

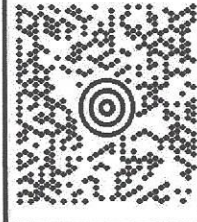
1 OF 1

0.0 LBS LTR

JENNIFER ILIADES
978-944-1804
CENTERLINE COMMUNICATIONS, LLC
750 WEST CENTER STREET
WEST BRIDGEWATER MA 02379

SHIP TO:

TOWN OF STONINGTON
(860) 535-5050
ROBERT SIMMONS, FIRST SELECTMAN
152 ELM STREET
STONINGTON CT 06378



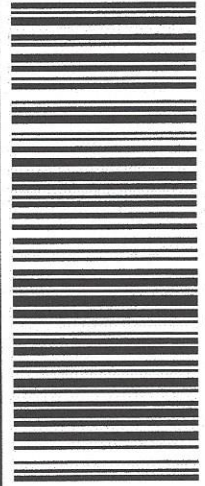
CT 063 0-02



UPS 2ND DAY AIR

TRACKING #: 1Z 9Y4 503 02 1329 4773

2



BILLING: P/P

Reference No.1: CT2177 - CSC to Robert Simmons

XCL 18.03.09 NY45 99.0A 04/2018





Proof of Delivery

[Close Window](#)

Dear Customer,

This notice serves as proof of delivery for the shipment listed below.

| | |
|---------------------------|----------------------|
| Tracking Number: | 1Z9Y45030213294773 |
| Service: | UPS 2nd Day Air® |
| Shipped/Billed On: | 06/13/2018 |
| Delivered On: | 06/15/2018 1:40 P.M. |
| Delivered To: | STONINGTON, CT, US |
| Received By: | BELL |
| Left At: | Office |

Thank you for giving us this opportunity to serve you.

Sincerely,

UPS

Tracking results provided by UPS: 06/22/2018 4:04 P.M. ET

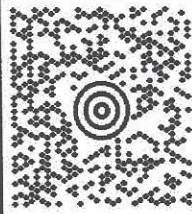
1 OF 1

0.0 LBS LTR

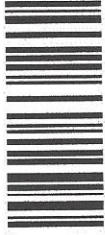
JENNIFER ILLADES
978-944-1804
CENTERLINE COMMUNICATIONS, LLC
750 WEST CENTER STREET
WEST BRIDGEWATER MA 02379

SHIP TO:

TOWN OF STONINGTON
(860) 535-5095
JASON VINCENT, DIRECTOR OF PLANNING
152 ELM STREET
STONINGTON CT 06378

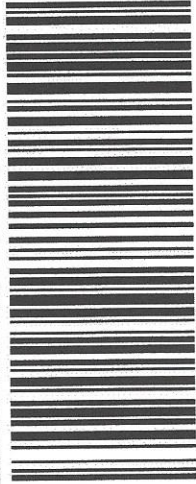


CT 063 0-02



UPS 2ND DAY AIR 2

TRACKING #: 1Z 9Y4 503 02 1225 1785



BILLING: P/P

Reference No.1: CT2177 - CSC to Jason Vincent

XOL 18.03.09 NY45 99.04 C4/2018



 **Proof of Delivery**

Close Window

Dear Customer,

This notice serves as proof of delivery for the shipment listed below.

| | |
|---------------------------|----------------------|
| Tracking Number: | 1Z9Y45030212251785 |
| Service: | UPS 2nd Day Air® |
| Shipped/Billed On: | 06/13/2018 |
| Delivered On: | 06/15/2018 1:41 P.M. |
| Delivered To: | STONINGTON, CT, US |
| Received By: | SADOWSKI |
| Left At: | Office |

Thank you for giving us this opportunity to serve you.

Sincerely,

UPS

Tracking results provided by UPS: 06/22/2018 4:04 P.M. ET

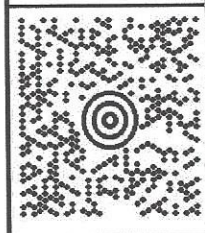
1 OF 1

0.0 LBS LTR

JENNIFER ILIADES
978-944-1804
CENTERLINE COMMUNICATIONS, LLC
750 WEST CENTER STREET
WEST BRIDGEWATER MA 02379

SHIP TO:

TOWN OF STONINGTON
(860) 535-5095
CANDACE PALMER, ZONING ENF. OFFICER
152 ELM STREET
STONINGTON CT 06378



CT 063 0-02



UPS 2ND DAY AIR 2
TRACKING #: 1Z 9Y4 503 02 0261 0790



BILLING: P/P

Reference No.1: CT2177 - CSC to Candace Palmer



X01.18.03.09 NY45 99.0A 04/2018



Proof of Delivery

Close Window

Dear Customer,

This notice serves as proof of delivery for the shipment listed below.

| | |
|---------------------------|----------------------|
| Tracking Number: | 1Z9Y45030202610790 |
| Service: | UPS 2nd Day Air® |
| Shipped/Billed On: | 06/13/2018 |
| Delivered On: | 06/15/2018 1:41 P.M. |
| Delivered To: | STONINGTON, CT, US |
| Received By: | SADOWSKI |
| Left At: | Office |

Thank you for giving us this opportunity to serve you.

Sincerely,

UPS

Tracking results provided by UPS: 06/22/2018 4:03 P.M. ET

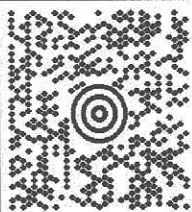
1 OF 1

0.0 LBS LTR

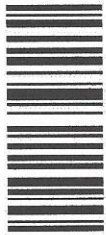
JENNIFER ILIADES
978-944-1804
CENTERLINE COMMUNICATIONS, LLC
750 WEST CENTER STREET
WEST BRIDGEWATER MA 02879

SHIP TO:

DEBBIE CASSELLA
732-404-9360 235
SBA COMMUNICATIONS CORPORATION
SUITE 303
1480 ROUTE 9 NORTH
WOODBIDGE NJ 07095



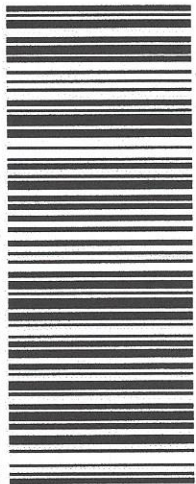
NJ 089 9-02



UPS 2ND DAY AIR

2

TRACKING #: 1Z 9Y4 503 02 2239 6011



BILLING: P/P

Reference No.1: CT2177 - CSC to SBA

X031.18.03.09 NY45 99.0A 04/2018





Proof of Delivery

[Close Window](#)

Dear Customer,

This notice serves as proof of delivery for the shipment listed below.

| | |
|---------------------------|----------------------|
| Tracking Number: | 1Z9Y45030222396011 |
| Service: | UPS 2nd Day Air® |
| Shipped/Billed On: | 06/13/2018 |
| Delivered On: | 06/15/2018 1:10 P.M. |
| Delivered To: | WOODBIDGE, NJ, US |
| Received By: | GIRGENTI |
| Left At: | Office |

Thank you for giving us this opportunity to serve you.

Sincerely,

UPS

Tracking results provided by UPS: 06/22/2018 4:03 P.M. ET

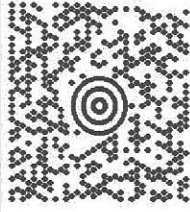
1 OF 1

0.0 LBS LTR

JENNIFER ILIADES
978-944-1804
CENTERLINE COMMUNICATIONS, LLC
750 WEST CENTER STREET
WEST BRIDGEWATER MA 02379

SHIP TO:

EDWARD PLANETA
PLANETA PROPERTIES
4343 CORSO VENETIA BLVD.
VENICE FL 34293

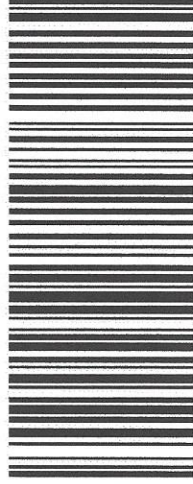


FL 335 0-03



UPS 2ND DAY AIR 2

TRACKING #: 1Z 9Y4 503 02 2905 6401



BILLING: P/P

Reference No.1: CT2177 - CSC to Planeta Properties

X01.18.03.09 NY45 99.0A 04/2018





Proof of Delivery

Close Window

Dear Customer,

This notice serves as proof of delivery for the shipment listed below.

| | |
|---------------------------|----------------------|
| Tracking Number: | 1Z9Y45030229056401 |
| Service: | UPS 2nd Day Air® |
| Shipped/Billed On: | 06/13/2018 |
| Delivered On: | 06/18/2018 3:17 P.M. |
| Delivered To: | VENICE, FL, US |
| Received By: | DRIVER RELEASE |
| Left At: | Front Door |

Thank you for giving us this opportunity to serve you.

Sincerely,

UPS

Tracking results provided by UPS: 06/22/2018 4:05 P.M. ET

June 13, 2018

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Regarding: Notice of Exempt Modification – AT&T Site CT2177
Address: 7 Broadway Avenue Extension, Stonington, CT 06355

Dear Ms. Bachman:

New Cingular Wireless, PCS, LLC (“AT&T”) currently maintains a wireless telecommunications facility on an existing 155-foot water tank at the above-referenced address, latitude 41.3495750, longitude -71.9637500. Said water tank facility is operated by MCM Acquisition 2017, LLC c/o SBA Communications Corporation.

AT&T desires to modify its existing telecommunications facility by swapping (6) antennas, adding (1) surge arrestor and accompanying feedlines, adding (3) combiners, swapping (3) TMA and adding (3) remote radio heads. The centerline height of the existing antennas is and will remain at 140 feet.

Please accept this letter as notification pursuant to R.C.S.A §16-50j-73 for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Robert Simmons, First Selectman of the Town of Stonington, Jason Vincent, Director of Planning of the Town of Stonington, Candace Palmer, Zoning/Inland Wetland Enforcement Officer of the Town of Stonington, MCM Acquisition 2017, LLC c/o SBA Communications Corporation as tower owner and Planeta Properties, as property owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2). Specifically:

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require an extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

4. The operation of the modified facility will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard. *Please see the RF emissions calculation for AT&T's modified facility enclosed herewith.*

5. The proposed modifications will not cause an ineligible change or alteration in the physical or environmental characteristics of the site.

6. The existing structure and its foundation can support the proposed loading. *Please see the structural analysis dated April 17, 2018 by Hudson Design Group LLC enclosed herewith.*

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,



Jennifer Iliades
Site Acquisition Consultant
Centerline Communications, LLC
750 West Center Street, Suite 301
West Bridgewater, MA 02379
jiliades@clinellc.com

Enclosures: Exhibit 1 – Field Card and GIS Map
Exhibit 2 – Construction Drawings
Exhibit 3 – Structural Analysis
Exhibit 4 – RF Emissions Analysis Report Evaluation

cc: Robert Simmons, First Selectman, Town of Stonington
Jason Vincent, Director of Planning, Town of Stonington
Candace Palmer, Zoning/Inland Wetland Enforcement Officer, Town of Stonington
MCM Acquisition 2017, LLC c/o SBA Communications Corporation, Tower Operator
Planeta Properties, Property Owner

EXHIBIT 1

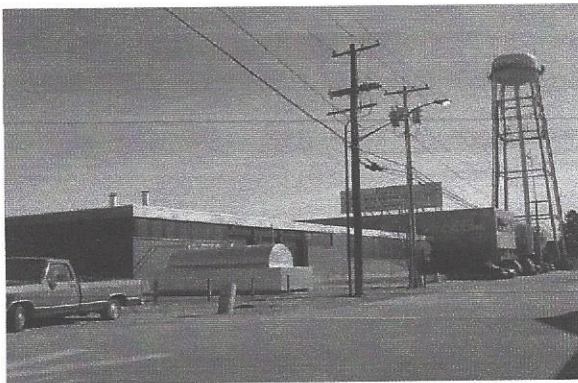


Property Information

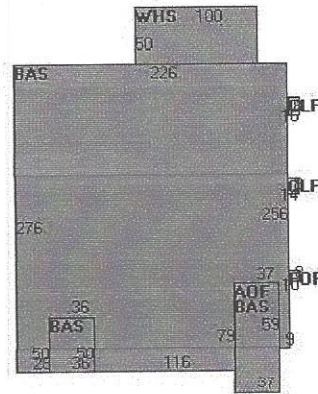
| | |
|-------------------|--|
| Property Location | 7 BROADWAY AVE EXT |
| Owner | PLANETA PROPERTIES |
| Co-Owner | C/O EDWARD PLANETA |
| Mailing Address | 4343 CORSO VENETIA BLVD VENICE FL 34293-705 |
| Land Use | 4000 INDUSTRIAL M-96 |
| Land Class | I |
| Survey Map # | NA |
| School District | |

| | |
|--------------------------|--------------------------|
| Fire District | Mystic |
| Census Tract | 7053 |
| Neighborhood | 3500 |
| Zoning Code | M-1 |
| Acreage | 4.3 |
| Utilities | |
| Lot Setting/Desc | Suburban Level |
| Trash Day | M TH |
| Polling Place (District) | Mystic Fire Department 4 |

Photo



Sketch



Primary Construction Details

| | |
|--------------------|----------------|
| Year Built | 1950 |
| Stories | 1 |
| Building Style | Industrial |
| Building Use | Ind/Comm |
| Building Condition | Ave/Good |
| Floors | Concr Abv Grad |
| Total Rooms | 0 |

| | |
|----------------|--------------|
| Bedrooms | 0 |
| Full Bathrooms | 0 |
| Half Bathrooms | 0 |
| Bath Style | NA |
| Kitchen Style | NA |
| Roof Style | Flat |
| Roof Cover | Tar & Gravel |

| | |
|-------------------|---------------|
| Exterior Walls | Brick/Masonry |
| Interior Walls | Minim/Masonry |
| Heating Type | Steam |
| Heating Fuel | Oil |
| AC Type | None |
| Gross Bldg Area | 71993 |
| Total Living Area | 69923 |



Valuation Summary (Assessed value = 70% of Appraised Value)

| Item | Appraised | Assessed |
|---------------------|-----------|----------|
| Buildings | 2529700 | 1770800 |
| Extras | 49900 | 35000 |
| Outbuildings | 259000 | 181200 |
| Land | 740300 | 518200 |
| Total | 3578900 | 2505200 |

Sub Areas

| Subarea Type | Gross Area (sq ft) | Living Area (sq ft) |
|----------------------------|--------------------|---------------------|
| First Floor | 62973 | 62973 |
| Loading Platform, Finished | 240 | 0 |
| Office, (Average) | 3700 | 3700 |
| Porch, Open | 80 | 0 |
| Warehouse | 5000 | 3250 |
| | | |
| | | |
| | | |
| | | |
| Total Area | 71993 | 69923 |

Outbuilding and Extra Items

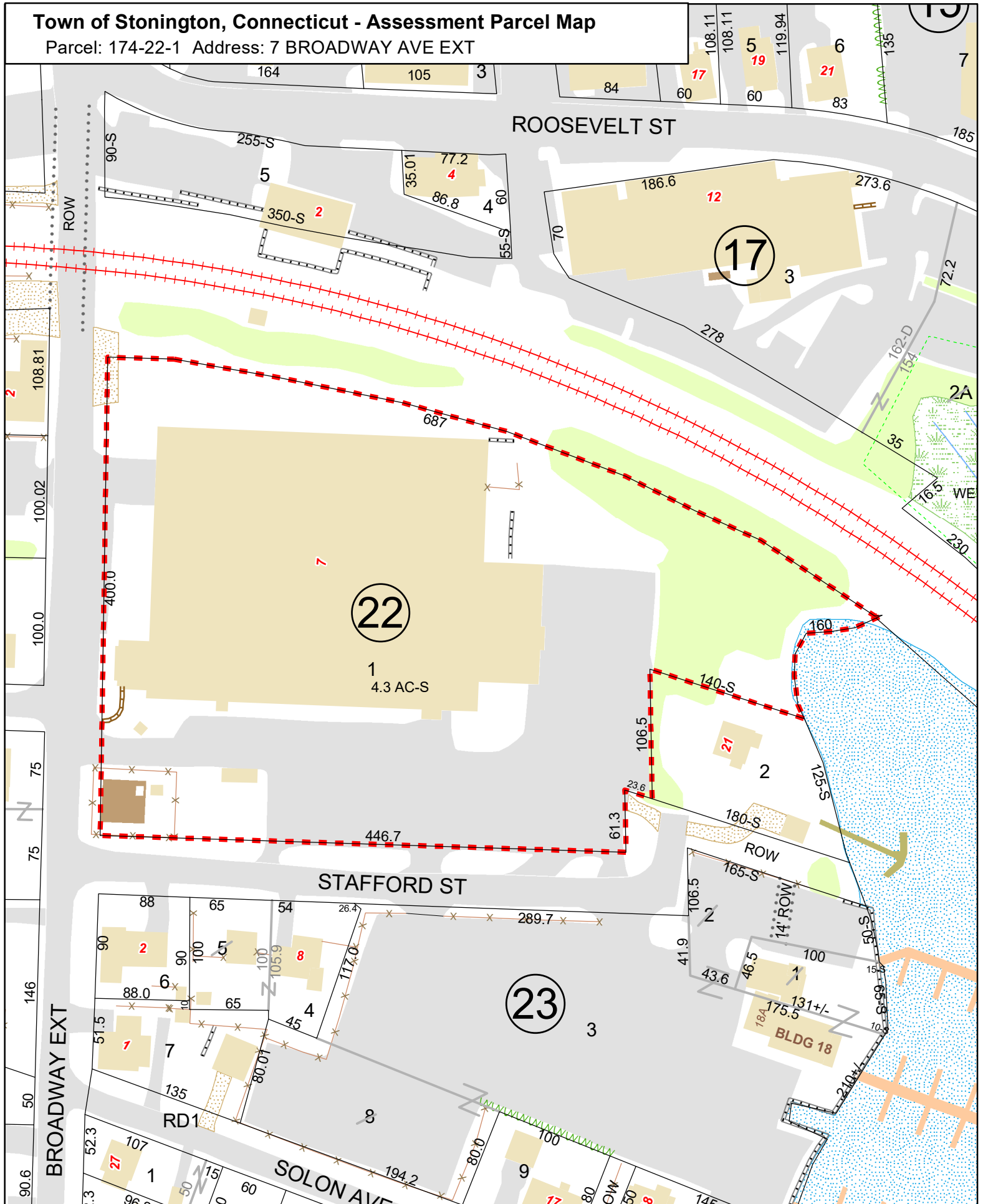
| Type | Description |
|---------------------|---------------|
| CELL EQ SHELTER GD | 360.00 S.F. |
| CELL STEEL PLATFORM | 160.00 S.F. |
| CELL STEEL PLATFORM | 140.00 S.F. |
| CELL STEEL PLATFORM | 68.00 S.F. |
| CELL TOWER | |
| ELEVATED TANK | 75000.00 GALS |
| FENCE-8' CHAIN | 218.00 L.F. |
| FENCE-6' CHAIN | 288.00 L.F. |
| SHED FRAME | 42.00 S.F. |
| SPRINKLERS-WET | 64683.00 S.F. |

Sales History

| Owner of Record | Book/ Page | Sale Date | Sale Price |
|--------------------|------------|------------|------------|
| PLANETA PROPERTIES | 409/ 933 | 10/20/1997 | 0 |
| PLANETA EDWARD J | 221/ 680 | 12/29/1978 | |

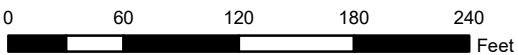
Town of Stonington, Connecticut - Assessment Parcel Map

Parcel: 174-22-1 Address: 7 BROADWAY AVE EXT



Approximate Scale:

1 inch = 100 feet



Revised To: October 2017

Map Produced: May 2018

Disclaimer: This map is for informational purposes only All information is subject to verification by any user. The Town of Stonington and its mapping contractors assume no legal responsibility for the information contained herein.

EXHIBIT 2

PROJECT INFORMATION

SCOPE OF WORK: TELECOMMUNICATIONS FACILITY UPGRADE (LTE 3C-4C 2018 UPGRADE):

SITE ADDRESS: 7 BROADWAY AVENUE EXTENSION
MYSTIC, CT 06355

LATITUDE: 41.349575° N 41° 20' 58.47" N

LONGITUDE: 71.963750° W 71° 57' 49.50" W

TYPE OF SITE: WATERTANK / OUTDOOR EQUIPMENT

TOWER HEIGHT: 156'±

RAD CENTER: 140'±

JURISDICTION: NATIONAL, STATE & LOCAL CODES OR ORDINANCES

CURRENT USE: TELECOMMUNICATIONS FACILITY

PROPOSED USE: TELECOMMUNICATIONS FACILITY



SITE NUMBER: CT2177

SITE NAME: SITE CT-305

PROJECT: LTE 3C-4C 2018 UPGRADE

DRAWING INDEX

| SHEET NO. | DESCRIPTION | REV. |
|-----------|-----------------------------|------|
| T-1 | TITLE SHEET | 1 |
| GN-1 | GENERAL NOTES | 1 |
| A-1 | COMPOUND & EQUIPMENT PLAN | 1 |
| A-2 | ANTENNA LAYOUTS & ELEVATION | 1 |
| A-3 | DETAILS | 1 |
| RF-1 | RF-PLUMBING DIAGRAM | 1 |
| G-1 | GROUNDING DETAILS | 1 |

VICINITY MAP

DIRECTIONS TO SITE:

START OUT GOING NORTHEAST ON ENTERPRISE DR TOWARD CAPITOL BLVD. TURN LEFT ONTO CAPITOL BLVD. TURN LEFT ONTO WEST ST. MERGE ONTO I-91 S VIA THE RAMP ON THE LEFT TOWARD NEW HAVEN. MERGE ONTO CT-9 S VIA EXIT 22S ON THE LEFT TOWARD MIDDLETOWN/OLD SAYBROOK. MERGE ONTO I-95 N VIA THE EXIT ON THE LEFT TOWARD NEW LONDON/PROVIDENCE. TAKE THE ALLYN STREET EXIT, EXIT 89. TAKE THE RAMP TOWARD MYSTIC. TURN RIGHT ONTO ALLYN ST. TURN LEFT ONTO NEW LONDON RD/US-1. CONTINUE TO FOLLOW US-1. TURN RIGHT ONTO BROADWAY AVE/US-1. CONTINUE TO FOLLOW BROADWAY AVE. BROADWAY AVE BECOMES BROADWAY AVE EXT. 7 BROADWAY AVE EXT IS ON THE LEFT.



GENERAL NOTES

1. THIS DOCUMENT IS THE CREATION, DESIGN, PROPERTY AND COPYRIGHTED WORK OF AT&T. ANY DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. DUPLICATION AND USE BY GOVERNMENT AGENCIES FOR THE PURPOSES OF CONDUCTING THEIR LAWFULLY AUTHORIZED REGULATORY AND ADMINISTRATIVE FUNCTIONS IS SPECIFICALLY ALLOWED.
2. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
3. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T MOBILITY REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.
4. CONSTRUCTION DRAWINGS ARE VALID FOR SIX MONTHS AFTER ENGINEER OF RECORD'S STAMPED AND SIGNED SUBMITTAL DATE LISTED HEREIN.

72 HOURS



CALL BEFORE YOU DIG



CALL TOLL FREE 1-800-922-4455

OR CALL 811

UNDERGROUND SERVICE ALERT



45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
FAX: (978) 336-5586



95 RYAN DRIVE #1
RAYNHAM, MA 02767

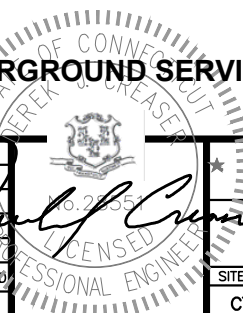
SITE NUMBER: CT2177
SITE NAME: SITE CT-305
7 BROADWAY AVENUE EXTENSION
MYSTIC, CT 06355
NEW LONDON COUNTY



550 COCHITUATE ROAD
FRAMINGHAM, MA 01701

| NO. | DATE | REVISIONS | BY | CHK | APP'D |
|-----|----------|-------------------------|----|-----|-------|
| 1 | 04/30/18 | ISSUED FOR CONSTRUCTION | EB | AT | DJC |
| 0 | 12/19/17 | ISSUED FOR REVIEW | SG | AT | DJC |
| A | 11/16/17 | ISSUED FOR REVIEW | AN | AT | DJC |

SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: AN



| | | |
|------------------------|----------------|-----|
| AT&T | | |
| TITLE SHEET | | |
| LTE 3C-4C 2018 UPGRADE | | |
| SITE NUMBER | DRAWING NUMBER | REV |
| CT2177 | T-1 | 1 |

GROUNDING NOTES

1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.
5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
7. APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO GROUND BAR.
9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWS COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
12. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50

GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:
 CONTRACTOR – CENTERLINE COMMUNICATIONS
 SUBCONTRACTOR – GENERAL CONTRACTOR (CONSTRUCTION)
 OWNER – AT&T MOBILITY
2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.
3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
6. "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.
7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.

14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.
15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
16. CONSTRUCTION SHALL COMPLY WITH LTE SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T SITES."
17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.
20. APPLICABLE BUILDING CODES:
 SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.
 BUILDING CODE: IBC 2012 WITH 2016 CT BUILDING CODE AMENDMENTS
 ELECTRICAL CODE: REFER TO ELECTRICAL DRAWINGS
 LIGHTENING CODE: REFER TO ELECTRICAL DRAWINGS

SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:

AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE;

AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC)

MANUAL OF STEEL CONSTRUCTION, ASD, FOURTEENTH EDITION;

TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-G, STRUCTURAL STANDARDS FOR STEEL

EQUIPMENT AND ANTENNA SUPPORTING STRUCTURES; REFER TO ELECTRICAL DRAWINGS FOR SPECIFIC ELECTRICAL STANDARDS.

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

ABBREVIATIONS

| | | | | | |
|------|-------------------------------|-----|---------------------------------|------|----------------------------|
| AGL | ABOVE GRADE LEVEL | EQ | EQUAL | REQ | REQUIRED |
| AWG | AMERICAN WIRE GAUGE | GC | GENERAL CONTRACTOR | RF | RADIO FREQUENCY |
| BBU | BATTERY BACKUP UNIT | GRC | GALVANIZED RIGID CONDUIT | TBD | TO BE DETERMINED |
| BTCW | BARE TINNED SOLID COPPER WIRE | MGB | MASTER GROUND BAR | TBR | TO BE REMOVED |
| BGR | BURIED GROUND RING | MIN | MINIMUM | TBRR | TO BE REMOVED AND REPLACED |
| BTS | BASE TRANSCEIVER STATION | P | PROPOSED | TYP | TYPICAL |
| E | EXISTING | NTS | NOT TO SCALE | UG | UNDER GROUND |
| EGB | EQUIPMENT GROUND BAR | RAD | RADIATION CENTER LINE (ANTENNA) | VIF | VERIFY IN FIELD |
| EGR | EQUIPMENT GROUND RING | REF | REFERENCE | | |



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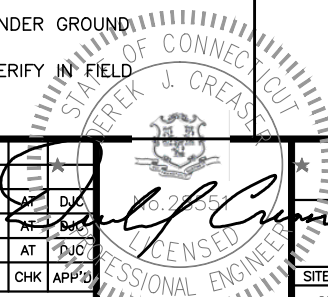
95 RYAN DRIVE #1
RAYNHAM, MA 02767

SITE NUMBER: CT2177
SITE NAME: SITE CT-305
 7 BROADWAY AVENUE EXTENSION
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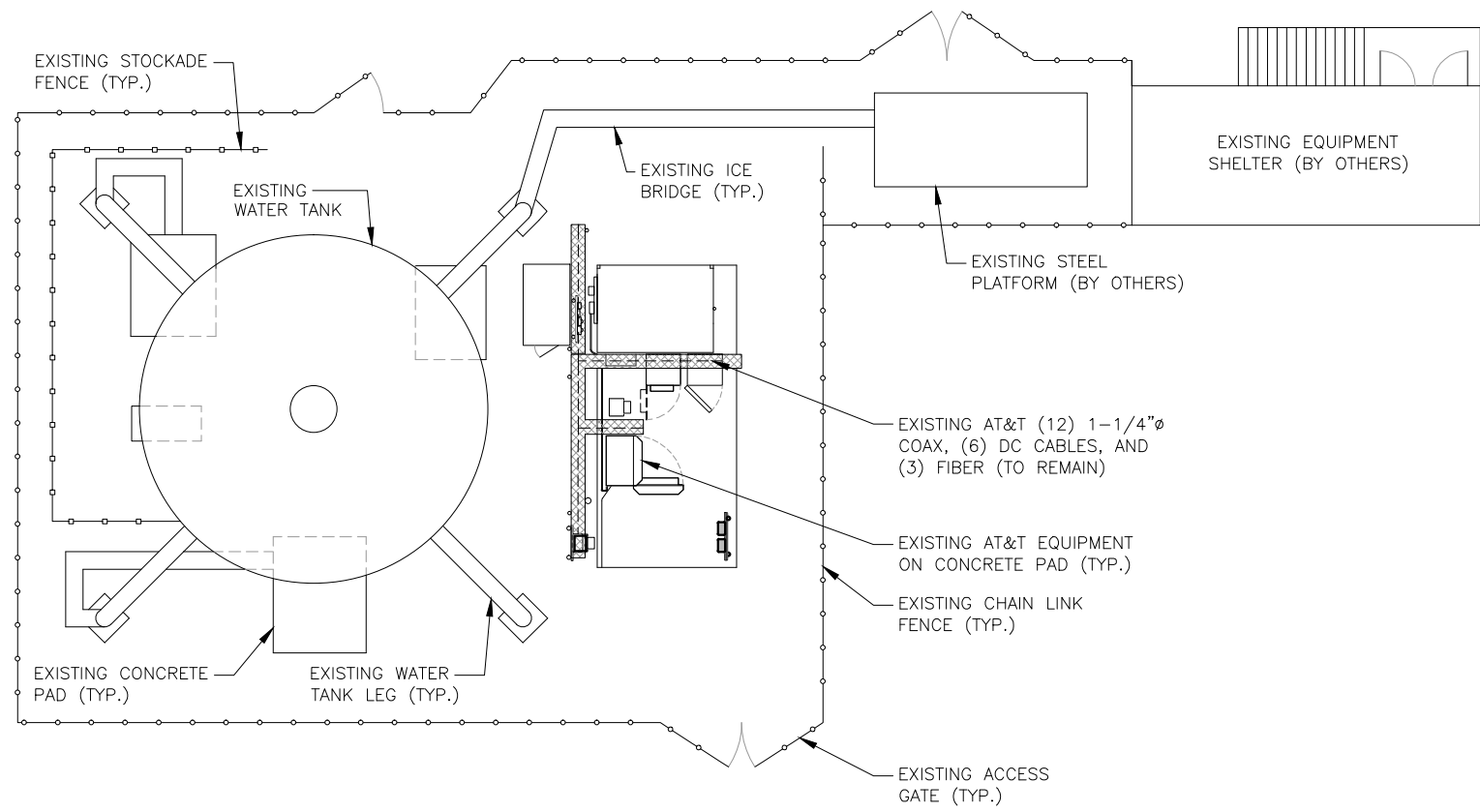
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| NO. | DATE | REVISIONS | BY | CHK | APP'D |
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| A | 11/16/17 | ISSUED FOR REVIEW | AN | AT | DJC |
| SCALE: AS SHOWN | | DESIGNED BY: AT | DRAWN BY: AN | | |



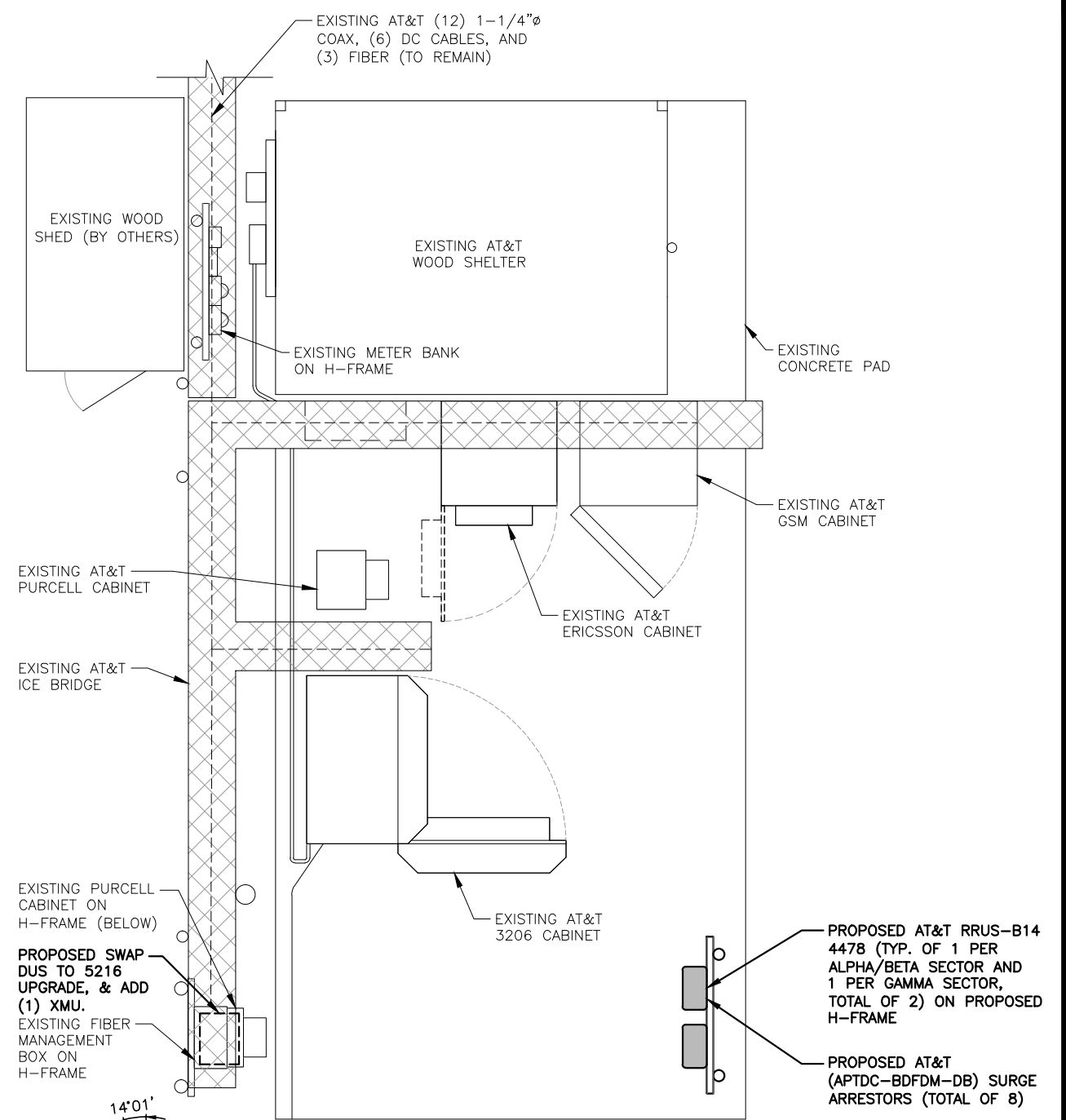
| | | |
|-------------------------------|----------------|-----|
| AT&T | | |
| GENERAL NOTES | | |
| LTE 3C-4C 2018 UPGRADE | | |
| SITE NUMBER | DRAWING NUMBER | REV |
| CT2177 | GN-1 | 1 |

NOTE:
REFER TO STRUCTURAL ANALYSIS BY:
HUDSON DESIGN GROUP, LLC, DATED:
APRIL 17, 2018, FOR THE CAPACITY
OF THE EXISTING STRUCTURES TO
SUPPORT THE PROPOSED EQUIPMENT.

NOTE:
REFER TO THE FINAL RF DATA SHEET
FOR FINAL ANTENNA SETTINGS.



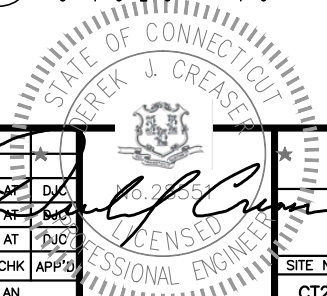
COMPOUND PLAN 1
22x34 SCALE: 1/8"=1'-0"
11x17 SCALE: 1/16"=1'-0"
A-1

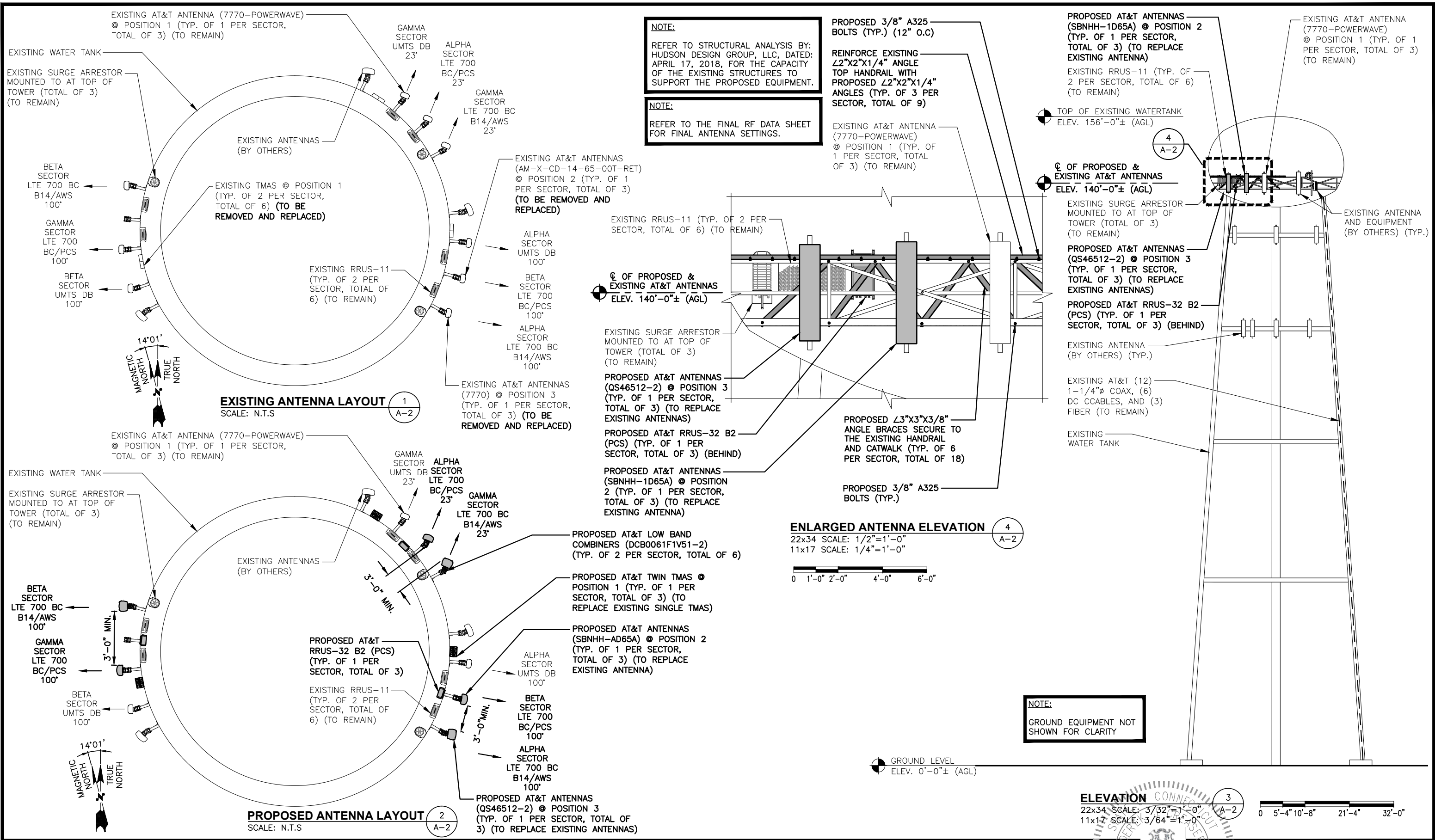


EQUIPMENT PLAN 2
22x34 SCALE: 1/2"=1'-0"
11x17 SCALE: 1/4"=1'-0"
A-1

POWER PLANT NOTE:
INSTALL (5) 30 AMP
BREAKERS IN EXISTING
OUTDOOR POWER PLANT.

| | | | | | |
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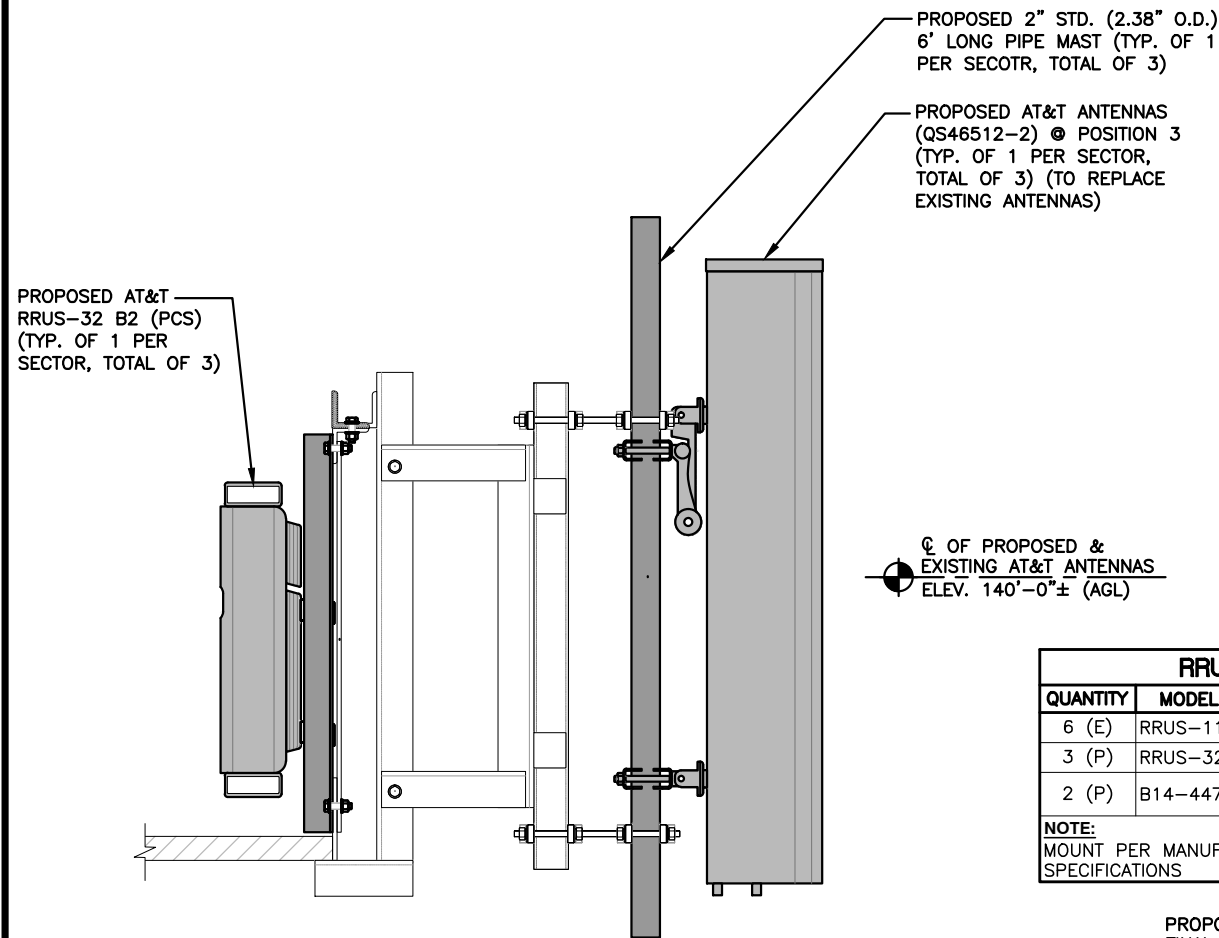
NOTE:
REFER TO THE FINAL RF DATA SHEET
FOR FINAL ANTENNA SETTINGS.

| FINAL ANTENNA SCHEDULE | | | | | | | | | | | | | | | |
|------------------------|--------------------|----------|------------------------------|-------------|----------|--------------------|-----------------------------|----------|------------------------------|------------------|---------------|------------|------------|--|--|
| SECTOR | BAND | ANTENNA | SIZE (INCHES) (L X W X D) | RAD CENTER | AZIMUTH | LOW BAND COMBINERS | TMA'S | RRU'S | SIZE (INCHES) (L X W X D) | DC JUMPERS | FIBER JUMPERS | COAX LINES | | | |
| ALPHA | UMTS DB | EXISTING | 7770 | 55X11X5 | 140'-0"± | 100' | - | - | PROPOSED (1) TT19-08BP111001 | - | - | (2) 1-1/4" | | | |
| | LTE 700 BC/PCS | PROPOSED | SBNHH-1D65A | 55x11.9x7.1 | 140'-0"± | 23' | - | - | EXISTING PROPOSED | RRUS-11 (700) | - | - | | | |
| | LTE 700 BC B14/AWS | PROPOSED | QS46512-2 | 52X12X10.8 | 140'-0"± | 100' | PROPOSED (1) DBC0061F1V51-2 | EXISTING | EXISTING | RRUS-32 B2 (PCS) | *2 | **1 | (2) 1-1/4" | | |
| BETA | UMTS DB | EXISTING | 7770 | 55X11X5 | 140'-0"± | 270' | - | - | (1) TT19-08BP111001 | - | - | (2) 1-1/4" | | | |
| | LTE 700 BC/PCS | PROPOSED | SBNHH-1D65A | 55x11.9x7.1 | 140'-0"± | 100' | - | - | EXISTING PROPOSED | RRUS-11 (700) | - | - | | | |
| | LTE 700 BC B14/AWS | PROPOSED | QS46512-2 | 52X12X10.8 | 140'-0"± | 270' | PROPOSED (1) DBC0061F1V51-2 | EXISTING | EXISTING | RRUS-32 B2 (PCS) | *2 | **1 | (2) 1-1/4" | | |
| GAMMA | UMTS DB | EXISTING | 7770 | 55X11X5 | 140'-0"± | 23' | - | - | (1) TT19-08BP111001 | - | - | (2) 1-1/4" | | | |
| | LTE 700 BC/PCS | PROPOSED | SBNHH-1D65A | 55x11.9x7.1 | 140'-0"± | 270' | - | - | EXISTING PROPOSED | RRUS-11 (700) | - | - | | | |
| | LTE 700 BC B14/AWS | PROPOSED | QS46512-2 | 52X12X10.8 | 140'-0"± | 23' | PROPOSED (1) DBC0061F1V51-2 | EXISTING | EXISTING | RRUS-32 B2 (PCS) | *2 | **1 | (2) 1-1/4" | | |

FINAL ANTENNA CONFIGURATION TABLE (5)
A-3

***DC JUMPER NOTE:**
COAX JUMPERS (2) PER SECTOR,
FROM EACH RRU (TOTAL OF 6).

****FIBER JUMPER NOTE:**
FIBER JUMPERS (1) PER SECTOR,
FROM THE SQUID TO EACH RRU
(TOTAL OF 3).



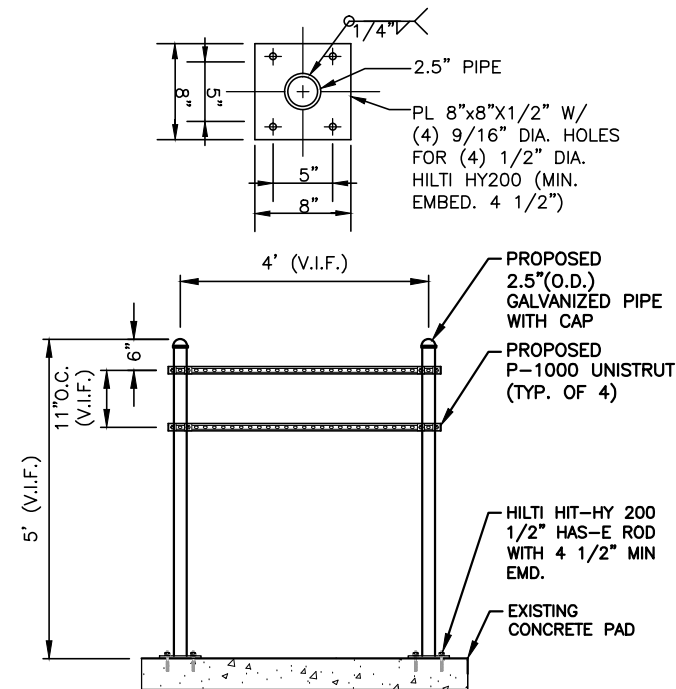
| RRU CHART | | | | |
|-----------|----------|-------|-------|------|
| QUANTITY | MODEL | L | W | D |
| 6 (E) | RRUS-11 | 19.7" | 17.0" | 7.2" |
| 3 (P) | RRUS-32 | 27.2" | 12.1" | 7.0" |
| 2 (P) | B14-4478 | 15.0" | 13.2" | 7.4" |

NOTE:
MOUNT PER MANUFACTURER'S
SPECIFICATIONS

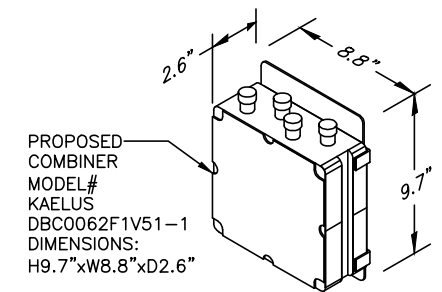
PROPOSED RRU REFER TO THE
FINAL RFDS AND CHART FOR
QUANTITY, MODEL AND DIMENSIONS
NOTE:
MOUNT PER MANUFACTURER'S
SPECIFICATIONS.

NOTE:
SEE RFDS FOR RRU
FREQUENCY AND
MODEL NUMBER

PROPOSED RRUS DETAIL (2)
SCALE: N.T.S.



H-FRAME DETAIL (3)
SCALE: N.T.S.



NOTE:
MOUNT PER MANUFACTURER'S
SPECIFICATIONS.

PROPOSED COMBINER DETAIL (4)
SCALE: N.T.S.

**PROPOSED ANTENNA & RRU
MOUNTING DETAIL @ POSITION 3** (1)
A-3

22x34 SCALE: 1-1/2"=1'-0"
11x17 SCALE: 3/4"=1'-0"

PROPOSED RRUS DETAIL (2)
SCALE: N.T.S.

H-FRAME DETAIL (3)
SCALE: N.T.S.

PROPOSED COMBINER DETAIL (4)
SCALE: N.T.S.



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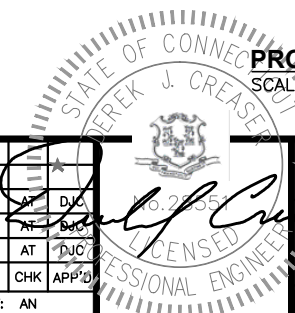
SITE NUMBER: CT2177
SITE NAME: SITE CT-305
7 BROADWAY AVENUE EXTENSION
MYSTIC, CT 06355
NEW LONDON COUNTY



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SCALE: AS SHOWN
DESIGNED BY: AT
DRAWN BY: AN



| AT&T | | |
|------------------------|----------------|-----|
| DETAILS | | |
| LTE 3C-4C 2018 UPGRADE | | |
| SITE NUMBER | DRAWING NUMBER | REV |
| CT2177 | A-3 | 1 |

STRUCTURAL NOTES:

- DESIGN REQUIREMENTS ARE PER STATE BUILDING CODE AND APPLICABLE SUPPLEMENTS, INTERNATIONAL BUILDING CODE, EIA/TIA-222-G STRUCTURAL STANDARDS FOR STEEL ANTENNA, TOWERS AND ANTENNA SUPPORTING STRUCTURES.
- CONTRACTOR SHALL VERIFY ALL DIMENSIONS AND CONDITIONS IN THE FIELD PRIOR TO FABRICATION AND ERECTION OF ANY MATERIAL. ANY UNUSUAL CONDITIONS SHALL BE REPORTED TO THE ATTENTION OF THE CONSTRUCTION MANAGER AND ENGINEER OF RECORD.
- DESIGN AND CONSTRUCTION OF STRUCTURAL STEEL SHALL CONFORM TO THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS".
- STRUCTURAL STEEL SHALL CONFORM TO ASTM A992 (Fy=50 ksi), MISCELLANEOUS STEEL SHALL CONFORM TO ASTM A36 UNLESS OTHERWISE INDICATED.
- STEEL PIPE SHALL CONFORM TO ASTM A500 "COLD-FORMED WELDED & SEAMLESS CARBON STEEL STRUCTURAL TUBING", GRADE B, OR ASTM A53 PIPE STEEL BLACK AND HOT-DIPPED ZINC-COATED WELDED AND SEAMLESS TYPE E OR S, GRADE B. PIPE SIZES INDICATED ARE NOMINAL. ACTUAL OUTSIDE DIAMETER IS LARGER.
- STRUCTURAL CONNECTION BOLTS SHALL BE HIGH STRENGTH BOLTS (BEARING TYPE) AND CONFORM TO ASTM A325 TYPE-X "HIGH STRENGTH BOLTS FOR STRUCTURAL JOINTS, INCLUDING SUITABLE NUTS AND PLAIN HARDENED WASHERS". ALL BOLTS SHALL BE 3/4" DIA UON.
- ALL STEEL MATERIALS SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT-DIP GALVANIZED) COATINGS ON IRON AND STEEL PRODUCTS", UNLESS OTHERWISE NOTED.
- ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC-COATING (HOT-DIP) ON IRON AND STEEL HARDWARE", UNLESS OTHERWISE NOTED.
- FIELD WELDS, DRILL HOLES, SAW CUTS AND ALL DAMAGED GALVANIZED SURFACES SHALL BE REPAIRED WITH AN ORGANIC ZINC REPAIR PAINT COMPLYING WITH REQUIREMENTS OF ASTM A780. GALVANIZING REPAIR PAINT SHALL HAVE 65 PERCENT ZINC BY WEIGHT, ZIRP BY DUNCAN GALVANIZING, GALVA BRIGHT PREMIUM BY CROWN OR EQUAL. THICKNESS OF APPLIED GALVANIZING REPAIR PAINT SHALL BE NOT NOT LESS THAN 4 COATS (ALLOW TIME TO DRY BETWEEN COATS) WITH A RESULTING COATING THICKNESS REQUIRED BY ASTM A123 OR A153 AS APPLICABLE.
- CONTRACTOR SHALL COMPLY WITH AWS CODE FOR PROCEDURES, APPEARANCE AND QUALITY OF WELDS, AND FOR METHODS USED IN CORRECTING WELDING. ALL WELDERS AND WELDING PROCESSES SHALL BE QUALIFIED IN ACCORDANCE WITH AWS "STANDARD QUALIFICATION PROCEDURES". ALL WELDING SHALL BE DONE USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC AND D.I.I. WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "STEEL CONSTRUCTION MANUAL". 14TH EDITION.
- INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON-CONFORMING MATERIALS OR CONDITIONS SHALL BE REPORTED TO THE CONSTRUCTION MANAGER PRIOR TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE CONSTRUCTION MANAGER APPROVAL.
- UNISTRUT SHALL BE FORMED STEEL CHANNEL STRUT FRAMING AS MANUFACTURED BY UNISTRUT CORP., WAYNE, MI OR EQUAL. STRUT MEMBERS SHALL BE 1 5/8"x1 5/8"x12GA, UNLESS OTHERWISE NOTED, AND SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION.
- EPOXY ANCHOR ASSEMBLY SHALL CONSIST OF STAINLESS STEEL ANCHOR ROD WITH NUTS & WASHERS. AN INTERNALLY THREADED INSERT, A SCREEN TUBE AND A EPOXY ADHESIVE. THE ANCHORING SYSTEM SHALL BE THE HILTI-HIT HY-70 AND OR HY-200 SYSTEMS (AS SPECIFIED IN DWG.) OR ENGINEERS APPROVED EQUAL.
- EXPANSION BOLTS SHALL CONFORM TO FEDERAL SPECIFICATION FF-S-325, GROUP II, TYPE 4, CLASS I, HILTI KWIK BOLT III OR APPROVED EQUAL. INSTALLATION SHALL BE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- LUMBER SHALL COMPLY WITH THE REQUIREMENTS OF THE AMERICAN INSTITUTE OF TIMBER CONSTRUCTION AND THE NATIONAL FOREST PRODUCTS ASSOCIATION'S NATIONAL DESIGN SPECIFICATION FOR WOOD CONSTRUCTION. ALL LUMBER SHALL BE PRESSURE TREATED AND SHALL BE STRUCTURAL GRADE NO. 2 OR BETTER.
- WHERE ROOF PENETRATIONS ARE REQUIRED, THE CONTRACTOR SHALL CONTACT AND COORDINATE RELATED WORK WITH THE BUILDING OWNER AND THE EXISTING ROOF INSTALLER. WORK SHALL BE PERFORMED IN SUCH A MANNER AS TO NOT VOID THE EXISTING ROOF WARRANTY. ROOF SHALL BE WATERTIGHT.
- ALL FIBERGLASS MEMBERS USED ARE AS MANUFACTURED BY STRONGWELL COMPANY OF BRISTOL, VA 24203. ALL DESIGN CRITERIA FOR THESE MEMBERS IS BASED ON INFORMATION PROVIDED IN THE DESIGN MANUAL. ALL REQUIREMENTS PUBLISHED IN SAID MANUAL MUST BE STRICTLY ADHERED TO.
- NO MATERIALS TO BE ORDERED AND NO WORK TO BE COMPLETED UNTIL SHOP DRAWINGS HAVE BEEN REVIEWED AND APPROVED IN WRITING.
- SUBCONTRACTOR SHALL FIREPROOF ALL STEEL TO PRE-EXISTING CONDITIONS.

SPECIAL INSPECTIONS (REFERENCE IBC CHAPTER 17):

GENERAL: WHERE APPLICATION IS MADE FOR CONSTRUCTION, THE OWNER OR THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE ACTING AS THE OWNER'S AGENT SHALL EMPLOY ONE OR MORE APPROVED AGENCIES TO PERFORM INSPECTIONS DURING CONSTRUCTION ON THE TYPES OF WORK LISTED IN THE INSPECTION CHECKLIST ABOVE.

THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE AND ENGINEERS OF RECORD INVOLVED IN THE DESIGN OF THE PROJECT ARE PERMITTED TO ACT AS THE APPROVED AGENCY AND THEIR PERSONNEL ARE PERMITTED TO ACT AS THE SPECIAL INSPECTOR FOR THE WORK DESIGNED BY THEM, PROVIDED THOSE PERSONNEL MEET THE QUALIFICATION REQUIREMENTS.

STATEMENT OF SPECIAL INSPECTIONS: THE APPLICANT SHALL SUBMIT A STATEMENT OF SPECIAL INSPECTIONS PREPARED BY THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE IN ACCORDANCE WITH SECTION 107.1 AS A CONDITION FOR ISSUANCE. THIS STATEMENT SHALL BE IN ACCORDANCE WITH SECTION 1705.

REPORT REQUIREMENT: SPECIAL INSPECTORS SHALL KEEP RECORDS OF INSPECTIONS. THE SPECIAL INSPECTOR SHALL FURNISH INSPECTION REPORTS TO THE BUILDING OFFICIAL, AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. REPORTS SHALL INDICATE THAT WORK INSPECTED WAS OR WAS NOT COMPLETED IN CONFORMANCE TO APPROVED CONSTRUCTION DOCUMENTS. DISCREPANCIES SHALL BE BROUGHT TO THE IMMEDIATE ATTENTION OF THE CONTRACTOR FOR CORRECTION. IF THEY ARE NOT CORRECTED, THE DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE BUILDING OFFICIAL AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. A FINAL REPORT DOCUMENTING REQUIRED SPECIAL INSPECTIONS SHALL BE SUBMITTED.

| SPECIAL INSPECTION CHECKLIST | |
|--|--|
| BEFORE CONSTRUCTION | |
| CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD) | REPORT ITEM |
| N/A | ENGINEER OF RECORD APPROVED SHOP DRAWINGS ¹ |
| N/A | MATERIAL SPECIFICATIONS REPORT ² |
| N/A | FABRICATOR NDE INSPECTION |
| N/A | PACKING SLIPS ³ |
| ADDITIONAL TESTING AND INSPECTIONS: | |
| DURING CONSTRUCTION | |
| CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD) | REPORT ITEM |
| REQUIRED | STEEL INSPECTIONS |
| N/A | HIGH STRENGTH BOLT INSPECTIONS |
| N/A | HIGH WIND ZONE INSPECTIONS ⁴ |
| N/A | FOUNDATION INSPECTIONS |
| N/A | CONCRETE COMP. STRENGTH, SLUMP TESTS AND PLACEMENT |
| N/A | POST INSTALLED ANCHOR VERIFICATION ⁵ |
| N/A | GROUT VERIFICATION |
| N/A | CERTIFIED WELD INSPECTION |
| N/A | EARTHWORK: LIFT AND DENSITY |
| N/A | ON SITE COLD GALVANIZING VERIFICATION |
| N/A | GUY WIRE TENSION REPORT |
| ADDITIONAL TESTING AND INSPECTIONS: | |
| AFTER CONSTRUCTION | |
| CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD) | REPORT ITEM |
| REQUIRED | MODIFICATION INSPECTOR REDLINE OR RECORD DRAWINGS ⁶ |
| N/A | POST INSTALLED ANCHOR PULL-OUT TESTING |
| REQUIRED | PHOTOGRAPHS |
| ADDITIONAL TESTING AND INSPECTIONS: | |

NOTES:

- REQUIRED FOR ANY NEW SHOP FABRICATED FRP OR STEEL.
- PROVIDED BY MANUFACTURER, REQUIRED IF HIGH STRENGTH BOLTS OR STEEL.
- PROVIDED BY GENERAL CONTRACTOR; PROOF OF MATERIALS.
- HIGH WIND ZONE INSPECTION CATB 120MPH OR CAT C,D 110MPH INSPECT FRAMING OF WALLS, ANCHORING, FASTENING SCHEDULE.
- ADHESIVE FOR REBAR AND ANCHORS SHALL HAVE BEEN TESTED IN ACCORDANCE WITH ACI 355.4 AND ICC-ES AC308 FOR CRACKED CONCRETE AND SEISMIC APPLICATIONS. DESIGN ADHESIVE BOND STRENGTH HAS BEEN BASED ON ACI 355.4 TEMPERATURE CATEGORY B WITH INSTALLATIONS INTO DRY HOLES DRILLED USING A CARBIDE BIT INTO CRACKED CONCRETE THAT HAS CURED FOR AT LEAST 21 DAYS. ADHESIVE ANCHORS REQUIRING CERTIFIED INSTALLATIONS SHALL BE INSTALLED BY A CERTIFIED ADHESIVE ANCHOR INSTALLER PER ACI 318-11 D.9.2.2. INSTALLATIONS REQUIRING CERTIFIED INSTALLERS SHALL BE INSPECTED PER ACI 318-11 D.8.2.4.
- AS REQUIRED; FOR ANY FIELD CHANGES TO THE ITEMS IN THIS TABLE.

NOTES:

- ALL CONNECTIONS TO BE SHOP WELDED & FIELD BOLTED USING 3/4"Ø A325-X BOLTS, UNLESS OTHERWISE NOTIFIED.
- SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED BEFORE ORDERING MATERIAL.
- SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED PRIOR TO STEEL FABRICATION.
- VERIFICATION OF EXISTING ROOF CONSTRUCTION IS REQUIRED PRIOR TO THE INSTALLATION OF THE ROOF PLATFORM. ENGINEER OF RECORD IS TO APPROVE EXISTING CONDITIONS IN ORDER TO MOVE FORWARD.
- CENTERLINE OF PROPOSED STEEL PLATFORM SUPPORT COLUMNS TO BE CENTRALLY LOCATED OVER THE EXISTING BUILDING COLUMNS.
- EXISTING BRICK MASONRY COLUMNS/BEARING TO BE REPAIRED/REPLACED AT ALL PROPOSED PLATFORM SUPPORT POINTS. ENGINEER OF RECORD TO REVIEW AND APPROVE.



45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
FAX: (978) 336-5586



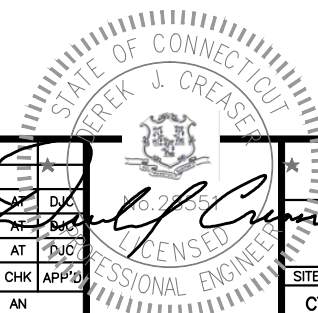
95 RYAN DRIVE #1
RAYNHAM, MA 02767

SITE NUMBER: CT2177
SITE NAME: SITE CT-305
7 BROADWAY AVENUE EXTENSION
MYSTIC, CT 06355
NEW LONDON COUNTY



550 COCHITUATE ROAD
FRAMINGHAM, MA 01701

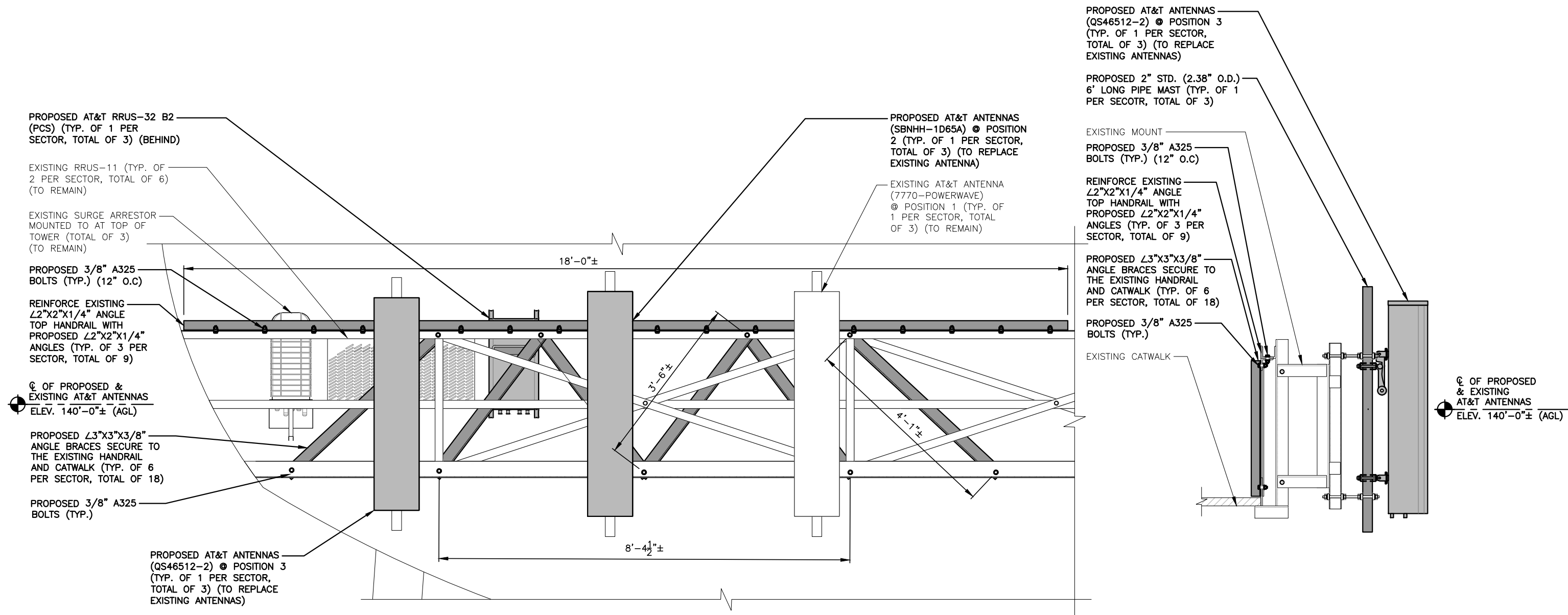
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| 0 | 12/19/17 | ISSUED FOR REVIEW | SG | AT | DJC |
| A | 11/16/17 | ISSUED FOR REVIEW | AN | AT | DJC |
| NO. | DATE | REVISIONS | BY | CHK | APP'D |
| SCALE: AS SHOWN | | DESIGNED BY: AT | DRAWN BY: AN | | |



| | | |
|------------------------|----------------|-----|
| AT&T | | |
| STRUCTURAL NOTES | | |
| LTE 3C-4C 2018 UPGRADE | | |
| SITE NUMBER | DRAWING NUMBER | REV |
| CT2177 | SN-1 | 1 |

NOTE:
REFER TO STRUCTURAL ANALYSIS BY:
HUDSON DESIGN GROUP, LLC, DATED:
APRIL 17, 2018, FOR THE CAPACITY
OF THE EXISTING STRUCTURES TO
SUPPORT THE PROPOSED EQUIPMENT.

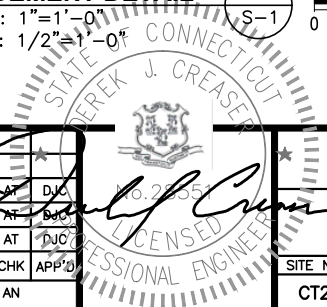
NOTE:
REFER TO THE FINAL RF DATA SHEET
FOR FINAL ANTENNA SETTINGS.

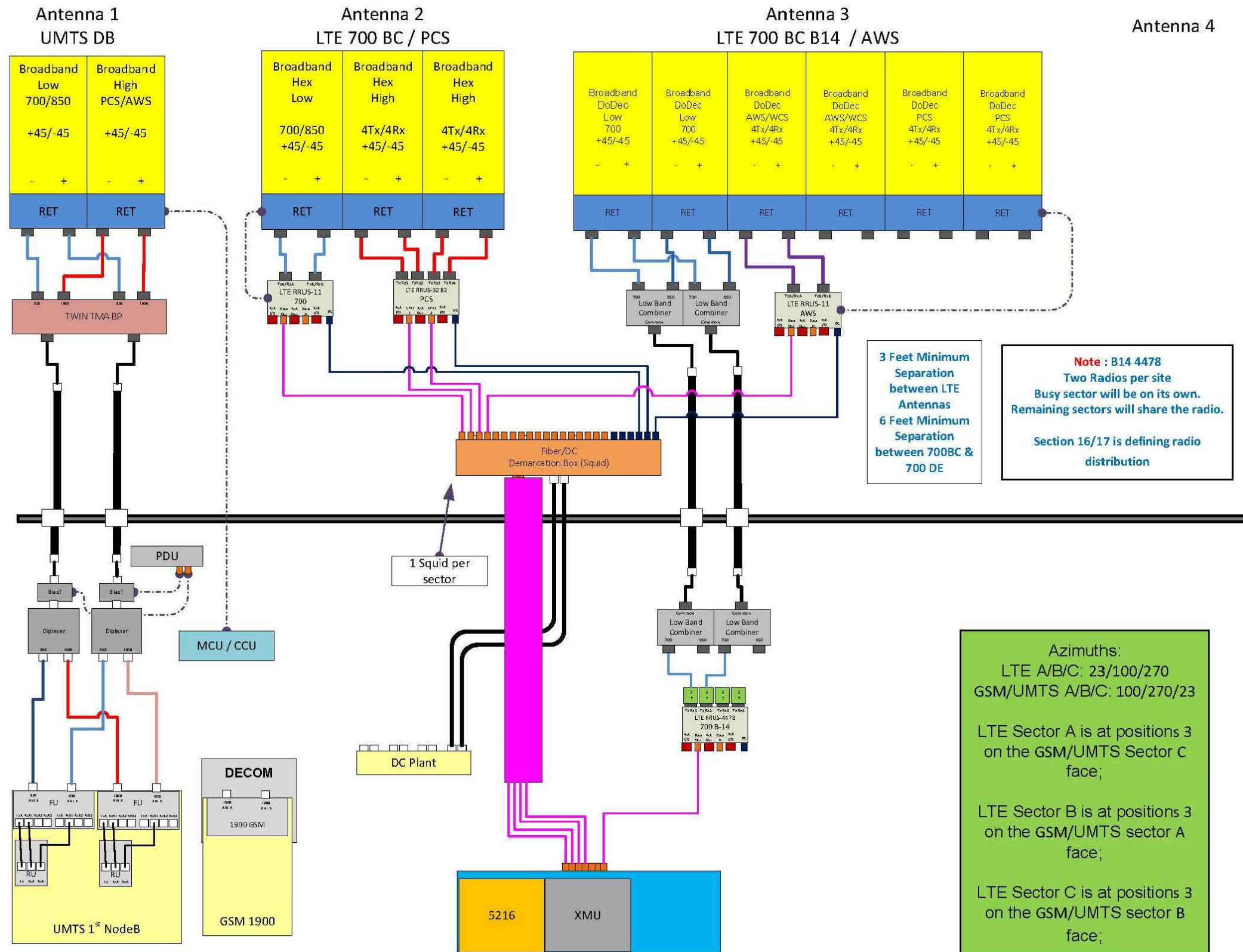


PROPOSED STRUCTURE REINFORCEMENT ELEVATION
22x34 SCALE: 1"=1'-0"
11x17 SCALE: 1/2"=1'-0"
1 S-1

PROPOSED STRUCTURE REINFORCEMENT DETAIL
22x34 SCALE: 1"=1'-0"
11x17 SCALE: 1/2"=1'-0"
2 S-1

| | | | | | |
|-----------------|----------|-------------------------|--------------|-----|-------|
| 1 | 04/30/18 | ISSUED FOR CONSTRUCTION | EB | AT | DJC |
| 0 | 12/19/17 | ISSUED FOR REVIEW | SG | AT | DJC |
| A | 11/16/17 | ISSUED FOR REVIEW | AN | AT | DJC |
| NO. | DATE | REVISIONS | BY | CHK | APP'D |
| SCALE: AS SHOWN | | DESIGNED BY: AT | DRAWN BY: AN | | |



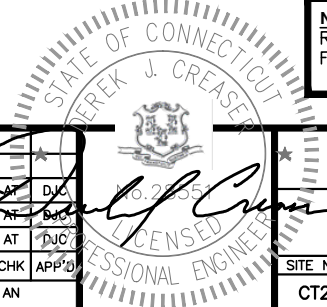


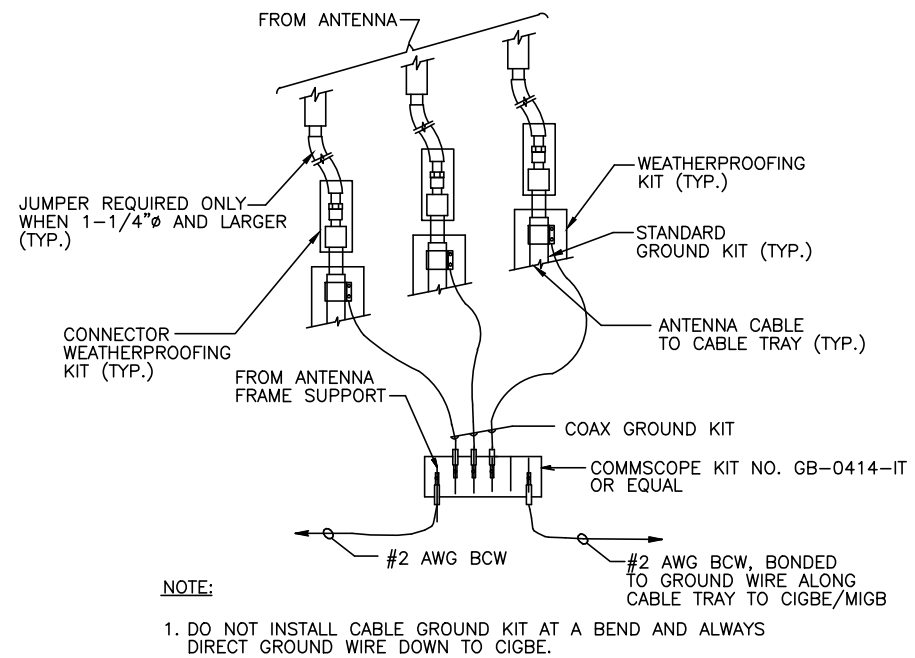
RF PLUMBING DIAGRAM 1
SCALE: N.T.S. RF-1

NOTE:
1. CONTRACTOR TO CONFIRM ALL PARTS.
2. INSTALL ALL EQUIPMENT TO MANUFACTURER'S RECOMMENDATIONS

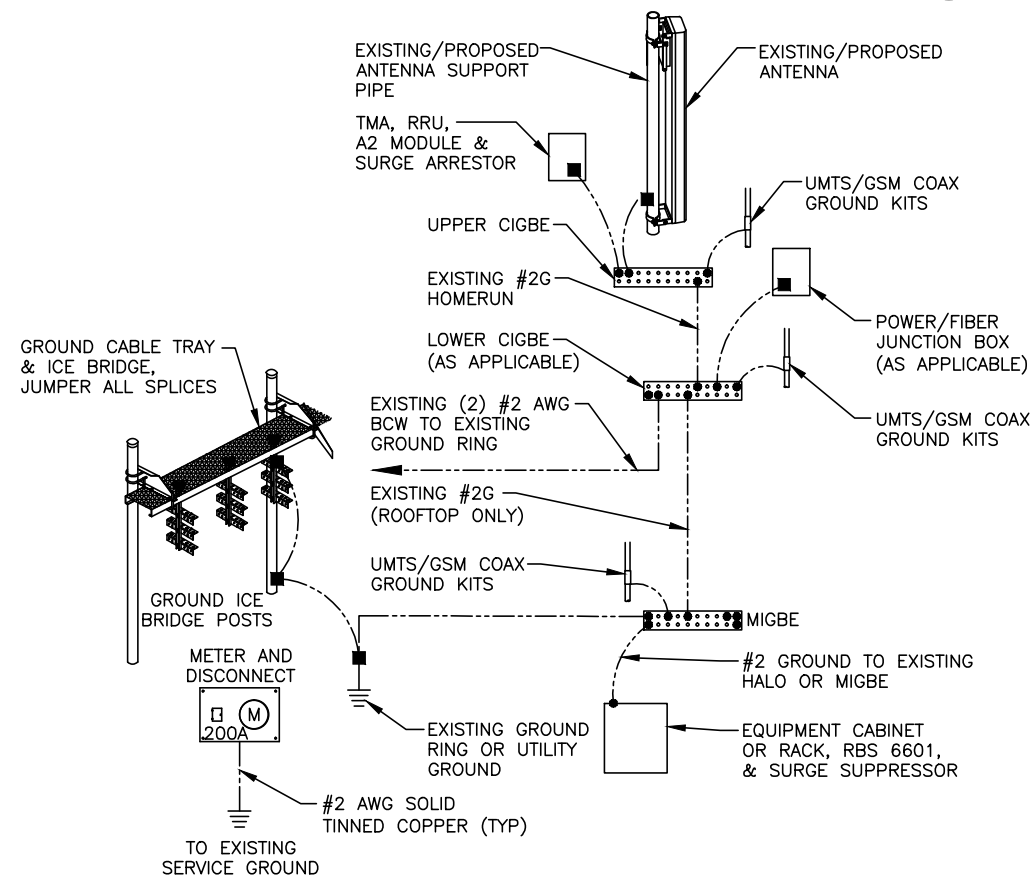
NOTE:
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

| | | | | | |
|-----------------|----------|-------------------------|--------------|-----|-------|
| 1 | 04/30/18 | ISSUED FOR CONSTRUCTION | EB | AT | DJC |
| 0 | 12/19/17 | ISSUED FOR REVIEW | SG | AT | DJC |
| A | 11/16/17 | ISSUED FOR REVIEW | AN | AT | DJC |
| NO. | DATE | REVISIONS | BY | CHK | APP'D |
| SCALE: AS SHOWN | | DESIGNED BY: AT | DRAWN BY: AN | | |

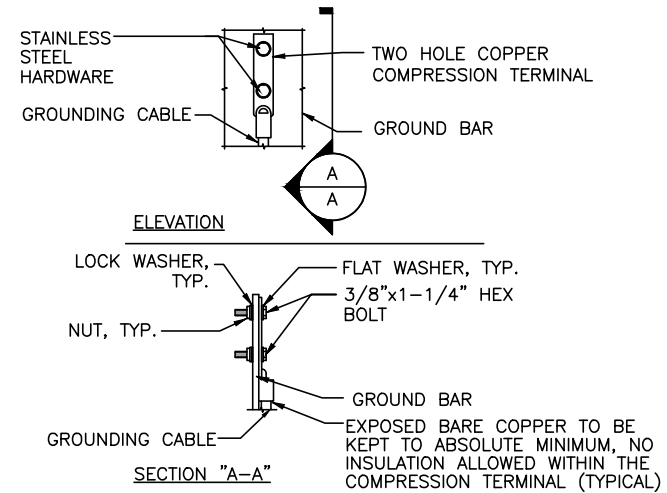




GROUND WIRE TO GROUND BAR CONNECTION DETAIL 1
SCALE: N.T.S. G-1



GROUNDING RISER DIAGRAM 2
SCALE: N.T.S. G-1



TYPICAL GROUND BAR CONNECTION DETAIL 3
SCALE: N.T.S. G-1

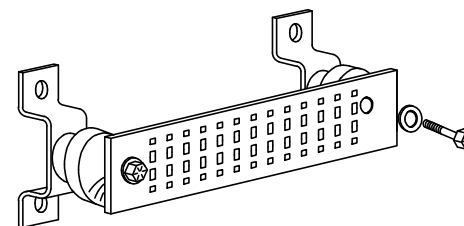
EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS ORIGIN AND DESTINATION.

SECTION "P" - SURGE PRODUCERS

- CABLE ENTRY PORTS (HATCH PLATES) (#2)
- GENERATOR FRAMEWORK (IF AVAILABLE) (#2)
- TELCO GROUND BAR
- COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2)
- +24V POWER SUPPLY RETURN BAR (#2)
- 48V POWER SUPPLY RETURN BAR (#2)
- RECTIFIER FRAMES.

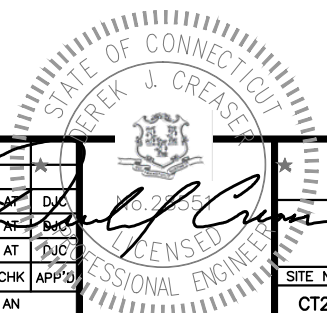
SECTION "A" - SURGE ABSORBERS

- INTERIOR GROUND RING (#2)
- EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2)
- METALLIC COLD WATER PIPE (IF AVAILABLE) (#2)
- BUILDING STEEL (IF AVAILABLE) (#2)



GROUND BAR - DETAIL 4
SCALE: N.T.S. G-1

| | | | | | |
|-----------------|----------|-------------------------|--------------|-----|-------|
| 1 | 04/30/18 | ISSUED FOR CONSTRUCTION | EB | AT | DJC |
| 0 | 12/19/17 | ISSUED FOR REVIEW | SG | AT | DJC |
| A | 11/16/17 | ISSUED FOR REVIEW | AN | AT | DJC |
| NO. | DATE | REVISIONS | BY | CHK | APP'D |
| SCALE: AS SHOWN | | DESIGNED BY: AT | DRAWN BY: AN | | |



| | | |
|------------------------|----------------|-----|
| AT&T | | |
| GROUNDING DETAILS | | |
| LTE 3C-4C 2018 UPGRADE | | |
| SITE NUMBER | DRAWING NUMBER | REV |
| CT2177 | G-1 | 1 |

EXHIBIT 3

STRUCTURAL ANALYSIS REPORT

For

CT2177 (3C/4C)

SITE CT-305

7 Broadway Avenue Extension

Mystic, CT 06355

Antennas Mounted on Water Tank Catwalk Handrail Equipment on Concrete Slab on Grade



Prepared for:



Dated: April 17, 2018

Prepared by:



45 Beechwood Drive
North Andover, MA 01845
Phone: (978) 557-5553

www.hudsondesigngroupllc.com





SCOPE OF WORK:

Hudson Design Group LLC (HDG) has been authorized by AT&T to conduct a structural evaluation of the structure supporting the proposed AT&T equipment located in the areas depicted in the latest HDG construction drawings.

This report represents this office's findings, conclusions and recommendations pertaining to the support of AT&T's proposed equipment.

An on-site visual survey of the above site was conducted on April 4, 2018.

CONCLUSION SUMMARY:

Water tank plans were not available and could not be obtained for our use. A limited visual survey of the structure was completed in or near the areas of the proposed work.

Based on our evaluation, we have determined that the existing structure **IS NOT CAPABLE** of supporting the proposed equipment loading. HDG recommends the following modifications:

- **Reinforce the existing L2x2x1/4 angle top handrail with new L2x2x1/4 angles (typ. of 3 per sector, total of 9).**
- **Install new L3x3x3/8 angle braces, secure to the existing handrail (typ. of 6 per sector, total of 18).**

APPURTENANCE/EQUIPMENT CONFIGURATION:

(3) 7770 Antennas (55.0"x11.0"x5.0" – Wt. = 35 lbs. /each)

(6) RRUS-11 RRH's (19.7"x17.0"x7.2" – Wt. = 51 lbs. /each)

(3) Surge Arrestors (10.3"x10.3" x6.2" – Wt. = 16 lbs. /each)

(3) SBNHH-1D65A Antennas (55.6"x11.9"x7.1" – Wt. = 34 lbs. /each)

(3) QS46512-2 Antennas (52.0"x12.0"x10.8" – Wt. = 75 lbs. /each)

(3) RRUS-32 B2 RRH's (27.2"x12.1"x7.0" – Wt. = 60 lbs. /each)

(3) TT19-08BP111-001 TMA's (9.9"x6.7"x5.4" - Wt. = 16 lbs. /each)

**Proposed Loading Shown in Bold.*



DESIGN CRITERIA:

1. International Building Code 2012 with 2005 Connecticut Supplement with 2016 Amendments; ASCE 7-10 Minimum Design Loads for Buildings and Other Structures.

Wind Analysis:

| | | |
|------------------------------------|---------|-------------------------|
| Ultimate Wind Speed (V_{ult}): | 135 mph | (CTSBC 2016 Appendix N) |
| Nominal Wind Speed (V_{asd}): | 105 mph | (CTSBC 2016 Appendix N) |
| Category: | D | |

2. EIA/TIA -222- G Structural Standards for Steel Antenna Towers and Antenna Supporting Structures

| | |
|------------------------|------------|
| City/Town: | Mystic |
| County: | New London |
| Wind Load: | 120 mph |
| Nominal Ice Thickness: | 3/4 inch |

3. Approximate height above grade to the center of the Antennas:

140'-0"+/-



ANTENNA SUPPORT RECOMMENDATIONS:

The new antennas are proposed to be mounted on new pipe masts installed on existing steel frames secured to the existing catwalk handrail.

RRH SUPPORT RECOMMENDATIONS:

The new RRH's are proposed to be mounted on new unistrut components secured to the existing catwalk handrail.

Limitations and assumptions:

1. Reference the latest HDG construction drawings for all the equipment locations details.
2. Mount all equipment per manufacturer's specifications.
3. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
4. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer requirements.
5. HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
6. If field conditions differ from what is assumed in this report, then the engineer of record is to be notified as soon as possible.



HUDSON
Design Group LLC

FIELD PHOTOS:



Photo 1: Sample photo illustrating the existing antennas and RRH's.



Photo 2: Sample photo illustrating the existing equipment cabinets.



HUDSON
Design Group LLC

Wind & Ice Calculations

Date: 4/17/2018

Project Name: SITE CT-305

Project Number: CT2177

Designed By: JN Checked By: MSC



HUDSON
Design Group LLC

2.6.5.2 Velocity Pressure Coeff:

$$K_z = 2.01 (z/z_g)^{2/\alpha}$$

z = 140 (ft)

z_g = 700 (ft)

α = 11.5

K_z = 1.519

$$K_{zmin} \leq K_z \leq 2.01$$

Table 2-4

| Exposure | Z _g | α | K _{zmin} | K _e |
|----------|----------------|------|-------------------|----------------|
| B | 1200 ft | 7.0 | 0.70 | 0.9 |
| C | 900 ft | 9.5 | 0.85 | 1.0 |
| D | 700 ft | 11.5 | 1.03 | 1.1 |

2.6.6.4 Topographic Factor:

Table 2-5

| Topo. Category | K _t | f |
|----------------|----------------|------|
| 2 | 0.43 | 1.25 |
| 3 | 0.53 | 2.0 |
| 4 | 0.72 | 1.5 |

$$K_{zt} = [1 + (K_e K_t / K_h)]^2$$

$$K_h = e^{(fz/H)}$$

K_{zt} = #DIV/0!

K_h = #DIV/0!

K_e = 0 (from Table 2-4)

K_t = 0 (from Table 2-5)

f = 0 (from Table 2-5)

z = 140

H = 0 (Ht. of the crest above surrounding terrain)

K_{zt} = 1.00

(If Category 1 then K_{zt} = 1.0)

Category = 1

Date: 4/17/2018
 Project Name: SITE CT-305
 Project Number: CT2177
 Designed By: JN Checked By: MSC



2.6.7 Gust Effect Factor

2.6.7.1 Self Supporting Lattice Structures

Gh = 1.0 Latticed Structures > 600 ft

Gh = 0.85 Latticed Structures 450 ft or less

Gh = 0.85 + 0.15 [h/150 - 3.0] h= ht. of structure

h= 156 Gh= 0.85

2.6.7.2 Guyed Masts Gh= 0.85

2.6.7.3 Pole Structures Gh= 1.1

2.6.9 Appurtenances Gh= 1.0

2.6.7.4 Structures Supported on Other Structures
 (Cantilivered tubular or latticed spines, pole, structures on buildings (ht. : width ratio > 5)

Gh= 1.35 Gh= 1.35

2.6.9.2 Design Wind Force on Appurtenances

$F = q_z * Gh * (EPA)_A$

$q_z = 0.00256 * K_z * K_{zt} * K_d * V_{max}^2 * I$

$K_z = 1.519$
 $K_{zt} = 1.0$
 $K_d = 0.95$
 $V_{max} = 120$
 $V_{max(ice)} = 50$
 $I = 1.0$

$q_z = 53.21$
 $q_z(ice) = 9.24$

Table 2-2

| Structure Type | Wind Direction Probability Factor, Kd |
|---|---------------------------------------|
| Latticed structures with triangular, square or rectangular cross sections | 0.85 |
| Tubular pole structures, latticed structures with other cross sections, appurtenances | 0.95 |

Date: 4/17/2018

Project Name: SITE CT-305

Project Number: CT2177

Designed By: JN Checked By: MSC



Determine Ca:

Table 2-8

| Force Coefficients (Ca) for Appurtenances | | | | |
|---|-------------------------------|--------------------|--------------------|-------------------|
| Member Type | | Aspect Ratio ≤ 2.5 | Aspect Ratio = 7 | Aspect Ratio ≥ 25 |
| | | Ca | Ca | Ca |
| Flat | | 1.2 | 1.4 | 2.0 |
| Round | C < 32 (Subcritical) | 0.7 | 0.8 | 1.2 |
| | 32 ≤ C ≤ 64 (Transitional) | $3.76/(C^{0.485})$ | $3.37/(C^{0.415})$ | $38.4/(C^{1.0})$ |
| | C > 64 (Supercritical) | 0.5 | 0.6 | 0.6 |

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.
(Aspect ratio is independent of the spacing between support points of a linear appurtenance, and the section length considered to have uniform wind load).

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness = **0.75 in**

| <u>Appurtenances</u> | <u>Height</u> | <u>Width</u> | <u>Depth</u> | <u>Flat Area</u> | <u>Aspect Ratio</u> | <u>Ca</u> | <u>Force (lbs)</u> | <u>Force (lbs) (3/4" Ice)</u> |
|----------------------|---------------|--------------|--------------|------------------|---------------------|-----------|--------------------|-----------------------------------|
| 7770 Antenna | 55.0 | 11.0 | 5.0 | 4.20 | 5.00 | 1.31 | 396 | 80 |
| SBNHH-1D65A Antenna | 55.6 | 11.9 | 7.1 | 4.59 | 4.67 | 1.30 | 428 | 86 |
| QS46512-2 Antenna | 52.0 | 12.0 | 10.8 | 4.33 | 4.33 | 1.28 | 399 | 80 |
| RRUS-11 RRH | 19.7 | 17.0 | 7.2 | 2.33 | 1.16 | 1.20 | 200 | 41 |
| RRUS-32 B2 RRH | 27.2 | 12.1 | 7.0 | 2.29 | 2.25 | 1.20 | 197 | 41 |
| TT19-08BP111-001 TMA | 9.9 | 6.7 | 5.4 | 0.46 | 1.48 | 1.20 | 40 | 10 |
| Squid Surge Arrestor | 24.0 | 9.7 | 9.7 | 1.62 | 2.47 | 0.70 | 81 | 17 |

Date: 4/17/2018

Project Name: SITE CT-305

Project Number: CT2177

Designed By: JN Checked By: MSC



HUDSON
Design Group LLC

ICE WEIGHT CALCULATIONS

Thickness of ice (in): 0.75

* Density of ice used = 56 PCF

7770 Antenna

Weight of ice based on total radial SF area:

Height (in): 55.0

Width (in): 11.0

Depth (in): 5.0

Total weight of ice on object: 45 lbs

Weight of object: 35 lbs

Combined weight of ice and object: 80 lbs

QS46512-2 Antenna

Weight of ice based on total radial SF area:

Height (in): 52.0

Width (in): 12.0

Depth (in): 10.8

Total weight of ice on object: 64 lbs

Weight of object: 75 lbs

Combined weight of ice and object: 139 lbs

RRUS-32 B2 RRH

Weight of ice based on total radial SF area:

Height (in): 27.2

Width (in): 12.1

Depth (in): 7.0

Total weight of ice on object: 29 lbs

Weight of object: 60 lbs

Combined weight of ice and object: 89 lbs

Surge Arrestor

Weight of ice based on total radial SF area:

Height (in): 10.3

Width (in): 10.3

Depth (in): 6.2

Total weight of ice on object: 11 lbs

Weight of object: 16 lbs

Combined weight of ice and object: 27 lbs

L2x2x1/4

Weight of ice based on total radial SF area:

Height (in): 2.0

Width (in): 2.0

Depth (in): 12.0

Total weight of ice on object: 3 lbs

L4x4x1/4

Weight of ice based on total radial SF area:

Height (in): 4.0

Width (in): 4.0

Depth (in): 12.0

Total weight of ice on object: 5 lbs

L6x4x3/8

Weight of ice based on total radial SF area:

Height (in): 6.0

Width (in): 4.0

Depth (in): 12.0

Total weight of ice on object: 7 lbs

2" pipe

Per foot weight of ice:

diameter (in): 2.375

Per foot weight of ice on object: 2 lbs/ft

SBNHH-1D65A Antenna

Weight of ice based on total radial SF area:

Height (in): 55.6

Width (in): 11.9

Depth (in): 7.1

Total weight of ice on object: 55 lbs

Weight of object: 34 lbs

Combined weight of ice and object: 89 lbs

RRUS-11 RRH

Weight of ice based on total radial SF area:

Height (in): 19.7

Width (in): 17.0

Depth (in): 7.2

Total weight of ice on object: 29 lbs

Weight of object: 51 lbs

Combined weight of ice and object: 80 lbs

TT19-08BP111-001 TMA

Weight of ice based on total radial SF area:

Height (in): 9.9

Width (in): 6.7

Depth (in): 5.4

Total weight of ice on object: 8 lbs

Weight of object: 16 lbs

Combined weight of ice and object: 24 lbs

PL2x1/4

Weight of ice based on total radial SF area:

Height (in): 2.0

Width (in): 0.25

Depth (in): 12.0

Total weight of ice on object: 1 lbs

L3x3x1/4

Weight of ice based on total radial SF area:

Height (in): 3.0

Width (in): 3.0

Depth (in): 12.0

Total weight of ice on object: 4 lbs

L5x3x1/4

Weight of ice based on total radial SF area:

Height (in): 5.0

Width (in): 3.0

Depth (in): 12.0

Total weight of ice on object: 5 lbs

Unistrut

Weight of ice based on total radial SF area:

Height (in): 1.6

Width (in): 1.6

Depth (in): 12.0

Total weight of ice on object: 2 lbs

3" pipe

Per foot weight of ice:

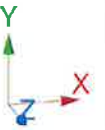
diameter (in): 3.5

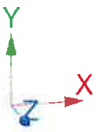
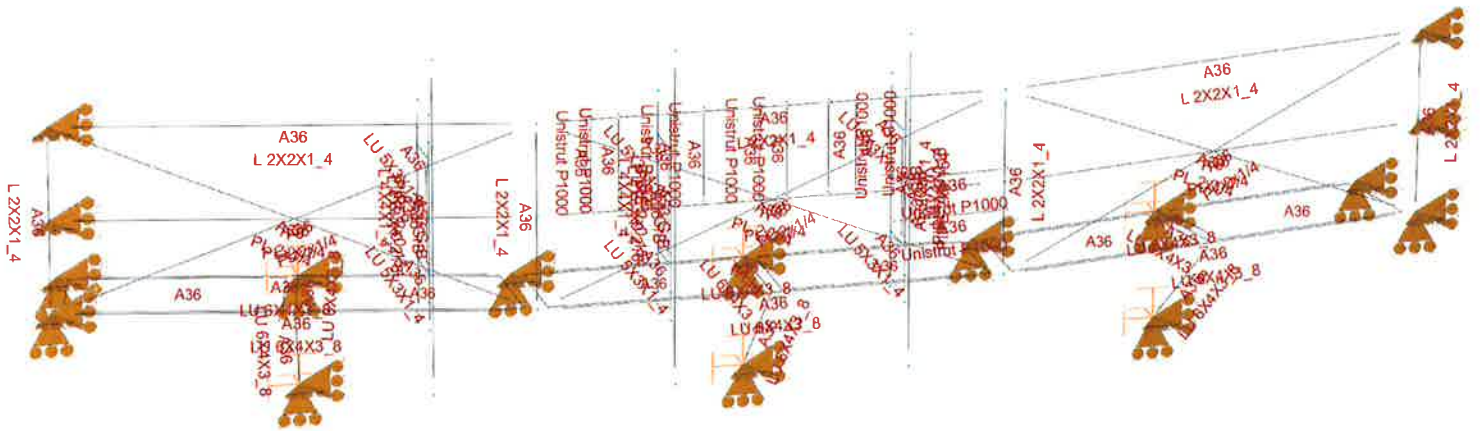
Per foot weight of ice on object: 3 lbs/ft



HUDSON
Design Group LLC

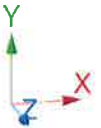
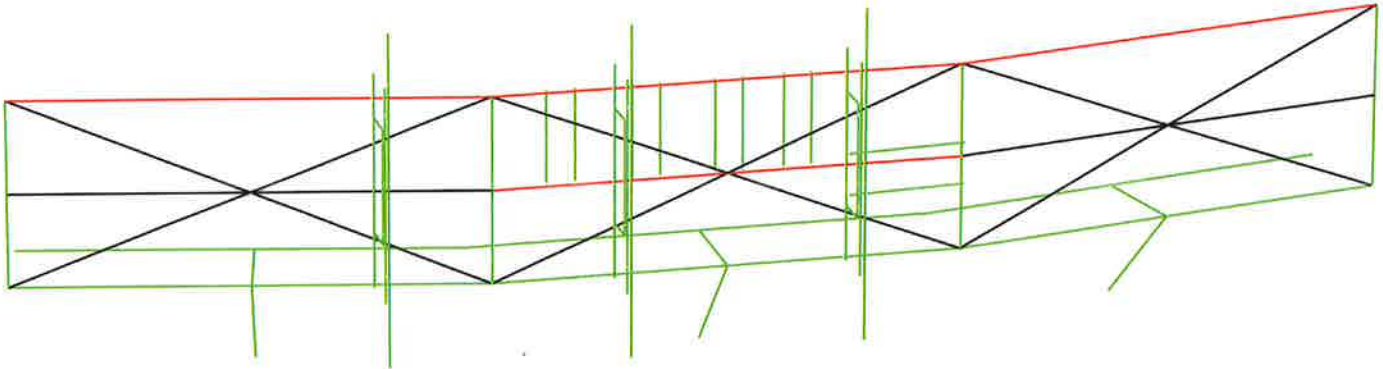
**Antenna Mount Calculations
(Existing Conditions)**

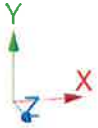
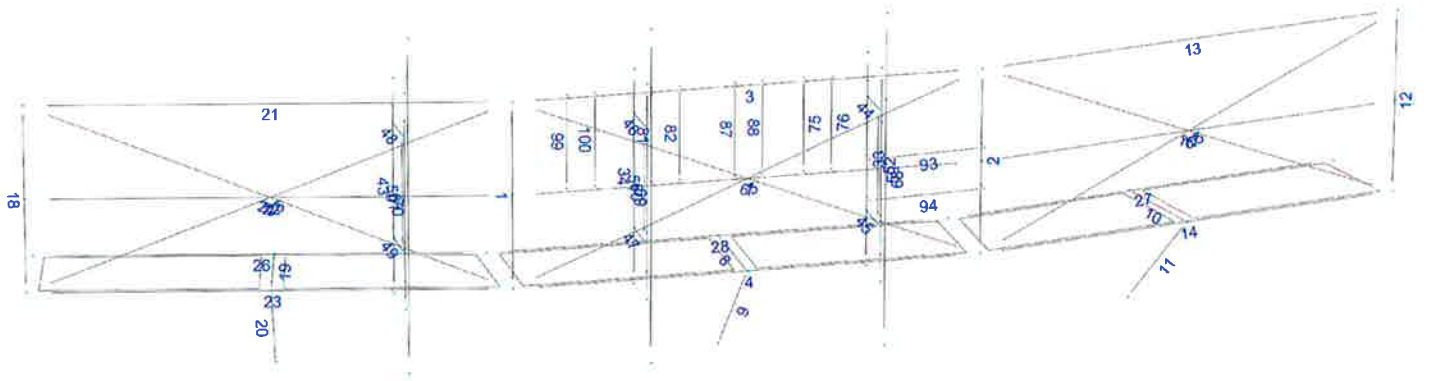




Design status

- Not designed
- Error on design
- Design O.K.
- With warnings





Current Date: 4/18/2018 9:30 AM

Units system: English

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Load data

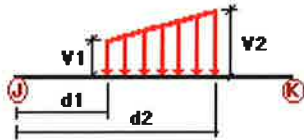
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

| Condition | Description | Comb. | Category |
|-----------|----------------------|-------|----------|
| DL | Dead Load | No | DL |
| Wo | Wind Load (No Ice) | No | WIND |
| Wi | Wind Load (With Ice) | No | WIND |
| Di | Ice Load | No | LL |

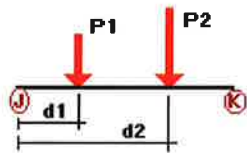
Distributed force on members



| Condition | Member | Dir1 | Val1 [Kip/ft] | Val2 [Kip/ft] | Dist1 [ft] | % | Dist2 [ft] | % |
|-----------|--------|------|------------------|------------------|---------------|----|---------------|----|
| Di | 1 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| | 2 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| | 3 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| | 4 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| | 5 | y | -0.001 | 0.00 | 0.00 | No | 0.00 | No |
| | 6 | y | -0.001 | 0.00 | 0.00 | No | 0.00 | No |
| | 7 | y | -0.001 | 0.00 | 0.00 | No | 0.00 | No |
| | 8 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| | 9 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| | 10 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| | 11 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| | 12 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| | 13 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| | 14 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| | 15 | y | -0.001 | 0.00 | 0.00 | No | 0.00 | No |
| | 16 | y | -0.001 | 0.00 | 0.00 | No | 0.00 | No |
| | 17 | y | -0.001 | 0.00 | 0.00 | No | 0.00 | No |
| | 18 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| | 19 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| | 20 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| | 21 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| | 22 | y | -0.001 | 0.00 | 0.00 | No | 0.00 | No |
| | 23 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| | 24 | y | -0.001 | 0.00 | 0.00 | No | 0.00 | No |
| | 25 | y | -0.001 | 0.00 | 0.00 | No | 0.00 | No |

| | | | | | | | |
|-----|---|--------|------|------|----|------|----|
| 26 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| 27 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| 28 | y | -0.007 | 0.00 | 0.00 | No | 0.00 | No |
| 33 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 34 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 43 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 44 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 45 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 46 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 47 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 48 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 49 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 50 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 51 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 52 | y | -0.005 | 0.00 | 0.00 | No | 0.00 | No |
| 59 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| 60 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| 61 | y | -0.003 | 0.00 | 0.00 | No | 0.00 | No |
| 68 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 69 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 70 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 75 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 76 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 81 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 82 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 87 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 88 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 93 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 94 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 99 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |
| 100 | y | -0.002 | 0.00 | 0.00 | No | 0.00 | No |

Concentrated forces on members



| Condition | Member | Dir1 | Value1 [Kip] | Dist1 [ft] | % |
|-----------|--------|------|-----------------|---------------|-----|
| DL | 68 | y | -0.018 | 1.00 | No |
| | | y | -0.018 | 5.00 | No |
| | 69 | y | -0.017 | 1.00 | No |
| | | y | -0.017 | 5.00 | No |
| | 70 | y | -0.038 | 1.00 | No |
| | | y | -0.038 | 5.00 | No |
| | 75 | y | -0.026 | 50.00 | Yes |
| | 76 | y | -0.026 | 50.00 | Yes |
| | 81 | y | -0.026 | 50.00 | Yes |
| | 82 | y | -0.026 | 50.00 | Yes |
| | 87 | y | -0.03 | 50.00 | Yes |
| | 88 | y | -0.03 | 50.00 | Yes |
| | 93 | y | -0.008 | 50.00 | Yes |
| | 94 | y | -0.008 | 50.00 | Yes |

| | | | | | |
|----|-----|---|--------|-------|-----|
| | 99 | y | -0.008 | 50.00 | Yes |
| | 100 | y | -0.008 | 50.00 | Yes |
| Wo | 68 | z | -0.198 | 1.00 | No |
| | | z | -0.198 | 5.00 | No |
| | 69 | z | -0.214 | 1.00 | No |
| | | z | -0.214 | 5.00 | No |
| | 70 | z | -0.20 | 1.00 | No |
| | | z | -0.20 | 5.00 | No |
| | 75 | z | -0.10 | 50.00 | Yes |
| | 76 | z | -0.10 | 50.00 | Yes |
| | 81 | z | -0.10 | 50.00 | Yes |
| | 82 | z | -0.10 | 50.00 | Yes |
| | 87 | z | -0.099 | 50.00 | Yes |
| | 88 | z | -0.099 | 50.00 | Yes |
| | 93 | z | -0.02 | 50.00 | Yes |
| | 94 | z | -0.02 | 50.00 | Yes |
| | 99 | z | -0.041 | 50.00 | Yes |
| | 100 | z | -0.041 | 50.00 | Yes |
| Wi | 68 | z | -0.04 | 1.00 | No |
| | | z | -0.04 | 5.00 | No |
| | 69 | z | -0.043 | 1.00 | No |
| | | z | -0.043 | 5.00 | No |
| | 70 | z | -0.04 | 1.00 | No |
| | | z | -0.04 | 5.00 | No |
| | 75 | z | -0.021 | 50.00 | Yes |
| | 76 | z | -0.021 | 50.00 | Yes |
| | 81 | z | -0.021 | 50.00 | Yes |
| | 82 | z | -0.021 | 50.00 | Yes |
| | 87 | z | -0.021 | 50.00 | Yes |
| | 88 | z | -0.021 | 50.00 | Yes |
| | 93 | z | -0.005 | 50.00 | Yes |
| | 94 | z | -0.005 | 50.00 | Yes |
| | 99 | z | -0.009 | 50.00 | Yes |
| | 100 | z | -0.009 | 50.00 | Yes |
| Di | 68 | y | -0.023 | 1.00 | No |
| | | y | -0.023 | 5.00 | No |
| | 69 | y | -0.028 | 1.00 | No |
| | | y | -0.028 | 5.00 | No |
| | 70 | y | -0.032 | 1.00 | No |
| | | y | -0.032 | 5.00 | No |
| | 75 | y | -0.015 | 50.00 | Yes |
| | 76 | y | -0.015 | 50.00 | Yes |
| | 81 | y | -0.015 | 50.00 | Yes |
| | 82 | y | -0.015 | 50.00 | Yes |
| | 87 | y | -0.015 | 50.00 | Yes |
| | 88 | y | -0.015 | 50.00 | Yes |
| | 93 | y | -0.004 | 50.00 | Yes |
| | 94 | y | -0.004 | 50.00 | Yes |
| | 99 | y | -0.006 | 50.00 | Yes |
| | 100 | y | -0.006 | 50.00 | Yes |

Self weight multipliers for load conditions

| Condition | Description | Self weight multiplier | | | |
|-----------|----------------------|------------------------|-------|-------|-------|
| | | Comb. | MultX | MultY | MultZ |
| DL | Dead Load | No | 0.00 | -1.00 | 0.00 |
| Wo | Wind Load (No Ice) | No | 0.00 | 0.00 | 0.00 |
| Wi | Wind Load (With Ice) | No | 0.00 | 0.00 | 0.00 |
| Di | Ice Load | No | 0.00 | 0.00 | 0.00 |

Earthquake (Dynamic analysis only)

| Condition | a/g | Ang. [Deg] | Damp. [%] |
|-----------|------|---------------|--------------|
| DL | 0.00 | 0.00 | 0.00 |
| Wo | 0.00 | 0.00 | 0.00 |
| Wi | 0.00 | 0.00 | 0.00 |
| Di | 0.00 | 0.00 | 0.00 |

Current Date: 4/18/2018 9:30 AM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT2177\CT2177 (LTE 3C-4C).et3

Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design :

- LC1=1.2DL+1.6Wo
- LC2=0.9DL+1.6Wo
- LC3=1.2DL+Wi+Di
- LC4=1.2DL
- LC5=0.9DL

| Description | Section | Member | Ctrl Eq. | Ratio | Status | Reference |
|-------------|------------------|-----------|----------------|-------------|---------------|-----------|
| | L 2X2X1_4 | 1 | LC1 at 0.00% | 0.42 | OK | |
| | | | LC2 at 0.00% | 0.43 | OK | Eq. H2-1 |
| | | | LC3 at 0.00% | 0.04 | OK | |
| | | | LC4 at 0.00% | 0.03 | OK | |
| | | | LC5 at 0.00% | 0.03 | OK | |
| | | 2 | LC1 at 100.00% | 0.43 | OK | |
| | | | LC2 at 100.00% | 0.46 | OK | Eq. H2-1 |
| | | | LC3 at 0.00% | 0.06 | OK | |
| | | | LC4 at 100.00% | 0.06 | OK | |
| | | | LC5 at 100.00% | 0.04 | OK | |
| | | 3 | LC1 at 47.73% | 3.85 | N.G. | |
| | | | LC2 at 47.73% | 3.92 | N.G. | Eq. H2-1 |
| | | | LC3 at 74.43% | 0.26 | With warnings | |
| | | | LC4 at 0.00% | 0.13 | With warnings | |
| | | | LC5 at 0.00% | 0.10 | With warnings | |
| | | 12 | LC1 at 0.00% | 0.07 | OK | |
| | | | LC2 at 0.00% | 0.07 | OK | Eq. H3-8 |
| | | | LC3 at 100.00% | 0.09 | OK | Eq. H2-1 |
| | | | LC4 at 100.00% | 0.06 | OK | |
| | | | LC5 at 100.00% | 0.04 | OK | |
| | | 13 | LC1 at 0.00% | 2.30 | N.G. | |
| | | | LC2 at 0.00% | 2.34 | N.G. | Eq. H2-1 |
| | | | LC3 at 100.00% | 0.15 | With warnings | |
| | | | LC4 at 0.00% | 0.07 | With warnings | |
| | | | LC5 at 0.00% | 0.05 | With warnings | |
| | | 18 | LC1 at 100.00% | 0.03 | OK | |
| | | | LC2 at 100.00% | 0.03 | OK | |
| | | | LC3 at 100.00% | 0.09 | OK | Eq. H2-1 |
| | | | LC4 at 100.00% | 0.06 | OK | |
| | | | LC5 at 100.00% | 0.04 | OK | |
| | | 21 | LC1 at 0.00% | 4.16 | N.G. | |
| | | | LC2 at 0.00% | 4.25 | N.G. | Eq. H2-1 |
| | | | LC3 at 25.00% | 0.16 | With warnings | |
| | | | LC4 at 0.00% | 0.14 | With warnings | |
| | | | LC5 at 0.00% | 0.11 | With warnings | |
| | L 4X4X1_4 | 33 | LC1 at 13.54% | 0.75 | OK | |
| | | | LC2 at 13.54% | 0.76 | OK | Eq. H3-8 |

LU 5X3X1_4

| | | | | |
|-----------|----------------|-------------|-----------|----------|
| | LC3 at 68.75% | 0.08 | OK | |
| | LC4 at 13.54% | 0.03 | OK | |
| | LC5 at 13.54% | 0.03 | OK | |
| 34 | LC1 at 75.00% | 0.52 | OK | Eq. H3-8 |
| | LC2 at 75.00% | 0.51 | OK | |
| | LC3 at 100.00% | 0.08 | OK | |
| | LC4 at 100.00% | 0.04 | OK | |
| | LC5 at 100.00% | 0.03 | OK | |
| 43 | LC1 at 14.06% | 0.31 | OK | Eq. H3-8 |
| | LC2 at 14.06% | 0.31 | OK | |
| | LC3 at 75.00% | 0.05 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| 50 | LC1 at 91.67% | 0.09 | OK | Eq. H3-8 |
| | LC2 at 91.67% | 0.09 | OK | |
| | LC3 at 91.67% | 0.03 | OK | |
| | LC4 at 0.00% | 0.01 | OK | |
| | LC5 at 0.00% | 0.01 | OK | |
| 51 | LC1 at 100.00% | 0.07 | OK | Eq. H2-1 |
| | LC2 at 100.00% | 0.07 | OK | |
| | LC3 at 91.67% | 0.02 | OK | |
| | LC4 at 0.00% | 0.01 | OK | |
| | LC5 at 0.00% | 0.01 | OK | |
| 52 | LC1 at 0.00% | 0.29 | OK | |
| | LC2 at 0.00% | 0.29 | OK | Eq. H3-8 |
| | LC3 at 91.67% | 0.03 | OK | |
| | LC4 at 100.00% | 0.01 | OK | |
| | LC5 at 100.00% | 0.01 | OK | |
| 44 | LC1 at 100.00% | 0.11 | OK | |
| | LC2 at 100.00% | 0.12 | OK | Eq. H2-1 |
| | LC3 at 0.00% | 0.04 | OK | |
| | LC4 at 0.00% | 0.02 | OK | |
| | LC5 at 0.00% | 0.02 | OK | |
| 45 | LC1 at 100.00% | 0.17 | OK | Eq. H2-1 |
| | LC2 at 100.00% | 0.17 | OK | |
| | LC3 at 100.00% | 0.03 | OK | |
| | LC4 at 0.00% | 0.01 | OK | |
| | LC5 at 0.00% | 0.01 | OK | |
| 46 | LC1 at 0.00% | 0.10 | OK | |
| | LC2 at 0.00% | 0.11 | OK | Eq. H2-1 |
| | LC3 at 0.00% | 0.04 | OK | |
| | LC4 at 0.00% | 0.04 | OK | |
| | LC5 at 0.00% | 0.03 | OK | |
| 47 | LC1 at 0.00% | 0.09 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.09 | OK | |
| | LC3 at 0.00% | 0.02 | OK | |
| | LC4 at 0.00% | 0.01 | OK | |
| | LC5 at 0.00% | 0.01 | OK | |
| 48 | LC1 at 100.00% | 0.06 | OK | |
| | LC2 at 100.00% | 0.06 | OK | Eq. H2-1 |
| | LC3 at 0.00% | 0.03 | OK | |
| | LC4 at 0.00% | 0.03 | OK | |
| | LC5 at 0.00% | 0.02 | OK | |

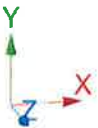
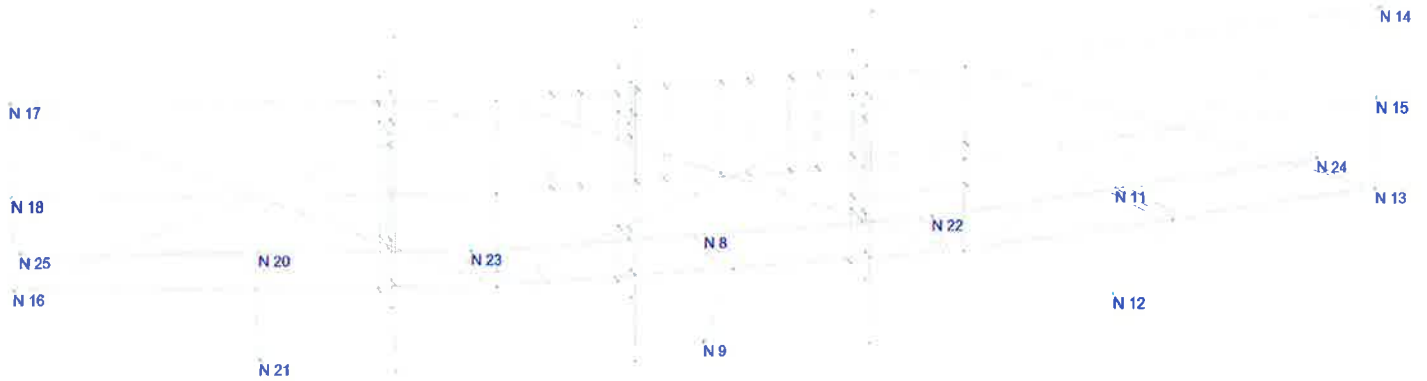
LU 6X4X3_8

| | | | | |
|----|----------------|-------------|-----------|----------|
| 49 | LC1 at 100.00% | 0.15 | OK | Eq. H2-1 |
| | LC2 at 100.00% | 0.14 | OK | |
| | LC3 at 100.00% | 0.06 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| 4 | LC1 at 62.50% | 0.46 | OK | Eq. H3-8 |
| | LC2 at 62.50% | 0.43 | OK | |
| | LC3 at 50.00% | 0.20 | OK | |
| | LC4 at 49.22% | 0.15 | OK | |
| | LC5 at 49.22% | 0.11 | OK | |
| 8 | LC1 at 100.00% | 0.06 | OK | Eq. H3-8 |
| | LC2 at 100.00% | 0.05 | OK | |
| | LC3 at 100.00% | 0.05 | OK | |
| | LC4 at 100.00% | 0.04 | OK | |
| | LC5 at 100.00% | 0.03 | OK | |
| 9 | LC1 at 0.00% | 0.10 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.10 | OK | |
| | LC3 at 100.00% | 0.04 | OK | |
| | LC4 at 0.00% | 0.04 | OK | |
| | LC5 at 0.00% | 0.03 | OK | |
| 10 | LC1 at 98.44% | 0.04 | OK | Eq. H3-8 |
| | LC2 at 98.44% | 0.03 | OK | |
| | LC3 at 98.44% | 0.03 | OK | |
| | LC4 at 98.44% | 0.02 | OK | |
| | LC5 at 98.44% | 0.02 | OK | |
| 11 | LC1 at 0.00% | 0.05 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.05 | OK | |
| | LC3 at 0.00% | 0.03 | OK | |
| | LC4 at 0.00% | 0.02 | OK | |
| | LC5 at 0.00% | 0.01 | OK | |
| 14 | LC1 at 0.00% | 0.11 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.10 | OK | |
| | LC3 at 50.00% | 0.06 | OK | |
| | LC4 at 50.00% | 0.04 | OK | |
| | LC5 at 50.00% | 0.03 | OK | |
| 19 | LC1 at 98.44% | 0.03 | OK | Eq. H3-8 |
| | LC2 at 98.44% | 0.03 | OK | |
| | LC3 at 100.00% | 0.02 | OK | |
| | LC4 at 100.00% | 0.01 | OK | |
| | LC5 at 100.00% | 0.01 | OK | |
| 20 | LC1 at 0.00% | 0.04 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.06 | OK | |
| | LC3 at 0.00% | 0.08 | OK | |
| | LC4 at 0.00% | 0.06 | OK | |
| | LC5 at 0.00% | 0.05 | OK | |
| 23 | LC1 at 75.00% | 0.10 | OK | Eq. H2-1 |
| | LC2 at 50.00% | 0.12 | OK | |
| | LC3 at 50.00% | 0.16 | OK | Eq. H2-1 |
| | LC4 at 50.00% | 0.13 | OK | |
| | LC5 at 50.00% | 0.09 | OK | |
| 26 | LC1 at 0.00% | 0.05 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.05 | OK | |
| | LC3 at 0.00% | 0.02 | OK | |
| | LC4 at 48.44% | 0.02 | OK | |

| | | | | | |
|---------------------|-----------|----------------|-------------|----------------------|-----------|
| | | LC5 at 48.44% | 0.01 | OK | |
| | 27 | LC1 at 100.00% | 0.04 | OK | Eq. H2-1 |
| | | LC2 at 100.00% | 0.04 | OK | |
| | | LC3 at 100.00% | 0.02 | OK | |
| | | LC4 at 100.00% | 0.02 | OK | |
| | | LC5 at 100.00% | 0.01 | OK | |
| | 28 | LC1 at 100.00% | 0.06 | OK | Eq. H3-8 |
| | | LC2 at 100.00% | 0.06 | OK | |
| | | LC3 at 100.00% | 0.03 | OK | |
| | | LC4 at 100.00% | 0.02 | OK | |
| | | LC5 at 100.00% | 0.01 | OK | |
| PIPE 2x0.154 | 68 | LC1 at 25.00% | 0.13 | OK | Eq. H1-1b |
| | | LC2 at 25.00% | 0.13 | OK | |
| | | LC3 at 25.00% | 0.02 | OK | |
| | | LC4 at 27.08% | 0.00 | OK | |
| | | LC5 at 27.08% | 0.00 | OK | |
| | 69 | LC1 at 25.00% | 0.14 | OK | Eq. H1-1b |
| | | LC2 at 25.00% | 0.14 | OK | |
| | | LC3 at 25.00% | 0.02 | OK | |
| | | LC4 at 27.08% | 0.00 | OK | |
| | | LC5 at 27.08% | 0.00 | OK | |
| | 70 | LC1 at 25.00% | 0.13 | OK | Eq. H1-1b |
| | | LC2 at 25.00% | 0.13 | OK | |
| | | LC3 at 25.00% | 0.02 | OK | |
| | | LC4 at 27.08% | 0.01 | OK | |
| | | LC5 at 27.08% | 0.00 | OK | |
| PIPE 3x0.216 | 59 | LC1 at 70.00% | 0.05 | OK | Eq. H1-1b |
| | | LC2 at 70.00% | 0.05 | OK | |
| | | LC3 at 68.75% | 0.01 | OK | |
| | | LC4 at 26.25% | 0.00 | OK | |
| | | LC5 at 26.25% | 0.00 | OK | |
| | 60 | LC1 at 70.00% | 0.05 | OK | Eq. H1-1b |
| | | LC2 at 70.00% | 0.05 | OK | |
| | | LC3 at 68.75% | 0.01 | OK | |
| | | LC4 at 26.25% | 0.00 | OK | |
| | | LC5 at 26.25% | 0.00 | OK | |
| | 61 | LC1 at 70.00% | 0.05 | OK | Eq. H1-1b |
| | | LC2 at 70.00% | 0.05 | OK | |
| | | LC3 at 68.75% | 0.01 | OK | |
| | | LC4 at 68.75% | 0.01 | OK | |
| | | LC5 at 68.75% | 0.00 | OK | |
| PL 2x1/4 | 5 | LC1 at 0.00% | 0.81 | With warnings | |
| | | LC2 at 0.00% | 0.82 | With warnings | Eq. H3-6 |
| | | LC3 at 0.00% | 0.08 | With warnings | Eq. H1-2 |
| | | LC4 at 0.00% | 0.05 | With warnings | |
| | | LC5 at 0.00% | 0.04 | With warnings | |
| | 6 | LC1 at 50.00% | 0.84 | With warnings | |
| | | LC2 at 50.00% | 0.85 | With warnings | Eq. H3-6 |
| | | LC3 at 100.00% | 0.06 | With warnings | |
| | | LC4 at 50.00% | 0.05 | With warnings | |
| | | LC5 at 50.00% | 0.04 | With warnings | |
| | 7 | LC1 at 0.00% | 1.15 | N.G. | |
| | | LC2 at 0.00% | 1.17 | N.G. | Eq. H3-6 |

| | | | | | |
|-----------------------|----------------|----------------|----------------------|-------------|-----------|
| | LC3 at 0.00% | 0.06 | With warnings | | |
| | LC4 at 47.50% | 0.07 | With warnings | | |
| | LC5 at 47.50% | 0.05 | With warnings | | |
| 15 | LC1 at 50.00% | 0.11 | With warnings | | |
| | LC2 at 50.00% | 0.11 | With warnings | Eq. H1-1b | |
| | LC3 at 0.00% | 0.05 | With warnings | | |
| | LC4 at 0.00% | 0.03 | With warnings | | |
| | LC5 at 0.00% | 0.02 | With warnings | | |
| 16 | LC1 at 0.00% | 0.38 | With warnings | | |
| | LC2 at 0.00% | 0.39 | With warnings | Eq. H1-1b | |
| | LC3 at 100.00% | 0.08 | With warnings | Sec. E1 | |
| | LC4 at 100.00% | 0.05 | With warnings | | |
| | LC5 at 100.00% | 0.04 | With warnings | | |
| 17 | LC1 at 100.00% | 0.21 | With warnings | | |
| | LC2 at 100.00% | 0.22 | With warnings | Eq. H1-1b | |
| | LC3 at 0.00% | 0.03 | With warnings | | |
| | LC4 at 100.00% | 0.02 | With warnings | | |
| | LC5 at 100.00% | 0.01 | With warnings | | |
| 22 | LC1 at 0.00% | 0.19 | With warnings | | |
| | LC2 at 0.00% | 0.20 | With warnings | Eq. H1-1b | |
| | LC3 at 100.00% | 0.03 | With warnings | | |
| | LC4 at 100.00% | 0.02 | With warnings | | |
| | LC5 at 100.00% | 0.01 | With warnings | | |
| 24 | LC1 at 100.00% | 0.11 | With warnings | Eq. H1-1b | |
| | LC2 at 100.00% | 0.10 | With warnings | | |
| | LC3 at 0.00% | 0.08 | With warnings | Eq. Sec. D2 | |
| | LC4 at 0.00% | 0.07 | With warnings | | |
| | LC5 at 0.00% | 0.05 | With warnings | | |
| 25 | LC1 at 15.63% | 0.08 | With warnings | Eq. H1-1b | |
| | LC2 at 34.38% | 0.09 | With warnings | Eq. H1-1b | |
| | LC3 at 100.00% | 0.08 | With warnings | Sec. E1 | |
| | LC4 at 100.00% | 0.05 | With warnings | | |
| | LC5 at 100.00% | 0.04 | With warnings | | |
| Unistrut P1000 | 75 | LC1 at 0.00% | 0.26 | OK | |
| | | LC2 at 0.00% | 0.26 | OK | Sec. C5.1 |
| | | LC3 at 0.00% | 0.04 | OK | |
| | | LC4 at 0.00% | 0.03 | OK | |
| | | LC5 at 0.00% | 0.02 | OK | |
| | 76 | LC1 at 0.00% | 0.76 | OK | |
| | | LC2 at 0.00% | 0.77 | OK | Sec. C5.2 |
| | | LC3 at 0.00% | 0.09 | OK | |
| | | LC4 at 0.00% | 0.04 | OK | |
| | | LC5 at 0.00% | 0.03 | OK | |
| | 81 | LC1 at 0.00% | 0.89 | OK | |
| | | LC2 at 0.00% | 0.90 | OK | Sec. C5.1 |
| | | LC3 at 0.00% | 0.08 | OK | |
| | | LC4 at 100.00% | 0.05 | OK | |
| | | LC5 at 100.00% | 0.04 | OK | |
| | 82 | LC1 at 0.00% | 0.42 | OK | |
| | | LC2 at 0.00% | 0.43 | OK | Sec. C5.1 |
| | | LC3 at 0.00% | 0.04 | OK | |
| | | LC4 at 0.00% | 0.05 | OK | |
| | | LC5 at 0.00% | 0.04 | OK | |

| | | | | |
|------------|----------------|-------------|-----------|-----------|
| 87 | LC1 at 50.00% | 0.26 | OK | Sec. C5.2 |
| | LC2 at 50.00% | 0.26 | OK | |
| | LC3 at 50.00% | 0.05 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.03 | OK | |
| 88 | LC1 at 50.00% | 0.24 | OK | Sec. C5.2 |
| | LC2 at 50.00% | 0.24 | OK | |
| | LC3 at 50.00% | 0.05 | OK | |
| | LC4 at 100.00% | 0.02 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| 93 | LC1 at 0.00% | 0.44 | OK | Sec. C5.2 |
| | LC2 at 0.00% | 0.44 | OK | |
| | LC3 at 0.00% | 0.06 | OK | |
| | LC4 at 50.00% | 0.02 | OK | |
| | LC5 at 50.00% | 0.01 | OK | |
| 94 | LC1 at 0.00% | 0.41 | OK | Sec. C5.2 |
| | LC2 at 0.00% | 0.41 | OK | |
| | LC3 at 0.00% | 0.06 | OK | |
| | LC4 at 100.00% | 0.02 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| 99 | LC1 at 0.00% | 0.42 | OK | Sec. C5.1 |
| | LC2 at 0.00% | 0.41 | OK | |
| | LC3 at 0.00% | 0.04 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| 100 | LC1 at 0.00% | 0.69 | OK | Sec. C5.1 |
| | LC2 at 0.00% | 0.69 | OK | |
| | LC3 at 0.00% | 0.07 | OK | |
| | LC4 at 100.00% | 0.04 | OK | |
| | LC5 at 100.00% | 0.03 | OK | |



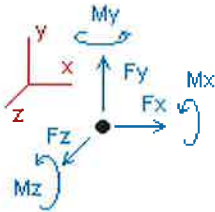
Current Date: 4/18/2018 9:30 AM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT2177\CT2177 (LTE 3C-4C).etz

Analysis result

Reactions



Direction of positive forces and moments

| Node | Forces [Kip] | | | Moments [Kip*ft] | | |
|----------------------------------|--------------|----------|----------|------------------|----------|----------|
| | FX | FY | FZ | MX | MY | MZ |
| Condition LC1=1.2DL+1.6Wo | | | | | | |
| 8 | -0.05208 | 0.37260 | 1.12693 | -0.24156 | 0.21413 | -0.00782 |
| 9 | 0.38374 | 0.63071 | 0.41078 | -0.16762 | 0.25947 | -0.23240 |
| 11 | -0.12563 | 0.17663 | 0.05954 | -0.07381 | -0.04898 | 0.03944 |
| 12 | -0.06247 | 0.29564 | 0.35925 | 0.02817 | -0.09624 | 0.08206 |
| 13 | -0.00512 | 0.41719 | 0.03551 | 0.00000 | 0.00000 | 0.00000 |
| 14 | -2.33384 | 0.00000 | 0.44291 | 0.00000 | 0.00000 | 0.00000 |
| 15 | -0.00271 | 0.00000 | 0.00261 | 0.00000 | 0.00000 | 0.00000 |
| 16 | 0.07104 | 0.11414 | 0.08108 | 0.00000 | 0.00000 | 0.00000 |
| 17 | 4.53218 | 0.00000 | 0.98306 | 0.00000 | 0.00000 | 0.00000 |
| 18 | -0.22060 | 0.00000 | -0.04780 | 0.00000 | 0.00000 | 0.00000 |
| 20 | 0.08505 | 0.15577 | -0.20950 | -0.05071 | 0.06390 | -0.04068 |
| 21 | -0.13129 | 0.06649 | 0.05235 | -0.00675 | -0.08108 | 0.07281 |
| 22 | -0.16504 | 0.25132 | -0.09436 | 0.00000 | 0.00000 | 0.00000 |
| 23 | -0.29328 | 0.33001 | -0.02108 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.06454 | 0.03076 | 0.00231 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.07124 | 0.03067 | 0.01573 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 149 | 0.02021 | 0.01448 | -0.01687 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 153 | -0.04856 | 0.02459 | 0.00508 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 160 | -0.39117 | -0.04575 | 0.15122 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 169 | -0.37760 | -0.06901 | -0.13771 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 173 | -0.77465 | -0.04594 | -0.31042 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 180 | -0.13890 | -0.03230 | 0.22374 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | -0.02050 | 0.02416 | 0.07141 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 188 | 0.04451 | 0.01319 | -0.07536 | 0.00000 | 0.00000 | 0.00000 |
| SUM | 0.00000 | 2.75537 | 3.11040 | -0.51227 | 0.31120 | -0.08659 |
| Condition LC2=0.9DL+1.6Wo | | | | | | |
| 8 | -0.05800 | 0.31729 | 1.14044 | -0.21252 | 0.20298 | -0.00743 |
| 9 | 0.41993 | 0.42664 | 0.18250 | -0.16813 | 0.28311 | -0.25354 |
| 11 | -0.11653 | 0.13869 | 0.07979 | -0.06178 | -0.05598 | 0.03358 |
| 12 | -0.06596 | 0.24385 | 0.30702 | 0.02945 | -0.09103 | 0.07700 |
| 13 | 0.00505 | 0.37720 | 0.02497 | 0.00000 | 0.00000 | 0.00000 |
| 14 | -2.44660 | 0.00000 | 0.46649 | 0.00000 | 0.00000 | 0.00000 |
| 15 | 0.00270 | 0.00000 | 0.00080 | 0.00000 | 0.00000 | 0.00000 |
| 16 | 0.10703 | 0.09689 | 0.09491 | 0.00000 | 0.00000 | 0.00000 |
| 17 | 4.68262 | 0.00000 | 1.01893 | 0.00000 | 0.00000 | 0.00000 |
| 18 | -0.22603 | 0.00000 | -0.04959 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|----------|----------|----------|----------|----------|----------|----------|
| 20 | 0.07236 | 0.13640 | -0.21245 | -0.04340 | 0.04258 | -0.03658 |
| 21 | -0.16868 | -0.09718 | -0.10666 | 0.00380 | -0.13186 | 0.12173 |
| 22 | -0.17315 | 0.21767 | -0.02611 | 0.00000 | 0.00000 | 0.00000 |
| 23 | -0.30045 | 0.29780 | 0.11143 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.05184 | 0.02310 | 0.00582 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.06349 | 0.02299 | 0.02515 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 149 | 0.04208 | 0.01133 | -0.00209 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 153 | -0.03879 | 0.01880 | 0.00674 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 160 | -0.40097 | -0.04452 | 0.17536 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 169 | -0.41863 | -0.06911 | -0.09653 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 173 | -0.77307 | -0.04776 | -0.26101 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 180 | -0.16072 | -0.03170 | 0.21604 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | -0.03229 | 0.01830 | 0.07322 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 188 | 0.03643 | 0.00986 | -0.06475 | 0.00000 | 0.00000 | 0.00000 |
| SUM | 0.00000 | 2.06653 | 3.11040 | -0.45259 | 0.24979 | -0.06524 |

Condition LC3=1.2DL+Wi+Di

| | | | | | | |
|----------|----------|----------|----------|----------|----------|----------|
| 8 | 0.09653 | 0.25509 | 0.00230 | -0.13621 | 0.09072 | 0.00242 |
| 9 | -0.01505 | 0.95784 | 1.00013 | -0.03883 | -0.00397 | 0.00342 |
| 11 | -0.06382 | 0.20044 | -0.06960 | -0.06400 | 0.01774 | 0.03005 |
| 12 | -0.00139 | 0.28410 | 0.30060 | 0.00155 | -0.04476 | 0.04069 |
| 13 | -0.02496 | 0.28445 | 0.04222 | 0.00000 | 0.00000 | 0.00000 |
| 14 | 0.32408 | 0.00000 | -0.07531 | 0.00000 | 0.00000 | 0.00000 |
| 15 | -0.02750 | 0.00000 | 0.00848 | 0.00000 | 0.00000 | 0.00000 |
| 16 | -0.06088 | 0.38579 | -0.02083 | 0.00000 | 0.00000 | 0.00000 |
| 17 | -0.80864 | 0.00000 | -0.19305 | 0.00000 | 0.00000 | 0.00000 |
| 18 | 0.02325 | 0.00000 | 0.00723 | 0.00000 | 0.00000 | 0.00000 |
| 20 | 0.11415 | 0.12963 | -0.02968 | -0.04118 | 0.10125 | -0.02266 |
| 21 | 0.08847 | 0.63231 | 0.61072 | -0.04101 | 0.15846 | -0.15447 |
| 22 | 0.00983 | 0.17281 | -0.30659 | 0.00000 | 0.00000 | 0.00000 |
| 23 | 0.06769 | 0.16149 | -0.33563 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.06749 | 0.03945 | -0.01461 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.06597 | 0.03951 | -0.01444 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 149 | -0.06972 | 0.01297 | -0.05127 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 153 | -0.03995 | 0.03067 | 0.01846 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 160 | 0.12817 | -0.00257 | 0.03912 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 169 | 0.18551 | 0.01187 | -0.23485 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 173 | -0.07066 | 0.01076 | -0.30387 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 180 | 0.04962 | -0.00314 | 0.07962 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | 0.05172 | 0.03088 | -0.00104 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 188 | 0.04506 | 0.01320 | -0.05812 | 0.00000 | 0.00000 | 0.00000 |
| SUM | 0.00000 | 3.64756 | 0.40000 | -0.31969 | 0.31943 | -0.10055 |

Condition LC4=1.2DL

| | | | | | | |
|----|----------|---------|----------|----------|----------|----------|
| 8 | 0.08435 | 0.17849 | -0.11861 | -0.08861 | 0.04996 | 0.00099 |
| 9 | -0.04230 | 0.70873 | 0.76045 | -0.01707 | -0.02348 | 0.02093 |
| 11 | -0.02751 | 0.15312 | -0.09134 | -0.04860 | 0.02735 | 0.02357 |
| 12 | 0.00782 | 0.20518 | 0.21050 | -0.00293 | -0.02510 | 0.02364 |
| 13 | -0.00905 | 0.18811 | 0.03486 | 0.00000 | 0.00000 | 0.00000 |
| 14 | 0.46055 | 0.00000 | -0.09814 | 0.00000 | 0.00000 | 0.00000 |
| 15 | 0.02210 | 0.00000 | -0.00235 | 0.00000 | 0.00000 | 0.00000 |
| 16 | -0.06143 | 0.32513 | -0.01665 | 0.00000 | 0.00000 | 0.00000 |
| 17 | -1.14173 | 0.00000 | -0.26136 | 0.00000 | 0.00000 | 0.00000 |
| 18 | 0.01432 | 0.00000 | 0.00548 | 0.00000 | 0.00000 | 0.00000 |
| 20 | 0.09046 | 0.10192 | -0.01901 | -0.03468 | 0.07167 | -0.01785 |
| 21 | 0.07501 | 0.49471 | 0.47799 | -0.03231 | 0.12787 | -0.12448 |
| 22 | 0.04135 | 0.13069 | -0.22342 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|----------|----------|----------|----------|---------|---------|---------|
| 23 | 0.07818 | 0.12047 | -0.26715 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.04754 | 0.03062 | -0.01661 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.04863 | 0.03068 | -0.01432 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 149 | -0.05153 | 0.01310 | -0.04167 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 153 | -0.03027 | 0.02325 | 0.01821 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 160 | 0.11155 | -0.00125 | 0.02067 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 169 | 0.19218 | 0.00883 | -0.15763 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 173 | 0.02199 | 0.00847 | -0.17892 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 180 | 0.08092 | -0.00166 | 0.03319 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | 0.05223 | 0.02343 | -0.01131 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 188 | 0.02972 | 0.01335 | -0.04284 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|-----|---------|---------|---------|----------|---------|----------|
| SUM | 0.00000 | 2.75537 | 0.00000 | -0.22420 | 0.22827 | -0.07320 |
|-----|---------|---------|---------|----------|---------|----------|

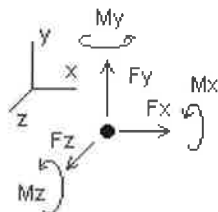
Condition **LC5=0.9DL**

| | | | | | | |
|----------|----------|----------|----------|----------|----------|----------|
| 8 | 0.06326 | 0.13387 | -0.08896 | -0.06646 | 0.03747 | 0.00074 |
| 9 | -0.03172 | 0.53155 | 0.57034 | -0.01281 | -0.01761 | 0.01570 |
| 11 | -0.02063 | 0.11484 | -0.06851 | -0.03645 | 0.02051 | 0.01768 |
| 12 | 0.00586 | 0.15388 | 0.15787 | -0.00220 | -0.01882 | 0.01773 |
| 13 | -0.00679 | 0.14108 | 0.02614 | 0.00000 | 0.00000 | 0.00000 |
| 14 | 0.34542 | 0.00000 | -0.07360 | 0.00000 | 0.00000 | 0.00000 |
| 15 | 0.01658 | 0.00000 | -0.00176 | 0.00000 | 0.00000 | 0.00000 |
| 16 | -0.04607 | 0.24385 | -0.01249 | 0.00000 | 0.00000 | 0.00000 |
| 17 | -0.85630 | 0.00000 | -0.19602 | 0.00000 | 0.00000 | 0.00000 |
| 18 | 0.01074 | 0.00000 | 0.00411 | 0.00000 | 0.00000 | 0.00000 |
| 20 | 0.06784 | 0.07644 | -0.01425 | -0.02601 | 0.05375 | -0.01339 |
| 21 | 0.05626 | 0.37103 | 0.35849 | -0.02423 | 0.09590 | -0.09336 |
| 22 | 0.03101 | 0.09802 | -0.16757 | 0.00000 | 0.00000 | 0.00000 |
| 23 | 0.05863 | 0.09035 | -0.20036 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.03565 | 0.02297 | -0.01246 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.03647 | 0.02301 | -0.01074 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 149 | -0.03865 | 0.00983 | -0.03126 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 153 | -0.02271 | 0.01744 | 0.01366 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 160 | 0.08366 | -0.00094 | 0.01550 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 169 | 0.14413 | 0.00663 | -0.11822 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 173 | 0.01649 | 0.00635 | -0.13419 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 180 | 0.06069 | -0.00125 | 0.02489 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | 0.03917 | 0.01757 | -0.00848 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 188 | 0.02229 | 0.01001 | -0.03213 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|-----|---------|---------|---------|----------|---------|----------|
| SUM | 0.00000 | 2.06653 | 0.00000 | -0.16815 | 0.17121 | -0.05490 |
|-----|---------|---------|---------|----------|---------|----------|

Envelope for nodal reactions

Note.- I_c is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for

LC1=1.2DL+1.6Wo

LC2=0.9DL+1.6Wo

LC3=1.2DL+Wi+Di

LC4=1.2DL

LC5=0.9DL

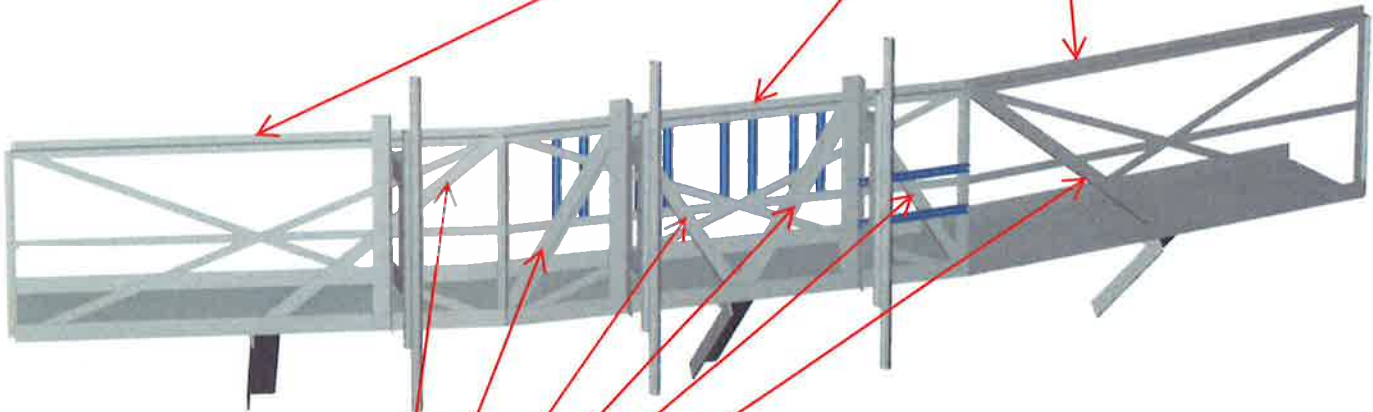
| Node | | Forces | | | | | | Moments | | | | | |
|------|-----|-------------|-----|-------------|-----|-------------|-----|----------------|-----|----------------|-----|----------------|-----|
| | | Fx [Kip] | lc | Fy [Kip] | lc | Fz [Kip] | lc | Mx [Kip*ft] | lc | My [Kip*ft] | lc | Mz [Kip*ft] | lc |
| 8 | Max | 0.097 | LC3 | 0.373 | LC1 | 1.140 | LC2 | -0.06646 | LC5 | 0.21413 | LC1 | 0.00242 | LC3 |
| | Min | -0.058 | LC2 | 0.134 | LC5 | -0.119 | LC4 | -0.24156 | LC1 | 0.03747 | LC5 | -0.00782 | LC1 |
| 9 | Max | 0.420 | LC2 | 0.958 | LC3 | 1.000 | LC3 | -0.01281 | LC5 | 0.28311 | LC2 | 0.02093 | LC4 |
| | Min | -0.042 | LC4 | 0.427 | LC2 | 0.182 | LC2 | -0.16813 | LC2 | -0.02348 | LC4 | -0.25354 | LC2 |
| 11 | Max | -0.021 | LC5 | 0.200 | LC3 | 0.080 | LC2 | -0.03645 | LC5 | 0.02735 | LC4 | 0.03944 | LC1 |
| | Min | -0.126 | LC1 | 0.115 | LC5 | -0.091 | LC4 | -0.07381 | LC1 | -0.05598 | LC2 | 0.01768 | LC5 |
| 12 | Max | 0.008 | LC4 | 0.296 | LC1 | 0.359 | LC1 | 0.02945 | LC2 | -0.01882 | LC5 | 0.08206 | LC1 |
| | Min | -0.066 | LC2 | 0.154 | LC5 | 0.158 | LC5 | -0.00293 | LC4 | -0.09624 | LC1 | 0.01773 | LC5 |
| 13 | Max | 0.005 | LC2 | 0.417 | LC1 | 0.042 | LC3 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.025 | LC3 | 0.141 | LC5 | 0.025 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 14 | Max | 0.461 | LC4 | 0.000 | LC1 | 0.466 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -2.447 | LC2 | 0.000 | LC1 | -0.098 | LC4 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 15 | Max | 0.022 | LC4 | 0.000 | LC1 | 0.008 | LC3 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.028 | LC3 | 0.000 | LC1 | -0.002 | LC4 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 16 | Max | 0.107 | LC2 | 0.386 | LC3 | 0.095 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.061 | LC4 | 0.097 | LC2 | -0.021 | LC3 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 17 | Max | 4.683 | LC2 | 0.000 | LC1 | 1.019 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -1.142 | LC4 | 0.000 | LC1 | -0.261 | LC4 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 18 | Max | 0.023 | LC3 | 0.000 | LC1 | 0.007 | LC3 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.226 | LC2 | 0.000 | LC1 | -0.050 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 20 | Max | 0.114 | LC3 | 0.156 | LC1 | -0.014 | LC5 | -0.02601 | LC5 | 0.10125 | LC3 | -0.01339 | LC5 |
| | Min | 0.068 | LC5 | 0.076 | LC5 | -0.212 | LC2 | -0.05071 | LC1 | 0.04258 | LC2 | -0.04068 | LC1 |
| 21 | Max | 0.088 | LC3 | 0.632 | LC3 | 0.611 | LC3 | 0.00380 | LC2 | 0.15846 | LC3 | 0.12173 | LC2 |
| | Min | -0.169 | LC2 | -0.097 | LC2 | -0.107 | LC2 | -0.04101 | LC3 | -0.13186 | LC2 | -0.15447 | LC3 |
| 22 | Max | 0.041 | LC4 | 0.251 | LC1 | -0.026 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.173 | LC2 | 0.098 | LC5 | -0.307 | LC3 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 23 | Max | 0.078 | LC4 | 0.330 | LC1 | 0.111 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.300 | LC2 | 0.090 | LC5 | -0.336 | LC3 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 24 | Max | -0.036 | LC5 | 0.039 | LC3 | 0.006 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.067 | LC3 | 0.023 | LC5 | -0.017 | LC4 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 25 | Max | 0.071 | LC1 | 0.040 | LC3 | 0.025 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | 0.036 | LC5 | 0.023 | LC2 | -0.014 | LC3 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |



HUDSON
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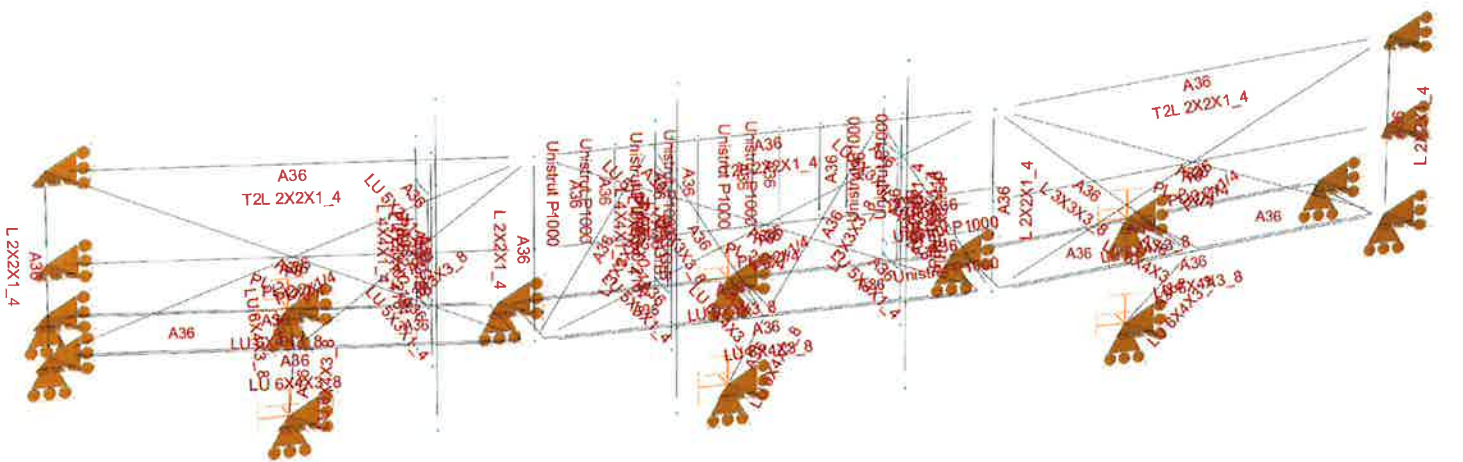
**Antenna Mount Calculations
(Proposed Conditions)**

REINFORCE THE EXISTING L2x2x1/4 ANGLE TOP HANDRAIL WITH NEW L2x2x1/4 ANGLES (TYP OF 3 PER SECTOR, TOTAL OF 9).



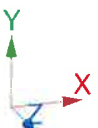
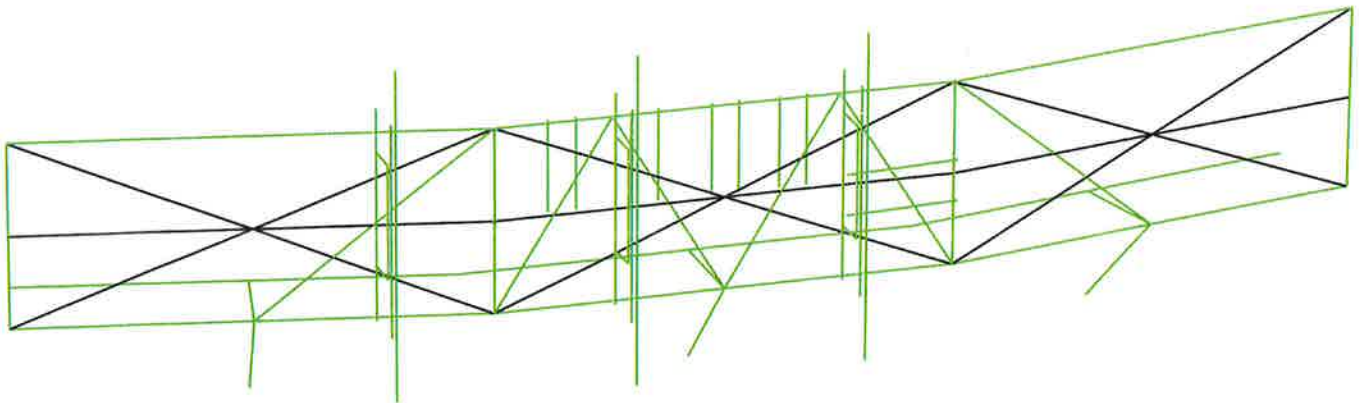
INSTALL NEW L3x3x3/8 ANGLE BRACES, SECURE TO THE EXISTING HANDRAIL (TYP. OF 6 PER SECTOR, TOTAL OF 18).

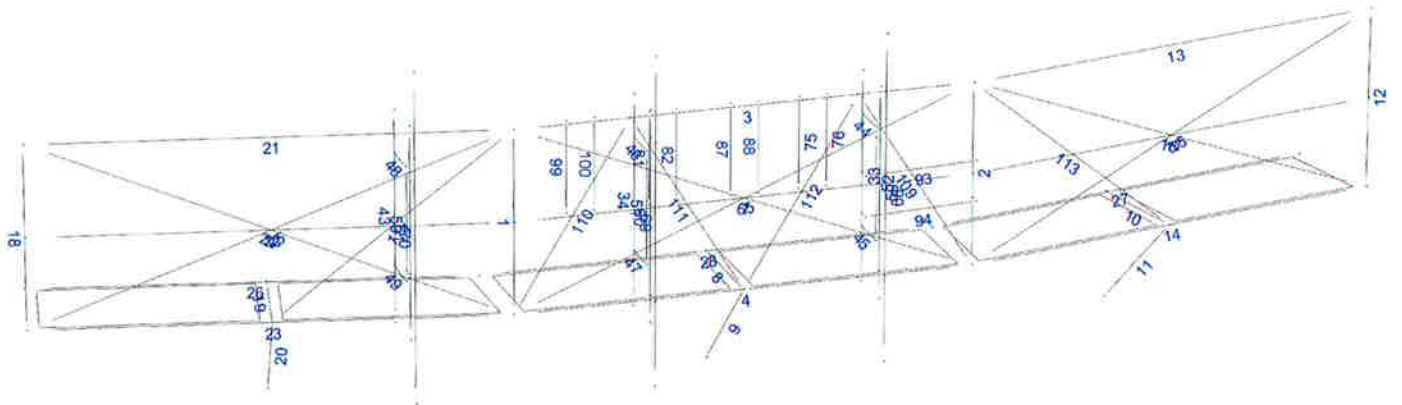




Design status

- Not designed
- Error on design
- Design O.K.
- With warnings





Current Date: 4/18/2018 9:31 AM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT2177\CT2177 (LTE 3C-4C) (MOD).et

Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design :

- LC1=1.2DL+1.6Wo
- LC2=0.9DL+1.6Wo
- LC3=1.2DL+Wi+Di
- LC4=1.2DL
- LC5=0.9DL

| Description | Section | Member | Ctrl Eq. | Ratio | Status | Reference |
|-------------|------------------|----------------|----------------|-------------|-----------|-----------|
| | <i>L 2X2X1_4</i> | 1 | LC1 at 0.00% | 0.10 | OK | Sec. F1 |
| | | | LC2 at 0.00% | 0.10 | OK | |
| | | | LC3 at 100.00% | 0.04 | OK | |
| | | | LC4 at 100.00% | 0.02 | OK | |
| | | | LC5 at 100.00% | 0.02 | OK | |
| | | 2 | LC1 at 100.00% | 0.25 | OK | Sec. F1 |
| | | | LC2 at 100.00% | 0.26 | OK | |
| | | | LC3 at 100.00% | 0.02 | OK | |
| | | | LC4 at 100.00% | 0.03 | OK | |
| | | | LC5 at 100.00% | 0.02 | OK | |
| | | 12 | LC1 at 100.00% | 0.05 | OK | Eq. H2-1 |
| | | | LC2 at 100.00% | 0.03 | OK | |
| | | | LC3 at 100.00% | 0.07 | OK | |
| | | | LC4 at 100.00% | 0.05 | OK | |
| | | | LC5 at 100.00% | 0.04 | OK | |
| | | 18 | LC1 at 100.00% | 0.04 | OK | Eq. H2-1 |
| | | | LC2 at 100.00% | 0.03 | OK | |
| | | | LC3 at 100.00% | 0.06 | OK | |
| | | | LC4 at 100.00% | 0.04 | OK | |
| | | | LC5 at 100.00% | 0.03 | OK | |
| | <i>L 3X3X3_8</i> | 109 | LC1 at 0.00% | 0.26 | OK | Eq. H2-1 |
| | | | LC2 at 0.00% | 0.27 | OK | |
| | | | LC3 at 0.00% | 0.02 | OK | |
| | | | LC4 at 0.00% | 0.02 | OK | |
| | | | LC5 at 0.00% | 0.01 | OK | |
| | | 110 | LC1 at 0.00% | 0.21 | OK | Eq. H2-1 |
| | | | LC2 at 0.00% | 0.21 | OK | |
| | | | LC3 at 0.00% | 0.03 | OK | |
| | | | LC4 at 100.00% | 0.01 | OK | |
| | | | LC5 at 100.00% | 0.01 | OK | |
| | 111 | LC1 at 100.00% | 0.60 | OK | Sec. F1 | |
| | | LC2 at 100.00% | 0.60 | OK | | |
| | | LC3 at 100.00% | 0.06 | OK | | |
| | | LC4 at 100.00% | 0.04 | OK | | |
| | | LC5 at 100.00% | 0.03 | OK | | |
| | 112 | LC1 at 0.00% | 0.52 | OK | Sec. F1 | |
| | | LC2 at 0.00% | 0.52 | OK | | |

| | | | | | |
|-------------------|----------------|----------------|-------------|-----------|----------|
| | LC3 at 0.00% | 0.06 | OK | | |
| | LC4 at 0.00% | 0.04 | OK | | |
| | LC5 at 0.00% | 0.03 | OK | | |
| 113 | LC1 at 0.00% | 0.20 | OK | | |
| | LC2 at 0.00% | 0.20 | OK | Eq. H2-1 | |
| | LC3 at 0.00% | 0.02 | OK | | |
| | LC4 at 0.00% | 0.02 | OK | | |
| | LC5 at 0.00% | 0.01 | OK | | |
| 114 | LC1 at 66.67% | 0.08 | OK | Eq. H2-1 | |
| | LC2 at 91.67% | 0.07 | OK | | |
| | LC3 at 0.00% | 0.05 | OK | | |
| | LC4 at 100.00% | 0.04 | OK | | |
| | LC5 at 100.00% | 0.03 | OK | | |
| L 4X4X1_4 | 33 | LC1 at 68.75% | 0.27 | OK | Eq. H3-8 |
| | | LC2 at 13.54% | 0.27 | OK | Eq. H3-8 |
| | | LC3 at 68.75% | 0.05 | OK | |
| | | LC4 at 75.00% | 0.02 | OK | |
| | | LC5 at 75.00% | 0.02 | OK | |
| | 34 | LC1 at 14.06% | 0.45 | OK | |
| | | LC2 at 14.06% | 0.45 | OK | Eq. H3-8 |
| | | LC3 at 14.06% | 0.05 | OK | |
| | | LC4 at 75.00% | 0.02 | OK | |
| | | LC5 at 75.00% | 0.01 | OK | |
| | 43 | LC1 at 14.06% | 0.40 | OK | |
| | | LC2 at 14.06% | 0.40 | OK | Eq. H3-8 |
| | | LC3 at 14.06% | 0.05 | OK | |
| | | LC4 at 100.00% | 0.02 | OK | |
| | | LC5 at 100.00% | 0.02 | OK | |
| | 50 | LC1 at 91.67% | 0.12 | OK | Eq. H3-8 |
| | | LC2 at 91.67% | 0.11 | OK | |
| | | LC3 at 91.67% | 0.03 | OK | |
| | | LC4 at 0.00% | 0.01 | OK | |
| | | LC5 at 0.00% | 0.01 | OK | |
| | 51 | LC1 at 0.00% | 0.10 | OK | Eq. H3-8 |
| | | LC2 at 0.00% | 0.10 | OK | |
| | | LC3 at 91.67% | 0.03 | OK | |
| | | LC4 at 91.67% | 0.01 | OK | |
| | | LC5 at 0.00% | 0.01 | OK | |
| | 52 | LC1 at 91.67% | 0.07 | OK | Eq. H3-8 |
| | | LC2 at 91.67% | 0.07 | OK | |
| | | LC3 at 91.67% | 0.02 | OK | |
| | | LC4 at 0.00% | 0.01 | OK | |
| | | LC5 at 91.67% | 0.01 | OK | |
| LU 5X3X1_4 | 44 | LC1 at 100.00% | 0.05 | OK | |
| | | LC2 at 100.00% | 0.06 | OK | Eq. H2-1 |
| | | LC3 at 0.00% | 0.01 | OK | |
| | | LC4 at 0.00% | 0.01 | OK | |
| | | LC5 at 0.00% | 0.01 | OK | |
| | 45 | LC1 at 100.00% | 0.09 | OK | Eq. H2-1 |
| | | LC2 at 100.00% | 0.08 | OK | |
| | | LC3 at 100.00% | 0.05 | OK | |
| | | LC4 at 100.00% | 0.03 | OK | |
| | | LC5 at 100.00% | 0.02 | OK | |

LU 6X4X3_8

| | | | | |
|----|----------------|-------------|----|----------------------|
| 46 | LC1 at 100.00% | 0.08 | OK | Eq. H2-1 |
| | LC2 at 100.00% | 0.08 | OK | |
| | LC3 at 0.00% | 0.02 | OK | |
| | LC4 at 0.00% | 0.01 | OK | |
| | LC5 at 0.00% | 0.01 | OK | |
| 47 | LC1 at 100.00% | 0.12 | OK | Eq. H2-1 |
| | LC2 at 100.00% | 0.11 | OK | |
| | LC3 at 100.00% | 0.05 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| 48 | LC1 at 100.00% | 0.07 | OK | Eq. H2-1 Eq. H2-1 |
| | LC2 at 100.00% | 0.07 | OK | |
| | LC3 at 0.00% | 0.03 | OK | |
| | LC4 at 0.00% | 0.03 | OK | |
| | LC5 at 0.00% | 0.02 | OK | |
| 49 | LC1 at 100.00% | 0.14 | OK | Eq. H2-1 |
| | LC2 at 100.00% | 0.14 | OK | |
| | LC3 at 100.00% | 0.06 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| 4 | LC1 at 62.50% | 0.08 | OK | Eq. H3-8 |
| | LC2 at 62.50% | 0.08 | OK | |
| | LC3 at 50.00% | 0.04 | OK | |
| | LC4 at 49.22% | 0.03 | OK | |
| | LC5 at 49.22% | 0.02 | OK | |
| 8 | LC1 at 0.00% | 0.27 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.26 | OK | |
| | LC3 at 100.00% | 0.07 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| 9 | LC1 at 0.00% | 0.22 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.22 | OK | |
| | LC3 at 100.00% | 0.06 | OK | |
| | LC4 at 100.00% | 0.04 | OK | |
| | LC5 at 100.00% | 0.03 | OK | |
| 10 | LC1 at 98.44% | 0.03 | OK | Eq. H3-8 |
| | LC2 at 98.44% | 0.02 | OK | |
| | LC3 at 98.44% | 0.03 | OK | |
| | LC4 at 98.44% | 0.02 | OK | |
| | LC5 at 98.44% | 0.02 | OK | |
| 11 | LC1 at 100.00% | 0.04 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.04 | OK | |
| | LC3 at 100.00% | 0.02 | OK | |
| | LC4 at 100.00% | 0.01 | OK | |
| | LC5 at 100.00% | 0.01 | OK | |
| 14 | LC1 at 0.00% | 0.08 | OK | Eq. H2-1 Eq. H3-8 |
| | LC2 at 0.00% | 0.08 | OK | |
| | LC3 at 51.56% | 0.03 | OK | |
| | LC4 at 51.56% | 0.02 | OK | |
| | LC5 at 51.56% | 0.02 | OK | |
| 19 | LC1 at 98.44% | 0.04 | OK | Eq. H3-8 |
| | LC2 at 98.44% | 0.03 | OK | |
| | LC3 at 98.44% | 0.02 | OK | |
| | LC4 at 98.44% | 0.02 | OK | |

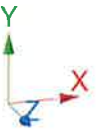
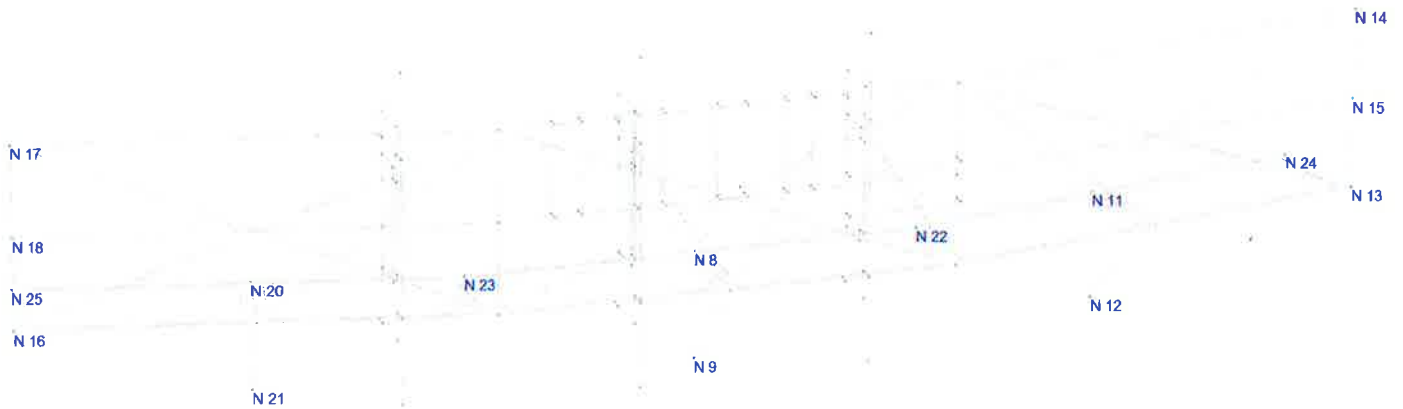
| | | | | | |
|-----------|---------------------|----------------|-------------|-----------|-----------|
| | | LC5 at 98.44% | 0.01 | OK | |
| 20 | | LC1 at 0.00% | 0.03 | OK | |
| | | LC2 at 0.00% | 0.03 | OK | |
| | | LC3 at 0.00% | 0.05 | OK | Eq. H2-1 |
| | | LC4 at 0.00% | 0.04 | OK | |
| | | LC5 at 0.00% | 0.03 | OK | |
| 23 | | LC1 at 50.00% | 0.09 | OK | Eq. H3-8 |
| | | LC2 at 50.00% | 0.07 | OK | |
| | | LC3 at 50.00% | 0.09 | OK | |
| | | LC4 at 50.00% | 0.06 | OK | |
| | | LC5 at 50.00% | 0.05 | OK | |
| 26 | | LC1 at 0.00% | 0.03 | OK | Eq. H2-1 |
| | | LC2 at 0.00% | 0.02 | OK | |
| | | LC3 at 48.44% | 0.02 | OK | Eq. H3-8 |
| | | LC4 at 48.44% | 0.02 | OK | |
| | | LC5 at 48.44% | 0.01 | OK | |
| 27 | | LC1 at 100.00% | 0.02 | OK | Eq. H2-1 |
| | | LC2 at 100.00% | 0.02 | OK | |
| | | LC3 at 51.56% | 0.02 | OK | Eq. H3-8 |
| | | LC4 at 51.56% | 0.02 | OK | |
| | | LC5 at 51.56% | 0.01 | OK | |
| 28 | | LC1 at 100.00% | 0.03 | OK | Eq. H3-8 |
| | | LC2 at 100.00% | 0.03 | OK | |
| | | LC3 at 100.00% | 0.02 | OK | |
| | | LC4 at 100.00% | 0.02 | OK | |
| | | LC5 at 100.00% | 0.01 | OK | |
| | PIPE 2x0.154 | | | | |
| 68 | | LC1 at 25.00% | 0.13 | OK | Eq. H1-1b |
| | | LC2 at 25.00% | 0.13 | OK | |
| | | LC3 at 25.00% | 0.02 | OK | |
| | | LC4 at 72.92% | 0.00 | OK | |
| | | LC5 at 72.92% | 0.00 | OK | |
| 69 | | LC1 at 25.00% | 0.14 | OK | Eq. H1-1b |
| | | LC2 at 25.00% | 0.14 | OK | |
| | | LC3 at 25.00% | 0.02 | OK | |
| | | LC4 at 27.08% | 0.00 | OK | |
| | | LC5 at 27.08% | 0.00 | OK | |
| 70 | | LC1 at 25.00% | 0.13 | OK | Eq. H1-1b |
| | | LC2 at 25.00% | 0.13 | OK | |
| | | LC3 at 25.00% | 0.02 | OK | |
| | | LC4 at 27.08% | 0.01 | OK | |
| | | LC5 at 27.08% | 0.00 | OK | |
| | PIPE 3x0.216 | | | | |
| 59 | | LC1 at 70.00% | 0.05 | OK | Eq. H1-1b |
| | | LC2 at 70.00% | 0.05 | OK | |
| | | LC3 at 68.75% | 0.01 | OK | |
| | | LC4 at 68.75% | 0.00 | OK | |
| | | LC5 at 68.75% | 0.00 | OK | |
| 60 | | LC1 at 70.00% | 0.05 | OK | Eq. H1-1b |
| | | LC2 at 70.00% | 0.05 | OK | |
| | | LC3 at 68.75% | 0.01 | OK | |
| | | LC4 at 68.75% | 0.00 | OK | |
| | | LC5 at 68.75% | 0.00 | OK | |
| 61 | | LC1 at 70.00% | 0.05 | OK | Eq. H1-1b |
| | | LC2 at 70.00% | 0.05 | OK | |

| | | | | | |
|--------------------|-----------|----------------|-------------|----------------------|-----------|
| | | LC3 at 68.75% | 0.01 | OK | |
| | | LC4 at 68.75% | 0.01 | OK | |
| | | LC5 at 68.75% | 0.00 | OK | |
| PL 2x1/4 | 5 | LC1 at 40.00% | 0.24 | With warnings | |
| | | LC2 at 40.00% | 0.25 | With warnings | Eq. H1-1b |
| | | LC3 at 80.00% | 0.03 | With warnings | Sec. E1 |
| | | LC4 at 40.00% | 0.03 | With warnings | |
| | | LC5 at 40.00% | 0.02 | With warnings | |
| | 6 | LC1 at 50.00% | 0.24 | With warnings | |
| | | LC2 at 50.00% | 0.25 | With warnings | Eq. H1-1b |
| | | LC3 at 0.00% | 0.03 | With warnings | |
| | | LC4 at 50.00% | 0.03 | With warnings | |
| | | LC5 at 50.00% | 0.02 | With warnings | |
| | 7 | LC1 at 62.50% | 0.54 | With warnings | Eq. H3-6 |
| | | LC2 at 62.50% | 0.54 | With warnings | |
| | | LC3 at 62.50% | 0.13 | With warnings | |
| | | LC4 at 62.50% | 0.07 | With warnings | |
| | | LC5 at 62.50% | 0.05 | With warnings | |
| | 15 | LC1 at 100.00% | 0.03 | With warnings | |
| | | LC2 at 100.00% | 0.03 | With warnings | Eq. H1-1b |
| | | LC3 at 16.67% | 0.02 | With warnings | Eq. H1-1b |
| | | LC4 at 47.92% | 0.01 | With warnings | |
| | | LC5 at 47.92% | 0.01 | With warnings | |
| | 16 | LC1 at 100.00% | 0.05 | With warnings | |
| | | LC2 at 100.00% | 0.04 | With warnings | |
| | | LC3 at 100.00% | 0.08 | With warnings | Sec. E1 |
| | | LC4 at 100.00% | 0.05 | With warnings | |
| | | LC5 at 100.00% | 0.04 | With warnings | |
| | 17 | LC1 at 0.00% | 0.02 | With warnings | Eq. H1-1b |
| | | LC2 at 75.00% | 0.02 | With warnings | Eq. H1-1b |
| | | LC3 at 0.00% | 0.02 | With warnings | |
| | | LC4 at 0.00% | 0.01 | With warnings | |
| | | LC5 at 0.00% | 0.01 | With warnings | |
| | 22 | LC1 at 100.00% | 0.04 | With warnings | Eq. H1-1b |
| | | LC2 at 100.00% | 0.03 | With warnings | |
| | | LC3 at 100.00% | 0.02 | With warnings | |
| | | LC4 at 100.00% | 0.02 | With warnings | |
| | | LC5 at 100.00% | 0.01 | With warnings | |
| | 24 | LC1 at 100.00% | 0.04 | With warnings | Eq. H1-1b |
| | | LC2 at 100.00% | 0.04 | With warnings | |
| | | LC3 at 16.67% | 0.02 | With warnings | Eq. H1-1b |
| | | LC4 at 14.58% | 0.02 | With warnings | |
| | | LC5 at 14.58% | 0.01 | With warnings | |
| | 25 | LC1 at 100.00% | 0.05 | With warnings | |
| | | LC2 at 100.00% | 0.04 | With warnings | Eq. H1-2 |
| | | LC3 at 100.00% | 0.08 | With warnings | Sec. E1 |
| | | LC4 at 100.00% | 0.05 | With warnings | |
| | | LC5 at 100.00% | 0.04 | With warnings | |
| T2L 2X2X1_4 | 3 | LC1 at 24.43% | 0.88 | OK | |
| | | LC2 at 24.43% | 0.89 | OK | Eq. H2-1 |
| | | LC3 at 48.30% | 0.05 | OK | |
| | | LC4 at 0.00% | 0.08 | OK | |
| | | LC5 at 0.00% | 0.06 | OK | |

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| | | | | |
|-----------|----------------|-------------|-----------|-----------|
| 13 | LC1 at 0.00% | 0.26 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.26 | OK | |
| | LC3 at 0.00% | 0.04 | OK | |
| | LC4 at 0.00% | 0.04 | OK | |
| | LC5 at 0.00% | 0.03 | OK | |
| <hr/> | | | | |
| 21 | LC1 at 0.00% | 0.59 | OK | Eq. H2-1 |
| | LC2 at 0.00% | 0.61 | OK | |
| | LC3 at 0.00% | 0.07 | OK | |
| | LC4 at 0.00% | 0.11 | OK | |
| | LC5 at 0.00% | 0.08 | OK | |
| <hr/> | | | | |
| 75 | LC1 at 50.00% | 0.21 | OK | Sec. C5.2 |
| | LC2 at 50.00% | 0.20 | OK | |
| | LC3 at 50.00% | 0.05 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| <hr/> | | | | |
| 76 | LC1 at 0.00% | 0.20 | OK | Sec. C5.1 |
| | LC2 at 0.00% | 0.20 | OK | |
| | LC3 at 0.00% | 0.03 | OK | |
| | LC4 at 100.00% | 0.02 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| <hr/> | | | | |
| 81 | LC1 at 0.00% | 0.24 | OK | Sec. C5.1 |
| | LC2 at 0.00% | 0.24 | OK | |
| | LC3 at 0.00% | 0.04 | OK | |
| | LC4 at 100.00% | 0.02 | OK | |
| | LC5 at 100.00% | 0.01 | OK | |
| <hr/> | | | | |
| 82 | LC1 at 50.00% | 0.20 | OK | Sec. C5.2 |
| | LC2 at 50.00% | 0.20 | OK | |
| | LC3 at 50.00% | 0.05 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| <hr/> | | | | |
| 87 | LC1 at 50.00% | 0.24 | OK | Sec. C5.2 |
| | LC2 at 50.00% | 0.23 | OK | |
| | LC3 at 50.00% | 0.05 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| <hr/> | | | | |
| 88 | LC1 at 50.00% | 0.24 | OK | Sec. C5.2 |
| | LC2 at 50.00% | 0.23 | OK | |
| | LC3 at 50.00% | 0.05 | OK | |
| | LC4 at 100.00% | 0.03 | OK | |
| | LC5 at 100.00% | 0.02 | OK | |
| <hr/> | | | | |
| 93 | LC1 at 100.00% | 0.12 | OK | Sec. C5.2 |
| | LC2 at 100.00% | 0.12 | OK | |
| | LC3 at 0.00% | 0.02 | OK | |
| | LC4 at 50.00% | 0.01 | OK | |
| | LC5 at 50.00% | 0.01 | OK | |
| <hr/> | | | | |
| 94 | LC1 at 0.00% | 0.12 | OK | Sec. C5.2 |
| | LC2 at 0.00% | 0.12 | OK | |
| | LC3 at 0.00% | 0.03 | OK | |
| | LC4 at 50.00% | 0.01 | OK | |
| | LC5 at 50.00% | 0.01 | OK | |
| <hr/> | | | | |
| 99 | LC1 at 0.00% | 0.09 | OK | Sec. C5.1 |
| | LC2 at 0.00% | 0.08 | OK | |
| | LC3 at 0.00% | 0.03 | OK | |
| | LC4 at 0.00% | 0.01 | OK | |

| | | | | |
|------------|--------------|-------------|-----------|-----------|
| | LC5 at 0.00% | 0.01 | OK | |
| 100 | LC1 at 0.00% | 0.10 | OK | Sec. C5.1 |
| | LC2 at 0.00% | 0.09 | OK | |
| | LC3 at 0.00% | 0.03 | OK | |
| | LC4 at 0.00% | 0.01 | OK | |
| | LC5 at 0.00% | 0.01 | OK | |



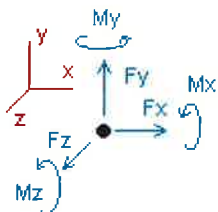
Current Date: 4/18/2018 9:31 AM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT2177\CT2177 (LTE 3C-4C) (MOD).et

Analysis result

Reactions



Direction of positive forces and moments

| Node | Forces [Kip] | | | Moments [Kip*ft] | | |
|----------------------------------|--------------|----------|----------|------------------|----------|----------|
| | FX | FY | FZ | MX | MY | MZ |
| Condition LC1=1.2DL+1.6Wo | | | | | | |
| 8 | 0.00034 | 0.80832 | 1.37151 | -0.48107 | 0.29478 | 0.02032 |
| 9 | 0.27859 | -0.36746 | -0.97196 | -0.33271 | 0.17197 | -0.15465 |
| 11 | -0.38628 | 0.16622 | -0.60276 | -0.06280 | -0.00809 | 0.02713 |
| 12 | 0.21766 | 1.08105 | 1.16931 | -0.00471 | -0.02488 | 0.02385 |
| 13 | -0.31486 | 0.12447 | 0.08972 | 0.00000 | 0.00000 | 0.00000 |
| 14 | -1.22270 | 0.00000 | 0.24964 | 0.00000 | 0.00000 | 0.00000 |
| 15 | -0.01215 | 0.00000 | 0.00621 | 0.00000 | 0.00000 | 0.00000 |
| 16 | 0.09086 | 0.09686 | 0.05387 | 0.00000 | 0.00000 | 0.00000 |
| 17 | 3.10735 | 0.00000 | 0.69992 | 0.00000 | 0.00000 | 0.00000 |
| 18 | 0.01548 | 0.00000 | 0.00489 | 0.00000 | 0.00000 | 0.00000 |
| 20 | 0.16516 | 0.18002 | -0.18271 | -0.08006 | 0.06270 | -0.02700 |
| 21 | -0.03735 | 0.54971 | 0.53027 | -0.03852 | 0.05962 | -0.06341 |
| 22 | -0.54819 | 0.16719 | -0.23876 | 0.00000 | 0.00000 | 0.00000 |
| 23 | -0.02522 | 0.17998 | -0.10065 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.10216 | 0.03065 | 0.06398 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.06583 | 0.03061 | 0.01067 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 163 | -0.00025 | 0.01372 | -0.02734 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 167 | -0.03247 | 0.02334 | 0.00667 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 174 | -0.08177 | -0.01184 | -0.11635 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 183 | 0.03974 | -0.01103 | 0.62986 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | -0.72365 | -0.00587 | 0.54374 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 194 | -0.33929 | -0.00983 | -0.18797 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 201 | -0.03781 | 0.02370 | 0.03324 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 202 | -0.11687 | 0.01329 | 0.07538 | 0.00000 | 0.00000 | 0.00000 |
| SUM | 0.00000 | 3.08310 | 3.11040 | -0.99988 | 0.55609 | -0.17375 |
| Condition LC2=0.9DL+1.6Wo | | | | | | |
| 8 | -0.01627 | 0.76891 | 1.57682 | -0.46442 | 0.28381 | 0.01991 |
| 9 | 0.28231 | -0.65606 | -1.28694 | -0.32758 | 0.17179 | -0.15446 |
| 11 | -0.38150 | 0.12939 | -0.55291 | -0.05215 | -0.01796 | 0.02150 |
| 12 | 0.20434 | 1.01810 | 1.10987 | -0.00028 | -0.02535 | 0.02331 |
| 13 | -0.30062 | 0.09459 | 0.07747 | 0.00000 | 0.00000 | 0.00000 |
| 14 | -1.28956 | 0.00000 | 0.26422 | 0.00000 | 0.00000 | 0.00000 |
| 15 | -0.00855 | 0.00000 | 0.00473 | 0.00000 | 0.00000 | 0.00000 |
| 16 | 0.07245 | 0.07215 | 0.04601 | 0.00000 | 0.00000 | 0.00000 |
| 17 | 3.27486 | 0.00000 | 0.73922 | 0.00000 | 0.00000 | 0.00000 |
| 18 | 0.01200 | 0.00000 | 0.00350 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|----------|----------|----------|----------|----------|---------|----------|
| 20 | 0.13391 | 0.14741 | -0.09306 | -0.06910 | 0.05228 | -0.02198 |
| 21 | -0.01955 | 0.39358 | 0.37100 | -0.03263 | 0.04589 | -0.04950 |
| 22 | -0.55628 | 0.13967 | -0.22459 | 0.00000 | 0.00000 | 0.00000 |
| 23 | -0.03621 | 0.15322 | -0.08552 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.08934 | 0.02300 | 0.06642 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.05077 | 0.02297 | 0.00930 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 163 | -0.00050 | 0.01031 | -0.02666 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 167 | -0.01848 | 0.01753 | 0.01443 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 174 | -0.10760 | -0.01269 | -0.08371 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 183 | 0.05146 | -0.01591 | 0.66401 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | -0.74120 | -0.01089 | 0.58232 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 194 | -0.34327 | -0.01075 | -0.18681 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 201 | -0.05355 | 0.01785 | 0.03943 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 202 | -0.11965 | 0.00996 | 0.08186 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|-----|---------|---------|---------|----------|---------|----------|
| SUM | 0.00000 | 2.31232 | 3.11040 | -0.94616 | 0.51046 | -0.16122 |
|-----|---------|---------|---------|----------|---------|----------|

Condition LC3=1.2DL+Wi+Di

| | | | | | | |
|----------|----------|---------|----------|----------|----------|----------|
| 8 | 0.09267 | 0.27602 | -0.77924 | -0.13353 | 0.08917 | 0.00483 |
| 9 | 0.01631 | 1.30354 | 1.35210 | -0.06478 | 0.02182 | -0.01973 |
| 11 | -0.06121 | 0.18992 | -0.29554 | -0.05361 | 0.04311 | 0.02698 |
| 12 | 0.08726 | 0.41840 | 0.41094 | -0.02152 | -0.00044 | 0.00513 |
| 13 | -0.10777 | 0.15452 | 0.06396 | 0.00000 | 0.00000 | 0.00000 |
| 14 | 0.15654 | 0.00000 | -0.03599 | 0.00000 | 0.00000 | 0.00000 |
| 15 | -0.01221 | 0.00000 | 0.00559 | 0.00000 | 0.00000 | 0.00000 |
| 16 | 0.11063 | 0.16689 | 0.04276 | 0.00000 | 0.00000 | 0.00000 |
| 17 | -0.50669 | 0.00000 | -0.12172 | 0.00000 | 0.00000 | 0.00000 |
| 18 | -0.02016 | 0.00000 | -0.00213 | 0.00000 | 0.00000 | 0.00000 |
| 20 | 0.16989 | 0.17366 | -0.41519 | -0.05797 | 0.06030 | -0.02424 |
| 21 | -0.09106 | 0.78418 | 0.79628 | -0.03122 | 0.06719 | -0.06861 |
| 22 | -0.01233 | 0.13362 | -0.08305 | 0.00000 | 0.00000 | 0.00000 |
| 23 | 0.06108 | 0.13222 | -0.05842 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.07349 | 0.03941 | -0.00251 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.08065 | 0.03938 | 0.00961 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 163 | 0.00108 | 0.01361 | -0.00198 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 167 | -0.06199 | 0.03054 | -0.03249 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 174 | 0.14903 | 0.00643 | -0.14900 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 183 | -0.04533 | 0.03034 | -0.09494 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | 0.02569 | 0.03160 | -0.12155 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 194 | -0.03698 | 0.00705 | -0.03475 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 201 | 0.07219 | 0.03075 | -0.03152 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 202 | 0.00621 | 0.01320 | -0.02122 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|-----|---------|---------|---------|----------|---------|----------|
| SUM | 0.00000 | 3.97528 | 0.40000 | -0.36263 | 0.28115 | -0.07566 |
|-----|---------|---------|---------|----------|---------|----------|

Condition LC4=1.2DL

| | | | | | | |
|----|----------|---------|----------|----------|---------|----------|
| 8 | 0.07745 | 0.15680 | -0.80426 | -0.06601 | 0.04461 | 0.00169 |
| 9 | -0.01146 | 1.12765 | 1.22819 | -0.02147 | 0.00295 | -0.00273 |
| 11 | -0.01922 | 0.14781 | -0.20644 | -0.04301 | 0.04004 | 0.02264 |
| 12 | 0.05498 | 0.26018 | 0.24692 | -0.01774 | 0.00168 | 0.00235 |
| 13 | -0.05762 | 0.11942 | 0.04921 | 0.00000 | 0.00000 | 0.00000 |
| 14 | 0.25865 | 0.00000 | -0.05649 | 0.00000 | 0.00000 | 0.00000 |
| 15 | 0.02311 | 0.00000 | -0.00236 | 0.00000 | 0.00000 | 0.00000 |
| 16 | 0.08051 | 0.13559 | 0.03477 | 0.00000 | 0.00000 | 0.00000 |
| 17 | -0.71245 | 0.00000 | -0.16650 | 0.00000 | 0.00000 | 0.00000 |
| 18 | -0.05971 | 0.00000 | -0.01076 | 0.00000 | 0.00000 | 0.00000 |
| 20 | 0.13096 | 0.13229 | -0.33930 | -0.04467 | 0.04334 | -0.02019 |
| 21 | -0.07200 | 0.60449 | 0.61603 | -0.02302 | 0.05099 | -0.05191 |
| 22 | 0.03584 | 0.11045 | -0.05689 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|----------|----------|---------|----------|---------|---------|---------|
| 23 | 0.05851 | 0.10715 | -0.04840 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.05140 | 0.03061 | -0.00949 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.06090 | 0.03059 | 0.00582 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 163 | 0.00410 | 0.01364 | -0.00165 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 167 | -0.05032 | 0.02325 | -0.02471 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 174 | 0.11341 | 0.00341 | -0.10955 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 183 | -0.03049 | 0.01954 | -0.13652 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | 0.07588 | 0.01987 | -0.14647 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 194 | 0.01687 | 0.00362 | -0.01013 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 201 | 0.06307 | 0.02339 | -0.02560 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 202 | 0.01044 | 0.01334 | -0.02542 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|-----|---------|---------|---------|----------|---------|----------|
| SUM | 0.00000 | 3.08310 | 0.00000 | -0.21590 | 0.18360 | -0.04815 |
|-----|---------|---------|---------|----------|---------|----------|

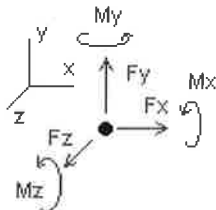
Condition **LC5=0.9DL**

| | | | | | | |
|----------|----------|---------|----------|----------|---------|----------|
| 8 | 0.05809 | 0.11760 | -0.60319 | -0.04951 | 0.03346 | 0.00127 |
| 9 | -0.00860 | 0.84574 | 0.92115 | -0.01610 | 0.00221 | -0.00205 |
| 11 | -0.01442 | 0.11086 | -0.15483 | -0.03226 | 0.03003 | 0.01698 |
| 12 | 0.04124 | 0.19513 | 0.18519 | -0.01330 | 0.00126 | 0.00176 |
| 13 | -0.04322 | 0.08957 | 0.03691 | 0.00000 | 0.00000 | 0.00000 |
| 14 | 0.19398 | 0.00000 | -0.04237 | 0.00000 | 0.00000 | 0.00000 |
| 15 | 0.01733 | 0.00000 | -0.00177 | 0.00000 | 0.00000 | 0.00000 |
| 16 | 0.06039 | 0.10170 | 0.02608 | 0.00000 | 0.00000 | 0.00000 |
| 17 | -0.53434 | 0.00000 | -0.12488 | 0.00000 | 0.00000 | 0.00000 |
| 18 | -0.04479 | 0.00000 | -0.00807 | 0.00000 | 0.00000 | 0.00000 |
| 20 | 0.09822 | 0.09922 | -0.25448 | -0.03350 | 0.03251 | -0.01514 |
| 21 | -0.05400 | 0.45337 | 0.46202 | -0.01726 | 0.03824 | -0.03893 |
| 22 | 0.02688 | 0.08284 | -0.04267 | 0.00000 | 0.00000 | 0.00000 |
| 23 | 0.04388 | 0.08036 | -0.03630 | 0.00000 | 0.00000 | 0.00000 |
| 24 | -0.03855 | 0.02295 | -0.00712 | 0.00000 | 0.00000 | 0.00000 |
| 25 | 0.04568 | 0.02294 | 0.00436 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 163 | 0.00307 | 0.01023 | -0.00124 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 167 | -0.03774 | 0.01744 | -0.01853 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 174 | 0.08506 | 0.00256 | -0.08216 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 183 | -0.02287 | 0.01465 | -0.10239 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 187 | 0.05691 | 0.01491 | -0.10985 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 194 | 0.01265 | 0.00271 | -0.00760 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 201 | 0.04731 | 0.01754 | -0.01920 | 0.00000 | 0.00000 | 0.00000 |
| FEM: 202 | 0.00783 | 0.01000 | -0.01906 | 0.00000 | 0.00000 | 0.00000 |

| | | | | | | |
|-----|---------|---------|---------|----------|---------|----------|
| SUM | 0.00000 | 2.31232 | 0.00000 | -0.16193 | 0.13770 | -0.03611 |
|-----|---------|---------|---------|----------|---------|----------|

Envelope for nodal reactions

Note.- I_c is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for

LC1=1.2DL+1.6Wo

LC2=0.9DL+1.6Wo

LC3=1.2DL+Wi+Di

LC4=1.2DL

LC5=0.9DL

| Node | | Forces | | | | | | Moments | | | | | |
|------|-----|-------------|-----|-------------|-----|-------------|-----|----------------|-----|----------------|-----|----------------|-----|
| | | Fx [Kip] | lc | Fy [Kip] | lc | Fz [Kip] | lc | Mx [Kip*ft] | lc | My [Kip*ft] | lc | Mz [Kip*ft] | lc |
| 8 | Max | 0.093 | LC3 | 0.808 | LC1 | 1.577 | LC2 | -0.04951 | LC5 | 0.29478 | LC1 | 0.02032 | LC1 |
| | Min | -0.016 | LC2 | 0.118 | LC5 | -0.804 | LC4 | -0.48107 | LC1 | 0.03346 | LC5 | 0.00127 | LC5 |
| 9 | Max | 0.282 | LC2 | 1.304 | LC3 | 1.352 | LC3 | -0.01610 | LC5 | 0.17197 | LC1 | -0.00205 | LC5 |
| | Min | -0.011 | LC4 | -0.656 | LC2 | -1.287 | LC2 | -0.33271 | LC1 | 0.00221 | LC5 | -0.15465 | LC1 |
| 11 | Max | -0.014 | LC5 | 0.190 | LC3 | -0.155 | LC5 | -0.03226 | LC5 | 0.04311 | LC3 | 0.02713 | LC1 |
| | Min | -0.386 | LC1 | 0.111 | LC5 | -0.603 | LC1 | -0.06280 | LC1 | -0.01796 | LC2 | 0.01698 | LC5 |
| 12 | Max | 0.218 | LC1 | 1.081 | LC1 | 1.169 | LC1 | -0.00028 | LC2 | 0.00168 | LC4 | 0.02385 | LC1 |
| | Min | 0.041 | LC5 | 0.195 | LC5 | 0.185 | LC5 | -0.02152 | LC3 | -0.02535 | LC2 | 0.00176 | LC5 |
| 13 | Max | -0.043 | LC5 | 0.155 | LC3 | 0.090 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.315 | LC1 | 0.090 | LC5 | 0.037 | LC5 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 14 | Max | 0.259 | LC4 | 0.000 | LC1 | 0.264 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -1.290 | LC2 | 0.000 | LC1 | -0.056 | LC4 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 15 | Max | 0.023 | LC4 | 0.000 | LC1 | 0.006 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.012 | LC3 | 0.000 | LC1 | -0.002 | LC4 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 16 | Max | 0.111 | LC3 | 0.167 | LC3 | 0.054 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | 0.060 | LC5 | 0.072 | LC2 | 0.026 | LC5 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 17 | Max | 3.275 | LC2 | 0.000 | LC1 | 0.739 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.712 | LC4 | 0.000 | LC1 | -0.167 | LC4 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 18 | Max | 0.015 | LC1 | 0.000 | LC1 | 0.005 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.060 | LC4 | 0.000 | LC1 | -0.011 | LC4 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 20 | Max | 0.170 | LC3 | 0.180 | LC1 | -0.093 | LC2 | -0.03350 | LC5 | 0.06270 | LC1 | -0.01514 | LC5 |
| | Min | 0.098 | LC5 | 0.099 | LC5 | -0.415 | LC3 | -0.08006 | LC1 | 0.03251 | LC5 | -0.02700 | LC1 |
| 21 | Max | -0.020 | LC2 | 0.784 | LC3 | 0.796 | LC3 | -0.01726 | LC5 | 0.06719 | LC3 | -0.03893 | LC5 |
| | Min | -0.091 | LC3 | 0.394 | LC2 | 0.371 | LC2 | -0.03852 | LC1 | 0.03824 | LC5 | -0.06861 | LC3 |
| 22 | Max | 0.036 | LC4 | 0.167 | LC1 | -0.043 | LC5 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.556 | LC2 | 0.083 | LC5 | -0.239 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 23 | Max | 0.061 | LC3 | 0.180 | LC1 | -0.036 | LC5 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.036 | LC2 | 0.080 | LC5 | -0.101 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 24 | Max | -0.039 | LC5 | 0.039 | LC3 | 0.066 | LC2 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | -0.102 | LC1 | 0.023 | LC5 | -0.009 | LC4 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| 25 | Max | 0.081 | LC3 | 0.039 | LC3 | 0.011 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |
| | Min | 0.046 | LC5 | 0.023 | LC5 | 0.004 | LC5 | 0.00000 | LC1 | 0.00000 | LC1 | 0.00000 | LC1 |

EXHIBIT 4



Radio Frequency Emissions Analysis Report

AT&T Existing Facility

Site ID: CT2177

FA#: 10035098

Site CT-305
7 Broadway Avenue Extension
Mystic, CT 06355

June 6, 2018

Centerline Communications Project Number: 950012-107

| Site Compliance Summary | |
|--|------------------|
| Compliance Status: | COMPLIANT |
| Site total MPE% of FCC general population allowable limit: | 16.10 % |



June 6, 2018

AT&T Mobility – New England
Attn: John Benedetto, RF Manager
550 Cochituate Road
Suite 550 – 13&14
Framingham, MA 06040

Emissions Analysis for Site: **CT2177 – Site CT-305**

Centerline Communications, LLC (“Centerline”) was directed to analyze the proposed AT&T facility located at **7 Broadway Avenue Extension, Mystic, CT**, for the purpose of determining whether the emissions from the Proposed AT&T Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications facility that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limits for the 700 and 850 MHz Bands are approximately $467 \mu\text{W}/\text{cm}^2$ and $567 \mu\text{W}/\text{cm}^2$ respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 2300 MHz (WCS) bands is $1000 \mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.



CALCULATIONS

Calculations were performed for the proposed AT&T Wireless antenna facility located at **7 Broadway Avenue Extension, Mystic, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since AT&T is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the water tank. For this report the sample point is the top of a 6-foot person standing at the base of the water tank.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in *Table 1*:

| Technology | Frequency Band | Channel Count | Transmit Power per Channel (W) |
|------------|-------------------|---------------|--------------------------------|
| UMTS | 850 MHz | 2 | 30 |
| UMTS | 1900 MHz (PCS) | 2 | 30 |
| LTE | 700 MHz | 2 | 40 |
| LTE | 1900 MHz (PCS) | 4 | 40 |
| LTE | 700 MHz (Band 14) | 4 | 40 |
| LTE | 2100 MHz (AWS) | 4 | 30 |

Table 1: Channel Data Table



The following antennas listed in *Table 2* were used in the modeling for transmission in the 700 MHz, 850 MHz, 1900 MHz (PCS) and 2100 MHz (AWS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

| Sector | Antenna Number | Antenna Make / Model | Antenna Centerline (ft) |
|--------|----------------|-----------------------|-------------------------|
| A | 1 | Powerwave 7770 | 140 |
| A | 2 | Commscope SBNHH-1D65A | 140 |
| A | 3 | Quintel QS46512-2 | 140 |
| B | 1 | Powerwave 7770 | 140 |
| B | 2 | Commscope SBNHH-1D65A | 140 |
| B | 3 | Quintel QS46512-2 | 140 |
| C | 1 | Powerwave 7770 | 140 |
| C | 2 | Commscope SBNHH-1D65A | 140 |
| C | 3 | Quintel QS46512-2 | 140 |

Table 2: Antenna Data

All calculations were done with respect to uncontrolled / general population threshold limits.



RESULTS

Per the calculations completed for the proposed AT&T configurations *Table 3* shows resulting emissions power levels and percentages of the FCC's allowable general population limit.

| Antenna ID | Antenna Make / Model | Frequency Bands | Antenna Gain (dBd) | Channel Count | Total TX Power (W) | ERP (W) | MPE % |
|-------------------------|-----------------------|--------------------------|--------------------|---------------|--------------------|----------|-------------|
| Antenna A1 | Powerwave 7770 | 850 MHz / 1900 MHz (PCS) | 11.4 / 13.4 | 4 | 120 | 2,140.89 | 0.56 |
| Antenna A2 | Commscope SBNHH-1D65A | 700 MHz / 1900 MHz (PCS) | 10.85 / 14.55 | 6 | 200 | 4,394.17 | 1.10 |
| Antenna A3 | Quintel QS46512-2 | 700 MHz / 2100 MHz (AWS) | 10.55 / 13.85 | 8 | 280 | 4,727.95 | 1.36 |
| Sector A Composite MPE% | | | | | | | 3.02 |
| Antenna B1 | Powerwave 7770 | 850 MHz / 1900 MHz (PCS) | 11.4 / 13.4 | 4 | 120 | 2,140.89 | 0.56 |
| Antenna B2 | Commscope SBNHH-1D65A | 700 MHz / 1900 MHz (PCS) | 10.85 / 14.55 | 6 | 200 | 4,394.17 | 1.10 |
| Antenna B3 | Quintel QS46512-2 | 700 MHz / 2100 MHz (AWS) | 10.55 / 13.85 | 8 | 280 | 4,727.95 | 1.36 |
| Sector B Composite MPE% | | | | | | | 3.02 |
| Antenna C1 | Powerwave 7770 | 850 MHz / 1900 MHz (PCS) | 11.4 / 13.4 | 4 | 120 | 2,140.89 | 0.56 |
| Antenna C2 | Commscope SBNHH-1D65A | 700 MHz / 1900 MHz (PCS) | 10.85 / 14.55 | 6 | 200 | 4,394.17 | 1.10 |
| Antenna C3 | Quintel QS46512-2 | 700 MHz / 2100 MHz (AWS) | 10.55 / 13.85 | 8 | 280 | 4,727.95 | 1.36 |
| Sector C Composite MPE% | | | | | | | 3.02 |

Table 3: AT&T Emissions Levels



The Following table (*table 4*) shows all additional carriers on site and their MPE% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum AT&T MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, all three sectors have the same configuration yielding the same results on all three sectors. *Table 5* below shows a summary for each AT&T Sector as well as the composite MPE value for the site.

| Site Composite MPE% | |
|----------------------------|----------------|
| Carrier | MPE% |
| AT&T – Max Sector Value | 3.02 % |
| American Messaging | 0.03 % |
| Town of Stonington | 0.00 % |
| Sprint | 3.10 % |
| T-Mobile | 3.30 % |
| Verizon Wireless | 6.65 % |
| Site Total MPE %: | 16.10 % |

Table 4: All Carrier MPE Contributions

| | |
|----------------------|----------------|
| AT&T Sector A Total: | 3.02 % |
| AT&T Sector B Total: | 3.02 % |
| AT&T Sector C Total: | 3.02 % |
| | |
| Site Total: | 16.10 % |

Table 5: Site MPE Summary



FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. *Table 6* below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated AT&T sector(s). For this site, all three sectors have the same configuration yielding the same results on all three sectors.

| AT&T _ Frequency Band / Technology Max Power Values (Per Sector) | # Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ($\mu\text{W}/\text{cm}^2$) | Frequency (MHz) | Allowable MPE ($\mu\text{W}/\text{cm}^2$) | Calculated % MPE |
|--|---------------|----------------------------|------------------|---|--------------------|---|---------------------|
| AT&T 850 MHz UMTS – Antenna 1 | 2 | 414.12 | 140 | 1.66 | 850 MHz | 567 | 0.29% |
| AT&T 1900 MHz (PCS) UMTS– Antenna 1 | 2 | 656.33 | 140 | 2.63 | 1900 MHz (PCS) | 1000 | 0.26% |
| AT&T 700 MHz LTE– Antenna 2 | 2 | 486.47 | 140 | 1.95 | 700 MHz | 467 | 0.42% |
| AT&T 1900 MHz (PCS) LTE– Antenna 2 | 4 | 855.31 | 140 | 6.85 | 1900 MHz (PCS) | 1000 | 0.68% |
| AT&T 700 MHz LTE (Band 14) – Antenna 3 | 4 | 454.00 | 140 | 3.64 | 700 MHz | 467 | 0.78% |
| AT&T 2100 MHz (AWS) LTE– Antenna 3 | 4 | 727.98 | 140 | 5.83 | 2100 MHz (AWS) | 1000 | 0.58% |
| | | | | | | Total: | 3.02% |

Table 6: AT&T Maximum Sector MPE Power Values



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the AT&T facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| AT&T Sector | Power Density Value (%) |
|-------------------------------------|-------------------------|
| Sector A: | 3.02 % |
| Sector B: | 3.02 % |
| Sector C: | 3.02 % |
| AT&T Maximum Total (per sector): | 3.02 % |
| | |
| Site Total: | 16.10 % |
| | |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is **16.10 %** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

A handwritten signature in black ink, appearing to read 'Scott Heffernan', is written over a light blue horizontal line.

Scott Heffernan

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