

Crown Castle 3530 Toringdon Way Suite 300 Charlotte, NC 28277 Tel: 704-405-6600

www.crowncastle.com

March 21, 2014

Melanie A. Bachman Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

RE: Sprint PCS-Exempt Modification - Crown Site BU: 803934

Sprint PCS Site ID: CT33XC554

Located at: 400 Main Street, Somers, CT 06071

Dear Ms. Bachman:

This letter and exhibits are submitted on behalf of Sprint PCS (Sprint). Sprint is making modifications to certain existing sites in its Connecticut system in order to implement their 2.5GHz LTE technology. Please accept this letter and exhibits as notification, pursuant to § 16-50j-73 of the Regulations of Connecticut State Agencies ("R.C.S.A."), of construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In compliance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Ms. Lisa Pellegrini, First Selectman of the Town of Somers.

Sprint plans to modify the existing wireless communications facility owned by Crown Castle and located at **400 Main Street, Somers, CT 06071**. Attached are a compound plan and elevation depicting the planned changes (Exhibit-1), and documentation of the structural sufficiency of the structure to accommodate the revised antenna configuration (Exhibit-2). Also included is a power density table report reflecting the modification to Sprint's operations at the site (Exhibit-3).

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes ("C.G.S.") § 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in the R.C.S.A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing tower. Sprint's additional antennas will be located at the same elevation on the existing tower.
- 2. There will be no proposed modifications to the ground and no extension of boundaries.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more.

- 4. A Structural Modification Report confirming that the tower and foundation can support Sprint's proposed modifications is included as Exhibit-2.
- 5. The operation of the additional antennas will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) adopted safety standard. A cumulative General Power Density table report for Sprint's modified facility is included as Exhibit-3.

For the foregoing reasons, Sprint respectfully submits the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Donna Neal.

Sincerely,

Jeff Barbadora

Real Estate Specialist

Jeff Barbla

### Enclosures

Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes

Tab 2: Exhibit-2: Structural Modification Report

Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)

cc: Ms. Lisa Pellegrini, First Selectman

Town of Somers 600 Main Street Somers, CT 06071



TOLLAND

PROJECT:

2.5 EQUIPMENT DEPLOYMENT

SITE NAME:

CT SOMERS FD CAC

SITE CASCADE:

CT33XC554

SITE NUMBER:

803934

SITE ADDRESS:

400 MAIN STREET **SOMERS, CT 06071** 

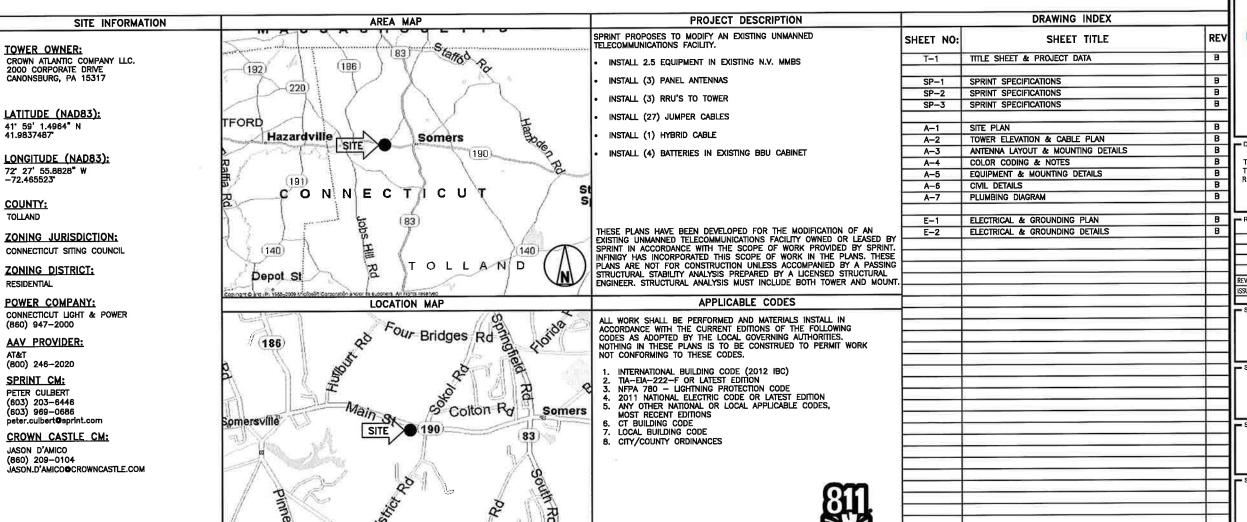
Know what's below. Call before you dig.

MONOPOLE TOWER

MARKET:

SITE TYPE:

NORTHERN CONNECTICUT





1033 Watervliet Shaker Albany, NY 12205 Office # (518) 690-0790 Fax # (518) 690-0793

JOB NUMBER 353-000



THESE DOCUMENTS ARE CONFIDENTIAL AND ARE THE SOLE PROPERTY OF SPRINT AND MAY NOT BE REPRODUCED, DISSEMINATED OR REDISTRIBUTED WITHOUT THE EXPRESS WRITTEN CONSENT OF

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	DESCRIPTION	DATE	BY	REV	
_					
	REVISED PER COMMENT	2/14/14	MAP	В	
	ISSUED FOR REVIEW	12/30/13	SKB	A	

CT SOMERS FD CAC

CT33XC554

400 MAIN STREET SOMERS, CT 06071

TITLE SHEET & PROJECT DATA

T-1

THESE OUTLINE SPECIFICATIONS IN CONJUNCTION WITH THE SPRINT STANDARD CONSTRUCTION SPECIFICATIONS, INCLUDING CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

#### SECTION 01 100 - SCOPE OF WORK

#### PART 1 - GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE SPRINT CONSTRUCTION STANDARDS FOR WIRELESS SITES, CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

#### 1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION
- B, SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.
- 1.3 PRECEDENCE: SHOULD CONFLICTS OCCUR BETWEEN THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES INCLUDING THE STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES AND THE CONSTRUCTION DRAWINGS, INFORMATION ON THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE. NOTIFY SPRINT CONSTRUCTION MANAGER IF THIS OCCURS.

#### 1.4 NATIONALLY RECOGNIZED CODES AND STANDARDS:

- A. THE WORK SHALL COMPLY WITH APPLICABLE NATIONAL AND LOCAL CODES AND STANDARDS, LATEST EDITION, AND PORTIONS THEREOF, INCLUDED BUT NOT LIMITED TO THE FOLLOWING:
- 1. GR-63-CORE NEBS REQUIREMENTS: PHYSICAL PROTECTION
- 5. GR-78-CORE GENERIC REQUIREMENTS FOR THE PHYSICAL DESIGN AND MANUFACTURE OF TELECOMMUNICATIONS EQUIPMENT.
- 3. GR-1089 CORE, ELECTROMAGNETIC COMPATIBILITY AND ELECTRICAL SAFETY
  -GENERIC CRITERIA FOR NETWORK TELECOMMUNICATIONS EQUIPMENT.
- NATIONAL FIRE PROTECTION ASSOCIATION CODES AND STANDARDS (NFPA) INCLUDING NFPA 70 (NATIONAL ELECTRICAL CODE — "NEC") AND NFPA 101 (LIFE SAFETY CODE).
- 5. AMERICAN SOCIETY FOR TESTING OF MATERIALS (ASTM)
- 6. INSTITUTE OF ELECTRONIC AND ELECTRICAL ENGINEERS (IEEE)
- 7. AMERICAN CONCRETE INSTITUTE (ACI)
- B. AMERICAN WIRE PRODUCERS ASSOCIATION (AWPA)
- 9. CONCRETE REINFORCING STEEL INSTITUTE (CRSI)
- 10. AMERICAN ASSOCIATION OF STATE HIGHWAY AND TRANSPORTATION OFFICIALS (AASHTO)
- 11, PORTLAND CEMENT ASSOCIATION (PCA)
- 12. NATIONAL CONCRETE MASONRY ASSOCIATION (NCMA)
- 13. BRICK INDUSTRY ASSOCIATION (BIA)
- 14. AMERICAN WELDING SOCIETY (AWS)
- 15. NATIONAL ROOFING CONTRACTORS ASSOCIATION (NRCA)
- 16. SHEET METAL AND AIR CONDITIONING CONTRACTORS' NATIONAL ASSOCIATION (SMACNA)
- 17. DOOR AND HARDWARE INSTITUTE (DHI)
- 1B. OCCUPATIONAL SAFETY AND HEALTH ACT (OSHA)
- 19. APPLICABLE BUILDING CODES INCLUDING UNIFORM BUILDING CODE, SOUTHERN BUILDING CODE, BOCA, AND THE INTERNATIONAL BUILDING CODE.

#### 1.5 DEFINITIONS:

- A. WORK: THE SUM OF TASKS AND RESPONSIBILITIES IDENTIFIED IN THE CONTRACT
- B. COMPANY: SPRINT CORPORATION
- C. ENGINEER: SYNONYMOUS WITH ARCHITECT & ENGINEER AND "A&E". THE DESIGN PROFESSIONAL HAVING PROFESSIONAL RESPONSIBILITY FOR DESIGN OF THE PROJECT.
- D. CONTRACTOR: CONSTRUCTION CONTRACTOR; CONSTRUCTION VENDOR; INDIVIDUAL OR ENTITY WHO AFTER EXECUTION OF A CONTRACT IS BOUND TO ACCOMPLISH THE WORK
- E. THIRD PARTY VENDOR OR AGENCY: A VENDOR OR AGENCY ENGAGED SEPARATELY BY THE COMPANY, A&E, OR CONTRACTOR TO PROVIDE MATERIALS OR TO ACCOMPLISH SPECIFIC TASKS RELATED TO BUT NOT INCLUDED IN THE WORK.
- F. OFCI: OWNER FURNISHED, CONTRACTOR INSTALLED EQUIPMENT.
- G. CONSTRUCTION MANAGER ALL PROJECTS RELATED COMMUNICATION TO FLOW THROUGH SPRINT REPRESENTATIVE IN CHARGE OF PROJECT...

- 1.6 SITE FAMILIARITY: CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING HIMSELF WITH ALL CONTRACT DOCUMENTS, FIELD CONDITIONS AND DIMENSIONS PRIOR TO PROCEEDING WITH CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE SPRINT CONSTRUCTION MANAGER PRIOR TO THE COMMENCEMENT OF WORK. NO COMPENSATION WILL BE AWARDED BASED ON CLAIM OF LACK OF KNOW FDGE OR FIELD CONDITIONS.
- 1.7 POINT OF CONTACT: COMMUNICATION BETWEEN SPRINT AND THE CONTRACTOR SHALL FLOW THROUGH THE SINGLE SPRINT CONSTRUCTION MANAGER APPOINTED TO MANAGE THE PROJECT FOR SPRINT.
- 1.8 ON-SITE SUPERVISION: THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE RESPONSIBLE FOR CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. THE CONTRACTOR SHALL EMPLOY A COMPETENT SUPERINTENDENT WHO SHALL BE IN ATTENDANCE AT THE SITE AT ALL TIMES DURING PERFORMANCE OF THE WORK.
- 1.9 DRAWINGS, SPECIFICATIONS AND DETAILS REQUIRED AT JOBSITE: THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A FULL SET OF THE CONSTRUCTION DRAWINGS, STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES AND THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES AT THE JOBSITE FROM MOBILIZATION THROUGH CONSTRUCTION COMPLETION.
- A. THE JOBSITE DRAWINGS, SPECIFICATIONS AND DETAILS SHALL BE CLEARLY MARKED DAILY IN RED PENCIL WITH ANY CHANGES IN CONSTRUCTION OVER WHAT IS DEPICTED IN THE DOCUMENTS. AT CONSTRUCTION COMPLETION, THIS JOBSITE MARKUP SET SHALL BE DELIVERED TO THE COMPANY OR COMPANY'S DESIGNATED REPRESENTATIVE TO BE FORWARDED TO THE COMPANY'S A&E VENDOR FOR PRODUCTION OF "AS—BUILTY DRAWINGS.
- B. DETAILS ARE INTENDED TO SHOW DESIGN INTENT. MODIFICATIONS MAY BE REQUIRED TO SUIT JOB DIMENSIONS OR CONDITIONS, AND SUCH MODIFICATIONS SHALL BE INCLUDED AS PART OF THE WORK. CONTRACTOR SHALL NOTIFY SPRINT CONSTRUCTION MANAGER OF ANY VARIATIONS PRIOR TO PROCEEDING WITH THE WORK.
- C. DIMENSIONS SHOWN ARE TO FINISH SURFACES UNLESS NOTED OTHERWISE.
  SPACING BETWEEN EQUIPMENT IS THE REQUIRED CLEARANCE. SHOULD THERE BE
  ANY QUESTIONS REGARDING THE CONTRACT DOCUMENTS, EXISTING CONDITIONS
  AND/OR DESIGN INTENT, THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING
  A CLARIFICATION FROM THE SPRINT CONSTRUCTION MANAGER PRIOR TO
  DEPOCEDIACE WITH THE WORK
- 1.10 USE OF JOB SITE: THE CONTRACTOR SHALL CONFINE ALL CONSTRUCTION AND RELATED OPERATIONS INCLUDING STAGING AND STORAGE OF MATERIALS AND EQUIPMENT, PARKING, TEMPORARY FACILITIES, AND WASTE STORAGE TO THE LEASE PARCEL UNLESS OTHERWISE PERMITTED BY THE CONTRACT DOCUMENTS.
- 1.11 UTILITIES SERVICES: WHERE NECESSARY TO CUT EXISTING PIPES, ELECTRICAL WIRES, CONDUITS, CABLES, ETC., OF UTILITY SERVICES, OR OF FIRE PROTECTION OR COMMUNICATIONS SYSTEMS, THEY SHALL BE CUT AND CAPPED AT SUITABLE PLACES OR WHERE SHOWN. ALL SUCH ACTIONS SHALL BE COORDINATED WITH THE UTILITY COMPANY INVOLVED:
- 1.12 PERMITS / FEES: WHEN REQUIRED THAT A PERMIT OR CONNECTION FEE BE PAID TO A PUBLIC UTILITY PROVIDER FOR NEW SERVICE TO THE CONSTRUCTION PROJECT, PAYMENT OF SUCH FEE SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR.
- 1.13 CONTRACTOR SHALL TAKE ALL MEASURES AND PROVIDE ALL MATERIAL NECESSARY FOR PROTECTING EXISTING EQUIPMENT AND PROPERTY.
- 1.14 METHODS OF PROCEDURE (MOPS) FOR CONSTRUCTION: CONTRACTOR SHALL PERFORM WORK AS DESCRIBED IN THE FOLLOWING INSTALLATION AND COMMISSIONING MOPS.

NOTE: IN SHORT-FORM SPECIFICATIONS ON THE DRAWINGS, A/E TO INSERT LIST OF APPLICABLE MOPS INCLUDING EN-2012-001, EN-2013-002, EL-0568, AND TS-0193

1.15 USE OF ELECTRONIC PROJECT MANAGEMENT SYSTEMS:

#### PART 2 - PRODUCTS (NOT USED)

#### PART 3 - EXECUTION

- 3.1 TEMPORARY UTILITIES AND FACILITIES: THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TEMPORARY UTILITIES AND FACILITIES NECESSARY EXCEPT AS OTHERWISE INDICATED IN THE CONSTRUCTION DOCUMENTS. TEMPORARY UTILITIES AND FACILITIES INCLUDE POTABLE WATER, HEAT, HVAC, ELECTRICITY, SANITARY FACILITIES, WASTE DISPOSAL FACILITIES, AND TELEPHONE/COMMUNICATION SERVICES. PROVIDE TEMPORARY UTILITIES AND FACILITIES IN ACCORDANCE WITH OSHA AND THE AUTHORITY HAVING JURISDICTION. CONTRACTOR MAY UTILIZE THE COMPANY ELECTRICAL SERVICE IN THE COMPLETION OF THE WORK WHEN IT BECOMES AVAILABLE. USE OF THE LESSORS OR SITE OWNER'S UTILITIES OF FACILITIES IS EXPRESSLY FORBIDDEN EXCEPT AS OTHERWISE ALLOWED IN THE CONTRACT DOCUMENTS.
- 3.2 ACCESS TO WORK: THE CONTRACTOR SHALL PROVIDE ACCESS TO THE JOB SITE FOR AUTHORIZED COMPANY PERSONNEL AND AUTHORIZED REPRESENTATIVES OF THE ARCHITECT/ENGINEER DURING ALL PHASES OF THE WORK.
- 3.3 TESTING: REQUIREMENTS FOR TESTING BY THIS CONTRACTOR SHALL BE AS INDICATED HEREWITH, ON THE CONSTRUCTION DRAWINGS, AND IN THE INDIVIDUAL SECTIONS OF THESE SPECIFICATIONS. SHOULD COMPANY CHOOSE TO ENGAGE ANY THIRD-PARTY TO CONDUCT ADDITIONAL TESTING, THE CONTRACTOR SHALL COOPERATE WITH AND PROVIDE A WORK AREA FOR COMPANY'S TEST AGENCY.
- 3.4 DIMENSIONS: VERIFY DIMENSIONS INDICATED ON DRAWINGS WITH FIELD DIMENSIONS BEFORE FABRICATION OR ORDERING OF MATERIALS. DO NOT SCALE DRAWINGS.

3.5 EXISTING CONDITIONS: NOTIFY THE SPRINT CONSTRUCTION MANAGER OF EXISTING CONDITIONS DIFFERING FROM THOSE INDICATED ON THE DRAWINGS, DO NOT REMOVE OR ALTER STRUCTURAL COMPONENTS WITHOUT PRIOR WRITTEN APPROVAL FROM THE ARCHITECT AND ENGINEER.

### SECTION 01 200 — COMPANY FURNISHED MATERIAL AND EQUIPMENT PART 1 — GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

#### 1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.
- PART 2 PRODUCTS (NOT USED)

#### PART 3 - EXECUTION

- 3.1 RECEIPT OF MATERIAL AND EQUIPMENT:
- A. A COMPANY FURNISHED MATERIAL AND EQUIPMENT IS IDENTIFIED ON THE RF DATA SHEET IN THE CONSTRUCTION DOCUMENTS.
- B. THE CONTRACTOR IS RESPONSIBLE FOR SPRINT PROVIDED MATERIAL AND EQUIPMENT AND UPON RECEIPT SHALL:
- 1 ACCEPT DELIVERIES AS SHIPPED AND TAKE RECEIPT.
- 2. VERIFY COMPLETENESS AND CONDITION OF ALL DELIVERIES.
- 3. TAKE RESPONSIBILITY FOR EQUIPMENT AND PROVIDE INSURANCE PROTECTION AS REQUIRED IN AGREEMENT.
- RECORD ANY DEFECTS OR DAMAGES AND WITHIN TWENTY—FOUR HOURS AFTER RECEIPT, REPORT TO SPRINT OR ITS DESIGNATED PROJECT REPRESENTATIVE OF SUCH.
- 5. PROVIDE SECURE AND NECESSARY WEATHER PROTECTED WAREHOUSING.
- COORDINATE SAFE AND SECURE TRANSPORTATION OF MATERIAL AND EQUIPMENT, DELIVERING AND OFF-LOADING FROM CONTRACTOR'S WAREHOUSE TO SIFE

#### 3.2 DELIVERABLES:

- A. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.
- B. IF APPLICABLE, COMPLETE LOST/STOLEN/DAMAGED DOCUMENTATION REPORT AS NECESSARY IN ACCORDANCE WITH COMPANY PRACTICE, AND AS DIRECTED BY COMPANY
- C. UPLOAD DOCUMENTATION INTO SPRINT SITE MANAGEMENT SYSTEM (SMS) AND/OR PROVIDE HARD COPY DOCUMENTATION AS REQUESTED.

### SECTION 01 300 - CELL SITE CONSTRUCTION CO.

#### PART 1 - GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

#### 1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.

#### 1.3 NOTICE TO PROCEED

- A. NO WORK SHALL COMMENCE PRIOR TO COMPANY'S WRITTEN NOTICE TO PROCEED AND THE ISSUANCE OF THE WORK ORDER.
- B. UPON RECEIVING NOTICE TO PROCEED, CONTRACTOR SHALL FULLY PERFORM ALL WORK NECESSARY TO PROVIDE SPRINT WITH AN OPERATIONAL WIRELESS FACILITY TOWER OWNER NOTIFICATION.

  ONCE THE CONTRACTOR HAS RECEIVED AND ACCEPTED THE NOTICE TO PROCEED,

CONTRACTOR WILL CONTACT THE CROWN CASTLE CONSTRUCTION MANAGER OF RECORD (NOTED ON THE FIRST PAGE ON THIS CONSTRUCTION DRAWING) A MINIMUM OF 48 HOURS PRIOR TO WORK START. UPON ARRIVAL TO THE JOB SITE, CONTRACTOR CREW IS REQUIRED CALL 1-800-788-7011 TO NOTIFY THE CROWN CASTLE NOC WORK HAS BEGUN.

PART 2 - PRODUCTS (NOT USED)

#### PART 3 - EXECUTION

- 3.1 FUNCTIONAL REQUIREMENTS:
- A. THE ACTIVITIES DESCRIBED IN THIS PARAGRAPH REPRESENT MINIMUM ACTIONS AND PROCESSES REQUIRED TO SUCCESSFULLY COMPLETE THE WORK. THE ACTIVITIES DESCRIBED ARE NOT EXHAUSTIVE, AND CONTRACTOR SHALL TAKE ANY AND ALL ACTIONS AS NECESSARY TO SUCCESSFULLY COMPLETE THE CONSTRUCTION OF A FULLY FUNCTIONING WIRELESS FACILITY AT THE SITE IN ACCORDANCE WITH COMPANY PROCESSES.
- B. SUBMIT SPECIFIC DOCUMENTATION AS INDICATED HEREIN, AND OBTAIN REQUIRED APPROVALS WHILE THE WORK IS BEING PERFORMED.
- C. MANAGE AND CONDUCT ALL FIELD CONSTRUCTION SERVICE RELATED ACTIVITIES
- D. PROVIDE CONSTRUCTION ACTIVITIES TO THE EXTENT REQUIRED BY THE CONTRACT DOCUMENTS, INCLUDING BUT NOT LIMITED TO THE FOLLOWING:

PLANS PREPARED FOR:



- PLANS PREPARED BY:

MLA PARTNER

## INFINIGY Build. Bellver.

1033 Watervliet Shaker Ro Albany, NY 12205 Office # (518) 690-0790 Fax # (518) 690-0793

JOB NUMBER 353-000



PENGINEERING LICENSE:

OF CONNECTION
S. STERRING
No. 24705

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P DRAWING NOTICE:

THESE DOCUMENTS ARE CONFIDENTIAL AND ARE
THE SOLE PROPERTY OF SPRINT AND MAY NOT BE
REPRODUCED, DISSEMINATED OR REDISTRIBUTED
WITHOUT THE EXPRESS WRITTEN CONSENT OF
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REVISIONS:			
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REVISED PER COMMENT	2/14/14	MAP	В
ISSUED FOR REVIEW	12/30/13	SKB	A

SITE NAME:

CT SOMERS FD CAC

SITE CASCADE: -

CT33XC554

SITE ADDRESS

400 MAIN STREET SOMERS, CT 06071

- SHEET DESCRIPTION: -

SPRINT SPECIFICATIONS

SHEET NUMBER: -

SP-1

#### CONTINUE FROM SP-1

- 1. PERFORM ANY REQUIRED SITE ENVIRONMENTAL MITIGATION.
- PREPARE GROUND SITES; PROVIDE DE-GRUBBING; AND ROUGH AND FINAL GRADING, AND COMPOUND SURFACE TREATMENTS.
- 3. MANAGE AND CONDUCT ALL ACTIVITIES FOR INSTALLATION OF UTILITIES INCLUDING ELECTRICAL AND TELCO BACKHAUL.
- 4. INSTALL UNDERGROUND FACILITIES INCLUDING UNDERGROUND POWER AND COMMUNICATIONS CONDUITS, AND UNDERGROUND GROUNDING SYSTEM.
- 5. INSTALL ABOVE GROUND GROUNDING SYSTEMS.
- 6. PROVIDE NEW HVAC INSTALLATIONS AND MODIFICATIONS.
- 7. INSTALL "H-FRAMES", CABINETS AND SHELTERS AS INDICATED.
- 8. INSTALL ROADS, ACCESS WAYS, CURBS AND DRAINS AS INDICATED.
- 9. ACCOMPLISH REQUIRED MODIFICATION OF EXISTING FACILITIES.
- 10. PROVIDE ANTENNA SUPPORT STRUCTURE FOUNDATIONS.
- 11. PROVIDE SLABS AND EQUIPMENT PLATFORMS.
- 12. INSTALL COMPOUND FENCING, SIGHT SHIELDING, LANDSCAPING AND ACCESS
- 13. PERFORM INSPECTION AND MATERIAL TESTING AS REQUIRED HEREINAFTER.
- 14. CONDUCT SITE RESISTANCE TO EARTH TESTING AS REQUIRED HEREINAFTER
- 15. INSTALL FIXED GENERATOR SETS AND OTHER STANDBY POWER SOLUTIONS.
- 16. INSTALL TOWERS, ANTENNA SUPPORT STRUCTURES AND PLATFORMS ON EXISTING TOWERS AS REQUIRED.
- 17. INSTALL CELL SITE RADIOS, MICROWAVE, GPS, COAXIAL MAINLINE, ANTENNAS, CROSS BAND COUPLERS, TOWER TOP AMPLIFIERS, LOW NOISE AMPLIFIERS AND RELATED EQUIPMENT.
- 18. PERFORM, DOCUMENT, AND CLOSE OUT ANY CONSTRUCTION CONTROL DOCUMENTS THAT MAY BE REQUIRED BY GOVERNMENT AGENCIES AND LANDLORDS
- 19. PERFORM ANTENNAL AND COAX SWEEP TESTING AND MAKE ANY AND ALL NECESSARY CORRECTIONS.
- 20. REMAIN ON SITE MOBILIZED THROUGHOUT HAND-OFF AND INTEGRATION TO ASSIST AS NEEDED UNTIL SITE IS DEEMED SUBSTANTIALLY COMPLETE AND PLACED "ON AIR"

#### 3.2 GENERAL REQUIREMENTS FOR CIVIL CONSTRUCTION:

- A. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH. AT THE COMPLETION OF THE WORK, CONTRACTOR SHALL REMOVE FROM THE SITE ALL REMAINING RUBBISH, IMPLEMENTS, TEMPORARY FACILITIES. AND SURPLUS MATERIALS.
- B. EQUIPMENT ROOMS SHALL AT ALL TIMES BE MAINTAINED "BROOM CLEAN" AND CLEAR OF DEBRIS.
- C. CONTRACTOR SHALL TAKE ALL REASONABLE PRECAUTIONS TO DISCOVER AND LOCATE ANY HAZARDOUS CONDITION.
- 1. IN THE EVENT CONTRACTOR ENCOUNTERS ANY HAZARDOUS CONDITION WHICH HAS NOT BEEN ABATED OR OTHERWISE MITIGATED, CONTRACTOR AND ALL OTHER PERSONS SHALL IMMEDIATELY STOP WORK IN THE AFFECTED AREA AND NOTIFY COMPANY IN WRITING. THE WORK IN THE AFFECTED AREA SHALL NOT BE RESUMED EXCEPT BY WRITTEN NOTIFICATION BY COMPANY.
- CONTRACTOR AGREES TO USE CARE WHILE ON THE SITE AND SHALL NOT TAKE ANY ACTION THAT WILL OR MAY RESULT IN OR CAUSE THE HAZARDOUS CONDITION TO BE FURTHER RELEASED IN THE ENVIRONMENT, OR TO FURTHER EXPOSE INDIVIDUALS TO THE HAZARD.
- D. CONTRACTOR'S ACTIVITIES SHALL BE RESTRICTED TO THE PROJECT LIMITS. SHOULD AREAS OUTSIDE THE PROJECT LIMITS BE AFFECTED BY CONTRACTOR'S ACTIVITIES, CONTRACTOR SHALL IMMEDIATELY RETURN THEM TO ORIGINAL CONDITION
- E. CONDUCT TESTING AS REQUIRED HEREIN.

#### 3.3 DELIVERABLES:

- A. CONTRACTOR SHALL REVIEW, APPROVE, AND SUBMIT TO SPRINT SHOP DRAWINGS, PRODUCT DATA, SAMPLES, AND SIMILAR SUBMITTALS AS REQUIRED HEREINAFTER
- B. PROVIDE DOCUMENTATION INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING. DOCUMENTATION SHALL BE FORWARDED IN ORIGINAL FORMAT AND/OR UPLOADED INTO SMS.
- 1. ALL CORRESPONDENCE AND PRELIMINARY CONSTRUCTION REPORTS.
- 2. PROJECT PROGRESS REPORTS.
- 3. CML CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- ELECTRICAL SERVICE COMPLETION DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).

- LINES AND ANTENNA INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- POWER INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- TELCO READY DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- 8. PPC (OR SHELTER) INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- TOWER CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- TOWER CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- BTS AND RADIO EQUIPMENT DELIVERED AT SITE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- 12. NETWORK OPERATIONS HANDOFF CHECKLIST (HOC WALK) COMPLETE (UPLOAD FORM IN SMS)
- CIVIL CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- 14. SITE CONSTRUCTION PROGRESS PHOTOS UNLOADED INTO SMS.

#### SECTION 01 400 - SUBMITTALS & TESTS

#### PART 1 - GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

#### 1.2 RELATED DOCUMENTS:

- THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.

#### 1.3 SUBMITTALS

- A. THE WORK IN ALL ASPECTS SHALL COMPLY WITH THE CONSTRUCTION DRAWINGS AND THESE SPECIFICATIONS.
- B. SUBMIT THE FOLLOWING TO COMPANY REPRESENTATIVE FOR APPROVAL.
  - CONCRETE MIX—DESIGNS FOR TOWER FOUNDATIONS, ANCHORS PIERS, AND CONCRETE PAYING.
  - 2. CONCRETE BREAK TESTS AS SPECIFIED HEREIN.
  - 3. SPECIAL FINISHES FOR INTERIOR SPACES, IF ANY.
  - 4. ALL EQUIPMENT AND MATERIALS SO IDENTIFIED ON THE CONSTRUCTION DRAWINGS.
  - 5. CHEMICAL GROUNDING DESIGN
- D. ALTERNATES: AT THE COMPANY'S REQUEST, ANY ALTERNATIVES TO THE MATERIALS OR METHODS SPECIFIED SHALL BE SUBMITTED TO SPRINT'S CONSTRUCTION MANAGER FOR APPROVAL PRIOR TO BEING SHIPPED TO SITE. SPRINT WILL REVIEW AND APPROVE ONLY THOSE REQUESTS MADE IN WRITING. NO VERBAL APPROVALS WILL BE CONSIDERED. SUBMITTAL FOR APPROVAL SHALL INCLUDE A STATEMENT OF COST REDUCTION PROPOSED FOR USE OF ALTERNATE PRODUCT.

#### 1.4 TESTS AND INSPECTIONS:

- A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL CONSTRUCTION TESTS, INSPECTIONS AND PROJECT DOCUMENTATION.
- B. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
  - COAX SWEEPS AND FIBER TESTS PER TS-0200 REV 4 ANTENNA LINE ACCEPTANCE STANDARDS.
- AGL, AZIMUTH AND DOWNTILT USING ELECTRONIC COMMERCIAL MADE-FOR-THE-PURPOSE ANTENNA ALIGNMENT TOOL.
- CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF TESTING.
- C. REQUIRED CLOSEOUT DOCUMENTATION INCLUDES, BUT IS NOT LIMITED TO THE FOLLOWING;
  - . AZIMUTH, DOWNTILT, AGL UPLOAD REPORT FROM ANTENNA ALIGNMENT TOOL TO SITERRA TASK 465. INSTALLED AZIMUTH, DOWNTILT, AND AGL MUST CONFORM TO THE RF DATA SHEETS. SWEEP AND FIBER TESTS
  - SCANABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT
- 3. ALL AVAILABLE JURISDICTIONAL INFORMATION
- 4. PDF SCAN OF REDLINES PRODUCED IN FIELD

5. ELECTRONIC AS—BUILT DRAWINGS IN AUTOCAD AND PDF FORMATS. ANY FIELD CHANGE MUST BE REFLECTED BY MODIFYING THE PLANS, ELEVATIONS, AND DETAILS IN THE DRAWING SETS. GENERAL NOTES INDICATING MODIFICATIONS WILL NOT BE ACCEPTED. CHANGES SHALL BE HIGHLIGHTED AS "CLOUDS" IDENTIFIED AS THE "AS—BUILT" CONDITION.

- 6. LIEN WAIVERS
- 7. FINAL PAYMENT APPLICATION
- 8. REQUIRED FINAL CONSTRUCTION PHOTOS
- 9 . CONSTRUCTION AND COMMISSIONING CHECKLIST COMPLETE WITH NO DEFICIENT ITEMS
- ALL POST NTP TASKS INCLUDING DOCUMENT UPLOADS COMPLETED IN SITERRA (SPRINTS DOCUMENT REPOSITORY OF RECORD).
- 1.5 COMMISSIONING: PERFORM ALL COMMISSIONING AS REQUIRED BY APPLICABLE
- 1.6 INTEGRATION: PERFORM ALL INTEGRATION ACTIVITIES AS REQUIRED BY APPLICABLE

PART 2 - PRODUCTS (NOT USED)

PART 3 - EXECUTION

#### 3.1 REQUIREMENTS FOR TESTING:

- A. THIRD PARTY TESTING AGENCY:
- 1. WHEN THE USE OF A THIRD PARTY INDEPENDENT TESTING AGENCY IS REQUIRED, THE AGENCY THAT IS SELECTED MUST PERFORM SUCH WORK ON A REGULAR BASIS IN THE STATE WHERE THE PROJECT IS LOCATED AND HAVE A THOROUGH UNDERSTANDING OF LOCAL AVAILABLE MATERIALS, INCLUDING THE SOIL, ROCK, AND GROUNDWATER CONDITIONS.
- 2. THE THIRD PARTY TESTING AGENCY IS TO BE FAMILIAR WITH THE APPLICABLE REQUIREMENTS FOR THE TESTS TO BE DONE, EQUIPMENT TO BE USED, AND ASSOCIATED HEALTH AND SAFETY ISSUES.
- 3. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASJTO, AND OTHER METHODS IS NEEDED.
- 4. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASJTO, AND OTHER METHODS IS NEEDED.

#### 3.2 REQUIRED TESTS:

- A. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE
  - CONCRETE CYLINDER BREAK TESTS FOR THE TOWER AND ANCHOR FOUNDATIONS AS SPECIFIED IN SECTION: PORTLAND CEMENT CONCRETE PAVING.
- ASPHALT ROADWAY COMPACTED THICKNESS, SURFACE SMOOTHNESS, AND COMPACTED DENSITY TESTING AS SPECIFIED IN SECTION: HOT MIX ASPHALT PAYING.
- FIELD QUALITY CONTROL TESTING AS SPECIFIED IN SECTION: PORTLAND CEMENT CONCRETE PAVING.
- 4. TESTING REQUIRED UNDER SECTION: AGGREGATE BASE FOR ACCESS ROADS, PADS AND ANCHOR LOCATIONS
- 5. STRUCTURAL BACKFILL COMPACTION TESTS FOR THE TOWER FOUNDATION.
- 6. SITE RESISTANCE TO EARTH TESTING PER EXHIBIT: CELL SITE GROUNDING SYSTEM DESIGN.
- ANTENNA AND COAX SWEEP TESTS PER EXHIBIT: ANTENNA TRANSMISSION LINE ACCEPTANCE STANDARDS.
- 8. GROUNDING AT ANTENNA MASTS FOR GPS AND ANTENNAS
- 9. ALL OTHER TESTS REQUIRED BY COMPANY OR JURISDICTION.

#### 3.3 REQUIRED INSPECTIONS

- A. SCHEDULE INSPECTIONS WITH COMPANY REPRESENTATIVE.
- B. CONDUCT INSPECTIONS INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
- GROUNDING SYSTEM INSTALLATION PRIOR TO EARTH CONCEALMENT DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
- FORMING FOR CONCRETE AND REBAR PLACEMENT PRIOR TO POUR DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
- COMPACTION OF BACKFILL MATERIALS; AGGREGATE BASE FOR ROADS, PADS, AND ANCHORS; ASPHALT PAVING; AND SHAFT BACKFILL FOR CONCRETE AND WOOD POLES, BY INDEPENDENT THIRD PARTY AGENCY.
- PRE— AND POST—CONSTRUCTION ROOFTOP AND STRUCTURAL INSPECTIONS ON EXISTING FACILITIES.

  TOWER EPECTION SECTION STACKING AND PLATFORM ATTACHMENT DOCUMENTED.
- TOWER ERECTION SECTION STACKING AND PLATFORM ATTACHMENT DOCUMENTED BY DIGITAL PHOTOGRAPHS BY THIRD PARTY AGENCY.
- 6. ANTENNA AZIMUTH , DOWN TILT AND PER SUNLIGHT TOOL SUNSIGHT INSTRUMENTS ANTENNALIGN ALIGNMENT TOOL (AAT)

Sprint

6580 Sprint Parkway
Overland Park, Kansas 66251

PLANS PREPARED BY:

MLA PARTNER

INFINIGY Build.

Belliver.

1033 Watervliet Shaker Rd Albany, NY 12205 Office # (518) 690-0790 Fax # (518) 690-0793

JOB NUMBER 353-000

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- SITE NAME

CT SOMERS FD CAC

SITE CASCADE: --

CT33XC554

SITE ADDRESS.

400 MAIN STREET SOMERS, CT 06071

SHEET DESCRIPTION: -

SPRINT SPECIFICATIONS

SHEET NUMBER:

SP-2

#### CONTINUE FROM SP-2

- VERIFICATION DOCUMENTED WITH THE ANTENNA CHECKLIST REPORT, BY A&E, SITE DEVELOPMENT REP, OR RF REP.
- 8. FINAL INSPECTION CHECKLIST AND HANDOFF WALK (HOC.). SIGNED FORM SHOWING ACCEPTANCE BY FIELD OPS IS TO BE UPLOADED INTO SMS.
- 9. COAX SWEEP AND FIBER TESTING DOCUMENTS SUBMITTED VIA SMS FOR RF
- 10. SCAN-ABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT
- 11. ALL AVAILABLE JURISDICTIONAL INFORMATION
- 12. PDF SCAN OF REDLINES PRODUCED IN FIELD
- C. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR
- D. CONSTRUCTION INSPECTIONS AND CORRECTIVE MEASURES SHALL BE DOCUMENTED BY THE CONTRACTOR WITH WRITTEN REPORTS AND PHOTOGRAPHS. PHOTOGRAPHS MUST BE DIGITAL AND OF SUFFICIENT QUALITY TO CLEARLY SHOW THE SITE CONSTRUCTION. PHOTOGRAPHS MUST CLEARLY IDENTIFY THE PHOTOGRAPHED ITEM AND BE LABELED WITH THE SITE CASCADE NUMBER, SITE NAME, DESCRIPTION, AND
- 3.4 DELIVERABLES: TEST AND INSPECTION REPORTS AND CLOSEOUT DOCUMENTATION SHALL BE UPLOADED TO THE SMS AND/OR FORWARDED TO SPRINT FOR INCLUSION INTO THE
- A. THE FOLLOWING TEST AND INSPECTION REPORTS SHALL BE PROVIDED AS APPLICABLE.
- 1. CONCRETE MIX AND CYLINDER BREAK REPORTS.
- 2. STRUCTURAL BACKFILL COMPACTION REPORTS
- SITE RESISTANCE TO EARTH TEST.
- 4. ANTENNA AZIMUTH AND DOWN TILT VERIFICATION
- 5. TOWER ERECTION INSPECTIONS AND MEASUREMENTS DOCUMENTING TOWER INSTALLED PER SUPPLIER'S REQUIREMENTS AND THE APPLICABLE SECTIONS
- 6. COAX CABLE SWEEP TESTS PER COMPANY'S "ANTENNA LINE ACCEPTANCE
- B. REQUIRED CLOSEOUT DOCUMENTATION INCLUDES THE FOLLOWING;
- 1. TEST WELLS AND TRENCHES: PHOTOGRAPHS OF ALL TEST WELLS; PHOTOGRAPHS SHOWING ALL OPEN EXCAVATIONS AND TRENCHING PRIOR TO BACKFILLING SHOWING A TAPE MEASURE VISIBLE IN THE EXCAVATIONS
- 2. CONDUITS, CONDUCTORS AND GROUNDING: PHOTOGRAPHS SHOWING TYPICAL INSTALLATION OF CONDUCTORS AND CONNECTORS; PHOTOGRAPHS SHOWING TYPICAL BEND RADIUS OF INSTALLED GROUND WIRES AND GROUND ROD
- 3. CONCRETE FORMS AND REINFORCING: CONCRETE FORMING AT TOWER AND EQUIPMENT/SHELTER PAD/FOUNDATIONS — PHOTOGRAPHS SHOWING ALL REINFORCING STEEL, UTILITY AND CONDUIT STUB OUTS; PHOTOGRAPHS SHOWING CONCRETE POUR OF SHELTER SLAB/FOUNDATION, TOWER FOUNDATION AND GUY ANCHORS WITH VIBRATOR IN USE; PHOTOGRAPHS SHOWING EACH ANCHOR ON GUYED TOWERS, BEFORE CONCRETE POUR.
- 4. TOWER, ANTENNAS AND MAINLINE: INSPECTION AND PHOTOGRAPHS OF SECTION STACKING; INSPECTION AND PHOTOGRAPHS OF PLATFORM COMPONENT ATTACHMENT POINTS; PHOTOGRAPHS OF TOWER TOP GROUNDING; PHOTOS OF TOWER COAX LINE COLOR CODING AT THE TOP AND AT GROUND LEVEL; INSPECTION AND PHOTOGRAPHS OF OPERATIONAL OF TOWER LIGHTING, AND PLACEMENT OF FAA REGISTRATION SIGN; PHOTOGRAPHS SHOWING ADDITIONAL GROUNDING POINTS FOR TOWERS GREATER THAN 200 FEET.; PHOTOS OF GROUNDING POINTS FOR TOWERS GREATER IHAN 200 FEEL; PHOTOS OF ANTENNA GROUND BAR, EQUIPMENT GROUND BAR, AND MASTER GROUND BAR; PHOTOS OF GPS ANTENNA(S); PHOTOS OF EACH SECTOR OF ANTENNAS; ONE PHOTOGRAPH LOOKING AT THE SECTOR AND ONE FROM BEHIND SHOWING THE PROJECTED COVERAGE AREA; PHOTOS OF COAX WEATHERPROOFING — TOP AND BOTTOM; PHOTOS OF COAX GROUNDING—TOP AND BOTTOM; PHOTOS OF ANTENNA AND MAST GROUNDING; PHOTOS OF COAX CABLE ENTRY INTO SHELTER; PHOTOS OF PLATFORM MECHANICAL CONNECTIONS TO TOWER/MONOPOLE.
- 5. ROOF TOPS: PRE—CONSTRUCTION AND POST—CONSTRUCTION VISUAL INSPECTION AND PHOTOGRAPHS OF THE ROOF AND INTERIOR TO DETERMINE AND DOCUMENT CONDITIONS; ROOF TOP CONSTRUCTION INSPECTIONS AS REQUIRED BY THE JURISDICTION; PHOTOGRAPHS OF CABLE TRAY AND/OR ICE BRIDGE; PHOTOGRAPHS OF DOGHOUSE/CABLE EXIT FROM ROOF;
- 6. SITE LAYOUT PHOTOGRAPHS OF THE OVERALL COMPOUND, INCLUDING EQUIPMENT PLATFORM FROM ALL FOUR CORNERS.
- 7. FINISHED UTILITIES: CLOSE-UP PHOTOGRAPHS OF THE PPC BREAKER PANEL; CLOSE-UP PHOTOGRAPH OF THE INSIDE OF THE TELCO PANEL AND NIU; CLOSE-UP PHOTOGRAPH OF THE POWER METER AND DISCONNECT; PHOTOS OF POWER AND TELCO ENTRANCE TO COMPANY ENCLOSURE; PHOTOGRAPHS AT METER BOX AND/OR FACILITY DISTRIBUTION PANEL.
- REQUIRED MATERIALS CERTIFICATIONS: CONCRETE MIX DESIGNS; MILL CERTIFICATION FOR ALL REINFORCING AND STRUCTURAL STEEL; AND ASPHALT
- 9. ANY AND ALL SUBMITTALS BY THE JURISDICTION OR COMPANY.

#### SECTION 01 400 - SUBMITTALS & TESTS

#### PART 1 — GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

#### 1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.

#### PART 2 - PRODUCTS (NOT USED)

#### PART 3 - EXECUTION

#### 3.1 WEEKLY REPORTS:

- A. CONTRACTOR SHALL PROVIDE SPRINT WITH WEEKLY REPORTS SHOWING PROJECT STATUS. THIS STATUS REPORT FORMAT WILL BE PROVIDED TO THE CONTRACTOR BY SPRINT. THE REPORT WILL CONTAIN SITE ID NUMBER, THE MILESTONES FOR EACH SITE, INCLUDING THE BASELINE DATE, ESTIMATED COMPLETION DATE AND ACTUAL
- B. REPORT INFORMATION WILL BE TRANSMITTED TO SPRINT VIA ELECTRONIC MEANS AS REQUIRED. THIS INFORMATION WILL PROVIDE A BASIS FOR PROGRESS MONITORING AND PAYMENT.

#### 3.2 PROJECT CONFERENCE CALLS:

A. SPRINT MAY HOLD WEEKLY PROJECT CONFERENCE CALLS. CONTRACTOR WILL BE REQUIRED TO COMMUNICATE SITE STATUS, MILESTONE COMPLETIONS AND UPCOMING MILESTONE PROJECTIONS, AND ANSWER ANY OTHER SITE STATUS QUESTIONS AS INCRESSED

#### 3.3 PROJECT TRACKING IN SMS:

A. CONTRACTOR SHALL PROVIDE SCHEDULE UPDATES AND PROJECTIONS IN THE SMS SYSTEM ON A WEEKLY BASIS.

A. ADDITIONAL OR ALTERNATE REPORTING REQUIREMENTS MAY BE ADDED TO THE REPORT AS DETERMINED TO BE REASONABLY NECESSARY BY COMPANY.

- A. FILE DIGITAL PHOTOGRAPHS OF COMPLETED SITE IN JPEG FORMAT IN THE SMS PHOTO LIBRARY FOR THE RESPECTIVE SITE. PHOTOGRAPHS SHALL BE CLEARLY LABELED WITH SITE NUMBER, NAME AND DESCRIPTION, AND SHALL INCLUDE AT A MINIMUM THE FOLLOWING AS APPLICABLE:
- 1. 1SHELTER AND TOWER OVERVIEW
- 2. TOWER FOUNDATION(S) FORMS AND STEEL BEFORE POUR (EACH ANCHOR ON GUYED TOWERS)
- 3. TOWER FOUNDATION(S) POUR WITH VIBRATOR IN USE (EACH ANCHOR ON GUYED TOWERS).
- 4. TOWER STEEL AS BEING INSTALLED INTO HOLE (SHOW ANCHOR STEEL ON GUYED TOWERS).
- 5. PHOTOS OF TOWER SECTION STACKING.
- 6. CONCRETE TESTING / SAMPLES.
- 7. PLACING OF ANCHOR BOLTS IN TOWER FOUNDATION.
- 8. BUILDING/WATER TANK FROM ROAD FOR TENANT IMPROVEMENTS OR COMMENTS.
- 9. SHELTER FOUNDATION -- FORMS AND STEEL BEFORE POURING.
- 10. SHELTER FOUNDATION POUR WITH VIBRATOR IN USE.
- 11. COAX CABLE ENTRY INTO SHELTER.
- 12. PLATFORM MECHANICAL CONNECTIONS TO TOWER/MONOPOLE.
- 13. ROOFTOP PRE AND POST CONSTRUCTION PHOTOS TO INCLUDE PENETRATIONS
- 14. PHOTOS OF TOWER TOP COAX LINE COLOR CODING AND COLOR CODING AT GROUND LEVEL.
- 15. PHOTOS OF ALL APPROPRIATE COMPANY OR REGULATORY SIGNAGE.
- 16. PHOTOS OF EQUIPMENT BOLT DOWN INSIDE SHELTER
- 17. POWER AND TELCO ENTRANCE TO COMPANY ENCLOSURE AND POWER AND TELCO SUPPLY LOCATIONS INCLUDING METER/DISCONNECT.
- 18. ELECTRICAL TRENCH(S) WITH ELECTRICAL / CONDUIT BEFORE BACKFILL
- 19. ELECTRICAL TRENCH(S) WITH FOIL-BACKED TAPE BEFORE FURTHER BACKFILL.
- 20. TELCO TRENCH WITH TELEPHONE / CONDUIT BEFORE BACKFILL.
- 21. TELCO TRENCH WITH FOIL-BACKED TAPE BEFORE FURTHER BACKFILL
- 22. SHELTER GROUND-RING TRENCH WITH GROUND-WIRE BEFORE BACKFILL (SHOW ALL CAD WELDS AND BEND RADII).
- 23. TOWER GROUND-RING TRENCH WITH GROUND-WIRE BEFORE BACKFILL (SHOW ALL CAD WELDS AND BEND RADII).

- 24. FENCE GROUND-RING TRENCH WITH GROUND-WIRE BEFORE BACKFILL (SHOW ALL CAD WELDS AND BEND RADII).
- 25. ALL BTS GROUND CONNECTIONS.
- 26. ALL GROUND TEST WELLS.
- 27. ANTENNA GROUND BAR AND EQUIPMENT GROUND BAR.
- 28. ADDITIONAL GROUNDING POINTS ON TOWERS ABOVE 200'.
- 29. HVAC UNITS INCLUDING CONDENSERS ON SPLIT SYSTEMS.
- 30. GPS ANTENNAS.
- 31. CABLE TRAY AND/OR WAVEGUIDE BRIDGE.
- 32. DOGHOUSE/CABLE EXIT FROM ROOF.
- 33. EACH SECTOR OF ANTENNAS; ONE PHOTOGRAPH LOOKING AT THE SECTOR AND ONE FROM BEHIND SHOWING THE PROJECTED COVERAGE AREA.
- 34. MASTER BUS BAR.
- 35. TELCO BOARD AND NIU.
- 36. ELECTRICAL DISTRIBUTION WALL.
- 37. CABLE ENTRY WITH SURGE SUPPRESSION.
- 38. ENTRANCE TO EQUIPMENT ROOM.
- 39. COAX WEATHERPROOFING-TOP AND BOTTOM OF TOWER.
- 40. COAX GROUNDING -TOP AND BOTTOM OF TOWER.
- 41. ANTENNA AND MAST GROUNDING
- 42. LANDSCAPING WHERE APPLICABLE.
- 3.6 FINAL PROJECT ACCEPTANCE: COMPLETE ALL REQUIRED REPORTING TASKS PER CONTRACT, CONTRACT DOCUMENTS OR THE SPRINT INTEGRATED CONSTRUCTION STANDARDS FOR WIRELESS SITES AND UPLOAD INTO SITERRA.



PLANS PREPARED BY:

MLA PARTNER:

033 Watervliet Shaker Ro Albany, NY 12205 Office # (518) 690-0790

JOB NUMBER 353-000

ENGINEERING LICENSE: HILLOF CONVENT CENSED ONAL ENGINE

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SITE CASCADE: -

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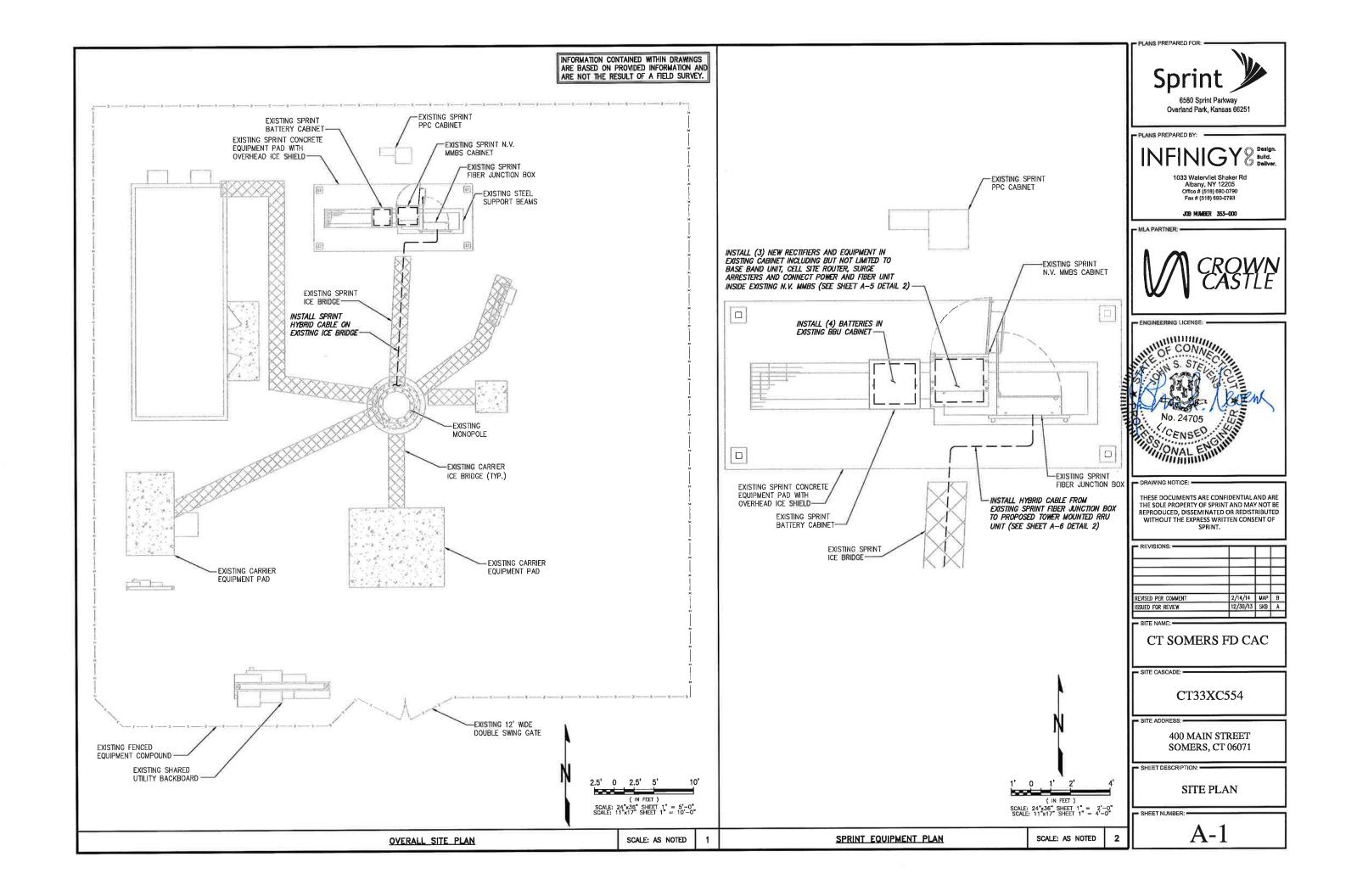
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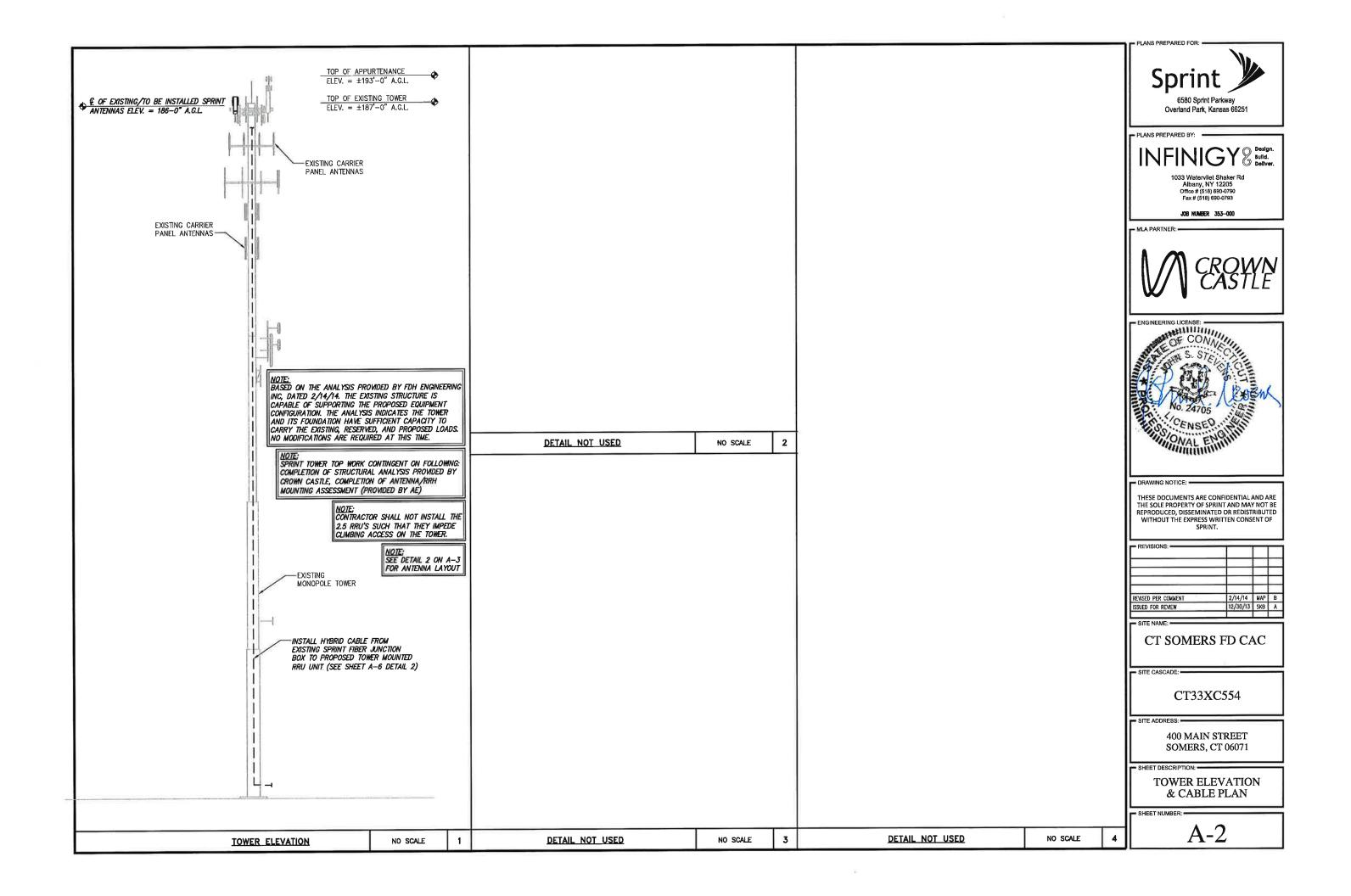
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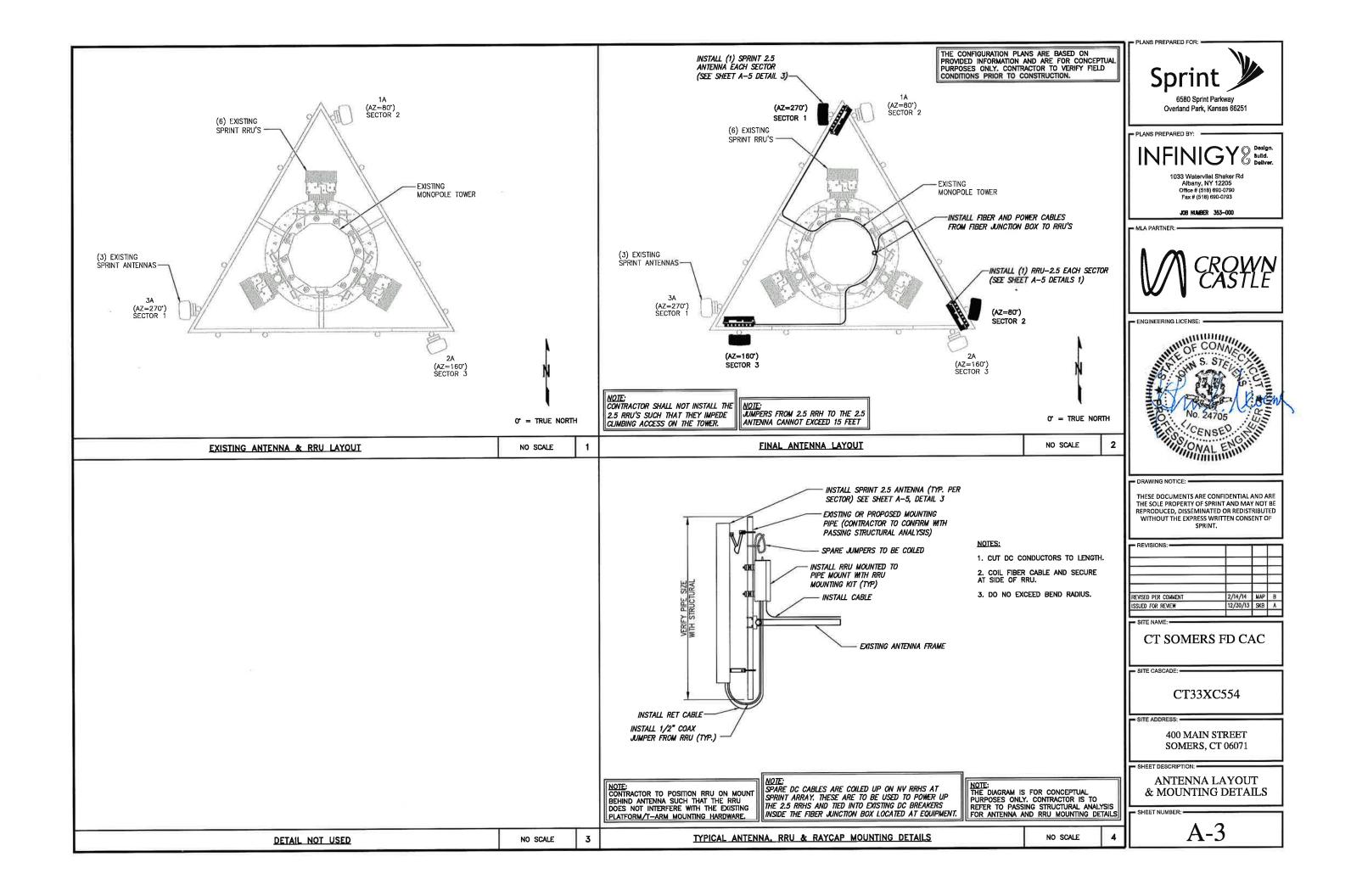
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SP-3







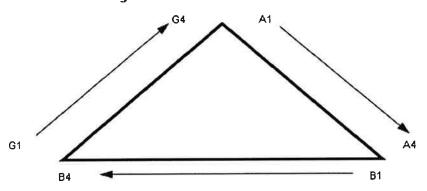
		NV CABLE	s	
BAND	INDIC	ATOR	PORT	COLOR
800-1	YEL	GRN	NV-1	GRN
1900-1	YEL	RED	NV-2	BLU
1900-2	YEL	BRN	NV-3	BRN
1900-3	YEL	BLU	NV-4	WHT
1900-4	YEL	SLT	NV-5	RED
800-2	YEL	ORG	NV-6	SLT
SPARE	YEL	WHT	NV-7	PP
2500	YEL	PPL TO T	NV-8	ORG

HYBR	ID
HYBRID	COLOR
1	GRN
2	BLU
3	BRN
4	WHT
5	RED
6	SLT
7	921
8	ORG

2.5 Band	i
2500 Radio 1	COLOR
YEL WHT	GRN
YEL WHT	BLU
YEL WHT	BRIVE
YEL WHT	WHT
YEL WHT	RED
YEL WHT	SLT
YEL WHT	PPI
YEL WHT	ORG

2.5 B	and
2500 Radio 1	COLOR
YEL WHT	GRN
YEL WHT	BLU
YEL WHT	BRITISH
YEL WHT	WHT
YEL WHT	REO
YEL WHT	SLT
YEL WHT	1911
YEL WHT	ORG

Figure 1: Antenna Orientation



#### NOTES:

- 1. ALL CABLES SHALL BE MARKED WITH 2" WIDE, UV STABILIZED, UL APPROVED TAPE.
- 2. THE FIRST RING SHALL BE CLOSEST TO THE END OF THE CABLE AND SPACED APPROXIMATELY 2" FROM THE END CONNECTOR, WEATHERPROOFING, OR BREAK-OUT CYLINDER. THERE SHALL BE A 1" SPACE BETWEEN EACH RING FOR THE CABLE IDENTIFIER, AND NO SPACES BETWEEN THE FREQUENCY BANDS.
- 3. A 2" GAP SHALL SEPARATE THE CABLE COLOR CODE FROM THE FREQUENCY COLOR CODE. THE 2" COLOR RINGS FOR THE FREQUENCY CODE SHALL BE PLACED NEXT TO EACH OTHER WITH NO
- 4. THE 2" COLORED TAPE(S) SHALL EACH BE WRAPPED A MINIMUM OF 3 TIMES AROUND THE INDIVIDUAL CABLES, AND THE TAPE SHALL BE KEPT IN THE SAME LOCATION AS MUCH AS POSSIBLE.
- 5. SITES WITH MORE THAN FOUR (4) SECTORS WILL REQUIRE ADDITIONAL RINGS FOR EACH SECTOR, FOLLOWING THE PATTERN. HIGH CAPACITY SITES WILL USE THE NEXT COLOR IN THE SEQUENCE FOR ADDITIONAL CABLES IN EACH SECTOR.
- 6. HYBRID FIBER CABLE SHALL BE SECTOR IDENTIFIED INSIDE THE CABINET ON FREQUENCY BUNDLES, ON THE SEALTITE, ON THE MAIN LINE UPON EXIT OF SEALTITE, AND BEFORE AND AFTER THE BREAKOUT UNIT (MEDUSA), AS WELL AS BEFORE AND AFTER ANY ENTRANCE OR EXIT.
- 7. HFC "MAIN TRUNK" WILL NOT BE MARKED WITH THE FREQUENCY CODES, AS IT CONTAINS ALL FREQUENCIES.
- B. INDIVIDUAL POWER PAIRS AND FIBER BUNDLES SHALL BE LABELED WITH BOTH THE CABLE AND FREQUENCY.

Sector	Cable	first Ring	Second Ring	Third Ring
1 Alpha	1	Green	No Tape	No Tape
1	2	a slue	No Tape	No Tape
1	3	1 1 Sept. 1	No Tape	No Tape
1	4	White	No Tape	No Tape
1	5	Red	No Tape	No Tape
1	6	Grey	No Tape	No Tape
1	7	Purple	No Tape	No Tape
1	8	Orange	No Tape	No Tape
2 Beta	1	Green	Green	No Tape
2	2	Blua	Bus	No Tape
2	3	Sec. 1		No Tape
2	4	White	White	No Tape
2	5	Red	Red	No Tape
2	6	Grey	Grey	No Tape
2	7	Purple	Purple	No Tape
2	8	Orange	Orange	No Tape
3 Gamma	1	Green	Green	Green
3	2	Blue	Blue	Bille
3	3	TUR WILL		
3	4	White	White	White
3	5	Red	Red	Red
3	6	Grey	Grey	Grey
3	7	Purple	Purple	Purple
3	8	Orange	Orange	Orange

NV FREQUENCY	INDICATOR	ID
800-1	YEL	GRN
1900-1	YEL	RED
1900-2	YEL	BRN
1900-3	YEL	BLU
1900-4	YEL	SLT
800-1	YEL	ORG
RESERVED	YEL	WHT
RESERVED	YEL	PPL

2.5 FREQUENCY	IN	DICATOR	ID
2500 -1	YEL	WHT	GRN
2500 -2	YEL	WHT	RED
2500 -3	YEL	WHT	BRN
2500 -4	YEL	WHT	BLU
2500 -5	YEL	WHT	SLT
2500 -6	YEL	WHT	ORG
2500 -7	YEL	WHT	WHT
2500 -8	YEL	WHT	1991/



Example - Sector 2, Cable 2, 800mhz Radio #1



Example - Sector 3, Cable 1, 1900mhz Radio #1



Example - Sector 1, Cable 4, 800 mhz Radio #1 and 1900mhz Radio #1

6580 Sprint Parkway Overland Park, Kansas 66251

MLA PARTNER:

Albany, NY 12205 Office # (518) 690-0790 Fax # (518) 690-0793

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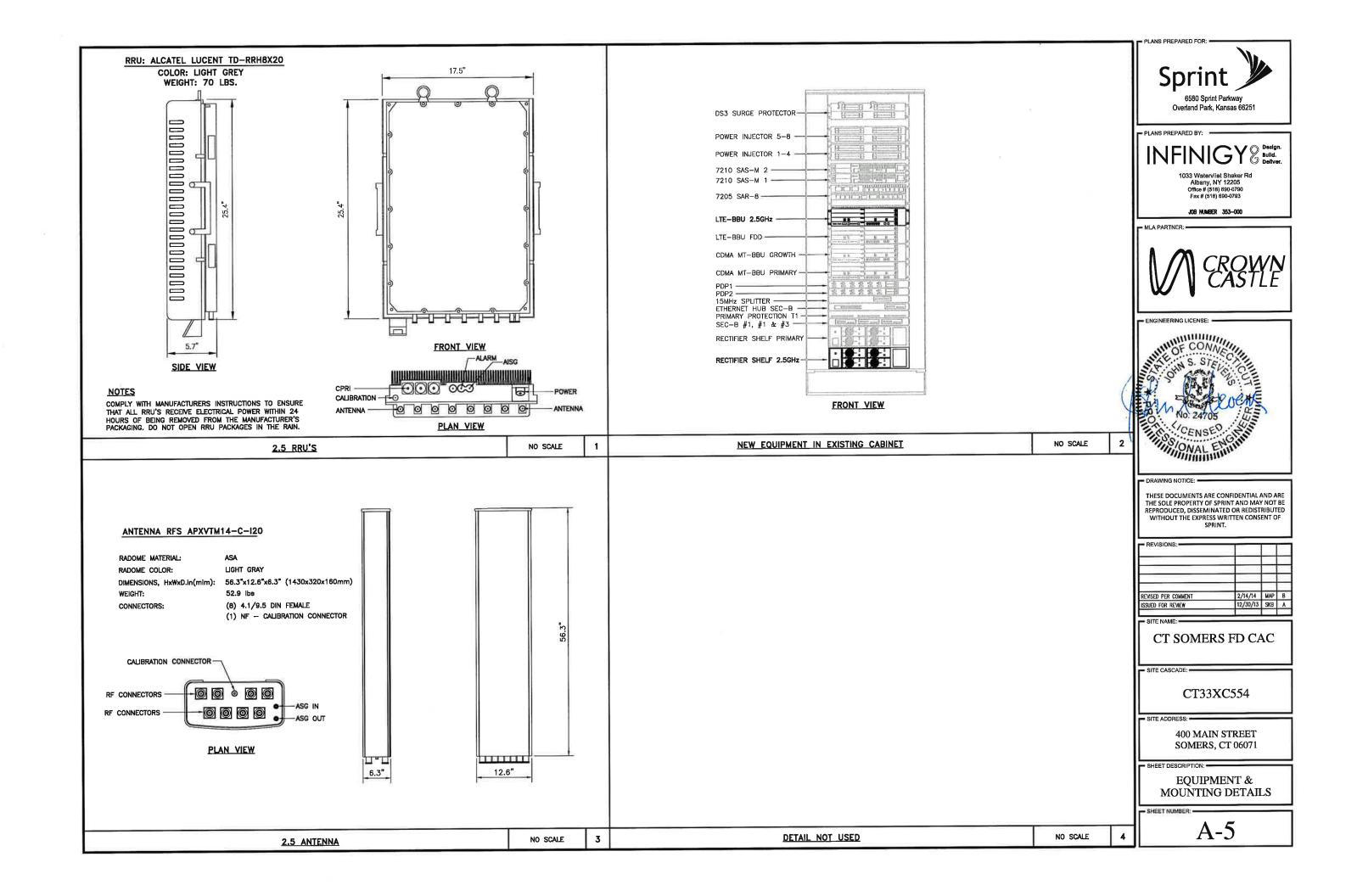
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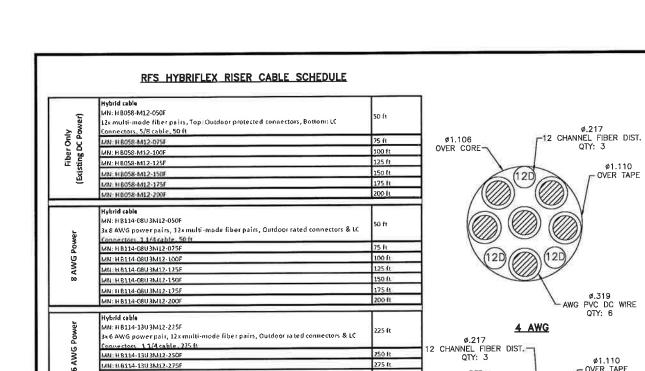
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400 MAIN STREET SOMERS, CT 06071

**COLOR CODING & NOTES** 

A-4





300 ft

5 ft

15 ft 20 (t

ø1.106 OVER CORE-

BLACK

#### RFS HYBRIFLEX JUMPER CABLE SCHEDULE

3x 4 AWG power pair, 12x multi-mode fiber pairs, Outdoor rated connectors & LC

MN: HB114-13U3M12-300F

AN: HB114-21U3NIL2-325F

Hybrid Jumper cable

MN: H6F078-21U1M3-5F1

MN: HBF078-21U1M3-10F1 MN: H8F078-21U1M3-15F1

MN: HBF078-21U1M3-20F1

MN: HBF078-21U1M3-25F1 N: HBC078-21U1M3-30F1

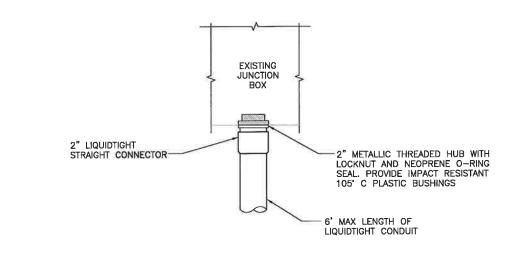
7/8 cable

onnectors, 11/4 cable, 325 ft MN: HB114-21U3M12-350F

	5 ft, 3x multi-mode fiber pairs, Outdoor & LC connectors, 1/2 cable		1
Fiber Only	MN: HBF012-M3-10F1	10 ft	ļ.
2	MN: HBF012-M3-15F1	15 ft	ø.598
Œ	MN: HBF012-M3-20F1	20 ft	INNER CORE-
	MN:H0F012-M3-25F1	25 ft	BLACK-
	MN: HBF012-M3-30F1	30 ft	l
	Hybrid Jumper cable		l
_	MN: HBF058-08U1M3-5F1	5 ft	l .
2	\$ ft, 1x 8 AWG power pair, 3x multi-mode liber pairs, Outdoor & LC Connectors,		
AWG Power	5/8 cable		Ø.217
5	IXN: HBF058-08U1M3-10F1	10 ft	12 CHANNEL FIBER QTY: 3
	MN: HBF058-08U1M3-15F1	15 ft	QII: 3
œ	MN: HBF058-08U1M3-20F1	20 ft	1
	MN: H8F058-06U1M3-25F1	25 ft	
	MH: HRF058-08U1 M3-30F1	30 ft	J /
	Hybrid Jumper cable		1 /
	MN: HBF058-13U1M3-5F1		
b.	S ft, 1x 6 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors,	5 fl	
ž	5/8 cable		
AWG Pawer	MN: HBF058-13U1M3-L0F1	10 ft	1
3	MN: HBF058-13U1M3-15F1	15 ft	ø.117
9	MN: HBF058-13UIM3-20F1	20 ft	INSULATED EPOXY
	MN: HBF058-13U1M3-2SF1	25 ft	GLASS ROD —
	MN: HBF058-13U1M3-30F1	30 ft	]
	Hybrid Jumper cable		II .

NOTE:
SPRINT CM TO CONFIRM HYBRID OR FIBER RISER CABLE
AND HYBRID OR FIBER JUMPER CABLE MODEL NUMBERS IF
HYBRID CABLES ARE REQUIRED BEFORE PREPARING BOM.

ft, 1x 4 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors



FIBER JUNCTION BOX PENETRATION

NO SCALE

2

PLANS PREPARED FOR 6580 Sprint Parkway Overland Park, Kansas 66251

- PLANS PREPARED BY: -

1033 Watervliet Shaker Rd Albany, NY 12205 Office # (518) 690-0790 Fax # (518) 690-0793

JOB NUMBER 353-000





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DESCRIPTION	DATE	BY	REV
REVISED PER COMMENT	2/14/14	MAP	В
ISSUED FOR REVIEW	12/30/13	SKB	A

CT SOMERS FD CAC

SITE CASCADE: -

CT33XC554

SITE ADDRESS: =

400 MAIN STREET SOMERS, CT 06071

- SHEET DESCRIPTION: -

CIVIL DETAILS

- SHEET NUMBER: -

A-6

Ø.217 12 CHANNEL FIBER DIST.-QTY: 3 12D 12D

8 & 6 AWG

FIBER ONLY

12D

OVER TAPE

FILLER

(120)

2.5 CABLE CROSS SECTION DATA

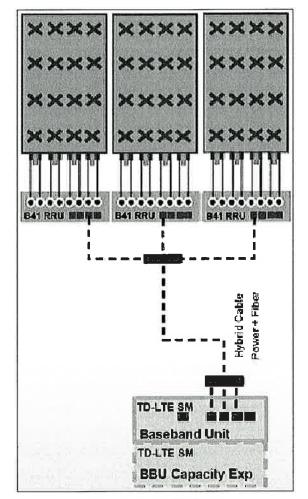
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1

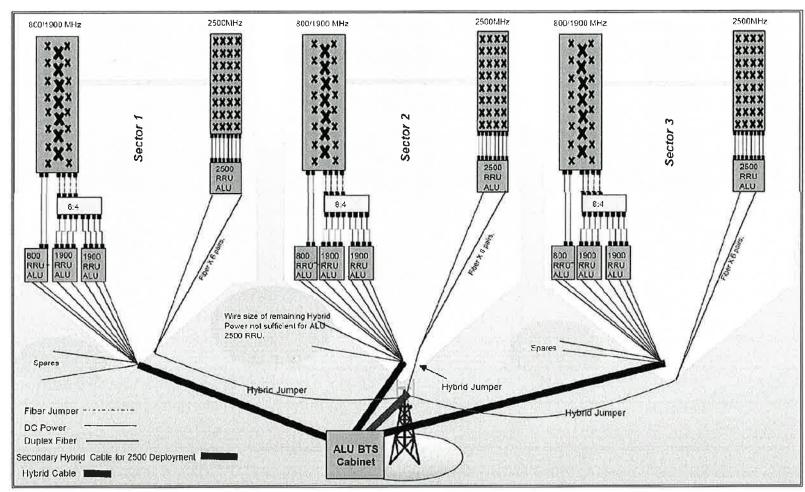
DETAIL NOT USED

NO SCALE

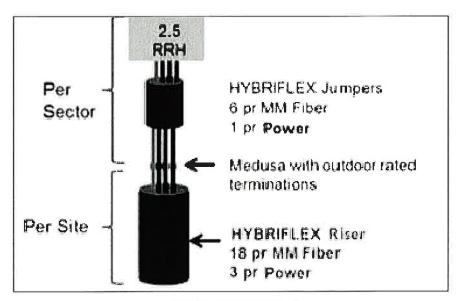
3



ALU 2.5 ALU SCENARIO 1



RAN WIRING DIAGRAM



RF 2.5 ALU SCENARIO 1



PLANS PREPARED BY:

MLA PARTNER:

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ISSUED FOR REVIEW	12/30/13	SKB	A

CT SOMERS FD CAC

SITE CASCADE:

CT33XC554

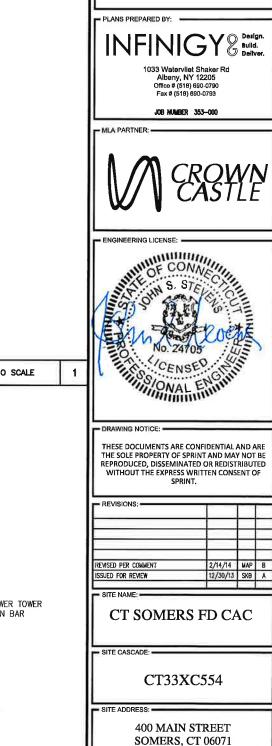
400 MAIN STREET SOMERS, CT 06071

- SHEET DESCRIPTION; -

PLUMBING DIAGRAM

- SHEET NUMBER:

A-7



- SHEET DESCRIPTION: -

- SHEET NUMBER: -

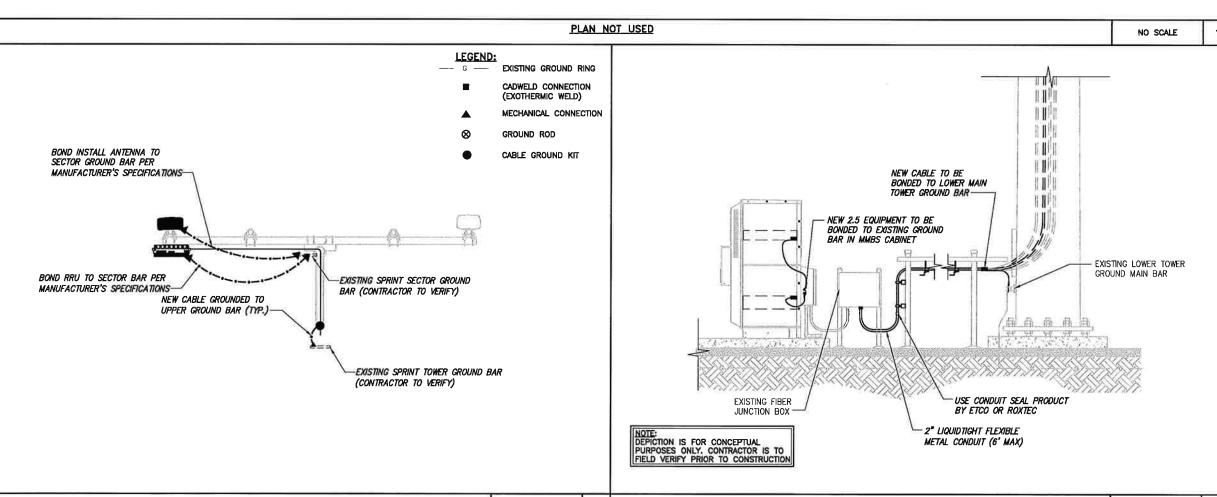
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3

ELECTRICAL & GROUNDING PLAN

E-1

6580 Sprint Parkway Overland Park, Kansas 66251

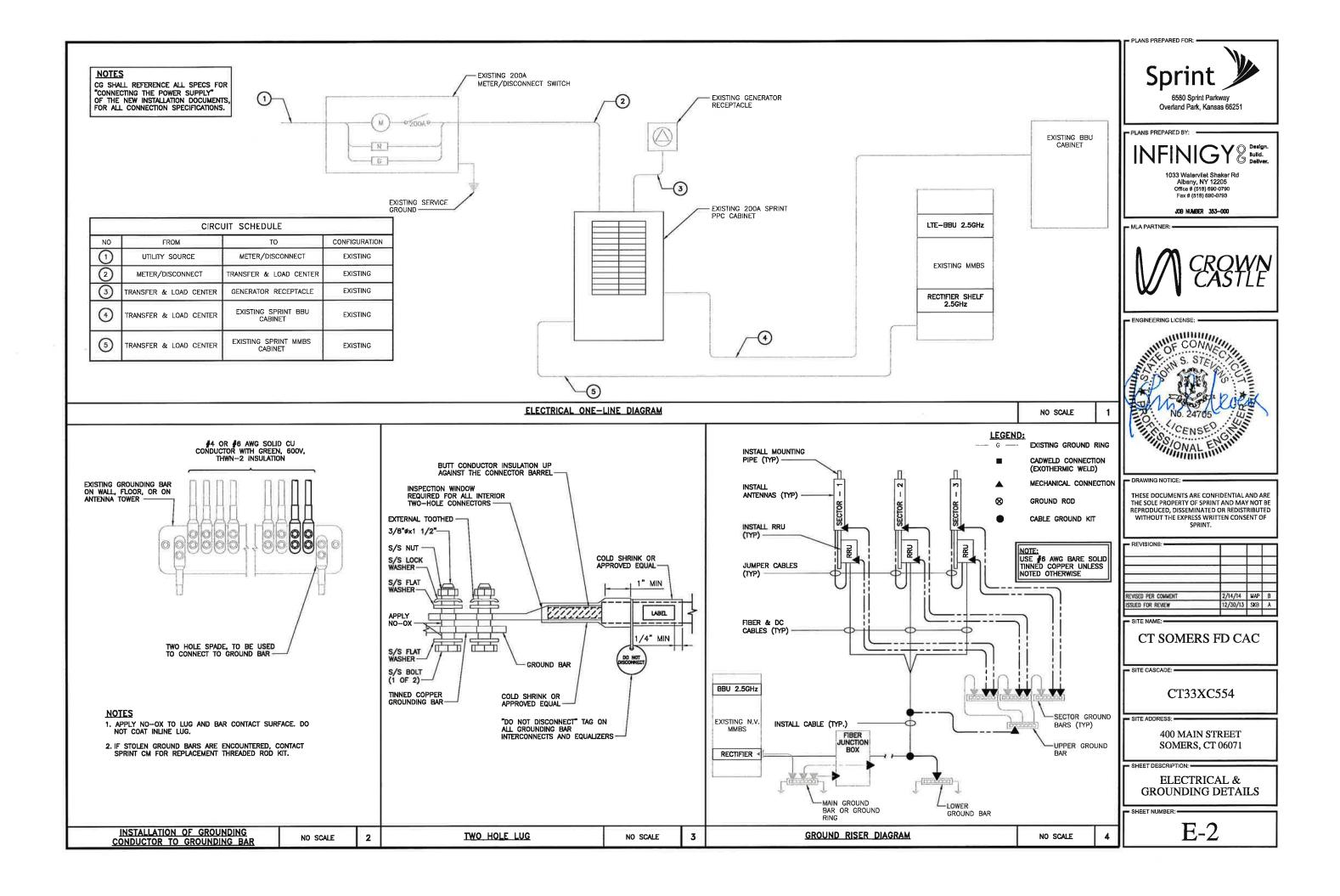


NO SCALE

2

TYPICAL EQUIPMENT GROUNDING PLAN (ELEVATION)

TYPICAL ANTENNA GROUNDING PLAN



Date: February 27, 2014

Timothy Liebrock Crown Castle 11 Grandview Circle Suite 220 Canonsburg, PA 15317



FDH Engineering, Inc. 6521 Meridien Drive Raleigh, NC 27616 (919) 755-1012

Subject: Structural Analysis Report

Carrier Designation: Sprint PCS Co-Locate Scenario 2.5B

Carrier Site Number: CT33XC554

Carrier Site Name: SOMERS-CROWN

Crown Castle BU Number: 803934

Crown Castle Site Name: CT SOMERS FD CAC

**Crown Castle JDE Job Number:** 252877 **Crown Castle Work Order Number:** 716677

Crown Castle Application Number: 208174 Rev. 6

Engineering Firm Designation: FDH Engineering, Inc. Project Number: 1423RV1400

Site Data: 400 MAIN STREET, SOMERS, Tolland County, CT

Latitude 41° 59′ 1.48″, Longitude -72° 27′ 56.87″

187 Foot - Monopole Tower

Dear Timothy Liebrock,

FDH Engineering, Inc. is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 620747, in accordance with application 208174, revision 6.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Existing + Reserved + Proposed Equipment

Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

**Sufficient Capacity** 

The analysis has been performed in accordance with the TIA/EIA-222-F standard and 2005 CT State Building Code with 2009 amendment based upon a wind speed of 85 mph fastest mile.

All modifications and equipment proposed in this report shall be installed in accordance with the attached drawings for the determined available structural capacity to be effective.

We at *FDH Engineering, Inc.* appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:

Kristi Gardner, El Project Engineer

It. Hach

Dennis D. Abel, PE

Reviewed by:

Director – Structural Engineering

CT PE License No. 23247

02-27-2014

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**Additional Calculations** 

#### 1) INTRODUCTION

This tower is a 187 ft Monopole tower designed by SUMMIT, Inc. and Paul J. Ford in April of 2001. The tower was originally designed for a wind speed of 80 mph per TIA/EIA-222-F.

#### 2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 85 mph with no ice, 38 mph with 1 inch ice thickness and 50 mph under service loads.

**Table 1 - Proposed Antenna and Cable Information** 

Mounting Level (ft)	Elevetion	Number of Antennas	Antenna Manufacturer		Number of Feed Lines	Feed Line Size (in)	Note
		3	alcatel lucent	TD-RRH8x20-25			
188.0	186.0	3	rfs celwave	APXVTM14-C-120 w/ Mount Pipe	1	1-1/4	-

Table 2 - Existing and Reserved Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
	193.0	1	andrew	DB404L-B	1	7/8	3
188.0	190.0	3	rfs celwave	APXVSPP18-C-A20 w/ Mount Pipe	3	1-1/4	1
	188.0	1	crown mounts	Platform Mount [LP 1201-1]	3		'
		3	alcatel lucent	800MHz 2X50W RRH W/FILTER			
186.0	186.0	3	alcatel lucent	PCS 1900MHz 4x45W- 65MHz	-	-	1
		1	crown mounts	Side Arm Mount [SO 102-3]			
		3	alcatel lucent	RRH2X40-AWS			
181.0 181.0		1	crown mounts	Side Arm Mount [SO 102-3]	-	-	2
178.0	179.0	3	antel	BXA-70080-6CF-EDIN-X	18	1-5/8	1

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
				w/ Mount Pipe			
		2	antel	LPA-80063/4CF w/ Mount Pipe			
		4	antel	LPA-80080-4CF-EDIN-0 w/ Mount Pipe			
1		6	kathrein	742 213 w/ Mount Pipe	1	1-1/4	2
1		1	rfs celwave	DB-T1-6Z-8AB-0Z	I	1-1/4	
	178.0	1	crown mounts	Platform Mount [LP 1201-	-	-	1
	169.0	3	ems wireless	RR90-17-02DP w/ Mount Pipe			
168.0		6	ericsson	KRY 112 71/1	6	1-5/8	1
	168.0	1	crown mounts	Platform Mount [LP 1201-			
		1	crown mounts	T-Arm Mount [TA 601-3]			
	6	ericsson	RRUS-11				
		3	kathrein	800 10121 w/ Mount Pipe	6	1-5/8	
160.0	160.0	6	powerwave technologies	LGP21401	6 2 . 1	3/4 3/8	1
		3	powerwave technologies	P65-17-XLH-RR w/ Mount Pipe			
		1	raycap	DC6-48-60-18-8F			
150.0	150.0	3	rfs celwave	APXV18-206517S-C w/ Mount Pipe	6	1-5/8	1
420.0	125.0	1	sinclair	SD212-SF2P2SNM Dipole	4	7/0	
120.0	120.0	1	crown mounts	Side Arm Mount [SO 702-	1	7/8	1
115.0	122.0	1	sinclair	SD110-SFXPASNM	1	1/2	1
	82.0	1	telewave	ANT450D3			
81.0	81.0	1	crown mounts	Side Arm Mount [SO 309-	1	7/8	1
48.0	48.0	1	crown mounts	Side Arm Mount [SO 701-1]	1	1/2	1
		1	lucent	KS24019-L112A			

### Notes:

Existing Equipment Reserved Equipment Existing Equipment for Carrier #2 1) 2) 3)

Table 3 - Design Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
188	188	12	generic	Panel Antennas (CaAa = 75 ft2)	-	-
178	178	12	generic	Panel Antennas (CaAa = 75 ft2)	-	-
168	168	12	generic	Panel Antennas (CaAa = 75 ft2)	-	-
158	158	12	generic	Panel Antennas (CaAa = 75 ft2)	-	-
148	148	12	generic	Panel Antennas (CaAa = 75 ft2)	-	-
138	138	12	generic	Panel Antennas (CaAa = 75 ft2)	-	-
128	128	12	generic	Panel Antennas (CaAa = 75 ft2)	-	-

#### 3) ANALYSIS PROCEDURE

**Table 4 - Documents Provided** 

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	URS	1095648	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	Summit	1058248	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Summit	419873	CCISITES

#### 3.1) Analysis Method

tnxTower (version 6.1.4.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

#### 3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) When applicable, transmission cables are considered as structural components for calculating wind loads as allowed by TIA/EIA-222-F.

This analysis may be affected if any assumptions are not valid or have been made in error. FDH Engineering, Inc. should be notified to determine the effect on the structural integrity of the tower.

### 4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	187 - 136	Pole	TP36.201x26x0.25	1	-13.171	1445.905	74.2	Pass
L2	136 - 89.5	Pole	TP45.003x34.801x0.375	2	-22.951	2690.300	84.0	Pass
L3	89.5 - 44.25	Pole	TP53.304x43.103x0.438	3	-36.370	3718.990	89.2	Pass
L4	44.25 - 0	Pole	TP61.28x51.079x0.5	4	-56.534	5014.559	88.1	Pass
							Summary	
						Pole (L3)	89.2	Pass
						RATING =	89.2	Pass

Table 6 - Tower Component Stresses vs. Capacity – LC7

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	79.8	Pass
1	Base Plate	0	72.4	Pass
1	Base Foundation	0	82.5	Pass
1	Base Foundation Soil Interaction	0	80.7	Pass

Structure Rating (max from all components) =	89.2%
--	-------

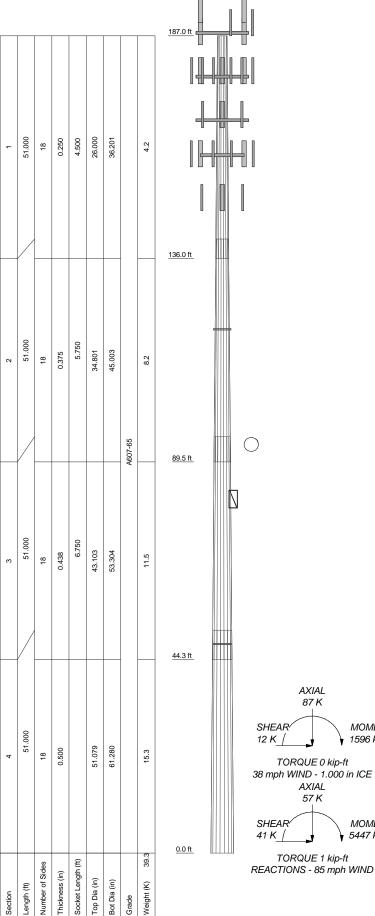
#### Notes:

#### 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the existing, reserved, and proposed loads. No modifications are required at this time.

<sup>1)</sup> See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

# APPENDIX A TNXTOWER OUTPUT



#### **DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
DB404L-B	188	(2) LPA-80080-4CF-EDIN-0 w/ Mount	178
APXVSPP18-C-A20 w/ Mount Pipe	188	Pipe	
APXVSPP18-C-A20 w/ Mount Pipe	188	(2) KRY 112 71/1	168
APXVSPP18-C-A20 w/ Mount Pipe	188	(2) KRY 112 71/1	168
APXVTM14-C-120 w/ Mount Pipe	188	Platform Mount [LP 1201-1]	168
APXVTM14-C-120 w/ Mount Pipe	188	RR90-17-02DP w/ Mount Pipe	168
APXVTM14-C-120 w/ Mount Pipe	188	RR90-17-02DP w/ Mount Pipe	168
TD-RRH8x20-25	188	RR90-17-02DP w/ Mount Pipe	168
TD-RRH8x20-25	188	(2) KRY 112 71/1	168
TD-RRH8x20-25	188	P65-17-XLH-RR w/ Mount Pipe	160
Platform Mount [LP 1201-1]	188	P65-17-XLH-RR w/ Mount Pipe	160
B00MHz 2X50W RRH W/FILTER	186	(2) RRUS-11	160
BOOMHz 2X50W RRH W/FILTER	186	(2) RRUS-11	160
Side Arm Mount [SO 102-3]	186	(2) RRUS-11	160
PCS 1900MHz 4x45W-65MHz	186	(2) LGP21401	160
PCS 1900MHz 4x45W-65MHz	186	(2) LGP21401	160
PCS 1900MHz 4x45W-65MHz	186	(2) LGP21401	160
800MHz 2X50W RRH W/FILTER	186	DC6-48-60-18-8F	160
RRH2X40-AWS	181	T-Arm Mount [TA 601-3]	160
RRH2X40-AWS	181	800 10121 w/ Mount Pipe	160
RRH2X40-AWS	181	800 10121 w/ Mount Pipe	160
Side Arm Mount [SO 102-3]	181	800 10121 w/ Mount Pipe	160
(2) LPA-80080-4CF-EDIN-0 w/ Mount	178	P65-17-XLH-RR w/ Mount Pipe	160
Pipe		APXV18-206517S-C w/ Mount Pipe	150
2) LPA-80063/4CF w/ Mount Pipe	178	APXV18-206517S-C w/ Mount Pipe	150
2) 742 213 w/ Mount Pipe	178	APXV18-206517S-C w/ Mount Pipe	150
2) 742 213 w/ Mount Pipe	178	Side Arm Mount [SO 702-1]	120
(2) 742 213 w/ Mount Pipe	178	SD212-SF2P2SNM Dipole	120
DB-T1-6Z-8AB-0Z	178	SD110-SFXPASNM	115
Platform Mount [LP 1201-1]	178	Side Arm Mount [SO 309-1]	81
BXA-70080-6CF-EDIN-X w/ Mount	178	ANT450D3	81
Pipe		Side Arm Mount [SO 701-1]	48
BXA-70080-6CF-EDIN-X w/ Mount Pipe	178	KS24019-L112A	48
BXA-70080-6CF-EDIN-X w/ Mount Pipe	178		

#### **MATERIAL STRENGTH**

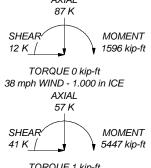
GRADE Fy		Fu GRADE		Fy	Fu						
A607-65	65 ksi	80 ksi									

#### **TOWER DESIGN NOTES**

- 1. Tower is located in Tolland County, Connecticut.
- Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
   Tower is also designed for a 38 mph basic wind with 1.00 in ice. Ice is considered to
- increase in thickness with height.

  4. Deflections are based upon a 50 mph wind.

  5. TOWER RATING: 89.2%



FDH Engineering, Inc. ob: CT Somers FD CAC, BU 803934 Project: **1423RV1400** FDH 6521 Meridien Drive Client: Crown Castle Drawn by: Kristi Gardner App'd: Raleigh, NC 27616 Scale: NTS Code: TIA/EIA-222-F Date: 02/27/14 Phone: (919) 755-1012 Dwg No. E-1 FAX: (919) 755-1013

FDH Engineering, Inc. 6521 Meridien Drive Raleigh, NC 27616 Phone: (919) 755-1012

FAX: (919) 755-1013

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Client	Crown Castle	Designed by Kristi Gardner

### **Tower Input Data**

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Tolland County, Connecticut.

Basic wind speed of 85 mph.

Nominal ice thickness of 1.000 in.

Ice thickness is considered to increase with height.

Ice density of 56.000 pcf.

A wind speed of 38 mph is used in combination with ice.

Temperature drop of 50.000 °F.

Deflections calculated using a wind speed of 50 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.333.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

### **Options**

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- Use Code Stress Ratios
- Use Code Safety Factors Guys

Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination

Distribute Leg Loads As Uniform Assume Legs Pinned

- Assume Rigid Index Plate
- Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
- Bypass Mast Stability Checks
- Use Azimuth Dish Coefficients
- Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Use TIA-222-G Tension Splice Capacity Exemption

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

- Consider Feedline Torque Include Angle Block Shear Check
  - Poles
- Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

### **Tapered Pole Section Geometry**

Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft	Sides	in	in	in	in	
L1	187.000-136.00 0	51.000	4.500	18	26.000	36.201	0.250	1.000	A607-65 (65 ksi)
L2	136.000-89.500	51.000	5.750	18	34.801	45.003	0.375	1.500	A607-65 (65 ksi)
L3	89.500-44.250	51.000	6.750	18	43.103	53.304	0.438	1.750	A607-65 (65 ksi)
L4	44.250-0.000	51.000		18	51.079	61.280	0.500	2.000	A607-65 (65 ksi)

FDH Engineering, Inc. 6521 Meridien Drive Raleigh, NC 27616 Phone: (919) 755-1012 FAX: (919) 755-1013

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Client		Designed by
	Crown Castle	Kristi Gardner

### **Tapered Pole Properties**

Section	Tip Dia.	Area	I	r	С	I/C	J	It/Q	w	w/t
	in	$in^2$	$in^4$	in	in	$in^3$	$in^4$	$in^2$	in	
L1	26.401	20.433	1711.654	9.141	13.208	129.592	3425.561	10.218	4.136	16.544
	36.759	28.527	4658.191	12.763	18.390	253.299	9322.512	14.266	5.931	23.726
L2	36.252	40.975	6135.246	12.221	17.679	347.039	12278.566	20.492	5.465	14.573
	45.697	53.118	13365.891	15.843	22.862	584.646	26749.369	26.564	7.261	19.361
L3	44.936	59.246	13625.291	15.146	21.896	622.267	27268.510	29.629	6.816	15.58
	54.126	73.412	25921.737	18.768	27.078	957.284	51877.583	36.713	8.612	19.683
L4	53.238	80.269	25943.042	17.955	25.948	999.807	51920.220	40.142	8.110	16.22
	62.225	96.458	45019.064	21.577	31.130	1446.152	90097.366	48.238	9.905	19.811

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_f$	$Adjust. \ Factor \ A_r$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals
ft	$ft^2$	in					in	in
L1	-			1	1	1		
187.000-136.0								
00								
L2				1	1	1		
136.000-89.50								
0								
L3				1	1	1		
89.500-44.250								
L4				1	1	1		
44.250-0.000								

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Sector	Component	Placement	Total	Number Per Row	Start/End Position	Width or Diameter	Perimeter	Weight
		Type	C.	Number	Per Row	Position			110
			ft				in	in	klf
HCC 78-50J(7/8")	A	Surface Ar (CaAa)	187.000 - 0.000	1	1	-0.500 -0.480	1.100		0.001
AVA5-50( 7/8")	В	Surface Ar	81.000 - 0.000	1	1	-0.350	1.102		0.000
		(CaAa)				-0.330			
** Face C **									
LDF4-50A(1/2")	C	Surface Ar	48.000 - 0.000	1	1	-0.470	0.630		0.000
, ,		(CaAa)				-0.450			
HB114-1-0813U4-M5J( 1 1/4")	C	Surface Ar	187.000 - 0.000	1	1	-0.450	1.540		0.001
· · · ·		(CaAa)				-0.430			
LDF7-50A(1-5/8")	C	Surface Ar	178.000 - 0.000	6	1	0.420	1.980		0.001
•		(CaAa)				0.480			
HB114-1-0813U4-M5J( 1 1/4")	С	Surface Ar	178.000 - 0.000	1	1	0.480	1.540		0.001
, ,		(CaAa)				0.500			
***		(=)							
Safety Line 3/8	C	Surface Ar	187.000 - 0.000	1	1	0.000	0.375		0.000
		(CaAa)				0.000			

### Feed Line/Linear Appurtenances - Entered As Area

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Client	Crown Castle	Designed by Kristi Gardner

Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg		- JF -	ft			ft²/ft	klf
** Face A **								
HB114-1-08U4-M5J(1	A	No	Inside Pole	187.000 - 0.000	3	No Ice	0.000	0.001
1/4")						1/2" Ice	0.000	0.001
						1" Ice	0.000	0.001
						2" Ice	0.000	0.001
						4" Ice	0.000	0.001
** HCC 78-50J(7/8")	A	No	Inside Pole	120.000 - 0.000	1	No Ice	0.000	0.001
HCC 78-303(7/8 )	A	NO	niside Fole	120.000 - 0.000	1	1/2" Ice	0.000	0.001
						1" Ice	0.000	0.001
						2" Ice	0.000	0.001
***						4" Ice	0.000	0.001
CR 50 1873(1-5/8")	Α	No	Inside Pole	150.000 - 0.000	6	No Ice	0.000	0.001
CR 30 1073(1 570 )	11	110	morae rote	150.000 0.000	O	1/2" Ice	0.000	0.001
						1" Ice	0.000	0.001
						2" Ice	0.000	0.001
** Face B **						4" Ice	0.000	0.001
HJ7-50A(1-5/8")	В	No	Inside Pole	168.000 - 0.000	6	No Ice	0.000	0.001
113 / 3011(1 3/0 )		110	morae role	100.000 0.000	O	1/2" Ice	0.000	0.001
						1" Ice	0.000	0.001
						2" Ice	0.000	0.001
**						4" Ice	0.000	0.001
HCC12-50J(1/2")	В	No	Inside Pole	115.000 - 0.000	1	No Ice	0.000	0.000
,						1/2" Ice	0.000	0.000
						1" Ice	0.000	0.000
						2" Ice	0.000	0.000
						4" Ice	0.000	0.000
**								
LDF7-50A(1-5/8")	C	No	Inside Pole	160.000 - 0.000	6	No Ice	0.000	0.001
						1/2" Ice	0.000	0.001
						1" Ice	0.000	0.001
						2" Ice	0.000	0.001
						4" Ice	0.000	0.001
FB-L98B-002-75000(	C	No	Inside Pole	160.000 - 0.000	1	No Ice	0.000	0.000
3/8")	-			,	-	1/2" Ice	0.000	0.000
/						1" Ice	0.000	0.000
						2" Ice	0.000	0.000
						4" Ice	0.000	0.000
WR-VG86ST-BRD( 3/4)	С	No	Inside Pole	160.000 - 0.000	2	No Ice	0.000	0.000
v IV- v (1000) 1-DIVD( 3/4)	C	NO	HISIUC FOIC	100.000 - 0.000	4	1/2" Ice		
							0.000	0.001
						1" Ice	0.000	0.001
						2" Ice	0.000	0.001
**						4" Ice	0.000	0.001
LDF7-50A(1-5/8")	С	No	Inside Pole	178.000 - 0.000	12	No Ice	0.000	0.001
	~	•				1/2" Ice	0.000	0.001
						1" Ice	0.000	0.001
						2" Ice	0.000	0.001
						4" Ice	0.000	0.001

## Feed Line/Linear Appurtenances Section Areas

Tower	Tower	Face	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		$ft^2$	$ft^2$	ft <sup>2</sup>	$ft^2$	K

FDH Engineering, Inc. 6521 Meridien Drive Raleigh, NC 27616 Phone: (919) 755-1012 FAX: (919) 755-1013

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Tower	Tower	Face	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		$ft^2$	$ft^2$	$ft^2$	$ft^2$	K
L1	187.000-136.000	A	0.000	0.000	5.610	0.000	0.262
		В	0.000	0.000	0.000	0.000	0.200
		C	0.000	0.000	24.551	0.000	0.890
L2	136.000-89.500	A	0.000	0.000	5.115	0.000	0.423
		В	0.000	0.000	0.000	0.000	0.297
		C	0.000	0.000	25.273	0.000	1.094
L3	89.500-44.250	A	0.000	0.000	4.978	0.000	0.420
		В	0.000	0.000	4.050	0.000	0.305
		C	0.000	0.000	24.830	0.000	1.065
L4	44.250-0.000	A	0.000	0.000	4.867	0.000	0.411
		В	0.000	0.000	4.876	0.000	0.300
		C	0.000	0.000	26.838	0.000	1.048

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness			In Face	Out Face	
	ft	Leg	in	$ft^2$	$ft^2$	$ft^2$	$ft^2$	K
L1	187.000-136.000	A	1.209	0.000	0.000	17.941	0.000	0.436
		В		0.000	0.000	0.000	0.000	0.200
		C		0.000	0.000	69.523	0.000	2.574
L2	136.000-89.500	Α	1.158	0.000	0.000	16.358	0.000	0.582
		В		0.000	0.000	0.000	0.000	0.297
		C		0.000	0.000	70.245	0.000	2.894
L3	89.500-44.250	A	1.088	0.000	0.000	15.459	0.000	0.565
		В		0.000	0.000	12.562	0.000	0.422
		C		0.000	0.000	67.625	0.000	2.724
L4	44.250-0.000	A	1.000	0.000	0.000	14.498	0.000	0.539
		В		0.000	0.000	14.507	0.000	0.429
		C		0.000	0.000	74.989	0.000	2.627

### **Feed Line Center of Pressure**

Section	Elevation	$CP_X$	$CP_Z$	$CP_X$	$CP_Z$
				Ice	Ice
	ft	in	in	in	in
L1	187.000-136.000	-0.348	0.494	-0.626	1.042
L2	136.000-89.500	-0.409	0.540	-0.765	1.178
L3	89.500-44.250	-0.355	0.426	-0.634	0.915
L4	44.250-0.000	-0.280	0.441	-0.385	0.976

### **Discrete Tower Loads**

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Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_AA_A$ Front	$C_A A_A$ Side	Weigh
	Leg		Lateral Vert						
			t ft	0	ft		$ft^2$	ft <sup>2</sup>	K
			ft ft		J		,	y	
PCS 1900MHz	A	From Leg	4.000	0.000	186.000	No Ice	2.709	2.611	0.060
4x45W-65MHz			0.000			1/2" Ice	2.948	2.847	0.083
			0.000			1" Ice	3.195	3.092	0.110
						2" Ice	3.716	3.608	0.173
						4" Ice	4.862	4.744	0.347
PCS 1900MHz	В	From Leg	4.000	0.000	186.000	No Ice	2.709	2.611	0.060
4x45W-65MHz			0.000			1/2" Ice	2.948	2.847	0.083
			0.000			1" Ice	3.195	3.092	0.110
						2" Ice	3.716	3.608	0.173
DCC 1000MH-	C	Europ I	4.000	0.000	196,000	4" Ice	4.862	4.744	0.347
PCS 1900MHz	C	From Leg	4.000	0.000	186.000	No Ice	2.709	2.611	0.060
4x45W-65MHz			0.000			1/2" Ice 1" Ice	2.948 3.195	2.847 3.092	0.083 0.110
			0.000			2" Ice	3.716	3.608	0.110
						4" Ice	4.862	4.744	0.173
800MHz 2X50W RRH	A	From Leg	4.000	0.000	186.000	No Ice	2.401	2.254	0.064
W/FILTER	А	1 Tolli Leg	0.000	0.000	100.000	1/2" Ice	2.613	2.460	0.086
W/TETEK			0.000			1" Ice	2.833	2.675	0.111
			0.000			2" Ice	3.300	3.132	0.172
						4" Ice	4.337	4.148	0.338
800MHz 2X50W RRH	В	From Leg	4.000	0.000	186.000	No Ice	2.401	2.254	0.064
W/FILTER			0.000			1/2" Ice	2.613	2.460	0.086
			0.000			1" Ice	2.833	2.675	0.111
						2" Ice	3.300	3.132	0.172
						4" Ice	4.337	4.148	0.338
800MHz 2X50W RRH	C	From Leg	4.000	0.000	186.000	No Ice	2.401	2.254	0.064
W/FILTER			0.000			1/2" Ice	2.613	2.460	0.086
			0.000			1" Ice	2.833	2.675	0.111
						2" Ice	3.300	3.132	0.172
						4" Ice	4.337	4.148	0.338
ide Arm Mount [SO 102-3]	C	None		0.000	186.000	No Ice	3.000	3.000	0.081
						1/2" Ice	3.480	3.480	0.111
						1" Ice	3.960	3.960	0.141
						2" Ice	4.920	4.920	0.201
*///*						4" Ice	6.840	6.840	0.321
DB404L-B	Λ.	From Leg	4.000	0.000	188.000	No Ice	1.140	1.140	0.014
DD404L-D	Α	I TOIL LOE	1.000	0.000	100.000	INO ICC			
DD404L-B	Α	Trom Leg	0.000	0.000	188.000	1/2" Ice	2.052	2.052	0.018
DB404L-B	A	Trom Leg		0.000	188.000		2.052 2.964	2.052 2.964	0.022
DB404L-B	A	Trom Leg	0.000	0.000	188.000	1/2" Ice			
DB404L-B	A	Trom Leg	0.000	0.000	188.000	1/2" Ice 1" Ice 2" Ice 4" Ice	2.964	2.964	0.022 0.031
APXVSPP18-C-A20 w/	A	From Leg	0.000 5.000 4.000	0.000	188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice	2.964 4.788 8.436 8.498	2.964 4.788	0.022 0.031 0.048
			0.000 5.000			1/2" Ice 1" Ice 2" Ice 4" Ice	2.964 4.788 8.436	2.964 4.788 8.436	0.022 0.031 0.048 0.083
APXVSPP18-C-A20 w/			0.000 5.000 4.000			1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice	2.964 4.788 8.436 8.498 9.149 9.767	2.964 4.788 8.436 6.946 8.127 9.021	0.022 0.031 0.048 0.083 0.151 0.227
APXVSPP18-C-A20 w/			0.000 5.000 4.000 0.000			1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031	2.964 4.788 8.436 6.946 8.127 9.021 10.844	0.022 0.031 0.048 0.083 0.151 0.227 0.406
APXVSPP18-C-A20 w/ Mount Pipe	A	From Leg	0.000 5.000 4.000 0.000 0.000	0.000	188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851	0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909
APXVSPP18-C-A20 w/ Mount Pipe APXVSPP18-C-A20 w/			0.000 5.000 4.000 0.000 0.000 4.000			1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679 8.498	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851 6.946	0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909
APXVSPP18-C-A20 w/ Mount Pipe	A	From Leg	0.000 5.000 4.000 0.000 0.000 4.000 0.000	0.000	188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679 8.498 9.149	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851 6.946 8.127	0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909 0.083 0.151
APXVSPP18-C-A20 w/ Mount Pipe APXVSPP18-C-A20 w/	A	From Leg	0.000 5.000 4.000 0.000 0.000 4.000	0.000	188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679 8.498 9.149 9.767	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851 6.946 8.127 9.021	0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909 0.083 0.151 0.227
APXVSPP18-C-A20 w/ Mount Pipe APXVSPP18-C-A20 w/	A	From Leg	0.000 5.000 4.000 0.000 0.000 4.000 0.000	0.000	188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1" Ice 1" Ice 1" Ice 1" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679 8.498 9.149 9.767 11.031	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851 6.946 8.127 9.021 10.844	0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909 0.083 0.151 0.227 0.406
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe	A B	From Leg	0.000 5.000 4.000 0.000 0.000 4.000 0.000 2.000	0.000	188.000 188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 1" Ice 1" Ice 1" Ice 1" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679 8.498 9.149 9.767 11.031 13.679	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851 6.946 8.127 9.021 10.844 14.851	0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909 0.083 0.151 0.227 0.406 0.909
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/	A	From Leg	0.000 5.000 4.000 0.000 0.000 4.000 2.000 4.000	0.000	188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1/2" Ice 1/2" Ice 1/2" Ice 1" Ice 2" Ice 1" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679 8.498 9.149 9.767 11.031 13.679 8.498	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851 6.946 8.127 9.021 10.844 14.851 6.946	0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909 0.083 0.151 0.227 0.406 0.909 0.083
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe	A B	From Leg	0.000 5.000 4.000 0.000 0.000 4.000 2.000 4.000 0.000	0.000	188.000 188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1/2" Ice 1/2" Ice 1" Ice 2" Ice 4" Ice 1/2" Ice 1/2" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679 8.498 9.149 9.767 11.031 13.679 8.498 9.149	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851 6.946 8.127 9.021 10.844 14.851 6.946 8.127	0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909 0.083 0.151 0.227 0.406 0.909 0.083
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/	A B	From Leg	0.000 5.000 4.000 0.000 0.000 4.000 2.000 4.000	0.000	188.000 188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 1/2" Ice 1" Ice 2" Ice 1" Ice 1" Ice 1" Ice 1" Ice 1" Ice 1" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679 8.498 9.149 9.767 11.031 13.679 8.498 9.149	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851 6.946 8.127 9.021 10.844 14.851 6.946 8.127 9.021	0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909 0.083 0.151 0.227 0.406 0.909 0.083
APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/ Mount Pipe  APXVSPP18-C-A20 w/	A B	From Leg	0.000 5.000 4.000 0.000 0.000 4.000 2.000 4.000 0.000	0.000	188.000 188.000	1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice 1/2" Ice 1/2" Ice 1/2" Ice 1" Ice 2" Ice 4" Ice 1/2" Ice 1/2" Ice	2.964 4.788 8.436 8.498 9.149 9.767 11.031 13.679 8.498 9.149 9.767 11.031 13.679 8.498 9.149	2.964 4.788 8.436 6.946 8.127 9.021 10.844 14.851 6.946 8.127 9.021 10.844 14.851 6.946 8.127	0.018 0.022 0.031 0.048 0.083 0.151 0.227 0.406 0.909 0.083 0.151 0.227 0.406 0.909 0.083 0.151

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Project		Date
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Client	Crown Castle	Designed by Kristi Gardner

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_AA_A$ Front	$C_AA_A$ Side	Weight
			Vert ft ft ft	0	ft		ft <sup>2</sup>	ft²	K
Mount Pipe			0.000			1/2" Ice	7.662	5.754	0.131
•			-2.000			1" Ice	8.183	6.472	0.193
						2" Ice	9.256	8.010	0.338
						4" Ice	11.526	11.412	0.752
APXVTM14-C-120 w/	В	From Leg	4.000	0.000	188.000	No Ice	7.134	4.959	0.077
Mount Pipe			0.000			1/2" Ice	7.662	5.754	0.131
			-2.000			1" Ice	8.183	6.472	0.193
						2" Ice	9.256	8.010	0.338
ADVI/TM14 C 120/	C	F I	4.000	0.000	100,000	4" Ice	11.526	11.412	0.752
APXVTM14-C-120 w/	C	From Leg	4.000	0.000	188.000	No Ice 1/2" Ice	7.134 7.662	4.959 5.754	0.077 0.131
Mount Pipe			0.000 -2.000			1/2 Ice 1" Ice	8.183	5.754 6.472	0.131
			-2.000			2" Ice	9.256	8.010	0.193
						4" Ice	11.526	11.412	0.338
TD-RRH8x20-25	A	From Leg	4.000	0.000	188.000	No Ice	4.720	1.700	0.732
1D-KK118X20-23	Λ	110iii Leg	0.000	0.000	188.000	1/2" Ice	5.014	1.917	0.070
			-2.000			1" Ice	5.316	2.143	0.128
			2.000			2" Ice	5.948	2.620	0.200
						4" Ice	7.314	3.677	0.397
TD-RRH8x20-25	В	From Leg	4.000	0.000	188.000	No Ice	4.720	1.700	0.070
15 14410.120 20	2	Trom Leg	0.000	0.000	100.000	1/2" Ice	5.014	1.917	0.097
			-2.000			1" Ice	5.316	2.143	0.128
						2" Ice	5.948	2.620	0.200
						4" Ice	7.314	3.677	0.397
TD-RRH8x20-25	C	From Leg	4.000	0.000	188.000	No Ice	4.720	1.700	0.070
		C	0.000			1/2" Ice	5.014	1.917	0.097
			-2.000			1" Ice	5.316	2.143	0.128
						2" Ice	5.948	2.620	0.200
						4" Ice	7.314	3.677	0.397
Platform Mount [LP 1201-1]	C	None		0.000	188.000	No Ice	23.100	23.100	2.100
						1/2" Ice	26.800	26.800	2.500
						1" Ice	30.500	30.500	2.900
						2" Ice	37.900	37.900	3.700
						4" Ice	52.700	52.700	5.300
*///*			4.000	0.000	450.000				0.042
BXA-70080-6CF-EDIN-X w/	Α	From Leg	4.000	0.000	178.000	No Ice	6.006	6.203	0.043
Mount Pipe			0.000			1/2" Ice	6.562	7.359	0.098
			1.000			1" Ice	7.083	8.229	0.160
						2" Ice 4" Ice	8.167 10.691	10.019 13.840	0.310 0.750
BXA-70080-6CF-EDIN-X w/	P	From Leg	4.000	0.000	178.000	No Ice	6.006	6.203	0.730
Mount Pipe	В	From Leg	0.000	0.000	178.000	1/2" Ice	6.562	7.359	0.043
Would Fipe			1.000			1" Ice	7.083	8.229	0.160
			1.000			2" Ice	8.167	10.019	0.310
						4" Ice	10.691	13.840	0.750
BXA-70080-6CF-EDIN-X w/	C	From Leg	4.000	0.000	178.000	No Ice	6.006	6.203	0.043
Mount Pipe	_	110m Log	0.000	0.000	170.000	1/2" Ice	6.562	7.359	0.043
1.20 and 1 spe			1.000			1" Ice	7.083	8.229	0.160
			500			2" Ice	8.167	10.019	0.310
						4" Ice	10.691	13.840	0.750
(2) LPA-80080-4CF-EDIN-0	Α	From Leg	4.000	0.000	178.000	No Ice	2.856	7.227	0.030
w/ Mount Pipe		- 6	0.000			1/2" Ice	3.220	7.922	0.076
1			1.000			1" Ice	3.592	8.634	0.128
						2" Ice	4.450	10.112	0.253
						4" Ice	6.318	13.339	0.613
(A) I DA 00000 ACE EDDI O	В	From Leg	4.000	0.000	179 000	Mo Ico	2.856	7 227	0.020
(2) LPA-80080-4CF-EDIN-0 w/ Mount Pipe	ь	rioni Leg	4.000 0.000	0.000	178.000	No Ice 1/2" Ice	3.220	7.227 7.922	0.030 0.076

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_AA_A$ Front	$C_AA_A$ Side	Weight
			Vert ft ft ft	o	ft		ft²	ft²	K
			1.000			1" Ice	3.592	8.634	0.128
						2" Ice	4.450	10.112	0.253
						4" Ice	6.318	13.339	0.613
(2) LPA-80063/4CF w/	C	From Leg	4.000	0.000	178.000	No Ice	7.111	7.128	0.038
Mount Pipe			0.000			1/2" Ice	7.584	7.829	0.103
			1.000			1" Ice	8.067	8.542	0.174
						2" Ice 4" Ice	9.063 11.195	10.023 13.247	0.339 0.786
(2) 742 213 w/ Mount Pipe	Α	From Leg	4.000	0.000	178.000	No Ice	5.373	4.620	0.780
(2) 742 213 W/ Would Tipe	А	1 Ioni Leg	0.000	0.000	176.000	1/2" Ice	5.950	6.000	0.094
			1.000			1" Ice	6.501	6.982	0.146
						2" Ice	7.611	8.852	0.277
						4" Ice	9.933	12.794	0.683
(2) 742 213 w/ Mount Pipe	В	From Leg	4.000	0.000	178.000	No Ice	5.373	4.620	0.049
			0.000			1/2" Ice	5.950	6.000	0.094
			1.000			1" Ice	6.501	6.982	0.146
						2" Ice	7.611	8.852	0.277
(2) 742 213 w/ Mount Pipe	С	From Leg	4.000	0.000	178.000	4" Ice No Ice	9.933 5.373	12.794 4.620	0.683 0.049
(2) 742 213 W/ Mount Pipe	C	From Leg	0.000	0.000	178.000	1/2" Ice	5.950	6.000	0.049
			1.000			1" Ice	6.501	6.982	0.034
			1.000			2" Ice	7.611	8.852	0.277
						4" Ice	9.933	12.794	0.683
DB-T1-6Z-8AB-0Z	C	From Leg	4.000	0.000	178.000	No Ice	5.600	2.333	0.044
			0.000			1/2" Ice	5.915	2.558	0.080
			1.000			1" Ice	6.240	2.791	0.120
						2" Ice	6.914	3.284	0.213
DI (C. M. (FLD 1001 1)	0	N		0.000	170,000	4" Ice	8.365	4.373	0.455
Platform Mount [LP 1201-1]	С	None		0.000	178.000	No Ice 1/2" Ice	23.100 26.800	23.100 26.800	2.100
						1" Ice	30.500	30.500	2.500 2.900
						2" Ice	37.900	37.900	3.700
						4" Ice	52.700	52.700	5.300
*///*									
RR90-17-02DP w/ Mount	A	From Leg	4.000	0.000	168.000	No Ice	4.593	3.319	0.034
Pipe			0.000			1/2" Ice	5.088	4.089	0.072
			1.000			1" Ice	5.578	4.784	0.115
						2" Ice	6.588	6.225	0.224
DD00 17 02DD/ Mt	D	F I	4.000	0.000	169,000	4" Ice	8.731	9.308	0.557
RR90-17-02DP w/ Mount Pipe	В	From Leg	4.000 0.000	0.000	168.000	No Ice 1/2" Ice	4.593 5.088	3.319 4.089	0.034 0.072
ripe			1.000			1" Ice	5.578	4.089	0.072
			1.000			2" Ice	6.588	6.225	0.224
						4" Ice	8.731	9.308	0.557
RR90-17-02DP w/ Mount	C	From Leg	4.000	0.000	168.000	No Ice	4.593	3.319	0.034
Pipe		_	0.000			1/2" Ice	5.088	4.089	0.072
			1.000			1" Ice	5.578	4.784	0.115
						2" Ice	6.588	6.225	0.224
(A) IZDAV 110 71 /1		г .	4.000	0.000	160,000	4" Ice	8.731	9.308	0.557
(2) KRY 112 71/1	A	From Leg	4.000	0.000	168.000	No Ice	0.681	0.450	0.013
			0.000 1.000			1/2" Ice 1" Ice	0.802 0.932	0.559 0.677	0.018 0.025
			1.000			2" Ice	1.219	0.677	0.025
						4" Ice	1.896	1.566	0.044
(2) KRY 112 71/1	В	From Leg	4.000	0.000	168.000	No Ice	0.681	0.450	0.013
. ,	-		0.000			1/2" Ice	0.802	0.559	0.018
			0.000			1/2 100	0.002	0.557	

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_AA_A$ Front	$C_AA_A$ Side	Weight
			Vert ft ft ft	0	ft		ft²	ft²	K
						2" Ice	1.219	0.939	0.044
						4" Ice	1.896	1.566	0.111
(2) KRY 112 71/1	C	From Leg	4.000	0.000	168.000	No Ice	0.681	0.450	0.013
			0.000			1/2" Ice	0.802	0.559	0.018
			1.000			1" Ice 2" Ice	0.932 1.219	0.677 0.939	0.025 0.044
						4" Ice	1.896	1.566	0.044
Platform Mount [LP 1201-1]	C	None		0.000	168.000	No Ice	23.100	23.100	2.100
						1/2" Ice	26.800	26.800	2.500
						1" Ice	30.500	30.500	2.900
						2" Ice	37.900	37.900	3.700
						4" Ice	52.700	52.700	5.300
*///*									
800 10121 w/ Mount Pipe	Α	From Leg	4.000	0.000	160.000	No Ice	5.685	4.600	0.066
			0.000			1/2" Ice 1" Ice	6.182	5.351	0.114
			0.000			2" Ice	6.676 7.695	6.046 7.526	0.168 0.298
						4" Ice	9.858	10.832	0.238
800 10121 w/ Mount Pipe	В	From Leg	4.000	0.000	160.000	No Ice	5.685	4.600	0.075
ood 10121 W Mount Tipe	2	Trom Leg	0.000	0.000	100.000	1/2" Ice	6.182	5.351	0.114
			0.000			1" Ice	6.676	6.046	0.168
						2" Ice	7.695	7.526	0.298
						4" Ice	9.858	10.832	0.675
800 10121 w/ Mount Pipe	C	From Leg	4.000	0.000	160.000	No Ice	5.685	4.600	0.066
			0.000			1/2" Ice	6.182	5.351	0.114
			0.000			1" Ice	6.676	6.046	0.168
						2" Ice 4" Ice	7.695 9.858	7.526 10.832	0.298 0.675
P65-17-XLH-RR w/ Mount	A	From Leg	4.000	0.000	160.000	No Ice	11.704	8.938	0.073
Pipe	А	Trom Leg	0.000	0.000	100.000	1/2" Ice	12.424	10.450	0.072
			0.000			1" Ice	13.153	11.986	0.273
						2" Ice	14.639	14.313	0.498
						4" Ice	17.906	19.144	1.126
P65-17-XLH-RR w/ Mount	В	From Leg	4.000	0.000	160.000	No Ice	11.704	8.938	0.092
Pipe			0.000			1/2" Ice	12.424	10.450	0.178
			0.000			1" Ice	13.153	11.986	0.273
						2" Ice	14.639	14.313	0.498
P65-17-XLH-RR w/ Mount	С	From Leg	4.000	0.000	160.000	4" Ice No Ice	17.906 11.704	19.144 8.938	1.126 0.092
Pipe	C	110III Leg	0.000	0.000	100.000	1/2" Ice	12.424	10.450	0.092
Търс			0.000			1" Ice	13.153	11.986	0.273
			0.000			2" Ice	14.639	14.313	0.498
						4" Ice	17.906	19.144	1.126
(2) RRUS-11	Α	From Leg	4.000	0.000	160.000	No Ice	2.942	1.246	0.055
			0.000			1/2" Ice	3.172	1.412	0.074
			0.000			1" Ice	3.410	1.587	0.097
						2" Ice	3.913	1.963	0.151
(2) DDIIC 11	P	Enong I	4.000	0.000	160,000	4" Ice No Ice	5.023	2.819	0.302
(2) RRUS-11	В	From Leg	4.000 0.000	0.000	160.000	No ice 1/2" Ice	2.942 3.172	1.246 1.412	0.055 0.074
			0.000			1" Ice	3.172	1.412	0.074
			0.000			2" Ice	3.913	1.963	0.057
						4" Ice	5.023	2.819	0.302
(2) RRUS-11	C	From Leg	4.000	0.000	160.000	No Ice	2.942	1.246	0.055
• •		3	0.000			1/2" Ice	3.172	1.412	0.074
			0.000			1" Ice	3.410	1.587	0.097
						2" Ice	3.913	1.963	0.151

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	Crown Castle	Kristi Gardner

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weight
			Vert ft ft ft	٥	ft		ft²	$ft^2$	K
						4" Ice	5.023	2.819	0.302
(2) LGP21401	Α	From Leg	4.000	0.000	160.000	No Ice	1.288	0.233	0.014
			0.000			1/2" Ice	1.445	0.313	0.021
			0.000			1" Ice	1.611	0.403	0.030
						2" Ice 4" Ice	1.969 2.788	0.608	0.055
(2) LGP21401	В	From Leg	4.000	0.000	160.000	No Ice	1.288	1.121 0.233	0.135 0.014
(2) LGF21401	ь	rioin Leg	0.000	0.000	100.000	1/2" Ice	1.445	0.233	0.014
			0.000			1" Ice	1.611	0.403	0.021
			0.000			2" Ice	1.969	0.403	0.055
						4" Ice	2.788	1.121	0.135
(2) LGP21401	C	From Leg	4.000	0.000	160.000	No Ice	1.288	0.233	0.014
(2) EGI 21401	C	Trom Ecg	0.000	0.000	100.000	1/2" Ice	1.445	0.313	0.021
			0.000			1" Ice	1.611	0.403	0.030
			0.000			2" Ice	1.969	0.608	0.055
						4" Ice	2.788	1.121	0.135
DC6-48-60-18-8F	Α	From Leg	4.000	0.000	160.000	No Ice	2.567	4.317	0.033
		C	0.000			1/2" Ice	2.798	4.596	0.064
			0.000			1" Ice	3.038	4.885	0.099
						2" Ice	3.543	5.488	0.181
						4" Ice	4.658	6.797	0.397
T-Arm Mount [TA 601-3]	C	None		0.000	160.000	No Ice	10.900	10.900	0.726
						1/2" Ice	14.650	14.650	0.926
						1" Ice	18.400	18.400	1.125
						2" Ice	25.900	25.900	1.524
						4" Ice	40.900	40.900	2.322
*///*									
APXV18-206517S-C w/	A	From Leg	4.000	0.000	150.000	No Ice	5.404	4.700	0.052
Mount Pipe			0.000			1/2" Ice	5.960	5.860	0.097
			0.000			1" Ice	6.481	6.734	0.150
						2" Ice	7.547	8.515	0.280
ADVIVIO 2005155 G	ъ	Б. Т	4.000	0.000	150,000	4" Ice	9.919	12.277	0.679
APXV18-206517S-C w/	В	From Leg	4.000	0.000	150.000	No Ice	5.404	4.700	0.052
Mount Pipe			0.000			1/2" Ice	5.960	5.860	0.097
			0.000			1" Ice	6.481	6.734	0.150
						2" Ice	7.547	8.515	0.280
APXV18-206517S-C w/	С	Enom Loo	4.000	0.000	150.000	4" Ice No Ice	9.919 5.404	12.277 4.700	0.679 0.052
	C	From Leg	0.000	0.000	130.000	1/2" Ice	5.960		0.032
Mount Pipe			0.000			1" Ice	6.481	5.860 6.734	0.097
			0.000			2" Ice	7.547	8.515	0.130
						4" Ice	9.919	12.277	0.280
*///*						4 100	9.919	12.277	0.079
SD212-SF2P2SNM Dipole	Α	From Leg	1.000	0.000	120.000	No Ice	4.510	4.510	0.048
5D212-51 21 251 WI Dipole	Α.	1 Ioni Leg	0.000	0.000	120.000	1/2" Ice	5.510	5.510	0.048
			5.000			1" Ice	6.510	6.510	0.002
			2.000			2" Ice	8.510	8.510	0.106
						4" Ice	12.510	12.510	0.163
Side Arm Mount [SO 702-1]	Α	From Leg	1.000	0.000	120.000	No Ice	1.000	1.430	0.027
,			0.000			1/2" Ice	1.000	2.050	0.038
			0.000			1" Ice	1.000	2.670	0.049
						2" Ice	1.000	3.910	0.071
						4" Ice	1.000	6.390	0.115
*///*									
	_	ъ т	1 000	0.000	117.000		4.510	4 = 40	0.040
SD110-SFXPASNM	В	From Leg	1.000	0.000	115.000	No Ice	4.510	4.510	0.048
SD110-SFXPASNM	В	From Leg	1.000 0.000 7.000	0.000	115.000	No Ice 1/2" Ice 1" Ice	4.510 5.510 6.510	4.510 5.510 6.510	0.048 0.062 0.077

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		$C_AA_A$ Front	$C_AA_A$ Side	Weight
			ft ft ft	۰	ft		ft <sup>2</sup>	ft²	K
			-			2" Ice 4" Ice	8.510 12.510	8.510 12.510	0.106 0.163
*///*	D	F I	4.000	0.000	91 000	N- I	5 500	5 500	0.041
ANT450D3	В	From Leg	4.000	0.000	81.000	No Ice	5.592	5.592	0.041
			0.000			1/2" Ice	7.656	7.656	0.082
			1.000			1" Ice	9.738	9.738	0.135
						2" Ice	13.950	13.950	0.282
g:1 4 M . rgo 200 11	ъ.		1 000	0.000	01.000	4" Ice	21.924	21.924	0.735
Side Arm Mount [SO 309-1]	В	From Leg	1.000	0.000	81.000	No Ice	2.820	2.200	0.040
			0.000			1/2" Ice	4.070	3.160	0.062
			0.000			1" Ice	5.320	4.120	0.084
						2" Ice	7.820	6.040	0.128
ate ///ate						4" Ice	12.820	9.880	0.216
*///* VC24010 I 1124		F I	4.000	0.000	10,000	N- I	0.156	0.156	0.005
KS24019-L112A	A	From Leg	4.000	0.000	48.000	No Ice	0.156	0.156	0.005
			0.000			1/2" Ice 1" Ice	0.225 0.302	0.225 0.302	0.007 0.009
			0.000						
						2" Ice	0.484	0.484	0.018
C: 1- A M+ [CO 701 1]		Farm I	1 000	0.000	10,000	4" Ice	0.951	0.951	0.056
Side Arm Mount [SO 701-1]	A	From Leg	1.000	0.000	48.000	No Ice	0.850	1.670	0.065
			0.000			1/2" Ice	1.140	2.340	0.079
			0.000			1" Ice	1.430	3.010	0.093
						2" Ice	2.010	4.350	0.121
*///*						4" Ice	3.170	7.030	0.177
RRH2X40-AWS	A	From Log	4.000	0.000	181.000	No Ice	2.522	1.589	0.044
KKHZA40-AWS	А	From Leg		0.000	181.000				0.044
			0.000			1/2" Ice 1" Ice	2.753 2.993	1.795 2.010	
			0.000						0.082
						2" Ice 4" Ice	3.499	2.465	0.132
DDII2V40 AWG	D	F I	4.000	0.000	101 000		4.615	3.479	0.275
RRH2X40-AWS	В	From Leg	4.000	0.000	181.000	No Ice	2.522 2.753	1.589 1.795	0.044
			0.000			1/2" Ice			0.061
			0.000			1" Ice	2.993	2.010	0.082
						2" Ice	3.499	2.465	0.132
DDIIOVAO ANIG		Б. Т	4.000	0.000	101.000	4" Ice	4.615	3.479	0.275
RRH2X40-AWS	C	From Leg	4.000	0.000	181.000	No Ice	2.522	1.589	0.044
			0.000			1/2" Ice	2.753	1.795	0.061
			0.000			1" Ice	2.993	2.010	0.082
						2" Ice	3.499	2.465	0.132
011 A M 4 F0O 102 01	C	N		0.000	101 000	4" Ice	4.615	3.479	0.275
Side Arm Mount [SO 102-3]	С	None		0.000	181.000	No Ice	3.000	3.000	0.081
						1/2" Ice	3.480	3.480	0.111
						1" Ice	3.960	3.960	0.141
						2" Ice	4.920	4.920	0.201
						4" Ice	6.840	6.840	0.321

### **Load Combinations**

Comb.	Description
No.	
1	D 101

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Comb.	Description
No.	P
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29 30	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service  Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service  Dead+Wind 180 deg - Service
33 34	Dead+Wind 180 deg - Service Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service  Dead+Wind 240 deg - Service
35 36	Dead+Wind 270 deg - Service  Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service
	Zead

### **Maximum Member Forces**

Section No.	Elevation ft	Component Type	Condition	Gov. Load	Force	Major Axis Moment	Minor Axis Moment
				Comb.	K	kip-ft	kip-ft
L1	187 - 136	Pole	Max Tension	30	0.000	0.000	-0.000
			Max. Compression	14	-29.172	3.620	-2.217
			Max. Mx	11	-13.196	757.862	-10.932
			Max. My	8	-13.267	11.185	-743.370
			Max. Vy	11	-23.928	757.862	-10.932
			Max. Vx	8	23.520	11.185	-743.370
			Max. Torque	10			-1.184
L2	136 - 89.5	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-43.449	6.769	-5.027
			Max. Mx	11	-22.969	1984.941	-23.834
			Max. My	8	-23.021	24.132	-1951.384
			Max. Vy	11	-30.168	1984.941	-23.834
			Max. Vx	8	29.738	24.132	-1951.384
			Max. Torque	10			-1.700
L3	89.5 - 44.25	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-61.491	9.210	-8.675

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Client		Designed by
	Crown Castle	Kristi Gardner

Section	Elevation	Component	Condition	Gov.	Force	Major Axis	Minor Axis
No.	ft	Type		Load		Moment	Moment
				Comb.	K	kip-ft	kip-ft
			Max. Mx	11	-36.378	3453.176	-36.362
			Max. My	8	-36.407	36.293	-3400.747
			Max. Vy	11	-35.898	3453.176	-36.362
			Max. Vx	8	35.460	36.293	-3400.747
			Max. Torque	10			-1.149
L4	44.25 - 0	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-86.837	12.848	-11.811
			Max. Mx	11	-56.534	5423.488	-49.942
			Max. My	8	-56.535	50.114	-5347.448
			Max. Vy	11	-41.150	5423.488	-49.942
			Max. Vx	8	40.700	50.114	-5347.448
			Max. Torque	7			0.906

### **Maximum Reactions**

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, Z
		Load	K	K	K
		Comb.			
Pole	Max. Vert	23	86.837	10.112	-5.810
	Max. H <sub>x</sub>	11	56.563	41.111	-0.252
	Max. H <sub>z</sub>	2	56.563	-0.252	40.661
	Max. M <sub>x</sub>	2	5344.185	-0.252	40.661
	Max. M <sub>z</sub>	5	5419.901	-41.111	0.252
	Max. Torsion	8	0.738	0.252	-40.661
	Min. Vert	1	56.563	0.000	0.000
	Min. H <sub>x</sub>	5	56.563	-41.111	0.252
	Min. Hz	8	56.563	0.252	-40.661
	Min. M <sub>x</sub>	8	-5347.448	0.252	-40.661
	Min. M <sub>z</sub>	11	-5423.488	41.111	-0.252
	Min. Torsion	2	-0.727	-0.252	40.661

## **Tower Mast Reaction Summary**

Load	Vertical	$Shear_x$	Shearz	Overturning	Overturning	Torque
Combination				Moment, $M_x$	Moment, $M_z$	_
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	56.563	0.000	0.000	1.574	1.732	0.000
Dead+Wind 0 deg - No Ice	56.563	0.252	-40.661	-5344.185	-46.487	0.727
Dead+Wind 30 deg - No Ice	56.563	20.774	-35.339	-4651.926	-2750.900	0.580
Dead+Wind 60 deg - No Ice	56.563	35.729	-20.549	-2712.901	-4717.591	0.277
Dead+Wind 90 deg - No Ice	56.563	41.111	-0.252	-46.652	-5419.901	-0.105
Dead+Wind 120 deg - No Ice	56.563	35.477	20.112	2632.711	-4669.601	-0.463
Dead+Wind 150 deg - No Ice	56.563	20.337	35.087	4607.211	-2667.415	-0.697
Dead+Wind 180 deg - No Ice	56.563	-0.252	40.661	5347.448	50.115	-0.738
Dead+Wind 210 deg - No Ice	56.563	-20.774	35.339	4655.187	2754.510	-0.578
Dead+Wind 240 deg - No Ice	56.563	-35.729	20.549	2716.176	4721.191	-0.264
Dead+Wind 270 deg - No Ice	56.563	-41.111	0.252	49.942	5423.488	0.117
Dead+Wind 300 deg - No Ice	56.563	-35.477	-20.112	-2629.420	4673.226	0.462
Dead+Wind 330 deg - No Ice	56.563	-20.337	-35.087	-4603.933	2671.050	0.684
Dead+Ice+Temp	86.837	-0.000	0.000	11.811	12.848	0.000
Dead+Wind 0 deg+Ice+Temp	86.837	0.051	-11.531	-1543.204	2.519	0.216
Dead+Wind 30 deg+Ice+Temp	86.837	5.868	-10.012	-1340.087	-783.074	0.312
Dead+Wind 60 deg+Ice+Temp	86.837	10.112	-5.810	-774.696	-1355.360	0.325

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Load	Vertical	$Shear_x$	$Shear_z$	Overturning	Overturning	Torque
Combination				Moment, $M_x$	Moment, $M_z$	
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 90 deg+Ice+Temp	86.837	11.647	-0.051	1.471	-1560.999	0.251
Dead+Wind 120 deg+Ice+Temp	86.837	10.061	5.721	780.444	-1344.891	0.109
Dead+Wind 150 deg+Ice+Temp	86.837	5.779	9.960	1353.498	-764.938	-0.062
Dead+Wind 180 deg+Ice+Temp	86.837	-0.051	11.531	1567.077	23.460	-0.217
Dead+Wind 210 deg+Ice+Temp	86.837	-5.868	10.012	1363.957	809.046	-0.313
Dead+Wind 240 deg+Ice+Temp	86.837	-10.112	5.810	798.572	1381.326	-0.325
Dead+Wind 270 deg+Ice+Temp	86.837	-11.647	0.051	22.412	1586.967	-0.250
Dead+Wind 300 deg+Ice+Temp	86.837	-10.061	-5.721	-756.559	1370.866	-0.108
Dead+Wind 330 deg+Ice+Temp	86.837	-5.779	-9.960	-1329.618	790.918	0.062
Dead+Wind 0 deg - Service	56.563	0.087	-14.069	-1851.000	-14.929	0.253
Dead+Wind 30 deg - Service	56.563	7.188	-12.228	-1611.166	-952.210	0.199
Dead+Wind 60 deg - Service	56.563	12.363	-7.110	-939.178	-1633.855	0.092
Dead+Wind 90 deg - Service	56.563	14.225	-0.087	-15.104	-1877.219	-0.041
Dead+Wind 120 deg - Service	56.563	12.276	6.959	913.464	-1617.120	-0.163
Dead+Wind 150 deg - Service	56.563	7.037	12.141	1597.715	-923.210	-0.241
Dead+Wind 180 deg - Service	56.563	-0.087	14.069	1854.282	18.565	-0.254
Dead+Wind 210 deg - Service	56.563	-7.188	12.228	1614.448	955.844	-0.199
Dead+Wind 240 deg - Service	56.563	-12.363	7.110	942.462	1637.488	-0.090
Dead+Wind 270 deg - Service	56.563	-14.225	0.087	18.389	1880.853	0.042
Dead+Wind 300 deg - Service	56.563	-12.276	-6.959	-910.178	1620.756	0.163
Dead+Wind 330 deg - Service	56.563	-7.037	-12.141	-1594.431	926.847	0.240

### **Solution Summary**

	Sum of Applied Forces			Sum of Reactions			
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
1	0.000	-56.563	0.000	0.000	56.563	0.000	0.000%
2	0.252	-56.563	-40.661	-0.252	56.563	40.661	0.000%
3	20.774	-56.563	-35.339	-20.774	56.563	35.339	0.000%
4	35.729	-56.563	-20.549	-35.729	56.563	20.549	0.000%
5	41.111	-56.563	-0.252	-41.111	56.563	0.252	0.000%
6	35.477	-56.563	20.112	-35.477	56.563	-20.112	0.000%
7	20.337	-56.563	35.087	-20.337	56.563	-35.087	0.000%
8	-0.252	-56.563	40.661	0.252	56.563	-40.661	0.000%
9	-20.774	-56.563	35.339	20.774	56.563	-35.339	0.000%
10	-35.729	-56.563	20.549	35.729	56.563	-20.549	0.000%
11	-41.111	-56.563	0.252	41.111	56.563	-0.252	0.000%
12	-35.477	-56.563	-20.112	35.477	56.563	20.112	0.000%
13	-20.337	-56.563	-35.087	20.337	56.563	35.087	0.000%
14	0.000	-86.837	0.000	0.000	86.837	-0.000	0.000%
15	0.051	-86.837	-11.531	-0.051	86.837	11.531	0.000%
16	5.868	-86.837	-10.012	-5.868	86.837	10.012	0.000%
17	10.112	-86.837	-5.810	-10.112	86.837	5.810	0.000%
18	11.647	-86.837	-0.051	-11.647	86.837	0.051	0.000%
19	10.061	-86.837	5.721	-10.061	86.837	-5.721	0.000%
20	5.779	-86.837	9.960	-5.779	86.837	-9.960	0.000%
21	-0.051	-86.837	11.531	0.051	86.837	-11.531	0.000%
22	-5.868	-86.837	10.012	5.868	86.837	-10.012	0.000%
23	-10.112	-86.837	5.810	10.112	86.837	-5.810	0.000%
24	-11.647	-86.837	0.051	11.647	86.837	-0.051	0.000%
25	-10.061	-86.837	-5.721	10.061	86.837	5.721	0.000%
26	-5.779	-86.837	-9.960	5.779	86.837	9.960	0.000%
27	0.087	-56.563	-14.069	-0.087	56.563	14.069	0.000%
28	7.188	-56.563	-12.228	-7.188	56.563	12.228	0.000%
29	12.363	-56.563	-7.110	-12.363	56.563	7.110	0.000%
30	14.225	-56.563	-0.087	-14.225	56.563	0.087	0.000%
31	12.276	-56.563	6.959	-12.276	56.563	-6.959	0.000%

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	Sui	n of Applied Force.	s		Sum of Reaction	is	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
32	7.037	-56.563	12.141	-7.037	56.563	-12.141	0.000%
33	-0.087	-56.563	14.069	0.087	56.563	-14.069	0.000%
34	-7.188	-56.563	12.228	7.188	56.563	-12.228	0.000%
35	-12.363	-56.563	7.110	12.363	56.563	-7.110	0.000%
36	-14.225	-56.563	0.087	14.225	56.563	-0.087	0.000%
37	-12.276	-56.563	-6.959	12.276	56.563	6.959	0.000%
38	-7.037	-56.563	-12.141	7.037	56.563	12.141	0.000%

#### **Non-Linear Convergence Results**

Combination         of Cycles         Tolerance         Tolerance           1         Yes         4         0.00000001         0.00000001           2         Yes         4         0.00000001         0.00077771           3         Yes         6         0.00000001         0.00005377           4         Yes         6         0.00000001         0.00005437           5         Yes         5         0.00000001         0.00004548           6         Yes         6         0.00000001         0.00005191           7         Yes         6         0.000000001         0.00005244           8         Yes         4         0.00000001         0.00005244           9         Yes         6         0.00000001         0.0005341           10         Yes         6         0.00000001         0.0005341           10         Yes         6         0.00000001         0.0005341           11         Yes         4         0.00000001         0.0005341           12         Yes         6         0.00000001         0.0005341           14         Yes         4         0.00000001         0.0005373           15 <t< th=""><th>Load</th><th>Converged?</th><th>Number</th><th>Displacement</th><th>Force</th></t<>	Load	Converged?	Number	Displacement	Force
2         Yes         4         0.00000001         0.00077771           3         Yes         6         0.00000001         0.00005377           4         Yes         6         0.00000001         0.00005437           5         Yes         5         0.00000001         0.0000448           6         Yes         6         0.00000001         0.00005244           8         Yes         4         0.00000001         0.00074443           9         Yes         6         0.00000001         0.00074443           9         Yes         6         0.00000001         0.00074443           9         Yes         6         0.00000001         0.00005341           10         Yes         6         0.00000001         0.00005341           10         Yes         6         0.00000001         0.0005341           11         Yes         4         0.00000001         0.0005341           12         Yes         6         0.00000001         0.0005341           12         Yes         6         0.00000001         0.0005373           13         Yes         5         0.00000001         0.0005373           14	Combination		of Cycles	Tolerance	Tolerance
3 Yes 6 0.00000001 0.0005377 4 Yes 6 0.00000001 0.00005437 5 Yes 5 0.00000001 0.00005437 6 Yes 6 0.00000001 0.00005438 6 Yes 6 0.00000001 0.00005191 7 Yes 6 0.00000001 0.00005244 8 Yes 4 0.00000001 0.00005244 9 Yes 6 0.00000001 0.00005443 9 Yes 6 0.00000001 0.00005444 10 Yes 6 0.00000001 0.00005381 11 Yes 4 0.00000001 0.0005381 11 Yes 6 0.00000001 0.0005381 12 Yes 6 0.00000001 0.0005373 13 Yes 6 0.00000001 0.00005272 13 Yes 6 0.00000001 0.00005373 15 Yes 5 0.00000001 0.0005373 15 Yes 5 0.00000001 0.0005373 16 Yes 5 0.00000001 0.0005196 17 Yes 5 0.00000001 0.0005196 18 Yes 5 0.00000001 0.00051961 18 Yes 5 0.00000001 0.000519630 20 Yes 5 0.00000001 0.00051630 20 Yes 5 0.00000001 0.00051534 21 Yes 5 0.00000001 0.00051630 20 Yes 5 0.00000001 0.00051630 21 Yes 5 0.00000001 0.00051630 22 Yes 5 0.00000001 0.00051630 23 Yes 5 0.00000001 0.00051656 24 Yes 5 0.00000001 0.00051656 25 Yes 5 0.00000001 0.00051656 27 Yes 4 0.00000001 0.00051656 27 Yes 4 0.00000001 0.000014552 31 Yes 5 0.00000001 0.000014552 31 Yes 5 0.00000001 0.000014552 32 Yes 5 0.00000001 0.000014552 33 Yes 5 0.00000001 0.000014552 34 Yes 5 0.00000001 0.000014552 35 Yes 5 0.00000001 0.000008627 36 Yes 5 0.00000001 0.000008627 37 Yes 5 0.00000001 0.0000011845 34 Yes 5 0.00000001 0.000011251 36 Yes 5 0.00000001 0.000011251 37 Yes 5 0.00000001 0.00001251		Yes	4	0.00000001	0.00000001
4         Yes         6         0.00000001         0.00005437           5         Yes         5         0.00000001         0.00005191           6         Yes         6         0.00000001         0.00005191           7         Yes         6         0.00000001         0.00005244           8         Yes         4         0.00000001         0.0005414           9         Yes         6         0.00000001         0.0005381           10         Yes         6         0.00000001         0.00053414           10         Yes         6         0.00000001         0.0005381           11         Yes         4         0.00000001         0.0005381           11         Yes         4         0.00000001         0.0005381           12         Yes         6         0.00000001         0.0005272           13         Yes         6         0.00000001         0.00005381           14         Yes         4         0.00000001         0.00005373           15         Yes         5         0.00000001         0.00005373           16         Yes         5         0.00000001         0.00037639           17	2	Yes	4	0.00000001	0.00077771
5         Yes         5         0.00000001         0.00004548           6         Yes         6         0.00000001         0.00005191           7         Yes         6         0.00000001         0.00005244           8         Yes         4         0.00000001         0.00074443           9         Yes         6         0.00000001         0.0005381           10         Yes         6         0.00000001         0.0005381           11         Yes         4         0.00000001         0.0005381           12         Yes         6         0.00000001         0.0005372           13         Yes         6         0.00000001         0.0005572           13         Yes         6         0.00000001         0.0000572           14         Yes         4         0.00000001         0.0005373           15         Yes         5         0.00000001         0.0005723           16         Yes         5         0.00000001         0.0005763           17         Yes         5         0.00000001         0.00057639           19         Yes         5         0.00000001         0.00057639           19		Yes	6	0.00000001	0.00005377
6         Yes         6         0.00000001         0.00005191           7         Yes         6         0.00000001         0.00005244           8         Yes         4         0.00000001         0.00074443           9         Yes         6         0.00000001         0.00005414           10         Yes         6         0.00000001         0.00053491           11         Yes         4         0.00000001         0.0005272           13         Yes         6         0.00000001         0.0005373           15         Yes         5         0.00000001         0.0005373           15         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051696           18         Yes         5         0.00000001         0.00051630           20	4	Yes	6	0.00000001	0.00005437
7 Yes 6 0.00000001 0.00005244 8 Yes 4 0.00000001 0.00074443 9 Yes 6 0.00000001 0.00005414 10 Yes 6 0.00000001 0.00005381 11 Yes 4 0.00000001 0.0005381 11 Yes 6 0.00000001 0.00005373 12 Yes 6 0.00000001 0.00005174 14 Yes 4 0.00000001 0.00005373 15 Yes 5 0.00000001 0.00005373 16 Yes 5 0.00000001 0.00005373 17 Yes 5 0.00000001 0.00051961 18 Yes 5 0.00000001 0.00051961 18 Yes 5 0.00000001 0.00051961 18 Yes 5 0.00000001 0.00051963 20 Yes 5 0.00000001 0.00051354 21 Yes 5 0.00000001 0.0005373 22 Yes 5 0.00000001 0.00054117 23 Yes 5 0.00000001 0.0005417 24 Yes 5 0.00000001 0.0005417 25 Yes 5 0.00000001 0.00051795 26 Yes 5 0.00000001 0.00051656 27 Yes 5 0.00000001 0.00051655 27 Yes 4 0.00000001 0.00051656 27 Yes 5 0.00000001 0.00051656 27 Yes 4 0.00000001 0.00051656 27 Yes 5 0.00000001 0.00051656 27 Yes 4 0.00000001 0.00051656 27 Yes 5 0.00000001 0.00051656 27 Yes 4 0.00000001 0.000182 29 Yes 5 0.00000001 0.000182 29 Yes 5 0.00000001 0.00018352 31 Yes 5 0.00000001 0.00009182 32 Yes 5 0.00000001 0.00008627 33 Yes 4 0.00000001 0.00008627 34 Yes 5 0.00000001 0.00008627 35 Yes 5 0.00000001 0.00008776 36 Yes 5 0.00000001 0.00001845 36 Yes 5 0.00000001 0.00001855 37 Yes 5 0.00000001 0.00001855		Yes		0.00000001	0.00004548
8         Yes         4         0.00000001         0.00074443           9         Yes         6         0.00000001         0.00005414           10         Yes         6         0.00000001         0.00005381           11         Yes         4         0.00000001         0.00053491           12         Yes         6         0.00000001         0.00005272           13         Yes         6         0.00000001         0.00005373           14         Yes         4         0.00000001         0.00005373           15         Yes         5         0.00000001         0.00037238           16         Yes         5         0.00000001         0.00037238           16         Yes         5         0.00000001         0.00037238           16         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051696           18         Yes         5         0.00000001         0.00051696           19         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051630	6		6	0.00000001	0.00005191
9 Yes 6 0.00000001 0.00005414 10 Yes 6 0.00000001 0.00005381 11 Yes 4 0.00000001 0.000053491 12 Yes 6 0.00000001 0.00005272 13 Yes 6 0.00000001 0.00005194 14 Yes 4 0.00000001 0.00005373 15 Yes 5 0.00000001 0.00005373 16 Yes 5 0.00000001 0.00005373 17 Yes 5 0.00000001 0.00051961 18 Yes 5 0.00000001 0.00051961 18 Yes 5 0.00000001 0.00051961 18 Yes 5 0.00000001 0.00051630 20 Yes 5 0.00000001 0.00051630 20 Yes 5 0.00000001 0.00051630 20 Yes 5 0.00000001 0.00051630 21 Yes 5 0.00000001 0.00051417 22 Yes 5 0.00000001 0.00054117 23 Yes 5 0.00000001 0.00054117 23 Yes 5 0.00000001 0.0005417 24 Yes 5 0.00000001 0.0005417 25 Yes 5 0.00000001 0.00054165 27 Yes 5 0.00000001 0.00051656 27 Yes 4 0.00000001 0.00051656 27 Yes 4 0.00000001 0.00051656 27 Yes 4 0.00000001 0.00051656 27 Yes 5 0.00000001 0.00051656 27 Yes 5 0.00000001 0.00051656 27 Yes 5 0.00000001 0.00051795 26 Yes 5 0.00000001 0.00051656 27 Yes 4 0.00000001 0.00051852 31 Yes 5 0.00000001 0.0005175 33 Yes 4 0.00000001 0.0000182 31 Yes 5 0.00000001 0.0000182 31 Yes 5 0.00000001 0.00008627 32 Yes 5 0.00000001 0.00008677 33 Yes 4 0.00000001 0.00008776 33 Yes 5 0.00000001 0.00008776 33 Yes 5 0.00000001 0.00009274 36 Yes 5 0.00000001 0.00009274 36 Yes 5 0.00000001 0.00001251 37 Yes 5 0.00000001 0.00009902		Yes	6	0.00000001	0.00005244
10         Yes         6         0.00000001         0.00005381           11         Yes         4         0.00000001         0.00053491           12         Yes         6         0.00000001         0.00005272           13         Yes         6         0.00000001         0.00005194           14         Yes         4         0.00000001         0.0005373           15         Yes         5         0.00000001         0.00037238           16         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051696           18         Yes         5         0.00000001         0.00051696           19         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051636 <td< td=""><td></td><td></td><td></td><td></td><td></td></td<>					
11         Yes         4         0.00000001         0.00053491           12         Yes         6         0.00000001         0.00005272           13         Yes         6         0.00000001         0.00005194           14         Yes         4         0.00000001         0.00005373           15         Yes         5         0.00000001         0.00037238           16         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051696           18         Yes         5         0.00000001         0.00051961           18         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051354           21         Yes         5         0.00000001         0.000541354           21         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00054267           <		Yes	6	0.00000001	0.00005414
12         Yes         6         0.00000001         0.00005272           13         Yes         6         0.00000001         0.00005194           14         Yes         4         0.00000001         0.00005373           15         Yes         5         0.00000001         0.00037238           16         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051961           18         Yes         5         0.00000001         0.00037639           19         Yes         5         0.00000001         0.000371554           21         Yes         5         0.00000001         0.00037171           <	10	Yes	6	0.00000001	0.00005381
13         Yes         6         0.00000001         0.00005194           14         Yes         4         0.00000001         0.00005373           15         Yes         5         0.00000001         0.00037238           16         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051961           18         Yes         5         0.00000001         0.00037639           19         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00037639           21         Yes         5         0.00000001         0.00037639           29         Yes         5         0.00000001         0.00037639           21         Yes         5         0.00000001         0.00037639           21         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.00054267 <t< td=""><td></td><td></td><td>4</td><td></td><td></td></t<>			4		
14         Yes         4         0.00000001         0.00005373           15         Yes         5         0.00000001         0.00037238           16         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051961           18         Yes         5         0.00000001         0.00037639           19         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051354           21         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.00054117           23         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00011992 <t< td=""><td>12</td><td>Yes</td><td>6</td><td>0.00000001</td><td>0.00005272</td></t<>	12	Yes	6	0.00000001	0.00005272
15         Yes         5         0.00000001         0.00037238           16         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051961           18         Yes         5         0.00000001         0.00037639           19         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051354           21         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.0005417           23         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00001192 <td< td=""><td></td><td></td><td></td><td></td><td></td></td<>					
16         Yes         5         0.00000001         0.00051696           17         Yes         5         0.00000001         0.00051961           18         Yes         5         0.00000001         0.00037639           19         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051354           21         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.00054117           23         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051656           27         Yes         4         0.00000001         0.00011992           28         Yes         5         0.00000001         0.0009411           30         Yes         4         0.00000001         0.00009411 <td< td=""><td></td><td>Yes</td><td>4</td><td>0.00000001</td><td>0.00005373</td></td<>		Yes	4	0.00000001	0.00005373
17         Yes         5         0.00000001         0.00051961           18         Yes         5         0.00000001         0.00037639           19         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051354           21         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.00054117           23         Yes         5         0.00000001         0.00054177           24         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00011992           28         Yes         5         0.00000001         0.00011992           28         Yes         5         0.00000001         0.00009411 <t< td=""><td></td><td></td><td></td><td></td><td></td></t<>					
18         Yes         5         0.00000001         0.00037639           19         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051354           21         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.00054117           23         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051656           27         Yes         4         0.00000001         0.00011992           28         Yes         5         0.00000001         0.00009182           29         Yes         5         0.00000001         0.00014352           31         Yes         5         0.00000001         0.00008627 <t< td=""><td></td><td>Yes</td><td></td><td>0.00000001</td><td>0.00051696</td></t<>		Yes		0.00000001	0.00051696
19         Yes         5         0.00000001         0.00051630           20         Yes         5         0.00000001         0.00051354           21         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.00054117           23         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051656           27         Yes         4         0.00000001         0.00011992           28         Yes         5         0.00000001         0.00009182           29         Yes         5         0.00000001         0.0009411           30         Yes         4         0.00000001         0.00014352           31         Yes         5         0.00000001         0.00008627 <td< td=""><td></td><td>Yes</td><td></td><td>0.00000001</td><td>0.00051961</td></td<>		Yes		0.00000001	0.00051961
20         Yes         5         0.00000001         0.00051354           21         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.00054117           23         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00038450           25         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051656           27         Yes         4         0.00000001         0.000011992           28         Yes         5         0.00000001         0.00009182           29         Yes         5         0.00000001         0.0009411           30         Yes         4         0.00000001         0.00014352           31         Yes         5         0.00000001         0.0008627           32         Yes         5         0.00000001         0.0008776           33         Yes         4         0.00000001         0.00011845           34         Yes         5         0.00000001         0.00009274					
21         Yes         5         0.00000001         0.00037917           22         Yes         5         0.00000001         0.00054117           23         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00038450           25         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051656           27         Yes         4         0.00000001         0.00011992           28         Yes         5         0.00000001         0.00009182           29         Yes         5         0.00000001         0.0000911           30         Yes         4         0.00000001         0.00014352           31         Yes         5         0.00000001         0.00014352           31         Yes         5         0.00000001         0.00008627           32         Yes         5         0.00000001         0.00001845           34         Yes         5         0.00000001         0.00009274           36         Yes         4         0.00000001         0.0001251		Yes		0.00000001	0.00051630
22         Yes         5         0.00000001         0.00054117           23         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00038450           25         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051656           27         Yes         4         0.00000001         0.00011992           28         Yes         5         0.00000001         0.00009182           29         Yes         5         0.00000001         0.00009411           30         Yes         4         0.00000001         0.00014352           31         Yes         5         0.00000001         0.00008627           32         Yes         5         0.00000001         0.00008776           33         Yes         4         0.00000001         0.0001845           34         Yes         5         0.00000001         0.00009274           36         Yes         4         0.00000001         0.0001251           37         Yes         5         0.00000001         0.00001251					
23         Yes         5         0.00000001         0.00054267           24         Yes         5         0.00000001         0.00038450           25         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051656           27         Yes         4         0.00000001         0.00011992           28         Yes         5         0.00000001         0.00009182           29         Yes         5         0.00000001         0.00009411           30         Yes         4         0.00000001         0.00014352           31         Yes         5         0.00000001         0.00008627           32         Yes         5         0.00000001         0.0000876           33         Yes         4         0.00000001         0.0001845           34         Yes         5         0.00000001         0.00009365           35         Yes         5         0.00000001         0.0001251           36         Yes         4         0.00000001         0.0001251           37         Yes         5         0.00000001         0.00001251		Yes		0.00000001	0.00037917
24         Yes         5         0.00000001         0.00038450           25         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051656           27         Yes         4         0.00000001         0.00011992           28         Yes         5         0.00000001         0.00009182           29         Yes         5         0.00000001         0.00009411           30         Yes         4         0.00000001         0.00014352           31         Yes         5         0.00000001         0.00008627           32         Yes         5         0.00000001         0.0000876           33         Yes         4         0.00000001         0.00011845           34         Yes         5         0.00000001         0.00009274           36         Yes         4         0.00000001         0.0001251           37         Yes         5         0.00000001         0.0001251		Yes			0.00054117
25         Yes         5         0.00000001         0.00051795           26         Yes         5         0.00000001         0.00051656           27         Yes         4         0.00000001         0.00011992           28         Yes         5         0.00000001         0.00009182           29         Yes         5         0.00000001         0.00009411           30         Yes         4         0.00000001         0.00014352           31         Yes         5         0.00000001         0.00008627           32         Yes         5         0.00000001         0.00008776           33         Yes         4         0.00000001         0.00011845           34         Yes         5         0.00000001         0.00009274           36         Yes         4         0.00000001         0.0001251           37         Yes         5         0.00000001         0.00008902					
26       Yes       5       0.00000001       0.00051656         27       Yes       4       0.00000001       0.00011992         28       Yes       5       0.00000001       0.00009182         29       Yes       5       0.00000001       0.00009411         30       Yes       4       0.00000001       0.00014352         31       Yes       5       0.00000001       0.00008627         32       Yes       5       0.00000001       0.00008776         33       Yes       4       0.00000001       0.00011845         34       Yes       5       0.00000001       0.00009274         36       Yes       4       0.00000001       0.00011251         37       Yes       5       0.00000001       0.00008902					
27     Yes     4     0.00000001     0.00011992       28     Yes     5     0.00000001     0.00009182       29     Yes     5     0.00000001     0.00009411       30     Yes     4     0.00000001     0.00014352       31     Yes     5     0.00000001     0.00008627       32     Yes     5     0.00000001     0.0008776       33     Yes     4     0.00000001     0.0001845       34     Yes     5     0.00000001     0.00009365       35     Yes     5     0.00000001     0.00009274       36     Yes     4     0.00000001     0.00011251       37     Yes     5     0.00000001     0.00008902					
28     Yes     5     0.00000001     0.00009182       29     Yes     5     0.00000001     0.00009411       30     Yes     4     0.00000001     0.00014352       31     Yes     5     0.00000001     0.00008627       32     Yes     5     0.00000001     0.00008776       33     Yes     4     0.00000001     0.00011845       34     Yes     5     0.00000001     0.00009365       35     Yes     5     0.00000001     0.00009274       36     Yes     4     0.00000001     0.00011251       37     Yes     5     0.00000001     0.00008902					
29       Yes       5       0.00000001       0.00009411         30       Yes       4       0.00000001       0.00014352         31       Yes       5       0.00000001       0.00008627         32       Yes       5       0.00000001       0.00008776         33       Yes       4       0.00000001       0.00011845         34       Yes       5       0.00000001       0.00009365         35       Yes       5       0.00000001       0.00009274         36       Yes       4       0.00000001       0.00011251         37       Yes       5       0.00000001       0.00008902					
30     Yes     4     0.00000001     0.00014352       31     Yes     5     0.00000001     0.00008627       32     Yes     5     0.00000001     0.00008776       33     Yes     4     0.00000001     0.00011845       34     Yes     5     0.00000001     0.00009365       35     Yes     5     0.00000001     0.00009274       36     Yes     4     0.00000001     0.00011251       37     Yes     5     0.00000001     0.00008902					
31       Yes       5       0.00000001       0.00008627         32       Yes       5       0.00000001       0.00008776         33       Yes       4       0.00000001       0.00011845         34       Yes       5       0.00000001       0.00009365         35       Yes       5       0.00000001       0.00009274         36       Yes       4       0.00000001       0.00011251         37       Yes       5       0.00000001       0.00008902					
32     Yes     5     0.00000001     0.00008776       33     Yes     4     0.00000001     0.00011845       34     Yes     5     0.00000001     0.00009365       35     Yes     5     0.00000001     0.00009274       36     Yes     4     0.00000001     0.00011251       37     Yes     5     0.00000001     0.00008902					
33     Yes     4     0.00000001     0.00011845       34     Yes     5     0.00000001     0.00009365       35     Yes     5     0.00000001     0.00009274       36     Yes     4     0.00000001     0.00011251       37     Yes     5     0.00000001     0.00008902					
34     Yes     5     0.00000001     0.00009365       35     Yes     5     0.00000001     0.00009274       36     Yes     4     0.00000001     0.00011251       37     Yes     5     0.00000001     0.00008902					
35     Yes     5     0.00000001     0.00009274       36     Yes     4     0.00000001     0.00011251       37     Yes     5     0.00000001     0.00008902					
36 Yes 4 0.00000001 0.00011251 37 Yes 5 0.00000001 0.00008902					
37 Yes 5 0.00000001 0.00008902					
38 Yes 5 0.00000001 0.00008624	38	Yes	5	0.00000001	0.00008624

### **Maximum Tower Deflections - Service Wind**

FDH Engineering, Inc. 6521 Meridien Drive Raleigh, NC 27616 Phone: (919) 755-1012 FAX: (919) 755-1013

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Client	Crown Castle	Designed by Kristi Gardner

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	187 - 136	47.222	35	2.264	0.002
L2	140.5 - 89.5	26.522	35	1.845	0.001
L3	95.25 - 44.25	11.857	35	1.203	0.000
L4	51 - 0	3.347	35	0.600	0.000

### **Critical Deflections and Radius of Curvature - Service Wind**

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	٥	0	ft
188.000	DB404L-B	35	47.222	2.264	0.002	34126
186.000	PCS 1900MHz 4x45W-65MHz	35	46.751	2.256	0.002	34126
181.000	RRH2X40-AWS	35	44.401	2.218	0.002	28438
178.000	BXA-70080-6CF-EDIN-X w/	35	42.995	2.195	0.002	18959
	Mount Pipe					
168.000	RR90-17-02DP w/ Mount Pipe	35	38.362	2.115	0.001	8980
160.000	800 10121 w/ Mount Pipe	35	34.748	2.046	0.001	6318
150.000	APXV18-206517S-C w/ Mount Pipe	35	30.406	1.949	0.001	4610
120.000	SD212-SF2P2SNM Dipole	35	19.110	1.571	0.001	3947
115.000	SD110-SFXPASNM	35	17.500	1.498	0.001	4022
81.000	ANT450D3	35	8.471	0.998	0.000	4070
48.000	KS24019-L112A	35	2.994	0.563	0.000	3813

### **Maximum Tower Deflections - Design Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	187 - 136	135.681	10	6.511	0.006
L2	140.5 - 89.5	76.303	10	5.309	0.003
L3	95.25 - 44.25	34.147	10	3.465	0.001
L4	51 - 0	9.646	10	1.731	0.000

### **Critical Deflections and Radius of Curvature - Design Wind**

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	٥	0	ft
188.000	DB404L-B	10	135.681	6.511	0.006	12178
186.000	PCS 1900MHz 4x45W-65MHz	10	134.332	6.489	0.006	12178
181.000	RRH2X40-AWS	10	127.593	6.380	0.005	10148
178.000	BXA-70080-6CF-EDIN-X w/	10	123.562	6.313	0.005	6764
	Mount Pipe					
168.000	RR90-17-02DP w/ Mount Pipe	10	110.274	6.084	0.005	3202
160.000	800 10121 w/ Mount Pipe	10	99.908	5.886	0.004	2251
150.000	APXV18-206517S-C w/ Mount Pipe	10	87.452	5.610	0.003	1640
120.000	SD212-SF2P2SNM Dipole	10	55.010	4.524	0.002	1393
115.000	SD110-SFXPASNM	10	50.381	4.313	0.002	1417

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Project		Date
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Client	Crown Castle	Designed by Kristi Gardner

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	٥	0	ft
81.000	ANT450D3	10	24.401	2.876	0.001	1421
48.000	KS24019-L112A	10	8.629	1.623	0.000	1325

### Compression Checks

			Pol	e Des	ign D	ata				
Section	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual	Allow.	Ratio
No.							. 2	P	$P_a$	P
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	$P_a$
L1	187 - 136 (1)	TP36.201x26x0.25	51.000	0.000	0.0	39.000	27.813	-13.171	1084.700	0.012
L2	136 - 89.5 (2)	TP45.003x34.801x0.375	51.000	0.000	0.0	39.000	51.749	-22.951	2018.230	0.011
L3	89.5 - 44.25 (3)	TP53.304x43.103x0.438	51.000	0.000	0.0	39.000	71.537	-36.370	2789.940	0.013
L4	44.25 - 0 (4)	TP61.28x51.079x0.5	51.000	0.000	0.0	39.000	96.458	-56.534	3761.860	0.015

	P	ole Be	ending	g Des	ign D	)ata			
Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
£.		$M_x$	$f_{bx}$	$F_{bx}$	$f_{bx}$	$M_y$	$f_{by}$	$F_{by}$	$f_{by}$
<u> </u>	TD26 201 v26v0 25								$F_{by} = 0.000$
136 - 89.5 (2)	TP45.003x34.801x0.375	1996.76 7	43.191	39.000	1.107	0.000	0.000	39.000	0.000
89.5 - 44.25 (3)	TP53.304x43.103x0.438	3470.76 7	45.828	39.000	1.175	0.000	0.000	39.000	0.000
44.25 - 0 (4)	TP61.28x51.079x0.5	5446.76 7	45.197	39.000	1.159	0.000	0.000	39.000	0.000
	ft 187 - 136 (1) 136 - 89.5 (2) 89.5 - 44.25 (3)	Elevation         Size           ft         187 - 136 (1)         TP36.201x26x0.25           136 - 89.5 (2)         TP45.003x34.801x0.375           89.5 - 44.25 (3)         TP53.304x43.103x0.438	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$

Pole Shear Design Data										
Section	Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
No.			V	$f_{v}$	$F_{v}$	$f_{v}$	T	$f_{vt}$	$F_{vt}$	$f_{vt}$
	ft		K	ksi	ksi	$F_{\nu}$	kip-ft	ksi	ksi	$F_{vt}$
L1	187 - 136 (1)	TP36.201x26x0.25	24.064	0.865	26.000	0.067	1.146	0.028	26.000	0.001
L2	136 - 89.5 (2)	TP45.003x34.801x0.375	30.299	0.586	26.000	0.045	1.172	0.012	26.000	0.000
L3	89.5 - 44.25 (3)	TP53.304x43.103x0.438	36.015	0.503	26.000	0.039	0.327	0.002	26.000	0.000
L4	44.25 - 0 (4)	TP61.28x51.079x0.5	41.256	0.428	26.000	0.033	0.264	0.001	26.000	0.000

## **Pole Interaction Design Data**

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Section No.	Elevation	Ratio P	Ratio $f_{bx}$	Ratio $f_{by}$	Ratio f <sub>v</sub>	Ratio $f_{vt}$	Comb. Stress	Allow. Stress	Criteria
	ft	$P_a$	$F_{bx}$	$F_{by}$	$F_{\nu}$	$F_{vt}$	Ratio	Ratio	
L1	187 - 136 (1)	0.012	0.976	0.000	0.067	0.001	0.989	1.333	H1-3+VT 🖊
L2	136 - 89.5 (2)	0.011	1.107	0.000	0.045	0.000	1.119	1.333	H1-3+VT
L3	89.5 - 44.25 (3)	0.013	1.175	0.000	0.039	0.000	1.188	1.333	H1-3+VT 🖊
L4	44.25 - 0 (4)	0.015	1.159	0.000	0.033	0.000	1.174	1.333	H1-3+VT 🗸

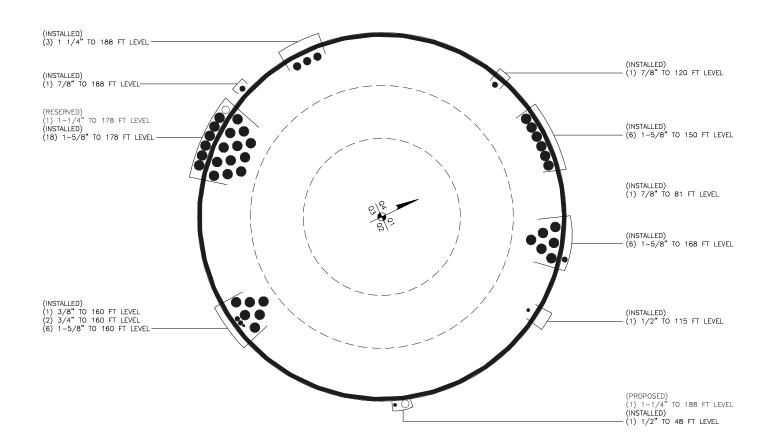
## **Section Capacity Table**

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$SF*P_{allow} \ K$	% Capacity	Pass Fail
L1	187 - 136	Pole	TP36.201x26x0.25	1	-13.171	1445.905	74.2	Pass
L2	136 - 89.5	Pole	TP45.003x34.801x0.375	2	-22.951	2690.300	84.0	Pass
L3	89.5 - 44.25	Pole	TP53.304x43.103x0.438	3	-36.370	3718.990	89.2	Pass
L4	44.25 - 0	Pole	TP61.28x51.079x0.5	4	-56.534	5014.559	88.1	Pass
							Summary	
						Pole (L3)	89.2	Pass
						RATING =	89.2	Pass

 $Program\ Version\ 6.1.4.1-12/17/2013\ File://fdh-server/Projects/2014\ Effective-Client\ Jobs/CROWNC\_Crown\ Castle\ USA\ Inc/CT/803934\_CT\ Somers\ FD\ CAC/1423RV1400/Analysis/CT\ Somers\ FD\ CAC,\ BU\ 803934.eri$ 

# APPENDIX B BASE LEVEL DRAWING





# APPENDIX C ADDITIONAL CALCULATIONS

#### Square, Stiffened / Unstiffened Base Plate, Any Rod Material - Rev. F /G

Assumptions: 1) Rod groups at corners. Total # rods divisible by 4. Maximum total # of rods = 48 (12 per Corner).

- 2) Rod Spacing = Straight Center-to-Center distance between any (2) adjacent rods (same corner)
- 3) Clear space between bottom of leveling nut and top of concrete not exceeding (1)\*(Rod Diameter)

Site Data

BU #: 803934

Site Name: CT Somers FD CAC

App #:

And	Anchor Rod Data					
Qty:	24					
Diam:	2.25	in				
Rod Material:	A615-J					
Yield, Fy:	75	ksi				
Strength, Fu:	100	ksi				
Bolt Circle:	69	in				
Anchor Spacing:	5	in				

Base Reactions				
TIA Revision:	F			
Unfactored Moment, M:	5447	ft-kips		
Unfactored Axial, P:	57	kips		
Unfactored Shear, V:	41	kips		

**Anchor Rod Results** 

TIA F --> Maximum Rod Tension 155.5 Kips
Allowable Tension: 195.0 Kips
Anchor Rod Stress Ratio: 79.8% Pass

	Plate Data	
W=Side:	70	in
Thick:	3.25	in
Grade:	55	ksi
Clip Distance:	14	in

Base Plate Results	Flexural Check
Base Plate Stress:	39.8 ksi
Allowable PL Bending Stress:	55.0 ksi
Base Plate Stress Ratio:	72.4% Pass

PL Ref. Data Yield Line (in): 37.71 Max PL Length: 37.71

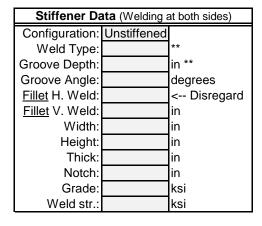
N/A - Unstiffened

Stiffener Results

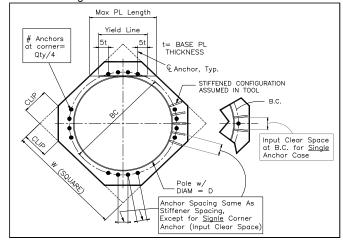
Horizontal Weld: N/A
Vertical Weld: N/A
Plate Flex+Shear, fb/Fb+(fv/Fv)^2: N/A
Plate Tension+Shear, ft/Ft+(fv/Fv)^2: N/A
Plate Comp. (AISC Bracket): N/A

**Pole Results** 

Pole Punching Shear Check: N/A



Pole Data		
Diam:	61.28	in
Thick:	0.5	in
Grade:	65	ksi
# of Sides:	18	"0" IF Round



Stress	Increase F	actor
ASD ASIF:	1.333	

<sup>\*\*</sup> Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

CCI Foundation Tool Suite - v1.0 2/27/2014 Date:

BU:	803934
Site Name:	CT Somers FD CAC
App Number:	
Work Order:	

8 ft

29 ft

4 in



#### **Monopole Drilled Pier**

mput			٠.	_		
	ı	ı	П	u	u	ı

Criteria TIA Revision: ACI 318 Revision: 2002 Seismic Category: В

Forces 57 kips Compression Shear 41 kips 5447 k-ft Moment 0 kips Swelling Force

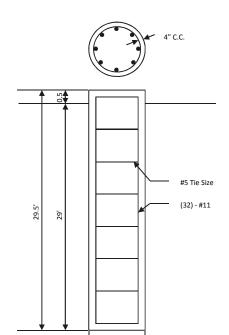
**Foundation Dimensions** Pier Diameter: Ext. above grade: 0.5 ft

Depth below grade:

**Material Properties** Number of Rebar: 32 Rebar Size: 11 Tie Size 5 60 ksi Rebar tensile strength: 3000 psi Concrete Strength: Ultimate Concrete Strain 0.003 in/in

Soil Profile:

Clear Cover to Ties:



Layer	Thickness (ft)	From (ft)	To (ft)	Unit Weight (pcf)	Cohesion (psf)	Friction Angle (deg)	Ultimate Uplift Skin Friction (ksf)	Ultimate Comp. Skin Friction (ksf)	Ultimate Bearing Capacity (ksf)	SPT 'N' Counts
1	4	0	4	120					0	
2	0.5	4	4.5	120		34			0	
3	25	4.5	29.5	60		34			24	

#### **Analysis Results**

Depth to Zero Shear: 5.99 ft 5671.10 k-ft Max Moment, Mu: Soil Safety Factor: 2.48 Safety Factor Req'd: RATING: 80.7%

Soil Axial Capacity

Skin Friction (k): 160.16 kips End Bearing (k): 603.19 kips Comp. Capacity (k), φCn: 763.35 kips Comp. (k), Cu: 74.10 kips RATING: 9.7%

Concrete/Steel Check Mu (from soil analysis)

фМп

RATING: 82.5% rho provided 0.69 rho required 0.33 OK Rebar Spacing 6.97 Spacing required 22.56 OK Dev. Length required 22.68 Dev. Length provided 61.78 OK

7372.43 k-ft

8932.00 k-ft

**Overall Foundation Rating:** 82.5%



## RADIO FREQUENCY FCC REGULATORY COMPLIANCE MAXIMUM PERMISSIBLE EXPOSURE (MPE) ASSESSMENT

**Sprint Existing Facility** 

Site ID: CT33XC554

CT Somers FD CAC

400 Main Street Somers, CT, 06071

March 19, 2014

EBI Project Number: 62141236

21 B Street Burlington, MA 01803 Tel: (781) 273.2500 Fax: (781) 273.3311



March 19, 2014

Sprint Attn: RF Engineering Manager 1 International Boulevard, Suite 800 Mahwah, NJ 07495

Re: Radio Frequency Maximum Permissible Exposure (MPE) Assessment for Site:

CT33XC554 - CT Somers FD CAC

Site Total: 42.207% - MPE% in full compliance

EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at 400 Main Street, Somers, CT, for the purpose of determining whether the radio frequency (RF) exposure levels from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu$ W/cm2). The number of  $\mu$ W/cm2 calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu$ W/cm²). The general population exposure limit for the cellular band (850 MHz Band) is approximately 567  $\mu$ W/cm², and the general population exposure limit for the 1900 MHz and 2500 MHz bands band is 1000  $\mu$ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

#### **CALCULATIONS**

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at 400 Main Street, Somers, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. All calculations were performed assuming the main lobe of the antenna was focused at the base of the tower to present a worst case scenario. Actual values seen from this site will be dramatically less than those shown in this report. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

- 1) 2 channels in the 1900 MHz Band were considered for each sector of the proposed installation.
- 2) 1 channel in the 800 MHz Band was considered for each sector of the proposed installation
- 3) 2 channels in the 2500 MHz Band were considered for each sector of the proposed installation.
- 4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications was used in this direction.



- 6) The antennas used in this modeling are the RFS APXVSPP18-C-A20 and the RFS APXVTMM-C-120. This is based on feedback from the carrier with regards to anticipated antenna selection. The RFS APXVSPP18-C-A20 has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz. The RFS APXVTMM-C-120 has a 15.9 dBd gain value at its main lobe at 2500 MHz. All calculations were performed assuming the main lobe of the antenna was focused at the base of the tower to present a worst case scenario.
- 7) The antenna mounting height centerline for the proposed antennas are 1 antenna per sector at **190 feet** above ground level (AGL) **and** 1 antenna per sector at **186 feet** above ground level (AGL).
- 8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits

Site ID CT33XC554 - CT Somers FD Cac																			
Site Addresss 400 Main Street, Somers, CT, 06071																			
	Site Type		Monopole																
	Sector 1																		
						Power			Antenna Gain										
						Out Per			in direction			Antenna						Power	Power
Antenna						Channel	Number of	Composite	of sample	Antenna	analysis	Height		Cable Loss	Additional			Density	Density
Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	(Watts)	Channels	Power		Height (ft)	height		Cable Size	(dB)	Loss (dB)	Gain Factor	ERP	Value	Percentage
1a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	190	184	56.08388	1/2 "	0.5	3	17.378008	695.12033	7.381257	0.73813%
1a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	190	184	56.08388	1/2 "	0.5	3	9.7723722	195.44744	2.075393	0.36603%
1B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	13.4	186	180	54.86467	1/2 "	0.5	3	9.7723722	390.89489	4.337315	0.76496%
													Sector to	tal Power D	Density Value:		1.869%		
	Sector 2																		
					1				1						1				
						Power			Antenna Gain										
						Out Per			in direction			Antenna						Power	Power
Antenna						Channel	Number of	Composite	of sample	Antenna	analysis	Height		Cable Loss	Additional			Density	Density
Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	(Watts)	Channels	Power	point (dBd)	Height (ft)	height	Meters	Cable Size	(dB)	Loss (dB)	Gain Factor	ERP	Value	Percentage
2a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	190	184	56.08388	1/2 "	0.5	3	17.378008	695.12033	7.381257	0.73813%
2a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	190	184	56.08388	1/2 "	0.5	3	9.7723722	195.44744		0.36603%
2B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	13.4	186	180	54.86467	1/2 "	0.5	3	9.7723722		4.337315	0.76496%
													Sector to	tal Power D	ensity Value:		1.869%		
	Sector 3																		
						Power			Antenna Gain									Davis	D
A 4						Out Per	Nihanaf	C:	in direction	A t		Antenna		Cabla Lasa	A al al (4) a a l			Power	Power
Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Channel (Watts)	Channels	Composite Power	of sample point (dBd)	Antenna Height (ft)	height	Height Meters	Cable Size	Cable Loss (dB)		Gain Factor	ERP	Density Value	Density
3a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	190	184	56.08388	1/2 "	0.5	3	17.378008	695.12033	7.381257	Percentage 0.73813%
3a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	190	184	56.08388	1/2 "	0.5	3	9.7723722	195.44744	2.075393	0.75813%
3B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	13.4	186	180	54.86467	1/2 "	0.5	3	9.7723722	390.89489	4.337315	0.76496%
30	5			2500 141112					23.7	130	100	300407	-	0.0	Density Value:	3.7.23722	1.869%		0.7043070
The state of the s																			

Site Composite MPE %							
Carrier	MPE %						
Sprint	5.607%						
MetroPCS	3.030%						
AT&T	14.670%						
Verizon Wireless	10.910%						
T-Mobile	2.820%						
Town	5.170%						
Total Site MPE %	42.207%						



#### **Summary**

All calculations performed for this analysis yielded results that were well within the allowable limits for general public Maximum Permissible Exposure (MPE) to radio frequency energy.

The anticipated Maximum Composite contributions from the Sprint facility are **5.607%** (**1.869%** from each sector) of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **42.207**% of the allowable FCC established general public limit sampled at 6 feet above ground level. This total composite site value is based upon MPE values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

Scott Heffernan

RF Engineering Director

**EBI Consulting** 

21 B Street

Burlington, MA 01803