# STATE OF CONNECTICUT 

connecticut siting council
Ten Franklin Square, New Britain, CT 06051
Phone: (860) 827-2935 Fax: (860) 827-2950
E-Mail: siting.council@ct.gov
Web Site: portal.ct.gov/csc

## VIA ELECTRONIC MAIL

September 25, 2023

Kenneth C. Baldwin, Esq. Robinson \& Cole LLP
280 Trumbull Street
Hartford, CT 06103-3597
kbaldwin@rc.com
RE: TS-VER-134-230731 - Cellco Partnership d/b/a Verizon Wireless request for an order to approve tower sharing at an existing telecommunications facility located at 169 Hampden Road, Stafford, Connecticut. Request for Project Change.

## Dear Attorney Baldwin:

The Connecticut Siting Council (Council) is in receipt of the correspondence dated September 20, 2023 regarding a project change for the above-referenced tower share request approved by the Council on August 17, 2023.

Pursuant to Condition No. 1 of the Council's August 17, 2023 tower share approval, the request to install three model MT6413-77A antennas, three model RF4461d-13A remote radio heads (RRHs), and three model RT4423-48A RRHs due to the unavailability of the approved antenna and RRH models is hereby approved.

This approval applies only to the project change referenced in the correspondence dated September 20, 2023.

Please be advised that deviations from the standards established by the Council in the tower share approval are enforceable under the provisions of Connecticut General Statutes $\S 16-50 \mathrm{u}$.

Thank you for your attention and cooperation.
Sincerely,


Melanie A. Bachman
Executive Director
MAB/ANM/lm
c: The Honorable Salviero Titus, First Selectperson, Town of Stafford (staffordtownhall@staffordct,org)

## Robinson+Cole

Kenneth C. Baldwin

280 Trumbull Street
Hartford, CT 06103-3597
Main (860) 275-8200
Fax (860) 275-8299
kbaldwin@rc.com
Direct (860) 275-8345
Also admitted in Massachusetts and New York

September 20, 2023
Melanie A. Bachman, Esq.
Executive Director/Staff Attorney
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## Re: TS-VER-134-230731 - Cellco Partnership d/b/a Verizon Wireless - 169 Hampden Road, Stafford, Connecticut

## Request for Staff Approval of Minor Changes for Equipment Modifications

## Dear Attorney Bachman:

On August 17, 2023, the Siting Council approved the above referenced application permitting Cellco Partnership d/b/a Verizon Wireless ("Cellco") to share the telecommunications facility located at 169 Hampden Road in Stafford. Since receiving that approval, Cellco has decided to change certain antenna and remote radio head ("RRH") models and seeks staff approval for these changes.

In lieu of three (3) model MT6407-77A antennas, Cellco will install three (3) model MT6413-77A antennas. Likewise, in lieu three (3) model RF4440d-13A RRHs and three (3) model RF4401-48A RRHs, Cellco will install three (3) RF4461d-13A RRHs and three (3) RT4423-48A RRHs. All new equipment will be installed on Cellco's antenna mounting system.

Enclosed is a revised Structural Analysis Report, a revised Structural Analysis \& Design Report (Mount Analysis), an updated set of project plans, and specifications for the new antennas and RRHs Cellco intends to install. Cellco respectfully requests staff approval of these minor equipment modifications.

Please contact me if you have any questions or need any additional information.


Kenneth C. Baldwin
Attachments
Copy: Tim Parks

## $P$ P PAUL J.FORD \& COMPANY

## Report Date: July 31, 2023

| Client: | Everest Infrastructure Partners <br> Two Allegheny Center <br>  <br> Pittsburgh, PA 15212 |
| :--- | :--- |
|  | Attn: Vince Larson <br> $(724)$ 996-7847 <br> vince.larson@everestinfrastructure.com |
|  | Existing 180-ft Guyed Tower |
|  | 1267993 |
| Structure: | Stafford 1 CDT |
| FCC ASR \#: | 596025 |
| Site Name: | 169 Hampden Rd |
| Site Reference \#: | Stafford Springs, Tolland County, CT <br> Site Address: <br> City, County, State: <br> Latitude, Longitude: |
|  | $41.999581^{\circ},-72.355646^{\circ}$ |
| PJF Project: | A13323-0004.002.8700 |

Paul J. Ford and Company is pleased to submit this "Structural Analysis Report" to determine the tower stress level.

## Analysis Criteria:

This analysis utilizes an ultimate 3-second gust wind speed of 117 mph as required by the 2022 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

## Proposed Appurtenance Loads:

The structure was analyzed with the loading configuration shown in Table 1 of this report.

## Summary of Analysis Results:

| Existing Structure: | Pass $-58.7 \%$ |
| :--- | :--- |
| Existing Foundation: | Pass $-91.8 \%$ |

We at Paul J. Ford and Company appreciate the opportunity of providing our continuing professional services to you and Everest Infrastructure Partners. If you have any questions or need further assistance on this or any other projects, please give us a call.

Respectfully Submitted by:
Paul J. Ford and Company


## TABLE OF CONTENTS

## 1) INTRODUCTION

## 2) ANALYSIS CRITERIA

Table 1 - Equipment Configuration
3) ANALYSIS PROCEDURE

Table 2 - Documents Provided
3.1) Analysis Method
3.2) Assumptions
4) ANALYSIS RESULTS

Table 3 - Section Capacity (Summary)
Table 4 - Tower Component Stresses vs. Capacity
4.1) Recommendations
5) APPENDIX A
tnxTower Output
6) APPENDIX B

Base Level Drawing
7) APPENDIX C

Additional Calculations

## 1) INTRODUCTION

This tower is a 180 ft Guyed tower designed by Rohn in April 1995. Per site photos an additional guy cable was added at the 120' level. Cable sizes were taken from previous analysis by Nudd.

## 2) ANALYSIS CRITERIA

TIA-222 Revision:
Risk Category:
Wind Speed:
Exposure Category:
Topographic Factor:
Ice Thickness:
Wind Speed with Ice:
Service Wind Speed:

TIA-222-H
II
117 mph
B
1
1.5 in

50 mph
60 mph

Table 1 - Equipment Configuration

| Status | Mounting Level (ft) | Center Line Elevation (ft) | $\begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}$ | Antenna Model | Mount | Number of Feed Lines | $\begin{array}{\|l} \text { Feed } \\ \text { Line } \\ \text { Size } \\ \text { (in) } \\ \hline \end{array}$ | $\left\lvert\, \begin{gathered} \text { Coax } \\ \text { Location } \end{gathered}\right.$ | Owner/ Tenant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Existing | 179.0 | 187.0 | 1 | $16 \mathrm{ft} \times 2.5$ " omni whip | - | 2 | 7/8 | C | Unk |
| To be Removed | 174.0 | 174.0 | 1 | - | Generic 3.5' $\times 6$ ' sidearm | - | - | - | Unk |
|  | 171.0 | 175.0 | 1 | DB809DK-Y | Sector Mount | 4 | $11 / 4$ | B | Unk |
|  |  | 171.0 | 3 | $1900 \mathrm{MHz} 4 \times 45 \mathrm{~W}$ RRH |  |  |  |  | Sprint |
|  |  |  | 3 | APXV9ERR18-C w/ Mount Pipe |  |  |  |  |  |
|  |  |  | 3 | TD-RRH8x20 |  |  |  |  |  |
|  |  |  | 3 | DT465B-2XR w/ Mount Pipe |  |  |  |  |  |
| Future |  |  | 6 | RRH $2 \times 50-800$ w/Notch Filter | (3) Site Pro 1 VFA12-HD | $\begin{aligned} & 3 \\ & 1 \end{aligned}$ | $\begin{array}{ll} 1 & 5 / 8 \\ 1 & 1 / 4 \end{array}$ | B | T-Mobile |
|  |  |  | 3 | AIR6449 B41 w/ Mount Pipe |  |  |  |  |  |
|  |  |  | 3 | RADIO 4460 B2/B25 B66_TMO |  |  |  |  |  |
|  |  |  | 3 | $\begin{aligned} & \text { RADIO } 4480 \\ & \text { B71_TMO } \end{aligned}$ |  |  |  |  |  |
|  |  |  | 3 | APXVAALL24_43-UNA20 w/ Mount Pipe |  |  |  |  |  |
| Existing | 163.0 | 167.0 | 1 | PD201 | $5^{\prime \prime} \times 2.375^{\prime \prime}$ <br> Pipe Mount | 1 | 7/8 | C | Unk |


| Status | Mounting Level (ft) | Center Line Elevation (ft) | $\left.\begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered} \right\rvert\,$ | Antenna Model | Mount | Number of Feed Lines | Feed <br> Line <br> Size <br> (in)$\|$ | $\left\|\begin{array}{c} \text { Coax } \\ \text { Location } \end{array}\right\|$ | Owner/ Tenant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Proposed | 153.0 | 154.0 | 3 | $\begin{aligned} & \text { MT6413-77A wl } \\ & \text { Mount Pipe } \end{aligned}$ | (3) Site Pro <br> 1 VFA12-HD | 2 | $11 / 4$ | B | Verizon |
|  |  | 153.0 | 3 | NHH-65B-R2B w/ Mount Pipe |  |  |  |  |  |
|  |  |  | 3 | NHHSS-65B-R2BT4 w/ Mount Pipe |  |  |  |  |  |
|  |  |  | 3 | B2/B66 RRH ORAN |  |  |  |  |  |
|  |  |  | 3 | RF4461d-13A |  |  |  |  |  |
|  |  |  | 3 | RT4423-48A |  |  |  |  |  |
|  |  |  | 1 | 12 OVP |  |  |  |  |  |
| To be removed | 150.0 | 150.0 | - | - | Sector Mount | - | - | - | Unk |
| Existing | 121.0 | 129.0 | 1 | DB420 | Generic 2' x <br> 3' sidearm | 1 | 7/8 | C | Unk |
| Existing | 77.0 | 81.0 | 1 | PD201 | $5^{\prime \prime} \times 2.375^{\prime \prime}$ <br> Pipe Mount | 1 | 1/2 | C | Unk |

## 3) ANALYSIS PROCEDURE

Table 2 - Documents Provided

| Document | Remarks | Reference |
| :---: | :---: | :---: |
| Tower Manufacturer Drawings | Rohn, 4/13/1995 | B951658/D950801 |
| Tower Inventory | TEP, 2/11/2023 | 306609.609527 |
| Previous Analysis | Nudd, $9 / 6 / 2021$ | $121-23082$ |

## 3.1) Analysis Method

tnxTower (version 8.1.1.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

## 3.2) Assumptions

1) Tower and structures were maintained in accordance with the TIA-222 Standard.
2) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
3) At the time of analysis, foundation information and/or a site-specific geotechnical report were not available. However, the base design reactions are noted on the original drawings. Assuming the existing foundation was properly designed for this loading, we have compared them to the reactions of this analysis.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J . Ford and Company should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 3 - Section Capacity (Summary)

| Section No. | Elevation (ft) | Component Type | Size | Critical Element | P (K) | $\begin{gathered} \text { SF*P_allow } \\ (\mathrm{K}) \end{gathered}$ | $\begin{gathered} \% \\ \text { Capacity } \end{gathered}$ | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 180-160 | Leg | Pipe $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \mathrm{XS})$ | 2 | -12.09 | 62.91 | 19.2 | Pass |
| T2 | 160-140 | Leg | Pipe $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \mathrm{XS})$ | 60 | -17.95 | 62.91 | 28.5 | Pass |
| T3 | 140-120 | Leg | Pipe $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \mathrm{XS})$ | 116 | -18.94 | 62.91 | 30.1 | Pass |
| T4 | 120-100 | Leg | Pipe $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \mathrm{XS})$ | 173 | -24.20 | 62.91 | 38.5 | Pass |
| T5 | 100-80 | Leg | Pipe 2.875" $\times 0.276^{\prime \prime}$ (2.5 XS) | 229 | -32.93 | 101.43 | 32.5 | Pass |
| T6 | 80-60 | Leg | Pipe $2.875^{\prime \prime} \times 0.276^{\prime \prime}$ (2.5 XS) | 287 | -32.68 | 79.98 | 40.9 | Pass |
| T7 | 60-40 | Leg | Pipe 2.875" $\times 0.203^{\prime \prime}$ (2.5 STD) | 319 | -35.24 | 61.33 | 57.5 | Pass |
| T8 | 40-20 | Leg | Pipe $2.875^{\prime \prime} \times 0.203^{\prime \prime}(2.5$ STD) | 352 | -36.00 | 61.33 | 58.7 | Pass |
| T9 | 20-4.81771 | Leg | Pipe 2.875" $\times 0.276^{\prime \prime}$ (2.5 XS) | 385 | -35.54 | 79.98 | 44.4 | Pass |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 \mathrm{e}-007 \end{gathered}$ | Leg | Pipe $2.875^{\prime \prime} \times 0.276^{\prime \prime}(2.5 \mathrm{XS})$ | 413 | -36.40 | 77.52 | 46.9 | Pass |
| T1 | 180-160 | Diagonal | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 15 | -1.67 | 6.52 | 25.6 | Pass |
| T2 | 160-140 | Diagonal | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 114 | -1.36 | 6.52 | 20.8 | Pass |
| T3 | 140-120 | Diagonal | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 127 | -1.20 | 6.52 | 18.3 | Pass |
| T4 | 120-100 | Diagonal | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 181 | -0.75 | 6.52 | 11.5 | Pass |
| T5 | 100-80 | Diagonal | Pipe 1.5 " $\times 0.058^{\prime \prime}$ ( 16 ga ) | 238 | -1.95 | 6.52 | 29.9 | Pass |
| T6 | 80-60 | Diagonal | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 316 | -1.57 | 6.52 | 24.2 | Pass |
| T7 | 60-40 | Diagonal | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 351 | -0.97 | 6.52 | 14.8 | Pass |
| T8 | 40-20 | Diagonal | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}$ ( 16 ga ) | 361 | -0.59 | 6.52 | 9.1 | Pass |
| T9 | 20-4.81771 | Diagonal | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 397 | -0.83 | 6.52 | $\begin{gathered} 12.8 \\ 13.3(b) \\ \hline \end{gathered}$ | Pass |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 e-007 \end{gathered}$ | Horizontal | L $4 \times 4 \times 1 / 4$ | 421 | 0.67 | 62.86 | 1.1 | Pass |
| T1 | 180-160 | Top Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 4 | 0.04 | 9.93 | $\begin{gathered} 0.4 \\ 0.7(b) \end{gathered}$ | Pass |
| T2 | 160-140 | Top Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 62 | 0.46 | 10.43 | $\begin{gathered} 4.4 \\ 7.4 \text { (b) } \\ \hline \end{gathered}$ | Pass |
| T3 | 140-120 | Top Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 118 | -0.35 | 7.33 | $\begin{gathered} 4.8 \\ 5.6 \text { (b) } \end{gathered}$ | Pass |
| T4 | 120-100 | Top Girt | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 176 | 2.42 | 10.43 | $\begin{gathered} 23.2 \\ 38.9(b) \end{gathered}$ | Pass |
| T5 | 100-80 | Top Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 234 | -0.57 | 7.40 | $\begin{gathered} 7.7 \\ 9.2 \text { (b) } \end{gathered}$ | Pass |
| T6 | 80-60 | Top Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 291 | -0.57 | 7.40 | $\begin{gathered} 7.7 \\ 12.2 \text { (b) } \end{gathered}$ | Pass |
| T7 | 60-40 | Top Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 324 | -0.61 | 7.40 | $\begin{gathered} 8.3 \\ 9.9 \text { (b) } \\ \hline \end{gathered}$ | Pass |
| T8 | 40-20 | Top Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 357 | -0.62 | 7.40 | $\begin{gathered} 8.4 \\ 10.0 \text { (b) } \end{gathered}$ | Pass |
| T9 | 20-4.81771 | Top Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058$ " (16 ga) | 390 | -0.62 | 7.40 | $\begin{gathered} 8.4 \\ 10.0(\mathrm{~b}) \\ \hline \end{gathered}$ | Pass |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 \mathrm{e}-007 \end{gathered}$ | Top Girt | L $4 \times 4 \times 1 / 4$ | 415 | 6.77 | 62.86 | 10.8 | Pass |
| T1 | 180-160 | Bottom Girt | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}$ ( 16 ga ) | 7 | 0.42 | 10.43 | $\begin{gathered} 4.0 \\ 6.7 \text { (b) } \end{gathered}$ | Pass |
| T2 | 160-140 | Bottom Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 65 | -0.31 | 7.33 | $\begin{gathered} 4.2 \\ 5.0(\mathrm{~b}) \end{gathered}$ | Pass |
| T3 | 140-120 | Bottom Girt | Pipe $1.51 \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 121 | -0.35 | 7.33 | $\begin{gathered} 4.8 \\ 7.5 \text { (b) } \end{gathered}$ | Pass |
| T4 | 120-100 | Bottom Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 178 | -0.42 | 7.33 | 5.7 | Pass |


| Section No. | Elevation (ft) | Component Type | Size | Critical Element | $\mathbf{P ( K )}$ | SF*P_allow (K) | $\%$ Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | 6.8 (b) |  |
| T5 | 100-80 | Bottom Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 237 | -0.57 | 7.40 | $\begin{gathered} 7.7 \\ 10.1(b) \end{gathered}$ | Pass |
| T6 | 80-60 | Bottom Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 294 | $-0.57$ | 7.40 | $\begin{gathered} 7.7 \\ 9.2 \text { (b) } \\ \hline \end{gathered}$ | Pass |
| T7 | 60-40 | Bottom Girt | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 327 | -0.61 | 7.40 | $\begin{gathered} 8.3 \\ 9.9(b) \end{gathered}$ | Pass |
| T8 | 40-20 | Bottom Girt | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 360 | -0.62 | 7.40 | $\begin{gathered} 8.4 \\ 10.0(\mathrm{~b}) \end{gathered}$ | Pass |
| T9 | 20-4.81771 | Bottom Girt | Pipe 1.5" $\times 0.058{ }^{\prime \prime}$ (16 ga) | 391 | 1.01 | 9.93 | $\begin{gathered} 10.1 \\ 16.2(\mathrm{~b}) \end{gathered}$ | Pass |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 \mathrm{e}-007 \\ \hline \end{gathered}$ | Bottom Girt | L $4 \times 4 \times 1 / 4$ | 419 | -0.24 | 67.37 | 2.8 | Pass |
| T1 | 180-160 | Guy A@162.523 | 3/4 | 432 | 14.30 | 36.73 | 38.9 | Pass |
| T4 | 120-100 | Guy A@119.385 | 1/2 | 435 | 6.36 | 16.95 | 37.6 | Pass |
| T5 | 100-80 | Guy A@82.5234 | 1/2 | 447 | 6.07 | 16.95 | 35.8 | Pass |
| T1 | 180-160 | Guy B@162.523 | 3/4 | 431 | 14.24 | 36.73 | 38.8 | Pass |
| T4 | 120-100 | Guy B@119.385 | 1/2 | 434 | 6.34 | 16.95 | 37.4 | Pass |
| T5 | 100-80 | Guy B@82.5234 | 1/2 | 443 | 6.03 | 16.95 | 35.6 | Pass |
| T1 | 180-160 | Guy C@162.523 | 3/4 | 427 | 14.40 | 36.73 | 39.2 | Pass |
| T4 | 120-100 | Guy C@119.385 | 1/2 | 433 | 6.38 | 16.95 | 37.6 | Pass |
| T5 | 100-80 | Guy C@82.5234 | 1/2 | 437 | 6.10 | 16.95 | 36.0 | Pass |
| T1 | 180-160 | Top Guy PullOff@162.523 | $2 \mathrm{~L} 2 \times 2 \times 1 / 4$ (3/8) | 430 | 4.34 | 51.56 | $\begin{gathered} 8.4 \\ 12.6(b) \\ \hline \end{gathered}$ | Pass |
| T5 | 100-80 | Top Guy PullOff@82.5234 | $2 \mathrm{~L} 2 \times 2 \times 1 / 4(3 / 8)$ | 441 | 2.89 | 51.56 | $\begin{gathered} 5.6 \\ 8.4(b) \end{gathered}$ | Pass |
| T5 | 100-80 | $\begin{aligned} & \text { Torque Arm } \\ & \text { Top@82.5234 } \\ & \hline \end{aligned}$ | C10×15.3 | 449 | 2.07 | 152.75 | 26.9 | Pass |
|  |  | . |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Leg (T8) | 58.7 | Pass |
|  |  |  |  |  |  | Diagonal (T5) | 29.9 | Pass |
|  |  |  |  |  |  | $\begin{gathered} \text { Horizontal } \\ (\mathrm{T} 10) \\ \hline \end{gathered}$ | 1.1 | Pass |
|  |  |  |  |  |  | Top Girt (T4) | 38.9 | Pass |
|  |  |  |  |  |  | Bottom Girt (T9) | 16.2 | Pass |
|  |  |  |  |  |  | Guy A (T1) | 38.9 | Pass |
|  |  |  |  |  |  | Guy B (T1) | 38.8 | Pass |
|  |  |  |  |  |  | Guy C (T1) | 39.2 | Pass |
|  |  |  |  |  |  | Top Guy Pull-Off (T1) | 12.6 | Pass |
|  |  |  |  |  |  | Torque Arm Top (T5) | 26.9 | Pass |
|  |  |  |  |  |  | Bolt Checks | 38.9 | Pass |
|  |  |  |  |  |  | RATING = | 58.7 | Pass |

Table 4 - Tower Component Stresses vs. Capacity

| Notes | Component | Elevation (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1,2 | Base Foundation <br> (Compared w/ Design Loads) | 0 | 91.8 | Pass |
| 1,2 | Guy Anchor Foundation <br> (Compared w/ Design Loads) | 0 | 50.0 | Pass |


| Structure Rating (max from all components) $=$ | $\mathbf{9 1 . 8 \%}$ |
| :--- | :--- |

Notes:

- All structural ratings are per T|A-222-H Section 15.5

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity consumed.
2) Foundation capacity determined by comparing analysis reactions to original design reactions.

## 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

## APPENDIX A

TNXTOWER OUTPUT


## Tower Input Data

The main tower is a $3 x$ guyed tower with an overall height of 180.00 ft above the ground line.
The base of the tower is set at an elevation of 0.00 ft above the ground line.
The face width of the tower is 3.42 ft at the top and tapered at the base.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:

1) Tower is located in Tolland County, Connecticut.
2) Tower base elevation above sea level: 1074.00 ft .
3) Basic wind speed of 117.0 mph .
4) Risk Category II.
5) Exposure Category B.
6) Simplified Topographic Factor Procedure for wind speed-up calculations is used.
7) Topographic Category: 1.
8) Crest Height: 0.00 ft .
9) Nominal ice thickness of 1.50 in.
10) Ice thickness is considered to increase with height.
11) Ice density of 56 pcf.
12) A wind speed of 50.0 mph is used in combination with ice.
13) Temperature drop of $50^{\circ} \mathrm{F}$.
14) Deflections calculated using a wind speed of 60.0 mph .
15) Pressures are calculated at each section.
16) Stress ratio used in tower member design is 1.05 .
17) Safety factor used in guy design is 0.9524 .
18) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs
Consider Moments - Horizontals
Consider Moments - Diagonals
Use Moment Magnification
Use Code Stress Ratios
Use Code Safety Factors - Guys
Escalate Ice
Always Use Max Kz
Use Special Wind Profile
$\sqrt{ }$ Include Bolts In Member Capacity
Leg Bolts Are At Top Of Section
$\sqrt{ } \sqrt{ }$ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric

Distribute Leg Loads As Uniform Assume Legs Pinned Assume Rigid Index Plate
$\checkmark$ Use Clear Spans For Wind Area
$\sqrt{ }$ Use Clear Spans For KL/r
$\sqrt{ }$ Retension Guys To Initial Tension Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt.
$\sqrt{ }$ Autocalc Torque Arm Areas
Add IBC .6D+W Combination
$\sqrt{ }$ Sort Capacity Reports By Component
$\sqrt{ }$ Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

Use ASCE 10 X-Brace Ly Rules
$\sqrt{ }$ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation
$\sqrt{ }$ Consider Feed Line Torque
$\sqrt{ }$ Include Angle Block Shear Check
Use TIA-222-H Bracing Resist.
Exemption
Use TIA-222-H Tension Splice Exemption

## Poles

Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets
Pole Without Linear Attachments
Pole With Shroud Or No
Appurtenances
Outside and Inside Corner Radii Are
Known


Corner \& Starmount Guved Tower


## Face Guyed

Tower Section Geometry

| Tower <br> Section | Tower <br> Elevation | Assembly <br> Database | Description | Section <br> Width | Number <br> of <br> Sections | Section <br> Length |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft |  |  | $f t$ |  |  |  |
| T1 | $180.00-160.00$ |  | $83 P H X$ | 3.42 | 1 | 20.00 |
| T2-T4 | $160.00-100.00$ |  | 83 PHX | 3.42 | 3 | 20.00 |
| T5 | $100.00-80.00$ |  | 84 HX | 3.42 | 1 | 20.00 |
| T6 | $80.00-60.00$ |  | 84 H | 3.42 | 1 | 20.00 |
| T7-T8 | $60.00-20.00$ |  | 84 | 3.42 | 2 | 20.00 |
| T9 | $20.00-4.82$ |  |  | 3.42 | 1 | 15.18 |
| T10 | $4.82-0.00$ | rohn \#80 | 84 HTB | 3.42 | 1 | 4.82 |

Tower Section Geometry (cont'd)

| Tower <br> Section | Tower <br> Elevation | Diagonal <br> Spacing | Bracing <br> Type | Has <br> KBrace <br> End | Has <br> Horizontals | Top Girt <br> Offset | Bottom Girt <br> Offset |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | ft |  |  | Panels |  | in |

tnxTower Report - version 8.1.1.0

| Tower |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Tower |  |  |  |  |  |  |  |
|  | Elevation | Diagonal <br> Spacing | Bracing <br> Type | Has <br> KBrace <br> End | Has | Horizontals | Top Girt | Offset |

## Tower Section Geometry (cont'd)

| Tower Elevation ft | $\begin{aligned} & \text { Leg } \\ & \text { Type } \end{aligned}$ | $\begin{aligned} & \text { Leg } \\ & \text { Size } \end{aligned}$ | Leg Grade | Diagonal Type | $\begin{aligned} & \text { Diagonal } \\ & \text { Size } \end{aligned}$ | Diagonal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { T1 } 180.00- \\ 160.00 \end{gathered}$ | Pipe | Pipe 2.375" x 0.218" (2 XS) | $\begin{aligned} & \text { A618-50 } \\ & (50 \mathrm{ksi}) \end{aligned}$ | Pipe | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| T2-T4 $160.00-100.00$ | Pipe | Pipe 2.375" x 0.218" (2 XS) | A618-50 <br> (50 ksi) | Pipe | Pipe 1.5" $\times 0.058{ }^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T5 100.00- } \\ 80.00 \end{gathered}$ | Pipe | $\text { Pipe } 2.875^{\prime \prime} \times 0.276^{\prime \prime}(2.5$ <br> XS) | A618-50 <br> (50 ksi) | Pipe | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| T6 80.00-60.00 | Pipe | $\begin{gathered} \text { Pipe } 2.875^{\prime \prime} \times 0.276^{\prime \prime}(2.5 \\ \text { XS }) \end{gathered}$ | A618-50 <br> ( 50 ksi ) | Pipe | Pipe 1.5" $\times 0.058{ }^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T7-T8 } \\ 60.00-20.00 \end{gathered}$ | Pipe | $\begin{aligned} & \text { Pipe } 2.875^{\prime \prime} \times 0.203^{\prime \prime}(2.5 \\ & \text { STD) } \end{aligned}$ | A618-50 <br> (50 ksi) | Pipe | Pipe 1.5" $\times 0.058^{\prime \prime}$ ( 16 ga ) Pipe $1^{\prime \prime} \mathrm{S}^{\prime \prime} 0.058^{\prime \prime}(16 \mathrm{ga})$ | A53-B-42 <br> (42 ksi) <br> A53-B-42 |
| T9 20.00-4.82 | Pipe | $\begin{gathered} \text { Pipe } 2.875^{\prime \prime} \times 0.276^{\prime \prime}(2.5 \\ \text { XS }) \end{gathered}$ | $\begin{aligned} & \text { A618-50 } \\ & \text { (50 ksi) } \end{aligned}$ | Pipe | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| T10 4.82-0.00 | Pipe | $\begin{gathered} \text { Pipe } 2.875^{\prime \prime} \times 0.276^{\prime \prime}(2.5 \\ \text { XS }) \end{gathered}$ | $\begin{aligned} & \text { A618-50 } \\ & (50 \mathrm{ksi}) \end{aligned}$ | Single Angie |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \\ \hline \end{gathered}$ |

## Tower Section Geometry (cont'd)

| Tower Elevation ft | Top Girt Type | Top Girt Size | Top Girt Grade | Bottom Girt Type | Bottom Girt Size | Bottom Girt Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { T1 180.00- } \\ 160.00 \end{gathered}$ | Pipe | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ | Pipe | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T2-T4 } \\ 160.00-100.00 \end{gathered}$ | Pipe | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ | Pipe | Pipe 1.5" $\times 0.058^{\prime \prime}$ ( 16 ga ) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T5 } 100.00- \\ 80.00 \end{gathered}$ | Pipe | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | A53-B-42 | Pipe | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| T6 80.00-60.00 | Pipe | Pipe 1.5 " $\times 0.058{ }^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ | Pipe | Pipe 1.5" x $0.058^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T7-T8 } \\ 60.00-20.00 \end{gathered}$ | Pipe | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ | Pipe | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| T9 20.00-4.82 | Pipe | Pipe 1.5" $\times 0.058{ }^{\prime \prime}$ (16 ga) | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ | Pipe | Pipe 1.5" $\times 0.058{ }^{\prime \prime}(16 \mathrm{ga})$ | $\begin{gathered} \text { A53-B-42 } \\ (42 \mathrm{ksi}) \end{gathered}$ |
| T10 4.82-0.00 | Single Angle | L $4 \times 4 \times 1 / 4$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Single Angle | L $4 \times 4 \times 1 / 4$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \\ \hline \end{gathered}$ |

Tower Section Geometry (cont'd)

| Tower Elevation <br> $f t$ | No. of Mid Girts | Mid Girt Type | $\begin{aligned} & \text { Mid Girt } \\ & \text { Size } \end{aligned}$ | Mid Gint Grade | Horizontal Type | Horizontal Size | Horizontal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T10 4.82-0.00 | None | Single Angle |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Single Angle | L $4 \times 4 \times 1 / 4$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |

## Tower Section Geometry (cont'd)



Tower Section Geometry (cont'd)

| Tower Elevation | Calc K Single Angles | Calc K Solid Rounds | $K$ Factors ${ }^{1}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Legs | $\begin{gathered} X \\ \text { Brace } \end{gathered}$ | $\begin{gathered} K \\ \text { Brace } \end{gathered}$ | Single Diags$x$$Y$ | Girts | Horiz. | Sec. <br> Horiz. | Inner Brace |
|  |  |  |  | Diags | Diags |  |  |  |  |  |
|  |  |  |  | X | X |  | $X$ | $X$ | $X$ | $X$ |
| $f t$ |  |  |  | $Y$ | $Y$ |  | $Y$ | $Y$ | $Y$ | $Y$ |
| T1 180.00- | No | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 160.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T2-T4 | No | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 160.00- |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 100.00 |  |  |  |  |  |  |  |  |  |  |
| T5 100.00- | No | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 80.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T6 80.00- | No | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 60.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T7-T8 | No | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 60.00-20.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T9 20.00- | No | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 4.82 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T10 4.82- | No | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 0.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |

'Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the $K$ factor in the out-ofplane direction applied to the overall length.

## Tower Section Geometry (cont'd)

| Tower Elevation $f t$ | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width Deduct in | $u$ |  | $u$ | Net Width <br> Deduct in | $U$ | Net Width Deduct in | U |  | U | Net Width Deduct in | $u$ | Net Width Deduct in | $u$ |
| $\begin{gathered} \hline \text { T1 180.00- } \\ 160.00 \end{gathered}$ | 0.00 | 1 |  | 1 |  | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 |
| $\begin{gathered} \text { T2-T4 } \\ 160.00- \\ 100.00 \end{gathered}$ | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 |

tnxTower Report - version 8.1.1.0

| Tower Elevation ft | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Widt Deduct in |  | Net Width Deduct in | $U$ | Net Width Deduct in |  | Net Width Deduct in | U | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ |
| T5 100.00- | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 |
| 80.00 T6 80.00- | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 |
| 60.00 $77-\mathrm{T8}$ | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 |
| 60.00-20.00 |  | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | 1 | 0.00 | ${ }^{1}$ |
| T9 20.00-4.82 T10 4.82-0.00 | 0.00 0.00 | 1 | 0.00 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 |


| Tower Elevation ft | Redundant Horizontal |  | Redundant Diagonal |  | Redundant SubDiagonal |  | Redundant SubHorizontal |  | Redundant Vertical |  | Redundant Hip |  | Redundant Hip Diagonal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width Deduct in |  | Net Width Deduct in | $U$ | Net Width Deduct in |  | Net Width Deduct in | $U$ | Net Width Deduct in | U | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ <br>  |
| T1 180.00- | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 |
| 160.00 T2-T4 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 |
| $\begin{aligned} & 160.00- \\ & 100.00 \end{aligned}$ | 0.00 | 0.75 | 0.00 |  |  |  |  |  |  |  |  |  | 0.00 | 0.75 |
| T5 100.00- | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 |
| 80.00 T6 80.00- | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 |
| $\begin{aligned} & 60.00 \\ & \mathrm{~T} 7-\mathrm{T} 8 \end{aligned}$ | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 |
| 60.00-20.00 |  |  |  |  |  |  | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 |
| T9 20.00-4.82 | 0.00 0.00 | 0.75 0.75 | 0.00 0.00 | 0.75 0.75 | 0.00 0.00 | 0.75 0.75 | 0.00 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 | 0.00 | 0.75 |

Tower Section Geometry (cont'd)

| Tower Elevation | Connection Offsets |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Diagonal |  |  |  | K-Bracing |  |  |  |
|  | $\begin{aligned} & \text { Vert. } \\ & \text { To } \end{aligned}$ | $\begin{aligned} & \text { Horiz. } \\ & \text { Top } \end{aligned}$ | Vert. Bot. | Horiz. Bot. | $\begin{aligned} & \text { Vert. } \\ & \text { Top } \end{aligned}$ | $\begin{gathered} \text { Horiz } \\ \text { Top } \end{gathered}$ | $\begin{aligned} & \text { Vert. } \\ & \text { Bot. } \end{aligned}$ | Horiz. Bot. |
| ft | in | in | in | in | in | in | in | in |
| T1 180.00- | 0.00 | 3.50 | 0.00 | 3.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 160.00 T2-T4 | 0.00 | 3.50 | 0.00 | 3.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| $\begin{aligned} & 160.00- \\ & 100.00 \end{aligned}$ |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { T5 100.00- } \\ 80.00 \end{gathered}$ | 0.00 | 3.50 | 0.00 | 3.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| T6 80.00- | 0.00 | 3.50 | 0.00 | 3.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| $\begin{aligned} & 60.00 \\ & \text { T7-T8 } \end{aligned}$ | 0.00 | 3.50 | 0.00 | 3.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 60.00-20.00 |  |  |  |  |  |  |  |  |
| T9 20.00-4.82 | 0.00 | 3.50 | 0.00 | 3.50 | 0.00 | 0.00 0.00 | 0.00 | 0.00 |
| T10 4.82-0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  |

Tower Section Geometry (cont'd)

| Tower Elevation ft | Leg Connection Type | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { Bolt Size } \\ \text { in } \\ \hline \end{gathered}$ | No. | Bolt Size in |  | Bolt Size in |  | Bolt Size in | No. | Bolt Size in |  | Bolt Size in | No. | Bolt Size in | No. |
| T1 180.00- | Flange | 0.75 | 4 | 0.50 | 1 | 0.50 | 1 | 0.50 | 1 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 |
| 160.00 |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  |
| T2-T4 | Flange | 0.75 | 4 | 0.50 | 1 | 0.50 | 1 | 0.50 | 1 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 |
| $\begin{aligned} & 160.00- \\ & 100.00 \end{aligned}$ |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X | 0 |
| T5 100.00- | Flange | 0.75 | 4 | 0.50 | 1 | 0.50 | 1 | 0.50 | 1 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 |
| 80.00 |  | A325X |  | A325X |  | A325X |  | A325X |  | A325x |  | A325X |  | A325X |  |
| T6 80.00- | Flange | 0.75 | 4 | 0.50 | 1 | 0.50 | 1 | 0.50 | 1 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 |
| 60.00 |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  |
| T7-78 | Flange | 0.75 | 4 | 0.50 | 1 | 0.50 | 1 | 0.50 | 1 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 |
| 60.00-20.00 |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  |
| T9 20.00-4.82 | Flange | 0.75 | 4 | 0.50 | 1 | 0.50 | 1 | 0.50 | 1 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 |
|  |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  | A325X |  |
| T10 4.82-0.00 | Flange | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 | 0.00 | 0 |
|  |  | A325X |  | A325X |  | A325X |  | A325X |  | A325x |  | A325X |  | A325X |  |

## Guy Data

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Guy Elevation
\(\qquad\) ft \& Guy Grade \& \& Guy Size \& Initial Tension \& \% \& \begin{tabular}{l}
Guy Modulus \\
ksi
\end{tabular} \& \begin{tabular}{l}
Guy Weight \\
plf
\end{tabular} \& Lt

ft \& \begin{tabular}{l}
Anchor Radius <br>
ft

 \& Anchor Azimuth Adj. \& 

Anchor Elevation <br>
ft
\end{tabular} \& End Fitting Efficiency \% <br>

\hline \multirow[t]{3}{*}{162.523} \& \multirow[t]{3}{*}{EHS} \& A \& 3/4 \& 5.83 \& 10\% \& 24000 \& 1.16 \& 213.08 \& 140.00 \& 0.000 \& 0.00 \& 100\% <br>
\hline \& \& B \& 3/4 \& 5.83 \& 10\% \& 24000 \& 1.16 \& 213.08 \& 140.00 \& 0.000 \& 0.00 \& 100\% <br>
\hline \& \& C \& 3/4 \& 5.83 \& 10\% \& 24000 \& 1.16 \& 213.08 \& 140.00 \& 0.000 \& 0.00 \& 100\% <br>
\hline \multirow[t]{3}{*}{119.385} \& \multirow[t]{3}{*}{EHS} \& A \& 1/2 \& 2.69 \& 10\% \& 23000 \& 0.52 \& 182.36 \& 140.00 \& 0.000 \& 0.00 \& 100\% <br>
\hline \& \& B \& 1/2 \& 2.69 \& 10\% \& 23000 \& 0.52 \& 182.36 \& 140.00 \& 0.000 \& 0.00 \& 100\% <br>
\hline \& \& C \& 1/2 \& 2.69 \& 10\% \& 23000 \& 0.52 \& 182.36 \& 140.00 \& 0.000 \& 0.00 \& 100\% <br>
\hline \multirow[t]{3}{*}{82.5234} \& \multirow[t]{3}{*}{EHS} \& A \& 1/2 \& 2.69 \& 10\% \& 23000 \& 0.52 \& 160.73 \& 140.00 \& 0.000 \& 0.00 \& 100\% <br>
\hline \& \& B \& 1/2 \& 2.69 \& 10\% \& 23000 \& 0.52 \& 160.73 \& 140.00 \& 0.000 \& 0.00 \& 100\% <br>
\hline \& \& C \& 1/2 \& 2.69 \& 10\% \& 23000 \& 0.52 \& 160.73 \& 140.00 \& 0.000 \& 0.00 \& 100\% <br>
\hline
\end{tabular}

## Guy Data(cont'd)

| Guy <br> Elevation <br> $f t$ | Mount <br> Type | Torque-Arm <br> Spread | Torque-Arm <br> Leg Angle | Torque-Arm <br> Style | Torque-Arm <br> Grade | Torque-Arm <br> Type | Torque-Arm Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 162.523 | Corner |  |  |  |  |  |  |
| 119.385 |  |  |  |  |  |  |  |
| 82.5234 | Corner <br> Torque Arm | 6.83 | 0.000 | Channel | A36 | Channel | C $10 \times 15.3$ |

## Guy Data (cont'd)

| Guy Elevation ft | Diagonal Grade | Diagonal Type | Upper Diagonal Size | Lower Diagonal Size | Is Strap. | Pull-Off <br> Grade | Pull-Off Type | Pull-Off Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 162.52 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round |  |  | No | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Double Equal Angle | $\begin{gathered} 2 \mathrm{~L} 2 \times 2 \times 1 / 4 \\ (3 / 8) \end{gathered}$ |
| 119.39 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round |  |  |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe |  |

tnxTower Report - version 8.1.1.0

180 Ft Guyed Tower Structural Analysis
Project Number 13323-0004.002.8700

| Guy Elevation ft | Diagonal Grade | Diagonal Type | Upper Diagonal Size | Lower Diagonal Size | Is Strap. | Pull-Off Grade | Pull-Off Type | Pull-Off Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\pi}{82.52}$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round |  |  | No | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Double Equal Angle | $\begin{gathered} 2 \mathrm{~L} 2 \times 2 \times 1 / 4 \\ (3 / 8) \end{gathered}$ |


| Guy Data (cont'd) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Cable | Cable | Tower | Tower | Tower | Tower |
| Guy | Cable <br> Weight | Weight | Weight | Weight | Intercept | Intercept | Intercept | Intercept |
| Elevation | Weight <br> A | Weight | C | D | A | B | C | D |
| $f t$ | K | K | $K$ | K | ft | $f t$ | $f t$ | $f$ |
| 162.523 | 0.25 | 0.25 | 0.25 |  | 4.43 | 4.43 | 4.43 |  |
|  |  |  |  |  | 3.6 | 3.6 | 3.6 sec/pulse |  |
|  |  |  |  |  | sec/pulse | sec/pulse |  |  |
| 119.385 | 0.09 | 0.09 | 0.09 |  | 3.16 | 3.16 3.1 | 3.1 sec/pulse |  |
|  |  |  |  |  | sec/pulse | sec/pulse |  |  |
| 82.5234 | 0.08 | 0.08 | 0.08 |  | 2.47 | 2.47 | 2.47 |  |
| 82.5234 | 0.08 | 0.08 |  |  | 2.7 | 2.7 | 2.7 sec/pulse |  |
|  |  |  |  |  | sec/pulse | sec/pulse |  |  |

## Guy Data (cont'd)

| Guy Elevation $f t$ | Calc K Single Angles | Calc K Solid Rounds | Torque Arm |  | Pull Off |  | Diagonal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $K_{x}$ | $K_{y}$ | $K_{x}$ | $K_{y}$ | $K_{x}$ | $K_{y}$ |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| 162.523 | No | No |  |  | 1 | 1 | 1 | 1 |
| 119.385 | No | No |  |  | 1 | 1 | 1 | 1 |
| 82.5234 | No | No | 1 | 1 | 1 | 1 | 1 | 1 |

## Guy Data (cont'd)

| Guy Elevation ft | Torque-Arm |  |  |  | Pull Off |  |  |  | Diagonal |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Bolt Size in | Number | Net Wid Deduct in | $U$ | Bolt Size in | Number | et Wi Deduct in | $U$ | Bolt Size in | Number | Net Wid <br> Deduc in | U |
| 162.523 | 0.00 | 0 | 0.00 | 1 | 0.63 | 2 | 0.00 | 0.75 | $0.63$ | 0 | 0.00 | 1 |
|  | A325N |  | 0.00 | 1 | A 325 N 0.50 | 0 | 0.00 | 1 | A325N 0.63 | 0 | 0.00 | 1 |
| 119.385 | $\begin{gathered} 0.00 \\ \mathrm{~A} 325 \mathrm{~N} \end{gathered}$ | 0 | 0.00 | 1 | A 325 N | 0 |  |  | A 325 N 0.63 | 0 | 0.00 | 1 |
| 82.5234 | $\begin{gathered} 0.00 \\ \mathrm{~A} 325 \mathrm{~N} \end{gathered}$ | 0 | 0.00 | 1 | $\begin{gathered} 0.63 \\ \mathrm{~A} 325 \mathrm{~N} \\ \hline \end{gathered}$ | 2 | 0.00 | 0.75 | $\mathrm{A} 325 \mathrm{~N}$ | 0 | 0.00 | 1 |

## Guy Pressures

| Guy <br> Elevation <br> $f t$ | Guy <br> Location | $z$ | $q_{z}$ | $q_{z}$ <br> lce | Ice <br> Thickness <br> in |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 162.523 | A | ft | 81.26 | $p s f$ | psf |

tnxTower Report - version 8.1.1.0

180 Ft Guyed Tower Structural Analysis
Project Number 13323-0004.002.8700
July 31, 2023
Stafford 1 CDT
Page 18

| Guy <br> Elevation <br> ft | Guy <br> Location | $z$ | $q_{z}$ | $q_{z}$ | Ice <br> lce |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $f t$ | $p s f$ | $p s f$ | Thickness <br> in |
| 82.5234 | C | 59.69 | 24 | 4 | 1.59 |
|  | A | 41.26 | 22 | 4 | 1.53 |
|  | B | 41.26 | 22 | 4 | 1.53 |
|  | C | 41.26 | 22 | 4 | 1.53 |

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Face Offset in | Lateral Offset (Frac FW) | \# |  | $\begin{gathered} \text { Clear } \\ \text { Spacin } \\ g \\ \text { in } \\ \hline \end{gathered}$ | Width or Diameter in | Perimete $r$ in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { LDF6-50A(1- } \\ 1 / 4) \end{gathered}$ | B | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 153.00- \\ 5.00 \end{gathered}$ | 0.00 | -0.25 | 2 | 2 | $\begin{aligned} & 1.00 \\ & 0.50 \end{aligned}$ | 1.55 |  | 0.60 |
| $\begin{gathered} \text { LDF7-50A(1- } \\ \left.5 / 8^{\prime \prime}\right) \end{gathered}$ | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 171.00- \\ 5.00 \end{gathered}$ | 0.00 | 0.25 | 3 | 3 | 1.00 | 1.98 |  | 0.82 |
| $\begin{aligned} & \text { LDF6-50́A(1- } \\ & 1 / 4) \end{aligned}$ | C | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 171.00- \\ 5.00 \end{gathered}$ | 0.00 | 0 | 1 | 1 | 1.00 | 1.55 |  | 0.60 |
| $\begin{aligned} & \text { LDF4P- } \\ & \text { 50A(1/2) } \end{aligned}$ | C | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 77.00 \\ 5.00 \end{gathered}$ | 0.00 | 0.1 | 1 | 1 | 0.63 | 0.63 |  | 0.15 |
| $\begin{aligned} & \text { LDF5- } \\ & \text { 50A(7/8) } \end{aligned}$ | C | No | No | Ar ( CaAa ) | $\begin{gathered} 180.00- \\ 163.00 \end{gathered}$ | 0.00 | 0.05 | 1 | 1 | 1.03 | 1.03 |  | 0.33 |
| $\begin{aligned} & \text { LDF5- } \\ & 50 \mathrm{~A}(7 / 8) \end{aligned}$ | C | No | No | Ar (CaAa) | $\begin{gathered} 163.00- \\ 5.00 \end{gathered}$ | 0.00 | 0.05 | 2 | 2 | 1.03 | 1.03 |  | 0.33 |
| $\begin{aligned} & \text { LDF5- } \\ & 50 \mathrm{~A}(7 / 8) \end{aligned}$ | C | No | No | Ar (CaAa) | $\begin{gathered} 180.00- \\ 121.00 \end{gathered}$ | 0.00 | -0.03 | 1 | 1 | 1.03 | 1.03 |  | 0.33 |
| $\begin{aligned} & \text { LDF5- } \\ & \text { 50A(7/8) } \\ & * \pm * * * * \end{aligned}$ | C | No | No | Ar (CaAa) | $\begin{gathered} 121.00- \\ 5.00 \end{gathered}$ | 0.00 | -0.03 | 2 | 2 | 1.03 | 1.03 |  | 0.33 |

## Feed Line/Linear Appurtenances - Entered As Area

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement <br> $f t$ | Total Number | $\begin{aligned} & C_{A} A_{A} \\ & \mathrm{ft}^{2} / \mathrm{ft} \end{aligned}$ | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Feed Line/Linear Appurtenances Section Areas

| Tower <br> Sectio | Tower <br> Elevation <br> $n$ | Face | $A_{R}$ | $A_{F}$ | $C_{A} A_{A}$ <br> $I n$ |  | $f^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

tnxTower Report - version 8.1.1.0

180 Ft Guyed Tower Structural Analysis
Project Number 13323-0004.002.8700

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Tower Sectio $n$ \& Tower Elevation ft \& Face \& $A_{R}$

$f t^{2}$ \& AF

$f^{2}$ \& $C_{A} A_{A}$

In Face $f^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$ \& Weight

$K$ <br>
\hline \multirow{4}{*}{T6} \& \multirow{4}{*}{80.00-60.00} \& C \& 0.000 \& 0.000 \& 11.340 \& 0.000 \& 0.04 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 18.080 \& 0.000 \& 0.07 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 12.411 \& 0.000 \& 0.04 <br>
\hline \multirow[t]{3}{*}{17} \& \multirow[t]{2}{*}{60.00-40.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 18.080 \& 0.000 \& 0.07 <br>
\hline \& \multirow{3}{*}{40.00-20.00} \& C \& 0.000 \& 0.000 \& 12.600 \& 0.000 \& 0.04 <br>
\hline \multirow[t]{3}{*}{T8} \& \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 18.080 \& 0.000 \& 0.07 <br>
\hline \& \multirow{3}{*}{20.00-4.82} \& C \& 0.000 \& 0.000 \& 12.600 \& 0.000 \& 0.04 <br>
\hline \multirow[t]{3}{*}{T9} \& \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 13.560 \& 0.000 \& 0.05 <br>
\hline \& \multirow{4}{*}{4.82-0.00} \& C \& 0.000 \& 0.000 \& 9.450 \& 0.000 \& 0.03 <br>
\hline \multirow[t]{3}{*}{T10} \& \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline
\end{tabular}

Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower Sectio n | Tower Elevation ft | Face or Leg | $\qquad$ | $A_{R}$ $f^{2}$ | $A_{F}$ $f t^{2}$ | $C_{A} A_{A}$ <br> In Face $f t^{2}$ | $\qquad$ | Weight $K$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 180.00-160.00 | A | 1.767 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 17.505 | 0.000 | 0.23 |
|  |  | C |  | 0.000 | 0.000 | 25.498 | 0.000 | 0.35 |
| T2 | 160.00-140.00 | A | 1.745 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 46.486 | 0.000 | 0.58 |
|  |  | C |  | 0.000 | 0.000 | 39.080 | 0.000 | 0.47 |
| T3 | 140.00-120.00 | A | 1.720 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 54.122 | 0.000 | 0.65 |
|  |  | C |  | 0.000 | 0.000 | 39.252 | 0.000 | 0.47 |
| T4 | 120.00-100.00 | A | 1.692 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 53.735 | 0.000 | 0.64 |
|  |  | C |  | 0.000 | 0.000 | 49.044 | 0.000 | 0.53 |
| T5 | 100.00-80.00 | A | 1.658 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 53.278 | 0.000 | 0.63 |
|  |  | C |  | 0.000 | 0.000 | 48.443 | 0.000 | 0.51 |
| T6 | 80.00-60.00 | A | 1.617 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 52.719 | 0.000 | 0.61 |
|  |  | C |  | 0.000 | 0.000 | 54.276 | 0.000 | 0.57 |
| 17 | 60.00-40.00 | A | 1.564 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 51.994 | 0.000 | 0.59 |
|  |  | C |  | 0.000 | 0.000 | 54.265 | 0.000 | 0.56 |
| T8 | 40.00-20.00 | A | 1.486 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 50.940 | 0.000 | 0.57 |
|  |  | C |  | 0.000 | 0.000 | 52.562 | 0.000 | 0.53 |
| T9 | 20.00-4.82 | A | 1.360 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 36.933 | 0.000 | 0.39 |
|  |  | C |  | 0.000 | 0.000 | 37.365 | 0.000 | 0.35 |
| T10 | 4.82-0.00 | A | 1.155 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |


| Feed Line Center of Pressure |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation ft | $C P_{x}$ in | $C P_{2}$ in | $\begin{gathered} C P_{x} \\ \text { lce } \\ \text { in } \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{CP}_{2} \\ \text { lce } \\ \text { in } \\ \hline \end{gathered}$ |
| T1 | 180.00-160.00 | 1.33 | 1.57 | 0.63 | 1.42 |
| T2 | 160.00-140.00 | 2.39 | 0.97 | 1.31 | 1.11 |
| T3 | 140.00-120.00 | 2.48 | 0.46 0.55 | 1.42 | 0.72 0.83 |
| T4 | 120.00-100.00 | 2.45 | 0.55 | 1.44 | 0.83 |


| Section | Elevation | $C P_{X}$ | $C P_{z}$ | $C P_{X}$ <br> Ice | $C P_{z}$ <br> Ice |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | in | in | in | in |
| T5 | $100.00-80.00$ | 2.28 | 0.51 | 1.30 | 0.74 |
| T6 | $80.00-60.00$ | 2.55 | 0.78 | 1.90 | 1.65 |
| T7 | $60.00-40.00$ | 2.53 | 0.81 | 1.88 | 1.71 |
| T8 | $40.00-20.00$ | 2.53 | 0.81 | 1.91 | 1.70 |
| T9 | $20.00-4.82$ | 2.46 | 0.80 | 1.89 | 1.62 |
| T10 | $4.82-0.00$ | 0.00 | 0.00 | 0.00 | 0.00 |

## Shielding Factor Ka

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 3 | LDF7-50A(1-5/8") | $\begin{array}{r} 160.00- \\ 171.00 \end{array}$ | 0.6000 | 0.3516 |
| T1 | 4 | LDF6-50A(1-1/4) | 160.00- | 0.6000 | 0.3516 |
| T1 | 6 | LDF5-50A(7/8) | 171.00 $163.00-$ | 0.6000 | 0.3516 |
|  |  |  | 180.00 |  |  |
| T1 | 7 | LDF5-50A(7/8) | $\begin{array}{r} 160.00- \\ 163.00 \end{array}$ | 0.6000 | 0.3516 |
| T1 | 8 | LDF5-50A(7/8) | $160.00-$ $180.00$ | 0.6000 | 0.3516 |
| T2 | 1 | LDF6-50A(1-1/4) | $\begin{array}{r} 140.00- \\ 153.00 \end{array}$ | 0.6000 | 0.3750 |
| T2 | 3 | LDF7-50A(1-5/8') | $\begin{array}{r} 140.00- \\ 160.00 \end{array}$ | 0.6000 | 0.3750 |
| T2 | 4 | LDF6-50A(1-1/4) | $140.00-$ $160.00$ | 0.6000 | 0.3750 |
| T2 | 7 | LDF5-50A(7/8) | $\begin{array}{r} 140.00- \\ 160.00 \end{array}$ | 0.6000 | 0.3750 |
| T2 | 8 | LDF5-50A(7/8) | $\begin{array}{r} 140.00- \\ 160.00 \end{array}$ | 0.6000 | 0.3750 |
| T3 | 1 | LDF6-50A(1-1/4) | $120.00-$ | 0.6000 | 0.3801 |
|  |  |  | 140.00 |  |  |
| T3 | 3 | LDF7-50A(1-5/8") | $120.00-$ 140.00 | 0.6000 | 0.3801 |
| T3 | 4 | LDF6-50A(1-1/4) | 120.00- | 0.6000 | 0.3801 |
| T3 | 7 | L.DF5-50A(7/8) | 140.00 | 0.6000 |  |
| T3 | 7 | LDF5-50A(718) | $\begin{gathered} 120.00- \\ 140.00 \end{gathered}$ | 0.6000 | 0.3801 |
| T3 | 8 | LDF5-50A(7/8) | $121.00-$ | 0.6000 | 0.3801 |
| T3 |  |  | 140.00 |  |  |
| T3 | 9 | LDF5-50A(7/8) | $\begin{array}{r} 120.00- \\ 121.00 \end{array}$ | 0.6000 | 0.3801 |
| T4 | 1 | LDF6-50A(1-1/4) | 100.00- | 0.6000 | 0.3859 |
|  |  |  | 120.00 |  |  |
| T4 | 3 | LDF7-50A(1-5/8') | $\begin{array}{r} 100.00- \\ 120.00 \end{array}$ | 0.6000 | 0.3859 |
| T4 | 4 | LDF6-50A(1-1/4) | 100.00- | 0.6000 | 0.3859 |
| T4 | 7 |  | 120.00 $100.00-$ |  |  |
| 14 | 7 | LDF5-50A(7/8) | $\begin{array}{r} 100.00- \\ 120.00 \end{array}$ | 0.6000 | 0.3859 |
| T4 | 9 | LDF5-50A(7/8) | $100.00-$ | 0.6000 | 0.3859 |
| T5 |  |  | 120.00 |  |  |
| 15 | 1 | LDF6-50A(1-1/4) | $\begin{aligned} & 80.00- \\ & 100.00 \end{aligned}$ | 0.6000 | 0.3606 |
| T5 | 3 | LDF7-50A(1-5/8') | $80.00-$ | 0.6000 | 0.3606 |
|  |  |  | 100.00 |  |  |
| T5 | 4 | LDF6-50A(1-1/4) | $80.00-$ | 0.6000 | 0.3606 |
| T5 | 7 | LDF5-50A(7/8) | 80.00- | 0.6000 | 0.3606 |
|  |  |  | 100.00 |  |  |
| T5 | 9 | LDF5-50A(7/8) | $80.00-1$ | 0.6000 | 0.3606 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | No lce | $\begin{aligned} & K_{a} \\ & \text { lce } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 100.00 |  |  |
| T6 | 1 | LDF6-50A(1-1/4) | $60.00-$ 80.00 | 0.6000 | 0.5440 |
| T6 | 3 | LDF7-50A(1-5/8") | $\begin{array}{r} 60.00- \\ 80.00 \end{array}$ | 0.6000 | 0.5440 |
| T6 | 4 | LDF6-50A(1-1/4) | $60.00-$ 80.00 | 0.6000 | 0.5440 |
| T6 | 5 | LDF4P-50A(1/2) | $\begin{array}{r} 60.00- \\ 77.00 \end{array}$ | 0.6000 | 0.5440 |
| T6 | 7 | LDF5-50A(7/8) | $\begin{array}{r} 60.00- \\ 80.00 \end{array}$ | 0.6000 | 0.5440 |
| T6 | 9 | LDF5-50A(7/8) | $\begin{array}{r} 60.00- \\ 80.00 \end{array}$ | 0.6000 | 0.5440 |
| T7 | 1 | LDF6-50A(1-1/4) | $40.00-$ 60.00 | 0.6000 | 0.5518 |
| T7 | 3 | LDF7-50A(1-5/8") | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.5518 |
| T7 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.5518 |
| T7 | 5 | LDF4P-50A(1/2) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.5518 |
| T7 | 7 | LDF5-50A(7/8) | 40.00 60.00 | 0.6000 | 0.5518 |
| T7 | 9 | LDF5-50A(7/8) | 40.00- | 0.6000 | 0.5518 |
| T8 | 1 | LDF6-50A(1-1/4) | 20.00 40.00 | 0.6000 | 0.5632 |
| T8 | 3 | LDF7-50A(1-5/8") | $20.00-$ 40.00 | 0.6000 | 0.5632 |
| T8 | 4 | LDF6-50A(1-1/4) | $20.00-$ 40.00 | 0.6000 | 0.5632 |
| T8 | 5 | LDF4P-50A(1/2) | $20.00-$ 40.00 | 0.6000 | 0.5632 |
| T8 | 7 | LDF5-50A(7/8) | $20.00-$ 40.00 | 0.6000 | 0.5632 |
| T8 | 9 | LDF5-50A(7/8) | $20.00-1$ | 0.6000 | 0.5632 |
| T9 | 1 | LDF6-50A(1-1/4) | 5.00-20.00 | 0.6000 | 0.5697 |
| T9 | 3 | LDF7-50A(1-5/8") | 5.00-20.00 | 0.6000 | 0.5697 |
| T9 | 4 | LDF6-50A(1-1/4) | 5.00-20.00 | 0.6000 | 0.5697 |
| T9 | 5 | LDF4P-50A(1/2) | 5.00-20.00 | 0.6000 | 0.5697 |
| T9 | 7 | LDF5-50A(7/8) | $5.00-20.00$ $5.00-20.00$ | 0.6000 0.6000 | 0.5697 0.5697 |
| T9 | 9 | LDF5-50A(7/8) | 5.00-20.00 | 0.6000 | 0.5697 |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral Vert ft ft \(f t\)
\end{tabular} \& Azimuth Adjustmen \(t\) \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) Front \\
\(\mathrm{tt}^{2}\)
\end{tabular} \& \(C_{A} A_{A}\)
Side

$f t^{2}$ \& Weight
K <br>

\hline $16 \mathrm{ft} \times 2.5$ " omni whip \& B \& From Leg \& \[
$$
\begin{aligned}
& 0.50 \\
& 0.00 \\
& 8.00
\end{aligned}
$$

\] \& 0.000 \& 179.00 \& \[

$$
\begin{gathered}
\text { No lce } \\
\text { 1/2" } \\
\text { Ice } \\
1^{\prime \prime} \text { Ice } \\
2^{\prime \prime} \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
4.00 \\
5.63 \\
7.28 \\
10.62
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
4.00 \\
5.63 \\
7.28 \\
10.62
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.03 \\
& 0.06 \\
& 0.10 \\
& 0.21
\end{aligned}
$$
\] <br>

\hline APXVAALL24_43-UNA20_TIA w/ Mount Pipe \& A \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.000 \& 171.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { lce }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 20.48 \\
& 21.23 \\
& 21.99
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 10.87 \\
& 12.39 \\
& 13.94
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.18 \\
& 0.32 \\
& 0.46
\end{aligned}
$$
\] <br>

\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& Offsets:
Horz
Lateral
Vert
ft
ft
ft \& Azimuth Adjustmen \(t\) \& Placement
ft \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \begin{tabular}{l}
\(C_{A} A_{A}\) side \\
\(f t^{2}\)
\end{tabular} \& Weight

$K$ <br>

\hline \multirow{4}{*}{APXVAALL24_43-UNA20_TIA w/ Mount Pipe} \& \multirow{3}{*}{B} \& \multirow{3}{*}{From Leg} \& \& \multirow{3}{*}{0.000} \& \multirow{3}{*}{171.00} \& $$
\begin{aligned}
& \text { 1" Ice }^{2 "} \text { Ice }
\end{aligned}
$$ \& 23.44 \& 16.29 \& 0.79 <br>

\hline \& \& \& 4.00
0.00 \& \& \& No Ice
1/2" \& 20.48
21.23 \& 10.87
12.39 \& 0.18
0.32 <br>
\hline \& \& \& 0.00 \& \& \& ice \& 21.99 \& 13.94 \& 0.46 <br>

\hline \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.000} \& \multirow{4}{*}{171.00} \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 23.44 \& 16.29 \& 0.79 <br>

\hline \multirow[t]{4}{*}{APXVAALL24_43-UNA20_TIA w/ Mount Pipe} \& \& \& 4.00 \& \& \& No Ice \& 20.48 \& 10.87 \& 0.18 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 21.23 \& 12.39 \& 0.32 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 21.99 \& 13.94 \& 0.46 <br>

\hline \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.000} \& \multirow{4}{*}{171.00} \& $$
\begin{aligned}
& 1^{\prime \prime} \text { Ice } \\
& 2^{\prime \prime} \text { Ice }
\end{aligned}
$$ \& 23.44 \& 16.29 \& 0.79 <br>

\hline \multirow[t]{4}{*}{AIR6449 B41_TIA w/ Mount Pipe} \& \& \& 4.00 \& \& \& No lce \& 5.89 \& 3.28 \& 0.12 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 6.26 \& 3.74 \& 0.17 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 6.63 \& 4.22 \& 0.22 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{171.00} \& 1"Ice \& 7.41 \& 5.21 \& 0.35 <br>
\hline \multirow{4}{*}{AIR6449 B41_TIA w/ Mount Pipe} \& \& \& \& \& \& 2" ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No lce \& 5.89 \& 3.28 \& 0.12 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 6.26 \& 3.74 \& 0.17 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 6.63 \& 4.22 \& 0.22 <br>
\hline \multirow{5}{*}{AIR6449 B41_TIA w/ Mount Pipe} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{171.00} \& $1{ }^{\prime \prime}$ Ice \& 7.41 \& 5.21 \& 0.35 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ lce \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No lce \& 5.89 \& 3.28 \& 0.12 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 6.26 \& 3.74 \& 0.17 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 6.63 \& 4.22 \& 0.22 <br>

\hline \multirow{5}{*}{$$
\begin{gathered}
\text { RADIO } 4460 \text { B2/B25 } \\
\text { B66_TMO }
\end{gathered}
$$} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{171.00} \& 1 Ice \& 7.41 \& 5.21 \& 0.35 <br>

\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 2.14 \& 1.69 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.32 \& 1.85 \& 0.13 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.51 \& 2.02 \& 0.16 <br>

\hline \multirow{5}{*}{$$
\begin{gathered}
\text { RADIO } 4460 \text { B2/B25 } \\
\text { B66_TMO }
\end{gathered}
$$} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{171.00} \& 1 " Ice \& 2.91 \& 2.39 \& 0.22 <br>

\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 2.14 \& 1.69 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.32 \& 1.85 \& 0.13 <br>
\hline \& \& \& 0.00 \& \& \& lce \& 2.51 \& 2.02 \& 0.16 <br>

\hline \multirow{5}{*}{$$
\begin{gathered}
\text { RADIO 4460 B2/B25 } \\
\text { B66_TMO }
\end{gathered}
$$} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{171.00} \& 1 " Ice \& 2.91 \& 2.39 \& 0.22 <br>

\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No lce \& 2.14 \& 1.69 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.32 \& 1.85 \& 0.13 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.51 \& 2.02 \& 0.16 <br>
\hline \multirow{5}{*}{RADIO 4480 B71_TMO} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{171.00} \& 1 " Ice \& 2.91 \& 2.39 \& 0.22 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 2.85 \& 1.38 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.06 \& 1.54 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.28 \& 1.71 \& 0.14 <br>
\hline \multirow{5}{*}{RADIO 4480 B71_TMO} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{179.00} \& 1 "' Ice \& 3.74 \& 2.07 \& 0.20 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& \& \& \& No lce \& 2.85 \& 1.38 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.06 \& 1.54 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.28 \& 1.71 \& 0.14 <br>

\hline \multirow{4}{*}{RADIO 4480 B71_TMO} \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.000} \& \multirow{4}{*}{171.00} \& | 1" lce |
| :--- |
| 2 " Ice | \& 3.74 \& 2.07 \& 0.20 <br>

\hline \& \& \& 4.00 \& \& \& No lce \& 2.85 \& 1.38 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.06 \& 1.54 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.28 \& 1.71 \& 0.14 <br>

\hline \multirow{4}{*}{(2) RRH $2 \times 50-800 \mathrm{w} /$ Notch Filter} \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.000} \& \multirow{4}{*}{171.00} \& $$
\begin{aligned}
& 1^{\prime \prime} \text { Ice } \\
& 2^{\prime \prime} \text { Ice }
\end{aligned}
$$ \& 3.74 \& 2.07 \& 0.20 <br>

\hline \& \& \& 4.00 \& \& \& Nolce \& 1.73 \& 1.33 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.90 \& 1.48 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& lce \& 2.07 \& 1.64 \& 0.11 <br>
\hline \multirow{5}{*}{(2) RRH $2 \times 50-800 \mathrm{w} /$ Notch Filter} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{171.00} \& 1" Ice \& 2.44 \& 1.97 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No lce \& 1.73 \& 1.33 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.90 \& 1.48 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.07 \& 1.64 \& 0.11 <br>
\hline
\end{tabular}

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset Type | Offsets: Horz Lateral Vert ft ft | Azimuth Adjustmen $t$ | Placement |  | $C_{A} A_{A}$ Front <br> $f^{2}$ | $C_{A} A_{A}$ Side <br> $f t^{2}$ | Weight K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (2) RRH $2 \times 50-800$ w/Notch Filter | C | From Leg |  | 0.000 | 171.00 | 1" Ice | 2.44 | 1.97 | 0.16 |
|  |  |  | 4.00 |  |  | 2" Ice |  |  |  |
|  |  |  | 4.00 0.00 |  |  | 1/2" | 1.90 | 1.48 | 0.09 |
|  |  |  | 0.00 |  |  | Ice | 2.07 | 1.64 | 0.11 |
|  |  |  |  |  |  | 1" Ice | 2.44 | 1.97 | 0.16 |
| Site Pro 1 VFA12-HD | A | From Leg |  | 0.000 | 171.00 | 2" Ice |  |  |  |
|  |  |  | 2.00 |  |  | No Ice | 13.20 | 9.20 | 0.66 |
|  |  |  | 0.00 |  |  | 1/2" | 19.50 | 14.60 | 0.80 |
|  |  |  | 0.00 |  |  | Ice | 25.80 | 19.50 | 1.01 |
|  |  |  |  |  |  | 1" Ice | 38.40 | 30.80 | 1.24 |
| Site Pro 1 VFA12-HD | B | From Leg |  | 0.000 | 171.00 | 2" Ice |  |  |  |
|  |  |  | 2.00 |  |  | No lce | 13.20 | 9.20 | 0.66 |
|  |  |  | 0.00 |  |  | 1/2" | 19.50 | 14.60 | 0.80 |
|  |  |  | 0.00 |  |  | Ice | 25.80 | 19.50 | 1.01 |
|  |  |  |  |  |  | 1" Ice | 38.40 | 30.80 | 1.24 |
| Site Pro 1 VFA12-HD | C | From Leg |  | 0.000 | 171.00 | 2" Ice |  |  |  |
|  |  |  | 2.00 |  |  | No lce | 13.20 | 9.20 | 0.66 |
|  |  |  | 0.00 |  |  | 1/2" | 19.50 | 14.60 | 0.80 |
|  |  |  | 0.00 |  |  | Ice | 25.80 | 19.50 | 1.01 |
|  |  |  |  |  |  | 1' Ice | 38.40 | 30.80 | 1.24 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| PD201 | B | From Leg |  | 0.000 | 163.00 | No Ice | 0.68 | 0.68 | 0.00 |
|  |  |  | $4.00$ |  |  | 1/2" | 1.80 | 1.80 | 0.01 |
|  |  |  | 4.00 |  |  | Ice | 2.92 | 2.92 | 0.02 |
|  |  |  |  |  |  | 1" Ice | 5.16 | 5.16 | 0.03 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| 5" $\times 2.375^{\prime \prime}$ Pipe Mount | B | From Leg | 2.00 | 0.000 | 163.00 | No lce | 1.19 | 1.19 | 0.02 |
|  |  |  | 0.00 |  |  | 1/2" | 1.50 | 1.50 | 0.03 |
|  |  |  | 0.00 |  |  | Ice | 1.81 | 1.81 | 0.04 |
|  |  |  |  |  |  | 1" Ice | 2.46 | 2.46 | 0.08 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| NHH-65B-R2B_TIA w/ Mount Pipe | A | From Leg |  | 0.000 | 153.00 |  |  | 7.00 | 0.07 |
|  |  |  | 4.00 0.00 |  |  | No ice 1/2" | 8.32 8.88 | 8.19 | 0.14 |
|  |  |  | 0.00 |  |  | Ice | 9.40 | 9.08 | 0.21 |
|  |  |  |  |  |  | 1" Ice | 10.47 | 10.90 | 0.39 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| NHH-65B-R2B_TIA w $/$ Mount Pipe | B | From Leg | 4.00 | 0.000 | 153.00 | No lce | 8.32 | 7.00 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 8.88 | 8.19 | 0.14 |
|  |  |  | 0.00 |  |  | Ice | 9.40 | 9.08 | 0.21 |
|  |  |  |  |  |  | 1" Ice | 10.47 | 10.90 | 0.39 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| NHH-65B-R2B_TIA w/ Mount Pipe | C | From Leg | 4.00 | 0.000 | 153.00 | No lce | 8.32 | 7.00 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 8.88 | 8.19 | 0.14 |
|  |  |  | 0.00 |  |  | Ice | 9.40 | 9.08 | 0.21 |
|  |  |  |  |  |  | 1 Ice | 10.47 | 10.90 | 0.39 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| NHHSS-65B-R2BT4_TIA w/ Mount Pipe | A | From Leg | 4.00 | 0.000 | 153.00 | No lce | 8.29 | 7.02 | 0.08 |
|  |  |  | 0.00 |  |  | 1/2" | 8.84 | 8.20 | 0.14 |
|  |  |  | 0.00 |  |  | Ice | 9.37 | 9.09 | 0.22 |
|  |  |  |  |  |  | 1" ice 2" Ice | 10.44 | 10.92 | 0.40 |
| NHHSS-65B-R2BT4_TIA w/ Mount Pipe | B | From Leg | 4.00 | 0.000 | 153.00 | No lce | 8.29 | 7.02 | 0.08 |
|  |  |  | 0.00 |  |  | 1/2" | 8.84 | 8.20 | 0.14 |
|  |  |  | 0.00 |  |  | Ice | 9.37 | 9.09 | 0.22 |
|  |  |  |  |  |  | 1" Ice | 10.44 | 10.92 | 0.40 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| NHHSS-65B-R2BT4_TIA w/ Mount Pipe <br> MT6413-77A | C | From Leg | 4.00 | 0.000 | 153.00 | No Ice | 8.29 | 7.02 | 0.08 |
|  |  |  | 0.00 |  |  | 1/2" | 8.84 | 8.20 | 0.14 |
|  |  |  | 0.00 |  |  | lce | 9.37 | 9.09 | 0.22 |
|  |  |  |  |  |  | 1" Ice | 10.44 | 10.92 | 0.40 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
|  | A | From Leg | 4.00 | 0.000 | 153.00 | No lce | 3.81 | 1.46 | 0.08 |

tnxTower Report - version 8.1.1.0

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
ft \\
ft \\
ft
\end{tabular} \& \[
\begin{gathered}
\text { Azimuth } \\
\text { Adjustmen } \\
t
\end{gathered}
\] \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f^{2}
\] \& \(C_{A} A_{A}\)
Side

$f t^{2}$ \& Weight

$K$ <br>
\hline \multirow{7}{*}{MT6413-77A} \& \multirow{6}{*}{B} \& \multirow{6}{*}{From Leg} \& 0.00 \& \multirow{6}{*}{0.000} \& \multirow{6}{*}{153.00} \& 1/2" \& 4.06 \& 1.65 \& 0.11 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 4.32 \& 1.84 \& 0.13 <br>
\hline \& \& \& \& \& \& 1" lce \& 4.86 \& 2.26 \& 0.20 <br>
\hline \& \& \& 4.00 \& \& \& Nolce \& 3.81 \& 1.46 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 4.06 \& 1.65 \& 0.11 <br>
\hline \& \& \& 1.00 \& \& \& lce \& 4.32 \& 1.84 \& 0.13 <br>

\hline \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.000} \& \multirow{4}{*}{153.00} \& $$
\begin{aligned}
& 1^{\prime \prime} \text { Ice } \\
& 2^{\prime \prime} \text { Ice }
\end{aligned}
$$ \& 4.86 \& 2.26 \& 0.20 <br>

\hline \multirow[t]{5}{*}{MT6413-77A} \& \& \& 4.00 \& \& \& No lce \& 3.81 \& 1.46 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 4.06 \& 1.65 \& 0.11 <br>
\hline \& \& \& \multirow[t]{2}{*}{1.00} \& \& \& Ice \& 4.32 \& 1.84 \& 0.13 <br>
\hline \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{153.00} \& 1 ' Ice \& 4.86 \& 2.26 \& 0.20 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{B2/B66 RRH ORAN} \& \& \& 4.00 \& \& \& No lce \& 1.85 \& 1.24 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.02 \& 1.38 \& 0.10 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.00} \& \& \& Ice \& 2.20 \& 1.53 \& 0.12 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{153.00} \& 1" Ice \& 2.57 \& 1.85 \& 0.17 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{B2/B66 RRH ORAN} \& \& \& 4.00 \& \& \& No Ice \& 1.85 \& 1.24 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.02 \& 1.38 \& 0.10 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.00} \& \& \& Ice \& 2.20 \& 1.53 \& 0.12 <br>
\hline \& \multirow{6}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{153.00} \& 1" Ice \& 2.57 \& 1.85 \& 0.17 <br>
\hline \multirow{5}{*}{B2/B66 RRH ORAN} \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 1.85 \& 1.24 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.02 \& 1.38 \& 0.10 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.00} \& \& \& Ice \& 2.20 \& 1.53 \& 0.12 <br>
\hline \& \& \& \& \& \& $1{ }^{1 \prime}$ Ice \& 2.57 \& 1.85 \& 0.17 <br>
\hline \multirow{6}{*}{RF4461d-13A} \& \multirow{5}{*}{A} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.000} \& \multirow{5}{*}{153.00} \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No lce \& 1.85 \& 1.27 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.02 \& 1.41 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& lce \& 2.20 \& 1.56 \& 0.12 <br>
\hline \& \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \& $1{ }^{1 \prime}$ lce \& 2.57 \& 1.88 \& 0.17 <br>
\hline \& \multirow{4}{*}{B} \& \& \& \& \multirow{4}{*}{153.00} \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{RF4461d-13A} \& \& \& 4.00 \& \& \& No lce \& 1.85 \& 1.27 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.02 \& 1.41 \& 0.10 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.00} \& \& \& lce \& 2.20 \& 1.56 \& 0.12 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{153.00} \& 1" Ice \& 2.57 \& 1.88 \& 0.17 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{RF4461d-13A} \& \& \& \& \& \& No Ice \& 1.85 \& 1.27 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.02 \& 1.41 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& lce \& 2.20 \& 1.56 \& 0.12 <br>
\hline \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{153.00} \& $1{ }^{\prime \prime}$ Ice \& 2.57 \& 1.88 \& 0.17 <br>
\hline \multirow{5}{*}{RT4423-48A} \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No lce \& 0.86 \& 0.49 \& <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.97 \& 0.59 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.10 \& 0.69 \& 0.03 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{153.00} \& $1^{\prime \prime}$ Ice \& 1.37 \& 0.92 \& 0.06 <br>
\hline \multirow{5}{*}{RT4423-48A} \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No lce \& 0.86 \& 0.49 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.97 \& 0.59 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.10 \& 0.69 \& 0.03 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \& $1{ }^{\prime \prime}$ lce \& 1.37 \& 0.92 \& 0.06 <br>
\hline \multirow{6}{*}{RT4423-48A} \& \& \& \& \& \multirow{4}{*}{153.00} \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No lce \& 0.86 \& 0.49 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.97 \& 0.59 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& lce \& 1.10 \& 0.69 \& 0.03 <br>
\hline \& \multirow{6}{*}{A} \& \multirow{7}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{153.00} \& $1{ }^{1 \prime}$ Ice \& 1.37 \& 0.92 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{12 OVP} \& \& \& 4.00 \& \& \& No lce \& 3.36 \& 2.19 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.60 \& 2.39 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.84 \& 2.61 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& 4.34 \& 3.05 \& 0.17 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline Site Pro 1 VFA12-HD \& A \& From Leg \& 2.00 \& 0.000 \& 153.00 \& No Ice \& 13.20 \& 9.20 \& 0.66 <br>
\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& Offsets: Horz Lateral Vert \(f t\) ft \& \begin{tabular}{l}
Azimuth Adjustmen \(t\) \\
-
\end{tabular} \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) Front \\
\(f t^{2}\)
\end{tabular} \& \(C_{A} A_{A}\) Side
\[
f t^{2}
\] \& Weight

$K$ <br>
\hline \multirow{6}{*}{Site Pro 1 VFA12-HD} \& \multirow{7}{*}{B} \& \multirow{6}{*}{From Leg} \& 0.00 \& \multirow{6}{*}{0.000} \& \multirow{6}{*}{153.00} \& 1/2" \& 19.50 \& 14.60 \& 0.80 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 25.80 \& 19.50 \& 1.01 <br>

\hline \& \& \& 0.0 \& \& \& $$
\begin{aligned}
& 1^{\prime \prime} \text { Ice } \\
& 2^{\prime \prime} \text { Ice }
\end{aligned}
$$ \& 38.40 \& 30.80 \& 1.24 <br>

\hline \& \& \& 2.00 \& \& \& No lce \& 13.20 \& 9.20 \& 0.66 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 19.50 \& 14.60 \& 0.80 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 25.80 \& 19.50 \& 1.01 <br>

\hline \& \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{153.00} \& | 1 " Ice |
| :--- |
| $2^{\prime \prime}$ Ice | \& 38.40 \& 30.80 \& 1.24 <br>

\hline \multirow[t]{5}{*}{Site Pro 1 VFA12-HD} \& \multirow[t]{4}{*}{C} \& \& 2.00 \& \& \& No lce \& 13.20 \& 9.20 \& 0.66 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 19.50 \& 14.60 \& 0.80 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 25.80 \& 19.50 \& 1.01 <br>
\hline \& \& \& 0.0 \& \& \& 1" Ice \& 38.40 \& 30.80 \& 1.24 <br>
\hline \& \& \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{153.00} \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{2.375" OD $\times 8^{\prime}$ ' Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \& \& No lce \& 1.90 \& 1.90 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.73 \& 2.73 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& lce \& 3.40 \& 3.40 \& 0.06 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 4.40 \& 4.40 \& 0.12 <br>
\hline \& \& \& \& \multirow{6}{*}{0.000} \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{2.375" OD x $8^{\prime}$ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \& \multirow[t]{4}{*}{153.00} \& No lce \& 1.90 \& 1.90 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.73 \& 2.73 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.40 \& 3.40 \& 0.06 <br>
\hline \& \& \& \& \& \& 1" Ice \& 4.40 \& 4.40 \& 0.12 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow{5}{*}{2.375" OD x $8^{\prime}$ ' Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{153.00} \& No Ice \& 1.90 \& 1.90 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.73 \& 2.73 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& lce \& 3.40 \& 3.40 \& 0.06 <br>
\hline \& \& \& \& \& \& 1" Ice \& 4.40 \& 4.40 \& 0.12 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline *** \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{4}{*}{138.00} \& No lce \& 0.58 \& 0.58 \& 0.03 <br>
\hline \multirow[t]{4}{*}{$3^{\prime} \times 2.375^{\prime \prime}$ Pipe Mount} \& \& \& 1.50
0.00 \& \& \& 1/2"' \& 0.77 \& 0.77 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.97 \& 0.97 \& 0.04 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.39 \& 1.39 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" lce \& \& \& <br>
\hline \multirow[t]{5}{*}{DB420} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{121.00} \& No lce \& 3.33 \& 3.33 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 5.99 \& 5.99 \& 0.04 <br>
\hline \& \& \& 8.00 \& \& \& Ice \& 8.66 \& 8.66 \& 0.05 <br>
\hline \& \& \& \& \& \& 1" Ice \& 13.99 \& 13.99 \& 0.07 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{Generic 2' x 3' sidearm} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 1.50 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{121.00} \& No lce \& 1.50 \& 3.00 \& 0.19 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.50 \& 4.00 \& 0.28 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.50 \& 5.00 \& 0.36 <br>
\hline \& \& \& \& \& \& 1" Ice \& 5.50 \& 7.00 \& 0.54 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{PD201} \& \multirow{5}{*}{B} \& \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{77.00} \& \& \& \& <br>
\hline \& \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \& \& Nolce \& 0.68
1.80 \& 1.80 \& 0.01 <br>
\hline \& \& \& 0.00
4.00 \& \& \& 1/2 \& 1.80
2.92 \& 2.92 \& 0.02 <br>
\hline \& \& \& 4.00 \& \& \& 1" Ice \& 5.16 \& 5.16 \& 0.03 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{5" $\times 2.375^{\prime \prime}$ Pipe Mount} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 2.00 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{77.00} \& No lce \& 1.19 \& 1.19 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.50 \& 1.50 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.81 \& 1.81 \& 0.04 <br>
\hline \& \& \& \& \& \& 1" lce \& 2.46 \& 2.46 \& 0.08 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>
\hline
\end{tabular}

## Load Combinations

| Comb. No. | Description |
| :---: | :---: |
| 1 | Dead Only |
| 2 | 1.2 Dead+1.0 Wind 0 deg - No Ice+1.0 Guy |
| 3 | 1.2D+1.0W (pattern 1) 0 deg - No Ice+1.0 Guy |
| 4 | 1.2D+1.0W (pattern 2) 0 deg - No lce+1.0 Guy |
| 5 | 1.2D+1.0W (pattern 3) 0 deg - No Ice+1.0 Guy |
| 6 | 1.2D+1.0W (pattern 4) 0 deg - No lce+1.0 Guy |
| 7 | 1.2 Dead+1.0 Wind 30 deg - No Ice+1.0 Guy |
| 8 | 1.2D+1.0W (pattern 1) 30 deg - No lce+1.0 Guy |
| 9 | 1.2D+1.0W (pattern 2) 30 deg - No Ice+1.0 Guy |
| 10 | 1.2D+1.0W (pattern 3) 30 deg - No Ice+1.0 Guy |
| 11 | 1.2D+1.0W (pattern 4) 30 deg - No Ice+1.0 Guy |
| 12 | 1.2 Dead+1.0 Wind 60 deg - No Ice+1.0 Guy |
| 13 | 1.2D+1.0W (pattern 1) 60 deg - No Ice+1.0 Guy |
| 14 | 1.2D+1.0W (pattern 2) 60 deg - No lce+1.0 Guy |
| 15 | 1.2D+1.0W (pattern 3) 60 deg - No lce+1.0 Guy |
| 16 | 1.2D+1.0W (pattern 4) 60 deg - No lce+1.0 Guy |
| 17 | 1.2 Dead+1.0 Wind 90 deg - No Ice+1.0 Guy |
| 18 | 1.2D+1.0W (pattern 1) 90 deg - No Ice+1.0 Guy |
| 19 | 1.2D+1.0W (pattern 2) 90 deg - No lce+1.0 Guy |
| 20 | $1.2 \mathrm{D}+1.0 \mathrm{~W}$ (pattern 3) 90 deg - No lce+1.0 Guy |
| 21 | 1.2D+1.0W (pattern 4) 90 deg - No Ice+1.0 Guy |
| 22 | 1.2 Dead+1.0 Wind 120 deg - No Ice+1.0 Guy |
| 23 | $1.2 \mathrm{D}+1.0 \mathrm{~W}$ (pattern 1) 120 deg - No Ice+1.0 Guy |
| 24 | 1.2D+1.0W (pattern 2) 120 deg - No lce+1.0 Guy |
| 25 | $1.2 \mathrm{D}+1.0 \mathrm{~W}$ (pattern 3) 120 deg - No lce+1.0 Guy |
| 26 | 1.2D+1.0W (pattern 4) 120 deg - No Ice+1.0 Guy |
| 27 | 1.2 Dead+1.0 Wind 150 deg - No Ice+1.0 Guy |
| 28 | 1.2D+1.0W (pattern 1) 150 deg - No Ice+1.0 Guy |
| 29 | 1.2D+1.0W (pattern 2) 150 deg - No lce+1.0 Guy |
| 30 | 1.2D+1.0W (pattern 3) 150 deg - No Ice+1.0 Guy |
| 31 | 1.2D+1.0W (pattern 4) 150 deg - No Ice+1.0 Guy |
| 32 | 1.2 Dead+1.0 Wind 180 deg - No lce+1.0 Guy |
| 33 | 1.2D+1.0W (pattern 1) 180 deg - No Ice+1.0 Guy |
| 34 | 1.2D+1.0W (pattern 2) 180 deg - No Ice+1.0 Guy |
| 35 | 1.2D+1.0W (pattern 3) 180 deg - No lice+1.0 Guy |
| 36 | 1.2D+1.0W (pattern 4) 180 deg - No Ice+1.0 Guy |
| 37 | 1.2 Dead+1.0 Wind 210 deg - No lce 1.0 Guy |
| 38 | 1.2D+1.0W (pattern 1) 210 deg - No lce+1.0 Guy |
| 39 | 1.2D+1.0W (pattern 2) 210 deg - No lce+1.0 Guy |
| 40 | 1.2D+1.0W (pattern 3) 210 deg - No lce+1.0 Guy |
| 41 | 1.2D+1.0W (pattern 4) 210 deg - No Ice+1.0 Guy |
| 42 | 1.2 Dead+1.0 Wind 240 deg - No Ice+1.0 Guy |
| 43 | 1.2D+1.0W (pattern 1) 240 deg - No lce+1.0 Guy |
| 44 | 1.2D+1.0W (pattern 2) 240 deg - No Ice+1.0 Guy |
| 45 | 1.2D+1.0W (pattern 3) 240 deg - No Ice+1.0 Guy |
| 46 | 1.2D+1.0W (pattern 4) 240 deg - No Ice+1.0 Guy |
| 47 | 1.2 Dead+1.0 Wind 270 deg - No Ice+1.0 Guy |
| 48 | 1.2D+1.0W (pattern 1) 270 deg - No lce+1.0 Guy |
| 49 | 1.2D+1.0W (pattern 2) 270 deg - No lce+1.0 Guy |
| 50 | 1.2D+1.0W (pattern 3) 270 deg - No Ice+1.0 Guy |
| 51 | 1.2D+1.0W (pattern 4) 270 deg - No Ice+1.0 Guy |
| 52 | 1.2 Dead+1.0 Wind 300 deg - No Ice+1.0 Guy |
| 53 | 1.2D+1.0W (pattern 1) 300 deg - No lce+1.0 Guy |
| 54 | 1.2D+1.0W (pattern 2) 300 deg - No lce+1.0 Guy |
| 55 | 1.2D+1.0W (pattern 3) 300 deg - No lce+1.0 Guy |
| 56 | $1.2 \mathrm{D}+1.0 \mathrm{~W}$ (pattern 4) 300 deg - No lce +1.0 Guy |
| 57 | 1.2 Dead+1.0 Wind 330 deg - No lce+1.0 Guy |
| 58 | 1.2D+1.0W (pattern 1) 330 deg - No Ice+1.0 Guy |
| 59 | 1.2D+1.0W (pattern 2) 330 deg - No lce+1.0 Guy |
| 60 | 1.2D+1.0W (pattern 3) 330 deg - No Ice+1.0 Guy |
| 61 | 1.2D+1.0W (pattern 4) 330 deg - No lce+1.0 Guy |
| 62 | 1.2 Dead+1.0 Ice+1.0 Temp+Guy |
| 63 | 1.2 Dead +1.0 Wind 0 deg+1.0 lce+1.0 Temp+1.0 Guy |
| 64 | 1.2 Dead+1.0 Wind $30 \mathrm{deg}+1.0 \mathrm{lce}+1.0$ Temp+1.0 Guy |
| 65 | 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 66 | 1.2 Dead+1.0 Wind 90 deg+1.0 lce+1.0 Temp+1.0 Guy |
| 67 | 1.2 Dead+1.0 Wind $120 \mathrm{deg}+1.0 \mathrm{lce}+1.0$ Temp+1.0 Guy |
| 68 | 1.2 Dead+1.0 Wind $150 \mathrm{deg}+1.0 \mathrm{lce}+1.0$ Temp+1.0 Guy |
| 69 | 1.2 Dead+1.0 Wind $180 \mathrm{deg}+1.0 \mathrm{lce}+1.0$ Temp+1.0 Guy |


| Comb. |  |
| :--- | :--- |
| No. |  |
| 70 | 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 71 | 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 72 | 1.2 Dead+1.0 Wind 270 deg+1.0 lce+1.0 Temp+1.0 Guy |
| 73 | 1.2 Dead+1.0 Wind 300 deg+1.0 lce+1.0 Temp+1.0 Guy |
| 74 | 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 75 | Dead+Wind 0 deg - Service+Guy |
| 76 | Dead+Wind 30 deg - Service+Guy |
| 77 | Dead+Wind 60 deg - Service+Guy |
| 78 | Dead+Wind 90 deg - Service+Guy |
| 79 | Dead+Wind 120 deg - Service+Guy |
| 80 | Dead+Wind 150 deg - Service+Guy |
| 81 | Dead+Wind 180 deg - Service+Guy |
| 82 | Dead+Wind 210 deg - Service+Guy |
| 83 | Dead+Wind 240 deg - Service+Guy |
| 84 | Dead+Wind 270 deg - Service+Guy |
| 85 | Dead+Wind 300 deg - Service+Guy |
| 86 | Dead+Wind 330 deg - Service+Guy |


|  | Maximum Reactions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Condition | Gov. <br> Load <br> Comb. | $\begin{gathered} \text { Vertical } \\ K \end{gathered}$ | $\underset{K}{\text { Horizontal, } X}$ | $\begin{gathered} \text { Horizontal, } Z \\ K \end{gathered}$ |
| Mast | Max. Vert | 71 | 102.08 | 0.38 | -0.18 |
|  | Max. $H_{x}$ | 50 | 48.05 | 1.09 | 0.01 |
|  | Max. $\mathrm{Hz}_{\mathrm{z}}$ | 5 | 47.03 | 0.00 | 1.11 |
|  | Max. M ${ }_{\text {x }}$ | 1 | 0 | 0.00 | 0.00 |
|  | Max. $\mathrm{M}_{\mathbf{z}}$ | 1 | 0 | 0.00 | 0.00 |
|  | Max. Torsion | 37 | 1 | 0.50 | -0.90 |
|  | Min. Vert | 1 | 42.25 | 0.00 | 0.00 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 20 | 48.08 | -1.08 | -0.00 |
|  | Min. $\mathrm{Hz}_{\mathbf{z}}$ | 35 | 48.49 | 0.01 | -1.07 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 1 | 0 | 0.00 | 0.00 |
|  | Min. $\mathrm{M}_{\mathbf{z}}$ | 1 | 0 | 0.00 -0.53 | 0.00 |
|  | Min. Torsion | 7 | -1 -1.67 | -0.53 -2.15 | 1.25 |
| Guy C@140f | Max. Vert | 42 | -1.67 | -2.15 | 1.25 |
| Azimuth 240 deg |  | 42 | -1.67 | -2.15 | 1.25 |
|  | $\text { Max. } \mathrm{H}_{\mathrm{z}}$ | 65 | -16.63 | -19.10 | 11.03 |
|  | Min. Vert | 12 | -18.59 | -18.35 | 10.59 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 65 | -16.63 | -19.10 | 11.03 |
|  | Min. $\mathrm{Hz}_{\mathbf{z}}$ | 42 | -1.67 | -2.15 | 1.25 |
| Guy B @ 140 ft | Max. Vert | 22 | -1.82 | 2.35 | 1.35 |
| Azimuth 120 deg | Max. $\mathrm{H}_{\mathrm{x}}$ | 73 | -16.45 | 18.95 | 10.94 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 73 | -16.45 | 18.95 | 10.94 |
|  | Min. Vert | 52 | -18.32 | 18.07 | 10.44 1.35 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 22 | -1.82 | 2.35 | 1.35 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 22 | -1.82 | 2.35 | 1.35 -2.66 |
| Guy A@140 ft | Max. Vert | 2 | -1.78 | 0.01 | -2.66 |
| Azimuth 0 deg |  | 72 | -13.59 | 0.50 | -18.39 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 2 | -1.78 | 0.01 | -2.66 |
|  | Min. Vert | 32 | -18.40 | -0.01 | -20.95 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 66 | -13.60 | -0.50 | -18.39 -21.98 |
|  | Min. $\mathrm{Hz}_{\mathbf{z}}$ | 69 | -16.57 | -0.00 | -21.98 |

Tower Mast Reaction Summary

180 Ft Guyed Tower Structural Analysis
July 31, 2023
Project Number 13323-0004.002.8700

|  | Vertical <br> $K$ | Shear <br> $K$ | Shear <br> $K$ | Overtuming Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 42.25 | -0.00 | -0.00 | 0 | 0 | 0 |
| 1.2 Dead+1.0 Wind 0 deg No Ice+1.0 Guy | 48.81 | -0.01 | -1.00 |  | 0 | 0 |
| 1.2D+1.0W (patterm 1) 0 deg <br> - No lce 1.0 Guy | 48.97 | -0.01 | -0.43 | 0 | 0 | 0 |
| $1.2 \mathrm{D}+1.0 \mathrm{~W}$ (pattem 2) 0 deg <br> - No Ice+1.0 Guy | 48.74 | -0.01 | -1.02 | 0 | 0 | 0 |
| 1.2D+1.0W (pattern 3) 0 deg <br> - No Ice+1.0 Guy | 47.03 | -0.00 | -1.11 | 0 | 0 | 0 |
| 1.2D+1.0W (pattern 4) 0 deg <br> - No Ice+1.0 Guy | 46.60 | -0.01 | -1.05 | 0 | 0 | 0 |
| 1.2 Dead+1.0 Wind 30 deg No Ice +1.0 Guy | 49.57 | 0.53 | -0.88 | 0 | 0 | 1 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattern 1) } 30 \\ & \text { deg - No Ice }+1.0 \text { Guy } \end{aligned}$ | 49.63 | 0.23 | -0.37 | 0 | 0 | 1 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattem 2) } 30 \\ & \text { deg - No Ice }+1.0 \text { Guy } \end{aligned}$ | 49.36 | 0.54 | -0.90 | 0 | 0 | 1 |
| 1.2D+1.0W (pattern 3) 30 deg - No lee +1.0 Guy | 48.10 | 0.57 | -0.99 | 0 | 0 | 1 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattern 4) } 30 \\ & \text { deg - No Ice }+1.0 \text { Guy } \end{aligned}$ | 47.95 | 0.53 | -0.92 | 0 | 0 | 1 |
| 1.2 Dead+1.0 Wind 60 deg No Ice+1.0 Guy | 49.28 | 0.89 | -0.52 | 0 | 0 | 0 |
| 1.2D+1.0W (pattern 1) 60 deg - No Ice+1.0 Guy | 49.23 | 0.38 | -0.23 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattern 2) } 60 \\ & \text { deg - No Ice } 1.0 \text { Guy } \end{aligned}$ | 49.10 | 0.91 | -0.53 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattern } 3 \text { ) } 60 \\ & \text { deg - No Ice } 1.0 \text { Guy } \end{aligned}$ | 48.54 | 0.97 | -0.56 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattern 4) } 60 \\ & \text { deg - No Ice }+1.0 \text { Guy } \end{aligned}$ | 48.55 | 0.90 | -0.53 | 0 | 0 | 0 |
| 1.2 Dead+1.0 Wind 90 deg No Ice+1.0 Guy | 49.50 | 0.98 | -0.02 | 0 | 0 | 0 |
| 1.2D+1.0W (pattern 1) 90 deg - No Ice+1.0 Guy | 49.56 | 0.41 | -0.02 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattern 2) } 90 \\ & \text { deg - No Ice }+1.0 \text { Guy } \end{aligned}$ | 49.32 | 1.00 | -0.02 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattem 3) } 90 \\ & \text { deg - No Ice } 1.0 \text { Guy } \end{aligned}$ | 48.08 | 1.08 | -0.00 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattern 4) } 90 \\ & \text { deg - No Ice+1.0 Guy } \end{aligned}$ | 47.89 | 1.01 | -0.00 | 0 | 0 | 0 |
| 1.2 Dead+1.0 Wind 120 deg <br> - No Ice+1.0 Guy | 48.81 | 0.86 | 0.50 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattern 1) } 120 \\ & \text { deg - No Ice }+1.0 \text { Guy } \end{aligned}$ | 48.97 | 0.37 | 0.21 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D }+1.0 \mathrm{~W} \text { (pattern 2) } 120 \\ & \text { deg - No Ice }+1.0 \text { Guy } \end{aligned}$ | 48.74 | 0.87 | 0.51 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D }+1.0 \mathrm{~W} \text { (pattern } 3 \text { ) } 120 \\ & \text { deg }-\mathrm{No} \text { Ice }+1.0 \text { Guy } \end{aligned}$ | 47.05 | 0.95 | 0.55 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D+1.0W (pattem 4) } 120 \\ & \text { deg - No lce }+1.0 \text { Guy } \end{aligned}$ | 46.60 | 0.90 | 0.52 | 0 | 0 | 0 |
| 1.2 Dead+1.0 Wind 150 deg <br> - No lce+1.0 Guy | 49.24 | 0.43 | 0.78 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D }+1.0 \mathrm{~W} \text { (pattern 1) } 150 \\ & \text { deg }- \text { No lce }+1.0 \text { Guy } \end{aligned}$ | 49.30 | 0.17 | 0.33 | 0 | 0 | 0 |
| 1.2D+1.0W (pattern 2) 150 deg - No Ice +1.0 Guy | 49.10 | 0.44 | 0.79 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D }+1.0 \mathrm{~W}(\text { pattem } 3 \text { ) } 150 \\ & \text { deg }- \text { No Ice }+1.0 \text { Guy } \end{aligned}$ | 47.97 | 0.49 | 0.86 | 0 | 0 | 0 |
| 1.2D+1.0W (pattern 4) 150 deg - No Ice +1.0 Guy | 47.77 | 0.46 | 0.80 | 0 | 0 | 0 |
| 1.2 Dead+1.0 Wind 180 deg <br> - No Ice +1.0 Guy | 49.21 | -0.01 | 0.98 | 0 | 0 | 0 |
| $\begin{aligned} & \text { 1.2D }+1.0 \mathrm{~W} \text { (pattern 1) } 180 \\ & \text { deg }- \text { No Ice }+1.0 \text { Guy } \end{aligned}$ | 49.16 | -0.00 | 0.42 | 0 | 0 | 0 |
| $\text { 1.2D+1.0W (pattern 2) } 180$ deg - No Ice+1.0 Guy | 49.04 | -0.00 | 1.00 | 0 | 0 | 0 |
| 1.2D+1.0W (pattern 3) 180 deg - No lce+1.0 Guy | 48.49 | -0.01 | 1.07 | 0 | 0 | 0 |



180 Ft Guyed Tower Structural Analysis
Project Number 13323-0004.002.8700
July 31, 2023
Stafford 1 CDT
Page 30

| Load Combination | Vertical $\qquad$ | Shear <br> K | Shear ${ }_{2}$ K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { 1.2 Dead+1.0 Wind } 150 \\ & \text { deg+1.0 Ice+1.0 Temp+1.0 } \end{aligned}$ | 101.73 | 0.16 | 0.28 | 0 | 0 | 0 |
| $\begin{aligned} & \text { Guy } \\ & \text { 1.2 Dead+1.0 Wind } 180 \\ & \text { deg+1.0 Ice+1.0 Temp+1.0 } \end{aligned}$ | 101.42 | -0.03 | 0.34 | 0 | 0 | 0 |
| Guy <br> 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 | 101.74 | -0.23 | 0.32 | 0 | 0 | 0 |
| Guy <br> 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 | 102.08 | -0.38 | 0.18 | 0 | 0 | 0 |
| $\begin{aligned} & \text { Guy } \\ & \text { 1.2 Dead+1.0 Wind } 270 \\ & \text { deg+1.0 Ice+1.0 Temp+1.0 } \end{aligned}$ | 101.72 | -0.40 | -0.01 | 0 | 0 | 0 |
| $\begin{aligned} & \text { Guy } \\ & \text { 1.2 Dead+1.0 Wind } 300 \\ & \text { deg+1.0 Ice+1.0 Temp+1.0 } \end{aligned}$ | 101.40 | -0.33 | -0.19 | 0 | 0 | 0 |
| Guy <br> 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 | 101.72 | -0.20 | -0.33 | 0 | 0 | 0 |
| Guy <br> Dead+Wind 0 deg - <br> Service+Guy | 42.43 | -0.00 | -0.28 | 0 | 0 | 0 |
| Dead+Wind 30 deg Service+Guy | 42.39 | 0.14 | -0.25 | 0 | 0 | 0 |
| Dead+Wind 60 deg Service+Guy | 42.36 | 0.24 | -0.14 | 0 | 0 | 0 |
| Dead+Wind 90 deg Service+Guy | 42.39 | 0.27 | -0.00 | 0 | 0 | 0 |
| Dead+Wind 120 deg Service+Guy | 42.43 | 0.23 | 0.14 | 0 | 0 | 0 |
| Dead+Wind 150 deg Service+Guy | 42.39 | 0.12 | 0.21 | 0 | 0 | 0 |
| Dead+Wind 180 deg Service+Guy | 42.36 | -0.00 | 0.27 | 0 | 0 | 0 |
| Dead+Wind 210 deg Service+Guy | 42.39 | -0.15 | 0.25 | 0 | 0 | 0 |
| Dead+Wind 240 deg Service+Guy | 42.43 | -0.26 | 0.14 | 0 | 0 | 0 |
| Dead+Wind 270 deg Service+Guy | 42.39 | -0.28 | -0.00 | 0 | 0 | 0 |
| Dead+Wind 300 deg - . Service+Guy | 42.35 | -0.23 | -0.13 | 0 | 0 | 0 |
| Dead+Wind 330 deg Service+Guy | 42.39 | -0.13 | -0.22 | 0 | 0 | 0 |

Solution Summary

| Load Comb. | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $P X$ | PY | $P Z$ | $P X$ | PY | $P Z$ |  |
|  | $K$ | K | $K$ | $K$ | $K$ | $K$ |  |
| 1 | 0.00 | -15.80 | 0.00 | 0.00 | 15.80 | 0.00 | 0.001\% |
| 2 | 0.02 | -18.77 | -15.19 | -0.02 | 18.77 | 15.19 | 0.001\% |
| 3 | 0.02 | -18.77 | -13.86 | -0.02 | 18.77 | 13.86 | 0.001\% |
| 4 | 0.02 | -18.77 | -14.11 | -0.02 | 18.77 | 14.11 | 0.001\% |
| 5 | 0.01 | -18.77 | -13.13 | -0.01 | 18.77 | 13.13 | 0.001\% |
| 6 | 0.02 | -18.77 | -13.59 | -0.02 | 18.77 | 13.59 | 0.002\% |
| 7 | 7.75 | -18.66 | -13.45 | -7.75 | 18.66 | 13.44 | 0.001\% |
| 8 | 7.05 | -18.66 | -12.24 | -7.05 | 18.66 | 12.24 | 0.001\% |
| 9 | 7.19 | -18.66 | -12.48 | -7.19 | 18.66 | 12.48 | 0.001\% |
| 10 | 6.71 | -18.66 | -11.63 | -6.71 | 18.66 | 11.63 | 0.001\% |
| 11 | 6.95 | -18.66 | -12.06 | -6.95 | 18.66 | 12.06 | 0.001\% |
| 12 | 13.34 | -18.55 | -7.73 | -13.34 | 18.55 | 7.73 | 0.001\% |
| 13 | 12.15 | -18.55 | -7.05 | -12.15 | 18.55 | 7.05 | 0.001\% |
| 14 | 12.38 | -18.55 | -7.18 | -12.38 | 18.55 | 7.18 | 0.001\% |
| 15 | 11.55 | -18.55 | -6.68 | -11.55 | 18.55 | 6.68 | 0.002\% |

tnxTower Report - version 8.1.1.0

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | PZ | $P X$ $K$ | PY | $\begin{gathered} P Z \\ K \end{gathered}$ |  |
| Comb. | $K$ | K | K | K | $K$ |  |  |
| 16 | 11.96 | -18.55 | -6.94 | -11.96 | 18.55 | 6.93 | 0.001\% |
| 17 | 15.20 | -18.66 | -0.02 | -15.20 | 18.66 | 0.02 | 0.001\% |
| 18 | 13.86 | -18.66 | -0.02 | -13.86 | 18.66 | 0.02 | 0.001\% |
| 19 | 14.12 | -18.66 | -0.02 | -14.12 | 18.66 | 0.02 | 0.001\% |
| 20 | 13.14 | -18.66 | -0.01 | -13.14 | 18.66 | 0.01 | 0.001\% |
| 21 | 13.60 | -18.66 | -0.02 | -13.60 | 18.66 | 0.02 | 0.001\% |
| 22 | 13.07 | -18.77 | 7.56 | -13.07 | 18.77 | -7.56 | 0.001\% |
| 23 | 11.92 | -18.77 | 6.90 | -11.92 | 18.77 | -6.90 | 0.001\% |
| 24 | 12.14 | -18.77 | 7.02 | -12.14 | 18.77 | -7.02 | 0.001\% |
| 25 | 11.31 | -18.77 | 6.54 | -11.31 | 18.77 | -6.54 | 0.001\% |
| 26 | 11.68 | -18.77 | 6.76 | -11.68 | 18.77 | -6.76 | 0.002\% |
| 27 | 7.22 | -18.66 | 12.56 | -7.22 | 18.66 | -12.56 | 0.001\% |
| 28 | 6.61 | -18.66 | 11.50 | -6.61 | 18.66 | -11.50 | 0.000\% |
| 29 | 6.72 | -18.66 | 11.69 | -6.72 | 18.66 | -11.69 | 0.001\% |
| 30 | 6.25 | -18.66 | 10.85 | -6.25 | 18.66 | -10.85 | 0.001\% |
| 31 | 6.43 | -18.66 | 11.19 | -6.43 | 18.66 | -11.19 | 0.002\% |
| 32 | -0.02 | -18.55 | 15.05 | 0.02 | 18.55 | -15.05 | 0.001\% |
| 33 | -0.02 | -18.55 | 13.74 | 0.02 | 18.55 | -13.74 | 0.001\% |
| 34 | -0.02 | -18.55 | 13.99 | 0.02 | 18.55 | -13.99 | 0.001\% |
| 35 | -0.01 | -18.55 | 13.02 | 0.01 | 18.55 | -13.02 | 0.001\% |
| 36 | -0.02 | -18.55 | 13.47 | 0.02 | 18.55 | -13.47 | 0.001\% |
| 37 | -7.75 | -18.66 | 13.45 | 7.75 | 18.66 | -13.45 | 0.001\% |
| 38 | -7.05 | -18.66 | 12.24 | 7.05 | 18.66 | -12.24 | 0.001\% |
| 39 | -7.19 | -18.66 | 12.48 | 7.19 | 18.66 | -12.48 | 0.001\% |
| 40 | -6.71 | -18.66 | 11.63 | 6.70 | 18.66 | -11.63 | 0.001\% |
| 41 | -6.95 | -18.66 | 12.06 | 6.95 | 18.66 | -12.06 | 0.001\% |
| 42 | -13.46 | -18.77 | 7.80 | 13.46 | 18.77 | -7.80 | 0.001\% |
| 43 | -12.25 | -18.77 | 7.10 | 12.25 | 18.77 | -7.10 | 0.001\% |
| 44 | -12.49 | -18.77 | 7.24 | 12.49 | 18.77 | -7.24 | 0.001\% |
| 45 | -11.65 | -18.77 | 6.74 | 11.65 | 18.77 | -6.74 | 0.001\% |
| 46 | -12.06 | -18.77 | 7.00 | 12.06 | 18.77 | -7.00 | 0.002\% |
| 47 | -15.20 | -18.66 | 0.02 | 15.20 | 18.66 | -0.02 | 0.001\% |
| 48 | -13.86 | -18.66 | 0.02 | 13.86 | 18.66 | -0.02 | 0.001\% |
| 49 | -14.12 | -18.66 | 0.02 | 14.12 | 18.66 | -0.02 | 0.000\% |
| 50 | -13.14 | -18.66 | 0.01 | 13.14 | 18.66 | -0.01 | 0.001\% |
| 51 | -13.60 | -18.66 | 0.02 | 13.60 | 18.66 | -0.02 | 0.001\% |
| 52 | -12.95 | -18.55 | -7.49 | 12.95 | 18.55 | 7.49 | 0.001\% |
| 53 | -11.82 | -18.55 | -6.84 | 11.82 | 18.55 | 6.84 | 0.001\% |
| 54 | -12.04 | -18.55 | -6.96 | 12.04 | 18.55 | 6.96 | 0.001\% |
| 55 | -11.21 | -18.55 | -6.48 | 11.21 | 18.55 | 6.48 | 0.001\% |
| 56 | -11.58 | -18.55 | -6.70 | 11.58 | 18.55 | 6.70 | 0.001\% |
| 57 | -7.22 | -18.66 | -12.56 | 7.22 | 18.66 | 12.56 | 0.001\% |
| 58 | -6.61 | -18.66 | -11.50 | 6.61 | 18.66 | 11.50 | 0.000\% |
| 59 | -6.72 | -18.66 | -11.69 | 6.72 | 18.66 | 11.69 | 0.001\% |
| 60 | -6.25 | -18.66 | -10.85 | 6.25 | 18.66 | 10.85 | 0.001\% |
| 61 | -6.43 | -18.66 | -11.19 | 6.43 | 18.66 | 11.19 | 0.002\% |
| 62 | 0.00 | -61.00 | 0.00 | -0.00 | 61.00 | -0.00 | 0.000\% |
| 63 | 0.00 | -61.13 | -6.64 | -0.00 | 61.13 | 6.64 | 0.002\% |
| 64 | 3.37 | -61.00 | -5.84 | -3.37 | 61.00 | 5.84 | 0.002\% |
| 65 | 5.84 | -60.86 | -3.38 | -5.84 | 60.86 | 3.38 | 0.001\% |
| 66 | 6.64 | -61.00 | -0.00 | -6.63 | 61.00 | 0.00 | 0.002\% |
| 67 | 5.65 | -61.13 | 3.27 | -5.65 | 61.13 | -3.27 | 0.002\% |
| 68 | 3.25 | -61.00 | 5.63 | -3.25 | 61.00 | -5.63 | 0.002\% |
| 69 | -0.00 | -60.86 | 6.62 | 0.00 | 60.86 | -6.62 | 0.001\% |
| 70 | -3.37 | -61.00 | 5.84 | 3.37 | 61.00 | -5.84 | 0.002\% |
| 71 | -5.86 | -61.13 | 3.39 | 5.86 | 61.13 | -3.39 | 0.002\% |
| 72 | -6.64 | -61.00 | 0.00 | 6.63 | 61.00 | -0.00 | . $0.001 \%$ |
| 73 | -5.64 | -60.86 | -3.26 | 5.64 | 60.86 | 3.26 | 0.001\% |
| 74 | -3.25 | -61.00 | -5.63 | 3.25 -0.00 | 61.00 15.83 | 5.63 3.99 | 0.001\% |
| 75 | 0.00 | -15.83 | -3.99 -3.54 | -0.00 | 15.83 | 3.54 | 0.001\% |
| 76 | 2.04 | -15.80 | -3.54 | -3.51 | 15.77 | 2.03 | 0.001\% |
| 77 | 3.51 4.00 | -15.77 | -0.00 | -4.00 | 15.80 | 0.00 | 0.001\% |
| 79 | 3.44 | -15.83 | 1.99 | -3.44 | 15.83 | -1.99 | 0.001\% |
| 80 | 1.90 | -15.80 | 3.30 | -1.90 | 15.80 | -3.30 | 0.001\% |
| 81 | -0.00 | -15.77 | 3.96 | 0.00 | 15.77 | -3.96 | 0.001\% |
| 82 | -2.04 | -15.80 | 3.54 | 2.04 | 15.80 | -3.54 | 0.001\% |
| 83 | -3.54 | -15.83 | 2.05 | 3.54 | 15.83 | -2.05 | 0.001\% |
| 84 | -4.00 | -15.80 | 0.00 | 4.00 | 15.80 | -0.00 | 0.001\% |


|  | Sum of Applied Forces |  |  |  |  | Sum of Reactions |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | $P Y$ | $P Z$ | $P X$ | $P Y$ | $P Z$ | \% Error |  |
| Comb. | $K$ | $K$ | $K$ | $K$ | $K$ | $K$ |  |  |
| 85 | -3.41 | -15.77 | -1.97 | 3.41 | 15.77 | 1.97 | $0.001 \%$ |  |
| 86 | -1.90 | -15.80 | -3.30 | 1.90 | 15.80 | 3.30 | $0.001 \%$ |  |

## Non-Linear Convergence Results

| Load Combination | Converged? | Number of Cycles | Displacement Tolerance | Force Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 7 | 0.00000001 | 0.00007965 |
| 2 | Yes | 15 | 0.00000001 | 0.00006832 |
| 3 | Yes | 15 | 0.00000001 | 0.00007848 |
| 4 | Yes | 15 | 0.00000001 | 0.00006178 |
| 5 | Yes | 13 | 0.00000001 | 0.00006221 |
| 6 | Yes | 12 | 0.00000001 | 0.00006578 |
| 7 | Yes | 15 | 0.00000001 | 0.00004681 |
| 8 | Yes | 15 | 0.00000001 | 0.00005448 |
| 9 | Yes | 15 | 0.00000001 | 0.00004190 |
| 10 | Yes | 13 | 0.00000001 | 0.00006943 |
| 11 | Yes | 13 | 0.00000001 | 0.00003975 |
| 12 | Yes | 12 | 0.00000001 | 0.00006677 |
| 13 | Yes | 11 | 0.00000001 | 0.00004380 |
| 14 | Yes | 12 | 0.00000001 | 0.00006909 |
| 15 | Yes | 12 | 0.00000001 | 0.00009887 |
| 16 | Yes | 12 | 0.00000001 | 0.00007193 |
| 17 | Yes | 15 | 0.00000001 | 0.00004486 |
| 18 | Yes | 15 | 0.00000001 | 0.00005193 |
| 19 | Yes | 15 | 0.00000001 | 0.00003966 |
| 20 | Yes | 13 | 0.00000001 | 0.00006965 |
| 21 | Yes | 13 | 0.00000001 | 0.00003937 |
| 22 | Yes | 15 | 0.00000001 | 0.00006706 |
| 23 | Yes | 15 | 0.00000001 | 0.00007690 |
| 24 | Yes | 15 | 0.00000001 | 0.00006114 |
| 25 | Yes | 13 | 0.00000001 | 0.00006399 |
| 26 | Yes | 12 | 0.00000001 | 0.00006463 |
| 27 | Yes | 14 | 0.00000001 | 0.00009850 |
| 28 | Yes | 15 | 0.00000001 | 0.00004378 |
| 29 | Yes | 14 | 0.00000001 | 0.00009069 |
| 30 | Yes | 13 | 0.00000001 | 0.00006131 |
| 31 | Yes | 12 | 0.00000001 | 0.00009292 |
| 32 | Yes | 12 | 0.00000001 | 0.00006197 |
| 33 | Yes | 11 | 0.00000001 | 0.00004562 |
| 34 | Yes | 12 | 0.00000001 | 0.00006424 |
| 35 | Yes | 12 | 0.00000001 | 0.00009304 |
| 36 | Yes | 12 | 0.00000001 | 0.00006669 |
| 37 | Yes | 15 | 0.00000001 | 0.00004603 |
| 38 | Yes | 15 | 0.00000001 | 0.00005368 |
| 39 | Yes | 15 | 0.00000001 | 0.00004118 |
| 40 | Yes | 13 | 0.00000001 | 0.00006793 |
| 41 | Yes | 13 | 0.00000001 | 0.00003842 |
| 42 | Yes | 15 | 0.00000001 | 0.00007451 |
| 43 | Yes | 15 | 0.00000001 | 0.00008643 |
| 44 | Yes | 15 | 0.00000001 | 0.00006476 |
| 45 | Yes | 13 | 0.00000001 | 0.00006811 |
| 46 | Yes | 12 | 0.00000001 | 0.00007216 |
| 47 | Yes | 15 | 0.00000001 | 0.00004359 |
| 48 | Yes | 15 | 0.00000001 | 0.00005045 |
| 49 | Yes | 15 | 0.00000001 | 0.00003928 |
| 50 | Yes | 13 | 0.00000001 | 0.00006657 |
| 51 | Yes | 13 | 0.00000001 | 0.00003770 |
| 52 | Yes | 12 | 0.00000001 | 0.00006161 |
| 53 | Yes | 11 | 0.00000001 | 0.00004261 |
| 54 | Yes | 12 | 0.0000000 .1 | 0.00006396 |
| 55 | Yes | 12 | 0.00000001 | 0.00009233 |
| 56 | Yes | 12 | 0.00000001 | 0.00006644 |
| 57 | Yes | 14 | 0.00000001 | 0.00009705 |
| 58 | Yes | 15 | 0.00000001 | 0.00004317 |

tnxTower Report - version 8.1.1.0

|  |  |  | 0.00000001 | 0.00008930 |
| :--- | :--- | :--- | :--- | :--- |
| 59 | Yes | 14 | 0.000000001 | 0.00005937 |
| 60 | Yes | 13 | 0.00000001 | 0.00009092 |
| 61 | Yes | 12 | 0.00000001 | 0.00000422 |
| 62 | Yes | 9 | 0.0000001 | 0.00008720 |
| 63 | Yes | 12 | 0.00000001 | 0.00008337 |
| 64 | Yes | 12 | 0.00000001 | 0.00006926 |
| 65 | Yes | 12 | 0.00000001 | 0.00000207 |
| 66 | Yes | 12 | 0.00000001 | 0.0006076 |
| 67 | Yes | 12 | 0.00000001 | 0.00005515 |
| 68 | Yes | 12 | 0.00000001 | 0.00006344 |
| 69 | Yes | 12 | 0.00000001 | 0.00008467 |
| 70 | Yes | 12 | 0.00000001 | 0.00009733 |
| 71 | Yes | 12 | 0.00000001 | 0.00007869 |
| 72 | Yes | 12 | 0.00000001 | 0.00006508 |
| 73 | Yes | 12 | 0.00000001 | 0.00007044 |
| 74 | Yes | 12 | 0.00000001 | 0.00005235 |
| 75 | Yes | 11 | 0.00000001 | 0.00005316 |
| 76 | Yes | 11 | 0.00000001 | 0.00005148 |
| 77 | Yes | 11 | 0.00000001 | 0.00004801 |
| 78 | Yes | 11 | 0.00000001 | 0.00004845 |
| 79 | Yes | 11 | 0.00000001 | 0.0000368 |
| 80 | Yes | 11 | 0.00000001 | 0.00004815 |
| 81 | Yes | 11 | 0.00000001 | 0.00005254 |
| 82 | Yes | 11 | 0.00000001 | 0.00006393 |
| 83 | Yes | 11 | 0.00000001 | 0.00005168 |
| 84 | Yes | 11 | 0.00000001 | 0.00005047 |
| 85 | Yes | 11 | 0.00000001 | 0.00004437 |
| 86 | Yes | 11 |  |  |

## Maximum Tower Deflections - Service Wind

\(\left.$$
\begin{array}{cccccc}\begin{array}{c}\text { Section } \\
\text { No. }\end{array} & \text { Elevation } & \begin{array}{c}\text { Horz. } \\
\text { Deflection } \\
\text { in }\end{array}
$$ \& \begin{array}{c}Gov. <br>
Load <br>

Comb.\end{array} \& Tilt\end{array}\right]\)| Twist |
| :---: |
|  |
| T1 |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 179.00 | $16 \mathrm{ft} \times 2.5$ " omni whip | 77 | 1.10 | 0.047 | 0.133 | 199237 |
| 171.00 | APXVAALL24_43-U-NA20_TIA w/ Mount Pipe | 77 | 1.01 | 0.041 0.037 | 0.131 0.128 | 110687 |
| 163.00 | PD201 | 77 | 0.92 | 0.037 | 0.128 | 59187 |
| 162.52 | Guy | 77 | 0.92 | 0.037 | 0.128 | 195314 |
| 153.00 | NHH-65B-R2B_TIA w/ Mount Pipe | 77 | 0.83 | 0.037 | 0.124 0.115 | 195314 |
| 138.00 | 3' $\times 2.375^{\prime \prime}$ Pipe Mount | 77 | 0.69 | 0.043 0.038 | 0.115 0.101 | 43699 |
| 121.00 | DB420 | 77 | 0.50 | 0.038 | 0.099 | 40747 |
| 119.39 | Guy | 77 | 0.48 | 0.037 | 0.043 | 34247 |
| 82.52 | Guy | 77 | 0.28 | 0.003 | 0.043 0.040 | 40442 |
| 77.00 | PD201 | 77 | 0.28 | 0.001 | 0.040 | 40442 |

tnxTower Report - version 8.1.1.0

## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | o |
| :---: | :---: | :---: | :---: | :---: | :---: | | ft | $180-160$ | 5.98 | 43 | 0.311 |
| :---: | :---: | :---: | :---: | :---: |
| T1 | $160-140$ | 4.57 | 43 | 0.266 |
| T2 | $140-120$ | 3.43 | 8 | 0.273 |
| T3 | $120-100$ | 2.24 | 38 | 0.217 |
| T4 | $100-80$ | 1.57 | 16 | 0.141 |
| T5 | $80-60$ | 1.28 | 16 | 0.071 |
| T6 | $60-40$ | 1.39 | 15 | 0.037 |
| T7 | $40-20$ | 1.37 | 15 | 0.057 |
| T8 | $20-4.81771$ | 0.84 | 15 | 0.1449 |
| T9 | $4.81771-$ | 0.18 | 15 | 0.177 |
| T10 | $3.33333 \mathrm{e}-007$ |  |  |  |
|  |  |  |  | 0.277 |
|  |  |  |  | 0.174 |


| Critical Deflections and Radius of Curvature - Design Wind |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Elevation ft | Appurtenance | Gov. <br> Load <br> Comb. | Deflection in | Tilt | Twist | Radius of Curvature ft |
| 179.00 | $16 \mathrm{ft} \times 2.5$ " omni whip | 43 | 5.91 | 0.308 | 0.506 | 41227 |
| 171.00 | APXVAALL24_43-U-NA20_TIA w/ Mount Pipe | 43 | 5.33 | 0.284 | 0.499 | 22904 |
| 163.00 | PD201 | 43 | 4.77 | 0.269 | 0.490 | 12200 |
| 162.52 | Guy | 43 | 4.74 | 0.268 | 0.489 | 11930 |
| 153.00 | $\underset{\text { Pipe }}{\text { NHH-65B-R2B_TIA }} \mathbf{w} /$ Mount | 43 | 4.14 | 0.268 | 0.475 | 15427 |
| 138.00 | 3 ' x 2.375" Pipe Mount | 8 | 3.31 | 0.271 | 0.445 | 9366 |
| 121.00 | DB420 | 38 | 2.29 | 0.221 | 0.395 | 6888 |
| 119.39 | Guy | 38 | 2.20 | 0.215 | 0.388 | 6575 |
| 82.52 | Guy | 16 | 1.29 | 0.079 | 0.180 | 8148 |
| 77.00 | PD201 | 16 | 1.28 | 0.062 | 0.170 | 9549 |

## Bolt Design Data

| Section No. | Elevation | Component Type | Bolt Grade | Bolt Size in | Number Of Bolts | Maximum Load per Bolt K | Allowable Load per Bolt K | Ratio <br> Load <br> Allowable | Allowable Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 180 | Leg | A325X | 0.75 | 4 | 1.00 | 30.10 | 0.033 | 1 | Bolt Tension |
|  |  | Diagonal | A325X | 0.50 | 1 | 1.47 | 5.92 | 0.248 | 1.05 | Member Bearing |
|  |  | Top Girt | A325X | 0.50 | 1 | 0.04 | 5.92 | 0.007 | 1 | Member Bearing |
|  |  | Bottom Girt | A325X | 0.50 | 1 | 0.42 | 5.92 | 0.071 | 1.05 | Member <br> Bearing |
|  |  | Top Guy PullOff@162.523 | A325N | 0.63 | 2 | 2.17 | 16.45 | 0.132 | 1.05 | Member Block Shear |
| T2 | 160 | Leg | A325X | 0.75 | 4 | 1.47 | 30.10 | 0.049 | 1.05 | Boit Tension |
|  |  | Diagonal | A325X | 0.50 | 1 | 1.18 | 5.92 | 0.199 | 1.05 | Member Bearing |
|  |  | Top Girt | A325X | 0.50 | 1 | 0.46 | 5.92 | 0.078 | 1.05 | Member Bearing |
|  |  | Bottom Girt | A325X | 0.50 | 1 | 0.31 | 5.92 | 0.053 | 1.05 | Member Bearing |
| T3 | 140 | Leg | A325X | 0.75 | 4 | 1.68 | 30.10 | 0.056 | 1.05 | Bolt Tension |

tnxTower Report - version 8.1.1.0


Guy Design Data

| $\begin{aligned} & \text { Section } \\ & \text { No. } \end{aligned}$ | Elevation | Size | Initial Tension K | Breaking Load K | Actual $T_{\mu}$ K | $\begin{gathered} \text { Allowable } \\ \phi T_{n} \\ K \\ \hline \end{gathered}$ | Required S.F. | Actual S.F. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | $\frac{162.52(A)}{}$ | 3/4 EHS | 5.83 | 58.30 | 14.30 | 36.73 | 0.952 | 2.446 |
|  | $\begin{gathered} (432) \\ 162.52(B) \\ (431) \end{gathered}$ | 3/4 EHS | 5.83 | 58.30 | 14.24 | 36.73 | 0.952 | 2.457 |

tnxTower Report - version 8.1.1.0

180 Ft Guyed Tower Structural Analysis
July 31, 2023
Project Number 13323-0004.002.8700

| Section No. | Elevation ft | Size | $\begin{gathered} \text { Initial } \\ \text { Tension } \\ K \\ \hline \end{gathered}$ | Breaking Load K | Actual $T_{u}$ $K$ | Allowable $\phi T_{n}$ $K$ | Required S.F. | Actual S.F. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T4 | $\begin{gathered} 162.52(C) \\ (427) \end{gathered}$ | 3/4 EHS | 5.83 | 58.30 | 14.40 | 36.73 | 0.952 | 2.429 |
|  | $\begin{gathered} 119.39(A) \\ (435) \end{gathered}$ | 1/2 EHS | 2.69 | 26.90 | 6.36 | 16.95 | 0.952 | 2.536 |
|  | $\begin{gathered} 119.39(B) \\ (434) \end{gathered}$ | 1/2 EHS | 2.69 | 26.90 | 6.34 | 16.95 | 0.952 | 2.545 |
| T5 | $\begin{gathered} 119.39 \text { (C) } \\ (433) \end{gathered}$ | 1/2 EHS | 2.69 | 26.90 | 6.38 | 16.95 | 0.952 | 2.531 |
|  | $\begin{gathered} 82.52(A) \\ (447) \end{gathered}$ | 1/2 EHS | 2.69 | 26.90 | 6.07 | 16.95 | 0.952 | 2.657 |
|  | $\begin{gathered} 82.52(A) \\ (448) \end{gathered}$ | 1/2 EHS | 2.69 | 26.90 | 5.99 | 16.95 | 0.952 | 2.697 |
|  | $\begin{gathered} 82.52(B) \\ (443) \end{gathered}$ | 1/2 EHS | 2.69 | 26.90 | 6.03 | 16.95 | 0.952 | 2.674 |
|  | $\begin{gathered} 82.52 \text { (B) } \\ (444) \end{gathered}$ | 1/2 EHS | 2.69 | 26.90 | 6.03 | 16.95 | 0.952 | 2.677 |
|  | $\begin{gathered} 82.52(C) \\ (436) \end{gathered}$ | 1/2 EHS | 2.69 | 26.90 | 6.00 | 16.95 | 0.952 | 2.690 |
|  | $\begin{gathered} 82.52 \text { (C) } \\ (437) \end{gathered}$ | 1/2 EHS | 2.69 | 26.90 | 6.10 | 16.95 | 0.952 | 2.645 |

## Compression Checks

| Leg Design Data (Compression) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section <br> No. | Elevation ft | Size | $L$ <br> $f t$ | $\begin{gathered} L_{u} \\ f t \end{gathered}$ | $\mathrm{K} / \mathrm{/r}$ | A $i^{2}$ | Mast Stability index | $\begin{gathered} P_{u} \\ K \end{gathered}$ | $\begin{gathered} \phi P_{n} \\ k \end{gathered}$ | $\begin{aligned} & \text { Ratio } \\ & P_{u} \\ & \hline \phi P_{n} \end{aligned}$ |
| T1 | 180-160 | $\begin{aligned} & \text { Pipe } 2.375^{\prime \prime} \mathrm{x} \\ & 0.218^{\prime \prime}(2 \mathrm{XS}) \end{aligned}$ | 20.00 | 2.41 | $\begin{gathered} 37.7 \\ K=1.00 \end{gathered}$ | 1.48 | 1.00 | -12.09 | 59.91 | $\frac{\varphi P_{n}^{1}}{0.202^{1}}$ |
| T2 | 160-140 | $\begin{aligned} & \text { Pipe } 2.375^{\prime \prime} x \\ & 0.218^{\prime \prime}(2 \mathrm{XS}) \end{aligned}$ | 20.00 | 2.41 | $\begin{gathered} 37.7 \\ K=1.00 \end{gathered}$ | 1.48 | 1.00 | -17.95 | 59.91 | $0.300^{1}$ |
| T3 | 140-120 | $\begin{aligned} & \text { Pipe } 2.375^{\prime \prime} \mathrm{x} \\ & 0.218^{\prime \prime}(2 \mathrm{XS}) \end{aligned}$ | 20.00 | 2.41 | $\begin{gathered} 37.7 \\ K=1.00 \end{gathered}$ | 1.48 | 1.00 | -18.94 | 59.91 | $0.316^{1}$ |
| T4 | 120-100 | $\begin{aligned} & \text { Pipe } 2.375^{\prime \prime} \mathrm{x} \\ & 0.218^{\prime \prime}(2 \mathrm{XS}) \end{aligned}$ | 20.00 | 2.41 | $\begin{gathered} 37.7 \\ K=1.00 \end{gathered}$ | 1.48 | 1.00 | $-24.20$ | 59.91 | $0.404^{1}$ |
| T5 | 100-80 | $\begin{gathered} \text { Pipe } 2.875^{\prime \prime} \times \\ 0.276^{\prime \prime}(2.5 \mathrm{XS}) \end{gathered}$ | 20.00 | 0.11 | $\begin{gathered} 1.5 \\ K=1.00 \end{gathered}$ | 2.25 | 0.95 | -32.93 | 96.60 | $0.341^{1}$ |
| T6 | 80-60 | $\begin{gathered} \text { Pipe } 2.875^{\prime \prime} \mathrm{x} \\ 0.276 \mathrm{k}(2.5 \mathrm{XS}) \end{gathered}$ | 20.00 | 2.41 | $\begin{gathered} 62.6 \\ K=2.00 \end{gathered}$ | 2.25 | 1.00 | -32.68 | 76.17 | $0.429^{1}$ |
| T7 | 60-40 | $\begin{gathered} \text { Pipe } 2.875^{\prime \prime} \times \\ 0.203^{\prime \prime}(2.5 \text { STD }) \end{gathered}$ | 20.00 | 2.41 | $\begin{aligned} & 61.0 \\ & K=2.00 \end{aligned}$ | 1.70 | 1.00 | -35.24 | 58.41 | $0.603^{1}$ |
| T8 | 40-20 | $\begin{gathered} \text { Pipe } 2.875^{\prime \prime} \mathrm{x} \\ 0.203 \text { " } 2.5 \mathrm{STD} \text { ) } \end{gathered}$ | 20.00 | 2.41 | $\begin{gathered} 61.0 \\ K=2.00 \end{gathered}$ | 1.70 | 1.00 | -36.00 | 58.41 | $0.616^{1}$ |
| T9 | 20-4.81771 | $\begin{gathered} \text { Pipe } 2.875^{\prime \prime} \times \\ 0.276^{\prime \prime}(2.5 \times S) \end{gathered}$ | 15.18 | 2.41 | $\begin{gathered} 62.6 \\ K=2.00 \end{gathered}$ | 2.25 | 1.00 | -35.54 | 76.17 | $0.467^{1}$ |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 e-007 \end{gathered}$ | $\begin{gathered} \text { Pipe } 2.875^{\prime \prime} \times \\ 0.276^{\prime \prime}(2.5 \times S) \end{gathered}$ | 5.21 | 1.38 | $\begin{gathered} 17.9 \\ K=1.00 \end{gathered}$ | 2.25 | 0.78 | -36.40 | 77.52 | $0.469^{41}$ |

* DL controls
${ }^{1} P_{u} / \phi P_{n}$ controls


## Diagonal Design Data (Compression)

| Section | Elevation | Size | $L$ | $L_{u}$ | $\mathrm{Kl/r}$ | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f$ |  | $f t$ | $f t$ |  | $i n^{2}$ | $K$ | $K$ | $\phi P_{n}$ |
| T1 | 180-160 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}$ (16 ga) | 3.72 | 3.72 | $\begin{gathered} 87.5 \\ K=1.00 \end{gathered}$ | 0.26 | -1.67 | 6.21 | $0.268^{1}$ |
| T2 | 160-140 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.72 | 3.72 | $\begin{gathered} 87.5 \\ K=1.00 \end{gathered}$ | 0.26 | -1.36 | 6.21 | $0.219^{\circ}$ |
| T3 | 140-120 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.72 | 3.72 | $\begin{gathered} 87.5 \\ K=1.00 \end{gathered}$ | 0.26 | -1.20 | 6.21 | $0.193^{1}$ |
| T4 | 120-100 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.72 | 3.72 | $\begin{gathered} 87.5 \\ K=1.00 \end{gathered}$ | 0.26 | -0.75 | 6.21 | $0.120^{1}$ |
| T5 | 100-80 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.72 | 3.72 | $\begin{gathered} 87.5 \\ K=1.00 \end{gathered}$ | 0.26 | -1.95 | 6.21 | $0.314^{1}$ |
| T6 | 80-60 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.72 | 3.72 | $\begin{gathered} 87.5 \\ K=1.00 \end{gathered}$ | 0.26 | -1.57 | 6.21 | $0.254^{1}$ |
| T7 | 60-40 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.72 | 3.72 | $\begin{gathered} 87.5 \\ K=1.00 \end{gathered}$ | 0.26 | -0.97 | 6.21 | $0.156^{1}$ |
| T8 | 40-20 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.72 | 3.72 | $\begin{gathered} 87.5 \\ \mathrm{~K}=1.00 \end{gathered}$ | 0.26 | -0.59 | 6.21 | $0.096^{1}$ |
| T9 | 20-4.81771 | Pipe 1.5" $\times 0.058$ " (16 ga) | 3.72 | 3.72 | $\begin{gathered} 87.5 \\ K=1.00 \end{gathered}$ | 0.26 | -0.83 | 6.21 | $0.134^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Horizontal Design Data (Compression)

| Section No. | Elevation | Size | $L$ | $L_{\mu}$ | K/r | A | $P_{u}$ | $\phi P_{\square}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft |  | $f t$ | $f$ |  | $i \mathrm{in}^{2}$ | $K$ | $K$ | $\phi P_{n}$ |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 \mathrm{e}-007 \end{gathered}$ | L $4 \times 4 \times 1 / 4$ | 2.51 | 2.27 | $\begin{gathered} 34.3 \\ K=1.00 \end{gathered}$ | 1.94 | -0.67 | 65.06 | $0^{0.010^{\circ}}$ |

* DL controls
${ }^{1} P_{u} / \phi P_{n}$ controls


## Top Girt Design Data (Compression)

| Section <br> No. | Elevation | Size | L | $L_{u}$ | KI/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i \mathrm{n}^{2}$ | $K$ | $K$ | $\phi P_{n}$ |
| T1 | 180-160 | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | $\begin{gathered} 75.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.03 | 6.99 | $0.004^{1}$ |
| T2 | 160-140 | Pipe 1.5' $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | $\begin{gathered} 75.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.31 | 6.99 | $0.045^{1}$ |
| T3 | 140-120 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | $\begin{gathered} 75.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.35 | 6.99 | $0.050^{1}$ |
| T4 | 120-100 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | $\begin{gathered} 75.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.42 | 6.99 | $0.060^{1}$ |
| T5 | 100-80 | Pipe 1.5" $\times 0.058^{\prime \prime}$ ( 16 ga ) | 3.42 | 3.18 | $\begin{gathered} 74.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.57 | 7.05 | $0.081^{1}$ |
| T6 | 80-60 | Pipe 1.5' $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | $\begin{gathered} 74.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.57 | 7.05 | $0.081^{1}$ |
| T7 | 60-40 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | $\begin{gathered} 74.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.61 | 7.05 | $0.087^{1}$ |
| T8 | 40-20 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.18 | $\begin{gathered} 74.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.62 | 7.05 | $0.088^{1}$ |
| T9 | 20-4.81771 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | 74.7 | 0.26 | -0.62 | 7.05 | $0.088^{1}$ |

[^0]

* DL controls
${ }^{1} P_{u} / \phi P_{n}$ controls


## Bottom Girt Design Data (Compression)

| Section No. | Elevation <br> ft | Size | $L$ <br> ft | $L_{u}$ <br> ft | Kl/r | $A$ $i n^{2}$ | $\begin{gathered} P_{u} \\ K \end{gathered}$ | $\phi P_{n}$ $K$ | $\begin{aligned} & \text { Ratio } \\ & P_{u} \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 180-160 | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.22 | $\begin{gathered} 75.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.21 | 6.99 | $0.030^{71}$ |
| T2 | 160-140 | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.22 | $\begin{gathered} 75.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.31 | 6.99 | $0.045^{1}$ |
| T3 | 140-120 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.22 | $\begin{gathered} 75.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.35 | 6.99 | $0.050^{1}$ |
| T4 | 120-100 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | $\begin{gathered} 75.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.42 | 6.99 | $0.060^{1}$ |
| T5 | 100-80 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | $\begin{gathered} 74.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.57 | 7.05 | $0.081^{1}$ |
| T6 | 80-60 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.18 | $\begin{gathered} 74.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.57 | 7.05 | $0.081{ }^{1}$ |
| T7 | 60-40 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.18 | $\begin{gathered} 74.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.61 | 7.05 | $0.087^{1}$ |
| T8 | 40-20 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | $\begin{gathered} 74.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.62 | 7.05 | $0.088^{1}$ |
| T9 | 20-4.81771 | Pipe 1.5' $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | $\begin{gathered} 74.7 \\ K=1.00 \end{gathered}$ | 0.26 | -0.62 | 7.05 | $0.088^{1}$ |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 e-007 \end{gathered}$ | L $4 \times 4 \times 1 / 4$ | 0.71 | 0.47 | $\begin{gathered} 7.1 \\ K=1.00 \end{gathered}$ | 1.94 | -0.24 | 67.37 | $0.004^{* 1}$ |

* DL controls
${ }^{1} P_{u} / \phi P_{n}$ controls


## Top Guy Pull-Off Design Data (Compression)

| Section No. | Elevation <br> ft | Size | $L$ <br> ft | $L_{u}$ <br> ft | $K / T$ | A $i n^{2}$ | $P_{u}$ $K$ | $\phi P_{n}$ $K$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \phi P_{n} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T5 | 100-80 | $2 \mathrm{~L} 2 \times 2 \times 1 / 4(3 / 8)$ <br> 2L 'a' > 18.36 in - 441 | 3.42 | 3.18 | $\begin{gathered} 104.9 \\ K=1.00 \end{gathered}$ | 1.88 | -1.79 | 43.61 | $0.041^{1}$ |

[^1]
## Top Guy Pull-Off Bending Design Data

180 Ft Guyed Tower Structural Analysis

| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | Ratio $M_{u x}$ | $M_{u y}$ kip-ft | $\phi M_{n y}$ kip-ft | Ratio $M_{u y}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft |  | kip-ft | kip-ft | $\phi M_{n x}$ | kip-ft | kip-ft | $\phi M_{n y}$ |
| T5 | 100-80 | 2L. $2 \times 2 \times 1 / 4$ (3/8) | 0 | 2 | 0.000 | 0 | 3 | 0.000 |

Top Guy Pull-Off Interaction Design Data

| Section No. | Elevation ft | Size | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \phi P_{n} \end{gathered}$ | Ratio $\frac{M_{u x}}{\phi M_{n x}}$ | $\begin{gathered} \text { Ratio } \\ M_{u y} \\ \hline \phi M_{n y} \end{gathered}$ | Comb. Stress Ratio | Allow. Stress Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T5 | 100-80 | $2 \mathrm{~L} 2 \times 2 \times 1 / 4(3 / 8)$ | 0.041 | 0.000 | 0.000 | $\begin{gathered} 0.041^{1} \\ \end{gathered}$ | 1.050 | 4.8.1 |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Torque-Arm Top Design Data

| Section No. | Elevation | Size | L | $L_{u}$ | KI/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | ft |  | ft | ft |  | $i n^{2}$ | $K$ | $K$ | $\phi P_{n}$ |
| T5 | 100-80 (438) | C10x15.3 | 3.42 | 3.30 | $\begin{gathered} 55.5 \\ K=1.00 \end{gathered}$ | 4.49 | -0.19 | 123.71 | 0.001 |
| T5 | 100-80 (439) | C10x15.3 | 3.42 | 3.30 | $\begin{gathered} 55.5 \\ K=1.00 \end{gathered}$ | 4.49 | -0.11 | 123.71 | 0.001 |
| T5 | 100-80 (445) | C10x15.3 | 3.42 | 3.30 | $\begin{gathered} 55.5 \\ K=1.00 \end{gathered}$ | 4.49 | -0.25 | 123.71 | 0.002 |
| T5 | 100-80 (446) | C10x15.3 | 3.42 | 3.30 | $\begin{gathered} 55.5 \\ K=1.00 \end{gathered}$ | 4.49 | -0.50 | 123.71 | 0.004 |
| T5 | 100-80 (449) | C10x15.3 | 3.42 | 3.30 | $\begin{gathered} 55.5 \\ K=1.00 \end{gathered}$ | 4.49 | -0.29 | 123.71 | 0.002 |
| T5 | 100-80 (450) | C10x15.3 | 3.42 | 3.30 | $\stackrel{55.5}{K=1.00}$ | 4.49 | -0.44 | 123.71 | 0.004 |


| Torque-Arm Top Bending Design Data |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | Ratio $M_{u x}$ | $M_{u y}$ | $\phi M_{n y}$ | Ratio $\mathrm{May}^{\mathbf{M a y}}$ |
|  | $f t$ |  | kip-ft | kip-ft | $\phi M_{n x}$ | kip-ft | kip-ft | $\phi M_{n y}$ |
| T5 | 100-80 (438) | C10×15.3 | -8 | 42 | 0.188 | 0 | 5 | 0.000 |
| T5 | 100-80(439) | C10x15.3 | -8 | 42 | 0.185 | 0 | 5 | 0.000 |
| T5 | 100-80(445) | C10x15.3 | -8 | 42 | 0.185 | 0 | 5 | 0.000 |
| T5 | 100-80(446) | C10x15.3 | -8 | 42 | 0.187 | 0 | 5 | 0.000 |
| T5 | 100-80 (449) | C10x15.3 | -8 | 42 | 0.185 | 0 | 5 | 0.000 0.000 |
| T5 | 100-80 (450) | C10×15.3 | -8 | 42 | 0.185 | 0 | 5 | 0.000 |

## Torque-Arm Top Interaction Design Data

| Section No. | Elevation | Size | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ M_{u x} \\ \hline \phi M_{n x} \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ M_{u y} \\ \hline \phi M_{n y} \end{gathered}$ | Comb. <br> Stress <br> Ratio | Allow. Stress Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T5 | 100-80 (438) | C10×15.3 | 0.001 | 0.188 | 0.000 | $0.189$ | 1.050 | 4.8 .1 |
| T5 | 100-80 (439) | C10x15.3 | 0.001 | 0.185 | 0.000 | $0.186$ | 1.050 | 4.8.1 |

180 Ft Guyed Tower Structural Analysis
July 31, 2023
Project Number 13323-0004.002.8700
Stafford 1 CDT
Page 40

| Section No. | Elevation <br> $f t$ | Size | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \phi P_{n} \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Ratio } \\ & M_{u x} \\ & \hline \phi M_{n x} \end{aligned}$ | $\begin{gathered} \text { Ratio } \\ M_{u \gamma} \\ \hline \phi M_{n y} \end{gathered}$ | Comb. Stress Ratio | Allow. Stress Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T5 | 100-80 (445) | C10x15.3 | 0.002 | 0.185 | 0.000 | $0.186$ | 1.050 | 4.8 .1 |
| T5 | 100-80 (446) | C10×15.3 | 0.004 | 0.187 | 0.000 | $0.189$ | 1.050 | 4.8 .1 |
| T5 | 100-80(449) | C10x15.3 | 0.002 | 0.185 | 0.000 | $0.186$ | 1.050 | 4.8 .1 |
| T5 | 100-80 (450) | C10×15.3 | 0.004 | 0.185 | 0.000 | $0.186$ | 1.050 | 4.8 .1 |

## Tension Checks

| Leg Design Data (Tension) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation ft | Size | $\begin{aligned} & L \\ & f t \end{aligned}$ | $\begin{aligned} & L_{u} \\ & f t \end{aligned}$ | KI/r | $\begin{gathered} A \\ i n^{2} \end{gathered}$ | Pu $K$ | $\phi P_{n}$ $\kappa$ | $$ |
| T1 | 180-160 | Pipe $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2$ <br> XS) | 20.00 | 2.41 | 37.7 | 1.48 |  | K 66.48 | $\frac{\phi P_{n}}{0.112^{i}}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

| Diagonal Design Data (Tension) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation ft | Size | $\begin{aligned} & L \\ & f t \end{aligned}$ | $\begin{gathered} L_{u} \\ f t \end{gathered}$ | K/Ir | A | $\begin{gathered} P_{u} \\ K \end{gathered}$ | $\phi P_{n}$ $K$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
| T1 | 180-160 | Pipe 1.5" $\times 0.058$ " (16 ga) | 3.72 | 3.72 | 87.5 | 0.26 | 1.47 | 9.93 | $\frac{\phi P_{n}}{0.148^{1}}$ |
| T2 | 160-140 | Pipe 1.5" x 0.058" (16 ga) | 3.72 | 3.72 | 87.5 | 0.26 | 1.18 | 9.93 | $0.118^{1}$ |
| T3 | 140-120 | Pipe 1.5" $\times 0.058$ " (16 ga) | 3.72 | 3.72 | 87.5 | 0.26 | 0.82 | 9.93 | $0.082^{1}$ |
| T4 | 120-100 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.72 | 3.72 | 87.5 | 0.26 | 0.60 | 9.93 | $\stackrel{y}{0.0601}$ |
| T5 | 100-80 | Pipe 1.5" ${ }^{\text {x }} 0.058^{\prime \prime}$ (16 ga) | 3.72 | 3.72 | 87.5 | 0.26 | 0.83 | 9.93 | 0.0841 |
| T6 | 80-60 | Pipe 1.5" $\times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.72 | 3.72 | 87.5 | 0.26 | 1.48 | 9.93 | $0.149^{1}$ |
| T7 | 60-40 | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.72 | 3.72 | 87.5 | 0.26 | 0.82 | 9.93 | $0.0821$ |
| T8 | 40-20 | Pipe 1.5" $\times 0.058{ }^{\prime \prime}$ (16 ga) | 3.72 | 3.72 | 87.5 | 0.26 | 0.44 | 9.93 | $0.04{ }^{1}$ |
| T9 | 20-4.81771 | Pipe 1.5" $\times 0.058$ " (16 ga) | 3.72 | 3.72 | 87.5 | 0.26 | 0.82 | 9.93 |  |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Horizontal Design Data (Tension)

| Section No. | Elevation | Size | $L$ | $L_{u}$ | $K / / r$ | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft |  | $f t$ | $f t$ |  | $i n^{2}$ | $K$ | K | $\phi P_{n}$ |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 \mathrm{e}-007 \end{gathered}$ | L $4 \times 4 \times 1 / 4$ | 1.61 | 1.37 | 13.2 | 1.94 | 0.67 | 62.86 | $0.011^{\circ}$ |

* DL controls
${ }^{1} P_{u} / \phi P_{n}$ controls


## Top Girt Design Data (Tension)

| Section No. | Elevation | Size | L | $L_{u}$ | KI/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f$ |  | ft | ft |  | $i n^{2}$ | $K$ | $K$ | $\phi P_{n}$ |
| T1 | 180-160 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | 75.7 | 0.26 | 0.04 | 9.93 | $0.004^{-1}$ |
| T2 | 160-140 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | 75.7 | 0.26 | 0.46 | 9.93 | $0.046^{1}$ |
| T3 | 140-120 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | 75.7 | 0.26 | 0.35 | 9.93 | $0.035^{1}$ |
| T4 | 120-100 | Pipe 1.5' $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | 75.7 | 0.26 | 2.42 | 9.93 | $0.244^{1}$ |
| T5 | 100-80 | Pipe 1.5" $\times 0.058{ }^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | 74.7 | 0.26 | 0.57 | 9.93 | $0.057^{1}$ |
| T6 | 80-60 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.18 | 74.7 | 0.26 | 0.76 | 9.93 | $0.076^{1}$ |
| T7 | 60-40 | Pipe 1.5 " $\times 0.058^{\prime \prime}$ ( 16 ga ) | 3.42 | 3.18 | 74.7 | 0.26 | 0.61 | 9.93 | $0.062^{1}$ |
| T8 | 40-20 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | 74.7 | 0.26 | 0.62 | 9.93 | $0.063^{1}$ |
| T9 | 20-4.81771 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.48 | 74.7 | 0.26 | 0.62 | 9.93 | $0.062^{1}$ |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 e-007 \end{gathered}$ | L $4 \times 4 \times 1 / 4$ | 3.42 | 3.18 | 30.5 | 1.94 | 6.77 | 62.86 | $0.108^{11}$ |

* DL controls
${ }^{1} P_{u} / \phi P_{n}$ controls

| Botom Girt Design Data (Tension) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation | Size | $L$ | $L_{u}$ | KI/r | A | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| No. | $f t$ |  | ft | $f t$ |  | $i 7^{2}$ | $K$ | $K$ | $\phi P_{n}$ |
| T1 | 180-160 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | 75.7 | 0.26 | 0.42 | 9.93 | $0.042^{1}$ |
| T2 | 160-140 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | 75.7 | 0.26 | 0.31 | 9.93 | $0.031^{1}$ |
| T3 | 140-120 | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | 75.7 | 0.26 | 0.47 | 9.93 | $0.047^{1}$ |
| T4 | 120-100 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.22 | 75.7 | 0.26 | 0.42 | 9.93 | $0.042^{1}$ |
| T5 | 100-80 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | 74.7 | 0.26 | 0.63 | 9.93 | $0.063^{1}$ |
| T6 | 80-60 | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.18 | 74.7 | 0.26 | 0.57 | 9.93 | $0.057^{1}$ |
| T7 | 60-40 | Pipe 1.5" $\times 0.058^{\prime \prime}$ (16 ga) | 3.42 | 3.18 | 74.7 | 0.26 | 0.61 | 9.93 | $0.062^{1}$ |

tnxTower Report - version 8.1.1.0

July 31, 2023
180 Ft Guyed Tower Structural Analysis
Stafford 1 CDT
Page 42

| Section No. | Elevation <br> ft | Size | $L$ <br> ft | $L_{u}$ <br> ft | KI/r | A $i n^{2}$ | $P_{u}$ $K$ | $\phi P_{n}$ $K$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T8 | 40-20 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.18 | 74.7 | 0.26 | 0.62 | 9.93 | $0.063{ }^{1}$ |
| T9 | 20-4.81771 | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 3.42 | 3.18 | 74.7 | 0.26 | 1.01 | 9.93 | $0.101^{\circ 1}$ |

" DL controls
${ }^{1} P_{u} / \phi P_{n}$ controls

## Top Guy Pull-Off Design Data (Tension)

| Section No. | Elevation ft | Size | L ft | $L_{u}$ <br> ft | KI/r | A $i n^{2}$ | $P_{u}$ $K$ | $\phi P_{n}$ $K$ | $\begin{aligned} & \text { Ratio } \\ & \frac{P_{u}}{\phi P_{n}} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 180-160 | $\begin{gathered} 2 \mathrm{~L} .2 \times 2 \times 1 / 4(3 / 8) \\ 2 \mathrm{~L} \text { 'a' }>18.60 \mathrm{in}-430 \end{gathered}$ | 3.42 | 3.22 | 63.4 | 1.13 | 4.34 | 49.10 | $\frac{\phi P_{n}}{0.088}{ }^{1}$ |
| T5 | 100-80 | $\begin{gathered} 2 \mathrm{~L} 2 \times 2 \times 1 / 4(3 / 8) \\ 2 \mathrm{~L} \text { 'a' }>18.36 \mathrm{in}-441 \end{gathered}$ | 3.42 | 3.18 | 62.6 | 1.13 | 2.89 | 49.10 | $0.059{ }^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Top Guy Pull-Off Bending Design Data

| Section No. | Elevation <br> ft | Size | $M_{u x}$ kip-ft | $\phi M_{n x}$ kip-ft | $\begin{gathered} \text { Ratio } \\ M_{u x} \\ \hline \end{gathered}$ | $\begin{gathered} M_{u y} \\ k i p-f t \end{gathered}$ | $\phi M_{n y}$ kip-ft | Ratio $M_{\mathrm{Ly}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 180-160 | $2 \mathrm{~L} 2 \times 2 \times 1 / 4(3 / 8)$ | 0 | 2 |  |  |  | $\phi M_{n y}$ |
| T5 | 100-80 | $2 \mathrm{~L} 2 \times 2 \times 1 / 4(3 / 8)$ | 0 | 2 | 0.000 | 0 | 3 | 0.000 0.000 |

## Top Guy Pull-Off Interaction Design Data

| Section No. | Elevation <br> ft | Size | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \phi P_{n} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ M_{u x} \\ \hline \phi M_{n x} \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ M_{u y} \\ \hline \phi M_{n y} \end{gathered}$ | Comb. <br> Stress <br> Ratio | Allow. Stress Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 180-160 | $2 \mathrm{~L} 2 \times 2 \times 1 / 4(3 / 8)$ | 0.088 | 0.000 | 0.000 | $0.088^{1}$ | 1.050 | $4.8 .1{ }^{\text {\% }}$ |
| T5 | 100-80 | $2 \mathrm{~L} 2 \times 2 \times 1 / 4(3 / 8)$ | 0.059 | 0.000 | 0.000 | $0.059^{1}$ | 1.050 | 4.8.1 |

${ }^{1} P_{u} / \phi P_{n}$ controls

| Torque-Arm Top Design Data |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | $L$ | $L_{u}$ | KI/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
|  | $f t$ |  | $f$ | $f t$ |  | $i n^{2}$ | K | $K$ | ${ }_{\phi} P_{n}$ |
| T5 | 100-80 (438) | C10×15.3 | 3.42 | 3.30 | 55.5 | 4.49 | 1.73 | 145.48 | 0.012 |
| T5 | 100-80 (439) | C10x15.3 | 3.42 | 3.30 | 55.5 | 4.49 | 1.74 | 145.48 | 0.012 |
| T5 | 100-80(445) | C10x15.3 | 3.42 | 3.30 | 55.5 | 4.49 | 2.07 | 145.48 | 0.014 |
| T5 | 100-80 (446) | C10x15.3 | 3.42 | 3.30 | 55.5 | 4.49 | 1.97 | 145.48 | 0.014 |

tnxTower Report - version 8.1.1.0

| Section No. | Elevation | Size | $L$ | $L_{u}$ | KI/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | ft | ft |  | $i n^{2}$ | $K$ | $K$ | $\phi P_{n}$ |
| T5 | 100-80 (449) | C10x15.3 | 3.42 | 3.30 | 55.5 | 4.49 | 2.07 | 145.48 | 0.014 |
| T5 | 100-80 (450) | C10x15.3 | 3.42 | 3.30 | 55.5 | 4.49 | 1.97 | 145.48 | 0.014 |

## Torque-Arm Top Bending Design Data

| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | $\begin{aligned} & \text { Ratio } \\ & M_{u x} \\ & \hline \end{aligned}$ | $M_{u y}$ | $\phi M_{n y}$ | Ratio $M_{u y}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | kip-ft | kip-ft | $\phi M_{n \mathrm{x}}$ | kip-ft | kip-ft | $\phi M_{n y}$ |
| T5 | 100-80 (438) | C10x15.3 | -12 | 42 | 0.276 | 0 | 5 | 0.000 |
| T5 | 100-80 (439) | C10×15.3 | -12 | 42 | 0.274 | 0 | 5 | 0.000 |
| T5 | 100-80 (445) | C10x15.3 | -12 | 42 | 0.275 | 0 | 5 | 0.000 |
| T5 | 100-80 (446) | C10x15.3 | -11 | 42 | 0.274 | 0 | 5 | 0.000 |
| T5 | 100-80 (449) | C10×15.3 | -12 | 42 | 0.275 | 0 | 5 | 0.000 |
| T5 | 100-80 (450) | C10x15.3 | -12 | 42 | 0.275 | 0 | 5 | 0.000 |

## Torque-Arm Top Interaction Design Data

| Section No. | Elevation | Size | Ratio $P_{u}$ | Ratio $M_{u x}$ | Ratio $M_{u y}$ | Comb. Stress Ratio | Allow. Stress Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $\phi P_{n}$ | $\phi M_{n x}$ |  |  |  |  |
| T5 | 100-80 (438) | C10x15.3 | 0.012 | 0.276 | 0.000 | $0.282$ | 1.050 | 4.8 .1 |
| T5 | 100-80 (439) | C10x15.3 | 0.012 | 0.274 | 0.000 | $0.280$ | 1.050 | 4.8.1 |
| T5 | 100-80 (445) | C10x15.3 | 0.014 | 0.275 | 0.000 | $0.282$ | 1.050 | 4.8.1 |
| T5 | 100-80 (446) | C10x15.3 | 0.014 | 0.274 | 0.000 | $0.281$ | 1.050 | 4.8.1 |
| T5 | 100-80 (449) | C10x15.3 | 0.014 | 0.275 | 0.000 | $0.282$ | 1.050 | 4.8.1 |
| T5 | 100-80(450) | C10x15.3 | 0.014 | 0.275 | 0.000 | $0.281$ | 1.050 | 4.8.1 |

## Section Capacity Table

$\left.\begin{array}{ccccccccc}\text { Section } & \begin{array}{c}\text { Elevation } \\ \text { ft }\end{array} & \begin{array}{c}\text { Component } \\ \text { Type }\end{array} & & \text { Size } & \begin{array}{c}\text { Critical } \\ \text { Element }\end{array} & \begin{array}{c}P \\ K\end{array} & \begin{array}{c}\text { oPallow } \\ \text { Ko. }\end{array} & \begin{array}{c}\text { \% } \\ \text { Capacity }\end{array} \\ \text { No. } & \text { Pass } \\ \text { Fail }\end{array}\right]$
tnxTower Report - version 8.1.1.0

| Section No. | $\begin{aligned} & \text { Elevation } \\ & \text { ft } \end{aligned}$ | Component Type | Size | Critical Element | $\begin{aligned} & \hline P \\ & K \end{aligned}$ | $\emptyset P_{\text {allow }}$ | $\begin{gathered} \% \\ \text { Capacity } \end{gathered}$ | $\begin{gathered} \hline \text { Pass } \\ \text { Fail } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T6 | 80-60 | Diagonal | Pipe $1.5^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 316 | -1.57 | 6.52 | 24.2 | Pass |
| T7 | 60-40 | Diagonal | Pipe 1.5" $\times 0.058$ " (16 ga) | 351 | -0.97 | 6.52 | 14.8 | Pass |
| T8 | 40-20 | Diagonal | Pipe 1.5" $\times 0.058$ " (16 ga) | 361 | -0.59 | 6.52 | 9.1 | Pass |
| T9 | 20-4.81771 | Diagonal | Pipe 1.5" $\times 0.058$ " ( 16 ga ) | 397 | -0.83 | 6.52 | $\begin{gathered} 12.8 \\ 13.3 \text { (b) } \end{gathered}$ | Pass |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 \mathrm{e}-007 \end{gathered}$ | Horizontal | L $4 \times 4 \times 1 / 4$ | 421 | 0.67 | 62.86 | 1.1 | Pass |
| T1 | 180-160 | Top Girt | Pipe 1.5" x 0.058" (16 ga) | 4 | 0.04 | 9.93 | $\begin{gathered} 0.4 \\ 0.7 \text { (b) } \end{gathered}$ | Pass |
| T2 | 160-140 | Top Girt | Pipe 1.5" $\times 0.058{ }^{\prime \prime}(16 \mathrm{ga})$ | 62 | 0.46 | 10.43 | 4.4 | Pass |
| T3 | 140-120 | Top Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 118 | -0.35 | 7.33 | $\begin{gathered} 7.4 \text { (b) } \\ 4.8 \\ 5.6 \text { (b) } \end{gathered}$ | Pass |
| T4 | 120-100 | Top Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 176 | 2.42 | 10.43 | $\begin{gathered} 23.2 \\ 38.9 \text { (b) } \end{gathered}$ | Pass |
| T5 | 100-80 | Top Girt | Pipe 1.5" ${ }^{\text {x 0.058" (16 ga) }}$ | 234 | -0.57 | 7.40 | $\begin{gathered} 7.7 \\ 9.2 \text { (b) } \end{gathered}$ | Pass |
| T6 | 80-60 | Top Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 291 | -0.57 | 7.40 | $\begin{gathered} 7.7 \\ 12.2 \text { (b) } \end{gathered}$ | Pass |
| T7 | 60-40 | Top Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 324 | -0.61 | 7.40 | $\begin{gathered} 8.3 \\ 9.9 \text { (b) } \end{gathered}$ | Pass |
| T8 | 40-20 | Top Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 357 | -0.62 | 7.40 | $\begin{gathered} 8.4 \\ 10.0 \text { (b) } \end{gathered}$ | Pass |
| T9 | 20-4.81771 | Top Git | Pipe 1.5" $\times 0.058$ " (16 ga) | 390 | -0.62 | 7.40 | $\begin{gathered} 8.4 \\ 10.0 \text { (b) } \end{gathered}$ | Pass |
| T10 | $\begin{gathered} 4.81771- \\ 3.33333 \mathrm{e}-007 \end{gathered}$ | Top Girt | L $4 \times 4 \times 1 / 4$ | 415 | 6.77 | 62.86 | 10.8 | Pass |
| T1 | 180-160 | Bottorn Girt | Pipe $1.5{ }^{\prime \prime} \times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 7 | 0.42 | 10.43 | $\begin{gathered} 4.0 \\ 6.7 \text { (b) } \end{gathered}$ | Pass |
| T2 | 160-140 | Bottorn Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 65 | -0.31 | 7.33 | $\begin{gathered} 4.2 \\ 5.0(\mathrm{~b}) \end{gathered}$ | Pass |
| T3 | 140-120 | Bottom Girt | Pipe 1.5" $\times 0.058^{\prime \prime}(16 \mathrm{ga})$ | 121 | -0.35 | 7.33 | $\begin{gathered} 4.8 \\ 7.5 \text { (b) } \end{gathered}$ | Pass |
| T4 | 120-100 | Bottom Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 178 | -0.42 | 7.33 | $\begin{gathered} 5.7 \\ 6.8 \text { (b) } \end{gathered}$ | Pass |
| T5 | 100-80 | Bottom Girt | Pipe 1.5" $\times 0.058$ " (16 ga) | 237 | -0.57 | 7.40 | $\begin{array}{r} 7.7 \\ 10.1 \text { (b) } \end{array}$ | Pass |
| T6 | 80-60 | Bottom Girt | Pipe 1.5" ${ }^{\text {x } 0.058 " ~(16 ~ g a) ~}$ | 294 | -0.57 | 7.40 | $\begin{gathered} 7.7 \\ 9.2 \text { (b) } \end{gathered}$ | Pass |
| T7 | 60-40 | Bottom Girt | Pipe 1.5" ${ }^{\text {x } 0.058 " ~(16 ~ g a) ~}$ | 327 | -0.61 | 7.40 | $\begin{gathered} 8.3 \\ 9.9 \text { (b) } \end{gathered}$ | Pass |
| T8 | 40-20 | Bottom Girt | Pipe 1.5" $\times 0.058 \mathrm{Cl}$ (16 ga) | 360 | -0.62 | 7.40 | $\begin{gathered} 8.4 \\ 10.0(b) \end{gathered}$ | Pass |
| T9 | 20-4.81771 | Bottom Girt | Pipe 1.5" $\times 0.058 \mathrm{Cl}$ (16 ga) | 391 | 1.01 | 9.93 | $\begin{gathered} 10.1 \\ 16.2 \text { (b) } \end{gathered}$ | Pass |
| T10 | $\begin{gathered} 4.81771- \\ 3.333330-007 \end{gathered}$ | Bottom Girt | L $4 \times 4 \times 1 / 4$ | 419 | -0.24 | 67.37 | 2.8 | Pass |
| T1 | 180-160 | Guy A@162.523 | $3 / 4$ | 432 | 14.30 | 36.73 | 38.9 | Pass |
| T4 | 120-100 | Guy A@119.385 | 1/2 | 435 | 6.36 | 16.95 | 37.6 | Pass |
| T5 | 100-80 | Guy A@82.5234 | 1/2 | 447 | 6.07 | 16.95 | 35.8 | Pass |
| T1 | 180-160 | Guy B@162.523 | 3/4 | 431 | 14.24 | 36.73 | 38.8 | Pass |
| T4 | 120-100 | Guy B@119.385 | 1/2 | 434 | 6.34 | 16.95 | 37.4 | Pass |
| T5 | 100-80 | Guy B@82.5234 | 1/2 | 443 | 6.03 | 16.95 | 35.6 | Pass |
| T1 | 180-160 | Guy C@162.523 | 3/4 | 427 | 14.40 | 36.73 | 39.2 | Pass |
| T4 | 120-100 | Guy C@119.385 | 1/2 | 433 | 6.38 | 16.95 | 37.6 | Pass |
| T1 | $100-80$ $180-160$ | Guy C@82.5234 <br> Top Guy PullOff@162.523 | 2L $\left.2 \times 2 \times 1 / 4{ }^{1 / 2} 18\right)$ | 437 430 | 6.10 4.34 | 16.95 51.56 | $\begin{gathered} 36.0 \\ 8.4 \\ 12.6 \text { (b) } \end{gathered}$ | Pass |
| T5 | 100-80 | Top Guy PuliOff@82.5234 | $2 \mathrm{~L} 2 \times 2 \times 1 / 4$ (3/8) | 441 | 2.89 | 51.56 | $\begin{gathered} 5.6 \\ 8.4(b) \end{gathered}$ | Pass |
| T5 | 100-80 | Torque Arm Top@82.5234 | C10x15.3 | 449 | 2.07 | 152.75 | 26.9 | Pass |
|  |  |  |  |  |  | Leg (T8) | 58.7 | Pass |
|  |  |  |  |  |  | Diagonal (T5) Horizontal (T10) | 29.9 1.1 | Pass |
|  |  |  |  |  |  | Top Girt (T4) | 38.9 | Pass |

tnxTower Report - version 8.1.1.0

| Section | Elevation | Component Type | Size | Critical Element | P | $\otimes P_{\text {allow }}$ | $\begin{gathered} \% \\ \text { Capacity } \end{gathered}$ | $\begin{gathered} \hline \text { Pass } \\ \text { Fail } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Bottom Girt <br> (T9) | 16.2 | Pass |
|  |  |  |  |  |  | Guy A (T1) | 38.9 | Pass |
|  |  |  |  |  |  | Guy B (T1) | 38.8 | Pass |
|  |  |  |  |  |  | Guy C (T1) | 39.2 | Pass |
|  |  |  |  |  |  | Top Guy Pull-Off (T1) | 12.6 | Pass |
|  |  |  |  |  |  | Torque Arm Top (T5) | 26.9 | Pass |
|  |  |  |  |  |  | Bolt | 38.9 | Pass |
|  |  |  |  |  |  | Checks RATING = | 58.7 | Pass |

## APPENDIX B

## BASE LEVEL DRAWING

## Feed Line Plan



| 180 Ft Guyed Tower Structural Analysis | July 31, 2023 |
| :--- | ---: |
| Project Number 13323-0004.002.8700 | Stafford 1 CDT |

## APPENDIX C

## ADDITIONAL CALCULATIONS


250 E Broad St. Ste 600 - Columbus, OH 43215
Phone $614.221 .6679 \quad$ WWw.pallford.com
Monopole and Tower Foundation Comparison Tool

Apply Capacity Normalization per Section 155
Cormparc Base Shear
Compare Base Axial Compression




## STANDARD CONDITIONS FOR FURNISHING OF PROFESSIONAL ENGINEERING SERVICES ON EXISTING STRUCTURES BY PAUL J. FORD AND COMPANY

1) Paul J . Ford and Company has not made a field inspection to verify the tower member sizes or the antenna/coax loading. If the existing conditions are not as represented on these drawings, we should be contacted immediately to evaluate the significance of the deviation.
2) No allowance was made for any damaged, missing, or rusted members. The analysis of this tower assumes that no physical deterioration has occurred in any of the structural components of the tower and that all the tower members have the same load carrying capacity as the day the tower was erected.
3) It is not possible to have all the detailed information to perform a thorough analysis of every structural subcomponent of an existing tower. The structural analysis by Paul J. Ford and Company verifies the adequacy of the main structural members of the tower. Paul J. Ford and Company provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc.
4) The structural integrity of the existing tower foundation can only be verified if exact foundation sizes and soil conditions are known. Paul J. Ford and Company will not accept any responsibility for the adequacy of the existing foundations unless the foundation sizes and a soils report are provided.
5) This tower has been analyzed according to the minimum design wind loads recommended by the Telecommunications Industry Association Standard ANSI/TIA-222-H. If the owner or local or state agencies require a higher design wind load, Paul J. Ford and Company should be made aware of this requirement.
6) The enclosed sketches are a schematic representation of the tower that we have analyzed. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions and for the proper fit and clearance in the field.
7) Miscellaneous items such as antenna mounts etc. have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

## MasTec Network Solutions

## Structural Analysis \& Design Report

Property Owner N/A<br>Structural Type<br>Site Address<br>Site ID<br>Site Name STAFFORD 4 CT<br>Latitude 41.999581<br>Longitude -72.355636<br>Verizon Wireless<br>Client 118 Flanders Road, 3rd Floor<br>Westborough, MA 01581<br>Site Type MACRO<br>Site ID 617359998<br>Site Name STAFFORD 4 CT<br>Location Code 780563<br>Structural Type Proposed Site Pro 1, P/N: VFA12-HD<br>Nexius Solutions, Inc.<br>Prepared by 1151 SE Cary Parkway, Suite 101 Cary, NC 27518<br>Job/Task Number STAFFORD 4 CT/16999206<br>Email Services@mastec.com<br>Phone 305-599-1800<br>Rev 1<br>Date 08/10/2023<br>Result Pass (53\%)

Dear Sir / Madam:
Mastec is pleased to submit this Report to determine the structural integrity of the equipment platform.
Referenced documents used for this analysis are listed in the section DOCUMENTS \& REFERENCES. This analysis has been performed in compliance with the:

- 2022 Connecticut State Building Code, (2021 IBC w/ State Amendments)
- ANSI/TIA-222-H w/ Addendums, Structural Standard for Antenna Supporting Structures and Antennas and Small Wind Turbine Support Structures

Detailed design parameters are listed in Table 1. Analysis loading is detailed in Table 2.
Based on our analysis we have determined the following result:

## Proposed Sector Mounts Site Pro 1 <br> Adequate (53\%)

P/N: VFA12-HD

Mastec appreciates the opportunity of providing continued engineering services. Should you have any questions, comments or require additional information, please do not hesitate to contact us.

Sincerely,

Analysis Prepared by: Salman Al Jurdi

Analysis Reviewed by: Raphael Mohamed, P.E.
Raphael.Mohamed@mastec.com
CT PE License No. 25112


DOCUMENTS \& REFERENCES
$>$ CD Drawings, Location Code: 780563, Verizon Site Name: STAFFORD 4 CT, by Nexius, dated 08/7/2023.
$>$ Site Visit Photos and Notes, Location Code: 780563, Verizon Site Name: STAFFORD 4 CT, by Nexius, dated 12/12/2022.
$>$ RFDS, Location Code: 780563, Verizon Site Name: STAFFORD 4 CT, by Verizon, dated 7/27/2023.
DESIGN STANDARDS \& PARAMETERS
TABLE 1 STANDARDS \& DESIGN PARAMETERS

| Codes and Standards |  |
| :---: | :---: |
| Building Code | 2022 Connecticut State Building Code <br> (2021 IBC w/ State Amendments) |
| TIA Standard | ANSI/TIA-222-H w/ Addendums |
| Wind Parameters |  |
| Ultimate Wind Speed | 117 mph |
| Nominal Wind Speed with Ice | 50 mph |
| Radial Ice Thickness | 1.5 in |
| Exposure Category | C |
| Structure Class | II |
| Topographic Category | 1 |
| Seismic Design Parameters* |  |
| Ss | 0.174 |
| $\mathrm{S}_{7}$ | 0.055 |

## RESULTS \& RECOMMENDATIONS

Based on our analysis, it is determined that the proposed mounts (Site Pro 1, P/N: VFA12-HD) to be ADEQUATE to support the proposed loading.

## *See construction drawings for proposed mounts.

If the site conditions are different or do not meet requirements, the analysis result would not be valid and Mastec should be notified for re-evaluation.

LOADING

Table 2 - Proposed Antenna Information

| Sector | Mount Elev. ft | Ant. Ctr. Elev. ft | Qty | Description | Mount Type | Status |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| All Sectors | 152.8 | 152.8 | 3 | NHH-65B-R2B | Proposed Site <br> Pro 1, P/N: <br> VFA12-HD | Proposed |
|  |  |  | 3 | NHHSS-65B-R2BT4 |  |  |
|  |  |  | 3 | MT6413-77A w/RRU |  |  |
|  |  |  | 3 | B2/B66A RRH ORAN (RF4439d-25A) |  |  |
|  |  |  | 3 | SAMSUNG (RF4461d-13A) |  |  |
|  |  |  | 1 | 12 OVP |  |  |
|  |  |  | 3 | CBRS RRH - RT4423-48A |  |  |

## ANALYSIS

Risa 3D (Version 17), a commercially available analysis software package, was used to create a threedimensional model of the tower and calculate member stresses for required loading cases. Selected output from the analysis is included in APPENDICES.

## ASSUMPTIONS

1) The existing building structure matches the drawings provided by the building owner and has no damage which may reduce the structural capacity of the building.

This analysis may be affected if any assumptions are not valid or have been made in error. Mastec should be notified to determine the effect on the structural integrity of the existing building.

## Standard Conditions for Providing Structural Consulting Services on Existing Structures

1. Mounting hardware is analyzed to the best of our ability using all information that is provided or can be obtained during fieldwork (if authorized by client). If the existing conditions are not as we have represented in this analysis, we should be contacted to evaluate the significance of the deviation and revise the assessment accordingly.
2. The structural analysis has been performed assuming that the hardware is in "like new" condition. No allowance was made for excessive corrosion, damaged or missing structural members, loose bolts, misaligned parts, or any reduction in strength due to the age or fatigue of the product.
3. The structural analysis provided is an assessment of the primary load carrying capacity of the hardware. We provided a limited scope of service. In some cases, we cannot verify the capacity of every weld, plate, connection detail, etc. In some cases, structural fabrication details are unknown at the time of our analysis, and the detailed field measurement of some of the required details may not be possible. In instances where we cannot perform connection capacity calculations, it is assumed that the existing manufactured connections develop the full capacity of the primary members being connected.
4. We cannot be held responsible for mounting hardware that is installed improperly or hardware that is loose or has a tendency of working loose over the lifetime of the mounting hardware. Our analysis has been performed assuming fully tightened connections, and proper installation and symmetry of the mounting hardware per manufacturer's instructions.
5. The structural analysis has been performed using information currently provided by the client and potentially field verified. We have been provided with a mounting arrangement for all telecommunications equipment, including antennas RRH's, TMA's, RRU's, diplexers, surge protection devices, etc. Our analysis has been based upon a particular mounting arrangement. We are not responsible for deviations in the mounting arrangements that may occur over time. If deviations in equipment type or mounting arrangements are proposed, then we should be contacted to revise the recommendations of this structural report.
6. We cannot be held responsible for temporary and unbalanced loads on mounting hardware. Our analysis is based on a particular mounting arrangement or as-build field condition. We are not responsible for the methods and means of how the mounting arrangement is accomplished by the contractor. These methods and means may include rigging of equipment or hardware to lift and locate, temporary hanging of equipment in locations other than the final arrangement, movement and tie off of tower riggers, personnel, and their equipment, etc.
7. Steel grade and strength is unknown and cannot be field tested. We cannot be held responsible for equipment manufactured from inferior steel or bolts. Our analysis assumes that standard structural grade steel has been used by the equipment manufacturer for all assembled parts of the mounting apparatus. Acceptable steels and connection components are specified by the American Institute of Steel Construction. It is assumed all welded connections are performed in the shop under the latest American
8. Welding Society Code. No field welds are permitted or assumed for the existing pre-manufactured equipment. In case no accurate info available, following material assumptions were used:

| Channel, Solid Round, Angle, Plate | ASTM A36 (GR 36) |
| :--- | :--- |
| HSS (Rectangular) | ASTM 500 (GR B-46) |
| HSS (Round) | ASTM 500 (GR B-42) |
| Pipe | ASTM A53 (GR 35) |
| Connection Bolts | ASTM A325 |
| U-Bolts | SAE 429 Gr.2 |

## Appendix \#1: Loading Parameters and Calculations

## ASCE 7 Hazards Report

Address:
No Address at This Location

Standard: ASCE/SEI 7-16 Latitude: 41.999581
Risk Category: ॥
Soil Class: D-Default (see Elevation: 1074.84 ft (NAVD 88)


## Wind

## Results:

| Wind Speed | 117 Vmph |
| :--- | :--- |
| 10 -year MRI | 75 Vmph |
| 25 -year MRI | 83 Vmph |
| 50 -year MRI | 90 Vmph |
| 100 -year MRI | 97 Vmph |

Data Source:
Date Accessed:

ASCE/SEI 7-16, Fig. 26.5-1B and Figs. CC.2-1-CC. 2-4, and Section 26.5.2
Fri Feb 032023

Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-16 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability = $0.00143, \mathrm{MRI}=700$ years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-16 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Seismic D - Default (see Section 11.4.3)

## Site Soil Class:

Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.174 | $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.088 |
| :--- | :--- | :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.055 | $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.6 | $\mathrm{PGA}:$ | 0.092 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.4 | $\mathrm{PGA}_{\mathrm{M}}:$ | 0.147 |
| $\mathrm{~S}_{\mathrm{MS}}:$ | 0.279 | $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.6 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.132 | $\mathrm{I}_{\mathrm{e}}:$ | 1 |
| $\mathrm{~S}_{\mathrm{DS}}:$ | 0.186 | $\mathrm{C}_{\mathrm{v}}:$ | 0.7 |






Data Accessed:
Fri Feb 032023

## Date Source:

USGS Seismic Design Maps based on ASCE/SEI 7-16 and ASCE/SEI 7-16 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-16 Ch. 21 are available from USGS.

AMEAICAN SOCIETY OF CIVL ENGINEERS

## Ice

## Results:

Ice Thickness: $\quad 1.50 \mathrm{in}$.
Concurrent Temperature: 5 F
Gust Speed

## Data Source:

Date Accessed:

50 mph
Standard ASCE/SEI 7-16, Figs. 10-2 through 10-8
Fri Feb 032023

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 500-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

[^2]
STAFFORD 4 CT.xlsm










Member Code Checks Displayed (Enveloped)
Envelope Only Solution

| Mastec | STAFFORD 4 CT - MKT 68 | BENDING CHECK |
| :---: | :---: | :---: |
| SJ |  | Aug 10, 2023 at 4:01 PM |
| 16999206 |  | STAFFORD 4 CT. 3 sd |





## Hot Rolled Steel Properties

|  | Label | E[ksi] | G [ksi] | Nu | Therm (/1. | Density[k/f*^3] | Yield[ksi] | Ry | Fulksi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A992 | 29000 | 11154 | . 3 | . 65 | . 49 | 50 | 1.1 | 65 | 1.1 |
| 2 | A36 Gr. 36 | 29000 | 11154 | 3 | 65 | 49 | 36 | 1.5 | 58 | 1.2 |
| 3 | A572 Gr. 50 | 29000 | 11154 | 3 | 65 | 49 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr.B RND | 29000 | 11154 | 3 | . 65 | 527 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | . 3 | . 65 | . 527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | . 3 | . 65 | 49 | 35 | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | 3 | . 65 | 49 | 50 | 1.4 | 65 | 1.3 |
| 8 | HR8 | 29000 | 11154 | . 3 | . 65 | 49 | 36 | 1.5 | 58 | 1.2 |

## Hot Rolled Steel Section Sets

| Label |  | Shape | Type | Design List | Material | Design... A [in2] lyy [in4] Izz [in4] J [in4] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | pipe mount | PIPE 2.5 | Column | Pipe | A53 Gr.B | Typical | 1.61 | 1.45 | 1.45 | 2.89 |
| 2 | top rail | PIPE 2.5 | Beam | Pipe | A53 Gr.B | Typical | 1.61 | 1.45 | 1.45 | 2.89 |
| 3 | diagonal bracing | SR 3/4 | Column | BAR | A36 Gr. 36 | Typical | . 442 | . 016 | 016 | . 031 |
| 4 | gusset plate | PL5/8X3.5 | Beam | RECT | A36 Gr. 36 | Typical | 2.188 | . 071 | 2.233 | . 253 |
| 5 | vertical bracina | SR 5/8 HRA | Column | BAR | A36 Gr. 36 | Tvpical | 307 | . 007 | . 007 | 015 |
| 6 | bottom rail | PIPE_2.5 | Beam | Pipe | A53 Gr.B | Typical | 1.61 | 1.45 | 1.45 | 2.89 |
| 7 | tie-back | PIPE 2.0 | Beam | Pipe | A53 Gr.B | Typical | 1.02 | . 627 | . 627 | 1.25 |
| 8 | v-arm | PIPE 2.0 | Beam | Pipe | A53 Gr.B | Typical | 1.02 | . 627 | . 627 | 1.25 |
| 9 | connection plate | PL5/8X8 | Beam | RECT | A36 Gr. 36 | Typical | 5 | . 163 | 26.667 | . 619 |
| 10 | RRU-Pipe | PIPE 2.0 | Column | Pipe | A53 Gr.B | Typical | 1.02 | . 627 | . 627 | 1.25 |

Joint Boundary Conditions

|  | Joint Label | $\mathrm{X}[\mathrm{k} / \mathrm{in}]$ | Y [k/in] | Z [k/in] | X Rot.[k-ft/rad] | Y Rot.[k-ft/rad] | Z Rot.[k-ft/rad] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N12A |  |  |  |  |  |  |
| 2 | N28 |  |  |  |  |  |  |
| 3 | N78 | Reaction | Reaction | Reaction | Reaction |  | Reaction |
| 4 | N79B | Reaction | Reaction | Reaction | Reaction |  | Reaction |
| 5 | N85B | Reaction | Reaction | Reaction | Reaction |  | Reaction |
| 6 | N86B | Reaction | Reaction | Reaction | Reaction |  | Reaction |

## Hot Rolled Steel Design Parameters

|  | Label | Shape | Length[ft] | Lbyy ft ] | Lbzz[ff] | Lcomp top[ft] | comp b | -tor | Kyy | Kzz | Cb | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M54 | bottom rail | 12.5 | 5.083 | 5.083 | 5.083 | 5.083 | 5.083 |  |  |  | Lateral |
| 2 | M6 | top rail | 12.5 | 5.083 | 5.083 | 5.083 | 5.083 | 5.083 |  |  |  | Lateral |
| 3 | M5 | pipe mount | 10 | 3.33 | 3.33 | 3.33 | 3.33 | 3.33 |  |  |  | Lateral |
| 4 | M11 | v -arm | 2.5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 5 | M12 | v-arm | 2.5 |  |  | Lbw |  |  |  |  |  | Lateral |
| 6 | M17 | connection ... | 417 |  |  |  |  |  |  |  |  | Lateral |
| 7 | M12A | gusset plate | 243 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 8 | M13 | gusset plate | 417 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 9 | M14 | gusset plate | 417 |  |  | Lbw |  |  |  |  |  | Lateral |
| 10 | M15A | gusset plate | 243 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 11 | M17A | v -arm | 2.5 |  |  | Lbw |  |  |  |  |  | Lateral |
| 12 | M18 | v -arm | 2.5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 13 | M21 | connection ... | 417 |  |  |  |  |  |  |  |  | Lateral |
| 14 | M22 | gusset plate | 243 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 15 | M23 | gusset plate | 417 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 16 | M24 | gusset plate | 417 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 17 | M25 | gusset plate | 243 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 18 | M34 | diagonal bra. | 3.667 | 3.33 | 3.33 | 3.33 | 3.33 | 3.33 | 7 | 7 |  | Lateral |



Joint Loads and Enforced Displacements (BLC 42 : Man 1 ( 500 lbs ))

| Joint Label |  | L.D.M | Direction | Magnitude[(k,k-ft), (in, rad). (k) $k^{*} s^{\wedge} 2 / f t$. |
| :---: | :---: | :---: | :---: | :---: |
|  |  | , |  |  |
| 2 | N51A | L | Y | -. 5 |


| Joint Label |  | D.M | Direction |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | N51A | L | Y | 0 |
| 2 | N63 | L | Y | -. 5 |

Joint Loads and Enforced Displacements (BLC 44 : Man 3 ( 500 lbs ))

| Joint Labe |  | L.D.M | Direction |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | N63 | L |  |  |
| 2 | N57 |  |  |  |

Joint Loads and Enforced Displacements (BLC 45 : Man 4 (250 (bs))

| 1 Joint Labe |  | L.D.M | Direction | Magnitude[(k,k-fti). (in,rad). (k*s*^2/tt. |
| :---: | :---: | :---: | :---: | :---: |
|  |  | L |  | 0 |
| 2 | N59 | L | Y | . 25 |

Joint Loads and Enforced Displacements (BLC 46 : Man 5 ( 250 lbs ))

| Joint Labe |  | L.D.M | Direction | Magnitudel(k, $k$-ft). (in, rad). $\left(k^{*} s^{\wedge} 2 / 4 \mathrm{t}\right.$. |
| :---: | :---: | :---: | :---: | :---: |
| 1 | N57 | L |  |  |
| 2 | N58 | L | Y | . 25 |


| Joint Label |  | L.D.M | Direction |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |


| M Member Labe |  | Direction | Magnitude[k. - -ft] | Location[ft\%] |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Y | - 044 | \%25 |
| 2 | M50 | Y | -. 025 | \%10 |

Company
Aug 10, 2023
Designer
Job Number
Model Name

Member Point Loads (BLC 1 : Dead) (Continued)

|  | Member Label | Direction | Magnitude[k. $k$-ft] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 3 | M50 | Y | -. 07 | \%25 |
| 4 | M50 | $Y$ | -. 023 | \%50 |
| 5 | M47 | Y | -. 022 | \%10 |
| 6 | M47 | Y | -. 075 | \%25 |
| 7 | M70 | $Y$ | -. 032 | \% 50 |
| 8 | M44 | $Y$ | -. 044 | \%55 |
| 9 | M50 | Y | -. 025 | \%71 |
| 10 | M47 | $Y$ | -. 022 | \%71 |

## Member Point Loads (BLC 2 : Ice Dead)

|  | Member Label | Direction | Magnitude[k. k -ft] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Y | -. 059 | \%25 |
| 2 | M50 | Y | -. 096 | \%10 |
| 3 | M50 | Y | -. 052 | \%25 |
| 4 | M50 | $Y$ | -. 029 | \%50 |
| 5 | M47 | $Y$ | -. 101 | \%10 |
| 6 | M47 | $Y$ | -. 053 | \%25 |
| 7 | M70 | $Y$ | -. 101 | \%50 |
| 8 | M44 | Y | -. 059 | \%55 |
| 9 | M50 | Y | -. 096 | \%71 |
| 10 | M47 | $Y$ | -. 101 | \%71 |

## Member Point Loads (BLC 3 : Full Wind Antenna 10 Deg))

| Member Label |  | Direction Magnitude[k,k-ft] |  | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | $Z$ | -.096 | $\% 25$ |
| 2 | M50 | $Z$ | -.155 | $\% 10$ |
| 3 | M50 | $Z$ | -.046 | $\% 25$ |
| 4 | M50 | $Z$ | -.02 | $\% 50$ |
| 5 | M47 | $Z$ | -.165 | $\% 10$ |
| 6 | M47 | $Z$ | -.051 | $\% 25$ |
| 7 | M70 | $Z$ | -.145 | $\% 50$ |
| 8 | M44 | $Z$ | -.096 | $\% 55$ |
| 9 | M50 | $Z$ | -.155 | $\% 71$ |
| 10 | M47 | $Z$ | -.165 | $\% 71$ |

## Member Point Loads (BLC 4 : Full Wind Antenna (30 Deg))

|  | Member Label | Direction | Magnitude[k.k-ft] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | -. 071 | \%25 |
| 2 | M50 | Z | -. 124 | \%10 |
| 3 | M50 | Z | -. 047 | \%25 |
| 4 | M50 | Z | -. 022 | \%50 |
| 5 | M47 | Z | -. 131 | \%10 |
| 6 | M47 | Z | -. 05 | \%25 |
| 7 | M70 | Z | -. 115 | \%50 |
| 8 | M44 | Z | -. 071 | \%55 |
| 9 | M50 | Z | -. 124 | \%71 |
| 10 | M47 | Z | -. 131 | \%71 |
| 11 | M44 | X | . 041 | \%25 |
| 12 | M50 | X | 072 | \%10 |
| 13 | M50 | X | . 027 | \%25 |
| 14 | M50 | X | . 013 | \%50 |
| 15 | M47 | X | . 076 | \%10 |
| 16 | M47 | X | . 029 | \%25 |
| 17 | M70 | X | . 067 | \%50 |
| 18 | M44 | X | . 041 | \%55 |

Member Point Loads (BLC 4 : Full Wind Antenna (30 Deg)) (Continued)

| Member Labe |  | Direction | Magnitude[ [k, $k$-f] | Location[ft\%] |
| :---: | :---: | :---: | :---: | :---: |
| 19 | M50 | X | . 072 | \%71 |
| 20 | M47 | X | . 076 | \%71 |

## Member Point Loads (BLC 5: Full Wind Antenna ( 60 Deg))

| Member Label |  | Directio | Magnitudelk.k | Locationfti, \% |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | -. 026 | \%25 |
| 2 | M50 | Z | -. 06 | \%10 |
| 3 | M50 | Z | -. 034 | \%25 |
| 4 | M50 | Z | -. 019 | \% 50 |
| 5 | M47 | Z | -. 062 | \%10 |
| 6 | M47 | Z | -. 035 | \% 25 |
| 7 | M70 | Z | -. 055 | \% $\% 5$ |
| 8 | M44 | Z | -. 026 | \%71 |
| 9 | M50 | Z | -. 062 | \%71 |
| 10 | M47 | Z | -. 045 | \%25 |
| 11 | M44 | X | 104 | \%10 |
| $\frac{12}{13}$ | M50 | X | . 06 | \%25 |
| 14 | M50 | X | . 032 | \%50 |
| 15 | M47 | X | 107 | \%10 |
| 16 | M47 | X | . 061 | \%25 |
| 17 | M70 | X | . 095 | \% 50 |
| 18 | M44 | X | . 045 | \% 57 |
| 19 | M50 | X | . 104 | \%71 |
| 20 | M47 | X | . 107 |  |


| Member Label |  | Direction | Magnitude[k, $k$-fti] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | 0 | \%25 |
| 2 | M50 | Z | 0 | \%10 |
| 3 | M50 | Z | O | \%25 |
| 4 | M50 | Z | 0 | \% 50 |
| 5 | M47 | Z | 0 | \%10 |
| 6 | M47 | Z | 0 | \% $\% 5$ |
| 8 | M44 | Z | 0 | \%55 |
| 9 | M50 | Z | 0 | \%71 |
| 10 | M47 | Z | 0 | \%71 |
| 11 | M44 | X | . 038 | \%25 |
| 12 | M50 | X | 108 | \%10 |
| 13 | M50 | X | . 076 | \%25 |
| $\begin{array}{r}14 \\ 15 \\ \hline\end{array}$ | M50 | X | . 043 | \% 10 |
| 15 | M47 | X | . 076 | \%25 |
| 17 | M70 | X | . 098 | \%50 |
| 18 | M44 | X | . 038 | \%55 |
| 19 | M50 | X | 108 | \%71 |
| 20 | M47 | X | 109 | \%71 |

Member Point Loads (BLC 7 : Full Wind Antenna (120 Deg))

| Member Label |  | Direction | Magnitudelk,k-fll] | .026 |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | $Z$ | .06 | $\%$ |
| 2 | M50 | $\mathbf{Z}$ | $\% 10$ |  |
| 3 | M50 | $Z$ | .034 | $\%$ |
| 4 | M50 | $\mathbf{Z}$ | .019 | $\% 50$ |

Company

## Mastec

Aug 10, 2023
Designer
SJ
4:01 PM
Job Number
16999206
STAFFORD 4 CT - MKT 68

## Member Point Loads (BLC 7 : Full Wind Antenna (120 Deg)) (Continued)

|  | Member Label | Direction | Magnitude[k, k -ft] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 5 | M47 | Z | . 062 | \%10 |
| 6 | M47 | Z | 035 | \%25 |
| 7 | M70 | Z | . 055 | \%50 |
| 8 | M44 | Z | . 026 | \%55 |
| 9 | M50 | Z | . 06 | \%71 |
| 10 | M47 | Z | 062 | \%71 |
| 11 | M44 | X | . 045 | \%25 |
| 12 | M50 | X | 104 | \%10 |
| 13 | M50 | X | . 06 | \%25 |
| 14 | M50 | X | 032 | \%50 |
| 15 | M47 | X | 107 | \%10 |
| 16 | M47 | X | . 061 | \%25 |
| 17 | M70 | X | . 095 | \%50 |
| 18 | M44 | X | . 045 | \%55 |
| 19 | M50 | X | 104 | \%71 |
| 20 | M47 | X | 107 | \%71 |

## Member Point Loads (BLC 8 : Full Wind Antenna (150 Deg))

|  | Member Label | Direction | Magnitude [k. k -ft] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | . 071 | \%25 |
| 2 | M50 | Z | . 124 | \%10 |
| 3 | M50 | Z | . 047 | \%25 |
| 4 | M50 | Z | . 022 | \%50 |
| 5 | M47 | Z | 131 | \%10 |
| 6 | M47 | Z | . 05 | \%25 |
| 7 | M70 | Z | . 115 | \%50 |
| 8 | M44 | 7 | . 071 | \%55 |
| 9 | M50 | Z | 124 | \%71 |
| 10 | M47 | Z | . 131 | \%71 |
| 11 | M44 | X | . 041 | \%25 |
| 12 | M50 | X | . 072 | \%10 |
| 13 | M50 | X | . 027 | \%25 |
| 14 | M50 | X | . 013 | \%50 |
| 15 | M47 | X | . 076 | \%10 |
| 16 | M47 | X | . 029 | \%25 |
| 17 | M70 | X | . 067 | \%50 |
| 18 | M44 | X | . 041 | \%55 |
| 19 | M50 | X | . 072 | \%71 |
| 20 | M47 | X | 076 | \%71 |

## Member Point Loads (BLC 15 : Ice Wind Antenna (0 Deg))

|  | Member Label | Direction | Magnitude[k,k-ft] | Location [ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | -. 024 | \%25 |
| 2 | M50 | Z | -. 038 | \%10 |
| 3 | M50 | Z | -. 015 | \%25 |
| 4 | M50 | Z | -. 008 | \%50 |
| 5 | M47 | Z | -. 04 | \%10 |
| 6 | M47 | Z | -. 016 | \%25 |
| 7 | M70 | Z | -. 037 | \%50 |
| 8 | M44 | Z | -. 024 | \%55 |
| 9 | M50 | Z | -. 038 | \%71 |
| 10 | M47 | Z | -. 04 | \%71 |

## Member Point Loads (BLC 16 : Ice Wind Antenna (30 Deg))

Member Point Loads (BLC 16 : Ice Wind Antenna (30 Deg)) (Continued)

|  | Member Label | Direction | Magnitude[k.k-ft] | Location [ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | -. 018 | \%25 |
| 2 | M50 | Z | -. 031 | \%10 |
| 3 | M50 | Z | -. 014 | \%25 |
| 4 | M50 | Z | -. 008 | \% 50 |
| 5 | M47 | Z | -. 032 | \%10 |
| 6 | M47 | Z | -. 015 | \%25 |
| 7 | M70 | Z | -. 03 | \%50 |
| 8 | M44 | Z | -. 018 | \%55 |
| 9 | M50 | Z | -. 031 | \%71 |
| 10 | M47 | Z | -. 032 | \%71 |
| 11 | M44 | X | . 01 | \%25 |
| 12 | M50 | X | 018 | \%10 |
| 13 | M50 | X | . 008 | \%25 |
| 14 | M50 | X | . 005 | \%10 |
| 16 | M47 | X | . 017 | \%50 |
| 18 | M 44 | X | . 01 | \%55 |
| 19 | M50 | X | . 018 | \%71 |
| 20 | M47 | X | 018 | \%71 |

Member Point Loads (BLC 17 : Ice Wind Antenna ( 60 Deg))

| Member Label |  | Direction | Magnitude[k. k -ft] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | -. 007 | \%25 |
| 2 | M50 | Z | -. 016 | \%10 |
| 3 | M50 | Z | -. 01 | \%25 |
| 4 | M50 | Z | -. 006 | \%50 |
| 5 | M47 | Z | -. 016 | \%10 |
| 6 | M47 | Z | -. 01 | \%25 |
| 7 | M70 | Z | -. 015 | \% 50 |
| 8 | M44 | Z | -. 007 | \%55 |
| $\frac{9}{10}$ | M50 | Z | -. 016 | \%71 |
| 13 | M50 | X | . 017 | \%25 |
| 14 | M50 | X | . 011 | \% 50 |
| 15 | M47 | X | . 028 | \%10 |
| 16 | M47 | X | . 017 | \%25 |
| 17 | M70 | X | . 025 | \%50 |
| 18 | M44 | X | . 013 | \%55 |
| 19 | M50 | X | . 027 | \%71 |
| 20 | M47 | X | . 028 | \%71 |

Member Point Loads (BLC 18 : Ice Wind Antenna (90 Deg))

| Member Labe |  | Direction | Magnitude[ $k, k$ - ft$]$ | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | 0 | \%25 |
| 2 | M50 | Z | 0 | \%10 |
| 3 | M50 | Z | 0 | \%25 |
| 4 | M50 | Z | 0 | \%50 |
| 5 | M47 | Z | 0 | \%10 |
| 6 | M47 | Z | 0 | \%25 |
| 7 | M70 | Z | 0 | \%50 |
| 8 | M44 | Z | 0 | \%55 |
| 9 | M50 | Z | 0 | \%71 |
| 10 | M47 | Z | 0 | \%71 |

Company
Mastec
Aug 10, 2023
Designer
Job Number
16999206
STAFFORD 4 CT - MKT 68

Member Point Loads (BLC 18 : Ice Wind Antenna (90 Deg))(Continued)

|  | Member Label | Direction | Magnitude[k.k-ff] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 11 | M44 | X | . 012 | \%25 |
| 12 | M50 | X | . 029 | \%10 |
| 13 | M50 | X | 021 | \%25 |
| 14 | M50 | X | 014 | \%50 |
| 15 | M47 | X | . 029 | \%10 |
| 16 | M47 | X | . 021 | \%25 |
| 17 | M70 | X | . 027 | \%50 |
| 18 | M44 | X | . 012 | \%55 |
| 19 | M50 | X | . 029 | \%71 |
| 20 | M47 | X | . 029 | \%71 |

## Member Point Loads (BLC 19 : Ice Wind Antenna (120 Deg))

|  | Member Label | Direction | Magnitudelk. k -ft] | Location[ft \%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | . 007 | \%25 |
| 2 | M50 | Z | . 016 | \%10 |
| 3 | M50 | Z | . 01 | \%25 |
| 4 | M50 | Z | . 006 | \% 50 |
| 5 | M47 | Z | . 016 | \%10 |
| 6 | M47 | Z | . 01 | \%25 |
| 7 | M70 | Z | 015 | \%50 |
| 8 | M44 | Z | . 007 | \%55 |
| 9 | M50 | Z | . 016 | \%71 |
| 10 | M47 | Z | 016 | \%71 |
| 11 | M44 | X | 013 | \%25 |
| 12 | M50 | X | . 027 | \%10 |
| 13 | M50 | X | . 017 | \%25 |
| 14 | M50 | X | 011 | \%50 |
| 15 | M47 | X | . 028 | \%10 |
| 16 | M47 | X | . 017 | \%25 |
| 17 | M70 | X | . 025 | \%50 |
| 18 | M44 | X | . 013 | \%55 |
| 19 | M50 | X | . 027 | \%71 |
| 20 | M47 | X | . 028 | \%71 |

Member Point Loads (BLC 20 : Ice Wind Antenna (150 Deg))

|  | Member Label | Direction | Magnitude[k.k-ff] | Location[ft.\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M44 | Z | . 018 | \%25 |
| 2 | M50 | Z | 016 | \%10 |
| 3 | M50 | Z | . 01 | \%25 |
| 4 | M50 | Z | . 006 | \%50 |
| 5 | M47 | Z | 016 | \%10 |
| 6 | M47 | Z | . 01 | \%25 |
| 7 | M70 | Z | . 015 | \%50 |
| 8 | M44 | Z | 018 | \%55 |
| 9 | M50 | Z | 016 | \%71 |
| 10 | M47 | Z | . 016 | \%71 |
| 11 | M44 | X | . 01 | \%25 |
| 12 | M50 | X | . 027 | \%10 |
| 13 | M50 | X | . 017 | \%25 |
| 14 | M50 | X | 011 | \%50 |
| 15 | M47 | X | 028 | \%10 |
| 16 | M47 | X | 017 | \%25 |
| 17 | M70 | X | . 025 | \%50 |
| 18 | M44 | X | . 01 | \%55 |
| 19 | M50 | X | 027 | \%71 |
| 20 | M47 | X | . 028 | \%71 |

Member Point Loads (BLC 27: Seismic Antenna (O Dea))

|  | Mirection | Magnitude $[k, k-f t]$ | Location[ft, \%] |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Member Label | $Z$ | -.008 | $\%$ |
| 2 | M44 | $Z$ | -.005 | $\% 40$ |
| 3 | M50 | $Z$ | -.007 | $\% 25$ |
| 4 | M50 | $Z$ | -.002 | $\%$ |
| 5 | M50 | $Z$ | -.004 | $\%$ |
| 6 | M47 | $Z$ | -.007 | $\% 25$ |
| 7 | M47 | $Z$ | -.003 | $\% 50$ |




| Member Point Loads (BLC 47: Man 6 (250 lbs)) |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Label |  |  |  |  | Direction | Magnitude[k.k-ft] | Location $[f t, \%$ ] |
| 1 |  |  |  |  |  |  |  |


| Member Area Loads |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Joint A | Joint B | Joint $C$ | Joint $D$ | Direction | Distribution | Magnitudelksfl |
|  |  | No Data to Print ... |  |  |  |  |


| BLC Description |  | Category | $X$ Gravity | Grav | Z Gravity | Joint | Point | Distribut. | ArealMe. | Surfacel... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Dead | None |  | -1 |  |  | 10 |  |  |  |
| 2 | Ice Dead | None |  |  |  |  | 10 | 67 |  |  |
| 3 | Full Wind Antenna (0 Deg) | None |  |  |  |  | 10 |  |  |  |
| 4 | Full Wind Antenna (30 Deg) | None |  |  |  |  | 20 |  |  |  |
| 5 | Full Wind Antenna (60 Deq) | None |  |  |  |  | 20 |  |  |  |
| 6 | Full Wind Antenna (90 Deg) | None |  |  |  |  | 20 |  |  |  |
| 7 | Full Wind Antenna (120 Deq) | None |  |  |  |  | 20 |  |  |  |
| 8 | Full Wind Antenna (150 Deg) | None |  |  |  |  | 20 |  |  |  |
| 9 | Full Wind Members (0 Deq) | None |  |  |  |  |  | 74 |  |  |
| 10 | Full Wind Members (30 Deg) | None |  |  |  |  |  | 74 |  |  |
| 11 | Full Wind Members (60 Deq) | None |  |  |  |  |  | 74 |  |  |
| 12 | Full Wind Members (90 Deg) | None |  |  |  |  |  | 74 |  |  |
| 13 | Full Wind Members (120 Deq) | None |  |  |  |  |  | 74 |  |  |
| 14 | Full Wind Members (150 Deg) | None |  |  |  |  |  | 74 |  |  |

Company
Designer
Job Number
Model Name

Basic Load Cases (Continued)

|  | BLC Description | Category | $X$ Gravity | Y Gravity | z Gravity | Joint | Point | Distribut. | Area(Me. | Surface |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | Ice Wind Antenna (0 Deq) | None |  |  |  |  | 10 |  |  |  |
| 16 | Ice Wind Antenna (30 Deg) | None |  |  |  |  | 20 |  |  |  |
| 17 | Ice Wind Antenna (60 Deq) | None |  |  |  |  | 20 |  |  |  |
| 18 | Ice Wind Antenna (90 Deg) | None |  |  |  |  | 20 |  |  |  |
| 19 | Ice Wind Antenna (120 Deq) | None |  |  |  |  | 20 |  |  |  |
| 20 | Ice Wind Antenna (150 Deg) | None |  |  |  |  | 20 |  |  |  |
| 21 | Ice Wind Members (0 Dea) | None |  |  |  |  |  | 138 |  |  |
| 22 | Ice Wind Members ( 30 Deg ) | None |  |  |  |  |  | 138 |  |  |
| 23 | lce Wind Members ( 60 Deq ) | None |  |  |  |  |  | 138 |  |  |
| 24 | Ice Wind Members (90 Deg) | None |  |  |  |  |  | 138 |  |  |
| 25 | Ice Wind Members (120 Deq) | None |  |  |  |  |  | 138 |  |  |
| 26 | Ice Wind Members (150 Deg) | None |  |  |  |  |  | 138 |  |  |
| 27 | Seismic Antenna (0 Deq) | None |  |  |  |  | 7 |  |  |  |
| 28 | Seismic Antenna (90 Deg) | None |  |  |  |  | 7 |  |  |  |
| 29 | Seismic Members (0 Dea) | None |  | -. 037 | -. 093 |  |  |  |  |  |
| 30 | Seismic Members ( 30 Deg ) | None | 046 | -. 037 | -. 081 |  |  |  |  |  |
| 31 | Seismic Members ( 60 Deq ) | None | . 081 | -. 037 | -. 046 |  |  |  |  |  |
| 32 | Seismic Members (90 Deg) | None | . 093 | -. 037 |  |  |  |  |  |  |
| 33 | Seismic Members (120 Deg) | None | 081 | -. 037 | 046 |  |  |  |  |  |
| 34 | Seismic Members (150 Deg) | None | . 046 | -. 037 | 081 |  |  |  |  |  |
| 35 | Seismic Members (180 Deq) | None |  | -. 037 | . 093 |  |  |  |  |  |
| 36 | Seismic Members (210 Deg) | None | -. 046 | -. 037 | . 081 |  |  |  |  |  |
| 37 | Seismic Members (240 Deq) | None | -. 081 | -. 037 | . 046 |  |  |  |  |  |
| 38 | Seismic Members (270 Deg) | None | -. 093 | -. 037 |  |  |  |  |  |  |
| 39 | Seismic Members (300 Deq) | None | -. 081 | -. 037 | -. 046 |  |  |  |  |  |
| 40 | Seismic Members (330 Deg) | None | -. 046 | -. 037 | -. 081 |  |  |  |  |  |
| 41 | Seismic Vertical Antennas | None |  |  |  |  | 7 |  |  |  |
| 42 | Man 1 ( 500 lbs ) | None |  |  |  | 2 |  |  |  |  |
| 43 | Man 2 ( 500 lbs ) | None |  |  |  | 2 |  |  |  |  |
| 44 | Man 3 ( 500 lbs ) | None |  |  |  | 2 |  |  |  |  |
| 45 | Man $4(250 \mathrm{lbs})$ | None |  |  |  | 2 |  |  |  |  |
| 46 | Man 5 (250 lbs) | None |  |  |  | 2 |  |  |  |  |
| 47 | Man 6 ( 250 lbs ) | None |  |  |  | 1 | 1 |  |  |  |

## Load Combinations

|  |  |  |  |  |  |  |  |  |  |  |  |  | ac. | BLCF | Fac. | BLCF | Fac. | BLCF | Fac. | BLCF | Fac.. ${ }^{\text {B }}$ | BLCFac. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.4D | Yes | Y | 1 | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 0^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 3 | 1 | 9 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 30^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 4 | 1 | 10 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 60^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 5 | 1 | 11 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 90^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 6 | 1 | 12 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 120^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 7 | 1 | 13 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 150^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 8 | 1 | 14 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 180^{\circ}$ | Yes | Y | 1 | 1.2 | 3 | -1 | 9 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 210^{\circ}$ | Yes | Y | 1 | 1.2 | 4 | -1 | 10 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 240^{\circ}$ | Yes | Y | 1 | 1.2 | 5 | -1 | 11 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 270^{\circ}$ | Yes | Y | 1 | 1.2 | 6 | -1 | 12 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | $1.2 \mathrm{D}+1.0 \mathrm{~W} 300^{\circ}$ | Yes | Y | 1 | 1.2 | 7 | -1 | 13 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | 1.2D + 1.0W $330^{\circ}$ | Yes | Y | 1 | 1.2 | 8 | -1 | 14 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14 | 1.2D + 1.0Di + 1.0Wi $0^{\circ}$ | Yes | Y | 1 | 1.2 | 2 | 1 | 15 | 1 | 21 | 1 |  |  |  |  |  |  |  |  |  |  |  |
| 15 | 1.2D + 1.0Di + 1.0Wi 3 .. | Yes | Y | 1 | 1.2 | 2 | 1 | 16 | 1 | 22 | 1 |  |  |  |  |  |  |  |  |  |  |  |
| 16 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 6 .$. | Yes | $Y$ | 1 | 1.2 | 2 | 1 | 17 | 1 | 23 | 1 |  |  |  |  |  |  |  |  |  |  |  |
| 17 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 9 .$. | Yes | Y | 1 | 1.2 | 2 | 1 | 18 | 1 | 24 | 1 |  |  |  |  |  |  |  |  |  |  |  |
| 18 | 1.2D + 1.0Di + 1.0Wi 1.. | Yes, | Y | 1 | 1.2 | 2 | 1 | 19 | 1 | 25 | 1 |  |  |  |  |  |  |  |  |  |  |  |
| 19 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 1 .$. | Yes, | Y | 1 | 1.2 | 2 | 1 | 20 | 1 | 26 | 1 |  |  |  |  |  |  |  |  |  |  |  |

## Load Combinations (Continued)

| Description |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 1.2D + 1.0Di + 1.0Wi 1.. | Yes | $Y$ | 1 | 1.2 | 2 | 1 | 15 | -1 | 21 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 2 .$. | Yes | $Y$ | 1 | 1.2 | 2 | 1 | 16 | -1 | 22 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 2$.. | Yes | $Y$ | 1 | 1.2 | 2 | 1 | 17 | -1 | 23 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 23 | 1.2D + 1.0Di + 1.0Wi 2 . | Yes | $Y$ | 1 | 1.2 | 2 | 1 | 18 | -1 | 24 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | 1.2D + 1.0Di + 1.0Wi 3.. | Yes | $Y$ | 1 | 1.2 | 2 | 1 | 19 | -1 | 25 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 3 .$. | Yes | $Y$ | 1 | 1.2 | 2 | 1 | 20 | -1 | 26 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ - $1+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 3 | . 068 | 9 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \quad 1+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 4 | . 068 | 10 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 1+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 5 | . 068 | 11 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 29 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$-1+1.0... | Yes | $Y$ | 1 | 1.2 | 6 | . 068 | 12 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$-1+1.0... | Yes | $Y$ | 1 | 1.2 | 7 | . 068 | 13 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $1+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 8 | . 068 | 14 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 32 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ - $1+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 3 | - 068 | 9 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 33 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $1+1.0 . .$. | Yes | $Y$ | 1 | 1.2 | 4 | - 068 | 10 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 34 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $1+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 5 | . 068 | 11 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 1+1.0 . .$. | Yes | $Y$ | 1 | 1.2 | 6 | -. 068 | 12 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 36 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ - $1+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 7 | - 068 | 13 | . 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 37 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _1+1.0... | Yes | $Y$ | 1 | 1.2 | 8 | -. 068 | 14 | - 068 | 42 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 38 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0$.. | Yes | $Y$ | 1 | 1.2 | 3 | . 068 | 9 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 39 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0 .$. | Yes | $Y$ | 1 | 1.2 | 4 | . 068 | 10 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 5 | . 068 | 11 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 41 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 6 | . 068 | 12 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 42 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 7 | . 068 | 13 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 43 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ 2 $2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 8 | . 068 | 14 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 44 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 3 | - 068 | 9 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 4 | -. 068 | 10 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 46 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 5 | . 068 | 11 | - 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 47 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 6 | -. 068 | 12 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 48 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 7 | -. 068 | 13 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 49 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 2+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 8 | -. 068 | 14 | . 068 | 43 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 50 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 3 | . 068 | 9 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 51. | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 4 | . 068 | 10 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 52 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 5 | . 068 | 11 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 53 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 6 | . 068 | 12 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 54 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 7 | . 068 | 13 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 55 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 8 | . 068 | 14 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 56 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 3 | -. 068 | 9 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 57 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 4 | -. 068 | 10 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 58 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 5 | -. 068 | 11 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 59 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 6 | -. 068 | 12 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 60 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} 3+1.0 \ldots$ | Yes | $Y$ | 1 | 1.2 | 7 | -. 068 | 13 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 61 | 1.2D + 1.5Lm_3+1.0... | Yes | $Y$ | 1 | 1.2 | 8 | -. 068 | 14 | . 068 | 44 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 62 | 1.2D + 1.5Lv $10^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 63 | 1.2D + 1.5LV $130^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 64 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 160^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 65 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 190^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 66 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ _ $1120^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 67 | 1.2D + 1.5Lv $1150^{\circ}$ | Yes | Y | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 68 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ - $1180^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 69 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ _ $1210^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}-1240^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 71 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ _ $1270^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 72 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ _ $1300^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7.3 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}$ _ $1330^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 45 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 74 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 20^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 75 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 230^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 76 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 260^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 46 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Company
Mastec
Designer

## Load Combinations (Continued)

Description
So..P... S... BLCFac. BLCFac.. BLCFac...BLCFac.. BLCFac...BLCFac.. BLCFac.. BLCFac., BLCFac, BLCFac..

| 77 |
| :--- |
| 78 |
| 79 |




| 79 | $1.2 \mathrm{D}+1.5 \mathrm{LV}$ _2 $150^{\circ}$ | Yes Y |  | 1 | 1.2 | 46 | 1.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 80 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 2$ | $180^{\circ}$ | Yes | Y |  | 1 | 1.2 |


| 81 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} \_2$ | $210^{\circ}$ | Yes | $Y$ |  | 1 | 1.2 | 46 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| 83 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} \_2$ | $270^{\circ}$ | Yes | Y |  | 1 | 1.2 | 46 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| 85 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 2330^{\circ}$ | Yes | Y |  | 1 | 1.2 | 46 | 1.5 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 86 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 30^{\circ}$ | Yes | Y |  | 1 | 1.2 | 47 | 1.5 |
| 87 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 3$ | $30^{\circ}$ | Yes | Y |  | 1 | 1.2 | 47 |



| 90 | $1.20+1.5 L \mathrm{LV} 3120^{\circ}$ | Y | 1 | 1.2 | 47 | 1.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 91 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}=3150^{\circ}$ | Yes Y | 1 | 1.2 | 47 | 1.5 |
| 92 | $1.2 \mathrm{D}+1.5 \mathrm{LV}$ - $3180^{\circ}$ | Yes | 1 | 1.2 | 47 | 1.5 |


| 93 | $1.2 \mathrm{D}+1.5 \mathrm{Lv}-3210^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 94 | $1.2 \mathrm{D}+1.5 \mathrm{LV}$ 3 $240^{\circ}$ | Yes | $Y$ | 1 | 1.2 | 47 | 1.5 |


| 95 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} \_3270^{\circ}$ | Yes | Y |  | 1 | 1.2 | 47 | 1.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 96 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 3300^{\circ}$ | Yes | Y |  | 1 | 1.2 | 47 | 1.5 |
| 97 | $1.2 \mathrm{D}+1.5 \mathrm{LV} 3330^{\circ}$ | Yes | Y | 1 | 1.2 | 47 | 1.5 |  |


| 98 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | Y | 1 | 1.2 | 27 | 1 | 28 |  | 29 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 99 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | Y | 1 | 12 | 27 | . 866 | 28 | 5 | 30 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 100 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | Y | 1 | 1.2 | 27 | 5 | 28 | . 866 | 31 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 101 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | Y | 1 | 1.2 | 27 |  | 28 | 1 | 32 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 102 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | $Y$ | 1 | 1.2 | 27 | -. 5 | 28 | . 866 | 33 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 103 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | $Y$ | 1 | 1.2 | 27 | . 866 | 28 | 5 | 34 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 104 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | Y | 1 | 1.2 | 27 | -1 | 28 |  | 35 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 105 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | Y | 1 | 1.2 | 27 | . 866 | 28 | -. 5 | 36 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 106 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$ | Yes | Y | 1 | 1.2 | 27 | $-.5$ | 28 | . 866 | 37 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 107 | 1.2D +1.0EV +1.0 EH . | Yes | Y | 1 | 1.2 | 27 |  | 28 | -1 | 38 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 108 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | Y | 1 | 1.2 | 27 | 5 | 28 | . 866 | 39 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |
| 109 | $1.2 \mathrm{D}+1.0 \mathrm{EV}+1.0 \mathrm{EH}$. | Yes | Y | 1 | 1.2 | 27 | . 866 | 28 | -. 5 | 40 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |  |

## Envelope Joint Reactions

| Joint |  |  | $X[k]$ | LC | $\mathrm{Y}[\mathrm{k}]$ | LC | Z [k] | LC | MX [k-ft] | LC | MY [k-ft] | LC | MZ [k-ft] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N78 | max | 1.142 | 11 | 1.157 | 17 | 752 | 13 | -. 535 | 7 | 0 | 109 | . 212 | 30 |
| 2 |  | min | -1.547 | 29 | 512 | 11 | -2.155 | 7 | -1.209 | 14 | 0 | 1 | -. 061 | 74 |
| 3 | N79B | max | 1.506 | 35 | 1.148 | 23 | 1.917 | 25 | -. 554 | 6 | 0 | 109 | 251 | 29 |
| 4 |  | min | -. 561 | 5 | . 513 | 6 | -. 25 | 6 | -1.241 | 23 | 0 | 1 | -. 076 | 74 |
| 5 | N85B | max | . 294 | 5 | . 061 | 23 | 1.136 | 5 | -. 021 | 85 | 0 | 109 | 118 | 28 |
| 6 |  | min | -. 275 | 11 | . 016 | 5 | -1.078 | 11 | -. 098 | 17 | 0 | 1 | . 008 | 74 |
| 7 | N86B | max | 2 | 5 | . 06 | 19 | . 807 | 5 | -. 021 | 85 | 0 | 109 | . 12 | 29 |
| 8 |  | min | -. 216 | 11 | 017 | 74 | -. 869 | 11 | -. 097 | 17 | 0 | 1 | 008 | 74 |
| 9 | Totals: | max | 1.562 | 11 | 2.407 | 17 | 1.865 | 2 |  |  |  |  |  |  |
| 10 |  | min | -1.562 | 5 | 1.102 | 11 | -1.865 | 8 |  |  |  |  |  |  |

## Envelope AISC 15th(360-16): LRFD Steel Code Checks

| Member |  | Shape | Code C... Loc[ff] LC Sh |  |  |  |  | ir LC phi*Pnc [k] |  | $\frac{\text { phi*Pnt [k] }}{50.715}$ | **Mn y - ...phi*Mnz- |  | Cb Eqn |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M54 | PIPE 2.5 | . 239 | 8.854 | 36 | . 071 | $8.724$ |  |  | 3.596 | 3.596 | 1 | H1-1b |
| 2 | M6 | PIPE 2.5 | 282 | 8.854 | 6 | . 094 | 3.776 | 2 | 41.05 |  | 50.715 | 3.596 | 3.596 | 1 | H1-1b |
| 3 | M5 | PIPE 2.5 | 126 | 6.667 | 85 | 025 | 3.333 | 85 | 46.315 | 50.715 | 3.596 | 3.596 | 1 | H1-1b |
| 4 | M11 | PIPE 2.0 | . 227 | . 052 | 5 | 054 | . 99 | 18 | 29.81 | 32.13 | 1.872 | 1.872 | 1... | H1-1b |
| 5 | M12 | PIPE_2.0 | . 152 | 234 | 29 | 068 | 2.448 | 31 | 29.81 | 32.13 | 1.872 | 1.872 | 2. | H1-1b |


| Member |  |  | Code C... Loclft] LC Shear |  |  |  | Loc[ft] | Dir LC phi*Pnc [k] |  |  | phi*Pnt [k] phi*Mn V - |  | $\frac{\text { phi*Mn } 2 . . .}{27}$ | Cb | Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | M17 | PL5/8X8 | . 253 | . 417 | 17 | . 181 |  |  |  |  | H1-1b |  |  |
| 7 | M12A | PL5/8X3.5 | 000 | 243 | 14 | . 000 | 0 | z | 25 | 69.904 |  |  | 70.875 | 923 | 5.168 | 1 | H1-1b |
| 8 | M13 | PL5/8X3.5 | 045 | 247 | 11 | . 017 | 247 | V | 7 | 68.066 | 70.875 | 923 | 5.168 | 2. | H1-1b |
| 9 | M14 | PL5/8X3.5 | . 058 | 247 | 29 | . 025 | 247 | v | 30 | 68.067 | 70.875 | 923 | 5.168 | $2 .$. | H1-1b |
| 10 | M15A | PL5/8X3.5 | 000 | 243 | 20 | . 000 | 0 | z | 25 | 69.904 | 70.875 | 923 | 5.168 | 1 | H1-1b |
| 11 | M17A | PIPE 2.0 | 182 | 052 | 35 | . 055 | . 99 |  | 24 | 29.81 | 32.13 | 1.872 | 1.872 | 2 | H1-1b |
| 12 | M18 | PIPE 2.0 | 152 | 234 | 35 | . 068 | 2.448 |  | 29 | 29.81 | 32.13 | 1.872 | 1.872 | 2 | H1-1b |
| 13 | M21 | PL5/8X8 | 249 | 417 | 23 | . 178 | 0 | $v$ | 28 | 155.571 | 162 | 2.109 | 27 | 1. | H1-1b |
| 14 | M22 | PL5/8X3.5 | 000 | 243 | 35 | . 000 | 051 | v | 12 | 69.904 | 70.875 | 923 | 5.168 | 2. | H1-1b |
| 15 | M23 | PL5/8X3.5 | . 038 | 247 | 12 | 013 | 247 | $v$ | 12 | 68.066 | 70.875 | 923 | 5.168 | 2 | H1-1b |
| 16 | M24 | PL5/8X3.5 | 057 | 247 | 35 | . 025 | 247 | $\checkmark$ | 29 | 68.067 | 70.875 | 923 | 5.168 | 2 | H1-1b |
| 17 | M25 | PL5/8X3.5 | 000 | 051 | 35 | . 000 | 0 | z | 16 | 69.904 | 70.875 | 923 | 5.168 | $2 .$. | H1-1b |
| 18 | M34 | SR 3/4 | 054 | 0 | 58 | . 011 | 3.667 |  | 29 | 4.484 | 14.314 | 179 | 179 | 1 | H1-1 ${ }^{\text {* }}$ |
| 19 | M35 | SR 3/4 | 000 | 0 | 09 | 011 | 0 |  | 35 | 4.484 | 14.314 | 179 | 179 | 1 | H1-1a |
| 20 | M36 | SR 3/4 | 086 | 3.667 | 29 | . 019 | 3.667 |  | 5 | 4.484 | 14.314 | 179 | 179 | 1 | $\mathrm{H}^{1-1} \mathrm{~b}^{*}$ |
| 21 | M37 | SR 3/4 | 000 | 0 | 109 | . 015 | 0 |  | 11 | 4.484 | 14.314 | 179 | 179 | 1 | H1-1a |
| 22 | M44 | PIPE 2.5 | 219 | 6.667 | 34 | . 037 | 3.333 |  | 26 | 46.315 | 50.715 | 3.596 | 3.596 | 1 | H1-1b |
| 23 | M47 | PIPE 2.5 | 133 | 3.333 | 8 | . 033 | 6.667 |  | 28 | 46.315 | 50.715 | 3.596 | 3.596 | 1 | H1-1b |
| 24 | M50 | PIPE_2.5 | 124 | 3.333 | 8 | . 022 | 3.333 |  | 7 | 46.315 | 50.715 | 3.596 | 3.596 | 1 | H1-1b |
| 25 | M59 | SR 5/8_HRA | 056 | 0 | 23 | 026 | 0 |  | 29 | 3.122 | 9.94 | 104 | 104 | 2 | H1-1b |
| 26 | M60 | SR 5/8_HRA | 097 | 2.771 | 3 | . 004 | 0 |  | 28 | 3.122 | 9.94 | 104 | 104 | 2 | H1-1b* |
| 27 | M61 | SR 5/8_HRA | 090 | 2.771 | 2 | . 002 | 0 |  | 2 | 3.122 | 9.94 | 104 | 104 | 2 | H1-1b* |
| 28 | M62 | SR 5/8_HRA | 109 | 2.771 | 35 | . 023 | 0 |  | 29 | 3.122 | 9.94 | 104 | 104 | 2 | H1-1b |
| 29 | M65A | PL5/8X3.5 | 263 | 5 | 58 | . 029 | 5 | $v$ | 9 | 66.866 | 70.875 | 923 | 5.168 | 1 | H1-1b |
| 30 | M66A | PL5/8X3.5 | 530 | 0 | 29 | . 066 | 0 | v | 6 | 66.866 | 70.875 | 923 | 5.168 | 1. | H1-1b |
| 31 | M63A | PL5/8X3.5 | 257 | 5 | 51 | . 027 | 5 | $v$ | 50 | 66.866 | 70.875 | 923 | 5.168 | 1 | H1-1b |
| 32 | M64A | PL5/8X3.5 | . 524 | 0 | 35 | . 064 | 0 | $v$ | 35 | 66.866 | 70.875 | 923 | 5.168 | 1. | H1-1b |
| 33 | M66C | PIPE 2.0 | 072 | 6.582 | 17 | . 059 | 6.582 |  | 28 | 19.112 | 32.13 | 1.872 | 1.872 | 2. | H1-1b |
| 34 | M67A | PIPE 2.0 | 066 | 6.582 | 17 | . 060 | 6.582 |  | 29 | 19.112 | 32.13 | 1.872 | 1.872 | 2 | H1-1b |
| 35 | M70 | PIPE 2.0 | 048 | 2.5 | 8 | 015 | 1.25 |  | 8 | 23.809 | 32.13 | 1.872 | 1.872 | 1. | H1-1b |

## verizon ${ }^{\vee}$

## SITE NAME: STAFFORD 4 CT SITE ID: 617359998 169 HAMPDEN ROAD STAFFORD, CT 06076




PROUECT SUMMARY









$x^{2}$

9. NTTM (3) PRocoses susum
B. NTTNL (3) Propocese Suscmic cmis rey (rT423-4a)



 12 mstuu new vivin mer



| PROMECT INFORMATION |  |
| :---: | :---: |
| ste | Swrome 4 |
| SIE D : | a17ssom |
| Stie nomess |  |
| npucw: |  |
| comint resome | MCHAE HUMPHREMS (CONSTRUCTON MNUCER) (560) 560-8410 |
| smaxer of recome | Covir ixilivilicin CARIO F. CENTORE, PE |
| sfre comennure | LATIURE: $41^{\circ} 50^{\circ} 58.40^{\circ}$ <br>  <br>  |


| 8HEET NDEX |  |  |
| :---: | :---: | :---: |
| suter . . | orsamprom | Rex. |
| ${ }^{T-1}$ | mes stur | 4 |
|  |  | , |
|  |  |  |
| c-1 |  | 4 |
| c-2 |  | 4 |
| c-s | Tmack bummer demis | 4 |
| c-4 | trick Exumer deme | 4 |
| c-s | Convor mesturno Deenc | 4 |
| n-1 | Hecawrel PMU No Notrs | 4 |
| E-1 |  | 4 |
| E-2 | EECTrack schemic onemum | 4 |
| E-s | Eectracl camamome pus | 4 |
| E- |  | 4 |
| E-5 | Track aicmich otnls | 4 |
| E-6 | Escrucu secancanow | 4 |




15

$>$

percn base




## gIE NOTE



3.



CEEFAL NOTES
Nu wom sul



 Nom








" (




19.





25.
2. Mackumed


2.




notes:




PVC CONDUTT PENEIRATION
(2 DETALL IN GYPSUM WALIBOAR DETALL IN GYF

Maw











E CONOU HOW 9 N. DUW (OR SWULR) Stres conour

3.


METAL PIPE THROUCH CONCREIE
(3)

METAL FIPE THROUGH CONCREIE
SCOLE NOT/ TO SCAIL OR BLOCK WALL


PIPE AND CONDUIT PENEIRATION
(4) DETALL $\mathbb{N}$ N

 Both sime of hoor muliz

> 5- 5 PIPE AND CONDUIT PENEIRATION
DETALL $\mathbb{N}$ CONCREIE OR MASONRY
SCNE NOT TO SCNE DETALL $\mathbb{N}$ CONCRETE OR MASONRY

208 \%. 20010.00
$\underset{\text { CONDUUTT }}{\text { PENETIC }}$
PENETRATIS
DETAALS
C-5






EFCTFICAL SPECFECATONS
SECTON 16010
A

2 new sit




Locu UTIUT courpens siwl Prover TiE Folumme:


1.02. cevew reanmeners














N. Stuop dommmas



## 

## SECTON NOHI


a.




| CONDUT SCHEDUL SECTION 18 mm |  |  |  |
| :---: | :---: | :---: | :---: |
| conour me |  | umbenow | 隹 |
| ar | Ance 358 |  | N/A |
| Rav, Regat cuv. |  |  | 0 mchis |
| pra, schimur to |  |  | 18 uctus |
| prac, schibue so |  |  | 18 \#chms |
| Loun Mex mix | ntole soo |  | N/n |
| rex mexich | NTECEE 348 |  | N/A |
| 'misru zua is | Sert mit And |  |  |

## $\frac{\text { SECTON } 16123}{1.01}$





 SeCCION 16130
-


## 







SECTION 18TO


sechavy

SECTOON NEDS






## gection 1 CASO


a.
c. Councum of pnesowes:












 SECTON 18470

ECHION 1647

## 

CWE SNNE

## 

a harre to conmer dewnmes for dexis no schevis.

CCTOW 12080
paber arctracel restwo fran









SECTON 109091






C-band 64T64R
Gen 2
700/850 4T4R Macro 320W ORU - New Filter (RF446ld-13A)
Specifications


* 5 MHz supporting in $\mathrm{BI} 3(700 \mathrm{MHz}$ ) depends on 3GPP std. and UE capability External filters in interferer and victim sides for Mexican boarder to support $5 \mid \mathrm{MHz}$ service need to be considered
(c) Samsumg Electronics. All Rights Reserved. Conlidential and Proprietary


## SAMSUNG

## Samsung <br> Micro Radio <br> CBRS(N48) <br> 4T4R Micro Radio

Samsung's CBRS 4T4R Micro Radio provides mobile
operators with a cost-effective solution to fill coverage
gaps encountered when Macro Radios are in use.

## Model Code <br> RT4423-48B(AC)



## Dual Personality

The new CBRS Radio supports existing CPRI and advanced eCPRI interfaces providing installation options for both legacy LTE and NR network equipment.


## High Capacity

The number of carriers required varies according to site(region). Supporting multiple carriers is essential to customers as they seek to utilize all frequencies available to them.
The new CBRS radio can support up to 5 carriers which is and increase of 3 carriers over the capacity of the previous CBRS product.


## O-RAN Compliant

A standardized O-RAN radio supports implementing cost-effective networks capable of enhanced data throughput without compromising existing or new network investments.
Samsung O-RAN products ensure state-of-the-art O-RAN technology will accelerate efforts for creating solid O-RAN ecosystems.


## Compact and Easy Installation

New CBRS RU is compact in it's design with a volume of 6 L and weighing only about 7 kg .
This compact design allows for various installation options including, tower, rooftop, pole, wall and shroud.
A clip on antenna is available providing flexibility to installation requirements.


## C Technical Specifications

| Item | Specification |
| :---: | :---: |
| Tech | LTE / NR |
| Band | B48, n48 / TDD |
| Frequency Band | $3,550-3,700 \mathrm{MHz}$ |
| RF Power | 20 W (5 W x 4 Ports) |
| IBW/OBW | $150 \mathrm{MHz} / 100 \mathrm{MHz}$ |
| Installation | Pole, Wall, Side by side (max 3 radio) |
| Size/ Weight | [Radio] <br> w/o Clip-on antenna : $8.7 \times 11.8 \times 3.6$ inch, $5.97 \mathrm{~L}, 7 \mathrm{~kg}$ <br> w/ Clip-on antenna : $8.7 \times 11.8 \times 5.0$ inch, $8.42 \mathrm{~L}, 8.5 \mathrm{~kg}$ <br> *AC and $D C$ type have same size and weight <br> [Bracket Weight] <br> Tilting \& Swivel (EP97-02038A) : 2.51 kg <br> Fixed (EP97-02037A) : 1.31kg <br> Side by side (EP97-02089A) : 8.0kg |


[^0]:    tnxTower Report - version 8.1.1.0

[^1]:    ${ }^{1} P_{u} / \phi P_{n}$ controls

[^2]:    The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

    ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.
    In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmiess ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

