# JULIE D. KOHLER 

PLEASE REPLY TO: Bridgeport WRITER'S DIRECT DIAL: (203) 337-4157 E-Mail Address: jkohler@cohenandwolf.com

September 18, 2014

Attorney Melanie Bachman<br>Acting Executive Director Connecticut Siting Council<br>Ten Franklin Square<br>New Britain, CT 06051

## Re: Notice of Exempt Modification <br> Town of Stratford/T-Mobile co-location <br> T-Mobile Site ID CT11872D <br> 900 Longbrook Road, Stratford CT

## Dear Attorney Bachman:

This office represents T-Mobile Northeast LLC ("T-Mobile") and has been retained to file exempt modification filings with the Connecticut Siting Council on its behalf.

In this case, the Town of Stratford owns the existing telecommunications tower and related facility on the Stratford Police Department building, 900 Longbrook Road, Stratford Connecticut (latitude 41.20177, longitude -73.12885). T-Mobile intends to add three antennas and related equipment at this existing rooftop facility in Stratford ("Stratford Facility"). Please accept this letter as notification, pursuant to R.C.S.A. § 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the Mayor, John A. Harkins. The City of Stratford also owns the property.

The existing Stratford Facility consists of a rooftop mounted 50 foot guyed tower and associated compound area on the top of the Police Department building. T-Mobile plans to add three antennas and three remote radio units (RRUS) mounted on the rooftop facility at a centerline of 47 feet ( 79 feet AGL). (See the plans revised to September 15, 2014 attached hereto as Exhibit A). The existing rooftop facility is structurally capable of supporting TMobile's proposed use, as indicated in the structural certification dated September 12, 2014 and attached hereto as Exhibit B.

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Site ID CT11872D
Page 2

The planned modifications to the Stratford Facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modification will not increase the height of the tower. T-Mobile's proposed antennas and equipment will be installed at the 47 foot level. The enclosed plans confirm that the proposed modification will not increase the height of the rooftop facility.
2. The installation of the T-Mobile replacement equipment in the existing rooftop compound area, as reflected on Sheet A-1 of the attached plans, will not require an extension of the site boundaries. T-Mobile's proposed equipment will be located entirely within the existing compound area.
3. The proposed modification to the Facility will not increase the noise levels at the existing facility by six decibels or more.
4. The operation of the replacement antennas will not increase the total radio frequency (RF) power density, measured at the base of the tower, to a level at or above the applicable standard. According to a Radio Frequency Emissions Analysis Report prepared by EBI dated September 16, 2014 T-Mobile's operations would add $22.65 \%$ of the FCC Standard. Therefore, the calculated "worst case" power density for the planned combined operation at the site including all of the proposed antennas would be $39.22 \%$ of the FCC Standard as calculated for a mixed frequency site as evidenced by the engineering exhibit attached hereto as Exhibit C.

For the foregoing reasons, T-Mobile respectfully submits that the proposed replacement antennas and equipment at the Strafford Facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Upon acknowledgement by the Council of this proposed exempt modification, T-Mobile shall commence construction approximately sixty days from the date of the Council's notice of acknowledgement.

Sincerely,


cc: Mayor John A. Harkins, Town of Stratford
Elizabeth Jamieson, Transcend Wireless

## EXHIBIT A






# STRUCTURAL ANALYSIS REPORT 

For
CT11872D
CT872/STRATFORD PD_GT
900 LONGBROOK ROAD STRATFORD, CT 06614
Antennas Mounted to the Tower


Prepared for:

Transcend Wireless


Dated: September 12, 2014


1600 Osgood Street Bldg. 20N Suite 3090
North Andover, MA 01845
(P) 978.557.5553 (F) 978.336.5586
www.hudsondesigngroupllc.com

## SCOPE OF WORK:

Hudson Design Group LLC (HDG) has been authorized by T-Mobile to conduct a structural evaluation of the 50' guyed tower supporting the existing and proposed TMobile's antennas located at elevation 79' above ground level.

This report represents this office's findings, conclusions and recommendations pertaining to the support of T-Mobile's existing and proposed antennas listed below.

Record drawings of the existing tower prepared by Radian Communication Services, dated June 21, 2005, were available for our use. The previous structural analysis report prepared by Tectonic Consultants, dated June 25, 2012, was also available and obtained for our use.

## CONCLUSION SUMMARY:

Based on our evaluation, we have determined that the existing tower is in conformance with the ANSI/TIA-222-F Standard for the loading considered under the criteria listed in this report. The tower structure is rated at $\mathbf{8 7 . 6 \%}$ - (Guys at EL.69.8' Controlling).

## APPURTANENCES CONFIGURATION:

| Tenant | Appurtenances | Elev. | Mount |
| :--- | :--- | :--- | :--- |
|  | $20^{\prime}$ Omni | $92^{\prime}$ | T-Frame |
|  | $16^{\prime}$ Omni | $90^{\prime}$ | T-Frame |
|  | $6^{\prime}$ Dipole | $80^{\prime}$ | T-Frame |
| T-Mobile | (6) AlR 21 Antennas | $79^{\prime}$ | T-Frame |
| T-Mobile | (3) TMA | $79^{\prime}$ | T-Frame |
| T-Mobile | (3) LNX-6515DS-VTM Antennas | $79^{\prime}$ | T-Frame |
| T-Mobile | (3) RRUS-11 | $79^{\prime}$ | T-Frame |
|  | (2) 3' Yagi | $74^{\prime}$ | Tower Leg |
|  | $3^{\prime}$ Yagi | $68^{\prime}$ | Tower Leg |
|  | Ground Plane Omni | $64^{\prime}$ | Side Mount Standoff |
|  | $3^{\prime}$ Yagi | $62^{\prime}$ | Tower Leg |

*Proposed T-Mobile Appurtenances shown in Bold.

## T-MOBILE EXISTING/PROPOSED COAX CABLES:

| Tenant | Coax Cables | Elev. | Mount |
| :---: | :--- | :---: | :--- |
| T-Mobile | (24) $7 / 8^{\prime \prime}$ Cables | $\mathbf{7 9}$ | Tower Face |
| T-Mobile | (1) $75 / 8^{\prime \prime}$ Cable | $\mathbf{7 9}$ | Tower Face |

*Proposed T-Mobile Appurtenances shown in Bold.

ANALYSIS RESULTS SUMMARY:

| Component | Max. Stress <br> Ratio | Elev. of Component <br> (ft) | Pass/Fail | Notes/Comments |
| :---: | :---: | :---: | :---: | :---: |
| Legs | $26.2 \%$ | $67-82$ | PASS |  |
| Diagonals | $42.4 \%$ | $52-67$ | PASS |  |
| Top Girts | $16.2 \%$ | $52-67$ | PASS |  |
| Bottom Girts | $17.8 \%$ | $32-37$ | PASS |  |
| Mid Girts | $0.5 \%$ | $32-37$ | PASS |  |
| Guy A | $87.6 \%$ | 69.8 | PASS | Controlling |
| Guy B | $82.2 \%$ | 69.8 | PASS |  |
| Guy C | $83.0 \%$ | 69.8 | PASS |  |
| Torque Arm | $40.9 \%$ | 69.8 | PASS |  |

## DESIGN CRITERIA:

1. EIA/TIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures

County: Fairfield Wind Load: 90 mph (fastest mile)

110 mph ( 3 second gust)
Nominal lce Thickness: 0.5 inch
2. Approximate height above grade to proposed antennas: 79'
*Calculations and referenced documents are attached*

## ASSUMPTIONS:

1. The tower geometry, member sizes and material strength are as indicated in the record drawings of the existing tower prepared by Radian Communication Services, dated June 21, 2005.
2. The appurtenances configuration is as stated in the previous structural analysis report prepared by Tectonic Consultants, dated June 25, 2012. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer requirements.
3. The tower and supports are properly constructed and maintained. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
4. The support mounts and platforms are not analyzed and are considered adequate to support the loading. The analysis is limited to the primary support structure itself.
5. All prior structural modification, if any, are assumed to be as per the data supplied (if available), and installed properly.

## SUPPORT RECOMMENDATIONS:

HDG recommends that the proposed antennas and RRHs be mounted on the existing Tframe supported by the tower.

Reference HDG's Latest Construction Drawings for all component and connection requirements (attached).

## ONGOING AND PERIODIC INSPTECTION AND MAINTENANCE:

After the Contractor has successfully completed the installation and the work has been accepted, the Owner will be responsible for the ongoing and periodic inspection and maintenance of the tower.

The owner shall refer to TIA/EIA-222-F for recommendations for maintenance and inspection. The frequency of the inspection and maintenance intervals is to be determined by the owner based upon actual site and environmental conditions. It is recommended that a complete and thorough inspection of the entire tower structural system be performed at least yearly and more frequently as conditions warrant. According to TIA/EIA-222-F section 14.1, Note 1: It is recommended that the structure be inspected after severe wind and/or ice storms or other extreme loading conditions.


Photo 1: Photo illustrating the Tower with Appurtenances shown.


## CALCULATIONS


32.0 ft

52.0 f
37.0 ft


| TYPE | ELEVATION | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| Omni $21 / 2^{\prime \prime} \times 20^{\prime}$ | 82 | Andrew LNX-6515DS-VTM wfmount | 79 |
| Omni $21 / 22^{\prime \prime} 1^{\prime} 6^{\prime}$ | 82 | pipe |  |
| 6' Dipole | 80 | Ericsson RRUS-11 | 79 |
| SM 409-3 (T-MOBILE- existing) | 79 | Ericsson RRUS-11 | 79 |
| (2) Air 21 antenna wimount pipe | 79 | Ericsson RRUS-11 | 79 |
| (2) Air 21 antenna wimount pipe | 79 | 3' Yagi antenna | 74 |
| (2) Air 21 antenna w/mount pipe | 79 | 3' Yagi antenna | 74 |
| Style 3 TMA | 79 | 3' Yagi antenna | 68 |
| Style 3 TMA | 79 | 3' Yagi antenna | 62 |
| Style 3 TMA | 79 | Pirod 6' Side Mount Standoff (1) | 61 |
| Andrew LNX-6515DS-VTM w/mount pipe (T-MOBILE - proposed) | 79 | Ground Plane Omni | 61 |
| Andrew LNX-6515DS-VTM w/mount pipe | 79 |  |  |

MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A572-42 | 42 ksi | 60 ksi | A36 | 36 ksi | 58 ksi |

TOWER DESIGN NOTES

1. Tower is located in Fairfield County, Connecticut.
. Tower designed for a 90 mph basic wind in accordance with the TIA/EIA-222-F Standard.
2. Tower is also designed for a 78 mph basic wind with 0.50 in ice.
3. Deflections are based upon a 50 mph wind.
4. TOWER RATING: $87.6 \%$

Hudson Design Group, LLC
1600 Osgood Street, Building 20 North, Suite 3090
Client: T-MOBILE

| ThXTOWEF | Job | PT11872D | Stratford, CT |
| :---: | :--- | :---: | :--- |

## Tower Input Data

The main tower is a $3 x$ guyed tower with an overall height of 82.00 ft above the ground line.
The base of the tower is set at an elevation of 32.00 ft above the ground line.
The face width of the tower is 3.42 ft at the top and tapered at the base.
This tower is designed using the TIA/EIA-222-F standard.
The following design criteria apply:
Tower is located in Fairfield County, Connecticut.
Basic wind speed of 90 mph .
Nominal ice thickness of 0.5000 in .
Ice density of 56 pcf .
A wind speed of 78 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 50 mph .
Pressures are calculated at each section.
Safety factor used in guy design is 2 .
Stress ratio used in tower member design is 1.333 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Tower Section Geometry

| Tower Section | Tower Elevation | Assembly <br> Database | Description | Section Width | Number of Sections | Section Length |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  |  | ft |  | $f t$ |
| T1 | 82.00-67.00 |  |  | 3.42 | 1 | 15.00 |
| T2 | 67.00-52.00 |  |  | 3.42 | 1 | 15.00 |
| T3 | 52.00-37.00 |  |  | 3.42 | 1 | 15.00 |
| T4 | 37.00-32.00 |  |  | 3.42 | 1 | 5.00 |

## Tower Section Geometry (cont'd)

| Tower <br> Section | Tower <br> Elevation | Diagonal <br> Spacing | Bracing <br> Type | Has <br> K Brace <br> End | Has <br> Horizontals | Top Girt <br> Offset | Bottom Girt <br> Offset |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | ft |  |  | Panels |  | in |

## Tower Section Geometry (cont'd)

| Tower <br> Elevation <br> $f t$ | Leg <br> Type | Size | Leg <br> Grade | Diagonal <br> Type | Diagonal <br> Size | Diagonal <br> Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 82.00-67.00 | Pipe | P2.5×.276 | A572-42 | Pipe | P1.5x.120 | A36 |


| tnxTower | Job | CT11872D | Stratford, CT | $\begin{aligned} & \text { Page } \\ & 2 \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Project 50 ft Guyed Tower |  |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 18:24:34 09/11/14 } \end{array}$ |
|  | Client |  | BILE | Designed by <br> kw |


| Tower Elevation $f t$ | $\begin{aligned} & \text { Leg } \\ & \text { Type } \end{aligned}$ | $\begin{aligned} & \text { Leg } \\ & \text { Size } \end{aligned}$ | Leg Grade | Diagonal Type | $\begin{aligned} & \text { Diagonal } \\ & \text { Size } \end{aligned}$ | Diagonal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | (42 ksi) |  |  | (36 ksi) |
| T2 67.00-52.00 | Pipe | P2.5x. 276 | $\begin{aligned} & \text { A572-42 } \\ & (42 \mathrm{ksi}) \end{aligned}$ | Pipe | P1.5x. 120 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T3 52.00-37.00 | Pipe | P2.5x. 276 | $\begin{aligned} & \text { AS72-42 } \\ & (42 \mathrm{ksi}) \end{aligned}$ | Pipe | P1.5x. 120 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T4 37.00-32.00 | Pipe | P2.5x. 276 | $\begin{gathered} \text { A572-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ | Pipe |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |

Tower Section Geometry (cont'd)

| Tower Elevation $f t$ | Top Girt Type | $\begin{gathered} \text { Top Girt } \\ \text { Size } \end{gathered}$ | Top Girt Grade | $\begin{aligned} & \text { Bottom Girt } \\ & \text { Type } \end{aligned}$ | $\begin{gathered} \text { Bottom Girt } \\ \text { Size } \end{gathered}$ | Bottom Girt Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 82.00-67.00 | Pipe | P1.5x. 120 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.5x. 120 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T2 67.00-52.00 | Pipe | P1.5x. 120 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.5x. 120 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T3 52.00-37.00 | Pipe | P1.5x. 120 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.5x, 120 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T4 37.00-32.00 | Equal Angle | L3x3x3/16 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Equal Angle | L3 $3 \times 3 \times 16$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |

Tower Section Geometry (cont'd)

| Tower Elevation <br> ft | No. of Mid Girts | Mid Girt Type | Mid Girt Size | Mid Girt Grade | Horizontal Type | Horizontal Size | Horizontal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T4 37.00-32.00 | 2 | Equal Angle | L3x3x3/16 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Equal Angle |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |

## Guy Data

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Guy Elevation \\
\(f t\)
\end{tabular} \& Guy Grade \& \& Guy Size \& Initial Tension
\[
l b
\] \& \% \& Guy Modulus
\[
k s i
\] \& \begin{tabular}{l}
Guy Weight \\
plf
\end{tabular} \& \(L_{u}\)

$f t$ \& | Anchor Radius |
| :--- |
| ft | \& Anchor Azimuth Adj. \& | Anchor Elevation |
| :--- |
| $f t$ | \& End Fitting Efficiency \% <br>

\hline \multirow[t]{3}{*}{69.8194} \& \multirow[t]{3}{*}{EHS} \& A \& 7/16 \& 2080.00 \& 10\% \& 21000 \& 0.399 \& 77.06 \& 60.75 \& 0.0000 \& 20.00 \& 100\% <br>
\hline \& \& B \& 7/16 \& 2080.00 \& 10\% \& 21000 \& 0,399 \& 64.70 \& 54.42 \& 0.0000 \& 32.00 \& 100\% <br>
\hline \& \& C \& 7/16 \& 2080.00 \& 10\% \& 21000 \& 0.399 \& 64.90 \& 54.67 \& 0.0000 \& 32.00 \& 100\% <br>
\hline
\end{tabular}

| Guy Data(cont'd) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Guy | Mount | Torque-Arm | Torque-Arm | Torque-Arm | Torque-Arm | Torque-Arm | Torque-Arm Size |
| Elevation <br> $f t$ | Type | Spread | Leg Angle | Style | Grade | Type |  |
|  |  | $f$ | - |  |  |  |  |


| InxTower | Job | CT11872D | Stratford, CT | $\begin{aligned} & \text { Page } \\ & \\ & \\ & \hline \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| Hudson Design Group, LLC <br> 1600 Osgood Street, Building 20 North, <br> Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | 50 ft Guyed Tower |  |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 18:24:34 09/11/14 } \end{array}$ |
|  | Client |  | OBILE | Designed by kw |


| Guy Elevation ft | $\begin{aligned} & \text { Mount } \\ & \text { Type } \end{aligned}$ | Torque-Arm Spread | Torque-Arm Leg Angle | Torque-Arm Style | Torque-Arm Grade | Torque-Arm Type | Torque-Arm Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 69.8194 | Torque Arm | 6.83 | 0.0000 | Channel | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Channel | C12×20.7 |

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \\ \hline \end{gathered}$ | Allow Shield | Component Type | Placement $\qquad$ <br> $f t$ | Total Number | Number Per Row | Clear Spacing in | Width or Diameter $\qquad$ in | Perimeter <br> in | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7/8 | A | Yes | Ar (CfAe) | 61.00-32.00 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 7/8 | A | Yes | Ar (CfAe) | 62.00-32.00 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 7/8 | A | Yes | Ar (CfAe) | 68.00-32.00 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 7/8 | A | Yes | Ar (CfAe) | 74.00-32.00 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 7/8 | A | Yes | Ar (CfAe) | 74.00-32.00 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 7/8 | A | Yes | Ar (CfAe) | 79.00-32.00 | 24 | 12 | 1.1100 | 1.1100 |  | 0.54 |
| $\begin{aligned} & \text { (T-MOBILE - existing) } \\ & 15 / 8 \text { Fiber Cable } \\ & \text { (T-MOBILE - existing) } \end{aligned}$ | A | Yes | Ar (CfAe) | 79.00-32.00 | 1 | 1 | 1.9800 | 1.9800 |  | 1.04 |
| 7/8 | A | Yes | Ar (CfAe) | 82.00-32.00 | 2 | 2 | 1.1100 | 1.1100 |  | 0.54 |
| Safety Line 3/8 | A | Yes | Ar (CfAe) | 82.00-32.00 | 1 | 1 | 0.3750 | 0.3750 |  | 0.22 |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) Front \\
\(f t^{2}\)
\end{tabular} \& \(C_{A} A_{A}\) Side \(f t^{2}\) \& Weight

$l b$ <br>

\hline Omni $21 / 2^{\prime \prime} \times 20^{\prime}$ \& B \& From Leg \& \[
$$
\begin{gathered}
4.00 \\
0.00 \\
10.00
\end{gathered}
$$

\] \& 0.0000 \& 82.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{1} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.00 \\
& 7.03
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.00 \\
& 7.03
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 40.00 \\
& 76.96
\end{aligned}
$$
\] <br>

\hline Omni $21 / 2^{\prime \prime} \times 16^{\prime}$ \& B \& From Leg \& \[
$$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 8.00
\end{aligned}
$$

\] \& 0.0000 \& 82.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{11} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.00 \\
& 5.63
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.00 \\
& 5.63
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 35.00 \\
& 64.63
\end{aligned}
$$
\] <br>

\hline $6{ }^{6}$ Dipole \& A \& From Leg \& \[
$$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 80.00 \& No Ice $1 / 2^{\text {" }}$ Ice \& \[

$$
\begin{aligned}
& 0.90 \\
& 1.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.90 \\
& 1.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 15.00 \\
& 22.49
\end{aligned}
$$
\] <br>

\hline ************ \& \& \& \& \& \& \& \& \& <br>

\hline $$
\begin{gathered}
\text { SM 409-3 } \\
\text { (T-MOBILE - existing) }
\end{gathered}
$$ \& A \& None \& \& 0.0000 \& 79.00 \& No Ice

$$
1 / 2^{11} \text { Ice }
$$ \& \& \[

$$
\begin{aligned}
& 22.47 \\
& 31.99
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1035.00 \\
& 1500.00
\end{aligned}
$$
\] <br>

\hline (2) Air 21 antenna w/mount pipe \& A \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 79.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.74 \\
& 7.30
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.60 \\
& 6.50
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 101.90 \\
& 158.52
\end{aligned}
$$
\] <br>

\hline (2) Air 21 antenna w/mount pipe \& B \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 79.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.74 \\
& 7.30
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.60 \\
& 6.50
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 101.90 \\
& 158.52
\end{aligned}
$$
\] <br>

\hline (2) Air 21 antenna w/mount pipe \& C \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 79.00 \& No Ice $1 / 2^{\prime \prime}$ Ice \& \[

$$
\begin{aligned}
& 6.74 \\
& 7.30
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.60 \\
& 6.50
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 101.90 \\
& 158.52
\end{aligned}
$$
\] <br>

\hline Style 3 TMA \& A \& From Leg \& \[
$$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 79.00 \& | No Ice |
| :--- |
| $1 / 2^{\prime \prime}$ Ice | \& \[

$$
\begin{aligned}
& 0.78 \\
& 0.90
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.21 \\
& 0.30
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 11.30 \\
& 15.86
\end{aligned}
$$
\] <br>

\hline
\end{tabular}

| tnxTower <br> Hudson Design Group, LLC 1600 Osgood Street, Building 20 North Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Job | CT11872D | Stratford, CT | $\begin{aligned} & \text { Page } 4 \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
|  | Project | 50 ft Gu | ed Tower | $\begin{array}{\|l\|} \text { Date } \\ \text { 18:24:34 09/11/14 } \end{array}$ |
|  | Client |  | BILE | Designed by kw |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | $\begin{aligned} & \text { Offset } \\ & \text { Type } \end{aligned}$ | Offsets: <br> Horz Lateral Vert $f t$ $f$ | Azimuth Adjustment <br> - | Placement |  | $C_{A} A_{A}$ Front $f t^{2}$ | $C_{A A}$ <br> Side <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Style 3 TMA | B | From Leg | 4.00 | 0.0000 | 79.00 | No Ice | 0.78 | 0.21 | 11.30 |
|  |  |  | 0.00 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 0.90 | 0.30 | 15.86 |
| Style 3 TMA | C | From Leg | 4.00 | 0.0000 | 79.00 | No Ice | 0.78 | 0.21 | 11.30 |
|  |  |  | 0.00 |  |  | $1 / 2^{\text {1 }}$ Ice | 0.90 | 0.30 | 15.86 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| ************ |  |  |  |  |  |  |  |  |  |
| Andrew LNX-6515DS-VTM w/mount pipe <br> (T-MOBLLE - proposed) | A | From Leg | 4.00 | 0.0000 | 79.00 | No Ice | 11.72 | 10.28 | 102.41 |
|  |  |  | 0,00 |  |  | 1/2" Ice | 12.44 | 11.81 | 196.22 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| Andrew LNX-6515DS-VTM w/mount pipe | B | From Leg | 4.00 | 0.0000 | 79.00 | No Ice | 11.72 | 10.28 | 102.41 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 12.44 | 11.81 | 196.22 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| Andrew LNX-6515DS-VTM w/mount pipe | C | From Leg | 4.00 | 0.0000 | 79.00 | No Ice | 11.72 | 10.28 | 102.41 |
|  |  |  | 0.00 |  |  | 1/2' Ice | 12.44 | 11.81 | 196.22 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| Ericsson RRUS-11 | A | From Leg | 3.00 | 0.0000 | 79.00 | No Ice | 3.26 | 1.38 | 50.70 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 3.50 | 1.56 | 71.57 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| Ericsson RRUS-11 | B | From Leg | 3.00 | 0.0000 | 79.00 | No Ice | 3.26 | 1.38 | 50.70 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 3.50 | 1.56 | 71.57 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| Ericsson RRUS-11 | C | From Leg | 3.00 | 0.0000 | 79.00 | No Ice | 3.26 | 1.38 | 50.70 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 3.50 | 1.56 | 71.57 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| ************ |  |  |  |  |  |  |  |  |  |
| 3' Yagi antenna | A | From Leg | 2.00 | 0.0000 | 74.00 | No Ice | 0.70 | 0.35 | 10.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 0.95 | 0.48 | 36.35 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| $3{ }^{1}$ Yagi antenna | B | From Leg | 2.00 | 0.0000 | 74.00 | No Ice | 0.70 | 0.35 | 10.00 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 0.95 | 0.48 | 36.35 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| 3' Yagi antenna | C | From Leg | 2.00 | 0.0000 | 68.00 | No Ice | 0.70 | 0.35 | 10.00 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 0.95 | 0.48 | 36.35 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| 3' Yagi antenna | C | From Leg | 2.00 | 0.0000 | 62.00 | No Ice | 0.70 | 0.35 | 10.00 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 0.95 | 0.48 | 36.35 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| Pirod 6' Side Mount Standoff <br> (1) | B | From Leg | 3.00 | 0.0000 | 61.00 | No Ice | 4.97 | 4.97 | 70.00 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 6.12 | 6.12 | 130.00 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| Ground Plane Omni | B | From Leg | 6.00 | 0.0000 | 61.00 | No Ice | 1.90 | 1.90 | 25.00 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 2.70 | 2.70 | 39.00 |
|  |  |  | 3.00 |  |  |  |  |  |  |

## Load Combinations

| Comb. <br> No. | Description |  |
| :---: | :--- | :--- |
| 1 | Dead Only |  |
| 2 | Dead+Wind 0 deg - No Ice+Guy |  |
| 3 | Dead+Wind 30 deg - No Ie+Guy |  |
| 4 | Dead+Wind 60 deg - No Iee+Guy |  |


| tnxTower <br> Hudson Design Group, LLC | Job | CT11872D | Stratford, CT | $\text { Page } 5 \text { of } 9$ |
| :---: | :---: | :---: | :---: | :---: |
| Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, Suite 3090 | 50 ft Guyed Tower |  |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 18:24:34 09/11/14 } \end{array}$ |
| $\begin{gathered} \text { North Andover, MA } 01845 \\ \text { Phone: (978) 557-5553 } \\ \text { FAX: (978) 226-5586 } \end{gathered}$ | Client | T-MOBILE |  | Designed by kw |


| Comb. No. |  | Description |
| :---: | :---: | :---: |
| 5 | Dead+Wind 90 deg - No Ice+Guy |  |
| 6 | Dead+Wind 120 deg - No Ice+Guy |  |
| 7 | Dead+Wind 150 deg - No Ice+Guy |  |
| 8 | Dead+Wind 180 deg - No Ice+Guy |  |
| 9 | Dead+Wind 210 deg - No Ice+Guy |  |
| 10 | Dead+Wind 240 deg - No Ice+Guy |  |
| 11 | Dead+Wind 270 deg - No Ice+Guy |  |
| 12 | Dead+Wind 300 deg - No Ice + Guy |  |
| 13 | Dead+Wind 330 deg - No Ice+Guy |  |
| 14 | Dead+Ice+Temp+Guy |  |
| 15 | Dead + Wind 0 deg + Ice + Temp+Guy |  |
| 16 | Dead + Wind 30 deg + Ice + Temp+Guy |  |
| 17 | Dead+Wind 60 deg+Ice + Temp+Guy |  |
| 18 | Dead+Wind 90 deg+Ice + Temp+Guy |  |
| 19 | Dead+Wind 120 deg+Ice+Temp+Guy |  |
| 20 | Dead+Wind 150 deg+Ice+Temp+Guy |  |
| 21 | Dead+Wind 180 deg+Ice+Temp+Guy |  |
| 22 | Dead + Wind 210 deg + Icc + Temp + Guy |  |
| 23 | Dead+Wind 240 deg+Ice +Temp+Guy |  |
| 24 | Dead + Wind 270 deg + Ice + Temp + Guy |  |
| 25 | Dead + Wind 300 deg + Ice + Temp + Guy |  |
| 26 | Dead+Wind 330 deg+Ice + Temp + Guy |  |
| 27 | Dead+Wind 0 deg - Service+Guy |  |
| 28 | Dead+Wind 30 deg - Service+Guy |  |
| 29 | Dead+Wind 60 deg - Service+Guy |  |
| 30 | Dead+Wind 90 deg - Service +Guy |  |
| 31 | Dead+Wind 120 deg - Service+Guy |  |
| 32 | Dead+Wind 150 deg - Service+Guy |  |
| 33 | Dead+Wind 180 deg - Service+Guy |  |
| 34 | Dead+Wind 210 deg - Service+Guy |  |
| 35 | Dead+Wind 240 deg - Service + Guy |  |
| 36 | Dead+Wind 270 deg - Service+Guy |  |
| 37 | Dead+Wind 300 deg - Service + Guy |  |
| 38 | Dead+Wind 330 deg - Service+Guy |  |


|  | Maximum Reactions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Condition | Gov. <br> Load <br> Comb. | Vertical $l b$ | $\begin{gathered} \text { Horizontal, } X \\ l b \end{gathered}$ | $\begin{gathered} \text { Horizontal, } Z \\ l b \end{gathered}$ |
| Mast | Max. Vert | 19 | 26538.47 | -1357.78 | -834.79 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 11 | 21326.39 | 2367.36 | 26.08 |
|  | Max. $\mathrm{H}_{\mathbf{z}}$ | 2 | 22525.53 | 42.47 | 2307.29 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 1 | 0.00 | 21.63 | -9.23 |
|  | Max. M ${ }_{z}$ | 1 | 0.00 | 21.63 | -9.23 |
|  | Max. Torsion | 8 | 576.25 | 53.05 | -2453.72 |
|  | Min. Vert | 33 | 13023.81 | 21.24 | -770.33 |
|  | Min. $\mathrm{H}_{x}$ | 5 | 21336.11 | -2322.25 | 24.76 |
|  | Min. $\mathrm{H}_{\mathbf{z}}$ | 8 | 17038.46 | 53.05 | -2453.72 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 1 | 0.00 | 21.63 | -9.23 |
|  | Min. $\mathrm{M}_{\mathrm{z}}$ | 1 | 0.00 | 21.63 | -9.23 |
|  | Min. Torsion | 16 | -448.62 | -786.63 | 1436.02 |
| Guy C @ 54.67 ft Elev 32 ft | Max. Vert | 10 | -23.35 | -19.27 | 11.11 |
| Azimuth 240 deg |  |  |  |  |  |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 10 | -23.35 | -19.27 | 11.11 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 3 | -9734.04 | -11835.68 | 6900.91 |
|  | Min. Vert | 3 | -9734.04 | -11835.68 | 6900.91 |


| HnXTOWer | Job | PT11872D | Stratford, CT |
| :---: | :--- | :---: | :--- |


| Location | Condition | Gov. <br> Load <br> Comb. | Vertical <br> $l b$ | Horizontal, $X$ <br> $l b$ | Horizontal, Z <br> Ib |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. $\mathrm{H}_{\mathrm{x}}$ | 5 | -9697.72 | -11868.68 |
| Guy B @ 54.42 ft | Min. $\mathrm{H}_{\mathrm{z}}$ | 10 | -23.35 | -19.27 | 6742.47 |
| Elev 32 ft | Max. Vert | 6 | -24.06 | 19.75 | 11.11 |
| Azimuth 120 deg |  |  |  |  | 11.36 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 11 | -9707.92 | 11825.02 |  |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 13 | -9762.06 | 11796.08 | 6717.14 |
|  | Min. Vert | 13 | -9762.06 | 11796.08 | 6918.59 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 6 | -24.06 | 6918.59 |  |
| Guy A @60.75 ft | Min. $\mathrm{H}_{\mathrm{z}}$ | 6 | -24.06 | 19.75 | 11.36 |
| Elev 20 ft | Max. Vert | 2 | -80.23 | 19.75 | 11.36 |
| Azimuth 0 deg |  |  |  | 0.07 | -71.61 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 24 | -5531.33 |  |  |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 2 | -80.23 | 244.87 | -6622.87 |
|  | Min. Vert | 7 | -11388.15 | 0.07 | -71.61 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 18 | -5562.82 | -95.81 | -13594.19 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 7 | -11388.15 | -945.31 | -6650.19 |
|  |  |  |  | -95.81 | -13594.19 |

## Tower Mast Reaction Summary

| Load Combination | Vertical <br> lb | Shear $r_{x}$ <br> lb | Shear $x_{x}$ <br> $l b$ | Overturning Moment, $M_{x}$ $l b-f t$ | Overturning Moment, $M_{z}$ $l b-f t$ | Torque <br> $l b-f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 13199.70 | -21.63 | 9.23 | 0.00 | 0.00 | 9.26 |
| Dead+Wind 0 deg - No | 22525.53 | -42.47 | -2307.29 | 0.00 | 0.00 | 358.77 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 30 deg - No | 20641.36 | 1159.23 | -2018.79 | 0.00 | 0.00 | 410.06 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 60 deg - No | 16302.36 | 2059.94 | -1220.50 | 0.00 | 0.00 | 422.84 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 90 deg - No | 21336.11 | 2322.25 | -24.76 | 0.00 | 0.00 | 130.43 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 120 deg - No | 23910.15 | 1947.32 | 1178.09 | 0.00 | 0.00 | -98.00 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 150 deg - No | 22175.96 | 1088.46 | 2092.29 | 0.00 | 0.00 | -292.72 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 180 deg - No | 17038.46 | -53.05 | 2453.72 | 0.00 | 0.00 | -576.25 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 210 deg - No | 22131.64 | -1148.26 | 2059.30 | 0.00 | 0.00 | -333.72 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 240 deg - No | 23884.12 | -2000.87 | 1157.88 | 0.00 | 0.00 | $-246.05$ |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 270 deg - No | 21326.39 | -2367.36 | -26.08 | 0.00 | 0.00 | -101.65 |
| Ice+Guy |  |  |  |  |  |  |
| Dead + Wind 300 deg - No | 16311.50 | -2116.06 | -1203.38 | 0.00 | 0.00 | 39.39 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Wind 330 deg - No | 20664.76 | -1238.01 | -2018.53 | 0.00 | 0.00 | 214.72 |
| Ice+Guy |  |  |  |  |  |  |
| Dead+Ice+Temp+Guy | 19182.94 | -37.25 | 3.72 | 0.00 | 0.00 | 12.95 |
| Dead+Wind 0 | 25504.33 | -58.01 | -1646.15 | 0.00 | 0.00 | 368.78 |
| deg+Ice+Temp+Guy |  |  |  |  |  |  |
| Dead+Wind 30 | 24537.18 | 786.63 | -1436.02 | 0.00 | 0.00 | 448.62 |
| deg+lce+Temp+Guy <br> Dead+Wind 60 |  |  |  |  |  |  |
|  | 22576.56 | 1422.99 | -854.34 | 0.00 | 0.00 | 372.84 |
| deg+Ice+Temp+Guy |  |  |  |  |  |  |


| tnxTower <br> Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Job | CT11872D | Stratford, CT | Page 7 of 9 |
| :---: | :---: | :---: | :---: | :---: |
|  | Project | 50 ft G | ed Tower | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 18:24:34 09/11/14 } \end{array}$ |
|  | Client |  | OBILE | Designed by kw |


| Load Combination | Vertical <br> lb | Shear $x_{x}$ <br> $l b$ | Shear $z_{z}$ <br> lb | Overturning Moment, $M_{x}$ $l b-f t$ | Overturning Moment, $M_{z}$ $l b-f t$ | Torque <br> $l b-f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead+Wind 90 deg+Ice+Temp+Guy | 24840.92 | 1620.43 | -16.07 | 0.00 | 0.00 | 120.21 |
| Dead+Wind 120 deg+Ice+Temp+Guy | 26538.47 | 1357.78 | 834.79 | 0.00 | 0.00 | -81.26 |
| Dead + Wind 150 deg+Ice+Temp+Guy | 25516.42 | 746.00 | 1477.65 | 0.00 | 0.00 | -256.64 |
| Dead+Wind 180 deg+Ice+Temp+Guy | 22698.14 | -59.01 | 1721.24 | 0.00 | 0.00 | -490.11 |
| Dead+Wind 210 deg+Ice+Temp+Guy | 25433.55 | -839.60 | 1446.50 | 0.00 | 0.00 | -400.10 |
| Dead+Wind 240 deg+Ice + Temp+Guy | 26465.02 | -1443.06 | 814.54 | 0.00 | 0.00 | -273.24 |
| Dead+Wind 270 <br> deg+Ice+Temp+Guy | 24796.74 | -1697.02 | -17.11 | 0.00 | 0.00 | -88.74 |
| Dead+Wind 300 deg+Ice+Temp+Guy | 22586.49 | -1507.99 | -842.51 | 0.00 | 0.00 | 55.39 |
| Dead+Wind 330 deg+Ice+Temp+Guy | 24560.19 | -894.86 | -1433.48 | 0.00 | 0.00 | 199.09 |
| Dead+Wind 0 deg Service+Guy | 13459.72 | $-22.71$ | -753.02 | 0.00 | 0.00 | 96.86 |
| Dead+Wind 30 deg Service+Guy | 13431.38 | 353.71 | -650.77 | 0.00 | 0.00 | 107.29 |
| Dead+Wind 60 deg Service+Guy | 13355.76 | 629.79 | -371.78 | 0.00 | 0.00 | 87.75 |
| Dead+Wind 90 deg Service+Guy | 13241.44 | 731.63 | 9.12 | 0.00 | 0.00 | 46.73 |
| Dead+Wind 120 deg Service+Gụy | 13144.97 | 631.22 | 390.21 | 0.00 | 0.00 | -1.78 |
| Dead+Wind 150 deg Service + Guy | 13053.43 | 355.62 | 668.87 | 0.00 | 0.00 | -46.59 |
| Dead + Wind 180 deg Service+Guy | 13023.81 | -21.24 | 770.33 | 0.00 | 0.00 | -80.46 |
| Dead+Wind 210 deg Service+Guy | 13059.77 | -398.33 | 667.85 | 0.00 | 0.00 | -91.48 |
| Dead+Wind 240 deg Service+Guy | 13155.33 | -674.27 | 389.06 | 0.00 | 0.00 | -71.08 |
| Dead+Wind 270 deg Service+Guy | 13254.56 | -775.05 | 8.67 | 0.00 | 0.00 | $-28.53$ |
| Dead+Wind 300 deg Service+Guy | 13367.38 | -674.09 | -371.98 | 0.00 | 0.00 | 18.69 |
| Dead+Wind 330 deg Service+Guy | 13437.64 | -398.82 | -650.86 | 0.00 | 0.00 | 63.13 |

Solution Summary

| Load <br> Comb. | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PX | PY | PZ | PX | PY | PZ |  |
|  | $1 b$ | $1 b$ | $1 b$ | $1 b$ | $l b$ | $7 b$ |  |
| 1 | 0.00 | -5727.63 | 0.00 | 0.03 | 5727.62 | 0.21 | 0.004\% |
| 2 | -0.26 | -5738.10 | -14182.42 | 0.25 | 5738.07 | 14182.34 | 0.001\% |
| 3 | 7091.46 | -5715.31 | -12278.34 | -7091.47 | 5715.25 | 12278.04 | 0.002\% |
| 4 | 12282.22 | -5695.46 | -7089.67 | -12282.39 | 5695.45 | 7089.27 | 0.003\% |
| 5 | 14183.09 | -5727.63 | 0.16 | -14182.92 | 5727.57 | -0.03 | 0.001\% |
| 6 | 12287.61 | -5759.77 | 7093.07 | -12287.33 | 5759.66 | -7092.88 | 0.002\% |
| 7 | 7091.90 | -5739.94 | 12278.78 | -7091.68 | 5739.86 | -12278.62 | 0.002\% |
| 8 | 0.26 | -5717.16 | 14176.53 | 0.42 | 5717.15 | -14176.49 | 0.004\% |
| 9 | -7091.46 | -5739.94 | 12278.34 | 7091.24 | 5739.86 | -12278.19 | 0.002\% |


| tnxTower <br> Hudson Design Group, LLC | Job | CT11872D | Stratford, CT | $\begin{aligned} & \text { Page } 8 \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, Suite 3090 | 50 ft Guyed Tower |  |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 18:24:34 09/11/14 } \end{array}$ |
| North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | T-MOBILE |  |  | Designed by kw |


|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | PX | PY | PZ | PX | PY | PZ |  |
| Comb. | $l b$ | $l b$ | $1 b$ | Ib | $l b$ | 16 |  |
| 10 | -12287.32 | -5759.79 | 7092.62 | 12287.05 | 5759.68 | -7092.43 | 0.002\% |
| 11 | -14183.09 | -5727.62 | -0.16 | 14182.92 | 5727.57 | 0.28 | 0.001\% |
| 12 | -12282.50 | -5695.48 | -7090.13 | 12282.77 | 5695.46 | 7089.50 | 0.004\% |
| 13 | -7091.90 | -5715.31 | -12278.78 | 7091.90 | 5715.24 | 12278.48 | 0.002\% |
| 14 | 0.00 | -9845.02 | 0.00 | 0.01 | 9845.02 | 0.13 | 0.001\% |
| 15 | -0.63 | -9870.82 | -12663.78 | 0.63 | 9870.76 | 12663.54 | 0.002\% |
| 16 | 6337.08 | -9814.68 | -10965.21 | -6337.09 | 9814.65 | 10965.06 | 0.001\% |
| 17 | 10977.42 | -9765.76 | -6334.19 | -10977.42 | 9765.74 | 6333.85 | 0.002\% |
| 18 | 12674.57 | -9845.03 | 0.39 | -12674.47 | 9845.00 | -0.31 | 0.001\% |
| 19 | 10980.13 | -9924.24 | 6336.48 | -10979.95 | 9924.17 | -6336.34 | 0.001\% |
| 20 | 6338.16 | -9875.37 | 10966.30 | -6338.02 | 9875.32 | -10966.21 | 0.001\% |
| 21 | 0.63 | -9819.23 | 12661.45 | -0.30 | 9819.19 | -12661.24 | 0.002\% |
| 22 | -6337.08 | -9875.36 | 10965.21 | 6336.94 | 9875.32 | -10965.12 | 0.001\% |
| 23 | -10979.44 | -9924.29 | 6335.35 | 10979.25 | 9924.22 | -6335.22 | 0.001\% |
| 24 | -12674.57 | -9845.02 | -0.39 | 12674.47 | 9844.99 | 0.47 | 0.001\% |
| 25 | -10978.11 | -9765.81 | -6335.31 | 10978.17 | 9765.79 | 633484 | 0.003\% |
| 26 | -6338.16 | -9814.68 | -10966.30 | 6338.16 | 9814.65 | 10966.15 | 0.001\% |
| 27 | -0.08 | -5730.86 | -4377.29 | 0.08 | 5730.85 | 4376.98 | 0.004\% |
| 28 | 2188.72 | -5723.83 | -3789.61 | -2188.78 | 5723.82 | 3789.32 | 0.004\% |
| 29 | 3790.81 | -5717.70 | -2188.17 | -3790.56 | 5717.69 | 2188.04 | 0.004\% |
| 30 | 4377.50 | -5727.63 | 0.05 | -4377.46 | 5727.63 | 0.01 | 0.001\% |
| 31 | 3792.47 | -5737.55 | 2189.22 | -3792.37 | 5737.54 | -2189.12 | 0.002\% |
| 32 | 2188.86 | -5731.43 | 3789.75 | -2188.79 | 5731.42 | -3789.69 | 0.001\% |
| 33 | 0.08 | -5724.39 | 4375.47 | -0.07 | 5724.39 | -4375.25 | 0.003\% |
| 34 | -2188.72 | -5731.43 | 3789.61 | 2188.65 | 5731.42 | -3789.56 | 0.001\% |
| 35 | -3792.38 | -5737.55 | 2189.08 | 3792.29 | 5737.55 | -2188.99 | 0.002\% |
| 36 | -4377.50 | -5727.62 | -0.05 | 4377.46 | 5727.62 | 0.10 | 0.001\% |
| 37 | -3790.90 | -5717.70 | -2188.31 | 3790.65 | 5717.70 | 2188.18 | 0.004\% |
| 38 | -2188.86 | -5723.82 | -3789.75 | 2188.91 | 5723.82 | 3789.47 | 0.004\% |

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation | Appurtenance | Gov. <br> Load <br> Comb. | Deflection <br> in | Tilt | Twist - | Radius of Curvature $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 82.00 | Omni $21 / 2^{\prime \prime} \times 20^{\prime}$ | 33 | 0.998 | 0.1040 | 0.0385 | 65624 |
| 80.00 | $6^{1}$ Dipole | 33 | 0.954 | 0.1013 | 0.0367 | 65624 |
| 79.00 | SM 409-3 | 33 | 0.932 | 0.1000 | 0.0357 | 65624 |
| 74.00 | $3{ }^{1}$ Yagi antenna | 33 | 0.824 | 0.0938 | 0.0317 | 41015 |
| 69.82 | Guy | 33 | 0.738 | 0.0898 | 0.0295 | 27380 |
| 68.00 | 3 ' Yagi antenna | 33 | 0.703 | 0.0886 | 0.0290 | 25662 |
| 62.00 | 3 ' Yagi antenna | 33 | 0.598 | 0.0872 | 0.0297 | 56823 |
| 61.00 | Pirod 6' Side Mount Standoff (1) | 33 | 0.581 | 0.0873 | 0.0300 | 83506 |


| Thx TMOWer | Job | PT11872D | Stratford, CT |
| :---: | :--- | :---: | :--- |

## Section Capacity Table

| Section No. | $\begin{gathered} \text { Elevation } \\ f t \\ \hline \end{gathered}$ | Component Type | Size | Critical Element | $\begin{gathered} P \\ I b \end{gathered}$ | $\begin{gathered} S F^{*} P_{\text {allow }} \\ l b \end{gathered}$ | $\%$ Capacity | $\begin{aligned} & \text { Pass } \\ & \text { Fail } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 82-67 | Leg | P2.5x. 276 | 3 | -18049.50 | 68948.49 | 26.2 | Pass |
| 'T2 | 67-52 | Leg | P2.5x. 276 | 47 | -14706.30 | 58516.83 | 25.1 | Pass |
| T3 | 52-37 | Leg | P2.5x. 276 | 75 | -13874.50 | 58098.14 | 23.9 | Pass |
| T4 | 37-32 | Leg | P2.5x. 276 | 102 | -11795.60 | 70683.79 | 16.7 | Pass |
| T1 | 82-67 | Diagonal | P1.5x. 120 | 13 | -4365.28 | 12871.63 | 33.9 | Pass |
| T2 | 67-52 | Diagonal | P1.5x. 120 | 70 | -3990.11 | 9417.08 | 42.4 | Pass |
| T3 | 52-37 | Diagonal | P1.5x. 120 | 83 | -1603.19 | 9370.23 | 17.1 | Pass |
| T1 | 82-67 | Top Girt | P1.5x. 120 | 6 | -250.71 | 10813.11 | 2.3 | Pass |
| T2 | 67-52 | Top Girt | P1.5x. 120 | 50 | -1752.39 | 10813.11 | 16.2 | Pass |
| T3 | 52-37 | Top Girt | P1.5x. 120 | 78 | -266.61 | 10813.11 | 2.5 | Pass |
| T4 | 37-32 | Top Girt | L3x3x3/16 | 104 | 1176.95 | 31384.15 | 3.8 | Pass |
| T1 | 82-67 | Bottom Girt | P1.5x. 120 | 7 | -1650.44 | 10813.11 | 15.3 | Pass |
| T2 | 67-52 | Bottom Girt | P1.5x. 120 | 54 | -401.20 | 10813.11 | 3.7 | Pass |
| T3 | 52-37 | Bottom Girt | P1.5x. 120 | 80 | 1510.80 | 14979.45 | 10.1 | Pass |
| T4 | 37-32 | Bottom Girt | L3x3x3/16 | 107 | -764.77 | 30321.75 | 17.8 | Pass |
| T4 | 37-32 | Mid Girt | L3 $\times 3 \times 3 / 16$ | 113 | -118.91 | 21804.95 | 0.5 | Pass |
| T1 | 82-67 | Guy A@69.8194 | 7/16 | 123 | 9108.11 | 10400.00 | 87.6 | Pass |
| T1 | 82-67 | Guy B@,69.8194 | 7/16 | 120 | 8549.42 | 10400.00 | 82.2 | Pass |
| T1 | 82-67 | Guy C@,69.8194 | 7/16 | 116 | 8627.04 | 10400.00 | 83.0 | Pass |
| T1 | 82-67 | Torque Arm <br> Top@69.8194 | C12x20.7 | 126 | -4221.81 | 102657.52 | 40.9 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Leg (T1) | 26.2 | Pass |
|  |  |  |  |  |  | Diagonal (T2) | 42.4 | Pass |
|  |  |  |  |  |  | Top Girt (T2) | 16.2 | Pass |
|  |  |  |  |  |  | Bottom Girt <br> (T4) | 17.8 | Pass |
|  |  |  |  |  |  | Mid Girt <br> (T4) | 0.5 | Pass |
|  |  |  |  |  |  | Guy A (T1) | 87.6 | Pass |
|  |  |  |  |  |  | Guy B (T1) | 82.2 | Pass |
|  |  |  |  |  |  | Guy C (T1) | 83.0 | Pass |
|  |  |  |  |  |  | Torque Arm Top (T1) | 40.9 | Pass |
|  |  |  |  |  |  | RATING = | 87.6 | Pass |

## EXHIBIT C

# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

T-Mobile Existing Facility

Site ID: CT11872D
Stratford PD Guyed Tower
900 Longbrook Road
Stratford, CT 06614
September 16, 2014
EBI Project Number: 62144962

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general public <br> allowable limit: | $39.22 \%$ |

environmental | engineering | due diligence

September 16, 2014

T-Mobile USA
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, CT 06002

## Emissions Analysis for Site: CT11872D - Stratford PD Guyed Tower

EBI Consulting was directed to analyze the proposed T-Mobile facility located at 900 Longbrook Road, Stratford, CT, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307 (b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The general population exposure limit for the 700 MHz Band is $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, and the general population exposure limit for the PCS and AWS bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 900 Longbrook Road, Stratford, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 2 GSM channels (PCS Band - 1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel
2) 2 UMTS channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
3) 2 LTE channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
4) 1 LTE channel ( 700 MHz Band) was considered for each sector of the proposed installation. This channel has a transmit power of 30 Watts.
5) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
environmental | engineering | due diligence
6) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
7) The antennas used in this modeling are the Ericsson AIR21 B4A/B2P for 1900 MHz (PCS) and 2100 MHz (AWS) channels and the Commscope LNX-6515DS-VTM for 700 MHz channels. This is based on feedback from the carrier with regards to anticipated antenna selection. The Ericsson AIR21 B4A/B2P has a maximum gain of $\mathbf{1 5 . 9} \mathbf{~ d B d}$ at its main lobe. The Commscope LNX-6515DS-VTM has a maximum gain of $\mathbf{1 4 . 6} \mathbf{~ d B d}$ at its main lobe. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
8) The antenna mounting height centerline of the proposed antennas is 79 feet above ground level (AGL).
9) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.

## EBI Consulting

environmental | engineering | due diligence

T-Mobile Site Inventory and Power Data

| Sector: | A | Sector: | B | Sector: | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna \#: | 1 | Antenna \#: | 1 | Antenna \#: | 1 |
| Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson ATR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 79 | Height (AGL): | 79 | Height (AGL): | 79 |
| Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\text { PCS }) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ |
| Channel Count | 2 | Channel Count | 2 | \# PCS Channels: | 2 |
| Total TX Power: | 120 | Total TX Power: | 120 | \# AWS Chammels: | 120 |
| ERP (W): | 1,906.06 | ERP (W): | 1,906.06 | ERP (W): | 1,906.06 |
| Antenna A1 MPE\% | 3.15 | Antenna B1 MPE\% | 3.15 | Antenna C1 MPE\% | 3.15 |
| Antenna \#: | 2 | Antenna \#: | 2 | Antenna\#: | 2 |
| Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B4A/B2P } \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson AR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson AlR21 } \\ \text { B4A/B2P } \end{gathered}$ |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 79 | Height (AGL): | 79 | Height (AGL): | 79 |
| Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ |
| Channel Count | 4 | Channel Count | 4 | Channel Count | 4 |
| Total TX Power: | 120 | Total TX Power: | 120 | Total TX Power: | 120 |
| ERP (W): | 1,906.06 | ERP (W): | 1,906.06 | ERP (W): | 1,906.06 |
| Antenna A2 MPE\% | 3.15 | Antenna B2 MPE\% | 3.15 | Antemaa C2 MPE\% | 3.15 |
| Antenna \#: | 3 | Antenna \#: | 3 | Antenna \#: | 3 |
| Make / Model: | Commscope LNX-6515DS-VTM | Make / Model: | Commscope LNX- 6515DS-VTM | Make / Model: | Commscope LNX-6515DS-VTM |
| Gain: | 14.6 dBd | Gain: | 14.6 dBd | Gain: | 14.6 dBd |
| Height (AGL): | 79 | Height (AGL): | 79 | Height (AGL): | 79 |
| Frequency Bands | 700 Mhz | Frequency Bands | 700 Mhz | Frequency Bands | 700 Mhz |
| Chamel Count | 1 | Channel Count | 1 | Channel Count | 1 |
| Total TX Power: | 30 | Total TX Power: | 30 | Total TX Power: | 30 |
| ERP (W): | 445.37 | ERP (W): | 445.37 | ERP (W): | 445.37 |
| Antenna A3 MPE\% | 1.25 | Antenna B3 MPE\% | 1.25 | Antenna C3 MPE\% | 1.25 |
|  | Site Composite MPE\% |  |  | T-Mobile Sector 1 Total: | 1: $7.55 \%$ |
|  | Carrier | MPE\% |  | T-Mobile Sector 2 Total: | I: $\quad 7.55 \%$ |
|  | T-Mobile | 22.65 |  | T-Mobile Sector 3 Total: | I: $7.55 \%$ |
|  | SPD - Omni | 1.70\% |  | Site Total: | 1: $39.22 \%$ |

## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

| T-Mobile Sector | Power Density Value (\%) |
| ---: | :--- |
| Sector 1: | $7.55 \%$ |
| Sector 2: | $7.55 \%$ |
| Sector 3: | $7.55 \%$ |
| T-Mobile Total: | $22.65 \%$ |
|  |  |
| Site Total: | $39.22 \%$ |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{3 9 . 2 2} \%$ of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


## Scott Heffernan

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