CC CROWN CASTLE

Crown Castle 3 Corporate Park Drive, Suite 101 Clifton Park, NY 12065

June 26, 2020

Melanie A. Bachman Acting Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

RE: Notice of Exempt Modification for T-Mobile: 823530 - T-Mobile Site ID: CT11364B 580 Chapel Street, Thomaston, CT 06787 Latitude: 41° 39' 48.48" / Longitude: -73° 4' 27.41"

Dear Ms. Bachman:

T-Mobile currently maintains six (6) antennas at the 172-foot mount on the existing 175-foot Monopole Tower, located at 580 Chapel Street, Thomaston, CT. The tower is owned by Crown Castle and the property is owned by the Town of Thomaston. T-Mobile now intends to replace three (3) existing antennas with three (3) new 600/700/1900/2100 MHz antennas. The new antennas will be installed at the 172-ft level of the tower.

Planned Modifications: Tower:

> <u>Remove and Replace</u>: (3) LNX 6515DS-A1M Antenna (**REMOVE**) - (3) RFS-APXVAARR24_43-U-NA20 Antenna 600/700/1900/2100 MHz (**REPLACE**)

<u>Install New:</u> (3) 1 5/8" Hybrid Fiber Line (3) TMA (3) Radio 4449 B12/B71

Existing to Remain: (12) 1 5/8" Coax (3) EMS RR90-17-02DP Antennas (Dormant) (3) TMA

Ground:

Upgrade to existing ground cabinet. (Internally)

The facility was approved by the Town of Thomaston Zoning Board of Appeals on July 18, 2000 with the conditions. T-Mobile's proposed exempt modification complies with those conditions.

Page 2

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Edmond V. Mone, First Selectman for the Town of Thomaston, as the municipality and property owner, Stacey Sefcik, Land Use Administrator and ZEO and Crown Castle is the tower owner.

- 1. The proposed modifications will not result in an increase in the height of the existing tower.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the abovereference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Anne Marie Zsamba.

Sincerely,

Anne Marie Zsamba Site Acquisition Specialist 3 Corporate Park Drive, Suite 101 Clifton Park, NY 12065 (201) 236-9224 AnneMarie.Zsamba@crowncastle.com

Attachments

cc:

Edmond V. Mone, First Selectman (*via email to emone@thomastonct.org*) Town of Thomaston – Town Hall 158 Main Street Thomaston, CT 06787 860-283-4421 Melanie A. Bachman

Page 3

Stacey Sefcik, ZEO (via email to ssefcik@thomastonct.org) Town of Thomaston – Town Hall 158 Main Street Thomaston, CT 06787 860-283-8411

Crown Castle, Tower Owner

Dear First Selectman Mone:

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council, today June 26, 2020.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable. If you could kindly confirm receipt. Thank you.

Best, Anne Marie Zsamba

ANNE MARIE ZSAMBA

Site Acquisition Specialist T: (201) 236-9224 M: (518) 350-3639 F: (724) 416-6112

CROWN CASTLE 3 Corporate Park Drive, Suite 101 Clifton Park, NY 12065 CrownCastle.com Dear Ms. Sefcik:

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council, today June 26, 2020.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable. If you could kindly confirm receipt. Thank you.

Best, Anne Marie Zsamba

ANNE MARIE ZSAMBA

Site Acquisition Specialist T: (201) 236-9224 M: (518) 350-3639 F: (724) 416-6112

CROWN CASTLE 3 Corporate Park Drive, Suite 101 Clifton Park, NY 12065 CrownCastle.com

Exhibit A

Original Facility Approval

THOMASTON ZONING BOARD OF APPEALS TOWN HALL THOMASTON, CT 06787

CERTIFICATE OF VARIANCE

This is to certify that the Thomaston Zoning Board of Appeals held a public hearing on July 18, 2000, at 7:45 pm in Meeting Room 1 of the Town Hall on an application from Voice Stream Wireless Corporation of 100 Filley St., Bloomfield, CT. The applicants sought a variance to permit their locating a ground mounted tower for a wireless communications facility on the west side of Chapel Street, approximately 1,000 feet distant from the intersection of Chapel Street with Prospect Street. The proposed tower is 175 feet in height. The applicants requested permission to locate the tower 201 feet from the property line. The property is owned by the Town of Thomaston and is located in an RA-40 zone.

Sec. 27.4.e of the Zoning Regulations of the Town of Thomaston provides that: "...the minimum distance from the base of any proposed ground mounted regulated facility to any property line, roadway, habitable dwelling, business or industrial use, public recreational areas, or public pathway shall be the height of the facility and mount, including any antennas or other appurtenances plus fifty per cent." Thus, 262.5 feet was the required setback.

With quorum present, the Board voted unanimously to grant the variance. The reasons were: topographic considerations; soll conditions on other parts of the site; and concerns over elevation on the site.

ATTEST:

Joseph F. Wassong, Jr.

Chairman, TZB

Town of Thomaston Planning & Zoning Board 158 Main Street Thomaston, Connecticut 06787

Return Receipt Requested

November 9, 2000

Voice Stream Wireless 100 Filley Street Bloomfield, CT 06002

> Re: Special Permit Approval for a Commercial Cellular Telecommunications Tower Chapel Street, Thomaston, Conn.

Dear Sirs:

At its meeting on Wednesday, November 1, 2000, the Thomaston Planning and Zoning Commission approved your Special Permit Application to construct a commercial cellular communications tower on municipal property at the end of Chapel Street.

The application was approved with the following conditions:

- 1. Conduct an annual RF inspection and submit the results to the Commission.
- Regrade the driveway as noted in Land Tech's letter dated. October 6, 2000.
- 3. Agreed to the terms and conditions as noted in a FAX from Flanimetrics dated November 1, 2000, regarding items 12-15.
- 4. If the Town decides not to have the tower removed, then the site plan and mylar must be revised. Any undertaking regarding the Town's tower shall be done in accordance with the conditions of the signed contract.

Sincerely,

ANNU

Samuel Barto Staff, TP2C Land Use Officer / ZEO

John of Thomaston Selectman's Office Town Hall 158 Main Street THOMASTON, CONNECTICUT 06787 283-4421

April 25, 2000

SELECTMEN'S MEETING MINUTES

At a meeting of the Board of Selectmen held on April 25, 2000 the following business was conducted:

The meeting opened at 4:00 p.m. with the Entire Board in attendance.

Also attending were Thomas C. Cusa of In Telecom, Inc., Sam Barto Town Planner and Attorney George Seabourne.

Selectman Brammer read a Fair Housing Resolution and a Fair Housing Policy Statement. (Copies Attached)

Selectman DuPont <u>made a motion</u> to adopt the Fair Housing Resolution and the Fair Housing Policy Statement seconded by Selectman O'Connell and passed unanimously by Selectman Brammer.

Selectman Brammer explained that as recipients of Small Cities Funding from the Department of Economic and Community Development we must adopt the above to reaffirm our commitment to Fair Housing. Larry Wagner the Town's Grants Coordinator has been the administrator of the Town's projects and programs and Lorraine Babb is our designated representative and is responsible for the enforcement and implementation of the Fair Housing Regulations.

Sam Barto reported to the Board of Selectmen that the roadway system in Phase III of the Highwood Farms Subdivision has been inspected by Town Engineer Bob Oley, Highway Superintendent Gerry Grohoski and by himself and it is their recommendation that it be accepted as a Town Road.

Selectman O'Connell <u>made a motion</u> to approve Phase III Section of the Highwood Farms Subdivision as a Town approved road seconded by Selectman DuPont and passed unanimously by Selectman Brammer.

Selectman DuPont <u>made</u> a <u>motion</u> to add Highwood Farms Subdivision--Phase V to today's Agenda seconded by Selectman O'Connell and passed unanimously by Selectman Brammer.

Selectman O'Connell <u>made a motion</u> to release the lots in Phase V of the Highwood Farms Subdivision in exchange for an irrevocable letter of credit in the amount of \$60,000.00 seconded by Selectman DuPont and passed unanimously by Selectman Brammer.

(Copy of Trrevocable Standby Letter of Credit Attached)

.

Selectman Brammer reported that Representatives from the Water Company will be meeting with him at 9:30 a.m. in his office on April 27th to discuss the design of the Water Extension to upper High Street.

SELECTMEN'S MEETING MINUTES (Cont'd)

The Board of Selectmen briefly went over Town Attorney Rybak's suggestions for the Proposed Lease Agreement between the Town of Thomaston and Omnipoint Communications, Inc. regarding the Communications Towar on Chapel Street.

Mr. Cusa said looking over the suggested changes, they will be acceptable, however items that might involve Federal Regulations would be out of their control.

Selectman O'Connell <u>made a motion</u> to accept the Proposed Lease Agreement between the Town of Thomaston and Omnipoint Communications, Inc. with the suggested changes made by Attorney Rybak and subject to the approval of the Inland Wetlands Commission, Planning and Zoning Commission and Town Meeting Approval seconded by Selectman DuPont and passed unanimously by Selectman Brammer.

Selectman DuPont <u>made a motion</u> to approve Glenn C. Clarks request that his remaining vacation time for this year (4 days) be held past his anniversary date of July 5,2000 as he is going on a cruise in May of 2001 seconded by Selectman O'Connell and passed unanimously by Selectman Brammer.

At 4:32 p.m. Selectman DuPont <u>made a motion</u> to adjourn the meeting seconded by Selectman O'Connell and passed unanimously by Selectman Branmer.

Signed Kford C. Brammer, Jr

First Selectman

Signed nogen

Roger *DuPont* Selectman

Signed Richard A, 0 Conne1. Selectman

Tofon of Ahomaston Planning & Zoning Board 158 Main Street Ahomaston, Connecticut 06787

August 7, 2000

Voice Stream Wireless 100 Filley Street Bloomfield, CT 06002

Attn: Mr. Rick Frazier

Re: Special Permit Application for a Commercial Telecommunications Tower and Facility

Dear Mr. Frazier:

At its meeting on August 2, 2000, the Thomaston Planning and Zoning Commission accepted your Special Permit Application. The public hearing is scheduled for Wednesday, September 6, 2000, at 7:00 p.m. The meeting will be held in the Lena Morton Art Gallery.

The Commission has scheduled an on-site inspection for Wednesday, August 30, 2000, at 6:30 p.m. In accordance with the Zoning Regulations, Section 27.7, Part L, the Commission requests that you send aloft a site identification balloon on or just prior to the day of inspection. My office will publish a legal notice prior to the raising. The site walk will be open to the public.

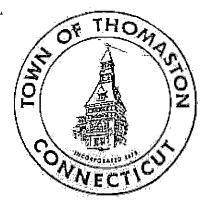
Please make sure to address each of the requirements in Article XXVII at the public hearing. This should insure a very thorough and informative public hearing.

If you have any questions, comments or suggestions, please feel free to call the Land Use Office at 283-8411.

Sincerely,

Samuel Barto Land Use Officer Please Note: The balloon shall also be raised at least 3 days prior to the public hearing.

cc: Bruce Hoben



SPECIAL PERMIT APPLICATION

Town of Thomaston, Connecticut

Date Received:

Application for a Special Permit

Applicant: Voice Strepm /Omnipoin + Wireless 06002 DO Filley Bloomfield, Address:

The undersigned hereby makes application to the Planning and Zoning Commission for a SPECIAL PERMIT in accordance with the provisions of Section 3.11 - Schedule A - Permitted Uses and Article IX of the Thomaston Zoning Regulations.

Date: 7/39/00 Signature:

Section 1. Previous Application

Has a previous Special Permit Application been filed with the Commission for the same premises? Yes: _____ No: _____

Section 2. Placement on Agenda

In order for the Commission to consider your application, it must be received in the Planning and Zoning Office (Land-Use Office) no later than five (5) working days prior to the next regularly scheduled meeting.

Section 3. Plans and Documentation

All Special Permit applications, unless otherwise prescribed in the Zoning Regulations or directed by the Commission, must be accompanied by the following documentation: Town of Chomaston Planning & Zoning Board 158 Main Street Chomaston, Connecticut 06787

August 7, 2000

Voice Stream Wireless 100 Filley Street Bloomfield, CT 06002

Attn: Mr. Rick Frazier

Re: Special Permit Application for a Commercial Telecommunications Tower and Facility

Dear Mr. Frazier:

At its meeting on August 2, 2000, the Thomaston Planning and Zoning Commission accepted your Special Permit Application. The public hearing is scheduled for Wednesday, September 6, 2000, at 7:00 p.m. The meeting will be held in the Lena Morton Art Callery.

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Please make sure to address each of the requirements in Article XXVII at the public hearing. This should insure a very thorough and informative public hearing.

If you have any questions, comments or suggestions, please feel free to call the Land Use Office at 283-8411.

Sincerely,

Samuel Barto Land Use Officer

Please Note: The balloon shall also be raised at least 3 days prior to the public hearing.

cc: Bruce Hoben

- a. A "Statement of Use" which shall detail the proposed use of the site.
- b. Site Plan and Landscaping Plan.
- c. Architectural and Construction Plan
- d. Flood Hazard Area Data
- e. Soil Erosion and Sedimentation Control Plan
- f. All other pertinent information and documentation that may be required by the Commission in order to make a decision on the application.

Section 4. Application Fees

- a. Standard Application Fee: \$ 150.00
- b. Home Occupation Permit: \$ 100.00

Section 5. Waiver of Requirements

Does the applicant request the Commission to waive any of the required documentation as specified in Sections 9.3.2, 9.3.3 or 9.3.4 of the Zoning Regulations?

Yes:_____ No:____

If yes, please specify: _

Section 6. Extension of Review Period

Will the applicant consent to a formal extension of time in order for the Commission to take action on this application?

Yes: ____ No: ____

If yes, please specify period or date: _____

Section 7. Failure to Submit

Failure by an applicant to submit any or all of the required or requested documentation under Section 3.11 or Article IX may be grounds for the Commission to consider the application as being incomplete.

Section 8. Review by Town Engineer

The applicant shall be responsible for paying all inspection and review costs incurred by the Town Engineer during the review process.

If additional on-site inspection and review is necessary and required by the Commission after the approval is granted and prior to completion of the project, the applicant shall also be responsible for these costs.

The costs shall be no more per hour than what is assessed to the Town in any given year by the Town Engineer.

Section 9. Public Hearing

The Thomaston Planning and Zoning Commission will conduct a "Public Hearing" on this application. The applicant, or their authorized agent, must be present at the hearing and should be prepared to present information showing how the proposed use of the site along with the buildings, structures, and facilities will conform to the standards as specified in these Regulations.

All standards as specified in Article IX are in addition to other requirements as contained in the Regulations which may be applicable in the District in which the Special Permit is proposed.

Section 10. Inspection of Property

The Commission is authorized by the submission of this application to inspect the premises. Section 11. Additional Information

The Commission may obtain additional documentation and information on its own initiative but will need to rely upon data presented to it by the applicant.

Section 12. Modification of Approval

If approval is granted by the Planning and Zoning Commission, it may be subject to modifications deemed necessary to con-form to specific standards of the Regulations. It may also be subject to appropriate conditions and safeguards necessary to conserve public health and safety, convenience, welfare and property values in the neighborhood.

Applicants Signature: Jun Meller 860 Home Phone. 692 Home Phone: 673 2727 Business Phone: 860-677 5267

OFFICE USE

Commission date when application was received:

Date of initial Public Hearing:

Public Hearing was continued to:

Date of Approval: _____ Disapproval; Was approval modified:

If yes, give specifics:

Yes: ____ No: ____

Land-Use Officer:	
	Samuel L. Barto Staff, PZC

____ Date:

Exhibit B

Property Card

Thomaston, CT : Commercial Property Record Card

[Back to Search Results]

Search For Properties

Account	Name	Street Name			
		CHAPEL ST	▼	Search	Reset

Account T0304400 Card Map-Block-Lot 55-03-08

Location 580 CHAPEL ST Zoning RA80

State Class MUNICIPALITIES Acres 6.540

Living Units 0

1

Thomaston Town Of 158 Main St

Thomaston CT 06787

Deed Information

Building Information

56/664

1966/05/04

Book/Page:

Deed Date:

Building No:

Year Built:

Grade:

No of Units:

Valuation Land:

Building:

Total:

Structure Type:

Identical Units:

Owner Information

0

0

0

0

\$0

\$218,700

\$218,700 \$153,090



Sales	History

Net Assessment:

Book/Page	Date	Price	Туре	Validit	t y
Out Building Information Structure Code	Width	Lgth/SqFt		Year	RCNLD

Exterior/Interior Information

Levels Size Use Type Ext. Walls Const. Type Partitions Heating A/C Plumbing Condition Func. Utility Unadj. RCNLD

Building Sketch

[Start a New Search][Help with Printing]



Notice

Tax Year 2019 Values

The information delivered through this on-line database is provided in the spirit of open access to government information and is intended as an enhanced service and convenience for citizens of Thomaston, CT.

The providers of this database: CLT, Big Room Studios, and Thomaston, CT assume no liability for any error or omission in the information provided here.

Comments regarding this service should be directed to: rdudek@thomastonct.org.



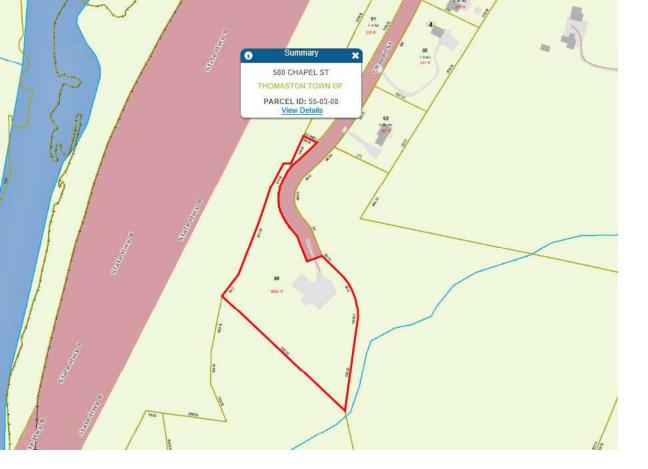
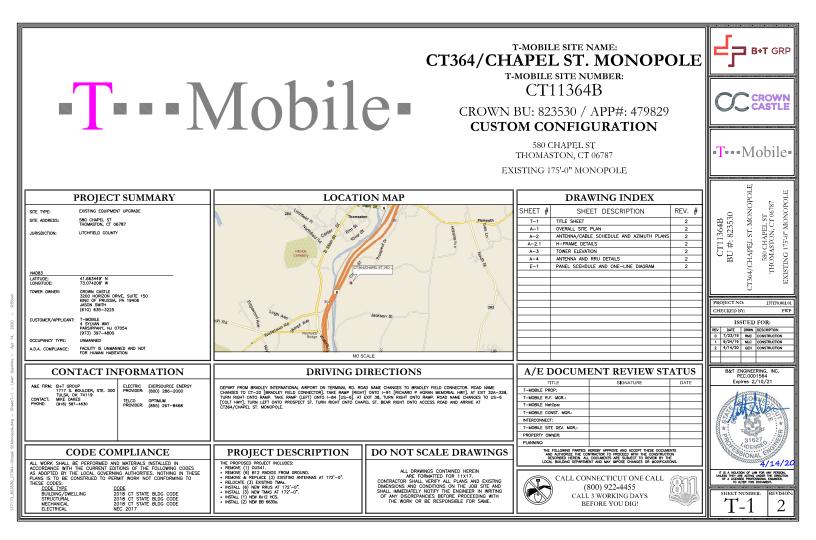
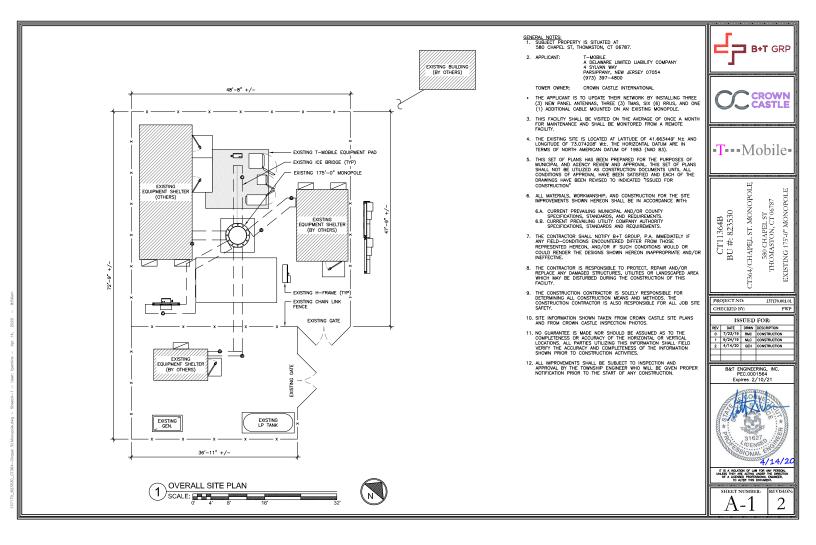
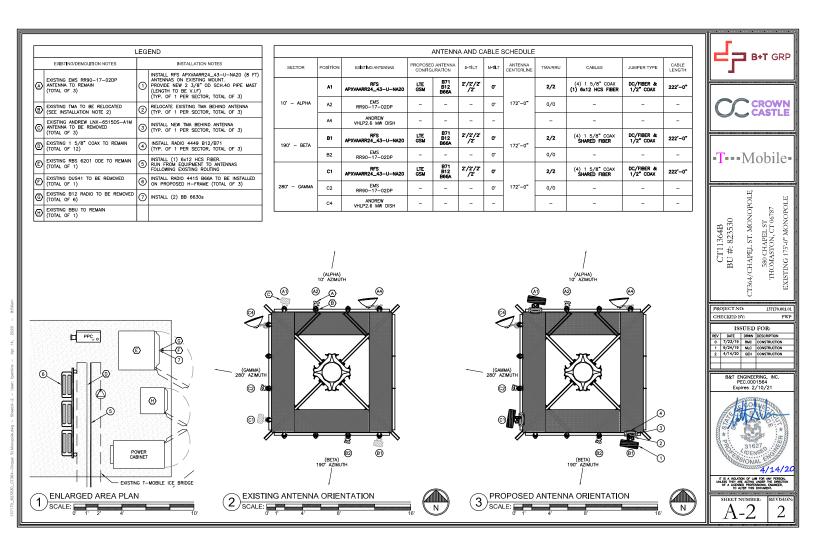


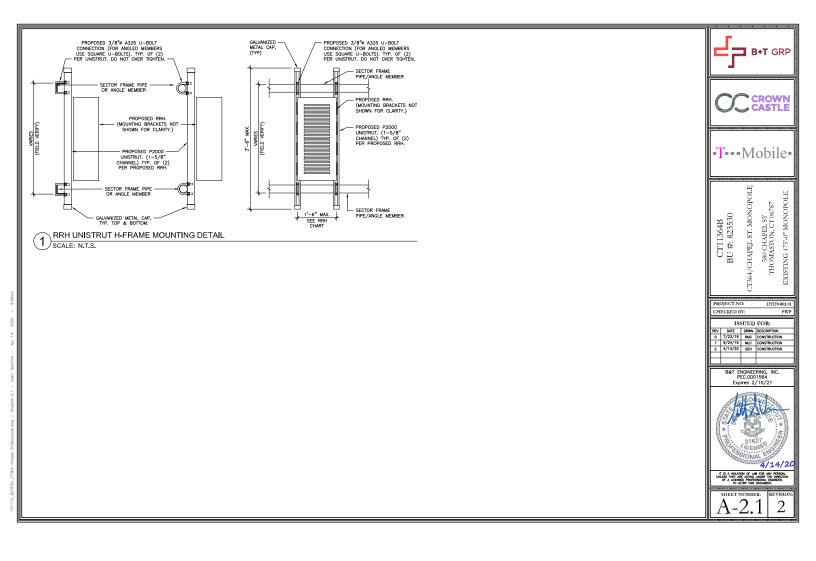
Exhibit C

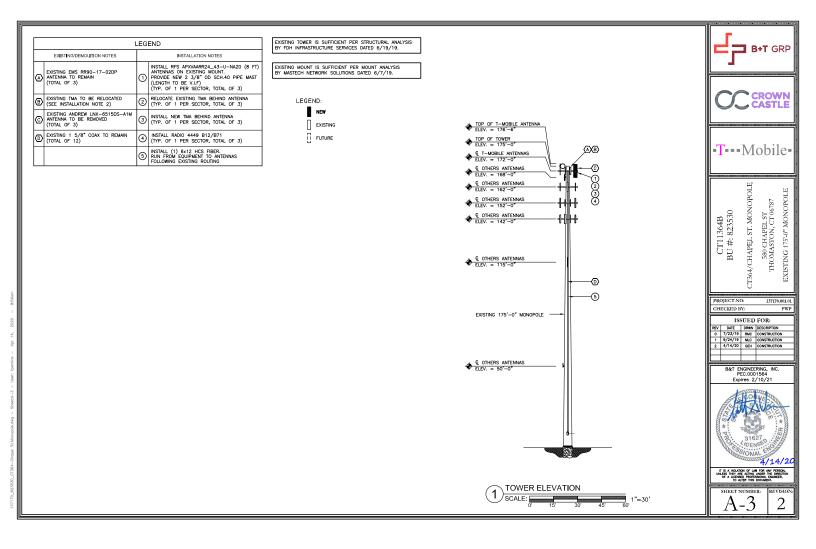
Construction Drawings

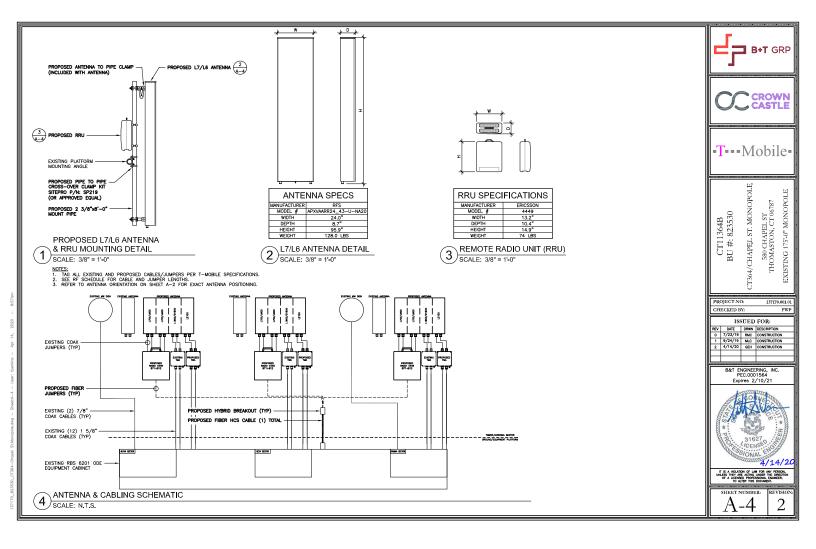












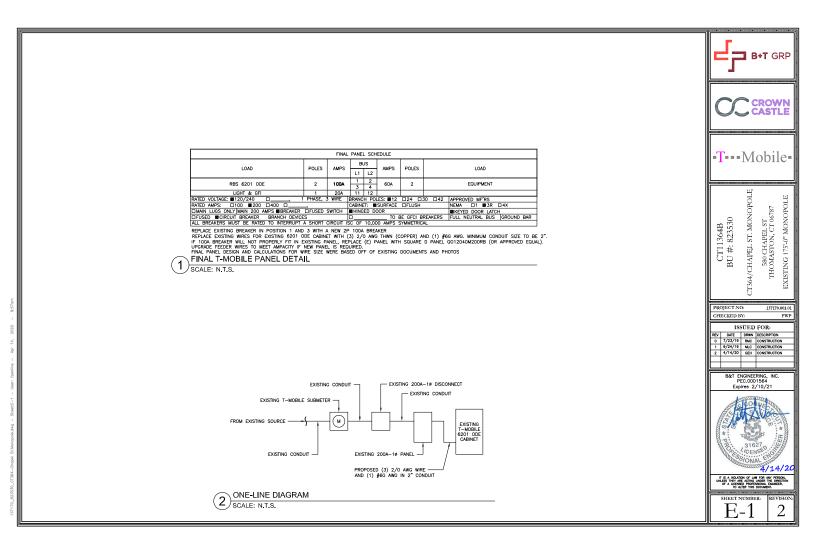


Exhibit D

Structural Analysis Report

INFRASTRUCTURE SERVICES Date: June 19, 2019 ENGINEERING INNOVATION **Denice Nicholson** FDH Infrastructure Services, LLC Crown Castle 6521 Meridien Drive Suite 107 3 Corporate Dr Raleigh, NC 27616 Clifton Park, NY 12065 919.755.1012 Subject: **Structural Analysis Report** Carrier Designation: *T-Mobile* Co-Locate **Carrier Site Number:** CT11364B Carrier Site Name: CT364/Chapel St. Monopole Crown Castle Designation: Crown Castle BU Number: 823530 Crown Castle Site Name: CT364/Chapel St. Monopole Crown Castle JDE Job Number: 559233 **Crown Castle Work Order Number:** 1749544 Crown Castle Order Number: 479829 Rev. 0 Engineering Firm Designation: **FDH-IS Project Number:** 19BMUT1400 580 Chapel Street, Thomaston, Litchfield County, CT Site Data: Latitude 41° 39' 48.48", Longitude -73° 4' 27.41" **175 Foot - Monopole Tower**

Dear Denice Nicholson,

FDH Infrastructure Services, LLC is pleased to submit this "**Structural Analysis Report**" to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Proposed Equipment Configuration

This analysis utilizes an ultimate 3-second gust wind speed of 120 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Respectfully Submitted by:

Aditya Chingale, El Project Engineer I

Reviewed by:

Krystyn M. Perez, PE Vice President of Structural Engineering CT PE License No. 32975



Sufficient Capacity-79.8%

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- 3.2) Assumptions

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tnxTower Output

6) APPENDIX B

Base Level Drawing

7) APPENDIX C

Additional Calculations

1) INTRODUCTION

This tower is a 175 ft Monopole tower designed by Pirod Manufactures Inc.

2) ANALYSIS CRITERIA

TIA-222 Revision:	TIA-222-H
Risk Category:	II
Wind Speed:	120 mph
Exposure Category:	B
Topographic Factor:	1
Ice Thickness:	1.5 in
Wind Speed with Ice:	50 mph
Service Wind Speed:	60 mph

Mounting Level (ft)	Flovation	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
		1	-	Platform Mount [LP 701-1]		
			3	ems wireless	RR90-17-02DP	
172.0	172.0	3	ericsson	KRY 112 144/1	10	1-5/8
172.0 172.0	3	ericsson	KRY 112 489/2	13	1-5/0	
	3	ericsson	RADIO 4449 B12/B71			
		3	rfs celwave	APXVAARR24_43-U-NA20	1	

Table 1 - Proposed Equipment Configuration

Table 2 - Other Considered Equipment

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
	175.0	2	andrew	VHLP2.6		
172.0		1	bird tech group	OA20-67-DIN	3	7/8
172.0	168.0	1	lone star electronics	LS-230C		110
168.0	171.0	1	lone star electronics	LS-230C	6	7/8
	168.0	1	-	Side Arm Mount [SO 701-1]		
		3	alcatel lucent	800MHz 2X50W RRH W/FILTER		
		3	alcatel lucent	PCS 1900MHz 2x40W		
162.0	162.0	3	alcatel lucent	TD-RRH8x20-25	4	1-1/4
		1	-	Platform Mount [LP 712-1]	1	ĺ
		3	rfs celwave	APXVSPP18-C-A20		
		3	rfs celwave	APXVTM14-C-120		

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
		1	-	Heavy 12' UPNY Boom [SM 801-3]		
1		6	antel	LPA-80080/4CF	1	
152.0	52.0 152.0	6	commscope	NNHH-65B-R4		1-3/8
1		1	raycap	RVZDC-6600-PF-48	6	1-5/8
		3	samsung telecomm	RFV01U-D1A		
1		3	samsung telecomm	RFV01U-D2A	1	
		1	cci antennas	HPA65R-BU4A		
[2	cci antennas	HPA65R-BU6A		
		3	ericsson	RADIO 4415 B30		3/8 3/4 1-5/8
		3	ericsson	RRUS 4449 B5/B12		
		3	ericsson	RRUS 4478 B14		
	143.0	3	ericsson	RRUS 8843 B2/B66A	2	
142.0		2	kathrein	80010964	6	
142.0		4	kathrein	80010965	12	
		3	powerwave tech	7770.00	2	Conduit
		6	powerwave tech	LGP21401		
		2	raycap	DC6-48-60-18-8F		
		1	-	Miscellaneous [NA 507-1]	1	
1	142.0	1	-	Platform Mount [LP 303-1]	1	
		1	raycap	DC6-48-60-18-8F	1	
115.0	115.0	3	rfs celwave	APXV18-206517S-C	6	1-5/8
50.0	50.0	1	-	Side Arm Mount [SO 701-1]	1	1/2
50.0	50.0	1	pctel	GPS-TMG-HR-26NCM		1/2

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	FDH Engineering, Inc.	3462674	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	Pirod, Inc.	3464631	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Pirod, Inc.	3462695	CCISITES

3.1) Analysis Method

tnxTower (version 8.0.5.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built and maintained in accordance with the manufacturer's specifications.
- 2) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 3) Base plate design methodology of the manufacturer has been reviewed and found to be an acceptable means of designing to resist the full capacity of the bolts and shaft.

This analysis may be affected if any assumptions are not valid or have been made in error. FDH Infrastructure Services, LLC should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Section No.	Elevation (ft)	Component Type	Size	Critical Element	Р (К)	SF*P_allow (K)	% Capacity²	Pass / Fail
L1	175 - 164.25	Pole	TP26x22x0.25	1	-5.07	1202.11	5.0	Pass
L2	164.25 - 129.67	Pole	TP34.0625x24.4135x0.3125	2	-19.14	1996.21	30.1	Pass
L3	129.67 - 96	Pole	TP41.75x32.452x0.375	3	-27.39	2940.31	41.4	Pass
L4	96 - 63.17	Pole	TP49.0625x39.8421x0.375	4	-37.02	3460.73	53.6	Pass
L5	63.17 - 31.17	Pole	TP56.125x46.9602x0.375	5	-48.16	3964.26	64.1	Pass
L6	31.17 - 0	Pole	TP62.9375x53.8475x0.375	6	-63.20	4574.01	74.8	Pass
							Summary	
						Pole (L6)	74.8	Pass
						RATING =	74.8	Pass

Table 4 - Section Capacity (Summary)

Table 5 - Tower Component Stresses vs. Capacity – LC7

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1, 2	Anchor Rods	0	67.5	Pass
1, 3	Base Plate	0	OK	Pass
1, 2	Base Foundation	0	79.8	Pass
1, 2	Base Foundation Soil Interaction	0	78.3	Pass

Structure Rating (max from all components) =	79.8% ²	

Notes:

1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

2) Ratings per TIA-222-H Section 15.5

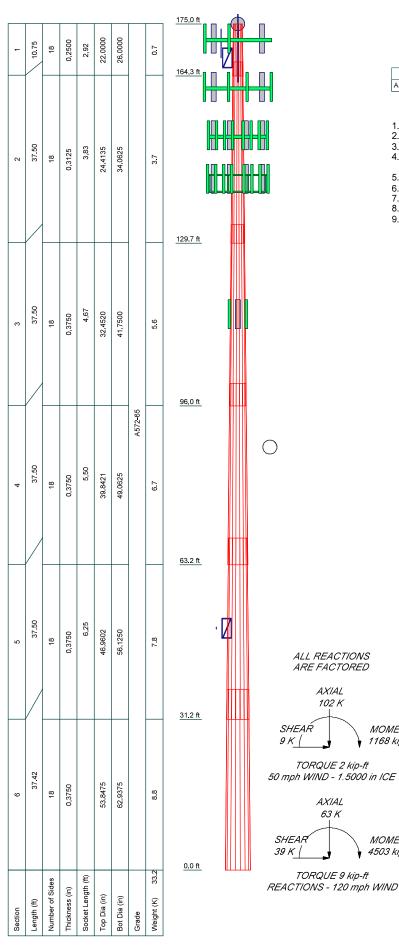
3) Base plate is assumed to have the same capacity as their respective anchor bolts or shaft.

4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

APPENDIX A

TNXTOWER OUTPUT



MATERIAL STRENGTH							
GRADE	Fy	Fu	GRADE	Fy	Fu		
A572-65	65 ksi	80 ksi					

TOWER DESIGN NOTES

- Tower is located in Litchfield County, Connecticut.
 Tower designed for Exposure B to the TIA-222-H Standard.
- 3. Tower designed for a 120 mph basic wind in accordance with the TIA-222-H Standard. Tower is also designed for a 50 mph basic wind with 1.50 in ice. Ice is considered to 4.

increase in thickness with height.

5. Deflections are based upon a 60 mph wind.

- Tower Risk Category II.
 Topographic Category 1 with Crest Height of 0.00 ft
 TIA-222-H Annex S
- 9. TOWER RATING: 74.8%

AXIAL 102 K

AXIAL 63 K

MOMENT

1168 kip-ft

MOMENT

4503 kip-ft

	FDH Infrastructure Services	S ^{lob:} CT364/Chapel St. Monopole (BU# 823530)			
FDH SERVICES	6521 Meridien Drive	Project: 19BMUT1400			
ENGINEERING NEOVATION	Raleigh, NC 27616	^{Client:} Crown Castle	^{Drawn by:} Aditya Chingale	App'd:	
Tower Analysis	Phone: 919.755.1012	^{Code:} TIA-222-H	^{Date:} 06/19/19	Scale: NTS	
	FAX: 919.755.1031	Path: #Docementation Encore demandational_cover code use	IncTRENSE_CTHORNER IS wongolarities. THE STANCE, TWO B, NAME SUBJECTS TO WHEN SOLUTION AND A MANAGEMENT	Dwg No. E-1	

Project

Client

Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-H standard. The following design criteria apply: Tower is located in Litchfield County, Connecticut. Tower base elevation above sea level: 543.00 ft. Basic wind speed of 120 mph. Risk Category II. Exposure Category B. Simplified Topographic Factor Procedure for wind speed-up calculations is used. Topographic Category: 1. Crest Height: 0.00 ft. Nominal ice thickness of 1.5000 in. Ice thickness is considered to increase with height. Ice density of 56 pcf. A wind speed of 50 mph is used in combination with ice. Temperature drop of 50 °F. Deflections calculated using a wind speed of 60 mph. TIA-222-H Annex S. A non-linear (P-delta) analysis was used. Pressures are calculated at each section. Stress ratio used in pole design is 1.05. Tower analysis based on target reliabilities in accordance with Annex S. Load Modification Factors used: $K_{es}(F_w) = 0.95$, $K_{es}(t_i) = 0.85$. Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification Use Code Stress Ratios $\sqrt{}$ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric

Distribute Leg Loads As Uniform Assume Legs Pinned Assume Rigid Index Plate Use Clear Spans For Wind Area Use Clear Spans For KL/r

- Retension Guys To Initial Tension Bypass Mast Stability Checks
- Use Azimuth Dish Coefficients
- Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination
- Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

- Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption Poles
- Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

Project

Client

CT364/Chapel St. Monopole (BU# 823530)

FDH Infrastructure Services 6521 Meridien Drive Raleigh, NC 27616 Phone: 919.755.1012 FAX: 919.755.1031

19BMUT1400

Crown Castle

Date 09:40:29 06/19/19 Designed by Aditya Chingale

Tapered Pole Section Geometry

Section	Elevation	Section	Splice	Number	Тор	Bottom	Wall	Bend	Pole Grade
		Length	Length	of	Diameter	Diameter	Thickness	Radius	
	ft	ft	ft	Sides	in	in	in	in	
L1	175.00-164.25	10.75	2.92	18	22.0000	26.0000	0.2500	1.0000	A572-65
									(65 ksi)
L2	164.25-129.67	37.50	3.83	18	24.4135	34.0625	0.3125	1.2500	A572-65
									(65 ksi)
L3	129.67-96.00	37.50	4.67	18	32.4520	41.7500	0.3750	1.5000	A572-65
									(65 ksi)
L4	96.00-63.17	37.50	5.50	18	39.8421	49.0625	0.3750	1.5000	À572-65
									(65 ksi)
L5	63.17-31.17	37.50	6.25	18	46.9602	56.1250	0.3750	1.5000	À572-65
									(65 ksi)
L6	31.17-0.00	37.42		18	53.8475	62.9375	0.3750	1.5000	A572-65
									(65 ksi)

Tapered Pole Properties

Section	Tip Dia.	Area	Ι	r	С	I/C	J	It/Q	W	w/t
	in	in ²	in⁴	in	in	in ³	in⁴	in ²	in	
L1	22.3008	17.2586	1031.4832	7.7212	11.1760	92.2945	2064.3237	8.6310	3.4320	13.728
	26.3625	20.4326	1711.6544	9.1412	13.2080	129.5922	3425.5610	10.2183	4.1360	16.544
L2	25.5048	23.9052	1754.2802	8.5559	12.4021	141.4508	3510.8687	11.9549	3.7468	11.99
	34.5398	33.4758	4817.4335	11.9812	17.3038	278.4040	9641.2058	16.7411	5.4450	17.424
L3	33.8591	38.1797	4963.1506	11.3873	16.4856	301.0593	9932.8318	19.0935	5.0516	13.471
	42.3362	49.2466	10650.9822	14.6881	21.2090	502.1916	21315.9793	24.6280	6.6880	17.835
L4	41.5648	46.9757	9244.4481	14.0108	20.2398	456.7464	18501.0602	23.4923	6.3522	16.939
	49.7615	57.9503	17355.1378	17.2841	24.9238	696.3293	34733.1119	28.9807	7.9750	21.267
L5	48.9917	55.4480	15202.6322	16.5377	23.8558	637.2728	30425.2683	27.7293	7.6050	20.28
	56.9330	66.3564	26056.1506	19.7913	28.5115	913.8821	52146.5865	33.1845	9.2180	24.581
L6	56.1620	63.6457	22991.5268	18.9827	27.3545	840.5012	46013.3064	31.8289	8.8172	23.512
	63.8506	74.4650	36822.8946	22.2097	31.9722	1151.7142	73694.2417	37.2396	10.4170	27.779

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A_f	Adjust. Factor A _r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals	Double Angle Stitch Bolt Spacing Redundants
ft	ft^2	in					in	in	in
L1				1	1	1			
175.00-164.25									
L2				1	1	1			
164.25 - 129.67									
L3				1	1	1			
129.67 - 96.00									
L4 96.00-63.17				1	1	1			
L5 63.17-31.17				1	1	1			
L6 31.17-0.00				1	1	1			

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Areas Tool of	Job		Page
tnxTower		CT364/Chapel St. Monopole (BU# 823530)	3 of 17
FDH Infrastructure Services 6521 Meridien Drive Raleigh, NC 27616 Phone: 919.755.1012 FAX: 919.755.1031	Project		Date
		19BMUT1400	09:40:29 06/19/19
	Client	Crown Castle	Designed by Aditya Chingale

Description	Sector	Exclude From Torque	Component Type	Placement ft	Total Number	Number Per Row	Start/End Position	Width or Diameter in	Perimeter in	Weight plf
		Calculation		<i>J</i> ŧ						P9

Safety Line 3/8	С	No	Surface Ar (CaAa)	175.00 - 0.00	1	1	$0.000 \\ 0.000$	0.3750		0.22

50										
LDF4-50A(1/2)	А	No	Surface Ar (CaAa)	50.00 - 0.00	1	1	-0.438 -0.438	0.6250		0.15

****115***										
LDF7-50A(1-5/8)	А	No	Surface Ar (CaAa)	115.00 - 0.00	6	1	-0.250 0.000	1.9800		0.82

MLCH 12X6 AWG(1-3/8)	В	No	Surface Ar (CaAa)	152.00 - 0.00	1	1	-0.313 -0.313	1.4300		1.72

	С	N	Surface Ar	172.00 -	1	1	0.250	1.6600		2.40
HCS 6X12 4AWG(1-5/8)	C	No	(CaAa)	0.00	1	1	0.250	1.6600		2.40

Feed Line/Linear Appurtena	nces - Entered As Area
----------------------------	------------------------

Description	Face or	Allow Shield	Exclude From	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg		Torque Calculation		ft			ft²/ft	plf

142									
AVA7-50(1-5/8)	С	No	No	Inside Pole	142.00 - 0.00	12	No Ice	0.00	0.70
							1/2" Ice	0.00	0.70
							1" Ice	0.00	0.70
							2" Ice	0.00	0.70
B-L98-002-XXX(3	С	No	No	Inside Pole	142.00 - 0.00	1	No Ice	0.00	0.06
/8)							1/2" Ice	0.00	0.06
,							1" Ice	0.00	0.06
							2" Ice	0.00	0.06
R-VG86ST-BRD(С	No	No	Inside Pole	142.00 - 0.00	2	No Ice	0.00	0.58
3/4)							1/2" Ice	0.00	0.58
,							1" Ice	0.00	0.58
							2" Ice	0.00	0.58
B-L98B-034-XXX(С	No	No	Inside Pole	142.00 - 0.00	1	No Ice	0.00	0.06
3/8)							1/2" Ice	0.00	0.06
<i>,</i>							1" Ice	0.00	0.06
							2" Ice	0.00	0.06
R-VG86ST-BRD(С	No	No	Inside Pole	142.00 - 0.00	4	No Ice	0.00	0.58
3/4)							1/2" Ice	0.00	0.58
,							1" Ice	0.00	0.58
							2" Ice	0.00	0.58
2"	С	No	No	Inside Pole	142.00 - 0.00	2	No Ice	0.00	1.15
							1/2" Ice	0.00	1.15
							1" Ice	0.00	1.15

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tnxTower		CT364/Chapel St. Monopole (BU# 823530)	4 of 17
EDH Infrastructure Services	Project		Date
FDH Infrastructure Services 6521 Meridien Drive		19BMUT1400	09:40:29 06/19/19
Raleigh, NC 27616	Client		Designed by
Phone: 919.755.1012 FAX: 919.755.1031		Crown Castle	Aditya Chingale

Description	Face	Allow	Exclude	Component	Placement	Total		$C_A A_A$	Weight
	or	Shield	From	Туре		Number			
	Leg		Torque		ft			ft²/ft	plf
			Calculation				2" Ice	0.00	1.15
****							2 100	0.00	1.15
168									
LDF5-50A(7/8)	С	No	No	Inside Pole	168.00 - 0.00	6	No Ice	0.00	0.33
							1/2" Ice	0.00	0.33
							1" Ice	0.00	0.33
							2" Ice	0.00	0.33

**162									
HB114-1-08U4-M5J	Α	No	No	Inside Pole	162.00 - 0.00	3	No Ice	0.00	1.08
(1-1/4)							1/2" Ice	0.00	1.08
							1" Ice	0.00	1.08
							2" Ice	0.00	1.08
HB114-21U3M12-X	Α	No	No	Inside Pole	162.00 - 0.00	1	No Ice	0.00	1.22
XXF(1-1/4)							1/2" Ice	0.00	1.22
							1" Ice	0.00	1.22
							2" Ice	0.00	1.22

152	P				1.50 00 0.00	,		0.00	
LDF7-50A(1-5/8)	В	No	No	Inside Pole	152.00 - 0.00	6	No Ice	0.00	0.82
							1/2" Ice	0.00	0.82
							1" Ice	0.00	0.82
****							2" Ice	0.00	0.82
172									
AVA5-50(7/8)	С	No	No	Inside Pole	172.00 - 0.00	3	No Ice	0.00	0.30
AVAJ-JU(1/8)	U	100	100	mside Pole	172.00 - 0.00	3	No Ice 1/2" Ice	0.00	0.30
							$1/2^{-1}$ Ice	0.00	0.30
							2" Ice	0.00	0.30
****							2 100	0.00	0.50
****172***									
LDF7-50A(1-5/8)	С	No	No	Inside Pole	172.00 - 0.00	12	No Ice	0.00	0.82
LDI / 50/1(1 5/0)	C	110	110	monue i ole	1,2.00 0.00	14	1/2" Ice	0.00	0.82
							172 Ice	0.00	0.82
							2" Ice	0.00	0.82
****							- 100	0.00	0.02

		Feed	d Line/l	_inear A	ppurter	nances S	Section Area	IS
Tower	Tower	Face	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight	
Section	Elevation ft		ft ²	ft ²	In Face ft ²	Out Face ft ²	K	
L1	175.00-164.25	А	0.000	0.000	0.000	0.000	0.00	
		В	0.000	0.000	0.000	0.000	0.00	
		С	0.000	0.000	1.690	0.000	0.11	
L2	164.25-129.67	А	0.000	0.000	0.000	0.000	0.14	
		В	0.000	0.000	3.193	0.000	0.15	
		С	0.000	0.000	7.037	0.000	0.71	
L3	129.67-96.00	А	0.000	0.000	3.762	0.000	0.24	

tnxTower	Job	CT364/Chapel St. Monopole (BU# 823530)	Page 5 of 17
FDH Infrastructure Services 6521 Meridien Drive	Project	19BMUT1400	Date 09:40:29 06/19/19
Raleigh, NC 27616 Phone: 919.755.1012 FAX: 919.755.1031	Client	Crown Castle	Designed by Aditya Chingale

Tower	Tower	Face	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		ft^2	ft^2	ft^2	ft^2	Κ
		В	0.000	0.000	4.815	0.000	0.22
		С	0.000	0.000	6.852	0.000	1.00
L4	96.00 - 63.17	А	0.000	0.000	6.500	0.000	0.31
		В	0.000	0.000	4.695	0.000	0.22
		С	0.000	0.000	6.681	0.000	0.97
L5	63.17-31.17	Α	0.000	0.000	7.513	0.000	0.30
		В	0.000	0.000	4.576	0.000	0.21
		С	0.000	0.000	6.512	0.000	0.95
L6	31.17-0.00	А	0.000	0.000	8.120	0.000	0.30
		В	0.000	0.000	4.457	0.000	0.21
		С	0.000	0.000	6.343	0.000	0.92

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness			In Face	Out Face	_
	ft	Leg	in	ft^2	ft^2	ft^2	ft^2	K
L1	175.00-164.25	А	1.502	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	7.246	0.000	0.19
L2	164.25-129.67	А	1.480	0.000	0.000	0.000	0.000	0.14
		В		0.000	0.000	9.900	0.000	0.27
		С		0.000	0.000	27.808	0.000	1.03
L3	129.67-96.00	А	1.441	0.000	0.000	9.385	0.000	0.96
		В		0.000	0.000	14.779	0.000	0.40
		С		0.000	0.000	26.780	0.000	1.30
L4	96.00-63.17	Α	1.392	0.000	0.000	15.963	0.000	1.49
		В		0.000	0.000	14.158	0.000	0.38
		С		0.000	0.000	25.607	0.000	1.26
L5	63.17-31.17	А	1.321	0.000	0.000	21.663	0.000	1.47
		В		0.000	0.000	13.484	0.000	0.37
		С		0.000	0.000	24.328	0.000	1.21
L6	31.17-0.00	А	1.180	0.000	0.000	24.594	0.000	1.39
		В		0.000	0.000	12.695	0.000	0.35
		С		0.000	0.000	22.818	0.000	1.16

Feed Line Center of Pressure

Section	Elevation	CP_X	CP_Z	CP_X	CP_Z
				Ice	Ice
	ft	in	in	in	in
L1	175.00-164.25	-0.4791	1.1089	-0.6467	2.3284
L2	164.25-129.67	-0.3407	0.6683	-0.4242	1.6082
L3	129.67-96.00	-1.0080	0.0644	-1.4533	0.7855
L4	96.00 - 63.17	-1.1958	-0.0628	-2.2652	0.5705
L5	63.17-31.17	-1.3314	0.0094	-2.8871	0.8569
L6	31.17-0.00	-1.7612	0.0713	-3.2600	1.0261

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

tnxTower

19BMUT1400

Crown Castle

	Page
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	Date 09:40:29 06/19/19
	Designed by Aditya Chingale

Shielding Factor Ka

Tower	Feed Line	Description	Feed Line	Ka	Ka
Section	Record No.		Segment Elev.	No Ice	Ice
L1	2	Safety Line 3/8	164.25 -	1.0000	1.0000
			175.00		
L1	35	HCS 6X12 4AWG(1-5/8)	164.25 -	1.0000	1.0000
			172.00		
L1	27	MLCH 12X6 AWG(1-3/8)	164.25 -	1.0000	1.0000
			152.00		
L2	2	Safety Line 3/8	129.67 -	1.0000	1.0000
			164.25		
L2	23	LDF7-50A(1-5/8)	129.67 -	1.0000	1.0000
			115.00		
L2	27	MLCH 12X6 AWG(1-3/8)	129.67 -	1.0000	1.0000
			152.00		
L2	35	HCS 6X12 4AWG(1-5/8)		1.0000	1.0000
			164.25		
L3	2	Safety Line 3/8		1.0000	1.0000
L3	23	LDF7-50A(1-5/8)		1.0000	1.0000
L3	27	MLCH 12X6 AWG(1-3/8)		1.0000	1.0000
L3	35	HCS 6X12 4AWG(1-5/8)		1.0000	1.0000
L4	2	Safety Line 3/8		1.0000	1.0000
L4	20	LDF4-50A(1/2)		1.0000	1.0000
L4	23	LDF7-50A(1-5/8)		1.0000	1.0000
L4	27	MLCH 12X6 AWG(1-3/8)		1.0000	1.0000
L4	35	HCS 6X12 4AWG(1-5/8)		1.0000	1.0000
L5	2	Safety Line 3/8		1.0000	1.0000
L5	20	LDF4-50A(1/2)		1.0000	1.0000
L5	23	LDF7-50A(1-5/8)		1.0000	1.0000
L5	27	MLCH 12X6 AWG(1-3/8)		1.0000	1.0000
L5	35	HCS 6X12 4AWG(1-5/8)	31.17 - 63.17	1.0000	1.0000

Job

Project

Client

Discrete Tower Loads

0	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weight
			ft ft ft	o	ft		ft²	ft ²	K
Lightning Rod 5/8x6'	А	From Leg	0.00	0.0000	175.00	No Ice	0.38	0.38	0.05
0 0		e	0.00			1/2" Ice	0.99	0.99	0.05
			0.00			1" Ice	1.62	1.62	0.06
172 ***						2" Ice	2.46	2.46	0.09
OA20-67-DIN	А	From Leg	4.00	-90.0000	172.00	No Ice	2.00	2.00	0.01
		e	0.00			1/2" Ice	3.03	3.03	0.02
			-4.00			1" Ice	4.06	4.06	0.03
						2" Ice	6.12	6.12	0.06
LS-230C	А	From Leg	4.00	-90.0000	172.00	No Ice	1.61	1.61	0.01
		5	0.00			1/2" Ice	2.34	2.34	0.02

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tnxTower		CT364/Chapel St. Monopole (BU# 823530)	7 of 17
EDIL La Grandania Anna Samiana	Project		Date
FDH Infrastructure Services 6521 Meridien Drive		19BMUT1400	09:40:29 06/19/19
Raleigh, NC 27616 Phone: 919.755.1012 FAX: 919.755.1031	Client	Crown Castle	Designed by Aditya Chingale

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weight
	Leg		Vert ft	o	ft		ft²	ft²	K
			ft ft		51		<i>J</i> •	<i></i>	
			-4.00			1" Ice	2.80	2.80	0.04
***						2" Ice	3.68	3.68	0.09
APXVAARR24_43-U-NA20	А	From Leg	4.00	0.0000	172.00	No Ice	14.69	6.87	0.19
w/ Mount Pipe			0.00			1/2" Ice	15.46	7.55	0.31
			0.00			1" Ice 2" Ice	16.23 17.82	8.25 9.67	0.46 0.79
APXVAARR24_43-U-NA20	С	From Leg	4.00	0.0000	172.00	No Ice	14.69	6.87	0.19
w/ Mount Pipe	-		0.00			1/2" Ice	15.46	7.55	0.31
-			0.00			1" Ice	16.23	8.25	0.46
						2" Ice	17.82	9.67	0.79
APXVAARR24_43-U-NA20	А	From Leg	4.00	-90.0000	172.00	No Ice	14.69	6.87	0.19
w/ Mount Pipe			0.00 0.00			1/2" Ice 1" Ice	15.46 16.23	7.55 8.25	0.31 0.46
			0.00			2" Ice	17.82	9.67	0.79
RR90-17-02DP w/ Mount	А	From Leg	4.00	0.0000	172.00	No Ice	4.59	3.32	0.03
Pipe		-	0.00			1/2" Ice	5.02	4.09	0.07
			0.00			1" Ice	5.44	4.78	0.12
	C	г т	1.00	0.0000	172.00	2" Ice	6.30	6.23	0.22
RR90-17-02DP w/ Mount	С	From Leg	4.00	0.0000	172.00	No Ice	4.59	3.32	0.03
Pipe			$\begin{array}{c} 0.00 \\ 0.00 \end{array}$			1/2" Ice 1" Ice	5.02 5.44	4.09 4.78	0.07 0.12
			0.00			2" Ice	6.30	6.23	0.12
RR90-17-02DP w/ Mount	А	From Face	4.00	-90.0000	172.00	No Ice	4.59	3.32	0.03
Pipe			0.00			1/2" Ice	5.02	4.09	0.07
-			0.00			1" Ice	5.44	4.78	0.12
						2" Ice	6.30	6.23	0.22
KRY 112 144/1	А	From Leg	4.00	0.0000	172.00	No Ice	0.35	0.16	0.01
			$\begin{array}{c} 0.00\\ 0.00\end{array}$			1/2" Ice 1" Ice	0.43 0.51	0.22 0.28	$\begin{array}{c} 0.01 \\ 0.02 \end{array}$
			0.00			2" Ice	0.31	0.28	0.02
KRY 112 144/1	С	From Leg	4.00	0.0000	172.00	No Ice	0.35	0.16	0.05
	÷		0.00			1/2" Ice	0.43	0.22	0.01
			0.00			1" Ice	0.51	0.28	0.02
						2" Ice	0.70	0.44	0.03
KRY 112 144/1	А	From Leg	4.00	-90.0000	172.00	No Ice	0.35	0.16	0.01
			0.00			1/2" Ice	0.43	0.22	0.01
			0.00			1" Ice 2" Ice	0.51 0.70	0.28 0.44	0.02 0.03
KRY 112 489/2	А	From Leg	4.00	0.0000	172.00	No Ice	0.70	0.44	0.03
KKT 112 409/2	11	Tiom Leg	0.00	0.0000	172.00	1/2" Ice	0.66	0.45	0.02
			0.00			1" Ice	0.76	0.54	0.03
						2" Ice	1.00	0.75	0.05
KRY 112 489/2	С	From Leg	4.00	0.0000	172.00	No Ice	0.56	0.37	0.02
			0.00			1/2" Ice	0.66	0.45	0.02
			0.00			1" Ice	0.76	0.54	0.03
KRY 112 489/2	А	From Leg	4.00	-90.0000	172.00	2" Ice No Ice	1.00 0.56	0.75 0.37	$0.05 \\ 0.02$
KK I 112 407/2	А	From Leg	4.00 0.00	-90.0000	172.00	1/2" Ice	0.36	0.37	0.02
			0.00			172 Ice	0.00	0.54	0.02
						2" Ice	1.00	0.75	0.05
(2) RADIO 4449 B12/B71	А	From Leg	4.00	0.0000	172.00	No Ice	1.65	1.30	0.08
			0.00			1/2" Ice	1.81	1.44	0.09
			0.00			1" Ice	1.98	1.60	0.11
DADIO 4440 D10/071	C	Eron Las	4.00	0.0000	172.00	2" Ice	2.34	1.92	0.16
RADIO 4449 B12/B71	С	From Leg	4.00	0.0000	172.00	No Ice	1.65	1.30	0.08

	Job		Page
tnxTower		CT364/Chapel St. Monopole (BU# 823530)	8 of 17
EDII Infrastructure Comicos	Project		Date
FDH Infrastructure Services 6521 Meridien Drive		19BMUT1400	09:40:29 06/19/19
Raleigh, NC 27616	Client		Designed by
Phone: 919.755.1012 FAX: 919.755.1031		Crown Castle	Aditya Chingale

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weigh
	Leg		Lateral						
			Vert ft	0	ft		ft ²	ft^2	K
			ft		Ji		ji	ji	K
						1/2" Ice	1.81	1.44	0.09
			0.00			172 Icc 1" Ice	1.98	1.44	0.11
			0.00			2" Ice	2.34	1.92	0.16
Pipe Mount	А	From Leg	4.00	0.0000	172.00	No Ice	1.20	1.20	0.02
			0.00			1/2" Ice	1.50	1.50	0.03
			0.00			1" Ice	1.81	1.81	0.04
						2" Ice	2.47	2.47	0.08
(3) Pipe Mount	С	From Leg	4.00	0.0000	172.00	No Ice	1.20	1.20	0.02
			0.00			1/2" Ice	1.50	1.50	0.03
			0.00			1" Ice	1.81	1.81	0.04
						2" Ice	2.47	2.47	0.08
(2) Pipe Mount	А	From Leg	4.00	-90.0000	172.00	No Ice	1.20	1.20	0.02
			0.00			1/2" Ice	1.50	1.50	0.03
			0.00			1" Ice	1.81	1.81	0.04
Dattorm Mount II D 701 11	C	Nona		0.0000	172.00	2" Ice	2.47	2.47	0.08
Platform Mount [LP 701-1]	С	None		0.0000	172.00	No Ice 1/2" Ice	59.15 71.12	59.15 71.12	2.75 3.42
						172 Ice	83.09	83.09	4.10
						2" Ice	107.03	107.03	5.45
168						2 100	107.05	107.05	5.45
LS-230C	А	From Face	3.00	0.0000	168.00	No Ice	1.61	1.61	0.01
2500	11	1101111400	0.00	0.0000	100.00	1/2" Ice	2.34	2.34	0.02
			3.00			1" Ice	2.80	2.80	0.04
						2" Ice	3.68	3.68	0.09
ide Arm Mount [SO 701-1]	А	From Face	1.50	0.0000	168.00	No Ice	0.85	1.67	0.07
			0.00			1/2" Ice	1.14	2.34	0.08
			0.00			1" Ice	1.43	3.01	0.09
						2" Ice	2.01	4.35	0.12
162									
APXVTM14-C-120 w/	А	From Leg	4.00	0.0000	162.00	No Ice	4.09	2.86	0.08
Mount Pipe			0.00			1/2" Ice	4.48	3.23	0.13
			0.00			1" Ice	4.88	3.61	0.19
APXVTM14-C-120 w/	р	Enom Loo	4.00	0.0000	162.00	2" Ice	5.71 4.09	4.40 2.86	0.33
Mount Pipe	В	From Leg	4.00 0.00	0.0000	162.00	No Ice 1/2" Ice	4.09	3.23	0.08 0.13
Mount Fipe			0.00			172 Ice	4.48	3.23	0.13
			0.00			2" Ice	5.71	4.40	0.19
APXVTM14-C-120 w/	С	From Leg	4.00	0.0000	162.00	No Ice	4.09	2.86	0.08
Mount Pipe	Ū.	110111 208	0.00	0.0000	102100	1/2" Ice	4.48	3.23	0.13
			0.00			1" Ice	4.88	3.61	0.19
						2" Ice	5.71	4.40	0.33
APXVSPP18-C-A20 w/	А	From Leg	4.00	0.0000	162.00	No Ice	4.60	4.01	0.10
Mount Pipe			0.00			1/2" Ice	5.05	4.45	0.16
			0.00			1" Ice	5.50	4.89	0.23
		_				2" Ice	6.44	5.82	0.42
APXVSPP18-C-A20 w/	в	From Leg	4.00	0.0000	162.00	No Ice	4.60	4.01	0.10
Mount Pipe			0.00			1/2" Ice	5.05	4.45	0.16
			0.00			1" Ice	5.50	4.89	0.23
ADVICIDD10 C A20 /	C	Enour I	4 00	0.0000	1(2.00	2" Ice	6.44	5.82	0.42
APXVSPP18-C-A20 w/ Mount Pine	С	From Leg	4.00	0.0000	162.00	No Ice 1/2" Ice	4.60	4.01	0.10
Mount Pipe			$\begin{array}{c} 0.00\\ 0.00\end{array}$			1/2" Ice	5.05 5.50	4.45 4.89	0.16 0.23
			0.00			2" Ice	5.50 6.44	4.89 5.82	0.23
TD-RRH8x20-25	А	From Leg	4.00	0.0000	162.00	No Ice	3.70	3.82 1.29	0.42
1D INV10720-23	17	110m Leg	0.00	0.0000	102.00	1/2" Ice	3.95	1.29	0.07
			0.00			172 Ice	4.20	1.64	0.12
			0.00			I ICC	4.20	1.04	

Project

Client

CT364/Chapel St. Monopole (BU# 823530)

FDH Infrastructure Services 6521 Meridien Drive Raleigh, NC 27616 Phone: 919.755.1012 FAX: 919.755.1031

Crown Castle

19BMUT1400

Designed by Aditya Chingale

09:40:29 06/19/19

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weight
	Leg		Lateral						
			Vert	0	C.		<i>c.</i> ?	c.2	V
			ft ft	Ŭ	ft		ft²	ft^2	K
TD DD119-20 25	D	Enom Loo	ft	0.0000	162.00	No Ioo	2 70	1.20	0.07
TD-RRH8x20-25	В	From Leg	$\begin{array}{c} 4.00\\ 0.00 \end{array}$	0.0000	162.00	No Ice 1/2" Ice	3.70 3.95	1.29 1.46	$\begin{array}{c} 0.07 \\ 0.09 \end{array}$
			0.00			1/2 Ice	3.93 4.20	1.46	0.09
			0.00			2" Ice	4.20	2.02	0.12
TD-RRH8x20-25	С	From Leg	4.00	0.0000	162.00	No Ice	4.72 3.70	1.29	0.18
1D-RR18820-25	C	From Leg	4.00 0.00	0.0000	102.00	1/2" Ice	3.95	1.46	0.07
			0.00			1" Ice	4.20	1.64	0.12
			0.00			2" Ice	4.72	2.02	0.12
800MHz 2X50W RRH	А	From Leg	4.00	0.0000	162.00	No Ice	2.06	1.93	0.06
W/FILTER		i iom Log	0.00	0.0000	102.00	1/2" Ice	2.24	2.11	0.09
			0.00			1" Ice	2.43	2.29	0.11
						2" Ice	2.83	2.68	0.17
800MHz 2X50W RRH	в	From Leg	4.00	0.0000	162.00	No Ice	2.06	1.93	0.06
W/FILTER		C	0.00			1/2" Ice	2.24	2.11	0.09
			0.00			1" Ice	2.43	2.29	0.11
						2" Ice	2.83	2.68	0.17
800MHz 2X50W RRH	С	From Leg	4.00	0.0000	162.00	No Ice	2.06	1.93	0.06
W/FILTER			0.00			1/2" Ice	2.24	2.11	0.09
			0.00			1" Ice	2.43	2.29	0.11
						2" Ice	2.83	2.68	0.17
PCS 1900MHz 2x40W	А	From Leg	4.00	0.0000	162.00	No Ice	2.35	1.28	0.04
			0.00			1/2" Ice	2.55	1.43	0.06
			0.00			1" Ice	2.75	1.60	0.08
						2" Ice	3.18	1.95	0.14
PCS 1900MHz 2x40W	в	From Leg	4.00	0.0000	162.00	No Ice	2.35	1.28	0.04
			0.00			1/2" Ice	2.55	1.43	0.06
			0.00			1" Ice	2.75	1.60	0.08
	~					2" Ice	3.18	1.95	0.14
PCS 1900MHz 2x40W	С	From Leg	4.00	0.0000	162.00	No Ice	2.35	1.28	0.04
			0.00			1/2" Ice	2.55	1.43	0.06
			0.00			1" Ice	2.75	1.60	0.08
(C) M (UD 712 1)	C	N		0.0000	1(2.00	2" Ice	3.18	1.95	0.14
atform Mount [LP 712-1]	С	None		0.0000	162.00	No Ice	24.53	24.53	1.34
						1/2" Ice 1" Ice	29.94 35.35	29.94 35.35	1.65
						2" Ice	33.33 46.17	35.55 46.17	1.96 2.58
Pipe Mount	А	From Leg	4.00	0.0000	162.00	No Ice	1.20	1.20	0.02
r ipe Mount	A	rioni Leg	4.00 0.00	0.0000	102.00	1/2" Ice	1.20	1.20	0.02
			0.00			172 Ice	1.81	1.81	0.03
			0.00			2" Ice	2.47	2.47	0.04
Pipe Mount	В	From Leg	4.00	0.0000	162.00	No Ice	1.20	1.20	0.03
Tipe Would	Ъ	110m Leg	0.00	0.0000	102.00	1/2" Ice	1.50	1.20	0.02
			0.00			172 Ice	1.81	1.81	0.04
			0.00			2" Ice	2.47	2.47	0.08
Pipe Mount	С	From Leg	4.00	0.0000	162.00	No Ice	1.20	1.20	0.02
i ipe tribuit	Ũ	Tiom Dog	0.00	0.0000	102.00	1/2" Ice	1.50	1.50	0.02
			0.00			1" Ice	1.81	1.81	0.04
						2" Ice	2.47	2.47	0.08
152									
NNHH-65B-R4 w/ Mount	А	From Leg	3.00	0.0000	152.00	No Ice	7.55	4.23	0.11
Pipe		Ũ	0.00			1/2" Ice	8.04	4.67	0.20
-			0.00			1" Ice	8.53	5.12	0.30
						2" Ice	9.56	6.05	0.53
NNHH-65B-R4 w/ Mount	В	From Leg	3.00	0.0000	152.00	No Ice	7.55	4.23	0.11
Pipe		-	0.00			1/2" Ice	8.04	4.67	0.20
			0.00			1" Ice	8.53	5.12	0.30
						2" Ice	9.56	6.05	0.53

	Job
tnxTower	

Project

Client

CT364/Chapel St. Monopole (BU# 823530)

19BMUT1400

FDH Infrastructure Services 6521 Meridien Drive Raleigh, NC 27616 Phone: 919.755.1012 FAX: 919.755.1031

Crown Castle

Date 09:40:29 06/19/19 Designed by Aditya Chingale

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Page

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_A A_A$ Front	C _A A _A Side	Weight
	Leg		Lateral						
			Vert	o	Ċ.		c.2	<i>c.</i> ?	17
			ft A	0	ft		ft^2	ft^2	K
			ft ft						
(2) NNHH-65B-R4 w/ Mount	С	From Leg	3.00	0.0000	152.00	No Ice	7.55	4.23	0.11
Pipe		Ū.	0.00			1/2" Ice	8.04	4.67	0.20
			0.00			1" Ice	8.53	5.12	0.30
						2" Ice	9.56	6.05	0.53
(2) LPA-80080/4CF w/	А	From Leg	3.00	0.0000	152.00	No Ice	2.62	5.40	0.01
Mount Pipe			0.00			1/2" Ice	2.92	5.73	0.05
			0.00			1" Ice 2" Ice	3.23	6.06 6.75	0.08
(2) LPA-80080/4CF w/	в	From Leg	3.00	0.0000	152.00	No Ice	3.85 2.62	6.75 5.40	$\begin{array}{c} 0.17\\ 0.01 \end{array}$
Mount Pipe	Б	FIOII Leg	0.00	0.0000	132.00	1/2" Ice	2.02	5.73	0.01
Would Tipe			0.00			172 Ice	3.23	6.06	0.03
			0.00			2" Ice	3.85	6.75	0.00
(2) LPA-80080/4CF w/	С	From Leg	3.00	0.0000	152.00	No Ice	2.62	5.40	0.01
Mount Pipe			0.00			1/2" Ice	2.92	5.73	0.05
1			0.00			1" Ice	3.23	6.06	0.08
						2" Ice	3.85	6.75	0.17
RFV01U-D2A	А	From Leg	3.00	0.0000	152.00	No Ice	1.88	1.01	0.07
			0.00			1/2" Ice	2.05	1.14	0.09
			0.00			1" Ice	2.22	1.28	0.11
						2" Ice	2.60	1.59	0.15
RFV01U-D2A	В	From Leg	3.00	0.0000	152.00	No Ice	1.88	1.01	0.07
			0.00			1/2" Ice	2.05	1.14	0.09
			0.00			1" Ice	2.22	1.28	0.11
DEVAIL DOA	C	Enom Loo	2.00	0.0000	152.00	2" Ice	2.60	1.59	0.15
RFV01U-D2A	С	From Leg	3.00 0.00	0.0000	152.00	No Ice 1/2" Ice	1.88 2.05	$\begin{array}{c} 1.01\\ 1.14\end{array}$	$0.07 \\ 0.09$
			0.00			172 Ice	2.03	1.14	0.09
			0.00			2" Ice	2.60	1.59	0.11
RFV01U-D1A	А	From Leg	3.00	0.0000	152.00	No Ice	1.88	1.25	0.08
la tore bill	11	Trom Leg	0.00	0.0000	152.00	1/2" Ice	2.05	1.39	0.00
			0.00			1" Ice	2.22	1.54	0.12
						2" Ice	2.60	1.86	0.18
RFV01U-D1A	В	From Leg	3.00	0.0000	152.00	No Ice	1.88	1.25	0.08
		-	0.00			1/2" Ice	2.05	1.39	0.10
			0.00			1" Ice	2.22	1.54	0.12
						2" Ice	2.60	1.86	0.18
RFV01U-D1A	С	From Leg	3.00	0.0000	152.00	No Ice	1.88	1.25	0.08
			0.00			1/2" Ice	2.05	1.39	0.10
			0.00			1" Ice	2.22	1.54	0.12
BWZDC 6600 DE 49	р	Enom Log	2.00	0.0000	152.00	2" Ice	2.60	1.86	0.18
RVZDC-6600-PF-48	В	From Leg	3.00 0.00	0.0000	152.00	No Ice 1/2" Ice	4.06 4.32	3.10 3.34	0.03 0.07
			0.00			172 Ice	4.52	3.54	0.07
			0.00			2" Ice	5.14	4.09	0.20
(2) 2.375" x 10' Horizontal	А	From Leg	3.00	0.0000	152.00	No Ice	2.38	0.05	0.04
Pipe	11	riom Leg	0.00	0.0000	152.00	1/2" Ice	3.06	0.08	0.06
			0.00			1" Ice	3.75	0.11	0.09
						2" Ice	5.15	0.21	0.18
(2) 2.375" x 10' Horizontal	В	From Leg	3.00	0.0000	152.00	No Ice	2.38	0.05	0.04
Pipe		-	0.00			1/2" Ice	3.06	0.08	0.06
			0.00			1" Ice	3.75	0.11	0.09
		_				2" Ice	5.15	0.21	0.18
(2) 2.375" x 10' Horizontal	С	From Leg	3.00	0.0000	152.00	No Ice	2.38	0.05	0.04
Pipe			0.00			1/2" Ice	3.06	0.08	0.06
			0.00			1" Ice	3.75	0.11	0.09
Harry 12 HDNIV D ICM	C	NLesse		0.0000	152.00	2" Ice	5.15	0.21	0.18
Heavy 12' UPNY Boom [SM	С	None		0.0000	152.00	No Ice	20.40	20.40	0.88

tnxTower	Job	CT364/Chapel St. Monopole (BU# 823530)	Page 11 of 17
FDH Infrastructure Services 6521 Meridien Drive	Project	19BMUT1400	Date 09:40:29 06/19/19
Raleigh, NC 27616 Phone: 919.755.1012 FAX: 919.755.1031	Client	Crown Castle	Designed by Aditya Chingale

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weight
	Leg		Lateral Vert						
			ft	0	ft		ft²	ft²	K
			ft		<i></i>		<i>J</i> •	55	
801-3]			ft			1/2" Ice	26.30	26.30	1.25
-						1" Ice	32.20	32.20	1.63
						2" Ice	44.00	44.00	2.39
142 7770.00 w/ Mount Pipe		Erom Log	3.00	0.0000	142.00	No Ice	5.75	4.25	0.06
7770.00 w/ Would Pipe	А	From Leg	0.00	0.0000	142.00	1/2" Ice	6.18	4.23 5.01	0.08
			1.00			1" Ice	6.61	5.71	0.16
			1.00			2" Ice	7.49	7.16	0.29
7770.00 w/ Mount Pipe	В	From Leg	3.00	0.0000	142.00	No Ice	5.75	4.25	0.06
		C	0.00			1/2" Ice	6.18	5.01	0.10
			1.00			1" Ice	6.61	5.71	0.16
	-					2" Ice	7.49	7.16	0.29
7770.00 w/ Mount Pipe	С	From Leg	3.00	0.0000	142.00	No Ice	5.75	4.25	0.06
			0.00			1/2" Ice	6.18	5.01	0.10
			1.00			1" Ice 2" Ice	6.61 7.49	5.71 7.16	0.16 0.29
HPA65R-BU6A w/ Mount	А	From Leg	3.00	0.0000	142.00	No Ice	7.49 8.09	7.16	0.29
Pipe	п	110m Leg	0.00	0.0000	142.00	1/2" Ice	8.64	8.36	0.14
Tipe			1.00			1" Ice	9.16	9.24	0.21
						2" Ice	10.22	11.05	0.39
HPA65R-BU6A w/ Mount	С	From Leg	3.00	0.0000	142.00	No Ice	8.09	7.19	0.07
Pipe			0.00			1/2" Ice	8.64	8.36	0.14
			1.00			1" Ice	9.16	9.24	0.21
						2" Ice	10.22	11.05	0.39
HPA65R-BU4A w/ Mount	В	From Leg	3.00	0.0000	142.00	No Ice	5.20	4.66	0.05
Pipe			0.00			1/2" Ice	5.58	5.27	0.10
			1.00			1" Ice	5.97	5.89	0.15
(2) 80010065/ Mount Ding		From Leg	3.00	0.0000	142.00	2" Ice No Ice	6.79 13.81	7.18 7.16	0.28 0.13
(2) 80010965 w/ Mount Pipe	А	FIOII Leg	0.00	0.0000	142.00	1/2" Ice	13.81	7.96	0.13
			1.00			172 Ice	14.35	8.77	0.22
			1.00			2" Ice	15.99	10.44	0.52
(2) 80010964 w/ Mount Pipe	В	From Leg	3.00	0.0000	142.00	No Ice	10.23	5.51	0.11
() · · · · · · · · · · · · · · · · · · ·			0.00			1/2" Ice	10.74	6.37	0.18
			1.00			1" Ice	11.24	7.12	0.26
						2" Ice	12.25	8.64	0.45
(2) 80010965 w/ Mount Pipe	С	From Leg	3.00	0.0000	142.00	No Ice	13.81	7.16	0.13
			0.00			1/2" Ice	14.35	7.96	0.22
			1.00			1" Ice	14.89	8.77	0.32
			2 00	0.0000	1.10.00	2" Ice	15.99	10.44	0.55
(2) LGP21401	А	From Leg	3.00	0.0000	142.00	No Ice	1.10	0.35	0.01
			0.00			1/2" Ice	1.24	0.44	0.02
			1.00			1" Ice 2" Ice	1.38 1.69	0.54 0.77	0.03 0.05
(2) LGP21401	В	From Leg	3.00	0.0000	142.00	No Ice	1.09	0.77	0.05
(2) LOI 21401	Б	From Leg	0.00	0.0000	142.00	1/2" Ice	1.10	0.33	0.01
			1.00			1" Ice	1.38	0.54	0.02
			1100			2" Ice	1.69	0.77	0.05
(2) LGP21401	С	From Leg	3.00	0.0000	142.00	No Ice	1.10	0.35	0.01
· ·		0	0.00			1/2" Ice	1.24	0.44	0.02
			1.00			1" Ice	1.38	0.54	0.03
						2" Ice	1.69	0.77	0.05
RRUS 4478 B14	А	From Leg	3.00	0.0000	142.00	No Ice	1.84	1.06	0.06
			0.00			1/2" Ice	2.01	1.20	0.08
			1.00			1" Ice	2.19	1.34	0.09
DDUG 4479 D14	P	Farm I	2.00	0.0000	142.00	2" Ice	2.57	1.66	0.14
RRUS 4478 B14	В	From Leg	3.00	0.0000	142.00	No Ice	1.84	1.06	0.06

	Job		Page
tnxTower		CT364/Chapel St. Monopole (BU# 823530)	12 of 17
	Project		Date
FDH Infrastructure Services 6521 Meridien Drive		19BMUT1400	09:40:29 06/19/19
Raleigh, NC 27616	Client		Designed by
Phone: 919.755.1012 FAX: 919.755.1031		Crown Castle	Aditya Chingale

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_A A_A$ Front	C _A A _A Side	Weight
	Leg		Lateral Vert						
			ft	o	ft		ft^2	ft^2	Κ
			ft ft		-		-	-	
			0.00			1/2" Ice	2.01	1.20	0.08
			1.00			1" Ice	2.19	1.34	0.09
	~		2 0 0	0.0000	1 49 00	2" Ice	2.57	1.66	0.14
RRUS 4478 B14	С	From Leg	3.00	0.0000	142.00	No Ice	1.84	1.06	0.06
			$\begin{array}{c} 0.00\\ 1.00\end{array}$			1/2" Ice 1" Ice	2.01 2.19	1.20 1.34	0.08 0.09
			1.00			2" Ice	2.19	1.66	0.14
DC6-48-60-18-8F	А	From Leg	3.00	0.0000	142.00	No Ice	1.21	1.21	0.03
			0.00			1/2" Ice	1.89	1.89	0.05
			1.00			1" Ice	2.11	2.11	0.08
						2" Ice	2.57	2.57	0.14
DC6-48-60-18-8F	В	From Leg	3.00	0.0000	142.00	No Ice	1.21	1.21	0.03
			0.00			1/2" Ice	1.89	1.89	0.05
			1.00			1" Ice	2.11	2.11	0.08
DC6-48-60-18-8F	С	From Face	1.00	0.0000	142.00	2" Ice No Ice	2.57 1.21	2.57 1.21	0.14 0.03
DC0-40-00-10-0F	C	FIOIII Face	0.00	0.0000	142.00	1/2" Ice	1.21	1.21	0.03
			0.00			1/2 Ice	2.11	2.11	0.03
			0.00			2" Ice	2.57	2.57	0.14
RADIO 4415 B30	А	From Leg	3.00	0.0000	142.00	No Ice	1.64	0.64	0.04
		0	0.00			1/2" Ice	1.80	0.75	0.05
			1.00			1" Ice	1.97	0.87	0.07
						2" Ice	2.33	1.13	0.11
RADIO 4415 B30	В	From Leg	3.00	0.0000	142.00	No Ice	1.64	0.64	0.04
			0.00			1/2" Ice	1.80	0.75	0.05
			1.00			1" Ice	1.97	0.87	0.07
RADIO 4415 B30	С	From Leg	3.00	0.0000	142.00	2" Ice No Ice	2.33 1.64	1.13 0.64	0.11 0.04
KADIO 4415 D50	C	rioin Leg	0.00	0.0000	142.00	1/2" Ice	1.80	0.04	0.04
			1.00			1/2 lee	1.97	0.87	0.05
			1.00			2" Ice	2.33	1.13	0.11
RRUS 4449 B5/B12	А	From Leg	3.00	0.0000	142.00	No Ice	1.97	1.41	0.07
			0.00			1/2" Ice	2.14	1.56	0.09
			1.00			1" Ice	2.33	1.73	0.11
						2" Ice	2.72	2.07	0.16
RRUS 4449 B5/B12	В	From Leg	3.00	0.0000	142.00	No Ice	1.97	1.41	0.07
			0.00			1/2" Ice	2.14	1.56	0.09
			1.00			1" Ice 2" Ice	2.33 2.72	1.73 2.07	0.11
RRUS 4449 B5/B12	С	From Leg	3.00	0.0000	142.00	No Ice	2.72 1.97	2.07	0.16 0.07
KKU5 4449 DJ/D12	C	From Leg	0.00	0.0000	142.00	1/2" Ice	2.14	1.56	0.07
			1.00			1" Ice	2.33	1.73	0.11
			1.00			2" Ice	2.72	2.07	0.16
RRUS 8843 B2/B66A	А	From Leg	3.00	0.0000	142.00	No Ice	1.64	1.35	0.07
		-	0.00			1/2" Ice	1.80	1.50	0.09
			1.00			1" Ice	1.97	1.65	0.11
	_					2" Ice	2.32	1.99	0.16
RRUS 8843 B2/B66A	В	From Leg	3.00	0.0000	142.00	No Ice	1.64	1.35	0.07
			0.00			1/2" Ice	1.80	1.50	0.09
			1.00			1" Ice 2" Ice	1.97 2.32	1.65 1.99	0.11 0.16
RRUS 8843 B2/B66A	С	From Leg	3.00	0.0000	142.00	No Ice	2.32 1.64	1.99	0.16
11100 0073 D2/D00A	C	r tom Leg	0.00	0.0000	172.00	1/2" Ice	1.80	1.55	0.07
			1.00			1" Ice	1.97	1.65	0.11
						2" Ice	2.32	1.99	0.16
latform Mount [LP 303-1]	С	None		0.0000	142.00	No Ice	14.66	14.66	1.25
						1/2" Ice	18.87	18.87	1.48

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FDH Infrastructure Services 6521 Meridien Drive	Project	19BMUT1400	Date 09:40:29 06/19/19
Raleigh, NC 27616 Phone: 919.755.1012 FAX: 919.755.1031	Client	Crown Castle	Designed by Aditya Chingale

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	C _A A _A Side	Weight
			Vert ft ft ft	o	ft		ft²	ft²	Κ
						1" Ice	23.08	23.08	1.71
						2" Ice	31.50	31.50	2.18
Miscellaneous [NA 507-1]	С	None		0.0000	142.00	No Ice	4.80	4.80	0.25
						1/2" Ice	6.70	6.70	0.29
						1" Ice	8.60	8.60	0.34
						2" Ice	12.40	12.40	0.44
115									
APXV18-206517S-C w/	А	From Leg	0.50	0.0000	115.00	No Ice	3.79	3.16	0.05
Mount Pipe			0.00			1/2" Ice	4.38	3.75	0.09
			0.00			1" Ice	4.99	4.35	0.15
						2" Ice	6.25	5.59	0.28
APXV18-206517S-C w/	в	From Leg	0.50	0.0000	115.00	No Ice	3.79	3.16	0.05
Mount Pipe			0.00			1/2" Ice	4.38	3.75	0.09
			0.00			1" Ice	4.99	4.35	0.15
						2" Ice	6.25	5.59	0.28
APXV18-206517S-C w/	С	From Leg	0.50	0.0000	115.00	No Ice	3.79	3.16	0.05
Mount Pipe			0.00			1/2" Ice	4.38	3.75	0.09
			0.00			1" Ice	4.99	4.35	0.15
						2" Ice	6.25	5.59	0.28
50	٨	From Face	0.50	0.0000	50.00	No Ice	0.85	1.67	0.07
Side Arm Mount [SO 701-1]	А	From Face	0.30	0.0000	50.00	1/2" Ice	0.85	2.34	0.07
			0.00			1/2 Ice	1.14	2.34	0.08
			0.00			2" Ice	2.01	4.35	0.09
GPS-TMG-HR-26NCM	А	From Face	3.00	0.0000	50.00	No Ice	0.13	4.33 0.13	0.12
UF 5- HVIU-FIK-20INCIM	А	From Face	3.00 0.00	0.0000	50.00	1/2" Ice	0.13	0.13	0.00
						1/2" Ice	0.18		
			0.00			1" Ice 2" Ice	0.24 0.37	0.24 0.37	0.01 0.01
***						2 100	0.57	0.57	0.01

Dishes											
Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				Vert ft	o	0	ft	ft		ft^2	K
VHLP2.6	А	Paraboloid	From	4.00	0.0000		172.00	2.92	No Ice	6.68	0.05
		w/Shroud (HP)	Leg	0.00					1/2" Ice	7.07	0.08
				3.00					1" Ice	7.46	0.12
									2" Ice	8.23	0.19
VHLP2.6	А	Paraboloid	From	4.00	0.0000		172.00	2.92	No Ice	6.68	0.05
		w/Shroud (HP)	Leg	0.00					1/2" Ice	7.07	0.08
				3.00					1" Ice	7.46	0.12
***									2" Ice	8.23	0.19

tnxTower

Project

Client

Load Combinations

Comb. No.	Description	
<u>1</u>	Dead Only	
2	1.2 Dead+1.0 Wind 0 deg - No Ice	
3	0.9 Dead+1.0 Wind 0 deg - No lice	
4	1.2 Dead+1.0 Wind 30 deg - No Ice	
5	0.9 Dead+1.0 Wind 30 deg - No Ice	
6	1.2 Dead+1.0 Wind 60 deg - No Ice	
7	0.9 Dead+1.0 Wind 60 deg - No Ice	
8	1.2 Dead+1.0 Wind 90 deg - No Ice	
9	0.9 Dead+1.0 Wind 90 deg - No Ice	
10	1.2 Dead+1.0 Wind 120 deg - No Ice	
11	0.9 Dead+1.0 Wind 120 deg - No Ice	
12	1.2 Dead+1.0 Wind 150 deg - No Ice	
12	0.9 Dead+1.0 Wind 150 deg - No Ice	
13	1.2 Dead+1.0 Wind 180 deg - No Ice	
14	0.9 Dead+1.0 Wind 180 deg - No Ice	
16	1.2 Dead+1.0 Wind 210 deg - No Ice	
17	0.9 Dead+1.0 Wind 210 deg - No Ice	
17	1.2 Dead+1.0 Wind 240 deg - No Ice	
19	0.9 Dead+1.0 Wind 240 deg - No Ice	
20	1.2 Dead+1.0 Wind 270 deg - No Ice	
20	0.9 Dead+1.0 Wind 270 deg - No Ice	
22	1.2 Dead+1.0 Wind 300 deg - No Ice	
23	0.9 Dead+1.0 Wind 300 deg - No Ice	
24	1.2 Dead+1.0 Wind 330 deg - No Ice	
25	0.9 Dead+1.0 Wind 330 deg - No Ice	
26	1.2 Dead+1.0 Ice+1.0 Temp	
20	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	
30	1.2 Dead+1.0 Wind 00 deg+1.0 Ice+1.0 Temp	
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp	
39	Dead+Wind 0 deg - Service	
40	Dead+Wind 30 deg - Service	
41	Dead+Wind 60 deg - Service	
42	Dead+Wind 90 deg - Service	
43	Dead+Wind 120 deg - Service	
44	Dead+Wind 150 deg - Service	
45	Dead+Wind 180 deg - Service	
46	Dead+Wind 210 deg - Service	
47	Dead+Wind 240 deg - Service	
48	Dead+Wind 270 deg - Service	
49	Dead+Wind 300 deg - Service	
50	Dead+Wind 330 deg - Service	

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FDH Infrastructure Services 6521 Meridien Drive	Project	19BMUT1400	Date 09:40:29 06/19/19	
Raleigh, NC 27616 Client Phone: 919.755.1012 FAX: 919.755.1031		Crown Castle	Designed by Aditya Chingale	

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	175 - 164.25	24.736	40	1.1867	0.0162
L2	167.17 - 129.67	22.794	40	1.1805	0.0137
L3	133.5 - 96	14.877	46	1.0329	0.0063
L4	100.67 - 63.17	8.528	46	0.7957	0.0034
L5	68.67 - 31.17	3.994	46	0.5400	0.0020
L6	37.42 - 0	1.214	46	0.2910	0.0009

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	o	0	ft
175.00	VHLP2.6	40	24.736	1.1867	0.0168	48091
172.00	OA20-67-DIN	40	23.991	1.1850	0.0158	48091
168.00	LS-230C	40	22.999	1.1816	0.0144	35179
162.00	APXVTM14-C-120 w/ Mount Pipe	40	21.521	1.1703	0.0126	22102
152.00	(2) NNHH-65B-R4 w/ Mount Pipe	40	19.102	1.1354	0.0100	14281
142.00	7770.00 w/ Mount Pipe	46	16.772	1.0847	0.0080	10542
115.00	APXV18-206517S-C w/ Mount Pipe	46	11.097	0.9045	0.0046	7761
50.00	Side Arm Mount [SO 701-1]	46	2.115	0.3905	0.0013	6346

Maximum Tower Deflections - Design Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	175 - 164.25	106.101	16	5.0657	0.0697
L2	167.17 - 129.67	97.817	16	5.0510	0.0593
L3	133.5 - 96	63.876	16	4.4396	0.0273
L4	100.67 - 63.17	36.600	16	3.4207	0.0145
L5	68.67 - 31.17	17.131	16	2.3189	0.0084
L6	37.42 - 0	5.203	16	1.2480	0.0039

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	o	0	ft
175.00	VHLP2.6	16	106.101	5.0657	0.0701	14350
172.00	OA20-67-DIN	16	102.923	5.0636	0.0658	14350
168.00	LS-230C	16	98.693	5.0545	0.0604	10368
162.00	APXVTM14-C-120 w/ Mount Pipe	16	92.384	5.0134	0.0530	5993
152.00	(2) NNHH-65B-R4 w/ Mount Pipe	16	82.036	4.8720	0.0422	3597
142.00	7770.00 w/ Mount Pipe	16	72.022	4.6594	0.0333	2559
115.00	APXV18-206517S-C w/ Mount Pipe	16	47.636	3.8901	0.0190	1828
50.00	Side Arm Mount [SO 701-1]	16	9.069	1.6757	0.0056	1480



Project

Client

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St. Monopole (BU# 823530)	10 01 17
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Crown Castle	Designed by Aditya Chingale

Compression Checks

			Po	le Des	sign l	Data			
Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	Ratio P _u
	ft		ft	ft		in^2	Κ	Κ	$\frac{P_u}{\phi P_n}$
L1	175 - 164.25 (1)	TP26x22x0.25	10.75	0.00	0.0	19.5705	-5.07	1144.87	0.004
L2	164.25 - 129.67 (2)	TP34.0625x24.4135x0.3125	37.50	0.00	0.0	32.4983	-19.14	1901.15	0.010
L3	129.67 - 96 (3)	TP41.75x32.452x0.375	37.50	0.00	0.0	47.8684	- 27.39	2800.30	0.010
L4	96 - 63.17 (4)	TP49.0625x39.8421x0.375	37.50	0.00	0.0	56.3407	-37.02	3295.93	0.011
L5	63.17 - 31.17 (5)	TP56.125x46.9602x0.375	37.50	0.00	0.0	64.5384	-48.16	3775.49	0.013
L6	31.17 - 0 (6)	TP62.9375x53.8475x0.375	37.42	0.00	0.0	74.4650	-63.20	4356.20	0.015

Pole Bending Design Data

Section No.	Elevation	Size	M_{ux}	ϕM_{nx}	Ratio M _{ux}	M_{uy}	ϕM_{ny}	Ratio M _{uy}
	ft		kip-ft	kip-ft	ϕM_{nx}	kip-ft	kip-ft	ϕM_{ny}
L1	175 - 164.25 (1)	TP26x22x0.25	34.32	729.12	0.047	0.00	729.12	0.000
L2	164.25 - 129.67 (2)	TP34.0625x24.4135x0.3125	481.43	1584.18	0.304	0.00	1584.18	0.000
L3	129.67 - 96 (3)	TP41.75x32.452x0.375	1208.12	2847.12	0.424	0.00	2847.12	0.000
L4	96 - 63.17 (4)	TP49.0625x39.8421x0.375	2066.02	3755.71	0.550	0.00	3755.71	0.000
L5	63.17 - 31.17 (5)	TP56.125x46.9602x0.375	3091.12	4686.62	0.660	0.00	4686.62	0.000
L6	31.17 - 0 (6)	TP62.9375x53.8475x0.375	4503.05	5847.24	0.770	0.00	5847.24	0.000

Pole Shear Design Data

Section No.	Elevation	Size	Actual V_u	ϕV_n	Ratio V_u	Actual T _u	ϕT_n	Ratio T_u
	ft		Κ	Κ	ϕV_n	kip-ft	kip-ft	ϕT_n
L1	175 - 164.25 (1)	TP26x22x0.25	6.22	343.46	0.018	3.31	741.85	0.004
L2	164.25 - 129.67 (2)	TP34.0625x24.4135x0.3125	20.32	570.35	0.036	6.47	1636.53	0.004
L3	129.67 - 96 (3)	TP41.75x32.452x0.375	24.06	840.09	0.029	6.46	2958.81	0.002
L4	96 - 63.17 (4)	TP49.0625x39.8421x0.375	29.87	988.78	0.030	7.55	4098.86	0.002
L5	63.17 - 31.17 (5)	TP56.125x46.9602x0.375	35.57	1132.65	0.031	8.98	5378.43	0.002
L6	31.17 - 0 (6)	TP62.9375x53.8475x0.375	39.43	1306.86	0.030	9.23	7160.17	0.001

<i>tnxTower</i>

Project

Client

CT364/C

FDH Infrastructure Services 6521 Meridien Drive Raleigh, NC 27616 Phone: 919.755.1012 FAX: 919.755.1031

Chapel St. Monopole (BU# 823530)	17 of 17
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Pole Interaction Design Data

Section No.	Elevation	Ratio P_u	Ratio M_{ux}	Ratio M_{uy}	Ratio V_u	Ratio T_u	Comb. Stress	Allow. Stress	Criteria
	ft	ϕP_n	ϕM_{nx}	ϕM_{ny}	ϕV_n	ϕT_n	Ratio	Ratio	
L1	175 - 164.25	0.004	0.047	0.000	0.018	0.004	0.052	1.050	4.8.2
	(1)								
L2	164.25 -	0.010	0.304	0.000	0.036	0.004	0.316	1.050	4.8.2
	129.67 (2)								
L3	129.67 - 96 (3)	0.010	0.424	0.000	0.029	0.002	0.435	1.050	4.8.2
L4	96 - 63.17 (4)	0.011	0.550	0.000	0.030	0.002	0.562	1.050	4.8.2
L5	63.17 - 31.17	0.013	0.660	0.000	0.031	0.002	0.673	1.050	4.8.2
	(5)								
L6	31.17 - 0 (6)	0.015	0.770	0.000	0.030	0.001	0.786	1.050	4.8.2

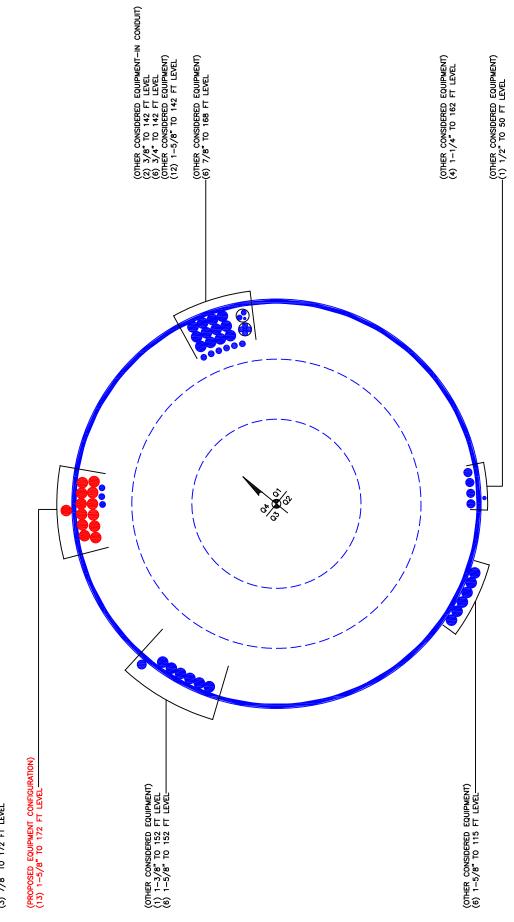
Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	${{{\mathscr O}P}_{allow}} \over K$	% Capacity	Pass Fail
L1	175 - 164.25	Pole	TP26x22x0.25	1	-5.07	1202.11	5.0	Pass
L2	164.25 - 129.67	Pole	TP34.0625x24.4135x0.3125	2	-19.14	1996.21	30.1	Pass
L3	129.67 - 96	Pole	TP41.75x32.452x0.375	3	-27.39	2940.31	41.4	Pass
L4	96 - 63.17	Pole	TP49.0625x39.8421x0.375	4	-37.02	3460.73	53.6	Pass
L5	63.17 - 31.17	Pole	TP56.125x46.9602x0.375	5	- 48.16	3964.26	64.1	Pass
L6	31.17 - 0	Pole	TP62.9375x53.8475x0.375	6	-63.20	4574.01	74.8	Pass
							Summary	
						Pole (L6)	74.8	Pass
						RATING =	74.8	Pass

Program Version 8.0.5.0 - 11/28/2018 File://FDH-server/Projects/2019 Effective - Client Jobs/CROWNC_Crown Castle USA Inc/CT/823530_CT364Chapel St. Monopole/19BMUT1400-STAMOO_TMO/R.0/Analysis/ReportedTower/823530_CT364Chapel St. Monopole_1749544_SA_06-19-2019.eri

APPENDIX B

BASE LEVEL DRAWING





(0THER (3) 7/

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APPENDIX C

ADDITIONAL CALCULATIONS

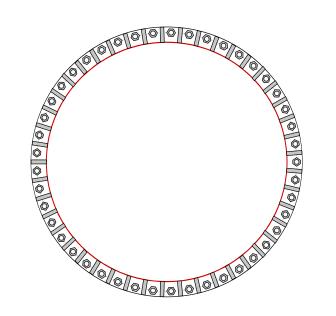
Monopole Base Plate Connection

Site Info		
BU	Ħ	823530
Site Nam	e	CT364/Chapel St
Order	Ħ	479829 Rev 0

Analysis Considerations		
TIA-222 Revision	Н	
Grout Considered:	No	
l _{ar} (in)	1.25	

Applied Loads				
Moment (kip-ft)	4503.05			
Axial Force (kips)	63.20			
Shear Force (kips)	39.43			
*TIA 222 U Castien 15 5 Applied				

*TIA-222-H Section 15.5 Applied



Connection Properties

Anchor Rod Data

(45) 1-1/4" ø bolts (A687 N; Fy=105 ksi, Fu=125 ksi) on 68" BC

Base Plate Data

71" OD x 1.5" Plate (A572-50; Fy=50 ksi, Fu=65 ksi)

Stiffener Data

(45) 12"H x 4"W x 1"T, Notch: 0.5" plate: Fy= 50 ksi ; weld: Fy= 70 ksi horiz. weld: 0.5" fillet vert. weld: 0.25" fillet

Pole Data

62.9375" x 0.375" 18-sided pole (A572-65; Fy=65 ksi, Fu=80 ksi)

A	nalysis Results	
Anchor Rod Summary	(u	nits of kips, kip-in)
Pu_c = 72.03	φPn_c = 101.75	Stress Rating
Vu = 0.88	φVn = 30.52	67.5%
Mu = n/a	φMn = n/a	Pass
Base Plate Summary		
Max Stress (ksi):	-	
Allowable Stress (ksi):	-	
Stress Rating:	Pirod OK	
Stiffener Summary		
Horizontal Weld:	Pirod OK	
Vertical Weld:	Pirod OK	
Plate Flexure+Shear:	Pirod OK	
Plate Tension+Shear:	Pirod OK	
Plate Compression:	Pirod OK	
Pole Summary		
Punching Shear:	Pirod OK	

CROWN

Pier and Pad Foundation

	823530	
	CT364/Chapel St	
App. Number:	479829 R0	

TIA-222 Revision: H Tower Type: Monopole Top & Bot. Pad Rein. Different?:

Superstructure Analysis Reactions			
Compression, P _{comp} :	63	kips	
Base Shear, Vu_comp:	39	kips	
Moment, M _u :	4503	ft-kips	
Tower Height, H:	175	ft	
BP Dist. Above Fdn, bp _{dist} :	2.5	in	

Pier Properties		
Pier Shape:	Circular	
Pier Diameter, dpier :	7.5	ft
Ext. Above Grade, E:	0.5	ft
Pier Rebar Size, Sc :	9	
Pier Rebar Quantity, mc :	36	
Pier Tie/Spiral Size, St:	4	
Pier Tie/Spiral Quantity, mt :	10	
Pier Reinforcement Type:	Tie	
Pier Clear Cover, cc _{pier} :	3	in

Pad Properties		
Depth, D:	8	ft
Pad Width, W :	22.5	ft
Pad Thickness, T :	2.75	ft
Pad Rebar Size (Bottom), Sp :	9	
Pad Rebar Quantity (Bottom), mp :	23	
Pad Clear Cover, cc_{pad}:	3	in

Material Properties			
Rebar Grade, Fy :	60	ksi	
Concrete Compressive Strength, F'c:	3	ksi	
Dry Concrete Density, 5c :	150	pcf	

Soil Properties			
Total Soil Unit Weight, γ:	110	pcf	
Ultimate Net Bearing, Qnet:	30.000	ksf	
Cohesion, Cu :	0.000	ksf	
Friction Ang l e, φ :	28	degrees	
SPT Blow Count, N _{blows} :	27		
Base Friction, µ :	0.45		
Neglected Depth, N:	3.75	ft	
Foundation Bearing on Rock?	No		
Groundwater Depth, gw:	12	ft	

Foundation Analysis Checks				
	Capacity	Demand	Rating*	Check
Lateral (Sliding) (kips)	277.25	39.00	13.4%	Pass
Bearing Pressure (ksf)	23.16	4.78	20.6%	Pass
Overturning (kip*ft)	6181.46	4842.63	78.3%	Pass
Pier Flexure (Comp.) (kip*ft)	6230.23	4727.25	72.3%	Pass
Pier Compression (kip)	21089.12	108.72	0.5%	Pass
Pad Flexure (kip*ft)	2826.15	2367.60	79.8%	Pass
Pad Shear - 1-way (kips)	627.95	406.39	61.6%	Pass
Pad Shear - 2-way (Comp) (ksi)	0.164	0.000	0.0%	Pass
Flexural 2-way (Comp) (kip*ft)	3889.71	2836.35	69.4%	Pass

*Rating per TIA-222-H Section 15.5

Soil Rating*:	78.3%
Structural Rating*:	79.8%

<---Toggle between Gross and Net





No Address at This

Location

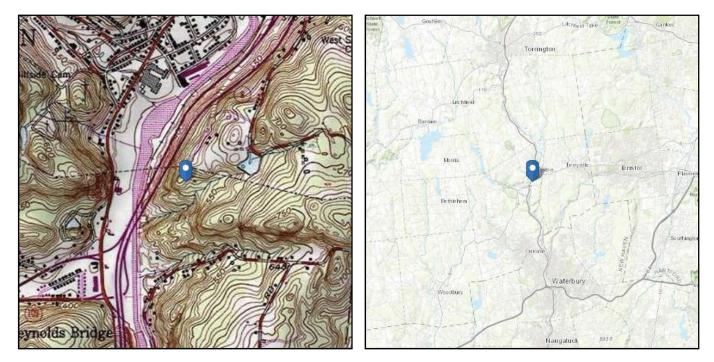
ASCE 7 Hazards Report

Standard:ASCE/SEI 7-10Risk Category:IISoil Class:D - Stiff Soil

 Elevation:
 543 ft (NAVD 88)

 Latitude:
 41.663467

 Longitude:
 -73.074281



Wind

Results:

Wind Speed:	118 Vmph	120 mph per JDX
10-year MRI	76 Vmph	
25-year MRI	85 Vmph	
50-year MRI	91 Vmph	
100-year MRI	97 Vmph	
Data Source:	ASCE/SEI 7-10 March 12, 2014	, Fig. 26.5-1A and Figs. CC-1–CC-4, incorporating errata of
Date Accessed:	Tue Jun 18 201	9

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

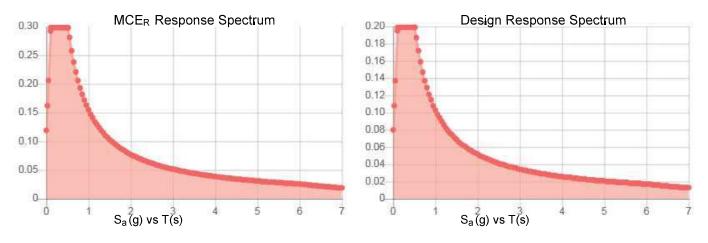
Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.



Site Soil Class: Results:	D - Stiff Soil			
S _S :	0.186	S _{DS} :	0.199	
S ₁ :	0.064	S _{D1} :	0.103	
F _a :	1.6	T _L :	6	
F _v :	2.4	PGA :	0.096	
S _{MS} :	0.298	PGA M :	0.153	
S _{M1} :	0.155	F _{PGA} :	1.6	
		e :	1	

Seismic Design Category B



Data Accessed: Date Source:

Tue Jun 18 2019

USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.



Ice

Results:

Ice Thickness:	0.75 in.
Concurrent Temperature:	5 F
Gust Speed:	50 mph
Data Source:	Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Date Accessed:	Tue Jun 18 2019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

Exhibit E

Mount Analysis

Date: June 7, 2019

Hastec

Charles McGuirt Crown Castle 3530 Toringdon Way Suite 300 Charlotte, NC 28277		MasTec Network Solutions 507 Airport Blvd, Suite 111 Morrisville, NC 27560 (919) 674-5866
Subject:	Mount Analysis	
Carrier Designation:	T-Mobile Equipment Change-C Carrier Site Number:	9ut CT11364B
	Carrier Site Name:	CT364/Chapel St Monopole
Crown Castle Designation:	Crown Castle BU Number: Crown Castle Site Name: Crown Castle JDE Number: Crown Castle Order Number:	823530 CT364/Chapel St Monopole 559233 479829 Revision 0
Engineering Firm Designation:	Crown Castle Project Number:	18813-MNO1
Site Data:	580 Chapel Street, Thomaston, Latitude: 41° 39' 48.48'' Longitu	
Structure Information	Tower Height & Type: Mount Elevation: Mount Width & Type:	175 ft Monopole 169 ft 14.5 ft Platform Mount

Dear Charles McGuirt,

Mastec Network Solutions is pleased to submit this "**Mount Analysis Report**" to determine the structural integrity of T-Mobile's antenna mounting system with the proposed appurtenance and equipment addition on the above mentioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point for fall protection or rigging is not part of this document.

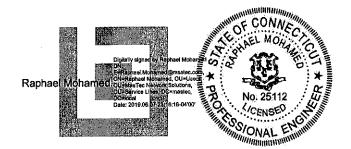
The purpose of the analysis is to determine acceptability of the mount stress level. Based on our analysis we have determined the mount stress level to be:

Platform Mount

This analysis utilizes an ultimate 3-second gust wind speed of 120 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Mount analysis prepared by: Richard Torbert, El

Respectfully Submitted by:



Raphael I. Mohamed, PE, Senior Director of Engineering CT PE License No. 25112

Sufficient

TABLE OF CONTENTS

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2) ANALYSIS CRITERIA

Table 1 - Proposed Equipment Configuration InformationTable 2 - Other Considered Equipment

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

3.1) Analysis Method

3.2) Assumptions

4) ANALYSIS RESULTS

Table 4 - Mount Component Stresses vs. Capacity4.1) Recommendations

5) APPENDIX A

Wire Frame and Rendered Models

6) APPENDIX B Software Input Calculations

7) APPENDIX C Software Analysis Output

8) APPENDIX D

Additional Calculations

1) INTRODUCTION

This is a 14.5 ft Platform Mount mapped by Pier Structural Engineering Corp., dated April 18, 2019.

2) ANALYSIS CRITERIA

TIA-222 Revision:	TIA-222-H
Risk Category	II
Wind Speed:	120 mph
Exposure Category:	B
Topographic Factor:	1
Ice Thickness:	1.5 in
Wind Speed with Ice:	40 mph
Seismic Ss:	0.186
Seismic S1:	0.064
Live Loading Wind Speed:	30 mph
Live Loading at Mid/End-Points:	250 lb
Man Live Loading at Mount Pipes	500 lb

Table 1 - Proposed Loading Configuration

Mount Centerline (ft)	Centerline		Antenna Manufacturer	Antenna Model	Mount / Modification Details
		3	EMS Wireless	RR90-17-02DP	
		3	RFS	APXVAARR24_43-U-NA20	
172.0	172.0	3	Ericsson	KRY 112 144/1	14.5-ft Platform
		3	Ericsson	KRY 112 489/2	
		3	Ericsson	Radio 4449 B12/B71	

Table 2 – Other Considered Equipment

	Antenna Centerline (ft)		Antenna Manufacturer	Antenna Model	Mount / Modification Details
	175.0	2	Andrew	VHLP2.6	
172.0	168.0	1	Bird Tech Group	OA20-67-DIN	14.5-ft Platform
	100.0	1	Lone Star Electronics	LS-230C	

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

Document	Remarks	Reference	Source
4-ORDER INFORMATION	CROWN CASTLE	Order No. 479829 Rev.0	CCIsites
4-MOUNT MAPPING	Pier Structural Engineering Corp.	Project No. 19651-06	On File

3.1) Analysis Method

RISA-3D (Version No. 17.0.2), a commercially available analysis software package, was used to create a three-dimensional model of the antenna mounting system and calculate member stresses for various loading cases.

This analysis was performed in accordance with Crown Castle's ENG-SOW-10208 *Tower Mount Analysis* (Revision C).

3.2) Assumptions

- 1) The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specifications.
- 2) The configuration of antennas, mounts, and other appurtenances are as specified in Tables 1 and the referenced drawings.
- 3) All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.

4)	Steel grades have been assumed as follows, unless noted otherwise:		
•	Channel, Solid Round, Angle, Plate	ASTM A36 (GR 36)	
	HSS (Rectangular)	ASTM 500 (GR B-46)	
	Pipe	ASTM A53 (GR B-35)	
	Connection Bolts	ASTM A325	

This analysis may be affected if any assumptions are not valid or have been made in error. Mastec should be notified to determine the effect on the structural integrity of the antenna mounting system.

4) ANALYSIS RESULTS

Table 4 - Mount Component Stresses vs. Capacity

Notes	Component	Beam No.	Centerline (ft)	% Capacity	Pass / Fail
1	Frame Rail		172	56.7	Pass
1	Support Angle 2		172	69.7	Pass
1	Support Angle 1		172	25.0	Pass
1	Arm		172	58.3	Pass
1	Mount Pipe		172	54.9	Pass
1	10' MP		172	60.7	Pass
1	Tower Connection		172	92.3	Pass

	Structure Rating (max from all components) =	92.3%
--	--	-------

Notes: 1)

See additional documentation in "Appendix C - Software Analysis Output" for calculations supporting the % capacity consumed.

4.1) Recommendations

The mount has sufficient capacity to carry the proposed loading configuration. No modifications are required at this time.

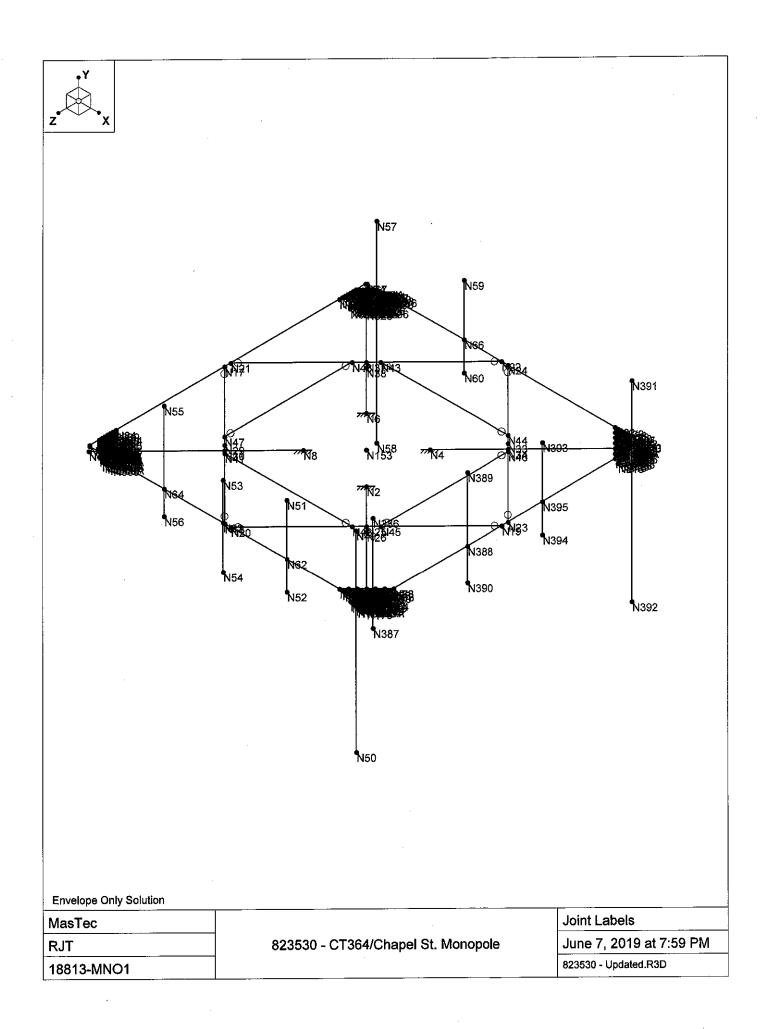
14.5 ft Platform Mount Analysis Order Number 479829, Revision 0 June 7, 2019 CCI BU No: 823530 Page 5

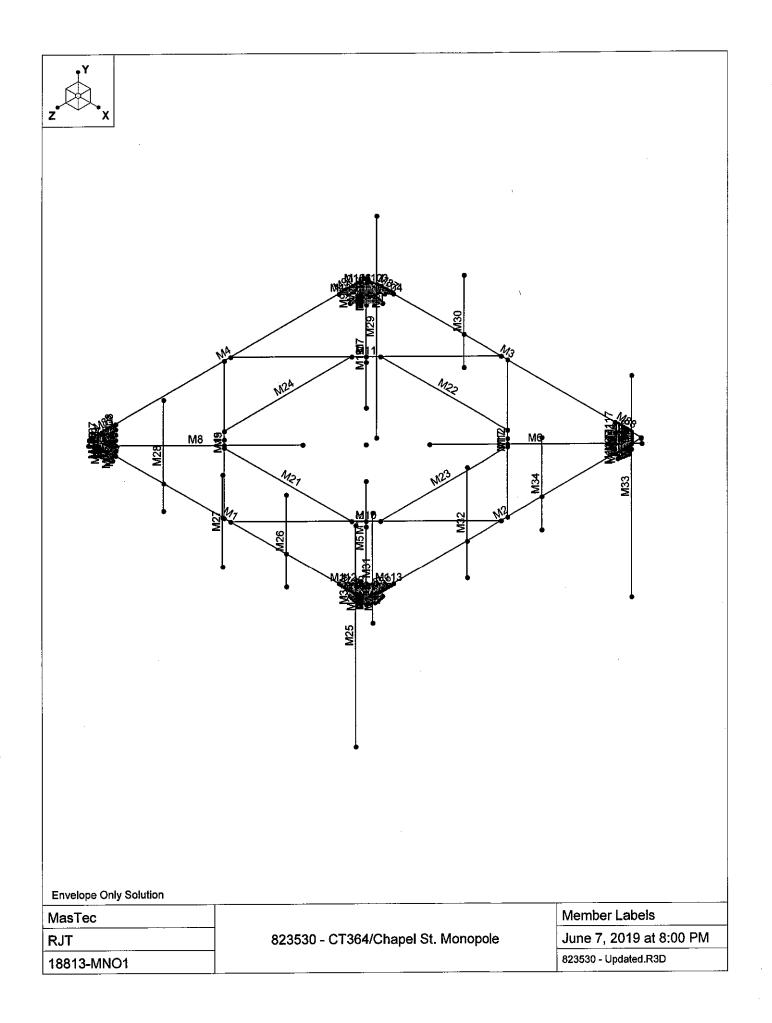
APPENDIX A

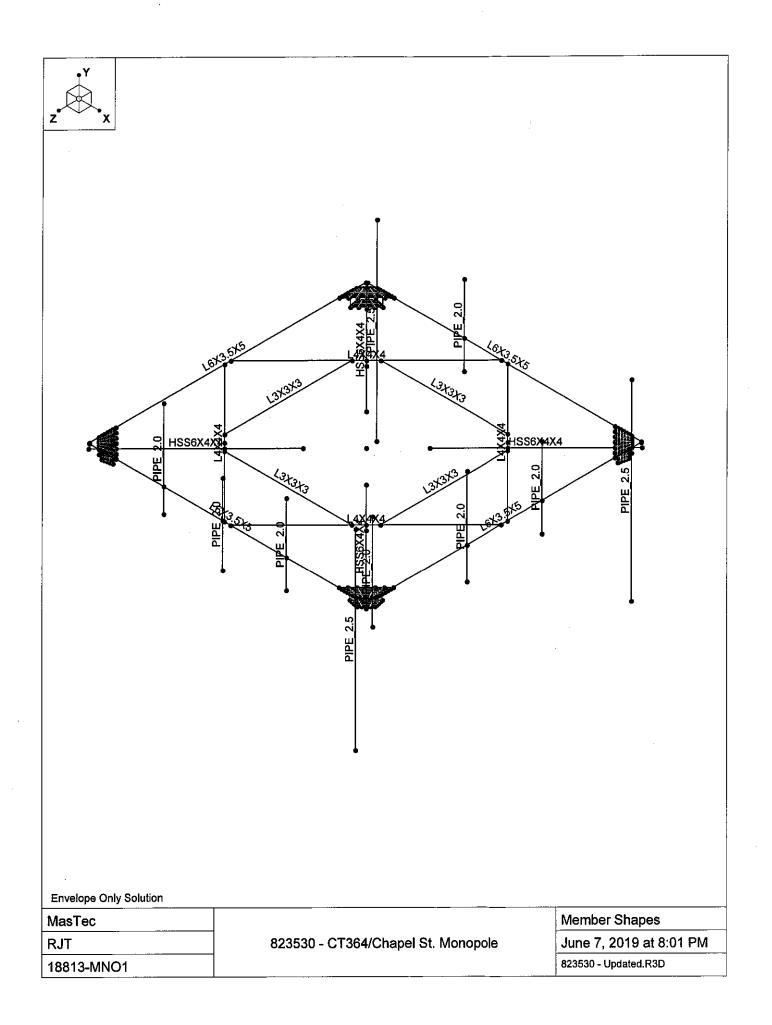
WIRE FRAME AND RENDERED MODELS

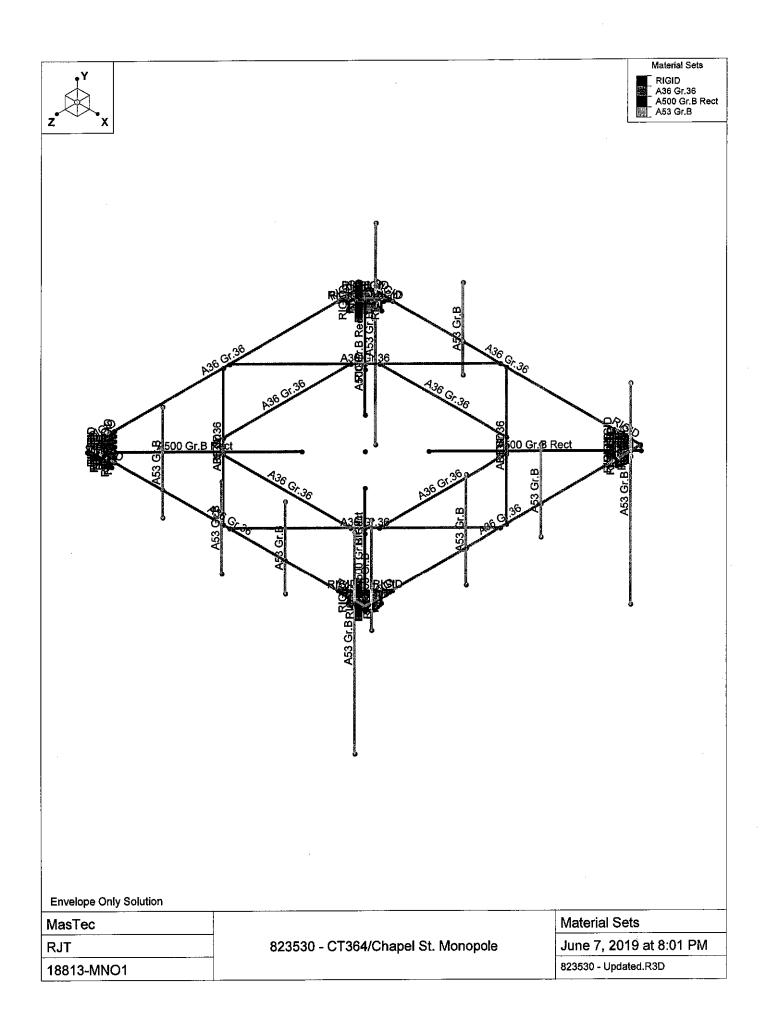
ENG-FRM-10208, Rev. C

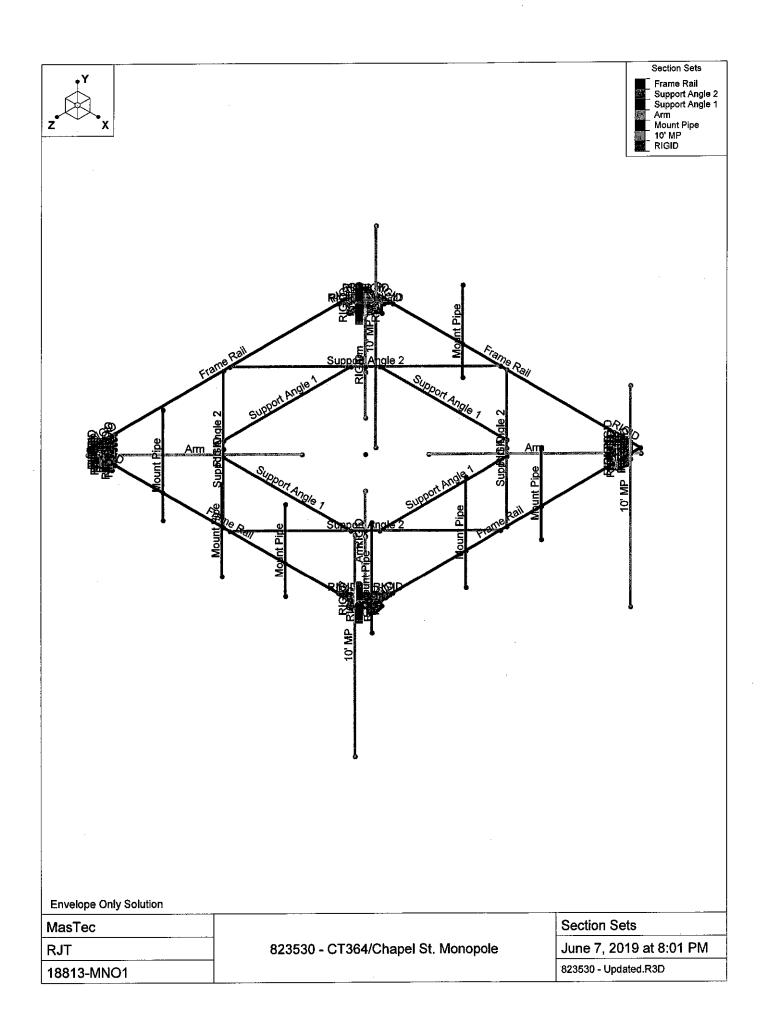
Envelope Only Solution		
MasTec RJT 18813-MNO1	823530 - CT364/Chapel St. Monopole	Rendered View June 7, 2019 at 8:00 PM 823530 - Updated.R3D

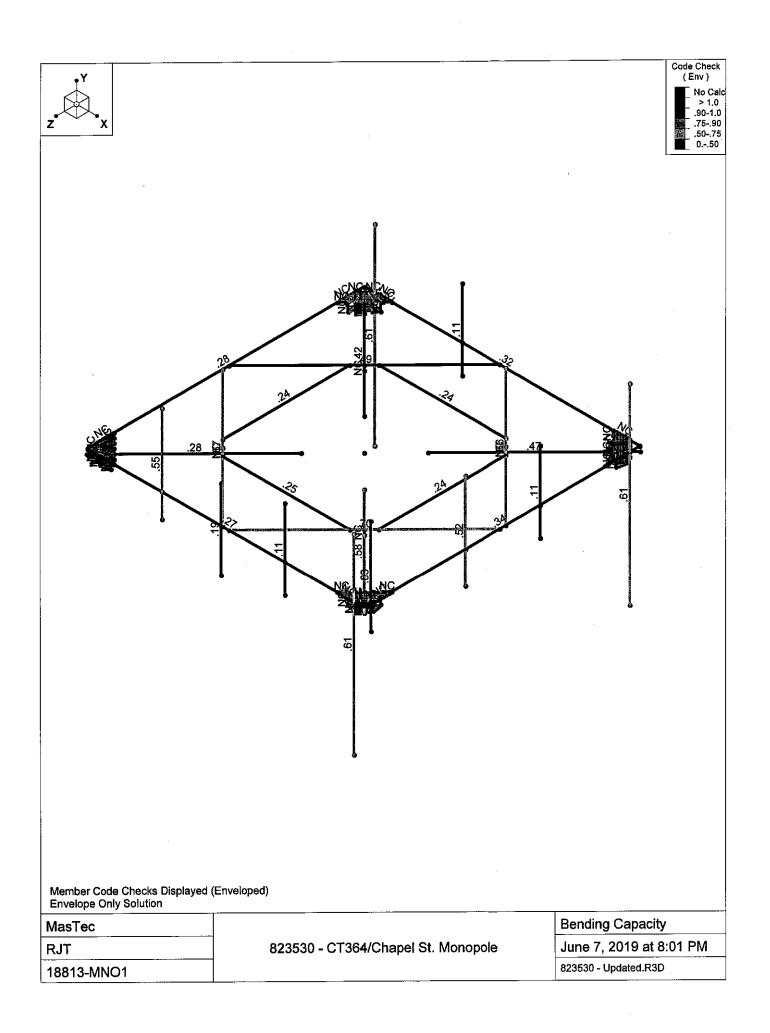


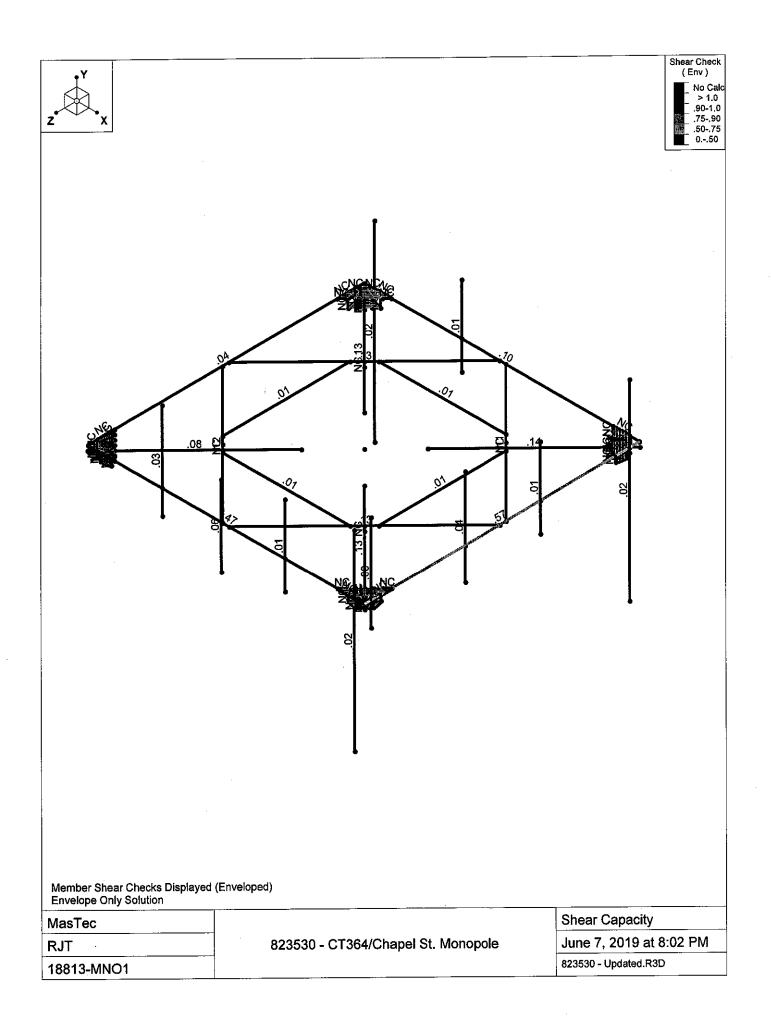












14.5 ft Platform Mount Analysis Order Number 479829, Revision 0 June 7, 2019 CCI BU No: 823530 Page 6

APPENDIX B

SOFTWARE INPUT CALCULATIONS

ENG-FRM-10208, Rev. C

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Mount Analysis Tool

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	Mount Existing?	Risk Category					and the second second						100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100
CT364/Chapel St. Monopole 823530	18813-MNO1	н	Analysis Parameters	172	æ	120	50	1.5	30	Yes	545	0.064	0.199
Site Name	Job Number	Code		MountHeight	Exposure Category	Ultimate Wind Speed	ke Wind Speed	Design ice Thickness, t	Maintenance Wind Speed	Run Earthquake Analysis?	Ground Elevation	5 10 10 10 10 10 10 10 10 10 10 10 10 10	<u> </u>

				_		_	_	_		_				_
					Diameter (in)	2.375	2.875	2.375	2.875	2.375	2.875	2.375	2.375	2.375
	1			wn) i faw	Length (in)	60	120	33	120	50	120	20	50	50
0.199	0:040	0.100	0:030	Pipe Mounts (Orientation Drawn Top-Down)	Elevation (R)	172	172	172	172	172	172	172	172	172
<u>ال</u>	Vertical Seismic Loads, E.	Seismic Response Coefficient, C	C, Min	Pipe W	Risa 30 Label	M28	M25	M32	MB3	0eW	M29	M26	M27	M34

NIGAUSEDID CAPACULY	69.7% PASS		1.000 1.000 1.000	N. 1	x, x, 0.900					1 (international and international	2 1, EQ
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		Appurtenances			ç i
Model	Type	38 X (III) 148H / The X	(iii) (iii)	Depth (in): Weight	(lbs)
EMS Wireless RR90-17-02DP	Antenna	9 5 - 21 5	8	2.75 - 25 - 25 - 25 - 25 - 25 - 25 - 25 -	
RFS APXVAARR24_43-U-NA20	Antenna	6'56	26 30. 24	8.7 28128	
Ericsson KRY 112 144/1	RRU, TMA, Etc.	14.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	11 TA	1.1	
Ericsson KRY 112 489/2	RRU, TMA, Etc.	就在Strate Transmission	第二19、18歳 三派	15.4	1.11.1
Ericsson Radio 4449 B12/B71	RRU, TMA, Etc.	14.95	經60°ET密導 與聽	9.25	
Andrew VHLP2.6 (By Others)	RRU, TMA, Etc.	SERVICE OF T	32 State	21.19.1 State 148	
OA20-67-DIN (By Others)	RRU; JMA, Etc.	100 A. S.	2	20 × 20 × 20	
LS-230C (By Others)	Round	78	2.3	11、11、11、11、11、11、11、11、11、11、11、11、11、	はない

Loads and Equipment

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MasTec Network Solutions

Mount Analysis Tool.xism

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Appurtenances

MaSTec Network Solutions

Mount Analysis Tool.xlsm

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Members

MasTec Network Solutions 14.5 ft Platform Mount Analysis Order Number 479829, Revision 0

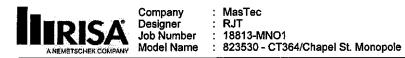
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APPENDIX C

SOFTWARE ANALYSIS OUTPUT

ENG-FRM-10208, Rev. C



<u>(Global) Model Settings</u>

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (ft/sec^2)	32.2
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y III III III III III III III III III I
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver
Hot Rolled Steel Code	AISC 14th(360-10): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 14th(360-10): LRFD
Cold Formed Steel Code	AISI S100-12: LRFD
Wood Code	AWC NDS-12: ASD

	AW0 100-12, A0D
Wood Temperature	<100F
Concrete Code	ACI 318-11
Masonry Code	ACI 530-11 ASD
Aluminum Code	AA ADM1-10: ASD - Building
Stainless Steel Code	AISC 14th(360-10): ASD
Adjust Stiffness?	Yes(Iterative)

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	Yes
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No.
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	
Max % Steel for Column	8



(Global) Model Settings, Continued

Seismic Code	ASCE 7-10
Seismic Base Elevation (ft)	Not Entered
Add Base Weight?	Yes
CLX	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec) RX	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1 SDS	
SDS S1	
SI TL (sec)	5
Risk Cat	l or II
Drift Cat	Other
Om Z	1
Om X	
Cd Z	4
Cd X	4
Rho Z	
Rho X	1

Hot Rolled Steel Properties

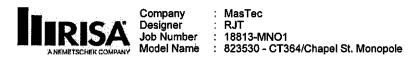
	Label	E [ksi]	G [ksi]	Nu	Therm (\1E	.Density[k/ft	. Yield[ksi]	Ry	Fu[ksi]	Rt
1	A992	29000	11154	.3	.65	.49	50	1.1	65	1.1
2	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
3	A572 Gr.50	29000	11154	.3	.65	.49	50	1,1	65	1.1
4	A500 Gr.B RND	29000	11154	.3	.65	.527	42	1.4	58 👘	1.3
5	A500 Gr.B Rect	29000	11154	.3	.65	.527	46	1.4	58	1.3
6	A53 Gr.B	29000	11154	3	.65	.49	35	1.6	60	1.2
7	A1085	29000	11154	.3	.65	.49	50	1.4	65	1.3

Hot Rolled Steel Section Sets

	Label	Shape	Туре	Design List	Material	Design Ru	A [in2]	lyy [in4]	zz [in4]	J [in4]
1	Frame Rail	L6X3.5X5	Beam	Single Angle	A36 Gr.36	Typical	2.89	2.84	10.9	.099
2	Support Angle 2	L4X4X4	Beam	Single Angle	A36 Gr.36	Typical	1.93	* 3 ***	3·3·2·2·2·2·2·2·2·2·2·2·2·2·2·2·2·2·2·2	.044
3	Support Angle 1	L3X3X3	Beam	Single Angle	A36 Gr.36	Typical	1,09	.948	.948	.014
4	Arm	HSS6X4X4	Beam	Tube	A500 Gr.B Rect	Typical	4.3	11.1	20.9	23.6
5	Mount Pipe	PIPE 2.0	Column	Pipe	A53 Gr.B	Typical	1.02	.627	.627	1.25
×6	10' MP	PIPE 2.5	Column	Pipe	A53 Gr.B	Typical	1,61		1,45	2.89

Joint Coordinates and Temperatures

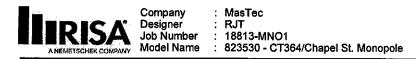
	Label	X [ft]	Y (ft)	Z [ft]	Temp [F]	Detach From Diap
1	N1	7.25	0.	7.25	Ó	
2	N2	1.652071	tan da si O rts da mar	1.652071	0	
3	N3	7.25	0.	-7.25	0	
4	N4	1,652071	0.	-1.652071	0	
5	N5	-7.25	0,	-7.25	0	
* 6	N6	-1.652071		-1.652071	0	
7	N7	-7.25	0.	7.25	0	
8	N8 · · ·	-1.652071	> 0 .	1.652071	0	



Joint Coordinates and Temperatures (Continued)

Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Diap
9 N17	-7.25	.25	0.166667	0	
10 N18		.25		<u>i 10 s</u>	6 J.B. 1 MALE
11 N19	7,25	.25	0.166667	0	
12 N20	0.166667	.25		0	
13 N21	-7,25	.25	-0.166667		
<u>14</u> N22	-0.166667	25	-7.25	0	
15 N23	7.25	.25	-0.166667	0	
16 N24	0.166667	.25	-7.25	<u> </u>	
17 N25	3.708333	.25	3.708333	0	
18 N26 19 N29	3,708333	0	3.708333		
20 N30	-3.708333	.25	<u>3.708333</u> 3.708333		
21 N33	3.708333	.25	-3.708333	0	
22 N34	3.708333		-3.708333	Service of the cal	
23 N37	-3.708333	.25	-3.708333	Ö	
24 N38	-3.708333		-3:708333	ŏ	
25 N41	-3.333333	.25	4.083333	0	Construction (1.5) intelligences - etc. (2016) (2016) (2016) (2016)
26 N42	3,333333	.25	4.083333	Ō	
27 N43	-3.333333	.25	-4.083333	0	The second delayer of the second s
28 N44	3,333333	.25	-4.083333		
29 N45	4.083333	.25	3.333333	0	
30 N46	4.083333	.25	-3.333333	0	
_31N47		.25	3.333333	0	
32 N48	-4.083333	.25	-3.333333	0	
33 N49	6.708333	3.333333	7.25	O	Recent 1 Participation - est material de 200 autor
34 N50	6.708333	-6.666667	7.25	0	
35 <u>N51</u>	3.083333	2.916667	7.25	0	The Read of Street and Street Stre
36 N52	3.083333	-1.25	7,25	0	Allowin Distribution
37 N53	25	2.166667	7.25	0	
38 N54 39 N55	25	-2	7.25	0	
39 <u>N55</u> 40 N56	-3.3333333	4 -1	7.25		
41 N57	-6.708333	3.333333	-7.25		
42 N58		-6.666667	-7.25	0	
43 N59	-2.166667	2.916667	-7.25	0	
44 N60	-2.166667	-1.25	-7.25	Est jõre i	
45 N62	3.083333	.25	7.25		Contraction of the second state of the second
46 N63	25	.25	7.25	<u>ō</u> .	
47 N64	-3.333333	.25	7.25	0	
48 N66	-2.166667		-7:25	0	
49 N67	-7.208333	.25	-7.25	0	
50 N68 **	-7.208333	.25	7.25	0	
51 N69	7.208333	.25	7.25	0	
52 N70	7,208333	.25	2 -7.25	0	
53 N71	7.25	.25	7.208333	0	·
<u>54</u> N72	-7:25	.25	7.208333	0	
<u>55 N73</u>	7.25	.25	-7.208333	0	Andre and weight the second second to be a
56 N74	A CONTRACTOR AND A CONTRACT OF A	.25	-7.208333	0	
57 N153	-0.	0.	-0.	0	WARDEN CONTRACTOR
58 N386	7,25	4 1	6.911458	0	
59 N387 60 N388	7.25	-1	6.911458	0 0	
		.25	1.994792		
61 N389 62 N390	7.25	3.583333	1.994792	0	
63 N390	7.25	-1:416667 3.3333333	1,994792 -6.708333		
64 N392	7.25	-6.666667	-6.708333	0	
65 N393	7.25	2.916667	-1.994792	0	THE REPORT OF
	1.20	2.310007	-1.334/34	<u> </u>	

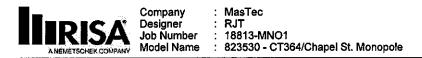
RISA-3D Version 17.0.2



Joint Coordinates and Temperatures (Continued)

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78 N80 -5.833333 25 7.25 0 79 N81 6.708333 25 -7.25 0 80 N82 5.833333 25 -7.25 0 81 N83 -7.25 $.25$ 6.708333 0 82 N84 -7.25 $.25$ 6.708333 0 83 N85 -7.25 $.25$ -6.708333 0 84 N86 -7.25 $.25$ -6.708333 0 84 N86 -7.25 $.25$ -6.708333 0 84 N86 -7.25 $.25$ -6.708333 0 85 N85A 6.069444 $.25$ 7.013889 0 86 N86A 6.305556 $.25$ 6.305566 0 87 N87 6.541667 $.25$ 6.3025566 0 88 N88 6.777778 $.25$ 6.3025566 0	
79 N81 6,708333 .25 -7.25 0 80 N82 5,833333 .25 .7.25 0 81 N83 -7.25 .25 6,708333 0 82 N84 .7.25 .25 5,833333 0 83 N85 .7.25 .25 5,833333 0 84 N86 .7.25 .25 .5,833333 0 85 N85A .6,069444 .25 .7,013889 0 86 N86A .6,305556 .25 .6,777.78 0 87 N87 .6,541667 .25 .6,541667 0 88 N88 .6,777.78 .25 .6,305556 0 90 N90 .5,979167 .25 .7,25 0 91 N91 .6,190972 .25 .7,038194 0 92 N92 .6,402.778 .25 .6,614583 .0 93 N93 .6,614583	
80 N82 5,833333 25 -7,25 0 81 N83 -7,25 .25 6,708333 0 82 N84 -7,25 .25 5,833333 0 83 N85 -7,25 .25 5,833333 0 84 N86 -7,25 .25 -6,708333 0 84 N86 -7,25 .25 -6,833333 0 85 N85A 6,069444 .25 7,013889 0 86 N86A 6,305556 .25 6,777778 0 87 N87 6,541667 .25 6,541667 0 88 N88 6,777778 .25 7,25 0 89 N89 7,013889 .25 6,069444 0 90 N90 5.979167 .25 7.25 0 91 N91 6,190972 .25 7.08194 0 92 N92 6,402778 .25<	ar load
81 N83 -7.25 .25 6,708333 0 82 N84 .725 .25 5,833333 0 83 N85 .7.25 .25 -6,708333 0 84 N86 .7.25 .25 -6,708333 0 85 N85A 6,069444 .25 .701389 0 86 N86A 6,05556 .25 .6,777778 0 87 N87 6,541667 .25 6,541667 0 88 N88 6,777778 .25 6,069444 0 90 N89 7,013889 .25 6,069444 0 90 N89 7,013889 .25 6,069444 0 90 N90 5.979167 .25 7.25 0 91 N91 6,190972 .25 7.038194 0 92 N92 6,402778 .25 6,840389 0 93 N93 6,614583	
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85 N85A 6.069444 .25 7.013889 0 86 N86A 16.305556 .25 6.777778 0	
86 N86A 6.305556 .25 6.777778 0 87 N87 6.541667 .25 6.541667 0 88 N88 6.777778 .25 6.305556 0 89 N89 7.013889 .25 6.069444 0 90 N90 5.979167 .25 7.25 0 91 N91 6.190972 .25 7.038194 0 92 N92 6.402778 .25 6.614583 0 93 N93 6.614583 .25 6.826389 0 94 N94 6.826389 .25 6.402778 0 95 N95 7.038194 .25 6.190972 0 96 N96 7.25 .25 7.25 0 97 N97 6.125 .25 7.25 0 98 N98 .6.3125 .25 7.25 0 98 N98 .6.3125 .25<	PORT AND A
87 N87 6.541667 .25 6.541667 0 88 N88 6.777778 .25 6.305556 0 89 N89 7.013889 .25 6.069444 0 90 N90 5.979167 .25 7.25 0 91 N91 6.190972 .25 7.038194 0 92 N92 6.402778 .25 6.826389 0 93 N93 6.614583 .25 6.614583 0 94 N94 6.826389 .25 6.402778 0 95 N95 7.038194 .25 6.190972 0 96 N96 7.25 .25 7.25 0 97 N97 6.125 .25 7.25 0 98 N98 6.3125 .25 7.25 0 99 N99 6.5 .25 6.875 0	
89 N89 7.013889 .25 6.069444 0 90 N90 5.979167 .25 7.25 0	
90 N90 5.979167 .25 7.25 0 91 N91 6.190972 .25 7.038194 0 92 N92 6.402778 .25 6.826389 0 93 N93 6.614583 .25 6.614583 0 94 N94 6.826389 .25 6.402778 0 95 N95 7.038194 .25 6.190972 0 96 N96 7.25 .25 5.979167 0 97 N97 6.125 .25 7.25 0 98 N98 6.3125 .25 7.0625 0 99 N99 6.5 .25 6.875 0	
91 N91 6.190972 .25 7.038194 0 92 N92 6.402778 25 6.826389 0 93 N93 6.614583 .25 6.614583 0 94 N94 6.826389 .25 6.402778 0 95 N95 7.038194 .25 6.190972 0 96 N96 7.25 .25 5.979167 0 97 N97 6.125 .25 7.25 0 98 N98 6.3125 .25 0 0 99 N99 6.5 .25 6.875 0 100 N100 6.8875 .25 6.875 0	
92 N92 6.402778 25 6.826389 0 93 N93 6.614583 .25 6.614583 0 94 N94 6.826389 .25 6.402778 0 95 N95 7.038194 .25 6.190972 0 96 N96 7.25 .25 7.25 0 97 N97 6.125 .25 7.25 0 98 N98 6.3125 .25 7.25 0 99 N99 6.5 .25 6.875 0 100 N100 6.8875 .25 0 0	
93 N93 6.614583 .25 6.614583 0 94 N94 6.826389 .25 6.402778 0 95 N95 7.038194 .25 6.190972 0 96 N96 7.25 .25 5.979167 0 97 N97 6.125 .25 7.25 0 98 N98 6.3125 .25 7.0625 0 99 N99 6.5 .25 6.875 0	
94 N94 6.826389 25 6.402778 0 95 N95 7.038194 .25 6.190972 0 96 N96 7.25 .25 5.979167 0 97 N97 6.125 .25 7.25 0 98 N98 6.3125 .25 7.0625 0 99 N99 6.5 .25 6.875 0 100 N100 6.6875 .25 0 0	
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96 N96 7.25 .25 5.979167 0 97 N97 6.125 .25 7.25 0 98 N98 6.3125 .25 7.0625 0 99 N99 6.5 .25 6.875 0 100 N100 6.6875 .25 6.6875 0	
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101 N101 6.875 .25 6.5 0	
102 N102 7:0625 125 6.3125 0	
103 N103 7.25 .25 6.125 0	il Malinter -
104 N104 6,270833 .25 7/25 0 105 N105 6.434028 .25 7.086806 0	
105 N105 6.434028 .25 7.086806 0 106 N106 6.597222 25 6.923611 0	
107 N107 6.760417 .25 6.760417 0	
108 N108 6.923611 25 6.597222 0	
109 N109 7.086806 .25 6.434028 0	ALL CONTRACTOR
110 N110 7.25 .25 6.270833 0	
<u>111</u> <u>N111</u> <u>6.416667</u> <u>.25</u> <u>7.25</u> 0	
112 N112 6.555556 .25 7.111111 0	
<u>113 N113 6.694444 .25 6.972222 0</u>	1
114 N114 6.833333 .25 6.833333 0	X E.S.
115 N115 6.972222 .25 6.694444 0 116 N116 7.111111 .25 6.555556 0	445870 P 10
117 N117 7.25 .25 6.416667 0 118 N118 6.5625 25 725 0	
<u>119 N119 6.677083 .25 7.135417 0</u>	MUNICIPALITY (
120 N120 0.6791667 25 7.020833 0	
121 N121 6.90625 .25 6.90625 0	<u>17998832</u>
122 N122 7/020833 25 6/791667 0	

RISA-3D Version 17.0.2

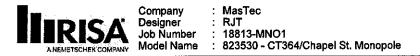


Joint Coordinates and Temperatures (Continued)

Label	X [ft]	Y [ft]	<u>Z [ft]</u>	Temp [F]	Detach From Diap
123 N123	7.135417	.25	6.677083	0	
124 N124		.25	6.5625	0	
125 N125	6.798611	.25	7.159722	0	Line and
126 N126		.25		and the second s	
127 N127	6.979167	.25	<u>6.979167</u>	0	
128 N128 129 N129	7.069444 7.159722	.25	6.888889 6.798611	0	
130 N130	6.190972		7.038194	- Ö	100 A 55
131 N131	6.402778	-,25	6.826389	0	
132 N132		25	6.614583	+ 10 e	
133 N133	6.826389	25	6.402778	Ō	
134 N134	7.038194		6 190972	0	
135 N135	6.3125	25	7.0625	0	
136 N136	6,5	-:25	6.875	0 (de 1	
137 N137	6.6875	25	6.6875	0	
138 N138	6.875	25		0	
139 N139	7.0625	25	6.3125	0	alta deva andara meri silata kenar ata dara dina menangan
140 N140	6,434028	25	7.086806	0	
141 N141	6.597222	25	6.923611	0	ALCONT OF THE REAL PROPERTY OF
142 N142		-,25	6.760417	<u> </u>	
143 N143	6.923611	25	6.597222	0	8
and the restance have a second state which is a second		25 25	<u>6:434028</u> 7.111111	0	
145 N145 146 N146	6.555556 6.694444	25			
147 N147	6.833333	25	6.833333	0	
148 N148	6.972222	25		- Č	
149 N149	7.111111	25	6.555556	0	Application of the AND STATEMENT A CONTRACT CONTRACT
	6677083	25	7.135417	n - S Ö	
151 N151	6.791667	25	7.020833	0	And of the second s
152 N152	6,90625		6.90625	ē (0	
153 N153A	7.020833	25	6.791667	0	
154 N154		25	6.677083	NO	
155 N155	6.541667		6.541667	0	The second s
156 N156		0	6:614583	0	
157 N157	6.6875	<u> </u>	6.6875	0	
158 N158	6.760417		6.760417		
159 N159 160 N160	6.833333	0	6.833333	0	
160 N160 161 N161	<u>6.90625</u> 6.979167		6.90625 6.979167		Sec. Sec. Sec. Sec. Sec. Sec. Sec. Sec.
162 N169	6.541667	- 25	6.541667	0	
163 N175	6.979167	25	6.979167	0	
164 N168	7.013889	.25	-6.069444	i i i o ana i i	
165 N169A	6.777778	.25	-6.305556	Ō	TRUETY 7 - C
166 N170	6,541667	.25	-6.541667	0 ***	
167 N171	6.305556	.25	-6.777778	0	
168 N172	6.069444	.25	-7.013889	0	
169 N173	7.25	.25	-5.979167	0	
170 N174		:25	-6.190972	0	
171 N175A	6.826389	.25	-6.402778	O	TAR CONTRACTOR
172 N176		.25	-6.614583	Q	
173 N177	6.402778	.25	-6.826389		184.8.1931年7月1日月1日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日
174 N178		.25		0	
175 N179 176 N180	5.979167	.25 .25	-7.25	0	
	7.25	.25	-6.3125	0 0	
	6,875	.25	-6.5	Ŭ.	
179 N183	6.6875	.25	-6.6875	0	ACTIVATION AND A PROPERTY
1131 1103		.20	-0.0010	<u>v</u>	I

RISA-3D Version 17.0.2

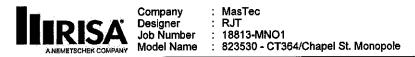
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Joint Coordinates and Temperatures (Continued)

			- P (A)	Tamm (F)	Detach From Diap
Label	<u>X (ft)</u> 6.5	Y [ft]	<u>Z [ft]</u> -6:875	<u>Temp (F)</u>	Detach From Diap
				0	
181 N185	6.3125	.25	-7.0625	0	
182 N186	6,125	.25	-7.25	and the second second second	
183 N187	7.25	.25	-6.270833	0	
184. N188	7.086806		-6,434028	Providence in the state of the	
185 N189	6.923611	.25	-6.597222		
186 N190	6.760417-		-6.760417	0	
187 N191	6.597222	.25	-6.923611	O	
188 N192		.25	-7.086806	0	
189 N193	6.270833	.25	-7.25	0	William Sector W 77.5 (20 mm West, s. 6.7) In proceeding of the
190 N194	7.25	25 C	-6.416667	0	由于16月 1日 - 日本
191 N195	7.111111	.25	-6.555556	0	
192 N196	6.972222	.25	-6.694444	0	建筑 系统计 山
193 N197	6.833333	.25	-6.833333	0	
194 N198	6,694444	.25	-6.972222	0	
195 N199	6.555556	.25	-7.111111	0	
196 N200	6,416667	25	-7.25	· · Ö men ·	
197 N201	7.25	.25	-6.5625	Ö	A PERSONAL AND A CONTRACTOR OF
198 N202 3	7/135417	.25	-6.677083	· · · o · · · ·	
199 N203	7.020833	.25	-6.791667	0	 N. Parcelogiere, J. 1997, Los Rendering and Marcelon and Ma And Marcelon and Marc And Marcelon and And And Marcelon and Marcelon and And And And And And And And
200 N204		.25	-6.90625		
	6.791667	.25	-7.020833	0	
201 N205		.20	-7.135417	Ŭ.	
202 N206	6.677083	.25			
203 N207	6.5625	. <u>.25</u>	-7.25		Production and second and second
204 N208	7,159722	25	-6.798611	<u> </u>	
205 N209	7.069444	.25	-6.888889	0	
206 N210	6.979167	.25	-6.979167	<u>ni i o se </u>	
207 N211	6.888889	.25	-7.069444		- Antesdeethebooknombio, sur reachementage au
208 N212	6.798611	.25	-7.159722	3 10 14 1	
209 N213	7.038194	25	<u>-6.190972</u>	0	Contraction of the second s
210 N214		25	-6,402778	0	
211 N215	6.614583	25	-6.614583	0	
212 N216	6.402778	25	-6.826389	0	
213 N217	6.190972	25	-7,038194	0	
214 N218	7,0625	-,25	-6:3125	- 10 - 赤	
215 N219	6.875	25	-6.5	0	
216 N220			-6.6875	0	
217 N221	6.5	25	-6.875	0	
218 N222	6,3125	25	-7.0625	1	
219 N223	7.086806	25	-6.434028	0	
220 N224	6.923611	- 25	-6.597222	Č	
221 N225	6.760417	25	-6.760417	0	
222 N226		25 25 · · ·	-6.923611		
223 N227	6.434028	25	-7.086806	0	tu guya ing ucability
223 N227		25	-6:555556	Ŭ EN Ö	
				0	
225 N229 226 N230	6.972222	25	<u>-6.694444</u>		
		- <u>.25</u>	6.073333		
227 N231	6.694444	25	-6.972222	0	
228 N232	All digitation in the second sec		-7.111111	<u> </u>	
229 N233	7.135417	25	-6.677083	0	Rect to the second state of the second state
230 N234		-,25		0	
231 N235	6.90625	25	-6.90625	0	
232 N236			-7.020833	0	
233 N237	6.677083	25	-7.135417	0	A CONTRACTOR OF
234 N238	6.541667	0	-6.541667	0	
235 N239	6.614583	0	-6.614583	0	
236 N240	6.6875			0	圣谷 西山水 杨鸿
The second	A REAL PROPERTY OF A REAL PROPER				

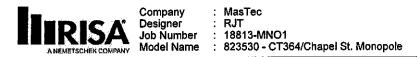
RISA-3D Version 17.0.2



Joint Coordinates and Temperatures (Continued)

	Label	X [ft]	Y [ft]	<u>Z [ft]</u>	Temp [F]	Detach From Diap
237	N241	6.760417	0	-6.760417	0	The state of the second st
	N242	6.833333	0	-6.833333	0	
239	<u>N243</u>	6.90625	0	-6.90625		
240	N244	6.979167	0	-6.979167		
241	N245	6.541667	25	-6.541667	0	
242	N246	6.979167	25	-61979167	0	
243	N251 N252	-6.069444	.25 .25	-7.013889		
244 245	N252	-6.541667	.25	-6,541667	0	
245		-6.777778	.25	-6.305556		
240	N255	-7.013889	.25	-6.069444	0	PERSON PROPERTY.
248	N256	-5.979167		-7.25	0	
249	N257	-6.190972	.25	-7.038194	0	
250	N258	-6,402778	.25	-6.826389	90 I O I I S	
251	N259	-6.614583	.25	-6.614583	0	Caller and the support of the second s
252	N260	-6.826389	.25	-6:402778	0	
253	N261	-7.038194	.25	-6.190972		New your net at the second state of the second s
254	N262	-7.25	.25	-5.979167	0	
255	N263	-6.125	.25	-7.25	0	
256	<u>N264</u>	-6.3125	.25	-7.0625	0	and a second
257	<u>N265</u>	-6.5	.25	-6.875	0	
258	N266	-6.6875	25	-6.6875	0	
259	<u>N267</u> N268	-6.875 -7.0625	. <u>25</u> .25	-6.5 -6.3125	0	
260	N268	-7.25	.25	-6.125	0	
261 262	N209	-7.25	.25	-7.25	A STANCE IN	
263	N270	-6.434028	.25	-7.086806	0	Manager - Manager - Andrew - A
264	N272	-6.597222	.25	-6.923611		
265	N273	-6.760417	.25	-6.760417	Ō	
266	N274	-6.923611		-6.597222	0	
267	N275	-7.086806	.25	-6.434028	0	
268	N276	-7,25		-6.270833	0	
269	N277	-6.416667	.25	-7.25		Manuel Loger Mittabellis No. Phatescold Science 24, 5, 477 (17)
270	N278	-6.555556	.25	-7.111111	0	
271	N279	-6.694444	.25	-6.972222	0	March Province Transformed The Second
272	N280	-6.833333	.25	-6.833333	<u>0</u>	
273	<u>N281</u>	-6.972222	.25	-6.694444	0	
274	N282	7.1111111	.25	-6.555556 -6.416667	0	
275	N283	<u>-7.25</u> -6.5625	<u>.25</u>	-7.25	<u> </u>	
276 277	N284 N285	-6.677083	.25	-7.135417	0	NARTE CARL REPORTED IN THE CONTRACT OF A
278		-6.791667	25	-7.020833	0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
279	N287	-6.90625	.25	-6.90625	Ō	100 C 200 C
	N288	-7.020833	.25	-6.791667		
281	N289	-7.135417	.25	-6.677083	0	
282	N290	-7,25	.25		0	
283	N291	-6.798611	.25	-7.159722	0	
284	N292	-6.888889	.25	-7:069444	0	, the state we
285	N293	-6.979167	.25	-6.979167	0	and the second
	N294	-7.069444	.25	-6.888889	<u> </u>	
287	<u>N295</u>	-7.159722	.25	-6.798611	0	AND DECK THE DECK OF THE OWNER
288	N296	-6.190972	- 25	-7.038194	0	
289	<u>N297</u>	-6.402778	25	<u>-6.826389</u>	<u>0</u> 0	
290		-6.614583	-:25	-6.614583 6.402778	0	
291	N299 N300	-6.826389	25 25	-6.402778 -6.190972	0 0	
292			25	-7.0625	0	
293	<u>N301</u>	-6.3125	23	-1.0020	<u> </u>	<u> </u>

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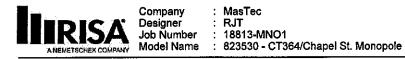


Joint Coordinates and Temperatures (Continued)

Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Diap
294 N302	-6,5	-:25	-6.875	0	
295 N303	-6.6875	25	-6.6875	0	
296 N304	-6.875	25	-6.5	<u> </u>	
297 N305	-7.0625	25	-6.3125	0	
298 N306	-6.434028	25	-7.086806	0	
299 N307	-6.597222 -6.760417	25	<u>-6.923611</u> -6,760417	, j	
300 N308 301 N309	-6.923611	25	-6.597222	0	
302 N310	-7.086806		-6.434028	ATTACH AND AND THE ATTACK TO AN ADDRESS TO AN ADDRESS AND ADDRESS	
303 N311	-6.555556	25	-7.1111111	0	
304 N312	-6.694444	25	-6.972222	0	
305 N313	-6.833333	25	-6.833333	0	
306 N314	-6.972222	-,25	-6,694444	0	
307 N315	-7.111111	25	<u>-6.555556</u>	0	- Library and the strength of
308 N316	-6.677083	25	7.135417	0	
309 N317	-6.791667	25	-7.020833	0	
310 N318		25 25	-6.90625 -6.791667	0	
311 N319 312 N320	-7.020833	25	-6.677083		
313 N321	-6.541667	0	-6.541667		A LOCATION OF A REPRESENCED TO A
314 N322	-0.541007	ŏ	-6.614583	Ŏ D	
315 N323	-6.6875	0	-6.6875	0	
316 N324	-6.760417		-6 760417	0	
317 N325	-6,833333	0	-6.833333	0	-
318 N326	-6:90625	0	-6.90625	0	
319 N327	-6.979167	0	<u>-6,979167</u>	0	AND AND A STATE OF A S
320 N328	-6,541667	25		0	
321 N329	<u>-6.979167</u>	25	-6.979167	0	
322 N334	-7.013889	.25	<u>6:069444</u> 6.305556	0	
323 N335 324 N336	-6.777778	.25	6.541667	0	
325 N337	-6.305556	.25	6.777778	0	
326 N338	6.069444	25	7.013889	0	
327 N339	-7.25	.25	5.979167	0	
328 N340		.25	6.190972	0	
329 N341	-6.826389	.25	6.402778	0	Annalistic and a second state
330 N342	-6.614583	.25	6.614583	0	
331 N343	-6.402778	.25	6.826389	0	
332 N344	6.190972		7:038194		
333 N345	-5.979167	.25	<u>7.25</u> 6.125	0	
334 N346 335 N347	-7.0625	.25	6.3125	0	
336 N348	-6.875	.25	65	<u> </u>	
337 N349	-6.6875	.25	6.6875	0	
338 N350	-6,5	.25	6.875	0	
339 N351	-6.3125	.25	7.0625	0	
340 N352	-6.125	,25	7.25	Ō	
341 N353	-7.25	.25	6.270833	0	A CHINA CONTRACTOR OF THE OWNER OWNER OF THE OWNER OWN
342 N354		.25	6.434028	0	
343 <u>N355</u>	-6.923611	.25	6.597222	0	
344 N356	-6.760417	:25	6.760417		
345 N357	-6.597222	.25	6.923611	0	
346 N358	<u>-6.434028</u> 6.270822	.25	7.086806	0	
347 N359 348 N360	-6.270833	.25	6.416667		
349 N361	-7.1 <u>11111</u>	.25	6.555556	0	- House of Constitution - House and Constitution - House and
350 N362	-6.972222	.25	6.694444	<u> </u>	
NOOL		<u></u>			

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[C:\...\...\...\823530 - Updated.R3D]



Joint Coordinates and Temperatures (Continued)

Label	X [ft]	Y [ft]	Z [代]	Temp [F]	Detach From Diap
351 N363	-6.833333	.25	6.833333	0	S C AT Man
	-6.694444	.25	6.972222	Ö	
353 N365	-6.555556	.25	7.111111	0	· · · · · · · · · · · · · · · · · · ·
354 N366	-6.416667	.25	7.25	0	
355 N367	-7.25	.25	6.5625	0	
356 N368	-7.135417	.25	6,677083	0	
357 N369	-7.020833	.25	6.791667	0	Color 1
358 N370	-6.90625	.25		- 0	
359 N371	-6.791667	.25	7.020833	0	
360 N372		.25	7.135417	<u> 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 </u>	577965-2E
361 N373	-6,5625	.25	7.25	0	
362 N374	-7.159722	.25	6.798611	0	
363 N375	-7.069444	.25	6.888889	0	
364 N376	-6.979167	.25	6,979167	0	
365 N377	-6.888889	.25	7.069444	0	
366 N378	-6.798611		7.159722	0	
367 N379	-7.038194	25	6.190972	0	Harman Valdau Indi ka shiri da matana
368 N380		25	6,402778	<u> </u>	·····································
369 N381	-6.614583	25	6.614583	0	
370 N382	-6,402778	25	6.826389	0	
371 N383	-6,190972	25	7.038194	0	
372 N384	-7.0625	25	6.3125		· 新教 · 新教主义
373 N385	-6.875	25	6.5	0	
374 N386A	-6,6875	25	6.6875	0	
375 N387A	-6.5	25	6.875	0	
376 N388A	-6,3125	25	7.0625	0	
377 N389A	-7.086806	25	6.434028	0	
378 N390A		25	6.597222	0	新学校である
379 N391A	-6.760417	25	6.760417	0	
380 N392A	-6,597222	25	6.923611	0	
381 N393A	-6.434028	25	7.086806	0	
382 N394A		25	6,555556	0	
383 N395A	-6.972222	25	6.694444	0	
384 N396	-6.833333	25	6.833333		
385 N397	-6.694444	25	6.972222	0	
386 N398		25	7.1111111	0	
387 N399	-7.135417	25	6.677083	0	
388 N400		25		0	
389 N401	-6.90625	25	6.90625	0	
390 N402	-6.791667	-:25	7.020833	0	
391 N403	-6,677083	25	7.135417	0	
392 N404	-6.541667	. 0 -	6.541667	- · · · O	
393 N405	-6.614583	0	6.614583	0	
394 N406	-6.6875	0		0	
395 N407	-6.760417	0	6.760417	0	
396 N408	-6.833333	0			
397 N409	-6.90625	0	6.90625	0	
398 N410	-6.979167	Ŏ.	6.979167	0	
399 N411	-6.541667	25	6.541667	0	
	-6.979167	-:25	6.979167	0	

Joint Boundary Conditions

Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
1 N6	Reaction	Reaction	Reaction	Reaction	Reaction	Reaction
2 N4	Reaction	Reaction	Reaction	Reaction	Reaction	Reaction

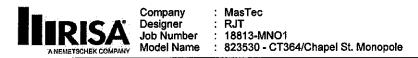
Joint Boundary Conditions (Continued)

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
3	N2	Reaction	Reaction	Reaction	Reaction	Reaction	Reaction
.4	N8	Reaction	Reaction	Reaction	Reaction	Reaction	Reaction

Member Primary Data

2 M2 N71 N73 180 Frame Rail Beam Single Angle A36 Gr.36 T 3 M3 N70 N67 180 Frame Rail Beam Single Angle A36 Gr.36 T 4 M44 N74 N72 180 Frame Rail Beam Single Angle A36 Gr.36 T 5 M5 N1 N2 180 Arm Beam Single Angle A36 Gr.36 T 6 M6 N3 N4 180 Arm Beam Tube A500 Gr.8. T 7 M7 N5 N6 180 Arm Beam Tube A500 Gr.8. T 8 M8 N7 N8 180 Arm Beam Single Angle A36 Gr.36 T 9 M9 N17 N18 180 Support Angle 2 Beam Single Angle A36 Gr.36 T 10 M10 N19 N20 90	voical voical
3 M3 N70 N67 180 Frame Rail Beam Single Angle A36 Gr.36 T 4 M4 N74 N72 180 Frame Rail Beam Single Angle A36 Gr.36 T 5 M5 N1 N2 180 Arm Beam Tube A500 Gr.8. T 6 M6 N3 N4 180 Arm Beam Tube A500 Gr.8. T 7 M7 N5 N6 180 Arm Beam Tube A500 Gr.8. T 8 M8 N7 N8 180 Arm Beam Tube A500 Gr.8. T 9 M9 N17 N18 180 Support Angle 2 Beam Single Angle A36 Gr.36 T 10 M10 N19 N20 90 Support Angle 2 Beam Single Angle A36 Gr.36 T 12 M12 N23 N24 180	/pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical
4 M4 N74 N72 180 Frame Rail Beam Single Angle A36 Gr.36 T 5 M5 N1 N2 180 Arm Beam Tube A500 Gr.B T 6 M6 N3 N4 180 Arm Beam Tube A500 Gr.B T 7 M7 N5 N6 180 Arm Beam Tube A500 Gr.B T 8 M8 N7 N8 180 Arm Beam Tube A500 Gr.B T 9 M9 N17 N18 180 Arm Beam Single Angle A36 Gr.36 T 10 M10 N19 N20 90 Support Angle 2 Beam Single Angle A36 Gr.36 T 11 M11 N21 N22 90 Support Angle 2 Beam Single Angle A36 Gr.36 T 12 M12 N23 N24 180	/pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical
5 M5 N1 N2 180 Arm Beam Tube A500 Gr.B. T 6 M6 N3 N4 180 Arm Beam Tube A500 Gr.B. T 7 M7 N5 N6 180 Arm Beam Tube A500 Gr.B. T 8 M8 N7 N8 180 Arm Beam Tube A500 Gr.B. T 9 M9 N17 N18 180 Arm Beam Single Angle A36 Gr.36 T 10 M10 N19 N20 90 Support Angle 2 Beam Single Angle A36 Gr.36 T 11 M11 N21 N22 90 Support Angle 2 Beam Single Angle A36 Gr.36 T 12 M12 N23 N24 180 Support Angle 2 Beam Single Angle A36 Gr.36 T 13 M13 N25 N26 RIGID	/pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical
6M6N3N4180ArmBeamTubeA500 Gr.B.T7M7N5N6180ArmBeamTubeA500 Gr.B.T8M8N7N8180ArmBeamTubeA500 Gr.B.T9M9N17N18180Support Angle 2BeamSingle AngleA36 Gr.36T10M10N19N2090Support Angle 2BeamSingle AngleA36 Gr.36T11M11N21N2290Support Angle 2BeamSingle AngleA36 Gr.36T12M12N23N24180Support Angle 2BeamSingle AngleA36 Gr.36T13M13N25N26RIGIDNoneNoneRIGIDT14M15N29N30RIGIDNoneNoneRIGIDT15M17N33N34RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle Angle A36 Gr.36T18M22N43N4490Support Angle 1BeamSingle Angle A36 Gr.36T19M23N45N46180Support Angle 1BeamSingle Angle A36 Gr.36T	/pical /pical /pical /pical /pical /pical /pical /pical /pical /pical /pical
7M7N5N6180ArmBeamTubeA500 Gr.B.T8M8N7N8180ArmBeamTubeA500 Gr.B.T9M9N17N18180Support Angle 2BeamSingle AngleA36 Gr.36T10M10N19N2090Support Angle 2BeamSingle AngleA36 Gr.36T11M11N21N2290Support Angle 2BeamSingle AngleA36 Gr.36T12M12N23N24180Support Angle 2BeamSingle AngleA36 Gr.36T13M13N25N26RIGIDNoneNoneRIGIDT14M15N29N30RIGIDNoneNoneRIGIDT15M17N33N34RIGIDNoneNoneRIGIDT16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle Angle A36 Gr.36T18M22N43N4490Support Angle 1BeamSingle Angle A36 Gr.36T19M23N45N46180Support Angle 1BeamSingle Angle A36 Gr.36T	/pical /pical /pical /pical /pical /pical /pical /pical /pical /pical
8M8N7N8180ArmBeamTubeA500 Gr.B.T9M9N17N18180Support Angle 2BeamSingle Angle A36 Gr.36T10M10N19N2090Support Angle 2BeamSingle Angle A36 Gr.36T11M11N21N2290Support Angle 2BeamSingle Angle A36 Gr.36T12M12N23N24180Support Angle 2BeamSingle Angle A36 Gr.36T13M13N25N26RIGIDNoneNoneRIGIDT14M15N29N30RIGIDNoneNoneRIGIDT15M17N33N34RIGIDNoneNoneRIGIDT16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle Angle A36 Gr.36T18M22N43N4490Support Angle 1BeamSingle Angle A36 Gr.36T19M23N45N46180Support Angle 1BeamSingle Angle A36 Gr.36T	vpical vpical vpical vpical vpical vpical vpical vpical vpical vpical
9M9N17N18180Support Angle 2BeamSingle AngleA36 Gr.36T10M10N19N2090Support Angle 2BeamSingle AngleA36 Gr.36T11M11N21N2290Support Angle 2BeamSingle AngleA36 Gr.36T12M12N23N24180Support Angle 2BeamSingle AngleA36 Gr.36T13M13N25N26RIGIDNoneNoneRIGIDT14M15N29N30RIGIDNoneNoneRIGIDT15M17N33N34RIGIDNoneNoneRIGIDT16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle AngleA36 Gr.36T18M22N43N4490Support Angle 1BeamSingle AngleA36 Gr.36T19M23N45N46180Support Angle 1BeamSingle AngleA36 Gr.36T	rpical rpical rpical rpical rpical rpical rpical rpical rpical
10M10N19N2090Support Angle 2BeamSingle Angle A36 Gr.36T11M11N21N2290Support Angle 2BeamSingle Angle A36 Gr.36T12M12N23N24180Support Angle 2BeamSingle Angle A36 Gr.36T13M13N25N26RIGIDNoneNoneRIGIDT14M15N29N30RIGIDNoneNoneRIGIDT15M17N33N34RIGIDNoneNoneRIGIDT16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle Angle A36 Gr.36T18M22N43N4490Support Angle 1BeamSingle Angle A36 Gr.36T19M23N45N46180Support Angle 1BeamSingle Angle A36 Gr.36T	/pical /pical /pical /pical /pical /pical /pical
11M11N21N2290Support Angle 2BeamSingle AngleA36 Gr.36T12M12N23N24180Support Angle 2BeamSingle AngleA36 Gr.36T13M13N25N26RIGIDNoneNoneRIGIDT14M15N29N30RIGIDNoneNoneRIGIDT15M17N33N34RIGIDNoneNoneRIGIDT16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle AngleA36 Gr.36T18M22N43N4490Support Angle 1BeamSingle AngleA36 Gr.36T19M23N45N46180Support Angle 1BeamSingle AngleA36 Gr.36T	vpical vpical vpical vpical vpical vpical vpical
12M12N23N24180Support Angle 2BeamSingle AngleA36 gr.36T13M13N25N26RIGIDNoneNoneNoneRIGIDT14M15N29N30RIGIDNoneNoneRIGIDT15M17N33N34RIGIDNoneNoneRIGIDT16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle AngleA36 gr.36T18M22N43N4490Support Angle 1BeamSingle AngleA36 gr.36T19M23N45N46180Support Angle 1BeamSingle AngleA36 gr.36T	(pical (pical (pical (pical (pical (pical
13M13N25N26RIGIDNoneNoneRIGIDT14M15N29N30RIGIDNoneNoneRIGIDT15M17N33N34RIGIDNoneNoneRIGIDT16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle AngleA36 Gr.36T18M22N43N4490Support Angle 1BeamSingle AngleA36 Gr.36T19M23N45N46180Support Angle 1BeamSingle AngleA36 Gr.36T	vpical vpical vpical vpical vpical
14M15N29N30RIGIDNoneNoneRIGIDT15M17N33N34RIGIDNoneNoneRIGIDT16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle AngleA36 Gr.36T18M22N43N4490Support Angle 1BeamSingle AngleA36 Gr.36T19M23N45N46180Support Angle 1BeamSingle AngleA36 Gr.36T	(pical (pical (pical (pical
15M17N33N34RIGIDNoneNoneRIGIDT16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle AngleA36 Gr.36T18M22N43N4490Support Angle 1BeamSingle AngleA36 Gr.36T19M23N45N46180Support Angle 1BeamSingle AngleA36 Gr.36T	/pical /pical /pical
16M19N37N38RIGIDNoneNoneRIGIDT17M21N41N42180Support Angle 1BeamSingle AngleA36 Gr.36T18M22N43N4490Support Angle 1BeamSingle AngleA36 Gr.36T19M23N45N46180Support Angle 1BeamSingle AngleA36 Gr.36T	/pical /pical
17M21N41N42180Support Angle 1BeamSingle AngleA36 Gr.36T18M22N43N4490Support Angle 1BeamSingle AngleA36 Gr.36T19M23N45N46180Support Angle 1BeamSingle AngleA36 Gr.36T	pical
18 M22 N43 N44 90 Support Angle 1 Beam Single Angle A36 Gr 36 T 19 M23 N45 N46 180 Support Angle 1 Beam Single Angle A36 Gr 36 T	
19 M23 N45 N46 180 Support Angle 1 Beam Single Angle A36 Gr.36 T	
	pical
20 M24 N47 N48 90 Support Angle 1 Beam Single Angle A36 Gr 36 T	pical
	pical
22 M26 N51 N52 180 Mount Pipe Column Pipe A53 Gr.B Ty	pical
23 M27 N53 N54 180 Mount Pipe Column Pipe A53 Gr.B T	pical
24 M28 N55 N56 180 Mount Pipe Column Pipe A53 Gr.B Tv	pical
25 M29 N57 N58 180 10' MP Column Pipe A53 Gr.B T	pical
	pical
	pical
	pical
29 M33 N392 N391 10' MP Column Pipe A53 Gr.B T	pical
39 M39 N107 N158 RIGID None RIGID To 40 M40 N114 N159 RIGID RIGID None RIGID To	pical pical
40 None None Rigid T	pical
	pical
50 M50 N183 N240 RIGID None None RIGID To	

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Member Primary Data (Continued)

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Туре	Design List	Material	Design Rules
51	M51	N190	N241			RIGID	None	None	RIGID	Typical
52	M52	N197	N242	网络高学校		RIGID	None	None	RIGID	Typical
53	M53	N204	N243	PGD THE INCOMPANY		RIGID	None	None	RIGID	Typical
54	M54	N210	N244			RIGID	None	None	RIGID	Typical
55	M55	N220	N240			RIGID	None	None	RIGID	Typical
<u>56</u> 57	M56	N225 N230	N241 N242			RIGID. RIGID	None None	None None	RIGID. RIGID	Typical Typical
57	M57 M58	N235		a de la compañía		RIGID	None	None	RIGID	Typical
59	M59	N253	N321	en an		RIGID	None	None	RIGID	Typical
60	M60		N322		1.18 12 32 22 3		None	None	RIGID	Typical
61	M61	N259	N322	The second se	Contranspondential and the second s	RIGID	None	None	RIGID	Typical
62	M62	N266	N323		复资, 通过	RIGID	None	None	RIGID	Typical
63	M63	N273	N324			RIGID	None	None	RIGID	Typical
64	M64	N280	s wearing a second start of start of	2. 刘康公、禄		RIGID	None	None	RIGID	Typical
65	M65	N287	N326		aligned Marson of the Science Aligned	RIGID	None	None	RIGID	Typical
66	M66		N327			RIGID	None	None	RIGID	Typical
67	M67	N303	N323	·····································		RIGID	None	None	RIGID	Typical
68	<u>M68</u>	N308			R. P. Los	RIGID	None	None	RIGID	Typical
69 70	<u>M69</u> M70	N313 N318	N325 N326			RIGID	None None	None None	RIGID RIGID	Typical Typical
71	M70 M71	N336	N404			RIGID	None	None	RIGID	Typical
72	M72	N381	N404			RIGID	None	None	RIGID	Typical
73	M73	N342	N405	States		RIGID	None	None	RIGID	Typical
74	M74	N349	N406			RIGID	None	None	RIGID	Typical
75	M75	N356	N407	11 Y Station and a Comparison		RIGID	None	None	RIGID	Typical
76	M76	N363	N408	1 1		RIGID	None	None	RIGID	Typical
77	M77	N370	N409			RIGID	None	None	RIGID	Typical
.78	<u>M78</u>	N376	N410			RIGID	None	None	RIGID	Typical
79	<u>M79</u>	N386A	N406			RIGID	None	None	RIGID	Typical
80	<u>M80</u>	N391A	N407		210	RIGID	None	None	RIGID	Typical
81	<u>M81</u>	N396	N408				None	None	RIGID	Typical
82	M82	N401	N68A	1984 - C.	<u> </u>	RIGID	None None	None None	RIGID	Typical Typical
83 84	<u>M83</u> M84	N72A	N73A			RIGID	None	None	RIGID	Typical
85	M85	N76	N70A			RIGID	None	None	RIGID	Typical
86	M86	N78	N77	a de la compañía de l		RIGID	None	None	RIGID	Typical
87	M87	N80	N71A	 C. A. Warden and Management and M Management and Management a Management and Management and Mana Management and Management and Manag Management and Management and Management	Philosophilicity 12 Color	RIGID	None	None	RIGID	Typical
88	M88		N81			RIGID	None	None	RIGID	Typical
89	M89	N84	N83			RIGID	None	None	RIGID	Typical
90	M90	N86	N85			RIGID	None	None	RIGID	Typical
91	<u>M91</u>	N174	N213	14.0	1.228-14. http://www.committed/2016	RIGID	None	None	RIGID	Typical
92	<u>M92</u>	N202	N233	an a	an a	RIGID	None	None	RIGID	Typical
93	<u>M93</u>	N206	N237			RIGID	None	None	RIGID	Typical
94	M94					RIGID	None	None	RIGID RIGID	Typical
95 96	M95 M96	N257 N285	N296 N316			RIGID	None None	None None	RIGID	Typical Typical
97	M97	N289	N320		ng yang salar 19	RIGID	None	None	RIGID	Typical
-98	M98 M	N261			Reference (*	RIGID	None	None	RIGID	
99	M99	N340	N379	with the state of		RIGID	None	None	RIGID	Typical
100	M100	N368	N399			RIGID	None	None	RIGID	Typical
101	M101	N372	N403			RIGID	None	None	RIGID	Typical
102	M102		N383			RIGID	None	None	RIGID	Typical
103	M103	N71A	N291			RIGID	None	None	RIGID	Typical
104	M104	N80				RIGID	113	None	RIGID	Typical
105	<u>M105</u>	<u>N86</u>	N255			RIGID	None	None	RIGID	Typical
106	M106	N85				RIGID	None	None	RIGID	Typical
107	<u>M107</u>	N83	N374			RIGID	None	None	RIGID	Typical

RISA-3D Version 17.0.2

[C:\...\...\...\...\823530 - Updated.R3D]

Member Primary Data (Continued)

	Label	i Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Туре	Design List	Material	Design Rules
108	M108	N84	N334			RIGID	None	None	RIGID	Typical
109	M109	N74A	N338			RIGID	None	None	RIGID	Typical
110	M110	N73A	N378			RIGID	None	None	RIGID	Typical
111	M111	N68A	N125			RIGID	None	None	RIGID	Typical
112	M112	N72A	N85A			RIGID	None	None	RIGID	Typical
113	M113	N78	N89			RIGID	None	None	RIGID	Typical
114	M114	N77	N129	er en se se se		RIGID	None	None	RIGID	Typical
115	M115	N70A	N208			RIGID	None	None	RIGID	Typical
116	M116	N76	N168	你都好了。		RIGID	None	None	RIGID	Typical
117	M117	N82	N172			RIGID	None	None	RIGID	Typical
118	M118	N81	N212			RIGID	None	None	RIGID	Typical
<u>Joint L</u>	oads and	d Enforce Joint Label	ed Displa	<u>icement</u>	<u>s (BLC 4</u> l,d,m	1 <u>2 : Man 1 (</u>	500 Ibs) Direction		eľ(k,k-ft), (in	,rad), (k*s^2/f
1		N20			L		Y		- 25	
Joint Loads and Enforced Displacements (BLC 43 : Man 2 (500 lbs))										
		Joint Label			L.D.M	·····	Direction	Magnitud		.rad). (k*s^2/f
1		N23			_		Y		25	
_Joint Lo	oads and	<u>l Enforce</u>	ed Displa	<u>icement</u>	<u>s (BLC 4</u>	4 : Man 3 (500 lbs))		
		Joint Label			L,D,M		Direction	Magnitud	<u>e[(k,k-ft), (in</u>	,rad), (k*s^2/f
1		N22			<u> </u>		Y		25	
_Joint Lo	oads and	<u>l Enforce</u>	ed Displa	cement	<u>s (BLC 4</u>	1 <mark>5 ; Man 4 (</mark> 2	250 (bs))		
		Joint Label			L,D,M		Direction	Magnitud	e[(k,k-ft), (in	rad), (k*s^2/f
1									0	
Joint Loads and Enforced Displacements (BLC 46 : Man 5 (250 lbs))										
		Joint Label			L,D,M		Direction	Magnitud	<u>e[(k,k-ft), (in</u>	.rad), (k*s^2/f
1							- ·		0	
Joint Loads and Enforced Displacements (BLC 47 : Man 6 (250 lbs))										
		Joint Label			L,D,M		Direction	Magnitud	e[(k,k-ft), (in	.rad). (k*s^2/f
1									0	
······································				•						···· · · · · · · · · · · · · · · · · ·

Member Point Loads (BLC 1 : Dead)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M28	Y	048	%9.6
2	M25	ette Y		%50
3	M25	Y	075	%30
4	M32	\mathbf{Y}	048	%9.6
5	M32	Y	011	%30
6	M33	Y Y	-128	%50
7	M33	Y	075	%30
8	M30	rasi Y d	5,014	%50
9	M30	Y	011	%4.5
10	M30	Y	<u>-015</u>	%6.5
11	M29	Y	- 128	%50
12	M29	Y	-,075	<u> </u>
13	M26	Y	014	%50

Member Point Loads (BLC 1 : Dead) (Continued)

	Member Label	Direction	Magnitude[k.k-ft]	Location[ft,%]
14	M26	Y	,1 ho	%4,5
15	M26	Y	015	%6.5
16	M27	, на ү к	- <u>009</u>	%30.5
17	M34	Y	014	%50
18	<u>M34</u>	Y	<u>-011 / / / / / / / / / / / / / / / / / / </u>	<u>%4.5</u>
19	M34	Y	015	%6.5

Member Point Loads (BLC 2 : Ice Dead)

Member Label	Direction	Magnitude[k.k-ft]	Location[ft,%]
1 M28	Y	263	%9.6
2 M25	Y	-,472	<u>%50</u>
3 M25	Y	048	%30
4 M32	Y Y	<u>263</u>	%9.6
5 M32	Y	062	%30
M33	Y S	-,472	<u>%50</u>
7 M33	Υ	048	%30
8 M30	• Ya-3	-,103	%50
9 M30	Y	011	%4.5
10 M30 M30	Ŷ	018	%6.5
11 M29	Y	472	%50
12 M29	Y Y	048	%30
13 M26	Y	103	%50
14 M26	Ý –	<u>-011</u>	%4.5
15 M26	Υ	018	%6.5
16 M27	Y A	327	4) - L %30.5 H
17 M34	Y	103	%50
18 M34	<u>Y</u> Y	-,011	%4.5
19 M34	Y	018	%6.5

Member Point Loads (BLC 3 : Full Wind Antenna (0 Deg))

Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1 M28	Z	- 104	%9.6
2 M25	• Z	-,362 (1)	%10
3 M32	Z	302	%9.6
4 M32	Z	-,058	%30
5 M33	Z	159	%10
6 M30	Ζ	- <u>.078</u>	0
7 M29	Z	-,362	%10
8 M26	25Z	-,078	and an and an and a second
9 M27	Z	082	%30.5
10 M34	• Z	082 - 035	0
11 M25	Z	362	%90
12 M33	Z	1/59	%90
13 M30	Z	078	%100
14 M29	-, Z	-362	%90
15 M26	Z	078	%100
16 M34	Z	035	%100

Member Point Loads (BLC 4 : Full Wind Antenna (30 Deg))

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft.%]
1	M28	Ζ.	133	%9.6
2	M25	Z Z	- 27	%10
3	M32	Z	218	%9.6
4	M32	r Z -	- 05 is in the second	<u>%30</u>
5	M33	<u>Z</u>	182	%10



Member Point Loads (BLC 4 : Full Wind Antenna (30 Deg)) (Continued)

	Member Label	Direction	Magnitude[k.k-ft]	Location[ft,%]
6	MBO	Z	058	0
7	M29	Z	27	<u>%10</u>
8	M26	Z	058	
9	M27	Ζ	167	<u>%30.5</u>
10	M34	Ζ	04	0
11	M25	<u>Z</u>	27	<u>%90</u>
12	M33	State Z	-,1 <u>82</u>	<u>%90</u>
13	M30	<u>Z</u>	058	%100
14	M29	<u>Z</u>	27	***
15	M26	<u>Z</u>	058	%100
16	M34	<u>Z</u>	04	%100
17	M28	X	.077	%9,6
18		X	156	%10
19	<u>M25</u>	<u> </u>	.005	%30
20	M32	× ×	126	%9.6
21	M32			%30
22	M33	Xe	<u>. 105. e se s</u>	%10
23	M33	X		%30
24	M30	X	<u>1034 - Electronic de la companya de</u>	0
25	<u>M30</u>	X	.001	%4.5
26	M30	X	.002	%6.5
27	M29	X	<u>.156</u>	%10
28	M29	X	.005	%30
29	M26	X	.034	0
30	M26	X	.001	%4.5
31	M26	X	.002	%6.5
32	M27	X	.097	%30.5
33	<u>M34</u>	X	.023	0
34	<u>M34</u>	<u>X</u>	002	%4.5 %6.5
35	M34	X	.005 .156	%6.5 %90
36	M25			<u>%90</u> %90
37	M33	X X	.105 .034	<u>%90</u>
-38	<u>M30</u>			<u>%100</u> %90
39	M29	X	. <u>156</u> .034	%90
40	<u>M26</u>		.023	%100
41	<u>M34</u>	X	.023	70 IUU

Member Point Loads (BLC 5 : Full Wind Antenna (60 Deg))

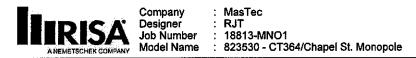
	Member Label	Direction	Magnitude[k.k-ft]	Location[ft,%]
1	M28	Z	126	%9.6
2	M25	- Z	≥1 <u>05</u>	<u>%10</u>
3	M32	Z	077	%9.6
4	M32	Z (<u>%30</u>
5	M33	Ζ	156	%10
6	M30		023	0
7	M29	Ζ	105	%10
8	M26	★ 2	023	0
9	M27	Ž	207	%30.5
10	M34	Z 2 2	-i034 ELA	
11	M25	<u>Z</u>	105	%90
12	M33	Z K	- 156	%90
13	M30	Z	023	%100
14	*M29	Z	- 105	%90
15	M26	Z	023	%100
16	M34	Z	-,034	%100
17	M28	X	.218	%9.6

Member Point Loads (BLC 5 : Full Wind Antenna (60 Deg)) (Continued)

	Member Label	Direction	Magnitude[k.k-ft]	Location[ft,%]
18	M25	X	.182	<u>%10</u>
19	M25	X	.027	%30
20	<u>M32</u>	X	.133	%9.6
21	<u>M32</u>	Х	.05	%30
22	M33	X	.27	%10
23	M33	X	.009	%30
24	<u>M30</u>	X	.04 – – – – – – – – – – – – – – – – – – –	0
25	M30	X	.004	%4.5
26	<u>M30</u>	X	.008	%6.5
27	M29	X	.182	%10
28	<u>M29</u>	A A A A	.027	<u>%30</u>
29	M26	X	.04	0
30	M26	X	,004	<u>%4,5</u>
31	M26	X	.008	%6.5
32	M27	Х — К	<u></u>	%30.5
33	<u>M34</u>		.058	
34	M34	X	.001	%4.5
35	M34	۲ <mark>X</mark>	.003_	%6.5
36	<u>M25</u>	X	182	<u>%90</u>
37	<u>M33</u>	X	.27	<u>%90</u>
-38	<u>M30</u>	X	.04	%100
39	M29	X	.182	%90
40	<u>M26</u>	X	.04	<u>%100</u>
41	M34	X	.058	%100

Member Point Loads (BLC 6 : Full Wind Antenna (90 Deg))

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M28	Z	0	%9.6
2	M25	- Z		%10
3	M32	Z	0	%9.6
4	M32	Z 2	Ō	<u>%30</u>
5	M33	Ζ	0	%10
6	M30	Z	<u>o</u>	
7	M29	Ζ	0	%10
8	M26	<u>z</u>	0	0
9	M27	Z	0	%30.5
10	M34	2 Z	<u>its o</u>	
11	M25	<u>Z</u>		%90
12	M33	<u>Z</u>	0	%90
13	M30	Z		%100
14	M29	Z	0	<u>%90</u>
15	M26	<u> </u>	0	%100
16	<u>M34</u>	Zinter	<u>0</u>	%100
17	<u>M28</u>	X	.302	%9.6
18	- <u>M25 mail and a</u>	<u>X</u>	.1 <u>59</u>	%10
19	M25		.041	%30
20	M32	<u>X</u>	d104	%9,6
21	M32	X	.058	%30
22	M33	X	<u>:362</u>	%10
23	M33	X	0	%30
24	<u>M30</u>	X	.035	0
25	M30	X	.006	<u>%4.5</u>
26	<u>M30</u>	X	.013	%6.5
27	M29	X	.159	%10
28	M29	X	.041	%30
29	M26	Х	.035	0

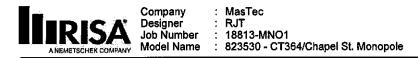


Member Point Loads (BLC 6 : Full Wind Antenna (90 Deg)) (Continued)

	Member Label	Direction	Magnitude[k.k-ft]	Location[ft.%]
30	M126	X	.006	%4.5
31	M26	Χ	.013	%6.5
32	M27	X	525	<u>%30.5</u>
33	M34	Х	.078	0
34	M34	X - 2	0	%4.5
35	M34	Х	0	%6.5
36	M25	X	.159	%90
37	M33	Х	.362	%90
38	M30	X	.035	%100
39	M29	X	.159	<u>%90</u>
40	<u>M26</u>	X	.035	%100
41	M34	Х	.078	%100

Member Point Loads (BLC 7 : Full Wind Antenna (120 Deg))

Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1 M28	Z	.126	%9.6
2 M25	- Z	.105	<u>%10</u>
3 M32	Z	.077	%9.6
4 M32	Z	.029	%30
5 M33	Z	.156	%10
6 M30	z z z	.023	.
7 M29	Ζ	.105	%10
8 M26	<u>Z</u>	. <u>023</u>	<u>0</u>
9 M27	Z	.207	%30.5
10 M34	Z		0
11 M25	Z	.105	%90
12 M33	\mathbf{Z}	156	%90
13 M30	Z	.023	<u>%100</u>
14 M29	Z (*)	.105	%90
15 M26	Z	.023	%100
<u>16</u>	<u>z</u> .	.034	%100
17 M28	X	.218	%9.6
18 M25	X	.182	%10
<u>19 M25</u>	X	.027	<u>%30</u>
20 M32	X	.133	<u>%9.6</u>
21 <u>M32</u>		<u>.05</u>	%30
22 M33	X		%10
23 M33			%30
24 M30	X	.04	
25 <u>M30</u>	<u>X</u>	.004	%4.5
26 M30	X	008	%6.5
27 M29	X X	.182	<u>%10</u> %30
28 M29			
29 <u>M26</u>	X	.04	0 %4.5
30 M26	A second	.004	%4.5 %6.5
31 M26	X	.008 359	%0.5 %30.5
VE			0
33 M34	X	<u>.058</u> 001	%4.5
34 M34		.003	%4.5 %6.5
35 M34 36 M25	X	.182	<u>%8.5</u> %90
			%90
37 <u>M33</u> 38 M30	X X		<u>%90</u> %100
	X	.182	%90
39 M29 40 M26	Î	.182	<u>%90</u>
		.04	<u>%100</u> %100
41 M34	X	060.	70100

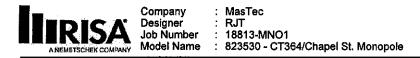


Member Point Loads (BLC 8 : Full Wind Antenna (150 Deg))

	Member Label	Direction	Magnitude[k.k-ft]	Location[ft.%]
1	M28	Z	.133	%9.6
2		<u>z</u>	27	%10
3	M32	Z	.218	<u>%9.6</u>
4		Z	.05	%30
5	<u>M33</u>		. <u>182</u>	<mark>%10</mark>
6	M30	<u> </u>	.058	0
7	<u>M29</u>	<u> </u>	.27	<u>%10</u>
8	M26		.058	Conditional and a subsection of the section of the
9	M27	Z Z	.167	<u>%30.5</u>
	M34	Z	.04 .27	%90
11	M25 M33	Z Z		%90 %90
13	M33 M30		.058	%100
14	M30 M29	Z 7	27	%100
15	M29 M26	7	.058	%100
16	M20 M34	Z******	.04	%100
17	MOT M28	X	.077	%9.6
18		X	.156	%10
19	M25	X	.005	%30
20	M32	X	126	<u>%9.6</u>
21	M32	Х	.029	%30
22		· X · · ·	.105	%10
23	M33	X	.015	%30
_24	M30	X	.034	0
25	M30	X	.001	%4.5
26	M30	X	.002	<u>%6.5</u>
27	M29	X	.156	%10
28	M29	X	.005	%30
29	M26	X	.034	0
30	M26	X	.001	%4,5
31	<u>M26</u>		.002	%6.5
32	M27	X .	097	%30.5
33	<u>M34</u>		.023	
34	M34	X	002	%4.5 %6.5
35	M34	<u>X</u>	<u>.005</u> 156	%6.5 %90 😤
36	M25	Providence and the state of the second s	.105	%90 %90
37 38	M33 M30	X	.034	<u>%90</u> %100
39	M30 M29	X	.156	%100
40	M29 M26	Ŷ	.138	%90 %100
41	M34	X	.034	<u>%100</u>
41	WI34	·····		70 100

Member Point Loads (BLC 15 : Ice Wind Antenna (0 Deg))

Me	mber Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M28	- <u>Z</u>	045	%9.6
2	M25	<u> – Z – – – – – – – – – – – – – – – – – </u>	074	%10
3	M32	Z	077	%9.6
4 1 1 1	M32	- Z	022	%30
5	M33	Z	038	%10
6	M30	Z / S - S	<u>e</u>	0
7	M29	Z	074	%10
8 8 1 1 1	M26	这些意义之 <mark>之</mark> 全的正式是	02	0
9	M27	Z	035	%30.5
10	M34	Z	<u>-,012</u>	
11	M25	Z	074	%90
12	M33	2	038	%90



Member Point Loads (BLC 15 : Ice Wind Antenna (0 Deg)) (Continued)

	Member Label	Direction	Magnitude[k.k-ft]	Location[ft.%]
13	M30	Z	02	%100
14	M29"	• Z	-074	<u>%90</u>
15	M26	Z	02	%100
16	M34	Z Z	- 012	%100

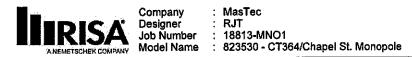
Member Point Loads (BLC 16 ; Ice Wind Antenna (30 Deg))

Member Label	Direction	Magnitude[k.k-ft]	Location[ft.%]
1 <u>M28</u>	Z	046	%9.6
2 M25	<u>Z</u>		<u>%10</u>
3 M32	Z	06	%9.6
4 M32	Z	-,019	%30
5 M33	<u>Z</u>	04	%10
<u>6</u> M30	Z	015	0
7 M29	<u>Z</u>	056	<u>%10</u>
<u>8</u> <u>M26</u>	Z	015	0
9 M27	<u>Z</u>	046	%30.5
10 M34	Ζ.	<u>-012</u>	<u> </u>
11 M25	Z Z	056	%90
12 M33		- 04	%90
13 M30	Z	015	%100
14 M29	· 🤹 Z	056	
15 M26	Z	015	%100
. 16 M34	Ż	012	%100
17 M28	X	.027	%9.6
18 M25	X	.032	%10
19 M25	X	.002	%30
20 M32	X	<u>.034</u>	%9.6
21 M32	X	.011	%30
.22 M33	X	.023	%10
23 M33	Х	.005	%30
24 M30	X	.009	0 🗧
25 M30	X	0	%4.5
26 M30	X	.001	%6.5
27 M29	X	.032	%10
28 M29	X	002 1	%30
29 M26	X	.009	0
30 M26	Х —	0 ² -	%4.5
	Х	.001	%6.5
<u>32</u> M27	X		**********
33 M34	X	.007	0
34. M34	X	.001	%4.5
35 M34	Х	.002	%6.5
<u>. 36 M25 M</u>	X	.032	<u>%90</u>
37 M33	X	.023	%90
38 M30	X	.009	%100
39 M29	Х	.032	%90
40 M26	X	.009	%100
_41M34	X	.007	%100

<u>Member Point Loads (BLC 17 : Ice Wind Antenna (60 Deg))</u>

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M28	Z	034	%9.6
2	M25	Z		%10
3	M32	Z	027	%9.6
4	M32	The Zala	011	%30
5	M33	Z	032	%10

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<u>Member Point Loads (BLC 17 : Ice Wind Antenna (60 Deg)) (Continued)</u>

Member Label	Direction	Magnitude[k,k-ft]	Location[ft.%]
6 M30	· 学生Z 单义	007	0
7 M29	<u> </u>	023	%10
8 M26	7 Z	007	Output Sale
9 <u>M27</u>	Ζ	<u>046</u>	%30.5
10 M34	Z Z	009	
11 M25	<u>Z</u>	023	%90
12. M33	Z	032	%90
13 M30		007	%100
14 M29	Z	 ,023	%90
15 M26	Z	007	%100
16 M34	Z (6.1)	.009	%100
17 <u>M28</u>	<u>X</u>	.06	%9.6
18 M25	X manual	04	%10
19 M25		.008	%30
20 M32	X		%9.6
21 M32	X	.019	%30
22 M33	Dooler Provide the second		%10
23 M33	X	.003	%30
24 Mi30		012	
25 <u>M30</u>	X	.002	%4.5 %6.5
26 M30			% 0.0 %10
27 M29 28 M29	X	<u>.04</u> .008	%10
20 No. 10 No.	The second s		0
29 <u>M26</u>	X	<u>.012</u> .002	%4.5
30 M26	X	.004	%6.5
31 M26 32 M27			%30:5
	A V	.015	0
33 M34 34 M34		013	%4,5
34 M34 35 M34	Y	.001	%6.5
36 M04	$\overline{\mathbf{x}}$		<u>%90</u>
37 M33	X	.056	%90
38 (M30	x X	012	%100 · · ·
39 M29	X	.04	%90
40 M26	× ×	.012	%100
41 M34	X	.015	%100

Member Point Loads (BLC 18 : Ice Wind Antenna (90 Deg))

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft.%]
1	M28	Ζ	0	%9.6
2	M25	<u>z</u>	0.	<u>%10</u>
3	M32	Ζ	0	%9.6
4 4	M32	Z	0	<u>%30</u>
5	M33	<u> </u>	0	%10
6	M30	Ζ	0	
7	M29	Z	0	%10
8	M26	z Z	<u> </u>	0
9	M27	Z	0	%30.5
10	M34	<u>Z</u>	0	0
11	M25	Z	0	%90
12	M33 E	<u>Z</u>	0	%90
13	M30	Ζ	0	%100
14世	M29	Z Z	0	%90
15	M26	Ζ	0	%100
16	M34	netse die en Zeroen zie en	0	<u>%100</u>
17	M28	X	.077	%9.6

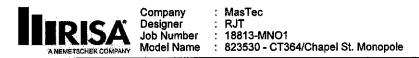


Member Point Loads (BLC 18 : Ice Wind Antenna (90 Deg)) (Continued)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
18	M25	X	.038	%10
19	M25	X	.012	%30
20	M32	- X	.045	%9.6
21	M32	<u>X</u>	.022	%30
22	<u>M33</u>	X	<u>1074 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 </u>	%10
23	M33	X		%30
24	M30	X	.012	0
25	M30	X	.004	%4.5
26	M30	X	.006	%6,5
27	M29	X	.038	<u>%10</u>
28	M29	<u> </u>	.012	%30
29	<u>M26</u>	X	.012	
30	<u>M26</u>	X	.004	%4.5
31	M26	X	.006	%6.5
32	M27	- X - A - A - A - A - A - A - A - A - A -		%30.5
33	<u>M34</u>	X	.02	
34	<u>M34</u>	X	0	%4,5
35	<u>M34</u>	X	U	%6.5
-36	M25	N	.038	%90 %00
37	<u>M33</u>	X	.074	<u>%90</u>
38	M30	X	.012	%100
39	M29		.038	<u>%90</u>
40	<u>M26</u>	X	.012	<u>%100</u>
41	<u>M34</u>	<u> </u>	.02	%100

Member Point Loads (BLC 19 : Ice Wind Antenna (120 Deg))

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M28	Z	.034	%9.6
2	M25	<u>Z</u>	.023	%10
3	M32	<u> </u>	.027	<u>%9.6</u>
- 4	<u>M32</u>	$z \in \mathbf{Z}$		%30
5	M33	Z	.032	%10
ି 6	<u>M30</u>	<u> </u>		
7	M29	Ζ	.023	%10
8	M26	Z	.007	0
9	M27	Z	.046	%30.5
10	M34	Z		0
11	M25	Z	.023	%90
12	M33	Z	.032	%90
13	<u>M30</u>	Ż.	.007	%100
-14	M29	Z		%90
15	<u>M26</u>	Z	.007	%100
16	M34	Z	009	%100
17	<u>M28</u>	X	.06	<u>%9.6</u>
18	<u>M25</u>	X	.04	%10
19	<u>M25</u>	X	.008	<u>%30</u>
20	M32	X	046	<u>%9,6</u>
21	<u>M32</u>	X	.019	%30
22	M33	X	056	<u>%10</u>
23	<u>M33</u>	X N	.003	<u>%30</u>
24	M30	X	.012	
25	<u>M30</u>	X 101 ¥45 - 11 - 41 - 44	<u>.002</u> 004	%4.5 %6.5
26	M30	λ V		%10
27	M29		.04 .008	%10 %30
28	M29	X V		
29	M26	<u> </u>	.012	0



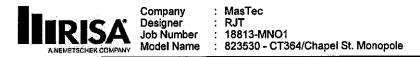
Member Point Loads (BLC 19 : Ice Wind Antenna (120 Deg)) (Continued)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
30	M26	X	.002	%4.5
31	M26	X	.004	%6.5
32	M27	<u>х</u>	±_079 = ₹ = ± ± ≤	<u>%30.5</u>
33	M34	Χ	.015	0
34	M34	× ×	.001	%4.5
35	M34	Х	.001	%6.5
36	M25	X	.04	%90
37	M33	Х	.056	%90
38	MB0	X	101 <u>2</u>	%100
39	M29	Х	.04	%90
40	M26	X	.012	%100
41	M34	Х	.015	%100

Member Point Loads (BLC 20 : Ice Wind Antenna (150 Deg))

	Member Label	Direction	Magnitude[k.k-ft]	Location[ft,%]
1	<u>M28</u>	<u>Z</u>	.046	<u>%9.6</u>
2	M25	Z	<u>.023</u> .027	%10 %9.6
3	M32 M32	<u> </u>	.011	%9.6 %30
4 5	M33	Z	.032	%10
Ğ	M30	-2	.007	0 1.0
7	M29	Z	.023	%10
8		Z Z	.007	0
9	M27	Z	.046	%30.5
10	M34	Z	. <u>00</u> 9	- O
11	M25	Z	.023	%90
-12	M33	Z - John S	032	<u>%90</u>
13	<u>M30</u>	Z	.007	%100 %00
14	M29	Z Z	.023 .007	%90 %100
<u>15</u>	M26	<u> </u>	.007	%100
17	M34	X	.027	%9.6
18	M25	$\hat{\mathbf{x}}$		%10 %10
19	M25	X	.008	%30
20	M32	X X	.046	%9.6
21	M32	Х	.019	%30
22	M33	X	.056	%10
23	M33	Х	.003	%30
24	M30	X	.012	
25	M30	X	.002	%4.5
26	<u>M30</u>	X	.004	%6.5
27	M29	X Maria X	<u>.04</u> .008	<u>%10</u> %30
28	<u>M29</u>	ALL THE LEASE AND A REPORT OF	.018	0
<u>29</u> 30	M26 M26	X X	002	%4.5
31	M20	X	.002	%6.5
32	M20 M27	X	.079	%30.5
33	M34	X	.015	0
34	M34	X	100.	%4.5
35	M34	X	.001	%6.5
£36	M25	X	.04	<u>%90</u>
37	M33	X	.056	%90
38	M30	X	.012	%100
39	<u>M29</u>	X	.04	%90
40	<u> </u>	X	012	%100
41	M34	Χ	015	%100

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Member Point Loads (BLC 27 : Seismic Antenna (0 Deg))

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft.%]
1	M28	Z	005	%9.6
2	M25	Z	<u>013</u>	<u>%50</u>
3	M25	Z	007	<u>%30</u>
4	M32	Z	005	<mark>%9.6</mark>
5	M32	Z	001	%30
6	M33	<u>z</u>	-013	<u> %50</u>
7	M33	<u>Z</u>	007	%30
8	M30	Z Z	4.001	%50
9	M30	<u>Z</u>	-,001	%4.5
10	MBO	<u>Z</u>	- <u>002</u>	<u>%6.5</u>
11	M29	<u> </u>	013	%50
- 12	<u>M29</u>	<u>z</u>	<u>007</u>	%30
13	M26	Z	001	%50
14	M26	<u>Z</u>	001	%4.5
15	M26	<u> </u>	002	%6.5
16	M27	n in 🖂 Z 👘 🖓 🚽	-:001	%30.5
17	M34	Z	001	%50
18	M34	Z	001	%4.5
19	M34	Z	002	%6.5

Member Point Loads (BLC 28 : Seismic Antenna (90 Deg))

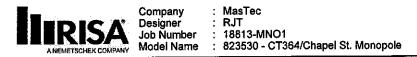
	Member Label	Direction	Magnitude[k.k-ft]	Location[ft.%]
1	M28	X	.005	%9.6
2	M25	X	<u>013</u>	<u>%50</u>
3	M25	Χ	.007	%30
4	M32	<u> </u>	.005	<u>%9.6</u>
5	M32	Χ	.001	%30
6	M33	X	.013	%50
7	M33	X	.007	%30 %50
8	M30	X * (* *		
9	M30	Χ	.001	%4.5
10	M30	<u>X x</u>	002	%6.5
11	M29	Χ	.013	%50
12	M29	X	<u>.007</u>	%30
13	M26	Х	.001	%50
14	M26	X	001	%4.5
15	M26	Х	.002	%6.5
16	M27/	<u>X - x</u>	.001	%30.5
17	M34	X	.001	<u>%50</u>
18	M34	X	.001	%4.5
19	M34	Х	.002	%6.5

Member Point Loads (BLC 41 : Seismic Vertical Antennas)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft.%]
1	M28	Y	01	%9.6
2	M25	Y	026	<u>%50</u>
3	M25	Υ	015	%30
4	M32	Y	01	%96
5	M32	Y	002	%30
6	M33	Y Y	- <u>026</u>	%50
7	M33	Y	015 003	%30
8	M30	Y	003	%50
9	M30	Y	002	%4.5
10	M30	Ye	<u>–003</u>	%6.5
11	M29	Y	026	%50
12	M29	Y	<u> </u>	%30

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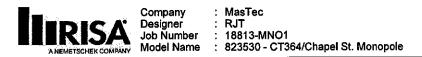


Member Point Loads (BLC 41 : Seismic Vertical Antennas) (Continued)

	Member Label	Direction	Magnitude[k.k-ft]	Location[ft.%]
13	M26	Y	003	%50
M14	M26	Y	002	%4.5
15	M26	Y	003	%6.5
16	M27	Y	- 002	%30.5
17	M34	Y	003	<u>%50</u>
18	M34	Y	- 002	%4.5
19	M34	Y	003	%6.5

Member Distributed Loads (BLC 2 : Ice Dead)

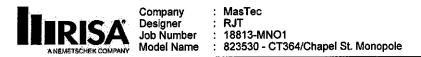
1	Member Label M1	Direction Y	Start Magnitude[k/ft 019	End Magnitude[k/ft.F 019	Start Location[ft.%] 0	End Location[ft,%] %100
2	M2	11 : - Y	019	019	0	%100
3	M3	Y	019	-,019	0	%100
4	M4	Ý	019	019	0	<u>%100</u>
5	M5	Y	019	019	0	<u>%100</u>
6	M6	Ý	019	019	0	%100
7	<u>M7</u>	Y	019	019	0	%100
8	M8N	• • • • • • • •	019	019	0	<u>%100</u>
9	<u>M9</u>	Y	016	<u>016</u>	0	<u>%100</u> %100
	<u>M10</u>	Y T	016	016	The second secon	<u>%100</u> %100
11	<u>M11</u>	Y.	016	016	0 0	%100
12	M12	<u> </u>	016	016	0	%100
13	<u>M13</u>	Y Y	<u>-,004</u> -,004	<u>004</u> 004		%100
14	M15		004	004	0	%100
15	<u>M17</u>	T V	004	004		%100
16 17	M19 M21	I V	013	013	0	%100
17	M22	l V	013	013	i n i i i i i i i i i i i i i i i i i i	%100
19	M23	Y	013	013	0	%100
20	M23	Y	Stor = 013	013		%100
21	M25	Y	01	01	0	%100
22	M26	Ý	009	-,009	0	%100
23	M27	Y	009	009	0	%100
24	M28	Y	009	-,009	0	%100
25	M29	Y	01	01	0	%100
26	M30	Y	009	009	0	%100
27	M31	<u> </u>	009	009		%100
.28	M32	Y	- 009	÷:009	0	%100
29	M33	Y	01	01	0	%100
30	<u>M34</u>	Ý	-009	009	0	%100
31	M31A	<u> </u>	004	004	0	<u>%100</u> %100
32	M32A	Ŷ	004	004	and the second sec	%100
33	M33A	Y	004	004 004	<u>0</u>	%100
34	M34A	Y -	004	004	0	%100
35	M35	Y Y	004	004	<u> </u>	%100
36	M36		004	004	0	%100
37	<u>M37</u> M38	Ý	004	004		<u>%100</u> %100
38	M38 M39	T T	004	004	0	%100
<u>39</u> 40	M39 M40	I I	004	004		%100
40	M40 M41		004	004	0	%100
41	- M42	V	004	-,004	<u> </u>	%100
42	M43	Y	004	004	0	%100
43	M44	Ý	004	004	Ŏ	%100
45	M45		004	004	Õ	%100
40		<u>ــــــــــــــــــــــــــــــــــــ</u>			······································	



Member Distributed Loads (BLC 2 : Ice Dead) (Continued)

Base Marc Y 2004 CO24 O 34100 47 M43 Y 2004 -004 0 34100 48 M43 Y 2004 -004 0 34100 50 M50 Y 2004 -004 0 34100 51 M51 Y -004 C024 0 34100 52 M52 Y 2004 C024 0 34100 54 M53 Y -004 004 0 34100 54 M55 Y -004 004 0 34100 56 M55 Y -004 004 0 34100 56 M58 Y -004 004 0 34100 58 M58 Y -004 004 0 34100 56 M58 Y -004 004 0 34100 58 M58 Y <th>Member Label</th> <th>Direction</th> <th>Start Magnitudeľk/ft</th> <th>End Magnitudeik/ft E</th> <th>Start Location[ft,%]</th> <th>End Location[ft,%]</th>	Member Label	Direction	Start Magnitudeľk/ft	End Magnitudeik/ft E	Start Location[ft,%]	End Location[ft,%]
International and the second		Y		- 004		
Has M43 Y 2004 -004 0 58100 50 M50 Y -004 -004 0 9100 51 M51 Y -004 004 0 9100 52 KM52 Y -004 004 0 9100 53 M53 Y -004 004 0 9100 54 M56 Y -004 004 0 9100 56 M56 Y -004 004 0 9100 57 M57 Y -004 -004 0 9100 58 M58 Y -004 -004 0 9100 58 M59 Y -004 -004 0 9100 59 M59 Y -004 -004 0 9100 51 M61 Y -004 -004 0 91		Y	1922 1 101		0	
Heat M49 Y 004 .004 0.004 <th0.004< th=""> <th0.004< th=""> <th0.004< th=""></th0.004<></th0.004<></th0.004<>		Ý		004	0	
SGC MMS1 Y CO4 CO4 CO4 C % M100 S2 MMS2 # NY CO04		Y				
SS MS3 Y D04 -004 0		Y	004			
53 M63 Y -004 -004 0 %100 58 M64 34 Y -004 -004 0 %100 56 M65 Y -004 -004 0 %100 56 M57 Y -004 -004 0 %100 57 M57 Y -004 -004 0 %100 %100 58 M58 Y -004 -004 0 %100 %100 59 M53 Y -004 -004 0 %100 %100 61 M61 Y -004 -004 0 %100 %100 63 M62 Y -004 -004 0 %100 %100 64 M64 Y -004 -004 0 %100 %100 65 M68 Y -004 -004 0 %100 %100 66 M68 Y <td></td> <td>Υ</td> <td></td> <td></td> <td>and the second second</td> <td></td>		Υ			and the second	
Fail MFS Y 2004 2004 2004 0 %100 F5 MFS Y -004 -004 0 %100 F7 MF7 Y -004 -004 0 %100 F7 MF7 Y -004 -004 0 %100 F8 MF8 Y -004 -004 0 %100 F7 MF7		Y .			and a second	
55 M55 Y -004 -004 0 %100 66 M68 M68 Y 004 004 0 %100 66 M68 M68 Y 004 004 0 %100 66 M68 M68 Y 004 004 0 %100 67 M70 Y 004 004 0 %100 67 M70 Y 004 004 004 0		M been approximate and a second second				
156 M56 Y .004 2004 0 %4100 57 M57 Y .004 .004 0 %6100 59 M59 Y .004 .004 0 %6100 50 M60 Y .004 .004 0 %100 61 M61 Y .004 .004 0 %100 62 M62 Y .004 .004 0 %100 63 M63 Y .004 .004 0 %100 63 M65 Y .004 .004 0 %100 64 M65 Y .004 .004 0 %100 66 M66 Y .004 .004 0 %100 67 M70 Y .004 .004 0 %100 71 M70 Y .004 .004 0 %100 72 M72 .004		Y.			A REAL PROPERTY OF A DESCRIPTION OF A DE	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		Y			where the second state of	
158 M58 Y .004 .004 0 .94100 59 M59 Y -004 -004 0 .96100 60 M60 Y -004 -004 0 .96100 61 M61 Y -004 -004 0 .96100 62 M62 Y -004 -004 0 .96100 63 M63 Y -004 -004 0 .96100 64 M64 W 004 -004 0 .96100 68 M65 Y -004 -004 0 .96100 69 M68 Y -004 -004 0 .96100 70 M70 Y -004 -004 0 .96100 73 M72 Y -004 -004 0 .96100 73 M73 Y -004 -004 0 .96100 74 M75	56 M56	<u> </u>			Service - Passing of the service	
59 MS9 Y 004 004 0 %100 60 MB0 Y 004 .004 0 %100 61 M61 Y 004 0.04 0 %100 62 M62 Y .004 0.04 0 %100 63 M63 Y .004 .004 0 %100 64 M64 Y .004 .004 0 %100 65 M65 Y .004 .004 0 %100 66 M66 Y .004 .004 0 %100 67 M67 Y .004 .004 0 %100 70 M71 Y .004 .004 0 %100 72 M72 M71 Y .004 .004 0 %100 74 M73 Y .004 .004 0 %100 74 M76		Y X				
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	101 M101	Y			0	
	102 M102		004	- <u>604</u>	0	%100

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Member Distributed Loads (BLC 2 : Ice Dead) (Continued)

	Member Label	Direction	Start Magnitude/k/ft	End Magnitude[k/ft.F	Start Location[ft,%]	End Location[ft.%]
103	M103	Y	004	004	0	<u>%100</u>
104	M104	Ý	004	004	0	%100
105	M105	Y	004	004	00	%100
106	M106	Ý	-,004	004	0	<u>%100</u>
107	M107	Y	004	004	0	%100
108	M108	N Y	004	004	0	%100
109	M109	Y	004	004	0	%100
110		Y =	004	004	0.	-%100
111	M111	Y	004	004	0	%100
112	M112	Y	-,004	004	0	%100
113	M113	Y	004	004	0	%100
114	M114	Y	-,004	4-,004	0	%100
115	M115	· Y	004	004	0	<u>%100</u>
116	M116	Y	004	-:004	0	%100
117	M117	Y	004	004	0	%100
118	M118	- Y - Y	004	004	0	%100

Member Distributed Loads (BLC 9 : Full Wind Members (0 Deg))

	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft,%]
1	M1	Z	036	036	0	%100
2	M2	- Z -	- 0 -	<u> </u>	<u> </u>	%100
3	<u>M3</u>	Z	036	036	0	%100
4	M4	1. Z	0	0	0	%100
5	<u>M5</u>	Z	018	018	0	%100
6	M6	Z	018	018	0	%100
7	M7	Z	<u>018</u>	018	0	%100
8	M8	Z	018	+.018	Q	%100
9			012	012	0	%100
10	M10	z Z	012	-012	0	%100
11	M11	<u>Z</u>	012	012	0	%100
12	<u>M12</u>	Z	-,012	012	0	%100
13	M21	Z	018	018	0	%100
14	M22	\mathbf{Z}	018	10. 11 - 018 3		%100
15	M23	Z	0	0	<u>0</u>	<u>%100</u>
16	M24	<u> </u>	0	0	The second s	%100
17	M25	Z	01	01	0	<u>%10</u>
18	M28	<u> </u>	009	009	COLUMN TRACTORY STATE	%100
19	<u>M29</u>	Z	01	01	0	%10
20	M31	Z	009	-,009	語語語の語ではない語言の「「語言」では、言語には、言語	%100
21	<u>M33</u>	<u> </u>	01	01	0	<u>%100</u>
22	M34	<u>z</u>	.009	009	SHELL MACH 1989 A COLL . PARTY AND A COMPANY AND A SHELL AND A SHE	<u>%100</u>
23	<u>M25</u>	<u> </u>	01	<u>01</u> 2009 ↓	<u>%90</u> %61	<u>%100</u> %100
24	M27		009			%100 %100
25	M29	<u> </u>	01 009	01 009 1	<u>%90</u> %60	<u>%100</u> %100
26	M32	2017 A. C.		_		<u>%100</u> %100
27	<u>M1</u>	X	0		0	%100
28	M2 1	X	A REAL PROPERTY AND A REAL	0	0	%100
29	<u>M3</u>	X	<u> </u>		u A	%100
30.	M4	N N N N N N N N N N N N N N N N N N N	0	0	0	%100
31	M5	X X			0	%100
32	M6		0	0	0	%100
33	M7	X	0 A			%100
34		and the second state of th	0	0	0	<u>%100</u>
35	M9	X	0 0	n v	- O	%100
36	M10	\sim	0	0	0	%100
37	M11	<u> </u>	U	U	U U	/0100



Member Distributed Loads (BLC 9 : Full Wind Members (0 Deg)) (Continued)

	Member Label	Direction	Start Magnitude[k/ft,	End Magnitudelk/ft.F	Start Location[ft,%]	End Location[ft,%]
38	M12	X	0 1 1	0	- I O ,	%100
39	M21	Х	0	0	0	%100
40	M22	X	0 . j. j	0	0	%100
41	M23	Х	0	0	0	%100
42	M24	X	0	0	0	%100
43	M25	Х	0	0	0	%100
-44	M26	X	0 4		0	%100
45	M27	Х	0	0	0	%100
46	M29	X	0	STA		%100
47	M30	Х	0	0	0	%100
48	M31	X	0	0	<u>O</u>	%100
49	M32	Х	0	0	0	%100
50	M33	X	- · · · · · · · · · · · · · · · · · · ·	0	0	%10
51	M28	Х	0	0	%19.2	%100
52	M33	X	0	0	%90	%100

Member Distributed Loads (BLC 10 : Full Wind Members (30 Deg))

	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft,%]	End Location[ft.%]
1	M1	Z	023	023	0	%100
2	M2	Z	008	008	0	%100
3	M3	Z	023	023	0	%100
4	M4	Z # * *	-:008			%100
5	M5	Z	029	029	0	%100
6	M6	Z	002	002	0	%100
7	M7	Z	029	029	0	%100
8	M8	Z	002	002	0	%100
9	M9	Z	019	019	0	%100
10	M10	Z	-,001	001	0	%100
11	M11	Z	001	001	0	%100
12	M12	<u>Z</u>	019	019	O>	%100
13	M21	Z	012	012	0	%100
14	M22	Z	-:012	012	<u> </u>	%100
15	M23	Z	004	004	0	%100
16	M24	<u>Z</u>	004	004	0	%100
17	M25	Z	009	009	0	<u>%10</u>
18	M28	Z 3	- .00 7	007	0	%100
19	M29	Z	-,009	009	0	%10
20	M31	Z	007	007	0	%100
21	M33	Z	009	009	0	%100
22	M34	Z	007	007	0	%100
23	M25	Z	009	009	%90	%100
24	M27	Z	007	007	%61	%100
25	M29	Z	009	009	%90	%100
26	M32	Z	007	007	%60	%100
27	M1	X	.013	.013	0	%100
28	M2	<u> </u>	.004	.004	0	%100
29	M3	X	.013	.013	0	%100
30	M4	X	.004	.004	0	%100
31	M5	X	.017	.017	0	%100
32	M6	X	.001	.001	0	<u>%100</u>
33	M7	X	.017	.017	0	%100
34	M8	Х	.001	.001	0	%100
35	M9	X	.011	.011	0	%100
36	M10 🛶 🚽	X	.001	.001	0	%100
37	M11	Х	.001	.001	0	%100
38	M12	X	.011	.011	0	%100

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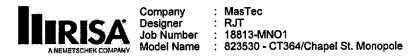
Member Distributed Loads (BLC 10 : Full Wind Members (30 Deg)) (Continued)

	Member Label	Direction	Start Magnitude/k/ft	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft.%]
39	M21	Х	.007	.007	0	%100
40	M22	X 5	.007	.007	0	%100
41	M23	Х	.002	.002	0	%100
42	1M24	X	.002	.002	0	%100
43	M25	X	.005	.005	0	%100
44	M26	X	.004	.004	<u>. 0 - 1</u>	<u> </u>
45	M27	X	.004	.004	0	%100
46	M29	X	.005	.005	0	%100
47	M30	X	.004	.004	0	%100
48	M31	X	004	.004	1 0 1 1	%100
49	M32	X	.004	.004	0	%100
50	M33	X	.005	.005	0	%10
51	M28	X	.004	.004	%19.2	%100
52	M33	X	.005	.005	%90	%100

Member Distributed Loads (BLC 11 : Full Wind Members (60 Deg))

	Member Label	Direction	Start Magnitudelk/ft	End Magnitude[k/ft,F	Start Location[ft,%]	End Location[ft.%]
1	M1	Z	004	004	0	%100
2	M2	• Z • •	-,013	013	0	%100
3	M3	Z	004	004	0	%100
4	M4	≤ Z ≤ Z	013	013	0	%100
5	M5	Z	017	017	0	%100
6	M6	Z	001	001	<u> </u>	%100
7	M7	<u>Z</u>	017	017	0	%100
8	<u>M8</u>	Z	-:001	001	<u> </u>	%100
9	M9	<u>Z</u>	011	011	0	%100
	M10	<u>z z z</u>	001	-:001	. 0	%100
11	M11	<u>Z</u>	001	001		%100
12	M12	<u>Z</u>	011	011	0	%100
13	<u>M21</u>	Z	002	002	0	%100
14	M22	R Z	-:002	002	0	%100
15	M23	<u> </u>	007	007	<u> </u>	%100
16	M24	Z	-,007	007	0	%100
17	M25	<u> </u>	005	005	0	%10
18	M28	Z	004	004	Q	%100
19	M29	Z	005	005	0	%10
20	M31	<u>z</u>	004	004	U state in the	%100
21	M33	Z	005	005	O Contraction (Contraction)	%100
22	<u>M34</u>	Z Z	-,004	004	The state in the second state of the second st	%100
23	M25	Z 7	005	005 004	<u>%90</u>	<u>%100</u> %100
24	<u>M27</u>	Carlo of Arriver and Street and Street and Street Street	004		<u>%61</u>	
25	M29	Z	005	005 004	<u>%90</u> ∞1== %60 ===	<u>%100</u> %100
26	M32		004		-	%100
27	<u>M1</u>	X X	.008	.008		%100
28	M2	A STREET CORP. CORP. CORP. STREET STOPPEN		.023	0	%100
29 30	M3		.008	.023		%100
30	M4 M5	X	.023	.029	0	%100
31	Mo	X	.029	.002		%100
	M7	X	.029	.029	0	%100 %100
<u>33</u> 34	M8	\sim	.023	.023		%100
	MO M9	X	.019	.019	0	%100
35 36	MI9 M10	x x	013	.013		%100
37	M10	X	.001	.001	0	%100
37	M11	Ŷ	.019	.019	i i n	%100
39	M21	X	.004	.004	0	%100
39		<u> </u>	.004		· · · · · · · · · · · · · · · · · · ·	70100

RISA-3D Version 17.0.2 [C:\...\...\...\823530 - Updated.R3D]

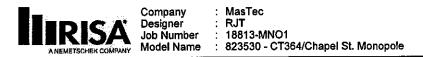


	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft,%]	End Location[ft,%]
40	M22	X	.004	.004	0	%100
41	M23	Х	.012	.012	0	%100
42	M24	X	.012	.012	0	%100
43	M25	X	.009	.009	0	%100
44	M26	× .	.007	,007	0	%100
45	M27	Х	.007	.007	0	%100
46	- M29	X	.009	.009	• • • • • • • • • • • • • • • • • • •	<u>%100</u>
47	M30	X	.007	.007	0	%100
48	M31	X	.007	.007	- 0	%100
49	M32	Х	.007	.007	0	%100
50	M33	X	.009	.009	0	%10
51	M28	Х	.007	.007	%19.2	%100
52	M33	X	.009	.009	<u>%90</u>	%100

Member Distributed Loads (BLC 12 : Full Wind Members (90 Deg))

Member Label	Direction		End Magnitude[k/ft,F		End Location[ft.%]
1 M1 2 M2		0	0		%100 %100
	A . (0	0	0	%100
3 <u>M3</u>	Z	0 0	O LAN	A S O S S O	%100
5 M5	Z	Ō	0	0	%100
6 3 M6 85	-	Ň	0		%100
7 M7	Z		0	0	%100
8 M8	Z I	Ŏ.	0	0/10/1	%100
9 <u>M</u> 9	Z	0	0	0	%100
10 M10	Z	• 0	0	0	%100
11 M11	Z	0	0	0	%100
12 M12	<u>Z</u>	- // _ / · / O	0	0	%100
13 M21	<u>z</u>			0	%100
14 M22	Z	<u> </u>	0	0	%100
15 M23	<u> </u>	0		0	%100
16 M24	Z	0	0	<u> </u>	%100
17 M25	Z	0	0	0	%10
18 M28	Z	0	<u>0</u>	0.000	%100
<u>19 M29</u>		0	0	0	%10
20 M31	<u>z</u>	<u> </u>	0	<u> </u>	%100
21 M33	Z	0			%100 %100
22 M34		0	0	%90	%100 %100
23 M25 24 M27	Z	0		<u>%90</u> %61	%100
24 <u>M27</u> 25 M29	Z	0	0	%90	%100
25 M29	Z	U D	C Total	%60 %60	%100
27 M1	X	0	0	0	%100
28 W2			.036	น เป็น ก็เป็น เป็น	%100
29 M3	X	0	0	0	%100
30 M4	X S		036	Č Č	%100
31 M5	X	.018	.018	0	%100
32 M6	X	.018	.018	0	%100
33 M7	X	.018	.018	0	%100
34 M8	X	.018		0	%100
35 M9	X	.012	.012	0	%100
36 M10	X	.012	012	0	%100
37 M11	X	.012	.012	0	%100
<u>38</u> M12	<u> </u>	.012	.012	0	%100
39 M21	<u> </u>	0			<u>%100</u>
40 M22	X	0	0	<u> </u>	%100

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	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft,F	Start Location[ft,%]	End Location[ft.%]
41	M23	X	.018	.018	0	<u>%100</u>
42	M24	X	.018	.018	0	%100
43	M25	X	.01	.01	0	<u>%100</u>
44	M26	X Lines	.009	.009	0	%100
45	M27	Х	.009	.009	0	<u>%100</u>
46	M29	×	.01	.01	0	%100
47	M30	X	.009	.009	0	%100
48	M31	** X **	.009	.009	0 +	%100
49	M32	X	.009	.009	0	%100
50	M33	X		.01	0	%10
51	M28	X	.009	.009	<u>%19.2</u>	%100
52	M33	X	.01	.01	<u>%90</u>	%100

Member Distributed Loads (BLC 13 : Full Wind Members (120 Deg))

Member Label	Direction	Start Magnitude[k/ft,	End Magnitude[k/ft,F	Start Location[ft.%]	End Location[ft.%]
1 M1	Ζ	.004	.004	0	%100
2 M2	Z	.013	.013	0	%100
3 M3	Z	.004	.004	0	<u>%100</u>
4 - M4 - L	Z	.013	.013	0	
5 M5	Z	.001	.001	0	%100
16 M6	Z	.017	.017	0	%100
7 <u>M7</u>	Z	.001	.001	0	%100
8 M8	Z	.017	.017	0	%100
9 M9	Z	.001	.001	0	<u>%100</u>
10 M10	Z	.011	.011	0	%100
11 M11	Z	.011	.011	0	<u>%100</u>
12 M12	Z	.001	:001	<u> </u>	%100
13 M21	Z	.002	,002	0	%100
	¥ ≥ Z esta	.002 👾 🗄	,002	0	%100
15 M23	<u> </u>	.007	.007		%100
16 M24	Z Z	.007	.007	0	%100
17 M25	<u>Z</u>	.005	.005	0	<u>%10</u>
18 M28	Z	.004	.004	0	%100=
19 M29	Z	.005	.005	0	%10
20 M31	Z	.004	.004	0	%100
21 M33	<u> </u>	.005	.005	0	<u>%100</u>
22 M34	z -	.004	.004	0	%100
23 M25	Z	.005	.005	%90	%100
24 M27	- Z	.004	.004	<u> </u>	%100
25 M29	Z	.005	.005	%90	%100
.26 M32	Z	.004	.004	<u>%60</u>	%100
27 M1	X	.008	.008	0	%100
28 M2	X	.023	.023	0	%100 11 18
29 M3	<u> </u>	.008	.008		<u>%100</u>
30 M4	× X	.023	.023	0	%100
31 M5	<u> </u>	.002	.002		%100
32 M6	×. •	.029	.029	0	%100
33 M7	<u> </u>	.002	.002		%100
34 M8	X	.029	.029	0	%100
35 M9	<u> </u>	.001	.001	0	%100
36 M10	X	.019	.019	0	%100
37 M11	<u> </u>	.019	.019	0	%100
38 M12	X	.001	.001	0	%100
39 M21	X	.004	.004		%100
40 M22	X	.004	.004	0	%100
41 M23	X	.012	.012	0	%100

	Member Label	Direction	Start Magnitude[k/ft,	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft,%]
42	M24	X	.012	.012	0	%100
43	M25	X	.009	.009	0	%100
44 -	M26		.007	.007		%100
45	M27	X	.007	.007	0	%100
46	M29	X ·	.009	.009	0	%100
47	M30	X	.007	.007	0	%100
48	M31	X	.007	.007	0	%100
49	M32	X	.007	.007	0	%100
50	M33	<u> </u>	.009	.009	. 0	%10
51	M28	X	.007	.007	%19.2	%100
52	M33	X	,009	.009	%90	%100

Member Distributed Loads (BLC 14 : Full Wind Members (150 Deg))

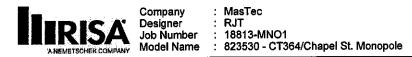
Member Label	Direction Z	.023	End Magnitude[k/ft.F .023	Start Location[ft,%] 0	End Location[ft.%] %100
2 M2	Z	.008	.008	1 / / 0 / II /	%100
<u>3 M3</u>	<u>Z</u>	.023	.023	0	%100
4 M4	<u>Z</u>	600;	.008	0	%100
5 <u>M5</u>	<u>Z</u>	.002	.002	0	<u>%100</u>
6 . M6	Z (.029	.029		%100
7 <u>M7</u>		.002	.002		%100
<u>8</u>	<u> </u>	029	.029	0	%100
9 <u>M</u> 9	Z	.001	.001	<u>0</u>	%100
10 M10	Z	.019	.019	0	%100
11 M11	Z	.019	.019	0	%100
12 M12	free contraction of the second se	.001	.001	0	%100
13 M21 14 M22	Z 7	.012 012	.012	0 ™051₽>	<u>%100</u>
14 M22 15 M23	a determined in this and the set had the set	.012	.012	0	%100 %100
16 M24	Z 7	.004	.004	o o	%100
17 M25	Z	.004	.004	0	%10
18 M28	7	.003	.003	i i i i i i i i i i i i i i i i i i i	%100
19 M29	Z	.009	.009	0	%10
20 M31	7	.007	.007	i i i i i i i i i i i i i i i i i i i	%100
21 M33	Z	.009	.009	0	%100
22 M34	Z Z	.007	.007	Ŏ	%100
23 M25	Z	.009	.009	%90	%100
24 M27	Z . (1)	.007	.007	%61	%100
25 M29	Z	.009	.009	%90	%100
26 M32	Z	.007	.007	%60	%100
27 M1	X	.013	.013	0	%100
28 M2	X	.004	.004	k - D O O O O	%100
29 M3	X	.013	.013	0	%100
<u>30</u> . M4	X	.004	.004	0	%100
31 M5	X	.001	.001	0	%100
.32 M6	X	.017	.017	0	%100
33 M7		.001	.001	0	<u>%100</u>
34 M8	X	.017	<u>.</u> 7 .017	0	%100
35 M9	X	.001	.001	0	<u>%100</u>
<u>36</u> M10	X	.011	.011	17. 0 5. 3	%100
37 M11	X	.011	.011	0	%100
38 M12	X	.001	.001	0	%100
<u>39 M21</u>		.007	.007	0	%100
40 M22	X	.007	.007	<u> </u>	%100
41 M23	X	.002	.002	0	%100
42 M24	X	.002	.002	0	%100

<u>Member Distributed Loads (BLC 14 : Full Wind Members (150 Deg)) (Continued)</u>

	Member Label	Direction	Start Magnitude[k/ft,	End Magnitude(k/ft.F	Start Location[ft,%]	End Location[ft.%]
43	M25	X	.005	.005	0	%100
44	M26	X	.004	.004	0	%100
45	M27	X	.004	.004	0	<u>%100</u>
46	M29	•X	.005	.005	0	<u>%100</u>
47	M30	X	.004	.004	0	%100
48	M31	X	.004	.004	0	%100
49	M32	X	.004	.004	0	%100
50	M33	X	.005		0	%10
51	M28	X	.004	.004	%19.2	%100
52	M33	X	:005	.005	%90	%100

Member Distributed Loads (BLC 21 : Ice Wind Members (0 Deg))

	Member Label	Direction	Start Magnitude[k/ft,	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft,%]
1	<u>M1</u>	<u>Z</u>	009	009	0	%100
2	M2	Z	0	0	0	%100
3	<u>M3</u>	Z	009	009	0	%100
4	M4	Z	0	0 166	0	%100
5	M5	<u>Z</u>	004	004	0	%100
and the second s	M6	<u> </u>	004	004	0	%100
7	M7		004	004	O CONTRACTOR CONTRACTOR OF CON	%100
8	<u>M8</u>	<u>Z</u>	004	-:004	0	%100
9	M9	Z	-,003	003	0	%100
10	<u>M10</u>	- Zi	003	003		%100
11	<u>M11</u>	<u>Z</u>	003	<u>003</u>	0	%100
Trixs 1. 0005-	M12	<u>Z</u> .	003	003	i i≤n . O	%100
13	M13	<u>Z</u>	007	007	0	%100
14	M15	Ż	007	007	<u> </u>	%100
15	M1 <u>7</u>		007	007		
<u> 16 </u>	<u>M19</u>	<u>Z</u>	007	007	0	%100
17	<u>M21</u>		005	005	0	%100
18	M22	<u>Z</u>	005	005	<u> </u>	%100
19	<u>M23</u>	<u>Z</u>	0	0	0	%100
20	M24	<u>Z</u>	0	0		%100
21	<u>M25</u>	Z	-,004	004	0	%10
22	<u>M28</u>	<u>Z</u>	004	004	1 1 0	%100
23	M29		004	004	0	%10
24	M31	Z see	004	-004		%100
25	M33	Z	004	004	0	%100
26	<u>M34</u>	2	004	004	0	%100
27	<u>M31A</u>	<u>Z</u>	005	005	0	%100
28	M32A	Z	005	- 005	NUMBER OF STREET, STREE	%100
29	M33A	<u>Z</u>	005	005	0	<u>%100</u>
30	<u>M34A</u>	Z	005	005	COMPANY OF CARDING AN A PERSON AND A PERSON AND A	%100
31	<u>M35</u>		007	007	0	<u>%100</u>
32	M36	<u>t * Z</u>	007	007	0	%100
33	<u>M37</u>	<u>Z</u>	007	007 007	0	<u>%100</u> %100
34	<u>M38</u>		007			
35	<u>M39</u>	Z	007	007 007	0	<u>%100</u> %100
36	M40		007		AND THE REAL PROPERTY AND A DESCRIPTION OF THE PARTY OF T	%100 %100
37	<u>M41</u>	Z –	007	<u>007</u> 007	<u>0</u>	%100
38	M42	200 - The second s		007		%100
39	M43	Z 7	007 007	007	<u>0</u>	%100
40	<u>M44</u>	Cold and the second second			A CARL CONTRACT OF A CARL CONTRACT OF A CARL	
41	M45	<u>Z</u>	007 007	007 007	0 0	%100 *** %100
42	<u>M46</u>					%100 %100
43	M47	<u>Z</u>	007	007	0	<u>%100</u>



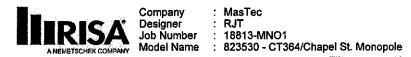
	Direction	Start Magnitudolk/#	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft.%]
Member Label 44. M48	Direction 7	007	=.007		%100
45 M49	7	007	007	0	%100
46 M50	Ž	007	007	O CONTRACTOR	%100
47 M51	Z	007	007	0	%100
48 M52	Z s	007	-,007	0	%100
49 M53	Z	007	007	0	%100
50 M54	Z Z	007			%100
51 M55	<u>Z</u>	007	007	0	%100
52 M56	<u>Z</u>	007	007	0	%100
53 M57	<u>Z</u>	007	007	0	%100
54 M58	Z	007	007		%100
55 M59	Z	007	007	0	<u>%100</u>
<u>56</u> M60	<u> 848 x Z</u>	007	007		%100
57 <u>M61</u>	<u> </u>	007	007		%100 %100
<u>58 M62</u>	<u>Z</u> 2.	007	007	0	%100 %100
<u>59 M63</u>		007 007	007		%100
60 M64	Z Z	007	007	0	%100
61 M65 62 M66	$\frac{z}{z}$	007	007	n in the second s	%100
63 M67	Z	007	007	0	%100
64 M68	ź.	II007	007	A DEL A DEL CAR	%100
65 M69	Z	007	007	0	%100
66 1. p. M70	2 Z	007	007	0	%100
67 M71	Z	007	007	0	%100
68 M72	Z	007	- 007	0	%100
69 M73	Z	007	007	0	%100
70 M74	Z	007	007	0	%100
71 M75	Ζ	007	007	0	<u>%100</u>
72 M76	Z	-:007	007	0	%100
73 M77	<u> </u>	007	007	0	%100
74 M78	<u> </u>	<u>-,007</u>	- 007	0	%100
75 M79	Z	007	007		<u>%100</u> %100
76 M80		007	007	CAMPAGE STREET, INC. PROC. PLANTING COMPANY	<u>%100</u> %100
77 <u>M81</u>	<u> Z</u>	007	-,007 - 007	0	%100
78 M82	<u> </u>	007	003	0	%100
79 <u>M83</u>	2 1 10 10 2	003	003	0	%100
80 M84 81 M85	7	0	0	0	%100
82 M86		<u> </u>	0.1.1	n n n n n n n n n n n n n n n n n n n	%100
83 M87	7	003	003	0	%100
84 M88	7 1-9	003	-003	je do	%100
85 M89	Z	0	0	0	%100
86 M90			0 1	0	%100
87 M91	Z	005	005	0	%100
88 M92	, Z	005	005	- - 0	%100
89 M93	Z	005	005	0	%100
90 M94	Z	005	005		%100
91 M95	<u> </u>	005	005	0	%100
92 M96	<u> </u>	-,005	005	0	%100
93 M97	<u> </u>	005	005	0	%100
<u>94 M98</u>	Z	-:005	005	<u>o</u>	%100 %400
<u>95 M99</u>	Z	005	005	0	<u>%100</u>
<u>96 M100</u>	Z	005	005	0	<u>%100</u>
<u>97 M101</u>	<u>Z</u>	005	005	0	<u>%100</u> %100
<u>98 M102</u>	Z	005	005		<u>%100</u> %100
99 M103		004 002	004	0	
100 M104	Z				

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Member Label	Direction	Start Magnitude[k/ft,	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft.%]
101 M105	Z	002	002	0	%100
102 M106	Z	004	004	0.000	<u>%100</u> %100
103 M107 104 M108	<u> </u>	004 002	004	0	%100
105 M109	Z	002	002	0	%100
106 M110	z Z	004	004	0	%100
107 M111	Z	-,004	004	0	%100
108 M112	<u> </u>	+.002	002	0	%100
109 M113	Z	<u>002</u> 004	002 004	0	%100 %100
110 M114	Z	004	004		%100
112 M116	Z	004	-002	The O real of	%100
113 M117	Z	002	002	0	%100
114 M118	<u> </u>	004	-:004	0	%100
115 M25	<u> </u>	004	004	%90	%100
116 M27	Z	-:004	004	<u>%61</u> %90	<u>%100</u> %100
117 M29 118 M32	Z	004 004	004	%60	%100
119 M1	X	0	0	0	%100
120 M2	X	0	0	0	%100
121 <u>M3</u>	X	0	0	0	%100
122 M4	×	0	0	<u> </u>	%100 %100
123 M5 124 M6	X	<u>0</u>	n v	0	%100
124 MO	X	0	0	0	%100
126 M8	X	0 x 建序基	0	0	%100
127 M9	X	0	O.	0	%100
128 M10	<u>X - </u>	0	Ö	<u> </u>	%100
129 M11 130 M12	X X	O SVIP O STAT	<u>0</u>	0	<u>%100</u> %100
131 M13	X	0	0	0	%100
132 M15	λ ή χ	i o i i i i i	Ŭ Ö		<u> </u>
133 M17	X	0	0	0	%100
134 M19	X X	0		0	%100
135 <u>M21</u>	X	0 0 1 1 1 1 1	0	0	<u>%100</u> %100
136 M22 137 M23	X	0	0	0	%100
138 M24	x x	<u>ŏ</u>	Ŏ	s o o	%100
139 M25	X	0	0	0	%100
140 M26	X	0	0	0	%100
141 <u>M27</u>	X	0		0	%100
142 M29 143 M30	X	0	0	0	%100 %100
144 M31	x *				%100
145 M32	X	Õ	Ō	0	%100
146 M33	X	0	<u>su o i i i i i i i i i i i i i i i i i i </u>	- 0	%10
147 M31A	X	0	0	0	<u>%100</u>
148 M32A	× X	0	0	<u>o</u>	<u>%100</u>
149 M33A 150 M34A	X	0	0		%100 %100
151 M35	X	0	0	0	%100
152 M36	Â	i de la companya de l	Ō	Ŏ	%100
153 M37	X	0	0	0	%100
154 M38	X	0			And the second
155 M39	X	0			<u>%100</u> %100
156 M40	X	0	0	0	%100 %100
		V	<u> </u>	<u> </u>	/0100

RISA-3D Version 17.0.2 [C:\...\...\...

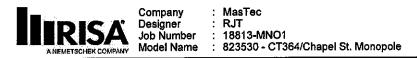


June 7, 2019 7:54 PM Checked By:____

Member Distributed Loads (BLC 21 : Ice Wind Members (0 Deg)) (Continued)

Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F.	Start Location[ft,%]	End Location[ft,%]
158 M42		0	0	0	%100 %100
159 M43 160 M44	X Anna Anna Anna Anna Anna Anna Anna Anna	0	0	0	%100 %100
161 M45	X	0	0	0	%100
162 M46	Â.	Ö .	S O State		%100
163 M47	X	Ō	0	0	%100
164 M48	- X -	<u>et 0</u> +	0	0	%100
165 M49	X X		0	0 0 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	%100 %100
166 M50 167 M51	X	0	0	0	%100
168 M52	x x	n in the second	Ő	Ő	%100
169 M53	X	Ō	0	0	%100
170 M54	X	0		0	%100
171 <u>M55</u>	X	0	0	0	%100
172 M56	X	<u> </u>		<u> </u>	%100 %100
173 M57 174 M58		0	O O		%100
175 M59	X	0	0	0	%100
176 M60	X X	0	0	Û X	%100
177 M61	X	0	0	0	%100
178 M62	X	0	<u>o</u>	<u>o</u>	%100
179 M63 180 M64	X	0	0	0	<u>%100</u> %100
181 M65	X	0	0	0	%100
182 M66	x x		Ŏ	j j j	%100
183 M67	X	0	0	0	%100
184 M68	X	0	0	0	%100
185 <u>M69</u>	X			0	%100 %100
186 M70 187 M71	X	0	0	0	%100 %100
188 M72	X	0	Č, N. Č	n j	%100
189 M73	X	0	Ō	Ó	%100
190 M74	X	0	0 .	0 -	%100
191 M75	X	0		0	<u>%100</u> %100
192 M76 193 M77	X	<u>0 1 1 5</u> 0	0	0	<u>%100</u> %100
194 M78	x x	0	, i i i i i i i i i i i i i i i i i i i		%100
195 M79	X	0	0	0	%100
196 M80	X		0	0	1%100
197 M81	X	0	0	0	%100
198 M82	X	0	0	<u>0</u>	<u>%100</u> %100
199 <u>M83</u> 200 M84	X	v			<u>%100</u> %100
201 M85	Х	0	0	0	%100
202 M86	X	0	0	0	%100
203 M87	X	0	0	0	%100
204 M88		And the second	-	0	%100
205 M89 206 M90	X	0 0	O VIII O VIII O	0 1439: 7 0 5 4-14	<u>%100</u> %100
206 W90	X	<u> </u>	0	0	%100
208 M92	X X	Ŏ		ILI ÖLL S	%100
209 M93	X	0	0	0	%100
210 M94	X	0	0	<u> </u>	%100
211 M95	X	0 	0	0	<u>%100</u> %100
212 M96 213 M97	X	<u> </u>	0	0	<u>%100</u> %100
213 M97	x x		0	ŏ	%100 %100
		2017/2017 1999 1997 1997 1997 1997 1997 1997 1			

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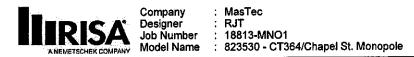
	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft,%]
215	M99	Х	0	0	0	%100
216	M100	X	0	0	0	%100
217	M101	X	0	0	0	<u>%100</u>
218	M102	X	Brak O Breek	0 1 2	0	%100
219	M103	X	0	0	0	%100
220	M104	X	0	0	<u> </u>	%100
221	M105	X	0		0	%100
222	M106	X	.0		с е 0 ексерств	%100
223	M107	<u> </u>	0	0	0	%100
224	M108	<u>x</u>	••••0	5 A 25 S	0	%100
225	M109	<u> </u>	0	0	0	%100
226	M110	<u> </u>	0	<u> 1995 - 1995</u> - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997	0	%100
227	M111	<u> </u>	0		0	%100
228	M112	<u> </u>	0	0	0	%100
229	M113	<u>X</u>	0			<u>%100</u>
230	M114	<u>X</u>	-0	0	0	%100
231	M115	<u> </u>	0			%100
232	<u>M116</u>	<u>X</u>	0	O (1 1 1 1	0	%100
233	M117	<u> </u>	0	0	0	%100
234	M118	8 X	0		0	%100
235	M28	<u> </u>	0	0	<u>%19.2</u>	<u>%100</u>
236	<u>M33 </u>	X (1)	0 🖉	0	%90	%100

Member Distributed Loads (BLC 22 : Ice Wind Members (30 Deg))

	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft.%]
1	M1	<u> </u>	006	006	0	<u>%100</u>
2	M2	Ζ	001	001	0 -	%100
3	M3	Z	-,006	006	0	%100
14	M4	Z	-:001	001	0	%100
5	M5	Z	006	006	0	%100
6	M6	Z Z	001	001		%100
7	M7	Z	006	0 <u>06</u>	0	<u>%100</u>
8	M8	<u>Z</u>	001	001	0 1	%100
9	M9	Z	004	004	0	<u>%100</u>
10	M10	Ζ.	001	001	e <u>o</u>	%100
11	M11	Z	001	001	0	<u>%100</u>
12	M12	Ζ.	004	-:004	0	%100
13	M13	Z	006	006	0	%100
14	M15	Z	006	006	0	%100
15	M17	<u>Z</u>	006	006	0	%100
16	M19	Z	006	006	0	%100
17	M21	<u>Z</u>	004	004	0	%100
18	M22	<u>Z</u>	-,004	004	0	%100
19	M23	<u>Z</u>	001	001	0	<u>%100</u>
20	M24	Z	-:001	001	0	%100
21	M25	<u>Z</u>	004	004	0	%10
22	M28	Z	004	004	- 0	%100
23	M29	<u> </u>	004	004	0	%10
24	M31	Z	004	-,004	0	%100
25	M33	<u>Z</u>	004	004	0	%100
26	M34	Z –	<u>-:004</u>	004 iii -	0	%100
27	M31A	<u>Z</u>	004	004	0 · · · · · · · · · · · · · · · · · · ·	%100
28	M32A	Z	-:004	-,004	0	%100
29	M33A	Z	004	004	0	%100
30	M34A	Z	-,004	+.004		%100
31	M35	<u>Z</u>	006	006	0	%100

Member Label	Disastian	Clark Magnikudall <i>ii</i> #	End Magnitude[k/ft.F Start	Location[ft,%] End Location[ft,%]
Member Label 32 M36	Direction 7	-:006	006	0 %100
33 M37	Z	006	006	0 %100
34 M38	ź	-,006		0 %100
35 M39	7	006	006	0 %100
36 M40	Ī	-,006		0 %100
37 M41	Z	006	006	0 %100
38 M42	2 Z			0 %100
39 M43	Z	006	006	0 %100
40 M44	* <u>Z</u>	-,006	006	0 %100
41 M45	Z	006	006	0 %100
42 M46	Z	006	006	0 %100
43 M47	Z	006	006	0 %100
44 M48	<u></u>	-006	006	0 %100
45 M49	7	006	006 006	0 %100 0 %100
46 M50 47 M51	Ζ.	006	006	0 %100
47 M51 48 M52	Z	008	-006	0 3 3%100
49 M53	7	006	006	0 %100
50 M54	7	006	006	0 1%100
51 M55	Z	006	006	0 %100
52 M56	Ż	- 006	-006	0 %100
53 M57	Z	006	006	0 %100
*54 M58	Z	006	- 006	0 %100
55 M59	Z	006	006	0 %100
56 M60	Z	006	006	0 %100
57 M61	<u>Z</u>	006	006	0 %100
58 M62		006	006	0 %100
59 <u>M63</u>	Z	006	006	0 %100 0 %100
60 M64 61 M65	4	<u>006</u> 006	006 006	0 %100 0 %100
61 M65 62 M66	Z	008	006	<u>%100</u>
63 M67	7	006	006	0 %100
64 M68	7		006	<u>%100</u>
65 M69	Z	006	006	0 %100
66 M70	Ż	006	006	0 %100
67 M71	Z	006	006	0 %100
68 M72	Z	-,006	006	0 %100
69 M73	<u>Z</u>	006	006	0 %100
70 M74	<u>. Z</u>	006	006	0 %100
71 M75	Z	006	006	0 %100
72 M76	Z.	006	006	0 %100
73 M77	Z	006	006	0 %100 0 %100
74 M78		006 006	006	0 %100
75 M79 76 M80	Z	008	006	0 %100
77 M81	Z	006	006	0 %100
78 M82		-,006	006	0 %100
79 M83	Z	003	003	0 %100
80 M84		003	-,003	0 %100
81 M85		0	0	0 %100
82 M86	Z Z	0	0	0 2 %100
83 M87	Z	003	·003	0 %100
84 M88	Z 3	003	-,003	
85 M89	Z	0	0	0 %100
86 M90		<u>0</u>	0	Annual Content of the second s
87 M91	<u> </u>	004	004	0 %100
88 M92	Z 2	004	-:004	0 %100

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	Member Label	Direction	Start Magnitude[k/ft	End Magnitude/k/ft.F	Start Location[ft,%]	End Location[ft,%]
89	M93	Z	004	0 <u>04</u>	0	%100
90	M94	1 Z 2 3	004	004	0	%100
91	M95	Z	004	-,004	0	%100
92	M96	Z	004	004	0	%100
93	<u>M97</u>	<u>Z</u>	004	004	0	%100
94	<u>M98</u>	<u> </u>	004	004	<u> </u>	%100
95	<u>M99</u>	Z	004	004	0	<u>%100</u>
96	<u>M100</u>	<u> </u>	004	004		<u>%100</u> %100
97	<u>M101</u>	Z 7	<u>004</u> -:004	004 004	0 2013 年 1	%100
<u>98</u>	M102	7	004	003	0	%100
<u>99</u> 100	<u>M103</u> M104	<u> </u>	003	003	<u>0</u>	%100
101	M104	Z	002	002	0	%100
102	M105	7	003	003	n i nee i	%100
102	M107	Z	003	003	0	%100
104	M108	7	= 002	002	0	%100
105	M109	Z	- 002	002	0	%100
106		Z Z	003	003	0	%100
107	M111	Z	003	003	0	%100
108	M112	Z	002	002		.%100
109	M113	Z	002	002	0	%100
110	M114	Z	003	003	- 0	%100
111	M115	Z	003	003		%100
112	M116	Z	002	+.002	0	%100
113	M117 '		002	002		%100
114	<u>M118</u>	<u>Z</u>	003	003		<u>%100</u> %100
115	M25	<u> </u>	004	004	<u>%90</u>	%100
116	M27	<u>Z</u>	004	- 004	<u>%61</u> %90	%100 %10 <u>0</u>
117	M29 M32	2	004 004	<u>004</u>	<u>%90</u> %60	%100
118 119	Moz M1	X	.003	.003	0	%100
120	M1 M2	- Â	.003	.001	Č Č	%100
121	<u>M3</u>	X	.003	.003	0	%100
122	M4	X X			0	%100
123	M5	X	.004	.004	0	%100
124	M6	X	.001	.001	0	%100
125	M7	X	.004	.004	0	<u>%100</u>
126	M8	X	.001	.001	<u>.</u>	%100
127	M9	X	.003	.003	0	%100
128	<u>M10</u>	<u> </u>		.001	0	%100
129	<u>M11</u>		.001	.001	0	%100
130	<u>M12</u>	<u> </u>	.003	.003	0	%100
131	<u>M13</u>	X.	.004	.004	0 0	%100 %100
132	M15	K - X	.004	.004	tentile off aft a runn anti-the state at a state at a	
133	<u>M17</u>	<u> </u>	.004	.004	0	<u>%100</u> %100
	<u>M19</u>	<u>x</u>	.004	.004	0	%100
135	<u>M21</u>	X X	.002			%100
136		X	002	0	0	%100
137	M23 M24	x i		<u> </u>		%100
139	M24 M25	X	.002	.002	0	%100
140	M25	Â	.002	.002	- Ö	%100
141	M20	X	.002	.002	0	%100
	M29		.002	.002	0	%100
143	M <u>30</u>	X	.002	.002	0	%100
	M31		.002		Ō	%100
145	M32	X	.002	.002	0	%100
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Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F.	Start Location[ft.%]	End Location[ft.%]
146 M33	X	.002	.002		%10
147 <u>M31A</u>	X	.002	.002	0	<u>%100</u> %100
148 <u>M32A</u>	X	.002 .002	.002	0	%100
149 <u>M33A</u> 150 <u>M34A</u>	X	.002	.002		%100
151 M35		.004	.004	0	%100
152 M36	$\hat{\mathbf{x}}$.004		· · · · · · · · · · · · · · · · · · ·	%100
153 M37	X	.004	.004	0	%100
154 M38	<u> </u>	.004	.004	0	%100
155 M39		.004	.004	0	%100
156 M40 **	X	.004	.004	<u>0</u>	<u>%100</u> %100
157 M41 158 M42		.004	<u>.004</u>	0	%100
158 M42 159 M43	X	.004	.004	0	%100
160 M44	$\hat{\mathbf{x}}$.004	004		%100
161 M45	X	.004	.004	0	%100
162 M46	× X	.004	.004	· • 0· • • •	%100
163 M47	X	.004	.004	0	%100
164 M48	X	.004	.004	<u>0</u>	%100
165 M49	X	.004	.004	0	<u>%100</u> %100
166 M50	X	.004	.004	<u> </u>	%100
167 M51 168 M52		.004	.004		%100
168 M52 169 M53	X	.004	.004	0	%100
170 M54	Â.	.004	004	o o est	%100
171 M55	X	.004	.004	0	%100
172 M56	X	.004	.004	0	%100
173 M57	<u> </u>	.004	.004	0	%100
174 M58	X	.004	.004	<u>O O</u>	%100
175 M59		.004	.004		<u>%100</u> %100
176 M60		.004	.004	0	%100
177 M61 178 M62	$\mathbf{\hat{\mathbf{v}}}$.004	.004		%100
179 M63	X	.004	.004	Õ	%100
180 M64	X	,004	004	11 0 0 1	%100
181 M65	X	.004	.004	0	%100
182 M66	X	.004	.004	1 1 0 2 3 4	%100
183 <u>M67</u>	<u> X</u>	· .004	.004	Q	%100
184 M68	X	.004	.004	0	<u>%100</u> %100
185 M69 186 M70	X	<u>.004</u> .004	.004	0 ⊐99317152_0 = 32,5545	%100
187 M70	X	.004	.004	0	%100
188 M72 N	X X	.004	.004		%100
189 M73	X Andrew State Sta	.004	.004	0	%100
190 M74	K X COURT		.004	0	%100
191 M75	X	.004	.004	0	%100
<u>192 M76</u>			.004	0	%100
193 M77	X	.004	.004	0	<u>%100</u>
194 M78	X	.004	<u>.004</u> .004	<u> </u>	%1 <u>00</u> %100
195 M79 196 M80		.004	1004	0	%100
196 Woo	X	.004	.004	0	%100
198 M82	Î Â	.004	.004	, Ö atta	%100
199 <u>M83</u>	X	.001	.001	0	%100
200 M84 -	X	.001	.001		%100
201 M85	X	0			%100
202 M86	<u>X</u>	0	0		%100

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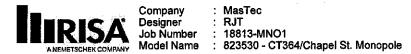
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	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft.%]
203	M87	<u> </u>	.001	.001	0	%100
204	M88-	X	.001	.001	0	%100
205	M89	Х	0	0	0	%100
206	M90	X	2	0	0	%100
207	M91	X	.002	.002	0	<u>%100</u>
208	M92	- X	.002	.002	0	%100
209	M93	X	.002	.002	0	%100
210	M94	X	.002	.002	0	%100
211	M95	<u>х</u>	.002	.002	0	<u>%100</u>
212	M96	X	.002	.002	0	%100
213	M97	X	.002	.002	0	%100
214	M98	X	.002	.002	0	%100
215	M99	Х	.002	.002	0	%100
216	M100	X	.002	.002	0	%100
217	M101	X	.002	.002	0	<u> </u>
218	M102	X	.002	.002	· · · · · · · · · · · · · · · · · · ·	%100
219	M103	Х	.002	.002	0	<u>%100</u>
220	M104	X	.001	.001	0	%100
221	M105	X	.001	.001	0	%100
222	M106	Х	.002	.002	0	%100
223	M107	X	.002	.002	0	<u>%100</u>
224	M108 🗰 👘 👘	Х	.001	.001	0	%100
225	M109	Х	.001	.001	0	<u>%100</u>
226	M110	X (1)	.002	.002	0	<u>%100</u>
227	M111	Х	.002	.002	0	<u>%100</u>
228	M112	X	.001	.001	0	%100
229	M113	X	.001	.001	0	%100
230	M114	х 🖓	.002	.002	0	%100
231	M115	<u>X</u>	.002	.002	0	%100
232	M116	<u>на X на </u>	.001	.001	0	%100
233	M117	X	.001	.001		%100
234	M118	X	.002	.002	0	%100
235	M28	Х	.002	.002	<u>%19.2</u>	%100
236	<u>M33</u>	X	.002	.002	<u>%90</u>	%100

Member Distributed Loads (BLC 23 : Ice Wind Members (60 Deg))

	Member Label	Direction	Start Magnitude/k/ft	End Magnitude[k/ft,F	Start Location[ft,%]	End Location[ft,%]
1	M1	Z	002	002	0	%100
2	M2	⇒ Z 1	002	002	0	<u>%100</u>
3	M3	Z	002	002	0	%100
4	M4 M4	Z	-:002	002	0 - 0	%100
5	M5	Z	004	004	0	%100
6	M6	Z	001	001	0	%100
7	M7	Z	004	004	0	%100
8	M8	- Z -	001	001	0	%100
9	M9	Z	003	003	0	%100
10	M10	- Z -	001	001	0	%100
11	M11	Z	001	001	0	%100
12	M12	Z	003	-1. 003	O	%100
13	M13	Z	004	004	0	%100
14	M15	Z	004	004	0	%100
15	M17	Z	004	004	0	%100
16	M19	2 - Z - E	004	004	0	%100
17	M21	Z	002	002	0	%100
18	M22	2	002	002		%100
19	M23	Z	001	001	0	<u>%1</u> 00



Member Label	Direction		End Magnitude[k/ft.F	The second se	End Location[ft,%]
20 M24 21 M25	Z	001 002	001 002	<u></u>	<u>%100</u> %10
21 M25 22 M28	7	002	002	o a la	%100
23 M29	Z	002	002	0	%10
24 M31	<u>Z</u>	-,002	002	<u> </u>	%100
25 M33	<u>Z</u>	002 -/002	002	0	<u>%100</u> %100
26 M34 27 M31A	Z	002	002	0	<u>%100</u> %100
28 M32A	z z	-002	- 002	, jõ	%100
29 M33A	Z	002	002	0	<u>%100</u>
30 M34A	Z	-,002	002		%100
31 <u>M35</u> 32 M36		004	004 	0	<u>%100</u> %100
33 M37	2 7	004	004	0	%100
34 M38	ž .	004	=.004	Ó.	%100
35 M39	Z	004	004	0	%100
<u>36</u> <u>M40</u>	1 <u>Z</u>	004	-n ≑004		%100
37 M41 38 M42	<u> </u>	004	004 004	0	%100 %100
39 M43	Z	-,004	004	0	%100
40 M44	$\overline{\mathbf{z}}$	004	- 004	Ó Í	%100
41 M45	Ζ	004	004	0	%100
42 M46	"Z	004	004	<u> </u>	<u>%100</u>
43 M47 44 M48	Z Z korej	004 004	004 004	0 0	<u>%100</u> %100
44 M48 45 M49	7	004	004	0	%100
46 M50 M50	e z	-004	004	Č IT TOČE STATISTICS	%100
47 M51	Z	004	004	0	%100
.48 M52	<u> </u>	004	004		%100
49 <u>M53</u> 50 M54	Z	004	004 004	0	%100 %100
51 <u>M55</u>	Z	004	004	0	%100
52 M56	$\overline{\mathbf{z}}$	004	004		%100
53 M57	Z	004	004		%100
54 M58	Z	004	004	0	<u>%100</u> %100
55 M59 56 M60	Z	<u>004</u> 004	<u>004</u>	0	<u>%100</u> %100
57 M61	Ζ	004	004	0	%100
58 M62	Z	004	004	0	%100
59 M63	Z	004	004	0	%100
60 M64	Z 7	004 004	<u>004</u> 004	0	%100 %100
61 M65 62 M66	Z Z	004	004	<u> </u>	%100
63 M67	Z	004	004	0	%100
64 M68	Z	-:004	004	- WEIGHT GERMAN, STREEMAN, WE WEIGHT AND	%100
65 <u>M69</u>	Z	004	004	<u> </u>	%100 %100
66 M70 67 M71	Z	-, <u>004</u> 004	004	0	%100 %100
68 M72	Z	-,004		Ň Š	%100
69 M73	7	004	004	0	%100
70 M74	server Z	004	004	0	%100
71 M75	<u></u>	004	004		%100 %100
72 M76 73 M77	Z	004 004	004 004	0	%100 %100
74 M78	Ž	004	004		%100
75 M79	Z	004	004	0	%100
76 M80	Z Z	004	004		<u>%100</u>

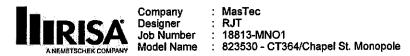


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Member Distributed Loads (BLC 23 : Ice Wind Members (60 Deg)) (Continued)

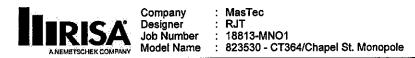
	Member Label	Direction	Start Magnitudelk/ft	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft.%]
77	M81	Z	004	004	0	%100
78	M82	Z	004	004	0	%100
79	<u>M83</u>	<u>Z</u>	001	001	0	%100
80	<u>M84</u>	<u>z</u>	001	001	0	%100
81	<u>M85</u>	Z	0	0	0	<u>%100</u> %100
82	<u>M86</u>		.0		0	%100
<u>83</u> 84	M87 M88	<u>Z</u>	001 - 001	001 *001	i n	%100
85	M89	7	- 001	0	0	%100
86 M	M90	2 2	Ő –	<u>0</u>	o e e	%100
87	M91	Z	002	002	0	%100
88	M92	Z	-,002	002	0	%100
89	M93	Z	002	002	0	%100
90	<u>M94</u>	Z = 45	002	002	<u>o</u>	%100
91	M95	<u> </u>	002	002		<u>%100</u>
92	<u>M96</u>	<u> </u>	-,002	002	0	%100 %100
93	<u>M97</u> M98	Z Z v v	002	002 002	0.45	%100
94 95	M98	7	002	002	0	%100
96	M100 //	7	-,002	002	Ő	%100
97	M101	Z	002	002	0	%100
98	M102	z	002	002	0	%100
99	M103	Z	002	002	0	%100
100	M104	Z	001	=.001	0	%100
101	<u>M105</u>	Z	001	001	0	%100
102	M106	<u> </u>	- 002	<u>-002</u>	0	%100
103	<u>M107</u>	<u> </u>	002	<u>002</u> -:001		%100 %100
104	<u>M108</u>	<u> </u>	001	001	0	%100
105	M109 M110	2	001 002	001		<u>%100</u>
107	M110	Z	002	002	0	%100
108	M112	- Z	=,001	001	** 0	%100
109	M113	Z	001	001	0	%100
110	M114	Ζ	002	002	0	%100
111	<u>M115</u>	<u>Z</u>	002	002	0	%100
112	M116	Z Z	- 001	001	0	%100
113	<u>M117</u>	Z	001	001	<u>0</u>	<u>%100</u> %100
114	M118		002	002 002	<u>%</u> 90	%100
115	<u>M25</u> M27		002	002	%61	%100
117	M29	7	002	002	%90	%100
118	M32		002	≓002	%60	%100
119	M1	X	.003	.003	0	%100
120	M2 ***	X	.004	.004	a i 0	%100
121	<u>M3</u>	X	.003	.003	0	%100
	M4	X	:004	.004	0	%100
123	<u>M5</u>	<u> </u>	.006	.006	0	<u>%100</u> %100
124	M6	<u> </u>	.001	.001	0	<u>%100</u> %100
125	M7 M8	<u> </u>	.006	. <u>006</u> .001	0	%100
126	M8 M9	X	.004	.004	0	%100
127	M10	Â	.004	.004	1	%100
129	M11	X	.001	.001	0	%100
	M12	Î Â	004	,004	0	%100
131	M13	X	.006	.006	0	%100
132	M15			.006	0	%100
133	M17	X	.006	.006	0	%100
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		<u> </u>			End Loostion(# 0/1
Member Label	Direction	Start Magnitude/k/ft	End Magnitude(k/it.F.		End Location[ft,%] %100
<u>134 M19</u>	X	.006	.006	0	%100
135 <u>M21</u>	<u> </u>	.003	.003	0	
136 M22	X	.003	,003	<u> </u>	%100
137 <u>M23</u>	<u> </u>	.002	.002	0	<u>%100</u>
138 M24	X	1.002	.002	0	%100
139 M25	<u> </u>	.004	.004		%100
140 M26	X	.004		0	%100
141 M27	X	.004	.004	0	%100
142 M29	X	.004	.004	-0	%100
143 M30	X	.004	.004	0	%100
144 M31	X	.004	.004	0	%100
145 M32	X	.004	.004	0	%100
146 M33	X	,004	.004	0	%10
147 M31A	X	.004	.004	0	%100
148 M32A	X	,004	.004	0	%100
149 M33A	X	.004	.004	0	%100
150 M34A	X	.004	.004	0 0	%100
	· X	.006	.006	0	%100
	x x	.006	.006	i i n a s	%100
	1	.006	.006	0	%100
153 <u>M37</u>	X		.008	o o	%100
154 M38	X	.006			%100
155 M39	X ► X	.006	.006	0	%100 %100
156 M40	and a second sec	.006	.006		
157 M41	X	.006	.006	0	%100
158 M42	X	.006	.006	0	%100
159 M43	X	.006	.006	0	%100
160 M44	X	.006	.006	0	%100
161 <u>M45</u>	<u> </u>	.006	.006	0	%100
162 M46	X	.006	.006	0	%100
163 M47	X	.006	.006	0	%100
164 M48	X	.006	.006	0	<u>%100</u>
165 M49	X	.006	.006	0	<u>%100</u>
166 M50	×<	.006		0	<u> </u>
167 M51	X	.006	.006	0	%100
168 M52	1996 X 1 8 8	.006	.006	0	%100
169 M53	X	.006	.006	0	%100
170 M54	X 1	.006	.006	0	%100
171 M55	X	.006	.006	0	%100
172 M56	Ries X Star	,006	.006	0	%100
173 M57	X	.006	.006	0	%100
174 M58	X	.006	006	0	%100
175 M59	X	.006	.006	0	%100
176 M60		.006	.006		
	X	.006	.006	0	%100
177 M61 178 M62	Â.	.006	.006 10	o o com	%100
		.006	.006	0	%100
179 M63			.006		<u>%100</u>
180 M64					%100
181 <u>M65</u>	L X	.006	.006		%100
182 M66	X		.006		
183 M67	X	.006	.006	0	<u>%100</u>
184 M68	X	April Act and the second	.006	0	%100
185 M69	X	.006	.006	0	%100
186 M70	X	.006	.006	0	%100
187 M71	<u> </u>	.006	.006	0	%100
188 M72	X	.006	.006	0 •••	%100
189 M73	X	.006	.006	0	<u>%100</u>
190 M74	X		.006	0	%100

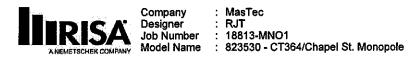
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r	Member Label	Direction		End Magnitude[k/ft.F		End Location[ft.%]
191	<u>M75</u>		.006 .006	.006		<u>%100</u> %100
192	M76 M77	X	.006	.006	0	%100
<u>193</u> 194	M78	$\hat{\mathbf{x}}$.006	.008		%100
195	M70	X	.006	.006	Õ	%100
196		x x	.006	.006	Ŏ	%100
197	M81	X	.006	.006	0	%100
198	M82	X	.006	.006	v the 0 +d	%100
199	M83	<u> </u>	.003	.003	0	%100
200	M84	X	.003	.003	60	%100
201	<u>M85</u>	X	0	0	0	%100
202	<u>M86</u>	X	0	0	0	%100
203	M87	X	.003	.003	0 	<u>%100</u> %100
204			.003	.003	0	%100
205 206	M89	X	0	0		%100
206	M90	Y	.004	.004	0	%100
207	M92	Â.	.004	.004	o i	%100
209	M93	X	.004	.004	0	%100
210	M94	X	.004	004	0	%100
211	M95	X	.004	.004	0	%100
212	M96	X		.004	0	%100
213	<u>M97</u>	<u>X</u>	.004	.004	O	%100
214	M98	X	.004	.004	0	%100
215	M99	X	.004	.004	0	%100
216	M100	X	.004	.004		%100 %100
217	M101	X	.004	.004	0	<u>%100</u> %100
<u>218</u> 219	M102 M103	N N	.003	.004	0	%100
220	M104	Ŷ	.002	.002		%100
221	M105	X	.002	.002	Ō	%100
222	M106	X		.003	0	%100
223	M107	Х	.003	.003	0	%100
224	M108	X	.002	.002	<u> </u>	%100
225	M109	X	.002	.002	0	%100
226	M110	X	.003	.003	0	%100
227	M111	X	.003	.003	0	%100
228	M112	X	.002	.002	0	<u>%100</u> %100
229	<u>M113</u> M114	X	<u>.002</u> :003	.002	0	%100
230 231	M114 M115	X	.003	.003	0	%100 %100
231	M116	$\hat{\mathbf{x}}$	+.002	.003		%100
232	M110	X	.002	.002	0	%100
234	M118	X	.003	.003	<u> </u>	%100
235	M28	X	.004	.004	%19.2	%100
236	M33	X	.004	.004	%90	%100

Member Distributed Loads (BLC 24 : Ice Wind Members (90 Deg))

	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft,F	Start Location[ft.%]	End Location[ft,%]
1	M1	Z	0	0	0	%100
2	M2	Z	0	0	0	%100 2
3	M3	Z	0	0	0	%100
4	M4	Z 🐳	0	0	.0	%100
5	M5	Z	0	0	0	%100
6	M6	Z	0	. 1 → 1 → 3 → 3 → 3 → 3 → 3 → 3 → 3 → 3 → 3	0	%100
7	M7	Z	0	0	0	%100



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Member Distributed Loads (BLC 24 : Ice Wind Members (90 Deg)) (Continued)

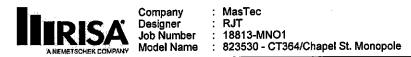
Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft,%]
8 M8	Ž		0	0	%100
9 M9	Z	0	0	0	%100
10 M10	Z.	<u> </u>		0	<u>%100</u>
11 M11 12 W12	<u> </u>	0	0	0	<u>%100</u> %100
13 M13	Z	0	0	0	%100
14 M15	- A. Z - A.	Ŏ	0	0	%100
15 M17	Z	0	0	0	%100
<u>16</u> <u>M19</u>	Z (14)	<u> </u>	0	0	%100 %100
17 M21 18 M22	<u>Z</u>	0	0	0	<u>%100</u> %100
19 M23	Z	0	0	0	% <u>100</u>
20 M24	Z	0	Ō	0	%100
21 M25		0	0		%10
22 M28	Z Z	0	0	0	%100 %10
23 M29 24 M31	Z	o o	0	Ŭ O	%100
25 <u>M33</u>	Z	0	0	0	%100
-26 M34	<u> </u>	0	0	0	%100
27 M31A	Z	0	0	0	<u>%100</u>
28 M32A 29 M33A	Z	<u> 0 </u>	04	0	<u>%100</u> %100
30 M34A	7	Ö	<u>,</u>	ŬI ÕT S	%100
31 M35	Z	Ō	0	0	%100
32 M36	Z	0	<u>0</u>	0	%100
33 M37	<u>Z</u>	0	0	0	%100 %100
34 M38 35 M39	Z	0	<u>0</u>	0	%100
36 M40	Ž	<u> </u>	Ŏ	Č – L	%100
37 M41	Z Z	0	0	0	%100
38 M42		0	0	Ŏ	<u>%100</u>
39 M43 40 M44	Z	0 • • • • • • • •	0 0	0	%100 %100
40 M45	Z	0	0	0	%100
42 M46	Z	<u>0</u>	0	0	%100
<u>43 M47</u>	Z	0	0	0	%100
44 M48	Z 7	0	0	0	<u>%100</u> %100
45 M49 46 M50	Ź	0	0	<u>v</u>	%100
47 M51	Z	0	0	0	%100
48 M52	Z a st	0	0	<u> </u>	%100
49 M53	Z Z	0 0		O O	<u>%100</u> %100
50 M54 51 M55		0	0	0	%100
52 M56	Z Z	Ŏ	ia a Ólasta i a	<u> </u>	%100
53 M57	Z Z	0	0	0	%100
54 M58			0 - N	<u> </u>	%100
55 M59 56 M60	Z	0 0	O Dec iii ii	0	<u>%100</u> %100
56 M60 57 M61	Z	0	0	0	%100
58 M62		Ŏ.	<u> </u>	i i õ 📾 Ster	%100
59 M63	Z	0	0	0	%100
60 V64	Z		0	0	<u>%100</u> %100
61 M65 62 M66	ZZ	<u>0</u> 0	<u>0</u>	0	<u>%100</u> %100
63 M67	Z	0	0	0	%100
64 M68	Z ·	<u>0</u>	0	0	%100

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	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft,F	Start Location[ft.%]	End Location[ft.%]
65	M69	<u>Z</u>	0	0	0	%100
66	<u>M70</u>	<u>z</u>	0	0	<u> </u>	%100
67	<u>M71</u>	<u>Z</u>				%100 %100
68 69	M72 M73	Z	0	<u></u>	0	%100
70	M75	Ž	<u>o</u>	n n n	0	%100
71	M75	Z	0	0	0	%100
72	M76	Z	0	0	0	%100
73	M77	Z	0		0	%100
74	M78	<u> </u>	0	0	0	<u>%100</u>
75	M79 M80		0	0	0	%100 %100
76 77	M80	Z	0	0	0	%100
78	M82-	2 Z	e e la company de la company	o i i i	, j	%100
79	M83	Z	0	0	0	%100
80	M84	Z = 1	<u> </u>	0	0	%100
81	<u>M85</u>	Z	0	<u> </u>	0	%100
82	<u>M86</u>	<u>z</u>	0	<u>0 - 2 - 1 - 1</u> 0	<u> </u>	<u>%100</u> %100
83 84	<u>M87</u> M88	2		n v		%100
85	M89	7	0	0	Ö	%100
86	M90	Ž.	0	0	0	%100
87	M91	Z	0	0	0	<u>%100</u>
88	M92	∴ Z	0	10	0	%100
89	<u>M93</u>		0	0	0	%100 %100
<u>90</u> 91	M94 M95	Z 7	0	0	0	%100
92	M95	ž – <u>2</u>	Ŏ	Č Č		%100
93	M97	Z	0	0	0	%100
94	M98	Z	оле те .0	0	0	%100
95	M99		0	0	0	%100
96	M100	Z	0	0	<u>0</u>	%100 <u>*</u>
97 98	M101 M102		<u> </u>	0 La ven de ser en la		<u>%100</u> %100
99	M102	Z	0	0	0	%100
100	M104	z z	0	0	0	%100 👘
101	M105	Z	0	0	0	%100
102	M106	Z	0	0	0	%100
103	<u>M107</u>	Z	0	0		<u>%100</u> %100
<u>104</u> 105	<u>M108</u> M109	<u> </u>	0	<u> </u>	0	<u>%100</u> %100
105	M110	7	ŏ	i - C	i i i i i i i i i i i i i i i i i i i	%100
107	M111	Z	0	0	0	%100
108	M112	Z 2	0	0	0	%100
109	<u>M113</u>	<u> </u>	0	0	0	%100
110			0		TARGET Suffer Chinese In Arthropic Tr Strengthering	<u>%100</u> %100
111	M115 M116	<u>Z</u>	0	0 1 0 1/2	0 1 0 1	<u>%100</u>
113	M110 M117	Z	0	0	0	%100
114	M118		0	<u> </u>	0	%100
115	M25	Z	0	0	%90	%100
WHERE A DESCRIPTION OF THE PARTY OF	M27	R + ≺Z	0	<u>0</u>	%61	%100
117	<u>M29</u>	Z	0	0	<u>%90</u>	<u>%100</u>
	M32	Z X	.002	.002	<u>%60</u> 0	<u>%100</u> %100
119	<u>M1</u> M2	X	.002	.002		%100
121	M3	X	.002	.002	0	%100

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<u>Member Distributed Loads (BLC 24 : Ice Wind Members (90 Dea)) (Continued)</u>

Member Label	Direction		End Magnitude[k/ft.F		End Location[ft,%]
122 M4	X	.006	.006	<u> </u>	<u>%100</u> %100
123 <u>M5</u> 124 M6	X	.004	.004	NE O LEED	%100
125 <u>M7</u>	X	.004	.004	0	%100
126 M8	X		.004	STO I	%100
127 M9	X	.003	.003	0	<u>%100</u>
128 M10	Xieta	.003	.003	0	<u>%100</u> %100
129 M11 130 M12	X	.00 <u>3</u> .003	.003		%100
131 M13	X	.007	.007	0	%100
132 M15	X x	007	.007	2 . 0	%100
133 M17	X	.007	.007	0	%100
134 M19	X	.007	007	0	<u>%100</u> %100
135 M21 136 M22	<u> </u>	.002	.002	<u>0</u>	%100
136 M22 137 M23	X	.002	.003	0	%100
138 M24	X .	.003	003	0	%100
139 M25	X	.004	.004	0	%100
140 M26	X	.004	.004		<u>%100</u>
141 M27	X	<u>.004</u> .004	.004	<u>0</u>	%100 %100
142 M29 143 M30	X	.004	.004	0	%100
144 M31	Â	.004	004	, Öler ser	%100
145 M32	X	.004	.004	0	%100
146. M33	X	.004	.004	0	%10
147 <u>M31A</u>	X	.005	.005	<u> </u>	%100 %100
148 M32A	X	.005 .005	.005	0	%100
149 M33A 150 M34A	$\hat{\mathbf{x}}$.005	.005		%100
151 <u>M35</u>	X	.007	.007	0	%100
152 M36	<u> </u>	.007	.007	0	%100
153 M37	<u> </u>	.007	.007	0	<u>%100</u> %100
154 M38	X	.007	.007	0	%100
155 M39 156 M40	X	.007	.007	i se a	%100
157 M41	X	.007	.007	0	%100
158 M42	×××	.007	.007	0	%100
159 M43	<u>X</u>	.007	.007	0	<u>%100</u>
160 M44	X	.007	.007	<u> </u>	<u>%100</u> %100
161 M45 162 M46		.007	.007	C L C	%100
163 M47	X	007	.007	0	%100
164 M48	X • 1	.007	.007		%100
165 M49	X	.007	.007	0	<u>%100</u>
166 M50	X	.007	.007	0	%100 %100
167 M51 168 M52	X V	<u>.007</u> :007	.007 .007		%100
168 M52 169 M53	X	.007	.007	0	%100
170 M54	X	.007	.007	0	%100
171 M55	X	.007	.007	0	%100
172 M56	X		.007		%100
173 M57		.007	.007	<u>0</u> * () 0 - (*)	<u>%100</u> %100
174 M58 175 M59	X	.007	.007	0	%100
176 M60	Â	.007	.007	Ŏ	%100
177 M61	Х	.007	.007	0	%100
178 M62	X	.007	.007	0	%100

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Member Distributed Loads (BLC 24 : Ice Wind Members (90 Deg)) (Continued)

	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft,F	Start Location[ft.%]	End Location[ft,%]
179	M63	⊤ x	.007	.007	0	%100
180	M64	X - 1	007	.007	0	%100
181	M65	<u> </u>	.007	.007	0	%100
182	M66 4	X	.007	.007	0 100	%100
183	M67	<u>X</u>	.007	.007	0	%100
184	M68	X	.007	.007	0	%100
185	M69	<u> X</u>	.007	.007		%100 %100
	<u>M70</u>	×	007	.007	0	<u>%100</u>
187	<u>M71</u>	<u> </u>	.007	.007		%100
188	M72	X	.007	.007	0	%100
189	<u>M73</u> M74	\sim	.007 .007	.007		%100
190 191	<u>W/4</u>	A to a	.007	.007	0	%100
192	M75		.007	.007	n n n seets i	%100 1
193	M77	X	.007	.007	0	%100
194	M78	X X	.007	007	0	%100
195	M79	T X	.007	.007	0	%100
196	M80	X	.007	.007	20	%100
197	M81	X	.007	.007	0	%100
198	M82	X	.007	.007	0	%100
199	M83	X	.003	.003	0	%100
200	M84	X	.003	.003	0	%100
201	M85	X	0	0	0	%100
202	M86	there is X and the	0	0	0	%100
203	<u>M87</u>	X	.003	.003		%100
204	M88	X	.003	<u> </u>	<u> </u>	<u>%100</u>
205	<u>M89</u>	X	0	0	0	%100
206	M90	X	0		0	%100 %100
207	<u>M91</u>	X	.005	.005 005	<u>0</u>	<u>%100</u> %100
208	<u>M92</u>	X	<u>.005</u> .005	.005	0	%100
209	<u>M93</u>		.005	.005	ine i o i i i i i i i i i i i i i i i i i	%100
210	M94	X X	.005	.005	0	%100
211 212	M95 M96		.005	.005		× 100
212	M97	X X	.005	.005	0	%100
214	M98	X	.005	005	o solar s	%100
215	M99	X	.005	.005	0	%100
216	M100	T X T	005	.005	0	%100
217	M101	X	.005	.005	0	%100
218	M102	<u>x</u>	.005	.005		%100
219	M103	X	.004	.004	0	%100
220		ie X -		.002	0	%100
221	M105	X	.002	.002	0	%100
222	M106	X	.004	,004	Q	%100
223	M107	<u> </u>	.004	.004	0	%100
	M108			.002	0	%100
225	<u>M109</u>	X	.002	.002	0	%100
	M110		.004	004	-	Construction of the second
227			.004	.004	0	<u>%100</u>
	M112	X	.002	.002		%100 %100
229	<u>M113</u>	<u> </u>	.002	.002	0	%100 %100
	M114		.004	A 19 ST TRADE OF A	0	<u>%100</u> %100
231	<u>M115</u>	X X	.004	.004	0	%100
	M116		.002	.002	0	%100
<u>233</u> 234	M117 M118		.002	Contraction of the second s	ALC OFFIC	%100
235	M110 M28	X	.004	.004	%19.2	%100
			+00.			Bogo 47

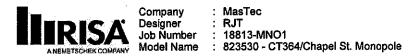
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Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft,%]	End Location[ft,%]
236 M33	X	.004	.004	%90	%100

Member Distributed Loads (BLC 25 : Ice Wind Members (120 Deg))

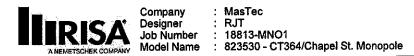
Member Label	Direction	Start Magnitude[k/ft			End Location[ft,%] %100
1 M1 2 M2	<u> </u>	.002	<u>.002</u> 002		%100
3 M3	Z	.002	.002	Ő	%100
4 M4	\bar{z}	.002	002	O D	%100
5 M5	Z	.001	.001	0	%100
6 M6	Z	.004	.004	-0	%100
M7	Z	.001	.001		%100
8 M8	<u>Z</u> 1	.004		0	%100
9 <u>M9</u>	<u>Z</u>	.001	.001	0	%100
10 M10	<u> 23 Z</u>	.003	.003	Sinchalds a redector one being an Cheville Cheville Cheville	<u>%100</u>
11 M11 12 M12 M12	2	.003 .001	.003 .001		%100 %100
13 M13	Z	.004	.004	0	%100
14 M15	<u> </u>	.004	.004		%100
15 M17	Z	.004	.004	0	%100
16 M19	ž	004	.004	0	%100
17 M21	Z	.002	.002	0	%100
18 M22	Z	,002	.002	is 45 0	%100
19 M23	Z	.001	.001	0	%100
20 M24	Z	.001		0	%100
21 M25	Z	.002	.002	0	%10
22 M28	<u> </u>	.002	.002	0	%100
23 <u>M29</u>	Z	.002	.002	0	%10
24 <u>M31</u>	2	002		0	<u>%100</u> %100
25 M33 26 M34	7	.002	.002	0 1 3 3 0 3 3 1	<u>%100</u> %100
27 M31A	Z	.002	.002	0	%100
28 M32A	7	.002	.002	Ó	%100
29 M33A	Z	.002	.002	0	%100
30 M34A	\overline{z}	.002	.002	A D	%100
31 M35	Z	.004	.004	0	%100
32 M36	Z 4	.004	.004	0	%100
33 M37	Z	.004	.004	0	%100
<u>.34</u> <u>M38</u>	Z *	.004	.004	0	%100
35 M39	<u>Z</u>	.004	.004	0	<u>%100</u> %100
36 W40	Z	.004	.004 .004	0	%100
37 M41 38 M42	Z	.004	.004		%100
39 M43	Z	.004	.004	0	%100
40	7	.004	.004	i î î î î î î	%100
41 M45	Z	.004	.004	0	%100
42 M46	Z	-004	.004	0	%100
43 M47	Z	.004	.004	0	%100
44 M48	Z	.004	.004	0	%100
45 M49	Z	.004	.004	0	%100
46 M50		.004	.004		%100
47 M51	Z	.004	.004	0	%100
			.004		
51 M55					%100
47 M51 48 M52 49 M53 50 M54 51 M55 52 M56	Z Z	.004 .004 .004 .004 .004 .004	.004 .004 .004 .004 .004 .004	0 0 0 0	%100 %100 %100 %100 %100 %100

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<u>MICIII</u>	Member Label	Direction	Start Magnitude[k/ft,	End Magnitude/k/ft.F.	Start Location[ft.%]	End Location[ft.%]
53	M57	Z	.004	.004	0	%100
54	M58	Z	.004	.004	<u>Ô</u>	%100
55	M59	Z	.004	.004	0	<u>%100</u> %100
56	M60	Z	.004	.004	0	%100
57	<u>M61</u> M62		.004	.004		%100
58 59	M62	7	.004	.004	0	%100
60	M64	7	004	.004	Ő -	%100
61	M65	Z	.004	.004	Ō	%100
62	M66	Z	.004	.004	0	%100
63	M67	<u>Z</u>	.004	.004	0	%100
64	M68	Z	.004	.004		%100
65	<u>M69</u>	<u>Z</u>	.004	.004	0	<u>%100</u> %100
66	M70	<u>Z</u>	.004	.004	0	<u>%100</u> %100
67 68	M71 M72	Z	.004	.004	C C	%100
69	M72	Z	.004	.004	0	%100
70		T Z	.004	004	. Ör	%100
71	M75	Z	.004	.004	0	%100
72	M76	Z	.004	.004	0	%100
73	M77	Z	.004	.004	0	%100
74	M7.8	Z	.004	.004	0	%100
75	M79		.004	.004	0	%100
76	M80	Z	.004	,004	0	<u>%100</u>
77	<u>M81</u>	<u> </u>	<u>.004</u> .004	<u>.004</u> .004	0	%100 %100
78 79	<u>M82</u> M83	7	.004	.004	0	%100
80	M84	7	.001	.001		%100
81	M85	Z	0	0	0	%100
82	M86	Z	0	0	- C 0	%100
83	M87	Z	.001	.001	0	%100
84	<u> 1 – M88</u>	2 Z	.001	.001		%100
85	M89	<u> </u>	0	0		<u>%100</u>
86	M90	<u> </u>	0 ***	.002	0	%100 %100
87 88	<u>M91</u> M92	Z	.002	.002	0	%100
89	M93	Z	.002	.002	0	%100
90	M94	ź	002	.002	0	%100
91	M95	a construction of the log of the	.002	.002	0	%100
92	M96	Z Z	.002	.002	. 0	%100
93	<u>M97</u>	<u>Z</u>	.002	<u>,002</u>	0	%100
94	<u>M98</u>	Z	.002	.002		%100
95	<u>M99</u>	Z Z	.002	.002	044	<u>%100</u> %100
96			.002	<u>:002</u> .002	0	%100
97 98	M101 M102	Z		.002	0	%100
99	M102	Z	.002	.002	0	%100
100	M104		001	001	i la constante de la constante	%100
101	M105	Z	.001	.001	Ō	%100
102				.002	0	%100
103	M107	Z	.002	.002		%100
104	M108			001	0	%100
105	M109	<u>Z</u>	.001	.001	0	%100
	M110	<u>Z</u>		002		<u>%100</u> %100
107	<u>M111</u> M112	Z	.002	.002	0	%100
108	M112 M113	Z	.001	.001	0	%100
109		<u> </u>				

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Weinder Distindled Lo				<u> </u>	
Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft,F	Start Location[ft.%]	End Location[ft,%]
110 M114		.002	.002	<u> </u>	<u>%100</u>
111 M115	Z	.002	.002	0	<u>%100</u>
112 M116	Ī	.001	.001	5	%100
	7	.001	.001	0	%100
	7	.002	002	n i n	%100
<u>114</u> M118				%90	%100
115 M25		.002	.002		
116 M27	<u>· Z</u>	.002	<u>,002 * </u>	%61	%100
117 M29	Z	.002	.002	%90	%100
118 M32	Z ***	.002	.002	%60	%100
119 <u>M1</u>	X	.003	.003	0	%100
120 M2	X	.004	.004	0	%100
		.003	.003	0	%100
121 M3		.004	.004	s s so n s su	%100
122 M4				And a second	<u>%100</u>
123 M5	<u> </u>	.001	.001	0	
124 M6	- X	.006	.006	<u>0</u>	%100
125 M7	X	.001	.001	0	%100
126 M8	· X	.006	.006	0	%100
127 M9	X	.001	.001	0	%100
128 M10	i x	.004	004	· · · · · · · · · · · · · · · · · · ·	%100
	·····	.004	.004	0	%100
129 M11	X X	.004	.004	i i i i i i i i i i i i i i i i i i i	%100
130 M12	<u> </u>			-	
131 M13	X	.006	.006	0	%100
132 M15	X	.006	.006	0	%100
133 M17	X	.006	.006	0	<u>%100</u>
134 M19	X	.006	.006	0	%100
135 M21	X	.003	.003	0	%100
136 M22	A CONTRACT OF	.003	.003	A 10 10	%100
		.002	.002	0	%100
<u>137 M23</u>			.002		%100
<u>138 M24 </u>		.002		TROOP COMPANY AND AND A COMPANY	%100
139 M25	X	.004	.004	0	
140 M26	X * -	.004	.004	0	%100
141 M27	<u> </u>	.004	.004	0	%100
142 M29	* X	.004		· · · · · · · · · · · · · · · · · · ·	%100
143 M30	X	.004	.004	0	%100
144 M31	Ŷ	.004	.004	· 0	%100
		.004	.004	Ō	%100
145 <u>M32</u>		.004	004	n n n	%10
146 <u>M33</u>				A DAK A DECINENTIAL AND DECINE AND A DATA AND AND AND AND AND AND AND AND AND AN	%100
147 <u>M31A</u>	X	.004	.004	0	
148 M32A	DOME NOW ADDRESS OF A DAME NOT ADDRESS OF ADDRE	:004	.004	<u> </u>	%100
149 M33A		.004	.004	0	<u>%100</u>
150 M34A	X X	.004	.004	0	<u>%100</u>
151 M35	X	.006	.006	0	%100
152 M36	X X	.006	.006	0	%100
	X	.006	.006	0	%100
153 M37	Â	006	006	0.0	%100
154 M38					%100
155 M39	X	.006	.006	0	
156 M40			.006	0	%100
157 M41	X	.006	.006	0	%100
158 M42	× ×	.006	.006	0	%100
159 M43		.006	.006	0	%100
160 M44		.006	,006	e de la companya de l	%100
		.006	.006	0	%100
161 M45			000.		%100 %100
162 M46		.006	.006		
163 M47	<u>X</u>	.006	.006	0	%100
164 M48	X		.006		%100
165 M49	X	.006	.006	0	%100
166 M50	X		.006	0	%100
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Member Label Direction Start Magnitudel/tf End Location (ft. %) End Location (ft. %) <thend %)<="" (ft.="" location="" th=""> End Location (ft. %)</thend>
168 M52 X 006 006 0 $\%100$ 169 M53 X 006 006 0 $\%100$ 170 M54 X 006 006 0 $\%100$ 171 M55 X 006 006 0 $\%100$ 173 M57 X 006 006 0 $\%100$ 173 M57 X 006 006 0 $\%100$ 174 M58 X 006 006 0 $\%100$ 175 M59 X 006 006 0 $\%100$ 175 M52 X 006 006 0 $\%100$ 176 M62 X 006 006 0 $\%100$ 177 M61 X 006 006 0 $\%100$ 178 M62 X 006 006 0 $\%100$ 180 M54
169 M53 X 006 006 0 %100 170 M54 X 006 006 0 %100 171 M55 X 006 006 0 %100 172 M56 X 006 006 0 %100 173 M57 X 006 006 0 %100 173 M58 X ¹¹ 006 006 0 %100 175 M59 X 006 006 0 %100 176 M61 X 006 006 0 %100 177 M61 X 006 006 0 %100 177 M63 X 006 006 0 %100 178 M62 X 006 006 0 %100 181 M66 X 006 006 0 %100 183 M70 X 00
171 M55 X 006 006 0 %100 172 M57 X 006 006 0 %400 173 M57 X 006 006 0 %400 174 M58 X 006 006 0 %400 175 M59 X 006 006 0 %400 176 M59 X 006 006 0 %400 177 M61 X 006 006 0 %400 177 M63 X 006 006 0 %400 178 M62 X 006 006 0 %400 181 M65 X 006 006 0 %400 182 M68 X 006 006 0 %400 183 M67 X 006 006 0 %400 184 M68 X 006
171 M55 X 006 006 0 %100 172 M57 X 006 006 0 %100 173 M57 X 006 006 0 %100 174 M58 X 006 006 0 %100 175 M59 X 006 006 0 %100 176 M50 X 006 006 0 %100 177 M61 X 006 006 0 %100 178 M62 X 006 006 0 %100 179 M63 X 006 006 0 %100 181 M64 X 006 006 0 %100 182 M68 X 006 006 0 %100 183 M57 X 006 006 0 %100 184 M70 X 006
173 M57 X 006 006 0 %100 174 M58 X1 006 006 0 %100 175 M59 X 006 006 0 %100 176 M60 X 006 006 0 %100 177 M61 X 006 006 0 %100 177 M62 X 006 006 0 %100 179 M63 X 006 006 0 %100 181 M65 X 006 006 0 %100 183 M67 X 006 006 0 %100 184 M68 X 006 006 0 %100 185 M69 X 006 006 0 %100 186 M70 X 006 006 0 %100 187 M71 X 006 </td
172 M58 X 006 006 0 9%10 175 M59 X 006 006 0 9%10 176 M60 X 006 006 0 9%10 177 M61 X 006 006 0 9%10 177 M61 X 006 006 0 9%10 178 M62 X 006 006 0 9%10 179 M63 X 006 006 0 9%10 180 M64 X 006 006 0 9%10 181 M65 X 006 006 0 9%10 182 M67 X 006 006 0 9%10 183 M67 X 006 006 0 9%10 184 M68 X 006 006 0 9%10 185 M70 X 006
175 M59 X 006 006 0 %100 176 M60 X 006 006 0 %100 177 M61 X 006 006 0 %100 177 M61 X 006 006 0 %100 178 M62 X 006 006 0 %100 180 M63 X 006 006 0 %100 181 M65 X 006 006 0 %100 183 M67 X 006 006 0 %100 184 M68 X 006 006 0 %100 184 M68 X 006 006 0 %100 185 M70 X 006 006 0 %100 186 M72 X 006 006 0 %100 189 M73 X 006
176 M60 X 006 006 0 96100 177 M61 X 006 006 0 96100 178 M62 X 006 006 0 96100 179 M63 X 006 006 0 96100 180 M64 X 006 006 0 96100 181 M65 X 006 006 0 96100 182 M66 X 006 006 0 96100 183 M67 X 006 006 0 96100 184 M68 X 006 006 0 96100 185 M69 X 006 006 0 96100 186 M70 X 006 006 0 96100 186 M72 X 006 006 0 96100 189 M73 X
177 M61 X .006
176 M52 X 006 006 0 %400 179 M53 X 006 006 0 %100 180 M64 X 006 006 0 %100 181 M65 X 006 006 0 %100 181 M65 X 006 006 0 %100 182 M66 X 006 006 0 %100 183 M67 X 006 006 0 %100 184 M68 X 006 006 0 %100 185 M69 X 006 006 0 %100 186 M70 X 006 006 0 %100 187 M71 X 006 006 0 %100 188 M72 X 006 006 0 %100 190 M74 X 006
179 M63 X .006 .006 0 %100 180 M64 X .006 .006 0 %100 181 M65 X .006 .006 0 %100 182 M66 X .006 .006 0 %100 183 M67 X .006 .006 0 %100 184 M68 X .006 .006 0 %100 185 M69 X .006 .006 0 %100 185 M69 X .006 .006 0 %100 186 M70 X .006 .006 0 %100 188 M72 X .006 .006 0 %100 189 M73 X .006 .006 0 %100 190 M74 X .006 .006 0 %100 192 M76 X
180 M64 X 006 006 0 %100 181 M65 X 006 008 0 %100 182 M66 X 006 008 0 %100 183 M67 X 006 008 0 %100 183 M67 X 006 008 0 %100 184 M68 X 006 008 0 %100 184 M69 X 006 006 0 %100 185 M69 X 006 006 0 %100 186 M70 X 006 006 0 %100 187 M71 X 006 006 0 %100 189 M73 X 006 006 0 %100 191 M75 X 006 006 0 %100 192 M76 X 006
181 M65 X .006 .006 0 %100 182 M66 X .006 .006 0 %100 183 M67 X .006 .006 0 %100 184 M68 X .006 .006 0 %100 184 M68 X .006 .006 0 %100 185 M69 X .006 .006 0 %100 186 M70 X .006 .006 0 %100 186 M72 X .006 .006 0 %100 188 M73 X .006 .006 0 %100 190 M74 X .006 .006 0 %100 191 M75 X .006 .006 .0 %100 193 M77 X .006 .006 .0 %100 193 M79 <td< td=""></td<>
182 M68 X 006 006 0 %100 183 M67 X 006 006 0 %100 184 M68 X 006 006 0 %100 185 M69 X 006 006 0 %100 185 M69 X 006 006 0 %100 186 M70 X 006 006 0 %100 187 M71 X 006 006 0 %100 188 M72 X 006 006 0 %100 189 M73 X 006 006 0 %100 190 M74 X 006 006 0 %100 191 M75 X 006 006 0 %100 192 M76 X 006 006 0 %100 193 M77 X 006
183 M67 X 006 006 0 %100 184 M68 X 006 006 0 %100 185 M69 X 006 006 0 %100 186 M70 X 006 006 0 %100 186 M70 X 006 006 0 %100 187 M71 X 006 006 0 %100 188 M72 X 006 006 0 %100 189 M73 X 006 006 0 %100 190 M74 X 006 006 0 %100 192 M76 X 006 006 0 %100 192 M77 X 006 006 0 %100 193 M77 X 006 006 0 %100 194 M78 X 006
184 M68 X 006 006 0 %100 185 M69 X 006 006 0 %100 186 M70 X 006 006 0 %100 186 M70 X 006 006 0 %100 187 M71 X 006 006 0 %100 188 M72 X 006 006 0 %100 189 M73 X 006 006 0 %100 190 M74 X 006 006 0 %100 192 M76 X 006 006 0 %100 193 M77 X 006 006 0 %100 193 M79 X 006 006 0 %100 194 M78 X 006 006 0 %100 195 M79 X 006
185 M69 X 006 006 0 %100 186 M70 X 006 006 0 %100 187 M71 X 006 006 0 %100 188 M72 X 006 006 0 %100 188 M72 X 006 006 0 %100 189 M73 X 006 006 0 %100 190 M74 X 006 006 0 %100 191 M75 X 006 006 0 %100 192 M76 X 006 006 0 %100 193 M77 X 006 006 0 %100 194 M78 X 006 006 0 %100 195 M79 X 006 006 0 %100 196 M80 X 006
186 M70 X 006 006 0 %100 187 M71 X 006 006 0 %100 188 M72 X 006 006 0 %100 188 M72 X 006 006 0 %100 189 M73 X 006 006 0 %100 190 M74 X 006 006 0 %100 191 M75 X 006 006 0 %100 192 M76 X 006 006 0 %100 193 M77 X 006 006 0 %100 193 M77 X 006 006 0 %100 194 M78 X 006 006 0 %100 196 M80 X 006 006 0 %100 197 M81 X 006
187 M71 X .006 .006 0 %100 188 M72 X 006 006 0 %100 189 M73 X 006 006 0 %100 190 M74 X 006 006 0 %100 191 M75 X .006 .006 0 %100 192 M76 X .006 .006 0 %100 192 M76 X .006 .006 0 %100 193 M77 X .006 .006 0 %100 193 M77 X .006 .006 0 %100 194 M78 X .006 .006 0 %100 195 M79 X .006 .006 0 %100 196 M80 X .006 .006 .006 .006 .006 198 M82
188 M72 X .006 006 0 %100 189 M73 X .006 .006 0 %100 190 M74 X .006 .006 0 %100 190 M74 X .006 .006 0 %100 191 M75 X .006 .006 0 %100 192 M76 X .006 .006 0 %100 193 M77 X .006 .006 0 %100 193 M77 X .006 .006 0 %100 194 M78 X .006 .006 0 %100 195 M79 X .006 .006 0 %100 196 M80 X .006 .006 .006 0 %100 198 M82 X .003 .003 .0 %100 200
189 M73 X .006 .006 0 %100 190 M74 X .006 006 0 %100 191 M75 X .006 .006 0 %100 192 M76 X .006 .006 0 %100 192 M76 X .006 .006 0 %100 193 M77 X .006 .006 0 %100 193 M77 X .006 .006 0 %100 194 M78 X .006 .006 0 %100 195 M79 X .006 .006 0 %100 195 M80 X .006 .006 0 %100 196 M80 X .006 .006 0 %100 197 M81 X .003 .003 .0 %100 200 M82 X
190 M74 X 006 006 0 %100 191 M75 X .006 .006 0 %100 192 M76 X .006 .006 0 %100 192 M76 X .006 .006 0 %100 193 M77 X .006 .006 0 %100 193 M77 X .006 .006 0 %100 194 M78 X .006 .006 0 %100 194 M79 X .006 .006 0 %100 195 M79 X .006 .006 0 %100 196 M80 X .003 .003 .0 %100 197 M81 X .003 .003 .0 %100 199 M83 X .003 .003 .0 %100 200 M84
191 M75 X .006 .006 0 %100 192 M76 X .006 006 0 %100 193 M77 X .006 .006 0 %100 193 M77 X .006 .006 0 %100 194 M78 X .006 .006 0 %100 195 M79 X .006 .006 0 %100 195 M79 X .006 .006 0 %100 196 M80 X .006 .006 0 %100 197 M81 X .006 .006 0 %100 198 M82 X .003 .003 0 %100 200 M84 X .003 .003 0 %100 201 M85 X .0 .0 .0 .0 %100 203 M87
192 M76 X 006 006 0 %100 193 M77 X 006 006 0 %100 194 M78 X 006 006 0 %100 194 M78 X 006 006 0 %100 195 M79 X 006 006 0 %100 196 M80 X 006 006 0 %100 196 M80 X 006 006 0 %100 197 M81 X 006 006 0 %100 198 M82 X 003 003 0 %100 200 M84 X 003 003 0 %100 201 M85 X 0 0 0 %100 203 M87 X 003 003 0 %100 205 M89 X 0
193 M77 X .006 .006 0 %100 194 M78 X .006 .006 0 %100 195 M79 X .006 .006 0 %100 195 M79 X .006 .006 0 %100 196 M80 X .006 .006 0 %100 197 M81 X .006 .006 0 %100 198 M82 X .006 .006 0 %100 198 M83 X .003 .003 0 %100 200 M84 X .003 .003 0 %100 201 M85 X 0 0 0 %100 203 M87 X .003 .003 0 %100 204 M88 X .003 .003 .0 %100 205 M89 X
194 M78 X 006 006 0 %100 195 M79 X 006 006 0 %100 196 M80 X 006 006 0 %100 196 M80 X 006 006 0 %100 197 M81 X .006 006 0 %100 198 M82 X .006 006 0 %100 198 M83 X .003 .003 0 %100 200 M84 X .003 .003 0 %100 201 M85 X 0 0 0 %100 203 M87 X .003 .003 0 %100 204 M88 X .003 .003 .0 %100 205 M89 X .0 .0 .0 .0 .0 206 M90 X
195 M79 X .006 .006 0 %100 196 M80 X 006 006 0 %100 197 M81 X .006 .006 0 %100 198 M82 X .006 .006 0 %100 198 M82 X .003 .003 0 %100 199 M83 X .003 .003 0 %100 200 M84 X .003 .003 0 %100 201 M85 X 0 0 0 %100 203 M87 X .003 .003 0 %100 204 M88 X .003 .003 .0 %100 205 M89 X .0 .0 .0 .0 %100 206 M90 X .0 .0 .0 .0 .0 .0 .0 <
196 M80 X 006 006 0 %100 197 M81 X .006 .006 0 %100 198 M82 X .006 .006 0 %100 198 M83 X .003 .003 0 %100 199 M83 X .003 .003 0 %100 200 M84 X .003 .003 0 %100 201 M85 X 0 0 0 %100 202 M86 X .003 .003 0 %100 203 M87 X .003 .003 0 %100 204 M88 X .003 .003 .0 %100 205 M89 X .0 .0 .0 .0 .0 206 M90 X .0 .0 .0 .0 .0
197 M81 X .006 .006 0 %100 198 M82 Xxxx 006 006 0 %100 199 M83 X .003 .003 0 %100 200 M84 X .003 .003 0 %100 201 M85 X 0 0 0 %100 203 M87 X .003 .003 0 %100 203 M87 X .003 .003 0 %100 204 M88 X .003 .003 0 %100 205 M89 X 0 0 0 %100 206 M90 X 0 0 0 %100
198 M82 Xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx
199 M83 X .003 .003 0 %100 200 M84 X .003 .003 0 %100 201 M85 X 0 0 0 %100 202 M86 X 0 0 0 %100 203 M87 X .003 .003 0 %100 204 M88 X .003 .003 0 %100 205 M89 X 0 0 0 %100 206 M90 X 0 0 0 %100
200 M84 X 003 003 0 %100 201 M85 X 0 0 0 %100 202 M86 X 0 0 0 %100 203 M87 X 0.003 0.003 0 %100 204 M88 X .003 .003 0 %100 205 M89 X 0 0 0 %100 206 M90 X 0 0 0 %100
201 M85 X 0 0 0 %100 202 M86 X 0 0 0 %100 203 M87 X 003 003 0 %100 204 M88 X 003 003 0 %100 205 M89 X 0 0 0 %100 206 M90 X 0 0 0 %100
202 M86 X 0 0 0 %100 203 M87 X .003 .003 0 %100 204 M88 X .003 .003 0 %100 205 M89 X 0 0 0 %100 206 M90 X 0 0 0 %100
203 M87 X .003 .003 0 %100 204 M88 X .003 .003 0 %100 205 M89 X 0 0 %100 %100 206 M90 X 0 0 %100 %100
204 M88 X (003 .003 0 %100 205 M89 X 0 0 0 %100 206 M90 X 0 0 0 %100
205 M89 X 0 0 0 %100 206 M90 X 0 0 %100 %100
206 M90 X 0 0 0 %100
207 M91 X .004 .004 0 %100
208 M92 X 004 0 %100
209 M93 X .004 .004 0 %100
210 X M94 0 X M100
211 M95 X .004 .004 0 %100
212 M96 X 004 0 %100
213 M97 X .004 .004 0 %100
214 M98 X .004 0 %100
215 M99 X .004 .004 0 %100
216 M100 X 004 0 %100
217 M101 X .004 .004 0 %100
218 M102 X .004 0 %100
219 M103 X .003 .003 0 %100
220 M104 X .002 .002 0 %100
221 M105 X .002 .002 0 %100
222 M106 X 003 003 0 %100
223 M107 X .003 .003 0 %100

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	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft.%]
224	M108	X	.002	.002	0	%100
225	M109	Х	.002	.002	00	%100
226	M110	X	.003	.003	0	%100
227	M111	Х	.003	.003	0	%100
228	M112	X	.002	.002	· · · · 0	%100
229	M113	X	.002	.002	0	<u> </u>
230	M114	X	.003	.003	0	%100
231	M115	X	.003	.003	0	%100
232	M116	X	.002	002	0	%100
233	M117	Х	.002	.002	0	<u>%100</u>
234	M118	· X	.003	.003	0	%100
235	M28	X	.004	.004	<u>%19.2</u>	<u> </u>
236	M33	X	.004	.004	%90	%100

Member Distributed Loads (BLC 26 : Ice Wind Members (150 Deg))

	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F		End Location[ft,%]
1 21	<u>M1</u> M2	<u>Z</u>	.006	<u>600.</u>		%100 %100
3	M3	<u>z</u>	.006	.006	0	%100
	<u></u>	7	.000	.000	0	%100
5	M5	7	.001	.001	0	%100
Ĕ	M6	4.0 7 - 1	.006112111	006	o e constante de la constante d	%100
7	M7	7	.001	.001	0	%100
8	M8	Z	.006		0	%100
9	M9	Z	.001	.001	0	%100
10	M10	Z	.004	.004	0	%100
11	M11	Z	.004	.004	0	%100
12	M12	S Z	.001		0	%100
13	M13	Z	.006	.006	0	%100
14	M15		1006	.006	0	%100
15	M17	<u> </u>	.006	.006	0	%100
16	M19454	<u> </u>	.006	.006	. 0	%100
17	<u>M21</u>	<u>Z</u>	.004	.004	0	%100
18	M22	Z	.004	.004	0	%100
19	M23	Z	.001	.001	<u> </u>	<u>%100</u>
20	M24	<u> </u>	.001	.001	P Could : 10 million - Survive and the American State of the	%100
21	M25		.004	.004	<u> </u>	%10 ≶%100
22	M28	Z Z	.004	.004	0	<u>%100</u> %10
23 24	<u>M29</u> M31	<u> </u>	.004	.004	i i i i i i i i i i i i i i i i i i i	%100
25	M33	7	.004	.004	0	%100
26	M33		.004	.004		%100
27	M31A	Z	.004	.004		%100
28	M32A	7	004	.004	n o m	%100
29	M33A	7	.004	.004	0	%100
30	M34A	- Z	.004	.004	0	%100
31	M35	Z	.006	.006	0	%100
32	M36	Second Z	.006	.006	0	%100
33	M37	Z	.006	.006	0	%100
34	M38	Z	.006	.006	0	<u>%100</u>
35	<u>M39</u>	<u>Z</u>	.006	.006	0	%100
36	M40	<u>Z</u>	.006	.006	0	%100
37	M41	<u>Z</u>	.006	.006	0	<u>%100</u>
38	M42	Z -	.006	,006	<u> </u>	%100
39	M43	<u>Z</u>	.006	.006	0	%100
40	M44	li e Z →	.006	.006	0	%100



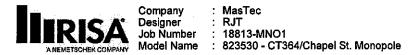
Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft,F	Start Location[ft.%]	End Location[ft,%]
41 M45	Z	.006	.006	0	%100
42 M46	Ż	.006	.006	<u> </u>	%100
43 M47		.006	.006		%100 %100
44 M48 45 M49	Z	.006	.006	0	%100
45 M49 46 M50	- -	.006	.006	n i n i i i i i i i i i i i i i i i i i	%100
47 M50	Z	.006	.006	0	%100
48 M52	Rati Z	.006	006-	. 0	%100
49 M53	<u>Z</u>	.006	.006		%100
50 M54	Z	.006	.006	0	%100
<u>51 M55</u>		.006	.006	<u> </u>	<u>%100</u> %100
52 M56 53 M57	Z	.006	.008	0	%100
53 M57	7	.006	.006	้ ได้ ได้ ได้ ได้ ได้ ได้ ได้ ได้ ได้ ได	%100
55 M59	Z	.006	.006	Ő	%100
56 M60	Z	.006	.006	0	%100
57 M61	Z	.006	.006	0	%100
58 M62	Z	.006	:006	0	%100
59 <u>M63</u>	<u> </u>	.006	.006 .006	<u>0</u>	%100 %100
60 M64 61 M65	Z	.006	.006	0	<u>%100</u> %100
61 <u>M65</u> 62 M66	7	.006	.006		<u>%100</u> %100
63 M67	Z	.006	.006	0	%100
64 M68	Z -	.006	.006	0	%100
65 M69	Z	.006	.006	0	%100
<u>66 M70 .</u>	<u>Z</u>	.006	.006	0	%100
<u>67 M71</u>	Z	.006	.006		<u>%100</u> %100
68 M72	7	.006	.006	0	%100 %100
69 M73 70 M74	200 7	.008	.008		×100
71 M75	Z	.006	.006	0	%100
72 M76	Z	.006	.006		%100
73 M77	Z	.006	.006		<u>%100</u>
74 M78	Z Z	.006	.006	. 0	%100
75 M79		.006	.006 .006	<u>0</u>	<u>%100</u> %100
76 M80 77 M81	Z	.006	.006	0	%100
77 M81 78 M82	Z	.006	.006	ា ស្ត្រីក ដាន់	%100 %100
79 <u>M83</u>	Z	.003	.003	Ō	%100
80 M84	Z	.003	.003	0	%100
81 M85	<u>Z</u>	0	0	0	%100
82 M86	<u> </u>	0	<u> </u>	<u>0</u>	%100
83 <u>M87</u>	<u>Z</u> 7 117	.003	.003 .003	O - C Services	<u>%100</u> %100
84 M88	Z	003	003	0	%100
85 M89 86 M90	Z	<u>o</u>	Ŭ,	<u> </u>	%100
87 M91	Z	.004	.004	0	%100
88 M92		.004	.004	0	%100
89 M93	Z	.004	.004	0	<u>%100</u>
<u>90 M94</u>	Z	.004	.004		%100
91 M95	<u> Z</u>	.004	.004	0 0 1 1	%100 %100
92 M96	Z Z	.004	.004	<u> </u>	<u>%100</u> %100
93 M97 94 M98	Z Z	.004	.004	<u> </u>	%100 %100
95 M99	Z	.004	.004	0	%100
96 M100		004		0	%100
97 M101	Z	.004	.004	0	%100

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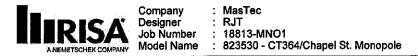


Monto Cr Digerio d	ted Double (<u>Direction</u>		Ford Magnikudoliki# E	. Start Location[ft,%]	End Location[ft.%]
Member La 98 M102	bel Direction Z		End Magnitude[k/ft.F .004		%100
99 M102	Z	.003	.003	0	%100
100 M104		.002	.002	strand real	%100
101 M105	7	.002	.002	Ō	%100
102 M106	$\overline{\mathbf{z}}$	003	.003	Ö 👘	%100
103 M107	Z	.003	.003	0	%100
104 M108	A State of the Z	.002	002	6 1 6 1	%100
105 M109	Z	.002	.002	0	%100
106 M110	Z		003	0	%100
107 M111	Z	.003	.003	0	%100
108 M112	<u>Z</u>	.002	.002 21	0	%100
109 M113	<u> </u>	.002	.002	0	%100
110 Mi114		.003	.003	0 11	%100
111 M115		.003	.003	0	%100
112 M116	Z - Z		.002	0	%100
113 M117	Z	.002	.002	0	%100
114 M118	L. R. Baster Z.	The second period and compared on a second prove that we have		0	%100
115 M25		.004	.004	%90	%100
<u>116 M27</u>	<u>z se z se z</u>	.004	.004	<u>%61</u>	%100
117 M29		.004	.004	<u>%90</u> %60	%100 %100
118 M32	<u> </u>	.004	.004		%100 %100
119 M1		.003	.003	0	%100
120 M2	<u> </u>	.001	.003	0	%100
121 <u>M3</u>	X X	.003	.003		%100
122 M4	X	.001	.001	0	%100 %100
123 M5 124 M6		.001	.004	0	%100
		.004	.004	0	%100
125 M7 126 M8	x x	.004	.004	0	%100
127 M9	X	.001	.001	0	%100
128 M10	X ···	.003	003	า กั 20	%100
129 M11	X	.003	.003	0	%100
130 M12		.001	001	, ő	%100
131 M13	X	.004	.004	Õ	%100
132 M15		.004	004	0 × 10	%100
133 M17	X	.004	.004	Ō	%100
134 M19	X X	.004	.004	Č	%100
135 M21	X	.002	.002	0	%100
136 M22	And the second	.002	.002	. 0	%100
137 M23	X	0	0	0	%100
138 M24	X X	0	O		%100
139 M25	X	.002	.002	0	%100
140 M26	X	.002	.002	0	%100
141 M27	X	.002	.002	0	%100
142 M29	X	.002	.002	0	%100
143 M30	X	.002	.002	0	%100
144 M31	<u> </u>		.002	0	%100
145 M32	X	.002	.002	0	<u>%100</u>
146 M33			.002	0	%10
147 M31A		.002	.002	0	%100
148 M32A	X	.002	.002	0	%100
149 <u>M33A</u>	X	.002	.002	0	%100
150 M34A		.002	002	0	%100
151 M35	X	.004	.004	0	<u>%100</u>
152 M36				0	%100
153 <u>M37</u>	X	.004	.004	0	<u>%100</u>
154 M38	<u>x</u>	.004		<u> </u>	<u>%100</u>

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	Member Label	Direction	Start Magnitude[k/ft	End Magnitude/k/ft.F	Start Location[ft.%]	End Location[ft,%]
155	Manber Laber	X	.004	.004	0	%100
156	M40	X	.004	.004	Ó	%100
157	M41	Х	.004	.004	0	%100
158	M42	×X	.004	.004	-0	%100
159	M43	X	.004	.004	0	<u>%100</u>
160	M44	X - X	.004	.004	0	%100
161	M45		.004	.004	0	%100
162	M46	X	.004	.004	<u> 0 - </u>	%100
163	<u>M47</u>	X	.004	.004	0	%100
164	<u>M48</u>	X	.004	.004	0	%100
165	<u>M49</u>		.004	.004	0	<u>%100</u>
166	<u>M50</u>		.004	.004	0	<u>%100</u> %100
<u>167</u> 168	<u>M51</u> M52	X X	.004	.004		%100
169	M53	X	.004	.004	0	%100
170	M55	x x	.004	.004	ະ ຈັງ 🖛 🚟	%100
171	M55	X	.004	.004	0	%100
172	M56	X	004	.004	e di di cara	%100
173	M57	X	.004	.004	Õ	%100
174	M58	X	.004	.004	0	%100
175	M59	X	.004	.004	0	%100
176	M60	X	.004		0	<u>%100</u>
177	M61	Х	.004	.004	0	%100
178	M62	X	.004	.004	0	%100
179	M63	XX	.004	.004	0	<u>%100</u>
180	M64	X	.004	.004	0	%100
181	M65	X	.004	.004	0	%100
182	M66	X	.004	.004	0	%100
183	<u>M67</u>	X	.004	.004	0	%100
184	M68	X	.004	.004	<u>i i o</u> i i i	%100
185	<u>M69</u>	X	.004 .004	.004	O N C	<u>%100</u> %100
186 187	<u>M70</u> M71	×	.004	.004	0	%100
188	W72	$\hat{\mathbf{x}}$.004	.004	1 <u>0</u> 1	%100
189	M73	X	.004	.004	0	%100
190	M74	x x	.004	.004	· · · · · · · · · · · ·	%100
191	M75	X	.004	.004	0	%100
192	M76	X		004	i <u>0</u>	······································
193	M77	X	.004	.004	0	%100
194	M78	X	.004	.004	0	%100
195	M79	Х	.004	.004	0	%100
196	M80	X	.004	.004	0	%100
197	M81	X	.004	.004	0	%100
198	M82			.004		%100
199	<u>M83</u>	X	.001	.001	0	%100
200	M84	X	.001	•	<u>8 - </u>	%100
201	M85	X	0			%100
	M86		· · · · · · · · · · · · · · · · · · ·		<u> </u>	<u>%100</u>
203	<u>M87</u>		.001	.001		<u>%100</u>
	M88				0	%100
205	<u>M89</u> M90	XX	0 0	0	0 0	<u>%100</u> %100
			.002	.002	0	%100 %100
207	<u>M91</u> M92	X	.002	.002		<u>%100</u> %100
<u>208</u> 209	<u>M92</u> M93	X	.002	.002	0	%100
209	M93	\$.002	.002	i (Öris vi	%100
211	M95	X	.002	.002	0	<u>%100</u>
	INIGO				<u> </u>	

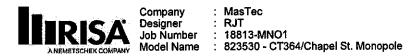


	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft,%]	End Location[ft,%]
212	M96	Х	, 002	.002	0	%100
213	M97	Х	.002	.002	0	%100
214	M98	X	.002	.002	. 0	%100
215	M99	X	.002	.002	0	%100
216	M100	X	.002	.002	.0	%100
217	M101	X	.002	.002	0	%100
218	M102	X 2 40	.002	.002	<u> </u>	%100
219	M103	X	.002	.002	0	%100
220	M104	X		.001	<u> </u>	%100
221	M105	<u> </u>	.001	.001	0	%100
222	M106	X	.002	.002	0	<u>%100</u>
223	M107	X	.002	.002	0	<u>%100</u>
224	M108	X	.001	.001	0	%100
225	M109	X	.001	.001	0	%100
226	M110	× X	.002	.002	<u> </u>	%100
227	M111	X	.002	.002	0	%100
228	M112	X	.001	.001	<u> </u>	%100
229	M113	X X	.001	.001	0	%100
230	M114	<u>X</u>	<u> </u>	.002	Ori and	%100
231	M115	X	.002	.002	0	%100
232	M116	X	.001		0	%100
233	M117	X	.001	.001	0	%100
234	M118	X	.002	.002	0	<u>%100</u>
235	M28	X	.002	.002	<u>%19.2</u>	<u>%100</u>
236	<u>M33</u>	X	.002		%90	%100

Member Distributed Loads (BLC 48 : BLC 1 Transient Area Loads)

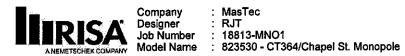
	Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft,F	Start Location[ft.%]	End Location[ft,%]
1	M1	Y	-,000318	005	0	2.06
2	M1 .	Y Y	005	- 006	2.06	4.119
3	M1	Ý	006	003	4.119	6.179
4	M1 3	Y	003	003	6.179	8.238
5	M1	Y	003	006	8,238	10.298
6	M1	Y	006	-:005	10.298	12.357
7	M1	Y	005	000318	12.357	14.417
8	M9 Meret	Ý	006	.009	5.009	6.01
9	M9	Y	009	01	6.01	7.012
10	M9	Y	01 +	01	7.012	8,014
11	M9	Y	01	007	8.014	9,016
12	M9	Ý	007	0004102	9,016	10.017
13	M10	Y	007	008	5.009	6.01
14	M10	Ý		009	- 6.01	7.012
15	M10	Y	009	009	7.012	8.014
16	MIQ	Y	-,009	007	8.014	9.016
17	M10	Y	007	003	9.016	10.017
18	M21	Y		003	.667	1.733
19	M21	Y	003	006	1.733	2.8
20	M21	Y	-,006	006	2.8	3.867
21	M21	Y	006	003	3.867	4.933
22	M21	Y	003		4,933	6
23	M109	Y	.002	.002	0	.083
24	M109	Y	.002	,000436	.083	#167
25	M109	Y	.000436	019	.167	.25
26	M109	Y	019	058	.25	.334
27	M110	Y	.0009358	004	0	.064
28	M110	Y Y	004	012	.064	.128

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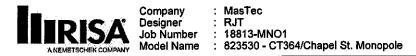
membe	I DISTINUTED FOR		<u> </u>		Chart Leastin (4.0/1	End Location[ft,%]
	Member Label	Direction	Start Magnitude[k/ft		Start Location[ft.%] 0	.064
29	<u>M111</u>	Y	.0009358 -004	004	.064	.128
30	M111					.083
31	<u>M112</u>	Y	.002	.002	0	.167
32	M112	Y Y	.002	.0004267		.25
33	M112	Y.	.0004267	019	.167	
34	M112	Y	019	058	.25	.334
35	<u>M2</u>	Y	000318	005	0	2.06
36	<u>M2</u>	<u>Y</u>	005	006	2.06	4.119
37	<u>M2</u>	Y .	006	003	<u>4.119</u>	6.179
38	M2	Y	003	<u> </u>	6.179	8.238
39	M2	<u>Y</u>	003	006	8.238	10.298
40	M2	· · Y	006	005	10:298	12.357
41	M2	Y	005	000318	12.357	<u>14.417</u>
42	M10	Y	0004102	007	0	1.002
43	M10	Y	007	01	1.002	2.003
44	M10	Y.	01	01	2.003	3.005
45	M10	Ý	01	009	3,005	4.007
46	M10	Ý	009	006	4.007	5.009
47	M12	Y	003	007	0	1.002
48	M12	Ý	007	009	1.002	2,003
49	M12	Y	009	009	2.003	3.005
50	M12	Section Y and the	009	008	3,005	4,007
51	M12	Y	008	007	4.007	5.009
52	M12 M23	V V			.667	1.733
53	M23	Y	003	006	1.733	2.8
54	M23	Y Y	-,006	-,006	2,8	3.867
	M23		006	003	3.867	4.933
55	M23	V V	003	003	4,933	6
564			.003	.002	0	.083
57	M113		.002	.000436		.003
<u>58</u>		V V	.000436	019	.167	.25
59	M113 M113	Y		068	.25	.23
60			Alleration and the second s			.064
61	<u>M114</u>	Y	.0009358	004 012	0	.004
62	M114	A CONTRACTOR	-,004			
63	<u>M115</u>	<u>Y</u>	.0009358	004	0	.064
64	M115	HALL Y HOLD	004	012	.064	
65	M116	Y	.002	.002	0	.083
66	M116	Y	.002	.0004267	.083	.167
67	M <u>116</u>	Y	.0004267	019	.167	.25
68	M116	Y	019	058	.25	.334
69	M3		000318	005	0	2.06
	M3	Y	-,005	006	2.06	4.119
71	<u>M3</u>	Y	006	003	4.119	6.179
72		Y .	-,003	003	6,179	8.238
73	<u>M3</u>	Y	003	006	<u>8.238</u>	10.298
74	<u>M3</u>	Y	-:006		10.298	12.357
75	M3	Y	005	<u>000318</u>	12.357	14.417
	M11	Y	006	008	5.009	6.01
77	M11	Y	-,008	009	<u>6.01</u>	7.012
	M11	Y	009	008	7.012	8.014
79	M11	Y	008	007	8.014	9.016
Lade The Cally Carden ?!	M11	Y Y	007	005	9.016	10.017
81	M12	Y	007	008	5.009	6.01
	M12	Note Y	008	009	6,01	7.012
83	M12	Υ	009	01	7.012	8.014
84	M12	Y	01	2007		9.016
85	M12	Y	007	0006361	9.016	10.017
			1001			Page 57

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Member Label			End Magnitude[k/ft.F		End Location[ft.%]
86 M22	Y The	001	003	.667	1.733
87 M22	Y	003	007	1.733	2.8
88 M22	Y Y	- 007	006	2.8	3.867
89 <u>M22</u>	<u> </u>	006	003	3.867	4.933
90 M22	Y .	003	001	4.933	
<u>91 M103</u>	Y N	.0009358	004	.064	.064
92 Miles		004	-,012 .002	0	.083
93 M104		.002 .002	.002		.167
94 M104 95 M104		.0004267	019	.167	.25
95 M104 96 M104		019	019	.25	.23
97 M117	V	.002	.002	0	.083
98 M117	× ·	.002	.000436	1.083	.167
99 M117		.000436	019	.167	.25
100 M117	y y		058	.25	.334
101 M118	Y	.0009358	004	0	.064
102 M118	19 Y	- 004	012	.064	.128
103 M4	Y	000318	005	0	2.06
104 M4	Ý	4.005	006	2.06	4,119
105 M4	Y	006	003	4.119	6.179
106 M4	Y	- 003	003 1	6:179	8.238
107 M4	Y	003	006	8.238	10.298
108 M4	Y	006	005	10.298	12.357
109 M4	Y	005	-,000318	12,357	14.417
110 M9.	<u> </u>	003	007	0	1.002
111 M9	Y	007	009	1.002	2.003
112 M9	<u> </u>	009	009	2:003	3.005
113 M9	Y	009	008	3.005	4.007
114 M9	Ý	-,008	007	4.007	5.009
115 M11	Ý	0004102	007	0	1.002
116 M11	<u> </u>	007	.01	1,002	2.003
117 M11	Y	01	01	2.003	3.005
118 M11	Y Y	01		3,005	4.007
119 M11	Y	009	006 003	4.007	5.009
120 M24		001	006	1.733	2.8
121 <u>M24</u> 122 M24	V V	003 006	008	2.8	3.867
122 M24 123 M24		006	003	3.867	4.933
123 W124	I V	003	005	4.933	6
125 <u>M105</u>	V	.002	.002	0	.083
126 M105	Y III	002	.000436	.083	.167
127 M105	Y	.000436	019	.167	.25
128 M105		019	058	-⊪	.334
129 M106	Y	.0009358	004	0	.064
130 M106	Ý	004	- 012		128
131 M107	Y	.0009358	004	0	.064
132 M107	Y S	004	012	064	.128 🚊
133 M108	Y	.002	.002	0	.083
134 M108	Ý	,002	.0004267	.083	. 167
135 M108	Y	.0004267	019	.167	.25
136 M108	Ŷ	+.019	A STATE OF A	.25	334
137 M1	Y	000159	-4.84e-5		.721
138 M1	Ŷ	-4.84e-5	000319	.721	1.442
139 M1	Y	000319	000319	1.442	2.162
140 M1	Ŷ	000319	6.914e-6	2,162	2,883
141 M4	Y	<u>6.914e-6</u>	000319	11.533	12.254
<u>142 M4</u>	· Y	<u>000319</u>	- 000319	12.254	12.975

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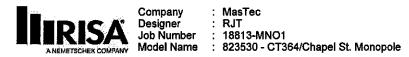
Member Label	Direction	Start Magnitude[k/ft	End Magnitude[k/ft.F	Start Location[ft.%]	End Location[ft.%]
143 M4	Ý	000319	-4.84e-5	12.975	13.696
144 M4	Y	-4.84e-5	000159	13.696	14.417
145 M9	<u> </u>	8.659e-19	004	4.007	4.408
146 M9.	Y Y	004	007 007	4.408 4.808	4 808 5.209
147 <u>M9</u> 148 M9	Y .	007	+.004	5.209	5.61
149 M9	V	004	8.659e-19	5.61	6.01
150 MI07	Ý	-,002	002	0	.128
151 M108	Y	005	005	0	.334
152 M109	Y	005	005	<u>0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1</u>	.334
153 M110	Y	002	002	0	.128
154 M1	<u> </u>	6.914e-6	0003189	11.533	12:254
1 <u>55 M1</u>	Y Y	0003189	0003189	<u>12.254</u> 12.975	12.975 13.696
156 <u>M1</u> 157 _M1	I V	0003189 -4.84e-5	-4.84e-5 000159	13.696	14.417
157 M1 158 M2	V III	000159	-4.84e-5	0 3 3	721
159 M2	Y	-4.84e-5	0003189	.721	1.442
160 M2	Ý	0003189	-,0003189	1,442	2.162
161 M2	Y	0003189	6.914e-6	2.162	2.883
162 M10	Y	-8.659e-19	- 004	4,007	4.408
163 M10		004	007	4.408	4.808
164 M10	<u> </u>	007	- 007	4,808	5,209
165 M10 166 M10	Y	007	004 -8.659e-19	5.209 5.61	5.61 6.01
166 M10 167 M111		004	002	0	.128
168 M112	· Y	002	002	i si se i o se i	
169 M1 <u>13</u>	Y	005	005	0	.334
170 M114	Ý	-,002	=.002	0	.128
171 M2	Y	6.914e-6	0003189	11.533	12.254
172 M2	k Y and	0003189	0003189	12.254	12.975
173 <u>M2</u>	l Y	0003189	-4.84e-5	12.975	13.696
174 W2	Ý	-4:846-5	000159 -4.84e-5	<u>13.696</u> 0	<u>14:417</u> .721
175 M3 176 M3	I I	000159 -4.84e-5	0003189	721	1.442
177 M3	Y	0003189	0003189	1.442	2.162
178 M3	Ý	-0003189	6.914e-6	2.162	2.883
179 M12	Y	0	004	4.007	4,408
180 M12	Y	004	007	4.408	4.808
181 M12	<u>Y</u>	-,007	007	4.808	5.209
182 M12	<u> </u>	007	004	5.209	5.61
183 M12	Y	004 002	0 - 002	<u>5.61</u>	6.01
184 M115 185 M116		002	005	0	.334
185 M116 186 M117	Ý	005	005		.334
187 M118	Y	002	002	0	.128
188 M3	Ý	6.914e-6	0003189	11.533	12,254
189 M3	Y	0003189	0003189	12.254	12.975
190 M3	<u> </u>	<u>0003189</u>	-4.84e-5	12.975	13.696
191 M3		-4.84e-5	<u>000159</u>	13.696	14.417
192 M4	Y I	000159	-4.84e-5	704	721
193 M4	Y Y	-4.84e-5 0003189	0003189 0003189	.721	1.442 2.162
194 M4 1		0003189	6.914e-6	2.162	2.883
195 M4 196 M11	Y	0003169	004	4,007	4,408
197 M <u>11</u>	Y	004	007	4.408	4.808
198 M11	Ý	-,007	- 007	4,808	5.209
199 M11	Y	007	004	5.209	5.61
		1022520 Undet			Page 50

	Member Label	Direction	Start Magnitude[k/ft	End Magnitude/k/ft.F	Start Location[ft,%]	End Location[ft,%]
200	M11	Y.	-:004	0	5.61	6.01
201	M103	Y	002	002	0	.128
202	M104	Ý	005	005	0	.334
203	M105	Y	005	005	00	.334
204	M106	Y	- 002	002	0	.128

Member Distributed Loads (BLC 49 : BLC 2 Transient Area Loads)

MGIII	iper Distributed Loa	-		ent Area Luaus		
	Member Label	Direction		End Magnitude[k/ft.F		End Location[ft.%]
	<u>M1</u>	Y	0005251	009	0	2.06
2	M1 ****	Y	009	011	2.06	4.119
3	<u>M1</u>	<u> </u>	011	005	<u>4.119</u>	6.179
4	M1	Y ≤ 1	005	-,005	6.179	8.238
5	M1	Y	005	011	8.238	10.298
6	M1	Y	- 011	009	10.298	12.357
7	M1	Y	009	0005251	12.357	14.417
8	M9	Y	011	- 014	5,009	6.01
9	M9	Y	014	016	6.01	7.012
10		Ý.	016	016	7:012	8.014
11	M9	Y	016	011	8.014	9.016
12	M9 + 1	Y Y	011	0006774	9.016	10.017
13	M10	Y	011	014	5.009	6.01
The set of a ball of the set of the	M10	× × × ×		6 STA - 015	6.01	7.012
15	M10	Y	015	015	7.012	8.014
16		Ý N D	015	-012	8.014	9.016
and the second se	M10	Y	012	005	9.016	10.017
17	M10 M21	Y	012	005	.667	1.733
1217		Y		01	1.733	2.8
19	M21	Y	<u>005</u> 01	01	2.8	3.867
20	M21	1.1.1 The state of			3.867	4.933
21	<u>M21</u>	Y Y	01	005	4,933	4.955
22		Y	005			.083
23	M109	Y Y	.004	.003	0	
24	M109	Y	.003	00072	.083	.167
25	<u>M109</u>	<u> </u>	.00072	032	. <u>167</u>	.25 .334
26	M109	Y	-,032	095	25	
27	<u>M110</u>	<u> </u>	.002	006	0	.064
28	M110	Y	006	•.02	.064	.128
29	M111	Y	.002	006		.064
30	M111	Y	006	02	.064	.128
31	M112	Y	.004	.003	0	.083
32	M112	Y	.003	.0007046	.083	.167
33	M112	Υ	.0007046	032	.167	.25
34	M112	$\mathbf{Y} \in \mathbf{Y}$	- 032	-:096	.25	.334
35	M2	Y	0005251	009	0	2.06
36	M2	Ŷ	009	=.011	2.06	4,119
37	M2	Y	011	005	4.119	6.179
38	M2	Ý	-,005	005	6.179	8.238
39	M2	Y	005	011	8.238	10.298
40	M2	Ý	0111	- 009	10.298	12.357
41	M2	Y	009	0005251	12.357	14.417
42	M10	ý -	-,0006774	011	0	1 002
43	M10		011	016	1.002	2.003
43	M10	Ý	016	016	2.003	3.005
			016	014	3.005	4.007
45	M10	Ý	016	+.014	4,007	4.007
46	M10			012	4,007 0	1.002
47	<u>M12</u>	l Y	005	012	1.002	2 003
- 48	M12	Press X	-:012	CIU		Z.UU3

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June 7, 2019 7:54 PM Checked By:____

Member Distributed Loads (BLC 49 : BLC 2 Transient Area Loads) (Continued)

	Member Label	Direction	Start Magnitude/k/ft	End Magnitude[k/ft,F	Start Location[ft.%]	End Location[ft.%]
49	M12	Y	015	015	2.003	3.005
50	M12	Y	015	014	3.005	4.007
51	M12	Y	014	011	4.007	5.009
52	M23	Y	-:002	005	.667	1.733
53	M23	National Warms And State States and a second s	005	01	1.733	2.8
54	M23	<u>⊫ +</u> +Y	01	<u>÷01</u> <u>к</u> ре	2.8	3.867
55	<u>M23</u>	Y	01	005	3.867	4.933
56	M23	Y	005	002	4,983	6
_57 _58	<u>M113</u> M113	Y	.004	.003 // 00072	0 •083	.083
59	M113		.00072	032	.167	.25
60	M113		-,032	032	25	.334
61	M114		.002	006	0	.064
62	M114	Y	006	02	064	128
63	M115	Y	.002	006	0	.064
64		Y	006		.064	128
65	M116	Y	.004	.003	0	.083
66	M116	Y	.003	.0007046	.083	167
67	M116	<u>Y</u>	.0007046	032	.167	.25
68	M116	Ŷ	-:032	096	.25	334
69	<u>M3</u>	Y	0005251	009	0	2.06
70	M3	Y	-,009	011	2,06	4.119
71			011	005	4.119	6.179
72	M3	arensar Yestaan	005	005	6.179	8,238
73	<u>M3</u>	Y	005	011	8.238	10.298
74	M3.	Y	0111	009	10.298	12.357
75	<u>M3</u>	Y New Y	009 011	0005251	12.357	14.417
76	Mit	Y		01 <u>3</u> 015	<u>5.009</u> 6.01	<u>6,01</u> 7.012
77	M11 M11	I VIEW	<u>013</u> 015	013	7,012	8.014
79	M11	Y	013	011	8.014	9.016
80	M11	Ý	011.1.2.42	009	9,016	10.017
81	M12	Y	011	014	5.009	6.01
82	M12	Ý	-014	016	6.01	7.012
83	M12	Y	016	-,016	7.012	8.014
84	M12	Y	016	- 011	8.014	9.016
85	M12	Y	011	001	9.016	10.017
86	M22	Y LI	002	005	.667	1.733
87	<u>M22</u>	Y	<u>005</u>	011	1.733	2.8
-88	<u>M22</u>	Y	-,011	011	2.8	3.867
89	M22	Y	<u>-,011</u>	005	3.867	4.933
90	M22	Y 2	005	002	4.933	6
91	<u>M103</u>	Y T Y	.002	006	0	.064
92	M103	The Children of a share of the second s	006	- 02	.064	.128
93	M104	Y	.004 .003	.003 .0007046	0 	.083 .167
94 95	<u>M104</u> M104	Y	.0007046	032	.167	.25
96	M104	Y N	032	-,096	.167	.334
97	M104	V	.004	.003	0	.083
98	M117	NY I	.003	.00072	.083	.167
99	M117	Y	.00072	032	.167	.25
100	M117	· · · · · · · ·	032	- 095	.25	334
101	M118	Ý	.002	006	0	.064
	M118	Y 25	006	02	1.064	.128
103	M4	Y	0005251	009	0	2.06
104	. M4	Y I	009	011	2.06	4.119
105	M4	Y	011	005	4.119	6.179
				4 0001		

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Member Label	Direction	Start Magnitudelk/ft	End Magnitude[k/ft.F	Start Location[ft,%]	End Location[ft,%]
106 M4	Y	005	005	6.179	8.238
107 M4	Y	005	011	8.238	10.298
108 M4	Ý	-,011	009	10.298	12,357
109 M4	Y	009	0005251	12.357	14.417
110 M9	Ŷ	005	012	0	1,002
111 M9	Y	012	015	1.002	2.003
112 M9	Ý	015	<u> </u>	2.003	3,005
113 M9	Y	015	014	3.005	4.007
114 M9	* Y	01.4	011	4.007	5.009
115 M11	Y	0006774	011	0	1.002
116 M11	Y	-,011	≓	1.002	2.003
117 M11	Y	016	<u>016</u>	2.003	3.005
118 M11	Y	-,016	-,014	3.005	4.007
119 M11		014	011	4.007	5.009
120 M24	Y we	-,002	.005	.667.	1.738
121 M24	Y	005	01	1.733	2.8
122 M24	× ×	01	01	2.8	3:867
123 <u>M24</u>	Ý	01	005	3.867	4.933
124 M24	Y V	005		4.933	.083
125 M105	Y	.004	.003	0	.083
126 M105	Y	.003	032	.167	.25
127 M105	Y	<u>.00072</u> 032	032	25	.23
128 M105		.002	095	0	.064
129 M106	T National Anna State	-:002	008	.064	.128
130 M106	V	.002	006	0	.064
131 M107 132 M107	V V	006	000	.064	.128
133 M1 <u>08</u>		.004	.003	0	.083
134 Mil <u>08</u>	× • • • •	.003	.0007046		167
135 M108	V	.0007046	032	.167	.25
136 M108	i i Gi 🍸 Statisti	032	096	.25	334
137 M1		0002626	-7.992e-5	0	.721
138 W1	in Y in the	-7.992e-5	0005268	721	1,442
139 M1	Y	0005268	0005268	1.442	2.162
140 M1	Ý 🕴	0005268	1.142e-5	2,162	2.883
141 M4	Y	1.142e-5	0005268	11.533	12.254
142 M4	Y	0005268	0005268	12.254	12.975
143 M4	Y	0005268	-7.992e-5	12.975	13,696
144 M4	Y	-7.992e-5	-:0002626	13,696	14,417
145 M9	Y	<u>1.732e-18</u>	006	4.007	4.408
146 M9	\mathbf{Y}	- 006	<u>= 011</u>	4.408	4,808
147 M9	Y	011	011	4.808	5.209
148 M9 M9	Y		006		
149 <u>M9</u>	<u> </u>	006	1.732e-18	5.61	6.01
150 M107	Y	004		0, 1	.128
151 M108	Y	009	009	0	.334
152 M109	Y		2,009	0	.334
153 <u>M110</u>	Y	004	004	0	.128
<u>154</u> <u>M1</u>	Ý	1,142e-5		11.533	12.254
155 <u>M1</u>	Y	0005267	0005267	12.254	12.975
156 M1	Y	- 0005267		12.975	13.696
157 <u>M1</u>	Y	<u>-7.992e-5</u>	0002626	13.696	14,417
158 M2	Ŷ	0002626	-7.992e-5	704	.721
159 <u>M2</u>	Y	-7.992e-5	0005267	.721	1.442
<u>160 M2</u>	<u> </u>	0005267	0005267	1.442	2.162
161 <u>M2</u>	Y	0005267	<u>1.142e-5</u>	2.162	2.883
162 <u>M10</u>	Y	8.659e-19		4.007	4.408

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	Member Label	Direction		End Magnitude[k/ft,F	Start Location[ft.%]	End Location[ft.%] 4.808
163	<u>M10</u>	<u>Y</u>	006	011	<u>4.408</u> 4.808	5.209
164	M10	Ŷ		011	5.209	5.61
165	M10		011	006	5.209	<u></u>
166	<u>M10</u>		006	8.659e-19		.128
167	M111	Y	004	004 009	0	334
168	M112	Y	009			.334
169	M113	Y	009	009	0	
170		Y	004	004	11.533	12.254
171	<u>M2</u>	Y	1.142e-5	0005267	12.254	12.975
172	M2	Station of Yoshical	- 0005267	-,0005267	12.975	13.696
173	<u>M2</u>	Y	0005267	-7.992e-5	13,696	14,417
174	M2	Y	-7.992e-5	0002626	0090	.721
175	M3	Ý	0002626	-7.992e-5	721 1	1.442
176	M3	Y	-7.992e-5	0005267	1.442	2.162
177	M3	Y CARGO C	-,0005267	0005267	2.162	2.883
178		N REAL PARTY	- 0005267	1.142e-5		4.408
179	<u>M12</u>	Y	0	006 011	4.007	4.808
180	M12	Y	006		4.808	5.209
181	M12	Y	011	<u>011</u> 006	5.209	5.61
182		Y Y	-011	AND ADDRESS OF A DECK	5.61	6.01
183	<u>M12</u>	Y Y	006	0	0.01	.128
<u>184</u>		A CONTRACTOR OF A CONTRACT OF A CONTRACT. A CONTRACT OF A	004		0	.334
185	M116	Y	009	009	0	.334
186	<u>M117 </u>	With Y Lets	009		0	.128
187	<u>M118</u>		004	004	11.533	12.254
188	MB	Y BURNER	1.142e-5	AN AS A SHOW A SHOW AND A	12.254	12.975
189	<u>M3</u>	Y	0005267	0005267 -7.992e-5	12.975	13.696
190		NAME	0005267		13.696	14.417
191	<u>M3</u>	Y	-7.992e-5	0002626 -7.992e-5	0	721
192				0005267	.721	1.442
193	<u>M4</u>	Y Y	-7.992e-5 0005267	0005267	1.442	2,162
194	M4 *	V V	0005267	1.142e-5	2.162	2.883
195	<u>M4</u>	Y Y	0	006	4.007	4.408
196	M11 《 编编 · 2		006	011	4,408	4.808
197	M11	L T	006	<u>011</u> ₩011 ₩	4.808	5 209
198	M11		011	006	5.209	5.61
199	<u>M11</u>	Y	011	000	5.61	3.01
200	M11	Y.		004	0	.128
201	M103	Y V	004	004		334
202				009	0	.334
203	M105		009	009	U O	128
204	M106	NY STATE	mUU4		1 × • • •	

Member Area Loads (BLC 1 : Dead)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[ksf]
1	N42	N69	N68	N41	Y	Two Way	005
2	N71	N45	N46	N73	Y	Two Way	005
3	N70	N44	N43	N67	Υ	Two Way	005
4	N74	N48	N47	N72	Y I	Two Way	005
5	N68	N72	N47	N41	Y	Two Way	005
6	N42	N45	N71	N69	Ŷ	Two Way	005
7	N46	N44	N70	N73	Y	Two Way	005
8	N48	N43	N67	N74	<u> </u>	Two Way	-,005

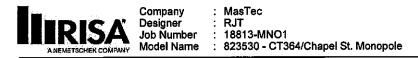
Member Area Loads (BLC 2 : Ice Dead)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[ksf]
1	N42	N69	N68	N41	Y	Two Way	008
2	N7.1	N45	N46	N73	Y	Two Way	008
3	N70	N44	N43	N67	Y	Two Way	008
4	N74	N48	N47	N72	Y	Two Way	008
5	N68	N72	N47	N41	Y	Two Way_	- 008
6	N42	N45	N71	N69	Y -	Two Way	- 008
7	N46	N44	N70	N73	Y	Two Way	008
8	N48	N43	• N67	N74	<u> </u>	Two Way	008

Basic Load Cases

BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut.	.Area(Me.	Surface(
1 Dead	None		-1			19		8	
2 Ice Dead	None	C. Martin	Ren 1. anti-			19	118	8	
3 Full Wind Antenna (0 Deg)	None					16			
4 Full Wind Antenna (30 Deg)	None		a a stati			41	- 生態 5		
5 Full Wind Antenna (60 Deg)	None					41			
6 Full Wind Antenna (90 Dec)	None	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	16. j. j.		$\mathbf{P}_{\mathbf{x}}$ is \mathbf{S}	41			
7 Full Wind Antenna (120 Deg)	None					41	C. M. C. Phillip and C. C.		
8 Full Wind Antenna (150 Deg)	None	刘叔云:				41			
9 Full Wind Members (0 Deg)	None						52		1
10 Full Wind Members (30 Deg)	None						52		
11 Full Wind Members (60 Deg)	None		and the second se			Automotics (1998)	52	olorite.com	Antibut for strangering and
12 Full Wind Members (90 Deg)			and first	Maile in A			52	-8-14	Research 1
13 Full Wind Members (120 Deg)	None		and the second	1 A 4 5 5 5 4 5 50 50 50 10 10 10 10 10 10 10 10 10 10 10 10 10	Law Sec. C. M. & Merrid		52	ALC: N. P. K. P. K	analisia analisia ang sa
14 Full Wind Members (150 Deg)	None	1. 19 3. 10 S. 10			周期的 二十		52		
15 Ice Wind Antenna (0 Deg)	None	THE POST PROPERTY POST		la, norma destrictioners and		16	e www.eukerensers.edeter		Anno and a state with
16 Vind Antenna (30 Deg)			in the second			41		Line II.	
17 Ice Wind Antenna (60 Deg)	None	Station and the state base	3365年9月25日,在三月1日	1000		41			·····································
18 Ice Wind Antenna (90 Deg)	None		<u></u>		L R D	41	Nale of	582	
19 Ice Wind Antenna (120 Deg)	None	String by Spinistering & String				41			试验的新生 动的注意
20 Ice Wind Antenna (150 Deg)	None					41	000	19 av	
21 Ice Wind Members (0 Deg)	None		Start And WELL COUNTY	12			236		
22 Ice Wind Members (30 Deg)	None					要自定主要的	236		
23 Ice Wind Members (60 Deg)	None		1000-1000-1400-1400-1400-1400-1400-1400	10.55		148.74.55 146 14	236		
24 Ice Wind Members (90 Deg)	None	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1		<u> </u>				200 A 7 10 10 10 10 10 10 10 10 10 10 10 10 10	Construction of the state
25 Ice Wind Members (120 Deg)	None		The second s				236		
26 Ice Wind Members (150 Deg)	None	States and the second			62040	19	230		
27 Seismic Antenna (0 Deg)	None	www.ee.ar.c		- 19 3		19		K 18	Sana di d
28 Seismic Antenna (90 Deg)	None		04	10 A		19			等合金的關聯網絡合計
29 Seismic Members (0 Dea)	None	.05	<u>04</u>	1 086	1. 11 1				
	None	.086	04	05	12 342 34	· 通行		STREET, STREET	多4684566899862-10
31 Seismic Members (60 Deg)	None None	1	04 M-04	-6.095e					
32 Seismic Members (90 Deg)	None	.086	04	.05				Service of the servic	BULL NEW STREET
33 Seismic Members (120 Deg) 34 Seismic Members (150 Deg)	None	.065	04			Sec. 1	195 - L.Y.	Mandariga Julian Lin	Heater in
34 Seismic Members (150 Deg) 35 Seismic Members (180 Deg)	None	1.219e-17	04	.1	6. 20. 60 12	Service and			
36 Seismic Members (100 Deg)	None	05	04	And a second		Store	111 - S.S.		
37 Seismic Members (240 Deg)	None	086	04	.05		11114 (J.)	E SECTION DUPLICATION	, a from a delan consultante en este	
38 Seismic Members (240 Deg)	None		04	1.829e-17		37			
39 Seismic Members (300 Deg)	None	086	04	05	ARACHER STREET, MICH.		R. Charlengerschaftengersch	a sum interest of the last	international and a subsection of the subsection
40 Seismic Members (300 Deg)	None	05	04	-,086	18441			2012012-001	
41 Seismic Vertical Antennas	None				1-12-1 <u>2-129-12-129</u> 2	19		ALCOLOGIES MARINA	1.4.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1
41 Seismic Vertical Antennas 42 Man 1 (500 bs)	None	1. - 1. 1. 1. 1. 1.			8 831 1210				
43 Man 2 (500 lbs)	None		na tana kata kata kata kata kata kata ka		1		- <u>-</u>	1. WERNESS LADING OF	ANI
44 Man 3 (500 lbs)	None		405		8 / A 😂			1 - 11 - 11 - 11 - 11 - 11 - 11 - 11 -	
		14.	國際的政策的目的	100 State St	<u>王 福 浩浩</u>	Lingspor 機能行 的行		Transference: Andre Ale	St. (211), 1098(200). 1

RISA-3D Version 17.0.2 [C:\...\...\...\823530 - Updated.R3D]



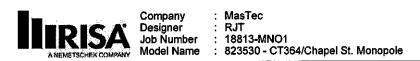
Basic Load Cases (Continued)

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut	.Area(Me.,	Surface(
45	Man 4 (250 lbs)	None			•	1				
46	Man 5 (250 lbs)	None								a and the second second
47	Man 6 (250 lbs)	None				1				
48	BLC 1 Transient Area Loads	None				$1 \leq i_{\rm eff} < i_{\rm eff}$		204		
49	BLC 2 Transient Area Loads	None						204		

Load Combinations

	Descriptio			SR	BLC	Fact.	.,BLC	Fact.	BLC	Fact.	BLC	Fact.	BLC	Fact	BLC	Fact	BLC	Fact.,	BLC	Fact	BLC	Fact	BLC	Fact
1	1.4D	Yes		8-3,53,600	1	1.4	3	1	9	1				影响影响				NEX EX					医黄疸	
3	1.2D + 1.0 1.2D + 1.0				1	1.2	4	1	10	1			100 C			980						and the second second		
	1.2D + 1.0			1.24	1	1.2	5		11			- 41 41 	2 (2 ₂ 3)		din e				\$					
5	1.2D + 1.0				1	1.2	6	1	12	1														
6	1.2D + 1.0				1	1.2			56212 0.7056	Contra and a capacit	2 			的感情				ê lat		<u>.</u>				
7	1.2D + 1.0				1	1.2	8	1	14	1	- - 2010713	and the second secon		1.			S. A. D.					41X - 244 44	8	an factor
	1,2D + 1,0 1,2D + 1,0					1.2	and a second second	-1	9	-1						C POLIN	臺灣道				i ya sa sha sa	Selami si mat Selami si mat	t szereletetetetetetetetetetetetetetetetetet	
9	1.2D + 1.0	the state of the second state of the			1	1.2	4	-1	10 51 m	-1		- <u>41</u>											1. 海道	in the second
11	1.2D + 1.0	CAR COMPANY	210 21727		1	1.2	6	<u>-1</u>	12	-1	8		96[325]()		Post Service S				10. 940468.	1.2019-0807-Cr.	D. CHORE		******	1000 100 100
Control of Chercology	1.2D + 1.0	CALLER TOPPOLITION A	NOT THE R.	14		1.2	7	-1	13		21 ⁻¹ -1		変勢			- Sa								離初
13	1.2D + 1.0	Yes	Y		1	1.2	8	-1	14	-1_					Values All' 1	a sumaissi 7		· · · · · · · · · · · · · · · · · · ·		Land Arriston and	2121246	ermittenen som	10112	Shitter
100 COL 100 CO	1.2D + 1.0	State and state at the	1010-0007			1.2	2	1态	15		21	1									(Andrews)			
	1.2D + 1.0				1	1.2	2	1	16	1	22	1	500 State			S 102 - 1	1			i Alf				27. XX
	1.2D+1.0 1.2D+1.0				//编辑 1	1.2	2	99188 1	<u>利</u> 加 18	2016) 1	<u>23</u> 24	然 1 案 1	新經濟									200		
	1,2D + 1.0	and Completes	Same and man		¥4	1.2	2 Z		19		<u>24</u> 25	廖 1餘	id di					的现法					1	1973 (L.
	1.2D + 1.0		10.000		10,621,910	1.2	2	1	20	1	26	1	C. WAR		Sport of California		100000004-0	contraction and a	entes plur inxe	59623435 (1971 <u>3</u> 8	aaxaalibada:	CANGE		CS " BARGERAGE
	1.2D + 1.0				1	1.2	2	71	15	14	21	321			45,579					Here				
21	1.2D + 1.0	Yes	Y	L	1_	1.2	2	1	16	-1	22	-1				2.8 W. 101 B		VERY AURIL		Pe Silve of 11800	NAURENNA PT			S. D
	1.2D + 1.0			100		1.2	2		17		23	-1		- 4 C	884					$\frac{1}{9.9}$		da.		
	1.2D + 1.0			1.508294538-0	1	1.2	2	1	18	-1	24	-1			s é sit	治清護道	6.882 6			193	Sec.		12. N	488 ⁽
	1.2D + 1.0			机制	調調	1.2	2			-1	<u>25</u> 26	-1	adin 18				18 HZ-		- <u>1</u>					
	1.2D + 1.0 1.2D + 1.5				1 1878	1.2	2	1	20	-1		1.5			11A.b.R			1			1920	影响新闻		
	1.2D + 1.5	a conversion du	_		<u>1</u>	1.2	4	.066		.066		1.5	17.80 E 90	SQUEELS.	27 Y 1999	Negroviški di	: 5. 200502 mil		9677268225		828 <u>95. 'I.'</u>	9-1-000 - 7 BC 5-	8947"1.0d	1000
A DOMESTIC ADDRESS OF ADDRESS OF ADDRESS ADDRES	1.2D + 1.5	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ALC: UNKERS	1		1.2	5	066	- 3446 - 14 - Caulon	2. Subabalation and			7:07					5					潮行的	
	1.2D + 1.5		-	Verselier s	1	1.2	6	.066		.066	42	1.5												
30	1.2D + 1.5	Yes	Y		1	1.2	-7					1.5					31			S. 1 In Space				
	1.2D + 1.5				1	1.2	8	.066				1.5	electron de	and the second states	1015101080	-1.088-553X	11100000144		11.1-2014.1		Konger (Y. C.
12.10	1.2D+1.5					12		And the part of th	1111	066			8(d)	a butic		a nişi		1 3 7			et ia			
	1.2D + 1.5 1.2D + 1.5	27.5 XXX0000 'A	Advest Advenue		1 1	1.2	4	066		066 066		1.5	1.1946		11 1 1		5 8 3	KI LE						See Sugar
	1.2D + 1.5	10.24 00X20 01	1		1151 1	1.2	6	066		066		1.5		现在记录 中		8. 201 - Al 2	1-5%器約研				TREASURY, S. S.	lin'n' vinner		an a
	1.2D + 1.5		· · · · · · · · · · · · · · · · · · ·			1.2	7	066								13		l.						
37	1.2D + 1.5				1	1.2	8	066		066	r	1.5												
	1.2D + 1.5	., Yes	Ŷ	1. s. s.		1.2	3	.066		.066	43	1.5						See.	較強					
	1.2D + 1.5	THE REAL PROPERTY.	272 N 100000 1	232.000.00	1	1.2	4	.066		.066	1000	1.5	S. S. C. C.	A CARGO IN		8.78800 ⁻¹ 11/4	10. (80.00-1%)		該応告が	<u></u>	888500 V.	1. Carlower	** ***	
- management	1.2D + 1.5		1	ic.		1.2	5	.066	A DESCRIPTION OF THE OWNER OF THE	.066								St.5 11.		影神波				
	1.2D + 1.5		100.000.000	1000	1	1.2	6	.066	CAL NO.LLO	.066	in the second	1.5		國際運行的	A.									- H
4 <u>2</u> 43	1.2D + 1.5 1.2D + 1.5			Sink:	1	1.2	<u>7</u> 8	.066		.066		1.5					938E.(\$	國家医療論	W EL		1. 12 2 2 2 2 2 2		编行公社	BE STREET
	1.2D + 1.5		L		6 2 43	1.2	3	the second is the	2000000000	A PARAMANANA	GRAD, DRUCT P	1.5	i të sh		ę				1	(k) generativ			Setende	
	1.2D + 1.5	the second s	<u> </u>	8.943 (A.B.)	1	1.2	4	066		066		1.5		Beheltudi [1978]		2-30000000	12: 00004'S		(mill (1994))	per artistelles	REAL STORY	<u></u> dr/kk	egx.up erfelt	
A NUMBER OF A DESCRIPTION OF A DESCRIPTI	1.2D + 1.5	and a state of the second	14.138.14.1			1.2	5			066							1	1						l and - is
	1.2D + 1.5	All a state of the state of the	Phone		1	1.2	6	066		066														

RISA-3D Version 17.0.2



Load Combinations (Continued)

			- 4 - 51	0.5-1			r.				Faab		East		East
Description SolPDSRBLC Fact. 48 12D + 15. Yes Y 1 1 12	BLC Fact.	BLUI			BLU F	aciBLU	Fact	BLU	ract		<u>гасі</u>		<u>гасі</u>		
49 1.2D + 1.5Yes Y 1 1.2	8066		066 4						STREE YANK	ANHER AND	17 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Malax 14	N DE NORM	9885-1.1985	
50 12D + 1.5. Yes Y 1 1 1.2			066 4			12			4.473		ŝ	in a participation of the second s			5
51 1.2D + 1.5Yes Y 1 1.22			.066 4			AND AND AN AND AND AND A	1.09.0002.62.007.0	96 49-28.°		3001-011-11	57.67.990 (P)	u asry and	STANDAU P		
52 1.2D + 1.5. Yes Y 1 1 1.2			066 4			NAR MOR	1.31	10.84	Han	2.3		6626			
53 1.2D + 1.5 Yes Y 1 1.2	6 .066		066 4			0.000 m (2.001-)	255 2. 4		L9981.2.5	Stir Laberatory of	10000-1700-	and the second	4-1-051-05-5	· 1300909951	994(com/9999000)
54 1.2D + 1.5. Yes Y 1 1.2			066 4					1955					彩石腰		
55 1.2D + 1.5 Yes Y 1 1 1.2	8 .066		066 4		200 975 (mm)	A COMPANY FOR STREET	<u>Georgeory</u>	2017 Billion	CERT MARKED ALCO	41,92,000	Max Colder Name		- Arninke.		
56 1.2D + 1.5. Yes Y 1 1.2.	3 -066		.066 4						d es	8		• <u>.</u> *.	90.X	<u>.</u>	
57 1.2D + 1.5 Yes Y 1 1.2	4066		.066 4		QUIMES 1 - 3 -	o koosaaa Too saada	212 AL 300000001	COMMPTHE P.V.		2300m/mppm	ORDANIA MARKA	232000001***	<u></u>		
58 1.2D + 1.5. Yes Y 1 1.2.	5 - 066		.066 4			122.027	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	26. je							
59 1.2D + 1.5. Yes Y 1 1.2	6066		.066 4		5 3 H 205 H 27 H	Indiana. Indiana	-10-40-400 (Magazine - 11-1	date of the second	1221101-11000		<u>1. 1.120</u>				
60 1.2D + 1.5. Yes Y 1 1.2	7066		.066 4				1 X 1	法 前日	- Q						
61 1.2D + 1.5 Yes Y 1 1.2	8066		.066 4												
62 1.2D + 1.5. Yes Y 1 1.2	45 1.5			1			4		2	ш. 37. 45. Стар					
63 1.2D + 1.5 Yes Y 1 1 1.2	45 1.5														
64 1.2D+1.5. Yes Y 1 1.2	45 1.5			建 路》						- <u>T</u>					
65 1.2D + 1.5 Yes Y 1 1.2	45 1.5						- Chulu - Teachulur		mar laure link.			Cala inter e el a	14.1.561 67-0-0-0		VARIA M. P.L.
66 1.2D + 1.5. Yes Y 1 1.2	45 1.5			5 (<u>(</u>				23	1,000	調査				<u>.</u>	Sec. Sec.
67 1.2D + 1.5 Yes Y 1 1.2	45 1.5	- 3-00-00-0000 800						- superior and	rac en climado	Section 2			1900 and to a second	1.00122	ittazia
68 1.20+1.5. Yes Y 1 1.2	45 1.5						888. 4 .9			and the second					
69 1.2D + 1.5. Yes Y 1 1 1.2	45 1.5	1922.2013	Coloradore to the second	ke-tr (Federation	and the second se		名はい場合を		iline, diale		. Contractionistic-	RIGER -	and the second	74	and the second se
70 1.2D+1.5 Yes Y 1. 1.2	- I data - Barris Contractor - Barrison - Bar		18 12 24		r			3.5	19 19		5 - D		UKUPUS N XXXXXXXXXX	ini in trans	
71 1.2D + 1.5 Yes Y 1 1 1.2	45 1.5	36.3389 X	alaana ahaa	1200 At 2002			MARCENER	19 N. 1	1000-11		on a contractor	102344		38-	
72 1.2D+1.5. Yes Y 1 1.2	45 1.5		2000		1000		4 K <u>e</u> (†	<u>* 1</u>	2		的思想	NR SK	. <u>3</u> 69		
73 1.2D + 1.5. Yes Y 1 1.2	45 1.5			1955 - Ser	100 A			acart a			8	19. Hellow			
74 1.2D + 1.5. Yes Y 1 1.2 75 1.2D + 1.5. Yes Y 1 1.2	46 1.5			PFF /#65506				8 (E.S.)	朝代部院	5.3865			Maria Arc		\$
75 1.2D + 1.5 Yes Y 1 1 1.2 76 1.2D + 1.5. Yes Y 1 1 1.2	46 1.5							の造品							
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79 1.2D + 1.5 Yes Y 1 1 1.2	46 1.5			CALL OF R. OAK	CLASS COLUMN CALLS		and the second		and address 1						
80. 1.2D + 1.5. Yes Y- 1 1.2	46 1.5				in.							101 <u>-</u> 1913			
81 1.2D + 1.5 Yes Y 1 1.2	46 1.5														
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86 1.2D + 1.5. Yes Y 1 1.2	47 1.5				r na		66. TA	<u> </u>					Your		
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98 1.2D + 1.0. Yes Y 1 1.2	27 1	28	2	9 1	40	1									
99 1.2D + 1.0Yes Y 1 1.2	27 .866	28	.5 3	0 1	40	1			_						
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103 1.2D + 1.0 Yes Y 1 1.2	27866			4 1	40	1	1580.000472*1			and the sum		ologoji.ote	All Minde	00.2837	tran deferminen i
104 1.2D + 1.0. Yes Y 1 1.2	27 -1	28	3	5 1	40	1					2				780s.

RISA-3D Version 17.0.2

Load Combinations (Continued)

	Desc	cripi	lion	Sol	PD.,	.SR	BLC	Fact.	BLC	Fact	.BLC	Fact.	BLC	Fact.	.BLC	Fact	.BLC	Fact	.BLC	Fact.	.BLC	Fact.	,BLC	Fact.	BLC	Fact
105	1,2D	+ 1	.0	Yes	Y		1	1.2	27	866	28	5	36	1	40	1										
106	1.2D	+1	.0.,	Yes	Y		1	1.2	27	4.5	28	866	37		40	1										
107	1.2D	+ 1	.0.,	Yes	Y		1	1.2	27		28	-1	38	1	40	1										
108	1.2D	+ 1	.0	Yes	Y			12	27	.5	28	-,866	39	1	40	1						<u>у</u> Х.		$\sim 1^{k}$		調整
109	1.2D	+ 1	.0	Yes	Y		1	1,2	27	.866	28	5	40	1	40	1										

Envelope Joint Reactions

	_Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N6	max	843	13	2.593	19	-1.074	13	7.804	20	.637	7	-2.212	10
2		min	-9 607	19	.941	12	-9.277	18	2.301	2	4	13	-6.933	16
3	N4	max	8.607	22	3.084	24	279	4	8.135	18	.953	7	8.829	14
4		min	53	-4	1.054	4 :	-8.845	22	2,706	4	895	13	2.631	5
5	N2	max	9.207	24	3.554	20	9.509	25	-2.72	11	.981	9	10.683	17
6	Add Statistic	min	1.529	5	1,121	3	1.487	7	-10.641	18	-1.248	3	3.112	11
7	N8	max	-1.28	9	2.33	14	8.002	15	-1.081	4	.672	8	742	5
8		min	-8.254	15	679	9	1.722	9	-5.58	22	696	\$2 3	4.431	22
9	Totals:	max	5,553	11	11.508	17	5.323	2						
10		min	-5.553	5	4,045	7	-5.323	8						

Envelope AISC 14th(360-10): LRFD Steel Code Checks

	Member	Shape	Code	Locift]	LC	Shear	. Loc[ft]	Dir	LC	phi*Pnc	.phi*Pnt .	phi*Mn	.phi*Mn	Cb	Eqn
1	M1	L6X3.5X5	.272	1.502	15	.471	1,502	z	7	12.833	93.636	2.872	9.893	2	H2-1
2	M2	L6X3.5X5	.342	1.502	19	.567	6.908	Z	12 斗	12.833	93.636	2.872	7.99		H2-1
3	M3	L6X3.5X5	.322	1.502	24	.097	7.509	z	8	12.833	93.636	2.872	7.92	1	H2-1
4	M4	L6X3.5X5	.278	12.915	20	,040	7,058	Ż	20	12.833	93.636			1.	H2-1
5	M5	HSS6X4X4	.583	7.917	16	.134	.66	z	8	140.712		22.252	29.428	; 2⊢	<u>11-1b</u>
6	M6	HSS6X4X4	.466	7.917	21	137	66	Z	5	140.712		22.252] 1-1b
7	<u>M7</u>	HSS6X4X4	.417	7.917	20	.135	.66	z	2	140.712		22.252			
8	<u>M8.</u>	HSS6X4X4	.284	7.917	22	080	7.917	У	18	140.712	178.02	22.252	29,428	2	<u> 1-1b</u>
9	M9	L4X4X4	.665	5.009	16	.123	5.009	z	14	43.004	62.532	3.138	6.003		H2-1
10	M10 🞋	L4X4X4	.697	5.009	15	.130	5.009	y	25	43.004	62.532	3.138	6.003		<u>H2-1</u>
11	M11	L4X4X4	.493	5.009	19	.129	5.009	Ý.	18		62.532		6.003	11	H2-1
12	M12	L4X4X4	.664	5.009	25	.113	5.009	Z	19		62.532		6.003	1	H2-1
13	M21	L3X3X3	.250	3.333	14	.011	0	V.	17	13.164	35.316	1.32	2.25	1	H2-1
14	M22	L3X3X3	244	3,333	20	.009	0	z	20	13.164	35.316	1.32	2.251		H2-1
15	M23	L3X3X3	.241	3.333	23	.009	0	V.	17	13,164			2.249	1	H2-1
16	M24	L3X3X3	.242	3:333	17	.010	6,667	Z	16	13.164	35.316	1.32	2.249	1	H2-1
17	M25	PIPE 2.5	.607	3.125	8	.024	1.042		8	22.373	50.715	3.596	3.596	1H	11-1 b
18	- M26	PIPE 2.0	.112	2.648	8	.008	O. II	2016	· · · · 8	26.092	32.13	1.872	1.872		11-1b
19	M27	PIPE 2.0	.188	1.91	5	.056	1.91		5	26.092	32.13	1.872	1.872		<u>11-1b</u>
20	M28	PIPE 2.0	.549	3.75	_5	.034	3.75		5	23.809	32.13	1.872	1.872	1H	<u>i1-1b</u>
21	M29	PIPE 2.5	.607	3.125	2	.024	1.042		2	22.373	50.715	3.596	3.596	1H	<u>i1-1b</u>
22	M30	PIPE 2.0	.112	2.648	2	.008	0	с ⁴⁴	2	26.092	32.13	1.872	1.872	1 H	<u>11-1b</u>
23	M31	PIPE 2.0	.034	3.75	5	.004	3.75		5	23.809	32.13	1.872	1.872	1H	 1-1b
24	M32	PIPE 2.0	.520	3.333	8	.038	3.333		8	23,809	32.13	1.872	1.872	1. F	11-1b
25	M33	PIPE 2.5	.606	6.875	5	.024	6.979		5	22.373	50.715	3.596	3.596	1H	11-1b
26	M34	PIPE 2.0	.112	2.648	2.5	800.	0	秋 寒	5	26.092	32.13	1.872	1.872	1 H	11-1b

Envelope Plate/Shell Principal Stresses

	Plate		Surf	Sigma1 [ksi]	LC	Sigma2 [ksi]	LC	Tau Max [ksi]	LC	Angle [rad]	LC	Von Mises [ksi]	LC
1	P2	max	Т	5.103	18	1.302	20	1.975	15	2.355	15	4.621	18
2		min		.195	11	-2.332	2	.087	11	- 784	38	.185	11



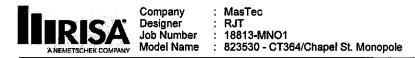
Envelope Plate/Shell Principal Stresses (Continued)

Plate	Surf	Sigma1 [ksi]	LC	Sigma2 [ksi]	LC	Tau Max [ksi]	LC	Angle [rad]	10	Von Mises [ksi]	LC
3 max	B	2.94	2	.008	11	2.206	2	1.529	11		18
4 min			20	-5.097	18	.082	11	089	10		11
5 P3 max	T	5.373	13	.102	12	4.591	8	2.215	50		20
6 min	12. S.	291	5	-8.909	20	.077	11	762	11		11
7 max	B	10.875	18	1.778	14	4.766	20	2.223	11		18
8 min	Acres 164	.392	11	-3,923	13	. 194	11		10		
9 P4 max	T	6.912	18	625	5	4.606	18	2.348	11		18
10 min		952	12	-2.929	13		114	556	10		11
11 max 12 min	B	3.011	13 20	959	12	5,413 .612	18 11	2.3 593	3		<u>18</u> 11
	T	6.719	15	092	13	4.66	<u>ana</u> 15	.743	9		15
13 P5 max 14 min	а	-,494	8	-2.752	20	625	8		5		7
15 max	В	.058	8	-2.274	8	5.418	14	1.379	13		14
16 min		-1.715	23	-12.453	24	1.142	7	1.007	8		8
17 P6 max	T	.582	7	.205	8	4.611	14	1,306	9		14
18 min.			13	-9.163	14	.152	8	.572	7	.443	8
19 max	B	11,218	14	1.244	15	4.997	14	.536	8		14
<u>20 min</u>		1 = 161	8	282	8	···· · · · · · · · · · · · · · · · · ·	8	656	7.	and the second se	7
21 P7 max	T	5.563	<u>15</u>	1.339	24	2.147	16	1.482	9		15
22 min.		.764	8	.148	9	.268	8	.716	3		8
23 max	B	084	9	577	8	2.223	15	2.306	7		15
24 min	T	-1.208	24	-5.577	15	207	<u>8</u> 18	<u>759</u> 1.123	12		8 8
25 P8 max 26 min		8.186 -4.063	2 8	2.823	2	4.058	10 11	325	10		11
20 27 max	B	10.597	8	4.23	8	4.707	<u>18</u>	2.352	11		8
28 min		-2.428	2	-9.073	2	.168	11	62	2		11
29 P9 max	1930 X223 (45	7.93	13	3.59	13	4.001	8	2.288	11		20
30 min		-8.471	20	-16.211	20	.326	ň	-775	10		11
31 max	В	13.94	7	11.831	18	3.157	8	2.324	15		20
<u>32</u> min		-2.522	13	-8,404	13	.01	62	722	107		11
<u>33 P10 max</u>	T	10.472	18	.786	8	6.006	18	2.175	12		18
34 min	18 A.		13	-1.861	14	.05	13	542	<u>11</u>		11
<u>35 max</u>	B	2.865	13	.602	2	3.517	18	2.327	11		18
36 min	<u> </u>		20	-10,291	18	617	2	<u>538</u> .501	2		3 15
37 P11 max 38 min	1	10.425	<u>15</u> 8	263 -2.183	2	6.265 .693	<u>15</u> 8	.195	9 7		8
39 max	В	107	8	-1.453	8	3.45	14	1.739	3		14
40 min		-3.053	24	-9.91	14	.673	8	.831	8		8
41 P12 max	Т	455	8	-1.542	8	4.129	24	.77	12		14
42 min	and in	-8.65	14	-16,741	14	.544	8	.104	7		8
43 max	В	14.047	14	12,207	14	1.244	13	2.223	4		14
44 min		1.384	8	019	8	136	4	771	2	The second se	8
45 P13 max		1.527	3	-1.033	8	4.431	15	.24	9		15
46 min		748		-7.88	14		ALINU CONTRACTOR	434			8
47 max	B	9.143	14	.72	10	5.108	15	1.687	9		15
48 min			8	-1:65	3		8	1.098	3		8
49 P14 max	T	3.736	<u>18</u> 11	<u>1.691</u> -1.451	<u>15</u>	2.094	8 50	<u>1.72</u> - 485	<u>10</u> 11		<u>8</u> 11
50 min	D D	<u>.21</u> 1.024	<u>13</u>	267	<u>8108</u> 11	2.14	20	1.929	高圖與 3		20
51 max 52 min	B	-:493	13 14	-4.539	18		11	655	4		20
53 P15 max	T	5.937	2	.902	2	5.268	20	2.311	6		20
54 min-		589	8	-10,358	8		11	775	56		11
55 max	B	8.685	8	1.792	20	3.613	8	2.343	12		8
56 min		-,355	2	-6	13	.315	4	17 - 537	11		4
57 P16 max	T	10.534	18	.523	3	5.824	18	.927	13		18
<u>58 min</u>		.365	12			.315		397	10		12
59 max	В	2.297	13	-1.281	11	2.647	18	1.959	61	6.564 1	18

RISA-3D Version 17.0.2

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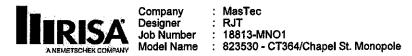
Page 68



Envelope Plate/Shell Principal Stresses (Continued)

Plate		Surf	. Sigma1 [ksi]	LC	Sigma2 [ksi]	LC	Tau Max (ksi)	LC	Angle [rad]		Von Mises [ksi	
	min		-2,095	16	-7.344	18	.554	10			A CONTRACT OF A	10
61 P17	max	T }	10.018	15	373	4	6.119	14	.444	10	11.284	14
62 63	min	B	.85	8 8	-2.376 937	<u>23</u> 9	. <u>793</u> 2.543	<u>8</u> 14	<u>.192</u> 1.723	7	<u>1.374</u> 5.867	<u>8</u> 14
64	max		-1.412	0 16	-6.421	15	484	9	.767	8	.952	9
65 P18	max	Т	1.208	16	897	7	5.53	24	.812	13	10.55	24
66	min	ALC Sec	.296	9	-9.954	24	.699	8	.385	7	1.257	8
67	max	В	6.757	14	1.867	24	2.454	14	.831	7	6.049	14
68	min	201	.5	7	43	8	.116	6	624	- 5	.594	6
<u>69</u> P19	max	T	4.01	15	1.729	16	1.189	14	2.326	5	3.488	15
70 15 5 2 18	min		.35	9	204	12	the second	8	-,709	6	.332	8
71	max	B	.403	13 18	<u>826</u> -4.835	9 15	2.198 .401	14 8	.784	7 13	<u>4.624</u> .833	14
73 P20	min max	Т	4.586	2	.516	14	2.279	2	2.229	10	4.572	8
74	min	as ar a	.049	10	-3,899	8	.048	58	248	11	17	57
75	max	B	3.588	8	27	10	2.54	18	2.313	3	4.561	18
76	min		27	3	-4.241	2		11	574	4	.63	11
77 P21	max	Т	4.83	18	.075	3	4.199	20	2.336	10	7.285	20
781	min		.469	11	-5.151	8	.544	11	- 716	6	.945	11
79	max	B	4.021	8	297	10	2.667	8	2.344	13	4.814	8
80	min			4	-3.436	2	<u>184</u>	4	652	12	.768	4
81 P22 82	max		10.82	18	1.028	3	5.205	18 11	.558	13 8	<u>10.621</u> 1.497	18
83	min max	В	1.263	13	7	o 10	1,924	13	2.316	<u>61</u>	4.194	18
84	min		-3.596	15	4.72	18		56	2.510	3	.61	10
85 P23	max	T	9.914	15	.375	7	5.733	14	.531	13	10.76	14
86	min	婚姻	1,666	8	-1:675	24	.784	8	.27	70	1.619	8
87	max	В	,444	9	283	10	1.319	14	2.308	45	3.525	15
88	min		-1.517	18	-4.004	15	.214	56	782	15	.454	11
89 P24	max	T	6.006	15	066	6	4.594	24	.656	13	8.062	14
90	min		.939	8	-3.408	24	.686	8	.204	<u>.</u>	1.215	8
91 92	max	B	1.413 - 548	13 6	527	10 15	1.487	<u>24</u> 5	.637	3	2.695	24 55
93 P25	min. max	T	2.577	17	.426	18	1.081	16	2.311	о 5	2.395	17
94	min		.083	10	-1.052	12	₩ 13 / 1	58	766	6	.339	58
95	max	B	1.381	24	615	9	2.745	15	.635	7	5.023	16
96	min		.025	6	-4.393	16	.536	9	042	13	.932	· 9
97 P26	max	Т	7,989	2	3.237	3	3.665	8	2.25	6	7.14	8
98	min		- 297	9	-6,933	<u>8</u>	.653	11	759	5	1.14	11
99	max	B	7.123	8	.176	9	3.828	8	2.169	12	7.404	8
100 101 P27	min	- <u>-</u>	<u>-4,2</u> 6,785	<u>3</u> 18	<u>-7,565</u> 2,483	2 8	<u>.297</u> 4.231	<u>11</u> 18	108 2.315	11 9	.538	11
102	max		-2,503	13	-4:542			12	2.315	9 7	7.76	10
103	max	B	5.121	13	3.023	13	4.188	18	.457	2	7,326	18
104	min		-2.081	7	-5.536				051	11	2.101	60
105 P28	max	Т	9.682	14	.466	12	5.313	15	.413	13	10.156	14
106	min		1.953		-3.588			10	707	8_	2.382	10
107	max	В	4.144	8	.206	9	2.994	13	2.356	43	5.628	13
108	min		,226	33	-5.182			43		103	.276	43
109 P29	max	<u> </u>	7.016	18	.142	8	5.328	14	.557	13	9.334	15
110	min	D	2.081	9	-3.946			<u>9</u> 12	068	7	2.06	9
112	max min	B	<u>3.75</u>	24	1.506	14 7	<u>1.442</u>	13 43	2.227 - 767	3	<u>3.272</u> 684	24 5
113 P30	max	Т	9.482	14	1.169	25	4.161	<u>ഷാം</u> 14	.6	6		14
114	min	1.16		8	347	8	.663	8		12	1.191	8
115	max	В	1.397	8	- 917	8	3.443	18	.118	9	7.03	14
116	min		-1.53	13	-7:296	14			-,493	3	1.971	

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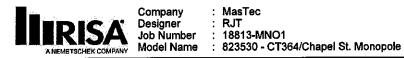
Envelope Plate/Shell Principal Stresses (Continued)

Plate		Surf	Sigma1 (ks	I LC	Sigma2 (ksi)	LC	Tau Max [ksi]	LC	Angle [rad]	LC	Von Mises [ksi	il LC
117 P31	max	T	7.161	16	2.022	6	2,93	24	.822	13	6.467	16
118	min		.604		-2.076	13		8	.176	7.	1.101	9
119	max	B	2.357	13	849	9	3.498	24	<u>099</u>	8	7.439	15
120	min		-2.18	6	-8.075	16	.235	7	617		1:31	8
121 P32 122	max min	T	14.903	2	<u>3.168</u> -15,2	2	5.868	2 11	.884	1 <u>3</u> 9	<u>13.599</u> 1.374	2
123	max	В	15.371	8	4.353	8	5.973	2	2.171	4	14.121	2
124	min		-3.637	COS 2 CANERS HUDE	-15.584	2	.476	11	773	3	.996	58
125 P33	max	Т	8.473	18	.042	3	7.199	18	1.024	13	12,533	18
126	min	41.5	377	11	-9.032	8	.805	11	364	9 .	1.459	11
127	max	B	<u>8.917</u>	8	3.001	20	5.447	13	1.924	5	9.489	2
128	min		.966	4	-7.565	2	332	32	712	4	1.391	43
129 P34 130	max		11.131	<u>14</u> 8	.968	10	6.902 .496	14 .9	<u>2.204</u> 733	7 6	<u>12.681</u> 1.579	14
130	min. max	В	9,239	18	.138	6	4.582	18	2.028	12	9.201	18
132	min		.209	12	-3.792	13	.659	11	-,476		1,142	11
133 P35	max	T	7.375	18	.28	9	7.087	15	.794	13	12.276	15
134	min	18 A	1.539	13	-7,188	15	1.389	10	.045	8	2.636	10
135	max	B	15.081	14	1.454	24	6.859	14	.003	9	14.448	14
136	min	-	1.131		276	6	.513	8		7	1.083	8
137 P36	max		14.293	<u>15</u>	<u>571</u> -4.62	6 24	9.31	<u>14</u> 8	.105	12	<u>16.877</u> 2,371	14
138 139	min max	В	3.03	9	.475	10	2.302	16	2.078	12	4.039	16
140	min	25	.042	3	-3.651	3	.386	60		1î.	.677	60
141 P37	max	T	3.346	7	717	7	5.531	16	.204	12	9.959	15
142	min		-1.458	13	-8.971	24	.943	-9	551	7.	2.009	9
143	max	B	6.077	24	1.52	13	3.629	16	2.303	9	6.517	15
144	min		075		-3.244	6	.479	8	.861	8	.997	8
145 P37A	max	and the second	1.455	13	<u>.334</u> -9.139	12	3.172 192	17 11	<u>1.422</u> .451	2	8.108 .333	18
147	min max	В	4.95	8	2.713	18	1.965	8 8	2.35	14	4.527	8
148	min		007	12	-3,459	213	.117	51	771	50	.221	
149 P38	max	T	11.044	20	2.773	18	4.158	20	1.615	3	9.964	20
150	min		- 878		-5.167	13		11	416	4	.158	11
151	max	B	1.575	13	156	11	4.471	<u>18</u>	2.219	13	9.99	18
152	min		-1.839	18	-10.782	18	.069	11	<u>757</u>	12	.148	11
153 P39 154	max min		<u>11.456</u> .645	<u> 14</u> 8	<u>2.745</u> 109	14 8	4.355	14 7	<u>.387</u> 105	6 8	10.36 .648	14
155	max	B	1.154	8	315	8	4.876	14	2.226	10	10.628	14
156	min		-1.574	Advert Contraction of the second	-11,327	14	.599	7	743	7	1.055	5 7 4
157 P40	max	Т	.416	8	718	9	3.051	15	2.217	6	8.308	15
158	min		-3.411		-9:462	15	.334	10		7	.798	
159	max	B	3.93	14	3.286	15	1.168	13	1.216	6	3.644	14
160	min	符 (* 〒	.51		481	7	.066	54	41	<u>3</u> 3	.443 2.548	9 8
161 P41 162	max min	T	<u>1.375</u> .16	7 61*	<u>101</u> -1.567	61 8	1,47	8 61	<u>1.715</u>	3 4	.228	61
163	max	B	2.392	13	152	11	2,989	7	2.353	2	5.276	7
164	min		.221	11	4.137		187		738	13	.325	
165 P42	max	Т	7.019	18	2.836	18	2.141	8	1.106	13	6.116	18
166	min		.096		_1.571	13	.14	3	354	8	.431	11
167	max	В	.907	13	572	11	3.508	18	2.285	12	8.433	18
168 100 D40	min		-2.442		-9.355	18	.191		.734	9	.504	11
169 P43	max		<u>6.87</u> 505	14	2.338	1 <u>5</u> 8	2.274	<u>14</u> 7	<u>2.296</u> 647	8	6.053 .576	14
170	min max	B	.394	9	-1.237	9	3.903	14	2.292	9	8.691	15
172					-9.374	15	.685	7	1.962	3	1,414	7
173 P44	max	T	1.893	14	168	9	1.66	14	2.305	8	2.885	14
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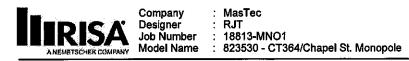
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Envelope Plate/Shell Principal Stresses (Continued)

Plate	Surf	Sigma1 [ksi] LC	Sigma2 [ksi]	LC	Tau Max [ksi] L		LC Von Mises [ksi] LC
	min	166 9	-1.428	14		478	7 .29 9
where a short of the fore the most state of the second state of the second state of the	<u>nax B</u>	2.3 14	199	8	<u>3.618 1</u>		<u>12 6.403 14</u> 8 .455 8
	<u>min</u> nav T	.322 9	<u>-4.936</u> .051	14 10	<u>.26</u> 8 2.651 1		3 5.201 18
	max∣ T min	5.095 18	-1.363	13	121 1		50 .271 10
	nax B	3.784 13	102	11	4.362 2		4 8.09 20
	min	2 61	-7.255em	20	.208 1		3 .375 11
	nax T	4.163 17	2.624	15	1.16 _ 2		8 3.644 17
	min	10	002	7		592	7 .493 10
	<u>nax B</u>	2.672 8	-1.038	_11_	3.016 8		<u>13 7.193 18</u>
	<u>min i i i i</u>	-3.608 14	-8,252	18		1 .793	8 .912 11
	<u>nax T</u>	3.502 15	1.739	16		<u>4 2.121</u> .104	7 <u>3.033</u> 15 62210
	min	. <u>214 10</u> .412 13	- <u>.286</u> -1.03 <u>4</u>	9 9		4 2.248	10 6.966 15
and the self-the design of the second s	nax∣_B_ min	-2,213 18	-1.034	15		1.411	8 1.024 9
	nax T	6.062 15	.094	9	3.221 1		8 6.261 15
and the second	min	.289 9	-:496	13		519	12 .255 .9
	max B	1.799 14	369	8	5.083 1	4 2.17	9 9.397 14
192	min	.169 8	-8.367	14		2.025	7 .477 8
	<u>max T</u>	<u>6.497 18</u>	2.995	8	<u>5.118 1</u>		2 8.905 16
	min	-1.857 13	-6.325	2	351 1		<u>9 .626 10</u> 8 6.41 7
	<u>max B</u>	5.473 13	2.716	2	<u>3.145 2</u> .302 1	<u>0 </u>	8 6.41 7 13
	min max T	-2.011 8 7.974 2	-7.169 2.184	2	2.895 2		8 7.137 2
	max T min	-1.871 8	-6.124	2	.344 1		3 602 10
	nax B	2.43 8	-1.472	10	3.155	2.108	13 7.64 15
	min	-3.336 15	-8.741	15		0 .958	7 1.384 10
	nax T	1.806 7	.967	7	1.084 1		16 2.615 13
	min 👘	- 736 13	-2.904	13		7783	41 .268 55
in the residue of the second second days and the second second second second second second second second second	<u>max B</u>	2.206 13	183	13	2.403 1		2 5.872 16
	<u>min</u>	-2.01 18	-6.599	18	the party of the second s	- 728	12 .706 9
	<u>nax </u> T	8.224 15	1.314	<u>13</u>	4.609 <u>1</u> .385 1	and and an all the "Bill of the reason which for a flater of the	9 8.722 16 13 89 9
	min nax B	.333 7	-1.787	8	2.988 1		4 7.072 14
	<u>max B</u> min	-1.859 24	-7.808	14		745	5 688 8
	nax T	4.389 16	1.165	17	1.831 1		47 3.941 16
	min	.601 9	-2.074	11		783	107 .565 8
211 r	nax B	2.774 11	393	9	2.131 1		10 4.199 5
	min	-1.103 17	4,472	16	.21		6 .41 8
	<u>nax T</u>	4.907 11	-,297	9	4.602 5		<u>35 8.583 5</u>
	min	-,325 24	-8.2	16		-,668	13 .967 8 9 9.11 16
	<u>nax B</u> min	<u>9.58</u> 16 889 9	1.598	23	4.595 8		
	nax T	6.045 16	439	4		6 1.676	9 7.223 16
	min	-1.073 9			406		
	nax B	2.781 11	-1.944	10	4.757 1	5 2.278	12 10.435 16
	min	17	-11.18	16	.946 8	754	9 2.25 8
221 P56 r	max T	4.858 25	18	11	3.626 2		6 6.4 25
	min	-269 5	-2.535	19	.57.9 8		12 1.313 5
	max B	.276 4	-1.457	4	4.517 2	2 1.348	11 9.837 22
	min	-1.446 22		22	.852 3		5 <u>1.613</u> 4 5 <u>7.587</u> 23
	max T min	.627 5 943 11	.43 <u>2</u> -7.524	5 23	3.824 2	3 <u>1.51</u> 1.003	10
	max B	8.89 23	1.444	<u>20</u> 11	3.963 2		5 8.449 23
	min	208 5		4	128		11 402 5
	nax T	4.495 25	1.105	25	1.695 2	5 1.103	5 4.057 25
230	min			6	.291 6		11 .733 6

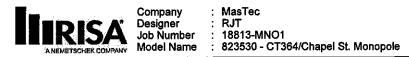
RISA-3D Version 17.0.2



Envelope Plate/Shell Principal Stresses (Continued)

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												34		6
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		P59		Т	7.563			11	3.454					
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	234		min		-4,145	5	-10.064	5	.397					
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228 min 7.757am 4. 15.472 5. 4.472 13 1.738 3. 1.569 8. 239 max B 14.885 5 10.457 16 3.522 36 12.905 5 240 min -2.738 10 9.05 11 0.04 176 2.3 1.271 8 241 P61 max T 9.041 16 1.118 5 5.116 16 207 3 9.691 16 243 max R 2.252 11 0.35 10 3.157 16 0.151 11.12 5 1.09 2.3 396 9 9.353 2.3 246 max T 8.14 2.3 .5119 2.3 .777 11 1.142 5 .488 4 .1424 5 .1385 2.3 .774 11 1.1425 2.3 .774 11 1.1425 .1438			min			1.1.1.2.2.1.2.2.0								
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244 min 2.986 17 9.9268 16 6.77 8 -7.18 9 1.515 12 245 P62 max T 8.14 23 -511 2 5109 23 396 9 9.353 23 246 min 403 5 2.938 5 2.821 23 1.72 12 7.236 23 248 min 2.516 23 8158 23 2244 4 7.94 5 888 4 249 P63 max T -548 5 -1.741 5 3.421 23 7.77 11 11.956 23 250 min 1.355 25 9.817 23 1.043 11 2.143 10.667 25 253 P64 max B 7.566 25 .17 5 4.109 25 1.493 5 7.912 25 2.586 min			1	R										
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268 min -1.781 14 -6.565 16 .644 34 655 12 1.39 8 269 P68 max T 7.958 23 643 3 5.071 23 .395 9 9.246 23 270 min .693 5 -2.194 22 .712 5 .198 4 .1234 5 270 min .693 5 -2.194 22 .712 5 .198 4 .1234 5 271 max B 034 6 548 5 2.02 24 1.73 13 4.63 24 272 min -1.02 22 -5.053 23 .244 5 .824 5 .521 5 273 P69 max T 1.122 21 .911 5 4.673 23 .79 11 8.857 23 274 m	266		min					· 5.		9				
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272 min -1:02 22 -5:053 23 244 5 824 5 .521 5 273 P69 max T 1.122 21 911 5 4.673 23 .79 11 8.857 23 274 min .003 4 -8:269 23 .546 5 .468 5 1.013 5 275 max B 5:29 25 1.591 23 1.857 25 2.346 4 4.704 25 276 min .433 5 036 5 134 4 719 3 .453 5 276 min .433 5 036 5 134 4 719 3 .453 5 276 min .416 6 184 9 .063 6 703 5 .37 6 278 min .416 1												diam'r i'r		
273 P69 max T 1.122 21 911 5 4.673 23 7.9 11 8.857 23 274 min .003 4 8269 23 .546 5 .468 5 1.013 5 275 max B 5.29 25 1.591 23 1.857 25 2.346 4 4.704 25 276 min .433 5 036 5 134 4 719 3 .453 5 276 min .433 5 036 5 134 4 719 3 .453 5 276 min .433 5 036 5 134 4 719 3 .453 5 277 P70 max T 3.201 25 1.296 14 .955 25 2.241 4 2.789 25 278 min	Contraction in the second	ere let an		B										
274 min .003 4 .8269 23 546 5 .468 5 1.013 5 275 max B 5.29 25 1.591 23 1.857 25 2.346 4 4.704 25 276 min .433 5 .036 5 .134 4 .719 3 .453 5 276 min .433 5 .036 5 .134 4 .719 3 .453 5 277 P70 max T 3.201 25 1.296 14 .955 25 2.241 4 2.789 25 278 min .416 6 .184 9 .063 6 .703 5 .37 6 279 max B .186 11 .822 6 1.843 23 .725 5 3.866 24 280 min .418 <	202 - YE BY - 4190	Dea	2	Ť	and the second sec	100 feet 100 100				Acade The Support				a set and and
275 max B 5.29 25 1.591 23 1.857 25 2.346 4 4.704 25 276 min .433 5 .036 5 .134 4 .719 3 .453 5 277 P70 max T 3.201 25 1.296 14 .955 25 2.241 4 2.789 25 278 min .416 6 .184 9 .063 6 .703 5 .37 6 279 max B .186 11 .822 6 1.843 23 .725 5 3.866 24 280 min			013-000329889523	HAR WORKS		DOD. A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A								
276 min .433 5 .036 5 134 4 .719 3 .453 5 277 P70 max T 3.201 25 1.296 14 .955 25 2.241 4 2.789 25 278 min .416 6 .184 9 .063 6 .703 5 .37 6 279 max B .186 11 822 6 1.843 23 .725 5 3.866 24 280 min 448 16 .4034 24 .374 5 245 11 .793 6 281 P71 max T 4.881 11 .453 23 2.439 11 2.069 7 4.879 11		anan di kasa di kasaran da kasara				Contraction of the								
277 P70 max T 3.201 25 1.296 14 .955 25 2.241 4 2.789 25 278 min .416 6 .184 9 .063 6 703 5 .37 6 279 max B .186 11 822 6 1.843 23 .725 5 3.866 24 280 min 448 16 -4034 24 .374 5 .245 11 .793 6 281 P71 max T 4.881 11 .453 23 2.439 11 2.069 7 4.879 11												XTYY N MORA IN		
278 min .416 6 .184 9 .063 6 703 5 .37 6 279 max B .186 11 822 6 1.843 23 .725 5 3.866 24 280 min 418 16 -4.034 24 .374 5 .245 11 .793 6 281 P71 max T 4.881 11 .453 23 2.439 11 2.069 7 4.879 11		1. 2. Manual -												
279 max B .186 11 822 6 1.843 23 .725 5 3.866 24 280 min 418 16 -4.034 24 .374 5 .245 11 .793 6 281 P71 max T 4.881 11 .453 23 2.439 11 2.069 7 4.879 11		at the support of the first of the deside of the state of the state of the	And the Association of	Fellowers and	416									
280 min 418 16 -4.034 24 .374 5 .245 11 .793 6 281 P71 max T 4.881 11 .453 23 2.439 11 2.069 7 4.879 11			1									_		
281 P71 max T 4.881 11 .453 23 2.439 11 2.069 7 4.879 11	280											Same Marriel - Walt		
					4,881	11	.453		2.439		2,069		4.879	
	282		min		.117		-3,723		.094	31	217	8	.245	30
283 max B 3.541 5343 6 2.338 11 2.293 12 4.804 11	283		max	B								·		
<u>284 min -:259 12 4:923 11 .521 8781 9 .921 8</u>	284		min											
285 P72 max T 4.417 11 .043 12 3.728 17 2.324 7 6.464 17				T								SS - 1772		
<u>286 min</u>														
287 max B 4.075 5 429 7 2.839 5 2.298 11 5.071 5	287		max	B	4.075	5	429	7	2.839	5	2.298	11	5.071	<u> </u>

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Envelope Plate/Shell Principal Stresses (Continued)

Plate	Su	rf Sig	ma1 [ksi]	LC	Sigma2 [ksi]	LC	Tau Max (ksi)	LC	Angle [rad]	LC Von Mises [ksi] LC
	min		<u>462</u>	13	4,229		.311	13	773	<u>10 .788 36</u> 11 9.177 16
	max min		<u>9.306</u> 2.082	<u>15</u> 9	1.022	1 <u>2</u> 5	4. <u>526</u> .821	<u>16</u> 9	.409 603	5 1.9
			2.0 <u>82</u> 1.442	10	-1.032	7	1.923	11	2.281	34 3.687 16
	min		3.063	25	-4.198	16	.046	31	-,689	12 .937 7
			7.987	23	021	4	4.86	23	.522	13 8.98 23
	min: 👌	The second second second	1.163	5	-1.733	23	.603	5	.36	5 1.185 5
	max I	в	.172	6	483	6	1.134	25	2.314	54 2.692 25
	min		763	19	-2,976	25	.184	9.	-,749	48 .525 5
	<u>max</u>		<u>5.161</u>	23	069	<u> 4 </u>	3.972	22	.618	<u>11 6.979 22</u>
			.855	5	-2.797	<u>22</u>	.507	4	.284	5
		B ·	<u>1.016</u>	<u>11</u>	58	4	1.057	23	.531	5 2.012 23 3 525 4
300 201 D76	min	T	441		-1.917 .327	<u>25</u> 19	.069	4 15	2.224	4 1.682 15
	max min		164	15 8	-,322	11	.043	8	708	5 142 8
		B '	1.092	22	961	6	2.3	23	.576	5 4.167 23
	615		.01	4	-3,542	24	.565	6	.101	11 1.055 6
	max	A CONTRACT OF A CONTRACT	8.828	11	3.051	12	3.823	5	2,305	7 7.846 11
THE REPORT OF A DESCRIPTION OF A DESCRIP	min	- F	.129	6	-6.856	5	.682	35	779	2 1.241 8
		3 (5. <u>903</u>	5	257	6	3.887	5	2.254	9 7.377 5
	min		4.03	12	-8.358	11	.247	13	.236	8 .887 8
			<u> 6.077</u>	16	2.636	5	3.61	<u>15</u>	2.33	<u>3 6.708 16</u>
	min		ITANAA	11	4.422	10	1.06	7	715	7 1.907 8
the second s	the second second second second second		5.347	11	3.116	10	3.598	16	.394	<u>13 6.345 16</u>
	min		2.665	5	-5.716	5	894	<u>10</u> 23	.013	9 1.974 33 11 9.091 23
	NACE AND A CONTRACT OF A DECEMBER OF A DECEMBE	Sec. 2004 Balant Party	8.771 1.275	23 4	.443 -3.993	9 5	4.691	<u>23</u> 7	.365	5 2.474 7
		B	1.375 3.938	<u>4</u> 5	.29	5 17	2.993	11	2.354	102 5.495 11
TO DESCRIPTION OF A DES	max <u>i</u> min			100	-4.815	112	.035	53	2.334	34 .25 100
			5.678	21	121	5	4.586	23	.494	11 8.012 22
sense development in the sense transfer of same had sense and others, sense it while the first	min		1.063	3	-3:595	23	771	4	06	5 1.397 4
			3.762	22	1.541	23	1.14	11	2	2 3.277 22
	min		156	.4	281	• 5	.197 -	2	- 731	51 .382 4
321 P81	max	T i	8.346	23	1.387	15	3.568	22	.877	4 7.796 23
322	min	1 1 1 1 1 1	1.011	5	119	9	.365	5	.388	9 .904 5
	<u>max </u> I	3	<u>.598</u>	6	-1.222	6	2.735	21	.029	6 5.88 25
	min		-1.15	11	-6.263	25	.791	3	392	12 1.553 5
	C Line and Company and Company		5. <u>635</u>	25	1.147	16	2.404	23	.883	3 5.252 25
	1		<u>1.281</u>	6	-1.138	11	.273	5	396	6 <u>1.128</u> 6 6 6.109 <u>25</u>
		3	1.398 1.184	<u>11</u> 4	-1.459 -6.436	<u>6</u> 25	2.886	<u>23</u>	2 569	<u>6 6.109 25</u> 3 1.284 6
328 329 P83	min max	T 1	6.057	4 11	3.241	<u>20</u> 11	6.408	<u>11</u>	.871	10 14.707 11
	min		4.592		15,382		1.019			6 1.765 8
			15.57	5	4.545	5	6.367	11	2.233	13 15.061 11
332	min				-16.624			8	746	12 .584 8
			8.695	11	.303	12	6.328	16	.863	11 10.981 16
	min		.862	7	-9.089	5	1.414	8	371	6 2.451 8
335	<u>max I</u>	B	8.473	5	2.93	17	6.197	11	2.345	41 10.851 11
336			1.076	2	-7.791		.274	41	731	<u>39 1.139 52</u>
			0.262	22	.528	7	6.161	23	2.294	3 11.411 23
			1.072	4	-4.546		1.032	6	-,581	2 1.825 6
		B	<u>8.152</u>	16	.337	22	4.034	16	2.254	9 8.111 16
	min	-	<u>.601</u>	9	-2:052		.406	9	005	8 .729 9
			5.991	21	<u>187</u>	5 25	5.905	23	.701	<u>12</u> <u>10.227</u> <u>23</u> 5 <u>2.024</u> <u>4</u>
	4		<u>1.323</u>	3	<u>-6.036</u> 1.56	<u>25</u> 22	1.148 6.103	4 23	<u>.162</u> 271	<u>5 2,024 4</u> 6 13.02 <u>4 23</u>
			<u>3.711</u> .87	23	354		438	<u>23</u>	271	<u> 6 13.024 23</u> 4
044	min	36 B	.0/.	J	004	<u>, 1</u>		<u>₩</u> U.%		

RISA-3D Version 17.0.2



: MasTec : RJT : 18813-MNO1 : 823530 - CT364/Chapel St. Monopole June 7, 2019 7:54 PM Checked By:____

Envelope Plate/Shell Principal Stresses (Continued)

	Plate		Surf	Sigma1 [ksi]	LC	Sigma2 [ksi]	LC	Tau Max [ksi]	LC	Angle [rad]	LC	Von Mises [ksi]	LC
345	P87	max	T	13.102	22	579	5	8.256	22	.039	11	15.099	22
346	and the second second	min	. es 14	1.614	5	-3.413	23	1.096	5	329	5	1.968	5
347		max	В	1.506	6	102	9	1,771	15	1.631	11	3.116	15
348		min		.005	10	-2.328	12	.163	9	491	9	.288	9
349	P88	max	Т	1.958	17	872	5	4.521	24	.016	11	8.352	23
350	and the state of the	min		-613	11	-7.432	23	1.035	_5	416	5	1.795	6
351		max	В	4.899	25	1.026	11	2,741	15	1,909	9	5.195	25
352		min		222	6	-1.19⊭	4	.38	6	1.065	-5	.677	6
353	P89	max	Т	1.366	10	427	9	2.695	15	1.502	10	6.917	15
354		min		-2.527	16	-7.803	16	.397	7	.563	6	.895	9
355	-	max	В	5.061	5	2.353	16	2,224	11	2.321	23	4.576	5
356		min	Jac J.	-:07	10	-3.836	11	.107	34	-,784	60	.364	8
357	P90	max	Т	9.86	16	2.422	16	3.944	5	1.561	12	8.899	16
358		min		-,698	11	-5,186	11	.397	8	+.543	13	1.009	8
359		max	B	.822	11	799	9	3.805	16	1.994	10	8.48	16
360	states and the states of the	min	dur bar	-1.554	15	-9.142	16	.533	8	.824	6	1.002	9
361	P91	max	Т	9.319	23	2.2	23	3.56	23_	.358	8		23
362		min		.73	5	102	5	.416	5	046	5	.786	5
363		max	В	1.37	5	355	5	3.979	23	2.248	3		23
364		min		-1.276	11	-9,141	23	65	6	602	4	1.129	6
365	P92	max	Т	.481	5	-1	6	2.354	25	2.17	2		23
366	运行 其 31	min		-2,822	23	-7,522	23	.548	6	755	3	1.051	6
367		max	В	3,193	23	2,715	25	1.023	11	1.157	5	2.969	23
368		min		.591	6	302	5		30	388	10		6
369	P93	max	Т	1.476	5	064	8	1.571	5	2.331	13	2.722	5
370		min		.086	8	-1.665 🐇	5	.075	8	593	35	.13	8
371		max	В	2.406	11	233	8	3.05	5	2.33	11	5.382	5
372		min	1. J.	.046	8	-4.079	5	.139	8.	727	9	.259	8
373	P94	max	Т	6.202	16	2.411	16	2.204	5	1.162	11	5.415	16
374		min.		211	11	-1,243		.238	12	-,351	5	.5181	12
375		max	В	.648	5	-1.329	8	3.049	16	2.168	10	7.214	16
376		min		-2.078	25	-7.963	16	.419	8	765	6	1,164	8
377	P95	max	Т	5.508	23	1.789	25	1.86	23	2.35	6	4.867	23
378	1. 计子数代码 经济	min	Ne wa	.538	6		5	.346	7	723	4	713	6
379	· · · · · · · · · · · · · · · · · · ·	max	В	.441	5	-1.573	6	3.205	25	2.265	5	7.01	23
380		min		-1:087	23	-7,49	23	.772	7	1.97	11	1.568	7
381	P96	max	Т	1.619	23	087	6	1,419	23	.623	11	2.466	23
382		min	$(f_{ij}^{(1)})_{ij}$.14	6	-1.221	25	114	6	542	5	.199	6
383	and the second se	max	В	1.952	25	-,36	5	3.027	25	2,123	11	5.352	25
384		min		.362	6	-4.102	25	.376	6	1.746	5	.651	6
385	P97	max	T	4.35	16	.005	7	2.253	16	2.244	8	4,43	16
386		min		.338	9	- 963	11		8	776	13	.444	8
387	and the second s	max	B	3.673	11	445	8	4.362	5	1.131	13	8.054	5
388	化学生 机动力化	min		.049	8	7,152	5		8	681	12		8
389	P98	max	Т	3.5	25	2.216	25	1.045	10	1,787	4		25
390		min		702	6	.339	7	.112	4	541	3	.608	6
391		max	В	2.672	5	-1.419	8	3.152	5	2.219	10	6.178	16
392		min		-3.072	23	-7.056	16		8	798	5	1.229	8
393	P99	max	Т	2.707	23	1.136	25	.794	23	1.773	3		23
394		min	<u>s</u> iye	.339	7	477	5	.061	7	.535	59	.297	7
395		max	В	098	11	-1.406	6	2.396	25	2.167	3		25
396			17 4 5		15	-6:152	25	.597	6	1.495	-5	1.313	6
397	P100	max	T	4.982	23	.095	4	2.658	23	1.213	5		23
398		min		.531	5	-,541	11	.249	5	.564		.515	5
399	A CONTRACTOR OF	max	B	1.521	25	652	5	4.229	25	2.116	4		25
		min		.244	6	-6,938			5	2.081	10		5
401	P101	max	T	5.736	16	3.072	5	4.358	25	2.134	10		15

RISA-3D Version 17.0.2

[C:\...\...\...\...\823530 - Updated.R3D]

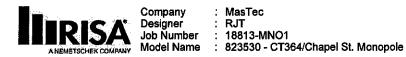
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Envelope Plate/Shell Principal Stresses (Continued)

Plate	5	Surf	Sigma1 (ksi)	LC	Sigma2 [ksi]	LC	Tau Max [ksi]	LC	Angle [rad]	LC	Von Mises [ksi] LC_
	nin Ì	1.19	-1.856	10	-6.531			6	1,486	6	7
	nax	В	5.511	11	2.662	10	2.796	16	.991	5	6.707 5
	nin	Maadana Karadhir (M	-2.233	5	-7.538	5		8.	263	10	.874 8
	<u>1ax </u>	T	8.344	11	2.419	11	2.963	11	1.561	5	7.436 11
	nin	ا الح	-1.935	5	-6.364	5	.333	29	.231	11	.608 29
)ax	B	2.437 -2.856	5 25	-1.98 -7.444	8 25	<u>3.211</u> .678	5	<u>2.143</u> .98	10 5	6.594 11 1.753 8
	nin 1ax	Т	1.124	- <u>25</u> 5	.383	5	.84	11	2.279	53	1.992 11
	nin		- 69	25		11	.085	8	.495	5	.265 3
	nax	В	1.556	11	313	11	1.937	25	2.284	9	4.431 25
		5 . jų	-1.211	16	-4.857	15	.492	7	77	10	1.022 9
	<u>nax</u>	T	6.882	25	.824	11	<u>3.441</u>	25	1.378	5	6.882 25
		Sec. 65	1,144	6	713	5	.778	6	.661	11	1.396 6
	<u>ax</u>	B	167	5	782	6	2.393	23	2.331	7	5.902 23
	nin		-1:896	15	-6,606	25	.255	6	-,669	3	<u>.687</u> 6 3.4612
			<u>3.45</u> 358	2	.738	14	1.836	8 5	782	46 34	351 5
	nin nax	B	2.889	8	-2.207	5	2.103	8	1.406	6	3.855 2
			655	12	-3.874	Ž	131	5	146	4	.228 5
	ax	Т	5.317	8	62	5	4.319	2	2.312	5	8.007 2
422 n	nin b		- 331	21	7.175	2	.35	5	626	10	.664 5
	<u>iax</u>	В	6.488	14	1.663	20	4.039	2	1.801	7	7.404 2
	nin		.954	5	-3.987	8		5	.181	3	83 5
	iax	T	4.135	2	516	12	2.444	2	1.524	<u>6</u> 4	4.558 2
	5	В	<u>824</u> 3.07	8	<u>-3:167</u> -1.6	8	.194 3.658	- <u>6</u> 22	457 2.322	9 9	734 5 8.21 24
THE ADDRESS NOT THE PARTY OF THE PARTY NEEDED AND THE PARTY OF THE PAR	nax nin	D	-1.821	。 14	-8.892	14	731	5	681	6	1.777 5
	ax	T	3.68	8	058	8	2.203	21	.967	2	3.816 21
State and a state of the state		國際黨	704	32	-2,359	15	.404	13	003	9	1.063 13
431 m	nax	В	.285	2	-1,113	13	3.309	20	1.351	8	7.416 20
	nin 🗋	s, is	-1,422	18	-8:015	20	.659	13	.808	2	1.228 13
	nax	T	1.14	2	.554	2	2.683	20	1.832	13	5.515 8
	nin	B	897 C 713	8	<u>-5.909</u> 1.392	8	.043 2.661	3 8	609 1.049	<u>2</u> 2	418 3 6.136 8
	nax∣ nin	P	6.713 - 305	8	-1.244	8	.09	13	-,482	 7	383 13
	nax	T	2.845	21	.702	22	1.072	21	1.428	2	2 567 21
A SUMMATES NEED ADDR. NAME AND ADDR. ADDR ADDR. ADDR. ADDR ADDR. ADDR. ADDR ADDR. ADDR. ADDR ADDR. ADDR.	nin		.264	3		3	.098	3		87	.237 3
	nax	В	.045	3	015	3	1.033	21	2.319	9	2.357 21
440 n	nin		512	23	-2.567	21	.03	3	771	43	.054 3
	ax	T	<u>7.781</u>	8	2.986	8	<u>2.674</u>	2	1.054	6	8.098 2
	<u>nin </u>		-3.969	2	-9.317	2	.209	5	356	3	.41 5
		В	<u>10.28</u> -2.658	2	4. <u>133</u> 8 -8.738	2	<u>3.074</u> .34	2 5	2.289	<u>5</u> 9	8.96 <u>2</u> .589 5
	nin nax	Т	8.624	8	3.698	8	3.752	2	2.321	5	12.136 2
446 m			-6,497	2	-14,001	2		10	773	4	.968 5
	ax	В	13.044	2	6.802	14	3.533	8	1.103	11	11.299 2
		$\mathbf{c} \sim \mathbf{b}$	-2.429	8	-9.496	8	.021	109	.709	10	.934 5
	<u>nax</u>	Т	5.786	14	.963	2	3.519	24	237	9	6.484 24
	121212		-1.262	. <u> </u>	-1.785	<u>8</u>	.203	7	705	7	1.225 6
	nax	B	2.534	8	.226	8	2.303	24	2.175	5	6.065 14
	<u>nin</u>	<u>і</u> т		2	-6.88	14	.657	20	694	<u>6</u>	1.313 6
453 P114 m 454 n			5.251 637	20 2	<u>499</u> -2.19	11 18	3.677 	<u>20</u>	.615 	3 12	6.561 20 .872 13
	nax	В	.584	2	-2,19 -,788	2	1.927	20	1.735	8	5.069 20
	nin		-1.888		-5.742			13	.558	2	767 13
	ax	T	.478	2	116	2	2.617	20	.805	7	8.061 20
	<u>nin</u>]		4.074			20		2		2	.546 2

RISA-3D Version 17.0.2



Envelope Plate/Shell Principal Stresses (Continued)

	Plate		Surf	Sigma1 [ksi]	LC	Sigma2 [ksi]	LC	Tau Max (ksi)	LC	Angle [rad]	LC	Von Mises [ksi]	LC
459		max	B	6.753	21	6.402	20	1.018	8	2.194	10	6.563	20
460		min	and a state of the second	.231	2	-1.219	2		44	627	9	.978	4
461	P116	max	T	.808	8	256	3	2.092	21	.451	3	4.002	21
462		min		068	13	-3.791	21	.155	3	492	7	286	3
463		max	B	4.626	21	.125	13	2.549	21	1.877	2	4.879	21
464		min		.324	3	-1.009	8	.122	3	1.026	7	.293	3
465	<u>P117</u>	max	NYA DIA	2.874	25	.955	21	2.034	<u>2</u> 45	<u>2.349</u> 759	31 43	<u>3.622</u> 28	2
466		min	B	.252 1.118	2 2	-1.641 257	6	.025 1.897	4 <u>3</u>	2.312	40 10	3.376	2
467 468		max min		267	10	-2.675	2		5	512	44	.434	5
469	P118	max	T	6.75	8	943	8	4.542	2	2.355	26	9.425	2
470	2.0100200	min		649	2	-9.732	2	.595	6	785	15	1.167	5
471	25 - 65 - 66 - 66 - 66 - 66 - 66 - 66 -	max	B	8.301	2	1.325	2	3.488	2	2.278	7	7,724	2
472		min		283	8	-7.054	8	.362	10	-,729	6	.628	10
473	P119	max	Т	6.425	14	.464	9	3.629	14	.927	7	6.88	14
474		min		.693	6	-2.048	2	.221	6	4	3	.608	6
475		max	B	2,13	8	-1.306	4	2.36	8	2.093	44	4.181	24
476		min		-1.273	24	-4.67	24	498	4	781	-5	1.182	4
477	P120	max	T	5.535	20	<u>542</u>	12	3.708	20	.485	3	6.677	20
478		min	a And	074	2	-1.891	19		2	.256	12	.611	2
479		max	B	<u>.618</u>	2	53	13	1.263	20	<u>1.716</u> 522	9	<u>2.92</u> .52	20
480	D101	min		723	7	-3.196	20	.255	<u>13</u> 20	<u>.522</u> .793	C	6.608	13 20
481 482	<u>P121</u>	max		1.232	18 12	266 -5.936	2 20	3.56 .331	20	.793	8	.578	2
483		min max	B	3.517	8	1.109	20	1.516	8	.772	2	3.301	8
484		min		.378	13	- 97	2	.242	12	- 581	1	.467	13
485	P122	max	T	1.692	21	.869	23	.506	8	2.151	12	1.465	21
486		min	ý . W	.18	3	.177	3	8 1 E	26	- 647	13	.252	4
487		max	В	.308	7	377	3	1.334	20	.881	2	2.665	21
488		min	1. 19	168	12	-2.676	21	.226	3	.208	8	.419	3
489	P123	max	Т	4.898	8	.259	23	2.46	8	2.349	39	4.909	8
490		min	16 K	.036	4	4.049	2	.006	108	-,617	36	101	99
491		max	B	3.711	2	168	4	2.272	8	2.274	9	4.662	8
492		min		237	9	-4.772	8	.4	5	764	6	695	5
493	<u>P124</u>	max		4.442	8	039	9	<u>3.502</u>	2	2.316	_4 12	6.26	2
494		min		.591	<u>5</u> 2	<u>-5.045</u> -,221	2 4	. <u>63</u> 2.584	<u>6</u> 8	<u>758</u> 2.292	8 8	<u>1.145</u> 4.749	8
495 496		max	B	4.032	2 10	22 I -4 174	4 8	407	10	<u> </u>	7	4.749	11
490	P125	max	Ť	7.285	22	1.022	20	3.423	<u>14</u>	.482	8	7.005	14
497	<u> </u>	min		1.947	6	-1.603	20	.779	6	627	2	1.785	6
499	nie w staat of staat	max	В	1.404	7	-,76	4	2	7	2,351	36	3.524	8
500		min		-1.934	24	-3.385	20	.118	54	784	104	.665	4
501	P126	max	T	5.903	20	.041	13	3.734	20	.523	10	6.822	20
502		min		77 🐖	2	-1.566			2	.207	2		2
503		max	В	.806	3	428	28	.809	9	2.325	11	1.641	9
504		min		382	23	-1.664			45		7	.4	31
505	P127	max	T	3.932	20	124	<u>13</u>	<u>3.189</u>	20	.621	8	5.574	20
		min		.552	2			.382		.134	2	.683	2
507	1. State of the st	max	B	1.018	8	465	12	1.018	18	.554	2	1.792	18
508	.	min		22	12	-1.358		.123	12	578	9		12
509	<u>P128</u>	max	T Million	.748	11	.361	21 7	.356	8	2.349	104	.709	11
		min	D	.152	32	<u>441</u>			44	<u>772</u> 62	<u>108</u> 2	<u></u>	31
511		max	B	1.013	20 13	592	3	<u>1.726</u> .376	20 3	.62	2	.686	<u>20</u> 3
513	P129	<u>min</u> max	T	.044 8.77	ा ः 8	2.676	9	3.514	2	2.218	12	7.841	.8 .8
512	<u> </u>	min		639		-7,147	2	63	43	-76		1.172	5
515		max	В	7.301	2	.557	3	3.606	2	2.226	6	7.263	8
		THUR A		1.941									Ť

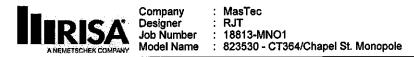
RISA-3D Version 17.0.2



Envelope Plate/Shell Principal Stresses (Continued)

Plate	SL	uf Sigma1 [ksi]	LC	Sigma2 [ksi]	LC	Tau Max [ksi]	LC	Angle [rad]	LC	Von Mises [ksi	
516	min	-3,573	9	-8.337	8	.122	10	.128	5	.598	5
517 P130	max	<u>T 4.879</u>	2	2.386	2	3.072	21	2.287	3	5.327	20
518	min	-2,048	8	-4.551	8	871	4	735	12	1.526	4
	independent and in the second state of the	B <u>5.438</u>	8	3.229	8	2.93	14 44	<u>.354</u> 035	<u>10</u> 3	<u>5.405</u> 1,765	20 48
<u>520</u>	min	<u>-2.123</u>	2	4.968	2	<u>.985</u> 4.118	<u>44</u> 20	2.356	2	8.362	20
521 P131	max	<u>T 8.483</u> 1.383	20	.508	6	4.118	4	724	3	2.059	4
<u>522</u> 523	min 👘	B 3.973	2	.257	2	3.109	8	2.282	7	5.782	8
524	min	215	STATISTICS AND ADDRESS	-5.215		105	50	- 756	6	.213	50
525 P132		T 5.064	18	.329	3	3.758	20	.517	8	6.623	20
526	min_	1.342	12	-2.616	8		13	251	2	1.525	13
		<u>B 3.633</u>	20	1.089	20	1.33	<u>18</u>	.968	12	3.253	18
528	min		13	499	13	.031	11	635	9	.352	12
529 P133	max	<u>T 6.272</u>	20	.527	10	3.025	<u>20</u> 2	.692	<u>13</u> 3	6.164 .475	20 2
530	min	.296	2	486	4	. <u>274</u> 2.215	<u>2</u> 19	.166	3	4.233	21
531 532	A 1998 Problem Press 2010	B <u>1.298</u> -1.103	3	481	21	61	7	383	8.	1.357	13
532 533 P134	min max	T 3.537	22	.702	12	1.762	20	.787	9	3.505	21
534		802	3	-1.222	8.4	**** <u>242</u>	13	039	2	.874	3
535		B 1.502	8	775	3	2.107	20	.281	2	4.088	21
536	min	807		4.011	22	.261	13	492	11	.785	3
537 P135	max	T 16.208	8	3.465	8	6.372	8	.874	7	14.783	8
538	min	-4.455	2	-15.128	2	.789	5.	503	3	1.379	5
	MANUAR AND STREET AND	B <u>15.38</u>	2	4.244	2	6.411	8	2.294	20	15.23	8
540	min	4.013	8	-16.835	8.	.233	40	726	2 9 7	423	40 2
	max	<u>T 8.278</u> 412	8	.143	9	5,461 .888	2 6	.945	3	1.647	6
542 543	menter of the two works	B 8,943	4	2.269	14	6.174	8	2.201	11	10.821	8
544	max	<u> </u>	C C Lindonbaarr - M	-7.83	8	.26	Ĭ	504	10	.728	11
545 P137	max	T 10.878	20	.932	4	5.608	20	2.353	12	11.05	20
546		1.069		-2.915	13	432	3	489	11	1.232	
547	max	B 6.193	2	.566	20	3.43	2	2,202	6	6.552	2
548	min	.438	6	-2.925	* 8 -	.536	6	345	5	.934	6
549 P138	Advertising the second s	T <u>5.976</u>	15	.357	2	4.445	20	.714	8	7.802	20
550	min	1.679	11	-3,685	8	1,232	13	077	2	2,347	12
551	PARTICIPATION OF TAXABLE PARTY	<u>B 10.937</u> .514	20	<u>1.571</u> - 445	18	<u>4.686</u> .283	20 13	. <u>548</u> 585	2	10.244	20 13
552 553 P139	min	T 10.556	20	381	2	6.648	20	.058	8	12.16	20
554 F159	max min	.925	2	-2.74	20	.653	2	395	2	1.163	$\tilde{2}$
555		B 2.627	3	- 197	44	1.624	15	1.923	7	2.929	15
556	min	162	7	-2.19	8	443	32	085	6	.792	32
557 P140	max	T 1.432	14	244	2	3.223	21	.063	8	5.977	20
558	min	731	8	-5.371		.656				1.157	
559		<u>B 3.424</u>	8	1.011	8	1.206	8	2.348	5	3.047	8
		313	2	-1.058			4	272	4		4
561 P141		T <u>1.402</u>	8	175	7	1.932	21	1.512	<u>6</u> 3	4.49	24
562	min	<u>-1.807</u>	<u>13</u> 2	<u>-5.006</u> 1.203	<u>24</u> 24	.178	4 8	1.83	10	4.379	2
563 564	max min	B 4.713 -,121		-3.979	8		43	764	20		
564 565 P142		T 8.212	2	1.62	14	3.485	2	1.52	9	7.667	2
566	min					.206	5	6	10	.563	5
567		B 1.216	7	991	5	2.451	24	2.1	7	5,578	24
568		-1.167	24		24	.387	5	.735	3	.902	5
569 P143		T 6.107	20	1.649	8	2.324	20	.43	4	5.525	20
570	min	065	2		2	.181			2		3
571	max	B <u>1.901</u>	2	. <u>195</u>	2	2.8	8	2.251	12	6.267	8
572	min		8	<u>-6.77</u>	8	.291	4	388	43	.571	-4

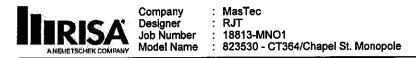
RISA-3D Version 17.0.2



Envelope Plate/Shell Principal Stresses (Continued)

	Tau Max [ksi] LC Angle [rad] LC Von Mises [ksi] LC
578 mn 122 29 -1517 2 104 30 $.752$ 29 16 579 max B 2.577 8 -119 5 2.685 2 2.351 8 4.736 580 min 051 5 3.577 22 035 5 7.76 7 151 581 P146 max T 4.383 2 1.714 14 2.002 2 1.64 8 4.206 583 P147 max T 3.677 20 1.717 20 1.253 20 2.287 13 3.254 585 P147 max T 3.677 20 1.717 20 1.253 20 2.287 13 3.254 586 P147 max B 544 2 -612 4 2.086 20 2.332 2 4.592 588 P148 max T 3.227 8 -0.78	
580 min Jobi 5 -3.677 22 Jobis 75 -7.36 7 .151 581 P146 max T 4.383 2 1.714 14 2.002 2 1.164 8 4.206 582 min 0.99 7 1.473 8 201 5 3.855 14 2.206 7 4.683 584 min 1.593 21 1.5265 24 3.15 5 67/2 3 .906 585 P147 max T 3.677 20 1.171 20 1.253 20 2.287 13 3.254 586 min 3.677 3 4.086 20 2.332 2 4.592 588 min .8544 2 -612 4 2.086 20 2.332 2 1.911 590 max T 1.327 8 -078 4 1.095 3 <td></td>	
581 P146 max T 4.383 2 1.714 14 2.002 2 1.164 8 4.206 582 min 0.09 7 1.1479 8 201 5 3.61 22 553 583 max B 875 2 -1.039 5 1.855 1.4 2.00 7 4.683 584 min 1.593 21 5.265 24 3.15 5 6.72 3 .906 585 P147 max T 3.677 20 1.171 20 1.253 20 2.287 1.3 3.254 586 min 895 8 492 20 2.986 20 2.332 2 4.592 588 min	
583 max B 375 2 -1.039 5 1.855 14 2.206 7 4.683 584 min 1.693 21 5.265 24 315 5 672 3 906 585 P147 max T 3.677 20 1.171 20 2.287 13 3.254 586 min .307 3 .1261 2 135 4 121 121 .345 588 max B .544 2 -612 4 2.086 20 2.332 2 4.592 588 max T 1.327 8 -078 4 1.095 8 2.193 2 1.911 590 min .057 4 .863 .8088 4 .595 13 .118 591 max T 2.515 24 .001 4 1.311 24 2.353 32	
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601 P151 max T 1.912 20 .709 21 .741 8 1.941 12 1.675 602 min .203 4 .612 2 .035 4 .514 5 .178 603 max B .198 2 678 4 1.531 21 2.137 12 3.53 604 min .816 24 -3.86 21 .25 44 1.26 2 .609 605 P152 max T 3.23 20 .032 12 1.807 8 1.792 2 3.387 606 min .217 3 511 8 183 4 .554 7 .359 607 max B .932 21 .039 2 2.639 21 2.119 4 4.879 608 min .125 4 .4346 21 .082 3<	
603 max B .198 2 678 4 1.531 21 2.137 12 3.53 604 min 816 24 -3.86 21 .25 41 1.26 2 609 605 P152 max T 3.23 20 .032 12 1.807 8 1.792 2 3.387 606 min .217 3 511 8 .183 4 .554 7 .359 607 max B .932 21 .039 2 2.639 21 2.119 4 4.879 608 min .125 4 -4.346 21 .082 3 .611 2 .182 609 P153 max T 3.955 2 2.837 2 3.043 21 2.204 4 6.008 610 min -1.828 7 -6.595 8 .262 4 9.36 3 .481 611 max B 5.829 <td< td=""><td></td></td<>	
604 min 816 24 -3.86 21 .25 41 1.26 2 609 605 P152 max T 3.23 20 .032 12 1.807 8 1.792 2 3.387 606 min .217 3 511 8 183 4 .554 7 .359 607 max B .932 21 .039 2 2.639 21 2.119 4 4.879 608 min .125 4 -4.346 21 .082 3 .611 2 .182 609 P153 max T 3.955 2 2.837 2 3.043 21 2.204 4 6.008 610 min -1.828 7 -6.595 8 .262 4 9.36 3 .481 611 max B 5.829 8 2.245 8 2.363 <td< td=""><td></td></td<>	
605 P152 max T 3.23 20 0.32 12 1.807 8 1.792 2 3.387 606 min 2/17 3 -511 8 183 4 .554 7 .359 607 max B .932 21 .039 2 2.639 21 2.119 4 4.879 608 min .125 4 -4.346 21 0.82 3 .611 2 .182 609 P153 max T 3.955 2 2.837 2 3.043 21 2.204 4 6.008 610 min -1.828 7 -6.595 8 .262 4 9.36 3 .481 611 max B 5.829 8 2.245 8 2.363 2 1.014 2 5.94 612 min -1.943 2 -6.668 2 .376 <t< td=""><td></td></t<>	
606 min 217 3 -511 8 183 4 .554 7 .359 607 max B .932 21 .039 2 2.639 21 2.119 4 4.879 608 min .125 4 .4346 21 .082 3 .611 2 .182 609 P153 max T 3.955 2 2.837 2 3.043 21 2.204 4 6.008 610 min -1.828 7 -6.595 8 .262 4 936 3 .481 611 max B 5.829 8 2.245 8 2.363 2 1.014 2 5.94 612 min -1.943 2 -6.668 2 .376 5 274 7 .839 613 P154 max T 8.445 8 2.441 8 3.002 8<	
607 max B .932 21 .039 2 2.639 21 2.119 4 4.879 608 min .125 4 .4346 21 .082 3 .611 2 .182 609 P153 max T 3.955 2 2.837 2 3.043 21 2.204 4 6.008 610 min -1.828 7 -6.595 8 .262 4 936 3 481 611 max B 5.829 8 2.245 8 2.363 2 1.014 2 5.94 612 min -1.943 2 -6.668 2 .376 5 274 7 .639 613 P154 max T 8.445 8 2.441 8 3.002 8 1.581 13 7.527 614 min -1.943 2 -6.271 2 .28	
608 min .125 4 .4.346 21 .082 3 .611 2 .182 609 P153 max T 3.955 2 2.837 2 3.043 21 2.204 4 6.008 610 min -1.828 7 -6.595 8 .262 4 936 3 .481 611 max B 5.829 8 2.245 8 2.363 2 1.014 2 5.94 612 min -1.943 2 -6.668 2 .376 5 274 7 .839 613 P154 max T 8.445 8 2.441 8 3.002 8 1.581 13 7.527 614 min -1.943 2 -6.271 2 .28 11 .218 10 .509 615 max B 2.732 2 -1.273 4 3.031	
609 P153 max T 3.955 2 2.837 2 3.043 21 2.204 4 6.008 610 min -1.828 7 -6.595 8 2.62 4 936 3 481 611 max B 5.829 8 2.245 8 2.363 2 1.014 2 5.94 612 min -1.943 2 -6.668 2 .376 5 .274 7 .839 613 P154 max T 8.445 8 2.441 8 3.002 8 1.581 13 7.527 614 min -1.943 2 -6.271 2 .28 11 218 10 .509 614 min -1.943 2 -6.271 2 .28 11 .218 10 .509 615 max B 2.732 2 -1.273 4 3.031	
610 min -1.828 7 -6.595 8 .262 4 936 3 .481 611 max B 5.829 8 2.245 8 2.363 2 1.014 2 5.94 612 min -1.943 2 -6.668 2 .376 5 274 7 .839 613 P154 max T 8.445 8 2.441 8 3.002 8 1.581 13 7.527 614 min -1.943 2 -6.274 2 .28 11 .218 10 .509 615 max B 2.732 2 -1.273 4 3.031 2 2.131 7 6.547	
611 max B 5.829 8 2.245 8 2.363 2 1.014 2 5.94 612 min -1.943 2 -6.668 2 .376 5 274 7 .839 613 P154 max T 8.445 8 2.441 8 3.002 8 1.581 13 7.527 614 min -1.943 2 -6.271 2 .28 11 .218 10 .509 615 max B 2.732 2 -1.273 4 3.031 2 2.131 7 6.547	
612 min -1.943 2 -6.668 2 .376 5 274 7 .639 613 P154 max T 8.445 8 2.441 8 3.002 8 1.581 13 7.527 614 min -1.943 2 -6.274 2 .28 11 .218 10 .509 615 max B 2.732 2 -1.273 4 3.031 2 2.131 7 6.547	
613 P154 max T 8.445 8 2.441 8 3.002 8 1.581 13 7.527 614 min -1.943 2 -6.271 2 .28 11 .218 10 .509 615 max B 2.732 2 -1.273 4 3.031 2 2.131 7 6.547	
614 min -1.943 2 -6.271 2 .28 11 .218 10 .509 615 max B 2.732 2 -1.273 4 3.031 2 2.131 7 6.547	3.002 8 1.581 13 7.527 8
616 min -2.103 22 -6.982 8 518 4 938 2 1.173	
617 P155 max T 1.495 2 .528 2 .818 8 2.349 39 1.922	818 8 2.349 39 1.922 8
618 min -483 8 -2.118 8 029 26 -735 38 101	
619 max B 1.734 8 025 7 1.192 20 2.348 9 2.629 620 min 686 14 -2.86 23 .211 .4 587 8 .585	
621 P156 max T 4.206 21 .732 8 2.046 21 1.495 2 4.15 622 min 171 3 808 2 .339 3 .53 7 .611	
623 max B .592 2099 3 1.603 20 2.286 11 3.803	
624 min -1.045 22 4:202 2018 4729 4403	18 4 -729 4 .403 4
625 P157 max T 3.475 19 .874 19 1.3 19 2.273 10 3.13	
	23 12 2.151 13 57 12
627 max B15 12598 12 1.337 19 .763 5 3.112	1.337 19 .763 5 3.112 19
628 min -741 19 -3.416 19 -224 12 657 12 539	
629 P158 max T .411 14471 12 2.876 19 2.136 10 5.628	2.876 19 2.136 10 5.628 19

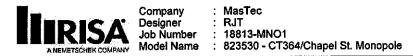
RISA-3D Version 17.0.2



Envelope Plate/Shell Principal Stresses (Continued)

Envelope Flate/S	Surf,	Sigma1 [ksi]	LC	Sigma2 [ksi]	LC	Tau Max (ksi)	LC	Angle [rad]	LC	Von Mises (ksi] LC
Plate 630	min	- 124	9	-5,496	119	371	12	1,978	L. Walksonson, A.L.	65 12
631	max B	6.401	19	.667	19	2.867	19	.505	4	6.095 19
632	min		12	.035		.247	12	.359	12	
633 P159	max T	3.017	21	432	9	2.737	19	052	11	4.748 19
634	min	- 011	4	-2.676	16	.39	12	381	4	.746 12
635	max B	253	10	-1.336	12	3.692	19	1.945	3	8.069 19
636	min 🚈	-1.331	16	-8.613	19	.493	12	1.908	10	1.2 12
637 P160	max T	5.043	19	482	11	3.582	20	.65	12	6.374 20
638	min	<u>.614 mt</u>	12	-2.288	15	.694	<u>11</u>	244	9	1.221 11
639	max B	.357	9	867	9	4.741	15	1.343	13	<u> 10.415 15</u>
640	min	-1.665	15	-11.147	15	.612	9	.855	9	1.09 9
641 P161	max T	.651	9	67	9	3.871	15	1.25	12	7.795 15
642	min	- 137	24	-7.846	15	.608	8	.336	9	1.058 8 7.027 15
643	max B	8.344	15	1.105	<u>19</u>	3.727	<u>15</u> 9	<u>395</u> 571	4	7.937 15 1.387 9
644	min	1.572	9	03		1.656	9 19	1.512	12	3.825 19
645 P162	max T	4.189	18 11	1.055	<u> 15</u> 9	331	11	.582	9	.775 11
	min max B	.152	10	849	12	1.759	<u>19</u>	2.326	11	3.941 18
647 648	max B	11 ISSUED (1997)	15	-4.27	18	.305	12	785	· Frank & Architek A. I.	.758 12
649 P163	max T	.338	19	918	12	2.658	19	.313	9	5.155 19
650	min	018	4	4.978	19	.461	12	.185	12	
651	max B	5.833	19	018	12	3.17	19	1.93	7	6.102 19
652	min	The state of the second s	12	- 507	19	.555	12	1,818	12	1.101 12
653 P164	max T	734	12	-1.582	12	2,718	19	515	11	9.257 19
654	min		19	-10.688	19	.424	12	668	4	1.371 12
655	max B	8.37	19	7.364	19	.6	14	1.939	4	7.915 19
656	min	1:404	12	.855	12	.126	45	.802	9	1.226 12
657 P165	max T	6.109	19	-,346	10	4.089	19	279	10	7.364 19
658	min	.627	12	-2.267	16	.621	12	433	4	1.076 12
659	max B	<u>378</u>	12	<u>-1.253</u>	12	2.142	19	1.938	3	5.649 19
660		-2.156	20	-6.402	119	.437	12	1.534	10	1.113 12
661 P166	max T	7.817	18	378	10	4.754	18	.498	12	8.785 18 1.955 12
662	min	1.588	12	-1.814	16	1.092 2.98	12 15	<u></u>	9	1,955 12 7.662 15
663	max B	203	9 15	898	9 15	2.98	9	1.351	12	.816 9
664	min T	141	9	-1.239	9	3.37	15	.804	12	11.823 15
665 P167	<u>max T</u>	-6.912	15	-13.651		.428	İŎ	-,204	9	1.175 9
667	max B	10.811	15	9.224	15	.794	15	2.043	12	10.111 15
668	min	1.78	9	1.08	9	.026	11	.579	10	1.553 9
669 P168	max T	1.657	9	604	9	3.358	19	.125	12	6.249 18
670	min	-1.123	3	-6.192	15		12	-,514	10	1:237 11
671	max B	7.122	15	.702	4	3.959	18	1.514	12	7.391 15
672	max B	.887	9.	-1.447	10	.764	12	.996	9	1,558 11
673 P169	max T	2.309	19	1.011	19	.655	21	1.672	4	2.005 19
674	min	.399	12	.22		<u>nee079</u>	12	1.109	12	.348 12
675	max B	05	11	626	12	1.485	19	353	10	3.116 19
676	min	293	25	-3.244			12	583		.6 12
677 P170	max T	.966	16	-1.039	12	3.72	19	<u>682</u>	12	7.023 19
678	min		10	-6.515			12	716	9	1.174 12
679	max B	3.712	19	1.288	16	1.213	21	.55	10	3.265 19
680	min 🖳		12			116	12	464	13	368 12
681 P171	max T	6.215	19	428	9	4.059	19	295 407	<u>10</u> 4	7.353 19
682	min		12			712	12	407 2.017	4	3.432 19
683	max B	119	12 20	774 -3.816	12	<u>1.416</u> .328	19 12	1.429	10	.722 19
<u>.684</u>	min max T	-1:02	18	.128	10	4.753	15	.446	13	8.718 15
685 P172		7.851		-1.883	15			.440	9	1.859 9
686	min	601/102		000.1*1.000	Sin		18 0 18			

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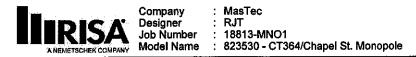
Envelope Plate/Shell Principal Stresses (Continued)

	Plate		Surf	Sigma1 [ksi]	LC	Sigma2 (ksi)	LC	Tau Max [ksi]	LC	Angle [rad]	LC	Von Mises [ksi]	LC
687		max		2	12	988	9	2.123	15	1.563	28	4,995	15
688		min	free al contra	-1.388	19	-5.503	-15	.271	9	1.214	10	.857	9
689	P173	max	T	.995	20	285	9	4.592	15	.854	12	8.77	15
690		min		.179	12	-8.288	15	498	<u>9</u>	.095	9	.886	10
<u>691</u>	and unified a state of the stat	max	B	5.097	15	1.594	15	1.751	15	042	10	4.516	15
<u>692</u>		imin		.232	9	118	10	.051	<u>9</u> 15	<u>532</u> 1.966	<u>29</u> 20	.201 2.528	<u>9</u> 18
693	<u>P174</u>	max		2,914 521	18 11	1.355	19 13	.943 .153	13 11	642	6	.453	11
<u>694</u> 695		min	В	.097	<u>高調務</u> 12	613	9	1.781	<u></u>	.808	9	3.743	15
696		max		-,465	19	-3,901	15	.22	29 L	.31	12	.547	9
697	P175	max	Т	1.172	22	.335	15	.446 _	22	1.267	5	1.06	22
698		min		176	5	.014	9	.03	. 5	152	4	.155	5
699		max	B	.838	19	- 691	12	1.893	19	26	9	3.445	18
700		min		.151	12	-2.956	18	.421	12	456	13	.778	12
701	P176	max	<u> </u>	4.119	19	- <u>.395</u>	12	3.182	19	502	12	5.591	19
702		min		.853	12	-2.265	20	.624	12	532	9	1.104	12
703		max	B	.311	4	369	11	.847	20	.537	10	1.619	20
704		min		-:018	35	-1.533	20	.203	11	423	<u>12</u> 41	.388 7.114	11 19
705	<u>P177</u>	max		6.37 1.181	20 12	067 -1.326	13	<u>3.842</u> 625	<u>19</u>	<u>456</u> 491	41	1.217	12
706 707		min	B	008	9	323	12	.784	21	.762	10	1.914	21
707		max		665	24	323	21	./04	12	609	13	.285	12
709	P178	max	T	8.33	15	.445	10	4.369	15	.558	4	8.541	15
710		min		1.856	9	793	4	74	9	.197	10	1,7	9
711		max	В	.138	4	211	12	.738	16	2.318	17	2.789	19
712		min		-1,848	21	-3.209	19	.005	11	736	5	.201	12
713	P179	max	Т	4.487	18	.14	9	3.743	15	.722	12	6.52	15
714		min		.955	11	-3.043	15	.554	<u>9</u>	.018	9	1.142	10
715		max	B	.909	12	32	12	1.283	15	.801	9 33	2.27	<u>15</u> 10
716	D400	min	Т	-,542	6	-1,769 .368	<u>18</u> 20	.09 .811	8	<u>-,382</u> 2.239	<u>33</u> 45	.468 1.826	19
717 718	<u>P180</u>	max min		1.98	19 12	-1.214	13	.043	11	739	-6	.139	11
719	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	max	В	1.119	15	455	12	2.147	18	.662	9	3.944	18
720		min		-:049		-3.485	The head of the	.498	İŤ	023	12	.896	1
721	P181	max	T	4,437	19	.756	24	1.894	19	473	3	4.151	19
722		min	an sinter	1.004	12	.014	8	.363	12	779	10	.898	12
723		max	B	.06	7	-1.073	12	2.241	19	.498	10	4.798	19
724		min		739	25	-5.061	19		12	.241	4	.96	12
725	P182	max	T	6.536	19	.915	20	2.852	19	445	52	6.162	19
726		min		1.219	12	069	12	.606 2.363	12	<u>507</u> .337	11 9	<u>1.216</u> 4,774	<u>12</u> 19
727		max	B	.744	3 9	- <u>,862</u> -4,853	12 19	.594	9	041		4.774	12
728 729	P183	max		4.848	15	311	12	3.629	18	225	4	6.379	18
730	<u> </u>	min		~869	9	-2.64	20		12	376	10	1.606	9
731		max	B	3.03	19	1,295	19	.868	19	.642	10	2.634	19
732		min		.553	11	-,148	12	.143		541	12	.479	11
733	P184	max		6.274	19	-,198	10	4.172	18	.443	4	7.515	18
734		min		1.455	12	-2.302	16		12	047	10	1.786	12
735	POINT OF THE REPORT OF THE POINT max		2,906	3	1.207	16	1.122	3	2.351	35	2.638	3	
VIIII 203 - 48 2154		min	_		10	-1.495	9		21		29		<u>11</u>
737	<u>P185</u>	max		7.128	15	.955	4	<u>3.337</u> 705	15	.615	9 4	6.913 1.221	15 9
738		min		693	<u>9</u> 10	- <u>.862</u> 572	<u>10</u> 10	.705 2.921	9 18	<u>.455</u> .021	4 4	5.526	9 15
739		max		1.158	4	-5.186	15	.764	12	-,407	9	1.356	8
<u>*//40</u> 741	P186	max		5.638	19	1.863	6	2.462	15	.788	13	5.06	19
742		min			12	-1.73	13	.328	8	063	- WY:	1.113	11
743		max	1 -	1.753	13	465	12	2.785	15	2.312	8	5.62	18
	A 2D Version 1											Page 8	

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Envelope Plate/Shell Principal Stresses (Continued)

Plate	Su	f Sigma1 [ksi]	LC	Sigma2 [ksi]	LC		C Angle [rad]	LC Von Mises [ksi] LC
744	min	-2:022	7	-6.205	19		9753	7 1.158 11
745 P187	max]	<u> </u>	15	983	12		9.321	12 6.694 19
746	min	152	9	-5.784	19		2 135	9 1.434 12 12 3.657 21
	max E min	3.422	21	.084 -:562	7 25		<u>21 1.957</u> 4 1.619	<u>12 3.657 21</u> 8 .488 4
748 749 P188	max]	10.465	19	592	12	And the second se	9 .113	13 12.074 19
749 P188 750	min	2.108	12	-2,746	19		2 .043	10 2,458 12
	max E		3	018	5		5 2.353	35 2.509 15
	torney of their second sector backs	.129	8	-1.15	10		6 .778	29 645 6
	max 1	5.951	15	251	12		8222	13 8.159 15
754	min		9	4,116	20		1	9 2.198 11
	<u>max E</u>		19	1.249	16		9.5	10 10.266 19
756		1,869	12	.232	10		2 .24	4 1.763 12
	max	<u>6.671</u>	19	<u>156</u>	12		9 .544 2 .333	4 9.657 19 11 1.581 12
758	<u>min</u> max E	Contraction of the second second second second second second second second second second second second second s	<u>12</u> 15	<u>-4.427</u> 1.154	15		5 2.323	7 10.92 15
759 760	max E min	1.26	9%	907	9		1699	6 1.759 10
	max 1	10.615	15	291	9		5 .105	12 13.03 15
Second St. Highlight Steels 1 - Characterized States States 1 200 - 1000	min	1.927		-3.927	15		9483	9 2.123 9
	max E		12	.979	25		7	37 3.044 6
764	min	.468	5	-2.709	6		722	4 .717 109
	max 1		9	113	9		9 .249	12 7.848 15
	min 🔅	-1.103	13	-7.138	15		1637	9 1.734 11
	max E		15	1.184	3		9 2.192	12 4.927 19
768	min	.019	9	-3.591	9 12	The set of the set of	1.916 9 1.252	9 798 11 9 4.982 19
	max 1	158	12 19	869 -5.683	19		2 786	12 .802 12
770	min max E		19	2.043	19		4 2.222	4 2.228 19
and the second	min	455	12	154	12		<u></u>	25 .401 12
	max 1	6.972	19	1.616	19		9283	4 6.321 19
774	min	855	12	.137 Line	12		2332	52 .796 12
	max E		12	675	12		9 1.186	9 6.338 19
776	min	- 743	19	-6.677	19		2. 921	12 .704 12
	<u>max </u>]		15	2.015	15		5 .541	9 7.925 15
778	<u>min in</u>		9	<u>.303</u>	9		9 .268	<u>12 .801 9</u> 4 7.833 18
	<u>max E</u>	153	4	-1.736 -8.382	12 18		8 2.125 2 1.823	4 7.833 18 10 1.649 12
	min max 1	318	9	-1.301	12		9 2.092	<u>4 6.403 18</u>
782	min	-2,502	15	-7,252	18		2 1.863	12 1.127 12
	max E		15	2.385	17		3 1.284	9 2.857 15
784	min 🐭	.666	11		9		175	13 .588 11
785 P197	max 1		19_	15	4	1.024 1	9 .016	12 1.779 19
		· 152			19	.152 1	2434	9
787	<u>max E</u>	1.488	19	45	12		9 1.168	12 4.037 19
	min						2 1.065	9 606 12
	<u>max </u>]		19	1.398	19		9094	4 <u>3.586</u> <u>19</u> 8 <u>.431</u> <u>12</u>
	min			.167 759	12 12		<u>2 - 36</u> 9 1.116	9 5.349 19
	<u>max E</u> min		<u>12</u>	/59 -5,699			2 .97	12
	max 1	5.262	15	1.815	19		5 .395	4 4.634 15
	min			.327	4	.184	9	
	max E		4	-1.455	12		5 2.214	4 6.459 18
		-1.425	21	-7.037	18		9 1.819	10 1.414 12
797 P200	max 1	1.263	15	085	9	1.142 1	5 .766	10 1.981 15
798	min	.159	9	-1.021			9 .233	4 .214 9
799	max E		15	526	10	2.666 1	<u>5 2.235</u>	12 4.721 15
800	min	.26	10	-3.65	15	.393	0 1.691	9 .694 10

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Envelope Plate/Shell Principal Stresses (Continued)

	Plate		Surf	Sigma1 [ksi]	LC	Sigma2 [ksi]	LC	Tau Max [ksi]	LC	Angle [rad]	<u> </u>	Von Mises [ksi	
801	P201	max	T	3.733	19	.009	13	1.966	19	596	9	3.836	19
802		min		.482	12	199	19	.237	12	753	13	.478	12
803		max	B	1.155	19	737	12	3.188	19	1.036	7	5.883	19
804		min		.196	12	-5:22	19	.467	12	1.013	4	.852	12
805	P202	max	<u> </u>	1.906	19	.902	19	.502	19	2.051	4	1.651	19
806		min		.233	12	.169	12	.011	3	65	36	.208	12
807		max	B	255	4	984	12	1.835	19	1.255	4	4.367	19
808	<u>(注意)</u> (1997年)	min		-1.159	18	-4.829	19	.344	12	1.006	12	.874	12
809	P203	max	T	2.77	19	<u> </u>	21	.637	15	<u>1.004</u>	4	2.406	19
810		min	13	.439	12	042	13	13	8	.017	10	.423	12
811		max	B	.662	4	-1.12	12	2.156	15	2.29	13	5.292	18
812		min		-2.085	21	-5.999	18	.354	9	1.64	9	1.171	12
813	P204	max	T	4.39	18	052	11	2,325	18	.803	9	4.526	18
814		min	1924 - S.	.863	12	259	18	.464	12	.475	12	.897	12
815		max	B	1.341	15	678	9	3.816	15	2.154	12	7.058	15
816		min	4.26	.128	10	-6.291	15	.406	9	2.012	-9	.754	9
817	P205	max	T	5.246	19	.12	9	2.704	19	2.133	9	5.329	19
818	and the second	min	$\mathcal{M} = \mathcal{U}$.891	12	406	3	.607	12	1,871	12	1.089	12
819		max	B	193	12	<u>719</u>	12	1.753	19	.964	9	4.364	19
820		min		-1:384	20	4.888	19	.263	12	.638	12	.644	12
821	P206	max	T	.234	4	.179	3	.201	23	1.691	8	.768	21
822		min	2000-000 2009-000	509	20	885	21	.011	8	-,521	4	.136	5
823		max	B	094	9	946	12	1.397	19	1.646	13	3.394	19
824		min			15		19	.378	12	1.146	9		12
825	P207	max	T	1.667	10	.409	10	.716	21	2.339	16	1.62	4
826	制度 计成本控制	min	推的。	538	4	-1.821	4	.083	49	784	52	.191	47
827		max	В	.859	3	885	12	1.945	15	2.197	13	5.092	19
828		min	1. A	-1.99	21	-5.783	19	,454	11	1.289	9	1.167	48
829	P208	max	Т	5.944	<u>17</u>	1.116	4	3.808	19	1.19	4	6.905	19
830		min		1.085	11	-1.838	21	.271	12	.887	12	1.002	12
831		max	B	.511	10	402	10	2.317	15	2.339	11	5.241	15
832		min	ŝ	-1.055	15	-5:689	15	.413	9	687	6	,715	9 (

APPENDIX D

ADDITIONAL CALCUATIONS

.



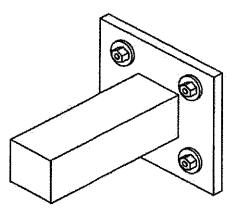
Bolt Calcuations:

Plate Calculations:

Bolt Size,	5/8	n na stran ang Sabanas
# Bolts	4	
Plate Width:	8.5	
Plate Height:	8.5	ality and the second second second second second second second second second second second second second second Second second
Bolt H Gap:	6	
Bolt V Gap:	6	
Plate Tra	0.75	
Bolt Grade:	A325N	
Fu _{bolt}	120	
r	4,243	
J. H.	72:000	
Bolt Area, _{Normal}	0.307	
Bolt Area, Net Tensile:	0.226	

Allowable Shear:	
Allowable Tension	20.3

Tension Capacity:	92 3%
Shear Capacity:	1176 219/6%
Combined Capacity:	85.7%



Bolt Capacity. 92.3%

Horizontal Member Height	6	i ner amera i signat
Horizontal Mémber Width	4	Mary Mary 1997 - Andrew State - Andr
Plate Grade:	A36	
Plate Fy		

Mix =7.860	:
Mz = 0.000	10.10

Zx =	1.195	14	
-Zz =	1.195		

	887/288 La mint -
ØMpx (X) =	38.728

Plate Capacity: 20.3%



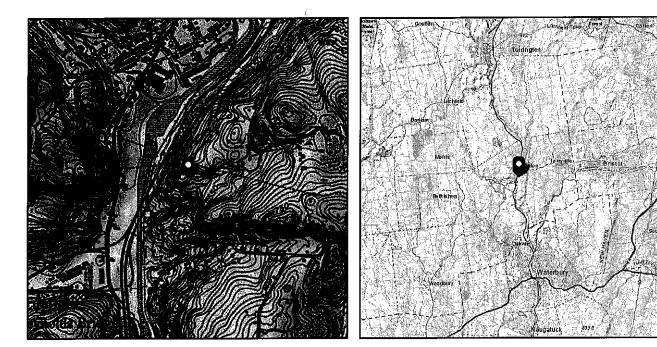
No Address at This

Location

ASCE 7 Hazards Report

Standard:ASCE/SEI 7-10Risk Category:IISoil Class:D - Stiff Soil

Elevation: 543 ft (NAVD 88) Latitude: 41.663467 Longitude: -73.074281



Wind

Results:

Wind Speed:	118 Vmph	Litchfield County and Thomaston Require an
10-year MRI	76 Vmph	ultimate wind speed of 120 mph.
25-year MRI	85 Vmph	
50-year MRI	91 Vmph	
100-year MRI	97 Vmph	
Data Source:	ASCE/SEI 7-10 March 12, 2014), Fig. 26.5-1A and Figs. CC-1–CC-4, incorporating errata of 4
Date Accessed:	Fri Jun 07 2019	9

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

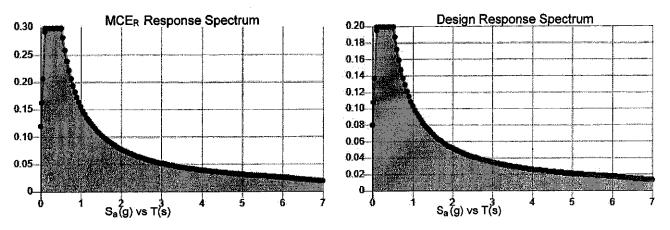
Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.



Site Soil Class: Results:	D - Stiff Soil			
S _s :	0.186	S _{DS} :	0.199	
S 1 :	0.064	S _{D1} :	0.103	
F _a :	1.6	Τ _L :	6	
F _v :	2.4	PGA :	0.096	
S _{MS} :	0.298	PGA M:	0.153	
S _{M1} :	0.155	F _{PGA} :	1.6	
		le :	1	

Seismic Design Category



Data Accessed: Date Source:

Fri Jun 07 2019

В

USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.



Ice

Results:

Ice Thickness:	0.75 in.
Concurrent Temperature:	5 F
Gust Speed:	50 mph
Data Source:	Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Date Accessed:	Fri Jun 07 2019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

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Exhibit F

Power Density/RF Emissions Report

Wireless Network Design and Deployment

Radio Frequency Emissions Analysis Report

T-MOBILE Existing Facility

Site ID: CT11364B

CT364/Chapel St. Monopole 580 Chapel Street Thomaston, CT 06787

May 31, 2019

Transcom Engineering Project Number: 737001-0110

Site Compliance Summary		
Compliance Status: COMPLIANT		
Site total MPE% of FCC general population allowable limit:	23.48 %	

Wireless Network Design and Deployment

May 31, 2019

T-MOBILE Attn: Jason Overbey, RF Manager 35 Griffin Road South Bloomfield, CT 6009

Emissions Analysis for Site: CT11364B - CT364/Chapel St. Monopole

Transcom Engineering, Inc ("Transcom") was directed to analyze the proposed upgrades to the T-MOBILE facility located at **580 Chapel Street, Thomaston, CT**, for the purpose of determining whether the emissions from the Proposed T-MOBILE Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter (μ W/cm2). The number of μ W/cm² calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

<u>General population/uncontrolled exposure</u> limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter (μ W/cm²). The general population exposure limits for the 600 & 700 MHz bands are approximately 400 μ W/cm² and 467 μ W/cm² respectively. The general population exposure limit for the 1900 MHz (PCS) and 2100 MHz (AWS) bands is 1000 μ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Wireless Network Design and Deployment

<u>Occupational/controlled exposure</u> limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over this or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

Wireless Network Design and Deployment

CALCULATIONS

Calculations were performed for the proposed upgrades to the T-MOBILE antenna facility located at **580 Chapel Street, Thomaston, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-MOBILE is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in *Table 1*:

Technology	Frequency Band	Channel Count	Transmit Power per Channel (W)
LTE	1900 MHz (PCS)	4	40
LTE	2100 MHz (AWS)	2	60
GSM	1900 MHz (PCS)	1	15
LTE / 5G NR	600 MHz	2	40
LTE	700 MHz	2	20

Table 1: Channel Data Table

Wireless Network Design and Deployment

The following antennas listed in *Table 2* were used in the modeling for transmission in the 600, 700 MHz, 1900 MHz (PCS) and 2100 MHz (AWS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

	Antenna		Antenna Centerline
Sector	Number	Antenna Make / Model	(ft)
А	1	RFS APXVAARR24_43-U-NA20	172
А	2	EMS RR90-17-XXDP (Dormant)	172
В	1	RFS APXVAARR24 43-U-NA20	172
В	2	EMS RR90-17-XXDP (Dormant)	172
С	1	RFS APXVAARR24 43-U-NA20	172
С	2	EMS RR90-17-XXDP (Dormant)	172

Table 2: Antenna Data

All calculations were done with respect to uncontrolled / general population threshold limits.

Cable losses were factored in the calculations for this site. Since all **1900 MHz (PCS) & 2100 MHz** (AWS) radios are ground mounted the following cable loss values were used. For each ground mounted **1900 MHz (PCS)** radio there was **2.06 dB** of cable loss calculated into the system gains / losses for this site. For each ground mounted **2100 MHz (AWS)** radio there was **2.12 dB** of cable loss calculated into the system gains / losses for this site. These values were calculated based upon the manufacturers specifications for **200 feet** of **1-5/8**" coax.

Wireless Network Design and Deployment

RESULTS

Per the calculations completed for the proposed T-MOBILE configurations *Table 3* shows resulting emissions power levels and percentages of the FCC's allowable general population limit.

•				C1 1	Total TX		
Antenna		1	Antenna Gain	Channel	Power		
ID	Antenna Make / Model	Frequency Bands	(dBd)	Count	(W)	ERP (W)	MPE %
		1900 MHz (PCS) /					
Antenna	RFS	2100 MHz (AWS) /	15.65 / 16.35 /				
A1	APXVAARR24 43-U-NA20	600 MHz / 700 MHz	12.95 / 13.35	11	335	7,497.52	1.41
Antenna	EMS						
A2	RR90-17-XXDP	Dormant	N/A	0	0	0.00	0.00
				5	Sector A Com	posite MPE%	1.41
		1900 MHz (PCS) /					
Antenna	RFS	2100 MHz (AWS) /	15.65 / 16.35 /				
B1	APXVAARR24 43-U-NA20	600 MHz / 700 MHz	12.95 / 13.35	11	335	7,497.52	1.41
Antenna	EMS						
B2	RR90-17-XXDP	Dormant	N/A	0	0	0.00	0.00
	Sector B Composite MPE%					1.41	
		1900 MHz (PCS) /					
Antenna	RFS	2100 MHz (AWS) /	15.65 / 16.35 /				
C1	APXVAARR24_43-U-NA20	600 MHz / 700 MHz	12.95 / 13.35	11	335	7,497.52	1.41
Antenna	EMS						
C2	RR90-17-XXDP	Dormant	N/A	0	0	0.00	0.00
Sector C Composite MPE%					1.41		

Table 3: T-MOBILE Emissions Levels

Wireless Network Design and Deployment

The Following table (*table 4*) shows all additional carriers on site and their MPE% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum T-MOBILE MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, all three sectors have the same configuration yielding the same results on all three sectors. *Table 5* below shows a summary for each T-MOBILE Sector as well as the composite MPE value for the site.

Site Composite MPE%				
Carrier	MPE%			
T-MOBILE – Max Per Sector Value	1.41 %			
Thomaston FD	0.18 %			
Thomaston PD	0.03 %			
Litch. Co. FD	0.18 %			
CT State Police	0.06 %			
Sprint	2.18 %			
MetroPCS	0.57 %			
Verizon Wireless	4.18 %			
AT&T	14.69 %			
Site Total MPE %:	23.48 %			

Table 4: All Carrier MPE Contributions

T-MOBILE Sector A Total:	1.41 %
T-MOBILE Sector B Total:	1.41 %
T-MOBILE Sector C Total:	1.41 %
Site Total:	23.48 %

Table 5: Site MPE Summary

Wireless Network Design and Deployment

FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. *Table 6* below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated T-MOBILE sector(s). For this site, all three sectors have the same configuration yielding the same results on all three sectors.

T-MOBILE _ Frequency Band / Technology Max Power Values (Per Sector)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (µW/cm ²)	Frequency (MHz)	Allowable MPE (µW/cm ²)	Calculated % MPE
T-Mobile 1900 MHz (PCS) LTE	4	914.24	172	4.77	1900 MHz (PCS)	1000	0.48%
T-Mobile 2100 MHz (AWS) LTE	2	529.70	172	1.38	2100 MHz (AWS)	1000	0.14%
T-Mobile 1900 MHz (PCS) GSM	1	338.14	172	0.44	1900 MHz (PCS)	1000	0.04%
T-Mobile 600 MHz LTE / 5G NR	2	788.97	172	2.06	600 MHz	400	0.51%
T-Mobile 700 MHz LTE	2	432.54	172	1.13	700 MHz	467	0.24%
						Total:	1.41%

Table 6: T-MOBILE Maximum Sector MPE Power Values

Wireless Network Design and Deployment

Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-MOBILE facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-MOBILE Sector	Power Density Value (%)		
Sector A:	1.41 %		
Sector B:	1.41 %		
Sector C:	1.41 %		
T-MOBILE Maximum Total (per sector):	1.41 %		
Site Total:	23.48 %		
Site Compliance Status:	COMPLIANT		

The anticipated composite MPE value for this site assuming all carriers present is **23.48 %** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

Ist All

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