

Crown Castle 3530 Toringdon Way Suite 300 Charlotte, NC 28277 Tel: 704-405-6600

www.crowncastle.com

March 25, 2014

Melanie A. Bachman Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

RE: T-Mobile-Exempt Modification - Crown Site BU: 876327

T-Mobile Site ID: CT11883C

Located at: 59 McGuire Road, South Windsor, CT 06074

Dear Ms. Bachman:

This letter and exhibits are submitted on behalf of T-Mobile. T-Mobile is making modifications to certain existing sites in its Connecticut system in order to implement their Modernization technology. Please accept this letter and exhibits as notification, pursuant to § 16-50j-73 of the Regulations of Connecticut State Agencies ("R.C.S.A."), of construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In compliance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to The Honorable M. Saud Anwar, Mayor for the Town of South Windsor.

T-Mobile plans to modify the existing wireless communications facility owned by Crown Castle and located at **59 McGuire Road, South Windsor, CT 06074**. Attached are a compound plan and elevation depicting the planned changes (Exhibit-1), and documentation of the structural sufficiency of the structure to accommodate the revised antenna configuration (Exhibit-2). Also included is a power density table report reflecting the modification to T-Mobile's operations at the site (Exhibit-3).

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes ("C.G.S.") § 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in the R.C.S.A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing tower. T-Mobile's replacement antennas will be located at the same elevation on the existing tower.
- 2. There will be no proposed modifications to the ground and no extension of boundaries.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more.

- 4. The operation of the replacement antennas will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) adopted safety standard. A cumulative General Power Density table report for T-Mobile's modified facility is included as Exhibit-3.
- 5. A Structural Modification Report confirming that the tower and foundation can support Sprint's proposed modifications is included as Exhibit-2.

For the foregoing reasons, T-Mobile respectfully submits the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Donna Neal.

Sincerely,

Jeff Barbadora

Real Estate Specialist

Enclosure

Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes

Tab 2: Exhibit-2: Structural Modification Report

Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)

cc: The Honorable M. Saud Anwar, Mayor

Town of South Windsor 1540 Sullivan Avenue South Windsor, CT 06074

-- T--Mobile--

NORTHEAST LLC.

SITE NAME: CT883/SPRINT S. WINDSOR

SITE ID NUMBER: CT11883C

SITE ADDRESS: 59 MCGUIRE ROAD

SOUTH WINDSOR, CT 06074

PROJECT SUMMARY

STRUCTURAL ENG:

SITE ID NUMBER: CT11883C

SITE NAME: CT883/SPRINT S. WINDSOR

CROWN BU#: 876327

SITE ADDRESS: 59 MCGUIRE ROAD

SOUTH WINDSOR, CT 06074

COUNTY: HARTFORD

CROWN CASTLE USA PROPERTY OWNER:

T-MOBILE NORTHEAST, LLC. APPLICANT:

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 0602

PHONE: (800) 692-7100

ENGINEER/ TECTONIC ENGINEERING CONSULTANTS P.C. SURVEYOR/

1279 ROUTE 300 NEWBURGH, NY 12550

CONTACT: TAMMY NOSEK

(845) 567-6656 EXT. 2807 PHONE:

SITE ACQUISITION: CROWN CASTLE

1200 MACARTHUR BLVD

SUITE 200

MAHWAH, NJ 07430 PAUL HUGHES

CONTACT: (585) 259-7604

PHONE:

MAP 5 LOT 14.1 PARCEL INFO:

LATITUDE: (NAD 83) 41.80290 N

72.61730 W LONGITUDE: (NAD 83)

SITE DIRECTIONS

HEAD NORTHEAST ON GRIFFIN RD S TOWARD W NEWBERRY RD. TAKE THE 1ST RIGHT ONTO W NEWBERRY RD. TURN LEFT ONTO WOODLAND AVE. TAKE THE 1ST RIGHT ONTO CT-187 S/BLUE HILLS AVE. TURN LEFT ONTO CT-218 E/COTTAGE GROVE RD. CONTINUE TO FOLLOW CT-218 E. TURN RIGHT ONTO THE INTERSTATE 291 E RAMP TO SOUTH WINDSOR. MERGE ONTO I-291 E. TAKE EXIT 4 TO MERGE ONTO US-5 S/ELLINGTON RD. TURN RIGHT ONTO BURNHAM ST. TURN RIGHT ONTO KING ST. TURN RIGHT ONTO MCGUIRE RD. DESTINATION WILL BE ON THE RIGHT.

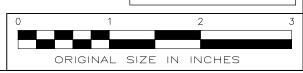


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A-1	SITE PLAN	0							
A-2	EQUIPMENT LAYOUT PLANS	0							
A-3	ELEVATION & DETAIL	0							
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A-5	DETAILS	0							
A-6	DETAILS	0							
A-7	NOTES	0							
A-8	NOTES	0							
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THIS SET OF PLANS SHALL NOT BE UTILIZED AS CONSTRUCTION DOCUMENTS UNTIL ALL ITEMS HAVE BEEN ADDRESSED AND EACH OF THE DRAWINGS HAS BEEN REVISED AND ISSUED "FOR CONSTRUCTION".



CONFIGURATION REFER TO LATEST T-MOBILE RF DATA SHEET FOR FINAL RF DESIGN & BOM.



- ENGINEERING

TECTONIC Engineering & Survey Consultants P.C. 1279 ROUTE 300 NEWBURGH, NY 12550

T-MOBILE NORTHEAST LLC.

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 PHONE: (860) 692-7100



LANDLORD
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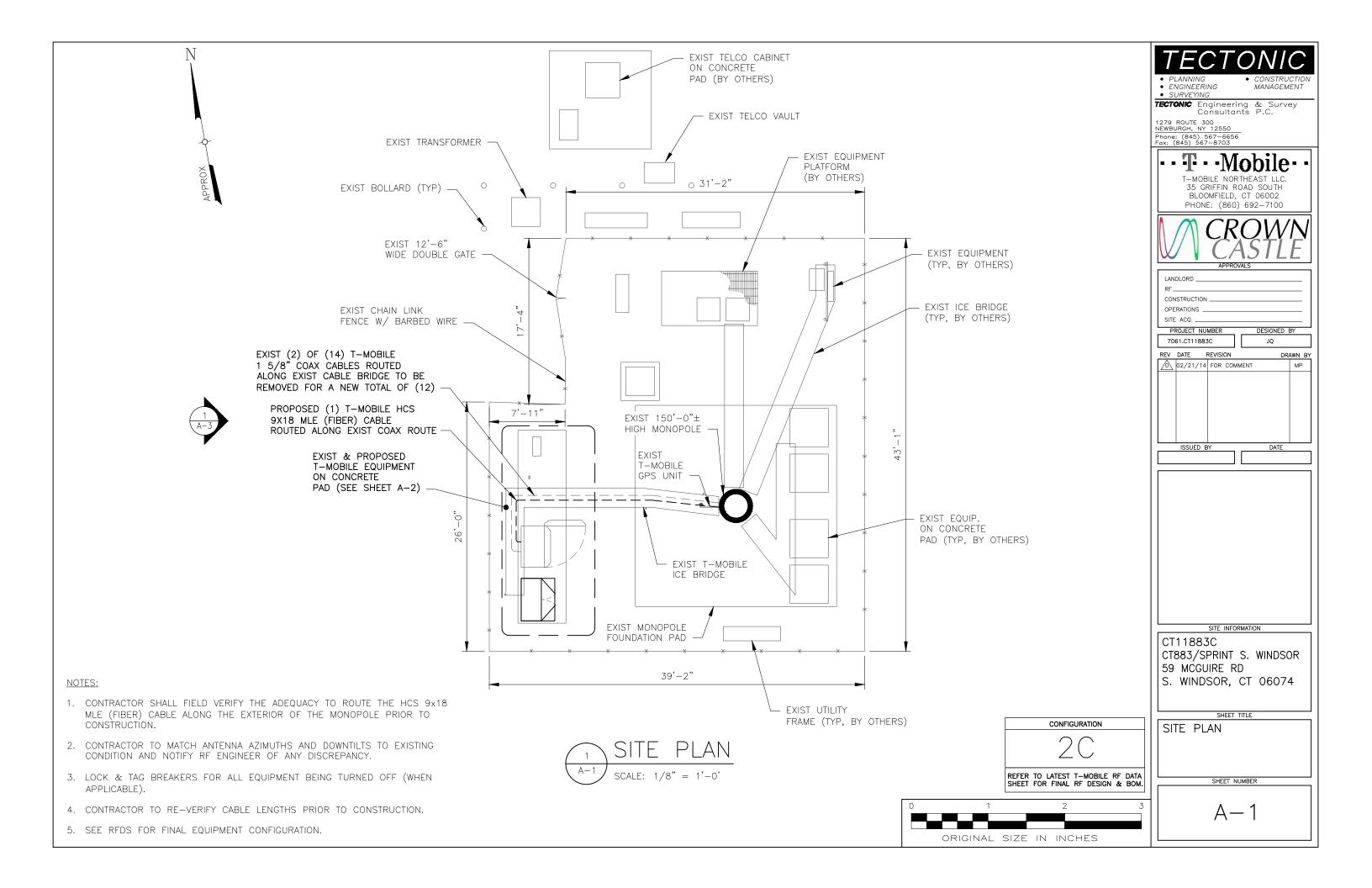
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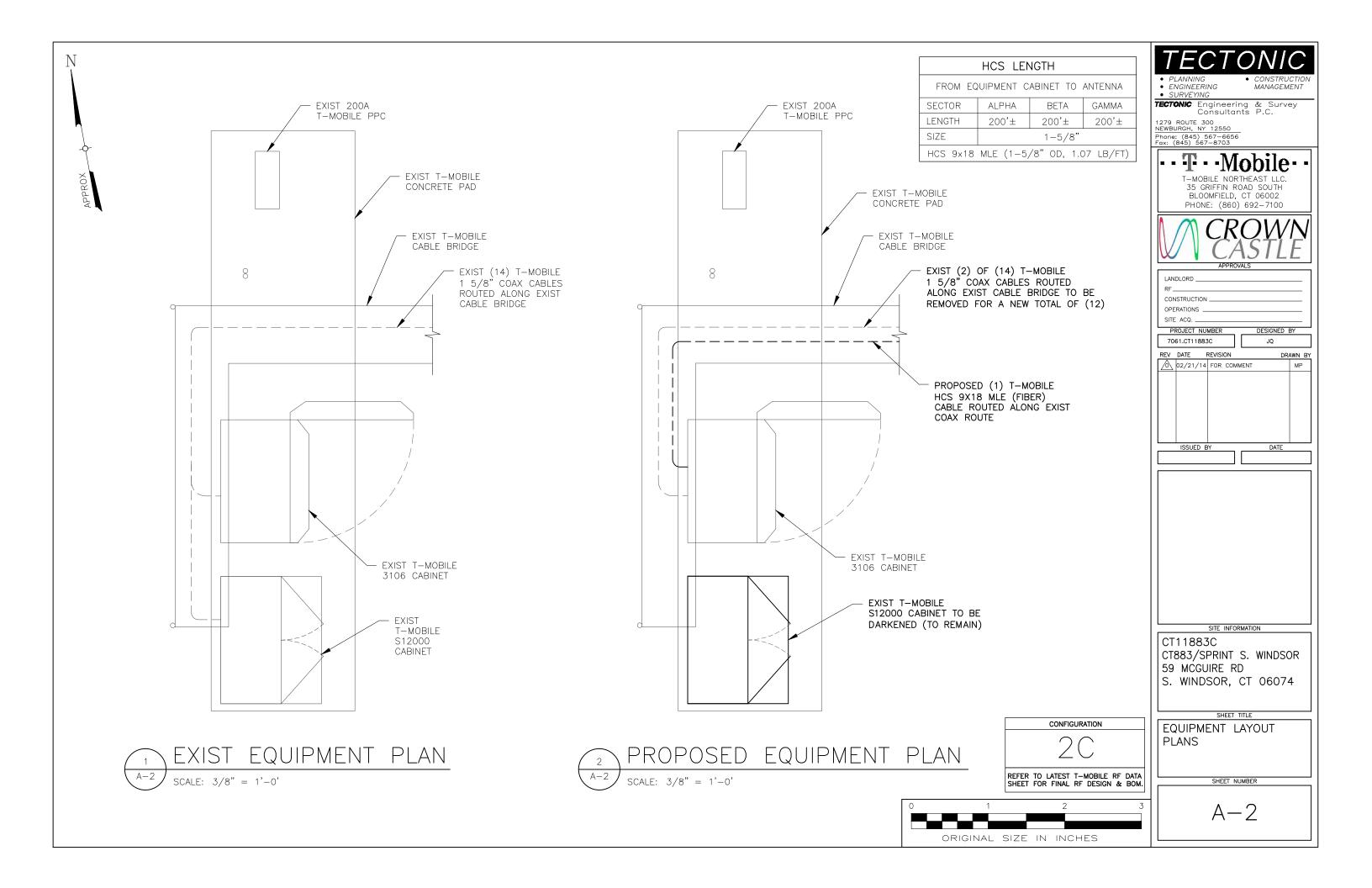
CT11883C CT883/SPRINT S. WINDSOR 59 MCGUIRE RD S. WINDSOR, CT 06074

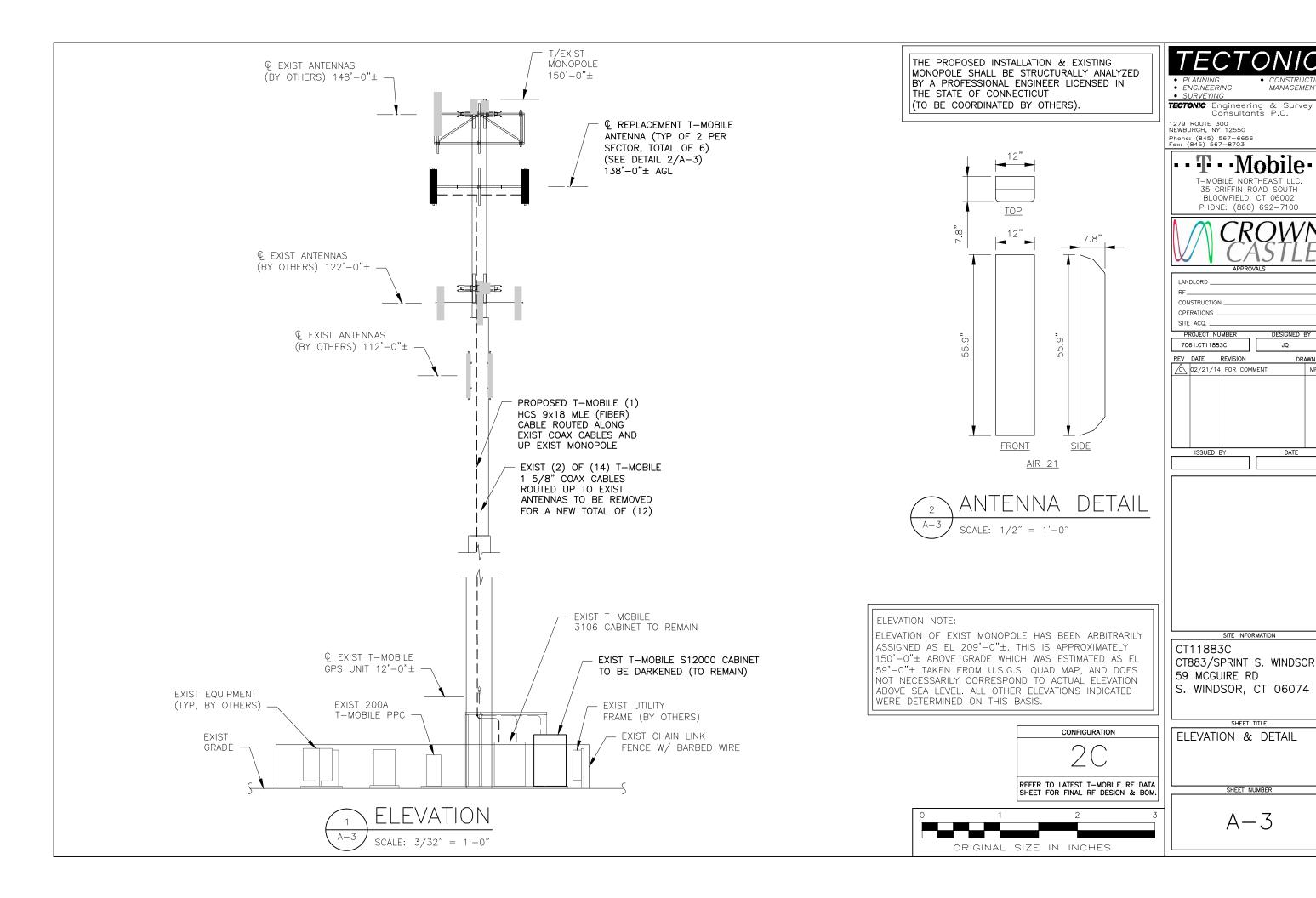
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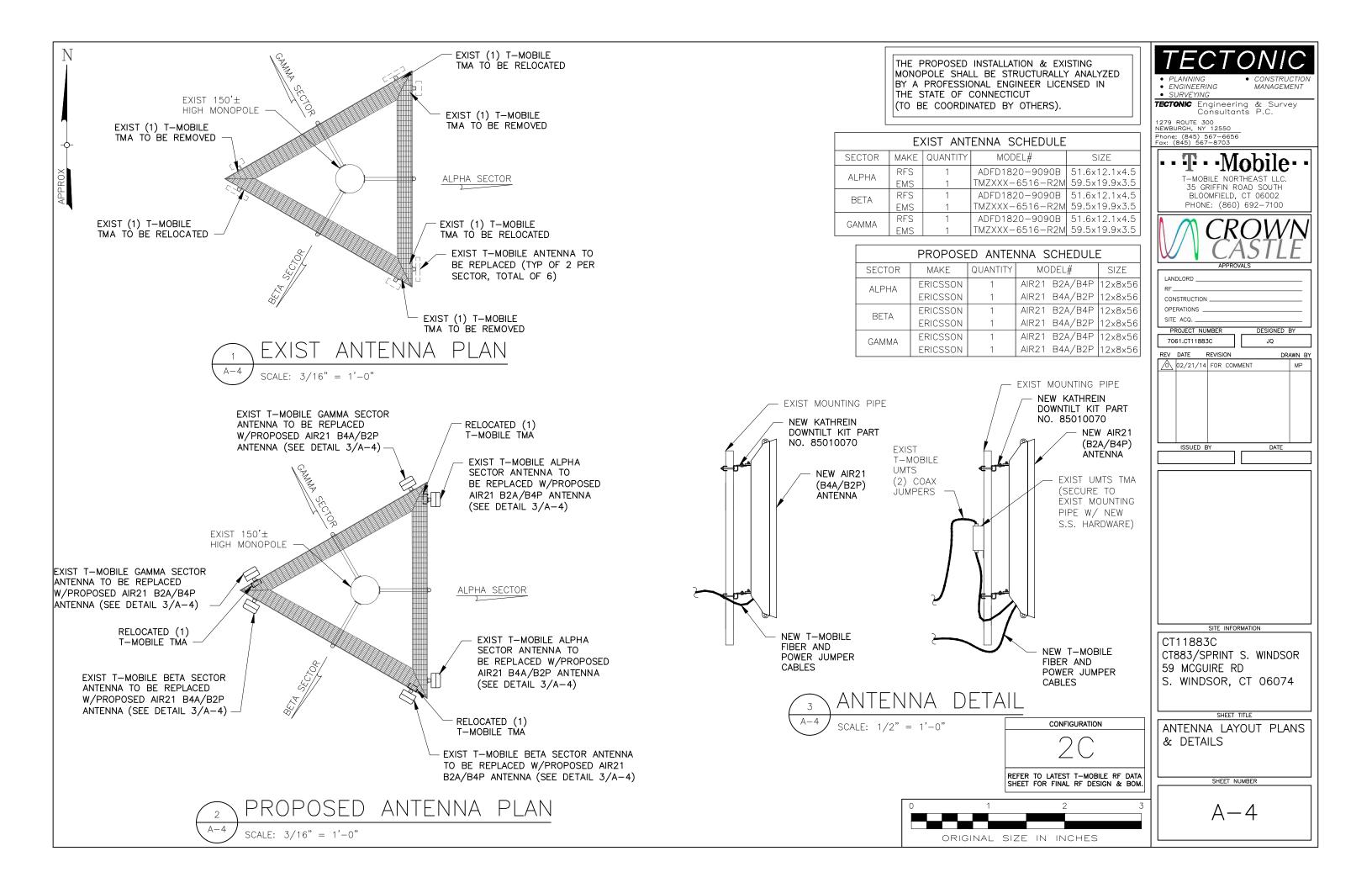
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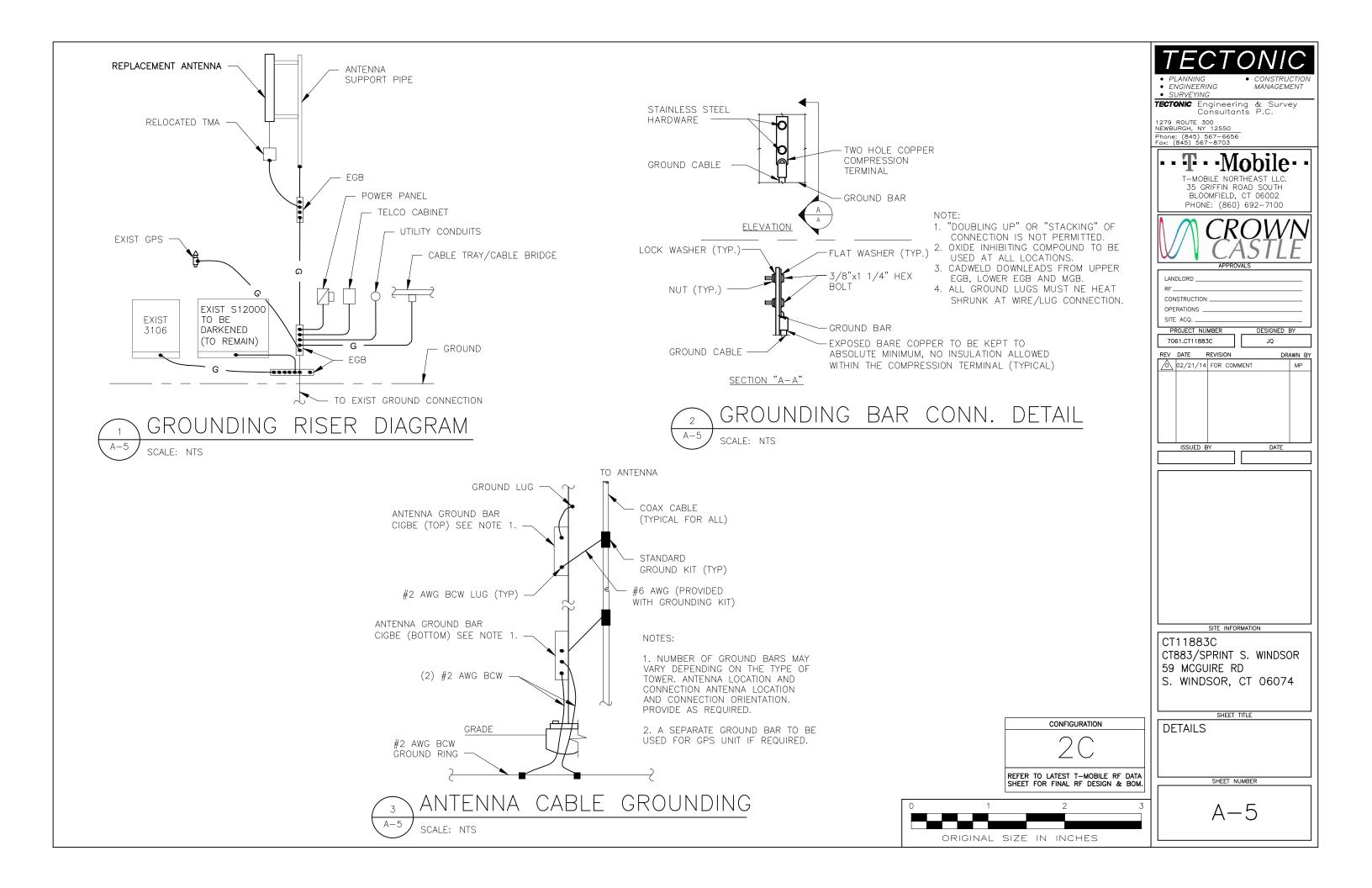
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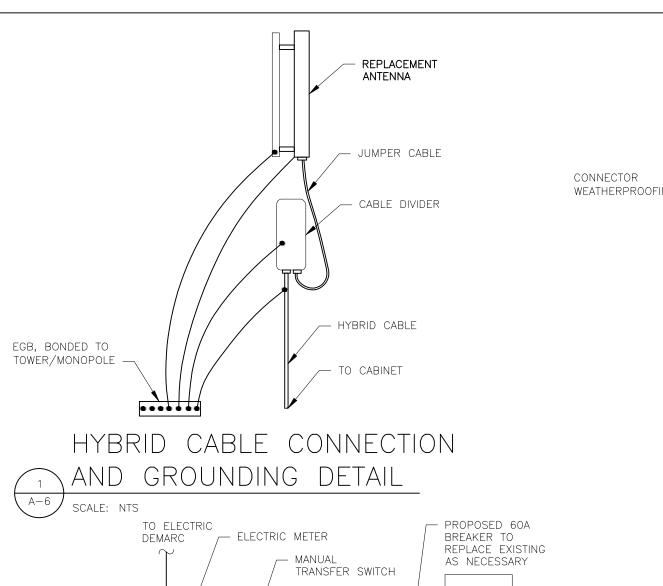


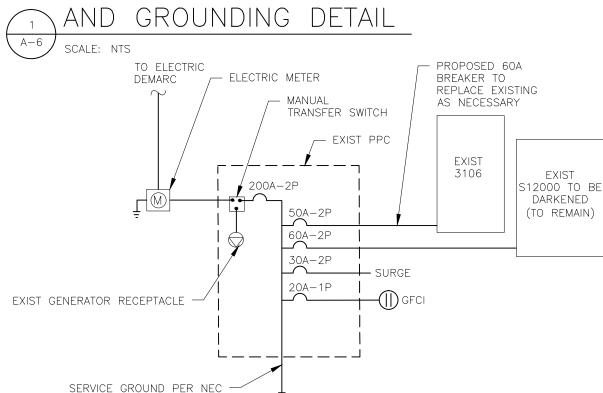






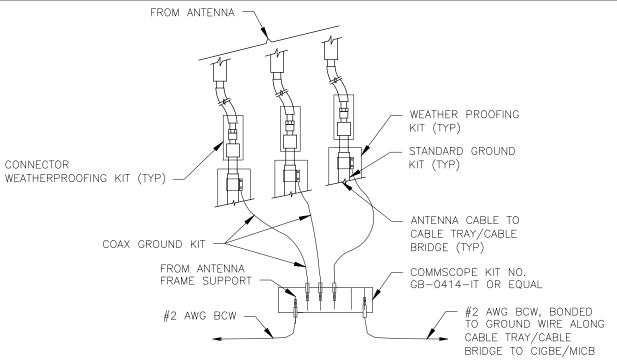






NOTE: CONTRACTOR TO VERIFY EXISTING CONDUCTORS ARE #6AWG OR LARGER FOR 60A CIRCUIT





NOTE:

DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

GROUND WIRE TO GROUND BAR CONNECTION DETAIL

4-6

SCALE: NTS



- PLANNING
- CONSTRUCT
- ENGINEERING

TECTONIC Engineering & Survey Consultants P.C.

1279 ROUTE 300 NEWBURGH, NY 12550 Phone: (845) 567-665 Fax: (845) 567-8703

·· T··Mobile·

T-MOBILE NORTHEAST LLC. 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 PHONE: (860) 692-7100



PROJECT NUMBER DESIGNED BY
7061.CT11883C JQ

REV DATE REVISION DRAWN E

ISSUED BY

DATE

SITE INFORMATION

CT11883C CT883/SPRINT S. WINDSOR 59 MCGUIRE RD

S. WINDSOR, CT 06074

SHEET TITLE

DETAILS

A - 6

SHEET NUMBER

CONFIGURATION

REFER TO LATEST T-MOBILE RF DATA SHEET FOR FINAL RF DESIGN & BOM.

0 1 2 3
ORIGINAL SIZE IN INCHES

GENERAL NOTES

- 1. CONTRACTOR SHALL NOT COMMENCE ANY WORK UNTIL HE OBTAINS, AT HIS OWN EXPENSE, ALL INSURANCE REQUIRED BY T-MOBILE, THE PROPERTY OWNER AND/OR PROPERTY MANAGEMENT COMPANY.
- 2. THIS SET OF PLANS HAS BEEN PREPARED FOR THE PURPOSES OF MUNICIPAL AND AGENCY REVIEW AND APPROVAL. THIS SET OF PLANS SHALL NOT BE UTILIZED AS CONSTRUCTION DOCUMENTS UNTIL ALL CONDITIONS OF APPROVAL HAVE BEEN SATISFIED AND EACH OF THE DRAWINGS HAVE BEEN REVISED TO INDICATE "ISSUED FOR PERMIT"
- 3. THIS PLAN IS SUBJECT TO ALL EASEMENTS AND RESTRICTIONS OF RECORD.
- 4. THE CONTRACTOR SHALL COMPLY WITH ALL APPLICABLE CODES, ORDINANCES, LAWS AND REGULATIONS OF ALL MUNICIPALITIES, UTILITIES OR OTHER PUBLIC AUTHORITIES.
- 5. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND INSPECTIONS THAT MAY BE REQUIRED BY ANY FEDERAL, STATE, COUNTY OR MUNICIPAL AUTHORITIES.
- 6. THE CONTRACTOR SHALL NOTIFY THE CONSTRUCTION MANAGER, IN WRITING, OF ANY CONFLICTS, ERRORS OR OMISSIONS PRIOR TO THE SUBMISSION OF BIDS OR PERFORMANCE OF WORK. MINOR OMISSIONS OR ERRORS IN THE BID DOCUMENTS SHALL NOT EXCUSE SAID CONTRACTOR FROM COMPLETING THIS PROJECT IN ACCORDANCE WITH THE OVERALL INTENT OF THESE DRAWINGS.
- 7. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING ALL EXISTING SITE IMPROVEMENTS PRIOR TO COMMENCING CONSTRUCTION. THE CONTRACTOR SHALL REPAIR ANY DAMAGE CAUSED AS A RESULT OF CONSTRUCTION OF THIS FACILITY.
- 8. THE SCOPE OF WORK FOR THIS PROJECT SHALL INCLUDE PROVIDING ALL MATERIALS, EQUIPMENT AND LABOR REQUIRED TO COMPLETE THIS PROJECT. ALL EQUIPMENT SHALL BE INSTALLED IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- 9. THE CONTRACTOR SHALL VISIT THE PROJECT SITE PRIOR TO SUBMITTING A BID TO VERIFY THAT THE PROJECT CAN BE CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS.
- 10. POWER TO THE FACILITY IS MONITORED BY AN EXISTING METER.
- 11. ALL STRUCTURAL ELEMENTS SHALL BE HOT DIPPED GALVANIZED STEEL.
- 12. CONTRACTOR SHALL MAKE A UTILITY "ONE CALL" TO LOCATE ALL UTILITIES PRIOR TO EXCAVATING.
- 13. IF ANY PIPING EXISTS BENEATH THE SITE AREA, CONTRACTOR MUST LOCATE IT AND CONTACT OWNER'S REPRESENTATIVE.
- 14. THE CONSTRUCTION CONTRACTOR IS SOLELY RESPONSIBLE FOR DETERMINING ALL CONSTRUCTION MEANS AND METHODS. THE CONSTRUCTION CONTRACTOR IS ALSO RESPONSIBLE FOR ALL JOB SITE SAFETY.
- 15. CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES AND EXISTING CONDITIONS AT THE SITE PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA AND SUBMIT TO THE ENGINEER ANY DISCREPANCIES FROM THE DRAWINGS.
- 16. THE CONTRACTOR IS TO REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. THE CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUB—CONTRACTORS AND RELATED PARTIES. THE SUB—CONTRACTOR SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
- 17. DETAILS ARE INTENDED TO SHOW END RESULT OF DESIGN. MINOR MODIFICATIONS MAY BE REQUIRED TO SUIT JOB DIMENSIONS OR CONDITIONS, AND SUCH MODIFICATIONS SHALL BE INCLUDED AS PART OF THE WORK.
- 18. ALL MATERIAL PROVIDED BY T-MOBILE IS TO BE REVIEWED BY THE CONTRACTOR AND ALL APPLICABLE SUB-CONTRACTORS PRIOR TO INSTALLATION. ANY DEFICIENCIES TO PROVIDE MATERIALS SHALL BE BROUGHT TO THE CONSTRUCTION MANAGER'S ATTENTION IMMEDIATELY.
- 19. THE MATERIALS INSTALLED SHALL MEET REQUIREMENTS OF CONTRACTORS DOCUMENTS. NO SUBSTITUTIONS ARE ALLOWED.
- 20. INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR CONFORMING MATERIALS OR CONDITIONS SHALL BE REPORTED TO THE ENGINEER PRIOR TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE ENGINEER APPROVAL.

GENERAL NOTES

- 21. THE CONTRACTOR SHALL RECEIVE CLARIFICATION AND AUTHORIZATION IN WRITING TO PROCEED BEFORE STARTING WORK ON ANY ITEMS NOT CLEARLY DEFINED OR IDENTIFIED BY THE CONSTRUCTION DOCUMENTS.
- 22. THE CONTRACTOR SHALL NOTIFY THE CONSTRUCTION MANAGER OF ALL PRODUCTS OR ITEMS NOTED AS "EXISTING" WHICH ARE NOT FOUND TO BE IN THE FIELD.
- 23. ERECTION SHALL BE DONE IN A WORKMANLIKE MANNER BY COMPETENT EXPERIENCED WORKMEN IN ACCORDANCE WITH APPLICABLE CODES AND THE BEST—ACCEPTED PRACTICE. ALL MEMBERS SHALL BE LAND PLUMB AND TRUE AS INDICATED ON THE DRAWINGS.
- 24. THE CONTRACTOR SHALL COORDINATE HIS WORK AND SCHEDULE HIS ACTIVITIES AND WORKING HOURS IN ACCORDANCE WITH THE REQUIREMENTS OF THE PROPERTY OWNER AND/OR PROPERTY MANAGEMENT COMPANY.
- 25. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATING HIS WORK WITH THE WORK OF OTHERS AS IT MAY RELATE TO RADIO EQUIPMENT, ANTENNAS AND ANY OTHER PORTIONS OF THE WORK.
- 26. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY INDICATED OR WHERE LOCAL CODES OR REGULATIONS MAY TAKE PRECEDENCE.
- 27. THE CONTRACTOR SHALL REPAIR ALL EXISTING SURFACES DAMAGED DURING CONSTRUCTION SUCH THAT THEY MATCH AND BLEND WITH ADJACENT SURFACES.
- 28. THE CONTRACTOR SHALL KEEP CONTRACT AREA CLEAN, HAZARD FREE AND DISPOSE OF ALL DEBRIS AND RUBBISH. EQUIPMENT NOT SPECIFIED AS REMAINING ON THE PROPERTY OF THE OWNER SHALL BE REMOVED. LEAVE PREMISES IN CLEAN CONDITIONS AND FREE FROM PAINT SPOTS, DUST OR SMUDGES OF ANY NATURE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING ALL ITEMS UNTIL COMPLETION OF CONSTRUCTION.
- 29. BEFORE FINAL ACCEPTANCE OF THE WORK, THE CONTRACTOR SHALL REMOVE ALL EQUIPMENT, TEMPORARY WORK, UNUSED AND USELESS MATERIALS, RUBBISH AND TEMPORARY STRUCTURES.
- 30. ALL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE 2005 CONNECTICUT STATE BUILDING CODE (INCLUDING AMENDMENTS) AND ALL OTHER APPLICABLE CODES AND ORDINANCES.
- 31. CONTRACTOR SHALL VISIT THE JOB SITE AND SHALL FAMILIARIZE HIMSELF WITH ALL CONDITIONS AFFECTING THE PROPOSED WORK AND SHALL MAKE PROVISIONS AS TO THE COST THEREOF. CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING HIMSELF WITH ALL CONTRACT DOCUMENTS, FIELD CONDITIONS AND DIMENSIONS AND CONFIRMING THAT THE WORK MAY BE ACCOMPLISHED AS SHOWN PRIOR TO PROCEEDING WITH CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER PRIOR TO THE COMMENCEMENT OF WORK.
- 32. PLANS ARE NOT TO BE SCALED. THESE PLANS ARE INTENDED TO BE A DIAGRAMMATIC OUTLINE ONLY UNLESS OTHERWISE NOTED. THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT AND APPURTENANCES, AND LABOR NECESSARY TO EFFECT ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
- 33. CONTRACTOR SHALL BE RESPONSIBLE FOR THE SAFETY OF THE WORK AREA, ADJACENT AREAS AND BUILDING OCCUPANTS THAT ARE LIKELY TO BE AFFECTED BY THE WORK UNDER THIS CONTRACT. WORK SHALL CONFORM TO ALL OSHA REQUIREMENTS.
- 34. CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK USING THE BEST CONSTRUCTION SKILLS AND ATTENTION. CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES AND PROCEDURES AND FOR COORDINATING ALL PORTIONS OF THE WORK UNDER CONTRACT, UNLESS OTHERWISE NOTED.

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CONFIGURATION

TECTONIC

- PLANNING
- CONSTRUCTION
- ENGINEERING SURVEYING

TECTONIC Engineering & Survey Consultants P.C.

1279 ROUTE 300 NEWBURGH, NY 12550 Phone: (845) 567-6656 Fax: (845) 567-8703

|··**T**··Mobile∙

T-MOBILE NORTHEAST LLC. 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 PHONE: (860) 692-7100



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ISSUED BY	DATE

SITE INFORMATION

CT11883C CT883/SPRINT S. WINDSOR 59 MCGUIRE RD S. WINDSOR, CT 06074

SHEET TITLE

NOTES

SHEET NUMBER

A-7

GROUNDING NOTES

- 1. THE ENTIRE ELECTRICAL INSTALLATION SHALL BE GROUNDED AS REQUIRED BY ALL APPLICABLE CODES.
- 2. ALL GROUNDING WORK SHALL BE IN ACCORDANCE WITH T-MOBILE STANDARD PRACTICE.
- 3. ALL BUS CONNECTORS SHALL BE TWO—HOLE, LONG—BARREL TYPE COMPRESSION LUGS, T&B OR EQUAL, UNLESS OTHERWISE NOTED ON DRAWINGS. ALL LUGS SHALL BE ATTACHED TO BUSSES USING BOLTS, NUTS, AND LOCK WASHERS. NO WASHERS ARE ALLOWED BETWEEN THE ITEMS BEING GROUNDED.
- 4. ALL CONNECTORS SHALL BE CRIMPED USING HYDRAULIC CRIMPING TOOLS, T&B #TBM 8 OR EQUIVALENT.
- 5. ALL CONNECTIONS SHALL BE MADE TO BARE METAL. ALL PAINTED SURFACES SHALL BE FILED TO ENSURE PROPER CONTACT. NO WASHERS ARE ALLOWED BETWEEN THE ITEMS BEING GROUNDED. ALL CONNECTIONS ARE TO HAVE A NON-OXIDIZING AGENT APPLIED PRIOR TO INSTALLATION.
- 6. ALL COPPER BUSSES SHALL BE CLEANED, POLISHED, AND A NON-OXIDIZING AGENT APPLIED. NO FINGERPRINTS OR DISCOLORED COPPER WILL BE PERMITTED.
- 7. ALL BENDS SHALL BE AS SHALLOW AS POSSIBLE, WITH NO TURN SHORTER THAN AN 8-INCH NOMINAL RADIUS.
- 8. GROUNDING CONDUCTORS SHALL BE SOLID TINNED COPPER AND ANNEALED #2. ALL GROUNDING CONDUCTORS SHALL RUN THROUGH PVC SLEEVES WHEREVER CONDUCTORS RUN THROUGH WALLS, FLOORS, OR CEILINGS. IF CONDUCTORS MUST RUN THROUGH EMT, BOTH ENDS OF CONDUIT SHALL BE GROUNDED. SEAL BOTH ENDS OF CONDUIT WITH SILICONE CAULK.
- 9. GROUNDING SYSTEM RESISTANCE SHALL NOT EXCEED 10 OHMS. IF THE RESISTANCE VALUE IS EXCEEDED, NOTIFY THE PROJECT MANAGER FOR FURTHER INSTRUCTION ON METHODS FOR REDUCING THE RESISTANCE VALUE.
- 10. ALL ROOF TOP ANTENNA MOUNTS SHALL BE GROUNDED WITH A #2 GROUND WIRE CONNECTED TO THE NEAREST GROUND BUS. ALL CONNECTIONS ARE TO BE CAD—WELDED IF POSSIBLE.
- 11. UPON COMPLETION OF WORK, CONDUCT CONTINUITY, SHORT CIRCUIT, AND FALL OF POTENTIAL GROUNDING TESTS FOR APPROVAL. SUBMIT TEST REPORTS TO THE PROJECT MANAGER.
- 12. GROUNDING CONNECTION TO TRAVEL IN A DOWNWARD DIRECTION.
- 13. ALL EXPOSED #2 WIRE MUST BE TINN NOT BTW.
- 14. TECTONIC TAKES NO RESPONSIBILITY OR LIABILITY FOR THE GROUNDING SYSTEM AS SHOWN ON THIS SITE. THIS IS A STANDARD GROUNDING SYSTEM.

ENGINEERING **TECTONIC** Engineering & Survey Consultants P.C. 1279 ROUTE 300 NEWBURGH, NY 12550 T-MOBILE NORTHEAST LLC. 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 PHONE: (860) 692-7100 LANDLORD . CONSTRUCTION OPERATIONS SITE ACQ. PROJECT NUMBER DESIGNED BY 7061.CT11883C REV DATE REVISION 02/21/14 FOR COMMENT ISSUED BY DATE SITE INFORMATION CT11883C CT883/SPRINT S. WINDSOR 59 MCGUIRE RD S. WINDSOR, CT 06074 SHEET TITLE **NOTES** SHEET NUMBER A-8

CONFIGURATION 2

REFER TO LATEST T-MOBILE RF DATA SHEET FOR FINAL RF DESIGN & BOM.

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ORIGINAL SIZE IN INCHES



Date: March 06, 2014

Patrick Byrum Crown Castle 3530 Toringdon Way Suite 300 Charlotte, NC 28277 704.405.6532 Paul J. Ford and Company 250 E. Broad Street, Suite 600 Columbus, OH 43215 614.221.6679 jmeinerding@pjfweb.com

Subject: Structural Analysis Report

Carrier Designation: T-Mobile Co-Locate

Carrier Site Number: CT11883C

Carrier Site Name: CT883/Sprint S. Windsor

Crown Castle Designation: Crown Castle BU Number: 876327

Crown Castle Site Name: KINGS LOT
Crown Castle JDE Job Number: 260414
Crown Castle Work Order Number: 713158

Crown Castle Application Number: 217370 Rev. 1

Engineering Firm Designation: Paul J. Ford and Company Project Number: 37514-0050 R1

Site Data: 59 McGuire Road, SOUTH WINDSOR, Hartford County, CT

Latitude 41° 48' 10.77", Longitude -72° 37' 1.96"

150 Foot - Monopole Tower

Dear Patrick Byrum,

Paul J. Ford and Company is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 622261, in accordance with application 217370, revision 1.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC4.7: Modified Structure w/ Existing + Reserved + Proposed Equipment Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

Sufficient Capacity

MAR 0 6 2014

The structural analysis was performed for this tower in accordance with the requirements of the 2005 Connecticut Building Code and the TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 80 mph with no ice, 37.6 mph with 1 inch ice thickness and 50 mph under service loads.

All modifications and equipment proposed in this report shall be installed in accordance with the referenced drawings for the determined available structural capacity to be effective.

We at Paul J. Ford and Company appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:

Joey Meinerding, E.I. Structural Designer

tnxTower Report - version 6.1.4.1



Date: March 06, 2014

Patrick Byrum Crown Castle 3530 Toringdon Way Suite 300 Charlotte, NC 28277 704.405.6532 Paul J. Ford and Company 250 E. Broad Street, Suite 600 Columbus, OH 43215 614.221.6679 jmeinerding@pjfweb.com

Subject: Structural Analysis Report

Carrier Designation: T-Mobile Co-Locate

Carrier Site Number: CT11883C

Carrier Site Name: CT883/Sprint S. Windsor

Crown Castle Designation: Crown Castle BU Number: 876327

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Respectfully submitted by:

Joey Meinerding, E.I. Structural Designer

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tnxTower Output

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Additional Calculations

1) INTRODUCTION

This tower is a 150 ft. Monopole tower designed by ROHN in December of 1996. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-E.

2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of the 2005 Connecticut Building Code and the TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 80 mph with no ice, 37.6 mph with 1 inch ice thickness and 50 mph under service loads.

Table 1 - Proposed Antenna and Cable Information

Mounting Level (ft)	Elevation	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
		3	ericsson	ERICSSON AIR 21 B2A B4P w/ Mount Pipe			
138.0	138.0	3	ericsson	ERICSSON AIR 21 B4A B2P w/ Mount Pipe	1	1-5/8	
		3	ericsson	KRY 112 144/1			

Table 2 - Existing and Reserved Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Model Antenna Model		Number of Feed Lines	Feed Line Size (in)	Note		
	149.0	3	alcatel lucent	800MHz 2X50W RRH W/FILTER					
148.0	149.0	3	alcatel lucent	PCS 1900MHz 4x45W- 65MHz			1		
	148.0	1	tower mounts	Side Arm Mount [SO 102-					
	148.0	3	rfs celwave	APXVTM14-C-120 w/ Mount Pipe	1	5/8	2		
		148.0	3	alcatel lucent	TD-RRH8x20-25				
146.0			148.0	148.0	1	rfs celwave	APXV9ERR18-C-A20 w/ Mount Pipe		
		2	rfs celwave	APXVSPP18-C-A20 w/ Mount Pipe	3	1-1/4	1		
	146.0	1	tower mounts	Platform Mount [LP 501-1]					
		3	andrew	ADFD1820-9090B-XDM w/ Mount Pipe					
138.0	138.0	6	andrew	ONEBASE TWIN DUAL DUPLEX TMA			3		
		3	andrew	TMZXXX-6516-R2M w/ Mount Pipe					
		1	tower mounts	Platform Mount [LP 712-1]	12	1-5/8	1		

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antonna		Number of Feed Lines	Feed Line Size (in)	Note
		3	ericsson	RRUS 11			
124.0	124.0	1	tower mounts	Side Arm Mount [SO 102-3]			1
		1	kmw communications	AM-X-CD-14-65-00T-RET w/ Mount Pipe			
		1	kmw communications	AM-X-CD-16-65-00T-RET w/ Mount Pipe		3/8 3/4 1-1/4	1
400.0	122.0	6	powerwave technologies	7770.00 w/ Mount Pipe	1 2 12		
122.0		12	powerwave technologies	LGP2140X			
		1	powerwave technologies	P65-17-XLH-RR w/ Mount Pipe			
		1	raycap	DC6-48-60-18-8F			
		1	tower mounts	T-Arm Mount [TA 602-3]			
112.0	112.0	3	rfs celwave	APX18-206517-CT2 w/ Mount Pipe	6	1-5/8	1
		1	tower mounts	Pipe Mount [PM 601-3]			
13.0	14.0	1	lucent	KS24019-L112A	1	1/2	1
13.0	13.0	1	tower mounts			1/2	1
12.0	13.0	1	lucent	KS24019-L112A	1	1/2	1
12.0	12.0	12.0 1 tower mounts Pipe		Pipe Mount [PM 601-1]	l I	1/2	'

Notes:

- Existing Equipment Reserved Equipment Equipment To Be Removed 1) 2) 3)

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	FDH<, 07-11433G, 09/30/2009	2192521	CCISITES
4-POST-MODIFICATION INSPECTION	Vertical Solutions, 080627.06, 11/11/2008	2366960	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	Rohn, 34738SW, 12/18/1996	1620564	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Rohn, 34738SW, 12/15/1996	1619441	CCISITES
4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA	PJF, 37514-0050 BP, 02/04/2014	4451202	CCISITES

3.1) Analysis Method

tnxTower (version 6.1.4.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Monopole was reinforced in conformance with the referenced modification drawings.
- 5) We found the reinforcement from 30' to 90' to be ineffective. Therefore, we did not consider it in the analysis. The reinforcement from 0' to 15' was effective and was considered in the analysis.
- 6) In accordance with discussions with CCI Corporate Engineering: Based on the assumption that the monopole manufacturer (ROHN/PiRod) has designed the flange plates at splices to adequately develop the full capacity of the unreinforced shaft section using unpublished and/or proprietary methodologies, we are assuming that if our analysis shows that both the existing shaft and the existing flange bolts are at a usage capacity of 100% or less, then the existing flange plates are at a usage capacity of 100% or less and no additional analysis of the flange plate is required. This assumption only applies to the flange plates at 90' and 120'.
- 7) Monopole will be reinforced in conformance with the referenced proposed modification drawings.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford and Company should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	150 - 120	Pole	P24x1/4	1	-7.31	589.19	75.5	Pass
L2	120 - 90	Pole	30" x 0.375"	2	-12.04	1166.57	92.8	Pass
L3	90 - 78.75	Pole	36" x 0.375"	3	-14.11	1325.68	87.1	Pass
L4	78.75 - 60	Pole	RPS 36" x 0.51087"	4	-18.37	1634.98	90.2	Pass
L5	60 - 30	Pole	RPS 42" x 0.58495"	5	-27.98	2092.73	92.0	Pass
L6	30 - 13.75	Pole	RPS 42" x 0.71391"	6	-34.40	2768.33	84.3	Pass
L7	13.75 - 7.25	Pole	RPS 42" x 0.82344"	7	-37.14	3038.05	82.7	Pass
L8	7.25 - 0	Pole	RPS 42" x 0.78565"	8	-39.93	2905.35	92.7	Pass
							Summary	
						Pole (L2)	92.8	Pass
						Rating =	92.8	Pass

Table 5 - Tower Component Stresses vs. Capacity

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	91.6	Pass
1	Base Plate	0	63.5	Pass
1	Base Foundation Structural Steel	0	30.5	Pass
1	Base Foundation Soil Interaction	0	85.1	Pass
1	Flange Connection	30	91.2	Pass
1	Flange Connection	60	82.1	Pass
1,2	Flange Connection	90	92.8	Pass
1,2	Flange Connection	120	75.5	Pass

Structure Rating (max from all components) = 92.8%
--

Notes:

4.1) Recommendations

Install the proposed modifications per the referenced drawings.

¹⁾ See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

²⁾ See assumption #6.

APPENDIX A TNXTOWER OUTPUT

Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

- Tower is located in Hartford County, Connecticut. 1)
- Basic wind speed of 80.0 mph. 2)
- Nominal ice thickness of 1.00 in. 3)
- Ice density of 56 pcf. 4)
- A wind speed of 37.6 mph is used in combination with ice. 5)
- Temperature drop of 50 °F. 6)
- Deflections calculated using a wind speed of 50.0 mph. 7)
- A non-linear (P-delta) analysis was used. 8)
- Pressures are calculated at each section. 9)
- Stress ratio used in pole design is 1.333. 10)
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are 11) not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- Use Code Stress Ratios Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination

Distribute Leg Loads As Uniform Assume Legs Pinned

- Assume Rigid Index Plate
- Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
- Bypass Mast Stability Checks
- Use Azimuth Dish Coefficients
- Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Use TIA-222-G Tension Splice Capacity Exemption

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

Consider Feedline Torque Include Angle Block Shear Check

Poles

√ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

Pole Section Geometry

Section	Elevation	Section	Pole	Pole	Socket Length
		Length	Size	Grade	ft
	ft	ft			
L1	150.00-120.00	30.00	P24x1/4	A53-B-42	
				(42 ksi)	
L2	120.00-90.00	30.00	30" x 0.375"	A53-B-42	
				(42 ksi)	
L3	90.00-78.75	11.25	36" x 0.375"	A53-B-42	
				(42 ksi)	
L4	78.75-60.00	18.75	RPS 36" x	Reinf 35.89	
			0.51087"	ksi	
				(36 ksi)	
L5	60.00-30.00	30.00	RPS 42" x	Reinf 34.38	
			0.58495"	ksi	
	00 00 10 75	40.05	DD0 40"	(34 ksi)	
L6	30.00-13.75	16.25	RPS 42" x	Reinf 37.38	
			0.71391"	ksi	
1.7	40.75.7.05	0.50	DDO 40"	(37 ksi)	
L7	13.75-7.25	6.50	RPS 42" x	Reinf 35.66	
			0.82344"	ksi (20 ksi)	
1.0	7.05.0.00	7.05	DDC 40"	(36 ksi)	
L8	7.25-0.00	7.25	RPS 42" x	Reinf 35.71	

Section	Elevation ft	Section Length ft	Pole Size	Pole Grade	Socket Length ft
			0.78565"	ksi (36 ksi)	

Tower	Gusset	Gusset	Gusset Grade Adjust. Factor	Adjust.	Weight Mult.	Double Angle	Double Angle
Elevation	Area (per face)	Thickness	A_f	Factor A _r	Ü	Stitch Bolt Spacing Diagonals	Stitch Bolt Spacing Horizontals
ft	ft ²	in				in	in
L1 150.00-			1	1	1		
120.00							
L2 120.00-			1	1	1		
90.00							
L3 90.00-			1	1	1		
78.75							
L4 78.75-			1	1	1		
60.00							
L5 60.00-			1	1	1		
30.00							
L6 30.00-			1	1	1		
13.75							
L7 13.75-7.25			1	1	1		
L8 7.25-0.00			1	1	1		

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or	Allow Shield	Component Type	Placement	Total Number		C_AA_A	Weight
	Leg			ft			ft²/ft	plf
HB114-1-08U4-M5J(1	С	No	CaAa (Out Of	146.00 - 0.00	2	No Ice	0.00	1.08
1/4'')			Face)			1/2" Ice	0.00	2.33
						1" Ice	0.00	4.18
HB114-1-08U4-M5J(1	С	No	CaAa (Out Of	112.00 - 0.00	1	No Ice	0.00	1.08
1/4")			Face)			1/2" Ice	0.00	2.33
						1" Ice	0.00	4.18
HB114-1-08U4-M5J(1	С	No	CaAa (Out Of	146.00 - 112.00	1	No Ice	0.15	1.08
1/4'')			Face)			1/2" Ice	0.25	2.33
						1" Ice	0.35	4.18
HB058-M12-	С	No	CaAa (Out Of	146.00 - 0.00	1	No Ice	0.00	0.24
XXXF(5/8")			Face)			1/2" Ice	0.00	1.06
						1" Ice	0.00	2.49

AL7-50(1 5/8)	С	No	Inside Pole	138.00 - 0.00	9	No Ice	0.00	0.52
						1/2" Ice	0.00	0.52
						1" Ice	0.00	0.52
AL7-50(1 5/8)	С	No	CaAa (Out Of	138.00 - 0.00	4	No Ice	0.00	0.52
			Face)			1/2" Ice	0.00	2.02
						1" Ice	0.00	4.14
AL7-50(1 5/8)	С	No	CaAa (Out Of	138.00 - 0.00	1	No Ice	0.20	0.52
			Face)			1/2" Ice	0.30	2.02
						1" Ice	0.40	4.14
MLE Hybrid	С	No	CaAa (Out Of	138.00 - 0.00	1	No Ice	0.00	1.07
9Power/18Fiber RL 2(Face)			1/2" Ice	0.00	2.37
1 5/8) ******						1" Ice	0.00	4.28
FB-L98B-002-75000(С	No	Inside Pole	122.00 - 0.00	1	No Ice	0.00	0.06
3/8")	Ü	110	moldo i olo	122.00 0.00	•	1/2" Ice	0.00	0.06
3,3)						1" Ice	0.00	0.06
WR-VG86ST-BRD(С	No	Inside Pole	122.00 - 0.00	2	No Ice	0.00	0.59
3/4)	•				_	1/2" Ice	0.00	0.59
S,						1" Ice	0.00	0.59
2" Conduit	С	No	Inside Pole	122.00 - 0.00	1	No Ice	0.00	1.16
	-				•	1/2" Ice	0.00	1.16
						1" Ice	0.00	1.16
						. 100	0.00	0

Description	Face or	Allow Shield	Component Type	Placement	Total Number		C_AA_A	Weight
	Leg	Siliela	туре	ft	INUITIDEI		ft²/ft	plf
LDF6-50A(1-1/4")	С	No	Inside Pole	122.00 - 0.00	12	No Ice	0.00	0.66
,						1/2" Ice	0.00	0.66
						1" Ice	0.00	0.66

AVA7-50(1-5/8)	С	No	CaAa (Out Of	112.00 - 0.00	5	No Ice	0.00	0.70
			Face)			1/2" Ice	0.00	2.23
						1" Ice	0.00	4.38
AVA7-50(1-5/8)	С	No	CaAa (Out Of	112.00 - 0.00	1	No Ice	0.20	0.70
			Face)			1/2" Ice	0.30	2.23
						1" Ice	0.40	4.38

LDF4-50A(1/2")	С	No	Inside Pole	13.00 - 0.00	1	No Ice	0.00	0.15
						1/2" Ice	0.00	0.15
						1" Ice	0.00	0.15

LDF4-50A(1/2")	С	No	Inside Pole	12.00 - 0.00	1	No Ice	0.00	0.15
						1/2" Ice	0.00	0.15
*****						1" Ice	0.00	0.15
1 1/4" Flat	С	No	CaAa (Out Of	59.75 - 0.00	1	No Ice	0.21	0.00
Reinforcement	9	. 10	Face)	0.00	•	1/2" Ice	0.32	0.00
			. 230)			1" Ice	0.43	0.00
" Flat Reinforcement	С	No	CaAa (Out Of	80.25 - 60.25	1	No Ice	0.17	0.00
	-		Face)	22	·	1/2" Ice	0.28	0.00
			. 2.30)			1" Ice	0.39	0.00

Feed Line/Linear Appurtenances Section Areas

Tower	Tower	Face	A_R	A_F	$C_A A_A$	C_AA_A	Weight
Sectio	Elevation				In Face	Out Face	
n	ft		ft ²	ft ²	ft ²	ft ²	K
L1	150.00-120.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	7.532	0.26
L2	120.00-90.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	11.534	0.76
L3	90.00-78.75	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	4.716	0.30
L4	78.75-60.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	10.527	0.49
L5	60.00-30.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	18.108	0.79
L6	30.00-13.75	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	9.837	0.43
L7	13.75-7.25	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	3.935	0.17
L8	7.25-0.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	4.389	0.19

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Sectio	Tower Elevation	Face or	Ice Thickness	A_R	A_F	C _A A _A In Face	C _A A _A Out Face	Weight
n	ft	Leg	in	ft ²	ft ²	iii Face ft ²	ft ²	K
L1	150.00-120.00	Α	1.000	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00

Tower	Tower	Face	Ice	A_R	A_F	C_AA_A	C_AA_A	Weight
Sectio	Elevation	or	Thickness			In Face	Out Face	
n	ft	Leg	in	ft ²	ft ²	ft ²	ft ²	K
		С		0.000	0.000	0.000	16.332	0.95
L2	120.00-90.00	Α	1.000	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	23.534	2.23
L3	90.00-78.75	Α	1.000	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	9.550	0.91
L4	78.75-60.00	Α	1.000	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	22.138	1.52
L5	60.00-30.00	Α	1.000	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	36.719	2.44
L6	30.00-13.75	Α	1.000	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	19.948	1.32
L7	13.75-7.25	Α	1.000	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	7.979	0.53
L8	7.25-0.00	Α	1.000	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	8.900	0.59

Feed Line Center of Pressure

Section	Elevation	CP _X	CPz	CP _X	CPz
				Ice	Ice
	ft	in	in	in	in
L1	150.00-120.00	-0.29	0.17	-0.52	0.30
L2	120.00-90.00	-0.43	0.25	-0.74	0.43
L3	90.00-78.75	-0.48	0.28	-0.82	0.48
L4	78.75-60.00	-0.61	0.35	-1.06	0.61
L5	60.00-30.00	-0.67	0.39	-1.14	0.66
L6	30.00-13.75	-0.67	0.39	-1.14	0.66
L7	13.75-7.25	-0.67	0.39	-1.14	0.66
L8	7.25-0.00	-0.67	0.39	-1.14	0.66

Discrete Tower Loads

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustmen	Placement		C _A A _A Front	C _A A _A Side	Weight
	Leg		Lateral Vert ft	t	ft		ft ²	ft ²	K
			ft ft	0					
800MHz 2X50W RRH	Α	From Leg	2.00	0.000	148.00	No Ice	2.40	2.25	0.06
W/FILTER			0.00			1/2"	2.61	2.46	0.09
			1.00			Ice 1" Ice	2.83	2.68	0.11
800MHz 2X50W RRH	В	From Leg	2.00	0.000	148.00	No Ice	2.40	2.25	0.06
W/FILTER			0.00			1/2"	2.61	2.46	0.09
			1.00			Ice 1" Ice	2.83	2.68	0.11
800MHz 2X50W RRH	С	From Leg	2.00	0.000	148.00	No Ice	2.40	2.25	0.06
W/FILTER		•	0.00			1/2"	2.61	2.46	0.09
			1.00			Ice 1" Ice	2.83	2.68	0.11
PCS 1900MHz 4x45W-	Α	From Leg	2.00	0.000	148.00	No Ice	2.71	2.61	0.06
65MHz		· ·	0.00			1/2"	2.95	2.85	0.08
			1.00			Ice	3.20	3.09	0.11

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustmen	Placement		C _A A _A Front	C _A A _A Side	Weight
	Leg		Lateral Vert ft	t	ft		ft ²	ft ²	K
			ft ft	0					
PCS 1900MHz 4x45W-	В	From Leg	2.00	0.000	148.00	1" Ice No Ice	2.71	2.61	0.06
65MHz		Ü	0.00 1.00			1/2" Ice 1" Ice	2.95 3.20	2.85 3.09	0.08 0.11
PCS 1900MHz 4x45W-	С	From Leg	2.00	0.000	148.00	No Ice 1/2"	2.71 2.95	2.61	0.06
65MHz			0.00 1.00			Ice 1" Ice	3.20	2.85 3.09	0.08 0.11
Side Arm Mount [SO 102- 3]	С	None		0.000	148.00	No Ice 1/2"	3.00 3.48	3.00 3.48	0.08 0.11
*******						Ice 1" Ice	3.96	3.96	0.14
APXV9ERR18-C-A20 w/	Α	From Leg	4.00	0.000	146.00	No Ice	8.50	7.47	0.09
Mount Pipe			0.00 2.00			1/2" Ice 1" Ice	9.15 9.77	8.66 9.56	0.16 0.24
APXVSPP18-C-A20 w/	В	From Leg	4.00	0.000	146.00	No Ice	8.50	6.95	0.08
Mount Pipe			0.00 2.00			1/2" Ice 1" Ice	9.15 9.77	8.13 9.02	0.15 0.23
APXVSPP18-C-A20 w/ Mount Pipe	С	From Leg	4.00 0.00	0.000	146.00	No Ice 1/2"	8.50 9.15	6.95 8.13	0.08 0.15
·			2.00			Ice 1" Ice	9.77	9.02	0.23
APXVTM14-C-120 w/ Mount Pipe	Α	From Leg	4.00 0.00	0.000	146.00	No Ice 1/2"	7.13 7.66	4.96 5.75	0.08 0.13
·	_		2.00	0.000	4.40.00	Ice 1" Ice	8.18	6.47	0.19
APXVTM14-C-120 w/ Mount Pipe	В	From Leg	4.00 0.00 2.00	0.000	146.00	No Ice 1/2" Ice	7.13 7.66 8.18	4.96 5.75 6.47	0.08 0.13 0.19
						1" Ice			
APXVTM14-C-120 w/ Mount Pipe	С	From Leg	4.00 0.00	0.000	146.00	No Ice 1/2"	7.13 7.66	4.96 5.75	0.08 0.13
·	٨	From Log	2.00	0.000	146.00	Ice 1" Ice	8.18	6.47	0.19
TD-RRH8x20-25	Α	From Leg	4.00 0.00	0.000	146.00	No Ice 1/2"	4.72 5.01	1.70 1.92	0.07 0.10
			2.00			Ice 1" Ice	5.32	2.15	0.13
TD-RRH8x20-25	В	From Leg	4.00 0.00	0.000	146.00	No Ice 1/2"	4.72 5.01	1.70 1.92	0.07 0.10
			2.00			Ice 1" Ice	5.32	2.15	0.13
TD-RRH8x20-25	С	From Leg	4.00 0.00	0.000	146.00	No Ice 1/2"	4.72 5.01	1.70 1.92	0.07 0.10
			2.00			Ice 1" Ice	5.32	2.15	0.13
2.375" OD x 5' Mount Pipe	Α	From Leg	4.00 0.00	0.000	146.00	No Ice 1/2"	1.19 1.50	1.19 1.50	0.02 0.03
			2.00			Ice 1" Ice	1.81	1.81	0.04
2.375" OD x 5' Mount Pipe	В	From Leg	4.00 0.00	0.000	146.00	No Ice 1/2"	1.19 1.50	1.19 1.50	0.02 0.03
			2.00			Ice 1" Ice	1.81	1.81	0.04
2.375" OD x 5' Mount Pipe	С	From Leg	4.00 0.00	0.000	146.00	No Ice 1/2"	1.19 1.50	1.19 1.50	0.02 0.03
			2.00			Ice 1" Ice	1.81	1.81	0.04
Platform Mount [LP 501-1]	С	None		0.000	146.00	No Ice 1/2"	32.04 45.28	32.04 45.28	0.98 1.28
						Ice	58.51	58.51	1.57

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			Vert ft ft ft	0	ft		ft ²	ft ²	К
*******			- n			1" Ice			
ERICSSON AIR 21 B2A B4P w/ Mount Pipe	Α	From Leg	4.00 0.00 0.00	0.000	138.00	No Ice 1/2" Ice 1" Ice	6.83 7.35 7.86	5.64 6.48 7.26	0.11 0.17 0.23
ERICSSON AIR 21 B2A B4P w/ Mount Pipe	В	From Leg	4.00 0.00 0.00	0.000	138.00	No Ice 1/2" Ice 1" Ice	6.83 7.35 7.86	5.64 6.48 7.26	0.11 0.17 0.23
ERICSSON AIR 21 B2A B4P w/ Mount Pipe	С	From Leg	4.00 0.00 0.00	0.000	138.00	No Ice 1/2" Ice 1" Ice	6.83 7.35 7.86	5.64 6.48 7.26	0.11 0.17 0.23
ERICSSON AIR 21 B4A B2P w/ Mount Pipe	Α	From Leg	4.00 0.00 0.00	0.000	138.00	No Ice 1/2" Ice 1" Ice	6.83 7.35 7.86	5.64 6.48 7.26	0.11 0.17 0.23
ERICSSON AIR 21 B4A B2P w/ Mount Pipe	В	From Leg	4.00 0.00 0.00	0.000	138.00	No Ice 1/2" Ice 1" Ice	6.83 7.35 7.86	5.64 6.48 7.26	0.11 0.17 0.23
ERICSSON AIR 21 B4A B2P w/ Mount Pipe	С	From Leg	4.00 0.00 0.00	0.000	138.00	No Ice 1/2" Ice 1" Ice	6.83 7.35 7.86	5.64 6.48 7.26	0.11 0.17 0.23
KRY 112 144/1	Α	From Leg	4.00 0.00 0.00	0.000	138.00	No Ice 1/2" Ice 1" Ice	0.41 0.50 0.59	0.20 0.27 0.35	0.01 0.01 0.02
KRY 112 144/1	В	From Leg	4.00 0.00 0.00	0.000	138.00	No Ice 1/2" Ice 1" Ice	0.41 0.50 0.59	0.20 0.27 0.35	0.01 0.01 0.02
KRY 112 144/1	С	From Leg	4.00 0.00 0.00	0.000	138.00	No Ice 1/2" Ice 1" Ice	0.41 0.50 0.59	0.20 0.27 0.35	0.01 0.01 0.02
Platform Mount [LP 712-1]	С	None		0.000	138.00	No Ice 1/2" Ice 1" Ice	24.53 29.94 35.35	24.53 29.94 35.35	1.34 1.65 1.96
RRUS 11	Α	From Leg	4.00 0.00 0.00	0.000	124.00	No Ice 1/2" Ice 1" Ice	3.25 3.49 3.74	1.37 1.55 1.74	0.05 0.07 0.10
RRUS 11	В	From Leg	4.00 0.00 0.00	0.000	124.00	No Ice 1/2" Ice 1" Ice	3.25 3.49 3.74	1.37 1.55 1.74	0.05 0.07 0.10
RRUS 11	С	From Leg	4.00 0.00 0.00	0.000	124.00	No Ice 1/2" Ice 1" Ice	3.25 3.49 3.74	1.37 1.55 1.74	0.05 0.07 0.10
Side Arm Mount [SO 102-3]	С	None		0.000	124.00	No Ice 1/2" Ice 1" Ice	3.00 3.48 3.96	3.00 3.48 3.96	0.08 0.11 0.14
(2) 7770.00 w/ Mount Pipe	Α	From Leg	4.00 0.00 0.00	0.000	122.00	No Ice 1/2" Ice	6.12 6.63 7.13	4.25 5.01 5.71	0.06 0.10 0.16
(2) 7770.00 w/ Mount Pipe	В	From Leg	4.00	0.000	122.00	1" Ice No Ice	6.12	4.25	0.06

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	٥	ft		ft ²	ft ²	K
			0.00			1/2"	6.63	5.01	0.10
			0.00			Ice 1" Ice	7.13	5.71	0.16
(2) 7770.00 w/ Mount Pipe	С	From Leg	4.00	0.000	122.00	No Ice	6.12	4.25	0.06
			0.00			1/2"	6.63	5.01	0.10
			0.00			Ice	7.13	5.71	0.16
AM-X-CD-14-65-00T-RET	Α	From Leg	4.00	0.000	122.00	1" Ice No Ice	5.74	4.02	0.05
w/ Mount Pipe		1 Tolli Log	0.00	0.000	122.00	1/2"	6.20	4.63	0.10
W Would he			0.00			Ice	6.66	5.28	0.15
						1" Ice			
P65-17-XLH-RR w/ Mount	В	From Leg	4.00	0.000	122.00	No Ice	11.82	9.06	0.09
Pipe			0.00			1/2"	12.59	10.62	0.18
			0.00			Ice	13.38	12.21	0.28
AM-X-CD-16-65-00T-RET	С	From Leg	4.00	0.000	122.00	1" Ice No Ice	8.50	6.30	0.07
w/ Mount Pipe	O	1 Tolli Log	0.00	0.000	122.00	1/2"	9.15	7.48	0.14
W Would I Ipo			0.00			Ice	9.77	8.37	0.21
						1" Ice			
(4) LGP2140X	Α	From Leg	4.00	0.000	122.00	No Ice	1.26	0.38	0.01
			0.00			1/2"	1.42	0.49	0.02
			0.00			lce 1" lce	1.58	0.62	0.03
(4) LGP2140X	В	From Leg	4.00	0.000	122.00	No Ice	1.26	0.38	0.01
(4) EGI 2140X	В	1 Tom Log	0.00	0.000	122.00	1/2"	1.42	0.49	0.02
			0.00			Ice	1.58	0.62	0.03
						1" Ice			
(4) LGP2140X	С	From Leg	4.00	0.000	122.00	No Ice	1.26	0.38	0.01
			0.00			1/2"	1.42	0.49	0.02
			0.00			Ice 1" Ice	1.58	0.62	0.03
DC6-48-60-18-8F	Α	From Leg	4.00	0.000	122.00	No Ice	2.57	2.57	0.02
			0.00			1/2"	2.80	2.80	0.04
			0.00			Ice	3.04	3.04	0.07
						1" Ice			
T-Arm Mount [TA 602-3]	С	None		0.000	122.00	No Ice	11.59	11.59	0.77
						1/2" Ice	15.44 19.29	15.44 19.29	0.99 1.21
						1" Ice	15.25	13.23	1.21

APX18-206517-CT2 w/	Α	From Leg	1.00	0.000	112.00	No Ice	5.36	4.73	0.05
Mount Pipe			0.00			1/2"	5.91	5.90	0.09
			0.00			Ice 1" Ice	6.44	6.79	0.15
APX18-206517-CT2 w/	В	From Leg	1.00	0.000	112.00	No Ice	5.36	4.73	0.05
Mount Pipe		i ioni Log	0.00	0.000	112.00	1/2"	5.91	5.90	0.09
·			0.00			Ice	6.44	6.79	0.15
	_					1" Ice			
APX18-206517-CT2 w/	С	From Leg	1.00	0.000	112.00	No Ice	5.36	4.73	0.05
Mount Pipe			0.00 0.00			1/2" Ice	5.91 6.44	5.90 6.79	0.09 0.15
			0.00			1" Ice	0.44	0.73	0.15
Pipe Mount [PM 601-3]	С	None		0.000	112.00	No Ice	4.39	4.39	0.20
						1/2"	5.48	5.48	0.24
						Ice	6.57	6.57	0.28
********						1" Ice			
KS24019-L112A	Α	From Leg	1.00	0.000	13.00	No Ice	0.16	0.16	0.01
NOZTO IO ETIZA	А	. Tom Log	0.00	0.000	10.00	1/2"	0.10	0.10	0.01
			1.00			Ice	0.30	0.30	0.01
						1" Ice			
Pipe Mount [PM 601-1]	Α	None		0.000	13.00	No Ice	3.00	0.90	0.07
						1/2" Ice	3.74 4.48	1.12 1.34	0.08 0.09
						1" Ice	7.70	1.04	0.08
						1 100			

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	o	ft		ft ²	ft ²	К
**************************************	Α	From Leg	1.00 0.00 1.00	0.000	12.00	No Ice 1/2" Ice 1" Ice	0.16 0.22 0.30	0.16 0.22 0.30	0.01 0.01 0.01
Pipe Mount [PM 601-1]	Α	None		0.000	12.00	No Ice 1/2" Ice 1" Ice	3.00 3.74 4.48	0.90 1.12 1.34	0.07 0.08 0.09
**************************************	Α	None		0.000	30.00	No Ice 1/2" Ice 1" Ice	1.93 2.18 2.45	1.05 1.26 1.48	0.08 0.09 0.10
Bridge Stiffener C8x18.7 (57" x 6")	Α	None		0.000	60.00	No Ice 1/2" Ice 1" Ice	4.45 4.86 5.29	2.14 2.48 2.84	0.19 0.21 0.24
Bridge Stiffener C6x13 (45" x 6")	Α	None		0.000	90.00	No Ice 1/2" Ice 1" Ice	2.66 2.96 3.30	1.56 1.84 2.12	0.10 0.12 0.14
Bridge Stiffener (106" x 15" x 1.25")	Α	None		0.000	30.00	No Ice 1/2" Ice 1" Ice	15.48 16.25 17.04	1.84 2.84 3.85	0.63 0.69 0.75
Bridge Stiffener (106" x 16" x 1.25")	Α	None		0.000	60.00	No Ice 1/2" Ice 1" Ice	16.49 17.28 18.09	1.84 2.84 3.85	0.67 0.73 0.80

Tower Pressures - No Ice

 $G_H = 1.690$

Section	Z	K_Z	q_z	A_G	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	C_AA_A
Elevation					а				%	In	Out
					С					Face	Face
ft	ft		psf	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
L1 150.00-	135.00	1.496	25	60.000	Α	0.000	60.000	60.000	100.00	0.000	0.000
120.00					В	0.000	60.000		100.00	0.000	0.000
					С	0.000	60.000		100.00	0.000	7.532
L2 120.00-	105.00	1.392	23	75.000	Α	0.000	75.000	75.000	100.00	0.000	0.000
90.00					В	0.000	75.000		100.00	0.000	0.000
					С	0.000	75.000		100.00	0.000	11.534
L3 90.00-	84.38	1.308	21	33.750	Α	0.000	33.750	33.750	100.00	0.000	0.000
78.75					В	0.000	33.750		100.00	0.000	0.000
					С	0.000	33.750		100.00	0.000	4.716
L4 78.75-	69.38	1.237	20	56.250	Α	0.000	56.250	56.250	100.00	0.000	0.000
60.00					В	0.000	56.250		100.00	0.000	0.000
					С	0.000	56.250		100.00	0.000	10.527
L5 60.00-	45.00	1.093	18	105.00	Α	0.000	105.000	105.000	100.00	0.000	0.000
30.00				0	В	0.000	105.000		100.00	0.000	0.000
					С	0.000	105.000		100.00	0.000	18.108
L6 30.00-	21.88	1	16	56.875	Α	0.000	56.875	56.875	100.00	0.000	0.000
13.75					В	0.000	56.875		100.00	0.000	0.000
					С	0.000	56.875		100.00	0.000	9.837
L7 13.75-7.25	10.50	1	16	22.750	Α	0.000	22.750	22.750	100.00	0.000	0.000

Section Elevation	Z	Kz	q_z	A_G	F a	A_F	A_R	A_{leg}	Leg %	C _A A _A In	C_AA_A Out
ft	ft		psf	ft²	c e	ft ²	ft²	ft²		Face ft²	Face ft²
					В	0.000	22.750		100.00	0.000	0.000
					С	0.000	22.750		100.00	0.000	3.935
L8 7.25-0.00	3.63	1	16	25.375	Α	0.000	25.375	25.375	100.00	0.000	0.000
					В	0.000	25.375		100.00	0.000	0.000
					С	0.000	25.375		100.00	0.000	4.389

Tower Pressure - With Ice

 $G_H = 1.690$

Section	Z	K_Z	q_z	t_Z	A_G	F	A_F	A_R	A _{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation	_	- 2	72	-2	0	а		/\	- neg	%	În	Out
						С					Face	Face
ft	ft		psf	in	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
L1 150.00-	135.00	1.496	5	1.00	65.000	Α	0.000	65.000	65.000	100.00	0.000	0.000
120.00						В	0.000	65.000		100.00	0.000	0.000
						С	0.000	65.000		100.00	0.000	16.332
L2 120.00-	105.00	1.392	5	1.00	80.000	Α	0.000	80.000	80.000	100.00	0.000	0.000
90.00						В	0.000	80.000		100.00	0.000	0.000
						С	0.000	80.000		100.00	0.000	23.534
L3 90.00-78.75	84.38	1.308	5	1.00	35.625	Α	0.000	35.625	35.625	100.00	0.000	0.000
						В	0.000	35.625		100.00	0.000	0.000
						С	0.000	35.625		100.00	0.000	9.550
L4 78.75-60.00	69.38	1.237	4	1.00	59.375	Α	0.000	59.375	59.375	100.00	0.000	0.000
						В	0.000	59.375		100.00	0.000	0.000
						С	0.000	59.375		100.00	0.000	22.138
L5 60.00-30.00	45.00	1.093	4	1.00	110.000	Α	0.000	110.000	110.000	100.00	0.000	0.000
						В	0.000	110.000		100.00	0.000	0.000
						С	0.000	110.000		100.00	0.000	36.719
L6 30.00-13.75	21.88	1	4	1.00	59.583	Α	0.000	59.583	59.583	100.00	0.000	0.000
						В	0.000	59.583		100.00	0.000	0.000
						С	0.000	59.583		100.00	0.000	19.948
L7 13.75-7.25	10.50	1	4	1.00	23.833	Α	0.000	23.833	23.833	100.00	0.000	0.000
						В	0.000	23.833		100.00	0.000	0.000
						С	0.000	23.833		100.00	0.000	7.979
L8 7.25-0.00	3.63	1	4	1.00	26.583	Α	0.000	26.583	26.583	100.00	0.000	0.000
						В	0.000	26.583		100.00	0.000	0.000
						С	0.000	26.583		100.00	0.000	8.900

Tower Pressure - Service

 $G_H = 1.690$

Section	Z	K_Z	q_z	A_{G}	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation					а				%	In	Out
				_	С	_	_	_		Face	Face
ft	ft		psf	ft ²	е	ft ²	ft ²	ft^2		ft ²	ft ²
L1 150.00-	135.00	1.496	10	60.000	Α	0.000	60.000	60.000	100.00	0.000	0.000
120.00					В	0.000	60.000		100.00	0.000	0.000
					С	0.000	60.000		100.00	0.000	7.532
L2 120.00-	105.00	1.392	9	75.000	Α	0.000	75.000	75.000	100.00	0.000	0.000
90.00					В	0.000	75.000		100.00	0.000	0.000
					С	0.000	75.000		100.00	0.000	11.534
L3 90.00-	84.38	1.308	8	33.750	Α	0.000	33.750	33.750	100.00	0.000	0.000
78.75					В	0.000	33.750		100.00	0.000	0.000
					С	0.000	33.750		100.00	0.000	4.716
L4 78.75-	69.38	1.237	8	56.250	Α	0.000	56.250	56.250	100.00	0.000	0.000
60.00					В	0.000	56.250		100.00	0.000	0.000
					С	0.000	56.250		100.00	0.000	10.527
L5 60.00-	45.00	1.093	7	105.00	Α	0.000	105.000	105.000	100.00	0.000	0.000

Section	Z	Kz	q _z	A_{G}	F	A_F	A_R	A _{leg}	Leg	C_AA_A	C_AA_A
Elevation					а				%	In	Out
				_	С	_		_		Face	Face
ft	ft		psf	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
30.00				0	В	0.000	105.000		100.00	0.000	0.000
					С	0.000	105.000		100.00	0.000	18.108
L6 30.00-	21.88	1	6	56.875	Α	0.000	56.875	56.875	100.00	0.000	0.000
13.75					В	0.000	56.875		100.00	0.000	0.000
					С	0.000	56.875		100.00	0.000	9.837
L7 13.75-7.25	10.50	1	6	22.750	Α	0.000	22.750	22.750	100.00	0.000	0.000
					В	0.000	22.750		100.00	0.000	0.000
					С	0.000	22.750		100.00	0.000	3.935
L8 7.25-0.00	3.63	1	6	25.375	Α	0.000	25.375	25.375	100.00	0.000	0.000
					В	0.000	25.375		100.00	0.000	0.000
					С	0.000	25.375		100.00	0.000	4.389

Load Combinations

Comb.	Description
No.	Zeecs.ip.de.i.
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

Maximum Member Forces

Sectio n	Elevation ft	Component Type	Condition	Gov. Load	Force	Major Axis Moment	Minor Axis Moment
No.				Comb.	K	kip-ft	kip-ft
L1	150 - 120	Pole	Max Tension	11	0.00	0	0
			Max Compression	14	-14 96	1	-1

Max. My	Sectio n	Elevation ft	Component Type	Condition	Gov. Load	Force	Major Axis Moment	Minor Axis Moment
Max Mx		7.	турс			K		
Max. My	140.			Max Mx				<u> </u>
Max. Vy								
Max Max								
L2				,				
L2						12.00	O	
Max. Compression	12	120 - 90	Pole	•		0.00	0	
Max, My		120 00	1 010					
Max My								
Max. Vy								
Max Ny								
L3				,				
L3						13.03	O	
Max. Compression	13	90 - 78 75	Pole	•		0.00	0	
Max. My	LO	30 - 70.73	1 010					
Max. My								
Max. Vy S 16.88 -835 -1								
L4 78.75 - 60 Pole Max Torque 9								
L4								
L4						10.02	O	
Max. Compression	1.4	78 75 - 60	Pole			0.00	0	
Max. My	L4	70.73 - 00	1 016					
Max. My				'				
L5								
L5								
L5								
L5						10.29	U	
Max. Compression	1.5	60 20	Dolo			0.00	0	
Max. Mx	LJ	00 - 30	Fole					
Max. My				•				
Max. Vy								
Max. Vx								
Max. Torque								
L6 30 - 13.75 Pole Max Tension 1 0.00 0 0 Max. Compression 14 -52.76 10 -6 Max. Mx 11 -34.40 2137 0 Max. My 8 -34.40 1 -2130 Max. Vy 5 22.85 -2134 -2 Max. Vx 8 22.80 1 -2130 Max. Torque 5 0 0 0 L7 13.75 - 7.25 Pole Max Tension 1 0.00 0 0 Max. Compression 14 -56.19 11 -6 7 11 -2284 -2 7 7 7 7 7 7 7 7 <td></td> <td></td> <td></td> <td></td> <td></td> <td>21.30</td> <td>U</td> <td></td>						21.30	U	
Max. Compression	1.6	20 12 75	Dolo	•		0.00	0	
Max. Mx	Lo	30 - 13.75	Pole					
Max. My				•				
Max. Vy								
Max. Vx 8 22.80 1 -2130 Max. Torque 5 0 0								
Max. Torque 5 0 0 0 0 0 0 0 0 0								
L7 13.75 - 7.25 Pole Max Tension 1 0.00 0 0 0 Max. Compression 14 -56.19 11 -6 Max. Mx 11 -37.14 2288 0 Max. My 8 -37.14 1 -2280 Max. Vy 5 23.41 -2284 -2 Max. Vx 8 23.36 1 -2280 Max. Torque 5 0 Max Tension 1 0.00 0 0 0 Max. Compression 14 -59.67 11 -7 Max. Mx 11 -39.93 2459 0 Max. My 8 -39.93 1 -2451 Max. Vy 5 23.80 -2455 -2						22.00	ı	
Max. Compression 14 -56.19 11 -6	17	12 75 7 25	Dolo	•		0.00	0	
Max. Mx 11 -37.14 2288 0 Max. My 8 -37.14 1 -2280 Max. Vy 5 23.41 -2284 -2 Max. Vx 8 23.36 1 -2280 Max. Torque 5 L8 7.25 - 0 Pole Max Tension 1 0.00 0 0 Max. Compression 14 -59.67 11 -7 Max. Mx 11 -39.93 2459 0 Max. My 8 -39.93 1 -2451 Max. Vy 5 23.80 -2455 -2	L/	13.75 - 7.25	Pole					
L8 7.25 - 0 Pole Max. My Max. Vx Max. Vx Max. Vx Max. Torque Max. Compression Max. Compression Max. Compression Max. Mx								
Max. Vy 5 23.41 -2284 -2 Max. Vx 8 23.36 1 -2280 Max. Torque 5 0 L8 7.25 - 0 Pole Max Tension 1 0.00 0 0 Max. Compression 14 -59.67 11 -7 Max. Mx 11 -39.93 2459 0 Max. My 8 -39.93 1 -2451 Max. Vy 5 23.80 -2455 -2								
Max. Vx 8 23.36 1 -2280 Max. Torque 5 0 L8 7.25 - 0 Pole Max Tension 1 0.00 0 0 Max. Compression 14 -59.67 11 -7 Max. Mx 11 -39.93 2459 0 Max. My 8 -39.93 1 -2451 Max. Vy 5 23.80 -2455 -2								
Max. Torque 5 L8 7.25 - 0 Pole Max Tension 1 0.00 0 0 Max. Compression 14 -59.67 11 -7 Max. Mx 11 -39.93 2459 0 Max. My 8 -39.93 1 -2451 Max. Vy 5 23.80 -2455 -2								
L8 7.25 - 0 Pole Max Tension 1 0.00 0 0 Max. Compression 14 -59.67 11 -7 Max. Mx 11 -39.93 2459 0 Max. My 8 -39.93 1 -2451 Max. Vy 5 23.80 -2455 -2						∠3.30	1	
Max. Compression 14 -59.67 11 -7 Max. Mx 11 -39.93 2459 0 Max. My 8 -39.93 1 -2451 Max. Vy 5 23.80 -2455 -2	1.0	7.05 0	Dela			0.00	0	
Max. Mx 11 -39.93 2459 0 Max. My 8 -39.93 1 -2451 Max. Vy 5 23.80 -2455 -2	Lδ	7.25 - 0	Pole					
Max. My 8 -39.93 1 -2451 Max. Vy 5 23.80 -2455 -2								
Max. Vy 5 23.80 -2455 -2								
Max. Vx 8 23.75 1 -2451								
						23.75	1	
Max. Torque 5				Max. Lorque	5			U

Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	14	59.67	-0.00	0.00
	Max. H _x	11	39.94	23.79	0.01
	Max. H _z	2	39.94	0.01	23.74
	Max. M _x	2	2449	0.01	23.74
	Max. M _z	5	2455	-23.79	-0.01

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
	Max. Torsion	11	0	23.79	0.01
	Min. Vert	11	39.94	23.79	0.01
	Min. H _x	5	39.94	-23.79	-0.01
	Min. H _z	8	39.94	-0.01	-23.74
	Min. M _x	8	-2451	-0.01	-23.74
	Min. M _z	11	-2459	23.79	0.01
	Min. Torsion	5	0	-23.79	-0.01

Tower Mast Reaction Summary

Load Combination	Vertical	Shear _x	Shearz	Overturning Moment, M _x	Overturning Moment, M _z	Torque
Combination	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	39.94	-0.00	0.00	1	2	C
Dead+Wind 0 deg - No Ice	39.94	-0.01	-23.74	-2449	3	C
Dead+Wind 30 deg - No Ice	39.94	11.89	-20.55	-2120	-1226	C
Dead+Wind 60 deg - No Ice	39.94	20.60	-11.86	-1223	-2126	C
Dead+Wind 90 deg - No Ice	39.94	23.79	0.01	2	-2455	Č
Dead+Wind 120 deg - No Ice	39.94	20.61	11.88	1227	-2127	C
Dead+Wind 150 deg - No Ice	39.94	11.91	20.56	2124	-1228	Č
Dead+Wind 180 deg - No Ice	39.94	0.01	23.74	2451	1	Ċ
Dead+Wind 210 deg - No Ice	39.94	-11.89	20.55	2123	1230	(
Dead+Wind 240 deg - No Ice	39.94	-20.60	11.86	1225	2130	(
Dead+Wind 270 deg - No Ice	39.94	-23.79	-0.01	0	2459	(
Dead+Wind 300 deg - No Ice	39.94	-20.61	-11.88	-1225	2131	(
Dead+Wind 330 deg - No Ice	39.94	-11.91	-20.56	-2122	1232	(
Dead+Ice+Temp	59.67	0.00	-0.00	7	11	(
Dead+Wind 0	59.67	0.00	-6.83	-722	11	(
deg+Ice+Temp						
Dead+Wind 30	59.67	3.42	-5.92	-625	-354	(
deg+Ice+Temp						
Dead+Wind 60	59.67	5.92	-3.42	-358	-621	(
deg+Ice+Temp						
Dead+Wind 90	59.67	6.84	-0.00	7	-718	(
deg+Ice+Temp						
Dead+Wind 120	59.67	5.92	3.42	371	-621	(
deg+Ice+Temp						
Dead+Wind 150	59.67	3.42	5.92	638	-353	(
deg+Ice+Temp						
Dead+Wind 180	59.67	-0.00	6.83	736	12	(
deg+Ice+Temp						
Dead+Wind 210	59.67	-3.42	5.92	638	377	(
deg+Ice+Temp						
Dead+Wind 240	59.67	-5.92	3.42	372	644	(
deg+Ice+Temp						
Dead+Wind 270	59.67	-6.84	0.00	7	741	(
deg+Ice+Temp						
Dead+Wind 300	59.67	-5.92	-3.42	-358	643	(
deg+Ice+Temp						
Dead+Wind 330	59.67	-3.42	-5.92	-625	376	(
deg+Ice+Temp						
Dead+Wind 0 deg - Service	39.94	-0.00	-9.27	-956	2	(
Dead+Wind 30 deg - Service	39.94	4.64	-8.03	-828	-478	(
Dead+Wind 60 deg - Service	39.94	8.05	-4.63	-477	-830	(
Dead+Wind 90 deg - Service	39.94	9.29	0.00	2	-958	(
Dead+Wind 120 deg -	39.94	8.05	4.64	480	-830	
Service						
Dead+Wind 150 deg -	39.94	4.65	8.03	831	-479	(
Service						
Dead+Wind 180 deg -	39.94	0.00	9.27	959	1	(
Service						
Dead+Wind 210 deg -	39.94	-4.64	8.03	830	482	
Service						
Dead+Wind 240 deg -	39.94	-8.05	4.63	480	833	(
Service						

Load Combination	Vertical	Shear _x	Shearz	Overturning Moment, M _x	Overturning Moment, M _z	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 270 deg - Service	39.94	-9.29	-0.00	1	962	0
Dead+Wind 300 deg - Service	39.94	-8.05	-4.64	-478	834	0
Dead+Wind 330 deg - Service	39.94	-4.65	-8.03	-828	483	0

Solution Summary

	Cun	n of Applied Force	20		Sum of Reactio	no	
Load	PX Sun	PY PY	PZ	PX	PY	ns PZ	% Error
Comb.	K	K	K	K	K	K	% ⊑ 1101
	0.00	-39.94	0.00	0.00	39.94	-0.00	0.000%
1	-0.00 -0.01	-39.94 -39.94	-23.74	0.00	39.94 39.94	-0.00 23.74	0.000%
2 3		-39.94 -39.94		-11.89		23.74	0.010%
	11.89		-20.55		39.94		
4	20.60	-39.94	-11.86	-20.60	39.94	11.86	0.000%
5	23.79	-39.94	0.01	-23.79	39.94	-0.01	0.004%
6	20.61	-39.94	11.88	-20.61	39.94	-11.88	0.000%
7	11.91	-39.94	20.56	-11.91	39.94	-20.56	0.000%
8	0.01	-39.94	23.74	-0.01	39.94	-23.74	0.010%
9	-11.89	-39.94	20.55	11.89	39.94	-20.55	0.000%
10	-20.60	-39.94	11.86	20.60	39.94	-11.86	0.000%
11	-23.79	-39.94	-0.01	23.79	39.94	0.01	0.010%
12	-20.61	-39.94	-11.88	20.61	39.94	11.88	0.000%
13	-11.91	-39.94	-20.56	11.91	39.94	20.56	0.000%
14	0.00	-59.67	0.00	-0.00	59.67	0.00	0.001%
15	0.00	-59.67	-6.83	-0.00	59.67	6.83	0.000%
16	3.42	-59.67	-5.92	-3.42	59.67	5.92	0.000%
17	5.92	-59.67	-3.42	-5.92	59.67	3.42	0.000%
18	6.84	-59.67	-0.00	-6.84	59.67	0.00	0.000%
19	5.92	-59.67	3.42	-5.92	59.67	-3.42	0.000%
20	3.42	-59.67	5.92	-3.42	59.67	-5.92	0.000%
21	-0.00	-59.67	6.83	0.00	59.67	-6.83	0.000%
22	-3.42	-59.67	5.92	3.42	59.67	-5.92	0.000%
23	-5.92	-59.67	3.42	5.92	59.67	-3.42	0.000%
24	-6.84	-59.67	0.00	6.84	59.67	-0.00	0.000%
25	-5.92	-59.67	-3.42	5.92	59.67	3.42	0.000%
26	-3.42	-59.67	-5.92	3.42	59.67	5.92	0.000%
27	-0.00	-39.94	-9.27	0.00	39.94	9.27	0.005%
28	4.64	-39.94	-8.03	-4.64	39.94	8.03	0.002%
29	8.05	-39.94	-4.63	-8.05	39.94	4.63	0.002%
30	9.29	-39.94	0.00	-9.29	39.94	-0.00	0.005%
31	8.05	-39.94	4.64	-8.05	39.94	-4.64	0.002%
32	4.65	-39.94	8.03	-4.65	39.94	-8.03	0.002%
33	0.00	-39.94	9.27	-0.00	39.94	-9.27	0.005%
34	-4.64	-39.94	8.03	4.64	39.94	-8.03	0.002%
35	-8.05	-39.94	4.63	8.05	39.94	-4.63	0.002%
36	-9.29	-39.94	-0.00	9.29	39.94	0.00	0.005%
37	-8.05	-39.94	-4.64	8.05	39.94	4.64	0.002%
38	-4.65	-39.94	-8.03	4.65	39.94	8.03	0.002%

Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination	_	of Cycles	Tolerance	Tolerance
1	Yes	6	0.0000001	0.00000001
2	Yes	13	0.00013163	0.00014455
3	Yes	17	0.0000001	0.00012844
4	Yes	17	0.0000001	0.00012627
5	Yes	14	0.00005729	0.00006678
6	Yes	17	0.0000001	0.00012853
7	Yes	17	0.0000001	0.00012811

8	Yes	13	0.00013163	0.00014618
9	Yes	17	0.0000001	0.00012686
10	Yes	17	0.0000001	0.00012934
11	Yes	13	0.00013160	0.00014836
12	Yes	17	0.0000001	0.00012779
13	Yes	17	0.0000001	0.00012790
14	Yes	9	0.0000001	0.00004136
15	Yes	16	0.0000001	0.00008228
16	Yes	16	0.0000001	0.00009155
17	Yes	16	0.0000001	0.00009141
18	Yes	16	0.0000001	0.00008191
19	Yes	16	0.0000001	0.00009295
20	Yes	16	0.0000001	0.00009308
21	Yes	16	0.0000001	0.00008383
22	Yes	16	0.0000001	0.00009542
23	Yes	16	0.0000001	0.00009565
24	Yes	16	0.0000001	0.00008438
25	Yes	16	0.0000001	0.00009401
26	Yes	16	0.0000001	0.00009381
27	Yes	13	0.00013512	0.00006884
28	Yes	14	0.0000001	0.00009981
29	Yes	14	0.0000001	0.00009454
30	Yes	13	0.00013513	0.00006934
31	Yes	14	0.0000001	0.00009916
32	Yes	14	0.0000001	0.00009840
33	Yes	13	0.00013512	0.00006905
34	Yes	14	0.0000001	0.00009588
35	Yes	14	0.0000001	0.00010160
36	Yes	13	0.00013512	0.00006953
37	Yes	14	0.0000001	0.00009746
38	Yes	14	0.0000001	0.00009779

Maximum Tower Deflections - Service Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	150 - 120	26.79	36	1.591	0.001
L2	120 - 90	17.16	36	1.381	0.001
L3	90 - 78.75	9.44	36	1.011	0.000
L4	78.75 - 60	7.22	36	0.871	0.000
L5	60 - 30	4.23	36	0.638	0.000
L6	30 - 13.75	1.09	36	0.339	0.000
L7	13.75 - 7.25	0.24	36	0.160	0.000
L8	7.25 - 0	0.07	36	0.089	0.000

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	o	ft
148.00	800MHz 2X50W RRH W/FILTER	36	26.12	1.580	0.001	29828
146.00	APXV9ERR18-C-A20 w/ Mount Pipe	36	25.46	1.569	0.001	29828
138.00	ERICSSON AIR 21 B2A B4P w/ Mount Pipe	36	22.81	1.522	0.001	12428
124.00	RRUS 11	36	18.36	1.419	0.001	5736
122.00	(2) 7770.00 w/ Mount Pipe	36	17.76	1.400	0.001	5350
112.00	APX18-206517-CT2 w/ Mount Pipe	36	14.86	1.293	0.001	4622
90.00	Bridge Stiffener C6x13 (45" x 6")	36	9.44	1.011	0.000	3950
60.00	Bridge Stiffener C8x18.7 (57" x 6")	36	4.23	0.638	0.000	5419
30.00	Bridge Stiffener C6x13 (33" x 6")	36	1.09	0.339	0.000	5347

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
13.00	KS24019-L112A	36	0.21	0.151	0.000	4931
12.00	KS24019-L112A	36	0.18	0.141	0.000	4751

Maximum Tower Deflections - Design Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	150 - 120	68.40	11	4.064	0.002
L2	120 - 90	43.82	11	3.527	0.002
L3	90 - 78.75	24.12	11	2.582	0.001
L4	78.75 - 60	18.44	11	2.225	0.001
L5	60 - 30	10.81	11	1.631	0.000
L6	30 - 13.75	2.80	11	0.865	0.000
L7	13.75 - 7.25	0.61	11	0.408	0.000
L8	7.25 - 0	0.17	11	0.227	0.000

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
148.00	800MHz 2X50W RRH W/FILTER	11	66.70	4.036	0.002	11781
146.00	APXV9ERR18-C-A20 w/ Mount Pipe	11	65.00	4.008	0.002	11781
138.00	ERICSSON AIR 21 B2A B4P w/ Mount Pipe	11	58.26	3.887	0.002	4908
124.00	RRUS 11	11	46.90	3.623	0.002	2263
122.00	(2) 7770.00 w/ Mount Pipe	11	45.35	3.577	0.002	2111
112.00	APX18-206517-CT2 w/ Mount Pipe	11	37.96	3.303	0.002	1821
90.00	Bridge Stiffener C6x13 (45" x 6")	11	24.12	2.582	0.001	1552
60.00	Bridge Stiffener C8x18.7 (57" x 6")	11	10.81	1.631	0.000	2125
30.00	Bridge Stiffener C6x13 (33" x 6")	11	2.80	0.865	0.000	2094
13.00	KS24019-L112A	11	0.54	0.387	0.000	1930
12.00	KS24019-L112A	11	0.46	0.360	0.000	1860

Compression Checks

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Section No.	Elevation	Size	L	Lu	KI/r	Fa	Α	Actual P	Allow. P _a	Ratio P
	ft		ft	ft		ksi	in ²	K	K	Pa
L1	150 - 120 (1)	P24x1/4	30.00	0.00	0.0	23.70	18.65	-7.31	442.00	0.017
L2	120 - 90 (2)	30" x 0.375"	30.00	0.00	0.0	25.07	34.90	-12.04	875.15	0.014
L3	90 - 78.75 (3)	36" x 0.375"	11.25	0.00	0.0	23.70	41.97	-14.11	994.51	0.014
L4	78.75 - 60 (4)	RPS 36" x 0.51087"	18.75	0.00	0.0	21.53	56.96	-18.37	1226.54	0.015
L5	60 - 30 (5)	RPS 42" x 0.58495"	30.00	0.00	0.0	20.63	76.11	-27.98	1569.94	0.018
L6	30 - 13.75 (6)	RPS 42" x 0.71391"	16.25	0.00	0.0	22.43	92.60	-34.40	2076.77	0.017
L7	13.75 - 7.25	RPS 42" x 0.82344"	6.50	0.00	0.0	21.40	106.52	-37.14	2279.11	0.016
	(7)									
L8	7.25 - 0 (8)	RPS 42" x 0.78565"	7.25	0.00	0.0	21.43	101.72	-39.93	2179.56	0.018

Section	Elevation	Size	L	Lu	KI/r	Fa	Α	Actual	Allow.	Ratio
No.								P	P_a	Р
	ft		ft	ft		ksi	in²	K	K	P_a

Pole	Bending	Design	Data

Section No.	Elevation	Size	Actual M _x	Actual f _{bx}	Allow. F _{bx}	Ratio f _{bx}	Actual M _y	Actual f _{by}	Allow. F _{by}	Ratio f _{by}
	ft		kip-ft	ksi	ksi	F _{bx}	kip-ft	ksi	ksi	F_{by}
L1	150 - 120 (1)	P24x1/4	213	23.30	23.70	0.983	0	0.00	23.70	0.000
L2	120 - 90 (2)	30" x 0.375"	651	30.59	25.07	1.220	0	0.00	25.07	0.000
L3	90 - 78.75 (3)	36" x 0.375"	836	27.11	23.70	1.144	0	0.00	23.70	0.000
L4	78.75 - 60 (4)	RPS 36" x 0.51087"	1166	28.09	23.69	1.186	0	0.00	23.69	0.000
L5	60 - 30 (5)	RPS 42" x 0.58495"	1773	27.38	22.69	1.207	0	0.00	22.69	0.000
L6	30 - 13.75 (6)	RPS 42" x 0.71391"	2137	27.29	24.67	1.106	0	0.00	24.67	0.000
L7	13.75 - 7.25 (7)	RPS 42" x 0.82344"	2288	25.53	23.54	1.085	0	0.00	23.54	0.000
L8	7.25 - 0 (8)	RPS 42" x 0.78565"	2459	28.68	23.57	1.217	0	0.00	23.57	0.000

Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V K	Actual f _v ksi	Allow. F _v ksi	Ratio f _v F _v	Actual T kip-ft	Actual f _{vt} ksi	Allow. F _{vt} ksi	Ratio f _{vt}
L1	150 - 120 (1)	P24x1/4	12.88	1.38	16.80	0.082	0	0.01	11.90	0.001
L2	120 - 90 (2)	30" x 0.375"	15.89	0.91	16.80	0.054	0	0.00	15.64	0.000
L3	90 - 78.75 (3)	36" x 0.375"	16.87	0.80	16.80	0.048	0	0.00	11.90	0.000
L4	78.75 - 60 (4)	RPS 36" x 0.51087"	18.34	0.64	14.36	0.045	0	0.00	14.36	0.000
L5	60 - 30 (5)	RPS 42" x 0.58495"	21.35	0.56	13.75	0.041	0	0.00	13.75	0.000
L6	30 - 13.75 (6)	RPS 42" x 0.71391"	22.85	0.49	14.95	0.033	0	0.00	14.95	0.000
L7	13.75 - 7.25 (7)	RPS 42" x 0.82344"	23.41	0.44	14.26	0.031	0	0.00	14.26	0.000
L8	7.25 - 0 (8)	RPS 42" x 0.78565"	23.80	0.47	14.28	0.033	0	0.00	14.28	0.000

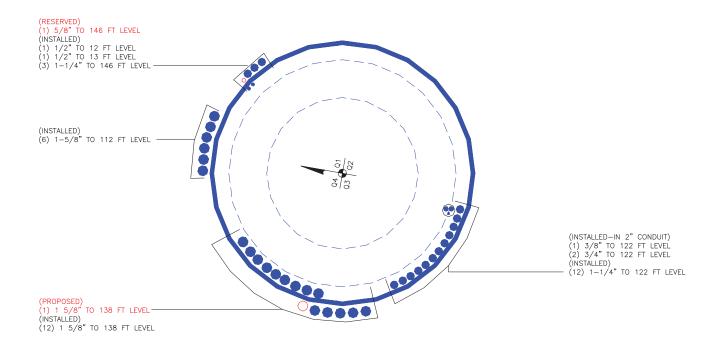
Pole Interaction Design Data

Section No.	Elevation	Ratio P	Ratio f _{bx}	Ratio f _{by}	Ratio f _v	Ratio f _{vt}	Comb. Stress	Allow. Stress	Criteria
	ft	Pa	F _{bx}	F_{by}	F_{v}	F _{vt}	Ratio	Ratio	
L1	150 - 120 (1)	0.017	0.983	0.000	0.082	0.001	1.007	1.333	H1-3+VT 🖊
L2	120 - 90 (2)	0.014	1.220	0.000	0.054	0.000	1.237	1.333	H1-3+VT 🖊
L3	90 - 78.75 (3)	0.014	1.144	0.000	0.048	0.000	1.161	1.333	H1-3+VT 🖊
L4	78.75 - 60 (4)	0.015	1.186	0.000	0.045	0.000	1.203	1.333	H1-3+VT 🖊
L5	60 - 30 (5)	0.018	1.207	0.000	0.041	0.000	1.226	1.333	H1-3+VT 🖊
L6	30 - 13.75 (6)	0.017	1.106	0.000	0.033	0.000	1.124	1.333	H1-3+VT 🖊
L7	13.75 - 7.25 (7)	0.016	1.085	0.000	0.031	0.000	1.102	1.333	H1-3+VT ✓
L8	7.25 - 0 (8)	0.018	1.217	0.000	0.033	0.000	1.236	1.333	H1-3+VT 🖊

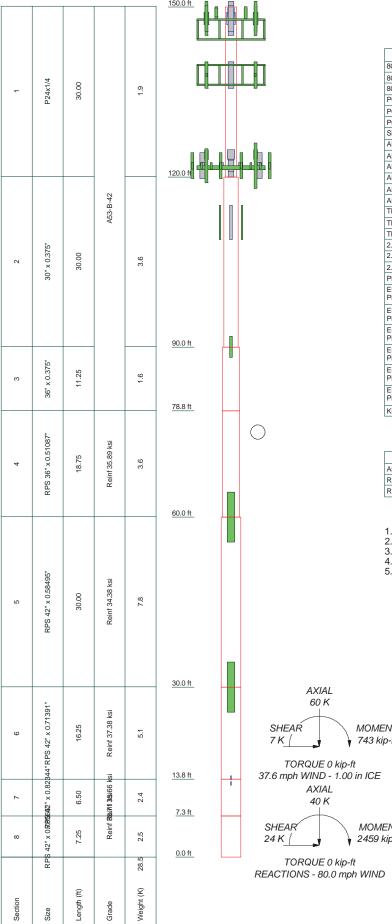
Section Capacity Table

Section	Elevation	Component	Size	Critical	P	SF^*P_{allow}	%	Pass
No.	ft	Type		Element	K	K	Capacity	Fail
L1	150 - 120	Pole	P24x1/4	1	-7.31	589.19	75.5	Pass
L2	120 - 90	Pole	30" x 0.375"	2	-12.04	1166.57	92.8	Pass
L3	90 - 78.75	Pole	36" x 0.375"	3	-14.11	1325.68	87.1	Pass
L4	78.75 - 60	Pole	RPS 36" x 0.51087"	4	-18.37	1634.98	90.2	Pass
L5	60 - 30	Pole	RPS 42" x 0.58495"	5	-27.98	2092.73	92.0	Pass
L6	30 - 13.75	Pole	RPS 42" x 0.71391"	6	-34.40	2768.33	84.3	Pass
L7	13.75 - 7.25	Pole	RPS 42" x 0.82344"	7	-37.14	3038.05	82.7	Pass
L8	7.25 - 0	Pole	RPS 42" x 0.78565"	8	-39.93	2905.35	92.7	Pass
							Summary	
						Pole (L2)	92.8	Pass
						RATING =	92.8	Pass

APPENDIX B BASE LEVEL DRAWING



APPENDIX C ADDITIONAL CALCULATIONS



DESIGNED APPURTENANCE LOADING

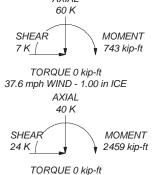
TYPE	ELEVATION	TYPE	ELEVATION
800MHz 2X50W RRH W/FILTER	148	KRY 112 144/1	138
800MHz 2X50W RRH W/FILTER	148	KRY 112 144/1	138
800MHz 2X50W RRH W/FILTER	148	Platform Mount [LP 712-1]	138
PCS 1900MHz 4x45W-65MHz	148	RRUS 11	124
PCS 1900MHz 4x45W-65MHz	148	RRUS 11	124
PCS 1900MHz 4x45W-65MHz	148	RRUS 11	124
Side Arm Mount [SO 102-3]	148	Side Arm Mount [SO 102-3]	124
APXV9ERR18-C-A20 w/ Mount Pipe	146	(2) 7770.00 w/ Mount Pipe	122
APXVSPP18-C-A20 w/ Mount Pipe	146	(2) 7770.00 w/ Mount Pipe	122
APXVSPP18-C-A20 w/ Mount Pipe	146	(2) 7770.00 w/ Mount Pipe	122
APXVTM14-C-120 w/ Mount Pipe	146	AM-X-CD-14-65-00T-RET w/ Mount	122
APXVTM14-C-120 w/ Mount Pipe	146	Pipe	
APXVTM14-C-120 w/ Mount Pipe	146	P65-17-XLH-RR w/ Mount Pipe	122
TD-RRH8x20-25	146	AM-X-CD-16-65-00T-RET w/ Mount	122
TD-RRH8x20-25	146	Pipe	100
TD-RRH8x20-25	146	(4) LGP2140X	122
2.375" OD x 5' Mount Pipe	146	(4) LGP2140X	122
2.375" OD x 5' Mount Pipe	146	(4) LGP2140X	122
2.375" OD x 5' Mount Pipe	146	DC6-48-60-18-8F	122
Platform Mount [LP 501-1]	146	T-Arm Mount [TA 602-3]	122
ERICSSON AIR 21 B2A B4P w/ Mount	138	APX18-206517-CT2 w/ Mount Pipe	112
Pipe		APX18-206517-CT2 w/ Mount Pipe	112
ERICSSON AIR 21 B2A B4P w/ Mount	138	APX18-206517-CT2 w/ Mount Pipe	112
Pipe		Pipe Mount [PM 601-3]	112
ERICSSON AIR 21 B2A B4P w/ Mount Pipe	138	Bridge Stiffener C6x13 (45" x 6")	90
ERICSSON AIR 21 B4A B2P w/ Mount	138	Bridge Stiffener C8x18.7 (57" x 6")	60
Pipe	136	Bridge Stiffener (106" x 16" x 1.25")	60
ERICSSON AIR 21 B4A B2P w/ Mount	138	Bridge Stiffener C6x13 (33" x 6")	30
Pipe		Bridge Stiffener (106" x 15" x 1.25")	30
ERICSSON AIR 21 B4A B2P w/ Mount	138	Pipe Mount [PM 601-1]	13
Pipe		KS24019-L112A	13
KRY 112 144/1	138	Pipe Mount [PM 601-1]	12
		KS24019-L112A	12

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A53-B-42	42 ksi	63 ksi	Reinf 37.38 ksi	37 ksi	47 ksi
Reinf 35.89 ksi	36 ksi	45 ksi	Reinf 35.66 ksi	36 ksi	45 ksi
Reinf 34.38 ksi	34 ksi	43 ksi	Reinf 35.71 ksi	36 ksi	45 ksi

TOWER DESIGN NOTES

- Tower is located in Hartford County, Connecticut.
 Tower designed for a 80.0 mph basic wind in accordance with the TIA/EIA-222-F Standard.
 Tower is also designed for a 37.6 mph basic wind with 1.00 in ice.
 Deflections are based upon a 50.0 mph wind.
 TOWER RATING: 92.8%



Paul J. Ford and Company 250 E. Broad Street, Suite 600 Columbus, OH 43215 Phone: 614.221.6679 FAX: 614.448.4105

^{ob:} 150 ft Monopole / Kings Lot					
Project: PJF 37514-0050 /	BU 876327				
Client: CCI	Drawn by: Joey Meinerding	App'd:			
Code: TIA/EIA-222-F	Date: 03/06/14	Scale: NTS			
Path:		Dwg No. F_1			

Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev F

Reactions

Site Data

Circle (in.):

BI I#- 876327

DU#. 0/032/		woment.	213	it-kips
Site Name: Kings Lot		Axial:	7.31	kips
App #:		Shear:	12.88	kips
		Elevation:	120	feet
Pole Manufacturer:	Rohn			

If No stiffeners, Criteria: **Bolt Data** Qty: 12 Diameter (in.) 1.5 Bolt Fu: 105 **Bolt Material:** A325 Bolt Fy: 81 N/A: <-- Disregard Bolt Fty: 0 <-- Disregard N/A: 0 44.00

Plate Data				
Diam:	41	in		
Thick, t:	2	in		
Grade (Fy):	36	ksi		
Strength, Fu:	58	ksi		
Single-Rod B-eff:	6.28	lin		

35

Stiffener Data (Welding at Both Sides)				
Config:	0	*		
Weld Type:	0			
Groove Depth:	0	in **		
Groove Angle:	0	degrees		
Fillet H. Weld:	0	< Disregard		
Fillet V. Weld:	0	in		
Width:	0	in		
Height:	0	in		
Thick:	0	in		
Notch:	0	in		
Grade:	0	ksi		
Weld str.:	0	ksi		

Pole Data				
Diam:	24	in		
Thick:	0.25	in		
Grade:	42	ksi		
# of Sides:	0	"0" IF Round		
Fu	63	ksi		
Reinf. Fillet Weld	0	"0" if None		

Stress Increase Factor				
333				

ii i vo otinonoro, oritoria.	007100	Omy Apploable	o to onoth	101104 04000
Flange Bolt Results				Rigid
Bolt Tension Cap	acity, B :	103.67	kips	Service, ASD
Max Bolt <u>directly</u> a	pplied T:	23.73	Kips	Fty*ASIF
Min. PL "tc" for B cap.	w/o Pry:	3.614	in	
Min PL "treq" for actual	Γ w/ Pry:	1.307	in	
Min PL "t1" for actual T	w/o Pry:	1.729	in	
T allowable wit	h Prying:	55.60	kips	α'>1 case
Prying F	Force, Q:	0.00	kips	
Total Bolt Tensi	on=T+Q:	23.73	kips	
Prying Bolt Stress Ratio=(7	+Q)/(B):	22.9%	Pass	

AISC ASD <-Only Applicable to Unstiffened Cases

Exterior Flange Plate Results Flexural Check Compression Side Plate Stress: Rohn/Pirod, OK Allowable Plate Stress: 36.0 ksi Rohn/Pirod, OK Compression Plate Stress Ratio: **No Prying**

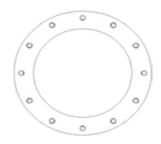
Rigid
Service ASD
0.75*Fy*ASIF
Comp. Y.L. Length:
25.48

Tension Side Stress Ratio, (treq/t)^2: 42.7% Pass

Stiffener Results N/A for Rohn / Pirod Horizontal Weld: N/A Vertical Weld: N/A Plate Flex+Shear, fb/Fb+(fv/Fv)^2: N/A Plate Tension+Shear, ft/Ft+(fv/Fv)^2: N/A Plate Comp. (AISC Bracket): N/A

Pole Results

N/A Pole Punching Shear Check:





Analysis Date: 3/6/2014

^{* 0 =} none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

^{**} Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev F

Site Data

BU#: 876327 Site Name: Kings Lot

App #:

N/A:

N/A:

Circle (in.)

Pole Manufacturer:		Rohn		
				lf
В	Bolt Data			F
Qty:	16			
Diameter (in.):	1.5	Bolt Fu:	105	1
Bolt Material:	A325	Bolt Fy:	81	1

<-- Disregard

<-- Disregard

Bolt Fty:

44.00

Plate Data							
Diam:	47	in					
Thick, t:	2	in					
Grade (Fy):	36	ksi					
Strength, Fu:	58	ksi					
Single-Rod B-eff:	5.89	in					

0

41

Stiffener Data (Welding at Both Sides)									
Config:	0	*							
Weld Type:	0								
Groove Depth:	0	in **							
Groove Angle:	0	degrees							
Fillet H. Weld:	0	< Disregard							
Fillet V. Weld:	0	in							
Width:	0	in							
Height:	0	in							
Thick:	0	in							
Notch:	0	in							
Grade:	0	ksi							
Weld str.:	0	ksi							

Pole Data								
Diam:	30	in						
Thick:	0.375	in						
Grade:	42	ksi						
# of Sides:	0	"0" IF Round						
Fu	63	ksi						
Reinf. Fillet Weld	0	"0" if None						

Stress Increase Factor						
ASIF:	1.3333333					

Reactions							
Moment:	651	ft-kips					
Axial:	12.04	kips					
Shear:	15.89	kips					
Elevation:	90	feet					

If No stiffeners, Criteria:	AISC ASD <-Only Applcable to Unstit	fened Cases
Flange Bolt Results		Rigid

Bolt Tension Capacity	, B :	103.67	kips	Service, ASD
Max Bolt directly applied	d T:	46.88	Kips	Fty*ASIF
Min. PL "tc" for B cap. w/o F	^o ry:	3.733	in .	
Min PL "treq" for actual T w/ F	ry:	1.906 i	in	
Min PL "t1" for actual T w/o F	ry:	2.510 i	in	
T allowable with Pryi	ng:	51.63	kips	α'>1 case
Prying Force,	, Q:	21.68	kips	
Total Bolt Tension=T-	+Q:	68.57	kips	
Prying Bolt Stress Ratio=(T+Q)/	(B):	66.1%	Pass	

Exterior Flange Plate Results
Compression Side Plate Stress:
Allowable Plate Stress:
Compression Plate Stress Ratio:
Rohn/Pirod, OK
Rohn/Pirod, OK

Prying Occurs, PL Check:

Tension Side Stress Ratio, (treq/t)^2: 90.8% Pass

Rigid
Service ASD
0.75*Fy*ASIF
Comp. Y.L. Length:
27.95

n/a

Stiffener Results

Horizontal Weld:

Vertical Weld:

Plate Flex+Shear, fb/Fb+(fv/Fv)^2:

Plate Tension+Shear, ft/Ft+(fv/Fv)^2:

N/A

Plate Comp. (AISC Bracket):

N/A

N/A

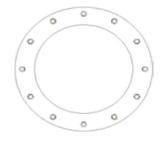
N/A

N/A

Pole Results

Pole Results

Pole Punching Shear Check: N/A





^{*} 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

^{**} Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Date: 3/6/2014
Project No: 37514-0050 R1
Site Name: Kings Lot
Site Number/BUN: 876327
Description:
Owner:

v2.0, Effective Date: 1-12-12

Engineer:Welded Bridge Stiffener Analysis per TIA/EIA-222-F & AISC 9th Ed. (Green)

Welded Bridge Stiffener Analysis per TIA/EIA-222-F & AISC 9th Ed. (Green)								
General Parameters ar	nd Loading:			Pole Parameters:				
Flange Elevation:		60.00	<mark>l</mark> ft		Upper Pole	Lower Pole		
TIA Reference Standard:		TIA/EIA-222-F	1	Pole Diameter, Dp:	36.00	42.00	in	
AISC Manual:		9th Ed. (Green)	1	Pole Thickness, tp:	0.3750	0.3750		
Method:		ASD	1	Pole Fy:	42	42		
ASD Stress Increase, ASIF:		1.333333333	i	Pole Fu:	63	63		
Moment, Mf:		1166.0	k-ft	Flange Diameter, Df:	53.00	53.00		
Axial, Pf:		18.4			33.33	00.00		
Shear, Vf:		18.3						
Bridge Stiffener Param	eters:	•		Flange Bolt Parameter	s:			
	Stiffener Type 1	Stiffener Type 2		Number of Bolt Circles:	(1) Bolt Circle			
Qty. Stiffeners:	3]		()	U.		
Upper Weld Length, L1:	50.00	0.00	in		Bolt Circle 1	Bolt Circle 2		
Lower Weld Length, L2:	50.00	0.00	in	Qty. Bolts:	0	0		
Weld Size, w:	0.3750	0.0000	in	Bolt Diameter:	1.50	0.00	in	
Electrode:	E70	E70		Bolt Circle:	47.00	0.00	in	
Effective Stiffener Width, Ws:	7.00	0.00	in	Bolt Spacing:	Symmetric	Symmetric		
Stiffener Thickness, ts:	1.25	0.00	in	Start Angle, for Symmetric:	0	0	degrees	
Notch, n:	0.50			Bolt Area, Ag:	0.0000	0.0000		
Stiffener Fy:	65		ksi	Max. Tension:	0.00	0.00	•	
Stiffener Fu:	80		ksi	Max. Net Tension:	0.00	0.00	•	
Unbraced Length, L:	6.00		in	Max. Net Compression:	0.00	0.00	kips	
K:	1.00			Manual () 0 () 0 ()			l. 4	
Stiffener Spacing:	Symmetric	Symmetric	dograna	Moment to Bolt Circle:	0.00	0.00		
Start Angle, for Symmetric: Stiffener Circle:	35 61.00		degrees in = Df + 2 n + Ws	Axial to Bolt Circle: Shear to Bolt Circle:	0.00	0.00	•	
Upper Eccentricity, e1:	12.50		in = (Df - Dp) / 2 + n + Ws / 2	Equivalent Bolt Circle:	0.00	0.00		
Lower Eccentricity, e2:	9.50		in = (Df - Dp) / 2 + n + Ws / 2	Equivalent Box Officie.	0.00	0.00		
Weld Analysis per AISC			(=: =p/;= :: ::::	Pole Analysis per AISC	Sect F4:			
Upper Pole	Stiffener Type 1	Stiffener Type 2		Upper Pole	Stiffener Type 1	Stiffener Type 2		
D:	6		Num. of Sixteenths in Weld	Stiffener Axial, P:	312.1	0.0	kips	
a:	0.2500		= e1 / L1	Effective Throat, te:	0.2651		in = 0.707 w	
k:	0	0	1	Shear Stress, fv:	3.1	0.0	kips/in= P / (2 L1)	
C:	1.2600	0.0000	Tabulated Cofficient	Section Modulus, S:	833.3	0.0	$in^2 = L1^2 / 3$	
C1:	1.0000	1.0000	Coefficient for Electrode	Bending Stress, fb:	4.7	0.0	kips/in = P e1 / S	
ASIF:	1.3333	1.3333		Combined Stress, f:	5.6	0.0	kips/in = $(fv^2 + fb^2)^{1/2}$	
Stiffener Axial, Ps:	312.1		kips	ASIF:	1.3333	0.0000		
Allowable Axial, Pa:	504.0	0.0	kips = ASIF C C1 D L	Allowable Stress, F:	8.4	0.0	kips/in = ASIF (0.4 Fy) tp	
Ratio:	61.9%	0.0%		Ratio:	67.0%	0.0%		
<u>Lower Pole</u>			•	<u>Lower Pole</u>				
D:	6		Num. of Sixteenths in Weld	Stiffener Axial, P:	312.1	0.0	•	
a:	0.1900		= e2 / L2	Effective Throat, te:	0.2651		in = 0.707 w	
k:	0			Shear Stress, fv:	3.1		ksi = P / (2 L2)	
C:	1.4140		Tabulated Cofficient	Section Modulus, S:	833.3		$in^2 = L2^2 / 3$	
C1:	1.0000		Coefficient for Electrode	Bending Stress, fb:	3.6		ksi = P e2 / S kips/in = $(fv^2 + fb^2)^{1/2}$	
ASIF:	1.3333		kina	Combined Stress, f:	4.7		kips/iii = (IV + ID)	
Stiffener Axial, Ps:	312.1		kips kips = ASIF C C1 D L	ASIF:	1.3333	0.0000	king/in = ACIE (0 4 Ev) to	
Allowable Axial, Pa:	565.6 55.2%		NIPO - MOIL O O I D L	Allowable Stress, F: Ratio:	8.4 56.4%	0.0%	kips/in = ASIF (0.4 Fy) tp	
Ratio:								
Stiffener 1 Analysis per Al		, r1.2 & App. B		Stiffener 2 Analysis per Al		11.2 & App. B		
Gross Area, Ag:	Stiffener Type 1 8.7500	lin²		Gross Area, Ag:	Stiffener Type 2 0.0000	in ²		
Net Area, An:	8.7500			Net Area. An:	0.0000			
Stiffener Axial, P:	312.1			Stiffener Axial, P:	0.000			
Stiffener Stress, f:		ksi = P / Ag		Stiffener Stress, f:		ksi = P / Ag		
b:		in = (Df - Dp) / 2 + n -	Ws, Upper Pole	b:		in = (Df - Dp) / 2 + n +	Ws, Upper Pole	
b/ts:	12.8000			b/ts:	0.0000	,		
Q, Where Qa = 1.0:		= Qa 1.340 - 0.00447	(b / ts) Fy ^{1/2}	Q, Where Qa = 1.0:	0.0000			
r:	0.3608			r:	0.0000	in ³		
KL/r:	16.6277]		KL/r:	0.0000			
ASIF:	1.3333			ASIF:	0.0000			
Allowable Axial, Fa:		/ 8 Cc' - (K L / r) ³ / 8 0	. / r) / 2 Cc ²] Fy / [5/3 + 3(K L / r) Cc ³]	Allowable Axial, Fa:		ksi = ASIF [1 - (K L / r 8 Cc - (K L / r) ³ / 8 Cc) / 2 Cc ²] Fy / [5/3 + 3(K L / r) / ³]	
ASIF:	1.3333			ASIF:	0.0000			
Allowable Bending, Fb:		ksi = ASIF 0.6 Fy Q		Allowable Bending, Fb:		ksi = ASIF 0.6 Fy		
ASIF:	1.3333			ASIF:	0.0000			
Allowable Net Tension, Ft:		ksi = ASIF 0.5 Fu		Allowable Net Tension, Ft:		ksi = ASIF 0.5 Fu		
Ratio:	82.1%			Ratio:	0.0%			
		<u>Bridge Stiffe</u>			Bridge Stiffe			
<u>Analysis</u>	Weld	l Analysis Ra	tio: 61.9% PASS	We	ld Analysis R	atio: 0.0% P	ASS	
C		•	tio: 67 0% DASS		lo Analysis D			

Summary:

Pole Analysis Ratio: 67.0% PASS

Stiffener Analysis Ratio: 82.1% PASS

Pole Analysis Ratio: 0.0% PASS

Stiffener Analysis Ratio: 0.0% PASS

Date: 3/6/2014
Project No: 37514-0050 R1
Site Name: Kings Lot
Site Number/BUN: 876327
Description:
Owner:

v2.0, Effective Date: 1-12-12

Engineer: Welded Bridge Stiffener Analysis per TIA/EIA-222-F & AISC 9th Ed. (Green)

	Welded Br	idge Stiffe	ner Analysis per	TIA/EIA-222-F & A	ISC 9th Ed. (<u>Green)</u>
General Parameters ar	nd Loading:			Pole Parameters:		
Flange Elevation:		30.00	ft		Upper Pole	Lower Pole
TIA Reference Standard:	•	TIA/EIA-222-F		Pole Diameter, Dp:	42.00	42.00 in
AISC Manual:		9th Ed. (Green)		Pole Thickness, tp:	0.3750	0.5000 in
Method:	,	ASD		Pole Fy:	42	42 ksi
ASD Stress Increase, ASIF:		1.333333333		Pole Fu:	63	63 ksi
Moment, Mf:		1773.0	k-ft	Flange Diameter, Df:	53.00	53.00 in
Axial, Pf:		28.0	kips			
Shear, Vf:		21.4	kips			
Bridge Stiffener Param	eters:			Flange Bolt Parameter	rs:	
	Stiffener Type 1	Stiffener Type 2		Number of Bolt Circles:	(1) Bolt Circle	
Qty. Stiffeners:	3	0				
Upper Weld Length, L1:	50.00	0.00	in		Bolt Circle 1	Bolt Circle 2
Lower Weld Length, L2:	50.00	0.00		Qty. Bolts:	0	0
Weld Size, w:	0.3750	0.0000	in	Bolt Diameter:	1.50	0.00 in
Electrode:		E70		Bolt Circle:	47.00	0.00 in
Effective Stiffener Width, Ws:	9.00	0.00		Bolt Spacing:	Symmetric	Symmetric
Stiffener Thickness, ts:	1.25	0.00		Start Angle, for Symmetric:	0	0 degrees
Notch, n:	0.50	0.00		Bolt Area, Ag:	0.0000	0.0000 in
Stiffener Fy:	65		ksi	Max. Tension:	0.00	0.00 kips
Stiffener Fu:	80		ksi	Max. Net Tension:	0.00	0.00 kips
Unbraced Length, L:	6.00	0.00	III	Max. Net Compression:	0.00	0.00 kips
K: Stiffener Speeing:	1.00	0.00		Moment to Delt Circles	0.00	0.00 k-ft
Stiffener Spacing: Start Angle, for Symmetric:	Symmetric 35	Symmetric 0	degrees	Moment to Bolt Circle: Axial to Bolt Circle:	0.00	0.00 kips
Stiffener Circle:	63.00		in = Df + 2 n + Ws	Shear to Bolt Circle:	0.00	0.00 kips
Upper Eccentricity, e1:	10.50		in = (Df - Dp) / 2 + n + Ws / 2	Equivalent Bolt Circle:	0.00	0.00 in
Lower Eccentricity, e2:	10.50		in = (Df - Dp) / 2 + n + Ws / 2	Equivalent Box Girole.	0.00	0.00
Weld Analysis per AISC			(B. BP)/2 · II · IIO/2	Pole Analysis per AISC	Sect FA:	
Upper Pole	Stiffener Type 1	Stiffener Type 2		Upper Pole	Stiffener Type 1	Stiffener Type 2
D:	6		Num. of Sixteenths in Weld	Stiffener Axial, P:	459.8	0.0 kips
a:	0.2100	0.0000		Effective Throat, te:	0.2651	0.0000 in = 0.707 w
k:	0.2.00	0.0000	01721	Shear Stress, fv:	4.6	0.0 kips/in= P / (2 L1)
C:	1.3640	0.0000	Tabulated Cofficient	Section Modulus, S:	833.3	0.0 $\sin^2 = L1^2 / 3$
C1:	1.0000		Coefficient for Electrode	Bending Stress, fb:	5.8	0.0 kips/in = P e1 / S
ASIF:	1.3333	1.3333		Combined Stress, f:	7.4	0.0 kips/in = $(fv^2 + fb^2)^{1/2}$
Stiffener Axial, Ps:	459.8	0.0	kips	ASIF:	1.3333	0.0000
Allowable Axial, Pa:	545.6		kips = ASIF C C1 D L	Allowable Stress, F:	8.4	0.0 kips/in = ASIF (0.4 Fy) tp
Ratio:	84.3%	0.0%		Ratio:	88.0%	0.0%
Lower Pole			ļ	Lower Pole		
D:	6	0	Num. of Sixteenths in Weld	Stiffener Axial, P:	459.8	0.0 kips
a:	0.2100	0.0000	= e2 / L2	Effective Throat, te:	0.2651	0.0000 in = 0.707 w
k:	0	0		Shear Stress, fv:	4.6	0.0 ksi = P / (2 L2)
C:	1.3640	0.0000	Tabulated Cofficient	Section Modulus, S:	833.3	0.0 $\sin^2 = L2^2 / 3$
C1:	1.0000	1.0000	Coefficient for Electrode	Bending Stress, fb:	5.8	0.0 ksi = P e2 / S
ASIF:	1.3333	1.3333		Combined Stress, f:	7.4	0.0 kips/in = $(fv^2 + fb^2)^{1/2}$
Stiffener Axial, Ps:	459.8	0.0		ASIF:	1.3333	0.0000
Allowable Axial, Pa:	545.6		kips = ASIF C C1 D L	Allowable Stress, F:	11.2	0.0 kips/in = ASIF (0.4 Fy) tp
Ratio:	84.3%	0.0%		Ratio:	66.0%	0.0%
Stiffener 1 Analysis per Al	SC Sect. D1, E2,	F1.2 & App. B		Stiffener 2 Analysis per A	ISC Sect. D1, E2,	F1.2 & App. B
	Stiffener Type 1				Stiffener Type 2	La
Gross Area, Ag:	11.2500			Gross Area, Ag:	0.0000	ā.
Net Area, An:	11.2500			Net Area, An:	0.0000	
Stiffener Axial, P:	459.8			Stiffener Axial, P:	0.0	
Stiffener Stress, f:		ksi = P / Ag		Stiffener Stress, f:		ksi = P / Ag
b:	$\overline{}$	in = (Df - Dp) / 2 + n +	ws, Upper Pole	b:		in = (Df - Dp) / 2 + n + Ws, Upper Pole
b/ts:	12.0000	IN - 0 - 4 240 - 0 00447	(h. (h-) = .1/2	b/ts:	0.0000	ın
Q, Where Qa = 1.0:		= Qa 1.340 - 0.00447	(D/tS) Fy	Q, Where Qa = 1.0:	0.0000	. 3
r:	0.3608	in.		r:	0.0000	in.
KL/r:	16.6277			KL/r:	0.0000	
ASIF: Allowable Axial, Fa:	1.3333	hai = AOIE O 11 - 111	1-) 10 C-1 ² 1 E-11E-10 - 0/44 1 1	ASIF: Allowable Axial, Fa:	0.0000	hai = ACIE M //X / 3 / 0 C-21 E / //C C//X / 3 / 0
Allowable AXIdi, Fd.		ksi = ASIF Q [1 - (K L / 8 Cc' - (K L / r) ³ / 8 (/ r) / 2 Cc ²] Fy / [5/3 + 3(K L / r)	AllOWable AXIal, Fa.		ksi = ASIF [1 - (K L / r) / 2 Cc ²] Fy / [5/3 + 3(K L / r) / 8 Cc - (K L / r) ³ / 8 Cc ³]
ASIF:	1.3333	0 CC - (K L / r)- / 8 (,c]	ASIF:	0.0000	0 CC - (N L / F) / 8 CC]
ASIF: Allowable Bending, Fb:		ksi = ASIF 0.6 Fy Q		ASIF: Allowable Bending, Fb:		ksi = ASIF 0.6 Fy
ASIF:	1.3333	/ioii 0.01 y Q		ASIF:	0.0000	7.01 0.01 j
Allowable Net Tension, Ft:		ksi = ASIF 0.5 Fu		Allowable Net Tension, Ft:		ksi = ASIF 0.5 Fu
Ratio:	91.2%			Ratio:	0.0%	
	ļ.	Bridge C+iffe	ner Tune 1			ener Tune 2
Analusia	_	Bridge Stiffe			Bridge Stiffe	
<u>Analysis</u>	Weld	Analysis Ra	tio: 84.3% PASS	We	eld Analysis R	Ratio: 0.0% PASS
	Dela	Analysis Da	Ha. 00 00/ DACC	D-	la Analysis D	ation 0.00/ DACC

Summary:

Pole Analysis Ratio: 88.0% PASS

Stiffener Analysis Ratio: 91.2% PASS

Pole Analysis Ratio: 0.0% PASS

Stiffener Analysis Ratio: 0.0% PASS



Date: 3/6/2014

PJF Project: 37514-0050 R1

Client Ref. # 876327

Site Name: Kings Lot Description: 150' Pole Owner: CCI

Engineer: JWM

v4.4 - Effective 7-12-13

Asymmetric Anchor Rod Analysis

Moment = 2459 k-ft
Axial = 40.0 kips
Shear = 24.0 kips
Anchor Qty = 25

TIA Ref.
ASIF = 1.3333
Max Ratio = 100.0%

 $\begin{array}{ccc} \text{Location} = & & \textbf{Base} \\ \eta = & & \textbf{N} \\ \text{Threads} = & & \textbf{N} \end{array}$

N/A fo

for BP, Rev. G Sect. 4.9.9 for FP, Rev. G

** For Post Installed Anchors: Check anchors for embedment, epoxy/grout bond, and capacity based on proof load. **

	Nominal						Area Override.		Max Net	Max Net	Load for	Capacity		
II .,	Anchor Dia,				Location,	Anchor	in ²		Compressio	Tension,	Capacity	Override,	Capacity,	Capacity
Item	in	Spec	Fy, ksi	Fu, ksi	degrees	Circle, in		Area, in ²	n, kips	kips	Calc, kips	kips	kips	Ratio
1		A354 Gr BC	109	125	0.0	47.00	0.00	1.77	71.94	69.47	69.47	0.00	97.19	71.5%
2	1.500	A354 Gr BC	109	125	20.0	47.00	0.00	1.77	69.58	67.11	67.11	0.00	97.19	69.0%
3	1.500	A354 Gr BC	109	125	40.0	47.00	0.00	1.77	66.06	63.59	63.59	0.00	97.19	65.4%
4	1.500	A354 Gr BC	109	125	60.0	47.00	0.00	1.77	63.15	60.67	60.67	0.00	97.19	62.4%
5		A354 Gr BC	109	125	80.0	47.00	0.00	1.77	62.52	60.05	60.05	0.00	97.19	61.8%
6	1.500	A354 Gr BC	109	125	100.0	47.00	0.00	1.77	64.70	62.22	62.22	0.00	97.19	64.0%
7	1.500	A354 Gr BC	109	125	120.0	47.00	0.00	1.77	68.59	66.12	66.12	0.00	97.19	68.0%
8	1.500	A354 Gr BC	109	125	140.0	47.00	0.00	1.77	72.35	69.87	69.87	0.00	97.19	71.9%
9	1.500	A354 Gr BC	109	125	160.0	47.00	0.00	1.77	74.37	71.89	71.89	0.00	97.19	74.0%
10	1.500	A354 Gr BC	109	125	180.0	47.00	0.00	1.77	73.84	71.37	71.37	0.00	97.19	73.4%
11	1.500	A354 Gr BC	109	125	200.0	47.00	0.00	1.77	70.89	68.42	68.42	0.00	97.19	70.4%
12	1.500	A354 Gr BC	109	125	220.0	47.00	0.00	1.77	66.59	64.11	64.11	0.00	97.19	66.0%
13	1.500	A354 Gr BC	109	125	240.0	47.00	0.00	1.77	62.72	60.24	60.24	0.00	97.19	62.0%
14	1.500	A354 Gr BC	109	125	260.0	47.00	0.00	1.77	61.14	58.66	58.66	0.00	97.19	60.4%
15	1.500	A354 Gr BC	109	125	280.0	47.00	0.00	1.77	62.60	60.12	60.12	0.00	97.19	61.9%
16	1.500	A354 Gr BC	109	125	300.0	47.00	0.00	1.77	66.14	63.66	63.66	0.00	97.19	65.5%
17	1.500	A354 Gr BC	109	125	320.0	47.00	0.00	1.77	69.85	67.38	67.38	0.00	97.19	69.3%
18	1.500	A354 Gr BC	109	125	340.0	47.00	0.00	1.77	72.07	69.60	69.60	0.00	97.19	71.6%
19	2.250	#18J A615 Gr 75	75	100	30.0	53.00	0.00	3.98	172.14	166.57	166.57	0.00	195.00	85.4%
20	2.250	#18J A615 Gr 75	75	100	110.0	53.00	0.00	3.98	168.31	162.74	162.74	0.00	195.00	83.5%
21	2.250	#18J A615 Gr 75	75	100	210.0	53.00	0.00	3.98	174.26	168.69	168.69	0.00	195.00	86.5%
22	2.250	#18J A615 Gr 75	75	100	290.0	53.00	0.00	3.98	163.07	157.50	157.50	0.00	195.00	80.8%
23	2.000	A193 Gr B7	105	125	95.0	60.00	0.00	3.14	143.99	139.59	139.59	0.00	172.79	80.8%
24	2.000	A193 Gr B7	105	125	230.0	60.00	0.00	3.14	145.68	141.28	141.28	0.00	172.79	81.8%
25	2.000	A193 Gr B7	105	125	335.0	60.00	0.00	3.14	162.75	158.35	158.35	0.00	172.79	91.6%
	57.15													

Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material

TIA Rev F

Site Data

BU#: 876327 Site Name: Kings Lot

App #:

Qty:

Diam:

Rod Material:

Strength (Fu):

Yield (Fy):

Bolt Circle:

Pole Manufacturer: Other

Anchor Rod Data

18 1.5

Other 125

109

47

in

ksi

ksi

in

Reactions									
Moment:	1288.9	ft-kips							
Axial:	22.3	kips							
Shear:	13.4	kips							

Reactions adjusted to account for additional anchor rods.

If No stiffeners, Criteria:

AISC ASD <-Only Applicable to Unstiffened Cases

A I	DI	D 14 -
Anchor	Roa	Results

Maximum Rod Tension: 71.9 Kips 97.2 Kips Allowable Tension: 74.0% Pass Anchor Rod Stress Ratio:

Stiffened
Service, ASD
Fty*ASIF

Plate Data		
Diam:	53	in
Thick:	2	in
Grade:	36	ksi
Single-Rod B-eff:	7.33	in

Plate Data			
Diam:	53	in	
Thick:	2	in	
Grade:	36	ksi	
Single-Rod B-eff:	7.33	in	

Stiffener Data (Welding at both sides)		
Config:	1	*
Weld Type:	Both	
Groove Depth:	0.25	in **
Groove Angle:	45	degrees
Fillet H. Weld:	0.25	in
Fillet V. Weld:	0.25	in
Width:	5.75	in
Height:	14.25	in
Thick:	0.5	in
Notch:	0.75	in
Grade:	50	ksi
Weld str.:	70	ksi

Pole Data			
Diam:	42	in	
Thick:	0.5	in	
Grade:	42	ksi	
# of Sides:	0	"0" IF Round	
Fu	63	ksi	
Reinf. Fillet Weld	0	"0" if None	

01		1
Stress Increase Factor		
ASIF:	1.333	

Base Plate Results	Flexural Check
Base Plate Stress:	22.9 ksi
Allowable Plate Stress:	36.0 ksi
Base Plate Stress Ratio:	63.5% Pass

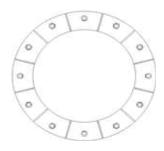
Stiffened
Service, ASD
0.75*Fy*ASIF
Y.L. Length:
N/A, Roark

Stiffener Results

Horizontal Weld: 38.5% Pass Vertical Weld: 29.9% Pass Plate Flex+Shear, fb/Fb+(fv/Fv)^2: 11.4% Pass Plate Tension+Shear, ft/Ft+(fv/Fv)^2: 38.8% Pass Plate Comp. (AISC Bracket): 42.6% Pass

Pole Results

Pole Punching Shear Check: 7.0% Pass





^{* 0 =} none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

^{**} Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material

TIA Rev F

Site Data

BU#: 876327 Site Name: Kings Lot

App #:

Pole Manufacturer: Other

Re	actions		
Λ	/loment:	757.4	ft-kips
	Axial:	11.1	kips
	Shear:	6.7	kips

Reactions adjusted to account for additional anchor rods.

If No stiffeners, Criter

AISC ASD <-Only Applicable to Unstiffened Cases

Qty: 4 2.25 Diam: in A615-J Rod Material: 100 Strength (Fu): ksi Yield (Fy): 75 ksi **Bolt Circle:** in

Anchor Rod Data

Plate Data		
Diam:	57.5	in
Thick:	2	in
Grade:	36	ksi
Single-Rod B-eff:	24.25	in

Stiffener Data (Welding at both sides)								
Config:	3	*						
Weld Type:	Both							
Groove Depth:	0.25	in **						
Groove Angle:	45	degrees						
Fillet H. Weld:	0.25	in						
Fillet V. Weld:	0.25	in						
Width:	7.75	in						
Height:	21.75	in						
Thick:	0.5	in						
Notch:	0.75	in						
Grade:	50	ksi						
Weld str.:	70	ksi						
Clear Space between Stiffeners (b):	5	in						

Pole Data							
Diam:	42	in					
Thick:	0.5	in					
Grade:	42	ksi					
# of Sides:	0	"0" IF Round					
Fu	63	ksi					
Reinf. Fillet Weld	0	"0" if None					

Stress	actor	
ASIF:	1.333	

Base Plate and Stiffener Check Only

Base Plate Results Shear Check Only Base Plate Stress: 5.6 ksi Allowable Plate Stress: 19.2 ksi Base Plate Stress Ratio: 29.3% Pass

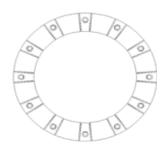
Stiffened
Service, ASD
0.75*Fy*ASIF
Y.L. Length:
N/A, Roark

Stiffener Results

Horizontal Weld: 26.3% Pass Vertical Weld: 19.5% Pass Plate Flex+Shear, fb/Fb+(fv/Fv)^2: 6.4% Pass Plate Tension+Shear, ft/Ft+(fv/Fv)^2: 26.5% Pass Plate Comp. (AISC Bracket): 30.1% Pass

Pole Results

Pole Punching Shear Check: 4.2% Pass





^{* 0 =} none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

^{**} Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

foundation loads

ft-kips kips kips 2459 40 24 Tower or Pole Weight = Total Horizontal Force = Overturning Moment = Tower Leg Tension = Tower Leg Compression =

soil properties

1	bcf	ksf	#
1.5	115	8	66
Safety factor against overturning =	Soil Density =	Allowable Soil Bearing =	Depth to water table =

mat dime

	2.5	9	21	21				3.5	0
ensions	Depth to Bottom of Footing =	Footing Thickness =	Footing Width =	Footing Length =	Base Plate Diameter =	Anchor Plate Diameter =	Depth of Anchor Plate =	Tower Base Width =	Tower Center Offset =

Summary of analysis results

(Stress Ratio = 0.851) < CONTROLLING CRITERIA	Calculated Overturning Moment = 2603 ft-kips	Resisting Moment = 4587.5 ft-kips	Factor of Safety against overturning = 1.762 > 1.5 okay
Overturning Moment: (S	Calculated		Factor of Safety ag

Soil Bearing

(Stress Ratio = 0.349)

Calculated Soil Bearing Pressure = 2.789 ksf < 8 ksf okay Allowable Soil Bearing = 8 ksf

Bending Moment

(Stress Ratio = 0.305)

Calculated Ultimate Bending Moment = 1591 ft-kips < 5216 ft-kips okay Ultimate Bending Moment Resistance = 5216 ft-kips

Bending Shear

##

####

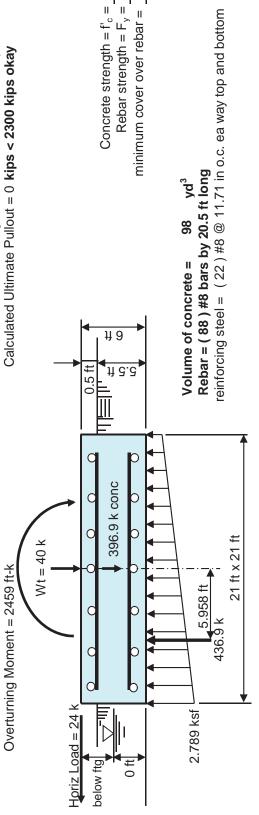
(Stress Ratio = 0.185)

Calculated Ultimate Bending Shear = 259 kips < 1398 kips okay Ultimate Bending Shear Resistance = 1398 kips

(Stress Ratio = 0)

Ultimate Tensile Punching Shear Resistance = 2300 kips

Calculated Ultimate Pullout = 0 kips < 2300 kips okay



inches (ksi) (ksi)

09



RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CT11883C

CT883 / Sprint South Windsor

59 McGuire Road South Windsor, CT 06074

March 20, 2014

EBI Project Number: 62141468

21 B Street Burlington, MA 01803 Tel: (781) 273.2500 Fax: (781) 273.3311



March 20, 2014

T-Mobile USA Attn: Jason Overbey, RF Manager 35 Griffin Road South Bloomfield, CT 06002

Re: Emissions Values for Site: CT11883C - CT883 / Sprint South Windsor

EBI Consulting was directed to analyze the proposed T-Mobile facility located at 59 McGuire Road, South Windsor, CT, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter (μ W/cm2). The number of μ W/cm2 calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter (μ W/cm2). The general population exposure limit for the cellular band is 567 μ W/cm2, and the general population exposure limit for the PCS and AWS bands is 1000 μ W/cm2. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 59 McGuire Road, South Windsor, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, the actual antenna pattern gain value in the direction of the sample area was used. For this report the sample point is a 6 foot person standing at the base of the tower

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 GSM channels (1935.000 MHz—to 1945.000 MHz) were considered for each sector of the proposed installation.
- 2) 2 UMTS channels (2110.000 MHz to 2120.000 MHz / 2140.000 MHz to 2145.000 MHz) were considered for each sector of the proposed installation
- 3) 2 LTE channels (2110.000 MHz to 2120.000 MHz / 2140.000 MHz to 2145.000 MHz) were considered for each sector of the proposed installation
- 4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The actual gain in this direction was used per the manufactures supplied specifications.
- 6) The antenna used in this modeling is the Ericsson AIR21 for LTE, UMTS and GSM. This is based on feedback from the carrier with regards to anticipated antenna selection. This antenna has a 15.6 dBd gain value at its main lobe. Actual antenna gain values were used for all calculations as per the manufacturers specifications



- 7) The antenna mounting height centerline of the proposed antennas is **138 feet** above ground level (AGL)
- 8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits

Site ID	CT11883C - CT883 / Sprint South Windsor
Site Addresss	59 McGuire Road, South Windsor, CT 06074
Site Type	Monopole

	Sector 1																
Antenna Number 1a 1b 2a 2B	Antenna Make Ericsson Ericsson Ericsson Ericsson	Antenna Model AIR21 B4A/B2P AIR21 B4A/B2P AIR21 B2A / B4P AIR21 B2A / B4P	Status Active Not Used Active Passive	Frequency Band AWS - 2100 MHz - PCS - 1950 MHz AWS - 2100 MHz	Technology LTE - GSM / UMTS UMTS	Power Out Per Channel (Watts) 60 30 30	Number of Channels 2 2 2	Composite Power 120 0 60 60	Antenna Gain in direction of sample point (dBd) -3.95 -3.95 -3.95 -3.95	Antenna Height (ft) 138 138 138 138	analysis height 132 132 132	None None 1-5/8" 1-5/8"	(dB) 0 0 0	Additional Loss 0 0 0 0	ERP 48.326044 0 24.163022 24.163022 0.199%	Power Density Value 0.997101 0 0.498551 0.498551	Power Density Percentage 0.09971% 0.0000% 0.04986% 0.04986%
	Sector 2																
Antenna Number 1a 1b	Antenna Make Ericsson Ericsson Ericsson	Antenna Model AIR21 B4A/B2P AIR21 B4A/B2P AIR21 B2A / B4P	Status Active Not Used Active	Frequency Band AWS - 2100 MHz - PCS - 1950 MHz	Technology LTE - GSM / UMTS	Power Out Per Channel (Watts) 60	Number of Channels	Composite Power 120 0 60	Antenna Gain in direction of sample point (dBd) -3.95 -3.95	Antenna Height (ft) 138 138	analysis height 132 132	Cable Size None None 1-5/8"	Cable Loss (dB)	Additional Loss 0	ERP 48.326044 0 24.163022	Power Density Value 0.997101 0 0.498551	Power Density Percentage 0.09971% 0.00000% 0.04986%
28	Ericsson	AIR21 B2A / B4P	Passive	AWS - 2100 MHz	UMTS	30	2	60	-3.95	138	132	1-5/8"	0	0	24.163022	0.498551	0.04986%
												Sector tot	al Power De	ensity Value:	0.199%		
							Se	ector 3									
						Power Out Per			Antenna Gain in direction							Power	Power
Antenna			6				Number of		of sample	Antenna	analysis			Additional		Density	Density
Number	Antenna Make	Antenna Model AIR21 B4A/B2P	Status	Frequency Band	Technology	(Watts)	Channels 2	Power	point (dBd) -3.95			Cable Size		Loss	ERP	Value	Percentage
1a 1b	Ericsson Ericsson	AIR21 B4A/B2P	Active Not Used	AWS - 2100 MHz	LTE	60	2	120	-3.95 -3.95	138 138	132 132	None None	0	0	48.326044	0.997101	0.09971%
2a	Ericsson	AIR21 B2A / B4P	Active	PCS - 1950 MHz	GSM / UMTS	30	2	60	-3.95	138	132	1-5/8"	0	0		0.498551	0.00000%
28	Ericsson	AIR21 B2A / B4P	Passive	AWS - 2100 MHz	UMTS	30	2	60	-3.95	138	132	1-5/8"	0	0	24.163022	0.498551	0.04986%
20	211033011	, LI DEN / D41	. 033140	2100 141112	014113	30			3.33	130	132		·	ensity Value:	0.199%	5.450551	3.04300/0
												Sector tot	OWIC: DO	value.	0.10070		

Site Composite MPE %							
Carrier	MPE %						
T-Mobile	0.598%						
Sprint	4.420%						
MetroPCS	9.690%						
AT&T	23.090%						
Total Site MPE %	37.798%						



Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public exposure to RF Emissions.

The anticipated Maximum Composite contributions from the T-Mobile facility are **0.598**% (**0.199**% **from each sector**) of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **37.798**% of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

Scott Heffernan

RF Engineering Director

EBI Consulting

21 B Street

Burlington, MA 01803

-- T--Mobile--

NORTHEAST LLC.

SITE NAME: CT883/SPRINT S. WINDSOR

SITE ID NUMBER: CT11883C

SITE ADDRESS: 59 MCGUIRE ROAD

SOUTH WINDSOR, CT 06074

PROJECT SUMMARY

SITE ID NUMBER:

CT11883C

SITE NAME:

CT883/SPRINT S. WINDSOR

CROWN BU#:

876327

SITE ADDRESS:

59 MCGUIRE ROAD

SOUTH WINDSOR, CT 06074

COUNTY:

HARTFORD

PROPERTY OWNER:

CROWN CASTLE USA

APPLICANT:

T-MOBILE NORTHEAST, LLC. 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 0602 PHONE: (800) 692-7100

TECTONIC ENGINEERING CONSULTANTS P.C.

NEWBURGH, NY 12550

ENGINEER/

SURVEYOR/ STRUCTURAL ENG:

STRUCTURAL ENG

CONTACT: PHONE:

TAMMY NOSEK (845) 567-6656 EXT. 2807

1279 ROUTE 300

SITE ACQUISITION:

CROWN CASTLE 1200 MACARTHUR BLVD

SUITE 200

MAHWAH, NJ 07430 PAUL HUGHES (585) 259-7604

CONTACT: PHONE:

MAP 5 LOT 14.1

LATITUDE: (NAD 83)

PARCEL INFO:

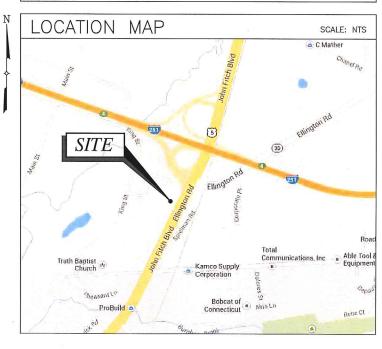
41.80290 N

LONGITUDE: (NAD 83)

72.61730 W

SITE DIRECTIONS

HEAD NORTHEAST ON GRIFFIN RD S TOWARD W NEWBERRY RD. TAKE THE 1ST RIGHT ONTO W NEWBERRY RD. TURN LEFT ONTO WOODLAND AVE. TAKE THE 1ST RIGHT ONTO CT-187 S/BLUE HILLS AVE. TURN LEFT ONTO CT-218 E/COTTAGE GROVE RD. CONTINUE TO FOLLOW CT-218 E. TURN RIGHT ONTO THE INTERSTATE 291 E RAMP TO SOUTH WINDSOR. MERGE ONTO I-291 E. TAKE EXIT 4 TO MERGE ONTO US-5 S/ELLINGTON RD. TURN RIGHT ONTO BURNHAM ST. TURN RIGHT ONTO KING ST. TURN RIGHT ONTO MCGUIRE RD. DESTINATION WILL BE ON THE RIGHT.



SHE	SHEET INDEX						
SHEET NO	DESCRIPTION	REV NO					
T-1	TITLE SHEET	1					
A-1	SITE PLAN	1					
A-2	EQUIPMENT LAYOUT PLANS	1					
A-3	ELEVATION & DETAIL	1					
A-4	ANTENNA LAYOUT PLANS & DETAILS	1					
A-5	DETAILS	1					
A-6	DETAILS	1					
A-7	NOTES	1					
A-8	NOTES	1					

THIS SET OF PLANS SHALL NOT BE UTILIZED AS CONSTRUCTION DOCUMENTS UNTIL ALL ITEMS HAVE BEEN ADDRESSED AND EACH OF THE DRAWINGS HAS BEEN REVISED AND ISSUED "FOR CONSTRUCTION".



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- ENGINEERINGSURVEYING

TECTONIC Engineering & Survey Consultants P.C.

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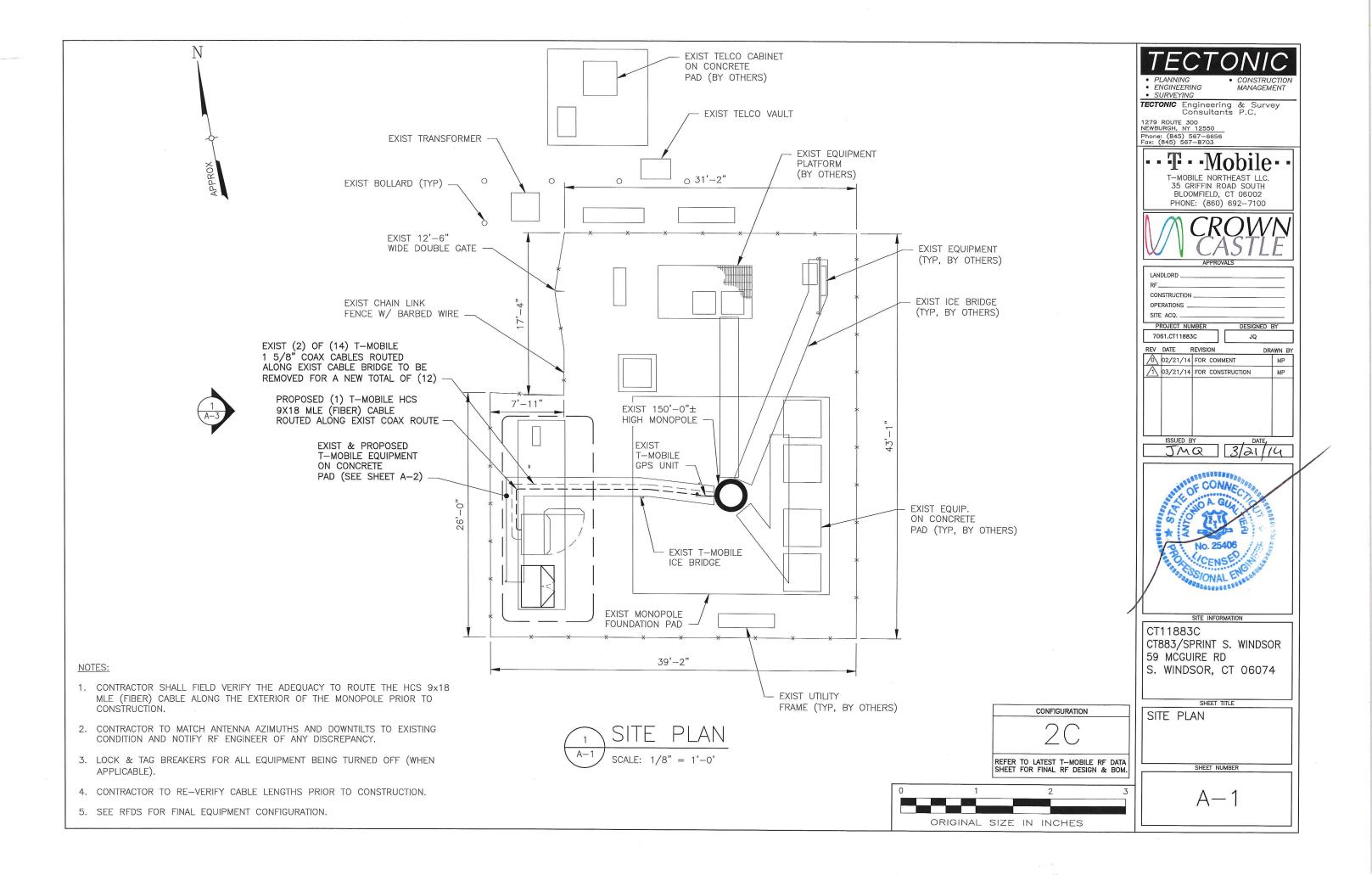


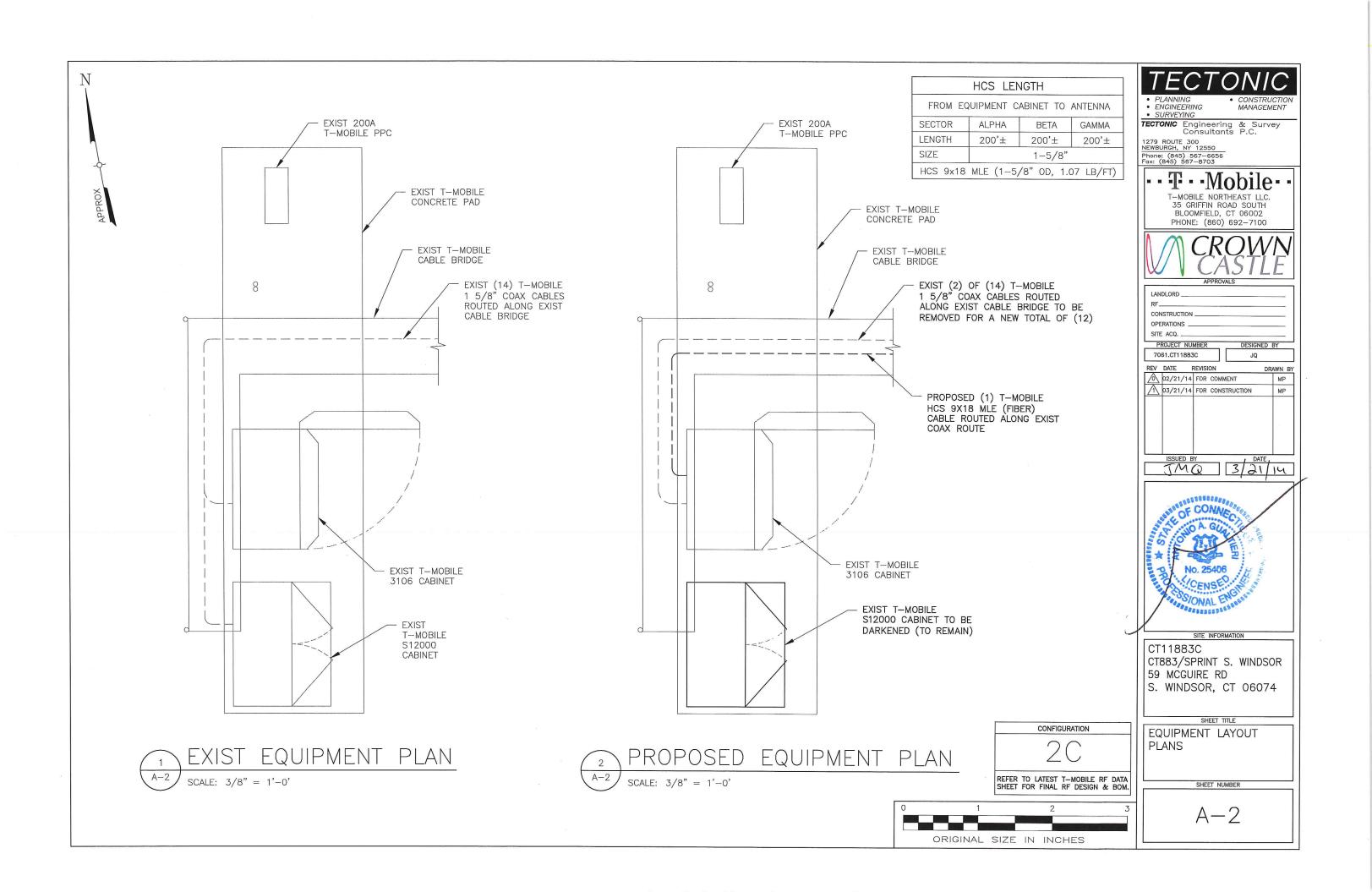
ı		SITE INFO	PRMATI	ON
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	59	MCGUIRE F	RD	
	S.	WINDSOR,	CT	06074

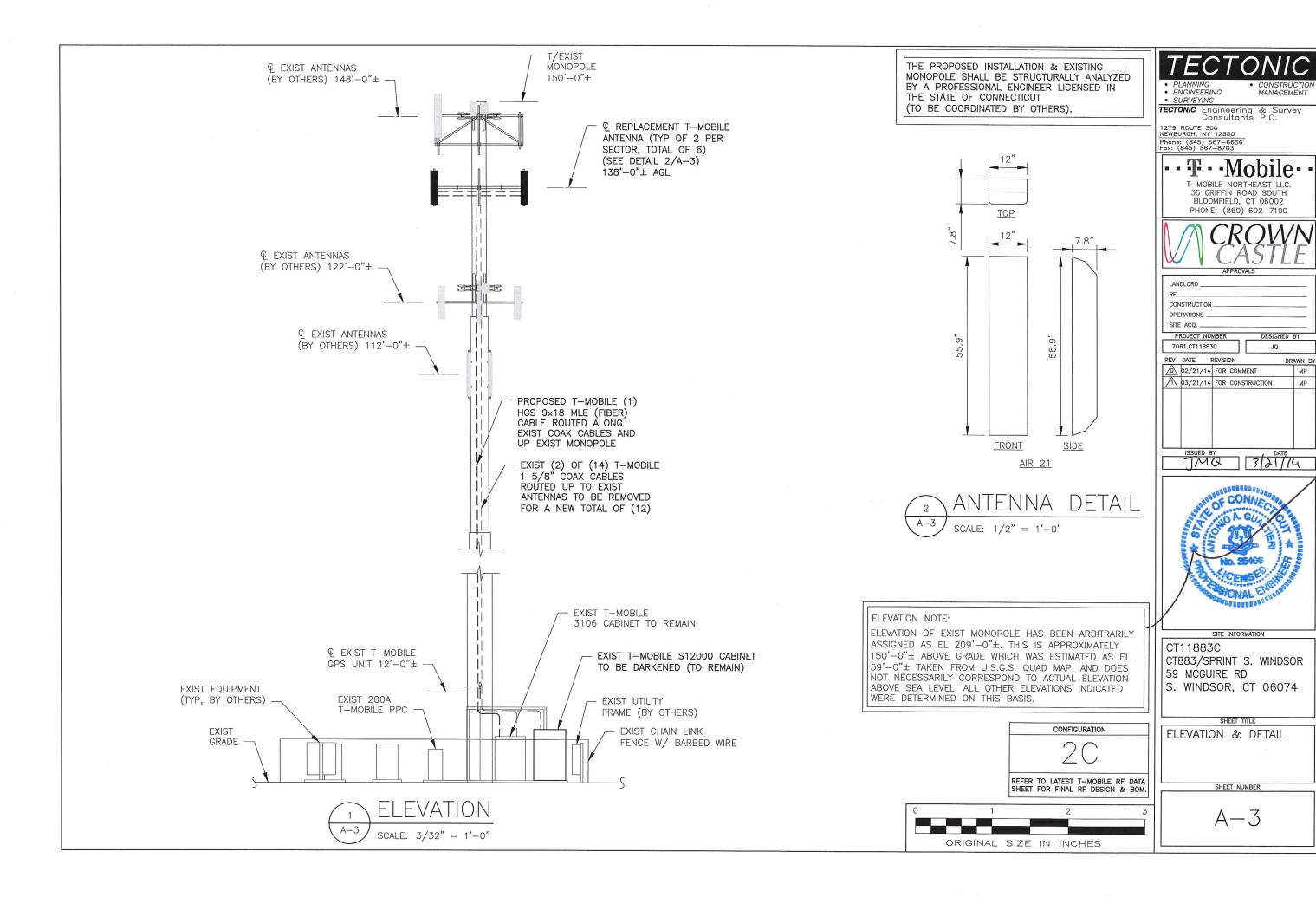
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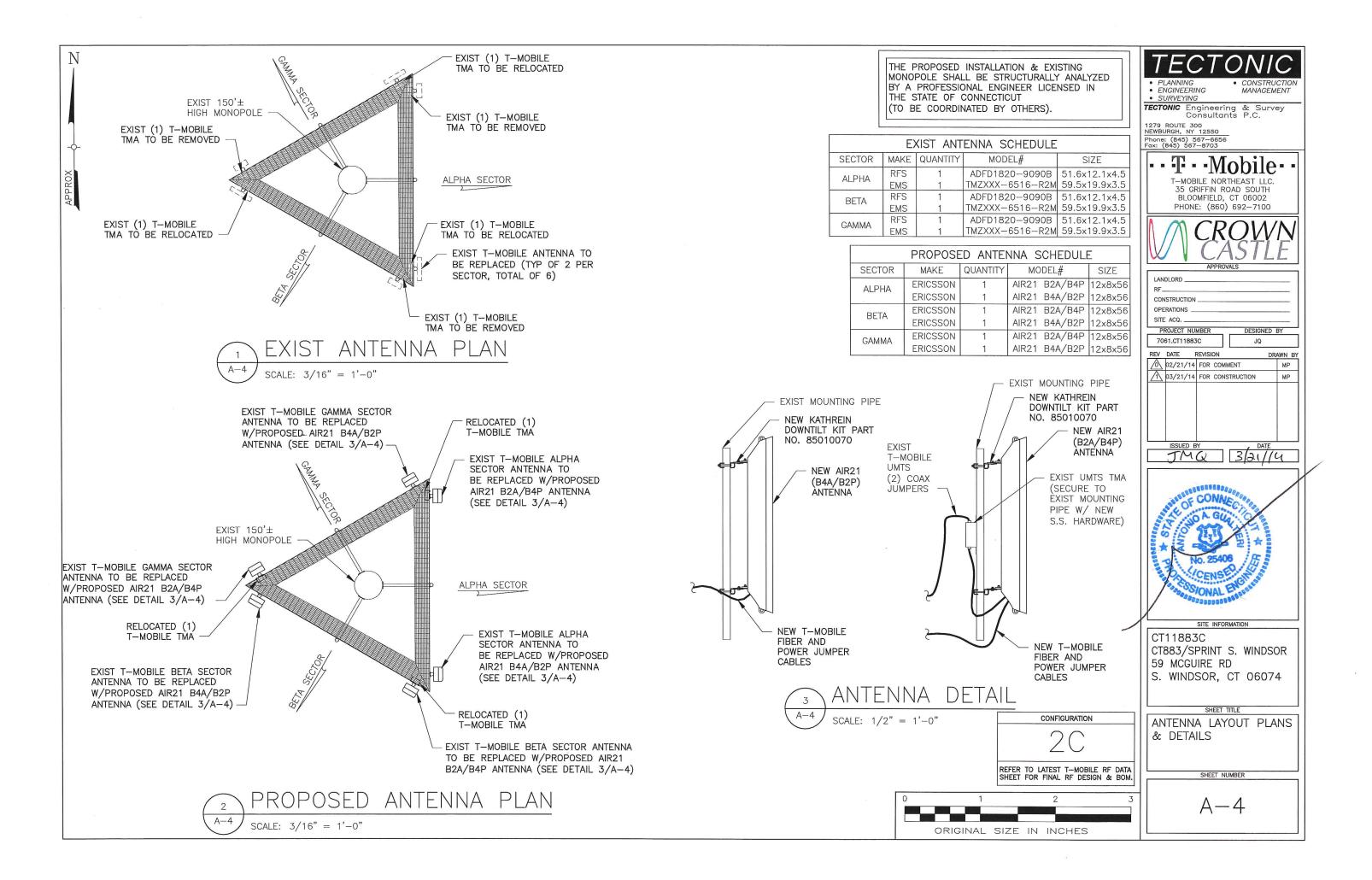
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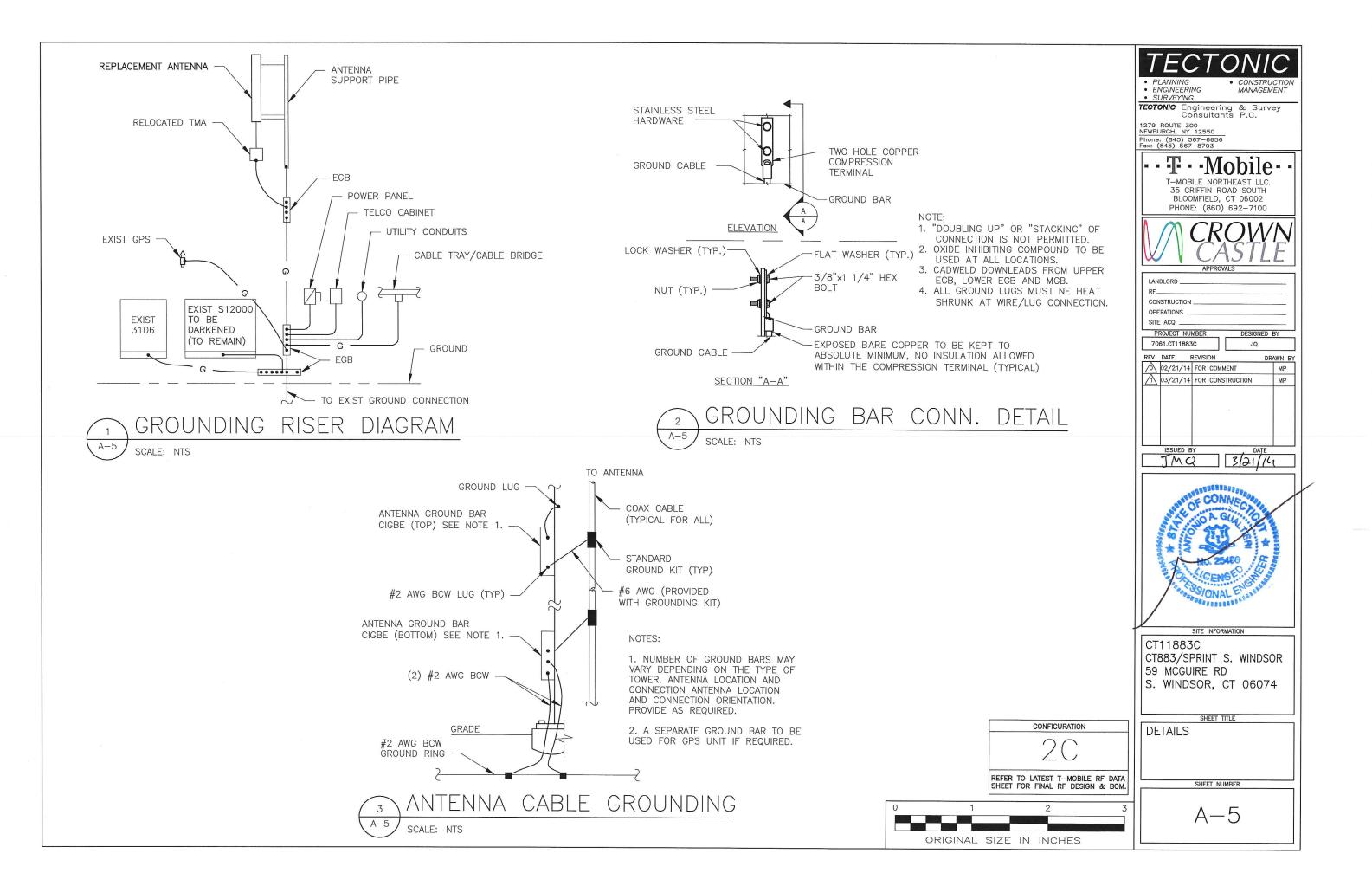
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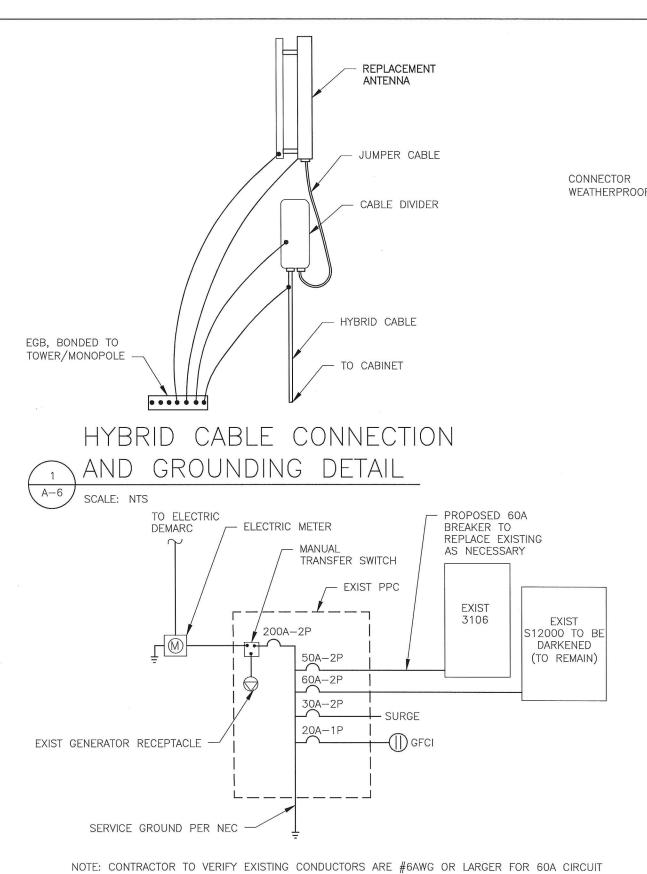






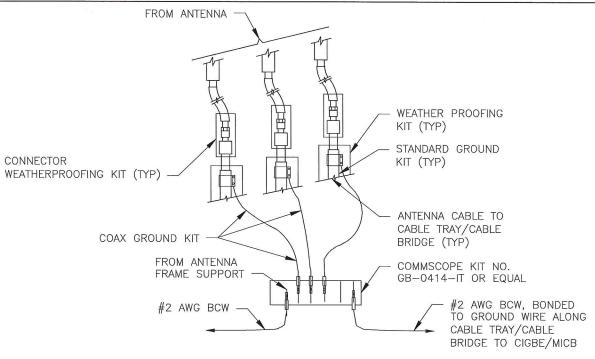






ONE-LINE POWER DIAGRAM

SCALE: NTS



NOTE:

SCALE: NTS

DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

GROUND WIRE TO GROUND

BAR CONNECTION DETAIL

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· T··Mobile·

T-MOBILE NORTHEAST LLC. 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 PHONE: (860) 692-7100



PROJECT NUMBER DESIGNED BY
7061.CT11883C JQ

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CT11883C CT883/SPRINT S. WINDSOR 59 MCGUIRE RD S. WINDSOR, CT 06074

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DETAILS

SHEET NUMBER

A-6

CONFIGURATION

2

REFER TO LATEST T-MOBILE RF DATA SHEET FOR FINAL RF DESIGN & BOM.

0 1 2 3
ORIGINAL SIZE IN INCHES

GENERAL NOTES

- 1. CONTRACTOR SHALL NOT COMMENCE ANY WORK UNTIL HE OBTAINS, AT HIS OWN EXPENSE, ALL INSURANCE REQUIRED BY T-MOBILE, THE PROPERTY OWNER AND/OR PROPERTY MANAGEMENT COMPANY.
- 2. THIS SET OF PLANS HAS BEEN PREPARED FOR THE PURPOSES OF MUNICIPAL AND AGENCY REVIEW AND APPROVAL. THIS SET OF PLANS SHALL NOT BE UTILIZED AS CONSTRUCTION DOCUMENTS UNTIL ALL CONDITIONS OF APPROVAL HAVE BEEN SATISFIED AND EACH OF THE DRAWINGS HAVE BEEN REVISED TO INDICATE "ISSUED FOR PERMIT"
- 3. THIS PLAN IS SUBJECT TO ALL EASEMENTS AND RESTRICTIONS OF RECORD.
- 4. THE CONTRACTOR SHALL COMPLY WITH ALL APPLICABLE CODES, ORDINANCES, LAWS AND REGULATIONS OF ALL MUNICIPALITIES, UTILITIES OR OTHER PUBLIC AUTHORITIES.
- 5. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND INSPECTIONS THAT MAY BE REQUIRED BY ANY FEDERAL, STATE, COUNTY OR MUNICIPAL AUTHORITIES.
- 6. THE CONTRACTOR SHALL NOTIFY THE CONSTRUCTION MANAGER, IN WRITING, OF ANY CONFLICTS, ERRORS OR OMISSIONS PRIOR TO THE SUBMISSION OF BIDS OR PERFORMANCE OF WORK. MINOR OMISSIONS OR ERRORS IN THE BID DOCUMENTS SHALL NOT EXCUSE SAID CONTRACTOR FROM COMPLETING THIS PROJECT IN ACCORDANCE WITH THE OVERALL INTENT OF THESE DRAWINGS.
- 7. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING ALL EXISTING SITE IMPROVEMENTS PRIOR TO COMMENCING CONSTRUCTION. THE CONTRACTOR SHALL REPAIR ANY DAMAGE CAUSED AS A RESULT OF CONSTRUCTION OF THIS FACILITY.
- 8. THE SCOPE OF WORK FOR THIS PROJECT SHALL INCLUDE PROVIDING ALL MATERIALS, EQUIPMENT AND LABOR REQUIRED TO COMPLETE THIS PROJECT. ALL EQUIPMENT SHALL BE INSTALLED IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- 9. THE CONTRACTOR SHALL VISIT THE PROJECT SITE PRIOR TO SUBMITTING A BID TO VERIFY THAT THE PROJECT CAN BE CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS.
- 10. POWER TO THE FACILITY IS MONITORED BY AN EXISTING METER.
- 11. ALL STRUCTURAL ELEMENTS SHALL BE HOT DIPPED GALVANIZED STEEL
- 12. CONTRACTOR SHALL MAKE A UTILITY "ONE CALL" TO LOCATE ALL UTILITIES PRIOR TO EXCAVATING.
- 13. IF ANY PIPING EXISTS BENEATH THE SITE AREA, CONTRACTOR MUST LOCATE IT AND CONTACT OWNER'S REPRESENTATIVE.
- 14. THE CONSTRUCTION CONTRACTOR IS SOLELY RESPONSIBLE FOR DETERMINING ALL CONSTRUCTION MEANS
 AND METHODS. THE CONSTRUCTION CONTRACTOR IS ALSO RESPONSIBLE FOR ALL JOB SITE SAFETY.
- 15. CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES AND EXISTING CONDITIONS AT THE SITE PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA AND SUBMIT TO THE ENGINEER ANY DISCREPANCIES FROM THE DRAWINGS.
- 16. THE CONTRACTOR IS TO REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. THE CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUB—CONTRACTORS AND RELATED PARTIES. THE SUB—CONTRACTOR SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
- 17. DETAILS ARE INTENDED TO SHOW END RESULT OF DESIGN. MINOR MODIFICATIONS MAY BE REQUIRED TO SUIT JOB DIMENSIONS OR CONDITIONS, AND SUCH MODIFICATIONS SHALL BE INCLUDED AS PART OF THE WORK.
- 18. ALL MATERIAL PROVIDED BY T-MOBILE IS TO BE REVIEWED BY THE CONTRACTOR AND ALL APPLICABLE SUB-CONTRACTORS PRIOR TO INSTALLATION. ANY DEFICIENCIES TO PROVIDE MATERIALS SHALL BE BROUGHT TO THE CONSTRUCTION MANAGER'S ATTENTION IMMEDIATELY.
- 19. THE MATERIALS INSTALLED SHALL MEET REQUIREMENTS OF CONTRACTORS DOCUMENTS, NO SUBSTITUTIONS ARE ALLOWED.
- 20. INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR CONFORMING MATERIALS OR CONDITIONS SHALL BE REPORTED TO THE ENGINEER PRIOR TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE ENGINEER APPROVAL.

GENERAL NOTES

- 21. THE CONTRACTOR SHALL RECEIVE CLARIFICATION AND AUTHORIZATION IN WRITING TO PROCEED BEFORE STARTING WORK ON ANY ITEMS NOT CLEARLY DEFINED OR IDENTIFIED BY THE CONSTRUCTION DOCUMENTS.
- 22. THE CONTRACTOR SHALL NOTIFY THE CONSTRUCTION MANAGER OF ALL PRODUCTS OR ITEMS NOTED AS "EXISTING" WHICH ARE NOT FOUND TO BE IN THE FIELD.
- 23. ERECTION SHALL BE DONE IN A WORKMANLIKE MANNER BY COMPETENT EXPERIENCED WORKMEN IN ACCORDANCE WITH APPLICABLE CODES AND THE BEST—ACCEPTED PRACTICE. ALL MEMBERS SHALL BE LAND PLUMB AND TRUE AS INDICATED ON THE DRAWINGS.
- 24. THE CONTRACTOR SHALL COORDINATE HIS WORK AND SCHEDULE HIS ACTIVITIES AND WORKING HOURS IN ACCORDANCE WITH THE REQUIREMENTS OF THE PROPERTY OWNER AND/OR PROPERTY MANAGEMENT COMPANY.
- 25. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATING HIS WORK WITH THE WORK OF OTHERS AS IT MAY RELATE TO RADIO EQUIPMENT, ANTENNAS AND ANY OTHER PORTIONS OF THE WORK.
- 26. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY INDICATED OR WHERE LOCAL CODES OR REGULATIONS MAY TAKE PRECEDENCE.
- 27. THE CONTRACTOR SHALL REPAIR ALL EXISTING SURFACES DAMAGED DURING CONSTRUCTION SUCH THAT THEY MATCH AND BLEND WITH ADJACENT SURFACES.
- 28. THE CONTRACTOR SHALL KEEP CONTRACT AREA CLEAN, HAZARD FREE AND DISPOSE OF ALL DEBRIS AND RUBBISH. EQUIPMENT NOT SPECIFIED AS REMAINING ON THE PROPERTY OF THE OWNER SHALL BE REMOVED. LEAVE PREMISES IN CLEAN CONDITIONS AND FREE FROM PAINT SPOTS, DUST OR SMUDGES OF ANY NATURE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING ALL ITEMS UNTIL COMPLETION OF CONSTRUCTION.
- 29. BEFORE FINAL ACCEPTANCE OF THE WORK, THE CONTRACTOR SHALL REMOVE ALL EQUIPMENT, TEMPORARY WORK, UNUSED AND USELESS MATERIALS, RUBBISH AND TEMPORARY STRUCTURES.
- 30. ALL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE 2005 CONNECTICUT STATE BUILDING CODE (INCLUDING AMENDMENTS) AND ALL OTHER APPLICABLE CODES AND ORDINANCES.
- 31. CONTRACTOR SHALL VISIT THE JOB SITE AND SHALL FAMILIARIZE HIMSELF WITH ALL CONDITIONS AFFECTING THE PROPOSED WORK AND SHALL MAKE PROVISIONS AS TO THE COST THEREOF. CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING HIMSELF WITH ALL CONTRACT DOCUMENTS, FIELD CONDITIONS AND DIMENSIONS AND CONFIRMING THAT THE WORK MAY BE ACCOMPLISHED AS SHOWN PRIOR TO PROCEEDING WITH CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER PRIOR TO THE COMMENCEMENT OF WORK.
- 32. PLANS ARE NOT TO BE SCALED. THESE PLANS ARE INTENDED TO BE A DIAGRAMMATIC OUTLINE ONLY UNLESS OTHERWISE NOTED. THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT AND APPURTENANCES, AND LABOR NECESSARY TO EFFECT ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
- 33. CONTRACTOR SHALL BE RESPONSIBLE FOR THE SAFETY OF THE WORK AREA, ADJACENT AREAS AND BUILDING OCCUPANTS THAT ARE LIKELY TO BE AFFECTED BY THE WORK UNDER THIS CONTRACT. WORK SHALL CONFORM TO ALL OSHA REQUIREMENTS.
- 34. CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK USING THE BEST CONSTRUCTION SKILLS AND ATTENTION. CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES AND PROCEDURES AND FOR COORDINATING ALL PORTIONS OF THE WORK UNDER CONTRACT, UNLESS OTHERWISE NOTED.

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- ENGINEERINGSURVEYING

TECTONIC Engineering & Survey
Consultants P.C.

1279 ROUTE 300 NEWBURGH, NY 12550 Phone: (845) 567-6656 Fax: (845) 567-8703

· · T · · Mobile · ·

T-MOBILE NORTHEAST LLC. 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 PHONE: (860) 692-7100



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CT11883C CT883/SPRINT S. WINDSOR 59 MCGUIRE RD S. WINDSOR, CT 06074

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NOTES

SHEET NUMBER

A-7

GROUNDING NOTES

- 1. THE ENTIRE ELECTRICAL INSTALLATION SHALL BE GROUNDED AS REQUIRED BY ALL APPLICABLE CODES.
- 2. ALL GROUNDING WORK SHALL BE IN ACCORDANCE WITH T-MOBILE STANDARD PRACTICE.
- 3. ALL BUS CONNECTORS SHALL BE TWO—HOLE, LONG—BARREL TYPE COMPRESSION LUGS, T&B OR EQUAL, UNLESS OTHERWISE NOTED ON DRAWINGS. ALL LUGS SHALL BE ATTACHED TO BUSSES USING BOLTS, NUTS, AND LOCK WASHERS. NO WASHERS ARE ALLOWED BETWEEN THE ITEMS BEING GROUNDED.
- 4. ALL CONNECTORS SHALL BE CRIMPED USING HYDRAULIC CRIMPING TOOLS, T&B #TBM 8 OR EQUIVALENT.
- 5. ALL CONNECTIONS SHALL BE MADE TO BARE METAL. ALL PAINTED SURFACES SHALL BE FILED TO ENSURE PROPER CONTACT. NO WASHERS ARE ALLOWED BETWEEN THE ITEMS BEING GROUNDED. ALL CONNECTIONS ARE TO HAVE A NON-OXIDIZING AGENT APPLIED PRIOR TO INSTALLATION.
- 6. ALL COPPER BUSSES SHALL BE CLEANED, POLISHED, AND A NON-OXIDIZING AGENT APPLIED. NO FINGERPRINTS OR DISCOLORED COPPER WILL BE PERMITTED.
- 7. ALL BENDS SHALL BE AS SHALLOW AS POSSIBLE, WITH NO TURN SHORTER THAN AN 8-INCH NOMINAL RADIUS.
- 8. GROUNDING CONDUCTORS SHALL BE SOLID TINNED COPPER AND ANNEALED #2. ALL GROUNDING CONDUCTORS SHALL RUN THROUGH PVC SLEEVES WHEREVER CONDUCTORS RUN THROUGH WALLS, FLOORS, OR CEILINGS. IF CONDUCTORS MUST RUN THROUGH EMT, BOTH ENDS OF CONDUIT SHALL BE GROUNDED. SEAL BOTH ENDS OF CONDUIT WITH SILICONE CAULK.
- 9. GROUNDING SYSTEM RESISTANCE SHALL NOT EXCEED 10 OHMS. IF THE RESISTANCE VALUE IS EXCEEDED, NOTIFY THE PROJECT MANAGER FOR FURTHER INSTRUCTION ON METHODS FOR REDUCING THE RESISTANCE VALUE.
- 10. ALL ROOF TOP ANTENNA MOUNTS SHALL BE GROUNDED WITH A #2 GROUND WIRE CONNECTED TO THE NEAREST GROUND BUS. ALL CONNECTIONS ARE TO BE CAD—WELDED IF POSSIBLE.
- 11. UPON COMPLETION OF WORK, CONDUCT CONTINUITY, SHORT CIRCUIT, AND FALL OF POTENTIAL GROUNDING TESTS FOR APPROVAL. SUBMIT TEST REPORTS TO THE PROJECT MANAGER.
- 12. GROUNDING CONNECTION TO TRAVEL IN A DOWNWARD DIRECTION.
- 13. ALL EXPOSED #2 WIRE MUST BE TINN NOT BTW.
- 14. TECTONIC TAKES NO RESPONSIBILITY OR LIABILITY FOR THE GROUNDING SYSTEM AS SHOWN ON THIS SITE. THIS IS A STANDARD GROUNDING SYSTEM.

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	SOMAL ENGINE
	SOUND ENGINEER

CT11883C CT883/SPRINT S. WINDSOR 59 MCGUIRE RD S. WINDSOR, CT 06074

SHEET TITLE NOTES

A-8

SHEET NUMBER

CONFIGURATION

REFER TO LATEST T-MOBILE RF DATA SHEET FOR FINAL RF DESIGN & BOM.

ORIGINAL SIZE IN INCHES