



Victoria Masse  
Northeast Site Solutions  
5 Melrose Drive,  
Farmington CT 06032  
860-306-2326  
victoria@northeastsitesolutions.com

June 5, 2024

Members of the Siting Council  
Connecticut Siting Council  
Ten Franklin Square  
New Britain, CT 06051

RE: Notice of Exempt Modification  
248 Hall Hill Road, Somers, CT 06071  
Latitude: 42.00259444  
Longitude: -72.48499722  
T-Mobile Site#: CTHA027B\_Anchor

Dear Ms. Bachman:

T-Mobile currently maintains six (6) antennas at the 175-foot level of the existing 180-foot monopole located at 248 Hall Hill Road, Somers, CT 06071. The property is owned by John A & Debra Romano and the tower is owned by Vertical Bridge. T-Mobile now intends to replace three (3) existing antennas with three (3) new 600/700/1900/2100 MHz. The new antennas would be installed at the 175-foot level of the tower. T-Mobile also intends to make the following modifications.

Planned Modifications

Remove:

None

Remove and Replace:

- (3) RFS APX18-206513 Antenna (Remove) - (3) AIR 6419 B41 600/700/1900/2100 MHz Antenna (Replace)
- (3) Hybrid lines (Remove) – (3) Hybrid lines (Replace)
- (3) RRUS 2217 Radio (Remove) – (3) 4460 B25+B66 Radio (Replace)

Install New:

None

Existing to Remain:

- (3) 4480 B71+B85 Radio (Relocated)
- (3) RFS APXVAALL24 Antenna (Relocated)
- (1) Commscope VHLP1-23-CR4B (Shown on Structural only for reserved loading)

5 Melrose Drive, Farmington CT 06032



This facility was approved by the Connecticut Siting Council, Docket No. 476 on February 15, 2018. Please see attached.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Tim Keeney, First Selectman for the Town of Somers, Jennifer Roy, Zoning Enforcement Officer for the Town of Somers, as well as the property owner Deborah and John Romano and Vertical Bridge tower owner.

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

*Victoria Masse*

Victoria Masse  
Mobile: 860-306-2326  
Fax: 413-521-0558  
Office: 5 Melrose Drive, Farmington CT 06032  
Email: [victoria@northeastsitesolutions.com](mailto:victoria@northeastsitesolutions.com)



Attachments:

Cc: Tim Keeney, First Selectman  
Town of Somers  
600 Main Street  
Somers, CT 06071

Jennifer Roy, Zoning Enforcement Officer  
Town of Somers  
600 Main Street  
Somers, CT 06071

Deborah and John Romano, Property Owner  
248 Hall Hill Road  
Somers, CT 06071

Vertical Bridge, Tower Owner  
750 Park of Commerce Dr #200,  
Boca Raton, FL 33487

# Exhibit A

## **Original Facility Approval**

<b>DOCKET NO. 476</b> – Eco-Site, Inc. and T-Mobile Northeast, LLC application for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of a telecommunications facility located at 248 Hall Hill Road, Somers, Connecticut.	} } }	Connecticut  Siting  Council
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February 15, 2018

### Decision and Order

Pursuant to Connecticut General Statutes §16-50p, and the foregoing Findings of Fact and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the construction, maintenance, and operation of a telecommunications facility, including effects on the natural environment, ecological balance, public health and safety, scenic, historic, and recreational values, agriculture, forests and parks, air and water purity, and fish, aquaculture and wildlife are not disproportionate, either alone or cumulatively with other effects, when compared to need, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application, and therefore directs that a Certificate of Environmental Compatibility and Public Need, as provided by General Statutes § 16-50k, be issued to Eco-Site, Inc., hereinafter referred to as the Certificate Holder, for a telecommunications facility at 248 Hall Hill Road, Somers, Connecticut.

Unless otherwise approved by the Council, the facility shall be constructed, operated, and maintained substantially as specified in the Council’s record in this matter, and subject to the following conditions:

1. The tower shall be constructed as a monopole at a height of 180 feet above ground level to provide the proposed wireless services, sufficient to accommodate the antennas of T-Mobile Northeast, LLC and other entities, both public and private. The height of the tower may be extended after the date of this Decision and Order pursuant to regulations of the Federal Communications Commission.
  
2. The Certificate Holder shall prepare a Development and Management (D&M) Plan for this site in compliance with Sections 16-50j-75 through 16-50j-77 of the Regulations of Connecticut State Agencies. The D&M Plan shall be served on the Town of Somers for comment, and all parties and intervenors as listed in the service list, and submitted to and approved by the Council prior to the commencement of facility construction and shall include:
  - a) final site plan(s) for development of the facility that employ the governing standard in the State of Connecticut for tower design in accordance with the currently adopted International Building Code and include specifications for the tower, tower foundation, antennas, and equipment compound including, but not limited to, fencing, radio equipment, access road, utility line, and emergency backup generator;
  - b) construction plans for site clearing, grading, landscaping, water drainage and stormwater control, and erosion and sedimentation controls consistent with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control, as amended;
  - c) plans for seasonal restrictions to protect the potential vernal pool;
  - d) hours of construction; and
  - e) plans for disposition of 30 cubic yards of net cut.

3. Prior to the commencement of operation, the Certificate Holder shall provide the Council worst-case modeling of the electromagnetic radio frequency power density of all proposed entities' antennas at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin No. 65, August 1997. The Certificate Holder shall ensure a recalculated report of the electromagnetic radio frequency power density be submitted to the Council if and when circumstances in operation cause a change in power density above the levels calculated and provided pursuant to this Decision and Order.
4. Upon the establishment of any new federal radio frequency standards applicable to frequencies of this facility, the facility granted herein shall be brought into compliance with such standards.
5. The Certificate Holder shall permit public or private entities to share space on the proposed tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
6. Unless otherwise approved by the Council, if the facility authorized herein is not fully constructed with at least one fully operational wireless telecommunications carrier providing wireless service within eighteen months from the date of the mailing of the Council's Findings of Fact, Opinion, and Decision and Order (collectively called "Final Decision"), this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapply for any continued or new use to the Council before any such use is made. The time between the filing and resolution of any appeals of the Council's Final Decision shall not be counted in calculating this deadline. Authority to monitor and modify this schedule, as necessary, is delegated to the Executive Director. The Certificate Holder shall provide written notice to the Executive Director of any schedule changes as soon as is practicable.
7. Any request for extension of the time period referred to in Condition 6 shall be filed with the Council not later than 60 days prior to the expiration date of this Certificate and shall be served on all parties and intervenors, as listed in the service list, and the Town of Somers
8. If the facility ceases to provide wireless services for a period of one year, this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapply for any continued or new use to the Council within 90 days from the one year period of cessation of service. The Certificate Holder may submit a written request to the Council for an extension of the 90 day period not later than 60 days prior to the expiration of the 90 day period.
9. Any nonfunctioning antenna, and associated antenna mounting equipment, on this facility shall be removed within 60 days of the date the antenna ceased to function.
10. In accordance with Section 16-50j-77 of the Regulations of Connecticut State Agencies, the Certificate Holder shall provide the Council with written notice two weeks prior to the commencement of site construction activities. In addition, the Certificate Holder shall provide the Council with written notice of the completion of site construction, and the commencement of site operation.
11. The Certificate Holder shall remit timely payments associated with annual assessments and invoices submitted by the Council for expenses attributable to the facility under Conn. Gen. Stat. §16-50v.

12. This Certificate may be transferred in accordance with Conn. Gen. Stat. §16-50k(b), provided both the Certificate Holder/transferor and the transferee are current with payments to the Council for their respective annual assessments and invoices under Conn. Gen. Stat. §16-50v. In addition, both the Certificate Holder/transferor and the transferee shall provide the Council a written agreement as to the entity responsible for any quarterly assessment charges under Conn. Gen. Stat. §16-50v(b)(2) that may be associated with this facility.
13. The Certificate Holder shall maintain the facility and associated equipment, including but not limited to, the tower, tower foundation, antennas, equipment compound, radio equipment, access road, utility line and landscaping in a reasonable physical and operational condition that is consistent with this Decision and Order and a Development and Management Plan to be approved by the Council.
14. If the Certificate Holder is a wholly-owned subsidiary of a corporation or other entity and is sold/transferred to another corporation or other entity, the Council shall be notified of such sale and/or transfer and of any change in contact information for the individual or representative responsible for management and operations of the Certificate Holder within 30 days of the sale and/or transfer.
15. This Certificate may be surrendered by the Certificate Holder upon written notification and approval by the Council.

We hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed in the Service List, dated September 21, 2017, and notice of issuance published in the Journal Inquirer.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section 16-50j-17 of the Regulations of Connecticut State Agencies.

# Exhibit B

## Property Card



## 248 HALL HILL RD

**Location** 248 HALL HILL RD

**Mblu** 07/ 72/ 11

**Acct#** 00110000

**Owner** ROMANO JOHN A & DEBRA

**Assessment** \$401,090

**Appraisal** \$795,300

**PID** 3008

**Building Count** 1

**Dev Lot**

**Dev Map**

**Exempt Code**

### Current Value

Appraisal			
Valuation Year	Improvements	Land	Total
2020	\$210,200	\$585,100	\$795,300

Assessment			
Valuation Year	Improvements	Land	Total
2020	\$147,100	\$253,990	\$401,090

### Owner of Record

**Owner** ROMANO JOHN A & DEBRA  
**Co-Owner**  
**Address** 248 HALL HILL RD  
SOMERS, CT 06071

**Sale Price** \$0  
**Certificate**  
**Book & Page** 0340/0652  
**Sale Date** 02/08/2017

### Ownership History

Ownership History				
Owner	Sale Price	Certificate	Book & Page	Sale Date
ROMANO JOHN A & DEBRA	\$0		0340/0652	02/08/2017
ROMANO DEBRA	\$0	1	0330/0868	07/21/2015
TURBAK STANLEY J EST OF	\$0		0299/0007	02/15/2011
TURBAK STANLEY J	\$0		0286/0550	06/19/2009

### Building Information

## Building 1 : Section 1

**Year Built:** 1966  
**Living Area:** 1,778  
**Replacement Cost:** \$294,358  
**Building Percent Good:** 66  
**Replacement Cost Less Depreciation:** \$194,300

### Building Attributes

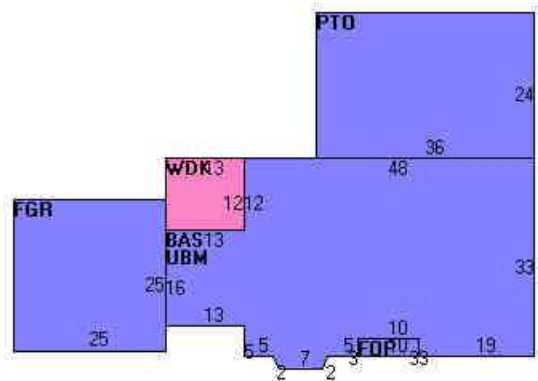
Field	Description
Style:	Ranch
Model	Residential
Grade:	C+
Stories:	1
Occupancy:	1
Exterior Wall 1:	Brick
Exterior Wall 2:	
Roof Structure:	Gable
Roof Cover:	Arch Shingles
Interior Wall 1:	Plywood Panel
Interior Wall 2:	
Interior Flr 1:	Hardwood
Interior Flr 2:	
Heat Fuel:	Oil
Heat Type:	Hot Water
AC Type:	Central
Total Bedrooms	2 Bedrooms
Total Full Baths	2
Total Half Baths	1
Total Xtra Fixtrs:	0
Total Rooms	7
Bath Style:	Average
Kitchen Style:	Average
Num Kitchens	2
Fireplace, Plain	2
Basement garage	0
Extra Kitchens	1
Fin Bsmt Area	700
Fin Bsmt Quality	Avg Qual.
Num Park	
Fireplaces	0
Whirlpool Tub	

### Building Photo



([https://images.vgsi.com/photos/SomersCTPhotos///0009/DSCF2847\\_9082](https://images.vgsi.com/photos/SomersCTPhotos///0009/DSCF2847_9082))

### Building Layout



Building Sub-Areas (sq ft)			<u>Legend</u>
Code	Description	Gross Area	Living Area
BAS	First Floor	1,778	1,778
FGR	Garage	625	0
FOP	Open Porch	30	0
PTO	Patio	864	0
UBM	Basement	1,778	0
WDK	Wood Deck	156	0
		5,231	1,778

Foundation	Poured Conc.
Fndtn Cndtn	
Basement	

### Extra Features

Extra Features	<u>Legend</u>
No Data for Extra Features	

### Land

#### Land Use

<b>Use Code</b>	101
<b>Description</b>	Single Family
<b>Zone</b>	A-1
<b>Neighborhood</b>	08
<b>Alt Land Appr Category</b>	No

#### Land Line Valuation

<b>Size (Acres)</b>	38.50
<b>Frontage</b>	1100
<b>Depth</b>	
<b>Assessed Value</b>	\$253,990
<b>Appraised Value</b>	\$585,100

### Outbuildings

Outbuildings						<u>Legend</u>
Code	Description	Sub Code	Sub Description	Size	Value	Bldg #
BRN3	Barn w Loft	FR	Frame	1656.00 SF	\$15,900	1

### Valuation History

Appraisal			
Valuation Year	Improvements	Land	Total
2022	\$210,200	\$585,100	\$795,300
2020	\$210,200	\$585,100	\$795,300
2019	\$177,100	\$619,400	\$796,500

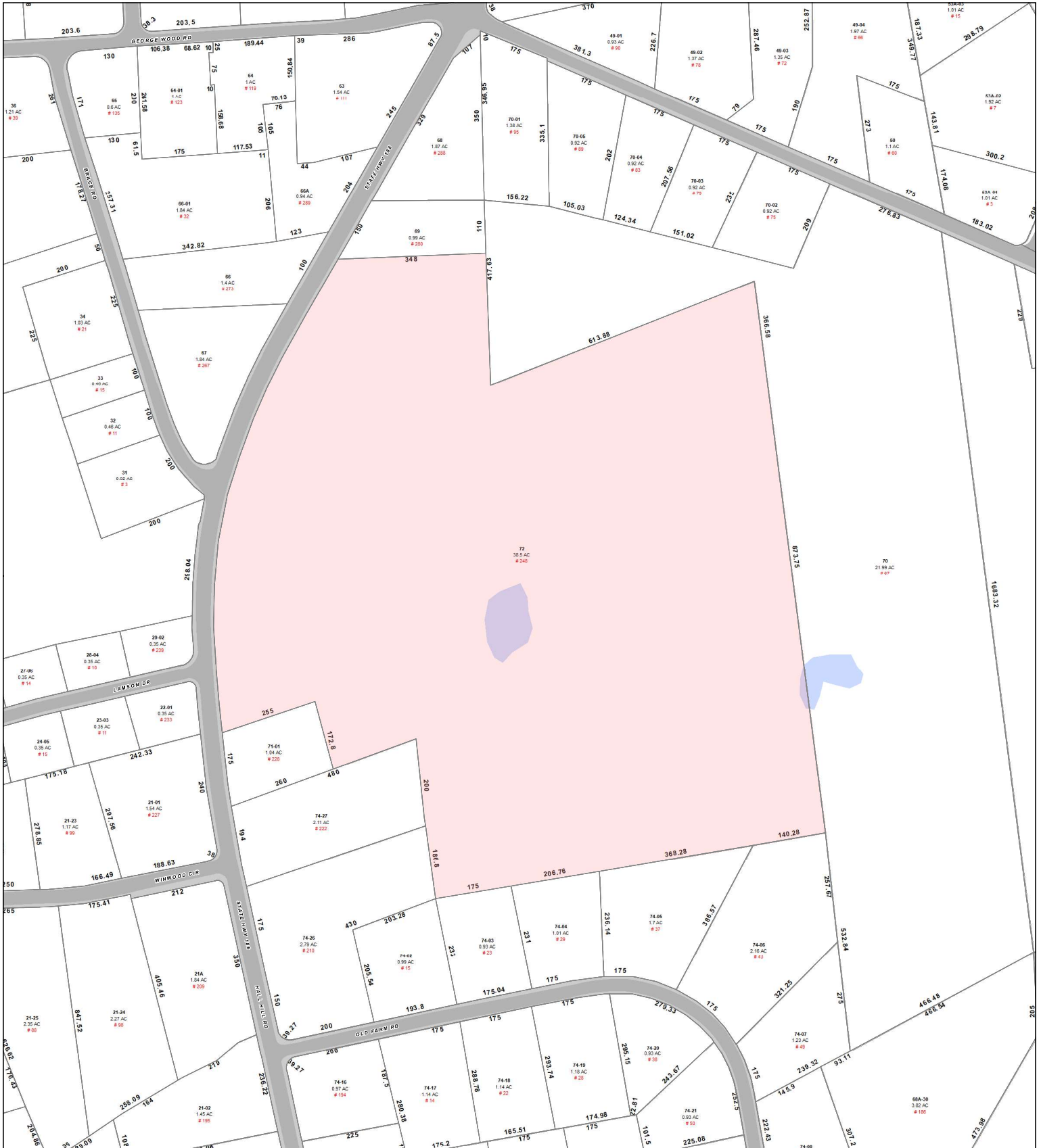
Assessment			
Valuation Year	Improvements	Land	Total
2022	\$147,100	\$253,990	\$401,090
2020	\$147,100	\$253,990	\$401,090
2019	\$123,900	\$252,760	\$376,660

# Town of Somers, Connecticut - Assessment Parcel Map



Parcel: 07-72

Address: 248 HALL HILL RD



Approximate Scale: 1 inch = 300 feet

Disclaimer: This map is for informational purposes only. All information is subject to verification by any user. The Town of Somers and its mapping contractors assume no legal responsibility for the information contained herein.

Map Produced June 2023

# Exhibit C

## **Construction Drawings**





# T-MOBILE NORTHEAST LLC ANCHOR

**SITE #: CTHA027B**  
**SITE NAME: ROMANO**  
**248 HALL HILL ROAD**  
**SOMERS, CT 06071**  
**TOLLAND COUNTY**

**CONSTRUCTION DRAWINGS**  
 ALL SCALES RELATIVE TO 24"x36" PAGE SIZE



Documents prepared by Elevated Engineering, including this document, are to be used only for the specific project and specific use for which they were intended. Any extension of use to any other projects, by owner or by any other party, without the expressed written consent of Elevated Engineering, is done unlawfully and at the users own risk. If used in a way other than that specifically intended, user will hold Elevated Engineering, harmless from all claims and losses.

Approved - Dave Deraleau  
 9:52 AM, Apr 4, 2024

APPROVED  
 By Ryan Monte de Ramos at 8:24 am, Apr 11, 2024

APPROVED  
 By Mike DeLia at 9:31 am, Apr 11, 2024

**RAN CONFIGURATION: 67E5D998E 6160**

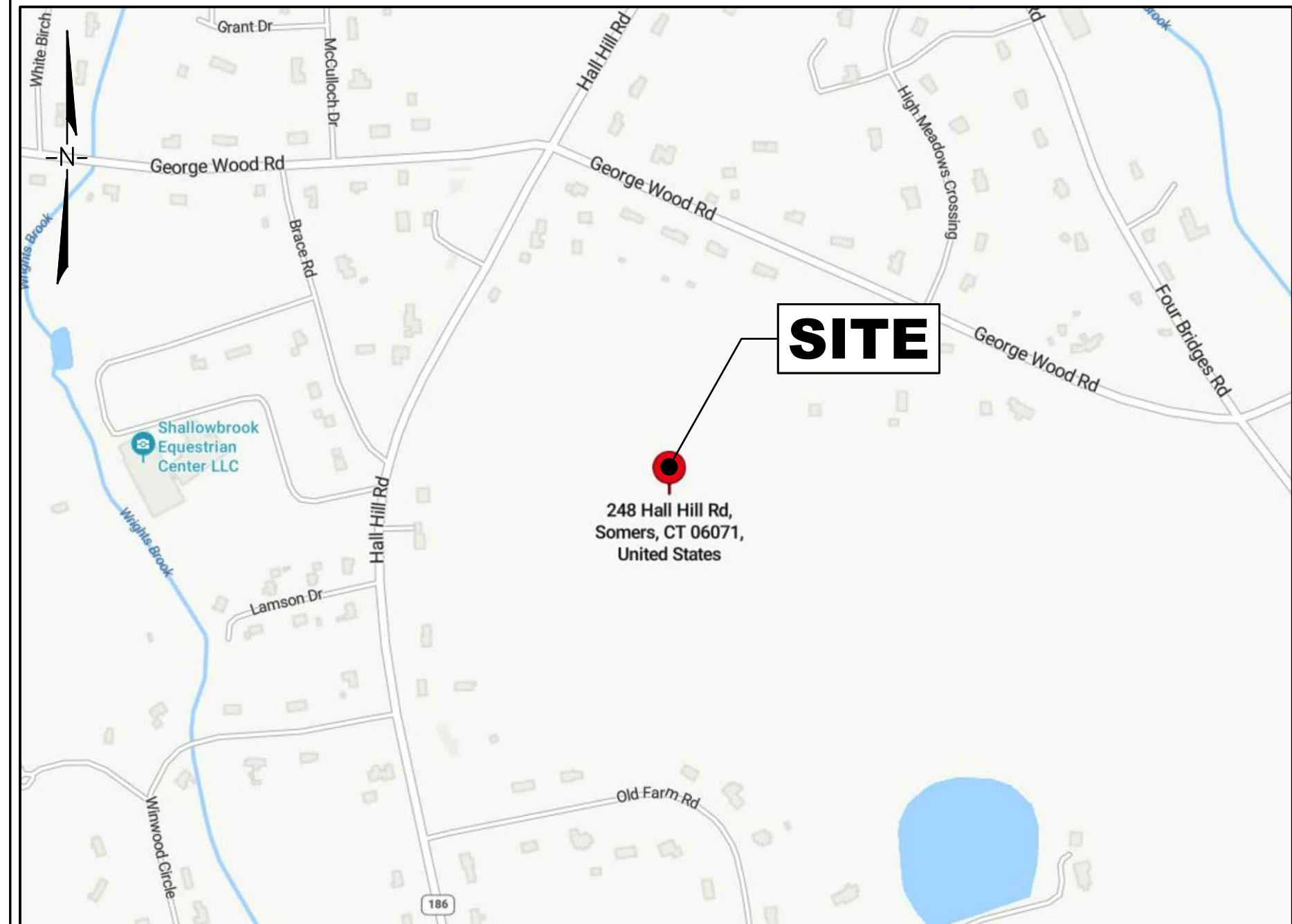
**A&L CONFIGURATION: 67E5998E\_1xAIR+1QP+1OP**

**GENERAL NOTES**

THIS DOCUMENT IS THE CREATION, DESIGN, PROPERTY, AND COPYRIGHTED WORK OF T-MOBILE. ANY DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. DUPLICATION AND USE BY GOVERNMENT AGENCIES FOR THE PURPOSES OF CONDUCTING THEIR LAWFULLY AUTHORIZED REGULATORY AND ADMINISTRATIVE FUNCTIONS IS SPECIFICALLY ALLOWED.

THE FACILITY IS AN UNMANNED, PRIVATE, AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND, THEREFORE, DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.

CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE T-MOBILE NORTHEAST, LLC REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.



**KEY MAP**  
 SCALE = N.T.S.

**SITE LOCATION INFORMATION**

SITE NUMBER: CTHA027B  
 SITE ADDRESS: 248 HALL HILL ROAD, SOMERS, CT 06071  
 JURISDICTION: TOWN OF SOMERS  
 COUNTY: TOLLAND COUNTY  
 PARCEL ID: 07-72  
 PROPERTY OWNER: DEBRA ROMANO, 248 HALL HILL ROAD, SOMERS, CT 07071  
 APPLICANT: T-MOBILE NORTHEAST LLC, 35 GRIFFIN ROAD SOUTH, BLOOMFIELD, CT 06002

**SITE CHARACTERISTICS**

LATITUDE: N 42° 00' 09.34"  
 LONGITUDE: W 72° 29' 05.99"  
 STRUCTURE TYPE: MONOPOLE  
 LOCATION OF EQUIPMENT: EXISTING CONCRETE PAD AT GRADE  
 STRUCTURE HEIGHT: ±180'-0" AGL  
 ANTENNA (RAD CENTER): ALPHA - ±175'-0" AGL, BETA - ±175'-0" AGL, GAMMA - ±175'-0" AGL

**SPECIAL STRUCTURAL NOTES**

STRUCTURE OWNER SHALL BE RESPONSIBLE FOR GLOBAL STRUCTURAL STABILITY ANALYSIS OF EXISTING SUPPORT STRUCTURE. GENERAL CONTRACTOR SCOPE OF WORK SHALL INCLUDE ALL REQUIRED STRUCTURAL MODIFICATIONS, RE-BUNDLING OF COAXIAL CABLES OR OTHER SPECIAL MODIFICATIONS AS OUTLINED THEREIN.

STRUCTURAL DESIGNS AND DETAILS FOR ANTENNA MOUNTS COMPLETED BY ELEVATED ENGINEERING, PLLC ON BEHALF OF T-MOBILE ARE INCLUSIVE OF THE ENTIRE ANTENNA SUPPORT STRUCTURE (GLOBAL STRUCTURAL STABILITY ANALYSIS BY OTHERS), EXISTING PLATFORM, EXISTING ANTENNA MOUNTS, AND ALL OTHER ASPECTS OF THE STRUCTURE THAT WILL SUPPORT THE T-MOBILE EQUIPMENT DEPLOYMENT AS DEPICTED HEREIN.

ELEVATED ENGINEERING, PLLC ASSUMES THAT THE STRUCTURE IS PROPERLY CONSTRUCTED AND MAINTAINED. ALL STRUCTURAL MEMBERS AND THEIR CONNECTIONS ARE ASSUMED TO BE IN GOOD CONDITION AND ARE FREE FROM DEFECTS WITH NOT DETERIORATION TO IT'S MEMBER CAPACITIES.

**UNDERGROUND SERVICE ALERT**

**SHEET INDEX**

SHEET NO.	SHEET DESCRIPTION
T-1	TITLE SHEET
GN-1	GENERAL NOTES
A-1	COMPOUND PLAN & ELEVATION
A-2	EQUIPMENT PLANS & ANTENNA PLANS
A-3	DETAILS
E-1	GROUNDING DETAILS & NOTES

**APPROVALS**

PROJECT MANAGER	DATE
CONSTRUCTION	DATE
RF ENGINEERING	DATE
ZONING / SITE ACQUISITION	DATE
OPERATIONS	DATE
OWNER	DATE

**SCHEDULE OF REVISIONS**

REV. NO.	DATE	DESCRIPTION OF CHANGES
7		
6		
5		
4		
3		
2		
1	04/02/24	REVISED PER CLIENT COMMENTS
0	03/05/24	INITIAL SUBMISSION

**DRAWN BY:** CJT  
**CHECKED BY:** NDB  
**SCALE:** AS NOTED  
**JOB NO:** 24008-NSS

INFORMATION ON THIS SET OF DRAWINGS IS NOT FOR OFFICIAL USE UNLESS ACCOMPANIED BY THE STAMPED SEAL & SIGNATURE OF A PROFESSIONAL ENGINEER

**NICHOLAS D. BARILE**  
 PROFESSIONAL ENGINEER, CT LIC. No. 28643

**SITE ID: CTHA027B**  
**SITE NAME: ROMANO**  
**248 HALL HILL ROAD**  
**SOMERS, CT 06071**  
**TOLLAND COUNTY**

**DRAWING TITLE:**

**TITLE SHEET**

**DRAWING SHEET:**

**T-1**



## GENERAL NOTES

- FOR THE PURPOSE OF THE CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:  
CONTRACTORS – TO BE DETERMINED  
SUBCONTRACTOR – GENERAL CONTRACTOR (CONSTRUCTION)  
OWNER – T-MOBILE
- PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF THE CONTRACTOR.
- ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
- DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
- UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
- "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE PROVIDED BY THE SUBCONTRACTOR.
- THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURERS RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSED AND ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY CONTRACTOR.
- SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
- THE SUBCONTRACTOR SHALL PROTECT THE EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTORS EXPENSE TO THE SATISFACTION OF OWNER.
- SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIAL SUCH AS COAXIAL CABLE AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNERS DESIGNATED LOCATION.
- SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
- ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.
- ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.
- ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCH UP ALL SCRATCHED AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
- CONSTRUCTION SHALL COMPLY WITH UMS SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF T-MOBILE SITES."
- SUBCONTRACTORS SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.

- THE EXISTING CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.

### 19. APPLICABLE BUILDING CODES:

SUBCONTRACTORS WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.

- BUILDING CODE: 2022 CONNECTICUT STATE BUILDING CODE
- ELECTRICAL CODE: NFPA 70 NATIONAL ELECTRICAL CODE, 2017 EDITION
- LIGHTNING CODE: NFPA 780-2014 LIGHTNING PROTECTION CODE

SUBCONTRACTORS WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:

- AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENT FOR STRUCTURAL CONCRETE
- AMERICAN INSTITUTE FOR STEEL CONSTRUCTION (AISC)
- MANUAL OF STEEL CONSTRUCTION, ASD, NINTH EDITION
- TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-H, STRUCTURAL STANDARDS FOR STEEL
- ANTENNA TOWER AND ANTENNA SUPPORTING STRUCTURES; REFER TO ELECTRICAL DRAWINGS FOR SPECIFIC ELECTRICAL STANDARDS.

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS A CONFLICT BETWEEN A GENERAL REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

## ELECTRICAL & GROUNDING NOTES

- THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE SPECIFIC (UL, LPI, OR NFPA) LIGHTNING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
- ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO LIGHTNING PROTECTION AND AS POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
- THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
- METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO THE BTS EQUIPMENT.
- EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
- EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
- APPROVED ANTIOXIDANT COATING (I.E. CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
- ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR.
- ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
- MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
- METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWS COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
- ALL NEW STRUCTURE WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50.
- ALL ELECTRICAL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE NATIONAL ELECTRICAL CODE (NEC) AS WELL AS APPLICABLE STATE AND LOCAL CODES.
- ALL ELECTRICAL ITEMS SHALL BE U.L. APPROVED OR LISTED AND PROCURED PER SPECIFICATION REQUIREMENTS.
- THE ELECTRICAL WORK INCLUDES ALL LABOR AND MATERIAL DESCRIBED BY DRAWINGS AND SPECIFICATIONS INCLUDING INCIDENTAL WORK TO PROVIDE COMPLETE OPERATING AND APPROVED ELECTRICAL SYSTEM.
- GENERAL CONTRACTOR SHALL PAY FEES FOR PERMITS, AND IS RESPONSIBLE FOR OBTAINING SAID PERMITS AND COORDINATION OF INSPECTIONS.
- ELECTRICAL AND TELCO WIRING OUTSIDE A BUILDING AND EXPOSED TO WEATHER SHALL BE IN WATER TIGHT GALVANIZED RIGID STEEL CONDUITS OR SCHEDULE 80 PVC (AS PERMITTED BY CODE) AND WHERE REQUIRED IN LIQUID TIGHT FLEXIBLE METAL OR NONMETALLIC CONDUITS.
- RIGID STEEL CONDUITS SHALL BE GROUNDED AT BOTH ENDS.
- ELECTRICAL WIRING SHALL BE COPPER WITH TYPE XHHW, THWN OR THIN INSULATION.
- RUN ELECTRICAL CONDUIT OR CABLE BETWEEN ELECTRICAL ROOM AND PROPOSED CELL SITE POWER PEDESTAL AS INDICATED ON THIS DRAWING. PROVIDE FULL LENGTH PULL ROPE. COORDINATE INSTALLATION WITH UTILITY COMPANY.
- RUN TELCO CONDUIT OR CABLE BETWEEN TELEPHONE UTILITY DEMARCATION POINT AND PROPOSED CELL SITE TELCO CABINET AND BTS CABINET AS INDICATED ON DRAWING A-1. PROVIDE FULL LENGTH PULL ROPE IN INSTALLED TELCO CONDUIT. PROVIDE GREENLEE CONDUIT MEASURING TAPE AT EACH END.
- ALL EQUIPMENT LOCATED OUTSIDE SHALL HAVE NEMA 3R ENCLOSURE.
- GROUNDING SHALL COMPLY WITH NEW ART. 250.
- GROUND COAXIAL CABLE SHIELDS MINIMUM AT BOTH ENDS USING MANUFACTURERS COAX CABLE GROUNDING KITS SUPPLIED BY PROJECT OWNER.
- USE #6 COPPER STRANDED WIRE WITH GREEN COLOR INSULATION FOR ABOVE GRADE GROUNDING (UNLESS OTHERWISE SPECIFIED) AND #2 SOLID TINNED BARE COPPER WIRE FOR BELOW GRADE GROUNDING AS INDICATED ON DRAWING.
- ALL GROUND CONNECTIONS TO BE BURNDY HYGROUND COMPRESSION TYPE CONNECTORS OR CADWELD EXOTHERMIC WELD. DO NOT ALLOW BARE COPPER WIRE TO BE IN CONTACT WITH GALVANIZED STEEL.
- ROUTE GROUNDING CONDUCTORS ALONG THE SHORTEST AND STRAIGHTEST PATH POSSIBLE EXCEPT AS OTHERWISE INDICATED. GROUNDING LEADS SHOULD NEVER BE BENT AT RIGHT ANGLE. ALWAYS MAKE AT LEAST 12" RADIUS BENDS. #6 WIRE CAN BE BENT AT 6" RADIUS WHEN NECESSARY. BOND ANY METAL OBJECTS WITHIN 7 FEET OF PROPOSED EQUIPMENT OR CABINET TO MASTER GROUND BAR.
- CONNECTIONS TO MGB SHALL BE ARRANGED IN THREE MAIN GROUPS: SURGE PRODUCERS (COAXIAL CABLE GROUND KITS, TELCO AND POWER PANEL GROUND); (GROUNDING ELECTRODE RING OR BUILDING STEEL); NON-SURGING OBJECTS (EGB GROUND IN BTS UNIT)
- CONNECTIONS TO GROUND BARS SHALL BE MADE WITH TWO HOLE COMPRESSION TYPE COPPER LUGS. APPLY OXIDE INHIBITING COMPOUND TO ALL LOCATIONS.
- BOND ANTENNA MOUNTING BRACKETS. COAXIAL CABLE GROUND KITS AND ALNA TO EGB PLACES NEAR THE ANTENNA LOCATION.
- BOND ANTENNA EGB'S AND MGB TO WATER MAIN.
- TEST COMPLETED GROUND SYSTEM AND RECORD RESULTS FOR PROJECT CLOSE-OUT DOCUMENTATION.
- BOND ANY METAL OBJECTS WITHIN 7 FEET OF PROPOSED EQUIPMENT OR CABINET TO MASTER GROUND BAR.
- VERIFY PROPOSED SERVICE UPGRADE WITH LOCAL UTILITY COMPANY PRIOR TO CONSTRUCTION.

## ABBREVIATIONS

AGL	ABOVE GRADE LEVEL	G.C.	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
AWG	AMERICAN WIRE GAUGE	MGB	MASTER GROUND BUS		
BCW	BARE COPPER WIRE	MIN	MINIMUM	TBD	TO BE DETERMINED
BTS	BASE TRANSCEIVER STATION	PROPOSED	NEW	TBR	TO BE REMOVED
EXISTING	EXISTING	N.T.S.	NOT TO SCALE	TBRR	TO BE REMOVED AND REPLACED
EG	EQUIPMENT GROUND	REF	REFERENCE	TYP	TYPICAL
EGR	EQUIPMENT GROUND RING	REQ	REQUIRED		

**T-Mobile**  
T-MOBILE NORTHEAST LLC

35 GRIFFIN ROAD SOUTH  
BLOOMFIELD, CT 06002

**ELEVATED**  
ENGINEERING

99 FANNY ROAD  
BOONTON, NJ 07005  
862-242-8050

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### SCHEDULE OF REVISIONS

7		
6		
5		
4		
3		
2		
1	04/02/24	REVISED PER CLIENT COMMENTS
0	03/05/24	INITIAL SUBMISSION

REV. NO.	DATE	DESCRIPTION OF CHANGES
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**DRAWN BY:** CJT

**CHECKED BY:** NDB

**SCALE:** AS NOTED

**JOB NO:** 24008-NSS

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**NICHOLAS D. BARILE**  
PROFESSIONAL ENGINEER, CT LIC. No. 28643

**SITE ID: CTHA027B**  
**SITE NAME: ROMANO**  
**248 HALL HILL ROAD**  
**SOMERS, CT 06071**  
**TOLLAND COUNTY**

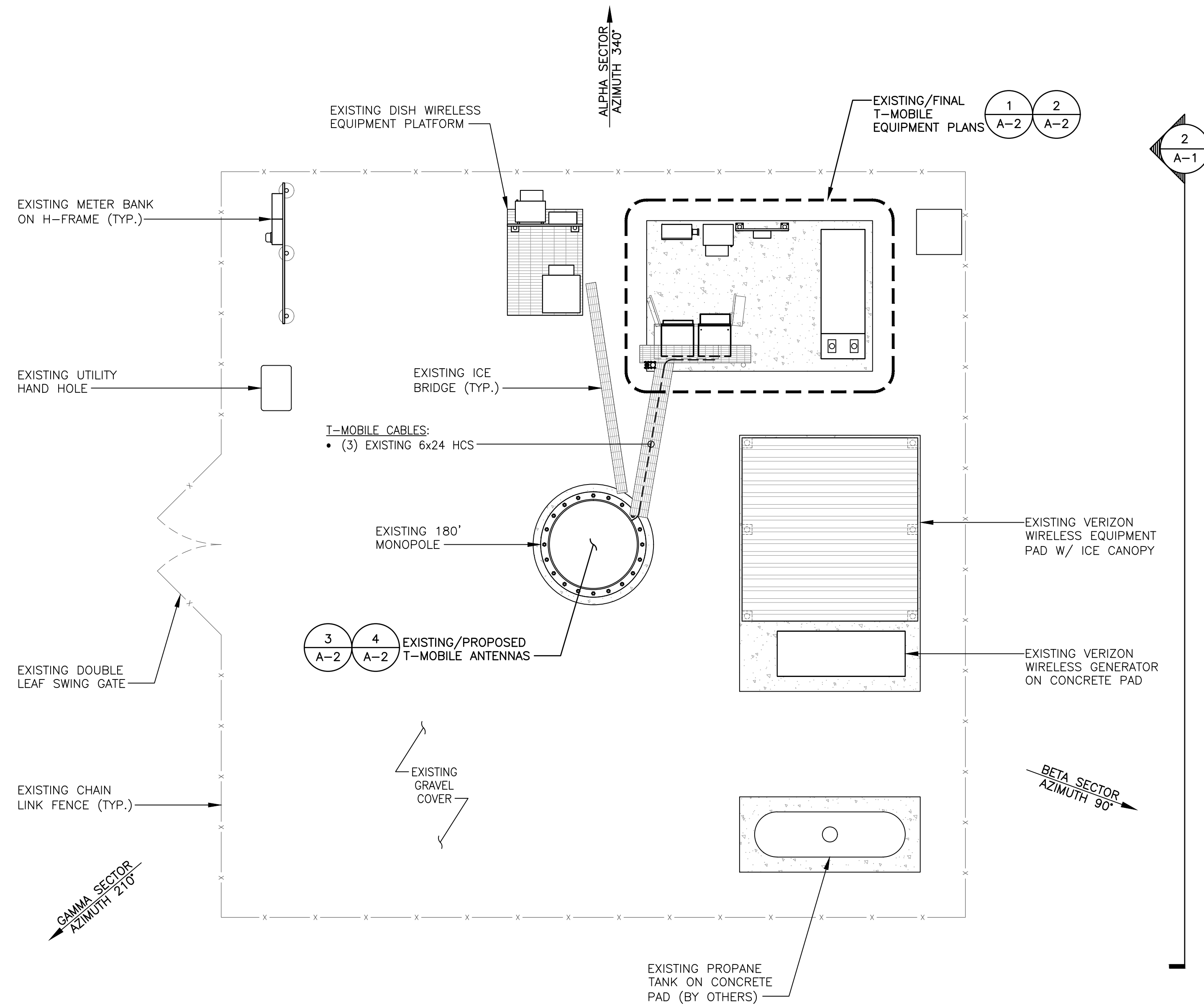
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**GENERAL NOTES**

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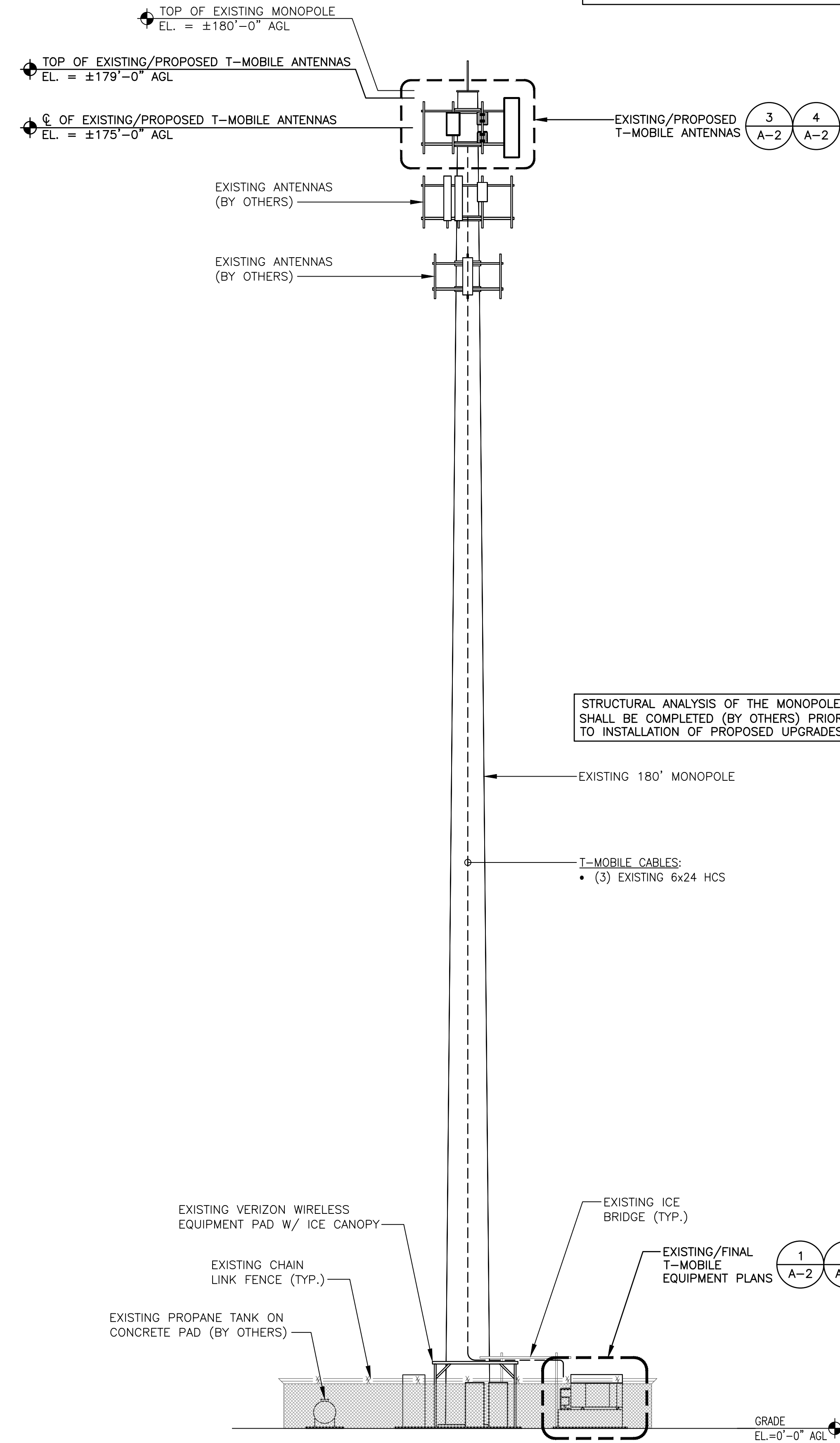
**GN-1**





1  
A-1  
COMPOUND PLAN  
SCALE: 3/16"=1'-0"

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2  
A-1  
ELEVATION  
SCALE: 3/32"=1'-0"



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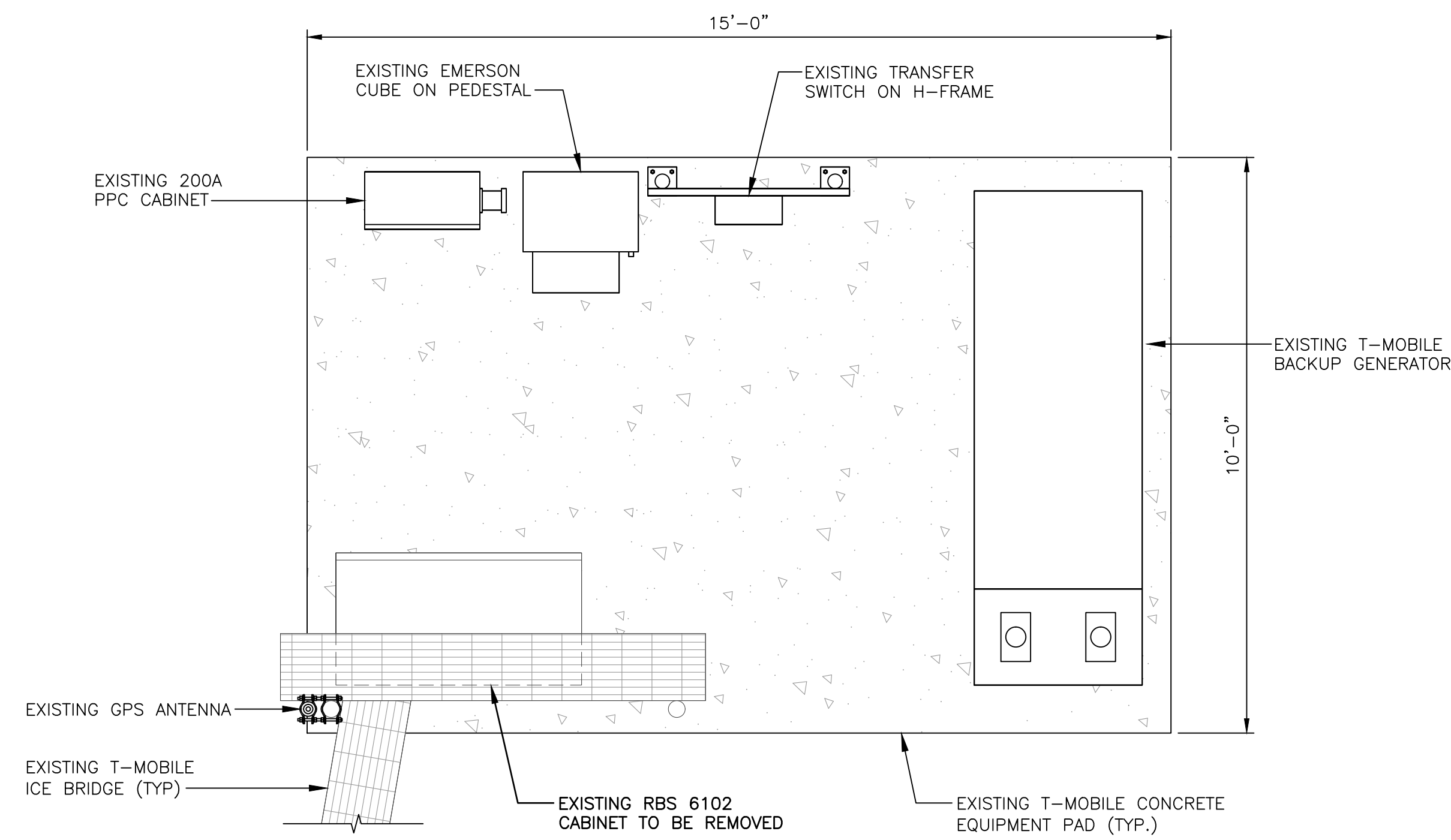
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COMPOUND PLAN & ELEVATION

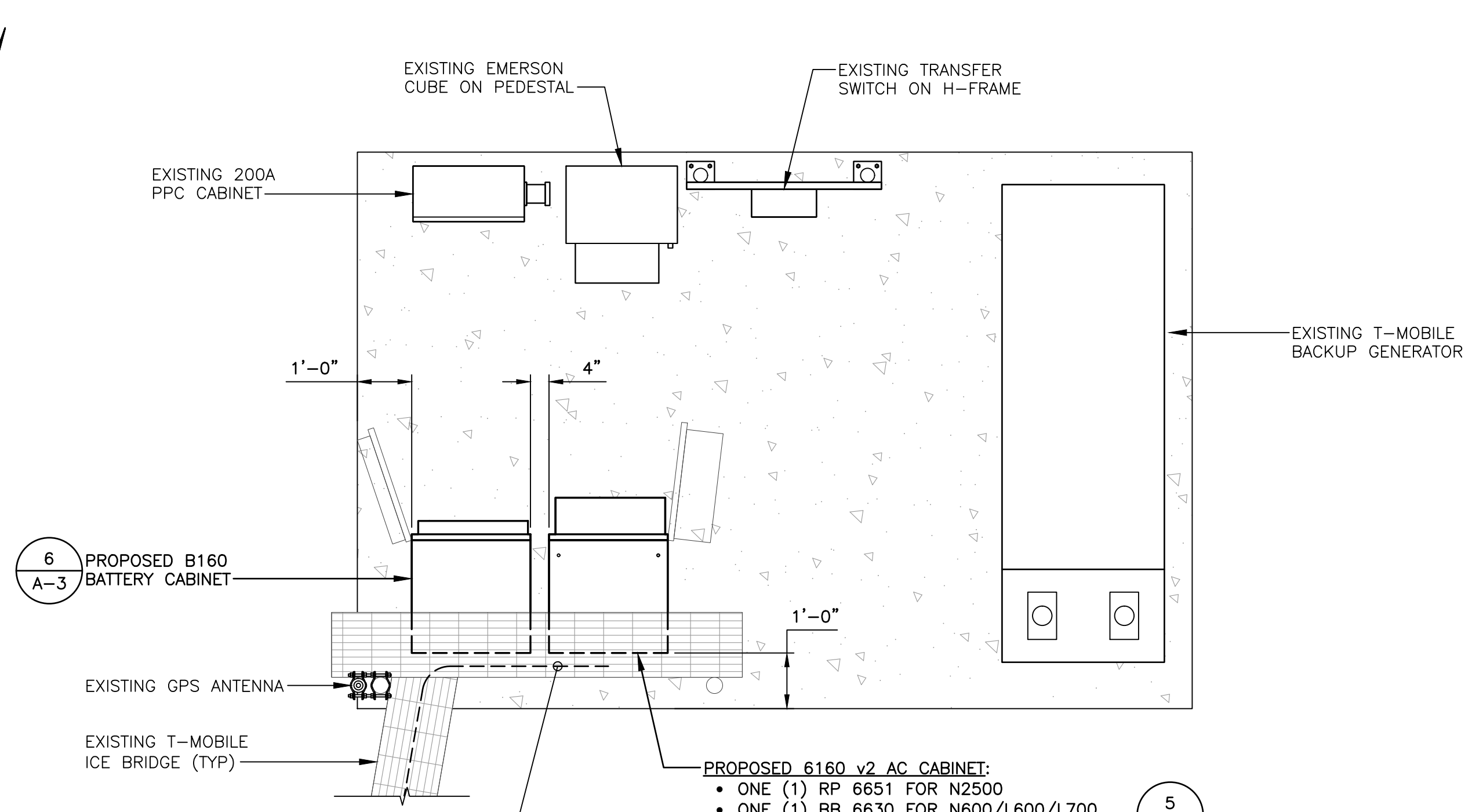
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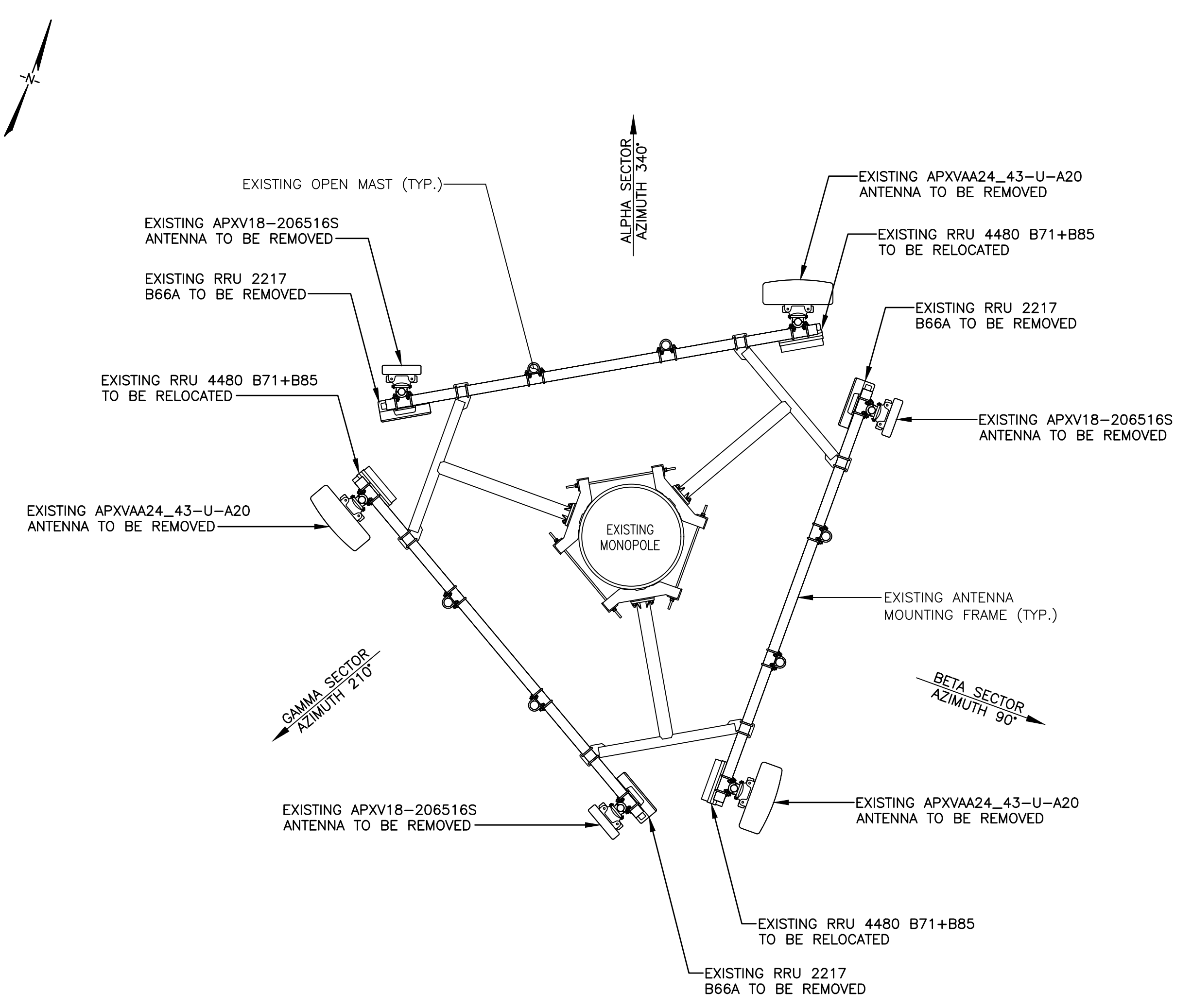




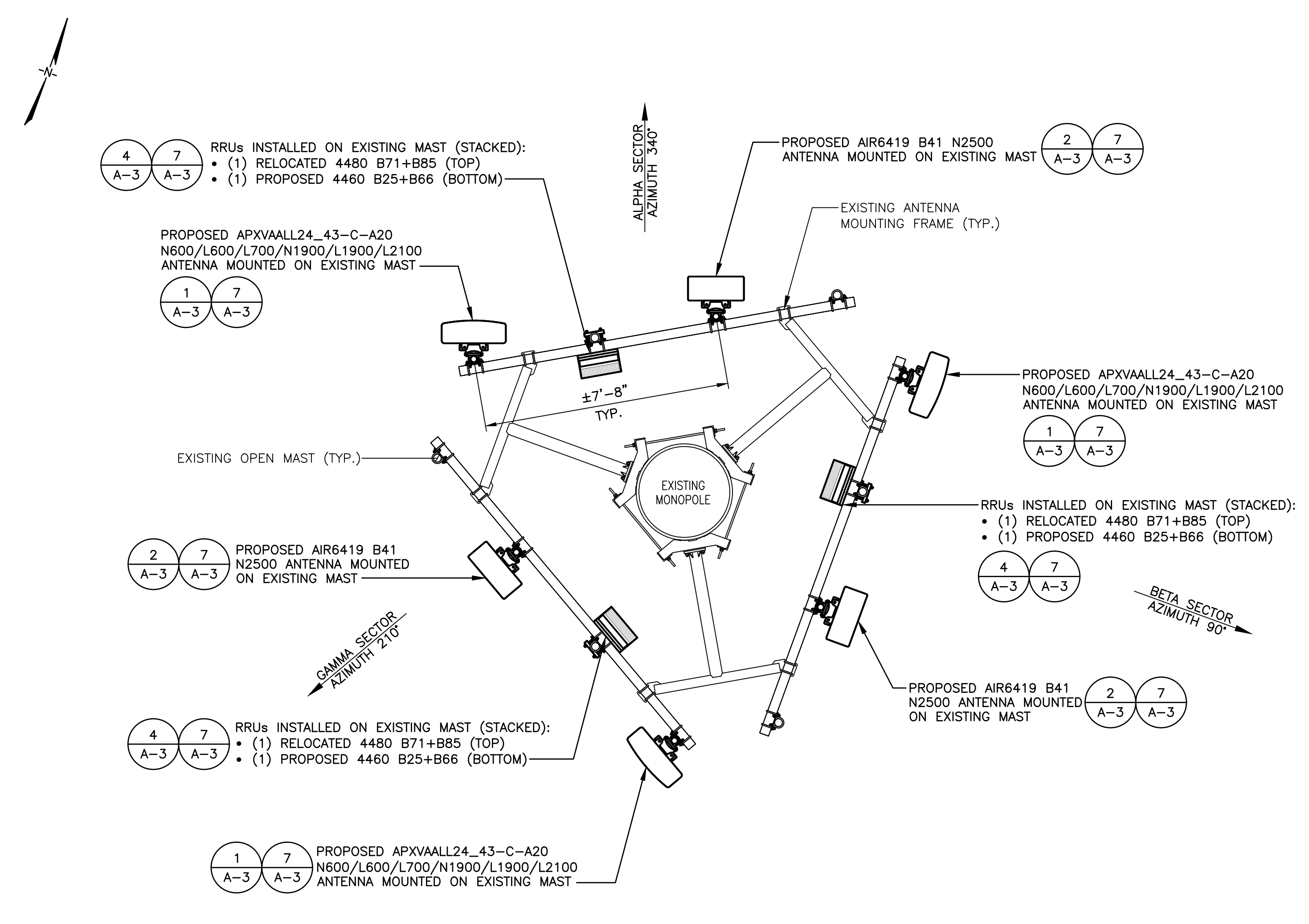
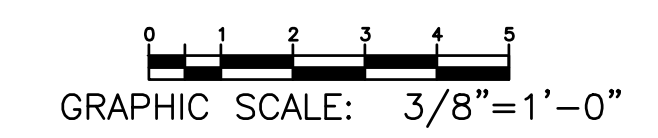
1 EXISTING EQUIPMENT PLAN  
A-2 SCALE: 1/2"=1'-0"



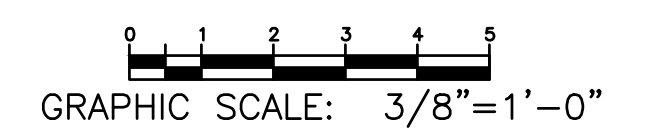
2 FINAL EQUIPMENT PLAN  
A-2 SCALE: 1/2"=1'-0"



3 TRUE NORTH EXISTING ANTENNA PLAN  
A-2 SCALE: 3/8"=1'-0"



4 TRUE NORTH PROPOSED ANTENNA PLAN  
A-2 SCALE: 3/8"=1'-0"



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T-MOBILE NORTHEAST LLC  
35 GRIFFIN ROAD SOUTH  
BLOOMFIELD, CT 06002

**ELEVATED ENGINEERING**  
99 FANNY ROAD  
BOONTON, NJ 07005  
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**SCALE:** AS NOTED  
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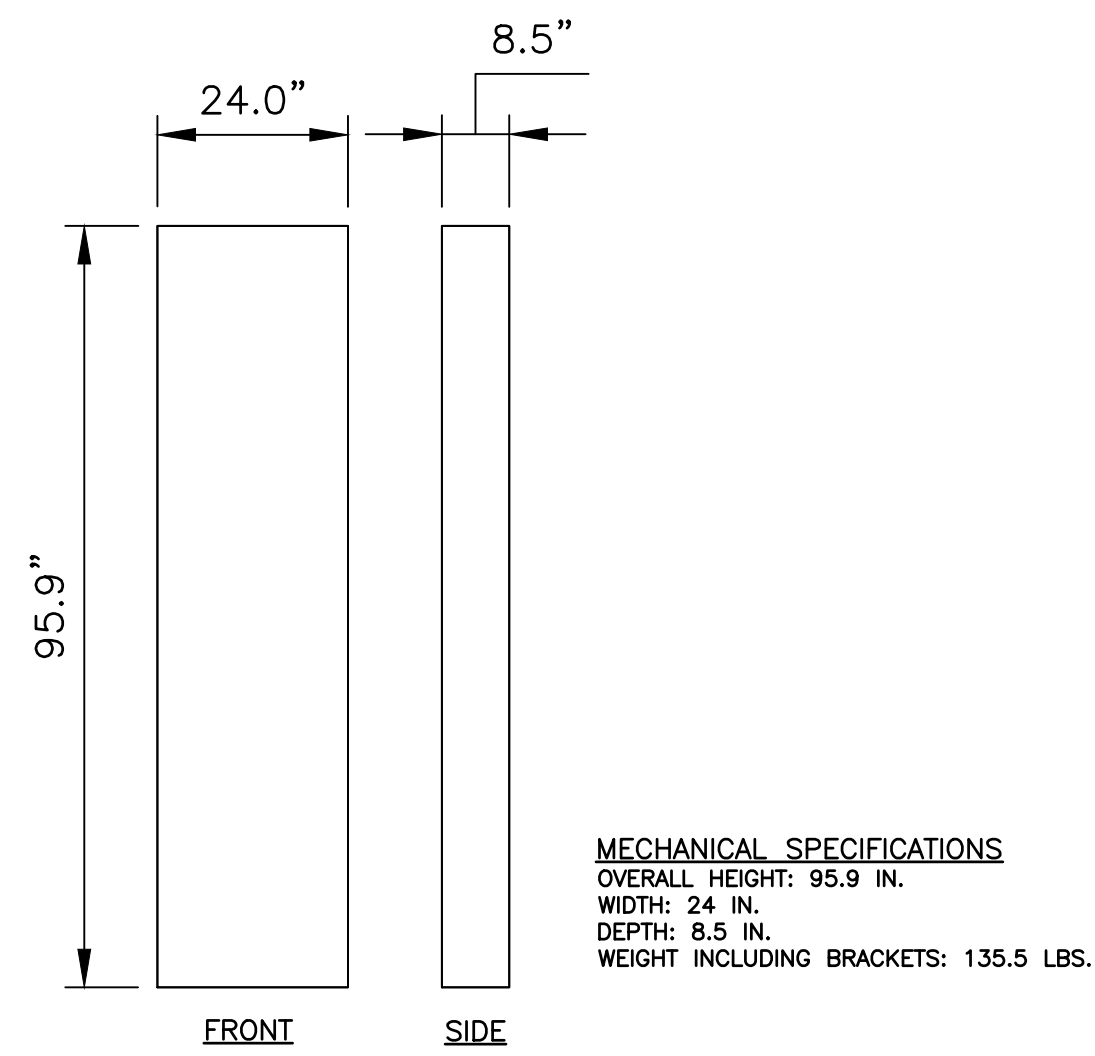
**NICHOLAS D. BARILE**  
PROFESSIONAL ENGINEER, CT LIC. No. 28643

**SITE ID: CTHA027B**  
**SITE NAME: ROMANO**  
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**SOMERS, CT 06071**  
**TOLLAND COUNTY**

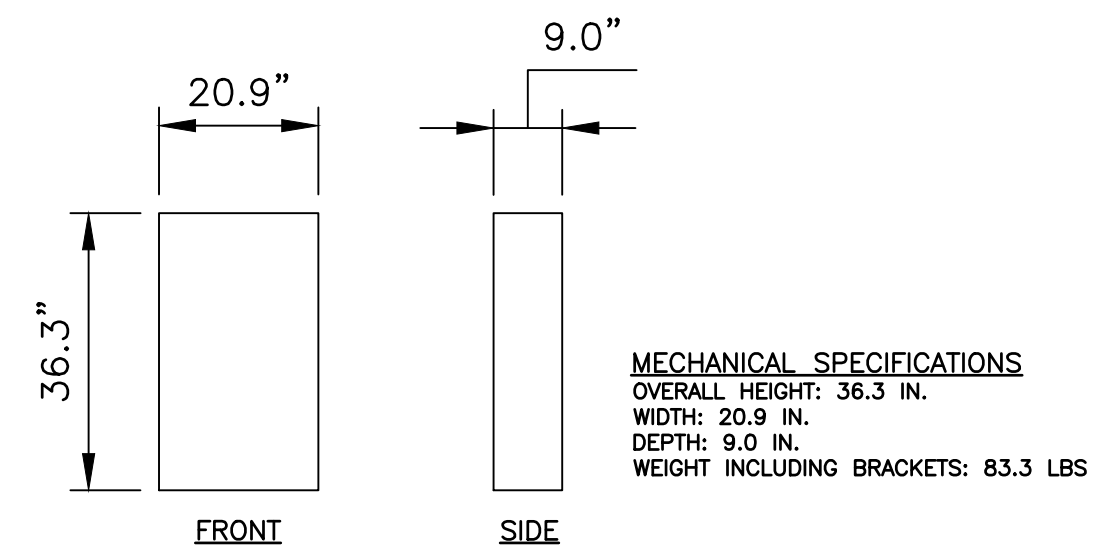
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**EQUIPMENT PLANS & ANTENNA PLANS**

**DRAWING SHEET:**  
**A-2**



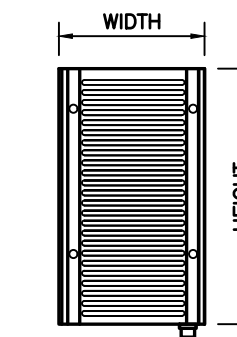


1 RFS: APXVAALL24\_43-C-A20  
 A-3 SCALE: N.T.S.



2 ERICSSON: AIR6419 B41  
 A-3 SCALE: N.T.S.

3 DETAIL NOT USED  
 A-3 SCALE: N.T.S.



RRH	HEIGHT	WIDTH	DEPTH	WEIGHT
RADIO 4460 B25+B66	17.0"	15.1"	11.9"	104 LBS.

4 RRU DETAILS  
 A-3 SCALE: N.T.S.

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 T-MOBILE NORTHEAST LLC  
 35 GRIFFIN ROAD SOUTH  
 BLOOMFIELD, CT 06002

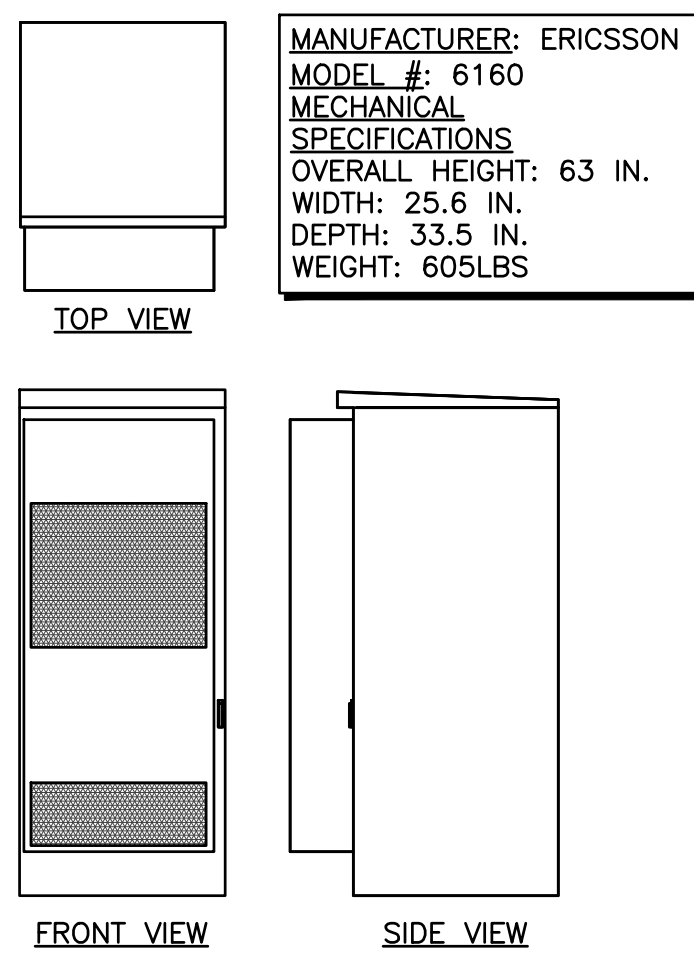
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 862-242-8050

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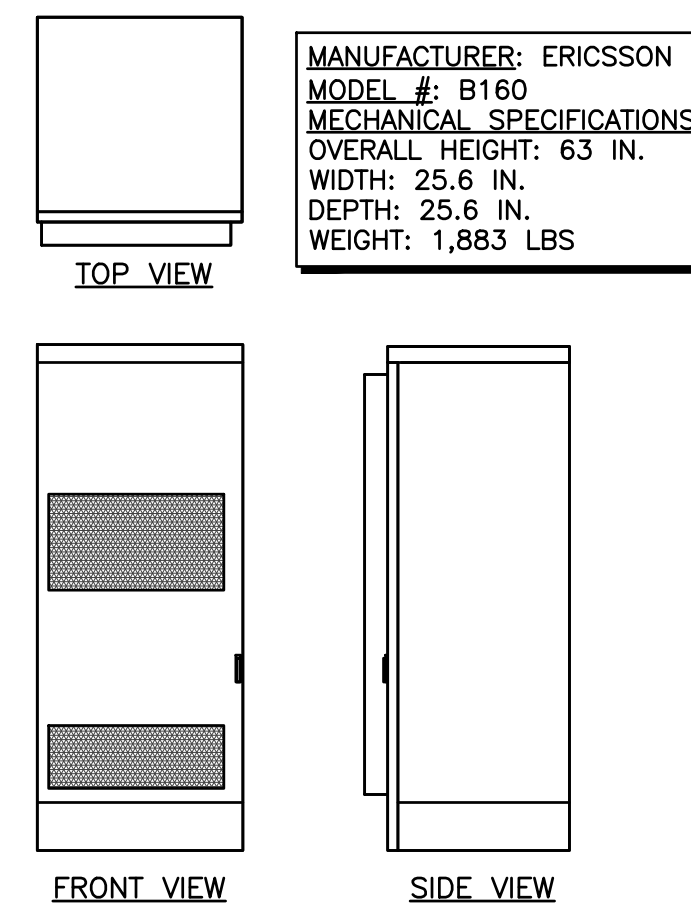
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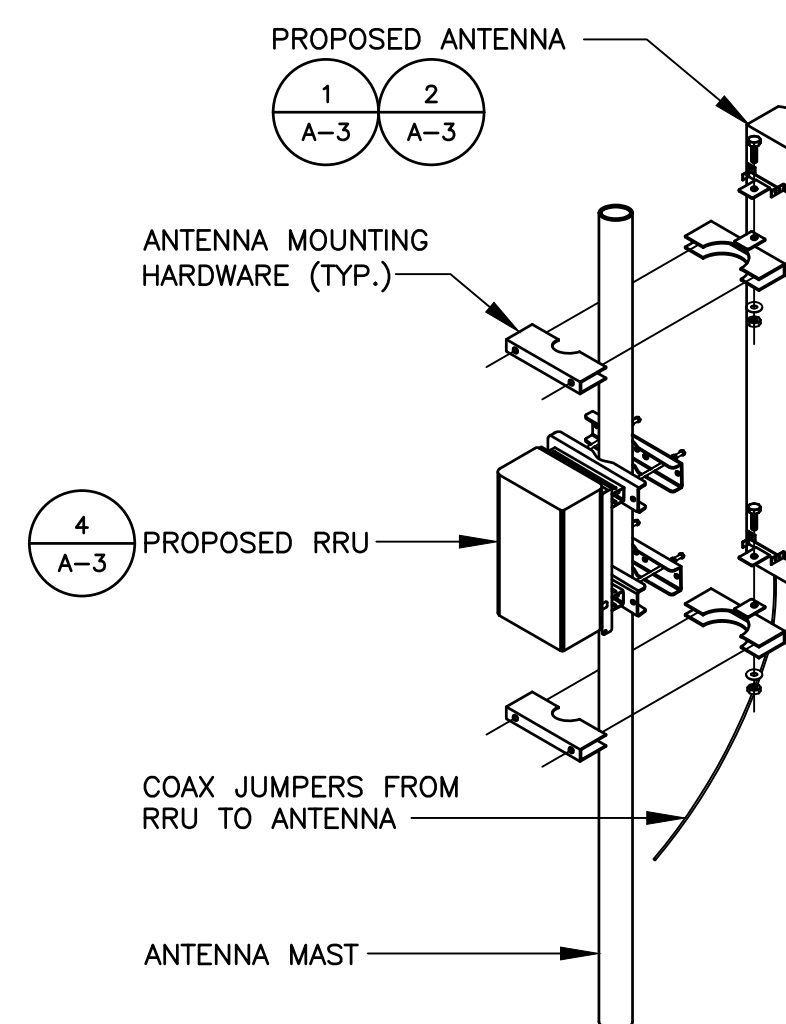
**DRAWN BY:** CJT  
**CHECKED BY:** NDB  
**SCALE:** AS NOTED  
**JOB NO:** 24008-NSS



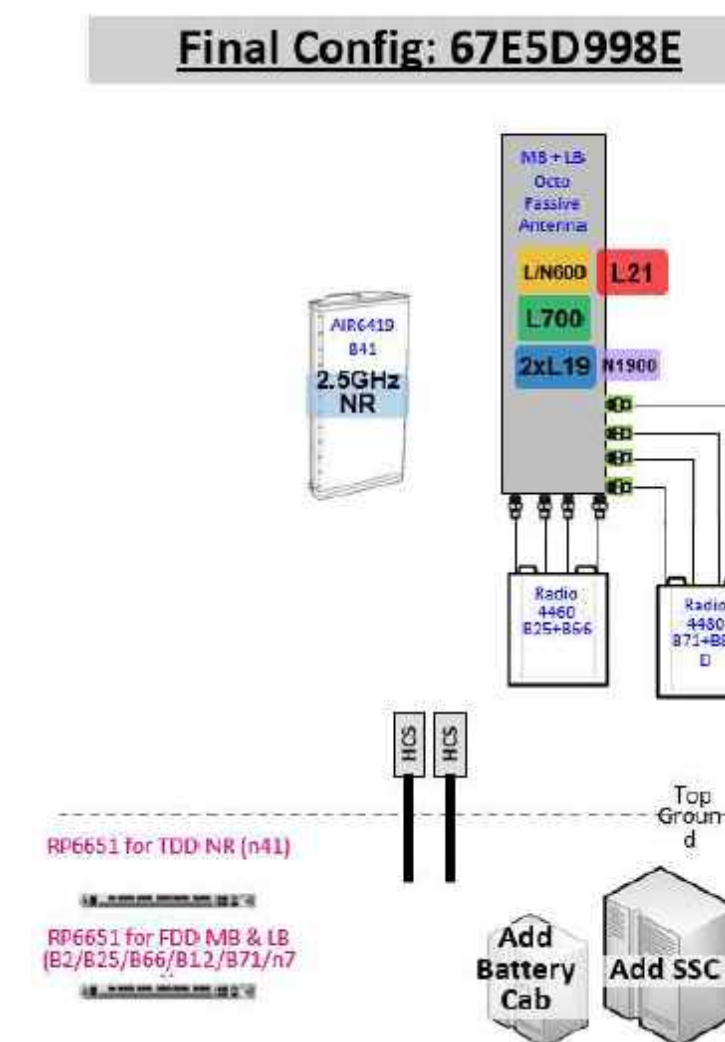
5 ERICSSON: 6160 CABINET  
 A-3 SCALE: N.T.S.



6 ERICSSON: B160 CABINET  
 A-3 SCALE: N.T.S.



7 TYPICAL ANTENNA INSTALLATION DETAIL  
 A-3 SCALE: N.T.S.



8 ANTENNA & COAX CABLE SCHEMATIC  
 A-3 SCALE: N.T.S.

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*Nicholas D. Barile*  
 NICHOLAS D. BARILE  
 PROFESSIONAL ENGINEER, CT LIC. No. 28643

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**TOLLAND COUNTY**

**DRAWING TITLE:**

**DETAILS**

**DRAWING SHEET:**

**A-3**

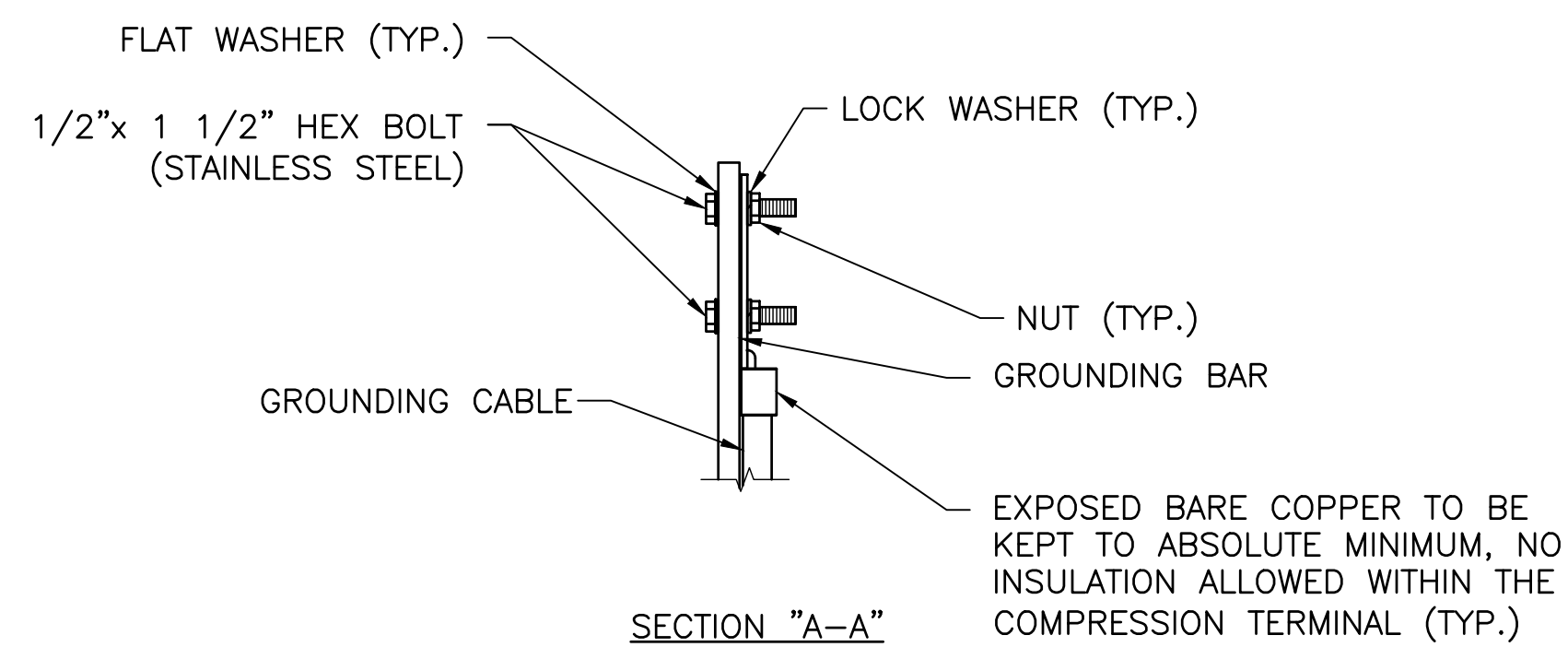
		ANTENNA INFORMATION													
SECTOR	POSITION (FROM REAR LEFT TO RIGHT)	EXISTING		PROPOSED											
		MODEL	QTY.	MODEL	ANT. C.L.	SECTOR MARK	QTY.	E-TILT	M-TILT	RRU MODEL/QUANTITY	DIPLEXER/COMBINERS	TMA	COAX/FIBER QUANTITY	COAX/FIBER SIZE	COAX/FIBER LENGTH
ALPHA 340°	R1	APXV18-206516S-C-A20	1	APXVAALL24_43-U-NA20	175'-0"	N600/L600/L700/N1900/L1900/L2100	1	2/2/0/0	0	(1) 4460 B25+B66 (1) 4480 B71+B85	-	-	8 4	COAX JUMPER FIBER JUMPER	10' 15'
	R2	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	R3	-	-	AIR6419 B41	175'-0"	N2500	1	2/2	0	-	-	-	1 4	6x24 HCS FIBER JUMPER	230' 15'
	R4	APXVAA24_43-U-A20	1	-	-	-	-	-	-	-	-	-	-	-	-
BETA 90°	W1	APXV18-206516S-C-A20	1	APXVAALL24_43-U-NA20	175'-0"	N600/L600/L700/N1900/L1900/L2100	1	2/2/0/0	0	(1) 4460 B25+B66 (1) 4480 B71+B85	-	-	8 4	COAX JUMPER FIBER JUMPER	10' 15'
	W2	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	W3	-	-	AIR6419 B41	175'-0"	N2500	1	2/2	0	-	-	-	1 4	6x24 HCS FIBER JUMPER	230' 15'
	W4	APXVAA24_43-U-A20	1	-	-	-	-	-	-	-	-	-	-	-	-
GAMMA 210°	B1	APXV18-206516S-C-A20	1	APXVAALL24_43-U-NA20	175'-0"	N600/L600/L700/N1900/L1900/L2100	1	2/2/0/0	0	(1) 4460 B25+B66 (1) 4480 B71+B85	-	-	8 4	COAX JUMPER FIBER JUMPER	10' 15'
	B2	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	B3	-	-	AIR6419 B41	175'-0"	N2500	1	2/2	0	-	-	-	1 4	6x24 HCS FIBER JUMPER	230' 15'
	B4	APXVAA24_43-U-A20	1	-	-	-	-	-	-	-	-	-	-	-	-

AT TIME OF CONSTRUCTION, CONTRACTOR TO VERIFY AZIMUTHS OF EXISTING ANTENNAS. IF DIFFERENT FROM RFDS, PLEASE NOTIFY THE RF ENGINEER AND CONSTRUCTION MANAGER WITH ACTUAL AZIMUTH TO ENSURE T-MOBILE'S DATABASE IS ACCURATE AND UP-TO-DATE.

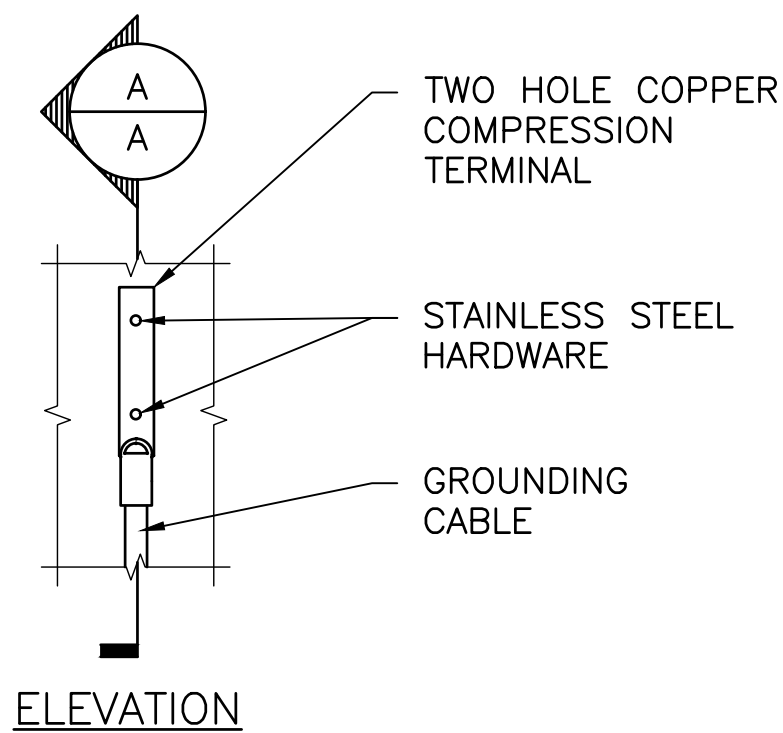
ANTENNA LOCATIONS TO BE VERIFIED IN FIELD. RFDS TO BE REDLINED ACCORDINGLY.

INFORMATION SHOWN PROVIDED ON T-MOBILE RFDS DATED 02/08/24.

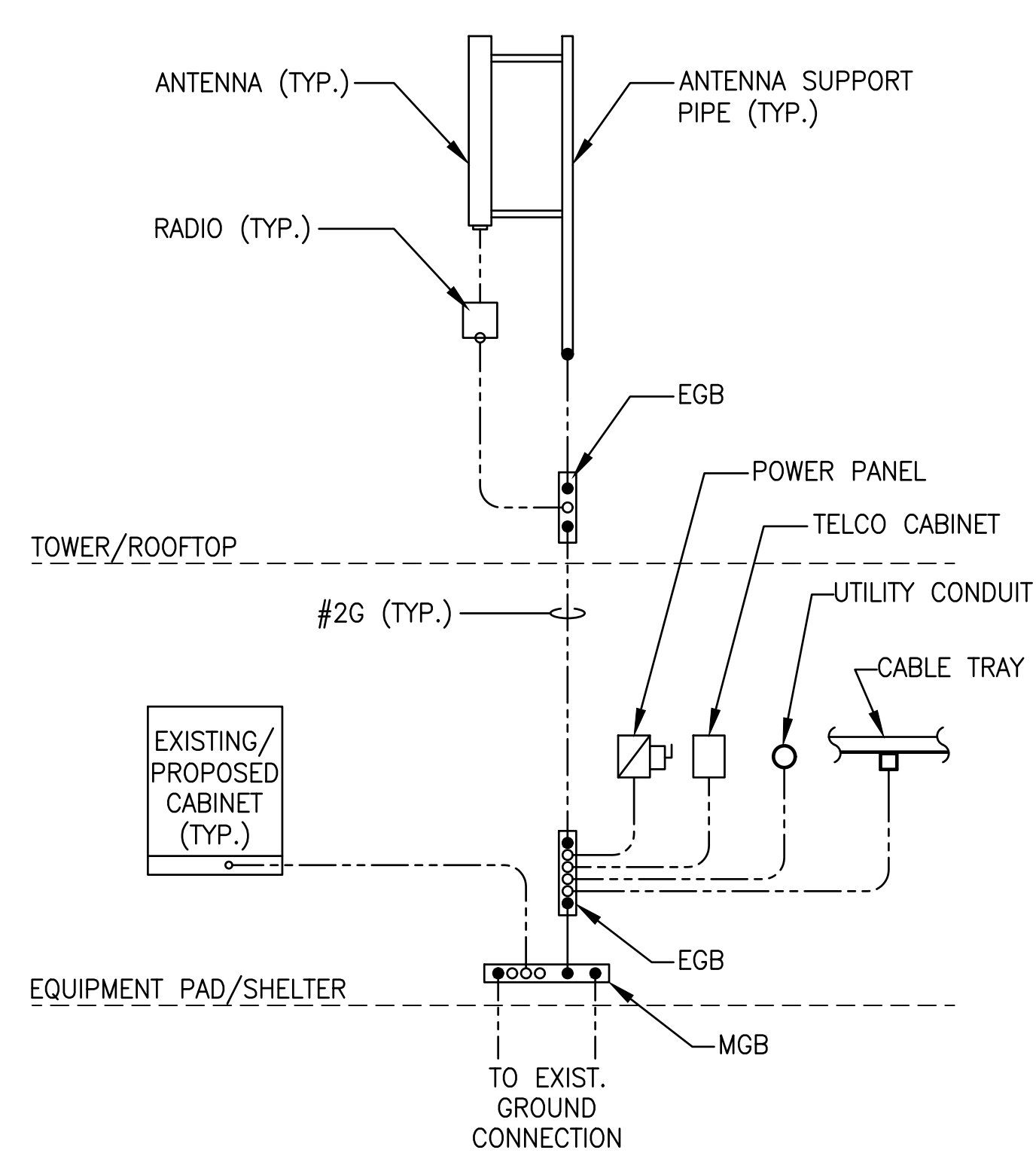




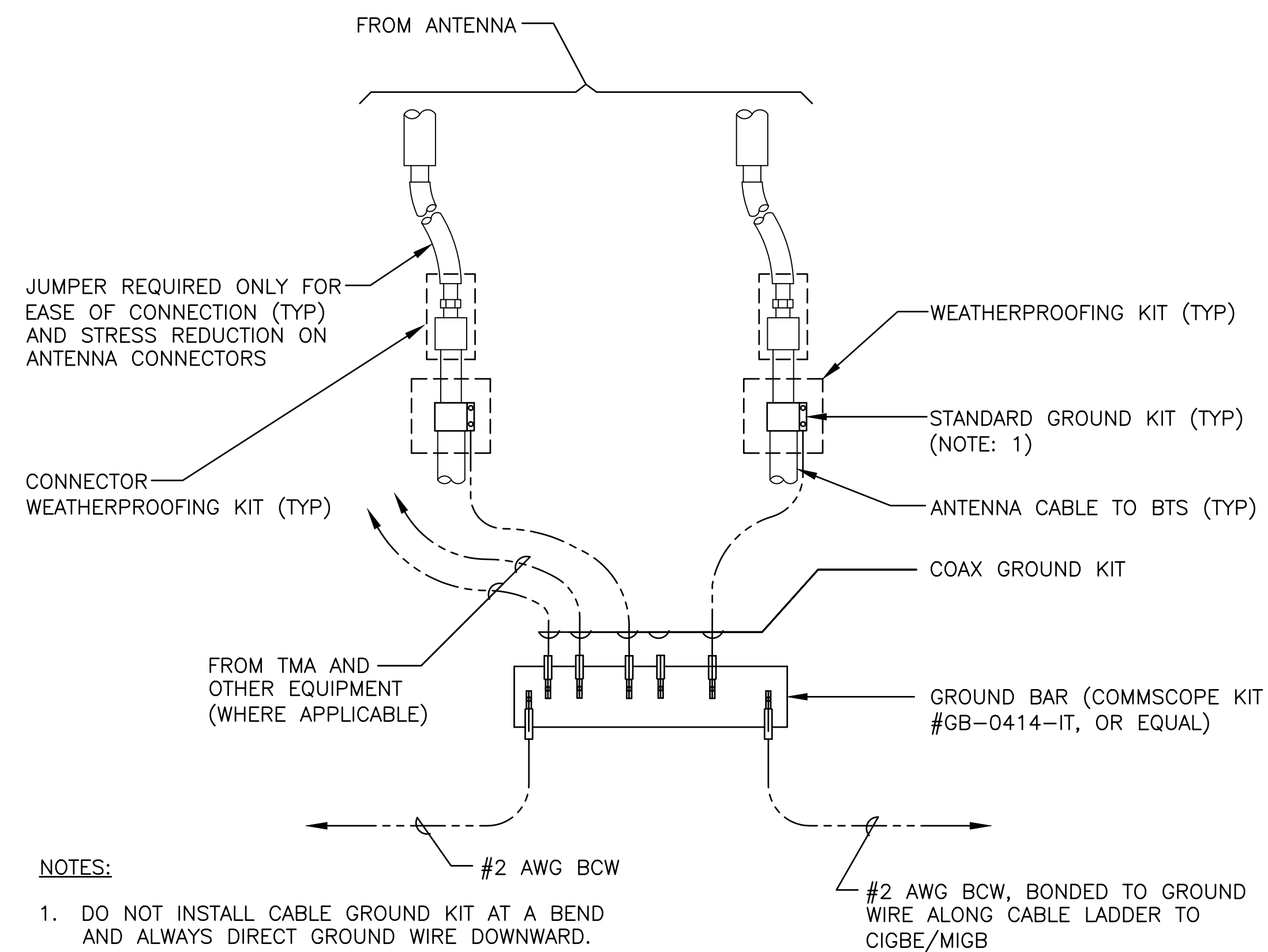
- NOTE:**
- "DOUBLING UP" OR "STACKING" OF CONNECTIONS IS NOT PERMITTED.
  - OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATIONS.



**1**  
E-1 TYPICAL GROUND BAR CONNECTION DETAIL  
SCALE: N.T.S.

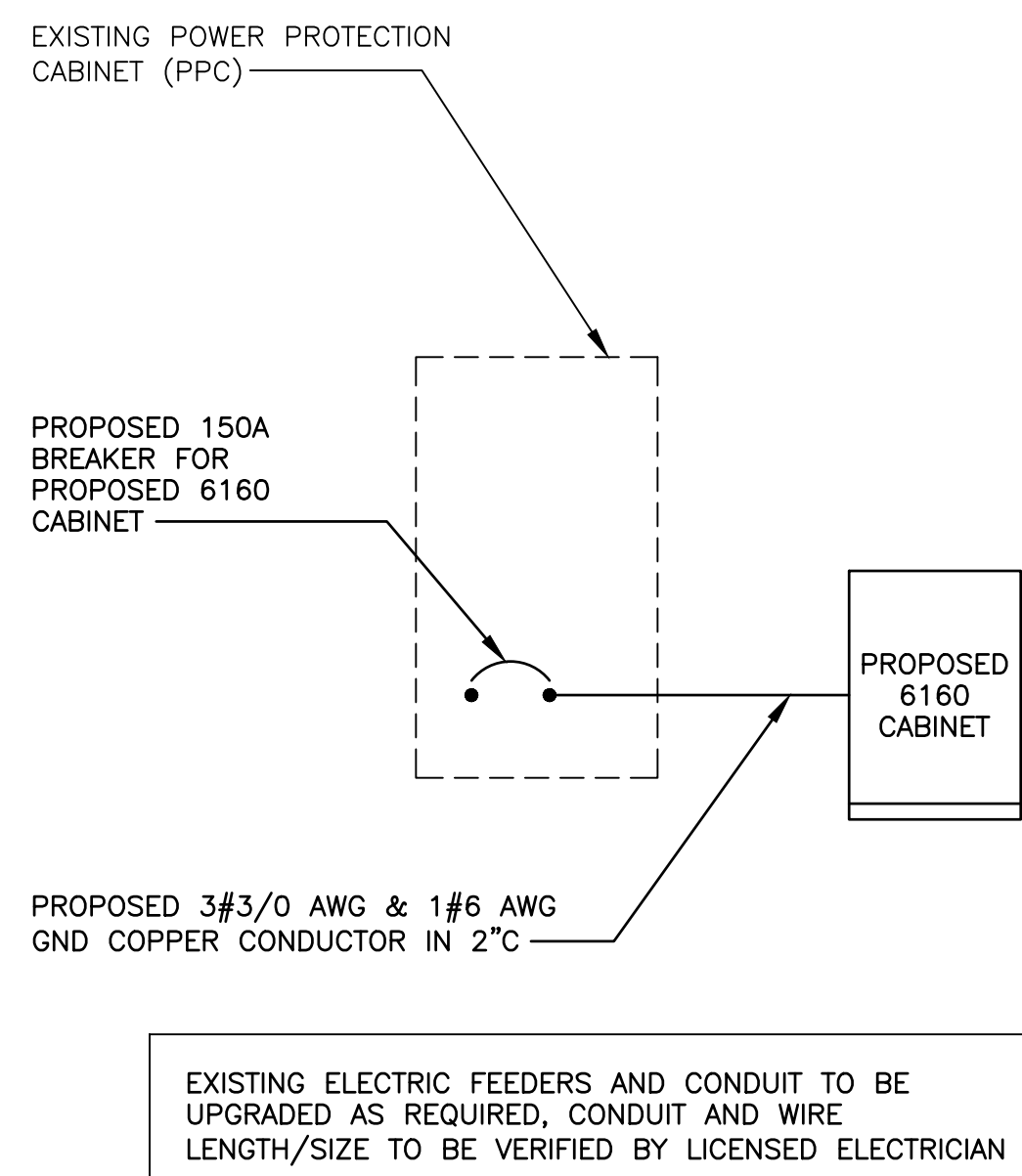


**2**  
E-1 GROUNDING RISER DIAGRAM  
SCALE: N.T.S.

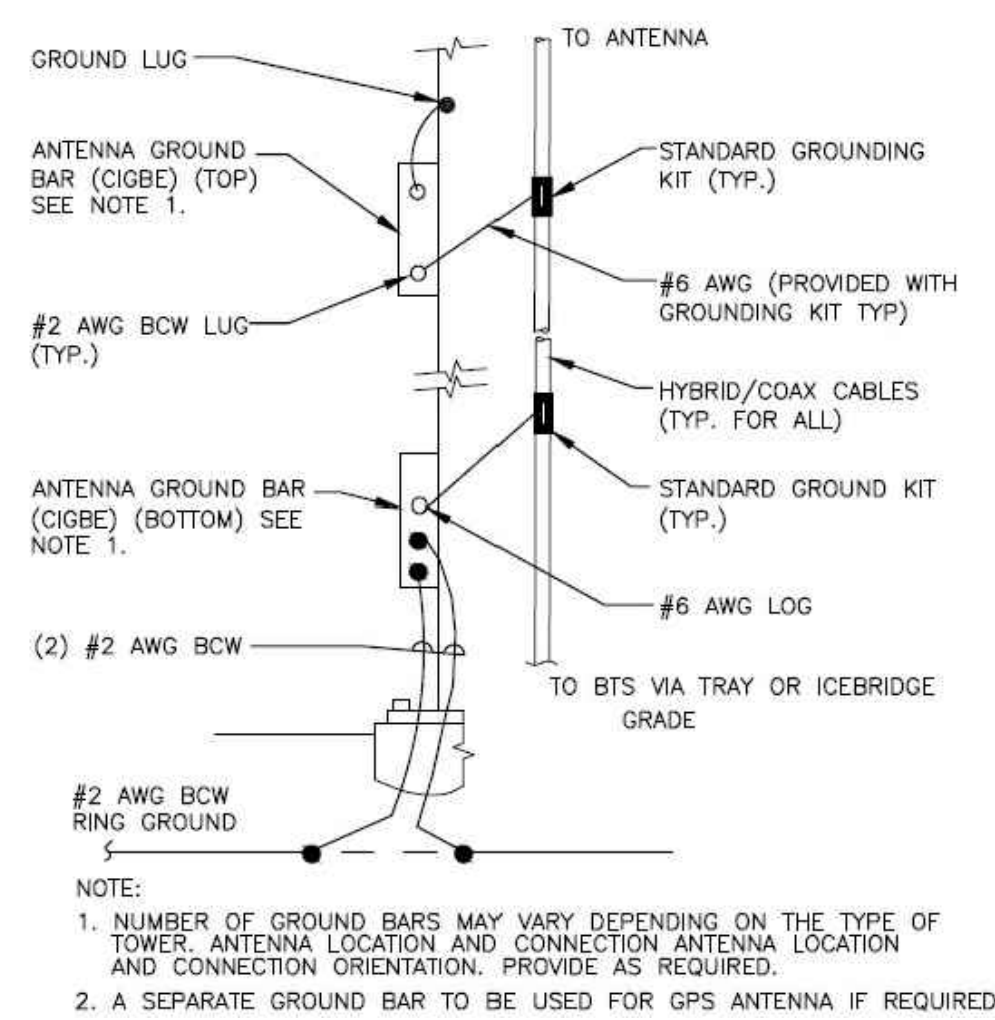


- NOTES:**
- DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWNWARD.

**3**  
E-1 GROUND WIRE TO GROUND BAR CONNECTION DETAIL  
SCALE: N.T.S.



**4**  
E-1 ONE LINE DIAGRAM  
SCALE: 1/4"=1'-0"



**5**  
E-1 ANTENNA CABLE GROUNDING  
SCALE: N.T.S.

ELECTRICAL LEGEND	
A	AMPERE
V	VOLT
KWH	KILOWATT - HOUR
C	CONDUIT
GRC	GALVANIZED RIGID CONDUIT
G	GROUND
MGB	GROUND
○	MECHANICAL CONNECTION
●	CADWELDED CONNECTION
○	MASTER GROUND BAR
○	EQUIPMENT GROUND BAR
—	GROUND COPPER WIRE, SIZE AS NOTED
—	EXPOSED WIRING
—	COAXIAL CABLE
○	5/8"x8" COPPER CLAD STAINLESS STEEL GROUND ROD
●	EXOTHERMIC (CAD WELD) OR MECHANICAL (COMPRESSION TYPE) CONNECTION
PPC	POWER PROTECTION CABINET
⊗	OMNI-DIRECTIONAL ELECTRONIC MARKER SYSTEM (EMS) BALL

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SCHEDULE OF REVISIONS		
7		
6		
5		
4		
3		
2		
1	04/02/24	REVISED PER CLIENT COMMENTS
0	03/05/24	INITIAL SUBMISSION
REV. NO.	DATE	DESCRIPTION OF CHANGES

**DRAWN BY:** CJT  
**CHECKED BY:** NDB  
**SCALE:** AS NOTED  
**JOB NO:** 24008-NSS

INFORMATION ON THIS SET OF DRAWINGS IS NOT FOR OFFICIAL USE UNLESS ACCOMPANIED BY THE STAMPED SEAL & SIGNATURE OF A PROFESSIONAL ENGINEER

**NICHOLAS D. BARILE**  
PROFESSIONAL ENGINEER, CT LIC. No. 28643

**SITE ID: CTHA027B**  
**SITE NAME: ROMANO**  
**248 HALL HILL ROAD**  
**SOMERS, CT 06071**  
**TOLLAND COUNTY**

**DRAWING TITLE:**  
**GROUNDING DETAILS & NOTES**

**DRAWING SHEET:**  
**E-1**

# Exhibit D

## **Structural Analysis Report**

# T Mobile™

## Structural Analysis Report

**Structure** : 180 Foot Monopole Tower  
**VB Site Name** : Blue Ridge  
**VB Site Number** : US-CT-5017  
**Deal Number** : P-049077  
**Proposed Carrier** : T-Mobile  
**Carrier Site Name** : ROMANO  
**Carrier Site Number** : CTHA027B  
**Site Location** : 248 Hall Hill Road  
Somers, CT 06071 (Tolland County)  
42.00259444, -72.48499722  
**Date** : May 24, 2024  
**Max Member Stress Level** : 59.2% (Foundation)  
54.1% (Tower)  
53.9% (Base Plate)  
**Result** : **PASS**

Prepared by:

  
VERTICAL BRIDGE ENGINEERING, LLC



05/24/2024

# **Table of Contents**

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Disclaimer of Warranties .....	6
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Attachment 2: Collocation Application.....	Attached

**Introduction**

We have completed our structural analysis of the proposed equipment installation on the foregoing tower to determine its ability to support the new loads proposed by T-Mobile. The objective of the analysis was to determine if the tower meets the current structural codes and standards with the proposed equipment installation.

**Existing Structural Information**

The following documents for the existing structure were made available for our structural analysis.

Tower Information	Sabre Tower Calculations Job No. 18-6446-JDS, dated 04/06/2018
Foundation Information	
Geotechnical Information	Delta Oaks Geotechnical Report Job No. GEO17-01159-08 Rev. 0, dated 07/18/2017
Existing Equipment Information	Vertical Bridge Collocation Application Version 2
Tower Reinforcement Information	Tower has not been previously modified
Mount Information	Elevated Engineering Mount Analysis, dated 02/26/2024

**Final Proposed Equipment Loading for T-Mobile**

The following proposed loading was obtained from the Vertical Bridge Collocation Application:

Antenna/Equipment					Coax	
Mount (ft)	RAD (ft)	Qty	Antenna	Type	Qty	Size/Type
175	-	3	Site Pro #ULPD12-4xx	Mount	3	1.58” Hybrid
	175	3	RFS APXVAALL24 43-U-NA20	Panel		
		3	Ericsson Radio 4480 B71+B85	RRU		
		<b>3</b>	<b>Ericsson AIR 6419 B41</b>	<b>Panel</b>		
		<b>3</b>	<b>RFS APX18-206513-C-A20</b>	<b>Panel</b>		
		<b>3</b>	<b>RFS APXVAALL24 43-U-NA20</b>	<b>Panel</b>		
		<b>3</b>	<b>Ericsson Radio 4460 B25+B66</b>	<b>RRU</b>		
		<b>1</b>	<b>Commscope VHLP1-23-CR4B</b>	<b>Dish</b>		

**Notes:**

- Proposed equipment shown in bold.
- Other existing loading can be found on the tower profile attached.
- All feedlines are assumed to be installed inside monopole shaft.
- The remainder of 25000 sq. in. reserved rights for T-Mobile has been included in this analysis.
- (3) 1.58” Hybrid, (3) RFS - Andrews APXV18-206516s- C-A20 Panels, and (3) Ericsson Radio 2217 B66A RRUS are to be removed.

## Design Criteria

The tower was analyzed using tnxTower (Version 8.2.4) tower analysis software using the following design criteria.

State	Connecticut
City/County Building Code	IBC 2021 / CSBC 2022
TIA/EIA Standard Code	TIA-222-H
Basic Wind Speed	120 mph ( $V_{ult}$ )
Basic Wind Speed w/Ice	50 mph w/1.5" Ice
Steel Grade	65 ksi Pole / 50 ksi Baseplate / A615-75 ksi Anchor Rods
Exposure Category	C
Topographic Category (height)	1 (0.0 ft.)
Risk Category	II
$S_s$	0.173
Seismic Design Category	B

## Analysis Results

Based on the foregoing information, our structural analysis determined that the existing tower **is structurally capable of supporting the proposed equipment loads without modification**. The existing tower anchor rods, base plate and foundation have also been evaluated and **was found to be structurally capable of supporting the proposed equipment load**. A seismic analysis has been performed on this tower and does not control.



## Assumptions

The below assumptions are true, complete, and accurate.

1. The existing tower has been maintained to manufacturer's specifications and is in good condition.
2. Foundations are considered to have been properly designed for the original design loads.
3. All member connections are considered to have been designed to meet the load carrying capacity of the connected member.
4. Antenna mount loads have been estimated based on generally accepted industry standards.
5. The mounts for the proposed antennas have been analyzed and designed by others.
6. See additional assumptions contained in the report attached.
7. Tower is within acceptable engineering tolerance at 105%.
8. Foundations are within acceptable engineering tolerance at 110%.

## Conclusions

The existing tower described above **has sufficient capacity** to support the proposed loading based on the governing Building Code. The existing tower anchor rods, base plate and foundation have also been evaluated and **are acceptable**. A seismic analysis has been performed on this tower and does not control.

We appreciate the opportunity of providing our continuing professional services to you. If you have any questions or need further assistance, please call us anytime at 561-948-6367.

Sincerely,

Analysis by:



Nicole Hoffman, EI  
Design Engineer III

Reviewed by:

Michael T. De Boer, PE  
Engineer



05/24/2024

## **Standard Conditions**

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but not necessarily limited, to:

- Information supplied by the client regarding the structure itself, the antenna and transmission line loading on the structure and its components, or relevant information.
- Information from drawings in possession of Vertical Bridge Engineering, LLC, or generated by field inspections or measurements of the structure.

It is the responsibility of the client to ensure that the information provided to Vertical Bridge Engineering, LLC and used in the performance of our engineering services is correct and complete. In the absence of information contrary, we consider that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated; and we, therefore consider that their capacity has not significantly changed from the original design condition.

All services will be performed to the codes and standards specified by the client, and we do not imply to meet any other code and standard requirements unless explicitly agreed to in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes and standards, the client shall specify the exact requirements. In the absence of information to the contrary, all work will be performed in accordance with the revision of ANSI/TIA/EIA-222-H requested.

All services are performed, results obtained and recommendations made in accordance with the generally accepted engineering principles and practices. Vertical Bridge Engineering LLC and its affiliates are not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

## **Disclaimer of Warranties**

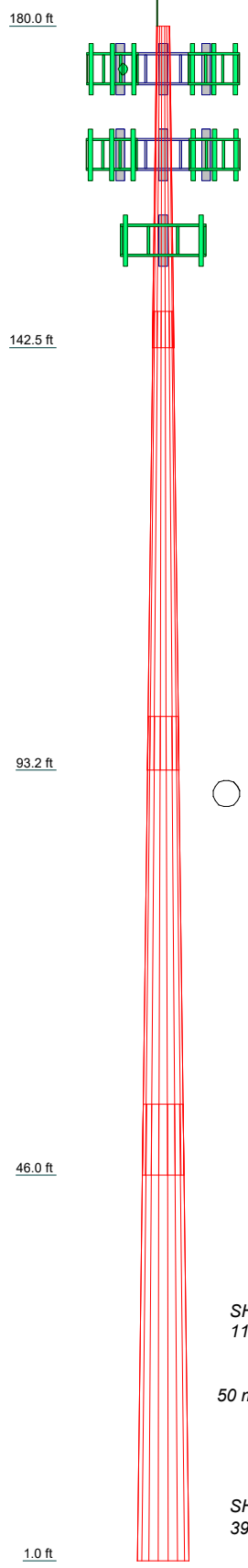
The engineering services by Vertical Bridge Engineering, LLC in connection with this Structural Analysis are limited to a computer analysis of the tower structure, size and capacity of its members. Vertical Bridge Engineering, LLC does not analyze the fabrication, including welding, except as may be expressly included in this report.

The purpose of this report is to assess the feasibility of adding appurtenances usually accompanied by transmission lines. Any mention of structural modifications are reasonable estimates and should not be used a precise construction document. Precise modification drawings are obtainable from Vertical Bridge Engineering, LLC but are beyond the scope of this report.

Vertical Bridge Engineering, LLC makes no warranties, express or implied, in connection with this report and disclaims any liability arising from material, fabrication and erection of this tower, or installation and compliance with legal and permitting requirements of the proposed equipment. Vertical Bridge Engineering, LLC will not be responsible whatsoever for or on account of, punitive, special, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of Vertical Bridge Engineering, LLC pursuant to this report will be limited to the total fee received for preparation of this report.

## Attachment 1: Calculations

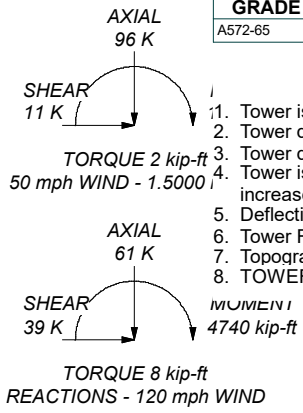
Section	1	2	3	4
Length (ft)	37.500	53.500	53.500	53.250
Number of Sides	18	18	18	18
Thickness (in)	0.2500	0.3750	0.4375	0.4375
Socket Length (ft)	4.250	6.250	8.250	55.2895
Top Dia (in)	18.7500	28.4733	42.2575	71.6700
Bot Dia (in)	30.2800	44.9300	58.7000	
Grade		A572-65		
Weight (K)	2.5	7.9	12.7	15.9



**DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
Lightning Rod 5/8x4'	180	COMMSCOPE NHHSS-65B-R2B (VZW)	165
Site Pro ULDP12-4xx (TMO)	175	COMMSCOPE NHHSS-65B-R2B (VZW)	165
(4) 2.0 STD Mount Pipe (96") (TMO)	175	COMMSCOPE NHHSS-65B-R2B (VZW)	165
(4) 2.0 STD Mount Pipe (96") (TMO)	175	COMMSCOPE NHHSS-65B-R2B (VZW)	165
(4) 2.0 STD Mount Pipe (96") (TMO)	175	COMMSCOPE NHHSS-65B-R2B (VZW)	165
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	175	COMMSCOPE NHH-65B-R2B (VZW)	165
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	175	COMMSCOPE NHH-65B-R2B (VZW)	165
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	175	COMMSCOPE NHH-65B-R2B (VZW)	165
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	175	SAMSUNG TELECOMMUNICATIONS MT6407-77A (VZW)	165
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	175	SAMSUNG TELECOMMUNICATIONS MT6407-77A (VZW)	165
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	175	SAMSUNG TELECOMMUNICATIONS MT6407-77A (VZW)	165
RFS/CELWAVE APX18-206513-C-A20 (TMO)	175	SAMSUNG TELECOMMUNICATIONS RFV01U-D2A (VZW)	165
RFS/CELWAVE APX18-206513-C-A20 (TMO)	175	SAMSUNG TELECOMMUNICATIONS RFV01U-D2A (VZW)	165
RFS/CELWAVE APX18-206513-C-A20 (TMO)	175	SAMSUNG TELECOMMUNICATIONS RFV01U-D2A (VZW)	165
RFS/CELWAVE APX18-206513-C-A20 (TMO)	175	SAMSUNG TELECOMMUNICATIONS RFV01U-D1A (VZW)	165
ERICSSON AIR 6419 B41_TMO (TMO)	175	SAMSUNG TELECOMMUNICATIONS RFV01U-D1A (VZW)	165
ERICSSON AIR 6419 B41_TMO (TMO)	175	SAMSUNG TELECOMMUNICATIONS RT4401-48A (VZW)	165
ERICSSON AIR 6419 B41_TMO (TMO)	175	SAMSUNG TELECOMMUNICATIONS RT4401-48A (VZW)	165
ERICSSON RADIO 4480 B71/B85 (TMO)	175	SAMSUNG TELECOMMUNICATIONS RT4401-48A (VZW)	165
ERICSSON RADIO 4480 B71/B85 (TMO)	175	SAMSUNG TELECOMMUNICATIONS RT4401-48A (VZW)	165
ERICSSON RADIO 4480 B71/B85 (TMO)	175	RAYCAP RC3DC-3315-PF-48 (VZW)	165
ERICSSON RADIO 4480 B71/B85 (TMO)	175	RAYCAP RC3DC-3315-PF-48 (VZW)	165
ERICSSON RADIO 4480 B71/B85 (TMO)	175	Site Pro RMQP-496-HK (VZW)	165
ERICSSON RADIO 4480 B71/B85 (TMO)	175	(3) 2.0 STD Mount Pipe (96") (DISH)	155
ERICSSON RADIO 4480 B71/B85 (TMO)	175	(3) 2.0 STD Mount Pipe (96") (DISH)	155
ERICSSON RADIO 4480 B71/B85 (TMO)	175	(3) 2.0 STD Mount Pipe (96") (DISH)	155
ERICSSON RADIO 4460 B2/B25 B66_TMO (TMO)	175	JMA WIRELESS MX08FRO665-20 (DISH)	155
ERICSSON RADIO 4460 B2/B25 B66_TMO (TMO)	175	JMA WIRELESS MX08FRO665-20 (DISH)	155
ERICSSON RADIO 4460 B2/B25 B66_TMO (TMO)	175	JMA WIRELESS MX08FRO665-20 (DISH)	155
1/3 Remaining Reserve Rights (25000 sq.in.) (TMO)	175	FUJITSU TA08025-B604 (DISH)	155
1/3 Remaining Reserve Rights (25000 sq.in.) (TMO)	175	FUJITSU TA08025-B604 (DISH)	155
1/3 Remaining Reserve Rights (25000 sq.in.) (TMO)	175	FUJITSU TA08025-B605 (DISH)	155
1/3 Remaining Reserve Rights (25000 sq.in.) (TMO)	175	FUJITSU TA08025-B605 (DISH)	155
1/3 Remaining Reserve Rights (25000 sq.in.) (TMO)	175	FUJITSU TA08025-B605 (DISH)	155
VHLP1-23 (TMO)	175	RAYCAP RDIDC-9181-PF-48 (DISH)	155
(4) 2.0 STD Mount Pipe (96") (VZW)	165	1/3 Remaining Reserve Rights (DISH)	155
(4) 2.0 STD Mount Pipe (96") (VZW)	165	1/3 Remaining Reserve Rights (DISH)	155
(4) 2.0 STD Mount Pipe (96") (VZW)	165	1/3 Remaining Reserve Rights (DISH)	155
(4) 2.0 STD Mount Pipe (96") (VZW)	165	Site Pro SNP8R-3xx (DISH)	155

ALL REACTIONS ARE FACTORED



**MATERIAL STRENGTH**

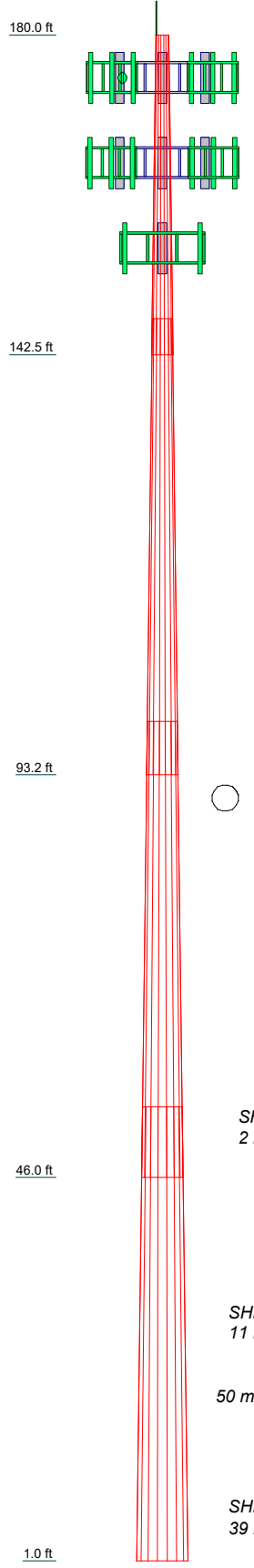
GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

**TOWER DESIGN NOTES**

1. Tower is located in Tolland County, Connecticut.
2. Tower designed for Exposure C to the TIA-222-H Standard.
3. Tower designed for a 120 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 50 mph basic wind with 1.50 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category II.
7. Topographic Category 1 with Crest Height of 0.000 ft
8. TOWER RATING: 54.1%

<b>Vertical Bridge, LLC</b>		Job: <b>US-CT-5017</b>	
750 Park of Commerce Drive		Project: <b>P-049077</b>	
Boca Raton, Florida 33487		Client: T-Mobile	Drawn by: Nicole.Hoffman
Phone:		Code: TIA-222-H	Date: 05/23/24
FAX:		Path:	Scale: NTS
			Dwg No. E-1

Section	1	2	3	4	
Length (ft)	37.500	53.500	53.500	53.250	
Number of Sides	18	18	18	18	
Thickness (in)	0.2500	0.3750	0.4375	0.4375	
Socket Length (ft)	4.250	6.250	8.250		
Top Dia (in)	18.7500	28.4733	42.2575	55.2895	
Bot Dia (in)	30.2800	44.9300	58.7000	71.6700	
Grade			A572-65		
Weight (K)	2.5	7.9	12.7	15.9	38.8



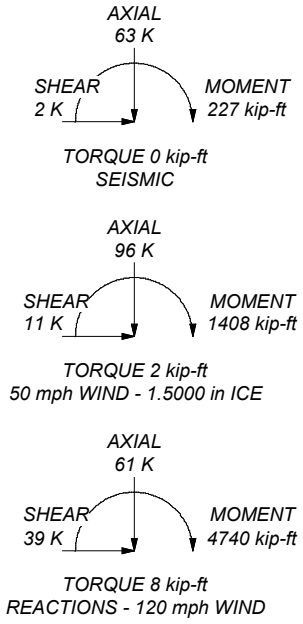
**MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

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5. Deflections are based upon a 60 mph wind.
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7. Topographic Category 1 with Crest Height of 0.000 ft
8. TOWER RATING: 54.1%

ALL REACTIONS ARE FACTORED

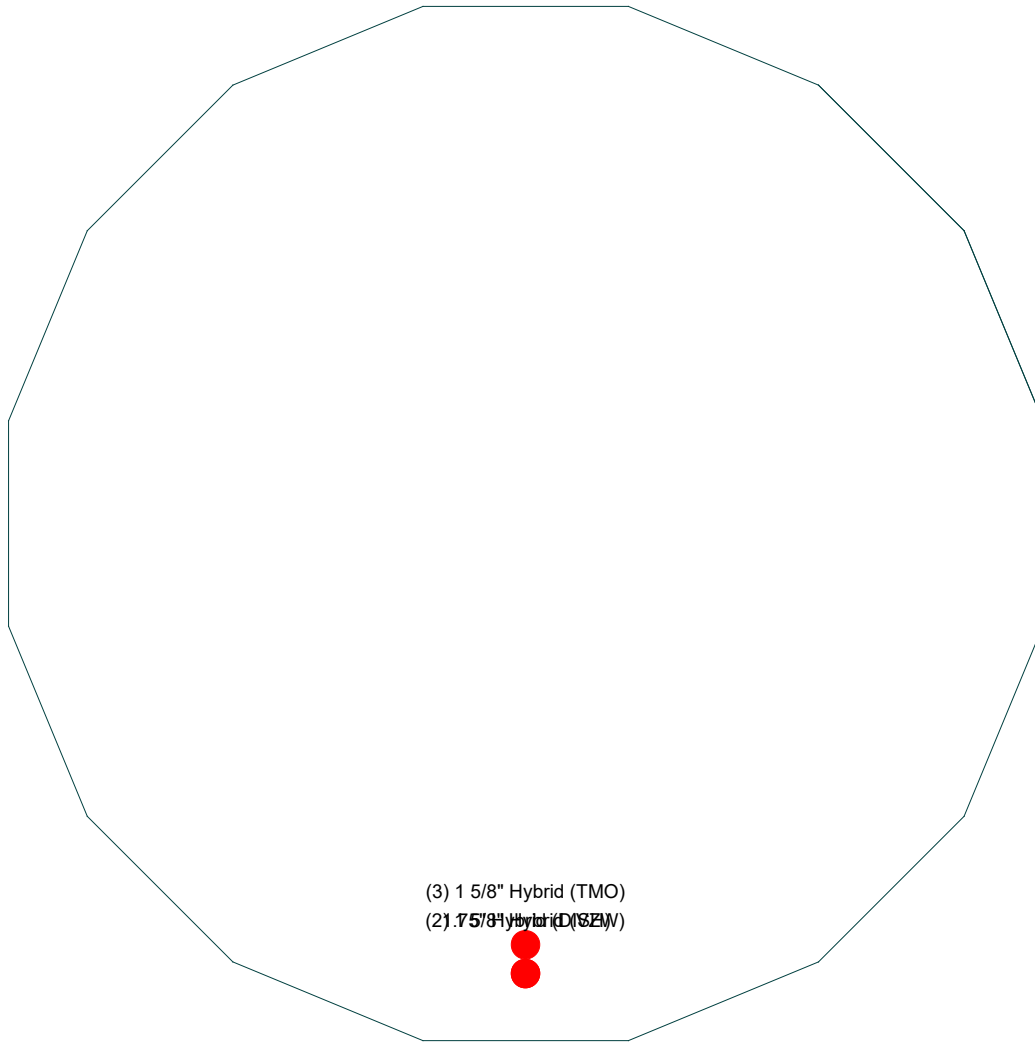


**Vertical Bridge, LLC**  
 750 Park of Commerce Drive  
 Boca Raton, Florida 33487  
 Phone:  
 FAX:

Job: <b>US-CT-5017</b>		
Project: <b>P-049077</b>		
Client: T-Mobile	Drawn by: Nicole Hoffman	App'd:
Code: TIA-222-H	Date: 05/23/24	Scale: NTS
Path:		Dwg No. E-1

# Feed Line Plan

Round Flat App In Face App Out Face



(3) 1 5/8" Hybrid (TMO)  
(2) 1 5/8" Hybrid (S2V)

<b>Vertical Bridge, LLC</b>		Job: <b>US-CT-5017</b>	
750 Park of Commerce Drive		Project: <b>P-049077</b>	
Boca Raton, Florida 33487		Client: T-Mobile	Drawn by: Nicole.Hoffman
Phone:		Code: TIA-222-H	Date: 05/23/24
FAX:		Path:	Scale: NTS
			Dwg No. E-7

<b>tnxTower</b>  <b>Vertical Bridge, LLC</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: FAX:	<b>Job</b> US-CT-5017	<b>Page</b> 1 of 18
	<b>Project</b> P-049077	<b>Date</b> 11:09:14 05/23/24
	<b>Client</b> T-Mobile	<b>Designed by</b> Nicole.Hoffman

## Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

- Tower is located in Tolland County, Connecticut.
- Tower base elevation above sea level: 231.700 ft.
- Basic wind speed of 120 mph.
- Risk Category II.
- Exposure Category C.
- Simplified Topographic Factor Procedure for wind speed-up calculations is used.
- Topographic Category: 1.
- Crest Height: 0.000 ft.
- Nominal ice thickness of 1.5000 in.
- Ice thickness is considered to increase with height.
- Ice density of 56.000 pcf.
- A wind speed of 50 mph is used in combination with ice.
- Temperature drop of 50.000 °F.
- Deflections calculated using a wind speed of 60 mph.
- A non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- Stress ratio used in pole design is 1.
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

- |   |   |  |
|---|---|--|
| <ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>Include Bolts In Member Capacity</li> <li>Leg Bolts Are At Top Of Section</li> <li>Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>SR Members Have Cut Ends</li> <li>SR Members Are Concentric</li> <li>Distribute Leg Loads As Uniform</li> </ul> | <ul style="list-style-type: none"> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>Use Clear Spans For KL/r</li> <li>Retension Guys To Initial Tension</li> <li>√ Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurtenances</li> <li>Alternative Appurt. EPA Calculation</li> <li>Autocalc Torque Arm Areas</li> <li>Add IBC .6D+W Combination</li> <li>√ Sort Capacity Reports By Component</li> <li>Triangulate Diamond Inner Bracing</li> <li>Treat Feed Line Bundles As Cylinder</li> <li>Ignore KL/ry For 60 Deg. Angle Legs</li> <li>Use ASCE 10 X-Brace Ly Rules</li> </ul> | <ul style="list-style-type: none"> <li>Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feed Line Torque</li> <li>Include Angle Block Shear Check</li> <li>Use TIA-222-H Bracing Resist. Exemption</li> <li>Use TIA-222-H Tension Splice Exemption</li> </ul> <p style="text-align: center; background-color: #e0e0e0; margin: 5px 0;">Poles</p> <ul style="list-style-type: none"> <li>√ Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> <li>Pole Without Linear Attachments</li> <li>Pole With Shroud Or No Appurtenances</li> <li>Outside and Inside Corner Radii Are Known</li> </ul> |
|---|---|--|

## Tapered Pole Section Geometry

Section	Elevation	Section Length	Splice Length	Number of Sides	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft		in	in	in	in	
L1	180.000-142.500	37.500	4.250	18	18.7500	30.2800	0.2500	1.0000	A572-65 (65 ksi)
L2	142.500-93.250	53.500	6.250	18	28.4733	44.9300	0.3750	1.5000	A572-65





<b>tnxTower</b>  <b>Vertical Bridge, LLC</b> 750 Park of Commerce Drive Boca Raton, Florida 33487 Phone: FAX:	<b>Job</b>	US-CT-5017	<b>Page</b>	3 of 18
	<b>Project</b>	P-049077	<b>Date</b>	11:09:14 05/23/24
	<b>Client</b>	T-Mobile	<b>Designed by</b>	Nicole.Hoffman

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Total Number		C <sub>AA</sub> ft <sup>2</sup> /ft	Weight klf
***									
1 5/8" Hybrid (TMO)	C	No	No	Inside Pole	175.000 - 6.000	3	No Ice 1/2" Ice 1" Ice 2" Ice	0.000 0.000 0.000 0.000	0.001 0.001 0.001 0.001
***									
1 5/8" Hybrid (VZW)	C	No	No	Inside Pole	165.000 - 6.000	2	No Ice 1/2" Ice 1" Ice 2" Ice	0.000 0.000 0.000 0.000	0.001 0.001 0.001 0.001
***									
1.75" Hybrid (DISH)	C	No	No	Inside Pole	165.000 - 6.000	1	No Ice 1/2" Ice 1" Ice 2" Ice	0.000 0.000 0.000 0.000	0.001 0.001 0.001 0.001
***									

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L1	180.000-142.500	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000	0.000
		C	0.000	0.000	4.219	0.000	0.279
L2	142.500-93.250	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000	0.000
		C	0.000	0.000	5.541	0.000	0.469
L3	93.250-46.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000	0.000
		C	0.000	0.000	5.316	0.000	0.450
L4	46.000-1.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000	0.000
		C	0.000	0.000	4.500	0.000	0.381

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L1	180.000-142.500	A	1.756	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	0.000	0.000	0.000
		C		0.000	0.000	30.565	0.000	0.652
L2	142.500-93.250	A	1.702	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	0.000	0.000	0.000
		C		0.000	0.000	40.142	0.000	0.959
L3	93.250-46.000	A	1.615	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	0.000	0.000	0.000

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Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L4	46.000-1.000	C		0.000	0.000	37.476	0.000	0.895
		A	1.451	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	0.000	0.000	0.000
		C		0.000	0.000	30.335	0.000	0.724

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>X</sub> in	CP <sub>Z</sub> in	CP <sub>X</sub> Ice in	CP <sub>Z</sub> Ice in
L1	180.000-142.500	0.0000	0.8705	0.0000	2.7995
L2	142.500-93.250	0.0000	0.8841	0.0000	3.1270
L3	93.250-46.000	0.0000	0.8913	0.0000	3.2571
L4	46.000-1.000	0.0000	0.7887	0.0000	2.8885

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

### Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>a</sub> No Ice	K <sub>a</sub> Ice
L1	2	Safety Line 3/8	142.50 - 180.00	1.0000	1.0000
L1	3	Step Pegs	142.50 - 180.00	1.0000	1.0000
L2	2	Safety Line 3/8	93.25 - 142.50	1.0000	1.0000
L2	3	Step Pegs	93.25 - 142.50	1.0000	1.0000
L3	2	Safety Line 3/8	46.00 - 93.25	1.0000	1.0000
L3	3	Step Pegs	46.00 - 93.25	1.0000	1.0000
L4	2	Safety Line 3/8	6.00 - 46.00	1.0000	1.0000
L4	3	Step Pegs	6.00 - 46.00	1.0000	1.0000

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
*** Lightning Rod 5/8x4'	C	From Leg	0.000 ft ft ft	0.0000	180.000	No Ice 0.250	0.250	0.031

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight	
			Horz	Vert						ft
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K	
			0.000			1/2" Ice	0.664	0.664	0.034	
			2.000			1" Ice	0.973	0.973	0.039	
						2" Ice	1.494	1.494	0.059	
***										
Site Pro ULPD12-4xx (TMO)	C	None			0.0000	175.000	No Ice	25.540	23.880	2.060
							1/2" Ice	31.800	30.600	2.356
							1" Ice	38.240	36.960	2.780
							2" Ice	50.580	50.760	3.244
(4) 2.0 STD Mount Pipe (96") (TMO)	A	From Leg	4.000		0.0000	175.000	No Ice	1.900	1.900	0.028
			0.000				1/2" Ice	2.728	2.728	0.043
			0.000				1" Ice	3.401	3.401	0.062
							2" Ice	4.396	4.396	0.118
(4) 2.0 STD Mount Pipe (96") (TMO)	B	From Leg	4.000		0.0000	175.000	No Ice	1.900	1.900	0.028
			0.000				1/2" Ice	2.728	2.728	0.043
			0.000				1" Ice	3.401	3.401	0.062
							2" Ice	4.396	4.396	0.118
(4) 2.0 STD Mount Pipe (96") (TMO)	C	From Leg	4.000		0.0000	175.000	No Ice	1.900	1.900	0.028
			0.000				1/2" Ice	2.728	2.728	0.043
			0.000				1" Ice	3.401	3.401	0.062
							2" Ice	4.396	4.396	0.118
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	A	From Leg	4.000		0.0000	175.000	No Ice	20.243	8.733	0.123
			0.000				1/2" Ice	20.890	9.330	0.235
			0.000				1" Ice	21.544	9.935	0.355
							2" Ice	22.874	11.166	0.622
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	B	From Leg	4.000		0.0000	175.000	No Ice	20.243	8.733	0.123
			0.000				1/2" Ice	20.890	9.330	0.235
			0.000				1" Ice	21.544	9.935	0.355
							2" Ice	22.874	11.166	0.622
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	C	From Leg	4.000		0.0000	175.000	No Ice	20.243	8.733	0.123
			0.000				1/2" Ice	20.890	9.330	0.235
			0.000				1" Ice	21.544	9.935	0.355
							2" Ice	22.874	11.166	0.622
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	A	From Leg	4.000		0.0000	175.000	No Ice	20.243	8.733	0.123
			0.000				1/2" Ice	20.890	9.330	0.235
			0.000				1" Ice	21.544	9.935	0.355
							2" Ice	22.874	11.166	0.622
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	B	From Leg	4.000		0.0000	175.000	No Ice	20.243	8.733	0.123
			0.000				1/2" Ice	20.890	9.330	0.235
			0.000				1" Ice	21.544	9.935	0.355
							2" Ice	22.874	11.166	0.622
RFS/CELWAVE APXVAALL24_43-U-NA20 (TMO)	C	From Leg	4.000		0.0000	175.000	No Ice	20.243	8.733	0.123
			0.000				1/2" Ice	20.890	9.330	0.235
			0.000				1" Ice	21.544	9.935	0.355
							2" Ice	22.874	11.166	0.622
RFS/CELWAVE APX18-206513-C-A20 (TMO)	A	From Leg	4.000		0.0000	175.000	No Ice	3.759	2.604	0.083
			0.000				1/2" Ice	4.112	2.944	0.106
			0.000				1" Ice	4.467	3.291	0.134
							2" Ice	5.176	4.008	0.203
RFS/CELWAVE APX18-206513-C-A20 (TMO)	B	From Leg	4.000		0.0000	175.000	No Ice	3.759	2.604	0.083
			0.000				1/2" Ice	4.112	2.944	0.106
			0.000				1" Ice	4.467	3.291	0.134
							2" Ice	5.176	4.008	0.203
RFS/CELWAVE APX18-206513-C-A20 (TMO)	C	From Leg	4.000		0.0000	175.000	No Ice	3.759	2.604	0.083
			0.000				1/2" Ice	4.112	2.944	0.106
			0.000				1" Ice	4.467	3.291	0.134
							2" Ice	5.176	4.008	0.203
ERICSSON AIR 6419	A	From Leg	4.000		0.0000	175.000	No Ice	6.317	2.878	0.097

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T-Mobile						Nicole.Hoffman		

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft		C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
B41_TMO (TMO)			0.000 0.000			1/2" Ice 1" Ice 2" Ice	6.638 6.966 7.646	3.125 3.378 3.907	0.140 0.188 0.298
ERICSSON AIR 6419 B41_TMO (TMO)	B	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	6.317 6.638 6.966 7.646	2.878 3.125 3.378 3.907	0.097 0.140 0.188 0.298
ERICSSON AIR 6419 B41_TMO (TMO)	C	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	6.317 6.638 6.966 7.646	2.878 3.125 3.378 3.907	0.097 0.140 0.188 0.298
ERICSSON RADIO 4480 B71/B85 (TMO)	A	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	2.878 3.091 3.312 3.775	1.397 1.558 1.727 2.090	0.077 0.099 0.124 0.184
ERICSSON RADIO 4480 B71/B85 (TMO)	B	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	2.878 3.091 3.312 3.775	1.397 1.558 1.727 2.090	0.077 0.099 0.124 0.184
ERICSSON RADIO 4480 B71/B85 (TMO)	C	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	2.878 3.091 3.312 3.775	1.397 1.558 1.727 2.090	0.077 0.099 0.124 0.184
ERICSSON RADIO 4480 B71/B85 (TMO)	A	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	2.878 3.091 3.312 3.775	1.397 1.558 1.727 2.090	0.077 0.099 0.124 0.184
ERICSSON RADIO 4480 B71/B85 (TMO)	B	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	2.878 3.091 3.312 3.775	1.397 1.558 1.727 2.090	0.077 0.099 0.124 0.184
ERICSSON RADIO 4480 B71/B85 (TMO)	C	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	2.878 3.091 3.312 3.775	1.397 1.558 1.727 2.090	0.077 0.099 0.124 0.184
ERICSSON RADIO 4460 B2/B25 B66_TMO (TMO)	A	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	2.139 2.321 2.511 2.912	1.686 1.850 2.022 2.387	0.109 0.131 0.156 0.217
ERICSSON RADIO 4460 B2/B25 B66_TMO (TMO)	B	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	2.139 2.321 2.511 2.912	1.686 1.850 2.022 2.387	0.109 0.131 0.156 0.217
ERICSSON RADIO 4460 B2/B25 B66_TMO (TMO)	C	From Leg	4.000 0.000 0.000	0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	2.139 2.321 2.511 2.912	1.686 1.850 2.022 2.387	0.109 0.131 0.156 0.217
1/3 Remaining Reserve Rights (25000 sq.in.) (TMO)	A	None		0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	5.730 6.720 7.710 9.690	5.730 6.720 7.710 9.690	0.061 0.092 0.123 0.185
1/3 Remaining Reserve Rights (25000 sq.in.) (TMO)	B	None		0.0000	175.000	No Ice 1/2" Ice 1" Ice 2" Ice	5.730 6.720 7.710 9.690	5.730 6.720 7.710 9.690	0.061 0.092 0.123 0.185
1/3 Remaining Reserve Rights (25000 sq.in.) (TMO)	C	None		0.0000	175.000	No Ice 1/2" Ice	5.730 6.720	5.730 6.720	0.061 0.092

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight	
			Horz	Vert						ft
						ft <sup>2</sup>	ft <sup>2</sup>	K		
(TMO)						1" Ice	7.710	7.710	0.123	
***						2" Ice	9.690	9.690	0.185	
Site Pro RMQP-496-HK (VZW)	C	None			0.0000	165.000	No Ice	34.540	31.940	1.945
							1/2" Ice	42.040	39.460	2.335
							1" Ice	49.600	47.160	2.845
							2" Ice	64.540	62.020	3.505
(4) 2.0 STD Mount Pipe (96") (VZW)	A	From Leg	4.000		0.0000	165.000	No Ice	1.900	1.900	0.028
			0.000				1/2" Ice	2.728	2.728	0.043
			0.000				1" Ice	3.401	3.401	0.062
							2" Ice	4.396	4.396	0.118
(4) 2.0 STD Mount Pipe (96") (VZW)	B	From Leg	4.000		0.0000	165.000	No Ice	1.900	1.900	0.028
			0.000				1/2" Ice	2.728	2.728	0.043
			0.000				1" Ice	3.401	3.401	0.062
							2" Ice	4.396	4.396	0.118
(4) 2.0 STD Mount Pipe (96") (VZW)	C	From Leg	4.000		0.0000	165.000	No Ice	1.900	1.900	0.028
			0.000				1/2" Ice	2.728	2.728	0.043
			0.000				1" Ice	3.401	3.401	0.062
							2" Ice	4.396	4.396	0.118
COMMSCOPE NHHSS-65B-R2B (VZW)	A	From Leg	4.000		0.0000	165.000	No Ice	8.079	5.342	0.066
			0.000				1/2" Ice	8.535	5.795	0.116
			0.000				1" Ice	8.998	6.255	0.172
							2" Ice	9.945	7.199	0.303
COMMSCOPE NHHSS-65B-R2B (VZW)	B	From Leg	4.000		0.0000	165.000	No Ice	8.079	5.342	0.066
			0.000				1/2" Ice	8.535	5.795	0.116
			0.000				1" Ice	8.998	6.255	0.172
							2" Ice	9.945	7.199	0.303
COMMSCOPE NHHSS-65B-R2B (VZW)	C	From Leg	4.000		0.0000	165.000	No Ice	8.079	5.342	0.066
			0.000				1/2" Ice	8.535	5.795	0.116
			0.000				1" Ice	8.998	6.255	0.172
							2" Ice	9.945	7.199	0.303
COMMSCOPE NHH-65B-R2B (VZW)	A	From Leg	4.000		0.0000	165.000	No Ice	8.079	5.342	0.044
			0.000				1/2" Ice	8.535	5.795	0.094
			0.000				1" Ice	8.998	6.255	0.150
							2" Ice	9.945	7.199	0.281
COMMSCOPE NHH-65B-R2B (VZW)	B	From Leg	4.000		0.0000	165.000	No Ice	8.079	5.342	0.044
			0.000				1/2" Ice	8.535	5.795	0.094
			0.000				1" Ice	8.998	6.255	0.150
							2" Ice	9.945	7.199	0.281
COMMSCOPE NHH-65B-R2B (VZW)	C	From Leg	4.000		0.0000	165.000	No Ice	8.079	5.342	0.044
			0.000				1/2" Ice	8.535	5.795	0.094
			0.000				1" Ice	8.998	6.255	0.150
							2" Ice	9.945	7.199	0.281
SAMSUNG TELECOMMUNICATIONS MT6407-77A (VZW)	A	From Leg	4.000		0.0000	165.000	No Ice	4.692	1.840	0.082
			0.000				1/2" Ice	4.980	2.063	0.111
			0.000				1" Ice	5.275	2.292	0.144
							2" Ice	5.887	2.772	0.223
SAMSUNG TELECOMMUNICATIONS MT6407-77A (VZW)	B	From Leg	4.000		0.0000	165.000	No Ice	4.692	1.840	0.082
			0.000				1/2" Ice	4.980	2.063	0.111
			0.000				1" Ice	5.275	2.292	0.144
							2" Ice	5.887	2.772	0.223
SAMSUNG TELECOMMUNICATIONS MT6407-77A (VZW)	C	From Leg	4.000		0.0000	165.000	No Ice	4.692	1.840	0.082
			0.000				1/2" Ice	4.980	2.063	0.111
			0.000				1" Ice	5.275	2.292	0.144
							2" Ice	5.887	2.772	0.223
SAMSUNG TELECOMMUNICATIONS	A	From Leg	4.000		0.0000	165.000	No Ice	1.875	1.012	0.070
			0.000				1/2" Ice	2.045	1.145	0.087

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	<b>Client</b>		T-Mobile				<b>Designed by</b>		Nicole.Hoffman

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	CAA Front ft <sup>2</sup>	CAA Side ft <sup>2</sup>	Weight K
RFV01U-D2A (VZW)			0.000			1" Ice 2.223	1.284	0.106
SAMSUNG TELECOMMUNICATIONS	B	From Leg	4.000	0.0000	165.000	2" Ice 2.601	1.585	0.153
RFV01U-D2A (VZW)			0.000			No Ice 1.875	1.012	0.070
SAMSUNG TELECOMMUNICATIONS			0.000			1/2" Ice 2.045	1.145	0.087
RFV01U-D2A (VZW)			0.000			1" Ice 2.223	1.284	0.106
SAMSUNG TELECOMMUNICATIONS	C	From Leg	4.000	0.0000	165.000	2" Ice 2.601	1.585	0.153
RFV01U-D2A (VZW)			0.000			No Ice 1.875	1.012	0.070
SAMSUNG TELECOMMUNICATIONS			0.000			1/2" Ice 2.045	1.145	0.087
RFV01U-D2A (VZW)			0.000			1" Ice 2.223	1.284	0.106
SAMSUNG TELECOMMUNICATIONS	A	From Leg	4.000	0.0000	165.000	2" Ice 2.601	1.585	0.153
RFV01U-D1A (VZW)			0.000			No Ice 1.875	1.250	0.084
SAMSUNG TELECOMMUNICATIONS			0.000			1/2" Ice 2.045	1.393	0.103
RFV01U-D1A (VZW)			0.000			1" Ice 2.223	1.543	0.124
SAMSUNG TELECOMMUNICATIONS	B	From Leg	4.000	0.0000	165.000	2" Ice 2.601	1.865	0.175
RFV01U-D1A (VZW)			0.000			No Ice 1.875	1.250	0.084
SAMSUNG TELECOMMUNICATIONS			0.000			1/2" Ice 2.045	1.393	0.103
RFV01U-D1A (VZW)			0.000			1" Ice 2.223	1.543	0.124
SAMSUNG TELECOMMUNICATIONS	C	From Leg	4.000	0.0000	165.000	2" Ice 2.601	1.865	0.175
RFV01U-D1A (VZW)			0.000			No Ice 1.875	1.250	0.084
SAMSUNG TELECOMMUNICATIONS			0.000			1/2" Ice 2.045	1.393	0.103
RFV01U-D1A (VZW)			0.000			1" Ice 2.223	1.543	0.124
SAMSUNG TELECOMMUNICATIONS	A	From Leg	4.000	0.0000	165.000	2" Ice 2.601	1.865	0.175
RT4401-48A (VZW)			0.000			No Ice 0.996	0.501	0.023
SAMSUNG TELECOMMUNICATIONS			0.000			1/2" Ice 1.125	0.602	0.031
RT4401-48A (VZW)			0.000			1" Ice 1.261	0.709	0.041
SAMSUNG TELECOMMUNICATIONS	B	From Leg	4.000	0.0000	165.000	2" Ice 1.555	0.948	0.067
RT4401-48A (VZW)			0.000			No Ice 0.996	0.501	0.023
SAMSUNG TELECOMMUNICATIONS			0.000			1/2" Ice 1.125	0.602	0.031
RT4401-48A (VZW)			0.000			1" Ice 1.261	0.709	0.041
SAMSUNG TELECOMMUNICATIONS	C	From Leg	4.000	0.0000	165.000	2" Ice 1.555	0.948	0.067
RT4401-48A (VZW)			0.000			No Ice 0.996	0.501	0.023
RAYCAP RC3DC-3315-PF-48 (VZW)	B	From Leg	4.000	0.0000	165.000	1/2" Ice 1.125	0.602	0.031
RC3DC-3315-PF-48 (VZW)			0.000			1" Ice 1.261	0.709	0.041
RAYCAP RC3DC-3315-PF-48 (VZW)			0.000			2" Ice 1.555	0.948	0.067
RAYCAP RC3DC-3315-PF-48 (VZW)	C	From Leg	4.000	0.0000	165.000	No Ice 0.996	0.501	0.023
RC3DC-3315-PF-48 (VZW)			0.000			1/2" Ice 1.125	0.602	0.031
RC3DC-3315-PF-48 (VZW)			0.000			1" Ice 1.261	0.709	0.041
RC3DC-3315-PF-48 (VZW)			0.000			2" Ice 1.555	0.948	0.067
***						No Ice 3.792	2.512	0.032
Site Pro SNP8HR-3xx (DISH)	C	None		0.0000	155.000	1/2" Ice 4.044	2.725	0.063
(3) 2.0 STD Mount Pipe (96") (DISH)						1" Ice 4.303	2.945	0.099
(3) 2.0 STD Mount Pipe (96") (DISH)						2" Ice 4.844	3.414	0.181
(3) 2.0 STD Mount Pipe (96") (DISH)	A	From Leg	4.000	0.0000	155.000	No Ice 3.792	2.512	0.032
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			1/2" Ice 4.044	2.725	0.063
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			1" Ice 4.303	2.945	0.099
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			2" Ice 4.844	3.414	0.181
(3) 2.0 STD Mount Pipe (96") (DISH)	B	From Leg	4.000	0.0000	155.000	No Ice 26.900	26.000	1.472
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			1/2" Ice 31.560	30.670	1.714
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			1" Ice 35.730	34.650	2.002
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			2" Ice 45.540	44.680	2.440
(3) 2.0 STD Mount Pipe (96") (DISH)	C	From Leg	4.000	0.0000	155.000	No Ice 1.900	1.900	0.028
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			1/2" Ice 2.728	2.728	0.043
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			1" Ice 3.401	3.401	0.062
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			2" Ice 4.396	4.396	0.118
(3) 2.0 STD Mount Pipe (96") (DISH)	B	From Leg	4.000	0.0000	155.000	No Ice 1.900	1.900	0.028
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			1/2" Ice 2.728	2.728	0.043
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			1" Ice 3.401	3.401	0.062
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			2" Ice 4.396	4.396	0.118
(3) 2.0 STD Mount Pipe (96") (DISH)	C	From Leg	4.000	0.0000	155.000	No Ice 1.900	1.900	0.028
(3) 2.0 STD Mount Pipe (96") (DISH)			0.000			1/2" Ice 2.728	2.728	0.043

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
			0.000			1" Ice 3.401	3.401	0.062
						2" Ice 4.396	4.396	0.118
JMA WIRELESS MX08FRO665-20 (DISH)	A	From Leg	4.000	0.0000	155.000	No Ice 4.900	0.923	0.072
			0.000			1/2" Ice 12.986	6.325	0.146
			0.000			1" Ice 13.490	6.790	0.226
						2" Ice 14.519	7.743	0.408
JMA WIRELESS MX08FRO665-20 (DISH)	B	From Leg	4.000	0.0000	155.000	No Ice 4.900	0.923	0.072
			0.000			1/2" Ice 12.986	6.325	0.146
			0.000			1" Ice 13.490	6.790	0.226
						2" Ice 14.519	7.743	0.408
JMA WIRELESS MX08FRO665-20 (DISH)	C	From Leg	4.000	0.0000	155.000	No Ice 4.900	0.923	0.072
			0.000			1/2" Ice 12.986	6.325	0.146
			0.000			1" Ice 13.490	6.790	0.226
						2" Ice 14.519	7.743	0.408
FUJITSU TA08025-B604 (DISH)	A	From Leg	4.000	0.0000	155.000	No Ice 1.964	0.981	0.064
			0.000			1/2" Ice 2.138	1.112	0.081
			0.000			1" Ice 2.320	1.250	0.100
						2" Ice 2.705	1.548	0.148
FUJITSU TA08025-B604 (DISH)	B	From Leg	4.000	0.0000	155.000	No Ice 1.964	0.981	0.064
			0.000			1/2" Ice 2.138	1.112	0.081
			0.000			1" Ice 2.320	1.250	0.100
						2" Ice 2.705	1.548	0.148
FUJITSU TA08025-B604 (DISH)	C	From Leg	4.000	0.0000	155.000	No Ice 1.964	0.981	0.064
			0.000			1/2" Ice 2.138	1.112	0.081
			0.000			1" Ice 2.320	1.250	0.100
						2" Ice 2.705	1.548	0.148
FUJITSU TA08025-B605 (DISH)	A	From Leg	4.000	0.0000	155.000	No Ice 1.964	1.129	0.075
			0.000			1/2" Ice 2.138	1.267	0.093
			0.000			1" Ice 2.320	1.411	0.114
						2" Ice 2.705	1.723	0.164
FUJITSU TA08025-B605 (DISH)	B	From Leg	4.000	0.0000	155.000	No Ice 1.964	1.129	0.075
			0.000			1/2" Ice 2.138	1.267	0.093
			0.000			1" Ice 2.320	1.411	0.114
						2" Ice 2.705	1.723	0.164
FUJITSU TA08025-B605 (DISH)	C	From Leg	4.000	0.0000	155.000	No Ice 1.964	1.129	0.075
			0.000			1/2" Ice 2.138	1.267	0.093
			0.000			1" Ice 2.320	1.411	0.114
						2" Ice 2.705	1.723	0.164
RAYCAP RDIDC-9181-PF-48 (DISH)	C	From Leg	4.000	0.0000	155.000	No Ice 2.012	1.168	0.022
			0.000			1/2" Ice 2.189	1.311	0.040
			0.000			1" Ice 2.373	1.461	0.060
						2" Ice 2.763	1.784	0.110
1/3 Remaining Reserve Rights (DISH)	A	None		0.0000	155.000	No Ice 5.774	5.774	0.062
						1/2" Ice 6.755	6.755	0.092
						1" Ice 7.736	7.736	0.122
						2" Ice 9.698	9.698	0.182
1/3 Remaining Reserve Rights (DISH)	B	None		0.0000	155.000	No Ice 5.774	5.774	0.062
						1/2" Ice 6.755	6.755	0.092
						1" Ice 7.736	7.736	0.122
						2" Ice 9.698	9.698	0.182
1/3 Remaining Reserve Rights (DISH)	C	None		0.0000	155.000	No Ice 5.774	5.774	0.062
						1/2" Ice 6.755	6.755	0.092
						1" Ice 7.736	7.736	0.122
						2" Ice 9.698	9.698	0.182

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## Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight
				Horz Lateral Vert							
				ft	°	°	ft	ft	ft <sup>2</sup>	K	
***											
VHLP1-23 (TMO)	C	Paraboloid w/Radome	From Leg	4.000 0.000 0.000	0.0000			175.000	1.275	No Ice 1/2" Ice 1" Ice 2" Ice	0.014 0.021 0.029 0.044
***											

## Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.0 Wind 0 deg - No Ice
3	0.9 Dead+1.0 Wind 0 deg - No Ice
4	1.2 Dead+1.0 Wind 30 deg - No Ice
5	0.9 Dead+1.0 Wind 30 deg - No Ice
6	1.2 Dead+1.0 Wind 60 deg - No Ice
7	0.9 Dead+1.0 Wind 60 deg - No Ice
8	1.2 Dead+1.0 Wind 90 deg - No Ice
9	0.9 Dead+1.0 Wind 90 deg - No Ice
10	1.2 Dead+1.0 Wind 120 deg - No Ice
11	0.9 Dead+1.0 Wind 120 deg - No Ice
12	1.2 Dead+1.0 Wind 150 deg - No Ice
13	0.9 Dead+1.0 Wind 150 deg - No Ice
14	1.2 Dead+1.0 Wind 180 deg - No Ice
15	0.9 Dead+1.0 Wind 180 deg - No Ice
16	1.2 Dead+1.0 Wind 210 deg - No Ice
17	0.9 Dead+1.0 Wind 210 deg - No Ice
18	1.2 Dead+1.0 Wind 240 deg - No Ice
19	0.9 Dead+1.0 Wind 240 deg - No Ice
20	1.2 Dead+1.0 Wind 270 deg - No Ice
21	0.9 Dead+1.0 Wind 270 deg - No Ice
22	1.2 Dead+1.0 Wind 300 deg - No Ice
23	0.9 Dead+1.0 Wind 300 deg - No Ice
24	1.2 Dead+1.0 Wind 330 deg - No Ice
25	0.9 Dead+1.0 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp



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Comb. No.	Description
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	180 - 142.5	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-32.612	0.707	-1.758
			Max. Mx	8	-14.169	-427.741	0.073
			Max. My	14	-14.184	0.133	-426.156
			Max. Vy	8	20.860	-427.741	0.073
			Max. Vx	2	-20.768	-0.033	425.894
			Max. Torque	9			-8.529
L2	142.5 - 93.25	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-46.255	0.730	-2.716
			Max. Mx	8	-23.635	-1530.629	-0.271
			Max. My	2	-23.644	-0.401	1524.259
			Max. Vy	8	26.036	-1530.629	-0.271
			Max. Vx	2	-25.944	-0.401	1524.259
			Max. Torque	9			-8.523
L3	93.25 - 46	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-66.338	0.730	-3.805
			Max. Mx	8	-38.432	-2843.823	-0.477
			Max. My	2	-38.436	-0.760	2833.096
			Max. Vy	8	32.056	-2843.823	-0.477
			Max. Vx	2	-31.965	-0.760	2833.096
			Max. Torque	9			-8.500
L4	46 - 1	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-96.197	0.730	-5.157
			Max. Mx	8	-61.336	-4739.670	-0.646
			Max. My	2	-61.336	-1.181	4723.881
			Max. Vy	8	38.878	-4739.670	-0.646
			Max. Vx	2	-38.790	-1.181	4723.881
			Max. Torque	9			-8.489

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	33	96.197	-0.001	-11.338
	Max. H <sub>x</sub>	20	61.353	38.832	-0.002
	Max. H <sub>z</sub>	2	61.353	-0.008	38.763

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Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
	Max. M <sub>x</sub>	2	4723.881	-0.008	38.763
	Max. M <sub>z</sub>	8	4739.670	-38.851	0.002
	Max. Torsion	21	8.454	38.832	-0.002
	Min. Vert	25	46.015	19.368	33.564
	Min. H <sub>x</sub>	8	61.353	-38.851	0.002
	Min. H <sub>z</sub>	14	61.353	-0.002	-38.745
	Min. M <sub>x</sub>	14	-4722.704	-0.002	-38.745
	Min. M <sub>z</sub>	20	-4736.640	38.832	-0.002
	Min. Torsion	9	-8.486	-38.851	0.002

## Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	51.128	0.000	0.000	0.825	0.177	0.000
1.2 Dead+1.0 Wind 0 deg - No Ice	61.353	0.008	-38.763	-4723.881	-1.181	-0.434
0.9 Dead+1.0 Wind 0 deg - No Ice	46.015	0.008	-38.763	-4685.079	-1.227	-0.433
1.2 Dead+1.0 Wind 30 deg - No Ice	61.353	19.406	-33.609	-4097.581	-2366.553	-7.594
0.9 Dead+1.0 Wind 30 deg - No Ice	46.015	19.406	-33.609	-4063.953	-2347.020	-7.595
1.2 Dead+1.0 Wind 60 deg - No Ice	61.353	33.642	-19.423	-2368.452	-4103.837	0.513
0.9 Dead+1.0 Wind 60 deg - No Ice	46.015	33.642	-19.423	-2349.116	-4069.944	0.514
1.2 Dead+1.0 Wind 90 deg - No Ice	61.353	38.851	-0.002	0.645	-4739.670	8.482
0.9 Dead+1.0 Wind 90 deg - No Ice	46.015	38.851	-0.002	0.399	-4700.514	8.486
1.2 Dead+1.0 Wind 120 deg - No Ice	61.353	33.609	19.395	2365.776	-4098.448	0.946
0.9 Dead+1.0 Wind 120 deg - No Ice	46.015	33.609	19.395	2345.950	-4064.602	0.948
1.2 Dead+1.0 Wind 150 deg - No Ice	61.353	19.384	33.555	4090.366	-2362.609	-6.856
0.9 Dead+1.0 Wind 150 deg - No Ice	46.015	19.384	33.555	4056.274	-2343.139	-6.857
1.2 Dead+1.0 Wind 180 deg - No Ice	61.353	0.002	38.745	4722.704	-0.174	0.397
0.9 Dead+1.0 Wind 180 deg - No Ice	46.015	0.002	38.745	4683.399	-0.229	0.397
1.2 Dead+1.0 Wind 210 deg - No Ice	61.353	-19.397	33.593	4096.709	2365.128	7.563
0.9 Dead+1.0 Wind 210 deg - No Ice	46.015	-19.397	33.593	4062.559	2345.522	7.564
1.2 Dead+1.0 Wind 240 deg - No Ice	61.353	-33.631	19.417	2369.438	4102.428	-0.513
0.9 Dead+1.0 Wind 240 deg - No Ice	46.015	-33.631	19.417	2349.578	4068.433	-0.514
1.2 Dead+1.0 Wind 270 deg - No Ice	61.353	-38.832	0.002	1.256	4736.640	-8.450
0.9 Dead+1.0 Wind 270 deg - No Ice	46.015	-38.832	0.002	1.003	4697.398	-8.454
1.2 Dead+1.0 Wind 300 deg - No Ice	61.353	-33.589	-19.395	-2363.658	4095.187	-0.909

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Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
No Ice						
0.9 Dead+1.0 Wind 300 deg - No Ice	46.015	-33.589	-19.395	-2344.366	4061.259	-0.911
1.2 Dead+1.0 Wind 330 deg - No Ice	61.353	-19.368	-33.564	-4089.909	2360.275	6.856
0.9 Dead+1.0 Wind 330 deg - No Ice	46.015	-19.368	-33.564	-4056.351	2340.687	6.857
1.2 Dead+1.0 Ice+1.0 Temp	96.197	-0.000	0.000	5.157	0.730	0.000
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	96.197	0.002	-11.343	-1396.504	0.403	-0.115
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	96.197	5.677	-9.832	-1210.189	-701.156	-1.479
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	96.197	9.838	-5.680	-697.051	-1215.920	0.109
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	96.197	11.361	-0.000	5.317	-1404.321	1.668
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	96.197	9.831	5.674	706.738	-1214.708	0.224
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	96.197	5.672	9.819	1218.750	-700.249	-1.283
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	96.197	0.001	11.338	1406.456	0.671	0.106
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	96.197	-5.674	9.827	1220.214	702.225	1.471
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	96.197	-9.835	5.678	707.583	1216.977	-0.109
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	96.197	-11.356	0.000	5.479	1404.946	-1.659
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	96.197	-9.826	-5.674	-695.902	1215.273	-0.214
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp	96.197	-5.668	-9.821	-1208.368	701.048	1.283
Dead+Wind 0 deg - Service	51.128	0.002	-8.671	-1051.049	-0.125	-0.098
Dead+Wind 30 deg - Service	51.128	4.341	-7.518	-911.622	-526.718	-1.714
Dead+Wind 60 deg - Service	51.128	7.525	-4.345	-526.661	-913.501	0.116
Dead+Wind 90 deg - Service	51.128	8.690	-0.000	0.784	-1055.057	1.915
Dead+Wind 120 deg - Service	51.128	7.518	4.338	527.321	-912.299	0.214
Dead+Wind 150 deg - Service	51.128	4.336	7.506	911.258	-525.857	-1.548
Dead+Wind 180 deg - Service	51.128	0.000	8.667	1052.042	0.099	0.089
Dead+Wind 210 deg - Service	51.128	-4.339	7.514	912.672	526.695	1.707
Dead+Wind 240 deg - Service	51.128	-7.523	4.343	528.137	913.462	-0.116
Dead+Wind 270 deg - Service	51.128	-8.686	0.000	0.919	1054.656	-1.908
Dead+Wind 300 deg - Service	51.128	-7.513	-4.338	-525.592	911.848	-0.205
Dead+Wind 330 deg - Service	51.128	-4.332	-7.508	-909.910	525.595	1.548

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.000	-51.128	0.000	0.000	51.128	0.000	0.000%
2	0.008	-61.353	-38.763	-0.008	61.353	38.763	0.000%
3	0.008	-46.015	-38.763	-0.008	46.015	38.763	0.000%
4	19.406	-61.353	-33.609	-19.406	61.353	33.609	0.000%
5	19.406	-46.015	-33.609	-19.406	46.015	33.609	0.000%
6	33.642	-61.353	-19.423	-33.642	61.353	19.423	0.000%
7	33.642	-46.015	-19.423	-33.642	46.015	19.423	0.000%
8	38.851	-61.353	-0.002	-38.851	61.353	0.002	0.000%

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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
9	38.851	-46.015	-0.002	-38.851	46.015	0.002	0.000%
10	33.609	-61.353	19.395	-33.609	61.353	-19.395	0.000%
11	33.609	-46.015	19.395	-33.609	46.015	-19.395	0.000%
12	19.384	-61.353	33.555	-19.384	61.353	-33.555	0.000%
13	19.384	-46.015	33.555	-19.384	46.015	-33.555	0.000%
14	0.002	-61.353	38.745	-0.002	61.353	-38.745	0.000%
15	0.002	-46.015	38.745	-0.002	46.015	-38.745	0.000%
16	-19.397	-61.353	33.593	19.397	61.353	-33.593	0.000%
17	-19.397	-46.015	33.593	19.397	46.015	-33.593	0.000%
18	-33.631	-61.353	19.417	33.631	61.353	-19.417	0.000%
19	-33.631	-46.015	19.417	33.631	46.015	-19.417	0.000%
20	-38.832	-61.353	0.002	38.832	61.353	-0.002	0.000%
21	-38.832	-46.015	0.002	38.832	46.015	-0.002	0.000%
22	-33.589	-61.353	-19.395	33.589	61.353	19.395	0.000%
23	-33.589	-46.015	-19.395	33.589	46.015	19.395	0.000%
24	-19.368	-61.353	-33.564	19.368	61.353	33.564	0.000%
25	-19.368	-46.015	-33.564	19.368	46.015	33.564	0.000%
26	0.000	-96.197	0.000	0.000	96.197	-0.000	0.000%
27	0.002	-96.197	-11.343	-0.002	96.197	11.343	0.000%
28	5.677	-96.197	-9.832	-5.677	96.197	9.832	0.000%
29	9.838	-96.197	-5.680	-9.838	96.197	5.680	0.000%
30	11.361	-96.197	-0.000	-11.361	96.197	0.000	0.000%
31	9.831	-96.197	5.674	-9.831	96.197	-5.674	0.000%
32	5.672	-96.197	9.819	-5.672	96.197	-9.819	0.000%
33	0.001	-96.197	11.338	-0.001	96.197	-11.338	0.000%
34	-5.674	-96.197	9.827	5.674	96.197	-9.827	0.000%
35	-9.835	-96.197	5.678	9.835	96.197	-5.678	0.000%
36	-11.356	-96.197	0.000	11.356	96.197	-0.000	0.000%
37	-9.826	-96.197	-5.674	9.826	96.197	5.674	0.000%
38	-5.668	-96.197	-9.821	5.668	96.197	9.821	0.000%
39	0.002	-51.128	-8.671	-0.002	51.128	8.671	0.000%
40	4.341	-51.128	-7.518	-4.341	51.128	7.518	0.000%
41	7.525	-51.128	-4.345	-7.525	51.128	4.345	0.000%
42	8.690	-51.128	-0.000	-8.690	51.128	0.000	0.000%
43	7.518	-51.128	4.338	-7.518	51.128	-4.338	0.000%
44	4.336	-51.128	7.506	-4.336	51.128	-7.506	0.000%
45	0.000	-51.128	8.667	-0.000	51.128	-8.667	0.000%
46	-4.339	-51.128	7.514	4.339	51.128	-7.514	0.000%
47	-7.523	-51.128	4.343	7.523	51.128	-4.343	0.000%
48	-8.686	-51.128	0.000	8.686	51.128	-0.000	0.000%
49	-7.513	-51.128	-4.338	7.513	51.128	4.338	0.000%
50	-4.332	-51.128	-7.508	4.332	51.128	7.508	0.000%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00017366
3	Yes	4	0.00000001	0.00008701
4	Yes	5	0.00000001	0.00029624
5	Yes	5	0.00000001	0.00013119
6	Yes	5	0.00000001	0.00032915
7	Yes	5	0.00000001	0.00014681
8	Yes	5	0.00000001	0.00010114
9	Yes	5	0.00000001	0.00004754

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10	Yes	5	0.0000001	0.00033740
11	Yes	5	0.0000001	0.00015091
12	Yes	5	0.0000001	0.00038229
13	Yes	5	0.0000001	0.00017315
14	Yes	4	0.0000001	0.00017013
15	Yes	4	0.0000001	0.00008401
16	Yes	5	0.0000001	0.00038918
17	Yes	5	0.0000001	0.00017640
18	Yes	5	0.0000001	0.00033574
19	Yes	5	0.0000001	0.00014998
20	Yes	5	0.0000001	0.00010086
21	Yes	5	0.0000001	0.00004751
22	Yes	5	0.0000001	0.00032528
23	Yes	5	0.0000001	0.00014508
24	Yes	5	0.0000001	0.00029656
25	Yes	5	0.0000001	0.00013143
26	Yes	4	0.0000001	0.00000872
27	Yes	5	0.0000001	0.00019675
28	Yes	5	0.0000001	0.00023434
29	Yes	5	0.0000001	0.00023592
30	Yes	5	0.0000001	0.00020164
31	Yes	5	0.0000001	0.00023912
32	Yes	5	0.0000001	0.00024323
33	Yes	5	0.0000001	0.00019896
34	Yes	5	0.0000001	0.00024525
35	Yes	5	0.0000001	0.00023984
36	Yes	5	0.0000001	0.00020205
37	Yes	5	0.0000001	0.00023575
38	Yes	5	0.0000001	0.00023433
39	Yes	4	0.0000001	0.00002219
40	Yes	4	0.0000001	0.00012671
41	Yes	4	0.0000001	0.00011356
42	Yes	4	0.0000001	0.00013767
43	Yes	4	0.0000001	0.00012414
44	Yes	4	0.0000001	0.00019309
45	Yes	4	0.0000001	0.00002208
46	Yes	4	0.0000001	0.00020272
47	Yes	4	0.0000001	0.00012148
48	Yes	4	0.0000001	0.00013720
49	Yes	4	0.0000001	0.00011087
50	Yes	4	0.0000001	0.00012067

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	180 - 142.5	20.282	47	1.1330	0.0184
L2	146.75 - 93.25	12.797	47	0.9440	0.0074
L3	99.5 - 46	5.373	47	0.5442	0.0023
L4	54.25 - 1	1.515	47	0.2630	0.0008

### Critical Deflections and Radius of Curvature - Service Wind

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Elevation	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
180.000	Lightning Rod 5/8x4'	47	20.282	1.1330	0.0184	37871
175.000	VHLP1-23	47	19.099	1.1082	0.0166	37871
165.000	Site Pro RMQP-496-HK	47	16.766	1.0566	0.0129	12623
155.000	Site Pro SNP8HR-3xx	47	14.527	0.9990	0.0096	7574

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	180 - 142.5	91.144	8	5.0920	0.0821
L2	146.75 - 93.25	57.528	8	4.2459	0.0327
L3	99.5 - 46	24.155	8	2.4477	0.0100
L4	54.25 - 1	6.811	8	1.1821	0.0035

### Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
180.000	Lightning Rod 5/8x4'	8	91.144	5.0920	0.0821	8554
175.000	VHLP1-23	8	85.833	4.9812	0.0736	8554
165.000	Site Pro RMQP-496-HK	8	75.354	4.7504	0.0573	2850
155.000	Site Pro SNP8HR-3xx	8	65.301	4.4923	0.0427	1708

### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio P <sub>u</sub> /φP <sub>n</sub>
L1	180 - 142.5 (1)	TP30.28x18.75x0.25	37.500	0.000	0.0	22.7919	-14.169	1333.330	0.011
L2	142.5 - 93.25 (2)	TP44.93x28.4733x0.375	53.500	0.000	0.0	50.7433	-23.635	2968.480	0.008
L3	93.25 - 46 (3)	TP58.7x42.2575x0.4375	53.500	0.000	0.0	77.3839	-38.432	4526.960	0.008
L4	46 - 1 (4)	TP71.67x55.2895x0.4375	53.250	0.000	0.0	98.9152	-61.336	5786.540	0.011

### Pole Bending Design Data

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Section No.	Elevation ft	Size	$M_{ux}$ kip-ft	$\phi M_{rx}$ kip-ft	Ratio $\frac{M_{ux}}{\phi M_{rx}}$	$M_{uy}$ kip-ft	$\phi M_{ry}$ kip-ft	Ratio $\frac{M_{uy}}{\phi M_{ry}}$
L1	180 - 142.5 (1)	TP30.28x18.75x0.25	427.741	949.625	0.450	0.000	949.625	0.000
L2	142.5 - 93.25 (2)	TP44.93x28.4733x0.375	1530.625	3147.725	0.486	0.000	3147.725	0.000
L3	93.25 - 46 (3)	TP58.7x42.2575x0.4375	2843.825	6054.425	0.470	0.000	6054.425	0.000
L4	46 - 1 (4)	TP71.67x55.2895x0.4375	4739.667	8950.833	0.530	0.000	8950.833	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual $V_u$ K	$\phi V_n$ K	Ratio $\frac{V_u}{\phi V_n}$	Actual $T_u$ kip-ft	$\phi T_n$ kip-ft	Ratio $\frac{T_u}{\phi T_n}$
L1	180 - 142.5 (1)	TP30.28x18.75x0.25	20.860	399.998	0.052	8.522	1006.167	0.008
L2	142.5 - 93.25 (2)	TP44.93x28.4733x0.375	26.036	890.545	0.029	8.498	3324.883	0.003
L3	93.25 - 46 (3)	TP58.7x42.2575x0.4375	32.056	1358.090	0.024	8.486	6627.859	0.001
L4	46 - 1 (4)	TP71.67x55.2895x0.4375	38.878	1735.960	0.022	8.482	10829.250	0.001

### Pole Interaction Design Data

Section No.	Elevation ft	Ratio $P_u$	Ratio $M_{ux}$	Ratio $M_{uy}$	Ratio $V_u$	Ratio $T_u$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
		$\phi P_n$	$\phi M_{rx}$	$\phi M_{ry}$	$\phi V_n$	$\phi T_n$			
L1	180 - 142.5 (1)	0.011	0.450	0.000	0.052	0.008	0.465	1.000	✓
L2	142.5 - 93.25 (2)	0.008	0.486	0.000	0.029	0.003	0.495	1.000	✓
L3	93.25 - 46 (3)	0.008	0.470	0.000	0.024	0.001	0.479	1.000	✓
L4	46 - 1 (4)	0.011	0.530	0.000	0.022	0.001	0.541	1.000	✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail
L1	180 - 142.5	Pole	TP30.28x18.75x0.25	1	-14.169	1333.330	46.5	Pass
L2	142.5 - 93.25	Pole	TP44.93x28.4733x0.375	2	-23.635	2968.480	49.5	Pass
L3	93.25 - 46	Pole	TP58.7x42.2575x0.4375	3	-38.432	4526.960	47.9	Pass
L4	46 - 1	Pole	TP71.67x55.2895x0.4375	4	-61.336	5786.540	54.1	Pass
Summary								
Pole (L4)							54.1	Pass
RATING =							54.1	Pass

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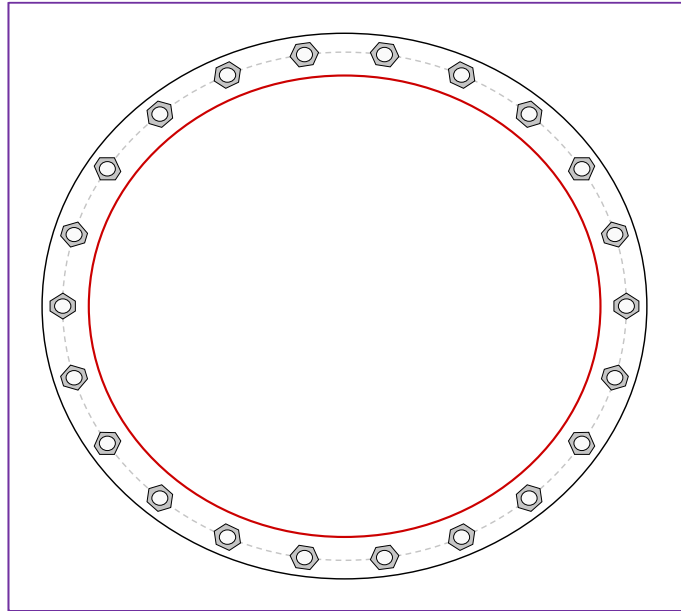


# Monopole Base Plate Connection

Site Info	
Site Number	US-CT-5017

Analysis Considerations	
TIA-222 Revision	H
Grout Considered:	No
$I_{gr}$ (in)	0

Applied Loads	
Moment (kip-ft)	4739.67
Axial Force (kips)	61.34
Shear Force (kips)	38.88



## Connection Properties Analysis Results

Anchor Rod Data	
(22) 2-1/4" $\phi$ bolts (A615-75 N; $F_y=75$ ksi, $F_u=100$ ksi) on 79" BC	
Base Plate Data	
84.75" OD x 2.25" Plate (A572-50; $F_y=50$ ksi, $F_u=65$ ksi)	
Stiffener Data	
N/A	
Pole Data	
71.67" x 0.4375" 18-sided pole (A572-65; $F_y=65$ ksi, $F_u=80$ ksi)	

Anchor Rod Summary <span style="float: right;">(units of kips, kip-in)</span>		
$Pu\_t = 128.07$	$\phi Pn\_t = 243.75$	<b>Stress Rating</b>
$Vu = 1.77$	$\phi Vn = 149.1$	<b>52.5%</b>
$Mu = n/a$	$\phi Mn = n/a$	<b>Pass</b>
Base Plate Summary		
Max Stress (ksi):	24.25	(Flexural)
Allowable Stress (ksi):	45	
Stress Rating:	<b>53.9%</b>	<b>Pass</b>

# Pier and Pad Foundation

Site Number: **US-CT-5017**

TIA-222 Revision: **H**  
 Tower Type: **Monopole**

Top & Bot. Pad Rein. Different?:   
 Block Foundation?:   
 Rectangular Pad?:

Superstructure Analysis Reactions		
Compression, <b>P<sub>comp</sub></b> :	61.35	kips
Base Shear, <b>V<sub>u_comp</sub></b> :	38.85	kips
Moment, <b>M<sub>u</sub></b> :	4739.67	ft-kips
Tower Height, <b>H</b> :	180	ft
BP Dist. Above Fdn, <b>bp<sub>dist</sub></b> :		in

Foundation Analysis Checks				
	Capacity	Demand	Rating	Check
<i>Lateral (Sliding) (kips)</i>	323.55	38.85	12.0%	Pass
<i>Bearing Pressure (ksf)</i>	23.09	1.91	8.3%	Pass
<i>Overturning (kip*ft)</i>	9939.69	4992.20	50.2%	Pass
<i>Pier Flexure (Comp.) (kip*ft)</i>	9329.85	4914.50	52.7%	Pass
<i>Pier Compression (kip)</i>	35992.10	102.07	0.3%	Pass
<i>Pad Flexure (kip*ft)</i>	5226.35	1721.84	32.9%	Pass
<i>Pad Shear - 1-way (kips)</i>	687.76	248.06	36.1%	Pass
<i>Pad Shear - 2-way (Comp) (ksi)</i>	0.201	0.080	39.7%	Pass
<i>Flexural 2-way (Comp) (kip*ft)</i>	4982.71	2948.70	59.2%	Pass

Pier Properties		
Pier Shape:	Circular	
Pier Diameter, <b>dpier</b> :	8	ft
Ext. Above Grade, <b>E</b> :	0.5	ft
Pier Rebar Size, <b>Sc</b> :	9	
Pier Rebar Quantity, <b>mc</b> :	50	
Pier Tie/Spiral Size, <b>St</b> :	5	
Pier Tie/Spiral Quantity, <b>mt</b> :	8	
Pier Reinforcement Type:	Tie	
Pier Clear Cover, <b>cc<sub>pier</sub></b> :	3	in

Structural Rating: **59.2%**  
 Soil Rating: **50.2%**

Pad Properties		
Depth, <b>D</b> :	6	ft
Pad Width, <b>W<sub>1</sub></b> :	29.5	ft
Pad Thickness, <b>T</b> :	2	ft
Pad Rebar Size (Bottom dir. 2), <b>Sp<sub>2</sub></b> :	9	
Pad Rebar Quantity (Bottom dir. 2), <b>mp<sub>2</sub></b> :	65	
Pad Clear Cover, <b>cc<sub>pad</sub></b> :	3	in

Material Properties		
Rebar Grade, <b>Fy</b> :	60	ksi
Concrete Compressive Strength, <b>F'c</b> :	4.5	ksi
Dry Concrete Density, <b>δc</b> :	150	pcf

Soil Properties		
Total Soil Unit Weight, <b>γ</b> :	130	pcf
Ultimate Net Bearing, <b>Qnet</b> :	30.000	ksf
Cohesion, <b>Cu</b> :	0.000	ksf
Friction Angle, <b>φ</b> :	40	degrees
SPT Blow Count, <b>N<sub>blows</sub></b> :		
Base Friction, <b>μ</b> :	0.35	
Neglected Depth, <b>N</b> :	3.33	ft
Foundation Bearing on Rock?	No	
Groundwater Depth, <b>gw</b> :	7.5	ft

<--Toggle between Gross and Net

Site: **US-CT-5017**

Structure: **A**

Location			
Decimal Degrees	Deg	Min	Sec
Lat: <input type="text"/>	+	<input type="text"/>	<input type="text"/>
Long: <input type="text"/>	-	<input type="text"/>	<input type="text"/>

Code and Site Parameters	
Seismic Design Code:	<b>TIA-222-H</b>
Site Soil:	<b>D (Default)</b> Default
Risk Category:	<b>II</b>
<u>USGS Seismic Reference</u>	
S <sub>S</sub> :	<b>0.1730</b> g
S <sub>1</sub> :	<b>0.0550</b> g
T <sub>L</sub> :	<b>6</b> s

Seismic Design Category Determination	
Importance Factor, I <sub>e</sub> :	<b>1</b>
Acceleration-based site coefficient, F <sub>a</sub> :	<b>1.6000</b>
Velocity-based site coefficient, F <sub>v</sub> :	<b>2.4000</b>
Design spectral response acceleration short period, S <sub>D5</sub> :	<b>0.1845</b> g
Design spectral response acceleration 1 s period, S <sub>D1</sub> :	<b>0.0880</b> g
Seismic Design Category Based on S <sub>D5</sub> :	<b>B</b>
Seismic Design Category Based on S <sub>D1</sub> :	<b>B</b>
Seismic Design Category Based on S <sub>1</sub> :	<b>N/A</b>
Controlling Seismic Design Category:	<b>B</b>

Site:

Structure:

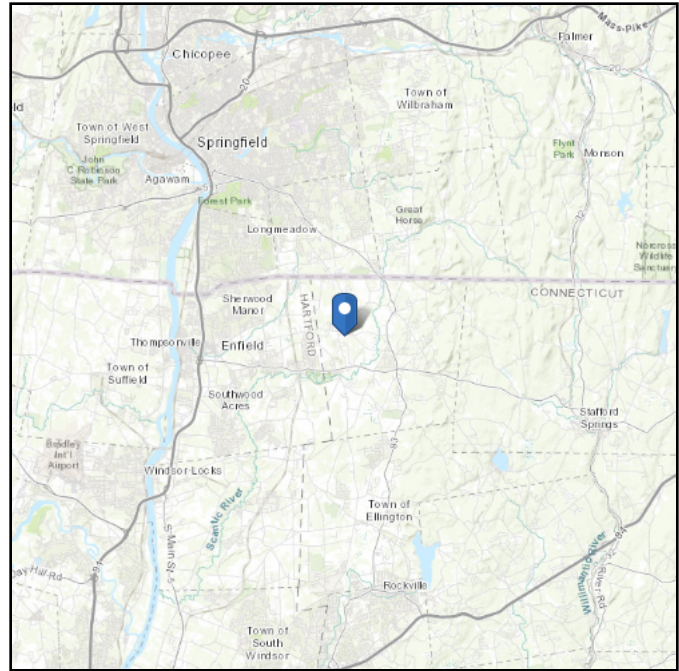
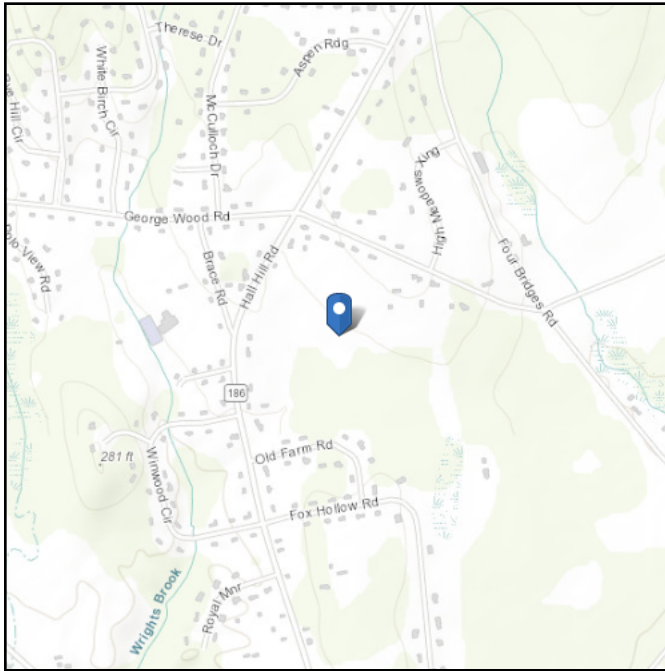
Tower Details		
Tower Type:	<input type="text" value="Tapered Monopole"/>	
Height, h:	<input type="text" value="179"/>	ft
Effective Seismic Weight, W:	<input type="text" value="51.13"/>	kips
Amplification Factor, A <sub>s</sub> :	<input style="background-color: yellow;" type="text" value="1.0"/>	2.7.8.1
Seismic Base Shear		
Response Modification Factor, R:	<input type="text" value="1.5"/>	
Discrete Appurtenance Weight in Top 1/3 of Structure, W <sub>u</sub> :	<input type="text" value="10.708"/>	kips
W <sub>L</sub> :	<input type="text" value="40.41810476"/>	kips
E:	<input style="background-color: yellow;" type="text" value="29000.0"/>	ksi
g:	<input type="text" value="386.088"/>	in/s <sup>2</sup>
Average Moment of Inertia, I <sub>avg</sub> :	<input type="text" value="20507.84597"/>	in <sup>4</sup>
F <sub>a</sub> :	<input type="text" value="0.294886361"/>	hz
Approximate Fundamental Period Monopole, T <sub>a</sub> :	<input type="text" value="3.3911"/>	s
		2.7.7.1.3.3
Seismic Response Coefficient, C <sub>s</sub>	<input type="text" value="0.1230"/>	2.7.7.1.1
Seismic Response Coefficient Max 1, C <sub>smax</sub>	<input type="text" value="0.0173"/>	2.7.7.1.1
Seismic Response Coefficient Max 2, C <sub>smax</sub>	<input type="text" value="N/A"/>	2.7.7.1.1
Seismic Response Coefficient Min 1, C <sub>smin</sub>	<input type="text" value="0.0300"/>	2.7.7.1.1
Seismic Response Coefficient Min 2, C <sub>smin</sub>	<input type="text" value="N/A"/>	2.7.7.1.1
Controlling Seismic Response Coefficient, C <sub>sc</sub>	<input type="text" value="0.0300"/>	
Seismic Base Shear, V	<input style="background-color: #00b050;" type="text" value="1.534"/>	kips
		2.7.7.1.1
Vertical Distribution Factors		
Period Related Exponent, k:	<input type="text" value="2.000"/>	2.7.7.1.2
Sum of w <sub>i</sub> h <sub>i</sub> <sup>k</sup>	<input type="text" value="562886.21"/>	2.7.7.1.2

# ASCE Hazards Report

**Address:**  
No Address at This Location

**Standard:** ASCE/SEI 7-16  
**Risk Category:** II  
**Soil Class:** D - Default (see Section 11.4.3)

**Latitude:** 42.002594  
**Longitude:** -72.484997  
**Elevation:** 230.68659061359796 ft (NAVD 88)



## Wind

### Results:

Wind Speed	120 mph
10-year MRI	75 Vmph
25-year MRI	83 Vmph
50-year MRI	90 Vmph
100-year MRI	97 Vmph

**Data Source:** ASCE/SEI 7-16, Fig. 26.5-1B and Figs. CC.2-1–CC.2-4, and Section 26.5.2  
**Date Accessed:** Thu May 23 2024

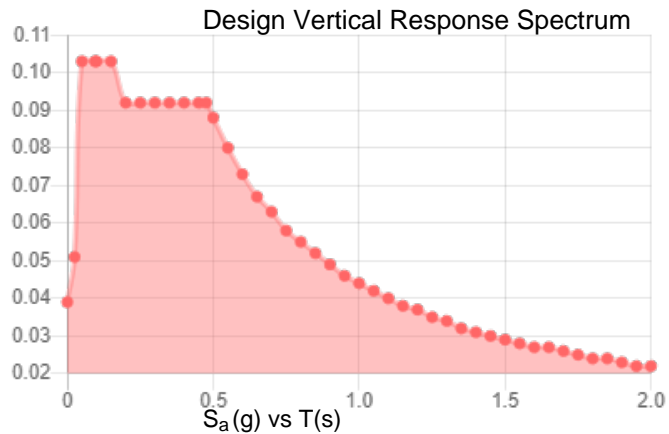
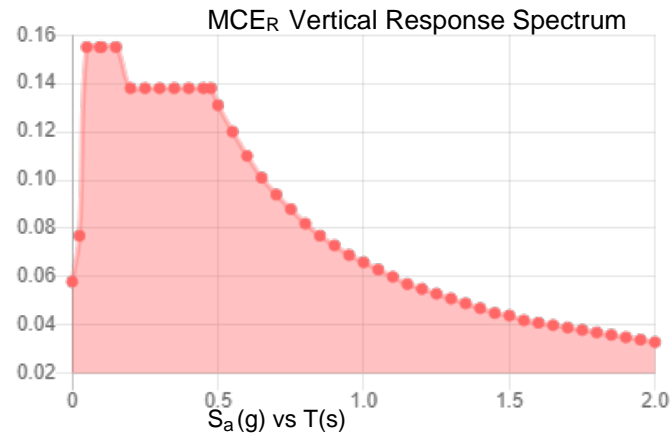
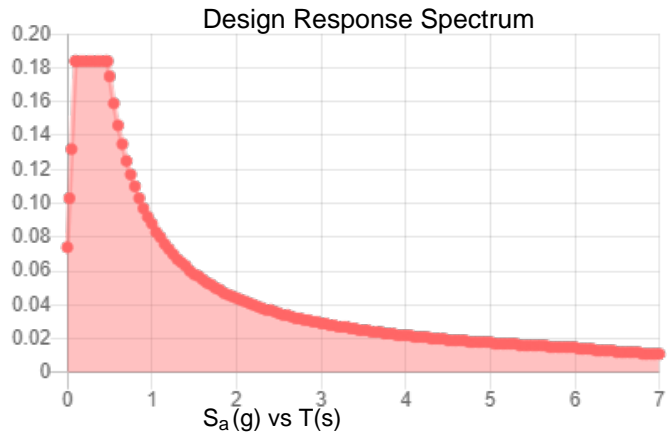
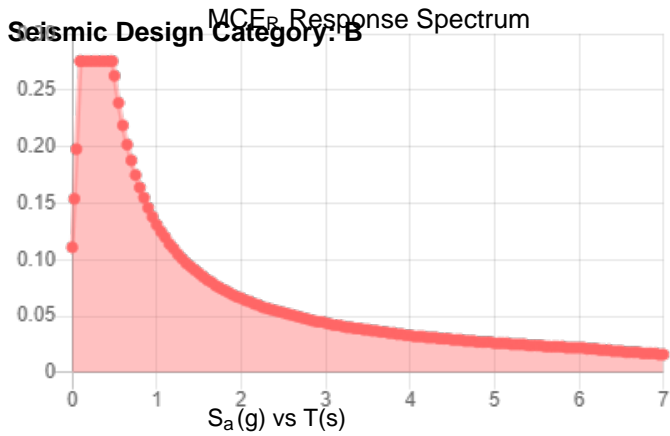
Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-16 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-16 Section 26.2. Glazed openings need not be protected against wind-borne debris.

**Site Soil Class:** D - Default (see Section 11.4.3)

**Results:**

$S_s$ :	0.173	$S_{D1}$ :	0.088
$S_1$ :	0.055	$T_L$ :	6
$F_a$ :	1.6	PGA :	0.091
$F_v$ :	2.4	PGA <sub>M</sub> :	0.145
$S_{MS}$ :	0.276	$F_{PGA}$ :	1.6
$S_{M1}$ :	0.131	$I_e$ :	1
$S_{DS}$ :	0.184	$C_v$ :	0.7



**Data Accessed:** Thu May 23 2024

**Date Source:**

**USGS Seismic Design Maps based on ASCE/SEI 7-16 and ASCE/SEI 7-16 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-16 Ch. 21 are available from USGS.**

## Ice

---

**Results:**

Ice Thickness: 1.50 in.  
Concurrent Temperature: 5 F  
Gust Speed 50 mph

**Data Source:** Standard ASCE/SEI 7-16, Figs. 10-2 through 10-8

**Date Accessed:** Thu May 23 2024

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 500-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

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The ASCE Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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## Attachment 2: Collocation Application





COLOCATION APPLICATION - P-049077  
 US-CT-5017  
 Version 2  
 T-Mobile Northeast LLC

Vertical Bridge REIT, LLC.  
 750 Park of Commerce Dr, ste 200  
 Boca Raton, FL 33487

## SUMMARY

### PRIMARY INFO

**Application #:** P-049077  
**Application Version:** 2 (Submitted: 4/30/2024 4:25:00 PM)  
**Application Type:** Broadband  
**Application Name:** CTHA027A amendment 6  
**Lease Type:** Amendment  
**ASR Number:**  
**Description:** Swapping (3) Antenna, Swapping (6) RRU

### VERTICAL BRIDGE SITE INFO

**VB Site #:** US-CT-5017  
**VB Site Name:** Blue Ridge  
**Latitude:** 42.00259444  
**Longitude:** -72.48499722  
**Structure Type:** Monopole  
**Structure Height:** 181.0000  
**Site Address:** 248 Hall Hill Road - Somers, CT 06071

### VERTICAL BRIDGE DEAL TEAM

**RLM:** Floyd Jenkins  
 Floyd.Jenkins@verticalbridge.com  
 (301) 667-0069

**LPM:** Sam Bowden  
 Sam.Bowden@verticalbridge.com

**ROM:** Joe Bascelli  
 Joe.Bascelli@verticalbridge.com  
 (484) 288-9586

### TENANT LEGAL INFO

**Tenant Legal Name:** T-Mobile Northeast LLC  
**State of Registration:** Delaware  
**Type of Entity:** LLC  
**Carrier NOC #:** 8776115868  
**Tenant Site #:** CTHA027B  
**Tenant Site Name:** ROMANO

### APPLICANT

**Name:** Phillip Sipe  
**Address:** 5 Melrose Drive  
 Farmington, CT 06032  
**Phone Number:** (860) 305-3084  
**Email Address:** phillip@northeastsitesolutions.com

## FINAL LEASED RIGHTS CONFIGURATION TOTALS

This is a summary of your remaining existing equipment plus the new equipment.

### FINAL EQUIPMENT

QTY	Equipment Type
1	Microwave Dish
9	RRU
12	Panel

### FINAL LINES

QTY	Line Type
3	Hybrid

## FREQUENCY & TECHNOLOGY INFO



COLOCATION APPLICATION - P-049077  
 US-CT-5017  
 Version 2  
 T-Mobile Northeast LLC

Vertical Bridge REIT, LLC.  
 750 Park of Commerce Dr, ste 200  
 Boca Raton, FL 33487

<b>Type of Tehnology:</b>	Broadband Wireless
<b>Is TX Frequency Licensed:</b>	Yes
<b>TX Frequency:</b>	668.000 - 678.000MHZ - 728.000 - 734.000MHZ - 1935.000 -1990.000MHZ 2120.000 -2155.000MHZ - 1930.000 -1990.000MHZ - 2496.000 -2690.000MHZ
<b>Is RX Frequency Licensed:</b>	Yes
<b>RX Frequency:</b>	668.000 - 678.000MHZ - 728.000 - 734.000MHZ - 1935.000 -1990.000MHZ 2120.000 -2155.000MHZ - 1930.000 -1990.000MHZ - 2496.000 -2690.000MHZ

## MOUNT & STRUCTURAL ANALYSIS

MOUNT ANALYSIS		STRUCTURAL HARD COPIES	
<b>Provided by Tenant:</b>	Yes	<b>Required:</b>	No
<b>To Be Run by VB:</b>		<b>Number of Hard Copies:</b>	
<b>Include Mount Mapping:</b>			

## CONTACTS

INVOICE CONTACT						
Attention To	Name	Address	Phone Number 1	Phone Number 2	Email 1	Email 2
Debbie Nichols	Debbie Nichols	5 Melrose Drive Farmington, CT 06032	(860) 543-4300		Dnichols @northeastsitesolutions.com	

PO CONTACT		
Name	Phone	Email
Debbie Nichols	(860) 543-4300	Dnichols@northeastsitesolutions.com

LEASING CONTACT		
Name	Phone	Email
Phillip Sipe	(860) 305-3841	Phillip@northeastsitesolutions.com

## LINE & EQUIPMENT

EXISTING LINE(S)					
Qty	Line Type	Line Diameter(In.)	Line Location	Comments	Remain
3	Hybrid	1.58	Interior		No

NEW LINE(S)					
Qty	Line Type	Line Diameter(In.)	Line Location	Comments	
3	Hybrid	1.58	Interior		



EXISTING EQUIPMENT											
Qty	Equipment Type	Mount RAD Height	Equipment RAD Height (H')	Mount Type	Manufacturer	Model Number	Dimensions (H"xW"xD")	Weight (Lbs.)	Azimuth	Comments	Remain
3	Panel	175.00	175.00	Platform (Handrail)	RFS - Andrews	APXVAALL24-U- NA20	495.90 x 24.00 x 8.50	122.00	340/90/210		Yes
3	Panel	175.00	175.00	Platform (Handrail)	RFS - Andrews	APXV18-206516s- C-A20	53.10 x 6.90 x 3.15	18.70	340/90/210		No
3	RRU	175.00	175.00	Platform (Handrail)	Ericsson	Radio 2217 B66A	13.81 x 11.70 x 5.03	26.40	340/90/210		No
3	RRU	175.00	175.00	Platform (Handrail)	Ericsson	Radio 4480 B71+B85	21.60 x 15.70 x 5.70	70.54	340/90/210		Yes

NEW EQUIPMENT											
Qty	Equipment Type	Mount RAD Height	Equipment RAD Height (H')	Mount Type	Manufacturer	Model Number	Dimensions (H"xW"xD")	Weight (Lbs.)	Azimuth	Comments	
3	Panel	175.00	175.00	Platform (Handrail)	Ericsson	AIR 6419 B41	36.30 x 20.90 x 9.00	83.30	340/90/210		
3	Panel	175.00	175.00	Platform (Handrail)	RFS - Andrews	APX18-206513- C-A20	54.80 x 6.90 x 4.30	35.00	340/90/210	This antenna is shown to reflect reserved loading	
1	Microwave Dish	175.00	175.00	Platform (Handrail)	Commscope	VHLP1- 23-CR4B	13.80 x 15.70 x	15.00	TBD		
3	RRU	175.00	175.00	Platform (Handrail)	Ericsson	Radio 4460 B25+B66	19.60 x 15.70 x 12.10	109.00	340/90/210		
3	Panel	175.00	175.00	Platform (Handrail)	RFS	APXVAALL24-U- NA20	496.00 x 24.00 x 8.50	56.00	340/90/210		
3	RRU	175.00	175.00	Platform (Handrail)	Ericsson	Radio 4480 B71+B85	21.65 x 15.74 x 5.70	70.54	340/90/210		

NEW EQUIPMENT CABINET(S)			
Qty of Cabinets	Cabinet Dimensions (H x W x D)	Manufacturer	Comments
1	63.00 x 25.60 x 25.60	Ericsson	B160
1	63.00 x 25.60 x 33.50	Ericsson	6160

## ADDITIONAL SITE REQUIREMENTS

GROUND & INTERIOR SPACE REQUIREMENTS						
Requirement Type	Total Lease Area (L x W)	Cabinet Required	Cabinet Area (L x W)	Shelter Required	Shelter Pad (L x W)	Comments
Not Required						



COLOCATION APPLICATION - P-049077  
US-CT-5017  
Version 2  
T-Mobile Northeast LLC

Vertical Bridge REIT, LLC.  
750 Park of Commerce Dr, ste 200  
Boca Raton, FL 33487

### GENERATOR REQUIREMENTS

Requirement Type	Fuel Type	Kilowatt Size	Pad Dimensions (L x D)	Generator Manufacturer	Fuel Tank Manufacturer	Comments
Not Required						

### AC POWER REQUIREMENTS

Meter Type	Additional Details	Comments
Existing Tenant Meter		

### BACKHAUL REQUIREMENTS

Requirement Type	Cable Type	Number of Points of Entry	Riser Size (Inches)	Comments
Not Required				

# Exhibit E

## **Mount Analysis**

# ELEVATED ENGINEERING

## CTHA027B

248 Hall Hill Road, Somers, CT 06071

### Mount Analysis

February 26, 2024

<u>Item</u>	<u>Pass/Fail</u>	<u>Capacity</u>
Antenna Pipe – Alpha/Beta/Gamma	PASS	41.8%
Antenna Mounts – Alpha/Beta/Gamma	PASS	29.9%



**Nicholas D. Barile, PE**

**CT PE License No.: 28643**

Elevated Engineering Project No.: 24008-NSS

# ELEVATED ENGINEERING

## Summary

At the request of T-Mobile, ELEVATED ENGINEERING has performed a structural analysis of the antenna mounting system for the antenna equipment loading under the *2022 Connecticut Building Code, ASCE 7, ANSI/TIA-222-H, and AISC (LRFD14)*. Information pertaining to the antenna mounts was obtained from:

- Construction drawings by FORESITE dated 5/5/2022.
- Valmont Site Pro 1's ULPD12-4xx mount.
- RFDS Version-3 last modified 02/08/2024.

## Loading Criteria

Wind Factors			
	Basic Wind Speed; Vult	116	mph
	Risk Category	II	
	Exposure	C	
	Flat Terrain		
	Ground Elevation	242	ft
	Ice Thickness	3/4"	
	Wi	40	mph
Seismic Factors			
	Ss:	0.173	
	S1:	0.055	
Loading Combinations at (12) 30° Intervals			

## Discussion

The tower supporting the antenna mounts was not analyzed in this report.

## Conclusions

Per our analysis, the antenna mounting system can support the proposed loading under the *2022 Connecticut Building Code*.

## General Comments

If there are substantial modifications to be made or the assumptions made in this analysis are not accurate, ELEVATED ENGINEERING should be notified immediately to perform a revised analysis. This report is not a condition assessment and assumes good workmanship will be used and systems will be properly maintained.

## Limitations

All opinions and conclusions are considered accurate to a reasonable degree of engineering certainty based upon the evidence available at the time of this report. All opinions and conclusions are subject to revision based upon receipt of new or additional/updated information. All services are provided exercising a level of care and diligence equivalent to the standard and care of our profession. No other warranty or guarantee, expressed or implied, is offered. Our services are confidential in nature, and we will not release this report to any other party without the client's consent. The use of this engineering work is limited to the express purpose for which it was commissioned, and it may not be reused, copied, or distributed for any other purpose without the written consent of ELEVATED ENGINEERING.

# ELEVATED ENGINEERING

## Attachment A Final Equipment Configuration

### Final Alpha Sector Antenna Configuration

#### **Rad Center is 175'-0"**

- (1) RFS APXVAALL24-43-U-NA20 Antenna
- (1) Ericsson AIR6419 B41 Antenna
- (1) Ericsson Radio 4460 B25+B66 RRU
- (1) Ericsson Radio 4480 B71+B85 RRU

### Final Beta Sector Antenna Configuration

#### **Rad Center is 175'-0"**

- (1) RFS APXVAALL24-43-U-NA20 Antenna
- (1) Ericsson AIR6419 B41 Antenna
- (1) Ericsson Radio 4460 B25+B66 RRU
- (1) Ericsson Radio 4480 B71+B85 RRU

### Final Gamma Sector Antenna Configuration

#### **Rad Center is 175'-0"**

- (1) RFS APXVAALL24-43-U-NA20 Antenna
- (1) Ericsson AIR6419 B41 Antenna
- (1) Ericsson Radio 4460 B25+B66 RRU
- (1) Ericsson Radio 4480 B71+B85 RRU



**Wind Analysis F = qz x Gh x ( EPA ) per TIA-222-H**

$Kz=2.01 (Z/Zg)^{(2/\alpha)}$  = 1.424  
 Zg = 900 Table 2-4 Exposure C  
 Alpha (α) = 9.5 Table 2-4  
 Z= 175 ft  
 Terrain Category I  
 $Kzt = (1+KcKt/Kh)^2$  1.00 for Category I  
 Kc= 1.00 Table 2-4  
 Kt= 0.53 Table 2-5  
 $Kh=e^{(f * z/H)}$  = 0.000 for H=0  
 f= 2.00 Table 2-5  
 H =Height of Crest Surrounding Terrain 0.00 ft  
 Kz = 1.424  
 Kzt = 1.0  
 Kd = 0.95  
 Importance Factor Table 2-3 = I = 1.0 Use Class II  
 Zs = 442 ft  
 $Ke= e^{(-0.0000362xZs)}$  = 0.98  
 Vult = 120 mph  
 $qz=0.00256xKzxKztxKdxKsxKexV^{2xl}$  = 49.1 psf  
 Gh = 1.00  
**qz Gh = 49.1 psf**

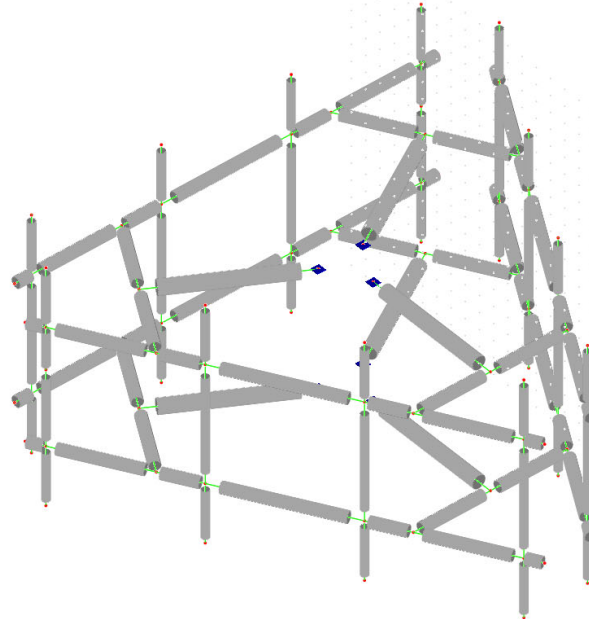
	Equipment Loading	CaAa (sf or sf/lf)	Wind (psf)	Ka	Wind Load (lb)	Weight (lb)
FN1	APXVAALL24-43-U-NA20	20.240	49.1	0.9	893.9	153.3
FN2	AIR6419	6.320	49.1	0.9	279.1	83.3
FN3	RRU 4460 B25 +B66	1.98	49.1	0.9	87.4	109
FN4	RRU 4480 B71+B85	2.850	49.1	0.9	125.9	84
FN5						
	2" Std. Pipe	0.238	49.1	0.9	10.5	
	3" Std. Pipe	0.3500	49.1	0.9	15.5	
	4" Std. Pipe	0.4500	49.1	0.9	19.9	
FT1	APXVAALL24-43-U-NA20	8.89	49.1	0.9	392.6	153.3
FT2	AIR6419	2.88	49.1	0.9	127.2	83.3
FT3	RRU 4460 B25 +B66	1.98	49.1	0.9	87.4	109
FT4	RRU 4480 B71+B85	1.380	49.1	0.9	60.9	84
FT5						

Company/Project: Elavated Engineering / 24008-NSS

**VersaFrame V9.0 (609.0)**  
(C) Digital Canal Corp.

Engineer:

Date/Time: 02/23/24 11:46:04



**Note:**

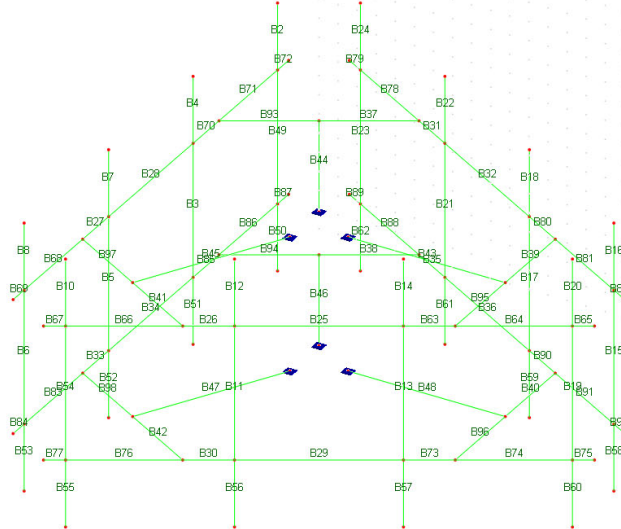


Company/Project: Elavated Engineering / 24008-NSS

**VersaFrame V9.0 (609.0)**  
(C) Digital Canal Corp.

Engineer:

Date/Time: 02/23/24 12:14:10



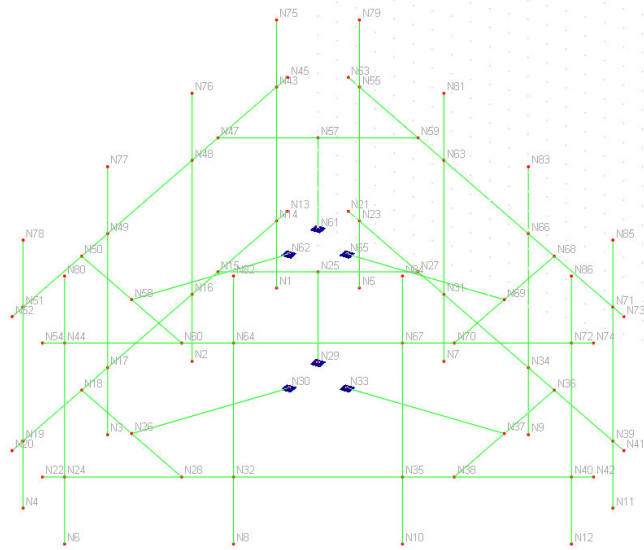
**Note:**

Company/Project: Elavated Engineering / 24008-NSS

**VersaFrame V9.0 (609.0)**  
(C) Digital Canal Corp.

Engineer:

Date/Time: 02/23/24 12:13:50



**Note:**

# Steel Check Report

Project:: 24008-NSS  
 Description: Antenna Mount  
 Date: 02/26/2024 11:35 AM

Company: Elevated Engineering  
 User:  
 Software: Digital Canal VersaFrame

## Code Check Results (LRFD14)

### CRITICAL STRESS SUMMARY

ID	Section Name	Status	Governing Criteria	Stress Ratio	Load Combination	Distance (ft)
2	Pipe2STD	OK	Axial-Bending	0.2331	TIA-222-H_240	0.0000
3	Pipe2STD	OK	Axial-Bending	0.1425	1.4Dead	3.5000
4	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_180	0.0000
5	Pipe2STD	OK	Axial-Bending	0.1358	1.4Dead	3.5000
6	Pipe2STD	OK	Axial-Bending	0.1699	TIA-222-H_150	3.5000
7	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_0	0.0000
8	Pipe2STD	OK	Axial-Bending	0.0410	TIA-222-H_300	0.0000
10	Pipe2STD	OK	Axial-Bending	0.2287	TIA-222-H_60	0.0000
11	Pipe2STD	OK	Axial-Bending	0.1107	TIA-222-H_330	0.0000
12	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_0	0.0000
13	Pipe2STD	OK	Axial-Bending	0.1393	1.2D+1.5Lm+1.0Wm	3.5000
14	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_0	0.0000
15	Pipe2STD	OK	Axial-Bending	0.4184	1.2D+1.5Lm+1.0Wm	3.5000
16	Pipe2STD	OK	Axial-Bending	0.2331	TIA-222-H_150	0.0000
17	Pipe2STD	OK	Axial-Bending	0.2702	1.2D+1.5Lm+1.0Wm	3.5000
18	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_270	0.0000
19	Pipe2STD	OK	Axial-Bending	0.2010	1.2D+1.5Lm+1.0Wm	3.5000
20	Pipe2STD	OK	Axial-Bending	0.0410	TIA-222-H_60	0.0000
21	Pipe2STD	OK	Axial-Bending	0.1251	1.2D+1.5Lv	0.0000
22	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_270	0.0000
23	Pipe2STD	OK	Axial-Bending	0.1838	TIA-222-H_60	3.5000
24	Pipe2STD	OK	Axial-Bending	0.0410	TIA-222-H_210	0.0000
25	Pipe3STD	OK	Axial-Bending	0.0667	TIA-222-H_150	0.0000
26	Pipe3STD	OK	Axial-Bending	0.1149	TIA-222-H_270	1.1753
27	Pipe3STD	OK	Axial-Bending	0.0960	TIA-222-H_150	1.1753
28	Pipe3STD	OK	Axial-Bending	0.0626	TIA-222-H_300	3.8333
29	Pipe3STD	OK	Axial-Bending	0.0800	TIA-222-H_300	0.0000
30	Pipe3STD	OK	Axial-Bending	0.1188	TIA-222-H_270	1.1753
31	Pipe3STD	OK	Axial-Bending	0.1096	TIA-222-H_0	1.1753
32	Pipe3STD	OK	Axial-Bending	0.0736	TIA-222-H_210	3.8333
33	Pipe3STD	OK	Axial-Bending	0.0942	TIA-222-H_300	1.1753
34	Pipe3STD	OK	Axial-Bending	0.0604	TIA-222-H_150	3.8333
35	Pipe3STD	OK	Axial-Bending	0.1100	TIA-222-H_180	1.1753
36	Pipe3STD	OK	Axial-Bending	0.0745	TIA-222-H_30	3.8333
37	Pipe3STD	OK	Axial-Bending	0.2085	TIA-222-H_180	2.2689
38	Pipe3STD	OK	Axial-Bending	0.2073	TIA-222-H_0	2.2689
39	Pipe3STD	OK	Axial-Bending	0.2091	TIA-222-H_150	2.2689
40	Pipe3STD	OK	Axial-Bending	0.2235	TIA-222-H_300	2.2689
41	Pipe3STD	OK	Axial-Bending	0.2164	TIA-222-H_0	2.2689
42	Pipe3STD	OK	Axial-Bending	0.2189	TIA-222-H_180	2.2689
43	Pipe4STD	OK	Axial-Bending	0.2988	TIA-222-H_120	0.0000
44	Pipe4STD	OK	Axial-Bending	0.2399	TIA-222-H_60	0.0000
45	Pipe4STD	OK	Axial-Bending	0.2420	TIA-222-H_240	0.0000
46	Pipe4STD	OK	Axial-Bending	0.2481	TIA-222-H_270	0.0000
47	Pipe4STD	OK	Axial-Bending	0.2428	TIA-222-H_60	0.0000
48	Pipe4STD	OK	Axial-Bending	0.2961	1.2D+1.5Lm+1.0Wm	0.0000
49	Pipe2STD	OK	Axial-Bending	0.2336	TIA-222-H_60	3.5000
50	Pipe2STD	OK	Axial-Bending	0.2327	TIA-222-H_240	0.0000
51	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_180	0.0000
52	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_0	0.0000
53	Pipe2STD	OK	Axial-Bending	0.0409	TIA-222-H_300	0.0000
54	Pipe2STD	OK	Axial-Bending	0.2105	TIA-222-H_150	3.5000
55	Pipe2STD	OK	Axial-Bending	0.2327	TIA-222-H_300	0.0000
56	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_0	0.0000

57	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_0	0.0000
58	Pipe2STD	OK	Axial-Bending	0.2327	TIA-222-H_30	0.0000
59	Pipe2STD	OK	Axial-Bending	0.0001	1.4Dead	0.0000
60	Pipe2STD	OK	Axial-Bending	0.0409	TIA-222-H_60	0.0000
61	Pipe2STD	OK	Axial-Bending	0.0087	TIA-222-H_270	0.0000
62	Pipe2STD	OK	Axial-Bending	0.0409	TIA-222-H_210	0.0000
63	Pipe3STD	OK	Axial-Bending	0.1085	TIA-222-H_270	1.1753
64	Pipe3STD	OK	Axial-Bending	0.1259	TIA-222-H_30	0.0000
65	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_210	0.0000
66	Pipe3STD	OK	Axial-Bending	0.2050	TIA-222-H_30	0.0000
67	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_30	0.0000
68	Pipe3STD	OK	Axial-Bending	0.1247	TIA-222-H_270	0.0000
69	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_270	0.0000
70	Pipe3STD	OK	Axial-Bending	0.1123	TIA-222-H_300	1.1753
71	Pipe3STD	OK	Axial-Bending	0.2707	TIA-222-H_270	0.0000
72	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_270	0.0000
73	Pipe3STD	OK	Axial-Bending	0.0965	TIA-222-H_150	1.1753
74	Pipe3STD	OK	Axial-Bending	0.1268	TIA-222-H_210	0.0000
75	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_210	0.0000
76	Pipe3STD	OK	Axial-Bending	0.2103	TIA-222-H_210	0.0000
77	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_30	0.0000
78	Pipe3STD	OK	Axial-Bending	0.1212	TIA-222-H_150	0.0000
79	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_0	0.0000
80	Pipe3STD	OK	Axial-Bending	0.1205	TIA-222-H_180	1.1753
81	Pipe3STD	OK	Axial-Bending	0.2449	TIA-222-H_150	0.0000
82	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_180	0.0000
83	Pipe3STD	OK	Axial-Bending	0.1134	TIA-222-H_60	0.0000
84	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_270	0.0000
85	Pipe3STD	OK	Axial-Bending	0.1074	TIA-222-H_150	1.1753
86	Pipe3STD	OK	Axial-Bending	0.2568	TIA-222-H_270	0.0000
87	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_270	0.0000
88	Pipe3STD	OK	Axial-Bending	0.1150	TIA-222-H_0	0.0000
89	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_0	0.0000
90	Pipe3STD	OK	Axial-Bending	0.1218	TIA-222-H_0	1.1753
91	Pipe3STD	OK	Axial-Bending	0.2425	TIA-222-H_0	0.0000
92	Pipe3STD	OK	Axial-Bending	0.0005	TIA-222-H_180	0.0000
93	Pipe3STD	OK	Axial-Bending	0.2343	TIA-222-H_240	0.0000
94	Pipe3STD	OK	Axial-Bending	0.2348	TIA-222-H_270	2.2689
95	Pipe3STD	OK	Axial-Bending	0.1947	TIA-222-H_60	0.0000
96	Pipe3STD	OK	Axial-Bending	0.1945	TIA-222-H_240	0.0000
97	Pipe3STD	OK	Axial-Bending	0.1992	TIA-222-H_300	0.0000
98	Pipe3STD	OK	Axial-Bending	0.1957	TIA-222-H_300	0.0000

### SELECTED LOAD COMBINATIONS

Load Combination	Code Check	Total	Live	Dependent	Conditional
TIA-222-H_0	x			-	-
TIA-222-H_30	x			-	-
TIA-222-H_60	x			-	-
TIA-222-H_90	x			-	-
TIA-222-H_120	x			-	-
TIA-222-H_150	x			-	-
TIA-222-H_180	x			-	-
TIA-222-H_210	x			-	-
TIA-222-H_240	x			-	-
TIA-222-H_270	x			-	-
TIA-222-H_300	x			-	-
TIA-222-H_330	x			-	-
1.2D+1.5Lv	x			-	-
1.2D+1.5Lm+1.0Wm	x			-	-
1.4Dead	x			-	-

## INPUT Contents

- General:
- Geometry: [[Nodes](#)] [[Supports](#)]
- Loads: [[Point Loads](#)] [[Line Loads](#)]

## OUTPUT Contents

- Nodal: [[Support Reactions](#)]
  - Members:
-



**Nodes**

Units: Coordinates X, Y, Z [in]

No.	X	Y	Z	No.	X	Y	Z
1	-52.86	-63.00	-69.00	2	-52.86	-63.00	-23.00
3	-52.86	-63.00	23.00	4	-52.86	-63.00	69.00
5	-33.33	-63.00	-80.28	6	-33.33	-63.00	80.28
7	6.51	-63.00	-57.28	8	6.51	-63.00	57.28
9	46.35	-63.00	-34.28	10	46.35	-63.00	34.28
11	86.19	-63.00	-11.28	12	86.19	-63.00	11.28
13	-52.86	-42.00	-75.00	14	-52.86	-42.00	-69.00
15	-52.86	-42.00	-37.10	16	-52.86	-42.00	-23.00
17	-52.86	-42.00	23.00	18	-52.86	-42.00	37.10
19	-52.86	-42.00	69.00	20	-52.86	-42.00	75.00
21	-38.52	-42.00	-83.28	22	-38.52	-42.00	83.28
23	-33.33	-42.00	-80.28	24	-33.33	-42.00	80.28
25	-29.28	-42.00	-50.72	26	-29.28	-42.00	50.72
27	-5.70	-42.00	-64.33	28	-5.70	-42.00	64.33
29	-4.59	-42.00	-7.96	30	-4.59	-42.00	7.96
31	6.51	-42.00	-57.28	32	6.51	-42.00	57.28
33	9.19	-42.00	-0.00	34	46.35	-42.00	-34.28
35	46.35	-42.00	34.28	36	58.56	-42.00	-27.23
37	58.56	-42.00	-0.00	38	58.56	-42.00	27.23
39	86.19	-42.00	-11.28	40	86.19	-42.00	11.28
41	91.38	-42.00	-8.28	42	91.38	-42.00	8.28
43	-52.86	0.00	-69.00	44	-33.33	0.00	80.28
45	-52.86	0.00	-75.00	47	-52.86	0.00	-37.10
48	-52.86	0.00	-23.00	49	-52.86	0.00	23.00
50	-52.86	0.00	37.10	51	-52.86	0.00	69.00
52	-52.86	0.00	75.00	53	-38.52	0.00	-83.28
54	-38.52	0.00	83.28	55	-33.33	0.00	-80.28
57	-29.28	0.00	-50.72	58	-29.28	0.00	50.72
59	-5.70	0.00	-64.33	60	-5.70	0.00	64.33
61	-4.59	0.00	-7.96	62	-4.59	0.00	7.96
63	6.51	0.00	-57.28	64	6.51	0.00	57.28
65	9.19	0.00	-0.00	66	46.35	0.00	-34.28
67	46.35	0.00	34.28	68	58.56	0.00	-27.23
69	58.56	0.00	-0.00	70	58.56	0.00	27.23
71	86.19	0.00	-11.28	72	86.19	0.00	11.28
73	91.38	0.00	-8.28	74	91.38	0.00	8.28
75	-52.86	21.00	-69.00	76	-52.86	21.00	-23.00
77	-52.86	21.00	23.00	78	-52.86	21.00	69.00
79	-33.33	21.00	-80.28	80	-33.33	21.00	80.28
81	6.51	21.00	-57.28	82	6.51	21.00	57.28
83	46.35	21.00	-34.28	84	46.35	21.00	34.28
85	86.19	21.00	-11.28	86	86.19	21.00	11.28

**Supports**

Units: Forced Displacements Dx, Dy, Dz [in]; Dox, Doy, Doz [rad]

Node	Flag	Dx	Dy	Dz	Dox	Doy	Doz
29	111111	0.000	0.000	0.000	0.000	0.000	0.000
30	111111	0.000	0.000	0.000	0.000	0.000	0.000
33	111111	0.000	0.000	0.000	0.000	0.000	0.000
61	111111	0.000	0.000	0.000	0.000	0.000	0.000
62	111111	0.000	0.000	0.000	0.000	0.000	0.000
65	111111	0.000	0.000	0.000	0.000	0.000	0.000

**Point Loads**

Units: Force [lb]; Moment [lb-ft]; Coord-Sys: Local=0, Global=1;  
 Direction: 0=X, 1=Y, 2=Z, 3=OX, 4=OY, 5=OZ

\*\*\*\*\* LOAD CASE - [ Lv ]\*\*\*\*\*

Member	Coord-Sys	Direction	Value	Distance
32	1	1	-250.000	0.5

\*\*\*\*\* LOAD CASE - [ Dead ]\*\*\*\*\*

Member	Coord-Sys	Direction	Value	Distance
2	1	1	-76.700	0.5
6	1	1	-109.000	0.5
8	1	1	-41.700	0.25
10	1	1	-76.700	0.5
15	1	1	-84.000	0.5
16	1	1	-76.700	0.5
19	1	1	-109.000	0.5
20	1	1	-41.700	0.25
23	1	1	-109.000	0.5
24	1	1	-41.700	0.25
49	1	1	-84.000	0.5
50	1	1	-76.700	0.5
53	1	1	-41.700	0.25
54	1	1	-84.000	0.5
55	1	1	-76.700	0.5
58	1	1	-76.700	0.5
60	1	1	-41.700	0.25
62	1	1	-41.700	0.25

\*\*\*\*\* LOAD CASE - [ Wind Normal ]\*\*\*\*\*

Member	Coord-Sys	Direction	Value	Distance
2	1	2	196.300	0.5
6	1	2	87.400	0.5
8	1	2	63.600	0.25
10	1	2	196.300	0.5
16	1	2	447.000	0.5
19	1	2	87.400	0.5
20	1	2	63.600	0.25
24	1	2	139.600	0.25
49	1	2	60.900	0.5
50	1	2	196.300	0.5
53	1	2	63.600	0.25
54	1	2	60.900	0.5
55	1	2	196.300	0.5
58	1	2	447.000	0.5
60	1	2	63.600	0.25
62	1	2	139.600	0.25

\*\*\*\*\* LOAD CASE - [ Wind Transverse ]\*\*\*\*\*

Member	Coord-Sys	Direction	Value	Distance
2	1	0	447.000	0.5
8	1	0	139.600	0.25
10	1	0	447.000	0.5
15	1	0	60.900	0.5
16	1	0	196.300	0.5
20	1	0	139.600	0.25
23	1	0	87.400	0.5
24	1	0	63.600	0.25
50	1	0	447.000	0.5
53	1	0	139.600	0.25
55	1	0	447.000	0.5
58	1	0	196.300	0.5
60	1	0	139.600	0.25
62	1	0	63.600	0.25

\*\*\*\*\* LOAD CASE - [ Lm ]\*\*\*\*\*

Member	Coord-Sys	Direction	Value	Distance
15	1	1	-500.000	0.5

**Line Loads**

Units: Force [lb/ft]; Coord-Sys: Local=0, Global=1; Direction: 0=X, 1=Y, 2=Z

\*\*\*\*\* LOAD CASE - [ Wind Normal ]\*\*\*\*\*

Member	Coord-Sys	Direction	Value1	Value2	Distance1	Distance2
2	1	2	10.500	10.500	0	1
3	1	2	10.500	10.500	0	1

4	1	2	10.500	10.500	0	1
5	1	2	10.500	10.500	0	1
6	1	2	10.500	10.500	0	1
7	1	2	10.500	10.500	0	1
8	1	2	10.500	10.500	0	1
11	1	2	10.500	10.500	0	1
12	1	2	10.500	10.500	0	1
13	1	2	10.500	10.500	0	1
14	1	2	10.500	10.500	0	1
19	1	2	10.500	10.500	0	1
20	1	2	10.500	10.500	0	1
25	1	2	15.500	15.500	0	1
26	1	2	15.500	15.500	0	1
27	1	2	15.500	15.500	0	1
28	1	2	15.500	15.500	0	1
29	1	2	15.500	15.500	0	1
30	1	2	15.500	15.500	0	1
31	1	2	15.500	15.500	0	1
32	1	2	15.500	15.500	0	1
33	1	2	15.500	15.500	0	1
34	1	2	15.500	15.500	0	1
35	1	2	15.500	15.500	0	1
36	1	2	15.500	15.500	0	1
37	1	2	15.500	15.500	0	1
38	1	2	15.500	15.500	0	1
39	1	2	15.500	15.500	0	1
40	1	2	15.500	15.500	0	1
41	1	2	15.500	15.500	0	1
42	1	2	15.500	15.500	0	1
43	1	2	19.900	19.900	0	1
44	1	2	19.900	19.900	0	1
45	1	2	19.900	19.900	0	1
46	1	2	19.900	19.900	0	1
47	1	2	19.900	19.900	0	1
49	1	2	10.500	10.500	0	1
50	1	2	10.500	10.500	0	1
51	1	2	10.500	10.500	0	1
52	1	2	10.500	10.500	0	1
53	1	2	10.500	10.500	0	1
54	1	2	10.500	10.500	0	1
55	1	2	10.500	10.500	0	1
56	1	2	10.500	10.500	0	1
57	1	2	10.500	10.500	0	1
60	1	2	10.500	10.500	0	1
63	1	2	15.500	15.500	0	1
64	1	2	15.500	15.500	0	1
65	1	2	15.500	15.500	0	1
66	1	2	15.500	15.500	0	1
67	1	2	15.500	15.500	0	1
68	1	2	15.500	15.500	0	1
69	1	2	15.500	15.500	0	1
70	1	2	15.500	15.500	0	1
71	1	2	15.500	15.500	0	1
72	1	2	15.500	15.500	0	1
73	1	2	15.500	15.500	0	1
74	1	2	15.500	15.500	0	1
75	1	2	15.500	15.500	0	1
76	1	2	15.500	15.500	0	1
77	1	2	15.500	15.500	0	1
78	1	2	15.500	15.500	0	1
79	1	2	15.500	15.500	0	1
80	1	2	15.500	15.500	0	1
81	1	2	15.500	15.500	0	1
82	1	2	15.500	15.500	0	1
83	1	2	15.500	15.500	0	1
84	1	2	15.500	15.500	0	1
85	1	2	15.500	15.500	0	1
86	1	2	15.500	15.500	0	1
87	1	2	15.500	15.500	0	1
88	1	2	15.500	15.500	0	1
89	1	2	15.500	15.500	0	1
90						

	1	2	15.500	15.500	0	1
91	1	2	15.500	15.500	0	1
92	1	2	15.500	15.500	0	1
93	1	2	15.500	15.500	0	1
94	1	2	15.500	15.500	0	1
95	1	2	15.500	15.500	0	1
96	1	2	15.500	15.500	0	1
97	1	2	15.500	15.500	0	1
98	1	2	15.500	15.500	0	1

\*\*\*\*\* LOAD CASE - [ Wind Transverse ]\*\*\*\*\*

Member	Coord-Sys	Direction	Value1	Value2	Distance1	Distance2
16	1	0	10.500	10.500	0	1
17	1	0	10.500	10.500	0	1
18	1	0	10.500	10.500	0	1
21	1	0	10.500	10.500	0	1
22	1	0	10.500	10.500	0	1
23	1	0	10.500	10.500	0	1
24	1	0	10.500	10.500	0	1
25	1	0	15.500	15.500	0	1
26	1	0	15.500	15.500	0	1
27	1	0	15.500	15.500	0	1
28	1	0	15.500	15.500	0	1
29	1	0	15.500	15.500	0	1
30	1	0	15.500	15.500	0	1
33	1	0	15.500	15.500	0	1
34	1	0	15.500	15.500	0	1
37	1	0	15.500	15.500	0	1
38	1	0	15.500	15.500	0	1
39	1	0	15.500	15.500	0	1
40	1	0	15.500	15.500	0	1
40	1	0	10.500	10.500	0	1
43	1	0	19.900	19.900	0	1
43	1	0	10.500	10.500	0	1
44	1	0	19.900	19.900	0	1
45	1	0	19.900	19.900	0	1
46	1	0	19.900	19.900	0	1
47	1	0	19.900	19.900	0	1
48	1	0	19.900	19.900	0	1
58	1	0	10.500	10.500	0	1
61	1	0	10.500	10.500	0	1
62	1	0	10.500	10.500	0	1
63	1	0	15.500	15.500	0	1
64	1	0	15.500	15.500	0	1
65	1	0	15.500	15.500	0	1
66	1	0	15.500	15.500	0	1
67	1	0	15.500	15.500	0	1
68	1	0	15.500	15.500	0	1
69	1	0	15.500	15.500	0	1
70	1	0	15.500	15.500	0	1
71	1	0	15.500	15.500	0	1
72	1	0	15.500	15.500	0	1
73	1	0	15.500	15.500	0	1
74	1	0	15.500	15.500	0	1
75	1	0	15.500	15.500	0	1
76	1	0	15.500	15.500	0	1
77	1	0	15.500	15.500	0	1
83	1	0	15.500	15.500	0	1
84	1	0	15.500	15.500	0	1
85	1	0	15.500	15.500	0	1
86	1	0	15.500	15.500	0	1
87	1	0	15.500	15.500	0	1
90	1	0	15.500	15.500	0	1
93	1	0	15.500	15.500	0	1
94	1	0	15.500	15.500	0	1
95	1	0	15.500	15.500	0	1
96	1	0	15.500	15.500	0	1

**Support Reactions**

Units: Force Reactions Rx, Ry, Rz [lb]; Moment Reactions Rox, Roy, Roz [lb-ft]

Load Combination 2: TIA-222-H 0

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	-484.530	498.869	-1014.517	1442.087	-44.910	-847.387
30	278.709	522.769	-959.847	-1506.891	-382.605	-847.010
33	207.195	477.480	-539.284	12.607	1260.524	1639.363
61	-448.084	518.519	-959.347	1493.118	-35.367	-883.167
62	307.522	497.079	-1000.763	-1445.139	-357.326	-825.590
65	139.188	540.197	-599.180	16.912	1342.381	1760.285

Load Combination 3: TIA-222-H 30

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	-789.638	480.622	-1080.722	1410.515	365.014	-823.819
30	-54.077	524.475	-683.889	-1502.298	-719.979	-848.272
33	-371.642	488.993	-412.455	15.558	932.164	1666.650
61	-752.355	536.318	-1023.763	1525.141	374.008	-907.518
62	-24.601	495.125	-727.518	-1452.621	-696.576	-826.340
65	-450.807	529.379	-464.815	14.552	1005.153	1730.446

Load Combination 4: TIA-222-H 60

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	-888.070	469.986	-865.018	1393.477	675.834	-810.700
30	-376.427	522.070	-217.007	-1491.646	-866.219	-846.553
33	-841.877	505.914	-175.230	18.322	352.855	1702.876
61	-850.355	546.872	-806.288	1541.023	684.498	-919.921
62	-345.774	496.936	-267.587	-1467.368	-848.327	-829.994
65	-928.982	513.133	-205.339	12.269	400.055	1692.454

Load Combination 5: TIA-222-H 90

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	717.727	548.432	368.179	1534.052	-813.306	-914.140
30	571.187	501.979	-257.112	-1481.469	771.162	-831.937
33	1144.184	494.566	-110.568	9.554	311.266	1661.701
61	751.655	471.013	421.981	1393.259	-802.321	-808.748
62	601.934	516.410	-316.089	-1474.081	780.559	-838.787
65	1099.552	522.513	-106.392	19.014	319.491	1743.566

Load Combination 6: TIA-222-H 120

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	307.052	529.721	544.177	1519.935	-99.809	-849.656
30	-117.905	503.717	472.123	-1468.672	206.809	-806.250
33	147.011	724.258	231.072	151.408	-585.345	2503.010
61	159.657	519.726	442.570	1494.518	138.988	-831.821
62	-175.306	516.514	508.242	-1499.594	163.295	-817.001
65	-320.509	693.977	338.285	149.272	-716.041	2442.757

Load Combination 7: TIA-222-H 150

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	18.760	498.312	627.040	1449.870	433.082	-850.610
30	-563.882	500.856	1029.632	-1455.198	-66.425	-831.199
33	-672.627	543.768	519.890	19.428	-1258.782	1771.603
61	54.890	520.214	686.979	1476.211	442.525	-872.402
62	-529.925	516.063	953.937	-1512.475	-69.791	-846.386
65	-750.336	475.700	575.686	10.987	-1310.567	1626.197

Load Combination 8: TIA-222-H 180

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	449.324	519.376	957.501	1487.568	33.917	-878.347
30	-310.137	495.461	1019.231	-1452.460	373.058	-827.277
33	-140.569	540.695	536.907	17.074	-1270.186	1760.551
61	484.442	499.839	1016.124	1436.599	43.981	-842.594
62	-276.158	521.291	941.293	-1514.268	367.408	-848.740
65	-206.903	478.251	601.881	12.799	-1332.425	1639.921

Load Combination 9: TIA-222-H 210

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	754.638	537.691	1023.719	1519.156	-375.387	-901.925

30	22.636	493.713	743.484	-1456.996	710.973	-825.991
33	438.081	529.172	409.859	14.127	-942.763	1733.287
61	788.921	481.969	1080.567	1404.572	-364.767	-818.231
62	55.943	523.290	668.258	-1506.820	707.180	-847.998
65	382.900	489.077	467.277	15.158	-996.148	1669.740

Load Combination 10: TIA-222-H 240

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	852.843	548.325	808.029	1536.165	-685.356	-915.022
30	345.234	496.096	276.303	-1467.608	856.596	-827.695
33	908.299	512.295	172.921	11.377	-364.029	1697.116
61	886.690	471.419	863.113	1388.712	-674.398	-805.846
62	377.357	521.507	208.015	-1492.118	858.310	-844.357
65	861.061	505.269	208.087	17.431	-391.624	1707.666

Load Combination 11: TIA-222-H 270

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	717.727	548.432	368.179	1534.052	-813.306	-914.140
30	571.187	501.979	-257.112	-1481.469	771.162	-831.937
33	1144.184	494.566	-110.568	9.554	311.266	1661.701
61	751.655	471.013	421.981	1393.259	-802.321	-808.748
62	601.934	516.410	-316.089	-1474.081	780.559	-838.787
65	1099.552	522.513	-106.392	19.014	319.491	1743.566

Load Combination 12: TIA-222-H 300

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	385.597	538.003	-177.985	1513.393	-724.962	-899.522
30	639.794	509.780	-713.596	-1494.859	477.919	-837.578
33	1082.359	480.718	-364.810	9.145	901.978	1636.527
61	420.104	480.833	-124.637	1416.989	-714.268	-826.153
62	669.340	509.370	-763.379	-1457.541	495.112	-832.780
65	1034.291	536.208	-392.061	19.485	946.447	1767.834

Load Combination 13: TIA-222-H 330

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	-474.654	491.052	-928.166	1419.046	26.623	-861.264
30	213.239	520.173	-796.897	-1501.963	-345.119	-860.709
33	68.364	366.649	-446.067	-65.307	1060.664	1201.677
61	-333.069	508.266	-781.191	1463.233	-95.947	-892.240
62	294.447	498.053	-900.980	-1448.488	-295.662	-842.158
65	231.672	420.719	-539.863	-61.570	1193.471	1306.402

Load Combination 14: 1.2D+1.5Lv

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	-1.631	608.435	-69.354	1785.823	-79.648	-926.260
30	7.242	501.493	-10.008	-1451.380	-4.905	-820.809
33	60.878	608.435	-35.800	120.445	69.838	2009.699
61	1.631	605.168	69.354	1769.908	79.648	-924.914
62	-7.242	501.214	10.008	-1450.780	4.905	-820.462
65	-60.878	605.168	35.800	113.653	-69.838	1995.242

Load Combination 15: 1.2D+1.5Lm+1.0Wm

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	140.275	535.990	109.328	1541.550	-203.118	-826.931
30	62.344	511.412	-61.144	-1483.957	34.540	-792.160
33	380.566	855.055	-64.806	249.466	85.735	3038.131
61	-140.275	535.990	-109.328	1541.550	203.118	-826.931
62	-62.344	511.412	61.144	-1483.957	-34.540	-792.160
65	-380.566	855.055	64.806	249.466	-85.735	3038.131

Load Combination 16: 1.4Dead

Node	Rx	Ry	Rz	Rox	Roy	Roz
29	-20.872	594.011	-33.194	1708.977	-5.723	-1006.682
30	-18.311	594.011	34.673	-1726.301	-5.723	-976.676
33	39.183	594.011	-1.479	17.324	-5.723	1983.359
61	20.872	594.011	33.194	1708.977	5.723	-1006.682
62	18.311	594.011	-34.673	-1726.301	5.723	-976.676
65	-39.183	594.011	1.479	17.324	5.723	1983.359

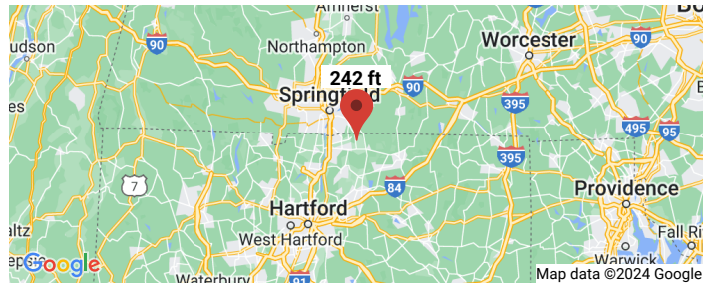
⚠ This is a beta release of the new ATC Hazards by Location website. Please [contact us](#) with feedback.

ℹ The ATC Hazards by Location website will not be updated to support ASCE 7-22. [Find out why.](#)

# ATC Hazards by Location

## Search Information

**Address:** 248 Hall Hill Road, Somers, CT 06071  
**Coordinates:** 42.0021997, -72.48819859999999  
**Elevation:** 242 ft  
**Timestamp:** 2024-02-23T16:35:10.310Z  
**Hazard Type:** Wind



### ASCE 7-16

MRI 10-Year ..... 74 mph  
MRI 25-Year ..... 83 mph  
MRI 50-Year ..... 89 mph  
MRI 100-Year ..... 96 mph  
Risk Category I ..... 107 mph  
Risk Category II ..... 116 mph  
Risk Category III ..... 125 mph  
Risk Category IV ..... ⚠ 130 mph

You are in a wind-borne debris region if you are also within 1 mile of the coastal mean high water line.

### ASCE 7-10

MRI 10-Year ..... 76 mph  
MRI 25-Year ..... 86 mph  
MRI 50-Year ..... 92 mph  
MRI 100-Year ..... 99 mph  
Risk Category I ..... 111 mph  
Risk Category II ..... 122 mph  
Risk Category III-IV ..... ⚠ 131 mph

If the structure under consideration is a healthcare facility and you are also within 1 mile of the coastal mean high water line, you are in a wind-borne debris region. If other occupancy, use the Risk Category II basic wind speed contours to determine if you are in a wind-borne debris region.

### ASCE 7-05

ASCE 7-05 Wind Speed ..... 97 mph

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

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## Disclaimer

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area – in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.

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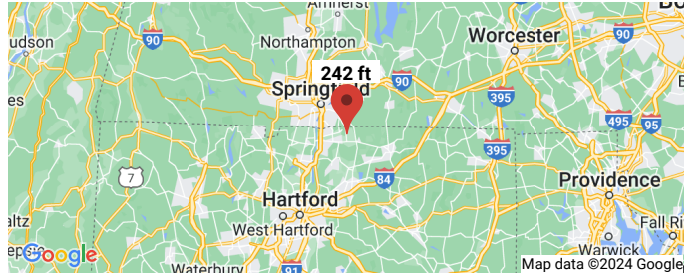
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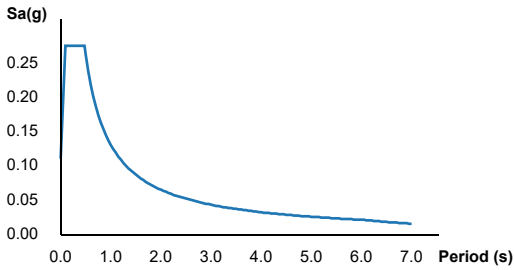
# ATC Hazards by Location

## Search Information

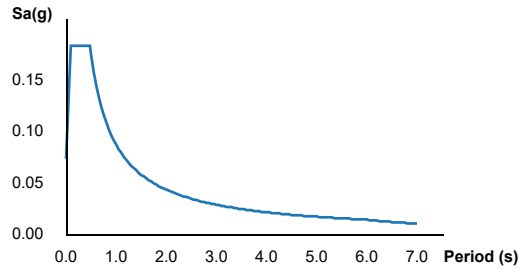
**Address:** 248 Hall Hill Road, Somers, CT 06071  
**Coordinates:** 42.0021997, -72.48819859999999  
**Elevation:** 242 ft  
**Timestamp:** 2024-02-23T16:36:20.684Z  
**Hazard Type:** Seismic  
**Reference Document:** ASCE7-16  
**Risk Category:** II  
**Site Class:** D



### MCER Horizontal Response Spectrum



### Design Horizontal Response Spectrum



## Basic Parameters

Name	Value	Description
$S_S$	0.173	MCE <sub>R</sub> ground motion (period=0.2s)
$S_1$	0.055	MCE <sub>R</sub> ground motion (period=1.0s)
$S_{MS}$	0.276	Site-modified spectral acceleration value
$S_{M1}$	0.131	Site-modified spectral acceleration value
$S_{DS}$	0.184	Numeric seismic design value at 0.2s SA
$S_{D1}$	0.088	Numeric seismic design value at 1.0s SA

## Additional Information

Name	Value	Description
SDC	B	Seismic design category
$F_a$	1.6	Site amplification factor at 0.2s
$F_v$	2.4	Site amplification factor at 1.0s
$CR_S$	0.935	Coefficient of risk (0.2s)
$CR_1$	0.917	Coefficient of risk (1.0s)
PGA	0.09	MCE <sub>G</sub> peak ground acceleration
$F_{PGA}$	1.6	Site amplification factor at PGA
$PGA_M$	0.145	Site modified peak ground acceleration
$T_L$	6	Long-period transition period (s)
$SsRT$	0.173	Probabilistic risk-targeted ground motion (0.2s)
$SsUH$	0.185	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
$SsD$	1.5	Factored deterministic acceleration value (0.2s)
$S1RT$	0.055	Probabilistic risk-targeted ground motion (1.0s)
$S1UH$	0.06	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)

S1D	0.6	Factored deterministic acceleration value (1.0s)
PGAd	0.5	Factored deterministic acceleration value (PGA)

*The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.*

*Please note that the ATC Hazards by Location website will not be updated to support ASCE 7-22. [Find out why.](#)*

## **Disclaimer**

Hazard loads are provided by the U.S. Geological Survey [Seismic Design Web Services](#).

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# Exhibit F

## **Power Density/RF Emissions Report**



FOX HILL TELECOM

## Radio Frequency Emissions Analysis Report

# T Mobile™

Site ID: CTHA027B

Romano  
248 Hall Hill Road  
Somers, CT 06071

June 5, 2024

Fox Hill Telecom Project Number: 240154

Site Compliance Summary	
Compliance Status:	COMPLIANT
Site total MPE% of FCC general population allowable limit:	7.17 %



June 5, 2024

T-MOBILE  
Attn: RF Manager  
35 Griffin Road South  
Bloomfield, CT 06009

## Emissions Analysis for Site: **CTHA027B – Romano**

Fox Hill Telecom, Inc (“Fox Hill”) was directed to analyze the proposed upgrades to the T-MOBILE facility located at **248 Hall Hill Road, Somers, CT**, for the purpose of determining whether the emissions from the Proposed T-MOBILE Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

General population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limits for the 600 MHz & 700 MHz bands are approximately  $400 \mu\text{W}/\text{cm}^2$  and  $467 \mu\text{W}/\text{cm}^2$  respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 2500 MHz (BRS) bands is  $1000 \mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



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Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.



## CALCULATIONS

Calculations were performed for the proposed upgrades to the T-MOBILE antenna facility located at **248 Hall Hill Road, Somers, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65 for far field modeling calculations.

In OET-65, plane wave power densities in the Far Field of an antenna are calculated by considering antenna gain and reflective waves that would contribute to exposure.

Since the radiation pattern of an antenna has developed in the **Far Field** region the power gain in specific directions needs to be considered in exposure predictions to yield an Effective Radiated Power (ERP) in each specific direction from the antenna. Also, since the vertical radiation pattern of the antenna is considered, the exposure calculations would most likely be reduced significantly at ground level, resulting in a more realistic estimate of the actual exposure levels. To determine a worst-case scenario at each point along the calculation radials, each point was calculated using the antenna gain value at each angle of incident and compared against the result using an isotropic radiator at the antenna height with the greater of the two used to yield the more pessimistic far field value for each point along the calculation radial.

Additionally, to model a truly "worst case" prediction of exposure levels at or near a surface, such as at ground-level or on a rooftop, reflection off the surface of antenna radiation power can be assumed, resulting in a potential 1.6 times increase in power density in calculating far field power density values.

With these factors Considered, the worst case **Far Field prediction model** utilized in this analysis is determined by the following equation:

Equation 9 per FCC OET65 for Far Field Modeling

$$S = \frac{33.4 ERP}{R^2}$$

S = Power Density (in  $\mu\text{w}/\text{cm}^2$ )

ERP = Effective Radiated Power from antenna (watts)

R = Distance from the antenna (meters)

Predicted far field power density values for all carriers identified in this report were calculated 6 feet above the ground level and are displayed as a percentage of the applicable FCC standards. All emissions values for other carriers were calculated using the same Far Field model outlined above, using industry standard radio configurations and frequency band selection based upon available licenses in this geographic area for emissions contribution estimates.



For each T-Mobile sector the following channel counts, frequency bands and power levels were utilized as shown in *Table 1*:

Technology	Frequency Band	Channel Count	Transmit Power per Channel (W)
LTE / 5G NR	600 MHz	4	40
LTE	700 MHz	2	20
LTE	1900 MHz (PCS)	4	35
5G	1900 MHz (PCS)	4	40
LTE	2100 MHz (AWS)	4	60
LTE / 5G NR	2500 MHz (BRS)	8	30

*Table 1: Channel Data Table*





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The following T-Mobile antennas listed in *Table 2* were used in the modeling for transmission in the 600 MHz, 700 MHz, 1900 MHz (PCS), 2100 MHz (AWS) and 2500 MHz (BRS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below.

Sector	Antenna Number	Antenna Make / Model	Antenna Centerline (ft)
A	1	RFS APXVAALL24_43-U-NA20	175
A	2	Ericsson AIR6419 B41	175
B	1	RFS APXVAALL24_43-U-NA20	175
B	2	Ericsson AIR6419 B41	175
C	1	RFS APXVAALL24_43-U-NA20	175
C	2	Ericsson AIR6419 B41	175

*Table 2: Antenna Data*

All calculations were done with respect to uncontrolled / general population threshold limits.



## RESULTS

Per the calculations completed for the proposed T-MOBILE configurations *Table 3* shows resulting emissions power levels and percentages of the FCC’s allowable general population limit.

Antenna ID	Antenna Make / Model	Frequency Bands	Antenna Gain (dBd)	Channel Count	Total TX Power (W)	ERP (W)	MPE %
Antenna A1	RFS APXVAALL24_43-U-NA20	600 MHz / 700 MHz / 1900 MHz (PCS) / 2100 MHz (AWS)	13.65 / 13.85 / 16.65 / 16.95	18	740	30,440.71	1.29
Antenna A2	Ericsson AIR6419 B41	2500 MHz (BRS)	21.5	8	240	33,900.90	1.20
Sector A Composite MPE%							<b>2.49</b>
Antenna B1	RFS APXVAALL24_43-U-NA20	600 MHz / 700 MHz / 1900 MHz (PCS) / 2100 MHz (AWS)	13.65 / 13.85 / 16.65 / 16.95	18	740	30,440.71	1.29
Antenna B2	Ericsson AIR6419 B41	2500 MHz (BRS)	21.5	8	240	33,900.90	1.20
Sector B Composite MPE%							<b>2.49</b>
Antenna C1	RFS APXVAALL24_43-U-NA20	600 MHz / 700 MHz / 1900 MHz (PCS) / 2100 MHz (AWS)	13.65 / 13.85 / 16.65 / 16.95	18	740	30,440.71	1.29
Antenna C2	Ericsson AIR6419 B41	2500 MHz (BRS)	21.5	8	240	33,900.90	1.20
Sector C Composite MPE%							<b>2.49</b>

*Table 3: T-MOBILE Emissions Levels*



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The Following table (*table 4*) shows all additional identified carriers on site and their emissions contribution estimates, along with the newly calculated maximum T-MOBILE MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, all three T-Mobile sectors have the same configuration yielding the same results for all three sectors. *Table 5* below shows a summary for each T-MOBILE Sector as well as the composite estimated MPE value for the site.

<b>Site Composite MPE%</b>	
<b>Carrier</b>	<b>MPE%</b>
T-MOBILE – Max Per Sector Value	<b>2.49 %</b>
Verizon Wireless	3.15 %
Dish Wireless	1.53 %
<b>Site Total MPE %:</b>	<b>7.17 %</b>

*Table 4: All Carrier MPE Contributions*

T-MOBILE Sector A Total:	2.49 %
T-MOBILE Sector B Total:	2.49 %
T-MOBILE Sector C Total:	2.49 %
Site Total:	7.17 %

*Table 5: Site MPE Summary*



# FOX HILL TELECOM

Table 6 below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated T-MOBILE sector(s). For this site, all three T-Mobile sectors have the same configuration yielding the same results on all three sectors.

T-MOBILE _ Frequency Band / Technology Max Power Values (Per Sector)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ( $\mu\text{W}/\text{cm}^2$ )	Frequency (MHz)	Allowable MPE ( $\mu\text{W}/\text{cm}^2$ )	Calculated % MPE
T-Mobile 600 MHz LTE / 5G NR	4	926.96	175	2.00	600 MHz	400	0.50%
T-Mobile 700 MHz LTE	2	485.32	175	0.51	700 MHz	467	0.11%
T-Mobile 1900 MHz (PCS) LTE	4	1,618.33	175	1.80	1900 MHz (PCS)	1000	0.18%
T-Mobile 1900 MHz (PCS) 5G	4	1,849.52	175	2.00	1900 MHz (PCS)	1000	0.20%
T-Mobile 2100 MHz (AWS) LTE	4	2,972.70	175	3.00	2100 MHz (AWS)	1000	0.30%
T-Mobile 2500 MHz (BRS) LTE / 5G NR	8	4,237.61	175	12.00	2500 MHz (BRS)	1000	1.20%
						<b>Total:</b>	<b>2.49 %</b>

Table 6: T-MOBILE Maximum Sector MPE Power Values



## Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-MOBILE facility as well as the site composite emissions estimates value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-MOBILE Sector	Power Density Value (%)
Sector A:	2.49 %
Sector B:	2.49 %
Sector C:	2.49 %
T-MOBILE Maximum Total (per sector):	2.49 %
Site Total:	7.17 %
Site Compliance Status:	<b>COMPLIANT</b>

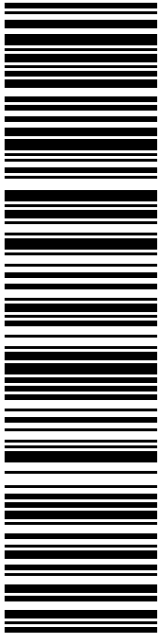
The estimated composite MPE value for this site assuming all carriers present is **7.17 %** of the allowable FCC established general population limit sampled at the ground level. This is based upon the far field calculations performed for all carriers identified in this report.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite estimated values calculated were well within the allowable 100% threshold standard per the federal government.

Scott Heffernan  
Principal RF Engineer  
**Fox Hill Telecom, Inc**  
Worcester, MA 01609  
(978)660-3998


# Exhibit G

## Recipient Mailings



**USPS TRACKING #**  
**9405 5036 9930 0692 6851 19**

Electronic Rate Approved #038555749



TIM KEENEY  
FIRST SELECTMAN  
600 MAIN ST  
SOMERS CT 06071-2119

**P**

USPS.com 9405 5036 9930 0692 6851 19 0098 5000 0020 6071  
**US POSTAGE \$9.85**  
 Flat Rate Env  
 U.S. POSTAGE PAID  
 Click-N-Ship®


06/06/2024 Mailed from 01606 986735388883506

**PRIORITY MAIL®**

DEB CHASE  
NORTHEAST SITE SOLUTIONS  
46 HUNTINGTON AVE  
WORCESTER MA 01606-3543

Expected Delivery Date: 06/08/24  
Ref#: CTHA027B  
**0003**

**R005**



**UNITED STATES POSTAL SERVICE®**

**Click-N-Ship®**



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### Instructions

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2. Place your label so it does not wrap around the edge of the package.
3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
4. To mail your package with PC Postage®, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office™, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.

### Click-N-Ship® Label Record

**USPS TRACKING # :**  
**9405 5036 9930 0692 6851 19**

Trans. #: 603057376	Priority Mail® Postage: <b>\$9.85</b>
Print Date: 06/06/2024	Total: <b>\$9.85</b>
Ship Date: 06/06/2024	
Expected Delivery Date: 06/08/2024	

**From:** DEB CHASE  
NORTHEAST SITE SOLUTIONS  
46 HUNTINGTON AVE  
WORCESTER MA 01606-3543


Ref#: CTHA027B

**To:** TIM KEENEY  
FIRST SELECTMAN  
600 MAIN ST  
SOMERS CT 06071-2119

\* Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date.

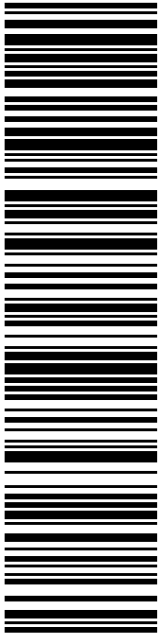


Thank you for shipping with the United States Postal Service!  
Check the status of your shipment on the USPS Tracking® page at usps.com



JENNIFER ROY  
ZONING ENFORCEMENT OFFICER  
600 MAIN ST  
SOMERS CT 06071-2119

**USPS TRACKING #**



**9405 5036 9930 0692 6851 26**

**P**

usps.com 9405 5036 9930 0692 6851 26 0098 5000 0020 6071  
**US POSTAGE \$9.85**  
 Flat Rate Env  
 U.S. POSTAGE PAID  
 Click-N-Ship®  
 Mailed from 01606 986735388881991


DEBORAH A CHASE  
NORTHEAST SITE SOLUTIONS  
46 HUNTINGTON AVE  
WORCESTER MA 01606-3543

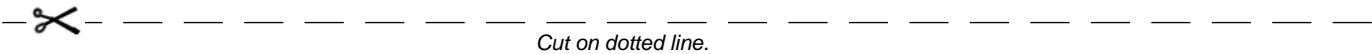
Expected Delivery Date: 06/08/24  
Ref#: CTHA027B  
**0003**

**PRIORITY MAIL®**

**R005**

Electronic Rate Approved #038555749





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### Click-N-Ship® Label Record

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**9405 5036 9930 0692 6851 26**

Trans. #: 603057376	Priority Mail® Postage: <b>\$9.85</b>
Print Date: 06/06/2024	Total: <b>\$9.85</b>
Ship Date: 06/06/2024	
Expected Delivery Date: 06/08/2024	


**From:** DEBORAH A CHASE  
NORTHEAST SITE SOLUTIONS  
46 HUNTINGTON AVE  
WORCESTER MA 01606-3543

Ref#: CTHA027B

**To:** JENNIFER ROY  
ZONING ENFORCEMENT OFFICER  
600 MAIN ST  
SOMERS CT 06071-2119

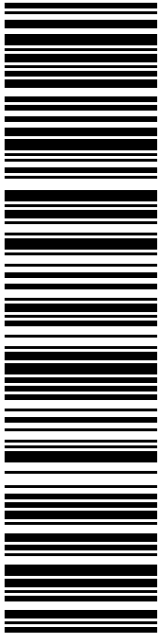
\* Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date.





DEBRA ROMANO  
248 HALL HILL RD  
SOMERS CT 06071-1401

**USPS TRACKING #**



**9405 5036 9930 0692 6851 57**

**P**

USPS.com 9405 5036 9930 0692 6851 57 0098 5000 0020 6071  
**US POSTAGE \$9.85**  
 Flat Rate Env  
 U.S. POSTAGE PAID  
 Click-N-Ship®


06/06/2024 Mailed from 01606 986735388880517

**PRIORITY MAIL®**

Expected Delivery Date: 06/08/24  
 Ref#: CTHA027B  
**0003**

**R003**

Electronic Rate Approved #038555749



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**USPS TRACKING # :**  
**9405 5036 9930 0692 6851 57**


Trans. #: 603057376	Priority Mail® Postage: <b>\$9.85</b>
Print Date: 06/06/2024	Total: <b>\$9.85</b>
Ship Date: 06/06/2024	
Expected Delivery Date: 06/08/2024	


**From:** DEBORAH A CHASE  
 NORTHEAST SITE SOLUTIONS  
 46 HUNTINGTON AVE  
 WORCESTER MA 01606-3543

Ref#: CTHA027B

**To:** DEBRA ROMANO  
 248 HALL HILL RD  
 SOMERS CT 06071-1401

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**UNITED STATES  
POSTAL SERVICE®**

**Click-N-Ship®**

**P**


usps.com 9405 5036 9930 0692 6851 71 0098 5000 0063 3487  
**US POSTAGE**  
 Flat Rate Env  
**U.S. POSTAGE PAID**  
Click-N-Ship®

06/06/2024 Mailed from 01606 986735388878324

**PRIORITY MAIL®**


DEBORAH A CHASE  
 NORTHEAST SITE SOLUTIONS  
 46 HUNTINGTON AVE  
 WORCESTER MA 01606-3543

Expected Delivery Date: 06/08/24  
 Ref#: CTHA027B  
**0003**



VERTICAL BRIDGE  
 STE 200  
 750 PARK OF COMMERCE DR  
 BOCA RATON FL 33487-3650


**USPS TRACKING #**



**9405 5036 9930 0692 6851 71**

**C057**

Electronic Rate Approved #038555749





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**9405 5036 9930 0692 6851 71**

Trans. #:	603057376	Priority Mail® Postage:	<b>\$9.85</b>
Print Date:	06/06/2024	Total:	<b>\$9.85</b>
Ship Date:	06/06/2024		
Expected			
Delivery Date:	06/08/2024		

**From:** DEBORAH A CHASE  
 NORTHEAST SITE SOLUTIONS  
 46 HUNTINGTON AVE  
 WORCESTER MA 01606-3543

Ref#: CTHA027B

**To:** VERTICAL BRIDGE  
 STE 200  
 750 PARK OF COMMERCE DR  
 BOCA RATON FL 33487-3650

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CTHA027B



GREENDALE  
290 W BOYLSTON ST  
WORCESTER, MA 01606-2378  
(800)275-8777

06/06/2024

03:22 PM

Product	Qty	Unit Price	Price
Prepaid Mail Somers, CT 06071 Weight: 0 lb 10.60 oz Acceptance Date: Thu 06/06/2024 Tracking #: 9405 5036 9930 0692 6851 57	1		\$0.00
Prepaid Mail Somers, CT 06071 Weight: 0 lb 10.50 oz Acceptance Date: Thu 06/06/2024 Tracking #: 9405 5036 9930 0692 6851 19	1		\$0.00
Prepaid Mail Boca Raton, FL 33487 Weight: 0 lb 10.60 oz Acceptance Date: Thu 06/06/2024 Tracking #: 9405 5036 9930 0692 6851 71	1		\$0.00
Prepaid Mail Somers, CT 06071 Weight: 0 lb 10.50 oz Acceptance Date: Thu 06/06/2024 Tracking #: 9405 5036 9930 0692 6851 26	1		\$0.00
Grand Total:			\$0.00