### ROBINSON & COLE

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts

May 12, 2014

Melanie A. Bachman Acting Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Re: Notice of Exempt Modification – Facility Modification 69 Guinea Road, Stamford, Connecticut

Dear Ms. Bachman:

Cellco Partnership d/b/a Verizon Wireless ("Cellco") currently maintains twelve (12) antennas at the 142-foot level of the existing 160-foot tower at 69 Guinea Road in Stamford, Connecticut (the "Property"). The tower is owned by Crown Castle. The Council approved Cellco's use of this tower in 1998 (Docket No. 180). Cellco now intends to modify its facility by adding three (3) model MGD3-800TX, 2100 MHz antennas, for a total of fifteen (15) antennas, all at the same 142-foot level on the tower. Cellco also intends to install three (3) remote radio heads ("RRHs") behind its 2100 MHz antennas and one (1) HYBRIFLEX<sup>TM</sup> antenna cable attached to the outside the monopole. Included in <u>Attachment 1</u> are specifications for Cellco's replacement antennas, RRHs and HYBRIFLEX<sup>TM</sup> cable.

Please accept this letter as notification pursuant to R.C.S.A. § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to David Martin, Mayor for the City of Stamford. A copy of this letter is also being sent to Global Signal Acquisitions IV LLC, the owner of the Property.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).



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12897851-v1

### ROBINSON & COLELLP

Melanie A. Bachman May 12, 2014 Page 2

- 1. The proposed modifications will not result in an increase in the height of the existing tower. Cellco's additional three (3) antennas and RRHs will be located at the 142-foot level on the 160-foot tower.
- 2. The proposed modifications will not involve any change to ground-mounted equipment and, therefore, will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. A cumulative General Power Density table for Cellco's modified facility is included in <a href="https://example.com/Attachment-2">Attachment 2</a>.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The tower and its foundation, with certain modifications, can support Cellco's proposed modifications. (*See* Structural Modification Report included in Attachment 3).

For the foregoing reasons, Cellco respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Kenneth C. Baldwin

Enclosures Copy to:

David Martin, Stamford Mayor Global Signal Acquisitions IV LLC Sandy M. Carter



# **ATTACHMENT 1**



# SINGLE-BAND PANEL ANTENNA

BROADBAND 1700-2170 MHZ

## **MGD3-800TX**

1710-1880	1850-1990	1920-2170
H66° V7.2°	H64º V6.6º	H63º V6.3º
Fixed Tilt	Fixed Tilt	Fixed Tilt

#### **ELECTRICAL SPECIFICATIONS**

#### BROADBAND 1710-2170 MHz

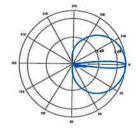
Antenna Model		MGD3-800TX	
Polarization		± 450	
Frequency	1710 - 1880	1850 - 1990	1920 - 2170
Horizontal Beamwidth	66°	640	630
Vertical Beamwidth	7.20	6.60	6.30
Gain (dBi)	17.9	18	18.5
Vertical Electrical Tilt	FIXED 0°, 2°, 4°, 6°	FIXED 0°, 2°, 4°, 6°	FIXED 0°, 2°, 4°, 6°
Upper Sidelobe Suppression for the 1 <sup>st</sup> lobe above main beam (dB)	20	20	20
Front-to-Back Ratio /Cpol @ ± 20° (dB)	> 30	> 30	> 30
VSWR	< 1.4 : 1	< 1.4 : 1	< 1.4 : 1
Cross Polar Ratio @ ± 60° (dB)	> 10	> 10	> 10
Isolation Between Ports (dB)	> 30	> 30	> 30
Maximum Power Per Input (W)		250	- 30
ntermodulation (dBc)		< - 150	
mpedance (Ω)	50		



Connectors	2 X 7/16 Female
Connector Position	Bottom
Survival Wind Speed mph (km/h)	124 (200)
Front Windload lbs (N) @ 160 km/h	83 (370)
Lateral Windload lbs (N) @ 160 km/h	38 (170)
Radome Color	Grey, paintable
Temperature Range F (°C)	-67° to 140° (-55° to +60°)
Humidity	100%
Antenna Weight Ibs (kg)	15.43 (7)
Antenna Dimension in (mm) H X W X D	53 X 6.29 X 3.54 (1340 X 160 X 90)



H&V Pattern



RYMSA Telecom Group (Headquarters)

de





### Alcatel-Lucent RRH2x40-AWS

REMOTE RADIO HEAD

The Alcatel-Lucent RRH2x40-AWS is a high-power, small form-factor Remote Radio Head (RRH) operating in the AWS frequency band (1700/2100MHz - 3GPP Band 4). The Alcatel-Lucent RRH2x40-AWS is designed with an eco-efficient approach, providing operators with the means to achieve high quality and capacity coverage with minimum site requirements.



A distributed eNodeB expands deployment options by using two components, a Base Band Unit (BBU) containing the digital assets and a separate RRH containing the radiofrequency (RF) elements. This modular design optimizes available space and allows the main components of an eNodeB to be installed separately, within the same site or several kilometres apart.

The Alcatel-Lucent RRH2x40-AWS is linked to the BBU by an optical-fiber connection carrying downlink and uplink digital radio signals along with operations, administration and maintenance (OA&M) information. The Alcatel-Lucent RRH2x40-AWS has two transmit RF paths, 40 W RF output power per transmit path, and is designed to manage up to four-way receive diversity. The device is ideally suited to support macro coverage, with multiple-input multiple-output (MIMO) 2x2 operation in up to 20 MHz of bandwidth.

The Alcatel-Lucent RRH2x40-AWS is designed to make available all the benefits of a distributed eNodeB, with excellent RF characteristics, with low

capital expenditures (CAPEX) and low operating expenditures (OPEX). The limited space available in some sites may prevent the installation of traditional single-cabinet BTS equipment or require costly cranes to be employed, leaving coverage holes. However, many of these sites can host an Alcatel-Lucent RRH2x40-AWS installation, providing more flexible site selection and improved network quality along with greatly reduced installation time and costs.

Fast, low-cost installation and deployment

The Alcatel-Lucent RRH2x40-AWS is a zero-footprint solution and operates noise-free, simplifying negotiations with site property owners and minimizing environmental impacts. Installation can easily be done by a single person because the Alcatel-Lucent RRH2x40-AWS is compact and weighs less than 20 kg (44 lb), eliminating the need for a crane to hoist the BTS cabinet to the rooftop. A site can be in operation in less than one day — a fraction of the time required for a traditional BTS.

#### Excellent RF performance

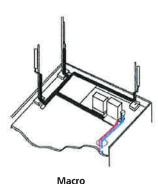
Because of its small size and weight, the Alcatel-Lucent RRH2x40-AWS can be installed close to the antenna. Operators can therefore locate the Alcatel-Lucent RRH2x40-AWS where RF engineering is deemed ideal, minimizing trade-offs between available sites and RF optimum sites. The RF feeder cost and installation costs are reduced or eliminated, and there is no need for a Tower Mounted Amplifier (TMA) because losses introduced by the RF feeder are greatly reduced. The Alcatel-Lucent RRH2x40-AWS provides more RF power while at the same time consuming less electricity.

### Features

- · Zero-footprint deployment
- Easy installation, with a lightweight unit can be carried and set up by one person
- Optimized RF power, with flexible site selection and elimination of a TMA
- Convection-cooled (fanless)
- Noise-free
- Best-in-class power efficiency, with significantly reduced energy consumption

#### Benefits

- Leverages existing real estate with lower site costs
- Reduces installation costs, with fewer installation materials and simplified logistics
- Decreases power costs and minimizes environmental impacts, with the potential for eco-sustainable power options
- Improves RF performance and adds flexibility to network planning



Antenna

RF feeder

Radio

Digital

Backhaul

Antenna

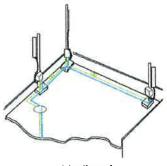
Antenna

Optical link

Digital

Backhaul

RRH for space-constrained cell sites



Distributed

#### Technical specifications

#### Physical dimensions

- Height: 620 mm (24.4 in.)
- Width: 270 mm (10.63 in.)
- Depth: 170m (6.7 in.)
- Weight (without mounting kit): less than 20 kg (44 lb)

#### Power

• Power supply: -48VDC

#### Operating environment

- Outdoor temperature range:
  - ¬ With solar load: -40°C to +50°C (-40°F to +122°F)
  - ¬ Without solar load: -40°C to +55°C (-40°F to +131°F)

- Passive convection cooling (no fans)
- Enclosure protection
  - ¬ IP65 (International Protection rating)

#### RF characteristics

- Frequency band: 1700/2100 MHz (AWS); 3GPP Band 4
- · Bandwidth: up to 20 MHz
- RF output power at antenna port:
   40 W nominal RF power for each
   Tx port
- Rx diversity: 2-way or 4-way with optional Rx Diversity module
- Noise figure: below 2.0 dB typical
- Antenna Line Device features
- ¬ TMA and Remote electrical tilt (RET) support via AISG v2.0

# Optical characteristics Type/number of fibers

- Single-mode variant
  - ¬ One Single Mode Single Fiber per RRH2x, carrying UL and DL using CWDM
  - ¬ Single mode dual fiber (SM/DF)
- · Multi-mode variant
  - ¬ Two Multi-mode fibers per RRH2x: one carrying UL, the other carrying DL

#### Optical fiber length

- Up to 500 m (0.31 mi), using MM fiber
- Up to 20 km (12.43 mi), using SM fiber

#### **Digital Ports and Alarms**

- Two optical ports to support daisy-chaining
- Six external alarms

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#### Product Description

RFS' HYBRIFLEX Remote Radio Head (RRH) hybrid feeder cabling solution combines optical fiber and DC power for RRHs in a single lightweight aluminum corrugated cable, making it the world's most innovative solution for RRH deployments.

It was developed to reduce installation complexity and costs at Cellular sites, HYBRIFLEX allows mobile operators deploying an RRH architecture to standardize the RRH installation process and eliminate the need for and cost of cable grounding. HYBRIFLEX combines optical fiber (multi-mode or single-mode) and power in a single corrugated cable. It eliminates the need for junction boxes and can connect multiple RRHs with a single feeder. Standard RFS CELLFLEX® accessories can be used with HYBRIFLEX cable. Both pre-connectorized and on-site options are available.

#### Features/Benefitts.

- Aluminum corrugated armor with outstanding bending characteristics minimizes installation time and enables mechanical protection and shielding
- Same accessories as 1 5/8" coaxial cable
- Outer conductor grounding Sliminates typical grounding requirements and saves on installation costs
- Lightweight solution and compact design Decreases tower loading
- Robust cabling Eliminates need for expensive cable trays and ducts
- o Installation of tight bundled fiber optic cable pairs directly to the RRH Reduces CAPEX and wind load by eliminating need for interconnection
- Optical fiber and power cables housed in single corrugated cable Saves CAPEX by standardizing RRH cable installation and reducing installation requirements
- Outdoor polyethylene jacket Ensures long-lasting cable protection



Figure 1: HYBRIFLEX Series

PE/UV external jacket

Optical cable (pair)

Aluminum OC

Power cable with

#### Pechinical Specifications

Steeds a			
Outer Conductor Armor.	Corrugated Aluminum	[mm (in)]	46.5 (1.83)
Jacket	Polyethylene, PE	[mm (in)]	50.3 (1.98)
UV-Protection -	Individual and External Jacket		Yes
Meccanical strangers.			
Weight, Approximate		[kg/m (lb/ft)]	1 9 (1.30)
Minimum Bending Radius	Single Bending	(mm (in)]	200 (8)
Minimum Bending Radius	Repeated Bending	[mm (in)]	500 (20)
Recommended/Maximum	Clamp Spacing	[m (ft)]	1 0 / 1.2 (3 25 / 4.0)
Elegrotal Skomertual			
DC-Resistance Outer Cond	ductor Armor	$[\Omega/\text{km} (\Omega/1000ft)]$	068 (0.205)
DC-Resistance Power Cab	le, 8.4mm <sup>t</sup> (8AWG)	[N/km (N/1000ft)]	2.1 (0.307)
- TREAT OF THE PERSON			
Version			Single-mode OM3
Quantity, Fiber Count			16 (8 pairs)
Core/Clad		(um)	50/125
Primary Coating (Acrylate)		(mm)	245
Buffer Diameter, Nominal		[µm]	900
Secondary Protection, Jack	et, Nominal	[mm (in)]	2 0 (0 08)
Minimum Bending Radius		[mm (:n)]	104 (4-1)
Insertion Loss @ waveleng		dB/km	3 0
Insertion Loss @ waveleng		d8/km	1.0
Standards (Meets or excee	ds)		UL94-V0, UL1665
			RoHS Compliant
PCF IVE VIDIE F DAY	(A)		
Size (Power)		[mm (AWG)]	8 4 (8)
Quantity, Wire Count (Pov	1061		16 (8 pairs)

OC Private Value Private Priva		
Size (Power)	[mm (AWG)]	8 4 (8)
Quantity, Wire Count (Power)		16 (8 pairs)
Size (Alarm)	[mm (AWG)]	0.8 (18)
Quantity, Wire Count (Alarm)		4 (2 pairs)
Туре		UV protected
Strands		19
Primary Jacket Diameter, Nominal	[mm (in/]	6.8 (0.27)
Standards (Meets or exceeds)		NFPA 130, ICEA S-95-658
PRODUCTION OF THE PROPERTY OF		UL Type XHHVV-2, UL 44
		UL-LS Emited Smoke, UL VW-1
		IEEE-383 (1974), IEEE1202/FT4
		RoHS Compliant

Installation Temperature	[°⊂ (°F)]	-40 to +65 (-40 to 149)
Operation Temperature	[°C (°F)]	-40 to +65 (-40 to149)

\* This data is provisional and subject to change

RFS The Clear Choice®

HB153-1-03U3-53J13

23v 21

Print Date: 27,6,2012

information contained in the present datasheet is subject to continuation at time of ordering

Alarm cable with

an internal lacket Figure 3: Construction Detail

# **ATTACHMENT 2**

	General	Power	Density					
Site Name: Riverbank (Stamford)	nford)							
Tower Height: 160Ft								
				CALC. POWER		MAX. PERMISS.	FRACTION	
CARRIER	# OF CHAN.	WATTS ERP	HEIGHT	DENS	FREQ.	EXP.	_	Total
*T-Mobile GSM/UMTS	2	12	118	9000.0	1950	1.0000	%90.0	
*T-Mobile UMTS	2	12	118	9000'0	2100	1.0000	0.06%	
*T-Mobile LTE	2	24	118	0.0012	2100	1.0000	0.12%	
*Metricom			98	0.0002	920	0.6133	0.03%	
*Sprint CDMA/LTE	2	693	160.4	0.0194	1900	1.0000	1.94%	
*Sprint CDMA/LTE	П	390	160.4	0.0055	850	0.5667	%96.0	
*Nextel			130	0.0106		0.5720	1.85%	
*AT&T UMTS	7	200	148	0.0082	880	0.5867	1.40%	
*AT&T UMTS	1	200	148	0.0082	1900	1.0000	0.82%	
*AT&T GSM	9	596	148	0.0292	880	0.5867	4.97%	
*AT&T GSM	9	427	148	0.0421	1900	1.0000	4.21%	
*AT&T LTE	1	200	148	0.0082	740	0.4933	1.66%	
Verizon	15	417	142	0.1115	1970	1.0000	11.15%	
Verizon	6	391	142	0.0628	869	0.5793	10.83%	
Verizon	-	1750	142	0.0312	2145	1.0000	3.12%	
Verizon	-	682	142	0.0122	869	0.4653	2.61%	
								45.81%
* Source: Siting Council								

# **ATTACHMENT 3**



Date: March 25, 2014

Andrew Bazinet Crown Castle 46 Broadway Albany, NY 12204 Paul J Ford and Company 250 E. Broad Street Suite 600 Columbus, OH 43215 614.221.6679

Subject:

Structural Modification Report

Carrier Designation:

Verizon Wireless Co-Locate

Carrier Site Number: Carrier Site Name:

N/A Riverbank

Crown Castle Designation:

Crown Castle BU Number:

806953

**Crown Castle Site Name:** 

BRG 2044 (A) 943097 246651

**Crown Castle JDE Job Number: Crown Castle Work Order Number:** 

704036

**Crown Castle Application Number:** 

200735 Rev. 3

Engineering Firm Designation:

Paul J Ford and Company Project Number: 37513-2318 BP

Site Data:

69 Guinea RD(Camp Rocky Craig), Stamford, Fairfield County, CT

Latitude 41° 6' 6.35", Longitude -73° 35' 41.45"

160 Foot - Monopole Tower

Dear Andrew Bazinet,

Paul J Ford and Company is pleased to submit this "Structural Modification Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 611786, in accordance with application 200735, revision 3.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC4.7: Modified Structure w/ Existing + Reserved + Proposed Equipment Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

**Sufficient Capacity** 

The analysis has been performed in accordance with the TIA/EIA-222-F standard and the 2005 CT State Building Code based upon a fastest mile wind speed of 85 mph with no ice, 37.6 mph with 0.75 inch ice thickness and 50 mph under service loads.

All modifications and equipment proposed in this report shall be installed in accordance with the attached drawings for the determined available structural capacity to be effective.

We at Paul J Ford and Company appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:

Joshua Frybarger, E.I.T. Structural Designer

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#### 2) ANALYSIS CRITERIA

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Table 2 - Existing and Reserved Antenna and Cable Information

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3.2) Assumptions

#### 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)
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4.1) Recommendations

#### 5) APPENDIX A

tnxTower Output

#### 6) APPENDIX B

**Base Level Drawing** 

#### 7) APPENDIX C

**Additional Calculations** 

#### 1) INTRODUCTION

This tower is a 160 ft Monopole tower designed by VALMONT in August of 1999. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-F.

#### 2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 85 mph with no ice, 37.6 mph with 0.75 inch ice thickness and 50 mph under service loads.

Table 1 - Proposed Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
			alcatel lucent	RRH2X40-AWS			
139.0	142.0	3	rymsa	RYMSA MG D3-800TX w/ Mount Pipe	1	1 5/8	i <del>le</del>
		1	rfs celwave	DB-T1-6Z-8AB-0Z			

Table 2 - Existing and Reserved Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
		3	alcatel lucent	TME-1900MHz RRH (65MHz) w/ Mount Pipe			
158.0	158.0	3	alcatel lucent	TME-800MHz RRH w/ mount pipe		唇	2
		2	tower mounts	Pipe Mount [PM 601-3]			
	160.0	6	decibel	DB980H90E-M w/Mount Pipe	6	1 5/8	3
157.0		3	alcatel lucent	800 EXTERNAL NOTCH FILTER		1 1/4 5/8	
	158.0	3	alcatel lucent	TD-RRH8x20-25	3 1		2
		3	rfs celwave	APXVSPP18-C-A20 w/ Mount Pipe			
		3	rfs celwave	APXVTM14-C-120 w/ Mount Pipe			
	157.0	9	rfs celwave	ACU-A20-N			
	157.0	1	tower mounts	Platform Mount [LP 713-1]	-	-	1
		6	powerwave	7770.00 w/ Mount Pipe			
	151.0	6	powerwave	LGP21401			
		6	powerwave	LGP21901	40	4.5/0	
149.0		3	ericsson	RRUS-11	12 2	1 5/8 3/8	1
149.0	149.0	3	powerwave	P65-16-XLH-RR w/ Mount Pipe	1	5/8	
		1	raycap	DC6-48-60-18-8F	r.		
		1	tower mounts	Platform Mount [LP 713-1]			

Mounting Level (ft)			Number Antenna Of Manufacturer Antenna Model		Number of Feed Lines	Feed Line Size (in)	Note
	31 3	1	gps	GPS_A	1	1/2	3
139.0		6	andrew	DB846F65ZAXY w/ Mount Pipe			
	142.0	3	powerwave technologies	P65.16.XL.2 w/ Mount 'Pipe			
		3	rymsa	RYMSA MG D3-800TV w/ Mount Pipe	12	1 5/8	1
	400.0	6	rfs celwave	FD9R6004/2C-3L			
	139.0	1	tower mounts	Platform Mount [LP 713-1]			
126.0	128.0	9	decibel	DB844H90E-XY w/Mount Pipe	9	1 1/4	3
120.0	126.0	1	tower mounts	Platform Mount [LP 712-1]			
	118.0	3	comm. components.	DTMA-1819-DD-12			
		3	ems wireless	RR90-17-02DP w/ Mount Pipe	-	-	3
		3	rfs celwave	APX16DWV-16DWV-S-E- ACU w/ Mount Pipe			
116.0		3	rfs celwave	ATMAA1412D-1A20			
		3	ericsson	ERICSSON AIR 21 B2A B4P w/ Mount Pipe			
		3	ericsson	ERICSSON AIR 21 B4A B2P w/ Mount Pipe	1	1 5/8	2
		3	ericsson	KRY 112 144/1			
	116.0	1	tower mounts	Platform Mount [LP 712-1]	12	1 5/8	1
	3.0	1	gps	GPS_A			
84.0	84.0	1	tower mounts	Side Arm Mount [SO 701-	1	1/2	1

Notes:

Existing Equipment Reserved Equipment Equipment To Be Removed 1) 2) 3)

#### 3) ANALYSIS PROCEDURE

**Table 3 - Documents Provided** 

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	Dr. Clarence Welti, 7/20/98	1104116	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	Towerkraft, 2622, 7/30/98	1104113	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Valmont, 18917-69, 8/5/99	823122	CCISITES
4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA	PJF, 41705-162, 8/30/09	1251715	CCISITES
4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA	PJF, 37512-1595, 10/1/12	3332716	CCISITES

#### 3.1) Analysis Method

tnxTower (version 6.1.4.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

#### 3.2) Assumptions

- Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Monopole was reinforced in conformance with the referenced modification drawings.
- 5) Based on pictures, (3) Powerwave LGP21401 and (3) Powerwave LGP21901 at the 149' level have been considered to be shielded by the existing antennas.
- 6) Any extraneous mount pipes at 116' are to be removed when the reserved loading is installed.
- 7) Monopole will be reinforced in conformance with the proposed modification drawings.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J Ford and Company should be notified to determine the effect on the structural integrity of the tower.

#### 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	160 - 111.33	Pole	TP31.29x19.6x0.25	1	-9.41	1252.07	90.0	Pass
L2	111.33 - 86.25	Pole	TP36.797x29.6683x0.3438	2	-16.63	2097.93	97.2	Pass
L3	86.25 - 80.75	Pole	TP38.1149x36.797x0.5054	3	-18.08	2587.75	85.1	Pass
L4	80.75 - 79	Pole	TP38.5342x38.1149x0.4221	4	-18.47	2619.68	85.4	Pass
L5	79 - 50.0833	Pole	TP44.787x38.5342x0.4063	5	-25.43	3018.50	98.4	Pass
L6	50.0833 - 36.33	Pole	TP48.088x44.787x0.5368	6	-27.69	3374.40	93.2	Pass
L7	36.33 - 32.25	Pole	TP48.2559x45.4135x0.5632	7	-33.10	3676.67	93.6	Pass
L8	32.25 - 15.5	Pole	TP52.278x48.2559x0.5525	8	-39.08	3918.65	96.7	Pass
L9	15.5 - 14.5	Pole	TP52.5182x52.278x0.6092	9	-39.48	4338.39	88.0	Pass
L10	14.5 - 0	Polé	TP56x52.5182x0.4902	10	-44.54	4432.50	92.3	Pass
							Summary	
						Pole (L5)	98.4	Pass
						Rating =	98.4	Pass

Table 5 - Tower Component Stresses vs. Capacity

Notes	Component	Elevation (ft)	% Capacity	Pass / Fai
1	Anchor Rods	0	86.1	Pass
1	Base Plate	0	69.3	Pass
1	Base Foundation Structural Steel	0	74.4	Pass
1	Base Foundation Soil Interaction	0	99.9	Pass

	Structure Rating (max from all components) =	99.9%
Notes:		

See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

#### 4.1) Recommendations

See attached modification drawings.

#### **APPENDIX A**

#### **TNXTOWER OUTPUT**

### **Tower Input Data**

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

- Tower is located in Fairfield County, Connecticut. 1)
- Basic wind speed of 85 mph. 2)
- Nominal ice thickness of 0.7500 in. 3)
- Ice thickness is considered to increase with height. 4)
- Ice density of 56.00 pcf. 5)
- A wind speed of 38 mph is used in combination with ice. 6)
- 7) Temperature drop of 50 °F.
- Deflections calculated using a wind speed of 50 mph. 8)
- A non-linear (P-delta) analysis was used. 9)
- Pressures are calculated at each section. 10)
- Stress ratio used in pole design is 1.333. 11)
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are 12) not considered.

### **Options**

Consider Moments - Leas Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification Use Code Stress Ratios

- Use Code Safety Factors Guys
  - Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination

Distribute Leg Loads As Uniform Assume Legs Pinned

- Assume Rigid Index Plate
- Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension Bypass Mast Stability Checks
- Use Azimuth Dish Coefficients
- Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends Triangulate Diamond Inner Bracing

Sort Capacity Reports By Component Use TIA-222-G Tension Splice Capacity Exemption

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

- Consider Feedline Torque Include Angle Block Shear Check Poles
- Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

### **Tapered Pole Section Geometry**

Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	fť	fť	Sides	in	in	in	in	
L1	160.0000-111.3300	48.6700	4.67	12	19.6000	31.2900	0.2500	1.0000	A572-65 (65 ksi)
L2	111.3300-86.2500	29.7500	0.00	12	29.6683	36.7970	0.3438	1.3752	A572-65 (65 ksi)
L3	86.2500-80.7500	5.5000	0.00	12	36.7970	38.1149	0.5054	2.0217	Reinf 52.86 ksi (53 ksl)
L4	80.7500-79.0000	1.7500	0.00	12	38.1149	38.5342	0.4221	1.6884	Reinf 63.23 ksi (63 ksi)
L5	79.0000-50.0833	28.9167	0.00	12	38.5342	44.7870	0.4063	1.6252	A572-65 (65 ksi)
L6	50.0833-36.3300	13.7533	6.67	12	44.7870	48.0880	0.5368	2.1472	Reinf 53.12 ksi (53 ksl)
L7	36.3300-32.2500	10.7500	0.00	12	45.4135	48.2559	0.5632	2.2528	Reinf 53.15 ksi (53 ksi)
L8	32.2500-15.5000	16.7500	0.00	12	48.2559	52.2780	0.5525	2.2101	Reinf 53.24 ksi (53 ksi)
L9	15.5000-14.5000	1.0000	0.00	12	52.2780	52.5181	0.6092	2.4368	Reinf 53.27 ksi (53 ksl)
L10	14.5000-0.0000	14.5000		12	52.5181	56.0000	0.4902	1.9608	Reinf 63.25 ksi (63 ksi)

Ta	per	<u>ed</u>	P	ole	P	ro	pe	rti	es

Section	Tip Dia. in	Area in²	l in⁴	r in	C in	I/C in³	J in⁴	It/Q in²	w in	w/t
L1	20.2914	15.5768	744.4315	6.9273	10.1528	73.3228	1508.4200	7.6664	4.5828	18.331
	32.3938	24.9872	3072.8897	11.1123	16.2082	189.5883	6226.5076	12.2979	7.7157	30.863
L2	31.8734	32.4633	3563.2009	10.4982	15.3682	231.8556	7220.0110	15.9774	7.0297	20.447
	38.0950	40.3550	6844.6814	13.0502	19.0608	359.0968	13869.1803	19.8615	8.9402	26.004
L3	38.0950	59.0639	9929.3009	12.9924	19.0608	520.9271	20119.4556	29.0695	8.5070	16.831
	39.4594	61.2088	11050.7840	13.4642	19.7435	559.7177	22391.8845	30.1251	8.8602	17.53
L4	39.4594	51.2318	9290.5395	13.4940	19.7435	470.5620	18825.1518	25.2147	9.0835	21.519
	39.8935	51.8017	9604.0722	13.6441	19.9607	481.1488	19460.4541	25.4952	9.1959	21.786
L5	39.8935	49.8822	9255.8639	13.6498	19.9607	463.7041	18754.8897	24.5505	9.2383	22.738
	46.3669	58.0627	14597.2613	15.8883	23.1997	629.2012	29578.0089	28.5767	10.9140	26.862
L6	46.3669	76.4863	19116.1459	15.8416	23.1997	823.9835	38734.4943	37.6442	10.5643	19.68
	49.7844	82.1921	23721.3157	17.0233	24.9096	952.2967	48065.8167	40.4524	11.4490	21.328
L7	48.8413	81.3362	20883.3728	16.0564	23.5242	887.7402	42315.3750	40.0312	10.6614	18.93
	49.9582	86.4909	25110.7480	17.0740	24.9965	1004.5687	50881.1834	42.5682	11.4232	20.283
L8	49.9582	84.8713	24651.5551	17.0778	24.9965	986.1985	49950.7340	41.7710	11.4518	20.726
	54.1222	92.0272	31427.6223	18.5177	27.0800	1160.5467	63680.8833	45.2930	12.5297	22.677
L9	54.1222	101.3564	34537.7645	18.4974	27.0800	1275.3968	69982.8744	49.8846	12.3778	20.318
	54.3708	101.8275	35021.5471	18.5834	27.2044	1287.3485	70963.1492	50.1164	12.4422	20.423
L10	54.3708	82.1249	28374.8700	18.6260	27.2044	1043.0250	57495.1794	40.4194	12.7611	26.032
	57.9755	87.6209	34461.3861	19.8725	29.0080	1187.9959	69828.1111	43.1243	13.6942	27.935

## Feed Line/Linear Appurtenances - Entered As Area

Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg			ft			ft²/ft	klf
HB058-M12-	Α	No	CaAa (Out Of	157.0000 - 0.0000	1	No Ice	0.0000	0.00
XXXF(5/8")			Face)			1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.01
						4" Ice	0.0000	0.02
HB114-1-0813U4-M5J(	Α	No	CaAa (Out Of	157.0000 -	1	No Ice	0.1540	0.00
1 1/4")			Face)	116.0000		1/2" Ice	0.2540	0.00
						1" Ice	0.3540	0.00
						2" Ice	0.5540	0.01
						4" Ice	0.9540	0.03
HB114-1-0813U4-M5J(	Α	No	CaAa (Out Of	157.0000 -	2	No Ice	0.0000	0.00
1 1/4")			Face)	116.0000		1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.01
						4" Ice	0.0000	0.03
HB114-1-0813U4-M5J(	Α	No	CaAa (Out Of	116.0000 - 0.0000	3	No Ice	0.0000	0.00
1 1/4")			Face)			1/2" Ice	0.0000	0.00
•						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.01
						4" Ice	0.0000	0.03
***								
LCF158-50JA-A0(1	С	No	Inside Pole	149.0000 - 0.0000	12	No Ice	0.0000	0.00
5/8")						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
						4" lce	0.0000	0.00
FB-L98B-002-75000(	С	No	Inside Pole	149.0000 - 0.0000	2	No Ice	0.0000	0.00
3/8")						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
						4" Ice	0.0000	0.00
WR-VG82ST-BRDA(	С	No	Inside Pole	149.0000 - 0.0000	1	No Ice	0.0000	0.00
5/8")						1/2" Ice	0.0000	0.00
·						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
						4" Ice	0.0000	0.00
***								
HB158-1-08U8-S8J18(	В	No	CaAa (Out Of	139.0000 - 0.0000	1	No Ice	0.1980	0.00
1-5/8)			Face)			1/2" Ice	0.2980	0.00

Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg	Omora	1,400	ft	ramoor		ft²/ft	klf
						1" Ice	0.3980	0.00
						2" Ice	0.5980	0.01
						4" Ice	0.9980	0.03
561(1-5/8")	В	No	Inside Pole	139.0000 - 0.0000	12	No Ice	0.0000	0.00
(/						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" lce	0.0000	0.00
						4" Ice	0.0000	0.00
***						7 100	0.0000	0.00
***								
MLE Hybrid	Α	No	CaAa (Out Of	116.0000 - 0.0000	1	No Ice	0.1625	0.00
Power/18Fiber RL 2(			Face)			1/2" Ice	0.2625	0.00
1 5/8)			,			1" Ice	0.3625	0.00
,						2" Ice	0.5625	0.01
						4" Ice	0.9625	0.01
LDF7-50A(1-5/8")	Α	No	Inside Pole	116.0000 - 0.0000	12	No Ice	0.0000	0.03
LDI 7-30A(1-3/6)	^	NO	Iliside Fole	110.0000 - 0.0000	12	1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice		
							0.0000	0.00
***						4" Ice	0.0000	0.00
LDF4-50A(1/2")	Α	No	Inside Pole	84.0000 - 0.0000	1	No Ice	0.0000	0.00
LDF4-30A(1/2 )	^	NO	Iliside Fole	04.0000 - 0.0000	'	1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
***						4" Ice	0.0000	0.00
3/4" Flat	С	No	CaAa (Out Of	12.2500 - 1.7500	ň	No Ice	0.1250	0.00
Reinforcement	O	140	Face)	12.2300 - 1.7300		1/2" Ice	0.12361	0.00
Reinforcement			race)			172 ice 1" ice	0.2301	0.00
						2" Ice	0.5694	0.00
0140 514	_	k1.	0-4-70-100	70 5000 77 0000	3	4" Ice	1.0139	0.00
3/4" Flat	С	No		78.5000 - 77.0000	1	No Ice	0.1250	0.00
Reinforcement			Face)			1/2" Ice	0.2361	0.00
					8	1" Ice	0.3472	0.00
						2" Ice	0.5694	0.00
			1.		39	4" Ice	1.0139	0.00
I" Flat Reinforcement	С	No		52.2500 - 12.2500	1	No Ice	0.1667	0.00
			Face)			1/2" Ice	0.2778	0.00
						1" Ice	0.3889	0.00
						2" Ice	0.6111	0.00
						4" Ice	1.0556	0.00
" Flat Reinforcement	С	No	CaAa (Out Of	88.5000 - 78.5000	1	No Ice	0.1667	0.00
			Face)			1/2" Ice	0.2778	0.00
			′			1" Ice	0.3889	0.00
						2" Ice	0.6111	0.00
						4" Ice	1.0556	0.00

# Feed Line/Linear Appurtenances Section Areas

Tower Sectio	Tower Elevation	Face	A <sub>R</sub>	A <sub>F</sub>	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
ก	ft		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	K
L1	160.0000-	Α	0.000	0.000	0.000	7.073	0.23
	111.3300	В	0.000	0.000	0.000	5.479	0.48
		С	0.000	0.000	0.000	0.000	0.05
L2	111.3300-	Α	0.000	0.000	0.000	4.076	0.37
	86.2500	В	0.000	0.000	0.000	4.966	0.44
		С	0.000	0.000	0.000	0.375	0.03
L3	86.2500-80.7500	Α	0.000	0.000	0.000	0.894	0.08
		В	0.000	0.000	0.000	1.089	0.10
		С	0.000	0.000	0.000	0.917	0.01
L4	80.7500-79.0000	Α	0.000	0.000	0.000	0.284	0.03
		В	0.000	0.000	0.000	0.346	0.03
		С	0.000	0.000	0.000	0.292	0.00
L5	79.0000-50.0833	Α	0.000	0.000	0.000	4.699	0.43
		В	0.000	0.000	0.000	5.726	0.51

Tower Sectio	Tower Elevation	Face	$A_R$	$A_F$	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
n	ft		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	κ
		С	0.000	0.000	0.000	0.632	0.04
L6	50.0833-36.3300	Α	0.000	0.000	0.000	2.235	0.20
		В	0.000	0.000	0.000	2.723	0.24
		С	0.000	0.000	0.000	2.292	0.02
L7	36.3300-32.2500	Α	0.000	0.000	0.000	0.663	0.06
		В	0.000	0.000	0.000	0.808	0.07
		С	0.000	0.000	0.000	0.680	0.01
L8	32.2500-15.5000	Α	0.000	0.000	0.000	2.722	0.25
		В	0.000	0.000	0.000	3.317	0.29
		С	0.000	0.000	0.000	2.792	0.02
L9	15.5000-14.5000	Α	0.000	0.000	0.000	0.163	0.01
		В	0.000	0.000	0.000	0.198	0.02
		С	0.000	0.000	0.000	0.167	0.00
L10	14.5000-0.0000	Α	0.000	0.000	0.000	2.356	0.22
		В	0.000	0.000	0.000	2.871	0.25
		С	0.000	0.000	0.000	1.688	0.02

# Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	$A_R$	$A_F$	$C_A A_A$	$C_AA_A$	Weigh
Sectio	Elevation	or	Thickness	4.2	·2	In Face	Out Face	
n	ft	Leg	in	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	K
L1	160.0000-	Α	0.887	0.000	0.000	0.000	15.179	0.70
	111.3300	В		0.000	0.000	0.000	10.390	0.57
		С		0.000	0.000	0.000	0.000	0.05
L2	111.3300-	Α	0.855	0.000	0.000	0.000	8.527	0.69
	86.2500	В		0.000	0.000	0.000	9.417	0.52
		С		0.000	0.000	0.000	0.819	0.03
L3	86.2500-80.7500	Α	0.838	0.000	0.000	0.000	1.816	0.15
		В		0.000	0.000	0.000	2.011	0.11
		С		0.000	0.000	0.000	1.941	0.01
L4	80.7500-79.0000	Α	0.834	0.000	0.000	0.000	0.576	0.05
		В		0.000	0.000	0.000	0.638	0.04
		С		0.000	0.000	0.000	0.616	0.00
L5	79.0000-50.0833	Α	0.812	0.000	0.000	0.000	9.397	0.76
		В		0.000	0.000	0.000	10.423	0.59
		С		0.000	0.000	0.000	1.384	0.04
L6	50.0833-36.3300	Α	0.774	0.000	0.000	0.000	4.365	0.35
		В		0.000	0.000	0.000	4.853	0.28
		С		0.000	0.000	0.000	4.659	0.02
L7	36.3300-32.2500	Α	0.753	0.000	0.000	0.000	1.295	0.10
		В		0.000	0.000	0.000	1.440	0.08
		С		0.000	0.000	0.000	1.382	0.01
L8	32.2500-15.5000	Α	0.750	0.000	0.000	0.000	5.234	0.42
		В		0.000	0.000	0.000	5.829	0.34
		С		0.000	0.000	0.000	5.583	0.02
L9	15.5000-14.5000	Α	0.750	0.000	0.000	0.000	0.313	0.03
		В		0.000	0.000	0.000	0.348	0.02
		С		0.000	0.000	0.000	0.333	0.00
L10	14.5000-0.0000	Α	0.750	0.000	0.000	0.000	4.531	0.37
		В		0.000	0.000	0.000	5.046	0.29
		C		0.000	0.000	0.000	3.812	0.02

### **Feed Line Center of Pressure**

Section	Elevation	CP <sub>X</sub>	CPz	CP <sub>X</sub> Ice	CPz Ice
	ft	in	in	in	in
L1	160.0000-	0.1433	-0.1146	0.2313	-0.2267
	111.3300				
L2	111.3300-86.2500	0.2084	-0.0733	0.3353	-0.1532
L3	86.2500-80.7500	0.0348	0.0255	0.0120	0.0317
L4	80.7500-79.0000	0.0349	0.0255	0.0121	0.0318
L5	79.0000-50.0833	0.2059	-0.0709	0.3245	-0.1448
L6	50.0833-36.3300	0.0358	0.0262	0.0142	0.0330
L7	36.3300-32.2500	0.0359	0.0263	0.0143	0.0332

Section	Elevation	CP <sub>X</sub>	CPz	CP <sub>X</sub>	CPz
				Ice	Ice
	ft	in	in	in	in
L8	32.2500-15.5000	0.0362	0.0264	0.0150	0.0333
L9	15.5000-14.5000	0.0363	0.0265	0.0152	0.0336
L10	14.5000-0.0000	0.0966	-0.0076	0.0909	-0.0093

			Disc	rete Tov	wer Load	ds			
Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			ft ft ft	٠	ft		ft²	ft²	Κ
TME-800MHz RRH w/ mount pipe	Α	From Face	2.0000 0.00 0.00	0.00	158.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	3.5250 4.1044 4.5973 5.6293 7.8776	3.4935 4.1955 4.7751 5.9880 8.6287	0.07 0.11 0.15 0.25 0.56
TME-800MHz RRH w/ mount pipe	В	From Face	2.0000 0.00 0.00	0.00	158.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	3.5250 4.1044 4.5973 5.6293 7.8776	3.4935 4.1955 4.7751 5.9880 8.6287	0.07 0.11 0.15 0.25 0.56
TME-800MHz RRH w/ mount pipe	С	From Face	2.0000 0.00 0.00	0.00	158.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	3.5250 4.1044 4.5973 5.6293 7.8776	3.4935 4.1955 4.7751 5.9880 8.6287	0.07 0.11 0.15 0.25 0.56
TME-1900MHz RRH (65MHz) w/ Mount Pipe	Α	From Face	2.0000 0.00 0.00	0.00	158.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	2.6979 2.9362 3.1832 3.7030 4.8463	2.7708 3.0111 3.2600 3.7837 4.9348	0.06 0.08 0.11 0.18 0.35
TME-1900MHz RRH (65MHz) w/ Mount Pipe	В	From Face	2.0000 0.00 0.00	0.00	158.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	2.6979 2.9362 3.1832 3.7030 4.8463	2.7708 3.0111 3.2600 3.7837 4.9348	0.06 0.08 0.11 0.18 0.35
TME-1900MHz RRH (65MHz) w/ Mount Pipe	С	From Face	2.0000 0.00 0.00	0.00	158.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	2.6979 2.9362 3.1832 3.7030 4.8463	2.7708 3.0111 3.2600 3.7837 4.9348	0.06 0.08 0.11 0.18 0.35
(2) Pipe Mount [PM 601-3]	С	None		0.00	158.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	4.3900 5.4800 6.5700 8.7500 13.1100	4.3900 5.4800 6.5700 8.7500 13.1100	0.20 0.24 0.28 0.36 0.53
APXVTM14-C-120 w/ Mount Pipe	А	From Face	4.0000 0.00 1.00	0.00	157.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	7.1342 7.6618 8.1830 9.2563 11.5262	4.9591 5.7544 6.4723 8.0099 11.4120	0.08 0.13 0.19 0.34 0.75
APXVTM14-C-120 w/ Mount Pipe	В	From Face	4.0000 0.00 1.00	0.00	157.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	7.1342 7.6618 8.1830 9.2563 11.5262	4.9591 5.7544 6.4723 8.0099 11.4120	0.08 0.13 0.19 0.34 0.75
APXVTM14-C-120 w/ Mount Pipe	С	From Face	4.0000 0.00 1.00	0.00	157.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	7.1342 7.6618 8.1830 9.2563 11.5262	4.9591 5.7544 6.4723 8.0099 11.4120	0.08 0.13 0.19 0.34 0.75
TD-RRH8x20-25	Α	From Face	4.0000 0.00 1.00	0.00	157.0000	No Ice 1/2" Ice 1" Ice	4.7198 5.0138 5.3165	1.7027 1.9196 2.1453	0.75 0.07 0.10 0.13

TD-RRH8x20-25  TD-RRH8x20-25  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	B C C	From Face From Face From Face	Vert ft ft ft ft 4.0000 0.00 1.00 4.0000 0.00 1.00 4.0000 0.00 1.00	0.00	ff 157.0000 157.0000 157.0000	2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	5.9478 7.3141 4.7198 5.0138 5.3165 5.9478 7.3141 4.7198 5.0138 5.3165 5.9478	ft <sup>2</sup> 2.6224 3.6805 1.7027 1.9196 2.1453 2.6224 3.6805 1.7027 1.9196 2.1453 2.6234	0.20 0.40 0.07 0.10 0.13 0.20 0.40 0.07 0.10 0.13
TD-RRH8x20-25  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	C A B	From Face	0.00 1.00 4.0000 0.00 1.00 4.0000 0.00	0.00	157.0000	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	7.3141 4.7198 5.0138 5.3165 5.9478 7.3141 4.7198 5.0138 5.3165 5.9478	3.6805 1.7027 1.9196 2.1453 2.6224 3.6805 1.7027 1.9196 2.1453	0.40 0.07 0.10 0.13 0.20 0.40 0.07 0.10 0.13
TD-RRH8x20-25  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	C A B	From Face	0.00 1.00 4.0000 0.00 1.00 4.0000 0.00	0.00	157.0000	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	4.7198 5.0138 5.3165 5.9478 7.3141 4.7198 5.0138 5.3165 5.9478	1.7027 1.9196 2.1453 2.6224 3.6805 1.7027 1.9196 2.1453	0.07 0.10 0.13 0.20 0.40 0.07 0.10 0.13
TD-RRH8x20-25  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	C A B	From Face	0.00 1.00 4.0000 0.00 1.00 4.0000 0.00	0.00	157.0000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	5.0138 5.3165 5.9478 7.3141 4.7198 5.0138 5.3165 5.9478	1.9196 2.1453 2.6224 3.6805 1.7027 1.9196 2.1453	0.10 0.13 0.20 0.40 0.07 0.10 0.13
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	АВ	From Face	4.0000 0.00 1.00 4.0000 0.00			1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	5.3165 5.9478 7.3141 4.7198 5.0138 5.3165 5.9478	2.1453 2.6224 3.6805 1.7027 1.9196 2.1453	0.13 0.20 0.40 0.07 0.10 0.13
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	АВ	From Face	4.0000 0.00 1.00 4.0000 0.00			2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	5.9478 7.3141 4.7198 5.0138 5.3165 5.9478	2.6224 3.6805 1.7027 1.9196 2.1453	0.20 0.40 0.07 0.10 0.13
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	АВ	From Face	0.00 1.00 4.0000 0.00			4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	7.3141 4.7198 5.0138 5.3165 5.9478	3.6805 1.7027 1.9196 2.1453	0.40 0.07 0.10 0.13
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	АВ	From Face	0.00 1.00 4.0000 0.00			No Ice 1/2" Ice 1" Ice 2" Ice	4.7198 5.0138 5.3165 5.9478	1.7027 1.9196 2.1453	0.07 0.10 0.13
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	АВ	From Face	0.00 1.00 4.0000 0.00			1/2" Ice 1" Ice 2" Ice	5.0138 5.3165 5.9478	1.9196 2.1453	0.10 0.13
Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	В		1.00 4.0000 0.00	0.00	157.0000	1" lce 2" lce	5.3165 5.9478	2.1453	0.13
Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	В		4.0000 0.00	0.00	157.0000	2" Ice	5.9478		
Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	В		0.00	0.00	157.0000				0.20
Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	В		0.00	0.00	157.0000	4 100	7.3141	2.6224 3.6805	0.20 0.40
Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	В		0.00	0.00	137.0000	No Ice	8.4975	6.9458	0.40
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER		From Face				1/2" Ice	9.1490	8.1266	0.08
Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER		From Face	1.00			1" lce	9.7672	9.0212	0.13
Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER		From Face				2" Ice	11.0311	10.8440	0.23
Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER		From Face				4" lce	13.6786	14.8507	0.41
Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER		1 TOTT I ACC	4.0000	0.00	157.0000	No Ice	8.4975	6.9458	0.08
APXVSPP18-C-A20 w/ Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	С		0.00	0.00	137.0000	1/2" Ice	9.1490	8.1266	0.15
Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH	С		1.00			1" lce	9.7672	9.0212	0.13
Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH	С		1.00			2" lce	11.0311	10.8440	0.41
Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER	С					4" lce	13.6786	14.8507	0.91
Mount Pipe  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH	•	From Face	4.0000	0.00	157.0000	No Ice	8.4975	6.9458	0.08
800 EXTERNAL NOTCH FILTER 800 EXTERNAL NOTCH FILTER 800 EXTERNAL NOTCH		1 101111 400	0.00	0.00	101.0000	1/2" Ice	9.1490	8.1266	0.15
FILTER  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH			1.00			1" Ice	9.7672	9.0212	0.23
FILTER  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH			1.00			2" lce	11.0311	10.8440	0.41
FILTER  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH						4" lce	13.6786	14.8507	0.91
FILTER  800 EXTERNAL NOTCH FILTER  800 EXTERNAL NOTCH	Α	From Face	4.0000	0.00	157.0000	No Ice	0.7701	0.3747	0.01
800 EXTERNAL NOTCH FILTER 800 EXTERNAL NOTCH			0.00	0.00	101.000	1/2" Ice	0.8898	0.4647	0.02
FILTER 800 EXTERNAL NOTCH			1.00			1" ice	1.0181	0.5634	0.02
FILTER 800 EXTERNAL NOTCH						2" Ice	1.3007	0.7868	0.04
FILTER 800 EXTERNAL NOTCH						4" Ice	1.9696	1.3372	0.11
FILTER 800 EXTERNAL NOTCH	В	From Face	4.0000	0.00	157.0000	No Ice	0.7701	0.3747	0.01
			0.00			1/2" Ice	0.8898	0.4647	0.02
			1.00			1" Ice	1.0181	0.5634	0.02
						2" Ice	1.3007	0.7868	0.04
						4" Ice	1.9696	1.3372	0.11
FILTER	С	From Face	4.0000	0.00	157.0000	No ice	0.7701	0.3747	0.01
			0.00			1/2" Ice	0.8898	0.4647	0.02
			1.00			1" Ice	1.0181	0.5634	0.02
						2" Ice	1.3007	0.7868	0.04
						4" Ice	1.9696	1.3372	0.11
(3) ACU-A20-N	Α	From Face	4.0000	0.00	157.0000	No Ice	0.0778	0.1361	0.00
			0.00			1/2" Ice	0.1210	0.1890	0.00
			0.00			1" Ice	0.1728	0.2506	0.00
						2" lce	0.3025	0.3997	0.01
						4" Ice	0.6654	0.8015	0.04
(3) ACU-A20-N	В	From Face	4.0000	0.00	157.0000	No Ice	0.0778	0.1361	0.00
			0.00			1/2" Ice	0.1210	0.1890	0.00
			0.00			1" Ice	0.1728	0.2506	0.00
						2" Ice	0.3025	0.3997	0.01
						4" Ice	0.6654	0.8015	0.04
(3) ACU-A20-N	С	From Face	4.0000	0.00	157.0000	No Ice	0.0778	0.1361	0.00
			0.00			1/2" Ice	0.1210	0.1890	0.00
			0.00			1" Ice	0.1728	0.2506	0.00
						2" Ice	0.3025	0.3997	0.01
					4==	4" Ice	0.6654	0.8015	0.04
Platform Mount [LP 713-1]	Α	None		0.00	157.0000	No Ice	31.2700	31.2700	1.51
						1/2" Ice	39.6800	39.6800	1.93
						1" Ice	48.0900	48.0900	2.35
						2" Ice	64.9100	64.9100	3.19
***						4" Ice	98.5500	98.5500	4.86
		Face: F	4.0000	0.00	4.40.0000	NI= I	0.4404	4.0540	
2) 7770.00 w/ Mount Pipe	Α	From Face	4.0000 0.00	0.00	149.0000	No Ice 1/2" Ice	6.1194 6.6258	4.2543 5.0137	0.06 0.10

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weigh
			ft ft ft	٥	ft		ft²	ft²	К
			2.00			1" Ice	7.1283	5.7109	0.16
						2" Ice	8.1643	7.1553	0.29
(0) 7770 00 w/ Marrat Diag			4 0000	0.00	4.40.0000	4" Ice	10.3599	10.4117	0.66
2) 7770.00 w/ Mount Pipe	В	From Face	4.0000	0.00	149.0000	No Ice	6.1194	4.2543	0.06
			0.00 2.00			1/2" Ice 1" Ice	6.6258 7.1283	5.0137 5.7109	0.10 0.16
			2.00			2" Ice	8.1643	7.1553	0.10
						4" Ice	10.3599	10.4117	0.66
2) 7770.00 w/ Mount Pipe	С	From Face	4.0000	0.00	149.0000	No Ice	6.1194	4.2543	0.06
			0.00			1/2" Ice	6.6258	5.0137	0.10
			2.00			1" Ice	7.1283	5.7109	0.16
						2" Ice	8.1643	7.1553	0.29
205 40 2/11 22		<b>-</b>	4.0000	0.00	440.0000	4" Ice	10.3599	10.4117	0.66
P65-16-XLH-RR w/ Mount	Α	From Face	4.0000	0.00	149.0000	No Ice	8.6375	6.3625	0.08
Pipe			0.00 0.00			1/2" lce 1" lce	9.2903 9.9098	7.5378	0.14
			0.00			2" Ice	9.9098	8.4270 10.2390	0.22
						4" Ice	13.8289	14.0988	0.39
P65-16-XLH-RR w/ Mount	В	From Face	4.0000	0.00	149.0000	No Ice	8.6375	6.3625	0.08
Pipe	_	1 10111 1 400	0.00	0.00	110.0000	1/2" Ice	9.2903	7.5378	0.14
			0.00			1" Ice	9.9098	8.4270	0.22
						2" Ice	11.1763	10.2390	0.39
						4" Ice	13.8289	14.0988	0.89
P65-16-XLH-RR w/ Mount	С	From Face	4.0000	0.00	149.0000	No Ice	8.6375	6.3625	0.08
Pipe			0.00			1/2" Ice	9.2903	7.5378	0.14
			0.00			1" Ice	9.9098	8.4270	0.22
						2" Ice	11.1763	10.2390	0.39
LGP21401	Α	From Food	4 0000	0.00	140,0000	4" Ice	13.8289	14.0988	0.89
LGP21401	А	From Face	4.0000 0.00	0.00	149.0000	No Ice 1/2" Ice	1.2880 1.4453	0.2326	0.01
			2.00			1" Ice	1.6112	0.3134 0.4028	0.02
			2.00			2" lce	1.9690	0.4020	0.05
						4" Ice	2.7882	1.1210	0.14
LGP21401	В	From Face	4.0000	0.00	149.0000	No Ice	1.2880	0.2326	0.01
			0.00			1/2" Ice	1.4453	0.3134	0.02
			2.00			1" Ice	1.6112	0.4028	0.03
						2" Ice	1.9690	0.6076	0.05
	10.					4" Ice	2.7882	1.1210	0.14
LGP21401	С	From Face	4.0000	0.00	149.0000	No Ice	1.2880	0.2326	0.01
			0.00			1/2" Ice	1.4453	0.3134	0.02
			2.00			1" Ice	1.6112	0.4028	0.03
						2" Ice 4" Ice	1.9690 2.7882	0.6076 1.1210	0.05 0.14
LGP21401	Α	From Face	4.0000	0.00	149.0000	No Ice	0.0000	0.0000	0.14
20121401	^	1101111 acc	0.00	0.00	148.0000	1/2" Ice	0.0000	0.0000	0.01
			2.00			1" Ice	0.0000	0.0000	0.03
						2" Ice	0.0000	0.0000	0.05
						4" Ice	0.0000	0.0000	0.14
LGP21401	В	From Face	4.0000	0.00	149.0000	No Ice	0.0000	0.0000	0.01
			0.00			1/2" Ice	0.0000	0.0000	0.02
			2.00			1" Ice	0.0000	0.0000	0.03
						2" Ice	0.0000	0.0000	0.05
LOD24404	0	From Food	4.0000	0.00	440,0000	4" Ice	0.0000	0.0000	0.14
LGP21401	С	From Face	4.0000 0.00	0.00	149.0000	No Ice 1/2" Ice	0.0000	0.0000	0.01
			2.00			1" lce	0.0000	0.0000	0.02 0.03
			2.00			2" ice	0.0000	0.0000	0.03
						4" lce	0.0000	0.0000	0.03
LGP21901	Α	From Face	4.0000	0.00	149.0000	No Ice	0.2695	0.1838	0.01
	-		0.00		- 3	1/2" Ice	0.3432	0.2483	0.01
			2.00			1" Ice	0.4255	0.3216	0.01
						2" Ice	0.6160	0.4940	0.02
						4" Ice	1.1009	0.9425	0.07
LGP21901	В	From Face	4.0000	0.00	149.0000	No Ice	0.2695	0.1838	0.01
			0.00			1/2" Ice	0.3432	0.2483	0.01

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Vert ft ft	•	ft		ft²	ft²	Κ
			ft			481	0.4055	0.0040	0.04
			2.00			1" Ice 2" Ice	0.4255 0.6160	0.3216 0.4940	0.01
						4" Ice	1.1009	0.4940	0.02 0.07
LGP21901	С	From Face	4.0000	0.00	149.0000	No Ice	0.2695	0.1838	0.07
201 21901	O	1 IOIII I ace	0.00	0.00	149.0000	1/2" Ice	0.2093	0.1638	3a 0.01
			2.00			1" Ice	0.4255	0.3216	0.01
			2.00			2" Ice	0.6160	0.4940	0.02
						4" Ice	1.1009	0.9425	0.07
LGP21901	Α	From Face	4.0000	0.00	149.0000	No Ice	0.0000	0.0000	0.01
			0.00		160	1/2" Ice	0.0000	0.0000	0.01
			2.00			1" Ice	0.0000	0.0000	0.01
						2" Ice	0.0000	0.0000	0.02
						4" Ice	0.0000	0.0000	0.07
LGP21901	В	From Face	4.0000	0.00	149.0000	No Ice	0.0000	0.0000	0.01
			0.00			1/2" Ice	0.0000	0.0000	0.01
			2.00			1" Ice	0.0000	0.0000	0.01
						2" lce	0.0000	0.0000	0.02
						4" Ice	0.0000	0.0000	0.07
LGP21901	С	From Face	4.0000	0.00	149.0000	No Ice	0.0000	0.0000	0.01
			0.00			1/2" Ice	0.0000	0.0000	0.01
			2.00			1" Ice	0.0000	0.0000	0.01
						2" Ice	0.0000	0.0000	0.02
						4" Ice	0.0000	0.0000	0.07
RRUS-11	Α	From Face	4.0000	0.00	149.0000	No Ice	3.2486	1.3726	0.05
			0.00			1/2" lce	3.4905	1.5510	0.07
			0.00			1" Ice	3.7411	1.7380	0.09
						2" lce	4.2682	2.1381	0.15
	27					4" Ice	5.4260	3.0418	0.31
RRUS-11	В	From Face	4.0000	0.00	149.0000	No Ice	3.2486	1.3726	0.05
			0.00			1/2" Ice	3.4905	1.5510	0.07
			0.00			1" Ice	3.7411	1.7380	0.09
						2" Ice	4.2682	2.1381	0.15
DDU0 44	_	F F	4 0000	0.00	4.40.0000	4" Ice	5.4260	3.0418	0.31
RRUS-11	С	From Face	4.0000	0.00	149.0000	No Ice	3.2486	1.3726	0.05
			0.00			1/2" Ice	3.4905	1.5510	0.07
			0.00			1" Ice 2" Ice	3.7411	1.7380	0.09
							4.2682	2.1381	0.15
DC6-48-60-18-8F	С	From Face	4.0000	0.00	149.0000	4" Ice	5.4260 2.5667	3.0418 2.5667	0.31
DC0-40-00-10-0F	C	FIOIII Face	0.00	0.00	149.0000	No Ice 1/2" Ice	2.7978	2.7978	0.02
			0.00			1" lce	3.0377	3.0377	0.04 0.07
			0.00			2" Ice	3.5432	3.5432	0.07
						4" Ice	4.6580	4.6580	0.13
Platform Mount [LP 713-1]	Α	None		0.00	149.0000	No Ice	31.2700	31.2700	1.51
riadomi Modrit [El 1710-1]		HONC		0.00	143.0000	1/2" Ice	39.6800	39.6800	1.93
						1" lce	48.0900	48.0900	2.35
				25		2" lce	64.9100	64.9100	3.19
***						4" lce	98.5500	98.5500	4.86
RYMSA MG D3-800TX w/	Α	From Face	4.0000	0.00	139.0000	No Ice	3.5960	3.4435	0.04
Mount Pipe			0.00	2.23		1/2" Ice	4.0150	4.1655	0.07
			3.00			1" Ice	4.4296	4.8367	0.11
			<del>-</del>			2" lce	5.3815	6.2291	0.21
						4" Ice	7.4264	9.2649	0.52
RYMSA MG D3-800TX w/	В	From Face	4.0000	0.00	139.0000	No Ice	3.5960	3.4435	0.04
Mount Pipe			0.00			1/2" Ice	4.0150	4.1655	0.07
-			3.00			1" Ice	4.4296	4.8367	0.11
						2" Ice	5.3815	6.2291	0.21
						4" Ice	7.4264	9.2649	0.52
RYMSA MG D3-800TX w/	С	From Face	4.0000	0.00	139.0000	No Ice	3.5960	3.4435	0.04
Mount Pipe			0.00			1/2" Ice	4.0150	4.1655	0.07
			3.00			1" Ice	4.4296	4.8367	0.11
						2" lce	5.3815	6.2291	0.21
						4 4			
					139.0000	4" Ice	7.4264 2.9764	9.2649	0.52

Description	Face or	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
	Leg		Vert ft	t e:	ft		ft <sup>2</sup>	ft <sup>2</sup>	K
			ft ft	n:					
			0.00			1/2" Ice	3.2363	1.8239	0.06
			3.00			1" Ice	3.5048	2.0605	0.08
						2" lce	4.0678	2.5596	0.14
DDI 107/40 474/0	Б	E E	4.0000	0.00	100 0000	4" Ice	5.2975	3.6614	0.29
RRH2X40-AWS	В	From Face	4.0000	0.00	139.0000	No Ice 1/2" Ice	2.9764	1.5960	0.04
			0.00 3.00			1/2 ice 1" ice	3.2363 3.5048	1.8239 2.0605	0.06 0.08
			0.00			2" ice	4.0678	2.5596	0.14
						4" Ice	5.2975	3.6614	0.29
RRH2X40-AWS	С	From Face	4.0000	0.00	139.0000	No Ice	2.9764	1.5960	0.04
			0.00			1/2" Ice	3.2363	1.8239	0.06
			3.00	3		1" Ice	3.5048	2.0605	0.08
59						2" Ice 4" Ice	4.0678 5.2975	2.5596	0.14
DB-T1-6Z-8AB-0Z	С	From Face	4.0000	0.00	139.0000	No Ice	5.6000	3.6614 2.3333	0.29 0.04
DB 11 02 0/1B 02	O	1101111 400	0.00	0.00	100.0000	1/2" Ice	5.9154	2.5580	0.04
			3.00			1" Ice	6.2395	2.7914	0.12
						2" Ice	6.9136	3.2840	0.21
		_				4" Ice	8.3654	4.3728	0.45
(2) DB846F65ZAXY w/	Α	From Face	4.0000	0.00	139.0000	No Ice	7.2708	7.8208	0.05
Mount Pipe			0.00 3.00			1/2" Ice 1" Ice	7.8773 8.4838	9.0097 9.9124	0.11
			3.00			2" Ice	9.7244	11.8119	0.19 0.37
						4" Ice	12.3252	15.9785	0.87
(2) DB846F65ZAXY w/	В	From Face	4.0000	0.00	139.0000	No Ice	7.2708	7.8208	0.05
Mount Pipe			0.00			1/2" Ice	7.8773	9.0097	0.11
			3.00			1" Ice	8.4838	9.9124	0.19
						2" Ice	9.7244	11.8119	0.37
(2) DB846F65ZAXY w/	С	From Face	4.0000	0.00	120 0000	4" Ice	12.3252	15.9785	0.87
Mount Pipe	C	FIOIII Face	0.00	0.00	139.0000	No Ice 1/2" Ice	7.2708 7.8773	7.8208 9.0097	0.05 0.11
Would Tipe			3.00			1" Ice	8.4838	9.9124	0.11
			0.00			2" Ice	9.7244	11.8119	0.37
						4" Ice	12.3252	15.9785	0.87
P65.16.XL.2 w/ Mount Pipe	Α	From Face	4.0000	0.00	139.0000	No Ice	8.6375	5.7792	0.06
			0.00			1/2" Ice	9.2903	6.9491	0.12
			3.00			1" Ice 2" Ice	9.9098 11.1763	7.8329 9.6341	0.19 0.36
						4" Ice	13.8289	13.4365	0.84
P65.16.XL.2 w/ Mount Pipe	В	From Face	4.0000	0.00	139.0000	No Ice	8.6375	5.7792	0.06
			0.00			1/2" Ice	9.2903	6.9491	0.12
			3.00			1" Ice	9.9098	7.8329	0.19
						2" Ice	11.1763	9.6341	0.36
Dec 16 VI 2 w/ Mount Dine	С	From Coop	4.0000	0.00	120 0000	4" Ice	13.8289 8.6375	13.4365	0.84
P65.16.XL.2 w/ Mount Pipe	C	From Face	0.00	0.00	139.0000	No Ice 1/2" Ice	9.2903	5.7792 6.9491	0.06 0.12
			3.00			1" Ice	9.9098	7.8329	0.12
						2" Ice	11.1763	9.6341	0.36
						4" Ice	13.8289	13.4365	0.84
RYMSA MG D3-800TV w/	Α	From Face	4.0000	0.00	139.0000	No Ice	3.4773	3.3248	0.04
Mount Pipe			0.00			1/2" Ice	3.8534	3.9564	0.07
			3.00			1" Ice 2" Ice	4.2373 5.1257	4.5989 5.9338	0.11
						4" Ice	7.0405	8.9033	0.20 0.51
RYMSA MG D3-800TV w/	В	From Face	4.0000	0.00	139.0000	No Ice	3.4773	3.3248	0.04
Mount Pipe	-		0.00			1/2" Ice	3.8534	3.9564	0.07
,			3.00			1" Ice	4.2373	4.5989	0.11
						2" Ice	5.1257	5.9338	0.20
DVMOA NO DO COSTI :	_	F F	4.0000	0.00	400 0000	4" Ice	7.0405	8.9033	0.51
RYMSA MG D3-800TV w/ Mount Pipe	С	From Face	4.0000 0.00	0.00	139.0000	No Ice 1/2" Ice	3.4773 3.8534	3.3248 3.9564	0.04
wount ripe			3.00			1/2 ice 1" ice	3.8534 4.2373	3.9564 4.5989	0.07 0.11
	i.		5.00			2" Ice	5.1257	5.9338	0.11
						4" Ice	7.0405	8.9033	0.51

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weigh
			ft ft ft	- <b></b>	ft		ft²	ft²	К
			0.00 0.00			1/2" Ice 1" Ice 2" Ice	0.4506 0.5433 0.7546	0.1362 0.1965 0.3430	0.01 0.01 0.02
						4" Ice	1.2808	0.7396	0.06
(2) FD9R6004/2C-3L	В	From Face	4.0000	0.00	139.0000	No Ice	0.3665	0.0846	0.00
			0.00			1/2" Ice	0.4506	0.1362	0.01
			0.00			1" Ice 2" Ice	0.5433 0.7546	0.1965 0.3430	0.01 0.02
						4" Ice	1.2808	0.7396	0.02
(2) FD9R6004/2C-3L	C	From Face	4.0000	0.00	139.0000	No Ice	0.3665	0.0846	0.00
, ,			0.00			1/2" Ice	0.4506	0.1362	0.01
			0.00			1" Ice	0.5433	0.1965	0.01
						2" Ice	0.7546	0.3430	0.02
DI-45 M (I D 740 41		Mana		0.00	400 0000	4" Ice	1.2808	0.7396	0.06
Platform Mount [LP 713-1]	Α	None		0.00	139.0000	No Ice 1/2" Ice	31.2700 39.6800	31.2700 39.6800	1.51 1.93
						1" Ice	48.0900	48.0900	2.35
						2" lce	64.9100	64.9100	3.19
***						4" Ice	98.5500	98.5500	4.86
*** ERICSSON AIR 21 B2A	Α	From Face	4.0000	0.00	116.0000	No Ice	6.8253	5.6424	0.11
B4P w/ Mount Pipe			0.00	0.00	110.0000	1/2" Ice	7.3471	6.4800	0.17
			2.00			1" Ice	7.8631	7.2567	0.23
						2" Ice	8.9261	8.8640	0.38
						4" Ice	11.1755	12.2932	0.81
ERICSSON AIR 21 B2A	В	From Face	4.0000	0.00	116.0000	No Ice	6.8253	5.6424	0.11
B4P w/ Mount Pipe			0.00			1/2" Ice	7.3471	6.4800	0.17
			2.00			1" Ice	7.8631 8.9261	7.2567	0.23
						2" ice 4" ice	11.1755	8.8640 12.2932	0.38 0.81
ERICSSON AIR 21 B2A	С	From Face	4.0000	0.00	116.0000	No Ice	6.8253	5.6424	0.01
B4P w/ Mount Pipe	_	1 10111 1 400	0.00	0.00	110.0000	1/2" Ice	7.3471	6.4800	0.17
			2.00			1" Ice	7.8631	7.2567	0.23
						2" Ice	8.9261	8.8640	0.38
						4" Ice	11.1755	12.2932	0.81
ERICSSON AIR 21 B4A	Α	From Face	4.0000	0.00	116.0000	No Ice	6.8155	5.6334	0.11
B2P w/ Mount Pipe			0.00			1/2" Ice 1" Ice	7.3373 7.8532	6.4717	0.17
			2.00			2" Ice	8.9160	7.2478 8.8537	0.23 0.38
						4" Ice	11.1650	12.2804	0.38
ERICSSON AIR 21 B4A	В	From Face	4.0000	0.00	116.0000	No Ice	6.8155	5.6334	0.11
B2P w/ Mount Pipe			0.00			1/2" Ice	7.3373	6.4717	0.17
			2.00			1" Ice	7.8532	7.2478	0.23
						2" Ice	8.9160	8.8537	0.38
EDICCCON AID 24 D4A	0	From Food	4.0000	0.00	116 0000	4" Ice	11.1650	12.2804	0.81
ERICSSON AIR 21 B4A B2P w/ Mount Pipe	С	From Face	4.0000 0.00	0.00	116.0000	No Ice 1/2" Ice	6.8155 7.3373	5.6334 6.4717	0.11
bzr w/ Modific Fipe			2.00			1" Ice	7.8532	7.2478	0.17 0.23
			2.00			2" Ice	8.9160	8.8537	0.38
						4" Ice	11.1650	12.2804	0.81
KRY 112 144/1	Α	From Face	4.0000	0.00	116.0000	No Ice	0.4083	0.2042	0.01
			0.00			1/2" Ice	0.4969	0.2733	0.01
			2.00			1" lce	0.5941	0.3511	0.02
						2" lce	0.8145	0.5326	0.03
KRY 112 144/1	В	Erom Econ	4.0000	0.00	116.0000	4" Ice	1.3590 0.4083	0.9992	0.08
MNI 112 (44/1	Ь	From Face	0.00	0.00	110.0000	No Ice 1/2" Ice	0.4083	0.2042 0.2733	0.01 0.01
			2.00			1" lce	0.4909	0.2733	0.01
			2.00			2" lce	0.8145	0.5326	0.02
						4" lce	1.3590	0.9992	0.08
KRY 112 144/1	С	From Face	4.0000	0.00	116.0000	No Ice	0.4083	0.2042	0.01
			0.00			1/2" Ice	0.4969	0.2733	0.01
			2.00			1" Ice	0.5941	0.3511	0.02
						2" Ice	0.8145	0.5326	0.03

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Vert ft ft ft	•	ft		ft²	ft²	Κ
						4" Ice	1.3590	0.9992	0.08
Platform Mount [LP 712-1]	Α	None		0.00	116.0000	No Ice	24.5300	24.5300	1.34
						1/2" Ice	29.9400	29.9400	1.65
						1" lce	35.3500	35.3500	1.96
						2" Ice	46.1700	46.1700	2.58
***						4" Ice	67.8100	67.8100	3.82
GPS_A	С	From Face	4.0000	0.00	84.0000	No Ice	0.2975	0.2975	0.00
			0.00			1/2" Ice	0.3739	0.3739	0.00
			0.00			1" Ice	0.4589	0.4589	0.01
						2" Ice	0.6549	0.6549	0.02
						4" Ice	1.1506	1.1506	0.08
Side Arm Mount [SO 701-	С	From Face	2.0000	0.00	84.0000	No Ice	0.8500	1.6700	0.07
1]	-		0.00	2.00		1/2" lce	1.1400	2.3400	0.08
•1			0.00			1" lce	1.4300	3.0100	0.09
			2.00			2" Ice	2.0100	4.3500	0.12
						4" lce	3.1700	7.0300	0.18

### **Tower Pressures - No Ice**

_						$G_H = 1$	1.690				
Section	Z	Kz	$q_z$	$A_{G}$	F	$A_F$	$A_R$	A <sub>leg</sub>	Leg	$C_A A_A$	$C_A A_A$
Elevation					a				%	In	Out
				. 1	С	_	_	_		Face	Façe
ft	ft		ksf	ft <sup>2</sup>	е	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
L1 160.0000-	134.1093	1.493	0.03	103.20	Α	0.000	103.201	103.201	100.00	0.000	7.073
111.3300				1	В	0.000	103.201		100.00	0.000	5.479
					С	0.000	103.201		100.00	0.000	0.000
L2 111.3300-	98.4183	1.366	0.03	70.626	Α	0.000	70.626	70.626	100.00	0.000	4.076
86,2500					В	0.000	70.626		100.00	0.000	4.966
· · · · · · · · · · · · · · · · · · ·					С	0.000	70.626		100.00	0.000	0.375
L3 86.2500-	83.4839	1.304	0.02	17.167	Α	0.000	17.167	17.167	100.00	0.000	0.894
80.7500					В	0.000	17.167		100.00	0.000	1.089
					С	0.000	17.167		100.00	0.000	0.917
L4 80.7500-	79.8734	1.287	0.02	5.589	Α	0.000	5.589	5.589	100.00	0.000	0.284
79.0000					В	0.000	5.589		100.00	0.000	0.346
					С	0.000	5.589		100.00	0.000	0.292
L5 79.0000-	64.1800	1.209	0.02	100.39	Α	0.000	100.391	100.391	100.00	0.000	4.699
50.0833				1	В	0.000	100.391		100.00	0.000	5.726
					C	0.000	100.391		100.00	0.000	0.632
L6 50.0833-	43.1252	1.079	0.02	53.222	Α	0.000	53.222	53.222	100.00	0.000	2.235
36.3300					В	0.000	53.222		100.00	0.000	2.723
					C	0.000	53.222		100.00	0.000	2.292
L7 36.3300-	34.2823	1.011	0.02	16.224	Ā	0.000	16.224	16.224	100.00	0.000	0.663
32.2500					В	0.000	16.224		100.00	0.000	0.808
			0.00	70.404	Ç	0.000	16.224	70.404	100.00	0.000	0.680
L8 32.2500-	23.7633	1	0.02	70.164	A	0.000	70.164	70.164	100.00	0.000	2.722
15.5000					В	0.000	70.164		100.00	0.000	3.317
	44,0000		0.00	4 007	Ċ	0.000	70.164	4 007	100.00	0.000	2.792
L9 15.5000-	14.9996	1	0.02	4.367	Ä	0.000	4.367	4.367	100.00	0.000	0.163
14.5000					В	0.000	4.367		100.00	0.000	0.198
1 40 44 5000	7 4705	الما	0.00	05 500	Č	0.000	4.367	65 563	100.00	0.000	0.167
L10 14.5000-	7.1725	1	0.02	65.563	A	0.000	65.563	65.563	100.00	0.000	2.356
0.0000		Ų			B	0.000	65.563		100.00	0.000	2.871
					U	0.000	65.563		100.00	0.000	1.688

Tower Pressure - With Ic	ce		h	it	V	V	_	ure	ess	Pr	er	w	T
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					(	3 <sub>H</sub> =	1.690					
Section	Z	Kz	$q_z$	tz	$A_G$	F	$A_F$	$A_R$	A <sub>leg</sub>	Leg	$C_A A_A$	$C_AA_A$
Elevation						a				%	In	Out
						С					Face	Façe
ft	ft		ksf	in	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
L1 160.0000-	134.1093	1.493	0.01	0.8874	110.399	Α	0.000	110.399	110.399	100.00		
111.3300	- 1					В	0.000	110.399		100.00		
						С	0.000	110.399		100.00		
L2 111.3300-	98.4183	1.366	0.00	0.8551	74.335	Α	0.000	74.335	74.335	100.00	0.000	8.527
86.2500	- 1					В	0.000	74.335		100.00		
						С	0.000	74.335		100.00		
L3 86.2500-	83.4839	1.304	0.00	0.8384	17.936	Α	0.000	17.936	17.936	100.00		
80.7500	- 1					В	0.000	17.936		100.00	0.000	2.011
	- 1					С	0.000	17.936		100.00	0.000	1.941
L4 80.7500-	79.8734	1.287	0.00	0.8339	5.832	Α	0.000	5.832	5.832	100.00	0.000	0.576
79.0000	- 1					В	0.000	5.832		100.00	0.000	0.638
	- 1					С	0.000	5.832		100.00	0.000	0.616
L5 79.0000-	64.1800	1.209	0.00	0.8123	104.306	Α	0.000	104.306	104.306	100.00	0.000	9.397
50.0833						В	0.000	104.306		100.00	0.000	10.423
1						С	0.000	104.306		100.00		
L6 50.0833-	43.1252	1.079	0.00	0.7745	54.998	Α	0.000	54.998	54.998	100.00		
36.3300	- 1					В	0.000	54.998	1	100.00	0.000	4.853
						С	0.000	54.998		100.00	0.000	4.659
L7 36.3300-	34.2823	1.011	0.00	0.7534	16.750	Α	0.000	16.750	16.750	100.00		
32.2500	- 1					В	0.000	16.750		100.00	0.000	1.440
1	- 1					С	0.000	16.750		100.00	0.000	1.382
L8 32.2500-	23.7633	1	0.00	0.7500	72.258	Α	0.000	72.258	72.258	100.00	0.000	5.234
15.5000	- 1					В	0.000	72.258		100.00	0.000	5.829
1	- 1					С	0.000	72.258		100.00	0.000	5.583
L9 15.5000-	14.9996	1	0.00	0.7500	4.492	Α	0.000	4.492	4.492	100.00	0.000	0.313
14.5000	- 1					В	0.000	4.492		100.00	0.000	0.348
						С	0.000	4.492		100.00	0.000	
L10 14.5000-	7.1725	1	0.00	0.7500	67.376	Α	0.000	67.376	67.376	100.00	0.000	
0.0000	- 1					В	0.000	67.376		100.00		
	I	I				С	0.000	67.376		100.00	0.000	

### **Tower Pressure - Service**

						$G_H = 1$	1.690				
Section	Z	Kz	$q_z$	$A_{G}$	F	A <sub>F</sub>	$A_R$	A <sub>leg</sub>	Leg	$C_A A_A$	$C_A A_A$
Elevation					а			ľ	%	In	Out
					С					Face	Façe
ft	ft		ksf	ft <sup>2</sup>	е	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
L1 160.0000-	134.1093	1.493	0.01	103.20	Α	0.000	103.201	103.201	100.00	0.000	7.073
111.3300				1	В	0.000	103.201		100.00	0.000	5.479
					С	0.000	103.201		100.00	0.000	0.000
L2 111.3300-	98.4183	1.366	0.01	70.626	Α	0.000	70.626	70.626	100.00	0.000	4.076
86.2500					В	0.000	70.626		100.00	0.000	4.966
					С	0.000	70.626		100.00	0.000	0.375
L3 86.2500-	83.4839	1.304	0.01	17.167	Α	0.000	17.167	17.167	100.00	0.000	0.894
80.7500					В	0.000	17.167		100.00	0.000	1.089
					C	0.000	17.167		100.00	0.000	0.917
L4 80.7500-	79.8734	1.287	0.01	5.589	Α	0.000	5.589	5.589	100.00	0.000	0.284
79.0000					В	0.000	5.589		100.00	0.000	0.346
					C	0.000	5.589		100.00	0.000	0.292
L5 79.0000-	64.1800	1.209	0.01	100.39	Α	0.000	100.391	100.391	100.00	0.000	4.699
50.0833				1	В	0.000	100.391		100.00	0.000	5.726
					C	0.000	100,391		100.00	0.000	0.632
L6 50.0833-	43.1252	1.079	0.01	53.222	Α.	0.000	53.222	53.222	100.00	0.000	2.235
36.3300					В	0.000	53.222		100.00	0.000	2.723
					C	0.000	53.222		100.00	0.000	2.292
L7 36.3300-	34.2823	1.011	0.01	16.224	<u>A</u>	0.000	16.224	16.224	100.00	0.000	0.663
32.2500					В	0.000	16.224		100.00	0.000	0.808
		5			C	0.000	16.224		100.00	0.000	0.680
L8 32.2500-	23.7633	1	0.01	70.164	A	0.000	70.164	70.164	100.00	0.000	2.722
15.5000					В	0.000	70.164		100.00	0.000	3,317
		2			Ç	0.000	70.164		100.00	0.000	2.792
L9 15.5000-	14.9996	1	0.01	4.367	Α	0.000	4.367	4.367	100.00	0.000	0.163

Section	Z	Kz	$q_z$	$A_G$	F	$A_F$	$A_R$	A <sub>leg</sub>	Leg	$C_A A_A$	$C_A A_A$
Elevation					a				%	ln	Out
					С					Face	Face
ft	ft		ksf	ft <sup>2</sup>	е	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
14.5000					В	0.000	4.367		100.00	0.000	0.198
					C	0.000	4.367		100.00	0.000	0.167
L10 14.5000-	7.1725	1	0.01	65.563	Α	0.000	65.563	65.563	100.00	0.000	2.356
0.0000	()				В	0.000	65.563		100,00	0.000	2.871
					С	0.000	65.563		100.00	0.000	1.688

## **Load Combinations**

Comb.		Description
No.	2 10 1	
1	Dead Only	
2	Dead+Wind 0 deg - No Ice	
3	Dead+Wind 30 deg - No Ice	
4	Dead+Wind 60 deg - No Ice	
5	Dead+Wind 90 deg - No Ice	
6	Dead+Wind 120 deg - No Ice	
7	Dead+Wind 150 deg - No Ice	
8	Dead+Wind 180 deg - No Ice	
9	Dead+Wind 210 deg - No Ice	
10	Dead+Wind 240 deg - No Ice	
11	Dead+Wind 270 deg - No Ice	
12	Dead+Wind 300 deg - No Ice	
13	Dead+Wind 330 deg - No Ice	
14	Dead+lce+Temp	
15	Dead+Wind 0 deg+Ice+Temp	
16	Dead+Wind 30 deg+lce+Temp	
17	Dead+Wind 60 deg+Ice+Temp	
18	Dead+Wind 90 deg+lce+Temp	
19	Dead+Wind 120 deg+lce+Temp	
20	Dead+Wind 150 deg+lce+Temp	
21	Dead+Wind 180 deg+lce+Temp	
22	Dead+Wind 210 deg+lce+Temp	
23	Dead+Wind 240 deg+lce+Temp	
24	Dead+Wind 270 deg+lce+Temp	
25	Dead+Wind 300 deg+lce+Temp	
26	Dead+Wind 330 deg+lce+Temp	
27	Dead+Wind 0 deg - Service	
28	Dead+Wind 30 deg - Service	
29	Dead+Wind 60 deg - Service	
30	Dead+Wind 90 deg - Service	
31	Dead+Wind 120 deg - Service	
32	Dead+Wind 150 deg - Service	
33	Dead+Wind 180 deg - Service	
34	Dead+Wind 210 deg - Service	
35	Dead+Wind 240 deg - Service	
36	Dead+Wind 270 deg - Service	
37	Dead+Wind 300 deg - Service	
38	Dead+Wind 330 deg - Service	

### **Maximum Member Forces**

Sectio n	Elevation ft	Component Type	Condition	Gov. Load	Force	Major Axis Moment	Minor Axis Moment
No.				Comb.	K	kip-ft	kip-ft
L1	160 - 111.33	Pole	Max Tension	8	0.00	0.00	0.00
			Max. Compression	14	-19.79	-0.11	-0.30
			Max. Mx	5	-9.43	-676.00	-0.09
			Max. My	8	-9.41	-0.03	-680.27
			Max. Vý	5	22.20	-676.00	-0.09
			Max. Vx	8	22.36	-0.03	-680.27
			Max. Torque	11			1.15
L2	111.33 - 86.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-29.71	-0.26	0.31
			Max. Mx	5	-16.65	-1489.31	0.04

Sectio n	Elevation ft	Component Type	Condition	Gov. Load	Force	Major Axis Moment	Minor Ax Momen
No.			March Mr.	Comb.	K	kip-ft	kip-ft
			Max. My	2	-16.63	-0.08	1498.18
			Max. Vy	5	29.30	-1489.31	0.04
			Max. Vx	2	-29.46	-0.08	1498.18
			Max. Torque	11			1.11
L3	86.25 - 80.75	Pole	Max Tension	1	0.00	0.00	0.00
	00.75		Max. Compression	14	-31.42	-0.29	0.08
			Max. Mx	5	-18.10	-1652.97	-0.15
			Max. My	8	-18.08	-0.09	-1662.7
			Max. Vy	5	30.22	-1652.97	-0.15
			Max. Vx	2	-30.35	-0.09	1662.4
			Max. Torque	11			1.41
L4	80.75 - 79	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-31.88	-0.30	0.12
			Max. Mx	5	-18.49	-1706.07	-0.14
			Max. My	8	-18.47	-0.09	-1716.0
			Max. Vy	5	30.49	-1706.07	-0.14
			Max. Vx	2	-30.62	-0.09	1715.7
			Max. Torque	11	-30.02	-0.03	1.41
L5	79 - 50.0833	Pole	Max Tension	1	0.00	0.00	0.00
LO	79 - 50.0655	Pole					
			Max. Compression	14	-39.83	-0.48	0.83
			Max. Mx	5	-25.44	-2644.62	0.06
			Max. My	2	-25.43	-0.15	2658.0
			Max. Vy	5	34.51	-2644.62	0.06
			Max. Vx	2	-34.64	-0.15	2658.0
			Max. Torque	11			1.41
L6	50.0833 <b>-</b> 36.33	Pole	Max Tension	1	0.00	0.00	0.00
	00.00		Max. Compression	14	-42.37	-0.53	1.02
			Max. Mx	5	-27.70	-2892.47	0.12
			Max. My	2	-27.69	-0.17	2906.8
			Max. Vy	5	35.50	-2892.47	0.12
			Max. Vx	2	-35.62	-0.17	2906.8
			Max. Torque	11		•	1.38
L7	36.33 -	Pole	Max Tension	1	0.00	0.00	0.00
	32.25		Max. Compression	14	-48.57	-0.60	1.31
			Max. Mx	5	-33.11	-3282.96	0.21
			Max. My	2	-33.10	-0.19	3298.7
			Max. Vy	5	37.10	-3282.96	0.21
			Max. Vx	2	-37.23	-0.19	3298.7
			Max. Torque	11	07.20	-0.13	1.39
L8	32.25 - 15.5	Pole	Max Tension	1	0.00	0.00	0.00
	JZ.ZU - 10.0	1 016	Max. Compression	14	-55.20	-0.72	1.77
			Max. Mx	5		-0.72 -3922.82	
					-39.08		0.36
			Max. My	2	-39.08	-0.23	3940.8
			Max. Vy	5	39.34	-3922.82	0.36
			Max. Vx	2	-39.46	-0.23	3940.8
			Max. Torque	11			1.39
L9	15.5 - 14.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-55.64	-0.73	1.80
			Max. Mx	5	-39.48	-3962.22	0.37
			Max. My	2	-39.48	-0.23	3980.3
			Max. Vy	5	39.48	-3962.22	0.37
			Max. Vx	2	-39.60	-0.23	3980.3
			Max. Torque	11			1.39
L10	14.5 - 0	Pole	Max Tension	1	0.00	0.00	0.00
	0	. 5.0	Max. Compression	14	-61.26	-0.84	2.24
			Max. Mx	5	-44.54	-4548.46	0.51
			Max. My	2	-44.54	-0.27	4568.4
			•	5			
			Max. Vy	2	41.42	-4548.46 0.27	0.51
			Max. Vx Max. Torque	11	-41.54	-0.27	4568.4 1.39

				4.5
Ma	YIM!	um	Kea	ctions

Location	Condition	Gov. Load	Vertical K	Horizontal, X K	Horizontal, 2 K
		Comb.			
Pole	Max. Vert	14	61.26	0.00	0.00
	Max. H <sub>x</sub>	11	44.56	41.40	-0.00
	Max. H <sub>z</sub>	2	44.56	-0.00	41.52
	Max. M <sub>x</sub>	2	4568.45	-0.00	41.52
	Max. M <sub>z</sub>	5	4548.46	-41.40	-0.00
	Max. Torsion	11	1.39	41.40	-0.00
	Min. Vert	1	44.56	0.00	0.00
	Min. H <sub>x</sub>	5	44.56	-41.40	-0.00
	Min. Hz	8	44.56	-0.00	-41.52
	Min. M <sub>x</sub>	8	-4567.45	-0.00	-41.52
	Min. M <sub>z</sub>	11	-4547.92	41.40	-0.00
	Min. Torsion	5	-1.39	-41.40	-0.00

# **Tower Mast Reaction Summary**

Load	Vertical	Shear <sub>x</sub>	Shearz	Overturning	Overturning	Torque
Combination				Moment, $M_x$	Moment, M <sub>z</sub>	
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	44.56	0.00	0.00	-0.50	-0.26	0.0
Dead+Wind 0 deg - No Ice	44.56	0.00	-41.52	-4568.45	-0.27	0.2
Dead+Wind 30 deg - No Ice	44.56	20.70	-35.96	-3956.48	-2274.33	0.8
Dead+Wind 60 deg - No Ice	44.56	35.86	-20.76	-2284.52	-3939.10	1.3
Dead+Wind 90 deg - No Ice	44.56	41.40	0.00	-0.51	-4548.46	1.3
Dead+Wind 120 deg - No Ice	44.56	35.86	20.76	2283.50	-3939.11	1.0
Dead+Wind 150 deg - No Ice	44.56	20.70	35.96	3955.48	-2274.34	0.5
Dead+Wind 180 deg - No Ice	44.56	0.00	41.52	4567.45	-0.27	-0.2
Dead+Wind 210 deg - No Ice	44.56	-20.70	35.96	3955.48	2273.80	-0.9
Dead+Wind 240 deg - No Ice	44.56	-35.86	20.76	2283.50	3938.57	-1.3
Dead+Wind 270 deg - No Ice	44.56	-41.40	0.00	-0.51	4547.92	-1.3
Dead+Wind 300 deg - No Ice	44.56	-35.86	-20.76	-2284.52	3938.56	-1.0
Dead+Wind 330 deg - No Ice	44.56	-20.70	-35.96	-3956.48	2273.79	-0.4
Dead+lce+Temp	61.26	0.00	0.00	-2.24	-0.84	0.0
Dead+Wind 0 deg+lce+Temp	61.26	0.00	-9.85	-1135.84	-0.88	0.0
Dead+Wind 30 dea+Ice+Temp	61.26	4.91	-8.53	-983.97	-565.77	0.2
Dead+Wind 60 dea+Ice+Temp	61.26	8.51	-4.92	-569.07	-979.30	0.3
Dead+Wind 90 dea+Ice+Temp	61.26	9.83	-0.00	-2.30	-1130.66	0.3
Dead+Wind 120 deg+lce+Temp	61.26	8.51	4.92	564.48	-979.30	0.2
Dead+Wind 150 deg+lce+Temp	61.26	4.91	8.53	979.38	-565.77	0.1
Dead+Wind 180 deg+lce+Temp	61.26	0.00	9.85	1131.25	-0.88	-0.0
Dead+Wind 210 deg+lce+Temp	61.26	-4.91	8.53	979.38	564.01	-0.2
Dead+Wind 240 deg+lce+Temp	61.26	-8.51	4.92	564.48	977.54	-0.3
Dead+Wind 270 deg+lce+Temp	61.26	-9.83	-0.00	-2.30	1128.90	-0.3
Dead+Wind 300 deg+lce+Temp	61.26	-8.51	-4.92	-569.07	977.53	-0.2
Dead+Wind 330 deg+lce+Temp	61.26	-4.91	-8.53	-983.97	564.01	-0.1
Dead+Wind 0 deg - Service	44.56	0.00	-14.37	-1583.65	-0.27	0.0
Dead+Wind 30 deg - Service	44.56	7.16	-12.44	-1371.56	-788.41	0.3
Dead+Wind 60 deg - Service	44.56	12.41	-7.18	-792.08	-1365.37	0.4
Dead+Wind 90 deg - Service	44.56	14.33	0.00	-0.50	-1576.55	0.4
Dead+Wind 120 deg - Service	44.56	12.41	7.18	791.08	-1365.37	0.3
Dead+Wind 150 deg - Service	44.56	7.16	12.44	1370.56	-788.41	0.1
Dead+Wind 180 deg - Service	44.56	0.00	14.37	1582.65	-0.27	-0.0
Dead+Wind 210 deg - Service	44.56	-7.16	12.44	1370.56	787.87	-0.3
Dead+Wind 240 deg - Service	44.56	-12.41	7.18	791.08	1364.83	-0.4
Dead+Wind 270 deg - Service	44.56	-14.33	0.00	-0.50	1576.01	-0.4
Dead+Wind 300 deg - Service	44.56	-12.41	-7.18	-792.08	1364.83	-0.3
Dead+Wind 330 deg - Service	44.56	-7.16	-12.44	-1371.56	787.87	-0.1

Sol	lution	Sumr	narv
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		n of Applied Force			Sum of Reactio		
Load	PX	PY	PZ	PX	PY	PZ	% Erro
Comb.	K	K	K	K	K	K	
1	0.00	-44.56	0.00	0.00	44.56	0.00	0.000%
2	0.00	-44.56	<b>-41.52</b>	-0.00	44.56	41.52	0.000%
3	20.70	-44.56	-35.96	-20.70	44.56	35.96	0.000%
4	35.86	-44.56	-20.76	-35.86	44.56	20.76	0.000%
5	41.40	-44.56	0.00	<i>-</i> 41.40	44.56	-0.00	0.000%
6	35.86	-44.56	20.76	-35.86	44.56	-20.76	0.000%
7	20.70	-44.56	35.96	-20.70	44.56	-35.96	0.000%
8	0.00	-44.56	41.52	-0.00	44.56	-41.52	0.000%
9	-20.70	-44.56	35.96	20.70	44.56	-35.96	0.000%
10	-35.86	-44.56	20.76	35.86	44.56	-20.76	0.000%
11	-41.40	-44.56	0.00	41.40	44.56	-0.00	0.000%
12	-35.86	-44.56	-20.76	35.86	44.56	20.76	0.000%
13	-20.70	-44.56	-35.96	20.70	44.56	35.96	0.000%
14	0.00	-61.26	0.00	0.00	61.26	0.00	0.000%
15	0.00	-61.26	-9.85	-0.00	61.26	9.85	0.000%
16	4.91	-61.26	-8.53	-4.91	61.26	8.53	0.000%
17	8.51	-61.26	-4.92	-8.51	61.26	4.92	0.000%
18	9.83	-61.26	0.00	-9.83	61.26	0.00	0.000%
19	8.51	-61.26	4.92	-8.51	61.26	-4.92	0.000%
20	4.91	-61.26	8.53	-4.91	61.26	-8.53	0.000%
21	0.00	-61.26	9.85	-0.00	61.26	-9.85	0.000%
22	-4.91	-61.26	8.53	4.91	61.26	-8.53	0.000%
23	-8.51	-61.26	4.92	8.51	61.26	-4.92	0.000%
24	-9.83	-61.26	0.00	9.83	61.26	0.00	0.000%
25	-8.51	-61.26	-4.92	8.51	61.26	4.92	0.000%
26	-4.91	-61.26	-8.53	4.91	61.26	8.53	0.000%
27	0.00	-44.56	-14.37	0.00	44.56	14.37	0.000%
28	7.16	-44.56	-12.44	-7.16	44.56	12.44	0.000%
29	12.41	-44.56	-7.18	-12.41	44.56	7.18	0.000%
30	14.33	-44.56	0.00	-14.33	44.56	-0.00	0.000%
31	12.41	-44.56	7.18	-12.41	44.56	-7.18	0.000%
32	7.16	-44.56	12.44	-7.16	44.56	-12.44	0.000%
33	0.00	-44.56	14.37	0.00	44.56	-14.37	0.000%
34	-7.16	-44.56	12.44	7.16	44.56	-12.44	0.000%
35	-12,41	-44.56	7.18	12.41	44.56	-7.18	0.000%
36	-14.33	-44.56	0.00	14.33	44.56	-0.00	0.000%
37	-12.41	-44.56	-7.18	12.41	44.56	7.18	0.000%
38	-7.16	-44.56	-12.44	7.16	44.56	12.44	0.000%

# Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	4	0.0000001	0.0000001
2	Yes	4	0.0000001	0.00027806
3	Yes	5	0.0000001	0.00087394
4	Yes	5	0.00000001	0.00085191
5	Yes	4	0.0000001	0.00072536
6	Yes	5	0.0000001	0.00087635
7	Yes	5	0.0000001	0.00085947
8	Yes	4	0.0000001	0.00027807
9	Yes	5	0.0000001	0.00085635
10	Yes	5	0.0000001	0.00087802
11	Yes	4	0.00000001	0.00072531
12	Yes	5	0.0000001	0.00085344
13	Yes	5	0.00000001	0.00087068
14	Yes	4	0.00000001	0.00000001
15	Yes	5	0.00000001	0.00040826
16	Yes	5	0.0000001	0.00047592
17	Yes	5	0.0000001	0.00047375
18	Yes	5	0.0000001	0.00040674
19	Yes	5	0.0000001	0.00047459
20	Yes	5	0.0000001	0.00047423
21	Yes	5	0.0000001	0.00040771

22	Yes	5	0.0000001	0.00047331
23	Yes	5	0.0000001	0.00047409
24	Yes	5	0.0000001	0.00040614
25	Yes	5	0.0000001	0.00047320
26	Yes	5	0.0000001	0.00047494
27	Yes	4	0.0000001	0.00015172
28	Yes	5	0.0000001	0.00008391
29	Yes	5	0.0000001	0.00007960
30	Yes	4	0.0000001	0.00020235
31	Yes	5	0.0000001	0.00008429
32	Yes	5	0.0000001	0.00008109
33	Yes	4	0.0000001	0.00015174
34	Yes	5	0.0000001	0.00008048
35	Yes	5	0.0000001	0.00008461
36	Yes	4	0.0000001	0.00020229
37	Yes	5	0.0000001	0.00007985
38	Yes	5	0.0000001	0.00008323

### **Maximum Tower Deflections - Service Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	٥
L1	160 - 111.33	40.78	33	2.42	0.00
L2	116 - 86.25	20.25	27	1.84	0.00
L3	86.25 - 80.75	10.48	27	1.25	0.00
L4	80.75 - 79	9.08	27	1.17	0.00
L5	79 - 50.0833	8.66	27	1.14	0.00
L6	50.0833 - 36.33	3.35	27	0.61	0.00
L7	43 - 32.25	2.51	27	0.52	0.00
L8	32.25 <b>-</b> 15.5	1.43	27	0.42	0.00
L9	15.5 - 14.5	0.34	27	0.21	0.00
L10	14.5 - 0	0.29	27	0.20	0.00

## Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	00 L	ft
158.0000	TME-800MHz RRH w/ mount pipe	33	39.77	2.40	0.00	22044
157.0000	APXVTM14-C-120 w/ Mount Pipe	33	39.27	2.38	0.00	22044
149.0000	(2) 7770.00 w/ Mount Pipe	33	35.28	2.30	0.00	10020
139.0000	RYMSA MG D3-800TX w/ Mount Pipe	27	30.41	2.19	0.00	5247
116.0000	ERICSSON AIR 21 B2A B4P w/ Mount Pipe	27	20.25	1.84	0.00	2562
84.0000	GPS_A	27	9.90	1.22	0.00	3361

### **Maximum Tower Deflections - Design Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	۰
L1	160 - 111.33	117.33	8	6.95	0.01
L2	116 - 86.25	58.33	2	5.29	0.00
L3	86.25 - 80.75	30.21	2	3.62	0.00
L4	80.75 - 79	26.18	2	3.38	0.00
L5	79 - 50.0833	24.96	2	3.29	0.00
L6	50.0833 - 36.33	9.65	2	1.77	0.00
L7	43 - 32.25	7.23	2	1.49	0.00
L8	32.25 - 15.5	4.13	2	1.21	0.00
L9	15.5 - 14.5	0.97	2	0.59	0.00
L10	14.5 - 0	0.85	2	0.56	0.00

Critical Deflections and Radius of Curvature - Design Wind
--

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	۰	۰	ft
158.0000	TME-800MHz RRH w/ mount pipe	8	114.44	6.89	0.01	7856
157.0000	APXVTM14-C-120 w/ Mount Pipe	8	113.00	6.86	0.01	7856
149.0000	(2) 7770.00 w/ Mount Pipe	8	101.54	6.62	0.01	3569
139.0000	RÝMSA MG D3-800TX w/ Mount Pipe	2	87.54	6.29	0.01	1867
116.0000	ERICSSON AIR 21 B2A B4P w/ Mount Pipe	2	58.33	5.29	0.00	907
84.0000	GPS A	2	28.53	3.52	0.00	1175

### **Compression Checks**

### **Pole Design Data**

Section No.	Elevation	Size	L	Lu	KI/r	Fa	Α	Actual P	Allow. $P_a$	Ratio P
	ft		ft	ft		ksi	in²	K	K	
L1	160 - 111.33 (1)	TP31.29x19.6x0.25	48.6700	0.0000	0.0	39.00	24.0842	-9.41	939.29	0.010
L2	111.33 - 86.25 (2)	TP36.797x29.6683x0.3438	29.7500	0.0000	0.0	39.00	40.3550	-16.63	1573.84	0.011
L3	86.25 - 80.75 (3)	TP38.1149x36.797x0.5054	5.5000	0.0000	0.0	31.72	61.2088	-18.08	1941.30	0.009
L4	80.75 - 79 (4)	TP38.5342x38.1149x0.4221	1.7500	0.0000	0.0	37.94	51.8017	-18.47	1965.25	0.009
L5	79 - 50.0833 (5)	TP44.787x38.5342x0.4063	28.9167	0.0000	0.0	39.00	58.0627	-25.43	2264.44	0.011
L6	50.0833 - 36.33 (6)	TP48.088x44.787x0.5368	13.7533	0.0000	0.0	31.87	79.4249	-27.69	2531.43	0.011
L7	36.33 - 32.25 (7)	TP48.2559x45.4135x0.5632	10.7500	0.0000	0.0	31.89	86.4909	-33.10	2758.19	0.012
L8	32.25 - 15.5 (8)	TP52.278x48.2559x0.5525	16.7500	0.0000	0.0	31.94	92.0272	-39.08	2939.72	0.013
L9	15.5 - 14.5 (9)	TP52.5182x52.278x0.6092	1.0000	0.0000	0.0	31.96	101.8270	-39.48	3254.61	0.012
L10	14.5 - 0 (1Ò)	TP56x52.5182x0.4902	14.5000	0.0000	0.0	37.95	87.6209	-44.54	3325.21	0.013

# Pole Bending Design Data

Section	Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
No.			$M_{x}$	$f_{bx}$	$F_{bx}$	$f_{bx}$	$M_{y}$	$f_{by}$	$F_{by}$	$f_{by}$
	ft		kip-ft	ksi	ksi	$F_{bx}$	kip-ft	ksi	ksi	F <sub>by</sub>
L1	160 - 111.33 (1)	TP31.29x19.6x0.25	680.27	46.36	39.00	1.189	0.00	0.00	39.00	0.000
L2	111.33 - 86.25 (2)	TP36.797x29.6683x0.3438	1498.18	50.07	39.00	1.284	0.00	0.00	39.00	0.000
L3	86.25 - 80.75 (3)	TP38.1149x36.797x0.5054	1662.76	35.65	31.72	1.124	0.00	0.00	31.72	0.000
L4	80.75 - 79 (4)	TP38.5342x38.1149x0.4221	1716.07	42.80	37.94	1.128	0.00	0.00	37.94	0.000
L5	79 - 50.0833 (5)	TP44.787x38.5342x0.4063	2658.08	50.69	39.00	1.300	0.00	0.00	39.00	0.000
L6	50.0833 - 36.33 (6)	TP48.088x44.787x0.5368	2906.86	39.24	31.87	1.231	0.00	0.00	31.87	0.000
L7	36.33 - 32.25 (7)	TP48.2559x45.4135x0.5632	3298.75	39.41	31.89	1.236	0.00	0.00	31.89	0.000
L8	32.25 - 15.5 (8)	TP52.278x48.2559x0.5525	3940.81	40.75	31.94	1.276	0.00	0.00	31.94	0.000
L9	15.5 - 14.5 (9)	TP52.5182x52.278x0.6092	3980.33	37.10	31.96	1.161	0.00	0.00	31.96	0.000
L10	14.5 - 0 (10)	TP56x52.5182x0.4902	4568.45	46.15	37.95	1.216	0.00	0.00	37.95	0.000

### Pole Shear Design Data

Section	Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
No.			V	$f_{\nu}$	$F_{v}$	$f_{\nu}$	Τ	$f_{vt}$	$F_{vt}$	$f_{vt}$
	ft		K	ksi	ksi	$F_{v}$	kip-ft	ksi	ksi	F <sub>vt</sub>
L1	160 - 111.33 (1)	TP31.29x19.6x0.25	22.36	0.93	26.00	0.073	0.06	0.00	26.00	0.000
L2	111.33 - 86.25 (2)	TP36.797x29.6683x0.3438	29.46	0.73	26.00	0.057	0.13	0.00	26.00	0.000
L3	86.25 - 80.75 (3)	TP38.1149x36.797x0.5054	30.35	0.50	21.14	0.048	0.13	0.00	21.14	0.000
L4	80.75 - 79 (4)	TP38.5342x38.1149x0.4221	30.62	0.59	25.29	0.047	0.13	0.00	25.29	0.000
L5	79 - 50.0833 (5)	TP44.787x38.5342x0.4063	34.64	0.60	26.00	0.047	0.20	0.00	26.00	0.000
L6	50.0833 - 36.33 (6)	TP48.088x44.787x0.5368	35.62	0.45	21.25	0.043	0.21	0.00	21.25	0.000

Section	Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
No.			V	$f_{\nu}$	$F_{\nu}$	$f_{\nu}$	Τ	$f_{vt}$	$F_{vl}$	$f_{vt}$
	ft		K	ksi	ksi	$F_{\nu}$	kip-ft	ksi	ksi	Fvt
L7	36.33 - 32.25 (7)	TP48.2559x45.4135x0.5632	37.23	0.43	21.26	0.041	0.21	0.00	21.26	0.000
L8	32.25 - 15.5 (8)	TP52.278x48.2559x0.5525	39.46	0.43	21.30	0.041	0.22	0.00	21.30	0.000
L9	15.5 - 14.5 (9)	TP52.5182x52.278x0.6092	39.60	0.39	21.31	0.037	0.22	0.00	21.31	0.000
L10	14.5 - 0 (10)	TP56x52.5182x0.4902	41.54	0.47	25.30	0.038	0.24	0.00	25.30	0.000

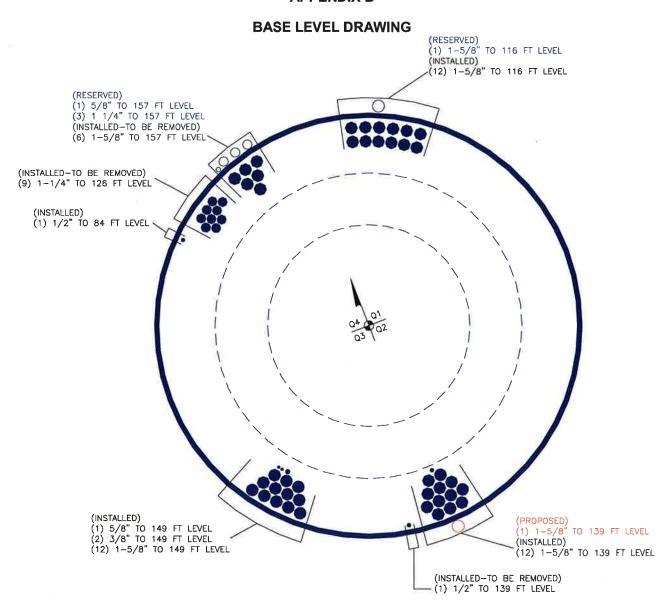
### **Pole Interaction Design Data**

Section No.	Elevation	Ratio P	Ratio f <sub>bx</sub>	Ratio f <sub>by</sub>	Ratio f <sub>v</sub>	Ratio f <sub>vt</sub>	Comb. Stress	Allow. Stress	Criteria
	ft	$P_a$	F <sub>bx</sub>	F <sub>by</sub>	F <sub>v</sub>	$F_{vt}$	Ratio	Ratio	
L1	160 - 111.33 (1)	0.010	1.189	0.000	0.073	0.000	1.200	1.333	H1-3+VT ✔
L2	111.33 - 86.25 (2)	0.011	1.284	0.000	0.057	0.000	1.295	1.333	H1-3+VT
L3	86.25 - 80.75 (3)	0.009	1.124	0.000	0.048	0.000	1.134	1.333	H1-3+VT <b>✓</b>
L4	80.75 - 79 (4)	0.009	1.128	0.000	0.047	0.000	1.138	1.333	H1-3+VT
L5	79 - 50.0833 (5)	0.011	1.300	0.000	0.047	0.000	1.312	1.333	H1-3+VT
L6	50.0833 - 36.33 (6)	0.011	1.231	0.000	0.043	0.000	1.243	1.333	H1-3+VT
L7	36.33 - 32.25 (7)	0.012	1.236	0.000	0.041	0.000	1.248	1.333	H1-3+VT
L8	32.25 - 15.5 (8)	0.013	1.276	0.000	0.041	0.000	1.289	1.333	H1-3+VT
L9	15.5 - 14.5 (9)	0.012	1.161	0.000	0.037	0.000	1.173	1.333	H1-3+VT
L10	14.5 - 0 (10)	0.013	1.216	0.000	0.038	0.000	1.230	1,333	H1-3+VT

# **Section Capacity Table**

Section	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
No.				Liomont				
L1	160 - 111.33	Pole	TP31.29x19.6x0.25	1	-9.41	1252.07	90.0	Pass
L2	111.33 - 86.25	Pole	TP36.797x29.6683x0.3438	2	-16.63	2097.93	97.2	Pass
L3	86.25 - 80.75	Pole	TP38.1149x36.797x0.5054	3	-18.08	2587.75	85.1	Pass
L4	80.75 - 79	Pole	TP38.5342x38.1149x0.4221	4	-18.47	2619.68	85.4	Pass
L5	79 - 50.0833	Pole	TP44.787x38.5342x0.4063	5	-25.43	3018.50	98.4	Pass
L6	50.0833 - 36.33	Pole	TP48.088x44.787x0.5368	6	-27.69	3374.40	93.2	Pass
L7	36.33 - 32.25	Pole	TP48.2559x45.4135x0.5632	7	-33.10	3676.67	93.6	Pass
L8	32.25 - 15.5	Pole	TP52.278x48.2559x0.5525	8	-39.08	3918.65	96.7	Pass
L9	15.5 - 14.5	Pole	TP52.5182x52.278x0.6092	9	-39.48	4338.39	88.0	Pass
L10	14.5 - 0	Pole	TP56x52.5182x0.4902	10	-44.54	4432.50	92.3	Pass
							Summary	
						Pole (L5)	98.4	Pass
						RATING =	98.4	Pass

#### **APPENDIX B**



### APPENDIX C ADDITIONAL CALCULATIONS



### **DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
TME-800MHz RRH w/ mount pipe	158	RRUS-11	149
TME-800MHz RRH w/ mount pipe	158	RRUS-11	149
TME-800MHz RRH w/ mount pipe	158	RRUS-11	149
TME-1900MHz RRH (65MHz) w/	158	DC6-48-60-18-8F	149
Mount Pipe		Platform Mount [LP 713-1]	149
TME-1900MHz RRH (65MHz) w/	158	RYMSA MG D3-800TX w/ Mount Pipe	139
Mount Pipe		RYMSA MG D3-800TX w/ Mount Pipe	139
TME-1900MHz RRH (65MHz) w/ Mount Pipe	158	RYMSA MG D3-800TX w/ Mount Pipe	139
(2) Pipe Mount [PM 601-3]	158	RRH2X40-AWS	139
APXVTM14-C-120 w/ Mount Pipe	157	RRH2X40-AWS	139
APXVTM14-C-120 w/ Mount Pipe	157	RRH2X40-AWS	139
APXVTM14-C-120 w/ Mount Pipe	157	DB-T1-6Z-8AB-0Z	139
TD-RRH8x20-25	157	(2) DB646F65ZAXY w/ Mount Pipe	139
TD-RRH8x20-25	157	(2) DB846F65ZAXY w/ Mount Pipe	139
		(2) DB846F65ZAXY w/ Mount Pipe	139
TD-RRH8x20-25	157	P65 16 XL 2 w/ Mount Pipe	139
APXVSPP18-C-A20 w/ Mount Pipe	157	P65.16.XL 2 w/ Mount Pipe	139
APXVSPP18-C-A20 w/ Mount Pipe		P65.16.XL.2 w/ Mount Pipe	139
APXVSPP18-C-A20 w/ Mount Pipe	157	RYMSA MG D3-800TV w/ Mount Pipe	139
800 EXTERNAL NOTCH FILTER	157	RYMSA MG D3-800TV w/ Mount Pipe	139
800 EXTERNAL NOTCH FILTER	157	RYMSA MG D3-800TV w/ Mount Pipe	139
800 EXTERNAL NOTCH FILTER	157	(2) FD9R6004/2C-3L	139
(3) ACU-A20-N	157	(2) FD9R6004/2C-3L	139
3) ACU-A20-N	157	(2) FD9R6004/2C-3L	139
(3) ACU-A20-N	157	Platform Mount [LP 713-1]	139
Platform Mount [LP 713-1]	157	ERICSSON AIR 21 B2A B4P w/ Mount	116
(2) 7770.00 w/ Mount Pipe	149	Pipe	110
(2) 7770.00 w/ Mount Pipe	149	ERICSSON AIR 21 B2A B4P w/ Mount	116
(2) 7770,00 w/ Mount Pipe	149	Pipe	
P65-16-XLH-RR w/ Mount Pipe	149	ERICSSON AIR 21 B2A B4P w/ Mount	116
P65-16-XLH-RR w/ Mount Pipe	149	Pipe	
P65-16-XLH-RR w/ Mount Pipe	149	ERICSSON AIR 21 B4A B2P w/ Mount	116
LGP21401	149	Pipe	
LGP21401	149	ERICSSON AIR 21 B4A B2P w/ Mount	116
LGP21401	149	Pipe	440
LGP21401	149	ERICSSON AIR 21 B4A B2P w/ Mount Pipe	116
LGP21401	149	KRY 112 144/1	116
LGP21401	149	KRY 112 144/1	116
LGP21901	149	KRY 112 144/1	116
LGP21901	149	Platform Mount (LP 712-1)	116
LGP21901	149	GPS A	84
LGP21901	149		84
LGP21901	149	Side Arm Mount [SO 701-1]	04
LGP21901	149		

**MATERIAL STRENGTH** 

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi	Reinf 53.15 ksi	53 ksi	65 ksi
Reinf 52,86 ksi	53 ksi	65 ksi	Reinf 53.24 ksi	53 ksi	67 ksi
Reinf 63,23 ksi	63 ksi	80 ksi	Reinf 53,27 kai	53 ksi	65 ksi
Reinf 53.12 ksi	53 ksi	67 ksi	Reinf 63 25 ksi	63 ksi	80 ksi

### **TOWER DESIGN NOTES**

1. Tower is located in Fairfield County, Connecticut.

- Tower is located in Painted County, Connected.
   Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
   Tower is also designed for a 38 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
   Deflections are based upon a 50 mph wind.
- 5. TOWER RATING: 98.4%



AXIAL 61 K

TORQUE 1 kip-ft REACTIONS - 85 mph WIND



Paul J Ford and Company 250 E. Broad Street Suite 600 Columbus, OH 43215

Phone: 614.221.6679 FAX: 614.448.4105

	lob: 160' MP; Stan	ford, CT; BRG 2044 (A	4) 943097
)	Project: PJF 37513-231		10
	Client: Crown Castle	Drawn by: Joshua Frybarger	App'd:
	Code: TIA/EIA-222-F	Date: 03/26/14	Scale: NTS
	Colle		Dun No -

### Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material

### TIA Rev F

Site Data

BU#: 806953

Site Name:

App #:

Qty:

Diam:

Rod Material:

Strength (Fu):

Yield (Fy):

**Bolt Circle:** 

Pole Manufacturer:

**Anchor Rod Data** 

20

2.25

A615-J

100

75

64.48

ksi

ksi

in

Other

Reactions		
Moment:	4568	ft-kips
Axial:	45	kips
Shear:	42	kips

If No stiffeners, Criteria:

AISC ASD <-Only Applicable to Unstiffened Cases

**Anchor Rod Results** 

Maximum Rod Tension:

Allowable Tension: Anchor Rod Stress Ratio: 167.8 Kips 195.0 Kips

86.1% Pass

Service, ASD Fty\*ASIF

Stiffened

Plate Data		
Diam:	70.48	in
Thick:	2.5	in
Grade:	60	ksi
Single-Rod B-eff:	9.00	in

Stiffener Data (Welding at both sides)		
Config:	1	*
Weld Type:	Both	
Groove Depth:	0.375	in **
Groove Angle:	45	degrees
Fillet H. Weld:	0.375	in
Fillet V. Weld:	0.3125	in
Width:	6	in
Height:	18	in
Thick:	0.75	in
Notch:	0.75	in
Grade:	50	ksi
Weld str.:	70	ksi

Pole Data		
Diam:	56	in
Thick:	0.4375	in
Grade:	65	ksi
# of Sides:	12	"0" IF Round
Fu	80	ksi
Reinf. Fillet Weld	0	"0" if None

Stress	Increase	Factor	
ASIF:	1.333		

**Base Plate Results** Flexural Check Base Plate Stress: 33.8 ksi Allowable Plate Stress: 60.0 ksi Base Plate Stress Ratio: 56.4% Pass

Stiffened Service, ASD 0.75\*Fy\*ASIF Y.L. Length: N/A, Roark

**Stiffener Results** 

Horizontal Weld: 68.6% Pass Vertical Weld: 52.3% Pass Plate Flex+Shear, fb/Fb+(fv/Fv)^2: 18.3% Pass Plate Tension+Shear, ft/Ft+(fv/Fv)^2: 69.3% Pass Plate Comp. (AISC Bracket): 69.2% Pass

**Pole Results** 

Pole Punching Shear Check:

10.1% Pass





<sup>\* 0 =</sup> none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

<sup>\*\*</sup> Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

# foundation loads

kips	kips	- ff-kips
45	42	4568
Tower or Pole Weight =	Total Horizontal Force =	Overturning Moment =

## soil properties

	bc	Ksi	=
1.5	125	20	66
Safety factor against overturning =	Soil density =	Allowable soil bearing =	Depth to water table =

# mat dimensions

¥	#	#	<b>#</b>	
3.5	2	56	56	0
depth to bottom of footing =	Footing thickness =	Footing Width =	Footing Length =	Tower/Pole Center Offset =

### **4** (ksi) -507 k conc Concrete strength = $f_c$ = 2.861 ksf q Overturning Moment = 4568 ft-k 552 k þ 26 ft x 26 ft Wt = 45 keccentricity = 8.656 ft Rebar = (72) #8 bars by 25.5 ft long 125.19 yd<sup>3</sup> Volume of concrete = d Horiz Load = 42 k 0# water table below ftg

ijĢ

# reinforcing steel = (18) #8 @ 18 in o.c. ea way top and bottom

# Summary of analysis results

(Stress Ratio = 0.999) < CONTROLLING CRITERIA Overturning Moment:

Calculated Overturning Moment = 4778 ft-kips

minimum cover over rebar = 3 inches

8

Rebar strength = F<sub>y</sub> =

Resisting Moment = 7176 ft-kips

1.502 > 1.5 okay Factor of Safety against overturning =

Soil Bearing

(Stress Ratio = 0.143)

Net Soil Bearing Resistance = 20 ksf

Calculated Soil Bearing Pressure = 2.861 ksf < 20 ksf okay

(Stress Ratio = 0.744)

Bending Moment (Stress Ratio = 0.744)
Ultimate Bending Moment Resistance = 3526 ft-kips

Calculated Ultimate Bending Moment = 2624 ft-kips < 3526 ft-kips okay

Bending Shear

(Stress Ratio = 0.245)

Ultimate Bending Shear Resistance = 1643 kips

Calculated Ultimate Bending Shear = 403 kips < 1643 kips okay

### MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

BU NUMBER; SITE NAME BU #806953; BRG 2044 (A) 943097

APP: 200735 REV. 3: WO: 704036

SITE ADDRESS

### 69 GUINEA RD. (CAMP ROCKY CRAIG STAMFORD, CONNECTICUT 06903 FAIRFIELD COUNTY

### **PROJECT NOTES**

- 1. DETAILED FIELD INFORMATION REGARDING INTERFERENCES AND/OR EXISTING FIELD CONDITIONS MAY BE AVAILABLE ON CROWN'S CCISITES AND FROM CONTRACTOR'S PRE-MOD MAPPING. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS AND COORDINATE WITH THE AVAILABLE SOURCES OF INFORMATION ABOVE AND WITH THE PROJECT PLANS BEFORE PROCEEDING WITH THE WORK. CONTRACTOR SHALL IMMEDIATELY REPORT ANY AND ALL DISCREPANCIES TO PAUL J. FORD AND COMPANY AND CROWN CASTLE FIELD PERSONNEL BEFORE PROCEEDING WITH THE WORK.
- ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
- ALL STRUCTURAL BOLTS SHALL BE FIELD INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31 2009.
- 4. (A.) <u>DTI'S REQUIRED:</u> ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND DETAILS ON SHEET S-3 FOR REQUIREMENTS ON THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
  - (B.) EFFECTIVE 5/30/2012: UNTIL FURTHER NOTICE, CROWN CASTLE WILL ACCEPT AJAX BOLTS TIGHTENED USING AISC "TURN-OF-NUT" METHOD. INSTALLERS SHALL FOLLOW CROWN GUIDELINES FOR AISC "TURN-OF-NUT" METHOD AND ALSO PROVIDE COMPLETE INSPECTION DOCUMENTATION IN THE PMI. PRIOR TO STARTING WORK, CONTRACTOR SHALL CONSULT WITH CROWN ENGINEERING TO DETERMINE WHETHER THIS POLICY IS STILL IN PLACE.
  - (C.) REQUIREMENT EFFECTIVE 04/20/2013, PER CROWN CASTLE DIRECTIVE: ANY AND ALL STRUCTURAL BOLTS THAT ARE TIGHTENED TO THE PRETENSIONED CONDITION USING THE PIGE TURN-OF-NUT TENSIONING PROCEDURE (NON-TENSION CONTROLLED [NON-TC] BOLTS AND/OR BOLTS WITHOUT DTI'S INSTALLED) SHALL BE INSPECTED ONSITE BY AN INDEPENDENT THIRD-PARTY BOLT INSPECTOR, AS APPROVED BY CROWN, THIS INSPECTION IS REQUIRED TO BE AN ONSITE FIELD INSPECTION. THE THIRD-PARTY BOLT INSPECTION SHALL FOLLOW THE PUBLISHED CROWN CASTLE INSPECTION PROCEDURE "MI NON-TC BOLT INSPECTION", DATED APRIL 2013. THE THIRD-PARTY BOLT INSPECTOR SHALL PREPARE A FULLY DOCUMENTED BOLT INSPECTION REPORT, AS SPECIFIED BY CROWN, AND SHALL SUBMIT A COPY OF THE BOLT INSPECTION REPORT TO THE MI INSPECTOR, THE EOR, AND TO CROWN CASTLE.

### **PROJECT CONTACTS:**

### MONOPOLE OWNER:

CROWN CASTLE

46 BROADWAY ALBANY, NY 12204

TSA: ANDREW BAZINET AT ANDREW.BAZINET@CROWNCASTLE.COM

PH: (585) 899-3442

MOD PM: EVA MORALES AT EVA.MORALES@CROWNCASTLE.COM PH: (704) 405-6612

### STRUCTURAL ENGINEER OF RECORD (EOR): PAUL J. FORD AND COMPANY

PAUL J. FORD AND COMPANY 250 EAST BROAD STREET, SUITE 600 COLUMBUS, OHIO 43215-3708

CONTACT: JOSH FRYBARGER AT JFRYBARGER@PJFWEB.COM

PHONE: 614-221-6679

### **DESIGN STANDARD**

THIS REINFORCEMENT DESIGN IS BASED UPON THE REQUIREMENTS OF THE TIMEIA-222-F-1996 STRUCTURAL STANDARD FOR ANTENNA SUPPORTING STRUCTURES AND ANTENNAS, USING A DESIGN BASIC WIND SPEED OF 85 MPH (FASTEST MILE) WITH NO ICE, 38 MPH WITH 3/4 INCH ICE AND 50 MPH SERVICE LOADS.

REFER TO THE POLE DESIGN AND ANTENNA LOADING DOCUMENTED IN THE PJF STRUCTURAL ANALYSIS FOR THIS SITE (PJF#37513-2318), DATED 3-25-2014.

### THIS PROJECT INCLUDES THE FOLLOWING REINFORCING ELEMENTS:

SHAFT REINFORCING

SHEET INDEX		
SHEET NUMBER	DESCRIPTION	
T-1	TITLE SHEET	
S-1	GENERAL NOTES	
S-2	GENERAL NOTES	
S-3	AJAX BOLT DETAIL	
S-4	MONOPOLE PROFILE	
S-5	SHAFT REINF. CHART AND DETAIL	
S-6	MI CHECKLIST	

DATE:

CROWN CASTLE PROJECT: BU #806953; BRG 2044 (A) 943097; STAMFORD, CONNECTICUT MONOPOLE RETROFIT PROJECT MASTER NOTES DOCUMENT (REV. 2, 1/22/2009)

- CROWN CASTLE PROJECT: BU #808095: BRG 2044 (A) 943097; STAMFORD, CONNECTICUT
  MONOPOLE RETROFIT PROJECT MASTER NOTES DOCUMENT (REV. 2, 1/2/2/2008)

  1, A. GENERAL NOTES

  A. GENERAL NOTES

  1. IT STALL BE HER RESPONSIBILITY OF THE CONTRACTOR TO FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS PRIOR TO FABRICATION AND CONSTRUCTION. THESE DRAWNIGS WERE PREPARED FROM INFORMATION AND DOCUMENTS PROVIDED TO PAUL 1 FORD 2 COMPANY SO FOROW CASTLE. HIS WIND AND CONTRACTOR AND

- - B. (SECTION NOT USED)

- C. SPECIAL INSPECTION AND TESTING

  ALL WORK SHALL BE SUBJECT TO REVIEW AND OBSERVATION BY THE OWNER'S REPRESENTATIVE AND THE OWNER'S AUTHORIZED INDEPENDENT INSPECTION AND TESTING AGENCY. REFER TO CROWN CASTLE DOCUMENT ENG SOW-1006 FOR SPECIFICATION.

  ANY SUPPORT SERVICES PERFORMED BY THE ENGINEER DURING CONSTRUCTION SHALL BE DISTINGUISHED FROM CONTINUOUS AND DETAILED INSPECTION SERVICES WHICH ARE FURNISHED BY OTHERS. THESE SUPPORT SERVICES PERFORMED BY THE ENGINEER ARE PERFORMED SOLELY FOR THE PURPOSE OF ASSISTING IN QUALITY CONTROL AND IN ACHIEVING CONFORMANCE WITH CONTRACT DOCUMENTS. THEY DO NOT GUARANTEE CONTRACTOR'S PERFORMANCE AND SHALL NOT BE CONSTRUCTED AS SUPPERVISION OF CONSTRUCTION.

  OSSERVED DISCREPANCIES BETWEEN THE WORK AND THE CONTRACT DOCUMENTS SHALL BE CORRECTED BY THE CONTRACTOR AND ADDITIONAL COST.

  AN INDEPENDENT QUALIFIED INSPECTION/TESTING AGENCY SHALL BE SELECTED, RETAINED AND PAID FOR BY THE CONTRACTOR THE SOLE PURPOSE OF INSPECTION, TESTING DOCUMENTING, AND APPROVING ALL WELDING AND FIELD WORK PERFORMED BY THE CONTRACTOR.

  (A.) ACCESS TO ANY PLACE WHERE WORK IS BEING DOME SHALL BE PERMITTED AT ALL TIMES, (B.) THE INSPECTION AS DECRESABILITY TO COORDINATE THE WORK SCHEDULE WITH THE TESTING AGENCY. THE CONTRACTOR'S RESPONSIBILITY TO COORDINATE THE WORK SCHEDULE WITH THE TESTING AGENCY. THE CONTRACTOR STALL ALL ALLOW FOR A DECOMET EITHE AND ACCESS FOR THE CONTRACTOR SHALL BLACE HER ADDITIONS.

  THE INSPECTION AND TESTING AGENCY SHALL BLIFT THE FISH THE FOLLOWING SERVICES FOR THE CONTRACTOR SHALL ALLOW FOR ADECUMENT HIME AND EXCESS FOR THE TESTING AGENCY. THE CONSTRUCTION DRAWNING. THE TESTING AGENCY TO PERFORM THEIR DUTIES.

  THE INSPECTION AND TESTING AGENCY SHALL BLIFT THE FISH THE FOLLOWING SERVICES FOR THE CONTRACTOR SHALL BLIFT THE FISH THE FISH AND ACCESS FOR THE CONTRACTOR SHALL BLIFT THE FISH THE FISH AND ACCESS FOR THE FOUNDED, THAT THE SOTH OR PROVINCE OF THE FISH OF AND COMMENSURATE WITH THE SET FOR AND TO CONTRACTOR SHALL HAVE THE TRINING, CREDENTIALS, AND EXPERTIEBLY A PROPRIMATE
- AND COMMENSURALE WITH THE SCOPE AND TYPE OF INSPECTION WORK TO BE PERFORMED.

  (1.5) PERFORM CONTINUOUS ON-SITE OBSERVATION, INSPECTION, VERIFICATION, AND TESTING DIRING THE TIME THE CONTRACTOR IS WORKING ON-SITE. AGENCY SHALL NOTIFY OWNER IMMEDIATELY WHEN FIELD PROBLEMS OR DISCREPANCIES OCCUR.

  B. FOUNDATIONS, CONCRETE, AND SOLP PERPARATION -, NOT REQUIRED)
- C. CONCRETE TESTING PER ACI (NOT REQUIRED)

- D. STRUCTURAL STEEL
  (1) CRECK THE STEEL ON THE JOB WITH THE PLANS,
  (2) CHECK MILL CERTRICATIONS.
  (3) CHECK MILL CERTRICATIONS.
  (3) CHECK GRADE OF STEEL MEMBERS, AND BOLTS FOR CONFORMANCE WITH DRAWINGS.
  (4) INSPECT STEEL MEMBERS FOR DISTORTION, EXCESSIVE RUST, FLAWS AND BURNED HOLES.
  (5) CALL FOR LABORATORY TEST REPORTS WHEN IN DOUBT.
  (6) CHECK STEEL MEMBERS FOR SIZES, SWEEP AND DIMENSIONAL TOLERANCES.
  (7) CHECK FOR SURFACE FINISH SPECIFIED, GALVANIZED.
  (8) CHECK BOLT TIGHTENING ACCORDING TO AISC TURN OF THE NUT METHOD.

- F. SPECIAL INSPECTION OF EXISTING SHAFT-TO-FLANGE WELD CONNECTIONS: (NOT REQUIRED)
- G. REPORTS:
  (1.7) COMPILE AND PERIODICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER.
- (1), COMPILE AND PERIODICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER.

  THE INSPECTION PLAN CUTLINED HEREIN IS INTENDED AS A DESCRIPTION OF GENERAL AND SPECIFIC TEMS OF CONCERN. IT IS NOT INTENDED TO BE ALL-INCLUSIVE. IT DOES NOT LIMIT THE TESTING AND INSPECTION AGENCY TO THE TIEMS LISTED. ADDITIONAL TESTING, INSPECTION, AND CHECKING MAY BE REQUIRED AND SHOULD BE ANTICIPATED. THE TESTING AGENCY SHALL USE THEIR PROFESSIONAL JUDGMENT AND KNOWLEDGE OF THE JOB SITE CONDITIONS AND THE CONTRACTOR'S PERFORMANCE TO DECIDE WHAT OTHER THEMS REQUIRE ADDITIONAL ATTENTION. THE TESTING AGENCY'S JUDGMENT MUST PREVAIL ON TEMS NOT SPECIFICALLY COVERED, ANY DISCREPANCIES AND PROBLEMS SHALL BE BROUGHT IMMEDIATELY TO THE OWNERS ATTENTION. RESOLUTIONS ARE NOT TO BE MADE WITHOUT THE OWNERS REVIEW AND SPECIFIC WRITTEN CONSENT. THE OWNER RESERVES THE RIGHT TO TETEMBRE WHAT IS AN ACCEPTABLE RESOLUTION OF DISCREPANCIES AND PROBLEMS.

  AFTER EACH INSPECTION, THE TESTING AGENCY WILL PREPARE A WRITTEN ACCEPTANCE OR REJECTION WHICH WILL BE GIVEN TO THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WRITTEN ACTION WILL GIVE THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WRITTEN ACTION WILL GIVE THE CONTRACTOR AND FILED CONTRACTION, AND/OR LODGING OF STRUCTURAL TEMS.

  RESPONSIBILITY: THE TESTING AGENCY DOES NOT RELIEVE THE CONTRACTOR CONTRACTUAL OR STATUTION'S DELIGATIONS. THE CONTRACTOR HAS THE SOLE RESPONSIBILITY OR ANY DEVIATIONS FROM THE OFFICIAL CONTRACT DOCUMENTS. THE TESTING AGENCY WILL NOT REPLACE THE CONTRACTOR'S QUALITY CONTROL PERSONNEL.



J.J.F.

PPROVED BY

DATE: 3-25-2014

- STRUCTURAL STEEL
  STRUCTURAL STEEL MATERIALS, FABRICATION, DETAILING, AND WORKMANSHIP SHALL CONFORM
  TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:
- IERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC): PECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL

- TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:
  BY THE MERICAN INSTITUTE OF STEEL, CONSTRUCTION (AISC):

  (A.) \*\*\*SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS.\*\*

  (B.) \*\*SPECIFICATION FOR STRUCTURAL JOINTS USING ASTM A325 OR A490 BOLTS, "AS APPROVED BY THE RESEARCH COUNCIL ON STRUCTURAL CONNECTIONS OF THE ENGINEERING FOUNDATION.

  (C.) \*\*CODE OF STANDARD PRACTICE FOR STEEL BUILDINGS AND BRIDGES\* (PARAGRAPH 4.2.1 SPECIFICALLY EXCLUDED).

  BY THE AMERICAN WELDING SOCIETY (AWB):

  (A.) \*\*STRUCTURAL WELDING SCOED \*\*STEEL BUILDINGS AND BRIDGES\* (PARAGRAPH 4.2.1 SPECIFICALLY EXCLUDED).

  BY THE AMERICAN WELDING SOCIETY (AWB):

  (B.) \*\*SYMBOLS FOR WELDING AND NON-DESTRUCTIVE TESTING\*

  ANY MATERIAL OR WORKMANSHIP WHICH IS OBSERVED TO BE DEFECTIVE OR INCONSISTENT WITH THE CONTRACT DOCUMENTS SHALL BE CORRECTED, MODIFIED, OR REPLACED AT THE CONTRACT DOCUMENTS SHALL BE CORRECTED, MODIFIED, OR REPLACED AT THE CONTRACT DOCUMENTS SHALL BE CORRECTED, MODIFIED, OR REPLACED AT THE CONTRACT DOCUMENTS SHALL BE CORRECTED, MODIFIED, OR REPLACED AT THE CONTRACT DOCUMENTS SHALL BE CORRECTED, MODIFIED, OR REPLACED AT THE CONTRACTOR'S EXPENSE.

  INCHEN ALL STRUCTURAL BOLTS, INCLUDING THE ALAX M20 BOLTS WITH SHEAR SLEEVES, ACCORDING TO THE REQUIREMENTS OF THE AISC "TURN OF THE NUT" METHOD. TIGHTEN BOLTS 1/3 TURN PAST THE SNUIG TIGHT CONDITION AS DEFINED BY A SISC.

  WELDED CONNECTIONS SHALL CONFORM TO THE LATEST REVISED CODE OF THE AMERICAN WELDING SOCIETY, AWB DIJ. ALL WELD ELECTRODES SHALL BE EROXX UNLESS NOTED OTHERWISE ON THE DRAWINGS.

  ALL WELDED CONNECTIONS SHALL BE MADE BY WELDERS CERTIFIED BY AWS, CONTRACTOR SHALL SUBMIT WELDERS' CERTIFICATION AND QUALIFICATION DOCUMENTATION TO THE OWNER'S TESTING AGENCY FOR REVIEW AND APPROVAL PRIOR TO CONSTRUCTION.

  STRUCTURAL STEEL PLATES SHALL CONFORM TO ASTM A572 GRADE 65 (FY = 66 KSI MIN.) UNLESS NOTED OTHERWISE ON THE DRAWINGS.

  SURFACES OF EXISTING STEEL SHALL BE PREPARED AS REQUIRED FOR FIELD WELDING.

  UNLESS OTHERWISE ON THE DRAWINGS.

  SUR

- STEEL AND THE INSPECTION/TESTING AGENCY SHALL VERIFY PROPOSED LAYOUT, LOCATION, AND DIMENSIONS.

  ANY REQUIRED CUTS IN THE STEEL SHALL BE CAREFULLY CUT BY MECHANICAL METHODS SUCH AS RRILLING, SAW CUTTING, AND GRINDING. THE CONTRACTOR IS RESPONSIBLE TO PREVENT ANY DAMAGE TO THE COAK CABLES, ANDIOR OF THER FOLDIFMENT ANDIOR THE STRUCTURE, BURING THE CUTTING WORK. ANY DAMAGE TO THE COAX CABLES, ANDIOR OTHER EQUIPMENT ANDIOR THE STRUCTURE, RESULTING FROM THE CONTRACTOR'S ACTIVITIES SHALL BE REPAIRED AT THE CONTRACTOR'S EXPENSE. THE INSPECTION/TESTING AGENCY SHALL CLOSELY AND CONTINUOUSLY MONITOR THIS ACTIVITY.

  ALL REQUIRED CLTS SHALL BE CUT WITHIN THE DIMENSIONS SHOWN ON THE DRAWINGS. NO CUTS SHALL EXTEND BEYOND THE OUTLINE OF THE DIMENSIONS SHOWN ON THE DRAWINGS. ALL CUT EDGES THAT ARE TO BE FIELD WELDED SHALL BE PREPARED FOR FIELD WELDING FERR AND IT, AND AS SHOWN ON THE DRAWINGS. ALL CUT EDGES THAT ARE TO BE FIELD WELDED SHALL BE PREPARED FOR FIELD WELDING FERR AND IT, AND AS SHOWN ON THE DRAWINGS. THE INSPECTION THE STRUCTURE SHALL BE CROWN ON THE DRAWINGS. THE INSPECTION THE STRUCTURE SHALL BE CROWN ON THE DRAWINGS. THE INSPECTION TESTING AGENCY SHALL CLOSELY AND CONTINUOUSLY MONITOR THIS ACTIVITY.
- BASE PLATE GROUT (NOT REQUIRED)
- FOUNDATION WORK (NOT REQUIRED)

- CAST-IN-PLACE CONCRETE (NOT REQUIRED)
- EPOXY GROUTED REINFORCING ANCHOR RODS (NOT REQUIRED)
- TOUCH UP OF GALVANIZING
  THE CONTRACTOR SPALL TOUCH UP ANY ANDIOR ALL AREAS OF GALVANIZING ON THE EXISTING
  STRUCTURE OR NEW COMPONENTS THAT ARE DAMAGED OR ABRADED DURING CONSTRUCTION.
  GALVANIZED SURFACES DAMAGED DURING TRANSPORTATION OR ERECTION AND ASSEMBLY AS
  WELL AS ANY AND ALL ABRASIONS, CUTS, FIELD DRILLING, AND ALL FRELD WELDING SHALL BE
  TUCKHED UP WITH TWO (2) COATS OF ZRC-BRAND ZING-RICH COLD GALVANIZING COMPOUND, FILM
  THICKNESS PER COAT SHALL BE: WET 3.0 MILS; DRY 1.5 MILS. APPLY PER ZR (MANUPACTURER)
  RECOMMENDED PROCEDURES. CONTACT ZRC AT 1-80-0831-3275 FOR PRODUCT INFORMATION.
  CONTRACTOR SHALL CLEAN AND PREPARE ALL FIELD WELDS ON GALVANIZED AND PRIME PAINTED
  SURFACES FOR TOUCH-UP COATING IN ACCORDANCE WITH AWS D.1. THE OWNERS TESTING
  AGENCY SHALL VERIEY THE PREPARED SURFACE PRIOR TO APPLICATION OF THE TOUCH-UP
  COATING.
- AGENCY SHALL VERIFY THE PREPARED SURFACE PRIOR TO APPLICATION OF THE TOUGHUP COATING.
  THE OWNER'S TESTING AGENCY SHALL TEST AND VERIFY THE COATING THICKNESS AFTER THE CONTRACTOR HAS APPLIED THE ZRC COLD GALVANIZING COMPOUND AND IT HAS SUFFICIENTLY DRIED. AREAS FOUND TO BE INADEQUATELY COATED, SHALL BE RE-COATED BY THE TESTING AGENCY.
- HOT DIP GALVANIZING
  HOT-DIP GALVANIZA LL STRUCTURAL STEEL MEMBERS AND ALL STEEL ACCESSORIES, BOLTS,
  WASHERS, ETC, PER ASTM A123 OR PER ASTM A153, AS APPROPRIATE,
  PROPERLY PREPARE STEEL ITEMS FOR GALVANIZING,
  DRILL OR PUNICH WEEP ANDIOR DRAINAGE HOLES AS REQUIRED,
  ALL GALVANIZING SHALL BE DONE AFTER FABRICATION IS COMPLETED AND PRIOR TO FIELD
- - PERPETUAL INSPECTION AND MAINTENANCE BY THE OWNER
    AFTER THE CONTRACTOR HAS SUCCESSFULLY COMPLETED THE INSTALLATION OF THE MONOPOLE
  - PERPETUAL INSPECTION AND MAINTENANCE BY THE OWNER
    AFTER THE CONTRACTOR THAS SUCCESSFULLY COMPLETED THE INSTALLATION OF THE MONOPOLE
    REINFORCING SYSTEM AND THE WORK HAS BEEN ACCEPTED BY THE OWNER. THE OWNER WILL BE
    RESPONSIBLE FOR THE LONG TERM AND PERPETUAL INSPECTION AND MAINTENANCE OF THE POLE
    AND REINFORCING SYSTEM.
    THE MONOPOLE REINFORCING SYSTEM INDICATED IN THESE DOCUMENTS USES REINFORCING
    COMPONENTS THAT INVOLVE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL
    POLE STRUCTURE. THESE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL
    POLE STRUCTURE. THESE FIELD WELDING SYSTEM MAINTAINED AND COVERED WITH CORROSION
    PREVENTIVE COATING SUCH AS THE ZRG GALVANIZING COMPOUND SPECIFIED PREVIOUSLY. THE
    STRUCTURAL LOAD CARRYING CAPACITY OF THE REINFORCED POLE SYSTEM IS DEPENDENT UPON
    THE INSTALLED SIZE AND QUALITY, MAINTAINED SOUND CONDITION AND STRENGTH OF THESE FIELD
    WELDED CONNECTIONS. ANY CORROSION OF, DAMAGE TO, FATGUE, FRACTURE, AND/OR
    DETERIORATION OF THESE WELDS AND/OR THE CONNECTED COMPONENTS WILL RESULT IN THE
    LOSS OF STRUCTURAL LOAD CARRYING CAPACITY AND MAY LEAD TO FAILURE OF THE
    STRUCTURAL SYSTEM. THEREFORE, IT IS IMPERATIVE THAT THE OWNER REGULARLY INSPECTS,
    MAINTAINS, AND REPAIRS AS NECESSARY, ALL OF THESE WELDS, CONNECTIONS, AND
    COMPONENTS FOR THE LIFE OF THE STRUCTURE.

    THE OWNER SHALL REFER TO TIMELE 2222-F-1996, SECTION 14 AND ANNEX E FOR RECOMMENDATIONS
    FOR MAINTENANCE AND INSPECTION. THE REQUENCY OF THE INSPECTION AND MAINTENANCE
    INTERVALS IS TO BE DETERMINED BY THE OWNER BASED UPON ACTUAL SITE AND ENVIRONMENTAL
    CONDITIONS. PAUL J. FORD SCOMENT OF THE SITUCTURAL SYSTEM THE POTTION OF THESE WELD WELDED ON THE REPRORED THE THE PROPERIOR OF THE SITUCTURAL SYSTEM THEODOLY
    HEROPACH THE STRUCTURE OF THE STRUCTURE SECTION OF THE SEPCREDING OF THE SEPC



46 BROADWAY ALBANY, NY 12204 PH: (585) 890-3442 FAX: (585) 890-344

### AJAX BOLT NOTE SHEET: REV. 1.4, 5-20-2013

NOTES

- 1. ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
- 2. ALL STRUCTURAL BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
- 3. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND DETAIL BELOW FOR THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
- 4. ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. DTI'S SHALL BE THE SQUIRTER® STYLE, MADE TO ASTM F959 LATEST REVISION; AND HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A HARDNESS OF RC 38 OR HIGHER.

### NOTES FOR AJAX M20 'ONE-SIDE' BOLTS WITH DIRECT TENSION INDICATORS (DTI'S):

DTI'S REQUIRED: DTI'S SHALL BE "SELF-INDICATING" SQUIRTER® STYLE DTI'S MADE WITH SILICONE EMBEDDED IN THEM, INSPECTED BY MEANS OF THE VISUAL EJECTION OF SILICONE AS THE DTI PROTRUSIONS COMPRESS. SQUIRTER® DTI'S SHALL BE CALIBRATED PER MANUFACTURER'S INSTRUCTIONS PRIOR TO USE.

THE DIRECT TENSION INDICATOR (DTI) WASHERS SHALL BE THE "SQUIRTER® STYLE" AS MANUFACTURED BY:

APPLIED BOLTING TECHNOLOGY PRODUCTS, INC. 1413 ROCKINGHAM ROAD BELLOWS FALLS, VERMONT, USA 05101 PHONE 1-800-552-1999

WEBSITE: WWW.APPLIEDBOLTING.COM

DISTRIBUTORS OF SQUIRTER® DTI'S: <u>HTTP://WWW.APPLIEDBOLTING.COM/APPLIED-BOLTING-DISTRIBUTORS.HTML</u>

DTI: USE DIRECT TENSION INDICATOR (DTI) WASHERS COMPATIBLE WITH 20 MM (M20) NOMINAL A325 BOLTS FOR THE AJAX M20 BOLTS, DTI'S SHALL NOT BE HOT-DIP GALVANIZED. DTI'S SHALL BE MECHANICALLY GALVANIZED (MG) BY THE COLD MECHANICAL PROCESS ONLY AS PROVIDED BY THE DTI MANUFACTURER.

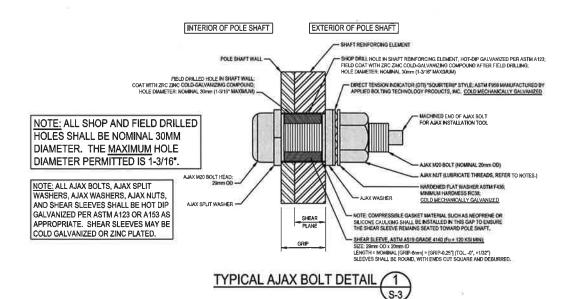
HARDENED WASHERS REQUIRED: USE A HARDENED WASHER FOR A 20 MM (M20) NOMINAL BOLT BETWEEN THE TOP OF THE DIRECT TENSION INDICATOR (DTI) WASHER AND THE NUT OF THE AJAX M20 BOLTS. HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A MINIMUM HARDNESS OF RC 38 OR HIGHER. THE HARDENED WASHERS SHALL BE MECHANICALLY GALVANIZED BY THE COLD MECHANICAL PROCESS. ALTERNATIVELY, CORRECTLY MADE HOT DIP GALVANIZED HARDENED FLAT WASHERS HAVING A MINIMUM HARDNESS OF RC 38 CAN BE USED; CONTRACTOR SHALL PROVIDE DOCUMENTATION OF WASHER SPECIFICATION AND HARDNESS.

NUT LUBRICATION REQUIRED: PROPERLY LUBRICATE THE THREADS OF THE NUT OF THE AJAX BOLT SO THAT IT CAN BE PROPERLY TIGHTENED WITHOUT GALLING AND/OR LOCKING UP ON THE BOLT THREADS. CONTRACTOR SHALL FOLLOW DTI MANUFACTURER INSTRUCTIONS FOR PROPER LUBRICATION AND TIGHTENING.

NOTE: COMPLETELY COMPRESSED DTI'S SHOWING NO VISIBLE REMAINING GAP ARE ACCEPTABLE. DTI WASHERS SHALL BE PLACED DIRECTLY AGAINST THE OUTER AJAX WASHER WITH THE DTI BUMPS FACING AWAY FROM THE AJAX WASHER. PLACE A HARDENED WASHER BETWEEN THE DTI AND THE AJAX NUT. THE DTI BUMPS SHALL BEAR AGAINST THE UNDERSIDE OF A HARDENED FLAT WASHER, NEVER DIRECTLY AGAINST THE NUT.

CONTRACTOR SHALL FOLLOW DTI MANUFACTURER'S INSTRUCTIONS FOR INSTALLATION, LUBRICATION, TIGHTENING AND INSPECTION.

INSPECTION REQUIRED: ALL AJAX BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009, BY A QUALIFIED BOLT INSPECTOR. DURING INSTALLATION, THE BOLT INSPECTOR SHALL VERIFY AND DOCUMENT: THE SHOP-DRILLED AND FIELD-DRILLED HOLE SIZES; THE INSTALLATION OF THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S TENSIONING PROCEDURE. IN ADDITION, ALL AJAX BOLTS AND DTI'S SHALL BE VISUALLY INSPECTED ACCORDING TO THE DTI MANUFACTURER'S INSTRUCTIONS. THE BOLT INSPECTOR SHALL PROVIDE COMPLETE PHOTO DOCUMENTATION OF ALL BOLTS AFTER TIGHTENING CLEARLY SHOWING THE CONDITION OF THE DTI'S.

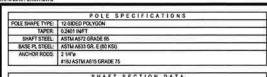




BU #806953; BRG 2044 (A) 943097 STAMFORD, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT No: 37513-2318 DRAWN BY: T.A.N. CHECKED BY: J.J.F. APPROVED BY

DATE:

ISSUE DATE OF PERMIT: 3-25-2014

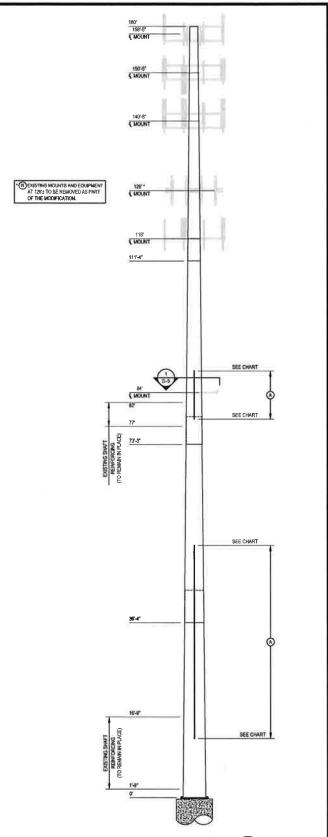


SHAFT SECTION	SECTION LENGTH (FT)	PLATE THICKNESS (IN)	LAP SPLICE		CROSS FLATS IN)
SECTION	V 17	fadi	JINY -	6106	@ BOTTOM
1	48,67	0.2500	F1.00	19,6000	31,2900
2	42.75	0,3438	54.00 69.00	29,6683	39.9120
3	42.67	0.4063	80.00	37,8486	48.0880
4	43.00	0.4375	80.00	45 6745	56.0000

CONTRACTOR SHALL PROVIDE ASTM AND SHEM PLATES BELOW SLIP JOINTS. THE SHM PLATES SHALL BE PLACED BETWEEN THE NEW SHAFT REMPORCEMENT AND THE EXISTING POLE SHAFT FROM THE SLIP JOINT TO THE NEW SHAFT REMPORCEMENT SHALLE PLATE LOCATION AND A EXTRA LONG SEXULCE SHAM SHALL BE PLACED SETMEN THE NEW UPPER AND LOWER SHAFT REMPORCEMENT PLATES AT THE SHAFT REMPORCEMENT SHIP PLATES AT THE SHAFT PLATES AT THE

### MODIFICATIONS:

- (A) INSTALL NEW SHAFT REINFORCING, SEE CHART.
- B REMOVE EXISTING MOUNT AND EQUIPMENT AT EL, 126's



POLE ELEVATION 1

CROWN CASTLE US PATENT NOS 8,046,972; 8,156,712; 7,849,559; 8.424,269 AND PATENT PENDING

PAUL J. FORD AND COMPANY
STRUCTURAL ENGINEERS
STRUCTURAL ENGINEERS
(814) 221-8679

CROWN CASTLE
48 BROADWAY ALBANY, NY 12204
Pt. (85) 889-3442
FX: (85) 599-3448

BU #806953; BRG 2044 (A) 943097 STAMFORD, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT No: 37513-2318 DRAWN BY: T.A.N. CHECKED BY: J.J.F. APPROVED BY:

> DATE: 3-25-2014

ISSUE DATE OF PERMIT: 3-25-2014

				NEW C	CIFLAT PLA	TE (65 KSI) R	EINFORCING S	CHEDULE				,
CROWN CASTLE CATALOG PART NUMBER	BOTTOM ELEVATION	TOP ELEVATION	FLAT#1 DEGREE SEPARATION	ELEMENT	ELEMENT LENGTH	ELEMENT QUANTITY	MINIMUM AJAX Bolts per Element	MINIMUM TOTAL AJAX BOLT QUANTITY	TERMINATION BOLTS (BOTTOM)	TERMINATION BOLTS (TOP)	MAXIMUM INTERMEDIATE BOLT SPACING	ESTIMATED TOTAL STEEL WEIGHT
CCHAFP- 06010020	12'-3"	32'-3"	3,7 & 11	1"x6"	20' - 0"	3	31	93	10	10	16"	1225 LBS
CCI-AFP- 06010020	32' - 4"	52' - 4"	3,78.11	1° # 6°	20' - 0°	3	31	93	10	10	16°	1225 LBS
CCFAFP- 06010010	78' - 6"	88' - 6"	3, 7 & 11	1° x 6°	10' - 0"	3	23	69	10	10	16"	612 LBS

### NOTES:

- 1) AIAX BOLTS ARE TO BE 20mm DUMETER WITH CORRESPONDING 29mm DUMETER SLEENE WITH MATCHING STEEL GRADE.
  2) ALL STEEL SHALL BE HOT JOP GALVANCED AFTER FARRICATION IN ACCORDANCE WITH ASTIM AI23. ALTERNATINELY, ALL NEWS I FFENER PLATE STEEL REINFORCING MAY BE COLD
  GALVANCED AS POLLOWS: APPLY VAININBIUM OF TWO COATS OF ZEAC SERVICE JOE. AVEX. COLD GALVANCED AND COMPOUND. FLM THICKNESS PER COAT SHALL BE: WET 3.0 MILLS; DRY
  1.5 MILS. APPLYPER ZRC (MANUFACTURER) RECOMMENDED PROCEDURES. CONTACT ZRC AT 1-800-831-9275 FOR PRODUCT INFORMATION,
  3) ALL REINFORCING SHALL BE ASTIM AST ZEAC RES
  4) WELDS ARE ASSUMED 680XOX OR GREATER. TERMINATION WELDS SHALL BE 38" FILLET WELDS.
  5) HOLES FOR AUX BOLTS AND SHEAR SLEEVES ARE 30mm UNILESS NOTED OTHERWISE.

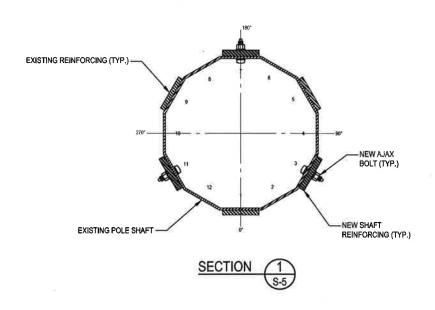
- 6) ALL SHIMS SHALL BE AST M A 36

		ACT SONOTON	SPLICEP	LATE INSTAL	LATION CHAR	Γ		
ELEVATION	FLAT PLATE THICKNESS	FLAT PLATE WIDTH	FLAT PLATE LENGTH	FLAT PLATE QUANTITY	WELD LENGTH PER SIDE	TOTAL WELD LENGTH	AJAX BOLTS PER SPLICE*	TOTAL STEEL WEIGHT
37-31	17.	8"	5.7	3		- 8	20	457 LBS

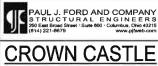
\*BOLTS INCLUDED IN THE TOTAL QUANTITY LISTED IN THE FLAT PLATE INSTALLATION CHART.

NEW SHIM CHART									
SHIM QUANTITY	SHIM WIDTH	SHIM LENGTH	SHIM THICKNESS	HOLE DIAMETER					
21	4"	4.	1/4*	5-114"					
39	4"	· L'	1/16"	1.14					

SHIM QUANTITIES ARE APPROXIMATE AND ARE FOR BIDDING PURPOSES







GENERAL
THE MODIFICATION INSPECTION (MI) IS A VISUAL INSPECTION OF TOMER MODIFICATIONS AND A REVIEW OF CONSTRUCTION INSPECTIONS
AND CHERR REPORTS TO ENSURE THE INSTALLATION WAS CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, INVALED THE
MODIFICATION DIVANTINGS AS DESIGNED BY THE ENGINEER OF RECORD (ECR).

THE M IS TO CONFIRM MISTALLATION CONFIGURATION AND WORKMANISHP ONLY AND IS NOT A REVIEW OF THE MIODIFICATION DESIGN TISELF, NOR DOES THE MI MISPECTOR TAME OWNERSHIP OF THE MODIFICATION DESIGN. OWNERSHIP OF THE STRUCTURAL MODIFICATION DESIGNE FFECTORINGS AND INTEREFOR RESIDES WITH THE EDRAT ALL THIS TERM.

ALL MIS SHALL BE CONDUCTED BY A CROWN ENGINEERING VENDOR (AEV) OR ENGINEERING SERVICE VENDOR (AESV) THAT IS APPROVED TO PERFORM ELEVATED WORK FOR CROWN. SEE ENG-BUL-10173 LIST OF APPROVED MI VENDORS

TO ENSURE THAT THE REQUIREMENTS OF THE MIJARE MET, IT IS VITAL THAT THE GENERAL CONTRACTOR (CC) AND THE MI MISSPECTOR BEGIN COMMANDALINDS AND COORDINATIONS AS SOLVEN AS POTS RECEIVED. IT IS EXPECTED THAT EXCHAPACTY MILL BE PROJECTIVE A PREJOHNS OUT TO THE OTHER PRATTY. IF CONTRACT MEDICANTORS NOT INCOMIN, CONTRICT YOUR CROWN FROM FORT OF CONTRACT (POC)

REFER TO ENG-SOW-10007 MODIFICATION INSPECTION SOW FOR FURTHER DETAILS AND REQUIREMENTS

MEMSPECTOR.

THE MEMSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A POFOR THE METO\_AT A MINIMUM.

- REVIEW THE REQUIREMENTS OF THE MICHECKLIST
   WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS

HE MINISPECTOR IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (GC) INSPECTION AND TEST REPORTS, REVIEWING THE OCUMENTS FOR ADHERENCE TO THE CONTRACT DOCUMENTS, CONDUCTING THE IN-FIELD INSPECTIONS, AND SUBMITTING THE MIREPORT

GENERAL CONTRACTOR.
THE GOIS REQUIRED TO CONTACT THE MI INSPECTOR AS SOON AS RECEIVING A PO FOR THE MODIFICATION INSTALLATION OR TURNKEY PROJECT TO, AT A MARMAM.

- REVENT THE REQUIREMENTS OF THE MI CHECKLET
   WORK WITH THE MINSPECTOR TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS. INCLUDING FOUNDATION INSPECTIONS
   BETTER UNDERSYMBO ALL INSPECTION AND TEST MORE REQUIREMENTS.

THE GC SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IN ACCORDANCE WITH THE REQUIREMENTS OF THE MI CHECKLIST AN DENGSOW-10007

RECOMMENDATIONS
THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING AND RECORT.

MINERCRIT

- IT IS SUGGESTED THAT THE GO PROVIDE A MINIALM OF 5 BUSINESS DAYS NOTICE, PREFERABLE 10, TO THE MI INSPECTIOR AS TO WHEN THE SITE WILL BE READY FOR THE MIT OR E CONDUCTED.

  THE GRADM INSPECTION CORROWNET CLOSELY THE MOVEMENT THE ENTIRE PROJECT.

  WHEN PROSSIBLE, IT IS PREFERRED TO HAVE THE GO AND MI INSPECTOR ON SITE SMALL TANEOUSLY FOR ANY GUY WIRE TENSIONING OR RE-TENSIONING OFFRATIONS.

  IT MAY BE BENEFICIAL TO INSTALL ALL TOWER MODIFICATIONS PRIOR TO CONDUCTING THE FOUNDATION INSPECTIONS TO ALLOW FOUNDATION AND MI INSPECTIONS IT OWNERS. WITH HONE SITE VISIT OF THE MIT OF HAVE ANY DEPICENCES CORRECTED DURING THE WITH THE MIT OF HAVE ANY DEPICENCES CORRECTED DURING THE WITH THE MIT OF HAVE ANY DEPICENCES CORRECTED DURING THE WITH THE MIT OF HAVE ANY DEPICENCES.

CAMPELIATION OR CELAYS IN SCHEOLED IN

FIRE OR AND MINSPECTOR AGREE TO A DATE ON WHICH THE MI WILL BE CONDUCTED, AND EITHER PARTY CANCELS OR DELAYS, CROWN
SHALL NOT BE RESPONGIBLE FOR ANY TWO COSTS, FEES, LOSS OF DEPOSITS AND/OR OTHER PERMITTES RELATED TO THE CANCELLATION OR
DELAY NUCHRED BY ESTHER PARTY FOR ANY TIME (E.G. TRAVEL AND LOCGING, COSTS OF KEEPING FOLD/HEADTH ON-STIE, ETC.). IF CROWN
CONTRACTS DIRECTLY FOR A THIRD PRATY ME (EXPERTINES MAY BE ANDE THE EVENT THAT THE DELAY/CANCELLATION IS CAUSED BY
WEATHER OR OTHER CONDITIONS THAT MAY COMPRIOMISE THE SAFETY OF THE PARTIES INVOLVED.

<u>CORRECTION OF FAILING MIS.</u> IF THE MODIFICATION INSTALLATION WOULD FAIL THE MI ("FAILED MIT), THE GC SHALL WORK WITH CROWN TO COORDINATE A REMEDIATION

- CORRECT FAILING ISSUES TO COMPLY WITH THE SPECIFICATIONS CONTAINED IN THE ORIGINAL CONTRACT DOCUMENTS AND
  COORDINATE A SUPPLEMENT MI
- OR, WITH CROWNS APPROVAL, THE GC MAY WORK WITH THE EOR TO RE-ANALYZE THE MODIFICATION/REINFORCEMENT USING THE AS BUILT CONDITION

IN VERFICATION INSPECTIONS.

GROWNINGSERVES THE RIGHT TO CONDUCT A MIVERIFICATION INSPECTION TO VERIFY THE ACCURACY AND COMPLETENESS OF PREVIOUSLY COMPLETED MINISPECTION(S) ON TOWER MODIFICATION PROJECTS.

ALL VERIFICATION INSPECTIONS SHALL BE HELD TO THE SAME SPECIFICATIONS AND REQUIREMENTS IN THE CONTRACT DOCUMENTS AND IN LOCORDANCE WITH EING SOW-10007

VERIFICATION INSPECTION MAY BE CONDUCTED BY AN INDEPENDENT AEVIAESV FIRM AFTER A MODIFICATION PROJECT IS COMPLETED, AS WARKED BY THE DATE OF AN ACCEPTED "PASSING MI," OR "PASS AS NOTED MI," REPORT FOR THE ORIGINAL PROJECT.

<u>PHOTOGRAPHS</u> BETWEEN THE GC AND THE MI INSPECTOR THE FOLLOWING PHOTOGRAPHS, AT A MINIMUM, ARE TO BE TAKEN AND INCLUDED IN THE MI

- PRE-CONSTRUCTION GENERAL SITE CONDITION
  PHOTOGRAPHS DURING THE REINFORCEMENT IMODIFICATION CONSTRUCTIONERECTION AND INSPECTION
  RAW MATERIALS
  PHOTOS OF ALL CRITICAL DETAILS
  FOUNDATION MODIFICATIONS
  WIELD PREPARATION
  BOLT INSTALLED CONDITION
  PHOLE INSTALLED CONDITION

- SURFACE COATING REPAIR
  POST CONSTRUCTION PHOTOGRAPHS
  FINAL INFIELD CONDITION

PHOTOS OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED INADEQUATE

THIS IS NOT A COMPLETE LIST OF REQUIRED PHOTOS, PLEASE REFER TO ENG-SOW-10007

ONSTRUCTIONINSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY EOR)	REPORT ITEM			
	PRE-CONSTRUCTION			
X	MI CHECKLIST DRAWINGS			
X	EOR APPROVED SHOP DRAWINGS			
х	FABRICATION INSPECTION			
NA.	FABRICATOR CERTIFIED WELD INSPECTION			
X	MATERIAL TEST REPORT (MTR)			
NA .	FABRICATOR NDE INSPECTION			
NA.	NDE REPORT OF MONOPOLE BASE PLATE (AS REQUIRED)			
X	PACKING SLIPS			
X	CONSTRUCTION INSPECTIONS			
X	CONSTRUCTION INSPECTIONS			
NA .	FOUNDATION INSPECTIONS			
NA	CONCRETE COMP, STRENGTH AND SLUMP TESTS			
NA.	POST INSTALLED ANCHOR ROD VERIFICATION			
NA.	BASE PLATE GROUT VERIFICATION			
NA.	CONTRACTOR'S CERTIFIED WELD INSPECTION			
NA.	EARTHWORK: LIFT AND DENSITY			
X	ON SITE COLD GALVANIZING VERIFICATION			
NA.	GUY WIRE TENSION REPORT			
X	GC AS-BUILT DOCUMENTS			
X	THIRD PARTY ONSITE INSPECTION OF BOLT PRETENSION PER CROWN REQUIREMENTS			
х	INSPECTION OF AJAX BOLTS AND DTI'S PER REQUIREMENTS ON SHEET S-3			
OFFICIAL TESTING AND INSPECTIONS:				
	POST-CONSTRUCTION			
	MI INSPECTOR REDLINE OR RECORD DRAWING(S)			
Х	THIRD PARTY ONSITE BOLT INSPECTION REPORT			
X X	THIRD PARTY ONSITE BOLT INSPECTION REPORT			
	THIRD PARTY ONSITE BOLT INSPECTION REPORT POST INSTALLED ANCHOR ROD PULL-OUT TESTING			

MICHECKLIST

PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 East Broad Street - Suste 600 - Columbia, Obio 43215 (614) 223-16579 **CROWN CASTLE** 

46 BROADWAY ALBANY, NY 12204

BU #806953; BRG 2044 (A) 943097 STAMFORD, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

37513-2318 DRAWN BY: T.A.N. CHECKED BY J.J.F. PROVED BY

ISSUE DATE OF PERMIT: 3-25-2014

### MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

BU NUMBER; SITE NAME BU #806953; BRG 2044 (A) 943097

APP: 200735 REV. 3; WO: 704036

SITE ADDRESS

### 69 GUINEA RD. (CAMP ROCKY CRAIG STAMFORD, CONNECTICUT 06903 FAIRFIELD COUNTY

### **PROJECT NOTES**

- 1. DETAILED FIELD INFORMATION REGARDING INTERFERENCES AND/OR EXISTING FIELD CONDITIONS MAY BE AVAILABLE ON CROWN'S CCISITES AND FROM CONTRACTOR'S PRE-MOD MAPPING. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS AND COORDINATE WITH THE AVAILABLE SOURCES OF INFORMATION ABOVE AND WITH THE PROJECT PLANS BEFORE PROCEEDING WITH THE WORK. CONTRACTOR SHALL IMMEDIATELY REPORT ANY AND ALL DISCREPANCIES TO PAUL J, FORD AND COMPANY AND CROWN CASTLE FIELD PERSONNEL BEFORE PROCEEDING WITH THE WORK.
- ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
- ALL STRUCTURAL BOLTS SHALL BE FIELD INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
- 4. (A.) <u>DTI'S REQUIRED:</u> ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED, SEE NOTES AND DETAILS ON SHEET S-3 FOR REQUIREMENTS ON THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
  - (B.) EFFECTIVE 5/30/2012: UNTIL FURTHER NOTICE, CROWN CASTLE WILL ACCEPT AJAX BOLTS TIGHTENED USING AISC "TURN-OF-NUT" METHOD. INSTALLERS SHALL FOLLOW CROWN GUIDELINES FOR AISC "TURN-OF-NUT" METHOD AND ALSO PROVIDE COMPLETE INSPECTION DOCUMENTATION IN THE PMIL. PRIOR TO STARTING WORK, CONTRACTOR SHALL CONSULT WITH CROWN ENGINEERING TO DETERMINE WHETHER THIS POLICY IS STILL IN PLACE.
  - (C.) REQUIREMENT EFFECTIVE (94/20/2013, PER CROWN CASTLE DIRECTIVE: ANY AND ALL STRUCTURAL BOLTS THAT ARE TIGHTENED TO THE PRETENSIONED CONDITION USING THE AISC "TURN-OF-NUT" TENSIONING PROCEDURE (NON-TENSION CONTROLLED [NON-TC] BOLTS AND/OR BOLTS WITHOUT DTPS INSTALLED) SHALL BE INSPECTED ONSITE BY AN INDEPENDENT THIRO-PARTY BOLT INSPECTOR, AS APPROVED BY CROWN. THIS INSPECTION IS REQUIRED TO BE AN ONSITE FIELD INSPECTION. THE THIRD-PARTY BOLT INSPECTOR SHALL FOLLOW THE PUBLISHED CROWN CASTLE INSPECTION PROCEDURE" MINON-TC BOLT INSPECTION, DATED APRIL 2013. THE THIRD-PARTY BOLT INSPECTOR SHALL PREPARE A FULLY DOCUMENTED BOLT INSPECTION REPORT, AS SPECIFIED BY CROWN, AND SHALL SUBMIT A COPY OF THE BOLT INSPECTION REPORT TO THE MI INSPECTOR, THE EOR, AND TO CROWN CASTLE.

### PROJECT CONTACTS:

### MONOPOLE OWNER:

CROWN CASTLE
46 BROADWAY ALBANY, NY 12204
TSA: ANDREW BAZINET AT ANDREW.BAZINET@CROWNCASTLE.COM
PH: (585) 899-3442

MOD PM: EVA MORALES AT EVA.MORALES@CROWNCASTLE.COM PH: (704) 405-6612

### STRUCTURAL ENGINEER OF RECORD (EOR):

PAUL J. FORD AND COMPANY
250 EAST BROAD STREET, SUITE 600
COLUMBUS, OHIO 43215-3708
CONTACT: JOSH FRYBARGER AT JFRYBARGER@PJFWEB.COM

PHONE: 614-221-6679

### **DESIGN STANDARD**

THIS REINFORCEMENT DESIGN IS BASED UPON THE REQUIREMENTS OF THE TIAZIA-222-F-1996 STRUCTURAL STANDARD FOR ANTENNA SUPPORTING STRUCTURES AND ANTENNAS, USING A DESIGN BASIC WIND SPEED OF 85 MPH (FASTEST MILE) WITH NO ICE, 38 MPH WITH 3/4 INCH ICE AND 50 MPH SERVICE LOADS.

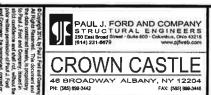
REFER TO THE POLE DESIGN AND ANTENNA LOADING DOCUMENTED IN THE PJF STRUCTURAL ANALYSIS FOR THIS SITE (PJF#37513-2318), DATED 3-25-2014.

### THIS PROJECT INCLUDES THE FOLLOWING REINFORCING ELEMENTS:

SHAFT REINFORCING

	SHEET INDEX					
SHEET NUMBER	DESCRIPTION					
T-1	TITLE SHEET					
S-1	GENERAL NOTES					
S-2	GENERAL NOTES					
S-3	AJAX BOLT DETAIL					
S-4	MONOPOLE PROFILE					
S-5	SHAFT REINF, CHART AND DETAIL					
S-6	MI CHECKLIST					





BU #806953; BRG 2044 (A) 943097 STAMFORD, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

J.J.F.

APPROVED

BLV

DATE:
3-25-2014

PROJECT No 37513-2318

DRAWN BY: T.A.N. ISSUE DATE OF PERMIT: 3-25-2014

T-1

CROWN CASTLE PROJECT: BU #806953; BRG 2044 (A) 943097; STAMFORD, CONNECTICUT MONOPOLE RETROFIT PROJECT MASTER NOTES DOCUMENT (REV. 2. 1/22/2009)

A. GENERAL NOTES

TO SPACE BETTER RESPONSIBILITY OF THE CONTRACTOR TO FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS PRIOR TO FABRICATION AND CONSTRUCTION. THESE DRAWINGS WERE REPEARED FROM INFORMATION AND DOCUMENTS PROVIDED TO PAUL. J. FORD & COMPANY BY CROWN CASTLE. THIS INFORMATION PROVIDED HAS NOT BEEN FIELD VERIFIED BY PAUL. J. FORD & COMPANY FOR ACCURACY AND THEREFORE DISCREPANCIES BETWEEN THESE DRAWINGS AND ACTUAL SITE CONDITIONS SHOULD BE ANTICIPATED. ANY DISCREPANCIES AND/OR CHANGES BETWEEN THE INFORMATION CONTAINED IN THESE DRAWINGS AND THE ACTUAL VERIFIED SITE CONDITIONS SHALL BE INMEDIATELY BROUGHT TO THE ATTENTION OF CROWN CASTLE AND PAUL. J. FORD & COMPANY SO THAT ANY CHANGES AND/OR ADJUSTMENTS. IF INCESSARY, CAN BE MADE TO THE DESIGN AND DRAWINGS.

THE EXISTING UNREINFORCED MONOPOLE STRUCTURE DOES NOT HAVE THE STRUCTURAL CAPACITY TO CARRY ALL OF THE ATTENTION AND PLATFORM LOADS SOMOWN ONT HISE DRAWINGS AT THE REQUIRED MINIMUM THAEIA 222 F BASIC WIND SPEEDS. DO NOT INSTALL MY ADDITIONAL OR NEW ANTENNA AND PLATFORM LOADS UNTIL THE MONOPOLE REINFORCING SYSTEM IS COMPLETELY AND SUCCESSFULLY INSTALLED.

THE ENSTING UNREINFORCED MONOPOLE STRUCTURE DOES NOT HAVE THE STRUCTURAL CAPACITY TO CARRY ALL OF THE ANTERNA AND PLATFORM LOADS SYMN ONT THESE DRAWINGS AT THE REQUIRED MINIMUM TAKEN-222-F BASIC WIND SPEEDS. DO NOT INSTALL ANY ADDITIONAL OR NEW ANTERNA AND PLATFORM LOADS UNTIL THE MONOPOLE REINFORCING SYSTEM IS COMPLETELY AND SUCCESSFULLY INSTALLED.

IF MATERIALS, QUANTITIES, STRENGTHS OR SIZES INDICATED BY THE DRAWINGS OR SPECIFICATIONS ARE NOT IN AGREEMENT WITH THESE NOTES, THE BETTER QUALITY ANDOR GREATER QUANTITY, STRENGTHOR OR SIZE MONCATED, SPECIFIED OR NOTED SHALL BE PROVIDED.

THIS STRUCTURE IS DESIGNED TO BE SELF-SUPPORTING AND STABLE AFTER THE INSTALLATION OF THE REINFORCING REPAIR SYSTEM HAS BEEN PROPERTY OF THE OWNER FOR THE MONOPOLE AND THIS STRUCTURE IS DESIGNED TO BE SELF-SUPPORTING AND STABLE AFTER THE INSTALLATION OF THE REINFORCING REPAIR SYSTEM HAS BEEN PROPERTY OF THE OWNER THE MONOPOLE AND THIS COMPONENT PARTS DEBINGS FIELD MODIFICATIONS. THIS INCLUDES, BUT IS NOT LIMITED IT. THE CONTRACTIONS SOLE RESPONSIBILITY TO INSTALLED.

CONTRACTIONS SOLE RESPONSIBILITY TO INSTALL REMAIN THE PROPERTY OF THE CONTRACTOR AFTER THE ADDITION OF VINATEVER TEMPORARY BRACING, GUYS OR THE DOWNS THAT MAY BE NECESSARY. SUCH AND THE ACTUAL OF THE ACTUAL OF THE ADDITION OF VINATEVER TEMPORARY BRACING, GUYS OR THE DOWNS THAT MAY BE NECESSARY. SUCH AND THE ACTUAL OF THE ACTUAL OF THE CONTRACTOR AFTER THE ADDITION OF THE ACTUAL OF THE ACTUAL OF THE ACTUAL OF THE CONTRACTOR AFTER THE ACTUAL OF TH

C. SPECIAL IMSPECTION AND TESTING
ALL WORK STALL BE SUBJECT TO REVIEW AND OBSERVATION BY THE OWNER'S REPRESENTATIVE AND
THE OWNER'S AUTHORIZED IMSPERDENT INSPECTION AND TESTING AGENCY, REFER TO CROWN
CASTLE DOCUMENT END SOW-1006 FOR SPECIFICATION.
ANY SUPPORT SERVICES PERFORMED BY THE ENGINEER DURING CONSTRUCTION SHALL BE
DISTINGUISHED FROM CONTINUOUS AND DETAILED INSPECTION SERVICES WHICH ARE PURNISHED BY
OTHERS. THESE SUPPORT SERVICES PERFORMED BY THE ENGINEER ARE PERFORMED SOLBLY FOR
THE PURPOSE OF ASSISTING IN QUALITY CONTROL AND IN ACHIEVING CONFORMANCE WITH CONTRACT
DOCUMENTS. THEY DO NOT GUARANTEE CONTRACTOR'S PERFORMANCE AND SHALL NOT BE
CONSTRUED AS SUPPERISHON OF CONSTRUCTION.
OBSERVED DISCREPANCIES BETWEEN THE WORK AND THE CONTRACT DOCUMENTS SHALL BE
CORRECTED BY THE CONTRACTOR AT NO ADDITIONAL COST.
AN INDEPENDENT QUALIFIED INSPECTIONITESTING AGENCY SHALL BE SELECTED. RETAINED AND PAID
POR BY THE OWNER FOR THE SOLE PURPOSE OF INSPECTION, TESTING, DOCUMENTING, AND
APPROVING ALL WELDING AND FIELD WORK PERFORMED BY THE CONTRACTOR.
(A) ACCESS TO ANY PLACE WHERE WORK IS BEING DONE SHALL BE PERMITTED AT ALL TIMES.
(B.) THE IMSPECTION AGENCY SHALL SO SCHEDULE THIS WORK AS TO CAUSE A MINIMUM OF
INTERRUPTION TO, AND COORDINATE WITH, THE WORK IN PROGRESS, IT IS THE
CONTRACTOR'S RESPONSIBILITY TO COORDINATE THE WORK SCHEDULE WITH THE TESTING
AGENCY. THE CONTRACTOR SHALL ALLOW FOR ADEQUATE THE AND ACCESS FOR THE
TESTING AGENCY TO PERFORM THEIR DUTIES.

THE IMSPECTION AND TESTING AGENCY SHALL IN THE TESTING AGENCY SHALL INSPECT THE FOLLOWING
SERVICES FOR THE OWNER. THE TESTING AGENCY SHALL INSPECT THE FOLLOWING
SERVICES FOR THE OWNER. THE TESTING AGENCY SHALL INSPECT THE FOLLOWING
SERVICES FOR THE OWNER. THE TESTING AGENCY SHALL INSPECT THE FOLLOWING
SERVICES FOR THE OWNER. THE TESTING AGENCY SHALL INSPECT THE FOLLOWING ITEMS IN
THE INSPECTION AND TESTING AGENCY SHALL ALLOW FOR ADECUATE THE AND ACCORDANCE WITH THE CONSTRUCTION DRAWNINGS. THE TESTING AGENCY SHALL BE SERVICED FOR THE FOLLOWING SERVICES FOR THE OWN

OMMERSON TO THE TIME THE CONTRACTOR IS WORKING ON-SITE AGENCY SHALL NOTIFY OWNER IMMEDIATELY WHEN FIELD PROBLEMS OR DISCREPANCES OCCUR.

B. FOUNDATIONS, CONCRETE, AND SOIL PREPARATION - (NOT REQUIRED)

C. CONCRETE TESTING PER ACI - (NOT REQUIRED)

D. STRUCTURAL STEEL

(1.) CHECK THE STEEL ON THE JOB WITH THE PLANS.
(2.) CHECK MILL CERTIFICATIONS.
(3.) CHECK GRIDE OF STEEL MEMBERS, AND BOLTS FOR CONFORMANCE WITH DRAWINGS.
(4.) INSPECT STEEL MEMBERS FOR DISTORTION, EXCESSIVE RUST, FLAWS AND BURNED HOLES.
(5.) CALL FOR LABORATORY TEST REPORTS WHEN IN DOUBT.
(6.) CHECK STEEL MEMBERS FOR SIZES, SWEEP AND DIMENSIONAL TOLERANCES.
(7.) CHECK FOR SURFACE FINISH SPECIFIED, GALVANIZED.
(8.) CHECK BOLT TIGHTENING ACCORDING TO AISC TURN OF THE NUT METHOD.

E. WELDING: -(NOT REQUIRED)

F. SPECIAL INSPECTION OF EXISTING SHAFT-TO-FLANGE WELD CONNECTIONS: - (NOT REQUIRED)

G. REPORTS:
(1.) COMPILE AND PERIODICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER.

(1). COMPILE AND PERIODICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER.

THE INSPECTION PLAN OUTLINED HERRIN IS INTENDED AS A DESCRIPTION OF GENERAL AND SPECIFIC TEMS OF CONCERN. IT IS NOT INTENDED TO BE ALL-INCLUSIVE. IT DOES NOT LIMIT THE TESTING AND INSPECTION AGENCY TO THE ITEMS LISTED. ADDITIONAL TESTING, INSPECTION, AND CHECKING MAY BE REQUIRED AND SHOULD BE ANTICIPATED. THE TESTING AGENCY SHALL USE THEIR PROFESSIONAL JUDGMENT AND KNOWLEDGE OF THE JOB SITE CONDITIONS AND THE CONTRACTOR'S PERFORMANCE TO DECIDE WHAT OTHER ITEMS REQUIRE ADDITIONAL ATTENTION. THE TESTING AGENCY'S JUDGMENT MUST PREVAIL ON ITEMS NOT SPECIFICALLY COVERED. ANY DISCREPANCIES AND PROBLEMS SHALL BE BROUGHT IMMEDIATELY TO THE OWNERS ATTENTION. RESOLUTIONS ARE NOT TO BE MADE WITHOUT THE OWNER'S REVIEW AND SPECIFIC WRITTEN CONSENT. THE OWNER RESERVES THE RIGHT TO THE CONTRACTOR AND FILED STOREPANCIES AND PROBLEMS.

AFTER EACH INSPECTION, THE TESTING AGENCY WILL PREPARE A WRITTEN ACCEPTANCE OR REJECTION WHICH WILL BE GRAYN TO THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE COWNER. THIS WRITTEN ACTION WILL GIVE THE CONTRACTOR AND FILED THEMS TO BE CORRECTED, PRIOR TO CONTINUING CONSTRUCTION, ANDOR LOADING OF STRUCTURAL TEMS.

RESPONSIBILITY: THE TESTING AGENCY DOES NOT RELIEVE THE CONTRACTOR'S CONTRACTUAL OR STATUTORY OBLIGATIONS. THE CONTRACTOR HAS THE SOLE RESPONSIBILITY FOR MY DEVIATIONS FROM THE OFFICIAL CONTRACT DOCUMENTS. THE TESTING AGENCY WILL NOT REPLACE THE CONTRACTOR'S CONTRACTUAL OR STATUTORY OBLIGATIONS. THE CONTRACTOR HAS THE SOLE RESPONSIBILITY FOR MY DEVIATIONS FROM THE OFFICIAL CONTRACT DOCUMENTS. THE TESTING AGENCY WILL NOT REPLACE THE CONTRACTOR'S CONTRACTUAL OR STATUTORY OBLIGATIONS. THE CONTRACTOR HAS THE SOLE RESPONSIBILITY FOR MY DEVIATIONS FROM THE OFFICIAL CONTRACT DOCUMENTS. THE TESTING AGENCY WILL NOT REPLACE THE CONTRACTOR'S QUALITY CONTROL PERSONNEL.



PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 East Broad Street - Suite 500 - Columbius, Onio 43216 www.pifesb.com

**CROWN CASTLE** 46 BROADWAY ALBANY, NY 12204

BU #806953; BRG 2044 (A) 943097 STAMFORD, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

PROJECT No 37513-2318 DRAWN BY: CHECKED BY

J.J.F.

ISSUE DATE OF PERMIT: 3-25-2014

BKK

STRUCTURAL STEEL

TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:

BY THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC):

(A)

"SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL

FOR BUILDINGS."

(B)

"SPECIFICATION FOR STRUCTURAL JOINTS USING ASTM A225 OR A#39 BOLTS," AS

APPROVED BY

THE RESEARCH COUNCIL ON STRUCTURAL CONNECTIONS OF THE

ENGINEERING FOUNDATION.

(C)

"CODE OF STANDARD PRACTICE FOR STEEL BUILDINGS AND BRIDGES" (PARAGRAPH 4.2.1

SPECIFICALLY EXCLUDED).

SPECIFICALLY EXCLUDED).

SPECIFICALLY EXCLUDED.

SPECIFICALLY EXCLUDED.

ANY MATERIAL OR WORKMANSHIP WHICH IS OBSERVED TO BE DEFECTIVE OR INCONSISTENT WITH

THE CONTRACTOR'S EXPENSE.

THE CONTRACTOR'S EXPENSE.

SHALL STRUCTURAL BOLTS, INCLUDING THE AIAX M20 BOLTS WITH SHEAR SLEEVES,

ACCORDING TO THE REQUIREMENTS OF THE AISC "TURN OF THE NUT METHOD. TIGHTEN BOLTS 137

TURN PAST THE SNUG TIGHT CONDITION AS DEFINED BY AISC.

WELDED CONNECTIONS SHALL CONFORM TO THE LATEST REVISED CODE OF THE AMERICAN

WELDING SOCIETY, AND SIT, ALL WELD ELECTRODES SHALL BE EBOXX UNLESS NOTED

DIL WELDED ONNECTIONS SHALL CONFORM TO THE LATEST REVISED CODE OF THE AMERICAN

WELDED ONNECTIONS SHALL CONFORM TO THE LATEST REVISED CODE OF THE AMERICAN

WELDED ONNECTIONS SHALL CONFORM TO THE LATEST REVISED CODE OF THE AMERICAN

WELDED ONNECTIONS SHALL CONFORM TO THE LATEST REVISED CODE OF THE AMERICAN

WELDED ONNECTIONS SHALL DE PROPARED AS REQUIRED BY AWS. CONTRACTOR SHALL

MELDER OF THE CONTROL OF THE SHALL CONFORM TO ASTA AST2 GRADE 65 (FY = 65 KS IMMIN,) UNLESS

SIES ISSUED ON THE STEEL SHALL CONFORM TO ASTA AST2 GRADE 65 (FY = 65 KS IMMIN,) UNLESS

NOTED OTHERWISE ON THE DRAWNINGS.

SUFFACES OF EXISTING STEEL SHALL END TO ASTA AST2 ORADE 50 FIRED WELDING PER ANS.

SEE SECTION I NOTES REGARDING TOUGHAP OF GALVANIZED SURFACES DAMAGED DURING

TRANSPORTATION OR PERETON AND ASPECTION TO STRUCTURE WITHOUT THE PRIOR APPROVAL AND SU

BASE PLATE GROUT - (NOT REQUIRED)

FOUNDATION WORK - (NOT REQUIRED)

CAST-IN-PLACE CONCRETE - (NOT REQUIRED)

EPOXY GROUTED REINFORCING ANCHOR RODS - (NOT REQUIRED)

TOUCH UP OF GALVANIZING
THE CONTRACTOR SHALL TOUCH UP ANY ANDIOR ALL AREAS OF GALVANIZING ON THE EXISTING
STRUCTURE OR NEW COMPONENTS THAT ARE DAMAGED OR ABRADED DURING CONSTRUCTION.
GALVANIZED SURFACES DAMAGED DURING TRANSPORTATION OR ERECTION AND ASSEMBLY AS
WELL AS ANY AND ALL ABRASIONS, CUTS, FIELD DRILLING, AND ALL FIELD WELDING SHALL BE
TOUCHED UP WITH TWO (2) COATS OF ZRC-BRAND ZINC-RICH COLD GALVANIZING COMPOUND. FILM
THICKNESS PER COAT SHALL BE: WET A OMINS, DRY 1-5 MILS. APPLY PRE ZRC (MANUFACTURER)
RECOMMENDED PROCEDURES. CONTACT ZRC AT 1-800-851-3275 FOR PRODUCT INFORMATION.
CONTRACTOR SHALL CLEAN AND PREPARE ALL FIELD WELDS ON GALVANIZED AND PRIME PUNITED
SUPFACES FOR TOUCH-UP COATING IN ACCORDANCE WITH AWS D1.1. THE OWNERS TESTING
AGENCY SHALL VERIFY THE PREPARED SUBFACES PIOR DA PRI ACTIONAL OF THE TOUGHLED.

SURFACES FOR TOUGH-UP CONTINUE IN ACCORDANCE WITH AWS D.T. THE OWNER'S TESTING AGENCY SHALL VERIFY THE PREPARED SURFACE PRIOR TO APPLICATION OF THE TOUGHTUP COATING. THE COMERS TESTING AGENCY SHALL TEST AND VERIFY THE COATING THICKNESS AFTER THE CONTRACTOR HAS APPLIED THE ZIC COLD GALVANIZING COMPOUND AND IT HAS SUFFICIENTLY DRIED. AREAS FOUND TO BE INADECUATELY COATED, SHALL BE RE-COATED BY THE CONTRACTOR AND RE-TESTED BY THE TESTING AGENCY.

HOT DIP GALVANIZING
HOT DIP GALVANIZING
HOT DIP GALVANIZING
HOT DIP GALVANIZI ALL STRUCTURAL STEEL MEMBERS AND ALL STEEL ACCESSORIES, BOLTS,
WASHERS, ETC. PER ASTM A123 OR PER ASTM A153, AS APPROPRIATE
PROPERLY PREPARE STEEL ITEMS FOR GALVANIZING,
DRILL OR PRINCH MEEP ANDIOR DRAINAGE HOLES AS REQUIRED,
ALL GALVANIZING SHALL BE DONE AFTER FABRICATION IS COMPLETED AND PRIOR TO FIELD
MEMORY AND PRIOR TO FIEL

PERFETUAL INSPECTION AND MAINTENANCE BY THE OWNER
ATHER THE CONTRACTOR HAS SUCCESSFULLY COMPLETED THE INSTALLATION OF THE MONOPOLE
REINFORCING SYSTEM AND THE WORK HAS BEEN ACCEPTED BY THE OWNER, THE OWNER WILL BE
RESPONSIBLE FOR THE LONG TERM AND PERPETUAL INSPECTION AND MAINTENANCE OF THE POLE
AND REINFORCING SYSTEM AND THE WORK HAS BEEN ACCEPTED BY THE OWNER, THE OWNER WILL BE
RESPONSIBLE FOR THE LONG TERM AND PERPETUAL INSPECTION AND MAINTENANCE OF THE POLE
AND REINFORCING SYSTEM INDICATED IN THESE DOCUMENTS USES REINFORCING
COMPONENTS THAT INVOLVE FIELD WELDON STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL
POLE STRUCTURE. THESE FELD WELDON CONNECTIONS ARE SUBJECT TO CORROSONO MAINAGE
AND DETERIORATION IN THEY ARE NOT PROPERLY MAINTAINED AND COVERED WITH CORROSION
PREVENTIVE COATING SUCH AS THE ZRG CALVANIZEDS COMPOUND SPECIFIED PREVIOUSLY. THE
STRUCTURAL LOAD CARRYING CAPACITY OF THE REINFORCED POLE SYSTEM IS DEPENDENT UPON
THE INSTALLED SUZE AND QUALITY, MAINTAINED SOUND CONDITION AND STREMSTH OF THESE FIELD
WELDED CONNECTIONS. ANY CORROSION OF, DAMAGE TO, FATIGUE, FRACTURE, ANDIOR
DETERIORATION OF THESE WELDS ANDIOR THE GOMENICETE COMPONENTS WILL RESULT IN THE
LOSS OF STRUCTURAL LOAD CARRYING CAPACITY AND MAY LEAD TO FAILURE OF THE
STRUCTURAL SYSTEM. THEREFORE, IT IS INFERANTE HAT THE OWNER REGULARLY INSPECTS,
MAINTAINS, AND REPAIRS AS NECESSARY, ALL OF THESE WELDS, CONNECTIONS, AND
COMPONENTS FOR THE LIFE OF THE STRUCTURE.
THE OWNER SHALL REFER TO TIMELE AZZZ-1998, SECTION 14 AND ANNEX E FOR RECOMMENDATIONS
FOR MAINTENANCE AND INSPECTION. THE FREQUENCY OF THE INSPECTION AND MAINTENANCE
INTERVALS IS TO BE DETERMINED BY THE OWNER BASED UPON ACTUAL SITE AND ENVIRONMENTAL
CONDITIONS, PAUL J. FORD COMPONEY PART AT A COMPONENT FROM THE WARD
FOR MAINTENANCE AND INSPECTION. THE FREQUENCY OF THE INSPECTION AND MAINTENANCE
INTERVALS IS TO BE DETERMINED BY THE OWNER BASED UPON ACTUAL SITE AND ENVIRONMENTAL
CONDITIONS. PAUL J. FORD COMPONEY PART AND THOROUGH
INSPECTION OF THE ENTIRE REINFORCED MONOPOLE STRUCTURAL SY



PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 Cast Broad Street - Suits 600 - Columbia, Ohio 43215 (914) 321-9679

**CROWN CASTLE** 46 BROADWAY ALBANY, NY 12204 PH: (585) 899-3442 FAX: (585) 899-3448

BU #806953; BRG 2044 (A) 943097 STAMFORD, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

PROJECT N 37513-2318 DRAWN BY CHECKED BY

ISSUE DATE OF PERMIT: 3-25-2014

APPROVED BY BKK

### AJAX BOLT NOTE SHEET: REV. 1.4, 5-20-2013

NOTES

- 1. ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS, DEC. 31, 2009.
- 2. ALL STRUCTURAL BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
- 3. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED, SEE NOTES AND DETAIL BELOW FOR THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
- 4. ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. DTI'S SHALL BE THE SQUIRTER® STYLE, MADE TO ASTM F959 LATEST REVISION; AND HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A HARDNESS OF RC 38 OR HIGHER.

### NOTES FOR AJAX M20 'ONE-SIDE' BOLTS WITH DIRECT TENSION INDICATORS (DTI'S):

DTI'S SHALL BE "SELF-INDICATING" SQUIRTER® STYLE DTI'S MADE WITH SILICONE EMBEDDED IN THEM, INSPECTED BY MEANS OF THE VISUAL EJECTION OF SILICONE AS THE DTI PROTRUSIONS COMPRESS. SQUIRTER® DTI'S SHALL BE CALIBRATED PER MANUFACTURER'S INSTRUCTIONS PRIOR TO USE.

THE DIRECT TENSION INDICATOR (DTI) WASHERS SHALL BE THE "SQUIRTER® STYLE" AS MANUFACTURED BY:

APPLIED BOLTING TECHNOLOGY PRODUCTS, INC. 1413 ROCKINGHAM ROAD BELLOWS FALLS, VERMONT, USA 05101 PHONE 1-800-552-1999

WEBSITE: WWW.APPLIEDBOLTING.COM

DISTRIBUTORS OF SQUIRTER® DTI'S: <u>HTTP://WWW.APPLIEDBOLTING.COM/APPLIED-BOLTING-DISTRIBUTORS.HTML</u>

<u>DTI:</u> USE DIRECT TENSION INDICATOR (DTI) WASHERS COMPATIBLE WITH 20 MM (M20) NOMINAL A325 BOLTS FOR THE AJAX M20 BOLTS. DTI'S SHALL <u>NOT</u> BE HOT-DIP GALVANIZED. DTI'S SHALL BE MECHANICALLY GALVANIZED (MG) BY THE COLD MECHANICAL PROCESS ONLY AS PROVIDED BY THE DTI MANUFACTURER.

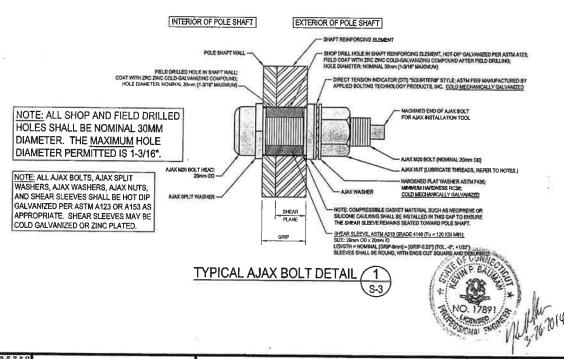
HARDENED WASHERS REQUIRED: USE A HARDENED WASHER FOR A 20 MM (M20) NOMINAL BOLT BETWEEN THE TOP OF THE DIRECT TENSION INDICATOR (DTI) WASHER AND THE NUT OF THE AJAX M20 BOLTS. HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A MINIMUM HARDNESS OF RC 38 OR HIGHER. THE HARDENED WASHERS SHALL BE MECHANICALLY GALVANIZED BY THE COLD MECHANICAL PROCESS. ALTERNATIVELY, CORRECTLY MADE HOT DIP GALVANIZED HARDENED FLAT WASHERS HAVING A MINIMUM HARDNESS OF RC 38 CAN BE USED; CONTRACTOR SHALL PROVIDE DOCUMENTATION OF WASHER SPECIFICATION AND HARDNESS.

NUT LUBRICATION REQUIRED: PROPERLY LUBRICATE THE THREADS OF THE NUT OF THE AJAX BOLT SO THAT IT CAN BE PROPERLY TIGHTENED WITHOUT GALLING AND/OR LOCKING UP ON THE BOLT THREADS. CONTRACTOR SHALL FOLLOW DTI MANUFACTURER INSTRUCTIONS FOR PROPER LUBRICATION AND TIGHTENING.

NOTE: COMPLETELY COMPRESSED DTI'S SHOWING NO VISIBLE REMAINING GAP ARE ACCEPTABLE. DTI WASHERS SHALL BE PLACED DIRECTLY AGAINST THE OUTER AJAX WASHER WITH THE DTI BUMPS FACING AWAY FROM THE AJAX WASHER. PLACE A HARDENED WASHER BETWEEN THE DTI AND THE AJAX NUT. THE DTI BUMPS SHALL BEAR AGAINST THE UNDERSIDE OF A HARDENED FLAT WASHER, NEVER DIRECTLY AGAINST THE NUT.

CONTRACTOR SHALL FOLLOW DTI MANUFACTURER'S INSTRUCTIONS FOR INSTALLATION, LUBRICATION, TIGHTENING AND INSPECTION.

INSPECTION REQUIRED: ALL AJAX BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009, BY A QUALIFIED BOLT INSPECTOR. DURING INSTALLATION, THE BOLT INSPECTOR SHALL VERIFY AND DOCUMENT: THE SHOP-DRILLED AND FIELD-DRILLED HOLE SIZES; THE INSTALLATION OF THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S TENSIONING PROCEDURE. IN ADDITION, ALL AJAX BOLTS AND DTI'S SHALL BE VISUALLY INSPECTED ACCORDING TO THE DTI MANUFACTURER'S INSTRUCTIONS. THE BOLT INSPECTOR SHALL PROVIDE COMPLETE PHOTO DOCUMENTATION OF ALL BOLTS AFTER TIGHTENING CLEARLY SHOWING THE CONDITION OF THE DTI'S.



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PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 270 East Broad Street - Suite 600 - Columbias, Chie 43215 (614) 221-0078

CROWN CASTLE
46 BROADWAY ALBANY, NY 12204
FIX: (885) 999-3442
FX: (885) 999-3442

BU #806953; BRG 2044 (A) 943097 STAMFORD, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT PROJECT No: 37513-2318 DRAWN BY: T.A.N. CHECKED BY: J.J.F.

ISSUE DATE OF PERMIT: 3-25-2014

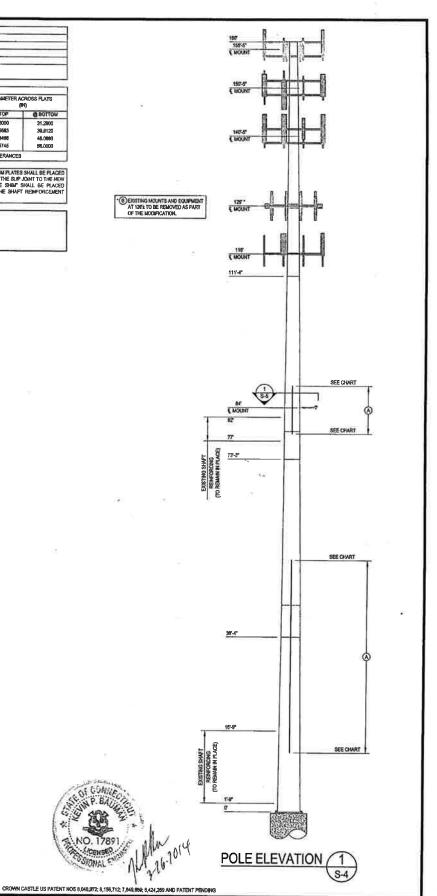
BKK DATE: 3-25-2014

	POLE SPECIFICATIONS
POLE SHAPE TYPE	12-SIDED POLYGON
TAPER	0.2401 PAFT
SHAFT STEEL:	ASTM ASTT GRADE 65
BASE PL STEEL:	ASTM A633 GR. E (60 KSI)
ANCHOR ROOS:	2 UATE #181 ASTM AS15 GRADE 75

SHAFT SECTION	SECTION LENGTH (FT)	PLATE THICKNESS (IN)	LAP SPLICE (IN)		CROSS FLATS IN)
QEO,IQII	6.9	(-1)	(7)	@ TOP	@ BOTTOM
. 1	48.57	0.2500	****	19,8000	31,2900
2	42.75	0.3438	51.00	29.6683	39,8120
3	42.87	.67 0.4053 69.00 37.8	37.8488	48,0880	
4	43.00	0.4375	80.00	45,6745	58,0000

CONTRACTOR SHALL PROVIDE ASTM AND SHEM PLATES BELOW SUP JOINTS. THE SHEM PLATES SHALL BE PLACED BETWEEN THE NEW SHAFT REMOTRICEMENT AND THE ENSINED POLE SHAFT FROM THE SUP JOINT TO THE NEW SHAFT REMOTRICEMENT SHALL BE PLATE LOCATION AND A EXTRA LONG SPEICE SHAFT SHALL BE PLACED BETWEEN THE NEW FOREIGN AND LOWER SHAFT REMOTRICEMENT PLATES AT THE SHAFT REMFORCEMENT SHAFT REMOTRICEMENT SHAFT REMOTRICEMENT

- (A) INSTALL NEW SHAFT REINFORCING, SEE CHART.
- B REMOVE EXISTING MOUNT AND EQUIPMENT AT EL. 1265





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DATE:
3-25-2014



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				NEW C	CIFLAT PLA	TE (65 KSI) R	EINFORCING S	CHEDULE				
CROWN CASTLE CATALOG PART NUMBER	BOTTOM BLEVATION	TOP ELEVATION	FLAT#/ DEGREE SEPARATION	ELEMENT	ELEMENT LENGTH	ELEMBIT	BINIMUM AJAX BOLTS PER ELEMENT	MINIMUM TOTAL AJAX BOLT QUANTITY	TERMINATION BOLTS (BOTTOM)	TERMINATION BOLTS (TOP)	MAXIMUM INTERMEDIATE BOLT SPACING	ESTIMATE TOTAL STEEL WEIGHT
CCFAFP- 06010020	12-3	32-3*	3,7811	1°x6"	20'-0"	3	31	93	10	10	16"	1225 LBS.
CCI-AFP- 06010020	32'-4"	52'-4"	3,7 & 11	1°x6°	20'-0"	3	31	93	10	10	16"	1225 LBS.
CCHAPP- 06010010	76 - 6	B8"-6"	3,7 & 11	1"xer	10" - 0"	3	23	69	10	10	16"	612 LBS.

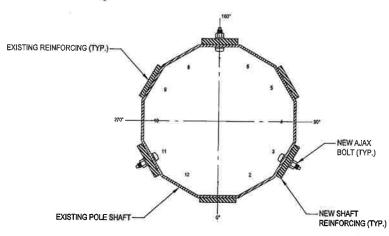
NOTES:

- 1) AUX BOLTS ARE TO BE 20mm DIMIETER WITH CORRESPONDING 29mm DIMIETER SLEEVE WITH MATCHING STEEL GRADE.
  2) ALL STEEL SHALL BE HOT-DP GRUNNIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123, A TERNAT NELY, ALL NEW STIFFENER PLATE STEEL RENFORCING NAY BE COLD GRUNNIZED AS FOLLOWS, APPLY ALL NEW STIFFENER PLATE STEEL RENFORCING NAY BE COLD GRUNNIZED AS FOLLOWS, APPLY ALL NEW STIFFENER PLATE STEEL RENFORCING NAY BE COLD GRUNNIZED AS FOLLOWS, APPLY ALL NEW STIFFENER PLATE STEEL RENFORCING NAY BE COLD TABLE STEEL ST

	on work or	C-27	SPLICE P	LATE INSTAL	LATION CHAR	ī		
ELEVATION	FLAT PLATE THICKNESS	FLAT PLATE WIDTH	FLAT PLATE LENGTH	PLAT PLATE QUANTITY	WELD LENGTH PER SIDE		AJAX BOLTS PER SPLICE	TOTAL STEE
32-3	1.	8*	S.T	3			20	457 LBS.

\*BOLTS INCLUDED IN THE TOTAL QUANTITY LISTED IN THE FLAT PLATE INSTALLATION CHART.

NEW SHIM CHART								
SHIM QUANTITY	SHIM WIDTH	SHIM LENGTH	SHIM THICKNESS	HOLE DIAMETER				
21	4		134"	1-14"				
39	•	4"	1/16"	1-14"				





PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 East Broed Street · Suits 600 · Columbus, Otto 43215 (141) 221-6679

CROWN CASTLE
46 BROADWAY ALBANY, NY 12204
PH (86) 699-3442
FAX (86) 899-3442

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GENERAL.

THE BOOFFCATION INSPECTION AND IS A VISUAL INSPECTION OF TOWER MODIFICATIONS AND A REVIEW OF CONSTRUCTION INSPECTIONS AND OTHER REPORTS TO ENSURE THE INSTALLATION WAS CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, MAKELY THE MODIFICATION ORWANDS, AS CESSORED BY THE ENGINEER OF RECORD (ECV).

THE MEST TO CONFIGURISTALLATION CONFIGURATION AND WORKGLANSHIP ONLY AND IS NOT A REVIEW OF THE MODIFICATION DESIGN TISSE, K ONC DOES THE MER REPECTION TAKE OWNERSHIP OF THE MODIFICATION DESIGN. OWNERSHIP OF THE STRUCTURAL MODIFICATION DESIGN EFFECTIONESS AND INTEGRAT RESIDES WITH THE CRICK TALLITHMENS AND AND RESIDENT RESIDES WITH THE CRICK TALLITHMENS AND INTEGRAT RESIDES WITH THE CRICK TALLITHMENS AND INTEGRAT RESIDES WITH THE CRICK TALLITHMENS AND INTEGRAT RESIDENT AND EACH THE CRICK TALLITHMENS AND INTEGRAT RESIDENT WITH SECRIT ALLITHMENS AND INTEGRAT RESIDENT AND A CONTROLLED THE CRICK TALLITHMENS AND INTEGRAT RESIDENT AND A CONTROLLED THE CRICK TALLITHMENS AND INTEGRAT.

ALL MTS SHALL BE CONDUCTED BY A CROWN ENGINEERING VENDOR (AEV) OR ENGINEERING SERVICE VENDOR (AESV) THAT IS APPROVED TO PERFORM ELEVATED WORK FOR CROWN. SEE ENG-BUL-10173 LIST OF APPROVED MI VENDORS.

TO ENSIRE THAT THE REQUIREMENTS OF THE MI ARE MET, IT IS VITAL THAT THE GENERAL CONTRACTOR (GC) AND THE MI INSPECTOR BECON COMMUNICATING AND COORDINATING AS SOON AS A POLS RECEIVED. IT IS EXPECTED THAT EACH PARTY WILL BE PROJECTIVE IN REACHING OUT TO THE OTHER PARTY. IF CONTACT REPORTANTION IS NOT INNOVING CONTACT YOUR CROWN POINT OF CONTACT (PCC).

REFER TO ENG-80W-10007; MODIFICATION INSPECTION SOW FOR FURTHER DETAILS AND REQUIREMENTS

MEMSPECTOR THE MEMSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A PO FOR THE METO, AT A MINIMUM:

<u>General Contractor</u> The GC is required to contact the Minspector as soon as receiving a PO for the Modification installation or turn Project 10, at a **min**ham:

- REVIEW THE REQUIREMENTS OF THE MICHECALIST
   WORK WITH THE MI INSPECTION TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLIDING FOUNDATION INSPECTIONS
   BETTER UNDERSTAND ALL INSPECTION AND TESTING REQUIREMENTS

<u>RECOMMENDATIONS</u>
THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING A MIREFORT:

- IT IS SUGGESTED THAT THE GC PROVIDE A MINIMUM OF 5 BUSINESS DAYS NOTICE, PREFERABLE 10, TO THE MINIPECTOR AS TO WHEN THE SITE WILL BE REJOY FOR THE ME TO BE CONDUCTED.

  THE STEWL MERRECION COORDINATE CLOSELY THROUGHOUT THE ENTIRE PROJECT.

  WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MENSPECTOR ON-SITE SIMULTANEOUSLY FOR ANY GUY WIFE TENSIONING OR RE-TENSIONING OFFERATIONS.

  IT MAY BE REMERICAN TO INSTALL ALL TOWER MODERCATIONS PRIOR TO CONDUCTING THE FOUNDATION INSPECTIONS TO ALLOW FOUNDATION AND INSPECTIONS, TO COMMENTE WITH ONE STEELY DURING THE MIN TO HAVE ANY DEPICIENCES.

  WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MENSPECTOR ON-SITE DURING THE MI TO HAVE ANY DEPICIENCES CORRECTED DURING THE MILL THE PROFESS. THE GC MAY CHOOSE TO COORDINATE THE MIN CAREFULLY TO ENSURE ALL CONSTRUCTION FACILITIES ARE AT THER DISPOSAL WHEN THE MENSPECTOR IS ON SITE.

CAMERILATION OR DELAYE IN SCHEWALED MY

FIRE GC AND MIRSPECTOR AGREE TO A DATE ON WHICH THE MI WALL BE CONDUCTED, AND EITHER PARTY CANCELS OR DELAYS, CROWN
SHALL NOT BE RESPONSIBLE FOR ANY COSTS, FEES, LOSS OF DEPOSITS AND OR OTHER POPULTES RELATED TO THE CANCELLATION OR
DELAY MOURRED BY EITHER PARTY FOR ANY THAN (E.C. TRAVEL AND LODGING, DOSTS OF REPRING EXPREED TO NISTE, ETC.). F CROWN
CONTRACTS DEPOCHTY FOR A THORD PARTY NIS, EXCEPTIONS HAVE BEING BY THE EVENT THE CELLY/CANCELLATION IS CAUSED BY
WEATHER OR OTHER CONDITIONS THAT MAY COMPROMISE THE SAFETY OF THE PARTIES INNOCATED.

CORRECTION OF FALING MES.

IF THE MODIFICATION INSTALLATION WOULD FAIL THE MI (FAILED ME), THE GC SHALL WORK WITH CROWN TO COORDINATE A REM

- CORRECT FALING ISSUES TO COMPLY WITH THE SPECIFICATIONS CONTAINED IN THE ORIGINAL CONTRACT DOCUMENTS AND
  COORDINATE A SUPPLIESH TILL.
   OR, WITH CONVINE APPROVAL, THE GC MAY WORK WITH THE EOR TO RE-ANALYZE THE MODIFICATION REINFORCEMENT USING THE
  AS-BURLT CONDITION

IN VERRICATION INSPECTIONS
CROWN RESERVES THE ROTHET CONDUCT A MI VERFICATION INSPECTION TO VERRY THE ACCURACY AND COMPLETENESS OF PREVIOUS COUNTY ETRO HE RED AN INSPECTION(S) ON TOWER MODIFICATION PROJECTS.

VERFICATION INSPECTION MAY BE CONDUCTED BY AN INDEPENDENT ADVIACES FROM AFTER A MODIFICATION PROJECT IS COMPLETED, AS MARKED BY THE DATE OF ANACCEPTED <u>PASSING MY</u> OR <u>PASS AS NOTED MY</u> REPORT FOR THE ORIGINAL PROJECT.

PHOTOGRAPHS
BETWEEN THE 6C AND THE MI INSPECTOR THE FOLLOWING PHOTOGRAPHS, AT A MINIMUM, ARE TO BE TAKEN AND INCLUDED IN THE MA REPORT:

- PRE-CONSTRUCTION GENERAL SITE CONDITION
  PHOTOGRAPHS DURBND THE RENFORCEMENT MODIFICATION CONSTRUCTION/ERECTION AND INSPECTION
  PHOTOS OF ALL CRITICAL DETAILS
  PHOTOS OF ALL CRITICAL DETAILS
  WILLD PREPARATION
  BOLT INSTALLED CONDITION
  FINAL INSTALLED CONDITION
  PAUL INSTALLED CONDITION
  PAUL INSTALLED CONDITION
  PAUL PREPARATION
  POSIT CONSTRUCTION PHOTOGRAPHS
  PAUL PRELIC CONDITION
  PRICE CONDITION
  PRICE PRELIC CONDITION
  PRICE PRICE PRELIC CONDITION
  PRICE PRELIC CONDITION
  PRICE PRELIC CONDITION
  PRICE PRICE PRELIC CONDITION
  PRICE PREPARATION
  PRICE PREPARATION
  PRICE PREPARATION
  PRICE P

PHOTOS OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED INADEQUATE

CONSTRUCTION INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY EOR)	REPORT ITEM			
	PRE-CONSTRUCTION			
x	IN CHECKLIST DRAWINGS			
X X	ECR APPROVED SHOP DRAWNIGS			
x	FABRICATION INSPECTION			
NA NA	FABRICATOR CERTIFIED WELD INSPECTION			
x	MATERIAL TEST REPORT (MTR)			
NA,	FABRICATOR NDE INSPECTION			
NA.	NDE REPORT OF MONOPOLE BASE PLATE (AS REQUIRED)			
х	PACKING SLIPS			
DOITIONAL TESTING AND INSPECTIONS:				
	CONSTRUCTION			
x	CONSTRUCTION INSPECTIONS			
NA.	POUNDATION INSPECTIONS			
NA	CONCRETE COMP. STRENGTH AND SLUMP TESTS			
NA.	POST INSTALLED ANCHOR ROD VERIFICATION			
NA	BASE PLATE GROUT VERIFICATION			
NA	CONTRACTOR'S CERTIFIED WELD INSPECTION			
NA	EARTHWORK: LIFT AND DENSITY			
×	ON SITE COLD GALVANIZING VERIFICATION			
NA	GUY WIRE TENSION REPORT			
x	GC AS-BUILT DOCUMENTS			
X	THIND PARTY ONSITE INSPECTION OF BOLT PRETENSION PER CROWN REQUIREMENTS			
×	INSPECTION OF AJAX BOLTS AND DTT'S PER REQUIREMENTS ON SHEET \$-3			
DITIONAL TESTING AND INSPECTIONS:				
	POST-CONSTRUCTION			
x	M INSPECTOR REDUNE OR RECORD DRAWING(S)			
X	THIRD PARTY ONSITE BOLT INSPECTION REPORT			
NA .	POST INSTALLED ANCHOR ROD PULL-OUT TESTING			
	PHOTOGRAPHS			

MI CHECKLIST



PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 Est Broad Stript - Softe 600 Columbia, Orio 43215 1014) 221-6575 **CROWN CASTLE** 

46 BROADWAY ALBANY, NY 12204 Pt (585) 599-3442 FAX: (585) 899-3448

BU #806953; BRG 2044 (A) 943097 STAMFORD, CONNECTICUT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

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