 8-Bay Dipole Antenna	HGT-14 CSP#11 (existing)	(2) 4' Side Arm Mounts	138'	(1) 7/8" coax cable
(1) Telewave ANT220F2 Omni Antenna	Eversource (Proposed)	(1) SitePro USF-4U (Mount Centerline Install @ 131')	134'	(1) 7/8"
(1) DS9A09F36D-N Omni Antenna	HGT-9 CSP (existing)	Shared with below mount	116'	(2) 7/8" coax cables
(1) DB-B1-6C-8AB-0Z Distribution Box	HGT-10 CSP-24 (existing)	4' Side Arm Mount	116'	(1) 7/8" coax cable (1) 1/2" coax cable
(1) PD458-1 4-Bay Dipole Antenna	HGT-8 CSP-14 (existing)	Pipe Mounted to Tower Face	105'	(1) 7/8" coax cable
(1) DB222 Dipole Antenna	HGT-7 CSP-13 (existing)	Pipe Mounted to Tower Face	100'	(1) 7/8" coax cable
(1) 15' 1-Bay Dipole Antenna	HGT-6 CSP-15 (existing)	<i>Shared with below Mount (HGT-5/CSP- 8)</i>	86'	(1) 7/8" coax cable
(1) DB 222 Omni Antenna	HGT-4 CSP-22 (existing)	<i>Pipe Mounted to Leg</i>	81'	(1) 1/2" coax cable
(1) (inverted) DB212-1 Omni Antenna	HGT-5 CSP-8 (existing)	4' Side Arm Mount	81'	(1) 1/2" coax cable
(1) 8 Foot Dish with Radome	HGT-3 CSP-16 (existing)	Pipe Mounted to Tower Leg	79'	(1) EW63 Elliptical Cable

Antenna Type	Carrier	Mount	Centerline Elevation	Cable
(1) DB-803M-XT Omni antenna	HGT-2 CSP-21 (existing)	4' Side Arm Mount	49'	(1) 1/2" coax cable

Notes: Antenna ID numbering (HTS-#) obtained from Tower Existing Inventory via tower climb, performed by Hightower Solutions, Inc on October 24, 2016. CSP numbering and elevations provided by CSP inventory obtained via e-mail dated October 11, 2017, with follow-up inventory update obtained via e-mail dated February 4, 2020. "HTS" elevations have been updated per Eastern Communications Inc tower climb.

This structural analysis of the communications tower was performed by AECOM, on behalf of Everosurce. The purpose of this analysis was to investigate the structural integrity of the modified tower and foundation for existing antenna loads and proposed antennas in compliance with the 2018 Connecticut State Building Code. This analysis was conducted to evaluate stress on the tower and the effect of forces to the foundation of the tower resulting from existing antenna arrangements and proposed antennas.

3. ANALYSIS METHODOLOGY AND LOADING CONDITIONS

The structural analysis was done in accordance with, the TIA-222-H–Structural Standard for Antenna Towers and Antenna Supporting Structures and Antennas, the 2015 International Building Code with 2018 Connecticut State Building Code Amendments and the American Institute of Steel Construction (AISC) Manual of Steel Construction – Load Resistance Factor Design (LRFD)

The structural analysis was conducted using TNX Tower version 8.0.7.4 and used the following conditions for this tower review (following the TIA-222-H Standard):

- Structure Class 3 – (Essential Communications)
 - NOTE: ASCE 7 and CT State Building Code Applied Risk Category 4 for design wind loads (see below)
- Topographic Category 3 – (Tower location on top of hill – rolling wind conditions considered)
 - NOTE: The use of Google Earth Pro software (version 7.3.1.4505) along with Survey Topographic Maps were used in determining the applied crest height for tower location.
 - Crest Height used for analysis: → **110 feet**
- **Exposure Class B** – (Urban/suburban areas, **Wooded areas** closely spaced obstructions – Wind speed-up disruptions)
- Load Conditions:
 - Two load conditions were evaluated as shown which were compared to design stresses according to AISC and TIA-222-H Standard.

Basic Wind Speed:

- IBC 2018 w/ 2018 CT State Building Code Amendment:
 - (2018) IBC Section 1609.1.1 – Determination of Wind Loads – Exception 5 “Designs using TIA-222” applies for determination of Design Wind Load obtained as “V.ult” are to be converted to “V.asd” when applying the TIA-222-H design Standard (under Section 1609.3) for Basic Wind Speed.
 - Due to tnxTower program options for TIA-222-H, the program appears to perform tower analysis with speeds according to ASCE 7-16 V.ult loads, therefore, V.ult speeds are to be used.
 - (2018) CT State Building Code Amendment to the IBC Section 1609.3 wind loads are obtained from Appendix N of the State Building Code.
 - **V.ult = 140 mph** (3-Second Gust) Wind Design Parameter for the Town of Thompson, Connecticut for Risk Category four (IV) for essential communications (Connecticut State Police). NOTE: Because the State of Connecticut has not officially published the design wind-speeds, use the state of Connecticut wind-speeds per municipality (indicated above).

LOAD CONDITION 1 = 140 MPH (3-SECOND GUST) WIND LOAD (WITHOUT ICE) + TOWER DEAD LOAD

Load Condition 2 = 50 mph (3-second gust) Wind Load (with ice) + Ice Load + Tower Dead Load

Ice thickness used for this analysis is **1.00 inch** (assumed to start at the base of the tower) and is considered to increase in thickness with height. The initial ice thickness for design is referenced in the Annex of TIA-222-H and follows the same design criteria as the ASCE 7 Standard.

3. ANALYSIS METHODOLOGY AND LOADING CONDITIONS (cont.)

Load Condition 3 = 90 mph (fastest mile) Wind Load (with Ice) + Ice Load + Dead Load

Seismic event consideration factors/values for design:

- $S_s = 0.172$ (2018 CT State Building Code – Location Specific Value)
- $S_1 = 0.063$ (2018 CT State Building Code – Location Specific Value)
- Site Classification = “D”
- Seismic Design Category = “A” – (2018 International Building Code)
- $F_a = 1.6$ (Obtained from TIA-222-H Table 2-11 Considering above conditions)
- $F_v = 2.4$ (Obtained from TIA-222-H Table 2-12 Considering above conditions)

Strength Limit State Load Combinations (TIA-222-H Section 2.3.2):

The structural analysis herein has considered the following load combinations within the analysis:

1. **1.2 Dead Load Tower structure + 1.0 Dead Load Guy Assemblies + 1.6 Wind load without ice**
2. 1.2 Dead Load Tower structure + 1.0 Dead Load Guy Assemblies + 1.0 Dead weight of ice due to factored ice thickness + 1.0 Concurrent wind load with factored ice thickness + 1.0 Load effects due to temperature
3. 1.2 Dead Load Tower structure + 1.0 Dead Load Guy Assemblies + 1.0 Earthquake Load

NOTE 1: The above **bolded** load combination is considered to create the governing design loads per the results of the analysis.

NOTE 2: The above “Dead Load Guy Assemblies” are not considered as part of the analysis and are considered as a value of zero.

NOTE 3: The “Load effects due to temperature” do not apply for structures that are self-sustaining (from the TIA-222-H Standard)

4. FINDINGS AND EVALUATION

Combined axial and bending stresses on the existing tower structure were evaluated to compare with strength design in accordance with AISC (LRFD). The results of an initial analysis indicated that the existing tower structure did not have enough capacity to support the proposed loading conditions. The tower structure require modifications shown on SK-1 through SK-2. **Once the modifications indicated on sheets SK-1 through SK-2 are performed, the modified structure and foundation are considered structurally adequate with the wind load classification specified with the existing and proposed antenna loading noted herein. The controlling structural capacity for all tower and foundation components for the proposed antenna loading after modifications are installed is 87.6 %.**

Proposed Tower Component Stress vs. Capacity Summary

Component / (Section No.)	Controlling Component/ Elevation	Stress (% capacity)	Pass/Fail
Leg (T4)	HSS 5.0x0.25 / Compression / 100' – 125'	87.6	Pass
Diagonal (T11)	(2) L3x3-1/2x5/16" (3/8" gap) / Compression / 0' – 25'	74.4	Pass
Horizontal (T10)	L3x3x1/4 / Compression / 25' – 37.5'	82.6	Pass
Top Girt (T1)	L3x3x1/4 / Compression / 175' – 180'	1.5	Pass
Redundant Horizontal Bracing (T11)	L3x3x1/4 / Compression / 0' – 25'	19.0	Pass
Redundant Diagonal Bracing (T11)	L3x3x1/4 / Compression / 0' – 25'	26.2	Pass
Inner Bracing (T8)	L2-1/2x2-1/2x3/16 / Compression / 50' – 75'	0.6	Pass
Bolt Checks(T10)	(2) 0.625" Diameter A325X Bolt / Member Block Shear / 37.5'	76.9	Pass

Foundation Summary

Component	Required	Computed	% Capacity	Pass/Fail
Anchor Rod Capacity (TIA-222-H – 4.9.9)	Ratio < 1.0	0.82	82.0	Pass
Foundation – Spread Foot (6'x6') Uplift Capacity	384.59 kip (Factored Resistance)	313.641	82.0	Pass
Foundation – Rock Anchorage – Bonded Embedment Length	15 feet (installed)	8.95 feet (calculated)	52.0	Pass
Foundation – Bearing on Rock Capacity	30.000 ksf (Factored Resistance)	12.689 ksf	42.3	Pass

Maximum Structure Rating (from all components) =	87.6 %	Pass
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4. FINDINGS AND EVALUATION (cont.)

Maximum Deformations – Proposed Condition

TIA-222-H Section 2.8.2 - Limit State Deformations

1. A rotation of 4 degrees about the vertical axis (twist) or any horizontal axis (sway) of the structure.
2. A horizontal displacement (in feet) of 3% of the height of the structure.

Load Case Description	Current		Allowable	
	Sway (degree)	Displacement (Feet)	Sway (degree)	Displacement (Feet)
Service Wind Load	0.120	0.228	4.0	5.97

5. CONCLUSIONS

The results of an initial analysis indicated the existing tower structure did not have enough capacity for the proposed loading conditions above. The tower structure requires modifications shown on SK-1 through SK-2. **Once the modifications indicated on sheets SK-1 through SK-2 are performed, the modified structure is considered structurally adequate with the wind load specification specified above with the existing and proposed antenna loading herein. The controlling structural capacity for all tower and foundation components for the proposed antenna loading after modifications are installed is 87.6 %.**

Limitations/Assumptions:

This report is based on the following:

- A. Tower inventory as listed in this report.
- B. Tower is properly installed and maintained.
- C. All members are as specified in the original design documents and are in good condition.
- D. All required members are in place.
- E. All bolts are in place and are properly tightened.
- F. Tower is in plumb condition.
- G. All member protective coatings are in good condition.
- H. All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- I. Foundations are in good condition without defects and were properly constructed to support original design loads as specified in the original design documents.

AECOM is not responsible for any modifications completed prior to or hereafter in which AECOM is not or was not directly involved. Modifications include but are not limited to:

- A. Adding antennas
- B. Removing/replacing antennas
- C. Adding coaxial cables

AECOM hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations, and conclusions are based upon information contained and set forth herein. If you are aware of any information which conflicts with that which is contained herein, or you are aware of any defects arising from original design, material, fabrication, or erection deficiencies, you should disregard this report and immediately contact AECOM. AECOM disclaims all liability for any representation, recommendation, or conclusion not expressly stated herein.

Ongoing and Periodic Inspection and Maintenance:

After the Contractor has successfully completed the installation and the work has been accepted, the owner will be responsible for the ongoing and periodic inspection and maintenance of the tower.

The owner shall refer to TIA-222-H Section 14.2 for recommendations for maintenance and inspection. The frequency of the inspection and maintenance intervals is to be determined by the owner based upon actual site and environmental conditions. It is recommended that a complete and thorough inspection of the entire tower structural system be performed at least yearly and more frequently as conditions warrant. It is also recommended that the structure be inspected after severe wind and/or ice storms or other extreme loading conditions.

6. DRAWINGS AND DATA

REINFORCEMENT DRAWINGS

GENERAL CONSTRUCTION NOTES

1. ALL WORK SHALL COMPLY WITH THE CONNECTICUT STATE BUILDING AND LIFE SAFETY CODES, SUPPLEMENTS AND AMENDMENTS.
2. CONTRACTOR IS TO REVIEW ALL DRAWINGS AND NOTES IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUB-CONTRACTORS AND ALL RELATED PARTIES. THE SUB-CONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
3. CONTRACTOR SHALL PROVIDE A COMPLETE BUILD-OUT WITH ALL FINISHES, STRUCTURAL, MECHANICAL, AND ELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON DRAWINGS OR WRITTEN IN SPECIFICATIONS.
4. CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OVER THE WORK.
5. CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION AND ELECTRICAL SUB-CONTRACTORS SHALL PAY FOR THEIR PERMITS.
6. CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS ON SITE AT ALL TIMES AND ENSURE THE DISTRIBUTION OF NEW DRAWINGS TO SUB-CONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE. ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. CONTRACTOR SHALL FURNISH 'AS-BUILT' SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
7. INSTALLATION OF THIS WIRELESS COMMUNICATIONS EQUIPMENT SITE REQUIRES WORK IN THE IMMEDIATE VICINITY OF EXISTING OPERATING TELECOMMUNICATION SYSTEMS. THE CONTRACTOR SHALL PROVIDE AND COORDINATE THE METHODS OF PROTECTION WITH THE VARIOUS TELECOMMUNICATION CARRIERS AND THE TOWER OWNER. THERE SHALL BE NO INTERRUPTION OF OPERATION WITHOUT TIMELY COORDINATION WITH AND APPROVAL BY THE VARIOUS COMMUNICATIONS OPERATORS INCLUDING THE CONNECTICUT STATE POLICE.
8. NO MOVEMENT, ALTERATION, OR DISCONNECTION OF CONNECTICUT STATE POLICE ANTENNAS MAY OCCUR WITHOUT THE NOTIFICATION AND APPROVAL OF THE CONNECTICUT STATE POLICE. CONTACT THE NETWORK CONTROL CENTER AT 860-865-8008.
9. TOWER REINFORCING WORK AFFECTING CRITICAL CONNECTICUT STATE POLICE ANTENNAS MAY BE REQUIRED TO BE CONDUCTED AT TIMES AS DETERMINED BY THE REQUIREMENTS OF THE CONNECTICUT STATE POLICE.
10. IT SHALL BE MANDATORY TO USE STEEL MATERIALS PLANNED FOR CONSTRUCTION THAT ARE MANUFACTURED IN THE UNITED STATES OF AMERICA. MATERIAL SPECIFICATION DOCUMENTS SHALL BE MADE AVAILABLE TO VERIFY STEEL FABRICATION PRIOR TO PURCHASE AND IMPLEMENTATION. DEVIATIONS FROM THIS SHALL REQUIRE EXPRESSED WRITTEN PERMISSION FROM THE ENGINEER AND CONNECTICUT STATE POLICE.
11. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUB-CONTRACTORS FOR ANY CONDITION PER MFR'S RECOMMENDATIONS. CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR ARCHITECT.
12. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON-SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
13. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ARCHITECT FOR REVIEW. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTAL TO THE ARCHITECT FOR REVIEW.
14. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES, AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA. SUBMIT ANY DISCREPANCIES FROM THE DRAWINGS TO THE ARCHITECT.
15. THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURE AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY.
16. CONTRACTOR SHALL COMPLY WITH OWNER ENVIRONMENTAL ENGINEER ON ALL METHODS AND PROVISIONS FOR ALL EXCAVATION ACTIVITIES INCLUDING SOIL DISPOSAL. ALL BACKFILL MATERIALS TO BE PROVIDED BY THE CONTRACTOR.
17. DIMENSIONS OF EXISTING TOWER ARE BASED ON MANUFACTURER'S DRAWINGS PREPARED BY STAINLESS INC., DATED DECEMBER 1993, AND ARE NOT GUARANTEED. CONTRACTOR SHALL TAKE FIELD DIMENSIONS AS NECESSARY TO ASSURE PROPER FIT OF ALL FINISHED WORK AND SHALL ASSUME FULL RESPONSIBILITY FOR THEIR ACCURACY. WHEN SHOP DRAWINGS BASED ON FIELD MEASUREMENT ARE SUBMITTED FOR REVIEW, DIMENSIONS ARE PROVIDED FOR THE ENGINEER'S REFERENCE ONLY.
18. TOWER INVENTORY IS BASED ON INFORMATION OBTAINED BY CONNECTICUT STATE POLICE DATED OCTOBER 11, 2017. TOWER MAPPING AND EXISTING INVENTORY OBTAINED FROM HIGH TOWER SOLUTIONS, INC. DATED OCTOBER 24, 2016.
19. CONTRACTOR TO VERIFY REQUIRED CLEARANCES INCLUDING BUT NOT LIMITED TO EXISTING BUILDINGS, EQUIPMENT PADS AND SHELTERS PRIOR TO COMMENCING WORK.
20. THE CONTRACTOR IS RESPONSIBLE FOR THE STABILITY OF THE STRUCTURE DURING CONSTRUCTION. NO MEMBER OF THE TOWER SHALL BE LEFT DISCONNECTED FOR THE NEXT WORKING DAY. THE CONTRACTOR SHALL BE AWARE OF WEATHER AND WIND CONDITIONS AND NOT PERFORM MEMBER REPLACEMENT IN A WIND.

STRUCTURAL NOTES

STRUCTURAL STEEL MATERIAL TO BE PROVIDED:

ANGLE A529-50
 STRUCTURAL PLATES A36
 ROUND HSS TUBE ASTM A501 Gr. 50

STRUCTURAL STEEL SHALL CONFORM TO ALL THE REQUIREMENTS OF THE ASTM SPECIFICATION, AS REFERENCED IN THE CODE.

UNLESS OTHERWISE NOTED, ALL STEEL WILL BE GALVANIZED IN ACCORDANCE WITH ASTM 123 AFTER FABRICATION. TOUCH UP ALL DAMAGED GALVANIZED STEEL WITH APPROVED COLD ZINC, "GALVANOX", "DRY GALV", "ZINC-IT", OR APPROVED EQUIVALENT, IN ACCORDANCE WITH MANUFACTURERS GUIDELINES. TOUCH-UP DAMAGED NON GALVANIZED STEEL WITH SAME PAINT APPLIED IN SHOP OR FIELD.

SHOP AND ERECTION DRAWINGS SHALL BE SUBMITTED FOR ALL STRUCTURAL STEEL WORK IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. SUBMIT 2 SETS OF PRINTS FOR THE ENGINEER REVIEW.

MILL BEARING ENDS OF COLUMNS, STIFFENERS, AND OTHER BEARING SURFACES TO TRANSFER LOAD OVER ENTIRE CROSS SECTION.

THE OMISSION OF ANY MATERIAL THAT WAS SHOWN ON THE CONTRACT DRAWINGS SHALL NOT RELIEVE THE CONTRACTOR OF PROVIDING THE SAME.

CONNECTIONS / FIELD ASSEMBLY:

BOLTED CONNECTIONS: UNLESS OTHERWISE NOTED, ALL JOINTS ARE SLIP CRITICAL TYPE, REQUIRING 5/8" & 1" DIA. A325-X BOLTS, A563 NUTS AND F436 WASHERS, ALL GALVANIZED. BEVELED WASHERS SHALL BE USED ON BEAM FLANGES HAVING A SLOPE GREATER THAN 1:20.

STRUCTURE IS DESIGNED TO BE LEVEL AND PLUMB. SELF-SUPPORTING AND STABLE AFTER WORK IS COMPLETED.

COMMENCEMENT OF WORK WITHOUT NOTIFYING THE ENGINEER OF ANY DISCREPANCIES WILL BE CONSIDERED ACCEPTANCE OF PRECEDING WORK.

INSPECTIONS:

SPECIAL INSPECTIONS ARE REQUIRED PER THE CODE FOR STRUCTURAL STEEL WORK.

EVERSOURCE WILL SUPPLY THE SERVICES OF A SPECIAL INSPECTOR AND TESTING AGENTS AS REQUIRED BY AUTHORITY HAVING JURISDICTION. CONTRACTOR SHALL COORDINATE INSPECTIONS OF FABRICATOR'S AND ERECTOR'S WORK AND MATERIALS TO MEET THE REQUIREMENTS OF THE STATEMENT OF SPECIAL INSPECTIONS FOR THIS PROJECT.

COPIES OF TESTING AND INSPECTION REPORTS WILL BE PROVIDED TO THE OWNER, BUILDING OFFICIAL, ENGINEER OF RECORD AND CONTRACTOR.



[Handwritten Signature]

PROJECT NO. 60619086
Designed by: CMC
Drawn by: GAT
Checked by: DJR
Approved by: RAS

AECOM

500 ENTERPRISE DRIVE
ROCKY HILL, CONNECTICUT
(860)-529-8882

EVERSOURCE

CSP TOWER #62
97 MOUNTAIN HILL ROAD
THOMPSON, CONNECTICUT

SITE ADDRESS:

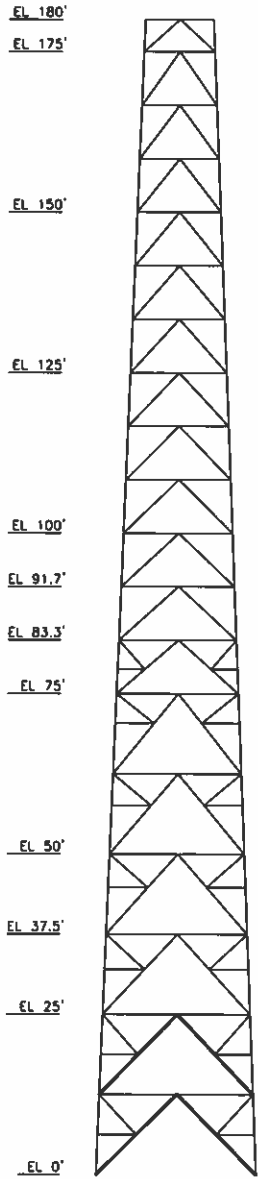
REV.	DATE	DESCRIPTION
Scale: AS NOTED	Date: 11/25/20	
Job No.	File No.	

Dwg. No.
SK-1

Dwg. 1 of 2

NOTES:

1. REFER TO STRUCTURAL NOTES ON SK-1 FOR STEEL GRADE REQUIREMENTS FOR REPLACEMENT MEMBERS.
2. CONTRACTOR SHALL FIELD VERIFY EXISTING TOWER INFORMATION AND ANGLE MEMBER ORIENTATION PRIOR TO ORDERING MATERIALS.
3. REINFORCEMENT OF TOWER IS REQUIRED FOR ALL 3 SIDES OF EXISTING TOWER STRUCTURE.
4. MEMBERS INDICATED FOR REPLACEMENT/INSTALLATION SHALL HAVE A MINIMUM OF 50 KSI (YIELD STRENGTH). COORDINATE WITH STRUCTURAL NOTES ON SK-1.
5. CONTRACTOR SHALL ASSESS U-BOLTS INDICATED TO BE INSTALLED AT ENDS OF 25' ELEVATION POINTS AND ADJUST WHERE REQUIRED. CONTRACTOR SHALL SUBMIT PROPOSED RE-LOCATIONS OF U-BOLTS PRIOR TO ORDERING OF MATERIALS RELATED TO THIS INSTALL. REUSE OF EXISTING U-BOLTS SHALL NOT BE PERMITTED.



REPLACE EXISTING DIAGONAL (2)3x3-1/2x1/4 w/ (2)3x3-1/2x5/16 (ELEVATION RANGE 0'-25')

1 TOWER ELEVATION
 SK-2 SCALE: 1/2"=1'-0"

PROJECT NO.
60619086
 Designed by:
CMC
 Drawn by:
GAT
 Checked by:
DJR
 Approved by:
RAS

AECOM
 500 ENTERPRISE DRIVE
 ROCKY HILL, CONNECTICUT
 (860)-529-8882

EVERSOURCE
 CSP TOWER #62
 SITE ADDRESS: 97 MOUNTAIN HILL ROAD
 THOMPSON, CONNECTICUT

REV.	DATE:	DESCRIPTION
Scale: AS NOTED	Date: 11/25/20	
Job No.	File No.	

Dwg. No.
SK-2
 Dwg. 2 of 2

TNX TOWER INPUT / OUTPUT SUMMARY

DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
OGT9-840 (HGT-29 / CSP#5)	181	Ericsson RRUS-12 RRH Unit (ATI)	149
PD440-2 (HGT-30 / CSP-19)	181	Ericsson RRUS-12 RRH Unit (ATI)	149
Pirot 4' Side Mount Standoff (1) (HGT-30 / CSP#19)	180	Ericsson RRUS-12 RRH Unit (ATI)	149
		RRUS-11 (ATI)	149
Pirot 4' Side Mount Standoff (1) (HGT-30 / CSP#19)	180	RRUS-11 (ATI)	149
		RRUS-11 (ATI)	149
432E-831-01T TTA Unit (CSP - Troop D)	180	20' 8 Bay Di-Pole (HGT-17 / CSP#20)	148
		(2) LPG21401 TMA (ATI)	147
10'6"x4" Pipe Mount (Tower)	180	(2) LPG21401 TMA (ATI)	147
Lightning Rod 5/8x4' (Tower)	180	(2) LPG21401 TMA (ATI)	147
4"x4" Pipe Mount (HGT-27 / CSP#1)	178	Pirot 4' Side Mount Standoff (1) (Shared HGT-1617 / CSP#12,#20)	143
DB225-A (HGT-31 / CSP#-17)	178	PD200 (HGT-15 / CSP#9)	140
OGT9-840 (HGT-24 / CSP#6)	177	Pirot 4' Side Mount Standoff (1) (HGT-11 / CSP)	138
OGT9-840 (HGT-25 / CSP#4)	177	(inverted) DB420 (HGT-16 / CSP#12)	138
DB-B1-6C-8AB-0Z Dist. Box (HGT-26)	177	12' Dipole (HGT-11 / CSP)	138
Pirot 4' Side Mount Standoff (1) (Shared HGT-24,25,26 / CSP# 4,6)	177	(inverted) 20' 8 Bay Di-Pole (HGT-14 / CSP#11)	136
3'4"x4" Pipe Mount (CSP - Troop D)	177	Pirot 4' Side Mount Standoff (1) (Shared HGT-1415 / CSP#11,#9)	136
(inverted) OGT9-840 (HGT-28 / CSP#7)	175	2'6"x4" Pipe Mount (HGT-13 / CSP)	136
Pirot 4' Side Mount Standoff (1) (Shared HGT-28, 29 / CSP# 5,7)	175	Pirot 4' Side Mount Standoff (1) (Shared HGT-1415 / CSP#11,#9)	136
Pirot 4' Side Mount Standoff (1) (Shared HGT-28, 29 / CSP# 5,7)	175	DB224-A (HGT-13 / CSP)	136
USF-2U w/ TAM-II adapter with 8' 2-3/8" Pipe (CSP - Troop D)	175	ANT220F2 w/clamps (Eversource - Proposed)	134
10 FT DISH (HGT-27 / CSP#1)	175	Site Pro USF-4U w/ (2) Stiff-Arm Supports (Eversource - Proposed)	134
(inverted) SC479-HF1LDF (CSP - Troop D)	173	Pirot 4' Side Mount Standoff (1) (HGT-9,10 / CSP#24)	116
(inverted) SC479-HF1LDF (CSP - Troop D)	173	10'6"x4" Pipe Mount (CSP - Troop D)	170
10'6"x4" Pipe Mount (CSP - Troop D)	170	SE4192-SWBP4LDF(Dxx-E6461) Panel Antenna (CSP - Troop D)	170
SE4192-SWBP4LDF(Dxx-E6461) Panel Antenna (CSP - Troop D)	170	4"x4" Pipe Mount (HGT-23 / CSP#3)	169
4"x4" Pipe Mount (HGT-23 / CSP#3)	169	8 FT DISH (HGT-23 / CSP#3)	169
8 FT DISH (HGT-23 / CSP#3)	169	4"x4" Pipe Mount (HGT-22 / CSP#2)	168
4"x4" Pipe Mount (HGT-22 / CSP#2)	168	8 FT DISH (HGT-22 / CSP#2)	167
8 FT DISH (HGT-22 / CSP#2)	167	ANT220F2 w/clamps (Eversource - Proposed)	157
ANT220F2 w/clamps (Eversource - Proposed)	157	Site Pro USF-4U w/ (2) Stiff-Arm Supports (Eversource - Proposed)	157
Site Pro USF-4U w/ (2) Stiff-Arm Supports (Eversource - Proposed)	157	Valmont 13' Lightweight T-Frame (ATI)	150
Valmont 13' Lightweight T-Frame (ATI)	150	Valmont 13' Lightweight T-Frame (ATI)	150
Valmont 13' Lightweight T-Frame (ATI)	150	Valmont 13' Lightweight T-Frame (ATI)	150
DC6-48-60-18-8F (ATI)	150	(2) 7770.00 panel antenna (ATI)	149
(2) 7770.00 panel antenna (ATI)	149	(2) 7770.00 panel antenna (ATI)	149
(2) 7770.00 panel antenna (ATI)	149	(2) 7770.00 panel antenna (ATI)	149
AM-X-CD-17-65-00T (ATI)	149	AM-X-CD-17-65-00T (ATI)	149
AM-X-CD-17-65-00T (ATI)	149	AM-X-CD-17-65-00T (ATI)	149
AM-X-CD-16-65-00T (ATI)	149		

SYMBOL LIST

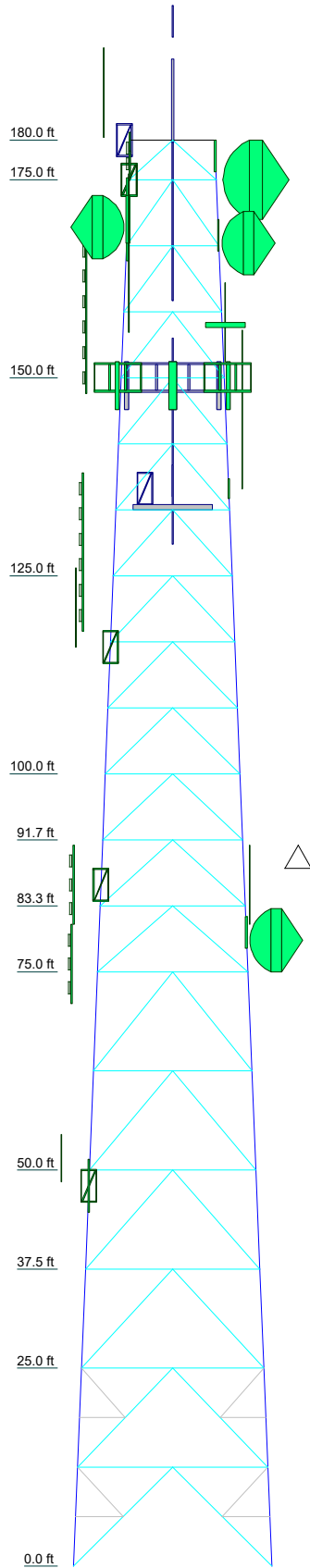
MARK	SIZE	MARK	SIZE
A	L3x3x1/4		

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A572-60	60 ksi	75 ksi
A36	36 ksi	58 ksi	A529-50	50 ksi	65 ksi

TOWER DESIGN NOTES

1. Tower is located in Windham County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-H Standard.
3. Tower designed for a 140 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category III.
7. Topographic Category 3 with Crest Height of 110.00 ft
8. "H" is based on the Difference between the Base Base Elevation above the Average Elevation within a 2 mile radius.
9. Elevations are based on Average elevations from Google Earth Measures measured from 0.5, 1.0, 1.5 2.0 Mile Radius distances from tower base
10. Average El = 430 feet; Tower Base Elevation = 540 feet "H" = 110ft
11. Updates to elevations previously climbed by High Tower (2016) have been adjusted per January 2020 tower climb from Eastern Communications Inc.



Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11
Legs			HSS5x.25								
Leg Grade			A572-50								
Diagonals				2L3x2 1/2x1/4x3/8							
Diagonal Grade				A36							
Top Glirts											
Horizontals											
Red. Horizontals											
Red. Diagonals											
Inner Bracing											
Face Width (ft)	25	11	10.6	13	15	17	17.6667	18.3333	18.3333	21	23
# Panels @ (ft)	35773.2	1 @ 5		12 @ 8.33333					6 @ 12.5		
Weight (lb)	35773.2	2596.2	3454.1	3078.8	1488.0	1488.7	1805.6	5810.4	3327.0	3385.5	8143.2

AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job: 180' Stainless, Inc. Self Supporting Lattice Project: 97 Mountain Hill Road, Thompson, CT-CSP Client: Eversource Phase (b.2) rev. 3 Drawn by: christina.carlos App'd: Code: TIA-222-H Date: 11/25/20 Scale: NTS Path: Dwg No. E-1
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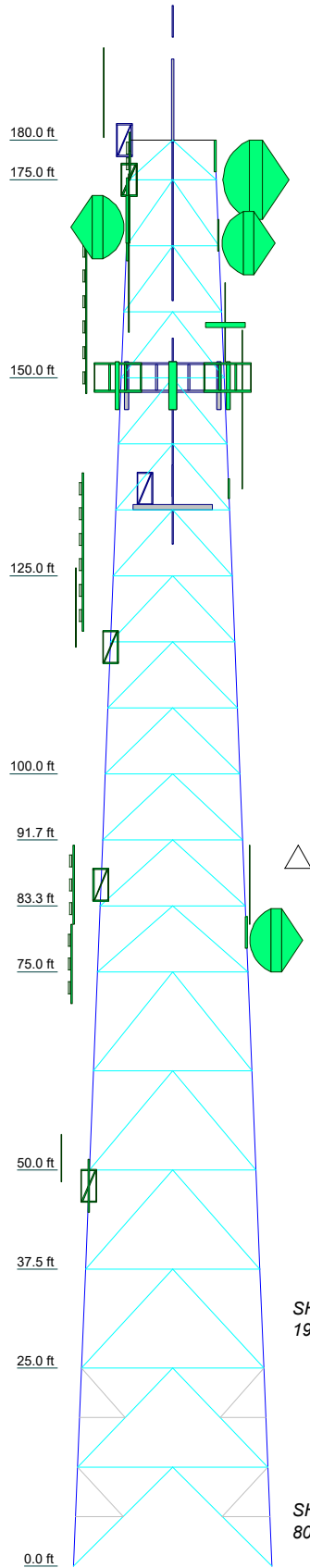
MARK	SIZE	MARK	SIZE
A	L3x3x1/4		

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A572-60	60 ksi	75 ksi
A36	36 ksi	58 ksi	A529-50	50 ksi	65 ksi

TOWER DESIGN NOTES

1. Tower is located in Windham County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-H Standard.
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5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category III.
7. Topographic Category 3 with Crest Height of 110.00 ft
8. "H" is based on the Difference between the Base Base Elevation above the Average Elevation within a 2 mile radius.
9. Elevations are based on Average elevations from Google Earth Measures measured from 0.5, 1.0, 1.5 .2.0 Mile Radius distances from tower base
10. Average EI = 430 feet; Tower Base Elevation = 540 feet "H" = 110ft
11. Updates to elevations previously climbed by High Tower (2016) have been adjusted per January 2020 tower climb from Eastern Communications Inc.
12. TOWER RATING: 87.6%

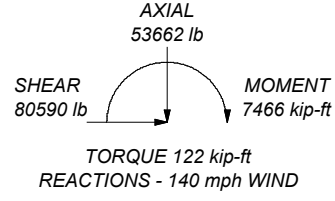
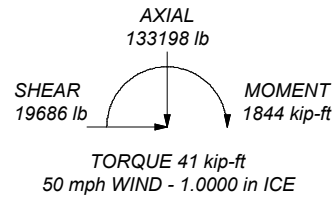


ALL REACTIONS ARE FACTORED

MAX. CORNER REACTIONS AT BASE:

DOWN: 362710 lb
SHEAR: 45184 lb

UPLIFT: -313641 lb
SHEAR: 39877 lb



Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11
Legs			HSS5x.25			HSS5x.375			HSS6.875x.375		HSS6.875x.5
Leg Grade			A572-50			A572-60			A572-60		A529-50
Diagonals			2L2 1/2x2x3/16x3/8			2L3x2 1/2x1/4x3/8			2L3 1/2x3x3/8x3/8		2L3x3 1/2x5/16x3/8
Diagonal Grade			A36			A36			A36		A36
Top Glirfs											
Horizontals			L3x3x1/4			L3x4x1/4			L3x4x1/2		L4x4x1/4
Red. Horizontals			N.A.			N.A.			N.A.		L3x3x1/4
Red. Diagonals											L3x3x1/4
Inner Bracing											L3x3x1/4
Face Width (ft)	11	10.6		13		17	18.3333	17.6667	21	22	23
# Panels @ (ft)	1 @ 5		12 @ 8	33333		1488.0	1485.7	1805.6	3327.0	6 @ 12.5	8143.2
Weight (lb)	628.8		3454.1	3078.8		1488.0	1485.7	1805.6	5810.4	3385.5	8143.2

AECOM
1255 Broad St. Suite 201
Clifton, NJ 07013
Phone: (973) 883-8663
FAX: (973) 883-8500

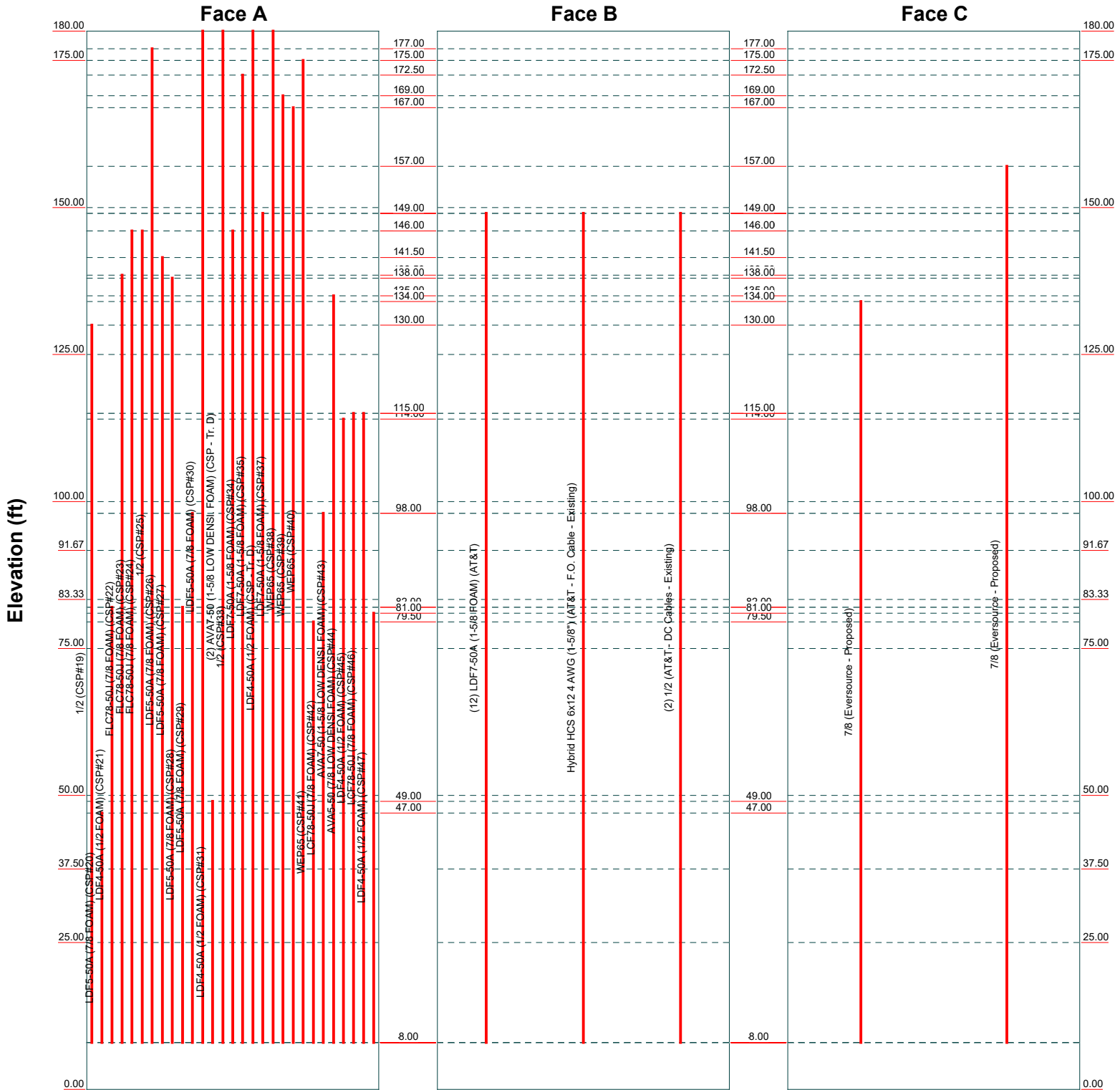
Job: 180' Stainless, Inc. Self Supporting Lattice		
Project: 97 Mountain Hill Road, Thompson, CT-CSP		
Client: Eversource Phase (b.2) rev. 3	Drawn by: christina.carlos	App'd:
Code: TIA-222-H	Date: 11/25/20	Scale: NTS
Path:		Dwg No. E-1

TNX TOWER FEEDLINE DISTRIBUTION CHART

Feed Line Distribution Chart

0' - 180'

— Round
 — Flat
 — App In Face
 — App Out Face
 — Truss Leg

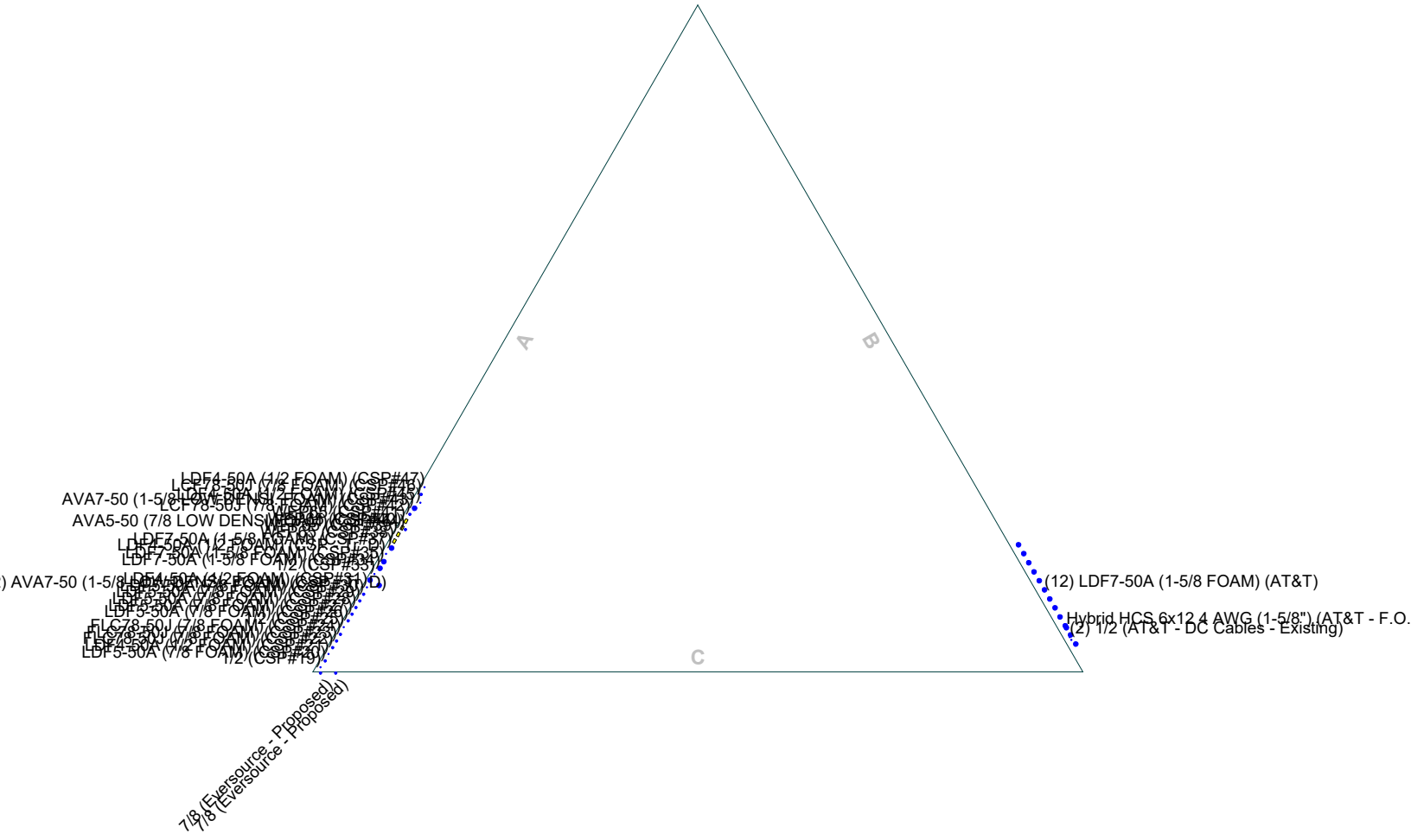


AECOM		Job: 180' Stainless, Inc. Self Supporting Lattice	
1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500		Project: 97 Mountain Hill Road, Thompson, CT--CSP	
Client: Eversource Phase (b.2) rev. 3	Code: TIA-222-H	Drawn by: christina.carlos	App'd:
Date: 11/25/20	Scale: NTS	Dwg No. E-7	

TNX TOWER FEEDLINE PLAN

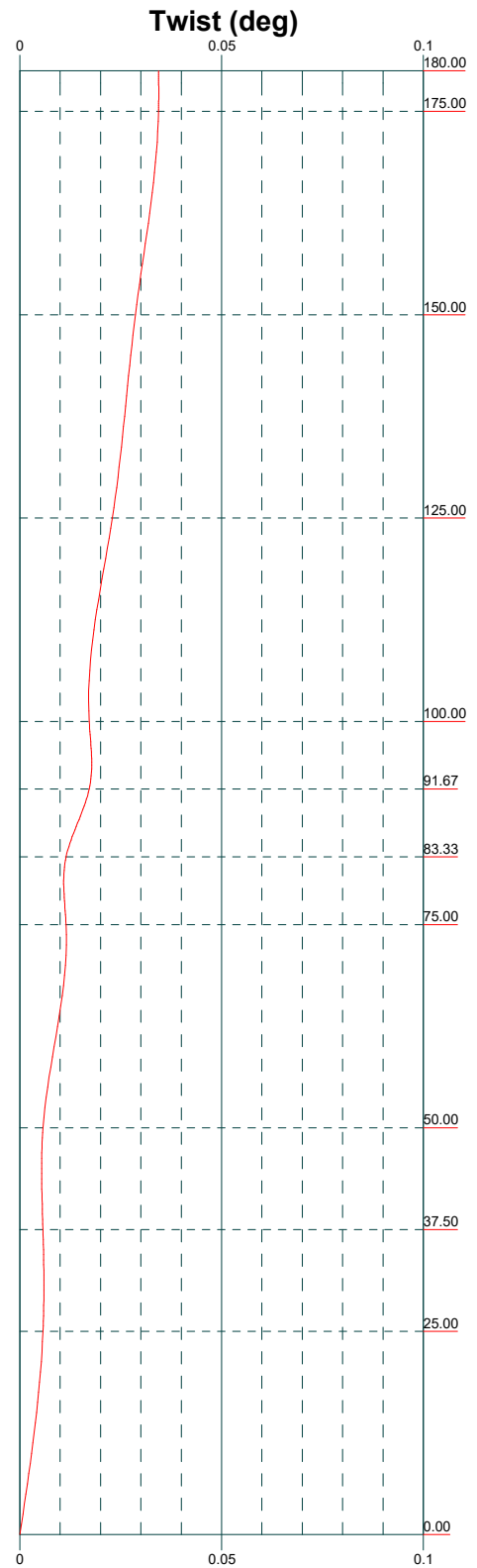
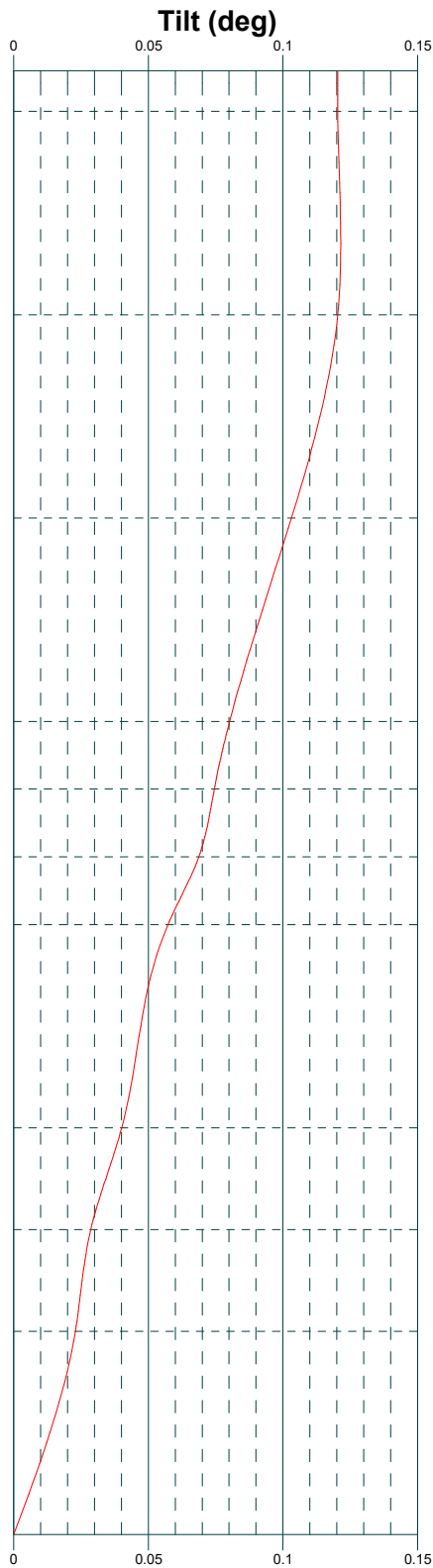
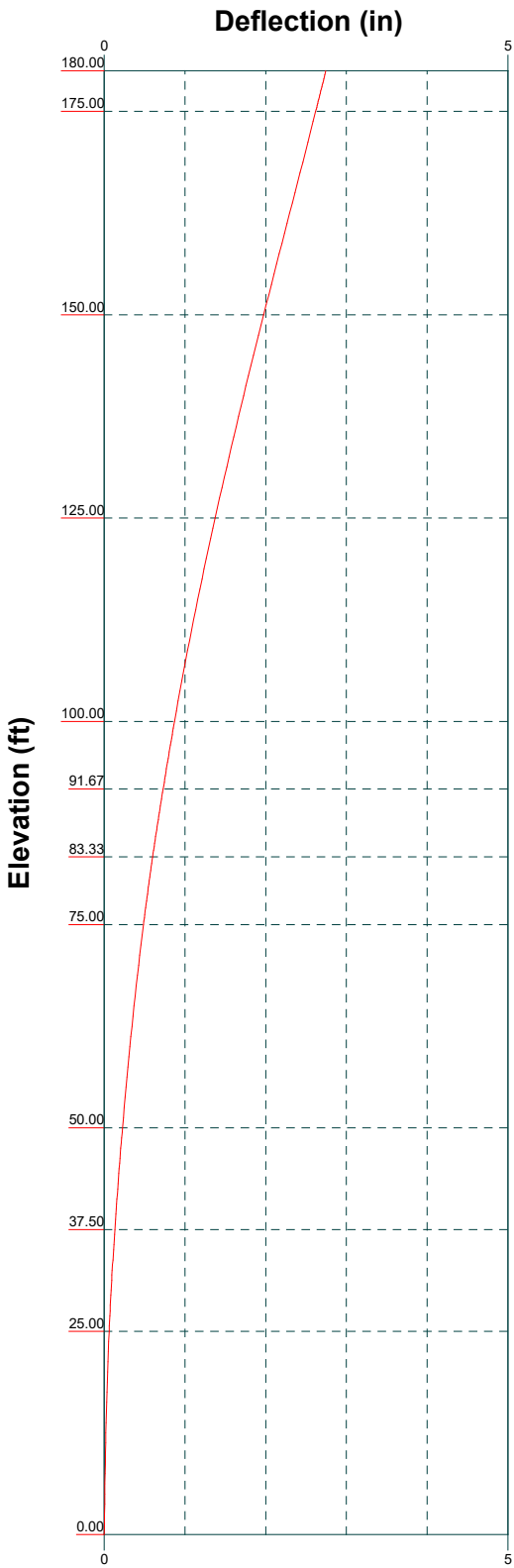
Feed Line Plan

— Round
 — Flat
 — App In Face
 — App Out Face



AECOM		Job: 180' Stainless, Inc. Self Supporting Lattice	
1255 Broad St. Suite 201		Project: 97 Mountain Hill Road, Thompson, CT--CSP	
Clifton, NJ 07013		Client: Eversource Phase (b.2) rev. 3	Drawn by: christina.carlos
Phone: (973) 883-8663		Code: TIA-222-H	Date: 11/25/20
FAX: (973) 883-8500		Path:	Scale: NTS
			Dwg No. E-7

TNX TOWER DEFLECTION, TILT, AND TWIST



AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500		Job: 180' Stainless, Inc. Self Supporting Lattice		
		Project: 97 Mountain Hill Road, Thompson, CT--CSP		
Client: Eversource Phase (b.2) rev. 3		Drawn by: christina.carlos		App'd:
Code: TIA-222-H		Date: 11/25/20		Scale: NTS
Path:				Dwg No. E-5

TNX TOWER DETAILED OUTPUT

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	1 of 65
	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Tower Input Data

The main tower is a 3x free standing tower with an overall height of 180.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 10.60 ft at the top and 25.00 ft at the base.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower is located in Windham County, Connecticut.

Tower base elevation above sea level: 0.00 ft.

Basic wind speed of 140 mph.

Risk Category III.

Exposure Category B.

Simplified Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Category: 3.

Crest Height: 110.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

"H" is based on the Difference between the Base Base Elevation above the Average Elevation within a 2 mile radius..

Elevations are based on Average elevations from Google Earth Measures measured from 0.5, 1.0, 1.5 & 2.0 Mile

Radius distances from tower base.

Average El = 430 feet; Tower Base Elevation = 540 feet "H" = 110ft.

Updates to elevations previously climbed by High Tower (2016) have been adjusted per January 2020 tower climb from Eastern Communications Inc..

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

<ul style="list-style-type: none"> Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification √ Use Code Stress Ratios √ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile √ Include Bolts In Member Capacity √ Leg Bolts Are At Top Of Section √ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric 	<ul style="list-style-type: none"> Distribute Leg Loads As Uniform Assume Legs Pinned √ Assume Rigid Index Plate √ Use Clear Spans For Wind Area √ Use Clear Spans For KL/r Retension Guys To Initial Tension √ Bypass Mast Stability Checks Use Azimuth Dish Coefficients √ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination √ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs 	<ul style="list-style-type: none"> Use ASCE 10 X-Brace Ly Rules √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA √ SR Leg Bolts Resist Compression √ All Leg Panels Have Same Allowable Offset Girt At Foundation √ Consider Feed Line Torque √ Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption <li style="text-align: center;">Poles Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known
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Tower Section	Tower Elevation <i>ft</i>	Diagonal Spacing <i>ft</i>	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset <i>in</i>	Bottom Girt Offset <i>in</i>
T1	180.00-175.00	5.00	K Brace Down	No	Yes	0.0000	0.0000
T2	175.00-150.00	8.33	K Brace Down	No	Yes	0.0000	0.0000
T3	150.00-125.00	8.33	K Brace Down	No	Yes	0.0000	0.0000
T4	125.00-100.00	8.33	K Brace Down	No	Yes	0.0000	0.0000
T5	100.00-91.67	8.33	K Brace Down	No	Yes	0.0000	0.0000
T6	91.67-83.33	8.33	K Brace Down	No	Yes	0.0000	0.0000
T7	83.33-75.00	8.33	K Brace Down	No	Yes	0.0000	0.0000
T8	75.00-50.00	12.50	K Brace Down	No	Yes	0.0000	0.0000
T9	50.00-37.50	12.50	K Brace Down	No	Yes	0.0000	0.0000
T10	37.50-25.00	12.50	K Brace Down	No	Yes	0.0000	0.0000
T11	25.00-0.00	12.50	K1 Down	No	Yes	0.0000	0.0000

Tower Section Geometry (cont'd)

Tower Elevation <i>ft</i>	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 180.00-175.00	Pipe	HSS5x.25	A572-50 (50 ksi)	Double Angle	2L2 1/2x2x3/16x3/8	A36 (36 ksi)
T2 175.00-150.00	Pipe	HSS5x.25	A572-50 (50 ksi)	Double Angle	2L2 1/2x2x3/16x3/8	A36 (36 ksi)
T3 150.00-125.00	Pipe	HSS5x.25	A572-50 (50 ksi)	Double Angle	2L3x2 1/2x1/4x3/8	A36 (36 ksi)
T4 125.00-100.00	Pipe	HSS5x.25	A572-50 (50 ksi)	Double Angle	2L3x2 1/2x1/4x3/8	A36 (36 ksi)
T5 100.00-91.67	Pipe	HSS5x.375	A572-50 (50 ksi)	Double Angle	2L3x2 1/2x1/4x3/8	A36 (36 ksi)
T6 91.67-83.33	Pipe	HSS5x.375	A572-60 (60 ksi)	Double Angle	2L3x2 1/2x1/4x3/8	A36 (36 ksi)
T7 83.33-75.00	Pipe	HSS5x.375	A572-60 (60 ksi)	Double Angle	2L3x2 1/2x1/4x3/8	A36 (36 ksi)
T8 75.00-50.00	Pipe	HSS6.875x.375	A572-60 (60 ksi)	Double Angle	2L3 1/2x3x3/8x3/8	A36 (36 ksi)
T9 50.00-37.50	Pipe	HSS6.875x.5	A572-60 (60 ksi)	Double Angle	2L3 1/2x3x3/8x3/8	A36 (36 ksi)
T10 37.50-25.00	Pipe	HSS6.875x.5	A572-60 (60 ksi)	Double Angle	2L3 1/2x3x3/8x3/8	A36 (36 ksi)
T11 25.00-0.00	Pipe	HSS6.875x.5	A572-60 (60 ksi)	Double Angle	2L3x3 1/2x5/16x3/8	A529-50 (50 ksi)

Tower Section Geometry (cont'd)

Tower Elevation <i>ft</i>	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T1 180.00-175.00	None	Flat Bar		A36 (36 ksi)	Equal Angle	L3x3x1/4	A36 (36 ksi)
T2 175.00-150.00	None	Flat Bar		A36 (36 ksi)	Equal Angle	L3x3x1/4	A36 (36 ksi)
T3 150.00-125.00	None	Flat Bar		A36 (36 ksi)	Equal Angle	L3x3x1/4	A36 (36 ksi)

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	4 of 65
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Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T4 125.00-100.00	None	Flat Bar		A36 (36 ksi)	Equal Angle	L3x3x1/4	A36 (36 ksi)
T5 100.00-91.67	None	Flat Bar		A36 (36 ksi)	Single Angle	L3x4x1/4	A36 (36 ksi)
T6 91.67-83.33	None	Flat Bar		A36 (36 ksi)	Single Angle	L3x4x1/4	A36 (36 ksi)
T7 83.33-75.00	None	Flat Bar		A36 (36 ksi)	Single Angle	L3x4x1/2	A36 (36 ksi)
T8 75.00-50.00	None	Flat Bar		A36 (36 ksi)	Equal Angle	L4x4x1/4	A36 (36 ksi)
T9 50.00-37.50	None	Flat Bar		A36 (36 ksi)	Equal Angle	L4x4x1/4	A36 (36 ksi)
T10 37.50-25.00	None	Flat Bar		A36 (36 ksi)	Equal Angle	L4x4x1/4	A36 (36 ksi)
T11 25.00-0.00	None	Flat Bar		A36 (36 ksi)	Equal Angle	L4x4x1/2	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Secondary Horizontal Type	Secondary Horizontal Size	Secondary Horizontal Grade	Inner Bracing Type	Inner Bracing Size	Inner Bracing Grade
T1 180.00-175.00	Solid Round		A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T2 175.00-150.00	Solid Round		A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T3 150.00-125.00	Solid Round		A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T4 125.00-100.00	Solid Round		A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T5 100.00-91.67	Solid Round		A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T6 91.67-83.33	Solid Round		A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T7 83.33-75.00	Solid Round		A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T8 75.00-50.00	Solid Round		A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T9 50.00-37.50	Solid Round		A572-50 (50 ksi)	Equal Angle	L3x3x1/4	A36 (36 ksi)
T10 37.50-25.00	Solid Round		A572-50 (50 ksi)	Equal Angle	L3x3x1/4	A36 (36 ksi)
T11 25.00-0.00	Solid Round		A572-50 (50 ksi)	Equal Angle	L3x3x1/4	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Calc K Single Angles	Calc K Solid Rounds	K Factors ¹									
			Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace		
			X Y	X Y	X Y	X Y	X Y	X Y	X Y	X Y		
T7 83.33-75.00	No	No	1	1	1	1	1	1	1	1	1	1
T8 75.00-50.00	No	No	1	1	1	1	1	1	1	1	1	1
T9 50.00-37.50	No	No	1	1	1	1	1	1	1	1	1	1
T10 37.50-25.00	No	No	1	1	1	1	1	1	1	1	1	1
T11 25.00-0.00	No	No	1	1	1	1	1	1	1	1	1	1

¹Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

Tower Section Geometry (cont'd)

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 180.00-175.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 175.00-150.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 150.00-125.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 125.00-100.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T5 100.00-91.67	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T6 91.67-83.33	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T7 83.33-75.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T8 75.00-50.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T9 50.00-37.50	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T10 37.50-25.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T11 25.00-0.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1 180.00-175.00	Flange	0.7500 A325X	0	1.0000 A325X	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0

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Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T2 175.00-150.00	Flange	0.7500 A325X	6	1.0000 A325X	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0
T3 150.00-125.00	Flange	0.7500 A325X	6	1.0000 A325X	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0
T4 125.00-100.00	Flange	0.7500 A325X	6	1.0000 A325X	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0
T5 100.00-91.67	Flange	0.7500 A325X	6	1.0000 A325X	1	0.6250 A325N	0	0.0000 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0
T6 91.67-83.33	Flange	0.7500 A325X	0	1.0000 A325X	1	0.6250 A325N	0	0.0000 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0
T7 83.33-75.00	Flange	0.7500 A325X	0	1.0000 A325X	1	0.6250 A325N	0	0.0000 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0
T8 75.00-50.00	Flange	1.0000 A325X	8	1.0000 A325X	1	0.6250 A325N	0	0.0000 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0
T9 50.00-37.50	Flange	1.0000 A325X	8	1.0000 A325X	1	0.6250 A325N	0	0.0000 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0
T10 37.50-25.00	Flange	1.0000 A325X	0	1.0000 A325X	1	0.6250 A325X	2	0.0000 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0
T11 25.00-0.00	Flange	1.0000 A325X	8	1.0000 A325X	1	0.6250 A325N	0	0.0000 A325N	0	0.6250 A325N	0	0.6250 A325X	2	0.6250 A325N	0

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
*** Hightower Inc Climb Report													
1/2 (CSP#19)	A	No	No	Ar (CaAa)	130.00 - 8.00	-1.5000	-0.49	1	1	0.5800	0.5800		0.25
LDF5-50A (7/8 FOAM) (CSP#20)	A	No	No	Ar (CaAa)	47.00 - 8.00	-1.5000	-0.48	1	1	1.0900	1.0900		0.33
LDF4-50A (1/2 FOAM) (CSP#21)	A	No	No	Ar (CaAa)	82.00 - 8.00	-1.5000	-0.47	1	1	0.6300	0.6300		0.15
FLC78-50J (7/8 FOAM) (CSP#22)	A	No	No	Ar (CaAa)	138.50 - 8.00	-1.5000	-0.46	1	1	1.1200	1.1200		0.40
FLC78-50J (7/8 FOAM) (CSP#23)	A	No	No	Ar (CaAa)	146.00 - 8.00	-1.5000	-0.45	1	1	1.1200	1.1200		0.40
FLC78-50J (7/8 FOAM) (CSP#24)	A	No	No	Ar (CaAa)	146.00 - 8.00	-1.5000	-0.44	1	1	1.1200	1.1200		0.40
1/2 (CSP#25)	A	No	No	Ar (CaAa)	177.00 - 8.00	-1.5000	-0.43	1	1	0.5800	0.5800		0.25
LDF5-50A (7/8 FOAM) (CSP#26)	A	No	No	Ar (CaAa)	141.50 - 8.00	-1.5000	-0.42	1	1	1.0900	1.0900		0.33
LDF5-50A (7/8 FOAM)	A	No	No	Ar (CaAa)	138.00 - 8.00	-1.5000	-0.41	1	1	1.0900	1.0900		0.33

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Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
(CSP#27) LDF5-50A (7/8 FOAM)	A	No	No	Ar (CaAa)	82.00 - 8.00	-1.5000	-0.4	1	1	1.0900	1.0900		0.33
(CSP#28) LDF5-50A (7/8 FOAM)	A	No	No	Ar (CaAa)	98.00 - 8.00	-1.5000	-0.39	1	1	1.0900	1.0900		0.33
(CSP#29) LDF5-50A (7/8 FOAM)	A	No	No	Ar (CaAa)	180.00 - 8.00	-1.5000	-0.38	1	1	1.0900	1.0900		0.33
(CSP#30) LDF4-50A (1/2 FOAM)	A	No	No	Ar (CaAa)	49.00 - 8.00	-1.5000	-0.37	1	1	0.6300	0.6300		0.15
(CSP#31) AVA7-50 (1-5/8 LOW DENS. FOAM)	A	No	No	Ar (CaAa)	180.00 - 8.00	-4.5000	-0.36	2	1	1.9800	1.9800		0.72
(CSP - Tr. D) 1/2 (CSP#33) LDF7-50A (1-5/8 FOAM)	A	No	No	Ar (CaAa)	146.00 - 8.00	-1.5000	-0.35	1	1	0.5800	0.5800		0.25
(CSP#34) LDF7-50A (1-5/8 FOAM)	A	No	No	Ar (CaAa)	172.50 - 8.00	-1.5000	-0.34	1	1	1.9800	1.9800		0.82
(CSP#35) LDF7-50A (1-5/8 FOAM)	A	No	No	Ar (CaAa)	180.00 - 8.00	-1.5000	-0.33	1	1	1.9800	1.9800		0.82
(CSP#35) LDF4-50A (1/2 FOAM)	A	No	No	Ar (CaAa)	149.00 - 8.00	-1.5000	-0.32	1	1	0.6300	0.6300		0.15
(CSP - Tr. D) LDF7-50A (1-5/8 FOAM)	A	No	No	Ar (CaAa)	180.00 - 8.00	-1.5000	-0.31	1	1	1.9800	1.9800		0.82
(CSP#37) WEP65 (CSP#38) WEP65 (CSP#39) WEP65 (CSP#40) WEP65 (CSP#41) LCF78-50J (7/8 FOAM)	A	No	No	Af (CaAa)	169.00 - 8.00	-1.5000	-0.3	1	1	1.5836	1.5836		0.53
(CSP#38) WEP65 (CSP#39) WEP65 (CSP#40) WEP65 (CSP#41) LCF78-50J (7/8 FOAM)	A	No	No	Af (CaAa)	167.00 - 8.00	-1.5000	-0.29	1	1	1.5836	1.5836		0.53
(CSP#39) WEP65 (CSP#40) WEP65 (CSP#41) LCF78-50J (7/8 FOAM)	A	No	No	Af (CaAa)	175.00 - 8.00	-1.5000	-0.28	1	1	1.5836	1.5836		0.53
(CSP#40) WEP65 (CSP#41) LCF78-50J (7/8 FOAM)	A	No	No	Af (CaAa)	79.50 - 8.00	-1.5000	-0.27	1	1	1.5836	1.5836		0.53
(CSP#41) LCF78-50J (7/8 FOAM)	A	No	No	Ar (CaAa)	98.00 - 8.00	-1.5000	-0.26	1	1	1.1000	1.1000		0.53
(CSP#42) AVA7-50 (1-5/8 LOW DENS. FOAM)	A	No	No	Ar (CaAa)	135.00 - 8.00	-1.5000	-0.25	1	1	1.9800	1.9800		0.72
(CSP#43) AVA5-50 (7/8 LOW DENS. FOAM)	A	No	No	Ar (CaAa)	114.00 - 8.00	-3.0000	-0.28	1	1	1.1000	1.1000		0.30
(CSP#44) LDF4-50A (1/2 FOAM)	A	No	No	Ar (CaAa)	115.00 - 8.00	-3.0000	-0.24	1	1	0.6300	0.6300		0.15
(CSP#45) LCF78-50J (7/8 FOAM)	A	No	No	Ar (CaAa)	115.00 - 8.00	-1.5000	-0.23	1	1	1.1000	1.1000		0.53
(CSP#46) LDF4-50A	A	No	No	Ar (CaAa)	81.00 - 8.00	-1.5000	-0.22	1	1	0.6300	0.6300		0.15

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	9 of 65
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Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
(1/2 FOAM) (CSP#47) *** Hightower Inc Climb Report *** T-Mobile Additions LDF7-50A (1-5/8 FOAM) (AT&T) Hybrid HCS 6x12 4 AWG (1-5/8") (AT&T - F.O. Cable - Existing) 1/2 (AT&T - DC Cables - Existing) **Eversource Proposed Cables** 7/8 (Eversource - Proposed) 7/8 (Eversource - Proposed) **	B	No	No	Ar (CaAa)	149.00 - 8.00	2.0000	0.39	12	12	1.9800	1.9800		0.82
	B	No	No	Ar (CaAa)	149.00 - 8.00	2.0000	0.44	1	1	1.9900	1.9900		2.59
	B	No	No	Ar (CaAa)	149.00 - 8.00	2.0000	0.455	2	2	0.5800	0.5800		0.25
	C	No	No	Ar (CaAa)	134.00 - 8.00	0.0000	0.47	1	1	1.1100	1.1100		0.54
	C	No	No	Ar (CaAa)	157.00 - 8.00	0.0000	0.49	1	1	1.1100	1.1100		0.54

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Total Number	C _{AA} ft ² /ft	Weight plf
*** Hightower Inc Climb Report **								

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight lb
T1	180.00-175.00	A	0.000	0.000	4.621	0.000	17.55
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.00
T2	175.00-150.00	A	0.000	0.000	44.530	0.000	142.28

<p>tnxTower</p> <p>AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500</p>	Job	180' Stainless, Inc. Self Supporting Lattice	Page	10 of 65
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Tower Section	Tower Elevation ft	Face	A_R ft ²	A_F ft ²	C_{AA} In Face ft ²	C_{AA} Out Face ft ²	Weight lb
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.777	0.000	3.78
T3	150.00-125.00	A	0.000	0.000	63.151	0.000	200.98
		B	0.000	0.000	64.584	0.000	310.37
		C	0.000	0.000	3.774	0.000	18.36
T4	125.00-100.00	A	0.000	0.000	76.130	0.000	246.90
		B	0.000	0.000	67.275	0.000	323.30
		C	0.000	0.000	5.550	0.000	27.00
T5	100.00-91.67	A	0.000	0.000	27.744	0.000	91.11
		B	0.000	0.000	22.425	0.000	107.77
		C	0.000	0.000	1.850	0.000	9.00
T6	91.67-83.33	A	0.000	0.000	28.182	0.000	92.83
		B	0.000	0.000	22.425	0.000	107.77
		C	0.000	0.000	1.850	0.000	9.00
T7	83.33-75.00	A	0.000	0.000	30.951	0.000	99.48
		B	0.000	0.000	22.425	0.000	107.77
		C	0.000	0.000	1.850	0.000	9.00
T8	75.00-50.00	A	0.000	0.000	97.018	0.000	307.50
		B	0.000	0.000	67.275	0.000	323.30
		C	0.000	0.000	5.550	0.000	27.00
T9	50.00-37.50	A	0.000	0.000	50.269	0.000	158.61
		B	0.000	0.000	33.638	0.000	161.65
		C	0.000	0.000	2.775	0.000	13.50
T10	37.50-25.00	A	0.000	0.000	50.659	0.000	159.75
		B	0.000	0.000	33.638	0.000	161.65
		C	0.000	0.000	2.775	0.000	13.50
T11	25.00-0.00	A	0.000	0.000	68.896	0.000	217.26
		B	0.000	0.000	45.747	0.000	219.84
		C	0.000	0.000	3.774	0.000	18.36

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A_R ft ²	A_F ft ²	C_{AA} In Face ft ²	C_{AA} Out Face ft ²	Weight lb
T1	180.00-175.00	A	1.379	0.000	0.000	13.518	0.000	158.09
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.00
T2	175.00-150.00	A	1.372	0.000	0.000	115.881	0.000	1351.65
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	2.698	0.000	32.91
T3	150.00-125.00	A	1.363	0.000	0.000	178.080	0.000	2057.34
		B		0.000	0.000	173.464	0.000	2285.57
		C		0.000	0.000	13.039	0.000	158.30
T4	125.00-100.00	A	1.356	0.000	0.000	224.148	0.000	2582.62
		B		0.000	0.000	180.550	0.000	2372.16
		C		0.000	0.000	19.107	0.000	231.19
T5	100.00-91.67	A	1.353	0.000	0.000	83.226	0.000	958.18
		B		0.000	0.000	60.167	0.000	789.71
		C		0.000	0.000	6.361	0.000	76.88
T6	91.67-83.33	A	1.353	0.000	0.000	84.729	0.000	975.66
		B		0.000	0.000	60.164	0.000	789.52
		C		0.000	0.000	6.359	0.000	76.84
T7	83.33-75.00	A	1.353	0.000	0.000	94.131	0.000	1077.53
		B		0.000	0.000	60.164	0.000	789.56
		C		0.000	0.000	6.360	0.000	76.85
T8	75.00-50.00	A	1.354	0.000	0.000	293.932	0.000	3360.95
		B		0.000	0.000	180.524	0.000	2370.54

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	11 of 65
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Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A_R ft ²	A_F ft ²	C_{AA} In Face ft ²	C_{AA} Out Face ft ²	Weight lb
T9	50.00-37.50	C		0.000	0.000	19.094	0.000	230.89
		A	1.356	0.000	0.000	154.525	0.000	1764.24
		B		0.000	0.000	90.277	0.000	1186.21
T10	37.50-25.00	C		0.000	0.000	9.554	0.000	115.62
		A	1.352	0.000	0.000	155.728	0.000	1774.14
		B		0.000	0.000	90.240	0.000	1183.92
T11	25.00-0.00	C		0.000	0.000	9.536	0.000	115.19
		A	1.308	0.000	0.000	207.279	0.000	2302.87
		B		0.000	0.000	122.101	0.000	1572.07
		C		0.000	0.000	12.665	0.000	149.67

Feed Line Center of Pressure

Section	Elevation ft	CP_x in	CP_z in	CP_x Ice in	CP_z Ice in
T1	180.00-175.00	-6.3146	2.8905	-11.4976	5.1117
T2	175.00-150.00	-13.8234	5.6149	-20.8064	8.4977
T3	150.00-125.00	1.2641	13.9320	0.0722	19.1225
T4	125.00-100.00	-1.6134	16.2124	-5.2259	22.2822
T5	100.00-91.67	-3.3608	17.2705	-8.2431	23.6967
T6	91.67-83.33	-3.7852	17.7631	-9.0040	24.4274
T7	83.33-75.00	-5.8909	18.5532	-12.3660	25.5134
T8	75.00-50.00	-7.2912	19.7649	-14.4410	27.1938
T9	50.00-37.50	-8.7442	21.1927	-17.2668	29.3625
T10	37.50-25.00	-9.2889	21.9735	-18.2779	30.5626
T11	25.00-0.00	-6.6752	16.0745	-14.1815	24.7061

Shielding Factor K_a

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
T1	8		175.00 - 177.00	0.6000	0.6000
T1	13	LDF5-50A (7/8 FOAM)	175.00 - 180.00	0.6000	0.6000
T1	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	175.00 - 180.00	0.6000	0.6000
T1	18	LDF7-50A (1-5/8 FOAM)	175.00 - 180.00	0.6000	0.6000
T1	20	LDF7-50A (1-5/8 FOAM)	175.00 - 180.00	0.6000	0.6000
T2	8		150.00 - 175.00	0.6000	0.6000
T2	13	LDF5-50A (7/8 FOAM)	150.00 - 175.00	0.6000	0.6000
T2	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	150.00 - 175.00	0.6000	0.6000
T2	17	LDF7-50A (1-5/8 FOAM)	150.00 - 172.50	0.6000	0.6000
T2	18	LDF7-50A (1-5/8 FOAM)	150.00 -	0.6000	0.6000

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
			175.00		
T2	20	LDF7-50A (1-5/8 FOAM)	150.00 -	0.6000	0.6000
			175.00		
T2	21	WEP65	150.00 -	0.6000	0.6000
			169.00		
T2	22	WEP65	150.00 -	0.6000	0.6000
			167.00		
T2	23	WEP65	150.00 -	0.6000	0.6000
			175.00		
T2	40	7/8	150.00 -	0.6000	0.6000
			157.00		
T3	2	1/2	125.00 -	0.6000	0.6000
			130.00		
T3	5	FLC78-50J (7/8 FOAM)	125.00 -	0.6000	0.6000
			138.50		
T3	6	FLC78-50J (7/8 FOAM)	125.00 -	0.6000	0.6000
			146.00		
T3	7	FLC78-50J (7/8 FOAM)	125.00 -	0.6000	0.6000
			146.00		
T3	8	1/2	125.00 -	0.6000	0.6000
			150.00		
T3	9	LDF5-50A (7/8 FOAM)	125.00 -	0.6000	0.6000
			141.50		
T3	10	LDF5-50A (7/8 FOAM)	125.00 -	0.6000	0.6000
			138.00		
T3	13	LDF5-50A (7/8 FOAM)	125.00 -	0.6000	0.6000
			150.00		
T3	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	125.00 -	0.6000	0.6000
			150.00		
T3	16	1/2	125.00 -	0.6000	0.6000
			146.00		
T3	17	LDF7-50A (1-5/8 FOAM)	125.00 -	0.6000	0.6000
			150.00		
T3	18	LDF7-50A (1-5/8 FOAM)	125.00 -	0.6000	0.6000
			150.00		
T3	19	LDF4-50A (1/2 FOAM)	125.00 -	0.6000	0.6000
			149.00		
T3	20	LDF7-50A (1-5/8 FOAM)	125.00 -	0.6000	0.6000
			150.00		
T3	21	WEP65	125.00 -	0.6000	0.6000
			150.00		
T3	22	WEP65	125.00 -	0.6000	0.6000
			150.00		
T3	23	WEP65	125.00 -	0.6000	0.6000
			150.00		
T3	26	AVA7-50 (1-5/8 LOW DENS. FOAM)	125.00 -	0.6000	0.6000
			135.00		
T3	35	LDF7-50A (1-5/8 FOAM)	125.00 -	0.6000	0.6000
			149.00		
T3	36	Hybrid HCS 6x12 4 AWG (1-5/8")	125.00 -	0.6000	0.6000
			149.00		
T3	37	1/2	125.00 -	0.6000	0.6000
			149.00		
T3	39	7/8	125.00 -	0.6000	0.6000
			134.00		
T3	40	7/8	125.00 -	0.6000	0.6000
			150.00		
T4	2	1/2	100.00 -	0.6000	0.6000
			125.00		
T4	5	FLC78-50J (7/8 FOAM)	100.00 -	0.6000	0.6000
			125.00		
T4	6	FLC78-50J (7/8 FOAM)	100.00 -	0.6000	0.6000

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Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K _a No Ice	K _a Ice
			125.00		
T4	7	FLC78-50J (7/8 FOAM)	100.00 - 125.00	0.6000	0.6000
T4	8	1/2	100.00 - 125.00	0.6000	0.6000
T4	9	LDF5-50A (7/8 FOAM)	100.00 - 125.00	0.6000	0.6000
T4	10	LDF5-50A (7/8 FOAM)	100.00 - 125.00	0.6000	0.6000
T4	13	LDF5-50A (7/8 FOAM)	100.00 - 125.00	0.6000	0.6000
T4	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	100.00 - 125.00	0.6000	0.6000
T4	16	1/2	100.00 - 125.00	0.6000	0.6000
T4	17	LDF7-50A (1-5/8 FOAM)	100.00 - 125.00	0.6000	0.6000
T4	18	LDF7-50A (1-5/8 FOAM)	100.00 - 125.00	0.6000	0.6000
T4	19	LDF4-50A (1/2 FOAM)	100.00 - 125.00	0.6000	0.6000
T4	20	LDF7-50A (1-5/8 FOAM)	100.00 - 125.00	0.6000	0.6000
T4	21	WEP65	100.00 - 125.00	0.6000	0.6000
T4	22	WEP65	100.00 - 125.00	0.6000	0.6000
T4	23	WEP65	100.00 - 125.00	0.6000	0.6000
T4	26	AVA7-50 (1-5/8 LOW DENS. FOAM)	100.00 - 125.00	0.6000	0.6000
T4	27	AVA5-50 (7/8 LOW DENS. FOAM)	100.00 - 114.00	0.6000	0.6000
T4	28	LDF4-50A (1/2 FOAM)	100.00 - 115.00	0.6000	0.6000
T4	29	LCF78-50J (7/8 FOAM)	100.00 - 115.00	0.6000	0.6000
T4	35	LDF7-50A (1-5/8 FOAM)	100.00 - 125.00	0.6000	0.6000
T4	36	Hybrid HCS 6x12 4 AWG (1-5/8")	100.00 - 125.00	0.6000	0.6000
T4	37	1/2	100.00 - 125.00	0.6000	0.6000
T4	39	7/8	100.00 - 125.00	0.6000	0.6000
T4	40	7/8	100.00 - 125.00	0.6000	0.6000
T5	2	1/2	91.67 - 100.00	0.6000	0.6000
T5	5	FLC78-50J (7/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	6	FLC78-50J (7/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	7	FLC78-50J (7/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	8	1/2	91.67 - 100.00	0.6000	0.6000
T5	9	LDF5-50A (7/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	10	LDF5-50A (7/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	12	LDF5-50A (7/8 FOAM)	91.67 - 98.00	0.6000	0.6000
T5	13	LDF5-50A (7/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	91.67 - 100.00	0.6000	0.6000
T5	16	1/2	91.67 - 100.00	0.6000	0.6000
T5	17	LDF7-50A (1-5/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	18	LDF7-50A (1-5/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	19	LDF4-50A (1/2 FOAM)	91.67 - 100.00	0.6000	0.6000

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
T5	20	LDF7-50A (1-5/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	21	WEP65	91.67 - 100.00	0.6000	0.6000
T5	22	WEP65	91.67 - 100.00	0.6000	0.6000
T5	23	WEP65	91.67 - 100.00	0.6000	0.6000
T5	25	LCF78-50J (7/8 FOAM)	91.67 - 98.00	0.6000	0.6000
T5	26	AVA7-50 (1-5/8 LOW DENS. FOAM)	91.67 - 100.00	0.6000	0.6000
T5	27	AVA5-50 (7/8 LOW DENS. FOAM)	91.67 - 100.00	0.6000	0.6000
T5	28	LDF4-50A (1/2 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	29	LCF78-50J (7/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	35	LDF7-50A (1-5/8 FOAM)	91.67 - 100.00	0.6000	0.6000
T5	36	Hybrid HCS 6x12 4 AWG (1-5/8")	91.67 - 100.00	0.6000	0.6000
T5	37	1/2	91.67 - 100.00	0.6000	0.6000
T5	39	7/8	91.67 - 100.00	0.6000	0.6000
T5	40	7/8	91.67 - 100.00	0.6000	0.6000
T6	2	1/2	83.33 - 91.67	0.6000	0.6000
T6	5	FLC78-50J (7/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	6	FLC78-50J (7/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	7	FLC78-50J (7/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	8	1/2	83.33 - 91.67	0.6000	0.6000
T6	9	LDF5-50A (7/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	10	LDF5-50A (7/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	12	LDF5-50A (7/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	13	LDF5-50A (7/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	83.33 - 91.67	0.6000	0.6000
T6	16	1/2	83.33 - 91.67	0.6000	0.6000
T6	17	LDF7-50A (1-5/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	18	LDF7-50A (1-5/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	19	LDF4-50A (1/2 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	20	LDF7-50A (1-5/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	21	WEP65	83.33 - 91.67	0.6000	0.6000
T6	22	WEP65	83.33 - 91.67	0.6000	0.6000
T6	23	WEP65	83.33 - 91.67	0.6000	0.6000
T6	25	LCF78-50J (7/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	26	AVA7-50 (1-5/8 LOW DENS. FOAM)	83.33 - 91.67	0.6000	0.6000
T6	27	AVA5-50 (7/8 LOW DENS. FOAM)	83.33 - 91.67	0.6000	0.6000
T6	28	LDF4-50A (1/2 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	29	LCF78-50J (7/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	35	LDF7-50A (1-5/8 FOAM)	83.33 - 91.67	0.6000	0.6000
T6	36	Hybrid HCS 6x12 4 AWG (1-5/8")	83.33 - 91.67	0.6000	0.6000
T6	37	1/2	83.33 - 91.67	0.6000	0.6000
T6	39	7/8	83.33 - 91.67	0.6000	0.6000
T6	40	7/8	83.33 - 91.67	0.6000	0.6000
T7	2	1/2	75.00 - 83.33	0.6000	0.6000
T7	4	LDF4-50A (1/2 FOAM)	75.00 - 82.00	0.6000	0.6000
T7	5	FLC78-50J (7/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	6	FLC78-50J (7/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	7	FLC78-50J (7/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	8	1/2	75.00 - 83.33	0.6000	0.6000
T7	9	LDF5-50A (7/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	10	LDF5-50A (7/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	11	LDF5-50A (7/8 FOAM)	75.00 - 82.00	0.6000	0.6000
T7	12	LDF5-50A (7/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	13	LDF5-50A (7/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	75.00 - 83.33	0.6000	0.6000

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Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
T7	16	1/2	75.00 - 83.33	0.6000	0.6000
T7	17	LDF7-50A (1-5/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	18	LDF7-50A (1-5/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	19	LDF4-50A (1/2 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	20	LDF7-50A (1-5/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	21	WEP65	75.00 - 83.33	0.6000	0.6000
T7	22	WEP65	75.00 - 83.33	0.6000	0.6000
T7	23	WEP65	75.00 - 83.33	0.6000	0.6000
T7	24	WEP65	75.00 - 79.50	0.6000	0.6000
T7	25	LCF78-50J (7/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	26	AVA7-50 (1-5/8 LOW DENS. FOAM)	75.00 - 83.33	0.6000	0.6000
T7	27	AVA5-50 (7/8 LOW DENS. FOAM)	75.00 - 83.33	0.6000	0.6000
T7	28	LDF4-50A (1/2 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	29	LCF78-50J (7/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	30	LDF4-50A (1/2 FOAM)	75.00 - 81.00	0.6000	0.6000
T7	35	LDF7-50A (1-5/8 FOAM)	75.00 - 83.33	0.6000	0.6000
T7	36	Hybrid HCS 6x12 4 AWG (1-5/8")	75.00 - 83.33	0.6000	0.6000
T7	37	1/2	75.00 - 83.33	0.6000	0.6000
T7	39	7/8	75.00 - 83.33	0.6000	0.6000
T7	40	7/8	75.00 - 83.33	0.6000	0.6000
T8	2	1/2	50.00 - 75.00	0.6000	0.6000
T8	4	LDF4-50A (1/2 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	5	FLC78-50J (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	6	FLC78-50J (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	7	FLC78-50J (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	8	1/2	50.00 - 75.00	0.6000	0.6000
T8	9	LDF5-50A (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	10	LDF5-50A (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	11	LDF5-50A (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	12	LDF5-50A (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	13	LDF5-50A (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	50.00 - 75.00	0.6000	0.6000
T8	16	1/2	50.00 - 75.00	0.6000	0.6000
T8	17	LDF7-50A (1-5/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	18	LDF7-50A (1-5/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	19	LDF4-50A (1/2 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	20	LDF7-50A (1-5/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	21	WEP65	50.00 - 75.00	0.6000	0.6000
T8	22	WEP65	50.00 - 75.00	0.6000	0.6000
T8	23	WEP65	50.00 - 75.00	0.6000	0.6000
T8	24	WEP65	50.00 - 75.00	0.6000	0.6000
T8	25	LCF78-50J (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	26	AVA7-50 (1-5/8 LOW DENS. FOAM)	50.00 - 75.00	0.6000	0.6000
T8	27	AVA5-50 (7/8 LOW DENS. FOAM)	50.00 - 75.00	0.6000	0.6000
T8	28	LDF4-50A (1/2 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	29	LCF78-50J (7/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	30	LDF4-50A (1/2 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	35	LDF7-50A (1-5/8 FOAM)	50.00 - 75.00	0.6000	0.6000
T8	36	Hybrid HCS 6x12 4 AWG (1-5/8")	50.00 - 75.00	0.6000	0.6000
T8	37	1/2	50.00 - 75.00	0.6000	0.6000
T8	39	7/8	50.00 - 75.00	0.6000	0.6000
T8	40	7/8	50.00 - 75.00	0.6000	0.6000
T9	2	1/2	37.50 - 50.00	0.6000	0.6000
T9	3	LDF5-50A (7/8 FOAM)	37.50 - 47.00	0.6000	0.6000
T9	4	LDF4-50A (1/2 FOAM)	37.50 - 50.00	0.6000	0.6000

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
T9	5	FLC78-50J (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	6	FLC78-50J (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	7	FLC78-50J (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	8	1/2	37.50 - 50.00	0.6000	0.6000
T9	9	LDF5-50A (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	10	LDF5-50A (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	11	LDF5-50A (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	12	LDF5-50A (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	13	LDF5-50A (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	14	LDF4-50A (1/2 FOAM)	37.50 - 49.00	0.6000	0.6000
T9	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	37.50 - 50.00	0.6000	0.6000
T9	16	1/2	37.50 - 50.00	0.6000	0.6000
T9	17	LDF7-50A (1-5/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	18	LDF7-50A (1-5/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	19	LDF4-50A (1/2 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	20	LDF7-50A (1-5/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	21	WEP65	37.50 - 50.00	0.6000	0.6000
T9	22	WEP65	37.50 - 50.00	0.6000	0.6000
T9	23	WEP65	37.50 - 50.00	0.6000	0.6000
T9	24	WEP65	37.50 - 50.00	0.6000	0.6000
T9	25	LCF78-50J (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	26	AVA7-50 (1-5/8 LOW DENS. FOAM)	37.50 - 50.00	0.6000	0.6000
T9	27	AVA5-50 (7/8 LOW DENS. FOAM)	37.50 - 50.00	0.6000	0.6000
T9	28	LDF4-50A (1/2 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	29	LCF78-50J (7/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	30	LDF4-50A (1/2 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	35	LDF7-50A (1-5/8 FOAM)	37.50 - 50.00	0.6000	0.6000
T9	36	Hybrid HCS 6x12 4 AWG (1-5/8")	37.50 - 50.00	0.6000	0.6000
T9	37	1/2	37.50 - 50.00	0.6000	0.6000
T9	39	7/8	37.50 - 50.00	0.6000	0.6000
T9	40	7/8	37.50 - 50.00	0.6000	0.6000
T10	2	1/2	25.00 - 37.50	0.6000	0.6000
T10	3	LDF5-50A (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	4	LDF4-50A (1/2 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	5	FLC78-50J (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	6	FLC78-50J (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	7	FLC78-50J (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	8	1/2	25.00 - 37.50	0.6000	0.6000
T10	9	LDF5-50A (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	10	LDF5-50A (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	11	LDF5-50A (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	12	LDF5-50A (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	13	LDF5-50A (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	14	LDF4-50A (1/2 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	15	AVA7-50 (1-5/8 LOW DENS. FOAM)	25.00 - 37.50	0.6000	0.6000
T10	16	1/2	25.00 - 37.50	0.6000	0.6000
T10	17	LDF7-50A (1-5/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	18	LDF7-50A (1-5/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	19	LDF4-50A (1/2 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	20	LDF7-50A (1-5/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	21	WEP65	25.00 - 37.50	0.6000	0.6000
T10	22	WEP65	25.00 - 37.50	0.6000	0.6000
T10	23	WEP65	25.00 - 37.50	0.6000	0.6000
T10	24	WEP65	25.00 - 37.50	0.6000	0.6000
T10	25	LCF78-50J (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	26	AVA7-50 (1-5/8 LOW DENS. FOAM)	25.00 - 37.50	0.6000	0.6000

Job	180' Stainless, Inc. Self Supporting Lattice	Page	17 of 65
Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
T10	27	AVA5-50 (7/8 LOW DENSIFOAM)	25.00 - 37.50	0.6000	0.6000
T10	28	LDF4-50A (1/2 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	29	LCF78-50J (7/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	30	LDF4-50A (1/2 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	35	LDF7-50A (1-5/8 FOAM)	25.00 - 37.50	0.6000	0.6000
T10	36	Hybrid HCS 6x12 4 AWG (1-5/8")	25.00 - 37.50	0.6000	0.6000
T10	37	1/2	25.00 - 37.50	0.6000	0.6000
T10	39	7/8	25.00 - 37.50	0.6000	0.6000
T10	40	7/8	25.00 - 37.50	0.6000	0.6000
T11	2	1/2	8.00 - 25.00	0.6000	0.6000
T11	3	LDF5-50A (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	4	LDF4-50A (1/2 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	5	FLC78-50J (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	6	FLC78-50J (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	7	FLC78-50J (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	8	1/2	8.00 - 25.00	0.6000	0.6000
T11	9	LDF5-50A (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	10	LDF5-50A (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	11	LDF5-50A (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	12	LDF5-50A (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	13	LDF5-50A (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	14	LDF4-50A (1/2 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	15	AVA7-50 (1-5/8 LOW DENSIFOAM)	8.00 - 25.00	0.6000	0.6000
T11	16	1/2	8.00 - 25.00	0.6000	0.6000
T11	17	LDF7-50A (1-5/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	18	LDF7-50A (1-5/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	19	LDF4-50A (1/2 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	20	LDF7-50A (1-5/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	21	WEP65	8.00 - 25.00	0.6000	0.6000
T11	22	WEP65	8.00 - 25.00	0.6000	0.6000
T11	23	WEP65	8.00 - 25.00	0.6000	0.6000
T11	24	WEP65	8.00 - 25.00	0.6000	0.6000
T11	25	LCF78-50J (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	26	AVA7-50 (1-5/8 LOW DENSIFOAM)	8.00 - 25.00	0.6000	0.6000
T11	27	AVA5-50 (7/8 LOW DENSIFOAM)	8.00 - 25.00	0.6000	0.6000
T11	28	LDF4-50A (1/2 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	29	LCF78-50J (7/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	30	LDF4-50A (1/2 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	35	LDF7-50A (1-5/8 FOAM)	8.00 - 25.00	0.6000	0.6000
T11	36	Hybrid HCS 6x12 4 AWG (1-5/8")	8.00 - 25.00	0.6000	0.6000
T11	37	1/2	8.00 - 25.00	0.6000	0.6000
T11	39	7/8	8.00 - 25.00	0.6000	0.6000
T11	40	7/8	8.00 - 25.00	0.6000	0.6000

Discrete Tower Loads

Job	180' Stainless, Inc. Self Supporting Lattice	Page	18 of 65
Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			ft ft ft	°	ft	ft ²	ft ²	lb
*** Hightower CLimb Inventory - 10/24/2016								
Pirod 4' Side Mount Standoff (1)	C	From Leg	0.00	0.0000	48.00	No Ice	2.72	50.00
(Shared HGT-1&2 / CSP#23,21)			0.00			1/2" Ice	4.91	89.00
			0.00			1" Ice	7.10	128.00
6'8"x4" Pipe Mount (Shared HGT-1&2 / CSP#23,21)	C	From Leg	0.00	0.0000	48.00	No Ice	1.93	72.00
			0.00			1/2" Ice	3.01	93.13
			0.00			1" Ice	3.42	118.95
DB803M-XT (HGT-2/CSP#21)	C	From Leg	4.00	0.0000	49.00	No Ice	0.50	4.30
			0.00			1/2" Ice	0.68	8.98
			2.50			1" Ice	0.87	15.80
4'x4" Pipe Mount (Shared HGT-3&4/CSP#16,#22)	B	From Leg	0.00	0.0000	80.00	No Ice	1.08	44.00
			0.00			1/2" Ice	1.58	56.99
			0.00			1" Ice	1.84	73.03
DB222 (HGT-4/CSP#22)	B	From Leg	0.50	0.0000	81.00	No Ice	1.60	16.00
			0.00			1/2" Ice	2.88	20.80
			5.00			1" Ice	4.16	25.60
(inverted) DB212-1 (HGT-5/CSP#8)	C	From Leg	4.00	0.0000	81.00	No Ice	4.50	31.00
			0.00			1/2" Ice	8.10	40.30
			-5.00			1" Ice	11.70	49.60
DB212-1 (HGT-6/CSP#15)	C	From Leg	4.00	0.0000	86.00	No Ice	4.50	31.00
			0.00			1/2" Ice	8.10	40.30
			0.00			1" Ice	11.70	49.60
Pirod 4' Side Mount Standoff (1)	C	From Leg	0.00	0.0000	86.00	No Ice	2.72	50.00
(Shared HGT-5&6 / CSP#8,15)			0.00			1/2" Ice	4.91	89.00
			0.00			1" Ice	7.10	128.00
DB222 (HGT-7 / CSP#13 (Twr Face Mt.))	C	From Face	0.00	0.0000	100.00	No Ice	1.60	16.00
			-3.00			1/2" Ice	2.88	20.80
			0.00			1" Ice	4.16	25.60
PD458-1 (HGT-8 / CSP#14 (Twr Face Mt.))	C	From Face	0.00	0.0000	105.00	No Ice	2.88	24.00
			-4.00			1/2" Ice	4.34	46.22
			0.00			1" Ice	5.83	77.59
DS9A09F36D-N 19 ft Omni w/ Mount Pipe (HGT-9 / CSP)	C	From Leg	5.00	0.0000	116.00	No Ice	6.95	98.25
			0.00			1/2" Ice	9.21	152.99
			5.00			1" Ice	11.49	221.39
DB-B1-6C-8AB-0Z Dist. Box (HGT-10 / CSP#24)	C	From Leg	2.50	0.0000	116.00	No Ice	5.60	45.00
			0.00			1/2" Ice	5.92	81.13
			0.00			1" Ice	6.24	121.22
Pirod 4' Side Mount Standoff (1)	C	From Leg	0.00	0.0000	116.00	No Ice	2.72	50.00
(HGT-9,10 / CSP#24)			0.00			1/2" Ice	4.91	89.00
			0.00			1" Ice	7.10	128.00
12' Dipole (HGT-11 / CSP)	A	From Leg	5.00	0.0000	138.00	No Ice	3.70	40.00
			0.00			1/2" Ice	3.95	78.90
			0.00			1" Ice	4.22	121.78
Pirod 4' Side Mount Standoff (1)	A	From Leg	0.00	0.0000	138.00	No Ice	2.72	50.00
(HGT-11 / CSP)			0.00			1/2" Ice	4.91	89.00
			0.00			1" Ice	7.10	128.00
DB224-A (HGT-13 / CSP)	B	From Leg	2.00	0.0000	136.00	No Ice	3.15	32.00
			0.00			1/2" Ice	5.67	41.60
			10.00			1" Ice	8.19	51.20
2'6"x4" Pipe Mount (HGT-13 / CSP)	B	From Leg	0.00	0.0000	136.00	No Ice	0.64	27.00
			0.00			1/2" Ice	0.91	35.41
			0.00			1" Ice	1.09	45.95
(inverted) 20' 8 Bay Di-Pole (HGT-14 / CSP#11)	A	From Face	4.00	0.0000	136.00	No Ice	4.00	55.00
			0.00			1/2" Ice	6.00	100.00

Job	180' Stainless, Inc. Self Supporting Lattice	Page	20 of 65
Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C _{AA} Front ft ²	C _{AA} Side ft ²	Weight lb	
5,7)									
Pirod 4' Side Mount Standoff (1) (HGT-30 / CSP#19)	A	From Leg	0.00 0.00 0.00	-30.0000	180.00	No Ice 1/2" Ice 1" Ice	2.72 4.91 7.10	2.72 4.91 7.10	50.00 89.00 128.00
Pirod 4' Side Mount Standoff (1) (HGT-30 / CSP#19)	A	From Face	4.00 0.00 0.00	30.0000	180.00	No Ice 1/2" Ice 1" Ice	2.72 4.91 7.10	2.72 4.91 7.10	50.00 89.00 128.00
PD440-2 (HGT-30 / CSP-19)	A	From Leg	4.00 0.00 5.00	0.0000	181.00	No Ice 1/2" Ice 1" Ice	1.38 2.48 3.59	1.38 2.48 3.59	19.00 24.70 30.40
DB225-A (HGT-31 / CSP#-17)	C	From Leg	0.00 0.00 0.00	0.0000	178.00	No Ice 1/2" Ice 1" Ice	3.21 5.78 8.35	3.21 5.78 8.35	37.00 48.10 59.20
*** Hightower CLimb Inventory - 10/24/2016									
*** CSP Additional Antennas - 10/2/2017									
USF-2U w/ TAM-II adapter with 8' 2-3/8" Pipe (CSP - Troop D)	C	From Leg	0.00 0.00 0.00	0.0000	175.00	No Ice 1/2" Ice 1" Ice	3.44 4.59 5.76	6.04 7.76 9.48	197.50 214.60 236.60
10'6"x4" Pipe Mount (CSP - Troop D)	C	From Leg	0.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice 1" Ice	3.20 5.62 6.25	3.20 5.62 6.25	114.00 146.84 186.71
SE4192-SWBP4LDF(Dxx-E6 461) Panel Anenna (CSP - Troop D)	C	From Leg	0.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice 1" Ice	8.70 10.73 12.78	25.50 26.96 28.25	56.00 144.00 246.93
(inverted) SC479-HF1LDF (CSP - Troop D)	C	From Leg	0.00 0.00 -7.25	0.0000	173.00	No Ice 1/2" Ice 1" Ice	5.06 6.54 8.04	5.06 6.54 8.04	30.00 69.82 114.98
3'4"x4" Pipe Mount (CSP - Troop D)	C	From Leg	0.00 0.00 0.00	0.0000	177.00	No Ice 1/2" Ice 1" Ice	0.87 1.27 1.49	0.87 1.27 1.49	36.00 46.95 60.55
(inverted) SC479-HF1LDF (CSP - Troop D)	C	From Leg	0.00 0.00 -7.25	0.0000	173.00	No Ice 1/2" Ice 1" Ice	5.06 6.54 8.04	5.06 6.54 8.04	30.00 69.82 114.98
432E-83I-01T TTA Unit (CSP - Troop D)	C	From Leg	0.00 0.00 0.00	0.0000	180.00	No Ice 1/2" Ice 1" Ice	3.33 3.57 3.82	1.11 1.27 1.45	25.00 44.70 67.39
*** CSP Additional Antennas - 10/2/2017									
*** T-Mobile Additions 12/2017									
*** SMK-006 Proposed AT&T Config (01202020)									
Valmont 13' Lightweight T-Frame (AT&T)	A	From Leg	0.50 0.00 0.00	30.0000	150.00	No Ice 1/2" Ice 1" Ice	10.60 16.80 23.00	10.60 16.80 23.00	255.00 359.00 463.00
Valmont 13' Lightweight T-Frame (AT&T)	B	From Leg	0.50 0.00 0.00	30.0000	150.00	No Ice 1/2" Ice 1" Ice	10.60 16.80 23.00	10.60 16.80 23.00	255.00 359.00 463.00
Valmont 13' Lightweight T-Frame (AT&T)	C	From Leg	0.50 0.00 0.00	30.0000	150.00	No Ice 1/2" Ice 1" Ice	10.60 16.80 23.00	10.60 16.80 23.00	255.00 359.00 463.00
(2) 7770.00 panel antenna (AT&T)	A	From Leg	0.50 0.00 0.00	0.0000	149.00	No Ice 1/2" Ice 1" Ice	5.90 6.34 6.78	4.01 4.64 5.28	52.03 97.08 148.33
(2) 7770.00 panel antenna	B	From Leg	0.50 0.00 0.00	0.0000	149.00	No Ice 1/2" Ice 1" Ice	5.90 6.34 6.78	4.01 4.64 5.28	52.03 97.08 148.33

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Vert					
			ft	ft	°	ft	ft ²	ft ²	lb
(AT&T)			0.00			1/2" Ice	6.34	4.64	97.08
			0.00			1" Ice	6.78	5.28	148.33
(2) 7770.00 panel antenna (AT&T)	C	From Leg	0.50		0.0000	No Ice	5.90	4.01	52.03
			0.00			1/2" Ice	6.34	4.64	97.08
			0.00			1" Ice	6.78	5.28	148.33
AM-X-CD-17-65-00T (AT&T)	C	From Face	3.00		0.0000	No Ice	4.62	3.70	30.00
			0.00			1/2" Ice	5.03	4.11	58.78
			0.00			1" Ice	5.46	4.53	92.82
AM-X-CD-17-65-00T (AT&T)	A	From Face	3.00		0.0000	No Ice	4.62	3.70	30.00
			0.00			1/2" Ice	5.03	4.11	58.78
			0.00			1" Ice	5.46	4.53	92.82
AM-X-CD-16-65-00T (AT&T)	B	From Face	3.00		0.0000	No Ice	4.62	3.70	30.00
			0.00			1/2" Ice	5.03	4.11	58.78
			0.00			1" Ice	5.46	4.53	92.82
(2) LPG21401 TMA (AT&T)	A	From Face	3.00		0.0000	No Ice	0.95	0.37	17.50
			0.00			1/2" Ice	1.09	0.48	23.31
			0.00			1" Ice	1.24	0.60	30.86
(2) LPG21401 TMA (AT&T)	B	From Face	3.00		0.0000	No Ice	0.95	0.37	17.50
			0.00			1/2" Ice	1.09	0.48	23.31
			0.00			1" Ice	1.24	0.60	30.86
(2) LPG21401 TMA (AT&T)	C	From Face	3.00		0.0000	No Ice	0.95	0.37	17.50
			0.00			1/2" Ice	1.09	0.48	23.31
			0.00			1" Ice	1.24	0.60	30.86
Ericsson RRUS-12 RRH Unit (AT&T)	A	From Leg	0.50		0.0000	No Ice	3.67	1.49	58.00
			0.00			1/2" Ice	3.93	1.67	81.22
			0.00			1" Ice	4.19	1.87	107.64
Ericsson RRUS-12 RRH Unit (AT&T)	B	From Leg	0.50		0.0000	No Ice	3.67	1.49	58.00
			0.00			1/2" Ice	3.93	1.67	81.22
			0.00			1" Ice	4.19	1.87	107.64
Ericsson RRUS-12 RRH Unit (AT&T)	C	From Leg	0.50		0.0000	No Ice	3.67	1.49	58.00
			0.00			1/2" Ice	3.93	1.67	81.22
			0.00			1" Ice	4.19	1.87	107.64
* tower Lightning Rod 10'6"x4" Pipe Mount (Tower)	A	From Leg	0.00		0.0000	No Ice	3.19	3.19	114.00
			0.00			1/2" Ice	5.62	5.62	146.84
			5.00			1" Ice	6.25	6.25	186.71
Lightning Rod 5/8x4' (Tower)	A	From Leg	0.00		0.0000	No Ice	0.25	0.25	31.00
			0.00			1/2" Ice	0.66	0.66	33.82
			15.00			1" Ice	0.97	0.97	39.29
DC6-48-60-18-8F (AT&T)	C	From Leg	0.00		0.0000	No Ice	1.33	1.33	30.00
			0.00			1/2" Ice	1.53	1.53	48.71
			0.00			1" Ice	1.73	1.73	67.01
RRUS-11 (AT&T)	C	From Face	3.00		0.0000	No Ice	2.57	1.07	50.00
			0.00			1/2" Ice	2.76	1.21	69.57
			0.00			1" Ice	2.97	1.36	92.08
RRUS-11 (AT&T)	B	From Face	3.00		0.0000	No Ice	2.57	1.07	50.00
			0.00			1/2" Ice	2.76	1.21	69.57
			0.00			1" Ice	2.97	1.36	92.08
RRUS-11 (AT&T)	A	From Face	3.00		0.0000	No Ice	2.57	1.07	50.00
			0.00			1/2" Ice	2.76	1.21	69.57
			0.00			1" Ice	2.97	1.36	92.08
Eversource Equipment									
ANT220F2 w/clamps (Eversource - Proposed)	A	From Leg	0.50		0.0000	No Ice	0.58	0.58	14.00
			0.00			1/2" Ice	0.81	0.81	25.19
			0.00			1" Ice	1.04	1.04	36.38
ANT220F2 w/clamps (Eversource - Proposed)	B	From Leg	0.50		0.0000	No Ice	0.58	0.58	14.00
			0.00			1/2" Ice	0.81	0.81	25.19

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	22 of 65
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	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Lateral					
			ft	ft	°	ft	ft ²	ft ²	lb
Site Pro USF-4U w/ (2) Stiff-Arm Supports (Eversource - Proposed)	A	From Leg	0.00		0.0000	134.00	1" Ice	1.04	36.38
			0.50				No Ice	1.25	165.00
			0.00				1/2" Ice	1.49	198.00
Site Pro USF-4U w/ (2) Stiff-Arm Supports (Eversource - Proposed)	B	From Leg	0.00		0.0000	157.00	1" Ice	3.02	231.00
			0.50				No Ice	1.25	165.00
			0.00				1/2" Ice	1.49	198.00
			0.00				1" Ice	1.73	231.00

Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight	
				Horz	Lateral							
				ft	ft	°	°	ft	ft	ft ²	lb	
10 FT DISH (HGT-27 / CSP#1)	B	Paraboloid w/Radome	From Leg	1.00		Worst		175.00	10.00	No Ice	78.54	317.00
				0.00						1/2" Ice	79.81	726.71
				0.00						1" Ice	81.09	1136.42
8 FT DISH (HGT-23 / CSP#3)	C	Paraboloid w/Radome	From Leg	0.50		Worst		169.00	8.00	No Ice	50.30	251.00
				0.00						1/2" Ice	51.29	514.30
				0.00						1" Ice	52.28	777.60
8 FT DISH (HGT-22 / CSP#2)	B	Paraboloid w/Radome	From Leg	0.50		Worst		167.00	8.00	No Ice	50.30	251.00
				0.00						1/2" Ice	51.29	514.30
				0.00						1" Ice	52.28	777.60
8 FT DISH (HGT-3/CSP#16)	B	Paraboloid w/Radome	From Leg	0.50		Worst		79.00	8.00	No Ice	50.30	251.00
				0.00						1/2" Ice	51.29	514.30
				0.00						1" Ice	52.28	777.60

222-H Verification Constants

Constant	Value
K _d	0.85
Ice Thickness Importance Factor	1.15
Z _g	1200
α	7
K _{zmin}	0.7
K _c	0.9
K _t	0.53
f	2
K _e	1

222-H Section Verification ArRr By Element

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Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section Elevation	Elem. Num.	Size	C	C w/Ice	F a c e	e	e w/Ice	A _r	A _r w/Ice	A _r R _r	A _r R _r w/Ice
ft								ft ²	ft ²	ft ²	ft ²
T1 180.00-175.00	1	HSS5x.25	64.134	35.536	C	0.173	0.308	2.086	3.236	1.002	1.946
	1	HSS5x.25	64.134	35.536	A	0.173	0.308	2.086	3.236	1.002	1.946
	2	HSS5x.25	64.134	35.536	C	0.173	0.308	2.086	3.236	1.002	1.946
	2	HSS5x.25	64.134	35.536	B	0.173	0.308	2.086	3.236	1.002	1.946
	3	HSS5x.25	64.134	35.536	B	0.173	0.308	2.086	3.236	1.002	1.946
	3	HSS5x.25	64.134	35.536	A	0.173	0.308	2.086	3.236	1.002	1.946
							Sum:		4.171	6.471	2.003
								4.171	6.471	2.003	3.892
								4.171	6.471	2.003	3.892
T2 175.00-150.00	16	HSS5x.25	63.699	35.236	C	0.135	0.236	10.428	16.151	4.880	9.397
	16	HSS5x.25	63.699	35.236	A	0.135	0.236	10.428	16.151	4.880	9.397
	17	HSS5x.25	63.699	35.236	C	0.135	0.236	10.428	16.151	4.880	9.397
	17	HSS5x.25	63.699	35.236	B	0.135	0.236	10.428	16.151	4.880	9.397
	18	HSS5x.25	63.699	35.236	B	0.135	0.236	10.428	16.151	4.880	9.397
	18	HSS5x.25	63.699	35.236	A	0.135	0.236	10.428	16.151	4.880	9.397
							Sum:		20.856	32.302	9.759
								20.856	32.302	9.759	18.793
								20.856	32.302	9.759	18.793
T3 150.00-125.00	55	HSS5x.25	63.064	34.798	C	0.13	0.223	10.428	16.111	4.889	9.327
	55	HSS5x.25	63.064	34.798	A	0.13	0.223	10.428	16.111	4.889	9.327
	56	HSS5x.25	63.064	34.798	C	0.13	0.223	10.428	16.111	4.889	9.327
	56	HSS5x.25	63.064	34.798	B	0.13	0.223	10.428	16.111	4.889	9.327
	57	HSS5x.25	63.064	34.798	B	0.13	0.223	10.428	16.111	4.889	9.327
	57	HSS5x.25	63.064	34.798	A	0.13	0.223	10.428	16.111	4.889	9.327
							Sum:		20.856	32.222	9.779
								20.856	32.222	9.779	18.655
								20.856	32.222	9.779	18.655
T4 125.00-100.00	94	HSS5x.25	62.611	34.487	C	0.12	0.208	10.428	16.082	4.877	9.261
	94	HSS5x.25	62.611	34.487	A	0.12	0.208	10.428	16.082	4.877	9.261
	95	HSS5x.25	62.611	34.487	C	0.12	0.208	10.428	16.082	4.877	9.261
	95	HSS5x.25	62.611	34.487	B	0.12	0.208	10.428	16.082	4.877	9.261
	96	HSS5x.25	62.611	34.487	B	0.12	0.208	10.428	16.082	4.877	9.261
	96	HSS5x.25	62.611	34.487	A	0.12	0.208	10.428	16.082	4.877	9.261
							Sum:		20.856	32.165	9.755
								20.856	32.165	9.755	18.523
								20.856	32.165	9.755	18.523
T5 100.00-91.67	133	HSS5x.375	62.451	34.377	C	0.115	0.199	3.476	5.357	1.623	3.077
	133	HSS5x.375	62.451	34.377	A	0.115	0.199	3.476	5.357	1.623	3.077
	134	HSS5x.375	62.451	34.377	C	0.115	0.199	3.476	5.357	1.623	3.077
	134	HSS5x.375	62.451	34.377	B	0.115	0.199	3.476	5.357	1.623	3.077
	135	HSS5x.375	62.451	34.377	B	0.115	0.199	3.476	5.357	1.623	3.077
	135	HSS5x.375	62.451	34.377	A	0.115	0.199	3.476	5.357	1.623	3.077
							Sum:		6.952	10.715	3.245
								6.952	10.715	3.245	6.155
								6.952	10.715	3.245	6.155
T6 91.67-83.33	148	HSS5x.375	62.422	34.358	C	0.113	0.196	3.476	5.357	1.621	3.074
	148	HSS5x.375	62.422	34.358	A	0.113	0.196	3.476	5.357	1.621	3.074
	149	HSS5x.375	62.422	34.358	C	0.113	0.196	3.476	5.357	1.621	3.074
	149	HSS5x.375	62.422	34.358	B	0.113	0.196	3.476	5.357	1.621	3.074
	150	HSS5x.375	62.422	34.358	B	0.113	0.196	3.476	5.357	1.621	3.074
	150	HSS5x.375	62.422	34.358	A	0.113	0.196	3.476	5.357	1.621	3.074
							Sum:		6.952	10.714	3.242
								6.952	10.714	3.242	6.147
								6.952	10.714	3.242	6.147
T7 83.33-75.00	163	HSS5x.375	62.428	34.361	C	0.111	0.193	3.476	5.357	1.619	3.071
	163	HSS5x.375	62.428	34.361	A	0.111	0.193	3.476	5.357	1.619	3.071

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Section Elevation	Elem. Num.	Size	C	C w/Ice	F a c e	e	e w/Ice	A _r	A _r w/Ice	A _r R _r	A _r R _r w/Ice	
ft								ft ²	ft ²	ft ²	ft ²	
T8 75.00-50.00	164	HSS5x.375	62.428	34.361	C	0.111	0.193	3.476	5.357	1.619	3.071	
	164	HSS5x.375	62.428	34.361	B	0.111	0.193	3.476	5.357	1.619	3.071	
	165	HSS5x.375	62.428	34.361	B	0.111	0.193	3.476	5.357	1.619	3.071	
	165	HSS5x.375	62.428	34.361	A	0.111	0.193	3.476	5.357	1.619	3.071	
					A			Sum:	6.952	10.714	3.237	6.141
					B				6.952	10.714	3.237	6.141
					C				6.952	10.714	3.237	6.141
	178	HSS6.875x.375	85.972	42.802	C	0.116	0.18	14.338	19.987	5.767	11.419	
	178	HSS6.875x.375	85.972	42.802	A	0.116	0.18	14.338	19.987	5.767	11.419	
	179	HSS6.875x.375	85.972	42.802	C	0.116	0.18	14.338	19.987	5.767	11.419	
	179	HSS6.875x.375	85.972	42.802	B	0.116	0.18	14.338	19.987	5.767	11.419	
	180	HSS6.875x.375	85.972	42.802	B	0.116	0.18	14.338	19.987	5.767	11.419	
180	HSS6.875x.375	85.972	42.802	A	0.116	0.18	14.338	19.987	5.767	11.419		
				A			Sum:	28.676	39.975	11.534	22.837	
				B				28.676	39.975	11.534	22.837	
				C				28.676	39.975	11.534	22.837	
T9 50.00-37.50	205	HSS6.875x.5	86.108	42.883	C	0.111	0.173	7.169	9.997	2.867	5.701	
	205	HSS6.875x.5	86.108	42.883	A	0.111	0.173	7.169	9.997	2.867	5.701	
	206	HSS6.875x.5	86.108	42.883	C	0.111	0.173	7.169	9.997	2.867	5.701	
	206	HSS6.875x.5	86.108	42.883	B	0.111	0.173	7.169	9.997	2.867	5.701	
	207	HSS6.875x.5	86.108	42.883	B	0.111	0.173	7.169	9.997	2.867	5.701	
	207	HSS6.875x.5	86.108	42.883	A	0.111	0.173	7.169	9.997	2.867	5.701	
					A			Sum:	14.338	19.994	5.734	11.402
				B				14.338	19.994	5.734	11.402	
				C				14.338	19.994	5.734	11.402	
T10 37.50-25.00	220	HSS6.875x.5	85.777	42.686	C	0.108	0.169	7.169	9.989	2.858	5.691	
	220	HSS6.875x.5	85.777	42.686	A	0.108	0.169	7.169	9.989	2.858	5.691	
	221	HSS6.875x.5	85.777	42.686	C	0.108	0.169	7.169	9.989	2.858	5.691	
	221	HSS6.875x.5	85.777	42.686	B	0.108	0.169	7.169	9.989	2.858	5.691	
	222	HSS6.875x.5	85.777	42.686	B	0.108	0.169	7.169	9.989	2.858	5.691	
	222	HSS6.875x.5	85.777	42.686	A	0.108	0.169	7.169	9.989	2.858	5.691	
					A			Sum:	14.338	19.979	5.715	11.381
				B				14.338	19.979	5.715	11.381	
				C				14.338	19.979	5.715	11.381	
T11 25.00-0.00	235	HSS6.875x.5	92.61	45.656	C	0.121	0.197	14.338	19.792	5.804	11.361	
	235	HSS6.875x.5	92.61	45.656	A	0.121	0.197	14.338	19.792	5.804	11.361	
	236	HSS6.875x.5	92.61	45.656	C	0.121	0.197	14.338	19.792	5.804	11.361	
	236	HSS6.875x.5	92.61	45.656	B	0.121	0.197	14.338	19.792	5.804	11.361	
	237	HSS6.875x.5	92.61	45.656	B	0.121	0.197	14.338	19.792	5.804	11.361	
	237	HSS6.875x.5	92.61	45.656	A	0.121	0.197	14.338	19.792	5.804	11.361	
					A			Sum:	28.676	39.584	11.607	22.722
				B				28.676	39.584	11.607	22.722	
				C				28.676	39.584	11.607	22.722	

222-H Section Verification Tables - No Ice

Section Elevation	z _{wind}	z _{ice}	K _z	K _h	K _{st}	t _z	q _z	F a c e	e	A _r R _r
ft	ft	ft				in	psf			ft ²
T1 180.00-175.00	177.50		1.164	25.211	1.038		52	A	0.173	2.003
								B	0.173	2.003
								C	0.173	2.003

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	25 of 65
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	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section Elevation	z_{wind}	z_{ice}	K_z	K_h	K_{zt}	t_z	q_z	F_{ac}	e	A_{R_r}
ft	ft	ft				in	psf	e		ft ²
T2 175.00-150.00	162.50		1.135	19.193	1.05		51	A B C	0.135 0.135 0.135	9.759 9.759 9.759
T3 150.00-125.00	137.50		1.082	12.182	1.08		50	A B C	0.13 0.13 0.13	9.779 9.779 9.779
T4 125.00-100.00	112.50		1.022	7.733	1.127		49	A B C	0.12 0.12 0.12	9.755 9.755 9.755
T5 100.00-91.67	95.83		0.976	5.711	1.174		49	A B C	0.115 0.115 0.115	3.245 3.245 3.245
T6 91.67-83.33	87.50		0.951	4.908	1.204		49	A B C	0.113 0.113 0.113	3.242 3.242 3.242
T7 83.33-75.00	79.17		0.924	4.218	1.239		49	A B C	0.111 0.111 0.111	3.237 3.237 3.237
T8 75.00-50.00	62.50		0.864	3.115	1.33		49	A B C	0.116 0.116 0.116	11.534 11.534 11.534
T9 50.00-37.50	43.75		0.78	2.215	1.477		49	A B C	0.111 0.111 0.111	5.734 5.734 5.734
T10 37.50-25.00	31.25		0.709	1.765	1.614		49	A B C	0.108 0.108 0.108	5.715 5.715 5.715
T11 25.00-0.00	12.50		0.7	1.255	1.904		57	A B C	0.121 0.121 0.121	11.607 11.607 11.607

222-H Section Verification Tables - Ice

Section Elevation	z_{wind}	z_{ice}	K_z	K_h	K_{zt}	t_z	q_z	F_{ac}	e	A_{R_r}
ft	ft	ft				in	psf	e		ft ²
T1 180.00-175.00	177.50	177.50	1.164	25.211	1.038	1.3787	7	A B C	0.308 0.308 0.308	7.276 7.276 7.276
T2 175.00-150.00	162.50	162.50	1.135	19.193	1.05	1.3721	6	A B C	0.236 0.236 0.236	31.283 31.283 31.283
T3 150.00-125.00	137.50	137.50	1.082	12.182	1.08	1.3626	6	A B C	0.223 0.223 0.223	32.302 32.302 32.302
T4 125.00-100.00	112.50	112.50	1.022	7.733	1.127	1.3557	6	A B C	0.208 0.208 0.208	33.355 33.355 33.355
T5 100.00-91.67	95.83	95.83	0.976	5.711	1.174	1.3533	6	A B C	0.199 0.199 0.199	11.376 11.376 11.376
T6 91.67-83.33	87.50	87.50	0.951	4.908	1.204	1.3528	6	A B C	0.196 0.196 0.196	11.512 11.512 11.512
T7 83.33-75.00	79.17	79.17	0.924	4.218	1.239	1.3529	6	A B	0.193 0.193	11.653 11.653

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	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
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Section Elevation	z_{wind}	z_{ice}	K_z	K_h	K_{zt}	t_z	q_z	$F_a c e$	e	$A_s R_r$
ft	ft	ft				in	psf			ft ²
T8 75.00-50.00	62.50	62.50	0.864	3.115	1.33	1.3544	6	C A B C	0.193 0.18 0.18 0.18	11.653 35.826 35.826 35.826
T9 50.00-37.50	43.75	43.75	0.78	2.215	1.477	1.3559	6	A B C	0.173 0.173 0.173	18.215 18.215 18.215
T10 37.50-25.00	31.25	31.25	0.709	1.765	1.614	1.3522	6	A B C	0.169 0.169 0.169	18.386 18.386 18.386
T11 25.00-0.00	12.50	12.50	0.7	1.255	1.904	1.3076	7	A B C	0.197 0.197 0.197	43.802 43.802 43.802

222-H Section Verification Tables - Service

Section Elevation	z_{wind}	z_{ice}	K_z	K_h	K_{zt}	t_z	q_z	$F_a c e$	e	$A_s R_r$
ft	ft	ft				in	psf			ft ²
T1 180.00-175.00	177.50		1.164	25.211	1.038		9	A B C	0.173 0.173 0.173	2.003 2.003 2.003
T2 175.00-150.00	162.50		1.135	19.193	1.05		9	A B C	0.135 0.135 0.135	9.759 9.759 9.759
T3 150.00-125.00	137.50		1.082	12.182	1.08		9	A B C	0.13 0.13 0.13	9.779 9.779 9.779
T4 125.00-100.00	112.50		1.022	7.733	1.127		9	A B C	0.12 0.12 0.12	9.755 9.755 9.755
T5 100.00-91.67	95.83		0.976	5.711	1.174		9	A B C	0.115 0.115 0.115	3.245 3.245 3.245
T6 91.67-83.33	87.50		0.951	4.908	1.204		9	A B C	0.113 0.113 0.113	3.242 3.242 3.242
T7 83.33-75.00	79.17		0.924	4.218	1.239		9	A B C	0.111 0.111 0.111	3.237 3.237 3.237
T8 75.00-50.00	62.50		0.864	3.115	1.33		9	A B C	0.116 0.116 0.116	11.534 11.534 11.534
T9 50.00-37.50	43.75		0.78	2.215	1.477		9	A B C	0.111 0.111 0.111	5.734 5.734 5.734
T10 37.50-25.00	31.25		0.709	1.765	1.614		9	A B C	0.108 0.108 0.108	5.715 5.715 5.715
T11 25.00-0.00	12.50		0.7	1.255	1.904		10	A B C	0.121 0.121 0.121	11.607 11.607 11.607

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	27 of 65
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Tower Pressures - No Ice

$$G_H = 0.850$$

Section Elevation	z	K _Z	q _z	A _G	F a c e	A _F	A _R	A _{leg}	Leg %	C _A A _A In Face	C _A A _A Out Face
ft	ft		psf	ft ²	e	ft ²	ft ²	ft ²		ft ²	ft ²
T1 180.00-175.00	177.50	1.164	52	56.085	A	5.526	4.171	4.171	43.01	4.621	0.000
					B	5.526	4.171	43.01	0.000	0.000	
					C	5.526	4.171	43.01	0.000	0.000	
T2 175.00-150.00	162.50	1.135	51	310.425	A	20.963	20.856	20.856	49.87	44.530	0.000
					B	20.963	20.856	49.87	0.000	0.000	
					C	20.963	20.856	49.87	0.777	0.000	
T3 150.00-125.00	137.50	1.082	50	360.425	A	25.950	20.856	20.856	44.56	63.151	0.000
					B	25.950	20.856	44.56	64.584	0.000	
					C	25.950	20.856	44.56	3.774	0.000	
T4 125.00-100.00	112.50	1.022	49	410.425	A	28.497	20.856	20.856	42.26	76.130	0.000
					B	28.497	20.856	42.26	67.275	0.000	
					C	28.497	20.856	42.26	5.550	0.000	
T5 100.00-91.67	95.83	0.976	49	147.919	A	10.075	6.952	6.952	40.83	27.744	0.000
					B	10.075	6.952	40.83	22.425	0.000	
					C	10.075	6.952	40.83	1.850	0.000	
T6 91.67-83.33	87.50	0.951	49	153.475	A	10.367	6.952	6.952	40.14	28.182	0.000
					B	10.367	6.952	40.14	22.425	0.000	
					C	10.367	6.952	40.14	1.850	0.000	
T7 83.33-75.00	79.17	0.924	49	159.031	A	10.660	6.952	6.952	39.47	30.951	0.000
					B	10.660	6.952	39.47	22.425	0.000	
					C	10.660	6.952	39.47	1.850	0.000	
T8 75.00-50.00	62.50	0.864	49	514.334	A	30.955	28.676	28.676	48.09	97.018	0.000
					B	30.955	28.676	48.09	67.275	0.000	
					C	30.955	28.676	48.09	5.550	0.000	
T9 50.00-37.50	43.75	0.78	49	275.917	A	16.271	14.338	14.338	46.84	50.269	0.000
					B	16.271	14.338	46.84	33.638	0.000	
					C	16.271	14.338	46.84	2.775	0.000	
T10 37.50-25.00	31.25	0.709	49	288.417	A	16.805	14.338	14.338	46.04	50.659	0.000
					B	16.805	14.338	46.04	33.638	0.000	
					C	16.805	14.338	46.04	2.775	0.000	
T11 25.00-0.00	12.50	0.7	57	614.334	A	45.951	28.676	28.676	38.43	68.896	0.000
					B	45.951	28.676	38.43	45.747	0.000	
					C	45.951	28.676	38.43	3.774	0.000	

Tower Pressure - With Ice

$$G_H = 0.850$$

Section Elevation	z	K _Z	q _z	t _z	A _G	F a c e	A _F	A _R	A _{leg}	Leg %	C _A A _A In Face	C _A A _A Out Face
ft	ft		psf	in	ft ²	e	ft ²	ft ²	ft ²		ft ²	ft ²
T1 180.00-175.00	177.50	1.164	7	1.3787	57.235	A	5.526	12.098	6.471	36.72	13.518	0.000
						B	5.526	12.098	36.72	0.000	0.000	
						C	5.526	12.098	36.72	0.000	0.000	
T2 175.00-150.00	162.50	1.135	6	1.3721	316.147	A	20.963	53.770	32.302	43.22	115.881	0.000
						B	20.963	53.770	43.22	0.000	0.000	
						C	20.963	53.770	43.22	2.698	0.000	
T3 150.00-125.00	137.50	1.082	6	1.3626	366.107	A	25.950	55.794	32.222	39.42	178.080	0.000
						B	25.950	55.794	39.42	173.464	0.000	
						C	25.950	55.794	39.42	13.039	0.000	

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Section Elevation ft	z ft	K _Z	q _z psf	t _z in	A _G ft ²	F a c e ft ²	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
T4 125.00-100.00	112.50	1.022	6	1.3557	416.078	A 28.497 B 28.497 C 28.497	28.497 57.921	57.921	32.165	37.22	224.148	0.000
T5 100.00-91.67	95.83	0.976	6	1.3533	149.800	A 10.075 B 10.075 C 10.075	10.075 19.805	19.805	10.715	35.86	83.226	0.000
T6 91.67-83.33	87.50	0.951	6	1.3528	155.355	A 10.367 B 10.367 C 10.367	10.367 20.063	20.063	10.714	35.21	84.729	0.000
T7 83.33-75.00	79.17	0.924	6	1.3529	160.911	A 10.660 B 10.660 C 10.660	10.660 20.329	20.329	10.714	34.57	94.131	0.000
T8 75.00-50.00	62.50	0.864	6	1.3544	519.982	A 30.955 B 30.955 C 30.955	30.955 62.711	62.711	39.975	42.68	293.932	0.000
T9 50.00-37.50	43.75	0.78	6	1.3559	278.744	A 16.271 B 16.271 C 16.271	16.271 31.941	31.941	19.994	41.47	154.525	0.000
T10 37.50-25.00	31.25	0.709	6	1.3522	291.237	A 16.805 B 16.805 C 16.805	16.805 32.274	32.274	19.979	40.71	155.728	0.000
T11 25.00-0.00	12.50	0.7	7	1.3076	619.787	A 45.951 B 45.951 C 45.951	45.951 76.309	76.309	39.584	32.38	207.279	0.000

Tower Pressure - Service

$G_H = 0.850$

Section Elevation ft	z ft	K _Z	q _z psf	A _G ft ²	F a c e ft ²	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
T1 180.00-175.00	177.50	1.164	9	56.085	A 5.526 B 5.526 C 5.526	5.526 4.171	4.171	4.171	43.01	4.621	0.000
T2 175.00-150.00	162.50	1.135	9	310.425	A 20.963 B 20.963 C 20.963	20.963 20.856	20.856	20.856	49.87	44.530	0.000
T3 150.00-125.00	137.50	1.082	9	360.425	A 25.950 B 25.950 C 25.950	25.950 20.856	20.856	20.856	44.56	63.151	0.000
T4 125.00-100.00	112.50	1.022	9	410.425	A 28.497 B 28.497 C 28.497	28.497 20.856	20.856	20.856	42.26	76.130	0.000
T5 100.00-91.67	95.83	0.976	9	147.919	A 10.075 B 10.075 C 10.075	10.075 6.952	6.952	6.952	40.83	27.744	0.000
T6 91.67-83.33	87.50	0.951	9	153.475	A 10.367 B 10.367 C 10.367	10.367 6.952	6.952	6.952	40.14	28.182	0.000
T7 83.33-75.00	79.17	0.924	9	159.031	A 10.660 B 10.660 C 10.660	10.660 6.952	6.952	6.952	39.47	30.951	0.000
T8 75.00-50.00	62.50	0.864	9	514.334	A 30.955	30.955	28.676	28.676	48.09	97.018	0.000

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	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section Elevation <i>ft</i>	<i>z</i> <i>ft</i>	<i>K_Z</i>	<i>q_z</i> <i>psf</i>	<i>A_G</i> <i>ft²</i>	<i>F_a</i> <i>c</i> <i>e</i>	<i>A_F</i> <i>ft²</i>	<i>A_R</i> <i>ft²</i>	<i>A_{leg}</i> <i>ft²</i>	<i>Leg</i> <i>%</i>	<i>C_{AA}</i> <i>In</i> <i>Face</i> <i>ft²</i>	<i>C_{AA}</i> <i>Out</i> <i>Face</i> <i>ft²</i>
T9 50.00-37.50	43.75	0.78	9	275.917	B	30.955	28.676	14.338	48.09	67.275	0.000
					C	30.955	28.676		48.09	5.550	0.000
					A	16.271	14.338		46.84	50.269	0.000
					B	16.271	14.338		46.84	33.638	0.000
T10 37.50-25.00	31.25	0.709	9	288.417	C	16.271	14.338	14.338	46.84	2.775	0.000
					A	16.805	14.338		46.04	50.659	0.000
					B	16.805	14.338		46.04	33.638	0.000
					C	16.805	14.338		46.04	2.775	0.000
T11 25.00-0.00	12.50	0.7	10	614.334	A	45.951	28.676	28.676	38.43	68.896	0.000
					B	45.951	28.676		38.43	45.747	0.000
					C	45.951	28.676		38.43	3.774	0.000
					C	45.951	28.676		38.43	3.774	0.000

Tower Forces - No Ice - Wind Normal To Face

Section Elevation <i>ft</i>	Add Weight <i>lb</i>	Self Weight <i>lb</i>	<i>F_a</i> <i>c</i> <i>e</i>	<i>e</i>	<i>C_F</i>	<i>q_z</i> <i>psf</i>	<i>D_F</i>	<i>D_R</i>	<i>A_E</i> <i>ft²</i>	<i>F</i> <i>lb</i>	<i>w</i> <i>plf</i>	<i>Ctrl.</i> <i>Face</i>
T1 180.00-175.00	17.55	628.79	A	0.173	2.689	52	1	1	7.529	1008.71	201.74	C
			B	0.173	2.689		1	1	7.529			
			C	0.173	2.689		1	1	7.529			
T2 175.00-150.00	146.06	2596.18	A	0.135	2.829	51	1	1	30.722	4931.54	197.26	C
			B	0.135	2.829		1	1	30.722			
			C	0.135	2.829		1	1	30.722			
T3 150.00-125.00	529.71	3454.06	A	0.13	2.847	50	1	1	35.729	7653.26	306.13	C
			B	0.13	2.847		1	1	35.729			
			C	0.13	2.847		1	1	35.729			
T4 125.00-100.00	597.20	3678.83	A	0.12	2.884	49	1	1	38.252	8339.86	333.59	C
			B	0.12	2.884		1	1	38.252			
			C	0.12	2.884		1	1	38.252			
T5 100.00-91.67	207.88	1457.98	A	0.115	2.904	49	1	1	13.321	2904.23	348.51	C
			B	0.115	2.904		1	1	13.321			
			C	0.115	2.904		1	1	13.321			
T6 91.67-83.33	209.60	1485.68	A	0.113	2.913	49	1	1	13.608	2952.15	354.26	C
			B	0.113	2.913		1	1	13.608			
			C	0.113	2.913		1	1	13.608			
T7 83.33-75.00	216.24	1805.56	A	0.111	2.921	49	1	1	13.897	3061.37	367.36	C
			B	0.111	2.921		1	1	13.897			
			C	0.111	2.921		1	1	13.897			
T8 75.00-50.00	657.80	5810.40	A	0.116	2.901	49	1	1	42.488	9377.69	375.11	C
			B	0.116	2.901		1	1	42.488			
			C	0.116	2.901		1	1	42.488			
T9 50.00-37.50	333.76	3327.03	A	0.111	2.92	49	1	1	22.005	4858.06	388.65	C
			B	0.111	2.92		1	1	22.005			
			C	0.111	2.92		1	1	22.005			
T10 37.50-25.00	334.90	3385.52	A	0.108	2.932	49	1	1	22.520	4903.81	392.30	C
			B	0.108	2.932		1	1	22.520			
			C	0.108	2.932		1	1	22.520			
T11 25.00-0.00	455.46	8143.22	A	0.121	2.879	57	1	1	57.558	11443.04	457.72	C
			B	0.121	2.879		1	1	57.558			
			C	0.121	2.879		1	1	57.558			
Sum Weight:	3706.17	35773.24						OTM	4844.90 kip-ft	61433.72		

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	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Tower Forces - No Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-175.00	17.55	628.79	A	0.173	2.689	52	0.825	1	6.562	894.76	178.95	C
			B	0.173	2.689		0.825	1	6.562			
			C	0.173	2.689		0.825	1	6.562			
T2 175.00-150.00	146.06	2596.18	A	0.135	2.829	51	0.825	1	27.054	4482.99	179.32	C
			B	0.135	2.829		0.825	1	27.054			
			C	0.135	2.829		0.825	1	27.054			
T3 150.00-125.00	529.71	3454.06	A	0.13	2.847	50	0.825	1	31.188	7105.45	284.22	C
			B	0.13	2.847		0.825	1	31.188			
			C	0.13	2.847		0.825	1	31.188			
T4 125.00-100.00	597.20	3678.83	A	0.12	2.884	49	0.825	1	33.265	7739.19	309.57	C
			B	0.12	2.884		0.825	1	33.265			
			C	0.12	2.884		0.825	1	33.265			
T5 100.00-91.67	207.88	1457.98	A	0.115	2.904	49	0.825	1	11.558	2691.48	322.98	C
			B	0.115	2.904		0.825	1	11.558			
			C	0.115	2.904		0.825	1	11.558			
T6 91.67-83.33	209.60	1485.68	A	0.113	2.913	49	0.825	1	11.794	2732.77	327.93	C
			B	0.113	2.913		0.825	1	11.794			
			C	0.113	2.913		0.825	1	11.794			
T7 83.33-75.00	216.24	1805.56	A	0.111	2.921	49	0.825	1	12.032	2835.11	340.21	C
			B	0.111	2.921		0.825	1	12.032			
			C	0.111	2.921		0.825	1	12.032			
T8 75.00-50.00	657.80	5810.40	A	0.116	2.901	49	0.825	1	37.071	8723.21	348.93	C
			B	0.116	2.901		0.825	1	37.071			
			C	0.116	2.901		0.825	1	37.071			
T9 50.00-37.50	333.76	3327.03	A	0.111	2.92	49	0.825	1	19.157	4510.63	360.85	C
			B	0.111	2.92		0.825	1	19.157			
			C	0.111	2.92		0.825	1	19.157			
T10 37.50-25.00	334.90	3385.52	A	0.108	2.932	49	0.825	1	19.579	4546.28	363.70	C
			B	0.108	2.932		0.825	1	19.579			
			C	0.108	2.932		0.825	1	19.579			
T11 25.00-0.00	455.46	8143.22	A	0.121	2.879	57	0.825	1	49.517	10324.07	412.96	C
			B	0.121	2.879		0.825	1	49.517			
			C	0.121	2.879		0.825	1	49.517			
Sum Weight:	3706.17	35773.24						OTM	4470.12 kip-ft	56585.94		

Tower Forces - No Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-175.00	17.55	628.79	A	0.173	2.689	52	0.8	1	6.424	878.48	175.70	C
			B	0.173	2.689		0.8	1	6.424			
			C	0.173	2.689		0.8	1	6.424			
T2 175.00-150.00	146.06	2596.18	A	0.135	2.829	51	0.8	1	26.530	4418.91	176.76	C
			B	0.135	2.829		0.8	1	26.530			
			C	0.135	2.829		0.8	1	26.530			
T3 150.00-125.00	529.71	3454.06	A	0.13	2.847	50	0.8	1	30.539	7027.19	281.09	C
			B	0.13	2.847		0.8	1	30.539			

Job	180' Stainless, Inc. Self Supporting Lattice	Page	31 of 65
Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T4 125.00-100.00	597.20	3678.83	C	0.13	2.847	49	0.8	1	30.539	7653.38	306.14	C
			A	0.12	2.884		0.8	1	32.552			
			B	0.12	2.884		0.8	1	32.552			
T5 100.00-91.67	207.88	1457.98	C	0.12	2.884	49	0.8	1	32.552	2661.08	319.33	C
			A	0.115	2.904		0.8	1	11.306			
			B	0.115	2.904		0.8	1	11.306			
T6 91.67-83.33	209.60	1485.68	C	0.115	2.904	49	0.8	1	11.306	2701.43	324.17	C
			A	0.113	2.913		0.8	1	11.535			
			B	0.113	2.913		0.8	1	11.535			
T7 83.33-75.00	216.24	1805.56	C	0.111	2.921	49	0.8	1	11.765	2802.79	336.33	C
			A	0.111	2.921		0.8	1	11.765			
			B	0.111	2.921		0.8	1	11.765			
T8 75.00-50.00	657.80	5810.40	C	0.111	2.92	49	0.8	1	18.751	4460.99	356.88	C
			A	0.116	2.901		0.8	1	36.297			
			B	0.116	2.901		0.8	1	36.297			
T9 50.00-37.50	333.76	3327.03	C	0.116	2.901	49	0.8	1	36.297	4495.21	359.62	C
			A	0.111	2.92		0.8	1	18.751			
			B	0.111	2.92		0.8	1	18.751			
T10 37.50-25.00	334.90	3385.52	C	0.111	2.92	49	0.8	1	18.751	4495.21	359.62	C
			A	0.108	2.932		0.8	1	19.159			
			B	0.108	2.932		0.8	1	19.159			
T11 25.00-0.00	455.46	8143.22	C	0.108	2.932	57	0.8	1	19.159	10164.22	406.57	C
			A	0.121	2.879		0.8	1	48.368			
			B	0.121	2.879		0.8	1	48.368			
Sum Weight:	3706.17	35773.24	C	0.121	2.879		0.8	1	48.368	55893.40		

Tower Forces - No Ice - Wind 90 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T1 180.00-175.00	17.55	628.79	A	0.173	2.689	52	0.85	1	6.701	911.04	182.21	C
			B	0.173	2.689		0.85	1	6.701			
			C	0.173	2.689		0.85	1	6.701			
T2 175.00-150.00	146.06	2596.18	A	0.135	2.829	51	0.85	1	27.578	4547.07	181.88	C
			B	0.135	2.829		0.85	1	27.578			
			C	0.135	2.829		0.85	1	27.578			
T3 150.00-125.00	529.71	3454.06	A	0.13	2.847	50	0.85	1	31.836	7183.71	287.35	C
			B	0.13	2.847		0.85	1	31.836			
			C	0.13	2.847		0.85	1	31.836			
T4 125.00-100.00	597.20	3678.83	A	0.12	2.884	49	0.85	1	33.977	7825.00	313.00	C
			B	0.12	2.884		0.85	1	33.977			
			C	0.12	2.884		0.85	1	33.977			
T5 100.00-91.67	207.88	1457.98	A	0.115	2.904	49	0.85	1	11.809	2721.87	326.62	C
			B	0.115	2.904		0.85	1	11.809			
			C	0.115	2.904		0.85	1	11.809			
T6 91.67-83.33	209.60	1485.68	A	0.113	2.913	49	0.85	1	12.053	2764.11	331.69	C
			B	0.113	2.913		0.85	1	12.053			
			C	0.113	2.913		0.85	1	12.053			
T7 83.33-75.00	216.24	1805.56	A	0.111	2.921	49	0.85	1	12.298	2867.43	344.09	C
			B	0.111	2.921		0.85	1	12.298			

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	32 of 65
	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T8 75.00-50.00	657.80	5810.40	C	0.111	2.921		0.85	1	12.298			
			A	0.116	2.901	49	0.85	1	37.845	8816.71	352.67	C
			B	0.116	2.901		0.85	1	37.845			
			C	0.116	2.901		0.85	1	37.845			
T9 50.00-37.50	333.76	3327.03	A	0.111	2.92	49	0.85	1	19.564	4560.26	364.82	C
			B	0.111	2.92		0.85	1	19.564			
			C	0.111	2.92		0.85	1	19.564			
T10 37.50-25.00	334.90	3385.52	A	0.108	2.932	49	0.85	1	19.999	4597.36	367.79	C
			B	0.108	2.932		0.85	1	19.999			
			C	0.108	2.932		0.85	1	19.999			
T11 25.00-0.00	455.46	8143.22	A	0.121	2.879	57	0.85	1	50.666	10483.93	419.36	C
			B	0.121	2.879		0.85	1	50.666			
			C	0.121	2.879		0.85	1	50.666			
Sum Weight:	3706.17	35773.24						OTM	4523.66 kip-ft	57278.48		

Tower Forces - With Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-175.00	158.09	1730.24	A	0.308	2.275	7	1	1	12.802	208.13	41.63	C
			B	0.308	2.275		1	1	12.802			
			C	0.308	2.275		1	1	12.802			
T2 175.00-150.00	1384.56	6929.86	A	0.236	2.479	6	1	1	52.246	1106.39	44.26	C
			B	0.236	2.479		1	1	52.246			
			C	0.236	2.479		1	1	52.246			
T3 150.00-125.00	4501.21	8447.54	A	0.223	2.52	6	1	1	58.252	1975.60	79.02	C
			B	0.223	2.52		1	1	58.252			
			C	0.223	2.52		1	1	58.252			
T4 125.00-100.00	5185.98	9037.62	A	0.208	2.57	6	1	1	61.852	2201.51	88.06	C
			B	0.208	2.57		1	1	61.852			
			C	0.208	2.57		1	1	61.852			
T5 100.00-91.67	1824.77	3393.79	A	0.199	2.598	6	1	1	21.451	771.55	92.59	C
			B	0.199	2.598		1	1	21.451			
			C	0.199	2.598		1	1	21.451			
T6 91.67-83.33	1842.02	3468.56	A	0.196	2.61	6	1	1	21.878	782.87	93.94	C
			B	0.196	2.61		1	1	21.878			
			C	0.196	2.61		1	1	21.878			
T7 83.33-75.00	1943.94	3836.72	A	0.193	2.621	6	1	1	22.313	820.20	98.42	C
			B	0.193	2.621		1	1	22.313			
			C	0.193	2.621		1	1	22.313			
T8 75.00-50.00	5962.38	11466.12	A	0.18	2.664	6	1	1	66.781	2518.19	100.73	C
			B	0.18	2.664		1	1	66.781			
			C	0.18	2.664		1	1	66.781			
T9 50.00-37.50	3066.07	6308.01	A	0.173	2.689	6	1	1	34.485	1307.48	104.60	C
			B	0.173	2.689		1	1	34.485			
			C	0.173	2.689		1	1	34.485			
T10 37.50-25.00	3073.25	6434.61	A	0.169	2.705	6	1	1	35.191	1314.05	105.12	C
			B	0.169	2.705		1	1	35.191			
			C	0.169	2.705		1	1	35.191			
T11 25.00-0.00	4024.61	15416.29	A	0.197	2.605	7	1	1	89.753	2706.48	108.26	C
			B	0.197	2.605		1	1	89.753			

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	33 of 65
	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
Sum Weight:	32966.87	76469.36	C	0.197	2.605		1	1 OTM	89.753 1232.90 kip-ft	15712.44		

Tower Forces - With Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-175.00	158.09	1730.24	A	0.308	2.275	7	0.825	1	11.835	195.84	39.17	C
			B	0.308	2.275		0.825	1	11.835			
			C	0.308	2.275		0.825	1	11.835			
T2 175.00-150.00	1384.56	6929.86	A	0.236	2.479	6	0.825	1	48.577	1056.25	42.25	C
			B	0.236	2.479		0.825	1	48.577			
			C	0.236	2.479		0.825	1	48.577			
T3 150.00-125.00	4501.21	8447.54	A	0.223	2.52	6	0.825	1	53.711	1913.74	76.55	C
			B	0.223	2.52		0.825	1	53.711			
			C	0.223	2.52		0.825	1	53.711			
T4 125.00-100.00	5185.98	9037.62	A	0.208	2.57	6	0.825	1	56.865	2133.23	85.33	C
			B	0.208	2.57		0.825	1	56.865			
			C	0.208	2.57		0.825	1	56.865			
T5 100.00-91.67	1824.77	3393.79	A	0.199	2.598	6	0.825	1	19.688	747.27	89.67	C
			B	0.199	2.598		0.825	1	19.688			
			C	0.199	2.598		0.825	1	19.688			
T6 91.67-83.33	1842.02	3468.56	A	0.196	2.61	6	0.825	1	20.064	757.80	90.94	C
			B	0.196	2.61		0.825	1	20.064			
			C	0.196	2.61		0.825	1	20.064			
T7 83.33-75.00	1943.94	3836.72	A	0.193	2.621	6	0.825	1	20.447	794.31	95.32	C
			B	0.193	2.621		0.825	1	20.447			
			C	0.193	2.621		0.825	1	20.447			
T8 75.00-50.00	5962.38	11466.12	A	0.18	2.664	6	0.825	1	61.363	2441.53	97.66	C
			B	0.18	2.664		0.825	1	61.363			
			C	0.18	2.664		0.825	1	61.363			
T9 50.00-37.50	3066.07	6308.01	A	0.173	2.689	6	0.825	1	31.638	1266.68	101.33	C
			B	0.173	2.689		0.825	1	31.638			
			C	0.173	2.689		0.825	1	31.638			
T10 37.50-25.00	3073.25	6434.61	A	0.169	2.705	6	0.825	1	32.250	1271.98	101.76	C
			B	0.169	2.705		0.825	1	32.250			
			C	0.169	2.705		0.825	1	32.250			
T11 25.00-0.00	4024.61	15416.29	A	0.197	2.605	7	0.825	1	81.711	2577.34	103.09	C
			B	0.197	2.605		0.825	1	81.711			
			C	0.197	2.605		0.825	1	81.711			
Sum Weight:	32966.87	76469.36						OTM	1190.31 kip-ft	15155.96		

Tower Forces - With Ice - Wind 60 To Face

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	34 of 65
	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T1 180.00-175.00	158.09	1730.24	A	0.308	2.275	7	0.8	1	11.697	194.08	38.82	C
			B	0.308	2.275		0.8	1	11.697			
			C	0.308	2.275		0.8	1	11.697			
T2 175.00-150.00	1384.56	6929.86	A	0.236	2.479	6	0.8	1	48.053	1049.09	41.96	C
			B	0.236	2.479		0.8	1	48.053			
			C	0.236	2.479		0.8	1	48.053			
T3 150.00-125.00	4501.21	8447.54	A	0.223	2.52	6	0.8	1	53.062	1904.91	76.20	C
			B	0.223	2.52		0.8	1	53.062			
			C	0.223	2.52		0.8	1	53.062			
T4 125.00-100.00	5185.98	9037.62	A	0.208	2.57	6	0.8	1	56.153	2123.47	84.94	C
			B	0.208	2.57		0.8	1	56.153			
			C	0.208	2.57		0.8	1	56.153			
T5 100.00-91.67	1824.77	3393.79	A	0.199	2.598	6	0.8	1	19.436	743.80	89.26	C
			B	0.199	2.598		0.8	1	19.436			
			C	0.199	2.598		0.8	1	19.436			
T6 91.67-83.33	1842.02	3468.56	A	0.196	2.61	6	0.8	1	19.805	754.22	90.51	C
			B	0.196	2.61		0.8	1	19.805			
			C	0.196	2.61		0.8	1	19.805			
T7 83.33-75.00	1943.94	3836.72	A	0.193	2.621	6	0.8	1	20.181	790.61	94.87	C
			B	0.193	2.621		0.8	1	20.181			
			C	0.193	2.621		0.8	1	20.181			
T8 75.00-50.00	5962.38	11466.12	A	0.18	2.664	6	0.8	1	60.590	2430.58	97.22	C
			B	0.18	2.664		0.8	1	60.590			
			C	0.18	2.664		0.8	1	60.590			
T9 50.00-37.50	3066.07	6308.01	A	0.173	2.689	6	0.8	1	31.231	1260.85	100.87	C
			B	0.173	2.689		0.8	1	31.231			
			C	0.173	2.689		0.8	1	31.231			
T10 37.50-25.00	3073.25	6434.61	A	0.169	2.705	6	0.8	1	31.830	1265.97	101.28	C
			B	0.169	2.705		0.8	1	31.830			
			C	0.169	2.705		0.8	1	31.830			
T11 25.00-0.00	4024.61	15416.29	A	0.197	2.605	7	0.8	1	80.563	2558.89	102.36	C
			B	0.197	2.605		0.8	1	80.563			
			C	0.197	2.605		0.8	1	80.563			
Sum Weight:	32966.87	76469.36						OTM	1184.23 kip-ft	15076.46		

Tower Forces - With Ice - Wind 90 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T1 180.00-175.00	158.09	1730.24	A	0.308	2.275	7	0.85	1	11.973	197.59	39.52	C
			B	0.308	2.275		0.85	1	11.973			
			C	0.308	2.275		0.85	1	11.973			
T2 175.00-150.00	1384.56	6929.86	A	0.236	2.479	6	0.85	1	49.101	1063.41	42.54	C
			B	0.236	2.479		0.85	1	49.101			
			C	0.236	2.479		0.85	1	49.101			
T3 150.00-125.00	4501.21	8447.54	A	0.223	2.52	6	0.85	1	54.359	1922.58	76.90	C
			B	0.223	2.52		0.85	1	54.359			
			C	0.223	2.52		0.85	1	54.359			
T4 125.00-100.00	5185.98	9037.62	A	0.208	2.57	6	0.85	1	57.578	2142.98	85.72	C
			B	0.208	2.57		0.85	1	57.578			
			C	0.208	2.57		0.85	1	57.578			

Job	180' Stainless, Inc. Self Supporting Lattice	Page	35 of 65
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Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T5 100.00-91.67	1824.77	3393.79	A	0.199	2.598	6	0.85	1	19.940	750.74	90.09	C
			B	0.199	2.598		0.85	1	19.940			
			C	0.199	2.598		0.85	1	19.940			
T6 91.67-83.33	1842.02	3468.56	A	0.196	2.61	6	0.85	1	20.323	761.38	91.37	C
			B	0.196	2.61		0.85	1	20.323			
			C	0.196	2.61		0.85	1	20.323			
T7 83.33-75.00	1943.94	3836.72	A	0.193	2.621	6	0.85	1	20.714	798.01	95.76	C
			B	0.193	2.621		0.85	1	20.714			
			C	0.193	2.621		0.85	1	20.714			
T8 75.00-50.00	5962.38	11466.12	A	0.18	2.664	6	0.85	1	62.137	2452.48	98.10	C
			B	0.18	2.664		0.85	1	62.137			
			C	0.18	2.664		0.85	1	62.137			
T9 50.00-37.50	3066.07	6308.01	A	0.173	2.689	6	0.85	1	32.045	1272.51	101.80	C
			B	0.173	2.689		0.85	1	32.045			
			C	0.173	2.689		0.85	1	32.045			
T10 37.50-25.00	3073.25	6434.61	A	0.169	2.705	6	0.85	1	32.670	1277.99	102.24	C
			B	0.169	2.705		0.85	1	32.670			
			C	0.169	2.705		0.85	1	32.670			
T11 25.00-0.00	4024.61	15416.29	A	0.197	2.605	7	0.85	1	82.860	2595.78	103.83	C
			B	0.197	2.605		0.85	1	82.860			
			C	0.197	2.605		0.85	1	82.860			
Sum Weight:	32966.87	76469.36						OTM	1196.40 kip-ft	15235.46		

Tower Forces - Service - Wind Normal To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T1 180.00-175.00	17.55	628.79	A	0.173	2.689	9	1	1	7.529	185.27	37.05	C
			B	0.173	2.689		1	1	7.529			
			C	0.173	2.689		1	1	7.529			
T2 175.00-150.00	146.06	2596.18	A	0.135	2.829	9	1	1	30.722	905.79	36.23	C
			B	0.135	2.829		1	1	30.722			
			C	0.135	2.829		1	1	30.722			
T3 150.00-125.00	529.71	3454.06	A	0.13	2.847	9	1	1	35.729	1405.70	56.23	C
			B	0.13	2.847		1	1	35.729			
			C	0.13	2.847		1	1	35.729			
T4 125.00-100.00	597.20	3678.83	A	0.12	2.884	9	1	1	38.252	1531.81	61.27	C
			B	0.12	2.884		1	1	38.252			
			C	0.12	2.884		1	1	38.252			
T5 100.00-91.67	207.88	1457.98	A	0.115	2.904	9	1	1	13.321	533.43	64.01	C
			B	0.115	2.904		1	1	13.321			
			C	0.115	2.904		1	1	13.321			
T6 91.67-83.33	209.60	1485.68	A	0.113	2.913	9	1	1	13.608	542.23	65.07	C
			B	0.113	2.913		1	1	13.608			
			C	0.113	2.913		1	1	13.608			
T7 83.33-75.00	216.24	1805.56	A	0.111	2.921	9	1	1	13.897	562.29	67.48	C
			B	0.111	2.921		1	1	13.897			
			C	0.111	2.921		1	1	13.897			
T8 75.00-50.00	657.80	5810.40	A	0.116	2.901	9	1	1	42.488	1722.43	68.90	C
			B	0.116	2.901		1	1	42.488			
			C	0.116	2.901		1	1	42.488			

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Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T9 50.00-37.50	333.76	3327.03	A	0.111	2.92	9	1	1	22.005	892.30	71.38	C
			B	0.111	2.92		1	1	22.005			
			C	0.111	2.92		1	1	22.005			
T10 37.50-25.00	334.90	3385.52	A	0.108	2.932	9	1	1	22.520	900.70	72.06	C
			B	0.108	2.932		1	1	22.520			
			C	0.108	2.932		1	1	22.520			
T11 25.00-0.00	455.46	8143.22	A	0.121	2.879	10	1	1	57.558	2101.78	84.07	C
			B	0.121	2.879		1	1	57.558			
			C	0.121	2.879		1	1	57.558			
Sum Weight:	3706.17	35773.24						OTM	889.88 kip-ft	11283.74		

Tower Forces - Service - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-175.00	17.55	628.79	A	0.173	2.689	9	0.825	1	6.562	164.34	32.87	C
			B	0.173	2.689		0.825	1	6.562			
			C	0.173	2.689		0.825	1	6.562			
T2 175.00-150.00	146.06	2596.18	A	0.135	2.829	9	0.825	1	27.054	823.41	32.94	C
			B	0.135	2.829		0.825	1	27.054			
			C	0.135	2.829		0.825	1	27.054			
T3 150.00-125.00	529.71	3454.06	A	0.13	2.847	9	0.825	1	31.188	1305.08	52.20	C
			B	0.13	2.847		0.825	1	31.188			
			C	0.13	2.847		0.825	1	31.188			
T4 125.00-100.00	597.20	3678.83	A	0.12	2.884	9	0.825	1	33.265	1421.48	56.86	C
			B	0.12	2.884		0.825	1	33.265			
			C	0.12	2.884		0.825	1	33.265			
T5 100.00-91.67	207.88	1457.98	A	0.115	2.904	9	0.825	1	11.558	494.35	59.32	C
			B	0.115	2.904		0.825	1	11.558			
			C	0.115	2.904		0.825	1	11.558			
T6 91.67-83.33	209.60	1485.68	A	0.113	2.913	9	0.825	1	11.794	501.94	60.23	C
			B	0.113	2.913		0.825	1	11.794			
			C	0.113	2.913		0.825	1	11.794			
T7 83.33-75.00	216.24	1805.56	A	0.111	2.921	9	0.825	1	12.032	520.73	62.49	C
			B	0.111	2.921		0.825	1	12.032			
			C	0.111	2.921		0.825	1	12.032			
T8 75.00-50.00	657.80	5810.40	A	0.116	2.901	9	0.825	1	37.071	1602.22	64.09	C
			B	0.116	2.901		0.825	1	37.071			
			C	0.116	2.901		0.825	1	37.071			
T9 50.00-37.50	333.76	3327.03	A	0.111	2.92	9	0.825	1	19.157	828.48	66.28	C
			B	0.111	2.92		0.825	1	19.157			
			C	0.111	2.92		0.825	1	19.157			
T10 37.50-25.00	334.90	3385.52	A	0.108	2.932	9	0.825	1	19.579	835.03	66.80	C
			B	0.108	2.932		0.825	1	19.579			
			C	0.108	2.932		0.825	1	19.579			
T11 25.00-0.00	455.46	8143.22	A	0.121	2.879	10	0.825	1	49.517	1896.26	75.85	C
			B	0.121	2.879		0.825	1	49.517			
			C	0.121	2.879		0.825	1	49.517			
Sum Weight:	3706.17	35773.24						OTM	821.04 kip-ft	10393.34		

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	37 of 65
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	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Tower Forces - Service - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-175.00	17.55	628.79	A	0.173	2.689	9	0.8	1	6.424	161.35	32.27	C
			B	0.173	2.689		0.8	1	6.424			
			C	0.173	2.689		0.8	1	6.424			
T2 175.00-150.00	146.06	2596.18	A	0.135	2.829	9	0.8	1	26.530	811.64	32.47	C
			B	0.135	2.829		0.8	1	26.530			
			C	0.135	2.829		0.8	1	26.530			
T3 150.00-125.00	529.71	3454.06	A	0.13	2.847	9	0.8	1	30.539	1290.71	51.63	C
			B	0.13	2.847		0.8	1	30.539			
			C	0.13	2.847		0.8	1	30.539			
T4 125.00-100.00	597.20	3678.83	A	0.12	2.884	9	0.8	1	32.552	1405.72	56.23	C
			B	0.12	2.884		0.8	1	32.552			
			C	0.12	2.884		0.8	1	32.552			
T5 100.00-91.67	207.88	1457.98	A	0.115	2.904	9	0.8	1	11.306	488.77	58.65	C
			B	0.115	2.904		0.8	1	11.306			
			C	0.115	2.904		0.8	1	11.306			
T6 91.67-83.33	209.60	1485.68	A	0.113	2.913	9	0.8	1	11.535	496.18	59.54	C
			B	0.113	2.913		0.8	1	11.535			
			C	0.113	2.913		0.8	1	11.535			
T7 83.33-75.00	216.24	1805.56	A	0.111	2.921	9	0.8	1	11.765	514.80	61.78	C
			B	0.111	2.921		0.8	1	11.765			
			C	0.111	2.921		0.8	1	11.765			
T8 75.00-50.00	657.80	5810.40	A	0.116	2.901	9	0.8	1	36.297	1585.05	63.40	C
			B	0.116	2.901		0.8	1	36.297			
			C	0.116	2.901		0.8	1	36.297			
T9 50.00-37.50	333.76	3327.03	A	0.111	2.92	9	0.8	1	18.751	819.37	65.55	C
			B	0.111	2.92		0.8	1	18.751			
			C	0.111	2.92		0.8	1	18.751			
T10 37.50-25.00	334.90	3385.52	A	0.108	2.932	9	0.8	1	19.159	825.65	66.05	C
			B	0.108	2.932		0.8	1	19.159			
			C	0.108	2.932		0.8	1	19.159			
T11 25.00-0.00	455.46	8143.22	A	0.121	2.879	10	0.8	1	48.368	1866.90	74.68	C
			B	0.121	2.879		0.8	1	48.368			
			C	0.121	2.879		0.8	1	48.368			
Sum Weight:	3706.17	35773.24						OTM	811.21 kip-ft	10266.13		

Tower Forces - Service - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	lb	lb				psf			ft ²	lb	plf	
T1 180.00-175.00	17.55	628.79	A	0.173	2.689	9	0.85	1	6.701	167.33	33.47	C
			B	0.173	2.689		0.85	1	6.701			
			C	0.173	2.689		0.85	1	6.701			
T2 175.00-150.00	146.06	2596.18	A	0.135	2.829	9	0.85	1	27.578	835.18	33.41	C
			B	0.135	2.829		0.85	1	27.578			
			C	0.135	2.829		0.85	1	27.578			

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	38 of 65
	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F lb	w plf	Ctrl. Face
T3 150.00-125.00	529.71	3454.06	A	0.13	2.847	9	0.85	1	31.836	1319.46	52.78	C
			B	0.13	2.847		0.85	1	31.836			
			C	0.13	2.847		0.85	1	31.836			
T4 125.00-100.00	597.20	3678.83	A	0.12	2.884	9	0.85	1	33.977	1437.24	57.49	C
			B	0.12	2.884		0.85	1	33.977			
			C	0.12	2.884		0.85	1	33.977			
T5 100.00-91.67	207.88	1457.98	A	0.115	2.904	9	0.85	1	11.809	499.94	59.99	C
			B	0.115	2.904		0.85	1	11.809			
			C	0.115	2.904		0.85	1	11.809			
T6 91.67-83.33	209.60	1485.68	A	0.113	2.913	9	0.85	1	12.053	507.69	60.92	C
			B	0.113	2.913		0.85	1	12.053			
			C	0.113	2.913		0.85	1	12.053			
T7 83.33-75.00	216.24	1805.56	A	0.111	2.921	9	0.85	1	12.298	526.67	63.20	C
			B	0.111	2.921		0.85	1	12.298			
			C	0.111	2.921		0.85	1	12.298			
T8 75.00-50.00	657.80	5810.40	A	0.116	2.901	9	0.85	1	37.845	1619.40	64.78	C
			B	0.116	2.901		0.85	1	37.845			
			C	0.116	2.901		0.85	1	37.845			
T9 50.00-37.50	333.76	3327.03	A	0.111	2.92	9	0.85	1	19.564	837.60	67.01	C
			B	0.111	2.92		0.85	1	19.564			
			C	0.111	2.92		0.85	1	19.564			
T10 37.50-25.00	334.90	3385.52	A	0.108	2.932	9	0.85	1	19.999	844.41	67.55	C
			B	0.108	2.932		0.85	1	19.999			
			C	0.108	2.932		0.85	1	19.999			
T11 25.00-0.00	455.46	8143.22	A	0.121	2.879	10	0.85	1	50.666	1925.62	77.02	C
			B	0.121	2.879		0.85	1	50.666			
			C	0.121	2.879		0.85	1	50.666			
Sum Weight:	3706.17	35773.24						OTM	830.88 kip-ft	10520.54		

Force Totals

Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Overturning Moments, M _x kip-ft	Sum of Overturning Moments, M _z kip-ft	Sum of Torques kip-ft
Leg Weight	10768.21					
Bracing Weight	25005.03					
Total Member Self-Weight	35773.24				1.84	
Total Weight	44718.64			18.19	1.84	
Wind 0 deg - No Ice		-241.07	-80589.15	-7692.92	46.15	-22.63
Wind 30 deg - No Ice		37796.99	-66073.17	-6359.48	-3615.81	41.26
Wind 45 deg - No Ice		53088.10	-53386.77	-5138.06	-5099.36	70.06
Wind 60 deg - No Ice		64507.86	-37315.64	-3584.84	-6215.68	94.09
Wind 90 deg - No Ice		76011.52	241.07	62.49	-7310.19	121.72
Wind 120 deg - No Ice		69546.99	40503.35	3912.11	-6630.91	116.73
Wind 135 deg - No Ice		55387.83	55686.50	5388.52	-5313.45	102.07
Wind 150 deg - No Ice		38214.53	66314.24	6440.16	-3692.54	80.46
Wind 180 deg - No Ice		241.07	75048.83	7300.99	-42.46	22.63
Wind 210 deg - No Ice		-37796.99	66073.17	6395.86	3619.49	-41.26
Wind 225 deg - No Ice		-53088.10	53386.77	5174.44	5103.04	-70.06
Wind 240 deg - No Ice		-69305.92	40085.80	3835.38	6590.29	-94.09
Wind 270 deg - No Ice		-76011.52	-241.07	-26.11	7313.87	-121.72
Wind 300 deg - No Ice		-64748.93	-37733.19	-3661.58	6263.66	-116.73

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Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Overturning Moments, M _x kip-ft	Sum of Overturning Moments, M _z kip-ft	Sum of Torques kip-ft
Wind 315 deg - No Ice		-53429.03	-53727.70	-5200.71	5165.70	-102.07
Wind 330 deg - No Ice		-38214.53	-66314.24	-6403.78	3696.22	-80.46
Member Ice	40696.12					
Total Weight Ice	124253.80			127.74	44.96	
Wind 0 deg - Ice		-28.67	-19685.71	-1689.48	50.30	-18.75
Wind 30 deg - Ice		9553.09	-16620.91	-1411.73	-835.85	1.95
Wind 45 deg - Ice		13468.74	-13506.14	-1123.33	-1199.16	12.46
Wind 60 deg - Ice		16437.42	-9500.04	-751.90	-1475.46	22.12
Wind 90 deg - Ice		19155.85	28.67	133.08	-1725.92	36.36
Wind 120 deg - Ice		17016.86	9867.69	1040.98	-1522.96	40.87
Wind 135 deg - Ice		13734.14	13771.54	1403.58	-1223.93	38.97
Wind 150 deg - Ice		9602.76	16649.59	1672.55	-845.11	34.42
Wind 180 deg - Ice		28.67	19049.74	1896.28	39.62	18.75
Wind 210 deg - Ice		-9553.09	16620.91	1667.21	925.77	-1.95
Wind 225 deg - Ice		-13468.74	13506.14	1378.81	1289.08	-12.46
Wind 240 deg - Ice		-16988.19	9818.03	1031.72	1607.53	-22.12
Wind 270 deg - Ice		-19155.85	-28.67	122.39	1815.84	-36.36
Wind 300 deg - Ice		-16466.10	-9549.70	-761.16	1570.72	-40.87
Wind 315 deg - Ice		-13509.29	-13546.69	-1130.89	1296.64	-38.97
Wind 330 deg - Ice		-9602.76	-16649.59	-1417.07	935.03	-34.42
Total Weight	44718.64			18.19	1.84	
Wind 0 deg - Service		-44.28	-14802.09	-1410.72	11.23	-4.16
Wind 30 deg - Service		6942.30	-12135.89	-1165.80	-661.37	7.58
Wind 45 deg - Service		9750.88	-9805.73	-941.46	-933.86	12.87
Wind 60 deg - Service		11848.38	-6853.89	-656.17	-1138.90	17.28
Wind 90 deg - Service		13961.30	44.28	13.75	-1339.93	22.36
Wind 120 deg - Service		12773.94	7439.39	720.82	-1215.17	21.44
Wind 135 deg - Service		10173.27	10228.13	992.00	-973.18	18.75
Wind 150 deg - Service		7019.00	12180.17	1185.15	-675.47	14.78
Wind 180 deg - Service		44.28	13784.48	1343.26	-5.04	4.16
Wind 210 deg - Service		-6942.30	12135.89	1177.02	667.56	-7.58
Wind 225 deg - Service		-9750.88	9805.73	952.67	940.05	-12.87
Wind 240 deg - Service		-12729.66	7362.70	706.72	1213.22	-17.28
Wind 270 deg - Service		-13961.30	-44.28	-2.53	1346.12	-22.36
Wind 300 deg - Service		-11892.66	-6930.59	-670.27	1153.22	-21.44
Wind 315 deg - Service		-9813.49	-9868.35	-952.96	951.56	-18.75
Wind 330 deg - Service		-7019.00	-12180.17	-1173.94	681.65	-14.78

Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.0 Wind 0 deg - No Ice
3	0.9 Dead+1.0 Wind 0 deg - No Ice
4	1.2 Dead+1.0 Wind 30 deg - No Ice
5	0.9 Dead+1.0 Wind 30 deg - No Ice
6	1.2 Dead+1.0 Wind 45 deg - No Ice
7	0.9 Dead+1.0 Wind 45 deg - No Ice
8	1.2 Dead+1.0 Wind 60 deg - No Ice
9	0.9 Dead+1.0 Wind 60 deg - No Ice
10	1.2 Dead+1.0 Wind 90 deg - No Ice
11	0.9 Dead+1.0 Wind 90 deg - No Ice
12	1.2 Dead+1.0 Wind 120 deg - No Ice
13	0.9 Dead+1.0 Wind 120 deg - No Ice
14	1.2 Dead+1.0 Wind 135 deg - No Ice

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<i>Comb. No.</i>	<i>Description</i>
15	0.9 Dead+1.0 Wind 135 deg - No Ice
16	1.2 Dead+1.0 Wind 150 deg - No Ice
17	0.9 Dead+1.0 Wind 150 deg - No Ice
18	1.2 Dead+1.0 Wind 180 deg - No Ice
19	0.9 Dead+1.0 Wind 180 deg - No Ice
20	1.2 Dead+1.0 Wind 210 deg - No Ice
21	0.9 Dead+1.0 Wind 210 deg - No Ice
22	1.2 Dead+1.0 Wind 225 deg - No Ice
23	0.9 Dead+1.0 Wind 225 deg - No Ice
24	1.2 Dead+1.0 Wind 240 deg - No Ice
25	0.9 Dead+1.0 Wind 240 deg - No Ice
26	1.2 Dead+1.0 Wind 270 deg - No Ice
27	0.9 Dead+1.0 Wind 270 deg - No Ice
28	1.2 Dead+1.0 Wind 300 deg - No Ice
29	0.9 Dead+1.0 Wind 300 deg - No Ice
30	1.2 Dead+1.0 Wind 315 deg - No Ice
31	0.9 Dead+1.0 Wind 315 deg - No Ice
32	1.2 Dead+1.0 Wind 330 deg - No Ice
33	0.9 Dead+1.0 Wind 330 deg - No Ice
34	1.2 Dead+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 45 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
39	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
40	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
41	1.2 Dead+1.0 Wind 135 deg+1.0 Ice+1.0 Temp
42	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
43	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
44	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
45	1.2 Dead+1.0 Wind 225 deg+1.0 Ice+1.0 Temp
46	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
47	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
48	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
49	1.2 Dead+1.0 Wind 315 deg+1.0 Ice+1.0 Temp
50	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
51	Dead+Wind 0 deg - Service
52	Dead+Wind 30 deg - Service
53	Dead+Wind 45 deg - Service
54	Dead+Wind 60 deg - Service
55	Dead+Wind 90 deg - Service
56	Dead+Wind 120 deg - Service
57	Dead+Wind 135 deg - Service
58	Dead+Wind 150 deg - Service
59	Dead+Wind 180 deg - Service
60	Dead+Wind 210 deg - Service
61	Dead+Wind 225 deg - Service
62	Dead+Wind 240 deg - Service
63	Dead+Wind 270 deg - Service
64	Dead+Wind 300 deg - Service
65	Dead+Wind 315 deg - Service
66	Dead+Wind 330 deg - Service

Maximum Member Forces

<i>Section No.</i>	<i>Elevation ft</i>	<i>Component Type</i>	<i>Condition</i>	<i>Gov. Load Comb.</i>	<i>Axial lb</i>	<i>Major Axis Moment kip-ft</i>	<i>Minor Axis Moment kip-ft</i>
T1	180 - 175	Leg	Max Tension	1	0.00	0.00	0.00

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment kip-ft	Minor Axis Moment kip-ft		
T2	175 - 150	Diagonal	Max. Compression	35	-1420.10	0.13	0.10		
			Max. Mx	3	-497.59	0.82	0.60		
			Max. My	32	-280.40	-0.03	1.51		
			Max. Vy	18	372.57	-0.81	-0.60		
			Max. Vx	2	-486.69	-0.37	1.37		
			Max Tension	25	519.47	0.00	0.00		
			Max. Compression	24	-666.11	0.00	0.00		
			Max. Mx	34	-187.70	0.09	0.00		
			Max. My	34	-171.55	0.00	-0.00		
			Max. Vy	34	-49.46	0.00	0.00		
			Max. Vx	34	1.54	0.00	0.00		
			Max Tension	9	477.73	0.01	-0.00		
		Top Girt	Max. Compression	24	-503.73	0.00	0.00		
			Max. Mx	48	-11.74	0.05	-0.00		
			Max. My	24	-21.54	0.02	-0.00		
			Max. Vy	48	-50.85	0.05	-0.00		
			Max. Vx	46	1.27	0.05	-0.00		
			Max Tension	24	8.73	0.00	0.00		
			Inner Bracing	Max. Compression	24	-9.98	0.00	0.00	
				Max. Mx	34	0.42	-0.04	0.00	
				Max. Vy	34	31.70	0.00	0.00	
				Max Tension	19	15129.87	0.12	0.08	
				Leg	Max. Compression	12	-18567.56	0.62	-0.17
					Max. Mx	2	-891.02	-1.20	0.55
		Max. My			32	-1597.59	-0.02	-2.50	
		Max. Vy			28	-1751.69	-0.80	0.49	
		Max. Vx			6	-2532.73	0.13	-0.36	
		Max Tension			11	9467.87	0.00	0.00	
		Diagonal			Max. Compression	10	-9623.08	0.00	0.00
					Max. Mx	34	-133.79	0.15	0.00
			Max. My		34	-144.68	0.00	-0.01	
			Max. Vy		34	-58.24	0.00	0.00	
			Max. Vx		34	-2.19	0.00	0.00	
			Max Tension		26	5710.19	0.03	-0.00	
			Horizontal	Max. Compression	11	-5676.86	0.00	0.00	
				Max. Mx	43	202.84	0.08	0.00	
				Max. My	2	1010.05	0.02	-0.02	
				Max. Vy	43	60.72	0.08	0.00	
				Max. Vx	2	3.49	0.02	-0.02	
				Max Tension	3	5.59	0.00	0.00	
		Inner Bracing		Max. Compression	18	-8.49	0.00	0.00	
				Max. Mx	34	-5.07	-0.06	0.00	
Max. Vy	34			36.72	0.00	0.00			
Max Tension	19			49381.38	-0.44	-0.03			
Leg	Max. Compression			2	-58249.12	0.24	-0.03		
	Max. Mx			3	-28005.24	0.63	0.08		
	Max. My		14	3755.33	-0.17	-0.76			
	Max. Vy		8	-1376.13	-0.62	-0.09			
	Max. Vx		16	-1476.13	-0.01	-0.75			
	Max Tension		11	13042.07	0.00	0.00			
	Diagonal		Max. Compression	10	-13291.42	0.00	0.00		
			Max. Mx	34	-205.51	0.25	0.00		
		Max. My	34	-201.11	0.00	-0.01			
		Max. Vy	34	-88.55	0.00	0.00			
		Max. Vx	34	3.06	0.00	0.00			
		Max Tension	10	8836.39	0.00	0.00			
Horizontal		Max. Compression	11	-8714.04	0.00	0.00			
		Max. Mx	43	194.00	0.12	0.00			
		Max. My	2	400.46	0.01	-0.02			
		Max. Vy	43	70.86	0.12	0.00			
		Max. Vx	2	3.65	0.01	-0.02			

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T4	125 - 100	Inner Bracing	Max Tension	3	5.25	0.00	0.00	
			Max. Compression	18	-9.38	0.00	0.00	
			Max. Mx	34	-6.49	-0.08	0.00	
		Leg	Max. Vy	34	42.42	0.00	0.00	
			Max Tension	19	92612.24	-0.38	-0.02	
			Max. Compression	2	-106296.13	0.34	-0.03	
			Max. Mx	3	-88484.98	0.40	0.02	
			Max. My	14	14627.93	-0.11	-0.47	
			Max. Vy	8	-295.76	-0.36	-0.06	
			Max. Vx	15	-500.23	-0.10	-0.46	
			Diagonal	Max Tension	11	15086.36	0.00	0.00
				Max. Compression	10	-15374.01	0.00	0.00
		Max. Mx		34	-191.62	0.30	0.00	
		Max. My		34	-243.32	0.00	-0.01	
		Max. Vy		34	-100.03	0.00	0.00	
		Horizontal	Max. Vx	34	3.24	0.00	0.00	
			Max Tension	10	10920.75	0.00	0.00	
			Max. Compression	11	-10760.80	0.00	0.00	
			Max. Mx	43	-193.78	0.15	0.00	
			Max. My	2	212.85	0.01	-0.02	
			Max. Vy	43	-80.37	0.15	0.00	
Max. Vx	2		-3.39	0.01	-0.02			
T5	100 - 91.6667	Inner Bracing	Max Tension	3	4.18	0.00	0.00	
			Max. Compression	18	-8.79	0.00	0.00	
			Max. Mx	34	-7.09	-0.10	0.00	
		Leg	Max. Vy	34	48.12	0.00	0.00	
			Max Tension	19	107752.28	-0.31	0.03	
			Max. Compression	2	-123314.29	0.32	0.14	
			Max. Mx	3	-121656.30	0.34	-0.03	
			Max. My	16	-7587.87	-0.01	-0.45	
			Max. Vy	3	108.75	0.34	-0.03	
			Max. Vx	25	162.89	-0.17	0.40	
			Diagonal	Max Tension	11	15666.47	0.00	0.00
				Max. Compression	10	-15980.51	0.00	0.00
		Max. Mx		34	-259.05	0.32	0.00	
		Max. My		34	-358.21	0.00	0.01	
		Max. Vy		34	103.84	0.00	0.00	
		Horizontal	Max. Vx	34	-3.30	0.00	0.00	
			Max Tension	10	11556.26	0.00	0.00	
			Max. Compression	11	-11387.11	0.00	0.00	
			Max. Mx	43	-167.85	0.18	0.01	
			Max. My	2	245.67	0.03	-0.04	
			Max. Vy	43	94.69	0.18	0.01	
Max. Vx	2		-5.76	0.03	-0.04			
T6	91.6667 - 83.3333	Inner Bracing	Max Tension	3	9.00	0.00	0.00	
			Max. Compression	18	-13.81	0.00	0.00	
			Max. Mx	34	-7.60	-0.11	0.00	
		Leg	Max. Vy	34	-50.01	0.00	0.00	
			Max Tension	19	123105.66	-0.30	-0.14	
			Max. Compression	2	-140692.38	0.88	-0.19	
			Max. Mx	3	-138977.59	0.88	-0.19	
			Max. My	22	23894.72	-0.23	1.21	
			Max. Vy	3	-242.49	0.88	-0.19	
			Max. Vx	14	367.23	-0.23	-0.96	
			Diagonal	Max Tension	11	16131.33	0.00	0.00
				Max. Compression	10	-16460.35	0.00	0.00
		Max. Mx		34	-234.20	0.33	0.00	
		Max. My		34	-298.07	0.00	-0.01	
		Max. Vy		34	107.73	0.00	0.00	
			Max. Vx	34	3.36	0.00	0.00	

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T7	83.3333 - 75	Horizontal	Max Tension	10	12114.68	0.00	0.00
			Max. Compression	11	-11924.86	0.00	0.00
			Max. Mx	43	-175.20	0.19	0.01
			Max. My	2	129.71	0.03	-0.04
			Max. Vy	43	-98.32	0.19	0.01
		Inner Bracing	Max. Vx	2	5.63	0.03	-0.04
			Max Tension	3	8.58	0.00	0.00
			Max. Compression	18	-13.53	0.00	0.00
			Max. Mx	34	-7.83	-0.11	0.00
			Max. Vy	34	-51.95	0.00	0.00
		Leg	Max Tension	19	138587.64	-0.85	0.19
			Max. Compression	12	-158754.46	1.19	-0.17
			Max. Mx	3	-156449.13	1.21	-0.41
			Max. My	20	-10580.23	-0.02	1.75
			Max. Vy	3	-490.82	1.21	-0.41
		Diagonal	Max. Vx	20	-847.54	-0.02	1.75
			Max Tension	11	17605.54	0.00	0.00
			Max. Compression	10	-18047.07	0.00	0.00
			Max. Mx	34	-338.21	0.35	0.00
			Max. My	34	-381.42	0.00	-0.01
Horizontal	Max. Vy	34	-111.66	0.00	0.00		
	Max. Vx	34	3.43	0.00	0.00		
	Max Tension	10	13455.53	0.00	0.00		
	Max. Compression	11	-13258.08	0.00	0.00		
	Max. Mx	43	-245.17	0.29	0.00		
Inner Bracing	Max. My	2	580.16	0.07	-0.04		
	Max. Vy	43	-140.18	0.29	0.00		
	Max. Vx	2	6.27	0.07	-0.04		
	Max Tension	3	7.19	0.00	0.00		
	Max. Compression	28	-14.07	0.00	0.00		
Leg	Max. Mx	34	-9.08	-0.12	0.00		
	Max. Vy	34	-53.91	0.00	0.00		
	Max Tension	19	180416.85	-0.94	-0.19		
	Max. Compression	12	-206994.02	0.80	-0.26		
	Max. Mx	3	-174869.43	1.21	-0.41		
Diagonal	Max. My	20	-11261.05	-0.02	1.75		
	Max. Vy	3	217.14	1.02	0.19		
	Max. Vx	25	310.58	-0.63	1.64		
	Max Tension	11	24129.85	0.00	0.00		
	Max. Compression	10	-24667.29	0.00	0.00		
Horizontal	Max. Mx	34	-262.89	0.71	0.00		
	Max. My	34	-342.84	0.00	-0.03		
	Max. Vy	34	174.19	0.00	0.00		
	Max. Vx	34	-6.26	0.00	0.00		
	Max Tension	10	15738.27	0.00	0.00		
Inner Bracing	Max. Compression	11	-15490.93	0.00	0.00		
	Max. Mx	43	-282.04	0.30	0.00		
	Max. My	2	810.09	-0.00	-0.05		
	Max. Vy	43	127.52	0.30	0.00		
	Max. Vx	2	-5.85	-0.01	-0.05		
Leg	Max Tension	3	6.75	0.00	0.00		
	Max. Compression	28	-16.06	0.00	0.00		
	Max. Mx	34	-12.08	-0.15	0.00		
	Max. Vy	34	-58.87	0.00	0.00		
	Max Tension	19	206277.36	-0.78	-0.08		
Diagonal	Max. Compression	12	-236965.64	1.79	-0.21		
	Max. Mx	2	-236412.52	1.80	0.12		
	Max. My	14	43815.40	-0.24	-1.22		
	Max. Vy	3	-291.71	1.79	0.12		
	Max. Vx	15	-435.95	-0.23	-1.22		
T9	50 - 37.5	Diagonal	Max Tension	11	25009.28	0.00	0.00

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T10	37.5 - 25	Horizontal	Max. Compression	10	-25598.57	0.00	0.00
			Max. Mx	34	-308.79	0.76	0.00
			Max. My	34	-384.29	0.00	-0.03
			Max. Vy	34	-182.58	0.00	0.00
			Max. Vx	34	6.38	0.00	0.00
			Max Tension	10	16762.82	0.00	0.00
			Max. Compression	11	-16505.16	0.00	0.00
			Max. Mx	43	413.35	0.31	0.00
			Max. My	2	1431.93	0.03	-0.05
			Max. Vy	43	-132.25	0.31	0.00
			Max. Vx	2	5.70	0.03	-0.05
			Max Tension	3	5.64	0.00	0.00
		Inner Bracing	Max. Compression	28	-16.09	0.00	0.00
			Max. Mx	34	-12.93	-0.21	0.00
			Max. Vy	34	-79.56	0.00	0.00
			Max Tension	19	232465.48	-1.63	-0.12
			Max. Compression	12	-267502.98	-1.37	-0.34
			Max. Mx	2	-266501.23	1.80	0.12
			Max. My	14	48956.49	0.08	-2.41
			Max. Vy	2	452.58	1.80	0.12
			Max. Vx	14	412.93	0.08	-2.41
			Max Tension	11	25962.59	0.00	0.00
			Max. Compression	10	-26579.99	0.00	0.00
			Diagonal	Max. Mx	34	-340.94	0.81
		Max. My		34	-411.85	0.00	-0.03
		Max. Vy		34	-190.62	0.00	0.00
		Max. Vx		34	6.50	0.00	0.00
		Max Tension		10	17870.61	0.00	0.00
		Max. Compression		11	-17541.45	0.00	0.00
		Max. Mx		43	-255.49	0.34	0.00
		Max. My		2	505.57	0.04	-0.05
		Max. Vy		43	138.06	0.34	0.00
		Max. Vx		2	-5.55	0.04	-0.05
		Max Tension		3	5.04	0.00	0.00
		Horizontal		Max. Compression	28	-15.82	0.00
			Max. Mx	34	-13.31	-0.23	0.00
Max. Vy	34		-83.18	0.00	0.00		
Max Tension	19		284456.85	4.80	-0.09		
Max. Compression	12		-329135.88	0.00	0.00		
Max. Mx	12		-328870.17	6.90	0.34		
Max. My	14		54181.94	0.79	-4.07		
Max. Vy	12		-2175.82	6.90	0.34		
Max. Vx	14		1140.24	0.79	-4.07		
Max Tension	27		28330.90	-0.19	0.01		
Max. Compression	10		-29256.20	0.00	0.00		
Diagonal	Max. Mx		28	17390.43	-0.28	-0.02	
	Max. My	38	-1980.04	-0.14	0.04		
	Max. Vy	43	111.18	-0.21	0.04		
	Max. Vx	35	-6.96	0.00	0.00		
	Max Tension	26	19864.86	0.29	-0.01		
	Max. Compression	11	-19693.89	0.00	0.00		
	Max. Mx	43	376.13	0.52	-0.00		
	Max. My	2	1221.08	0.13	-0.05		
	Max. Vy	43	197.46	0.47	0.00		
	Max. Vx	2	-6.60	0.13	-0.05		
	Max Tension	12	5707.70	0.00	0.00		
	Redund Horz 1 Bracing	Max. Compression	12	-5707.70	0.00	0.00	
Max. Mx		34	753.48	-0.07	0.00		
Max. My		34	818.58	0.00	0.00		
Max. Vy		34	-44.23	0.00	0.00		
Max. Vx		34	-44.23	0.00	0.00		

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	45 of 65
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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
		Redund Diag 1 Bracing	Max. Vx	34	-1.02	0.00	0.00
			Max Tension	12	4132.70	0.00	0.00
		Inner Bracing	Max. Compression	12	-4132.70	0.00	0.00
			Max. Mx	34	528.32	-0.09	0.00
			Max. My	34	619.00	0.00	0.00
			Max. Vy	34	-42.38	0.00	0.00
			Max. Vx	34	-1.45	0.00	0.00
			Max Tension	3	2.86	0.00	0.00
			Max. Compression	38	-17.78	0.00	0.00
			Max. Mx	34	-15.55	-0.27	0.00
			Max. Vy	34	88.48	0.00	0.00

Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal, X lb	Horizontal, Z lb
Leg C	Max. Vert	24	359342.43	39933.49	-20539.31
	Max. H _x	24	359342.43	39933.49	-20539.31
	Max. H _z	5	-269241.36	-28235.44	20611.07
	Min. Vert	9	-307971.28	-35324.15	17898.27
	Min. H _x	9	-307971.28	-35324.15	17898.27
	Min. H _z	20	301581.19	30312.56	-21790.13
Leg B	Max. Vert	12	362709.97	-40405.58	-20223.58
	Max. H _x	29	-311648.13	35798.49	17586.44
	Max. H _z	33	-273466.50	28942.30	19974.85
	Min. Vert	29	-311648.13	35798.49	17586.44
	Min. H _x	12	362709.97	-40405.58	-20223.58
	Min. H _z	14	344748.79	-36826.11	-21419.52
Leg A	Max. Vert	2	362210.63	-509.48	45152.36
	Max. H _x	27	14705.78	6504.69	1155.14
	Max. H _z	2	362210.63	-509.48	45152.36
	Min. Vert	19	-313640.51	507.23	-39874.18
	Min. H _x	10	14833.02	-6506.94	1199.08
	Min. H _z	19	-313640.51	507.23	-39874.18

Tower Mast Reaction Summary

Load Combination	Vertical lb	Shear _x lb	Shear _z lb	Overturning Moment, M _x kip-ft	Overturning Moment, M _z kip-ft	Torque kip-ft
Dead Only	44718.64	-0.00	0.00	18.19	1.84	-0.00
1.2 Dead+1.0 Wind 0 deg - No Ice	53662.37	-241.07	-80589.15	-7454.82	46.51	-22.63
0.9 Dead+1.0 Wind 0 deg - No Ice	40246.78	-241.07	-80589.15	-7460.27	45.96	-22.63
1.2 Dead+1.0 Wind 30 deg - No Ice	53662.37	37796.99	-66073.17	-6163.36	-3504.31	41.25
0.9 Dead+1.0 Wind 30 deg - No Ice	40246.78	37796.99	-66073.17	-6168.81	-3504.86	41.25
1.2 Dead+1.0 Wind 45 deg - No Ice	53662.37	53088.10	-53386.78	-4978.69	-4943.27	70.06

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Load Combination	Vertical <i>lb</i>	Shear _x <i>lb</i>	Shear _z <i>lb</i>	Overturning Moment, M _x <i>kip-ft</i>	Overturning Moment, M _z <i>kip-ft</i>	Torque <i>kip-ft</i>
0.9 Dead+1.0 Wind 45 deg - No Ice	40246.78	53088.10	-53386.78	-4984.15	-4943.82	70.06
1.2 Dead+1.0 Wind 60 deg - No Ice	53662.37	64507.86	-37315.64	-3472.11	-6026.35	94.09
0.9 Dead+1.0 Wind 60 deg - No Ice	40246.78	64507.86	-37315.64	-3477.56	-6026.90	94.09
1.2 Dead+1.0 Wind 90 deg - No Ice	53662.37	76011.53	241.07	66.13	-7087.56	121.71
0.9 Dead+1.0 Wind 90 deg - No Ice	40246.78	76011.53	241.07	60.67	-7088.11	121.71
1.2 Dead+1.0 Wind 120 deg - No Ice	53662.37	69546.99	40503.35	3798.52	-6427.49	116.72
0.9 Dead+1.0 Wind 120 deg - No Ice	40246.78	69546.99	40503.35	3793.06	-6428.04	116.72
1.2 Dead+1.0 Wind 135 deg - No Ice	53662.37	55387.83	55686.50	5230.68	-5151.60	102.07
0.9 Dead+1.0 Wind 135 deg - No Ice	40246.78	55387.83	55686.50	5225.22	-5152.15	102.07
1.2 Dead+1.0 Wind 150 deg - No Ice	53662.37	38214.54	66314.24	6251.31	-3581.04	80.46
0.9 Dead+1.0 Wind 150 deg - No Ice	40246.78	38214.54	66314.24	6245.86	-3581.59	80.46
1.2 Dead+1.0 Wind 180 deg - No Ice	53662.37	241.07	75048.83	7086.43	-42.09	22.63
0.9 Dead+1.0 Wind 180 deg - No Ice	40246.78	241.07	75048.83	7080.97	-42.65	22.63
1.2 Dead+1.0 Wind 210 deg - No Ice	53662.37	-37796.99	66073.17	6207.01	3508.72	-41.25
0.9 Dead+1.0 Wind 210 deg - No Ice	40246.78	-37796.99	66073.17	6201.55	3508.17	-41.25
1.2 Dead+1.0 Wind 225 deg - No Ice	53662.37	-53088.10	53386.78	5022.35	4947.68	-70.06
0.9 Dead+1.0 Wind 225 deg - No Ice	40246.78	-53088.10	53386.78	5016.89	4947.13	-70.06
1.2 Dead+1.0 Wind 240 deg - No Ice	53662.37	-69305.92	40085.80	3721.78	6387.60	-94.09
0.9 Dead+1.0 Wind 240 deg - No Ice	40246.78	-69305.92	40085.80	3716.32	6387.05	-94.09
1.2 Dead+1.0 Wind 270 deg - No Ice	53662.37	-76011.53	-241.07	-22.48	7091.98	-121.71
0.9 Dead+1.0 Wind 270 deg - No Ice	40246.78	-76011.53	-241.07	-27.93	7091.42	-121.71
1.2 Dead+1.0 Wind 300 deg - No Ice	53662.37	-64748.93	-37733.19	-3548.84	6075.07	-116.72
0.9 Dead+1.0 Wind 300 deg - No Ice	40246.78	-64748.93	-37733.19	-3554.30	6074.52	-116.72
1.2 Dead+1.0 Wind 315 deg - No Ice	53662.37	-53429.03	-53727.70	-5041.35	5010.34	-102.07
0.9 Dead+1.0 Wind 315 deg - No Ice	40246.78	-53429.03	-53727.70	-5046.80	5009.79	-102.07
1.2 Dead+1.0 Wind 330 deg - No Ice	53662.37	-38214.54	-66314.24	-6207.66	3585.46	-80.46
0.9 Dead+1.0 Wind 330 deg - No Ice	40246.78	-38214.54	-66314.24	-6213.12	3584.91	-80.46
1.2 Dead+1.0 Ice+1.0 Temp	133197.53	-0.00	0.00	131.37	45.33	0.00
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	133197.53	-28.67	-19685.71	-1617.76	50.67	-18.75
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	133197.53	9553.09	-16620.91	-1350.47	-802.21	1.95
1.2 Dead+1.0 Wind 45 deg+1.0 Ice+1.0 Temp	133197.53	13468.75	-13506.14	-1072.83	-1151.92	12.46

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Load Combination	Vertical lb	Shear _x lb	Shear _z lb	Overturing Moment, M _x kip-ft	Overturing Moment, M _z kip-ft	Torque kip-ft
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	133197.53	16437.42	-9500.04	-715.26	-1417.91	22.12
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	133197.53	19155.85	28.67	136.72	-1659.01	36.36
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	133197.53	17016.87	9867.69	1010.57	-1463.62	40.86
1.2 Dead+1.0 Wind 135 deg+1.0 Ice+1.0 Temp	133197.53	13734.14	13771.54	1359.61	-1175.96	38.97
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	133197.53	9602.76	16649.59	1618.56	-811.47	34.42
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	133197.53	28.67	19049.74	1833.89	39.98	18.75
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	133197.53	-9553.09	16620.91	1613.21	892.87	-1.95
1.2 Dead+1.0 Wind 225 deg+1.0 Ice+1.0 Temp	133197.53	-13468.75	13506.14	1335.57	1242.58	-12.46
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	133197.53	-16988.19	9818.03	1001.31	1548.93	-22.12
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	133197.53	-19155.85	-28.67	126.03	1749.66	-36.36
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	133197.53	-16466.10	-9549.70	-724.51	1513.91	-40.86
1.2 Dead+1.0 Wind 315 deg+1.0 Ice+1.0 Temp	133197.53	-13509.29	-13546.69	-1080.38	1250.13	-38.97
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp	133197.53	-9602.76	-16649.59	-1355.81	902.12	-34.42
Dead+Wind 0 deg - Service	44718.64	-44.28	-14802.09	-1355.07	9.98	-4.16
Dead+Wind 30 deg - Service	44718.64	6942.30	-12135.89	-1117.86	-642.21	7.58
Dead+Wind 45 deg - Service	44718.64	9750.88	-9805.73	-900.27	-906.51	12.87
Dead+Wind 60 deg - Service	44718.64	11848.38	-6853.89	-623.55	-1105.44	17.28
Dead+Wind 90 deg - Service	44718.64	13961.30	44.28	26.33	-1300.36	22.36
Dead+Wind 120 deg - Service	44718.64	12773.94	7439.39	711.87	-1179.12	21.44
Dead+Wind 135 deg - Service	44718.64	10173.27	10228.13	974.92	-944.78	18.75
Dead+Wind 150 deg - Service	44718.64	7019.00	12180.17	1162.38	-656.31	14.78
Dead+Wind 180 deg - Service	44718.64	44.28	13784.48	1315.77	-6.30	4.16
Dead+Wind 210 deg - Service	44718.64	-6942.30	12135.89	1154.24	645.89	-7.58
Dead+Wind 225 deg - Service	44718.64	-9750.88	9805.73	936.65	910.19	-12.87
Dead+Wind 240 deg - Service	44718.64	-12729.66	7362.70	697.77	1174.67	-17.28
Dead+Wind 270 deg - Service	44718.64	-13961.30	-44.28	10.05	1304.04	-22.36
Dead+Wind 300 deg - Service	44718.64	-11892.66	-6930.59	-637.65	1117.26	-21.44
Dead+Wind 315 deg - Service	44718.64	-9813.49	-9868.35	-911.78	921.70	-18.75
Dead+Wind 330 deg - Service	44718.64	-7019.00	-12180.17	-1126.00	659.99	-14.78

Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX lb	PY lb	PZ lb	PX lb	PY lb	PZ lb	
1	0.00	-44718.64	0.00	0.00	44718.64	-0.00	0.000%
2	-241.07	-53662.37	-80589.15	241.07	53662.37	80589.15	0.000%
3	-241.07	-40246.78	-80589.15	241.07	40246.78	80589.15	0.000%
4	37796.99	-53662.37	-66073.17	-37796.99	53662.37	66073.17	0.000%
5	37796.99	-40246.78	-66073.17	-37796.99	40246.78	66073.17	0.000%
6	53088.10	-53662.37	-53386.77	-53088.10	53662.37	53386.78	0.000%
7	53088.10	-40246.78	-53386.77	-53088.10	40246.78	53386.78	0.000%
8	64507.86	-53662.37	-37315.64	-64507.86	53662.37	37315.64	0.000%
9	64507.86	-40246.78	-37315.64	-64507.86	40246.78	37315.64	0.000%
10	76011.52	-53662.37	241.07	-76011.53	53662.37	-241.07	0.000%

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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX lb	PY lb	PZ lb	PX lb	PY lb	PZ lb	
11	76011.52	-40246.78	241.07	-76011.53	40246.78	-241.07	0.000%
12	69546.99	-53662.37	40503.35	-69546.99	53662.37	-40503.35	0.000%
13	69546.99	-40246.78	40503.35	-69546.99	40246.78	-40503.35	0.000%
14	55387.83	-53662.37	55686.50	-55387.83	53662.37	-55686.50	0.000%
15	55387.83	-40246.78	55686.50	-55387.83	40246.78	-55686.50	0.000%
16	38214.53	-53662.37	66314.24	-38214.54	53662.37	-66314.24	0.000%
17	38214.53	-40246.78	66314.24	-38214.54	40246.78	-66314.24	0.000%
18	241.07	-53662.37	75048.83	-241.07	53662.37	-75048.83	0.000%
19	241.07	-40246.78	75048.83	-241.07	40246.78	-75048.83	0.000%
20	-37796.99	-53662.37	66073.17	37796.99	53662.37	-66073.17	0.000%
21	-37796.99	-40246.78	66073.17	37796.99	40246.78	-66073.17	0.000%
22	-53088.10	-53662.37	53386.77	53088.10	53662.37	-53386.78	0.000%
23	-53088.10	-40246.78	53386.77	53088.10	40246.78	-53386.78	0.000%
24	-69305.92	-53662.37	40085.80	69305.92	53662.37	-40085.80	0.000%
25	-69305.92	-40246.78	40085.80	69305.92	40246.78	-40085.80	0.000%
26	-76011.52	-53662.37	-241.07	76011.53	53662.37	241.07	0.000%
27	-76011.52	-40246.78	-241.07	76011.53	40246.78	241.07	0.000%
28	-64748.93	-53662.37	-37733.19	64748.93	53662.37	37733.19	0.000%
29	-64748.93	-40246.78	-37733.19	64748.93	40246.78	37733.19	0.000%
30	-53429.03	-53662.37	-53727.70	53429.03	53662.37	53727.70	0.000%
31	-53429.03	-40246.78	-53727.70	53429.03	40246.78	53727.70	0.000%
32	-38214.53	-53662.37	-66314.24	38214.54	53662.37	66314.24	0.000%
33	-38214.53	-40246.78	-66314.24	38214.54	40246.78	66314.24	0.000%
34	0.00	-133197.53	0.00	0.00	133197.53	-0.00	0.000%
35	-28.67	-133197.53	-19685.71	28.67	133197.53	19685.71	0.000%
36	9553.09	-133197.53	-16620.91	-9553.09	133197.53	16620.91	0.000%
37	13468.74	-133197.53	-13506.14	-13468.75	133197.53	13506.14	0.000%
38	16437.42	-133197.53	-9500.04	-16437.42	133197.53	9500.04	0.000%
39	19155.85	-133197.53	28.67	-19155.85	133197.53	-28.67	0.000%
40	17016.86	-133197.53	9867.69	-17016.87	133197.53	-9867.69	0.000%
41	13734.14	-133197.53	13771.54	-13734.14	133197.53	-13771.54	0.000%
42	9602.75	-133197.53	16649.59	-9602.76	133197.53	-16649.59	0.000%
43	28.67	-133197.53	19049.74	-28.67	133197.53	-19049.74	0.000%
44	-9553.09	-133197.53	16620.91	9553.09	133197.53	-16620.91	0.000%
45	-13468.74	-133197.53	13506.14	13468.75	133197.53	-13506.14	0.000%
46	-16988.19	-133197.53	9818.03	16988.19	133197.53	-9818.03	0.000%
47	-19155.85	-133197.53	-28.67	19155.85	133197.53	28.67	0.000%
48	-16466.10	-133197.53	-9549.70	16466.10	133197.53	9549.70	0.000%
49	-13509.29	-133197.53	-13546.69	13509.29	133197.53	13546.69	0.000%
50	-9602.75	-133197.53	-16649.59	9602.76	133197.53	16649.59	0.000%
51	-44.28	-44718.64	-14802.09	44.28	44718.64	14802.09	0.000%
52	6942.30	-44718.64	-12135.89	-6942.30	44718.64	12135.89	0.000%
53	9750.88	-44718.64	-9805.73	-9750.88	44718.64	9805.73	0.000%
54	11848.38	-44718.64	-6853.89	-11848.38	44718.64	6853.89	0.000%
55	13961.30	-44718.64	44.28	-13961.30	44718.64	-44.28	0.000%
56	12773.94	-44718.64	7439.39	-12773.94	44718.64	-7439.39	0.000%
57	10173.27	-44718.64	10228.13	-10173.27	44718.64	-10228.13	0.000%
58	7019.00	-44718.64	12180.17	-7019.00	44718.64	-12180.17	0.000%
59	44.28	-44718.64	13784.48	-44.28	44718.64	-13784.48	0.000%
60	-6942.30	-44718.64	12135.89	6942.30	44718.64	-12135.89	0.000%
61	-9750.88	-44718.64	9805.73	9750.88	44718.64	-9805.73	0.000%
62	-12729.66	-44718.64	7362.70	12729.66	44718.64	-7362.70	0.000%
63	-13961.30	-44718.64	-44.28	13961.30	44718.64	44.28	0.000%
64	-11892.66	-44718.64	-6930.59	11892.66	44718.64	6930.59	0.000%
65	-9813.49	-44718.64	-9868.35	9813.49	44718.64	9868.35	0.000%
66	-7019.00	-44718.64	-12180.17	7019.00	44718.64	12180.17	0.000%

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	49 of 65
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Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 175	2.745	56	0.1200	0.0366
T2	175 - 150	2.619	56	0.1201	0.0369
T3	150 - 125	1.975	56	0.1178	0.0284
T4	125 - 100	1.374	56	0.1053	0.0228
T5	100 - 91.6667	0.871	56	0.0819	0.0175
T6	91.6667 - 83.3333	0.730	56	0.0750	0.0157
T7	83.3333 - 75	0.600	56	0.0675	0.0140
T8	75 - 50	0.487	56	0.0592	0.0123
T9	50 - 37.5	0.227	56	0.0391	0.0080
T10	37.5 - 25	0.132	56	0.0303	0.0058
T11	25 - 0	0.061	56	0.0208	0.0037

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
181.00	OGT9-840	56	2.745	0.1200	0.0366	155978
180.00	Pirod 4' Side Mount Standoff (1)	56	2.745	0.1200	0.0366	155978
178.00	4'x4" Pipe Mount	56	2.694	0.1200	0.0368	155978
177.00	OGT9-840	56	2.669	0.1200	0.0369	155978
175.00	10 FT DISH	56	2.619	0.1201	0.0369	155978
173.00	(inverted) SC479-HF1LDF	56	2.568	0.1201	0.0368	149240
170.00	10'6"x4" Pipe Mount	56	2.491	0.1200	0.0363	187307
169.00	8 FT DISH	56	2.466	0.1200	0.0360	210518
168.00	4'x4" Pipe Mount	56	2.440	0.1200	0.0357	240296
167.00	8 FT DISH	56	2.414	0.1200	0.0354	279885
157.00	ANT220F2 w/clamps	56	2.155	0.1192	0.0314	303506
150.00	Valmont 13' Lightweight T-Frame	56	1.975	0.1178	0.0284	140835
149.00	(2) 7770.00 panel antenna	56	1.950	0.1176	0.0280	133602
148.00	20' 8 Bay Di-Pole	56	1.925	0.1173	0.0277	127949
147.00	(2) LPG21401 TMA	56	1.900	0.1170	0.0274	123341
143.00	Pirod 4' Side Mount Standoff (1)	56	1.800	0.1157	0.0262	109546
140.00	PD200	56	1.726	0.1145	0.0255	101211
138.00	12' Dipole	56	1.677	0.1136	0.0251	96325
136.00	DB224-A	56	1.629	0.1126	0.0247	91889
134.00	ANT220F2 w/clamps	56	1.582	0.1115	0.0243	87843
116.00	DS9A09F36D-N 19 ft Omni w/ Mount Pipe	56	1.180	0.0972	0.0210	67703
105.00	PD458-1	56	0.963	0.0864	0.0186	61937
100.00	DB222	56	0.871	0.0819	0.0175	61319
86.00	DB212-1	56	0.640	0.0700	0.0145	55112
81.00	DB222	56	0.567	0.0652	0.0135	51208
80.00	4'x4" Pipe Mount	56	0.553	0.0642	0.0133	51975
79.00	8 FT DISH	56	0.539	0.0632	0.0131	53006
49.00	DB803M-XT	56	0.218	0.0384	0.0078	87869
48.00	Pirod 4' Side Mount Standoff (1)	56	0.210	0.0377	0.0076	88369

Maximum Tower Deflections - Design Wind

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Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	180 - 175	14.877	12	0.6506	0.1992
T2	175 - 150	14.195	12	0.6507	0.2009
T3	150 - 125	10.708	12	0.6388	0.1547
T4	125 - 100	7.448	12	0.5711	0.1240
T5	100 - 91.6667	4.721	12	0.4433	0.0951
T6	91.6667 - 83.3333	3.954	12	0.4062	0.0855
T7	83.3333 - 75	3.255	12	0.3652	0.0760
T8	75 - 50	2.641	12	0.3204	0.0671
T9	50 - 37.5	1.231	12	0.2115	0.0434
T10	37.5 - 25	0.718	3	0.1640	0.0317
T11	25 - 0	0.333	3	0.1127	0.0202

Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
181.00	OGT9-840	12	14.877	0.6506	0.1992	29976
180.00	Pirod 4' Side Mount Standoff (1)	12	14.877	0.6506	0.1992	29976
178.00	4'x4" Pipe Mount	12	14.605	0.6507	0.2003	29976
177.00	OGT9-840	12	14.468	0.6507	0.2006	29976
175.00	10 FT DISH	12	14.195	0.6507	0.2009	29976
173.00	(inverted) SC479-HF1LDF	12	13.920	0.6507	0.2002	28843
170.00	10'6"x4" Pipe Mount	12	13.504	0.6505	0.1974	36851
169.00	8 FT DISH	12	13.365	0.6504	0.1960	41819
168.00	4'x4" Pipe Mount	12	13.225	0.6503	0.1945	48335
167.00	8 FT DISH	12	13.085	0.6501	0.1929	57256
157.00	ANT220F2 w/clamps	12	11.682	0.6457	0.1707	63441
150.00	Valmont 13' Lightweight T-Frame	12	10.708	0.6388	0.1547	27114
149.00	(2) 7770.00 panel antenna	12	10.570	0.6375	0.1527	25617
148.00	20' 8 Bay Di-Pole	12	10.433	0.6361	0.1508	24450
147.00	(2) LPG21401 TMA	12	10.296	0.6346	0.1490	23504
143.00	Pirod 4' Side Mount Standoff (1)	12	9.755	0.6274	0.1428	20701
140.00	PD200	12	9.355	0.6209	0.1389	19016
138.00	12' Dipole	12	9.091	0.6160	0.1366	18030
136.00	DB224-A	12	8.830	0.6106	0.1345	17141
134.00	ANT220F2 w/clamps	12	8.572	0.6046	0.1325	16317
116.00	DS9A09F36D-N 19 ft Omni w/ Mount Pipe	12	6.396	0.5269	0.1143	12403
105.00	PD458-1	12	5.216	0.4680	0.1011	11374
100.00	DB222	12	4.721	0.4433	0.0951	11272
86.00	DB212-1	12	3.470	0.3790	0.0790	10164
81.00	DB222	12	3.074	0.3527	0.0735	9463
80.00	4'x4" Pipe Mount	12	2.999	0.3473	0.0724	9608
79.00	8 FT DISH	12	2.925	0.3419	0.0713	9802
49.00	DB803M-XT	12	1.186	0.2077	0.0425	16242
48.00	Pirod 4' Side Mount Standoff (1)	12	1.141	0.2039	0.0416	16334

Bolt Design Data

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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt lb	Allowable Load per Bolt lb	Ratio Load Allowable	Allowable Ratio	Criteria
T1	180	Diagonal	A325X	1.0000	1	519.47	18288.30	0.028 ✓	1	Member Block Shear
T2	175	Leg	A325X	0.7500	6	245.23	30101.40	0.008 ✓	1	Bolt Tension
		Diagonal	A325X	1.0000	1	9467.87	18288.30	0.518 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	2855.09	10263.30	0.278 ✓	1	Member Block Shear
T3	150	Leg	A325X	0.7500	6	4051.53	30101.40	0.135 ✓	1	Bolt Tension
		Diagonal	A325X	1.0000	1	13042.10	27103.10	0.481 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	4418.20	10263.30	0.430 ✓	1	Member Block Shear
T4	125	Leg	A325X	0.7500	6	10577.50	30101.40	0.351 ✓	1	Bolt Tension
		Diagonal	A325X	1.0000	1	15086.40	27103.10	0.557 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	5460.37	10263.30	0.532 ✓	1	Member Block Shear
T5	100	Leg	A325X	0.7500	6	17958.70	30101.40	0.597 ✓	1	Bolt Tension
		Diagonal	A325X	1.0000	1	15666.50	27103.10	0.578 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	5778.13	10263.30	0.563 ✓	1	Member Block Shear
T6	91.6667	Diagonal	A325X	1.0000	1	16131.30	27103.10	0.595 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	6057.34	10263.30	0.590 ✓	1	Member Block Shear
T7	83.3333	Diagonal	A325X	1.0000	1	17605.50	27103.10	0.650 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	6727.76	17257.30	0.390 ✓	1	Bolt Shear
T8	75	Leg	A325X	1.0000	8	19370.50	54517.00	0.355 ✓	1	Bolt Tension
		Diagonal	A325X	1.0000	1	24129.90	48810.90	0.494 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	7869.13	11622.70	0.677 ✓	1	Member Block Shear
T9	50	Leg	A325X	1.0000	8	25784.70	54517.00	0.473 ✓	1	Bolt Tension
		Diagonal	A325X	1.0000	1	25009.30	48810.90	0.512 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	8381.41	11622.70	0.721 ✓	1	Member Block Shear
T10	37.5	Diagonal	A325X	1.0000	1	25962.60	48810.90	0.532 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	8935.31	11622.70	0.769 ✓	1	Member Block Shear
T11	25	Leg	A325X	1.0000	8	32141.90	54517.00	0.590 ✓	1	Bolt Tension
		Diagonal	A325X	1.0000	1	28330.90	38085.90	0.744 ✓	1	Member Block Shear
		Horizontal	A325X	0.6250	2	9932.43	17257.30	0.576 ✓	1	Bolt Shear

Compression Checks

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Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 175	HSS5x.25	5.01	5.01	35.6 K=1.00	3.4894	-1420.10	143130.00	0.010 ¹ ✓
T2	175 - 150	HSS5x.25	25.03	8.34	59.3 K=1.00	3.4894	-18567.60	121395.00	0.153 ¹ ✓
T3	150 - 125	HSS5x.25	25.03	8.34	59.3 K=1.00	3.4894	-58249.10	121395.00	0.480 ¹ ✓
T4	125 - 100	HSS5x.25	25.03	8.34	59.3 K=1.00	3.4894	-106296.00	121395.00	0.876 ¹ ✓
T5	100 - 91.6667	HSS5x.375	8.34	8.34	60.7 K=1.00	5.0994	-123314.00	175270.00	0.704 ¹ ✓
T6	91.6667 - 83.3333	HSS5x.375	8.34	8.34	60.7 K=1.00	5.0994	-140692.00	199288.00	0.706 ¹ ✓
T7	83.3333 - 75	HSS5x.375	8.34	8.34	60.7 K=1.00	5.0994	-158754.00	199288.00	0.797 ¹ ✓
T8	75 - 50	HSS6.875x.375	25.03	12.51	65.0 K=1.00	7.1552	-206994.00	266736.00	0.776 ¹ ✓
T9	50 - 37.5	HSS6.875x.5	12.51	12.51	66.1 K=1.00	9.3640	-236966.00	344700.00	0.687 ¹ ✓
T10	37.5 - 25	HSS6.875x.5	12.51	12.51	66.1 K=1.00	9.3640	-267503.00	344700.00	0.776 ¹ ✓
T11	25 - 0	HSS6.875x.5	25.03	6.26	33.0 K=1.00	9.3640	-329136.00	459464.00	0.716 ¹ ✓

¹ P_u / φP_n controls

Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 175	2L2 1/2x2x3/16x3/8	7.43	7.15	114.6 K=1.00	1.6200	-666.11	31902.60	0.021 ¹ ✓
T2	175 - 150	2L2 1/2x2x3/16x3/8	10.57	10.23	164.0 K=1.00	1.6200	-9297.80	16563.10	0.561 ¹ ✓
T3	150 - 125	2L3x2 1/2x1/4x3/8	11.21	10.90	142.2 K=1.00	2.6300	-13291.40	35690.50	0.372 ¹ ✓
T4	125 - 100	2L3x2 1/2x1/4x3/8	11.91	11.61	151.5 K=1.00	2.6300	-15374.00	31623.00	0.486 ¹ ✓
T5	100 - 91.6667	2L3x2 1/2x1/4x3/8	12.15	11.86	154.7 K=1.00	2.6300	-15980.50	30376.70	0.526 ¹ ✓
T6	91.6667 - 83.3333	2L3x2 1/2x1/4x3/8	12.39	12.11	157.9 K=1.00	2.6300	-16460.40	29183.60	0.564 ¹ ✓
T7	83.3333 - 75	2L3x2 1/2x1/4x3/8	12.64	12.36	161.3 K=1.00	2.6300	-18047.10	28042.30	0.644 ¹ ✓
T8	75 - 50	2L3 1/2x3x3/8x3/8	16.33	15.88	174.8 K=1.00	4.5900	-24667.30	42971.90	0.574 ¹ ✓

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T9	50 - 37.5	2L3 1/2x3x3/8x3/8	16.65	16.22	178.6 K=1.00	4.5900	-25598.60	41201.20	0.621 ¹ ✓
T10	37.5 - 25	2L3 1/2x3x3/8x3/8	16.99	16.56	182.4 K=1.00	4.5900	-26580.00	39503.20	0.673 ¹ ✓
T11	25 - 0	2L3x3 1/2x5/16x3/8	17.68	17.28	137.0 K=1.00	3.8700	-29256.20	57793.70	0.506 ¹ ✓

¹ P_u / φP_n controls

Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T2	175 - 150	L3x3x1/4	12.33	5.96	120.8 K=1.00	1.4400	-5621.16	28061.80	0.200 ¹ ✓
T3	150 - 125	L3x3x1/4	14.33	6.96	141.0 K=1.00	1.4400	-8714.04	20717.20	0.421 ¹ ✓
T4	125 - 100	L3x3x1/4	16.33	7.96	161.3 K=1.00	1.4400	-10760.80	15837.90	0.679 ¹ ✓
T5	100 - 91.6667	L3x4x1/4	17.00	8.29	152.8 K=1.00	1.6900	-11387.10	20706.20	0.550 ¹ ✓
T6	91.6667 - 83.3333	L3x4x1/4	17.67	8.63	159.0 K=1.00	1.6900	-11924.90	19136.60	0.623 ¹ ✓
T7	83.3333 - 75	L3x4x1/2	18.33	8.96	168.2 K=1.00	3.2500	-13258.10	32867.40	0.403 ¹ ✓
T8	75 - 50	L4x4x1/4	20.00	9.71	146.6 K=1.00	1.9400	-15490.90	25829.50	0.600 ¹ ✓
T9	50 - 37.5	L4x4x1/4	21.00	10.21	154.2 K=1.00	1.9400	-16505.20	23362.50	0.706 ¹ ✓
T10	37.5 - 25	L4x4x1/4	22.00	10.71	161.7 K=1.00	1.9400	-17541.40	21232.70	0.826 ¹ ✓
T11	25 - 0	L4x4x1/2	24.00	11.71	179.7 K=1.00	3.7500	-19693.90	33220.30	0.593 ¹ ✓

¹ P_u / φP_n controls

Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 175	L3x3x1/4	10.60	5.09	103.2 K=1.00	1.4400	-503.73	34476.00	0.015 ¹ ✓

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¹ P_u / φP_n controls

Redundant Horizontal (1) Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T11	25 - 0	L3x3x1/4	6.00	5.71	115.8 K=1.00	1.4400	-5707.70	29975.50	0.190 ¹ ✓

¹ P_u / φP_n controls

Redundant Diagonal (1) Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T11	25 - 0	L3x3x1/4	8.49	8.07	163.6 K=1.00	1.4400	-4040.04	15399.40	0.262 ¹ ✓

¹ P_u / φP_n controls

Inner Bracing Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 175	L2 1/2x2 1/2x3/16	5.30	5.30	128.5 K=1.00	0.9020	-9.98	15638.70	0.001 ¹ ✓
T2	175 - 150	L2 1/2x2 1/2x3/16	5.83	5.83	141.4 K=1.00	0.9020	-8.49	12909.80	0.001 ¹ ✓
T3	150 - 125	L2 1/2x2 1/2x3/16	7.17	7.17	173.7 K=1.00	0.9020	-8.99	8552.99	0.001 ¹ ✓
T4	125 - 100	L2 1/2x2 1/2x3/16	8.17	8.17	198.0 K=1.00	0.9020	-8.64	6586.62	0.001 ¹ ✓
T5	100 - 91.6667	L2 1/2x2 1/2x3/16	8.50	8.50	206.1 K=1.00	0.9020	-13.81	6080.15	0.002 ¹ ✓
T6	91.6667 - 83.3333	L2 1/2x2 1/2x3/16	8.83	8.83	214.1 K=1.00	0.9020	-13.53	5629.93	0.002 ¹ ✓
T7	83.3333 - 75	L2 1/2x2 1/2x3/16	9.17	9.17	222.2 K=1.00	0.9020	-14.07	5227.92	0.003 ¹ ✓
T8	75 - 50	L2 1/2x2 1/2x3/16	10.00	10.00	242.4 K=1.00	0.9020	-15.78	4392.91	0.004 ¹ ✓
T9	50 - 37.5	L3x3x1/4	10.50	10.50	212.8 K=1.00	1.4400	-16.09	9098.35	0.002 ¹ ✓
T10	37.5 - 25	L3x3x1/4	11.00	11.00	223.0 K=1.00	1.4400	-15.82	8290.02	0.002 ¹ ✓
T11	25 - 0	L3x3x1/4	12.00	12.00	243.2	1.4400	-17.77	6965.92	0.003 ¹ ✓

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
K=1.00									✓

¹ P_u / φP_n controls

Tension Checks

Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T2	175 - 150	HSS5x.25	25.03	8.34	59.3	3.4894	15129.90	157023.00	0.096 ¹
T3	150 - 125	HSS5x.25	25.03	8.34	59.3	3.4894	49381.40	157023.00	0.314 ¹
T4	125 - 100	HSS5x.25	25.03	8.34	59.3	3.4894	92612.20	157023.00	0.590 ¹
T5	100 - 91.6667	HSS5x.375	8.34	8.34	60.7	5.0994	107752.00	229474.00	0.470 ¹
T6	91.6667 - 83.3333	HSS5x.375	8.34	8.34	60.7	5.0994	123106.00	275369.00	0.447 ¹
T7	83.3333 - 75	HSS5x.375	8.34	8.34	60.7	5.0994	138588.00	275369.00	0.503 ¹
T8	75 - 50	HSS6.875x.375	25.03	12.51	65.0	7.1552	180417.00	386381.00	0.467 ¹
T9	50 - 37.5	HSS6.875x.5	12.51	12.51	66.1	9.3640	206277.00	505655.00	0.408 ¹
T10	37.5 - 25	HSS6.875x.5	12.51	12.51	66.1	9.3640	232465.00	505655.00	0.460 ¹
T11	25 - 0	HSS6.875x.5	25.03	6.26	33.0	9.3640	284457.00	505655.00	0.563 ¹

¹ P_u / φP_n controls

Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 175	2L2 1/2x2x3/16x3/8	7.43	7.15	108.2	0.8986	519.47	39088.80	0.013 ¹
T2	175 - 150	2L2 1/2x2x3/16x3/8	10.37	10.03	151.8	0.8986	9467.87	39088.80	0.242 ¹
T3	150 - 125	2L3x2 1/2x1/4x3/8	11.21	10.90	138.4	1.5506	13042.10	67452.20	0.193 ¹

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	Client Eversource Phase (b.2) rev. 3	Designed by christina.carlos

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T4	125 - 100	2L3x2 1/2x1/4x3/8	11.91	11.61	147.5	1.5506	15086.40	67452.20	0.224 ¹
T5	100 - 91.6667	2L3x2 1/2x1/4x3/8	12.15	11.86	150.6	1.5506	15666.50	67452.20	0.232 ¹
T6	91.6667 - 83.3333	2L3x2 1/2x1/4x3/8	12.39	12.11	153.8	1.5506	16131.30	67452.20	0.239 ¹
T7	83.3333 - 75	2L3x2 1/2x1/4x3/8	12.64	12.36	157.0	1.5506	17605.50	67452.20	0.261 ¹
T8	75 - 50	2L3 1/2x3x3/8x3/8	16.33	15.88	174.8	2.8097	24129.90	122221.00	0.197 ¹
T9	50 - 37.5	2L3 1/2x3x3/8x3/8	16.65	16.22	178.6	2.8097	25009.30	122221.00	0.205 ¹
T10	37.5 - 25	2L3 1/2x3x3/8x3/8	16.99	16.56	182.4	2.8097	25962.60	122221.00	0.212 ¹
T11	25 - 0	2L3x3 1/2x5/16x3/8	17.68	17.28	124.9	2.3752	28330.90	115789.00	0.245 ¹

¹ P_u / φP_n controls

Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T2	175 - 150	L3x3x1/4	11.67	5.63	72.6	0.9394	5710.19	40862.80	0.140 ¹
T3	150 - 125	L3x3x1/4	14.33	6.96	89.8	0.9394	8836.39	40862.80	0.216 ¹
T4	125 - 100	L3x3x1/4	16.33	7.96	102.7	0.9394	10920.70	40862.80	0.267 ¹
T5	100 - 91.6667	L3x4x1/4	17.00	8.29	110.9	1.1269	11556.30	49019.10	0.236 ¹
T6	91.6667 - 83.3333	L3x4x1/4	17.67	8.63	115.4	1.1269	12114.70	49019.10	0.247 ¹
T7	83.3333 - 75	L3x4x1/2	18.33	8.96	124.6	2.1563	13455.50	93796.90	0.143 ¹
T8	75 - 50	L4x4x1/4	20.00	9.71	93.3	1.3144	15738.30	57175.30	0.275 ¹
T9	50 - 37.5	L4x4x1/4	21.00	10.21	98.1	1.3144	16762.80	57175.30	0.293 ¹
T10	37.5 - 25	L4x4x1/4	22.00	10.71	102.8	1.3144	17870.60	57175.30	0.313 ¹
T11	25 - 0	L4x4x1/2	24.00	11.71	115.2	2.5313	19864.90	110109.00	0.180 ¹

¹ P_u / φP_n controls

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Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 175	L3x3x1/4	10.60	5.09	65.7	1.4400	477.73	46656.00	0.010 ¹ ✓

¹ P_u / φP_n controls

Redundant Horizontal (1) Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T11	25 - 0	L3x3x1/4	6.00	5.71	73.7	1.4400	5707.70	46656.00	0.122 ¹ ✓

¹ P_u / φP_n controls

Redundant Diagonal (1) Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T11	25 - 0	L3x3x1/4	8.33	7.90	102.0	1.4400	4132.70	46656.00	0.089 ¹ ✓

¹ P_u / φP_n controls

Inner Bracing Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio $\frac{P_u}{\phi P_n}$
T1	180 - 175	L2 1/2x2 1/2x3/16	5.30	5.30	81.7	0.9020	8.73	29224.80	0.000 ¹ ✓
T2	175 - 150	L2 1/2x2 1/2x3/16	5.83	5.83	90.0	0.9020	5.59	29224.80	0.000 ¹ ✓
T3	150 - 125	L2 1/2x2 1/2x3/16	6.50	6.50	100.3	0.9020	5.25	29224.80	0.000 ¹ ✓
T4	125 - 100	L2 1/2x2 1/2x3/16	7.83	7.83	120.8	0.9020	4.18	29224.80	0.000 ¹ ✓
T5	100 - 91.6667	L2 1/2x2 1/2x3/16	8.50	8.50	131.1	0.9020	9.00	29224.80	0.000 ¹ ✓
T6	91.6667 -	L2 1/2x2 1/2x3/16	8.83	8.83	136.2	0.9020	8.58	29224.80	0.000 ¹ ✓

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u lb	φP _n lb	Ratio P _u / φP _n
	83.3333								✓
T7	83.3333 - 75	L2 1/2x2 1/2x3/16	9.17	9.17	141.4	0.9020	7.19	29224.80	0.000 ¹ ✓
T8	75 - 50	L2 1/2x2 1/2x3/16	9.50	9.50	146.5	0.9020	6.75	29224.80	0.000 ¹ ✓
T9	50 - 37.5	L3x3x1/4	10.50	10.50	135.5	1.4400	5.64	46656.00	0.000 ¹ ✓
T10	37.5 - 25	L3x3x1/4	11.00	11.00	141.9	1.4400	5.04	46656.00	0.000 ¹ ✓
T11	25 - 0	L3x3x1/4	12.00	12.00	154.8	1.4400	2.86	46656.00	0.000 ¹ ✓

¹ P_u / φP_n controls

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	φP _{allow} lb	% Capacity	Pass Fail
T1	180 - 175	Leg	HSS5x.25	1	-737.94	143130.00	1.1	Pass
		Leg	HSS5x.25	2	-156.30	143130.00	0.8	Pass
T2	175 - 150	Leg	HSS5x.25	3	-1420.10	143130.00	1.0	Pass
		Leg	HSS5x.25	16	-18196.10	121395.00	15.0	Pass
		Leg	HSS5x.25	17	-18567.60	121395.00	15.3	Pass
T3	150 - 125	Leg	HSS5x.25	18	-18157.00	121395.00	15.0	Pass
		Leg	HSS5x.25	55	-56771.40	121395.00	46.8	Pass
		Leg	HSS5x.25	56	-58044.70	121395.00	47.8	Pass
T4	125 - 100	Leg	HSS5x.25	57	-58249.10	121395.00	48.0	Pass
		Leg	HSS5x.25	94	-104437.00	121395.00	86.0	Pass
		Leg	HSS5x.25	95	-106217.00	121395.00	87.5	Pass
T5	100 - 91.6667	Leg	HSS5x.25	96	-106296.00	121395.00	87.6	Pass
		Leg	HSS5x.375	133	-121308.00	175270.00	69.2	Pass
		Leg	HSS5x.375	134	-123281.00	175270.00	70.3	Pass
T6	91.6667 - 83.3333	Leg	HSS5x.375	135	-123314.00	175270.00	70.4	Pass
		Leg	HSS5x.375	148	-138658.00	199288.00	69.6	Pass
		Leg	HSS5x.375	149	-140692.00	199288.00	70.6	Pass
T7	83.3333 - 75	Leg	HSS5x.375	150	-140692.00	199288.00	70.6	Pass
		Leg	HSS5x.375	163	-156229.00	199288.00	78.4	Pass
		Leg	HSS5x.375	164	-158754.00	199288.00	79.7	Pass
T8	75 - 50	Leg	HSS5x.375	165	-158334.00	199288.00	79.4	Pass
		Leg	HSS6.875x.375	178	-204148.00	266736.00	76.5	Pass
		Leg	HSS6.875x.375	179	-206994.00	266736.00	77.6	Pass
T9	50 - 37.5	Leg	HSS6.875x.375	180	-206475.00	266736.00	77.4	Pass
		Leg	HSS6.875x.5	205	-234114.00	344700.00	67.9	Pass
		Leg	HSS6.875x.5	206	-236966.00	344700.00	68.7	Pass
T10	37.5 - 25	Leg	HSS6.875x.5	207	-236413.00	344700.00	68.6	Pass
		Leg	HSS6.875x.5	220	-264504.00	344700.00	76.7	Pass
		Leg	HSS6.875x.5	221	-267503.00	344700.00	77.6	Pass
T11	25 - 0	Leg	HSS6.875x.5	222	-266914.00	344700.00	77.4	Pass
		Leg	HSS6.875x.5	235	-325896.00	459464.00	70.9	Pass
		Leg	HSS6.875x.5	236	-329136.00	459464.00	71.6	Pass
T1	180 - 175	Diagonal	2L2 1/2x2x3/16x3/8	7	-303.16	31902.60	1.0	Pass
		Diagonal	2L2 1/2x2x3/16x3/8	8	-314.27	31902.60	1.0	Pass

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Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	ϕP_{allow} lb	% Capacity	Pass Fail		
T2	175 - 150	Diagonal	2L2 1/2x2x3/16x3/8	9	-588.86	31902.60	1.8	Pass		
							2.3 (b)			
		Diagonal	2L2 1/2x2x3/16x3/8	10	-566.20	31902.60	1.8	Pass		
							2.4 (b)			
		Diagonal	2L2 1/2x2x3/16x3/8	11	-647.02	31902.60	2.0	Pass		
							2.8 (b)			
		Diagonal	2L2 1/2x2x3/16x3/8	12	-666.11	31902.60	2.1	Pass		
							2.8 (b)			
		Diagonal	2L2 1/2x2x3/16x3/8	20	-9288.38	16563.10	56.1	Pass		
		Diagonal	2L2 1/2x2x3/16x3/8	21	-9297.80	16563.10	56.1	Pass		
		Diagonal	2L2 1/2x2x3/16x3/8	23	-6335.69	16563.10	38.3	Pass		
		Diagonal	2L2 1/2x2x3/16x3/8	24	-6590.19	16563.10	39.8	Pass		
		Diagonal	2L2 1/2x2x3/16x3/8	26	-6462.83	16563.10	39.0	Pass		
		Diagonal	2L2 1/2x2x3/16x3/8	27	-6198.82	16563.10	37.4	Pass		
		Diagonal	2L2 1/2x2x3/16x3/8	32	-9602.06	17204.40	55.8	Pass		
		Diagonal	2L2 1/2x2x3/16x3/8	33	-9623.08	17204.40	55.9	Pass		
		Diagonal	2L2 1/2x2x3/16x3/8	35	-6349.71	17204.40	36.9	Pass		
		Diagonal	2L2 1/2x2x3/16x3/8	36	-6530.89	17204.40	38.0	Pass		
		T3	150 - 125	Diagonal	2L2 1/2x2x3/16x3/8	38	-6544.07	17204.40	38.0	Pass
				Diagonal	2L2 1/2x2x3/16x3/8	39	-6341.87	17204.40	36.9	Pass
Diagonal	2L2 1/2x2x3/16x3/8			44	-5498.06	17858.70	30.8	Pass		
Diagonal	2L2 1/2x2x3/16x3/8			45	-5512.78	17858.70	30.9	Pass		
Diagonal	2L2 1/2x2x3/16x3/8			47	-4288.32	17858.70	24.0	Pass		
Diagonal	2L2 1/2x2x3/16x3/8			48	-4376.90	17858.70	24.5	Pass		
Diagonal	2L2 1/2x2x3/16x3/8			50	-3500.42	17858.70	19.6	Pass		
Diagonal	2L2 1/2x2x3/16x3/8			51	-3397.10	17858.70	19.0	Pass		
Diagonal	2L3x2 1/2x1/4x3/8			59	-13278.90	35690.50	37.2	Pass		
							48.1 (b)			
Diagonal	2L3x2 1/2x1/4x3/8			60	-13291.40	35690.50	37.2	Pass		
							48.1 (b)			
Diagonal	2L3x2 1/2x1/4x3/8			62	-10342.20	35690.50	29.0	Pass		
							37.3 (b)			
Diagonal	2L3x2 1/2x1/4x3/8			63	-10349.30	35690.50	29.0	Pass		
							37.2 (b)			
Diagonal	2L3x2 1/2x1/4x3/8			65	-10675.30	35690.50	29.9	Pass		
							38.4 (b)			
Diagonal	2L3x2 1/2x1/4x3/8			66	-10655.70	35690.50	29.9	Pass		
							38.5 (b)			
Diagonal	2L3x2 1/2x1/4x3/8	71	-12621.00	37104.10	34.0	Pass				
					45.7 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	72	-12634.50	37104.10	34.1	Pass				
					45.7 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	74	-9477.20	37104.10	25.5	Pass				
					34.2 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	75	-9495.93	37104.10	25.6	Pass				
					34.1 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	77	-9825.92	37104.10	26.5	Pass				
					35.1 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	78	-9734.92	37104.10	26.2	Pass				
					35.3 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	83	-11786.60	38560.40	30.6	Pass				
					42.7 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	84	-11799.60	38560.40	30.6	Pass				
					42.7 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	86	-8375.39	38560.40	21.7	Pass				
					30.5 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	87	-8498.08	38560.40	22.0	Pass				
					30.1 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	89	-8819.43	38560.40	22.9	Pass				
					30.6 (b)					
Diagonal	2L3x2 1/2x1/4x3/8	90	-8521.23	38560.40	22.1	Pass				

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Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	ϕP_{allow} lb	% Capacity	Pass Fail
T4	125 - 100	Diagonal	2L3x2 1/2x1/4x3/8	98	-15356.10	31623.00	31.7 (b) 48.6	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	99	-15374.00	31623.00	55.7 (b) 48.6	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	101	-11597.10	31623.00	55.6 (b) 36.7	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	102	-11614.00	31623.00	41.8 (b) 36.7	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	104	-12439.90	31623.00	41.7 (b) 39.3	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	105	-12405.10	31623.00	44.7 (b) 39.2	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	110	-14719.50	32890.90	44.8 53.4 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	111	-14739.00	32890.90	44.8 53.3 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	113	-11087.90	32890.90	33.7 40.0 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	114	-11101.80	32890.90	33.8 39.9 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	116	-11922.70	32890.90	36.2 42.9 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	117	-11889.30	32890.90	36.1 43.0 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	122	-13716.00	34206.30	40.1 49.7 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	123	-13725.70	34206.30	40.1 49.7 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	125	-10699.50	34206.30	31.3 38.6 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	126	-10711.00	34206.30	31.3 38.5 (b)	Pass
		T5	100 - 91.6667	Diagonal	2L3x2 1/2x1/4x3/8	128	-10971.70	34206.30
Diagonal	2L3x2 1/2x1/4x3/8			129	-10950.50	34206.30	32.0 39.5 (b)	Pass
Diagonal	2L3x2 1/2x1/4x3/8			137	-15965.80	30376.70	52.6 57.8 (b)	Pass
Diagonal	2L3x2 1/2x1/4x3/8			138	-15980.50	30376.70	52.6 57.8 (b)	Pass
Diagonal	2L3x2 1/2x1/4x3/8			140	-12123.70	30376.70	39.9 43.6 (b)	Pass
Diagonal	2L3x2 1/2x1/4x3/8			141	-12144.30	30376.70	40.0 43.6 (b)	Pass
Diagonal	2L3x2 1/2x1/4x3/8			143	-12875.50	30376.70	42.4 46.2 (b)	Pass
T6	91.6667 - 83.3333	Diagonal	2L3x2 1/2x1/4x3/8	144	-12839.50	30376.70	42.3 46.3 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	152	-16444.30	29183.60	56.3 59.5 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	153	-16460.40	29183.60	56.4 59.5 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	155	-12446.40	29183.60	42.6 44.8 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	156	-12467.40	29183.60	42.7 44.7 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	158	-13457.90	29183.60	46.1 48.3 (b)	Pass
		Diagonal	2L3x2 1/2x1/4x3/8	159	-13410.00	29183.60	46.0 48.4 (b)	Pass

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Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	ϕP_{allow} lb	% Capacity	Pass Fail	
T7	83.3333 - 75	Diagonal	2L3x2 1/2x1/4x3/8	167	-18035.40	28042.30	64.3	Pass	
		Diagonal	2L3x2 1/2x1/4x3/8	168	-18047.10	28042.30	65.0 (b)	Pass	
		Diagonal	2L3x2 1/2x1/4x3/8	170	-13597.80	28042.30	64.9 (b)	Pass	
		Diagonal	2L3x2 1/2x1/4x3/8	171	-13628.80	28042.30	48.5	Pass	
		Diagonal	2L3x2 1/2x1/4x3/8	173	-14328.50	28042.30	48.6 (b)	Pass	
		Diagonal	2L3x2 1/2x1/4x3/8	174	-14208.30	28042.30	51.1	Pass	
								50.7	Pass
T8	75 - 50	Diagonal	2L3 1/2x3x3/8x3/8	182	-24663.50	42971.90	51.2 (b)	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	183	-24667.30	42971.90	57.4	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	185	-18797.00	42971.90	43.7	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	186	-18853.40	42971.90	43.9	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	188	-19278.50	42971.90	44.9	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	189	-19105.50	42971.90	44.5	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	194	-23936.50	44739.90	53.5	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	195	-23939.80	44739.90	53.5	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	197	-18230.40	44739.90	40.7	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	198	-18356.00	44739.90	41.0	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	200	-18344.30	44739.90	41.0	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	201	-18157.00	44739.90	40.6	Pass	
		T9	50 - 37.5	Diagonal	2L3 1/2x3x3/8x3/8	209	-25590.20	41201.20	62.1
Diagonal	2L3 1/2x3x3/8x3/8			210	-25598.60	41201.20	62.1	Pass	
Diagonal	2L3 1/2x3x3/8x3/8			212	-19387.80	41201.20	47.1	Pass	
Diagonal	2L3 1/2x3x3/8x3/8			213	-19440.50	41201.20	47.2	Pass	
Diagonal	2L3 1/2x3x3/8x3/8			215	-20224.40	41201.20	49.1	Pass	
Diagonal	2L3 1/2x3x3/8x3/8			216	-20015.70	41201.20	48.6	Pass	
T10	37.5 - 25	Diagonal	2L3 1/2x3x3/8x3/8	224	-26571.50	39503.20	67.3	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	225	-26580.00	39503.20	67.3	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	227	-20206.80	39503.20	51.2	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	228	-20259.30	39503.20	51.3	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	230	-21256.30	39503.20	53.8	Pass	
		Diagonal	2L3 1/2x3x3/8x3/8	231	-21074.20	39503.20	53.3	Pass	
T11	25 - 0	Diagonal	2L3x3 1/2x5/16x3/8	239	-29234.60	57793.70	50.6	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	242	-29256.20	57793.70	74.4 (b)	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	246	-22713.40	57793.70	50.6	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	249	-23184.60	57793.70	74.4 (b)	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	253	-24602.80	57793.70	39.3	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	256	-23870.00	57793.70	57.4 (b)	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	263	-28192.10	60138.30	40.1	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	266	-28218.20	60138.30	57.3 (b)	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	270	-21958.00	60138.30	42.6	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	273	-22542.70	60138.30	60.3 (b)	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	277	-23768.30	60138.30	41.3	Pass	
		Diagonal	2L3x3 1/2x5/16x3/8	280	-22936.70	60138.30	60.4 (b)	Pass	
								46.9	Pass
								71.6 (b)	Pass
T2	175 - 150	Horizontal	L3x3x1/4	19	-5621.16	28061.80	46.9	Pass	
		Horizontal	L3x3x1/4	22	-4068.59	28061.80	71.7 (b)	Pass	
							58.0 (b)	Pass	

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	62 of 65
	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	ϕP_{allow} lb	% Capacity	Pass Fail
		Horizontal	L3x3x1/4	25	-3966.90	28061.80	19.3 (b) 14.1	Pass
		Horizontal	L3x3x1/4	31	-5676.86	30647.90	18.8 (b) 18.5	Pass
		Horizontal	L3x3x1/4	34	-4330.01	30647.90	27.8 (b) 14.1	Pass
		Horizontal	L3x3x1/4	37	-4412.36	30647.90	20.8 (b) 14.4	Pass
		Horizontal	L3x3x1/4	43	-3401.41	33085.10	21.1 (b) 10.3	Pass
		Horizontal	L3x3x1/4	46	-3035.58	33085.10	16.6 (b) 9.2	Pass
		Horizontal	L3x3x1/4	49	-2605.50	33085.10	14.9 (b) 7.9	Pass
T3	150 - 125	Horizontal	L3x3x1/4	58	-8714.04	20717.20	12.7 (b) 42.1	Pass
		Horizontal	L3x3x1/4	61	-6876.68	20717.20	43.0 (b) 33.2	Pass
		Horizontal	L3x3x1/4	64	-7205.70	20717.20	33.5 (b) 34.8	Pass
		Horizontal	L3x3x1/4	70	-8073.39	22854.40	35.3 39.9 (b)	Pass
		Horizontal	L3x3x1/4	73	-6298.25	22854.40	27.6 29.9 (b)	Pass
		Horizontal	L3x3x1/4	76	-6583.30	22854.40	28.8 31.3 (b)	Pass
		Horizontal	L3x3x1/4	82	-7352.33	25340.20	29.0 36.0 (b)	Pass
		Horizontal	L3x3x1/4	85	-5795.25	25340.20	22.9 27.4 (b)	Pass
		Horizontal	L3x3x1/4	88	-6000.88	25340.20	23.7 28.4 (b)	Pass
T4	125 - 100	Horizontal	L3x3x1/4	97	-10760.80	15837.90	67.9	Pass
		Horizontal	L3x3x1/4	100	-8209.63	15837.90	51.8	Pass
		Horizontal	L3x3x1/4	103	-8936.50	15837.90	56.4	Pass
		Horizontal	L3x3x1/4	109	-10116.00	17252.90	58.6	Pass
		Horizontal	L3x3x1/4	112	-7740.49	17252.90	44.9	Pass
		Horizontal	L3x3x1/4	115	-8438.76	17252.90	48.9	Pass
		Horizontal	L3x3x1/4	121	-9210.89	18866.30	48.8	Pass
		Horizontal	L3x3x1/4	124	-7221.07	18866.30	38.3	Pass
T5	100 - 91.6667	Horizontal	L3x3x1/4	127	-7502.28	18866.30	39.8	Pass
		Horizontal	L3x4x1/4	136	-11387.10	20706.20	55.0	Pass
		Horizontal	L3x4x1/4	139	-8737.16	20706.20	56.3 (b) 42.2	Pass
		Horizontal	L3x4x1/4	142	-9396.57	20706.20	45.4 42.7 (b)	Pass
T6	91.6667 - 83.3333	Horizontal	L3x4x1/4	151	-11924.90	19136.60	62.3	Pass
		Horizontal	L3x4x1/4	154	-9079.74	19136.60	47.4	Pass
		Horizontal	L3x4x1/4	157	-9961.54	19136.60	52.1	Pass
T7	83.3333 - 75	Horizontal	L3x4x1/2	166	-13258.10	32867.40	40.3	Pass
		Horizontal	L3x4x1/2	169	-10281.60	32867.40	31.3	Pass
		Horizontal	L3x4x1/2	172	-10863.50	32867.40	33.1	Pass
T8	75 - 50	Horizontal	L4x4x1/4	181	-15490.90	25829.50	60.0	Pass
		Horizontal	L4x4x1/4	184	-12176.20	25829.50	67.7 (b) 47.1	Pass
		Horizontal	L4x4x1/4	187	-12449.30	25829.50	51.6 (b) 48.2	Pass
		Horizontal	L4x4x1/4	193	-14583.30	28709.00	52.5 (b) 50.8	Pass
							63.9 (b)	

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	63 of 65
	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	ϕP_{allow} lb	% Capacity	Pass Fail
		Horizontal	L4x4x1/4	196	-11518.20	28709.00	40.1	Pass
		Horizontal	L4x4x1/4	199	-11508.00	28709.00	48.7 (b)	Pass
T9	50 - 37.5	Horizontal	L4x4x1/4	208	-16505.20	23362.50	40.1	Pass
							48.6 (b)	
							70.6	Pass
							72.1 (b)	
		Horizontal	L4x4x1/4	211	-12906.00	23362.50	55.2	Pass
T10	37.5 - 25	Horizontal	L4x4x1/4	214	-13430.60	23362.50	57.5	Pass
		Horizontal	L4x4x1/4	223	-17541.40	21232.70	82.6	Pass
		Horizontal	L4x4x1/4	226	-13576.10	21232.70	63.9	Pass
		Horizontal	L4x4x1/4	229	-14296.00	21232.70	67.3	Pass
T11	25 - 0	Horizontal	L4x4x1/2	238	-19693.90	33220.30	59.3	Pass
		Horizontal	L4x4x1/2	245	-15778.70	33220.30	47.5	Pass
		Horizontal	L4x4x1/2	252	-16778.80	33220.30	50.5	Pass
		Horizontal	L4x4x1/2	262	-18667.20	36248.90	51.5	Pass
							54.6 (b)	
		Horizontal	L4x4x1/2	269	-14572.60	36248.90	40.2	Pass
							42.2 (b)	
		Horizontal	L4x4x1/2	276	-15427.90	36248.90	42.6	Pass
							44.7 (b)	
T1	180 - 175	Top Girt	L3x3x1/4	4	-159.29	34476.00	0.5	Pass
		Top Girt	L3x3x1/4	5	-453.03	34476.00	1.3	Pass
		Top Girt	L3x3x1/4	6	-503.73	34476.00	1.5	Pass
T11	25 - 0	Redund Horz 1	L3x3x1/4	240	-5651.50	29975.50	18.9	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	243	-5707.70	29975.50	19.0	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	247	-5707.70	29975.50	19.0	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	250	-5697.64	29975.50	19.0	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	254	-5697.64	29975.50	19.0	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	257	-5651.50	29975.50	18.9	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	264	-5651.50	31847.00	17.7	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	267	-5707.70	31847.00	17.9	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	271	-5707.70	31847.00	17.9	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	274	-5697.64	31847.00	17.9	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	278	-5697.64	31847.00	17.9	Pass
		Bracing						
		Redund Horz 1	L3x3x1/4	281	-5651.50	31847.00	17.7	Pass
		Bracing						
T11	25 - 0	Redund Diag 1	L3x3x1/4	241	-4000.26	15399.40	26.0	Pass
		Bracing						
		Redund Diag 1	L3x3x1/4	244	-4040.04	15399.40	26.2	Pass
		Bracing						
		Redund Diag 1	L3x3x1/4	248	-4040.04	15399.40	26.2	Pass
		Bracing						
		Redund Diag 1	L3x3x1/4	251	-4032.91	15399.40	26.2	Pass
		Bracing						
		Redund Diag 1	L3x3x1/4	255	-4032.91	15399.40	26.2	Pass
		Bracing						
		Redund Diag 1	L3x3x1/4	258	-4000.26	15399.40	26.0	Pass
		Bracing						
		Redund Diag 1	L3x3x1/4	265	-4092.01	16057.80	25.5	Pass
		Bracing						

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	64 of 65
	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	ϕP_{allow} lb	% Capacity	Pass Fail
		Redund Diag 1 Bracing	L3x3x1/4	268	-4132.70	16057.80	25.7	Pass
		Redund Diag 1 Bracing	L3x3x1/4	272	-4132.70	16057.80	25.7	Pass
		Redund Diag 1 Bracing	L3x3x1/4	275	-4125.42	16057.80	25.7	Pass
		Redund Diag 1 Bracing	L3x3x1/4	279	-4125.42	16057.80	25.7	Pass
		Redund Diag 1 Bracing	L3x3x1/4	282	-4092.01	16057.80	25.5	Pass
T1	180 - 175	Inner Bracing	L2 1/2x2 1/2x3/16	13	-9.09	15638.70	0.3	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	14	-9.98	15638.70	0.3	Pass
T2	175 - 150	Inner Bracing	L2 1/2x2 1/2x3/16	15	-9.98	15638.70	0.3	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	28	-6.65	11551.80	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	29	-6.69	11551.80	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	30	-6.52	11551.80	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	40	-8.47	12909.80	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	41	-8.49	12909.80	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	42	-8.13	12909.80	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	52	-7.00	14522.00	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	53	-7.08	14522.00	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	54	-6.79	14522.00	0.4	Pass
T3	150 - 125	Inner Bracing	L2 1/2x2 1/2x3/16	67	-8.98	8552.99	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	68	-8.99	8552.99	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	69	-8.89	8552.99	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	79	-9.04	9407.78	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	80	-9.06	9407.78	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	81	-8.93	9407.78	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	91	-9.35	10397.40	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	92	-9.38	10397.40	0.4	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	93	-9.21	10397.40	0.4	Pass
T4	125 - 100	Inner Bracing	L2 1/2x2 1/2x3/16	106	-8.64	6586.62	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	107	-8.64	6586.62	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	108	-8.60	6586.62	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	118	-8.78	7159.11	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	119	-8.79	7159.11	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	120	-8.74	7159.11	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	130	-8.64	7809.62	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	131	-8.65	7809.62	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	132	-8.55	7809.62	0.5	Pass
T5	100 - 91.6667	Inner Bracing	L2 1/2x2 1/2x3/16	145	-13.80	6080.15	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	146	-13.81	6080.15	0.5	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	147	-13.73	6080.15	0.5	Pass
T6	91.6667 - 83.3333	Inner Bracing	L2 1/2x2 1/2x3/16	160	-13.52	5629.93	0.6	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	161	-13.53	5629.93	0.6	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	162	-13.46	5629.93	0.6	Pass
T7	83.3333 - 75	Inner Bracing	L2 1/2x2 1/2x3/16	175	-14.07	5227.92	0.6	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	176	-14.07	5227.92	0.6	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	177	-14.03	5227.92	0.6	Pass
T8	75 - 50	Inner Bracing	L2 1/2x2 1/2x3/16	190	-15.78	4392.91	0.6	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	191	-15.77	4392.91	0.6	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	192	-15.73	4392.91	0.6	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	202	-16.06	4867.49	0.6	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	203	-16.05	4867.49	0.6	Pass
		Inner Bracing	L2 1/2x2 1/2x3/16	204	-16.01	4867.49	0.6	Pass
T9	50 - 37.5	Inner Bracing	L3x3x1/4	217	-16.09	9098.35	0.5	Pass
		Inner Bracing	L3x3x1/4	218	-16.08	9098.35	0.5	Pass
		Inner Bracing	L3x3x1/4	219	-16.05	9098.35	0.5	Pass
T10	37.5 - 25	Inner Bracing	L3x3x1/4	232	-15.82	8290.02	0.6	Pass
		Inner Bracing	L3x3x1/4	233	-15.81	8290.02	0.6	Pass

tnxTower AECOM 1255 Broad St. Suite 201 Clifton, NJ 07013 Phone: (973) 883-8663 FAX: (973) 883-8500	Job	180' Stainless, Inc. Self Supporting Lattice	Page	65 of 65
	Project	97 Mountain Hill Road, Thompson, CT--CSP	Date	10:43:35 11/25/20
	Client	Eversource Phase (b.2) rev. 3	Designed by	christina.carlos

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	ϕP_{allow} lb	% Capacity	Pass Fail	
T11	25 - 0	Inner Bracing	L3x3x1/4	234	-15.79	8290.02	0.6	Pass	
		Inner Bracing	L3x3x1/4	259	-17.73	6965.92	0.6	Pass	
		Inner Bracing	L3x3x1/4	260	-17.64	6965.92	0.6	Pass	
		Inner Bracing	L3x3x1/4	261	-17.77	6965.92	0.6	Pass	
		Inner Bracing	L3x3x1/4	283	-17.45	7584.82	0.6	Pass	
		Inner Bracing	L3x3x1/4	284	-17.35	7584.82	0.6	Pass	
		Inner Bracing	L3x3x1/4	285	-17.49	7584.82	0.6	Pass	
							Summary		
							Leg (T4)	87.6	Pass
							Diagonal (T11)	74.4	Pass
							Horizontal (T10)	82.6	Pass
							Top Girt (T1)	1.5	Pass
							Redund Horz 1 Bracing (T11)	19.0	Pass
							Redund Diag 1 Bracing (T11)	26.2	Pass
							Inner Bracing (T8)	0.6	Pass
							Bolt Checks	76.9	Pass
							RATING =	87.6	Pass

Program Version 8.0.7.4 - 5/11/2020 File:C:/Users/christina.carlos/Desktop/tnxTower/Thompson, CT/Nov '20 - no T&S, with dish back on - MOD/tnxTower/_H_TNX - no leg change/180' Thompson (CSP Tower)_H_w. ES_worst case dish_MOD_re-added dish.eri

ANCHOR BOLT EVALUATION

ANCHOR BOLT ANALYSIS

Input Data

Tower Reactions:

Uplift:	Uplift := 313.641·kips	<i>user input</i>
Shear:	Shear := 45.184·kips	<i>user input</i>
Compression:	Compression := 362.710·kips	<i>user input</i>

Anchor Bolt Data:

Use ASTM A36 Actual material strength unknown, therefore assume minimum design values for anchor

Number of Anchor Bolts = N	$N := 6$	<i>user input</i>
Bolt Ultimate Strength:	$F_u := 58\text{-ksi}$	<i>user input</i>
Bolt Yield Strength:	$F_y := 36\text{-ksi}$	<i>user input</i>
Bolt Modulus:	$E := 29000\text{-ksi}$	<i>user input</i>
Thickness of Anchor Bolts	$D := 1.75\text{in}$	<i>user input</i>
Threads per Inch:	$n := 5$	<i>user input</i>
Coefficient of Friction:	$\mu := 0.55$	<i>user input</i> (for baseplate with grout ASCE 10-15)
Length from top of pier to bottom of leveling nut:	$L_{ar} := 0\text{in}$	<i>user input</i>
Bolt Modulus:	$E_{\text{WW}} := 29000\text{-ksi}$	<i>user input</i>

TIA-222-H 4.9.9 Calculate Equation Variables Strength Design:

Design Tensile Strength, R_{nt}:

$$R_{nt} := F_u \cdot A_n$$

$$R_{nt} = 110.17 \cdot \text{ft} \cdot \text{kip}$$

$$\phi_t \cdot R_{nt} = 82.63 \cdot \text{ft} \cdot \text{kip}$$

Design Compression Strength, R_{nc}:

$$R_{nc} := F_y \cdot A_g$$

$$R_{nc} = 86.59 \cdot \text{ft} \cdot \text{kip}$$

$$\phi_c \cdot R_{nc} = 77.93 \cdot \text{ft} \cdot \text{kip}$$

Design Shear Strength (Tension), R_{nv}:

$$R_{nv} := 0.5 \cdot F_u \cdot A_g$$

$$R_{nv} = 69.75 \cdot \text{ft} \cdot \text{kip}$$

$$\phi_v \cdot R_{nv} = 52.31 \cdot \text{ft} \cdot \text{kip}$$

Design Shear Strength (Compression), R_{nvc}:

$$R_{nvc} := 0.6 \cdot F_y \cdot 0.75 A_g$$

$$R_{nvc} = 38.97 \cdot \text{ft} \cdot \text{kip}$$

$$\phi_c \cdot R_{nvc} = 35.07 \cdot \text{ft} \cdot \text{kip}$$

NOTE: Per TIA-222-H The determination of capacity formulas are based on the existing constructed condition of exposed anchor rod from the top of the foundation to the bottom of the (base) leveling nut., Therefore the following equations next page), reflects for this tower site, the first formula shall be applied:

lar = 3" - 1.75" (nut height) = 1.25" < 1.75" Bolt Diameter

Job	<u>180' Stainless SST - Thompson, CT</u>	Project No.	<u>EVS-017 Rev. 3 (b.2)</u>	Sheet	<u>4</u>	of	<u>4</u>
Description	<u>Anchor Bolt Analysis (TIA-222-H)</u>	Computed by	<u>CMC</u>	Date	<u>11/25/20</u>		
	<u>Proposed Inventory - S. Analysis</u>	Checked by	<u> </u>	Date	<u> </u>		

TIA-222-H 4.9.9 Combined Shear and Tension:

$$\left[\frac{T_{ub}}{(\phi_t \cdot R_{nt})} \right]^2 + \left[\frac{V_{ub}}{(\phi_v \cdot R_{nv})} \right]^2 \leq 1$$

$$\left[\frac{T_{ub}}{(\phi_t \cdot R_{nt})} \right]^2 + \left(\frac{V_{ub}}{\phi_v \cdot R_{nv}} \right)^2 = 0.42$$

TIA-222-H 4.9.9 Combined Shear and Compression:

$$\left[\frac{P_{ucb}}{(\phi_c \cdot R_{nc})} \right] + \left(\frac{V_{ub}}{\phi_c \cdot R_{nvc}} \right)^2 \leq 1$$

$$\left[\frac{P_{ucb}}{(\phi_c \cdot R_{nc})} \right] + \left(\frac{V_{ub}}{\phi_c \cdot R_{nvc}} \right)^2 = 0.82$$

NOTE: Larger ratio number shown above Governs design Capacity.

Combined Shear and Tension/Compression Check:

$$\text{ShearAndTensionCheck} := \text{if} \left[\max \left[\left[\frac{V_{ub}}{(\phi_v \cdot R_{nv})} \right]^2 + \left[\frac{T_{ub}}{(\phi_t \cdot R_{nt})} \right]^2, \left[\frac{P_{ucb}}{(\phi_c \cdot R_{nc})} \right] + \left(\frac{V_{ub}}{\phi_c \cdot R_{nvc}} \right)^2 \right] \leq 1, \text{"OK"}, \text{"NO GOOD"} \right]$$

ShearAndTensionCheck = "OK"

FOUNDATION EVALUATION

Job 180' Stainless SST - Thompson, CT
 Description Foundation with Rock Anchors - TIA-222-H Check
Modification Analysis

Project No. EVS-017 Rev. 3 (b.2) Sheet 1 of 3
 Computed by CMC Date 11/25/20
 Checked by Date

ROCK ANCHORED FOUNDATION CHECK

INPUT DATA

Factored Max Pier Reactions:

Uplift: Uplift := 313.641 · kips
 Shear: Shear := 45.184 · kips
 Compression: Compression := 362.710 · kips

NOTE: Footing Dimensions/Depths obtained from original Construction Drawings (from Stainless, Inc.) Bearing Capacity and bonding strengths are obtained from Welti Geotechnical Report dated 3/26/2018.

Foundation Structure

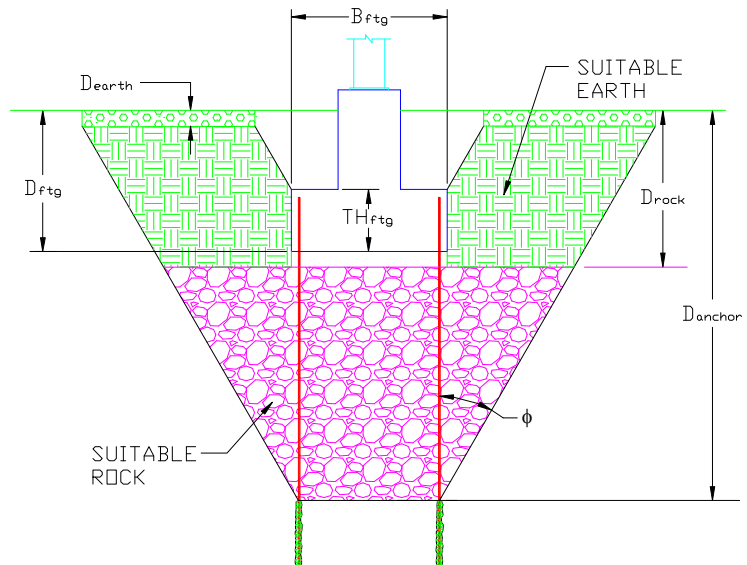
Footing Width: $B_{ftg} := 6\text{ft}$
 Footing Length: $L_{ftg} := 6\text{ft}$
 Footing Thickness: $TH_{ftg} := 2.5\text{ft}$

Depths:

Depth to Bottom of Footing: $D_{ftg} := 4.75\text{ft}$
 (from grade line)
 Depth to Suitable Rock: $D_{rock} := 3.5\text{ft}$
 (from grade line)
 Depth to Suitable Earth: $D_{earth} := 1\text{ft}$
 (from grade line)
 Anchor Depth: $D_{anchor} := 21.75\text{ft}$

Soil Properties:

Internal Friction Angle: $\phi := 30\text{deg}$
 Unit Weight of Earth: $\gamma_{earth} := 120 \frac{\text{lb}}{\text{ft}^3}$
 Unit Weight of Rock: $\gamma_{rock} := 165 \frac{\text{lb}}{\text{ft}^3}$
 Allowable Bearing: Bearing := 20000 · psf
 Ultimate Bearing: $U_{Bearing} := 2 \cdot \text{Bearing}$



KM Concrete Slab DL --> 52 cy / 3 piers applied within "DL.foot"

$$DL_{foot} := 0.90 \left[\left(B_{ftg} \cdot L_{ftg} \cdot TH_{ftg} \right) + \left[\frac{\pi}{4} \cdot (3\text{ft})^2 \cdot 3.25\text{ft} \right] \cdot 0.150 \frac{\text{kips}}{\text{ft}^3} + \left[\frac{52\text{yd}^3}{3} \cdot \left(0.1500 \frac{\text{kips}}{\text{ft}^3} \right) \right] \right] \quad DL_{foot} = 78431.34 \cdot \text{lb}$$

$DL_{Soil} := 0\text{lb}$ *NOTE: "0" APPLIED DUE TO REMOVAL OF SOIL PER KM MODIFICATION DESIGN 2017. CONCRETE DL CONSIDERED*

Job	<u>180' Stainless SST - Thompson, CT</u>	Project No.	<u>EVS-017 Rev. 3 (b.2)</u>	Sheet	<u>2</u> of <u>3</u>
Description	<u>Foundation with Rock Anchors - TIA-222-H Check Modification Analysis</u>	Computed by	<u>CMC</u>	Date	<u>11/25/20</u>
		Checked by	<u> </u>	Date	<u> </u>

Anchors:

Number of Anchors (along width):	NW _{anchor} := 2	Number of Anchors (along length):	NL _{anchor} := 2
Anchor Spacing* (along width):	SW _{anchor} := 3ft	Anchor Spacing* (along length):	SL _{anchor} := 3ft
Hole Diameter:	hole _d := 3in	Ultimate Bond Stress:	σ _{bond} := 100·psi·2.0

Value obtained from Weli(geotech) via e-mail dated April 5, 2018.

Ultimate Bond Stress:

$$P_{design} := \frac{Uplift - [0.9 \cdot (DL_{foot} + DL_{Soil})]}{NW_{anchor} + NL_{anchor}} \quad \sigma_{Work.bond} := \frac{\sigma_{bond}}{2}$$

P_{design} = 60.76·kips

CALCULATE RESISTANCE

Intermediate Dimensions:

Suitable Earth Height:	$H := D_{rock} - D_{earth}$	H = 2.50 ft
Suitable Rock Height:	$Z := D_{anchor} - D_{earth} - D_{rock}$	Z = 17.25 ft
Total Anchor Width:	$W := (NW_{anchor} - 1) \cdot SW_{anchor}$	W = 3.00 ft
Total Anchor Length:	$L := (NL_{anchor} - 1) \cdot SL_{anchor}$	L = 3.00 ft
Earth Above Footing:	$PD := D_{ftg} - TH_{ftg} - 2.25ft$	PD = 0.00 ft

Volumes:

Gross Volume:

$$GV_1 := W \cdot L \cdot (Z + H) \quad GV_1 = 177.75 \cdot ft^3$$

$$GV_2 := \left[\frac{1}{2} \cdot (Z + H) \cdot \tan(\phi) \cdot (Z + H) \right] \cdot (W + L) \cdot 2 \quad GV_2 = 1351.22 \cdot ft^3$$

$$GV_3 := \frac{1}{3} \cdot \pi \cdot [(Z + H) \cdot \tan(\phi)]^2 \cdot (Z + H) \quad GV_3 = 2689.11 \cdot ft^3$$

$$GV := GV_1 + GV_2 + GV_3 \quad GV = 4218.08 \cdot ft^3$$

Rock Volume:

$$RV_1 := W \cdot L \cdot (Z) \quad RV_1 = 155.25 \cdot ft^3$$

$$RV_2 := \left[\frac{1}{2} \cdot (Z) \cdot \tan(\phi) \cdot (Z) \right] \cdot (W + L) \cdot 2 \quad RV_2 = 1030.79 \cdot ft^3$$

$$RV_3 := \frac{1}{3} \cdot \pi \cdot [(Z) \cdot \tan(\phi)]^2 \cdot (Z) \quad RV_3 = 1791.74 \cdot ft^3$$

$$RV := RV_1 + RV_2 + RV_3 \quad RV = 2977.78 \cdot ft^3$$

Volume of Soil between KM Modification Slab:

NOTE: **Conservatively,** consider NO soil uplift resistance within these calculations, therefore, the value of "EV" = 0

Job 180' Stainless SST - Thompson, CT Project No. EVS-017 Rev.3 (b.2) Sheet 3 of 3
 Description Foundation with Rock Anchors - TIA-222-H Check Computed by CMC Date 11/25/20
Modification Analysis Checked by Date

Resisting Forces:

Resisting Rock Force: $F_{rock} := RV \cdot \gamma_{rock}$ $F_{rock} = 491.33 \cdot \text{kips}$

Resisting Earth Force: $F_{earth} := 0 \text{kips}$ $F_{earth} = 0.00 \cdot \text{kips}$

Resisting Concrete Force: $F_{conc} := DL_{foot}$ $F_{conc} = 78.43 \cdot \text{kips}$

NOTE: "0.9" is TIA-222-H Reducing factor for uplift resistance (LC2)

Total Resisting Force: $F_{total} := (F_{rock} + F_{earth} + F_{conc}) \cdot 0.9$ $F_{total} = 512.79 \cdot \text{kips}$

Check Uplift:

Condition1 := if $\left(\frac{\text{Uplift}}{F_{total} \cdot 0.75} \leq 1.00, "OK", "Overstressed" \right)$ $\frac{\text{Uplift}}{F_{total} \cdot 0.75} = 0.82$ Condition1 = "OK"

Embedment Length:

$L_b := \frac{P_{design}}{\pi \cdot \text{hole}_d \cdot \sigma_{Work.bond} \cdot 0.60}$ $L_b = 8.95 \text{ ft}$

NOTE: "0.60" reduction factor from TIA-222-H for uplift resistance for Rock Anchor

Condition2 := if $\left(\frac{Z}{L_b} \geq 1.00, "OK", "Overstressed" \right)$ $\frac{Z}{L_b} = 1.93$ Condition2 = "OK"

$\left(\frac{Z}{L_b} \right)^{-1} = 0.52$

Check Bearing:

MaxBearing := $\frac{\text{Compression} + 1.2 \cdot DL_{foot}}{B_{ftg} \cdot L_{ftg}}$

Condition3 := if $\left(\frac{\text{MaxBearing}}{U_{Bearing} \cdot 0.75} \leq 1.00, "OK", "Overstressed" \right)$

NOTE: "0.75" is TIA-222-H Reducing factor for bearing resistance

MaxBearing = 12689.66 psf

$U_{Bearing} \cdot 0.75 = 30000.00 \cdot \text{psf}$

$\frac{\text{MaxBearing}}{U_{Bearing} \cdot 0.75} = 0.4230$

Condition3 = "OK"

About AECOM

AECOM (NYSE: ACM) is a global provider of professional technical and management support services to a broad range of markets, including transportation, facilities, environmental, energy, water and government. With approximately 45,000 employees around the world, AECOM is a leader in all of the key markets that it serves. AECOM provides a blend of global reach, local knowledge, innovation, and collaborative technical excellence in delivering solutions that enhance and sustain the world's built, natural, and social environments. A Fortune 500 company, AECOM serves clients in more than 100 countries and has annual revenue in excess of \$6 billion.

More information on AECOM and its services can be found at www.aecom.com.

ATTACHMENT F – PROOF OF DELIVERY OF NOTICE

Ref: ES-051 THOMPSON Date: 27Jan21
Dep: BL GRAPHICS Wgt: 1.65 LBS
DV: 0.00

SHIPPING: 0.00
SPECIAL: 0.00
HANDLING: 0.00
TOTAL: 0.00

Svcs: PRIORITY OVERNIGHT
TRCK: 9544 9955 4440

ORIGIN ID:RSPA (800) 301-3077

BL COMPANIES
355 RESEARCH PARKWAY

MERIDEN, CT 06450
UNITED STATES US

SHIP DATE: 27JAN21
ACTWGT: 1.65 LB
CAD: 0765627/CAFE3407

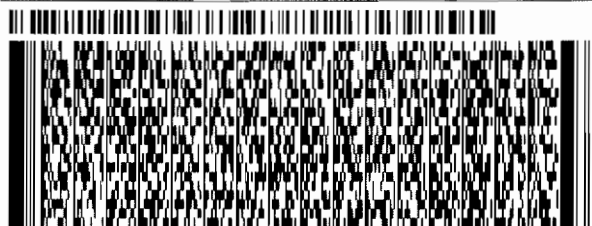
BILL THIRD PARTY

TO HONORABLE AMY ST, ONGE
TOWN OF THOMPSON
815 RIVERSIDE DRIVE

NORTH GROSVENORDALE CT 06255

REF: ES-051 THOMPSON

DEPT: BL GRAPHICS



FedEx
Express



J201019110601W

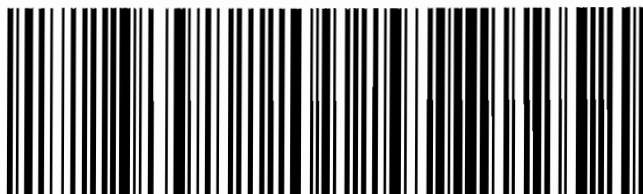
TRK# 9544 9955 4440
0201

THU - 28 JAN 4:30P
PRIORITY OVERNIGHT

EM FICA

06255
CT-US BOS

Part # 156148-034 RIT EXP 09/21



56DC1/1136/0542

Ref: ES-051 THOMPSON Date: 27Jan21
Dep: BL GRAPHICS Wgt: 1.65 LBS
DV:

SHIPPING: 0.00
SPECIAL: 0.00
HANDLING: 0.00
TOTAL: 0.00

Svcs: PRIORITY OVERNIGHT
TRCN: 9544 9955 4450

ORIGIN ID:RSPA (800) 301-3077

BL COMPANIES
355 RESEARCH PARKWAY

MERIDEN, CT 06450
UNITED STATES US

SHIP DATE: 27JAN21
ACTWGT: 1.65 LB MAN
CAD: 0765627/CAFE3407

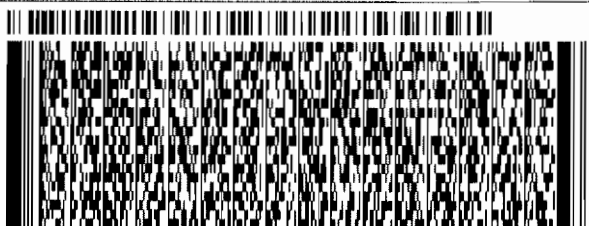
BILL THIRD PARTY

TO TYRA PENN - GESEK
TOWN OF THOMPSON
815 RIVERSIDE DRIVE

NORTH GROSVENORDALE CT 06255

REF: ES-051 THOMPSON

DEPT: BL GRAPHICS



FedEx
Express



J201019110601uv

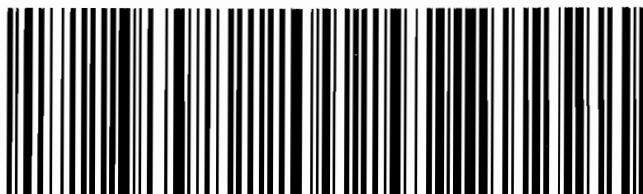
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0201

THU - 28 JAN 4:30P
PRIORITY OVERNIGHT

EM FICA

06255
CT - US BOS

Part # 156148-494 RIT EXP 09/21 ee



568C1/1136/0562

Ref: ES-051 THOMPSON Date: 27Jan21
Dep: BL GRAPHICS Wgt: 1.65 LBS
DV:

SHIPPING: 0.00
SPECIAL: 0.00
HANDLING: 0.00
TOTAL: 0.00

Svcs: PRIORITY OVERNIGHT
TRCK: 9544 9955 4461

ORIGIN ID:RSPA (800) 301-3077

BL COMPANIES
355 RESEARCH PARKWAY

MERIDEN, CT 06450
UNITED STATES US

SHIP DATE: 27JAN21
ACTWGT: 1.65 LB MAN
CAD: 0765627/CAFE3407

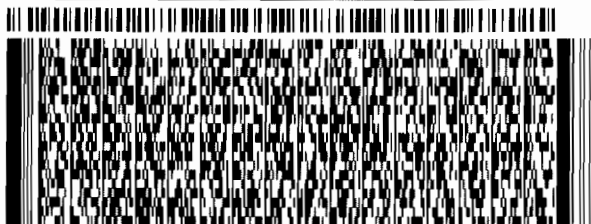
BILL THIRD PARTY

TO **BRIAN BENITO**
DEPT OF EMERGENCY SERVICES
1111 COUNTRY CLUB ROAD

MIDDLETOWN CT 06457

REF: ES-051 THOMPSON

DEPT: BL GRAPHICS



FedEx
Express



J2010191106010Y

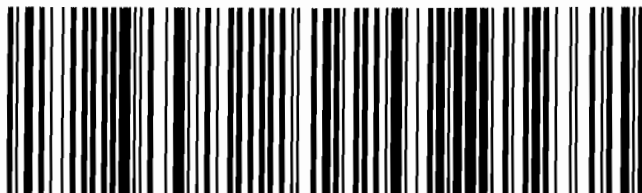
TRK# 9544 9955 4461
0201

THU - 28 JAN 10:30A
PRIORITY OVERNIGHT

00 BDLA

06457
CT-US BDL

Part # 155148-434 RIT EXP 09/21



56DC1/1136/05A2

Ref: ES-051 THOMPSON Date: 27Jan21
Dep: BL GRAPHICS Wgt: 1.65 LBS
DV:

SHIPPING: 0.00
SPECIAL: 0.00
HANDLING: 0.00
TOTAL: 0.00

Svcs: PRIORITY OVERNIGHT
TRCK: 9544 9955 4472

ORIGIN ID:RSPA (800) 301-3077

BL COMPANIES
355 RESEARCH PARKWAY

MERIDEN, CT 06450
UNITED STATES US

SHIP DATE: 27JAN21
ACTWGT: 1.65 LB MAN
CAD: 0765627/CAFE3407

BILL THIRD PARTY

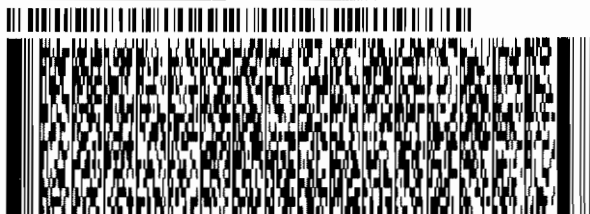
TO

CONNECTICUT SITING COUNCIL
10 FRANKLIN SQUARE

NEW BRITAIN CT 06051

REF: ES-051 THOMPSON

DEPT: BL GRAPHICS



FedEx
Express



56DC1/1136/05A2

J201019110601uy

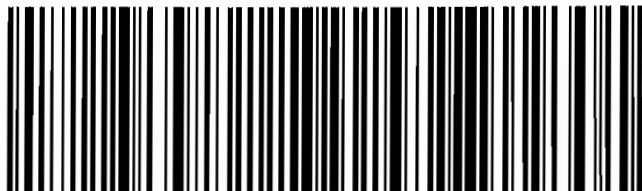
TRK# 9544 9955 4472
0201

THU - 28 JAN 10:30A
PRIORITY OVERNIGHT

00 BDLA

06051
CT-US BDL

Part # 155148-434 PUT EXP 03/21 ep



ATTACHMENT G - POWER DENSITY REPORT



C Squared Systems, LLC
65 Dartmouth Drive
Auburn, NH 03032
603-644-2800
support@csquaredsystems.com

Calculated Radio Frequency Emissions Report



ES-051

97 Mountain Hill Road

Thompson, CT 06255

December 18, 2020

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1. Introduction

The purpose of this report is to investigate compliance with applicable FCC regulations for the proposed Eversource installation on the self-support tower at 97 Mountain Hill Road in Thompson, CT. Eversource is proposing to install two omnidirectional antennas – one transmit and one receive-only antenna – as part of its 220 MHz communications system.

This report considers the proposed antenna configuration as detailed by Eversource along with % MPE (Maximum Permissible Exposure) measurements of the existing tower to determine FCC compliance of the facility.



Figure 1: View of ES-051 Thompson

Site Address	97 Mountain Hill Road
Latitude	41° 59' 11.7" N
Longitude	71° 54' 49.1" W
Site Elevation AMSL	558'
Survey Engineer	Marc Salas
Survey Date/Time	6/16/2020; 9:00 AM – 9:45 AM

Table 1: Survey Information

2. FCC Guidelines for Evaluating RF Radiation Exposure Limits

In 1985, the FCC established rules to regulate radio frequency (RF) exposure from FCC licensed antenna facilities. In 1996, the FCC updated these rules, which were further amended in August 1997 by OET Bulletin 65 Edition 97-01. These new rules include Maximum Permissible Exposure (MPE) limits for transmitters operating between 300 kHz and 100 GHz. The FCC MPE limits are based upon those recommended by the National Council on Radiation Protection and Measurements (NCRP), developed by the Institute of Electrical and Electronics Engineers, Inc., (IEEE) and adopted by the American National Standards Institute (ANSI).

The FCC general population/uncontrolled limits set the maximum exposure to which most people may be subjected. General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

Public exposure to radio frequencies is regulated and enforced in units of milliwatts per square centimeter (mW/cm^2). The general population exposure limits for the various frequency ranges are defined in the attached “FCC Limits for Maximum Permissible Exposure (MPE)” in Attachment B of this report.

Higher exposure limits are permitted under the occupational/controlled exposure category, but only for persons who are exposed as a consequence of their employment and who have been made fully aware of the potential for exposure, and they must be able to exercise control over their exposure. General population/uncontrolled limits are five times more stringent than the levels that are acceptable for occupational, or radio frequency trained individuals. Attachment B contains excerpts from OET Bulletin 65 and defines the Maximum Exposure Limit.

Finally, it should be noted that the MPE limits adopted by the FCC for both general population/uncontrolled exposure and for occupational/controlled exposure incorporate a substantial margin of safety and have been established to be well below levels generally accepted as having the potential to cause adverse health effects.

3. Power Density Calculation Methods

The power density calculation results were generated using the following formula as outlined in FCC bulletin OET 65, and Connecticut Siting Council recommendations:

$$\text{Power Density} = \left(\frac{1.6^2 \times 1.64 \times \text{ERP}}{4\pi \times R^2} \right) \times \text{Off Beam Loss}$$

Where:

EIRP = Effective Isotropic Radiated Power = 1.64 x ERP

R = Radial Distance = $\sqrt{H^2 + V^2}$

H = Horizontal Distance from antenna

V = Vertical Distance from radiation center of antenna

Ground reflection factor of 1.6

Off Beam Loss is determined by the selected antenna pattern

These calculations assume that the antennas are operating at 100 percent capacity and full power, and that all antenna channels are transmitting simultaneously. Obstructions (trees, buildings, etc.) that would normally attenuate the signal are not taken into account. The calculations assume even terrain in the area of study and do not consider actual terrain elevations which could attenuate the signal. As a result, the calculated power density and corresponding % MPE levels reported below are much higher than the actual levels will be from the final installation.

4. Proposed Antenna Configuration

Table 2 below lists the technical details of the proposed Eversource installation. These parameters are applied to the above calculation methods in order to calculate the % MPE values of the proposed equipment. Any proposed receive-only antennas have not been included in the table as they are irrelevant in terms of the % MPE calculations.

Operator	Antenna Model	TX Freq. (MHz)	Ant Gain (dBd)	Power ERP (Watts)	Number of Channels	Vertical Beamwidth	Length (ft)	Antenna Centerline Height (ft)
Eversource	Telewave ANT220F2	217	2.5	124	4	38°	4.25	134

Table 2: Eversource Antenna Configuration (Proposed)^{1 2}

¹ Transmit power assumes 0 dB of cable loss.

² Antenna height listed for the proposed antenna is based on the AECOM Structural Analysis Report dated November 25, 2020 (Rev. 3).

5. Measurement Procedure

Frequencies from 300 KHz to 50 GHz were measured using the Narda Probe EA 5091, E-Field, shaped, FCC probe in conjunction with the NBM550 survey meter. The EA 5091 probe is “shaped” such that in a mixed signal environment (i.e.: more than one frequency band is used in a particular location), it accurately measures the percent of MPE.

From FCC OET Bulletin No. 65 - Edition 97-01 – “A useful characteristic of broadband probes used in multiple-frequency RF environments is a frequency-dependent response that corresponds to the variation in MPE limits with frequency. Broadband probes having such a “shaped” response permit direct assessment of compliance at sites where RF fields result from antennas transmitting over a wide range of frequencies. Such probes can express the composite RF field as a percentage of the applicable MPEs”.

Probe Description - As suggested in FCC OET Bulletin No. 65 - Edition 97-01, the response of the measurement instrument should be essentially isotropic, (i.e., independent of orientation or rotation angle of the probe). For this reason, the Narda EA 5091 probe was used for these measurements.

Sampling Description - At each measurement location, a spatially averaged measurement is collected over the height of an average human body. The NBM550 survey meter performs a time average measurement while the user slowly moves the probe over a distance range of 20 cm to 200 cm (about 6 feet) above ground level. The results recorded at each measurement location include average values over the spatial distance.

Instrumentation Information - A summary of specifications for the equipment used is provided in the table below.

Manufacturer	Narda Microwave			
Probe	EA 5091, Serial# 01116			
Calibration Date	May 2020			
Calibration Interval	24 Months			
Meter	NBM550, Serial# E-1069			
Calibration Date	May 2020			
Calibration Interval	24 Months			
Probe Specifications	Frequency Range	Field Measured	Standard	Measurement Range
	300 KHz-50 GHz	Electric Field	U.S. FCC 1997 Occupational/Controlled	0.2 – 600 % of Standard

Table 3: Instrumentation Information

Instrument Measurement Uncertainty - The total measurement uncertainty of the NARDA measurement probe and meter is no greater than ± 3 dB (0.5% to 6%), ± 1 dB (6% to 100%), ± 2 dB (100% to 600%). The factors which contribute to this include the probe’s frequency response deviation, calibration uncertainty, ellipse ratio, and isotropic response³. Every effort is taken to reduce the overall uncertainty during measurement collection including pointing the probe directly at the likely highest source of emissions.

³ For further details, please refer to Narda Safety Test Solutions NBM550 Probe Specifications, pg. 64
http://www.narda-sts.us/pdf_files/DataSheets/NBM-Probes_DataSheet.pdf

6. Surveyed and Calculated % MPE Results

Measured and calculated results and a description of each survey location are detailed in the table below. Measurements were recorded on June 16, 2020 between 9:00 AM and 9:45 AM. The calculated % MPE contribution from the proposed equipment modifications was then added to the measured % MPE values in the “Composite % MPE” column. These calculated values incorporate the antenna pattern of the antenna model specified by Eversource to determine the “Off Beam Loss” factor shown in the power density formula from Section 3. All % MPE values are in reference to the FCC Uncontrolled/General Population exposure limit.

Table 4 below lists 11 measurements recorded in the vicinity of the tower. The highest spatially averaged measurement was 9.89% (Average Uncontrolled/General Population MPE) and was recorded at Location 10 near 66 Mountain Hill Road. The highest composite (measured + calculated) % MPE value is calculated to be 10.02% (Average Uncontrolled/General Population) and is also calculated to occur at Location 10.

Meas. Location	Location Description	Latitude	Longitude	Dist. From Site (feet)	Measured % MPE (Uncontrolled / General)	Calculated % MPE (Eversource Proposed)	Composite % MPE (Uncontrolled / General)
1	Western corner of fenced compound	41.98653	-71.91400	100	1.64%	0.02%	1.66%
2	Southwest side of fenced compound gate	41.98648	-71.91392	86	1.82%	0.04%	1.86%
3	Left of fenced compound gate	41.98645	-71.91384	76	2.14%	0.05%	2.20%
4	Fenced compound gate	41.98640	-71.91376	79	2.26%	0.05%	2.31%
5	Parking area in front of compound gate	41.98634	-71.91383	105	2.48%	0.02%	2.49%
6	Along access way to tower	41.98616	-71.91388	172	1.03%	0.22%	1.25%
7	Access road, split with private drive	41.98582	-71.91397	297	2.08%	0.37%	2.45%
8	Tower access road and Mountain Hill Road	41.98500	-71.91471	652	1.87%	0.17%	2.04%
9	Cul-de-sac at end of Mountain Hill Road	41.98529	-71.91526	650	7.22%	0.18%	7.40%
10	66 Mountain Hill Road	41.98458	-71.91423	755	9.89%	0.13%	10.02%
11	86 Mountain Hill Road	41.98419	-71.91360	878	9.58%	0.10%	9.67%

Table 4: Measured and Calculated % MPE Results ^{4 5}

⁴ Due to measurement uncertainty at low levels (See Table 3), any readings outside the measurement range of the probe (< 1.00 % FCC General Population/Uncontrolled MPE) are noted as such.

⁵ Measured and calculated % MPE values listed are rounded to two decimal points and the composite % MPE listed is a summation of each unrounded contribution. Therefore, summing each rounded value may not identically match the total composite values reflected in the table.

Figures 2 and 3 below are aerial views of the tower location and the surrounding area, along with the measurement locations listed in Table 4.



Figure 2: Measurement Points – Zoom In



Figure 3: All Measurement Points

7. Conclusion

A number of accessible areas around the tower at 97 Mountain Hill Road in Thompson, CT were surveyed and found to be well within the mandated General Population/Uncontrolled limits for Maximum Permissible Exposure, as delineated in the Federal Communications Commission's Radio Frequency exposure rules published in 47 CFR 1.1307(b)(1)-(b)(3).

The highest spatially averaged % MPE measurement of all surveyed points based on the 1997 FCC standard for exposure to the general population is 9.89% MPE. This measurement was recorded at Location 10, near 66 Mountain Hill Road.

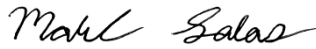
The highest composite (measured + calculated) power density is **10.02% of the FCC General Population MPE limit** with the proposed Eversource equipment and is also calculated to occur at Location 10.

The above analysis concludes that RF exposure at ground level around the tower, both currently and with the proposed antenna installation, will be below the maximum power density limits as outlined by the FCC in the OET Bulletin 65 Ed. 97-01.

As noted previously, the calculated % MPE levels are more conservative (higher) than the actual levels will be from the finished installation.

8. Statement of Certification


I certify to the best of my knowledge that the statements in this report are true and accurate. The calculations follow guidelines set forth in FCC OET Bulletin 65 Edition 97-01, IEEE Std. C95.1, and IEEE Std. C95.3.



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C Squared Systems, LLC

December 18~~+~~, 2020

Date



Reviewed/Approved By: Keith Vellante
Director of RF Services
C Squared Systems, LLC

December ~~023~~21, 2020

Date

Attachment A: References

OET Bulletin 65 - Edition 97-01 - August 1997 Federal Communications Commission Office of Engineering & Technology

IEEE C95.1-2005, IEEE Standard Safety Levels With Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz IEEE-SA Standards Board

IEEE C95.3-2002 (R2008), IEEE Recommended Practice for Measurements and Computations of Radio Frequency Electromagnetic Fields With Respect to Human Exposure to Such Fields, 100 kHz-300 GHz IEEE-SA Standards Board

Attachment B: FCC Limits for Maximum Permissible Exposure (MPE)

(A) Limits for Occupational/Controlled Exposure⁶

Frequency Range (MHz)	Electric Field Strength (E) (V/m)	Magnetic Field Strength (E) (A/m)	Power Density (S) (mW/cm ²)	Averaging Time E ² , H ² or S (minutes)
0.3-3.0	614	1.63	(100)*	6
3.0-30	1842/f	4.89/f	(900/f ²)*	6
30-300	61.4	0.163	1.0	6
300-1500	-	-	f/300	6
1500-100,000	-	-	5	6

(B) Limits for General Population/Uncontrolled Exposure⁷

Frequency Range (MHz)	Electric Field Strength (E) (V/m)	Magnetic Field Strength (E) (A/m)	Power Density (S) (mW/cm ²)	Averaging Time E ² , H ² or S (minutes)
0.3-1.34	614	1.63	(100)*	30
1.34-30	824/f	2.19/f	(180/f ²)*	30
30-300	27.5	0.073	0.2	30
300-1500	-	-	f/1500	30
1500-100,000	-	-	1.0	30

f = frequency in MHz * Plane-wave equivalent power density

Table 5: FCC Limits for Maximum Permissible Exposure (MPE)

⁶ Occupational/controlled limits apply in situations in which persons are exposed as a consequence of their employment provided those persons are fully aware of the potential for exposure and can exercise control over their exposure. Limits for occupational/controlled exposure also apply in situations when an individual is transient through a location where occupational/controlled limits apply provided he or she is made aware of the potential for exposure

⁷ General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure

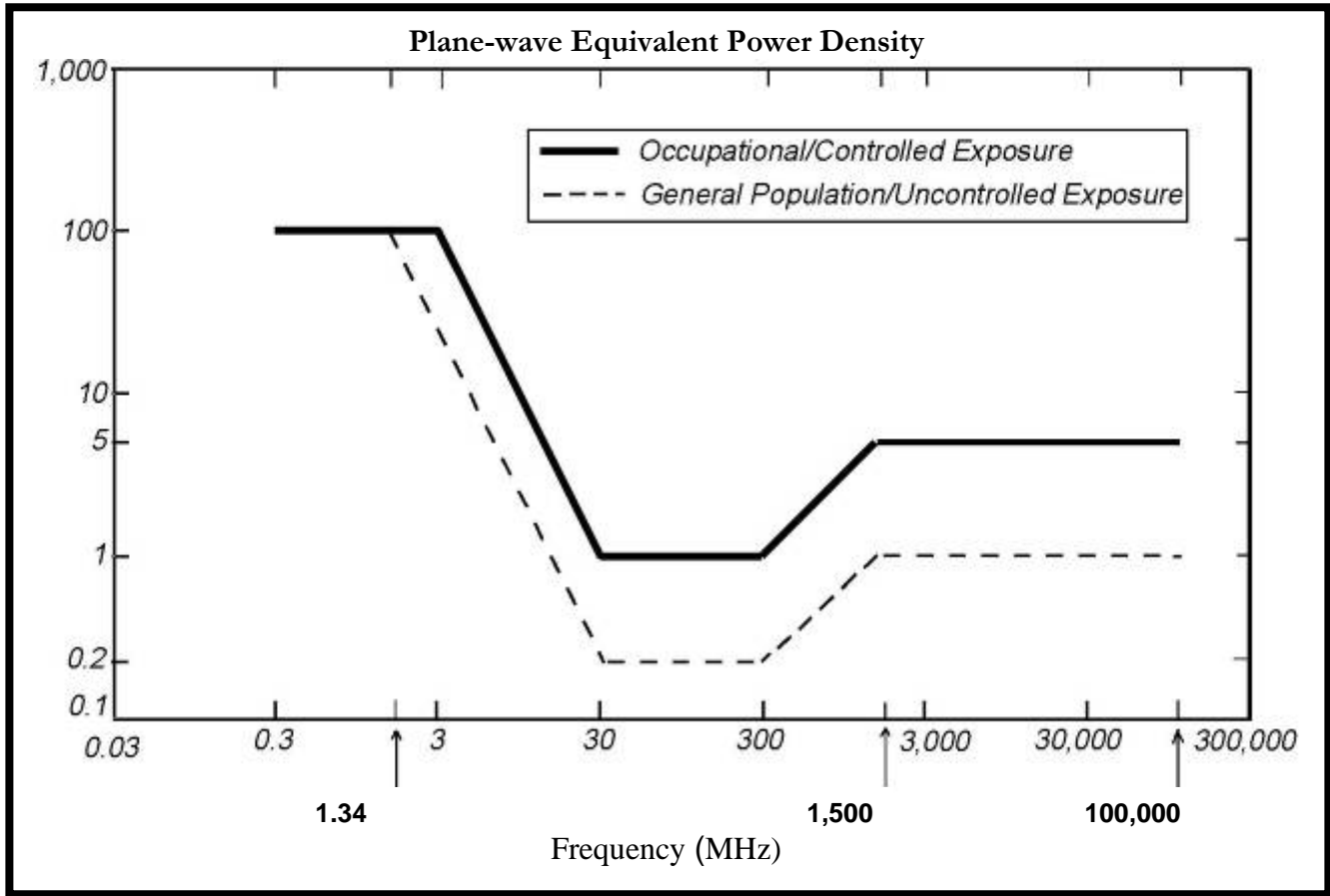
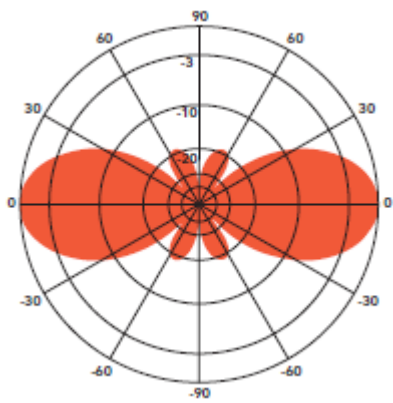


Figure 4: Graph of FCC Limits for Maximum Permissible Exposure (MPE)

Attachment C: Eversource Antenna Data Sheet and Electrical Patterns

<p>217 MHz</p> <p>Manufacturer: Telewave Model #: ANT220F2 Frequency Band: 195-260 MHz Gain: 2.5 dBd Vertical Beamwidth: 38° Horizontal Beamwidth: 360° Polarization: Vertical-Polarization Length: 4.25'</p>	 <p>The diagram is a polar plot of an antenna radiation pattern. The vertical axis represents the elevation angle, with 0 degrees at the top and 90 degrees at the bottom. The horizontal axis represents the azimuth angle, with 0, 30, 60, and 90 degrees marked. The plot shows a central lobe at 0 degrees, with two side lobes extending to approximately +/- 30 degrees. The main lobe is shaded in red, and the side lobes are also shaded in red. The plot is overlaid on a grid of concentric circles and radial lines.</p>
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