10 Industrial Ave, Suite 3 Mahwah NJ 07430

PHONE: 201.684.0055 FAX: 201.684.0066



March 4, 2022

Members of the Siting Council Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

RE: Notice of Exempt Modification

157/169 Hampden Road, Stafford Springs, CT 06076

Latitude: 41.595861 Longitude: -72.212016

T-Mobile Site#: CTHA830A - Sprint Keep Project - Refile with revised plans

### Dear Ms. Bachman:

T-Mobile/Sprint currently maintains six (6) antennas at the 171-foot level of the existing 180-foot Guyed Tower at 169 Hampden Road, Stafford Springs, Connecticut. The 180-foot Guyed Tower is owned and operated by Everest Infrastructure. The ground space is owned by BJM IRA Joint Ventures. T-Mobile now intends to remove all Sprint equipment including antennas, cables, and ground equipment. T-mobile will be adding six (6) antennas. The new antennas will be installed at the same 171-foot level. The new antennas support 5G services.

### **Planned Modifications:**

### Tower:

Remove

(6) Sprint Antennas

(12) Sprint RRHs

All Sprint Hybrid Cables

### Install New:

- (3) APXVAALL24 43-U-NA20 Antennas
- (3) AIR6449 Antennas
- (3) Ericsson Radio 4480 B71+B85
- (3) Ericsson 4460 B25+B66
- (3) 6/24 Hybrid Cables

### **Ground:**

### Install New:

- (1) B160 Cabinet
- (1) Enclosure 6160
- (1) 48 KW Diesel Fueled Back-up Generator

### To Be Removed:

All Sprint Ground Equipment

The earliest Siting Council submission was from May 31, 2011. The original building permit for the tower construction was unavailable but attached is a permit application from June 24, 2011

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies§ 16- SOj-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.SA. § 16-SOj-73, a copy of this letter is being sent to First Selectman - Sal Titus, Elected Official, and David Perkins, Zoning Enforcement Officer, as well as the tower and property owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S;A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing structure.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

### **Eric Breun**

Transcend Wireless Cell: 201-658-7728

Email: ebreun@transcendwireless.com

### **Attachments**

cc: Sal Titus - as First Selectman of Stafford David Perkins - Zoning Enforcement Officer Everest Infrastructure Partnership - Tower Owner BJM IRA Joint Venture - Land Owner



SHIP TO:
SHANAL NI 07495
SHIP TO:
SHAND PERKINS ZEO
1 MAIN STREET
STAFFORD CT 06076

CT 061 9-99

UPS GROUND
TRACKING #: 12 V25 742 03 9701 7633

BILLING: P/P

Reference #1: CTHAB30A

TRACKING #: 12 V25 742 03 9701 7633

ERIC BREUN 2016587728 10 INDUSTRIAL AVE MAHWAH NJ 07430 10F1 SHIP TO:
EVEREST INFRASTRUCTURE PARTNERS
SUITE 703
NOVA TOWER 2
2 ALLEGHENY CENTER
ALLEGHENY PA 15212 ERIC BREUN 2016587728 10 INDUSTRIAL AVE MAHWAH NJ 07430

10F1

**1LBS** 



PA 152 9-42

**UPS GROUND** 

TRACKING #: 1Z V25 742 03 9080 0414



BILLING: P/P

Reference #1: CTHA830A

PA 193 9-01 SHIP TO:
BIM IRA JOINT VENTURE
60 HARRY STREET
CONSHOHOCKEN PA 19428

**UPS GROUND** 

TRACKING #: 1Z V25 742 03 9203 4409



BILLING: P/P

Reference #1: CTHA830A

XOL 22.02.16

## Hello, your package has been delivered.

Delivery Date: Thursday, 03/03/2022

Delivery Time: 11:00 AM

Left At: OFFICE
Signed by: DADAULT

## TRANSCEND WIRELESS

Tracking Number: <u>1ZV257420393072394</u>

FIRST SELECTMAN SAL TITUS

1 MAIN STREET

Ship To: STAFFORD, CT 06076

US

Number of Packages: 1

UPS Service: UPS Ground

Package Weight: 1.0 LBS

Reference Number: CTHA830A

## Hello, your package has been delivered.

**Delivery Date:** Thursday, 03/03/2022

Delivery Time: 11:00 AM

Left At: OFFICE
Signed by: DADAULT

## TRANSCEND WIRELESS

Tracking Number: <u>1ZV257420397017633</u>

DAVID PERKINS ZEO

Ship To: 1 MAIN STREET STAFFORD, CT 06076

US

Number of Packages: 1

UPS Service: UPS Ground

Package Weight: 1.0 LBS

Reference Number: CTHA830A

## TRANSCEND WIRELESS

Estimated delivery

# Monday, March 07 between 9:15 A.M. - 11:15 A.M. @



### Ship To

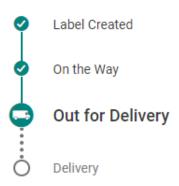
EVEREST INFRASTRUCTURE PARTNERS 2 ALLEGHENY CENTER NOVA TOWER 2 SUITE 703 ALLEGHENY, PA 15212 US

Your shipment from

# TRANSCEND WIRELESS

Estimated delivery

# Today, March 03 by 7:00 P.M.



### Ship To

BJM IRA JOINT VENTURE 60 HARRY STREET CONSHOHOCKEN, PA 19428 US

## 169 HAMPDEN RD



Location 169 HAMPDEN RD Mblu 23//60//

Acct# 00109700 Owner BJM IRA JOINT VENTURE

Assessment \$260,140 Appraisal \$473,800

PID 1227 Building Count 1

### **Current Value**

Appraisal								
Valuation Year Improvements Land Total								
2020	\$358,100	\$473,800						
Assessment								
Valuation Year	Improvements	Land	Total					
2020	\$80,990	\$179,150	\$260,140					

### Owner of Record

Owner BJM IRA JOINT VENTURE Sale Price \$525,000

Co-Owner Certificate

 Address
 60 HARRY ST
 Book & Page
 704/159

 CONSHOHOCKEN , PA 19428
 Sale Date
 11/10/2021

Instrument 0G

### Ownership History

Ownership History									
Owner Sale Price Certificate Book & Page Instrument Sale Date									
BJM IRA JOINT VENTURE	\$525,000		704/159	0G	11/10/2021				
ANGELO MICHAEL+SHELLY M	\$0		0595/0005	01	09/24/2012				
ANGELO MICHAEL	\$0		0595/0002	01	09/24/2012				
ANGELO MICHAEL J	\$0	1	0326/0545		03/31/1995				

### **Building Information**

## Building 1 : Section 1

Year Built: 1999 Living Area: 768 Replacement Cost: \$91,353 **Building Percent Good:** 87

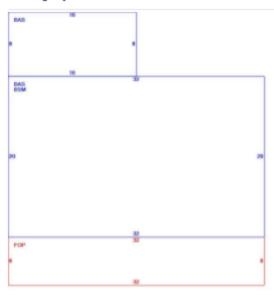
Replacement Cost

Less Depreciation: \$79,500							
Building	Attributes						
Field	Description						
STYLE	Single Family						
MODEL	Comm/Ind						
Grade	С						
Stories:	1						
Occupancy	1.00						
Exterior Wall 1	Logs						
Exterior Wall 2							
Roof Structure	Gable						
Roof Cover	Asph/F Gls/Cmp						
Interior Wall 1	Drywall/Sheet						
Interior Wall 2							
Interior Floor 1	Average						
Interior Floor 2							
Heating Fuel	Gas						
Heating Type	Forced Hot Air						
AC Type	None						
Struct Class							
Bldg Use	SFD - Comm						
Total Bedrooms	2						
Total Baths	1						

## **Building Photo**



## **Building Layout**



1st Floor Use:	
Heat/AC	None
Frame Type	Wood Frame
Baths/Plumbing	Average
Ceiling/Wall	Ceil & Wall
Rooms/Prins	Average
Wall Height	8.00
Num Fixtures	

	Legend		
Code	Description	Gross Area	Living Area
BAS	First Floor	768	768
BSM	Basement	640	0
FOP	Open Porch	192	0
		1,600	768

### Extra Features

Extra Features <u>Legend</u>							
Code	Description	Size	Value	Bldg #			
FPL	Com Fireplace	1.00 UNITS	\$1,700	1			

### Land

Land Use		Land Line Valuation			
Use Code	101C	Size (Acres)	43.54		
Description	SFD - Comm 0	Frontage			
Zone		Depth			
Neighborhood	502	Assessed Value	\$179,150		
Alt Land Appr Category	No	Appraised Value	\$358,100		

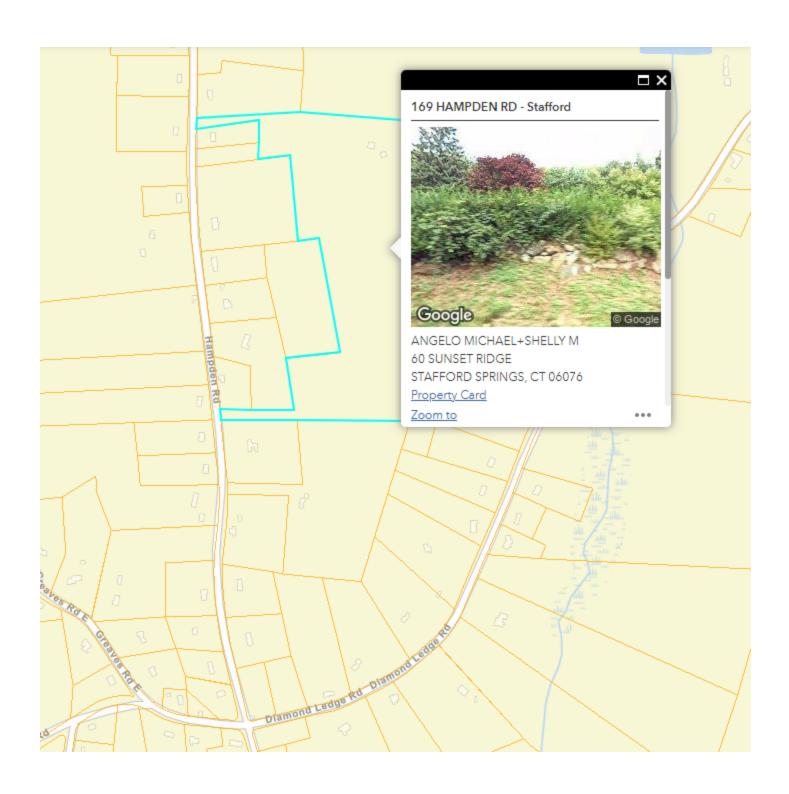
### Outbuildings

Outbuildings								
Code	Description	Sub Code	Sub Description	Size	Value	Bldg #		
FGR2	Garage w/ Loft			1024.00 S.F.	\$18,600	1		
FGR2	Garage w/ Loft			676.00 S.F.	\$12,300	1		
FN3	FENCE-6' CHAIN			150.00 L.F.	\$900	1		
FCP	Carport			384.00 S.F.	\$2,700	1		

### Valuation History

Appraisal								
Valuation Year	Improvements	Land	Total					
2019	\$99,100	\$376,400	\$475,500					
2018	\$99,100	\$376,400	\$475,500					
2017	\$99,100	\$376,400	\$475,500					

Assessment								
Valuation Year Improvements Land Total								
2019	\$69,370	\$176,000	\$245,370					
2018	\$69,370	\$176,000	\$245,370					
2017	\$69,370	\$176,000	\$245,370					





## STATE OF CONNECTICUT

## CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051
Phone: (860) 827-2935 Fax: (860) 827-2950
E-Mail: siting.council@ct.gov
www.ct.gov/csc

May 31, 2011

Mark Hulshart, Principal Hulshart & Associates, LLC 3009 Federal Hill Drive Falls Church, VA 22044

RE: **EM-SPRINT-134-110505** – Sprint Spectrum L.P. notice of intent to modify an existing telecommunications facility located at 169 Hampden Road, Stafford, Connecticut.

Dear Mr. Hulshart:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies with the following conditions:

- Any deviation from the proposed modification as specified in this notice and supporting materials with Council shall render this acknowledgement invalid;
- Any material changes to this modification as proposed shall require the filing of a new notice with the Council;
- Not less than 45 days after completion of construction, the Council shall be notified in writing that construction has been completed;
- The validity of this action shall expire one year from the date of this letter; and
- The applicant may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration;

The proposed modifications including the placement of all necessary equipment and shelters within the tower compound are to be implemented as specified here and in your notice dated April 29, 2011. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Thank you for your attention and cooperation.

Very truly yours,

Linda Roberts
Executive Director

LR/CDM/laf

c: The Honorable Michael P. Krol, First Selectman, Town of Stafford Wendell Avery, Zoning Enforcement Officer, Town of Stafford Michael Angelo

G:\EM & TS\SPRINT SPECTRUM\Stafford\dc053111HampdenRd,DOC



# BUILDING PERMIT

Building Official

1 Main Street - Town Hall
Stafford Springs, CT 06076

Let., (860) 684-1775 - Fax: (860) 684-1768

"A certificate of Use or Occupancy is required upon completion of new work, alteration or change of use." Separate permits are required for plumbing, heating and electrical

Date:			Licens	e:		Ex	piration Date:		
Esti.nated Cost: \$1	Date: License:  Esti.nated Cost: \$14,000 Fee: 196 N			∕ap: _	23 /060 L	nt: P	ermit#: /	5906	
Location of Constri	uction	: 169 Hampden Roa	d, St	afford CT 0607	75		TO A PARTY OF THE	CONT. DOCUMENT	COLUMN TO THE WAY OF THE PARTY.
		ss: Sprint c/o Blac							
		ead, Suite 420, Bi		Farms. MI 480	25				
Contractor's Name	& A	ddress: Overland Co	ntrac	ting Inc.			The state of the s		20102-2-002
		8400 Ward Pa	rkwav	. Kansas City	MO (	54114			13
Sigpature of Applic	eant, I	Homeowner, Great	Te	lephone Number		Building Of	ficial Signature	Ī	Date
Kurstin	M	Faren	(24	18) 594-9330 19) (013-3933)	زد ۱۱	Demla	nouch	6-7	-11
Describe Nature of	Mari	Add fuel cell &	sto	age cabinets o	on 6'	x 9' concrete	pad inside existi	ng lease	area.
Describe Hature of	******	·							
								<del></del>	
TYPE		FOUNDATIO	NS	ROOF TYP	E	FOOTING	FRAMING	SIZE	SPAN
Single Family		Thickness	<del></del>	Gable		Size	Joist	<u> </u>	
Two Family	<u> </u>	Concrete slab	×	Hip	<u> </u>	Stone	2 <sup>nd</sup> Floor	<u> </u>	<u> </u>
Apt House	<u></u>	Concrete Blocks		Gambrel	20	Concrete	Rafter	<u> </u>	
Agricultural		Piers		Truss		Drains	Girder		<u> </u>
Accessory		Stone	<u>.</u>	Flat		Depth	Column		1
Office				Roof Pitch			Sill	<u> </u>	<u> </u>
Factory		CONSTRUCTIO	N		,	CHIMNEYS Post			
Gas Station		Frame	<u> </u>	ROOFING	N/A	Size / Flues	Plate		
Commercial	x	Masonry		Asphalt Shingle		Stone	Stud	<u> </u>	
Demolition		I.C.F.	<u> </u>	Wood Shingle		Brick			
Other:		Other:	<u> </u>	Built-up		Block	Species & Grade	· ·	
			<u> </u>	Other:		Factory Built			<u> </u>
Number of Rooms		EXTERIOR				Fire Place			
Number of Bathrooms		Clapboard or Wood Shingle		Cellar <sup>1</sup>	A/N				
Number of Bedrooms		Vinyl		Whole		Built to Conform t	o:		
Insulation		Masonry		Part		Residential Code (IRC)			
Ceiling		Other		None		Commercial Code (IBC)			
Walls				Slab					
Floors		l		Other		F.M. Approval			
SWIMMING PO	OL:	Above Ground		In Ground 🗆		Fence □ N/A			

Work shall not proceed until the inspector has inspected and approved the various stages of construction. Final inspection is required upon completion of work. Permit will become null and void if construction work is not started within six months of the date the permit is issued. Permit grants the right to entry to any official from the building, health, or zoning departments during normal business hours for the purpose of inspection. If signed by other than the owner, applicant attests compliance with CGS20-388B and has authorization by owner to apply for this permit.

SBP 708 DD Printing





SPRINT ID: CT33XC553 SITE ID: CTHA830A 157 HAMPDEN RD STAFFORD SPRINGS, CT 06076

T-MOBILE RAN TEMPLATE (PROVIDED BY RFDS)

67E5A998E 6160

T-MOBILE A+L TEMPLATE (PROVIDED BY RFDS)

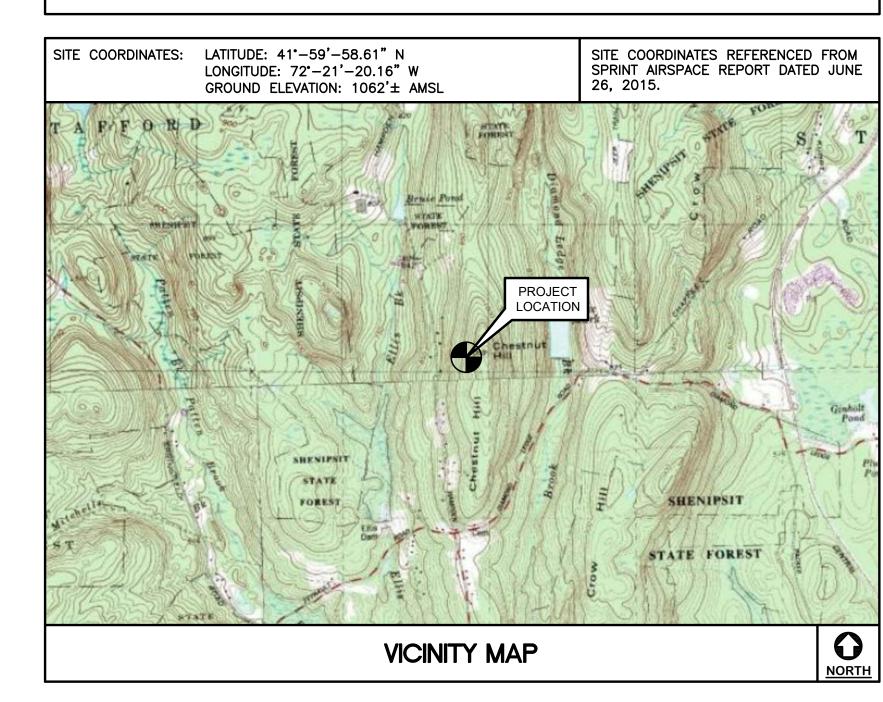
67E5998E\_1xAIR+10P

# **GENERAL NOTES**

- ALL WORK SHALL BE IN ACCORDANCE WITH THE 2015 INTERNATIONAL BUILDING CODE AS MODIFIED BY THE 2018 CONNECTICUT SUPPLEMENT, INCLUDING THE TIA/EIA-222 REVISION "G" "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND SUPPORTING STRUCTURES." 2017 CONNECTICUT FIRE SAFETY CODE, NATIONAL ELECTRICAL CODE AND LOCAL CODES.
- CONTRACTOR SHALL REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUBCONTRACTORS AND ALL RELATED PARTIES. THE SUBCONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
- CONTRACTOR SHALL PROVIDE A COMPLETE BUILD-OUT WITH ALL FINISHES, STRUCTURAL, MECHANICAL, AND ELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON THE DRAWINGS OR IN THE WRITTEN SPECIFICATIONS.
- CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OVER THE WORK.
- CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION, PLUMBING, ELECTRICAL, AND HVAC. PERMITS SHALL BE PAID FOR BY THE RESPECTIVE SUBCONTRACTORS.
- CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS AND SPECIFICATIONS ON SITE AT ALL TIMES AND INSURE DISTRIBUTION AND SPECIFICATIONS ON SITE AT ALL TIMES AND INSURE DISTRIBUTION OF NEW DRAWINGS TO SUBCONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE. ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. THE CONTRACTOR SHALL FURNISH AN 'AS-BUILT' SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
- LOCATION OF EQUIPMENT, AND WORK SUPPLIED BY OTHERS THAT IS DIAGRAMMATICALLY INDICATED ON THE DRAWINGS SHALL BE DETERMINED BY THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE LOCATIONS AND DIMENSIONS SUBJECT TO STRUCTURAL CONDITIONS AND WORK OF THE SUBCONTRACTORS.
- THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURES AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY.
- DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.

- 10. ALL UTILITY WORK SHALL BE IN ACCORDANCE WITH LOCAL UTILITY COMPANY REQUIREMENTS AND SPECIFICATIONS.
- 11. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUBCONTRACTORS FOR ANY CONDITION PER MANUFACTURER'S RECOMMENDATIONS. CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR CONSTRUCTION
- 12. ANY AND ALL ERRORS, DISCREPANCIES, AND 'MISSED' ITEMS ARE TO BE BROUGHT TO THE ATTENTION OF THE T-MOBILE CONSTRUCTION MANAGER DURING THE BIDDING PROCESS BY THE CONTRACTOR. ALL THESE ITEMS ARE TO BE INCLUDED IN THE BID. NO 'EXTRA' WILL BE ALLOWED FOR MISSED ITEMS.
- 13. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON-SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
- 14. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE CONSTRUCTION MANAGER FOR
- 15. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT
- 16. COORDINATION, LAYOUT, FURNISHING AND INSTALLATION OF CONDUITS AND ALL APPURTENANCES REQUIRED FOR PROPER INSTALLATION OF ELECTRICAL AND TELECOMMUNICATION SERVICE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR.
- 17. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
- 18. THE CONTRACTOR SHALL CONTACT 'CALL BEFORE YOU DIG' AT LEAST 48 HOURS PRIOR TO ANY EXCAVATIONS AT 1-800-922-4455. ALL UTILITIES SHALL BE IDENTIFIED AND CLEARLY MARKED. CONTRACTOR SHALL MAINTAIN AND PROTECT MARKED UTILITIES THROUGHOUT PROJECT COMPLETION.
- 19. CONTRACTOR SHALL COMPLY WITH THE OWNER'S ENVIRONMENTAL ENGINEER ON ALL METHODS AND PROVISIONS FOR ALL EXCAVATION ACTIVITIES INCLUDING SOIL DISPOSAL. ALL BACKFILL MATERIALS TO BE PROVIDED BY THE CONTRACTOR.

### SITE DIRECTIONS TO: 157 HAMPDEN RD STAFFORD SPRINGS, CT 06076 FROM: 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 GET ON I-91 S IN WINDSOR FROM DAY HILL RD. 4.30 MI. 3.60 MI. MERGE ONTO I-91 S. TAKE EXIT 35A FOR I-291 TOWARD MANCHESTER. 0.60 MI. CONTINUE ONTO I-291 E. 5.60 MI. 5. USE THE LEFT LANE TO MERGE ONTO I-84 E TOWARD BOSTON. 8.50 MI. 6. TAKE EXIT 67 FOR CT-31. 0.30 MI. TURN RIGHT ONTO CT-31 S. 0.20 MI. 8. TURN LEFT ONTO LOEHR RD. 1.00 MI. 9. TURN LEFT ONTO MOUNTAIN SPRING RD/ REED RD. 0.70 MI. 10. TURN LEFT ONTO OLD POST RD. DESTINATION WILL BE ON THE LEFT. 0.07 MI.



## PROJECT SUMMARY

THE PROPOSED SCOPE OF WORK CONSISTS OF A MODIFICATION TO THE EXISTING UNMANNED TELECOMMUNICATIONS FACILITY INCLUDING

- 1. REMOVE EXISTING SPRINT EQUIPMENT
- 2. REMOVE EXISTING STEEL BEAMS AND GRATING AT GRADE
- INSTALL (1) APXVAALL24\_43-U-NA20 ANTENNA PER SECTOR
- 4. INSTALL (1) ERICSSON AIR6449 B41 ANTENNA PER SECTOR
- 5. INSTALL (1) RADIO 4480 B71+B85 PER SECTOR. TOTAL OF (3)
- 6. INSTALL (1) RADIO 4460 B25+B66 PER SECTOR. TOTAL OF (3)
- 7. INSTALL 150A CIRCUIT BREAKER
- 8. REMOVE ALL EXISTING HYBRID, INSTALL (3) 6/24 4AWG HYBRIDS
- 9. INSTALL (1) T-MOBILE POWER ENCLOSURE 6160
- 10. INSTALL (1) T-MOBILE BATTERY CABINET B160
- 11. INSTALL 48KW DIESEL FUELED BACK-UP GENERATOR
- 12. INSTALL (1) 200A AUTOMATIC TRANSFER SWITCH MOUNTED TO NEW 2' EQUIPMENT FRAME
- 13. RELOCATE EXISTING ANTENNA MOUNTS TO NEW ANTENNA FRAMES 14. INSTALL (1) 9' MAST PER SECTOR FOR POS. 1 ANTENNA
- TOTAL OF (3)
- 15. INSTALL (3) NEW ANTENNA FRAMES

## PROJECT SUMMARY (STRUCTURAL)

FOR REQUIRED STRUCTURAL MODIFICATIONS, SEE SHEET(S) S-1 FOR

## PROJECT INFORMATION SPRINT ID: CT33XC553 CTHA830A SITE ID: 157 HAMPDEN RD SITE ADDRESS: STAFFORD SPRINGS, CT 06076 T-MOBILE NORTHEAST, LLC **APPLICANT:** 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 KYLE RICHERS CONTACT PERSON TRANSCEND WIRELESS, (908) 447-4716 ENGINEER OF RECORD: CENTEK ENGINEERING, INC. 63-2 NORTH BRANFORD RD. BRANFORD, CT 06405 CARLO F. CENTORE, PE (203) 488-0580 EXT. 122 LATITUDE: 41°-59'-58.61" N PROJECT COORDINATES: LONGITUDE: 72°-21'-20.16" W GROUND ELEVATION: 1062'± AMSL SITE COORDINATES REFERENCED

FROM SPRINT AIRSPACE REPORT

DATED JUNE 26, 2015.

SHE	ET INDEX	
SHT. NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	3
N-1	GENERAL NOTES AND SPECIFICATIONS	3
C-1	SITE LOCATION PLAN	3
C-2	COMPOUND PLAN AND ELEVATION	3
C-3	EQUIPMENT PLANS	3
C-4	ANTENNA PLANS AND ELEVATIONS	3
C-5	TYPICAL EQUIPMENT DETAILS	3
C-6	TYPICAL EQUIPMENT DETAILS	3
S-1	STRUCTURAL DETAILS	3
E-1	ELECTRICAL RISER DIAGRAM AND CONDUIT ROUTING	3
E-2	TYPICAL ELECTRICAL DETAILS	3
E-3	ELECTRICAL SPECIFICATIONS	3

04/22/21 SCALE: AS NOTED JOB NO. 21005.22

SHEET

## NOTES AND SPECIFICATIONS

## **DESIGN BASIS:**

GOVERNING CODE: 2015 INTERNATIONAL BUILDING (IBC) AS MODIFIED BY THE 2018 CONNECTICUT STATE BUILDING CODE.

- DESIGN CRITERIA:
- RISK CATEGORY II (BASED ON IBC TABLE 1604.5)
- ULTIMATE DESIGN SPEED (TOWER STRUCTURE): 123 MPH (Vasd) (EXPOSURE B/ IMPORTANCE FACTOR 1.0 BASED ON ASCE 7-10).

## SITE NOTES

- 1. THE CONTRACTOR SHALL CALL UTILITIES PRIOR TO THE START OF
- 2. ACTIVE EXISTING UTILITIES, WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES. THE ENGINEER SHALL BE NOTIFIED IMMEDIATELY, PRIOR TO PROCEEDING, SHOULD ANY UNCOVERED EXISTING UTILITY PRECLUDE COMPLETION OF THE WORK IN ACCORDANCE WITH THE CONTRACT DOCUMENTS.
- 3. THE AREAS OF THE COMPOUND DISTURBED BY THE WORK SHALL BE RETURNED TO THEIR ORIGINAL CONDITION.
- 4. CONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES, SHALL BE IN CONFORMANCE WITH THE LOCAL GUIDELINES FOR EROSION AND SEDIMENT
- 5. IF ANY FIELD CONDITIONS EXIST WHICH PRECLUDE COMPLIANCE WITH THE DRAWINGS, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ENGINEER AND SHALL PROCEED WITH AFFECTED WORK AFTER CONFLICT IS SATISFACTORILY RESOLVED.

## **GENERAL NOTES**

- ALL WORK SHALL BE IN ACCORDANCE WITH THE 2015 INTERNATIONAL BUILDING CODE AS MODIFIED BY THE 2018 CONNECTICUT SUPPLEMENT, INCLUDING THE TIA/EIA-222 REVISION "G" "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND SUPPORTING STRUCTURES." 2017 CONNECTICUT FIRE SAFETY CODE, NATIONAL ELECTRICAL CODE AND LOCAL
- 2. CONTRACTOR SHALL REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUBCONTRACTORS AND ALL RELATED PARTIES. THE SUBCONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
- CONTRACTOR SHALL PROVIDE A COMPLETE BUILD-OUT WITH ALL FINISHES, STRUCTURAL, MECHANICAL, AND ELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON THE DRAWINGS OR IN THE WRITTEN SPECIFICATIONS.
- 4. CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OVER THE WORK.
- 5. CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION, PLUMBING, ELECTRICAL AND HVAC. PERMITS SHALL BE PAID FOR BY THE RESPECTIVE SUBCONTRACTORS.
- CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS AND SPECIFICATIONS ON SITE AT ALL TIMES AND INSURE DISTRIBUTION OF NEW DRAWINGS TO SUBCONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE. ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. THE CONTRACTOR SHALL FURNISH AN 'AS-BUILT' SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
- 7. LOCATION OF EQUIPMENT AND WORK SUPPLIED BY OTHERS THAT IS DIAGRAMMATICALLY INDICATED ON THE DRAWINGS, SHALL BE DETERMINED BY THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE LOCATIONS AND DIMENSIONS SUBJECT TO STRUCTURAL CONDITIONS AND WORK OF THE SUBCONTRACTORS.
- THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURES AND IT'S COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING. BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY.
- DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES. LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
- 10. ALL UTILITY WORK SHALL BE IN ACCORDANCE WITH LOCAL UTILITY COMPANY REQUIREMENTS AND SPECIFICATIONS.
- 11. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUBCONTRACTORS FOR ANY CONDITION PER MFR.'S RECOMMENDATIONS. CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR CONSTRUCTION MANAGER.
- 12. ANY AND ALL ERRORS, DISCREPANCIES, AND "MISSED" ITEMS, ARE TO BE BROUGHT TO THE ATTENTION OF THE SITE OWNER'S CONSTRUCTION MANAGER DURING THE BIDDING PROCESS BY THE CONTRACTOR. ALL THESE ITEMS ARE TO BE INCLUDED IN THE BID. NO 'EXTRA' WILL BE ALLOWED FOR MISSED ITEMS.
- 13. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON-SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
- 14. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE CONSTRUCTION MANAGER FOR REVIEW.
- 15. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES, AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA.
- 16. COORDINATION, LAYOUT, FURNISHING AND INSTALLATION OF CONDUIT AND ALL APPURTENANCES REQUIRED FOR PROPER INSTALLATION OF ELECTRICAL AND TELECOMMUNICATION SERVICE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR.
- 17. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
- 18. THE CONTRACTOR SHALL CONTACT 'CALL BEFORE YOU DIG' AT LEAST 48 HOURS PRIOR TO ANY EXCAVATIONS AT 1-800-922-4455. ALL UTILITIES SHALL BE IDENTIFIED AND CLEARLY MARKED. CONTRACTOR SHALL MAINTAIN AND PROTECT MARKED UTILITIES THROUGHOUT PROJECT
- 18. CONTRACTOR SHALL COMPLY WITH OWNER'S ENVIRONMENTAL ENGINEER ON ALL METHODS AND PROVISIONS FOR ALL EXCAVATION ACTIVITIES INCLUDING SOIL DISPOSAL. ALL BACKFILL MATERIALS TO BE PROVIDED BY THE CONTRACTOR.
- 19. THE COUNTY/CITY/TOWN WILL MAKE PERIODIC FIELD OBSERVATION AND INSPECTIONS TO MONITOR THE INSTALLATION, MATERIALS, WORKMANSHIP AND EQUIPMENT INCORPORATED INTO THE PROJECT TO ENSURE COMPLIANCE WITH THE DESIGN PLANS, SPECIFICATIONS, CONTRACT DOCUMENTS AND APPROVED SHOP DRAWINGS.
- 20. THE COUNTY/CITY/TOWN MUST BE NOTIFIED (2) WORKING DAYS PRIOR TO CONCEALMENT/BURIAL OF ANY SYSTEM OR MATERIAL THAT WILL PREVENT THE DIRECT INSPECTION OF MATERIALS, METHODS OR WORKMANSHIP. EXAMPLES OF THESE PROCESSES ARE BACKFILLING A GROUND RING OR TOWER FOUNDATION, POURING TOWER FOUNDATIONS, BURYING GROUND RODS, PLATES OR GRIDS, ETC. THE CONTRACTOR MAY PROCEED WITH THE SCHEDULED PROCESS (2) WORKING DAYS AFTER PROVIDING NOTICE UNLESS NOTIFIED OTHERWISE BY THE COUNTY/CITY/TOWN.

## STRUCTURAL STEEL

- 1. ALL STRUCTURAL STEEL IS DESIGNED BY ALLOWABLE STRESS DESIGN (ASD)
  - A. STRUCTURAL STEEL (W SHAPES)---ASTM A992 (FY = 50 KSI) B. STRUCTURAL STEEL (OTHER SHAPES)——ASTM A36 (FY = 36 KSI) C. STRUCTURAL HSS (RECTANGULAR SHAPES) -- ASTM A500 GRADE B,
- (FY = 46 KSI)D. STRUCTURAL HSS (ROUND SHAPES) --- ASTM A500 GRADE B,
  - (FY = 42 KSI)PIPE---ASTM A53 (FY = 35 KSI)
- CONNECTION BOLTS---ASTM A325-N U-BOLTS---ASTM A36
- ANCHOR RODS---ASTM F 1554
- WELDING ELECTRODE --- ASTM E 70XX
- 2. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE ENGINEER FOR REVIEW. SHOP DRAWINGS SHALL INCLUDE THE FOLLOWING: SECTION PROFILES, SIZES, CONNECTION ATTACHMENTS, REINFORCING, ANCHORAGE, SIZE AND TYPE OF FASTENERS AND ACCESSORIES. INCLUDE ERECTION DRAWINGS, ELEVATIONS AND DETAILS.
- STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH THE LATEST PROVISIONS OF AISC MANUAL OF STEEL
- 4. PROVIDE ALL PLATES, CLIP ANGLES, CLOSURE PIECES, STRAP ANCHORS, MISCELLANEOUS PIECES AND HOLES REQUIRED TO COMPLETE THE STRUCTURE.
- 5. FIT AND SHOP ASSEMBLE FABRICATIONS IN THE LARGEST PRACTICAL SECTIONS FOR DELIVERY TO SITE.
- 6. INSTALL FABRICATIONS PLUMB AND LEVEL, ACCURATELY FITTED, AND FREE FROM DISTORTIONS OR DEFECTS.
- 7. AFTER ERECTION OF STRUCTURES, TOUCHUP ALL WELDS, ABRASIONS AND NON-GALVANIZED SURFACES WITH A 95% ORGANIC ZINC RICH PAINT IN ACCORDANCE WITH ASTM 780.
- 8. ALL STEEL MATERIAL (EXPOSED TO WEATHER) SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT DIPPED GALVANIZED) COATINGS" ON IRONS AND STEEL PRODUCTS.
- 9. ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC COATING (HOT-DIP) ON IRON AND STEEL HARDWARE".
- 10. THE ENGINEER SHALL BE NOTIFIED OF ANY INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON CONFORMING MATERIALS OR CONDITIONS TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE ENGINEER REVIEW.
- 11. CONNECTION ANGLES SHALL HAVE A MINIMUM THICKNESS OF 1/4 INCHES.
- 12. STRUCTURAL CONNECTION BOLTS SHALL CONFORM TO ASTM A325. ALL BOLTS SHALL BE 3/4" DIAMETER MINIMUM AND SHALL HAVE A MINIMUM OF TWO BOLTS, UNLÉSS OTHERWISE ON THE DRAWINGS.
- 13. LOCK WASHER ARE NOT PERMITTED FOR A325 STEEL ASSEMBLIES.
- 14. SHOP CONNECTIONS SHALL BE WELDED OR HIGH STRENGTH BOLTED.
- 15. MILL BEARING ENDS OF COLUMNS, STIFFENERS, AND OTHER BEARING SURFACES TO TRANSFER LOAD OVER ENTIRE CROSS SECTION.
- 16. FABRICATE BEAMS WITH MILL CAMBER UP.
- 17. LEVEL AND PLUMB INDIVIDUAL MEMBERS OF THE STRUCTURE TO AN ACCURACY OF 1:500, BUT NOT TO EXCEED 1/4" IN THE FULL HEIGHT OF THE COLUMN.
- 18. COMMENCEMENT OF STRUCTURAL STEEL WORK WITHOUT NOTIFYING THE ENGINEER OF ANY DISCREPANCIES WILL BE CONSIDERED ACCEPTANCE OF PRECEDING WORK.
- 19. INSPECTION AND TESTING OF ALL WELDING AND HIGH STRENGTH BOLTING SHALL BE PERFORMED BY AN INDEPENDENT TESTING LABORATORY.
- 20. FOUR COPIES OF ALL INSPECTION TEST REPORTS SHALL BE SUBMITTED TO THE ENGINEER WITHIN TEN (10) WORKING DAYS OF THE DATE OF INSPECTION.

NORTHEAST

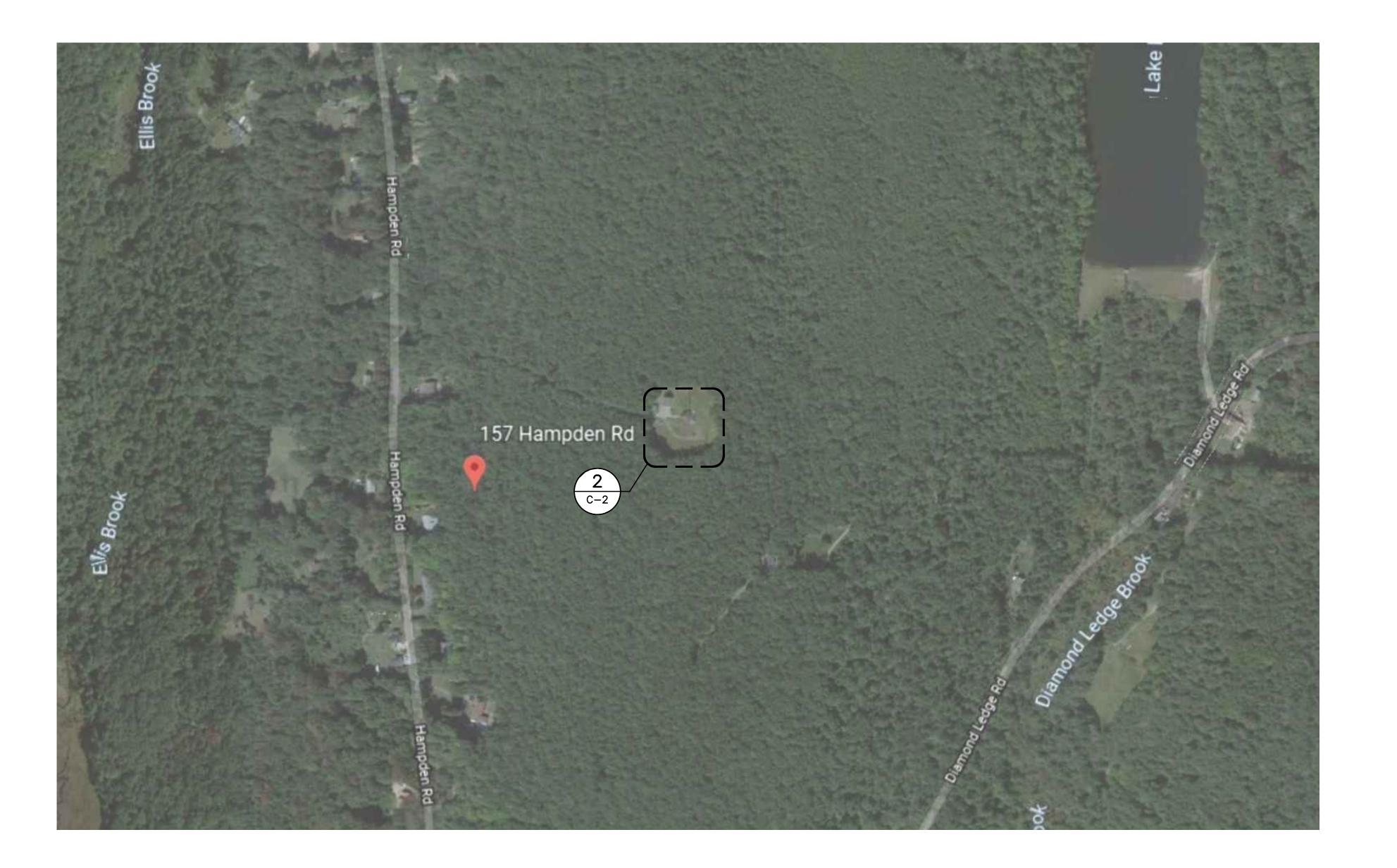
04/22/21 SCALE: AS NOTED JOB NO. 21005.22

GENERAL NOTES AND **SPECIFICATIONS** 



Sheet No. 2

						ANTENNA SCHEDULE		
SECTOR	R EXISTING/PROPOSED	ANTENNA	SIZE (INCHES) (L x W x D)	ANTENNA & HEIGHT	AZIMUTH	(E/P) RRU (QTY)	(E/P) TMA (QTY)	(QTY) PROPOSED COAX (LENGTH)
A1	PROPOSED	RFS-APXVAALL24_43-U-NA20	95.9 x 24 x 8.5	171'	0.	(P) RADIO 4480 B71+B85 (1), (P) RADIO 4460 B25+B66 (1)		(1) 6/24 4AWG HYBRID
A2	PROPOSED	ERICSSON-AIR6449 B41	33.1 x 20.6 x 8.6	171'	0°			CABLE (±210')
B1	PROPOSED	RFS-APXVAALL24_43-U-NA20	95.9 x 24 x 8.5	171'	120°	(P) RADIO 4480 B71+B85 (1), (P) RADIO 4460 B25+B66 (1)		(1) 6/24 4AWG HYBRID
B2	PROPOSED	ERICSSON-AIR6449 B41	33.1 x 20.6 x 8.6	171'	120°			CABLE (±210')
C1	PROPOSED	RFS-APXVAALL24_43-U-NA20	95.9 x 24 x 8.5	171'	240°	(P) RADIO 4480 B71+B85 (1), (P) RADIO 4460 B25+B66 (1)		(1) 6/24 4AWG HYBRID
C2	PROPOSED	ERICSSON-AIR6449 B41	33.1 x 20.6 x 8.6	171'	240°			CABLE (±210')





## ENGINEER SEAL CONVICTION OF AWINGS - REVISED PER GENERATOR LOCATION OF AWINGS - REVISED COORDINATES PER AIRSIONAL BY CONSTRUCTION DRAWINGS - REVISED STRUCTURAL COMPLIANC TUR CONSTRUCTION DRAWINGS - REVISED STRUCTURAL COMPLIANC OF 09/29/21 RTS TUR CONSTRUCTION DRAWINGS - REVISED PER NEW RFDS

Sprint > Mr. Th. Mo. T

Centered on Solutions (203) 488-0580 (203) 488-8587 Fax 63-2 North Branford Road Branford, CT 06405

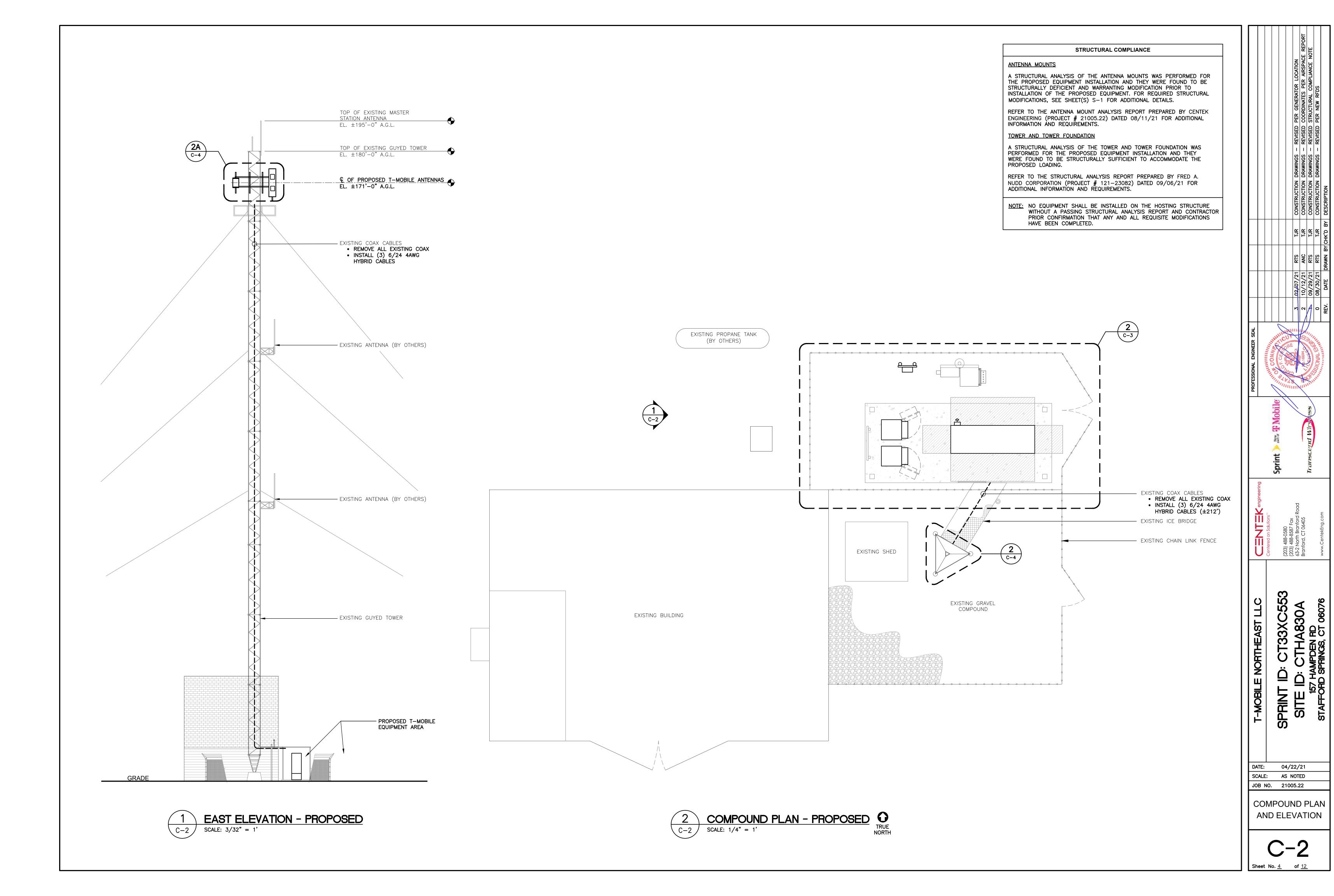
IT ID: CT33XC553 E ID: CTHA830A 157 HAMPDEN RD

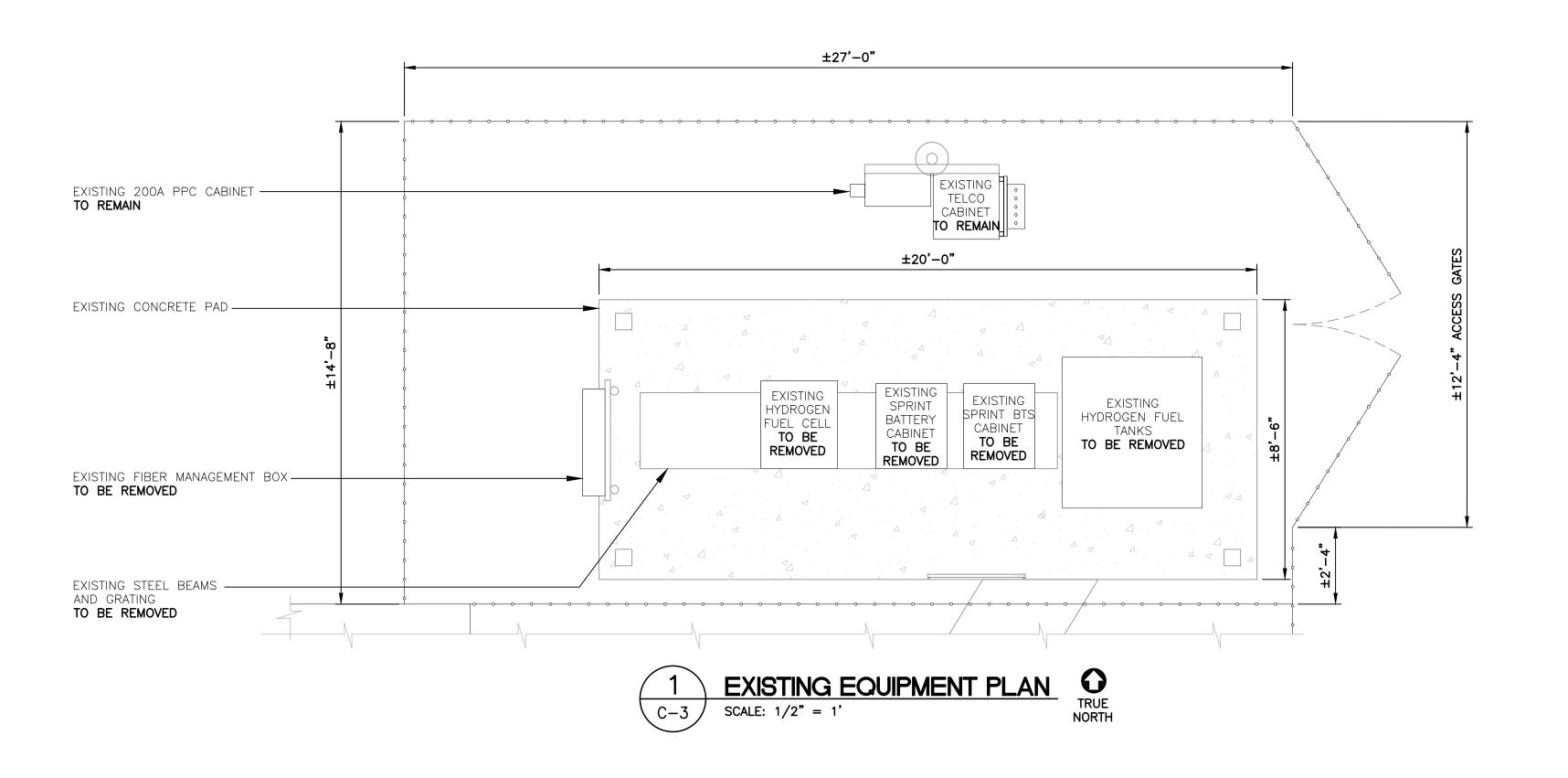
SPRINT ID: CT

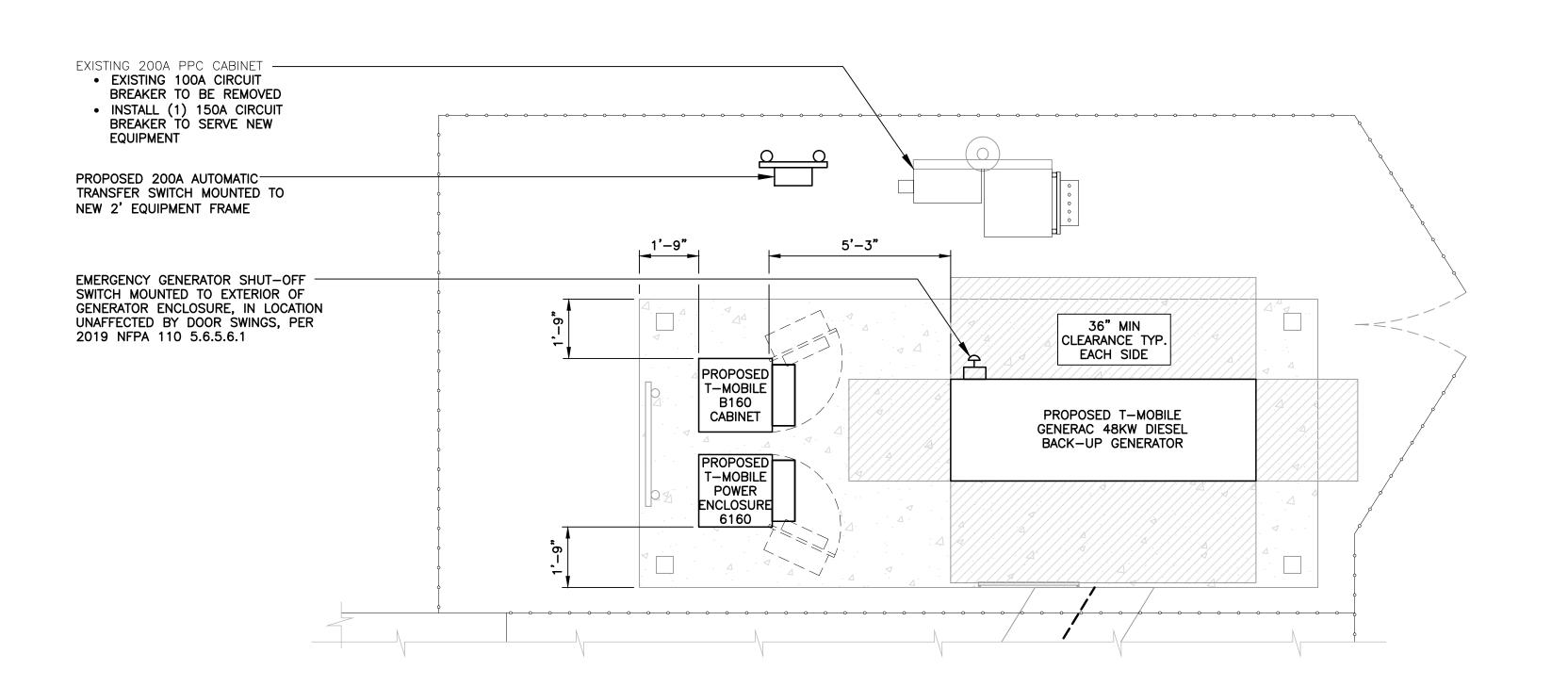
DATE: 04/22/21
SCALE: AS NOTED
JOB NO. 21005.22

SITE LOCATION PLAN

**C**-1
Sheet No. 3 of 12



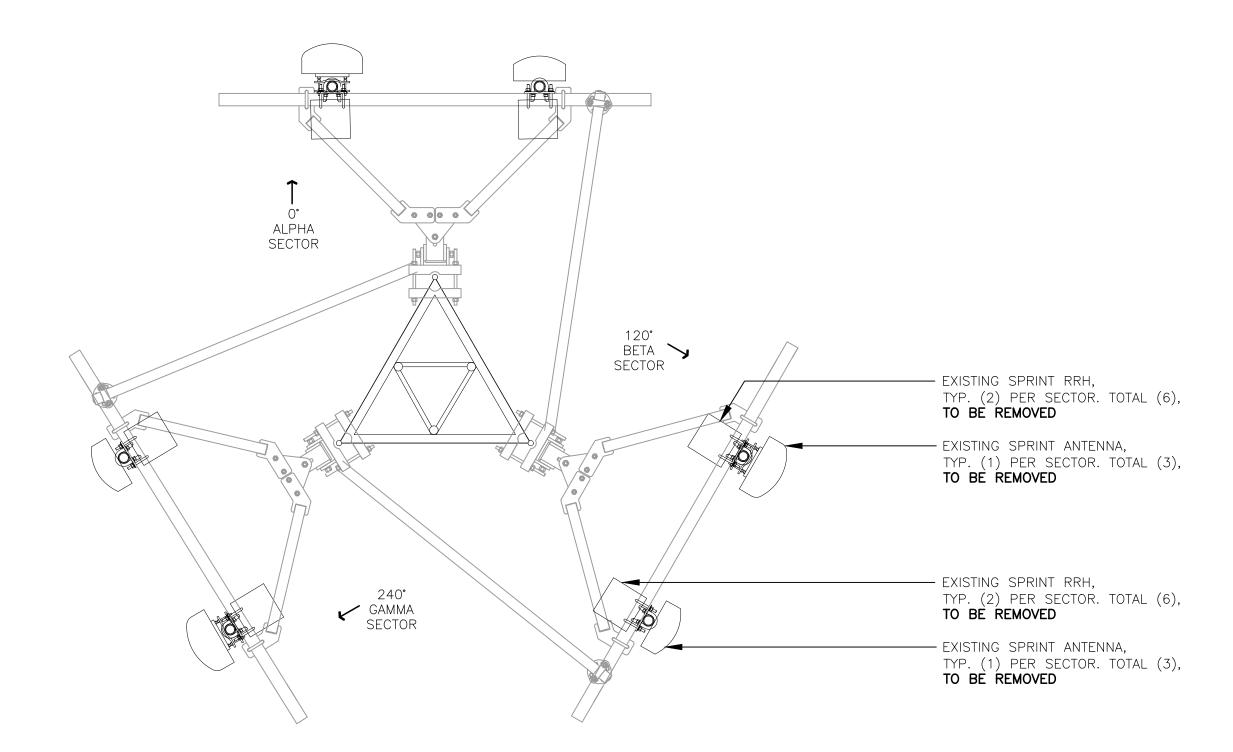




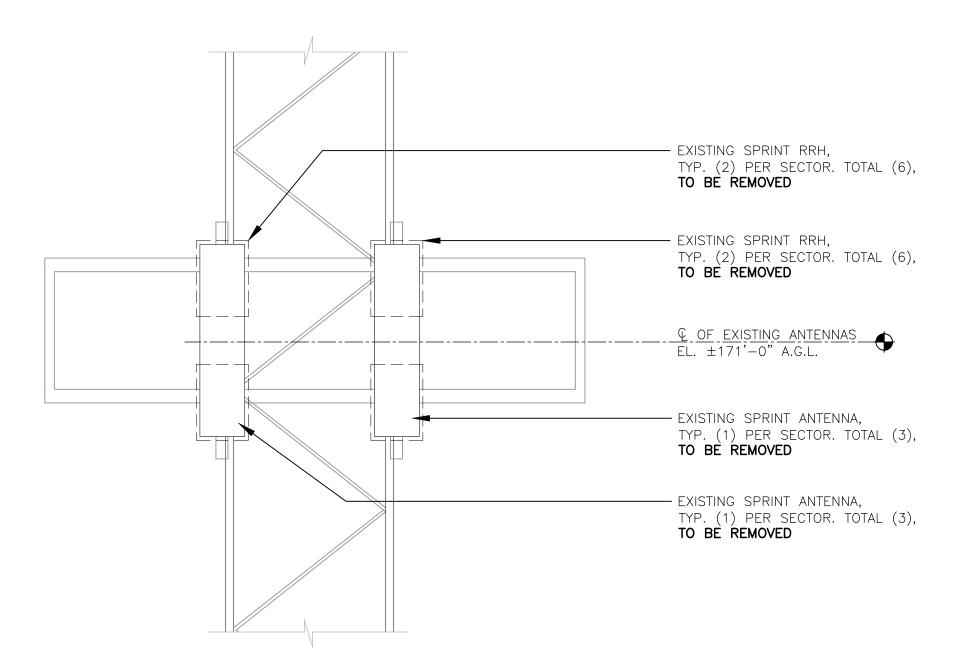


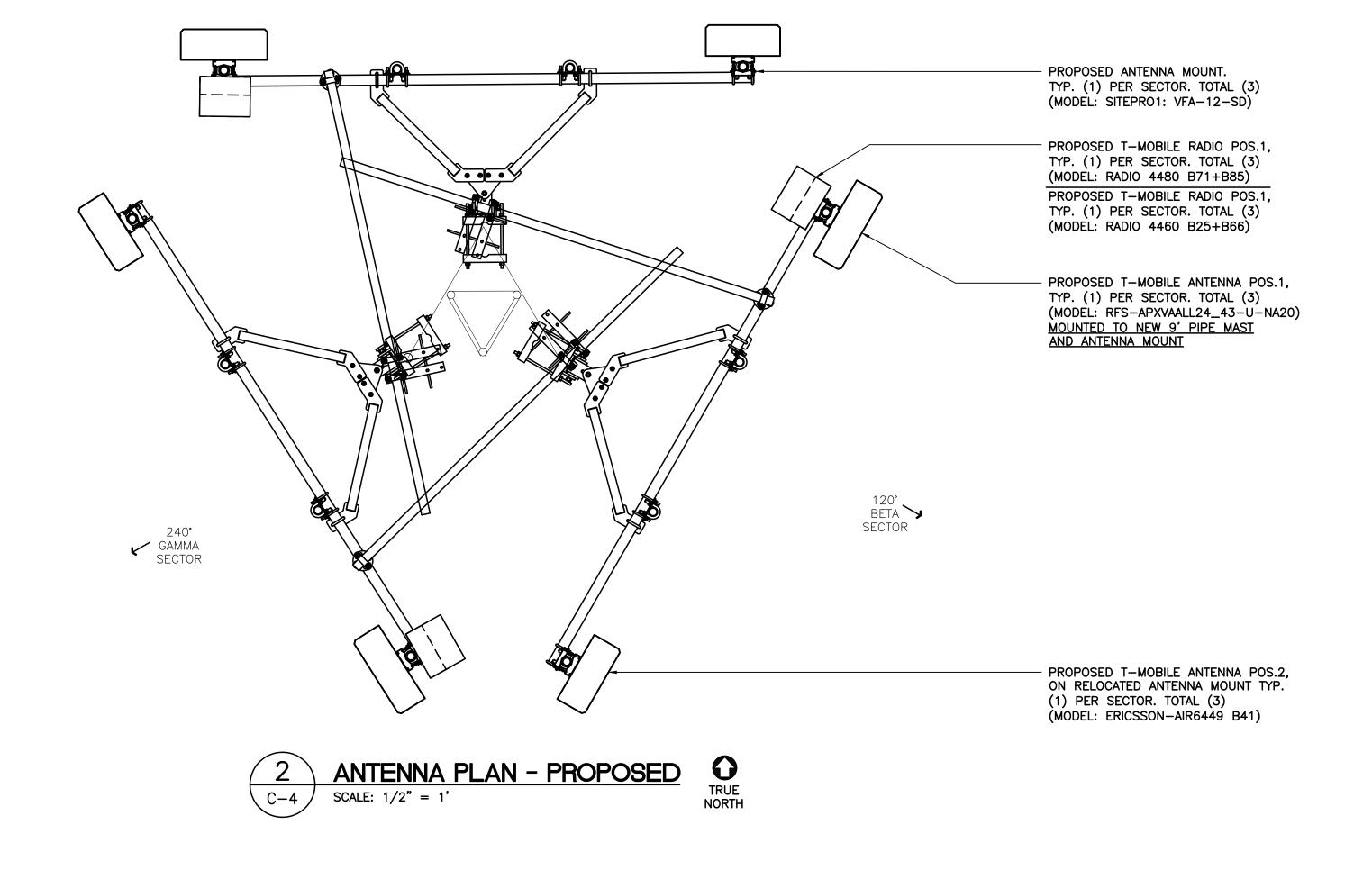
R TJR J T-MOBILE NORTHEAST LLC DATE: 04/22/21 SCALE: AS NOTED JOB NO. 21005.22 **EQUIPMENT PLANS** 

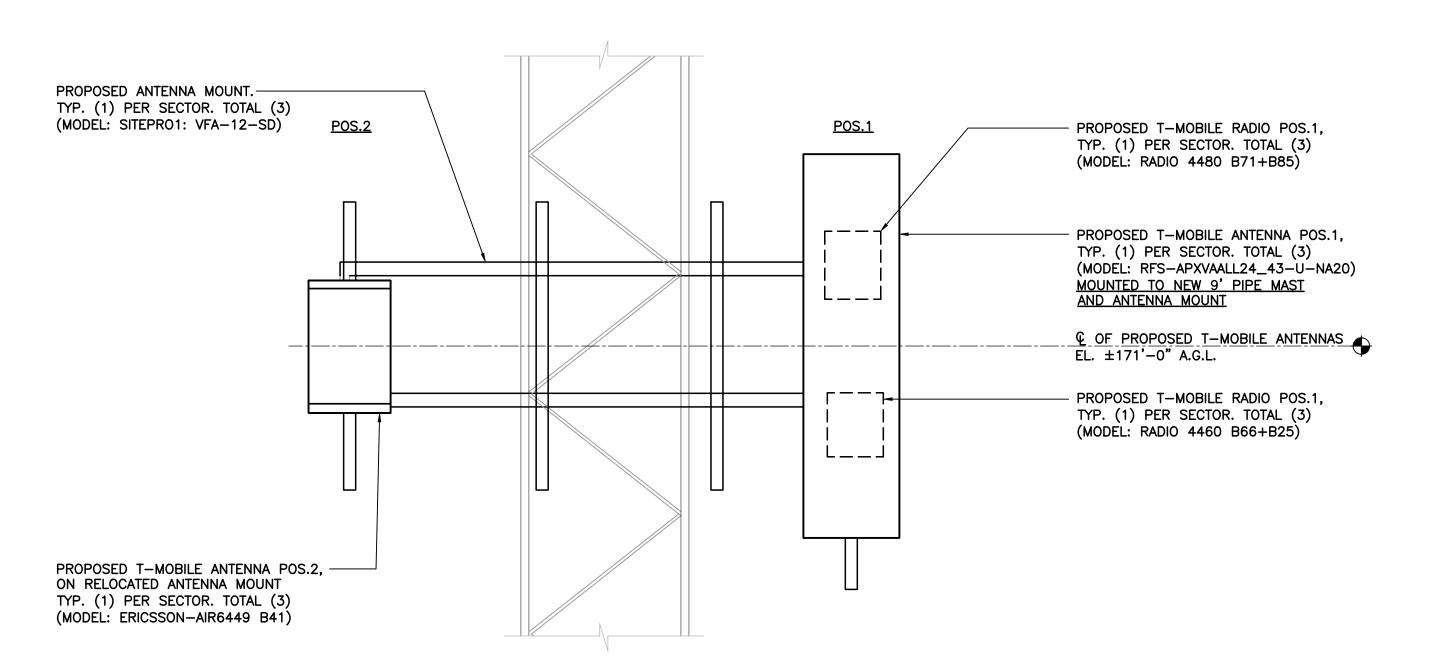
















3 02/07/21 RTS TJR CONSTRUCTION DRAWINGS – REVISED PER GENERATOR LOCATION
2 10/12/21 ANC TJR CONSTRUCTION DRAWINGS – REVISED COORDINATES PER AIRSPACE REPC
5 09/29/21 RTS TJR CONSTRUCTION DRAWINGS – REVISED STRUCTURAL COMPLIANCE NOTE
6 08/30/21 RTS TJR CONSTRUCTION DRAWINGS – REVISED PER NEW RFDS

Sprint > Men. T Mobile

(203) 488-0580 (203) 488-8587 Fax 63-2 North Branford Road Branford, CT 06405

T-MOBILE NORTHEAST LLC

NT ID: CT33XC553 E ID: CTHA830A 157 HAMPDEN RD

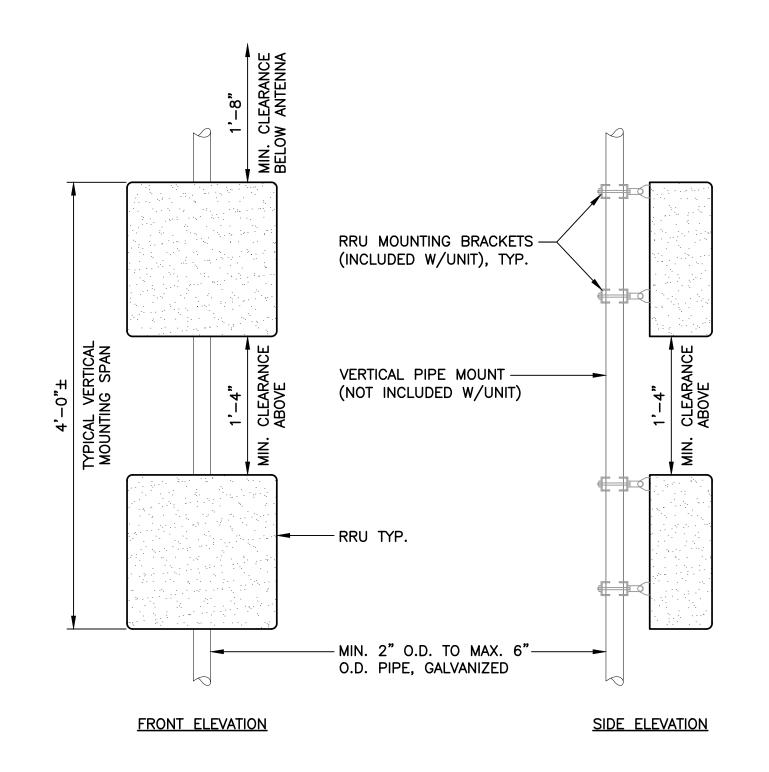
DATE: 04/22/21

SCALE: AS NOTED

JOB NO. 21005.22

ANTENNA PLANS AND ELEVATIONS

C-4



# END CAPS, (TYP) -\_\_ANCHOR/FASTENER, (TYP)

## NOTES: (PIPE MOUNTING)

- 1. T-MOBILE SHALL SUPPLY RRU, AND RRU POLE-MOUNTING BRACKET. CONTRACTOR SHALL SUPPLY POLE/PIPE AND INSTALL ALL MOUNTING HARDWARE INCLUDING ERICSSON RRU POLE-MOUNTING BRACKET.
- 2. NO PAINTING OF THE RRU OR SOLAR SHIELD IS ALLOWED.

**EQUIPMENT CABINET** 

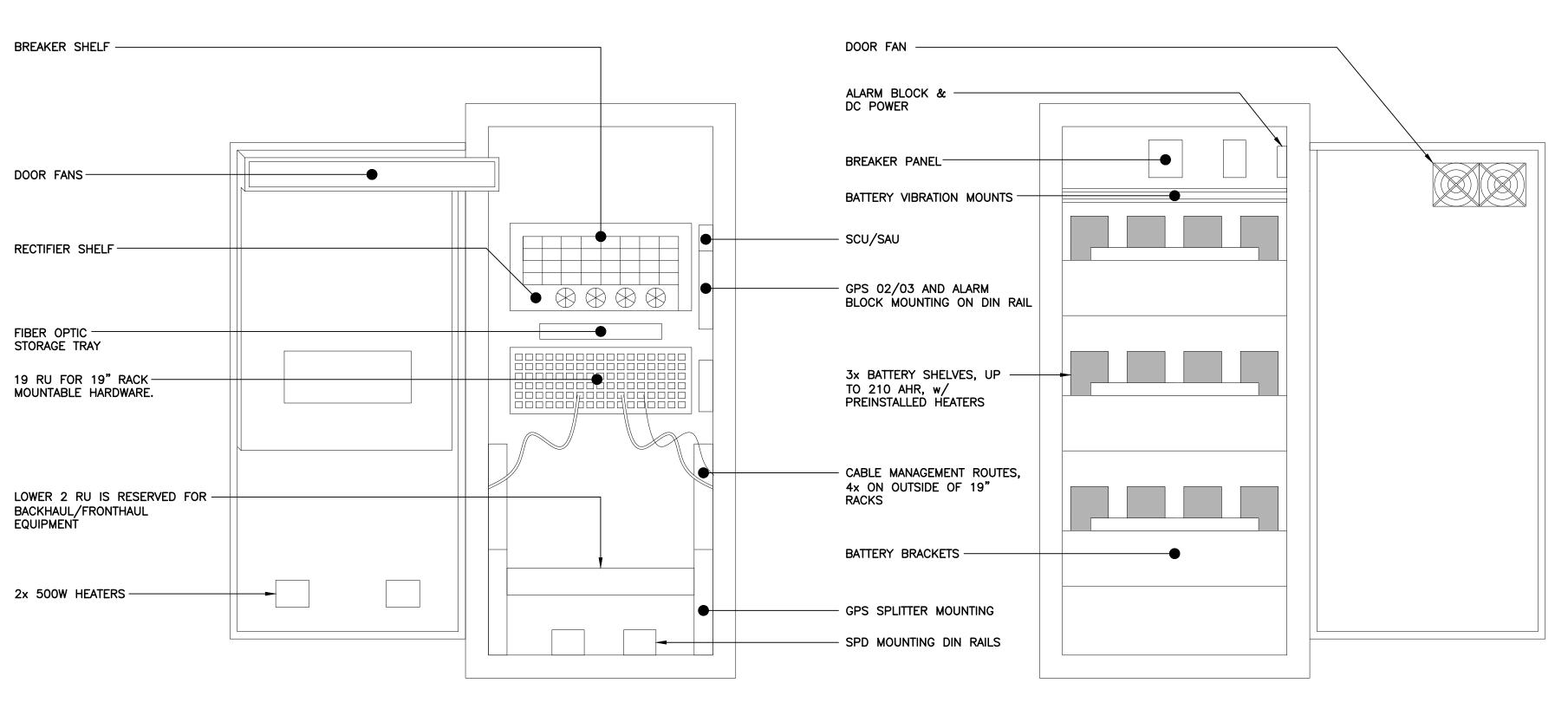
## NOTES: (UNISTRUT MOUNTING)

- 1. INSTALL A MINIMUM OF (2) ANCHORS PER UNISTRUT (± 16"o/c MIN).
- 2. MOUNT RRU TO UNISTRUT WITH 3/8" WINISTRUT BOLTING HARDWARE AND SPRING NUTS. TYPICAL FOUR PER BRACKET.

FRONT ELEVATION

3. NO PAINTING OF THE RRU OR SOLAR SHIELD IS ALLOWED.

# TYPICAL RRU MOUNTING DETAIL SCALE: NOT TO SCALE



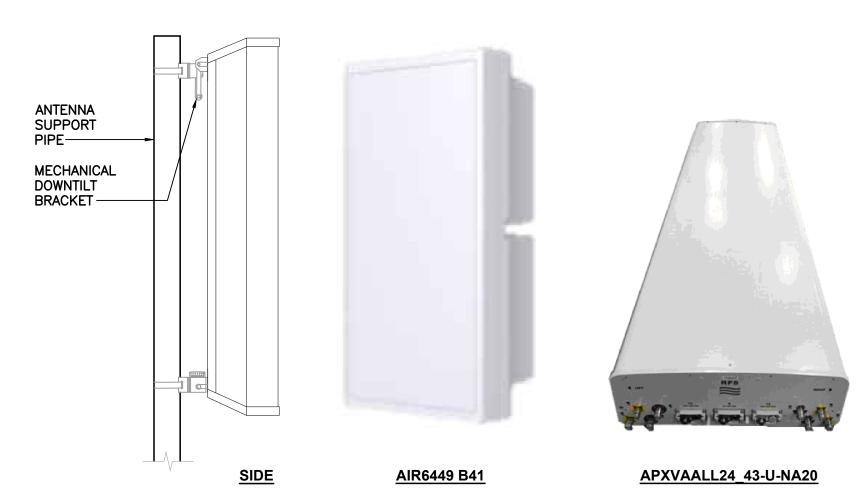
EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: ERICSSON MODEL: ENCLOSURE 6160 CABINET	62.0"H × 26.0"W × 26.0"D	±1200 LBS

SCALE: NOT TO SCALE

**ENCLOSURE 6160 CABINET DETAIL** 

## **EQUIPMENT CABINET EQUIPMENT DIMENSIONS** WEIGHT MAKE: ERICSSON MODEL: BATTERY B160 CABINET ±1883 LBS 62.0"H × 26.0"W × 26.0"D





	ALPHA	A/BETA/GAMMA ANTENNA	
	EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: ERICS: MODEL: AIR64	SON 49 B41	33.1"L × 20.6"W × 8.6"D	±104 LBS.
MAKE: RFS MODEL: APXVA	ALL24_43-U-NA20	95.9"L x 24.0"W x 8.5"D	±150 LBS.







RADIO 4460 B25+B66

RADIO 4480 B71+B85

	EQUIPMENT	DIMENSIONS	WEIGHT	CLEARANCES
MAKE: MODEL:	ERICSSON RADIO 4460 B25+B66	19.6"L x 15.7"W x 12.1"D	±109 LBS.	BEHIND ANT.: 8" MIN BELOW ANT.: 20" MIN BELOW RRU: 16" MIN
MAKE: MODEL:	ERICSSON RADIO 4480 B71+B85	21.8"L × 15.7"W × 7.5"D	±84 LBS.	BEHIND ANT.: 8" MIN BELOW ANT.: 20" MIN BELOW RRU: 16" MIN

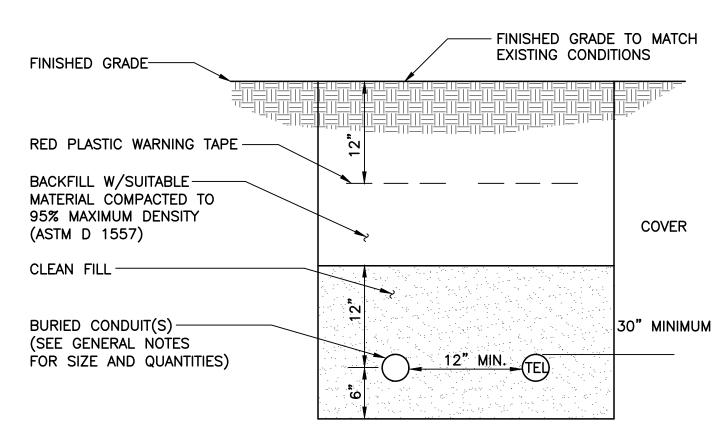


\\		PROFESSIONAL ENGINEER SEAL					
Centered on Solutions **		William William					
	Sprint Very T. Mobile:	THE CONNECTION OF THE PERSON O					
(202) 400 0500		IN THE CONTROL OF THE					
(203) 460-0360		がいる。					
(203) 400-0307 1 00 63-2 North Branford Road		2	3 0′	02/07/21	RTS	TJR	CONSTRUCTION DRAWINGS - REVISED PER GENERATOR LOCATION
Branford, CT 06405		A. 10.16694 O. I.	2 10	10/12/21	ANC	TJR	CONSTRUCTION DRAWINGS - REVISED COORDINATES PER AIRSPACE REPO
	Tellectrical National	The state of the s	8	09/29/21	RTS	TJR	CONSTRUCTION DRAWINGS - REVISED STRUCTURAL COMPLIANCE NOTE
		SONAL GOOD	0	08/30/21	RTS	TJR	CONSTRUCTION DRAWINGS - REVISED PER NEW RFDS
www.CentekEng.com			REV.	DATE	RAWN BY	снк'р ву	DRAWN BY CHK'D BY DESCRIPTION

T-MOBILE NORTHEAST LLC

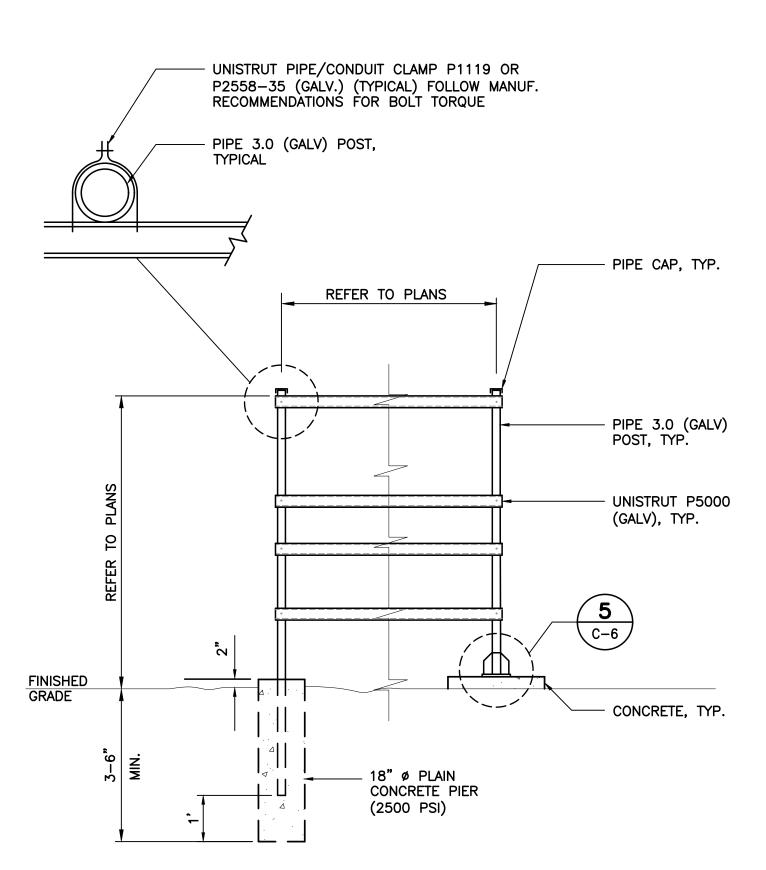
DATE: 04/22/21 SCALE: AS NOTED JOB NO. 21005.22 **TYPICAL** 

**EQUIPMENT DETAILS** 

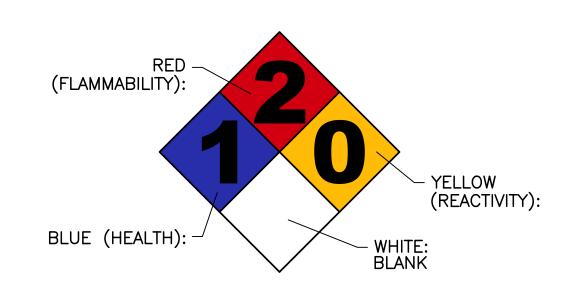


- 1. THE CLEAN FILL SHALL PASS THROUGH A 3/8" MESH SCREEN AND SHALL NOT CONTAIN SHARP STONES. OTHER BACKFILL SHALL NOT CONTAIN ASHES, CINDERS, SHELLS, FROZEN MATERIAL, LOOSE DEBRIS OR STONES LARGER THAN 2" IN MAXIMUM DIMENSION.
- 2. WHERE EXISTING UTILITIES ARE LIKELY TO BE ENCOUNTERED, CONTRACTOR SHALL HAND DIG AND PROTECT EXISTING UTILITIES.







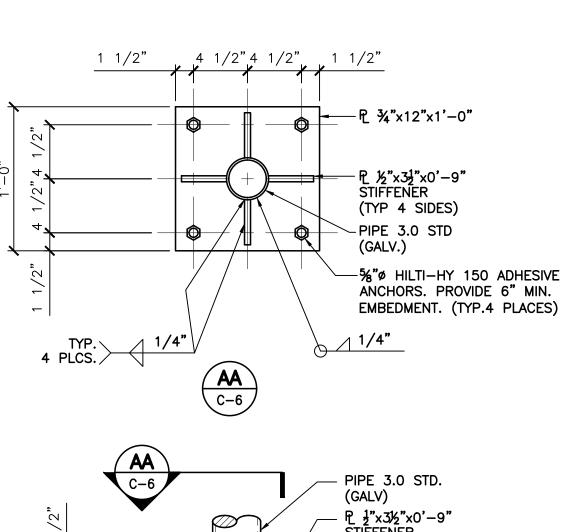


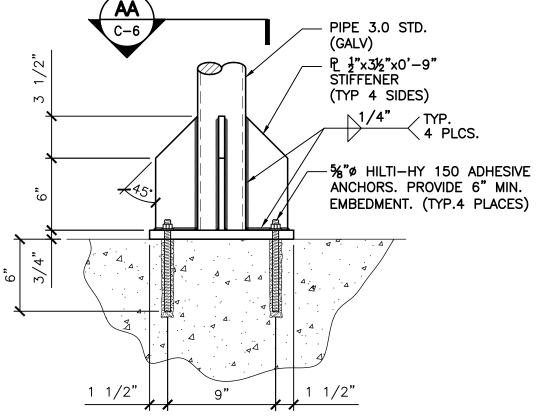
SIGN NAME: REGULATORY, NFPA 704 HAZARD ID

MOUNT ON GENERATOR ACCESS DOOR.
CONSULT WITH GENERATOR MANUFACTURER MSDS SHEET FOR BLUE AND RES POSITIONS DESCRIPTION: NOTES:

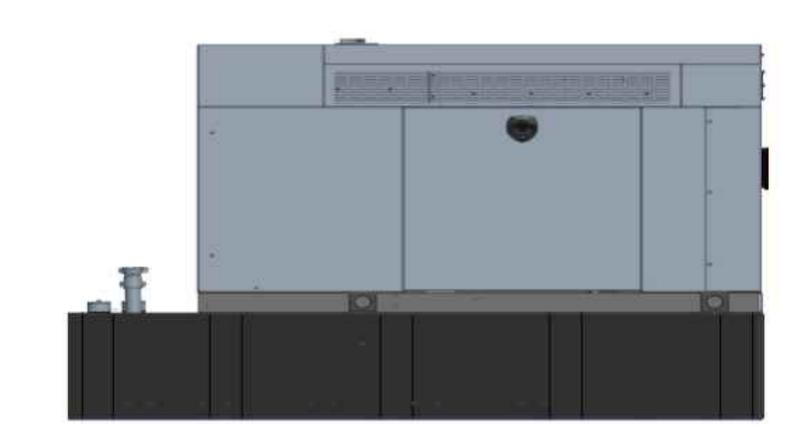
- 1) SIGNS EXPOSED TO WEATHER SHOULD BE CHECKED ANNUALLY FOR READABILITY.
- 2) SIGNS MUST BE UPDATED IF CHEMICAL STORAGE OR HAZARD INFORMATION FOR THE LOCATION CHANGES.
- 3) THE GC MUST REVIEW WITH LOCAL JURISDICTION WHEN FILLING FOR PERMITS, AS EACH JURISDICTION MAY HAVE DIFFERENT REQUIREMENTS AND COMPLY WITH POSTING REQUIREMENTS OR DIRECTIVES FROM THE LOCAL JURISDICTION.







FRAME TO CONCRETE CONNECTION DETAIL SCALE: NOT TO SCALE



			BACKUP POWER G	SENERATOR		
EQUIPMENT	POWER GENERATED	FUEL	MODEL NUMBER	FUEL TANK SIZE (GAL)	DIMENSIONS	WEIGHT
MAKE: GENERAC MODEL: RD48	48 KW, AC	DIESEL	7194	229	103.4"L x 35.0"W x 91.7"H	2915 LBS.

1. FUEL LEVEL/SECONDARY CONTAINMENT SHALL BE ALARMED AND IN COMMUNICATION WITH T-MOBILE'S

2. CONTRACTOR TO COORDINATE FINAL EQUIPMENT MODEL SELECTION AND ALL OPTIONAL FEATURES WITH T-MOBILE'S CONSTRUCTION MANAGER PRIOR TO ORDERING.





		AUT	OMATIC TRANSFER SWIT	СН	
EQUIPMENT	PHASE	VOLTAGE	ENCLOSURE	AMP	DIMENSIONS
MAKE: GENERAC MODEL: RXSC200A3	1-PHASE	120/240	NEMA-3R	200	17.3"L x 12.5"W



	•				10000000000000000000000000000000000000
CONSTRUCTION DRAWINGS - REVISED PER NEW RFDS	TJR	RTS	08/30/21	0	WAL ENGLAND
CONSTRUCTION DRAWINGS - REVISED STRUCTURAL COMPLIANCE NOTE	TJR	RTS	09/29/21	1	NO. TO STATE OF THE PARTY OF TH
CONSTRUCTION DRAWINGS - REVISED COORDINATES PER AIRSPACE R	TJR	ANC	10/12/21	2	116694
CONSTRUCTION DRAWINGS - REVISED PER GENERATOR LOCATION	TJR	RTS	02/07/21	3	Carlos Carlos
					NO RE
					CENTON
					NAME OF THE PARTY
					William Comment
					4
					. ENGINEER SEAL

(203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203) (203)

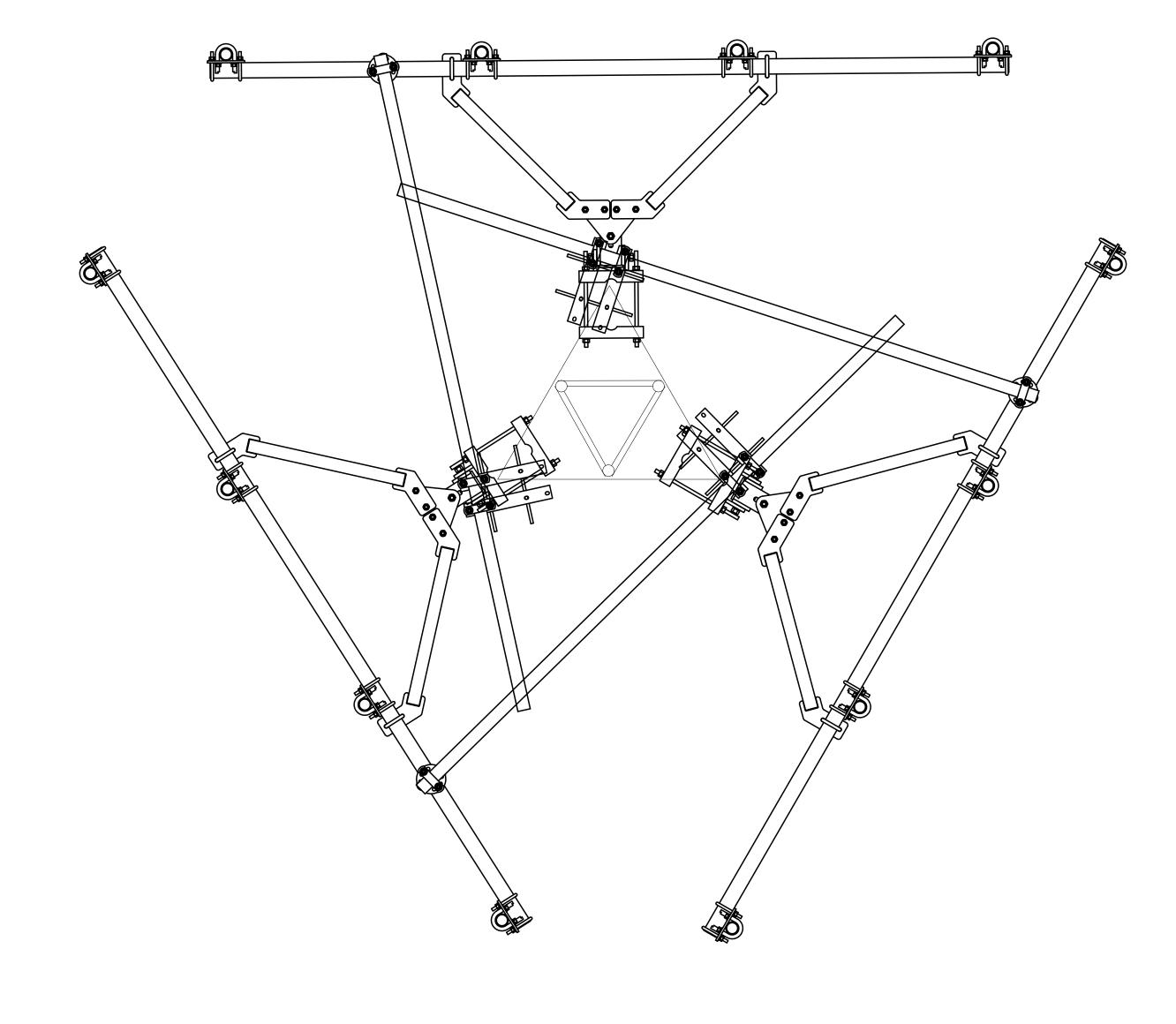
YII ZIII

NORTHEAST LLC T-MOBILE

04/22/21 SCALE: AS NOTED JOB NO. 21005.22 **TYPICAL** 

> **EQUIPMENT DETAILS**

Sheet No. <u>8</u> of <u>12</u>



SITEPRO1: VFA-12-SD

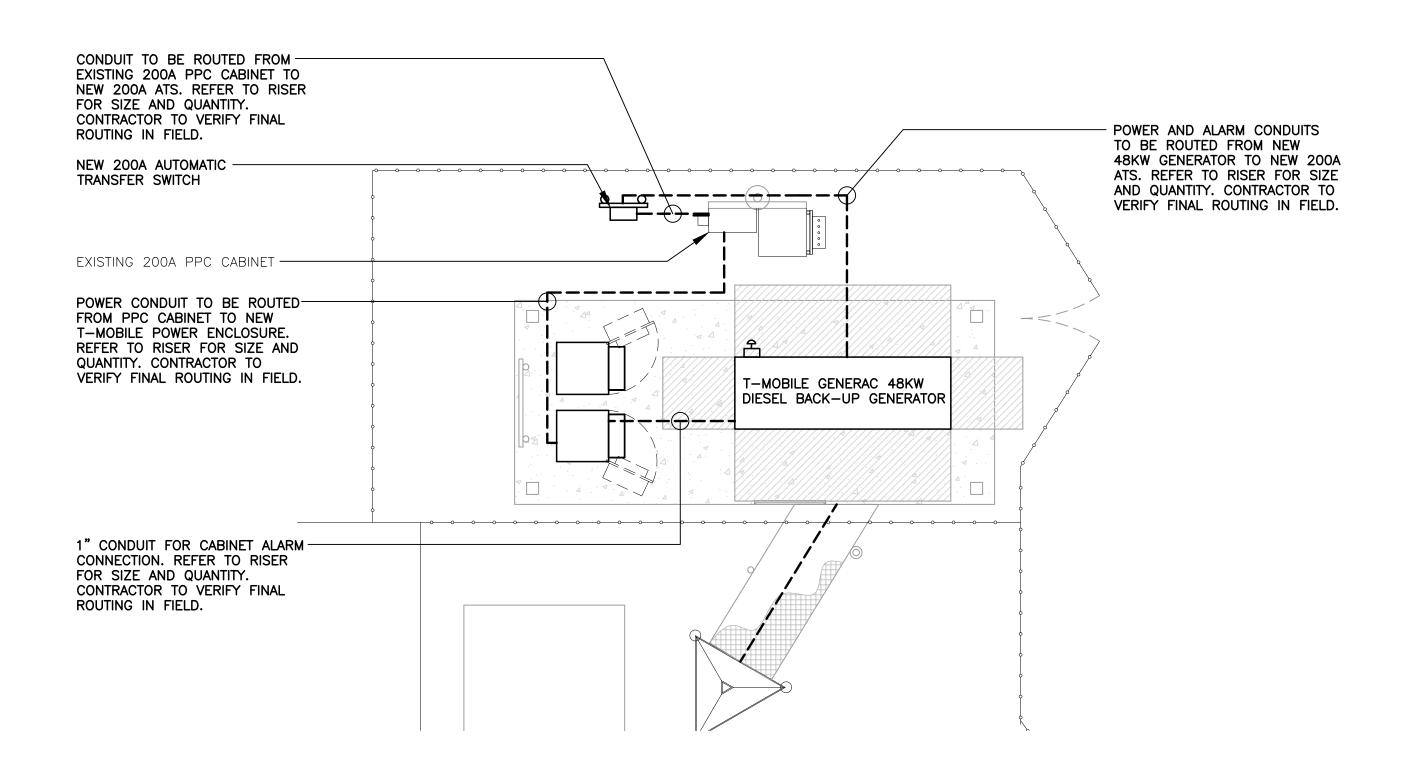
TYPICAL ANTENNA MOUNT DETAIL

SCALE: NOT TO SCALE

Centered on Solutions\*\* SPRINT ID: CT33XC553
SITE ID: CTHA830A
157 HAMPDEN RD
STAFFORD SPRINGS, CT 06076 T-MOBILE NORTHEAST LLC DATE: 04/22/21
SCALE: AS NOTED JOB NO. 21005.22 STRUCTURAL DETAILS

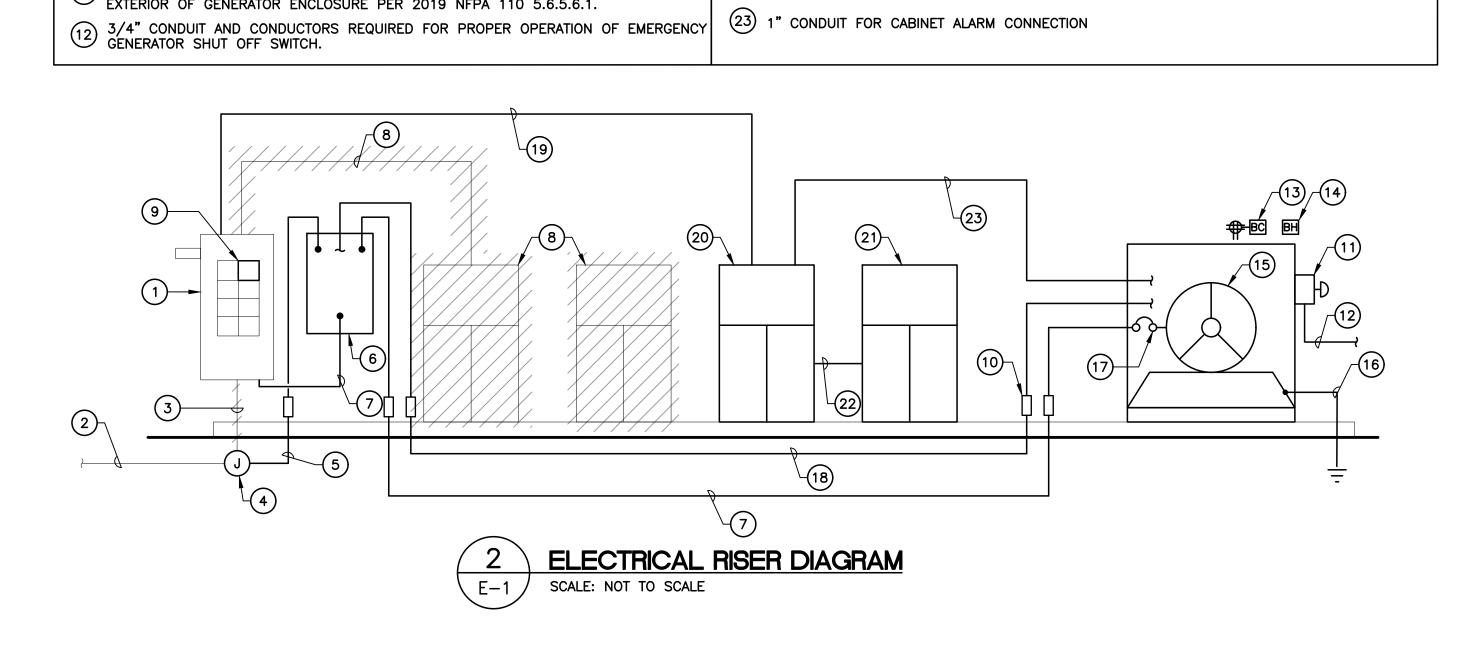
S-1

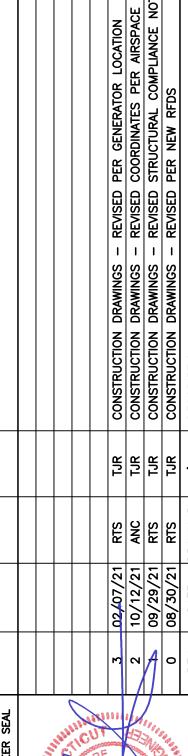
Sheet No. <u>9</u> of <u>12</u>



1 ELECTRICAL CONDUIT ROUTING PLAN
SCALE: 1/4" = 1'

## RISER DIAGRAM NOTES RISER DIAGRAM NOTES GENERATOR BATTERY CHARGER AND CONVENIENCE GFCI OUTLET WIRED TO EXISTING PANEL. OUTLET TO BE MOUNTED IN WEATHERPROOF ENCLOSURE. (1) EXISTING PPC CABINET TO REMAIN. 2 EXISTING POWER CONDUIT AND CONDUCTORS PREVIOUSLY SERVING EXISTING PANEL. (14) GENERATOR BLOCK HEATER WIRED TO EXISTING PANEL SERVING T-MOBILE EQUIPMENT. 3 SECTION OF CONDUIT AND CONDUCTORS TO BE REMOVED. 15) EMERGENCY BACK UP GENERATOR. GENERATOR GROUNDING PER NEC AND MANUFACTURER'S REQUIREMENTS. BOND TO EXISTING GROUNDING SYSTEM. (MINIMUM OF (1) #2 AWG GROUND) 4 JUNCTION BOX SIZED PER NEC. 5 EXTEND EXISTING CONDUITS AND CONDUCTORS TO NEW ATS. (17) GENERATOR OUTPUT CIRCUIT BREAKER. (6) NEW 200A, 2 SOURCE AUTOMATIC TRANSFER SWITCH. (18) 1" CONDUIT FOR GENERATOR CONTROL AND SIGNAL WIRING. 7 (3) #3/0 AWG, (1) #6 AWG GROUND, 2-1/2" CONDUIT. (19) (1) 1/0 AWG, (1) #6 AWG GROUND, 1-1/2" CONDUIT. 8 EXISTING CABINETS AND ASSOCIATED CONDUITS, CONDUCTORS AND CIRCUIT BREAKERS TO BE REMOVED 20 NEW T-MOBILE EQUIPMENT CABINET 9) NEW 150A/2P CIRCUIT BREAKER TO SERVE NEW EQUIPMENT. 21) NEW T-MOBILE BATTERY CABINET (10) EXPANSION COUPLING TYPICAL. DC CONDUIT AND CONDUCTORS FOR BATTERY CABINET CONNECTION PER REMOTE GENERATOR SHUT OFF SWITCH IN BREAK GLASS ENCLOSURE MOUNTED TO EXTERIOR OF GENERATOR ENCLOSURE PER 2019 NFPA 110 5.6.5.6.1. MANUFACTURERS SPECIFICATIONS.





int > Mean The Mobile Conversion of Conversi

203) 488-0580 203) 488-8587 Fax 3-2 North Branford Road ranford, CT 06405

E NORTHEAST LLC
ID: CT33XC553

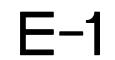
SPRINT ID: CT33
SITE ID: CTHA

DATE: 04/22/21

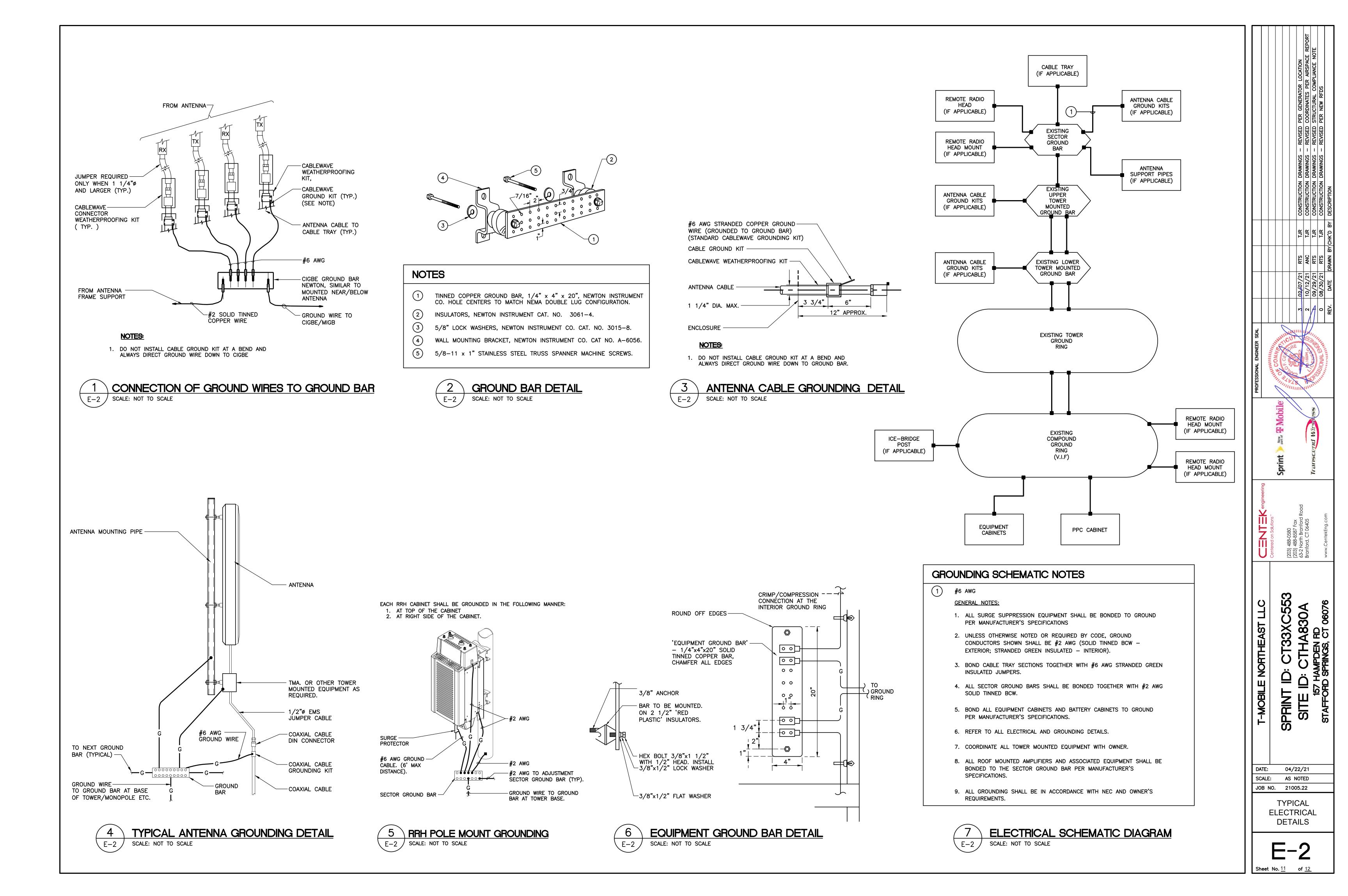
SCALE: AS NOTED

JOB NO. 21005.22

ELECTRICAL RISER
DIAGRAM AND
CONDUIT ROUTING



Sheet No. 10 of 12



## **ELECTRICAL SPECIFICATIONS**

## **SECTION 16010**

1.02. GENERAL REQUIREMENTS

- A. THE ENTIRE ELECTRICAL INSTALLATION SHALL BE MADE IN STRICT ACCORDANCE WITH ALL LOCAL, STATE AND NATIONAL CODES AND REGULATIONS WHICH MAY APPLY AND NOTHING IN THE DRAWINGS OR SPECIFICATIONS SHALL BE INTERPRETED AS AN INFRINGEMENT OF SUCH CODES OR REGULATIONS.
- B. THE ELECTRICAL CONTRACTOR IS TO BE RESPONSIBLE FOR THE COMPLETE INSTALLATION AND COORDINATION OF THE ENTIRE ELECTRICAL SERVICE. ALL ACTIVITIES TO BE COORDINATED THROUGH OWNERS REPRESENTATIVE, DESIGN ENGINEER AND OTHER AUTHORITIES HAVING JURISDICTION OF TRADES.
- C. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND PAY ALL FEES THAT MAY BE REQUIRED FOR THE ELECTRICAL WORK AND FOR THE SCHEDULING OF ALL INSPECTIONS THAT MAY BE REQUIRED BY THE LOCAL AUTHORITY.
- D. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATION WITH THE BUILDING OWNER FOR NEW AND/OR DEMOLITION WORK INVOLVED.
- E. NO MATERIAL OTHER THAN THAT CONTAINED IN THE "LATEST LIST OF ELECTRICAL FITTINGS" APPROVED BY THE UNDERWRITERS' LABORATORIES, SHALL BE USED IN ANY PART OF THE WORK. ALL MATERIAL FOR WHICH LABEL SERVICE HAS BEEN ESTABLISHED SHALL BEAR THE U.L. LABEL.
- F. THE CONTRACTOR SHALL GUARANTEE ALL NEW WORK FOR A PERIOD OF ONE YEAR FROM THE ACCEPTANCE DATE BY THE OWNER. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING WARRANTIES FROM ALL EQUIPMENT MANUFACTURERS FOR SUBMISSION TO THE OWNER.
- G. DRAWINGS INDICATE GENERAL ARRANGEMENT OF WORK INCLUDED IN CONTRACT. CONTRACTOR SHALL, WITHOUT EXTRA CHARGE, MAKE MODIFICATIONS TO THE LAYOUT OF THE WORK TO PREVENT CONFLICT WITH WORK OF OTHER TRADES AND FOR THE PROPER INSTALLATION OF WORK. CHECK ALL DRAWINGS AND VISIT JOB SITE TO VERIFY SPACE AND TYPE OF EXISTING CONDITIONS IN WHICH WORK WILL BE DONE, PRIOR TO SUBMITTAL OF BID.
- H. THE ELECTRICAL CONTRACTOR SHALL SUPPLY THREE (3) COMPLETE SETS OF APPROVED DRAWINGS, ENGINEERING DATA SHEETS, MAINTENANCE AND OPERATING INSTRUCTION MANUALS FOR ALL SYSTEMS AND THEIR RESPECTIVE EQUIPMENT. THESE MANUALS SHALL BE INSERTED IN VINYL COVERED 3—RING BINDERS AND TURNED OVER TO OWNER'S REPRESENTATIVE ONE (1) WEEK PRIOR TO FINAL PUNCH LIST.
- I. ALL WORK SHALL BE INSTALLED IN A NEAT AND WORKMAN LIKE MANNER AND WILL BE SUBJECT TO THE APPROVAL OF THE OWNER'S REPRESENTATIVE.
- J. ALL EQUIPMENT AND MATERIALS TO BE INSTALLED SHALL BE NEW, UNLESS OTHERWISE NOTED.
- K. BEFORE FINAL PAYMENT, THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF PRINTS (AS-BUILTS), LEGIBLY MARKED IN RED PENCIL TO SHOW ALL CHANGES FROM THE ORIGINAL PLANS.
- L. PROVIDE TEMPORARY POWER AND LIGHTING IN WORK AREAS AS REQUIRED.
- M. SHOP DRAWINGS:
- 1. CONTRACTOR SHALL SUBMIT SIX (6) COPIES OF SHOP DRAWINGS ON ALL EQUIPMENT AND MATERIALS PROPOSED FOR USE ON THIS PROJECT, GIVING ALL DETAILS, WHICH INCLUDE DIMENSIONS, CAPACITIES, ETC.
- 2. CONTRACTOR SHALL SUBMIT SIX (6) COPIES OF ALL TEST REPORTS CALLED FOR IN THE SPECIFICATIONS AND DRAWINGS.
- N. THE ENTIRE ELECTRICAL INSTALLATION SHALL BE IN ACCORDANCE WITH OWNER'S SPECIFICATIONS, AND REQUIREMENTS OF ALL LOCAL AUTHORITIES HAVING JURISDICTION. IT IS THE CONTRACTOR'S RESPONSIBILITY TO COORDINATE WITH APPROPRIATE INDIVIDUALS TO OBTAIN ALL SUCH SPECIFICATIONS AND REQUIREMENTS. NOTHING CONTAINED IN. OR OMITTED FROM. THESE DOCUMENTS SHALL RELIEVE CONTRACTOR FROM THIS OBLIGATION.

## SECTION 16111

1.01. CONDUITS

- A. MINIMUM CONDUIT SIZE FOR BRANCH CIRCUITS, LOW VOLTAGE CONTROL AND ALARM CIRCUITS SHALL BE 3/4". CONDUITS SHALL BE PROPERLY FASTENED AS REQUIRED BY THE N.E.C.
- B. THE INTERIOR OF RACEWAYS/ENCLOSURES INSTALLED UNDERGROUND SHALL BE CONSIDERED TO BE WET LOCATION, INSULATED CONDUCTORS SHALL BE LISTED FOR USE IN WET LOCATIONS. PROVIDE WEATHERPROOF CONSTRUCTION IN WET LOCATIONS.
- C. CONDUIT INSTALLED UNDERGROUND SHALL BE INSTALLED TO MEET MINIMUM COVER REQUIREMENTS OF TABLE 300.5.
- D. PROVIDE RIGID GALVANIZED STEEL CONDUIT (RMC) FOR THE FIRST 10 FOOT SECTION WHEN LEAVING A BUILDING OR SECTIONS PASSING THROUGH FLOOR SLABS
- E. ONLY LISTED PVC CONDUIT AND FITTINGS ARE PERMITTED FOR THE INSTALLATION OF ELECTRICAL CONDUCTORS, SUITABLE FOR UNDERGROUND APPLICATIONS.

	CONDUI	T SCHEDULE SECTION 16111	
CONDUIT TYPE	NEC REFERENCE	APPLICATION	MIN. BURIAL DEPTH (PER NEC TABLE 300.5) <sup>2,3</sup>
ЕМТ	ARTICLE 358	INTERIOR CIRCUITING, EQUIPMENT ROOMS, SHELTERS	N/A
RMC, RIGID GALV. STEEL	ARTICLE 344, 300.5, 300.50	ALL INTERIOR/ EXTERIOR CIRCUITING, ALL UNDERGROUND INSTALLATIONS.	6 INCHES
PVC, SCHEDULE 40	ARTICLE 352, 300.5, 300.50	INTERIOR/ EXTERIOR CIRCUITING AND GROUNDING SYSTEMS, UNDERGROUND INSTALLATIONS, WHERE NOT SUBJECT TO PHYSICAL DAMAGE. 1	18 INCHES
PVC, SCHEDULE 80	ARTICLE 352, 300.5, 300.50	INTERIOR/ EXTERIOR CIRCUITING AND GROUNDING SYSTEMS, UNDERGROUND INSTALLATIONS, WHERE SUBJECT TO PHYSICAL DAMAGE. 1	18 INCHES
LIQUID TIGHT FLEX. METAL	ARTICLE 350	SHORT LENGTHS (MAX. 3FT.) WIRING TO VIBRATING EQUIPMENT IN WET LOCATIONS.	N/A
FLEX. METAL	ARTICLE 348	SHORT LENGTHS (MAX. 3FT.) WIRING TO VIBRATING EQUIPMENT IN WET LOCATIONS.	N/A
1 DUVETON DAMACE TO CL	ID IFOT TO THE AUTHO	IDITY HAV/INC HIDIODICTION	

1 PHYSICAL DAMAGE IS SUBJECT TO THE AUTHORITY HAVING JURISDICTION.

<sup>2</sup> UNDERGROUND CONDUIT INSTALLED UNDER ROADS, HIGHWAYS, DRIVEWAYS, PARKING LOTS SHALL HAVE MINIMUM DEPTH OF 24".

<sup>3</sup> WHERE SOLID ROCK PREVENTS COMPLIANCE WITH MINIMUM COVER DEPTHS, WIRING SHALL BE INSTALLED IN PERMITTED RACEWAY FOR DIRECT BURIAL. THE RACEWAY SHALL BE COVERED BY A MINIMUM OF 2" OF CONCRETE EXTENDING DOWN TO ROCK.

## **SECTION 16123**

1.01. CONDUCTORS

A. ALL CONDUCTORS SHALL BE TYPE THWN (INT. APPLICATION) AND XHHW (EXT. APPLICATION), 75 DEGREE C, 600 VOLT INSULATION, SOFT ANNEALED STRANDED COPPER. #10 AWG AND SMALLER SHALL BE SPLICED USING ACCEPTABLE SOLDERLESS PRESSURE CONNECTORS. #8 AWG AND LARGER SHALL BE SPLICED USING COMPRESSION SPLIT—BOLT TYPE CONNECTORS. #12 AWG SHALL BE THE MINIMUM SIZE CONDUCTOR FOR LINE VOLTAGE BRANCH CIRCUITS. REFER TO PANEL SCHEDULE FOR BRANCH CIRCUIT CONDUCTOR SIZE(S). CONDUCTORS SHALL BE COLOR CODED FOR CONSISTENT PHASE IDENTIFICATION:

120/208/240V 277/480V

LINE COLOR
A BLACK BROWN
B RED ORANGE
C BLUE YELLOW
N CONTINUOUS WHITE GREY
G CONTINUOUS GREEN GREEN WITH YELLOW STRIPE

B. MINIMUM BENDING RADIUS FOR CONDUCTORS SHALL BE 12 TIMES THE LARGEST DIAMETER OF BRANCH CIRCUIT CONDUCTOR.

## **SECTION 16130**

1.01. BOXES

- A. FURNISH AND INSTALL OUTLET BOXES FOR ALL DEVICES, SWITCHES, RECEPTACLES, ETC.. BOXES TO BE ZINC COATED STEEL.
- B. FURNISH AND INSTALL PULL BOXES IN MAIN FEEDERS RUNS WHERE REQUIRED. PULL BOXES SHALL BE GALVANIZED STEEL WITH SCREW REMOVABLE COVERS, SIZE AND QUANTITY AS REQUIRED. PROVIDE WEATHERPROOF CONSTRUCTION IN WET LOCATIONS.

## <u>SECTION 16140</u>

1.01. WIRING DEVICES

- A. THE FOLLOWING LIST IS PROVIDED TO CONVEY THE QUALITY AND RATING OF WIRING DEVICES WHICH ARE TO BE INSTALLED. A COMPLETE LIST OF ALL DEVICES MUST BE SUBMITTED BEFORE INSTALLATION FOR APPROVAL.
- 1. 15 MINUTE TIMER SWITCH INTERMATIC #FF15M (INTERIOR LIGHTS)
- 2. DUPLEX RECEPTACLE P&S #2095 (GFCI) SPECIFICATION GRADE
- 3. SINGLE POLE SWITCH P&S #CSB20AC2 (20A-120V HARD USE) SPECIFICATION GRADE
- 4. DUPLEX RECEPTACLE P&S #5362 (20A-120V HARD USE) SPECIFICATION GRADE
- B. PLATES ALL PLATES USED SHALL BE CORROSION RESISTANT TYPE 304 STAINLESS STEEL. PLATES SHALL BE FROM SAME MANUFACTURER AS SWITCHES AND RECEPTACLES. PROVIDE WEATHERPROOF HOUSING FOR DEVICES LOCATED IN WET LOCATIONS.
- C. OTHER MANUFACTURERS OF THE SWITCHES, RECEPTACLES AND PLATES MAY BE SUBMITTED FOR APPROVAL BY THE ENGINEER.

## **SECTION 16170**

1.01. DISCONNECT SWITCHES

A. FUSIBLE AND NON-FUSIBLE, 600V, HEAVY DUTY DISCONNECT SWITCHES SHALL BE AS MANUFACTURED BY SQUARE "D". PROVIDE FUSES AS CALLED FOR ON THE CONTRACT DRAWINGS. AMPERE RATING SHALL BE CONSISTENT WITH LOAD BEING SERVED. DISCONNECT SWITCH COVER SHALL BE MECHANICALLY INTERLOCKED TO PREVENT COVER FROM OPENING WHEN THE SWITCH IS IN THE "ON" POSITION. EXTERIOR APPLICATIONS SHALL BE NEMA 3R CONSTRUCTION WITH PADLOCK FEATURE.

## SECTION 16190

1.01. SEISMIC RESTRAINT

A. ALL DEVICES SHALL BE INSTALLED IN ACCORDANCE WITH ZONE 2 SEISMIC REQUIREMENTS.

## **SECTION 16195**

- 1.01. LABELING AND IDENTIFICATION NOMENCLATURE FOR ELECTRICAL EQUIPMENT
- A. CONTRACTOR SHALL FURNISH AND INSTALL NON-METALLIC ENGRAVED BACK-LIT NAMEPLATES ON ALL PANELS AND MAJOR ITEMS OF ELECTRICAL EQUIPMENT.
- B. LETTERS TO BE WHITE ON BLACK BACKGROUND WITH LETTERS 1-1/2 INCH HIGH WITH 1/4 INCH MARGIN.
- C. IDENTIFICATION NOMENCLATURE SHALL BE IN ACCORDANCE WITH OWNER'S STANDARDS.

## **SECTION 16450**

1.01. GROUNDING

- A. ALL NON-CURRENT CARRYING PARTS OF THE ELECTRICAL AND TELEPHONE CONDUIT SYSTEMS SHALL BE MECHANICALLY AND ELECTRICALLY CONNECTED TO PROVIDE AN INDEPENDENT RETURN PATH TO THE EQUIPMENT GROUNDING SOURCES.
- B. GROUNDING SYSTEM WILL BE IN ACCORDANCE WITH THE LATEST ACCEPTABLE EDITION OF THE NATIONAL ELECTRICAL CODE AND REQUIREMENTS PER LOCAL INSPECTOR HAVING JURISDICTION.
- C. GROUNDING OF PANELBOARDS:
- 1. PANELBOARD SHALL BE GROUNDED BY TERMINATING THE PANELBOARD FEEDER'S EQUIPMENT GROUND CONDUCTOR TO THE EQUIPMENT GROUND BAR KIT(S) LUGGED TO THE CABINET. ENSURE THAT THE SURFACE BETWEEN THE KIT AND CABINET ARE BARE METAL TO BARE METAL. PRIME AND PAINT OVER TO PREVENT CORROSION.
- 2. CONDUIT(S) TERMINATING INTO THE PANELBOARD SHALL HAVE GROUNDING TYPE BUSHINGS. THE BUSHINGS SHALL BE BONDED TOGETHER WITH BARE #10 AWG COPPER CONDUCTOR WHICH IN TURN IS TERMINATED INTO THE PANELBOARD'S EQUIPMENT GROUND BAR KIT(S).
- D. EQUIPMENT GROUNDING CONDUCTOR:
- 1. EACH EQUIPMENT GROUND CONDUCTOR SHALL BE SIZED IN ACCORDANCE WITH THE N.E.C. ARTICLE 250-122.
- 2. THE MINIMUM SIZE OF EQUIPMENT GROUND CONDUCTOR SHALL BE #12 AWG COPPER.
- 3. EACH FEEDER OR BRANCH CIRCUIT SHALL HAVE EQUIPMENT GROUND CONDUCTOR(S) INSTALLED IN THE SAME RACEWAY(S).
- E. CELLULAR GROUNDING SYSTEM:

CONTRACTOR SHALL PROVIDE A CELLULAR GROUNDING SYSTEM WITH THE MAXIMUM AC RESISTANCE TO GROUND OF 10 OHM BETWEEN ANY POINT ON THE GROUNDING SYSTEM AS MEASURED BY 3-POINT GROUNDING TEST. (REFER TO SECTION 16960).

PROVIDE THE CELLULAR GROUNDING SYSTEM AS SPECIFIED ON DRAWINGS, INCLUDING, BUT NOT LIMITED TO:

- 1. GROUND BARS
- 2. EXTERIOR GROUNDING (WHERE REQUIRED DUE TO MEASURED AC RESISTANCE GREATER THAN SPECIFIED).
- 3. ANTENNA GROUND CONNECTIONS AND PLATES.
- F. CONTRACTOR, AFTER COMPLETION OF THE COMPLETE GROUNDING SYSTEM BUT PRIOR TO CONCEALMENT/BURIAL OF SAME, SHALL NOTIFY OWNER'S PROJECT ENGINEER WHO WILL HAVE A DESIGN ENGINEER VISIT SITE AND MAKE A VISUAL INSPECTION OF THE GROUNDING GRID AND CONNECTIONS OF THE SYSTEM.
- G. ALL EQUIPMENT SHALL BE BONDED TO GROUND AS REQUIRED BY N.E.C., MFG. SPECIFICATIONS, AND OWNER'S SPECIFICATIONS.

## SECTION 16470

1.01. DISTRIBUTION EQUIPMENT

A. REFER TO CONTRACT DRAWINGS FOR DETAILS AND SCHEDULES.

## **SECTION 16477**

01. FUSES

A. FUSES SHALL BE NONRENEWABLE TYPE AS MANUFACTURED BY "BUSSMAN" OR APPROVED EQUAL. FUSES RATED TO 1/10 AMPERE UP TO 600 AMPERES SHALL BE EQUIVALENT TO BUSSMAN TYPE LPN-RK (250V) UL CLASS RK1, LOW PEAK, DUAL ELEMENT, TIME-DELAY FUSES. FUSES SHALL HAVE SEPARATE SHORT CIRCUIT AND OVERLOAD ELEMENTS AND HAVE AN INTERRUPTING RATING OF 200 KAIC. UPON COMPLETION OF WORK, PROVIDE ONE SPARE SET OF FUSES FOR EACH TYPE INSTALLED.

## **SECTION 16960**

- 1.01. TESTS BY INDEPENDENT ELECTRICAL TESTING FIRM
- A. CONTRACTOR SHALL RETAIN THE SERVICES OF A LOCAL INDEPENDENT ELECTRICAL TESTING FIRM (WITH MINIMUM 5 YEARS COMMERCIAL EXPERIENCE IN THE ELECTRICAL TESTING INDUSTRY) AS SPECIFIED BY OWNER TO PERFORM:
- TEST 1: THERMAL OVERLOAD AND MAGNETIC TRIP TEST, AND CABLE INSULATION TEST FOR ALL CIRCUIT BREAKERS RATED 100 AMPS OR GREATER.
- TEST 2: RESISTANCE TO GROUND TEST ON THE CELLULAR GROUNDING SYSTEM.
- THE TESTING FIRM SHALL INCLUDE THE FOLLOWING INFORMATION WITH THE REPORT:
- 1. TESTING PROCEDURE INCLUDING THE MAKE AND MODEL OF TEST EQUIPMENT.
- 2. CERTIFICATION OF TESTING EQUIPMENT CALIBRATION WITHIN SIX (6) MONTHS OF DATE OF TESTING. INCLUDE CERTIFICATION LAB ADDRESS AND TELEPHONE NUMBER.
- 3. GRAPHICAL DESCRIPTION OF TESTING METHOD ACTUALLY IMPLEMENTED.
- B. THESE TESTS SHALL BE PERFORMED IN THE PRESENCE AND TO THE SATISFACTION OF OWNER'S CONSTRUCTION REPRESENTATIVE. TESTING DATA SHALL BE INITIALED AND DATED BY THE CONSTRUCTION REPRESENTATIVE AND INCLUDED WITH THE WRITTEN REPORT/ANALYSIS.
- C. THE CONTRACTOR SHALL FORWARD SIX (6) COPIES OF THE INDEPENDENT ELECTRICAL TESTING FIRM'S REPORT/ANALYSIS TO ENGINEER A MINIMUM OF TEN (10) WORKING DAYS PRIOR TO THE JOB TURNOVER.
- D. CONTRACTOR TO PROVIDE A MINIMUM OF ONE (1) WEEK NOTICE TO OWNER AND ENGINEER FOR ALL TESTS REQUIRING WITNESSING.

## <u>SECTION 16961</u>

1.01. TESTS BY CONTRACTOR

- A. ALL TESTS AS REQUIRED UPON COMPLETION OF WORK, SHALL BE MADE BY THIS CONTRACTOR. THESE SHALL BE CONTINUITY AND INSULATION TESTS; TEST TO DETERMINE THE QUALITY OF MATERIALS, ETC. AND SHALL BE MADE IN ACCORDANCE WITH N.E.C. RECOMMENDATIONS. ALL FEEDERS AND BRANCH CIRCUIT WIRING (EXCEPT CLASS 2 SIGNAL CIRCUITS) MUST BE TESTED FREE FROM SHORT CIRCUIT AND GROUND FAULT CONDITIONS AT 500V IN A REASONABLY DRY AMBIENT OF APPROXIMATELY 70 DEGREES F.
- B. CONTRACTOR SHALL PERFORM LOAD PHASE BALANCING TESTS. CIRCUITS SHALL BE CONNECTED TO THE PANELBOARDS SO THAT THE NEW LOAD IS DISTRIBUTED AS EQUALLY AS POSSIBLE BETWEEN EACH LOAD AND NEUTRAL. 10% SHALL BE CONSIDERED AS A REASONABLE AND ACCEPTABLE ALLOWANCE. BRANCH CIRCUITS SHALL BE BALANCED ON THEIR OWN PANELBOARDS; FEEDER LOADS SHALL, IN TURN, BE BALANCED ON THE SERVICE EQUIPMENT. REASONABLE LOAD TEST SHALL BE ARRANGED TO VERIFY LOAD BALANCE IF REQUESTED BY THE ENGINEER.
- C. ALL TESTS, UPON REQUEST, SHALL BE REPEATED IN THE PRESENCE OF OWNER'S REPRESENTATIVE. ALL TESTS SHALL BE DOCUMENTED AND TURNED OVER TO OWNER. OWNER SHALL HAVE THE AUTHORITY TO STOP ANY OF THE WORK NOT BEING PROPERLY INSTALLED. ALL SUCH DETECTED WORK SHALL BE REPAIRED OR REPLACED AT NO ADDITIONAL EXPENSE TO THE OWNER AND THE TESTS SHALL BE REPEATED.

/21 RTS TJR CONSTRUCTION DRAWINGS – REVISED PER GENERATOR LO
/21 ANC TJR CONSTRUCTION DRAWINGS – REVISED COORDINATES PER /
/21 RTS TJR CONSTRUCTION DRAWINGS – REVISED STRUCTURAL COMPL
/21 RTS TJR CONSTRUCTION DRAWINGS – REVISED PER NEW RFDS

obile conversion conversion as a second conversion conv

Sprint > Mov T M

203) 488-0580 203) 488-8587 Fax 53-2 North Branford Road Stanford, CT 06405

AST

D: CT33XC553
): CTHA830A

HAMPDEN RD

DATE: 04/22/21

SCALE: AS NOTED

JOB NO. 21005.22

ELECTRICAL SPECIFICATION

| E-3

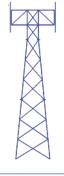
Sheet No. 12



## FRED A. NUDD CORPORATION

1743 ROUTE 104, BOX 577 ONTARIO, NY 14519 (315) 524-2531 FAX (315) 524-4249

www.nuddtowers.com



Mark LeGault Cordless Data Transfer, Inc. 600 Old Hartford Road Colchester, CT 06415 September 6, 2021

Fred A. Nudd Job Number: 121-23082

Location: 169 Hampden Road, Stafford Springs, CT 06076, Tolland County

Subject: Structural Analysis of a 180 ft Guyed Tower

Fred A. Nudd Corporation has completed a structural analysis of an existing 180 ft guyed tower. The tower was originally designed by Rohn Industries, to #80 specifications. The tower analysis was completed considering TIA-222-G design standards, which is the enforced design standard of the 2015 International Building Code, including 2018 Connecticut State Building Code. Tower dimensions have been taken from drawings by Rohn Industries, File Number 32343PH, dated April 17, 1995. Design criteria per each analysis are noted on the following page. The tower is assumed to be in good, undamaged and equivalent to as new condition and has been maintained / inspected per criteria by TIA-222.

The purpose of this analysis is to determine the structure's ability to support new Sprint equipment installed at a rad center of 171 ft above ground level (AGL). The new equipment to be installed, which included antennas, coax, mounts and associated hardware are listed on the following page in the appurtenance loading table.

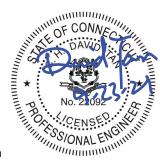
Results of the analysis indicate the tower will be able to the support the design loads noted in the appurtenance loading table on the following pages when considering the existing and proposed loading. Specific section design loads, capacities and stress ratios are provided on the following pages. Maximum member usage was found to be 93%.

The tower base foundation was analyzed based on dimensions provided by CDT and assumed geotechnical values. The anchors were analyzed by comparing the reactions from this analysis to the original design loads. Based on comparison to the calculated results and comparison to the original design reaction, it is reasonable to expect to expect the foundations have adequate capacity to support the existing and proposed loading noted above.

In conclusion, the tower superstructure can support the existing and proposed equipment noted above. The tower substructure is expected to be able to support this loading as well.

We trust this report satisfies your needs. Please contact us with any questions or concerns regarding this report.

Best Regards,



Fred. A. Nudd Corporation

### **Code Design Criteria**

ANSI/TIA-222-G

Windspeed = 97 mph, 3-Second Gust, V<sub>asd</sub> / 123 mph, 3-Second Gust, V<sub>ult</sub>

Structure Class = II

Topographic Category = 1

Exposure = B

Radial Ice = 1.0 inch

Ice Windspeed = 50 mph, 3-Second Gust

 $S_s < 1.0$ , thus seismic loading does not need to be considered

## Appurtenance Loading – Existing and To Remain on Tower

Height (ft)	Appurtenance	Mount	Coax (in)
180	(1) Station Master Antenna	Leg	(2) 7/8 (1) 1-1/4
179	(1) Decibel DB809	Side Arm	(1) 1-1/4
177	(1) Decibel DB809	Boom	(1) 7/8
163	(1) Celwave PD201	Pipe	(1) 7/8
150		Frame / Boom	
127	(1) Decibel DB420	Side Arm	(1) 7/8
83	(1) Celwave PD201	Pipe	(1) 1/2

<sup>•</sup> Height measurement taken as distance from top of base foundation to center of appurtenance.

### <u>Appurtenance Loading – Final Equipment Configuration For Sprint</u>

Height (ft)	Carrier	Appurtenance	Mount	Coax (in)
171	Sprint	(3) RFS APXVAALL24_43-U-NA20 (3) Ericsson AIR6449 B41 (3) Ericsson Radio 4460 B25+B86 (3) Ericsson Radio 4480 B71 B85	(3) V-Frame	(3) 6/24 4AWG Hybrid

- Height measurement taken as distance from top of base foundation to center of appurtenance.
- The proposed coax can be installed on any tower face.

## **Maximum Member Usage**

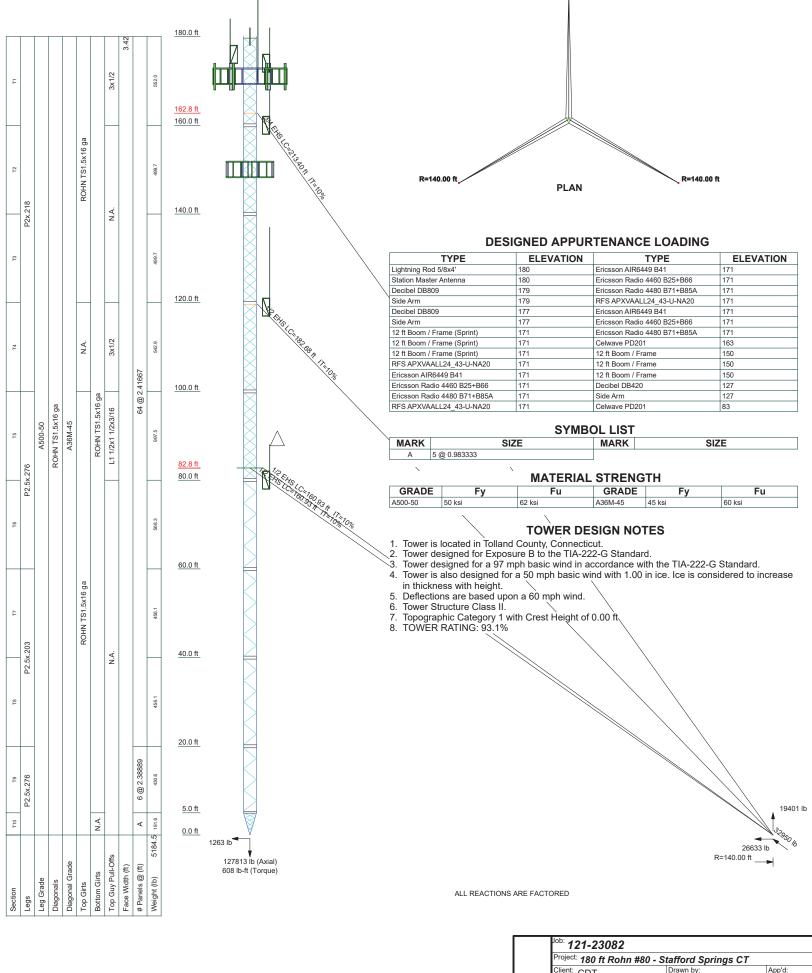
Member	Percentage
Leg	78
Diagonal	35
Horizontal	93
Guys	50
Splice/Connection Bolts	93

- Percentage equal to or less than 100% denote member stress levels are satisfactory for loading.
- Percentage greater than 100% indicates member strengthening is required.

### **Foundation Usage**

	Original Design or Calculated		
Design Load	Capacity (kips)	Analysis (kips)	Percentage
Base Axial	150.0 (Calculated)	127.8	88
Anchor Uplift	26.8 (Original Design)	19.4	54
Anchor Shear	32.4 (Original Design)	26.6	61

- The anchor percentages are divided by 1.35 to account for unfactored to factored load comparison
- Percentage less than 100% denote foundation is satisfactory for loading
- Percentage greater than 100% indicates foundation analysis is required



		<sup>Job:</sup> 121-23082		
		Project: 180 ft Rohn #80 - S	tafford Springs CT	
		Client: CDT	Drawn by:	App'd:
	Phone:	Code: TIA-222-G	Date: 09/06/21	Scale: NTS
١		Path:	Southout Scotnoon SA for Sported PISA Files (127-2008) Hampaden Road Stafford Analysis For Spor	Dwg No. E-1

R=140.00 ft

tnxTower	ob	121-23082	Page 1 of 48
	Project 180 ft Rohn ‡	#80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

## **Tower Input Data**

The main tower is a 3x guyed tower with an overall height of 180.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 3.42 ft at the top and tapered at the base.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in Tolland County, Connecticut.

Basic wind speed of 97 mph.

Structure Class II.

Exposure Category B.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.

Safety factor used in guy design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- Use Code Stress Ratios
- Use Code Safety Factors Guys Escalate Ice Always Use Max Kz
- Use Special Wind Profile
- Include Bolts In Member Capacity
- Leg Bolts Are At Top Of Section
- Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric

Distribute Leg Loads As Uniform Assume Legs Pinned

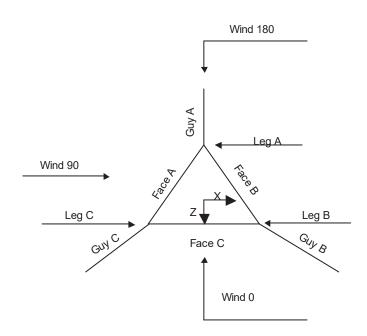
- Assume Rigid Index Plate
- Use Clear Spans For Wind Area
- Use Clear Spans For KL/r
- Retension Guys To Initial Tension Bypass Mast Stability Checks
- Use Azimuth Dish Coefficients
- Project Wind Area of Appurt.
- Autocalc Torque Arm Areas Add IBC .6D+W Combination Sort Capacity Reports By Component
- Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

Use ASCE 10 X-Brace Ly Rules

- Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression
- √ All Leg Panels Have Same Allowable Offset Girt At Foundation
- Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-G Bracing Resist. Exemption Use TIA-222-G Tension Splice Exemption Poles

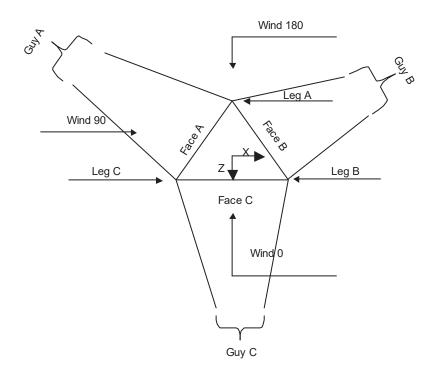
Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

tnxTower	Job	121-23082	Page 2 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by



Corner & Starmount Guyed Tower

tnxTower	Job	121-23082	Page 3 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by



Face Guyed

## Tower Section Geometry

Tower	Tower	Assembly	Description	Section	Number	Section
Section	Elevation	Database	_	Width	of	Length
					Sections	
	ft			ft		ft
T1	180.00-160.00			3.42	1	20.00
T2	160.00-140.00			3.42	1	20.00
T3	140.00-120.00			3.42	1	20.00
T4	120.00-100.00			3.42	1	20.00
T5	100.00-80.00			3.42	1	20.00
T6	80.00-60.00			3.42	1	20.00
T7	60.00-40.00			3.42	1	20.00
T8	40.00-20.00			3.42	1	20.00
Т9	20.00-5.00			3.42	1	15.00
T10	5.00-0.00			3.42	1	5.00

tnxTower	Job	121-23082	Page 4 of 48
	Project	121-20002	Date
	1.0,000	180 ft Rohn #80 - Stafford Springs CT	19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Tower	Tower	Diagonal	Bracing	Has	Has	Top Girt	Bottom Girt
Section	Elevation	Spacing	Туре	K Brace	Horizontals	Offset	Offset
		_		End			
	ft	ft		Panels		in	in
T1	180.00-160.00	2.42	CX Brace	No	Yes	4.0000	4.0000
T2	160.00-140.00	2.42	CX Brace	No	Yes	4.0000	4.0000
T3	140.00-120.00	2.42	CX Brace	No	Yes	4.0000	4.0000
T4	120.00-100.00	2.42	CX Brace	No	Yes	4.0000	4.0000
T5	100.00-80.00	2.42	CX Brace	No	Yes	4.0000	4.0000
T6	80.00-60.00	2.42	K Brace Left	No	Yes	4.0000	4.0000
T7	60.00-40.00	2.42	K Brace Left	No	Yes	4.0000	4.0000
T8	40.00-20.00	2.42	K Brace Left	No	Yes	4.0000	4.0000
Т9	20.00-5.00	2.39	K Brace Left	No	Yes	4.0000	4.0000
T10	5.00-0.00	0.98	X Brace	No	Yes	1.0000	0.0000

Tower	Leg	Leg	Leg	Diagonal	Diagonal	Diagonal
Elevation ft	Туре	Size	Grade	Туре	Size	Grade
T1 180.00-160.00	Pipe	P2x.218	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T2 160.00-140.00	Pipe	P2x.218	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T3 140.00-120.00	Pipe	P2x.218	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T4 120.00-100.00	Pipe	P2x.218	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T5 100.00-80.00	Pipe	P2.5x.276	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T6 80.00-60.00	Pipe	P2.5x.276	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T7 60.00-40.00	Pipe	P2.5x.203	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T8 40.00-20.00	Pipe	P2.5x.203	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T9 20.00-5.00	Pipe	P2.5x.276	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T10 5.00-0.00	Pipe	P2.5x.276	A500-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)

Tower	Top Girt	Top Girt	Top Girt	Bottom Girt	Bottom Girt	Bottom Girt
Elevation	Туре	Size	Grade	Туре	Size	Grade
ft						
T1 180.00-160.00	Pipe	ROHN TS1.5x16 ga	A36M-45	Pipe	ROHN TS1.5x16 ga	A36M-45
			(45 ksi)			(45 ksi)
T2 160.00-140.00	Pipe	ROHN TS1.5x16 ga	A36M-45	Pipe	ROHN TS1.5x16 ga	A36M-45
			(45 ksi)			(45 ksi)
T3 140.00-120.00	Pipe	ROHN TS1.5x16 ga	A36M-45	Pipe	ROHN TS1.5x16 ga	A36M-45
	_	_	(45 ksi)	_	_	(45 ksi)
T4 120.00-100.00	Pipe	ROHN TS1.5x16 ga	A36M-45	Pipe	ROHN TS1.5x16 ga	A36M-45
	_	_	(45 ksi)	_	_	(45 ksi)
T5 100.00-80.00	Pipe	ROHN TS1.5x16 ga	A36M-45	Pipe	ROHN TS1.5x16 ga	A36M-45

tnxTower	Job	121-23082	Page 5 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Tower Elevation	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
Ji			(45 ksi)			(45 ksi)
T6 80.00-60.00	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T7 60.00-40.00	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T8 40.00-20.00	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T9 20.00-5.00	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)
T10 5.00-0.00	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)	Pipe	ROHN TS1.5x16 ga	A36M-45 (45 ksi)

Tower	Section	Geometry	(cont'd)
IOMEI	<b>Je</b> Chon	Ocumen v	I COIIL UI

Tower	Gusset	Gusset	Gusset Grade	Adjust. Factor	Adjust.	Weight Mult.	Double Angle	0	Double Angle
Elevation	Area (per face)	Thickness		$A_f$	Factor		Stitch Bolt Spacing	Stitch Bolt Spacing	Stitch Bolt Spacing
	(per juce)				$A_r$		Diagonals	Horizontals	Redundants
ft	$ft^2$	in					in	in	in
T1	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
180.00-160.00			(36 ksi)						
T2	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
160.00-140.00			(36 ksi)						
T3	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
140.00-120.00			(36 ksi)						
T4	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
120.00-100.00			(36 ksi)						
T5	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
100.00-80.00			(36 ksi)						
T6 80.00-60.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						
T7 60.00-40.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						
T8 40.00-20.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						
T9 20.00-5.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						
T10 5.00-0.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						

			K Factors <sup>1</sup>										
Tower	Calc	Calc	Legs	X	K	Single	Girts	Horiz.	Sec.	Inner			
Elevation	K	K		Brace	Brace	Diags			Horiz.	Brace			
	Single	Solid		Diags	Diags								
	Angles	Rounds		X	X	X	X	X	X	X			
ft				Y	Y	Y	Y	Y	Y	Y			
T1	No	Yes	1	1	1	1	1	1	1	1			
180.00-160.00				1	1	1	1	1	1	1			
T2	No	Yes	1	1	1	1	1	1	1	1			
160.00-140.00				1	1	1	1	1	1	1			

tnxTower	Job	121-23082	Page 6 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

						K Fac	ctors1			
Tower Elevation	Calc K Single	Calc K Solid	Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
C.	Angles	Rounds		X	X Y	X	X $Y$	X	$X_{\mathbf{v}}$	X
ft				<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u>Y</u>	<u> </u>	
T3	No	Yes	1	1	1	1	I .	1	1	1
140.00-120.00				1	1	1	1	1	1	1
T4	No	Yes	1	1	1	1	1	1	1	1
120.00-100.00				1	1	1	1	1	1	1
T5	No	Yes	1	1	1	1	1	1	1	1
100.00-80.00				1	1	1	1	1	1	1
T6	No	Yes	1	1	1	1	1	1	1	1
80.00-60.00				1	1	1	1	1	1	1
T7	No	Yes	1	1	1	1	1	1	1	1
60.00-40.00				1	1	1	1	1	1	1
Т8	No	Yes	1	1	1	1	1	1	1	1
40.00-20.00	110	1 65	•	1	1	1	1	1	1	1
Т9 20.00-5.00	No	Yes	1	1	1	1	1	1	1	1
1 / 20.00-3.00	110	103	1	1	1	1	1	1	1	1
Т10 5.00-0.00	No	Yes	1	1	1	1	1	1	1	1
1 10 3.00-0.00	110	1 68	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1

<sup>&</sup>lt;sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom	Bottom Girt		Mid Girt		rizontal	Short Ho	rizontal
	Net Width	U	Net Width	U	Net Width	U	Net	U	Net	U	Net	U	Net	U
	Deduct		Deduct		Deduct		Width		Width		Width		Width	
	in		in		in		Deduct		Deduct		Deduct		Deduct	
							in		in		in		in	
T1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
180.00-160.00														
T2	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
160.00-140.00														
T3	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
140.00-120.00														
T4	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
120.00-100.00														
T5	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
100.00-80.00														
T6 80.00-60.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T7 60.00-40.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T8 40.00-20.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T9 20.00-5.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75
T10 5.00-0.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	0.75	0.0000	1	0.0000	0.75

tnxTower	Job	121-23082	Page 7 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Tower Elevation	Reduna Horizo		Redundant Diagonal		Redundant Sub-Diagonal		Redundant Sub-Horizontal		Redundant Vertical		Redundant Hip		Redundant Hip Diagonal	
ft	Net Width	U	Net Width	U	Net Width	U	Net	U	N/ -4	U	Net	U	Net	U
		U	Deduct	U	Deduct	U	Width	U	Net Width	U	Net Width	U	Width	U
	Deduct													
	in		in		in		Deduct		Deduct		Deduct		Deduct	
	0.0000	0.75	0.0000	0.75	0.0000	0.75	in	0.75	in	0.75	in	0.75	in	0.75
T1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
180.00-160.00		0.55		0.77		0.75		0.55		0.75	0.0000	0.55	0.0000	0.55
T2	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
160.00-140.00														
T3	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
140.00-120.00														
T4	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
120.00-100.00														
T5	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
100.00-80.00														
T6 80.00-60.00	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T7 60.00-40.00	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T8 40.00-20.00	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T9 20.00-5.00	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T10 5.00-0.00	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

Tower	Leg	Leg		Diago	nal	Top G	irt	Bottom	Girt	Mid G	irt	Long Hori	izontal	Short Horizontal	
Elevation	Connection														
ft	Туре														
		Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.						
		in		in		in		in		in		in		in	
T1	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
180.00-160.00	_	A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T2	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
160.00-140.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T3	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
140.00-120.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T4	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
120.00-100.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T5	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
100.00-80.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T6 80.00-60.00	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T7 60.00-40.00	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T8 40.00-20.00	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T9 20.00-5.00	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
	-	A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T10 5.00-0.00	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	

## **Guy Data**

tnxTower	Job	121-23082	Page 8 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Guy Elevation	Guy Grade		Guy Size	Initial Tension	%	Guy Modulus	Guy Weight	$L_u$	Anchor Radius	Anchor Azimuth	Anchor Elevation	End Fitting
ft				lb		ksi	plf	ft	ft	Adj. ∘	ft	Efficiency %
82.75	EHS	Α	1/2	2690.00	10%	21000	0.517	160.79	140.00	0.0000	0.00	100%
		В	1/2	2690.00	10%	21000	0.517	160.79	140.00	0.0000	0.00	100%
		C	1/2	2690.00	10%	21000	0.517	160.79	140.00	0.0000	0.00	100%
162.75	EHS	A	3/4	5830.00	10%	19000	1.155	213.21	140.00	0.0000	0.00	100%
		В	3/4	5830.00	10%	19000	1.155	213.21	140.00	0.0000	0.00	100%
		C	3/4	5830.00	10%	19000	1.155	213.21	140.00	0.0000	0.00	100%
119.667	EHS	A	1/2	2690.00	10%	21000	0.517	182.52	140.00	0.0000	0.00	100%
		В	1/2	2690.00	10%	21000	0.517	182.52	140.00	0.0000	0.00	100%
		C	1/2	2690.00	10%	21000	0.517	182.52	140.00	0.0000	0.00	100%

Guy Data(cont'd)										
Guy Elevation ft	Mount Type	Torque-Arm Spread ft	Torque-Arm Leg Angle	Torque-Arm Style	Torque-Arm Grade	Torque-Arm Type	Torque-Arm Size			
82.75 162.75	Torque Arm Strap	7.00	0.0000	Channel	A36 (36 ksi)	Channel	C10x15.3			
119.667	Strap									

	Guy Data (cont'd)										
Guy Elevation ft	Diagonal Grade	Diagonal Type	Upper Diagonal Size	Lower Diagonal Size	Is Strap.	Pull-Off Grade	Pull-Off Type	Pull-Off Size			
82.75	A572-50 (50 ksi)	Solid Round			No	A36 (36 ksi)	Equal Angle	L1 1/2x1 1/2x3/16			
162.75	A572-50 (50 ksi)	Solid Round			No	A36 (36 ksi)	Flat Bar	3x1/2			
119.67	A572-50 (50 ksi)	Solid Round			No	A36 (36 ksi)	Flat Bar	3x1/2			

Guy Data (cont'd)											
Guy	Cable	Cable	Cable	Cable	Tower	Tower	Tower	Tower			
Elevation	Weight A	Weight B	Weight C	Weight D	Intercept A	Intercept B	Intercept C	Intercept D			
ft	lb	lb	lb	lb	ft	ft	ft	ft			
82.75	83.13	83.13	83.13		2.47	2.47	2.47				
162.75	246.25	246.25	246.25		2.7 sec/pulse 4.44	2.7 sec/pulse 4.44	2.7 sec/pulse 4.44				
119.667	94.37	94.37	94.37		3.6 sec/pulse 3.17	3.6 sec/pulse 3.17	3.6 sec/pulse 3.17				
					3.1 sec/pulse	3.1 sec/pulse	3.1 sec/pulse				

tnxTower	Job	121-23082	Page 9 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

			Guy Data (cont'd)									
			Torqu	ıe Arm	Pul	l Off	Diag	gonal				
Guy	Calc	Calc	$K_x$	$K_y$	$K_x$	$K_y$	$K_x$	$K_y$				
Elevation	K	K										
ft	Single	Solid										
	Angles	Rounds										
82.75	No	No	1	1	1	1	1	1				
162.75	No	No			1	1	1	1				
119.667	No	No			1	1	1	1				

		Torqi	ıe-Arm			Pui	ll Off			Dia	gonal	
Guy	Bolt Size	Number	Net Width	U	Bolt Size	Number	Net Width	U	Bolt Size	Number	Net Width	U
Elevation	in		Deduct		in		Deduct		in		Deduct	
ft			in				in				in	
82.75	0.7500	2	0.0000	1	0.0000	0	0.0000	1	0.6250	0	0.0000	1
	A325N				A325N				A325N			
162.75	0.6250	0	0.0000	0.75	0.0000	0	0.0000	1	0.6250	0	0.0000	1
	A325N				A325N				A325N			
119.667	0.6250	0	0.0000	0.75	0.0000	0	0.0000	1	0.6250	0	0.0000	1
	A 325NI				A 325NI				A 325NI			

Guy Data (cont'd)

Guy Pressures									
Guy Elevation ft	Guy Location	z ft	$q_z$	q <sub>z</sub> Ice psf	Ice Thickness in				
82.75	A	41.38	16	4	2.0457				
	В	41.38	16	4	2.0457				
	C	41.38	16	4	2.0457				
162.75	A	81.38	19	5	2.1889				
	В	81.38	19	5	2.1889				
	C	81.38	19	5	2.1889				
119.667	A	59.83	17	5	2.1226				
	В	59.83	17	5	2.1226				
	C	59.83	17	5	2.1226				

Guy-Mast Forces (Excluding Wind) - No Ice											
Guy	Guy	Chord	Guy Tension	$F_{\rm x}$	$F_v$	$F_z$	$M_{x}$	$M_{\nu}$	$M_z$		
Elevation	Location	Angle	Top Bottom lb		,	-		,	-		
ft		0	io	lb	lb	lb	lb-ft	lb-ft	lb-ft		
82.75	A	30.9442	2732.74 2690.00	-58.96	1435.72	-2324.46	-2901.19	8254.77	-5025.01		
	A	30.9442	2732.74	58.96	1435.72	-2324.46	-2901.19	-8254.77	5025.01		

tnxTower	Job	121-23082	Page 10 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom lb	$F_x$	$F_y$	$F_z$	$M_x$	$M_{y}$	$M_z$
ft		0	10	lb	lb	lb	lb-ft	lb-ft	lb-ft
			2690.00						
	В	30.9442	2732.74 2690.00	2042.53	1435.72	1111.17	5802.38	8254.77	0.00
	В	30.9442	2732.74 2690.00	1983.56	1435.72	1213.30	-2901.19	-8254.77	-5025.01
	C	30.9442	2732.74 2690.00	-1983.56	1435.72	1213.30	-2901.19	8254.77	5025.01
	С	30.9442	2732.74 2690.00	-2042.53	1435.72	1111.17	5802.38	-8254.77	0.00
			Sum:	0.00	8614.30	0.00	-0.00	0.00	0.00
162.75	A	49.6993	6017.80 5830.00	0.00	4640.87	-3830.96	-9163.58	0.00	0.00
	В	49.6993	6017.80 5830.00	3317.71	4640.87	1915.48	4581.79	0.00	-7935.89
	С	49.6993	6017.80 5830.00	-3317.71	4640.87	1915.48	4581.79	-0.00	7935.89
			Sum:	0.00	13922.62	-0.00	0.00	0.00	0.00
119.667	A	40.9250	2751.81 2690.00	0.00	1829.52	-2055.57	-3612.45	0.00	0.00
	В	40.9250	2751.81 2690.00	1780.17	1829.52	1027.78	1806.22	0.00	-3128.47
	C	40.9250	2751.81 2690.00	-1780.17	1829.52	1027.78	1806.22	-0.00	3128.47
			Sum:	0.00	5488.55	-0.00	0.00	0.00	0.00

	Guy-Mast Forces (Excluding Wind) - Ice											
Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom lb	$F_x$	$F_y$	$F_z$	$M_x$	$M_y$	$M_z$			
ft		0		lb	lb	lb	lb-ft	lb-ft	lb-ft			
82.75	A	30.9442	6764.07 6195.76	-140.46	3882.09	-5537.35	-7844.65	19664.57	-13587.3			
	A	30.9442	6764.07 6195.76	140.46	3882.09	-5537.35	-7844.65	-19664.57	13587.33			
	В	30.9442	6764.07 6195.76	4865.72	3882.09	2647.03	15689.29	19664.57	0.00			
	В	30.9442	6764.07 6195.76	4725.26	3882.09	2890.32	-7844.65	-19664.57	-13587.3			
	C	30.9442	6764.07 6195.76	-4725.26	3882.09	2890.32	-7844.65	19664.57	13587.3			
	C	30.9442	6764.07 6195.76	-4865.72	3882.09	2647.03	15689.29	-19664.57	0.00			
			Sum:	0.00	23292.56	0.00	-0.00	0.00	0.00			
162.75	A	49.6993	11880.60 10415.60	0.00	9458.73	-7188.96	-18676.62	0.00	0.00			
	В	49.6993	11880.60 10415.60	6225.82	9458.73	3594.48	9338.31	0.00	-16174.4			
	C	49.6993	11880.60 10415.60	-6225.82	9458.73	3594.48	9338.31	-0.00	16174.4			
119.667	A	40.9250	Sum: 7118.36 6244.19	0.00 0.00	28376.19 5040.37	-0.00 -5026.50	0.00 -9952.40	0.00 0.00	0.00 0.00			

tnxTower	Job	121-23082	Page 11 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Guy	Guy	Chord	Guy Tension	$F_x$	$F_y$	$F_z$	$M_x$	$M_y$	$M_z$
Elevation	Location	Angle	Тор						
			Bottom						
			lb						
ft		0		lb	lb	lb	lb-ft	lb-ft	lb-ft
	В	40.9250	7118.36	4353.08	5040.37	2513.25	4976.20	0.00	-8619.04
			6244.19						
	C	40.9250	7118.36	-4353.08	5040.37	2513.25	4976.20	-0.00	8619.04
			6244.19						
			Sum:	0.00	15121.11	-0.00	0.00	0.00	0.00

Guy	Guy	Chord	Guy Tension	$F_x$	$F_y$	$F_z$	$M_x$	$M_y$	$M_z$
Elevation	Location	Angle	Top Bottom lb						
ft		0		lb	lb	lb	lb-ft	lb-ft	lb-ft
82.75	A	30.9442	2732.74 2690.00	-58.96	1435.72	-2324.46	-2901.19	8254.77	-5025.01
	A	30.9442	2732.74 2690.00	58.96	1435.72	-2324.46	-2901.19	-8254.77	5025.01
	В	30.9442	2732.74 2690.00	2042.53	1435.72	1111.17	5802.38	8254.77	0.00
	В	30.9442	2732.74 2690.00	1983.56	1435.72	1213.30	-2901.19	-8254.77	-5025.01
	С	30.9442	2732.74 2690.00	-1983.56	1435.72	1213.30	-2901.19	8254.77	5025.01
	С	30.9442	2732.74 2690.00	-2042.53	1435.72	1111.17	5802.38	-8254.77	0.00
			Sum:	0.00	8614.30	0.00	-0.00	0.00	0.00
162.75	A	49.6993	6017.80 5830.00	0.00	4640.87	-3830.96	-9163.58	0.00	0.00
	В	49.6993	6017.80 5830.00	3317.71	4640.87	1915.48	4581.79	0.00	-7935.89
	С	49.6993	6017.80 5830.00	-3317.71	4640.87	1915.48	4581.79	-0.00	7935.89
			Sum:	0.00	13922.62	-0.00	0.00	0.00	0.00
119.667	A	40.9250	2751.81 2690.00	0.00	1829.52	-2055.57	-3612.45	0.00	0.00
	В	40.9250	2751.81 2690.00	1780.17	1829.52	1027.78	1806.22	0.00	-3128.47
	С	40.9250	2751.81 2690.00	-1780.17	1829.52	1027.78	1806.22	-0.00	3128.47
			Career	0.00	5100 55	0.00	0.00	0.00	0.00

0.00

Sum:

# **Guy-Tensioning Information**

5488.55

-0.00

0.00

0.00

0.00

											7: O.C.T.						
					Temperature At Time Of Tensioning												
					) F	2	0 F	40	0 F	60	0 F	80	) F	10	00 F	12	0 F
Guy		H	V	Initial	Intercept	Initial	Intercept	Initial	Intercept	Initial	Intercept	Initial	Intercept	Initial	Intercept	Initial	Intercept
Elevation				Tension		Tension		Tension		Tension		Tension		Tension		Tension	
ft		ft	ft	lb	ft	lb	ft	lb	ft	lb	ft	lb	ft	lb	ft	lb	ft
82.75	Α	138.02	82.75	3555	1.87	3263	2.04	2975	2.23	2690	2.47	2411	2.75	2140	3.10	1881	3.52
	В	138.02	82.75	3555	1.87	3263	2.04	2975	2.23	2690	2.47	2411	2.75	2140	3.10	1881	3.52
	C	138.02	82.75	3555	1.87	3263	2.04	2975	2.23	2690	2.47	2411	2.75	2140	3.10	1881	3.52

tnxTower	Job	121-23082	<b>Page</b> 12 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

					Temperature At Time Of Tensioning												
				0	F	20	0 F	4	0 F	60	0 F	80	0 F	10	00 F	12	0 F
Guy		H	V	Initial	Intercept	Initial	Intercept	Initial	Intercept	Initial	Intercept	Initial	Intercept	Initial	Intercept	Initial	Intercept
Elevation				Tension	•	Tension	•	Tension	•	Tension	•	Tension	•	Tension	•	Tension	•
ft		ft	ft	lb	ft	lb	ft	lb	ft	lb	ft	lb	ft	lb	ft	lb	ft
162.75	Α	138.03	162.75	6822	3.80	6489	3.99	6158	4.20	5830	4.44	5505	4.69	5185	4.98	4869	5.30
	В	138.03	162.75	6822	3.80	6489	3.99	6158	4.20	5830	4.44	5505	4.69	5185	4.98	4869	5.30
	C	138.03	162.75	6822	3.80	6489	3.99	6158	4.20	5830	4.44	5505	4.69	5185	4.98	4869	5.30
119.667	Α	138.03	119.67	3359	2.54	3134	2.72	2911	2.93	2690	3.17	2473	3.44	2260	3.76	2053	4.14
	В	138.03	119.67	3359	2.54	3134	2.72	2911	2.93	2690	3.17	2473	3.44	2260	3.76	2053	4.14
	C	138.03	119.67	3359	2.54	3134	2.72	2911	2.93	2690	3.17	2473	3.44	2260	3.76	2053	4.14

# Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or	Allow Shield	Exclude From	Component Type		Face Offset	Lateral Offset	#		1 0	Width or Diameter	Perimeter	Weight
	Leg		Torque Calculation		ft	in	(Frac FW)		Row	in	in	in	plf
Feedline Ladder (Af)	С	No	No	Ar (CaAa)	171.50 - 6.00	0.1000	0	1	1	3.0000	3.0000		8.40
Safety Line 3/8	A	No	No	Ar (CaAa)	180.00 - 6.00	0.0000	0	1	1	0.3750	0.3750		0.22
4AWG	C	No	No	Ar (CaAa)	171.00 - 6.00	0.1000	0	3	3	1.5500	1.2500		0.66
1 1/4	В	No	No	Ar (CaAa)	180.00 - 6.00	0.1000	0	1	1	1.5500	1.5500		0.66
7/8	В	No	No	Ar (CaAa)	180.00 - 6.00	0.1000	0	2	2	1.1100	1.1100		0.54
1 1/4	В	No	No	Ar (CaAa)	179.00 - 6.00	0.1000	0	1	1	1.5500	1.5500		0.66
7/8	В	No	No	Ar (CaAa)	177.00 - 6.00	0.1000	0	1	1	1.1100	1.1100		0.54
7/8	В	No	No	Ar (CaAa)	163.00 -	0.1000	0	1	1	1.1100	1.1100		0.54
7/8	В	No	No	Ar (CaAa)	6.00 127.00 -	0.1000	0	1	1	1.1100	1.1100		0.54
1/2	В	No	No	Ar (CaAa)	6.00 83.00 - 6.00	0.1000	0	1	1	0.5800	0.5800		0.25

# Feed Line/Linear Appurtenances Section Areas

Tower	Tower	Face	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		$ft^2$	ft²	$ft^2$	ft <sup>2</sup>	lb
T1	180.00-160.00	A	0.000	0.000	0.750	0.000	4.40
		В	0.000	0.000	12.705	0.000	58.14
		C	0.000	0.000	7.575	0.000	118.38
T2	160.00-140.00	A	0.000	0.000	0.750	0.000	4.40
		В	0.000	0.000	15.080	0.000	69.60
		C	0.000	0.000	13.500	0.000	207.60
T3	140.00-120.00	A	0.000	0.000	0.750	0.000	4.40
		В	0.000	0.000	15.857	0.000	73.38
		C	0.000	0.000	13.500	0.000	207.60
T4	120.00-100.00	A	0.000	0.000	0.750	0.000	4.40
		В	0.000	0.000	17.300	0.000	80.40
		C	0.000	0.000	13.500	0.000	207.60
T5	100.00-80.00	A	0.000	0.000	0.750	0.000	4.40
		В	0.000	0.000	17.474	0.000	81.15

tnxTower	Job	121-23082	Page 13 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Tower Section	Tower Elevation	Face	$A_R$	$A_F$	$C_AA_A$ In Face	$C_AA_A$ Out Face	Weight
section	ft Elevation		ft²	$ft^2$	ft <sup>2</sup>	ft <sup>2</sup>	lb
		С	0.000	0.000	13.500	0.000	207.60
T6	80.00-60.00	A	0.000	0.000	0.750	0.000	4.40
		В	0.000	0.000	18.460	0.000	85.40
		C	0.000	0.000	13.500	0.000	207.60
T7	60.00-40.00	A	0.000	0.000	0.750	0.000	4.40
		В	0.000	0.000	18.460	0.000	85.40
		C	0.000	0.000	13.500	0.000	207.60
T8	40.00-20.00	A	0.000	0.000	0.750	0.000	4.40
		В	0.000	0.000	18.460	0.000	85.40
		C	0.000	0.000	13.500	0.000	207.60
T9	20.00-5.00	A	0.000	0.000	0.525	0.000	3.08
		В	0.000	0.000	12.922	0.000	59.78
		C	0.000	0.000	9.450	0.000	145.32
T10	5.00-0.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.00

# Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness	$ft^2$	$ft^2$	In Face ft²	Out Face	lb
T-1	JI	Leg	in		J.	J.	ft²	
T1	180.00-160.00	A	2.356	0.000	0.000	10.175	0.000	161.65
		В		0.000	0.000	60.891	0.000	988.84
TT-2	160 00 140 00	C	2 227	0.000	0.000	26.757	0.000	542.23
T2	160.00-140.00	A	2.327	0.000	0.000	10.058	0.000	158.03
		В		0.000	0.000	72.489	0.000	1188.73
		C		0.000	0.000	47.634	0.000	951.92
T3	140.00-120.00	A	2.294	0.000	0.000	9.926	0.000	153.99
		В		0.000	0.000	75.718	0.000	1234.28
		C		0.000	0.000	47.279	0.000	938.14
T4	120.00-100.00	A	2.256	0.000	0.000	9.774	0.000	149.42
		В		0.000	0.000	82.100	0.000	1331.65
		C		0.000	0.000	46.872	0.000	922.43
T5	100.00-80.00	A	2.211	0.000	0.000	9.594	0.000	144.12
		В		0.000	0.000	82.391	0.000	1315.87
		C		0.000	0.000	46.391	0.000	904.09
T6	80.00-60.00	A	2.156	0.000	0.000	9.375	0.000	137.76
		В		0.000	0.000	89.195	0.000	1394.52
		C		0.000	0.000	45.804	0.000	881.90
T7	60.00-40.00	A	2.085	0.000	0.000	9.089	0.000	129.71
		В		0.000	0.000	86.986	0.000	1326.15
		C		0.000	0.000	45.040	0.000	853.49
T8	40.00-20.00	A	1.981	0.000	0.000	8.674	0.000	118.45
		В		0.000	0.000	83.771	0.000	1229.76
		C		0.000	0.000	43.931	0.000	813.03
T9	20.00-5.00	Ā	1.815	0.000	0.000	5.607	0.000	71.06
		В		0.000	0.000	55.042	0.000	758.28
		C		0.000	0.000	29.513	0.000	525.36
T10	5.00-0.00	A	1.545	0.000	0.000	0.000	0.000	0.00
-10	5.00 0.00	В	1.5 15	0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.00

#### **Feed Line Center of Pressure**

Job		Page
	121-23082	14 of 48
Project		Date
	180 ft Rohn #80 - Stafford Springs CT	19:45:40 09/06/21
Client		Designed by
	CDT	
	Project	121-23082  Project  180 ft Rohn #80 - Stafford Springs CT

Section	Elevation	$CP_X$	$CP_Z$	$CP_X$	$CP_Z$
				Ice	Ice
	ft	in	in	in	in
T1	180.00-160.00	2.0412	0.2146	1.0873	-0.1960
T2	160.00-140.00	2.2538	1.0865	1.4658	0.2052
T3	140.00-120.00	2.3486	1.0054	1.5807	0.1577
T4	120.00-100.00	2.4452	0.8398	1.7304	0.0607
T5	100.00-80.00	2.3896	0.7955	1.6353	0.0432
T6	80.00-60.00	2.8228	0.7978	3.3469	-0.1024
T7	60.00-40.00	2.8228	0.7978	3.3739	-0.0831
T8	40.00-20.00	2.8228	0.7978	3.4105	-0.0524
T9	20.00-5.00	2.7009	0.7633	3.2969	0.0033
T10	5.00-0.00	0.0000	0.0000	0.0000	0.0000

# Shielding Factor Ka

Tower	Feed Line	Description	Feed Line	$K_a$	$K_a$
Section	Record No.		Segment Elev.	No Ice	Ice
T1	1	Feedline Ladder (Af)	160.00 - 171.50	0.6000	0.2306
T1	2	Safety Line 3/8	160.00 -	0.6000	0.2306
		4.4776	180.00	0.6000	0.2206
T1	3	4AWG	160.00 - 171.00	0.6000	0.2306
T1	4	1 1/4	160.00 -	0.6000	0.2306
			180.00		
T1	5	7/8	160.00 -	0.6000	0.2306
T1	6	1 1/4	180.00 160.00 -	0.6000	0.2306
11	U	1 1/4	179.00	0.0000	0.2300
T1	7	7/8	160.00 -	0.6000	0.2306
			177.00		
T1	8	7/8	160.00 -	0.6000	0.2306
772	,	E 11: 1 11 (10	163.00	0.6000	0.0600
T2	1	Feedline Ladder (Af)	140.00 - 160.00	0.6000	0.2622
T2	2	Safety Line 3/8	140.00 -	0.6000	0.2622
	_		160.00		**
T2	3	4AWG	140.00 -	0.6000	0.2622
T2	4	1 1/4	160.00 140.00 -	0.6000	0.2622
12	4	1 1/4	160.00	0.0000	0.2622
T2	5	7/8	140.00 -	0.6000	0.2622
			160.00		
T2	6	1 1/4	140.00 -	0.6000	0.2622
772	7	7/0	160.00	0.6000	0.0600
T2	7	7/8	140.00 - 160.00	0.6000	0.2622
T2	8	7/8	140.00 -	0.6000	0.2622
1.2		,,,	160.00	0.0000	0.2022
T3	1	Feedline Ladder (Af)	120.00 -	0.6000	0.2688
		g 0 . ** **	140.00	0.000	0.000
T3	2	Safety Line 3/8	120.00 - 140.00	0.6000	0.2688
Т3	3	4AWG	120.00 -	0.6000	0.2688
		111113	140.00	0.0000	0.2000
Т3	4	1 1/4	120.00 -	0.6000	0.2688

tnxTower	Job	121-23082	<b>Page</b> 15 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

<i>T</i> .	T 11.	D	F 11:	77	7/
Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>a</sub> No Ice	$K_a$ Ice
Section	Record Ivo.		140.00	No ice	ice
Т3	5	7/8	120.00 -	0.6000	0.2688
15	J	,,,	140.00	0.0000	0.2000
Т3	6	1 1/4	120.00 -	0.6000	0.2688
			140.00		
T3	7	7/8	120.00 -	0.6000	0.2688
TO .	0	7/0	140.00	0.6000	0.2600
Т3	8	7/8	120.00 - 140.00	0.6000	0.2688
Т3	9	7/8	120.00 -	0.6000	0.2688
13		770	127.00	0.0000	0.2000
T4	1	Feedline Ladder (Af)	100.00 -	0.6000	0.2712
		, ,	120.00		
T4	2	Safety Line 3/8	100.00 -	0.6000	0.2712
	2	4. W.G	120.00	0.6000	0.0710
T4	3	4AWG	100.00 -	0.6000	0.2712
T4	4	1 1/4	120.00 100.00 -	0.6000	0.2712
14	7	1 1/4	120.00	0.0000	0.2/12
T4	5	7/8	100.00 -	0.6000	0.2712
			120.00		
T4	6	1 1/4	100.00 -	0.6000	0.2712
	_		120.00		
T4	7	7/8	100.00 -	0.6000	0.2712
T4	8	7/8	120.00 100.00 -	0.6000	0.2712
14	8	778	120.00	0.0000	0.2/12
T4	9	7/8	100.00 -	0.6000	0.2712
			120.00		
T5	1	Feedline Ladder (Af)		0.6000	0.2579
T5	2	Safety Line 3/8		0.6000	0.2579
T5	3	4AWG		0.6000	0.2579
T5 T5	4 5	1 1/4	80.00 - 100.00 80.00 - 100.00	0.6000 0.6000	0.2579 0.2579
T5	6	1 1/4	80.00 - 100.00	0.6000	0.2579
T5	7	7/8		0.6000	0.2579
T5	8	7/8	80.00 - 100.00	0.6000	0.2579
T5	9		80.00 - 100.00	0.6000	0.2579
T5	10	1/2	80.00 - 83.00	0.6000	0.2579
T6 T6	1 2	Feedline Ladder (Af) Safety Line 3/8	60.00 - 80.00	0.6000 0.6000	0.4759
T6	3	4AWG	60.00 - 80.00 60.00 - 80.00	0.6000	0.4759 0.4759
T6	4	1 1/4		0.6000	0.4759
Т6	5	7/8	60.00 - 80.00	0.6000	0.4759
T6	6	1 1/4		0.6000	0.4759
T6	7	7/8	60.00 - 80.00	0.6000	0.4759
T6	8	7/8	60.00 - 80.00	0.6000	0.4759
T6	9	7/8 1/2	60.00 - 80.00	0.6000	0.4759 0.4759
T6 T7	10 1	Feedline Ladder (Af)	60.00 - 80.00 40.00 - 60.00	0.6000 0.6000	0.4759
T7	2	Safety Line 3/8		0.6000	0.4858
T7	3	4AWG	40.00 - 60.00	0.6000	0.4858
T7	4	1 1/4	40.00 - 60.00	0.6000	0.4858
T7	5	7/8	40.00 - 60.00	0.6000	0.4858
T7	6	1 1/4	40.00 - 60.00	0.6000	0.4858
T7	7 8	7/8	40.00 - 60.00 40.00 - 60.00	0.6000	0.4858
T7 T7	8	7/8 7/8		0.6000 0.6000	0.4858 0.4858
T7	10	1/2		0.6000	0.4858
T8	1	Feedline Ladder (Af)		0.6000	0.5004
Т8	2	Safety Line 3/8	20.00 - 40.00	0.6000	0.5004
Т8	3	4AWG	20.00 - 40.00	0.6000	0.5004

tnxTower	Job	121-23082	<b>Page</b> 16 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Tower	Feed Line	Description	Feed Line	$K_a$	$K_a$
Section	Record No.		Segment Elev.	No Ice	Ice
T8	4	1 1/4	20.00 - 40.00	0.6000	0.5004
T8	5	7/8	20.00 - 40.00	0.6000	0.5004
T8	6	1 1/4	20.00 - 40.00	0.6000	0.5004
T8	7	7/8	20.00 - 40.00	0.6000	0.5004
T8	8	7/8	20.00 - 40.00	0.6000	0.5004
T8	9	7/8	20.00 - 40.00	0.6000	0.5004
T8	10	1/2	20.00 - 40.00	0.6000	0.5004
T9	1	Feedline Ladder (Af)	6.00 - 20.00	0.6000	0.5132
T9	2	Safety Line 3/8	6.00 - 20.00	0.6000	0.5132
T9	3	4AWG	6.00 - 20.00	0.6000	0.5132
T9	4	1 1/4	6.00 - 20.00	0.6000	0.5132
T9	5	7/8	6.00 - 20.00	0.6000	0.5132
T9	6	1 1/4	6.00 - 20.00	0.6000	0.5132
T9	7	7/8	6.00 - 20.00	0.6000	0.5132
Т9	8	7/8	6.00 - 20.00	0.6000	0.5132
T9	9	7/8	6.00 - 20.00	0.6000	0.5132
Т9	10	1/2	6.00 - 20.00	0.6000	0.5132

## **Discrete Tower Loads**

Description	Face	Offset	Offsets:	Azimuth	Placement		$C_A A_A$	$C_A A_A$	Weight
	or	Туре	Horz Lateral	Adjustment			Front	Side	
	Leg		Vert						
			ft	0	ft		$ft^2$	$ft^2$	lb
			ft		Ji		Ji	Ji	w
			ft						
Lightning Rod 5/8x4'	С	None	v	0.0000	180.00	No Ice	0.25	0.25	31.00
						1/2" Ice	0.66	0.66	33.82
						1" Ice	0.97	0.97	39.29
12 ft Boom / Frame	A	From Leg	2.00	0.0000	150.00	No Ice	18.00	9.00	500.00
			0.00			1/2" Ice	22.00	11.00	650.00
			0.00			1" Ice	26.00	13.00	800.00
12 ft Boom / Frame	В	From Leg	2.00	0.0000	150.00	No Ice	18.00	9.00	500.00
			0.00			1/2" Ice	22.00	11.00	650.00
			0.00			1" Ice	26.00	13.00	800.00
12 ft Boom / Frame	C	From Leg	2.00	0.0000	150.00	No Ice	18.00	9.00	500.00
			0.00			1/2" Ice	22.00	11.00	650.00
			0.00			1" Ice	26.00	13.00	800.00
Station Master Antenna	В	From Leg	0.50	0.0000	180.00	No Ice	3.64	3.64	10.20
		_	0.00			1/2" Ice	4.21	4.21	30.00
			0.00			1" Ice	4.78	4.78	50.00
Decibel DB809	C	From Leg	3.00	0.0000	179.00	No Ice	3.68	3.68	27.00
			0.00			1/2" Ice	4.93	4.93	60.90
			0.00			1" Ice	6.21	6.21	104.80
Side Arm	C	From Leg	2.00	0.0000	179.00	No Ice	4.97	4.97	70.00
			0.00			1/2" Ice	6.12	6.12	130.00
			0.00			1" Ice	7.27	7.27	190.00
Decibel DB809	В	From Leg	3.00	0.0000	177.00	No Ice	3.68	3.68	27.00
			0.00			1/2" Ice	4.93	4.93	60.90
			0.00			1" Ice	6.21	6.21	104.80
Side Arm	В	From Leg	2.00	0.0000	177.00	No Ice	4.97	4.97	70.00
		Ü	0.00			1/2" Ice	6.12	6.12	130.00
			0.00			1" Ice	7.27	7.27	190.00
Celwave PD201	В	From Leg	3.00	0.0000	163.00	No Ice	1.18	1.18	4.00
		_							

tnxTower	Job	121-23082	Page 17 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_AA_A$ Front	$C_AA_A$ Side	Weight
	Leg		Lateral Vert						
			ft	0	ft		$ft^2$	$ft^2$	lb
			ft ft		J		J	,	
			0.00			1/2" Ice	2.09	2.09	16.80
			0.00			1" Ice	3.02	3.02	36.90
Celwave PD201	В	From Leg	3.00	0.0000	83.00	No Ice	1.18	1.18	4.00
		C	0.00			1/2" Ice	2.09	2.09	16.80
			0.00			1" Ice	3.02	3.02	36.90
Decibel DB420	В	From Leg	3.00	0.0000	127.00	No Ice	5.19	5.19	35.00
			0.00			1/2" Ice	7.19	7.19	83.50
			0.00			1" Ice	9.20	9.20	147.80
Side Arm	В	From Leg	2.00	0.0000	127.00	No Ice	4.97	4.97	70.00
		_	0.00			1/2" Ice	6.12	6.12	130.00
			0.00			1" Ice	7.27	7.27	190.00
12 ft Boom / Frame	A	From Leg	2.00	0.0000	171.00	No Ice	18.00	9.00	500.00
(Sprint)			0.00			1/2" Ice	22.00	11.00	650.00
			0.00			1" Ice	26.00	13.00	800.00
12 ft Boom / Frame	В	From Leg	2.00	0.0000	171.00	No Ice	18.00	9.00	500.00
(Sprint)			0.00			1/2" Ice	22.00	11.00	650.00
			0.00			1" Ice	26.00	13.00	800.00
12 ft Boom / Frame	C	From Leg	2.00	0.0000	171.00	No Ice	18.00	9.00	500.00
(Sprint)			0.00			1/2" Ice	22.00	11.00	650.00
			0.00			1" Ice	26.00	13.00	800.00
RFS	A	From Leg	2.00	0.0000	171.00	No Ice	20.27	5.07	149.90
APXVAALL24_43-U-NA20			0.00			1/2" Ice	20.88	5.71	262.00
			0.00			1" Ice	21.50	6.33	382.00
Ericsson AIR6449 B41	A	From Leg	2.00	0.0000	171.00	No Ice	5.68	2.49	104.00
			0.00			1/2" Ice	5.95	2.71	143.00
			0.00			1" Ice	6.22	2.93	187.00
Ericsson Radio 4460	A	From Leg	2.00	0.0000	171.00	No Ice	2.56	1.98	109.00
B25+B66			0.00			1/2" Ice	2.74	2.14	134.00
			0.00			1" Ice	2.93	2.30	163.00
Ericsson Radio 4480	A	From Leg	2.00	0.0000	171.00	No Ice	2.85	1.38	84.00
B71+B85A			0.00			1/2" Ice	3.04	1.53	106.00
			0.00			1" Ice	3.24	4.69	131.00
RFS	В	From Leg	2.00	0.0000	171.00	No Ice	20.27	5.07	149.90
APXVAALL24_43-U-NA20			0.00			1/2" Ice	20.88	5.71	262.00
			0.00			1" Ice	21.50	6.33	382.00
Ericsson AIR6449 B41	В	From Leg	2.00	0.0000	171.00	No Ice	5.68	2.49	104.00
			0.00			1/2" Ice	5.95	2.71	143.00
	_		0.00			1" Ice	6.22	2.93	187.00
Ericsson Radio 4460	В	From Leg	2.00	0.0000	171.00	No Ice	2.56	1.98	109.00
B25+B66			0.00			1/2" Ice	2.74	2.14	134.00
T: T: 1100			0.00	0.0000	171.00	1" Ice	2.93	2.30	163.00
Ericsson Radio 4480	В	From Leg	2.00	0.0000	171.00	No Ice	2.85	1.38	84.00
B71+B85A			0.00			1/2" Ice	3.04	1.53	106.00
PEG			0.00	0.0000	171.00	1" Ice	3.24	4.69	131.00
RFS	С	From Leg	2.00	0.0000	171.00	No Ice	20.27	5.07	149.90
APXVAALL24_43-U-NA20			0.00			1/2" Ice	20.88	5.71	262.00
F : A ID (440 D41	C	г т	0.00	0.0000	171.00	1" Ice	21.50	6.33	382.00
Ericsson AIR6449 B41	С	From Leg	2.00	0.0000	171.00	No Ice	5.68	2.49	104.00
			0.00			1/2" Ice	5.95	2.71	143.00
Enissan D. 11 4460	C	F *	0.00	0.0000	171.00	1" Ice	6.22	2.93	187.00
Ericsson Radio 4460	С	From Leg	2.00	0.0000	171.00	No Ice	2.56	1.98	109.00
B25+B66			0.00			1/2" Ice	2.74	2.14	134.00
E-i D 1' 4400	C	F *	0.00	0.0000	171.00	1" Ice	2.93	2.30	163.00
Ericsson Radio 4480	С	From Leg	2.00	0.0000	171.00	No Ice	2.85	1.38	84.00
B71+B85A			0.00			1/2" Ice	3.04	1.53	106.00
			0.00			1" Ice	3.24	4.69	131.00

tnxTower	ob 121-23082	<b>Page</b> 18 of 48
	Project	Date
	180 ft Rohn #80 - Stafford Springs	CT 19:45:40 09/06/21
Phone: FAX:	Client CDT	Designed by

#### **Tower Pressures - No Ice**

 $G_H = 0.850$ 

Section	Z	$K_Z$	$q_z$	$A_G$	F	$A_F$	$A_R$	$A_{leg}$	Leg	$C_A A_A$	$C_A A_A$
Elevation					а				%	In	Out
					С					Face	Face
ft	ft		psf	$ft^2$	е	ft <sup>2</sup>	ft <sup>2</sup>	$ft^2$		$ft^2$	$ft^2$
T1	170.00	1.15	24	72.358	Α	0.806	16.613	7.917	45.45	0.750	0.000
180.00-160.00					В	0.806	16.613		45.45	12.705	0.000
					C	0.806	16.613		45.45	7.575	0.000
T2	150.00	1.11	23	72.358	Α	0.000	16.613	7.917	47.65	0.750	0.000
160.00-140.00					В	0.000	16.613		47.65	15.080	0.000
					C	0.000	16.613		47.65	13.500	0.000
Т3	130.00	1.065	22	72.358	Α	0.000	16.613	7.917	47.65	0.750	0.000
140.00-120.00					В	0.000	16.613		47.65	15.857	0.000
					C	0.000	16.613		47.65	13.500	0.000
T4	110.00	1.016	21	72.358	Α	0.806	16.210	7.917	46.53	0.750	0.000
120.00-100.00					В	0.806	16.210		46.53	17.300	0.000
					C	0.806	16.210		46.53	13.500	0.000
T5	90.00	0.959	20	73.192	Α	0.398	18.167	9.583	51.62	0.750	0.000
100.00-80.00					В	0.398	18.167		51.62	17.474	0.000
					C	0.398	18.167		51.62	13.500	0.000
T6 80.00-60.00	70.00	0.892	18	73.192	Α	0.000	14.273	9.583	67.14	0.750	0.000
					В	0.000	14.273		67.14	18.460	0.000
					C	0.000	14.273		67.14	13.500	0.000
T7 60.00-40.00	50.00	0.811	17	73.192	Α	0.000	14.273	9.583	67.14	0.750	0.000
					В	0.000	14.273		67.14	18.460	0.000
					C	0.000	14.273		67.14	13.500	0.000
T8 40.00-20.00	30.00	0.701	14	73.192	Α	0.000	14.273	9.583	67.14	0.750	0.000
					В	0.000	14.273		67.14	18.460	0.000
					C	0.000	14.273		67.14	13.500	0.000
T9 20.00-5.00	12.50	0.7	14	54.894	Α	0.000	10.892	7.188	65.99	0.525	0.000
					В	0.000	10.892		65.99	12.922	0.000
					C	0.000	10.892		65.99	9.450	0.000
T10 5.00-0.00	2.50	0.7	14	9.816	Α	0.000	4.968	2.576	51.85	0.000	0.000
					В	0.000	4.968		51.85	0.000	0.000
					С	0.000	4.968		51.85	0.000	0.000

#### **Tower Pressure - With Ice**

 $G_H = 0.850$ 

Section Elevation	z	$K_Z$	$q_z$	$t_Z$	$A_G$	F a	$A_F$	$A_R$	$A_{leg}$	Leg %	$C_AA_A$ In	$C_AA_A$ Out
ft	ft		psf	in	ft²	c e	ft²	ft²	ft²	, 0	Face ft <sup>2</sup>	Face ft <sup>2</sup>
T1	170.00	1.15	6	2.3563	80.213	Α	0.806	60.907	23.625	38.28	10.175	0.000
180.00-160.00						В	0.806	60.907		38.28	60.891	0.000
						С	0.806	60.907		38.28	26.757	0.000
T2	150.00	1.11	6	2.3270	80.115	Α	0.000	59.107	23.430	39.64	10.058	0.000
160.00-140.00						В	0.000	59.107		39.64	72.489	0.000
						С	0.000	59.107		39.64	47.634	0.000

tnxTower	Job	121-23082	<b>Page</b> 19 of 48
		121-23002	
	Project		Date
		180 ft Rohn #80 - Stafford Springs CT	19:45:40 09/06/21
	Client		Designed by
Phone:		CDT	
FAX:			

Section	z	$K_Z$	$q_z$	$t_Z$	$A_G$	F	$A_F$	$A_R$	$A_{leg}$	Leg	$C_A A_A$	$C_A A_A$
Elevation						а				%	In	Out
					_	$\mathcal{C}$	_	_	_		Face	Face
ft	ft		psf	in	$ft^2$	е	ft <sup>2</sup>	$ft^2$	$ft^2$		ft <sup>2</sup>	$ft^2$
T3	130.00	1.065	6	2.2939	80.005	A	0.000	58.503	23.209	39.67	9.926	0.000
140.00-120.00						В	0.000	58.503		39.67	75.718	0.000
						C	0.000	58.503		39.67	47.279	0.000
T4	110.00	1.016	6	2.2559	79.878	Α	0.806	57.406	22.956	39.44	9.774	0.000
120.00-100.00						В	0.806	57.406		39.44	82.100	0.000
						C	0.806	57.406		39.44	46.872	0.000
T5 100.00-80.00	90.00	0.959	5	2.2111	80.562	A	0.398	59.385	24.324	40.69	9.594	0.000
						В	0.398	59.385		40.69	82.391	0.000
						C	0.398	59.385		40.69	46.391	0.000
T6 80.00-60.00	70.00	0.892	5	2.1562	80.379	A	0.000	42.129	23.958	56.87	9.375	0.000
						В	0.000	42.129		56.87	89.195	0.000
						C	0.000	42.129		56.87	45.804	0.000
T7 60.00-40.00	50.00	0.811	4	2.0849	80.141	A	0.000	41.207	23.482	56.99	9.089	0.000
						В	0.000	41.207		56.99	86.986	0.000
						C	0.000	41.207		56.99	45.040	0.000
T8 40.00-20.00	30.00	0.701	4	1.9810	79.795	A	0.000	39.866	22.790	57.17	8.674	0.000
						В	0.000	39.866		57.17	83.771	0.000
						C	0.000	39.866		57.17	43.931	0.000
T9 20.00-5.00	12.50	0.7	4	1.8150	59.431	A	0.000	28.932	16.262	56.21	5.607	0.000
						В	0.000	28.932		56.21	55.042	0.000
						C	0.000	28.932		56.21	29.513	0.000
T10 5.00-0.00	2.50	0.7	4	1.5452	11.177	A	0.000	12.665	5.345	42.20	0.000	0.000
						В	0.000	12.665		42.20	0.000	0.000
						C	0.000	12.665		42.20	0.000	0.000

#### **Tower Pressure - Service**

 $G_H = 0.850$ 

Section	Z	$K_Z$	$q_z$	$A_G$	F	$A_F$	$A_R$	$A_{leg}$	Leg	$C_AA_A$	$C_AA_A$
Elevation			_		а			_	%	In	Out
					С					Face	Face
ft	ft		psf	$ft^2$	е	ft <sup>2</sup>	ft <sup>2</sup>	$ft^2$		$ft^2$	$ft^2$
T1	170.00	1.15	9	72.358	Α	0.806	16.613	7.917	45.45	0.750	0.000
180.00-160.00					В	0.806	16.613		45.45	12.705	0.000
					С	0.806	16.613		45.45	7.575	0.000
T2	150.00	1.11	9	72.358	Α	0.000	16.613	7.917	47.65	0.750	0.000
160.00-140.00					В	0.000	16.613		47.65	15.080	0.000
					С	0.000	16.613		47.65	13.500	0.000
T3	130.00	1.065	8	72.358	Α	0.000	16.613	7.917	47.65	0.750	0.000
140.00-120.00					В	0.000	16.613		47.65	15.857	0.000
					С	0.000	16.613		47.65	13.500	0.000
T4	110.00	1.016	8	72.358	Α	0.806	16.210	7.917	46.53	0.750	0.000
120.00-100.00					В	0.806	16.210		46.53	17.300	0.000
					С	0.806	16.210		46.53	13.500	0.000
T5	90.00	0.959	8	73.192	Α	0.398	18.167	9.583	51.62	0.750	0.000
100.00-80.00					В	0.398	18.167		51.62	17.474	0.000
					С	0.398	18.167		51.62	13.500	0.000
T6 80.00-60.00	70.00	0.892	7	73.192	Α	0.000	14.273	9.583	67.14	0.750	0.000
					В	0.000	14.273		67.14	18.460	0.000
					С	0.000	14.273		67.14	13.500	0.000
T7 60.00-40.00	50.00	0.811	6	73.192	Α	0.000	14.273	9.583	67.14	0.750	0.000
					В	0.000	14.273		67.14	18.460	0.000
					С	0.000	14.273		67.14	13.500	0.000
T8 40.00-20.00	30.00	0.701	5	73.192	Α	0.000	14.273	9.583	67.14	0.750	0.000

tnxTower	Job	121-23082	Page 20 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section	Z	$K_Z$	$q_z$	$A_G$	F	$A_F$	$A_R$	$A_{leg}$	Leg	$C_AA_A$	$C_AA_A$
Elevation					а				%	In	Out
					С					Face	Face
ft	ft		psf	$ft^2$	е	$ft^2$	$ft^2$	$ft^2$		ft <sup>2</sup>	$ft^2$
					В	0.000	14.273		67.14	18.460	0.000
					С	0.000	14.273		67.14	13.500	0.000
T9 20.00-5.00	12.50	0.7	5	54.894	Α	0.000	10.892	7.188	65.99	0.525	0.000
					В	0.000	10.892		65.99	12.922	0.000
					C	0.000	10.892		65.99	9.450	0.000
T10 5.00-0.00	2.50	0.7	5	9.816	Α	0.000	4.968	2.576	51.85	0.000	0.000
					В	0.000	4.968		51.85	0.000	0.000
					С	0.000	4.968		51.85	0.000	0.000

#### **Tower Forces - No Ice - Wind Normal To Face**

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf						
ft	lb	lb	е						ft <sup>2</sup>	lb	plf	
T1	180.92	552.04	Α	0.241	2.466	24	1	1	10.487	770.03	38.50	С
180.00-160.00			В	0.241	2.466		1	1	10.487			
			C	0.241	2.466		1	1	10.487			
T2	281.60	499.67	Α	0.23	2.5	23	1	1	9.640	805.24	40.26	С
160.00-140.00			В	0.23	2.5		1	1	9.640			
			C	0.23	2.5		1	1	9.640			
T3	285.38	499.67	Α	0.23	2.5	22	1	1	9.640	781.62	39.08	С
140.00-120.00			В	0.23	2.5		1	1	9.640			
			С	0.23	2.5		1	1	9.640			
T4	292.40	542.87	Α	0.235	2.483	21	1	1	10.232	783.50	39.18	С
120.00-100.00			В	0.235	2.483		1	1	10.232			
			С	0.235	2.483		1	1	10.232			
T5	293.15	676.58	Α	0.254	2.427	20	1	1	11.042	764.79	38.24	С
100.00-80.00		TA 320.88	В	0.254	2.427		1	1	11.042			
			С	0.254	2.427		1	1	11.042			
T6	297.40	568.31	Α	0.195	2.613	18	1	1	8.187	637.07	31.85	С
80.00-60.00			В	0.195	2.613		1	1	8.187			
			C	0.195	2.613		1	1	8.187			
T7	297.40	456.12	Α	0.195	2.613	17	1	1	8.187	578.68	28.93	С
60.00-40.00			В	0.195	2.613		1	1	8.187			
			С	0.195	2.613		1	1	8.187			
T8	297.40	456.12	Α	0.195	2.613	14	1	1	8.187	500.09	25.00	С
40.00-20.00			В	0.195	2.613		1	1	8.187			
			C	0.195	2.613		1	1	8.187			
T9 20.00-5.00	208.18	430.56	Α	0.198	2.601	14	1	1	6.254	365.55	24.37	С
			В	0.198	2.601		1	1	6.254			
			С	0.198	2.601		1	1	6.254			
T10 5.00-0.00	0.00	181.65	Α	0.506	1.892	14	1	1	3.420	78.82	15.76	С
			В	0.506	1.892		1	1	3.420			
			С	0.506	1.892		1	1	3.420			
Sum Weight:	2433.83	5184.46					-			6065.40		

#### **Tower Forces - No Ice - Wind 60 To Face**

tnxTower	Job	121-23082	Page 21 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf						
ft	lb	lb	е						$ft^2$	lb	plf	
T1	180.92	552.04	A	0.241	2.466	24	0.8	1	10.326	762.08	38.10	C
180.00-160.00			В	0.241	2.466		0.8	1	10.326			
			C	0.241	2.466		0.8	1	10.326			
T2	281.60	499.67	Α	0.23	2.5	23	0.8	1	9.640	805.24	40.26	C
160.00-140.00			В	0.23	2.5		0.8	1	9.640			
			C	0.23	2.5		0.8	1	9.640			
T3	285.38	499.67	Α	0.23	2.5	22	0.8	1	9.640	781.62	39.08	C
140.00-120.00			В	0.23	2.5		0.8	1	9.640			
			C	0.23	2.5		0.8	1	9.640			
T4	292.40	542.87	Α	0.235	2.483	21	0.8	1	10.071	776.43	38.82	C
120.00-100.00			В	0.235	2.483		0.8	1	10.071			
			C	0.235	2.483		0.8	1	10.071			
T5	293.15	676.58	Α	0.254	2.427	20	0.8	1	10.962	761.57	38.08	C
100.00-80.00		TA 320.88	В	0.254	2.427		0.8	1	10.962			
			C	0.254	2.427		0.8	1	10.962			
T6	297.40	568.31	Α	0.195	2.613	18	0.8	1	8.187	637.07	31.85	C
80.00-60.00			В	0.195	2.613		0.8	1	8.187			
			C	0.195	2.613		0.8	1	8.187			
T7	297.40	456.12	A	0.195	2.613	17	0.8	1	8.187	578.68	28.93	C
60.00-40.00			В	0.195	2.613		0.8	1	8.187			
			C	0.195	2.613		0.8	1	8.187			
T8	297.40	456.12	A	0.195	2.613	14	0.8	1	8.187	500.09	25.00	C
40.00-20.00			В	0.195	2.613		0.8	1	8.187			
			C	0.195	2.613		0.8	1	8.187			
T9 20.00-5.00	208.18	430.56	Α	0.198	2.601	14	0.8	1	6.254	365.55	24.37	C
			В	0.198	2.601		0.8	1	6.254			
			С	0.198	2.601		0.8	1	6.254			
T10 5.00-0.00	0.00	181.65	Α	0.506	1.892	14	0.8	1	3.420	78.82	15.76	C
			В	0.506	1.892		0.8	1	3.420			
			С	0.506	1.892		0.8	1	3.420			
Sum Weight:	2433.83	5184.46								6047.16		

#### **Tower Forces - No Ice - Wind 90 To Face**

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а			_						Face
			С			psf						
ft	lb	lb	е						$ft^2$	lb	plf	
T1	180.92	552.04	Α	0.241	2.466	24	0.85	1	10.366	764.07	38.20	С
180.00-160.00			В	0.241	2.466		0.85	1	10.366			
			С	0.241	2.466		0.85	1	10.366			
T2	281.60	499.67	Α	0.23	2.5	23	0.85	1	9.640	805.24	40.26	C
160.00-140.00			В	0.23	2.5		0.85	1	9.640			
			C	0.23	2.5		0.85	1	9.640			
T3	285.38	499.67	Α	0.23	2.5	22	0.85	1	9.640	781.62	39.08	С
140.00-120.00			В	0.23	2.5		0.85	1	9.640			
			С	0.23	2.5		0.85	1	9.640			
T4	292.40	542.87	Α	0.235	2.483	21	0.85	1	10.111	778.20	38.91	С
120.00-100.00			В	0.235	2.483		0.85	1	10.111			
			C	0.235	2.483		0.85	1	10.111			
T5	293.15	676.58	Α	0.254	2.427	20	0.85	1	10.982	762.37	38.12	С
100.00-80.00		TA 320.88	В	0.254	2.427		0.85	1	10.982			
			С	0.254	2.427		0.85	1	10.982			
T6	297.40	568.31	Α	0.195	2.613	18	0.85	1	8.187	637.07	31.85	С

tnxTower	Job	121-23082	Page 22 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а			_						Face
			С			psf						
ft	lb	lb	е						$ft^2$	lb	plf	
80.00-60.00			В	0.195	2.613		0.85	1	8.187			
			C	0.195	2.613		0.85	1	8.187			
T7	297.40	456.12	Α	0.195	2.613	17	0.85	1	8.187	578.68	28.93	C
60.00-40.00			В	0.195	2.613		0.85	1	8.187			
			C	0.195	2.613		0.85	1	8.187			
T8	297.40	456.12	Α	0.195	2.613	14	0.85	1	8.187	500.09	25.00	С
40.00-20.00			В	0.195	2.613		0.85	1	8.187			
			C	0.195	2.613		0.85	1	8.187			
T9 20.00-5.00	208.18	430.56	Α	0.198	2.601	14	0.85	1	6.254	365.55	24.37	C
			В	0.198	2.601		0.85	1	6.254			
			C	0.198	2.601		0.85	1	6.254			
T10 5.00-0.00	0.00	181.65	A	0.506	1.892	14	0.85	1	3.420	78.82	15.76	C
			В	0.506	1.892		0.85	1	3.420			
			C	0.506	1.892		0.85	1	3.420			
Sum Weight:	2433.83	5184.46								6051.72		

# **Tower Forces - With Ice - Wind Normal To Face**

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf			_			
ft	lb	lb	е						ft <sup>2</sup>	lb	plf	
T1	1692.72	3987.87	Α	0.769	1.797	6	1	1	53.310	629.26	31.46	C
180.00-160.00			В	0.769	1.797		1	1	53.310			
			С	0.769	1.797		1	1	53.310			
T2	2298.67	3711.87	Α	0.738	1.783	6	1	1	49.558	628.55	31.43	C
160.00-140.00			В	0.738	1.783		1	1	49.558			
			С	0.738	1.783		1	1	49.558			
T3	2326.41	3640.14	Α	0.731	1.781	6	1	1	48.771	603.81	30.19	C
140.00-120.00			В	0.731	1.781		1	1	48.771			
			С	0.731	1.781		1	1	48.771			
T4	2403.51	3645.41	Α	0.729	1.781	6	1	1	48.557	582.70	29.13	C
120.00-100.00			В	0.729	1.781		1	1	48.557			
			С	0.729	1.781		1	1	48.557			
T5	2364.07	3841.79	Α	0.742	1.785	5	1	1	50.377	556.88	27.84	C
100.00-80.00		TA	В	0.742	1.785		1	1	50.377			
		1032.51	С	0.742	1.785		1	1	50.377			
T6	2414.17	2529.17	Α	0.524	1.871	5	1	1	29.420	510.64	25.53	C
80.00-60.00			В	0.524	1.871		1	1	29.420			
			C	0.524	1.871		1	1	29.420			
T7	2309.35	2319.20	Α	0.514	1.882	4	1	1	28.547	458.41	22.92	C
60.00-40.00			В	0.514	1.882		1	1	28.547			
			С	0.514	1.882		1	1	28.547			
T8	2161.24	2180.93	Α	0.5	1.901	4	1	1	27.300	389.15	19.46	C
40.00-20.00			В	0.5	1.901		1	1	27.300			
			С	0.5	1.901		1	1	27.300			
T9 20.00-5.00	1354.71	1601.34	Α	0.487	1.918	4	1	1	19.615	271.52	18.10	C
			В	0.487	1.918		1	1	19.615			
			С	0.487	1.918		1	1	19.615			
T10 5.00-0.00	0.00	689.01	Α	1	2.1	4	1	1	12.665	$75.97^*$	15.19	C
			В	1	2.1		1	1	12.665			
			С	1	2.1		1	1	12.665			
Sum Weight:	19324.86	29179.25			*2.1A <sub>g</sub>					4706.88		
					limit							

tnxTower	Job	121-23082	Page 23 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

#### **Tower Forces - With Ice - Wind 60 To Face**

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а			_						Face
			С			psf						
ft	lb	lb	е						ft <sup>2</sup>	lb	plf	
T1	1692.72	3987.87	Α	0.769	1.797	6	0.8	1	53.149	627.72	31.39	С
180.00-160.00			В	0.769	1.797		0.8	1	53.149			
			С	0.769	1.797		0.8	1	53.149			
T2	2298.67	3711.87	Α	0.738	1.783	6	0.8	1	49.558	628.55	31.43	С
160.00-140.00			В	0.738	1.783		0.8	1	49.558			
			С	0.738	1.783		0.8	1	49.558			
T3	2326.41	3640.14	Α	0.731	1.781	6	0.8	1	48.771	603.81	30.19	С
140.00-120.00			В	0.731	1.781		0.8	1	48.771			
			С	0.731	1.781		0.8	1	48.771			
T4	2403.51	3645.41	Α	0.729	1.781	6	0.8	1	48.396	581.35	29.07	С
120.00-100.00			В	0.729	1.781		0.8	1	48.396			
			С	0.729	1.781		0.8	1	48.396			
T5	2364.07	3841.79	Α	0.742	1.785	5	0.8	1	50.298	556.25	27.81	С
100.00-80.00		TA	В	0.742	1.785		0.8	1	50.298			
		1032.51	С	0.742	1.785		0.8	1	50.298			
T6	2414.17	2529.17	Α	0.524	1.871	5	0.8	1	29.420	510.64	25.53	С
80.00-60.00			В	0.524	1.871		0.8	1	29.420			
			С	0.524	1.871		0.8	1	29.420			
T7	2309.35	2319.20	Α	0.514	1.882	4	0.8	1	28.547	458.41	22.92	С
60.00-40.00			В	0.514	1.882		0.8	1	28.547			
			C	0.514	1.882		0.8	1	28.547			
T8	2161.24	2180.93	Α	0.5	1.901	4	0.8	1	27.300	389.15	19.46	С
40.00-20.00			В	0.5	1.901		0.8	1	27.300			
			С	0.5	1.901		0.8	1	27.300			
T9 20.00-5.00	1354.71	1601.34	Α	0.487	1.918	4	0.8	1	19.615	271.52	18.10	С
			В	0.487	1.918		0.8	1	19.615			
			С	0.487	1.918		0.8	1	19.615			
T10 5.00-0.00	0.00	689.01	Α	1	2.1	4	0.8	1	12.665	75.97*	15.19	C
			В	1	2.1		0.8	1	12.665			
			С	1	2.1		0.8	1	12.665			
Sum Weight:	19324.86	29179.25			*2.1A <sub>g</sub>					4703.37		
					limit							

#### **Tower Forces - With Ice - Wind 90 To Face**

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf						
ft	lb	lb	е						$ft^2$	lb	plf	
T1	1692.72	3987.87	Α	0.769	1.797	6	0.85	1	53.190	628.11	31.41	С
180.00-160.00			В	0.769	1.797		0.85	1	53.190			
			С	0.769	1.797		0.85	1	53.190			
T2	2298.67	3711.87	Α	0.738	1.783	6	0.85	1	49.558	628.55	31.43	С
160.00-140.00			В	0.738	1.783		0.85	1	49.558			
			С	0.738	1.783		0.85	1	49.558			
Т3	2326.41	3640.14	A	0.731	1.781	6	0.85	1	48.771	603.81	30.19	C

tnxTower	Job	121-23082	Page 24 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section	Add	Self	F	e	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а			-						Face
			С			psf						
ft	lb	lb	е						$ft^2$	lb	plf	
140.00-120.00			В	0.731	1.781		0.85	1	48.771			
			С	0.731	1.781		0.85	1	48.771			
T4	2403.51	3645.41	Α	0.729	1.781	6	0.85	1	48.436	581.69	29.08	C
120.00-100.00			В	0.729	1.781		0.85	1	48.436			
			C	0.729	1.781		0.85	1	48.436			
T5	2364.07	3841.79	Α	0.742	1.785	5	0.85	1	50.317	556.41	27.82	C
100.00-80.00		TA	В	0.742	1.785		0.85	1	50.317			
		1032.51	С	0.742	1.785		0.85	1	50.317			
T6	2414.17	2529.17	Α	0.524	1.871	5	0.85	1	29.420	510.64	25.53	C
80.00-60.00			В	0.524	1.871		0.85	1	29.420			
			C	0.524	1.871		0.85	1	29.420			
T7	2309.35	2319.20	Α	0.514	1.882	4	0.85	1	28.547	458.41	22.92	C
60.00-40.00			В	0.514	1.882		0.85	1	28.547			
			С	0.514	1.882		0.85	1	28.547			
T8	2161.24	2180.93	Α	0.5	1.901	4	0.85	1	27.300	389.15	19.46	C
40.00-20.00			В	0.5	1.901		0.85	1	27.300			
			С	0.5	1.901		0.85	1	27.300			
T9 20.00-5.00	1354.71	1601.34	Α	0.487	1.918	4	0.85	1	19.615	271.52	18.10	C
			В	0.487	1.918		0.85	1	19.615			
			C	0.487	1.918		0.85	1	19.615			
T10 5.00-0.00	0.00	689.01	Α	1	2.1	4	0.85	1	12.665	75.97*	15.19	C
			В	1	2.1		0.85	1	12.665			
			С	1	2.1		0.85	1	12.665			
Sum Weight:	19324.86	29179.25			*2.1A <sub>g</sub>					4704.25		
					limit							

#### **Tower Forces - Service - Wind Normal To Face**

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf						
ft	lb	lb	е						$ft^2$	lb	plf	
T1	180.92	552.04	Α	0.241	2.466	9	1	1	10.487	294.62	14.73	С
180.00-160.00			В	0.241	2.466		1	1	10.487			
			C	0.241	2.466		1	1	10.487			
T2	281.60	499.67	Α	0.23	2.5	9	1	1	9.640	308.10	15.40	С
160.00-140.00			В	0.23	2.5		1	1	9.640			
			C	0.23	2.5		1	1	9.640			
T3	285.38	499.67	Α	0.23	2.5	8	1	1	9.640	299.06	14.95	С
140.00-120.00			В	0.23	2.5		1	1	9.640			
			C	0.23	2.5		1	1	9.640			
T4	292.40	542.87	Α	0.235	2.483	8	1	1	10.232	299.78	14.99	С
120.00-100.00			В	0.235	2.483		1	1	10.232			
			C	0.235	2.483		1	1	10.232			
T5	293.15	676.58	Α	0.254	2.427	8	1	1	11.042	292.62	14.63	С
100.00-80.00		TA 320.88	В	0.254	2.427		1	1	11.042			
			С	0.254	2.427		1	1	11.042			
T6	297.40	568.31	Α	0.195	2.613	7	1	1	8.187	243.75	12.19	С
80.00-60.00			В	0.195	2.613		1	1	8.187			
			С	0.195	2.613		1	1	8.187			
T7	297.40	456.12	Α	0.195	2.613	6	1	1	8.187	221.41	11.07	С
60.00-40.00			В	0.195	2.613		1	1	8.187			
			C	0.195	2.613		1	1	8.187			
Т8	297.40	456.12	Α	0.195	2.613	5	1	1	8.187	191.34	9.57	С

tnxTower	Job	121-23082	Page 25 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf						
ft	lb	lb	е						$ft^2$	lb	plf	
40.00-20.00			В	0.195	2.613		1	1	8.187			
			С	0.195	2.613		1	1	8.187			
T9 20.00-5.00	208.18	430.56	Α	0.198	2.601	5	1	1	6.254	139.86	9.32	C
			В	0.198	2.601		1	1	6.254			
			С	0.198	2.601		1	1	6.254			
T10 5.00-0.00	0.00	181.65	Α	0.506	1.892	5	1	1	3.420	30.16	6.03	C
			В	0.506	1.892		1	1	3.420			
			С	0.506	1.892		1	1	3.420			
Sum Weight:	2433.83	5184.46								2320.70		

#### **Tower Forces - Service - Wind 60 To Face**

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf						
ft	lb	lb	е						$ft^2$	lb	plf	
T1	180.92	552.04	Α	0.241	2.466	9	0.8	1	10.326	291.58	14.58	С
180.00-160.00			В	0.241	2.466		0.8	1	10.326			
			C	0.241	2.466		0.8	1	10.326			
T2	281.60	499.67	Α	0.23	2.5	9	0.8	1	9.640	308.10	15.40	C
160.00-140.00			В	0.23	2.5		0.8	1	9.640			
			C	0.23	2.5		0.8	1	9.640			
T3	285.38	499.67	Α	0.23	2.5	8	0.8	1	9.640	299.06	14.95	C
140.00-120.00			В	0.23	2.5		0.8	1	9.640			
			C	0.23	2.5		0.8	1	9.640			
T4	292.40	542.87	Α	0.235	2.483	8	0.8	1	10.071	297.07	14.85	С
120.00-100.00			В	0.235	2.483		0.8	1	10.071			
			C	0.235	2.483		0.8	1	10.071			
T5	293.15	676.58	Α	0.254	2.427	8	0.8	1	10.962	291.38	14.57	С
100.00-80.00		TA 320.88	В	0.254	2.427		0.8	1	10.962			
			C	0.254	2.427		0.8	1	10.962			
T6	297.40	568.31	Α	0.195	2.613	7	0.8	1	8.187	243.75	12.19	С
80.00-60.00			В	0.195	2.613		0.8	1	8.187			
			C	0.195	2.613		0.8	1	8.187			
T7	297.40	456.12	Α	0.195	2.613	6	0.8	1	8.187	221.41	11.07	С
60.00-40.00			В	0.195	2.613		0.8	1	8.187			
			C	0.195	2.613		0.8	1	8.187			
T8	297.40	456.12	Α	0.195	2.613	5	0.8	1	8.187	191.34	9.57	С
40.00-20.00			В	0.195	2.613		0.8	1	8.187			
			C	0.195	2.613		0.8	1	8.187			
T9 20.00-5.00	208.18	430.56	A	0.198	2.601	5	0.8	1	6.254	139.86	9.32	С
			В	0.198	2.601		0.8	1	6.254			
			С	0.198	2.601		0.8	1	6.254			
T10 5.00-0.00	0.00	181.65	Α	0.506	1.892	5	0.8	1	3.420	30.16	6.03	С
			В	0.506	1.892		0.8	1	3.420			
			С	0.506	1.892		0.8	1	3.420			
Sum Weight:	2433.83	5184.46								2313.72		

#### **Tower Forces - Service - Wind 90 To Face**

tnxTower	Job	121-23082	Page 26 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section	Add	Self	F	е	$C_F$	$q_z$	$D_F$	$D_R$	$A_E$	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf						
ft	lb	lb	е						ft <sup>2</sup>	lb	plf	
T1	180.92	552.04	Α	0.241	2.466	9	0.85	1	10.366	292.34	14.62	C
180.00-160.00			В	0.241	2.466		0.85	1	10.366			
			С	0.241	2.466		0.85	1	10.366			
T2	281.60	499.67	Α	0.23	2.5	9	0.85	1	9.640	308.10	15.40	С
160.00-140.00			В	0.23	2.5		0.85	1	9.640			
			С	0.23	2.5		0.85	1	9.640			
T3	285.38	499.67	A	0.23	2.5	8	0.85	1	9.640	299.06	14.95	С
140.00-120.00			В	0.23	2.5		0.85	1	9.640			
	202.40	5.40.05	C	0.23	2.5	0	0.85	1	9.640	207.75	1.4.00	
T4	292.40	542.87	A	0.235	2.483	8	0.85	1	10.111	297.75	14.89	С
120.00-100.00			В	0.235	2.483		0.85	1	10.111			
TE	202.15	(7( 50	C	0.235	2.483	0	0.85	1	10.111	201.60	14.50	
T5 100.00-80.00	293.15	676.58	A B	0.254 0.254	2.427 2.427	8	0.85 0.85	1 1	10.982 10.982	291.69	14.58	С
100.00-80.00		TA 320.88	С	0.254	2.427		0.85	1	10.982			
Т6	297.40	568.31	A	0.254	2.427	7	0.85	1	8.187	243.75	12.19	С
80.00-60.00	297.40	308.31	В	0.195	2.613	/	0.85	1	8.187	243.73	12.19	C
80.00-00.00			C	0.195	2.613		0.85	1	8.187			
Т7	297.40	456.12	A	0.195	2.613	6	0.85	1	8.187	221.41	11.07	С
60.00-40.00	277.40	730.12	В	0.195	2.613	O	0.85	1	8.187	221.71	11.07	
00.00 10.00			C	0.195	2.613		0.85	1	8.187			
Т8	297.40	456.12	A	0.195	2.613	5	0.85	1	8.187	191.34	9.57	С
40.00-20.00	2,,		В	0.195	2.613		0.85	1	8.187	1,71.5 .	,,	
			C	0.195	2.613		0.85	1	8.187			
T9 20.00-5.00	208.18	430.56	A	0.198	2.601	5	0.85	1	6.254	139.86	9.32	С
			В	0.198	2.601		0.85	1	6.254			
			С	0.198	2.601		0.85	1	6.254			
T10 5.00-0.00	0.00	181.65	Α	0.506	1.892	5	0.85	1	3.420	30.16	6.03	С
			В	0.506	1.892		0.85	1	3.420			
			С	0.506	1.892		0.85	1	3.420			
Sum Weight:	2433.83	5184.46								2315.46		

## Force Totals (Does not include forces on guys)

Load	Vertical	Sum of	Sum of	Sum of Torques
Case	Forces	Forces	Forces	
		X	Z	
	lb	lb	lb	lb-ft
Leg Weight	3291.20			
Bracing Weight	1893.26			
Total Member Self-Weight	5184.46			
Guy Weight	1520.64			
Total Weight	13827.83			
Wind 0 deg - No Ice		0.00	-9176.89	2299.71
Wind 30 deg - No Ice		4581.61	-7935.58	2883.23
Wind 60 deg - No Ice		7931.63	-4579.33	2694.19
Wind 90 deg - No Ice		9163.22	0.00	1783.25
Wind 120 deg - No Ice		7947.42	4588.45	394.49
Wind 150 deg - No Ice		4581.61	7935.58	-1099.98
Wind 180 deg - No Ice		0.00	9158.66	-2299.71
Wind 210 deg - No Ice		-4581.61	7935.58	-2883.23
Wind 240 deg - No Ice		-7947.42	4588.45	-2694.19
Wind 270 deg - No Ice		-9163.22	0.00	-1783.25

tnxTower	Job	121-23082	Page
litx I ower		27 of 48	
	Project		Date
		180 ft Rohn #80 - Stafford Springs CT	19:45:40 09/06/21
	Client		Designed by
Phone:		CDT	
FAX:			

Load	Vertical	Sum of	Sum of	Sum of Torques
Case	Forces	Forces	Forces	J
		X	Z	
	lb	lb	lb	lb-ft
Wind 300 deg - No Ice		-7931.63	-4579.33	-394.49
Wind 330 deg - No Ice		-4581.61	-7935.58	1099.98
Member Ice	23994.80			
Guy Ice	14889.73			
Total Weight Ice	79026.47			
Wind 0 deg - Ice		0.00	-6549.42	1659.20
Wind 30 deg - Ice		3273.39	-5669.68	1919.06
Wind 60 deg - Ice		5668.92	-3272.95	1664.71
Wind 90 deg - Ice		6546.78	0.00	964.30
Wind 120 deg - Ice		5671.96	3274.71	5.50
Wind 150 deg - Ice		3273.39	5669.68	-954.76
Wind 180 deg - Ice		0.00	6545.90	-1659.20
Wind 210 deg - Ice		-3273.39	5669.68	-1919.06
Wind 240 deg - Ice		-5671.96	3274.71	-1664.71
Wind 270 deg - Ice		-6546.78	0.00	-964.30
Wind 300 deg - Ice		-5668.92	-3272.95	-5.50
Wind 330 deg - Ice		-3273.39	-5669.68	954.76
Total Weight	13827.83			
Wind 0 deg - Service		0.00	-3511.19	879.90
Wind 30 deg - Service		1752.98	-3036.25	1103.16
Wind 60 deg - Service		3034.74	-1752.11	1030.83
Wind 90 deg - Service		3505.96	0.00	682.29
Wind 120 deg - Service		3040.78	1755.60	150.94
Wind 150 deg - Service		1752.98	3036.25	-420.87
Wind 180 deg - Service		0.00	3504.22	-879.90
Wind 210 deg - Service		-1752.98	3036.25	-1103.16
Wind 240 deg - Service		-3040.78	1755.60	-1030.83
Wind 270 deg - Service		-3505.96	0.00	-682.29
Wind 300 deg - Service		-3034.74	-1752.11	-150.94
Wind 330 deg - Service		-1752.98	-3036.25	420.87

## **Load Combinations**

Comb.	Description
No.	
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy
3	1.2D+1.6W (pattern 1) 0 deg - No Ice+1.0 Guy
4	1.2D+1.6W (pattern 2) 0 deg - No Ice+1.0 Guy
5	1.2D+1.6W (pattern 3) 0 deg - No Ice+1.0 Guy
6	1.2D+1.6W (pattern 4) 0 deg - No Ice+1.0 Guy
7	1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy
8	1.2D+1.6W (pattern 1) 30 deg - No Ice+1.0 Guy
9	1.2D+1.6W (pattern 2) 30 deg - No Ice+1.0 Guy
10	1.2D+1.6W (pattern 3) 30 deg - No Ice+1.0 Guy
11	1.2D+1.6W (pattern 4) 30 deg - No Ice+1.0 Guy
12	1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy
13	1.2D+1.6W (pattern 1) 60 deg - No Ice+1.0 Guy
14	1.2D+1.6W (pattern 2) 60 deg - No Ice+1.0 Guy
15	1.2D+1.6W (pattern 3) 60 deg - No Ice+1.0 Guy
16	1.2D+1.6W (pattern 4) 60 deg - No Ice+1.0 Guy
17	1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy
18	1.2D+1.6W (pattern 1) 90 deg - No Ice+1.0 Guy
19	1.2D+1.6W (pattern 2) 90 deg - No Ice+1.0 Guy

tnxTower	Job 121-23082	Page 28 of 48
	Project 180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	Designed by

mb.	Description
Vo.	1.2D   1.6W (nottorn 2) 00 dec. No Ioo   1.0 C
20	1.2D+1.6W (pattern 3) 90 deg - No Ice+1.0 Guy
21	1.2D+1.6W (pattern 4) 90 deg - No Ice+1.0 Guy
22	1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy
23	1.2D+1.6W (pattern 1) 120 deg - No Ice+1.0 Guy
24	1.2D+1.6W (pattern 2) 120 deg - No Ice+1.0 Guy
25	1.2D+1.6W (pattern 3) 120 deg - No Ice+1.0 Guy
26	1.2D+1.6W (pattern 4) 120 deg - No Ice+1.0 Guy
27	1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy
28	1.2D+1.6W (pattern 1) 150 deg - No Ice+1.0 Guy
29	1.2D+1.6W (pattern 2) 150 deg - No Ice+1.0 Guy
30	1.2D+1.6W (pattern 3) 150 deg - No Ice+1.0 Guy
31	1.2D+1.6W (pattern 4) 150 deg - No Ice+1.0 Guy
32	1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy
33	1.2D+1.6W (pattern 1) 180 deg - No Ice+1.0 Guy
34	1.2D+1.6W (pattern 2) 180 deg - No Ice+1.0 Guy
35	1.2D+1.6W (pattern 3) 180 deg - No Ice+1.0 Guy
36	1.2D+1.6W (pattern 4) 180 deg - No Ice+1.0 Guy
37	1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy
38	1.2D+1.6W (pattern 1) 210 deg - No Ice+1.0 Guy
39	1.2D+1.6W (pattern 2) 210 deg - No Ice+1.0 Guy
40	1.2D+1.6W (pattern 3) 210 deg - No Ice+1.0 Guy
41	1.2D+1.6W (pattern 4) 210 deg - No Ice+1.0 Guy
42	1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy
43	1.2D+1.6W (pattern 1) 240 deg - No Ice+1.0 Guy
44	1.2D+1.6W (pattern 2) 240 deg - No Ice+1.0 Guy
45	1.2D+1.6W (pattern 3) 240 deg - No Ice+1.0 Guy
46	1.2D+1.6W (pattern 4) 240 deg - No Ice+1.0 Guy
47	1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy
48	1.2D+1.6W (pattern 1) 270 deg - No Ice+1.0 Guy
49	1.2D+1.6W (pattern 2) 270 deg - No Ice+1.0 Guy
50	1.2D+1.6W (pattern 3) 270 deg - No Ice+1.0 Guy
51	1.2D+1.6W (pattern 4) 270 deg - No Ice+1.0 Guy
52	1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy
53	1.2D+1.6W (pattern 1) 300 deg - No Ice+1.0 Guy
54	1.2D+1.6W (pattern 2) 300 deg - No Ice+1.0 Guy
55	1.2D+1.6W (pattern 3) 300 deg - No Ice+1.0 Guy
56	1.2D+1.6W (pattern 4) 300 deg - No Ice+1.0 Guy
57	1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy
58	1.2D+1.6W (pattern 1) 330 deg - No Ice+1.0 Guy
59	1.2D+1.6W (pattern 2) 330 deg - No Ice+1.0 Guy
60	1.2D+1.6W (pattern 3) 330 deg - No Ice+1.0 Guy
61	1.2D+1.6W (pattern 4) 330 deg - No Ice+1.0 Guy
62	1.2 Dead+1.0 Ice+1.0 Temp+Guy
63	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy
64	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy
65	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy
66	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy
67	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy
68	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy
69	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy
70	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy
71	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy
72	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy
73	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy
74	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy
75	Dead+Wind 0 deg - Service+Guy
76	Dead+Wind 30 deg - Service+Guy
77	Dead+Wind 50 deg - Service+Guy  Dead+Wind 60 deg - Service+Guy
78	Dead+Wind 90 deg - Service+Guy
79	Dead+Wind 120 deg - Service+Guy
	Dead+Wind 150 deg - Service+Guy  Dead+Wind 150 deg - Service+Guy
80	

tnxTower	Job	121-23082	<b>Page</b> 29 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Comb.	Description
No.	
82	Dead+Wind 210 deg - Service+Guy
83	Dead+Wind 240 deg - Service+Guy
84	Dead+Wind 270 deg - Service+Guy
85	Dead+Wind 300 deg - Service+Guy
86	Dead+Wind 330 deg - Service+Guy

## **Maximum Reactions**

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, Z
		Load	lb	lb	lb
		Comb.			
Mast	Max. Vert	67	127812.69	-372.44	-236.95
	Max. H <sub>x</sub>	50	46621.27	1244.32	26.36
	Max. H <sub>z</sub>	5	45775.39	3.46	1260.56
	Max. M <sub>x</sub>	1	0.00	2.83	7.68
	Max. M <sub>z</sub>	1	0.00	2.83	7.68
	Max. Torsion	37	568.04	533.52	-979.26
	Min. Vert	1	40311.38	2.83	7.68
	Min. H <sub>x</sub>	20	46641.77	-1235.38	26.14
	Min. H <sub>z</sub>	35	46951.51	5.65	-1244.73
	Min. M <sub>x</sub>	1	0.00	2.83	7.68
	Min. M <sub>z</sub>	1	0.00	2.83	7.68
	Min. Torsion	7	-607.59	-587.97	963.13
Guy C @ 140 ft	Max. Vert	42	-1606.75	-1918.91	1116.87
Elev 0 ft					
Azimuth 240 deg					
	Max. H <sub>x</sub>	42	-1606.75	-1918.91	1116.87
	Max. H <sub>z</sub>	65	-19400.68	-23066.76	13312.58
	Min. Vert	65	-19400.68	-23066.76	13312.58
	Min. H <sub>x</sub>	65	-19400.68	-23066.76	13312.58
	Min. H <sub>z</sub>	42	-1606.75	-1918.91	1116.87
Guy B @ 140 ft Elev 0 ft	Max. Vert	22	-1603.72	1920.09	1109.92
Azimuth 120 deg					
	$Max. H_x$	73	-19279.91	23004.32	13281.15
	Max. H <sub>z</sub>	73	-19279.91	23004.32	13281.15
	Min. Vert	73	-19279.91	23004.32	13281.15
	Min. H <sub>x</sub>	22	-1603.72	1920.09	1109.92
	Min. H <sub>z</sub>	22	-1603.72	1920.09	1109.92
Guy A @ 140 ft Elev 0 ft	Max. Vert	2	-1603.67	6.51	-2212.55
Azimuth 0 deg					
	Max. H <sub>x</sub>	72	-15290.17	674.57	-21684.68
	Max. H <sub>z</sub>	2	-1603.67	6.51	-2212.55
	Min. Vert	69	-19396.42	-4.41	-26610.21
	Min. H <sub>x</sub>	66	-15309.16	-675.25	-21698.91
	Min. H <sub>z</sub>	69	-19396.42	-4.41	-26610.21

## **Tower Mast Reaction Summary**

Load Combination	Vertical	$Shear_x$	Shear <sub>z</sub>	Overturning Moment, $M_x$	Overturning Moment, M <sub>z</sub>	Torque
	lb	lb	lb	lb-ft	lb-ft	lb-ft
Dead Only	40311.38	-2.83	-7.68	0.00	0.00	14.84
1.2 Dead+1.6 Wind 0 deg - No	47413.57	-3.64	-1118.03	0.00	0.00	510.01

tnxTower	Job	121-23082	90 Page 30 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Load Combination	Vertical	$Shear_x$	$Shear_z$	Overturning Moment, $M_x$	Overturning Moment, $M_z$	Torque
	lb	lb	lb	lb-ft	lb-ft	lb-ft
ce+1.0 Guy 1.2D+1.6W (pattern 1) 0 deg - No Ice+1.0 Guy	47578.39	-3.43	-441.21	0.00	0.00	506.
2D+1.6W (pattern 2) 0 deg - No Ice+1.0 Guy	47109.41	-3.20	-1147.07	0.00	0.00	502.
.2D+1.6W (pattern 3) 0 deg - No Ice+1.0 Guy	45775.39	-3.46	-1260.56	0.00	0.00	476.
.2D+1.6W (pattern 4) 0 deg - No Ice+1.0 Guy	44687.58	-3.86	-1235.96	0.00	0.00	509.
.2 Dead+1.6 Wind 30 deg - No ce+1.0 Guy	47810.71	587.97	-963.13	0.00	0.00	607.
.2D+1.6W (pattern 1) 30 deg - lo Ice+1.0 Guy	47836.19	253.58	-375.44	0.00	0.00	592.
.2D+1.6W (pattern 2) 30 deg - lo Ice+1.0 Guy	47509.62	595.49	-982.41	0.00	0.00	591
.2D+1.6W (pattern 3) 30 deg - lo Ice+1.0 Guy	46607.73	630.22	-1077.76	0.00	0.00	566.
2D+1.6W (pattern 4) 30 deg - lo Ice+1.0 Guy	45937.89	600.91	-1051.13	0.00	0.00	593
.2 Dead+1.6 Wind 60 deg - No ce+1.0 Guy	47566.08	999.65	-591.35	0.00	0.00	508
2D+1.6W (pattern 1) 60 deg - lo Ice+1.0 Guy	47481.56	416.50	-254.65	0.00	0.00	499
2D+1.6W (pattern 2) 60 deg - lo Ice+1.0 Guy	47316.84	1011.95	-598.01	0.00	0.00	496
2D+1.6W (pattern 3) 60 deg - o Ice+1.0 Guy	46948.89	1081.53	-638.00	0.00	0.00	469
2D+1.6W (pattern 4) 60 deg - o Ice+1.0 Guy	46671.52	1037.29	-612.68	0.00	0.00	474
2 Dead+1.6 Wind 90 deg - No ee+1.0 Guy	47857.22	1114.53	-47.82	0.00	0.00	256
.2D+1.6W (pattern 1) 90 deg - lo Ice+1.0 Guy	47890.11	438.16	-51.46	0.00	0.00	255
2D+1.6W (pattern 2) 90 deg - o Ice+1.0 Guy	47561.06	1134.78	-43.56	0.00	0.00	250
2D+1.6W (pattern 3) 90 deg - fo Ice+1.0 Guy	46641.77	1235.38	-26.14	0.00	0.00	232
2D+1.6W (pattern 4) 90 deg - o Ice+1.0 Guy	45938.21 47485.60	1198.42	-14.69	0.00	0.00	217 -13
2 Dead+1.6 Wind 120 deg - to Ice+1.0 Guy 2D+1.6W (pattern 1) 120 deg	47483.86	953.47 367.57	543.81 205.43	0.00	0.00	-13
No Ice+1.0 Guy 2D+1.6W (pattern 2) 120 deg	47182.76	978.94	558.59	0.00	0.00	-13
No Ice+1.0 Guy 2D+1.6W (pattern 3) 120 deg	45833.89	1077.47	615.42	0.00	0.00	-13
No Ice+1.0 Guy 2D+1.6W (pattern 4) 120 deg	44698.81	1056.97	603.43	0.00	0.00	-41
No Ice+1.0 Guy 2 Dead+1.6 Wind 150 deg -	47850.32	521.79	978.71	0.00	0.00	-268
o Ice+1.0 Guy 2D+1.6W (pattern 1) 150 deg	47883.97	180.65	394.75	0.00	0.00	-269
No Ice+1.0 Guy 2D+1.6W (pattern 2) 150 deg	47555.00	535.55	994.27	0.00	0.00	-264
No Ice+1.0 Guy 2D+1.6W (pattern 3) 150 deg	46637.01	601.01	1072.63	0.00	0.00	-246
No Ice+1.0 Guy 2D+1.6W (pattern 4) 150 deg	45937.73	592.38	1034.75	0.00	0.00	-282
No Ice+1.0 Guy 2 Dead+1.6 Wind 180 deg - o Ice+1.0 Guy	47569.17	-6.08	1150.46	0.00	0.00	-496

tnxTower	Job	121-23082	Page 31 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overturning Moment, $M_x$	Overturning Moment, $M_z$	Torque
	lb	lb	lb	lb-ft	lb-ft	lb-ft
1.2D+1.6W (pattern 1) 180 deg	47485.54	-5.85	477.09	0.00	0.00	-489.77
- No Ice+1.0 Guy 1.2D+1.6W (pattern 2) 180 deg	47320.64	-5.77	1164.45	0.00	0.00	-485.75
- No Ice+1.0 Guy 1.2D+1.6W (pattern 3) 180 deg	46951.51	-5.65	1244.73	0.00	0.00	-459.02
- No Ice+1.0 Guy 1.2D+1.6W (pattern 4) 180 deg - No Ice+1.0 Guy	46675.42	-6.02	1193.82	0.00	0.00	-494.99
1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy	47845.36	-533.52	979.26	0.00	0.00	-568.04
1.2D+1.6W (pattern 1) 210 deg - No Ice+1.0 Guy	47872.13	-191.56	396.01	0.00	0.00	-553.36
1.2D+1.6W (pattern 2) 210 deg - No Ice+1.0 Guy	47545.40	-546.39	995.40	0.00	0.00	-552.02
1.2D+1.6W (pattern 3) 210 deg - No Ice+1.0 Guy	46634.04	-611.89	1073.30	0.00	0.00	-527.87
1.2D+1.6W (pattern 4) 210 deg - No Ice+1.0 Guy	45951.86	-603.71	1034.73	0.00	0.00	-555.20
1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy	47464.39	-963.23	544.12	0.00	0.00	-438.58
1.2D+1.6W (pattern 1) 240 deg - No Ice+1.0 Guy	47628.98	-376.76	206.19	0.00	0.00	-433.72
1.2D+1.6W (pattern 2) 240 deg - No Ice+1.0 Guy	47158.54	-988.11	559.09	0.00	0.00	-430.71
1.2D+1.6W (pattern 3) 240 deg - No Ice+1.0 Guy	45816.17	-1086.73	615.67	0.00	0.00	-406.51
1.2D+1.6W (pattern 4) 240 deg - No Ice+1.0 Guy	44703.77	-1066.11	603.14	0.00	0.00	-412.74
1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy	47831.18	-1123.52	-48.00	0.00	0.00	-217.46
1.2D+1.6W (pattern 1) 270 deg - No Ice+1.0 Guy	47862.93	-447.09	-51.37	0.00	0.00	-215.94
1.2D+1.6W (pattern 2) 270 deg - No Ice+1.0 Guy	47535.11	-1143.69	-43.78	0.00	0.00	-211.16
1.2D+1.6W (pattern 3) 270 deg - No Ice+1.0 Guy	46621.27	-1244.32	-26.36	0.00	0.00	-194.54
1.2D+1.6W (pattern 4) 270 deg - No Ice+1.0 Guy	45928.10	-1207.04	-15.11	0.00	0.00	-180.38
1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy 1.2D+1.6W (pattern 1) 300 deg	47539.01 47454.71	-1008.29 -425.35	-590.32 -253.57	0.00	0.00	46.84 48.28
- No Ice+1.0 Guy 1.2D+1.6W (pattern 2) 300 deg	47291.48	-1020.47	-597.28	0.00	0.00	48.19
- No Ice+1.0 Guy 1.2D+1.6W (pattern 3) 300 deg	46927.75	-1020.47	-637.39	0.00	0.00	47.01
- No Ice+1.0 Guy 1.2D+1.6W (pattern 4) 300 deg	46651.02	-1045.95	-611.73	0.00	0.00	77.47
- No Ice+1.0 Guy 1.2 Dead+1.6 Wind 330 deg -	47790.83	-596.38	-961.20	0.00	0.00	307.89
No Ice+1.0 Guy 1.2D+1.6W (pattern 1) 330 deg	47821.65	-261.48	-373.60	0.00	0.00	309.16
- No Ice+1.0 Guy 1.2D+1.6W (pattern 2) 330 deg	47494.50	-602.96	-980.89	0.00	0.00	303.74
- No Ice+1.0 Guy 1.2D+1.6W (pattern 3) 330 deg	46590.96	-638.12	-1076.43	0.00	0.00	284.39
- No Ice+1.0 Guy 1.2D+1.6W (pattern 4) 330 deg	45913.99	-609.65	-1049.41	0.00	0.00	319.86
- No Ice+1.0 Guy 1.2 Dead+1.0 Ice+1.0	126383.73	-47.09	-4.80	0.00	0.00	48.49
Temp+Guy 1.2 Dead+1.0 Wind 0 deg+1.0	127752.64	-51.25	-499.95	0.00	0.00	346.27

tnxTower	Job	121-23082	Page
that I ower		32 of 48	
	Project		Date
		180 ft Rohn #80 - Stafford Springs CT	19:45:40 09/06/21
	Client		Designed by
Phone:		CDT	,
FAX:			

Load Combination	Vertical	$Shear_x$	Shear <sub>z</sub>	Overturning Moment, $M_x$	Overturning Moment, Mz	Torque
	lb	lb	lb	lb-ft	lb-ft	lb-ft
Ice+1.0 Temp+1.0 Guy						
1.2 Dead+1.0 Wind 30 deg+1.0	127306.44	183.17	-436.39	0.00	0.00	368.31
Ice+1.0 Temp+1.0 Guy						
1.2 Dead+1.0 Wind 60 deg+1.0	126904.46	363.43	-248.71	0.00	0.00	263.91
Ice+1.0 Temp+1.0 Guy						
1.2 Dead+1.0 Wind 90 deg+1.0	127341.30	435.02	1.39	0.00	0.00	102.57
Ice+1.0 Temp+1.0 Guy	127012 (0	272.44	236.95	0.00	0.00	-32.55
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy	127812.69	372.44	230.93	0.00	0.00	-32.33
1.2 Dead+1.0 Wind 150	127341.45	199.63	408.68	0.00	0.00	-145.88
deg+1.0 Ice+1.0 Temp+1.0 Guy	12/341.43	199.03	400.00	0.00	0.00	-143.00
1.2 Dead+1.0 Wind 180	126905.73	-52.93	471.58	0.00	0.00	-248.05
deg+1.0 Ice+1.0 Temp+1.0 Guy	120,001,0	02.00	.,1.00	0.00	0.00	2.0.00
1.2 Dead+1.0 Wind 210	127309.79	-305.49	409.08	0.00	0.00	-270.40
deg+1.0 Ice+1.0 Temp+1.0 Guy						
1.2 Dead+1.0 Wind 240	127757.07	-477.53	237.66	0.00	0.00	-166.00
deg+1.0 Ice+1.0 Temp+1.0 Guy						
1.2 Dead+1.0 Wind 270	127283.92	-538.99	2.42	0.00	0.00	-4.10
deg+1.0 Ice+1.0 Temp+1.0 Guy						
1.2 Dead+1.0 Wind 300	126859.72	-466.30	-247.84	0.00	0.00	130.43
deg+1.0 Ice+1.0 Temp+1.0 Guy	127200 70	205.01	125.60	0.00	0.00	242.05
1.2 Dead+1.0 Wind 330	127280.79	-285.81	-435.68	0.00	0.00	243.95
deg+1.0 Ice+1.0 Temp+1.0 Guy	40.400.51	2.20	200.22	0.00	0.00	121.01
Dead+Wind 0 deg - Service+Guy	40482.51	-3.30	-298.33	0.00	0.00	131.91
Dead+Wind 30 deg -	40445.68	140.40	-259.06	0.00	0.00	147.91
Service+Guy	40445.00	140.40	-239.00	0.00	0.00	147.91
Dead+Wind 60 deg -	40413.59	246.30	-152.00	0.00	0.00	123.64
Service+Guy	10113.59	210.50	152.00	0.00	0.00	125.01
Dead+Wind 90 deg -	40444.98	285.99	-6.76	0.00	0.00	70.98
Service+Guy						
Dead+Wind 120 deg -	40482.00	248.02	137.35	0.00	0.00	9.10
Service+Guy						
Dead+Wind 150 deg -	40444.90	142.15	242.25	0.00	0.00	-51.07
Service+Guy						
Dead+Wind 180 deg -	40413.55	-3.50	280.44	0.00	0.00	-97.99
Service+Guy	10115.01	1.40.12	242.15	0.00	0.00	11101
Dead+Wind 210 deg -	40445.84	-149.13	242.15	0.00	0.00	-114.24
Service+Guy Dead+Wind 240 deg -	40482.85	-254.94	137.25	0.00	0.00	-90.27
Service+Guy	40462.63	-234.94	137.23	0.00	0.00	-90.27
Dead+Wind 270 deg -	40444.90	-292.85	-6.94	0.00	0.00	-37.39
Service+Guy	70777.90	-272.03	-0.94	0.00	0.00	-51.59
Dead+Wind 300 deg -	40412.59	-253.06	-152.18	0.00	0.00	25.19
Service+Guy		200.00	102.10	0.00	0.00	20.17
Dead+Wind 330 deg -	40444.65	-147.14	-259.14	0.00	0.00	84.81
Service+Guy						

## **Solution Summary**

	Sı	ım of Applied Force.	S		Sum of Reaction	S	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	lb	lb	lb	lb	lb	lb	
1	0.00	-13827.69	0.00	3.31	13816.34	6.81	0.099%
2	-0.00	-16414.60	-16528.82	-0.01	16414.33	16521.12	0.033%
3	-0.00	-16414.60	-14973.46	-0.01	16414.33	14966.09	0.033%
4	-0.00	-16414.60	-15227.90	-0.01	16414.33	15220.11	0.035%
5	-0.00	-16414.60	-14829.26	-0.02	16414.35	14820.72	0.039%

4 Town Town or	Job		Page
tnxTower		33 of 48	
	Project		Date
	18	0 ft Rohn #80 - Stafford Springs CT	19:45:40 09/06/21
	Client		Designed by
Phone: FAX:		CDT	

		n of Applied Force.		****	Sum of Reaction		0.15
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	<u>lb</u>	lb	lb	lb	lb	lb	
6	-0.00	-16414.60	-14534.27	-0.06	16414.40	14518.74	0.071%
7	8251.08	-16289.13	-14291.29	-8252.05	16288.88	14282.57	0.038%
8	7473.40	-16289.13	-12944.31	-7474.31	16288.88	12936.08	0.037%
9	7603.40	-16289.13	-13169.47	-7604.41	16288.87	13160.49	0.041%
10	7401.30	-16289.13	-12819.43	-7402.46	16288.91	12809.59	0.045%
11	7255.95	-16289.13	-12567.67	-7256.41	16288.93	12552.41	0.070%
12 13	14289.10 12942.13	-16163.65 -16163.65	-8249.82 -7472.14	-14273.11 -12929.70	16163.34 16163.37	8241.58 7465.87	0.078% 0.063%
13	13168.89		-7472.14 -7603.06	-12929.70	16163.37	7595.61	0.003%
15	12817.24	-16163.65 -16163.65	-7400.04	-13134.33	16163.36	7390.45	0.074%
16	12566.73	-16163.65	-7255.40	-12547.33	16163.37	7244.66	0.102%
17	16502.16	-16289.13	0.00	-16494.77	16288.87	5.35	0.10270
18	14946.80	-16289.13	0.00	-14939.84	16288.87	5.04	0.039%
19	15206.80	-16289.13	0.00	-15199.97	16288.89	4.97	0.039%
20	14802.60	-16289.13	0.00	-14795.09	16288.92	5.54	0.042%
21	14511.90	-16289.13	0.00	-14500.03	16288.93	7.43	0.064%
22	14314.38	-16414.60	8264.41	-14307.49	16414.32	-8260.44	0.034%
23	12967.40	-16414.60	7486.73	-12960.81	16414.32	-7482.93	0.034%
24	13187.75	-16414.60	7613.95	-13180.75	16414.32	-7609.91	0.036%
25	12842.51	-16414.60	7414.63	-12835.50	16414.36	-7410.59	0.037%
26	12587.04	-16414.60	7267.13	-12574.69	16414.41	-7260.01	0.065%
27	8251.08	-16289.13	14291.29	-8242.73	16288.87	-14287.58	0.039%
28	7473.40	-16289.13	12944.31	-7465.53	16288.87	-12940.81	0.039%
29	7603.40	-16289.13	13169.47	-7595.66	16288.89	-13166.06	0.038%
30	7401.30	-16289.13	12819.43	-7392.74	16288.92	-12815.72	0.042%
31	7255.95	-16289.13	12567.67	-7243.59	16288.94	-12561.14	0.064%
32	0.00	-16163.65	16499.64	0.38	16163.34	-16481.63	0.078%
33	0.00	-16163.65	14944.28	0.32	16163.37	-14930.35	0.063%
34	0.00	-16163.65	15206.13	0.36	16163.36	-15189.76	0.074%
35	0.00	-16163.65	14800.08	0.30	16163.35	-14779.73	0.093%
36	0.00	-16163.65	14510.81	0.19	16163.37	-14488.61	0.102%
37	-8251.08	-16289.13	14291.29	8242.87	16288.88	-14287.68	0.039%
38	-7473.40 7602.40	-16289.13	12944.31	7465.66	16288.87	-12940.90	0.038%
39	-7603.40	-16289.13	13169.47	7595.81	16288.89	-13166.16	0.037%
40 41	-7401.30 -7255.95	-16289.13 -16289.13	12819.43 12567.67	7391.94 7243.74	16288.90 16288.94	-12815.39 -12561.28	0.046% 0.063%
42	-14314.38	-16414.60	8264.41	14307.59	16414.33	-8260.51	0.003%
43	-12967.40	-16414.60	7486.73	12960.91	16414.33	-7483.00	0.034%
44	-13187.75	-16414.60	7613.95	13180.87	16414.32	-7610.00	0.034%
45	-12842.51	-16414.60	7414.63	12834.88	16414.34	-7410.25	0.03376
46	-12587.04	-16414.60	7267.13	12574.85	16414.41	-7260.15	0.040%
47	-16502.16	-16289.13	-0.00	16494.89	16288.87	5.27	0.039%
48	-14946.80	-16289.13	-0.00	14939.95	16288.87	4.97	0.039%
49	-15206.80	-16289.13	-0.00	15200.09	16288.89	4.89	0.037%
50	-14802.60	-16289.13	-0.00	14794.36	16288.90	6.06	0.046%
51	-14511.90	-16289.13	-0.00	14500.20	16288.94	7.31	0.063%
52	-14289.10	-16163.65	-8249.82	14273.36	16163.34	8241.28	0.078%
53	-12942.13	-16163.65	-7472.14	12927.93	16163.33	7464.53	0.073%
54	-13168.89	-16163.65	-7603.06	13154.57	16163.37	7595.33	0.073%
55	-12817.24	-16163.65	-7400.04	12799.53	16163.36	7390.23	0.092%
56	-12566.73	-16163.65	-7255.40	12547.49	16163.38	7244.55	0.102%
57	-8251.08	-16289.13	-14291.29	8252.01	16288.88	14282.53	0.038%
58	-7473.40	-16289.13	-12944.31	7474.28	16288.88	12936.06	0.038%
59	-7603.40	-16289.13	-13169.47	7604.38	16288.87	13160.45	0.041%
60	-7401.30	-16289.13	-12819.43	7402.42	16288.91	12809.54	0.045%
61	-7255.95	-16289.13	-12567.67	7256.32	16288.92	12552.42	0.070%
62	-0.00	-81486.45	0.00	4.49	81486.43	0.37	0.006%
63	-0.00	-81664.64	-9039.36	-0.10	81664.55	9026.00	0.016%
64	4514.80	-81486.45	-7819.86	-4511.74	81486.36	7805.18	0.018%
65	7825.27	-81308.26	-4517.92	-7809.37	81308.14	4509.59	0.022%
66	9029.60	-81486.45	0.00	-9017.61	81486.37	4.47	0.016%

b	Page
121-23082	34 of 48
roject	Date
180 ft Rohn #80 - Stafford Springs CT	19:45:40 09/06/21
lient	Designed by
CDT	- •
re	121-23082 Dject 180 ft Rohn #80 - Stafford Springs CT

	Sui	n of Applied Forces	7		Sum of Reaction	!S	
Load	PX	PY	PZ	PX	PY	PZ	% Erro
Comb.	lb	lb	lb	lb	lb	lb	
67	7828.31	-81664.64	4519.68	-7817.32	81664.54	-4513.36	0.015%
68	4514.80	-81486.45	7819.86	-4504.88	81486.37	-7811.76	0.016%
69	0.00	-81308.26	9035.84	0.83	81308.15	-9017.98	0.022%
70	-4514.80	-81486.45	7819.86	4503.66	81486.36	-7809.91	0.018%
71	-7828.31	-81664.64	4519.68	7816.72	81664.55	-4513.11	0.016%
72	-9029.60	-81486.45	-0.00	9015.12	81486.36	4.64	0.019%
73	-7825.27	-81308.26	-4517.92	7809.71	81308.15	4508.86	0.022%
74	-4514.80	-81486.45	-7819.86	4511.62	81486.36	7804.94	0.019%
75	0.00	-13857.69	-3952.58	0.01	13857.68	3924.98	0.192%
76	1973.10	-13827.69	-3417.52	-1958.28	13827.66	3393.84	0.1949
77	3416.99	-13797.68	-1972.80	-3392.04	13797.64	1958.47	0.200%
78	3946.21	-13827.69	0.00	-3918.20	13827.66	-0.89	0.195%
79	3423.04	-13857.69	1976.29	-3399.02	13857.68	-1962.39	0.193%
80	1973.10	-13827.69	3417.52	-1959.91	13827.66	-3392.77	0.195%
81	-0.00	-13797.68	3945.60	0.03	13797.64	-3916.76	0.2019
82	-1973.10	-13827.69	3417.52	1959.97	13827.66	-3392.76	0.195%
83	-3423.04	-13857.69	1976.29	3399.08	13857.68	-1962.39	0.192%
84	-3946.21	-13827.69	-0.00	3918.25	13827.66	-0.88	0.195%
85	-3416.99	-13797.68	-1972.80	3392.07	13797.64	1958.49	0.200%
86	-1973.10	-13827.69	-3417.52	1958.30	13827.66	3393.84	0.194%

# Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination	C	of Cycles	Tolerance	Tolerance
1	Yes	75	0.00000001	0.00000000
2	Yes	199	0.00000001	0.00007812
3	Yes	200	0.00000001	0.00007862
4	Yes	196	0.00000001	0.00008039
5	Yes	186	0.00000001	0.00008461
6	Yes	168	0.00000001	0.00007071
7	Yes	192	0.00000001	0.00007800
8	Yes	193	0.00000001	0.00007905
9	Yes	190	0.00000001	0.00008198
10	Yes	182	0.00000001	0.00007938
11	Yes	171	0.00000001	0.00006733
12	Yes	165	0.00000001	0.00006930
13	Yes	166	0.00000001	0.00007569
14	Yes	165	0.00000001	0.00006823
15	Yes	163	0.00000001	0.00006937
16	Yes	162	0.00000001	0.00007875
17	Yes	192	0.00000001	0.00008150
18	Yes	193	0.00000001	0.00008232
19	Yes	191	0.00000001	0.00007788
20	Yes	183	0.00000001	0.00007681
21	Yes	172	0.00000001	0.00006717
22	Yes	199	0.00000001	0.00008056
23	Yes	200	0.00000001	0.00008094
24	Yes	196	0.00000001	0.00008308
25	Yes	187	0.00000001	0.00008135
26	Yes	169	0.00000001	0.00007060
27	Yes	192	0.00000001	0.00008153
28	Yes	193	0.00000001	0.00008243
29	Yes	191	0.00000001	0.00007785
30	Yes	183	0.00000001	0.00007672
31	Yes	172	0.00000001	0.00006679

tnxTower	Job	Јоb 121-23082				
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21			
Phone: FAX:	Client	CDT	Designed by			

32	Yes	165	0.00000001	0.00006931
33	Yes	166	0.00000001	0.00007595
34	Yes	165	0.00000001	0.00006839
35	Yes	163	0.0000001	0.00006930
36	Yes	162	0.00000001	0.00007842
37	Yes	192	0.00000001	0.00007970
38	Yes	193	0.00000001	0.00008068
39	Yes	191	0.0000001	0.00007615
40	Yes	182	0.00000001	0.00008173
41	Yes	172	0.00000001	0.00006363
42	Yes	199	0.00000001	0.00007925
43	Yes	200	0.0000001	0.00007967
44	Yes	196	0.00000001	0.00008163
45	Yes	186	0.00000001	0.00008710
46	Yes	169	0.0000001	0.00006731
47	Yes	192	0.00000001	0.00008009
48	Yes	193	0.00000001	0.00008105
49	Yes	191	0.00000001	0.00007657
50	Yes	182	0.00000001	0.00008254
51	Yes	172	0.0000001	0.00006524
52	Yes	165	0.00000001	0.00006868
53	Yes	165	0.00000001	0.00008465
54	Yes	165	0.0000001	0.00006769
55	Yes	163	0.00000001	0.00006892
56	Yes	162	0.0000001	0.00007844
57	Yes	192	0.00000001	0.00007861
58	Yes	193	0.00000001	0.00007959
59	Yes	190	0.00000001	0.00008263
60	Yes	182	0.00000001	0.00008023
61	Yes	171	0.0000001	0.00006903
62	Yes	136	0.00000001	0.00005606
63	Yes	185	0.00000001	0.00001714
64	Yes	181	0.0000001	0.00001743
65	Yes	176	0.0000001	0.00002342
66	Yes	183	0.00000001	0.00002069
67	Yes	186	0.00000001	0.00002111
68	Yes	183	0.0000001	0.00002033
69	Yes	176	0.00000001	0.00002267
70	Yes	181	0.0000001	0.00001772
71	Yes	185	0.0000001	0.00001780
72	Yes	181	0.00000001	0.00001956
73	Yes	176	0.00000001	0.00002269
74	Yes	181	0.0000001	0.00001889
75	Yes	146	0.00000001	0.00009151
76	Yes	146	0.00000001	0.00009215
77	Yes	146	0.0000001	0.00009419
78	Yes	146	0.00000001	0.00009163
79	Yes	146	0.0000001	0.00009042
80	Yes	146	0.00000001	0.00009101
81	Yes	146	0.00000001	0.00009373
82	Yes	146	0.00000001	0.00009055
83	Yes	146	0.00000001	0.00009101
84	Yes	146	0.00000001	0.00009239
85	Yes	146	0.00000001	0.00009459
86	Yes	146	0.00000001	0.00009263

tnxTower	Job		Page
thx10wer		36 of 48	
	Project		Date
		180 ft Rohn #80 - Stafford Springs CT	19:45:40 09/06/21
	Client		Designed by
Phone:		CDT	
FAX:			

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
T1	180 - 160	1.346	81	0.0851	0.2214
T2	160 - 140	1.001	81	0.0679	0.2035
T3	140 - 120	0.750	77	0.0585	0.1830
T4	120 - 100	0.522	85	0.0447	0.1488
T5	100 - 80	0.381	85	0.0240	0.0968
T6	80 - 60	0.315	85	0.0045	0.0510
T7	60 - 40	0.340	85	0.0016	0.0576
T8	40 - 20	0.321	85	0.0170	0.0560
T9	20 - 5	0.199	85	0.0394	0.0471
T10	5 - 0	0.051	85	0.0471	0.0266

#### **Critical Deflections and Radius of Curvature - Service Wind**

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	0	0	ft
180.00	Lightning Rod 5/8x4'	81	1.346	0.0851	0.2214	128053
179.00	Decibel DB809	81	1.328	0.0842	0.2204	128053
177.00	Decibel DB809	81	1.291	0.0822	0.2183	128053
171.00	12 ft Boom / Frame	81	1.182	0.0766	0.2122	71141
163.00	Celwave PD201	81	1.047	0.0699	0.2059	37932
162.75	Guy	81	1.043	0.0698	0.2057	37491
150.00	12 ft Boom / Frame	81	0.868	0.0628	0.1944	87174
127.00	Decibel DB420	77	0.596	0.0505	0.1628	67311
119.67	Guy	85	0.519	0.0444	0.1481	39316
83.00	Celwave PD201	85	0.319	0.0068	0.0546	37599
82.75	Guy	85	0.318	0.0066	0.0542	37361

## **Maximum Tower Deflections - Design Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
T1	180 - 160	8.059	23	0.5411	0.9292
T2	160 - 140	5.924	23	0.4743	0.8489
T3	140 - 120	4.171	23	0.4157	0.7707
T4	120 - 100	2.697	17	0.3199	0.6354
T5	100 - 80	1.932	56	0.2029	0.4268
T6	80 - 60	1.620	56	0.1084	0.2448
T7	60 - 40	1.675	56	0.0537	0.2587
T8	40 - 20	1.526	56	0.0897	0.2375
Т9	20 - 5	0.928	56	0.1871	0.1851
T10	5 - 0	0.237	56	0.2200	0.1116

#### Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	0	0	ft

tnxTower	Job	121-23082	<b>Page</b> 37 of 48
		0. 00	
	Project		Date
		180 ft Rohn #80 - Stafford Springs CT	19:45:40 09/06/21
	Client		Designed by
Phone:		CDT	3 11 1,
FAX:			

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
180.00	Lightning Rod 5/8x4'	23	8.059	0.5411	0.9292	29656
179.00	Decibel DB809	23	7.947	0.5376	0.9250	29656
177.00	Decibel DB809	23	7.724	0.5304	0.9165	29656
171.00	12 ft Boom / Frame	23	7.063	0.5093	0.8911	16476
163.00	Celwave PD201	23	6.221	0.4832	0.8585	8769
162.75	Guy	23	6.196	0.4824	0.8577	8660
150.00	12 ft Boom / Frame	23	5.016	0.4475	0.8142	10909
127.00	Decibel DB420	18	3.155	0.3552	0.6915	8519
119.67	Guy	17	2.678	0.3181	0.6325	5825
83.00	Celwave PD201	56	1.640	0.1204	0.2596	7444
82.75	Guy	56	1.638	0.1193	0.2581	7412

<b>Bolt</b>	Design	Data
DOIL	Desidii	Data

Section No.	Elevation	Component Type	Bolt Grade	Bolt Size	Number Of	Maximum Load	Allowable Load	Ratio Load	Allowable Ratio	Criteria
	ft			in	Bolts	per Bolt lb	per Bolt lb	Allowable		
T1	180	Leg	A325N	0.7500	4	13.47	29820.60	0.000	1	Bolt Tension
		Diagonal	A325N	0.5000	1	2081.29	5904.86	0.352	1	Member Bearing
		Top Girt	A325N	0.5000	1	16.26	5904.86	0.003	1	Member Bearing
		Bottom Girt	A325N	0.5000	1	361.29	3967.20	0.091	1	Member Bearing
T2	160	Leg	A325N	0.7500	4	1400.53	29820.60	0.047	1	Bolt Tension
		Diagonal	A325N	0.5000	1	1158.32	6681.60	0.173	1	Member Bearing
		Top Girt	A325N	0.5000	1	423.30	5904.86	0.072	1	Member Bearing
		Bottom Girt	A325N	0.5000	1	310.95	3967.20	0.078	1	Member Bearing
T3	140	Leg	A325N	0.7500	4	1487.80	29820.60	0.050	1	Bolt Tension
		Diagonal	A325N	0.5000	1	1693.12	6681.60	0.253	1	Member Bearing
		Top Girt	A325N	0.5000	1	423.71	5904.86	0.072	1	Member Bearing
		Bottom Girt	A325N	0.5000	1	423.71	3967.20	0.107	1	Member Bearing
T4	120	Leg	A325N	0.7500	4	2039.62	29820.60	0.068	1	Bolt Tension
		Diagonal	A325N	0.5000	1	987.43	6681.60	0.148	1	Member Bearing
		Bottom Girt	A325N	0.5000	1	525.41	3967.20	0.132	1	Member Bearing
T5	100	Leg	A325N	0.7500	4	2529.02	29820.60	0.085	1	Bolt Tension
		Diagonal	A325N	0.5000	1	1740.35	6681.60	0.260	1	Member Bearing
		Top Girt	A325N	0.5000	1	712.34	5904.86	0.121	1	Member Bearing
		Bottom Girt	A325N	0.5000	1	712.34	3967.20	0.180	1	Member Bearing
		Torque Arm Top@82.75	A325N	0.7500	2	2120.69	16077.60	0.132	1	Member Bearing
T6	80	Leg	A325N	0.7500	4	3428.39	29820.60	0.115	1	Bolt Tension
		Diagonal	A325N	0.5000	1	2038.00	5904.86	0.345	1	Member Bearing
		Top Girt	A325N	0.5000	1	856.57	5904.86	0.145	1	Member Bearing
		Bottom Girt	A325N	0.5000	1	712.58	3967.20	0.180	1	Member Bearing
T7	60	Leg	A325N	0.7500	4	3357.28	29820.60	0.113	1	Bolt Tension

tnxTower	Job	121-23082	Page 38 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section No.	Elevation	Component Type	Bolt Grade	Bolt Size	Number Of	Maximum Load	Allowable Load	Ratio Load	Allowable Ratio	Criteria
	ft			in	Bolts	per Bolt lb	per Bolt lb	Allowable	•	
		Diagonal	A325N	0.5000	1	1243.24	6681.60	0.186	1	Member Bearing
		Top Girt	A325N	0.5000	1	775.11	5904.86	0.131	1	Member Bearing
		Bottom Girt	A325N	0.5000	1	775.11	3967.20	0.195	1	Member Bearing
T8	40	Leg	A325N	0.7500	4	3730.23	29820.60	0.125	1	Bolt Tension
		Diagonal	A325N	0.5000	1	684.62	6681.60	0.102	1	Member Bearing
		Top Girt	A325N	0.5000	1	790.25	5904.86	0.134	1	Member Bearing
		Bottom Girt	A325N	0.5000	1	790.25	3967.20	0.199	1	Member Bearing
Т9	20	Leg	A325N	0.7500	4	3778.39	29820.60	0.127	1	Bolt Tension
		Diagonal	A325N	0.5000	1	1137.47	5904.86	0.193	1	Member Bearing
		Top Girt	A325N	0.5000	1	785.32	5904.86	0.133	1	Member Bearing
		Bottom Girt	A325N	0.5000	1	3694.05	3967.20	0.931	1	Member Bearing
T10	5	Leg	A325N	0.7500	4	3568.69	29820.60	0.120	1	Bolt Tension
		Diagonal	A325N	0.5000	1	1671.62	5904.86	0.120	1	Member Bearing
		Top Girt	A325N	0.5000	1	4009.92	5904.86	0.679	1	Member Bearing

	Guy Design Data												
Section No.	Elevation ft	Size	Initial Tension lb	Breaking Load lb	Actual T <sub>u</sub> lb	Allowable $\phi T_n$ lb	Required S.F.	Actual S.F.					
T1	162.75 (A) (462)	3/4 EHS	5830.00	58299.91	14593.30	34980.00	1.000	2.397					
	162.75 (B) (461)	3/4 EHS	5830.00	58299.91	14533.50	34980.00	1.000	2.407					
	162.75 (C) (460)	3/4 EHS	5830.00	58299.91	14561.50	34980.00	1.000	2.402					
T4	119.67 (A) (465)	1/2 EHS	2690.00	26900.04	7962.06	16140.00	1.000	2.027					
	119.67 (B) (464)	1/2 EHS	2690.00	26900.04	7983.52	16140.00	1.000	2.022					
	119.67 (C) (463)	1/2 EHS	2690.00	26900.04	7988.98	16140.00	1.000	2.020					
T5	82.75 (A) (453)	1/2 EHS	2690.00	26900.04	7468.01	16140.00	1.000	2.161					
	82.75 (A) (454)	1/2 EHS	2690.00	26900.04	7341.44	16140.00	1.000	2.198					
	82.75 (B) (449)	1/2 EHS	2690.00	26900.04	7466.01	16140.00	1.000	2.162					
	82.75 (B) (450)	1/2 EHS	2690.00	26900.04	7457.48	16140.00	1.000	2.164					
	82.75 (C) (442)	1/2 EHS	2690.00	26900.04	7360.56	16140.00	1.000	2.193					
	82.75 (C) (443)	1/2 EHS	2690.00	26900.04	7480.48	16140.00	1.000	2.158					

tnxTower	Job	121-23082	<b>Page</b> 39 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

## Compression Checks

## Leg Design Data (Compression)

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	Mast Stability	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	Index	lb	lb	$\phi P_n$
T1	180 - 160	P2x.218	20.00	2.42	37.8 K=1.00	1.4773	1.00	-16794.20	59870.70	0.281 1
T2	160 - 140	P2x.218	20.00	2.42	37.8 K=1.00	1.4773	1.00	-17952.60	59870.70	0.300 1
T3	140 - 120	P2x.218	20.00	2.42	37.8 K=1.00	1.4773	1.00	-24463.00	59870.70	0.409 1
T4	120 - 100	P2x.218	20.00	2.42	37.8 K=1.00	1.4773	1.00	-30334.60	59870.70	0.507 1
T5	100 - 80	P2.5x.276	20.00	2.42	31.4 K=1.00	2.2535	1.00	-41127.00	94363.10	0.436 1
Т6	80 - 60	P2.5x.276	20.00	2.42	62.8 K=2.00	2.2535	1.00	-41140.60	76028.20	0.541 1
T7	60 - 40	P2.5x.203	20.00	2.42	61.2 K=2.00	1.7040	1.00	-44751.00	58302.40	0.768 1
Т8	40 - 20	P2.5x.203	20.00	2.42	61.2 K=2.00	1.7040	1.00	-45625.30	58302.40	0.783 1
Т9	20 - 5	P2.5x.276	15.00	2.39	62.0 K=2.00	2.2535	1.00	-45340.60	76530.40	0.592 1
T10	5 - 0	P2.5x.276	5.38	1.06	13.7 K=1.00	2.2535	0.78	-47135.30	78031.70	0.604 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

# **Diagonal Design Data (Compression)**

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	$Ratio$ $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	180 - 160	ROHN TS1.5x16 ga	4.19	3.95	92.8 K=1.00	0.2627	-1998.96	6038.67	0.331 1
T2	160 - 140	ROHN TS1.5x16 ga	4.19	3.95	92.8 K=1.00	0.2627	-1158.32	6038.67	0.192 1
Т3	140 - 120	ROHN TS1.5x16 ga	4.19	3.95	92.8 K=1.00	0.2627	-1693.12	6038.67	0.280 1
T4	120 - 100	ROHN TS1.5x16 ga	4.19	3.95	92.8 K=1.00	0.2627	-987.43	6038.67	0.164 <sup>1</sup>
T5	100 - 80	ROHN TS1.5x16 ga	4.19	3.89	91.6 K=1.00	0.2627	-1740.35	6127.23	0.284 1
T6	80 - 60	ROHN TS1.5x16 ga	4.19	3.89	91.6 K=1.00	0.2627	-2156.65	6127.23	0.352 1
T7	60 - 40	ROHN TS1.5x16 ga	4.19	3.89	91.6 K=1.00	0.2627	-1243.24	6127.23	0.203 1
T8	40 - 20	ROHN TS1.5x16 ga	4.19	3.89	91.6	0.2627	-684.62	6127.23	$0.112^{-1}$

tnxTower	Job	121-23082	Page 40 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
					K=1.00				~
Т9	20 - 5	ROHN TS1.5x16 ga	4.17	3.88	91.2 K=1.00	0.2627	-1101.96	6153.03	0.179 1
T10	5 - 0	ROHN TS1.5x16 ga	1.42	0.78	18.4 K=1.00	0.2627	-1043.10	10407.00	0.100 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	$Ratio$ $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	180 - 160	ROHN TS1.5x16 ga	3.42	3.22	75.8 K=1.00	0.2627	-18.00	7292.66	0.002 1
T2	160 - 140	ROHN TS1.5x16 ga	3.42	3.22	75.8 K=1.00	0.2627	-310.95	7292.66	0.043 1
Т3	140 - 120	ROHN TS1.5x16 ga	3.42	3.22	75.8 K=1.00	0.2627	-423.71	7292.66	0.058 1
T5	100 - 80	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-712.34	7363.82	0.097 1
Т6	80 - 60	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-712.58	7363.82	0.097
Т7	60 - 40	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-775.11	7363.82	0.105
Т8	40 - 20	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-790.25	7363.82	0.107
Т9	20 - 5	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-785.32	7363.82	0.107
T10	5 - 0	ROHN TS1.5x16 ga	3.36	3.12	73.5 K=1.00	0.2627	-861.14	7460.76	0.115

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

# **Bottom Girt Design Data (Compression)**

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	180 - 160	ROHN TS1.5x16 ga	3.42	3.22	75.8 K=1.00	0.2627	-290.88	7292.66	0.040 1
T2	160 - 140	ROHN TS1.5x16 ga	3.42	3.22	75.8 K=1.00	0.2627	-310.95	7292.66	0.043 1
Т3	140 - 120	ROHN TS1.5x16 ga	3.42	3.22	75.8 K=1.00	0.2627	-423.71	7292.66	0.058 1
T4	120 - 100	ROHN TS1.5x16 ga	3.42	3.22	75.8 K=1.00	0.2627	-525.41	7292.66	0.072 1

tnxTower	Job	121-23082	Page 41 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	$Ratio$ $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
									~
T5	100 - 80	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-712.34	7363.82	0.097 1
Т6	80 - 60	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-712.58	7363.82	$0.097^{-1}$
Т7	60 - 40	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-775.11	7363.82	0.105 1
Т8	40 - 20	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-790.25	7363.82	0.107 1
Т9	20 - 5	ROHN TS1.5x16 ga	3.42	3.18	74.8 K=1.00	0.2627	-785.32	7363.82	0.107 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

		Top Guy P	ull-Off	Desi	ign Da	ita (Co	mpress	sion)	
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P
110.	ft		ft	ft		$in^2$	lb	lb	$\frac{1}{\Phi P_n}$
T5	100 - 80	L1 1/2x1 1/2x3/16	3.42	3.18	130.1 K=1.00	0.5273	-1761.99	7008.98	0.251 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

	Top Guy Pull-Off Bending Design Data											
Section No.	Elevation	Size	$M_{ux}$	$\phi M_{nx}$	Ratio M <sub>ux</sub>	$M_{uy}$	$\phi M_{ny}$	Ratio Muy				
110.	ft		lb-ft	lb-ft	$\phi M_{nx}$	lb-ft	lb-ft	$\phi M_{ny}$				
T5	100 - 80	L1 1/2x1 1/2x3/16	0.00	711.05	0.000	0.00	368.03	0.000				

	Top Guy Pull-Off Interaction Design Data									
Section No.	Elevation ft	Size	$ \begin{array}{c} Ratio \\ P_u \\ \hline                                   $	$Ratio$ $M_{ux}$ $\phi M_{nx}$	$Ratio$ $M_{uy}$ $\phi M_{ny}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria		
T5	100 - 80	L1 1/2x1 1/2x3/16	0.251	0.000	0.000	0.251 1	1.000	4.8.1		

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

tnxTower	Job	121-23082	Page 42 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	$Ratio$ $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T5	100 - 80 (444)	C10x15.3	3.50	3.38	56.9 K=1.00	4.4900	-361.84	122682.00	0.003
T5	100 - 80 (445)	C10x15.3	3.50	3.38	56.9 K=1.00	4.4900	-363.40	122682.00	0.003
T5	100 - 80 (451)	C10x15.3	3.50	3.38	56.9 K=1.00	4.4900	-618.69	122682.00	0.005
T5	100 - 80 (452)	C10x15.3	3.50	3.38	56.9 K=1.00	4.4900	-840.71	122682.00	0.007
T5	100 - 80 (455)	C10x15.3	3.50	3.38	56.9 K=1.00	4.4900	-595.66	122682.00	0.005
T5	100 - 80 (456)	C10x15.3	3.50	3.38	56.9 K=1.00	4.4900	-830.32	122682.00	0.007

Section No.	Elevation	Size	$M_{ux}$	$\phi M_{nx}$	Ratio $M_{ux}$	$M_{uy}$	$\phi M_{ny}$	Ratio $M_{uy}$
	ft		lb-ft	lb-ft	$\phi M_{nx}$	lb-ft	lb-ft	$\phi M_{ny}$
T5	100 - 80 (444)	C10x15.3	-8692.92	41799.58	0.208	0.00	4698.00	0.000
T5	100 - 80 (445)	C10x15.3	-8648.58	41799.58	0.207	-0.00	4698.00	0.000
T5	100 - 80 (451)	C10x15.3	-8633.33	41799.58	0.207	0.00	4698.00	0.000
T5	100 - 80 (452)	C10x15.3	-8553.83	41799.58	0.205	0.00	4698.00	0.000
T5	100 - 80 (455)	C10x15.3	-8619.25	41799.58	0.206	-0.00	4698.00	0.000
T5	100 - 80 (456)	C10x15.3	-8584.00	41799.58	0.205	-0.00	4698.00	0.000

Section No.	Elevation	Size	$Ratio$ $P_u$	Ratio $M_{ux}$	Ratio $M_{uv}$	Comb. Stress	Allow. Stress	Criteria
110.	ft		$\frac{1}{\phi P_n}$	$\phi M_{nx}$	$\phi M_{nv}$	Ratio	Ratio	
T5	100 - 80 (444)	C10x15.3	0.003	0.208	0.000	0.209	1.000	4.8.1
T5	100 - 80 (445)	C10x15.3	0.003	0.207	0.000	0.208	1.000	4.8.1
T5	100 - 80 (451)	C10x15.3	0.005	0.207	0.000	0.209	1.000	4.8.1
T5	100 - 80 (452)	C10x15.3	0.007	0.205	0.000	0.208	1.000	4.8.1
T5	100 - 80 (455)	C10x15.3	0.005	0.206	0.000	0.209	1.000	4.8.1
T5	100 - 80 (456)	C10x15.3	0.007	0.205	0.000	0.209	1.000	4.8.1

## Tension Checks

tnxTower	Job	121-23082	<b>Page</b> 43 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

			Leg Des	sign E	ata (	Tensio	on)		
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	180 - 160	P2x.218	20.00	2.42	37.8	1.4773	10812.30	66476.60	0.163 1
T2	160 - 140	P2x.218	20.00	2.42	37.8	1.4773	1285.53	66476.60	0.019 1
Т3	140 - 120	P2x.218	20.00	2.42	37.8	1.4773	1602.97	66476.60	0.024 1
T4	120 - 100	P2x.218	20.00	2.42	37.8	1.4773	1602.21	66476.60	0.024 1
T5	100 - 80	P2.5x.276	20.00	2.42	31.4	2.2535	1954.27	101409.00	0.019 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

			,	<u> </u>		a (Ten			
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	180 - 160	ROHN TS1.5x16 ga	4.19	3.95	92.8	0.2627	2081.29	10641.40	0.196 1
T2	160 - 140	ROHN TS1.5x16 ga	4.19	3.95	92.8	0.2627	1016.06	10641.40	0.095 1
Т3	140 - 120	ROHN TS1.5x16 ga	4.19	3.95	92.8	0.2627	1417.73	10641.40	0.133 1
T4	120 - 100	ROHN TS1.5x16 ga	4.19	3.95	92.8	0.2627	852.99	10641.40	0.080 1
T5	100 - 80	ROHN TS1.5x16 ga	4.19	3.89	91.6	0.2627	1199.61	10641.40	0.113 1
Т6	80 - 60	ROHN TS1.5x16 ga	4.19	3.89	91.6	0.2627	2038.00	10641.40	0.192 1
T7	60 - 40	ROHN TS1.5x16 ga	4.19	3.89	91.6	0.2627	1089.11	10641.40	0.102 1
Т8	40 - 20	ROHN TS1.5x16 ga	4.19	3.89	91.6	0.2627	590.03	10641.40	0.055 1
Т9	20 - 5	ROHN TS1.5x16 ga	4.17	3.88	91.2	0.2627	1137.47	10641.40	0.107 1
T10	5 - 0	ROHN TS1.5x16 ga	3.19	1.61	37.8	0.2627	1671.62	10641.40	0.157 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

# Top Girt Design Data (Tension)

tnxTower	Job	121-23082	Page 44 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	180 - 160	ROHN TS1.5x16 ga	3.42	3.22	75.8	0.2627	16.26	10641.40	0.002 1
T2	160 - 140	ROHN TS1.5x16 ga	3.42	3.22	75.8	0.2627	423.30	10641.40	0.040 1
Т3	140 - 120	ROHN TS1.5x16 ga	3.42	3.22	75.8	0.2627	423.71	10641.40	0.040 1
T5	100 - 80	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	712.34	10641.40	0.067 1
Т6	80 - 60	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	856.57	10641.40	0.080 1
T7	60 - 40	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	775.11	10641.40	0.073 1
Т8	40 - 20	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	790.25	10641.40	0.074 1
Т9	20 - 5	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	785.32	10641.40	0.074 1
T10	5 - 0	ROHN TS1.5x16 ga	3.36	3.12	73.5	0.2627	4009.92	10641.40	0.377 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

<b>Bottom Girt Design Data (Tension</b>
-----------------------------------------

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	180 - 160	ROHN TS1.5x16 ga	3.42	3.22	75.8	0.2627	361.29	10641.40	0.034 1
T2	160 - 140	ROHN TS1.5x16 ga	3.42	3.22	75.8	0.2627	310.95	10641.40	0.029 1
Т3	140 - 120	ROHN TS1.5x16 ga	3.42	3.22	75.8	0.2627	423.71	10641.40	0.040 1
T4	120 - 100	ROHN TS1.5x16 ga	3.42	3.22	75.8	0.2627	525.41	10641.40	0.049 1
T5	100 - 80	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	712.34	10641.40	0.067 1
T6	80 - 60	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	712.58	10641.40	0.067 1
T7	60 - 40	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	775.11	10641.40	0.073 1
Т8	40 - 20	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	790.25	10641.40	0.074 1
Т9	20 - 5	ROHN TS1.5x16 ga	3.42	3.18	74.8	0.2627	3694.05	10641.40	0.347 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

tnxTower	Job	121-23082	<b>Page</b> 45 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

	Top Guy Pull-Off Design Data (Tension)										
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$		
	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$		
T1	180 - 160	3x1/2	3.42	3.22	267.9	1.5000	4661.73	48600.00	0.096 1		
T4	120 - 100	3x1/2	3.42	3.22	267.9	1.5000	3447.08	48600.00	$0.071^{-1}$		
T5	100 - 80	L1 1/2x1 1/2x3/16	3.42	3.18	83.6	0.5273	2641.60	17085.90	0.155 1		

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

	Top Guy Pull-Off Bending Design Data										
Section	Elevation	Size	$M_{ux}$	$\phi M_{nx}$	Ratio	$M_{uy}$	$\phi M_{ny}$	Ratio			
No.	ft		lb-ft	lb-ft	$\frac{M_{ux}}{\phi M_{nx}}$	lb-ft	lb-ft	$\frac{M_{uy}}{\phi M_{ny}}$			
T1	180 - 160	3x1/2	0.00	3037.50	0.000	0.00	506.25	0.000			
T4	120 - 100	3x1/2	0.00	3037.50	0.000	0.00	506.25	0.000			
T5	100 - 80	L1 1/2x1 1/2x3/16	0.00	711.05	0.000	0.00	368.03	0.000			

Section No.	Elevation	Size	$Ratio$ $P_u$	$Ratio$ $M_{ux}$	$Ratio$ $M_{uy}$	Comb. Stress	Allow. Stress	Criteria
	ft		$\phi P_n$	$\phi M_{nx}$	$\phi M_{nv}$	Ratio	Ratio	
T1	180 - 160	3x1/2	0.096	0.000	0.000	0.096 1	1.000	4.8.1
T4	120 - 100	3x1/2	0.071	0.000	0.000	0.071 1	1.000	4.8.1
T5	100 - 80	L1 1/2x1 1/2x3/16	0.155	0.000	0.000	0.155 1	1.000	4.8.1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

Section No.	Elevation	Size	L ft	$L_u$ ft	Kl/r	A	$P_u$	$\phi P_n$ $lb$	Ratio $P_u$
	ft					$in^2$	lb		$\phi P_n$
T5	100 - 80 (444)	C10x15.3	3.50	3.38	56.9	4.4900	2399.53	145476.00	0.016
T5	100 - 80 (445)	C10x15.3	3.50	3.38	56.9	4.4900	2426.68	145476.00	0.017
T5	100 - 80 (451)	C10x15.3	3.50	3.38	56.9	4.4900	2390.75	145476.00	0.016
T5	100 - 80 (452)	C10x15.3	3.50	3.38	56.9	4.4900	2291.52	145476.00	0.016
T5	100 - 80 (455)	C10x15.3	3.50	3.38	56.9	4.4900	2386.61	145476.00	0.016
T5	100 - 80 (456)	C10x15.3	3.50	3.38	56.9	4.4900	2289.71	145476.00	0.016

tnxTower	Job	121-23082	Page 46 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Torque-Arm Top Bending Design Data								
Section No.	Elevation	Size	$M_{ux}$	$\phi M_{nx}$	Ratio M <sub>ux</sub>	$M_{uy}$	$\phi M_{ny}$	Ratio M <sub>uy</sub>
	ft		lb-ft	lb-ft	$\frac{M_{ux}}{\phi M_{nx}}$	lb-ft	lb-ft	$\phi M_{nv}$
T5	100 - 80 (444)	C10x15.3	-14881.75	41799.58	0.356	0.00	4698.00	0.000
T5	100 - 80 (445)	C10x15.3	-14800.83	41799.58	0.354	-0.00	4698.00	0.000
T5	100 - 80 (451)	C10x15.3	-14927.50	41799.58	0.357	0.00	4698.00	0.000
T5	100 - 80 (452)	C10x15.3	-14793.08	41799.58	0.354	0.00	4698.00	0.000
T5	100 - 80 (455)	C10x15.3	-14892.92	41799.58	0.356	-0.00	4698.00	0.000
T5	100 - 80 (456)	C10x15.3	-14804.50	41799.58	0.354	-0.00	4698.00	0.000

Section No.	Elevation	Size	$Ratio$ $P_u$	$Ratio \ M_{ux}$	Ratio $M_{uy}$	Comb. Stress	Allow. Stress	Criteria
	ft		$\phi P_n$	$\phi M_{nx}$	$\phi M_{nv}$	Ratio	Ratio	
T5	100 - 80 (444)	C10x15.3	0.016	0.356	0.000	0.364	1.000	4.8.1
T5	100 - 80 (445)	C10x15.3	0.017	0.354	0.000	0.362	1.000	4.8.1
T5	100 - 80 (451)	C10x15.3	0.016	0.357	0.000	0.365	1.000	4.8.1
T5	100 - 80 (452)	C10x15.3	0.016	0.354	0.000	0.362	1.000	4.8.1
T5	100 - 80 (455)	C10x15.3	0.016	0.356	0.000	0.364	1.000	4.8.1
T5	100 - 80 (456)	C10x15.3	0.016	0.354	0.000	0.362	1.000	4.8.1

Section Capacity Table								
Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	øP <sub>allow</sub> lb	% Capacity	Pass Fail
T1	180 - 160	Leg	P2x.218	2	-16794.20	59870.70	28.1	Pass
		Diagonal	ROHN TS1.5x16 ga	29	-1998.96	6038.67	33.1 35.2 (b)	Pass
		Top Girt	ROHN TS1.5x16 ga	5	-18.00	7292.66	0.4	Pass
		Bottom Girt	ROHN TS1.5x16 ga	7	-290.88	7292.66	4.0 9.1 (b)	Pass
		Guy A@162.75	3/4	462	14593.30	34980.00	41.7	Pass
		Guy B@162.75	3/4	461	14533.50	34980.00	41.5	Pass
		Guy C@162.75	3/4	460	14561.50	34980.00	41.6	Pass
		Top Guy Pull-Off@162.75	3x1/2	457	4661.73	48600.00	9.6	Pass
T2	160 - 140	Leg	P2x.218	59	-17952.60	59870.70	30.0	Pass
		Diagonal	ROHN TS1.5x16 ga	113	-1158.32	6038.67	19.2	Pass
		Top Girt	ROHN TS1.5x16 ga	61	-310.95	7292.66	4.3 7.2 (b)	Pass
		Bottom Girt	ROHN TS1.5x16 ga	64	-310.95	7292.66	4.3	Pass

tnxTower	Job	121-23082	<b>Page</b> 47 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section No.	Elevation ft	Component Type	Size	Critical Element	$P \ lb$	$ otin P_{allow} \\ lb $	% Capacity	Pass Fail
							7.8 (b)	
T3	140 - 120	Leg	P2x.218	116	-24463.00	59870.70	40.9	Pass
		Diagonal	ROHN TS1.5x16 ga	124	-1693.12	6038.67	28.0	Pass
		Top Girt	ROHN TS1.5x16 ga	118	-423.71	7292.66	5.8	Pass
		1	Z .				7.2 (b)	
		Bottom Girt	ROHN TS1.5x16 ga	121	-423.71	7292.66	5.8	Pass
							10.7 (b)	
T4	120 - 100	Leg	P2x.218	173	-30334.60	59870.70	50.7	Pass
	120 100	Diagonal	ROHN TS1.5x16 ga	181	-987.43	6038.67	16.4	Pass
		Bottom Girt	ROHN TS1.5x16 ga	178	-525.41	7292.66	7.2	Pass
		Bottom Girt	KOIII VISI.SXIO ga	170	323.41	7272.00	13.2 (b)	1 433
		Guy A@119.667	1/2	465	7962.06	16140.00	49.3	Pass
		Guy B@119.667	1/2	464	7983.52	16140.00	49.5	Pass
		Guy C@119.667	1/2	463	7988.98	16140.00	49.5	Pass
		Top Guy	3x1/2	175	3447.08	48600.00	7.1	Pass
m.e	100 00	Pull-Off@119.667	DO 5 056	220	44407.00	0.42.62.4.0	12.6	-
T5	100 - 80	Leg	P2.5x.276	230	-41127.00	94363.10	43.6	Pass
		Diagonal	ROHN TS1.5x16 ga	240	-1740.35	6127.23	28.4	Pass
		Top Girt	ROHN TS1.5x16 ga	232	-712.34	7363.82	9.7	Pass
							12.1 (b)	
		Bottom Girt	ROHN TS1.5x16 ga	235	-712.34	7363.82	9.7	Pass
							18.0 (b)	
		Guy A@82.75	1/2	453	7468.01	16140.00	46.3	Pass
		Guy B@82.75	1/2	449	7466.01	16140.00	46.3	Pass
		Guy C@82.75	1/2	443	7480.48	16140.00	46.3	Pass
		Top Guy	L1 1/2x1 1/2x3/16	447	-1761.99	7008.98	25.1	Pass
		Pull-Off@82.75	E1 1/2X1 1/2X3/10	,	1701.77	7000.70	23.1	1 455
		Torque Arm	C10x15.3	451	2390.75	145476.00	36.5	Pass
			C10X13.3	431	2390.13	143470.00	30.3	1 455
т6	90 60	Top@82.75	D2 5 - 276	207	41140.60	76029 20	5.4.1	Dagg
T6	80 - 60	Leg	P2.5x.276	287	-41140.60	76028.20	54.1	Pass
		Diagonal	ROHN TS1.5x16 ga	317	-2156.65	6127.23	35.2	Pass
		Top Girt	ROHN TS1.5x16 ga	289	-712.58	7363.82	9.7	Pass
							14.5 (b)	
		Bottom Girt	ROHN TS1.5x16 ga	292	-712.58	7363.82	9.7	Pass
							18.0 (b)	
T7	60 - 40	Leg	P2.5x.203	320	-44751.00	58302.40	76.8	Pass
		Diagonal	ROHN TS1.5x16 ga	350	-1243.24	6127.23	20.3	Pass
		Top Girt	ROHN TS1.5x16 ga	322	-775.11	7363.82	10.5	Pass
		1					13.1 (b)	
		Bottom Girt	ROHN TS1.5x16 ga	325	-775.11	7363.82	10.5	Pass
		Bottom Girt	Rom visionio ga	323	775.11	7303.02	19.5 (b)	1 455
Т8	40 - 20	Leg	P2.5x.203	353	-45625.30	58302.40	78.3	Pass
10	40 - 20	Diagonal	ROHN TS1.5x16 ga	362	-684.62	6127.23	11.2	Pass
		•	•					
		Top Girt	ROHN TS1.5x16 ga	355	-790.25	7363.82	10.7	Pass
		D G.	DOVDY MOLENIA	2.50	<b>5</b> 00 <b>25</b>	<b>5</b> 2.62.02	13.4 (b)	-
		Bottom Girt	ROHN TS1.5x16 ga	358	-790.25	7363.82	10.7	Pass
							19.9 (b)	
T9	20 - 5	Leg	P2.5x.276	386	-45340.60	76530.40	59.2	Pass
		Diagonal	ROHN TS1.5x16 ga	395	-1101.96	6153.03	17.9	Pass
							19.3 (b)	
		Top Girt	ROHN TS1.5x16 ga	388	-785.32	7363.82	10.7	Pass
		1	Č				13.3 (b)	
		Bottom Girt	ROHN TS1.5x16 ga	392	3694.05	10641.40	34.7	Pass
				27 <b>-</b>			93.1 (b)	_ 400
T10	5 - 0	Leg	P2.5x.276	413	-47135.30	78031.70	60.4	Pass
110	5 - 0	Diagonal						
		Diagonai	ROHN TS1.5x16 ga	439	1671.62	10641.40	15.7	Pass
		т. С:	DOIDITC! 5 16	416	4000.02	10641 40	28.3 (b)	P
		Top Girt	ROHN TS1.5x16 ga	416	4009.92	10641.40	37.7	Pass
							67.9 (b)	
						Leg (T8)	Summary	

tnxTower	Job	121-23082	Page 48 of 48
	Project	180 ft Rohn #80 - Stafford Springs CT	Date 19:45:40 09/06/21
Phone: FAX:	Client	CDT	Designed by

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	øP <sub>allow</sub> lb	% Capacity	Pass Fail
						Diagonal (T1)	35.2	Pass
						Top Girt (T10)	67.9	Pass
						Bottom Girt (T9)	93.1	Pass
						Guy A (T4)	49.3	Pass
						Guy B (T4)	49.5	Pass
						Guy C (T4)	49.5	Pass
						Top Guy Pull-Off (T5)	25.1	Pass
						Torque Arm Top (T5)	36.5	Pass
						Bolt Checks	93.1	Pass
						RATING =	93.1	Pass

Site Name: Hampden Road
Client: CDT
Job Number: 121-23082
Date: 9/6/2021

### Design Base Loads (Factored) per TIA-222-G

Moment (M <sub>u</sub> ):	0.0	k-ft
Shear/Leg (V <sub>u</sub> ):	1.3	k
Compression/Leg (P <sub>u</sub> ):	127.8	k
Uplift/Leg (T <sub>u</sub> ):	0.0	k
Diameter of Prismatic Portion of Pier (d):	1.0	ft
Depth to Base of Foundation:	4.0	ft
Pier Height Above Ground (h):	1.7	ft
Length / Width of Pad (w):	5.0	ft
Thickness of Pad (t):	4.0	ft
Depth Below Ground Surface to Water Table (w):	20.0	ft
Unit Weight of Concrete:	150.0	pcf
Unit Weight of Water:	62.4	pcf
Unit Weight of Soil Above Water Table:	120.0	pcf
Unit Weight of Soil Below Water Table:	65.0	pcf
Friction Angle of Uplift from Top of Pad:	30	Degrees
Friction Angle of Uplift from Base of Pad:	30	Degrees
Uplift Angle Started at Top or Base of Pad (T/B):	Т	
Ultimate Skin Friction:	0	psf
Ultimate Compressive Bearing Pressure:	10000	psf
Capacity Increase (Due to Transient Loads):	1.00	
Bearing Strength Reduction Factor ( $\phi_s$ ):	0.60	
Uplift Strength Reduction Factor ( $\phi_s$ ):	0.75	

### **Axial Capacities**

Nominal Uplift Capacity per Leg ( $\phi_s T_n$ ):	11.4 k
Nominal Compressive Capacity per Leg ( $\phi_s P_n$ ):	150.0 k
P <sub>u</sub> :	131.6 k

 $T_u/\varphi_s T_n$ : 0.00 Result: OK  $P_u/\varphi_s P_n$ : 0.88 Result: OK



Centered on Solutions

# Structural Analysis Report

Antenna Mount Analysis

T-Mobile Site #: CTHA830A

157 Hampden Road Stafford Springs, CT

Centek Project No. 21005.22

Date: May 4, 2021
Rev 1: August 11, 2021

Max Stress Ratio = 70.8%



T-Mobile USA 35 Griffin Road Bloomfield, CT 06002



CENTEK Engineering, Inc.

Structural Analysis – Mount Analysis T-Mobile Site Ref. ~ CTHA830A Stafford Springs, CT Rev 1 ~ August 11, 2021

# Table of Contents

### SECTION 1 - REPORT

- ANTENNA AND APPURTENANCE SUMMARY
- STRUCTURE LOADING
- CONCLUSION

### SECTION 2 - CALCULATIONS

- WIND LOAD ON APPURTENANCES
- RISA3D OUTPUT REPORT

### SECTION 3 - REFERENCE MATERIALS (NOT INCLUDED WITHIN REPORT)

RF DATA SHEET, DATED 07/20/2021

TABLE OF CONTENTS TOC-1



#### Centered on Solutions

August 11, 2021

Mr. Kyle Richers **Transcend Wireless** 10 Industrial Ave., Suite 3 Mahwah, NJ 07430

Re: Structural Letter ~ Antenna Mount T-Mobile - Site Ref: CTHA830A 157 Hampden Road Stafford Springs, CT 06076

Centek Project No. 21005.22

Dear Mr. Richers,

Centek Engineering, Inc. has reviewed the T-Mobile antenna installation at the above referenced site. The purpose of the review is to determine the structural adequacy of the proposed mount, consisting of three (3) V-frame sector mounts (SitePro P/N: VFA12) to support the proposed equipment configuration. The review considered the effects of wind load, dead load and ice load in accordance with the 2015 International Building Code as modified by the 2018 Connecticut State Building Code (CTBC) including ASCE 7-10 and ANSI/TIA-222-G Structural Standards for Steel Antenna Towers and Supporting Structures.

The loads considered in this analysis consist of the following:

#### T-Mobile:

V-Frames: Three (3) Ericsson AIR6449 panel antennas, three (3) RFS APXVAALL24\_43-U-NA20 panel antennas, three (3) Ericsson 4480 remote radio heads and three (3) Ericsson 4460 remote radio heads mounted on three (3) V-Frames with a RAD center elevation of 171-ft +/- AGL.

The antenna mount was analyzed per the requirements of the 2015 International Building Code as modified by the 2018 Connecticut State Building Code considering a nominal design wind speed of 97 mph for Stafford as required in Appendix N of the 2018 Connecticut State Building Code.

A structural analysis of tower and foundation needs to be completed prior to any work.

ELITES SIONAL

Based on our review of the installation, it is our opinion that the subject antenna mount has sufficient capacity to support the aforementioned antenna configuration. If there are any questions regarding this matter, please feel free to call.

Respectfully Submitted by:

Timothy J. Lynn, PE Structural Engineer

Prepared by:

Fernando J. Palacios

**Engineer** 

CENTEK Engineering, Inc.
Structural Analysis – Mount Analysis
T-Mobile Site Ref. ~ CTHA830A
Stafford Springs, CT
Rev 1 ~ August 11, 2021

# Section 2 - Calculations

Subject: Location:

Rev. 0: 08/04/2021

Loads on Equipment

Stafford Springs, CT

Prepared by: F.J.P.. Checked by: T.J.L. Job No. 21005.22

#### **Development of Design Heights, Exposure Coefficients,** and Velocity Pressures Per TIA-222-G

#### Wind Speeds

**Basic Wind Speed** V := 97mph (User Input - 2018 CSBC Appendix N) Basic Wind Speed with Ice  $V_i := 50$ mph (User Input per Annex B of TIA-222-G)

#### Input

Structure Type = (User Input)  $Structure\_Type := Lattice$ Structure Category = SC := II(User Input) Exposure Category = Exp := C(User Input)

Structure Height = h := 180ft (User Input) Height to Center of Antennas = z := 171ft (User Input)

Radial Ice Thickness =  $t_i := 1.00$ in (User Input per Annex B of TIA-222-G)

Radial Ice Density = Id := 56.00pcf (User Input) Topographic Factor =  $K_{zt} := 1.0$ (User Input)  $K_a := 1.0$ (User Input) Gust Response Factor =

 $G_{H} = 1.12$ 

#### Output

Wind Direction Probability Factor =

$$\begin{aligned} K_d &:= \left| \begin{array}{c} \text{if } \text{ } \text{Structure\_Type} = \text{Pole} \\ \left\| \begin{array}{c} 0.95 \\ \text{if } \text{ } \text{Structure\_Type} = \text{Lattice} \\ \left\| \begin{array}{c} 0.85 \\ \end{array} \right| \end{aligned} \right|$$

(Per Table 2-2 of TIA-222-G)

(User Input)

(Per Table 2-3 of TIA-222-G)

Importance Factors =

$$I_{Wind} := \left\| \begin{array}{c} \text{if } SC = 1 \\ \left\| 0.87 \\ \end{array} \right\| = 1$$

$$\left\| 1.00 \\ \text{if } SC = 2 \\ \left\| 1.00 \\ \end{array} \right\|$$

$$\left\| 1.15 \right\|$$

$$I_{ice} := \left| \begin{array}{c} \text{if SC} = 1 \\ 0 \\ \text{if SC} = 2 \\ \left\| \begin{array}{c} 1.00 \\ \text{If SC} = 3 \\ \end{array} \right\| 1.25$$

 $K_{iz} := \left(\frac{z}{33}\right)^{0.1} = 1.179$ 

 $t_{iz} := 2.0 \cdot t_i \cdot I_{ice} \cdot K_{i\underline{z}} \cdot K_{zt}^{0.35} = 2.358$ 

$$Kz := 2.01 \cdot \left( \left( \frac{z}{zq} \right) \right)^{\frac{z}{\alpha}} = 1.417$$

Velocity Pressure w/o Ice Antennas =

Velocity Pressure Coefficient Antennas =

 $qz := 0.00256 \cdot K_d \cdot Kz \cdot V^2 \cdot I_{Wind} = 29$ 

psf

Velocity Pressure with Ice Antennas =

 $qz_{ice} := 0.00256 \cdot K_d \cdot Kz \cdot V_i^2 \cdot I_{Wind} = 8$ 



Loads on Equipment

Location:

Stafford Springs, CT

Rev. 0: 08/04/2021

Prepared by: F.J.P.. Checked by: T.J.L. Job No. 21005.22

#### **Development of Wind & Ice Load on Antennas**

#### **Antenna Data:**

Antenna Model = RFS APXVAALL24\_43-U-NA20

Antenna Shape = Flat (User Input)

Antenna Height =  $L_{ant} = 95.9$  in (User Input)

Antenna Width = W<sub>ant</sub> := 24.0 in (User Input)

Antenna Thickness =  $T_{ant} = 8.5$  in (User Input)

Antenna Weight = WT<sub>ant</sub> := 150 lbs (User Input)

Number of Antennas = N<sub>ant</sub> := 1 (User Input)

Antenna Aspect Ratio =  $Ar_{ant} := \frac{L_{ant}}{W_{ant}} = 4.0$ 

Antenna Force Coefficient = Ca<sub>ant</sub> = 1.27

#### Wind Load (without ice)

Surface Area for One Antenna = 
$$SA_{antF} := \frac{L_{ant} \cdot W_{ant}}{144} = 16$$
 sf

Total Antenna Wind Force Front = 
$$F_{ant} := qz \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{antF} = 658$$
 lbs

Surface Area for One Antenna = 
$$SA_{antS} := \frac{L_{ant} \cdot T_{ant}}{144} = 5.7$$
 sf

Total Antenna Wind Force Side = 
$$F_{ant} := qz \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{antS} = 233$$
 | lbs

#### Wind Load (with ice)

Surface Area for One Antenna w/ Ice = 
$$SA_{ICEantF} := \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(W_{ant} + 2 \cdot t_{iz}\right)}{144} = 20.1$$
 sf

Total Antenna Wind Force w/ Ice Front = 
$$Fi_{ant} := qz_{ice} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{ICEantF} = 219$$
 lbs

Surface Area for One Antenna w/ Ice = 
$$SA_{ICEantS} := \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(T_{ant} + 2 \cdot t_{iz}\right)}{144} = 9.2$$
 sf

Total Antenna Wind Force w/ Ice Side = 
$$Fi_{ant} := qz_{lce} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{ICEantS} = 101$$
 lbs

#### **Gravity Load (without ice)**

#### Gravity Loads (ice only)

Volume of Each Antenna = 
$$V_{ant} := L_{ant} \cdot W_{ant} \cdot T_{ant} = 2 \cdot 10^4$$
 cu in

$$\text{Volume of Ice on Each Antenna} = \qquad V_{\text{ice}} \coloneqq \left( L_{\text{ant}} + 2 \cdot t_{\text{iz}} \right) \cdot \left( W_{\text{ant}} + 2 \cdot t_{\text{iz}} \right) \cdot \left( T_{\text{ant}} + 2 \cdot t_{\text{iz}} \right) - V_{\text{ant}} = 2 \cdot 10^4$$

Weight of Ice on Each Antenna = 
$$W_{ICEant} := \frac{V_{ice}}{1728} \cdot Id = 603$$
 lbs

Weight of Ice on All Antennas = 
$$W_{ICEant} \cdot N_{ant} = 603$$



Loads on Equipment

Location:

Stafford Springs, CT

Rev. 0: 08/04/2021

Prepared by: F.J.P.. Checked by: T.J.L. Job No. 21005.22

#### **Development of Wind & Ice Load on Antennas**

#### Antenna Data:

Antenna Model = Ericsson - AIR6449 B41

Antenna Shape = Flat (User Input)

Antenna Height =  $L_{ant} := 33.1$  in (User Input)

Antenna Width = W<sub>ant</sub> := 20.5 in (User Input)

Antenna Thickness =  $T_{ant} = 8.3$  in (User Input)

Antenna Weight = WT<sub>ant</sub> := 103 lbs (User Input)

Number of Antennas =  $N_{ant} = 1$  (User Input)

Antenna Aspect Ratio =  $Ar_{ant} := \frac{L_{ant}}{W_{ant}} = 1.6$ 

Antenna Force Coefficient = Ca<sub>ant</sub> = 1.2

#### Wind Load (without ice)

Surface Area for One Antenna = 
$$SA_{antF} := \frac{L_{ant} \cdot W_{ant}}{144} = 4.7$$
 sf

Total Antenna Wind Force Front = 
$$F_{ant} := qz \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{antF} = 184$$

Surface Area for One Antenna = 
$$SA_{antS} := \frac{L_{ant} \cdot T_{ant}}{144} = 1.9$$
 sf

Total Antenna Wind Force Side = 
$$F_{ant} := qz \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{antS} = 74$$
 lbs

#### Wind Load (with ice)

Surface Area for One Antenna w/ Ice = 
$$SA_{ICEantF} := \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(W_{ant} + 2 \cdot t_{iz}\right)}{144} = 6.6$$
 sf

Total Antenna Wind Force w/ Ice Front = 
$$Fi_{ant} := qz_{ice} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{ICEantF} = 69$$
 lbs

Surface Area for One Antenna w/ Ice = 
$$SA_{ICEantS} := \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(T_{ant} + 2 \cdot t_{iz}\right)}{144} = 3.4$$
 sf

Total Antenna Wind Force w/ Ice Side = 
$$Fi_{ant} := qz_{ice} \cdot G_H \cdot Ca_{ant} \cdot K_a \cdot SA_{ICEantS} = 35$$
 lbs

#### **Gravity Load (without ice)**

#### **Gravity Loads (ice only)**

Volume of Each Antenna = 
$$V_{ant} := L_{ant} \cdot W_{ant} \cdot T_{ant} = 5632$$
 cu in

$$\text{Volume of Ice on Each Antenna} = \qquad \quad V_{\text{ice}} \coloneqq \left( L_{\text{ant}} + 2 \cdot t_{\text{iz}} \right) \cdot \left( W_{\text{ant}} + 2 \cdot t_{\text{iz}} \right) \cdot \left( T_{\text{ant}} + 2 \cdot t_{\text{iz}} \right) - V_{\text{ant}} = 6778$$

Weight of Ice on Each Antenna = 
$$W_{ICEant} := \frac{V_{Ice}}{1728} \cdot Id = 220$$
 lbs

Weight of Ice on All Antennas = 
$$W_{ICEant} \cdot N_{ant} = 220$$



Loads on Equipment

Location:

Stafford Springs, CT

Rev. 0: 08/04/2021

Prepared by: F.J.P.. Checked by: T.J.L. Job No. 21005.22

### **Development of Wind & Ice Load on RRUS's**

#### **RRUS Data:**

RRUS Model = Ericsson 4480 B71+B85

RRUS Shape = Flat (User Input) RRUS Height =  $L_{RRUS} = 21.8$  in (User Input)

RRUS Width =  $W_{RRUS} := 15.7$  in (User Input) RRUS Thickness =  $T_{RRUS} := 7.5$  in (User Input)

RRUS Weight = WT<sub>RRUS</sub> := 84 lbs (User Input)

Number of RRUS's =  $N_{RRUS} := 1$ 

RRUS Aspect Ratio =  $Ar_{RRUS} := \frac{L_{RRUS}}{W_{RRUS}} = 1.4$ 

RRUS Force Coefficient = Ca<sub>RRUS</sub> = 1.2

#### Wind Load (without ice)

Surface Area for One RRUS =  $SA_{RRUSF} := \frac{L_{RRUS} \cdot W_{RRUS}}{144} = 2.4$  sf

Total RRUS Wind Force =  $F_{RRUS} := qz \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{RRUSF} = 93$  lbs

Surface Area for One RRUS =  $SA_{RRUS} := \frac{L_{RRUS} \cdot T_{RRUS}}{144} = 1.1$  sf

Total RRUS Wind Force =  $F_{RRUS} := qz \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{RRUSS} = 44$  lbs

#### Wind Load (with ice)

Surface Area for One RRUS w/ Ice =  $SA_{ICERRUSF} := \frac{\left(L_{RRUS} + 2 \cdot t_{iz}\right) \cdot \left(W_{RRUS} + 2 \cdot t_{iz}\right)}{144} = 3.8$  sf

Total RRUS Wind Force w/ Ice =  $Fi_{RRUS} := qZ_{Ice} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{ICERRUSF} = 39$  lbs

Surface Area for One RRUS w/ Ice =  $SA_{ICERRUSS} := \frac{\left(L_{RRUS} + 2 \cdot t_{iz}\right) \cdot \left(T_{RRUS} + 2 \cdot t_{iz}\right)}{144} = 2.2 \quad \text{sf}$ 

Total RRUS Wind Force w/ Ice =  $Fi_{RRUS} := qZ_{ice} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{ICERRUSS} = 23$  lbs

#### **Gravity Load (without ice)**

Weight of All RRUSs = WT<sub>RRUS</sub> • N<sub>RRUS</sub> = 84

#### Gravity Loads (ice only)

Volume of Each RRUS =  $V_{RRUS} = L_{RRUS} \cdot W_{RRUS} \cdot T_{RRUS} = 2567$  cu in

Volume of Ice on Each RRUS =  $V_{ice} := (L_{RRUS} + 2 \cdot t_{iz}) \cdot (W_{RRUS} + 2 \cdot t_{iz}) \cdot (T_{RRUS} + 2 \cdot t_{iz}) - V_{RRUS} = 4045$ 

Weight of Ice on Each RRUS =  $W_{ICERRUS} := \frac{V_{Ice}}{1778} \cdot Id = 131$  lbs

Weight of Ice on All RRUSs =  $W_{ICERRUS} \cdot N_{RRUS} = 131$ 



Loads on Equipment

Location:

Stafford Springs, CT

Rev. 0: 08/04/2021

Prepared by: F.J.P.. Checked by: T.J.L. Job No. 21005.22

#### **Development of Wind & Ice Load on RRUS's**

#### **RRUS Data:**

RRUS Model = Ericsson 4460 B25+B66

RRUS Shape = Flat (User Input) RRUS Height =  $L_{RRUS} := 19.6$  in (User Input)

RRUS Width =  $W_{RRUS} := 15.7$  in (User Input) RRUS Thickness =  $T_{RRUS} := 12.1$  in (User Input)

RUS Thickness =  $T_{RRUS} = 12.1$  in (User Input) RRUS Weight =  $WT_{RRUS} = 109$  lbs (User Input)

Number of RRUS's =  $N_{RRUS} := 1$ 

RRUS Aspect Ratio =  $Ar_{RRUS} := \frac{L_{RRUS}}{W_{RRUS}} = 1.2$ 

RRUS Force Coefficient = Ca<sub>RRUS</sub> = 1.2

#### Wind Load (without ice)

Surface Area for One RRUS =  $SA_{RRUSF} := \frac{L_{RRUS} \cdot W_{RRUS}}{144} = 2.1$  sf

Total RRUS Wind Force =  $F_{RRUS} := qz \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{RRUSF} = 83$  lbs

Surface Area for One RRUS =  $SA_{RRUS} := \frac{L_{RRUS} \cdot T_{RRUS}}{144} = 1.6$  sf

Total RRUS Wind Force =  $F_{RRUS} := qz \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{RRUSS} = 64$  lbs

#### Wind Load (with ice)

Surface Area for One RRUS w/ Ice =  $SA_{ICERRUSF} := \frac{\left(L_{RRUS} + 2 \cdot t_{iz}\right) \cdot \left(W_{RRUS} + 2 \cdot t_{iz}\right)}{144} = 3.4$  sf

Total RRUS Wind Force w/ Ice =  $Fi_{RRUS} := qz_{Ice} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{ICERRUSF} = 36$  lbs

Surface Area for One RRUS w/ Ice =  $SA_{ICERRUSS} := \frac{\left(L_{RRUS} + 2 \cdot t_{iz}\right) \cdot \left(T_{RRUS} + 2 \cdot t_{iz}\right)}{144} = 2.8 \quad \text{sf}$ 

Total RRUS Wind Force w/ Ice =  $Fi_{RRUS} := qz_{ice} \cdot G_H \cdot Ca_{RRUS} \cdot K_a \cdot SA_{ICERRUSS} = 29$  lbs

#### **Gravity Load (without ice)**

Weight of All RRUSs = WT<sub>RRUS</sub> • N<sub>RRUS</sub> = 109

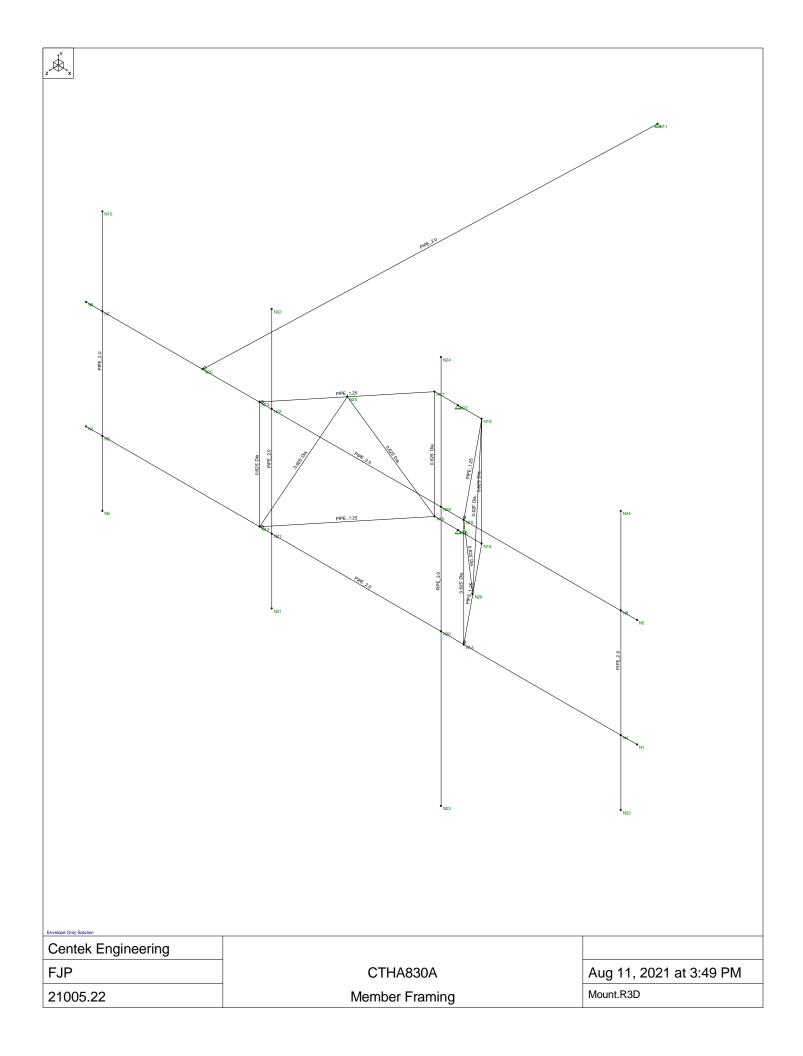
#### Gravity Loads (ice only)

Volume of Each RRUS =  $V_{RRUS} = L_{RRUS} \cdot W_{RRUS} \cdot T_{RRUS} = 3723$  cu in

Volume of Ice on Each RRUS =  $V_{ice} := (L_{RRUS} + 2 \cdot t_{iz}) \cdot (W_{RRUS} + 2 \cdot t_{iz}) \cdot (T_{RRUS} + 2 \cdot t_{iz}) - V_{RRUS} = 4624$ 

Weight of Ice on Each RRUS =  $W_{ICERRUS} := \frac{V_{ice}}{1728} \cdot Id = 150$  lbs

Weight of Ice on All RRUSs =  $W_{ICERRUS} \cdot N_{RRUS} = 150$ 



 Centered on Solutions
 www.centekeng.com

 63-2 North Branford Road
 P: (203) 488-0580

 Branford, CT 06405
 F: (203) 488-8587

### fţ`cVUŁAcXY`GYHjb[g

i, croent chijag	
Öãr]  æ ÂÛ^&dã } • ÁÇ ¦ÁT ^{ à^¦ÁÔæ}&•	lí Á
T acc AQ c^; at AU^&ca[} • A[   AT ^{ a^; AO ab&•	JΪÁ
Q&  å^A) @ ab AO^-1   { acat } N	ΫΛ•
(0,84 ^ æ • ^ ÁÞ æ áða) * ÁÐ æð æ 8 áð Á ( ¦ ÁY ð) å Ñ	Ϋ^•
Q&  a^A/ æ] a * Ñ	ΫΛ•
V¦æ) • ÁŠ[æå ÁÖc } ÁQ c^¦• ^ & c3 * ÁY [[å ÁY æ  Ñ	ΫΛ•
Œ^æKs[æåAT^•@Ka}âGD	FII
T^\*^Á/[  ^\a) &^Á@JD	ÈG
ÚĒÖ^ cæ605; æ î•ã•Á/[ ^¦æ); &^	€É €Ã
(D) &  ` å^ÁÚ ÉÖ^   cæÁ( ¦Á / æ  •Ñ	Ÿ^•
OE ({ aea8a+  ^ÁQ^\ ae^\Á\Jca-}^••Á[   Á/ a+  •Ñ	ΫΛ•
Tæ¢Á@^¦æ@aj}•Á[¦ÁYæþÁÙ@~}^••	Н
Ö kaçı ac ÁOB&\   ^ kacaqı } ÁÇab ^ & a GD	HŒĞ
Yæ ÁT^•@Ûã^ÁÇÃD	FG
Òã ^} •[  * cā[ } ÁÔ[ ] ç ^   * ^ } & ^ Á/[   ÞÁÇF ÐÐ	
X^¦a®æk/Oo¢ã	Ÿ
Ő∥(àæþÁT^{ à^¦ÁU¦ã^}cænaã[}ÁÚ æ}^	ÝΖ
Ùæ <b>38AÛ[ ç</b> ^	Ù]æ•^ÁŒ&^ ^¦æ•^å
Ö^}æ{ 8&AÛ[  ç^	OB&\ ^ \ae^\\\ \ AU[  ç^\
P[ œÜ[   ^ å ÁÛ œ^^  ÁÔ[ å^	OEDÙÔÁFI c@ÇHÎ €ËF€DKAŠÜØÖ
Œábĕ•œÛœã-}^••Ñ	Ÿ^∙Ç@\¦æaãç^D
ÜOÙOEÔ[}}^&ca[}ÂÔ[å^	OEDÙÔÁFI c@ÇHÎ €ËF€DMÁCEÙÖ
Ô[ åÁØ[¦{ ^åÁÙ¢^ ÁÔ[å^	OED) CÂÙ F€€ËF€KÂOEÙ Ö
Y [ [ å ÆO[ å^	OEY ÔÁÞ ÖÙÉFGKÁÐEÙÖ
Y [[åÁv^{] ^ aæč  ^	ŁÆ€€Ø
Ô[ } & ^¢\ÁÔ[ å^	OEÔ CÁHFÌ ÉFF
Tæ[}¦^ÂÔ[å^	OEÔCà H€ÉFFKÁOEÙÔ
OĘ~{ ā,~{ ÂÔ[ å^	OEDZÁOZÖT FÉF€KÁOZLÚÖÁZÄÓ* ájáðj.*
Ùœ <b>a</b> ,  ^••ÂÛc^^ ÆÔ[ å^	OEDJÔÁFI c@ÇHÎ €ÉF€DMÁCELJÖ
Œabŏ•œÛœ~}^••Ñ	Ÿ^• <b>@</b> \¦æãç^D
Þ`{ à^¦¼, ÂÛ@\æÁÜ^* ã;}•	1
Ü^* [4] } ÁÙ] æ&a] * ÁQ,& ^{ ^} cÁQ] D	
Óãæ¢ãæ†ÁÔ[ ˇ{}ÁT^oQ[å	Ò¢æ&oÁQ;c^*¦æaá[}
Úæl{ ^ÁÓ^œÁØæ&q ¦ÁÇÚÔŒD	ĒÍ
Ö[}& ^&\AUd^••AO [&\	Ü^&ca); *
W•^ÁÔ¦æ&\^åÁÙ^&@{ }}•Ñ	Ÿ^•
W•^ÁÔ¦æ&\^åÁÙ^&aaa ) • ÁÙ æàÑ	Þ[
ÓæåÁØlæ{ ∄ * ÁÝ æ}}ã * • Ñ	Þ[
W, `•^å.ÃØ[¦&^ÁYæ}}ā, *•Ñ	ΫΛ•
TāļÁFÁÓæÁÖææ(EÀÚjáæ&āj*Ñ	Þ[
Ô[ } & ^ c^ ÁÜ^àæ ÁÙ^c	ÜÒӌܴÙÒV´ŒÙVTŒÎFÍ
T \$\text{\$\tilde{A}} \tilde{A}\tilde{U}c^\ \tilde{A}\tilde{\tilde{U}} \tilde{\tilde{A}} \tilde{\tilde{U}} \tilde{\tilde{U}} \tilde{\tilde{A}} \tilde{\tilde{U}} \tilde{\tilde{U}} \tilde{\tilde{A}} \tilde{\tilde{U}} \tilde{	F
T æ¢ÁÑ ÁÙ¢^^ Á[¦ÁÔ[ °{})	Ì

P: (203) 488-0580 F: (203) 488-8587

R[àÁÞ˚{à^¦ K GF€€ÍÈGG T[å^|ÁÞæ{^ KÔVPOÈH€Œ

### fł, `cVUŁ'A cXY 'GYltijb[ gž7 cblijbi YX

Ù^ã{ 88,4Ô[ å^	ŒÙÔÒÄ ËF€
Ù^ã{ 88/40æ ^AÒ ^cæaa } AGaD	Þ[ ơ�Ô} c^\^å
Ođá ÅÓæ ^ ÁY ^ð T @Ñ	Ϋ́Λ•
ÔœÝ	È€G
ÔæZ	ÆG
V <i>Ř</i> ÝÆĢ^&D	Þ[ ðÔ} &\^å
VÆÆĢ^&D	Þ[ ðÔ} &\^å
ÜŔ	H
ÜÆ	H
ÔớÔ¢] ĐÝ	Ĕĺ
ÔáÔ¢] ÉZ	ĔÍ
ÙÖF	F
ÙÖÙ	F
ÙF	F
VŠÁĢ^&D	ĺ
Üã \ ÂÔæ	CÁI, LÁCO.
Ölão/Ôæc	U @\
U{ ÂZ	F
U{ Ä′	F
	F
ÔåÃÝ	F
Ü @ <i>Ā</i> Z	F
Ü <b>Ģ</b> Á	F

## <chFc``YX'GhYY`DfcdYff]Yg

	Šæà^	ÒÆŽ•ãã	ÕÆŽ•ãã	þř	V@N¦{ ÁÇEDFÈÌ	ÈÖ^}•ãĉŽÐcâHá	Ÿã∿ åŽo•ãã	Ü^	ØŽ•ãa	Üc
F	OEHÎ ÁÕ¦ÈHÎ	GJ€€€	FFFÍ I	ÈH	ÊÍ	ÈΙ	HÎ	FĚ	ĺĺ	FÈG
G	OÉÏGÁզɀ	GJ€€€	FFFÍ I	ÈH	ÊÍ	ÈΙ	Í€	FÈ	ĺĺ	FÈG
Н	ŒJG	GJ€€€	FFFÍ I	ÈH	Ēĺ	ÈΙ	Í€	FÈ	ĺĺ	FÈG
1	OÉ €€ÁÕ¦ÈIG	GJ€€€	FFFÍ I	ÈH	ÊÍ	ÈΙ	IG	FÈH	ĺĺ	FÈ
ĺ	OÉ €€ÁÕ¦ÈÌÎ	GJ€€€	FFFÍ I	ÈH	Ēĺ	ÈΙ	ΙÎ	FÈG	ĺĺ	FÈ
Î	OÉ HÁŐ kæå^ÁÓ	GJ€€€	FFFÍ I	ÈH	ÊÍ	ÈΙ	HÍ	FĚ	ĺĺ	FÈG

### <chFc``YX'GhYY`GYWfjcb'GYhg</pre>

	Šæà^	Ù@a}^	V^]^	Ö^• ã} ÁŠã c	: Tæe^¦ãæ¢	Ö^• ã} Áܡ È	ÈOEÄŽjGá	Q^Ããjlá	Q:Æãjlá	RÁŽ)lá
F	OE;c^}}æÁTæ•c	ÚŒÓ ŒÈ	Ô[  `{ }		01 1 0 0 1 00 1	v j accep	FÈ€G	ĒĠ	ĖĠΪ	FÈGÍ
G	GÄÁÚ₫^	ÚŒÓ ŒÈ	Ó^æ{		OÉ HÁŐ kaá EE	•   •	FÈ€G	ĒĞ	ĒĠ	FÈGÍ
Н	FÄÁÚÃ ^	ÚŒÓ FÈ€	Ó^æ		OÉ HÁŐ¦ æå EE	. ] ~~~	ÈÎJ	ÈÈÌH	ÈÈÌH	ÈÎÎ
1	U ď at * ^ l ´ FÌĐÍ ÄÁÚa] ^	ÚÓJÓ FÉGÍ	Ó^æ{		OÉ HÁŐ kaá EE	•   •	Ēď	ÈÌI	ÈÌΙ	ÈĤÌ
ĺ	Ùœàãã^¦	ÚŒÓ ŒÈ	Ó^æ	Úą ^	OÉ HÁŐ¦ æå EE	V^] a&ae	FÈ€G	ĒĠ	ĒĠ	FÈGÍ
Î	ÉGÁÁÓæ	€É G ØÖæ€È	Ô[  `{ }	ÓŒÜ	OHÎ ÁÕ¦ ÈHÎ	V^] ã&æ	ÈH€Ï	È€Ë	È€Ë	È€FÍ

### <chFc``YX'GhYY`8 Yg][ b'DUfUa YhYfg</pre>

	Šæà^	Ù@ <b>≱</b> ^	Š^}* c@Že	á Šà^^Žoá	Šà::Žeá	Š&[{]Á[]ŽÊ	HŠ&[{]Áa[cŽH	EŠËq¦ĭÈ	È S^^	S::	Ôà	Ø″}&da⊞E
F	TF	GÄÁÚ jā ^	FŒÏ Í	Ù^*{ ^}	c Ù^*{ ^}c	Šà^^			GÈ	ŒÈ		Šæe^¦æ¢
G	TG	GÄŰÃ ^	FŒÎÍ	Ù^*{ ^}	c Ù^*{ ^}c	Šà^^			GÈ	ŒÈ		Šæe^læ
Н	TH	Ùœàãã^	F∰ìÎ			Šà^^			F	F		Šæe^¦æ
1	TI	U`dã*^¦´E	i £io	Ù^*{ ^}	c Ù^*{ ^}c	Šà^^			È	È		Šæe^læ¢

P: (203) 488-0580 F: (203) 488-8587

Ô[{]æ}^ Ö^• ã} ^¦

K Ô^} c^\ ÁÒ} \* 3 ^^ \ 3 \*

K ØRÚ R[àÁÞ\*{à^¦ T[å^|ÁÞæ{^ K OFۃÍÈGG KÔVPOÈH€Œ

Œ\*ÁFFÉÆGEGF IK€ÍÁÚT Ô@^&\^åÁÓ^KÁ/RŠ

### <chFc``YX'GhYY'8 Yg][ b'DUfUa YhYfg'f7 cbh]bi YXŁ</pre>

	Šæà^∣	Ù@A}^ Š^}*c@Žc	á Šà^^Žoá	Šà∷Žoá	Š&[{]Á[]ŽĦ	HŠ&[{]Áa[cŽH	EŠEq¦ĭEES^^	S::	Ôà	Ø″}&ca⊞
ĺ	ΤÍ	Uˇdẫ*^l´雦 <b>GÈÌ</b>	Ù^*{ ^}c	Ù^*{ ^}c	Šà^^		È	È		Šæe^læ
Î	ΤÎ	Uˇdẫ*시´ GÈÌ	Ù^*{ ^}c	Ù^*{ ^}c	Šà^^		È	È		Šæe^¦æ
Ϊ	ΤÏ	Uˇdẫ*^l´誰 GÈÌ	Ù^*{ ^}c	Ù^*{ ^}c	Šà^^		È	È		Šæe^¦æ¢
Ì	ΤÌ	ÉLGÍÄ ÁÓÆ GÉL					ĒÍ	Ēί		Šæe^¦æ
J	TJ	ÉT GÍ ÄHÓÆ HET					ĒÍ	Ēί		Šæe^¦æ¢
F€	TF€	ĒlGÍÄKÓæd GÈÌÌÍ					Èí	Ēί		Šæe^¦æ
FF	TFF	ĒlGÍÄHÓæd GEÌÌÍ					ĒÍ	Ēί		Šæe^¦æ¢
FG	TFG	ÉLGÍÄÁÓæ HOÈLÌÍ					ĒÍ	Ēί		Šæe^¦æ
FH	T FH	EÈGÍÄÁÓæd GÈÈÌÍ					ĒÍ	Ēί		Šæe^¦æ¢
FI	TFI	LÊGÍÄÁÓæ HGLĚ					Èí	Ēί		Šæe^¦æ¢
FÍ	T FÍ	ĒlgíÄKÓæl Geli					Èí	Ēί		Šæe^¦æ¢
FÎ	T FÎ	OB; c^}}æÁT EEE Î	Ù^*{ ^}c	Ù^*{ ^}c	Šà^^		GÈ	ŒÈ		Šæe^¦æ
FΪ	T FÏ	Οξισ'}}æÁΤΕΕΕ J	Ù^*{ ^}c	Ù^*{ ^}c	Šà^^		GÈ	Œ		Šæe^¦æ¢
FÌ	TG€	OB; c^} } æÁT È Ê Î	Ù^*{ ^}c		Šà^^		GÈ	ŒÈ		Šæe^¦æ¢
FJ	TŒF	OB; c^}}æÁT EEE	Ù^*{ ^}c	Ù^*{ ^}c	Šà^^		GÈ	ŒÈ		Šæe^¦æ¢

### A Ya VYf Df Ja Ufmi8 UfU

	Šæà^	OÁR[ãjc	RÁR[ã}c	SÁR[ãjcÜ[œæ^QÈÈ	È Ù^&cã[}⊕ù@æ}^	V^]^	Ö^• ã} ÁŠã d	c_Tæe^\¦ãa⇔;Ö^•ã*}AEÈ
F	TF	ÞG	ÞF		GÄŰ₫^	Ó^æŧ	Úą ^	OÉ HÁÕ¦ ÈÈV^] a&ae
G	TG	þÎ	ÞÍ		GÄŰĄ ^	Ó^æŧ	Úą ^	OÉ HÁÕ¦ ÈÈV^] aßae
Н	TH	ÞŒ	ÞFF		Ùœàãã^¦	Ó^æŧ	Úą ^	OÉ HÁÕ¦ ÈÈV^] a&æ
	TI	ÞFH	ÞFÏ		Uřdát*^¦íFÌEGÍÄÄÚaj^	Ó^æŧ	Úą ^	OÉ HÁÕ¦ ÈÈV^] å&æ
ĺ	Τĺ	ÞFG	ÞFÎ		Uřdát*^¦′FÉGÍÄÁÚaji^	Ó^æŧ	Úą ^	OÉ HÁŐ¦ ÉÉV^] aßae
Î	ΤÎ	ÞFI	ÞFÌ		Uĭdât*^¦′FÈGÍÄÁÚāj^	Ó^æŧ	Úą ^	OÉ HÁÕ¦ ÈÈV^] å&æ
Ϊ	ΤÏ	ÞFÍ	ÞFJ		Uřdát*^¦′FÉGÍÄÁÚaja^	Ó^æŧ	Úą ^	OÉ HÁÕ¦ ÈÈV^] a&æ
Ì	ΤÌ	ÞFH	ÞFG		ÉGÍÄ ÁÓæl	Ô[   Ĕ		OHÎ ÁÕ¦ HHV^] alkad
J	TJ	ÞFÍ	ÞFI		PÊG ÄKÓæl	Ô[  Ĕ		OEHÎ ÁÕ¦ ÈÈÈV^] aßee
F€	TF€	ÞFG	ÞĞ		ÉLGÍÄ ÁÓæl	Ô[  Ĕ		OHÎ ÁÕ¦ HHV^] alkad
FF	T FF	ÞĞ	ÞFÎ		PÊGÍÄ (Óæ)	Ô[  Ĕ		OHÎ ÁÕ¦ ÈÈV^] ã&æ
FG	T FG	ÞFJ	ÞĜ		PÊGÍÄKÓæk	Ô[  Ĕ	ÓŒÜ	OHÎ ÁÕ¦ HÌ V^] abaq
FH	T FH	ÞĜ	ÞFÍ		ÉGÍÄ ÁÓæl	Ô[  Ĕ		OHÎ ÁÕ¦ HEV^] å&æ
FI	T FI	ÞFJ	ÞFÌ		PÊGÍÄ (Óæ)	Ô[  Ĕ		OHÎ ÁÕ HÊV^] å&æ
FÍ	T FÍ	ÞFÏ	ÞFÎ		PÊG ÄKÓæl	Ô[  Ĕ		OEHÎ ÁÕ¦ ÈÈV^] aßaa
FÎ	T FÎ	ÞF€	ÞJ		ΟΕ;e^}}æÁΤæ•c	Ô[ ˘ Ħ	Úą ^	OÉ HÁÕ¦ ÈÈV^] aßae
FΪ	T FÏ	ÞG	ÞЭH		OE; c^}}æÁTæ•c	Ô[  Ĕ	Úą^	OÉ HÁÕ¦ ÈÈV^] aßae
FÌ	T FÌ	ÞFÏ	ÞFJ		ÜÕÕ	Þ[}^	Þ[}^	ÜÕÖÖ V^] 38æ
FJ	T FJ	ÞFÎ	ÞFÌ		ÜÕÖÖ	þ[}^	þ[}^	ÜÕÖÖ V^] 88æ
G€	TŒ	ÞHG	ÞÆ		OE; c^}}æÁTæ•c	Ô[   Ĕ	Úą^	OÉ HÁÕ¦ ÈÈV^] aßae
GF	T GF	ÞH	ÞН		OE; c^}}æÁTæ•c	Ô[   Ĕ	Úą ^	OÉ HÁŐ HÉV^] asæ

### >c]bh7ccfX]bUhYg'UbX'HYa dYfUhi fYg

	Šæà^	ÝÆká	ŸÆčá	ZÆicá	V^{ ] <i>Ä</i> ŽZ∕á	Ö^cæ&@ÁØ[{ÁÖãæ]@æ*{
F	ÞF	FŒHÏÍ	Ě	GÈGH€GÍJ	€	
G	ÞG	⊞ïí	Ě	GÈGH€GÍJ	€	
Н	ÞH	€	Ě	GÈGH€GÍJ	€	
1	ÞI	FG	Ě	GÈGH€GÍJ	€	
ĺ	ÞÍ	FŒHÏÍ	Н	GÈGH€GÍJ	€	
Î	ÞÎ	⊞ïí	Н	GÈGH€GÍJ	€	
Ϊ	ÞÏ	€	Н	GÉGH€GÍJ	€	

Ô[{]æ}^ Ö^• ã} ^¦ R[àÁÞ˚{à^¦

K Ô^} c^\ ÁÒ} \* 3 ^^ \ 3 \* K ØRÚ

Œ\*ÁFFÉÆGEGF IK€ÍÁÚT Ô@^&\^åÁÓ^KÁ/RŠ

P: (203) 488-0580 F: (203) 488-8587

K GF€€ÍÈGG T[å^|Á¬æ{ ^ KÔVPOÈH€Œ

### >c]bh7ccfX]bUhYg'UbX'HYa dYfUhi fYg'ff/cbh]bi YXŁ

	Šæà^	ÝÆKá	ŸÆïcá	Z <i>Ä</i> Ž-cá	V^{ ] <i>Ä</i> ŽØá	Ö^cæ&@Ø1[{ÁÖãæ @æ* {
Ì	ÞÌ	FG	Н	GÈGH€GÍ J	€	
J	ÞJ	€	Ë	GÈGH€GÍ J	€	
F€	ÞF€	€	ĺ	GÈGH€GÍ J	€	
FF	ÞFF	ŒÎÏ	Н	ËÐIJÏIF	€	
FG	ÞFG	HĒHGÌ	Ě	G <b>ÉGH€</b> GÍJ	€	
FH	₹	HĒHGÌ	Η	G <b>ÉGH€</b> GÍJ	€	
FI	ΞĪ	ÌÈĤIÏIG	Ě	G <b>ÉGH€</b> GÍJ	€	
FÍ	ÞÉ	ÌÈĤIÏIG	Η	G <b>ÉGH€</b> GÍJ	€	
FÎ	ÞFÎ	ÍÈÍÏÏFI	Ě	ËEÌÈCC€€H	€	
FΪ	ÞFÏ	ÍÈÍÏÏFI	Н	ËEÈ€€€€€	€	
FÌ	ÞFÌ	ÎĚIŒÎÎ	Ě	€È€€€€H	€	
FJ	Ð.	ÎĚLOGÌÎ	Η	€È€€€€H	€	
G€	₽Œ	GÈHFÌ HHH	Η	G <b>ÉGH€</b> GÍJ	€	
GF	₽	HÐÌFÎÎÎÏ	Ě	G <b>ÉGH€</b> GÍJ	€	
GG	904	HÐFÎÎÎÏ	Н	G <b>ÉGH€</b> GÍJ	€	
GH	Ð	Ϊ <b>È</b> ΗΗΗΗ	ËH	G <b>ÉGH€</b> GÍJ	€	
G	Ðd	Ϊ <b>È</b> ΗΗΗΗ	Î	G <b>ÉGH€</b> GÍJ	€	
GÍ	ÞĞ	l Ě l Î l Ì Î	Н	FÈFÍ FĠ	€	
Ĝ	ÞĜ	ΪÈÍHÍFI	Ě	FÈFÍ FHF	€	
ĞÏ	ÞĞ	ÎÈ	Н	Ë€È	€	
GÌ	ÐĢ	ÎÈ	Ě	Ë€È	€	
GJ	ÞGJ	ΪÈΗΗΗ	Н	GÈGH€GÍJ	€	
H€	ÞH€	ΪÈΗΗΗ	Ě	G <b>É</b> GH€GÍ J	€	
HF	ÞF	HÐFÍÍÍÏ	Ë	GÈGH€GÍJ	€	
HG	ÞHG	HÐFÎÎÏÏ	ĺ	GÈGH€GÍ J	€	
HH	ÞН	FG	Ë	GÈGH€GÍ J	€	
Н	ÞН	FG	ĺ	GÈGH€GÍ J	€	

### >c]bh6ci bXUfm7cbX]h]cbg

	R[ā]oÁŠæà^	ÝÁŽÐajá	ŸÄŽÐajá	ZÁŽE3já	ÝÁÜ[dĚŽËdĐæåá	ŸÁÜ[dĚŽËdĐæåá	ZÁÜ[dĚŽË-6Dænaaá
F	ÞFF	Ü^æ <b>&amp;</b> æ <b>[</b> ] }	Ü^æ&a <b>i</b> }	Ü^æ <b>\$</b> æ <b>[</b> ]			
G	ÞFÎ						
Н	ÞFÏ						
1	ÞFÌ						
ĺ	ÞFJ						
Î	ÞĞ	Ü^æ <b>%</b> æ <b>[</b> }	Ü^æ&a <b>i</b> }	Ü^æ <b>&amp;</b> æ <b>[</b> ]			
Ï	ÞĠ	Ü^æ <b>%</b> æ <b>[</b> }	Ü^æ&di}	Ü^æ <b>\$</b> æ <b>[</b> }			
Ì	ÞŒ						
J	Þ <b>G</b>						
F€	ьG						
FF	ÞH€						

### A Ya VYf 'Dc]bhi@:UXg'f6 @ '&. '8 YUX'@:UXŁ

	T^{à^¦ÁŠæà^	Öã^&cã}	Tæ*}ããå^ŽLÊËcá	Š[&aedā[}ŽadĒĀá
F	T FÎ	Ÿ	ÉÉÉ G	Ě
G	T FÎ	Ϋ	⊞é G	Н
Н	T FÏ	Ϋ	ilei í	Ě
1	T FÏ	Ϋ	ilei í	ΪĚ
ĺ	T FÏ	Ÿ	⊞÷€J	Н

Ô[{]a≱^ Ö^•ã\*}^¦ R[àÁn>\*{à^¦ T[å^|Án>aa{^

K Ô^} &^\ÂÒ}\*ãj^^¦āj\* KØRÚ ¦ KGF€€ÍÈGG ^ KÔVPOÈH€Œ

A Ya VYf 'Dc]bh'@cUXg'f6 @ '&'. '8 YUX'@cUXŁff cbhjbi YXŁ

	T^{ à^¦ÁŠæà^	Öã^&cã}}	Tæ*}ããå^ŽÉËæá	Š[&æqā[}ŽedĒĀá
Î	T FÏ	Ÿ	ËE I	Î

### 

	T^{ à^¦ÁŠæà^	Öã^&ã}	Tæ*}ããå^ŽÊËcá ⊞HF	Š[&andal}ŽedĒĀá
F	T FÎ	Ÿ		Ě
G	T FÎ	Ÿ	⊞F	Н
Н	T FÏ	Ÿ	<del>⊞</del> €G	Ě
1	T FÏ	Ÿ	<del>⊞l</del> €G	ΪĚ
ĺ	T FÏ	Ϋ	<del>III</del> Í	H
Î	T FÏ	Ÿ	⊞HF	Î

### A Ya VYf 'Dc]bh@cUXg f6 @r ( . K]bX k Jh \=\N LŁ

	T^{ à^¦ÁŠæà^	Öā^&cā[}	Tæ*}ããå^ŽÉËcá	Š[& <b>encā</b> [}ŽeDĀ(á
F	T FÎ	Ý	È€FÌ	Ě
G	T FÎ	Ý	ÈEFÌ	H
Н	T FÏ	Ý	ÈÉÍ F	Ě
- 1	T FÏ	Ý	<b>È</b> Í F	ΪĚ
ĺ	T FÏ	Ý	ÈEGJ	Н
Î	T FÏ	Ý	È€GH	Î

### A Ya VYf 'Dc]bh@cUXg'f6 @ ') . 'K ]bX'LŁ

	T^{ à^¦ÁŠæà^	Öã^&cã}}	Tæ*}ãcå^ŽLĒĠá	Š[&aea[a]}ŽadĒĀá
F	T FÎ	Ý	<b>È</b> HÏ	Ě
G	T FÎ	Ý	ŒHÏ	Н
Н	T FÏ	Ý	ÈFÏ	Ě
1	T FÏ	Ý	ÈFÏ	ΪĚ
ĺ	T FÏ	Ý	<b>E</b> Î I	Н
Î	T FÏ	Ý	È I	Î

### A Ya VYf 'Dc]bh'@cUXg'f6 @7 '\* . 'K ]bX'k ]th '⇒M'`NL

	T^{ à^¦ÁSacà^	Öã^&cã}}	Tæ*}ãã å^ŽÊËcá	Š[&andai}ŽedŽáá
F	T FÎ	Z	ŒHÍ	Ě
G	T FÎ	Z	ŒHÍ	Н
Н	T FÏ	Z	ÈF	Ě
1	T FÏ	Z	ÈF	ΪĚ
ĺ	T FÏ	Z	<b>E</b> Î I	Н
Î	T FÏ	Z	<b>È</b> I I	ĵ

### A Ya VYf 'Dc]bh'@:UXg'f6 @ '+ . 'K]bX'NL

	T^{ à^¦ÁŠæà^	Öã^&cã[}	Tæ*}ããå^ŽÉËcá	Š[&anda[}ŽedĒĀá
F	T FÎ	Z	È€JG	Ě
G	T FÎ	Z	ÆJG	Н
Н	T FÏ	Z	ÈHGJ	Ě
1	T FÏ	Z	ÈHGJ	ΪĚ
ĺ	T FÏ	Z	È H	Н
Î	T FÏ	Z	ÆJH	Î

P: (203) 488-0580 F: (203) 488-8587

R[àÁÞ˚{à^¦ K GF€€ÍÈGG T[å^|ÁÞæ{ ^ KÔVPOÈH€Œ

### A Ya VYf 8 jgff jvi hYX @ UXg f6 @ ( . K jbX k jh \ \N LŁ

	T^{à^¦ÁŠæàà^	Öã^&cã[}	ÙcæbcÁTæ*}ããå^ŽiÐe£21Ê•-á	Ò}åÁTæ*;ãčå^ŽÐ棣£•~á	ÙœdoÁŠ[&ænā[}ŽedŽÃá	Ò}åÆq̃[&ææa[[}ŽedÉÃá
F	T FÎ	Ý	È€€H	È€H	€	€
G	T FÏ	Ý	È€EH	È€H	€	€
Н	Τĺ	Ý	È€€H	È€H	€	€
- 1	TI	Ý	È€H	Ì <b>€</b> €H	€	€
ĺ	ΤÏ	Ý	È€€H	È€H	€	€
Î	ΤÎ	Ý	È€EH	Ì <b>€</b> €H	€	€
Ï	TH	Ý	È€€H	Ì <b>€</b> €H	€	€
Ì	TG€	Ý	È€€H	Ì <b>€</b> €H	€	€
J	TŒ	Ý	È€EH	Ì <b>€</b> €H	€	€

### A Ya VYf'8 ]gff ]Vi hYX' @ UXg'f6 @7') '. 'K ]bX'LŁ

	T^{à^¦ÁŠæà^	Öã^&cã[}	ÙœaboÁTæ*}ããå^ŽiÐaBÊÆ€•~á	Ò}åÁTæt}ãčå^ŽÐdÊØÊ•-á	ÙceboÁŠ[&ænā[}ŽedŽāá	Ò}åÆŠ[&ææā[}Žæ£Ãá
F	T FÎ	Ý	Ì <b>E</b> €J	Ì <b>€</b> €J	€	€
G	T FÏ	Ý	Ì <b>E</b> €J	L€€J	€	€
Н	Τĺ	Ý	ÌŒ€J	L€€J	€	€
I	TI	Ý	È€J	Ì <b>€</b> €J	€	€
ĺ	ΤÏ	Ý	Ì <b>E</b> €J	Ì <b>€</b> €J	€	€
Î	ΤÎ	Ý	È€J	Ì€€J	€	€
Ϊ	TH	Ý	È€J	Ì <b>€</b> €J	€	€
Ì	TŒ	Ý	ÌŒ€J	Ì <b>€</b> €J	€	€
J	T GF	Ý	ÌŒ€J	Ì <b>€</b> €J	€	€

### A Ya VYf 8 JgHf JVi hYX @ UXg f6 @ \* . K JbX k Jh \ \=\W NL

	T^{à^¦ÆŠæà^	Öã^&dã}	ÙœaboÁTæ*}ããå^ŽiÐaBÊÆ€•~á	Ò}åÁTæt}ãčå^ŽÐdÊØÊ•~á	ÙcæloÁŠ[&ænā[}ŽedŽáá	Ò}åÆŠ[&ææā[}Žœ£Ãá
F	TG	Z	ÈE€H	Ì <b>E</b> €H	€	€
G	TF	Z	È€H	Ì <b>E</b> €H	€	€
Н	ΤÌ	Z	ÈE€H	Ì <b>E</b> €H	€	€
- 1	TI	Z	È€H	Ì <b>E</b> €H	€	€
ĺĺ	Τĺ	Z	ÌŒ€H	Ì <b>E</b> €H	€	€
Î	T FÍ	Z	È€H	Ì <b>€</b> €H	€	€
Ϊ	ΤÏ	Z	È€€H	Ì <b>€</b> €H	€	€
ì	ΤÎ	Z	È€H	Ì <b>€</b> €H	€	€
J	TFI	Z	È€EH	Ì <b>€</b> €H	€	€
F€	TJ	Z	È€H	Ì <b>€</b> €H	€	€
FF	T FG	Z	ÌŒ€H	Ì <b>E</b> €H	€	€
FG	T FH	Z	ÌŒ€H	Ì <b>E</b> €H	€	€
FH	TFF	Z	ÌŒ€H	Ì <b>E</b> €H	€	€
FI	TF€	Z	Ì <b>E</b> €H	Ì <b>E</b> €H	€	€
FÍ	TŒ	Z	Ì <b>E</b> €H	Ì <b>E</b> €H	€	€
FÎ	T GF	Z	ÈE€H	Ì <b>€</b> €H	€	€

### A Ya VYf 8 ]gff ]Vi hYX @ UXg f6 @ + . K ]bX NL

	T^{à^¦ÁŠæà^	Öã^&cã[}	Ù cæbcÁTæ*}ãã å^ŽiÐe£21Ê•-á	Ò}åÁTæ*;ãčå^ŽÐæÉÆ•~á	ÙcæloÁš[&ænā[}ŽedŽiá	Ò}åÆq̃[&ææa[[}Žæd£Ãá
F	TG	Z	ÈE€J	È€J	€	€
G	TF	Z	È€J	Ì <b>€</b> €J	€	€
Н	ΤÌ	Z	È€J	È€J	€	€
	TI	Z	È€J	Ì <b>E</b> €J	€	€
ĺ	Τĺ	Z	È€J	È€J	€	€
Î	T FÍ	Z	Ì <b>E</b> €J	È€J	€	€

K Ô^} c^\ ÁÒ} \* 3 ^^ \ 3 \* R[àÁÞ˚{à^¦ K CF€€ÍÈCG T[å^|ÁÞæ{^ KÔVPOÈH€Œ

Œ\*ÁFFÉÆG€GF IK€ÍÁÚT Ô@^&\^åÁÓ^KÁ/RŠ

 Centered on Solutions
 www.centekeng.com

 63-2 North Branford Road
 P: (203) 488-0580

 Branford, CT 06405
 F: (203) 488-8587

A Ya VYf 8 ]glf ]Vi hYX @ UXg f6 @ + . K ]bX NL f7 c bhjbi YXL

	T^{ à^¦ÆSæà^	Öã^&cã[}	ÙædoÁTæt*}ããå^ŽiÐeÂĐ•~á	Ò}åÁTæ≛}ãčå^ŽðÐæÊØÊ•~á	ÙcæboÁŠ[&ænā[}ŽedÉĀá	Ò}åÆŠ[&ææã[}ŽæÉÃá
Ϊ	ΤÏ	Z	ÈE€J	Ì <b>€</b> €J	€	€
Ì	ΤÎ	Z	È€J	È€J	€	€
J	TFI	Z	È€J	Ì <b>€</b> €J	€	€
F€	TJ	Z	È€J	Ì <b>€</b> €J	€	€
FF	TFG	Z	È€J	Ì <b>€</b> €J	€	€
FG	T FH	Z	Ì <b>E</b> €J	È€J	€	€
FH	TFF	Z	È€J	Ì <b>€</b> €J	€	€
FI	TF€	Z	È€J	Ì <b>€</b> €J	€	€
FÍ	TG€	Z	Ì <b>E</b> €J	Ì <b>€</b> €J	€	€
FÎ	TŒ	Z	Ì <b>E</b> €J	È€J	€	€

6 Ug]W @ UX 7 UgYg

	ÓŠÔÁÖ^∙&¦∄;æ[}	Ôæc^*[¦^	ÝÁÕ¦æçãc ŸÁÕ¦æ	acî ZÁŐ¦æqacî l	R⊞È Ú[ãjc	Öãrdãa řÉ	ÉDE^æÇTÉÉ	:Ù`¦æ&∧ <b>:</b> È
F	Ù^ -ÁY ^∄ @c	ÖŠ	Ë					
G	Ö^æåÆŠ[æå	þ[}^			Î			
Н	<b>(3</b> ,^ÁŠ[æå	Þ[}^			Î			
1	Yā¦åÁ,ãc@ÁQ3\^ÁÝ	Þ[}^			Î	J		
ĺ	Y a åÁÝ	Þ[}^			Î	J		
Î	Y āļåÁ,ãc@ <b>Á3</b> A^ÁZ	Þ[}^			Î	FÎ		
Ϊ	Y <sup>*</sup> ą, åÆ	Þ[}^			Î	FÎ		

@UX7ca V]bUh]cbg

Ö^•&¦ā;cā;} Ù[ ç^	ÚÖ^∣æ	e HEÓHEØæHEÓŠÔ	ØæHÓHOÆHÓH		
F FECOÁÉÁFE Y ÁZÝ É á A & CÁHÉ Y A		F FÈG G	FÈG Í FÉ		
G €DÖÆÆFERY ÁÇÝ ÉBÂN & CÂNEEÝ N. •		F 🖨 G	₿ĺFĒ		
H FÉGÖÆÆÆÆÆÆÆÆÆÆÆÆÆÆÆ		F FÈG G	FÈG H F I	F	
FESÖÆÆFE Y ÁZÆBAA^&æEY^•		F FÈG G	FÈG Ï FĒ		
Í €ÐÖÆÆÆÐ YÁZÆÃÃ^&æÐÝ^•	Ÿ	F 🖨 G	₿ÏFÊ		
Î FÊGÖÆÆÆÆÆÆÆÆÆÆÆ	Ÿ	F FÈG G	FÈG H F Î	F	

9bj YcdY'>c]bhFYUMJcbg

	Rją̃c		ÝÆŽá	ŠÔ	ŸÆXá	ŠÔ	ZÆŽá	ŠÔ	ΤΥΆΧΕ̈ά	ŠÔ	ΤΫ́ΑӁΕ̈́ά	ŠÔ	TZÁŽĞ-cá	šô
F	ÞĦ	{ æ¢	ËŒG	Î	ÈEGF	F	ÈÄG	1	€	Î	€	Î	€	Î
G		{ <b>ā</b> }	Ë€IÌ	G	ÈEFÎ	ĺ	⊞ïlì	F	€	F	€	F	€	F
Н	ÞĞ	{ æ¢	È€HÏ		FÈÈÎ	Î	ÈF	G	€	Î	€	Î	€	Î
- 1		{ <b>ā</b> }	⊞FÏ	G	ÈÌÎ	G	ËŒĬIJ	1	€	F	€	F	€	F
ĺ	ÞĠ	{ æ¢	Ï€JÏ	Î	ÈΙÍ	Н	FË€G	Н	€	Î	€	Î	€	Î
Î		{ <b>ā</b> }	⊞€	F	ÈÍF	ĺ	ËFÌ	ĺ	€	F	€	F	€	F
Ϊ	V[œ <b>∲</b> K	{ æ¢	€	Î	FÈÍJ	Î	€	F						
Ì		{ <b>ā</b>	ËÈĤÍ	F	Ě۱	G	ËŒÎIÍ	1						

9bj YcdY'>c]bh8]gd`UWYa Ybhg

	R[ã]c		ÝÆŽjá	ŠÔ	ΫÃÃγá	ŠÔ	ZÆŽajá	ŠÔ	ÝÁÜ[cægā]}ÁÄEEŠĈ	ŸÁÜ[cæcā[}ÁZEEŠÔ	ZÁÜ[cægā]}ÁŽEEŠÔ
F	ÞF	{ æ¢	ÈÌÍ	F	ËŒH	Н	Èίί	ĺ	FÐÍÏ^Ħ H	ÌĐÏÏ^ËH F	FÈI H' ËH H
G		{ <b>ā</b>	ŒJÌ	ĺĺ	⊞€H		⊞EÌ	F		ËËÎÍ^ËG Í	ËËÍJ^Ë Í
Н	ÞG	{ æ¢	ÈÌÍ	F	Ë€IÏ	J	ÈHFÎ	1	ÎËĕÖ∧ËH∫Í	FĚ FÏ ^ËG I	GËJ^ËH H

Ô[{]æ}^ Ö^• ã} ^¦

K Ô^} c^\ ÁÒ} \* ã^^ ¦ã \* K ØRÚ

R[àÁÞ\*{à^¦ T[å^|ÁÞæ{^ K ŒŒÍÈGG KÔVPOÈH€Œ

Œ\*ÁFFÉÆGEGF I K€Í ÁÚT Ô@^&\^åÁÓ^KÁ/RŠ

## 9bj YcdY'>c]bh8]gd`UWYa Ybhg`fl7cbh]bi YXŁ

	R[ã]c		ÝÆŽjá	ŠÔ	ŸÆĄjá	ŠÔ	ZÃŽajá	· ŠÔÝÁÜ[œenā]}ÁPÉEŠÔŸÁÜ[œenā]}ÁPÉEŠÔZÁÜ[œenā]}ÁPÉEŠÔ
	-	{ <b>a</b>	⊞ĴÎ	ĺĺ	⊞JÍ	Н	ËEGÏ	G É ÉHÍ Î A ËH F É É Ì GA ËH G FE JGA Ë I
ĺ	ÞH	{ æ¢	ÈÌÍ	F	Ë≘î	ĺ	ÈΘΪ	I ÎËËÄÄËHÍ FËFÄÄËG I QËÌJAËH H
Î		{ <b>a</b>	⊞ĴÎ	ĺ	⊞ì H	Н	ËE€G	GÉHÍÎ^H FÉÈÌG^H GFÈÌJ^Ë Í
Ϊ	ÞI	{ æ¢	ÈÌÍ	F	⊞€EÌ	Н	Èì	Í FÐÍÏ^Ë HÌÐÏÏ^Ë F FÈIHÆH H
ì		{ <b>a</b>	ŒIJÌ	ĺĺ	ËEGÌ		ËΪÎΪ	F EGÈFHYEH Í EFÈÍÍ/EG Í EIÈÍÍ/E Í
J	ÞÍ	{ æ¢	<u>È</u> ( ì	G	⊞€€I	Н	<u> </u>	Í GÀUGNÉH I JÉGÍNÉH F FÉGGNÉH H
F€		{ <b>ā</b>	iii) i	Ī	ËΞΗ	ĺ	⊞ÎG	F FÌHIÎ^ËH G ËFÊJF^ËG Í ËIÊ€G^Ë Í
FF	ÞÎ	{ æ¢	<u>È</u> ÍÌ	G	<u>⊞</u> e î	Τί	ĚÎÏ	I Ì È JHYËH Í FÈ FÏ YËG I QË GHYËH H
FG		{ <b>a</b>	<u></u>	Ī	<u>⊞</u> JI	Н	⊞JÏ	G É ÉHÍ JA ÉH F É ÉÍ HA ÉH G Ï È G A É Í
FH	ÞÏ	{ æ¢	<u>Ē</u> (ì	G	<u>⊞</u> aî	Τί	<u>È</u> ÌÍ	I ÌÈJHYËH Í FÈFÎYËG I QËGHYËH H
FI		{ <b>a</b>	<u> </u>	Ĭ	<u>⊞</u> i H	H	⊞i F	G É ÉÍ J^Ë F É ÉÍ HYËH G Ë È^É Í
FÍ	ÞÌ	{ æ¢	<u>È</u> (ì	G	Œ€ì	Н	Èïì	Í GÀUGNÊH I JEÉIÍNÉH F FEEGGNÉH H
FÎ	- F 1	{ <b>a</b>	i i	Ĭ	⊞EGÌ	ΙΉ	⊞ĞF	F FEHÎ^EH G EFÊJ^EG Í ELÊJJ^E Í
FΪ	ÞJ	{ æ¢	<u>E</u> EFÏ	F	<u> </u>	T i	<u> </u>	I ÎËËAËH Í FĚFÏAËG I GÈÊAËH H
FÌ		{ <b>ā</b>	<u>⊞</u> JI	ĺ	H H	Н	EJG	G É ÉHÍ Î ^ ËH F É É Ì G Č FÈ Ì J ^ Ë Í
FJ	ÞF€	{ æ¢	<u>ш</u> јі	G	<u>⊞</u>	T i	ĒĞ	
G€	PIE	{ <b>ā</b>	<u>⊞</u> JÍ	l l	H H	Н	<u>⊞G</u> i	F ÉÉIME F ÉÉIME G ÉÉJMÉ G
GF	ÞFF		<u>ш</u> л	î		î	€	Î GEÎHYÊH Î ÎÊÎÎAÊH G ÎÊHÎAÊH H
Œ	PFF	{ æ¢	€	F	€	F	€	F FÈEJ^ËH G ËFĚFÌ^ËH I FËFH^ËH Í
GH	ÞFG		<u> </u>	F	<u>       €                             </u>	Н	<u>E</u> ï G	F Ë E E E
G	PFG	{ æ¢	<u> </u>	Í	<u>⊞€</u> €Í		ETG-	Í ËFĚIHYËH FËHËHJYË G QËÍÎYË Í
GÍ	ÞFH		<u>ШЭІ</u> ÈÍÏ	G	<u>E</u> FG	Н	ÈG	G HÈ GF^ËH Í Í BEJG^ËH I GREJÌ^ËH H
GÎ	РГП	{ æ¢	<u> </u>	G	<u>ŒFG</u>		<u> </u>	I ËËHAË FËËGAË GIË AË Í
	ьп	{ <b>ā</b>	<u>E</u> ÌÍ	F	<u>⊞€</u> EÏ	+	EGFI	/ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
Ğ	ÞFI	{ æ¢		F	<u>⊞e</u> lí		<u> </u>	
GÌ		{ <b>a</b>	<u>⊞</u> JÌ ÈÍÌ	+ -	<u>=====</u> ==============================	H		
GJ	ÞFÍ	{ æ¢		G	<u>⊞</u> ∃		<u> </u>	
H€	ÞFÎ	{ <b>ā</b>	<u>#</u>	Î	<u>====</u> 1	H		G   FREJONËH   G   ËFREJONËG     ËFREJONË     F   I E G NË   F   F   FREJONË   F   FREJONË   F   FREJONË   FREJONE   FREJONE
HF	PFI	{ æ¢	€	F	<u>⊞€</u> €H	F	<u>EGG</u> EE€Í	
HG		{ <b>a</b>	€	Î		T T	€	
HH	ÞFÏ	{ æ¢			<u>È</u> FF	1		
H		{ <b>a</b>	€	F	<u>⊞EEG</u>	G F	EEÍ H ÈEÍ	
HÍ	ÞFÌ	{ æ¢	€		<u>Ì</u> E€H	Ť	EEGG	Í Í ÉGG-NÉIF HÉHÍNÉH FILÉGÍNÉIF FÉHÁFÍNA Í FIFIÍNA HI Í FEHAN ÁH Í
HÎ	LF:	{ <b>a</b>		F	ËE€J			
HÏ	ÞFJ	{ æ¢	€	+-	È€G	G	<u>È</u> H	
HÌ	- CC	{ <b>a</b> }	€ <del>È</del> (ï	F	<del>É</del> FF		€ ÌCCI	
HJ	ÞŒ	{ æ¢	ÈÍÏ	G		G	<u>IE</u> €J	
l€	<b>-</b>	{ <b>a</b>	iii) í	+	EEÉ H		ŒŒÌ Èï F	
I F	ÞŒ	{ æ¢		F	<u>Æ</u> FÏ	H	<u>Ē</u> ĪF	
IG	<u> </u>	{ <b>a</b>	<u>∰</u> JÏ		<u>⊞eel</u>			
IH	ÞŒ	{ æ¢	<u>È</u> ÍÏ	G	<u>É</u> FÏ	Н	ĖHÌ	
	L 0.1	{ <b>a</b>	<u> </u>	+	<u>∰€€</u> I	<del>                                     </del>	<u>⊞G€Î</u>	
11	ÞGH	{ æ¢	<u>Ē</u> IJÏ	F	ËE€Ï	1 1	<u> </u>	Í FÈIGHA H JÈIÌA H F Í ÐÏA H F
11		{ <b>a</b> }	ŒŒÍ		<u>⊞</u> eí G	H		
ΙΪ	₽Ġ	{ æ¢	<u>Ė</u> Į	G	ŒŒ		<u> </u>	
l Ì		{ <b>a</b> }			⊞EÉÉ G	Н	<u>⊞€</u> HH	
IJ	ÞĠ	{ æ¢	<u>Ē</u>	G	ÈF	Н	<u>Ē</u>	F FEIGH Í Í LÍNH G Ï EÍNE F
Í€		{ <b>a</b> }	<u>⊞a</u> j		€	Ļ	∰FH → /	
ÍF	ÞĜ	{ æ¢	<u>E</u> ÎÎ	F	Œ€Î		<u>ÈH</u>	Í FÈHH-MËH H ÏËHÌGMËH F FÈÈFJMË F
ÍG		{ <b>ā</b>	⊞EH		ËEGÎ	H	<u> </u>	
ÍΗ	ÞĞ	{ æ¢	€		€		€	Î ÎÈ Î I A Î Î Î Î Î Î Î Î Î Î Î Î Î Î Î Î Î
İ		{ <b>ā</b>	€	F	€	F	€	F EGEGI A G E E E CHA H I E E FIA H I
ĺĺĺ	ÞĠ	{ æ¢	€		€		€	<u>Î   ÎESGHYE   F   HEHÎYEH   F   ÎEĞYE   F</u>

 Centered on Solutions
 www.centekeng.com

 63-2 North Branford Road
 P: (203) 488-0580

 Branford, CT 06405
 F: (203) 488-8587

Ô[{]æ}^ K Ô^} c^\ ÁÒ} \* 3 ^^ \ 3 \* Ö^• ã} ^¦ K ØRÚ R[àÁÞ\*{à^¦ T[å^|ÁÞæ{^ K GF€€ÍÈGG KÔVPOÈH€Œ

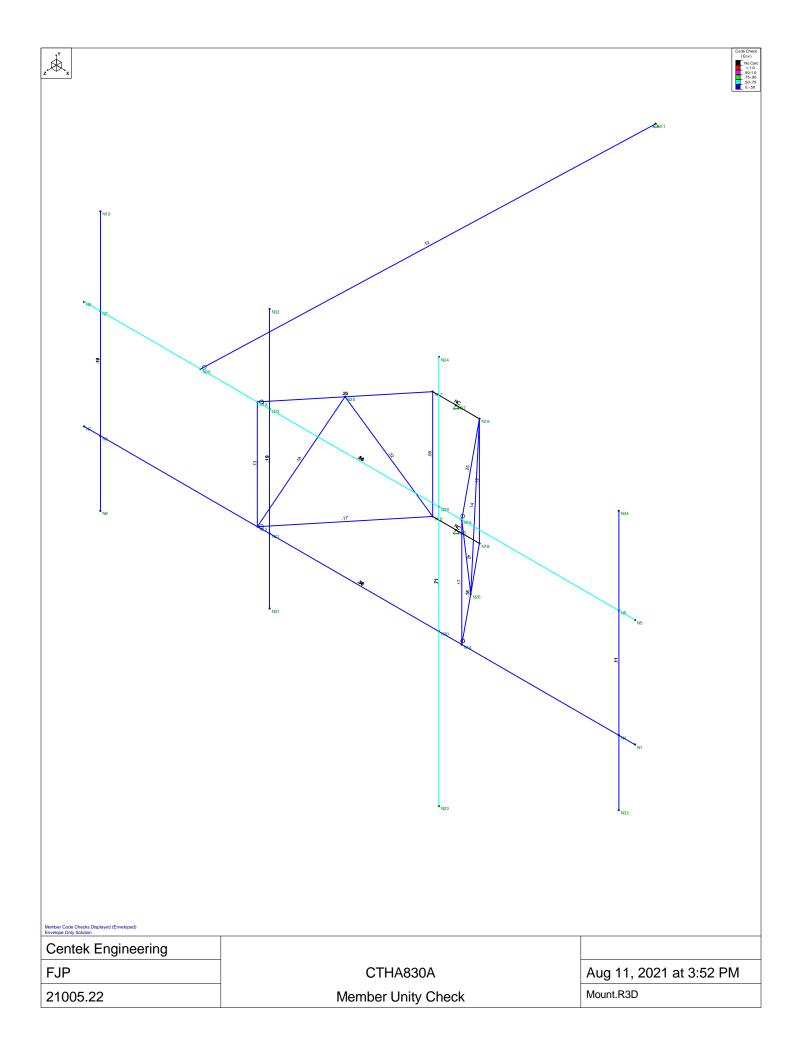
Œ\*ÁFFÉÆG€GF IK€ÍÁÚT Ô@^&\^åÁÓ^KÁ/RŠ

### 9bj YcdY'>c]bh8]gd`UWYa Ybhg'fl'cbhjbi YXŁ

	R[ã]c		ÝÆŽjá	ŠÔ	ΫÆğjá	ŠÔ	Z <b>ÁŽ</b> ajá	ŠÔ	ÝÁÜ[cægā[}ÁÄEEŠÔ	ŸÁÜ[cæcā[}ÁZEEŠÔ	ZÁÜ[cægā]}ÁZEEŠÔ
ÍÎ	-	{ <b>a</b>	€	F	€	F	€	F	ËHÈÉÍI^Ë Í	E E IÍAEH Í	ËËG^Ë Î
ÍΪ	ÞGJ	{ æ¢	ÈĺÌ	G	ËŒΕΪ	ĺ	ÈĠ	1	JÈÍI^ËH I	ÌÈÌÍ^ËH G	
ĺÌ		{ <b>ā</b>	ËÌΪ	1	⊞ÉÍF	Н	⊞eïG	G	FÈEÏ HY ËH G	ËËHË	ËÈH^Ë G
ĺJ	ÞH€	{ æ¢	ÈÌÍ	F	ËŒΕΪ	ĺ	ÈΗÌ	ĺ	FÈHJ^ËH H	JÈIÌ^ËH F	FÈ€Í^ËH F
΀		{ <b>ā</b>	ŒIJÌ	ĺĺ	⊞ÉÍF	Н	⊞FI	F	ÜÈÌI^# Í	ËË Ë ČË Š	ËÈ CG^Ë Í
ÎF	ÞÆ	{ æ¢	ÈΕJÍ	F	È€FÏ	Н	ÈΊΙ	F	##FF^# Í	FÈÏHYËH Î	ÌÈEG∿Ë⊟H
ÎG		{ <b>ā</b>	ŒIJÏ	ĺĺ	ËŒ	1	⊞JÎ	ĺ	EE EE I ^EH H	IËIÌ^Ë G	
ÎΗ	ÞHG	{ æ¢	ÈΕΙÎ	G	È€FÏ	Н	ÈF	G	HÈGHÌ ^ËH   Í	HÈHI^ËH I	FÈFI ^ËH H
Îl		{ <b>a</b>	∰JF		ËŒ	1	ËHF		ËË E Î I ^ËH F	ËŒÉÍJ^ËH G	
ÎÍ	ÞН	{ æ¢	È	F	⊞€EÌ	Н	ÐЭН	ĺ	FÐÍÏ^⊞ H	ÌÙÏÏ^⊞ F	FÈÎ^ËH H
ÎÎ		{ <b>a</b>	⊞G€Î	ĺĺ	ËEGÌ	1	⊞ĭJÍ	F	ESÈUHY EH Í	ËËÎÍ^ËG Í	H H Í Í Í
ÎΪ	ÞH	{ æ¢	ÈΙJ	G	Œ€Ì	Н	ÈΗÌ		GĚÌ HY ËH I	JÈEÏÍ∧ËH F	JÈHYË H
ÎÌ		{ <b>a</b>	ŒΪÌ	I	⊞€GJ	I	曲ìì	G	FÈHÎ^ËH G	ËË J^ËG Í	Ë Ě JJ^Ë Í

### 9bj YcdY5=G7 % h fl \*\$!%\$L @F: 8 GhYY 7cXY7\ YWg

	T∧ <b>⊞</b> Ù@ <b>d</b>	BÖ[å^ÁÔ⊞	ÈŠĮÈÈ	ŠÔ	Ù@æ#£Šį&#</th><th>ŠÔ</th><th>]@aEÚ}&-AXáá</th><th>]@aEÚ}oÁŽá</th><th>]@aET}ÁÈÈ</th><th>Èj@aET}ÈÈ</th><th>ÈÔà</th><th>Ò~}</th></tr><tr><td>F</td><td>TFÚÓÚÉ</td><td>ĖĤI</td><td>IÈ</td><td>ĺ</td><td>ÈÌ€ÌĒŒ</td><td></td><td>FI ÈĞ Ï</td><td>HŒH</td><td>FÈÏG</td><td>FÈÏG</td><td>GĚÏÌ</td><td>PFЁà</td></tr><tr><td>G</td><td>TGÚŒ</td><td>ÈĚÎF</td><td>曲曲</td><td>1</td><td>ÈGFG Ì Ē ÈÈ</td><td></td><td>GIÈFÍ</td><td>HŒH</td><td>FÈÏG</td><td>FÈÏG</td><td>ŒÌ</td><td>PFËrà</td></tr><tr><td>Н</td><td>THÚÓ</td><td></td><td>ÍÈ€ÈÈÈ</td><td>F</td><td>È€ÈÌ €</td><td>F</td><td>JÈÌF</td><td>HŒH</td><td>FÈÏG</td><td>FÈÏG</td><td>FÈFHÎ</td><td>PFËrà</td></tr><tr><td>1</td><td>TI ÚŒ</td><td>Ė</td><td>ŒÌ Ì</td><td>G</td><td>ÈEÎ   GEÌÌ</td><td>Н</td><td>FJÈ⊟I</td><td>FJËÌÌ</td><td>È€F</td><td>È€F</td><td>FÀJJ</td><td>PFËrà</td></tr><tr><td>ĺ</td><td>TÍ ÚŒÜÈ</td><td>ÈËF</td><td>ŒÌ Ì</td><td>F</td><td>ÈE Ì ŒÈÌ</td><td>Н</td><td>fi ÈgHi</td><td>FJËÌÌ</td><td>È€F</td><td>È€F</td><td>FĚ G</td><td>PFËrà</td></tr><tr><td>Î</td><td>TÎ ÚŒÜË</td><td>-</td><td>ŒÎ Ì</td><td>F</td><td>È FÈ I</td><td>ĺ</td><td>FJÈ⊟I</td><td>FJËÌÌ</td><td>È€F</td><td>È€F</td><td>G<u>Ì</u>UÏ</td><td>PFËrà</td></tr><tr><td>Ϊ</td><td>TÏ ÚŒÛË</td><td>É</td><td>ŒÌÌ</td><td>G</td><td>ÈEÌ ŒÈÌ</td><td></td><td>fi ÈgHi</td><td>FJË Ì Ì</td><td>È€F</td><td>È€F</td><td>FËÌG</td><td>PFËrà</td></tr><tr><td>Ì</td><td>TÌ ∰ Ĥ</td><td>-</td><td>€</td><td>1</td><td>ÈEGÎ €</td><td>F</td><td>ΙĖÜÌ</td><td>JÈI</td><td>È€</td><td>È€l</td><td>ŒĜ</td><td>PFËrà</td></tr><tr><td>J</td><td>TJ∉∄⊞</td><td></td><td>€</td><td></td><td>ÈE€ÎGĚ</td><td>Î</td><td>ΙĖΗΪÌ</td><td>JÈI</td><td>È€I</td><td>È€l</td><td>GÉGÍ H</td><td>PFËrà</td></tr><tr><td>F€</td><td>TF€ŒÎ⊞</td><td>Ġ</td><td>€</td><td>1</td><td>ÈEIG €</td><td></td><td>HÈHF</td><td>JÈI</td><td>È€</td><td>È€l</td><td>GĚJH</td><td>PFËrà</td></tr><tr><td>FF</td><td>T FF €Î Ĥ</td><td></td><td>OHÌ Ì⊞È</td><td>Н</td><td>È€FÌ €</td><td>G</td><td>HÈHF</td><td>JÈI</td><td>È€I</td><td>È€l</td><td>GË FF</td><td>PFËæ</td></tr><tr><td>FG</td><td>TFG€ĒÈ</td><td></td><td>ŒÎ ŒË</td><td>1</td><td>ÈEHG €</td><td>F</td><td>HÈHF</td><td>JÈI</td><td>È€</td><td>È€l</td><td>GÈÍJ</td><td>PFËrà</td></tr><tr><td>FH</td><td>TFH€ĒÈ</td><td>ÈĠ</td><td>OÈ È</td><td>Î</td><td>ÈEEÌ GÈÈÈÈ</td><td></td><td>HÈHF</td><td>JÈI</td><td>È€I</td><td>È€l</td><td>GËÍG</td><td>PFËæ</td></tr><tr><td>FI</td><td>TFI €ĒĖ</td><td></td><td>€</td><td>1</td><td>ÈEGF €</td><td>Н</td><td>l ÈHÏ Ì</td><td>JÈI</td><td>È€</td><td>È€l</td><td>GÈGÎÍ</td><td>PFËrà</td></tr><tr><td>FÍ</td><td>TFÍ €Ë ÈÈ</td><td>EJI</td><td>€</td><td></td><td>ÈEGF €</td><td>Н</td><td>I ÈHÏ Ì</td><td>JÈI</td><td>È€I</td><td>È€l</td><td>GÉGÍÍ</td><td>PFËFà</td></tr><tr><td>FÎ</td><td>T FÎ ÚŒÛ</td><td>ÈÈÌÎ</td><td>ΙĚ</td><td>Î</td><td>È Ï HÈ ÈÈ</td><td>I</td><td>G<del>-È</del>ÈÌÌ</td><td>HŒH</td><td>FÈÏG</td><td>FÈÏG</td><td>GÈ€ÈÌ</td><td>PFËrà</td></tr><tr><td>FΪ</td><td>TFÏ ÚŒÛĖĖ</td><td>ÈËEÌ</td><td>Н</td><td></td><td>È E I E I E E</td><td>ĺ</td><td>FJÈJÎ I</td><td>HŒH</td><td>FÈÏG</td><td>FÈÏG</td><td>ĺ</td><td>PFËrà</td></tr><tr><td>FÌ</td><td>T G€ ÚÓÚÈ</td><td>ĖĖ</td><td>G</td><td>I</td><td>ÈÈÌÎ G</td><td>F</td><td>GÎÈŒŰ</td><td>HŒH</td><td>FÈÏG</td><td>FÈÏG</td><td>ĺ</td><td>PFËrà</td></tr><tr><td>FJ</td><td>T GF ÚÓÚÉ</td><td>ÈÈ€Í</td><td>G</td><td>ĺ</td><td>È€J G</td><td>ĺ</td><td>GÎÈŒÍ</td><td>HŒH</td><td>FÈÏG</td><td>FÈÏG</td><td>GÈ€I</td><td>PFËà</td></tr></tbody></table>
--	-------------------------	----------	-------	----	---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------



**RAN Template:** A&L Template: 67E5A998E 6160 67E5998E\_1xAIR+1OP

CTHA830A\_Sprint Retain\_1\_draft

Print Name: Standard (2) PORs: New Build\_Sprint Keep

Section 1 - Site Information

Site ID: CTHA830A Status: Draft

Version: 1
Project Type: Sprint Retain
Approved: Not Approved Approved By: Not Approved Last Modified: 7/9/2021 4:16:47 PM

**RAN Template:** 67E5A998E 6160

Last Modified By: Michael.Low1@T-Mobile.com

Site Name: CTHA830A Site Class: Monopole Site Type: Structure Non Building
Plan Year: 2021
Market: CONNECTICUT CT
Vendor: Ericsson
Landlord: Not Specified

Latitude: 41.99961388 Longitude: -72.35560000
Address: 157 Hampden Rd
City, State: Stafford Springs, CT
Region: NORTHEAST

AL Template: 67E5998E\_1xAIR+1OP

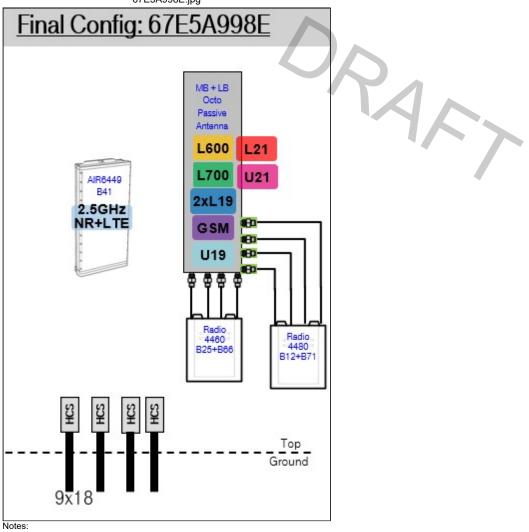
Sector Count: 3 Antenna Count: 6 Coax Line Count: 0 TMA Count: 0 RRU Count: 6

### Section 2 - Existing Template Images

---- This section is intentionally blank. ----

### Section 3 - Proposed Template Images

67E5A998E.jpg



### Section 4 - Siteplan Images

----- This section is intentionally blank. -----



**RAN Template:** 67E5A998E 6160 **A&L Template:** 67E5998E\_1xAIR+1OP

### CTHA830A\_Sprint Retain\_1\_draft

Print Name: Standard (2) PORs: New Build\_Sprint Keep

### Section 5 - RAN Equipment

### **Existing RAN Equipment**

---- This section is intentionally blank. ----

	Proposed RAN Equipment								
	Template: 67E5A998E 6160								
Enclosure	1	2	3						
Enclosure Type	Enclosure 6160	RBS 6601	B160						
Baseband	BB 6648 L700 L600 N600  BB 6648 L2500 N2500  BB 6648 L2100 L1900	DUG20 (G1900)							
Transport System	CSR IXRe V2 (Gen2)								
Functionality Groups	Ericsson Hybrid Trunk 6/24 4AWG *Select Length* (x 3)								

#### **RAN Scope of Work:**

CT33XC553
Existing & planned azimuth: 0 / 120 / 240
Existing 200A service
SA @ 66%

Antenna - omni to be researched - Fire Dept possible

Generator needed - space is available

**RAN Template:** 67E5A998E 6160 **A&L Template:** 67E5998E\_1xAIR+1OP

### CTHA830A\_Sprint Retain\_1\_draft

Print Name: Standard (2)
PORs: New Build\_Sprint Keep

### Section 6 - A&L Equipment

Existing Template: Custom
Proposed Template: 67E5998E\_1xAIR+10P

Sector 1 (Proposed) view from behind								
Coverage Type	A - Outdoor Macro							
Antenna		1			2			
Antenna Model	RFS - APXVAALL	24_43-U-NA20 (Octo			Ericsson - AIR6449 B41 (Active Anteni	na - Massive MIMO)		
Azimuth	0				0			
M. Tilt	0				0			
Height	171				171			
Ports	P1	P2	Р3	P4	P5	P6		
Active Tech.	L700 L600 N600	L700 L600 N600	(L2100) (L1900) (G1900)	L2100 L1900 G1900	(L2500) (N2500)	L2500 N2500		
Dark Tech.								
Restricted Tech.								
Decomm. Tech.								
E. Tilt	2	2	2	2	2	2		
Cables	Coax Jumper (x2)	Coax Jumper (x2)	Coax Jumper (x2)	Coax Jumper (x2)				
TMAs								
Diplexers / Combiners								
Radio	Radio 4480 B71+B85 (At Antenna)	SHARED Radio 4480 B71+B85 (At Antenna)	Radio 4460 B25+B66 (At Antenna)	SHARED Radio 4460 B25+B66 (At Antenna)				
Sector Equipment								
Unconnected Equipment: Scope of Work:								
*A dashed border indicates shared equipment. Any connected equipment is denoted with the SHARED keyword.								

 RAN Template:
 A&L Template:

 67E5A998E 6160
 67E5998E\_1xAIR+1OP

### CTHA830A\_Sprint Retain\_1\_draft

Print Name: Standard (2)
PORs: New Build\_Sprint Keep

			Sector 2 (Pro	oposed) view fr	om behind			
Coverage Type	A - Outdoor Macro							
Antenna		1			2			
Antenna Model	RFS - APXVAALL	24_43-U-NA20 (Octo			Ericsson - AIR6449 B41 (Active Anteni	na - Massive MIMO)		
Azimuth	120				120			
M. Tilt	0				0			
Height	171				171			
Ports	P1	P2	P3	P4	P5	P6		
Active Tech.	L700 (L600) N600	L700 L600 N600	(L2100) (L1900) (G1900)	L2100 L1900 G1900	L2500 N2500	L2500 (N2500)		
Dark Tech.								
Restricted Tech.								
Decomm. Tech.								
E. Tilt	2	2	2	2	2	2		
Cables	Coax Jumper (x2)	Coax Jumper (x2)	Coax Jumper (x2)	Coax Jumper (x2)				
TMAs								
Diplexers / Combiners								
Radio	Radio 4480 B71+B85 (At Antenna)	SHARED Radio 4480 B71+B85 (At Antenna)	Radio 4460 B25+B66 (At Antenna)	SHARED Radio 4460 B25+B66 (At Antenna)				
Sector Equipment								
Unconnected Equip	Unconnected Equipment:							
Scope of Work:								
*A dashad hardar ind								

**RAN Template:** 67E5A998E 6160 **A&L Template:** 67E5998E\_1xAIR+1OP

### CTHA830A\_Sprint Retain\_1\_draft

Print Name: Standard (2)
PORs: New Build\_Sprint Keep

Sector 3 (Proposed) view from behind								
Coverage Type	A - Outdoor Macro							
Antenna		1			2			
Antenna Model	RFS - APXVAALL	24_43-U-NA20 (Octo			(Ericsson - AIR6449 B41 (Active Antenna - Massive MIMO))			
Azimuth	240				240			
M. Tilt	0				0			
Height	171				171			
Ports	P1	P2	P3	P4	P5	P6		
Active Tech.	L700 (L600) N600	L700 L600 N600	(L2100) (L1900) (G1900)	(L2100) (L1900) (G1900)	(L2500) (N2500)	L2500 N2500		
Dark Tech.								
Restricted Tech.								
Decomm. Tech.								
E. Tilt	2	2	2	2	2	2		
Cables	Coax Jumper (x2)	Coax Jumper (x2)	Coax Jumper (x2)	Coax Jumper (x2)				
TMAs								
Diplexers / Combiners								
Radio	Radio 4480 B71+B85 (At Antenna)	SHARED Radio 4480 B71+B85 (At Antenna)	Radio 4460 B25+B66 (At Antenna)	SHARED Radio 4460 B25+B66 (At Antenna)				
Sector Equipment								
Unconnected Equipment:								
Scope of Work:								
*A dashed border indicates shared equipment. Any connected equipment is denoted with the SHARED keyword.								

**RAN Template:** 67E5A998E 6160 **A&L Template:** 67E5998E\_1xAIR+1OP

### CTHA830A\_Sprint Retain\_1\_draft

Print Name: Standard (2)

		PORs: New Build_Sprint Keep				
	Section 7 - Power Systems Ed	quipment				
	Existing Power Systems Equi	pment				
	This section is intentionally blank					
	Proposed Power Systems Equ	ipment				
Enclosure	1					
Enclosure Type	Enclosure 6160					



# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CTHA830A

157 Hampden Road Stafford Springs, Connecticut 06076

October 18, 2021

EBI Project Number: 6221006192

Site Compliance Summary						
Compliance Status:	COMPLIANT					
Site total MPE% of FCC general population allowable limit:	7.92%					



October 18, 2021

T-Mobile
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, Connecticut 06002

Emissions Analysis for Site: CTHA830A

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **157 Hampden Road** in **Stafford Springs, Connecticut** for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu$ W/cm²). The number of  $\mu$ W/cm² calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu$ W/cm²). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately 400  $\mu$ W/cm² and 467  $\mu$ W/cm², respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 11 GHz frequency bands is 1000  $\mu$ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

### **CALCULATIONS**

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 157 Hampden Road in Stafford Springs, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6-foot person standing at the base of the tower. For power density calculations, the broadcast footprint of the AIR6449 antenna has been considered. Due to the beamforming nature of this antenna, the actual beam locations vary depending on demand and are narrow in nature. Using the broadcast footprint accounts for the potential location of beams at any given time.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 LTE channels (600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) I NR channel (600 MHz Band) was considered for each sector of the proposed installation. This Channel has a transmit power of 80 Watts.
- 3) 2 LTE channels (700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 4) 4 GSM channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 5) 2 LTE channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.



- 6) 2 LTE channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 7) I LTE Traffic channel (LTE IC and 2C BRS Band 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of 60 Watts.
- 8) I LTE Broadcast channel (LTE IC and 2C BRS Band 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of 20 Watts.
- 9) I NR Traffic channel (BRS Band 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of I20 Watts.
- 10) I NR Broadcast channel (BRS Band 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of 40 Watts.
- 11) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 12) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 13) The antennas used in this modeling are the RFS APXVAALL24\_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz / 2500 MHz / 2500 MHz channel(s) in Sector A, the RFS APXVAALL24\_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz / 2500 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 1900 MHz / 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz / 1900 MHz / 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz / 2500 MHz / 2500 MHz channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied



specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

- 14) The antenna mounting height centerline of the proposed antennas is 171 feet above ground level (AGL).
- 15) Emissions from additional carriers were not included because emissions data for the site location are not available.
- 16) All calculations were done with respect to uncontrolled / general population threshold limits.



### **T-Mobile Site Inventory and Power Data**

Sector:	Α	Sector:	В	Sector:	С
Antenna #:	I	Antenna #:	I	Antenna #:	I
Make / Model:	RFS APXVAALL24_43- U-NA20	Make / Model:	RFS APXVAALL24_43- U-NA20	Make / Model:	RFS APXVAALL24_43- U-NA20
Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz	Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz	Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz
Gain:	12.95 dBd / 12.95 dBd / 13.65 dBd / 15.45 dBd / 15.45 dBd / 16.45 dBd	Gain:	12.95 dBd / 12.95 dBd / 13.65 dBd / 15.45 dBd / 15.45 dBd / 16.45 dBd	Gain:	12.95 dBd / 12.95 dBd / 13.65 dBd / 15.45 dBd / 15.45 dBd / 16.45 dBd
Height (AGL):	171 feet	Height (AGL):	I7I feet	Height (AGL):	171 feet
Channel Count:	13	Channel Count:	13	Channel Count:	13
Total TX Power (W):	560 Watts	Total TX Power (W):	560 Watts	Total TX Power (W):	560 Watts
ERP (W):	17,868.72	ERP (W):	17,868.72	ERP (W):	17,868.72
Antenna A1 MPE %:	3.12%	Antenna B1 MPE %:	3.12%	Antenna C1 MPE %:	3.12%
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	Ericsson AIR 6449	Make / Model:	Ericsson AIR 6449	Make / Model:	Ericsson AIR 6449
Frequency Bands:	2500 MHz / 2500 MHz / 2500 MHz / 2500 MHz	Frequency Bands:	2500 MHz / 2500 MHz / 2500 MHz / 2500 MHz	Frequency Bands:	2500 MHz / 2500 MHz / 2500 MHz / 2500 MHz
Gain:	22.65 dBd / 17.3 dBd / 22.65 dBd / 17.3 dBd	Gain:	22.65 dBd / 17.3 dBd / 22.65 dBd / 17.3 dBd	Gain:	22.65 dBd / 17.3 dBd / 22.65 dBd / 17.3 dBd
Height (AGL):	171 feet	Height (AGL):	171 feet	Height (AGL):	I7I feet
Channel Count:	4	Channel Count:	4	Channel Count:	4
Total TX Power (W):	240 Watts	Total TX Power (W):	240 Watts	Total TX Power (W):	240 Watts
ERP (W):	36,356.09	ERP (W):	36,356.09	ERP (W):	36,356.09
Antenna A2 MPE %:	4.80%	Antenna B2 MPE %:	4.80%	Antenna C2 MPE %:	4.80%

#### environmental | engineering | due diligence

Site Composite MPE %		
Carrier	MPE %	
T-Mobile (Max at Sector A):	7.92%	
no additional carriers	N/A	
Site Total MPE %:	7.92%	

T-Mobile MPE % Per Sector			
T-Mobile Sector A Total:	7.92%		
T-Mobile Sector B Total:	7.92%		
T-Mobile Sector C Total:	7.92%		
Site Total MPE % :	7.92%		

T-Mobile Maximum MPE Power Values (Sector A)							
T-Mobile Frequency Band / Technology (Sector A)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (µW/cm²)	Frequency (MHz)	Allowable MPE (μW/cm²)	Calculated % MPE
T-Mobile 600 MHz LTE	2	591.73	171.0	1.56	600 MHz LTE	400	0.39%
T-Mobile 600 MHz NR	I	1577.94	171.0	2.08	600 MHz NR	400	0.52%
T-Mobile 700 MHz LTE	2	695.22	171.0	1.84	700 MHz LTE	467	0.39%
T-Mobile 1900 MHz GSM	4	1052.26	171.0	5.56	1900 MHz GSM	1000	0.56%
T-Mobile 1900 MHz LTE	2	2104.51	171.0	5.56	1900 MHz LTE	1000	0.56%
T-Mobile 2100 MHz LTE	2	2649.42	171.0	7.00	2100 MHz LTE	1000	0.70%
T-Mobile 2500 MHz LTE IC & 2C Traffic	I	11044.63	171.0	14.58	2500 MHz LTE IC & 2C Traffic	1000	1.46%
T-Mobile 2500 MHz LTE IC & 2C Broadcast	I	1074.06	171.0	1.42	2500 MHz LTE IC & 2C Broadcast	1000	0.14%
T-Mobile 2500 MHz NR Traffic	I	22089.26	171.0	29.17	2500 MHz NR Traffic	1000	2.92%
T-Mobile 2500 MHz NR Broadcast	I	2148.13	171.0	2.84	2500 MHz NR Broadcast	1000	0.28%
			,			Total:	7.92%

<sup>•</sup> NOTE: Totals may vary by approximately 0.01% due to summation of remainders in calculations.



### **Summary**

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)
Sector A:	7.92%
Sector B:	7.92%
Sector C:	7.92%
T-Mobile Maximum MPE % (Sector A):	7.92%
Site Total:	7.92%
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **7.92**% of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

## **Protector**™ **Series**



#### **Diesel Generator Set**

#### **INCLUDES:**

- Two Line LCD Multilingual Digital Evolution™ Controller (English/Spanish/French/ Portuguese) with external viewing window for easy indication of generator status and breaker position.
- Isochronous Electronic Governor
- Sound Attenuated Aluminum Enclosure
- Smart Battery Charger
- UV/Ozone Resistant Hoses
- ±1% Voltage Regulation
- Integrated Base Tank Provides Up to 40 Hours of Run Time
- 5 Year Limited Warranty\*
- UL 2200 / UL142 / ULC S601 Listed
- Meets code requirements for External Vent and Fill

#### Standby Power Rating

Model RD015 - 15 kW 60 Hz Model RD020 - 20 kW 60 Hz Model RD030 - 30 kW 60 Hz

Model RD048 - 48 kW 60 Hz (single phase only) Model RD050 - 50 kW 60 Hz (three phase only)





Meets EPA Emission Regulations CA/MA Emissions Compliant

\* 5 year warranty applicable to U.S. and Territories/Canada. International warranty is 3 year limited.

#### **FEATURES**

- **INNOVATIVE DESIGN & PROTOTYPE TESTING** are key components of GENERAC'S success in "IMPROVING POWER BY DESIGN." But it doesn't stop there. Total commitment to component testing, reliability testing, environmental testing, destruction and life testing, plus testing to applicable CSA, NEMA, EGSA, and other standards, allows you to choose GENERAC POWER SYSTEMS with the confidence that these systems will provide superior performance.
- TEST CRITERIA:
  - **V** PROTOTYPE TESTED
  - **√** SYSTEM TORSIONAL TESTED
- √ NEMA MG1-22 EVALUATION **V** MOTOR STARTING ABILITY

SOLID-STATE. FREQUENCY COMPENSATED VOLTAGE REGULATION.

This state-of-the-art power maximizing regulation system is standard on all Generac models. It provides optimized FAST RESPONSE to changing load conditions and MAXIMUM MOTOR STARTING CAPABILITY by electronically torque-matching the surge loads to the engine. Digital voltage regulation at  $\pm 1\%$ .

- SINGLE SOURCE SERVICE RESPONSE from Generac's extensive dealer network provides parts and service know-how for the entire unit, from the engine to the smallest electronic component.
- GENERAC TRANSFER SWITCHES. Long life and reliability are synonymous with GENERAC POWER SYSTEMS. One reason for this confidence is that the GENERAC product line includes its own transfer systems and controls for total system compatibility.





## **GENERAC**

### 15 • 20 • 30 • 48 • 50 kW

## application & engineering data

#### **GENERATOR SPECIFICATIONS**

Туре	Synchronous
Rotor Insulation Class	H (15 & 20 kW) or F (30, 48 & 50 kW)
Stator Insulation Class	Н
Telephone Interference Factor (TIF)	<50
Alternator Output Leads 1-Phase	3 wire
Alternator Output Leads 3-Phase	6 wire
Bearings	Single Sealed Cartridge
Coupling	Direct, Flexible Disc
Excitation System	Direct

#### **VOLTAGE REGULATION**

Туре	Electronic
Sensing	Single Phase
Regulation	± 1%
Features	Adjustable Voltage & Gain

#### **GOVERNOR SPECIFICATIONS**

Туре	Electronic Isochronous
Steady State Regulation	± 0.25%

#### **ELECTRICAL SYSTEM**

Battery Charge Alternator	50 Amp (15 & 20 kW) or 70 Amp (30, 48 & 50 kW)
Smart Battery Charger	2 Amp
Recommended Battery (battery not included)	Group 27F, 700 CCA
System Voltage	12 Volts

#### **GENERATOR FEATURES**

Revolving field heavy duty generator

Directly connected to the engine

Operating temperature rise 120°C above a 40°C ambient

Class H insulation is NEMA rated

Class F insulation is NEMA rated

All models fully prototype tested

#### **ENCLOSURE FEATURES**

Aluminum weather protective enclosure	Ensures protection against mother nature. Electrostatically applied textured epoxy paint for added durability.	
Enclosed critical grade muffler	Quiet, critical grade muffler is mounted inside the unit to prevent injuries and maximize sound dampening.	
Small, compact, attractive	Makes for an easy, eye appealing installation.	
SAE	Sound attenuated enclosure ensures quiet operation.	

### 15 • 20 • 30 • 48 • 50 kW

## application & engineering data

#### **ENGINE SPECIFICATIONS: 15 & 20 kW**

Make	Generac
Model	In-line
Cylinders	4
Displacement (Liters)	2.28
Bore (in./mm)	3.46/88
Stroke (in./mm)	3.70/94
Compression Ratio	21.3:1
Intake Air System	Naturally Aspirated
Cylinder Head Type	Cast Iron OHV
Piston Type	Aluminum
EPA Emissions Compliance	Emergency Stationary

#### **ENGINE SPECIFICATIONS: 30 kW**

ENGINE OF EON FORMOUS. OF RW			
Make	Generac		
Model	In-line		
Cylinders	4		
Displacement (Liters)	2.4		
Bore (in/mm)	3.54/90		
Stroke (in/mm)	3.70/94		
Compression Ratio	21.3:1		
Intake Air System	Turbocharged		
Cylinder Head Type	Cast Iron OHV		
Piston Type	Aluminum		
EPA Emissions Compliance	Emergency Stationary		
71			

#### **ENGINE SPECIFICATIONS: 48/50 kW**

Make	Generac
Model	In-Line
Cylinders	4
Displacement (Liters)	3.4
Bore in/mm	3.86/98
Stroke in/mm	4.45/113
Compression Ratio	18.5:1
Intake Air System	Turbocharged/Aftercooled
Cylinder Head Type	Cast Iron OHV
Piston Type	Aluminum
EPA Emissions Compliance	Emergency Stationary

#### **ENGINE LUBRICATION SYSTEM**

Oil Pump Type	Gear
Oil Filter Type	Full flow spin-on canister
Crankcase Capacity (quarts/liters)	6.87/6.5 - 15 & 20 kW
	6.8/6.4 - 30 kW
	7.4/7 - 48 & 50 kW

#### **ENGINE COOLING SYSTEM**

Туре	Pressurized radiator - 15 & 20 kW Closed recovery - 30, 48 & 50 kW		
Water Pump	Pre-lubed, self-seatin		
Fan Speed (rpm)	1800 - 15 & 20 kW 2061 - 30 kW 2029 - 48 & 50 kW		
Fan Diameter (in/mm)	18.11/460 (15 & 20 kW) 22/559 (30, 48 & 50 kW)		
Fan Mode	Pusher		

#### **FUEL SYSTEM**

TOLL OTOTLIN	
Fuel Type	Ultra Low Sulfur Diesel Fuel
Fuel Pump Type	Mechanical Engine Driven Gear
Injector Type	Mechanical
Fuel Supply Line (mm/in)	7.94/0.31 (ID)
Fuel Return Line (mm/in)	7.94/0.31(ID)
Fuel Specification	ASTM
Fuel Filtering (microns)	5 - 15, 20 & 30 kW 10 - 48 & 50 kW

#### TANK SPECIFICATIONS

Total Size (gallons/liters)	34/128.7 - 15 & 20 kW 62/234.7 - 30, 48 & 50 kW
Usable Size (gallons/liters)	32/121.1 - 15 & 20 kW 57/215.8 - 30, 48 & 50 kW
Run Time @ 1/2 Load (hrs)	41 - 15 kW 31 - 20 kW 38 - 30 kW 25 - 48 & 50 kW
Listings	UL142 ULC-S601

#### **WEIGHTS AND DIMENSIONS**

	15 kW	20 kW	30 kW	48 kW	50 kW
Weight (lb/kg)	1380	)/626	1927/874	2197	7/997
Dimensions (LxWxH) (in/cm)	81 x 31 x 50/205 x 78 x 128			95 x 35 x 57/242 x 89 x 145	5

## **GENERAC**

## 15 • 20 • 30 • 48 • 50 kW

### operating data

#### **GENERATOR OUTPUT VOLTAGE/kW - 60 Hz**

		kW (Standby)	Amp (Standby)	CB Size
	120/240 V, 1Ø, 1.0 pf	15	62	70
RD015	120/208 V, 3Ø, 0.8 pf	15	52	60
	120/240 V, 3Ø, 0.8 pf	15	45	50
	120/240 V, 1Ø, 1.0 pf	20	83	100
RD020	120/208 V, 3Ø, 0.8 pf	20	69	80
	120/240 V, 3Ø, 0.8 pf	20	60	70
	120/240 V, 1Ø, 1.0 pf	30	125	150
RD030	120/208 V, 3Ø, 0.8 pf	30	104	125
ופטעח	120/240 V, 3Ø, 0.8 pf	30	90	100
	277/480 V, 3Ø, 0.8 pf	30	45	50
	120/240 V, 1Ø, 1.0 pf	48	200	200
RD048/	120/208 V, 3Ø, 0.8 pf	50	173	200
RD050	120/240 V, 3Ø, 0.8 pf	50	150	175
	277/480 V, 3Ø, 0.8 pf	50	75	90

#### **SURGE CAPACITY IN AMPS**

#### Voltage Dip @ < .4 pf 15% 30%

		1070	0070
	120/240 V, 1Ø	53	129
RD015	120/208 V, 3Ø	37	90
	120/240 V, 3Ø	32	78
	120/240 V, 1Ø	87	211
RD020	120/208 V, 3Ø	59	143
	120/240 V, 3Ø	51	124
	120/240 V, 1Ø	66	168
מפחם	120/208 V, 3Ø	59	144
ทบบอบ	120/240 V, 3Ø	51	125
	277/480 V, 3Ø	26	64
	120/240 V, 1Ø	69	189
RD048/	120/208 V, 3Ø	90	218
RD050	120/240 V, 3Ø	78	189
	277/480 V, 3Ø	36	87
,	120/240 V, 3Ø 277/480 V, 3Ø 120/240 V, 1Ø 120/208 V, 3Ø 120/240 V, 3Ø	51 26 69 90 78	125 64 189 218 189

#### **ENGINE FUEL CONSUMPTION**

		gal/hr	L/hr
	25% of rated load	0.51	1.93
RD015	50% of rated load	0.79	2.99
כוטעא	75% of rated load	1.14	4.31
	100% of rated load	1.48	5.58
	25% of rated load	0.67	2.6
RD020	50% of rated load	1.05	3.97
NDUZU	75% of rated load	1.52	5.32
	100% of rated load	1.98	7.48
	25% of rated load	0.92	3.5
RD030	50% of rated load	1.45	5.5
טפטעח	75% of rated load	1.96	7.4
	100% of rated load	2.74	10.4
	25% of rated load	1.35	5.11
RD048/	50% of rated load	2.15	8.14
RD050	75% of rated load	3.06	11.58
	100% of rated load	3.98	15.07

## **GENERAC®**

operating data

### 15 • 20 • 30 • 48 • 50 kW

### **ENGINE COOLING**

	15 kW	20 kW	30 kW	48/50 kW
Air flow (inlet air including alternator and combustion air in cfm/cmm)	2824/80	2824/80	3038/86	2824/80
System coolant capacity (gal/liters)	2.8/10.6	2.8/10.6	2.8/10.6	2.8/10.6
Heat rejection to coolant (BTU per hr/MJ per hr)	63,535/67	63,535/67	111,000/117.1	135,900/143.4
Maximum operation air temperature on radiator (°C/°F)	50/122			
Maximum ambient temperature (°C/°F)	50/122			

#### **COMBUSTION REQUIREMENTS**

Flow at rated power (cfm/cmm)	84.76/2.4	84.76/2.4	90/2.55	190/5.38
-------------------------------	-----------	-----------	---------	----------

#### **SOUND EMISSIONS**

Sound output in dB(A) at 23 ft (7 m) with generator in exercise mode*	65
Sound output in dB(A) at 23 ft (7 m) with generator operating at normal load*	70

<sup>\*</sup>Sound levels are taken from the front of the generator. Sound levels taken from other sides of the generator may be higher depending on installation parameters.

#### **EXHAUST**

Exhaust flow at rated output (cfm/cmm)	98.88/2.8	98.88/2.8	230/6.51	448/12.7
Exhaust temperature at rated output (°C/°F)	604.4/1120	604.4/1120	454.4/850	604.4/1120

#### **ENGINE PARAMETERS**

Rated Synchronous RPM	1800			
HP at rated kW	26.4	33.5	49	85

#### POWER ADJUSTMENT FOR AMBIENT CONDITIONS

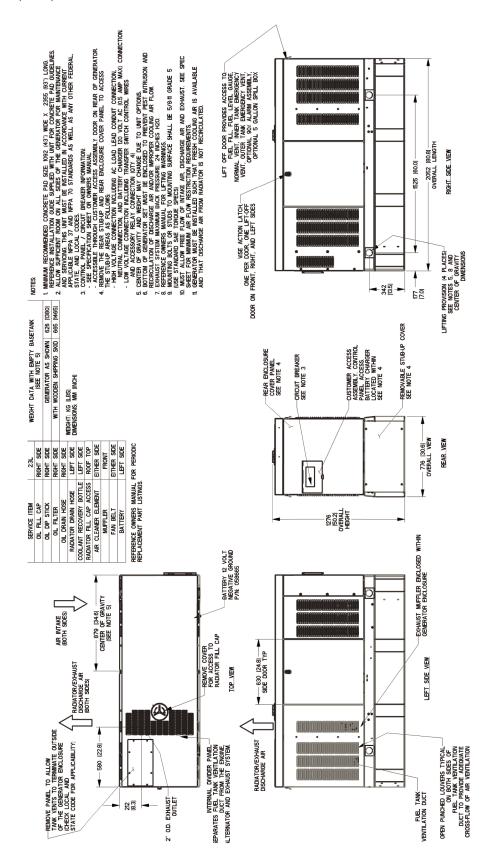
Temperature Deration	
Altitude Deration (15, 30, 48 & 50 kW)	1% for every 100 m above 915 m or 3% for every 1000 ft above 3000 ft
Altitude Deration (20 kW)	1% for every 100 m above 305 m or 3% for every 1000 ft above 1000 ft

#### **CONTROLLER FEATURES**

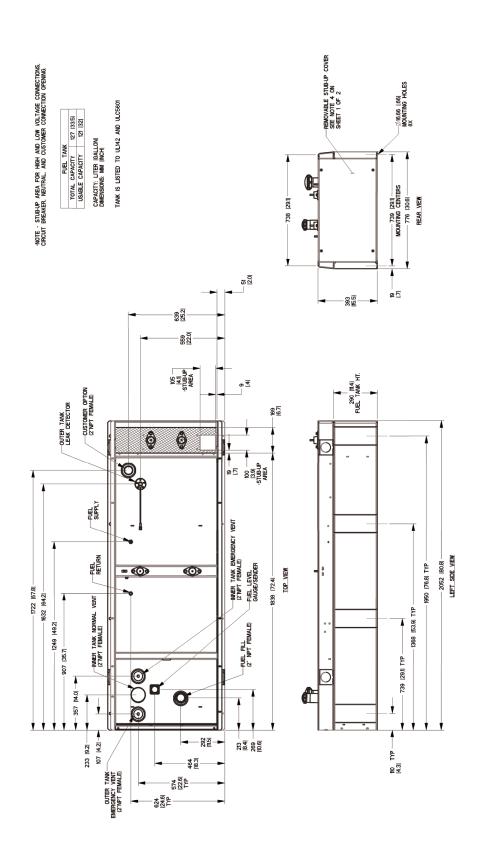
CONTROLLER I LATORLO	
2-Line Plain Text Multilingual LCD Display	Simple user interface for ease of operation.
Mode Buttons: Auto	
Manual	Start with starter control, unit stays on. If utility fails, transfer to load takes place.
Off	Stops unit. Power is removed. Control and charger still operate.
	Standard
Engine Run Hours Indication	
Programmable start delay between 2-1500 seconds	Standard (programmable by dealer only)
	From 140-171 V/190-216 V
	Standard
Run/Alarm/Maintenance Logs	50 Events Each
Engine Start Sequence	
Starter Lock-out	Starter cannot re-engage until 5 sec after engine has stopped.
Smart Battery Charger	Standard
Charger Fault/Missing AC Warning	Standard
Low Battery/Battery Problem Protection and Battery Condition Indication	Standard
Automatic Voltage Regulation with Over and Under Voltage Protection	Standard
Under-Frequency/Overload/Stepper Overcurrent Protection	
Safety Fused/Fuse Problem Protection	Standard
Automatic Low Oil Pressure/High Oil Temperature Shutdown	Standard
	Standard
	Standard
	Standard
Common External Fault Capability	Standard
Field Upgradable Firmware	Standard

**GENERAC** 

Drawing #0K7025-C (1 of 2)



Drawing #0K7025-C (2 of 2)

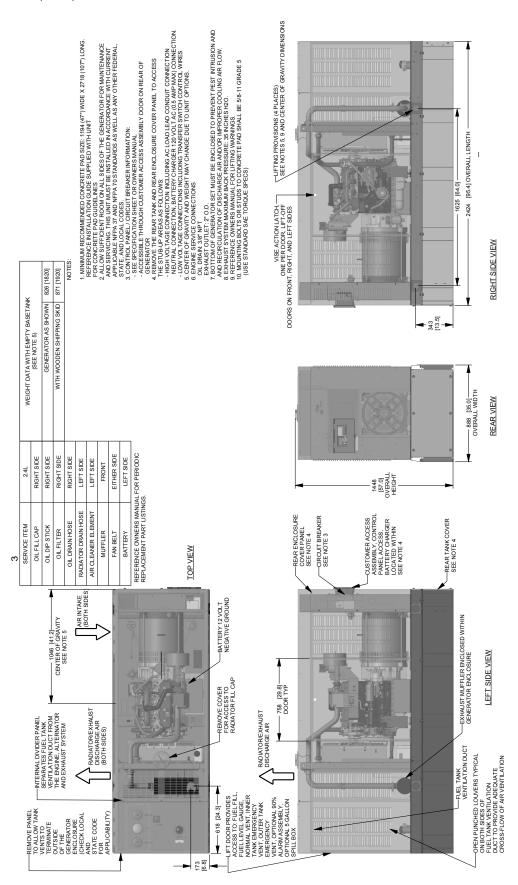


7 of 12

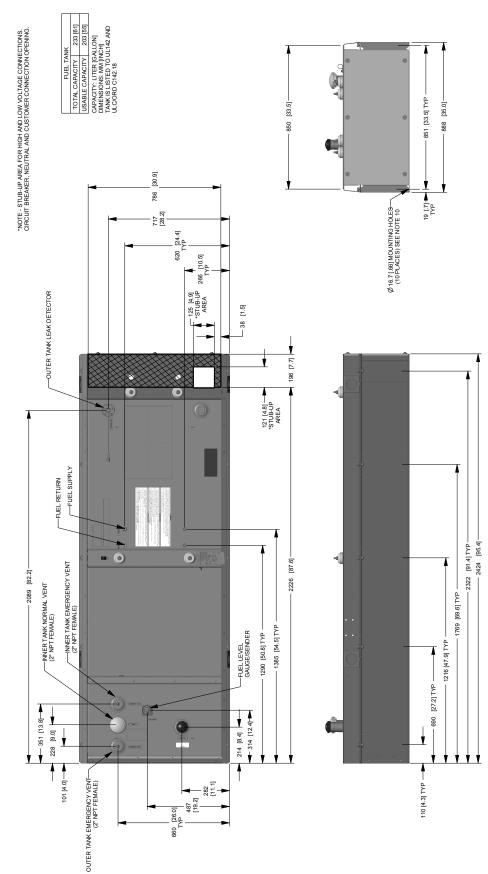
# installation layout

**GENERAC** 

Drawing #0K7002-C (1 of 2)



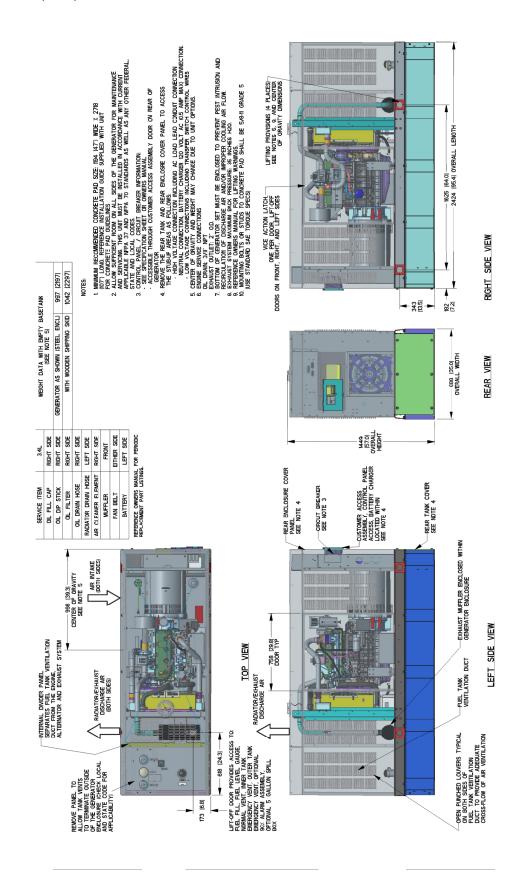
Drawing #0K7002-B (2 of 2)



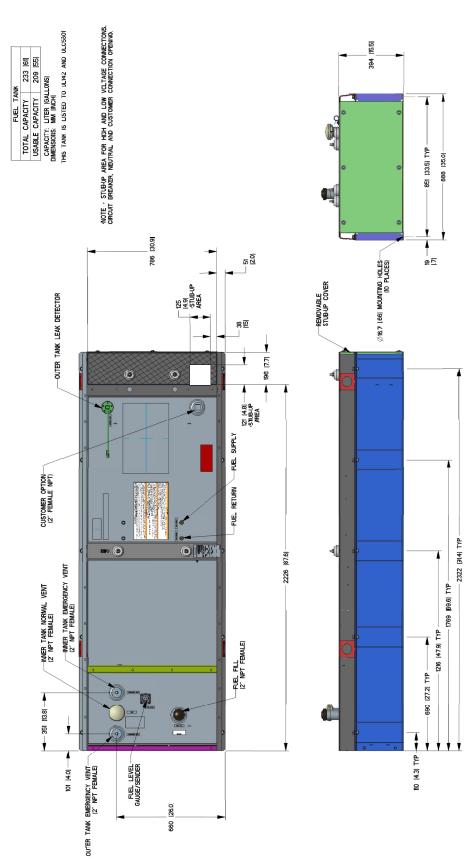
9 of 12

**GENERAC** 

Drawing #0K6968-C (1 of 2)



Drawing #0K6968-A (2 of 2)



11 of 12

## **GENERAC**

### 15 • 20 • 30 • 48 • 50 kW

### available accessories

Model #	Product	Description
G006463-4	Mobile Link™	Generac's Mobile Link allows you to check the status of your generator from anywhere that you have access to an Internet connection from a PC or with any smart device. You will even be notified when a change in the generator's status occurs via e-mail or text message. Note: Harness Adapter Kit required. Available in the U.S. only.
G006478-0	Harness Adapter Kit	The Harness Adapter Kit is required to make liquid-cooled units compatible with Mobile $Link^TM$ .
G006502-0	Spill Box	The 5-gallon spill box screws into the existing fuel fill port of the base tank. It captures and contains fuel if over fueling or spilling occurs during the fill process.
G006504-0	90% Fuel Level Alarm	The 90% fuel level alarm alerts the fuel fill operator when the tank reaches a 90% fill level by sounding an audible alarm and triggering an LED warning light.
G006505-0 - 15 & 20 kW G006506-0 - 30, 48 & 50 kW	Tank Risers	Tank risers are required in some municipalities to help avoid potential base tank corrosion caused by mounting on rough surfaces.
G006507-0	Fuel Fill Drop Tube	A powder coat painted, steel fuel fill drop tube is required in some municipalities to prevent sparking due to static electricity buildup, which can be caused by the fuel dropping into the tank from the fill area. Using a drop tube also results in submerged filling, which increases the fuel delivery flow rate and reduces vapors, foam and potential tank evaporation.
G006513-0 - 15 & 20 kW G006517-0 - 30 kW G006516-0 - 48 & 50 kW	Stainless Steel Fuel Lines	Some municipalities require the use of stainless steel fuel lines instead of the standard hoses provided with the diesel generator products. These stainless steel lines are fire resistant for additional safety.
G006510-0	E-Stop	E-stop allows for immediate fuel shutoff and generator shutdown in the event of an emergency.
006511-0	Spill Box Drainback Kit	The spill box drainback kit allows fuel that was captured in the 5-gallon spill box to be drained directly back into the fuel tank to avoid vapors.
G006588-1	Vent Extension Support Kit	The vent extension support kit consists of two aluminum plates with the appropriate pipe cutouts to secure the vent extension pipes coming through the top of the generator enclosure. It helps to minimize stress on the NPT fittings integrated on the tank and also helps protect against pests.
G006512-0	Lockable Fuel Cap	The cast iron, lockable fuel cap provides the ability to lock the fuel system to prevent unwanted fuel tampering or fuel siphoning.
G006572-0 - 15 & 20 kW G006571-0 - 30 kW G006570-0 - 48 & 50 kW	Maintenance Kits	The Protector Maintenance Kits offer all the hardware necessary to perform complete maintenance on Generac Protector generators.
G006560-0 - 15 & 20 kW G006559-0 - 30 kW G006558-0 - 48 & 50 kW	Cold Weather Kits	Recommended for generators installed in regions where the temperature regularly falls below 32 °F (0 °C). The Cold Weather Kits consist of a block heater with all necessary mounting hardware and a battery warmer with a thermostat built into the battery wrap.
G005704-0	Paint Kit	If the generator enclosure is scratched or damaged, it is important to touch-up the paint to protect from future corrosion. The paint kit includes the necessary paint to properly maintain or touch-up a generator enclosure.
G006664-0	Local Wireless Remote	Completely wireless and battery powered, Generac's wireless remote monitor provides you with instant status information without ever leaving the house.
G006665-0	Wireless Remote Extension Harness	Recommended for use with the Wireless Remote on units up to 60 kW, required for use on units 70 kW or greater.
G006873-0	Smart Management Module (50 Amps)	Manage large loads by utilizing up to 8 individual Smart Management modules. These devices are installed directly in line with existing appliance wiring for easy installation.

