March 24, 2020

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## RE: Notice of Exempt Modification for T-Mobile: <br> 806953 - T-Mobile Site ID: CT11071E <br> 69 Guinea Road, Stamford Connecticut <br> Latitude: $\mathbf{4 1}^{\circ} \mathbf{6}^{\mathbf{\prime}} \mathbf{6 . 3 5}{ }^{\prime \prime}$ / Longitude: $-\mathbf{7 3}^{\circ} \mathbf{3 5} \mathbf{~}^{\prime} \mathbf{4 1 . 4 5 \prime \prime}$

Dear Ms. Bachman:
T-Mobile currently maintains nine (9) antennas at the 116 -foot mount on the existing 160 -foot Monopole Tower, located at 69 Guinea Road, Stamford, CT. The tower is owned by Crown Castle and the property is owned by the Girl Scouts of Connecticut, Inc. T-Mobile now intends to replace six (6) existing antennas with three (3) new $1900 / 2100 \mathrm{MHz}$ antennas and three (3) new $600 / 700 \mathrm{MHz}$ antennas. The new antennas will be installed at the $116-\mathrm{ft}$ level of the tower. T-Mobile is also proposing tower mount modifications. As shown on the enclosed mount analysis.

The facility was approved by the Connecticut Siting Council on April 2, 1998 in Docket No. 180. The approval was given with conditions which this proposed exempt modification complies with.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § $16-50 \mathrm{j}-73$, a copy of this letter is being sent electronically to David Martin, Mayor for the City of Stamford, David Woods, Deputy Director of Planning, Crown Castle as the tower owner, and Girl Scouts of Connecticut, Inc., the property owner.

1. The proposed modifications will not result in an increase in the height of the existing tower.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

Page 2

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the abovereference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Anne Marie Zsamba.

Sincerely,

Anne Marie Zsamba
Real Estate Specialist
3 Corporate Park Drive, Suite 101
Clifton Park, NY 12065
(201) 236-9224

AnneMarie.Zsamba@crowncastle.com

Attachments
cc:
David Martin, Mayor (via email to mayorsoffice@stamfordct.gov)
City of Stamford
Stamford Government Center
888 Washington Blvd. $-10^{\text {th }}$ Floor
Stamford, CT 06901
David W. Woods, Deputy Director of Planning (via email to dwoods@stamfordct.gov)
City of Stamford
Stamford Government Center
888 Washington Blvd. $-7^{\text {th }}$ Floor
Stamford, CT 06901
Girl Scouts of Connecticut, Inc.
Michele Velez, Director of Property Services (via email to mvelez@gsofct.org)
340 Washington Street
Hartford, CT 06106
Crown Castle, Tower Owner

| From: | $\underline{\text { Zsamba, Anne Marie }}$ |
| :--- | :--- |
| To: | $\underline{\text { mvelez@gsofct.org }}$ |
| Subject: | Notice of Exempt Modification Submission to the Connecticut Siting Council - 69 Guinea Road, Stamford CT |
| Date: | Tuesday, March 24, 2020 1:47:00 PM |
| Attachments: | EM-T-MOBILE 69 GUINEA RD STAMFORD 806953 CT11071E 2.pdf |

Good afternoon Ms. Velez,

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council, today March 24, 2020.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable. If you could kindly confirm receipt. Thank you.

Best,
Anne Marie Zsamba

ANNE MARIE ZSAMBA
Network Real Estate Specialist
T: (201) 236-9224
M: (518) 350-3639
F: (724) 416-6112

## CROWN CASTLE

3 Corporate Park Drive, Suite 101
Clifton Park, NY 12065
CrownCastle.com

| From: | Zsamba, Anne Marie |
| :--- | :--- |
| To: | "mayorsoffice@stamfordct.gov" |
| Subject: | Notice of Exempt Modification Submission to the Connecticut Siting Council - 69 Guinea Road, Stamford CT |
| Date: | Tuesday, March 24, 2020 1:45:00 PM |
| Attachments: | EM-T-MOBILE 69 GUINEA RD STAMFORD 806953 CT11071E 2.pdf |

Good afternoon Mayor Martin,

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council, today March 24, 2020.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable. If you could kindly confirm receipt. Thank you.

Best,
Anne Marie Zsamba

ANNE MARIE ZSAMBA
Network Real Estate Specialist
T: (201) 236-9224
M: (518) 350-3639
F: (724) 416-6112

## CROWN CASTLE

3 Corporate Park Drive, Suite 101
Clifton Park, NY 12065
CrownCastle.com

| From: | Zsamba, Anne Marie |
| :--- | :--- |
| To: | dwoods@stamfordct.gov |
| Subject: | Notice of Exempt Modification Submission to the Connecticut Siting Council - 69 Guinea Road, Stamford CT |
| Date: | Tuesday, March 24, 2020 1:46:00 PM |
| Attachments: | EM-T-MOBILE 69 GUINEA RD STAMFORD 806953 CT11071E 2.pdf |

Good afternoon Mr. Woods,

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council, today March 24, 2020.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable. If you could kindly confirm receipt.

Thank you.

Best,
Anne Marie Zsamba

## ANNE MARIE ZSAMBA

Network Real Estate Specialist
T: (201) 236-9224
M: (518) 350-3639
F: (724) 416-6112
CROWN CASTLE
3 Corporate Park Drive, Suite 101
Clifton Park, NY 12065
CrownCastle.com

## Exhibit A

## Original Facility Approval

Governor Ned Lamont


# CONNECTICUT SITING COUNCIL 

Home About Us Pending Matters Decisions Forms Contact Us

## Filing Guides

Meetings \& Minutes
Public Participation
Audio Link to New Britain Hearing Rooms
Programs \& Services
Telecommunications Database
Maps
Publications
Other Resources
Statutes \& Regulations
Frequently Asked Questions


Melanie Bachman,
Executive Director

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DOCKET NO. 180 - Cellco Partnership d/b/a Bell Atlantic Mobile application for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of a cellular telecommunications tower and associated equipment located immediately north of the Merritt Parkway off Guinea Road (prime and alternate one sites), or 141 Den Road (alternate two site) in Stamford, Connecticut.

## Connecticut Siting Council

April 2, 1998

## Decision and Order

Pursuant to the foregoing Findings of Fact and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the construction, operation, and maintenance of a telecommunications tower and equipment buildings at the proposed prime site in Stamford, Connecticut, including effects on the natural environment; ecological integrity and balance; public health and safety; scenic, historic, and recreational values; forests and parks; air and water purity; and fish and wildlife are not disproportionate either alone or cumulatively with other effects when compared to need, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application and therefore directs that a Certificate of Environmental Compatibility and Public Need, as provided by General Statutes § 16-50k, be issued to Bell Atlantic Mobile (BAM) for the construction, operation, and maintenance of a telecommunications tower, associated equipment, and buildings at the proposed prime site, located within a 28 -acre parcel at Guinea Road, Stamford, Connecticut. We find the effects on scenic resources and adjacent land uses of the first alternate site and second alternate site to be significant, and therefore deny certification of these sites.

The facility shall be constructed, operated, and maintained substantially as specified in the Council's record in this matter, and subject to the following conditions:

1. The tower shall be constructed as a monopole, no taller than necessary to provide the proposed telecommunications services, sufficient to accommodate the antennas of BAM, Springwich Cellular Limited Partnership (Springwich), Sprint PCS (Sprint), and Nextel Communications of the Mid-Atlantic, Inc. (Nextel); and such tower shall not exceed a height of 160 feet above ground level (AGL).
2. The Certificate Holder shall prepare a Development and Management (D\&M) Plan for this site in compliance with Sections $16-50 j-75$ through 16-50j-77 of the Regulations of Connecticut State Agencies. The D\&M Plan shall be submitted to and approved by the Council prior to the commencement of facility construction and shall include: adjustment of the tower location within the leased parcel to protect a nearby stream and minimize grade; a final site plan(s) for site development to include the location and specifications for the tower foundation, antennas, equipment buildings, emergency generator and fuel tank, security fence, access road, and utility line; construction plans for site clearing, tree trimming, water drainage, and erosion and sedimentation controls consistent with the Connecticut Guidelines for Soil Erosion and Sediment Control, as amended; provisions for the tower finish that may include painting; and provisions for the prevention and containment of spills and/or other discharge into surface water and ground water bodies.
3. Upon the establishment of any new State or federal radio frequency standards applicable to frequencies of this facility, the facility granted herein shall be brought into compliance with such standards.
4. The Certificate Holder shall provide the Council a recalculated report of electromagnetic radio frequency power density if and when circumstances in operation cause a change in power density above the levels originally calculated and provided in the application.
5. The Certificate Holder shall permit public or private entities to share space on the proposed tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
6. If the facility does not initially provide, or permanently ceases to provide cellular services following completion of construction, this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapplication for any continued or new use shall be made to the Council before any such use is made.
7. Any antenna that becomes obsolete and ceases to function shall be removed within 60 days after such antennas become obsolete and cease to function.
8. Unless otherwise approved by the Council, this Decision and Order shall be void if all construction authorized herein is not completed within three years of the effective date of this Decision and Order or within three years after all appeals to this Decision and Order have been resolved.

Pursuant to General Statutes § 16-50p, we hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed below, and notice of issuance shall be published in The Hartford Courant and Stamford Advocate.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section 16-50j-17 of the Regulations of Connecticut State Agencies.

The parties and intervenors to this proceeding are:

APPLICANT
Bell Atlantic Mobile

## ITS REPRESENTATIVE

Kenneth C. Baldwin, Esq.
Brian C. S. Freeman, Esq.
Robinson \& Cole
One Commercial Plaza
Hartford, CT 06103-3597
Mr. David S. Malko, P.E.
Jennifer Young Gaudet
Bell Atlantic Mobile
20 Alexander Drive
Wallingford, CT 06492

## INTERVENORS

Sprint Spectrum, L.P. d/b/a Sprint PCS

## ITS REPRESENTATIVE

Elias A. Alexiades

John W. Knuff
Harris, Beach \& Wilcox, LLP
147 North Broad Street
Milford, CT 06460
Nextel Communications of the Mid-Atlantic, Inc.d/b/a Nextel
Communications
Christopher B. Fisher, Esq.
Cuddy, Feder \& Worby, Esq.
90 Maple Avenue
White Plains, NY 10601
Springwich Cellular Limited Partnership Peter J. Tyrrell, Esq.
General Counsel
500 Enterprise Drive
Rocky Hill, CT 06067-3900

## PARTIES

Charles H. Nobs, Maurice Lucas, and Ben and Myrna Raphan

ITS REPRESENTATIVE
Jeffrey J. Mirman, Esq.
Levy \& Droney, P.C.
P.O. Box 887

Farmington, CT 06034

## Exhibit B

## Property Card

## 69 GUINEA ROAD

| Location | 69 GUINEA ROAD | Mblu | 002/6848/// |
| :---: | :---: | :---: | :---: |
| Acct\# | 002-6848 | Owner | GIRL SCOUTS OF CONNECTICUT INC |
| Assessment | \$1,028,420 | Appraisal | \$1,469,120 |
| PID | 24323 | ding Count | 1 |

## Current Value

| Appraisal |  |  |  |
| :---: | :---: | :---: | :---: |
| Valuation Year | Improvements | Land | Total |
| 2019 | \$461,570 | \$1,007,550 | \$1,469,120 |
| Assessment |  |  |  |
| Valuation Year | Improvements | Land | Total |
| 2019 | \$323,130 | \$705,290 | \$1,028,420 |

## Owner of Record

| Owner | GIRL SCOUTS OF CONNECTICUT INC | Sale Price | $\$ 0$ |
| :--- | :--- | :--- | :--- |
| Co-Owner |  | Book \& Page | $9322 / 0308$ |
| Address | 340 WASHINGTON STREET | Sale Date | $04 / 16 / 2008$ |
|  | HARTFORD, CT 06106-3317 | Instrument | 25 |

## Ownership History

| Ownership History |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Owner | Sale Price | Book \& Page | Instrument | Sale Date |
| GIRL SCOUTS OF CONNECTICUT INC | \$0 | 9322/0308 | 25 | 04/16/2008 |
| GIRL SCOUT COUNCIL SW CT INC | \$0 | 4405/0321 |  | 05/12/1995 |
| SOUTHWESTERN CT GIRL SCT | \$0 | 1035/0131 | 25 | 12/29/1964 |

## Building Information

Building 1 : Section 1

| Year Built: | 1963 |
| :--- | :--- |
| Living Area: | 1,960 |


| Field | Description |
| :---: | :---: |
| Style | Ranch |
| Model | Residential |
| Grade: | C+ |
| Stories: | 1 Story |
| Occupancy | 1 |
| Exterior Wall 1 | Cement fiberbd |
| Exterior Wall 2 |  |
| Roof Structure: | Gable/Hip |
| Roof Cover | Asph/F Gls/Cmp |
| Interior Wall 1 | Drywall |
| Interior Wall 2 |  |
| Interior Flr 1 | Hardwood |
| Interior Flr 2 |  |
| Heat Fuel | Electric |
| Heat Type: | Electr Basebrd |
| AC Type: | Central |
| Total Bedrooms: | 00 |
| Total Bthrms: | 1 |
| Total Half Baths: | 0 |
| Total Xtra Fixtrs: | 3 |
| Total Rooms: | 4 |
| Bath Style: | Average |
| Kitchen Style: | Typical |
| Fireplace Msnry. |  |
| Fpl. Gas/Prefab | 1 |
| Fpl. Outdoor |  |
| Fpl. Addnl. Open |  |
| Usrffld 105 |  |
| Usrffld 106 |  |
| Bsmt. Garage |  |
| Num Park |  |
| Fireplaces |  |
| Usrffld 108 |  |
| Usrffld 101 |  |
| Usffld 102 |  |
| Usffld 100 |  |
| Usrffld 300 |  |
| Usrfld 301 |  |

## Building Photo


(http://images.vgsi.com/photos/StamfordCTPhotos/^00111194179.jpg)
Building Layout

(http://images.vgsi.com/photos/StamfordCTPhotos//Sketches/24323_2432:

| Building Sub-Areas (sq ft) |  |  | Legend |
| :--- | :--- | ---: | ---: |
| Code | Description | Gross <br> Area | Living <br> Area |
| BAS | First Floor | 1,960 | 1,960 |
| RP2 | Porch Covered | 392 | 0 |
| UBM | Basement, Unfinished | 1,960 | 0 |
| WD1 | Deck, Wood | 252 | 0 |
|  |  | 4,564 | 1,960 |


| Extra Features Legend |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Code | Description | Size | Value | Bldg \# |
| RP2 | Porch Coverd | 1056.00 S.F | \$28,050 | 1 |
| RP2 | Porch Coverd | 756.00 S.F | \$20,080 | 1 |
| RP2 | Porch Coverd | 672.00 S.F | \$17,850 | 1 |
| RP2 | Porch Coverd | 216.00 S.F | \$5,740 | 1 |
| RP2 | Porch Coverd | 176.00 S.F | \$4,670 | 1 |

## Land

| Land Use |  | Land Line Valuation |  |
| :---: | :---: | :---: | :---: |
| Use Code | 901 | Size (Acres) | 16.86 |
| Description | Exmpt Res MDL-01 | Depth |  |
| Zone | RA3 | Assessed Value | \$705,290 |
| Neighborhood | 1100 | Appraised Value | \$1,007,550 |
| Alt Land Appr | No |  |  |
| Category |  |  |  |

Outbuildings

| Outbuildings |  |  |  |  |  | Legend |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Code | Description | Sub Code | Sub Description | Size | Value | Bldg \# |
| FC1 | Shed Wood |  |  | 240.00 S.F. | \$2,880 | 1 |
| MS1 | Misc Structure |  |  | 528.00 S.F. | \$3,170 | 1 |
| WD1 | Wood Deck |  |  | 252.00 S.F. | \$5,480 | 1 |
| CEL1 | Cell Tower |  |  | 1.00 SITES | \$146,250 | 1 |

Valuation History

| Appraisal |  |  |  |
| :---: | :---: | :---: | :---: |
| Valuation Year | Improvements | Land | Total |
| 2018 | \$461,570 | \$1,007,550 | \$1,469,120 |
| 2017 | \$461,570 | \$1,007,550 | \$1,469,120 |
| 2016 | \$438,650 | \$995,580 | \$1,434,230 |


| Assessment |  |  |  |
| :---: | :---: | :---: | :---: |
| Valuation Year | Improvements | Land | Total |
| 2018 | \$323,130 | \$705,290 | \$1,028,420 |
| 2017 | \$323,130 | \$705,290 | \$1,028,420 |
| 2016 | \$307,060 | \$696,910 | \$1,003,970 |



## Exhibit C

## Construction Drawings





|  | $2 \amalg$ $0 \leftrightarrows$ 0 0 0 0 | － | H＇TOdONON „0‥09I 9NLLSIXG <br> $\varepsilon 0690$ Lつ＇＇ণצOHNVLS वY V＇ヨNIก〇 69 <br> © C NGC <br>  <br> £૬6908：\＃Пя GILOILLS |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


（1）TOWER ELEVATION


| 足弟－ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\Theta$ | （） | （1） | ¢ |  |  |  |
|  | $\begin{array}{\|c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0.0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ \hline \end{array}$ |  |  |  |  |  |  |  |
|  |  | 陦 | （10910 | 㕩 | 踉 | 4 | （1） | （141） |





## Exhibit D

## Structural Analysis Report

Date: June 28, 2019
Darcy Tarr
Crown Castle
3530 Toringdon Way Suite 300
Charlotte, NC 28277

F<br>BLACK \& VEATCH<br>Building a world of difference. Black \& Veatch Corp.<br>6800 W. 115th St., Suite 2292<br>Overland Park, KS 66211<br>(913) 458-6909

| Subject: | Structural Analysis Report |  |
| :---: | :---: | :---: |
| Carrier Designation: | T-Mobile Co-Locate Carrier Site Number: Carrier Site Name: | CT11071E <br> Stamford/ MP X32/ <br> Den Rd. |
| Crown Castle Designation: | Crown Castle BU Number: <br> Crown Castle Site Name: <br> Crown Castle JDE Job Number: <br> Crown Castle Work Order Number: <br> Crown Castle Order Number: | $\begin{aligned} & 806953 \\ & \text { BRG } 2044 \text { (A) } 943097 \\ & 559199 \\ & 1747502 \\ & 479803 \text { Rev. } 0 \end{aligned}$ |
| Engineering Firm Designation: | Black \& Veatch Corp. Project Number: | 400087 |
| Site Data: | 69 Guinea Rd(Camp Rocky Craig), Stamford, Fairfield County, CT Latitude $41^{\circ} 6^{\prime} 6.35^{\prime \prime}$, Longitude - $73^{\circ} 35^{\prime} 41.45{ }^{\prime \prime}$ 160 Foot - Monopole Tower |  |

Dear Darcy Tarr,
Black \& Veatch Corp. is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Proposed Equipment Configuration
Sufficient Capacity - 66.3\%
This analysis utilizes an ultimate 3-second gust wind speed of 120 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Structural analysis prepared by: Kanchanaporn Rattanachan / Justin Vibbert
Respectfully submitted by:
Joshua J. Riley, P.E. Professional Engineer


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tnxTower Output

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## 1) INTRODUCTION

This tower is a 160 ft Monopole tower designed by Valmont Microflect.
The tower has been modified multiple times in the past to accommodate additional loading.
The tower has been modified per reinforcement drawings prepared by Aero Solutions LLC, in August of 2009. Reinforcement consists of addition of base plate stiffeners. This modification has not been considered due to a lack of a post modification inspection report.

The tower was later modified per reinforcement drawings prepared by Paul J. Ford \& Company in October of 2012. Reinforcement consisted of addition of flat plate reinforcement from $1.75^{\prime}$ to $16.75^{\prime}$ and $77^{\prime}$ to 82 '. It also consists of the installation of transition stiffeners. Refer to Modification Inspection report by Tower Engineering Professionals, Inc. in August of 2013. These modifications were found to be ineffective.

The tower was later modified per reinforcement drawings prepared by Paul J. Ford \& Company in April of 2014. Reinforcement consisted of addition of flat plate reinforcement from $12.25^{\prime}$ to $32.25^{\prime}, 32.33^{\prime}$ to $52.33^{\prime}$, and $78.5^{\prime}$ to $88.5^{\prime}$. Refer to Modification Inspection Report by Sinnott Gering and Schmitt Towers, Inc. in August of 2014. The $78.5^{\prime}$ to $88.5^{\prime}$ reinforcements were found to be effective and all others were found to be ineffective.

## 2) ANALYSIS CRITERIA

| TIA-222 Revision: | TIA-222-H |
| :--- | :--- |
| Risk Category: | II |
| Wind Speed: | 120 mph |
| Exposure Category: | B |
| Topographic Factor: | 1 |
| Ice Thickness: | 1.500 in |
| Wind Speed with Ice: | 50 mph |
| Service Wind Speed: | 60 mph |

Table 1 - Proposed Equipment Configuration

| Mounting Level (ft) | Center Line Elevation (ft) | $\begin{array}{\|l} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array}$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 118.0 | 118.0 | 1 | site pro 1 | HRK 12 [NA 507-1] | 10 | 1-5/8 |
|  |  | 3 | ericsson | AIR 32 B2A/B66AA w/ Mount Pipe |  |  |
|  |  | 3 | ericsson | ERICSSON AIR 21 B2A B4P w/ Mount Pipe |  |  |
|  |  | 3 | ericsson | RADIO 4449 B12/B71 |  |  |
|  |  | 3 | rfs celwave | APXVAARR24 43-U-NA20 w/ Mount Pipe |  |  |
|  |  | 1 | cci tower mounts | Platform Mount [LP 712-1] |  |  |
|  | 116.0 | 3 | ericsson | KRY 112 144/1 |  |  |

Table 2-Other Considered Equipment

| Mounting <br> Level (ft) | Center <br> Line <br> Elevation <br> (ft) | Number <br> of <br> ontennas | Antenna <br> Manufacturer | Antenna Model | Number <br> of Feed <br> Lines | Feed <br> Line <br> Size (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 157.0 | 158.0 | 3 | alcatel lucent | TD-RRH8x20-25 |  |  |
|  | 3 | argus technologies | LLPX310R-V1 <br> w/ Mount Pipe |  |  |  |


| Mounting Level (ft) | Center Line Elevation (ft) | $\left\lvert\, \begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}\right.$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | $\begin{array}{\|c} \text { Feed } \\ \text { Line } \\ \text { Size (in) } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1 | box enclosures and assembly | BEN-92P | $\begin{aligned} & 1 \\ & 4 \end{aligned}$ | $\begin{gathered} 1 / 8 \\ 17 / 64 \end{gathered}$ |
|  |  | 3 | nokia | FWHR | 1 | 1/2 |
|  |  | 3 | rfs celwave | APXVSPP18-C-A20 w/ Mount Pipe | $\begin{aligned} & 1 \\ & 3 \end{aligned}$ | $\begin{gathered} 5 / 8 \\ 7 / 8 \\ 1-1 / 4 \end{gathered}$ |
|  |  | 3 | rfs celwave | APXVTM14-ALU-I20 <br> w/ Mount Pipe |  |  |
|  | 157.0 | 1 | cci tower mounts | Platform Mount [LP 713-1] |  |  |
|  |  | 9 | rfs celwave | ACU-A20-N |  |  |
| 154.0 | 155.0 | 3 | alcatel lucent | 800 EXTERNAL NOTCH FILTER | - | - |
|  |  | 3 | alcatel lucent | 800MHZ RRH |  |  |
|  | 154.0 | 1 | cci tower mounts | Pipe Mount [PM 601-3] |  |  |
|  | 153.0 | 3 | alcatel lucent | $1900 \mathrm{MHz} \mathrm{RRH} \mathrm{(65MHz)}$ |  |  |
| 149.0 | 151.0 | 3 | cci antennas | HPA-65R-BUU-H6 w/ Mount Pipe | $\begin{gathered} 12 \\ 4 \\ 2 \\ 1 \end{gathered}$ | $\begin{gathered} 1-5 / 8 \\ 5 / 8 \\ 3 / 8 \\ 2 " \text { conduit } \end{gathered}$ |
|  |  | 3 | ericsson | RRUS 32 |  |  |
|  |  | 3 | ericsson | RRUS 4478 B5 |  |  |
|  |  | 3 | ericsson | RRUS12/RRUS A2 |  |  |
|  |  | 3 | kmw communications | $\begin{aligned} & \text { EPBQ-654L8H6-L2 } \\ & \text { w/ Mount Pipe } \end{aligned}$ |  |  |
|  |  | 3 | powerwave technologies | 7770.00 w/ Mount Pipe |  |  |
|  | 149.0 | 1 | cci tower mounts | Platform Mount [LP 713-1] |  |  |
|  |  | 3 | ericsson | RRUS 11 |  |  |
|  |  | 6 | powerwave technologies | LGP21401 |  |  |
|  |  | 6 | powerwave technologies | LGP21901 |  |  |
|  |  | 2 | raycap | DC6-48-60-18-8F |  |  |
| 139.0 | 142.0 | 3 | alcatel lucent | B13 RRH 4X30 | 13 | 1-5/8 |
|  |  | 3 | alcatel lucent | B66A RRH4X45 |  |  |
|  |  | 6 | andrew | DB846F65ZAXY w/ Mount Pipe |  |  |
|  |  | 6 | commscope | JAHH-65B-R3B w/ Mount Pipe |  |  |
|  |  | 1 | rfs celwave | DB-T1-6Z-8AB-0Z |  |  |
|  | 139.0 | 1 | cci tower mounts | Platform Mount [LP 713-1] |  |  |
| 84.0 | 84.0 | 1 | gps | GPS_A | - | - |
| 40.0 | 40.0 | 1 | andrew | GPS-QBW-20N | - | - |
|  |  | 1 | cci tower mounts | Pipe Mount [PM 601-1] |  |  |

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| 4-GEOTECHNICAL REPORTS | FDH Velocitel | 1104116 | CCISITES |
| 4-TOWER FOUNDATION <br> DRAWINGS/DESIGN/SPECS | Valmont Industries, Inc. | 1104113 | CCISITES |
| 4-TOWER MANUFACTURER <br> DRAWINGS | Valmont Microflect | 823122 | CCISITES |
| 4-TOWER REINFORCEMENT <br> DESIGN/DRAWINGS/DATA | Aero Solutions LLC | 1251715 | CCISITES |
| 4-TOWER REINFORCEMENT <br> DESIGN/DRAWINGS/DATA | Paul J. Ford \& Company | 3332716 | CCISITES |
| 4-POST-MODIFICATION <br> INSPECTION | Tower Engineering Professionals | 4015064 | CCISITES |
| 4-TOWER REINFORCEMENT <br> DESIGN/DRAWINGS/DATA | Paul J. Ford \& Company | 4837035 | CCISITES |
| 4-POST-MODIFICATION <br> INSPECTION | Sinnott Gering and Schmitt |  |  |
| Towers, Inc. | 5577141 | CCISITES |  |
| 4-EXPOSURE <br> CATEGORY/TOPOGRAPHIC <br> FACTOR | Crown Castle | 6124352 | CCISITES |

## 3.1) Analysis Method

tnxTower (version 8.0.5.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.
tnxTower was used to determine the loads on the modified structure. Additional calculations were performed to determine the stresses in the pole and in the reinforcing elements. These calculations are presented in Appendix C.

## 3.2) Assumptions

1) Tower and structures were built and maintained in accordance with the manufacturer's specifications.
2) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
3) The wind loading EPA of the panel antennas has been analyzed and determined by the tower owner. Verification of its accuracy is outside the scope of this structural analysis/design. Black \& Veatch does not assume any responsibility for its accuracy.
4) The wind loading Exposure Category and Topographic Category for this site have been analyzed and determined by the tower owner. Black \& Veatch does not assume any responsibility for its accuracy.
5) This analysis was performed under the assumption that all information provided to Black \& Veatch is current and correct. This is to include site data, appurtenance loading,
tower/foundation details, and geotechnical data. The loading on the structure is based on CAD level drawings and carrier orders provided by the owner. If any of this information is not current and correct, this report should be considered obsolete and further analysis will be required.

This analysis may be affected if any assumptions are not valid or have been made in error. Black \& Veatch Corp. should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary) (Monopole Tower)

| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass I Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 160-155 | Pole | TP20.801×19.6x0.25 | Pole | 2.2\% | Pass |
| 155-150 | Pole | TP22.002x20.801×0.25 | Pole | 5.9\% | Pass |
| 150-145 | Pole | TP23.203x22.002×0.25 | Pole | 13.4\% | Pass |
| 145-140 | Pole | TP24.404×23.203×0.25 | Pole | 19.7\% | Pass |
| 140-135 | Pole | TP25.605x24.404×0.25 | Pole | 29.8\% | Pass |
| 135-130 | Pole | TP26.806x25.605×0.25 | Pole | 37.7\% | Pass |
| 130-125 | Pole | TP28.007×26.806x0.25 | Pole | 44.8\% | Pass |
| 125-120 | Pole | TP29.208x28.007×0.25 | Pole | 51.2\% | Pass |
| 120-116 | Pole | TP31.29x29.208×0.25 | Pole | 57.0\% | Pass |
| 116-111 | Pole | TP30.867×29.669x0.3438 | Pole | 42.4\% | Pass |
| 111-106 | Pole | TP32.065 $30.867 \times 0.3438$ | Pole | 46.4\% | Pass |
| 106-101 | Pole | TP33.263×32.065x0.3438 | Pole | 50.1\% | Pass |
| 101-96 | Pole | TP34.461×33.263x0.3438 | Pole | 53.4\% | Pass |
| 96-91 | Pole | TP35.659x34.461×0.3438 | Pole | 56.5\% | Pass |
| 91-86 | Pole | TP36.857x35.659x0.3438 | Pole | 59.3\% | Pass |
| 86-85.75 | Pole + Reinf. | TP36.917x36.857x0.5125 | Reinf. 5 Tension Rupture | 56.6\% | Pass |
| 85.75-81 | Pole + Reinf. | TP38.055×36.917×0.5063 | Reinf. 5 Tension Rupture | 58.8\% | Pass |
| 81-80.75 | Pole | TP38.115 $38.055 \times 0.3438$ | Pole | 62.1\% | Pass |
| 80.75-80.5 | Pole | TP38.175×38.115×0.3438 | Pole | 62.2\% | Pass |
| 80.5-79 | Pole | TP39.912×38.175×0.3438 | Pole | 63.0\% | Pass |
| 79-72.25 | Pole | TP39.467×37.847×0.4063 | Pole | 54.0\% | Pass |
| $\begin{gathered} 72.25- \\ 67.25 \end{gathered}$ | Pole | TP40.667x39.467x0.4063 | Pole | 55.6\% | Pass |
| $\begin{aligned} & 67.25- \\ & 62.25 \end{aligned}$ | Pole | TP41.867×40.667x0.4063 | Pole | 57.2\% | Pass |
| $\begin{gathered} 62.25- \\ 57.25 \end{gathered}$ | Pole | TP43.067×41.867x0.4063 | Pole | 58.6\% | Pass |
| $\begin{gathered} 57.25- \\ 52.25 \end{gathered}$ | Pole | TP44.268x43.067x0.4063 | Pole | 60.0\% | Pass |
| $\begin{gathered} 52.25- \\ 49.83 \end{gathered}$ | Pole | TP44.848x44.268x0.4063 | Pole | 60.7\% | Pass |
| $\begin{array}{r} 49.83- \\ 49.58 \\ \hline \end{array}$ | Pole | TP44.908x44.848x0.4063 | Pole | 60.7\% | Pass |
| $\begin{array}{r} 49.58- \\ 44.58 \end{array}$ | Pole | TP46.109x44.908x0.4063 | Pole | 62.1\% | Pass |
| 44.58-43 | Pole | TP48.088×46.109x0.4063 | Pole | 62.5\% | Pass |
| 43-35.33 | Pole | TP47.516x45.675×0.4375 | Pole | 59.5\% | Pass |
| $\begin{gathered} 35.33 \\ 32.25 \end{gathered}$ | Pole | TP48.256x47.516x0.4375 | Pole | 60.2\% | Pass |
| 32.25-32 | Pole | TP48.317×48.256x0.4375 | Pole | 60.2\% | Pass |


| $32-27$ | Pole | TP49.517x48.317x0.4375 | Pole | $61.2 \%$ | Pass |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $27-22$ | Pole | TP50.718x49.517x0.4375 | Pole | $62.2 \%$ | Pass |
| $22-17$ | Pole | TP5 $1.918 \times 50.718 \times 0.4375$ | Pole | $63.2 \%$ | Pass |
| $17-15.5$ | Pole | TP52.278 $51.918 \times 0.4375$ | Pole | $63.4 \%$ | Pass |
| $15.5-15.25$ | Pole | TP52.338 $\times 52.278 \times 0.4375$ | Pole | $63.5 \%$ | Pass |
| $15.25-$ |  |  |  |  |  |
| 14.75 | Pole | TP52.458x52.338x0.4375 | Pole | $63.6 \%$ | Pass |
| $14.75-14.5$ | Pole | TP52.518x52.458x0.4375 | Pole | $63.6 \%$ | Pass |
| $14.5-9.5$ | Pole | TP53.719x52.518x0.4375 | Pole | $64.6 \%$ | Pass |
| $9.5-4.5$ | Pole | TP54.92x53.719x0.4375 | Pole | $65.5 \%$ | Pass |
| $4.5-0$ | Pole | TP56x54.92x0.4375 | Pole | $66.3 \%$ | Pass |
|  |  |  |  | Summary |  |
|  |  |  | Pole | $66.3 \%$ | Pass |
|  |  |  | Overall | $66.3 \%$ | Pass |

Table 5 - Tower Component Stresses vs. Capacity (Monopole Tower) - LC7

| Notes | Component | Elevation (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Anchor Rods | 0 | 55.8 | Pass |
|  | Base Plate |  | 38.8 | Pass |
| 1 | Base Foundation | 0 | 20.8 | Pass |
|  | Base Foundation Soil Interaction |  | 62.1 | Pass |
| Structure Rating (max from all components) = |  |  |  | 66.3\% |

Notes:

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity. Rating per TIA-222-H Section 15.5.

## 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

## APPENDIX A

TNXTOWER OUTPUT

| Section | 42 | 41 | 403236 |  | 34 | 333 | 323180 | 30 | 282726 | 25 | 24 | 23 | 222 | 21 | 20 | 㛵 1711 | 11515 | 14 | 13 | 12 | 1110 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Length (ft) | 4.50 | 5.00 | 5.000025 | 5.00 | 5.00 | 5.000. | 25. 08 | 7.8725 | 5.000 .2542 | 5.00 | 5.00 | 5.00 | 5.00 |  | 6.7625 | (1) $5^{5} 5.750$. | 2. 55.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.0®. 67 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 |
| Number of Sides | 12 | 12 | 12 12an | 212 | 12 | 1212 | 121212 | $2 \quad 12$ | $12 \quad 1212$ | 12 | 12 | 12 | 12 | 12 | 12 | 性 12 12 | 1212 | 12 | 12 | 12 | 1212 | 212 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Thickness (in) | 0.4375 | 0.4375 | 0.43 amas | \$. 4375 | 0.4375 | 0.43654 | 4.4 .78753 | 33750.4063 | 0.408300600930 | 30.4063 | 0.4063 | 0.4063 | 0.40634 | 40630 | 30.34380 .3 | 343\%063 | ${ }^{253438}$ | 0.3438 | 0.3438 | 0.3438 | 0.340843 | 380.2500 | 0.2500 | 0.2500 | 0.2500 | 0.2500 | 0.2500 | 0.2500 | 0.2500 | 0.2500 |
| Socket Length (ft) |  |  |  |  |  |  |  | 6.67 |  |  |  |  |  |  | 5.75 |  |  |  |  |  |  | 4.67 |  |  |  |  |  |  |  |  |
| Top Dia (in) | 54.9195 | 553.7190 | 52.54 Bxa | 880.717 | 49.517 | \|48.34882| | 24xatar | 22546.1086 | 44.99845489483 | 43.06 | 1.8673 | 340.6671 | 39.46370 |  | 88.174389 | .1485C036.8 | \%35.6591\|34 | 34.4611 | 33.2631 | 32.0650 | 30.889 ¢6 6 | $69 ¢ 9.2082$ | 28.00722 | 26.8062 | 25.605 | 24.4041 | 23.2031 | 22.0021 | 20.801 | 19.6000 |
| Bot Dia (in) | 56.00 | . 91 |  | 88.918 | 50.717 | 49.5488* | 4.9.185051 | 516248.0880 | 46.1980 | 26 | 3.06 | 1.86 | 40.66 |  | 9.912 38. | Hase 56.8 | . P6BC8571\| $^{\text {a }}$ | 35.65 | 34.461 | 33.263 | 32.08686 | 67031.2900 | 29.20822 | 28.007 | 26.806 | 25.605 | 24.404 | 23.203 | 22.002 | 120.8010 |
| Grade |  |  |  |  |  |  |  |  |  |  |  |  |  |  | A572 | 2-65 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Weight (K) 27.7 | 1.2 | 1.3 | 1.3 contu. 4 | 41.2 | 1.2 | 1.20 | 0. 10.71 .7 | -7 1.7 | 1.000 .5 | 1.0 | 0.9 | 0.9 | 0.9 | 1.1 | 1.1 | O\|| 1.00 | $0 . \mid 00.7$ | 0.7 | 0.6 | 0.6 | 0.60 .6 | $6 \quad 0.7$ | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |



ALL REACTIONS ARE FACTORED


TORQUE 0 kip-ft 50 mph WIND - 1.5000 in ICE


TORQUE 2 kip-ft REACTIONS - 120 mph WIND

## Tower Input Data

The tower is a monopole.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:

1) Tower is located in Fairfield County, Connecticut.
2) Tower base elevation above sea level: 220.00 ft .
3) Basic wind speed of 120 mph .
4) Risk Category II.
5) Exposure Category B.
6) Simplified Topographic Factor Procedure for wind speed-up calculations is used.
7) Topographic Category: 1.
8) Crest Height: 0.00 ft .
9) Nominal ice thickness of 1.5000 in.
10) Ice thickness is considered to increase with height.
11) Ice density of 56 pcf.
12) A wind speed of 50 mph is used in combination with ice.
13) Temperature drop of $50^{\circ} \mathrm{F}$.
14) Deflections calculated using a wind speed of 60 mph .
15) TIA-222-H Annex S.
16) A non-linear (P-delta) analysis was used.
17) Pressures are calculated at each section.
18) Stress ratio used in pole design is 1.05 .
19) Tower analysis based on target reliabilities in accordance with Annex S.
20) Load Modification Factors used: $\mathrm{K}_{\mathrm{es}}\left(\mathrm{F}_{\mathrm{w}}\right)=0.95, \mathrm{~K}_{\text {es }}\left(\mathrm{t}_{\mathrm{i}}\right)=0.85$.
21) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

## Consider Moments - Legs

Consider Moments - Horizontals
Consider Moments - Diagonals
Use Moment Magnification
Use Code Stress Ratios
$\checkmark$ Use Code Safety Factors - Guys
Escalate Ice
Always Use Max Kz
Use Special Wind Profile
Include Bolts In Member Capacity
Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric

Distribute Leg Loads As Uniform Assume Legs Pinned $\checkmark$ Assume Rigid Index Plate
$\checkmark$ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
$\checkmark$ Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt.
Autocalc Torque Arm Areas
Add IBC . 6D+W Combination
Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

Use ASCE 10 X-Brace Ly Rules
Calculate Redundant Bracing Forces
Ignore Redundant Members in FEA
SR Leg Bolts Resist Compression
All Leg Panels Have Same Allowable
Offset Girt At Foundation
$\checkmark$ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption
Use TIA-222-H Tension Splice Exemption

## Poles

$\sqrt{ }$ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

## Tapered Pole Section Geometry

| Section | Elevation | Section <br> Length <br> ft | Splice <br> Length <br> ft | Number <br> of <br> Sides | Top <br> Diameter <br> in | Bottom <br> Diameter <br> in | Wall <br> Thickness <br> in | Bend <br> Radius <br> in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $160.00-155.00$ | 5.00 | 0.00 | 12 | 19.6000 | 20.8010 | 0.2500 | 1.0000 | A572-65 |

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| Section | Elevation ft | Section <br> Length ft | Splice <br> Length ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L2 | 155.00-150.00 | 5.00 | 0.00 | 12 | 20.8010 | 22.0021 | 0.2500 | 1.0000 | (65 ksi) |
|  |  |  |  |  |  |  |  |  | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L3 | 150.00-145.00 | 5.00 | 0.00 | 12 | 22.0021 | 23.2031 | 0.2500 | 1.0000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L4 | 145.00-140.00 | 5.00 | 0.00 | 12 | 23.2031 | 24.4041 | 0.2500 | 1.0000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L5 | 140.00-135.00 | 5.00 | 0.00 | 12 | 24.4041 | 25.6051 | 0.2500 | 1.0000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L6 | 135.00-130.00 | 5.00 | 0.00 | 12 | 25.6051 | 26.8062 | 0.2500 | 1.0000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L7 | 130.00-125.00 | 5.00 | 0.00 | 12 | 26.8062 | 28.0072 | 0.2500 | 1.0000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L8 | 125.00-120.00 | 5.00 | 0.00 | 12 | 28.0072 | 29.2082 | 0.2500 | 1.0000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L9 | 120.00-111.33 | 8.67 | 4.67 | 12 | 29.2082 | 31.2900 | 0.2500 | 1.0000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L10 | 111.33-111.00 | 5.00 | 0.00 | 12 | 29.6690 | 30.8670 | 0.3438 | 1.3750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L11 | 111.00-106.00 | 5.00 | 0.00 | 12 | 30.8670 | 32.0650 | 0.3438 | 1.3750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L12 | 106.00-101.00 | 5.00 | 0.00 | 12 | 32.0650 | 33.2631 | 0.3438 | 1.3750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L13 | 101.00-96.00 | 5.00 | 0.00 | 12 | 33.2631 | 34.4611 | 0.3438 | 1.3750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L14 | 96.00-91.00 | 5.00 | 0.00 | 12 | 34.4611 | 35.6591 | 0.3438 | 1.3750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L15 | 91.00-86.00 | 5.00 | 0.00 | 12 | 35.6591 | 36.8571 | 0.3438 | 1.3750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L16 | 86.00-85.75 | 0.25 | 0.00 | 12 | 36.8571 | 36.9170 | 0.5125 | 2.0500 |  |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L17 | 85.75-81.00 | 4.75 | 0.00 | 12 | 36.9170 | 38.0551 | 0.5062 | 2.0250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L18 | 81.00-80.75 | 0.25 | 0.00 | 12 | 38.0551 | 38.1150 | 0.3438 | 1.3750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L19 | 80.75-80.50 | 0.25 | 0.00 | 12 | 38.1150 | 38.1749 | 0.3438 | 1.3750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L20 | 80.50-73.25 | 7.25 | 5.75 | 12 | 38.1749 | 39.9120 | 0.3438 | 1.3750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L21 | 73.25-72.25 | 6.75 | 0.00 | 12 | 37.8468 | 39.4670 | 0.4063 | 1.6250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L22 | 72.25-67.25 | 5.00 | 0.00 | 12 | 39.4670 | 40.6671 | 0.4063 | 1.6250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L23 | 67.25-62.25 | 5.00 | 0.00 | 12 | 40.6671 | 41.8673 | 0.4063 | 1.6250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L24 | 62.25-57.25 | 5.00 | 0.00 | 12 | 41.8673 | 43.0674 | 0.4063 | 1.6250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L25 | 57.25-52.25 | 5.00 | 0.00 | 12 | 43.0674 | 44.2675 | 0.4063 | 1.6250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L26 | 52.25-49.83 | 2.42 | 0.00 | 12 | 44.2675 | 44.8484 | 0.4063 | 1.6250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L27 | 49.83-49.58 | 0.25 | 0.00 | 12 | 44.8484 | 44.9084 | 0.4063 | 1.6250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L28 | 49.58-44.58 | 5.00 | 0.00 | 12 | 44.9084 | 46.1086 | 0.4063 | 1.6250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L29 | 44.58-36.33 | 8.25 | 6.67 | 12 | 46.1086 | 48.0880 | 0.4063 | 1.6250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L30 | 36.33-35.33 | 7.67 | 0.00 | 12 | 45.6753 | 47.5162 | 0.4375 | 1.7500 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L31 | 35.33-32.25 | 3.08 | 0.00 | 12 | 47.5162 | 48.2565 | 0.4375 | 1.7500 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L32 | 32.25-32.00 | 0.25 | 0.00 | 12 | 48.2565 | 48.3165 | 0.4375 | 1.7500 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L33 | 32.00-27.00 | 5.00 | 0.00 | 12 | 48.3165 | 49.5171 | 0.4375 | 1.7500 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L34 | 27.00-22.00 | 5.00 | 0.00 | 12 | 49.5171 | 50.7176 | 0.4375 | 1.7500 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L35 | 22.00-17.00 | 5.00 | 0.00 | 12 | 50.7176 | 51.9181 | 0.4375 | 1.7500 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |


| Section | Elevation | Section <br> Length <br> $f t$ | Splice <br> Length <br> ft | Number <br> of <br> Sides | Top <br> Diameter <br> in | Bottom <br> Diameter <br> in | Wall <br> Thickness <br> in | Bend <br> Radius |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in |  |  |  |  |  |  |  |  |

Tapered Pole Properties

| Section | $\begin{gathered} \text { Tip Dia. } \\ \text { in } \end{gathered}$ | Area $i n^{2}$ | $\begin{gathered} 1 \\ i n^{4} \end{gathered}$ | $\begin{gathered} r \\ \text { in } \end{gathered}$ | $\begin{gathered} \text { C } \\ \text { in } \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{gathered} I t / Q \\ i n^{2} \end{gathered}$ | $\begin{aligned} & \text { w } \\ & \text { in } \end{aligned}$ | w/t |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 20.2032 | 15.5768 | 744.4315 | 6.9273 | 10.1528 | 73.3228 | 1508.4200 | 7.6664 | 4.5828 | 18.331 |
|  | 21.4466 | 16.5436 | 891.8307 | 7.3573 | 10.7749 | 82.7690 | 1807.0908 | 8.1422 | 4.9047 | 19.619 |
| L2 | 21.4466 | 16.5436 | 891.8307 | 7.3573 | 10.7749 | 82.7690 | 1807.0908 | 8.1422 | 4.9047 | 19.619 |
|  | 22.6900 | 17.5104 | 1057.5054 | 7.7872 | 11.3971 | 92.7875 | 2142.7926 | 8.6181 | 5.2266 | 20.906 |
| L3 | 22.6900 | 17.5104 | 1057.5054 | 7.7872 | 11.3971 | 92.7875 | 2142.7926 | 8.6181 | 5.2266 | 20.906 |
|  | 23.9334 | 18.4772 | 1242.5239 | 8.2172 | 12.0192 | 103.3783 | 2517.6902 | 9.0939 | 5.5484 | 22.194 |
| L4 | 23.9334 | 18.4772 | 1242.5239 | 8.2172 | 12.0192 | 103.3783 | 2517.6902 | 9.0939 | 5.5484 | 22.194 |
|  | 25.1768 | 19.4441 | 1447.9539 | 8.6472 | 12.6413 | 114.5413 | 2933.9472 | 9.5698 | 5.8703 | 23.481 |
| L5 | 25.1768 | 19.4441 | 1447.9539 | 8.6472 | 12.6413 | 114.5413 | 2933.9472 | 9.5698 | 5.8703 | 23.481 |
|  | 26.4202 | 20.4109 | 1674.8639 | 9.0771 | 13.2635 | 126.2766 | 3393.7282 | 10.0456 | 6.1922 | 24.769 |
| L6 | 26.4202 | 20.4109 | 1674.8639 | 9.0771 | 13.2635 | 126.2766 | 3393.7282 | 10.0456 | 6.1922 | 24.769 |
|  | 27.6636 | 21.3777 | 1924.3214 | 9.5071 | 13.8856 | 138.5841 | 3899.1969 | 10.5215 | 6.5141 | 26.056 |
| L7 | 27.6636 | 21.3777 | 1924.3214 | 9.5071 | 13.8856 | 138.5841 | 3899.1969 | 10.5215 | 6.5141 | 26.056 |
|  | 28.9070 | 22.3445 | 2197.3950 | 9.9371 | 14.5077 | 151.4638 | 4452.5181 | 10.9973 | 6.8359 | 27.344 |
| L8 | 28.9070 | 22.3445 | 2197.3950 | 9.9371 | 14.5077 | 151.4638 | 4452.5181 | 10.9973 | 6.8359 | 27.344 |
|  | 30.1504 | 23.3114 | 2495.1526 | 10.3670 | 15.1299 | 164.9158 | 5055.8556 | 11.4731 | 7.1578 | 28.631 |
| L9 | 30.1504 | 23.3114 | 2495.1526 | 10.3670 | 15.1299 | 164.9158 | 5055.8556 | 11.4731 | 7.1578 | 28.631 |
|  | 32.3056 | 24.9872 | 3072.8897 | 11.1123 | 16.2082 | 189.5883 | 6226.5076 | 12.2979 | 7.7157 | 30.863 |
| L10 | 31.7520 | 32.4594 | 3562.9622 | 10.4985 | 15.3686 | 231.8345 | 7219.5273 | 15.9755 | 7.0301 | 20.451 |
|  | 31.8347 | 33.7855 | 4017.7105 | 10.9273 | 15.9891 | 251.2777 | 8140.9708 | 16.6282 | 7.3511 | 21.385 |
| L11 | 31.8347 | 33.7855 | 4017.7105 | 10.9273 | 15.9891 | 251.2777 | 8140.9708 | 16.6282 | 7.3511 | 21.385 |
|  | 33.0749 | 35.1115 | 4509.5937 | 11.3562 | 16.6097 | 271.5037 | 9137.6595 | 17.2808 | 7.6722 | 22.319 |
| L12 | 33.0749 | 35.1115 | 4509.5937 | 11.3562 | 16.6097 | 271.5037 | 9137.6595 | 17.2808 | 7.6722 | 22.319 |
|  | 34.3152 | 36.4376 | 5040.0701 | 11.7851 | 17.2303 | 292.5127 | $\begin{gathered} 10212.548 \\ 6 \end{gathered}$ | 17.9335 | 7.9932 | 23.253 |
| L13 | 34.3152 | 36.4376 | 5040.0701 | 11.7851 | 17.2303 | 292.5127 | $\begin{gathered} 10212.548 \\ 6 \end{gathered}$ | 17.9335 | 7.9932 | 23.253 |
|  | 35.5555 | 37.7636 | 5610.5969 | 12.2140 | 17.8508 | 314.3045 | $\begin{gathered} 11368.590 \\ 4 \end{gathered}$ | 18.5861 | 8.3143 | 24.187 |
| L14 | 35.5555 | 37.7636 | 5610.5969 | 12.2140 | 17.8508 | 314.3045 | $\begin{gathered} 11368.590 \\ 4 \end{gathered}$ | 18.5861 | 8.3143 | 24.187 |
|  | 36.7957 | 39.0896 | 6222.6314 | 12.6429 | 18.4714 | 336.8793 | ${ }_{3}^{12608.738}$ | 19.2387 | 8.6354 | 25.121 |
| L15 | 36.7957 | 39.0896 | 6222.6314 | 12.6429 | 18.4714 | 336.8793 | $\begin{gathered} 12608.738 \\ 3 \end{gathered}$ | 19.2387 | 8.6354 | 25.121 |
|  | 38.0360 | 40.4157 | 6877.6307 | 13.0718 | 19.0920 | 360.2369 | $\begin{gathered} 13935.944 \\ 5 \end{gathered}$ | 19.8914 | 8.9564 | 26.055 |
| L16 | 37.9765 | 59.9776 | $10112.409$ | 13.0114 | 19.0920 | 529.6683 | $\begin{gathered} 20490.483 \\ 6 \end{gathered}$ | 29.5192 | 8.5042 | 16.594 |
|  | 38.0385 | 60.0765 | $\begin{array}{r} 10162.492 \\ \hline \end{array}$ | 13.0328 | 19.1230 | 531.4278 | $\begin{gathered} 20591.964 \\ 3 \end{gathered}$ | 29.5678 | 8.5203 | 16.625 |
| L17 | 38.0407 | 59.3540 | $\begin{gathered} 10043.730 \\ 5 \end{gathered}$ | 13.0350 | 19.1230 | 525.2174 | $\begin{gathered} 20351.321 \\ 1 \end{gathered}$ | 29.2123 | 8.5370 | 16.863 |
|  | 39.2189 | 61.2093 | $\begin{gathered} 11015.300 \\ 9 \end{gathered}$ | 13.4425 | 19.7125 | 558.7968 | $\begin{gathered} 22319.985 \\ 9 \end{gathered}$ | 30.1254 | 8.8420 | 17.466 |
| L18 | 39.2763 | 41.7417 | 7577.0535 | 13.5007 | 19.7125 | 384.3774 | 15353.164 | 20.5440 | 9.2775 | 26.989 |

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| Section | Tip Dia. in | Area $i n^{2}$ | $\stackrel{I}{i n^{4}}$ | $\begin{aligned} & r \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { C } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & I / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{gathered} I t / Q \\ i i^{2} \end{gathered}$ | $\begin{aligned} & \text { w } \\ & \text { in } \end{aligned}$ | w/t |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L19 | 39.3383 | 41.8080 | 7613.2166 | 13.5221 | 19.7436 | 385.6050 | $\begin{gathered} 6 \\ 15426.440 \\ 9 \end{gathered}$ | 20.5766 | 9.2936 | 27.036 |
|  | 39.3383 | 41.8080 | 7613.2166 | 13.5221 | 19.7436 | 385.6050 | $\begin{gathered} 15426.440 \\ 9 \end{gathered}$ | 20.5766 | 9.2936 | 27.036 |
| L20 | 39.4003 | 41.8743 | 7649.4953 | 13.5435 | 19.7746 | 386.8345 | $\begin{gathered} 15499.951 \\ 3 \end{gathered}$ | 20.6093 | 9.3096 | 27.083 |
|  | 39.4003 | 41.8743 | 7649.4953 | 13.5435 | 19.7746 | 386.8345 | $\begin{gathered} 15499.951 \\ 3 \end{gathered}$ | 20.6093 | 9.3096 | 27.083 |
| L21 | 41.1987 | 43.7971 | 8752.3577 | 14.1654 | 20.6744 | 423.3424 | $\begin{gathered} 17734.649 \\ 5 \end{gathered}$ | 21.5556 | 9.7752 | 28.437 |
|  | 40.4674 | 48.9769 | 8763.1762 | 13.4037 | 19.6046 | 446.9951 | $\begin{gathered} 17756.570 \\ 7 \end{gathered}$ | 24.1049 | 9.0542 | 22.287 |
| L22 | 40.7159 | 51.0963 | 9950.7610 | 13.9837 | 20.4439 | 486.7351 | $\begin{gathered} 20162.939 \\ 6 \end{gathered}$ | 25.1481 | 9.4884 | 23.356 |
|  | 40.7159 | 51.0963 | 9950.7610 | 13.9837 | 20.4439 | 486.7351 | $\begin{gathered} 20162.939 \\ 6 \end{gathered}$ | 25.1481 | 9.4884 | 23.356 |
| L23 | 41.9584 | 52.6663 | $\begin{gathered} 10896.442 \\ 4 \end{gathered}$ | 14.4134 | 21.0656 | 517.2631 | $\begin{gathered} 22079.146 \\ 4 \end{gathered}$ | 25.9207 | 9.8100 | 24.148 |
|  | 41.9584 | 52.6663 | $\begin{gathered} 10896.442 \\ 4 \end{gathered}$ | 14.4134 | 21.0656 | 517.2631 | $\begin{gathered} 22079.146 \\ 4 \end{gathered}$ | 25.9207 | 9.8100 | 24.148 |
| L24 | 43.2009 | 54.2362 | $\begin{gathered} 11900.218 \\ 1 \end{gathered}$ | 14.8430 | 21.6872 | 548.7198 | $\begin{gathered} 24113.068 \\ 3 \end{gathered}$ | 26.6934 | 10.1317 | 24.94 |
|  | 43.2009 | 54.2362 | $\begin{gathered} 11900.218 \\ 1 \end{gathered}$ | 14.8430 | 21.6872 | 548.7198 | $\begin{gathered} 24113.068 \\ 3 \end{gathered}$ | 26.6934 | 10.1317 | 24.94 |
| L25 | 44.4433 | 55.8061 | $\begin{gathered} 12963.819 \\ 1 \end{gathered}$ | 15.2727 | 22.3089 | 581.1049 | $\begin{gathered} 26268.212 \\ 2 \end{gathered}$ | 27.4661 | 10.4533 | 25.731 |
|  | 44.4433 | 55.8061 | $\begin{gathered} 12963.819 \\ 1 \end{gathered}$ | 15.2727 | 22.3089 | 581.1049 | $\begin{gathered} 26268.212 \\ 2 \end{gathered}$ | 27.4661 | 10.4533 | 25.731 |
| L26 | 45.6858 | 57.3761 | $\begin{gathered} 14088.978 \\ 8 \end{gathered}$ | 15.7023 | 22.9306 | 614.4186 | $\begin{gathered} 28548.090 \\ 8 \end{gathered}$ | 28.2387 | 10.7750 | 26.523 |
|  | 45.6858 | 57.3761 | $\begin{gathered} 14088.978 \\ 8 \end{gathered}$ | 15.7023 | 22.9306 | 614.4186 | $\begin{gathered} 28548.090 \\ 8 \end{gathered}$ | 28.2387 | 10.7750 | 26.523 |
| L27 | 46.2872 | 58.1359 | $\begin{gathered} 14656.178 \\ 0 \end{gathered}$ | 15.9103 | 23.2315 | 630.8758 | $\begin{gathered} 29697.390 \\ 1 \end{gathered}$ | 28.6127 | 10.9306 | 26.906 |
|  | 46.2872 | 58.1359 | $\begin{gathered} 14656.178 \\ 0 \end{gathered}$ | 15.9103 | 23.2315 | 630.8758 | $\begin{gathered} 29697.390 \\ 1 \end{gathered}$ | 28.6127 | 10.9306 | 26.906 |
| L28 | 46.3493 | 58.2144 | $\begin{gathered} 14715.625 \\ 7 \end{gathered}$ | 15.9318 | 23.2626 | 632.5884 | $\begin{gathered} 29817.847 \\ 2 \end{gathered}$ | 28.6514 | 10.9467 | 26.946 |
|  | 46.3493 | 58.2144 59.7843 | $\begin{gathered} 14715.625 \\ 7 \end{gathered}$ | 15.9318 16.3614 | 23.2626 | 632.5884 | $\begin{gathered} 29817.847 \\ 2 \end{gathered}$ | 28.6514 | 10.9467 | 26.946 |
| L29 | 47.5918 | 59.7843 | $\begin{gathered} 15938.580 \\ 9 \end{gathered}$ | 16.3614 | 23.8842 | 667.3264 | $\begin{gathered} 32295.886 \\ 1 \end{gathered}$ | 29.4240 | 11.2683 | 27.737 |
|  | 47.5918 | 59.7843 | $\begin{gathered} 15938.580 \\ 9 \end{gathered}$ | 16.3614 | 23.8842 | 667.3264 | $\begin{gathered} 32295.886 \\ 1 \end{gathered}$ | 29.4240 | 11.2683 | 27.737 |
| L30 | 49.6411 | 62.3737 | $\begin{gathered} 18100.549 \\ 3 \end{gathered}$ | 17.0701 | 24.9096 | 726.6500 | $\begin{gathered} 36676.620 \\ 2 \end{gathered}$ | 30.6984 | 11.7988 | 29.043 |
|  | 48.7894 | 63.7288 | $\begin{gathered} 16646.557 \\ 0 \end{gathered}$ | 16.1951 | 23.6598 | 703.5796 | $\begin{gathered} 33730.437 \\ 7 \end{gathered}$ | 31.3654 | 11.0685 | 25.299 |
| L31 | 49.0380 | 66.3220 | $\begin{gathered} 18762.550 \\ 8 \end{gathered}$ | 16.8542 | 24.6134 | 762.2911 | $\begin{gathered} 38018.014 \\ 7 \end{gathered}$ | 32.6417 | 11.5618 | 26.427 |
|  | 49.0380 | 66.3220 | $\begin{gathered} 18762.550 \\ 8 \end{gathered}$ | 16.8542 | 24.6134 | 762.2911 | $\begin{gathered} 38018.014 \\ 7 \end{gathered}$ | 32.6417 | 11.5618 | 26.427 |
| L32 | 49.8044 | 67.3650 | $\begin{gathered} 19661.685 \\ 7 \end{gathered}$ | 17.1192 | 24.9969 | 786.5664 | $\begin{gathered} 39839.905 \\ 8 \end{gathered}$ | 33.1550 | 11.7602 | 26.881 |
|  | 49.8044 | 67.3650 | $\begin{gathered} 19661.685 \\ 7 \end{gathered}$ | 17.1192 | 24.9969 | 786.5664 | $\begin{gathered} 39839.905 \\ 8 \end{gathered}$ | 33.1550 | 11.7602 | 26.881 |
| L33 | 49.8666 | 67.4495 | $\begin{gathered} 19735.823 \\ 7 \end{gathered}$ | 17.1407 | 25.0280 | 788.5513 | $\begin{gathered} 39990.129 \\ 4 \end{gathered}$ | 33.1966 | 11.7763 | 26.917 |
|  | 49.8666 | 67.4495 | $\begin{gathered} 19735.823 \\ 7 \end{gathered}$ | 17.1407 | 25.0280 | 788.5513 | $\begin{gathered} 39990.129 \\ 4 \end{gathered}$ | 33.1966 | 11.7763 | 26.917 |
| L34 | 51.1095 | 69.1408 | $\begin{gathered} 21257.963 \\ 1 \end{gathered}$ | 17.5705 | 25.6498 | 828.7759 | $\begin{gathered} 43074.396 \\ 5 \end{gathered}$ | 34.0290 | 12.0981 | 27.653 |
|  | 51.1095 | 69.1408 | $\begin{gathered} 21257.963 \\ 1 \end{gathered}$ | 17.5705 | 25.6498 | 828.7759 | $\begin{gathered} 43074.396 \\ 5 \end{gathered}$ | 34.0290 | 12.0981 | 27.653 |
| L35 | 52.3524 | 70.8321 | $\begin{gathered} 22856.420 \\ 9 \end{gathered}$ | 18.0003 | 26.2717 | 870.0011 | $\begin{gathered} 46313.305 \\ 5 \end{gathered}$ | 34.8614 | 12.4198 | 28.388 |
|  | 52.3524 | 70.8321 | $\begin{gathered} 22856.420 \\ 9 \end{gathered}$ | 18.0003 | 26.2717 | 870.0011 | $\begin{gathered} 46313.305 \\ 5 \end{gathered}$ | 34.8614 | 12.4198 | 28.388 |
|  | 53.5953 | 72.5234 | 24533.064 | 18.4301 | 26.8936 | 912.2269 | 49710.639 | 35.6938 | 12.7416 | 29.124 |

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| Section | $\begin{gathered} \text { Tip Dia. } \\ \text { in } \end{gathered}$ | Area $i n^{2}$ | $\stackrel{I}{i n^{4}}$ | $\begin{gathered} r \\ \text { in } \end{gathered}$ | $\begin{aligned} & C \\ & \text { in } \end{aligned}$ | $\begin{aligned} & I / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{gathered} I t / Q \\ i n^{2} \end{gathered}$ | $\begin{aligned} & w \\ & \text { in } \end{aligned}$ | w/t |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L36 | 53.5953 | 72.5234 | $\begin{gathered} 0 \\ 24533.064 \\ 0 \end{gathered}$ | 18.4301 | 26.8936 | 912.2269 | $\begin{gathered} 0 \\ 49710.639 \\ 0 \end{gathered}$ | 35.6938 | 12.7416 | 29.124 |
| L37 | 53.9682 | 73.0307 | $\begin{gathered} 25051.581 \\ 0 \end{gathered}$ | 18.5590 | 27.0802 | 925.0897 | $\begin{gathered} 50761.295 \\ 0 \end{gathered}$ | 35.9435 | 12.8381 | 29.344 |
|  | 53.9682 | 73.0307 | $\begin{gathered} 25051.581 \\ 0 \end{gathered}$ | 18.5590 | 27.0802 | 925.0897 | $\begin{gathered} 50761.295 \\ 0 \end{gathered}$ | 35.9435 | 12.8381 | 29.344 |
| L38 | 54.0303 | 73.1153 | $\begin{gathered} 25138.705 \\ 7 \end{gathered}$ | 18.5805 | 27.1113 | 927.2423 | $\begin{gathered} 50937.833 \\ 3 \end{gathered}$ | 35.9851 | 12.8542 | 29.381 |
|  | 54.0303 | 73.1153 | $\begin{gathered} 25138.705 \\ 7 \end{gathered}$ | 18.5805 | 27.1113 | 927.2423 | $\begin{gathered} 50937.833 \\ 3 \end{gathered}$ | 35.9851 | 12.8542 | 29.381 |
| L39 | 54.1546 | 73.2844 | $\begin{gathered} 25313.557 \\ 8 \end{gathered}$ | 18.6235 | 27.1734 | 931.5550 | $\begin{gathered} 51292.130 \\ 9 \end{gathered}$ | 36.0684 | 12.8863 | 29.455 |
|  | 54.1546 | 73.2844 | $\begin{gathered} 25313.557 \\ 8 \end{gathered}$ | 18.6235 | 27.1734 | 931.5550 | $\begin{gathered} 51292.130 \\ 9 \end{gathered}$ | 36.0684 | 12.8863 | 29.455 |
| L40 | 54.2167 | 73.3690 | $\begin{gathered} 25401.288 \\ 5 \end{gathered}$ | 18.6450 | 27.2045 | 933.7151 | $\begin{gathered} 51469.897 \\ 0 \end{gathered}$ | 36.1100 | 12.9024 | 29.491 |
|  | 54.2167 | 73.3690 | $\begin{gathered} 25401.288 \\ 5 \end{gathered}$ | 18.6450 | 27.2045 | 933.7151 | $\begin{gathered} 51469.897 \\ 0 \end{gathered}$ | 36.1100 | 12.9024 | 29.491 |
| L41 | 55.4596 | 75.0603 | $\begin{gathered} 27198.709 \\ 8 \end{gathered}$ | 19.0748 | 27.8264 | 977.4418 | $\begin{gathered} 55111.959 \\ 9 \end{gathered}$ | 36.9424 | 13.2242 | 30.227 |
|  | 55.4596 | 75.0603 | $\begin{gathered} 27198.709 \\ 8 \end{gathered}$ | 19.0748 | 27.8264 | 977.4418 | $\begin{gathered} 55111.959 \\ 9 \end{gathered}$ | 36.9424 | 13.2242 | 30.227 |
| L42 | 56.7025 | 76.7515 | $\begin{gathered} 29078.983 \\ 4 \end{gathered}$ | 19.5046 | 28.4483 | 1022.1693 | $\begin{gathered} 58921.904 \\ 1 \end{gathered}$ | 37.7748 | 13.5459 | 30.962 |
|  | 56.7025 | 76.7515 | $\begin{gathered} 29078.983 \\ 4 \end{gathered}$ | 19.5046 | 28.4483 | 1022.1693 | $\begin{gathered} 58921.904 \\ 1 \end{gathered}$ | 37.7748 | 13.5459 | 30.962 |
|  | 57.8211 | 78.2737 | $\begin{gathered} 30843.610 \\ 8 \end{gathered}$ | 19.8914 | 29.0080 | 1063.2795 | $\begin{gathered} 62497.517 \\ 6 \end{gathered}$ | 38.5239 | 13.8355 | 31.624 |


| Tower Elevation $f t$ | Gusset Area (per face) $f t^{2}$ | Gusset Thickness in | Gusset GradeAdjust. Factor $A_{f}$ | Adjust. Factor $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle <br> Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { L1 160.00- } \\ 155.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L2 } 155.00- \\ 150.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L3 } 150.00- \\ 145.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L4 145.00- } \\ 140.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L5 140.00- } \\ 135.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L6 } 135.00- \\ 130.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L7 130.00- } \\ 125.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L8 } 125.00- \\ 120.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L9 120.00- } \\ 111.33 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L10 111.33- } \\ 111.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L11 111.00- } \\ 106.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L12 106.00- } \\ 101.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L13 101.00- } \\ 96.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L14 96.00- } \\ 91.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L15 } 91.00- \\ 86.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L16 86.00- } \\ 85.75 \end{gathered}$ |  |  | 1 | 1 | 0.973888 |  |  |  |
| $\begin{gathered} \text { L17 85.75- } \\ 81.00 \end{gathered}$ |  |  | 1 | 1 | 0.976445 |  |  |  |

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160 Ft Monopole Tower Structural Analysis

| Tower Elevation <br> ft | Gusset Area (per face) $f t^{2}$ | Gusset Thickness in | Gusset Grade Adjust. Factor $A_{f}$ | Adjust. Factor $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle <br> Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { L18 81.00- } \\ 80.75 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L19 80.75- } \\ 80.50 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L20 80.50- } \\ 73.25 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L21 73.25- } \\ 72.25 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L22 72.25- } \\ 67.25 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L23 67.25- } \\ 62.25 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L24 } 62.25- \\ 57.25 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L25 57.25- } \\ 52.25 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L26 52.25- } \\ 49.83 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L27 } 49.83- \\ 49.58 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L28 } 49.58- \\ 44.58 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L29 44.58- } \\ 36.33 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L30 } 36.33- \\ 35.33 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L31 35.33- } \\ 32.25 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L32 32.25- } \\ 32.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L33 32.00- } \\ 27.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L34 } 27.00- \\ 22.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L35 22.00- } \\ 17.00 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L36 17.00- } \\ 15.50 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L37 15.50- } \\ 15.25 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L38 15.25- } \\ 14.75 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L39 14.75- } \\ 14.50 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| $\begin{gathered} \text { L40 14.50- } \\ 9.50 \end{gathered}$ |  |  | 1 | 1 | 1 |  |  |  |
| L41 9.50-4.50 |  |  | 1 | 1 | 1 |  |  |  |
| L42 4.50-0.00 |  |  | 1 | 1 | 1 |  |  |  |

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Sector | Exclude <br> From <br> Torque | Componen <br> Calculation | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

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| Description | Sector | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number | Number Per Row | Start/En $d$ Position | Width or Diamete $r$ in | Perimete <br> $r$ <br> in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | (CaAa) | 1.75 |  |  | 0.000 |  |  |  |
| MK SR 2 | A | No | Surface Af (CaAa) | $\begin{gathered} 82.00- \\ 77.00 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.0000 | 9.5000 | 10.21 |
| MK SR 2 | B | No | Surface Af (CaAa) | $\begin{gathered} 82.00- \\ 77.00 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.0000 | 9.5000 | 10.21 |
| MK SR 2 | C | No | Surface Af (CaAa) | $\begin{gathered} 82.00- \\ 77.00 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.0000 | 9.5000 | 10.21 |
| CCI-AFP-060100 | A | No | Surface Af (CaAa) | $\begin{gathered} 32.25- \\ 12.25 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 6.0000 | 14.0000 | 20.42 |
| CCI-AFP-060100 | B | No | Surface Af (CaAa) | $\begin{gathered} 32.25- \\ 12.25 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 6.0000 | 14.0000 | 20.42 |
| CCI-AFP-060100 | C | No | Surface Af (CaAa) | $\begin{gathered} 32.25- \\ 12.25 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 6.0000 | 14.0000 | 20.42 |
| CCI-AFP-060100 | A | No | Surface Af (CaAa) | $\begin{gathered} 52.33 \\ 32.33 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 6.0000 | 14.0000 | 20.42 |
| CCI-AFP-060100 | B | No | Surface Af (CaAa) | $\begin{gathered} 52.33- \\ 32.33 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 6.0000 | 14.0000 | 20.42 |
| CCI-AFP-060100 | C | No | Surface Af (CaAa) | $\begin{gathered} 52.33- \\ 32.33 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 6.0000 | 14.0000 | 20.42 |
| CCI-AFP-060100 | A | No | Surface Af (CaAa) | $\begin{gathered} 88.50- \\ 78.50 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 6.0000 | 14.0000 | 0.00 |
| CCI-AFP-060100 | B | No | Surface Af (CaAa) | $\begin{gathered} 88.50- \\ 78.50 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 6.0000 | 14.0000 | 0.00 |
| CCI-AFP-060100 | C | No | Surface Af (CaAa) | $\begin{gathered} 88.50- \\ 78.50 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 6.0000 | 14.0000 | 0.00 |

## Feed Line/Linear Appurtenances - Entered As Area

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude From <br> Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement <br> ft | Total Number |  | $C_{A} A_{A}$ <br> $f t^{2} f t$ | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| *** |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { 004U8X- } \\ 32125 \mathrm{E} 2 \mathrm{G}(1 / 8) \end{gathered}$ | C | No | No | Inside Pole | 157.00-0.00 | 1 | No Ice | 0.00 | 0.01 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.01 |
|  |  |  |  |  |  |  | 1 " Ice | 0.00 | 0.01 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.01 |
| 7919A(17/64) | C | No | No | Inside Pole | 157.00-0.00 | 4 | No Ice | 0.00 | 0.03 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.03 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.03 |
|  |  |  |  |  |  |  | 2 " Ice | 0.00 | 0.03 |
| LDF4-50A(1/2) | C | No | No | Inside Pole | 157.00-0.00 | 1 | No Ice | 0.00 | 0.15 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.15 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.15 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.15 |
| $\begin{aligned} & \text { HB058-M12- } \\ & \text { XXXF(5/8) } \end{aligned}$ | C | No | No | Inside Pole | 157.00-0.00 | 1 | No Ice | 0.00 | 0.24 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.24 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.24 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.24 |
| $\begin{gathered} \text { TYPE SOOW } \\ \text { 12/9(7/8) } \end{gathered}$ | C | No | No | Inside Pole | 157.00-0.00 | 1 | No Ice | 0.00 | 0.51 |
|  |  |  |  |  |  |  | $1 / 2 \text { " Ice }$ | 0.00 | 0.51 |
|  |  |  |  |  |  |  | 1 ' Ice | 0.00 | 0.51 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.51 |
| $\begin{gathered} \text { HB114-1-0813U4- } \\ \text { M5J(1-1/4) } \end{gathered}$ | C | No | No | Inside Pole | 157.00-0.00 | 3 | No Ice | 0.00 | 1.20 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 1.20 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 1.20 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 1.20 |
| *** |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \text { FB-L98B-002- } \\ & 75000(3 / 8) \end{aligned}$ | C | No | No | Inside Pole | 149.00-0.00 | 1 | No Ice | 0.00 | 0.06 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.06 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.06 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.06 |
| WR-VG82STBRDA(5/8) | C | No | No | Inside Pole | 149.00-0.00 | 2 | No Ice | 0.00 | 0.31 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.31 |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement <br> ft | Total Number |  | $C_{A} A_{A}$ $f t^{2} / f t$ | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { FB-L98B-002- } \\ & 75000(3 / 8) \end{aligned}$ | C | No | No | Inside Pole | 149.00-0.00 | 1 | 1" Ice | 0.00 | 0.31 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.31 |
|  |  |  |  |  |  |  | No Ice | 0.00 | 0.06 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.06 |
|  |  |  |  |  |  |  | 1 " Ice | 0.00 | 0.06 |
|  | C | No |  |  |  |  | 2" Ice | 0.00 | 0.06 |
| WR-VG82STBRDA(5/8) |  |  | No | Inside Pole | 149.00-0.00 | 2 | No Ice | 0.00 | 0.31 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.31 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.31 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.31 |
| 2" innerduct conduit | C | No | No | Inside Pole | 149.00-0.00 | 1 | No Ice | 0.00 | 0.20 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.20 |
|  |  |  |  |  |  |  | 1 " Ice | 0.00 | 0.20 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.20 |
| LCF158-50JA-A0(1-5/8) | C | No | No | Inside Pole | 149.00-0.00 | 12 | No Ice | 0.00 | 0.80 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.80 |
|  |  |  |  |  |  |  | 1 " Ice | 0.00 | 0.80 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.80 |
| *** |  |  |  |  |  |  |  |  |  |
| 561(1-5/8) | C | No | No | Inside Pole | 139.00-0.00 | 12 | No Ice | 0.00 | 1.35 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 1.35 |
|  |  |  |  |  |  |  | 1 " Ice | 0.00 | 1.35 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 1.35 |
| $\begin{aligned} & \text { HB158-1-08U8- } \\ & \text { S8J18(1-5/8) } \end{aligned}$ | C | No | No | Inside Pole | 139.00-0.00 | 1 | No Ice | 0.00 | 1.30 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 1.30 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 1.30 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 1.30 |
| *** |  |  |  |  |  |  |  |  |  |
| LDF7-50A(1-5/8) | C | No | No | Inside Pole | 116.00-0.00 | 6 |  | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 1 " Ice | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.82 |
| MLE Hybrid 9Power/18Fiber RL 2(1-5/8) | C | No | No | Inside Pole | 116.00-0.00 | 1 | No Ice | 0.00 | 1.07 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 1.07 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 1.07 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 1.07 |
| $\begin{gathered} \text { HCS } 6 \times 12 \\ \text { 4AWG(1-5/8) } \end{gathered}$ | C | No | No | Inside Pole | 116.00-0.00 | 3 | No Ice | 0.00 | 2.40 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 2.40 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 2.40 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 2.40 |
| *** |  |  |  |  |  |  |  |  |  |

Feed Line/Linear Appurtenances Section Areas

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
n
\end{tabular} \& Tower Elevation ft \& Face \& \(A_{R}\)

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
f t^{2} \\
\hline
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$
\] \& Weight

K <br>
\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{160.00-155.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{155.00-150.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{150.00-145.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.07 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{145.00-140.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.08 <br>
\hline \multirow[t]{3}{*}{L5} \& \multirow[t]{3}{*}{140.00-135.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.15 <br>
\hline
\end{tabular}

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160 Ft Monopole Tower Structural Analysis

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Tower Sectio $n$ \& Tower Elevation ft \& Face \& $A_{R}$

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
f t^{2} \\
\hline
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$
\] \& Weight

K <br>
\hline \multirow[t]{3}{*}{L6} \& \multirow[t]{3}{*}{135.00-130.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.17 <br>
\hline \multirow[t]{3}{*}{L7} \& \multirow[t]{3}{*}{130.00-125.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.17 <br>
\hline \multirow[t]{3}{*}{L8} \& \multirow[t]{3}{*}{125.00-120.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.17 <br>
\hline \multirow[t]{3}{*}{L9} \& \multirow[t]{3}{*}{120.00-111.33} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.325 \& 0.000 \& 0.35 <br>
\hline \multirow[t]{3}{*}{L10} \& \multirow[t]{3}{*}{111.33-111.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.012 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L11} \& \multirow[t]{3}{*}{111.00-106.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.23 <br>
\hline \multirow[t]{3}{*}{L12} \& \multirow[t]{3}{*}{106.00-101.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.23 <br>
\hline \multirow[t]{3}{*}{L13} \& \multirow[t]{3}{*}{101.00-96.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.23 <br>
\hline \multirow[t]{3}{*}{L14} \& \multirow[t]{3}{*}{96.00-91.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.23 <br>
\hline \multirow[t]{3}{*}{L15} \& \multirow[t]{3}{*}{91.00-86.00} \& A \& 0.000 \& 0.000 \& 2.280 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.280 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 2.468 \& 0.000 \& 0.23 <br>
\hline \multirow[t]{3}{*}{L16} \& \multirow[t]{3}{*}{86.00-85.75} \& A \& 0.000 \& 0.000 \& 0.228 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.228 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.237 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L17} \& \multirow[t]{3}{*}{85.75-81.00} \& A \& 0.000 \& 0.000 \& 4.885 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.885 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 5.063 \& 0.000 \& 0.23 <br>
\hline \multirow[t]{3}{*}{L18} \& \multirow[t]{3}{*}{81.00-80.75} \& A \& 0.000 \& 0.000 \& 0.366 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.366 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.376 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L19} \& \multirow[t]{3}{*}{80.75-80.50} \& A \& 0.000 \& 0.000 \& 0.366 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.366 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.376 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L20} \& \multirow[t]{3}{*}{80.50-73.25} \& A \& 0.000 \& 0.000 \& 3.759 \& 0.000 \& 0.04 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 3.759 \& 0.000 \& 0.04 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 4.031 \& 0.000 \& 0.37 <br>
\hline \multirow[t]{3}{*}{L21} \& \multirow[t]{3}{*}{73.25-72.25} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.037 \& 0.000 \& 0.05 <br>
\hline \multirow[t]{3}{*}{L22} \& \multirow[t]{3}{*}{72.25-67.25} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.23 <br>
\hline \multirow[t]{3}{*}{L23} \& \multirow[t]{3}{*}{67.25-62.25} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.23 <br>
\hline \multirow[t]{3}{*}{L24} \& \multirow[t]{3}{*}{62.25-57.25} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.23 <br>
\hline \multirow[t]{3}{*}{L25} \& \multirow[t]{3}{*}{57.25-52.25} \& A \& 0.000 \& 0.000 \& 0.080 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.080 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.268 \& 0.000 \& 0.24 <br>
\hline \multirow[t]{3}{*}{L26} \& \multirow[t]{3}{*}{52.25-49.83} \& A \& 0.000 \& 0.000 \& 2.420 \& 0.000 \& 0.05 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.420 \& 0.000 \& 0.05 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 2.511 \& 0.000 \& 0.16 <br>
\hline \multirow[t]{3}{*}{L27} \& \multirow[t]{3}{*}{49.83-49.58} \& A \& 0.000 \& 0.000 \& 0.250 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.250 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.259 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L28} \& \multirow[t]{3}{*}{49.58-44.58} \& A \& 0.000 \& 0.000 \& 5.000 \& 0.000 \& 0.10 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 5.000 \& 0.000 \& 0.10 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 5.188 \& 0.000 \& 0.34 <br>
\hline
\end{tabular}

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160 Ft Monopole Tower Structural Analysis

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
n
\end{tabular} \& Tower Elevation ft \& Face \& \(A_{R}\)

$f t^{2}$ \& AF

$\mathrm{ft}^{2}$ \& $C_{A} A_{A}$ In Face ft ${ }^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
f t^{2} \\
\hline
\end{gathered}
$$ \& Weight

K <br>
\hline \multirow[t]{3}{*}{L29} \& \multirow[t]{3}{*}{44.58-36.33} \& A \& 0.000 \& 0.000 \& 8.247 \& 0.000 \& 0.17 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 8.247 \& 0.000 \& 0.17 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 8.556 \& 0.000 \& 0.55 <br>
\hline \multirow[t]{3}{*}{L30} \& \multirow[t]{3}{*}{36.33-35.33} \& A \& 0.000 \& 0.000 \& 1.000 \& 0.000 \& 0.02 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.000 \& 0.000 \& 0.02 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 1.038 \& 0.000 \& 0.07 <br>
\hline \multirow[t]{3}{*}{L31} \& \multirow[t]{3}{*}{35.33-32.25} \& A \& 0.000 \& 0.000 \& 3.003 \& 0.000 \& 0.06 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 3.003 \& 0.000 \& 0.06 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 3.119 \& 0.000 \& 0.21 <br>
\hline \multirow[t]{3}{*}{L32} \& \multirow[t]{3}{*}{32.25-32.00} \& A \& 0.000 \& 0.000 \& 0.250 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.250 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.259 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L33} \& \multirow[t]{3}{*}{$32.00-27.00$} \& A \& 0.000 \& 0.000 \& 5.000 \& 0.000 \& 0.10 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 5.000 \& 0.000 \& 0.10 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 5.188 \& 0.000 \& 0.34 <br>
\hline \multirow[t]{3}{*}{L34} \& \multirow[t]{3}{*}{27.00-22.00} \& A \& 0.000 \& 0.000 \& 5.000 \& 0.000 \& 0.10 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 5.000 \& 0.000 \& 0.10 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 5.188 \& 0.000 \& 0.34 <br>
\hline \multirow[t]{3}{*}{L35} \& \multirow[t]{3}{*}{22.00-17.00} \& A \& 0.000 \& 0.000 \& 5.000 \& 0.000 \& 0.10 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 5.000 \& 0.000 \& 0.10 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 5.188 \& 0.000 \& 0.34 <br>
\hline \multirow[t]{3}{*}{L36} \& \multirow[t]{3}{*}{17.00-15.50} \& A \& 0.000 \& 0.000 \& 2.333 \& 0.000 \& 0.04 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.333 \& 0.000 \& 0.04 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 2.390 \& 0.000 \& 0.11 <br>
\hline \multirow[t]{3}{*}{L37} \& \multirow[t]{3}{*}{15.50-15.25} \& A \& 0.000 \& 0.000 \& 0.417 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.417 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.426 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L38} \& \multirow[t]{3}{*}{15.25-14.75} \& A \& 0.000 \& 0.000 \& 0.833 \& 0.000 \& 0.02 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.833 \& 0.000 \& 0.02 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.852 \& 0.000 \& 0.04 <br>
\hline \multirow[t]{3}{*}{L39} \& \multirow[t]{3}{*}{14.75-14.50} \& A \& 0.000 \& 0.000 \& 0.417 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.417 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.426 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L40} \& \multirow[t]{3}{*}{14.50-9.50} \& A \& 0.000 \& 0.000 \& 5.583 \& 0.000 \& 0.10 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 5.583 \& 0.000 \& 0.10 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 5.752 \& 0.000 \& 0.33 <br>
\hline \multirow[t]{3}{*}{L41} \& \multirow[t]{3}{*}{9.50-4.50} \& A \& 0.000 \& 0.000 \& 3.333 \& 0.000 \& 0.05 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 3.333 \& 0.000 \& 0.05 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 3.333 \& 0.000 \& 0.28 <br>
\hline \multirow[t]{3}{*}{L42} \& \multirow[t]{3}{*}{4.50-0.00} \& A \& 0.000 \& 0.000 \& 1.833 \& 0.000 \& 0.03 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.833 \& 0.000 \& 0.03 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 1.833 \& 0.000 \& 0.24 <br>
\hline
\end{tabular}

Feed Line/Linear Appurtenances Section Areas - With Ice

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
\(n\)
\end{tabular} \& Tower Elevation ft \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Ice Thickness in \& AR

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$ \& Weight

K <br>
\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{160.00-155.00} \& A \& \multirow[t]{3}{*}{1.491} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.678 \& 0.000 \& 0.03 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{155.00-150.00} \& A \& \multirow[t]{3}{*}{1.486} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.673 \& 0.000 \& 0.04 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{150.00-145.00} \& A \& \multirow[t]{3}{*}{1.481} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.668 \& 0.000 \& 0.09 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{145.00-140.00} \& A \& \multirow[t]{3}{*}{1.476} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.663 \& 0.000 \& 0.10 <br>
\hline \multirow[t]{3}{*}{L5} \& \multirow[t]{3}{*}{140.00-135.00} \& A \& \multirow[t]{3}{*}{1.471} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.658 \& 0.000 \& 0.17 <br>
\hline \multirow[t]{3}{*}{L6} \& \multirow[t]{3}{*}{135.00-130.00} \& A \& \multirow[t]{3}{*}{1.465} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.653 \& 0.000 \& 0.18 <br>
\hline
\end{tabular}

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160 Ft Monopole Tower Structural Analysis
Project Number 400087, Order 479803, Revision 0

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Tower Sectio n \& Tower Elevation ft \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& lce
Thickness
in \& $A_{R}$

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
{f t^{2}}^{2} \\
\hline
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
\text { ft }^{2}
\end{gathered}
$$
\] \& Weight

$$
K
$$ <br>

\hline \multirow[t]{3}{*}{L7} \& \multirow[t]{3}{*}{130.00-125.00} \& A \& \multirow[t]{3}{*}{1.459} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.647 \& 0.000 \& 0.18 <br>
\hline \multirow[t]{3}{*}{L8} \& \multirow[t]{3}{*}{125.00-120.00} \& A \& \multirow[t]{3}{*}{1.454} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.641 \& 0.000 \& 0.18 <br>
\hline \multirow[t]{3}{*}{L9} \& \multirow[t]{3}{*}{120.00-111.33} \& A \& \multirow[t]{3}{*}{1.445} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 2.830 \& 0.000 \& 0.38 <br>
\hline \multirow[t]{3}{*}{L10} \& \multirow[t]{3}{*}{111.33-111.00} \& A \& \multirow[t]{3}{*}{1.440} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.109 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L11} \& \multirow[t]{3}{*}{111.00-106.00} \& A \& \multirow[t]{3}{*}{1.436} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.624 \& 0.000 \& 0.25 <br>
\hline \multirow[t]{3}{*}{L12} \& \multirow[t]{3}{*}{106.00-101.00} \& A \& \multirow[t]{3}{*}{1.429} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.617 \& 0.000 \& 0.25 <br>
\hline \multirow[t]{3}{*}{L13} \& \multirow[t]{3}{*}{101.00-96.00} \& A \& \multirow[t]{3}{*}{1.422} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.610 \& 0.000 \& 0.25 <br>
\hline \multirow[t]{3}{*}{L14} \& \multirow[t]{3}{*}{96.00-91.00} \& A \& \multirow[t]{3}{*}{1.415} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.602 \& 0.000 \& 0.25 <br>
\hline \multirow[t]{3}{*}{L15} \& \multirow[t]{3}{*}{91.00-86.00} \& A \& \multirow[t]{3}{*}{1.407} \& 0.000 \& 0.000 \& 2.654 \& 0.000 \& 0.03 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.654 \& 0.000 \& 0.03 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 4.249 \& 0.000 \& 0.28 <br>
\hline \multirow[t]{3}{*}{L16} \& \multirow[t]{3}{*}{86.00-85.75} \& A \& \multirow[t]{3}{*}{1.403} \& 0.000 \& 0.000 \& 0.265 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.265 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.345 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L17} \& \multirow[t]{3}{*}{85.75-81.00} \& A \& \multirow[t]{3}{*}{1.399} \& 0.000 \& 0.000 \& 5.741 \& 0.000 \& 0.07 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 5.741 \& 0.000 \& 0.07 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 7.248 \& 0.000 \& 0.30 <br>
\hline \multirow[t]{3}{*}{L18} \& \multirow[t]{3}{*}{81.00-80.75} \& A \& \multirow[t]{3}{*}{1.395} \& 0.000 \& 0.000 \& 0.441 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.441 \& 0.000 \& 0.01 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.520 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L19} \& \multirow[t]{3}{*}{80.75-80.50} \& A \& \multirow[t]{3}{*}{1.394} \& 0.000 \& 0.000 \& 0.441 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.441 \& 0.000 \& 0.01 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.520 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L20} \& \multirow[t]{3}{*}{80.50-73.25} \& A \& \multirow[t]{3}{*}{1.387} \& 0.000 \& 0.000 \& 4.573 \& 0.000 \& 0.08 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 4.573 \& 0.000 \& 0.08 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 6.857 \& 0.000 \& 0.44 <br>
\hline \multirow[t]{3}{*}{L21} \& \multirow[t]{3}{*}{73.25-72.25} \& A \& \multirow[t]{3}{*}{1.380} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.315 \& 0.000 \& 0.05 <br>
\hline \multirow[t]{3}{*}{L22} \& \multirow[t]{3}{*}{72.25-67.25} \& A \& \multirow[t]{3}{*}{1.374} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.562 \& 0.000 \& 0.25 <br>
\hline \multirow[t]{3}{*}{L23} \& \multirow[t]{3}{*}{67.25-62.25} \& A \& \multirow[t]{3}{*}{1.364} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.551 \& 0.000 \& 0.25 <br>
\hline \multirow[t]{3}{*}{L24} \& \multirow[t]{3}{*}{62.25-57.25} \& A \& \multirow[t]{3}{*}{1.353} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.540 \& 0.000 \& 0.25 <br>
\hline \multirow[t]{3}{*}{L25} \& \multirow[t]{3}{*}{57.25-52.25} \& A \& \multirow[t]{3}{*}{1.341} \& 0.000 \& 0.000 \& 0.101 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.101 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.630 \& 0.000 \& 0.25 <br>
\hline \multirow[t]{3}{*}{L26} \& \multirow[t]{3}{*}{52.25-49.83} \& A \& 1.332 \& 0.000 \& 0.000 \& 3.065 \& 0.000 \& 0.07 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 3.065 \& 0.000 \& 0.07 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.800 \& 0.000 \& 0.19 <br>
\hline \multirow[t]{3}{*}{L27} \& \multirow[t]{3}{*}{49.83-49.58} \& A \& 1.328 \& 0.000 \& 0.000 \& 0.316 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.316 \& 0.000 \& 0.01 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.392 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L28} \& \multirow[t]{3}{*}{49.58-44.58} \& A \& 1.321 \& 0.000 \& 0.000 \& 6.321 \& 0.000 \& 0.15 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 6.321 \& 0.000 \& 0.15 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 7.830 \& 0.000 \& 0.40 <br>
\hline \multirow[t]{3}{*}{L29} \& \multirow[t]{3}{*}{44.58-36.33} \& A \& 1.301 \& 0.000 \& 0.000 \& 10.393 \& 0.000 \& 0.25 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 10.393 \& 0.000 \& 0.25 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 12.848 \& 0.000 \& 0.65 <br>
\hline
\end{tabular}

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160 Ft Monopole Tower Structural Analysis
CCI BU No 806953
Project Number 400087, Order 479803, Revision 0

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Tower Sectio $n$ \& Tower Elevation ft \& Face or Leg \& $\qquad$ \& AR

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& \[
$$
\begin{gathered}
\mathrm{C}_{A} A_{A} \\
\text { In Face } \\
\mathrm{ft}^{2} \\
\hline
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
f t^{2} \\
\hline
\end{gathered}
$$
\] \& Weight

K <br>
\hline \multirow[t]{3}{*}{L30} \& \multirow[t]{3}{*}{36.33-35.33} \& A \& \multirow[t]{3}{*}{1.286} \& 0.000 \& 0.000 \& 1.260 \& 0.000 \& 0.03 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.260 \& 0.000 \& 0.03 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.558 \& 0.000 \& 0.08 <br>
\hline \multirow[t]{3}{*}{L31} \& \multirow[t]{3}{*}{35.33-32.25} \& A \& \multirow[t]{3}{*}{1.278} \& 0.000 \& 0.000 \& 3.771 \& 0.000 \& 0.09 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 3.771 \& 0.000 \& 0.09 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 4.675 \& 0.000 \& 0.24 <br>
\hline \multirow[t]{3}{*}{L32} \& \multirow[t]{3}{*}{32.25-32.00} \& A \& \multirow[t]{3}{*}{1.272} \& 0.000 \& 0.000 \& 0.314 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.314 \& 0.000 \& 0.01 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.387 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L33} \& \multirow[t]{3}{*}{$32.00-27.00$} \& A \& \multirow[t]{3}{*}{1.261} \& 0.000 \& 0.000 \& 6.261 \& 0.000 \& 0.15 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 6.261 \& 0.000 \& 0.15 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 7.709 \& 0.000 \& 0.39 <br>
\hline \multirow[t]{3}{*}{L34} \& \multirow[t]{3}{*}{27.00-22.00} \& A \& \multirow[t]{3}{*}{1.238} \& 0.000 \& 0.000 \& 6.238 \& 0.000 \& 0.15 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 6.238 \& 0.000 \& 0.15 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 7.663 \& 0.000 \& 0.39 <br>
\hline \multirow[t]{3}{*}{L35} \& \multirow[t]{3}{*}{22.00-17.00} \& A \& \multirow[t]{3}{*}{1.210} \& 0.000 \& 0.000 \& 6.210 \& 0.000 \& 0.15 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 6.210 \& 0.000 \& 0.15 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 7.607 \& 0.000 \& 0.39 <br>
\hline \multirow[t]{3}{*}{L36} \& \multirow[t]{3}{*}{17.00-15.50} \& A \& \multirow[t]{3}{*}{1.188} \& 0.000 \& 0.000 \& 2.987 \& 0.000 \& 0.06 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.987 \& 0.000 \& 0.06 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.399 \& 0.000 \& 0.14 <br>
\hline \multirow[t]{3}{*}{L37} \& \multirow[t]{3}{*}{15.50-15.25} \& A \& \multirow[t]{3}{*}{1.181} \& 0.000 \& 0.000 \& 0.535 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.535 \& 0.000 \& 0.01 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.603 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L38} \& \multirow[t]{3}{*}{15.25-14.75} \& A \& \multirow[t]{3}{*}{1.178} \& 0.000 \& 0.000 \& 1.069 \& 0.000 \& 0.02 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.069 \& 0.000 \& 0.02 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.206 \& 0.000 \& 0.05 <br>
\hline \multirow[t]{3}{*}{L39} \& \multirow[t]{3}{*}{14.75-14.50} \& A \& \multirow[t]{3}{*}{1.175} \& 0.000 \& 0.000 \& 0.534 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.534 \& 0.000 \& 0.01 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.602 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L40} \& \multirow[t]{3}{*}{14.50-9.50} \& A \& \multirow[t]{3}{*}{1.152} \& 0.000 \& 0.000 \& 7.254 \& 0.000 \& 0.15 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 7.254 \& 0.000 \& 0.15 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 8.460 \& 0.000 \& 0.39 <br>
\hline \multirow[t]{3}{*}{L41} \& \multirow[t]{3}{*}{$9.50-4.50$} \& A \& \multirow[t]{3}{*}{1.092} \& 0.000 \& 0.000 \& 4.425 \& 0.000 \& 0.08 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 4.425 \& 0.000 \& 0.08 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 4.425 \& 0.000 \& 0.31 <br>
\hline \multirow[t]{3}{*}{L42} \& \multirow[t]{3}{*}{4.50-0.00} \& A \& \multirow[t]{3}{*}{0.974} \& 0.000 \& 0.000 \& 2.369 \& 0.000 \& 0.04 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.369 \& 0.000 \& 0.04 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 2.369 \& 0.000 \& 0.25 <br>
\hline
\end{tabular}

Feed Line Center of Pressure

| Section | Elevation | $C P_{X}$ | $C P_{z}$ | $C P_{X}$ <br> lce | $C P_{z}$ <br> lce |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | in | in | in | in |
| L1 | $160.00-155.00$ | 0.1651 | 0.1584 | 0.9175 | 0.8799 |
| L2 | $155.00-150.00$ | 0.1651 | 0.1584 | 0.9265 | 0.8885 |
| L3 | $150.00-145.00$ | 0.1651 | 0.1584 | 0.9345 | 0.8961 |
| L4 | $145.00-140.00$ | 0.1651 | 0.1584 | 0.9414 | 0.9028 |
| L5 | $140.00-135.00$ | 0.1651 | 0.1584 | 0.9475 | 0.9086 |
| L6 | $135.00-130.00$ | 0.1651 | 0.1584 | 0.9528 | 0.9137 |
| L7 | $130.00-125.00$ | 0.1651 | 0.1584 | 0.9573 | 0.9180 |
| L8 | $125.00-120.00$ | 0.1651 | 0.1584 | 0.9612 | 0.9217 |
| L9 | $120.00-111.33$ | 0.1651 | 0.1584 | 0.9654 | 0.9258 |
| L10 | $111.33-111.00$ | 0.1653 | 0.1585 | 0.9690 | 0.9292 |
| L11 | $111.00-106.00$ | 0.1653 | 0.1585 | 0.9673 | 0.9276 |
| L12 | $106.00-101.00$ | 0.1653 | 0.1585 | 0.9691 | 0.9293 |
| L13 | $101.00-96.00$ | 0.1653 | 0.1585 | 0.9703 | 0.9304 |
| L14 | $96.00-91.00$ | 0.1653 | 0.1585 | 0.9709 | 0.9311 |
| L15 | $91.00-86.00$ | 0.1135 | 0.1088 | 0.7105 | 0.6813 |
| L16 | $86.00-85.75$ | 0.0872 | 0.0836 | 0.5641 | 0.5409 |
| L17 | $85.75-81.00$ | 0.0829 | 0.0795 | 0.5361 | 0.5141 |
| L18 | $81.00-80.75$ | 0.0617 | 0.0592 | 0.4443 | 0.4261 |
| L19 | $80.75-80.50$ | 0.0618 | 0.0593 | 0.4446 | 0.4264 |
| L20 | $80.50-73.25$ | 0.1115 | 0.1069 | 0.6878 | 0.6596 |

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| Section | Elevation | $C P_{x}$ | $C P_{z}$ | $C P_{x}$ <br> lce <br> in | $C P_{z}$ <br> lce <br> in |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | in | in | 0.9309 |  |
|  | L21 | $73.25-72.25$ | 0.1654 | 0.1586 | 0.9707 |
| L22 | $72.25-67.25$ | 0.1653 | 0.1586 | 0.9655 | 0.9259 |
| L23 | $67.25-62.25$ | 0.1653 | 0.1586 | 0.9632 | 0.9237 |
| L24 | $62.25-57.25$ | 0.1653 | 0.1585 | 0.9602 | 0.9208 |
| L25 | $57.25-52.25$ | 0.1632 | 0.1565 | 0.9452 | 0.9064 |
| L26 | $52.25-49.83$ | 0.0911 | 0.0873 | 0.5494 | 0.5269 |
| L27 | $49.83-49.58$ | 0.0913 | 0.0876 | 0.5503 | 0.5277 |
| L28 | $49.58-44.58$ | 0.0919 | 0.0881 | 0.5517 | 0.5291 |
| L29 | $44.58-36.33$ | 0.0933 | 0.0895 | 0.5544 | 0.5317 |
| L30 | $36.33-35.33$ | 0.0936 | 0.0897 | 0.5561 | 0.5333 |
| L31 | $35.33-32.25$ | 0.0950 | 0.0911 | 0.5573 | 0.5344 |
| L32 | $32.25-32.00$ | 0.0943 | 0.0904 | 0.5515 | 0.5288 |
| L33 | $32.00-27.00$ | 0.0948 | 0.0909 | 0.5512 | 0.5286 |
| L34 | $27.00-22.00$ | 0.0958 | 0.0919 | 0.5497 | 0.5271 |
| L35 | $22.00-17.00$ | 0.0967 | 0.0928 | 0.5461 | 0.5237 |
| L36 | $17.00-15.50$ | 0.0792 | 0.0760 | 0.4390 | 0.4210 |
| L37 | $15.50-15.25$ | 0.0766 | 0.0734 | 0.4222 | 0.4049 |
| L38 | $15.25-14.75$ | 0.0766 | 0.0735 | 0.4219 | 0.4045 |
| L39 | $14.75-14.50$ | 0.0767 | 0.0736 | 0.4215 | 0.4042 |
| L40 | $14.50-9.50$ | 0.0842 | 0.0808 | 0.4511 | 0.4326 |
| L41 | $9.50-4.50$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L42 | $4.50-0.00$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

## Shielding Factor Ka

| Tower Section | Feed Line <br> Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 1 | Safety Line 3/8 | $\begin{array}{r} 155.00- \\ 160.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 1 | Safety Line 3/8 | $\begin{array}{r} 150.00- \\ 155.00 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 1 | Safety Line 3/8 | $\begin{aligned} & 145.00- \\ & 150.00 \end{aligned}$ | 1.0000 | 1.0000 |
| L4 | 1 | Safety Line 3/8 | $\begin{array}{r} 140.00-0 \\ 145.00 \end{array}$ | 1.0000 | 1.0000 |
| L5 | 1 | Safety Line 3/8 | $\begin{array}{r} 135.00- \\ 140.00 \end{array}$ | 1.0000 | 1.0000 |
| L6 | 1 | Safety Line 3/8 | $\begin{array}{r} 130.00 \\ 135.00 \end{array}$ | 1.0000 | 1.0000 |
| L7 | 1 | Safety Line 3/8 | $\begin{array}{r} 125.00- \\ 130.00 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 1 | Safety Line 3/8 | $\begin{array}{r} 120.00- \\ 125.00 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 1 | Safety Line 3/8 | $\begin{array}{r} 111.33- \\ 120.00 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 1 | Safety Line 3/8 | $\begin{array}{r} 106.00- \\ 111.00 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 1 | Safety Line 3/8 | $\begin{array}{r} 101.00- \\ 106.00 \end{array}$ | 1.0000 | 1.0000 |
| L13 | 1 | Safety Line 3/8 | $\begin{aligned} & 96.00- \\ & 101.00 \end{aligned}$ | 1.0000 | 1.0000 |
| L14 | 1 | Safety Line 3/8 | $\begin{array}{r} 91.00- \\ 96.00 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 1 | Safety Line 3/8 | $\begin{array}{r} 86.00- \\ 91.00 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 40 | CCI-AFP-060100 | $\begin{array}{r} 86.00 \\ 88.50 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 41 | CCI-AFP-060100 | $\begin{array}{r} 80.00 \\ 86.00 \\ 88.50 \end{array}$ | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ <br> No lce | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L15 | 42 | CCI-AFP-060100 | $\begin{array}{r} 86.00- \\ 88.50 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 1 | Safety Line 3/8 | $\begin{array}{r} 85.75- \\ 86.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 40 | CCI-AFP-060100 | $\begin{array}{r} 85.75- \\ 86.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 41 | CCI-AFP-060100 | $\begin{array}{r} 85.75- \\ 86.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 42 | CCI-AFP-060100 | $85.75-$ 86.00 | 1.0000 | 1.0000 |
| L17 | 1 | Safety Line 3/8 | $\begin{array}{r} 81.00- \\ 85.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 31 | MK SR 2 | $81.00-$ 82.00 | 1.0000 | 1.0000 |
| L17 | 32 | MK SR 2 | $\begin{array}{r} 81.00- \\ 82.00 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 33 | MK SR 2 | $\begin{array}{r} 81.00- \\ 82.00 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 40 | CCI-AFP-060100 | $\begin{array}{r} 81.00- \\ 85.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 41 | CCI-AFP-060100 | $\begin{array}{r} 81.00- \\ 85.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 42 | CCI-AFP-060100 | $\begin{array}{r} 81.00- \\ 85.75 \end{array}$ | 1.0000 | 1.0000 |
| L18 | 1 | Safety Line 3/8 | $\begin{array}{r} 80.75- \\ 81.00 \end{array}$ | 1.0000 | 1.0000 |
| L18 | 31 | MK SR 2 | $80.75-$ 81.00 | 1.0000 | 1.0000 |
| L18 | 32 | MK SR 2 | $80.75-$ 81.00 | 1.0000 | 1.0000 |
| L18 | 33 | MK SR 2 | $80.75-$ 81.00 | 1.0000 | 1.0000 |
| L18 | 40 | CCI-AFP-060100 | $80.75-$ 81.00 | 1.0000 | 1.0000 |
| L18 | 41 | CCI-AFP-060100 | $80.75-$ 81.00 | 1.0000 | 1.0000 |
| L18 | 42 | CCI-AFP-060100 | $\begin{array}{r} 80.75- \\ 81.00 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 1 | Safety Line 3/8 | $\begin{array}{r} 80.50- \\ 80.75 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 31 | MK SR 2 | $\begin{array}{r} 80.50- \\ 80.75 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 32 | MK SR 2 | $\begin{array}{r} 80.50- \\ 80.75 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 33 | MK SR 2 | $\begin{array}{r} 80.50- \\ 80.75 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 40 | CCI-AFP-060100 | $\begin{array}{r} 80.50- \\ 80.75 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 41 | CCI-AFP-060100 | $\begin{array}{r} 80.50- \\ 80.75 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 42 | CCI-AFP-060100 | $\begin{array}{r} 80.50- \\ 80.75 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 1 | Safety Line 3/8 | $73.25-$ 80.50 | 1.0000 | 1.0000 |
| L20 | 31 | MK SR 2 | $77.00-$ 80.50 | 1.0000 | 1.0000 |
| L20 | 32 | MK SR 2 | $\begin{array}{r} 77.00- \\ 80.50 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 33 | MK SR 2 | 77.00 80.50 | 1.0000 | 1.0000 |
| L20 | 40 | CCI-AFP-060100 | $\begin{array}{r} 78.50- \\ 80.50 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 41 | CCI-AFP-060100 | $\begin{array}{r} 78.50- \\ 80.50 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 42 | CCI-AFP-060100 | $\begin{array}{r} 78.50- \\ 80.50 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 1 | Safety Line 3/8 | $\begin{array}{r} 67.25- \\ 72.25 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 1 | Safety Line 3/8 | $62.25-$ | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ <br> No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 67.25 |  |  |
| L24 | 1 | Safety Line 3/8 | $57.25-$ 62.25 | 1.0000 | 1.0000 |
| L25 | 1 | Safety Line 3/8 | $\begin{array}{r} 52.25- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 37 | CCI-AFP-060100 | $\begin{array}{r} 52.25- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 38 | CCI-AFP-060100 | $\begin{array}{r} 52.25- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 39 | CCI-AFP-060100 | $\begin{array}{r} 52.25- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 1 | Safety Line 3/8 | $\begin{array}{r} 49.83- \\ 52.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 37 | CCI-AFP-060100 | $\begin{array}{r} 49.83- \\ 52.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 38 | CCI-AFP-060100 | $\begin{array}{r} 49.83- \\ 52.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 39 | CCI-AFP-060100 | $\begin{array}{r} 49.83- \\ 52.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 1 | Safety Line 3/8 | $\begin{array}{r} 49.58- \\ 49.83 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 37 | CCI-AFP-060100 | $\begin{array}{r} 49.58- \\ 49.83 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 38 | CCI-AFP-060100 | $\begin{array}{r} 49.58- \\ 49.83 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 39 | CCI-AFP-060100 | $\begin{array}{r} 49.58- \\ 49.83 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 1 | Safety Line 3/8 | $\begin{array}{r} 44.58- \\ 49.58 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 37 | CCI-AFP-060100 | $\begin{array}{r} 44.58- \\ 49.58 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 38 | CCI-AFP-060100 | $\begin{array}{r} 44.58- \\ 49.58 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 39 | CCI-AFP-060100 | $\begin{array}{r} 44.58- \\ 49.58 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 1 | Safety Line 3/8 | $\begin{array}{r} 36.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 37 | CCI-AFP-060100 | $\begin{array}{r} 36.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 38 | CCI-AFP-060100 | $\begin{array}{r} 36.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 39 | CCI-AFP-060100 | $\begin{array}{r} 36.33 \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 1 | Safety Line 3/8 | $\begin{array}{r} 32.25- \\ 35.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 37 | CCI-AFP-060100 | $\begin{array}{r} 32.33- \\ 35.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 38 | CCI-AFP-060100 | $\begin{array}{r} 32.33- \\ 35.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 39 | CCI-AFP-060100 | $\begin{array}{r} 32.33- \\ 35.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 1 | Safety Line 3/8 | $\begin{array}{r} 32.00- \\ 32.25 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 34 | CCI-AFP-060100 | $\begin{array}{r} 32.00- \\ 32.25 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 35 | CCI-AFP-060100 | $\begin{array}{r} 32.00- \\ 32.25 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 36 | CCI-AFP-060100 | $\begin{array}{r} 32.00- \\ 32.25 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 1 | Safety Line 3/8 | $27.00-$ 32.00 | 1.0000 | 1.0000 |
| L33 | 34 | CCI-AFP-060100 | $\begin{array}{r} 27.00- \\ 32.00 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 35 | CCI-AFP-060100 | $\begin{array}{r} 27.00- \\ 32.00 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 36 | CCI-AFP-060100 | $\begin{array}{r} 27.00-0 \\ 32.00 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 1 | Safety Line 3/8 | $\begin{array}{r} 22.00- \\ 27.00 \end{array}$ | 1.0000 | 1.0000 |

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| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L34 | 34 | CCI-AFP-060100 | $\begin{array}{r} 22.00 \\ 27.00 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 35 | CCI-AFP-060100 | $\begin{array}{r} 22.00- \\ 27.00 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 36 | CCI-AFP-060100 | $\begin{array}{r} 22.00- \\ 27.00 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 1 | Safety Line 3/8 | $\begin{array}{r} 17.00- \\ 22.00 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 34 | CCI-AFP-060100 | $\begin{array}{r} 17.00- \\ 22.00 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 35 | CCI-AFP-060100 | $\begin{array}{r} 17.00- \\ 22.00 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 36 | CCI-AFP-060100 | $\begin{array}{r} 17.00- \\ 22.00 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 1 | Safety Line 3/8 | $\begin{array}{r} 15.50- \\ 17.00 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 28 | MK SR 1 | $\begin{array}{r} 15.50- \\ 16.75 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 29 | MK SR 1 | $\begin{array}{r} 15.50- \\ 16.75 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 30 | MK SR 1 | $\begin{array}{r} 15.50- \\ 16.75 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 34 | CCI-AFP-060100 | $\begin{array}{r} 15.50- \\ 17.00 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 35 | CCI-AFP-060100 | $\begin{array}{r} 15.50- \\ 17.00 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 36 | CCI-AFP-060100 | $\begin{array}{r} 15.50- \\ 17.00 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 1 | Safety Line 3/8 | $\begin{array}{r} 15.25- \\ 15.50 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 28 | MK SR 1 | $\begin{array}{r} 15.25- \\ 15.50 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 29 | MK SR 1 | $\begin{array}{r} 15.25- \\ 15.50 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 30 | MK SR 1 | $15.25-$ 15.50 | 1.0000 | 1.0000 |
| L37 | 34 | CCI-AFP-060100 | $\begin{array}{r} 15.25- \\ 15.50 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 35 | CCI-AFP-060100 | $\begin{array}{r} 15.25- \\ 15.50 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 36 | CCI-AFP-060100 | $\begin{array}{r} 15.25- \\ 15.50 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 1 | Safety Line 3/8 | $\begin{array}{r} 14.75- \\ 15.25 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 28 | MK SR 1 | $\begin{array}{r} 14.75- \\ 15.25 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 29 | MK SR 1 | $\begin{array}{r} 14.75 \\ 15.25 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 30 | MK SR 1 | $\begin{array}{r} 14.75- \\ 15.25 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 34 | CCI-AFP-060100 | $\begin{array}{r} 14.75- \\ 15.25 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 35 | CCI-AFP-060100 | $\begin{array}{r} 14.75- \\ 15.25 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 36 | CCI-AFP-060100 | $\begin{array}{r} 14.75- \\ 15.25 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 1 | Safety Line 3/8 | $\begin{array}{r} 14.50- \\ 14.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 28 | MK SR 1 | $\begin{array}{r} 14.50- \\ 14.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 29 | MK SR 1 | $\begin{array}{r} 14.50- \\ 14.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 30 | MK SR 1 | $\begin{array}{r} 14.50- \\ 14.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 34 | CCI-AFP-060100 | $\begin{array}{r} 14.50- \\ 14.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 35 | CCI-AFP-060100 | $\begin{array}{r} 14.50- \\ 14.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 36 | CCI-AFP-060100 | 14.50-1 | 1.0000 | 1.0000 |

160 Ft Monopole Tower Structural Analysis

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No lce } \end{gathered}$ | $\begin{aligned} & \hline K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L40 | 1 | Safety Line 3/8 | $\begin{array}{r} 14.75 \\ 10.00- \\ 14.50 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 28 | MK SR 1 | 9.50-14.50 | 1.0000 | 1.0000 |
| L40 | 29 | MK SR 1 | 9.50-14.50 | 1.0000 | 1.0000 |
| L40 | 30 | MK SR 1 | 9.50-14.50 | 1.0000 | 1.0000 |
| L40 | 34 | CCI-AFP-060100 | $\begin{array}{r} 12.25 \\ 14.50 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 35 | CCI-AFP-060100 | $\begin{array}{r} 12.25 \\ 14.50 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 36 | CCI-AFP-060100 | $\begin{array}{r} 12.25- \\ 14.50 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 28 | MK SR 1 | 4.50-9.50 | 1.0000 | 1.0000 |
| L41 | 29 | MK SR 1 | 4.50-9.50 | 1.0000 | 1.0000 |
| L41 | 30 | MK SR 1 | 4.50-9.50 | 1.0000 | 1.0000 |
| L42 | 28 | MK SR 1 | 1.75-4.50 | 1.0000 | 1.0000 |
| $\llcorner 42$ | 29 | MK SR 1 | 1.75-4.50 | 1.0000 | 1.0000 |
| L42 | 30 | MK SR 1 | 1.75-4.50 | 1.0000 | 1.0000 |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen \(t\) \& Placement

ft \& \& \begin{tabular}{l}
$C_{A} A_{A}$ Front <br>
$f t^{2}$

 \& 

$C_{A} A_{A}$ Side <br>
$f t^{2}$
\end{tabular} \& Weight

K <br>
\hline \multirow[t]{4}{*}{Platform Mount [LP 713-1]} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{None} \& \multirow[t]{4}{*}{} \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{157.00} \& No Ice \& 31.27 \& 31.27 \& 1.51 <br>
\hline \& \& \& \& \& \& 1/2" \& 39.68 \& 39.68 \& 1.93 <br>
\hline \& \& \& \& \& \& Ice \& 48.09 \& 48.09 \& 2.35 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 64.91 \& 64.91 \& 3.19 <br>

\hline \multirow[t]{5}{*}{4'x2" Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{157.00} \& No lce \& 0.87 \& 0.87 \& 0.01 <br>
\hline \& \& \& 6.00 \& \& \& 1/2" \& 1.11 \& 1.11 \& 0.02 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& Ice \& 1.36 \& 1.36 \& 0.03 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.90 \& 1.90 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{4'x2" Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{157.00} \& No Ice \& 0.87 \& 0.87 \& 0.01 <br>
\hline \& \& \& -2.00 \& \& \& 1/2" \& 1.11 \& 1.11 \& 0.02 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& Ice \& 1.36 \& 1.36 \& 0.03 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.90 \& 1.90 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{4'x2" Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{157.00} \& No Ice \& 0.87 \& 0.87 \& 0.01 <br>
\hline \& \& \& -2.00 \& \& \& 1/2" \& 1.11 \& 1.11 \& 0.02 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& Ice \& 1.36 \& 1.36 \& 0.03 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.90 \& 1.90 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{4'x3"x3"x3/16" Horizontal Angle} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{157.00} \& No Ice \& 1.20 \& 0.07 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.49 \& 0.11 \& 0.03 <br>
\hline \& \& \& \multirow[t]{3}{*}{2.00} \& \& \& Ice \& 1.78 \& 0.16 \& 0.05 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.39 \& 0.27 \& 0.09 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{4'x3"x3"x3/16" Horizontal Angle} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Face} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{157.00} \& No Ice \& 1.20 \& 0.07 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.49 \& 0.11 \& 0.03 <br>
\hline \& \& \& \multirow[t]{3}{*}{2.00} \& \& \& Ice \& 1.78 \& 0.16 \& 0.05 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.39 \& 0.27 \& 0.09 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{4'x3"x3"x3/16" Horizontal Angle} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 3.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{157.00} \& No lce \& 1.20 \& 0.07 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.49 \& 0.11 \& 0.03 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 1.78 \& 0.16 \& 0.05 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.39 \& 0.27 \& 0.09 <br>
\hline
\end{tabular}

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: Horz Lateral Vert ft ft ft | Azimuth Adjustmen $t$ | Placement <br> ft |  | $C_{A} A_{A}$ Front <br> $f t^{2}$ | $C_{A} A_{A}$ Side <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| APXVTM14-ALU-I20 w/ Mount Pipe | A | From Leg | $\begin{gathered} 4.00 \\ -6.00 \\ 1.00 \end{gathered}$ | 0.0000 | 157.00 | 2" Ice <br> No Ice 1/2" Ice 1" Ice <br> 2" Ice | $\begin{aligned} & 4.09 \\ & 4.48 \\ & 4.88 \\ & 5.71 \end{aligned}$ | $\begin{aligned} & 2.86 \\ & 3.23 \\ & 3.61 \\ & 4.40 \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.13 \\ & 0.19 \\ & 0.33 \end{aligned}$ |
| APXVTM14-ALU-I20 w/ Mount Pipe | B | From Leg | $\begin{aligned} & 4.00 \\ & 6.00 \\ & 1.00 \end{aligned}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 4.09 \\ & 4.48 \\ & 4.88 \\ & 5.71 \end{aligned}$ | $\begin{aligned} & 2.86 \\ & 3.23 \\ & 3.61 \\ & 4.40 \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.13 \\ & 0.19 \\ & 0.33 \end{aligned}$ |
| APXVTM14-ALU-I20 w/ Mount Pipe | C | From Leg | $\begin{gathered} 4.00 \\ -6.00 \\ 1.00 \end{gathered}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 4.09 \\ & 4.48 \\ & 4.88 \\ & 5.71 \end{aligned}$ | $\begin{aligned} & 2.86 \\ & 3.23 \\ & 3.61 \\ & 4.40 \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.13 \\ & 0.19 \\ & 0.33 \end{aligned}$ |
| APXVSPP18-C-A20 w/ Mount Pipe | A | From Leg | $\begin{gathered} 4.00 \\ -2.00 \\ 1.00 \end{gathered}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 4.60 \\ & 5.05 \\ & 5.50 \\ & 6.44 \end{aligned}$ | $\begin{aligned} & 4.01 \\ & 4.45 \\ & 4.89 \\ & 5.82 \end{aligned}$ | $\begin{aligned} & 0.10 \\ & 0.16 \\ & 0.23 \\ & 0.42 \end{aligned}$ |
| APXVSPP18-C-A20 w/ Mount Pipe | B | From Leg | $\begin{aligned} & 4.00 \\ & 2.00 \\ & 1.00 \end{aligned}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 4.60 \\ & 5.05 \\ & 5.50 \\ & 6.44 \end{aligned}$ | $\begin{aligned} & 4.01 \\ & 4.45 \\ & 4.89 \\ & 5.82 \end{aligned}$ | $\begin{aligned} & 0.10 \\ & 0.16 \\ & 0.23 \\ & 0.42 \end{aligned}$ |
| APXVSPP18-C-A20 w/ Mount Pipe | C | From Leg | $\begin{aligned} & 4.00 \\ & 2.00 \\ & 1.00 \end{aligned}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 4.60 \\ & 5.05 \\ & 5.50 \\ & 6.44 \end{aligned}$ | $\begin{aligned} & 4.01 \\ & 4.45 \\ & 4.89 \\ & 5.82 \end{aligned}$ | $\begin{aligned} & 0.10 \\ & 0.16 \\ & 0.23 \\ & 0.42 \end{aligned}$ |
| LLPX310R-V1 w/ Mount Pipe | A | From Leg | $\begin{aligned} & 4.00 \\ & 2.00 \\ & 1.00 \end{aligned}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 4.54 \\ & 4.89 \\ & 5.25 \\ & 6.01 \end{aligned}$ | $\begin{aligned} & 2.98 \\ & 3.53 \\ & 4.09 \\ & 5.24 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.08 \\ & 0.13 \\ & 0.23 \end{aligned}$ |
| LLPX310R-V1 w/ Mount Pipe | B | From Leg | $\begin{gathered} 4.00 \\ -6.00 \\ 1.00 \end{gathered}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 4.54 \\ & 4.89 \\ & 5.25 \\ & 6.01 \end{aligned}$ | $\begin{aligned} & 2.98 \\ & 3.53 \\ & 4.09 \\ & 5.24 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.08 \\ & 0.13 \\ & 0.23 \end{aligned}$ |
| LLPX310R-V1 w/ Mount Pipe | C | From Leg | $\begin{aligned} & 4.00 \\ & 6.00 \\ & 1.00 \end{aligned}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 4.54 \\ & 4.89 \\ & 5.25 \\ & 6.01 \end{aligned}$ | $\begin{aligned} & 2.98 \\ & 3.53 \\ & 4.09 \\ & 5.24 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.08 \\ & 0.13 \\ & 0.23 \end{aligned}$ |
| (3) ACU-A20-N | A | From Leg | $\begin{aligned} & 4.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 0.07 \\ & 0.10 \\ & 0.15 \\ & 0.26 \end{aligned}$ | $\begin{aligned} & 0.12 \\ & 0.16 \\ & 0.21 \\ & 0.34 \end{aligned}$ | $\begin{aligned} & 0.00 \\ & 0.00 \\ & 0.00 \\ & 0.01 \end{aligned}$ |
| (3) ACU-A20-N | B | From Leg | $\begin{aligned} & 4.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 0.07 \\ & 0.10 \\ & 0.15 \\ & 0.26 \end{aligned}$ | $\begin{aligned} & 0.12 \\ & 0.16 \\ & 0.21 \\ & 0.34 \end{aligned}$ | $\begin{aligned} & 0.00 \\ & 0.00 \\ & 0.00 \\ & 0.01 \end{aligned}$ |
| (3) ACU-A20-N | C | From Leg | $\begin{aligned} & 4.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 157.00 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 0.07 \\ & 0.10 \\ & 0.15 \\ & 0.26 \end{aligned}$ | $\begin{aligned} & 0.12 \\ & 0.16 \\ & 0.21 \\ & 0.34 \end{aligned}$ | $\begin{aligned} & 0.00 \\ & 0.00 \\ & 0.00 \\ & 0.01 \end{aligned}$ |
| TD-RRH8x20-25 | A | From Leg | $\begin{aligned} & 4.00 \\ & 0.00 \\ & 1.00 \end{aligned}$ | 0.0000 | 157.00 | $\begin{gathered} \text { No Ice } \\ \text { 1/2" } \\ \text { Ice } \\ 1 " \text { Ice } \end{gathered}$ | $\begin{aligned} & 4.05 \\ & 4.30 \\ & 4.56 \\ & 5.10 \end{aligned}$ | $\begin{aligned} & 1.53 \\ & 1.71 \\ & 1.90 \\ & 2.30 \end{aligned}$ | $\begin{aligned} & 0.07 \\ & 0.10 \\ & 0.13 \\ & 0.20 \end{aligned}$ |

160 Ft Monopole Tower Structural Analysis



\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen \(t\) \& Placement

ft \& \& $C_{A} A_{A}$ Front

\[
f t^{2}

\] \& | $C_{A} A_{A}$ Side |
| :--- |
| $f t^{2}$ | \& Weight

K <br>
\hline \multirow{5}{*}{(2) LGP21401} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& 2.00 \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& Ice \& 6.61 \& 5.71 \& 0.16 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 7.49 \& 7.16 \& 0.29 <br>

\hline \& \& \& 4.00 \& \& \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.38 \& 0.54 \& 0.03 <br>

\hline \multirow{4}{*}{(2) LGP21401} \& \multirow{4}{*}{B} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{149.00} \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 1.69 \& 0.77 \& 0.05 <br>

\hline \& \& \& 4.00 \& \& \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.38 \& 0.54 \& 0.03 <br>
\hline \multirow{5}{*}{(2) LGP21401} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 1.69 \& 0.77 \& 0.05 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.38 \& 0.54 \& 0.03 <br>
\hline \multirow{5}{*}{RRUS 4478 B5} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 1.69 \& 0.77 \& 0.05 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 1.84 \& 1.06 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.01 \& 1.20 \& 0.08 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 2.19 \& 1.34 \& 0.09 <br>
\hline \multirow{5}{*}{RRUS 4478 B5} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 2.57 \& 1.66 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 1.84 \& 1.06 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.01 \& 1.20 \& 0.08 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 2.19 \& 1.34 \& 0.09 <br>
\hline \multirow{5}{*}{RRUS 4478 B5} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 2.57 \& 1.66 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 1.84 \& 1.06 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.01 \& 1.20 \& 0.08 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 2.19 \& 1.34 \& 0.09 <br>
\hline \multirow{5}{*}{DC6-48-60-18-8F} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 2.57 \& 1.66 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 1.00 \& \& \& No Ice \& 0.92 \& 0.92 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.46 \& 1.46 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.64 \& 1.64 \& 0.06 <br>
\hline \multirow{5}{*}{DC6-48-60-18-8F} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 2.04 \& 2.04 \& 0.11 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 1.00 \& \& \& No Ice \& 0.92 \& 0.92 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.46 \& 1.46 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.64 \& 1.64 \& 0.06 <br>
\hline \multirow{5}{*}{RRUS12/RRUS A2} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 2.04 \& 2.04 \& 0.11 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 3.14 \& 1.84 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.36 \& 2.01 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 3.59 \& 2.20 \& 0.13 <br>
\hline \multirow{7}{*}{RRUS12/RRUS A2} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 4.07 \& 2.59 \& 0.20 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 3.14 \& 1.84 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.36 \& 2.01 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 3.59 \& 2.20 \& 0.13 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 4.07 \& 2.59 \& 0.20 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{RRUS12/RRUS A2} \& \& \& 4.00 \& \& \& No Ice \& 3.14 \& 1.84 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.36 \& 2.01 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 3.59 \& 2.20 \& 0.13 <br>
\hline \& \multirow{6}{*}{A} \& \multirow{6}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 1" Ice \& 4.07 \& 2.59 \& 0.20 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{RRUS 11} \& \& \& 4.00 \& \& \& No Ice \& 2.78 \& 1.19 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.99 \& 1.33 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.21 \& 1.49 \& 0.10 <br>
\hline \& \& \& \& \& \& 1" Ice \& 3.66 \& 1.83 \& 0.15 <br>
\hline \& \multirow{3}{*}{B} \& \multirow{3}{*}{From Leg} \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{2}{*}{RRUS 11} \& \& \& 4.00 \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{149.00} \& No Ice \& 2.78 \& 1.19 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.99 \& 1.33 \& 0.07 <br>
\hline
\end{tabular}




\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& Offset Type \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen \(t\) \& \multicolumn{2}{|l|}{Placement} \& \(C_{A} A_{A}\) Front \& \begin{tabular}{l}
\[
C_{A} A_{A}
\] \\
Side
\end{tabular} \& Weight

K <br>
\hline \multirow{7}{*}{B66A RRH4X45} \& \multirow{7}{*}{C} \& \multirow{7}{*}{From Leg} \& 0.00 \& \multirow{7}{*}{0.0000} \& \multirow{7}{*}{139.00} \& 1/2" \& 2.79 \& 1.81 \& 0.08 <br>
\hline \& \& \& \multirow[t]{2}{*}{3.00} \& \& \& Ice \& 3.01 \& 2.00 \& 0.10 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 3.48 \& 2.40 \& 0.16 <br>

\hline \& \& \& 4.00 \& \& \& No Ice \& 2.58 \& 1.63 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.79 \& 1.81 \& 0.08 <br>
\hline \& \& \& \multirow[t]{3}{*}{3.00} \& \& \& Ice \& 3.01 \& 2.00 \& 0.10 <br>
\hline \& \& \& \& \& \& 1" Ice \& 3.48 \& 2.40 \& 0.16 <br>
\hline \multirow{5}{*}{B13 RRH 4X30} \& \multirow{6}{*}{A} \& \& \& \& \& 2 ' Ice \& \& \& <br>
\hline \& \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{139.00} \& No Ice \& 2.06 \& 1.32 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.24 \& 1.48 \& 0.07 <br>
\hline \& \& \& \multirow[t]{3}{*}{3.00} \& \& \& Ice \& 2.43 \& 1.64 \& 0.09 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 2.84 \& 2.00 \& 0.14 <br>
\hline \multirow{6}{*}{B13 RRH 4X30} \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{139.00} \& No Ice \& 2.06 \& 1.32 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.24 \& 1.48 \& 0.07 <br>
\hline \& \& \& \multirow[t]{3}{*}{3.00} \& \& \& Ice \& 2.43 \& 1.64 \& 0.09 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 2.84 \& 2.00 \& 0.14 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{B13 RRH 4X30} \& \multirow[t]{6}{*}{C} \& \multirow[t]{6}{*}{From Leg} \& 4.00 \& \multirow[t]{6}{*}{0.0000} \& \multirow[t]{6}{*}{139.00} \& No Ice \& 2.06 \& 1.32 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.24 \& 1.48 \& 0.07 <br>
\hline \& \& \& \multirow[t]{4}{*}{3.00} \& \& \& Ice \& 2.43 \& 1.64 \& 0.09 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 2.84 \& 2.00 \& 0.14 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{5}{*}{Platform Mount [LP 712-1]} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{None} \& \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{118.00} \& No Ice \& 24.53 \& 24.53 \& 1.34 <br>
\hline \& \& \& \& \& \& 1/2" \& 29.94 \& 29.94 \& 1.65 <br>
\hline \& \& \& \& \& \& Ice \& 35.35 \& 35.35 \& 1.96 <br>
\hline \& \& \& \& \& \& 1" Ice \& 46.17 \& 46.17 \& 2.58 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{HRK 12 [NA 507-1]} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 0.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{118.00} \& No Ice \& 4.80 \& 4.80 \& 0.26 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 6.70 \& 6.70 \& 0.31 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& Ice \& 8.60 \& 8.60 \& 0.37 <br>
\hline \& \& \& \& \& \& 1" Ice \& 12.40 \& 12.40 \& 0.47 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{6'x2" Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{118.00} \& No Ice \& 1.43 \& 1.43 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.92 \& 1.92 \& 0.03 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& Ice \& 2.29 \& 2.29 \& 0.05 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 3.06 \& 3.06 \& 0.09 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{6'x2" Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{118.00} \& No Ice \& 1.43 \& 1.43 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.92 \& 1.92 \& 0.03 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& Ice \& 2.29 \& 2.29 \& 0.05 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 3.06 \& 3.06 \& 0.09 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{6'x2" Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{118.00} \& No Ice \& 1.43 \& 1.43 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.92 \& 1.92 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.29 \& 2.29 \& 0.05 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 3.06 \& 3.06 \& 0.09 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{APXVAARR24_43-U-NA20 w/ Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{118.00} \& No Ice \& 14.69 \& 6.87 \& 0.19 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" \& 15.46 \& 7.55 \& 0.31 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 16.23 \& 8.25 \& 0.46 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 17.82 \& 9.67 \& 0.79 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{APXVAARR24_43-U-NA20 w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{118.00} \& No Ice \& 14.69 \& 6.87 \& 0.19 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" \& 15.46 \& 7.55 \& 0.31 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 16.23 \& 8.25 \& 0.46 <br>
\hline \& \& \& \& \& \& 1" Ice \& 17.82 \& 9.67 \& 0.79 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{APXVAARR24_43-U-NA20 w/ Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{118.00} \& No Ice \& 14.69 \& 6.87 \& 0.19 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" \& 15.46 \& 7.55 \& 0.31 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& Ice \& 16.23 \& 8.25 \& 0.46 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 17.82 \& 9.67 \& 0.79 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen \(t\) \& Placement

ft \& \& $C_{A} A_{A}$ Front

\[
f t^{2}

\] \& | $C_{A} A_{A}$ Side |
| :--- |
| $f t^{2}$ | \& Weight

K <br>

\hline AIR 32 B2A/B66AA w/ Mount Pipe \& A \& From Leg \& $$
\begin{gathered}
4.00 \\
-2.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 118.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
\text { 1/2" } \\
\text { Ice } \\
1 " \text { Ice } \\
2 \text { 2" Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 6.75 \\
& 7.20 \\
& 7.65 \\
& 8.57
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.07 \\
& 6.87 \\
& 7.58 \\
& 9.06
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.15 \\
& 0.21 \\
& 0.28 \\
& 0.44
\end{aligned}
$$
\] <br>

\hline AIR 32 B2A/B66AA w/ Mount Pipe \& B \& From Leg \& \[
$$
\begin{gathered}
4.00 \\
-2.00 \\
0.00
\end{gathered}
$$

\] \& 0.0000 \& 118.00 \& | No Ice |
| :--- |
| 1/2" |
| Ice |
| 1" Ice |
| 2" Ice | \& \[

$$
\begin{aligned}
& 6.75 \\
& 7.20 \\
& 7.65 \\
& 8.57
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.07 \\
& 6.87 \\
& 7.58 \\
& 9.06
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.15 \\
& 0.21 \\
& 0.28 \\
& 0.44
\end{aligned}
$$
\] <br>

\hline AIR 32 B2A/B66AA w/ Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
4.00 \\
-2.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 6.75 \\
& 7.20 \\
& 7.65 \\
& 8.57
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.07 \\
& 6.87 \\
& 7.58 \\
& 9.06
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.15 \\
& 0.21 \\
& 0.28 \\
& 0.44
\end{aligned}
$$
\] <br>

\hline ERICSSON AIR 21 B2A B4P w/ Mount Pipe \& A \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 6.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 6.33 \\
& 6.78 \\
& 7.21 \\
& 8.12
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.64 \\
& 6.43 \\
& 7.13 \\
& 8.59
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.11 \\
& 0.17 \\
& 0.23 \\
& 0.38
\end{aligned}
$$
\] <br>

\hline ERICSSON AIR 21 B2A B4P w/ Mount Pipe \& B \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 6.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 6.33 \\
& 6.78 \\
& 7.21 \\
& 8.12
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.64 \\
& 6.43 \\
& 7.13 \\
& 8.59
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.11 \\
& 0.17 \\
& 0.23 \\
& 0.38
\end{aligned}
$$
\] <br>

\hline ERICSSON AIR 21 B2A B4P w/ Mount Pipe \& C \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 6.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 6.33 \\
& 6.78 \\
& 7.21 \\
& 8.12
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.64 \\
& 6.43 \\
& 7.13 \\
& 8.59
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.11 \\
& 0.17 \\
& 0.23 \\
& 0.38
\end{aligned}
$$
\] <br>

\hline RADIO 4449 B12/B71 \& A \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 1.65 \\
& 1.81 \\
& 1.98 \\
& 2.34
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.30 \\
& 1.44 \\
& 1.60 \\
& 1.92
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.09 \\
& 0.11 \\
& 0.16
\end{aligned}
$$
\] <br>

\hline RADIO 4449 B12/B71 \& B \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 1.65 \\
& 1.81 \\
& 1.98 \\
& 2.34
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.30 \\
& 1.44 \\
& 1.60 \\
& 1.92
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.09 \\
& 0.11 \\
& 0.16
\end{aligned}
$$
\] <br>

\hline RADIO 4449 B12/B71 \& C \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 1.65 \\
& 1.81 \\
& 1.98 \\
& 2.34
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.30 \\
& 1.44 \\
& 1.60 \\
& 1.92
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.09 \\
& 0.11 \\
& 0.16
\end{aligned}
$$
\] <br>

\hline KRY 112 144/1 \& A \& From Leg \& $$
\begin{array}{r}
4.00 \\
0.00 \\
-2.00
\end{array}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 0.35 \\
& 0.43 \\
& 0.51 \\
& 0.70
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.17 \\
& 0.23 \\
& 0.30 \\
& 0.46
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.01 \\
& 0.01 \\
& 0.02 \\
& 0.03
\end{aligned}
$$
\] <br>

\hline KRY 112 144/1 \& B \& From Leg \& $$
\begin{array}{r}
4.00 \\
0.00 \\
-2.00
\end{array}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 0.35 \\
& 0.43 \\
& 0.51 \\
& 0.70
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.17 \\
& 0.23 \\
& 0.30 \\
& 0.46
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.01 \\
& 0.01 \\
& 0.02 \\
& 0.03
\end{aligned}
$$
\] <br>

\hline KRY 112 144/1 \& C \& From Leg \& $$
\begin{gathered}
4.00 \\
0.00 \\
-2.00
\end{gathered}
$$ \& 0.0000 \& 118.00 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 0.35 \\
& 0.43 \\
& 0.51 \\
& 0.70
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.17 \\
& 0.23 \\
& 0.30 \\
& 0.46
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.01 \\
& 0.01 \\
& 0.02 \\
& 0.03
\end{aligned}
$$
\] <br>

\hline 3'x2" Horizontal Pipe \& C \& From Leg \& $$
\begin{aligned}
& 1.50 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 84.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
\text { 1/2" } \\
\text { Ice } \\
1 " \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.58 \\
& 0.77 \\
& 0.97 \\
& 1.42
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.01 \\
& 0.04 \\
& 0.07 \\
& 0.13
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.01 \\
& 0.02 \\
& 0.02 \\
& 0.05
\end{aligned}
$$
\] <br>

\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
ft \\
ft \\
ft
\end{tabular} \& Azimuth Adjustmen \(t\) \& Placement

ft \& \& $C_{A} A_{A}$ Front

\[
f t^{2}

\] \& | $C_{A} A_{A}$ Side |
| :--- |
| $f t^{2}$ | \& Weight <br>

\hline \multirow{6}{*}{GPS_A} \& \multirow{6}{*}{C} \& \multirow{6}{*}{From Leg} \& \& \multirow{6}{*}{0.0000} \& \multirow{6}{*}{84.00} \& 2" Ice \& \& \& <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 0.26 \& 0.26 \& 0.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.32 \& 0.32 \& 0.00 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& Ice \& 0.39 \& 0.39 \& 0.01 <br>
\hline \& \& \& \& \& \& 1" Ice \& 0.56 \& 0.56 \& 0.02 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multicolumn{10}{|l|}{***} <br>
\hline \multirow[t]{5}{*}{Pipe Mount [PM 601-1]} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 1.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{40.00} \& No Ice \& 3.00 \& 0.90 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.74 \& 1.12 \& 0.08 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& Ice \& 4.48 \& 1.34 \& 0.09 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 5.96 \& 1.78 \& 0.12 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{GPS-QBW-20N} \& \multirow[t]{6}{*}{A} \& \multirow[t]{6}{*}{From Leg} \& 1.00 \& \multirow[t]{6}{*}{0.0000} \& \multirow[t]{6}{*}{40.00} \& No Ice \& 0.13 \& 0.13 \& 0.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.18 \& 0.18 \& 0.00 <br>
\hline \& \& \& \multirow[t]{4}{*}{0.00} \& \& \& Ice \& 0.23 \& 0.23 \& 0.00 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.37 \& 0.37 \& 0.01 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>
\hline
\end{tabular}

## Load Combinations

| Comb. |  |
| :---: | :--- |
| No. |  |
| 1 | Dead Only |
| 2 | 1.2 Dead+1.0 Wind 0 deg - No Ice |
| 3 | 0.9 Dead+1.0 Wind 0 deg - No Ice |
| 4 | 1.2 Dead+1.0 Wind 30 deg - No Ice |
| 5 | 0.9 Dead+1.0 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.0 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.0 Wind 60 deg - No Ice |
| 8 | 1.2 Dead+1.0 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.0 Wind 90 deg - No Ice |
| 10 | 1.2 Dead+1.0 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.0 Wind 120 deg - No Ice |
| 12 | 1.2 Dead+1.0 Wind 150 deg - No Ice |
| 13 | 0.9 Dead+1.0 Wind 150 deg - No Ice |
| 14 | 1.2 Dead+1.0 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.0 Wind 180 deg - No Ice |
| 16 | 1.2 Dead+1.0 Wind 210 deg - No Ice |
| 17 | 0.9 Dead+1.0 Wind 210 deg - No Ice |
| 18 | 1.2 Dead+1.0 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.0 Wind 240 deg - No Ice |
| 20 | 1.2 Dead+1.0 Wind 270 deg - No Ice |
| 21 | 0.9 Dead+1.0 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.0 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.0 Wind 300 deg - No Ice |
| 24 | 1.2 Dead+1.0 Wind 330 deg - No Ice |
| 25 | 0.9 Dead+1.0 Wind 330 deg - No Ice |
| 26 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 27 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |
| 28 | 1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp |
| 29 | 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp |
| 30 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp |
| 32 | 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp |
| 33 | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp |
| 34 | 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp |
| 35 | 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp |
| 36 | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp |


| Comb. <br> No. | Description |
| :---: | :--- |
| 37 | 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp |
| 38 | 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp |
| 39 | Dead+Wind 0 deg - Service |
| 40 | Dead+Wind 30 deg - Service |
| 41 | Dead+Wind 60 deg - Service |
| 42 | Dead+Wind 90 deg - Service |
| 43 | Dead+Wind 120 deg - Service |
| 44 | Dead+Wind 150 deg - Service |
| 45 | Dead+Wind 180 deg - Service |
| 46 | Dead+Wind 210 deg - Service |
| 47 | Dead+Wind 240 deg - Service |
| 48 | Dead+Wind 270 deg - Service |
| 49 | Dead+Wind 300 deg - Service |
| 50 | Dead+Wind 330 deg - Service |

## Maximum Member Forces

| Sectio $n$ No. | Elevation ft | Component Type | Condition | Gov. Load Comb | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 160-155 | Pole | Max Tension | 8 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -7.23 | 2.25 | -0.76 |
|  |  |  | Max. Mx | 20 | -3.07 | 10.17 | -0.33 |
|  |  |  | Max. My | 14 | -3.07 | 0.69 | -9.72 |
|  |  |  | Max. Vy | 20 | -3.73 | 10.17 | -0.33 |
|  |  |  | Max. Vx | 14 | 3.74 | 0.69 | -9.72 |
|  |  |  | Max. Torque | 2 |  |  | 1.10 |
| L2 | 155-150 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -9.17 | 2.28 | -0.78 |
|  |  |  | Max. Mx | 20 | -4.00 | 32.62 | -0.34 |
|  |  |  | Max. My | 14 | -4.00 | 0.70 | -32.21 |
|  |  |  | Max. Vy | 20 | -4.82 | 32.62 | -0.34 |
|  |  |  | Max. Vx | 14 | 4.83 | 0.70 | -32.21 |
|  |  |  | Max. Torque | 2 |  |  | 1.10 |
| L3 | 150-145 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -18.21 | 2.17 | -0.74 |
|  |  |  | Max. Mx | 20 | -7.66 | 82.75 | -0.33 |
|  |  |  | Max. My | 14 | -7.66 | 0.69 | -82.40 |
|  |  |  | Max. Vy | 20 | -10.08 | 82.75 | -0.33 |
|  |  |  | Max. Vx | 14 | 10.09 | 0.69 | -82.40 |
|  |  |  | Max. Torque | 2 |  |  | 1.10 |
| L4 | 145-140 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -18.94 | 2.21 | -0.77 |
|  |  |  | Max. Mx | 20 | -8.12 | 134.21 | -0.34 |
|  |  |  | Max. My | 14 | -8.12 | 0.71 | -133.90 |
|  |  |  | Max. Vy | 20 | -10.50 | 134.21 | -0.34 |
|  |  |  | Max. Vx | 14 | 10.51 | 0.71 | -133.90 |
|  |  |  | Max. Torque | 2 |  |  | 1.05 |
| L5 | 140-135 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -27.89 | 3.01 | -1.25 |
|  |  |  | Max. Mx | 20 | -11.58 | 219.50 | -0.73 |
|  |  |  | Max. My | 14 | -11.58 | 1.20 | -218.84 |
|  |  |  | Max. Vy | 20 | -16.15 | 219.50 | -0.73 |
|  |  |  | Max. Vx | 14 | 16.12 | 1.20 | -218.84 |
|  |  |  | Max. Torque | 14 |  |  | -1.35 |
| L6 | 135-130 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -28.79 | 3.05 | -1.29 |
|  |  |  | Max. Mx | 20 | -12.22 | 301.31 | -0.94 |
|  |  |  | Max. My | 14 | -12.22 | 1.42 | -300.47 |
|  |  |  | Max. Vy | 20 | -16.58 | 301.31 | -0.94 |
|  |  |  | Max. Vx | 14 | 16.55 | 1.42 | -300.47 |
|  |  |  | Max. Torque | 14 |  |  | -1.35 |
| L7 | 130-125 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -29.71 | 3.10 | -1.33 |
|  |  |  | Max. Mx | 20 | -12.89 | 385.29 | -1.15 |
|  |  |  | Max. My | 14 | -12.89 | 1.64 | -384.27 |
|  |  |  | Max. Vy | 20 | -17.02 | 385.29 | -1.15 |

160 Ft Monopole Tower Structural Analysis
CCI BU No 806953
Project Number 400087, Order 479803, Revision 0

| Sectio $n$ $n$ No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L8 | 125-120 | Pole | Max. Vx | 14 | 16.98 | 1.64 | $\begin{gathered} -384.27 \\ -1.35 \end{gathered}$ |
|  |  |  | Max. Torque | 14 |  |  |  |
|  |  |  | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -30.67 | 3.13 | -1.37 |
|  |  |  | Max. Mx | 20 | -13.60 | 471.45 | -1.36 |
|  |  |  | Max. My | 14 | -13.60 | 1.86 | -470.26 |
|  |  |  | Max. Vy | 20 | -17.46 | 471.45 | -1.36 |
|  |  | Pole | Max. Vx | 14 | 17.43 | 1.86 | $\begin{gathered} -470.26 \\ -1.35 \end{gathered}$ |
|  |  |  | Max. Torque | 14 |  |  |  |
| L9 | $\begin{gathered} 120- \\ 111.333 \end{gathered}$ |  | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -39.25 | 3.66 | -1.69 |
|  |  |  | Max. Mx | 20 | -17.84 |  |  |
|  |  |  | Max. My | 14 | -17.84 | $2.35$ | $-548.37$ |
|  |  |  | Max. Vy | 20 | -21.60 | $549.85$ | $-1.71$ |
|  |  |  | Max. Vx | 14 | 21.57 | 2.35 | -548.37 |
|  |  |  | Max. Torque | 14 |  |  | -1.57 |
| L10 | $\begin{gathered} 111.333- \\ 111 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -41.21 | 3.70 | -1.73 |
|  |  |  | Max. Mx | 20 | -19.25 | 659.16 | -1.93 |
|  |  |  | Max. My | 14 | -19.25 | 2.57 | -657.51 |
|  |  |  | Max. Vy | 20 | -22.13 | 659.16 | -1.93 |
|  |  |  | Max. Vx | 14 | 22.10 | 2.57 | -657.51 |
|  |  |  | Max. Torque | $\begin{array}{cc}14 & \\ 1 & 0.00\end{array}$ |  |  | -1.57 |
| L11 | 111-106 | Pole | Max Tension |  |  |  | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -42.51 | 3.74 | -1.78 |
|  |  |  | Max. Mx | 20 | -20.28 | 770.95 | -2.14 |
|  |  |  | Max. My | 14 | -20.28 | 2.79 | -769.14 |
|  |  |  | Max. Vy | 20 | -22.60 | 770.95 | -2.14 |
|  |  |  | Max. Vx | 14 | 22.57 | 2.79 | -769.14 |
|  |  |  | Max. Torque | 14 |  |  | -1.57 |
| L12 | 106-101 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -43.84 | 3.78 | -1.82 |
|  |  |  | Max. Mx | 20 | -21.35 | 885.06 | -2.35 |
|  |  |  | Max. My | 14 | -21.35 | 3.01 | -883.08 |
|  |  |  | Max. Vy | 20 | -23.06 | 885.06 | -2.35 |
|  |  |  | Max. Vx | 14 | 23.03 | 3.01 | -883.08 |
|  |  |  | Max. Torque | 14 |  |  | -1.57 |
| L13 | 101-96 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -45.21 | 3.81 | -1.86 |
|  |  |  | Max. Mx | 20 | -22.45 | 1001.50 | -2.56 |
|  |  |  | Max. My | 14 | -22.45 | 3.23 | -999.35 |
|  |  |  | Max. Vy | 20 | -23.53 | 1001.50 | -2.56 |
|  |  |  | Max. Vx | 14 | 23.50 | 3.23 | $\begin{gathered} -999.35 \\ -1.57 \end{gathered}$ |
|  |  |  | Max. Torque | $\begin{array}{cc}14 & \\ 1 & 0.00\end{array}$ |  |  |  |
| L14 | 96-91 | Pole | Max Tension |  |  |  | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -46.61 | 3.84 | -1.90 |
|  |  |  | Max. Mx | 20 | -23.59 | 1120.27 | -2.78 |
|  |  |  | Max. My | 14 | -23.59 | 3.45 | -1117.96 |
|  |  |  | Max. Vy | 20 | -24.00 | 1120.27 | -2.78 |
|  |  |  | Max. Vx | 14 | 23.97 | 3.45 | -1117.96-1.57 |
|  |  |  | Max. Torque | 14 |  |  |  |
| L15 | 91-86 | Pole | Max Tension | 1 | 0.00 | 0.00 | -1.57 |
|  |  |  | Max. Compression | 26 | -48.13 | 3.86 | -1.94 |
|  |  |  | Max. Mx | 20 | -24.76 | 1241.38 | -2.99 |
|  |  |  | Max. My | 14 | -24.76 | 3.66 | -1238.91 |
|  |  |  | Max. Vy | 20 | -24.47 | 1241.38 | -2.99 |
|  |  |  | Max. Vx | 14 | 24.44 | 3.66 | -1238.91 |
|  |  |  | Max. Torque | $\begin{array}{cc}14 & \\ 1 & 0.00\end{array}$ |  |  | -1.57 |
| L16 | 86-85.75 | Pole | Max Tension |  |  |  | $0.00$ | 0.00 |
|  |  |  | Max. Compression | 26 | -48.23 | 3.87 | -1.94 |
|  |  |  | Max. Mx | 20 | -24.84 | 1247.50 | -3.00 |
|  |  |  | Max. My | 14 | -24.84 | 3.68 | -1245.02 |
|  |  |  | Max. Vy | 20 | -24.49 | 1247.50 | -3.00 |
|  |  |  | Max. Vx | 14 | 24.46 | 3.68 | -1245.02 |
|  |  |  | Max. Torque | 14 |  |  | -1.57 |
| L17 | 85.75-81 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -50.24 | 4.04 | -2.07 |

160 Ft Monopole Tower Structural Analysis

| Sectio <br> $n$ No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L18 | 81-80.75 | Pole | Max. Mx | 20 | -26.34 | 1365.07 | -3.24 |
|  |  |  | Max. My | 14 | -26.32 | 3.94 | -1362.82 |
|  |  |  | Max. Vy | 20 | -25.01 | 1365.07 | -3.24 |
|  |  |  | Max. Vx | 14 | 25.14 | 3.94 | -1362.82 |
|  |  |  | Max. Torque | 14 |  |  | -1.60 |
|  |  |  | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -50.33 | 4.05 | -2.07 |
|  |  |  | Max. Mx | 20 | -26.41 | 1371.33 | -3.25 |
|  |  |  | Max. My | 14 | -26.40 | 3.95 | -1369.10 |
|  |  |  | Max. Vy | 20 | -25.04 | 1371.33 | -3.25 |
|  |  | Pole | Max. Vx | 14 | 25.17 | 3.95 | -1369.10-1.60 |
|  |  |  | Max. Torque | 14 |  |  |  |
| L19 | 80.75-80.5 |  | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -50.43 | 4.05 | -2.07 |
|  |  |  | Max. Mx | 20 | -26.48 | 1377.59 | -3.27 |
|  |  |  | Max. My | 14 | -26.47 | 3.96 | -1375.40 |
|  |  |  | Max. Vy | 20 | -25.07 | 1377.59 | -3.27 |
|  |  |  | Max. Vx | 14 | 25.20 | 3.96 | $\begin{gathered} -1375.40 \\ -1.60 \end{gathered}$ |
|  |  | Pole | Max. Torque | 14 |  |  |  |
| L20 | 80.5-73.25 |  | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -50.94 | 4.05 | -2.08 |
|  |  |  | Max. Mx | 20 | -26.86 | 1415.29 | -3.34 |
|  |  |  | Max. My | 14 | -26.85 | 4.04 | -1413.30 |
|  |  |  | Max. Vy | 20 | -25.22 | 1415.29 | -3.34 |
|  |  |  | Max. Vx | 14 | 25.36 | 4.04 | -1413.30 |
|  |  |  | Max. Torque | 14 |  |  | $\begin{gathered} -1.60 \\ 0.00 \end{gathered}$ |
| L21 | $\begin{gathered} 73.25- \\ 72.25 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 |  |
|  |  |  | Max. Compression | 26 | -54.82 | 4.05 | -2.12 |
|  |  |  | Max. Mx | 20 | -29.78 | 1588.09 | -3.68 |
|  |  |  | Max. My | 14 | -29.77 | 4.39 | -1587.00 |
|  |  |  | Max. Vy | 20 | -25.99 | 1588.09 | -3.68 |
|  |  |  | Max. Vx | 14 | 26.12 | 4.39 | $\begin{gathered} -1587.00 \\ -1.60 \end{gathered}$ |
|  |  |  | Max. Torque | 14 |  |  |  |
| L22 | $\begin{gathered} 72.25 \\ 67.25 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -56.53 | 4.05 | -2.14 |
|  |  |  | Max. Mx | 20 | -31.20 | 1719.14 | -3.94 |
|  |  |  | Max. My | 14 | -31.19 | 4.64 | -1718.71 |
|  |  |  | Max. Vy | 20 | -26.46 | 1719.14 | -3.94 |
|  |  |  | Max. Vx | 14 | 26.59 | 4.64 | $\begin{gathered} -1718.71 \\ -1.60 \end{gathered}$ |
|  |  |  | Max. Torque | 14 |  |  |  |
| L23 | $\begin{gathered} 67.25- \\ 62.25 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -58.28 | 4.05 | -2.17 |
|  |  |  | Max. Mx | 20 | -32.65 | 1852.53 | -4.19 |
|  |  |  | Max. My | 14 | -32.64 | 4.89 | -1852.77 |
|  |  |  | Max. Vy | 20 | -26.93 | 1852.53 | -4.19 |
|  |  |  | Max. Vx | 14 | 27.06 | 4.89 | -1852.77 |
|  |  |  | Max. Torque | 14 |  |  | -1.60 |
| L24 | $\begin{gathered} 62.25- \\ 57.25 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -60.07 | 4.05 | -2.20 |
|  |  |  | Max. Mx | 20 | -34.13 | 1988.25 | -4.44 |
|  |  |  | Max. My | 14 | -34.12 | 5.15 | -1989.15 |
|  |  |  | Max. Vy | 20 | -27.39 | 1988.25 | -4.44 |
|  |  |  | Max. Vx | 14 | 27.52 | 5.15 | -1989.15 |
|  |  |  | Max. Torque | 14 |  |  | -1.60 |
| L25 | $\begin{gathered} 57.25- \\ 52.25 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -61.91 | 4.05 | -2.23 |
|  |  |  | Max. Mx | 20 | -35.66 | 2126.26 | -4.69 |
|  |  |  | Max. My | 14 | -35.65 | 5.40 | -2127.84 |
|  |  |  | Max. Vy | 20 | -27.84 | 2126.26 | -4.69 |
|  |  |  | Max. Vx | 14 | 27.98 | 5.40 | -2127.84 |
|  |  |  | Max. Torque | 14 |  |  | -1.59 |
| L26 | $\begin{gathered} 52.25- \\ 49.83 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -63.06 | 4.05 | -2.24 |

160 Ft Monopole Tower Structural Analysis
CCI BU No 806953
Project Number 400087, Order 479803, Revision 0


160 Ft Monopole Tower Structural Analysis


## Maximum Reactions

| Location | Condition | Gov. <br> Load | Vertical <br> Comb. | Horizontal, $X$ <br> $K$ | Horizontal, $Z$ <br> $K$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Pole | Max. Vert | 26 | 90.85 | 0.00 | -0.00 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 20 | 59.41 | 32.30 | -0.05 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 2 | 59.41 | -0.05 | 32.31 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 2 | 3696.43 | -0.05 | 32.31 |
|  | Max. $\mathrm{M}_{\mathrm{z}}$ | 8 | 3699.37 | -32.30 | 0.05 |

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| Location | Condition | Gov. Load Comb. | Vertical K | $\begin{gathered} \text { Horizontal, X } \\ K \end{gathered}$ | Horizontal, Z K |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Max. Torsion | 2 | 1.58 | -0.05 | 32.31 |
|  | Min. Vert | 11 | 44.56 | -27.95 | -16.12 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 8 | 59.41 | -32.30 | 0.05 |
|  | Min. $\mathrm{Hz}_{\mathrm{z}}$ | 14 | 59.41 | 0.05 | -33.77 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 14 | -3752.36 | 0.05 | -33.77 |
|  | Min. $\mathrm{M}_{\mathrm{z}}$ | 20 | -3702.30 | 32.30 | -0.05 |
|  | Min. Torsion | 14 | -1.59 | 0.05 | -33.77 |

## Tower Mast Reaction Summary

| Load Combination | Vertical <br> K | Shear $_{x}$ <br> K | Shear $_{z}$ <br> K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 49.51 | 0.00 | 0.00 | 0.40 | 1.13 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg - | 59.41 | 0.05 | -32.31 | -3696.43 | -5.03 | -1.58 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 0 deg - | 44.56 | 0.05 | -32.31 | -3651.35 | -5.34 | -1.54 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 30 deg - | 59.41 | 16.19 | -28.01 | -3204.36 | -1854.58 | -1.27 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 30 deg - | 44.56 | 16.19 | -28.01 | -3165.29 | -1832.25 | -1.25 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 60 deg - | 59.41 | 29.26 | -16.92 | -1881.00 | -3254.33 | -0.63 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 60 deg - | 44.56 | 29.26 | -16.92 | -1858.33 | -3215.23 | -0.62 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 90 deg - | 59.41 | 32.30 | -0.05 | -5.96 | -3699.37 | 0.18 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 90 deg - | 44.56 | 32.30 | -0.05 | -6.02 | -3654.48 | 0.17 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 120 deg | 59.41 | 27.95 | 16.12 | 1843.38 | -3200.33 | 0.95 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 120 deg | 44.56 | 27.95 | 16.12 | 1820.70 | -3161.54 | 0.92 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 150 deg | 59.41 | 16.11 | 27.96 | 3198.94 | -1843.36 | 1.47 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 150 deg | 44.56 | 16.11 | 27.96 | 3159.68 | -1821.18 | 1.43 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 180 deg | 59.41 | -0.05 | 33.77 | 3752.36 | 7.94 | 1.59 |
| - No lce |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 180 deg | 44.56 | -0.05 | 33.77 | 3706.74 | 7.47 | 1.56 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 210 deg | 59.41 | -16.19 | 28.01 | 3205.41 | 1857.49 | 1.28 |
| - No lce |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 210 deg | 44.56 | -16.19 | 28.01 | 3166.06 | 1834.38 | 1.27 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 240 deg | 59.41 | -28.00 | 16.20 | 1854.61 | 3209.71 | 0.63 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 240 deg | 44.56 | -28.00 | 16.20 | 1831.78 | 3170.06 | 0.62 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 270 deg | 59.41 | -32.30 | 0.05 | 7.01 | 3702.30 | -0.20 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 270 deg | 44.56 | -32.30 | 0.05 | 6.78 | 3656.62 | -0.18 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 300 deg | 59.41 | -29.21 | -16.84 | -1869.79 | 3250.79 | -0.97 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 300 deg | 44.56 | -29.21 | -16.84 | -1847.26 | 3210.99 | -0.94 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 330 deg | 59.41 | -16.11 | -27.96 | -3197.91 | 1846.27 | -1.47 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 330 deg | 44.56 | -16.11 | -27.96 | -3158.92 | 1823.31 | -1.43 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Ice+1.0 Temp | 90.85 | -0.00 | 0.00 | 2.10 | 4.05 | 0.00 |
| 1.2 Dead+1.0 Wind 0 | 90.85 | 0.01 | -7.90 | -960.71 | 2.87 | -0.42 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |


| Load Combination | Vertical | Shear $_{x}$ <br> K | Shear $_{z}$ <br> K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp | 90.85 | 3.96 | -6.85 | -832.39 | -478.72 | -0.32 |
| 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp | 90.85 | 6.86 | -3.97 | -480.99 | -831.85 | -0.14 |
| 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp | 90.85 | 7.89 | -0.01 | 0.83 | -959.30 | 0.09 |
| 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp | 90.85 | 6.83 | 3.94 | 482.47 | -829.52 | 0.29 |
| 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp | 90.85 | 3.94 | 6.84 | 835.42 | -476.34 | 0.41 |
| 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp | 90.85 | -0.01 | 7.92 | 966.22 | 5.62 | 0.42 |
| 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp | 90.85 | -3.96 | 6.85 | 836.80 | 487.21 | 0.32 |
| 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp | 90.85 | -6.84 | 3.96 | 484.85 | 839.39 | 0.14 |
| 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp | 90.85 | -7.89 | 0.01 | 3.58 | 967.80 | -0.09 |
| 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp | 90.85 | -6.85 | -3.95 | -478.61 | 838.97 | -0.29 |
| 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp | 90.85 | -3.94 | -6.84 | -831.01 | 484.83 | -0.41 |
| Dead+Wind 0 deg - Service | 49.51 | 0.01 | -7.61 | -864.03 | -0.31 | -0.37 |
| Dead+Wind 30 deg - Service | 49.51 | 3.81 | -6.59 | -748.97 | -432.79 | -0.30 |
| Dead+Wind 60 deg - Service | 49.51 | 6.89 | -3.98 | -439.56 | -760.15 | -0.15 |
| Dead+Wind 90 deg - Service | 49.51 | 7.61 | -0.01 | -1.09 | -864.16 | 0.04 |
| Dead+Wind 120 deg - | 49.51 | 6.58 | 3.79 | 431.34 | -747.47 | 0.22 |
| Service Dead+Wind 150 deg - | 49.51 | 3.79 | 6.58 | 748.31 | -430.17 | 0.34 |
| Service |  |  |  |  |  |  |
| Dead+Wind 180 deg Service | 49.51 | -0.01 | 7.95 | 877.78 | 2.72 | 0.37 |
| Dead+Wind 210 deg Service | 49.51 | -3.81 | 6.59 | 749.83 | 435.20 | 0.30 |
| Dead+Wind 240 deg Service | 49.51 | -6.59 | 3.81 | 433.97 | 751.39 | 0.15 |
| Dead+Wind 270 deg Service | 49.51 | -7.61 | 0.01 | 1.94 | 866.57 | -0.04 |
| Dead+Wind 300 deg Service | 49.51 | -6.88 | -3.97 | -436.94 | 761.05 | -0.22 |
| Dead+Wind 330 deg Service | 49.51 | -3.79 | -6.58 | -747.46 | 432.58 | -0.34 |

## Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | PX | PY | $P Z$ | PX | PY | $P Z$ |  |
| Comb. | K | K | K | K | K | K |  |
| 1 | 0.00 | -49.51 | 0.00 | 0.00 | 49.51 | 0.00 | 0.000\% |
| 2 | 0.05 | -59.41 | -32.31 | -0.05 | 59.41 | 32.31 | 0.000\% |
| 3 | 0.05 | -44.56 | -32.31 | -0.05 | 44.56 | 32.31 | 0.000\% |
| 4 | 16.19 | -59.41 | -28.01 | -16.19 | 59.41 | 28.01 | 0.000\% |
| 5 | 16.19 | -44.56 | -28.01 | -16.19 | 44.56 | 28.01 | 0.000\% |
| 6 | 29.26 | -59.41 | -16.92 | -29.26 | 59.41 | 16.92 | 0.000\% |
| 7 | 29.26 | -44.56 | -16.92 | -29.26 | 44.56 | 16.92 | 0.000\% |
| 8 | 32.30 | -59.41 | -0.05 | -32.30 | 59.41 | 0.05 | 0.000\% |
| 9 | 32.30 | -44.56 | -0.05 | -32.30 | 44.56 | 0.05 | 0.000\% |
| 10 | 27.95 | -59.41 | 16.12 | -27.95 | 59.41 | -16.12 | 0.000\% |
| 11 | 27.95 | -44.56 | 16.12 | -27.95 | 44.56 | -16.12 | 0.000\% |
| 12 | 16.11 | -59.41 | 27.96 | -16.11 | 59.41 | -27.96 | 0.000\% |
| 13 | 16.11 | -44.56 | 27.96 | -16.11 | 44.56 | -27.96 | 0.000\% |
| 14 | -0.05 | -59.41 | 33.77 | 0.05 | 59.41 | -33.77 | 0.000\% |
| 15 | -0.05 | -44.56 | 33.77 | 0.05 | 44.56 | -33.77 | 0.000\% |
| 16 | -16.19 | -59.41 | 28.01 | 16.19 | 59.41 | -28.01 | 0.000\% |
| 17 | -16.19 | -44.56 | 28.01 | 16.19 | 44.56 | -28.01 | 0.000\% |
| 18 | -28.00 | -59.41 | 16.20 | 28.00 | 59.41 | -16.20 | 0.000\% |

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|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | $P Z$ | $P X$ | PY | $P Z$ |  |
| Comb. | K | K | K | K | K | K |  |
| 19 | -28.00 | -44.56 | 16.20 | 28.00 | 44.56 | -16.20 | 0.000\% |
| 20 | -32.30 | -59.41 | 0.05 | 32.30 | 59.41 | -0.05 | 0.000\% |
| 21 | -32.30 | -44.56 | 0.05 | 32.30 | 44.56 | -0.05 | 0.000\% |
| 22 | -29.21 | -59.41 | -16.84 | 29.21 | 59.41 | 16.84 | 0.000\% |
| 23 | -29.21 | -44.56 | -16.84 | 29.21 | 44.56 | 16.84 | 0.000\% |
| 24 | -16.11 | -59.41 | -27.96 | 16.11 | 59.41 | 27.96 | 0.000\% |
| 25 | -16.11 | -44.56 | -27.96 | 16.11 | 44.56 | 27.96 | 0.000\% |
| 26 | 0.00 | -90.85 | 0.00 | 0.00 | 90.85 | -0.00 | 0.000\% |
| 27 | 0.01 | -90.85 | -7.90 | -0.01 | 90.85 | 7.90 | 0.000\% |
| 28 | 3.96 | -90.85 | -6.85 | -3.96 | 90.85 | 6.85 | 0.000\% |
| 29 | 6.86 | -90.85 | -3.97 | -6.86 | 90.85 | 3.97 | 0.000\% |
| 30 | 7.89 | -90.85 | -0.01 | -7.89 | 90.85 | 0.01 | 0.000\% |
| 31 | 6.83 | -90.85 | 3.94 | -6.83 | 90.85 | -3.94 | 0.000\% |
| 32 | 3.94 | -90.85 | 6.84 | -3.94 | 90.85 | -6.84 | 0.000\% |
| 33 | -0.01 | -90.85 | 7.92 | 0.01 | 90.85 | -7.92 | 0.000\% |
| 34 | -3.96 | -90.85 | 6.85 | 3.96 | 90.85 | -6.85 | 0.000\% |
| 35 | -6.84 | -90.85 | 3.96 | 6.84 | 90.85 | -3.96 | 0.000\% |
| 36 | -7.89 | -90.85 | 0.01 | 7.89 | 90.85 | -0.01 | 0.000\% |
| 37 | -6.85 | -90.85 | -3.95 | 6.85 | 90.85 | 3.95 | 0.000\% |
| 38 | -3.94 | -90.85 | -6.84 | 3.94 | 90.85 | 6.84 | 0.000\% |
| 39 | 0.01 | -49.51 | -7.61 | -0.01 | 49.51 | 7.61 | 0.000\% |
| 40 | 3.81 | -49.51 | -6.59 | -3.81 | 49.51 | 6.59 | 0.000\% |
| 41 | 6.89 | -49.51 | -3.98 | -6.89 | 49.51 | 3.98 | 0.000\% |
| 42 | 7.61 | -49.51 | -0.01 | -7.61 | 49.51 | 0.01 | 0.000\% |
| 43 | 6.58 | -49.51 | 3.79 | -6.58 | 49.51 | -3.79 | 0.000\% |
| 44 | 3.79 | -49.51 | 6.58 | -3.79 | 49.51 | -6.58 | 0.000\% |
| 45 | -0.01 | -49.51 | 7.95 | 0.01 | 49.51 | -7.95 | 0.000\% |
| 46 | -3.81 | -49.51 | 6.59 | 3.81 | 49.51 | -6.59 | 0.000\% |
| 47 | -6.59 | -49.51 | 3.81 | 6.59 | 49.51 | -3.81 | 0.000\% |
| 48 | -7.61 | -49.51 | 0.01 | 7.61 | 49.51 | -0.01 | 0.000\% |
| 49 | -6.88 | -49.51 | -3.97 | 6.88 | 49.51 | 3.97 | 0.000\% |
| 50 | -3.79 | -49.51 | -6.58 | 3.79 | 49.51 | 6.58 | 0.000\% |

## Non-Linear Convergence Results

| Load <br> Combination | Converged? | Number <br> of Cycles | Displacement <br> Tolerance | Force <br> Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 4 | 0.00000001 | 0.00000001 |
| 2 | Yes | 5 | 0.00000001 | 0.00068950 |
| 3 | Yes | 5 | 0.00000001 | 0.00031327 |
| 4 | Yes | 6 | 0.00000001 | 0.00090912 |
| 5 | Yes | 6 | 0.00000001 | 0.00030180 |
| 6 | Yes | 6 | 0.00000001 | 0.00093988 |
| 7 | Yes | 6 | 0.00000001 | 0.00031181 |
| 8 | Yes | 5 | 0.00000001 | 0.00029608 |
| 9 | Yes | 5 | 0.00000001 | 0.00010719 |
| 10 | Yes | 6 | 0.00000001 | 0.00093330 |
| 11 | Yes | 6 | 0.00000001 | 0.00031098 |
| 12 | Yes | 6 | 0.00000001 | 0.00089962 |
| 13 | Yes | 6 | 0.00000001 | 0.00029886 |
| 14 | Yes | 5 | 0.00000001 | 0.00082638 |
| 15 | Yes | 5 | 0.00000001 | 0.00037865 |
| 16 | Yes | 6 | 0.00000001 | 0.00094663 |
| 17 | Yes | 6 | 0.00000001 | 0.00031498 |
| 18 | Yes | 6 | 0.00000001 | 0.00092180 |
| 19 | Yes | 6 | 0.00000001 | 0.00030583 |
| 20 | Yes | 5 | 0.00000001 | 0.00034915 |
| 21 | Yes | 5 | 0.00000001 | 0.00013653 |
| 22 | Yes | 6 | 0.00000001 | 0.00091365 |
| 23 | Yes | Yes | 6 | 0.00000001 |
| 24 | Yes | Yes | 6 | 0.00030259 |
| 25 | Yes | Yes | 7 | 0.00094133 |
| 26 |  |  | 0.00031378 |  |
| 27 | 28 |  |  | 0.00069477 |
|  |  |  | 0.00000001 | 0.00092366 |
|  |  |  | 0.00013335 |  |


| 29 | Yes | 7 | 0.00000001 | 0.00013378 |
| :--- | :--- | :--- | :--- | :--- |
| 30 | Yes | 6 | 0.00000001 | 0.00091918 |
| 31 | Yes | 7 | 0.00000001 | 0.00013452 |
| 32 | Yes | 7 | 0.00000001 | 0.00013402 |
| 33 | Yes | 6 | 0.00000001 | 0.00093338 |
| 34 | Yes | 7 | 0.00000001 | 0.00013748 |
| 35 | Yes | 7 | 0.00000001 | 0.00013718 |
| 36 | Yes | 6 | 0.00000001 | 0.00093811 |
| 37 | Yes | 7 | 0.00000001 | 0.00013547 |
| 38 | Yes | 7 | 0.00000001 | 0.00013583 |
| 39 | Yes | 5 | 0.00000001 | 0.00006780 |
| 40 | Yes | 5 | 0.00000001 | 0.00024316 |
| 41 | Yes | 5 | 0.00000001 | 0.00026297 |
| 42 | Yes | 5 | 0.00000001 | 0.00005746 |
| 43 | Yes | 5 | 0.00000001 | 0.00026282 |
| 44 | Yes | 5 | 0.00000001 | 0.00023995 |
| 45 | Yes | 5 | 0.00000001 | 0.00006930 |
| 46 | Yes | 5 | 0.00000001 | 0.00027102 |
| 47 | Yes | 5 | 0.00000001 | 0.00025255 |
| 48 | Yes | 5 | 0.00000001 | 0.00005803 |
| 49 | Yes | 5 | 0.00000001 | 0.00024826 |
| 50 | Yes | 5 | 0.00000001 | 0.00026979 |

## Maximum Tower Deflections - Service Wind

| Section | Elevation | Horz. <br> Deflection <br> No. | ft | Gov. <br> Load <br> Comb. | Tilt |
| :---: | :---: | :---: | :---: | :---: | :---: |

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| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $0.5-4.5$ | 0.078 | 41 | 0.0784 |
| L41 | $4.5-0$ | 0.017 | 41 | 0.0368 | $\circ$ |
| L42 |  |  |  |  | 0.0000 |
|  |  |  |  |  |  |

Critical Deflections and Radius of Curvature - Service Wind

| Elevation | Appurtenance | Gov. <br> Load | Deflection | Tilt | Twist |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  | Comb. | in | $\circ$ | 0 | Radius of <br> Curvature <br> $f t$ |
| 157.00 | Platform Mount [LP 713-1] | 49 | 23.469 | 1.3856 | 0.0040 | 63777 |
| 154.00 | Pipe Mount [PM 601-3] | 49 | 22.601 | 1.3837 | 0.0038 | 50494 |
| 149.00 | Platform Mount [LP 713-1] | 49 | 21.161 | 1.3741 | 0.0034 | 20649 |
| 139.00 | Platform Mount [LP 713-1] | 49 | 18.334 | 1.3258 | 0.0027 | 8300 |
| 118.00 | Platform Mount [LP 712-1] | 49 | 12.957 | 1.1009 | 0.0015 | 5232 |
| 84.00 | 3'x2" Horizontal Pipe | 45 | 6.359 | 0.7386 | 0.0007 | 6198 |
| 40.00 | Pipe Mount [PM 601-1] | 41 | 1.421 | 0.3294 | 0.0002 | 9842 |

\(\left.$$
\begin{array}{cccccc}\hline \text { Section } & \text { Elevation } & \begin{array}{c}\text { Horz. } \\
\text { Deflection } \\
\text { in }\end{array}
$$ \& \begin{array}{c}Gov. <br>
Load <br>

Comb.\end{array} \& Comilt \& Tilt\end{array}\right]\)| Twist |
| :---: |
|  |
| L1 |

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| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | 0.332 | 6 | $\circ$ | $\circ$ |
| L41 | $9.5-4.5$ | 0.074 | 6 | 0.3356 | 0.0002 |
| L42 | $4.5-0$ |  |  | 0.1574 | 0.0001 |

## Critical Deflections and Radius of Curvature - Design Wind

| Elevation | Appurtenance | Gov. <br> Load | Deflection | Tilt | Twist | Radius of <br> Curvature |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  | Comb. | in | 。 | o |  |
| 157.00 | Platform Mount [LP 713-1] | 6 | 100.372 | 5.9082 | 0.0172 | 17813 |
| 154.00 | Pipe Mount [PM 601-3] | 6 | 96.677 | 5.9013 | 0.0164 | 13756 |
| 149.00 | Platform Mount [LP 713-1] | 6 | 90.537 | 5.8636 | 0.0144 | 5157 |
| 139.00 | Platform Mount [LP 713-1] | 6 | 78.474 | 5.6620 | 0.0115 | 2003 |
| 118.00 | Platform Mount [LP 712-1] | 6 | 55.501 | 4.7127 | 0.0064 | 1246 |
| 84.00 | 3'x2" Horizontal Pipe | 6 | 27.252 | 3.1671 | 0.0029 | 1460 |
| 40.00 | Pipe Mount [PM 601-1] | 6 | 6.090 | 1.4119 | 0.0009 | 2298 |

## Compression Checks

## Pole Design Data



| Section No. | Elevation | Size | L | $L_{u}$ | KI/r | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft |  | ft | ft |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
|  | (18) | 8 |  |  |  | 0 |  |  |  |
| L19 | $\begin{gathered} 80.75-80.5 \\ (19) \end{gathered}$ | TP38.1749×38.115×0.343 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 41.874 \\ 3 \end{gathered}$ | -26.48 | 2449.65 | 0.011 |
| L20 | $\begin{gathered} 80.5-73.25 \\ (20) \end{gathered}$ | $\begin{gathered} \text { TP39.912×38.1749x0.343 } \\ 8 \end{gathered}$ | 7.25 | 0.00 | 0.0 | $\begin{gathered} 42.272 \\ 2 \end{gathered}$ | -26.86 | 2472.92 | 0.011 |
| L21 | $\begin{gathered} 73.25-72.25 \\ (21) \end{gathered}$ | $\begin{gathered} \mathrm{TP} 39.467 \times 37.8468 \times 0.406 \\ 3 \end{gathered}$ | 6.75 | 0.00 | 0.0 | $\begin{gathered} 51.096 \\ 3 \end{gathered}$ | -29.78 | 2989.13 | 0.010 |
| L22 | $\begin{gathered} 72.25-67.25 \\ (22) \end{gathered}$ | $\begin{gathered} \text { TP40.6671×39.467×0.406 } \\ 3 \end{gathered}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 52.666 \\ 3 \end{gathered}$ | -31.18 | 3080.98 | 0.010 |
| L23 | $\begin{gathered} 67.25-62.25 \\ (23) \end{gathered}$ | $\begin{gathered} \text { TP41.8673×40.6671×0.40 } \\ 63 \end{gathered}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 54.236 \\ 2 \end{gathered}$ | -32.63 | 3172.82 | 0.010 |
| L24 | $62.25-57.25$ <br> (24) | TP43.0674×41.8673×0.40 63 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 55.806 \\ 1 \end{gathered}$ | -34.12 | 3264.66 | 0.010 |
| L25 | $\begin{gathered} 57.25-52.25 \\ (25) \end{gathered}$ | $\begin{gathered} \text { TP44.2675×43.0674×0.40 } \\ 63 \end{gathered}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 57.376 \\ 1 \end{gathered}$ | -35.65 | 3356.50 | 0.011 |
| L26 | $\begin{gathered} 52.25-49.83 \\ (26) \end{gathered}$ | TP44.8484×44.2675×0.40 63 | 2.42 | 0.00 | 0.0 | $\begin{gathered} 58.135 \\ 9 \end{gathered}$ | -36.57 | 3400.95 | 0.011 |
| L27 | $\begin{gathered} 49.83-49.58 \\ (27) \end{gathered}$ | TP44.9084×44.8484×0.40 63 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 58.214 \\ 4 \end{gathered}$ | -36.68 | 3405.54 | 0.011 |
| L28 | $49.58-44.58$ <br> (28) | $\begin{aligned} & \text { TP46.1086x44.9084×0.40 } \\ & 63 \end{aligned}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 59.784 \\ 3 \end{gathered}$ | -38.60 | 3497.38 | 0.011 |
| L29 | $\begin{gathered} 44.58- \\ 36.3333(29) \end{gathered}$ | TP48.088×46.1086x0.406 3 | 8.25 | 0.00 | 0.0 | $\begin{gathered} 60.280 \\ 4 \end{gathered}$ | -39.22 | 3526.41 | 0.011 |
| L30 | $\begin{gathered} 36.3333- \\ 35.3333(30) \end{gathered}$ | TP47.5162×45.6753×0.43 75 | 7.67 | 0.00 | 0.0 | $\begin{gathered} 66.322 \\ 1 \end{gathered}$ | -44.06 | 3879.84 | 0.011 |
| L31 | $\begin{aligned} & 35.3333- \\ & 32.25(31) \end{aligned}$ | $\begin{gathered} \text { TP48.2565×47.5162×0.43 } \\ 75 \end{gathered}$ | 3.08 | 0.00 | 0.0 | $\begin{gathered} 67.365 \\ 0 \end{gathered}$ | -45.35 | 3940.85 | 0.012 |
| L32 | $\begin{gathered} 32.25-32 \\ (32) \end{gathered}$ | TP48.3165×48.2565×0.43 75 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 67.449 \\ 5 \end{gathered}$ | -45.47 | 3945.80 | 0.012 |
| L33 | 32-27(33) | $\begin{gathered} \text { TP49.5171×48.3165×0.43 } \\ 75 \end{gathered}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 69.140 \\ 8 \end{gathered}$ | -47.60 | 4044.74 | 0.012 |
| L34 | 27-22 (34) | $\begin{gathered} \text { TP50.7176×49.5171×0.43 } \\ 75 \end{gathered}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 70.832 \\ 1 \end{gathered}$ | -49.77 | 4143.68 | 0.012 |
| L35 | 22-17 (35) | $\begin{gathered} \text { TP51.9181×50.7176×0.43 } \\ 75 \end{gathered}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 72.523 \\ 4 \end{gathered}$ | -51.97 | 4242.62 | 0.012 |
| L36 | 17-15.5 (36) | $\begin{aligned} & \text { TP52.2783×51.9181×0.43 } \\ & 75 \end{aligned}$ | 1.50 | 0.00 | 0.0 | $\begin{gathered} 73.030 \\ 7 \end{gathered}$ | -52.68 | 4272.30 | 0.012 |
| L37 | $\begin{gathered} 15.5-15.25 \\ (37) \end{gathered}$ | $\begin{gathered} \text { TP52.3383 } \times 52.2783 \times 0.43 \\ 75 \end{gathered}$ | 0.25 | 0.00 | 0.0 | $\begin{gathered} 73.115 \\ 3 \end{gathered}$ | -52.82 | 4277.25 | 0.012 |
| L38 | $15.25-14.75$ <br> (38) | $\begin{gathered} \text { TP52.4584×52.3383×0.43 } \\ 75 \end{gathered}$ | 0.50 | 0.00 | 0.0 | $\begin{gathered} 73.284 \\ 4 \end{gathered}$ | -53.06 | 4287.14 | 0.012 |
| L39 | $\begin{gathered} 14.75-14.5 \\ (39) \end{gathered}$ | $\begin{gathered} \text { TP52.5184×52.4584×0.43 } \\ 75 \end{gathered}$ | 0.25 | 0.00 | 0.0 | $\begin{gathered} 73.369 \\ 0 \end{gathered}$ | -53.18 | 4292.09 | 0.012 |
| L40 | 14.5-9.5 (40) | TP53.719×52.5184×0.437 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 75.060 \\ 3 \end{gathered}$ | -55.42 | 4391.03 | 0.013 |
| L41 | 9.5-4.5 (41) | $\begin{gathered} \text { TP54.9195 } 53.719 \times 0.437 \\ 5 \end{gathered}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 76.751 \\ 5 \end{gathered}$ | -57.53 | 4489.96 | 0.013 |
| L42 | 4.5-0 (42) | TP56x54.9195x0.4375 | 4.50 | 0.00 | 0.0 | $\begin{gathered} 78.273 \\ 7 \end{gathered}$ | -59.40 | 4579.01 | 0.013 |

## Pole Bending Design Data

| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | Ratio $M_{u x}$ | $M_{u y}$ | $\phi M_{n y}$ | Ratio $M_{u y}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft |  |  | kip-ft | kip-ft | ${ }_{\phi} M_{n x}$ | kip-ft | kip-ft | $\phi M_{n y}$ |
| L1 | 160-155 (1) | TP20.801x19.6x0.25 | 10.23 | 508.14 | 0.020 | 0.00 | 508.14 | 0.000 |
| L2 | 155-150 (2) | TP22.0021x20.801x0.25 | 32.69 | 559.87 | 0.058 | 0.00 | 559.87 | 0.000 |
| L3 | 150-145 (3) | TP23.2031x22.0021x0.25 | 82.84 | 612.89 | 0.135 | 0.00 | 612.89 | 0.000 |
| L4 | 145-140 (4) | TP24.4041x23.2031x0.25 | 134.30 | 667.00 | 0.201 | 0.00 | 667.00 | 0.000 |
| L5 | 140-135 (5) | TP25.6051x24.4041x0.25 | 219.80 | 722.04 | 0.304 | 0.00 | 722.04 | 0.000 |
| L6 | 135-130 (6) | TP26.8062x25.6051x0.25 | 301.74 | 777.82 | 0.388 | 0.00 | 777.82 | 0.000 |
| L7 | 130-125 (7) | TP28.0072x26.8062x0.25 | 385.85 | 834.16 | 0.463 | 0.00 | 834.16 | 0.000 |
| L8 | 125-120 (8) | TP29.2082x28.0072x0.25 | 472.14 | 890.88 | 0.530 | 0.00 | 890.88 | 0.000 |
| L9 | 120-111.333 | TP31.29x29.2082x0.25 | 550.69 | 936.40 | 0.588 | 0.00 | 936.40 | 0.000 |

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| Section No. | Elevation <br> ft | Size | $\begin{gathered} M_{u x} \\ \text { kip-ft } \end{gathered}$ | $\phi M_{n x}$ | Ratio $M_{u x}$ | $M_{u y}$ kip-ft | $\phi M_{n y}$ <br> kip-ft | Ratio $M_{u y}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $\phi M_{n x}$ |  |  | $\phi M_{n y}$ |
| L10 | $\begin{gathered} 111.333-111 \\ (10) \end{gathered}$ | TP30.867x29.669x0.3438 | 660.13 | 1506.34 | 0.438 | 0.00 | 1506.34 | 0.000 |
| L11 | 111-106 (11) | TP32.065x30.867x0.3438 | 772.05 | 1606.85 | 0.480 | 0.00 | 1606.85 | 0.000 |
| L12 | 106-101 (12) | TP33.2631×32.065×0.343 | 886.30 | 1708.83 | 0.519 | 0.00 | 1708.83 | 0.000 |
| L13 | 101-96 (13) | TP34.4611×33.2631×0.34 38 | 1002.87 | 1812.13 | 0.553 | 0.00 | 1812.13 | 0.000 |
| L14 | 96-91 (14) | $\begin{gathered} \text { TP35.6591×34.4611×0.34 } \\ 38 \end{gathered}$ | 1121.77 | 1916.55 | 0.585 | 0.00 | 1916.55 | 0.000 |
| L15 | 91-86 (15) | $\begin{gathered} \text { TP36.8571×35.6591×0.34 } \\ 38 \end{gathered}$ | 1243.00 | 2021.91 | 0.615 | 0.00 | 2021.91 | 0.000 |
| L16 | $\begin{gathered} 86-85.75 \\ (16) \end{gathered}$ | $\begin{gathered} \text { TP36.917x36.8571×0.512 } \\ 5 \end{gathered}$ | 1249.13 | 3264.29 | 0.383 | 0.00 | 3264.29 | 0.000 |
| L17 | $\begin{gathered} 85.75-81 \\ (17) \end{gathered}$ | TP38.0551×36.917×0.506 3 | 1366.85 | 3432.41 | 0.398 | 0.00 | 3432.41 | 0.000 |
| L18 | $\begin{gathered} 81-80.75 \\ (18) \end{gathered}$ | TP38.115×38.0551×0.343 8 | 1373.11 | 2133.36 | 0.644 | 0.00 | 2133.36 | 0.000 |
| L19 | $80.75-80.5$ <br> (19) | TP38.1749×38.115×0.343 8 | 1379.38 | 2138.68 | 0.645 | 0.00 | 2138.68 | 0.000 |
| L20 | $80.5-73.25$ <br> (20) | TP39.912×38.1749×0.343 <br> 8 | 1417.13 | 2170.66 | 0.653 | 0.00 | 2170.66 | 0.000 |
| L21 | $73.25-72.25$ <br> (21) | TP39.467x37.8468×0.406 3 | 1590.14 | 2839.37 | 0.560 | 0.00 | 2839.37 | 0.000 |
| L22 | $\begin{gathered} 72.25-67.25 \\ (22) \end{gathered}$ | $\begin{gathered} \text { TP40.6671×39.467×0.406 } \\ 3 \end{gathered}$ | 1721.41 | 2983.96 | 0.577 | 0.00 | 2983.96 | 0.000 |
| L23 | $67.25-62.25$ <br> (23) | TP41.8673×40.6671×0.40 63 | 1855.86 | 3129.88 | 0.593 | 0.00 | 3129.88 | 0.000 |
| L24 | $\begin{gathered} 62.25-57.25 \\ (24) \end{gathered}$ | $\begin{gathered} \text { TP43.0674×41.8673×0.40 } \\ 63 \end{gathered}$ | 1992.63 | 3276.97 | 0.608 | 0.00 | 3276.97 | 0.000 |
| L25 | $57.25-52.25$ <br> (25) | TP44.2675×43.0674×0.40 63 | 2131.70 | 3425.04 | 0.622 | 0.00 | 3425.04 | 0.000 |
| L26 | $\begin{gathered} 52.25-49.83 \\ (26) \end{gathered}$ | TP44.8484×44.2675×0.40 63 | 2199.93 | 3497.01 | 0.629 | 0.00 | 3497.01 | 0.000 |
| L27 | $\begin{gathered} 49.83-49.58 \\ (27) \end{gathered}$ | $\begin{gathered} \text { TP44.9084×44.8484×0.40 } \\ 63 \end{gathered}$ | 2207.02 | 3504.46 | 0.630 | 0.00 | 3504.46 | 0.000 |
| L28 | $\begin{gathered} 49.58-44.58 \\ (28) \end{gathered}$ | TP46.1086×44.9084×0.40 63 | 2350.38 | 3653.68 | 0.643 | 0.00 | 3653.68 | 0.000 |
| L29 | $\begin{gathered} 44.58- \\ 36.3333(29) \end{gathered}$ | TP48.088×46.1086×0.406 3 | 2396.31 | 3700.96 | 0.647 | 0.00 | 3700.96 | 0.000 |
| L30 | $\begin{gathered} 36.3333- \\ 35.3333(30) \end{gathered}$ | $\begin{gathered} \text { TP47.5162×45.6753×0.43 } \\ 75 \end{gathered}$ | 2624.25 | 4255.33 | 0.617 | 0.00 | 4255.33 | 0.000 |
| L31 | $\begin{aligned} & 35.3333- \\ & 32.25(31) \end{aligned}$ | $\begin{gathered} \text { TP48.2565×47.5162×0.43 } \\ 75 \end{gathered}$ | 2718.00 | 4361.67 | 0.623 | 0.00 | 4361.67 | 0.000 |
| L32 | $\begin{gathered} 32.25-32 \\ (32) \end{gathered}$ | TP48.3165×48.2565×0.43 75 | 2725.65 | 4370.30 | 0.624 | 0.00 | 4370.30 | 0.000 |
| L33 | 32-27 (33) | $\begin{gathered} \text { TP49.5171×48.3165×0.43 } \\ 75 \end{gathered}$ | 2879.98 | 4543.38 | 0.634 | 0.00 | 4543.38 | 0.000 |
| L34 | 27-22 (34) | $\begin{gathered} \text { TP50.7176×49.5171×0.43 } \\ 75 \end{gathered}$ | 3036.98 | 4717.04 | 0.644 | 0.00 | 4717.04 | 0.000 |
| L35 | 22-17(35) | $\begin{gathered} \text { TP51.9181×50.7176×0.43 } \\ 75 \end{gathered}$ | 3196.65 | 4891.11 | 0.654 | 0.00 | 4891.11 | 0.000 |
| L36 | 17-15.5 (36) | $\begin{gathered} \text { TP52.2783×51.9181×0.43 } \\ 75 \end{gathered}$ | 3245.09 | 4943.38 | 0.656 | 0.00 | 4943.38 | 0.000 |
| L37 | 15.5-15.25 | $\begin{aligned} & \text { TP52.3383×52.2783×0.43 } \\ & 75 \end{aligned}$ | 3253.18 | 4952.09 | 0.657 | 0.00 | 4952.09 | 0.000 |
| L38 | $\begin{gathered} 15.25-14.75 \\ (38) \end{gathered}$ | TP52.4584×52.3383×0.43 75 | 3269.40 | 4969.52 | 0.658 | 0.00 | 4969.52 | 0.000 |
| L39 | $\begin{gathered} 14.75-14.5 \\ (39) \end{gathered}$ | $\begin{gathered} \text { TP52.5184×52.4584×0.43 } \\ 75 \end{gathered}$ | 3277.53 | 4978.23 | 0.658 | 0.00 | 4978.23 | 0.000 |
| L40 | 14.5-9.5 (40) | TP53.719×52.5184×0.437 | 3441.35 | 5152.57 | 0.668 | 0.00 | 5152.57 | 0.000 |
| L41 | 9.5-4.5 (41) | TP54.9195 $\times 53.719 \times 0.437$ 5 | 3607.55 | 5326.86 | 0.677 | 0.00 | 5326.86 | 0.000 |
| L42 | 4.5-0 (42) | TP56x54.9195x0.4375 | 3758.83 | 5483.53 | 0.685 | 0.00 | 5483.53 | 0.000 |

## Pole Shear Design Data

| Section No. | Elevation <br> ft | Size | Actual $V_{u}$ K | $\phi V_{n}$ $K$ | Ratio $V_{u}$ | Actual $T_{u}$ kip-ft | $\phi T_{n}$ kip-ft | Ratio $T_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $\phi V_{n}$ | kip | kip-ft | $\phi T_{n}$ |
| L1 | 160-155 (1) | TP20.801x19.6x0.25 | 3.73 | 290.34 | 0.013 | 0.56 | 524.86 | 0.001 |
| L2 | 155-150 (2) | TP22.0021x20.801x0.25 | 4.83 | 307.31 | 0.016 | 0.56 | 588.00 | 0.001 |
| L3 | 150-145 (3) | TP23.2031x22.0021x0.25 | 10.09 | 324.27 | 0.031 | 0.56 | 654.72 | 0.001 |
| L4 | 145-140 (4) | TP24.4041x23.2031x0.25 | 10.51 | 341.24 | 0.031 | 0.56 | 725.03 | 0.001 |
| L5 | 140-135 (5) | TP25.6051x24.4041x0.25 | 16.18 | 358.21 | 0.045 | 0.56 | 798.92 | 0.001 |
| L6 | 135-130 (6) | TP26.8062x25.6051x0.25 | 16.61 | 375.18 | 0.044 | 0.56 | 876.40 | 0.001 |
| L7 | 130-125 (7) | TP28.0072x26.8062x0.25 | 17.05 | 392.15 | 0.043 | 0.56 | 957.47 | 0.001 |
| L8 | 125-120 (8) | TP29.2082x28.0072x0.25 | 17.49 | 409.11 | 0.043 | 0.56 | 1042.12 | 0.001 |
| L9 | $\begin{gathered} 120-111.333 \\ \text { (9) } \end{gathered}$ | TP31.29x29.2082x0.25 | 21.63 | 422.69 | 0.051 | 0.56 | 1112.42 | 0.001 |
| L10 | $\begin{gathered} 111.333-111 \\ (10) \end{gathered}$ | TP30.867x29.669x0.3438 | 22.17 | 592.93 | 0.037 | 0.56 | 1591.98 | 0.000 |
| L11 | 111-106 (11) | TP32.065x30.867x0.3438 | 22.63 | 616.21 | 0.037 | 0.56 | 1719.40 | 0.000 |
| L12 | 106-101 (12) | TP33.2631×32.065×0.343 8 | 23.09 | 639.48 | 0.036 | 0.56 | 1851.72 | 0.000 |
| L13 | 101-96 (13) | $\begin{gathered} \text { TP34.4611×33.2631×0.34 } \\ 38 \end{gathered}$ | 23.56 | 662.75 | 0.036 | 0.56 | 1988.96 | 0.000 |
| L14 | 96-91 (14) | $\begin{gathered} \text { TP35.6591×34.4611×0.34 } \\ 38 \end{gathered}$ | 24.03 | 686.02 | 0.035 | 0.56 | 2131.09 | 0.000 |
| L15 | 91-86 (15) | TP36.8571×35.6591×0.34 38 | 24.49 | 709.29 | 0.035 | 0.56 | 2278.13 | 0.000 |
| L16 | $\begin{gathered} 86-85.75 \\ (16) \end{gathered}$ | TP36.917×36.8571×0.512 5 | 24.52 | 1054.34 | 0.023 | 0.56 | 3376.27 | 0.000 |
| L17 | $\begin{gathered} 85.75-81 \\ (17) \end{gathered}$ | TP38.0551×36.917×0.506 3 | 25.04 | 1074.22 | 0.023 | 0.56 | 3548.06 | 0.000 |
| L18 | $81-80.75$ <br> (18) | TP38.115×38.0551×0.343 8 | 25.08 | 733.73 | 0.034 | 0.56 | 2437.80 | 0.000 |
| L19 | $\begin{gathered} 80.75-80.5 \\ (19) \end{gathered}$ | TP38.1749×38.115×0.343 8 | 25.11 | 734.89 | 0.034 | 0.56 | 2445.54 | 0.000 |
| L20 | $\begin{gathered} 80.5-73.25(20) \end{gathered}$ | TP39.912×38.1749×0.343 8 | 25.25 | 741.88 | 0.034 | 0.56 | 2492.22 | 0.000 |
| L21 | $\begin{gathered} 73.25-72.25 \\ (21) \end{gathered}$ | TP39.467×37.8468×0.406 3 | 26.02 | 896.74 | 0.029 | 0.56 | 3081.11 | 0.000 |
| L22 | $\begin{gathered} 72.25-67.25 \\ (22) \end{gathered}$ | $\begin{gathered} \text { TP40.6671×39.467×0.406 } \\ 3 \end{gathered}$ | 26.67 | 924.29 | 0.029 | 0.56 | 3273.35 | 0.000 |
| L23 | $67.25-62.25$ <br> (23) | TP41.8673×40.6671×0.40 63 | 27.14 | 951.85 | 0.029 | 0.56 | 3471.41 | 0.000 |
| L24 | $\begin{gathered} 62.25-57.25 \\ (24) \end{gathered}$ | TP43.0674×41.8673×0.40 63 | 27.60 | 979.40 | 0.028 | 0.56 | 3675.29 | 0.000 |
| L25 | $\begin{gathered} 57.25-52.25 \\ (25) \end{gathered}$ | TP44.2675×43.0674×0.40 63 | 28.06 | 1006.95 | 0.028 | 0.56 | 3884.98 | 0.000 |
| L26 | $52.25-49.83$ <br> (26) | TP44.8484×44.2675×0.40 63 | 28.36 | 1020.29 | 0.028 | 0.56 | 3988.57 | 0.000 |
| L27 | $\begin{gathered} 49.83-49.58 \\ (27) \end{gathered}$ | TP44.9084×44.8484×0.40 63 | 28.38 | 1021.66 | 0.028 | 0.56 | 3999.34 | 0.000 |
| L28 | $\begin{gathered} 49.58-44.58 \\ (28) \end{gathered}$ | TP46.1086×44.9084×0.40 63 | 28.99 | 1049.22 | 0.028 | 0.56 | 4217.96 | 0.000 |
| L29 | $\begin{gathered} 44.58- \\ 36.3333(29) \end{gathered}$ | TP48.088×46.1086×0.406 3 | 29.18 | 1057.92 | 0.028 | 0.56 | 4288.25 | 0.000 |
| L30 | $\begin{array}{r} 36.3333- \\ 35.3333(30) \end{array}$ | $\begin{gathered} \text { TP47.5162×45.6753×0.43 } \\ 75 \end{gathered}$ | 30.25 | 1163.95 | 0.026 | 0.63 | 4820.13 | 0.000 |
| L31 | $\begin{aligned} & 35.3333- \\ & 32.25(31) \end{aligned}$ | $\begin{gathered} \text { TP48.2565×47.5162×0.43 } \\ 75 \end{gathered}$ | 30.59 | 1182.26 | 0.026 | 0.63 | 4972.92 | 0.000 |
| L32 | $\begin{gathered} 32.25-32 \\ (32) \end{gathered}$ | $\begin{gathered} \text { TP48.3165×48.2565×0.43 } \\ 75 \end{gathered}$ | 30.61 | 1183.74 | 0.026 | 0.63 | 4985.42 | 0.000 |
| L33 | 32-27 (33) | $\begin{gathered} \text { TP49.5171×48.3165×0.43 } \\ 75 \end{gathered}$ | 31.15 | 1213.42 | 0.026 | 0.63 | 5238.56 | 0.000 |
| L34 | 27-22 (34) | $\begin{gathered} \text { TP50.7176×49.5171×0.43 } \\ 75 \end{gathered}$ | 31.68 | 1243.10 | 0.025 | 0.63 | 5497.98 | 0.000 |
| L35 | 22-17 (35) | $\begin{gathered} \text { TP51.9181×50.7176x0.43 } \\ 75 \end{gathered}$ | 32.22 | 1272.78 | 0.025 | 0.63 | 5763.67 | 0.000 |
| L36 | 17-15.5 (36) | $\begin{gathered} \text { TP52.2783×51.9181×0.43 } \\ 75 \end{gathered}$ | 32.40 | 1281.69 | 0.025 | 0.63 | 5844.59 | 0.000 |
| L37 | $\begin{gathered} 15.5-15.25 \\ (37) \end{gathered}$ | $\begin{gathered} \text { TP52.3383×52.2783×0.43 } \\ 75 \end{gathered}$ | 32.41 | 1283.17 | 0.025 | 0.63 | 5858.14 | 0.000 |
| L38 | 15.25-14.75 | TP52.4584×52.3383x0.43 | 32.47 | 1286.14 | 0.025 | 0.63 | 5885.27 | 0.000 |


| Section No. | Elevation ft | Size | Actual <br> $V_{u}$ <br> $K$ | $\begin{gathered} \phi V_{n} \\ K \end{gathered}$ | Ratio $V_{u}$ $\phi V_{n}$ | Actual $T_{u}$ kip-ft | $\phi T_{n}$ <br> kip-ft | Ratio $T_{u}$ $\qquad$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (38) | 75 |  |  |  |  |  |  |
| L39 | $\begin{gathered} 14.75-14.5 \\ (39) \end{gathered}$ | TP52.5184×52.4584×0.43 75 | 32.50 | 1287.63 | 0.025 | 0.63 | 5898.86 | 0.000 |
| L40 | 14.5-9.5 (40) | TP53.719x52.5184x0.437 5 | 33.06 | 1317.31 | 0.025 | 0.63 | 6173.95 | 0.000 |
| L41 | 9.5-4.5 (41) | TP54.9195 $\times 53.719 \times 0.437$ 5 | 33.46 | 1346.99 | 0.025 | 0.63 | 6455.31 | 0.000 |
| L42 | 4.5-0 (42) | TP56x54.9195x0.4375 | 33.82 | 1373.70 | 0.025 | 0.63 | 6713.89 | 0.000 |

## Pole Interaction Design Data

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Section No. \& Elevation
ft \& \[
\begin{gathered}
\hline \text { Ratio } \\
P_{u} \\
\hline \phi P_{n} \\
\hline
\end{gathered}
\] \& Ratio
\[
\frac{M_{u x}}{\phi M_{n x}}
\] \& Ratio
\[
\frac{M_{u y}}{\phi M_{n y}}
\] \& Ratio
\[
\begin{gathered}
V_{u} \\
\hline \phi V_{n}
\end{gathered}
\] \& Ratio
\[
\begin{gathered}
T_{u} \\
\hline \phi T_{n} \\
\hline
\end{gathered}
\] \& \begin{tabular}{l}
Comb. \\
Stress \\
Ratio
\end{tabular} \& \begin{tabular}{l}
Allow. \\
Stress Ratio
\end{tabular} \& Criteria \\
\hline L1 \& 160-155 (1) \& 0.003 \& 0.020 \& 0.000 \& 0.013 \& 0.001 \& 0.023 \& 1.050 \& 4.8.2 \\
\hline L2 \& 155-150 (2) \& 0.004 \& 0.058 \& 0.000 \& 0.016 \& 0.001 \& 0.063 \& 1.050 \& 4.8 .2 \\
\hline L3 \& 150-145 (3) \& 0.007 \& 0.135 \& 0.000 \& 0.031 \& 0.001 \& 0.143 \& 1.050 \& 4.8.2 \\
\hline L4 \& 145-140 (4) \& 0.007 \& 0.201 \& 0.000 \& 0.031 \& 0.001 \& 0.209 \& 1.050 \& 4.8.2 \\
\hline L5 \& 140-135 (5) \& 0.010 \& 0.304 \& 0.000 \& 0.045 \& 0.001 \& 0.316 \& 1.050 \& 4.8 .2 \\
\hline L6 \& 135-130 (6) \& 0.010 \& 0.388 \& 0.000 \& 0.044 \& 0.001 \& 0.400 \& 1.050 \& 4.8.2 \\
\hline L7 \& 130-125 (7) \& 0.010 \& 0.463 \& 0.000 \& 0.043 \& 0.001 \& 0.474 \& 1.050 \& 4.8.2 \\
\hline L8 \& 125-120 (8) \& 0.010 \& 0.530 \& 0.000 \& 0.043 \& 0.001 \& 0.542 \& 1.050 \& 4.8.2 \\
\hline L9 \& \[
\begin{gathered}
120-111.333 \\
(9)
\end{gathered}
\] \& 0.013 \& 0.588 \& 0.000 \& 0.051 \& 0.001 \& 0.603 \& 1.050 \& 4.8.2 \\
\hline L10 \& \[
\begin{gathered}
111.333-111 \\
(10)
\end{gathered}
\] \& 0.010 \& 0.438 \& 0.000 \& 0.037 \& 0.000 \& 0.449 \& 1.050 \& 4.8.2 \\
\hline L11 \& 111-106 (11) \& 0.010 \& 0.480 \& 0.000 \& 0.037 \& 0.000 \& 0.492 \& 1.050 \& 4.8.2 \\
\hline L12 \& 106-101 (12) \& 0.010 \& 0.519 \& 0.000 \& 0.036 \& 0.000 \& 0.530 \& 1.050 \& 4.8.2 \\
\hline L13 \& 101-96 (13) \& 0.010 \& 0.553 \& 0.000 \& 0.036 \& 0.000 \& 0.565 \& 1.050 \& 4.8 .2 \\
\hline L14 \& 96-91 (14) \& 0.010 \& 0.585 \& 0.000 \& 0.035 \& 0.000 \& 0.597 \& 1.050 \& 4.8.2 \\
\hline L15 \& 91-86 (15) \& 0.010 \& 0.615 \& 0.000 \& 0.035 \& 0.000 \& 0.626 \& 1.050 \& 4.8.2 \\
\hline L16 \& \[
\begin{gathered}
86-85.75 \\
(16)
\end{gathered}
\] \& 0.007 \& 0.383 \& 0.000 \& 0.023 \& 0.000 \& 0.390 \& 1.050 \& 4.8.2 \\
\hline L17 \& \[
\begin{gathered}
85.75-81 \\
(17)
\end{gathered}
\] \& 0.007 \& 0.398 \& 0.000 \& 0.023 \& 0.000 \& 0.406 \& 1.050 \& 4.8.2 \\
\hline L18 \& \[
\begin{gathered}
81-80.75 \\
(18)
\end{gathered}
\] \& 0.011 \& 0.644 \& 0.000 \& 0.034 \& 0.000 \& 0.656 \& 1.050 \& 4.8.2 \\
\hline L19 \& \[
\begin{gathered}
80.75-80.5 \\
(19)
\end{gathered}
\] \& 0.011 \& 0.645 \& 0.000 \& 0.034 \& 0.000 \& 0.657 \& 1.050 \& 4.8.2 \\
\hline L20 \& \[
\begin{gathered}
80.5-73.25 \\
(20)
\end{gathered}
\] \& 0.011 \& 0.653 \& 0.000 \& 0.034 \& 0.000 \& 0.665 \& 1.050 \& 4.8.2 \\
\hline L21 \& \begin{tabular}{l}
\[
73.25-72.25
\] \\
(21)
\end{tabular} \& 0.010 \& 0.560 \& 0.000 \& 0.029 \& 0.000 \& 0.571 \& 1.050 \& 4.8.2 \\
\hline L22 \& \[
\begin{gathered}
72.25-67.25 \\
(22)
\end{gathered}
\] \& 0.010 \& 0.577 \& 0.000 \& 0.029 \& 0.000 \& 0.588 \& 1.050 \& 4.8.2 \\
\hline L23 \& \[
\begin{gathered}
67.25-62.25 \\
(23)
\end{gathered}
\] \& 0.010 \& 0.593 \& 0.000 \& 0.029 \& 0.000 \& 0.604 \& 1.050 \& 4.8.2 \\
\hline L24 \& \[
\begin{gathered}
62.25-57.25 \\
(24)
\end{gathered}
\] \& 0.010 \& 0.608 \& 0.000 \& 0.028 \& 0.000 \& 0.619 \& 1.050 \& 4.8.2 \\
\hline L25 \& \[
\begin{gathered}
57.25-52.25 \\
(25)
\end{gathered}
\] \& 0.011 \& 0.622 \& 0.000 \& 0.028 \& 0.000 \& 0.634 \& 1.050 \& 4.8.2 \\
\hline L26 \& \[
\begin{gathered}
52.25-49.83 \\
(26)
\end{gathered}
\] \& 0.011 \& 0.629
0.630 \& 0.000 \& 0.028 \& 0.000 \& 0.641 \& 1.050

1.050 \& 4.8.2 <br>

\hline L27 \& $$
\begin{gathered}
49.83-49.58 \\
(27)
\end{gathered}
$$ \& 0.011 \& 0.630 \& 0.000 \& 0.028 \& 0.000 \& 0.641 \& 1.050 \& 4.8.2 <br>

\hline L28 \& $$
\begin{gathered}
49.58-44.58 \\
(28)
\end{gathered}
$$ \& 0.011 \& 0.643 \& 0.000 \& 0.028 \& 0.000 \& 0.655 \& 1.050 \& 4.8.2 <br>

\hline L29 \& $$
\begin{gathered}
44.58- \\
36.3333(29)
\end{gathered}
$$ \& 0.011 \& 0.647 \& 0.000 \& 0.028 \& 0.000 \& 0.659 \& 1.050 \& 4.8.2 <br>

\hline L30 \& $$
\begin{gathered}
36.3333- \\
35.3333(30)
\end{gathered}
$$ \& 0.011 \& 0.617 \& 0.000 \& 0.026 \& 0.000 \& 0.629 \& 1.050 \& 4.8.2 <br>

\hline L31 \& $$
\begin{aligned}
& 35.3333- \\
& 3275(31)
\end{aligned}
$$ \& 0.012 \& 0.623 \& 0.000 \& 0.026 \& 0.000 \& 0.635 \& 1.050 \& 4.8.2 <br>

\hline
\end{tabular}

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| Section No. | Elevation | Ratio $P_{u}$ | Ratio $M_{u x}$ | Ratio $M_{u y}$ | Ratio $V_{u}$ | Ratio $T_{u}$ | Comb. <br> Stress | Allow. <br> Stress | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $\phi P_{n}$ | ${ }_{\phi} M_{n x}$ | $\phi M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ | Ratio | Ratio |  |
| L32 | $\begin{gathered} 32.25-32 \\ (32) \end{gathered}$ | 0.012 | 0.624 | 0.000 | 0.026 | 0.000 | 0.636 | 1.050 | 4.8.2 |
| L33 | 32-27 (33) | 0.012 | 0.634 | 0.000 | 0.026 | 0.000 | 0.646 | 1.050 | 4.8.2 |
| L34 | 27-22 (34) | 0.012 | 0.644 | 0.000 | 0.025 | 0.000 | 0.656 | 1.050 | 4.8.2 |
| L35 | 22-17 (35) | 0.012 | 0.654 | 0.000 | 0.025 | 0.000 | 0.666 | 1.050 | 4.8.2 |
| L36 | 17-15.5 (36) | 0.012 | 0.656 | 0.000 | 0.025 | 0.000 | 0.669 | 1.050 | 4.8 .2 |
| L37 | $\begin{gathered} 15.5-15.25 \\ (37) \end{gathered}$ | 0.012 | 0.657 | 0.000 | 0.025 | 0.000 | 0.670 | 1.050 | 4.8.2 |
| L38 | $\begin{gathered} 15.25-14.75 \\ (38) \end{gathered}$ | 0.012 | 0.658 | 0.000 | 0.025 | 0.000 | 0.671 | 1.050 | 4.8.2 |
| L39 | $14.75-14.5$ <br> (39) | 0.012 | 0.658 | 0.000 | 0.025 | 0.000 | 0.671 | 1.050 | 4.8.2 |
| L40 | 14.5-9.5 (40) | 0.013 | 0.668 | 0.000 | 0.025 | 0.000 | 0.681 | 1.050 | 4.8.2 |
| L41 | 9.5-4.5 (41) | 0.013 | 0.677 | 0.000 | 0.025 | 0.000 | 0.691 | 1.050 | 4.8.2 |
| L42 | 4.5-0 (42) | 0.013 | 0.685 | 0.000 | 0.025 | 0.000 | 0.699 | 1.050 | 4.8.2 |

Section Capacity Table

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $ø P_{\text {allow }}$ K | \% <br> Capacity | $\begin{gathered} \text { Pass } \\ \text { Fail } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 160-155 | Pole | TP20.801x19.6x0.25 | 1 | -3.07 | 1016.19 | 2.2 | Pass |
| L2 | 155-150 | Pole | TP22.0021×20.801×0.25 | 2 | -4.00 | 1075.58 | 6.0 | Pass |
| L3 | 150-145 | Pole | TP23.2031x22.0021x0.25 | 3 | -7.66 | 1134.97 | 13.6 | Pass |
| L4 | 145-140 | Pole | TP24.4041×23.2031x0.25 | 4 | -8.12 | 1194.35 | 20.0 | Pass |
| L5 | 140-135 | Pole | TP25.6051x24.4041x0.25 | 5 | -11.57 | 1253.74 | 30.1 | Pass |
| L6 | 135-130 | Pole | TP26.8062x25.6051x0.25 | 6 | -12.22 | 1313.13 | 38.1 | Pass |
| L7 | 130-125 | Pole | TP28.0072x26.8062x0.25 | 7 | -12.89 | 1372.52 | 45.2 | Pass |
| L8 | 125-120 | Pole | TP29.2082x28.0072x0.25 | 8 | -13.59 | 1431.90 | 51.6 | Pass |
| L9 | 120-111.333 | Pole | TP31.29x29.2082x0.25 | 9 | -17.84 | 1479.41 | 57.5 | Pass |
| L10 | 111.333-111 | Pole | TP30.867x29.669x0.3438 | 10 | -19.24 | 2075.27 | 42.8 | Pass |
| L11 | 111-106 | Pole | TP32.065x30.867x0.3438 | 11 | -20.27 | 2156.72 | 46.8 | Pass |
| L12 | 106-101 | Pole | TP33.2631×32.065x0.3438 | 12 | -21.35 | 2238.18 | 50.5 | Pass |
| L13 | 101-96 | Pole | TP34.4611x33.2631x0.3438 | 13 | -22.45 | 2319.63 | 53.8 | Pass |
| L14 | 96-91 | Pole | TP35.6591×34.4611×0.3438 | 14 | -23.59 | 2401.08 | 56.8 | Pass |
| L15 | 91-86 | Pole | TP36.8571×35.6591×0.3438 | 15 | -24.76 | 2482.54 | 59.7 | Pass |
| L16 | 86-85.75 | Pole | TP36.917x36.8571x0.5125 | 16 | -24.84 | 3690.20 | 37.2 | Pass |
| L17 | 85.75-81 | Pole | TP38.0551×36.917x0.5063 | 17 | -26.33 | 3759.78 | 38.7 | Pass |
| L18 | 81-80.75 | Pole | TP38.115×38.0551×0.3438 | 18 | -26.41 | 2568.06 | 62.4 | Pass |
| L19 | 80.75-80.5 | Pole | TP38.1749x38.115x0.3438 | 19 | -26.48 | 2572.13 | 62.6 | Pass |
| L20 | 80.5-73.25 | Pole | TP39.912x38.1749x0.3438 | 20 | -26.86 | 2596.57 | 63.3 | Pass |
| L21 | 73.25-72.25 | Pole | TP39.467x37.8468x0.4063 | 21 | -29.78 | 3138.59 | 54.4 | Pass |
| L22 | 72.25-67.25 | Pole | TP40.6671×39.467x0.4063 | 22 | -31.18 | 3235.03 | 56.0 | Pass |
| L23 | 67.25-62.25 | Pole | TP41.8673x40.6671x0.4063 | 23 | -32.63 | 3331.46 | 57.5 | Pass |
| L24 | 62.25-57.25 | Pole | TP43.0674×41.8673x0.4063 | 24 | -34.12 | 3427.89 | 59.0 | Pass |
| L25 | 57.25-52.25 | Pole | TP44.2675x43.0674x0.4063 | 25 | -35.65 | 3524.32 | 60.4 | Pass |
| L26 | 52.25-49.83 | Pole | TP44.8484×44.2675x0.4063 | 26 | -36.57 | 3571.00 | 61.0 | Pass |
| L27 | 49.83-49.58 | Pole | TP44.9084×44.8484x0.4063 | 27 | -36.68 | 3575.82 | 61.1 | Pass |
| L28 | 49.58-44.58 | Pole | TP46.1086x44.9084x0.4063 | 28 | -38.60 | 3672.25 | 62.4 | Pass |
| L29 | 44.58-36.3333 | Pole | TP48.088x46.1086x0.4063 | 29 | -39.22 | 3702.73 | 62.8 | Pass |
| L30 | $\begin{gathered} 36.3333- \\ 35.3333 \end{gathered}$ | Pole | TP47.5162x45.6753x0.4375 | 30 | -44.06 | 4073.83 | 59.9 | Pass |
| L31 | 35.3333-32.25 | Pole | TP48.2565×47.5162x0.4375 | 31 | -45.35 | 4137.89 | 60.5 | Pass |
| L32 | 32.25-32 | Pole | TP48.3165×48.2565x0.4375 | 32 | -45.47 | 4143.09 | 60.6 | Pass |
| L33 | 32-27 | Pole | TP49.5171x48.3165×0.4375 | 33 | -47.60 | 4246.98 | 61.6 | Pass |
| L34 | 27-22 | Pole | TP50.7176x49.5171x0.4375 | 34 | -49.77 | 4350.86 | 62.5 | Pass |
| L35 | 22-17 | Pole | TP51.9181x50.7176x0.4375 | 35 | -51.97 | 4454.75 | 63.5 | Pass |
| L36 | 17-15.5 | Pole | TP52.2783x51.9181×0.4375 | 36 | -52.68 | 4485.91 | 63.8 | Pass |
| L37 | 15.5-15.25 | Pole | TP52.3383x52.2783x0.4375 | 37 | -52.82 | 4491.11 | 63.8 | Pass |
| L38 | 15.25-14.75 | Pole | TP52.4584×52.3383×0.4375 | 38 | -53.06 | 4501.50 | 63.9 | Pass |
| L39 | 14.75-14.5 | Pole | TP52.5184×52.4584x0.4375 | 39 | -53.18 | 4506.69 | 63.9 | Pass |
| L40 | 14.5-9.5 | Pole | TP53.719x52.5184x0.4375 | 40 | -55.42 | 4610.58 | 64.9 | Pass |
| L41 | 9.5-4.5 | Pole | TP54.9195x53.719x0.4375 | 41 | -57.53 | 4714.46 | 65.8 | Pass |

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160 Ft Monopole Tower Structural Analysis

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} \varnothing P_{\text {allow }} \\ K \end{gathered}$ | \% Capacity | $\begin{aligned} & \text { Pass } \\ & \text { Fail } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L42 | 4.5-0 | Pole | TP56x54.9195x0.4375 | 42 | -59.40 | $4807.96$ <br> Pole (L42) <br> RATING = | 66.6 Summary 66.6 66.6 | $\begin{aligned} & \text { Pass } \\ & \text { Pass } \\ & \text { Pass } \end{aligned}$ |

*NOTE: Above stress ratios for reinforced sections are approximate. More exact calculations are presented in Appendix C

## APPENDIX B

## BASE LEVEL DRAWING



## APPENDIX C

## ADDITIONAL CALCULATIONS



| Pole Geometry |  | Site BU: <br> Work Order: $\qquad$ 1747502 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |
|  | Pole Height Above Base (ft) | Section Length (ft) | Lap Splice Length <br> (ft) | Number of Sides | Top Diameter (in) | Bottom Diameter (in) | Wall Thickness (in) | Bend Radius (in) | Pole Material |
| 1 | 160 | 48.6667 | 4.6667 | 12 | 19.6 | 31.29 | 0.25 | Auto | A572-65 |
| 2 | 116 | 42.75 | 5.75 | 12 | 29.67 | 39.912 | 0.34375 | Auto | A572-65 |
| 3 | 79 | 42.6667 | 6.6667 | 12 | 37.85 | 48.088 | 0.40625 | Auto | A572-65 |
| 4 | 43 | 43 | 0 | 12 | 45.68 | 56 | 0.4375 | Auto | A572-65 |
|  |  |  |  |  |  |  |  |  |  |

Reinforcement Configuration

|  | $\begin{array}{c}\text { Bottom Effective } \\ \text { Elevation (ft) }\end{array}$ | $\begin{array}{c}\text { Top Effective } \\ \text { Elevation (ft) }\end{array}$ |
| ---: | :---: | :---: |
| 1 | 0 | 15.5 |
| 2 | 78.25 | 80.75 |
| 3 | 14.75 | 32.25 |
| 4 | 32.25 | 49.83 |
| 5 | 81 | 86 |
| 6 |  |  |
| 7 |  |  |
| 8 |  |  |
| 9 |  |  |
| 10 |  |  |

Reinforcement Details

|  | B (in) | H (in) | Gross Area ( $\mathrm{in}^{2}$ ) | Pole Face to Centroid (in) | Bottom Termination Length (in) | Top Termination Length (in) | $\mathrm{L}_{u}$ (in) | Net Area ( $\mathrm{in}^{2}$ ) | Bolt Hole Size (in) | Reinforcement Material |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4 | 0.75 | 3 | 0.375 | 15.000 | 15.000 | 15.000 | 2.063 | 1.1875 | A572-65 |
| 2 | 4 | 0.75 | 3 | 0.375 | 15.000 | 15.000 | 15.000 | 2.063 | 1.1875 | A572-65 |
| 3 | 6 | 1 | 6 | 0.5 | 30.000 | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |
| 4 | 6 | 1 | 6 | 0.5 | 30.000 | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |
| 5 | 6 | 1 | 6 | 0.5 | 30.000 | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |

## TNX Geometry Input

Increment (ft): 5

|  | Section | Height (ft) | Section Length (ft) | Lap Splice Length <br> (ft) | Number of Sides | Top Diameter (in) | Bottom Diameter (in) | Wall Thickness (in) | Tapered Pole Grade | Weight Multiplier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 160 | - 155 | 5 |  | 12 | 19.600 | 20.801 | 0.25 | A572-65 | 1.000 |
| 2 | 155 | - 150 | 5 |  | 12 | 20.801 | 22.002 | 0.25 | A572-65 | 1.000 |
| 3 | 150 | - 145 | 5 |  | 12 | 22.002 | 23.203 | 0.25 | A572-65 | 1.000 |
| 4 | 145 | - 140 | 5 |  | 12 | 23.203 | 24.404 | 0.25 | A572-65 | 1.000 |
| 5 | 140 | - 135 | 5 |  | 12 | 24.404 | 25.605 | 0.25 | A572-65 | 1.000 |
| 6 | 135 | - 130 | 5 |  | 12 | 25.605 | 26.806 | 0.25 | A572-65 | 1.000 |
| 7 | 130 | - 125 | 5 |  | 12 | 26.806 | 28.007 | 0.25 | A572-65 | 1.000 |
| 8 | 125 | - 120 | 5 |  | 12 | 28.007 | 29.208 | 0.25 | A572-65 | 1.000 |
| 9 | 120 | - 116 | 8.6667 | 4.6667 | 12 | 29.208 | 31.290 | 0.25 | A572-65 | 1.000 |
| 10 | 116 | - 111 | 5 |  | 12 | 29.669 | 30.867 | 0.34375 | A572-65 | 1.000 |
| 11 | 111 | - 106 | 5 |  | 12 | 30.867 | 32.065 | 0.34375 | A572-65 | 1.000 |
| 12 | 106 | - 101 | 5 |  | 12 | 32.065 | 33.263 | 0.34375 | A572-65 | 1.000 |
| 13 | 101 | - 96 | 5 |  | 12 | 33.263 | 34.461 | 0.34375 | A572-65 | 1.000 |
| 14 | 96 | - 91 | 5 |  | 12 | 34.461 | 35.659 | 0.34375 | A572-65 | 1.000 |
| 15 | 91 | - 86 | 5 |  | 12 | 35.659 | 36.857 | 0.34375 | A572-65 | 1.000 |
| 16 | 86 | - 85.75 | 0.25 |  | 12 | 36.857 | 36.917 | 0.5125 | A572-65 | 0.974 |
| 17 | 85.75 | - 81 | 4.75 |  | 12 | 36.917 | 38.055 | 0.50625 | A572-65 | 0.976 |
| 18 | 81 | - 80.75 | 0.25 |  | 12 | 38.055 | 38.115 | 0.34375 | A572-65 | 1.000 |
| 19 | 80.75 | - 80.5 | 0.25 |  | 12 | 38.115 | 38.175 | 0.34375 | A572-65 | 1.000 |
| 20 | 80.5 | - 79 | 7.25 | 5.75 | 12 | 38.175 | 39.912 | 0.34375 | A572-65 | 1.000 |
| 21 | 79 | - 72.25 | 6.75 |  | 12 | 37.847 | 39.467 | 0.40625 | A572-65 | 1.000 |
| 22 | 72.25 | - 67.25 | 5 |  | 12 | 39.467 | 40.667 | 0.40625 | A572-65 | 1.000 |
| 23 | 67.25 | - 62.25 | 5 |  | 12 | 40.667 | 41.867 | 0.40625 | A572-65 | 1.000 |
| 24 | 62.25 | - 57.25 | 5 |  | 12 | 41.867 | 43.067 | 0.40625 | A572-65 | 1.000 |
| 25 | 57.25 | - 52.25 | 5 |  | 12 | 43.067 | 44.268 | 0.40625 | A572-65 | 1.000 |
| 26 | 52.25 | - 49.83 | 2.42 |  | 12 | 44.268 | 44.848 | 0.40625 | A572-65 | 1.000 |
| 27 | 49.83 | - 49.58 | 0.25 |  | 12 | 44.848 | 44.908 | 0.40625 | A572-65 | 1.000 |
| 28 | 49.58 | - 44.58 | 5 |  | 12 | 44.908 | 46.109 | 0.40625 | A572-65 | 1.000 |
| 29 | 44.58 | - 43 | 8.2467 | 6.6667 | 12 | 46.109 | 48.088 | 0.40625 | A572-65 | 1.000 |
| 30 | 43 | - 35.3333 | 7.6667 |  | 12 | 45.675 | 47.516 | 0.4375 | A572-65 | 1.000 |
| 31 | 35.3333 | - 32.25 | 3.0833 |  | 12 | 47.516 | 48.256 | 0.4375 | A572-65 | 1.000 |
| 32 | 32.25 | - 32 | 0.25 |  | 12 | 48.256 | 48.317 | 0.4375 | A572-65 | 1.000 |
| 33 | 32 | - 27 | 5 |  | 12 | 48.317 | 49.517 | 0.4375 | A572-65 | 1.000 |
| 34 | 27 | - 22 | 5 |  | 12 | 49.517 | 50.718 | 0.4375 | A572-65 | 1.000 |
| 35 | 22 | - 17 | 5 |  | 12 | 50.718 | 51.918 | 0.4375 | A572-65 | 1.000 |
| 36 | 17 | - 15.5 | 1.5 |  | 12 | 51.918 | 52.278 | 0.4375 | A572-65 | 1.000 |
| 37 | 15.5 | - 15.25 | 0.25 |  | 12 | 52.278 | 52.338 | 0.4375 | A572-65 | 1.000 |
| 38 | 15.25 | - 14.75 | 0.5 |  | 12 | 52.338 | 52.458 | 0.4375 | A572-65 | 1.000 |
| 39 | 14.75 | - 14.5 | 0.25 |  | 12 | 52.458 | 52.518 | 0.4375 | A572-65 | 1.000 |
| 40 | 14.5 | - 9.5 | 5 |  | 12 | 52.518 | 53.719 | 0.4375 | A572-65 | 1.000 |
| 41 | 9.5 | - 4.5 | 5 |  | 12 | 53.719 | 54.920 | 0.4375 | A572-65 | 1.000 |
| 42 | 4.5 | - 0 | 4.5 |  | 12 | 54.920 | 56.000 | 0.4375 | A572-65 | 1.000 |

## TNX Section Forces



## Analysis Results

| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 160-155 | Pole | TP20.801x19.6x0.25 | Pole | 2.2\% | Pass |
| 155-150 | Pole | TP22.002x20.801x0.25 | Pole | 5.9\% | Pass |
| 150-145 | Pole | TP23.203x22.002x0.25 | Pole | 13.4\% | Pass |
| 145-140 | Pole | TP24.404x23.203x0.25 | Pole | 19.7\% | Pass |
| 140-135 | Pole | TP25.605x24.404x0.25 | Pole | 29.8\% | Pass |
| 135-130 | Pole | TP26.806x25.605x0.25 | Pole | 37.7\% | Pass |
| 130-125 | Pole | TP28.007x26.806x0.25 | Pole | 44.8\% | Pass |
| 125-120 | Pole | TP29.208x28.007x0.25 | Pole | 51.2\% | Pass |
| 120-116 | Pole | TP31.29x29.208x0.25 | Pole | 57.0\% | Pass |
| 116-111 | Pole | TP30.867x29.669x0.3438 | Pole | 42.4\% | Pass |
| 111-106 | Pole | TP32.065x30.867x0.3438 | Pole | 46.4\% | Pass |
| 106-101 | Pole | TP33.263x32.065x0.3438 | Pole | 50.1\% | Pass |
| 101-96 | Pole | TP34.461x33.263x0.3438 | Pole | 53.4\% | Pass |
| 96-91 | Pole | TP35.659x34.461x0.3438 | Pole | 56.5\% | Pass |
| 91-86 | Pole | TP36.857x35.659x0.3438 | Pole | 59.3\% | Pass |
| 86-85.75 | Pole + Reinf. | TP36.917x36.857x0.5125 | Reinf. 5 Tension Rupture | 56.6\% | Pass |
| 85.75-81 | Pole + Reinf. | TP38.055x36.917x0.5063 | Reinf. 5 Tension Rupture | 58.8\% | Pass |
| 81-80.75 | Pole | TP38.115x38.055x0.3438 | Pole | 62.1\% | Pass |
| 80.75-80.5 | Pole | TP38.175x38.115x0.3438 | Pole | 62.2\% | Pass |
| 80.5-79 | Pole | TP39.912x38.175x0.3438 | Pole | 63.0\% | Pass |
| 79-72.25 | Pole | TP39.467x37.847x0.4063 | Pole | 54.0\% | Pass |
| 72.25-67.25 | Pole | TP40.667x39.467x0.4063 | Pole | 55.6\% | Pass |
| 67.25-62.25 | Pole | TP41.867x40.667x0.4063 | Pole | 57.2\% | Pass |
| 62.25-57.25 | Pole | TP43.067x41.867x0.4063 | Pole | 58.6\% | Pass |
| 57.25-52.25 | Pole | TP44.268x43.067x0.4063 | Pole | 60.0\% | Pass |
| 52.25-49.83 | Pole | TP44.848x44.268x0.4063 | Pole | 60.7\% | Pass |
| 49.83-49.58 | Pole | TP44.908x44.848x0.4063 | Pole | 60.7\% | Pass |
| 49.58-44.58 | Pole | TP46.109x44.908x0.4063 | Pole | 62.1\% | Pass |
| 44.58-43 | Pole | TP48.088x46.109x0.4063 | Pole | 62.5\% | Pass |
| 43-35.33 | Pole | TP47.516x45.675x0.4375 | Pole | 59.5\% | Pass |
| 35.33-32.25 | Pole | TP48.256x47.516x0.4375 | Pole | 60.2\% | Pass |
| 32.25-32 | Pole | TP48.317x48.256x0.4375 | Pole | 60.2\% | Pass |
| 32-27 | Pole | TP49.517x48.317x0.4375 | Pole | 61.2\% | Pass |
| 27-22 | Pole | TP50.718x49.517x0.4375 | Pole | 62.2\% | Pass |
| 22-17 | Pole | TP51.918x50.718x0.4375 | Pole | 63.2\% | Pass |
| 17-15.5 | Pole | TP52.278x51.918x0.4375 | Pole | 63.4\% | Pass |
| 15.5-15.25 | Pole | TP52.338x52.278x0.4375 | Pole | 63.5\% | Pass |
| 15.25-14.75 | Pole | TP52.458x52.338x0.4375 | Pole | 63.6\% | Pass |
| 14.75-14.5 | Pole | TP52.518x52.458x0.4375 | Pole | 63.6\% | Pass |
| 14.5-9.5 | Pole | TP53.719x52.518x0.4375 | Pole | 64.6\% | Pass |
| 9.5-4.5 | Pole | TP54.92x53.719x0.4375 | Pole | 65.5\% | Pass |
| 4.5-0 | Pole | TP56x54.92x0.4375 | Pole | 66.3\% | Pass |
|  |  |  |  | Summary |  |
|  |  |  | Pole | 66.3\% | Pass |
|  |  |  | Reinforcement | 58.8\% | Pass |
|  |  |  | Overall | 66.3\% | Pass |

## Additional Calculations

|  | Moment of Inertia (in ${ }^{4}$ ) |  |  | Area (in ${ }^{2}$ ) |  |  | \% Capacity* |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pole | Reinf. | Total | Pole | Reinf. | Total | Pole | R1 | R2 | R3 | R4 | R5 |
| 160-155 | 893 | n/a | 893 | 16.52 | n/a | 16.52 | 2.2\% |  |  |  |  |  |
| 155-150 | 1059 | n/a | 1059 | 17.49 | n/a | 17.49 | 5.9\% |  |  |  |  |  |
| 150-145 | 1244 | n/a | 1244 | 18.45 | n/a | 18.45 | 13.4\% |  |  |  |  |  |
| 145-140 | 1450 | n/a | 1450 | 19.42 | n/a | 19.42 | 19.7\% |  |  |  |  |  |
| 140-135 | 1677 | n/a | 1677 | 20.38 | n/a | 20.38 | 29.8\% |  |  |  |  |  |
| 135-130 | 1927 | n/a | 1927 | 21.35 | n/a | 21.35 | 37.7\% |  |  |  |  |  |
| 130-125 | 2200 | n/a | 2200 | 22.31 | n/a | 22.31 | 44.8\% |  |  |  |  |  |
| 125-120 | 2499 | n/a | 2499 | 23.28 | n/a | 23.28 | 51.2\% |  |  |  |  |  |
| 120-116 | 2756 | n/a | 2756 | 24.05 | n/a | 24.05 | 57.0\% |  |  |  |  |  |
| 116-111 | 4023 | n/a | 4023 | 33.74 | n/a | 33.74 | 42.4\% |  |  |  |  |  |
| 111-106 | 4516 | n/a | 4516 | 35.06 | n/a | 35.06 | 46.4\% |  |  |  |  |  |
| 106-101 | 5047 | n/a | 5047 | 36.39 | n/a | 36.39 | 50.1\% |  |  |  |  |  |
| 101-96 | 5618 | n/a | 5618 | 37.71 | n/a | 37.71 | 53.4\% |  |  |  |  |  |
| 96-91 | 6231 | n/a | 6231 | 39.03 | n/a | 39.03 | 56.5\% |  |  |  |  |  |
| 91-86 | 6887 | n/a | 6887 | 40.36 | n/a | 40.36 | 59.3\% |  |  |  |  |  |
| 86-85.75 | 6921 | 3263 | 10183 | 40.42 | 18.00 | 58.42 | 39.1\% |  |  |  |  | 56.6\% |
| 85.75-81 | 7587 | 3460 | 11047 | 41.68 | 18.00 | 59.68 | 41.2\% |  |  |  |  | 58.8\% |
| 81-80.75 | 7623 | n/a | 7623 | 41.75 | n/a | 41.75 | 62.1\% |  |  |  |  |  |
| 80.75-80.5 | 7660 | n/a | 7660 | 41.81 | n/a | 41.81 | 62.2\% |  |  |  |  |  |
| 80.5-79 | 7880 | n/a | 7880 | 42.21 | n/a | 42.21 | 63.0\% |  |  |  |  |  |
| 79-72.25 | 9964 | n/a | 9964 | 51.02 | n/a | 51.02 | 54.0\% |  |  |  |  |  |
| 72.25-67.25 | 10911 | n/a | 10911 | 52.59 | n/a | 52.59 | 55.6\% |  |  |  |  |  |
| 67.25-62.25 | 11916 | n/a | 11916 | 54.16 | n/a | 54.16 | 57.2\% |  |  |  |  |  |
| 62.25-57.25 | 12981 | n/a | 12981 | 55.73 | n/a | 55.73 | 58.6\% |  |  |  |  |  |
| 57.25-52.25 | 14108 | n/a | 14108 | 57.29 | n/a | 57.29 | 60.0\% |  |  |  |  |  |
| 52.25-49.83 | 14676 | n/a | 14676 | 58.05 | n/a | 58.05 | 60.7\% |  |  |  |  |  |
| 49.83-49.58 | 14735 | n/a | 14735 | 58.13 | n/a | 58.13 | 60.7\% |  |  |  |  |  |
| 49.58-44.58 | 15960 | n/a | 15960 | 59.70 | n/a | 59.70 | 62.1\% |  |  |  |  |  |
| 44.58-43 | 16361 | n/a | 16361 | 60.19 | n/a | 60.19 | 62.5\% |  |  |  |  |  |
| 43-35.33 | 18788 | n/a | 18788 | 66.23 | n/a | 66.23 | 59.5\% |  |  |  |  |  |
| 35.33-32.25 | 19688 | n/a | 19688 | 67.27 | n/a | 67.27 | 60.2\% |  |  |  |  |  |
| 32.25-32 | 19762 | n/a | 19762 | 67.35 | n/a | 67.35 | 60.2\% |  |  |  |  |  |
| 32-27 | 21287 | n/a | 21287 | 69.04 | n/a | 69.04 | 61.2\% |  |  |  |  |  |
| 27-22 | 22887 | n/a | 22887 | 70.73 | n/a | 70.73 | 62.2\% |  |  |  |  |  |
| 22-17 | 24566 | n/a | 24566 | 72.42 | n/a | 72.42 | 63.2\% |  |  |  |  |  |
| 17-15.5 | 25085 | n/a | 25085 | 72.93 | n/a | 72.93 | 63.4\% |  |  |  |  |  |
| 15.5-15.25 | 25172 | n/a | 25172 | 73.01 | n/a | 73.01 | 63.5\% |  |  |  |  |  |
| 15.25-14.75 | 25348 | n/a | 25348 | 73.18 | n/a | 73.18 | 63.6\% |  |  |  |  |  |
| 14.75-14.5 | 25435 | n/a | 25435 | 73.26 | n/a | 73.26 | 63.6\% |  |  |  |  |  |
| 14.5-9.5 | 27235 | n/a | 27235 | 74.95 | n/a | 74.95 | 64.6\% |  |  |  |  |  |
| 9.5-4.5 | 29118 | n/a | 29118 | 76.64 | n/a | 76.64 | 65.5\% |  |  |  |  |  |
| 4.5-0 | 30885 | n/a | 30885 | 78.16 | n/a | 78.16 | 66.3\% |  |  |  |  |  |

Note: Section capacity checked in 5 degree increments.
Rating per TIA-222-H Section 15.5.

| Site Info |  |
| ---: | :---: |
| BU \# | 806953 |
| Site Name | BRG 2044 (A) 943097 |
| Order \# | 478803 Rev.0 |


| Analysis Considerations |  |
| ---: | :---: |
| TIA-222 Revision | H |
| Grout Considered: | No |
| $\mathrm{I}_{\mathrm{ar}}$ (in) | 1.0625 |


| $\|$Applied Loads  <br> Moment (kip-ft) 3758.83 <br> Axial Force (kips) 59.40 <br> Shear Force (kips) 33.82 |
| :--- |
| ${ }^{\text {TTIA-222-H Section 15.5 Applied }}$ |



| Connection Properties | Analysis Results |  |  |
| :---: | :---: | :---: | :---: |
| Anchor Rod Data | Anchor Rod Summary | (units of kips, kip-in) |  |
| (20) 2-1/4" $\varnothing$ bolts (A615-75 N; Fy=75 ksi, Fu=100 ksi) on 64.48" BC | Pu_c = 142.81 | фPn_c = 243.75 | Stress Rating |
|  | $\mathrm{Vu}=1.69$ | $\phi V n=73.13$ | 55.8\% |
| Base Plate Data | $\mathrm{Mu}=\mathrm{n} / \mathrm{a}$ | $\phi \mathrm{Mn}=\mathrm{n} / \mathrm{a}$ | Pass |
| 70.48" OD x 2.75" Plate (A633-60; Fy=60 ksi, Fu=80 ksi) |  |  |  |
|  | Base Plate Summary |  |  |
| Stiffener Data | Max Stress (ksi): | 22 | (Flexural) |
| N/A | Allowable Stress (ksi): | 54 |  |
|  | Stress Rating: | 38.8\% | Pass |
| Pole Data |  |  |  |
| $56 \mathrm{l} \times 0.4375$ " 12-sided pole (A572-65; Fy=65 ksi, Fu=80 ksi) |  |  |  |

## Pier and Pad Foundation

BU \# : 806953
Site Name: BRG 2044 (A) 943 App. Number: 479803 Rev. 0


| Top \& Bot. Pad Rein. Different?: | $\overline{/}$ |
| ---: | ---: |
| Block Foundation?: | $\sqrt{\boldsymbol{V}}$ |


| Superstructure Analysis Reactions |  |  |
| ---: | :---: | :--- |
| Compression, $\mathbf{P}_{\text {comp }}:$ | 59.4 | kips |
| Base Shear, Vu_comp: | 33.82 | kips |
|  |  |  |
| ${\text { Moment, } \mathbf{M}_{\mathbf{u}}:}$ | 3758.83 | ft -kips |
| Tower Height, H: | 160 | ft |
|  |  |  |
| Bolt Circle / Bearing Plate Width, BC: | 64.48 | in |


| Foundation Analysis Checks |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating $^{*}$ | Check |
|  |  |  |  |  |
| Lateral (Sliding) (kips) | 194.46 | 33.82 | $\mathbf{1 6 . 6 \%}$ | Pass |
| Bearing Pressure (ksf) | 30.34 | 2.27 | $\mathbf{7 . 5 \%}$ | Pass |
| Overturning (kip*t) | 6352.61 | 3944.84 | $\mathbf{6 2 . 1 \%}$ | Pass |
|  |  |  |  |  |
|  |  |  |  |  |
| Pad Flexure (kip*ft) | 8047.81 | 1757.30 | $\mathbf{2 0 . 8 \%}$ | Pass |
| Pad Shear - 2-way (Comp) (ksi) | 0.190 | 0.002 | $\mathbf{1 . 1 \%}$ | Pass |
| Flexural 2-way (Comp) (kip*t) | 6537.76 | 0.00 | $\mathbf{0 . 0 \%}$ | Pass |

*Rating per TIA-222-H Section
15.5

| Soil Rating*: | $\mathbf{6 2 . 1 \%}$ |
| ---: | ---: |
| Structural Rating* | $\mathbf{2 0 . 8 \%}$ |

Pad Properties

| Pad Properties |  |  |
| ---: | :---: | :--- |
| Depth, D: | 3.5 | ft |
| Pad Width, W: | 26 | ft |
| Pad Thickness, T: | 5 | ft |
| Pad Rebar Size (Top), $\mathbf{S p}_{\text {top }}:$ | 8 |  |
| Pad Top Rebar Quantity (Top), $\mathbf{m p}_{\text {top }}:$ | 18 |  |
| Pad Rebar Size (Bottom), Sp: | 10 |  |
| Pad Rebar Quantity (Bottom), mp: | 26 |  |
| Pad Clear Cover, $\mathbf{c c}$ | pad: $:$ | 3 |


| Material Properties |  |  |
| ---: | :---: | :--- |
| Rebar Grade, Fy: | 60 | ksi |
| Concrete Compressive Strength, F'c: | 4 | ksi |
| Dry Concrete Density, $\delta \mathbf{c}:$ | 150 | pcf |


| Soil Properties |  |  |
| ---: | :---: | :--- |
| Total Soil Unit Weight, $\gamma:$ | 130 | pcf |
| Ultimate Net Bearing, Qnet: | 40.000 | ksf |
| Cohesion, Cu: | 0.000 | ksf |
| Friction Angle, $\varphi:$ | 40 | degrees |
| SPT Blow Count, N blows: | 50 |  |
| Base Friction, $\mu:$ | 0.5 |  |
| Neglected Depth, N: | 3.33 | ft |
| Foundation Bearing on Rock? | No |  |
| Groundwater Depth, gw: | $\mathrm{N} / \mathrm{A}$ | ft |

AMERICAN SOCIETY OF CIVIL ENGINEERS
Address:
No Address at This Location

## ASCE 7 Hazards Report

Standard: ASCE/SEI 7-10 Elevation: 220 ft (NAVD 88)<br>Risk Category: II<br>Soil Class: D-Stiff Soil<br>Latitude: 41.101764<br>Longitude: -73.594847



Ultimate 3-second gust wind speed of 120 mph used per jurisdictional requirements.

AMERICAN SOCIETY OF CIVIL ENGINEERS

## Seismic

Site Soil Class:
D - Stiff Soil

## Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.253 |
| :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.07 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.598 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.4 |
| $\mathrm{~S}_{\mathrm{Ms}}:$ | 0.404 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.168 |


| $\mathrm{S}_{\mathrm{DS}}:$ | 0.269 |
| :--- | :--- |
| $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.112 |
| $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{PGA}:$ | 0.148 |
| $\mathrm{PGA}_{\mathrm{M}}:$ | 0.222 |
| $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.505 |
| $\mathrm{I}_{\mathrm{e}}:$ | 1 |

## Seismic Design Category <br> B




Data Accessed:
Date Source:

Wed Jun 262019
USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating
Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2.
Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.

## Ice

## Results

Ice Thickness:
Concurrent Temperature:
Gust Speed:
Data Source:
Date Accessed:
0.75 in.

15 F
50 mph
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Wed Jun 262019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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## Exhibit E

## Mount Analysis

Date: June 21, 2019
Charles McGuirt
Crown Castle
3530 Toringdon Way Suite 300
Charlotte, NC 28277
Subject:
Carrier Designation:

## Crown Castle Designation:

## Engineering Firm Designation:

Site Data:

Structure Information

## Mount Modification Analysis

T-Mobile Equipment Change-Out Carrier Site Number:

CT11071E Carrier Site Name:

Stamford/MP X32 / Den Rd.

## Crown Castle BU Number: <br> Crown Castle Site Name: Crown Castle JDE Number: Crown Castle Order Number:

806953
BRG 2044 (A) 943097
559199
479803 Revision 0
MasTec Networks Solutions Project Number: 18809-MOD1
69 Guinea Road (Camp Rocky Craig), Stamford, Fairfield County, CT Latitude: $41^{\circ \circ} 6^{\prime} 6.35^{\prime \prime}$ Longitude: $-73^{\circ} 35^{\prime} 41.45^{\prime \prime}$

Tower Height \& Type:
Mount Elevation:
Mount Width \& Type:
160 ft Monopole
116 ft
12 ft Platform Mount
Dear Charles McGuirt,
MasTec Network Solutions is pleased to submit this "Mount Modification Analysis Report" to determine the structural integrity of T-Mobile's antenna mounting system with the proposed appurtenance and equipment addition on the above mentioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point for fall protection or rigging is not part of this document.

The purpose of the analysis is to determine acceptability of the mount stress level. Based on our analysis we have determined the mount stress level to be:

## Platform Mount

## Sufficient Capacity

This analysis utilizes an ultimate 3-second gust wind speed of 120 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Mount analysis prepared by: NDN
Respectfully Submitted by:

Raphael I. Mohamed, PE, PEng
Senior Director of Engineering CT PE License No. 25112

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## 1) INTRODUCTION

This is a 12 ft Platform Mount mapped by Pier Structural Engineering Corp., dated April 15, 2019.

## 2) ANALYSIS CRITERIA

TIA-222 Revision:
Risk Category
Ultimate Wind Speed:
Exposure Category:
Topographic Category:
Ice Thickness:
Wind Speed with Ice:
Seismic Ss:
Seismic S1:
Live Loading Wind Speed:
Live Loading at Mid/End-Points:
Man Live Loading at Mount Pipes

TIA-222-H
II
120 mph
B
1
1.5 in

50 mph
0.253
0.07

30 mph
250 lb
500 lb

Table 1 - Proposed Loading Configuration

| Mount Centerline <br> (ft) | Antenna Centerline (ft) | $\begin{gathered} \begin{array}{c} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array} \end{gathered}$ | Antenna Manufacturer | Antenna Model | Mount / Modification Details |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 116 | 118 | 3 | Ericsson | AIR 21 B2A B4P | 12-ft Platform |
|  |  | 3 | Ericsson | AIR 32 B2A/B66AA |  |
|  |  | 3 | RFS | APXVAARR24_43-U-NA20 |  |
|  |  | 3 | Ericsson | Radio 4449 B12/B71 |  |
|  | 116 | 3 | Ericsson | KRY 112 144/1 |  |

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| 4-MOUNT ANALYSIS ORDER <br> INFORMATION | CROWN CASTLE | Order No. 479803 | CCIsites |
| 4-MOUNT ANALYSIS REPORT | MasTec | 8458758 | CCIsites |
| 4-MOUNT MAPPING | Pier Structural <br> Engineering Corp. | Project No. 19651-13 | On File |
| 4-MODIFICATION DRAWINGS | MasTec | Appendix E | On File |

## 3.1) Analysis Method

RISA-3D (Version 17.0.2), a commercially available analysis software package, was used to create a three-dimensional model of the antenna mounting system and calculate member stresses for various loading cases.

This analysis was performed in accordance with Crown Castle's ENG-SOW-10208 Tower Mount Analysis (Revision C).

## 3.2) Assumptions

1) The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specifications.
2) The configuration of antennas, mounts, and other appurtenances are as specified in Tables 1 and the referenced drawings.
3) All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
4) Steel grades have been assumed as follows, unless noted otherwise:

Channel, Solid Round, Angle, Plate ASTM A36 (GR 36)
HSS (Rectangular) ASTM 500 (GR B-46)
Pipe ASTM A53 (GR B-35)
Connection Bolts ASTM A325
This analysis may be affected if any assumptions are not valid or have been made in error. MasTec should be notified to determine the effect on the structural integrity of the antenna mounting system.

## 4) ANALYSIS RESULTS

Table 4- Mount Component Stresses vs. Capacity

| Notes | Component | Beam No. | Centerline (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Handrails | -- | 116 | 32.3 | Pass |
| 1 | Mount Pipe | -- |  | 29.4 | Pass |
| 1 | Support Angle 2 | -- |  | 15.5 | Pass |
| 1 | Support Angle 1 | -- |  | 30.7 | Pass |
| 1 | Frame Rail | -- |  | 47.5 | Pass |
| 1 | Arm | -- |  | 57.9 | Pass |
| 1 | Corner Angles | -- |  | 58.2 | Pass |
| 1 | Mount to Tower Connection | -- |  | 41.0 | Pass |


|  | Structure Rating (max from all components) $=$ |
| :--- | :--- |
| 58.2\% |  |

Notes:

1) See additional documentation in "Appendix C - Software Analysis Output" for calculations supporting the \% capacity consumed.

## 4.1) Recommendations

The mount has sufficient capacity to carry the proposed loading configuration. In order for the results of the analysis to be considered valid, the structural modifications listed below must be completed.

1. Handrail Kit

Engineering Detail Drawings have been provided in Appendix E- Mount Modification Drawings. Connection from the mount to the tower and local stresses on the tower are sufficient.

## APPENDIX A

## WIRE FRAME AND RENDERED MODELS



| MasTec |  | Render |
| :--- | :---: | :--- |
| NDN | 806953 - BRG 2044 (A) 943097 | June 20, 2019 at 12:53 PM |
| 18809-MOD1 |  | 806953. R3D |



| MasTec |  | Member Labels |
| :--- | :---: | :--- |
| NDN | 806953 - BRG 2044 (A) 943097 | June 20, 2019 at 12:53 PM |
| 18809-MOD1 |  | 806953. R3D |



| MasTec |  | Joint Labels |
| :--- | :---: | :--- |
| NDN | 806953 - BRG 2044 (A) 943097 | June 20, 2019 at 12:54 PM |
| 18809-MOD1 |  | 806953. R3D |



| MasTec |  | Shapes |
| :--- | :---: | :--- |
| NDN | 806953 - BRG 2044 (A) 943097 | June 20, 2019 at 12:54 PM |
| 18809-MOD1 |  | 806953. R3D |



Member Code Checks Displayed (Enveloped)
Envelope Only Solution

| MasTec |  | Unity Bending Check |
| :--- | :---: | :--- |
| NDN | 806953 - BRG 2044 (A) 943097 | June 20, 2019 at $12: 55$ PM |
| 18809-MOD1 |  | 806953. R3D |



Member Shear Checks Displayed (Enveloped)
Envelope Only Solution

| MasTec |  | Shear Check |
| :--- | :---: | :--- |
| NDN | 806953 - BRG 2044 (A) 943097 | June 20, 2019 at 12:56 PM |
| 18809-MOD1 |  | $806953 . R 3 D$ |

## APPENDIX B

SOFTWARE INPUT CALCULATIONS

## APPENDIX B

SOFTWARE INPUT CALCULATIONS
MasTec
$\square$




## APPENDIX C

## SOFTWARE ANALYSIS OUTPUT

## Hot Rolled Steel Properties

|  | Label | E [ksi] | G [ksi] | Nu | Therm (11E. | Density[k/ft. | Yield[ksi] | Ry | Fu[ksi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A992 | 29000 | 11154 | 3 | 65 | 49 | 50 | 1.1 | 65 | 1.1 |
| 2 | A36 Gr. 36 | 29000 | 11154 | 3 | . 65 | 49 | 36 | 1.5 | 58 | 1.2 |
| 3 | A572 Gr. 50 | 29000 | 11154 | 3 | 65 | 49 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr.B RND | 29000 | 11154 | 3 | 65 | 527 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | 3 | 65 | 527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | 3 | 65 | 49 | 35 | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | 3 | 65 | 49 | 50 | 1.4 | 65 | 1.3 |

## Hot Rolled Steel Section Sets

| Label |  | Type |  | Design List Material |  | Design R... A [in2] |  | lyy [in4] Izz [in4] |  | $J$ [in4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Corners | L2.5x2.5x4 | Beam | Single Angle | A36 Gr. 36 | Typical | 1.19 | 692 | 692 | 026 |
| 2 | Handrails | PIPE 2.0 | Beam | Pipe | A53 Gr.B | Typical | 1.02 | 627 | 627 | 1.25 |
| 3 | Mount Pipe | PIPE 2.0 | Column | Pipe | A53 Gr.B | Typical | 1.02 | 627 | 627 | 1.25 |
| 4 | Support Angle 2 | L3 $\times 1.75 \times 4$ | Beam | Single Angle | A36 Gr. 36 | Typical | 1.125 | 266 | 1.037 | 022 |
| 5 | Support Angle 1 | L2x2x3 | Beam | Single Angle | A36 Gr. 36 | Typical | 722 | 271 | 271 | 009 |
| 6 | Frame Rail | C5X6.7 | Beam | Channel | A36 Gr. 36 | Typical | 1.97 | 47 | 7.48 | 055 |
| 7 | Arm | HSS4X4X3 | Beam | Tube | A500 Gr... | Typical | 2.58 | 6.21 | 6.21 | 10 |
| 8 | Corner Angles | L2.5×2.5×4 | Beam | Single Angle | A36 Gr. 36 | Typical | 1.19 | 692 | 692 | 026 |

Joint Coordinates and Temperatures

|  | Label | $\mathrm{X}[\mathrm{ft}]$ | $\mathrm{Y}[\mathrm{ft}]$ | Z [ft] | Temp [F] | Detach From Diap... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | -0. | 0 | -1.726923 | 0 |  |
| 2 | N2 | -0. | 0 | -7.060256 | 0 |  |
| 3 | N3 | -1.495559 | 0 | 0.863462 | 0 |  |
| 4 | N4 | -6.114361 | 0 | 3.530128 | 0 |  |
| 5 | N5 | 1.495559 | 0 | 0.863462 | 0 |  |
| 6 | N6 | 6.114361 | 0 | 3.530128 | 0 |  |
| 7 | N7 | 0.229167 | 0 | -7.060256 | 0 |  |
| 8 | N8 | 6.228945 | 0 | 3.331664 | 0 |  |
| 9 | N9 | -0.229167 | 0 | -7.060256 | 0 |  |
| 10 | N10 | -6.228945 | 0 | 3.331664 | 0 |  |
| 11 | N11 | -5.999778 | 0 | 3.728592 | 0 |  |
| 12 | N12 | 5.999778 | 0 | 3.728592 | 0 |  |
| 13 | N13 | 1.166667 | 0 | -1.89359 | 0 |  |
| 14 | N14 | 2.700774 | 0 | -2.779307 | 0 |  |
| 15 | N15 | -1.166667 | 0 | -1.89359 | 0 |  |
| 16 | N16 | -2.700774 | 0 | -2.779307 | 0 |  |
| 17 | N17 | -1.056563 | 0 | 1.957158 | 0 |  |
| 18 | N18 | -1.056563 | 0 | 3.728592 | 0 |  |
| 19 | N19 | -2.22323 | 0 | -0.063568 | 0 |  |
| 20 | N20 | -3.757337 | 0 | -0.949285 | 0 |  |
| 21 | N21 | 2.22323 | 0 | -0.063568 | 0 |  |
| 22 | N22 | 3.757337 | 0 | -0.949285 | 0 |  |
| 23 | N23 | 1.056563 | 0 | 1.957158 | 0 |  |
| 24 | N24 | 1.056563 | 0 | 3.728592 | 0 |  |
| 25 | N25 | 5.666445 | 4.666667 | 3.728592 | 0 |  |
| 26 | N26 | 5.666445 | -1.666667 | 3.728592 | 0 |  |
| 27 | N27 | 2.249778 | 4 | 3.728592 | 0 |  |
| 28 | N28 | 2.249778 | -1 | 3.728592 | 0 |  |
| 29 | N29 | -5.666445 | 4 | 3.728592 | 0 |  |
| 30 | N30 | -5.666445 | -1 | 3.728592 | 0 |  |
| 31 | N31 | -2.249778 | 6.5 | 3.728592 | 0 |  |
| 32 | N32 | -2.249778 | -2.75 | 3.728592 | 0 |  |


|  | Label | X [ft] | Y [ft] | Z [ft] | Temp [F] | Detach From Diap... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 33 | N33 | 6.062278 | 4 | 3.042989 | 0 |  |
| 34 | N34 | 6.062278 | -1 | 3.042989 | 0 |  |
| 35 | N35 | 4.353945 | 6.5 | 0.084069 | 0 |  |
| 36 | N36 | 4.353945 | -2.75 | 0.084069 | 0 |  |
| 37 | N37 | 0.395833 | 4.666667 | -6.771581 | 0 |  |
| 38 | N38 | 0.395833 | -1.666667 | -6.771581 | 0 |  |
| 39 | N39 | 2.104167 | 4 | -3.812661 | 0 |  |
| 40 | N40 | 2.104167 | -1 | -3.812661 | 0 |  |
| 41 | N41 | -6.062278 | 4.666667 | 3.042989 | 0 |  |
| 42 | N42 | -6.062278 | -1.666667 | 3.042989 | 0 |  |
| 43 | N43 | -0.395833 | 4 | -6.771581 | 0 |  |
| 44 | N44 | -0.395833 | -1 | -6.771581 | 0 |  |
| 45 | N45 | -2.104167 | 6.5 | -3.812661 | 0 |  |
| 46 | N46 | -2.104167 | -2.75 | -3.812661 | 0 |  |
| 47 | N47 | -4.353945 | 4 | 0.084069 | 0 |  |
| 48 | N48 | -4.353945 | -1 | 0.084069 | 0 |  |
| 49 | N49 | -0. | 0 | -1.89359 | 0 |  |
| 50 | N50 | -1.639897 | 0 | 0.946795 | 0 |  |
| 51 | N51 | 1.639897 | 0 | 0.946795 | 0 |  |
| 52 | N52 | 6.062278 | 0 | 3.042989 | 0 |  |
| 53 | N53 | 4.353945 | 0 | 0.084069 | 0 |  |
| 54 | N54 | 0.395833 | 0 | -6.771581 | 0 |  |
| 55 | N55 | 2.104167 | 0 | -3.812661 | 0 |  |
| 56 | N56 | -6.062278 | 0 | 3.042989 | 0 |  |
| 57 | N57 | -0.395833 | 0 | -6.771581 | 0 |  |
| 58 | N58 | -2.104167 | 0 | -3.812661 | 0 |  |
| 59 | N59 | -4.353945 | 0 | 0.084069 | 0 |  |
| 60 | N60 | 5.666445 | 0 | 3.728592 | 0 |  |
| 61 | N61 | 2.249778 | 0 | 3.728592 | 0 |  |
| 62 | N62 | -5.666445 | 0 | 3.728592 | 0 |  |
| 63 | N63 | -2.249778 | 0 | 3.728592 | 0 |  |
| 64 | N64 | 0.229167 | 3 | -7.060256 | 0 |  |
| 65 | N65 | 6.228945 | 3 | 3.331664 | 0 |  |
| 66 | N66 | -0.229167 | 3 | -7.060256 | 0 |  |
| 67 | N67 | -6.228945 | 3 | 3.331664 | 0 |  |
| 68 | N68 | -5.999778 | 3 | 3.728592 | 0 |  |
| 69 | N69 | 5.999778 | 3 | 3.728592 | 0 |  |
| 70 | N70 | 5.666445 | 3 | 3.728592 |  |  |
| 71 | N71 | 2.249778 | 3 | 3.728592 | 0 |  |
| 72 | N72 | -5.666445 | 3 | 3.728592 | O |  |
| 73 | N73 | -2.249778 | 3 | 3.728592 | 0 |  |
| 74 | N74 | 6.062278 | 3 | 3.042989 | 0 |  |
| 75 | N75 | 4.353945 | 3 | 0.084069 | 0 |  |
| 76 | N76 | 0.395833 | 3 | -6.771581 | 0 |  |
| 77 | N77 | 2.104167 | 3 | -3.812661 | 0 |  |
| 78 | N78 | -6.062278 | 3 | 3.042989 | 0 |  |
| 79 | N79 | -0.395833 | 3 | -6.771581 | 0 |  |
| 80 | N80 | -2.104167 | 3 | -3.812661 | 0 |  |
| 81 | N81 | -4.353945 | 3 | 0.084069 | 0 |  |
| 82 | N82 | -1.999778 | 3 | 3.728592 | 0 |  |
| 83 | N83 | 1.999778 | 3 | 3.728592 | 0 |  |
| 84 | N84 | 4.228945 | 3 | -0.132438 | 0 |  |
| 85 | N85 | 2.229167 | 3 | -3.596155 | 0 |  |
| 86 | N86 | -2.229167 | 3 | -3.596155 | 0 |  |
| 87 | N87 | -4.228945 | 3 | -0.132438 | 0 |  |
| 88 | N88 | -4.999778 | 3 | 3.728592 | 0 |  |
| 89 | N89 | 4.999778 | 3 | 3.728592 | 0 |  |


|  | Label | X [ft] | Y [ftl | Z [ft] | Temp [F] | Detach From Diap... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90 | N90 | 5.728945 | 3 | 2.465639 | 0 |  |
| 91 | N91 | 0.729167 | 3 | -6.194231 | 0 |  |
| 92 | N92 | -0.729167 | 3 | -6.194231 | 0 |  |
| 93 | N93 | -5.728945 | 3 | 2.465639 | 0 |  |

## Joint Boundary Conditions

|  | Joint Label | X [k/in] | Y [k/in] | Z [k/in] | X Rot.[k-ft/rad] | Y Rot.[k-ft/rad] | Z Rot.[k-ft/rad] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N3 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 2 | N1 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 3 | N5 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |

## Member Primary Data

|  | Label | 1 Joint | $J$ Joint | K Joint | Rotate(deg) | Section/Shape | Type | Design List | Material | Design Rules |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | N1 | N2 |  | 180 | Arm | Beam | Tube | A500 Gr.B.. | Typical |
| 2 | M2 | N3 | N4 |  | 180 | Arm | Beam | Tube | A500 Gr.B... | Typical |
| 3 | M3 | N5 | N6 |  | 180 | Arm | Beam | Tube | A500 Gr.B. | Typical |
| 4 | M4 | N9 | N7 |  | 180 | RIGID | None | None | RIGID | Typical |
| 5 | M5 | N10 | N11 |  | 180 | RIGID | None | None | RIGID | Typical |
| 6 | M6 | N12 | N8 |  | 180 | RIGID | None | None | RIGID | Typical |
| 7 | M7 | N7 | N8 |  | 180 | Frame Rail | Beam | Channel | A36 Gr. 36 | Typical |
| 8 | M8 | N9 | N10 |  | 180 | Frame Rail | Beam | Channel | A36 Gr. 36 | Typical |
| 9 | M9 | N11 | N12 |  | 180 | Frame Rail | Beam | Channel | A36 Gr. 36 | Typical |
| 10 | M10 | N15 | N13 |  | 90 | Support Angle 1 | Beam | Single Angle | A36 Gr. 36 | Typical |
| 11 | M11 | N14 | N13 |  | 90 | Support Angle 2 | Beam | Single Angle | A36 Gr. 36 | Typical |
| 12 | M12 | N15 | N16 |  | 90 | Support Angle 2 | Beam | Single Angle | A36 Gr. 36 | Typical |
| 13 | M13 | N19 | N17 |  | 180 | Support Angle 1 | Beam | Single Angle | A36 Gr. 36 | Typical |
| 14 | M14 | N17 | N18 |  | 90 | Support Angle 2 | Beam | Single Angle | A36 Gr. 36 | Typical |
| 15 | M15 | N20 | N19 |  | 90 | Support Angle 2 | Beam | Single Angle | A36 Gr. 36 | Typical |
| 16 | M16 | N23 | N21 |  | 180 | Support Angle 1 | Beam | Single Angle | A36 Gr. 36 | Typical |
| 17 | M17 | N21 | N22 |  | 90 | Support Angle 2 | Beam | Single Angle | A36 Gr. 36 | Typical |
| 18 | M18 | N24 | N23 |  | 90 | Support Angle 2 | Beam | Single Angle | A36 Gr. 36 | Typical |
| 19 | M19 | N25 | N26 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 20 | M20 | N27 | N28 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 21 | M21 | N29 | N30 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 22 | M22 | N31 | N32 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 23 | M23 | N33 | N34 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 24 | M24 | N35 | N36 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 25 | M25 | N37 | N38 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 26 | M26 | N39 | N40 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 27 | M27 | N41 | N42 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 28 | M28 | N43 | N44 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 29 | M29 | N45 | N46 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 30 | M30 | N47 | N48 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 31 | M31 | N68 | N69 |  |  | Handrails | Beam | Pipe | A53 Gr.B | Typical |
| 32 | M32 | N65 | N64 |  |  | Handrails | Beam | Pipe | A53 Gr.B | Typical |
| 33 | M33 | N67 | N66 |  |  | Handrails | Beam | Pipe | A53 Gr.B | Typical |
| 34 | M37 | N88 | N93 |  | 90 | Corner Angles | Beam | Single Angle | A36 Gr. 36 | Typical |
| 35 | M38 | N92 | N91 |  | 90 | Corner Angles | Beam | Single Anale | A36 Gr. 36 | Typical |
| 36 | M39 | N89 | N90 |  | 180 | Corner Angles | Beam | Single Angle | A36 Gr. 36 | Typical |



|  | Joint Label | L.D.M | Direction | Magnitudel(k,k-ft). (in,rad). ( $\mathbf{k}^{\star} \mathrm{s}^{\wedge} 2 / f$.. |
| :---: | :---: | :---: | :---: | :---: |
| 1 | N63 | L | Y | -. 5 |

## Joint Loads and Enforced Displacements (BLC 43 : Man 2 (500 lbs))

| Joint Label |  |  | L,D,M | Direction |
| :---: | :---: | :---: | :---: | :---: |
| 1 | N53 | L | $Y$ | Magnitude[(k,k-ft), (in,rad), (k*s^2/f... |


|  | Joint Label | L.D.M | Direction | Magnitude[(k,k-ft), (in,rad). (k*s^2/f |
| :---: | :---: | :---: | :---: | :---: |
| 1 | N58 | L | Y | -. 5 |




| Joint Label |  | L,D,M | Direction | Magnitudel(k,k-ft), (in,rad), (k*s^2/f.. |
| :---: | :---: | :---: | :---: | :---: |
| 1 | N20 | L | Y | -. 25 |


| Member Point Loads (BLC 1: Dead) |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Label |  |  |  | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| 1 |  |  |  |  |  |  |


| Member Point Loads (BLC 2 : Ice Dead) |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Member Label |  |  | Direction | Magnitude[k,k-ftt] | Location[ft,\%] |
| 1 |  |  |  |  |  |

Member Point Loads (BLC 2 : Ice Dead) (Continued)

| Member Label |  |  |  |  |  | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | M30 | Y | -.169 | $\% 50$ |  |  |  |  |
| 11 | M25 | Y | -.452 | $\% 50$ |  |  |  |  |
| 12 | M25 | Y | -.046 | $\% 50$ |  |  |  |  |
| 13 | M23 | Y | -.156 | $\% 50$ |  |  |  |  |
| 14 | M23 | Y | -.01 | $\% 50$ |  |  |  |  |
| 15 | M26 | Y | -.169 |  |  |  |  |  |

## Member Point Loads (BLC 3 : Full Wind Antenna (0 Deg))

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | -. 327 | \%. 1 |
| 2 | M21 | Z | -. 099 | \%3.3 |
| 3 | M20 | Z | -. 105 | \%2.8 |
| 4 | M27 | Z | -. 19 | \%. 1 |
| 5 | M28 | Z | -. 077 | \%3.3 |
| 6 | M30 | Z | -. 083 | \%2.8 |
| 7 | M25 | Z | -. 19 | \%. 1 |
| 8 | M23 | Z | -. 077 | \%3.3 |
| 9 | M26 | Z | -. 083 | \%2.8 |
| 10 | M19 | Z | -. 327 | \%99.9 |
| 11 | M21 | Z | -. 099 | \%96.7 |
| 12 | M20 | Z | -. 105 | \%97.2 |
| 13 | M27 | Z | -. 19 | \%99.9 |
| 14 | M28 | Z | -. 077 | \%96.7 |
| 15 | M30 | Z | -. 083 | \%97.2 |
| 16 | M25 | Z | -. 19 | \%99.9 |
| 17 | M23 | Z | -. 077 | \%96.7 |
| 18 | M26 | Z | -. 083 | \%97.2 |

## Member Point Loads (BLC 4 : Full Wind Antenna (30 Deg))

|  | Member Label | Direction | Magnitude[k.k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | -. 244 | \%. 1 |
| 2 | M21 | Z | -. 079 | \%3.3 |
| 3 | M20 | Z | -. 085 | \%2.8 |
| 4 | M27 | Z | -. 124 | \%. 1 |
| 5 | M28 | Z | -. 06 | \%3.3 |
| 6 | M30 | Z | -. 066 | \%2.8 |
| 7 | M25 | Z | -. 244 | \%. 1 |
| 8 | M23 | Z | -. 079 | \%3.3 |
| 9 | M26 | Z | -. 085 | \%2.8 |
| 10 | M19 | Z | -. 244 | \%99.9 |
| 11 | M21 | Z | -. 079 | \%96.7 |
| 12 | M20 | Z | -. 085 | \%97.2 |
| 13 | M27 | Z | -. 124 | \%99.9 |
| 14 | M28 | Z | -. 06 | \%96.7 |
| 15 | M30 | Z | -. 066 | \%97.2 |
| 16 | M25 | Z | -. 244 | \%99.9 |
| 17 | M23 | Z | -. 079 | \%96.7 |
| 18 | M26 | Z | -. 085 | \%97.2 |
| 19 | M19 | X | 141 | \%. 1 |
| 20 | M19 | X | 005 | \%25 |
| 21 | M21 | X | 046 | \%3.3 |
| 22 | M21 | X | . 001 | \%50 |
| 23 | M20 | X | 049 | \%2.8 |
| 24 | M27 | X | 072 | \%. 1 |
| 25 | M27 | X | 019 | \%25 |
| 26 | M28 | X | 035 | \%3.3 |

Member Point Loads (BLC 4 : Full Wind Antenna (30 Deg)) (Continued)

| Member Label |  | Direction | Magnitudelk,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 27 | M28 | X | .003 | $\% 50$ |
| 28 | M30 | X | .038 | $\% 2.8$ |
| 29 | M25 | X | .141 | $\% .1$ |
| 30 | M25 | X | .005 | $\% 25$ |
| 31 | M23 | X | .046 | $\% 3.3$ |
| 32 | M23 | X | .001 | $\% 50$ |
| 33 | M26 | X | .049 | $\% 2.8$ |
| 34 | M19 | X | .141 | $\% 99.9$ |
| 35 | M21 | X | .046 | $\% 96.7$ |
| 36 | M20 | X | .049 | $\% 97.2$ |
| 37 | M27 | X | .072 | $\% 99.9$ |
| 38 | M28 | X | .035 | $\% 96.7$ |
| 39 | M30 | X | .038 | $\% 97.2$ |
| 40 | M25 | X | .141 | $\% 99.9$ |
| 41 | M23 | X | .046 | $\% 96.7$ |
| 42 | M26 | X | .049 | $\% 97.2$ |

## Member Point Loads (BLC 5 : Full Wind Antenna (60 Deg))

|  | Member Label | Direction | Magnitude[[,k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | -. 095 | \%. 1 |
| 2 | M21 | Z | -. 038 | \%3.3 |
| 3 | M20 | Z | -. 042 | \%2.8 |
| 4 | M27 | Z | -. 095 | \%. 1 |
| 5 | M28 | Z | -. 038 | \%3.3 |
| 6 | M30 | Z | -. 042 | \%2.8 |
| 7 | M25 | Z | -. 164 | \%. 1 |
| 8 | M23 | Z | -. 049 | \%3.3 |
| 9 | M26 | Z | -. 053 | \%2.8 |
| 10 | M19 | Z | -. 095 | \%99.9 |
| 11 | M21 | Z | -. 038 | \%96.7 |
| 12 | M20 | Z | -. 042 | \%97.2 |
| 13 | M27 | Z | -. 095 | \%99.9 |
| 14 | M28 | Z | -. 038 | \%96.7 |
| 15 | M30 | Z | -. 042 | \%97.2 |
| 16 | M25 | Z | -. 164 | \%99.9 |
| 17 | M23 | Z | -. 049 | \%96.7 |
| 18 | M26 | Z | -. 053 | \%97.2 |
| 19 | M19 | X | 164 | \%. 1 |
| 20 | M19 | X | . 024 | \%25 |
| 21 | M21 | X | . 066 | \%3.3 |
| 22 | M21 | X | . 004 | \%50 |
| 23 | M20 | X | . 072 | \%2.8 |
| 24 | M27 | X | 164 | \%. 1 |
| 25 | M27 | X | . 024 | \%25 |
| 26 | M28 | X | . 066 | \%3.3 |
| 27 | M28 | X | . 004 | \%50 |
| 28 | M30 | X | . 072 | \%2.8 |
| 29 | M25 | X | 283 | \%. 1 |
| 30 | M25 | X | 0 | \%25 |
| 31 | M23 | X | . 085 | \%3.3 |
| 32 | M23 | X | 0 | \%50 |
| 33 | M26 | X | . 091 | \%2.8 |
| 34 | M19 | X | 164 | \%99.9 |
| 35 | M21 | X | . 066 | \%96.7 |
| 36 | M20 | X | . 072 | \%97.2 |
| 37 | M27 | X | 164 | \%99.9 |

Member Point Loads (BLC 5 : Full Wind Antenna (60 Deg)) (Continued)

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: |
| 38 | M28 | X | 066 | \%96.7 |
| 39 | M30 | X | 072 | \%97.2 |
| 40 | M25 | X | 283 | \%99.9 |
| 41 | M23 | X | 085 | \%96.7 |
| 42 | M26 | X | 091 | \%97.2 |

## Member Point Loads (BLC 6 : Full Wind Antenna (90 Deg))

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | 0 | \%. 1 |
| 2 | M21 | Z | 0 | \%3.3 |
| 3 | M20 | Z | 0 | \%2.8 |
| 4 | M27 | Z | 0 | \%. 1 |
| 5 | M28 | Z | 0 | \%3.3 |
| 6 | M30 | Z | 0 | \%2.8 |
| 7 | M25 | Z | 0 | \%. 1 |
| 8 | M23 | Z | 0 | \%3.3 |
| 9 | M26 | Z | 0 | \%2.8 |
| 10 | M19 | Z | 0 | \%99.9 |
| 11 | M21 | Z | 0 | \%96.7 |
| 12 | M20 | Z | 0 | \%97.2 |
| 13 | M27 | Z | 0 | \%99.9 |
| 14 | M28 | Z | 0 | \%96.7 |
| 15 | M30 | Z | 0 | \%97.2 |
| 16 | M25 | Z | 0 | \%99.9 |
| 17 | M23 | Z | 0 | \%96.7 |
| 18 | M26 | Z | 0 | \%97.2 |
| 19 | M19 | X | 144 | \%. 1 |
| 20 | M19 | X | 037 | \%25 |
| 21 | M21 | X | 069 | \%3.3 |
| 22 | M21 | X | 006 | \%50 |
| 23 | M20 | X | 076 | \%2.8 |
| 24 | M27 | X | . 281 | \%. 1 |
| 25 | M27 | X | 009 | \%25 |
| 26 | M28 | X | . 091 | \%3.3 |
| 27 | M28 | X | . 001 | \%50 |
| 28 | M30 | X | 098 | \%2.8 |
| 29 | M25 | X | 281 | \%. 1 |
| 30 | M25 | X | . 009 | \%25 |
| 31 | M23 | X | . 091 | \%3.3 |
| 32 | M23 | X | . 001 | \%50 |
| 33 | M26 | X | . 098 | \%2.8 |
| 34 | M19 | X | 144 | \%99.9 |
| 35 | M21 | X | 069 | \%96.7 |
| 36 | M20 | X | . 076 | \%97.2 |
| 37 | M27 | X | 281 | \%99.9 |
| 38 | M28 | X | . 091 | \%96.7 |
| 39 | M30 | X | 098 | \%97.2 |
| 40 | M25 | X | 281 | \%99.9 |
| 41 | M23 | X | . 091 | \%96.7 |
| 42 | M26 | X | . 098 | \%97.2 |

Member Point Loads (BLC 7 : Full Wind Antenna (120 Deg))

| Member Label | Direction Magnitude[k,k-ft] | Location[ft,\%] |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M 19 | Z | .095 | $\% .1$ |
| 2 | M 21 | Z | .038 | $\% 3.3$ |
| 3 | M 20 | Z | .042 | $\% 2.8$ |

Member Point Loads (BLC 7 : Full Wind Antenna (120 Deg)) (Continued)

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 4 | M27 | Z | 164 | \%. 1 |
| 5 | M28 | Z | 049 | \%3.3 |
| 6 | M30 | Z | 053 | \%2.8 |
| 7 | M25 | Z | 095 | \%. 1 |
| 8 | M23 | Z | 038 | \%3.3 |
| 9 | M26 | Z | 042 | \%2.8 |
| 10 | M19 | Z | 095 | \%99.9 |
| 11 | M21 | Z | 038 | \%96.7 |
| 12 | M20 | Z | 042 | \%97.2 |
| 13 | M27 | Z | 164 | \%99.9 |
| 14 | M28 | Z | 049 | \%96.7 |
| 15 | M30 | Z | . 053 | \%97.2 |
| 16 | M25 | Z | 095 | \%99.9 |
| 17 | M23 | Z | . 038 | \%96.7 |
| 18 | M26 | Z | 042 | \%97.2 |
| 19 | M19 | X | 164 | \%. 1 |
| 20 | M19 | X | . 024 | \%25 |
| 21 | M21 | X | 066 | \%3.3 |
| 22 | M21 | X | 004 | \%50 |
| 23 | M20 | X | . 072 | \%2.8 |
| 24 | M27 | X | 283 | \%. 1 |
| 25 | M28 | X | . 085 | \%3.3 |
| 26 | M30 | X | . 091 | \%2.8 |
| 27 | M25 | X | 164 | \%. 1 |
| 28 | M25 | X | . 024 | \%25 |
| 29 | M23 | X | . 066 | \%3.3 |
| 30 | M23 | X | . 004 | \%50 |
| 31 | M26 | X | . 072 | \%2.8 |
| 32 | M19 | X | 164 | \%99.9 |
| 33 | M21 | X | . 066 | \%96.7 |
| 34 | M20 | X | . 072 | \%97.2 |
| 35 | M27 | X | 283 | \%99.9 |
| 36 | M28 | X | . 085 | \%96.7 |
| 37 | M30 | X | . 091 | \%97.2 |
| 38 | M25 | X | 164 | \%99.9 |
| 39 | M23 | X | . 066 | \%96.7 |
| 40 | M26 | X | 072 | \%97.2 |

## Member Point Loads (BLC 8 : Full Wind Antenna (150 Deg))

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | . 244 | \%. 1 |
| 2 | M21 | Z | 079 | \%3.3 |
| 3 | M20 | Z | 085 | \%2.8 |
| 4 | M27 | Z | 244 | \%. 1 |
| 5 | M28 | Z | 079 | \%3.3 |
| 6 | M30 | Z | 085 | \%2.8 |
| 7 | M25 | Z | 124 | \%. 1 |
| 8 | M23 | Z | . 06 | \%3.3 |
| 9 | M26 | Z | 066 | \%2.8 |
| 10 | M19 | Z | 244 | \%99.9 |
| 11 | M21 | Z | 079 | \%96.7 |
| 12 | M20 | Z | . 085 | \%97.2 |
| 13 | M27 | Z | 244 | \%99.9 |
| 14 | M28 | Z | . 079 | \%96.7 |
| 15 | M30 | Z | . 085 | \%97.2 |
| 16 | M25 | Z | 124 | \%99.9 |

Member Point Loads (BLC 8 : Full Wind Antenna (150 Deg)) (Continued)

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 17 | M23 | Z | . 06 | \%96.7 |
| 18 | M26 | Z | . 066 | \%97.2 |
| 19 | M19 | X | 141 | \%. 1 |
| 20 | M19 | X | . 005 | \%25 |
| 21 | M21 | X | 046 | \%3.3 |
| 22 | M21 | X | . 001 | \%50 |
| 23 | M20 | X | . 049 | \%2.8 |
| 24 | M27 | X | 141 | \%. 1 |
| 25 | M27 | X | . 005 | \%25 |
| 26 | M28 | X | 046 | \%3.3 |
| 27 | M28 | X | . 001 | \%50 |
| 28 | M30 | X | 049 | \%2.8 |
| 29 | M25 | X | . 072 | \%. 1 |
| 30 | M25 | X | . 019 | \%25 |
| 31 | M23 | X | . 035 | \%3.3 |
| 32 | M23 | X | . 003 | \%50 |
| 33 | M26 | X | . 038 | \%2.8 |
| 34 | M19 | X | . 141 | \%99.9 |
| 35 | M21 | X | . 046 | \%96.7 |
| 36 | M20 | X | . 049 | \%97.2 |
| 37 | M27 | X | . 141 | \%99.9 |
| 38 | M28 | X | . 046 | \%96.7 |
| 39 | M30 | X | . 049 | \%97.2 |
| 40 | M25 | X | . 072 | \%99.9 |
| 41 | M23 | X | . 035 | \%96.7 |
| 42 | M26 | X | . 038 | \%97.2 |

## Member Point Loads (BLC 15 : Ice Wind Antenna (0 Deq))

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | -. 066 | \%. 1 |
| 2 | M21 | Z | -. 023 | \%3.3 |
| 3 | M20 | Z | -. 024 | \%2.8 |
| 4 | M27 | Z | -. 042 | \%. 1 |
| 5 | M28 | Z | -. 019 | \%3.3 |
| 6 | M30 | Z | -. 02 | \%2.8 |
| 7 | M25 | Z | -. 042 | \%. 1 |
| 8 | M23 | Z | -. 019 | \%3.3 |
| 9 | M26 | Z | -. 02 | \%2.8 |
| 10 | M19 | Z | -. 066 | \%99.9 |
| 11 | M21 | Z | -. 023 | \%96.7 |
| 12 | M20 | Z | -. 024 | \%97.2 |
| 13 | M27 | Z | -. 042 | \%99.9 |
| 14 | M28 | Z | -. 019 | \%96.7 |
| 15 | M30 | Z | -. 02 | \%97.2 |
| 16 | M25 | Z | -. 042 | \%99.9 |
| 17 | M23 | Z | -. 019 | \%96.7 |
| 18 | M26 | Z | -. 02 | \%97.2 |

## Member Point Loads (BLC 16 : Ice Wind Antenna (30 Deg))

| Member Label | Direction | Magnitude[k.k-ft] | Location[ft,\%] |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | $Z$ | -.05 | $\% .1$ |
| 2 | M21 | $Z$ | -.018 | $\% 3.3$ |
| 3 | M20 | $Z$ | -.02 | $\% .8$ |
| 4 | M27 | $Z$ | -.029 | $\% 3.3$ |
| 5 | M28 | $Z$ | -.015 | $\% 2.8$ |
| 6 | M30 | $Z$ | -.016 |  |

Member Point Loads (BLC 16 : Ice Wind Antenna (30 Deg)) (Continued)

|  | Member Label | Directio | Magnitude[k,k-ft] | Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: |
| 7 | M25 | Z | -. 05 | \%. 1 |
| 8 | M23 | Z | -. 018 | \%3.3 |
| 9 | M26 | Z | -. 02 | \%2.8 |
| 10 | M19 | Z | -. 05 | \%99.9 |
| 11 | M21 | Z | -. 018 | \%96.7 |
| 12 | M20 | Z | -. 02 | \%97.2 |
| 13 | M27 | Z | -. 029 | \%99.9 |
| 14 | M28 | Z | -. 015 | \%96.7 |
| 15 | M30 | Z | -. 016 | \%97.2 |
| 16 | M25 | Z | -. 05 | \%99.9 |
| 17 | M23 | Z | -. 018 | \%96.7 |
| 18 | M26 | Z | -. 02 | \%97.2 |
| 19 | M19 | X | . 029 | \%. 1 |
| 20 | M19 | X | . 001 | \%25 |
| 21 | M21 | X | 011 | \%3.3 |
| 22 | M21 | X | 0 | \%50 |
| 23 | M20 | X | 011 | \%2.8 |
| 24 | M27 | X | . 017 | \%. 1 |
| 25 | M27 | X | 005 | \%25 |
| 26 | M28 | X | 009 | \%3.3 |
| 27 | M28 | X | 002 | \%50 |
| 28 | M30 | X | 009 | \%2.8 |
| 29 | M25 | X | 029 | \%. 1 |
| 30 | M25 | X | . 001 | \%25 |
| 31 | M23 | X | . 011 | \%3.3 |
| 32 | M23 | X | 0 | \%50 |
| 33 | M26 | X | . 011 | \%2.8 |
| 34 | M19 | X | 029 | \%99.9 |
| 35 | M21 | X | . 011 | \%96.7 |
| 36 | M20 | X | . 011 | \%97.2 |
| 37 | M27 | X | 017 | \%99.9 |
| 38 | M28 | X | 009 | \%96.7 |
| 39 | M30 | X | 009 | \%97.2 |
| 40 | M25 | X | 029 | \%99.9 |
| 41 | M23 | X | 011 | \%96.7 |
| 42 | M26 | X | 011 | \%97.2 |

Member Point Loads (BLC 17 : Ice Wind Antenna (60 Deg))

|  | Member Label | Direction | Magnitude[k,k-ft] | Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | -. 021 | \%. 1 |
| 2 | M21 | Z | -. 009 | \%3.3 |
| 3 | M20 | Z | -. 01 | \%2.8 |
| 4 | M27 | Z | -. 021 | \%. 1 |
| 5 | M28 | Z | -. 009 | \%3.3 |
| 6 | M30 | Z | -. 01 | \%2.8 |
| 7 | M25 | Z | -. 033 | \%. 1 |
| 8 | M23 | Z | -. 011 | \%3.3 |
| 9 | M26 | Z | -. 012 | \%2.8 |
| 10 | M19 | Z | -. 021 | \%99.9 |
| 11 | M21 | Z | -. 009 | \%96.7 |
| 12 | M20 | Z | -. 01 | \%97.2 |
| 13 | M27 | Z | -. 021 | \%99.9 |
| 14 | M28 | Z | -. 009 | \%96.7 |
| 15 | M30 | Z | -. 01 | \%97.2 |
| 16 | M25 | Z | -. 033 | \%99.9 |
| 17 | M23 | Z | -. 011 | \%96.7 |

Member Point Loads (BLC 17 : Ice Wind Antenna (60 Deg)) (Continued)

|  | Member Label | Direction | Magnitude[k, k -ft] | Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: |
| 18 | M26 | Z | -. 012 | \%97.2 |
| 19 | M19 | X | 036 | \%. 1 |
| 20 | M19 | X | . 007 | \%25 |
| 21 | M21 | X | 016 | \%3.3 |
| 22 | M21 | X | . 002 | \%50 |
| 23 | M20 | X | 017 | \%2.8 |
| 24 | M27 | X | 036 | \%. 1 |
| 25 | M27 | X | 007 | \%25 |
| 26 | M28 | X | 016 | \%3.3 |
| 27 | M28 | X | . 002 | \%50 |
| 28 | M30 | X | 017 | \%2.8 |
| 29 | M25 | X | 057 | \%. 1 |
| 30 | M25 | X | 0 | \%25 |
| 31 | M23 | X | 02 | \%3.3 |
| 32 | M23 | X | 0 | \%50 |
| 33 | M26 | X | 021 | \%2.8 |
| 34 | M19 | X | 036 | \%99.9 |
| 35 | M21 | X | 016 | \%96.7 |
| 36 | M20 | X | . 017 | \%97.2 |
| 37 | M27 | X | . 036 | \%99.9 |
| 38 | M28 | X | . 016 | \%96.7 |
| 39 | M30 | X | 017 | \%97.2 |
| 40 | M25 | X | 057 | \%99.9 |
| 41 | M23 | X | 02 | \%96.7 |
| 42 | M26 | X | . 021 | \%97.2 |

Member Point Loads (BLC 18 : Ice Wind Antenna (90 Deq))

|  | Member Label | Direction | Magnitude[k, k -ft] | Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | 0 | \%. 1 |
| 2 | M21 | Z | 0 | \%3.3 |
| 3 | M20 | Z | 0 | \%2.8 |
| 4 | M27 | Z | 0 | \%. 1 |
| 5 | M28 | Z | 0 | \%3.3 |
| 6 | M30 | Z | 0 | \%2.8 |
| 7 | M25 | Z | 0 | \%. 1 |
| 8 | M23 | Z | 0 | \%3.3 |
| 9 | M26 | Z | 0 | \%2.8 |
| 10 | M19 | Z | 0 | \%99.9 |
| 11 | M21 | Z | 0 | \%96.7 |
| 12 | M20 | Z | 0 | \%97.2 |
| 13 | M27 | Z | 0 | \%99.9 |
| 14 | M28 | Z | 0 | \%96.7 |
| 15 | M30 | Z | 0 | \%97.2 |
| 16 | M25 | Z | 0 | \%99.9 |
| 17 | M23 | Z | 0 | \%96.7 |
| 18 | M26 | Z | 0 | \%97.2 |
| 19 | M19 | X | 034 | \%. 1 |
| 20 | M19 | X | . 011 | \%25 |
| 21 | M21 | X | 017 | \%3.3 |
| 22 | M21 | X | . 003 | \%50 |
| 23 | M20 | X | 019 | \%2.8 |
| 24 | M27 | X | 058 | \%. 1 |
| 25 | M27 | X | 003 | \%25 |
| 26 | M28 | X | 021 | \%3.3 |
| 27 | M28 | X | . 001 | \%50 |
| 28 | M30 | X | 023 | \%2.8 |

Member Point Loads (BLC 18 : Ice Wind Antenna (90 Deg)) (Continued)

|  | Member Label | Direction | Magnitude[k.,k-tt] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 29 | M25 | X | . 058 | \%. 1 |
| 30 | M25 | X | . 003 | \%25 |
| 31 | M23 | X | . 021 | \%3.3 |
| 32 | M23 | X | . 001 | \%50 |
| 33 | M26 | X | . 023 | \%2.8 |
| 34 | M19 | X | . 034 | \%99.9 |
| 35 | M21 | X | 017 | \%96.7 |
| 36 | M20 | X | . 019 | \%97.2 |
| 37 | M27 | X | . 058 | \%99.9 |
| 38 | M28 | X | . 021 | \%96.7 |
| 39 | M30 | X | . 023 | \%97.2 |
| 40 | M25 | X | . 058 | \%99.9 |
| 41 | M23 | X | . 021 | \%96.7 |
| 42 | M26 | X | . 023 | \%97.2 |

Member Point Loads (BLC 19 : Ice Wind Antenna (120 Deg))

|  | Member Label | Direction | Magnitude[k, ,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | . 021 | \%. 1 |
| 2 | M21 | Z | 009 | \%3.3 |
| 3 | M20 | Z | 01 | \%2.8 |
| 4 | M27 | Z | . 033 | \%. 1 |
| 5 | M28 | Z | . 011 | \%3.3 |
| 6 | M30 | Z | . 012 | \%2.8 |
| 7 | M25 | Z | . 021 | \%. 1 |
| 8 | M23 | Z | . 009 | \%3.3 |
| 9 | M26 | Z | . 01 | \%2.8 |
| 10 | M19 | Z | 021 | \%99.9 |
| 11 | M21 | Z | . 009 | \%96.7 |
| 12 | M20 | Z | . 01 | \%97.2 |
| 13 | M27 | Z | . 033 | \%99.9 |
| 14 | M28 | Z | . 011 | \%96.7 |
| 15 | M30 | Z | . 012 | \%97.2 |
| 16 | M25 | Z | . 021 | \%99.9 |
| 17 | M23 | Z | . 009 | \%96.7 |
| 18 | M26 | Z | . 01 | \%97.2 |
| 19 | M19 | X | . 036 | \%. 1 |
| 20 | M19 | X | . 007 | \%25 |
| 21 | M21 | X | . 016 | \%3.3 |
| 22 | M21 | X | . 002 | \%50 |
| 23 | M20 | X | . 017 | \%2.8 |
| 24 | M27 | X | . 057 | \%. 1 |
| 25 | M28 | X | . 02 | \%3.3 |
| 26 | M30 | X | . 021 | \%2.8 |
| 27 | M25 | X | . 036 | \%. 1 |
| 28 | M25 | X | . 007 | \%25 |
| 29 | M23 | X | . 016 | \%3.3 |
| 30 | M23 | X | . 002 | \%50 |
| 31 | M26 | X | . 017 | \%2.8 |
| 32 | M19 | X | . 036 | \%99.9 |
| 33 | M21 | X | . 016 | \%96.7 |
| 34 | M20 | X | . 017 | \%97.2 |
| 35 | M27 | X | . 057 | \%99.9 |
| 36 | M28 | X | . 02 | \%96.7 |
| 37 | M30 | X | . 021 | \%97.2 |
| 38 | M25 | X | . 036 | \%99.9 |
| 39 | M23 | X | . 016 | \%96.7 |


| Member Label |  |  |  |  |  |  |  | Direction | Magnitudelk,k-ftl | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40 | M26 | X | .017 | $\% 97.2$ |  |  |  |  |  |  |

Member Point Loads (BLC 20 : Ice Wind Antenna (150 Deg))

|  | Member Label | Directi | Magnitude[k, k -ft] | Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | Z | . 05 | \%. 1 |
| 2 | M21 | Z | 009 | \%3.3 |
| 3 | M20 | Z | 01 | \%2.8 |
| 4 | M27 | Z | 033 | \%. 1 |
| 5 | M28 | Z | 011 | \%3.3 |
| 6 | M30 | Z | 012 | \%2.8 |
| 7 | M25 | Z | 021 | \%. 1 |
| 8 | M23 | Z | 009 | \%3.3 |
| 9 | M26 | Z | 01 | \%2.8 |
| 10 | M19 | Z | 05 | \%99.9 |
| 11 | M21 | Z | 009 | \%96.7 |
| 12 | M20 | Z | 01 | \%97.2 |
| 13 | M27 | Z | 033 | \%99.9 |
| 14 | M28 | Z | 011 | \%96.7 |
| 15 | M30 | Z | 012 | \%97.2 |
| 16 | M25 | Z | 021 | \%99.9 |
| 17 | M23 | Z | 009 | \%96.7 |
| 18 | M26 | Z | . 01 | \%97.2 |
| 19 | M19 | X | 029 | \%. 1 |
| 20 | M19 | X | 007 | \%25 |
| 21 | M21 | X | 016 | \%3.3 |
| 22 | M21 | X | 002 | \%50 |
| 23 | M20 | X | . 017 | \%2.8 |
| 24 | M27 | X | . 057 | \%. 1 |
| 25 | M28 | X | 02 | \%3.3 |
| 26 | M30 | X | 021 | \%2.8 |
| 27 | M25 | X | 036 | \%. 1 |
| 28 | M25 | X | . 007 | \%25 |
| 29 | M23 | X | . 016 | \%3.3 |
| 30 | M23 | X | 002 | \%50 |
| 31 | M26 | X | 017 | \%2.8 |
| 32 | M19 | X | . 029 | \%99.9 |
| 33 | M21 | X | . 016 | \%96.7 |
| 34 | M20 | X | . 017 | \%97.2 |
| 35 | M27 | X | . 057 | \%99.9 |
| 36 | M28 | X | 02 | \%96.7 |
| 37 | M30 | X | . 021 | \%97.2 |
| 38 | M25 | X | . 036 | \%99.9 |
| 39 | M23 | X | . 016 | \%96.7 |
| 40 | M26 | X | . 017 | \%97.2 |

## Member Point Loads (BLC 27 : Seismic Antenna (0 Deg))

| Member Label | Direction |  | Magnitude[k,k-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M 19 | Z | -.017 | $\% 50$ |
| 2 | M 19 | Z | -.01 | $\% 25$ |
| 3 | M 21 | Z | -.012 | $\% 50$ |
| 4 | M 21 | Z | -.001 | $\% 50$ |
| 5 | M 20 | Z | -.018 | $\% 50$ |
| 6 | M 27 | Z | -.017 | $\% 50$ |
| 7 | M 27 | Z | -.01 | $\% 25$ |
| 8 | M 28 | Z | -.012 | $\% 50$ |
| 9 | M 28 | Z | -.001 | $\% 50$ |

Member Point Loads (BLC 27 : Seismic Antenna (0 Deg)) (Continued)

| Member Label |  |  |  |  |  | Direction | Magnitude[k,k-ftl | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | M30 | $\mathbf{Z}$ | -.018 | $\% 50$ |  |  |  |  |
| 11 | M25 | $Z$ | -.017 | $\% 50$ |  |  |  |  |
| 13 | $M 25$ | $Z$ | -.01 | $\% 25$ |  |  |  |  |
| 14 | $M 23$ | $Z$ | -.012 | $\% 50$ |  |  |  |  |
| 15 | $M 23$ | $Z$ | -.001 | $\% 50$ |  |  |  |  |

## Member Point Loads (BLC 28 : Seismic Antenna (90 Deg))

| Member Label | Direction | Magnitude[k,k-ft] | Location[ft,\%] |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M19 | X | .017 | $\% 50$ |
| 2 | M 19 | X | .01 | $\% 25$ |
| 3 | M 21 | X | .012 | $\% 50$ |
| 4 | M 21 | X | .001 | $\% 50$ |
| 5 | M 20 | X | .018 | $\% 50$ |
| 6 | M 27 | X | .017 | $\% 50$ |
| 7 | M 27 | X | .01 | $\% 25$ |
| 8 | M 28 | X | .012 | $\% 50$ |
| 9 | M 28 | X | .001 | $\% 50$ |
| 10 | M 30 | X | .018 | $\% 50$ |
| 11 | M 25 | X | .017 | $\% 50$ |
| 12 | M 25 | X | .01 | $\% 25$ |
| 13 | M 23 | X | .012 | $\% 50$ |
| 14 | M 23 | X | .001 | $\% 50$ |
| 15 | M 26 | X | .018 | $\% 50$ |

Member Point Loads (BLC 41 : Seismic Vertical Antennas)

| Member Label |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M 19 | Y | Magnitude[k,k-ft] | Location[ft, \%] |
| 2 | M 19 | Y | -.026 | $\% 50$ |
| 3 | M 21 | Y | -.015 | $\% 25$ |
| 4 | M 21 | Y | -.018 | $\% 50$ |
| 5 | M 20 | Y | -.002 | $\% 50$ |
| 6 | M 27 | Y | -.026 | $\% 50$ |
| 7 | M 27 | Y | -.026 | $\% 50$ |
| 8 | M 28 | Y | -.015 | $\% 25$ |
| 9 | M 28 | Y | -.018 | $\% 50$ |
| 10 | M 30 | Y | -.002 | $\% 50$ |
| 11 | M 25 | Y | -.026 | $\% 50$ |
| 12 | M 25 | Y | -.026 | $\% 50$ |
| 13 | M 23 | Y | -.015 | $\% 25$ |
| 14 | M 23 | Y | -.018 | $\% 50$ |
| 15 | M 26 | Y | -.002 | $\% 50$ |

Member Distributed Loads (BLC 2 : Ice Dead)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/ft,F,ksf] | Start Location[ft,.. | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Y | -. 015 | -. 015 | 0 | \%100 |
| 2 | M2 | Y | -. 015 | -. 015 | 0 | \%100 |
| 3 | M3 | Y | -. 015 | -. 015 | 0 | \%100 |
| 4 | M4 | Y | -. 004 | -. 004 | 0 | \%100 |
| 5 | M5 | Y | -. 004 | -. 004 | 0 | \%100 |
| 6 | M6 | Y | -. 004 | -. 004 | 0 | \%100 |
| 7 | M7 | Y | -. 015 | -. 015 | 0 | \%100 |
| 8 | M8 | Y | -. 015 | -. 015 | 0 | \%100 |
| 9 | M9 | Y | -. 015 | -. 015 | 0 | \%100 |

Member Distributed Loads (BLC 2 : Ice Dead) (Continued)

|  | Member Label | Direction | Start Magnitudelk/ft.F. . ksfl | End Magnitude[kff.F. .ksfl | Start Locationft.. | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | M10 | Y | -. 009 | -. 009 | 0 | \%100 |
| 11 | M11 | Y | -. 011 | -. 011 | 0 | \%100 |
| 12 | M12 | Y | -. 011 | -. 011 | 0 | \%100 |
| 13 | M13 | Y | -. 009 | -. 009 | 0 | \%100 |
| 14 | M14 | Y | -. 011 | -. 011 | 0 | \%100 |
| 15 | M15 | Y | -. 011 | -. 011 | 0 | \%100 |
| 16 | M16 | Y | -. 009 | -. 009 | 0 | \%100 |
| 17 | M17 | Y | -. 011 | -. 011 | 0 | \%100 |
| 18 | M18 | Y | -. 011 | -. 011 | 0 | \%100 |
| 19 | M19 | Y | -. 008 | -. 008 | 0 | \%100 |
| 20 | M20 | Y | -. 008 | -. 008 | 0 | \%100 |
| 21 | M21 | Y | -. 008 | -. 008 | 0 | \%100 |
| 22 | M22 | Y | -. 008 | -. 008 | 0 | \%100 |
| 23 | M23 | Y | -. 008 | -. 008 | 0 | \%100 |
| 24 | M24 | Y | -. 008 | -. 008 | 0 | \%100 |
| 25 | M25 | Y | -. 008 | -. 008 | 0 | \%100 |
| 26 | M26 | Y | -. 008 | -. 008 | 0 | \%100 |
| 27 | M27 | Y | -. 008 | -. 008 | 0 | \%100 |
| 28 | M28 | Y | -. 008 | -. 008 | 0 | \%100 |
| 29 | M29 | Y | -. 008 | -. 008 | 0 | \%100 |
| 30 | M30 | Y | -. 008 | -. 008 | 0 | \%100 |
| 31 | M31 | Y | -. 008 | -. 008 | 0 | \%100 |
| 32 | M32 | Y | -. 008 | -. 008 | 0 | \%100 |
| 33 | M33 | Y | -. 008 | -. 008 | 0 | \%100 |
| 34 | M37 | Y | -. 011 | -. 011 | 0 | \%100 |
| 35 | M38 | Y | -. 011 | -. 011 | 0 | \%100 |
| 36 | M39 | Y | -. 011 | -. 011 | 0 | \%100 |

## Member Distributed Loads (BLC 9 : Full Wind Members (0 Deg))

|  | Member Label | Direction | Start Magnitude[l/ft.F. .ksf] | End Magnitude[l/fit.F.ksf] | Start Location[ft... | End Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | 0 | 0 | 0 | \%100 |
| 2 | M2 | Z | -. 016 | -. 016 | 0 | \%100 |
| 3 | M3 | Z | -. 016 | -. 016 | 0 | \%100 |
| 4 | M7 | Z | -. 007 | -. 007 | 0 | \%100 |
| 5 | M8 | Z | -. 007 | -. 007 | 0 | \%100 |
| 6 | M9 | Z | -. 027 | -. 027 | 0 | \%100 |
| 7 | M10 | Z | -. 011 | -. 011 | 0 | \%100 |
| 8 | M11 | Z | -. 012 | -. 012 | 0 | \%100 |
| 9 | M12 | Z | -. 012 | -. 012 | 0 | \%100 |
| 10 | M13 | Z | -. 003 | -. 003 | 0 | \%100 |
| 11 | M14 | Z | 0 | 0 | 0 | \%100 |
| 12 | M15 | Z | -. 012 | -. 012 | 0 | \%100 |
| 13 | M16 | Z | -. 003 | -. 003 | 0 | \%100 |
| 14 | M17 | Z | -. 012 | -. 012 | 0 | \%100 |
| 15 | M18 | Z | 0 | 0 | 0 | \%100 |
| 16 | M19 | Z | -. 008 | -. 008 | 0 | \%. 1 |
| 17 | M20 | Z | -. 008 | -. 008 | 0 | \%2.8 |
| 18 | M21 | Z | -. 008 | -. 008 | 0 | \%3.3 |
| 19 | M22 | Z | -. 008 | -. 008 | 0 | \%100 |
| 20 | M23 | Z | -. 008 | -. 008 | 0 | \%3.3 |
| 21 | M24 | Z | -. 008 | -. 008 | 0 | \%100 |
| 22 | M25 | Z | -. 008 | -. 008 | 0 | \%. 1 |
| 23 | M26 | Z | -. 008 | -. 008 | 0 | \%2.8 |
| 24 | M27 | Z | -. 008 | -. 008 | 0 | \%. 1 |
| 25 | M28 | Z | -. 008 | -. 008 | 0 | \%3.3 |
| 26 | M29 | Z | -. 008 | -. 008 | 0 | \%100 |

Company

Member Distributed Loads (BLC 9 : Full Wind Members (0 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/ft,F,ksf] | Start Location[ft, | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | M30 | Z | -. 008 | -. 008 | 0 | \%2.8 |
| 28 | M31 | Z | -. 008 | -. 008 | 0 | \%100 |
| 29 | M32 | Z | -. 002 | -. 002 | 0 | \%100 |
| 30 | M33 | Z | -. 002 | -. 002 | 0 | \%100 |
| 31 | M37 | Z | -. 003 | -. 003 | 0 | \%100 |
| 32 | M38 | Z | -. 013 | -. 013 | 0 | \%100 |
| 33 | M39 | Z | -. 003 | -. 003 | 0 | \%100 |
| 34 | M19 | Z | -. 008 | -. 008 | \%99.9 | \%100 |
| 35 | M20 | Z | -. 008 | -. 008 | \%97.2 | \%100 |
| 36 | M21 | Z | -. 008 | -. 008 | \%96.7 | \%100 |
| 37 | M23 | Z | -. 008 | -. 008 | \%96.7 | \%100 |
| 38 | M25 | Z | -. 008 | -. 008 | \%99.9 | \%100 |
| 39 | M26 | Z | -. 008 | -. 008 | \%97.2 | \%100 |
| 40 | M27 | Z | -. 008 | -. 008 | \%99.9 | \%100 |
| 41 | M28 | Z | -. 008 | -. 008 | \%96.7 | \%100 |
| 42 | M30 | Z | -. 008 | -. 008 | \%97.2 | \%100 |
| 43 | M1 | X | 0 | 0 | 0 | \%100 |
| 44 | M2 | X | 0 | 0 | 0 | \%100 |
| 45 | M3 | X | 0 | 0 | 0 | \%100 |
| 46 | M7 | X | 0 | 0 | 0 | \%100 |
| 47 | M8 | X | 0 | 0 | 0 | \%100 |
| 48 | M9 | X | 0 | 0 | 0 | \%100 |
| 49 | M10 | X | 0 | 0 | 0 | \%100 |
| 50 | M11 | X | 0 | 0 | 0 | \%100 |
| 51 | M12 | X | 0 | 0 | 0 | \%100 |
| 52 | M13 | X | 0 | 0 | 0 | \%100 |
| 53 | M14 | X | 0 | 0 | 0 | \%100 |
| 54 | M15 | X | 0 | 0 | 0 | \%100 |
| 55 | M16 | X | 0 | 0 | 0 | \%100 |
| 56 | M17 | X | 0 | 0 | 0 | \%100 |
| 57 | M18 | X | 0 | 0 | 0 | \%100 |
| 58 | M19 | X | 0 | 0 | 0 | \%100 |
| 59 | M20 | X | 0 | 0 | 0 | \%100 |
| 60 | M21 | X | 0 | 0 | 0 | \%100 |
| 61 | M22 | X | 0 | 0 | 0 | \%100 |
| 62 | M23 | X | 0 | 0 | 0 | \%3.3 |
| 63 | M24 | X | 0 | 0 | 0 | \%100 |
| 64 | M25 | X | 0 | 0 | 0 | \%. 1 |
| 65 | M26 | X | 0 | 0 | 0 | \%2.8 |
| 66 | M27 | X | 0 | 0 | 0 | \%. 1 |
| 67 | M28 | X | 0 | 0 | 0 | \%3.3 |
| 68 | M29 | X | 0 | 0 | 0 | \%100 |
| 69 | M30 | X | 0 | 0 | 0 | \%2.8 |
| 70 | M31 | X | 0 | 0 | 0 | \%100 |
| 71 | M32 | X | 0 | 0 | 0 | \%100 |
| 72 | M33 | X | 0 | 0 | 0 | \%100 |
| 73 | M37 | X | 0 | 0 | 0 | \%100 |
| 74 | M38 | X | 0 | 0 | 0 | \%100 |
| 75 | M39 | X | 0 | 0 | 0 | \%100 |
| 76 | M23 | X | 0 | 0 | \%96.7 | \%100 |
| 77 | M25 | X | 0 | 0 | \%99.9 | \%100 |
| 78 | M26 | X | 0 | 0 | \%97.2 | \%100 |
| 79 | M27 | X | 0 | 0 | \%99.9 | \%100 |
| 80 | M28 | X | 0 | 0 | \%96.7 | \%100 |
| 81 | M30 | X | 0 | 0 | \%97.2 | \%100 |

Company

Member Distributed Loads (BLC 10 : Full Wind Members (30 Deg))

|  | Member Label | Direction | Start Magnitude[k/ft,F, ksf] | End Magnitude[kflt, F.ksf] | Start Location[ft, | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | -. 005 | -. 005 | 0 | \%100 |
| 2 | M2 | Z | -. 005 | -. 005 | 0 | \%100 |
| 3 | M3 | Z | -. 019 | -. 019 | 0 | \%100 |
| 4 | M7 | Z | -. 018 | -. 018 | 0 | \%100 |
| 5 | M8 | Z | 0 | 0 | 0 | \%100 |
| 6 | M9 | Z | -. 018 | -. 018 | 0 | \%100 |
| 7 | M10 | Z | -. 007 | -. 007 | 0 | \%100 |
| 8 | M11 | Z | -. 004 | -. 004 | 0 | \%100 |
| 9 | M12 | Z | -. 014 | -. 014 | 0 | \%100 |
| 10 | M13 | Z | -. 007 | -. 007 | 0 | \%100 |
| 11 | M14 | Z | -. 004 | -. 004 | 0 | \%100 |
| 12 | M15 | Z | -. 014 | -. 014 | 0 | \%100 |
| 13 | M16 | Z | 0 | 0 | 0 | \%100 |
| 14 | M17 | Z | -. 004 | -. 004 | 0 | \%100 |
| 15 | M18 | Z | -. 004 | -. 004 | 0 | \%100 |
| 16 | M19 | Z | -. 007 | -. 007 | 0 | \%. 1 |
| 17 | M20 | Z | -. 007 | -. 007 | 0 | \%2.8 |
| 18 | M21 | Z | -. 007 | -. 007 | 0 | \%3.3 |
| 19 | M22 | Z | -. 007 | -. 007 | 0 | \%100 |
| 20 | M23 | Z | -. 007 | -. 007 | 0 | \%3.3 |
| 21 | M24 | Z | -. 007 | -. 007 | 0 | \%100 |
| 22 | M25 | Z | -. 007 | -. 007 | 0 | \%. 1 |
| 23 | M26 | Z | -. 007 | -. 007 | 0 | \%2.8 |
| 24 | M27 | Z | -. 007 | -. 007 | 0 | \%. 1 |
| 25 | M28 | Z | -. 007 | -. 007 | 0 | \%3.3 |
| 26 | M29 | Z | -. 007 | -. 007 | 0 | \%100 |
| 27 | M30 | Z | -. 007 | -. 007 | 0 | \%2.8 |
| 28 | M31 | Z | -. 005 | -. 005 | 0 | \%100 |
| 29 | M32 | Z | -. 005 | -. 005 | 0 | \%100 |
| 30 | M33 | Z | 0 | 0 | 0 | \%100 |
| 31 | M37 | Z | -. 009 | -. 009 | 0 | \%100 |
| 32 | M38 | Z | -. 009 | -. 009 | 0 | \%100 |
| 33 | M39 | Z | 0 | 0 | 0 | \%100 |
| 34 | M19 | Z | -. 007 | -. 007 | \%99.9 | \%100 |
| 35 | M20 | Z | -. 007 | -. 007 | \%97.2 | \%100 |
| 36 | M21 | Z | -. 007 | -. 007 | \%96.7 | \%100 |
| 37 | M23 | Z | -. 007 | -. 007 | \%96.7 | \%100 |
| 38 | M25 | Z | -. 007 | -. 007 | \%99.9 | \%100 |
| 39 | M26 | Z | -. 007 | -. 007 | \%97.2 | \%100 |
| 40 | M27 | Z | -. 007 | -. 007 | \%99.9 | \%100 |
| 41 | M28 | Z | -. 007 | -. 007 | \%96.7 | \%100 |
| 42 | M30 | Z | -. 007 | -. 007 | \%97.2 | \%100 |
| 43 | M1 | X | . 003 | . 003 | 0 | \%100 |
| 44 | M2 | X | . 003 | . 003 | 0 | \%100 |
| 45 | M3 | X | . 011 | . 011 | 0 | \%100 |
| 46 | M7 | X | . 01 | . 01 | 0 | \%100 |
| 47 | M8 | X | 0 | 0 | 0 | \%100 |
| 48 | M9 | X | . 01 | 01 | 0 | \%100 |
| 49 | M10 | X | . 004 | . 004 | 0 | \%100 |
| 50 | M11 | X | . 002 | . 002 | 0 | \%100 |
| 51 | M12 | X | . 008 | . 008 | 0 | \%100 |
| 52 | M13 | X | . 004 | 004 | 0 | \%100 |
| 53 | M14 | X | . 002 | . 002 | 0 | \%100 |
| 54 | M15 | X | . 008 | . 008 | 0 | \%100 |
| 55 | M16 | X | 0 | 0 | 0 | \%100 |
| 56 | M17 | X | 002 | 002 | 0 | \%100 |
| 57 | M18 | X | . 002 | . 002 | 0 | \%100 |

Member Distributed Loads (BLC 10 : Full Wind Members (30 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F.ksfl | End Magnitude[k/ft,F.ksfl | Start Locationfft... | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 58 | M19 | X | 004 | 004 | 0 | \%100 |
| 59 | M20 | X | 004 | 004 | 0 | \%100 |
| 60 | M21 | X | 004 | 004 | 0 | \%100 |
| 61 | M22 | X | 004 | 004 | 0 | \%100 |
| 62 | M23 | X | 004 | 004 | 0 | \%3.3 |
| 63 | M24 | X | 004 | 004 | 0 | \%100 |
| 64 | M25 | X | 004 | 004 | 0 | \%. 1 |
| 65 | M26 | X | 004 | 004 | 0 | \%2.8 |
| 66 | M27 | X | 004 | 004 | 0 | \%. 1 |
| 67 | M28 | X | 004 | 004 | 0 | \%3.3 |
| 68 | M29 | X | 004 | 004 | 0 | \%100 |
| 69 | M30 | X | 004 | 004 | 0 | \%2.8 |
| 70 | M31 | X | 003 | 003 | 0 | \%100 |
| 71 | M32 | X | 003 | 003 | 0 | \%100 |
| 72 | M33 | X | 0 | 0 | 0 | \%100 |
| 73 | M37 | X | . 005 | . 005 | 0 | \%100 |
| 74 | M38 | X | 005 | . 005 | 0 | \%100 |
| 75 | M39 | X | 0 | 0 | 0 | \%100 |
| 76 | M23 | X | . 004 | 004 | \%96.7 | \%100 |
| 77 | M25 | X | . 004 | 004 | \%99.9 | \%100 |
| 78 | M26 | X | . 004 | . 004 | \%97.2 | \%100 |
| 79 | M27 | X | . 004 | . 004 | \%99.9 | \%100 |
| 80 | M28 | X | 004 | 004 | \%96.7 | \%100 |
| 81 | M30 | X | . 004 | 004 | \%97.2 | \%100 |

## Member Distributed Loads (BLC 11 : Full Wind Members (60 Deg))

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/ft,F,ksf] | Start Location[ft,.. | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | -. 008 | -. 008 | 0 | \%100 |
| 2 | M2 | Z | 0 | 0 | 0 | \%100 |
| 3 | M3 | Z | -. 008 | -. 008 | 0 | \%100 |
| 4 | M7 | Z | -. 013 | -. 013 | 0 | \%100 |
| 5 | M8 | Z | -. 003 | -. 003 | 0 | \%100 |
| 6 | M9 | Z | -. 003 | -. 003 | 0 | \%100 |
| 7 | M10 | Z | -. 001 | -. 001 | 0 | \%100 |
| 8 | M11 | Z | 0 | 0 | 0 | \%100 |
| 9 | M12 | Z | -. 006 | -. 006 | 0 | \%100 |
| 10 | M13 | Z | -. 005 | -. 005 | 0 | \%100 |
| 11 | M14 | Z | -. 006 | -. 006 | 0 | \%100 |
| 12 | M15 | Z | -. 006 | -. 006 | 0 | \%100 |
| 13 | M16 | Z | -. 001 | -. 001 | 0 | \%100 |
| 14 | M17 | Z | 0 | 0 | 0 | \%100 |
| 15 | M18 | Z | -. 006 | -. 006 | 0 | \%100 |
| 16 | M19 | Z | -. 004 | -. 004 | 0 | \%. 1 |
| 17 | M20 | Z | -. 004 | -. 004 | 0 | \%2.8 |
| 18 | M21 | Z | -. 004 | -. 004 | 0 | \%3.3 |
| 19 | M22 | Z | -. 004 | -. 004 | 0 | \%100 |
| 20 | M23 | Z | -. 004 | -. 004 | 0 | \%3.3 |
| 21 | M24 | Z | -. 004 | -. 004 | 0 | \%100 |
| 22 | M25 | Z | -. 004 | -. 004 | 0 | \%. 1 |
| 23 | M26 | Z | -. 004 | -. 004 | 0 | \%2.8 |
| 24 | M27 | Z | -. 004 | -. 004 | 0 | \%. 1 |
| 25 | M28 | Z | -. 004 | -. 004 | 0 | \%3.3 |
| 26 | M29 | Z | -. 004 | -. 004 | 0 | \%100 |
| 27 | M30 | Z | -. 004 | -. 004 | 0 | \%2.8 |
| 28 | M31 | Z | -. 001 | -. 001 | 0 | \%100 |
| 29 | M32 | Z | -. 004 | -. 004 | 0 | \%100 |

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Member Distributed Loads (BLC 11 : Full Wind Members (60 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksfl | End Magnitude[k/ft,F.ksfl | Start Locationfft, | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | M33 | Z | -. 001 | -. 001 | 0 | \%100 |
| 31 | M37 | Z | -. 007 | -. 007 | 0 | \%100 |
| 32 | M38 | Z | -. 002 | -. 002 | 0 | \%100 |
| 33 | M39 | Z | -. 002 | -. 002 | 0 | \%100 |
| 34 | M19 | Z | -. 004 | -. 004 | \%99.9 | \%100 |
| 35 | M20 | Z | -. 004 | -. 004 | \%97.2 | \%100 |
| 36 | M21 | Z | -. 004 | -. 004 | \%96.7 | \%100 |
| 37 | M23 | Z | -. 004 | -. 004 | \%96.7 | \%100 |
| 38 | M25 | Z | -. 004 | -. 004 | \%99.9 | \%100 |
| 39 | M26 | Z | -. 004 | -. 004 | \%97.2 | \%100 |
| 40 | M27 | Z | -. 004 | -. 004 | \%99.9 | \%100 |
| 41 | M28 | Z | -. 004 | -. 004 | \%96.7 | \%100 |
| 42 | M30 | Z | -. 004 | -. 004 | \%97.2 | \%100 |
| 43 | M1 | X | 014 | 014 | 0 | \%100 |
| 44 | M2 | X | 0 | 0 | 0 | \%100 |
| 45 | M3 | X | 014 | 014 | 0 | \%100 |
| 46 | M7 | X | 023 | 023 | 0 | \%100 |
| 47 | M8 | X | 006 | . 006 | 0 | \%100 |
| 48 | M9 | X | 006 | 006 | 0 | \%100 |
| 49 | M10 | X | 002 | 002 | 0 | \%100 |
| 50 | M11 | X | 0 | 0 | 0 | \%100 |
| 51 | M12 | X | 011 | 011 | 0 | \%100 |
| 52 | M13 | X | . 009 | . 009 | 0 | \%100 |
| 53 | M14 | X | 011 | . 011 | 0 | \%100 |
| 54 | M15 | X | 011 | . 011 | 0 | \%100 |
| 55 | M16 | X | 002 | 002 | 0 | \%100 |
| 56 | M17 | X | 0 | 0 | 0 | \%100 |
| 57 | M18 | X | . 011 | . 011 | 0 | \%100 |
| 58 | M19 | X | 007 | . 007 | 0 | \%100 |
| 59 | M20 | X | 007 | . 007 | 0 | \%100 |
| 60 | M21 | X | 007 | 007 | 0 | \%100 |
| 61 | M22 | X | 007 | 007 | 0 | \%100 |
| 62 | M23 | X | . 007 | . 007 | 0 | \%3.3 |
| 63 | M24 | X | 007 | . 007 | 0 | \%100 |
| 64 | M25 | X | 007 | 007 | 0 | \%. 1 |
| 65 | M26 | X | 007 | 007 | 0 | \%2.8 |
| 66 | M27 | X | 007 | 007 | 0 | \%. 1 |
| 67 | M28 | X | 007 | . 007 | 0 | \%3.3 |
| 68 | M29 | X | 007 | 007 | 0 | \%100 |
| 69 | M30 | X | . 007 | . 007 | 0 | \%2.8 |
| 70 | M31 | X | 002 | 002 | 0 | \%100 |
| 71 | M32 | X | 007 | . 007 | 0 | \%100 |
| 72 | M33 | X | 002 | . 002 | 0 | \%100 |
| 73 | M37 | X | . 012 | . 012 | 0 | \%100 |
| 74 | M38 | X | . 003 | . 003 | 0 | \%100 |
| 75 | M39 | X | 003 | 003 | 0 | \%100 |
| 76 | M23 | X | 007 | . 007 | \%96.7 | \%100 |
| 77 | M25 | X | 007 | . 007 | \%99.9 | \%100 |
| 78 | M26 | X | 007 | 007 | \%97.2 | \%100 |
| 79 | M27 | X | 007 | . 007 | \%99.9 | \%100 |
| 80 | M28 | X | 007 | . 007 | \%96.7 | \%100 |
| 81 | M30 | X | 007 | . 007 | \%97.2 | \%100 |

## Member Distributed Loads (BLC 12 : Full Wind Members (90 Deg))

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/ft,F,ksf] | Start Location[ft, | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | 0 | 0 | 0 |  |

Member Distributed Loads (BLC 12 : Full Wind Members (90 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft.F.ksfl | End Magnitude[k/ft,F.ksfl | Start Location[ft, | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | M2 | Z | 0 | 0 | 0 | \%100 |
| 3 | M3 | Z | 0 | 0 | 0 | \%100 |
| 4 | M7 | Z | 0 | 0 | 0 | \%100 |
| 5 | M8 | Z | 0 | 0 | 0 | \%100 |
| 6 | M9 | Z | 0 | 0 | 0 | \%100 |
| 7 | M10 | Z | 0 | 0 | 0 | \%100 |
| 8 | M11 | Z | 0 | 0 | 0 | \%100 |
| 9 | M12 | Z | 0 | 0 | 0 | \%100 |
| 10 | M13 | Z | 0 | 0 | 0 | \%100 |
| 11 | M14 | Z | 0 | 0 | 0 | \%100 |
| 12 | M15 | Z | 0 | 0 | 0 | \%100 |
| 13 | M16 | Z | 0 | 0 | 0 | \%100 |
| 14 | M17 | Z | 0 | 0 | 0 | \%100 |
| 15 | M18 | Z | 0 | 0 | 0 | \%100 |
| 16 | M19 | Z | 0 | 0 | 0 | \%. 1 |
| 17 | M20 | Z | 0 | 0 | 0 | \%2.8 |
| 18 | M21 | Z | 0 | 0 | 0 | \%3.3 |
| 19 | M22 | Z | 0 | 0 | 0 | \%100 |
| 20 | M23 | Z | 0 | 0 | 0 | \%3.3 |
| 21 | M24 | Z | 0 | 0 | 0 | \%100 |
| 22 | M25 | Z | 0 | 0 | 0 | \%. 1 |
| 23 | M26 | Z | 0 | 0 | 0 | \%2.8 |
| 24 | M27 | Z | 0 | 0 | 0 | \%. 1 |
| 25 | M28 | Z | 0 | 0 | 0 | \%3.3 |
| 26 | M29 | Z | 0 | 0 | 0 | \%100 |
| 27 | M30 | Z | 0 | 0 | 0 | \%2.8 |
| 28 | M31 | Z | 0 | 0 | 0 | \%100 |
| 29 | M32 | Z | 0 | 0 | 0 | \%100 |
| 30 | M33 | Z | 0 | 0 | 0 | \%100 |
| 31 | M37 | Z | 0 | 0 | 0 | \%100 |
| 32 | M38 | Z | 0 | 0 | 0 | \%100 |
| 33 | M39 | Z | 0 | 0 | 0 | \%100 |
| 34 | M19 | Z | 0 | 0 | \%99.9 | \%100 |
| 35 | M20 | Z | 0 | 0 | \%97.2 | \%100 |
| 36 | M21 | Z | 0 | 0 | \%96.7 | \%100 |
| 37 | M23 | Z | 0 | 0 | \%96.7 | \%100 |
| 38 | M25 | Z | 0 | 0 | \%99.9 | \%100 |
| 39 | M26 | Z | 0 | 0 | \%97.2 | \%100 |
| 40 | M27 | Z | 0 | 0 | \%99.9 | \%100 |
| 41 | M28 | Z | 0 | 0 | \%96.7 | \%100 |
| 42 | M30 | Z | 0 | 0 | \%97.2 | \%100 |
| 43 | M1 | X | . 022 | 022 | 0 | \%100 |
| 44 | M2 | X | . 005 | 005 | 0 | \%100 |
| 45 | M3 | X | . 005 | 005 | 0 | \%100 |
| 46 | M7 | X | . 02 | . 02 | 0 | \%100 |
| 47 | M8 | X | . 02 | . 02 | 0 | \%100 |
| 48 | M9 | X | 0 | 0 | 0 | \%100 |
| 49 | M10 | X | 0 | 0 | 0 | \%100 |
| 50 | M11 | X | . 004 | 004 | 0 | \%100 |
| 51 | M12 | X | . 004 | . 004 | 0 | \%100 |
| 52 | M13 | X | . 008 | 008 | 0 | \%100 |
| 53 | M14 | X | . 016 | . 016 | 0 | \%100 |
| 54 | M15 | X | . 004 | 004 | 0 | \%100 |
| 55 | M16 | X | . 008 | . 008 | 0 | \%100 |
| 56 | M17 | X | . 004 | . 004 | 0 | \%100 |
| 57 | M18 | X | 016 | 016 | 0 | \%100 |
| 58 | M19 | X | . 008 | 008 | 0 | \%100 |

Member Distributed Loads (BLC 12 : Full Wind Members (90 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/ft,F,ksf] | Start Location[ft., | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 59 | M20 | X | . 008 | . 008 | 0 | \%100 |
| 60 | M21 | X | 008 | 008 | 0 | \%100 |
| 61 | M22 | X | 008 | 008 | 0 | \%100 |
| 62 | M23 | X | 008 | 008 | 0 | \%3.3 |
| 63 | M24 | X | 008 | 008 | 0 | \%100 |
| 64 | M25 | X | 008 | 008 | 0 | \%. 1 |
| 65 | M26 | X | 008 | 008 | 0 | \%2.8 |
| 66 | M27 | X | 008 | 008 | 0 | \%. 1 |
| 67 | M28 | X | 008 | 008 | 0 | \%3.3 |
| 68 | M29 | X | 008 | 008 | 0 | \%100 |
| 69 | M30 | X | 008 | 008 | 0 | \%2.8 |
| 70 | M31 | X | 0 | 0 | 0 | \%100 |
| 71 | M32 | X | 006 | 006 | 0 | \%100 |
| 72 | M33 | X | 006 | 006 | 0 | \%100 |
| 73 | M37 | X | . 01 | . 01 | 0 | \%100 |
| 74 | M38 | X | 0 | 0 | 0 | \%100 |
| 75 | M39 | X | . 01 | 01 | 0 | \%100 |
| 76 | M23 | X | 008 | . 008 | \%96.7 | \%100 |
| 77 | M25 | X | 008 | 008 | \%99.9 | \%100 |
| 78 | M26 | X | 008 | . 008 | \%97.2 | \%100 |
| 79 | M27 | X | 008 | . 008 | \%99.9 | \%100 |
| 80 | M28 | X | 008 | . 008 | \%96.7 | \%100 |
| 81 | M30 | X | . 008 | . 008 | \%97.2 | \%100 |

Member Distributed Loads (BLC 13 : Full Wind Members (120 Deg))

|  | Member Label | Direction | Start Magnitude[k/ft.F. . ksf] | End Magnitude[k/ft. F. .sf] | Start Location[ft. | End Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | . 008 | . 008 | 0 | \%100 |
| 2 | M2 | Z | 008 | 008 | 0 | \%100 |
| 3 | M3 | Z | 0 | 0 | 0 | \%100 |
| 4 | M7 | Z | . 003 | 003 | 0 | \%100 |
| 5 | M8 | Z | 013 | 013 | 0 | \%100 |
| 6 | M9 | Z | . 003 | 003 | 0 | \%100 |
| 7 | M10 | Z | 001 | 001 | 0 | \%100 |
| 8 | M11 | Z | . 006 | . 006 | 0 | \%100 |
| 9 | M12 | Z | 0 | 0 | 0 | \%100 |
| 10 | M13 | Z | . 001 | . 001 | 0 | \%100 |
| 11 | M14 | Z | . 006 | 006 | 0 | \%100 |
| 12 | M15 | Z | 0 | 0 | 0 | \%100 |
| 13 | M16 | Z | . 005 | 005 | 0 | \%100 |
| 14 | M17 | Z | . 006 | 006 | 0 | \%100 |
| 15 | M18 | Z | . 006 | . 006 | 0 | \%100 |
| 16 | M19 | Z | . 004 | . 004 | 0 | \%. 1 |
| 17 | M20 | Z | 004 | 004 | 0 | \%2.8 |
| 18 | M21 | Z | . 004 | . 004 | 0 | \%3.3 |
| 19 | M22 | Z | . 004 | 004 | 0 | \%100 |
| 20 | M23 | Z | . 004 | . 004 | 0 | \%3.3 |
| 21 | M24 | Z | . 004 | 004 | 0 | \%100 |
| 22 | M25 | Z | . 004 | 004 | 0 | \%. 1 |
| 23 | M26 | Z | . 004 | 004 | 0 | \%2.8 |
| 24 | M27 | Z | . 004 | . 004 | 0 | \%. 1 |
| 25 | M28 | Z | . 004 | . 004 | 0 | \%3.3 |
| 26 | M29 | Z | . 004 | . 004 | 0 | \%100 |
| 27 | M30 | Z | . 004 | . 004 | 0 | \%2.8 |
| 28 | M31 | Z | . 001 | 001 | 0 | \%100 |
| 29 | M32 | Z | . 001 | 001 | 0 | \%100 |
| 30 | M33 | Z | 004 | 004 | 0 | \%100 |

Company

Member Distributed Loads (BLC 13 : Full Wind Members (120 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/ft,F,ksf] | Start Location [ft,.. | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 31 | M37 | Z | . 002 | . 002 | 0 | \%100 |
| 32 | M38 | Z | 002 | 002 | 0 | \%100 |
| 33 | M39 | Z | 007 | 007 | 0 | \%100 |
| 34 | M19 | Z | 004 | 004 | \%99.9 | \%100 |
| 35 | M20 | Z | . 004 | 004 | \%97.2 | \%100 |
| 36 | M21 | Z | . 004 | 004 | \%96.7 | \%100 |
| 37 | M23 | Z | 004 | 004 | \%96.7 | \%100 |
| 38 | M25 | Z | 004 | 004 | \%99.9 | \%100 |
| 39 | M26 | Z | 004 | 004 | \%97.2 | \%100 |
| 40 | M27 | Z | . 004 | 004 | \%99.9 | \%100 |
| 41 | M28 | Z | 004 | 004 | \%96.7 | \%100 |
| 42 | M30 | Z | . 004 | 004 | \%97.2 | \%100 |
| 43 | M1 | X | 014 | 014 | 0 | \%100 |
| 44 | M2 | X | 014 | 014 | 0 | \%100 |
| 45 | M3 | X | 0 | 0 | 0 | \%100 |
| 46 | M7 | X | 006 | 006 | 0 | \%100 |
| 47 | M8 | X | . 023 | 023 | 0 | \%100 |
| 48 | M9 | X | 006 | 006 | 0 | \%100 |
| 49 | M10 | X | 002 | 002 | 0 | \%100 |
| 50 | M11 | X | 011 | 011 | 0 | \%100 |
| 51 | M12 | X | 0 | 0 | 0 | \%100 |
| 52 | M13 | X | . 002 | . 002 | 0 | \%100 |
| 53 | M14 | X | . 011 | . 011 | 0 | \%100 |
| 54 | M15 | X | 0 | 0 | 0 | \%100 |
| 55 | M16 | X | . 009 | . 009 | 0 | \%100 |
| 56 | M17 | X | 011 | 011 | 0 | \%100 |
| 57 | M18 | X | 011 | . 011 | 0 | \%100 |
| 58 | M19 | X | . 007 | . 007 | 0 | \%100 |
| 59 | M20 | X | 007 | . 007 | 0 | \%100 |
| 60 | M21 | X | 007 | 007 | 0 | \%100 |
| 61 | M22 | X | 007 | 007 | 0 | \%100 |
| 62 | M23 | X | . 007 | 007 | 0 | \%3.3 |
| 63 | M24 | X | . 007 | . 007 | 0 | \%100 |
| 64 | M25 | X | 007 | 007 | 0 | \%. 1 |
| 65 | M26 | X | 007 | 007 | 0 | \%2.8 |
| 66 | M27 | X | 007 | 007 | 0 | \%. 1 |
| 67 | M28 | X | 007 | 007 | 0 | \%3.3 |
| 68 | M29 | X | . 007 | 007 | 0 | \%100 |
| 69 | M30 | X | 007 | 007 | 0 | \%2.8 |
| 70 | M31 | X | 002 | 002 | 0 | \%100 |
| 71 | M32 | X | 002 | 002 | 0 | \%100 |
| 72 | M33 | X | 007 | 007 | 0 | \%100 |
| 73 | M37 | X | 003 | . 003 | 0 | \%100 |
| 74 | M38 | X | . 003 | . 003 | 0 | \%100 |
| 75 | M39 | X | . 012 | . 012 | 0 | \%100 |
| 76 | M23 | X | 007 | 007 | \%96.7 | \%100 |
| 77 | M25 | X | . 007 | . 007 | \%99.9 | \%100 |
| 78 | M26 | X | 007 | 007 | \%97.2 | \%100 |
| 79 | M27 | X | 007 | . 007 | \%99.9 | \%100 |
| 80 | M28 | X | . 007 | 007 | \%96.7 | \%100 |
| 81 | M30 | X | 007 | 007 | \%97.2 | \%100 |

Member Distributed Loads (BLC 14 : Full Wind Members (150 Deg))

|  | Member Label | Direction | Start Magnitude[k/ft,F.ksf] | End Magnitude[k/ft.F.ksf] | Start Location [ft, | End Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | 005 | 005 | 0 | \%100 |
| 2 | M2 | Z | 019 | 019 | 0 | \%100 |

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Member Distributed Loads (BLC 14 : Full Wind Members (150 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F, ksf] | End Magnitude[kfft,F,ksf] | Start Location[ft, | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | M3 | Z | . 005 | . 005 | 0 | \%100 |
| 4 | M7 | Z | 0 | 0 | 0 | \%100 |
| 5 | M8 | Z | . 018 | . 018 | 0 | \%100 |
| 6 | M9 | Z | . 018 | . 018 | 0 | \%100 |
| 7 | M10 | Z | . 007 | 007 | 0 | \%100 |
| 8 | M11 | Z | . 014 | . 014 | 0 | \%100 |
| 9 | M12 | Z | 004 | 004 | 0 | \%100 |
| 10 | M13 | Z | 0 | 0 | 0 | \%100 |
| 11 | M14 | Z | . 004 | . 004 | 0 | \%100 |
| 12 | M15 | Z | 004 | 004 | 0 | \%100 |
| 13 | M16 | Z | . 007 | . 007 | 0 | \%100 |
| 14 | M17 | Z | . 014 | . 014 | 0 | \%100 |
| 15 | M18 | Z | . 004 | . 004 | 0 | \%100 |
| 16 | M19 | Z | . 007 | . 007 | 0 | \%. 1 |
| 17 | M20 | Z | . 007 | . 007 | 0 | \%2.8 |
| 18 | M21 | Z | . 007 | 007 | 0 | \%3.3 |
| 19 | M22 | Z | . 007 | . 007 | 0 | \%100 |
| 20 | M23 | Z | . 007 | . 007 | 0 | \%3.3 |
| 21 | M24 | Z | . 007 | . 007 | 0 | \%100 |
| 22 | M25 | Z | . 007 | . 007 | 0 | \%. 1 |
| 23 | M26 | Z | . 007 | . 007 | 0 | \%2.8 |
| 24 | M27 | Z | . 007 | . 007 | 0 | \%. 1 |
| 25 | M28 | Z | . 007 | . 007 | 0 | \%3.3 |
| 26 | M29 | Z | . 007 | 007 | 0 | \%100 |
| 27 | M30 | Z | . 007 | . 007 | 0 | \%2.8 |
| 28 | M31 | Z | . 005 | 005 | 0 | \%100 |
| 29 | M32 | Z | 0 | 0 | 0 | \%100 |
| 30 | M33 | Z | 005 | . 005 | 0 | \%100 |
| 31 | M37 | Z | 0 | 0 | 0 | \%100 |
| 32 | M38 | Z | . 009 | . 009 | 0 | \%100 |
| 33 | M39 | Z | . 009 | . 009 | 0 | \%100 |
| 34 | M19 | Z | . 007 | . 007 | \%99.9 | \%100 |
| 35 | M20 | Z | . 007 | . 007 | \%97.2 | \%100 |
| 36 | M21 | Z | . 007 | . 007 | \%96.7 | \%100 |
| 37 | M23 | Z | . 007 | . 007 | \%96.7 | \%100 |
| 38 | M25 | Z | . 007 | . 007 | \%99.9 | \%100 |
| 39 | M26 | Z | . 007 | . 007 | \%97.2 | \%100 |
| 40 | M27 | Z | . 007 | . 007 | \%99.9 | \%100 |
| 41 | M28 | Z | . 007 | . 007 | \%96.7 | \%100 |
| 42 | M30 | Z | . 007 | . 007 | \%97.2 | \%100 |
| 43 | M1 | X | . 003 | . 003 | 0 | \%100 |
| 44 | M2 | X | . 011 | . 011 | 0 | \%100 |
| 45 | M3 | X | . 003 | . 003 | 0 | \%100 |
| 46 | M7 | X | 0 | 0 | 0 | \%100 |
| 47 | M8 | X | . 01 | 01 | 0 | \%100 |
| 48 | M9 | X | . 01 | . 01 | 0 | \%100 |
| 49 | M10 | X | . 004 | . 004 | 0 | \%100 |
| 50 | M11 | X | . 008 | . 008 | 0 | \%100 |
| 51 | M12 | X | . 002 | . 002 | 0 | \%100 |
| 52 | M13 | X | 0 | 0 | 0 | \%100 |
| 53 | M14 | X | . 002 | . 002 | 0 | \%100 |
| 54 | M15 | X | . 002 | 002 | 0 | \%100 |
| 55 | M16 | X | . 004 | . 004 | 0 | \%100 |
| 56 | M17 | X | . 008 | 008 | 0 | \%100 |
| 57 | M18 | X | . 002 | . 002 | 0 | \%100 |
| 58 | M19 | X | . 004 | . 004 | 0 | \%100 |
| 59 | M20 | X | . 004 | . 004 | 0 | \%100 |

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Member Distributed Loads (BLC 14 : Full Wind Members (150 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft.F.ksfl | End Magnitude[k/ft,F.ksfl | Start Location [ft. | .End Location[ft, \%l |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60 | M21 | X | 004 | 004 | 0 | \%100 |
| 61 | M22 | X | 004 | 004 | 0 | \%100 |
| 62 | M23 | X | . 004 | 004 | 0 | \%3.3 |
| 63 | M24 | X | 004 | 004 | 0 | \%100 |
| 64 | M25 | X | 004 | 004 | 0 | \%. 1 |
| 65 | M26 | X | 004 | 004 | 0 | \%2.8 |
| 66 | M27 | X | 004 | 004 | 0 | \%. 1 |
| 67 | M28 | X | 004 | 004 | 0 | \%3.3 |
| 68 | M29 | X | 004 | 004 | 0 | \%100 |
| 69 | M30 | X | 004 | 004 | 0 | \%2.8 |
| 70 | M31 | X | 003 | 003 | 0 | \%100 |
| 71 | M32 | X | 0 | 0 | 0 | \%100 |
| 72 | M33 | X | 003 | 003 | 0 | \%100 |
| 73 | M37 | X | 0 | 0 | 0 | \%100 |
| 74 | M38 | X | 005 | . 005 | 0 | \%100 |
| 75 | M39 | X | 005 | 005 | 0 | \%100 |
| 76 | M23 | X | 004 | 004 | \%96.7 | \%100 |
| 77 | M25 | X | 004 | . 004 | \%99.9 | \%100 |
| 78 | M26 | X | 004 | 004 | \%97.2 | \%100 |
| 79 | M27 | X | 004 | . 004 | \%99.9 | \%100 |
| 80 | M28 | X | 004 | . 004 | \%96.7 | \%100 |
| 81 | M30 | X | 004 | . 004 | \%97.2 | \%100 |

Member Distributed Loads (BLC 21 : Ice Wind Members (0 Deg))

|  | Member Label | Direction | Start Magnitude[k/ft,F, ksf] | End Magnitude[k/ft,F, ksf] | Start Location[ft... | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | 0 | 0 | 0 | \%100 |
| 2 | M2 | Z | -. 004 | -. 004 | 0 | \%100 |
| 3 | M3 | Z | -. 004 | -. 004 | 0 | \%100 |
| 4 | M4 | Z | -. 003 | -. 003 | 0 | \%100 |
| 5 | M5 | Z | -. 001 | -. 001 | 0 | \%100 |
| 6 | M6 | Z | -. 001 | -. 001 | 0 | \%100 |
| 7 | M7 | Z | -. 002 | -. 002 | 0 | \%100 |
| 8 | M8 | Z | -. 002 | -. 002 | 0 | \%100 |
| 9 | M9 | Z | -. 007 | -. 007 | 0 | \%100 |
| 10 | M10 | Z | -. 004 | -. 004 | 0 | \%100 |
| 11 | M11 | Z | -. 004 | -. 004 | 0 | \%100 |
| 12 | M12 | Z | -. 004 | -. 004 | 0 | \%100 |
| 13 | M13 | Z | -. 001 | -. 001 | 0 | \%100 |
| 14 | M14 | Z | 0 | 0 | 0 | \%100 |
| 15 | M15 | Z | -. 004 | -. 004 | 0 | \%100 |
| 16 | M16 | Z | -. 001 | -. 001 | 0 | \%100 |
| 17 | M17 | Z | -. 004 | -. 004 | 0 | \%100 |
| 18 | M18 | Z | 0 | 0 | 0 | \%100 |
| 19 | M19 | Z | -. 004 | -. 004 | 0 | \%. 1 |
| 20 | M20 | Z | -. 004 | -. 004 | 0 | \%2.8 |
| 21 | M21 | Z | -. 004 | -. 004 | 0 | \%3.3 |
| 22 | M22 | Z | -. 003 | -. 003 | 0 | \%100 |
| 23 | M23 | Z | -. 004 | -. 004 | 0 | \%3.3 |
| 24 | M24 | Z | -. 003 | -. 003 | 0 | \%100 |
| 25 | M25 | Z | -. 004 | -. 004 | 0 | \%. 1 |
| 26 | M26 | Z | -. 004 | -. 004 | 0 | \%2.8 |
| 27 | M27 | Z | -. 004 | -. 004 | 0 | \%. 1 |
| 28 | M28 | Z | -. 004 | -. 004 | 0 | \%3.3 |
| 29 | M29 | Z | -. 003 | -. 003 | 0 | \%100 |
| 30 | M30 | Z | -. 004 | -. 004 | 0 | \%2.8 |
| 31 | M31 | Z | -. 003 | -. 003 | 0 | \%100 |

Company

Member Distributed Loads (BLC 21 : Ice Wind Members (0 Deg))(Continued)

|  | Member Label | Direction | Start Magnitude[k/ft.F.ksfl | End Magnitude[k/ft,F.ksfl | Start Locationfft, | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 32 | M32 | Z | -. 001 | -. 001 | 0 | \%100 |
| 33 | M33 | Z | -. 001 | -. 001 | 0 | \%100 |
| 34 | M37 | Z | -. 001 | -. 001 | 0 | \%100 |
| 35 | M38 | Z | -. 005 | -. 005 | 0 | \%100 |
| 36 | M39 | Z | -. 001 | -. 001 | 0 | \%100 |
| 37 | M19 | Z | -. 004 | -. 004 | \%99.9 | \%100 |
| 38 | M20 | Z | -. 004 | -. 004 | \%97.2 | \%100 |
| 39 | M21 | Z | -. 004 | -. 004 | \%96.7 | \%100 |
| 40 | M23 | Z | -. 004 | -. 004 | \%96.7 | \%100 |
| 41 | M25 | Z | -. 004 | -. 004 | \%99.9 | \%100 |
| 42 | M26 | Z | -. 004 | -. 004 | \%97.2 | \%100 |
| 43 | M27 | Z | -. 004 | -. 004 | \%99.9 | \%100 |
| 44 | M28 | Z | -. 004 | -. 004 | \%96.7 | \%100 |
| 45 | M30 | Z | -. 004 | -. 004 | \%97.2 | \%100 |
| 46 | M1 | X | 0 | 0 | 0 | \%100 |
| 47 | M2 | X | 0 | 0 | 0 | \%100 |
| 48 | M3 | X | 0 | 0 | 0 | \%100 |
| 49 | M4 | X | 0 | 0 | 0 | \%100 |
| 50 | M5 | X | 0 | 0 | 0 | \%100 |
| 51 | M6 | X | 0 | 0 | 0 | \%100 |
| 52 | M7 | X | 0 | 0 | 0 | \%100 |
| 53 | M8 | X | 0 | 0 | 0 | \%100 |
| 54 | M9 | X | 0 | 0 | 0 | \%100 |
| 55 | M10 | X | 0 | 0 | 0 | \%100 |
| 56 | M11 | X | 0 | 0 | 0 | \%100 |
| 57 | M12 | X | 0 | 0 | 0 | \%100 |
| 58 | M13 | X | 0 | 0 | 0 | \%100 |
| 59 | M14 | X | 0 | 0 | 0 | \%100 |
| 60 | M15 | X | 0 | 0 | 0 | \%100 |
| 61 | M16 | X | 0 | 0 | 0 | \%100 |
| 62 | M17 | X | 0 | 0 | 0 | \%100 |
| 63 | M18 | X | 0 | 0 | 0 | \%100 |
| 64 | M19 | X | 0 | 0 | 0 | \%100 |
| 65 | M20 | X | 0 | 0 | 0 | \%100 |
| 66 | M21 | X | 0 | 0 | 0 | \%100 |
| 67 | M22 | X | 0 | 0 | 0 | \%100 |
| 68 | M23 | X | 0 | 0 | 0 | \%3.3 |
| 69 | M24 | X | 0 | 0 | 0 | \%100 |
| 70 | M25 | X | 0 | 0 | 0 | \%. 1 |
| 71 | M26 | X | 0 | 0 | 0 | \%2.8 |
| 72 | M27 | X | 0 | 0 | 0 | \%. 1 |
| 73 | M28 | X | 0 | 0 | 0 | \%3.3 |
| 74 | M29 | X | 0 | 0 | 0 | \%100 |
| 75 | M30 | X | 0 | 0 | 0 | \%2.8 |
| 76 | M31 | X | 0 | 0 | 0 | \%100 |
| 77 | M32 | X | 0 | 0 | 0 | \%100 |
| 78 | M33 | X | 0 | 0 | 0 | \%100 |
| 79 | M37 | X | 0 | 0 | 0 | \%100 |
| 80 | M38 | X | 0 | 0 | 0 | \%100 |
| 81 | M39 | X | 0 | 0 | 0 | \%100 |
| 82 | M23 | X | 0 | 0 | \%96.7 | \%100 |
| 83 | M25 | X | 0 | 0 | \%99.9 | \%100 |
| 84 | M26 | X | 0 | 0 | \%97.2 | \%100 |
| 85 | M27 | X | 0 | 0 | \%99.9 | \%100 |
| 86 | M28 | X | 0 | 0 | \%96.7 | \%100 |
| 87 | M30 | X | 0 | 0 | \%97.2 | \%100 |

Company

Member Distributed Loads (BLC 22 : Ice Wind Members (30 Deg))

|  | Member Label | Direction | Start Magnitude[k/ft,F, ksf] | End Magnitude[[k/ft,F,ksf] | Start Location[ft, | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | -. 001 | -. 001 | 0 | \%100 |
| 2 | M2 | Z | -. 002 | -. 002 | 0 | \%100 |
| 3 | M3 | Z | -. 005 | -. 005 | 0 | \%100 |
| 4 | M4 | Z | -. 003 | -. 003 | 0 | \%100 |
| 5 | M5 | Z | -. 001 | -. 001 | 0 | \%100 |
| 6 | M6 | Z | -. 001 | -. 001 | 0 | \%100 |
| 7 | M7 | Z | -. 003 | -. 003 | 0 | \%100 |
| 8 | M8 | Z | 0 | 0 | 0 | \%100 |
| 9 | M9 | Z | -. 005 | -. 005 | 0 | \%100 |
| 10 | M10 | Z | -. 003 | -. 003 | 0 | \%100 |
| 11 | M11 | Z | -. 002 | -. 002 | 0 | \%100 |
| 12 | M12 | Z | -. 004 | -. 004 | 0 | \%100 |
| 13 | M13 | Z | -. 002 | -. 002 | 0 | \%100 |
| 14 | M14 | Z | -. 001 | -. 001 | 0 | \%100 |
| 15 | M15 | Z | -. 004 | -. 004 | 0 | \%100 |
| 16 | M16 | Z | 0 | 0 | 0 | \%100 |
| 17 | M17 | Z | -. 002 | -. 002 | 0 | \%100 |
| 18 | M18 | Z | -. 001 | -. 001 | 0 | \%100 |
| 19 | M19 | Z | -. 003 | -. 003 | 0 | \%. 1 |
| 20 | M20 | Z | -. 003 | -. 003 | 0 | \%2.8 |
| 21 | M21 | Z | -. 003 | -. 003 | 0 | \%3.3 |
| 22 | M22 | Z | -. 003 | -. 003 | 0 | \%100 |
| 23 | M23 | Z | -. 003 | -. 003 | 0 | \%3.3 |
| 24 | M24 | Z | -. 003 | -. 003 | 0 | \%100 |
| 25 | M25 | Z | -. 003 | -. 003 | 0 | \%. 1 |
| 26 | M26 | Z | -. 003 | -. 003 | 0 | \%2.8 |
| 27 | M27 | Z | -. 003 | -. 003 | 0 | \%. 1 |
| 28 | M28 | Z | -. 003 | -. 003 | 0 | \%3.3 |
| 29 | M29 | Z | -. 003 | -. 003 | 0 | \%100 |
| 30 | M30 | Z | -. 003 | -. 003 | 0 | \%2.8 |
| 31 | M31 | Z | -. 003 | -. 003 | 0 | \%100 |
| 32 | M32 | Z | -. 001 | -. 001 | 0 | \%100 |
| 33 | M33 | Z | 0 | 0 | 0 | \%100 |
| 34 | M37 | Z | -. 002 | -. 002 | 0 | \%100 |
| 35 | M38 | Z | -. 004 | -. 004 | 0 | \%100 |
| 36 | M39 | Z | -. 001 | -. 001 | 0 | \%100 |
| 37 | M19 | Z | -. 003 | -. 003 | \%99.9 | \%100 |
| 38 | M20 | Z | -. 003 | -. 003 | \%97.2 | \%100 |
| 39 | M21 | Z | -. 003 | -. 003 | \%96.7 | \%100 |
| 40 | M23 | Z | -. 003 | -. 003 | \%96.7 | \%100 |
| 41 | M25 | Z | -. 003 | -. 003 | \%99.9 | \%100 |
| 42 | M26 | Z | -. 003 | -. 003 | \%97.2 | \%100 |
| 43 | M27 | Z | -. 003 | -. 003 | \%99.9 | \%100 |
| 44 | M28 | Z | -. 003 | -. 003 | \%96.7 | \%100 |
| 45 | M30 | Z | -. 003 | -. 003 | \%97.2 | \%100 |
| 46 | M1 | X | 0 | 0 | 0 | \%100 |
| 47 | M2 | X | . 001 | . 001 | 0 | \%100 |
| 48 | M3 | X | . 003 | . 003 | 0 | \%100 |
| 49 | M4 | X | . 002 | . 002 | 0 | \%100 |
| 50 | M5 | X | 0 | 0 | 0 | \%100 |
| 51 | M6 | X | 0 | 0 | 0 | \%100 |
| 52 | M7 | X | 002 | 002 | 0 | \%100 |
| 53 | M8 | X | 0 | 0 | 0 | \%100 |
| 54 | M9 | X | . 003 | . 003 |  | \%100 |
| 55 | M10 | X | . 002 | 002 | 0 | \%100 |
| 56 | M11 | X | . 001 | . 001 | 0 | \%100 |
| 57 | M12 | X | . 002 | . 002 | 0 | \%100 |

Company

## Member Distributed Loads (BLC 22 : Ice Wind Members (30 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitudelk/ft.F. . ksfl | End Magnitude[k/ft.F.ksfl | Start Locationfft | .End Locationfft.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 58 | M13 | X | . 001 | . 001 | 0 | \%100 |
| 59 | M14 | X | 0 | 0 | 0 | \%100 |
| 60 | M15 | X | . 002 | . 002 | 0 | \%100 |
| 61 | M16 | X | 0 | 0 | 0 | \%100 |
| 62 | M17 | X | . 001 | . 001 | 0 | \%100 |
| 63 | M18 | X | 0 | 0 | 0 | \%100 |
| 64 | M19 | X | 002 | 002 | 0 | \%100 |
| 65 | M20 | X | . 002 | . 002 | 0 | \%100 |
| 66 | M21 | X | 002 | . 002 | 0 | \%100 |
| 67 | M22 | X | 002 | 002 | 0 | \%100 |
| 68 | M23 | X | 002 | . 002 | 0 | \%3.3 |
| 69 | M24 | X | 002 | 002 | 0 | \%100 |
| 70 | M25 | X | . 002 | . 002 | 0 | \%. 1 |
| 71 | M26 | X | 002 | 002 | 0 | \%2.8 |
| 72 | M27 | X | 002 | . 002 | 0 | \%. 1 |
| 73 | M28 | X | 002 | . 002 | 0 | \%3.3 |
| 74 | M29 | X | . 002 | . 002 | 0 | \%100 |
| 75 | M30 | X | . 002 | . 002 | 0 | \%2.8 |
| 76 | M31 | X | 001 | . 001 | 0 | \%100 |
| 77 | M32 | X | . 001 | . 001 | 0 | \%100 |
| 78 | M33 | X | 0 | 0 | 0 | \%100 |
| 79 | M37 | X | 001 | 001 | 0 | \%100 |
| 80 | M38 | X | . 002 | . 002 | 0 | \%100 |
| 81 | M39 | X | 0 | 0 | 0 | \%100 |
| 82 | M23 | X | . 002 | . 002 | \%96.7 | \%100 |
| 83 | M25 | X | 002 | 002 | \%99.9 | \%100 |
| 84 | M26 | X | . 002 | . 002 | \%97.2 | \%100 |
| 85 | M27 | X | . 002 | . 002 | \%99.9 | \%100 |
| 86 | M28 | X | . 002 | . 002 | \%96.7 | \%100 |
| 87 | M30 | X | . 002 | . 002 | \%97.2 | \%100 |

## Member Distributed Loads (BLC 23 : Ice Wind Members (60 Deg))

|  | Member Label | Direction | Start Magnitude[kft, F., ksf] | End Magnitude[k/ft,F.ksf] | Start Location[ft., | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | -. 001 | -. 001 | 0 | \%100 |
| 2 | M2 | Z | -. 001 | -. 001 | 0 | \%100 |
| 3 | M3 | Z | -. 002 | -. 002 | 0 | \%100 |
| 4 | M4 | Z | -. 002 | -. 002 | 0 | \%100 |
| 5 | M5 | Z | 0 | 0 | 0 | \%100 |
| 6 | M6 | Z | 0 | 0 | 0 | \%100 |
| 7 | M7 | Z | -. 003 | -. 003 | 0 | \%100 |
| 8 | M8 | Z | -. 001 | -. 001 | 0 | \%100 |
| 9 | M9 | Z | -. 002 | -. 002 | 0 | \%100 |
| 10 | M10 | Z | -. 001 | -. 001 | 0 | \%100 |
| 11 | M11 | Z | -. 001 | -. 001 | 0 | \%100 |
| 12 | M12 | Z | -. 002 | -. 002 | 0 | \%100 |
| 13 | M13 | Z | -. 001 | -. 001 | 0 | \%100 |
| 14 | M14 | Z | -. 001 | -. 001 | 0 | \%100 |
| 15 | M15 | Z | -. 002 | -. 002 | 0 | \%100 |
| 16 | M16 | Z | -. 001 | -. 001 | 0 | \%100 |
| 17 | M17 | Z | -. 001 | -. 001 | 0 | \%100 |
| 18 | M18 | Z | -. 001 | -. 001 | 0 | \%100 |
| 19 | M19 | Z | -. 002 | -. 002 | 0 | \%. 1 |
| 20 | M20 | Z | -. 002 | -. 002 | 0 | \%2.8 |
| 21 | M21 | Z | -. 002 | -. 002 | 0 | \%3.3 |
| 22 | M22 | Z | -. 002 | -. 002 | 0 | \%100 |
| 23 | M23 | Z | -. 002 | -. 002 | 0 | \%3.3 |

Company

Member Distributed Loads (BLC 23 : Ice Wind Members (60 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft.F.ksfl | End MagnitudeIkft.F.ksfl | Start Locationft | End Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 24 | M24 | Z | -. 002 | -. 002 | 0 | \%100 |
| 25 | M25 | Z | -. 002 | -. 002 | 0 | \%. 1 |
| 26 | M26 | Z | -. 002 | -. 002 | 0 | \%2.8 |
| 27 | M27 | Z | -. 002 | -. 002 | 0 | \%. 1 |
| 28 | M28 | Z | -. 002 | -. 002 | 0 | \%3.3 |
| 29 | M29 | Z | -. 002 | -. 002 | 0 | \%100 |
| 30 | M30 | Z | -. 002 | -. 002 | 0 | \%2.8 |
| 31 | M31 | Z | -. 001 | -. 001 | 0 | \%100 |
| 32 | M32 | Z | -. 001 | -. 001 | 0 | \%100 |
| 33 | M33 | Z | 0 | 0 | 0 | \%100 |
| 34 | M37 | Z | -. 001 | -. 001 | 0 | \%100 |
| 35 | M38 | Z | -. 002 | -. 002 | 0 | \%100 |
| 36 | M39 | Z | -. 001 | -. 001 | 0 | \%100 |
| 37 | M19 | Z | -. 002 | -. 002 | \%99.9 | \%100 |
| 38 | M20 | Z | -. 002 | -. 002 | \%97.2 | \%100 |
| 39 | M21 | Z | -. 002 | -. 002 | \%96.7 | \%100 |
| 40 | M23 | Z | -. 002 | -. 002 | \%96.7 | \%100 |
| 41 | M25 | Z | -. 002 | -. 002 | \%99.9 | \%100 |
| 42 | M26 | Z | -. 002 | -. 002 | \%97.2 | \%100 |
| 43 | M27 | Z | -. 002 | -. 002 | \%99.9 | \%100 |
| 44 | M28 | Z | -. 002 | -. 002 | \%96.7 | \%100 |
| 45 | M30 | Z | -. 002 | -. 002 | \%97.2 | \%100 |
| 46 | M1 | X | . 002 | . 002 | 0 | \%100 |
| 47 | M2 | X | . 001 | . 001 | 0 | \%100 |
| 48 | M3 | X | . 004 | 004 | 0 | \%100 |
| 49 | M4 | X | . 003 | . 003 | 0 | \%100 |
| 50 | M5 | X | . 001 | . 001 | 0 | \%100 |
| 51 | M6 | X | . 001 | 001 | 0 | \%100 |
| 52 | M7 | X | . 004 | . 004 | 0 | \%100 |
| 53 | M8 | X | . 001 | . 001 | 0 | \%100 |
| 54 | M9 | X | . 003 | . 003 | 0 | \%100 |
| 55 | M10 | X | . 002 | 002 | 0 | \%100 |
| 56 | M11 | X | . 002 | . 002 | 0 | \%100 |
| 57 | M12 | X | . 003 | . 003 | 0 | \%100 |
| 58 | M13 | X | 002 | . 002 | 0 | \%100 |
| 59 | M14 | X | . 002 | . 002 | 0 | \%100 |
| 60 | M15 | X | . 003 | . 003 | 0 | \%100 |
| 61 | M16 | X | . 001 | . 001 | 0 | \%100 |
| 62 | M17 | X | . 002 | . 002 | 0 | \%100 |
| 63 | M18 | X | . 002 | . 002 | 0 | \%100 |
| 64 | M19 | X | . 003 | . 003 | 0 | \%100 |
| 65 | M20 | X | . 003 | 003 | 0 | \%100 |
| 66 | M21 | X | . 003 | . 003 | 0 | \%100 |
| 67 | M22 | X | . 003 | 003 | 0 | \%100 |
| 68 | M23 | X | . 003 | . 003 | 0 | \%3.3 |
| 69 | M24 | X | . 003 | . 003 | 0 | \%100 |
| 70 | M25 | X | . 003 | . 003 | 0 | \%. 1 |
| 71 | M26 | X | . 003 | . 003 | 0 | \%2.8 |
| 72 | M27 | X | . 003 | . 003 | 0 | \%. 1 |
| 73 | M28 | X | . 003 | . 003 | 0 | \%3.3 |
| 74 | M29 | X | . 003 | 003 | 0 | \%100 |
| 75 | M30 | X | . 003 | . 003 | 0 | \%2.8 |
| 76 | M31 | X | . 002 | 002 |  | \%100 |
| 77 | M32 | X | . 002 | 002 | 0 | \%100 |
| 78 | M33 | X | . 001 | . 001 | 0 | \%100 |
| 79 | M37 | X | . 003 | 003 | 0 | \%100 |
| 80 | M38 | X | . 003 | . 003 | 0 | \%100 |

Member Distributed Loads (BLC 23 : Ice Wind Members (60 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/ft,F,ksf] | Start Location[ft, | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 81 | M39 | X | 001 | . 001 | 0 | \%100 |
| 82 | M23 | X | 003 | 003 | \%96.7 | \%100 |
| 83 | M25 | X | 003 | 003 | \%99.9 | \%100 |
| 84 | M26 | X | 003 | 003 | \%97.2 | \%100 |
| 85 | M27 | X | 003 | . 003 | \%99.9 | \%100 |
| 86 | M28 | X | 003 | 003 | \%96.7 | \%100 |
| 87 | M30 | X | 003 | 003 | \%97.2 | \%100 |

Member Distributed Loads (BLC 24 : Ice Wind Members (90 Deg))

|  | Member Label | Direction | Start Magnitude[kft.F. .ksf] | End Magnitude[k/ft.F.ksf] | Start Locationft | .End Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | 0 | 0 | 0 | \%100 |
| 2 | M2 | Z | 0 | 0 | 0 | \%100 |
| 3 | M3 | Z | 0 | 0 | 0 | \%100 |
| 4 | M4 | Z | 0 | 0 | 0 | \%100 |
| 5 | M5 | Z | 0 | 0 | 0 | \%100 |
| 6 | M6 | Z | 0 | 0 | 0 | \%100 |
| 7 | M7 | Z | 0 | 0 | 0 | \%100 |
| 8 | M8 | Z | 0 | 0 | 0 | \%100 |
| 9 | M9 | Z | 0 | 0 | 0 | \%100 |
| 10 | M10 | Z | 0 | 0 | 0 | \%100 |
| 11 | M11 | Z | 0 | 0 | 0 | \%100 |
| 12 | M12 | Z | 0 | 0 | 0 | \%100 |
| 13 | M13 | Z | 0 | 0 | 0 | \%100 |
| 14 | M14 | Z | 0 | 0 | 0 | \%100 |
| 15 | M15 | Z | 0 | 0 | 0 | \%100 |
| 16 | M16 | Z | 0 | 0 | 0 | \%100 |
| 17 | M17 | Z | 0 | 0 | 0 | \%100 |
| 18 | M18 | Z | 0 | 0 | 0 | \%100 |
| 19 | M19 | Z | 0 | 0 | 0 | \%. 1 |
| 20 | M20 | Z | 0 | 0 | 0 | \%2.8 |
| 21 | M21 | Z | 0 | 0 | 0 | \%3.3 |
| 22 | M22 | Z | 0 | 0 | 0 | \%100 |
| 23 | M23 | Z | 0 | 0 | 0 | \%3.3 |
| 24 | M24 | Z | 0 | 0 | 0 | \%100 |
| 25 | M25 | Z | 0 | 0 | 0 | \%. 1 |
| 26 | M26 | Z | 0 | 0 | 0 | \%2.8 |
| 27 | M27 | Z | 0 | 0 | 0 | \%. 1 |
| 28 | M28 | Z | 0 | 0 | 0 | \%3.3 |
| 29 | M29 | Z | 0 | 0 | 0 | \%100 |
| 30 | M30 | Z | 0 | 0 | 0 | \%2.8 |
| 31 | M31 | Z | 0 | 0 | 0 | \%100 |
| 32 | M32 | Z | 0 | 0 | 0 | \%100 |
| 33 | M33 | Z | 0 | 0 | 0 | \%100 |
| 34 | M37 | Z | 0 | 0 | 0 | \%100 |
| 35 | M38 | Z | 0 | 0 | 0 | \%100 |
| 36 | M39 | Z | 0 | 0 | 0 | \%100 |
| 37 | M19 | Z | 0 | 0 | \%99.9 | \%100 |
| 38 | M20 | Z | 0 | 0 | \%97.2 | \%100 |
| 39 | M21 | Z | 0 | 0 | \%96.7 | \%100 |
| 40 | M23 | Z | 0 | 0 | \%96.7 | \%100 |
| 41 | M25 | Z | 0 | 0 | \%99.9 | \%100 |
| 42 | M26 | Z | 0 | 0 | \%97.2 | \%100 |
| 43 | M27 | Z | 0 | 0 | \%99.9 | \%100 |
| 44 | M28 | Z | 0 | 0 | \%96.7 | \%100 |
| 45 | M30 | Z | 0 | 0 | \%97.2 | \%100 |
| 46 | M1 | X | 004 | 004 | 0 | \%100 |

Company

Member Distributed Loads (BLC 24 : Ice Wind Members (90 Deg))(Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksf] | End Magnitude[k/ft,F,ksf] | Start Location[ft, | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 47 | M2 | X | . 003 | . 003 | 0 | \%100 |
| 48 | M3 | X | 003 | 003 | 0 | \%100 |
| 49 | M4 | X | 003 | 003 | 0 | \%100 |
| 50 | M5 | X | 001 | 001 | 0 | \%100 |
| 51 | M6 | X | 001 | 001 | 0 | \%100 |
| 52 | M7 | X | 004 | 004 | 0 | \%100 |
| 53 | M8 | X | 004 | 004 | 0 | \%100 |
| 54 | M9 | X | 002 | 002 | 0 | \%100 |
| 55 | M10 | X | 002 | 002 | 0 | \%100 |
| 56 | M11 | X | 003 | 003 | 0 | \%100 |
| 57 | M12 | X | 003 | 003 | 0 | \%100 |
| 58 | M13 | X | . 002 | 002 | 0 | \%100 |
| 59 | M14 | X | . 003 | . 003 | 0 | \%100 |
| 60 | M15 | X | 003 | 003 | 0 | \%100 |
| 61 | M16 | X | . 002 | 002 | 0 | \%100 |
| 62 | M17 | X | 003 | 003 | 0 | \%100 |
| 63 | M18 | X | . 003 | . 003 | 0 | \%100 |
| 64 | M19 | X | . 004 | . 004 | 0 | \%100 |
| 65 | M20 | X | 004 | 004 | 0 | \%100 |
| 66 | M21 | X | . 004 | 004 | 0 | \%100 |
| 67 | M22 | X | . 003 | 003 | 0 | \%100 |
| 68 | M23 | X | 004 | 004 | 0 | \%3.3 |
| 69 | M24 | X | . 003 | . 003 | 0 | \%100 |
| 70 | M25 | X | 004 | 004 | 0 | \%. 1 |
| 71 | M26 | X | . 004 | 004 | 0 | \%2.8 |
| 72 | M27 | X | 004 | 004 | 0 | \%. 1 |
| 73 | M28 | X | . 004 | . 004 | 0 | \%3.3 |
| 74 | M29 | X | . 003 | . 003 | 0 | \%100 |
| 75 | M30 | X | . 004 | . 004 | 0 | \%2.8 |
| 76 | M31 | X | 002 | 002 | 0 | \%100 |
| 77 | M32 | X | . 001 | 001 | 0 | \%100 |
| 78 | M33 | X | . 001 | 001 | 0 | \%100 |
| 79 | M37 | X | . 002 | . 002 | 0 | \%100 |
| 80 | M38 | X | . 003 | 003 | 0 | \%100 |
| 81 | M39 | X | 002 | 002 | 0 | \%100 |
| 82 | M23 | X | 004 | 004 | \%96.7 | \%100 |
| 83 | M25 | X | . 004 | 004 | \%99.9 | \%100 |
| 84 | M26 | X | 004 | 004 | \%97.2 | \%100 |
| 85 | M27 | X | . 004 | 004 | \%99.9 | \%100 |
| 86 | M28 | X | 004 | 004 | \%96.7 | \%100 |
| 87 | M30 | X | 004 | 004 | \%97.2 | \%100 |

## Member Distributed Loads (BLC 25 : Ice Wind Members (120 Deg))

|  | Member Label | Direction | Start Magnitude[k/ft,F.ksf] | End Magnitude[k/ft,F.ksf] | Start Location [ft, | End Location[ft, \%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | 001 | 001 | 0 | \%100 |
| 2 | M2 | Z | 002 | 002 | 0 | \%100 |
| 3 | M3 | Z | 001 | 001 | 0 | \%100 |
| 4 | M4 | Z | 002 | 002 | 0 | \%100 |
| 5 | M5 | Z | 0 | 0 | 0 | \%100 |
| 6 | M6 | Z | 0 | 0 | 0 | \%100 |
| 7 | M7 | Z | . 001 | . 001 | 0 | \%100 |
| 8 | M8 | Z | 003 | 003 | 0 | \%100 |
| 9 | M9 | Z | 002 | 002 | 0 | \%100 |
| 10 | M10 | Z | . 001 | . 001 | 0 | \%100 |
| 11 | M11 | Z | 002 | 002 | 0 | \%100 |
| 12 | M12 | Z | 001 | 001 | 0 | \%100 |

Company

Member Distributed Loads (BLC 25 : Ice Wind Members (120 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F.ksf] | End Magnitude[k/ft,F, ksf] | Start Location[ft | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13 | M13 | Z | . 001 | . 001 | 0 | \%100 |
| 14 | M14 | Z | 001 | 001 | 0 | \%100 |
| 15 | M15 | Z | . 001 | . 001 | 0 | \%100 |
| 16 | M16 | Z | 001 | 001 | 0 | \%100 |
| 17 | M17 | Z | . 002 | 002 | 0 | \%100 |
| 18 | M18 | Z | . 001 | 001 | 0 | \%100 |
| 19 | M19 | Z | . 002 | 002 | 0 | \%. 1 |
| 20 | M20 | Z | . 002 | 002 | 0 | \%2.8 |
| 21 | M21 | Z | . 002 | 002 | 0 | \%3.3 |
| 22 | M22 | Z | . 002 | 002 | 0 | \%100 |
| 23 | M23 | Z | . 002 | 002 | 0 | \%3.3 |
| 24 | M24 | Z | 002 | 002 | 0 | \%100 |
| 25 | M25 | Z | . 002 | . 002 | 0 | \%. 1 |
| 26 | M26 | Z | 002 | 002 | 0 | \%2.8 |
| 27 | M27 | Z | . 002 | 002 | 0 | \%. 1 |
| 28 | M28 | Z | 002 | 002 | 0 | \%3.3 |
| 29 | M29 | Z | . 002 | 002 | 0 | \%100 |
| 30 | M30 | Z | 002 | 002 | 0 | \%2.8 |
| 31 | M31 | Z | . 001 | . 001 | 0 | \%100 |
| 32 | M32 | Z | 0 | 0 | 0 | \%100 |
| 33 | M33 | Z | . 001 | . 001 | 0 | \%100 |
| 34 | M37 | Z | . 001 | 001 | 0 | \%100 |
| 35 | M38 | Z | . 002 | . 002 | 0 | \%100 |
| 36 | M39 | Z | . 001 | 001 | 0 | \%100 |
| 37 | M19 | Z | 002 | 002 | \%99.9 | \%100 |
| 38 | M20 | Z | 002 | 002 | \%97.2 | \%100 |
| 39 | M21 | Z | . 002 | . 002 | \%96.7 | \%100 |
| 40 | M23 | Z | 002 | 002 | \%96.7 | \%100 |
| 41 | M25 | Z | . 002 | . 002 | \%99.9 | \%100 |
| 42 | M26 | Z | . 002 | 002 | \%97.2 | \%100 |
| 43 | M27 | Z | . 002 | 002 | \%99.9 | \%100 |
| 44 | M28 | Z | . 002 | . 002 | \%96.7 | \%100 |
| 45 | M30 | Z | . 002 | . 002 | \%97.2 | \%100 |
| 46 | M1 | X | . 002 | 002 | 0 | \%100 |
| 47 | M2 | X | 004 | 004 | 0 | \%100 |
| 48 | M3 | X | . 001 | 001 | 0 | \%100 |
| 49 | M4 | X | . 003 | 003 | 0 | \%100 |
| 50 | M5 | X | . 001 | . 001 | 0 | \%100 |
| 51 | M6 | X | . 001 | 001 | 0 | \%100 |
| 52 | M7 | X | 001 | 001 | 0 | \%100 |
| 53 | M8 | X | . 004 | . 004 | 0 | \%100 |
| 54 | M9 | X | . 003 | 003 | 0 | \%100 |
| 55 | M10 | X | . 002 | 002 | 0 | \%100 |
| 56 | M11 | X | . 003 | . 003 | 0 | \%100 |
| 57 | M12 | X | . 002 | . 002 | 0 | \%100 |
| 58 | M13 | X | . 001 | 001 | 0 | \%100 |
| 59 | M14 | X | . 002 | . 002 | 0 | \%100 |
| 60 | M15 | X | . 002 | 002 | 0 | \%100 |
| 61 | M16 | X | . 002 | 002 | 0 | \%100 |
| 62 | M17 | X | . 003 | 003 | 0 | \%100 |
| 63 | M18 | X | . 002 | . 002 | 0 | \%100 |
| 64 | M19 | X | . 003 | . 003 | 0 | \%100 |
| 65 | M20 | X | . 003 | . 003 | 0 | \%100 |
| 66 | M21 | X | 003 | 003 | 0 | \%100 |
| 67 | M22 | X | . 003 | . 003 | 0 | \%100 |
| 68 | M23 | X | 003 | 003 | 0 | \%3.3 |
| 69 | M24 | X | . 003 | . 003 | 0 | \%100 |

Company
MasTec
June 20, 2019
Designer
Job Number
NDN
12:56 PM
Model Name

Member Distributed Loads (BLC 25 : Ice Wind Members (120 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft.F.ksfl | End Magnitude[k/ft.F.ksfl | Start Locationfft.. | .End Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 70 | M25 | X | . 003 | 003 | 0 | \%. 1 |
| 71 | M26 | X | 003 | 003 | 0 | \%2.8 |
| 72 | M27 | X | 003 | 003 | 0 | \%. 1 |
| 73 | M28 | X | 003 | 003 | 0 | \%3.3 |
| 74 | M29 | X | 003 | 003 | 0 | \%100 |
| 75 | M30 | X | 003 | 003 | 0 | \%2.8 |
| 76 | M31 | X | 002 | 002 | 0 | \%100 |
| 77 | M32 | X | 001 | 001 | 0 | \%100 |
| 78 | M33 | X | 002 | 002 | 0 | \%100 |
| 79 | M37 | X | 001 | 001 | 0 | \%100 |
| 80 | M38 | X | 003 | 003 | 0 | \%100 |
| 81 | M39 | X | . 003 | 003 | 0 | \%100 |
| 82 | M23 | X | . 003 | 003 | \%96.7 | \%100 |
| 83 | M25 | X | 003 | 003 | \%99.9 | \%100 |
| 84 | M26 | X | 003 | 003 | \%97.2 | \%100 |
| 85 | M27 | X | 003 | 003 | \%99.9 | \%100 |
| 86 | M28 | X | . 003 | . 003 | \%96.7 | \%100 |
| 87 | M30 | X | 003 | 003 | \%97.2 | \%100 |

Member Distributed Loads (BLC 26 : Ice Wind Members (150 Deg))

|  | Member Label | Direction | Start Magnitude[k/ft,F, ksf] | End Magnitude[k/ft.F.ksf] | Start Location[ft., | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | . 001 | . 001 | 0 | \%100 |
| 2 | M2 | Z | 005 | 005 | 0 | \%100 |
| 3 | M3 | Z | . 002 | . 002 | 0 | \%100 |
| 4 | M4 | Z | . 003 | . 003 | 0 | \%100 |
| 5 | M5 | Z | . 001 | 001 | 0 | \%100 |
| 6 | M6 | Z | 001 | . 001 | 0 | \%100 |
| 7 | M7 | Z | 0 | 0 | 0 | \%100 |
| 8 | M8 | Z | . 003 | 003 | 0 | \%100 |
| 9 | M9 | Z | . 005 | 005 | 0 | \%100 |
| 10 | M10 | Z | . 003 | 003 | 0 | \%100 |
| 11 | M11 | Z | . 004 | 004 | 0 | \%100 |
| 12 | M12 | Z | . 002 | 002 | 0 | \%100 |
| 13 | M13 | Z | 0 | 0 | 0 | \%100 |
| 14 | M14 | Z | . 001 | 001 | 0 | \%100 |
| 15 | M15 | Z | . 002 | . 002 | 0 | \%100 |
| 16 | M16 | Z | . 002 | 002 | 0 | \%100 |
| 17 | M17 | Z | . 004 | 004 | 0 | \%100 |
| 18 | M18 | Z | . 001 | 001 | 0 | \%100 |
| 19 | M19 | Z | . 003 | 003 | 0 | \%. 1 |
| 20 | M20 | Z | . 003 | . 003 | 0 | \%2.8 |
| 21 | M21 | Z | . 003 | 003 | 0 | \%3.3 |
| 22 | M22 | Z | . 003 | 003 | 0 | \%100 |
| 23 | M23 | Z | . 003 | . 003 | 0 | \%3.3 |
| 24 | M24 | Z | . 003 | . 003 | 0 | \%100 |
| 25 | M25 | Z | . 003 | . 003 | 0 | \%. 1 |
| 26 | M26 | Z | . 003 | 003 | 0 | \%2.8 |
| 27 | M27 | Z | . 003 | . 003 | 0 | \%. 1 |
| 28 | M28 | Z | . 003 | . 003 | 0 | \%3.3 |
| 29 | M29 | Z | . 003 | . 003 | 0 | \%100 |
| 30 | M30 | Z | . 003 | . 003 | 0 | \%2.8 |
| 31 | M31 | Z | . 003 | . 003 | 0 | \%100 |
| 32 | M32 | Z | 0 | 0 | 0 | \%100 |
| 33 | M33 | Z | . 001 | . 001 | 0 | \%100 |
| 34 | M37 | Z | . 001 | . 001 | 0 | \%100 |
| 35 | M38 | Z | . 004 | 004 | 0 | \%100 |

Company

Member Distributed Loads (BLC 26 : Ice Wind Members (150 Deg)) (Continued)

|  | Member Label | Direction | Start Magnitude[k/ft,F,ksfl | End Magnitude[k/ft.F.ksfl | Start Locationfft, | End Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 36 | M39 | Z | 002 | . 002 | 0 | \%100 |
| 37 | M19 | Z | 003 | 003 | \%99.9 | \%100 |
| 38 | M20 | Z | 003 | 003 | \%97.2 | \%100 |
| 39 | M21 | Z | 003 | 003 | \%96.7 | \%100 |
| 40 | M23 | Z | 003 | 003 | \%96.7 | \%100 |
| 41 | M25 | Z | 003 | 003 | \%99.9 | \%100 |
| 42 | M26 | Z | 003 | 003 | \%97.2 | \%100 |
| 43 | M27 | Z | 003 | 003 | \%99.9 | \%100 |
| 44 | M28 | Z | 003 | 003 | \%96.7 | \%100 |
| 45 | M30 | Z | 003 | 003 | \%97.2 | \%100 |
| 46 | M1 | X | 0 | 0 | 0 | \%100 |
| 47 | M2 | X | . 003 | 003 | 0 | \%100 |
| 48 | M3 | X | . 001 | 001 | 0 | \%100 |
| 49 | M4 | X | 002 | 002 | 0 | \%100 |
| 50 | M5 | X | 0 | 0 | 0 | \%100 |
| 51 | M6 | X | 0 | 0 | 0 | \%100 |
| 52 | M7 | X | 0 | 0 | 0 | \%100 |
| 53 | M8 | X | . 002 | 002 | 0 | \%100 |
| 54 | M9 | X | 003 | 003 | 0 | \%100 |
| 55 | M10 | X | . 002 | 002 | 0 | \%100 |
| 56 | M11 | X | 002 | 002 | 0 | \%100 |
| 57 | M12 | X | . 001 | 001 | 0 | \%100 |
| 58 | M13 | X | 0 | 0 | 0 | \%100 |
| 59 | M14 | X | 0 | 0 | 0 | \%100 |
| 60 | M15 | X | . 001 | 001 | 0 | \%100 |
| 61 | M16 | X | 001 | 001 | 0 | \%100 |
| 62 | M17 | X | . 002 | 002 | 0 | \%100 |
| 63 | M18 | X | 0 | 0 | 0 | \%100 |
| 64 | M19 | X | 002 | 002 | 0 | \%100 |
| 65 | M20 | X | 002 | 002 | 0 | \%100 |
| 66 | M21 | X | 002 | 002 | 0 | \%100 |
| 67 | M22 | X | 002 | 002 | 0 | \%100 |
| 68 | M23 | X | . 002 | . 002 | 0 | \%3.3 |
| 69 | M24 | X | . 002 | . 002 | 0 | \%100 |
| 70 | M25 | X | 002 | 002 | 0 | \%. 1 |
| 71 | M26 | X | 002 | 002 | 0 | \%2.8 |
| 72 | M27 | X | 002 | 002 | 0 | \%. 1 |
| 73 | M28 | X | 002 | 002 | 0 | \%3.3 |
| 74 | M29 | X | . 002 | 002 | 0 | \%100 |
| 75 | M30 | X | . 002 | . 002 | 0 | \%2.8 |
| 76 | M31 | X | 001 | 001 | 0 | \%100 |
| 77 | M32 | X | 0 | 0 | 0 | \%100 |
| 78 | M33 | X | 001 | 001 | 0 | \%100 |
| 79 | M37 | X | 0 | 0 | 0 | \%100 |
| 80 | M38 | X | . 002 | . 002 | 0 | \%100 |
| 81 | M39 | X | 001 | 001 | 0 | \%100 |
| 82 | M23 | X | . 002 | 002 | \%96.7 | \%100 |
| 83 | M25 | X | 002 | 002 | \%99.9 | \%100 |
| 84 | M26 | X | . 002 | . 002 | \%97.2 | \%100 |
| 85 | M27 | X | . 002 | . 002 | \%99.9 | \%100 |
| 86 | M28 | X | . 002 | 002 | \%96.7 | \%100 |
| 87 | M30 | X | . 002 | 002 | \%97.2 | \%100 |

Company

## Member Area Loads

$\begin{array}{|cccccc}\text { Joint A } & \text { Joint B } & \text { Joint C } & \text { Joint D } & \text { Direction } & \text { Distribution }\end{array}$ Magnitude[ksf] $]$

## Basic Load Cases

|  | BLC Description | Category | X Gravity | Y Gravity | Z Gravity | Joint | Point | Distribut. | Area(Me.. | Surface(... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Dead | None |  | -1 |  |  | 15 |  |  |  |
| 2 | Ice Dead | None |  |  |  |  | 15 | 36 |  |  |
| 3 | Full Wind Antenna (0 Deq) | None |  |  |  |  | 18 |  |  |  |
| 4 | Full Wind Antenna (30 Deg) | None |  |  |  |  | 42 |  |  |  |
| 5 | Full Wind Antenna (60 Deg) | None |  |  |  |  | 42 |  |  |  |
| 6 | Full Wind Antenna (90 Deg) | None |  |  |  |  | 42 |  |  |  |
| 7 | Full Wind Antenna (120 Deg) | None |  |  |  |  | 40 |  |  |  |
| 8 | Full Wind Antenna (150 Deg) | None |  |  |  |  | 42 |  |  |  |
| 9 | Full Wind Members (0 Deg) | None |  |  |  |  |  | 81 |  |  |
| 10 | Full Wind Members (30 Deg) | None |  |  |  |  |  | 81 |  |  |
| 11 | Full Wind Members (60 Deg) | None |  |  |  |  |  | 81 |  |  |
| 12 | Full Wind Members (90 Deg) | None |  |  |  |  |  | 81 |  |  |
| 13 | Full Wind Members (120 Deg) | None |  |  |  |  |  | 81 |  |  |
| 14 | Full Wind Members (150 Deg) | None |  |  |  |  |  | 81 |  |  |
| 15 | Ice Wind Antenna (0 Deq) | None |  |  |  |  | 18 |  |  |  |
| 16 | Ice Wind Antenna (30 Deg) | None |  |  |  |  | 42 |  |  |  |
| 17 | Ice Wind Antenna (60 Deg) | None |  |  |  |  | 42 |  |  |  |
| 18 | Ice Wind Antenna (90 Deg) | None |  |  |  |  | 42 |  |  |  |
| 19 | Ice Wind Antenna (120 Deg) | None |  |  |  |  | 40 |  |  |  |
| 20 | Ice Wind Antenna (150 Deg) | None |  |  |  |  | 40 |  |  |  |
| 21 | Ice Wind Members (0 Deg) | None |  |  |  |  |  | 87 |  |  |
| 22 | Ice Wind Members (30 Deg) | None |  |  |  |  |  | 87 |  |  |
| 23 | Ice Wind Members (60 Deg) | None |  |  |  |  |  | 87 |  |  |
| 24 | Ice Wind Members (90 Deg) | None |  |  |  |  |  | 87 |  |  |
| 25 | Ice Wind Members (120 Deg) | None |  |  |  |  |  | 87 |  |  |
| 26 | Ice Wind Members (150 Deg) | None |  |  |  |  |  | 87 |  |  |
| 27 | Seismic Antenna (0 Deg) | None |  |  |  |  | 15 |  |  |  |
| 28 | Seismic Antenna (90 Deg) | None |  |  |  |  | 15 |  |  |  |
| 29 | Seismic Members (0 Deq) | None |  | -. 054 | -. 135 |  |  |  |  |  |
| 30 | Seismic Members (30 Deg) | None | 067 | -. 054 | -. 116 |  |  |  |  |  |
| 31 | Seismic Members (60 Deq) | None | 116 | -. 054 | -. 067 |  |  |  |  |  |
| 32 | Seismic Members (90 Deg) | None | 135 | -. 054 | -8.239e-... |  |  |  |  |  |
| 33 | Seismic Members (120 Deg) | None | 116 | -. 054 | . 067 |  |  |  |  |  |
| 34 | Seismic Members (150 Deg) | None | 067 | -. 054 | 116 |  |  |  |  |  |
| 35 | Seismic Members (180 Deg) | None | 1.648e-17 | -. 054 | . 135 |  |  |  |  |  |
| 36 | Seismic Members (210 Deg) | None | -. 067 | -. 054 | 116 |  |  |  |  |  |
| 37 | Seismic Members (240 Deg) | None | -. 116 | -. 054 | 067 |  |  |  |  |  |
| 38 | Seismic Members (270 Deg) | None | -. 135 | -. 054 | 2.472e-17 |  |  |  |  |  |
| 39 | Seismic Members (300 Deg) | None | -. 116 | -. 054 | -. 067 |  |  |  |  |  |
| 40 | Seismic Members (330 Deg) | None | -. 067 | -. 054 | -. 116 |  |  |  |  |  |
| 41 | Seismic Vertical Antennas | None |  |  |  |  | 15 |  |  |  |
| 42 | Man 1 ( 500 lbs ) | None |  |  |  | 1 |  |  |  |  |
| 43 | Man 2 ( 500 lbs ) | None |  |  |  | 1 |  |  |  |  |
| 44 | Man 3 ( 500 lbs ) | None |  |  |  | 1 |  |  |  |  |
| 45 | Man 4 (250 lbs) | None |  |  |  | 1 |  |  |  |  |
| 46 | Man 5 (250 lbs) | None |  |  |  | 1 |  |  |  |  |
| 47 | Man 6 (250 lbs) | None |  |  |  | 1 |  |  |  |  |


|  | Description S |  |  | B... |  | B. |  |  |  |  |  |  |  | B... |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.4D | Yes | Y | 1 | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 0^{\circ}$ | Yes | Y | 1 | 1.2 | 3 | 1 | 9 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 30^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 4 | 1 | 10 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 60^{\circ}$ Y | Yes | Y | 1 | 1.2 | 5 | 1 | 11 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 90^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 6 | 1 | 12 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 120^{\circ}$ | Yes | Y | 1 | 1.2 | 7 | 1 | 13 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 150^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 8 | 1 | 14 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 180^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 3 | -1 | 9 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 210^{\circ}$ | Yes | Y | 1 | 1.2 | 4 | -1 | 10 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 240^{\circ}$ | Yes | Y | 1 | 1.2 | 5 | -1 | 11 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 270^{\circ}$ | Yes | Y | 1 | 1.2 | 6 | -1 | 12 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 300^{\circ}$ | Yes | Y | 1 | 1.2 | 7 | -1 | 13 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 330^{\circ}$ | Yes | Y | 1 | 1.2 | 8 | -1 | 14 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 0^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 15 | 1 | 21 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 15 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 30^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 16 | 1 | 22 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 16 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 60^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 17 | 1 | 23 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 17 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 90^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 18 | 1 | 24 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 18 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 120^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 19 | 1 | 25 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 19 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 150^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 20 | 1 | 26 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 180^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 15 | -1 | 21 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 210^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 16 | -1 | 22 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 240^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 17 | -1 | 23 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 23 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 270^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 18 | -1 | 24 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 300^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 19 | -1 | 25 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 330^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 20 | -1 | 26 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 0^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 3 | . 066 | 9 | . 066 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 30^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 4 | . 066 | 10 | . 066 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 60^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 5 | . 066 | 11 | . 066 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 29 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 90^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 6 | . 066 | 12 | . 066 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 120^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 7 | . 066 | 13 | . 066 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} \mathrm{150}{ }^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 8 | . 066 | 14 | . 066 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 32 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 180^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 3 | -.0... | 9 | -.0... | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 33 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}-1+1.0 \mathrm{Wm} 210^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 4 | -.0... | 10 | -.0... | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 34 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 240^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 5 | -.0... | 11 | -.0... | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 270^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 6 | -.0... | 12 | -.0... | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 36 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 300^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 7 | -.0... | 13 | -.0... | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 37 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_1+1.0 \mathrm{Wm} 330^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 8 | -.0... | 14 | -.0... | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 38 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 0^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 3 | . 066 | 9 | . 066 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 39 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 30^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 4 | . 066 | 10 | . 066 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 60^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 5 | . 066 | 11 | . 066 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 41 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 90^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 6 | . 066 | 12 | . 066 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 42 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 120^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 7 | . 066 | 13 | . 066 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 43 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 150^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 8 | . 066 | 14 | . 066 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 44 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}=2+1.0 \mathrm{Wm} 180^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 3 | -.0... | 9 | -.0... | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 210^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 4 | -.0... | 10 | -.0... | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 46 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 240^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 5 | -.0... | 11 | -.0... | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 47 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 270^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 6 | -.0... | 12 | -.0... | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 48 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}=2+1.0 \mathrm{Wm} 300^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 7 | -.0... | 13 | -.0... | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 49 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \mathrm{Wm} 330^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 8 | -.0... | 14 | -.0... | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 50 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _3+1.0Wm $0^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 3 | . 066 | 9 | . 066 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 51 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _3 + 1.0Wm $30^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 4 | . 066 | 10 | . 066 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 52 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_3+1.0 \mathrm{Wm} 60^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 5 | . 066 | 11 | . 066 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 53 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_3+1.0 \mathrm{Wm} 90^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 6 | . 066 | 12 | . 066 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 54 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}=3+1.0 \mathrm{Wm} 120^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 7 | . 066 | 13 | . 066 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 55 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_3+1.0 \mathrm{Wm} \mathrm{150}{ }^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 8 | . 066 | 14 | . 066 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 56 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}=3+1.0 \mathrm{Wm} 180^{\circ} \mathrm{Y}$ | Yes | Y | 1 | 1.2 | 3 | -.0... | 9 | -.0... | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |

Company Designer Job Number

## Load Combinations (Continued)

|  | Description |  |  | S... B. | Fa. |  |  |  |  |  |  |  |  | B. | Fa... | B... | Fa... | B... | Fa.. |  | Fa.. | B... Fa... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 57 | 1.2D + 1.5Lm_3 + $1.0 \mathrm{Wm} 210^{\circ}$ | Yes | Y | 1 | 1.2 | 4 | -.0... | 10 | -.0... | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 58 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $3+1.0 \mathrm{Wm} \mathrm{240}$ | Yes | Y | 1 | 1.2 | 5 | -.0... | 11 | -.0.. | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 59 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $3+1.0 \mathrm{Wm} 270^{\circ}$ | Yes | Y | 1 | 1.2 | 6 | -.0... | 12 | -.0.. | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 60 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $3+1.0 \mathrm{Wm} 300^{\circ}$ | Yes | Y | 1 | 1.2 | 7 | -.0... | 13 | -.0.. | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 61 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _3 + 1.0Wm $330^{\circ}$ | Yes | Y | 1 | 1.2 | 8 | -.0... | 14 | -.0.. | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 62 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ - $10^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 63 | $1.2 \mathrm{D}+1.5 \mathrm{LV}-130^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 64 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}-160^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 65 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}-190^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 66 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ - $1120^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 67 | $1.2 \mathrm{D}+1.5 \mathrm{LV}-1150^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 68 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ - $1180^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 69 | $1.2 \mathrm{D}+1.5 \mathrm{LV}-1210^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ - $1240^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 71 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}-1270^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 72 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}-1300^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 73 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 1330^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 74 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 20^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 75 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 230^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 76 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} \_260^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 77 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 290^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 78 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ 2 $2120^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 79 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 2150^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 80 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ 2 $2180^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 81 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 2210^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 82 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ 2 $240^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 83 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 2270^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 84 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 22300^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 85 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 2330^{\circ}$ | Yes | Y | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 86 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ _ $30^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 87 | $1.2 \mathrm{D}+1.5 \operatorname{Lv} 330^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ 3 $360^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 89 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 390^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 90 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 3120^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 3150^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 92 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 3180^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 93 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 3210^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 94 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 3240^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 95 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}-3270^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 96 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 33300^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 97 | $1.2 \mathrm{D}+1.5 \mathrm{LV}-3330^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 98 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 0^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | 1 | 28 |  | 29 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 99 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 30^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | 866 | 28 | . 5 | 30 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 100 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 60^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | . 5 | 28 | . 866 | 31 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 101 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} \mathrm{90}$ | Yes | Y | 1 | 1.2 | 27 |  | 28 | 1 | 32 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 102 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 120^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | -. 5 | 28 | . 866 | 33 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 103 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 150^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | -.8... | 28 | . 5 | 34 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 104 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 180^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | -1 | 28 |  | 35 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 105 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 210^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | -.8... | 28 | -. 5 | 36 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 106 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 240^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | -. 5 | 28 | -.8.. | 37 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 107 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 270^{\circ}$ | Yes | Y | 1 | 1.2 | 27 |  | 28 | -1 | 38 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 108 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 300^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | . 5 | 28 | -.8... | 39 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |
| 109 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH} 330^{\circ}$ | Yes | Y | 1 | 1.2 | 27 | 866 | 28 | -. 5 | 40 | 1 | 40 | 1 |  |  |  |  |  |  |  |  |  |



Envelope Joint Reactions

| Joint |  |  | X [k] | LC Y [k] |  | LC Z [k] |  | LC | MX [k-ft] | LC | MY [k-ft] | LC | MZ [k-ft] | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N3 | max | 1.613 | 10 | 2.49 | 22 | 1.031 | 4 | -. 235 | 4 | 666 | 13 | -. 358 |  |
| 2 |  | min | -1.754 | 4 | 322 | 4 | -. 949 | 10 | -3.54 | 22 | -. 665 | 7 | -6.32 | 22 |
| 3 | N1 | max | 744 | 11 | 2.474 | 14 | 1.781 | 2 | 7.183 | 14 | 558 | 5 | 332 | 5 |
| 4 |  | min | -. 744 | 5 | 355 | 8 | -1.944 | 8 | . 559 | 8 | -. 556 | 11 | -. 271 | 11 |
| 5 | N5 | max | 1.83 | 12 | 2.49 | 18 | 1.134 | 2 | -. 214 | 12 | . 684 | 9 | 6.231 | 18 |
| 6 |  | min | -1.689 | 6 | 322 | 12 | -1.053 | 8 | -3.696 | 19 | -. 683 | 3 | 372 | 12 |
| 7 | Totals: | max | 3.83 | 11 | 7.022 | 14 | 3.658 | 2 |  |  |  |  |  |  |
| 8 |  | min | -3.83 | 5 | 2.608 | 8 | -3.658 | 8 |  |  |  |  |  |  |

## Envelope AISC 14th(360-10): LRFD Steel Code Checks

|  | Mem... | Shape | Code Check | Loc[ft] | LC | Shear C. | Loc[ft] | Dir | LC | phi*...phi**...phi*...phi*.. | Cb | Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | HSS4X4X3 | . 571 | 0 | 14 | . 095 | . 167 | V | 16 | 95.2..106...12.6..12.6. | .2.237 | H1 |
| 2 | M2 | HSS4X4X3 | . 575 | 0 | 22 | . 096 | 0 | y | 24 | 95.2...106...12.6...12.6. | .2.236 | H1. |
| 3 | M3 | HSS4X4X3 | . 579 | 0 | 18 | . 094 | 167 | V | 20 | 95.2..106...12.6..12.6. | .2.236 | H1.. |
| 4 | M7 | C5X6.7 | 468 | 12 | 21 | . 276 | 3.75 | y | 24 | 29.6..63.8..1.6048.226 | 1 | H1.. |
| 5 | M8 | C5X6.7 | 466 | 12 | 20 | . 273 | 3.75 | V | 16 | 29.6..63.8..1.6048.226 | 1 | H1.. |
| 6 | M9 | C5X6.7 | 475 | 12 | 15 | 275 | 3.75 | y | 25 | 29.6..63.8..1.6048.226 | 1 | H1.. |
| 7 | M10 | L2x2x3 | 306 | 1.167 | 10 | . 052 | 1.167 | z | 15 | 17.8.23.3...5581.239 | 1.432 | H2.. |
| 8 | M11 | L3x1.75x4 | 120 | 0 | 3 | . 027 | 1.771 | z | 14 | 30.9.36.45.6552.324 | 1.656 | H2. |
| 9 | M12 | L3x1.75x4 | 127 | 1.771 | 5 | . 025 | 0 | z | 14 | 30.9.36.45.6552.324 | 1.658 | H2.. |
| 10 | M13 | L2x2x3 | 306 | 1.167 | 6 | . 051 | 1.167 | $y$ | 23 | 17.8.23.3... 5581.239 | 1.438 | H2. |
| 11 | M14 | L3x1.75x4 | 153 | 1.771 | 13 | . 025 | 0 | z | 22 | 30.9.36.45.6552.324 | 1.661 | H2. |
| 12 | M15 | L3x1.75x4 | 140 | 0 | 7 | . 027 | 1.771 | z | 22 | 30.9.36.45.6552.324 | 1.656 | H2.. |
| 13 | M16 | L2x2x3 | . 307 | 1.167 | 2 | . 051 | 1.167 | V | 19 | 17.8..23.3... 5581.239 | 1.436 | H2.. |
| 14 | M17 | L3x1.75×4 | 155 | 1.771 | 9 | . 025 | 0 | z | 18 | 30.9.36.45.6552.324 | 1.658 | H 2 |
| 15 | M18 | L3x1.75x4 | 145 | 0 | 3 | . 027 | 1.771 | Z | 18 | 30.9.36.45.6552.324 | 1.661 | H2.. |
| 16 | M19 | PIPE 2.0 | 292 | 4.618 | 8 | . 044 | 4.618 |  | 9 | 19.8.32.131.8721.872 | 2.933 | H1 |
| 17 | M20 | PIPE 2.0 | 284 | 3.958 | 11 | . 067 | 3.958 |  | 13 | 23.8.32.131.8721.872 | 1.668 | H1.. |
| 18 | M21 | PIPE_2.0 | 288 | 3.958 | 17 | . 070 | 3.958 |  | 6 | 23.8.32.131.8721.872 | 1.719 | H1.. |
| 19 | M22 | PIPE 2.0 | 261 | 6.456 | 5 | . 061 | 6.456 |  | 9 | 11.4.32.131.8721.872 | 3.551 | H1.. |
| 20 | M23 | PIPE_2.0 | 278 | 3.958 | 14 | . 067 | 1.042 |  | 2 | 23.8.32.131.8721.872 | 1.715 | H1.. |
| 21 | M24 | PIPE 2.0 | 239 | 6.456 | 13 | . 058 | 6.456 |  | 5 | 11.4.32.131.8721.872 | 4.28 | H1. |
| 22 | M25 | PIPE 2.0 | 294 | 4.618 | 4 | . 043 | 1.715 |  | 5 | 19.8.32.131.8721.872 | 1.217 | H1 |
| 23 | M26 | PIPE 2.0 | 260 | 3.958 | 7 | . 064 | 1.042 |  | 9 | 23.8.32.131.8721.872 | 1.637 | H1.. |
| 24 | M27 | PIPE 2.0 | 293 | 4.618 | 12 | . 043 | 1.715 |  | 13 | 19.8.32.131.8721.872 | 1.215 | H1. |
| 25 | M28 | PIPE 2.0 | 280 | 3.958 | 22 | . 068 | 2.5 |  | 10 | 23.8.32.131.8721.872 | 1.708 | H1.. |
| 26 | M29 | PIPE_2.0 | 241 | 6.456 | 10 | . 058 | 6.456 |  | 13 | 11.4.32.131.8721.872 | 2.898 | H1. |
| 27 | M30 | PIPE 2.0 | 257 | 3.958 | 3 | . 064 | 1.042 |  | 5 | 23.8.32.131.8721.872 | 1.665 | H |
| 28 | M31 | PIPE 2.0 | 300 | 11 | 3 | 317 | 11 |  | 2 | 6.83132 .131 .8721 .872 | 3.425 | H3.. |
| 29 | M32 | PIPE 2.0 | 298 | 11 | 11 | . 319 | 11 |  | 10 | 6.831132 .131 .8721 .872 | 3.469 | H3.. |
| 30 | M33 | PIPE 2.0 | 302 | 1 | 12 | . 323 | 1 |  | 6 | 6.831132 .131 .8721 .872 | 3.616 | H3.. |
| 31 | M37 | L2.5x $2.5 \times 4$ | . 582 | 1.458 | 6 | . 066 | 0 | z | 6 | 35.9..38.5..1.1142.537 | 1.618 | H2. |
| 32 | M38 | L2.5x2.5x4 | 579 | 1.458 | 10 | . 065 | 0 | Z | 10 | 35.9..38.5..1.1142.537 | 1.617 | H2.. |
| 33 | M39 | L2.5x2.5x4 | . 573 | 0 | 2 | . 065 | 1.458 | $y$ | 2 | 35.9..38.5..1.1142.537 | 1.602 | H2.. |

## APPENDIX D

## ADDITIONAL CALCUATIONS

## Bolt Calcuations:

| Bolt Size: | $5 / 8$ | in |
| :---: | :---: | :---: |
| \# Bolts: | 4 |  |
| Plate Width: | 8 | in |
| Plate Height: | 8 | in |
| Bolt H Gap: | 6 | in |
| Bolt V Gap: | 6 | in |
| Plate T: | 0.75 | in |
| Bolt Grade: | A 325 N |  |
| Fu |  |  |
| bolt | 120 | ksi |
| r: | 4.243 | in $^{\text {J: }}$ |
| 72.000 | $\mathrm{in}^{4} / \mathrm{in}^{2}$ |  |
| Bolt Area, Normal: | 0.307 |  |
| Bolt Area, Net Tensile: | 0.226 | $\mathrm{in}^{2}$ |



| Allowable Shear: | 12.4 | kip |
| :---: | :---: | :---: |
| Allowable Tension: | 20.3 | kip |


| Tension Capacity: | $35.8 \%$ |
| :---: | ---: |
| Shear Capacity: | $41.0 \%$ |
| Combined Capacity: | $19.9 \%$ |


| Bolt Capacity: | $41.0 \%$ |
| :--- | ---: |

## Plate Calculations:

| Horizontal Member Height: | 4 | in |
| :---: | :---: | :---: |
| Horizontal Member Width: | 4 | in |
| Plate Grade: | A36 |  |
| Plate Fy: | 36 | ksi |


| $\mathrm{Mx}=$ | 1.752 | $\mathrm{k}^{*}$ in |
| ---: | :---: | :--- |
| $\mathrm{Mz}=$ | 14.488 | $\mathrm{k}^{*}$ in |


| $\mathrm{Zx}=$ | 1.125 | $\mathrm{in}^{3}$ |
| ---: | :--- | :--- |
| $\mathrm{Zz}=$ | 1.125 | $\mathrm{in}^{3}$ |


| $\varnothing \mathrm{Mpy}(\mathrm{X})=$ | 36.450 | $\mathrm{k}-\mathrm{in}$ |
| :--- | :--- | :--- |
| $\varnothing \mathrm{Mpx}(\mathrm{X})=$ | 36.450 | $\mathrm{k}-\mathrm{in}$ |



## Address:

No Address at This Location

## ASCE 7 Hazards Report



## Wind

## Results:

Wind Speed:
10-year MRI
25-year MRI
50-year MRI
100-year MRI
Data Source:

117 Vmph
76 Vmph
85 Vmph
90 Vmph
97 Vmph
ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of March 12, 2014

Fri May 172019

## Date Accessed:

Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability $=$ $0.00143, \mathrm{MRI}=700$ years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

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## Seismic

Site Soil Class:
D - Stiff Soil

## Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.253 |
| :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.07 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.598 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.4 |
| $\mathrm{~S}_{\mathrm{Ms}}:$ | 0.404 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.168 |


| $\mathrm{S}_{\mathrm{DS}}:$ | 0.269 |
| :--- | :--- |
| $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.112 |
| $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{PGA}:$ | 0.148 |
| $\mathrm{PGA}_{\mathrm{M}}:$ | 0.222 |
| $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.505 |
| $\mathrm{I}_{\mathrm{e}}:$ | 1 |

## Seismic Design Category <br> B




Data Accessed:
Date Source:

Fri May 172019
USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating
Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2.
Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.

AMERICAN SOCIETY OF CIVIL ENGINEERS

## Ice

## Results

Ice Thickness:
Concurrent Temperature:
Gust Speed:
Data Source:
Date Accessed:
0.75 in .

15 F
50 mph
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Fri May 172019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

## APPENDIX E

MODIFICATION DRAWINGS




TECOMMENDATIONS:
ENFALLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED THE EFFICIENCY AND EFFECTIVENESS OF DELLVERING A MI REPORT: - ITIS SUGGESTED TAAT THE GC PROVIDE A MIIIMUM OF 5 BUSIINESS DAYS
NOTICE. PREFERABLY 10 , TO THE MIINSPECTOR AS TO WHEN THE SITE WILL BE READY FOR THE MI TO BE CONDUCTED.

- THE GC AND MINSPECOR COORDINATE CLOSELY THROUGHOUT THE
ENTIRE PROJECT. - ENTIRE ARONECT.
- WHEN POSSIBLE IT IS PREFERRED TO HAVE THE GC AND MI INSPECTOR
ON-SITE SIMULTANEOUSLY FOR ANY GUY WIRE TENSIONING OR RE-TENSIONING OPERATIONS.
- IT AMY BE BENEFICIAL TO INSTALL ALL TOWER MODIFICATIONS PRIOR TO
CONOUCTING THE FOUNDATION INSPECTIONS TO ALLOW FOUNDATION

 DISPOSAL WHEN THE MI INSPECTOR IS ON SITE.
CANCELLATION OR DELAYS IN SCHEDULED MI: IF THE GC AND MI INSPECTOR AGREE TO A DATE ON WHHCH THE MI WILL BE







 |  |  |  |  |  | $\sum_{亏}^{5}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |



RAPHAELI. MOHAMED, PE.PENg
SENIOR DIRECTOR OF EEGINEERING
 0




 THE CONTRACTORIS ATTESTING THAT HE HAS SUFFIIIIENT
EXPERIENCE, ABLITY, AND KNWLEOE OF TE WORK TO
EE
PERORMED AND IS PROPERLY LLCENSED AND REGISTERED TO
$\qquad$ THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING ALL

$$
\begin{aligned}
& \text { BE RESOLVED BEFORE THE CONTRACTOR MAY PROCEED WITH THE } \\
& \text { PROJECT. } \\
& \text { ANY WORK PERFORMED WITHOUT A PREFABRICATION MAPPING II } \\
& \text { DONE AT THE RISK OF THE CONTRACTOR ANDIOR FABRICATOR. }
\end{aligned}
$$

 DRAWINGS, THE MANOFACTURER SPECIICATIONS SHALL GOVERN.
 MATERIALS SHALL BE WARRANTED FOR ONE YEAR FROM

 . THE CONTRACTOR IS RESPONSIBLE FOR ALL CONSTRUCTION MEANS THE CONTRACTOR IS RESPONSIBLE FOR ALL CONSTRUCTION MEAN,
AND METHODS. INCLUDING BUT NOT LIMTED TO. ERETON PLANS, CONSTRUCTION OF THE RROPOSED WORS SHALL MEET ANSIIASSE
A10.48, OSHA, AND GENERAL INDUSTRY STANDARDE. ALLRIGGING
PLANS SHALL AD A


## MODIFICATION MATERIALS

| MODIFICATION MATERIALS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| SCOPE | SHAPE | GRADE | YIELD STRENGTH (Fy) | ULTIMATE STRENGTH (Fu) |
| ALL | PIPE | A53 GR. B | 35 KSI | 60 KSI |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |





## Exhibit F

## Power Density/RF Emissions Report

## Transcom Engineering, Inc.

# Radio Frequency Emissions Analysis Report 

T-MOBILE Existing Facility
Site ID: CT11071E
Stamford/ MP X32/ Den Rd
70 Guinea Road (Girl Scout Camp)
Stamford, CT 06903
June 12, 2019

Transcom Engineering Project Number: 737001-0153

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of FCC <br> general population <br> allowable limit: | $\mathbf{1 3 . 3 2 \%}$ |

# Transcom Engineering, Inc. 

June 12, 2019
T-MOBILE
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, CT 6009

## Emissions Analysis for Site: CT11071E - Stamford/ MP X32/ Den Rd

Transcom Engineering, Inc ("Transcom") was directed to analyze the proposed upgrades to the T-MOBILE facility located at 70 Guinea Road (Girl Scout Camp), Stamford, CT, for the purpose of determining whether the emissions from the Proposed T-MOBILE Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR $1.1307(\mathrm{~b})(1)-(\mathrm{b})(3)$, to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$. The general population exposure limits for the $600 \mathrm{MHz} \& 700 \mathrm{MHz}$ bands are approximately $400 \mu \mathrm{~W} / \mathrm{cm}^{2}$ and $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$ respectively. The general population exposure limit for the 1900 MHz (PCS) and 2100 MHz (AWS) bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

## Transcom Engineering, Inc.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## Transcom Engineering, Inc.

## CALCULATIONS

Calculations were performed for the proposed upgrades to the T-MOBILE antenna facility located at 70
Guinea Road (Girl Scout Camp), Stamford, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-MOBILE is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was focused at the base of the tower. For this report the sample point is the top of a 6 -foot person standing at the base of the tower.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in Table 1:

| Technology | Frequency Band | Channel Count | Transmit Power per <br> Channel (W) |
| :---: | :---: | :---: | :---: |
| LTE | $1900 \mathrm{MHz}(\mathrm{PCS})$ | 4 | 40 |
| LTE | $2100 \mathrm{MHz}($ AWS $)$ | 2 | 60 |
| GSM | $1900 \mathrm{MHz}($ PCS $)$ | 1 | 15 |
| UMTS | $2100 \mathrm{MHz}($ AWS $)$ | 1 | 40 |
| LTE / 5G NR | 600 MHz | 2 | 40 |
| LTE | 700 MHz | 2 | 20 |

Table 1: Channel Data Table

## Transcom Engineering, Inc.

The following antennas listed in Table 2 were used in the modeling for transmission in the $600 \mathrm{MHz}, 700$ $\mathrm{MHz}, 1900 \mathrm{MHz}(\mathrm{PCS})$ and 2100 MHz (AWS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

| Sector | Antenna <br> Number | Antenna Make / Model | Antenna <br> Centerline <br> $(\mathrm{ft})$ |
| :---: | :---: | :---: | :---: |
| A | 1 | Ericsson AIR32 B66A / B2A | 118 |
| A | 2 | Ericsson AIR21 B2A/B4P | 118 |
| A | 3 | RFS APXVAARR24_43-U-NA20 | 118 |
| B | 1 | Ericsson AIR32 B66A / B2A | 118 |
| B | 2 | Ericsson AIR21 B2A/B4P | 118 |
| B | 3 | RFS APXVAARR24_43-U-NA20 | 118 |
| C | 1 | Ericsson AIR32 B66A / B2A | 118 |
| C | 2 | Ericsson AIR21 B2A/B4P | 118 |
| C | 3 | RFS APXVAARR24 43-U-NA20 | 118 |

Table 2: Antenna Data

All calculations were done with respect to uncontrolled / general population threshold limits.

Cable losses were factored in the calculations for this site. Since all $\mathbf{2 1 0 0} \mathbf{~ M H z}$ (AWS) UMTS radios are ground mounted the following cable loss values were used. or each ground mounted $\mathbf{2 1 0 0} \mathbf{~ M H z}$ (AWS) UMTS radio there was $\mathbf{1 . 5 8} \mathbf{d B}$ of cable loss calculated into the system gains / losses for this site. These values were calculated based upon the manufacturers specifications for 149 feet of $\mathbf{1 - 5 / 8}$ " coax.

## Transcom Engineering, Inc.

## RESULTS

Per the calculations completed for the proposed T-MOBILE configurations Table 3 shows resulting emissions power levels and percentages of the FCC's allowable general population limit.

| $\begin{gathered} \text { Antenna } \\ \text { ID } \\ \hline \end{gathered}$ | Antenna Make / Model | Frequency Bands | Antenna Gain (dBd) | Channel Count | Total TX Power (W) | ERP (W) | MPE \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Antenna } \\ \text { A1 } \\ \hline \end{gathered}$ | Ericsson AIR32 B66A / B2A | $\begin{aligned} & 1900 \mathrm{MHz} \text { (PCS) / } \\ & 2100 \mathrm{MHz} \text { (AWS) } \\ & \hline \end{aligned}$ | 15.85 / 15.85 | 6 | 280 | 10,768.57 | 3.08 |
| $\begin{gathered} \hline \text { Antenna } \\ \text { A2 } \\ \hline \end{gathered}$ | Ericsson AIR21 B2A/B4P | $\begin{aligned} & 1900 \mathrm{MHz} \text { (PCS) / } \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | 15.9 / 15.9 | 2 | 55 | 1,665.15 | 0.48 |
| Antenna A3 | RFS APXVAARR24_43-U-NA20 | $600 \mathrm{MHz} / 700 \mathrm{MHz}$ | 12.95 / 13.35 | 4 | 120 | 2,443.03 | 1.66 |
| Sector A Composite MPE\% |  |  |  |  |  |  | 5.22 |
| Antenna | Ericsson AIR32 B66A / B2A | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \\ & \hline \end{aligned}$ | 15.85 / 15.85 | 6 | 280 | 10,768.57 | 3.08 |
| $\begin{gathered} \text { Antenna } \\ \text { B2 } \end{gathered}$ | $\begin{gathered} \text { Ericsson } \\ \text { AIR21 B2A/B4P } \end{gathered}$ | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | 15.9 / 15.9 | 2 | 55 | 1,665.15 | 0.48 |
| $\begin{gathered} \text { Antenna } \\ \text { B3 } \\ \hline \end{gathered}$ | $\begin{gathered} \text { RFS } \\ \text { APXVAARR24_43-U-NA20 } \end{gathered}$ | $600 \mathrm{MHz} / 700 \mathrm{MHz}$ | 12.95 / 13.35 | 4 | 120 | 2,443.03 | 1.66 |
| Sector B Composite MPE\% |  |  |  |  |  |  | 5.22 |
| Antenna $\mathrm{C} 1$ | Ericsson AIR32 B66A / B2A | $\begin{aligned} & 1900 \mathrm{MHz} \text { (PCS) / } \\ & 2100 \mathrm{MHz} \text { (AWS) } \\ & \hline \end{aligned}$ | 15.85 / 15.85 | 6 | 280 | 10,768.57 | 3.08 |
| Antenna $\mathrm{C} 2$ | $\begin{gathered} \text { Ericsson } \\ \text { AIR21 B2A/B4P } \\ \hline \end{gathered}$ | $\begin{aligned} & 1900 \mathrm{MHz} \text { (PCS) / } \\ & 2100 \mathrm{MHz} \text { (AWS) } \\ & \hline \end{aligned}$ | 15.9 / 15.9 | 2 | 55 | 1,665.15 | 0.48 |
| Antenna C3 | RFS APXVAARR24_43-U-NA20 | $600 \mathrm{MHz} / 700 \mathrm{MHz}$ | 12.95 / 13.35 | 4 | 120 | 2,443.03 | 1.66 |
| Sector C Composite MPE\% |  |  |  |  |  |  | 5.22 |

Table 3: T-MOBILE Emissions Levels

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The Following table (table 4) shows all additional carriers on site and their MPE\% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum T-MOBILE MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, all three sectors have the same configuration yielding the same results on all three sectors. Table 5 below shows a summary for each T-MOBILE Sector as well as the composite MPE value for the site.

| Site Composite MPE\% |  |
| :---: | :---: |
| Carrier | MPE\% |
| T-MOBILE - Max Per Sector Value | $\mathbf{5 . 2 2} \%$ |
| Sprint | $2.29 \%$ |
| AT\&T | $2.81 \%$ |
| Verizon Wireless | $2.81 \%$ |
| Metricom | $0.00 \%$ |
| Nextel | $0.19 \%$ |
| Site Total MPE \%: | $\mathbf{1 3 . 3 2} \%$ |

Table 4: All Carrier MPE Contributions

| T-MOBILE Sector A Total: | $5.22 \%$ |
| ---: | :---: |
| T-MOBILE Sector B Total: | $5.22 \%$ |
| T-MOBILE Sector C Total: | $5.22 \%$ |
| Site Total: |  |

Table 5: Site MPE Summary

## Transcom Engineering, Inc.

FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. Table 6 below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated T-MOBILE sector(s). For this site, all three sectors have the same configuration yielding the same results on all three sectors.

| T-MOBILE _Frequency Band / Technology <br> Max Power Values <br> (Per Sector) | \# <br> Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Frequency (MHz) | $\begin{aligned} & \text { Allowable } \\ & \text { MPE } \\ & \left(\mu W / \mathbf{c m}^{2}\right) \end{aligned}$ | Calculated \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T-Mobile 1900 MHz (PCS) LTE | 4 | 1,538.37 | 118 | 17.64 | 1900 MHz (PCS) | 1000 | 1.76\% |
| T-Mobile 2100 MHz (AWS) LTE | 2 | 2,307.55 | 118 | 13.23 | 2100 MHz (AWS) | 1000 | 1.32\% |
| T-Mobile 1900 MHz (PCS) GSM | 1 | 583.57 | 118 | 1.67 | 1900 MHz (PCS) | 1000 | 0.17\% |
| T-Mobile 2100 MHz (AWS) UMTS | 1 | 1,081.58 | 118 | 3.10 | 2100 MHz (AWS) | 1000 | 0.31\% |
| T-Mobile 600 MHz LTE / 5G NR | 2 | 788.97 | 118 | 4.52 | 600 MHz | 400 | 1.13\% |
| T-Mobile 700 MHz LTE | 2 | 432.54 | 118 | 2.48 | 700 MHz | 467 | 0.53\% |
|  |  |  |  |  |  | Total: | 5.22\% |

Table 6: T-MOBILE Maximum Sector MPE Power Values

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## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-MOBILE facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| T-MOBILE Sector | Power Density Value (\%) |
| ---: | :--- |
| Sector A: | $5.22 \%$ |
| Sector B: | $5.22 \%$ |
| Sector C: | $5.22 \%$ |
| T-MOBILE Maximum | $5.22 \%$ |
| Total (per sector): |  |
| Site Total: | $13.32 \%$ |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{1 3 . 3 2} \%$ of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


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