# JULIE D. KOHLER 

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September 11, 2014

Melanie Bachman, Esq.<br>Acting Executive Director<br>Connecticut Siting Council<br>Ten Franklin Square<br>New Britain, CT 06051

## Re: Notice of Exempt Modification <br> Crown/T-Mobile co-location <br> T-Mobile Site ID CT11410A <br> 555 Main Street, Stamford CT

Dear Attorney Bachman:
This office represents T-Mobile Northeast LLC ("T-Mobile") and has been retained to file exempt modification filings with the Connecticut Siting Council on its behalf.

On March 15, 2013 T-Mobile filed a notice of exempt modification to modify a telecommunication facility pursuant to R.C.S.A. § 16-50j-73. The Council issued an acknowledgment on April 9, 2103. T-Mobile was unable to complete construction prior to the expiration of the one year time frame and hereby requests that the Council reconsider and acknowledge the notice of exempt modification for an additional year. T-Mobile represents that the proposal contained in its March 15, 2013 filing remains unchanged, and that according to the Council's database, no other carrier has filed for co-location on this facility since the date of T-Mobile's acknowledgement.

Please accept this letter as notification of construction which constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the Mayor David Martin, and the property owner, Southern New England Telephone Company.

To recap the proposal provided in the March 15, 2013 filing.

- The existing Stamford Facility consists of a rooftop mounted tower facility, which extends to a height of approximately $235^{\prime} 10^{\prime \prime}$ AGL, including the existing TMobile antennas.
- T-Mobile plans to replace 3 antenna mounted on the rooftop tower facility at a

[^0]158 Deer Hill Avenue

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centerline of 210' $10^{\prime \prime}$, will replace 3 antenna mounted on the rooftop tower facility at a centerline of $205^{\prime} 10^{\prime \prime}$, and will add 3 tower mounted amplifiers ("TMAs") at a height of 205' 10." (See plans revised to April 27, 2012, attached hereto as Exhibit A).

- Finally, T-Mobile will add 2 equipment cabinets to the rooftop equipment compound, remove 3 existing cabinets from the same area and run fiber conduit along existing coaxial cabling.
- The existing rooftop tower facility is structurally capable of supporting T-Mobile's proposed use, as indicated in the Structural Analysis Report dated February 28, 2013 and attached hereto as Exhibit B. The planned modifications to the Stamford Facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modification will not increase the height of the tower. T-Mobile's replacement antennas will be installed at the $210^{\prime} 10^{\prime \prime}$ and $205^{\prime} 10^{\prime \prime}$ foot level. The enclosed plans confirm that the proposed modification will not increase the height of the rooftop facility.
2. The installation of the T-Mobile replacement equipment in the existing equipment room, as reflected on the attached plans, will not require an extension of the site boundaries. T-Mobile's proposed equipment will be located entirely within the existing equipment area.
3. The proposed modification to the Facility will not increase the noise levels at the existing facility by six decibels or more.
4. The operation of the replacement antennas will not increase the total radio frequency (RF) power density, measured at the base of the tower, to a level at or above the applicable standard. According to a Radio Frequency Emissions Analysis Report prepared by EBI dated August 14, 2012, attached hereto as Exhibit C, T-Mobile's operations would add $0.257 \%$ of the FCC Standard. Therefore, the calculated "worst case" power density for the planned combined operation at the site including all of the proposed antennas would be $11.457 \%$ of the FCC Standard as calculated for a mixed frequency site.

For the foregoing reasons, T-Mobile respectfully submits that the proposed replacement antennas and equipment at the Stamford Facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

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Sincerely,


Julie D. Kohler, Esq.
cc: Mayor David Martin, Mayor of Stamford
Southern New England Telephone Company, property owner
Crown
Halene Fujimoto, HPC Wireless





HPC Development
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Danbury, CT 06811
(203) 797-1112

GPD GROUP。
Glaus, pyle, Schomeer, Burns 点 Dehaven, inc.
Kevin Clements
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kclements@gpdgroup.com
GPD \#: 2012814.17 Rev. 1
February 28, 2013

## STRUCTURAL ANALYSIS REPORT

## AT\&T DESIGNATION:

ANALYSIS CRITERIA:
Site USID:
Site FA:
Site Name:
AT\&T Project:

## Codes:

SNET026
10137413
STAMFORD CO
T-Mobile (modrn) Rooftop 06-18-12
TIA/EIA-222-F, 2003 IBC, \& ASCE 7-05
85 mph with $0^{\prime \prime}$ ice
37 mph with $3 / 4^{\prime \prime}$ ice
555 East Main Street, Stamford, CT 06902, Fairfield County Latitude $41^{\circ} 3^{\prime} 11.999 " \mathrm{~N}$, Longitude $73^{\circ} 32^{\prime} 9.999^{\prime \prime} \mathrm{W}$
Market: NEW ENGLAND
125' Modified Self Support Tower
Mr. Thomas Wilson,
GPD is pleased to submit this Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

## Analysis Results

Tower Stress Level with Proposed Equipment: $93.8 \%$ Pass
We at GPD appreciate the opportunity of providing our continuing professional services to you and HPC Development. If you have any questions or need further assistance on this or any other projects please do not hesitate to call.

Respectfully submitted,

John N. Kabak, P.E.
Connecticut \#: PEN. 0028336


## SUMMARY \& RESULTS

The purpose of this analysis was to verify whether the existing structure is capable of carrying the proposed loading configuration as specified by T-Mobile to AT\&T Towers. This report was commissioned by Mr. Thomas Wilson of AT\&T Towers.

No foundation or geotechnical information was available or provided for this report. Therefore, the in place capacity of the foundation could not be verified. A more thorough and accurate assessment of foundation capacity will require a site specific geotechnical report and foundation information.

Insufficient information regarding the frame that connects the tower to the building was available or provided for this report. Therefore, the in place capacity of the frame could not be verified. A more thorough and accurate assessment of the mounting frame capacity will require a tower mapping.

Modifications designed by MEI Project \#: CT02786-11V0, dated 7/28/11 were found to be ineffective and were not considered in this analysis.

The proposed coax shall be placed next to the existing coax on tower face $C$ in order for the results of this analysis to be valid. See Appendix C for more details.

TOWER SUMMARY AND RESULTS

| Member | Capacity | Results |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Legs | $76.2 \%$ | Pass |  |  |  |
| Leg Bolts | $56.3 \%$ | Pass |  |  |  |
| Diagonals | $93.8 \%$ | Pass |  |  |  |
| Horizontals | $58.6 \%$ | Pass |  |  |  |
| Redundants | $84.1 \%$ | Pass |  |  |  |
| Member Bolts | $51.6 \%$ | Pass |  |  |  |
|  |  |  |  |  |  |
| Base Frame |  |  |  | Not Verified | N/A |

## ANALYSIS METHOD

tnxTower (Version 6.0.4.0), a commercially available software program, was used to create a three-dimensional model of the tower and calculate primary member stresses for various dead, live, wind, and ice load cases. Selected output from the analysis is included in Appendix B. The following table details the information provided to complete this structural analysis. This analysis is solely based on this information and is being completed without the benefit of a GPD detailed site visit.

DOCUMENTS PROVIDED

| Document | Remarks | Source |
| :--- | :--- | :---: |
| Site Lease Application | T-Mobile Application, dated 7/19/12 | Siterra |
| Tower Design | Not Provided | $\mathrm{N} / \mathrm{A}$ |
| Foundation Design | Not Provided | $\mathrm{N} / \mathrm{A}$ |
| Geotechnical Report | Not Provided | $\mathrm{N} / \mathrm{A}$ |
| Previous Structural Analysis | MEI Project \#: CT02786-11V0, dated 7/28/11 | Siterra |
| Modification Drawings | MEI Project \#: CT02786-11V0, dated 7/28/11 | Siterra |

## ASSUMPTIONS

This structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analyzing the tower only.
5. The soil parameters are as per data supplied or as assumed and stated in the calculations. If no data is available, the foundation system is not verified. In the case of absent foundation data, it is the tower owner's responsibility to insure that the foundation system is adequate to support the structure with its new reactions.
6. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
7. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
8. Modifications designed by MEI Project \#: CT02786-11V0, dated 7/28/11 were found to be ineffective and were not considered in this analysis.
9. Loading interpreted from photos is accurate to $\pm 5^{\prime} \mathrm{AGL}$, antenna size accurate to $\pm 3.3 \mathrm{sf}$, and coax equal to the number of existing antennas without reserve.
10. All existing loading was obtained from the previous structural analysis by MEI Project \#: CT02786-11V0, dated 7/28/11, site photos, the provided Site Lease Application, and is assumed to be accurate.
11. Tower Leg A is assumed to be at an azimuth of $315^{\circ}$ based on satellite imagery.
12. The proposed coax shall be placed next to the existing coax on tower face $C$ in order for the results of this analysis to be valid.
13. The existing T-Mobile loading elevations found in site photos and the Site Lease Application were found to vary from the elevations listed within the previous structural analysis by MEI Project \#: CT02786-11V0, dated $7 / 28 / 11$. The existing and proposed elevations have been modeled based on elevations listed within site photos and the Site Lease Application.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD Group should be allowed to review any new information to determine its effect on the structural integrity of the tower.

## DISCLAIMER OF WARRANTIES

GPD GROUP has not performed a site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD GROUP in connection with this Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. All tower components. have been assumed to only resist dead loads when no other loads are applied. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

GPD GROUP does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD GROUP provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the feasibility of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the specified code recommended amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD GROUP, but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

GPD GROUP makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD GROUP will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD GROUP pursuant to this report will be limited to the total fee received for preparation of this report.

## APPENDIX A

Tower Analysis Summary Form

Tower Analysis Summary Form

Loadlng

| Antennia |  |  |  |  |  |  |  | Mount |  |  | Transmission Line |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Owner | Mount Height (it) | $\begin{gathered} \hline \text { Antenina } \\ \text { CL ( } \mathrm{tt}) \\ \hline \end{gathered}$ | Quantity | Type | Manufacturer | Model | Azimuth | Quantity | Manufacturer | Type | Quantity | Model | Size | Attachment Leg/Face |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## APPENDIX B

tnxTower Output File

| tnxTower | SNET026 STAMFORD CO |  | $\begin{array}{ll} \hline \text { Page } & \\ & 1 \text { of } 9 \end{array}$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Ste 2531 <br> Akron, OH <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2012814.17 Rev. 1 | $\begin{array}{\|l\|l\|} \hline \text { Date } \\ \text { 14:32:08 02/28/13 } \end{array}$ |
|  | Client | HPC Development | Designed by tclark |

## Tower Input Data

The main tower is a 4 x free standing tower with an overall height of 231.50 ft above the ground line.
The base of the tower is set at an elevation of 106.50 ft above the ground line.
The face width of the tower is 5.60 ft at the top and 13.58 ft at the base.
This tower is designed using the TIA/EIA-222-F standard.
The following design criteria apply:
Tower is located in Fairfield County, Connecticut.
Basic wind speed of 85 mph .
Nominal ice thickness of 0.7500 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf .
A wind speed of 37 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 50 mph .
Pressures are calculated at each section.
Stress ratio used in tower member design is 1.333.
Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.
Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \\ \hline \end{gathered}$ | Allow Shield | Component Type | Placement <br> ft | Face Offset in | Lateral Offset <br> (Frac FW) | \# | \# <br> Per <br> Row | Clear Spacing in | Width or Diameter in | Perimeter <br> in | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Feedline Ladder (Af) | A | No | Af (CfAe) | 210.00-106.50 | 0.0000 | -0.3 | 1 | 1 | 3.0000 | 3.0000 | 12.0000 | 8.40 |
| LDF7-50A (1-5/8 FOAM) | A | Yes | Ar (CfAe) | 205.00-106.50 | 0.0000 | -0.3 | 12 | 8 | 0.7500 | 1.9800 |  | 0.82 |
| LDF7-50A (1-5/8 FOAM) | A | Yes | Ar (CfAe) | 210.00-205.00 | 0.0000 | -0.3 | 6 | 6 | 0.7500 | 1.9800 |  | 0.82 |
| 40 mm Hybrid Cable | A | Yes | Ar (CfAe) | 210.00-106.50 | 3.0000 | -0.255 | 1 | 1 | 1.5500 | 0.0000 |  | 0.66 |
| Feedline Ladder (Af) | B | No | Af (Leg) | 231.50-106.50 | 0.0000 | 0.15 | 1 | 1 | 3.0000 | 3.0000 | 12.0000 | 8.40 |
| LDF7-50A (1-5/8 FOAM) | B | No | Ar (Leg) | 231.50-106.50 | 0.0000 | 0.15 | 12 | 1 | 0.7500 | 1.9800 |  | 0.82 |
| 2" Flex Conduit | B | No | Ar (Leg) | 231.50-106.50 | 0.0000 | 0.1 | 1 | 1 | 2.0000 | 2.0000 |  | 0.32 |
| 5/8" DC cable | B | No | At (Leg) | 231.50-106.50 | 0.0000 | 0.1 | 6 | 2 | 0.6250 | 0.0000 |  | 0.30 |
| 3/8" Fiber Cable | B | No | Ar (Leg) | 231.50-106.50 | 0.0000 | 0.1 | 3 | 2 | 0.3750 | 0.0000 |  | 0.10 |
| LDF4-50A (1/2 FOAM) | B | No | Ar (Leg) | 132.00-106.50 | 0.0000 | 0.1 | 2 | 2 | 0.6300 | 0.0000 |  | 0.15 |
| LDF4-50A (1/2 FOAM) | B | No | Ar (Leg) | 229.00-132.00 | 0.0000 | 0.1 | 1 | 1 | 0.6300 | 0.0000 |  | 0.15 |
| EW90 | B | No | Af (Leg) | 223.50-106.50 | 0.0000 | 0.1 | 2 | 1 | 0.9869 | 0.9869 | 3.2550 | 0.32 |
| LDF2-50A (3/8 FOAM) | B | No | Ar (Leg) | 221.00-106.50 | 0.0000 | 0.1 | 3 | 2 | 0.4400 | 0.0000 |  | 0.08 |
| LDF2-50A (3/8 FOAM) | B | No | Ar (Leg) | 221.50-221.00 | 0.0000 | 0.1 | 2 | 2 | 0.4400 | 0.0000 |  | 0.08 |
| . $3^{\prime \prime}$ coax | B | No | Ar (Leg) | 231.50-106.50 | 0.0000 | 0.1 | 1 | 1 | 0.4400 | 0.0000 |  | 0.08 |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz Lateral Vert \(f t\) \(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement

ft \& \& \begin{tabular}{l}
$C_{A} A_{A}$ <br>
Front <br>
$f t^{2}$

 \& 

$C_{A} A_{A}$ <br>
Side <br>
$f t^{2}$
\end{tabular} \& Weight

$l b$ <br>
\hline \multirow[t]{5}{*}{Top Platform} \& C \& None \& \& 0.0000 \& 234.00 \& No Ice \& 42.50 \& 12.60 \& 1700.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 53.13 \& 15.75 \& 2125.00 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 63.75 \& 18.90 \& 2550.00 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 85.00 \& 25.20 \& 3400.00 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 127.50 \& 37.80 \& 5100.00 <br>
\hline AM-X-CD-14-65-00T-RET w/ 8' Mount Pipe \& B \& From \& 4.00 \& -60,0000 \& 234.00 \& No Ice \& 6.91 \& 5.63 \& 91.44 <br>
\hline
\end{tabular}

| tnxTower | SNET026 STAMFORD CO |  | $\begin{aligned} & \text { Page } 2 \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Ste 2531 <br> Akron, OH <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2012814.17 Rev. 1 | Date $14: 32: 08 \text { 02/28/13 }$ |
|  | Client | HPC Development | Designed by tclark |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
ft \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement

ft \& \& $C_{A} A_{A}$ Front $f t^{2}$ \& $C_{A} A_{A}$
Side

$f^{2}$ \& Weight

$l b$ <br>

\hline \& \& \multirow[t]{4}{*}{Centroid-Face} \& \multirow[t]{4}{*}{$$
\begin{gathered}
-10.50 \\
0.00
\end{gathered}
$$} \& \& \& 1/2" Ice \& 7.60 \& 6.54 \& 153.88 <br>

\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 8.25 \& 7.36 \& 220.61 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 9.58 \& 9.12 \& 382.75 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 12.39 \& 12.85 \& 825.53 <br>
\hline \multirow[t]{5}{*}{AM-X-CD-14-65-00T-RET w/ 8' Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Centroid-Face} \& 4.00 \& \multirow[t]{5}{*}{60.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 6.91 \& 5.63 \& 91.44 <br>
\hline \& \& \& 10.50 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 7.60 \& 6.54 \& 153.88 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 8.25 \& 7.36 \& 220.61 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 9.58 \& 9.12 \& 382.75 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 12.39 \& 12.85 \& 825.53 <br>

\hline \multirow[t]{5}{*}{AM-X-CD-14-65-00T-RET w/ 8' Mount Pipe} \& \multirow[t]{5}{*}{D} \& \multirow[t]{5}{*}{| From |
| :--- |
| Centroid-Face |} \& 5.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 6.91 \& 5.63 \& 91.44 <br>

\hline \& \& \& 11.50 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 7.60 \& 6.54 \& 153.88 <br>
\hline \& \& \& \& \& \& 1 I' Ice \& 8.25 \& 7.36 \& 220.61 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 9.58 \& 9.12 \& 382.75 <br>
\hline \& \& \& \& \& \& $4^{\prime \prime}$ Ice \& 12.39 \& 12.85 \& 825.53 <br>
\hline \multirow[t]{5}{*}{P65-15-XLH-RR w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Centroid-Face} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 5.97 \& 4.05 \& 56.82 <br>
\hline \& \& \& -4.00 \& \& \& 1/2" Ice \& 6.39 \& 4.64 \& 100.95 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 6.81 \& 5.25 \& 153.59 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 7.69 \& 6.60 \& 279.06 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 9.56 \& 9.67 \& 635.70 <br>
\hline \multirow[t]{5}{*}{P65-15-XLH-RR w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Centroid-Face} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 5.97 \& 4.05 \& 56.82 <br>
\hline \& \& \& -8.00 \& \& \& 1/2" Ice \& 6.39 \& 4.64 \& 100.95 <br>
\hline \& \& \& 0.00 \& \& \& 1 I' Ice \& 6.81 \& 5.25 \& 153.59 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 7.69 \& 6.60 \& 279.06 <br>
\hline \& \& \& \& \& \& 4 "Ice \& 9.56 \& 9.67 \& 635.70 <br>
\hline \multirow[t]{5}{*}{P65-15-XLH-RR w/ Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Centroid-Face} \& \& \multirow[t]{5}{*}{20.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 5.97 \& 4.05 \& 56.82 <br>
\hline \& \& \& 4.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 6.39 \& 4.64 \& 100.95 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 6.81 \& 5.25 \& 153.59 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 7.69 \& 6.60 \& 279.06 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 9.56 \& 9.67 \& 635.70 <br>

\hline \multirow[t]{5}{*}{P65-15-XLH-RR w/ Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Centroid-Face} \& \& \multirow[t]{5}{*}{20.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 5.97 \& 4.05 \& $$
56.82
$$ <br>

\hline \& \& \& $$
2.00
$$ \& \& \& \[

1 / 2^{\prime \prime} Ice

\] \& 6.39 \& 4.64 \& \[

100.95
\] <br>

\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 6.81 \& 5.25 \& 153.59 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 7.69 \& 6.60 \& 279.06 <br>
\hline \& \& \& \& \& \& 4" Ice \& 9.56 \& 9.67 \& 635.70 <br>
\hline \multirow[t]{5}{*}{P65-15-XLH-RR w/ Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Centroid-Face} \& \& \multirow[t]{5}{*}{10.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 5.97 \& 4.05 \& 56.82 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 6.39 \& 4.64 \& 100.95 <br>
\hline \& \& \& 0.00 \& \& \& 1 " Ice \& 6.81 \& 5.25 \& 153.59 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 7.69 \& 6.60 \& 279.06 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 9.56 \& 9.67 \& 635.70 <br>
\hline \multirow[t]{5}{*}{P65-15-XLH-RR w/ Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Centroid-Face} \& 11.50 \& \multirow[t]{5}{*}{10.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 5.97 \& 4.05 \& 56.82 <br>
\hline \& \& \& -5.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 6.39 \& 4.64 \& 100.95 <br>
\hline \& \& \& 0.00 \& \& \& 1 "Ice \& 6.81 \& 5.25 \& 153.59 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 7.69 \& 6.60 \& 279.06 <br>
\hline \& \& \& \& \& \& $4^{\prime \prime}$ Ice \& 9.56 \& 9.67 \& 635.70 <br>
\hline \multirow[t]{5}{*}{(2) RRUS 11} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Centroid-Face} \& 4.00 \& \multirow[t]{5}{*}{-60.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 2.94 \& 1.25 \& 55.00 <br>
\hline \& \& \& -10.50 \& \& \& $1 / 2^{1 \prime}$ Ice \& 3.17 \& 1.41 \& 74.32 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 3.41 \& 1.59 \& 96.56 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.91 \& 1.96 \& 150.56 <br>
\hline \& \& \& \& \& \& 4 Itce \& 5.02 \& 2.82 \& 302.12 <br>
\hline \multirow[t]{5}{*}{(2) RRUS 11} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Centroid-Face} \& 4.00 \& \multirow[t]{5}{*}{60.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 2.94 \& 1.25 \& 55.00 <br>
\hline \& \& \& 10.50 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.17 \& 1.41 \& 74.32 <br>
\hline \& \& \& 0.00 \& \& \& 1 Ice \& 3.41 \& 1.59 \& 96.56 <br>
\hline \& \& \& \& \& \& 2" Ice \& 3.91 \& 1.96 \& 150.56 <br>
\hline \& \& \& \& \& \& $4^{\prime \prime}$ Ice \& 5.02 \& 2.82 \& 302.12 <br>
\hline \multirow[t]{3}{*}{(2) RRUS 11} \& \multirow[t]{3}{*}{D} \& \multirow[t]{3}{*}{From Centroid-Face} \& 5.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{234.00} \& No Ice \& 2.94 \& 1.25 \& 55.00 <br>
\hline \& \& \& 11.50 \& \& \& $1 / 2^{\text {" }}$ Ice \& 3.17 \& 1.41 \& 74.32 <br>
\hline \& \& \& 0.00 \& \& \& 1 "Ice \& 3.41 \& 1.59 \& 96.56 <br>
\hline
\end{tabular}

| tnxTower | SNET026 STAMFORD CO |  | $\begin{aligned} & \text { Page } \quad 3 \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Ste 2531 <br> Akron, OH <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2012814.17 Rev. 1 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:32:08 02/28/13 } \end{array}$ |
|  | Client | HPC Development | Designed by tclark |


| Description | $\begin{aligned} & \text { Face } \\ & \text { or } \\ & \text { Leg } \end{aligned}$ | Offset <br> Type |  | Azimuth Adjustment <br> 0 | Placement |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Side <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC6-48-60-18-8F Surge Suppression Unit | B | From Centroid-Face |  | 0.0000 | 234.00 | $2^{\prime \prime}$ Ice | 3.91 | 1.96 | 150.56 |
|  |  |  |  |  |  | $4^{\prime \prime}$ Ice | 5.02 | 2.82 | 302.12 |
|  |  |  | 4.00 |  |  | No Ice | 1.47 | 1.47 | 32.80 |
|  |  |  | -10.00 |  |  | $1 / 2^{\text {" }}$ Ice | 1.67 | 1.67 | 50.52 |
|  |  |  | 0.00 |  |  | $1^{\prime \prime}$ Ice | 1.88 | 1.88 | 70.72 |
|  |  |  |  | 0.0000 | 234.00 | 2" Ice | 2.33 | 2.33 | 119.24 |
|  | B | From <br> Centroid-Face |  |  |  | $4^{\prime \prime}$ Ice | 3.38 | 3.38 | 252.92 |
| LGP21401 |  |  | 4.00 |  |  | No Ice | 1.29 | 0.23 | 14.10 |
|  |  |  | -4.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 1.45 | 0.31 | 21.26 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 1.61 | 0.40 | 30.32 |
|  | B | From Centroid-Face |  | 0.0000 | 234.00 | $2^{\prime \prime}$ Ice | 1.97 | 0.61 | 54.89 |
|  |  |  |  |  |  | $4{ }^{\prime \prime}$ Ice | 2.79 | 1.12 | 135.29 |
| LGP21401 |  |  | 4.00 |  |  | No Ice | 1.29 | 0.23 | 14.10 |
|  |  |  | -8.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 1.45 | 0.31 | 21.26 |
|  |  |  | 0.00 |  |  | 1 " Ice | 1.61 | 0.40 | 30.32 |
|  | C | From Centroid-Face |  | 20.0000 | 234.00 | $2^{\prime \prime}$ Ice | 1.97 | 0.61 | 54.89 |
|  |  |  |  |  |  | $4^{\prime \prime}$ Ice | 2.79 | 1.12 | 135.29 |
| LGP21401 |  |  | 10.50 |  |  | No Ice | 1.29 | 0.23 | 14.10 |
|  |  |  | 4.00 |  |  | 1/2" Ice | 1.45 | 0.31 | 21.26 |
|  |  |  |  |  |  | $1^{\prime \prime}$ Ice | 1.61 | 0.40 | 30.32 |
|  | C | From Centroid-Face |  | 20.0000 | 234.00 | $2^{\prime \prime}$ Ice | 1.97 | 0.61 | 54.89 |
|  |  |  |  |  |  | $4^{\prime \prime}$ Ice | 2.79 | 1.12 | 135.29 |
| LGP21401 |  |  | 10.50 |  |  | No Ice | 1.29 | 0.23 | 14.10 |
|  |  |  | 2.00 |  |  | $1 / 2^{1 \prime}$ Ice | 1.45 | 0.31 | 21.26 |
|  |  |  | 0.00 |  |  | 1 I' Ice | 1.61 | 0.40 | 30.32 |
|  | A | From Centroid-Face |  | 10.0000 | 234.00 | $2^{\prime \prime}$ Ice | 1.97 | 0.61 | 54.89 |
| LGP21401 |  |  |  |  |  | $4^{\prime \prime}$ Ice | 2.79 | 1.12 | 135.29 |
|  |  |  | 10.50 |  |  | No Ice | 1.29 | 0.23 | 14.10 |
|  |  |  | 0.00 |  |  | $1 / 2^{\text {n }}$ Ice | 1.45 | 0.31 | 21.26 |
|  |  |  | 0.00 |  |  | 1" Ice | 1.61 | 0.40 | 30.32 |
|  | A |  |  | 10.0000 | 234.00 | $2^{\prime \prime}$ Ice | 1.97 | 0.61 | 54.89 |
| LGP21401 |  | From Centroid-Face |  |  |  | 4 " Ice | 2.79 | 1.12 | 135.29 |
|  |  |  | 11.50 |  |  | No Ice | 1.29 | 0.23 | 14.10 |
|  |  |  | -5.00 |  |  | $1 / 2^{\text {n }}$ Ice | 1.45 | 0.31 | 21.26 |
|  |  |  | 0.00 |  |  | 1 " Ice | 1.61 | 0.40 | 30.32 |
| $13^{\prime}$ T Beam | D | From Leg |  | 0.0000 | 234.00 | $2^{\prime \prime}$ Ice | 1.97 | 0.61 | 54.89 |
|  |  |  |  |  |  | $4^{\prime \prime}$ Ice | 2.79 | 1.12 | 135.29 |
|  |  |  |  |  |  | No Ice | 11.11 | 11.11 | 372.00 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 11.84 | 11.84 | 440.74 |
|  |  |  | 6.50 |  |  | 1" Ice | 12.58 | 12.58 | 518.48 |
| (2) Beacon Light | D | From Leg |  | 0.0000 | 234.00 | $2^{\prime \prime}$ Ice | 14.08 | 14.08 | 701.78 |
|  |  |  |  |  |  | $4^{\prime \prime}$ Ice | 17.18 | 17.18 | 1185.04 |
|  |  |  |  |  |  | No Ice | 0.28 | 0.28 | 10.00 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 0.36 | 0.36 | 13.82 |
|  |  |  | 13.00 |  |  | $1^{\prime \prime}$ Ice | 0.46 | 0.46 | 18.82 |
| 6 Lightning Rod | D | From Leg |  | 0.0000 | 234.00 | $2^{\prime \prime}$ Ice | 0.69 | 0.69 | 32.93 |
|  |  |  |  |  |  | $4^{\prime \prime}$ Ice | 1.27 | 1.27 | 81.93 |
|  |  |  | 0.00 |  |  | No Ice | 0.45 | 0.45 | 10.00 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 1.06 | 1.06 | 14.66 |
| Pipe Mount 6'x ${ }^{\text {2 }} 37{ }^{\prime \prime}$ |  | From <br> Centroid-Leg | 16.00 |  |  | $1^{\prime \prime}$ Ice | 1.70 | 1.70 | 23.21 |
|  | A |  |  | 0.0000 | 234.00 | $2^{\prime \prime}$ Ice | 2.51 | 2.51 | 52.61 |
|  |  |  |  |  |  | 4 " Ice | 4.12 | 4.12 | 164.87 |
|  |  |  | 10.50 |  |  | No Ice | 1.43 | 1.43 | 26.10 |
|  |  |  | 4.00 |  |  | 1/2" Ice | 1.92 | 1.92 | 36.93 |
|  |  |  | $-2.50$ |  |  | $1{ }^{\prime \prime}$ Ice | 2.29 | 2.29 | 51.81 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 3.06 | 3.06 | 94.38 |
|  |  |  |  |  |  | 4" Ice | 4.70 | 4.70 | 234.94 |


| tnxTower | SNET026 STAMFORD CO |  | $\begin{aligned} & \text { Page } 4 \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Ste 2531 <br> Akron, OH <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2012814.17 Rev. 1 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:32:08 02/28/13 } \end{array}$ |
|  | Client | HPC Development | Designed by tclark |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{aligned}
\& \text { Face } \\
\& \text { or } \\
\& \text { Leg }
\end{aligned}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\)
\end{tabular} \& Azimuth Adjustment \& Placernent

$f t$ \& \& $C_{A} A_{A}$ Front $f t^{2}$ \& $C_{A} A_{A}$
Side

$f t^{2}$ \& Weight

$l b$ <br>
\hline \multirow[t]{5}{*}{1.5 Yagi} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Centroid-Leg} \& 10.50 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{234.00} \& No Ice \& 0.30 \& 0.30 \& 5.00 <br>
\hline \& \& \& 4.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 0.43 \& 0.43 \& 8.28 <br>
\hline \& \& \& \multirow[t]{3}{*}{$-5.00$} \& \& \& $1{ }^{1 \prime}$ Ice \& 0.58 \& 0.58 \& 13.14 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 0.93 \& 0.93 \& 28.21 <br>
\hline \& \& \& \& \& \& $4{ }^{\text {" Ice }}$ \& 1.78 \& 1.78 \& 84.01 <br>
\hline \multirow[t]{5}{*}{Pipe Mount 10.5 'x4.5"} \& \multirow[t]{5}{*}{D} \& \multirow[t]{5}{*}{From Leg} \& 2.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{223.50} \& No Ice \& 4.72 \& 4.72 \& 117.80 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 5,62 \& 5.62 \& 150.64 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& 1" Ice \& 6.25 \& 6.25 \& 190.51 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 7.55 \& 7.55 \& 291.92 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 10.27 \& 10.27 \& 585.77 <br>
\hline \multirow[t]{5}{*}{Pipe Mount 6'x $2.375^{\prime \prime}$} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{221.00} \& No Ice \& 1.43 \& 1.43 \& 26.10 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.92 \& 1.92 \& 36.93 <br>
\hline \& \& \& \multirow[t]{8}{*}{0.00} \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.29 \& 2.29 \& 51.81 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.06 \& 3.06 \& 94.38 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 4.70 \& 4.70 \& 234.94 <br>
\hline \multirow[t]{5}{*}{Platform} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{None} \& \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{216.50} \& No Ice \& 25.20 \& 9.45 \& 1050.00 <br>
\hline \& \& \& \& \& \& $1 / 2$ " Ice \& 31.50 \& 11.81 \& 1312.50 <br>
\hline \& \& \& \& \& \& 1" Ice \& 37.80 \& 14.18 \& 1575.00 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 50.40 \& 18.90 \& 2100.00 <br>
\hline \& \& \& \& \& \& $4^{\prime \prime}$ Ice \& 75.60 \& 28.35 \& 3150.00 <br>
\hline \multirow[t]{5}{*}{MTS $10{ }^{\prime}$ Boom Gate} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 0.86 \& \multirow[t]{5}{*}{55.0000} \& \multirow[t]{5}{*}{210.00} \& No Ice \& 15.43 \& 10.89 \& 434.00 <br>
\hline \& \& \& 1.23 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 20.15 \& 15.23 \& 614.25 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& 1" Ice \& 24.87 \& 19.57 \& 794.50 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 34.31 \& 28.25 \& 1154.99 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 53.19 \& 45.61 \& 1875.98 <br>
\hline \multirow[t]{5}{*}{MTS $10{ }^{\text {B }}$ Boom Gate} \& \multirow[t]{5}{*}{D} \& \multirow[t]{5}{*}{From Leg} \& 1.49 \& \multirow[t]{5}{*}{-5.0000} \& \multirow[t]{5}{*}{210.00} \& No Ice \& 15.43 \& 10.89 \& 434.00 <br>
\hline \& \& \& -0.13 \& \& \& 1/2" Ice \& 20.15 \& 15.23 \& 614.25 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& 1" Ice \& 24.87 \& 19.57 \& 794.50 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 34.31 \& 28.25 \& 1154.99 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 53.19 \& 45.61 \& 1875.98 <br>
\hline \multirow[t]{5}{*}{MTS $10^{\prime}$ Boom Gate} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 1.45 \& \multirow[t]{5}{*}{15.0000} \& \multirow[t]{5}{*}{210.00} \& No Ice \& 15.43 \& 10.89 \& 434.00 <br>
\hline \& \& \& 0.39 \& \& \& $1 / 2^{1}$ Ice \& 20.15 \& 15.23 \& 614.25 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& 1"Ice \& 24.87 \& 19.57 \& 794.50 <br>
\hline \& \& \& \& \& \& 2 Ince \& 34.31 \& 28.25 \& 1154.99 <br>
\hline \& \& \& \& \& \& $4^{\prime \prime}$ Ice \& 53.19 \& 45.61 \& 1875.98 <br>
\hline \multirow[t]{5}{*}{MTS $10^{\prime}$ Boom Gate} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 0.86 \& \multirow[t]{5}{*}{55.0000} \& \multirow[t]{5}{*}{205.00} \& No Ice \& 15.43 \& 10.89 \& 434.00 <br>
\hline \& \& \& 1.23 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 20.15 \& 15.23 \& 614.25 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& 1 " Ice \& 24.87 \& 19.57 \& 794.50 <br>
\hline \& \& \& \& \& \& 2 "Ice \& 34.31 \& 28.25 \& 1154.99 <br>
\hline \& \& \& \& \& \& 4 "Ice \& 53.19 \& 45.61 \& 1875.98 <br>
\hline \multirow[t]{5}{*}{MTS 10' Boom Gate} \& \multirow[t]{5}{*}{D} \& \multirow[t]{5}{*}{From Leg} \& 1.49 \& \multirow[t]{5}{*}{-5.0000} \& \multirow[t]{5}{*}{205.00} \& No Ice \& 15.43 \& 10.89 \& 434.00 <br>
\hline \& \& \& -0.13 \& \& \& 1/2" Ice \& 20.15 \& 15.23 \& 614.25 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& 1 I' Ice \& 24.87 \& 19.57 \& 794.50 <br>
\hline \& \& \& \& \& \& 2" Ice \& 34.31 \& 28.25 \& 1154.99 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 53.19 \& 45.61 \& 1875.98 <br>
\hline \multirow[t]{5}{*}{MTS $10{ }^{\prime}$ Boom Gate} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 1.45 \& \multirow[t]{5}{*}{15.0000} \& \multirow[t]{5}{*}{205.00} \& No Ice \& 15.43 \& 10.89 \& 434.00 <br>
\hline \& \& \& 0.39 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 20.15 \& 15.23 \& 614.25 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 24.87 \& 19.57 \& 794.50 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 34.31 \& 28.25 \& 1154.99 <br>
\hline \& \& \& \& \& \& 4 Ice \& 53.19 \& 45.61 \& 1875.98 <br>
\hline \multirow[t]{5}{*}{APX16PV-16PVL w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 1.72 \& \multirow[t]{5}{*}{55.0000} \& \multirow[t]{5}{*}{210.00} \& No Ice \& 6.79 \& 3.05 \& 62.15 <br>
\hline \& \& \& 2.46 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 7.23 \& 3.65 \& 103.99 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 7.68 \& 4.27 \& 154.52 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 8.60 \& 5.55 \& 276.05 <br>
\hline \& \& \& \& \& \& 4" Ice \& 10.54 \& 8.43 \& 626.53 <br>
\hline \multirow[t]{2}{*}{APX16PV-16PVL w/ Mount Pipe} \& \multirow[t]{2}{*}{D} \& \multirow[t]{2}{*}{From Leg} \& 2.99 \& \multirow[t]{2}{*}{$-5.0000$} \& \multirow[t]{2}{*}{210.00} \& No Ice \& 6.79 \& 3.05 \& 62.15 <br>
\hline \& \& \& -0.26 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 7.23 \& 3.65 \& 103.99 <br>
\hline
\end{tabular}



| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | $\begin{aligned} & \text { Offset } \\ & \text { Type } \end{aligned}$ | Offsets: Horz <br> Lateral Vert $f t$ ft $f t$ | Azimuth Adjustment <br> 0 | $f t$ |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $f t^{2}$ | $l b$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| APX16PV-16PVL w/ Mount Pipe | A | From Leg | 0.00 | 15.0000 | 210.00 | 1" Ice | 7.68 | 4.27 | 154.52 |
|  |  |  |  |  |  | 2" Ice | 8.60 | 5.55 | 276.05 |
|  |  |  |  |  |  | 4 " Ice | 10.54 | 8.43 | 626.53 |
|  |  |  | 2.90 |  |  | No Ice | 6.79 | 3.05 | 62.15 |
|  |  |  | 0.78 |  |  | $1 / 2^{\text {n }}$ Ice | 7.23 | 3.65 | 103.99 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 7.68 | 4.27 | 154.52 |
|  | B | From Leg |  | 55.0000 | 210.00 | $2^{\prime \prime}$ Ice | 8.60 | 5.55 | 276.05 |
| ATR 21 B4AB2P w/ Mount Pipe |  |  |  |  |  | 4 " Ice | 10.54 | 8.43 | 626.53 |
|  |  |  | 1.72 |  |  | No Ice | 6.61 | 5.50 | 109.25 |
|  |  |  | 2.46 |  |  | $1 / 2^{\prime \prime}$ Ice | 7.08 | 6.22 | 162.18 |
|  |  |  | 0.00 |  |  | 1 " Ice | 7.55 | 6.95 | 224.58 |
|  | D | From Leg |  | -5.0000 | 210.00 | $2^{\prime \prime}$ Ice | 8.53 | 8.48 | 371.47 |
|  |  |  |  |  |  | $4^{\prime \prime}$ Ice | 10.60 | 11.81 | 780.90 |
| AIR 21 B4AB2P w/ Mount Pipe |  |  | 2.99 |  |  | No Ice | 6.61 | 5.50 | 109.25 |
|  |  |  | -0.26 |  |  | 1/2" Ice | 7.08 | 6.22 | 162.18 |
|  |  |  | 0.00 |  |  | $1{ }^{\text {" }}$ Ice | 7.55 | 6.95 | 224.58 |
|  |  | From Leg |  | 15.0000 |  | $2^{\prime \prime}$ Ice | 8.53 | 8.48 | 371.47 |
|  | A |  |  |  | 210.00 | $4^{\prime \prime}$ Ice | 10.60 | 11.81 | 780.90 |
| AIR 21 B4AB2P w/ Mount Pipe |  |  | 2.90 |  |  | No Ice | 6.61 | 5.50 | 109.25 |
|  |  |  | 0.78 |  |  | 1/2" Ice | 7.08 | 6.22 | 162.18 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 7.55 | 6.95 | 224.58 |
|  | B | From Leg |  | 55.0000 | 205.00 | $2^{\prime \prime}$ Ice | 8.53 | 8.48 | 371.47 |
|  |  |  |  |  |  | 4 " Ice | 10.60 | 11.81 | 780.90 |
| AIR 21 B4AB2P w/ Mount Pipe |  |  | 1.72 |  |  | No Ice | 6.61 | 5.50 | 109.25 |
|  |  |  | 2.46 |  |  | $1 / 2^{\prime \prime}$ Ice | 7.08 | 6.22 | 162.18 |
|  |  |  | 0.00 |  |  | $1^{\prime \prime}$ Ice | 7.55 | 6.95 | 224.58 |
|  | D | From Leg |  | -5.0000 | 205.00 | $2^{\prime \prime}$ Ice | 8.53 | 8.48 | 371.47 |
|  |  |  |  |  |  | 4 " Ice | 10.60 | 11.81 | 780.90 |
| AIR 21 B4AB2P w/ Mount Pipe |  |  |  |  |  | No Ice | 6.61 | 5.50 | 109.25 |
|  |  |  | $-0.26$ |  |  | $1 / 2^{\prime \prime}$ Ice | 7.08 | 6.22 | 162.18 |
|  |  |  | 0.00 |  |  | $1^{\prime \prime}$ Ice | 7.55 | 6.95 | 224.58 |
|  |  | From Leg |  | 15.0000 | 205.00 | $2^{\prime \prime}$ Ice | 8.53 | 8.48 | 371.47 |
|  | A |  |  |  |  | $4^{\prime \prime}$ Ice | 10.60 | 11.81 | 780.90 |
| AIR 21 B4AB2P w/ Mount Pipe |  |  |  |  |  | No Ice | 6.61 | 5.50 | 109.25 |
|  |  |  | 0.78 |  |  | $1 / 2$ Ice | 7.08 | 6.22 | 162.18 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 7.55 | 6.95 | 224.58 |
|  | B | From Leg |  | 55.0000 | 205.00 | 2"Ice | 8.53 | 8.48 | 371.47 |
|  |  |  |  |  |  | 4 " Ice | 10.60 | 11.81 | 780.90 |
| ATMAA1412D-1A20 |  |  |  |  |  | No Ice | 1.17 | 0.47 | 13.00 |
|  |  |  | 2.46 |  |  | $1 / 2^{\prime \prime}$ Ice | 1.31 | 0.57 | 20.62 |
|  |  |  | 0.00 |  |  | 1 I' Ice | 1.47 | 0.69 | 30.11 |
|  | D | From Leg |  | -5.0000 | 205.00 | $2^{\prime \prime}$ Ice | 1.81 | 0.95 | 55.52 |
|  |  |  |  |  |  | $4^{\prime \prime}$ Ice | 2.58 | 1.57 | 137.44 |
| ATMAA1412D-1A20 |  |  | 2.99 |  |  | No Ice | 1.17 | 0.47 | 13.00 |
|  |  |  | -0.26 |  |  | $1 / 2^{11}$ Ice | 1.31 | 0.57 | 20.62 |
|  |  |  | 0.00 |  |  | $1^{\prime \prime}$ Ice | 1.47 | 0.69 | 30.11 |
|  | A | From Leg |  | 15.0000 |  | $2^{\prime \prime}$ Ice | 1.81 | 0.95 | 55.52 |
|  |  |  |  |  | 205.00 | 4 " Ice | 2.58 | 1.57 | 137.44 |
| ATMAA1412D-1A20 |  |  | 2.90 |  |  | No Ice | 1.17 | 0.47 | 13.00 |
|  |  |  | 0.78 |  |  | 1/2" Ice | 1.31 | 0.57 | 20.62 |
|  |  |  | 0.00 |  |  | 1 " Ice | 1.47 | 0.69 | 30.11 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 1.81 | 0.95 | 55.52 |
|  |  | From Leg |  |  |  | 4 " Ice | 2.58 | 1.57 | 137.44 |
| 2' Sidearm - Flat (GPD) | A |  | 1.00 | 0.0000 | 132.00 | No Ice | 0.80 | 1.60 | 31.31 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ Ice | 1.05 | 2.00 | 39.47 |
|  |  |  | 0.00 |  |  | 1" Ice | 1.30 | 2.40 | 47.63 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 1.80 | 3.20 | 63.95 |


| tnxTower | SNET026 STAMFORD CO |  | $\begin{aligned} & \text { Page } 6 \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Ste 2531 <br> Akron, OH <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2012814.17 Rev. 1 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:32:08 } 02 / 28 / 13 \end{array}$ |
|  | Client | HPC Development | Designed by tclark |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \[
\begin{gathered}
\text { Offsets: } \\
\text { Horz } \\
\text { Lateral } \\
\text { Vert } \\
f t \\
f t \\
f t \\
\hline
\end{gathered}
\] \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) \\
Front \\
\(f t^{2}\)
\end{tabular} \& \(C_{A} A_{A}\)
Side \& Weight

$l b$ <br>
\hline \multirow{6}{*}{4' Yagi} \& \multirow{6}{*}{A} \& \multirow{6}{*}{From Leg} \& \& \multirow{6}{*}{0.0000} \& \multirow{6}{*}{132.00} \& 4"Ice \& 2.80 \& 4.80 \& 96.59 <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 0.79 \& 0.79 \& 5.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2' Ice \& 1.03 \& 1.03 \& 11.34 <br>
\hline \& \& \& 0.00 \& \& \& 1 " Ice \& 1.28 \& 1.28 \& 20.48 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 1.81 \& 1.81 \& 47.76 <br>
\hline \& \& \& \& \& \& $4^{\prime \prime}$ Ice \& 3.11 \& 3.11 \& 142.65 <br>
\hline
\end{tabular}

## Dishes

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face or \\
Leg
\end{tabular} \& \begin{tabular}{l}
Dish \\
Type
\end{tabular} \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
ft
\end{tabular} \& Azimuth Adjustment \& \begin{tabular}{l}
\(3 d B\) \\
Beam \\
Width
\end{tabular} \& Elevation

$f t$ \& | Outside |
| :--- |
| Diameter |
| ft | \& \& Aperture Area

$$
f t^{2}
$$ \& Weight

$l b$ <br>
\hline 10' HP Dish \& D \& Paraboloid w/Shroud (HP) \& From \& 4.00 \& 0.0000 \& \& 223.50 \& 10.00 \& No Ice \& 78.54 \& 320.00 <br>
\hline \& \& \& Leg \& 0.00 \& \& \& \& \& 1/2" Ice \& 79.85 \& 730.00 <br>
\hline \& \& \& \& 0.00 \& \& \& \& \& 1 " Ice \& 81.17 \& 1140.00 <br>
\hline \& \& \& \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 83.80 \& 1960.00 <br>
\hline \& \& \& \& \& \& \& \& \& 4" Ice \& 89.06 \& 3590.00 <br>
\hline 1' MW \& C \& Paraboloid w/Shroud (HP) \& From \& 4.00 \& 0.0000 \& \& 221.00 \& 1.00 \& No Ice \& 0.79 \& 30.00 <br>
\hline \& \& \& Leg \& 0.00 \& \& \& \& \& 1/2" Ice \& 0.92 \& 30.00 <br>
\hline \& \& \& \& 0.00 \& \& \& \& \& $1^{\prime \prime}$ Ice \& 1.06 \& 40.00 <br>
\hline \& \& \& \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 1.33 \& 50.00 <br>
\hline \& \& \& \& \& \& \& \& \& $4^{\prime \prime}$ Ice \& 1.88 \& 70.00 <br>
\hline
\end{tabular}

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation <br> $f_{t}$ | Appurtenance | Gov. <br> Load <br> Comb. | Deflection <br> in | Tilt | Twist $=$ | Radius of Curvature $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 234.00 | Top Platform | 20 | 2.032 | 0.1296 | 0.0364 | 154780 |
| 223.50 | 10' HP Dish | 20 | 1.819 | 0.1269 | 0.0355 | 133644 |
| 221.00 | 1' MW | 20 | 1.754 | 0.1251 | 0.0348 | 172199 |
| 216.50 | Platform | 20 | 1.635 | 0.1222 | 0.0323 | 174115 |
| 210.00 | MTS 10' Boom Gate | 20 | 1.465 | 0.1182 | 0.0282 | 88494 |
| 205.00 | MTS 10' Boom Gate | 20 | 1.337 | 0.1140 | 0.0256 | 71142 |
| 132.00 | 2' Sidearm - Flat (GPD) | 20 | 0.103 | 0.0286 | 0.0059 | 40642 |

Bolt Design Data

| Section No. | Elevation <br> $f t$ | Component Type | Bolt Grade | Bolt Size $\dot{m}$ | Number Of Bolts | Maximum <br> Load per Bolt lb | Allowable Load $l b$ | Ratio <br> Load <br> Allowable | Allowable Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TI | 231.5 | Diagonal | A325N | 0.7500 | 2 | 977.63 | 13956.30 | $\begin{aligned} & 0.070 \\ & 0.025 \end{aligned}$ | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.7500 | 2 | 229.23 | 9277.52 |  | 1.333 | Bolt Shear |



| Section No. | $f t$ | Component Type | Bolt Grade | in | Of Bolts | Maximum Load per Bolt $l b$ | $\begin{gathered} \text { Load } \\ l b \end{gathered}$ | Ratio <br> Load <br> Allowable | Allowable Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T2 | 227.333 | Diagonal | A325N | 0.7500 | 2 | 1285.97 | 13956.30 | 0.092 | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.7500 | 2 | 125.37 | 6978.13 | 0.018 | 1.333 | Member Block Shear |
| T3 | 223.167 | Leg | A325N | 0.7500 | 8 | 3023.42 | 18555.00 | 0.163 | 1.333 | Bolt DS |
|  |  | Diagonal | A 325 N | 0.7500 | 2 | 1970.94 | 13956.30 | 0.141 | 1.333 | Member Block Shear |
| T4 | 219 | Diagonal | A325N | 0.7500 | 2 | 1968.49 | 6978.13 | 0.282 | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.7500 | 2 | 322.35 | 9277.52 | , | 1.333 | Bolt Shear |
| T5 | 214.2 | Diagonal | A325N | 0.7500 | 2 | 2554.81 | 6978.13 | 0.366 | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.7500 | 2 | 328.22 | 6978.13 | 0.047 | 1.333 | Member Block Shear |
| T6 | 204.6 | Leg | A 325 N | 0.7500 | 12 | 8209.69 | 18555.00 | 0.442 | 1.333 | Bolt DS |
|  |  | Diagonal | A325N | 0.7500 | 2 | 2842.74 | 6978.13 | 0.407 | 1.333 | Member Block Shear |
|  |  | Top Girt | A 325 N | 0.7500 | 2 | 264.83 | 6978.13 | 0.038 | 1.333 | Member Block Shear |
| T7 | 195 | Diagonal | A 325 N | 0.7500 | 2 | 4152.57 | 7431.25 | 0.559 | 1.333 | Member Block Shear |
|  |  | Secondary Horizontal | A325N | 0.7500 | 2 | 441.84 | 6978.13 | 0.063 | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.7500 | 2 | 1087.80 | 6978.13 | 0.156 | 1.333 | Member Block Shear |
| T8 | 185 | Leg | A325N | 0.7500 | 16 | 9306.44 | 18555.00 | 0.502 | 1.333 | Bolt DS |
|  |  | Diagonal | A325N | 0.7500 | 2 | 4217.41 | 7431.25 | 0.568 | 1.333 | Member Block Shear |
|  |  | Secondary Horizontal | A 325 N | 0.7500 | 2 | 567.37 | 6978.13 | 0.568 | 1.333 | Member Block Shear |
|  |  | Top Girt | A 325 N | 0.7500 | 2 | 2100.78 | 6978.13 | , | 1.333 | Member Block Shear |
| T9 | 175 | Diagonal | A 325 N | 0.7500 | 2 | 4315.30 | 7431.25 | 0.581 | 1.333 | Member Block Shear |
|  |  | Secondary Horizontal | A.325N | 0.7500 | 2 | 689.48 | 5233.59 | 0.132 | 1.333 | Member Block Shear |
|  | 165 | Top Girt | A325N | 0.7500 | 2 | 2337.76 | 6978.13 |  | 1.333 | Member Block Shear |
| T10 |  | Leg | A325N | 0.7500 | 20 | 10688.60 | 18555.00 | 0.576 | 1.333 | Bolt DS |
|  |  | Diagonal | A325N | 0.7500 | 2 | 4457.01 | 7431.25 | $0.600$ | 1.333 | Member Block Shear |
|  |  | Secondary Horizontal | A 325 N | 0.7500 | 2 | 809.84 | 6978.13 |  | 1.333 | Member Block Shear |
|  | 155 | Top Girt | A 325 N | 0.7500 | 2 | 2612.99 | 6978.13 | 0.374 | 1.333 | Member Block Shear |
| T11 |  | Diagonal | A 325 N | 0.7500 | 2 | 4294.02 | 7431.25 | 0.578 | 1.333 | Member Block Shear |
|  |  | Secondary Horizontal | A325N | 0.7500 | 2 | 940.01 | 6978.13 | 0.135 | 1.333 | Member Block Shear |
|  | 145 | Top Girt | A325N | 0.7500 | 2 | 2495.87 | 6978.13 | 0.358 | 1.333 | Member Block Shear |
| T12 |  | Leg | A325N | 0.7500 | 20 | 13913.40 | 18555.00 | 0.750 | 1.333 | Bolt DS |
|  |  | Diagonal | A325N | 0.7500 | 2 | 4660.38 | 7431.25 | 0.627 | 1.333 | Member Block Shear |
|  |  | Secondary Horizontal | A325N | 0.7500 | 2 | 1051.26 | 6978.13 | 0.151 / | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.7500 | 2 | 2611.77 | 6978.13 | 0374 | 1.333 | Member Block Shear |
| T13 | 135 | Diagonal | A325N | 0.7500 | 2 | 7736.68 | 13956.30 | 0.554 | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.7500 | 2 | 3750.02 | 13956.30 | 0.260 | 1.333 | Member Block Shear |
| T14 | 120.75 | Leg | A325N | 0.7500 | 28 | 11365.80 | 18555.00 | 0.613 | 1.333 | Bolt DS |
|  |  | Diagonal | A325N | 0.7500 | 2 | 9601.48 | 13956.30 | 88 | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.7500 | 2 | 4204.50 | 13956.30 | 0.301 | 1.333 | Member Block Shear |


| tnxTower | SNET026 STAMFORD CO |  | $\text { Page } \quad 8 \text { of } 9$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Ste 2531 <br> Akron, OH <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2012814.17 Rev. 1 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:32:08 02/28/13 } \end{array}$ |
|  | Client | HPC Development | Designed by tclark |


| Section Capacity Table |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation $f t$ | Component Type | Size | Critical Element | $\begin{aligned} & \hline P \\ & l b \end{aligned}$ | $\begin{aligned} & S F * P_{\text {allow }} \\ & \quad l b \end{aligned}$ | $\begin{gathered} \% \\ \text { Capacity } \end{gathered}$ | $\begin{aligned} & \hline \text { Pass } \\ & \text { Fail } \end{aligned}$ |
| T1 | 231.5-227.333 | Leg | L $4 \times 4 \times 3 / 8$ | 4 | -4061.02 | 65166.90 | 6.2 | Pass |
| T2 | 227.333-223.167 | Leg | L4x4x3/8 | 17 | -8371.42 | 65166.90 | 12.8 | Pass |
| T3 | 223.167-219 | Leg | L4x4x3/8 | 33 | -12093.70 | 65166.90 | 18.6 | Pass |
| T4 | 219-214.2 | Leg | L5x5x1/2 | 45 | -17585.50 | 111164.33 | 15.8 | Pass |
| T5 | 214.2-204.6 | Leg | L5 $5 \times 5 \times 1 / 2$ | 63 | -32176.40 | 111165.67 | 28.9 | Pass |
| T6 | 204.6-195 | Leg | L5 $55 \times 1 / 2$ | 87 | -49258.10 | 111165.00 | 44.3 | Pass |
| T7 | 195-185 | Leg | L6x6x5/8 | 111 | -57658.40 | 171154.53 | 33.7 | Pass |
| T8 | 185-175 | Leg | L6x6x5/8 | 136 | -74451.50 | 171325.15 | 43.5 | Pass |
| T9 | 175-165 | Leg | L6x6x5/8 | 161 | -90790.50 | 171469.11 | 52.9 | Pass |
| T10 | 165-155 | Leg | L6x6x5/8 | 186 | -106886.00 | 171593.08 | 62.3 | Pass |
| T11 | 155-145 | Leg | L6x6x $3 / 4$ | 211 | -124276.00 | 203401.13 | 61.1 | Pass |
| T12 | 145-135 | Leg | L6x6x3/4 | 236 | -139134.00 | 203418.46 | 68.4 | Pass |
| T13 | 135-120.75 | Leg | L6x6x7/8 | 261 | -150312.00 | 208794.45 | 72.0 | Pass |
| T14 | 120.75-106.5 | Leg | L6x6x7/8 | 298 | -159121.00 | 208789.11 | 76.2 | Pass |
| T1 | 231.5-227.333 | Diagonal | $2 \mathrm{~L} 21 / 2 \times 2 \times 1 / 4 \times 3 / 8$ | 15 | -2372.16 | 38732.05 | 6.1 | Pass |
| T2 | 227.333-223.167 | Diagonal | 2L2 1/2×2×1/4×3/8 | 31 | -2465.15 | 38732.05 | 6.4 | Pass |
| T3 | 223.167-219 | Diagonal | 2L2 1/2×2×1/4×3/8 | 44 | -4095.49 | 38732.05 | 10.6 | Pass |
| T4 | 219-214.2 | Diagonal | L2 $1 / 2 \times 2 \times 1 / 4$ | 60 | -4133.10 | 17013.61 | 24.3 | Pass |
| T5 | 214.2-204.6 | Diagonal | L2 $1 / 2 \times 2 \times 1 / 4$ | 76 | -5225.57 | 15959.88 | 32.7 | Pass |
| T6 | 204.6-195 | Diagonal | L2 $1 / 2 \times 2 \times 1 / 4$ | 100 | -5648.43 | 14807.76 | 38.1 | Pass |
| T7 | 195-185 | Diagonal | 13x3x1/4 | 123 | -8962.92 | 17803.15 | 50.3 | Pass |
| T8 | 185-175 | Diagonal | L3x3x1/4 | 148 | -9070.10 | 16942.56 | 53.5 | Pass |
| T9 | 175-165 | Diagonal | L3x3x1/4 | 173 | -9286.51 | 16089.84 | 57.7 | Pass |
| T10 | 165-155 | Diagonal | L3x3x1/4 | 203 | -9598.53 | 15257.52 | 62.9 | Pass |
| T11 | 155-145 | Diagonal | L3x3x1/4 | 223 | -9119.50 | 14479.58 | 63.0 | Pass |
| T12 | 145-135 | Diagonal | L3x3x1/4 | 253 | -10047.20 | 13668.05 | 73.5 | Pass |
| T13 | 135-120.75 | Diagonal | 2L2 1/2×2 1/2x1/4×3/8 | 293 | -15804.00 | 19482.46 | 81.1 | Pass |
| T14 | 120.75-106.5 | Diagonal | 2L2 1/2×2 1/2x1/4×3/4 | 330 | -21092.60 | 22488.51 | 93.8 | Pass |
| T7 | 195-185 | Secondary Horizontal | L2 $1 / 2 \times 2 \times 1 / 4$ | 132 | -883.68 | 6918.08 | 12.8 | Pass |
| T8 | 185-175 | Secondary Horizontal | L2 $1 / 2 \times 2 \times 1 / 4$ | 157 | -1134.74 | 5934.57 | 19.1 | Pass |
| T9 | 175-165 | Secondary Horizontal | L2 $1 / 2 \times 2 \times 3 / 16$ | 182 | -1378.97 | 3984.27 | 34.6 | Pass |
| T10 | 165-155 | Secondary Horizontal | L2 $1 / 2 \times 21 / 2 \times 1 / 4$ | 207 | -1619.68 | 6593.58 | 24.6 | Pass |
| T11 | 155-145 | Secondary Horizontal | L2 1/2×2×1/4 | 232 | -1880.02 | 4017.26 | 46.8 | Pass |
| T12 | 145-135 | Secondary Horizontal | L2 1/2 $\times 2 \times 1 / 4$ | 257 | -2102.52 | 3586.72 | 58.6 | Pass |
| T1 | 231.5-227.333 | Top Girt | C8x11.5 | 6 | -278.47 | 43272.78 | 0.6 | Pass |
| T2 | 227.333-223.167 | Top Girt | L2 1/2x2 1/2x1/4 | 24 | 207.32 | 21124.70 | 1.0 | Pass |
| T4 | 219-214.2 | Top Girt | C789.8 | 50 | -490.32 | 41637.85 | 1.2 | Pass |
| T5 | 214.2-204.6 | Top Girt | L2 $1 / 2 \times 2 \times 1 / 4$ | 66 | -502.36 | 10501.27 | 4.8 | Pass |
| T6 | 204.6-195 | Top Girt | L2 1/2×2 $1 / 2 \times 1 / 4$ | 90 | -439.35 | 12279.94 | 3.6 | Pass |
| T7 | 195-185 | Top Girt | L2 1/2x2 $1 / 2 \times 1 / 4$ | 114 | -1806.93 | 20213.21 | 8.9 | Pass |
| T8 | 185-175 | Top Girt | L2 1/2×2 $1 / 2 \times 1 / 4$ | 138 | -3479.62 | 19322.23 | 18.0 | Pass |
| T9 | 175-165 | Top Girt | L2 1/2x2 $1 / 2 \times 1 / 4$ | 166 | -3934.02 | 18407.13 | 21.4 | Pass |
| T10 | 165-155 | Top Girt | L2 1/2x2 $1 / 2 \times 1 / 4$ | 191 | -4433.15 | 17467.10 | 25.4 | Pass |
| T11 | 155-145 | Top Girt | L2 1/2×2 1/2x1/4 | 216 | -4250.75 | 16501.47 | 25.8 | Pass |
| T12 | 145-135 | Top Girt | L2 1/2x2 1/2x1/4 | 241 | -4466.43 | 15107.16 | 29.6 | Pass |
| T13 | 135-120.75 | Top Girt | 2L2 $1 / 2 \times 21 / 2 \times 1 / 4 \times 3 / 8$ | 266 | -7043.55 | 39825.64 | 17.7 | Pass |
| T14 | 120.75-106.5 | Top Girt | 2L2 1/2x2 1/2x1/4×3/4 | 303 | -7827.10 | 41573.20 | 18.8 | Pass |
| T13 | 135-120.75 | Redund Horz 1 Bracing | L2 1/2x2 $\times 3 / 16$ | 282 | -2256.78 | 13910.65 | 16.2 | Pass |
| T14 | 120.75-106.5 | Redund Horz 1 Bracing | L2 1/2×2 $\times 3 / 16$ | 320 | -2388.71 | 15539.98 | 15.4 | Pass |
| T13 | 135-120.75 | Redund Diag 1 Bracing | L2 1/2×2×3/16 | 283 | -2967.80 | 3527.66 | 84.1 | Pass |
| T14 | 120.75-106.5 | Redund Diag 1 Bracing | L2 1/2×2 $\times 3 / 16$ | 321 | -9783.11 | 12864.85 | 76.0 | Pass |
| T14 | 120.75-106.5 | Redund Sub Horz Bracing | 2L2 1/2×2 1/2x1/4×3/8 | 322 | -7868.03 | 38538.23 | 20.4 | Pass |
| T7 | 195-185 | Inner Bracing | L2 1/2×2 $1 / 2 \times 3 / 16$ | 121 | -29.73 | 5721.66 | 0.5 | Pass |
| T8 | 185-175 | Inner Bracing | L2 1/2x2 1/2x3/16 | 146 | -57.41 | 4755.04 | 1.2 | Pass |
| T9 | 175-165 | Inner Bracing | L2 1/2×2 1/2×3/16 | 171 | -64.30 | 4014.29 | 1.6 | Pass |
| T10 | 165-155 | Inner Bracing | L2 1/2×2 1/2×3/16 | 196 | -72.03 | 3434.01 | 2.1 | Pass |
| T11 | 155-145 | Inner Bracing | L2×2 1/2x3/16 | 221 | -68.87 | 1982.86 | 3.5 | Pass |


| tnxTower | SNET026 STAMFORD CO |  | $\begin{aligned} & \text { Page } \\ & \\ & 9 \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Ste 2531 | Project | 2012814.17 Rev. 1 | Date 14:32:08 02/28/13 |
| Akron, OH Phone: (330) 572-2100 FAX: (330) 572-2101 | Client | HPC Development | Designed by tclark |


| Section No. | Elevation $f t$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} S F^{*} P_{\text {allow }} \\ l b \end{gathered}$ | \% Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T12 | 145-135 | Inner Bracing | L2×2 1/2×3/16 | 246 | -72.16 | 1737.39 | 4.2 | Pass |
| T13 | 135-120.75 | Inner Bracing | L3x3x3/16 | 271 | -109.91 | 4003.45 | 2.7 | Pass |
| T14 | 120.75-106.5 | Inner Bracing | L3 $\times 3 \times 3 / 16$ | 308 | -122.48 | 3391.46 | 3.6 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Leg (T14) | 76.2 | Pass |
|  |  |  |  |  |  | Diagonal (T14) | 93.8 | Pass |
|  |  |  |  |  |  | Secondary Horizontal (T12) | 58.6 | Pass |
|  |  |  |  |  |  | Top Girt (T12) | 29.6 | Pass |
|  |  |  |  |  |  | Redund Horz 1 Bracing (T13) | 16.2 | Pass |
|  |  |  |  |  |  | Redund Diag 1 Bracing (T13) | 84.1 | Pass |
|  |  |  |  |  |  | Redund Sub Horz Bracing (T14) | 20.4 | Pass |
|  |  |  |  |  |  | Inner Bracing (T12) | 4.2 | Pass |
|  |  |  |  |  |  | Bolt Checks | 56.3 | Pass |
|  |  |  |  |  |  | RATING = | 93.8 | Pass |

## APPENDIX C

Tower Elevation Drawing



Feedline Distribution Chart
$\qquad$ Round $\qquad$ Flat $\qquad$ App In Face $\qquad$ App Out Face $\qquad$ Truss Leg


|  | GPD Group <br> 520 South Main Street, Ste 2531 <br> Akron, OH <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | 1ob: SNET026 STAMFORD CO |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  | Client: HPC Development | : tclark | App'd: |
|  |  | Code: TIA/EIA-222-F | Date: | Scale: NTS |
|  |  |  |  | No. |

## Feedline Plan

$\qquad$ Round $\qquad$ Flat $\qquad$ App In Face $\qquad$ App Out Face


Iob: SNET026 STAMFORD CO Project: 2012814.17



# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

T-Mobile Existing Facility

> Site ID: CT11410A

Stamford Downtown
555 Main Street
Stamford, CT 06901
August 14, 2012

August 14, 2012

T-Mobile USA
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, CT 06002

Re: Emissions Values for Site CT11410A - Stamford Downtown

EBI Consulting was directed to analyze the proposed T-Mobile facility located at 555 Main Street, Stamford, CT, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm} 2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR $1.1307(b)(1)-(b)(3)$, to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter $(\mu \mathrm{W} / \mathrm{cm} 2)$. The general population exposure limit for the cellular band is $567 \mu \mathrm{~W} / \mathrm{cm} 2$, and the general population exposure limit for the PCS band is $1000 \mu \mathrm{~W} / \mathrm{cm} 2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 555 Main Street, Stamford, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, the actual antenna pattern gain value in the direction of the sample area was used. For this report the sample point is a 6 foot person standing at the base of the tower

For all calculations, all equipment was calculated using the following assumptions:

1) 2 GSM channels ( 1940.000 MHz -to 1950.000 MHz ) were considered for each sector of the proposed installation.
2) 2 UMTS channels ( 2110.000 MHz to $2120.000 \mathrm{MHz} / 2140.000 \mathrm{MHz}$ to 2145.000 MHz ) were considered for each sector of the proposed installation
3) 2 LTE channels ( 2110.000 MHz to $2120.000 \mathrm{MHz} / 2140.000 \mathrm{MHz}$ to 2145.000 MHz ) were considered for each sector of the proposed installation
4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The actual gain in this direction was used per the manufactures supplied specifications.
6) The antenna used in this modeling is the Ericsson AIR21 for LTE, UMTS and GSM. This is based on feedback from the carrier with regards to anticipated antenna selection. This antenna has a 15.6 dBd gain value at its main lobe. Actual antenna gain values were used for all calculations as per the manufacturers specifications
7) The antenna mounting height centerlines of the proposed antennas are 210.83 feet and 205.83 feet above ground level (AGL)
8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits


| Sector 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Number | Antenna Make | Antenna Model | Status | Frequency Band | Technology | Power Out Per Channel (Watts) | Number of Channels | Composite Power | Antenna Gain In direction of sample point (dBd) | Antenna Height ( ft ) | analysis height | Cable Size | $\begin{gathered} \text { Cable Loss } \\ \text { (dB) } \\ \hline \end{gathered}$ | Additlonal Loss | ERP | Power <br> Density <br> Value | Power Density Percentage |
| 1a | Ericsson | AIR21 B4A/B2P | Active | AWS-2100 MHz | LTE | 60 | 2 | 120 | -3,95 | 210 | 204 | None | , | , | 48.326044 | 0.417472 | 0.04175\% |
| 1 b | Ericsson | AlR21 $184 \mathrm{~A} / \mathrm{B2P}$ | Not Used | - | - |  |  | 0 | -3.95 | 210 | 204 | None | 0 | 0 | 0 | 0 | 0.00000\% |
| 2 a | Ericsson | AlR21 B2A/ $/$ 4P | Active | PCS - 1950 MHz | GSM / UMTS | 30 | 2 | 60 | -3.95 | 205 | 199 | 1-5/8 ${ }^{\text {" }}$ | 0 | 0 | 24.163022 | 0.219357 | 0.02194\% |
| 2 B | Ericsson | AlR21 B2A / B4P | Passive | AWS -2100 MHz | UMTS | 30 | 2 | 60 | -3.95 | 205 | 199 | 1-5/8" | 0 | 0 | 24.163022 | 0.219357 | 0.02194\% |
| Sector total Power Density Value: $\quad 0.086 \%$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Sector 2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Antenna Number | Antenna Make | Antenna Model | Status | Frequency Band | Technology | Power Out Per Channel (Watts) | Number of Channels | Composite Power | Antenna Gain in direction of sample point (dBd) | Antenлa Height (ft) | analysis helght | Cable Size | $\begin{gathered} \text { Cable Loss } \\ (\mathrm{dB}) \\ \hline \end{gathered}$ | Additional Loss | ERP | Power Density Value | Power Density Percentage |
| 1 a | Ericsson | AlR21 B4A/B2P | Active | AWS - 2100 MHz | LTE | 60 | 2 | 120 | -3.95 | 21. | 204 | None | 0 | 0 | 48.326044 | 0.417472 | 0.04175\% |
| 1 b | Ericsson | AIR21 B4A/B2P | Not Used | $\cdots$ | - |  |  | 0 | -3.95 | 210 | 204 | None | 0 | 0 | , | 0 | 0,00000\% |
| 2a | Ericsson | AlR21 B2A / B4P | Active | PCS - 1950 MHz | GSM / UMTS | 30 | 2 | 60 | -3.95 | 205 | 199 | 1-5/8 ${ }^{\text {n }}$ | 0 | 0 | 24.1.63022 | 0.219357 | 0.02194\% |
| 28 | Ericsson | AIR21 B2A / B4P | Passive | AWS - 21.00 MHz | UMTS | 30 | 2 | 60 | -3.95 | 205 | 199 | 1-5/8 ${ }^{\text {n }}$ | 0 | 0 | 24.163022 | 0.219357 | 0.02194\% |
| Sector total Power Density Value: $\quad 0.086 \%$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Sector 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Anterina Number | Antenna Make | Antenna Model | Status | Frequency Band | Technology | Power Out Per Channe! (Watts) | Number of Channels | Composite | Antenna Gain in direction of sample point (dBd) | $\begin{array}{\|c\|} \hline \text { Antenna } \\ \text { Height (ft) } \end{array}$ | analysis height | Cable Stze | $\begin{gathered} \text { Cable Los5 } \\ (\mathrm{dB}) \end{gathered}$ | $\begin{gathered} \text { Additlonal } \\ \text { Loss } \end{gathered}$ | ERP | Power Density Value | Power Denslty Percentage |
| 12 | Ericsson | AIR21 B4A/B2P | Active | AWS - 2100 MHz | LTE | 60 | 2 | 120 | -3.95 | 210 | 204 | None | , | 0 | 48.326044 | 0.417472 | 0.04175\% |
| 1 b | Ericsson | AIR21 B4A/B2P | Not Used | - . | - |  |  | 0 | -3.95 | 210 | 204 | None | 0 | 0 | 0 | 0 | 0.00000\% |
| 2a | Ericsson | AlR21 B2A/B4P | Active | PCS - 1950 MHz | GSM / UMTS | 30 | 2 | 60 | -3.95 | 205 | 199 | 1-5/8" | 0 | 0 | 24.163022 | 0.219357 | 0.02194\% |
| 28 | Ericsson | AlR21. B2A / B4P | Passive | AWS - 2100 MHz | UMTS | 30 | 2 | 60 | -3.95 | 205 | 199 | 1-5/8" | 0 | 0 | 24.163022 | 0.219357 | 0.02194\% |
|  |  |  |  |  |  |  |  |  |  |  |  | Sector tot | tal Power De | ensity Value: | 0.086\% |  |  |



## Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public exposure to RF Emissions.

The anticipated Maximum Composite contributions from the T-Mobile facility are $\mathbf{0 . 2 5 7 \%}$ ( $\mathbf{0 . 0 8 6 \%}$ from each sector) of the allowable FCC established general public limit considering all three sectors simultaneously.

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{1 1 . 4 5 7} \%$ of the allowable FCC established general public limit. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were within the allowable $100 \%$ threshold standard per the federal government


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