

June 3, 2022

Melanie A. Bachman Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Re: Notice of Exempt Modification – Antenna and RRU Add

Property Address: 200 Oronoque Lane Stratford, CT 06614

Applicant: AT&T Mobility, LLC

Dear Ms. Bachman:

On behalf of AT&T, please accept this application as notification pursuant to R.C.S.A. §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16- 50j-72(b) (2).

AT&T currently maintains a wireless telecommunications facility consisting of twelve (12) wireless telecommunication antennas at an antenna center line height of 121-feet on an existing 150'-foot Monopole, owned by the Town of Stratford at 2725 Main St, Stratford, CT 06615.

AT&T desires to modify its existing telecommunications facility by swapping nine (9) existing antennas with (9) new antennas, swapping six (6) existing remote radio units with (6) new remote radio units and adding associated cables. The centerline height of said antennas is and will remain at 121' on the existing antenna mount.

Attached is a summary of the planned modifications including power density calculations reflecting the change in AT&T's operations at the site. Also included is documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration.

Please accept this letter pursuant to Regulation of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-5l0j-72(b) (2). In accordance with R.C.S.A., a copy of this letter is being sent to The Honorable Laura R. Hoydick, Mayor, Town of Stratford at 2725 Main Street, Stratford, CT 06615, Daniel Brennan, Zoning Enforcement Officer, Town of Stratford at 2725 Main Street, Stratford, CT 06615 and Brian Donovan, Building Official, Town of Stratford at 2725 Main Street, Stratford, CT 06615.

The following is a list of subsequent decisions by the Connecticut Siting Council:

**EM-AT&T-138-1901424** – New Cingular Wireless, PCS, LLC (AT&T) notice of intent to modify an existing telecommunications facility located at 200 Oronogue Lane Stratford, Connecticut 06614.

The planned modifications to AT&T's facility fall squarely within those activities explicitly provided for in R.C.S.A. §16-50j-72(b) (2).

- 1. The proposed modifications will not result in an increase in the height of the existing tower. AT&T's replacement antennas will be installed at the 121-foot level of the 150-foot Monopole.
- 2. The proposed modifications will not involve any changes to ground-mounted equipment and, therefore, will not require and extension of the site boundary.
- 3. The proposed modifications will not increase the noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the modified facility will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. A cumulative worst-case RF emissions calculation for AT&T's modified facility is provided in the RF Emissions Compliance Report, included in Tab 2.



- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The tower and its foundation can support AT&T's proposed modifications. (See Structural Analysis Report Included in <u>Tab 3</u>).

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitutes an exempt modification under R.C.S.A. §16-50j-72(b) (2).

Sincerely,

Carolyn Seeley Real Estate Project Manager Smartlink on behalf of AT&T (978) 760-5577 Carolyn.seeley@smartlinkgroup.com

CC w/enclosures The Honorable Laura R. Hoydick, Mayor, Town of Stratford Daniel Brennan, Zoning Enforcement Officer, Town of Stratford Brian Donovan, Building Official, Town of Stratford

# STATE OF CONNECTICUT



### CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051 Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov www.ct.gov/csc

June 27, 2014

Christopher B. Fisher, Esq. Cuddy & Feder LLP 445 Hamilton Avenue, 14th Floor White Plains, NY 10601

RE: TS-CING-138-140509 - New Cingular Wireless PCS, LLC request for an order to approve tower sharing at an existing telecommunications facility located at 200 Oronoque Lane, Stratford, Connecticut.

Dear Attorney Fisher:

At a public meeting held June 26, 2014, the Connecticut Siting Council (Council) ruled that the shared use of this existing tower site is technically, legally, environmentally, and economically feasible and meets public safety concerns, and therefore, in compliance with General Statutes § 16-50aa, the Council has ordered the shared use of this facility to avoid the unnecessary proliferation of tower structures with the following conditions:

- Any deviation from the proposed installation as specified in the original tower share request and supporting materials with the Council shall render this decision invalid;
- Any material changes to the proposed installation as specified in the original tower share request and supporting materials filed with the Council shall require an explicit request for modification to the Council pursuant to Connecticut General Statutes § 16-50aa, including all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65;
- Not less than 45 days after completion of the proposed installation, the Council shall be notified in writing that the installation has been completed;
- Any nonfunctioning antenna and associated antenna mounting equipment on this facility owned and
  operated by New Cingular Wireless PCS, LLC shall be removed within 60 days of the date the
  antenna ceased to function.
- The validity of this action shall expire one year from the date of this letter; and
- The applicant may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration.

This decision is under the exclusive jurisdiction of the Council and applies only to this request for tower sharing dated May 1, 2014. This facility has been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower. Any deviation from the approved tower sharing request is enforceable under the provisions of Connecticut General Statutes § 16-50u.

The proposed shared use is to be implemented as specified in your letter dated May 1, 2014, including the placement of all necessary equipment and shelters within the tower compound.

Please be advised that the validity of this action shall expire one year from the date of this letter.



Thank you for your attention and cooperation.

Very truly yours

Robert Steir Chairman

RS/DM/cm

c: The Honorable John A. Harkins, Mayor, Town of Stratford Gary Lorentson, Planning & Zoning Administrator

### **200 ORONOQUE LN**

Location 200 ORONOQUE LN Mblu 60/20 2/ 1//

Acct# 1289400 Owner TOWN OF STRATFORD

PBN Assessment \$772,170

**Appraisal** \$1,103,100 **PID** 13349

Building Count 1 Sewer Use BZZ

**EPA Action** 

#### **Current Value**

| Appraisal Appraisal                    |              |           |             |  |  |  |  |  |  |
|--|--------------|-----------|-------------|--|--|--|--|--|--|
| Valuation Year Improvements Land Total |              |           |             |  |  |  |  |  |  |
| 2019                                   | \$775,300    | \$327,800 | \$1,103,100 |  |  |  |  |  |  |
|  | Assessment   |           |             |  |  |  |  |  |  |
| Valuation Year                         | Improvements | Land      | Total       |  |  |  |  |  |  |
| 2019                                   | \$542,710    | \$229,46  | \$772,170   |  |  |  |  |  |  |

#### **Owner of Record**

Owner TOWN OF STRATFORD Sale Price \$30,000

Co-Owner FIRE HOUSE Certificate

 Address
 200 ORONOQUE LN
 Book
 0493

 STRATFORD, CT 06614-1357
 Page
 0583

Sale Date 07/23/1974

#### **Ownership History**

| Ownership History                              |          |  |            |      |      |  |  |  |
|--|----------|--|------------|------|------|--|--|--|
| Owner Sale Price Certificate Sale Date Book Pa |          |  |            |      |      |  |  |  |
| TOWN OF STRATFORD                              | \$30,000 |  | 07/23/1974 | 0493 | 0583 |  |  |  |
| POWELL EFFIE V                                 | \$0      |  | 03/27/1973 | 0460 | 1124 |  |  |  |

### **Building Information**

### **Building 1: Section 1**

Year Built: 1978 Living Area: 6,658 Building Percent Good: 78

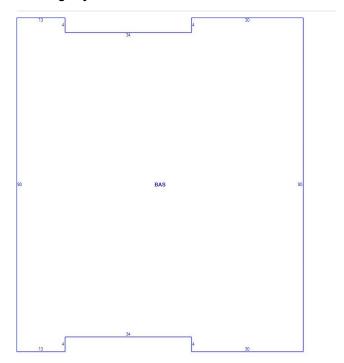
| Building Attributes |                |  |  |  |  |
|---------------------|----------------|--|--|--|--|
| Field               | Description    |  |  |  |  |
| Style:              | Fire Station   |  |  |  |  |
| Model               | Commercial     |  |  |  |  |
| Grade               | B-             |  |  |  |  |
| Stories:            | 1 Story        |  |  |  |  |
| Occupancy           | 1.00           |  |  |  |  |
| Exterior Wall 1     | Cedar or Redwd |  |  |  |  |
| Exterior Wall 2     |                |  |  |  |  |
| Roof Structure      | Flat           |  |  |  |  |
| Roof Cover          | T&G/Rubber     |  |  |  |  |
| Interior Wall 1     | Drywall/Sheet  |  |  |  |  |
| Interior Wall 2     |                |  |  |  |  |
| Interior Floor 1    | Concr-Finished |  |  |  |  |
| Interior Floor 2    |                |  |  |  |  |
| Heating Fuel        | Oil            |  |  |  |  |
| Heating Type        | Hot Water      |  |  |  |  |
| AC Type             | Central        |  |  |  |  |
| Struct Class        |                |  |  |  |  |
| Bldg Use            | Fire Dept      |  |  |  |  |
| 1st Floor Use:      | 932            |  |  |  |  |
| Heat/AC             | Heat/AC Split  |  |  |  |  |
| Frame Type          | Masonry        |  |  |  |  |
| Baths/Plumbing      | Average        |  |  |  |  |
| Ceiling/Wall        | Ceil & Min WL  |  |  |  |  |
| Rooms/Prtns         | Average        |  |  |  |  |
| Wall Height         | 16.00          |  |  |  |  |
| % Comm Wall         |                |  |  |  |  |

Danaing i noto

Building Photo

 $(https://images.vgsi.com/photos/StratfordCTPhotos///0089/IMG\_5405\_8968) and the strategies of the control of$ 

### **Building Layout**



(ParcelSketch.ashx?pid=13349&bid=13349)

|      | <u>Legend</u>    |       |                |
|------|------------------|-------|----------------|
| Code | Code Description |       | Living<br>Area |
| BAS  | BAS First Floor  |       | 6,658          |
|      |                  | 6,658 | 6,658          |

# **Extra Features**

| Extra Features             | Legend |
|----------------------------|--------|
| No Data for Extra Features |        |

#### Land

| Land Use |     | Land Line Valuation |      |  |
|----------|-----|---------------------|------|--|
| Use Code | 932 | Size (Acres)        | 0.98 |  |

DescriptionFire DeptZoneRS-1Neighborhood100Alt Land ApprNoCategoryNo

 Depth
 0

 Assessed Value
 \$229,460

 Appraised Value
 \$327,800

0

Frontage

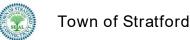
# Outbuildings

|      | Outbuildings         |    |                 |              |          |        |  |  |
|------|----------------------|----|-----------------|--------------|----------|--------|--|--|
| Code | Description Sub Code |    | Sub Description | Size         | Value    | Bldg # |  |  |
| PAV  | Paving               | AS | Asphalt         | 3000.00 S.F. | \$2,500  | 1      |  |  |
| SHD1 | Shed                 | CF | ConBlk\Frm      | 180.00 S.F.  | \$3,100  | 1      |  |  |
| ANTG | Guyed Tower          | R  | Radio           | 100.00 L.F.  | \$12,800 | 1      |  |  |
| LT1  | Lights in with pole  |    |                 | 6.00 Units   | \$8,600  | 1      |  |  |

### **Valuation History**

| Appraisal                              |           |           |             |  |  |  |  |  |
|--|-----------|-----------|-------------|--|--|--|--|--|
| Valuation Year Improvements Land Total |           |           |             |  |  |  |  |  |
| 2021                                   | \$775,300 | \$327,800 | \$1,103,100 |  |  |  |  |  |
| 2020                                   | \$775,300 | \$327,800 | \$1,103,100 |  |  |  |  |  |
| 2019                                   | \$775,300 | \$327,800 | \$1,103,100 |  |  |  |  |  |

| Assessment                       |           |           |           |  |  |  |  |
|----------------------------------|-----------|-----------|-----------|--|--|--|--|
| Valuation Year Improvements Land |           |           |           |  |  |  |  |
| 2021                             | \$542,710 | \$229,460 | \$772,170 |  |  |  |  |
| 2020                             | \$542,710 | \$229,460 | \$772,170 |  |  |  |  |
| 2019                             | \$542,710 | \$229,460 | \$772,170 |  |  |  |  |



Created by Greater Bridgeport Regional Council

# Map Title





THIS MAP IS NOT TO BE USED FOR NAVIGATION





## Radio Frequency Safety Survey Report Predictive (RFSSRP) Prepared For AT&T



Site Name: STRATFORD ORONOQUE ROAD

FA# 10152336 USID: 163489 Site ID: CTL02638

Address: 200 ORONOQUE LANE STRATFORD,

CT 06614

County: FAIRFIELD
Latitude: 41.2514110
Longitude: -73.1171510
Structure Type: MONOPOLE

Property Owner: NA

Pace job: MRCTB054248 **RFDS technology:** 5G NR 1SR CBAND

**Report Information** 

Report Writer: Sunita Sati Report Generated Date: 05-20-2022

### **Compliance Statement**

**AT&T Mobility Compliance Statement:** Based on the information collected, AT&T Mobility will be Compliant when the remediation recommended in section 5 or appropriate remediation determined by AT&T is implemented



# **Table of Contents**

| 1. Exe  | cutive Summary   | 3    |
|---------|--|------|
| 1.1     | Site Summary   |      |
| 1.2     | Signage Summary (Proposed)   | 3    |
| 1.3     | List of Documents used to prepare this Report  | 3    |
| 2. Site | Scale Map  |      |
|         | enna Inventory   |      |
|         | dicted Emission  |      |
| 4.1     | Predictive Cumulative MPE Contribution from All Sources at Antennas Centerline Level (121 ft.) | 7    |
| 4.2     | Predictive Cumulative MPE Contribution from All Sources at Adjacent Building Level (18 ft.)    | 8    |
| 4.3     | Predictive Cumulative MPE Contribution from All Sources at Ground Level (0 ft.)                | 9    |
| 5. Sta  | ement of Compliance  | . 10 |
| 5.1     | Statement of AT&T Mobility Compliance  |      |
| Apper   | dix A – Statement of Limiting Conditions   | . 12 |
|         | dix B – FCC Guidelines and Emissions Threshold Limits  |      |
| Apper   | dix C – Rules & Regulations  | . 15 |
| Apper   | dix D – General Safety Recommendations   | . 16 |
| Apper   | dix E – References   | . 17 |
| Apper   | dix F – Proprietary Statement  | . 20 |



### 1. Executive Summary

### 1.1 Site Summary

| Max Predictive Spatial Average MPE% & Location on Site (General Public) | 271926.0% on Antennas Centerline Level & at AT&T Sec-A antenna no. #A3-2                                 |  |  |  |  |
|---|--|--|--|--|--|
| Max Predictive Spatial Average MPE% at Ground Level (General Public)    | 1.4%   |  |  |  |  |
| AT&T Mobility Site Compliance   | AT&T Mobility will be Compliant by implementing remediation recommended as per section 5 in this report. |  |  |  |  |
| TABLE 1: Site Summary   |  |  |  |  |  |

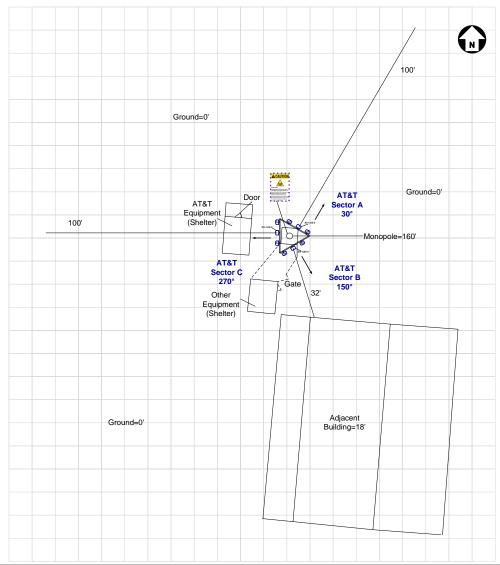
### 1.2 Signage Summary (Proposed)

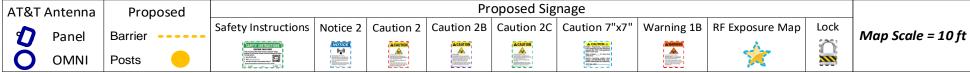
| AT&T                 | Sign Type              |                  |                   |                    |                    |                  |                    |                    |      |          |
|----------------------|------------------------|------------------|-------------------|--------------------|--------------------|------------------|--------------------|--------------------|------|----------|
| Signage<br>Locations | Safety<br>Instructions | Notice<br>Sign 2 | Caution<br>Sign 2 | Caution<br>Sign 2B | Caution<br>Sign 2C | Caution<br>7"x7" | Warning<br>Sign 1B | RF Exposure<br>Map | Lock | Barriers |
| Access<br>Point(s)   |                        |                  |                   | 1                  |                    |                  |                    |                    |      |          |
| Alpha                |                        |                  |                   |                    |                    |                  |                    |                    |      |          |
| Beta                 |                        |                  |                   |                    |                    |                  |                    |                    |      |          |
| Gamma                |                        |                  |                   |                    |                    |                  |                    |                    |      |          |
|                      |                        | •                |                   | TABLE 2: Signag    | e Summary (Pro     | posed)           | •                  | •                  | •    | •        |

# 1.3 List of Documents used to prepare this Report

- > 10152336\_AE201\_220428\_CTL02638\_REV0
- > NEW-ENGLAND\_CONNECTICUT\_CT2638\_2021-5G-NR-Radio\_5G-NR-1SR-CBAND\_pn5165\_2051A11PJ8\_10152336\_163489\_11-06-2021\_Final-Approved\_v2.00

# 2. Site Scale Map







# 3. Antenna Inventory

| Ant ID | Operator | Antenna Mfg | Antenna Model  | Antenna<br>Type | FREQ.<br>(MHz) | тесн.  | AZ.<br>(0) | H<br>B<br>W<br>(0) | Antenna<br>Gain (dBd) | Antenna<br>Aperture (ft) | Transmitter<br>Power (Watts) | Total Loss<br>(dB) | Total ERP<br>(Watts) | Total EIRP<br>(Watts) |
|--------|----------|-------------|----------------|-----------------|----------------|--------|------------|--------------------|-----------------------|--------------------------|------------------------------|--------------------|----------------------|-----------------------|
| A2     | AT&T     | CCI         | TPA65R-BU8D    | Panel           | 700            | LTE    | 30         | 73                 | 13.45                 | 8                        | 120.00                       | 0.5                | 2366.91              | 3883.12               |
| A2     | AT&T     | CCI         | TPA65R-BU8D    | Panel           | 1900           | LTE/5G | 30         | 66                 | 15.95                 | 8                        | 120.00                       | 0.5                | 4209.02              | 6905.28               |
| A2     | AT&T     | CCI         | TPA65R-BU8D    | Panel           | 2100           | LTE/5G | 30         | 66                 | 16.15                 | 8                        | 120.00                       | 0.5                | 4407.39              | 7230.72               |
| A3-1   | AT&T     | Ericsson    | AIR 6419 B77G^ | Panel           | 3450           | 5G     | 30         | 11                 | 23.5                  | 2.55                     | 108.44*                      | 0                  | 24277.05*            | 39828.68*             |
| A3-2   | AT&T     | Ericsson    | AIR 6449 B77D^ | Panel           | 3840           | 5G     | 30         | 11                 | 23.5                  | 2.55                     | 108.44*                      | 0                  | 24277.05*            | 39828.68*             |
| A4     | AT&T     | CCI         | DMP65R-BU8D    | Panel           | 700            | LTE    | 30         | 75                 | 12.95                 | 8                        | 120.00                       | 0.5                | 2109.51              | 3460.84               |
| A4     | AT&T     | CCI         | DMP65R-BU8D    | Panel           | 850            | 5G     | 30         | 64                 | 13.85                 | 8                        | 120.00                       | 0.5                | 2595.26              | 4257.76               |
| A4     | AT&T     | CCI         | DMP65R-BU8D    | Panel           | 2300           | LTE    | 30         | 64                 | 15.95                 | 8                        | 75.00                        | 0.5                | 2630.64              | 4315.80               |
| B2     | AT&T     | CCI         | TPA65R-BU8D    | Panel           | 700            | LTE    | 150        | 73                 | 13.45                 | 8                        | 120.00                       | 0.5                | 2366.91              | 3883.12               |
| B2     | AT&T     | CCI         | TPA65R-BU8D    | Panel           | 1900           | LTE/5G | 150        | 66                 | 15.95                 | 8                        | 120.00                       | 0.5                | 4209.02              | 6905.28               |
| B2     | AT&T     | CCI         | TPA65R-BU8D    | Panel           | 2100           | LTE/5G | 150        | 66                 | 16.15                 | 8                        | 120.00                       | 0.5                | 4407.39              | 7230.72               |
| B3-1   | AT&T     | Ericsson    | AIR 6419 B77G^ | Panel           | 3450           | 5G     | 150        | 11                 | 23.5                  | 2.55                     | 108.44*                      | 0                  | 24277.05*            | 39828.68*             |
| B3-2   | AT&T     | Ericsson    | AIR 6449 B77D^ | Panel           | 3840           | 5G     | 150        | 11                 | 23.5                  | 2.55                     | 108.44*                      | 0                  | 24277.05*            | 39828.68*             |
| В4     | AT&T     | CCI         | DMP65R-BU8D    | Panel           | 700            | LTE    | 150        | 75                 | 12.95                 | 8                        | 120.00                       | 0.5                | 2109.51              | 3460.84               |
| В4     | AT&T     | CCI         | DMP65R-BU8D    | Panel           | 850            | 5G     | 150        | 64                 | 13.85                 | 8                        | 120.00                       | 0.5                | 2595.26              | 4257.76               |
| В4     | AT&T     | CCI         | DMP65R-BU8D    | Panel           | 2300           | LTE    | 150        | 64                 | 15.95                 | 8                        | 75.00                        | 0.5                | 2630.64              | 4315.80               |
| C2     | AT&T     | CCI         | TPA65R-BU8D    | Panel           | 700            | LTE    | 270        | 73                 | 13.45                 | 8                        | 120.00                       | 0.5                | 2366.91              | 3883.12               |
| C2     | AT&T     | CCI         | TPA65R-BU8D    | Panel           | 1900           | LTE/5G | 270        | 66                 | 15.95                 | 8                        | 120.00                       | 0.5                | 4209.02              | 6905.28               |
| C2     | AT&T     | CCI         | TPA65R-BU8D    | Panel           | 2100           | LTE/5G | 270        | 66                 | 16.15                 | 8                        | 120.00                       | 0.5                | 4407.39              | 7230.72               |
| C3-1   | AT&T     | Ericsson    | AIR 6419 B77G^ | Panel           | 3450           | 5G     | 270        | 11                 | 23.5                  | 2.55                     | 108.44*                      | 0                  | 24277.05*            | 39828.68*             |
| C3-2   | AT&T     | Ericsson    | AIR 6449 B77D^ | Panel           | 3840           | 5G     | 270        | 11                 | 23.5                  | 2.55                     | 108.44*                      | 0                  | 24277.05*            | 39828.68*             |
| C4     | AT&T     | CCI         | DMP65R-BU8D    | Panel           | 700            | LTE    | 270        | 75                 | 12.95                 | 8                        | 120.00                       | 0.5                | 2109.51              | 3460.84               |
| C4     | AT&T     | CCI         | DMP65R-BU8D    | Panel           | 850            | 5G     | 270        | 64                 | 13.85                 | 8                        | 120.00                       | 0.5                | 2595.26              | 4257.76               |
| C4     | AT&T     | CCI         | DMP65R-BU8D    | Panel           | 2300           | LTE    | 270        | 64                 | 15.95                 | 8                        | 75.00                        | 0.5                | 2630.64              | 4315.80               |

**Table 3.1: Antenna Inventory Table** 

Note: ^ Mechanical Tilt value of "0°" MUST be retained for C-BAND and/or DoD AAS antenna(s) at all times to ensure that "EME (Predictive) Study" shall remain valid.

\* 75% TDD duty Cycle, 1.5dB Power Tolerance & 0.32 Power Reduction factor¹ are used to calculate Transmitter Power & ERP/EiRP



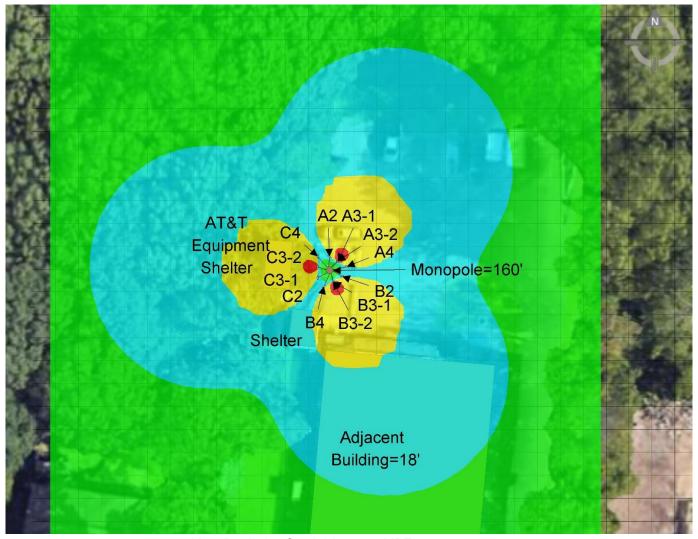
# **Antenna Heights (Z)**

| Ant ID | Operator | Antenna<br>Radiation<br>Centerline | Z-Height<br>from Adj.<br>Bldg | Z-Height<br>from<br>Ground |
|--------|----------|------------------------------------|-------------------------------|----------------------------|
| A2     | AT&T     | 121.00                             | 99.00                         | 117.00                     |
| A3-1   | AT&T     | 122.77                             | 103.50                        | 121.50                     |
| A3-2   | AT&T     | 119.22                             | 99.95                         | 117.95                     |
| A4     | AT&T     | 121.00                             | 99.00                         | 117.00                     |
| B2     | AT&T     | 121.00                             | 99.00                         | 117.00                     |
| B3-1   | AT&T     | 122.77                             | 103.50                        | 121.50                     |
| B3-2   | AT&T     | 119.22                             | 99.95                         | 117.95                     |
| B4     | AT&T     | 121.00                             | 99.00                         | 117.00                     |
| C2     | AT&T     | 121.00                             | 99.00                         | 117.00                     |
| C3-1   | AT&T     | 122.77                             | 103.50                        | 121.50                     |
| C3-2   | AT&T     | 119.22                             | 99.95                         | 117.95                     |
| C4     | AT&T     | 121.00                             | 99.00                         | 117.00                     |

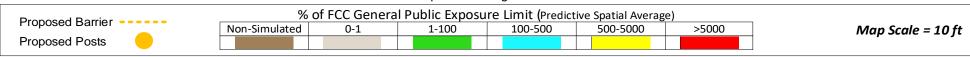
Table 3.2: Antenna Height(s) Summary Table

### 4. Predicted Emission

### 4.1 Predictive Cumulative MPE Contribution from All Sources at Antennas Centerline Level (121 ft.)



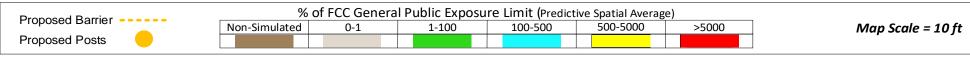
Max. Predictive Spatial Average MPE% = 271926.0%



# 2.2 Predictive Cumulative MPE Contribution from All Sources at Adjacent Building Level (18 ft.)



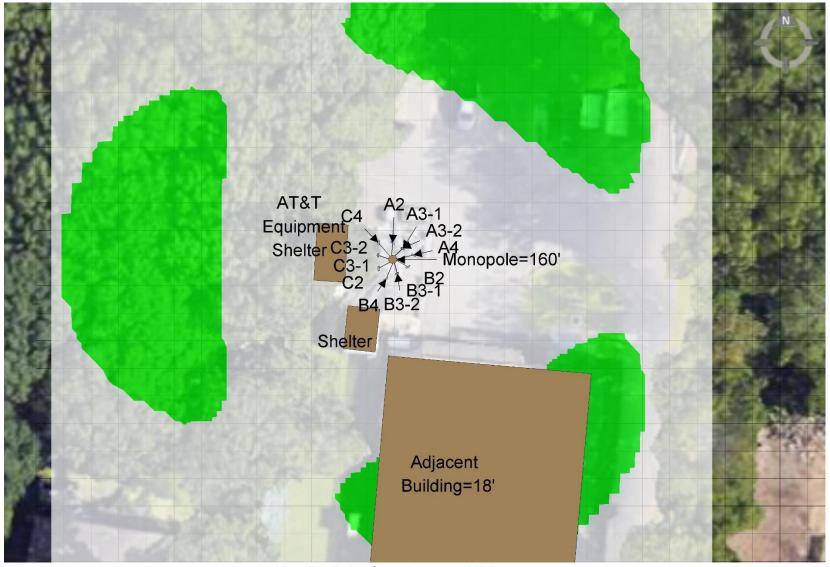
Max. Predictive Spatial Average MPE% = 2.0 %



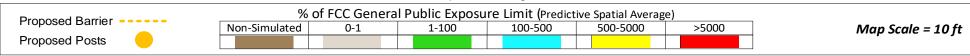




# Predictive Cumulative MPE Contribution from All Sources at Ground Level (0 ft.)



Max. Predictive Spatial Average MPE% = 1.4%





### **5. Statement of Compliance**

### 5.1 Statement of AT&T Mobility Compliance

At the time of our Analysis, AT&T Mobility is required to take action to fulfill their Obligations to comply with the FCC's mandate as defined in OET-65

#### **Recommendations**

#### **AT&T Alpha Sector:**

No Action Required.

#### **AT&T Beta Sector:**

No Action Required.

#### **AT&T Gamma Sector:**

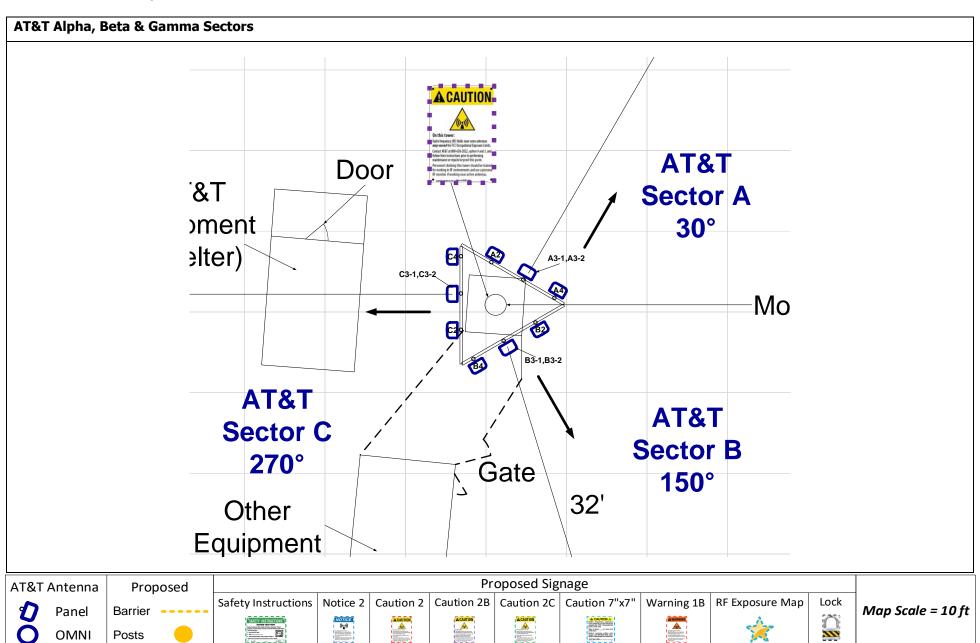
No Action Required.

### Monopole:

• One Caution 2B Sign to be posted on the Monopole at climbing access, facing outwards so approaching people can see as shown in "Recommendations Map – Detailed View" on page 11. (1 Total Sign)



### **Recommendations Map – Detailed View**





### **Appendix A – Statement of Limiting Conditions**

#### **General Model Assumptions**

In this site compliance report, it is assumed that all antennas are operating at full power at all times. AT&T has further recommended to assume a 75% duty cycle of maximum radiated power for all LTE & 5G carriers (& consider 100% duty cycle for all UMTS carriers).

In this site compliance report, it is assumed that Mechanical Tilt value of "0°" MUST be retained for C-BAND and/or DoD AAS^ antenna(s) at all times to ensure that "EME (Predictive) Study" shall remain valid.

AT&T recommended to consider - For C-BAND and/or DoD AAS^ antenna(s) 75% TDD duty Cycle, 1.5dB Power Tolerance & 0.32 Power Reduction factor¹ are used to calculate Transmitter Power & ERP/EiRP.

AT&T recommended to use worst-case tilts for the simulations.

- <sup>1</sup> **Power Reduction Factor**: IEC Standard 62232: 2017 allows for a statistically conservative power density model to more realistically define the RF exposure area. AT&T recommends a "0.32" factor to calculate the "Actual Maximum" (time averaged) power value, which accounts for "Beam Scanning," "Scheduling," and "RBS Utilization" This recommended value is a conservative figure modelled and supported by other vendors and through measurements published in scientific articles and white papers by IEEE and others. Those publication are listed below:
- 1. IEEE Access, Time-Averaged Realistic Maximum Power Levels for the Assessment of RF Exposure for 5G Radio Base Stations Using Massive MIMO (Published Sept. 18, 2017 / BJÖRN THORS, ANDERS FURUSKÄR, DAVIDE COLOMBI, AND CHRISTER TÖRNEVIK)
- 2. IEEE Explore, A Statistical Approach for RF Exposure Compliance Boundary Assessment in Massive MIMO Systems (Published Jan. 25, 2018 / Paolo Baracca, Andreas Weber, Thorsten Wild, Christophe Grangeat)
- 3. IEEE Access, In-situ Measurement Methodology for the Assessment of 5G NR Massive MIMO Base Station Exposure at Sub-6 GHz Frequencies (Published Dec. 20, 2019 / SAM AERTS, LEEN VERLOOCK, MATTHIAS VAN DEN BOSSCHE, DAVIDE COLOMBI, LUC MARTENS, CHRISTER TÖRNEVIK AND WOUT JOSEPH)
- 4. Applied Sciences, Analysis of the Actual Power and EMF Exposure from Base Stations in a Commercial 5G Network (Published July 30, 2020 / Davide Colombi, Paramananda Joshi, Bo Xu, Fatemeh Ghasemifard, Vignesh Narasaraju and Christer Törnevik)
- 5. Ofcom Technical Report, Electromagnetic Field (EMF) measurements near 5G mobile phone base stations (Published Feb. 21, 2020 / Davide Colombi, Paramananda Joshi, Bo Xu, Fatemeh Ghasemifard, Vignesh Narasaraju and Christer Törnevik)

MobileComm believes these areas to be safe for entry by occupationally trained personnel utilizing appropriate personal protective equipment (in most cases, a personal monitor). Thus, at any time, if power density measurements were made, we believe the real time measurements would indicate levels below those depicted in the RF emission diagram(s) in this report. By modelling in this way, MobileComm has conservatively shown exclusion areas – areas that should not be entered without the use of a personal monitor, carriers reducing power, or performing real-time measurements to indicate real-time exposure levels.

#### **Use of Generic Antennas**

For the purposes of this report, the use of "Generic" as an antenna model, or "Other Carrier" for an operator means the information about a carrier, their FCC license and/or antenna information was not provided and could not be obtained while on site. In the event of unknown information, MobileComm will use our industry specific knowledge of equipment, antenna models, and transmit power to model the site. Information about similar facilities is used when the service is identified and associated with a particular antenna. If no information is available regarding the transmitting service associated with an unidentified antenna, using the antenna manufacturer's published data regarding the antenna's physical characteristics makes more conservative assumptions.

Where the frequency is unknown, MobileComm uses the closest frequency in the antenna's range that corresponds to the highest Maximum Exposure Limit (MPE), resulting in a conservative analysis.



### **Appendix B – FCC Guidelines and Emissions Threshold Limits**

All power density values used in this report were analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter (µW/cm2). The number of µW/cm2 calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General Population/Uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu$ W/cm2). The general population exposure limit for the 700 and 800 MHz Bands is approximately 467  $\mu$ W/cm2 and 567  $\mu$ W/cm2 respectively, and the general population exposure limit for the 1900 MHz PCS and 2100 MHz AWS bands is 1000  $\mu$ W/cm2. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/Controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure, have been properly trained in RF safety and can exercise control over their exposure. Occupational/Controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure, have been trained in RF safety and can exercise control over his or her exposure by leaving the area or by some other appropriate means. The Occupational/Controlled exposure limits all utilized frequency bands is five (5) times the FCC's General Public / Uncontrolled exposure limit.

Additional details can be found in FCC OET 65.



|                          | Table 1: Limits for               | r Maximum Permissible Exp         | osure (MPE)                |   |
|--------------------------|-----------------------------------|-----------------------------------|----------------------------|---|
| (A) Limits for Occupatio | nal/Controlled Exposure           |                                   |                            |   |
| Frequency Range<br>(MHz) | Electric Field Strength (E) (V/m) | Magnetic Field Strength (H) (A/m) | Power Density (S) (mW/cm²) | Averaging Time [E] <sup>2</sup> ,<br>[H] <sup>2</sup> , or S<br>(minutes) |
| 0.3-3.0                  | 614                               | 1.63                              | (100)*                     |   |
|                          |                                   |                                   |                            | 6   |
| 3.0-30                   | 1842/f                            | 4.89/f                            | (900/f²)*                  | 6   |
| 30-300                   | 61.4                              | 0.163                             | 1.0                        | 6   |
| 300-I,500                |                                   |                                   | f/300                      | 6   |
| 1,500-100,000            |                                   |                                   | 5                          | 6   |
| (B) Limits for General P | ublic/Uncontrolled Exposur        | e                                 |                            | -   |
| Frequency Range<br>(MHz) | Electric Field Strength (E)       | Magnetic Field Strength<br>(H)    | Power Density (S)          | Averaging Time [E] <sup>2</sup> ,<br>[H] <sup>2</sup> , or S              |
|                          | (V/m)                             | (A/m)                             | $(mW/cm^2)$                | (minutes)   |
| 0.3-1.34                 | 614                               | 1.63                              | (100)*                     | 30  |
| 1.34-30                  | 824/f                             | 2.19/f                            | (180/f²)*                  | 30  |
| 30-300                   | 27.5                              | 0.073                             | 0.2                        | 30  |
| 300-I,500                |                                   | -                                 | f/1,500                    | 30  |
| 1,500-100,000            | -                                 | -                                 | 1.0                        | 30  |



### **Appendix C – Rules & Regulations**

#### **Explanation of Applicable Rules and Regulations**

FCC has set forth guidelines in OET Bulletin 65 for human exposure to radio frequency electromagnetic fields. Currently, there are two different levels of MPE - General Public MPE and Occupational MPE. An individual classified as Occupational can be defined as an individual who has received appropriate RF training and meets the conditions outlined below. General Public is defined as anyone who does not meet the conditions of being Occupational. FCC Rules and Regulations define compliance in terms of total exposure to total RF energy, regardless of location of or proximity to the sources of energy.

It is the responsibility of all licensees to ensure these guidelines are maintained at all times. It is the ongoing responsibility of all licensees composing the site to maintain ongoing compliance with FCC rules and regulations.

A building owner or site manager can use this report as part of an overall RF Health and Safety Policy. It is important for building owners/site managers to identify areas in excess of the General Population MPE and ensure that only persons qualified as Occupational are granted access to those areas.

#### **Occupational Environment Explained**

The FCC definition of Occupational exposure limits apply to persons who:

- are exposed to RF energy as a consequence of their employment;
- have been made aware of the possibility of exposure; and
- can exercise control over their exposure.

FCC guidelines go further to state that persons must complete RF Safety Awareness training and must be trained in the use of appropriate personal protective equipment.

In order to consider this site an Occupational Environment, the site must be controlled to prevent access by any individuals classified as the General Public. Compliance is also maintained when any non-occupational individuals (the General Public) are prevented from accessing areas indicated as Red or Yellow in the attached RF Emissions diagram. In addition, a person must be aware of the RF environment into which they are entering. This can be accomplished by an RF Safety Awareness class, and by appropriate written documentation such as this Site Compliance Report.



### **Appendix D – General Safety Recommendations**

The following are general recommendations appropriate for any site with accessible areas in excess of 100% General Public MPE. These recommendations are not specific to this site. These are safety recommendations appropriate for typical site management, building management, and other tenant operations.

- 1. All individuals needing access to the main site should be instructed to read and obey all posted placards and signs.
- 2. The site should be routinely inspected and this or similar report updated with the addition of any antennas or upon any changes to the RF environment including:
  - adding new antennas that may have been located on the site
  - removing of any existing antennas
  - changes in the radiating power or number of RF emitters
- 3. Post the appropriate SAFETY INSTRUCTIONS, NOTICE, CAUTION & WARNING sign at the main site access point(s) and other locations as required. Note: Please refer to RF Exposure Diagrams in the report section above, to inform everyone who has access to this site that beyond posted signs there may be levels in excess of the limits prescribed by the FCC. The signs below are examples of signs meeting FCC guidelines.



- 4. Ensure that the site door remains locked (or appropriately controlled) to deny access to the general public if deemed as policy by the building/site owner.
- 5. For a General Public environment the five color levels identified in measured RF emission diagram can be interpreted in the following manner:
  - White represents areas predicted to be greater than or equal to 0% and less than 1% of the MPE general public limits
  - Green represents areas predicted to be greater than or equal to 1% and less than 100% of the MPE general public limits
  - Blue represents areas predicted to be greater than or equal to 100% and lesser than 500% of the MPE general public limits.
  - Yellow represents areas predicted to be greater than or equal to 500% and lesser than 5000% of the MPE general public limits.
  - Red areas indicates predicted levels greater than or equal to 5000% of the MPE general public limits.



### Appendix E - References

#### 1 - FCC Definition

FCC defines an Occupational or Controlled environment as one where persons are exposed to RF fields as a consequence of their employment and where those persons exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Typical criteria for an Occupational or Controlled environment is restricted access (i.e. locked doors, gates, etc.) to areas where antennas are located coupled with proper RF warning signage.

FCC defines a site as a General Public or Uncontrolled environment when human exposure to RF fields occurs to the general public or in which persons who are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over the exposure. Typical criteria for a General Public or Uncontrolled environment are unrestricted access (i.e. unlocked or no restrictions) to areas where antennas are located without proper RF warning signage being posted.

#### 2 - Physical Testing measurement procedure and Tools

The Narda Broadband Field Meter NBM-550 can make rapid conformance measurements with evaluation in the time domain when used in conjunction EA5091 probe. This probe is a so-called Shaped Probe, i.e. it is frequency weighted so that it automatically takes account of the FCC Occupational limit values. To collect data, the probe is pointed towards the potential source(s) of EME radiation and moved slowly from ground level up to slightly above head height (approx. 6 ft).

Spatial Average Measurement A technique used to average a minimum of ten (10) measurements taken in a ten (10) second interval from zero (0) to six (6) feet. This measurement is intended to model the average energy an average sized human body will absorb while present in an electromagnetic field of energy.

### 3 - Site Safety Procedures

The following items are general safety recommendations that should be administered on a site by site basis as needed by the carrier.

**General Maintenance Work:** Any maintenance personnel required to work immediately in front of antennas and / or in areas indicated as above 100% of the Occupational MPE limits should coordinate with the wireless operators to disable transmitters during their work activities.

**Training and Qualification Verification:** All personnel accessing areas indicated as exceeding the General Population MPE limits should have a basic understanding of EME awareness and RF Safety procedures when working around transmitting antennas. Awareness training increases a workers understanding to potential RF exposure scenarios. Awareness can be achieved in a number of ways (e.g. videos, formal classroom lecture or internet based courses).

**Physical Access Control:** Access restrictions to transmitting antennas locations is the primary element in a site safety plan. Examples of access restrictions are as follows:

- Locked door or gate
- Alarmed door
- Locked ladder access
- Restrictive Barrier at antenna locations (e.g. Chain link with posted RF Sign)



**RF Signage:** Everyone should obey all posted signs at all times. RF signs play an important role in properly warning a worker prior to entering into a potential RF Exposure area.

**Assume all antennas are active:** Due to the nature of telecommunications transmissions, an antenna transmits intermittently. Always assume an antenna is transmitting. Never stop in front of an antenna. If you have to pass by an antenna, move through as quickly and safely as possible thereby reducing any exposure to a minimum.

**Maintain a 3 foot clearance from all antennas:** There is a direct correlation between the strength of an EME field and the distance from the transmitting antenna. The further away from an antenna, the lower the corresponding EME field is.

Rooftop RF Emissions Diagram: Section 4 of this report contains an RF Emissions Diagram that outlines various theoretical Maximum Permissible Exposure (MPE) areas on the rooftop. This analysis is all theoretical and assumes a duty cycle of 75% for each transmitting antenna at full power. This analysis is a worst case scenario. This analysis is based on one of two access control criteria: General Public criteria means the access to the site is uncontrolled and anyone can gain access. Occupational criteria means the access is restricted and only properly trained individuals can gain access to the antenna locations.

#### <u>4 - Definitions</u>

Compliance- The determination of whether a site is safe or not with regards to Human Exposure to Radio Frequency Radiation from transmitting antennas.

**Decibel (dB) –** A unit for measuring power or strength of a signal.

**Duty Cycle –** The percent of pulse duration to the pulse period of a periodic pulse train. Also, may be a measure of the temporal transmission characteristic of an intermittently transmitting RF source such as a paging antenna by dividing average transmission duration by the average period for transmission. A duty cycle of 75% corresponds to continuous operation.

Effective (or Equivalent) Isotropic Radiated Power (EIRP) – The product of the power supplied to the antenna and the antenna gain in a given direction relative to an isotropic antenna, this product is divided by the cable losses

**Effective Radiated Power (ERP) –** In a given direction, the relative gain of a transmitting antenna with respect to the maximum directivity of a half wave dipole multiplied by the net power accepted by the antenna from the connecting transmitter.

**Gain (of an antenna in dbd) –** The ratio of the maximum intensity in a given direction to the maximum radiation in the same direction from a reference dipole. Gain is a measure of the relative efficiency of a directional antennas as compared to a reference dipole.

**General Population/Uncontrolled Environment –** Defined by the FCC, as an area where RFR exposure may occur to persons who are unaware of the potential for exposure and who have no control of their exposure. General Population is also referenced as General Public.

**Generic Antenna –** For the purposes of this report, the use of "Generic" as an antenna model means the antenna information was not provided and could not be obtained while on site. In the event of unknown information, MobileComm will use our industry specific knowledge of antenna models to select a worst case scenario antenna to model the site.

Isotropic Antenna – An antenna that is completely non-directional. In other words, an antenna that radiates energy equally in all directions.

Maximum Measurement - This measurement represents the single largest measurement recorded when performing a spatial average measurement.



Maximum Exposure Limit (MPE) – The RMS and peak electric and magnetic field strength, their squares, or the plane-wave equivalent power densities associated with these fields to which a person may be exposed without harmful effect and with acceptable safety factor.

**Occupational/Controlled Environment –** Defined by the FCC, as an area where Radio Frequency Radiation (RFR) exposure may occur to persons who are aware of the potential for exposure as a condition of employment or specific activity and can exercise control over their exposure.

Radio Frequency Radiation – Electromagnetic waves that are propagated from antennas through space.

**Spatial Average Measurement –** A technique used to average a minimum of ten (10) measurements taken in a ten (10) second interval from zero (0) to six (6) feet. This measurement is intended to model the average energy an average sized human body will absorb while present in an electromagnetic field of energy.

**Transmitter Power Output (TPO) –** The radio frequency output power of a transmitter's final radio frequency stage as measured at the output terminal while connected to a load.



### **Appendix F – Proprietary Statement**

This report was prepared for the use of AT&T Mobility, LLC to meet requirements specified in AT&T's corporate RF safety guidelines. It was performed in accordance with generally accepted practices of other consultants undertaking similar studies at the same time and in the same locale under like circumstances. The conclusions provided by MobileComm are based solely on the information provided by AT&T Mobility and all observations in this report are valid on the date of the investigation. Any additional information that becomes available concerning the site should be provided to MobileComm so that our conclusions may be revised and modified, if necessary. This report has been prepared in accordance with Standard Conditions for Engagement and authorized proposal, both of which are integral parts of this report. No other warranty, expressed or implied, is made.



May 31, 2022

Scope: MOUNT ANALYSIS REPORT

Prepared for: SmartLink
Carrier: AT&T
Site Number: CTL02638
FA Number: 10152336

Site Name: Stratford Oronoque Road Site Address: 200 Oronoque Lane

Stratford, CT 06614

Latitude/ Longitude: 41.2514110° / -73.1171510°

Structure Type: MONOPOLE

Mount Type: Existing Low-Profile Platform

Rad Center: 121'-0"

Fullerton Engineering P.C. is pleased to submit this "Mount Analysis Report" to determine the adequacy of the antenna mounting system with the proposed appurtenance and equipment addition on the abovementioned structure.

**Analysis Criteria:** 

Reference Standard: TIA-222-H Standard

Wind Parameters: Basic Wind Speed: 119 mph (3-Sec gust)

Ice Wind Speed: 50 mph (3-Sec gust)

Design Ice Thickness: 1.00 in.

Risk Category II Exposure Category: B Topographic Feature: None Topographic Method: Method 2 Ground Elevation Factor,  $K_e$ : 0.99

Seismic Parameters: S<sub>s</sub>: 0.205

S<sub>1</sub>: 0.054

Analysis Software: RISA-3D (V17)

#### **Appurtenance Loads:**

The antenna mounting system was analyzed with the final loading configuration shown in Page 2 of this report.

Summary of Analysis Result: PASS (MAX STRESS RATIO = 85.8%)

Barbara T. Kotecki, P.E.



#### **Summary:**

This structural assessment is in regards to the adequacy of the antenna mounting system for the final loading configuration described below. The purpose was to determine conformance of the antenna mounting system under the applicable codes and standards.

This PE certification completed by Fullerton Engineering P.C. is inclusive of the antenna mounting system that will support the existing and proposed loading provided by the client.

This certification assumes that all structural members of the antenna mounting system are in good condition and have not been altered from the manufacturer's original design. Prior to installation of new equipment, contractor shall inspect the condition of all relevant members and connectors. The contractor shall be responsible for the means and methods of construction.

#### Sources:

| Reference Document                                  | Date           |
|---|----------------|
| RFDS Ver. 2.00 provided by AT&T                     | 05/23/2022     |
| Mount Mapping by FDH Infrastructure Services        | 04/11/2022     |
| Construction Drawings by Fullerton Engineering P.C. | Latest Version |

### **Final Loading Configuration:**

| i mai Loading Co     | om garation.               |        |              |                                       |            |
|----------------------|----------------------------|--------|--------------|---------------------------------------|------------|
| Mount Elevation (ft) | Antenna Rad<br>Center (Ft) | QTY.   | MANUFACTURER | MODEL                                 | Status     |
|                      |                            | 3      | CCI          | TPA65R-BU8DA-K                        |            |
|                      |                            | 3      | Ericsson     | AIR 6449 B77D + AIR 6419 B77G Stacked | Dronocod   |
|                      |                            |        | Ericsson     | RRUS-4478 B14                         | Proposed   |
| 121'-0"              | 121'-0"                    | 3      | Ericsson     | RRUS-8843 B2/B66A                     |            |
| 121 -0               |                            | 121 -0 | 3            | Kathrein                              | 800-10966  |
|                      |                            | 3      | Ericsson     | RRUS-4449 B5/B12                      | - Fyisting |
|                      |                            | 3      | Ericsson     | RRUS-32 B30                           | Existing   |
|                      |                            | 4      | Raycap       | DC6-48-60-18-8F                       |            |

#### **Member Component Capacity Table:**

| Component   | % Capacity  | Pass / Fail |  |  |  |  |
|---|---|-------------|--|--|--|--|
| Face Horizontals                                      | 54.1%   | Pass        |  |  |  |  |
| Standoff Members                                      | 85.8%   | Pass        |  |  |  |  |
| Mounting Pipes  | 52.6%   | Pass        |  |  |  |  |
| Mount-to-Tower Connection, Collar Mount Threaded Rods | 7.6%  | Pass        |  |  |  |  |
| Structural Rating (max fro                            | Structural Rating (max from all components) = 85.8% |             |  |  |  |  |

Site Number: CTL02638 Project Number: 2021.0215.0011



Site Number: Site Name: Created By: Checked By: Date: Code: CTL02638 STRATFORD ORONOQUE ROAD GO BTK 5/27/2022 ANSI/TIA-222-H

|                     | ,                             |          |          |                   |
|---------------------|-------------------------------|----------|----------|-------------------|
| Base Structure Ty   | rpe                           | Туре     | Monopole | )                 |
| Structure Height    | Above Grade (ft)              | Ht       | 150.00   |                   |
| RAD Center (ft)     |                               | z        | 121.00   |                   |
| Windspeed no ice    | (mph, 3-sec gust)             | v        | 119.00   | see wind maps     |
| Windspeed with      | ce (mph, 3-sec gust)          | Vi       | 50.00    | see ice maps      |
| Windspeed for m     | aintenance (mph, 3-sec gust)  | Vm       | 30.00    | Section 16.6      |
| Ice Thickness       |                               | ti       | 1.00     | see ice maps      |
| Exposure Catego     | ry (B/C/D)                    | Exposure | В        | Section 2.6.5.1.2 |
| Risk Category (I,II | ,III, IV)                     | Cat      | П        | Table 2-1         |
| Topographic Feat    | ure                           | K.1'     | None     | Figure 2-1        |
| Crest Height        |                               | н        | 5.00     | Section 2.6.6.2.1 |
| Length of Feature   | 2                             | L        | 5.00     |                   |
| Distance from Cr    | est to Tower                  | x        | 0.00     |                   |
| Escarpment Dow      | nwind?                        |          | No       |                   |
| Height above sea    | level                         | Zs       | 257.53   |                   |
| Exposure Catego     | ry Coefficient                | zg       | 1200.00  | Table 2-4         |
| Mid-Point of Stru   | cture                         | Ht.mid   | 75.00    |                   |
| Min Velocity Pres   | sure Coefficient              | Kzmin    | 0.70     | Table 2-4         |
| Exposure Catego     | ry Coefficient                | α'       | 7.00     | Table 2-4         |
| Velocity Pressure   | Coefficient                   | Kz       | 1.04     | Section 2.6.5.2   |
| Ground Elevation    | Factor                        | Ke       | 0.99     | Section 2.6.8     |
| Topographic Feat    | ure Factor Adjusted for Slope | K1       | 1.00     | Figure 2-1        |
| Horizontal Distan   | ce Factor                     | K2       | 1.00     | Figure 2-1        |
| Vertical Distance   | Factor                        | K3       | 0.00     | Figure 2-1        |
| Topographic Fact    | or                            | Kzt      | 1.00     | Section 2.6.6.2.1 |
| Rooftop Wind Sp     |                               | Ks       | 1.00     | Section 2.6.7     |
| Ice Load Importa    |                               | Iti      | 1.00     | Table 2-3         |
| Wind Direction P    |                               | Kd       | 0.95     | Table 2-2         |
| Height Escalation   |                               |          | 1.14     | Section 2.6.10    |
| Gust Effect Facto   |                               |          | 1.00     | Section 16.6      |
| Design Ice Thickn   | ess                           |          | 1.14     | Section 2.6.10    |
| Ice Density         |                               |          | 56.00    | lbf/ft^3          |
|                     | for Maintenance               |          | 2.26     | Section 2.6.11.6  |
| Velocity Pressure   |                               |          | 6.29     | Section 2.6.11.6  |
| Velocity Pressure   | No Ice                        | qz       | 35.61    | Section 2.6.11.6  |

| Ka= | 0.9 |
|-----|-----|
|     |     |

| Importance Factor (Earthquake)               | I <sub>e</sub>  | 1.00        | Table 2-3  |
|--|-----------------|-------------|------------|
| Site Class                                   | Class           | D - Default |            |
| Seismic Design Category                      | Cat             | В           |            |
| MCE <sub>R</sub> Ground Motion (period=0.2s) | Ss              | 0.205       |            |
| MCE <sub>R</sub> Ground Motion (period=1.0s) | S <sub>1</sub>  | 0.054       |            |
| Seismic Design Value at 0.2s                 | S <sub>DS</sub> | 0.218       |            |
| Long-Period Site Coefficient Fv              | Fv              | 0.80        | Table 2-12 |
| Seismic Design Value at 1.0s                 | S <sub>D1</sub> | 0.029       | Sec. 2.7.5 |
| Long-period Transition Period (s)            | T <sub>L</sub>  | 6           |            |

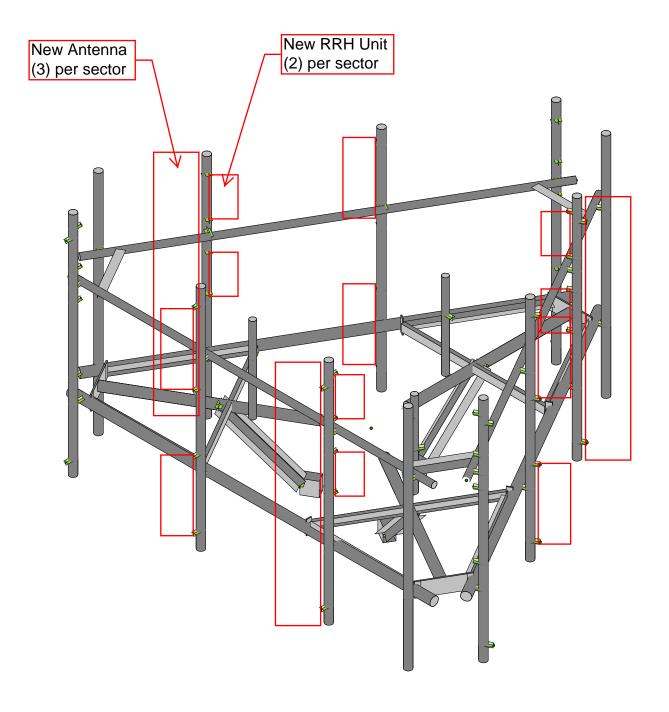
|                     | Sesimic Shear    |               |  |  |  |  |  |  |  |  |  |
|---------------------|------------------|---------------|--|--|--|--|--|--|--|--|--|
| R                   | R 2.000 See 16.7 |               |  |  |  |  |  |  |  |  |  |
| C <sub>S-calc</sub> | 0.109            | See 2.7.7.1.1 |  |  |  |  |  |  |  |  |  |
| C <sub>S-min</sub>  | 0.010            | See 2.7.7.1.1 |  |  |  |  |  |  |  |  |  |
| Cs                  | 0.109            | See 2.7.7.1.1 |  |  |  |  |  |  |  |  |  |
| As                  | 1.000            | See 16.7      |  |  |  |  |  |  |  |  |  |

| Rooftop Wind Speed-Up Factor                                  | Ks      | No     |               |
|---|---------|--------|---------------|
| Horizontal distance from windward face to center of structure | Xb (ft) | 1      | Section 2.6.7 |
| Width of windward face of the building                        | Ws (ft) | 100    | Section 2.6.7 |
| Height of the parapet wall                                    | Hp (ft) | 5      | Section 2.6.7 |
| Height of windward face of the building                       | Hs (ft) | 150.00 | Section 2.6.7 |
| Height of structure above roof                                | Zr (ft) | 10.00  | Section 2.6.7 |
|   | H1 (ft) | 5.2    | Section 2.6.7 |
|   | H2 (ft) | 105.00 | Section 2.6.7 |

| Appurtenance Properties |                   |       |      |      |      |        |        |      | Loads (force per connection) |          |          |       |       |    |    |    |    |       |
|-------------------------|-------------------|-------|------|------|------|--------|--------|------|------------------------------|----------|----------|-------|-------|----|----|----|----|-------|
| Manufacturer            | Model             | R/F   | L    | w    | D    | Weight | # Conn | Wt   | Ice Wt                       | F no ice | S no ice | F ice | S ice | Fm | Sm | Eh | Ev | EPA.F |
| Kathrein                | 800-10966         | Flat  | 96   | 20   | 6.9  | 114.6  | 2      | 57.3 | 52.8                         | 278      | 120      | 55    | 27    | 18 | 8  | 6  | 2  | 1     |
| Ericsson                | AIR 6449 B77D     | Flat  | 30.4 | 15.9 | 8.1  | 81.6   | 2      | 40.8 | 21.3                         | 65       | 34       | 14    | 8     | 4  | 2  | 4  | 2  |       |
| Ericsson                | AIR 6419 B77G     | Flat  | 28.3 | 16.1 | 7.9  | 77     | 2      | 38.5 | 19.9                         | 61       | 31       | 13    | 7     | 4  | 2  | 4  | 2  |       |
| CCIAntennas             | TPA65R-BU8DA-K    | Flat  | 96   | 20.7 | 7.7  | 87.1   | 2      | 43.6 | 57.5                         | 286      | 130      | 57    | 29    | 18 | 8  | 5  | 2  | 1     |
| Ericsson                | RRUS-4478 B14     | Flat  | 16.5 | 13.4 | 7.7  | 44     | 2      | 22.0 | 13.0                         | 30       | 17       | 7     | 4     | 2  | 1  | 2  | 1  |       |
| Ericsson                | RRUS-8843 B2/B66A | Flat  | 15   | 13.2 | 11.1 | 75     | 2      | 37.5 | 16.4                         | 26       | 22       | 6     | 5     | 2  | 1  | 4  | 2  |       |
| Ericsson                | RRUS-4449 B5/B12  | Flat  | 15   | 13.2 | 9.3  | 70     | 2      | 35.0 | 14.2                         | 26       | 19       | 6     | 5     | 2  | 1  | 4  | 2  |       |
| Ericsson                | RRUS-32 B30       | Flat  | 27.2 | 12.1 | 7    | 60     | 2      | 30.0 | 16.6                         | 44       | 27       | 10    | 7     | 3  | 2  | 3  | 1  |       |
| Raycap                  | DC6-48-60-18-8F   | Round | 24   | 9.7  | 9.7  | 32.8   | 1      | 32.8 | 15.1                         | 26       | 26       | 6     | 6     | 2  | 2  | 4  | 1  |       |

| Shape Properties |              |       |       |      | Loads (force per connection) |          |         |       |        |          |          |       | ļ     |     |     |     |     |       |
|------------------|--------------|-------|-------|------|------------------------------|----------|---------|-------|--------|----------|----------|-------|-------|-----|-----|-----|-----|-------|
| Shape Type       | Shape        | R/F   | L     | w    | D                            | Wt (plf) | # Conn  | Wt    | Ice Wt | F no ice | S no ice | F ice | S ice | Fm  | Sm  | Eh  | Ev  | EPA.F |
| Pipe             | Pipe 3 Std.  | Round | 153.5 | 3.5  | 3.5                          | 7.58     | 12.7917 | 96.96 | 6.5    | 11       | 11       | 3     | 3     | 0.7 | 0.7 | 0.8 | 0.3 |       |
| Pipe             | Pipe 2 Std.  | Round | 153.5 | 2.38 | 2.38                         | 3.66     | 12.7917 | 46.82 | 4.9    | 8        | 8        | 3     | 3     | 0.5 | 0.5 | 0.4 | 0.2 |       |
| Pipe             | Pipe 2½ Std. | Round | 96    | 2.88 | 2.88                         | 5.80     | 8       | 46.40 | 5.6    | 9        | 9        | 3     | 3     | 0.6 | 0.6 | 1   | 0.3 |       |
| Pipe             | Pipe 3 Std.  | Round | 68.64 | 3.5  | 3.5                          | 7.58     | 5.72    | 43.36 | 6.5    | 10       | 10       | 3     | 3     | 1   | 1   | 1   | 0.3 |       |
| Angle            | L3x3x¼       | Flat  | 34.8  | 3    | 3                            | 4.90     | 2.9     | 14.21 | 7.5    | 12       | 12       | 4     | 4     | 1   | 1   | 1   | 0.2 |       |
| Angle            | L2x2x3/16    | Flat  | 46.5  | 2    | 2                            | 2.44     | 3.875   | 9.46  | 5.5    | 10       | 10       | 3     | 3     | 1   | 1   | 0.3 | 0.1 |       |
| HSS              | HSS6x4x1/4   | Flat  | 6     | 6    | 4                            | 15.62    | 0.5     | 7.81  | 11.6   | 19       | 13       | 6     | 5     | 1   | 1   | 2   | 0.7 | 0.    |
| Pipe             | Pipe 2 Std.  | Round | 36    | 2.38 | 2.38                         | 3.66     | 3       | 10.98 | 4.9    | 6        | 6        | 2     | 2     | 0.4 | 0.4 | 0.4 | 0.2 |       |
| Channel          | C3x3.5       | Flat  | 60.39 | 3    | 1.37                         | 3.50     | 5.0325  | 17.61 | 6.2    | 15       | 7        | 4     | 3     | 1   | 0.5 | 0.4 | 0.2 |       |
| Plate            | PL½"x6"      | Flat  | 14.5  | 6    | 0.5                          | 10.21    | 1.20833 | 12.34 | 10.0   | 19       | 3        | 5     | 2     | 1   | 0.2 | 1   | 0.4 |       |
| Angle            | L3x3x3/8     | Flat  | 21.9  | 3    | 3                            | 7.20     | 1.825   | 13.14 | 7.5    | 11       | 11       | 4     | 4     | 1   | 1   | 1   | 0.3 |       |
|                  |              |       |       |      |                              |          |         |       |        |          |          |       |       |     |     |     |     |       |

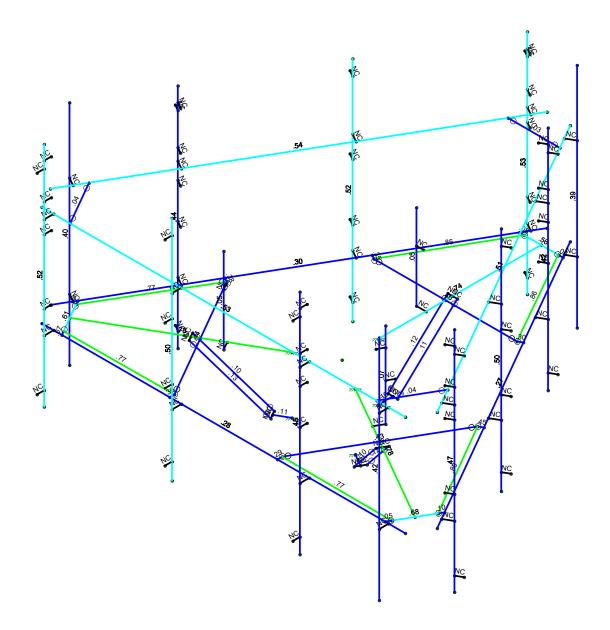




| Fullerton Engineering P.C. |                | SK - 1                          |
|----------------------------|----------------|---------------------------------|
| GO                         | Mount Analysis | May 27, 2022 at 1:00 PM         |
| CTL02638                   | 3D Render      | CTL02638-Mount Analysis - Rev H |



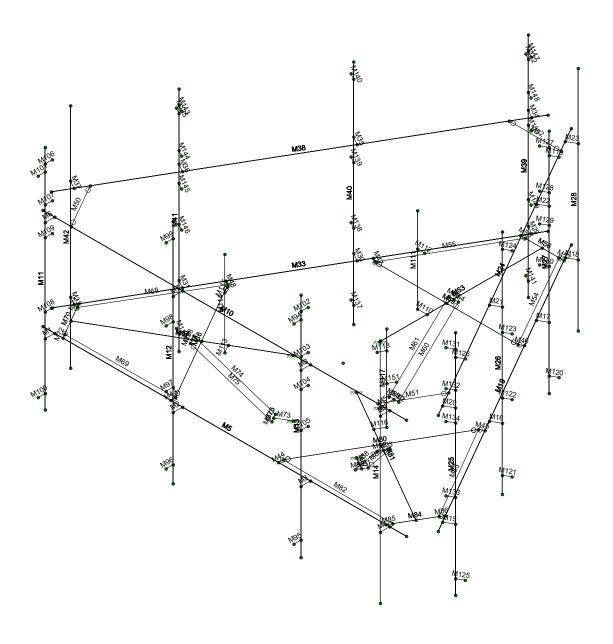




Member Code Checks Displayed (Enveloped) Envelope Only Solution

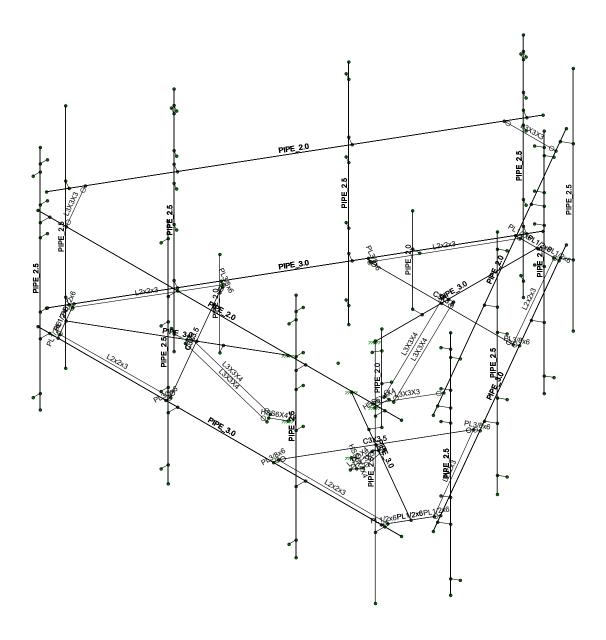
| Fullerton Engineering P.C. |                | SK - 2                          |
|----------------------------|----------------|---------------------------------|
| GO                         | Mount Analysis | May 27, 2022 at 1:03 PM         |
| CTL02638                   | Unity Graphic  | CTL02638-Mount Analysis - Rev H |





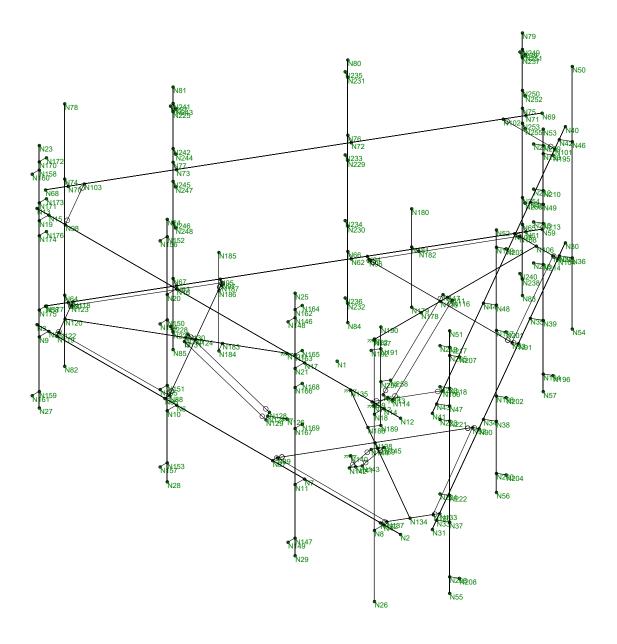
| Fullerton Engineering P.C. |                | SK - 3                          |
|----------------------------|----------------|---------------------------------|
| GO                         | Mount Analysis | May 27, 2022 at 1:03 PM         |
| CTL02638                   | Member Label   | CTL02638-Mount Analysis - Rev H |





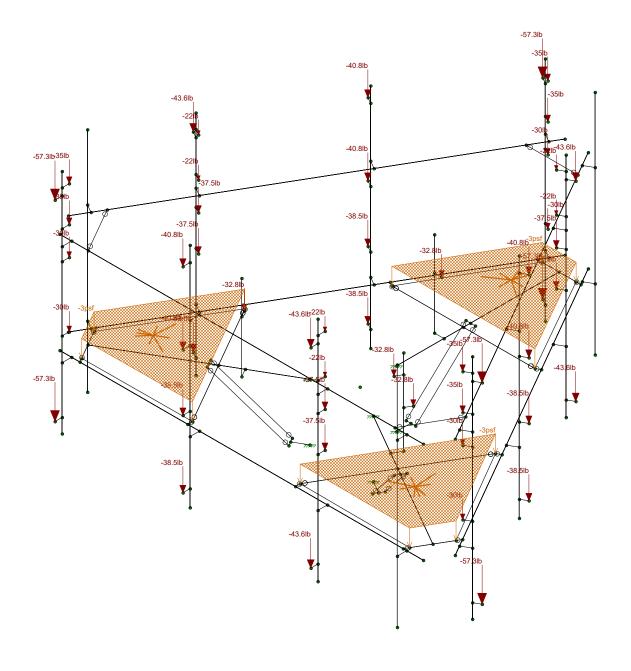
| Fullerton Engineering P.C. |                | SK - 4                          |
|----------------------------|----------------|---------------------------------|
| GO                         | Mount Analysis | May 27, 2022 at 1:03 PM         |
| CTL02638                   | Shape          | CTL02638-Mount Analysis - Rev H |





| Fullerton Engineering P.C. |                | SK - 5                          |
|----------------------------|----------------|---------------------------------|
| GO                         | Mount Analysis | May 27, 2022 at 1:04 PM         |
| CTL02638                   | Nodes          | CTL02638-Mount Analysis - Rev H |

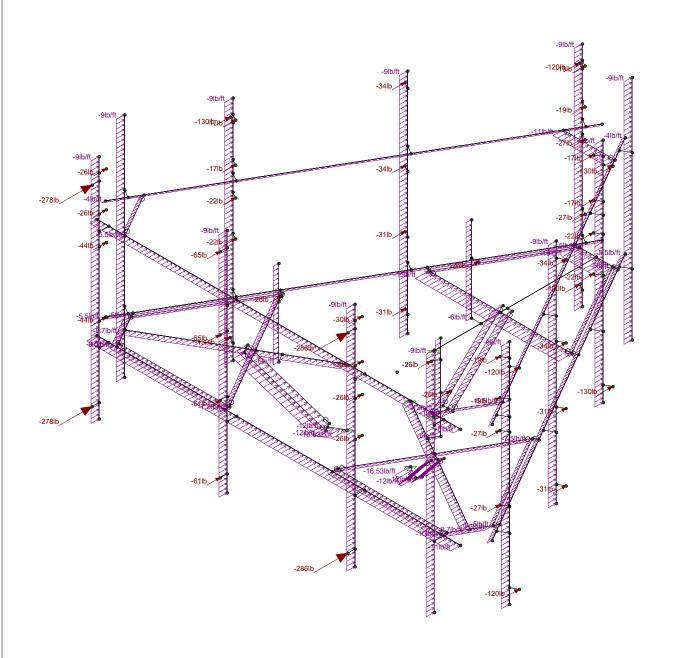




Loads: BLC 1, DL Envelope Only Solution

| Fullerton Engineering P.C. |                | SK - 6                          |
|----------------------------|----------------|---------------------------------|
| GO                         | Mount Analysis | May 27, 2022 at 1:04 PM         |
| CTL02638                   | Dead Load      | CTL02638-Mount Analysis - Rev H |

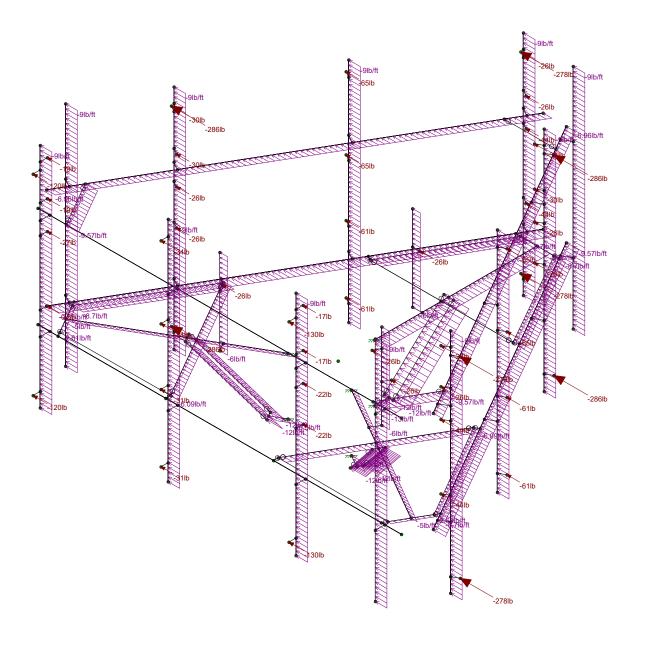




Loads: BLC 3, WL(0) Envelope Only Solution

| Fullerton Engineering P.C. |                         | SK - 7                          |
|----------------------------|-------------------------|---------------------------------|
| GO                         | Mount Analysis          | May 27, 2022 at 1:04 PM         |
| CTL02638                   | Wind Load (Z-Direction) | CTL02638-Mount Analysis - Rev H |

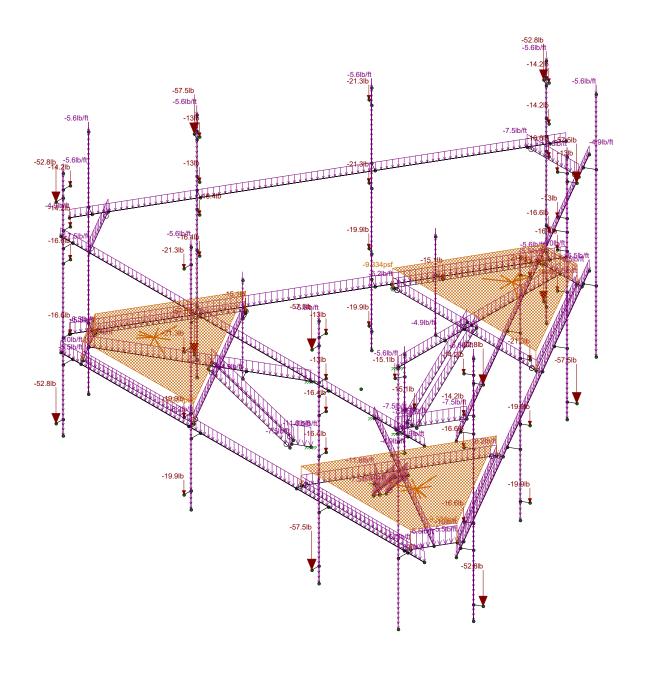




Loads: BLC 4, WL(90) Envelope Only Solution

| Fullerton Engineering P.C. |                         | SK - 8                          |  |
|----------------------------|-------------------------|---------------------------------|--|
| GO                         | Mount Analysis          | May 27, 2022 at 1:05 PM         |  |
| CTL02638                   | Wind Load (X-Direction) | CTL02638-Mount Analysis - Rev H |  |

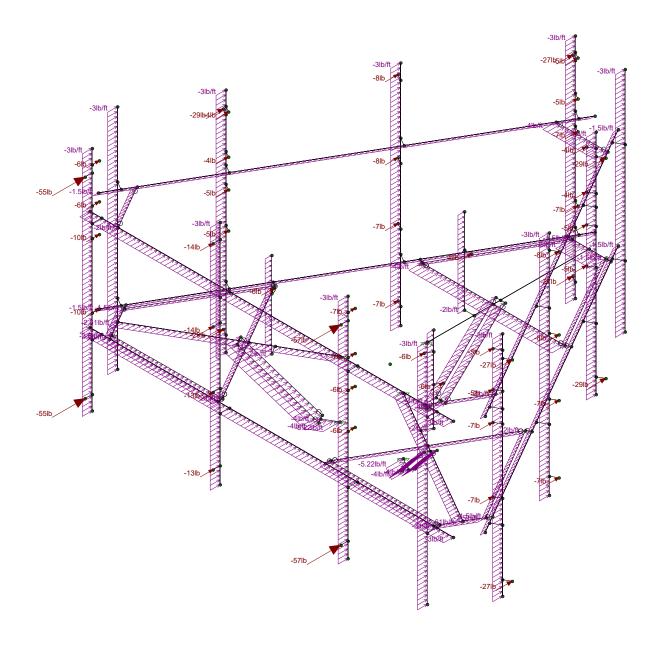




Loads: BLC 2, DLi Envelope Only Solution

| Fullerton Engineering P.C. |                | SK - 9                          |
|----------------------------|----------------|---------------------------------|
| GO                         | Mount Analysis | May 27, 2022 at 1:05 PM         |
| CTL02638                   | Ice Load       | CTL02638-Mount Analysis - Rev H |

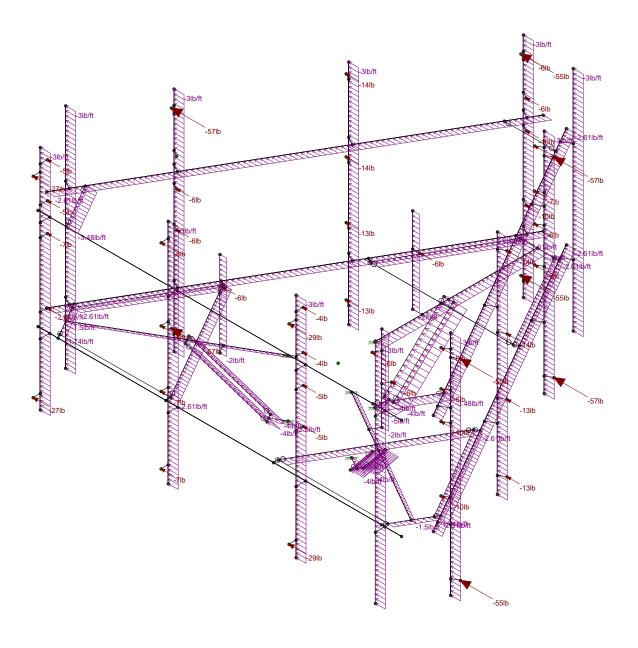




Loads: BLC 5, WL.i(0) Envelope Only Solution

| Fullerton Engineering P.C. |                                  | SK - 10                         |
|----------------------------|----------------------------------|---------------------------------|
| GO                         | Mount Analysis                   | May 27, 2022 at 1:05 PM         |
| CTL02638                   | Wind Load with Ice (Z-Direction) | CTL02638-Mount Analysis - Rev H |

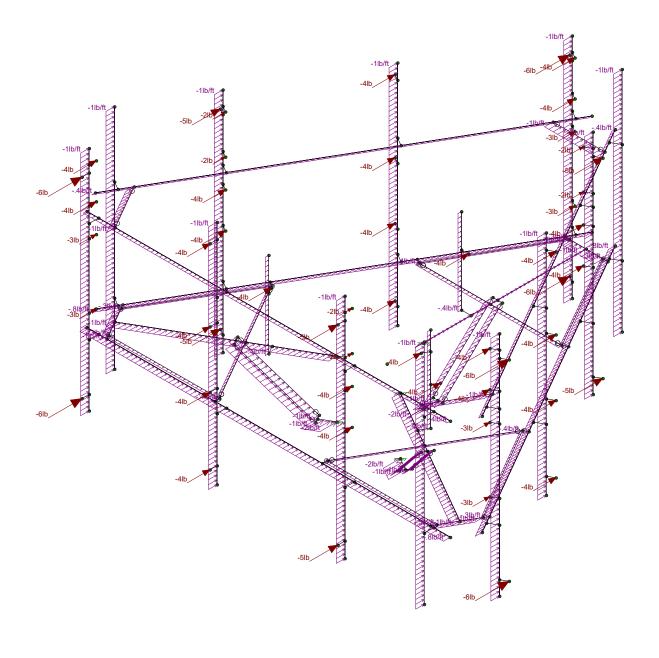




Loads: BLC 6, WL.i(90) Envelope Only Solution

| Fullerton Engineering P.C. |                                  | SK - 11                         |
|----------------------------|----------------------------------|---------------------------------|
| GO                         | Mount Analysis                   | May 27, 2022 at 1:06 PM         |
| CTL02638                   | Wind Load with Ice (X-Direction) | CTL02638-Mount Analysis - Rev H |

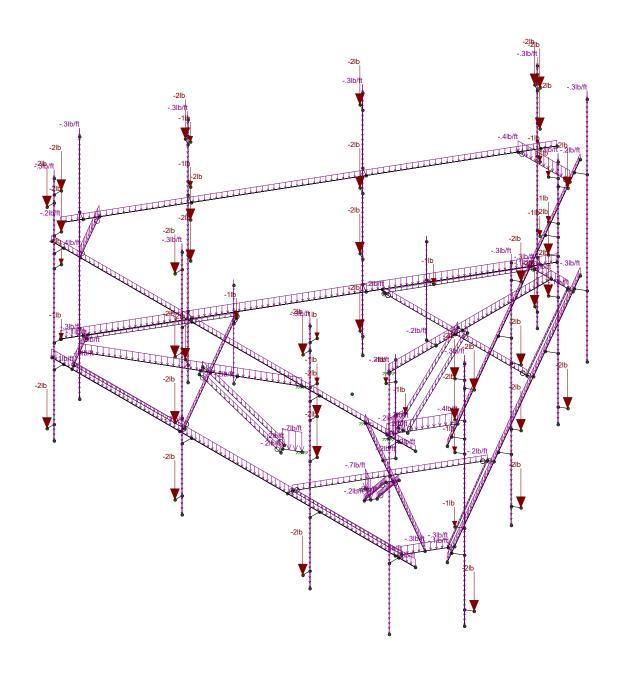




Loads: BLC 8, EH(0) Envelope Only Solution

| Fullerton Engineering P.C. |                         | SK - 12                         |
|----------------------------|-------------------------|---------------------------------|
| GO                         | Mount Analysis          | May 27, 2022 at 1:06 PM         |
| CTL02638                   | Horizontal Seismic Load | CTL02638-Mount Analysis - Rev H |

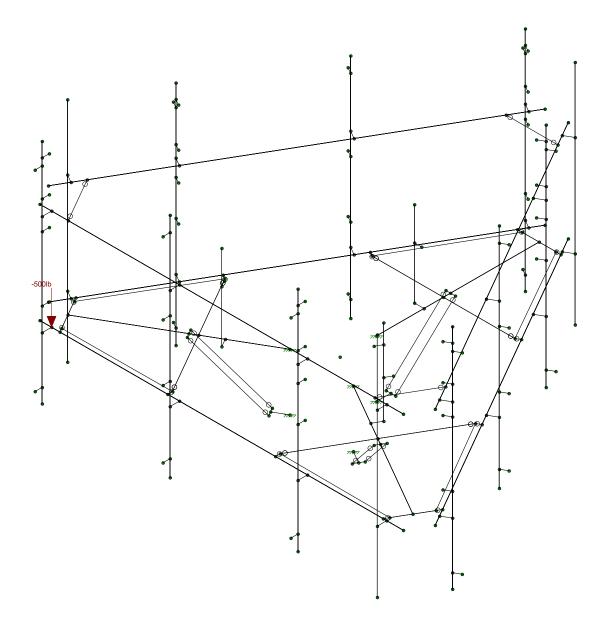




Loads: BLC 10, EV Envelope Only Solution

| Fullerton Engineering P.C. |                       | SK - 13                         |  |
|----------------------------|-----------------------|---------------------------------|--|
| GO                         | Mount Analysis        | May 27, 2022 at 1:06 PM         |  |
| CTL02638                   | Vertical Seismic Load | CTL02638-Mount Analysis - Rev H |  |

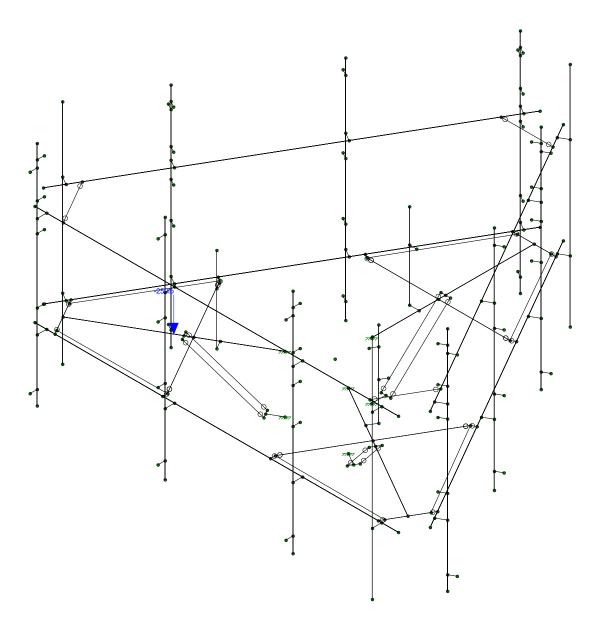




Loads: BLC 13, LM1 Envelope Only Solution

| Fullerton Engineering P.C. |                 | SK - 14                         |  |
|----------------------------|-----------------|---------------------------------|--|
| GO                         | Mount Analysis  | May 27, 2022 at 1:07 PM         |  |
| CTL02638                   | 500lb Live Load | CTL02638-Mount Analysis - Rev H |  |





Loads: BLC 25, LV1 Envelope Only Solution

| Fullerton Engineering P.C. |                 | SK - 15                         |
|----------------------------|-----------------|---------------------------------|
| GO                         | Mount Analysis  | May 27, 2022 at 1:07 PM         |
| CTL02638                   | 250lb Live Load | CTL02638-Mount Analysis - Rev H |

: Fullerton Engineering P.C.: GO: CTL02638

Mount Analysis

May 27, 2022 12:55 PM Checked By: BTK

#### (Global) Model Settings

| Display Sections for Member Calcs          | 5                  |
|--|--------------------|
| Max Internal Sections for Member Calcs     | 97                 |
| Include Shear Deformation?                 | Yes                |
| Increase Nailing Capacity for Wind?        | Yes                |
| Include Warping?                           | Yes                |
| Trans Load Btwn Intersecting Wood Wall?    | Yes                |
| Area Load Mesh (in^2)                      | 144                |
| Merge Tolerance (in)                       | .12                |
| P-Delta Analysis Tolerance                 | 0.50%              |
| Include P-Delta for Walls?                 | Yes                |
| Automatically Iterate Stiffness for Walls? | Yes                |
| Max Iterations for Wall Stiffness          | 3                  |
| Gravity Acceleration (in/sec^2)            | 386.4              |
| Wall Mesh Size (in)                        | 12                 |
| Eigensolution Convergence Tol. (1.E-)      | 4                  |
| Vertical Axis                              | Υ                  |
| Global Member Orientation Plane            | XZ                 |
| Static Solver                              | Sparse Accelerated |
| Dynamic Solver                             | Accelerated Solver |

| Hot Rolled Steel Code  | AISC 15th(360-16): LRFD |
|------------------------|-------------------------|
| Adjust Stiffness?      | Yes(Iterative)          |
| RISAConnection Code    | AISC 15th(360-16): LRFD |
| Cold Formed Steel Code | AISI S100-16: LRFD      |
| Wood Code              | None                    |
| Wood Temperature       | < 100F                  |
| Concrete Code          | None                    |
| Masonry Code           | None                    |
| Aluminum Code          | None - Building         |
| Stainless Steel Code   | AISC 14th(360-10): LRFD |
| Adjust Stiffness?      | Yes(Iterative)          |

| Number of Shear Regions       | 4                  |
|-------------------------------|--------------------|
| Region Spacing Increment (in) | 4                  |
| Biaxial Column Method         | Exact Integration  |
| Parme Beta Factor (PCA)       | .65                |
| Concrete Stress Block         | Rectangular        |
| Use Cracked Sections?         | Yes                |
| Use Cracked Sections Slab?    | No                 |
| Bad Framing Warnings?         | No                 |
| Unused Force Warnings?        | Yes                |
| Min 1 Bar Diam. Spacing?      | No                 |
| Concrete Rebar Set            | REBAR_SET_ASTMA615 |
| Min % Steel for Column        | 1                  |
| Max % Steel for Column        | 8                  |

: Fullerton Engineering P.C.: GO: CTL02638

Mount Analysis

May 27, 2022 12:55 PM Checked By: BTK

#### (Global) Model Settings, Continued

| Seismic Code                | ASCE 7-16   |
|-----------------------------|-------------|
| Seismic Base Elevation (in) | Not Entered |
| Add Base Weight?            | Yes         |
| Ct X                        | .02         |
| Ct Z                        | .02         |
| T X (sec)                   | Not Entered |
| T Z (sec)                   | Not Entered |
| RX                          | 3           |
| RZ                          | 3           |
| Ct Exp. X                   | .75         |
| Ct Exp. Z                   | .75         |
| SD1                         | 1           |
| SDS                         | 1           |
| S1                          | 1           |
| TL (sec)                    | 5           |
| Risk Cat                    | I or II     |
| Drift Cat                   | Other       |
| Om Z                        | 1           |
| Om X                        | 1           |
| Cd Z                        | 1           |
| Cd X                        | 1           |
| Rho Z                       | 1           |
| Rho X                       | 1           |
|                             |             |

# Hot Rolled Steel Design Parameters

|    | Label | Shape                  | Length[in] | Lbyy[in] | Lbzz[in] | Lcomp to | .Lcomp b | L-torque[i | . Kyy | Kzz | Cb Func |
|----|-------|------------------------|------------|----------|----------|----------|----------|------------|-------|-----|---------|
| 1  | M5    | Face Horizontal Bottom | 153.5      | 45.5     | 45.5     | 45.5     | 45.5     | 45.5       | 2.1   | 2.1 | Lateral |
| 2  | M10   | Face Horizontal Top    | 153.5      | 54       | 54       | 54       | 54       | 54         | 2.1   | 2.1 | Lateral |
| 3  | M11   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 4  | M12   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 5  | M13   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 6  | M14   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 7  | M19   | Face Horizontal Bottom | 153.5      | 45.5     | 45.5     | 45.5     | 45.5     | 45.5       | 2.1   | 2.1 | Lateral |
| 8  | M24   | Face Horizontal Top    | 153.5      | 54       | 54       | 54       | 54       | 54         | 2.1   | 2.1 | Lateral |
| 9  | M25   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 10 | M26   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 11 | M27   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 12 | M28   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 13 | M33   | Face Horizontal Bottom | 153.5      | 45.5     | 45.5     | 45.5     | 45.5     | 45.5       | 2.1   | 2.1 | Lateral |
| 14 | M38   | Face Horizontal Top    | 153.5      | 54       | 54       | 54       | 54       | 54         | 2.1   | 2.1 | Lateral |
| 15 | M39   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 16 | M40   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 17 | M41   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 18 | M42   | Mounting Pipe          | 96         | 42.5     | 42.5     | 42.5     | 42.5     | 42.5       | 2.1   | 2.1 | Lateral |
| 19 | M43   | Plate 1                | 2          |          |          |          |          |            |       |     | Lateral |
| 20 | M44   | Plate 1                | 2          |          |          |          |          |            |       |     | Lateral |
| 21 | M45   | Plate 1                | 2          |          |          |          |          |            |       |     | Lateral |
| 22 | M46   | Plate 1                | 2          |          |          |          |          |            |       |     | Lateral |
| 23 | M47   | Plate 1                | 2          |          |          |          |          |            |       |     | Lateral |
| 24 | M48   | Plate 1                | 2          |          |          |          |          |            |       |     | Lateral |
| 25 | M49   | Standoff Channel       | 60.388     |          |          | Lbyy     |          |            | 1     | 1   | Lateral |
| 26 | M50   | Angel 1                | 21.853     |          |          | Lbyy     |          |            | 1     | 1   | Lateral |
| 27 | M51   | Angel 1                | 21.853     |          |          | Lbyy     |          |            | 1     | 1   | Lateral |
| 28 | M52   | Angel 1                | 21.853     |          |          | Lbyy     |          |            | 1     | 1   | Lateral |
| 29 | M53   | Standoff Pipe          | 68.639     |          |          | Lbyy     |          |            | .65   | .65 | Lateral |
| 30 | M54   | Angel 2                | 46.501     |          |          | Lbyy     |          |            | .65   | .65 | Lateral |



: Fullerton Engineering P.C.: GO: CTL02638

: Mount Analysis

May 27, 2022 12:55 PM Checked By: BTK

#### Hot Rolled Steel Design Parameters (Continued)

|    | Label | Shape            | Length[in] | Lbyy[in] | Lbzz[in] | Lcomp to | Lcomp b | L-torque[i | . Kyy | Kzz | Cb | Func    |
|----|-------|------------------|------------|----------|----------|----------|---------|------------|-------|-----|----|---------|
| 31 | M55   | Angel 2          | 46.501     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 32 | M56   | Plate            | 14.353     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 33 | M57   | Plate            | 2          |          |          |          |         |            |       |     |    | Lateral |
| 34 | M58   | Plate            | 2          |          |          |          |         |            |       |     |    | Lateral |
| 35 | M59   | Tube             | 6          |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 36 | M60   | Angel 3          | 34.825     |          |          | Lbyy     |         |            | 1     | 1   |    | Lateral |
| 37 | M61   | Angel 3          | 34.825     |          |          | Lbyy     |         |            | 1     | 1   |    | Lateral |
| 38 | M66   | Standoff Channel | 60.388     |          |          | Lbyy     |         |            | 1     | 1   |    | Lateral |
| 39 | M67   | Standoff Pipe    | 68.639     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 40 | M68   | Angel 2          | 46.501     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 41 | M69   | Angel 2          | 46.501     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 42 | M70   | Plate            | 14.353     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 43 | M71   | Plate            | 2          |          |          |          |         |            |       |     |    | Lateral |
| 44 | M72   | Plate            | 2          |          |          |          |         |            |       |     |    | Lateral |
| 45 | M73   | Tube             | 6          |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 46 | M74   | Angel 3          | 34.825     |          |          | Lbyy     |         |            | 1     | 1   |    | Lateral |
| 47 | M75   | Angel 3          | 34.825     |          |          | Lbyy     |         |            | 1     | 1   |    | Lateral |
| 48 | M80   | Standoff Channel | 60.388     |          |          | Lbyy     |         |            | 1     | 1   |    | Lateral |
| 49 | M81   | Standoff Pipe    | 68.639     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 50 | M82   | Angel 2          | 46.501     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 51 | M83   | Angel 2          | 46.501     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 52 | M84   | Plate            | 14.353     |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 53 | M85   | Plate            | 2          |          |          |          |         |            |       |     |    | Lateral |
| 54 | M86   | Plate            | 2          |          |          |          |         |            |       |     |    | Lateral |
| 55 | M87   | Tube             | 6          |          |          | Lbyy     |         |            | .65   | .65 |    | Lateral |
| 56 | M88   | Angel 3          | 34.825     |          |          | Lbyy     |         |            | 1     | 1   |    | Lateral |
| 57 | M89   | Angel 3          | 34.825     |          |          | Lbyy     |         |            | 1     | 1   |    | Lateral |
| 58 | M111  | Pipe             | 36         | 36       | 36       | 36       | 36      | 36         | 2.1   | 2.1 |    | Lateral |
| 59 | M114  | Pipe Pipe        | 36         | 36       | 36       | 36       | 36      | 36         | 2.1   | 2.1 |    | Lateral |
| 60 | M117  | Pipe             | 36         | 36       | 36       | 36       | 36      | 36         | 2.1   | 2.1 |    | Lateral |

#### Material Takeoff

|    | Material         | Size     | Pieces | Length[in] | Weight[K] |
|----|------------------|----------|--------|------------|-----------|
| 1  | General          |          |        |            |           |
| 2  | RIGID            |          | 91     | 288        | 0         |
| 3  | Total General    |          | 91     | 288        | 0         |
| 4  |                  |          |        |            |           |
| 5  | Hot Rolled Steel |          |        |            |           |
| 6  | A36 Gr.36        | C3X3.5   | 3      | 181.2      | .056      |
| 7  | A36 Gr.36        | L2x2x3   | 6      | 279        | .057      |
| 8  | A36 Gr.36        | L3X3X3   | 3      | 65.6       | .02       |
| 9  | A36 Gr.36        | L3X3X4   | 6      | 209        | .085      |
| 10 | A36 Gr.36        | PL3/8x6  | 6      | 12         | .008      |
| 11 | A36 Gr.36        | PL1/2x6  | 9      | 55.1       | .047      |
| 12 | A500 Gr.46       | HSS6X4X4 | 3      | 18         | .022      |
| 13 | A53 Gr. B        | PIPE 2.0 | 6      | 568.5      | .164      |
| 14 | A53 Gr. B        | PIPE 2.5 | 12     | 1152       | .526      |
| 15 | A53 Gr. B        | PIPE 3.0 | 6      | 666.4      | .391      |
| 16 | Total HR Steel   |          | 60     | 3206.7     | 1.377     |



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: Mount Analysis

May 27, 2022 12:55 PM Checked By: BTK

#### **Basic Load Cases**

|    | BLC Description            | Category | X Gravity | Y Gravity | Z Gravity | Joint | Point | Distribu | .Area(M | .Surface |
|----|----------------------------|----------|-----------|-----------|-----------|-------|-------|----------|---------|----------|
| 1  | DL .                       | None     |           | -1        |           | 52    |       |          | 3       |          |
| 2  | DLi                        | None     |           |           |           | 52    |       | 48       | 3       |          |
| 3  | WL(0)                      | None     |           |           |           | 56    |       | 46       |         |          |
| 4  | WL(90)                     | None     |           |           |           | 52    |       | 41       |         |          |
| 5  | WL.i(0)                    | None     |           |           |           | 52    |       | 46       |         |          |
| 6  | WL.i(90)                   | None     |           |           |           | 50    |       | 41       |         |          |
| 7  | Ť                          | None     |           |           |           |       |       |          |         |          |
| 8  | EH(0)                      | None     |           |           |           | 52    |       | 48       |         |          |
| 9  | EH(90)                     | None     |           |           |           | 52    |       | 48       |         |          |
| 10 | EV                         | None     |           |           |           | 52    |       | 48       |         |          |
| 11 | WM(0)                      | None     |           |           |           | 52    |       | 46       |         |          |
| 12 | WM(90)                     | None     |           |           |           | 52    |       | 41       |         |          |
| 13 | LM1                        | None     |           |           |           | 1     |       |          |         |          |
| 14 | LM2                        | None     |           |           |           | 1     |       |          |         |          |
| 15 | LM3                        | None     |           |           |           | 1     |       |          |         |          |
| 16 | LM4                        | None     |           |           |           | 1     |       |          |         |          |
| 17 | LM5                        | None     |           |           |           | 1     |       |          |         |          |
| 18 | LM6                        | None     |           |           |           | 1     |       |          |         |          |
| 19 | LM7                        | None     |           |           |           | 1     |       |          |         |          |
| 20 | LM8                        | None     |           |           |           | 1     |       |          |         |          |
| 21 | LM9                        | None     |           |           |           | 1     |       |          |         |          |
| 22 | LM10                       | None     |           |           |           | 1     |       |          |         |          |
| 23 | LM11                       | None     |           |           |           | 1     |       |          |         |          |
| 24 | LM12                       | None     |           |           |           | 1     |       |          |         |          |
| 25 | LV1                        | None     |           |           |           |       | 1     |          |         |          |
| 26 | LV2                        | None     |           |           |           |       | 1     |          |         |          |
| 27 | LV3                        | None     |           |           |           |       | 1     |          |         |          |
| 28 | BLC 1 Transient Area Loads | None     |           |           |           |       |       | 69       |         |          |
| 29 | BLC 2 Transient Area Loads | None     |           |           |           |       |       | 69       |         |          |

#### **Load Combinations**

|    | Description                        | S | .PD | S | В | .Fa | .B | .Fa  | .B | .Fa  | .B | .Fa  | В | Fa | BLC | Fa | .BLC | Fa. | .B | .Fa | .B | <u>.Fa</u> | .B | .Fa |
|----|------------------------------------|---|-----|---|---|-----|----|------|----|------|----|------|---|----|-----|----|------|-----|----|-----|----|------------|----|-----|
| 1  | 1.4*DL                             | Υ | Υ   |   | 1 | 1.4 |    |      |    |      |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 2  | 1.2*DL + 1.0* WL(0)                | Y | Υ   |   | 1 | 1.2 |    | 1    |    |      |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 3  | 1.2*DL + 1.0* WL(30)               | Υ | Υ   |   | 1 | 1.2 | 3  | .869 | 4  |      |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 4  | 1.2*DL + 1.0* WL(60)               | Y | Υ   |   | 1 | 1.2 | 3  | .5   | 4  | .869 |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 5  | 1.2*DL + 1.0*WL(90)                | Υ | Υ   |   | 1 | 1.2 | 4  | 1    |    |      |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 6  | 1.2*DL + 1.0*WL(120)               | Y | Υ   |   | 1 | 1.2 | 3  | 5    | 4  | .869 |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 7  | 1.2*DL +1.0*WL(150)                | Y | Υ   |   | 1 | 1.2 | 3  | 8    | 4  | .5   |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 8  | 1.2*DL + 1.0 * WL(180)             | Y | Υ   |   | 1 | 1.2 | 3  | -1   |    |      |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 9  | 1.2*DL + 1.0* WL(210)              | Υ | Υ   |   | 1 | 1.2 | 3  | 8    | 4  | 5    |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 10 | 1.2*DL + 1.0* WL(240)              | Υ | Υ   |   | 1 | 1.2 | 3  | 5    | 4  | 8    |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 11 | 1.2*DL + 1.0*WL(270)               | Υ | Υ   |   | 1 | 1.2 | 4  | -1   |    |      |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 12 | 1.2*DL + 1.0*WL(300)               | Y | Υ   |   | 1 | 1.2 | 3  | .5   | 4  | 8    |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 13 | 1.2*DL +1.0*WL(330)                | Υ | Υ   |   | 1 | 1.2 | 3  | .869 | 4  | 5    |    |      |   |    |     |    |      |     |    |     |    |            |    |     |
| 14 | 1.2*DL+1.0*DLi+1.0*WL.i(0)+1.0*T   | Y | Υ   |   | 1 | 1.2 | 2  | 1    | 5  | 1    | 7  | 1    |   |    |     |    |      |     |    |     |    |            |    |     |
| 15 | 1.2*DL+1.0*DLi+1.0*WL.i(30)+1.0*T  | Υ | Υ   |   | 1 | 1.2 | 2  | 1    | 5  | .866 | 6  |      | 7 | 1  |     |    |      |     |    |     |    |            |    |     |
| 16 | 1.2*DL+1.0*DLi+1.0*WL.i(60)+1.0*T  | Y | Υ   |   | 1 | 1.2 | 2  | 1    | 5  | .5   | 6  | .866 | 7 | 1  |     |    |      |     |    |     |    |            |    |     |
| 17 | 1.2*DL+1.0*DLi+1.0*WL.i(90)+1.0*T  | Y | Υ   |   | 1 | 1.2 | 2  | 1    | 6  | 1    | 7  | 1    |   |    |     |    |      |     |    |     |    |            |    |     |
| 18 | 1.2*DL+1.0*DLi+1.0*WL.i(120)+1.0*T |   |     |   | 1 | 1.2 | 2  | 1    | 5  | 5    | 6  | .866 | 7 | 1  |     |    |      |     |    |     |    |            |    |     |
| 19 | 1.2*DL+1.0*DLi+1.0*WL.i(150)+1.0*T | Υ | Υ   |   | 1 | 1.2 | 2  | 1    | 5  | 8    | 6  | .5   | 7 | 1  |     |    |      |     |    |     |    |            |    |     |
| 20 | 1.2*DL+1.0*DLi+1.0*WL.i(180)+1.0*T | Υ | Υ   |   | 1 | 1.2 | 2  | 1    | 5  | -1   | 7  | 1    |   |    |     |    |      |     |    |     |    |            |    |     |
| 21 | 1.2*DL+1.0*DLi+1.0*WL.i(210)+1.0*T |   |     |   | 1 | 1.2 | 2  | 1    | 5  | 8    | 6  | 5    | 7 | 1  |     |    |      |     |    |     |    |            |    |     |
| 22 | 1.2*DL+1.0*DLi+1.0*WL.i(240)+1.0*T | Υ | Υ   |   | 1 | 1.2 | 2  | 1    | 5  | 5    | 6  | 8    | 7 | 1  |     |    |      |     |    |     |    |            |    |     |
| 23 | 1.2*DL+1.0*DLi+1.0*WL.i(270)+1.0*T | Υ | Υ   |   | 1 | 1.2 | 2  | 1    | 6  | -1   | 7  | 1    |   |    |     |    |      |     |    |     |    |            |    |     |



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Mount Analysis

May 27, 2022 12:55 PM Checked By: BTK

#### **Load Combinations (Continued)**

|    | a combinations (continues)           |   |     |          |        |       |       |            |          |            |     |   |                  |           |           |            |           |         |            | _              |    |
|----|--------------------------------------|---|-----|----------|--------|-------|-------|------------|----------|------------|-----|---|------------------|-----------|-----------|------------|-----------|---------|------------|----------------|----|
|    | Description SP                       |   |     |          |        |       |       | <u>Fa.</u> | <u>В</u> | <u>.Fa</u> | .B  |   | BLC <sub>F</sub> | <u>BL</u> | <u>CF</u> | <u>аВ.</u> | <u>Fa</u> | B       | <u>.Fa</u> | <u>.B</u>      | Fa |
| 24 |                                      | Υ |     |          | .2     |       |       | 5 .5       | 6        | 8          | . 7 | 1 |                  |           |           |            |           |         |            |                |    |
| 25 | 1.2*DL+1.0*DLi+1.0*WL.i(330)+1.0*T Y | Υ |     |          | .2     |       |       | .866       | 6        | 5          | 7   | 1 |                  |           |           |            |           |         |            |                |    |
| 26 | 1.2*DL+1.0*EH(0)+1.0*EV(+) Y         | Υ | 1   | 1        | .2 8   | 8     | 1 1   | 0 1        |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 27 |                                      | Υ | 1   | l 1      | .2     | 8     | 1 1   | 0 -1       |          |            |     |   |                  |           |           |            |           |         |            | П              |    |
| 28 |                                      | Υ |     |          | .2 9   |       |       | 0 1        |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 29 |                                      | Ÿ |     |          |        |       |       | 0 -1       |          |            |     |   |                  |           |           |            |           |         |            | П              |    |
|    | 1.2*DL+1.0*EH(180)+1.0*EV(+) Y       |   |     |          |        |       |       | 0 1        |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 31 |                                      | Ÿ |     |          |        |       |       | 0 -1       |          |            |     |   |                  |           |           |            |           |         |            | $\Box$         |    |
|    |                                      | Y |     |          |        |       |       | 0 1        |          |            |     |   |                  |           |           |            |           |         |            |                |    |
|    |                                      | Y |     |          | .2     |       |       | 0 -1       |          |            |     |   |                  |           |           |            |           |         |            | $\vdash$       |    |
| 33 | 1.2 DL+1.0 EH(2/0)+1.0 EV(-)   1     | Y |     |          | 9 8    |       |       | 0 -1       |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 34 | 0.9*DL+1.0*EH(0)-1.0*EV(+) Y         | Y |     |          |        |       |       |            |          |            |     |   |                  |           |           |            |           | +       |            | $\blacksquare$ |    |
| 35 |                                      |   |     | <u>.</u> | 9 8    | 5     | 1 1   | 0 1        |          |            |     |   | _                | _         |           |            |           |         |            | $\vdash$       |    |
|    |                                      | Y |     |          | 9 9    |       |       | 0 -1       |          |            |     |   |                  |           |           |            |           | +       |            | $\blacksquare$ |    |
| 37 |                                      | Υ |     |          | 9 9    |       |       | 0 1        |          |            |     |   |                  |           |           |            |           |         |            | $\vdash$       |    |
| 38 |                                      | Υ | 1   |          | 9 8    | 8 -   | .1 1  | 0 -1       |          |            |     |   |                  |           |           |            |           |         |            | $\square$      |    |
| 39 |                                      | Υ |     |          |        |       |       | 0 1        |          |            |     |   |                  |           |           |            | _         |         |            | ш              |    |
|    | 0.9*DL+1.0*EH(270)-1.0*EV(+) Y       |   |     | <u> </u> | 9   9  | 9   - | ·1  1 | 0 -1       |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 41 |                                      | Υ |     | L .      | 9   9  | 9   - | .1  1 | 0 1        |          |            |     |   |                  | $\perp$   |           |            |           | $\perp$ |            | Ш              |    |
| 42 |                                      | Υ |     |          |        |       |       | 1 1        |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 43 |                                      | Υ |     |          |        |       |       | 1.866      |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 44 | 1.2*DL+1.5*LM1+1.0*WM(60) Y          | Υ |     |          |        |       |       | 1 .5       |          | .866       |     |   |                  |           |           |            |           |         |            |                |    |
| 45 |                                      | Υ |     |          |        |       |       | 2 1        |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 46 | 1.2*DL+1.5*LM1+1.0*WM(120) Y         | Υ | 1   | l  1     | .2 1   | 3 1   | .5 1  | 15         | 12       | .866       |     |   |                  |           |           |            |           |         |            |                |    |
| 47 |                                      | Υ | 1   | l 1      | .2 1   | 31    | .5 1  | 18.        | 12       | .5         |     |   |                  |           |           |            |           |         |            |                |    |
| 48 |                                      | Υ |     |          |        |       |       | 1 -1       |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 49 |                                      | Υ | 1   | 1        | .2 1   | 31    | .5 1  | 18.        | 12       | 5          |     |   |                  |           |           |            |           |         |            | П              |    |
|    |                                      | Υ |     |          |        |       |       | 15         |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 51 |                                      | Ÿ |     |          |        |       |       | 2 -1       |          |            |     |   |                  |           |           |            |           |         |            | П              |    |
|    |                                      | Y |     |          |        |       |       | 1 .5       |          | - 8        |     |   |                  |           |           |            |           |         |            |                |    |
| 53 |                                      | Y |     |          |        |       |       | 1.866      |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 54 |                                      | Y |     |          |        |       |       | 1 1        | 12       | 0          |     |   |                  |           |           |            |           |         |            |                |    |
| 55 |                                      | Y | -   | 1        | 21     | 11    | 5 1   | 1.866      | 12       | 5          |     |   |                  |           |           |            |           |         |            | П              |    |
| 56 |                                      | Y |     |          |        |       |       | 1 .5       |          |            |     |   |                  |           |           |            |           |         |            |                |    |
|    |                                      | Y |     |          |        |       |       | 2 1        | 12       | .000       |     |   |                  |           |           |            |           |         |            | $\vdash$       |    |
| 57 | 1.2 DL+1.5 LIVIZ+1.0 VVIVI(90) 1     |   |     |          |        |       |       |            | 40       | 066        |     |   |                  |           |           |            |           |         |            |                |    |
| 58 |                                      | Y |     |          |        |       |       | 15         |          |            |     |   |                  |           |           |            |           |         |            | $\vdash$       |    |
| 59 |                                      | Y |     |          |        |       |       | 18         | 12       | .5         |     |   |                  |           |           |            |           |         |            |                |    |
| 60 | 1.2*DL+1.5*LM2+1.0*WM(180) Y         | Y |     |          |        |       |       | 1 -1       | 4.0      | _          |     |   |                  |           |           |            |           |         |            | $\vdash$       |    |
|    | 1.2*DL+1.5*LM2+1.0*WM(210) Y         |   |     |          |        |       |       | 18.        |          |            |     |   |                  |           |           |            | -         |         |            | $\vdash$       |    |
| 62 | 1.2*DL+1.5*LM2+1.0*WM(240) Y         |   |     |          |        |       |       | 15         |          | 8          |     |   |                  |           |           |            |           |         |            |                |    |
|    |                                      | Υ |     |          |        |       |       | 2 -1       |          |            |     |   |                  |           |           |            |           | -       |            |                |    |
| 64 |                                      | Υ |     |          |        |       |       | 1 .5       |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 65 |                                      | Υ |     |          |        |       |       | 1.866      | 12       | 5          |     |   |                  | $\perp$   |           |            |           | $\perp$ |            | Ш              |    |
| 66 |                                      | Υ |     |          |        |       | .5 1  |            |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 67 |                                      | Υ | _ 1 | 1        | .2 1   | 5 1   | .5 1  | 1.866      | 12       | .5         |     |   |                  |           |           |            |           |         |            | Ш              |    |
| 68 |                                      | Υ | 1   |          |        |       |       | 1 .5       | 12       | .866       |     |   |                  |           |           |            |           |         |            |                |    |
| 69 | 1.2*DL+1.5*LM3+1.0*WM(90) Y          | Υ | 1   | 1        | .2 1   | 5 1   | .5 1  | 2 1        |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 70 | 1.2*DL+1.5*LM3+1.0*WM(120) Y         | Υ | 1   | 1 1      | .2 1   | 51    | .5 1  | 15         | 12       | .866       |     |   |                  |           |           |            |           |         |            |                |    |
| 71 |                                      | Υ | 1   |          |        |       |       | 18.        |          |            |     |   |                  |           | T         | $\top$     |           | T       |            | П              |    |
|    |                                      | Υ | 1   |          |        |       |       | 1 -1       |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 73 |                                      | Ÿ | 1   |          |        |       |       | 18.        |          | 5          |     |   |                  |           |           |            |           |         |            |                |    |
| 74 |                                      | Ÿ |     |          |        |       |       | 15         |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 75 |                                      | Ÿ | _   |          |        |       |       | 2 -1       |          |            |     |   |                  |           |           |            |           |         |            |                |    |
|    |                                      | Y | -   |          |        |       |       | 1 .5       |          | 8.         |     |   |                  |           |           |            |           |         |            |                |    |
| 77 |                                      | Ÿ |     |          |        |       |       | 1.866      |          |            |     |   |                  |           |           |            |           |         |            |                |    |
| 78 |                                      | Y | 1   |          |        |       |       | 1 1        | 12       |            |     |   |                  |           |           |            |           |         |            |                |    |
| 79 |                                      | Y |     | 1        | 21     | 61    | 5 1   | 1.866      | 12       | 5          |     |   |                  |           |           |            |           |         |            |                |    |
| 80 | 1.2*DL+1.5*LM4+1.0*WM(60) Y          | Y | -   | 1        | 21     | 61    | 51    | 1 .5       | 12       | .866       |     |   |                  |           |           |            |           |         |            |                |    |
| 00 | 1.2 DE 1.3 EIVI4 1.0 VVIVI(00) 1.4   |   |     |          | ا   ۷. | U     | ا ال. | I .U       | 14       |            |     |   |                  |           |           |            |           |         |            |                |    |



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May 27, 2022 12:55 PM Checked By: BTK

#### **Load Combinations (Continued)**

| Luad Cumbinations (Cuntinued)        |            |     |    |     |     |             |    |      |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
|--------------------------------------|------------|-----|----|-----|-----|-------------|----|------|----|------|---|----|------|-----|-----|----|---|-----|-----|-----|---------------|-----|
| Description S                        | .PD        | S   | В  | Fa  | .Bl | Fa          | В  | Fa   | В  | .Fa  | В | Fa | BLCI | Fa  | BLC | Fa | В | .Fa | В   | Fa  | В             | Fa. |
| 81 1.2*DL+1.5*LM4+1.0*WM(90) Y       |            |     |    |     | 16  |             |    |      |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 82 1.2*DL+1.5*LM4+1.0*WM(120) Y      |            |     |    |     |     |             |    | 5    | 12 | 866  |   |    |      |     |     |    |   |     |     |     |               |     |
| 83 1.2*DL+1.5*LM4+1.0*WM(150) Y      | Y          |     |    |     |     |             |    | 8    |    |      |   |    |      |     |     |    |   |     |     |     | $\neg$        |     |
| 03 1.2 DLT1.3 LIVI4T1.0 VVIVI(130) 1 | · I        |     |    |     |     |             |    |      | 12 | .5   |   |    |      |     |     |    |   |     |     |     |               |     |
| 84 1.2*DL+1.5*LM4+1.0*WM(180) Y      | Υ .        |     |    |     | 16  |             |    |      |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 85 1.2*DL+1.5*LM4+1.0*WM(210) Y      |            |     |    |     |     |             |    | 8    |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 86 1.2*DL+1.5*LM4+1.0*WM(240) Y      | . Y        |     | 1  | 1.2 | 16  | 1.5         | 11 | 5    | 12 | 8    |   |    |      |     |     |    |   |     |     |     |               |     |
| 87 1.2*DL+1.5*LM4+1.0*WM(270) Y      | Υ .        |     | 1  | 1.2 | 16  | 1.5         | 12 | -1   |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 88 1.2*DL+1.5*LM4+1.0*WM(300) Y      |            |     |    |     |     |             |    | .5   |    | 8    |   |    |      |     |     |    |   |     |     |     |               |     |
| 89 1.2*DL+1.5*LM4+1.0*WM(330) Y      |            |     |    |     |     |             |    | .866 |    |      |   |    |      |     |     |    |   |     |     |     | $\neg$        |     |
|                                      |            |     |    |     |     |             |    |      | 12 | 5    |   |    |      |     |     |    |   |     |     |     |               |     |
| 90 1.2*DL+1.5*LM5+1.0*WM(0) Y        |            |     |    |     | 17  |             |    |      | 40 | _    |   |    |      |     |     |    |   |     |     |     | -             |     |
| 91 1.2*DL+1.5*LM5+1.0*WM(30) Y       | Υ .        |     |    |     |     |             |    | .866 |    |      |   |    |      |     |     | _  |   |     |     |     | _             |     |
| 92 1.2*DL+1.5*LM5+1.0*WM(60) Y       | Υ .        |     |    |     |     |             |    | .5   |    | .866 |   |    |      |     |     |    |   |     |     |     |               |     |
| 93 1.2*DL+1.5*LM5+1.0*WM(90) Y       | . Y        |     |    |     |     |             |    | 1    |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 94 1.2*DL+1.5*LM5+1.0*WM(120) Y      | Υ .        |     | 1  | 1.2 | 17  | 1.5         | 11 | 5    | 12 | .866 |   |    |      |     |     |    |   |     |     |     |               |     |
| 95 1.2*DL+1.5*LM5+1.0*WM(150) Y      | Υ          |     |    |     |     |             |    | 8    |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 96 1.2*DL+1.5*LM5+1.0*WM(180) Y      |            |     |    |     |     |             |    | -1   |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 97 1.2*DL+1.5*LM5+1.0*WM(210) Y      | Y          |     |    |     |     |             |    | 8    |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 00 4 0*DL 4 5*LM5 4 0*MM(210) 1      | T V        |     |    |     |     |             |    |      |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 98 1.2*DL+1.5*LM5+1.0*WM(240) Y      | . Y        |     |    |     |     |             |    | 5    |    | ŏ    |   |    |      |     |     | _  |   |     |     |     |               |     |
| 99 1.2*DL+1.5*LM5+1.0*WM(270) Y      |            |     |    |     |     |             |    | -1   |    |      |   |    |      |     |     | _  |   |     |     |     |               |     |
| 100 1.2*DL+1.5*LM5+1.0*WM(300) Y     |            |     |    |     |     |             |    | .5   |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 101 1.2*DL+1.5*LM5+1.0*WM(330) Y     | . Y        |     |    |     |     |             |    | .866 | 12 | 5    | L |    |      |     |     |    | L | L   |     |     |               |     |
| 102 1.2*DL+1.5*LM6+1.0*WM(0) Y       | Υ          |     |    |     | 18  |             |    |      |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 103 1.2*DL+1.5*LM6+1.0*WM(30) Y      |            |     |    |     |     |             |    | .866 | 12 | 5    |   |    |      |     |     |    |   |     |     |     |               |     |
| 104 1.2*DL+1.5*LM6+1.0*WM(60) Y      |            |     |    |     |     |             |    | .5   |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 105 1.2*DL+1.5*LM6+1.0*WM(90) Y      | \ <u>'</u> |     |    |     |     |             |    | 1    |    | .000 |   |    |      |     |     |    |   |     |     |     | _             |     |
| 105 1.2"DL+1.5"LIVIO+1.0"VVIVI(90) 1 | . Y        |     |    | 1.2 | 10  | 1.5         | 12 |      | 40 | 000  |   |    |      |     |     |    |   |     |     |     | $\rightarrow$ |     |
| 106 1.2*DL+1.5*LM6+1.0*WM(120) Y     | Υ .        |     | 1_ | 1.2 | 18  | <u>1.5</u>  | 11 | 5    | 12 | .860 |   |    |      |     |     |    |   |     |     |     | _             |     |
| 107 1.2*DL+1.5*LM6+1.0*WM(150) Y     | Υ .        |     |    |     |     |             |    | 8    |    | .5   |   |    |      |     |     |    |   |     |     |     |               |     |
| 108 1.2*DL+1.5*LM6+1.0*WM(180) Y     | . Y        |     |    |     |     |             |    | -1   |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 109 1.2*DL+1.5*LM6+1.0*WM(210) Y     | Υ .        |     | 1  | 1.2 | 18  | 1.5         | 11 | 8    | 12 | 5    |   |    |      |     |     |    |   |     |     |     |               |     |
| 110 1.2*DL+1.5*LM6+1.0*WM(240) Y     |            |     |    |     |     |             |    | 5    |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 111 1.2*DL+1.5*LM6+1.0*WM(270) Y     |            |     |    |     |     |             |    | -1   |    |      |   |    |      |     |     |    |   |     |     |     | $\neg$        |     |
| 112 1.2*DL+1.5*LM6+1.0*WM(300) Y     |            |     |    |     |     |             |    | .5   |    | Q    |   |    |      |     |     |    |   |     |     |     |               |     |
|                                      |            |     |    |     |     |             |    |      |    |      |   |    |      |     |     | _  |   |     |     |     | -             |     |
| 113 1.2*DL+1.5*LM6+1.0*WM(330) Y     |            |     |    |     |     |             |    | .866 | 12 | 5    |   |    |      |     |     |    |   |     |     |     | _             |     |
| 114 1.2*DL+1.5*LM7+1.0*WM(0) Y       | Υ .        |     |    |     | 19  |             |    |      |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 115 1.2*DL+1.5*LM7+1.0*WM(30) Y      |            |     |    |     |     |             |    | .866 |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 116 1.2*DL+1.5*LM7+1.0*WM(60) Y      | Υ          |     | 1  | 1.2 | 19  | 1.5         | 11 | .5   | 12 | .866 |   |    |      |     |     |    |   |     |     |     |               |     |
| 117 1.2*DL+1.5*LM7+1.0*WM(90) Y      | Υ          |     |    |     | 19  |             |    |      |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 118 1.2*DL+1.5*LM7+1.0*WM(120) Y     | Y          |     |    |     |     |             |    | 5    | 12 | .866 |   |    |      |     |     |    |   |     |     |     |               |     |
| 119 1.2*DL+1.5*LM7+1.0*WM(150) Y     |            |     |    |     |     |             |    | 8    |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
|                                      |            |     |    |     |     |             |    |      |    | .o   |   |    |      |     |     |    |   |     |     |     | $\rightarrow$ |     |
| 120 1.2*DL+1.5*LM7+1.0*WM(180) Y     |            |     |    |     |     |             |    | -1   |    | _    |   |    |      |     |     |    |   |     |     |     |               |     |
| 121 1.2*DL+1.5*LM7+1.0*WM(210) Y     |            |     |    |     |     |             |    | 8    |    |      |   |    |      |     |     | L  |   |     |     |     |               |     |
| 122 1.2*DL+1.5*LM7+1.0*WM(240) Y     |            |     |    |     |     |             |    | 5    |    | 8    |   |    |      |     |     |    |   |     |     |     |               |     |
| 123 1.2*DL+1.5*LM7+1.0*WM(270) Y     | Υ          | L T | 1  | 1.2 | 19  | 1.5         | 12 | -1   | L  | L    | L | L  | 「    | _ 1 |     | L  | L | L   | L 1 | _ 1 | _ [           |     |
| 124 1.2*DL+1.5*LM7+1.0*WM(300) Y     |            |     |    |     |     |             |    | .5   |    | 8    |   |    |      |     |     |    |   |     |     |     |               |     |
| 125 1.2*DL+1.5*LM7+1.0*WM(330) Y     |            |     |    |     |     |             |    | .866 |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 126 1.2*DL+1.5*LM8+1.0*WM(0) Y       |            |     | 1  | 1.2 | 20  | 1.5         | 11 | 1    | 14 | ٠.٠  |   |    |      |     |     |    |   |     |     |     |               |     |
|                                      |            |     | 1  | 1.2 | 20  | 1. <u>0</u> | 11 | .866 | 10 |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 127 1.2*DL+1.5*LM8+1.0*WM(30) Y      | Y          |     |    |     |     |             |    |      |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 128 1.2*DL+1.5*LM8+1.0*WM(60) Y      |            |     |    |     |     |             |    | .5   | 12 | .000 |   |    |      |     |     |    |   |     |     |     |               |     |
| 129 1.2*DL+1.5*LM8+1.0*WM(90) Y      |            |     |    |     | 20  |             |    |      |    |      |   |    |      |     |     |    |   |     | Ш   |     |               |     |
| 130 1.2*DL+1.5*LM8+1.0*WM(120) Y     |            |     |    |     |     |             |    | 5    |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 131   1.2*DL+1.5*LM8+1.0*WM(150)   Y |            | ]   | 1  | 1.2 | 20  | 1.5         | 11 | 8    | 12 | .5   |   |    | Ī    |     | _   | 1  |   |     |     | 1   |               | _   |
| 132 1.2*DL+1.5*LM8+1.0*WM(180) Y     |            |     |    |     |     |             |    | -1   |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 133 1.2*DL+1.5*LM8+1.0*WM(210) Y     |            |     |    |     |     |             |    | 8    |    | _ 5  |   |    |      |     |     |    |   |     |     |     |               |     |
|                                      |            |     |    |     |     |             |    | 5    |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 134 1.2*DL+1.5*LM8+1.0*WM(240) Y.    |            |     |    |     |     |             |    |      |    | 0    |   |    |      |     |     |    |   |     |     |     |               |     |
| 135 1.2*DL+1.5*LM8+1.0*WM(270) Y     |            |     |    |     |     |             |    | -1   |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 136 1.2*DL+1.5*LM8+1.0*WM(300) Y     |            |     |    |     |     |             |    | .5   |    |      |   |    |      |     |     |    |   |     |     |     |               |     |
| 137   1.2*DL+1.5*LM8+1.0*WM(330)   Y | Υ .        |     | 1  | 1.2 | 20  | 1.5         | 11 | .866 | 12 | 5    |   |    |      |     |     |    |   |     |     |     |               |     |



: Fullerton Engineering P.C.: GO: CTL02638 Mount Analysis

May 27, 2022 12:55 PM Checked By: BTK

#### **Load Combinations (Continued)**

| Description                      |     | .PD | S | В | F | a  | .B | .Fa | a  | В         | Fa.  | B.   | Fa   | B        | Fa. | BLC | Fa | .BLC | Fa | .B | Fa | В | Fa | В | Fa |
|----------------------------------|-----|-----|---|---|---|----|----|-----|----|-----------|------|------|------|----------|-----|-----|----|------|----|----|----|---|----|---|----|
| 138 1.2*DL+1.5*LM9+1.0*WM(0)     |     |     |   |   |   |    |    |     |    |           | 1    |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 139 1.2*DL+1.5*LM9+1.0*WM(30)    |     | Υ   |   |   |   |    |    |     |    |           |      | 12   | 2 .5 | ;        |     |     |    |      |    |    |    |   |    |   |    |
| 140 1.2*DL+1.5*LM9+1.0*WM(60)    |     | Υ   |   | 1 | 1 | .2 | 21 | 1.  | .5 | <u>11</u> | .5   | 12   | .86  | 6        |     |     |    |      |    |    |    |   |    |   |    |
| 141 1.2*DL+1.5*LM9+1.0*WM(90)    | Υ   | Υ   |   | 1 | 1 | .2 | 21 | 1.  | .5 | 12        | 1    |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 142 1.2*DL+1.5*LM9+1.0*WM(120)   |     |     |   |   |   |    |    |     |    |           |      | 12   | .86  | 6        |     |     |    |      |    |    |    |   |    |   |    |
| 143 1.2*DL+1.5*LM9+1.0*WM(150)   | Υ   | Υ   |   | 1 | 1 | .2 | 21 | 1.  | .5 | 11        | 8.   | . 12 | 2 .5 |          |     |     |    |      |    |    |    |   |    |   |    |
| 144 1.2*DL+1.5*LM9+1.0*WM(180)   | Υ   | Υ   |   | 1 | 1 | .2 | 21 | 1.  | .5 | <u>11</u> | -1   |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 145 1.2*DL+1.5*LM9+1.0*WM(210)   |     |     |   | 1 | 1 | .2 | 21 | 1.  | .5 | <u>11</u> | 8.   | 12   | 25   | 5        |     |     |    |      |    |    |    |   |    |   |    |
| 146 1.2*DL+1.5*LM9+1.0*WM(240)   |     |     |   |   |   |    |    |     |    |           |      |      | 28   |          |     |     |    |      |    |    |    |   |    |   |    |
| 147 1.2*DL+1.5*LM9+1.0*WM(270)   | Υ   | Υ   |   |   |   |    |    |     |    |           | -1   |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 148 1.2*DL+1.5*LM9+1.0*WM(300)   | Υ   | Υ   |   | 1 | 1 | .2 | 21 | 1.  | .5 | <u>11</u> | .5   | 12   | 28   |          |     |     |    |      |    |    |    |   |    |   |    |
| 149 1.2*DL+1.5*LM9+1.0*WM(330)   | Υ   |     |   |   |   |    |    |     |    |           |      |      | 25   |          |     |     |    |      |    |    |    |   |    |   |    |
| 150 1.2*DL+1.5*LM10+1.0*WM(0)    |     |     |   |   |   |    |    |     |    |           | 1    |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 151 1.2*DL+1.5*LM10+1.0*WM(30)   |     | Υ   |   | 1 | 1 | .2 | 22 | 1   | .5 | <u>11</u> | .866 | 12   | 2 .5 | ;        |     |     |    |      |    |    |    |   |    |   |    |
| 152 1.2*DL+1.5*LM10+1.0*WM(60)   |     |     |   |   |   |    |    |     |    |           |      |      | .86  |          |     |     |    |      |    |    |    |   |    |   |    |
| 153 1.2*DL+1.5*LM10+1.0*WM(90)   |     |     |   | 1 | 1 | .2 | 22 | 1.  | .5 | 12        | 1    |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 154 1.2*DL+1.5*LM10+1.0*WM(120   |     |     |   | 1 | 1 | .2 | 22 | 1.  | .5 | <u>11</u> | 5    | 12   | .86  | 6        |     |     |    |      |    |    |    |   |    |   |    |
| 155 1.2*DL+1.5*LM10+1.0*WM(150   |     |     |   | 1 | 1 | .2 | 22 | 1.  | .5 | 11        | 8.   | 12   | 2 .5 |          |     |     |    |      |    |    |    |   |    |   |    |
| 156 1.2*DL+1.5*LM10+1.0*WM(180   | ) Y | Υ   |   | 1 | 1 | .2 | 22 | 1.  | .5 | <u>11</u> | -1   |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 157 1.2*DL+1.5*LM10+1.0*WM(210   | ) Y | Υ   |   | 1 | 1 | .2 | 22 | 1.  | .5 | 11        | 8.   | 12   | 25   | 5        |     |     |    |      |    |    |    |   |    |   |    |
| 158 1.2*DL+1.5*LM10+1.0*WM(240   | ) Y | Υ   |   |   |   |    |    |     |    |           |      |      | 28   |          |     |     |    |      |    |    |    |   |    |   |    |
| 159 1.2*DL+1.5*LM10+1.0*WM(270   | ) Y | Υ   |   | 1 | 1 | .2 | 22 | 1.  | .5 | 12        | -1   |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 160 1.2*DL+1.5*LM10+1.0*WM(300   | ) Y | Υ   |   | 1 | 1 | .2 | 22 | 1.  | .5 | 11        | .5   | 12   | 28   |          |     |     |    |      |    |    |    |   |    |   |    |
| 161 1.2*DL+1.5*LM10+1.0*WM(330   | ) Y | Υ   |   | 1 | 1 | .2 | 22 | 1.  | .5 | 11        | .866 | 12   | 25   | 5        |     |     |    |      |    |    |    |   |    |   |    |
| 162 1.2*DL+1.5*LM11+1.0*WM(0)    |     |     |   |   |   |    | 23 |     |    |           |      |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 163 1.2*DL+1.5*LM11+1.0*WM(30)   | Υ   | Υ   |   |   |   |    |    |     |    |           |      |      | 2 .5 |          |     |     |    |      |    |    |    |   |    |   |    |
| 164 1.2*DL+1.5*LM11+1.0*WM(60)   |     |     |   | 1 | 1 | .2 | 23 | 1.  | .5 | <u>11</u> | .5   | 12   | .86  | 6        |     |     |    |      |    |    |    |   |    |   |    |
| 165 1.2*DL+1.5*LM11+1.0*WM(90)   |     |     |   |   |   |    |    |     |    |           | 1    |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 166 1.2*DL+1.5*LM11+1.0*WM(120   |     |     |   | 1 | 1 | .2 | 23 | 1.  | .5 | <u>11</u> | 5    | 12   | .86  | 6        |     |     |    |      |    |    |    |   |    |   |    |
| 167 1.2*DL+1.5*LM11+1.0*WM(150   | ) Y | Υ   |   |   |   |    |    |     |    |           |      |      | 2 .5 | <u> </u> |     |     |    |      |    |    |    |   |    |   |    |
| 168 1.2*DL+1.5*LM11+1.0*WM(180   | ) Y | Υ   |   |   |   |    |    |     |    |           | -1   |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 169 1.2*DL+1.5*LM11+1.0*WM(210   |     |     |   |   |   |    |    |     |    |           |      |      | 25   |          |     |     |    |      |    |    |    |   |    |   |    |
| 170 1.2*DL+1.5*LM11+1.0*WM(240   |     |     |   |   |   |    |    |     |    |           |      |      | 28   |          |     |     |    |      |    |    |    |   |    |   |    |
| 171   1.2*DL+1.5*LM11+1.0*WM(270 |     |     |   |   |   |    |    |     |    |           | -1   |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 172   1.2*DL+1.5*LM11+1.0*WM(300 |     |     |   |   |   |    |    |     |    |           |      |      | 28   |          |     |     |    |      |    |    |    |   |    |   |    |
| 173   1.2*DL+1.5*LM11+1.0*WM(330 |     |     |   |   |   |    |    |     |    |           |      | 12   | 25   | 5        |     |     |    |      |    |    |    |   |    |   |    |
| 174 1.2*DL+1.5*LM12+1.0*WM(0)    | Υ   | Υ   |   |   |   |    | 24 |     |    |           |      |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 175 1.2*DL+1.5*LM12+1.0*WM(30)   | Υ   | Υ   |   |   |   |    |    |     |    |           |      |      | 2 .5 |          |     |     |    |      |    |    |    |   |    |   |    |
| 176   1.2*DL+1.5*LM12+1.0*WM(60) | Υ   | Υ   |   |   |   |    |    |     |    |           |      | 12   | 2.86 | 6        |     |     |    |      |    |    |    |   |    |   |    |
| 177 1.2*DL+1.5*LM12+1.0*WM(90)   | Υ   | Υ   |   | 1 | 1 | .2 | 24 | 1.  | .5 | <u>12</u> | 1    |      | -    |          |     |     |    |      |    |    |    |   |    |   |    |
| 178 1.2*DL+1.5*LM12+1.0*WM(120   |     |     |   |   |   |    |    |     |    |           |      |      | 2.86 |          |     |     |    |      |    |    |    |   |    |   |    |
| 179 1.2*DL+1.5*LM12+1.0*WM(150   | _   | 1   |   |   |   |    |    |     |    |           |      |      | 2 .5 | <u> </u> |     |     |    |      |    |    |    |   |    |   |    |
| 180 1.2*DL+1.5*LM12+1.0*WM(180   |     |     |   |   |   |    |    |     |    |           | -1   |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 181 1.2*DL+1.5*LM12+1.0*WM(210   |     |     |   |   |   |    |    |     |    |           |      |      | 25   |          |     |     |    |      |    |    |    |   |    |   |    |
| 182 1.2*DL+1.5*LM12+1.0*WM(240   |     |     |   |   |   |    |    |     |    |           |      |      | 28   |          |     |     |    |      |    |    |    |   |    |   |    |
| 183 1.2*DL+1.5*LM12+1.0*WM(270   |     |     |   |   |   |    |    |     |    |           | -1   |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 184 1.2*DL+1.5*LM12+1.0*WM(300   |     |     |   |   |   |    |    |     |    |           |      |      | 28   |          |     |     |    |      |    |    |    |   |    |   |    |
| 185 1.2*DL+1.5*LM12+1.0*WM(330   |     |     |   |   |   |    |    |     |    | <u>11</u> | .866 | 12   | 25   |          |     |     |    |      |    |    |    |   |    |   |    |
| 186 1.2*DL+1.5*LV1               | Υ   |     |   |   |   |    | 25 |     |    |           |      |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 187 1.2*DL+1.5*LV2               | Υ   |     |   |   |   |    | 26 |     |    |           |      |      |      |          |     |     |    |      |    |    |    |   |    |   |    |
| 188 1.2*DL+1.5*LV3               | Υ   | Y   |   | 1 | 1 | .2 | 27 | 1.  | .5 |           |      |      |      |          |     |     |    |      |    |    |    |   |    |   |    |

: Fullerton Engineering P.C. : GO

: GO : CTL02638 : Mount Analysis May 27, 2022 12:55 PM Checked By: BTK

#### **Envelope Joint Reactions**

|    | Joint   |     | X [lb]    | LC | Y [lb]    | LC | Z [lb]    | LC | MX [k-ft] | LC | MY [k-ft] | LC | MZ [k-ft] | LC |
|----|---------|-----|-----------|----|-----------|----|-----------|----|-----------|----|-----------|----|-----------|----|
| 1  | N107    | max | 1733.386  | 5  | 368.923   | 8  | 6876.739  | 2  | .275      | 8  | 2.919     | 11 | .313      | 5  |
| 2  |         | min | -1746.909 | 11 | -2178.418 | 2  | -2654.216 | 8  | -1.685    | 2  | -2.865    | 5  | 403       | 11 |
| 3  | N112    | max | 30.511    | 6  | 4587.22   | 14 | -14.895   | 8  | 2.291     | 14 | .449      | 11 | .404      | 11 |
| 4  |         | min | -31.256   | 10 | 6.89      | 8  | -4757.859 | 14 | .001      | 8  | 544       | 5  | 495       | 5  |
| 5  | N121    | max | 6244.03   | 6  | 531.618   | 12 | 1889.093  | 12 | .914      | 6  | 1.828     | 2  | 1.533     | 6  |
| 6  |         | min | -2609.592 | 12 | -2307.558 | 6  | -3985.327 | 6  | 359       | 12 | -1.713    | 8  | 257       | 12 |
| 7  | N126    | max | 244.697   | 12 | 4790.144  | 6  | 2490.333  | 6  | .196      | 12 | .265      | 2  | .05       | 12 |
| 8  |         | min | -4304.476 | 6  | -278.812  | 12 | -138.269  | 12 | -1.45     | 6  | 392       | 7  | -1.93     | 18 |
| 9  | N135    | max | 2608.962  | 4  | 561.087   | 4  | 1909.562  | 4  | 1.032     | 98 | 1.437     | 8  | .353      | 4  |
| 10 |         | min | -6261.919 | 10 | -2307.211 | 10 | -4052.121 | 10 | 228       | 4  | -1.41     | 2  | -1.465    | 10 |
| 11 | N140    | max | 4333.711  | 10 | 4821.729  | 10 | 2506.605  | 10 | .187      | 4  | .219      | 84 | 2.073     | 10 |
| 12 |         | min | -238.116  | 4  | -271.815  | 4  | -134.671  | 4  | -1.228    | 10 | 355       | 90 | 052       | 4  |
| 13 | Totals: | max | 6080.71   | 5  | 7317.526  | 18 | 5456.653  | 2  |           |    |           |    |           |    |
| 14 |         | min | -6080.675 | 11 | 2931.203  | 40 | -5456.624 | 8  |           |    |           |    |           |    |

Stress ratio <1.0, members are adquate

# Envelope AISC 15th(360-16): LRFD Steel Code Checks

|    | <i></i> | 130 1311(300 | 10/1 = 111 |         | $\overline{}$ |          |          |    |                           |       |
|----|---------|--------------|------------|---------|---------------|----------|----------|----|---------------------------|-------|
|    | Member  | Shape        | Code Check | Loc[in] |               | Shear Ch |          | LC | phi*Pnphi*Pnphi*Mphi*M    | Eqn   |
| 1  | M54     | L2x2x3       | .858       | 0       | 5             | .364     | 46.501 y | 24 | 1702323392.8 .558 1.212   | H2-1  |
| 2  | M55     | L2x2x3       | .852       | 0       | 11            | .345     | 46.501 z | 15 | 1702323392.8 .558 1.21    | H2-1  |
| 3  | M83     | L2x2x3       | .795       | 0       | 6             | .356     | 46.501 y | 11 | 1702323392.8 .558 1.224   | H2-1  |
| 4  | M67     | PIPE 3.0     | .784       | 37.894  | 6             | .211     | 37.894   | 44 | 60554 65205 5.749 5.749   | H1-1b |
| 5  | M81     | PIPE 3.0     | .784       | 37.894  | 10            | .221     | 37.894   | 10 | 6055465205 5.749 5.749    | H1-1b |
| 6  | M68     | L2x2x3       | .773       | 0       | 9             | .364     | 46.501 y | 16 | 1702323392.8 .558 1.221   | H2-1  |
| 7  | M82     | L2x2x3       | .771       | 0       | 13            | .362     | 46.501 y | 21 | 1702323392.8 .558 1.22    | H2-1  |
| 8  | M69     | L2x2x3       | .767       | 0       | 2             | .344     | 46.501 z | 19 | 1702323392.8 .558 1.22    | H2-1  |
| 9  | M53     | PIPE 3.0     | .739       | 37.894  | 2             | .251     | 37.894   | 12 | 6055465205 5.749 5.749    | H1-1b |
| 10 | M84     | PL1/2x6      | .681       | 7.176   | 5             | .757     | 7.326 y  | 12 | 7801097200 1.012 12.15    | H1-1b |
| 11 | M70     | PL1/2x6      |            | 7.176   | 11            | .720     | 7.176 y  | 9  | 7801097200 1.012 12.15    | H1-1b |
| 12 | M56     | PL1/2x6      | .563       | 7.176   | 9             | .772     | 7.176 y  | 5  | 7801097200 1.012 12.15    | H1-1b |
| 13 | M38     | PIPE 2.0     | .541       | 11.193  | 6             | .348     | 12.792   | 6  | 1101432130 1.872 1.872 1  | H3-6  |
| 14 | M10     | PIPE 2.0     | .529       | 11.193  | 10            | .339     | 147      | 5  | 1101432130 1.872 1.872 1  | H3-6  |
| 15 | M39     | PIPE 2.5     | .526       | 70      | 12            | .151     | 33       | 13 | 3225050715 3.596 3.596 1  | H1-1b |
| 16 | M11     | PIPE 2.5     | .523       | 70      | 5             | .165     | 33       | 5  | 3225050715 3.596 3.596 1  | H1-1b |
| 17 | M40     | PIPE 2.5     | .516       | 70      | 13            | .282     | 70       | 13 | 3225050715 3.596 3.596 1  | H3-6  |
| 18 | M24     | PIPE 2.0     | .508       | 40.7    | 10            | .310     | 47       | 9  | 1101432130 1.872 1.872 1  | H3-6  |
| 19 | M12     | PIPE 2.5     | .503       | 70      | 5             | .297     | 70       | 5  | 3225050715 3.596 3.596 1  | H3-6  |
| 20 | M26     | PIPE 2.5     | .496       | 70      | 9             | .280     | 70       | 9  | 3225050715 3.596 3.596 1  | H3-6  |
| 21 | M25     | PIPE 2.5     | .466       | 70      | 9             | .145     | 33       | 9  | 3225050715 3.596 3.596 1  | H1-1b |
| 22 | M49     | C3X3.5       | .462       | 30.194  | 12            | .539     | 30.194 y | 25 | 1046935316 .788 3.348     | H1-1b |
| 23 | M45     | PL3/8x6      | .450       | 0       | 5             | .427     | 0 v      | 6  | 7158372900 .57 9.113      | H1-1b |
| 24 | M13     | PIPE 2.5     | .448       | 70      | 11            | .300     | 34       | 10 | 3225050715 3.596 3.596 1  | H3-6  |
| 25 | M41     | PIPE 2.5     | .444       | 70      | 7             | .300     | 34       | 6  | 3225050715 3.596 3.596 1  | H3-6  |
| 26 | M66     | C3X3.5       | . 101      | 30.194  | 5             | .538     | 30.194 y | 16 | 1046935316 .788 3.348     | H1-1b |
| 27 | M80     | C3X3.5       | .429       | 30.194  | 9             | .535     | 30.194 y | 21 | 1046935316 .788 3.348     | H1-1b |
| 28 | M14     | PIPE 2.5     | .425       | 70      | 11            | .195     | 28       | 10 | 3225050715 3.596 3.596 1  | H1-1b |
| 29 | M27     | PIPE 2.5     | .420       | 70      | 4             | .251     | 34       | 2  | 3225050715 3.596 3.596 1  | H1-1b |
| 30 | M42     | PIPE 2.5     | .404       | 70      | 7             | .191     | 28       | 6  | 3225050715 3.596 3.596 1  | H1-1b |
| 31 | M28     | PIPE 2.5     | .387       | 70      | 3             | .155     | 28       | 2  | 3225050715 3.596 3.596 1  | H1-1b |
| 32 | M48     | PL3/8x6      | .377       | 0       | 11            | .396     | 0 y      | 9  | 71583 72900  .57   9.113  | H1-1b |
| 33 | M43     | PL3/8x6      | .364       | 0       | 13            | .384     | 0 y      | 2  | 7158372900 .57 9.113      | H1-1b |
| 34 | M47     | PL3/8x6      | .347       | 0       | 9             | .385     | 2 y      | 10 | 7158372900 .57 9.113      | H1-1b |
| 35 | M33     | PIPE 3.0     | .303       | 41.573  | 13            | .328     | 54.365   | 6  | 4643965205 5.749 5.749 1  | H3-6  |
| 36 | M46     | PL3/8x6      | .298       | 0       | 7             | .395     | 0 y      | 5  | 7158372900 .57 9.113      | H1-1b |
| 37 | M44     | PL3/8x6      | .293       | 0       | 3             | .401     | 0 y      | 13 | 7158372900 .57 9.113      | H1-1b |
| 38 | M5      | PIPE_3.0     | .284       | 41.573  | 5             | .344     | 145      | 5  | 46439 65205 5.749 5.749 1 | H3-6  |

: Fullerton Engineering P.C. : GO

: CTL02638 Mount Analysis

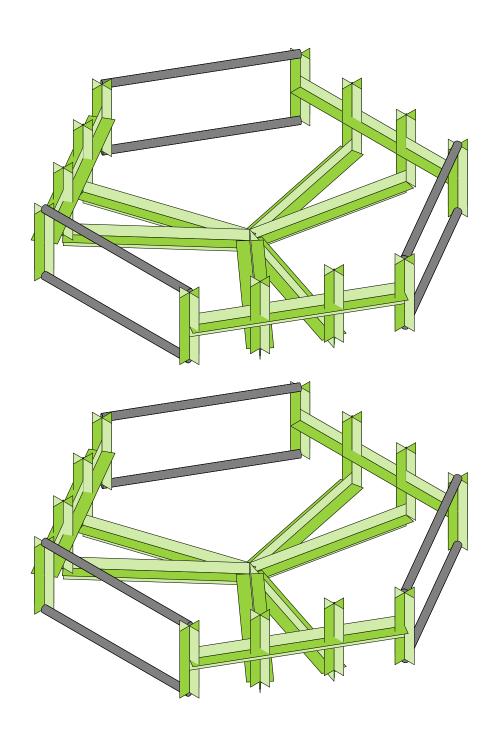
May 27, 2022 12:55 PM Checked By: BTK

#### Envelope AISC 15th(360-16): LRFD Steel Code Checks (Continued)

|    | Member | Shape    | Code Check | Loc[in] | LC  | Shear Ch | Loc[in] |   | LC  | phi*Pnp | hi*Pn | phi*M  | phi*M   | Eqn   |
|----|--------|----------|------------|---------|-----|----------|---------|---|-----|---------|-------|--------|---------|-------|
| 39 | M19    | PIPE 3.0 | .269       | 41.573  | 9   | .312     | 145     |   | 9   | 464396  | 55205 | 5.749  | 5.749 1 | H3-6  |
| 40 | M75    | L3X3X4   | .130       | 17.775  | 6   | .011     | 34.825  | У | 2   | 387154  | 16656 | 1.688  | 3.677   | H2-1  |
| 41 | M61    | L3X3X4   | .118       | 17.05   | 140 | .017     | 0       | У | 11  | 387154  | 16656 | 1.688  | 3.677   | H2-1  |
| 42 | M89    | L3X3X4   | .118       | 17.05   | 99  | .008     | 0       | У | 8   | 387154  | 16656 | 1.688  | 3.677   | H2-1  |
| 43 | M60    | L3X3X4   | .113       | 17.413  | 12  | .017     | 0       | y | 11  | 387154  | 16656 | 1.688  | 3.677   | H2-1  |
| 44 | M73    | HSS6X4X4 | .109       | 0       | 6   | .092     | 0       | У | 6   | 177941  | 78020 | 22.252 | 29.428  | H1-1b |
| 45 | M88    | L3X3X4   | .104       | 17.05   | 86  | .008     | 34.825  | У | 8   | 387154  | 16656 | 1.688  | 3.677   | H2-1  |
| 46 | M74    | L3X3X4   | .103       | 17.05   | 176 | .011     | 34.825  | У | 2   | 387154  | 16656 | 1.688  | 3.677   | H2-1  |
| 47 | M87    | HSS6X4X4 | .099       | 0       | 98  | .084     | 0       | У | 99  | 177941  | 78020 | 22.252 | 29.428  | H1-1b |
| 48 | M59    | HSS6X4X4 | .099       | 0       | 139 | .084     | 0       | У | 139 | 177941  |       |        | 29.428  | H1-1b |
| 49 | M86    | PL1/2x6  | .098       | 0       | 11  | 1.271    | 0       | У | 7   | 962229  | 7200  | 1.012  | 12.15   | H1-1b |
| 50 | M58    | PL1/2x6  | .079       | 0       | 10  | 1.365    | 0       | У | 11  | 962229  | 7200  | 1.012  | 12.15   | H1-1b |
| 51 | M71    | PL1/2x6  | .075       | 0       | 5   | 1.329    | 0       | У | 9   |         | 7200  |        | 12.15   | H1-1b |
| 52 | M72    | PL1/2x6  | .073       | 0       | 2   | 1.279    | 0       | y | 3   | 962229  | 7200  | 1.012  | 12.15   | H1-1b |
| 53 | M117   | PIPE 2.0 | .068       | 0       | 10  | .008     | 6.125   |   | 10  | 199633  |       | 1.872  | 1.872 1 | H1-1b |
| 54 | M57    | PL1/2x6  | .056       | 0       | 13  | 1.418    | 0       | У | 5   | 962229  | 7200  | 1.012  | 12.15   | H1-1b |
| 55 | M85    | PL1/2x6  | .049       | 0       | 2   | 1.337    | 0       | У | 13  | 962229  | 7200  | 1.012  | 12.15   | H1-1b |
| 56 | M114   | PIPE_2.0 | .047       | 0       | 3   | .008     | 0       |   | 6   | 199633  | 32130 | 1.872  | 1.872 1 | H1-1b |
| 57 | M111   | PIPE 2.0 | .046       | 0       | 11  | .008     | 0       |   | 2   | 199633  | 32130 | 1.872  | 1.872 1 | H1-1b |
| 58 | M51    | L3X3X3   | .040       | 10.926  | 4   | .197     | 0       | Z | 13  |         | 35316 | 1.32   | 2.905   | H2-1  |
| 59 | M50    | L3X3X3   | .040       | 10.926  | 12  | .195     | 0       | Z | 9   | 276583  | 35316 | 1.32   | 2.905   | H2-1  |
| 60 | M52    | L3X3X3   | .032       | 10.926  | 2   | .213     | 21.853  | Z | 5   | 276583  | 35316 | 1.32   | 2.833   | H2-1  |

Stress ratio <1.0, members are adquate

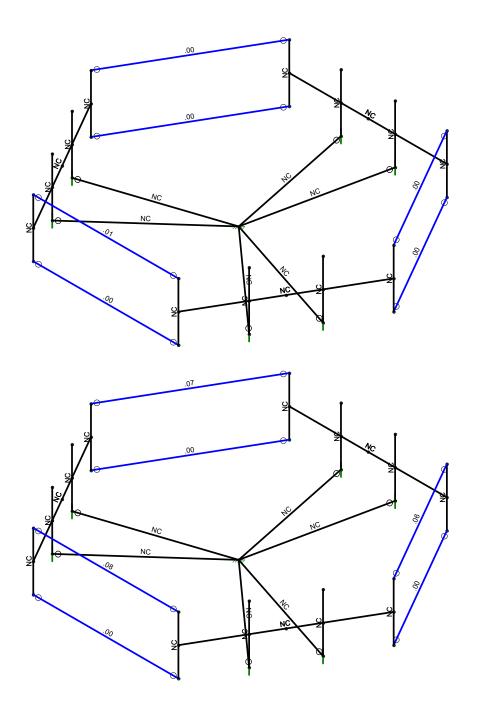




| Fullerton Engineering P.C. |                       | SK - 1                             |
|----------------------------|-----------------------|------------------------------------|
| GO                         | Collar Mount Analysis | May 31, 2022 at 9:30 AM            |
| CTL02638                   | 3D Render             | CTL02638-Collar Mount Analysis.r3d |



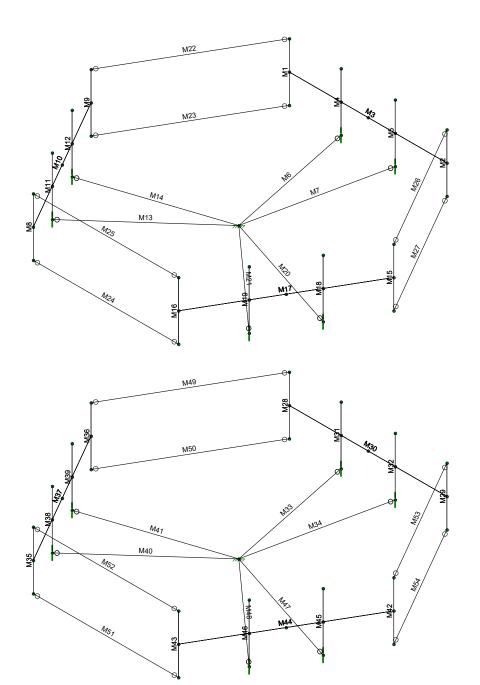




Member Code Checks Displayed (Enveloped) Envelope Only Solution

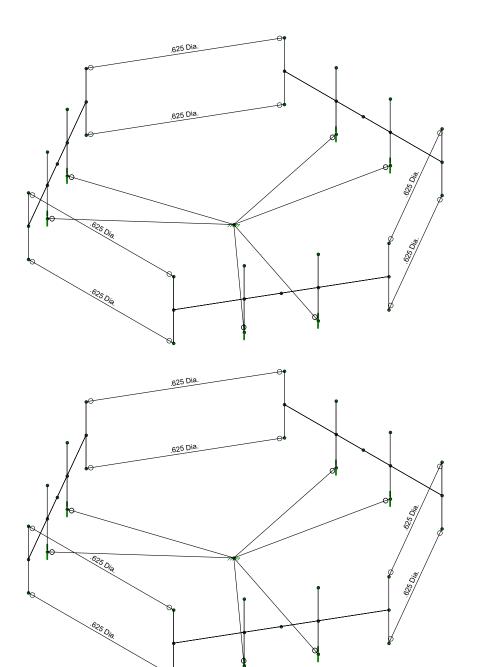
| Fullerton Engineering P.C. |                       | SK - 2                             |  |
|----------------------------|-----------------------|------------------------------------|--|
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| CTL02638                   | Unity Graphic         | CTL02638-Collar Mount Analysis.r3d |  |





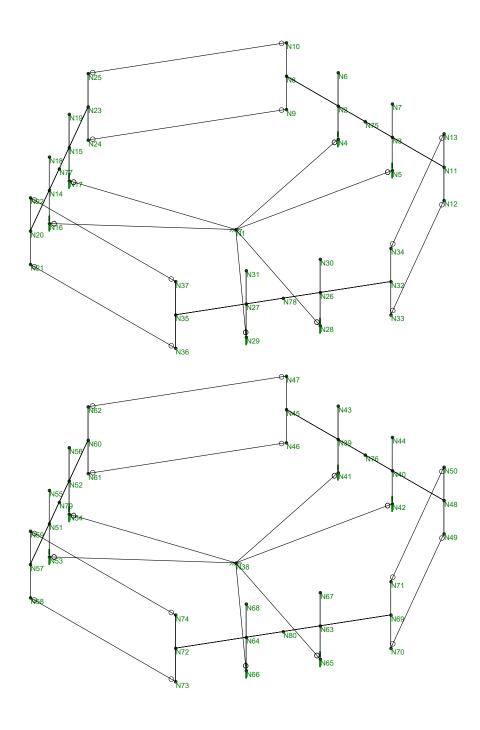
| Fullerton Engineering P.C. |                       | SK - 3                             |  |
|----------------------------|-----------------------|------------------------------------|--|
| GO                         | Collar Mount Analysis | May 31, 2022 at 9:31 AM            |  |
| CTL02638                   | Member Label          | CTL02638-Collar Mount Analysis.r3d |  |





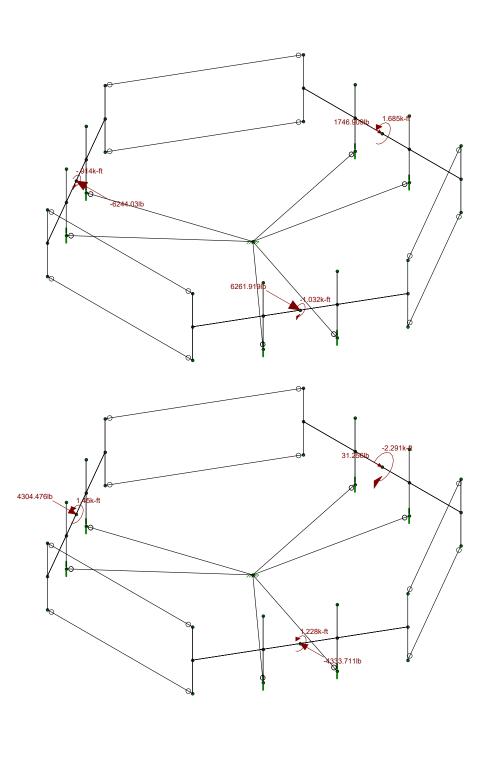
| Fullerton Engineering P.C. |                       | SK - 4                             |  |
|----------------------------|-----------------------|------------------------------------|--|
| GO                         | Collar Mount Analysis | May 31, 2022 at 9:31 AM            |  |
| CTL02638                   | Shape                 | CTL02638-Collar Mount Analysis.r3d |  |





| Fullerton Engineering P.C. |                       | SK - 5                             |
|----------------------------|-----------------------|------------------------------------|
| GO                         | Collar Mount Analysis | May 31, 2022 at 9:31 AM            |
| CTL02638                   | Nodes                 | CTL02638-Collar Mount Analysis.r3d |

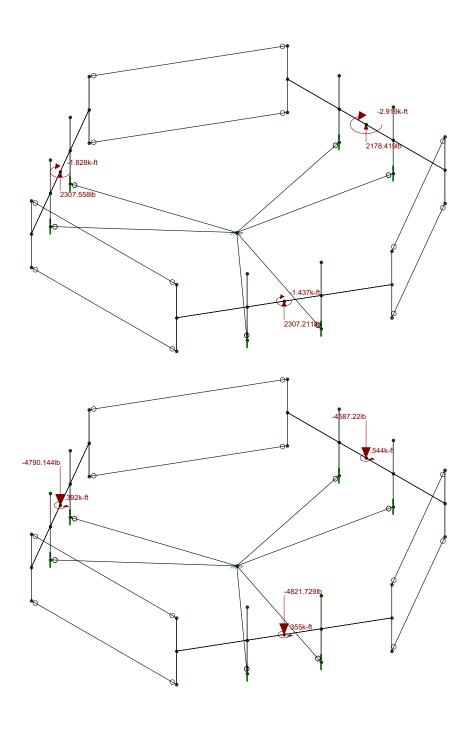




Loads: BLC 1, Max X Envelope Only Solution

| Fullerton Engineering P.C. |                       | SK - 6                             |
|----------------------------|-----------------------|------------------------------------|
| GO                         | Collar Mount Analysis | May 31, 2022 at 9:32 AM            |
| CTL02638                   | Max X Reactions       | CTL02638-Collar Mount Analysis.r3d |

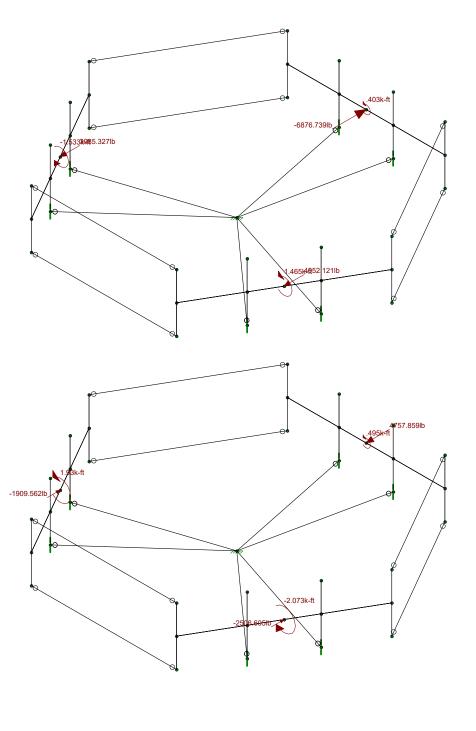




Loads: BLC 2, Max Y Envelope Only Solution

| Fullerton Engineering P.C. |                       | SK - 7                             |  |
|----------------------------|-----------------------|------------------------------------|--|
| GO                         | Collar Mount Analysis | May 31, 2022 at 9:32 AM            |  |
| CTL02638                   | Max Y Reactions       | CTL02638-Collar Mount Analysis.r3d |  |





Loads: BLC 3, Max Z Envelope Only Solution

| Fullerton Engineering P.C. |                       | SK - 8                             |  |
|----------------------------|-----------------------|------------------------------------|--|
| GO                         | Collar Mount Analysis | May 31, 2022 at 9:32 AM            |  |
| CTL02638                   | Max Z Reactions       | CTL02638-Collar Mount Analysis.r3d |  |

: Fullerton Engineering P.C.: GO: CTL02638

Collar Mount Analysis

May 31, 2022 9:18 AM Checked By: BTK

#### (Global) Model Settings

| Display Sections for Member Calcs          | 5                  |
|--|--------------------|
| Max Internal Sections for Member Calcs     | 97                 |
| Include Shear Deformation?                 | Yes                |
| Increase Nailing Capacity for Wind?        | Yes                |
| Include Warping?                           | Yes                |
| Trans Load Btwn Intersecting Wood Wall?    | Yes                |
| Area Load Mesh (in^2)                      | 144                |
| Merge Tolerance (in)                       | .12                |
| P-Delta Analysis Tolerance                 | 0.50%              |
| Include P-Delta for Walls?                 | Yes                |
| Automatically Iterate Stiffness for Walls? | Yes                |
| Max Iterations for Wall Stiffness          | 3                  |
| Gravity Acceleration (in/sec^2)            | 386.4              |
| Wall Mesh Size (in)                        | 12                 |
| Eigensolution Convergence Tol. (1.E-)      | 4                  |
| Vertical Axis                              | Υ                  |
| Global Member Orientation Plane            | XZ                 |
| Static Solver                              | Sparse Accelerated |
| Dynamic Solver                             | Accelerated Solver |

| Hot Rolled Steel Code  | AISC 15th(360-16): LRFD |
|------------------------|-------------------------|
| Adjust Stiffness?      | Yes(Iterative)          |
| RISAConnection Code    | AISC 15th(360-16): LRFD |
| Cold Formed Steel Code | None                    |
| Wood Code              | None                    |
| Wood Temperature       | < 100F                  |
| Concrete Code          | None                    |
| Masonry Code           | None                    |
| Aluminum Code          | None - Building         |
| Stainless Steel Code   | None                    |

| Number of Shear Regions       | 4                  |
|-------------------------------|--------------------|
| Region Spacing Increment (in) | 4                  |
| Biaxial Column Method         | Exact Integration  |
| Parme Beta Factor (PCA)       | .65                |
| Concrete Stress Block         | Rectangular        |
| Use Cracked Sections?         | Yes                |
| Use Cracked Sections Slab?    | No                 |
| Bad Framing Warnings?         | No                 |
| Unused Force Warnings?        | Yes                |
| Min 1 Bar Diam. Spacing?      | No                 |
| Concrete Rebar Set            | REBAR SET ASTMA615 |
| Min % Steel for Column        | 1                  |
| Max % Steel for Column        | 8                  |



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: Collar Mount Analysis

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# (Global) Model Settings, Continued

| Seismic Code                | ASCE 7-16   |
|-----------------------------|-------------|
| Seismic Base Elevation (in) | 3090.36     |
| Add Base Weight?            | Yes         |
| Ct X                        | .02         |
| Ct Z                        | .02         |
| T X (sec)                   | Not Entered |
| T Z (sec)                   | Not Entered |
| RX                          | 3           |
| RZ                          | 3           |
| Ct Exp. X                   | .75         |
| Ct Exp. Z                   | .75         |
| SD1                         | .086        |
| SDS                         | .218        |
| S1                          | .054        |
| TL (sec)                    | 6           |
| Risk Cat                    | I or II     |
| Drift Cat                   | Other       |
| Om Z                        | 1           |
| Om X                        | 1           |
| Cd Z                        | 4           |
| Cd X                        | 4           |
| Rho Z                       | 1           |
| Rho X                       | 1           |
|                             |             |

# Hot Rolled Steel Design Parameters

|    | Label | Shape     | Length[in] | Lbyy[in] | Lbzz[in] Lcomp toLcomp | b L-torque[i | . Kyy | Kzz | Cb | Func    |
|----|-------|-----------|------------|----------|------------------------|--------------|-------|-----|----|---------|
| 1  | M22   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 2  | M23   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 3  | M24   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 4  | M25   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 5  | M26   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 6  | M27   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 7  | M49   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 8  | M50   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 9  | M51   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 10 | M52   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 11 | M53   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |
| 12 | M54   | .625 Dia. | 15.083     |          | Lbyy                   |              | .65   | .65 |    | Lateral |

#### **Material Takeoff**

|   | Material         | Size      | Pieces | Length[in] | Weight[K] |
|---|------------------|-----------|--------|------------|-----------|
| 1 | General          |           |        |            |           |
| 2 | RIGID            |           | 42     | 407        | 0         |
| 3 | Total General    |           | 42     | 407        | 0         |
| 4 |                  |           |        |            |           |
| 5 | Hot Rolled Steel |           |        |            |           |
| 6 | A36 Gr.36        | .625 Dia. | 12     | 181        | .016      |
| 7 | Total HR Steel   |           | 12     | 181        | .016      |

#### **Basic Load Cases**

|   | BLC Description | Category | X Gravity Y Gravity | Z Gravity | Joint | Point | Distribu | .Area(M | Surface |
|---|-----------------|----------|---------------------|-----------|-------|-------|----------|---------|---------|
| 1 | Max X           | None     |                     |           | 12    |       |          | ,       |         |
| 2 | Max Y           | None     | -1                  |           | 12    |       |          |         |         |



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May 31, 2022 9:18 AM Checked By: BTK

#### **Basic Load Cases (Continued)**

|   | BLC Description | Category | X Gravity | Y Gravity | Z Gravity | Joint | Point | Distribu | .Area(M | .Surface |  |
|---|-----------------|----------|-----------|-----------|-----------|-------|-------|----------|---------|----------|--|
| 3 | Max Ż           | None     |           |           |           | 12    |       |          |         |          |  |

#### **Load Combinations**

|   | Description   | S | .PD | S | В | Fa. | B | Fa | B. | Fa | aB | Fa | B | Fa | BLC | Fa | .BLC | Fa | .B | Fa | .B | Fa | .BI | Fa |
|---|---------------|---|-----|---|---|-----|---|----|----|----|----|----|---|----|-----|----|------|----|----|----|----|----|-----|----|
| 1 | Max Reactions | Υ | Y   |   | 1 | 1   | 2 | 1  | 3  | 1  |    |    |   |    |     |    |      |    |    |    |    |    |     |    |

#### **Envelope Joint Reactions**

|    | Joint   |     | X [lb]     | LC | V [lb]    | LC | Z [lb]    | 1.0     | MV (L #1  | LC | MAX/ FIZ #1        | LC | M7 (L #1       | LC      |
|----|---------|-----|------------|----|-----------|----|-----------|---------|-----------|----|--------------------|----|----------------|---------|
| 1  | N1      | may | -1764.798  |    | Y [lb]    | 1  | -1160.709 | LC<br>1 | MX [k-ft] | 1  | MY [k-ft]<br>8.194 | 1  | MZ [k-ft]<br>0 |         |
| 2  | INI     |     | -1764.798  |    | 0         | 1  | -1160.709 | 1       | 0         | 1  | 8.194              | 1  | 0              | 1       |
| 3  | N4      | max | 0          | 1  | -1174.757 | 1  | 0         | 1       | 0         | 1  | <u> </u>           | 1  | 0              | 1       |
| 4  | 114     | min | 0          | 1  | -1174.757 | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 5  | N5      | max | 0          | 1  | -1001.037 | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 6  | 110     | min | 0          | 1  | -1001.037 | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 7  | N16     | max | 0          | 1  | -976.867  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 8  | 1110    | min | 0          | 1  | -976.867  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 9  | N17     | max | 0          | 1  | -1328.066 | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 10 |         | min | 0          | 1  | -1328.066 | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 11 | N28     | max | 0          | 1  | -1048.519 | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 12 |         | min | 0          | 1  | -1048.519 | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 13 | N29     | max | 0          | 1  | -1256.068 | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 14 |         | min | 0          | 1  | -1256.068 | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 15 | N38     | max | -2.021     | 1  | 0         | 1  | -341.692  | 1       | 0         | 1  | -1.818             | 1  | 0              | 1       |
| 16 |         | min | -2.021     | 1  | 0         | 1  | -341.692  | 1       | 0         | 1  | -1.818             | 1  | 0              | 1       |
| 17 | N41     | max | 0          | 1  | 3418.302  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 18 |         | min | 0          | 1  | 3418.302  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 19 | N42     | max | 0          | 1  | 1171.542  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 20 |         | min | 0          | 1  | 1171.542  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 21 | N53     | max | 0          | 1  | 3351.785  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 22 |         | min | 0          | 1  | 3351.785  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 23 | N54     | max | 0          | 1  | 1440.984  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 24 |         | min | 0          | 1  | 1440.984  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 25 | N65     | max | 0          | 1  | 2203.548  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 26 |         | min | 0          | 1  | 2203.548  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 27 | N66     | max | 0          | 1  | 2620.805  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 28 |         | min | 0          | 1  | 2620.805  | 1  | 0         | 1       | 0         | 1  | 0                  | 1  | 0              | 1       |
| 29 | Totals: |     | 17 00.0 10 | 1  | 7421.651  | 1  | -1502.401 | 1       |           |    |                    |    |                | $\perp$ |
| 30 |         | min | -1766.819  | 1_ | 7421.651  | 1  | -1502.401 | 1       |           |    |                    |    |                |         |

Stress ratio <1.0, members are adequate

# Envelope AISC 15th(360-16): LRFD Steel Code Checks

|    | Member | Shape     | Code Check/ | Loc[in] | LG | Shear Ch | Loc[in] | LC | phi*Pnphi*Pnphi*Mphi*M | Egn   |
|----|--------|-----------|-------------|---------|----|----------|---------|----|------------------------|-------|
| 1  | M52    | .625 Dia. | .076        | 7.542   | 1  | .001     | 5.083   | 1  | 80799940.19 .104 .104  | H1-1b |
| 2  | M49    | .625 Dia. | .070        | 7.542   | 1  | .001     | 5.083   | 1  | 8079 9940.19 .104 .104 | H1-1b |
| 3  | M53    | .625 Dia. | .062        | 7.542   | 1  | .000     | 5.083   | 1  | 8079 9940.19 .104 .104 | H1-1b |
| 4  | M25    | .625 Dia. | .008        | 7.542   | 1  | .000     | 5.083   | 1  | 8079 9940.19 .104 .104 | H1-1b |
| 5  | M26    | .625 Dia. | .005        | 7.542   | 1  | .000     | 5.083   | 1  | 8079 9940.19 .104 .104 | H1-1b |
| 6  | M22    | .625 Dia. | .003        | 7.542   | 1  | .000     | 5.083   | 1  | 8079 9940.19 .104 .104 | H1-1b |
| 7  | M27    | .625 Dia. | .002        | 7.542   | 1  | .000     | 5.083   | 1  | 8079 9940.19 .104 .104 | H1-1b |
| 8  | M23    | .625 Dia. | .002        | 7.542   | 1  | .000     | 5.083   | 1  | 8079 9940.19 .104 .104 | H1-1b |
| 9  | M51    | .625 Dia. | .002        | 7.542   | 1  | .001     | 0       | 1  | 8079 9940.19 .104 .104 | H1-1b |
| 10 | M54    | .625 Dia. | .002        | 7.542   | 1  | .000     | 5.083   | 1  | 8079 9940.19 .104 .104 | H1-1b |
| 11 | M50    | .625 Dia. | .002        | 7.542   | 1  | .001     | 5.083   | 1  | 8079 9940.19 .104 .104 | H1-1b |

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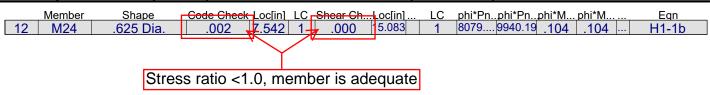
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: CTL02638

Collar Mount Analysis

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#### Envelope AISC 15th(360-16): LRFD Steel Code Checks (Continued)





#### ANTENNA MOUNT MAPPING CHECKLIST

| Mount Detail  |           |
|---|-----------|
| Mount Type  | Platform  |
| Mount Model Number                                  |           |
| If RT, then how is it attached                      |           |
| If WT, then how is it attached                      |           |
|   |           |
| Mount Mapping Detail                                |           |
|   |           |
| Material condition (discoloration, cracks, pitting) | Good      |
| Mfg. drawing, cutsheet, spec. available?            | No        |
| Date of mount mapping (if one exists)               | 4/11/2022 |
| Searched prior OOM for material?                    |           |
| Photos of installation available?                   |           |
| Original tower drawings show mounts?                |           |
| Searched for previous mapping?                      |           |
| Is latest mod design (dwgs) available?              |           |
| Is the latest structural analysis available?        |           |

| Project Detail                           |  |
|--|--|
| Market                                   | CONNECTICUT  |
| PACE Project ID                          | MRCTB054248/MRCTB055469/MRCTB056066<br>MRCTB055837/MRCTB056148 |
| Site Name                                | Stratford Oronoque Road  |
| City, State                              | Stratford, CT  |
| RFDS Version Number                      | 2  |
| Initiative (list mult., if applicable)   | 5G NR CBAN + DoD + 5C Add +5G NR 1DR-1                         |
| Tower Owner                              |  |
| SA Vendor                                |  |
| A&E firm (for structural analysis)       |  |
| A&E firm (for mapping, if different)     |  |
| Last amendment date or last site visit   |  |
| Is a site audit required on this project |  |

| Site Information    |          |
|---------------------|----------|
| Original Lease Date |          |
|                     |          |
|                     |          |
| FA Code             | 10152336 |
| Tower Type          | Monopole |
| Tower Height (Ft)   | 150      |
| AT&T Rad Center # 1 | 121      |
| AT&T Rad Center # 2 |          |
|                     |          |

| Measurements and Deliverables on sketches |  |
|---|--|
| Pipe / Angle dimenions and lengths        |  |
| bolt diameters and lengths                |  |
| U-Bolt diameters and lengths              |  |
| Steel Grade if indicated                  |  |
| welds :length and sizes                   |  |
| appurtenance relative locations           |  |
| Grounding Condition                       |  |

| <b>Equipment Detail</b>       | Model                      | Height  | Approz Az     | mount location |
|-------------------------------|----------------------------|---------|---------------|----------------|
| Antennas                      | CCI TPA65R-BU8DA-K         | 121'-0" | 30°/150°/270° | A2/B2/C2       |
| Antennas                      | Ericsson AIR 6449 B77D     | 121'-0" | 30°/150°/270° | A3/B3/C3       |
| Antennas                      | Ericsson AIR 6419 B77G     | 121'-0" | 30°/150°/270° | A3/B3/C3       |
| Antennas                      | Kathrein 800-10966         | 121'-0" | 30°/150°/270° | A4/B4/C4       |
| RRU                           | Ericsson RRUS-4478 B14     | 121'-0" | N/A           | A2/B2/C2       |
| RRU                           | Ericsson RRUS-8843 B2/B66A | 121'-0" | N/A           | A2/B2/C2       |
| RRU                           | Ericsson RRUS-4449 B5/B12  | 121'-0" | N/A           | A4/B4/C4       |
| RRU                           | Ericsson RRUS-32 B30       | 121'-0" | N/A           | A4/B4/C4       |
| TMA                           |                            |         |               |                |
| Coax                          |                            |         |               |                |
| RET (not imbedded in antenna) |                            |         |               |                |
| DC Cable                      |                            |         |               |                |
| Fiber Cable                   |                            |         |               |                |
| Squid                         | Raycap DC6-48-60-18-8F     | 121'-0" | N/A           | Standoff       |

| Co |  |  |
|----|--|--|
|    |  |  |
|    |  |  |

# STRUCTURAL ANALYSIS REPORT

STRUCTURE: MONOPOLE

PREPARED FOR: SMARTLINK

**CARRIER: AT&T** 

SITE NUMBER: CTL02638

FA NUMBER: 10152336

SITE LOCATION: 200 Oronoque Lane Stratford, CT 06614 N41.2514110, W73.1171510

DATE: May 2, 2022

#### **RESULTS**

PASS (MAX STRESS RATIO: 44.3%)

Barbara T. Kotecki, P.E.

Fullerton Engineering, P.C. 1100 E. Woodfield Road, Suite 500 Schaumburg, IL 60173 Tel: 847.908.8400 www.fullertonengineering.com

Project Number: 2021.0215.0011



# Summary

A structural analysis was performed by Fullerton, as requested by the client, to determine the adequacy of the existing structure with the proposed appurtenance and equipment addition on the abovementioned structure. The analysis considers the tower properties, existing and proposed appurtenances, and the required loading criteria.

#### Conclusion

| Component                  | % Capacity | Pass / Fail |
|----------------------------|------------|-------------|
| Tower                      | 44.3%      | PASS        |
| Anchor Rods/Base Plate     | 42.8%      | PASS        |
| Foundation                 | 41.0%      | PASS        |
| Structural Rating (max fro | PASS       |             |

### Analysis Criteria

Reference Standard: TIA-222-H Standard

Wind Parameters: Basic Wind Speed: 119 mph (3-Sec gust)

Ice Wind Speed: 50 mph (3-Sec gust)

Design Ice Thickness: 1.00 in.

Risk Category II
Exposure Category: B

Topographic Category: 1

#### Sources

The following documents for the existing structure were made available for our structural analysis.

| Reference Document                     | Date       |
|--|------------|
| Structural Analysis Report by Infinigy | 04/07/2019 |
| RFDS by AT&T Version 2.00              | 03/07/2022 |
| Site Visit Photos                      | 02/09/2022 |

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# Final Proposed Appurtenance Loading Schedule

| ANTENNA/EQUIPMENT |      |  |                |      | COAXIAL          |  |  |
|-------------------|------|--|----------------|------|------------------|--|--|
| Elev.<br>(Ft)     | QTY. | MANUFACTURER/MODEL                                 | MOUNT<br>TYPE  | QTY. | SIZE/TYPE.       |  |  |
|                   | 3    | (N) CCIAntennas TPA65R-BU6DA-K                     |                | 6    | (E) DC Cables    |  |  |
|                   | 3    | (N) Ericsson AIR 6449 B77D + AIR 6419 B77G Stacked |                | 3    | (E) Fiber Cables |  |  |
|                   | 3    | (N) CCIAntennas DMP65R-BU8DA                       | l a.v.         | 3    | (E) RET Cables   |  |  |
| 121.0             | 3    | (N) Ericsson Radio 4478 B14                        | Low<br>Profile |      |                  |  |  |
| 121.0             | 3    | (N) Ericsson Radio 8843 B2/B66A                    | Platform       |      |                  |  |  |
|                   | 3    | (E) Ericsson Radio 4449 B5/B12                     | Platioiiii     |      |                  |  |  |
|                   | 3    | (E) Ericsson RRUS-32 B30                           |                |      |                  |  |  |
|                   | 3    | (E) Raycap DC6-48-60-18-8F                         |                | ·    |                  |  |  |

<sup>(</sup>E) denotes existing loading

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SITE NUMBER : CTL02638 Project Number: 2021.0215.0011

DATE: MAY 2, 2022: Page 3 of 35

<sup>(</sup>N) denotes proposed loading

# Results

#### Tower

| Section No. | Elevation<br>ft | Component<br>Type | Size                   | Critical<br>Element | P<br>lb   | øP <sub>allow</sub><br>lb | % Capacity | Pass<br>Fail |
|-------------|-----------------|-------------------|------------------------|---------------------|-----------|---------------------------|------------|--------------|
| L1          | 150 - 97.25     | Pole              | TP31.76x20x0.25        | 1                   | -8410.51  | 1416120.00                | 30.3       | Pass         |
| L2          | 97.25 - 48.25   | Pole              | TP42.19x30.2568x0.3125 | 2                   | -16486.60 | 2352270.00                | 43.0       | Pass         |
| L3          | 48.25 - 1       | Pole              | TP52.1x40.2267x0.375   | 3                   | -30427.40 | 3601590.00                | 44.3       | Pass         |
|             |                 |                   |                        |                     |           |                           | Summary    |              |
|             |                 |                   |                        |                     |           | Pole (L3)                 | 44.3       | Pass         |
|             |                 |                   |                        |                     |           | Base Plate                | 42.8       | Pass         |
|             |                 |                   |                        |                     |           | RATING =                  | 44.3       | Pass         |

#### Foundation

| Components             | %Capacity | PASS/FAIL |
|------------------------|-----------|-----------|
| ANCHOR RODS/BASE PLATE | 42.8%     | PASS      |
| FOUNDATION             | 41.0%     | PASS      |

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SITE NUMBER : CTL02638

DATE: MAY 2, 2022

# Assumptions

This analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. The analysis is based solely on the information supplied, and the results, in turn, are only as accurate as data extracted from this information. Fullerton has been instructed by the client to assume the information supplied is accurate, and Fullerton has made no independent determination of its accuracy. The exception to the previous statement is if Fullerton has been contracted by the client to provide an independent structural mapping report of the tower and related appurtenances, in which case Fullerton has made an independent determination of the accuracy of the information resulting from the mapping report.

- The tower member sizes and geometry are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and stated in the materials section.
- The existing tower is assumed to have been properly maintained in accordance with the TIA/EIA standard and/or its original manufacturer's recommendations. The existing tower is assumed to be in good condition with no structural defects and with no deterioration to its member capacities.
- The antenna configuration is as supplied and/or stated in the analysis section. It is assumed to be complete and accurate. All antennas, mounts, remote radios, cables, and cable supports are assumed to be properly installed and supported as per the manufacturer's requirements.
- The antennas, mounts, remote radios, cables, and cable supports, and lines stated in the appurtenance loading schedule represent Fullerton's understanding of the overall antenna configuration. If the actual configuration is different than above, then this analysis is invalid. Please refer to this report for the projected wind areas used in the calculations for antennas and mounts. If variations or discrepancies are identified, please inform Fullerton.
- Some assumptions are made regarding antenna and mount sizes and their projected areas based on a best interpretation of the data supplied and a best knowledge of antenna type and industry practice.
- The existing foundation is assumed to be in good condition with no structural defects and with no deterioration to its member capacities.
- The soil parameters are as per data supplied, or as assumed, and stated in the calculations.
- All welds and connections are assumed to develop at least the member capacity, unless determined otherwise and explicitly stated in this report.
- All prior structural modifications, if any, are assumed to be as per date supplied/ available, to be properly installed and to be fully effective.

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## Scope and Limitations

The engineering services rendered by Fullerton Engineering, P.C. (Fullerton) in connection with this structural analysis are limited to an analysis of the structure, size, and capacity of its members. Fullerton does not analyze the fabrication, including welding and connection capacities, except as included in this report.

The information and conclusions contained in this report were determined by application of the current engineering standards and analysis procedures and formulae, and Fullerton assumes no obligation to revise any of the information or conclusions contained in this report in the event such engineering and analysis procedures and formulae are hereafter modified or revised.

Fullerton makes no warranties, expressed, or implied in connection with this report and disclaims any liability arising from original design, material, fabrication, and erection deficiencies or the "as-built" condition of this tower.

Installation procedures are not within the scope of this report and should be performed and evaluated by a competent tower erection contractor.

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SITE NUMBER : CTL02638

DATE: MAY 2, 2022

Project Number: 2021.0215.0011 Page 6 of 35

# **Structural Calculations**

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SITE NUMBER : CTL02638

DATE: MAY 2, 2022

#### **Tower Analysis Summary Form**

General Info

| Site Name                     | STRATFORD ORONOQUE ROAD     |
|-------------------------------|-----------------------------|
| Site Number                   | CTL02638                    |
| FA Number                     | 10152336                    |
| Date of Analysis              | 5/2/2022                    |
| Company Performing Evaluation | Fullerton Engineering, P.C. |

The information contained in this summary report is not to be used independently from the PE stamped tower analysis.

Design Parameters

| Design Code Used                      | 2015 IBC            |
|---------------------------------------|---------------------|
|                                       | TIA-222-H           |
| Location of Tower (County, State)     | Fairfield, CT       |
| Basic Wind Speed (mph)                | 119 (3-second gust) |
| Ice Thickness (in)                    | 1                   |
| Structure Classification (I, II, III) | II                  |
| Exposure Category (B, C, D)           | В                   |
| Topographic Category (1 to 5)         | 1                   |
|                                       |                     |

Analysis Results (% Maximum Usage)

| Existing/Reserved + Proposed | l Condition |  |
|------------------------------|-------------|--|
| Tower (%)                    | 44.3%       |  |
| Anchor Rods (%)              | 42.8%       |  |
| Base Plate (%)               | 42.0 /0     |  |
| Foundation (%)               | 41.0%       |  |
| Foundation Adequate?         | Yes         |  |

Steel Yield Strength (ksi)

| Pole         | 65 |
|--------------|----|
| Anchor Bolts | 81 |
| Base Plate   | 50 |

Note: Material grade assumed based on preferred material specifications.

Existing / Reserved Loading

| Antenna                          |                      |                    |          |          |              |                 |         | Mount    |              | Transmission Line     |          |        |        |  |
|----------------------------------|----------------------|--------------------|----------|----------|--------------|-----------------|---------|----------|--------------|-----------------------|----------|--------|--------|--|
| Antenna Owner                    | Mount<br>Height (ft) | Antenna CL<br>(ft) | Quantity | Туре     | Manufacturer | Model           | Azimuth | Quantity | Manufacturer | Туре                  | Quantity | Model  | Size   | Attachment<br>Internal/External                  |
| AT&T                             | 121                  | 121                | 3        | RRH      | Ericsson     | 4449 B5/B12     |         | 1        | N/A          | Platform w/ Handrails | 6        | DC     | 3/4"   | Internal   |
| AT&T                             | 121                  | 121                | 3        | RRH      |              | RRUS-32 B30     |         |          |              | Platform w/ Handrails | 3        |        |        | Internal   |
| AT&T                             | 121                  | 121                | 3        | Squid    | Raycap       | DC6-48-60-18-8F |         |          |              | Platform w/ Handrails | 3        | RET    | 7/16"  | Internal   |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        |  |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        |  |
| Unknown                          | 149                  | 159                | 2        | Omni     | N/A          | N/A             |         | 2        | N/A          | Standoff Mount        | 3        | Hybrid | 1-5/8" | Internal   |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        |  |
| Unknown                          | 149                  | 153                | 2        | Omni     | N/A          | N/A             |         | 2        | N/A          | Standoff Mount        | 3        | Hybrid | 1-5/8" | Internal   |
|                                  |                      |                    |          |          | ļ            |                 |         |          |              |                       |          |        |        |  |
| Unknown                          | 133                  | 138                | 2        | Omni     | N/A          | N/A             |         | 2        | N/A          | Standoff Mount        |          |        |        |  |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        |  |
| Unknown                          | 133                  | 137                | 2        | Omni     | N/A          | N/A             |         | 2        | N/A          | Standoff Mount        |          |        |        |  |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        |  |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        | 4  |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        |  |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        |  |
|                                  |                      |                    |          |          | -            |                 |         |          |              |                       |          |        |        |  |
|                                  |                      |                    |          |          | 4            |                 |         |          |              |                       |          |        |        |  |
|                                  |                      |                    |          |          | 1            |                 |         |          |              |                       |          |        |        |  |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        |  |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       |          |        |        |  |
|                                  |                      |                    |          |          |              |                 |         |          |              |                       | -        |        |        |  |
|                                  | -                    |                    |          |          |              |                 |         |          |              |                       | 1        |        |        | -  |
|                                  | -                    |                    |          |          |              |                 |         |          |              |                       | 1        |        |        | -  |
|                                  | -                    | -                  |          | <b>+</b> |              |                 |         |          | -            |                       | 1        |        | -      | <del>                                     </del> |
| Note: The existing loading shall |                      | . P.C              |          | L        | <u> </u>     |                 |         |          | 1            | l                     | <u> </u> | l .    | 1      |  |

Note: The existing loading shall be re-used, in addition to the proposed loading.

Proposed Loading

|               | Antenna              |                    |          |         |              |                |            |          | Mount        |      | Trans    | mission Line |      |                                 |
|---------------|----------------------|--------------------|----------|---------|--------------|----------------|------------|----------|--------------|------|----------|--------------|------|---------------------------------|
| Antenna Owner | Mount<br>Height (ft) | Antenna CL<br>(ft) | Quantity | Туре    | Manufacturer | Model          | Azimuth    | Quantity | Manufacturer | Туре | Quantity | Model        | Size | Attachment<br>Internal/External |
| AT&T          | 121                  | 121                | 3        | Antenna | CCI          | TPA65R-BU6DA-K | 30/150/270 |          |              |      |          |              |      |                                 |
| AT&T          | 121                  | 121                | 3        | Antenna | Ericsson     | AIR 6449 B77D  | 30/150/270 |          |              |      |          |              |      |                                 |
| AT&T          | 121                  | 121                | 3        | Antenna | Ericsson     | AIR 6419 B77G  | 30/150/270 |          |              |      |          |              |      |                                 |
| AT&T          | 121                  | 121                | 3        | RRH     | Ericsson     | 4478 B14       |            |          |              |      |          |              |      |                                 |
| AT&T          | 121                  | 121                | 3        | RRH     | Ericsson     | 8843 B2/B66A   |            |          |              |      |          |              |      |                                 |
|               |                      |                    |          |         |              |                |            |          |              |      |          |              |      |                                 |

Note: The proposed equipment shall be installed in addition to the existing/reserved loading at the same elevation.

Future Loading

| ruture Loading | v                    |                    |          |      |              |       |                   |          |              |      |          |       |      |                                 |
|----------------|----------------------|--------------------|----------|------|--------------|-------|-------------------|----------|--------------|------|----------|-------|------|---------------------------------|
| Antenna        |                      |                    |          |      | Mount        |       | Transmission Line |          |              |      |          |       |      |                                 |
| Antenna Owner  | Mount<br>Height (ft) | Antenna CL<br>(ft) | Quantity | Туре | Manufacturer | Model | Azimuth           | Quantity | Manufacturer | Туре | Quantity | Model | Size | Attachment<br>Internal/External |
|                |                      |                    |          |      |              |       |                   | 1        |              |      |          |       |      | 1                               |

# 150.0 ft 0.2500 52.75 4.50 18 97.3 ft 53.50 A572-65 48 48.3 ft ALL REACTIONS ARE FACTORED AXIAL 42804 lb SHEAR MOMENT 52.1000 5524 lb 528248 lb-ft 9 TORQUE 801 lb-ft 50 mph WIND - 1.0000 in ICE AXIAL 30438 lb SHEAR 19266 lb 1.0 ft 20010.2 TORQUE 2887 lb-ft REACTIONS - 119 mph WIND Thickness (in) Socket Length Top Dia (in) Bot Dia (in) Weight (Ib) Length (ft)

#### **DESIGNED APPURTENANCE LOADING**

| TYPE                   | ELEVATION | TYPE                        | ELEVATION |
|------------------------|-----------|-----------------------------|-----------|
| 20' Omni               | 149       | Raycap DC6-48-60-18-8F      | 122       |
| 20' Omni               | 149       | Raycap DC6-48-60-18-8F      | 122       |
| 8' DiPole              | 149       | 12-ft Platform w/ Handrails | 122       |
| 8' DiPole              | 149       | CCI TPA65R-BU6D             | 122       |
| 4' Standoff            | 149       | CCI TPA65R-BU6D             | 122       |
| 4' Standoff            | 149       | CCI TPA65R-BU6D             | 122       |
| 4' Standoff            | 149       | Ericsson Air6449 B77D       | 122       |
| 4' Standoff            | 149       | Ericsson Air6449 B77D       | 122       |
| 6' Dish w/ Shroud (HP) | 141       | Ericsson Air6449 B77D       | 122       |
| 10' Omni               | 133       | Ericsson Air6419 B77G       | 122       |
| 8' DiPole              | 133       | Ericsson Air6419 B77G       | 122       |
| 8' DiPole              | 133       | Ericsson Air6419 B77G       | 122       |
| 4' Standoff            | 133       | CCI DMP65R-BU8DA-K          | 122       |
| 4' Standoff            | 133       | CCI DMP65R-BU8DA-K          | 122       |
| 4' Standoff            | 133       | CCI DMP65R-BU8DA-K          | 122       |
| 4' Standoff            | 133       | Ericsson RRUS 4478 B14      | 122       |
| 10' Omni               | 133       | Ericsson RRUS 4478 B14      | 122       |
| RRUS-4449 B5/B12       | 122       | Ericsson RRUS 4478 B14      | 122       |
| RRUS-4449 B5/B12       | 122       | RRUS-8843 B2/B66A           | 122       |
| RRUS-32 B30            | 122       | RRUS-8843 B2/B66A           | 122       |
| RRUS-32 B30            | 122       | RRUS-8843 B2/B66A           | 122       |
| RRUS-32 B30            | 122       | RRUS-4449 B5/B12            | 122       |
| Raycap DC6-48-60-18-8F | 122       |                             | '         |

#### **MATERIAL STRENGTH**

| GRADE   | Fy     | Fy Fu  |  | Fy | Fu |
|---------|--------|--------|--|----|----|
| Δ572-65 | 65 kei | 80 kei |  |    |    |

#### **TOWER DESIGN NOTES**

- 1. Tower is located in Fairfield County, Connecticut.

- Tower designed for Exposure B to the TIA-222-H Standard.
   Tower designed for a 119 mph basic wind in accordance with the TIA-222-H Standard.
   Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
- 5. Deflections are based upon a 60 mph wind.
- Tower Risk Category II.
- 7. Topographic Category 1 with Crest Height of 0.00 ft
- 8. TOWER RATING: 44.3%

MOMENT 1886067 lb-ft

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| b: CTL02638           |                  |             |
|-----------------------|------------------|-------------|
| roject:               |                  |             |
| lient: Smartlink/AT&T | Drawn by: LA     | App'd:      |
| ode: TIA-222-H        | Page 9: 05852/22 | Scale: NTS  |
| ath:                  |                  | Dwg No.   1 |

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| Job     |                | Page              |
|---------|----------------|-------------------|
|         | CTL02638       | 1 of 20           |
| Project |                | Date              |
|         |                | 12:41:35 05/02/22 |
| Client  | 0 41 1 (4707   | Designed by       |
|         | Smartlink/AT&T | LA                |

# **Tower Input Data**

The tower is a monopole.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower is located in Fairfield County, Connecticut.

Tower base elevation above sea level: 259.00 ft.

Basic wind speed of 119 mph.

Risk Category II.

Exposure Category B.

Simplified Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Category: 1. Crest Height: 0.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

# **Options**

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- √ Use Code Stress Ratios
- √ Use Code Safety Factors Guys Escalate Ice

Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric

- Distribute Leg Loads As Uniform Assume Legs Pinned Assume Rigid Index Plate
- √ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
- √ Bypass Mast Stability Checks
- √ Use Azimuth Dish Coefficients
- √ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination
- √ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing
- √ Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs
- Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation
- ✓ Consider Feed Line Torque
   Include Angle Block Shear Check
   Use TIA-222-H Bracing Resist. Exemption
   Use TIA-222-H Tension Splice Exemption
   Poles
- ✓ Include Shear-Torsion Interaction
   Always Use Sub-Critical Flow
   Use Top Mounted Sockets
   Pole Without Linear Attachments
   Pole With Shroud Or No Appurtenances
   Outside and Inside Corner Radii Are
   Known

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| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 2 of 20                   |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Tapered Pole Section Geometr | У |
|------------------------------|---|
|------------------------------|---|

| Section | Elevation    | Section<br>Length | Splice<br>Length | Number<br>of | Top<br>Diameter | Bottom<br>Diameter | Wall<br>Thickness | Bend<br>Radius | Pole Grade          |
|---------|--------------|-------------------|------------------|--------------|-----------------|--------------------|-------------------|----------------|---------------------|
|         | ft           | ft                | ft               | Sides        | in              | in                 | in                | in             |                     |
| L1      | 150.00-97.25 | 52.75             | 4.50             | 18           | 20.0000         | 31.7600            | 0.2500            | 1.0000         | A572-65<br>(65 ksi) |
| L2      | 97.25-48.25  | 53.50             | 6.00             | 18           | 30.2568         | 42.1900            | 0.3125            | 1.2500         | À572-65<br>(65 ksi) |
| L3      | 48.25-1.00   | 53.25             |                  | 18           | 40.2267         | 52.1000            | 0.3750            | 1.5000         | A572-65<br>(65 ksi) |

# **Tapered Pole Properties**

| Section | Tip Dia. | Area    | I          | r       | С       | I/C      | J          | It/Q    | w      | w/t    |
|---------|----------|---------|------------|---------|---------|----------|------------|---------|--------|--------|
|         | in       | $in^2$  | $in^4$     | in      | in      | $in^3$   | $in^4$     | $in^2$  | in     |        |
| L1      | 20.2700  | 15.6716 | 772.2994   | 7.0112  | 10.1600 | 76.0137  | 1545.6150  | 7.8373  | 3.0800 | 12.32  |
|         | 32.2114  | 25.0032 | 3136.3866  | 11.1861 | 16.1341 | 194.3951 | 6276.9002  | 12.5040 | 5.1498 | 20.599 |
| L2      | 31.6945  | 29.7010 | 3364.6191  | 10.6302 | 15.3704 | 218.9019 | 6733.6654  | 14.8533 | 4.7752 | 15.281 |
|         | 42.7926  | 41.5372 | 9203.1529  | 14.8665 | 21.4325 | 429.4013 | 18418.4155 | 20.7726 | 6.8754 | 22.001 |
| L3      | 42.1479  | 47.4335 | 9517.3496  | 14.1474 | 20.4352 | 465.7340 | 19047.2224 | 23.7212 | 6.4199 | 17.12  |
|         | 52.8459  | 61.5657 | 20810.2424 | 18.3624 | 26.4668 | 786.2772 | 41647.8674 | 30.7887 | 8.5096 | 22.692 |

| Tower          | Gusset          | Gusset    | Gusset Grade | Adjust. Factor | Adjust. | Weight Mult. | Double Angle | Double Angle | Double Angle |
|----------------|-----------------|-----------|--------------|----------------|---------|--------------|--------------|--------------|--------------|
| Elevation      | Area            | Thickness |              | $A_f$          | Factor  |              | Stitch Bolt  | Stitch Bolt  | Stitch Bolt  |
|                | (per face)      |           |              |                | $A_r$   |              | Spacing      | Spacing      | Spacing      |
|                |                 |           |              |                |         |              | Diagonals    | Horizontals  | Redundants   |
| ft             | ft <sup>2</sup> | in        |              |                |         |              | in           | in           | in           |
| L1             |                 |           |              | 1              | 1       | 1            |              |              |              |
| 150.00-97.25   |                 |           |              |                |         |              |              |              |              |
| L2 97.25-48.25 |                 |           |              | 1              | 1       | 1            |              |              |              |
| L3 48.25-1.00  |                 |           |              | 1              | 1       | 1            |              |              |              |

# **Monopole Base Plate Data**

| Base Plate D          | ata         |
|-----------------------|-------------|
| Base plate is square  |             |
| Base plate is grouted |             |
| Anchor bolt grade     | A325X       |
| Anchor bolt size      | 2.2500 in   |
| Number of bolts       | 14          |
| Embedment length      | 84.0000 in  |
| f'c                   | 3 ksi       |
| Grout space           | 2.0000 in   |
| Base plate grade      | A572-50     |
| Base plate thickness  | 2.5000 in   |
| Bolt circle diameter  | 58.5000 in  |
| Outer diameter        | 64.5000 in  |
| Inner diameter        | 50.5000 in  |
| Base plate type       | Plain Plate |

#### Page Job *tnxTower* 3 of 20 CTL02638 **Project** Date Fullerton Engineering, P.C. 1100 E. Woodfield Road, Suite 500 12:41:35 05/02/22 Client Designed by Smartlink/AT&T

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| Description    | Sector | Exclude<br>From       | Component<br>Type    | Placement        | Total<br>Number | Number<br>Per Row | Start/End<br>Position |        | Perimeter | Weight |
|----------------|--------|-----------------------|----------------------|------------------|-----------------|-------------------|-----------------------|--------|-----------|--------|
|                |        | Torque<br>Calculation |                      | ft               |                 |                   |                       | in     | in        | plf    |
| Step Rungs 3/4 | С      | No                    | Surface Ar<br>(CaAa) | 150.00 -<br>1.00 | 1               | 1                 | 0.000                 | 0.7500 |           | 0.48   |

# Feed Line/Linear Appurtenances - Entered As Area

| Description         | Face<br>or | Allow<br>Shield | Exclude<br>From       | Component<br>Type     | Placement     | Total<br>Number |                              | $C_A A_A$                    | Weight               |
|---------------------|------------|-----------------|-----------------------|-----------------------|---------------|-----------------|------------------------------|------------------------------|----------------------|
|                     | Leg        |                 | Torque<br>Calculation | - 7 F                 | ft            |                 |                              | ft²/ft                       | plf                  |
| Safety Line 3/8     | С          | No              | No                    | CaAa (Out<br>Of Face) | 150.00 - 1.00 | 1               | No Ice<br>1/2" Ice<br>1" Ice | 0.04<br>0.14<br>0.24         | 0.22<br>0.75<br>1.28 |
| 1-5/8" Hybrid       | С          | No              | No                    | Inside Pole           | 150.00 - 2.00 | 6               | No Ice<br>1/2" Ice<br>1" Ice | 0.00<br>0.00<br>0.00         | 1.20<br>1.20<br>1.20 |
| 3/4" DC power cable | С          | No              | No                    | Inside Pole           | 122.00 - 2.00 | 6               | No Ice<br>1/2" Ice<br>1" Ice | 0.00<br>0.00<br>0.00         | 0.40<br>0.40<br>0.40 |
| 1/2" Fiber          | С          | No              | No                    | Inside Pole           | 122.00 - 2.00 | 3               | No Ice<br>1/2" Ice<br>1" Ice | 0.00<br>0.00<br>0.00         | 0.15<br>0.15<br>0.15 |
| RET Cable           | С          | No              | No                    | Inside Pole           | 122.00 - 2.00 | 3               | No Ice<br>1/2" Ice<br>1" Ice | 0.00<br>0.00<br>0.00<br>0.00 | 0.25<br>0.25<br>0.25 |

# Feed Line/Linear Appurtenances Section Areas

| Tower   | Tower        | Face | $A_R$           | $A_F$           | $C_AA_A$        | $C_A A_A$       | Weight |
|---------|--------------|------|-----------------|-----------------|-----------------|-----------------|--------|
| Section | Elevation    |      | a 2             | a 2             | In Face         | Out Face        |        |
|         | ft           |      | ft <sup>2</sup> | ft <sup>2</sup> | ft <sup>2</sup> | ft <sup>2</sup> | lb     |
| L1      | 150.00-97.25 | A    | 0.000           | 0.000           | 0.000           | 0.000           | 0.00   |
|         |              | В    | 0.000           | 0.000           | 0.000           | 0.000           | 0.00   |
|         |              | C    | 0.000           | 0.000           | 3.956           | 1.978           | 505.82 |
| L2      | 97.25-48.25  | A    | 0.000           | 0.000           | 0.000           | 0.000           | 0.00   |
|         |              | В    | 0.000           | 0.000           | 0.000           | 0.000           | 0.00   |
|         |              | C    | 0.000           | 0.000           | 3.675           | 1.838           | 563.50 |
| L3      | 48.25-1.00   | A    | 0.000           | 0.000           | 0.000           | 0.000           | 0.00   |
|         |              | В    | 0.000           | 0.000           | 0.000           | 0.000           | 0.00   |
|         |              | C    | 0.000           | 0.000           | 3.544           | 1.772           | 532.58 |

LA

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| Job            | Page              |
|----------------|-------------------|
| CTL02638       | 4 of 20           |
| Project        | Date              |
|                | 12:41:35 05/02/22 |
| Client         | Designed by       |
| Smartlink/AT&T | LA                |

# Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower<br>Section | Tower<br>Elevation | Face      | Ice<br>Thickness | $A_R$  | $A_F$  | C <sub>A</sub> A <sub>A</sub><br>In Face | C <sub>A</sub> A <sub>A</sub><br>Out Face | Weight |
|------------------|--------------------|-----------|------------------|--------|--------|--|---|--------|
| Section          | Elevation<br>ft    | or<br>Leg | in               | $ft^2$ | $ft^2$ | ft <sup>2</sup>                          | Oui Face<br>ft²                           | lb     |
| L1               | 150.00-97.25       | A         | 1.140            | 0.000  | 0.000  | 0.000                                    | 0.000                                     | 0.00   |
|                  |                    | В         |                  | 0.000  | 0.000  | 0.000                                    | 0.000                                     | 0.00   |
|                  |                    | C         |                  | 0.000  | 0.000  | 15.980                                   | 14.002                                    | 708.35 |
| L2               | 97.25-48.25        | A         | 1.081            | 0.000  | 0.000  | 0.000                                    | 0.000                                     | 0.00   |
|                  |                    | В         |                  | 0.000  | 0.000  | 0.000                                    | 0.000                                     | 0.00   |
|                  |                    | C         |                  | 0.000  | 0.000  | 14.844                                   | 13.007                                    | 751.63 |
| L3               | 48.25-1.00         | A         | 0.969            | 0.000  | 0.000  | 0.000                                    | 0.000                                     | 0.00   |
|                  |                    | В         |                  | 0.000  | 0.000  | 0.000                                    | 0.000                                     | 0.00   |
|                  |                    | C         |                  | 0.000  | 0.000  | 13.762                                   | 11.991                                    | 701.05 |

# **Feed Line Center of Pressure**

| Section | Elevation    | $CP_X$  | $CP_Z$ | $CP_X$  | $CP_Z$ |
|---------|--------------|---------|--------|---------|--------|
|         |              |         |        | Ice     | Ice    |
|         | ft           | in      | in     | in      | in     |
| L1      | 150.00-97.25 | -0.2459 | 0.7264 | -0.8697 | 1.6814 |
| L2      | 97.25-48.25  | -0.2508 | 0.7357 | -0.9362 | 1.7994 |
| L3      | 48.25-1.00   | -0.2533 | 0.7407 | -0.9376 | 1.8039 |

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

# **Shielding Factor Ka**

| T  | Tower  | Feed Line  | Description    | Feed Line      | $K_a$  | $K_a$  |
|----|--------|------------|----------------|----------------|--------|--------|
| Se | ection | Record No. |                | Segment Elev.  | No Ice | Ice    |
|    | L1     | 2          | Step Rungs 3/4 | 97.25 - 150.00 | 1.0000 | 1.0000 |
|    | L2     | 2          | Step Rungs 3/4 | 48.25 - 97.25  | 1.0000 | 1.0000 |
|    | L3     | 2          | Step Rungs 3/4 | 1.00 - 48.25   | 1.0000 | 1.0000 |

# **Discrete Tower Loads**

| Description | Face<br>or<br>Leg | Offset<br>Type | Offsets:<br>Horz<br>Lateral<br>Vert | Azimuth<br>Adjustment | Placement |                    | $C_A A_A$<br>Front | C <sub>A</sub> A <sub>A</sub><br>Side | Weight         |
|-------------|-------------------|----------------|-------------------------------------|-----------------------|-----------|--------------------|--------------------|---------------------------------------|----------------|
|             |                   |                | ft<br>ft<br>ft                      | 0                     | ft        |                    | ft²                | ft <sup>2</sup>                       | lb             |
| 20' Omni    | A                 | From Face      | 4.00<br>0.00                        | 90.0000               | 149.00    | No Ice<br>1/2" Ice | 4.00<br>6.03       | 4.00<br>6.03                          | 40.00<br>70.77 |

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| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 5 of 20                   |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Description         | Face<br>or | Offset<br>Type | Offsets:<br>Horz | Azimuth<br>Adjustment | Placement |                  | $C_AA_A$<br>Front | $C_AA_A$<br>Side | Weigi         |
|---------------------|------------|----------------|------------------|-----------------------|-----------|------------------|-------------------|------------------|---------------|
|                     | Leg        |                | Lateral          |                       |           |                  |                   |                  |               |
|                     |            |                | Vert             | 0                     |           |                  | 0.2               | a 2              |               |
|                     |            |                | ft<br>ft         | Ŭ                     | ft        |                  | ft <sup>2</sup>   | $ft^2$           | lb            |
|                     |            |                | ft               |                       |           |                  |                   |                  |               |
|                     |            |                | 10.00            |                       |           | 1" Ice           | 8.07              | 8.07             | 114.1         |
| 20' Omni            | C          | From Face      | 4.00             | 30.0000               | 149.00    | No Ice           | 4.00              | 4.00             | 40.00         |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 6.03              | 6.03             | 70.7          |
| O' DiDala           | D          | Енон Есс       | 10.00            | 00,0000               | 149.00    | 1" Ice<br>No Ice | 8.07              | 8.07             | 114.1         |
| 8' DiPole           | В          | From Face      | 4.00<br>0.00     | 90.0000               | 149.00    | 1/2" Ice         | 1.60<br>2.42      | 1.60<br>2.42     | 20.0<br>32.4  |
|                     |            |                | 4.00             |                       |           | 1" Ice           | 3.24              | 3.24             | 50.1          |
| 8' DiPole           | В          | From Face      | 4.00             | -90.0000              | 149.00    | No Ice           | 1.60              | 1.60             | 20.0          |
| o Bir oic           | ь          | r rom r acc    | 0.00             | 70.0000               | 117.00    | 1/2" Ice         | 2.42              | 2.42             | 32.4          |
|                     |            |                | 4.00             |                       |           | 1" Ice           | 3.24              | 3.24             | 50.1          |
| 10' Omni            | A          | From Face      | 4.00             | 90.0000               | 133.00    | No Ice           | 3.19              | 3.19             | 53.2          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 4.52              | 4.52             | 82.0          |
|                     |            |                | 5.00             |                       |           | 1" Ice           | 5.87              | 5.87             | 118.7         |
| 10' Omni            | C          | From Face      | 4.00             | 30.0000               | 133.00    | No Ice           | 3.19              | 3.19             | 53.2          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 4.52              | 4.52             | 82.0          |
|                     |            |                | 5.00             |                       |           | 1" Ice           | 5.87              | 5.87             | 118.7         |
| 8' DiPole           | В          | From Face      | 4.00             | 90.0000               | 133.00    | No Ice           | 1.60              | 1.60             | 20.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 2.42              | 2.42             | 32.4          |
|                     |            |                | 4.00             |                       |           | 1" Ice           | 3.24              | 3.24             | 50.1          |
| 8' DiPole           | В          | From Face      | 4.00             | -90.0000              | 133.00    | No Ice           | 1.60              | 1.60             | 20.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 2.42              | 2.42             | 32.4          |
| 41.00. 1.00         |            | Б Б            | 4.00             | 0.0000                | 1.40.00   | 1" Ice           | 3.24              | 3.24             | 50.14         |
| 4' Standoff         | Α          | From Face      | 2.00             | 0.0000                | 149.00    | No Ice           | 3.41              | 3.41             | 80.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 4.47              | 4.47             | 104.0         |
| 4' Standoff         | В          | From Face      | 0.00<br>2.00     | 0.0000                | 140.00    | 1" Ice<br>No Ice | 5.53<br>3.41      | 5.53<br>3.41     | 128.0         |
| 4 Standon           | Б          | From Face      | 0.00             | 0.0000                | 149.00    | 1/2" Ice         | 4.47              | 4.47             | 80.0<br>104.0 |
|                     |            |                | 0.00             |                       |           | 1" Ice           | 5.53              | 5.53             | 128.0         |
| 4' Standoff         | C          | From Face      | 2.00             | 0.0000                | 149.00    | No Ice           | 3.41              | 3.41             | 80.0          |
| Dungon              | C          | r rom r acc    | 0.00             | 0.0000                | 117.00    | 1/2" Ice         | 4.47              | 4.47             | 104.0         |
|                     |            |                | 0.00             |                       |           | 1" Ice           | 5.53              | 5.53             | 128.0         |
| 4' Standoff         | C          | From Face      | 2.00             | 30.0000               | 149.00    | No Ice           | 3.41              | 3.41             | 80.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 4.47              | 4.47             | 104.0         |
|                     |            |                | 0.00             |                       |           | 1" Ice           | 5.53              | 5.53             | 128.0         |
| 4' Standoff         | A          | From Face      | 2.00             | 0.0000                | 133.00    | No Ice           | 3.41              | 3.41             | 80.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 4.47              | 4.47             | 104.0         |
|                     |            |                | 0.00             |                       |           | 1" Ice           | 5.53              | 5.53             | 128.0         |
| 4' Standoff         | В          | From Face      | 2.00             | 0.0000                | 133.00    | No Ice           | 3.41              | 3.41             | 80.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 4.47              | 4.47             | 104.0         |
| 41.00               |            |                | 0.00             | 0.0000                | 122.00    | 1" Ice           | 5.53              | 5.53             | 128.0         |
| 4' Standoff         | С          | From Face      | 2.00             | 0.0000                | 133.00    | No Ice           | 3.41              | 3.41             | 80.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 4.47              | 4.47             | 104.0         |
| A' Standoff         | С          | From Face      | 0.00             | 20,0000               | 133.00    | 1" Ice<br>No Ice | 5.53<br>3.41      | 5.53             | 128.0<br>80.0 |
| 4' Standoff         | C          | From Face      | 2.00<br>0.00     | 30.0000               | 155.00    | 1/2" Ice         | 3.41<br>4.47      | 3.41<br>4.47     | 104.0         |
|                     |            |                | 0.00             |                       |           | 1" Ice           | 5.53              | 5.53             | 128.0         |
| ***                 |            |                |                  |                       |           | -20              |                   |                  | -20.0         |
| RRUS-4449 B5/B12    | A          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice           | 1.64              | 1.30             | 73.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 1.80              | 1.45             | 90.1          |
|                     |            |                | 0.00             |                       |           | 1" Ice           | 1.97              | 1.60             | 110.0         |
| RRUS-4449 B5/B12    | В          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice           | 1.64              | 1.30             | 73.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 1.80              | 1.45             | 90.1          |
| PPT70 1116 = = = :: | _          |                | 0.00             | 0.0000                | 400.00    | 1" Ice           | 1.97              | 1.60             | 110.0         |
| RRUS-4449 B5/B12    | C          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice           | 1.64              | 1.30             | 73.0          |
|                     |            |                | 0.00             |                       |           | 1/2" Ice         | 1.80              | 1.45             | 90.19         |
| DD110 22 D20        | A          | Enom E         | 0.00             | 0.0000                | 122.00    | 1" Ice           | 1.97              | 1.60             | 110.0         |
| RRUS-32 B30         | Α          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice           | 2.74              | 1.67             | 60.0          |

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| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 6 of 20                   |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Description                | Face<br>or | Offset<br>Type | Offsets:<br>Horz | Azimuth<br>Adjustment | Placement |                    | $C_AA_A$<br>Front | $C_AA_A$<br>Side | Weigh          |
|----------------------------|------------|----------------|------------------|-----------------------|-----------|--------------------|-------------------|------------------|----------------|
|                            | Leg        |                | Lateral<br>Vert  |                       |           |                    |                   |                  |                |
|                            |            |                | ft<br>ft         | 0                     | ft        |                    | $ft^2$            | $ft^2$           | lb             |
|                            |            |                | ft               |                       |           |                    |                   |                  |                |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 2.96              | 1.86             | 81.11          |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 3.19              | 2.05             | 105.4          |
| RRUS-32 B30                | В          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 2.74              | 1.67             | 60.0           |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 2.96              | 1.86             | 81.1           |
| DD110 22 D20               |            | Б Б            | 0.00             | 0.0000                | 122.00    | 1" Ice             | 3.19              | 2.05             | 105.4          |
| RRUS-32 B30                | C          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 2.74              | 1.67             | 60.0           |
|                            |            |                | 0.00<br>0.00     |                       |           | 1/2" Ice<br>1" Ice | 2.96<br>3.19      | 1.86<br>2.05     | 81.1<br>105.4  |
| Raycap DC6-48-60-18-8F     | Α          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 0.83              | 0.83             | 22.0           |
| Kaycap Deo 40 00 10 01     | 11         | i ioni i acc   | 0.00             | 0.0000                | 122.00    | 1/2" Ice           | 1.34              | 1.34             | 37.9           |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 1.52              | 1.52             | 56.2           |
| Raycap DC6-48-60-18-8F     | В          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 0.83              | 0.83             | 22.0           |
| 7 1                        |            |                | 0.00             |                       |           | 1/2" Ice           | 1.34              | 1.34             | 37.9           |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 1.52              | 1.52             | 56.2           |
| Raycap DC6-48-60-18-8F     | C          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 0.83              | 0.83             | 22.0           |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 1.34              | 1.34             | 37.9           |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 1.52              | 1.52             | 56.2           |
| 2-ft Platform w/ Handrails | C          | None           |                  | 0.0000                | 122.00    | No Ice             | 45.00             | 45.00            | 500.0          |
|                            |            |                |                  |                       |           | 1/2" Ice           | 53.00             | 53.00            | 600.0          |
| alcalcaleTO Laborate       |            |                |                  |                       |           | 1" Ice             | 63.00             | 63.00            | 700.0          |
| ***Proposed***             |            | г г            | 4.00             | 0.0000                | 122.00    | NT T               | 15.52             | 7.01             | 1040           |
| CCI TPA65R-BU6D            | A          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 15.53             | 7.21             | 124.3          |
|                            |            |                | 0.00             |                       |           | 1/2" Ice<br>1" Ice | 16.16<br>16.75    | 8.39<br>9.28     | 228.8<br>342.0 |
| CCI TPA65R-BU6D            | В          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 15.53             | 9.28<br>7.21     | 124.3          |
| CCI II AOSK-BOOD           | ь          | 110m race      | 0.00             | 0.0000                | 122.00    | 1/2" Ice           | 16.16             | 8.39             | 228.8          |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 16.75             | 9.28             | 342.0          |
| CCI TPA65R-BU6D            | C          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 15.53             | 7.21             | 124.3          |
| CCI II II IOSK BEOD        | C          | r rom r ucc    | 0.00             | 0.0000                | 122.00    | 1/2" Ice           | 16.16             | 8.39             | 228.8          |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 16.75             | 9.28             | 342.0          |
| Ericsson Air6449 B77D      | Α          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 4.03              | 2.15             | 81.6           |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 4.29              | 2.36             | 111.2          |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 4.56              | 2.57             | 144.5          |
| Ericsson Air6449 B77D      | В          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 4.03              | 2.15             | 81.6           |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 4.29              | 2.36             | 111.2          |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 4.56              | 2.57             | 144.5          |
| Ericsson Air6449 B77D      | C          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 4.03              | 2.15             | 81.6           |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 4.29              | 2.36             | 111.2          |
| Eni AinC410 D77C           |            | F F            | 0.00             | 0.0000                | 122.00    | 1" Ice             | 4.56              | 2.57             | 144.5          |
| Ericsson Air6419 B77G      | A          | From Face      | 4.00<br>0.00     | 0.0000                | 122.00    | No Ice             | 3.80              | 1.94             | 77.0<br>104.8  |
|                            |            |                | 0.00             |                       |           | 1/2" Ice<br>1" Ice | 4.05<br>4.31      | 2.14<br>2.34     | 136.3          |
| Ericsson Air6419 B77G      | В          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 3.80              | 1.94             | 77.0           |
| Elicsson Allo417 B77G      | ь          | 1 Tom 1 acc    | 0.00             | 0.0000                | 122.00    | 1/2" Ice           | 4.05              | 2.14             | 104.8          |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 4.31              | 2.34             | 136.3          |
| Ericsson Air6419 B77G      | C          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 3.80              | 1.94             | 77.0           |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 4.05              | 2.14             | 104.8          |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 4.31              | 2.34             | 136.3          |
| CCI DMP65R-BU8DA-K         | A          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 17.87             | 8.12             | 95.7           |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 18.50             | 8.72             | 193.2          |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 19.14             | 9.32             | 299.1          |
| CCI DMP65R-BU8DA-K         | В          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 17.87             | 8.12             | 95.7           |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 18.50             | 8.72             | 193.2          |
| COLDANGED PAYOR :          | ~          |                | 0.00             | 0.0000                | 100.00    | 1" Ice             | 19.14             | 9.32             | 299.1          |
| CCI DMP65R-BU8DA-K         | C          | From Face      | 4.00             | 0.0000                | 122.00    | No Ice             | 17.87             | 8.12             | 95.70          |
|                            |            |                | 0.00             |                       |           | 1/2" Ice           | 18.50             | 8.72             | 193.2          |
|                            |            |                | 0.00             |                       |           | 1" Ice             | 19.14             | 9.32             | 299.1          |

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| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 7 of 20                   |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Description             | Face<br>or<br>Leg | Offset<br>Type | Offsets:<br>Horz<br>Lateral | Azimuth<br>Adjustment | Placement |          | C <sub>A</sub> A <sub>A</sub><br>Front | $C_AA_A$<br>Side | Weight |
|-------------------------|-------------------|----------------|-----------------------------|-----------------------|-----------|----------|--|------------------|--------|
|                         | 208               |                | Vert<br>ft<br>ft<br>ft      | ٥                     | ft        |          | ft <sup>2</sup>                        | ft²              | lb     |
| Ericsson RRUS 4478 B14  | A                 | From Face      | 4.00                        | 0.0000                | 122.00    | No Ice   | 1.84                                   | 1.06             | 59.90  |
| Elicsson Rices 1170 B11 |                   | r rom r acc    | 0.00                        | 0.0000                | 122.00    | 1/2" Ice | 2.01                                   | 1.20             | 75.78  |
|                         |                   |                | 0.00                        |                       |           | 1" Ice   | 2.19                                   | 1.34             | 94.29  |
| Ericsson RRUS 4478 B14  | В                 | From Face      | 4.00                        | 0.0000                | 122.00    | No Ice   | 1.84                                   | 1.06             | 59.90  |
|                         |                   |                | 0.00                        |                       |           | 1/2" Ice | 2.01                                   | 1.20             | 75.78  |
|                         |                   |                | 0.00                        |                       |           | 1" Ice   | 2.19                                   | 1.34             | 94.29  |
| Ericsson RRUS 4478 B14  | C                 | From Face      | 4.00                        | 0.0000                | 122.00    | No Ice   | 1.84                                   | 1.06             | 59.90  |
|                         |                   |                | 0.00                        |                       |           | 1/2" Ice | 2.01                                   | 1.20             | 75.78  |
|                         |                   |                | 0.00                        |                       |           | 1" Ice   | 2.19                                   | 1.34             | 94.29  |
| RRUS-8843 B2/B66A       | A                 | From Face      | 4.00                        | 0.0000                | 122.00    | No Ice   | 1.64                                   | 1.35             | 72.00  |
|                         |                   |                | 0.00                        |                       |           | 1/2" Ice | 1.80                                   | 1.50             | 89.60  |
|                         |                   |                | 0.00                        |                       |           | 1" Ice   | 1.97                                   | 1.65             | 109.91 |
| RRUS-8843 B2/B66A       | В                 | From Face      | 4.00                        | 0.0000                | 122.00    | No Ice   | 1.64                                   | 1.35             | 72.00  |
|                         |                   |                | 0.00                        |                       |           | 1/2" Ice | 1.80                                   | 1.50             | 89.60  |
|                         |                   |                | 0.00                        |                       |           | 1" Ice   | 1.97                                   | 1.65             | 109.91 |
| RRUS-8843 B2/B66A       | C                 | From Face      | 4.00                        | 0.0000                | 122.00    | No Ice   | 1.64                                   | 1.35             | 72.00  |
|                         |                   |                | 0.00                        |                       |           | 1/2" Ice | 1.80                                   | 1.50             | 89.60  |
|                         |                   |                | 0.00                        |                       |           | 1" Ice   | 1.97                                   | 1.65             | 109.91 |

| Dishes            |                   |               |                |                                     |                       |                       |           |                     |          |                  |        |
|-------------------|-------------------|---------------|----------------|-------------------------------------|-----------------------|-----------------------|-----------|---------------------|----------|------------------|--------|
| Description       | Face<br>or<br>Leg | Dish<br>Type  | Offset<br>Type | Offsets:<br>Horz<br>Lateral<br>Vert | Azimuth<br>Adjustment | 3 dB<br>Beam<br>Width | Elevation | Outside<br>Diameter |          | Aperture<br>Area | Weight |
|                   |                   |               |                | ft                                  | 0                     | 0                     | ft        | ft                  |          | $ft^2$           | lb     |
| 6' Dish w/ Shroud | С                 | Paraboloid    | From           | 1.00                                | 0.0000                |                       | 141.00    | 6.00                | No Ice   | 28.27            | 350.00 |
| (HP)              |                   | w/Shroud (HP) | Face           | 0.00                                |                       |                       |           |                     | 1/2" Ice | 29.05            | 500.00 |
|                   |                   |               |                | 0.00                                |                       |                       |           |                     | 1" Ice   | 29.80            | 650.00 |

# **Tower Pressures - No Ice**

 $G_H=1.100$ 

| Section        | z      | $K_Z$ | $q_z$ | $A_G$   | F | $A_F$           | $A_R$   | $A_{leg}$       | Leg    | $C_AA_A$        | $C_AA_A$ |
|----------------|--------|-------|-------|---------|---|-----------------|---------|-----------------|--------|-----------------|----------|
| Elevation      |        |       |       |         | a |                 |         |                 | %      | In              | Out      |
|                |        |       |       |         | С |                 |         |                 |        | Face            | Face     |
| ft             | ft     |       | psf   | $ft^2$  | e | ft <sup>2</sup> | $ft^2$  | ft <sup>2</sup> |        | ft <sup>2</sup> | $ft^2$   |
| L1             | 122.02 | 1.046 | 36    | 115.350 | A | 0.000           | 115.350 | 115.350         | 100.00 | 0.000           | 0.000    |
| 150.00-97.25   |        |       |       |         | В | 0.000           | 115.350 |                 | 100.00 | 0.000           | 0.000    |
|                |        |       |       |         | C | 0.000           | 115.350 |                 | 100.00 | 3.956           | 1.978    |
| L2 97.25-48.25 | 72.13  | 0.9   | 31    | 152.078 | Α | 0.000           | 152.078 | 152.078         | 100.00 | 0.000           | 0.000    |
|                |        |       |       |         | В | 0.000           | 152.078 |                 | 100.00 | 0.000           | 0.000    |
|                |        |       |       |         | C | 0.000           | 152.078 |                 | 100.00 | 3.675           | 1.838    |
| L3 48.25-1.00  | 24.06  | 0.7   | 25    | 187.019 | Α | 0.000           | 187.019 | 187.019         | 100.00 | 0.000           | 0.000    |
|                |        |       |       |         | В | 0.000           | 187.019 |                 | 100.00 | 0.000           | 0.000    |
|                |        |       |       |         | C | 0.000           | 187.019 |                 | 100.00 | 3.544           | 1.772    |

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| Job            | Page              |
|----------------|-------------------|
| CTL02638       | 8 of 20           |
| Project        | Date              |
|                | 12:41:35 05/02/22 |
| Client         | Designed by       |
| Smartlink/AT&T | LA                |

# **Tower Pressure - With Ice**

 $G_H = 1.100$ 

| Section         | z      | $K_Z$ | $q_z$ | $t_Z$  | $A_G$   | F | $A_F$           | $A_R$   | $A_{leg}$       | Leg    | $C_A A_A$ | $C_A A_A$ |
|-----------------|--------|-------|-------|--------|---------|---|-----------------|---------|-----------------|--------|-----------|-----------|
| Elevation       |        |       |       |        |         | a |                 |         |                 | %      | In        | Out       |
|                 |        |       |       |        |         | c |                 |         |                 |        | Face      | Face      |
| ft              | ft     |       | psf   | in     | $ft^2$  | e | ft <sup>2</sup> | $ft^2$  | ft <sup>2</sup> |        | $ft^2$    | $ft^2$    |
| L1 150.00-97.25 | 122.02 | 1.046 | 6     | 1.1397 | 125.370 | A | 0.000           | 125.370 | 125.370         | 100.00 | 0.000     | 0.000     |
|                 |        |       |       |        |         | В | 0.000           | 125.370 |                 | 100.00 | 0.000     | 0.000     |
|                 |        |       |       |        |         | C | 0.000           | 125.370 |                 | 100.00 | 15.980    | 14.002    |
| L2 97.25-48.25  | 72.13  | 0.9   | 5     | 1.0813 | 161.386 | Α | 0.000           | 161.386 | 161.386         | 100.00 | 0.000     | 0.000     |
|                 |        |       |       |        |         | В | 0.000           | 161.386 |                 | 100.00 | 0.000     | 0.000     |
|                 |        |       |       |        |         | C | 0.000           | 161.386 |                 | 100.00 | 14.844    | 13.007    |
| L3 48.25-1.00   | 24.06  | 0.7   | 4     | 0.9689 | 195.534 | Α | 0.000           | 195.534 | 195.534         | 100.00 | 0.000     | 0.000     |
|                 |        |       |       |        |         | В | 0.000           | 195.534 |                 | 100.00 | 0.000     | 0.000     |
|                 |        |       |       |        |         | C | 0.000           | 195.534 |                 | 100.00 | 13.762    | 11.991    |

# **Tower Pressure - Service**

 $G_H=1.100$ 

| Section        | z      | $K_Z$ | $q_z$ | $A_G$   | F | $A_F$           | $A_R$   | $A_{leg}$       | Leg    | $C_A A_A$ | $C_A A_A$ |
|----------------|--------|-------|-------|---------|---|-----------------|---------|-----------------|--------|-----------|-----------|
| Elevation      |        |       |       |         | а |                 |         |                 | %      | In        | Out       |
|                |        |       |       |         | С |                 |         |                 |        | Face      | Face      |
| ft             | ft     |       | psf   | $ft^2$  | e | ft <sup>2</sup> | $ft^2$  | ft <sup>2</sup> |        | $ft^2$    | $ft^2$    |
| L1             | 122.02 | 1.046 | 8     | 115.350 | A | 0.000           | 115.350 | 115.350         | 100.00 | 0.000     | 0.000     |
| 150.00-97.25   |        |       |       |         | В | 0.000           | 115.350 |                 | 100.00 | 0.000     | 0.000     |
|                |        |       |       |         | C | 0.000           | 115.350 |                 | 100.00 | 3.956     | 1.978     |
| L2 97.25-48.25 | 72.13  | 0.9   | 7     | 152.078 | Α | 0.000           | 152.078 | 152.078         | 100.00 | 0.000     | 0.000     |
|                |        |       |       |         | В | 0.000           | 152.078 |                 | 100.00 | 0.000     | 0.000     |
|                |        |       |       |         | C | 0.000           | 152.078 |                 | 100.00 | 3.675     | 1.838     |
| L3 48.25-1.00  | 24.06  | 0.7   | 6     | 187.019 | Α | 0.000           | 187.019 | 187.019         | 100.00 | 0.000     | 0.000     |
|                |        |       |       |         | В | 0.000           | 187.019 |                 | 100.00 | 0.000     | 0.000     |
|                |        |       |       |         | C | 0.000           | 187.019 |                 | 100.00 | 3.544     | 1.772     |

# **Tower Forces - No Ice - Wind Normal To Face**

| Section       | Add     | Self     | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$     | F        | w     | Ctrl. |
|---------------|---------|----------|---|---|-------|-------|-------|-------|-----------|----------|-------|-------|
| Elevation     | Weight  | Weight   | а |   |       |       |       |       |           |          |       | Face  |
|               |         |          | c |   |       | psf   |       |       |           |          |       |       |
| ft            | lb      | lb       | e |   |       |       |       |       | $ft^2$    | lb       | plf   |       |
| L1            | 505.82  | 3650.51  | Α | 1 | 0.73  | 36    | 1     | 1     | 115.350   | 3376.47  | 64.01 | C     |
| 150.00-97.25  |         |          | В | 1 | 0.73  |       | 1     | 1     | 115.350   |          |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 115.350   |          |       |       |
| L2            | 563.50  | 6484.44  | Α | 1 | 0.73  | 31    | 1     | 1     | 152.078   | 3792.42  | 77.40 | C     |
| 97.25-48.25   |         |          | В | 1 | 0.73  |       | 1     | 1     | 152.078   |          |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 152.078   |          |       |       |
| L3 48.25-1.00 | 532.58  | 9875.25  | Α | 1 | 0.73  | 25    | 1     | 1     | 187.019   | 3729.39  | 78.93 | C     |
|               |         |          | В | 1 | 0.73  |       | 1     | 1     | 187.019   |          |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 187.019   |          |       |       |
| Sum Weight:   | 1601.90 | 20010.20 |   |   |       |       |       | OTM   | 764368.22 | 10898.28 |       |       |

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| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 9 of 20                   |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Section   | Add    | Self   | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$  | F  | w   | Ctrl. |
|-----------|--------|--------|---|---|-------|-------|-------|-------|--------|----|-----|-------|
| Elevation | Weight | Weight | а |   |       |       |       |       |        |    |     | Face  |
|           |        |        | С |   |       | psf   |       |       |        |    |     |       |
| ft        | lb     | lb     | e |   |       |       |       |       | $ft^2$ | lb | plf |       |
|           |        |        |   |   |       |       |       |       | lb-ft  |    |     |       |

# **Tower Forces - No Ice - Wind 60 To Face**

| Section       | Add     | Self     | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$           | F        | w     | Ctrl. |
|---------------|---------|----------|---|---|-------|-------|-------|-------|-----------------|----------|-------|-------|
| Elevation     | Weight  | Weight   | a |   |       |       |       |       |                 |          |       | Face  |
|               |         |          | c |   |       | psf   |       |       |                 |          |       |       |
| ft            | lb      | lb       | e |   |       |       |       |       | ft <sup>2</sup> | lb       | plf   |       |
| L1            | 505.82  | 3650.51  | Α | 1 | 0.73  | 36    | 1     | 1     | 115.350         | 3376.47  | 64.01 | C     |
| 150.00-97.25  |         |          | В | 1 | 0.73  |       | 1     | 1     | 115.350         |          |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 115.350         |          |       |       |
| L2            | 563.50  | 6484.44  | Α | 1 | 0.73  | 31    | 1     | 1     | 152.078         | 3792.42  | 77.40 | C     |
| 97.25-48.25   |         |          | В | 1 | 0.73  |       | 1     | 1     | 152.078         |          |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 152.078         |          |       |       |
| L3 48.25-1.00 | 532.58  | 9875.25  | Α | 1 | 0.73  | 25    | 1     | 1     | 187.019         | 3729.39  | 78.93 | C     |
|               |         |          | В | 1 | 0.73  |       | 1     | 1     | 187.019         |          |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 187.019         |          |       |       |
| Sum Weight:   | 1601.90 | 20010.20 |   |   |       |       |       | OTM   | 764368.22       | 10898.28 |       |       |
| _             |         |          |   |   |       |       |       |       | lb-ft           |          |       |       |

# **Tower Forces - No Ice - Wind 90 To Face**

| Section       | Add     | Self     | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$           | F        | w     | Ctrl. |
|---------------|---------|----------|---|---|-------|-------|-------|-------|-----------------|----------|-------|-------|
| Elevation     | Weight  | Weight   | а |   |       |       |       |       |                 |          |       | Face  |
|               |         |          | С |   |       | psf   |       |       |                 |          |       |       |
| ft            | lb      | lb       | e |   |       |       |       |       | ft <sup>2</sup> | lb       | plf   |       |
| L1            | 505.82  | 3650.51  | Α | 1 | 0.73  | 36    | 1     | 1     | 115.350         | 3376.47  | 64.01 | C     |
| 150.00-97.25  |         |          | В | 1 | 0.73  |       | 1     | 1     | 115.350         |          |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 115.350         |          |       |       |
| L2            | 563.50  | 6484.44  | Α | 1 | 0.73  | 31    | 1     | 1     | 152.078         | 3792.42  | 77.40 | C     |
| 97.25-48.25   |         |          | В | 1 | 0.73  |       | 1     | 1     | 152.078         |          |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 152.078         |          |       |       |
| L3 48.25-1.00 | 532.58  | 9875.25  | Α | 1 | 0.73  | 25    | 1     | 1     | 187.019         | 3729.39  | 78.93 | C     |
|               |         |          | В | 1 | 0.73  |       | 1     | 1     | 187.019         |          |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 187.019         |          |       |       |
| Sum Weight:   | 1601.90 | 20010.20 |   |   |       |       |       | OTM   | 764368.22       | 10898.28 |       |       |
|               |         |          |   |   |       |       |       |       | lb-ft           |          |       |       |

# **Tower Forces - With Ice - Wind Normal To Face**

| Г | Section   | Add    | Self   | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$  | F  | w   | Ctrl. |
|---|-----------|--------|--------|---|---|-------|-------|-------|-------|--------|----|-----|-------|
|   | Elevation | Weight | Weight | а |   |       |       |       |       |        |    |     | Face  |
|   |           |        |        | c |   |       | psf   |       |       | _      |    |     |       |
|   | ft        | lb     | lb     | e |   |       |       |       |       | $ft^2$ | lb | plf |       |

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| Job                   | Page                      |
|-----------------------|---------------------------|
| CTL02638              | 10 of 20                  |
| Project               | Date<br>12:41:35 05/02/22 |
| Client Smartlink/AT&T | Designed by LA            |

| Section       | Add     | Self     | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$     | F       | w     | Ctrl. |
|---------------|---------|----------|---|---|-------|-------|-------|-------|-----------|---------|-------|-------|
| Elevation     | Weight  | Weight   | а |   |       |       |       |       |           |         |       | Face  |
|               |         |          | С |   |       | psf   |       |       |           |         |       |       |
| ft            | lb      | lb       | e |   |       |       |       |       | $ft^2$    | lb      | plf   |       |
| L1            | 708.35  | 5655.57  | Α | 1 | 1.2   | 6     | 1     | 1     | 125.370   | 1137.39 | 21.56 | C     |
| 150.00-97.25  |         |          | В | 1 | 1.2   |       | 1     | 1     | 125.370   |         |       |       |
|               |         |          | C | 1 | 1.2   |       | 1     | 1     | 125.370   |         |       |       |
| L2            | 751.63  | 8957.04  | Α | 1 | 1.2   | 5     | 1     | 1     | 160.909   | 1222.69 | 24.95 | C     |
| 97.25-48.25   |         |          | В | 1 | 1.2   |       | 1     | 1     | 160.909   |         |       |       |
|               |         |          | C | 1 | 1.2   |       | 1     | 1     | 160.909   |         |       |       |
| L3 48.25-1.00 | 701.05  | 12576.41 | Α | 1 | 1.2   | 4     | 1     | 1     | 194.649   | 1169.09 | 24.74 | C     |
|               |         |          | В | 1 | 1.2   |       | 1     | 1     | 194.649   |         |       |       |
|               |         |          | C | 1 | 1.2   |       | 1     | 1     | 194.649   |         |       |       |
| Sum Weight:   | 2161.03 | 27189.02 |   |   |       |       |       | OTM   | 251573.65 | 3529.17 |       |       |
|               |         |          |   |   |       |       |       |       | lb-ft     |         |       |       |

# **Tower Forces - With Ice - Wind 60 To Face**

| Section       | Add     | Self     | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$           | F       | w     | Ctrl. |
|---------------|---------|----------|---|---|-------|-------|-------|-------|-----------------|---------|-------|-------|
| Elevation     | Weight  | Weight   | а |   |       |       |       |       |                 |         |       | Face  |
|               |         |          | c |   |       | psf   |       |       |                 |         |       |       |
| ft            | lb      | lb       | e |   |       |       |       |       | ft <sup>2</sup> | lb      | plf   |       |
| L1            | 708.35  | 5655.57  | Α | 1 | 1.2   | 6     | 1     | 1     | 125.370         | 1137.39 | 21.56 | C     |
| 150.00-97.25  |         |          | В | 1 | 1.2   |       | 1     | 1     | 125.370         |         |       |       |
|               |         |          | C | 1 | 1.2   |       | 1     | 1     | 125.370         |         |       |       |
| L2            | 751.63  | 8957.04  | Α | 1 | 1.2   | 5     | 1     | 1     | 160.909         | 1222.69 | 24.95 | C     |
| 97.25-48.25   |         |          | В | 1 | 1.2   |       | 1     | 1     | 160.909         |         |       |       |
|               |         |          | C | 1 | 1.2   |       | 1     | 1     | 160.909         |         |       |       |
| L3 48.25-1.00 | 701.05  | 12576.41 | Α | 1 | 1.2   | 4     | 1     | 1     | 194.649         | 1169.09 | 24.74 | C     |
|               |         |          | В | 1 | 1.2   |       | 1     | 1     | 194.649         |         |       |       |
|               |         |          | C | 1 | 1.2   |       | 1     | 1     | 194.649         |         |       |       |
| Sum Weight:   | 2161.03 | 27189.02 |   |   |       |       |       | OTM   | 251573.65       | 3529.17 |       |       |
|               |         |          |   |   |       |       |       |       | lb-ft           |         |       |       |

# **Tower Forces - With Ice - Wind 90 To Face**

| Section       | Add     | Self     | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$     | F       | w     | Ctrl. |
|---------------|---------|----------|---|---|-------|-------|-------|-------|-----------|---------|-------|-------|
| Elevation     | Weight  | Weight   | a |   |       |       |       |       |           |         |       | Face  |
|               |         |          | С |   |       | psf   |       |       |           |         |       |       |
| ft            | lb      | lb       | e |   |       |       |       |       | $ft^2$    | lb      | plf   |       |
| L1            | 708.35  | 5655.57  | Α | 1 | 1.2   | 6     | 1     | 1     | 125.370   | 1137.39 | 21.56 | C     |
| 150.00-97.25  |         |          | В | 1 | 1.2   |       | 1     | 1     | 125.370   |         |       |       |
|               |         |          | C | 1 | 1.2   |       | 1     | 1     | 125.370   |         |       |       |
| L2            | 751.63  | 8957.04  | Α | 1 | 1.2   | 5     | 1     | 1     | 160.909   | 1222.69 | 24.95 | C     |
| 97.25-48.25   |         |          | В | 1 | 1.2   |       | 1     | 1     | 160.909   |         |       |       |
|               |         |          | C | 1 | 1.2   |       | 1     | 1     | 160.909   |         |       |       |
| L3 48.25-1.00 | 701.05  | 12576.41 | Α | 1 | 1.2   | 4     | 1     | 1     | 194.649   | 1169.09 | 24.74 | C     |
|               |         |          | В | 1 | 1.2   |       | 1     | 1     | 194.649   |         |       |       |
|               |         |          | C | 1 | 1.2   |       | 1     | 1     | 194.649   |         |       |       |
| Sum Weight:   | 2161.03 | 27189.02 |   |   |       |       |       | OTM   | 251573.65 | 3529.17 |       |       |
|               |         |          |   |   |       |       |       |       | lb-ft     |         |       |       |

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| Job     |                | Page              |
|---------|----------------|-------------------|
|         | CTL02638       | 11 of 20          |
| Project |                | Date              |
|         |                | 12:41:35 05/02/22 |
| Client  | 0 # 1/4-70-7   | Designed by       |
|         | Smartlink/AT&T | LA                |

# **Tower Forces - Service - Wind Normal To Face**

| Section       | Add     | Self     | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$     | F       | w     | Ctrl. |
|---------------|---------|----------|---|---|-------|-------|-------|-------|-----------|---------|-------|-------|
| Elevation     | Weight  | Weight   | а |   |       |       |       |       |           |         |       | Face  |
|               |         |          | c |   |       | psf   |       |       |           |         |       |       |
| ft            | lb      | lb       | e |   |       |       |       |       | $ft^2$    | lb      | plf   |       |
| L1            | 505.82  | 3650.51  | Α | 1 | 0.73  | 8     | 1     | 1     | 115.350   | 768.01  | 14.56 | C     |
| 150.00-97.25  |         |          | В | 1 | 0.73  |       | 1     | 1     | 115.350   |         |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 115.350   |         |       |       |
| L2            | 563.50  | 6484.44  | Α | 1 | 0.73  | 7     | 1     | 1     | 152.078   | 862.62  | 17.60 | C     |
| 97.25-48.25   |         |          | В | 1 | 0.73  |       | 1     | 1     | 152.078   |         |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 152.078   |         |       |       |
| L3 48.25-1.00 | 532.58  | 9875.25  | Α | 1 | 0.73  | 6     | 1     | 1     | 187.019   | 848.29  | 17.95 | C     |
|               |         |          | В | 1 | 0.73  |       | 1     | 1     | 187.019   |         |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 187.019   |         |       |       |
| Sum Weight:   | 1601.90 | 20010.20 |   |   |       |       |       | OTM   | 173862.74 | 2478.92 |       |       |
|               |         |          |   |   |       |       |       |       | lb-ft     |         |       |       |

# **Tower Forces - Service - Wind 60 To Face**

| Section       | Add     | Self     | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$     | F       | w     | Ctrl. |
|---------------|---------|----------|---|---|-------|-------|-------|-------|-----------|---------|-------|-------|
| Elevation     | Weight  | Weight   | а |   |       |       |       |       |           |         |       | Face  |
|               |         |          | С |   |       | psf   |       |       |           |         |       |       |
| ft            | lb      | lb       | e |   |       |       |       |       | $ft^2$    | lb      | plf   |       |
| L1            | 505.82  | 3650.51  | Α | 1 | 0.73  | 8     | 1     | 1     | 115.350   | 768.01  | 14.56 | C     |
| 150.00-97.25  |         |          | В | 1 | 0.73  |       | 1     | 1     | 115.350   |         |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 115.350   |         |       |       |
| L2            | 563.50  | 6484.44  | Α | 1 | 0.73  | 7     | 1     | 1     | 152.078   | 862.62  | 17.60 | C     |
| 97.25-48.25   |         |          | В | 1 | 0.73  |       | 1     | 1     | 152.078   |         |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 152.078   |         |       |       |
| L3 48.25-1.00 | 532.58  | 9875.25  | Α | 1 | 0.73  | 6     | 1     | 1     | 187.019   | 848.29  | 17.95 | C     |
|               |         |          | В | 1 | 0.73  |       | 1     | 1     | 187.019   |         |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 187.019   |         |       |       |
| Sum Weight:   | 1601.90 | 20010.20 |   |   |       |       |       | OTM   | 173862.74 | 2478.92 |       |       |
|               |         |          |   |   |       |       |       |       | lb-ft     |         |       |       |

# **Tower Forces - Service - Wind 90 To Face**

| Section      | Add    | Self    | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$   | F      | w     | Ctrl. |
|--------------|--------|---------|---|---|-------|-------|-------|-------|---------|--------|-------|-------|
| Elevation    | Weight | Weight  | a |   |       |       |       |       |         |        |       | Face  |
|              |        |         | c |   |       | psf   |       |       |         |        |       |       |
| ft           | lb     | lb      | e |   |       |       |       |       | $ft^2$  | lb     | plf   |       |
| L1           | 505.82 | 3650.51 | Α | 1 | 0.73  | 8     | 1     | 1     | 115.350 | 768.01 | 14.56 | C     |
| 150.00-97.25 |        |         | В | 1 | 0.73  |       | 1     | 1     | 115.350 |        |       |       |
|              |        |         | C | 1 | 0.73  |       | 1     | 1     | 115.350 |        |       |       |
| L2           | 563.50 | 6484.44 | Α | 1 | 0.73  | 7     | 1     | 1     | 152.078 | 862.62 | 17.60 | C     |
| 97.25-48.25  |        |         | В | 1 | 0.73  |       | 1     | 1     | 152.078 |        |       |       |
|              |        |         | C | 1 | 0.73  |       | 1     | 1     | 152.078 |        |       |       |

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| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 12 of 20                  |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Section       | Add     | Self     | F | e | $C_F$ | $q_z$ | $D_F$ | $D_R$ | $A_E$     | F       | w     | Ctrl. |
|---------------|---------|----------|---|---|-------|-------|-------|-------|-----------|---------|-------|-------|
| Elevation     | Weight  | Weight   | а |   |       |       |       |       |           |         |       | Face  |
|               |         |          | С |   |       | psf   |       |       |           |         |       |       |
| ft            | lb      | lb       | e |   |       |       |       |       | $ft^2$    | lb      | plf   |       |
| L3 48.25-1.00 | 532.58  | 9875.25  | Α | 1 | 0.73  | 6     | 1     | 1     | 187.019   | 848.29  | 17.95 | C     |
|               |         |          | В | 1 | 0.73  |       | 1     | 1     | 187.019   |         |       |       |
|               |         |          | C | 1 | 0.73  |       | 1     | 1     | 187.019   |         |       |       |
| Sum Weight:   | 1601.90 | 20010.20 |   |   |       |       |       | OTM   | 173862.74 | 2478.92 |       |       |
|               |         |          |   |   |       |       |       |       | lb-ft     |         |       |       |

# **Force Totals**

| Load                     | Vertical | Sum of    | Sum of    | Sum of         | Sum of         | Sum of Torques |
|--------------------------|----------|-----------|-----------|----------------|----------------|----------------|
| Case                     | Forces   | Forces    | Forces    | Overturning    | Overturning    |                |
|                          |          | X         | Z         | Moments, $M_x$ | Moments, $M_z$ |                |
|                          | lb       | lb        | lb        | lb-ft          | lb-ft          | lb-ft          |
| Leg Weight               | 20010.20 |           |           |                |                |                |
| Bracing Weight           | 0.00     |           |           |                |                |                |
| Total Member Self-Weight | 20010.20 |           |           | 1305.14        | 99.96          |                |
| Total Weight             | 25365.25 |           |           | 1305.14        | 99.96          |                |
| Wind 0 deg - No Ice      |          | 0.00      | -19265.78 | -1838562.43    | 99.96          | -352.75        |
| Wind 30 deg - No Ice     |          | 9174.29   | -16821.44 | -1611216.86    | -855629.16     | 280.79         |
| Wind 60 deg - No Ice     |          | 15845.49  | -9996.61  | -969549.59     | -1475789.45    | 1318.02        |
| Wind 90 deg - No Ice     |          | 18529.30  | 126.51    | 19016.77       | -1736660.61    | 2920.59        |
| Wind 120 deg - No Ice    |          | 15926.82  | 9725.51   | 934206.37      | -1487175.50    | 2607.43        |
| Wind 150 deg - No Ice    |          | 9106.51   | 16527.75  | 1572710.84     | -846140.79     | 1550.75        |
| Wind 180 deg - No Ice    |          | 0.00      | 18981.13  | 1801321.54     | 99.96          | 352.75         |
| Wind 210 deg - No Ice    |          | -9106.51  | 16527.75  | 1572710.84     | 846340.71      | -939.77        |
| Wind 240 deg - No Ice    |          | -15926.82 | 9725.51   | 934206.37      | 1487375.43     | -2254.68       |
| Wind 270 deg - No Ice    |          | -18529.30 | 126.51    | 19016.77       | 1736860.54     | -2920.59       |
| Wind 300 deg - No Ice    |          | -15845.49 | -9996.61  | -969549.59     | 1475989.38     | -1670.77       |
| Wind 330 deg - No Ice    |          | -9174.29  | -16821.44 | -1611216.86    | 855829.09      | -891.77        |
| Member Ice               | 7178.82  |           |           |                |                |                |
| Total Weight Ice         | 37161.09 |           |           | 3015.84        | 425.59         |                |
| Wind 0 deg - Ice         |          | 0.00      | -5524.09  | -507185.36     | 425.59         | -327.08        |
| Wind 30 deg - Ice        |          | 2676.03   | -4809.65  | -442423.12     | -242632.78     | -60.28         |
| Wind 60 deg - Ice        |          | 4626.61   | -2830.26  | -261635.49     | -419386.57     | 312.50         |
| Wind 90 deg - Ice        |          | 5385.95   | 23.73     | 6337.83        | -490436.86     | 773.82         |
| Wind 120 deg - Ice       |          | 4641.86   | 2779.42   | 260548.61      | -421522.14     | 815.26         |
| Wind 150 deg - Ice       |          | 2663.32   | 4754.57   | 440743.03      | -240853.15     | 629.84         |
| Wind 180 deg - Ice       |          | 0.00      | 5470.70   | 505742.55      | 425.59         | 327.08         |
| Wind 210 deg - Ice       |          | -2663.32  | 4754.57   | 440743.03      | 241704.33      | -63.32         |
| Wind 240 deg - Ice       |          | -4641.86  | 2779.42   | 260548.61      | 422373.32      | -488.18        |
| Wind 270 deg - Ice       |          | -5385.95  | 23.73     | 6337.83        | 491288.05      | -773.82        |
| Wind 300 deg - Ice       |          | -4626.61  | -2830.26  | -261635.49     | 420237.76      | -639.58        |
| Wind 330 deg - Ice       |          | -2676.03  | -4809.65  | -442423.12     | 243483.97      | -506.24        |
| Total Weight             | 25365.25 |           |           | 1305.14        | 99.96          |                |
| Wind 0 deg - Service     |          | 0.00      | -4386.32  | -417825.29     | 57.27          | -80.24         |
| Wind 30 deg - Service    |          | 2088.85   | -3829.78  | -366046.31     | -194836.77     | 63.87          |
| Wind 60 deg - Service    |          | 3607.79   | -2275.89  | -219909.74     | -336081.37     | 299.80         |
| Wind 90 deg - Service    |          | 4218.80   | 28.78     | 5199.38        | -395486.07     | 664.31         |
| Wind 120 deg - Service   |          | 3626.29   | 2214.23   | 213618.27      | -338671.23     | 593.08         |
| Wind 150 deg - Service   |          | 2073.43   | 3762.98   | 359035.43      | -192678.55     | 352.73         |
| Wind 180 deg - Service   |          | 0.00      | 4321.58   | 411102.18      | 57.27          | 80.24          |
| Wind 210 deg - Service   |          | -2073.43  | 3762.98   | 359035.43      | 192793.10      | -213.76        |
| Wind 240 deg - Service   |          | -3626.29  | 2214.23   | 213618.27      | 338785.78      | -512.85        |
| Wind 270 deg - Service   |          | -4218.80  | 28.78     | 5199.38        | 395600.61      | -664.31        |
| Wind 300 deg - Service   |          | -3607.79  | -2275.89  | -219909.74     |                | -380.03        |
|                          |          | 2007.77   | 22.3.07   | 21//0///       | 2201,3.72      | 203.03         |

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| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 13 of 20                  |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Load                   | Vertical | Sum of   | Sum of   | Sum of         | Sum of         | Sum of Torques |
|------------------------|----------|----------|----------|----------------|----------------|----------------|
| Case                   | Forces   | Forces   | Forces   | Overturning    | Overturning    |                |
|                        |          | X        | Z        | Moments, $M_x$ | Moments, $M_z$ |                |
|                        | lb       | lb       | lb       | lb-ft          | lb-ft          | lb-ft          |
| Wind 330 deg - Service |          | -2088.85 | -3829.78 | -366046.31     | 194951.32      | -202.84        |

# **Load Combinations**

| Comb.    | Description   |
|----------|---|
| No.      | •   |
| 1        | Dead Only   |
| 2        | 1.2 Dead+1.0 Wind 0 deg - No Ice  |
| 3        | 0.9 Dead+1.0 Wind 0 deg - No Ice  |
| 4        | 1.2 Dead+1.0 Wind 30 deg - No Ice                                       |
| 5        | 0.9 Dead+1.0 Wind 30 deg - No Ice                                       |
| 6        | 1.2 Dead+1.0 Wind 60 deg - No Ice                                       |
| 7        | 0.9 Dead+1.0 Wind 60 deg - No Ice                                       |
| 8        | 1.2 Dead+1.0 Wind 90 deg - No Ice                                       |
| 9        | 0.9 Dead+1.0 Wind 90 deg - No Ice                                       |
| 10       | 1.2 Dead+1.0 Wind 120 deg - No Ice                                      |
| 11       | 0.9 Dead+1.0 Wind 120 deg - No Ice                                      |
| 12       | 1.2 Dead+1.0 Wind 150 deg - No Ice                                      |
| 13       | 0.9 Dead+1.0 Wind 150 deg - No Ice                                      |
| 14       | 1.2 Dead+1.0 Wind 180 deg - No Ice                                      |
| 15       | 0.9 Dead+1.0 Wind 180 deg - No Ice                                      |
| 16       | 1.2 Dead+1.0 Wind 210 deg - No Ice                                      |
| 17       | 0.9 Dead+1.0 Wind 210 deg - No Ice                                      |
| 18       | 1.2 Dead+1.0 Wind 240 deg - No Ice                                      |
| 19       | 0.9 Dead+1.0 Wind 240 deg - No Ice                                      |
| 20       | 1.2 Dead+1.0 Wind 270 deg - No Ice                                      |
| 21       | 0.9 Dead+1.0 Wind 270 deg - No Ice                                      |
| 22       | 1.2 Dead+1.0 Wind 300 deg - No Ice                                      |
| 23       | 0.9 Dead+1.0 Wind 300 deg - No Ice                                      |
| 24       | 1.2 Dead+1.0 Wind 330 deg - No Ice                                      |
| 25       | 0.9 Dead+1.0 Wind 330 deg - No Ice                                      |
| 26       | 1.2 Dead+1.0 Ice+1.0 Temp   |
| 27       | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp                                |
| 28       | 1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp                               |
| 29       | 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp                               |
| 30       | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp                               |
| 31       | 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp                              |
| 32       | 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp                              |
| 33       | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp                              |
| 34       | 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp                              |
| 35       | 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp                              |
| 36       | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp                              |
| 37<br>38 | 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp                              |
| 36<br>39 | 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp<br>Dead+Wind 0 deg - Service |
| 40       | Dead+Wind 30 deg - Service  |
| 41       | Dead+Wind 50 deg - Service  Dead+Wind 60 deg - Service                  |
| 42       | Dead+Wind 90 deg - Service  Dead+Wind 90 deg - Service                  |
| 43       | Dead+Wind 120 deg - Service   |
| 43<br>44 | Dead+Wind 150 deg - Service  Dead+Wind 150 deg - Service                |
| 45       | Dead+Wind 180 deg - Service  Dead+Wind 180 deg - Service                |
| 46       | Dead+Wind 210 deg - Service  Dead+Wind 210 deg - Service                |
| 47       | Dead+Wind 240 deg - Service   |
| 48       | Dead+Wind 270 deg - Service   |
| 49       | Dead+Wind 300 deg - Service   |
| .,       | 2000-1-100  |
|          |   |

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| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 14 of 20                  |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Comb. |                             | Description |  |
|-------|-----------------------------|-------------|--|
| No.   |                             |             |  |
| 50    | Dead+Wind 330 deg - Service |             |  |

# **Maximum Member Forces**

| Section | Elevation     | Component | Condition        | Gov.  | Axial     | Major Axis | Minor Axis |
|---------|---------------|-----------|------------------|-------|-----------|------------|------------|
| No.     | ft            | Туре      |                  | Load  |           | Moment     | Moment     |
|         |               |           |                  | Comb. | lb        | lb-ft      | lb-ft      |
| L1      | 150 - 97.25   | Pole      | Max Tension      | 27    | 0.00      | -0.03      | -0.36      |
|         |               |           | Max. Compression | 26    | -15064.64 | 241.22     | -2712.85   |
|         |               |           | Max. Mx          | 20    | -8484.62  | 283780.96  | -6518.28   |
|         |               |           | Max. My          | 2     | -8410.51  | 78.90      | 311939.89  |
|         |               |           | Max. Vy          | 20    | -11075.34 | 283780.96  | -6518.28   |
|         |               |           | Max. Vx          | 2     | -11839.71 | 78.90      | 311939.89  |
|         |               |           | Max. Torque      | 21    |           |            | 2794.23    |
| L2      | 97.25 - 48.25 | Pole      | Max Tension      | 1     | 0.00      | 0.00       | 0.00       |
|         |               |           | Max. Compression | 26    | -25692.19 | 339.11     | -3067.01   |
|         |               |           | Max. Mx          | 20    | -16526.92 | 895609.34  | -12913.83  |
|         |               |           | Max. My          | 2     | -16486.56 | 100.18     | 960037.53  |
|         |               |           | Max. Vy          | 20    | -14693.38 | 895609.34  | -12913.83  |
|         |               |           | Max. Vx          | 2     | -15454.51 | 100.18     | 960037.53  |
|         |               |           | Max. Torque      | 21    |           |            | 2835.77    |
| L3      | 48.25 - 1     | Pole      | Max Tension      | 1     | 0.00      | 0.00       | 0.00       |
|         |               |           | Max. Compression | 26    | -42804.22 | 463.42     | -3449.42   |
|         |               |           | Max. Mx          | 20    | -30428.42 | 1781687.95 | -19890.26  |
|         |               |           | Max. My          | 2     | -30427.43 | 124.01     | 1886066.63 |
|         |               |           | Max. Vy          | 20    | -18545.51 | 1781687.95 | -19890.26  |
|         |               |           | Max. Vx          | 2     | -19282.94 | 124.01     | 1886066.63 |
|         |               |           | Max. Torque      | 21    |           |            | 2886.89    |

# **Maximum Reactions**

| Location | Condition           | Gov.  | Vertical    | Horizontal, X | Horizontal, 2 |
|----------|---------------------|-------|-------------|---------------|---------------|
|          |                     | Load  | lb          | lb            | lb            |
|          |                     | Comb. |             |               |               |
| Pole     | Max. Vert           | 33    | 42804.22    | 0.00          | -5470.74      |
|          | Max. H <sub>x</sub> | 20    | 30438.30    | 18529.30      | -126.51       |
|          | Max. H <sub>z</sub> | 2     | 30438.30    | 0.00          | 19265.78      |
|          | $Max. M_x$          | 2     | 1886066.63  | 0.00          | 19265.78      |
|          | Max. M <sub>z</sub> | 8     | 1781438.56  | -18529.30     | -126.51       |
|          | Max. Torsion        | 21    | 2886.92     | 18529.30      | -126.51       |
|          | Min. Vert           | 11    | 22828.72    | -15926.82     | -9725.51      |
|          | Min. H <sub>x</sub> | 8     | 30438.30    | -18529.30     | -126.51       |
|          | Min. H <sub>z</sub> | 14    | 30438.30    | 0.00          | -18981.13     |
|          | Min. M <sub>x</sub> | 14    | -1848322.55 | 0.00          | -18981.13     |
|          | Min. M <sub>z</sub> | 20    | -1781687.96 | 18529.30      | -126.51       |
|          | Min. Torsion        | 9     | -2886.91    | -18529.30     | -126.51       |

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| Job     |                | Page              |
|---------|----------------|-------------------|
|         | CTL02638       | 15 of 20          |
| Project |                | Date              |
|         |                | 12:41:35 05/02/22 |
| Client  |                | Designed by       |
|         | Smartlink/AT&T | LA                |

# **Tower Mast Reaction Summary**

| Load<br>Combination                             | Vertical | $Shear_x$ | $Shear_z$ | Overturning Moment, $M_x$ | Overturning Moment, $M_z$ | Torque   |
|---|----------|-----------|-----------|---------------------------|---------------------------|----------|
|   | lb       | lb        | lb        | lb-ft                     | lb-ft                     | lb-ft    |
| Dead Only                                       | 25365.25 | 0.00      | 0.00      | 1320.54                   | 100.85                    | 0.00     |
| 1.2 Dead+1.0 Wind 0 deg - No<br>Ice             | 30438.30 | -0.00     | -19265.78 | -1886066.63               | 123.95                    | -350.52  |
| 0.9 Dead+1.0 Wind 0 deg - No<br>Ice             | 22828.72 | -0.00     | -19265.78 | -1873993.37               | 91.99                     | -350.83  |
| 1.2 Dead+1.0 Wind 30 deg - No Ice               | 30438.30 | 9174.29   | -16821.44 | -1652918.76               | -877561.62                | 256.19   |
| 0.9 Dead+1.0 Wind 30 deg - No<br>Ice            | 22828.72 | 9174.29   | -16821.44 | -1642364.36               | -871860.83                | 260.16   |
| 1.2 Dead+1.0 Wind 60 deg - No Ice               | 30438.30 | 15845.49  | -9996.61  | -994754.93                | -1513664.48               | 1272.93  |
| 0.9 Dead+1.0 Wind 60 deg - No<br>Ice            | 22828.72 | 15845.49  | -9996.61  | -988518.26                | -1503815.88               | 1280.09  |
| 1.2 Dead+1.0 Wind 90 deg - No                   | 30438.30 | 18529.30  | 126.51    | 19889.81                  | -1781438.56               | 2878.29  |
| Ice<br>0.9 Dead+1.0 Wind 90 deg - No<br>Ice     | 22828.72 | 18529.30  | 126.51    | 19323.83                  | -1769798.73               | 2886.91  |
| 1.2 Dead+1.0 Wind 120 deg -                     | 30438.30 | 15926.82  | 9725.51   | 958912.13                 | -1525417.37               | 2576.15  |
| No Ice<br>0.9 Dead+1.0 Wind 120 deg -<br>No Ice | 22828.72 | 15926.82  | 9725.51   | 952132.67                 | -1515475.64               | 2583.62  |
| 1.2 Dead+1.0 Wind 150 deg -<br>No Ice           | 30438.30 | 9106.51   | 16527.75  | 1613862.99                | -867809.70                | 1534.13  |
| 0.9 Dead+1.0 Wind 150 deg -<br>No Ice           | 22828.72 | 9106.51   | 16527.75  | 1602788.56                | -862183.72                | 1538.48  |
| 1.2 Dead+1.0 Wind 180 deg -<br>No Ice           | 30438.30 | -0.00     | 18981.13  | 1848322.55                | 123.98                    | 350.61   |
| 0.9 Dead+1.0 Wind 180 deg -<br>No Ice           | 22828.72 | -0.00     | 18981.13  | 1835719.01                | 92.02                     | 350.91   |
| 1.2 Dead+1.0 Wind 210 deg -<br>No Ice           | 30438.30 | -9106.51  | 16527.75  | 1613863.52                | 868058.01                 | -926.83  |
| 0.9 Dead+1.0 Wind 210 deg -<br>No Ice           | 22828.72 | -9106.51  | 16527.75  | 1602789.33                | 862368.19                 | -930.68  |
| 1.2 Dead+1.0 Wind 240 deg -<br>No Ice           | 30438.30 | -15926.82 | 9725.51   | 958912.66                 | 1525666.39                | -2225.51 |
| 0.9 Dead+1.0 Wind 240 deg -<br>No Ice           | 22828.72 | -15926.82 | 9725.51   | 952133.06                 | 1515660.45                | -2232.67 |
| 1.2 Dead+1.0 Wind 270 deg -<br>No Ice           | 30438.30 | -18529.30 | 126.51    | 19889.80                  | 1781687.96                | -2878.30 |
| 0.9 Dead+1.0 Wind 270 deg -<br>No Ice           | 22828.72 | -18529.30 | 126.51    | 19323.82                  | 1769983.82                | -2886.92 |
| 1.2 Dead+1.0 Wind 300 deg -<br>No Ice           | 30438.30 | -15845.49 | -9996.61  | -994755.45                | 1513913.48                | -1623.47 |
| 0.9 Dead+1.0 Wind 300 deg -<br>No Ice           | 22828.72 | -15845.49 | -9996.61  | -988518.65                | 1504000.68                | -1630.95 |
| 1.2 Dead+1.0 Wind 330 deg -<br>No Ice           | 30438.30 | -9174.29  | -16821.44 | -1652919.29               | 877809.87                 | -863.31  |
| 0.9 Dead+1.0 Wind 330 deg -<br>No Ice           | 22828.72 | -9174.29  | -16821.44 | -1642364.76               | 872045.07                 | -867.82  |
| 1.2 Dead+1.0 Ice+1.0 Temp                       | 42804.22 | -0.00     | 0.00      | 3449.42                   | 463.42                    | 0.02     |
| 1.2 Dead+1.0 Wind 0 deg+1.0                     | 42804.22 | -0.00     | -5524.13  | -528248.13                | 473.14                    | -326.06  |
| Ice+1.0 Temp<br>1.2 Dead+1.0 Wind 30 deg+1.0    | 42804.22 | 2676.05   | -4809.70  | -460778.79                | -252758.54                | -67.99   |
| Ice+1.0 Temp 1.2 Dead+1.0 Wind 60 deg+1.0       | 42804.22 | 4626.64   | -2830.29  | -272398.48                | -436900.37                | 298.24   |
| Ice+1.0 Temp                                    |          |           |           |                           |                           |          |
| 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp       | 42804.22 | 5386.00   | 23.73     | 7021.77                   | -510980.12                | 757.41   |

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| Job     | CTL02638       | Page 16 of 20             |
|---------|----------------|---------------------------|
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Load<br>Combination         | Vertical | $Shear_x$ | $Shear_z$ | Overturning<br>Moment, M <sub>x</sub> | Overturning<br>Moment, M <sub>z</sub> | Torque  |
|-----------------------------|----------|-----------|-----------|---------------------------------------|---------------------------------------|---------|
|                             | lb       | lb        | lb        | lb-ft                                 | lb-ft                                 | lb-ft   |
| 1.2 Dead+1.0 Wind 120       | 42804.22 | 4641.90   | 2779.44   | 271976.67                             | -439145.63                            | 801.08  |
| deg+1.0 Ice+1.0 Temp        |          |           |           |                                       |                                       |         |
| 1.2 Dead+1.0 Wind 150       | 42804.22 | 2663.34   | 4754.61   | 459734.44                             | -250888.57                            | 621.34  |
| deg+1.0 Ice+1.0 Temp        |          |           |           |                                       |                                       |         |
| 1.2 Dead+1.0 Wind 180       | 42804.22 | -0.00     | 5470.74   | 527453.36                             | 473.13                                | 326.11  |
| deg+1.0 Ice+1.0 Temp        |          |           |           |                                       |                                       |         |
| 1.2 Dead+1.0 Wind 210       | 42804.22 | -2663.34  | 4754.61   | 459734.66                             | 251834.98                             | -56.50  |
| deg+1.0 Ice+1.0 Temp        |          |           |           |                                       |                                       |         |
| 1.2 Dead+1.0 Wind 240       | 42804.22 | -4641.90  | 2779.44   | 271976.89                             | 440092.33                             | -474.98 |
| deg+1.0 Ice+1.0 Temp        |          |           |           |                                       |                                       |         |
| 1.2 Dead+1.0 Wind 270       | 42804.22 | -5386.00  | 23.73     | 7021.76                               | 511926.97                             | -757.39 |
| deg+1.0 Ice+1.0 Temp        |          |           |           |                                       |                                       |         |
| 1.2 Dead+1.0 Wind 300       | 42804.22 | -4626.64  | -2830.29  | -272398.71                            | 437847.07                             | -624.24 |
| deg+1.0 Ice+1.0 Temp        |          |           |           |                                       |                                       |         |
| 1.2 Dead+1.0 Wind 330       | 42804.22 | -2676.05  | -4809.70  | -460779.02                            | 253704.96                             | -496.74 |
| deg+1.0 Ice+1.0 Temp        |          |           |           |                                       |                                       |         |
| Dead+Wind 0 deg - Service   | 25365.25 | -0.00     | -4386.32  | -426850.71                            | 103.46                                | -80.01  |
| Dead+Wind 30 deg - Service  | 25365.25 | 2088.85   | -3829.78  | -373950.81                            | -199017.72                            | 60.60   |
| Dead+Wind 60 deg - Service  | 25365.25 | 3607.79   | -2275.89  | -224630.11                            | -343320.30                            | 293.98  |
| Dead+Wind 90 deg - Service  | 25365.25 | 4218.80   | 28.78     | 5493.24                               | -404045.32                            | 658.05  |
| Dead+Wind 120 deg - Service | 25365.25 | 3626.29   | 2214.23   | 218492.06                             | -345977.93                            | 587.93  |
| Dead+Wind 150 deg - Service | 25365.25 | 2073.43   | 3762.98   | 367075.30                             | -196803.70                            | 349.80  |
| Dead+Wind 180 deg - Service | 25365.25 | -0.00     | 4321.58   | 420270.57                             | 103.46                                | 80.02   |
| Dead+Wind 210 deg - Service | 25365.25 | -2073.43  | 3762.98   | 367075.32                             | 197010.64                             | -211.20 |
| Dead+Wind 240 deg - Service | 25365.25 | -3626.29  | 2214.23   | 218492.08                             | 346184.89                             | -507.92 |
| Dead+Wind 270 deg - Service | 25365.25 | -4218.80  | 28.78     | 5493.24                               | 404252.30                             | -658.05 |
| Dead+Wind 300 deg - Service | 25365.25 | -3607.79  | -2275.89  | -224630.13                            | 343527.26                             | -373.98 |
| Dead+Wind 330 deg - Service | 25365.25 | -2088.85  | -3829.78  | -373950.84                            | 199224.65                             | -199.18 |

# **Solution Summary**

|       | Sur       | n of Applied Force: | S         |           | Sum of Reaction       | ıs        |         |
|-------|-----------|---------------------|-----------|-----------|-----------------------|-----------|---------|
| Load  | PX        | PY                  | PZ        | PX        | $\overset{\circ}{P}Y$ | PZ        | % Error |
| Comb. | lb        | lb                  | lb        | lb        | lb                    | lb        |         |
| 1     | 0.00      | -25365.25           | 0.00      | 0.00      | 25365.25              | -0.00     | 0.000%  |
| 2     | 0.00      | -30438.30           | -19265.78 | 0.00      | 30438.30              | 19265.78  | 0.000%  |
| 3     | 0.00      | -22828.72           | -19265.78 | 0.00      | 22828.72              | 19265.78  | 0.000%  |
| 4     | 9174.29   | -30438.30           | -16821.44 | -9174.29  | 30438.30              | 16821.44  | 0.000%  |
| 5     | 9174.29   | -22828.72           | -16821.44 | -9174.29  | 22828.72              | 16821.44  | 0.000%  |
| 6     | 15845.49  | -30438.30           | -9996.61  | -15845.49 | 30438.30              | 9996.61   | 0.000%  |
| 7     | 15845.49  | -22828.72           | -9996.61  | -15845.49 | 22828.72              | 9996.61   | 0.000%  |
| 8     | 18529.30  | -30438.30           | 126.51    | -18529.30 | 30438.30              | -126.51   | 0.000%  |
| 9     | 18529.30  | -22828.72           | 126.51    | -18529.30 | 22828.72              | -126.51   | 0.000%  |
| 10    | 15926.82  | -30438.30           | 9725.51   | -15926.82 | 30438.30              | -9725.51  | 0.000%  |
| 11    | 15926.82  | -22828.72           | 9725.51   | -15926.82 | 22828.72              | -9725.51  | 0.000%  |
| 12    | 9106.51   | -30438.30           | 16527.75  | -9106.51  | 30438.30              | -16527.75 | 0.000%  |
| 13    | 9106.51   | -22828.72           | 16527.75  | -9106.51  | 22828.72              | -16527.75 | 0.000%  |
| 14    | 0.00      | -30438.30           | 18981.13  | 0.00      | 30438.30              | -18981.13 | 0.000%  |
| 15    | 0.00      | -22828.72           | 18981.13  | 0.00      | 22828.72              | -18981.13 | 0.000%  |
| 16    | -9106.51  | -30438.30           | 16527.75  | 9106.51   | 30438.30              | -16527.75 | 0.000%  |
| 17    | -9106.51  | -22828.72           | 16527.75  | 9106.51   | 22828.72              | -16527.75 | 0.000%  |
| 18    | -15926.82 | -30438.30           | 9725.51   | 15926.82  | 30438.30              | -9725.51  | 0.000%  |
| 19    | -15926.82 | -22828.72           | 9725.51   | 15926.82  | 22828.72              | -9725.51  | 0.000%  |
| 20    | -18529.30 | -30438.30           | 126.51    | 18529.30  | 30438.30              | -126.51   | 0.000%  |
| 21    | -18529.30 | -22828.72           | 126.51    | 18529.30  | 22828.72              | -126.51   | 0.000%  |
| 22    | -15845.49 | -30438.30           | -9996.61  | 15845.49  | 30438.30              | 9996.61   | 0.000%  |
| 23    | -15845.49 | -22828.72           | -9996.61  | 15845.49  | 22828.72              | 9996.61   | 0.000%  |
| 24    | -9174.29  | -30438.30           | -16821.44 | 9174.29   | 30438.30              | 16821.44  | 0.000%  |
|       |           |                     |           |           |                       |           |         |

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Schaumburg, IL 60173 Phone: (847) 908-8400 FAX: (847) 413-4733

| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 17 of 20                  |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

|       | Sui      | n of Applied Forces | S         |          | Sum of Reaction | S        |         |
|-------|----------|---------------------|-----------|----------|-----------------|----------|---------|
| Load  | PX       | PY                  | PZ        | PX       | PY              | PZ       | % Error |
| Comb. | lb       | lb                  | lb        | lb       | lb              | lb       |         |
| 25    | -9174.29 | -22828.72           | -16821.44 | 9174.29  | 22828.72        | 16821.44 | 0.000%  |
| 26    | 0.00     | -42804.22           | 0.00      | 0.00     | 42804.22        | -0.00    | 0.000%  |
| 27    | 0.00     | -42804.22           | -5524.09  | 0.00     | 42804.22        | 5524.13  | 0.000%  |
| 28    | 2676.03  | -42804.22           | -4809.65  | -2676.05 | 42804.22        | 4809.70  | 0.000%  |
| 29    | 4626.61  | -42804.22           | -2830.26  | -4626.64 | 42804.22        | 2830.29  | 0.000%  |
| 30    | 5385.95  | -42804.22           | 23.73     | -5386.00 | 42804.22        | -23.73   | 0.000%  |
| 31    | 4641.86  | -42804.22           | 2779.42   | -4641.90 | 42804.22        | -2779.44 | 0.000%  |
| 32    | 2663.32  | -42804.22           | 4754.57   | -2663.34 | 42804.22        | -4754.61 | 0.000%  |
| 33    | 0.00     | -42804.22           | 5470.70   | 0.00     | 42804.22        | -5470.74 | 0.000%  |
| 34    | -2663.32 | -42804.22           | 4754.57   | 2663.34  | 42804.22        | -4754.61 | 0.000%  |
| 35    | -4641.86 | -42804.22           | 2779.42   | 4641.90  | 42804.22        | -2779.44 | 0.000%  |
| 36    | -5385.95 | -42804.22           | 23.73     | 5386.00  | 42804.22        | -23.73   | 0.000%  |
| 37    | -4626.61 | -42804.22           | -2830.26  | 4626.64  | 42804.22        | 2830.29  | 0.000%  |
| 38    | -2676.03 | -42804.22           | -4809.65  | 2676.05  | 42804.22        | 4809.70  | 0.000%  |
| 39    | 0.00     | -25365.25           | -4386.32  | 0.00     | 25365.25        | 4386.32  | 0.000%  |
| 40    | 2088.85  | -25365.25           | -3829.78  | -2088.85 | 25365.25        | 3829.78  | 0.000%  |
| 41    | 3607.79  | -25365.25           | -2275.89  | -3607.79 | 25365.25        | 2275.89  | 0.000%  |
| 42    | 4218.80  | -25365.25           | 28.78     | -4218.80 | 25365.25        | -28.78   | 0.000%  |
| 43    | 3626.29  | -25365.25           | 2214.23   | -3626.29 | 25365.25        | -2214.23 | 0.000%  |
| 44    | 2073.43  | -25365.25           | 3762.98   | -2073.43 | 25365.25        | -3762.98 | 0.000%  |
| 45    | 0.00     | -25365.25           | 4321.58   | 0.00     | 25365.25        | -4321.58 | 0.000%  |
| 46    | -2073.43 | -25365.25           | 3762.98   | 2073.43  | 25365.25        | -3762.98 | 0.000%  |
| 47    | -3626.29 | -25365.25           | 2214.23   | 3626.29  | 25365.25        | -2214.23 | 0.000%  |
| 48    | -4218.80 | -25365.25           | 28.78     | 4218.80  | 25365.25        | -28.78   | 0.000%  |
| 49    | -3607.79 | -25365.25           | -2275.89  | 3607.79  | 25365.25        | 2275.89  | 0.000%  |
| 50    | -2088.85 | -25365.25           | -3829.78  | 2088.85  | 25365.25        | 3829.78  | 0.000%  |

# **Non-Linear Convergence Results**

| Load        | Converged? | Number    | Displacement | Force      |
|-------------|------------|-----------|--------------|------------|
| Combination |            | of Cycles | Tolerance    | Tolerance  |
| 1           | Yes        | 4         | 0.00000001   | 0.00000001 |
| 2           | Yes        | 4         | 0.00000001   | 0.00005180 |
| 3           | Yes        | 4         | 0.00000001   | 0.00002924 |
| 4           | Yes        | 5         | 0.00000001   | 0.00005754 |
| 5           | Yes        | 5         | 0.00000001   | 0.00002661 |
| 6           | Yes        | 5         | 0.00000001   | 0.00005469 |
| 7           | Yes        | 5         | 0.00000001   | 0.00002529 |
| 8           | Yes        | 4         | 0.00000001   | 0.00052584 |
| 9           | Yes        | 4         | 0.00000001   | 0.00034353 |
| 10          | Yes        | 5         | 0.00000001   | 0.00006211 |
| 11          | Yes        | 5         | 0.00000001   | 0.00002905 |
| 12          | Yes        | 5         | 0.00000001   | 0.00004956 |
| 13          | Yes        | 4         | 0.00000001   | 0.00099391 |
| 14          | Yes        | 4         | 0.00000001   | 0.00005095 |
| 15          | Yes        | 4         | 0.00000001   | 0.00002894 |
| 16          | Yes        | 5         | 0.00000001   | 0.00005067 |
| 17          | Yes        | 5         | 0.00000001   | 0.00002340 |
| 18          | Yes        | 5         | 0.00000001   | 0.00006137 |
| 19          | Yes        | 5         | 0.00000001   | 0.00002867 |
| 20          | Yes        | 4         | 0.00000001   | 0.00052597 |
| 21          | Yes        | 4         | 0.00000001   | 0.00034358 |
| 22          | Yes        | 5         | 0.00000001   | 0.00005442 |
| 23          | Yes        | 5         | 0.00000001   | 0.00002516 |
| 24          | Yes        | 5         | 0.00000001   | 0.00005899 |
| 25          | Yes        | 5         | 0.00000001   | 0.00002732 |

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FAX: (847) 413-4733

| Job     | CTL02638       | Page 18 of 20             |
|---------|----------------|---------------------------|
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| 26 | Yes | 4 | 0.00000001 | 0.00000853 |
|----|-----|---|------------|------------|
| 27 | Yes | 4 | 0.00000001 | 0.00060302 |
| 28 | Yes | 4 | 0.00000001 | 0.00066346 |
| 29 | Yes | 4 | 0.0000001  | 0.00065241 |
| 30 | Yes | 4 | 0.00000001 | 0.00058665 |
| 31 | Yes | 4 | 0.00000001 | 0.00066970 |
| 32 | Yes | 4 | 0.00000001 | 0.00066443 |
| 33 | Yes | 4 | 0.00000001 | 0.00060837 |
| 34 | Yes | 4 | 0.00000001 | 0.00066685 |
| 35 | Yes | 4 | 0.00000001 | 0.00066871 |
| 36 | Yes | 4 | 0.00000001 | 0.00058840 |
| 37 | Yes | 4 | 0.0000001  | 0.00065428 |
| 38 | Yes | 4 | 0.00000001 | 0.00066838 |
| 39 | Yes | 4 | 0.00000001 | 0.00000001 |
| 40 | Yes | 4 | 0.00000001 | 0.00002775 |
| 41 | Yes | 4 | 0.00000001 | 0.00002487 |
| 42 | Yes | 4 | 0.00000001 | 0.00002802 |
| 43 | Yes | 4 | 0.00000001 | 0.00004063 |
| 44 | Yes | 4 | 0.00000001 | 0.00002144 |
| 45 | Yes | 4 | 0.00000001 | 0.00000001 |
| 46 | Yes | 4 | 0.0000001  | 0.00002170 |
| 47 | Yes | 4 | 0.00000001 | 0.00003893 |
| 48 | Yes | 4 | 0.0000001  | 0.00002805 |
| 49 | Yes | 4 | 0.00000001 | 0.00002534 |
| 50 | Yes | 4 | 0.00000001 | 0.00003037 |
|    |     |   |            |            |

# **Maximum Tower Deflections - Service Wind**

| Section | Elevation      | Horz.      | Gov.  | Tilt   | Twist  |
|---------|----------------|------------|-------|--------|--------|
| No.     |                | Deflection | Load  |        |        |
|         | ft             | in         | Comb. | ۰      | 0      |
| L1      | 150 - 97.25    | 14.042     | 39    | 0.7792 | 0.0082 |
| L2      | 101.75 - 48.25 | 6.606      | 39    | 0.6323 | 0.0028 |
| L3      | 54.25 - 1      | 1.798      | 39    | 0.3122 | 0.0008 |
|         |                |            |       |        |        |

# **Critical Deflections and Radius of Curvature - Service Wind**

| Elevation | Appurtenance           | Gov.  | Deflection | Tilt   | Twist  | Radius of |
|-----------|------------------------|-------|------------|--------|--------|-----------|
|           |                        | Load  |            |        |        | Curvature |
| ft        |                        | Comb. | in         | ۰      | 0      | ft        |
| 149.00    | 20' Omni               | 39    | 13.878     | 0.7770 | 0.0081 | 92604     |
| 141.00    | 6' Dish w/ Shroud (HP) | 39    | 12.569     | 0.7607 | 0.0071 | 51447     |
| 133.00    | 10' Omni               | 39    | 11.275     | 0.7429 | 0.0061 | 27236     |
| 122.00    | RRUS-4449 B5/B12       | 39    | 9.543      | 0.7133 | 0.0048 | 16536     |

# **Maximum Tower Deflections - Design Wind**

| Section | Elevation   | Horz.      | Gov.  | Tilt   | Twist  |
|---------|-------------|------------|-------|--------|--------|
| No.     |             | Deflection | Load  |        |        |
|         | ft          | in         | Comb. | 0      | 0      |
| L1      | 150 - 97.25 | 62.320     | 2     | 3.4775 | 0.0359 |

#### Page Job *tnxTower* 19 of 20 CTL02638 **Project** Fullerton Engineering, P.C. 12:41:35 05/02/22 1100 E. Woodfield Road, Suite 500 Schaumburg, IL 60173 Client

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|----------------|------|--------|--|---------------|
|                |      |        |  |               |
| Tilt           | Gov. | Horz.  | Elevation  | Section<br>No |

RRUS-4449 B5/B12

122.00

| Section | Elevation      | Horz.      | Gov.  | Tilt   | Twist  |
|---------|----------------|------------|-------|--------|--------|
| No.     |                | Deflection | Load  |        |        |
|         | ft             | in         | Comb. | 0      | 0      |
| L2      | 101.75 - 48.25 | 29.250     | 2     | 2.8041 | 0.0123 |
| L3      | 54.25 - 1      | 7.954      | 2     | 1.3815 | 0.0037 |

#### Critical Deflections and Radius of Curvature - Design Wind Elevation Gov. Deflection Appurtenance TiltTwist Radius of LoadCurvature ft Comb. 149.00 21003 20' Omni 2 2 61.590 3.4681 0.0353 141.00 6' Dish w/ Shroud (HP) 55.764 3.3913 0.0308 11668 133.00 10' Omni 2 3.3077 6176 50.0040.0265

42.301

3.1709

0.0208

3748

|           |           | Base Plate Design Data |           |             |           |           |             |       |  |
|-----------|-----------|------------------------|-----------|-------------|-----------|-----------|-------------|-------|--|
| Plate     | Number    | Anchor Bolt            | Actual    | Actual      | Actual    | Actual    | Controlling | Ratio |  |
| Thickness | of Anchor | Size                   | Allowable | Allowable   | Allowable | Allowable | Condition   |       |  |
|           | Bolts     |                        | Ratio     | Ratio       | Ratio     | Ratio     |             |       |  |
|           |           |                        | Bolt      | Bolt        | Plate     | Stiffener |             |       |  |
|           |           |                        | Tension   | Compression | Stress    | Stress    |             |       |  |
| in        |           | in                     | lb        | lb          | ksi       | ksi       |             |       |  |
| 2.5000    | 14        | 2.2500                 | 105593.88 | 109940.66   | 19.259    |           | Plate       | 0.43  |  |
|           |           |                        | 292291.37 | 485203.68   | 45.000    |           |             | ~     |  |
|           |           |                        | 0.36      | 0.23        | 0.43      |           |             | •     |  |

# **Compression Checks**

|                | Pole Design Data     |                        |       |       |      |         |           |            |                         |  |
|----------------|----------------------|------------------------|-------|-------|------|---------|-----------|------------|-------------------------|--|
| Section<br>No. | Elevation            | Size                   | L     | $L_u$ | Kl/r | A       | $P_u$     | $\phi P_n$ | Ratio<br>P <sub>u</sub> |  |
| 110.           | ft                   |                        | ft    | ft    |      | $in^2$  | lb        | lb         | $\frac{1}{\phi P_n}$    |  |
| L1             | 150 - 97.25 (1)      | TP31.76x20x0.25        | 52.75 | 0.00  | 0.0  | 24.2071 | -8410.51  | 1416120.00 | 0.006                   |  |
| L2             | 97.25 - 48.25<br>(2) | TP42.19x30.2568x0.3125 | 53.50 | 0.00  | 0.0  | 40.2098 | -16486.60 | 2352270.00 | 0.007                   |  |
| L3             | 48.25 - 1 (3)        | TP52.1x40.2267x0.375   | 53.25 | 0.00  | 0.0  | 61.5657 | -30427.40 | 3601590.00 | 0.008                   |  |

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| Job     |                | Page                      |
|---------|----------------|---------------------------|
|         | CTL02638       | 20 of 20                  |
| Project |                | Date<br>12:41:35 05/02/22 |
| Client  | Smartlink/AT&T | Designed by LA            |

| Pole E | Bending | Design | Data |
|--------|---------|--------|------|
|--------|---------|--------|------|

| Section | Elevation            | Size                   | $M_{ux}$   | $\phi M_{nx}$ | Ratio         | $M_{uy}$ | $\phi M_{ny}$ | Ratio         |
|---------|----------------------|------------------------|------------|---------------|---------------|----------|---------------|---------------|
| No.     |                      |                        |            |               | $M_{ux}$      |          |               | $M_{uy}$      |
|         | ft                   |                        | lb-ft      | lb-ft         | $\phi M_{nx}$ | lb-ft    | lb-ft         | $\phi M_{nv}$ |
| L1      | 150 - 97.25 (1)      | TP31.76x20x0.25        | 311940.00  | 1051575.00    | 0.297         | 0.00     | 1051575.00    | 0.000         |
| L2      | 97.25 - 48.25<br>(2) | TP42.19x30.2568x0.3125 | 960041.67  | 2274216.67    | 0.422         | 0.00     | 2274216.67    | 0.000         |
| L3      | 48.25 - 1 (3)        | TP52.1x40.2267x0.375   | 1886066.67 | 4344708.33    | 0.434         | 0.00     | 4344708.33    | 0.000         |

# Pole Shear Design Data

| Section<br>No. | Elevation            | Size                   | $Actual$ $V_u$ | $\phi V_n$ | $Ratio$ $V_u$        | Actual<br>T <sub>u</sub> | $\phi T_n$ | Ratio<br>T <sub>u</sub> |
|----------------|----------------------|------------------------|----------------|------------|----------------------|--------------------------|------------|-------------------------|
| 1,0.           | ft                   |                        | lb             | lb         | $\frac{-}{\phi V_n}$ | lb-ft                    | lb-ft      | $\phi T_n$              |
| L1             | 150 - 97.25 (1)      | TP31.76x20x0.25        | 11839.70       | 424835.00  | 0.028                | 181.41                   | 1135000.00 | 0.000                   |
| L2             | 97.25 - 48.25<br>(2) | TP42.19x30.2568x0.3125 | 15454.50       | 705682.00  | 0.022                | 259.31                   | 2505325.00 | 0.000                   |
| L3             | 48.25 - 1 (3)        | TP52.1x40.2267x0.375   | 19282.90       | 1080480.00 | 0.018                | 350.52                   | 4894366.67 | 0.000                   |

# **Pole Interaction Design Data**

| Section<br>No. | Elevation            | Ratio $P_u$ | Ratio $M_{ux}$ | $Ratio$ $M_{uy}$ | $Ratio$ $V_u$ | Ratio $T_u$ | Comb.<br>Stress | Allow.<br>Stress | Criteria |
|----------------|----------------------|-------------|----------------|------------------|---------------|-------------|-----------------|------------------|----------|
|                | ft                   | $\phi P_n$  | $\phi M_{nx}$  | $\phi M_{ny}$    | $\phi V_n$    | $\phi T_n$  | Ratio           | Ratio            |          |
| L1             | 150 - 97.25 (1)      | 0.006       | 0.297          | 0.000            | 0.028         | 0.000       | 0.303           | 1.000            | 4.8.2    |
| L2             | 97.25 - 48.25<br>(2) | 0.007       | 0.422          | 0.000            | 0.022         | 0.000       | 0.430           | 1.000            | 4.8.2    |
| L3             | 48.25 - 1 (3)        | 0.008       | 0.434          | 0.000            | 0.018         | 0.000       | 0.443           | 1.000            | 4.8.2    |

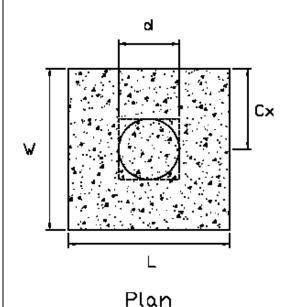
# **Section Capacity Table**

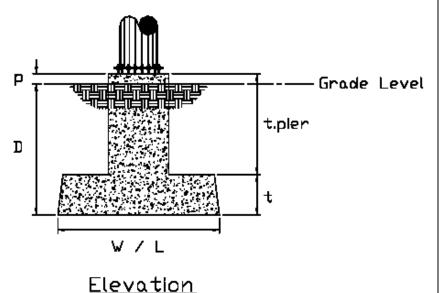
| Section<br>No. | Elevation<br>ft | Component<br>Type | Size                   | Critical<br>Element | P<br>lb   | $\phi P_{allow} \ lb$ | %<br>Capacity | Pass<br>Fail |
|----------------|-----------------|-------------------|------------------------|---------------------|-----------|-----------------------|---------------|--------------|
| L1             | 150 - 97.25     | Pole              | TP31.76x20x0.25        | 1                   | -8410.51  | 1416120.00            | 30.3          | Pass         |
| L2             | 97.25 - 48.25   | Pole              | TP42.19x30.2568x0.3125 | 2                   | -16486.60 | 2352270.00            | 43.0          | Pass         |
| L3             | 48.25 - 1       | Pole              | TP52.1x40.2267x0.375   | 3                   | -30427.40 | 3601590.00            | 44.3          | Pass         |
|                |                 |                   |                        |                     |           |                       | Summary       |              |
|                |                 |                   |                        |                     |           | Pole (L3)             | 44.3          | Pass         |
|                |                 |                   |                        |                     |           | Base Plate            | 42.8          | Pass         |
|                |                 |                   |                        |                     |           | RATING =              | 44.3          | Pass         |

 $t_{pier} = 5 ft$ 

Site No.: CTL02638 Prepared By: LA Checked By: BK

# Monopole Foundation - Pad & Pier





#### Pad & Pier Dimensions

W := 25.5 ft

L = 25.5 ft

d := 7ft

 $Cx := 12.75 \, ft$ 

p := 6in

D := 6.5 ft

t := 2ft

 $t_{pier} := D + p - t$ 

 $f_c := 4 \cdot ksi$ 

Pier Shape := "Circular" ○ "Square"

Width of Pad

Length of Pad

Diameter of Pier

Minimum distance to center of gravity of tower from outer edge (based on foundation drawings)

Projection of Pier above grade

Depth from grade to the bottom of foundation

Thickness of Pad

Length of Pier

Concrete compressive strength

Site Name: STRATFORD ORONOQUE ROAD

**Fullerton Engineering, P.C.** 

Site No.: CTL02638 Prepared By: LA Checked By: BK

**Tower Reactions** 

 $M_{u} := 18860671bf \cdot ft$  Factored moment reaction

P<sub>u</sub> := 304381bf Factored download reaction

V<sub>u</sub> := 192661bf Factored shear reaction

Soil Properties

 $\gamma_{\text{soil}} := 125 \text{pcf}$ 

 $\gamma_{H20} \coloneqq 62.4pcf$ 

Bearing := 5.2ksf Ultimate bearing pressure

Bearing<sub>Ult</sub> := Bearing Bearing<sub>Ult</sub> =  $5.2 \cdot \text{ksf}$  Ultimate bearing pressure

φ<sub>soil</sub> := 30deg

Angle of internal friction

P<sub>p</sub> := 100psf Passive pressure (conservatively assumed)

 $\mu := 0.25$  Coefficient of friction

H<sub>water</sub> := 4ft Depth of water table

 $H_{\text{frost}} := 3 \text{ ft}$ 

Frost depth

 $\gamma_{\rm conc} := 150 {\rm pcf}$ 

 $\varphi_b := 0.75$  Soil resistance factor for bearing per TIA-222-H Section 9.7

 $\varphi_u \coloneqq 0.75$  Soil resistance factor for uplift per

TIA-222-H Section 9.7

 $\phi_o := 0.75$  Soil resistance factor for overturning

per TIA-222-H Section 9.7

Soil resistance factor for lateral

 $\phi_l := 0.75$  Soil resistance factor for lateral load per TIA-222-H Section 9.7

Date: 5/2/2022

# Fullerton Engineering, P.C.

Site No.: CTL02638 Prepared By: LA Checked By: BK

#### **Overturning Calculations**

$$A_{pad} := W \cdot L$$

$$A_{\text{pad}} = 650.25 \text{ ft}^2$$

Area of pad

$$A_{\text{pier}} := \begin{bmatrix} \frac{d^2}{4} & \text{if Pier Shape} = \text{"Circular"} \\ \frac{d^2}{4} & \text{of Pier Shape} = \text{"Circular"} \end{bmatrix}$$

$$A_{pier} = 38.48 \text{ ft}^2$$

Area of pier

$$D_{tpad} := t_{pier} - p$$

$$D_{tpad} = 4.5 \, ft$$

$$y := tan(30deg) \cdot D_{tpad}$$

$$y = 2.6 \, ft$$

•

$$Wt_{pad} \coloneqq 0.9Wt_{pad.nominal}$$

$$Wt_{pad} = 102.53 \cdot kip$$

Factored weight of the concrete pad

Date: 5/2/2022

per TIA-222-H Section 9.4 (bouyancy considered if applicable)

$$Wt_{pier} := 0.9Wt_{pier.nominal}$$

$$Wt_{pier} = 24.9 \cdot kip$$

(bouyancy considered if applicable)

$$V_{soil} := V_{soil.resist}$$

$$V_{soil} = 3220.39 \cdot ft^3$$

overturning

coefficient

$$Wt_{soil} := 0.9Wt_{soil.nominal}$$

$$Wt_{soil} = 344.8 \cdot kip$$

$$K_p := \frac{1 + \sin(\phi_{\text{soil}})}{1 - \sin(\phi_{\text{soil}})}$$

$$K_p = 3$$

(bouyancy considered if applicable)

$$A := H_{water} - H_{frost}$$

$$A = 1 \text{ ft}$$

$$B := D - H_{water}$$

$$B = 2.5 \, ft$$

$$\begin{split} M_{passive \ pressure} \coloneqq & \left[ d \cdot \left[ \gamma_{soil} \cdot K_p \cdot H_{frost} \cdot \left(D - H_{frost}\right) \left(\frac{D - H_{frost}}{2}\right) + 0.5 \gamma_{soil} \cdot K_p \cdot \left(D - H_{frost}\right)^2 \left(\frac{D - H_{frost}}{3}\right) \right] \ if \ H_{water} > D \\ d \cdot \left[ \gamma_{soil} \cdot K_p \cdot H_{frost} \cdot A \left(B + \frac{A}{2}\right) + 0.5 \gamma_{soil} \cdot K_p \cdot \left(A\right)^2 \left(B + \frac{A}{3}\right) \dots \right] \ if \ H_{water} < D \\ + \gamma_{soil} \cdot K_p \cdot H_{water} \cdot B \left(\frac{B}{2}\right) + 0.5 \gamma_{soil\_sub} \cdot K_p \cdot \left(B\right)^2 \left(\frac{B}{3}\right) \end{split}$$

 $M_{passive pressure} = 63.58 \cdot kip \cdot ft$ 

$$M_v := V_u \cdot (D + p)$$

$$M_v = 134.86 \cdot \text{kip} \cdot \text{ft}$$

$$M_{resist} := min(M_{passive pressure}, M_v + M_u)$$

$$M_{resist} = 63.58 \cdot kip \cdot ft$$

$$M_u := M_u + M_v - M_{resist}$$
  $M_u = 1957.35 \cdot kip \cdot ft$ 

#### Check overturning capacity

$$\varphi M_n \coloneqq \left. \varphi_o \cdot \overline{\left( P_u + W t_{pier} \right) \cdot C x + \left( W t_{pad} + W t_{soil} \right) \cdot \frac{min(W,L)}{2}} \right] \\ \qquad \qquad \varphi M_n = 4807 \cdot kip \cdot ft$$

$$\phi M_n = 4807 \cdot kip \cdot ft$$

$$\frac{M_{\rm u}}{\phi M_{\rm n}} = 0.41$$

OverturningCheck = "Foundation is adequate to resist the overturning moment."

#### Soil Bearing Calculations

$$A_{\text{pad}} := W \cdot L$$

$$A_{pad} = 650.25 \text{ ft}^2$$

Area of pad

Apper: 
$$\pi \frac{d^2}{4}$$
 if Pier Shape = "Circular"  $d^2$  if Pier Shape = "Square"

$$A_{pier} = 38.48 \text{ ft}^2$$

Area of pier

$$S := \frac{A_{pad} \cdot min(W, L)}{6}$$

$$S = 2763.56 \cdot ft^3$$

Section modulus of pad base

$$D_{tpad} = t_{pier} - p$$

$$D_{tpad} = 4.5 \, ft$$

Depth of soil to top of pad

$$\label{eq:continuous_problem} \begin{array}{ll} \underset{\longleftarrow}{\text{Vsail}} := \ D_{tpad} \cdot W \cdot L \ - \ D_{tpad} \cdot A_{pier} \end{array}$$

$$V_{soil} = 2752.94 \cdot ft^3$$

Volume of soil above concrete pad

Date: 5/2/2022

$$\underset{soil}{\text{Wt}_{soil}} := V_{soil} \cdot \gamma_{soil}$$

$$Wt_{soil} = 344.12 \cdot kip$$

Weight of soil above concrete pad

$$Wt_{pad} = 32.51 \cdot kip$$

Weight of concrete pad (Bouyancy

 $Wt_{pier} = 7.22 \cdot kip$ 

Weight of concrete pier (Bouyancy conservatively not conssidered)

conservatively not conssidered)

 $Wt_{soils} = 0 \cdot kip$ 

Weight of soil is ignored if Net Bearing Pressure is given

$$Wt_{total} := 1.2Wt_{pad} + 1.2Wt_{pier} + 1.2Wt_{soils}$$

$$Wt_{total} = 47.67 \cdot kip$$

Total factored weight of concrete foundation and soil above pad

#### Check soil bearing capacity

$$\varphi R_s := \varphi_b \cdot Bearing_{Ult}$$

$$\phi R_s = 3.9 \cdot ksf$$

$$R_u \coloneqq \frac{\left(P_u + Wt_{total}\right)}{A_{pad}} + \frac{M_u + \left[P_u \cdot \left(\frac{min(L, W)}{2} - Cx\right)\right]}{S} \qquad R_u = 0.83 \cdot ksf$$

$$R_u = 0.83 \cdot ksf$$

$$\frac{R_{\rm u}}{\Phi R_{\rm s}} = 0.21$$

BearingCheck = "Soil bearing strength is adequate."

#### Lateral Calculations

**.**l.

$$Wt_{pad.nominal} + 0.9Wt_{pier.nominal} + 0.9Wt_{soil.nominal} = 419.96 \cdot kip$$

Total factored weight of foundation per TIA-222-H Section 9.4

Date: 5/2/2022

(bouyancy considered if applicable)

$$\begin{split} P_{resist} \coloneqq & \begin{bmatrix} P_p {\cdot} \min(L,W) {\cdot} (t) & \text{if } D_{tpad} \geq H_{frost} \\ \\ \left[ P_p {\cdot} \min(L,W) {\cdot} \left( D - H_{frost} \right) \right] & \text{otherwise} \\ \end{bmatrix} \end{split}$$

Lateral load resistance provided by

soil passive pressure

$$f := \mu \cdot (P_u + Wt_{total})$$

$$f = 112.6 \cdot kip$$

 $P_{resist} = 5.1 \cdot kip$ 

Lateral load resistance provided by friction force

Check lateral capacity

$$\Phi R_s := \Phi_l \cdot (f + P_{resist})$$

$$\Phi R_s = 88.27 \cdot \text{kip}$$

$$R_u := V_u$$

$$R_u = 19.27 \cdot \text{kip}$$

$$\frac{R_u}{\Phi R_c} = 0.22$$

LateralCheck = "Foundation is adequate to support lateral load."

## Concrete Pad and Pier Bearing Strength Calculations

ACI 318-14 Sections 22.8

$$\underbrace{Wt_{pier}} := t_{pier} \cdot A_{pier} \cdot \gamma_{conc}$$

$$Wt_{pier} = 28.86 \cdot kip$$

Weight of concrete pier (Bouyancy conservatively not considered)

$$A_1 := A_{pier}$$

$$A_1 = 38.48 \text{ ft}^2$$

$$A_2 \coloneqq min \!\! \left[ \frac{\left(d+4t\right)^2}{4} \! \cdot \! \pi, \frac{min(L,W)^2}{4} \! \cdot \! \pi \right]$$

$$A_2 = 176.71 \text{ ft}^2$$

$$B_n := \min \left[ \sqrt{\frac{A_2}{A_1}} \cdot \left( 0.85 \cdot f_c \cdot A_{pier} \right), 2 \cdot \left( 0.85 \cdot f_c \cdot A_1 \right) \right]$$

$$B_n = 3.77 \times 10^4 \cdot \text{kips}$$

Nominal bearing strength based on the fact that the supporting surface is wider than the loaded area

 $\phi B_n := \phi_b \cdot B_n$ 

$$\phi B_n = 2.45 \times 10^4 \cdot \text{kip}$$

Design bearing strength

$$B_u := P_u + 1.2 \cdot Wt_{pier}$$

$$B_u = 65.07 \cdot \text{kip}$$

$$\frac{B_u}{\varphi B_n} = \, 0.0027$$

Bearing Strength Check = "Concrete pier/pad bearing strength is adequate."

Site Name: STRATFORD ORONOQUE ROAD

Fullerton Engineering, P.C.

Site No.: CTL02638 Prepared By: LA Checked By: BK

## Concrete Pad and Pier Two-Way Shear Strength Calculations

ACI 318-14 Sections 8.4.4 and 22.6

 $t_1 := t - 3.5in$  $t_1 = 1.71 \text{ ft}$ Distance from extreme compression

fiber to centroid of tension

Date: 5/2/2022

reinforcement

 $b_o := \begin{bmatrix} \pi(d+t) & \text{if Pier Shape} = \text{"Circular"} \\ 4(d+t) & \text{if Pier Shape} = \text{"Square"} \end{bmatrix}$ Perimeter at critical section  $b_0 = 28.27 \text{ ft}$ 

 $A_{crit\ shear} = 56.55\ ft^2$ Area of critical section  $A_{crit shear} := b_o \cdot t$ 

 $\lambda := 1$ Concrete modification factor

 $\beta := 1$ Length to width ratio of the pier

Constant for "interior" columns  $\alpha_s := 40$ 

 $v_{c_a} := 4 \cdot \lambda \cdot \sqrt{\frac{f_c}{psi}} psi$ Nominal two-way shear strength  $v_{c\ a} = 252.98 \cdot psi$ 

provided by concrete

 $v_{c_b} := \left(2 + \frac{4}{\beta}\right) \lambda \cdot \sqrt{\frac{f_c}{psi}} psi$ Nominal two-way shear strength  $v_{c\ b} = 379.47 \, psi$ 

provided by concrete

 $v_{c\_c} := \left(2 + \frac{\alpha_s \cdot t}{b_o}\right) \lambda \cdot \sqrt{\frac{f_c}{psi}} psi$  $v_{c c} = 305.44 \, psi$ Nominal two-way shear strength

provided by concrete

 $\phi_s := 0.75$ Shear strength reduction factor

 $\phi V_n := \phi_s \cdot \min(v_{c a}, v_{c b}, v_{c c})$ Two-way shear strength provided by  $\phi V_n = 189.74 \cdot psi$ 

concrete

 $V_{11} = 7.99 \, \text{psi}$ Factored design two-way shear

stress

 $\frac{V_u}{\Phi V_n} = 0.04$ 

Two-Way Shear Strength Check = "Two-way shear strength provided by the concrete foundation pad is adequate."



PROJECT: LTE 5G NR CBAND + DoD + LTE 5C ADD + 5G NR 1DR-1

SITE NUMBER: CTL02638

USID: 163489

10152336 FA NUMBER:

PTN NUMBER: 2051A11PJ8, 2051A11LWG, 2051A11LTR, 2051A11LW8, 2051A11LTS

MRCTB054248, MRCTB055469, MRCTB056066, MRCTB055837, PACE NUMBER:

MRCTB056148 SITE NAME: STRATFORD ORONOQUE ROAD

200 ORONOQUE LANE SITE ADDRESS:

STRATFORD, CT 06614

**AUTHORITIES** 

**BUILDING CODE:** 

ELECTRICAL CODE:



550 COCHITUATE ROAD SUITE 550 13 AND 14 FRAMINGHAM, MA 01701



1100 E. WOODFIELD ROAD, SUITE 500 SCHAUMBURG, ILLINOIS 60173 TEL: 847-908-8400 COA# PEC.0001899 www.FullertonEngineering.com

I HEREBY CERTIFY THAT THESE DRAWINGS WERE PREPARED BY ME OR UNDER MY DIRECT SUPERVISION AND CONTROL, AND TO THE BEST OF MY KNOWLEDGE AND BELIEF COMPLY WITH THE REQUIREMENTS OF ALL APPLICABLE CODES.

90% REVIEW

REVISED 90% FINAL

DATE

0 04/27/2

1 05/26/22

6/2/22

|   | PROJECT INFORMATION   | SCOPE OF WORK   |
|---|---|---|
| SITE NAME: SITE NUMBER: SITE ADDRESS:  FA NUMBER: PTN NUMBER: PACE NUMBER: USID NUMBER:  APPLICANT: | STRATFORD ORONOQUE ROAD CTL02638 200 ORONOQUE LANE STRATFORD, CT 06614 10152336 2051A11PUB, 2051A11LURG, 2051A11LURB, 2051A11LUTS MRCTB054248, MRCTB055469, MRCTB056066, MRCTB055837, MRCTB056148 163489  AT&T WIRELESS 550 COCHITUATE ROAD SUITE 550 13 AND 14 | SCOPE HEREIN BASED ON RFDS ID # 4846452, VERSION 2.00 LAST UPDATED 05/2   |
| OWNER:  JURISDICTION:/ ZONING:  | FRAMINGHAM, MA 01701  TOWN OF STRATFORD 200 ORONOQUE LANE STRATFORD, CT 06614  - / -  | <ul> <li>(1) NEW RBS 6648 BBU AND XCEDE CABLES</li> <li>CONTRACTOR SHALL FURNISH ALL MATERIAL WITH THE EXCEPTION OF AT&amp;T SUPPLIED M</li> <li>ALL MATERIAL SHALL BE INSTALLED BY THE CONTRACTOR, UNLESS STATED OTHERWISE.</li> </ul> |
| COUNTY:<br>SITE COORDINATES FROM  | : FAIRFIELD<br>(RFDS)   | SITE LOCATION MAP   |
| LATITUDE: LONGITUDE: GROUND ELEV.: PROPOSED USE; AT&T RF MANAGER: PHONE: EMAIL:                     | 41.251411'/41'15'05.1"<br>-73.117151' /-73'07'01.7"<br>264'<br>TELECOMMUNICATIONS FACILITY<br>PRASHANTH SIMHA<br>(201)628-5071<br>pn5165@att.com  | Portion And And And And And And And And And An  |

| SCOPE OF WORK | APPLICABLE BUILDING CODES AND STANDARDS  |
|---------------|--|
|               | ALL WORK AND MATERIALS SHALL BE PERFORMED AND INSTALLED IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING |

FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION. JRNISH ALL MATERIAL WITH THE EXCEPTION OF AT&T SUPPLIED MATERIAL ADA ACCESS REQUIREMENTS ARE NOT REQUIRED.

TITLE SHEET

THIS FACILITY DOES NOT REQUIRE POTABLE WATER AND WILL NOT PRODUCE ANY SEWAGE

2018 CONNECTICUT STATE BUILDING CODE SUPPLEMENT

# SITE NO SCALE

**DIRECTIONS** 

## DRAWING INDEX

2015 INTERNATIONAL BUILDING CODE

2017 NATIONAL ELECTRIC CODE

| SP1 | NOTES AND SPECIFICATIONS      | l |
|-----|-------------------------------|---|
| SP2 | NOTES AND SPECIFICATIONS      | İ |
| A1  | COMPOUND PLAN                 | İ |
| A2  | EQUIPMENT PLAN                | S |
| A3  | ELEVATIONS                    | ľ |
| A4  | ANTENNA PLANS                 | İ |
| A5  | EQUIPMENT DETAILS             | İ |
| A5A | EQUIPMENT DETAILS             | İ |
| A6  | ANTENNA & CABLE CONFIGURATION | Ļ |
| A7  | CABLE NOTES AND COLOR CODING  | S |
| A8  | GROUNDING DETAILS             | İ |
| A9  | PLUMBING DIAGRAMS             | İ |
|     |                               | ĺ |
|     |                               |   |

SITE NAME

STRATFORD ORONOQUE ROAD

SITE NUMBER:

CTL02638

SITE ADDRESS

200 ORONOQUE LANE STRATFORD, CT 06614

SHEET NAME

TITLE SHEET

SHEET NUMBER

#### PROJECT CONSULTANTS

PROJECT MANAGER:

CONTACT:

EMAIL:

SMARTI INK 85 RANGEWAY ROAD, SUITE 102

NORTH BILLERICA, MA 01862 SHARON KEEFE (978) 930-3918 Sharon.Keefe@smartlinkllc.com

FULLERTON ENGINEERING, P.C.

1100 E. WOODFIELD ROAD, SUITE 500

SMARTI INK

SITE AQUISITION: ADDRESS: 85 RANGEWAY ROAD, SUITE 102 NORTH BILLERICA, MA 01862 KRISTINA COTTONE (978) 551-8627 CONTACT: Kristina.Cottone@smartlinkllc.com EMAIL:

**ENGINEER/ARCHITECT:** 

ADDRESS:

SCHAUMBURG, IL 60173 CONTACT: KIP HITTER (847) 908-8400 EMAIL: KHitter@FullertonEngineering.com

**CONSTRUCTION:** 

SMARTLINK 85 RANGEWAY ROAD, SUITE 102 ADDRESS: NORTH BILLERICA, MA 01862 CONTACT: KRISTINA COTTONE (978) 551-8627 kristina.cottone@smartlinkgroup.com EMAIL:

SCAN QR CODE FOR LINK TO SITE LOCATION MAP





NOTE: DRAWING SCALES ARE FOR 11"x17" SHEETS UNLESS OTHERWISE NOTED

PROJECT# 2021.0215.0011

#### GENERAL CONSTRUCTION

- 1. FOR THE PURPOSE OF CONSTRUCTION DRAWINGS, THE FOLLOWING DEFINITIONS SHALL APPLY:
  CONTRACTOR/CM SMARTLINK
  OWNER AT&T WIRELESS
- 2. ALL SITE WORK SHALL BE COMPLETED AS INDICATED ON THE DRAWINGS AND AT&T PROJECT SPECIFICATIONS.
- I. GENERAL CONTRACTOR SHALL VISIT THE SITE AND SHALL FAMILIARIZE HIMSELF WITH ALL CONDITIONS AFFECTING THE PROPOSED WORK AND SHALL MAKE PROVISIONS. GENERAL CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING HIMSELF WITH ALL CONTRACT DOCUMENTS, FIELD CONDITIONS, DIMENSIONS, AND CONFIRMING THAT THE WORK MAY BE ACCOMPLISHED AS SHOWN PRIOR TO PROCEEDING WITH CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER PRIOR TO THE COMMENCEMENT OF WORK.
- 4. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. GENERAL CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF WORK PERFORMANCE OF WORK.
- ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES, AND APPLICABLE REGULATIONS.
- 6. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AN LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS
- PLANS ARE NOT TO BE SCALED. THESE PLANS ARE INTENDED TO BE A DIAGRAMMATIC OUTLINE ONLY UNLESS OTHERWISE NOTED. DIMENSIONS SHOWN ARE TO FINISH SURFACES UNLESS OTHERWISE NOTED. SPACING BETWEEN EQUIPMENT IS THE MINIMUM REQUIRED CLEARANCE. THEREFORE, IT IS CRITICAL TO FIELD VERIFY DIMENSIONS, SHOULD THERE BE ANY QUESTIONS REGARDING THE CONTRACT DOCUMENTS, THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING A CLARIFICATION FROM THE ENGINEER PRIOR TO PROCEEDING WITH THE WORK. DETAILS ARE INTENDED TO SHOW DESIGN INTENT. MODIFICATIONS MAY BE REQUIRED TO SUIT JOB DIMENSIONS OR CONDITIONS AND SUCH MODIFICATIONS SHALL BE INCLUDED AS PART OF WORK AND PREPARED BY THE ENGINEER PRIOR TO PROCEEDING WITH WORK. PROCEEDING WITH WORK.
- 8. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE ENGINEER PRIOR TO PROCEEDING.
- 10. GENERAL CONTRACTOR SHALL BE RESPONSIBLE FOR THE SAFETY OF WORK AREA, ADJACENT AREAS AND BUILDING OCCUPANTS THAT ARE LIKELY TO BE AFFECTED BY THE WORK UNDER THIS CONTRACT. WORK SHALL CONFIRM TO ALL OSHA REQUIREMENTS AND THE LOCAL JURISDICTION.
- 11. GENERAL CONTRACTOR SHALL COORDINATE WORK AND SCHEDULE WORK ACTIVITIES WITH OTHER DISCIPLINES.
- 12. ERECTION SHALL BE DONE IN A WORKMANLIKE MANNER BY COMPETENT EXPERIENCED WORKMAN IN ACCORDANCE WITH APPLICABLE CODES AND THE BEST ACCEPTED PRACTICE. AL MEMBERS SHALL BE LAID PLUMB AND TRUE AS INDICATED
- 13. SEAL PENETRATIONS THROUGH FIRE RATED AREAS WITH UL LISTED MATERIALS APPROVED BY LOCAL JURISDICTION. CONTRACTOR SHALL KEEP AREA CLEAN, HAZARD FREE, AND DISPOSE OF ALL DEBRIS.
- 14. WORK PREVIOUSLY COMPLETED IS REPRESENTED BY LIGHT SHADED LINES AND NOTES. THE SCOPE OF WORK FOR THIS PROJECT IS REPRESENTED BY DARK SHADED LINES AND NOTES. CONTRACTOR SHALL NOTIFY THE GENERAL CONTRACTOR OF ANY EXISTING CONDITIONS THAT DEVIATE FROM THE DRAWINGS PRIOR TO BEGINNING CONSTRUCTION.
- 15. CONTRACTOR SHALL PROVIDE WRITTEN NOTICE TO THE CONSTRUCTION MANAGER 48 HOURS PRIOR TO COMMENCEMENT OF WORK.
- 16. THE CONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT CONTRACTOR'S EXPENSE TO THE SATISFACTION OF THE OWNER.
- 17. THE CONTRACTOR SHALL CONTACT UTILITY LOCATING SERVICES PRIOR TO THE START OF CONSTRUCTION.
- 18. GENERAL CONTRACTOR SHALL COORDINATE AND MAINTAIN ACCESS FOR ALL TRADES AND CONTRACTORS TO THE SITE AND/OR BUILDING.
- 19. THE GENERAL CONTRACTOR SHALL BE RESPONSIBLE FOR SECURITY OF THE SITE FOR THE DURATION OF CONSTRUCTION UNTIL JOB COMPLETION.

- 20. THE GENERAL CONTRACTOR SHALL MAINTAIN IN GOOD CONDITION ONE COMPLETE SET OF PLANS WITH ALL REVISIONS, ADDENDA, AND CHANGE ORDERS ON THE PREMISES AT ALL TIMES.
- 21. THE GENERAL CONTRACTOR SHALL PROVIDE PORTABLE FIRE EXTINGUISHERS WITH A RATING OF NOT LESS THAN 2-A OT 2-A:10-B:C AND SHALL BE WITHIN 25 FEET OF TRAVEL DISTANCE TO ALL PORTIONS OF WHERE THE WORK IS BEING
- 22. ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC, AND OTHER UTILITIES SHALL BE PROTECTED AT ALL TIMES, AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SHALL BE RELOCATED AS DIRECTED BY THE ENGINEER. EXTREME CAUTION SHOULD BE USED BY THE CONTRACTOR WHEN EXCAVATING OR DRILLING PIERS AROUND OR NEAR UTILITIES. CONTRACTOR SHALL PROVIDE SAFETY TRAINING FOR THE WORKING CREW. THIS SHALL INCLUDE BUT NOT BE LIMITED TO A) FALL PROTECTION, B) CONFINED SPACE, C) ELECTRICAL SAFETY, AND D) TRENCHING &
- 23. ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC, AND OTHER UTILITIES, WHICH INTERFERE WITH THE EXECUTION OF THE WORK, SHALL BE REMOVED, CAPPED, PLUGGED OR OTHERWISE DISCONNECTED AT POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, AS DIRECTED BY THE RESPONSIBLE ENGINEER, AND SUBJECT TO THE WORK OF THE APPROVAL OF THE OWNER AND/OR LOCAL UTILITIES.
- 24. THE AREAS OF THE OWNER'S PROPERTY DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUIPMENT OR DRIVEWAY, SHALL BE GRADED TO A UNIFORM SLOPE, AND STABILIZED TO PREVENT EROSION.
- 25. CONTRACTOR SHALL MINIMIZE DISTURBANCE TO THE EXISTING SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES, IF REQUIRED DURING CONSTRUCTION, SHALL BE IN CONFORMANCE WITH THE FEDERAL AND LOCAL JURISDICTION FOR EROSION AND SEDIMENT CONTROL.
- 26. NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN GROUNDING. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OR EMBANKMENT.
- 27. THE SUBGRADE SHALL BE BROUGHT TO A SMOOTH UNIFORM GRADE AND COMPACTED TO 95 PERCENT STANDARD PROCTOR DENSITY UNDER PAVEMENT AND STRUCTURES AND 80 PERCENT STANDARD PROCTOR DENSITY IN OPEN SPACE. ALL TRENCHES IN PUBLIC RIGHT OF WAY SHALL BE BACKFILLED WITH FLOWABLE FILL OR OTHER MATERIAL PRE-APPROVED BY THE LOCAL JURISDICTION.
- 28. ALL NECESSARY RUBBISH, STUMPS, DEBRIS, STICKS, STONES, AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF IN A LAWFUL MANNER.
- 29. ALL BROCHURES, OPERATING AND MAINTENANCE MANUALS, CATALOGS, SHOP DRAWINGS, AND OTHER DOCUMENTS SHALL BE TURNED OVER TO THE GENERAL CONTRACTOR AT COMPLETION OF CONSTRUCTION AND PRIOR TO PAYMENT.
- 30. CONTRACTOR SHALL SUBMIT A COMPLETE SET OF AS-BUILT REDLINES TO THE GENERAL CONTRACTOR UPON COMPLETION OF PROJECT AND PRIOR TO FINAL PAYMENT.
- 31. CONTRACTOR SHALL LEAVE PREMISES IN A CLEAN CONDITION.
- 32. THE PROPOSED FACILITY WILL BE UNMANNED AND DOES NOT REQUIRE POTABLE WATER OR SEWER SERVICE, AND IS NOT FOR HUMAN HABITAT (NO HANDICAP ACCESS REQUIRED).
- 33. OCCUPANCY IS LIMITED TO PERIODIC MAINTENANCE AND INSPECTION, APPROXIMATELY 2 TIMES PER MONTH, BY AT&T
- 34. NO OUTDOOR STORAGE OR SOLID WASTE CONTAINERS ARE PROPOSED.
- 35. ALL MATERIAL SHALL BE FURNISHED AND WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE LATEST REVISION AT&T MOBILITY GROUNDING STANDARD "TECHNICAL SPECIFICATION FOR CONSTRUCTION OF GSM/GPRS WIRELESS SITES" AND "TECHNICAL SPECIFICATION FOR FACILITY GROUNDING". IN CASE OF A CONFLICT BETWEEN THE CONSTRUCTION SPECIFICATION AND THE DRAWINGS, THE DRAWINGS SHALL GOVERN.
- 36. CONTRACTORS SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND INSPECTIONS REQUIRED FOR CONSTRUCTION. IF CONTRACTOR CANNOT OBTAIN A PERMIT, THEY MUST NOTIFY THE GENERAL CONTRACTOR IMMEDIATELY.
- 37. CONTRACTOR SHALL REMOVE ALL TRASH AND DEBRIS FROM THE SITE ON A DAILY BASIS.
- 38. INFORMATION SHOWN ON THESE DRAWINGS WAS OBTAINED FROM SITE VISITS AND/OR DRAWINGS PROVIDED BY THE SITE OWNER. CONTRACTORS SHALL NOTIFY THE ENGINEER OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
- 39. NO WHITE STROBE LIGHTS ARE PERMITTED. LIGHTING IF REQUIRED, WILL MEET FAA STANDARDS AND REQUIREMENTS.

#### ANTENNA MOUNTING

40. DESIGN AND CONSTRUCTION OF ANTENNA SUPPORTS SHALL CONFORM TO CURRENT ANSI/TIA-222 OR APPLICABLE LOCAL

- 41. ALL STEEL MATERIALS SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT-DIP GALVANIZED) COATINGS ON IRON AND STEEL PRODUCTS", UNLESS NOTED OTHERWISE.
- 42. ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC-COATING (HOT-DIP) ON IRON AND STEEL HARDWARE", UNLESS NOTED OTHERWISE.
- 43. DAMAGED GALVANIZED SURFACES SHALL BE REPAIRED BY COLD GALVANIZING IN ACCORDANCE WITH ASTM A780.
- 44. ALL ANTENNA MOUNTS SHALL BE INSTALLED WITH LOCK NUTS, DOUBLE NUTS AND SHALL BE TORQUED TO
- 45. CONTRACTOR SHALL INSTALL ANTENNA PER MANUFACTURER'S RECOMMENDATION FOR INSTALLATION AND GROUNDING.
- 46. ALL UNUSED PORTS ON ANY ANTENNAS SHALL BE TERMINATED WITH A 50-OHM LOAD TO ENSURE ANTENNAS PERFORM AS DESIGNED.
- 47. PRIOR TO SETTING ANTENNA AZIMUTHS AND DOWNTILTS, ANTENNA CONTRACTOR SHALL CHECK THE ANTENNA MOUNT FOR TIGHTNESS AND ENSURE THAT THEY ARE PLUMB. ANTENNA AZIMUTHS SHALL BE SET FROM TRUE NORTH AND BE ORIENTED WITHIN +/- 5% AS DEFINED BY THE RFDS. ANTENNA DOWNTILTS SHALL BE WITHIN +/- 0.5% AS DEFINED BY THE RFDS. REFER TO ND-00246.
- 48. JUMPERS FROM THE TMA'S MUST TERMINATE TO OPPOSITE POLARIZATION'S IN EACH SECTOR.
- 49. CONTRACTOR SHALL RECORD THE SERIAL #, SECTOR, AND POSITION OF EACH ACTUATOR INSTALLED AT THE ANTENNAS AND PROVIDE THE INFORMATION TO AT&T.
- 50. TMA'S SHALL BE MOUNTED ON PIPE DIRECTLY BEHIND ANTENNAS AS CLOSE TO ANTENNA AS FEASIBLE IN A VERTICAL POSITION.

#### TORQUE REQUIREMENTS

- 51. ALL RF CONNECTIONS SHALL BE TIGHTENED BY A TORQUE WRENCH.
- 52. ALL RF CONNECTIONS, GROUNDING HARDWARE AND ANTENNA HARDWARE SHALL HAVE A TORQUE MARK INSTALLED IN A CONTINUOUS STRAIGHT LINE FROM BOTH SIDES OF THE
- CONNECTION.

  A. RF CONNECTION BOTH SIDES OF THE CONNECTOR.

  B. GROUNDING AND ANTENNA HARDWARE ON THE NUT
  SIDE STARTING FROM THE THREADS TO THE SOLID
  SURFACE. EXAMPLE OF SOLID SURFACE: GROUND BAR,
  ANTENNA BRACKET METAL.

#### FIBER & POWER CABLE MOUNTING

- 53. THE FIBER OPTIC TRUNK CABLES SHALL BE INSTALLED INTO CONDUITS, CHANNEL CABLE TRAYS, OR CABLE TRAY. WHEN INSTALLING FIBER OPTIC TRUNK CABLES INTO A CABLE TRAY SYSTEM, THEY SHALL BE INSTALLED INTO AN INTER DUCT AND A PARTITION BARRIER SHALL BE INSTALLED BETWEEN THE 600 VOLT CABLES AND THE INTER DUCT IN ORDER TO SEGREGATE CABLE TYPES. OPTIC FIBER TRUNK CABLES SHALL HAVE APPROVED CABLE RESTRAINTS EVERY (60) SIXTY FEET AND SECURELY FASTENED TO THE CABLE TRAY SYSTEM. NFPA 70 (NEC) ARTICLE 770 RULES SHALL APPLY.
- 54. THE TYPE TC-ER CABLES SHALL BE INSTALLED INTO CONDUITS, CHANNEL CABLE TRAYS, OR CABLE TRAY AND SHALL BE SECURED AT INTERVALS NOT EXCEEDING (6) SIX FEET. AN EXCEPTION; WHERE TYPE TC-ER CABLES ARE NOT SUBJECT TO PHYSICAL DAMAGE, CABLES SHALL BE PERMITTED TO MAKE A TRANSITION BETWEEN CONDUITS, CHANNEL CABLE TRAYS, OR CABLE TRAY WHICH ARE SERVING UTILIZATION EQUIPMENT OR DEVICES, A DISTANCE (6) SIX FEET SHALL NOT BE EXCEEDED WITHOUT CONTINUIDIUS SUIPPORTING NEPA 70 (NEC) ARTICLES 336 CONTINUOUS SUPPORTING. NFPA 70 (NEC) ARTICLES 336 AND 392 RULES SHALL APPLY.
- 55. WHEN INSTALLING OPTIC FIBER TRUNK CABLES OR TYPE TC-ER CABLES INTO CONDUITS, NFPA 70 (NEC) ARTICLE 300 RULES SHALL APPLY.

#### COAXIAL CABLE NOTES

- 62. TYPES AND SIZES OF THE ANTENNA CABLE ARE BASED ON ESTIMATED LENGTHS. PRIOR TO  $\,$ 
  - ORDERING CABLE, CONTRACTOR SHALL VERIFY ACTUAL LENGTH BASED ON CONSTRUCTION LAYOUT AND NOTIFY THE PROJECT MANAGER IF ACTUAL LENGTHS EXCEED ESTIMATED
- 63. CONTRACTOR SHALL VERIFY THE DOWN-TILT OF EACH ANTENNA WITH A DIGITAL LEVEL.
- 64. CONTRACTOR SHALL CONFIRM COAX COLOR CODING PRIOR TO CONSTRUCTION.
- 65. ALL JUMPERS TO THE ANTENNAS FROM THE MAIN TRANSMISSION LINE SHALL BE 1/2" DIA. LDF AND SHALL NOT EXCEED 6'-0".

- 66. ALL COAXIAL CABLE SHALL BE SECURED TO THE DESIGNED SUPPORT STRUCTURE, IN AN APPROVED MANNER, AT DISTANCES NOT TO EXCEED 4'-0" OC.
- 67. CONTRACTOR SHALL FOLLOW ALL MANUFACTURER'S RECOMMENDATIONS REGARDING BOTH THE INSTALLATION AND GROUNDING OF ALL COAXIAL CABLES, CONNECTORS, ANTENNAS, AND ALL OTHER EQUIPMENT.
- 68. CONTRACTOR SHALL GROUND ALL EQUIPMENT. INCLUDING ANTENNAS, RET MOTORS, TMA'S, COAX CABLES, AND RET CONTROL CABLES AS A COMPLETE SYSTEM. GROUNDING SHALL BE EXECUTED BY QUALIFIED WIREMEN IN COMPLIANCE WITH MANUFACTURER'S SPECIFICATION AND RECOMMENDATION.
- 69. CONTRACTOR SHALL PROVIDE STRAIN—RELIEF AND CABLE SUPPORTS FOR ALL CABLE ASSEMBLIES, COAX CABLES, AND RET CONTROL CABLES. CABLE STRAIN—RELIEFS AND CABLE SUPPORTS SHALL BE APPROVED FOR THE PURPOSE. INSTALLATION SHALL BE IN ACCORDANCE WITH MANUFACTURER'S SPECIFICATIONS AND RECOMMENDATIONS.
- 70. CONTRACTOR TO VERIFY THAT EXISTING COAX HANGERS ARE STACKABLE SNAP IN HANGERS. IF EXISTING HANGERS ARE NOT STACKABLE SNAP IN HANGERS THE CONTRACTOR SHALL REPLACE EXISTING HANGERS WITH NEW SNAP IN HANGERS IF

#### GENERAL CABLE AND EQUIPMENT NOTES

- 71. CONTRACTOR SHALL BE RESPONSIBLE TO VERIFY ANTENNA, TMAS, DIPLEXERS, AND COAX CONFIGURATION, MAKE AND MODELS PRIOR TO INSTALLATION.
- 72. ALL CONNECTIONS FOR HANGERS, SUPPORTS, BRACING, ETC. SHALL BE INSTALLED PER TOWER MANUFACTURER'S
- 73. CONTRACTOR SHALL REFERENCE THE TOWER STRUCTURAL ANALYSIS/DESIGN DRAWINGS FOR DIRECTIONS ON CABLE DISTRIBUTION/ROUTING.
- 74. ALL OUTDOOR RF CONNECTORS/CONNECTIONS SHALL BE WEATHERPROOFED, EXCEPT THE RET CONNECTORS, USING BUTYL TAPE AFTER INSTALLATION AND FINAL CONNECTIONS ARE MADE. BUTYL TAPE SHALL HAVE A MINIMUM OF ONE—HALF TAPE WIDTH OVERLAP ON EACH TURN AND EACH LAYER SHALL BE WRAPPED THREE TIMES. WEATHERPROOFING SHALL BE SMOOTH WITHOUT BUCKLING. BUTYL BLEEDING IS NOT ALLOWED.
- 75. IF REQUIRED TO PAINT ANTENNAS AND/OR COAX:
  A. TEMPERATURE SHALL BE ABOVE 50' F.
  B. PAINT COLOR MUST BE APPROVED BY BUILDING OWNER/LANDLORD. C. FOR REGULATED TOWERS, FAA/FCC APPROVED PAINT
  - D. DO NOT PAINT OVER COLOR CODING OR ON EQUIPMENT MODEL NUMBERS
- 76. ALL CABLES SHALL BE GROUNDED WITH COAXIAL CABLE
- GROUND KITS. FOLLOW THE MANUFACTURER'S
  RECOMMENDATIONS.
  A. GROUNDING AT THE ANTENNA LEVEL.
  B. GROUNDING AT MID LEVEL, TOWERS WHICH ARE OVER
  200'-0", ADDITIONAL CABLE GROUNDING REQUIRED.
  C. GROUNDING AT BASE OF TOWER PRIOR TO TURNING HORIZONTAL.

  D. GROUNDING OUTSIDE THE EQUIPMENT SHELTER AT ENTRY
- GROUNDING INSIDE THE EQUIPMENT SHELTER AT THE
- 77. ALL PROPOSED GROUND BAR DOWNLEADS ARE TO BE TERMINATED TO THE EXISTING ADJACENT GROUND BAR DOWNLEADS A MINIMUM DISTANCE OF 4'-0" BELOW GROUND BAR. TERMINATIONS MAY BE EXOTHERMIC OR COMPRESSION.



550 COCHITUATE ROAD SUITE 550 13 AND 14 FRAMINGHAM, MA 01701



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| REV | DATE     | DESCRIPTION | BY |
|-----|----------|-------------|----|
| 0   | 04/27/22 | 90% REVIEW  | MS |
| 1   | 05/26/22 | REVISED 90% | SM |
| 2   | 6/2/22   | FINAL       | KR |
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Jun 3 2022

# STRATFORD ORONOQUE ROAD

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CTL02638

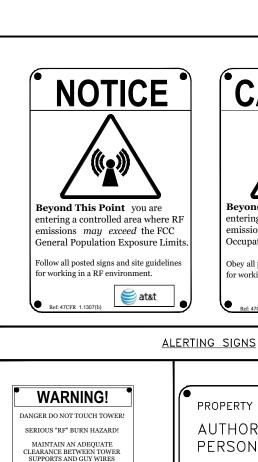
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SHEET NAME

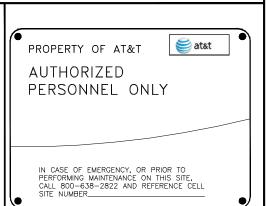
**NOTES AND SPECIFICATIONS** 

SHEET NUMBER



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**ALERTING SIGN** 



INFO SIGN #4

CAUTION

**Beyond This Point** you are entering a controlled area where RF

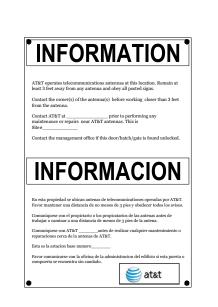
Occupational Exposure Limits.

for working in a RF environment.

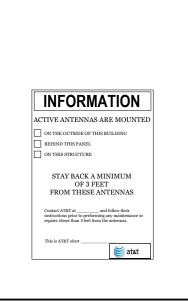
emissions may exceed the FCC

Obey all posted signs and site guidelines

at&t



INFO SIGN #1





ALERTING SIGN (FOR CELL SITE BATTERIES)

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ALERTING SIGN (FOR DIESEL FUEL)



ALERTING SIGN (FOR PROPANE)

# at&t

550 COCHITUATE ROAD SUITE 550 13 AND 14 FRAMINGHAM, MA 01701



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|                 | REV | DATE                         | DESCRIPTION | BY |  |  |  |
| IGHT OF         | 0   | 04/27/22                     | 90% REVIEW  | MS |  |  |  |
| CLIMBING        | 1   | 05/26/22                     | REVISED 90% | SM |  |  |  |
| N 9 FT<br>ROUND | 2   | 6/2/22                       | FINAL       | KR |  |  |  |
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Jun 3 2022

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STRATFORD ORONOQUE ROAD

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SITE ADDRESS

200 ORONOQUE LANE STRATFORD, CT 06614

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NOTES AND SPECIFICATIONS

SHEET NUMBER

SP2

# **GENERAL SIGNAGE GUIDELINES**

| STRUCTURE TYPE                               | INFO SIGN #1  | INFO SIGN #2   | INFO SIGN #3               | INFO SIGN #4  | STRIPING   | NOTICE SIGN   | CAUTION SIGN  |                  |
|--|---|--|----------------------------|---|--|---|---|------------------|
| TOWERS                                       |   |  |                            |   |  |   |   | REV              |
| MONOPOLE/MONOPINE/MONOPALM                   | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS | CLIMBING SIDE OF<br>THE TOWER  | ON BACKSIDE OF<br>ANTENNAS | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS |  |   | AT THE HEIGHT OF<br>THE FIRST CLIMBING<br>STEP, MIN 9 FT<br>ABOVE GROUND                      | 0<br>1<br>2      |
| SEC TOWERS/TOWERS WITH HIGH<br>VOLTAGE       | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS | CLIMBING SIDE OF<br>THE TOWER  | ON BACKSIDE OF<br>ANTENNAS | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS |  |   |   | E                |
| LIGHT POLES/FLAG POLES                       | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS | ON THE POLE, NO LESS THAN 3FT BELOW THE ANTENNA AND LESS THAN 9FT ABOVE GROUND | ON BACKSIDE OF<br>ANTENNAS | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS |  |   |   | SUF<br>OF<br>THE |
| UTILITY WOOD POLES (JPA)                     | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS | ON THE POLE, NO LESS THAN 3FT BELOW THE ANTENNA AND LESS THAN 9FT ABOVE GROUND | ON BACKSIDE OF<br>ANTENNAS | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS |  | LEVEL IS: 0-99%; NO CAUTION SIGN AT NO  | OF MPE AT ANTENNA<br>TICE SIGN; OVER 99%:<br>LESS THAN 3FT BELOW<br>T ABOVE GROUND            |                  |
| MICROCELLS MOUNTED ON NON-JPA<br>POLES       | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS | ON THE POLE, NO LESS THAN 3FT BELOW THE ANTENNA AND LESS THAN 9FT ABOVE GROUND | ON BACKSIDE OF<br>ANTENNAS | ENTRANCE GATES,<br>SHELTER DOORS OR<br>ON THE OUTDOOR<br>CABINETS |  | 9FT ABOVE GROU<br>EXPOSURE EXCEEDS<br>PUBLIC EXPOSURE A<br>ABOVE GROUND OR AT | IGN AT NO LESS THAN IND: ONLY IF THE 90% OF THE GENERAL .T EXPOSURE AT 6FT OUTSIDE OF SURFACE |                  |
| TOWERS                                       |   |  |                            |   |  |   |   | 1                |
| AT ALL ACCESS POINTS TO THE ROOF             | X   |  |                            | X   |  |   |   | 1                |
| ON ANTENNAS                                  | X   |  | X                          | X   |  |   |   | SI               |
| CONCEALED ANTENNAS                           | Х   | Х  |                            | Х   |  |   |   | 1                |
| ANTENNAS MOUNTED FACING OUTSIDE THE BUILDING | ×   | ×  |                            | ×   |  |   |   | 1                |
| ANTENNAS ON SUPPORT STRUCTURE                | Х   | X  |                            | Х   |  |   |   |                  |
| ROOFVIEW GRAPH                               |   |  |                            |   |  |   |   | <u> </u>         |
| RADIATION AREA IS WITHIN 3FT FROM ANTENNA    | x   | ADJACENT TO EACH<br>ANTENNA  |                            | х   |  |   | JTION SIGN (BASED ON  | SIT              |
| RADIATION AREA IS BEYOND 3FT FROM<br>ANTENNA | ×   | ADJACENT TO EACH<br>ANTENNA  |                            | х   | DIAGONAL, YELLOW<br>STRIPING AS TO<br>ROOFVIEW GRAPH | 1 KOOFVIEW KESULIS)   | AT ANTENNA /BARRIER   |                  |
| CHURCH STEEPLES                              | ACCESS TO<br>STEEPLE  | ADJACENT TO<br>ANTENNAS IF<br>ANTENNAS ARE<br>CONCEALED                        | ON BACKSIDE OF<br>ANTENNAS | ACCESS TO<br>STEEPLE  |  |   | CAUTION SIGN AT THE<br>ANTENNAS   | SI               |
| WATER STATIONS                               | ACCESS TO LADDER  | ADJACENT TO<br>ANTENNAS IF<br>ANTENNAS ARE<br>CONCEALED                        | ON BACKSIDE OF<br>ANTENNAS | ACCESS TO LADDER  |  |   | CAUTION SIGN BESIDE<br>INFO SIGN #1, MIN.<br>9FT ABOVE GROUND                                 |                  |

NOTES FOR ROOFTOP SITES:

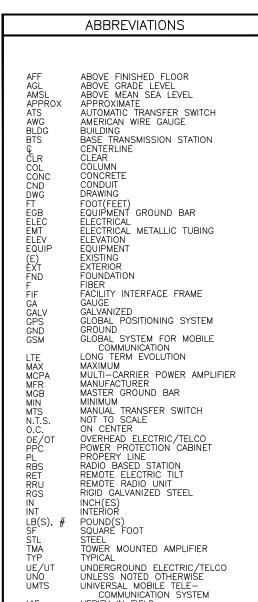
. EITHER NOTICE OR CAUTION SIGNS NEED TO BE POSTED AT EACH SECTOR AS CLOSE AS POSSIBLE TO: THE OUTER EDGE OF THE STRIPED OFF AREA OR THE OUTER ANTENNAS OF THE ECTOR

2. IF ROOFVIEWS SHOWS: ONLY BLUE = NOTICE SIGN, BLUE AND YELLOW = CAUTION SIGN, ONLY YELLOW = CAUTION SIGN TO BE INSTALLED

3. SHOULD THE REQUIRED STRIPING AREAS INTERFERE WITH ANY STRUCTURE OR EQUIPMENT (A/C, VENTS, ROOF HATCH, DOORS, OTHER ANTENNAS, DISHES, ETC.). PLEASE NOTIFY AT&T TO MODIFY THE STRIPING AREA, PRIOR TO STARTING THE WORK.

INFO SIGN #2 INFO SIGN #3

SIGNAGE GUIDELINES CHART

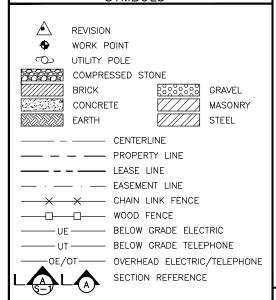


#### SYMBOLS

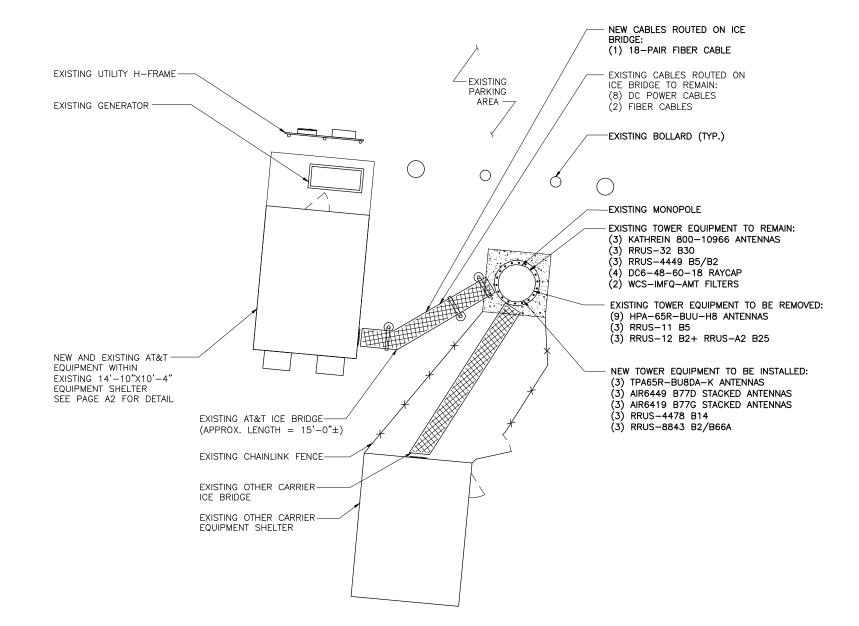
VERIFY IN FIELD WITH TRANSFORMER

VIF

XÉMR



COMPOUND PLAN





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Jun 3 2022

SITE NAME

# **STRATFORD ORONOQUE ROAD**

SITE NUMBER:

CTL02638

SITE ADDRESS

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SHEET NAME

**COMPOUND** PLAN

SHEET NUMBER

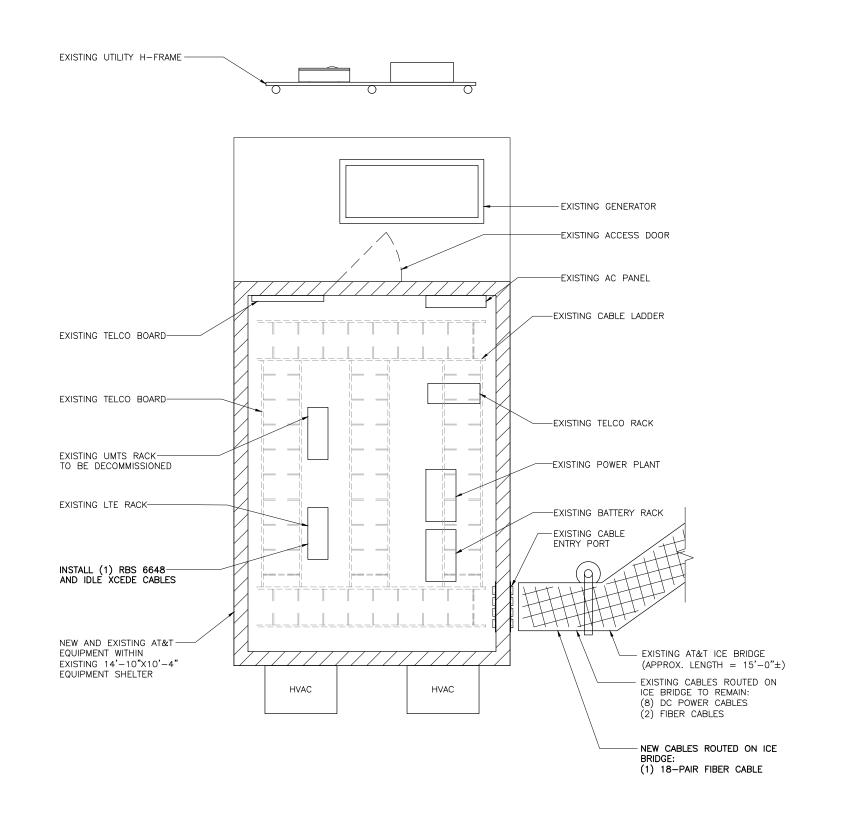
3



SITE PHOTO 1 SCALE: N.T.S

 $\frac{1}{16}$ , SCALE: 3/32" = 1'-0"

SITE PHOTO 2 SCALE: N.T.S.





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SHEET NAME

EQUIPMENT PLAN

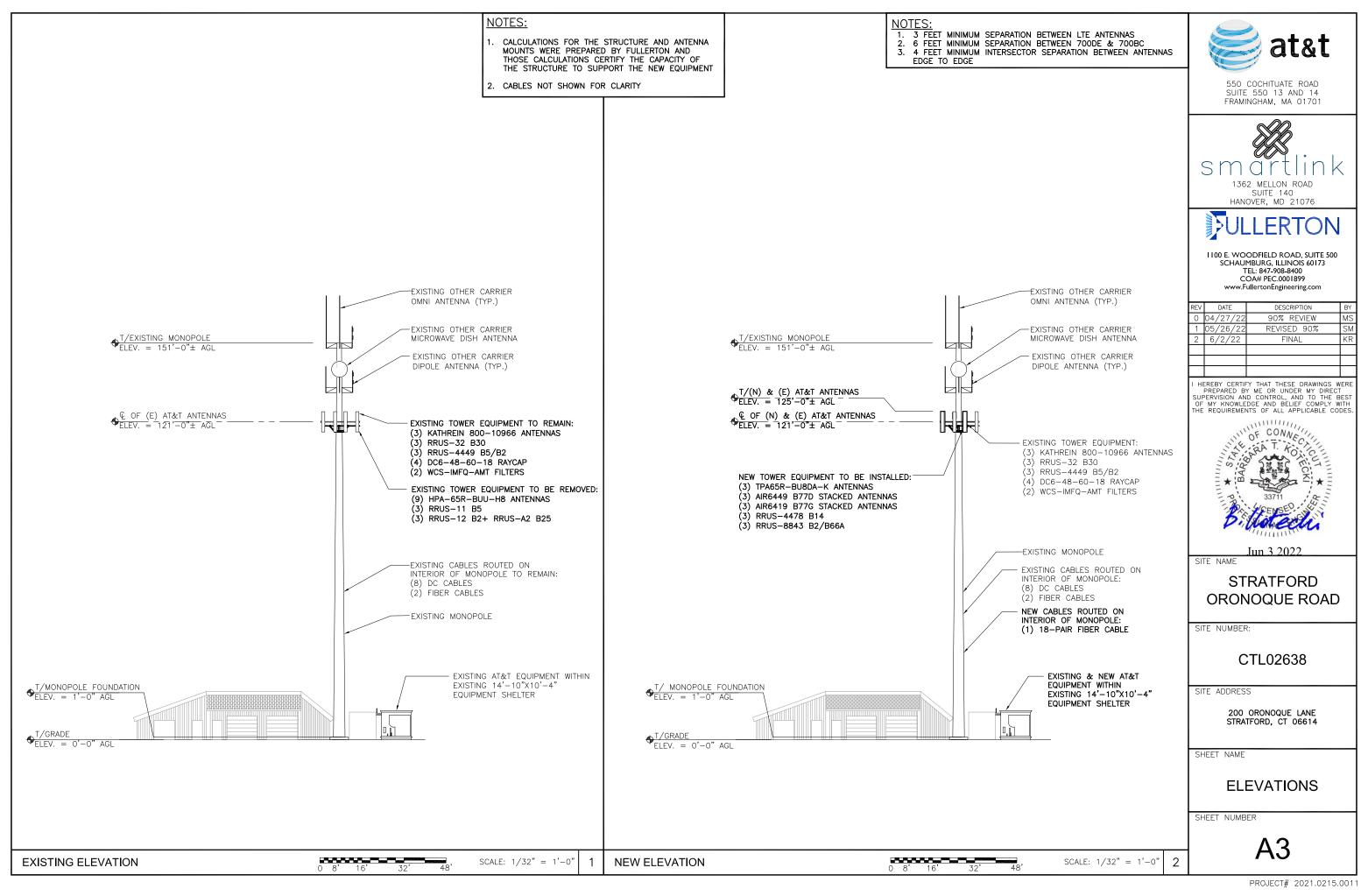
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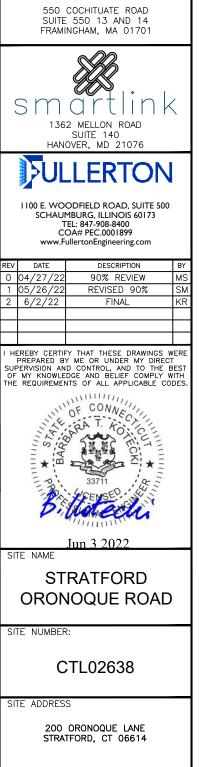
**A2** 

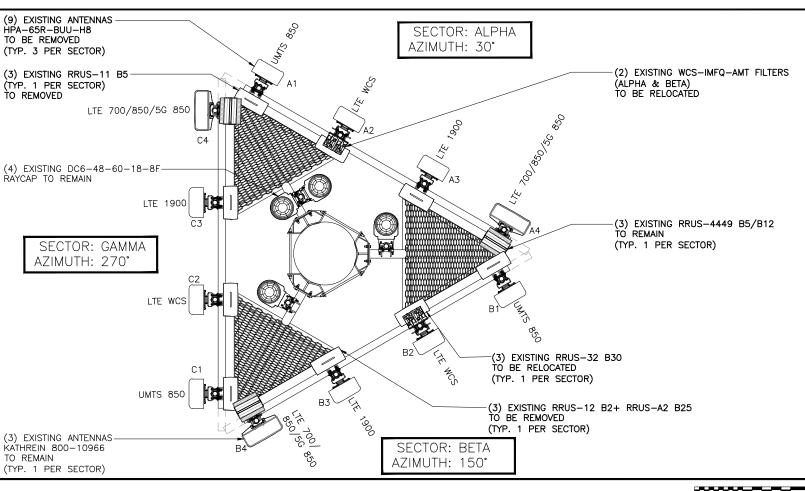
(N)

EQUIPMENT PLAN

0 1' 2' 4' 6' SCALE: 1/4" = 1'-0"





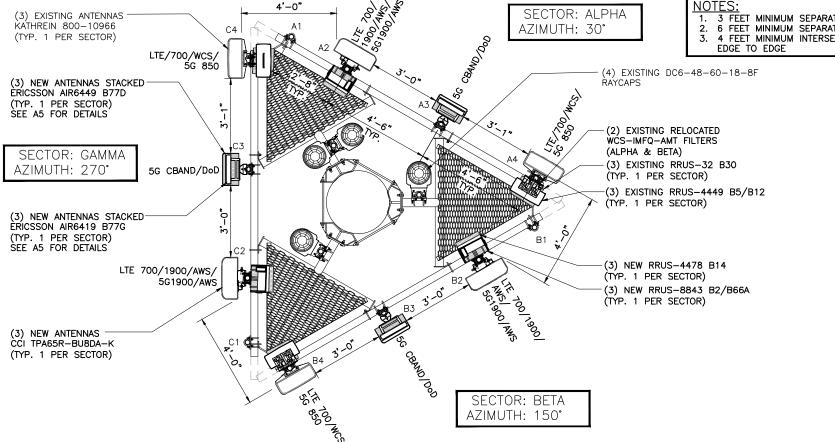


\_\_\_\_ **EXISTING ANTENNA PLAN** SCALE: 1/4" = 1'-0"

EXISTING ANTENNA MOUNTING PIPE TO BE REUSED, RELOCATED OR REPLACED AS REQUIRED

PIPE(S) 2.5 STD. (2-7/8" O.D.)

FINAL ANTENNA PLAN





SCALE: 1/4" = 1'-0"

NOTES:

1. 3 FEET MINIMUM SEPARATION BETWEEN LTE ANTENNAS 6 FEET MINIMUM SEPARATION BETWEEN 700DE & 700BC
 4 FEET MINIMUM INTERSECTOR SEPARATION BETWEEN ANTENNAS

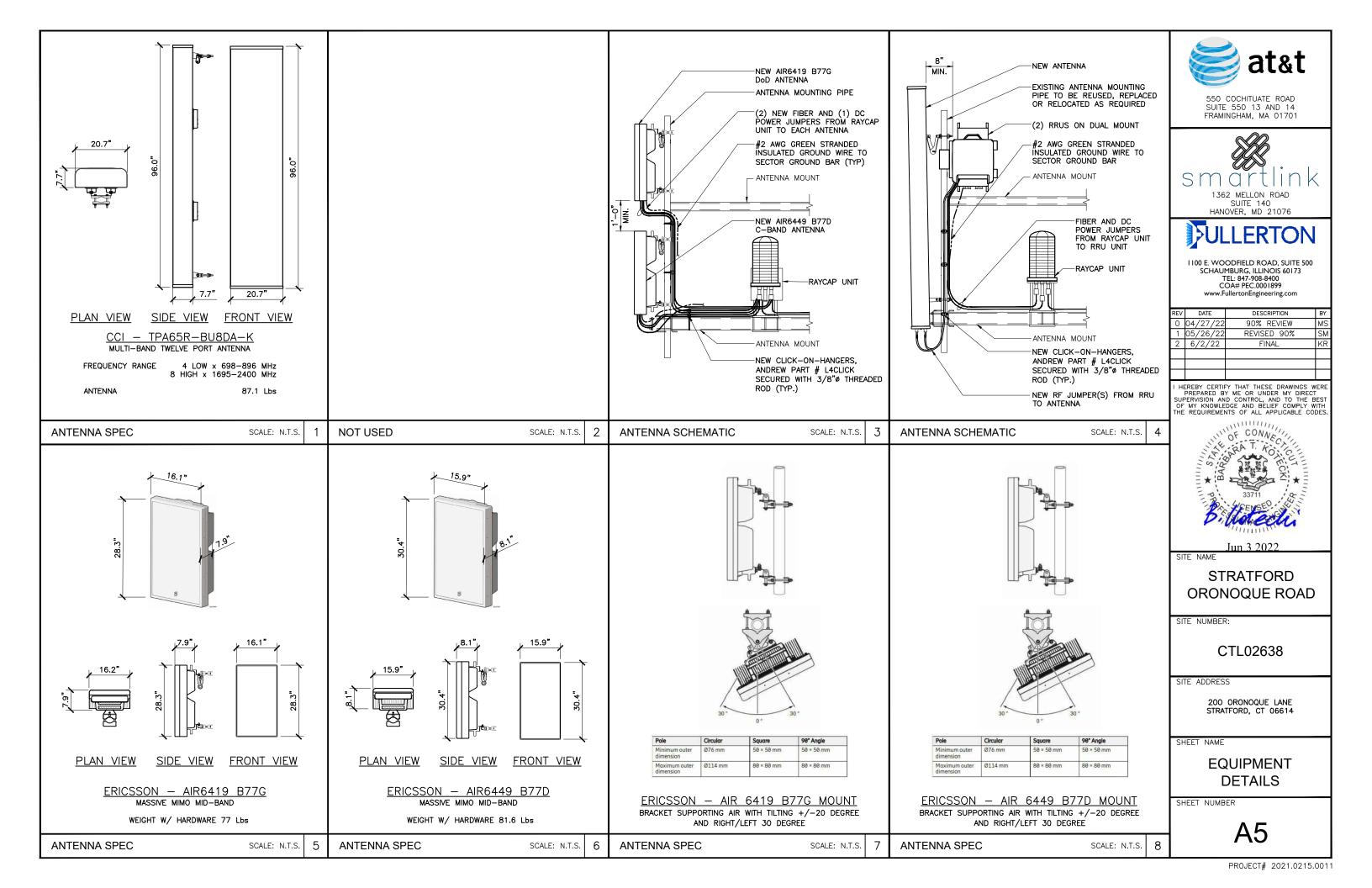
SHEET NAME

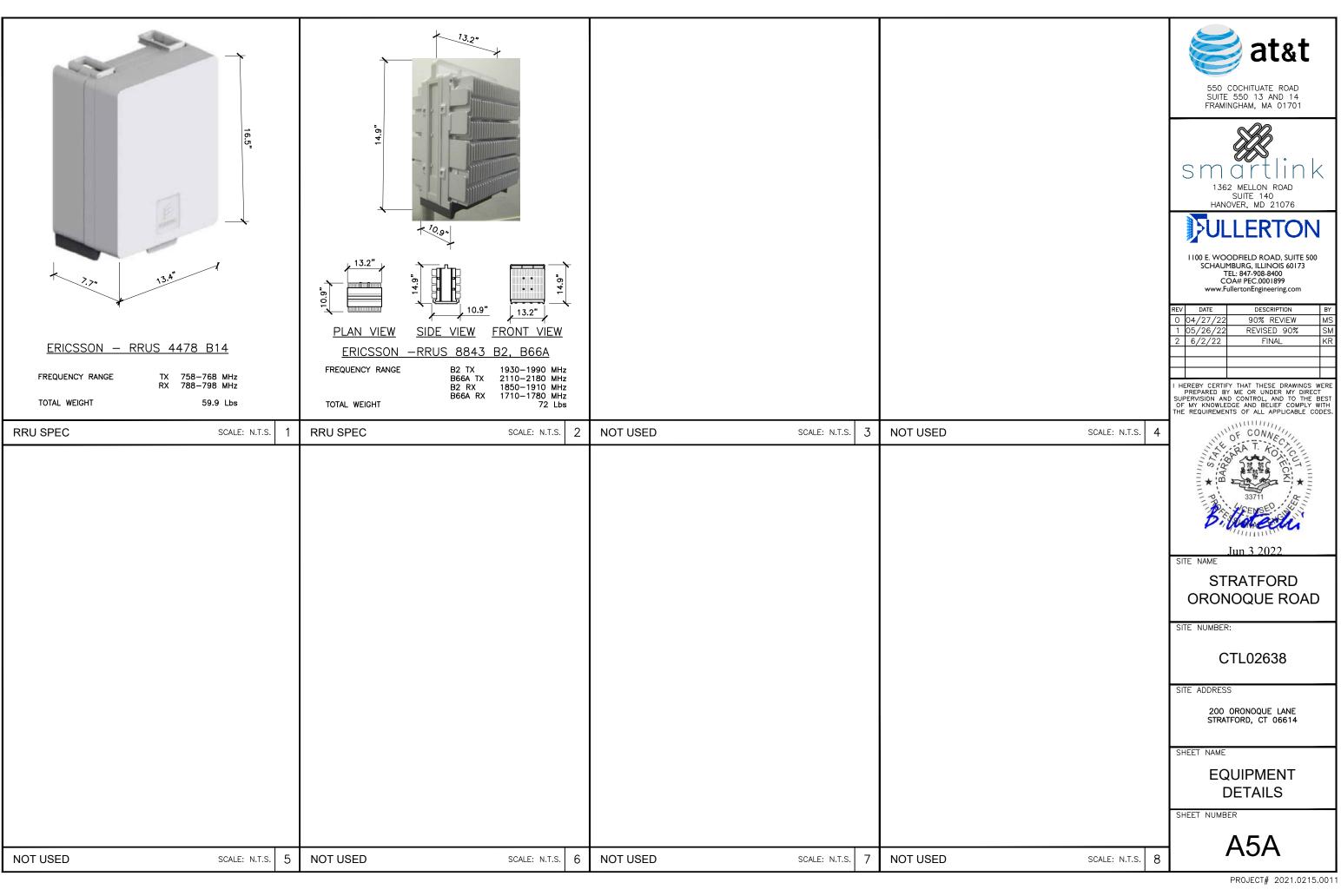
**ANTENNA PLANS** 

SHEET NUMBER

EXI

(9) (3)





# FINAL ANTENNA CONFIGURATION AND CABLE SCHEDULE SUPPLIED BY AT&T WIRELESS, FROM RF CONFIG. DATED (05/23/22, V2)

| SECTOR      | ANTENNA | ANTENNA<br>STATUS                | ANTENNA                 |          |  | ?            | RAYCAP  |  |         |                 |
|-------------|---------|----------------------------------|-------------------------|----------|--|--------------|---------|--|---------|-----------------|
| SECTOR      | NUMBER  | & TYPE                           | MODEL NUMBER            | VENDOR   | TMAY KRO ONTI  | AZIMUTH      | GROUND  | TYPE   | LENGTH  | UNIT            |
|             | A-1     | _                                |                         | _        | _  |              | _       | _  | 1       | TINU            |
|             |         |                                  |                         |          |  |              |         | _  | ı       |                 |
| ALPHA       | A-2     | (N) LTE<br>700/1900              | TPA65R-BU8DA-K          | CCI      | (1) NEW RRUS-4478 B14<br>(1) NEW RRUS-8843 B2 B66A<br>(1) NEW Y-CABLE                              | 30°          | 121'-0" | SEE ANTENNA A-3 FO<br>SIZE AND LENG          |         | DC6-48-60-18-8F |
| ALP.        |         | (N)<br>5G CBAND                  | AIR6449 B77D<br>+       |          |  | 701          |         | (1) EXISTING<br>FIBER CABLE                  | 160'-0" | 6-48            |
|             | A-3     | /DoD                             | AIR6419 B77G<br>STACKED | ERICSSON | _  | 30*          | 121'-0" | (4) EXISTING<br>DC CABLES                    | 160'-0" | (E) DC          |
|             | A-4     | (E)<br>LTE<br>700/WCS/<br>5G 850 | 800-10966               | KATHREIN | (1) EXISTING 4449 B5/B12<br>(1) EXISTING RRUS-32 B30<br>(1) EXISTING WCS FILTER<br>(1) NEW Y-CABLE | 30°          | 121'-0" | SEE ANTENNA A-3 FC<br>SIZE AND LENG          |         | (2) (E          |
|             | B-1     | -1 -                             |                         |          | -  | -            | -       | _  | ı       | UNIT            |
|             |         |                                  | _                       | _        |  |              |         | _  | -       |                 |
| Ą           | B-2     | (N) LTE<br>700/1900              | TPA65R-BU8DA-K          | CCI      | (1) NEW RRUS-4478 B14<br>(1) NEW RRUS-8843 B2 B66A<br>(1) NEW Y-CABLE                              | 150°         | 121'-0" | SEE ANTENNA B-3 FOR CABLE<br>SIZE AND LENGTH |         | DC6-48-60-18-8F |
| BETA        | 50      | (N) /<br>5G CBAND                |                         |          |  | . =          |         | (1) NEW 18-PAIR FIBER<br>CABLE               | 160'-0" | 76-4            |
|             | B-3     | /DoD                             | AIR6419 B77G<br>STACKED | ERICSSON | _  | 150°         | 121'-0" | (2) EXISTING<br>DC CABLES                    | 160'-0" | (E) DC          |
|             | B-4     | (E)<br>LTE<br>700/WCS/<br>5G 850 | 800-10966               | KATHREIN | (1) EXISTING 4449 B5/B12<br>(1) EXISTING RRUS-32 B30<br>(1) EXISTING WCS FILTER<br>(1) NEW Y-CABLE | 150°         | 121'-0" | SEE ANTENNA B-3 FC<br>SIZE AND LENG          |         | (1) (           |
|             | C-1     | _                                | _                       | _        | _  | _            | _       | -  | -       | . ⊢             |
|             | 0-1     | _                                | _                       | _        | _  |              | _       | _  | ı       | LINU .          |
| M<br>A<br>M | C-2     | (N) LTE<br>700/1900              | TPA65R-BU8DA-K          | CCI      | (1) NEW RRUS-4478 B14<br>(1) NEW RRUS-8843 B2 B66A<br>(1) NEW Y-CABLE                              | 270°         | 121'-0" | SEE ANTENNA C-3 FC<br>SIZE AND LENG          |         | DC6-48-60-18-8F |
| GAMMA       | 0.7     | (N)<br>5G CBAND                  | AIR6449 B77D            | EDIOCON: |  | 070          |         | (1) EXISTING<br>FIBER CABLE                  | 160'-0" | 1 48-           |
|             | C-3     | /DoD                             | AIR6419 B77G<br>STACKED | ERICSSON | _  | 270 <b>°</b> | 121'-0" | (2) EXISTING<br>DC CABLES                    | 160'-0" |                 |
|             | C-4     | (E)<br>LTE<br>700/WCS/<br>5G 850 | 800-10966               | KATHREIN | (1) EXISTING RRUS-4449<br>B5/B12<br>(1) EXISTING RRUS-32 B30<br>(1) NEW Y-CABLE                    | 270°         | 121'-0" | SEE ANTENNA C-3 FC<br>SIZE AND LENG          |         | (1) (E)         |



550 COCHITUATE ROAD SUITE 550 13 AND 14 FRAMINGHAM, MA 01701



1100 E. WOODFIELD ROAD, SUITE 500 SCHAUMBURG, ILLINOIS 60173 TEL: 847-908-8400 COA# PEC.0001899 www.FullertonEngineering.com

| REV | DATE     | DATE DESCRIPTION |    |  |  |
|-----|----------|------------------|----|--|--|
| 0   | 04/27/22 | 90% REVIEW       | SW |  |  |
| 1   | 05/26/22 | REVISED 90%      | SM |  |  |
| 2   | 6/2/22   | FINAL            | KR |  |  |
|     |          |                  |    |  |  |
|     |          |                  |    |  |  |
|     |          |                  |    |  |  |

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Jun 3 2022

SITE NAME

**STRATFORD** ORONOQUE ROAD

SITE NUMBER:

CTL02638

SITE ADDRESS

200 ORONOQUE LANE STRATFORD, CT 06614

SHEET NAME

ANTENNA & CABLE CONFIGURATION

SHEET NUMBER

**A6** 

- 1. CONTRACTOR IS TO REFER TO AT&T'S MOST CURRENT RADIO FREQUENCY DATA SHEET (RFDS) PRIOR TO
- THE SIZE, HEIGHT, AND DIRECTION OF THE ANTENNAS SHALL BE ADJUSTED TO ACHIEVE THE AZIMUTHS SPECIFIED AND LIMIT SHADOWING AND TO MEET THE SYSTEM REQUIREMENTS.
- 3. CONTRACTOR SHALL VERIFY THE HEIGHT OF THE ANTENNA WITH THE AT&T WIRELESS PROJECT MANAGER.
- VERIFY TYPE AND SIZE OF TOWER LEG PRIOR TO ORDERING ANY ANTENNA MOUNT.
- UNLESS NOTED OTHERWISE THE CONTRACTOR MUST PROVIDE ALL MATERIAL NECESSARY.
- ANTENNA AZIMUTHS ARE DEGREES OFF OF TRUE NORTH, BEARING CLOCKWISE, IN WHICH ANTENNA FACE IS DIRECTED. ALL ANTENNAS (AND SUPPORTING STRUCTURES AS PRACTICAL) SHALL BE ACCURATELY ORIENTED IN THE SPECIFIED
- 7. CONTRACTOR SHALL VERIFY ALL RF INFORMATION PRIOR TO CONSTRUCTION.
- SWEEP TEST SHALL BE PERFORMED BY GENERAL CONTRACTOR AND SUBMITTED TO AT&T WIRELESS CONSTRUCTION SPECIALIST. TEST SHALL BE PERFORMED PER AT&T WIRELESS STANDARDS.
- CABLE LENGTHS WERE DETERMINED BASED ON THE DESIGN DRAWING. CONTRACTOR TO VERIFY ACTUAL LENGTH DURING PRE-CONSTRUCTION WALK.
- 10. CONTRACTOR TO USE ROSENBERGER FIBER LINE HANGER COMPONENTS (OR ENGINEER APPROVED EQUAL).

#### ANTENNA AND CABLING NOTES

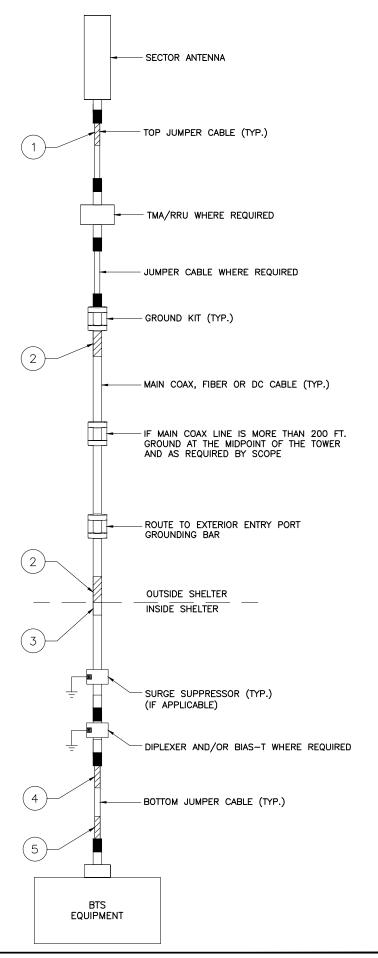
SCALE: N.T.S.

|    | RF, DC, & COAX CABLE MARKING LOCATIONS TABLE   |  |  |  |  |  |
|----|--|--|--|--|--|--|
| NO | LOCATIONS  |  |  |  |  |  |
| 1  | EACH TOP-JUMPER SHALL BE COLOR CODED WITH (1) SET OF 3" WIDE BANDS.  |  |  |  |  |  |
| 2  | EACH MAIN COAX SHALL BE COLOR CODED WITH (1) SET OF 3" WIDE BANDS NEAR THE TOP-JUMPER CONNECTION AND WITH (1) SET OF 3/4" WIDE COLOR BANDS JUST PRIOR TO ENTERING THE BTS OR TRANSMITTER BUILDING. |  |  |  |  |  |
| 3  | CABLE ENTRY PORT ON THE INTERIOR OF THE SHELTER.   |  |  |  |  |  |
| 4  | ALL BOTTOM JUMPERS SHALL BE COLOR CODED WITH (1) SET OF 3/4" WIDE BANDS ON EACH END OF THE BOTTOM JUMPER.  |  |  |  |  |  |
| 5  | ALL BOTTOM JUMPERS SHALL BE COLOR CODED WITH (1) SET OF 3/4" WIDE BANDS ON EACH END OF THE BOTTOM JUMPER.  |  |  |  |  |  |

#### CABLE MARKING DIAGRAM

2 SCALE: N.T.S.

- 1. THE ANTENNA SYSTEM COAX SHALL BE LABELED WITH VINYL TAPE.
- 2. THE STANDARD IS BASED ON EIGHT COLORED TAPES-RED, BLUE, GREEN, YELLOW, ORANGE, BROWN, WHITE, AND VIOLET. THESE TAPES MUST BE 3/4" WIDE & UV RESISTANT SUCH AS SCOTCH 35 VINYL ELECTRICAL COLOR CODING TAPE AND SHOULD BE READILY AVAILABLE TO THE ELECTRICIAN OR CONTRACTOR ON SITE.
- 3. USING COLOR BANDS ON THE CABLES, MARK ALL RF CABLE BY SECTOR AND CABLE NUMBER AS SHOWN ON "CABLE COLOR CHART"
- WHEN AN EXISTING COAXIAL LINE THAT IS INTENDED TO BE A SHARED LINE BETWEEN TECHNOLOGIES IS ENCOUNTERED, THE CONTRACTOR SHALL REMOVE THE EXISTING COLOR CODING SCHEME AND REPLACE IT WITH THE COLOR CODING STANDARD. IN THE ABSENCE OF AN EXISTING COLOR CODING AND TAGGING SCHEME, OR WHEN INSTALLING PROPOSED COAXIAL CABLES, THIS GUIDELINE SHALL BE IMPLEMENTED AT THAT SITE REGARDLESS OF TECHNOLOGY.
- ALL COLOR CODE TAPE SHALL BE 3M-35 AND SHALL BE INSTALLED USING A MINIMUM OF (3) THREE WRAPS OF TAPE AND SHALL BE NEATLY TRIMMED AND SMOOTHED OUT SO AS TO AVOID UNRAVELING.
- 6. ALL COLOR BANDS INSTALLED AT THE TOP OF THE TOWER SHALL BE A MINIMUM OF 3" WIDE, AND SHALL HAVE A MINIMUM OF 3/4" OF SPACE BETWEEN EACH COLOR.
- 7. ALL COLOR CODES SHALL BE INSTALLED SO AS TO ALIGN NEATLY WITH ONE ANOTHER FROM SIDE-TO-SIDE.
- IF EXISTING CABLES AT THE SITE ALREADY HAVE A COLOR CODING SCHEME AND THEY ARE NOT INTENDED TO BE REUSED OR SHARED WITH THE NEW TECHNOLOGY, THE EXISTING COLOR CODING SCHEME SHALL REMAIN UNTOUCHED.





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| REV | DATE     | DESCRIPTION | BY |
|-----|----------|-------------|----|
| 0   | 04/27/22 | 90% REVIEW  | MS |
| 1   | 05/26/22 | REVISED 90% | SM |
| 2   | 6/2/22   | FINAL       | KR |
|     |          |             |    |
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|     |          |             |    |

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Jun 3 2022

SITE NAME

**STRATFORD ORONOQUE ROAD** 

SITE NUMBER:

CTL02638

SITE ADDRESS

200 ORONOQUE LANE STRATFORD, CT 06614

SHEET NAME

**CABLE NOTES** AND COLOR CODING

SHEET NUMBER

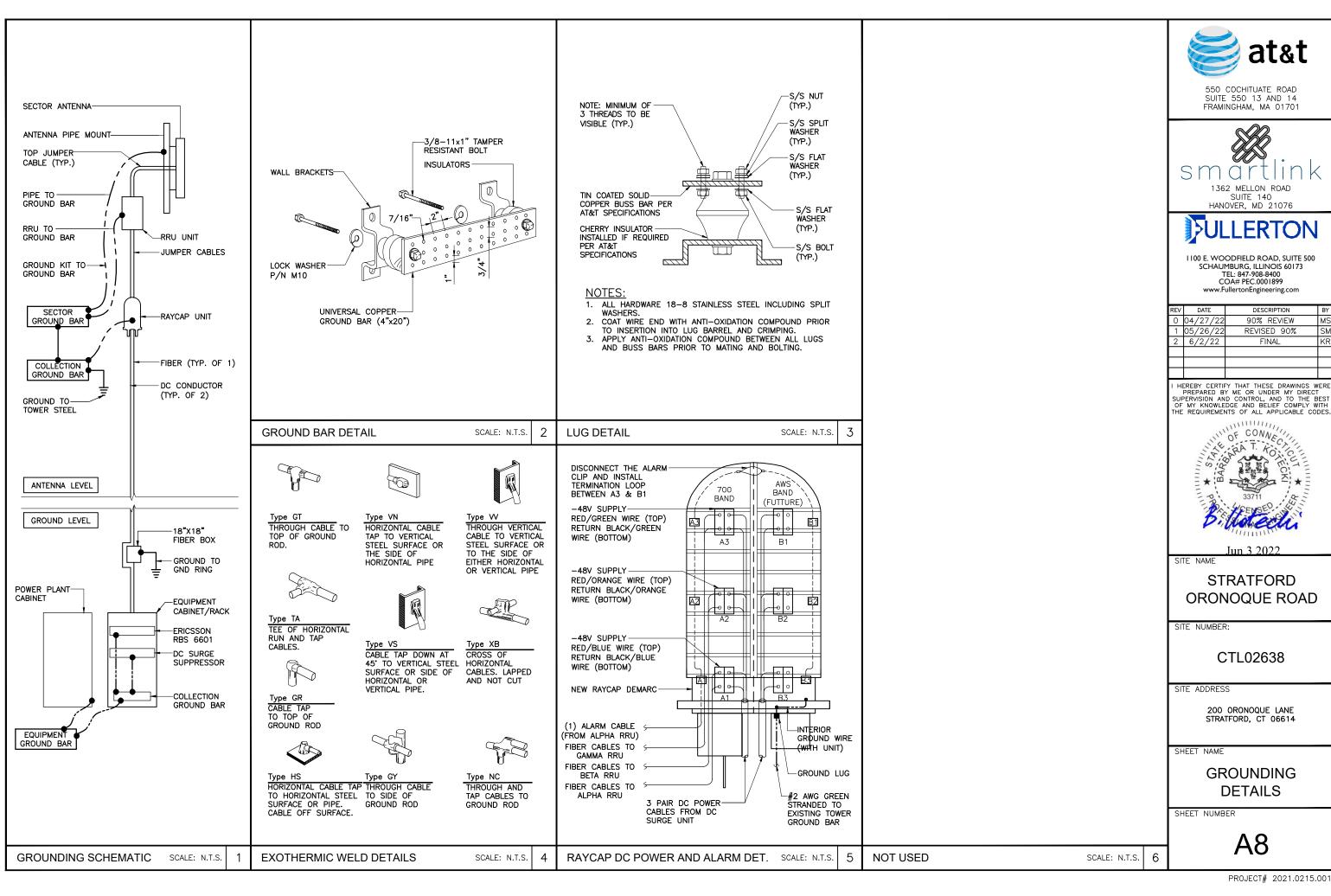
CABLE MARKING NOTES

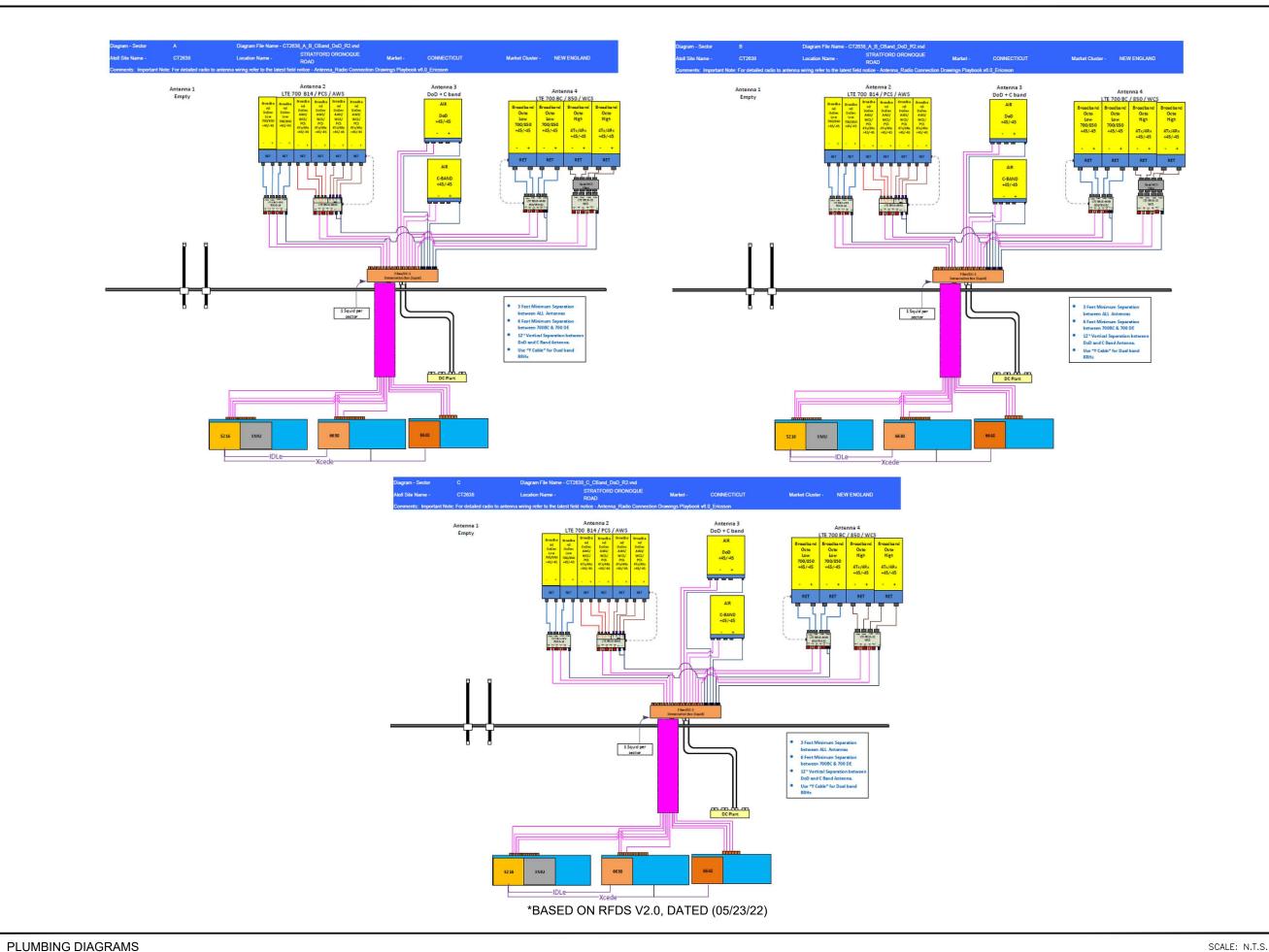
SCALE: N.T.S.

3

CABLE COLOR CODING DIAGRAM

SCALE: N.T.S.







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SITE NAME

# **STRATFORD** ORONOQUE ROAD

SITE NUMBER:

CTL02638

SITE ADDRESS

200 ORONOQUE LANE STRATFORD, CT 06614

SHEET NAME

#### PLUMBING DIAGRAMS

SHEET NUMBER

Showing 2 of 2

#### 777017276337







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