

10 INDUSTRIAL AVE, SUITE 3 MAHWAH NJ 07430

PHONE: 201.684.0055 FAX: 201.684.0066

October 1, 2019

Members of the Siting Council Connecticut Siting Council Ten Franklin Square New Britain, CT 06051

RE: Notice of Exempt Modification

27 Wintonbury Rd. Simsbury, CT 06070

Latitude: 41.89245 Longitude: -72.769542

Sprint Site#: CT03XC071 - DO Macro

Dear Ms. Bachman:

Sprint currently maintains three (3) antennas at the 75-foot level of the existing 100-foot lattice tower at 27 Wintonbury Rd. Simsbury, CT. The 100-foot lattice tower and property are owned by The Connecticut Light & Power Company, d/b/a Eversource Energy. Sprint now intends to replace three (3) of its existing antennas with three (3) new 800/1900/2500 MHz antennas, add (3) additional 2500 MHz antennas, and add (3) RRHs. The new antennas will be installed at the same 75-foot level of the tower.

Planned Modifications:

Tower:

Remove

N/A

Remove and Replace:

- (2) RFS APXVSPP18-C antennas (Remove) CommScope NNVV-65B-R4 antennas (Replace) 800/1900/2500 MHz
- (1) RFS APXV9ERR18-C antenna (Remove) CommScope NNVV-65B-R4 antennas (Replace) 800/1900/2500 MHz

Install New:

- (3) Nokia AAHC panel antennas
- (3) FD-RRH2X50-800 RRHs
- (1) 1-1/4" hybrid cable

Existing to Remain:

- (3) FD-RRH2X50-800 RRHs
- (3) FD-RRH4x45 1900 RRHs

(3) 1-1/4" hybrid cable

Ground:

Install New: (1) Eltek Model ESOA220-SCA02

This facility was approved by the CSC for Sprint use per the attached approval letter dated April 3, 1997. This modification complies with this approval. Please see the enclosed.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies§ 16- SOj-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.SA. § 16-SOj-73, a copy of this letter is being sent to First Selectman - Eric Wellman, Elected Official, and Janell Mullen, Zoning Enforcement Officer for the Town of Simsbury, as well as the owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S;A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing structure.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Sprint respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Jake Shappy

Transcend Wireless Cell: 845-553-3330

Email: jshappy@transcendwireless.com

Attachments

cc: Eric Wellman - Town of Simsbury First Selectman

Janell Mullen - Town of Simsbury Zoning Enforcement Officer

The Connecticut Light & Power Company, d/b/a Eversource Energy – property and tower owner



August 21, 2019

Mr. Jake Shappy Transcend Wireless, LLC. 10 Industrial Ave. Suite 3 Mahwah, New Jersey. 07430

RE:

Letter of Authorization

Project: Sprint Site # CT03XC071

27 Wintonbury Road Simsbury, CT. 06070

Owner: Eversource Energy

Dear Mr. Shappy,

Eversource Energy, owner of the tower facility located at the address identified above, do hereby authorize Sprint PCS, and/or it's agent, to use this authorization letter for the sole purpose of filing and consummating any land-use or building permit application(s) as may be required by the applicable permitting authorities for the Licensee's telecommunication's installation.

> Sincerely, to ff

Steven J. Florio **Eversource Energy**

REF: CENTEK Engineering, LLC Project # 17159.09 Structural Analysis Rev. Date 09/17/2018 CD's Rev. Date 02/15/2019



STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

10 Franklin Square New Britain, Connecticut 06051 Phone: (860) 827-2935 Fax: (860) 827-2950

071

April 3, 1997

Larry Woods Site Development Manager Sprint PCS 9 Barnes Industrial Road Wallingford, CT 06492

Re:

Sprint PCS notice of intent to modify an existing telecommunications facility located off Wintonbury Road in the Town of Simsbury, Connecticut.

Dear Mr. Woods:

At a public meeting held on April 2, 1997, the Connecticut Siting Council (Council) acknowledged your notice to modify an existing telecommunications facility in Simsbury, Connecticut, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies.

The proposed modification is to be implemented as specified in your notice dated January 9, 1997, and amendment dated March 5, 1997. The modification is in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequency electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes # 22a-162. This change has been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequency now used and proposed for use on this tower. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Science and Technology, Bulletin No. 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

This decision is conditioned on a field investigation by the Council after the submittal of a final plan to the Council one week prior to the commencement of construction to include the following provisions:

- installation of silt fence for erosion and sediment control at the site of the proposed telecommunications equipment compound;
- surveying and marking of the property surrounding the proposed equipment compound to ensure that site work and equipment installation do not encroach onto adjacent property owned by the Simsbury Land Conservation Trust, Inc.:
- consolidation of the telecommunications equipment configuration to ensure maximum compaction of the equipment while allowing sufficient space to install a future emergency generator;
- cooperation with CL&P to install the new poles for the overhead utility line in a manner and configuration consistent with the transmission line pole gaps to minimize impacts to wetlands along the existing transmission line; and

_arry Woods Page 2

• relocation of the proposed transition/riser pole leading into the equipment compound to the southeast of the tower structure to minimize tree clearing.

No clearing, grading, or placement of pole structures may commence until authorized by the Chairman of the Council after the receipt of final plan(s) and a field investigation to make necessary alterations in the final configuration consistent with this decision.

Enclosed is a staff report on this project dated April 2, 1997.

Thank you for your attention and cooperation.

Very truly yours,

Mortiner A. Gelston

Chairman

MAG/RKE/ss

c: Honorable Mary A. Glassman, First Selectman Dorian Hill, CL&P

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BechtelInteroffice Memorandum

To

Scott M. Chasse, P.E.

File No.

23224-390-BLSS-573

Subject

Transmittal

06/23/97

Date

From

J. M. McSpadden

G. Rivenburgh, File

Δ

Wallingford, CT

Ext 203-294-

5633

Scott:

The following items are being transmitted to Sprint for the sites listed below:

Site CT03XC011 - Montowese

Tower Erection Drawings (2 copies)

Site CT03XC023 - Madison

Siting Council Drawings (3 copies)

Site CT03XC039 - North Haven, BANM

Revised Siting Council Drawings (2 "D" size)

NOTE: The requested 8 ½ x 11 will be delivered Tuesday, June 24th

Site CT03XC071 Bloomfield/Tarriffville, NU Tower

Revised Zoning Drawings (4 copies)

Site CT03XC102 - Old Saybrook, 430 Middlesex Turnpike

Revised Lease Exhibit (5 copies)

Site CT03XC153 - Roscommon Building

Copy of letter from Allied Roofing and "okay'd" by Flatley

Site CT03XC207E - Tolland, 23 Rhodes Rd.

RF Sketch

Site CT03XC211 - Manchester, Buckland Hills Mall

RF Sketch



June 23, 1997 Page 2

Site CT03XC212 - No. Vernon, 31 Stacy Lane

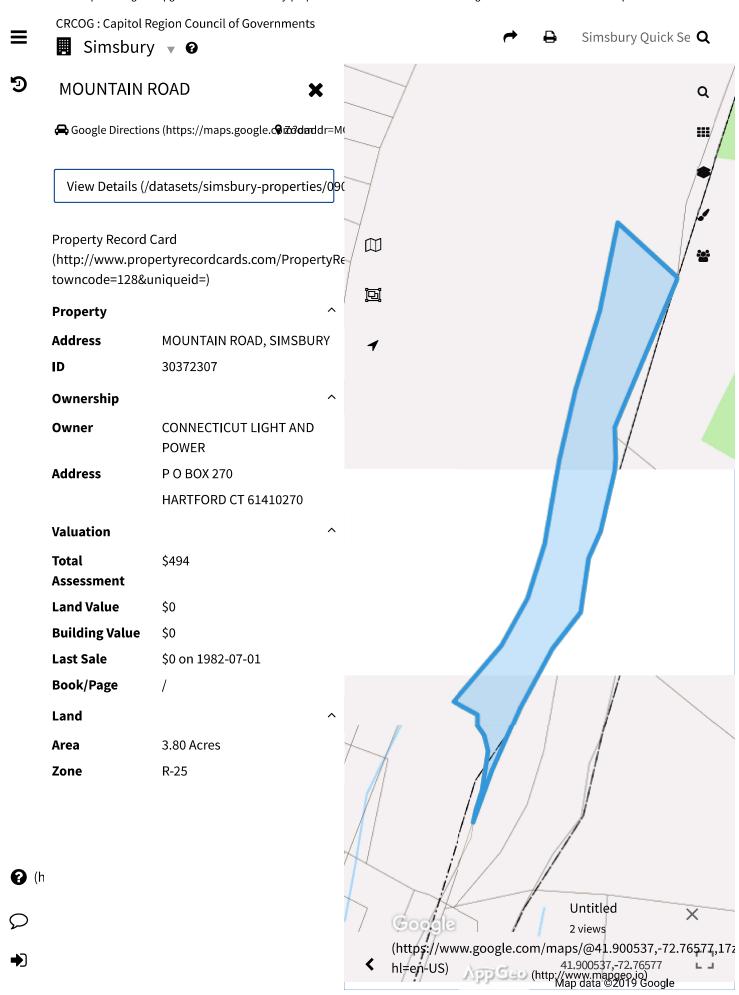
Site CT03XC368 - Newtown, CT Engineering Associated Corp. RF Sketch (1 copy)

Site CT03XC375 - Noroton
Revised Structural Analysis Letter & Computaions (2 copies)

Wade Sokirme For JMM

J. M. McSpadden

Field Construction Manager



Account 30372307

Property Information

Owner	CONNECTICUT LIGHT AND POWER	
Address	MOUNTAIN ROAD	
Mailing Address	P O BOX 270	
	HARTFORD CT 061410270	
Land Use	- Commercial Vacant Land	
Land Class	Vacant Land	

Census Tract	4664000
Neighborhood	12
Zoning	R-25
Acreage	3.8
Utilities	
Lot Setting/ Desc	I

Photo



PARCEL VALUATIONS (Assessed value = 70% of Appraised Value)

	Appraised	Assessed
Buildings		
Outbuildings		
Improvements		
Extras		
Land		
Total	912	640
Previous		

Construction Details

Year Built	
Stories	
Building Style	
Building Use	
Building Condition	
Total Rooms	
Bedrooms	
Full Bathrooms	
Half Bathrooms	
Bath Style	
Kitchen Style	
Roof Style	
Roof Cover	

EXTERIOR WALLS:

Primary	
Secondary	
INTERIOR WAL	LS:
Primary	
Secondary	
FLOORS:	
Primary	
Secondary	
HEATING/AC:	
Heating Type	
Heating Fuel	
AC Type	

BUILDING AREA:

Effective Building Area	
Gross Building Area	
Total Living Area	

SALES HISTORY:

Sale Date	07/01/1982
Sale Price	0
Book/ Page	0260/0201



WIRELESS COMMUNICATIONS FACILITY

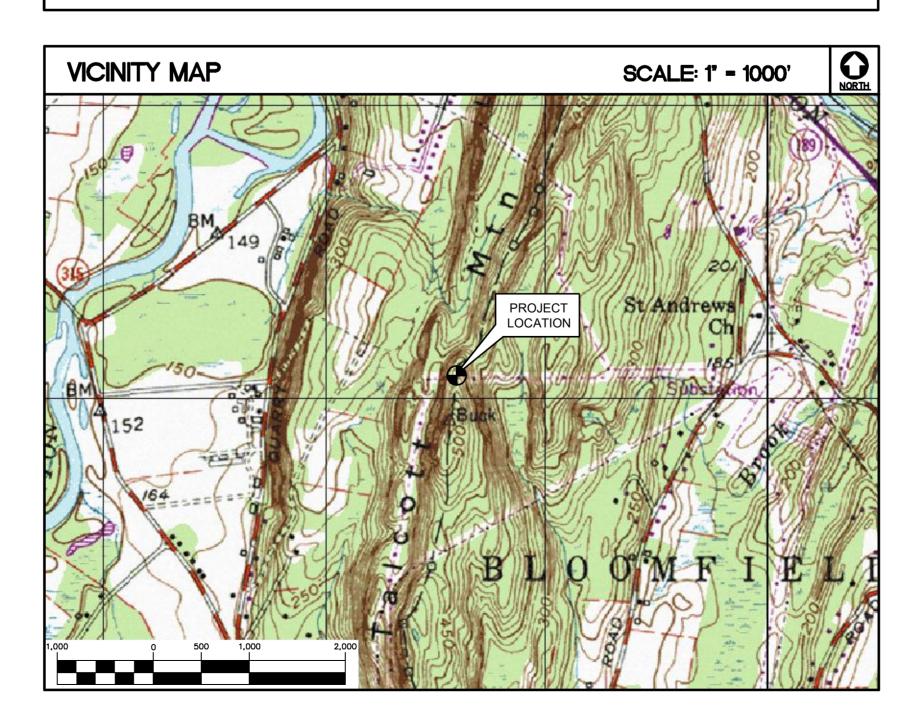
SITE ID: CT03XC071 27 WINTONBURY ROAD SIMSBURY, CT 06070

GENERAL NOTES

- 1. ALL WORK SHALL BE IN ACCORDANCE WITH THE 2015 INTERNATIONAL BUILDING CODE AS MODIFIED BY THE 2018 CONNECTICUT SUPPLEMENT, INCLUDING THE TIA/EIA-222 REVISION "G" "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND SUPPORTING STRUCTURES." 2016 CONNECTICUT FIRE SAFETY CODE, NATIONAL ELECTRICAL CODE AND LOCAL CODES.
- 2. CONTRACTOR SHALL REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUBCONTRACTORS AND ALL RELATED PARTIES. THE SUBCONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
- 3. CONTRACTOR SHALL PROVIDE A COMPLETE BUILD—OUT WITH ALL FINISHES, STRUCTURAL, MECHANICAL, AND ELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON THE DRAWINGS OR IN THE WRITTEN SPECIFICATIONS.
- 4. CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OVER THE WORK.
- 5. CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION, PLUMBING, ELECTRICAL AND HVAC. PERMITS SHALL BE PAID FOR BY THE RESPECTIVE SUBCONTRACTORS.
- 6. CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS AND SPECIFICATIONS ON SITE AT ALL TIMES AND INSURE DISTRIBUTION OF NEW DRAWINGS TO SUBCONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE. ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. THE CONTRACTOR SHALL FURNISH AN 'AS—BUILT' SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
- 7. LOCATION OF EQUIPMENT, AND WORK SUPPLIED BY OTHERS THAT IS DIAGRAMMATICALLY INDICATED ON THE DRAWINGS SHALL BE DETERMINED BY THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE LOCATIONS AND DIMENSIONS SUBJECT TO STRUCTURAL CONDITIONS AND WORK OF THE SUBCONTRACTORS.
- 8. THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURES AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY.
- 9. DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
- 10. ALL UTILITY WORK SHALL BE IN ACCORDANCE WITH LOCAL UTILITY COMPANY REQUIREMENTS AND SPECIFICATIONS.

- 11. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUBCONTRACTORS FOR ANY CONDITION PER MFR.'S RECOMMENDATIONS. CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR CONSTRUCTION MANAGER.
- 12. ANY AND ALL ERRORS, DISCREPANCIES, AND 'MISSED" ITEMS ARE TO BE BROUGHT TO THE ATTENTION OF THE SPRINT CONSTRUCTION MANAGER DURING THE BIDDING PROCESS BY THE CONTRACTOR. ALL THESE ITEMS ARE TO BE INCLUDED IN THE BID. NO 'EXTRA' WILL BE ALLOWED FOR MISSED ITEMS.
- 13. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON—SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
- 14. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE CONSTRUCTION MANAGER FOR REVIEW.
- 15. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES, AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT
- 16. COORDINATION, LAYOUT, FURNISHING AND INSTALLATION OF CONDUIT AND ALL APPURTENANCES REQUIRED FOR PROPER INSTALLATION OF ELECTRICAL AND TELECOMMUNICATION SERVICE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR.
- 17. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
- 18. THE CONTRACTOR SHALL CONTACT "CALL BEFORE YOU DIG" AT LEAST 48 HOURS PRIOR TO ANY EXCAVATIONS AT 1-800-922-4455. ALL UTILITIES SHALL BE IDENTIFIED AND CLEARLY MARKED. CONTRACTOR SHALL MAINTAIN AND PROTECT MARKED UTILITIES THROUGHOUT PROJECT COMPLETION.
- 19. CONTRACTOR SHALL COMPLY WITH OWNERS ENVIRONMENTAL ENGINEER ON ALL METHODS AND PROVISIONS FOR ALL EXCAVATION ACTIVITIES INCLUDING SOIL DISPOSAL. ALL BACKFILL MATERIALS TO BE PROVIDED BY THE CONTRACTOR.

SITE DIRECTIONS START OUT BY GOING TO WAYSIDE ROAD. 0.12 MI. . TURN LEFT ONTO CAMBRIDGE ST/US-3 N/MA 0.12 MI. MERGE ONTO I-95 S/MA-128 S/YANKEE DIVISION HWY S TOWARD WALTHAM/LOWELL 0.27 MI. . TAKE THE I-90/MASS PIKE EXIT, EXIT 25, TOWARD BOSTON/ALBANY NY. 12.32 MI. MERGE ONTO I-90 W/MASSACHUSETTS TPKE W TOWARD WORCESTER (PORTIONS TOLL). 44.30 MI. MERGE ONTO I-84 W/WILBUR CROSS HWY S VIA EXIT 9 TOWARD US-20(PORTIONS TOLL). 0.90 MI. CONTINUE ON I-84. 36.50 MI TAKE EXIT 61 FOR I-291 W TOWARD WINDSOR. 0.60 MI CONTINUE ONTO I-291 W. 5.10 MI 2.20 MI 10. TAKE EXIT 2B TO MERGE ONTO I-91 N TOWARD SPRINGFIELD. 0.20 MI 11. TAKE EXIT 37 FOR CT-305/BLOOMFIELD AVE TOWARD WINDSOR CENTER. 12. TURN LEFT ONTO CT-305/BLOOMFIELD AVE. 2.50 MI. 3.30 MI 13. TURN RIGHT ONO CT-187 N. 14. TAKE THE CT-189 N RAMP TO TARIFFVILLE/GRANBY 1.60 MI. 1.10 MI. 15. TURN LEFT ONTO ELM STREET. 16. TURN LEFT INTO QUARRY ROAD. 1.00 MI. 17. MERGE ONTO TERRY'S PLAIN ROAD. 0.20 MI. 18. TURN LEFT ONTO WINTONBURY ROAD. 0.40 MI.



PROJECT SUMMARY

- 1. THE PROPOSED SCOPE OF WORK CONSISTS OF A MODIFICATION TO THE EXISTING UNMANNED TELECOMMUNICATIONS FACILITY
- A. REMOVE (3) EXISTING PANEL ANTENNAS FROM EXISTIN TOWER MOUNT.
- B. INSTALL (6) PROPOSED PANEL ANTENNAS, (2) PER SECTOR.
- C. INSTALL (3) PROPOSED REMOTE RADIO UNITS ON TOWER.
- D. INSTALL (1) HYBRID CABLE FROM EQUIPMENT AT GRADE TO RRHs ON TOWER.
- D. INSTALL (1) EQUIPMENT CABINET AT GRADE ON EXISTING CONCRETE PAD.

PROJECT INFORMATION

SITE ID: CT03XC071

SITE ADDRESS: 27 WINTONBURY ROAD

SIMSBURY, CT 06070

APPLICANT: SPRINT
5 WAYSIDE ROAD
BURLINGTON. MA 01803

CONTACT PERSON: DOUG TALMADGE (PROJECT MANAGER)

(475)434-4292

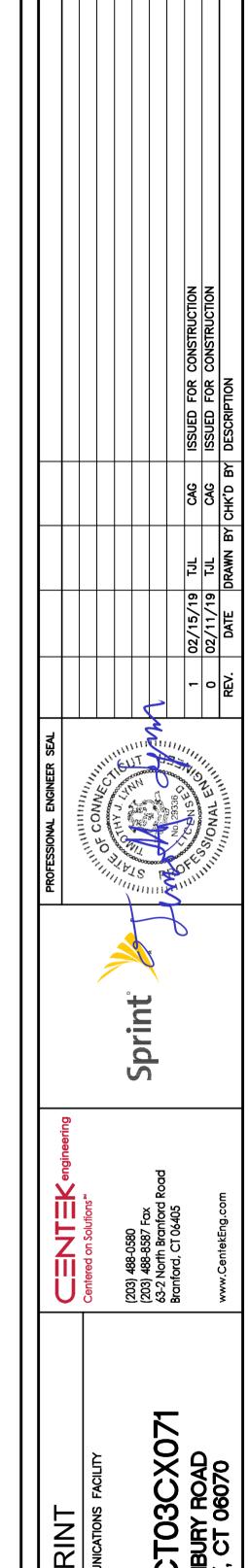
ENGINEER: CENTEK ENGINEERING, INC. 63–2 NORTH BRANFORD RD. BRANFORD, CT 06405

PROJECT COORDINATES: LATITUDE: 41° 53' 32.82"N

LONGITUDE: 72° 46' 10.35"W
GROUND ELEVATION: ±470' AMSL

SITE COORDINATES AND GROUND ELEVATION REFERENCED FROM GOOGLE EARTH.

SHEET	INDEX	
SHT. NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	0
N-1	DESIGN BASIS AND SITE NOTES	0
C-1	COMPOUND PLANS AND ELEVATION	0
C-2	TYPICAL DETAILS	0
C-3	COLOR CODE AND CPRI DETAILS	0
·		



DATE: 09/28/18

SCALE: AS NOTED

JOB NO. 17159.04

TITLE



SHEET

DESIGN BASIS:

GOVERNING CODE: 2015 INTERNATIONAL BUILDING (IBC) AS MODIFIED BY THE 2018 CT STATE BUILDING CODE AND AMENDMENTS.

- 1. DESIGN CRITERIA:
 - RISK CATEGORY: III (BASED ON IBC TABLE 1604.5)
 - NOMINAL DESIGN SPEED (OTHER STRUCTURE): 93 MPH (Vasd) (EXPOSURE C/IMPORTANCE FACTOR 1.0 BASED ON ASCE 7-10) PER 2015 INTERNATIONAL BUILDING CODE (IBC) AS MODIFIED BY THE 2018 CONNECTICUT STATE BUILDING
 - SEISMIC LOAD (DOES NOT CONTROL): PER ASCE 7-10 MINIMUM DESIGN LOADS FOR BUILDING AND OTHER STRUCTURES.

GENERAL NOTES:

- 1. ALL CONSTRUCTION SHALL BE IN COMPLIANCE WITH THE GOVERNING BUILDING
- 2. DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
- 3. BEFORE BEGINNING THE WORK, THE CONTRACTOR IS RESPONSIBLE FOR MAKING SUCH INVESTIGATIONS CONCERNING PHYSICAL CONDITIONS (SURFACE AND SUBSURFACE) AT OR CONTIGUOUS TO THE SITE WHICH MAY AFFECT PERFORMANCE AND COST OF THE WORK.
- 4. DIMENSIONS AND DETAILS SHALL BE CHECKED AGAINST EXISTING FIELD CONDITIONS.
- THE CONTRACTOR SHALL VERIFY AND COORDINATE THE SIZE AND LOCATION OF ALL OPENINGS. SLEEVES AND ANCHOR BOLTS AS REQUIRED BY ALL TRADES.
- 6. ALL DIMENSIONS, ELEVATIONS, AND OTHER REFERENCES TO EXISTING STRUCTURES, SURFACE, AND SUBSURFACE CONDITIONS ARE APPROXIMATE. NO GUARANTEE IS MADE FOR THE ACCURACY OR COMPLETENESS OF THE INFORMATION SHOWN. THE CONTRACTOR SHALL VERIFY AND COORDINATE ALL DIMENSIONS, ELEVATIONS, ANGLES WITH EXISTING CONDITIONS AND WITH ARCHITECTURAL AND SITE DRAWINGS BEFORE PROCEEDING WITH ANY WORK.
- 7. AS THE WORK PROGRESSES, THE CONTRACTOR SHALL NOTIFY THE OWNER OF ANY CONDITIONS WHICH ARE IN CONFLICT OR OTHERWISE NOT CONSISTENT WITH THE CONSTRUCTION DOCUMENTS AND SHALL NOT PROCEED WITH SUCH WORK UNTIL THE CONFLICT IS SATISFACTORILY RESOLVED.
- 8. THE CONTRACTOR SHALL COMPLY WITH ALL APPLICABLE SAFETY CODES AND REGULATIONS DURING ALL PHASES OF CONSTRUCTION. THE CONTRACTOR IS SOLELY RESPONSIBLE FOR PROVIDING AND MAINTAINING ADEQUATE SHORING, BRACING, AND BARRICADES AS MAY BE REQUIRED FOR THE PROTECTION OF EXISTING PROPERTY, CONSTRUCTION WORKERS, AND FOR PUBLIC SAFETY.
- 9. THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURES AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY. MAINTAIN EXISTING SITE OPERATIONS, COORDINATE WORK WITH NORTHEAST UTILITIES
- 10. THE STRUCTURE IS DESIGNED TO BE SELF-SUPPORTING AND STABLE AFTER FOUNDATION REMEDIATION WORK IS COMPLETE. IT IS THE CONTRACTOR'S SOLE RESPONSIBILITY TO DETERMINE ERECTION PROCEDURE AND SEQUENCE AND TO ENSURE THE SAFETY OF THE STRUCTURE AND ITS COMPONENT PARTS DURING ERECTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, TEMPORARY BRACING, GUYS OR TIEDOWNS, WHICH MIGHT BE NECESSARY.
- 11. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
- 12. SHOP DRAWINGS, CONCRETE MIX DESIGNS, TEST REPORTS, AND OTHER SUBMITTALS PERTAINING TO STRUCTURAL WORK SHALL BE FORWARDED TO THE OWNER FOR REVIEW BEFORE FABRICATION AND/OR INSTALLATION IS MADE. SHOP DRAWINGS SHALL INCLUDE ERECTION DRAWINGS AND COMPLETE DETAILS OF CONNECTIONS AS WELL AS MANUFACTURER'S SPECIFICATION DATA WHERE APPROPRIATE. SHOP DRAWINGS SHALL BE CHECKED BY THE CONTRACTOR AND BEAR THE CHECKER'S INITIALS BEFORE BEING SUBMITTED FOR REVIEW.
- 13. NO DRILLING WELDING OR TAPING ON EVERSOURCE OWNED EQUIPMENT.
- 14. REFER TO DRAWING T1 FOR ADDITIONAL NOTES AND REQUIREMENTS.

STRUCTURAL STEEL

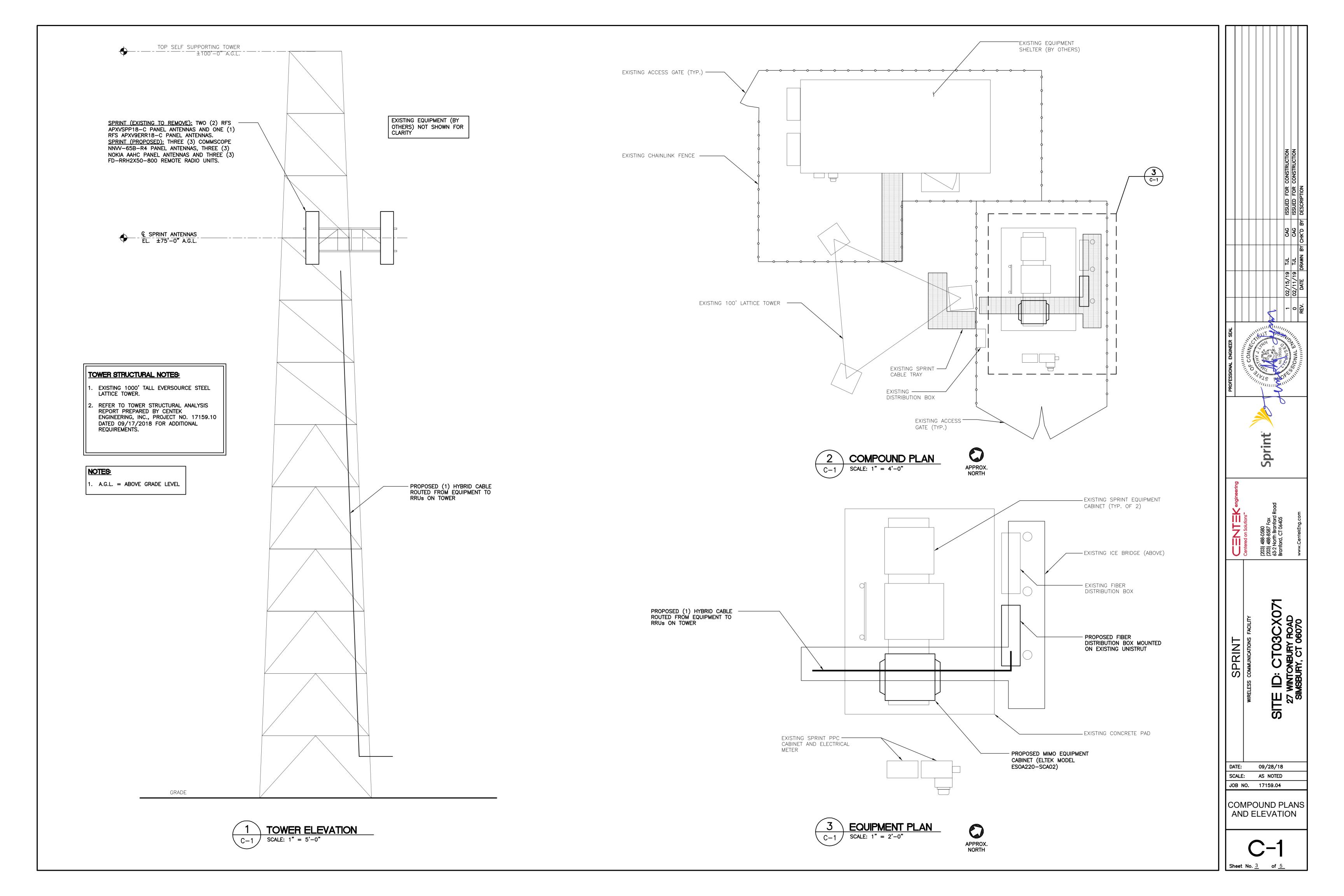
- 1. ALL STRUCTURAL STEEL IS DESIGNED BY ALLOWABLE STRESS DESIGN (ASD)
 - STRUCTURAL STEEL (W SHAPES)---ASTM A992 (FY = 50 KSI)
 - STRUCTURAL STEEL (OTHER SHAPES)---ASTM A36 (FY = 36 KSI) C. STRUCTURAL HSS (RECTANGULAR SHAPES) --- ASTM A500 GRADE B,
 - (FY = 46 KSI)D. STRUCTURAL HSS (ROUND SHAPES) --- ASTM A500 GRADE B,
 - (FY = 42 KSI)
 - PIPE---ASTM A53 (FY = 35 KSI)
 - CONNECTION BOLTS---ASTM A325-N U-BOLTS---ASTM A36
 - ANCHOR RODS---ASTM F 1554
- WELDING ELECTRODE --- ASTM E 70XX
- 2. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE ENGINEER FOR REVIEW. SHOP DRAWINGS SHALL INCLUDE THE FOLLOWING: SECTION PROFILES, SIZES, CONNECTION ATTACHMENTS, REINFORCING, ANCHORAGE, SIZE AND TYPE OF FASTENERS AND ACCESSORIES. INCLUDE ERECTION DRAWINGS, ELEVATIONS AND DETAILS.
- 3. STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH THE LATEST PROVISIONS OF AISC MANUAL OF STEEL CONSTRUCTION.
- 4. PROVIDE ALL PLATES, CLIP ANGLES, CLOSURE PIECES, STRAP ANCHORS, MISCELLANEOUS PIECES AND HOLES REQUIRED TO COMPLETE THE STRUCTURE.
- 5. FIT AND SHOP ASSEMBLE FABRICATIONS IN THE LARGEST PRACTICAL SECTIONS FOR DELIVERY TO SITE.
- 6. INSTALL FABRICATIONS PLUMB AND LEVEL, ACCURATELY FITTED, AND FREE FROM DISTORTIONS OR DEFECTS.
- 7. AFTER ERECTION OF STRUCTURES, TOUCHUP ALL WELDS, ABRASIONS AND NON-GALVANIZED SURFACES WITH A 95% ORGANIC ZINC RICH PAINT IN ACCORDANCE WITH ASTM 780.
- 8. ALL STEEL MATERIAL (EXPOSED TO WEATHER) SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT DIPPED GALVANIZED) COATINGS" ON IRONS AND STEEL PRODUCTS.
- 9. ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC COATING (HOT-DIP) ON IRON AND STEEL
- 10. THE ENGINEER SHALL BE NOTIFIED OF ANY INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON CONFORMING MATERIALS OR CONDITIONS TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE ENGINEER
- 11. CONNECTION ANGLES SHALL HAVE A MINIMUM THICKNESS OF 1/4 INCHES.
- 12. STRUCTURAL CONNECTION BOLTS SHALL CONFORM TO ASTM A325. ALL BOLTS SHALL BE 3/4" DIAMETER MINIMUM AND SHALL HAVE A MINIMUM OF TWO BOLTS, UNLESS OTHERWISE ON THE DRAWINGS.
- 13. LOCK WASHER ARE NOT PERMITTED FOR A325 STEEL ASSEMBLIES.
- 14. SHOP CONNECTIONS SHALL BE WELDED OR HIGH STRENGTH BOLTED.
- 15. MILL BEARING ENDS OF COLUMNS, STIFFENERS, AND OTHER BEARING SURFACES TO TRANSFER LOAD OVER ENTIRE CROSS SECTION.
- 16. FABRICATE BEAMS WITH MILL CAMBER UP.
- 17. LEVEL AND PLUMB INDIVIDUAL MEMBERS OF THE STRUCTURE TO AN ACCURACY OF 1:500, BUT NOT TO EXCEED 1/4" IN THE FULL HEIGHT OF THE COLUMN.
- 18. COMMENCEMENT OF STRUCTURAL STEEL WORK WITHOUT NOTIFYING THE ENGINEER OF ANY DISCREPANCIES WILL BE CONSIDERED ACCEPTANCE OF PRECEDING WORK.
- 19. INSPECTION AND TESTING OF ALL WELDING AND HIGH STRENGTH BOLTING SHALL BE PERFORMED BY AN INDEPENDENT TESTING LABORATORY.
- 20. FOUR COPIES OF ALL INSPECTION TEST REPORTS SHALL BE SUBMITTED TO THE ENGINEER WITHIN TEN (10) WORKING DAYS OF THE DATE OF INSPECTION.

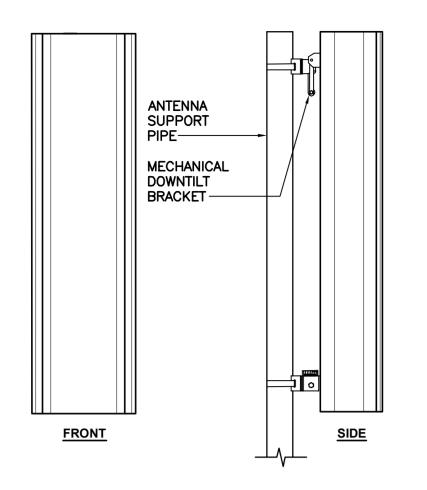
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09/28/18

DESIGN BASIS AND SITE NOTES

SCALE: AS NOTED JOB NO. 17159.04







BOTTOM - AAHC



BOTTOM - NNVV-65B-R4 ANTENNA

ALPI	HA/BETA/GAMMA ANTENNA	
EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: COMMSCOPE MODEL: NNVV-65B-R4	72.0"L × 19.6"W × 7.8"D	78 LBS.
MAKE: NOKIA MODEL: AAHC	25.6"L x 19.7"W x 9.6"D	104 LBS.

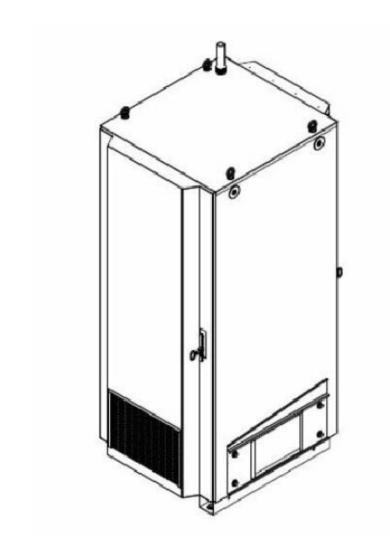




RRH-2x50-800

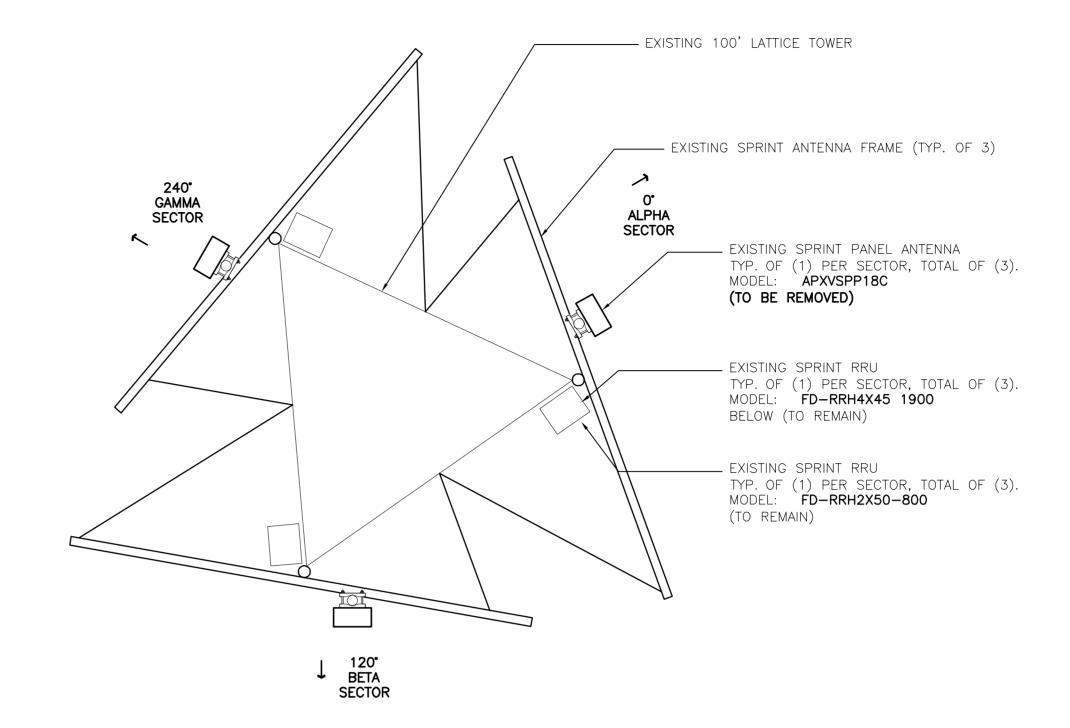
RRU (REMOTE RADIO UNIT)			
EQUIPMENT	DIMENSIONS	WEIGHT	CLEARANCES
MAKE: ALCATEL-LUCENT MODEL: RRH-2x50-800	15.7"L x 13.0"W x 9.8"D	53 LBS.	ABOVE: 16" MIN. BELOW: 12" MIN. FRONT: 36" MIN.
	DINATE FINAL EQUIPMENT MODER PRIOR TO ORDERING.	EL SELECTION W	/ITH SPRINT



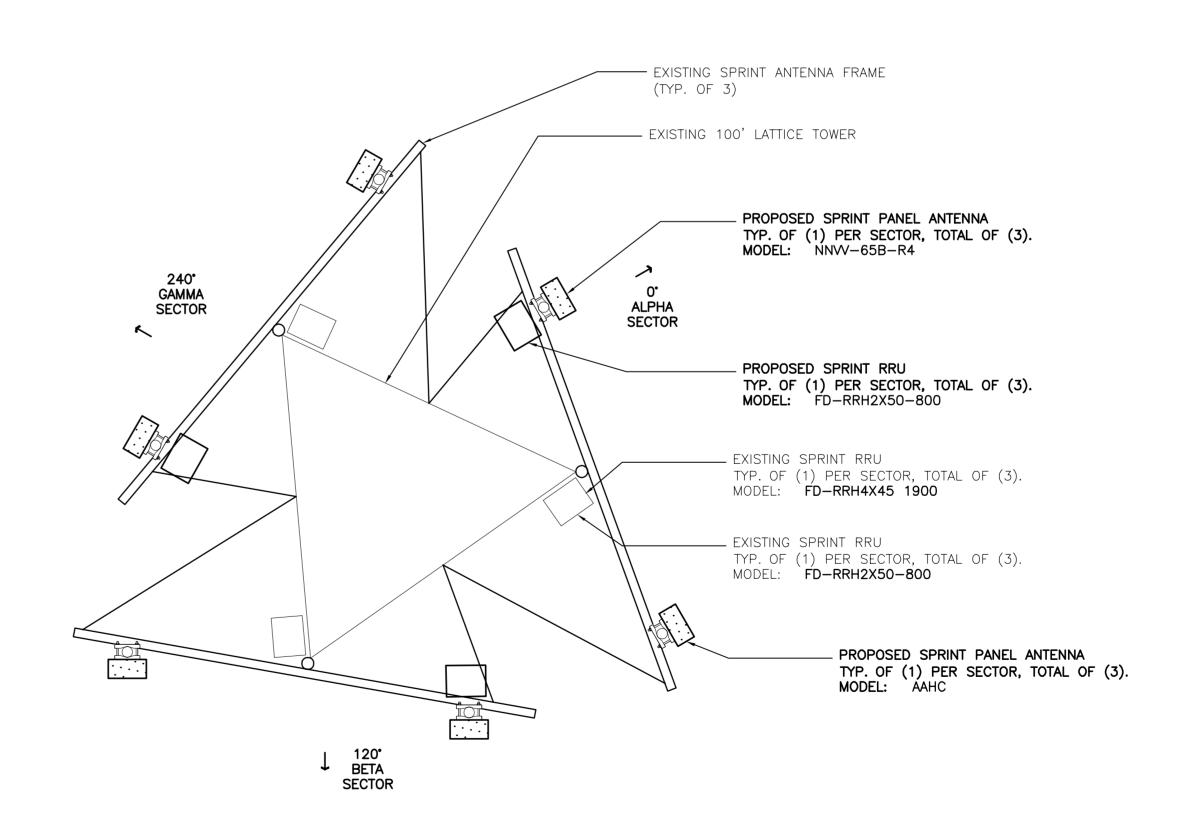


EQUIPMEN	<u>IT </u>	DIMENSIONS	WEIGHT
MAKE: MODEL:	ELTEK ES0A220-SCA02	30.0"W × 38.0"D × 73.5"H	505 LBS.
NOTES:			











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TYPICAL DETAILS

NV CABLES					
BAND	INDICA	ATOR	PORT	COLOR	
800-1	YEL	GRN	NV-1	GRN	
1900-1	YEL	RED	NV-2	BLU	
1900-2	YEL	BRN	NV-3	BRN	
1900-3	YEL	BLU	NV-4	WHT	
1900-4	YEL	SLT	NV-5	RED	
800-2	YEL	ORG	NV-6	SLT	
SPARE	YEL	WHT	NV-7	PPL	
2500	YEL	PPL	NV-8	ORG	

HYBRII)
HYBRID	COLOR
1	GRN
2	BLU
3	BRN
4	WHT
5	RED
6	SLT
7	PPL
8	ORG

	2.5 Band	
2500 Ra	adio 1	COLOR
YEL	WHT	GRN
YEL	WHT	BLU
YEL	WHT	BRN
YEL	WHT	WHT
YEL	WHT	RED
YEL	WHT	SLT
YEL	WHT	PPL
YEL	WHT	ORG

Figure 1: Antenna Orientation

G4

A1

NOTES

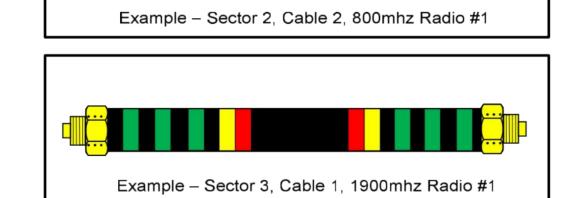
- 1. All cables shall be marked at the top and bottom with 2" colored tape, stencil tag colored tape, or colored heat shrink tubing
- 2. Colored tape may be obtained from Graybar Electronic. UV stabilized tape or heat shrink are preferred.
- 3. The first ring shall be closest to the end of the cable, and there shall be a 1" space between each ring.
- 4. The cable color code shall be applied in accordance to Table 19-1.
- A. Table 19-1 only shows 3 sectors, but additional sectors are easily supported by adding the appropriate number of colored rings to the cable color code.
- 5. After the cable color code is applied, the frequency color code, Table 19-2, must be applied for the specific frequency band in use on a A.2" gap shall separate the cable color code from the frequency color code.
 - B. The 2" color rings for the frequency code shall be placed next to each other with no spaces.
- 6. Wrap 2" colored tape a minimum of 3 times around the coax, and keep the tape in the same area as much as possible. This will allow remova
- 7. Examples of the cable and frequency color codes are shown in Figure 19-1 and Figure 19-2.

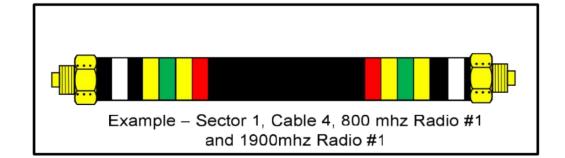
FIGURE 19.1 CABLE COLOR CODE

FIGURE 19.1 CABLE COLOR CODE					
			Second		
Sector	Cable	First Ring	Ring	Third Ring	
1 Alpha	1	Green	No Tape	No Tape	
1	2		No Tape	No Tape	
1	3	Brown	No Tape	No Tape	
1	4	White	No Tape	No Tape	
1	5	Red	No Tape	No Tape	
1	6	Grey	No Tape	No Tape	
1	7	Purple	No Tape	No Tape	
1	8	Orange	No Tape	No Tape	
2 Beta	1	Green	Green	No Tape	
2	2			No Tape	
2	3	Brown	Brown	No Tape	
2	4	White	White	No Tape	
2	5	Red	Red	No Tape	
2	6	Grey	Grey	No Tape	
2	7	Purple	Purple	No Tape	
2	8	Orange	Orange	No Tape	
3 Gamma	1	Green	Green	Green	
3	2				
3	3	Brown	Brown	Brown	
3	4	White	White	White	
3	5	Red	Red	Red	
3	6	Grey	Grey	Grey	
3	7	Purple	Purple	Purple	
3	8	Orange	Orange	Orange	

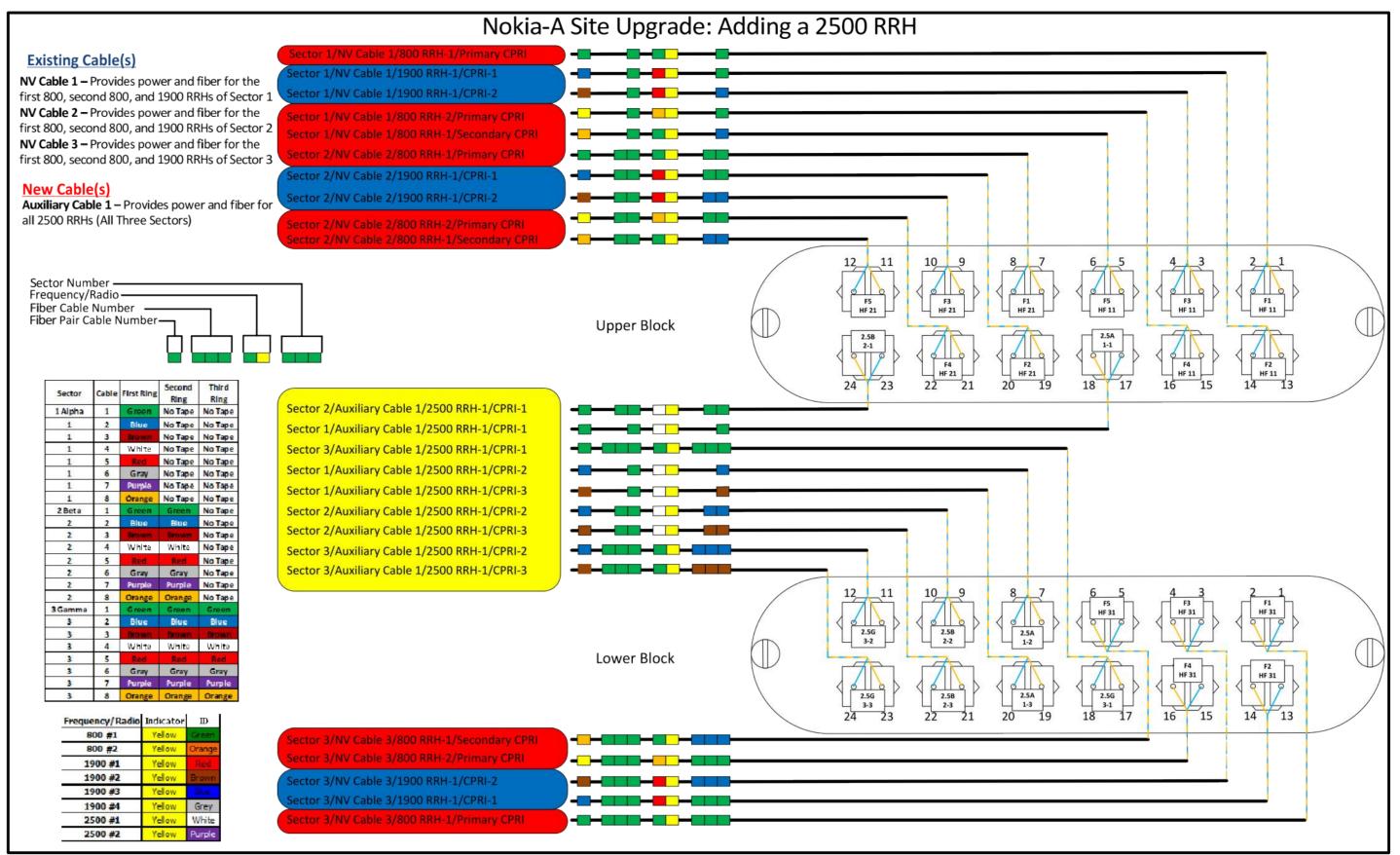
FIGURE 19.2 COLOR CODE

				702071.00			
EQUENC	INDICATOR	ID		FREQUE	INDIC	CATOR	ID
0-1	YEL	GRN		2500 -1	YEL	WHT	GRN
00-1	YEL	RED		2500 -2	YEL	WHT	RED
00-2	YEL	BRN		2500 -3	YEL	WHT	BRN
00-3	YEL	BLU		2500 -4	YEL	WHT	BLU
00-4	YEL	SLT		2500 -5	YEL	WHT	SLT
0-1	YEL	ORG		2500 -6	YEL	WHT	ORG
SERVED	YEL	WHT		2500 -7	YEL	WHT	WHT
SERVED	YEL	PPL		2500 -8	YEL	WHT	PPL
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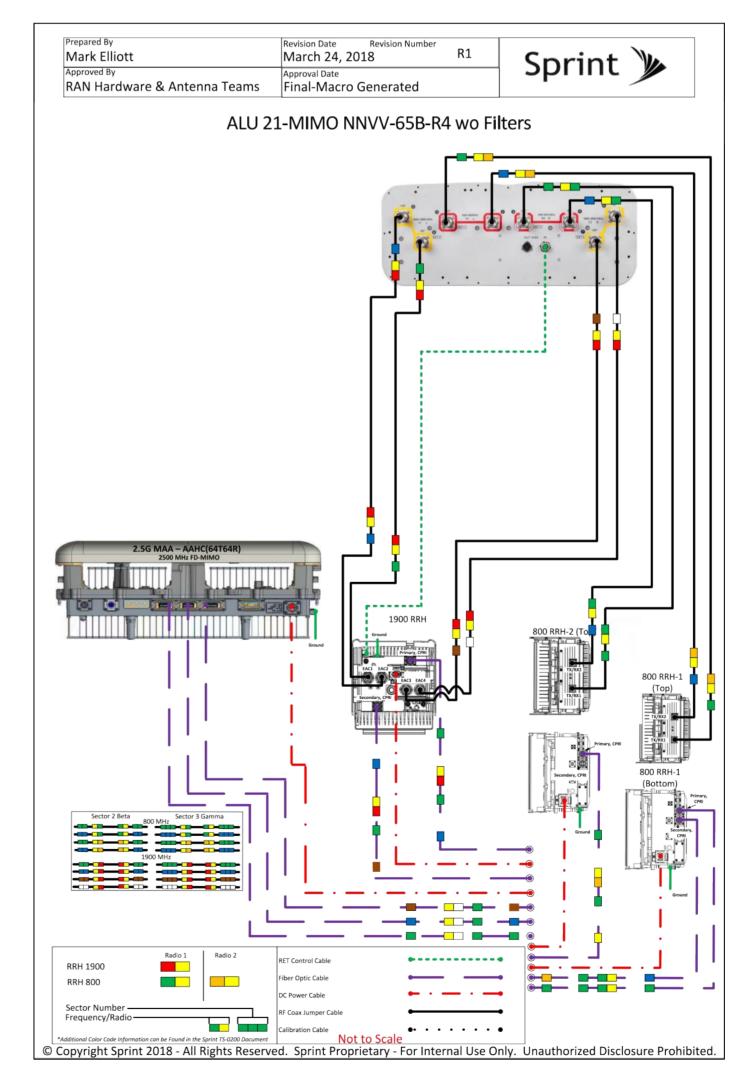




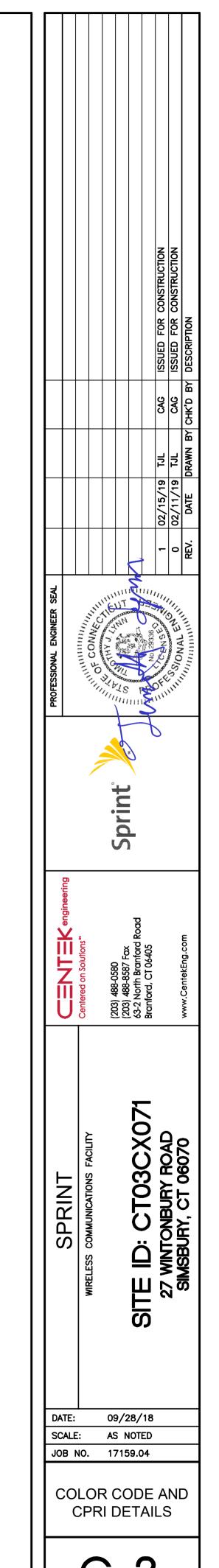














Centered on Solutions 544

Structural Analysis Report

100-ft Existing Self-Supporting Lattice Tower

Proposed Sprint Antenna Upgrade

Sprint Site Ref: CT03XC071

Wintonbury Avenue Simsbury, CT

CENTEK Project No. 17159.04

Date: June 13, 2018

Rev 1: September 17, 2018

OF CONNECTION OF

Prepared for: Transcend Wireless 10 Industrial Ave, Suite 3 Mahwah, NJ 07430

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

Table of Contents

SECTION 1 – REPORT

- INTRODUCTION
- ANTENNA AND APPURTENANCE SUMMARY
- PRIMARY ASSUMPTIONS USED IN THE ANALYSIS
- ANALYSIS
- TOWER LOADING
- TOWER CAPACITY
- FOUNDATION AND ANCHORS
- CONCLUSION

SECTION 2 - CONDITIONS & SOFTWARE

- STANDARD ENGINEERING CONDITIONS
- GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM

SECTION 3 – CALCULATIONS

- tnxTower INPUT/OUTPUT SUMMARY
- tnxTower FEED LINE PLAN
- tnxTower FEED LINE DISTRIBUTION
- tnxTower DETAILED OUTPUT
- ANCHOR BOLT ANALYSIS
- FOUNDATION ANALYSIS

SECTION 4 – REFERENCE MATERIALS

EQUIPMENT CUT SHEETS.

TABLE OF CONTENTS TOC-1

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

Introduction

The purpose of this report is to summarize the results of the non-linear, $P-\Delta$ structural analysis of the antenna upgrade proposed by Sprint on the existing self-supporting lattice tower located in Simsbury, Connecticut.

The host tower is a 100-ft, four-section, three legged, self-supporting tapered lattice tower originally designed and manufactured by Stainless Inc., report no. 1935-S, dated November 3, 1967. The tower geometry, structure member sizes and the foundation system information were obtained from the aforementioned design documents.

Antenna and appurtenance information were obtained from a previous structural report prepared by Centek project no. 13003.06 dated August 1, 2013, a Sprint RF sheet and visual verification from grade conducted by Centek personnel on January 25, 2018.

The existing tower consists of four (4) tapered steel pipe leg sections conforming to ASTM A53 Grade B. Diagonal lateral support bracing consists of steel pipe sections conforming to ASTM A53 Grade B. Horizontal support bracing consists of A36 steel angle construction. The vertical tower sections are connected by bolted flange plates while the pipe legs and bracing are connected by bolted and welded gusset connections. The width of the tower face is 7-ft at the top and 15-ft at the base.

Antenna and Appurtenance Summary

The existing tower was designed to support several communication antennas. The existing, proposed and future loads considered in this analysis consist of the following:

Eversource (Existing):

Appurtenance: One (1) 20-ft dipole leg mounted to the top of the tower. Conduit: One (1) 1-1/4" \varnothing coax cable.

Eversource (Existing):

Appurtenance: Two (2) 3-ft \varnothing microwave dishes on a pipe mast with a RAD center elevations of 89-ft and 85-ft above existing grade.

Conduit: Two (2) 1-1/4" Ø coax cable.

UNKNOWN (Existing):

<u>Antennas</u>: One (1) GPS antenna leg mounted with an elevation of 56-ft above existing grade.

Coax Cable: One (1) 1/2" Ø coax cable.

UNKNOWN (Existing):

Antennas: One (1) GPS antenna leg mounted with an elevation of 12-ft above existing grade.

Coax Cable: One (1) 1/2" Ø coax cable.

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

SPRINT (Existing to Remain):

Antennas: Three (3) 1900MHz 4X45W RRHs and three (3) 800MHz 2X50W RRHs mounted on three (3) existing 12-ft T-Arms with a RAD center elevation of 75-ft above existing grade.

<u>Coax Cables</u>: Three (3) 1-1/4"Ø Hybriflex cables running on a face of the existing tower as specified in Section 3 of this report.

SPRINT (Existing to Remove):

Antennas: Two (2) RFS APXVSPP18-C-A20 and one (1) RFS APXV9ERR18-C-A20 panel antennas mounted on three (3) existing 12-ft T-Arms with a RAD center elevation of 75-ft above existing grade.

SPRINT (Proposed):

Antennas: Three (3) Commscope NNVV-65B-R4 panel antennas, three (3) Nokia AAHC panel antennas and three (3) 800MHz 2X50W RRHs mounted on three (3) existing 12-ft T-Arms with a RAD center elevation of 75-ft above existing grade.

Coax Cables: One (1) 1-1/4" Hybriflex cable running on a face of the existing tower as specified in Section 3 of this report.

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

Primary Assumptions Used in the Analysis

- The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- The tower carries the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- Tower is properly installed and maintained.
- Tower is in plumb condition.
- Tower loading for antennas and mounts as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original tower design documents.
- All members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.
- All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

Analysis

The existing tower was analyzed using a comprehensive computer program entitled tnxTower. The program analyzes the tower, considering the worst case loading condition. The tower is considered as loaded by concentric forces along the tower, and the model assumes that the tower members are subjected to bending, axial, and shear forces.

The existing tower was analyzed for the controlling basic wind speed (3-second gust) with no ice and the applicable wind and ice combination to determine stresses in members as per guidelines of TIA-222-G-2005 entitled "Structural Standard for Antenna Support Structures and Antennas", the American Institute of Steel Construction (AISC) and the Manual of Steel Construction; Load and Resistance Factor Design (LRFD).

The controlling wind speed is determined by evaluating the local available wind speed data as provided in Appendix N of the CSBC¹ and the wind speed data available in the TIA-222-G-2005 Standard.

Tower Loading

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA-222-G-2005, gravity loads of the tower structure and its components, and the application of 1.00" radial ice on the tower structure and its components.

Basic Wind Speed:	Hartford County; v = 90-105 mph (3-second gust)	[Annex B of TIA-222-G-2005]
	Simsbury; v = 93 mph (Nominal)	[Appendix N of the 2018 CT Building Code]

Load Cases: Load Case 1; 93 mph wind speed w/

no ice plus gravity load – used in calculation of tower stresses and rotation.

Load Case 2; 50 mph wind speed w/

1.00" radial ice plus gravity load – used in calculation of tower stresses.

[Annex B of TIA-222-G-2005]

[Appendix N of the 2018 CT

Building Code1

¹ The 2015 International Building Code as amended by the 2018 Connecticut State Building Code (CSBC).

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

Tower Capacity

 Calculated stresses were found to be within allowable limits. This tower was found to be at 88.4% of its total capacity.

Tower Section	Elevation	Stress Ratio (percentage of capacity)	Result
Leg (T4)	0'-0"-25'-0"	77.3%	PASS
Diagonal (T3)	25'-0"-50'-0"	88.4%	PASS

• The tower combined deflection is **0.2782 degrees**.

Deflection (degrees)	Proposed	Allowable	Result
Sway (Tilt)	0.2645	0.5	PASS
Twist	0.0863	0.5	PASS
Combined	0.2782	0.5	PASS

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

Foundation and Anchors

The existing foundation consists of three (3) individual 2'-6" square tapering to 4'-0" square by 4'-0" long piers with eight (8) rock anchors per pier. The foundation properties and sub-grade conditions used in the analysis of the existing foundation were obtained from the aforementioned original Stainless design documents. Tower legs are connected to the foundation by means of (6) 1-1/2"Ø, ASTM A36 anchor bolts per leg, embedded into the concrete foundation structure.

The tower base maximum corner reactions developed from the governing Load Case
 2 were used in the verification of the foundation and its anchors:

Vector	Proposed Reactions
Compression	115 kips
Uplift	101 kips
Shear	15 kips
Total Shear	27 kips
Overturning Moment	1438 kip-ft

The foundation was found to be within allowable limits.

Foundation	Design Limit	TIA-222-G Section 9.4 FS ⁽¹⁾	Proposed Loading (FS) ⁽¹⁾	Result
Reinf. Conc. Pier w/ Rock Anchors	Uplift	1.0	1.16	PASS

Note 1: FS denotes Factor of Safety

The anchor bolts were found to be within allowable limits.

Tower Component	Design Limit	Stress Ratio (percentage of capacity)	Result
Anchor Bolts	Tension	25.8%	PASS

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

Conclusion

This analysis shows that the subject tower <u>is adequate</u> to support the proposed modified antenna configuration.

The analysis is based, in part, on the information provided to this office by Sprint. If the existing conditions are different than the information in this report, Centek Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:

Timothy J. Lynn, PE Structural Engineer

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

Standard Conditions for Furnishing of Professional Engineering Services on Existing Structures

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of Centek Engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to Centek Engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an uncorroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the "as new" condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. Centek Engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

100-ft Existing Self-Supporting Lattice Tower Sprint Antenna Upgrade – CT03XC071 Simsbury, CT Rev 1 ~ September 17, 2018

<u>GENERAL DESCRIPTION OF STRUCTURAL</u> ANALYSIS PROGRAM

tnxTower, is an integrated structural analysis and design software package for Designed specifically for the telecommunications industry, tnxTower, formerly ERITower, automates much of the tower analysis and design required by the TIA/EIA 222 Standard.

tnxTower Features:

- tnxTower can analyze and design 3- and 4-sided guyed towers, 3- and 4-sided selfsupporting towers and either round or tapered ground mounted poles with or without guys.
- The program analyzes towers using the TIA-222-G (2005) standard or any of the previous TIA/EIA standards back to RS-222 (1959). Steel design is checked using the AISC ASD 9th Edition or the AISC LRFD specifications.
- Linear and non-linear (P-delta) analyses can be used in determining displacements and forces in the structure. Wind pressures and forces are automatically calculated.
- Extensive graphics plots include material take-off, shear-moment, leg compression, displacement, twist, feed line, guy anchor and stress plots.
- tnxTower contains unique features such as True Cable behavior, hog rod take-up, foundation stiffness and much more.

100.0 ft 75.0 ft 1.9 12 @ 8.33333 A53-B-35 A53-B-35 50.0 ft HSS5x.312 Ä. 2.2 25.0 ft 5 HSS5x.375 5.9 0.0 ft Face Width (ft) # Panels @ (ft) Diagonal Grade Horizontals Weight (K) Leg Grade Top Girts Diagonals

DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
20' 8 Bay Di-Pole	100	FD-RRH 2x50 800 (Sprint - Existing)	75
3-ft Dish	89	FD-RRH 4x45 1900 (Sprint - Existing)	75
10'x2.5" Pipe Mount	87.5	FD-RRH 4x45 1900 (Sprint - Existing)	75
3-ft Dish	85	FD-RRH 4x45 1900 (Sprint - Existing)	75
NNVV-65B-R4 (Sprint - Proposed)	75	FD-RRH 2x50 800 (Sprint - Proposed)	75
AAHC (Sprint - Proposed)	75	FD-RRH 2x50 800 (Sprint - Proposed)	75
NNVV-65B-R4 (Sprint - Proposed)	75	FD-RRH 2x50 800 (Sprint - Proposed)	75
AAHC (Sprint - Proposed)	75	Rohn T-Arm (1) (Sprint - Existing)	75
NNVV-65B-R4 (Sprint - Proposed)	75	Rohn T-Arm (1) (Sprint - Existing)	75
AAHC (Sprint - Proposed)	75	Rohn T-Arm (1) (Sprint - Existing)	75
FD-RRH 2x50 800 (Sprint - Existing)	75	GPS	56
FD-RRH 2x50 800 (Sprint - Existing)	75	GPS	12

MATERIAL STRENGTH

			-		
GRADE	Fy	Fu	GRADE	Fy	Fu
A53-R-35	35 kei	63 kei			

TOWER DESIGN NOTES

- Tower designed for Exposure C to the TIA-222-G Standard.
 Tower designed for a 93 mph basic wind in accordance with the TIA-222-G Standard.
- Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
- 4. Deflections are based upon a 60 mph wind.
- 5. Tower Structure Class III.
- 6. Topographic Category 4 with Crest Height of 150.00 ft7. TOWER RATING: 88.4%

ALL REACTIONS ARE FACTORED

MAX. CORNER REACTIONS AT BASE:

DOWN: 115 K SHEAR: 15 K

UPLIFT: -101 K

SHEAR: 14 K

AXIAL 66 K

MOMENT SHEAR! 544 kip-ft

TORQUE 1 kip-ft

50 mph WIND - 1.0000 in ICE

AXIAL 14 K

MOMENT SHEAR 1438 kip-ft

TORQUE 7 kip-ft REACTIONS - 93 mph WIND

Centek Engineering Inc.
63-2 North Branford Rd.
Branford, CT 06405
Phone: (203) 488-0580
FAX: (203) 488-8587

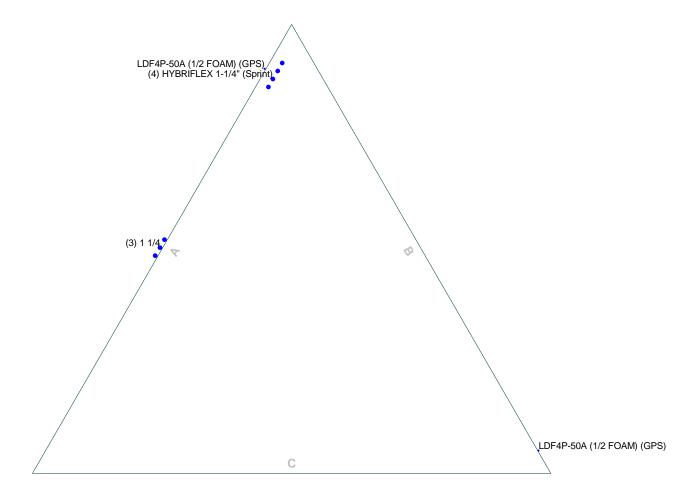
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Project: 100-ft Stainless L		bury Rd, Simsbury, (
Client: Sprint	Drawn by: TJL	App'd:
Code: TIA-222-G	Date: 06/13/18	Scale: NTS
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Feed Line Plan

Flat _____ App In Face

__ Round __

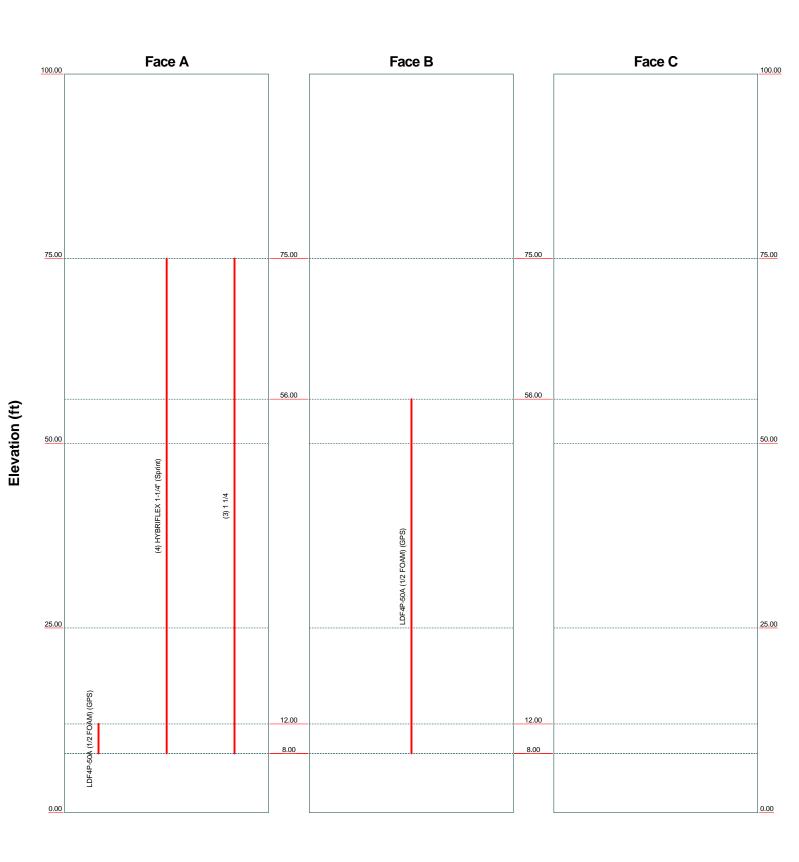
App Out Face



Centek Engineering Inc.	Job:
63-2 North Branford Rd.	Proj
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Phone: (203) 488-0580	Cod
FAX: (203) 488-8587	Path

² 17159.04 - CT03XC	071	
oject: 100-ft Stainless Lattic	e Tower - Wintonbury R	d, Simsbury, C
	' IJL	App'd:
ode: TIA-222-G		Scale: NTS
ath: J:Uobs1715900.Wf04_CT03XC071 Simsbury04_Structural/Backs	up Documentation/ERI Files/100' Self-supporting Lattice Simsbury.eri	Dwg No. E-7

Round ______ Flat _____ App In Face _____ App Out Face _____ Truss Leg



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Branford, CT 06405
Phone: (203) 488-0580
FAX: (203) 488-8587

^{ob:} 17159.04 - CT03X0	b: 17159.04 - CT03XC071				
Project: 100-ft Stainless Lattic	ce Tower - Wintonbury R	d, Simsbury, C			
Op	Drawn by: TJL	App'd:			
Code: TIA-222-G	Date: 06/13/18	Scale: NTS			
Path:		Dwg No. F-7			

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,	Job	Page
	17159.04 - CT03XC071	1 of 25
	Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
	Client Sprint	Designed by TJL

Tower Input Data

The main tower is a 3x free standing tower with an overall height of 100.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 7.00 ft at the top and 15.00 ft at the base.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Basic wind speed of 93 mph.

Structure Class III.

Exposure Category C.

Topographic Category 4.

Crest Height 150.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- √ Use Code Stress Ratios
- √ Use Code Safety Factors Guys Escalate Ice Always Use Max Kz Use Special Wind Profile
- √ Include Bolts In Member Capacity Leg Bolts Are At Top Of Section
- √ Secondary Horizontal Braces Leg
 Use Diamond Inner Bracing (4 Sided)

 SR Members Have Cut Ends
 SR Members Are Concentric

- Distribute Leg Loads As Uniform Assume Legs Pinned
- √ Assume Rigid Index Plate
- √ Use Clear Spans For Wind Area
- √ Use Clear Spans For KL/r
 Retension Guys To Initial Tension
 Bypass Mast Stability Checks
- √ Use Azimuth Dish Coefficients
- √ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination
- √ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder

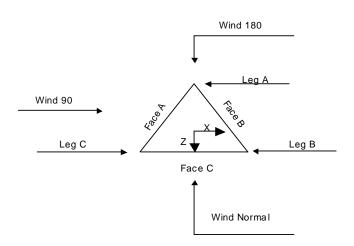
- Use ASCE 10 X-Brace Ly Rules
- √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression
- √ All Leg Panels Have Same Allowable Offset Girt At Foundation
- ✓ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-G Bracing Resist. Exemption Use TIA-222-G Tension Splice Exemption Poles

Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

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63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	2 of 25
Project	Date
100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	14:46:41 06/13/18
Client	Designed by
Sprint	TJL



Triangular Tower

Tower Section Geometry						
Tower	Tower	Assembly	Description	Section	Number	Section
Section	Elevation	Database		Width	of	Length
					Sections	
	ft			ft		ft
T1	100.00-75.00			7.00	1	25.00
T2	75.00-50.00			9.00	1	25.00
Т3	50.00-25.00			11.00	1	25.00
T4	25.00-0.00			13.00	1	25.00

Tower Section Geometry (cont'd)

Tower	Tower	Diagonal	Bracing	Has	Has	Top Girt	Bottom Girt
Section	Elevation	Spacing	Type	K Brace	Horizontals	Offset	Offset
				End			
	ft	ft		Panels		in	in
T1	100.00-75.00	8.33	Diag Down	No	Yes	0.0000	0.0000
T2	75.00-50.00	8.33	Diag Down	No	Yes	0.0000	0.0000
Т3	50.00-25.00	8.33	K Brace Down	No	Yes	0.0000	0.0000
T4	25.00-0.00	8.33	K Brace Down	No	Yes	0.0000	0.0000

Tower Section Geometry (cont'd)

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	3 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client Sprint	Designed by TJL

Tower	Leg	Leg	Leg	Diagonal	Diagonal	Diagonal
Elevation	Type	Size	Grade	Type	Size	Grade
ft						
T1 100.00-75.00	Pipe	HSS5x.188	A53-B-35	Pipe	HSS3x.188	A53-B-35
			(35 ksi)			(35 ksi)
T2 75.00-50.00	Pipe	HSS5x.188	A53-B-35	Pipe	HSS3x.188	A53-B-35
	_		(35 ksi)	_		(35 ksi)
T3 50.00-25.00	Pipe	HSS5x.312	A53-B-35	Pipe	HSS2.5x.125	A53-B-35
	_		(35 ksi)	_		(35 ksi)
T4 25.00-0.00	Pipe	HSS5x.375	A53-B-35	Pipe	HSS2.875x.188	A53-B-35
	-		(35 ksi)	-		(35 ksi)

Tower	No.	Mid Girt	Mid Girt	Mid Girt	Horizontal	Horizontal	Horizontal
Elevation	of	Type	Size	Grade	Type	Size	Grade
	Mid						
ft	Girts						
T1 100.00-75.00	None	Flat Bar		A36	Equal Angle	L3x3x1/4	A36
				(36 ksi)			(36 ksi)
T2 75.00-50.00	None	Flat Bar		A36	Equal Angle	L4x4x1/4	A36
				(36 ksi)			(36 ksi)
T3 50.00-25.00	None	Flat Bar		A36	Equal Angle	L3x3x1/4	A36
				(36 ksi)			(36 ksi)
T4 25.00-0.00	None	Flat Bar		A36	Equal Angle	L3x3x1/4	A36
				(36 ksi)	-		(36 ksi)

Tower Section Geometry (cont'd)

Tower	Gusset	Gusset	Gusset Grade	Adjust. Factor	Adjust.	Weight Mult.	Double Angle	Double Angle	Double Angle
Elevation	Area	Thickness		A_f	Factor		Stitch Bolt	Stitch Bolt	Stitch Bolt
	(per face)			-	A_r		Spacing	Spacing	Spacing
							Diagonals	Horizontals	Redundants
ft	ft ²	in					in	in	in
T1	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
100.00-75.00			(36 ksi)						
T2 75.00-50.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						
T3 50.00-25.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						
T4 25.00-0.00	0.00	0.0000	A36	1	1	1	36.0000	36.0000	36.0000
			(36 ksi)						

Tower Section Geometry (cont'd)

	K Factors ¹										
Tower Elevation	Calc	Calc	Legs	X Brace	K Brace	Single	Girts	Horiz.	Sec. Horiz.	Inner Brace	
Elevation	K Single	Solid		Diags	Diags	Diags			попід.	Бгасе	
	Angles	Rounds		X	X	X	X	X	X	X	
ft				Y	Y	Y	Y	Y	Y	Y	

Centek Engineering Inc.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	4 of 25
Project	Date
100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	14:46:41 06/13/18
Client	Designed by
Sprint	TJL

						K Fac	ctors			
Tower Elevation	Calc K Single	Calc K Solid	Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
ft	Angles	Rounds		X Y	X Y	$X \\ Y$	X Y	X Y	X Y	X Y
T1	Yes	Yes	1	1	1	1	1	1	1	1
100.00-75.00				1	1	1	1	1	1	1
T2	Yes	Yes	1	1	1	1	1	1	1	1
75.00-50.00				1	1	1	1	1	1	1
T3	Yes	Yes	1	1	1	1	1	1	1	1
50.00-25.00				1	1	1	1	1	1	1
T4 25.00-0.00	Yes	Yes	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1

Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

Tower Section Geometry (cont'd)

Tower Elevation	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
ft														
	Net Width	U	Net Width	U	Net Width	U	Net	U	Net	U	Net	U	Net	U
	Deduct		Deduct		Deduct		Width		Width		Width		Width	
	in		in		in		Deduct		Deduct		Deduct		Deduct	
							in		in		in		in	
T1	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
100.00-75.00														
T2 75.00-50.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 50.00-25.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 25.00-0.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

Tower Section Geometry (cont'd)

Tower	Leg	Leg		Diagonal		Top G	irt	Bottom	Girt	Mid G	rt	Long Horizontal		Short Horizontal	
Elevation	Connection														
ft	Type														
		Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.						
		in		in		in		in		in		in		in	
T1	Flange	0.7500	4	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	2	0.6250	0
100.00-75.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T2 75.00-50.00	Flange	0.7500	4	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	2	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T3 50.00-25.00	Flange	0.7500	8	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	2	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T4 25.00-0.00	Flange	1.5000	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	2	0.6250	0
		A36		A325N		A325N		A325N		A325N		A325N		A325N	

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Centek Engineering Inc.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	5 of 25
Project	Date
100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	14:46:41 06/13/18
Client	Designed by
Sprint	TJL

Description	Face or	Allow Shield	Component Type	Placement	Face Offset	Lateral Offset	#	# Per	Clear Spacing	Width or Diameter	Perimeter	Weight
	Leg		71	ft	in	(Frac FW)		Row	in	in	in	plf
LDF4P-50A	A	No	Ar (CaAa)	12.00 - 8.00	0.0000	0.4	1	1	0.6300	0.6300		0.15
(1/2 FOAM)												
(GPS)												
LDF4P-50A	В	No	Ar (CaAa)	56.00 - 8.00	0.0000	0.45	1	1	0.6300	0.6300		0.15
(1/2 FOAM)												
(GPS)												
HYBRIFLEX	Α	No	Ar (CaAa)	75.00 - 8.00	-3.0000	0.4	4	4	1.5400	1.5400		1.30
1-1/4''												
(Sprint)												
1 1/4	Α	No	Ar (CaAa)	75.00 - 8.00	0.0000	0	3	3	1.5500	1.5500		0.66

Feed Line/Linear Appurtenances Section Areas

Tower	Tower	Face	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		ft^2	ft^2	ft^2	ft^2	K
T1	100.00-75.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.00
T2	75.00-50.00	A	0.000	0.000	27.025	0.000	0.18
		В	0.000	0.000	0.378	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.00
T3	50.00-25.00	A	0.000	0.000	27.025	0.000	0.18
		В	0.000	0.000	1.575	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.00
T4	25.00-0.00	A	0.000	0.000	18.629	0.000	0.12
		В	0.000	0.000	1.071	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.00

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness			In Face	Out Face	
	ft	Leg	in	ft^2	ft^2	ft^2	ft^2	K
T1	100.00-75.00	A	3.312	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.00
T2	75.00-50.00	A	3.348	0.000	0.000	112.353	0.000	2.33
		В		0.000	0.000	4.396	0.000	0.10
		C		0.000	0.000	0.000	0.000	0.00
T3	50.00-25.00	A	3.355	0.000	0.000	112.474	0.000	2.33
		В		0.000	0.000	18.351	0.000	0.41
		C		0.000	0.000	0.000	0.000	0.00
T4	25.00-0.00	A	3.201	0.000	0.000	76.635	0.000	1.56
		В		0.000	0.000	11.955	0.000	0.26
		C		0.000	0.000	0.000	0.000	0.00

Feed Line Center of Pressure

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63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	6 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client Sprint	Designed by TJL

Section	Elevation	CP_X	CP_Z	CP_X	CP_Z
				Ice	Ice
	ft	in	in	in	in
T1	100.00-75.00	0.0000	0.0000	0.0000	0.0000
T2	75.00-50.00	-1.2230	-3.4919	-0.4302	-1.9782
T3	50.00-25.00	-1.1708	-3.8640	0.4022	-1.6147
T4	25.00-0.00	-0.9690	-3.2066	0.2825	-1.6021

Shielding Factor Ka

Tower	Feed Line	Description	Feed Line	K_a	K_a
Section	Record No.	_	Segment Elev.	No Ice	Ice
T2	2	LDF4P-50A (1/2 FOAM)	50.00 - 56.00	0.6000	0.6000
T2	3	HYBRIFLEX 1-1/4"	50.00 - 75.00	0.6000	0.6000
T2	4	1 1/4	50.00 - 75.00	0.6000	0.6000
T3	2	LDF4P-50A (1/2 FOAM)	25.00 - 50.00	0.6000	0.6000
T3	3	HYBRIFLEX 1-1/4"	25.00 - 50.00	0.6000	0.6000
T3	4	1 1/4	25.00 - 50.00	0.6000	0.6000
T4	1	LDF4P-50A (1/2 FOAM)	8.00 - 12.00	0.6000	0.6000
T4	2	LDF4P-50A (1/2 FOAM)	8.00 - 25.00	0.6000	0.6000
T4	3	HYBRIFLEX 1-1/4"	8.00 - 25.00	0.6000	0.6000
T4	4	1 1/4	8.00 - 25.00	0.6000	0.6000

Discrete Tower Loads

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		C _A A _A Front	C _A A _A Side	Weight
	Leg	25/20	Lateral	Trajustinent			1.0	Side	
	· ·		Vert						
			ft	0	ft		ft^2	ft^2	K
			ft						
			ft						
Rohn T-Arm (1)	A	From Leg	0.00	0.0000	75.00	No Ice	7.33	7.33	0.38
(Sprint - Existing)			0.00			1/2" Ice	10.00	10.00	0.49
			0.00			1" Ice	12.67	12.67	0.60
Rohn T-Arm (1)	В	From Leg	0.00	0.0000	75.00	No Ice	7.33	7.33	0.38
(Sprint - Existing)			0.00			1/2" Ice	10.00	10.00	0.49
			0.00			1" Ice	12.67	12.67	0.60
Rohn T-Arm (1)	C	From Leg	0.00	0.0000	75.00	No Ice	7.33	7.33	0.38
(Sprint - Existing)			0.00			1/2" Ice	10.00	10.00	0.49
			0.00			1" Ice	12.67	12.67	0.60
GPS	В	From Leg	0.00	0.0000	12.00	No Ice	1.00	1.00	0.01
			0.00			1/2" Ice	1.50	1.50	0.01
			0.00			1" Ice	2.00	2.00	0.02
GPS	A	From Leg	0.00	0.0000	56.00	No Ice	1.00	1.00	0.01
		C	0.00			1/2" Ice	1.50	1.50	0.01
			0.00			1" Ice	2.00	2.00	0.02
NNVV-65B-R4	A	From Leg	3.00	0.0000	75.00	No Ice	14.61	9.17	0.11
(Sprint - Proposed)		Ü	3.00			1/2" Ice	15.13	9.63	0.21
1 1			0.00			1" Ice	15.65	10.11	0.32
AAHC	A	From Leg	3.00	0.0000	75.00	No Ice	4.20	2.06	0.10

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	7 of 25
Project	Date
100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	14:46:41 06/13/18
Client	Designed by
Sprint	TJL

Description	Face or	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C_AA_A Front	C_AA_A Side	Weigh
	Leg		Laierai Vert						
			ft ft	0	ft		ft^2	ft^2	K
			ft						
(Sprint - Proposed)			-3.00			1/2" Ice	4.46	2.25	0.14
			0.00			1" Ice	4.72	2.45	0.17
NNVV-65B-R4	В	From Leg	3.00	0.0000	75.00	No Ice	14.61	9.17	0.11
(Sprint - Proposed)			3.00			1/2" Ice	15.13	9.63	0.21
	_		0.00			1" Ice	15.65	10.11	0.32
AAHC	В	From Leg	3.00	0.0000	75.00	No Ice	4.20	2.06	0.10
(Sprint - Proposed)			-3.00			1/2" Ice	4.46	2.25	0.14
10.000 cen n.			0.00		====	1" Ice	4.72	2.45	0.17
NNVV-65B-R4	C	From Leg	3.00	0.0000	75.00	No Ice	14.61	9.17	0.11
(Sprint - Proposed)			3.00			1/2" Ice	15.13	9.63	0.21
AAHO	0	г т	0.00	0.0000	75.00	1" Ice	15.65	10.11	0.32
AAHC	C	From Leg	3.00	0.0000	75.00	No Ice	4.20	2.06	0.10
(Sprint - Proposed)			-3.00			1/2" Ice 1" Ice	4.46	2.25	0.14
FD-RRH 2x50 800	A	Enom I ao	0.00 3.00	0.0000	75.00	No Ice	4.72 2.06	2.45 1.93	0.17
	Α	From Leg	0.00	0.0000	73.00	1/2" Ice	2.06	2.11	0.09
(Sprint - Existing)			0.00			1" Ice	2.43	2.11	0.09
FD-RRH 2x50 800	В	From Leg	3.00	0.0000	75.00	No Ice	2.43	1.93	0.06
	ь	rioni Leg	0.00	0.0000	73.00	1/2" Ice	2.24	2.11	0.00
(Sprint - Existing)			0.00			1" Ice	2.43	2.11	0.05
FD-RRH 2x50 800	C	From Leg	3.00	0.0000	75.00	No Ice	2.06	1.93	0.06
(Sprint - Existing)	C	110III Leg	0.00	0.0000	75.00	1/2" Ice	2.24	2.11	0.09
(Sprint Existing)			0.00			1" Ice	2.43	2.29	0.11
FD-RRH 4x45 1900	A	From Leg	3.00	0.0000	75.00	No Ice	2.32	2.38	0.06
(Sprint - Existing)		Trom Leg	0.00	0.0000	75.00	1/2" Ice	2.52	2.59	0.08
(Sprint Existing)			0.00			1" Ice	2.74	2.80	0.11
FD-RRH 4x45 1900	В	From Leg	3.00	0.0000	75.00	No Ice	2.32	2.38	0.06
(Sprint - Existing)			0.00			1/2" Ice	2.52	2.59	0.08
(-T			0.00			1" Ice	2.74	2.80	0.11
FD-RRH 4x45 1900	C	From Leg	3.00	0.0000	75.00	No Ice	2.32	2.38	0.0ϵ
(Sprint - Existing)		C	0.00			1/2" Ice	2.52	2.59	0.08
. 1			0.00			1" Ice	2.74	2.80	0.11
FD-RRH 2x50 800	A	From Leg	3.00	0.0000	75.00	No Ice	2.06	1.93	0.06
(Sprint - Proposed)			0.00			1/2" Ice	2.24	2.11	0.09
			0.00			1" Ice	2.43	2.29	0.11
FD-RRH 2x50 800	В	From Leg	3.00	0.0000	75.00	No Ice	2.06	1.93	0.0ϵ
(Sprint - Proposed)			0.00			1/2" Ice	2.24	2.11	0.09
			0.00			1" Ice	2.43	2.29	0.11
FD-RRH 2x50 800	C	From Leg	3.00	0.0000	75.00	No Ice	2.06	1.93	0.06
(Sprint - Proposed)			0.00			1/2" Ice	2.24	2.11	0.09
	_		0.00			1" Ice	2.43	2.29	0.11
20' 8 Bay Di-Pole	C	From Leg	0.50	0.0000	100.00	No Ice	4.00	4.00	0.06
			0.00			1/2" Ice	6.00	6.00	0.10
101.0.511.01		Б Б	10.00	0.0000	07.50	1" Ice	8.00	8.00	0.14
10'x2.5" Pipe Mount	Α	From Face	0.50	0.0000	87.50	No Ice	2.67	2.67	0.06
1			0.00			1/2" Ice	3.91	3.91	0.08

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	8 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client	Designed by TJL

Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				ft	0	0	ft	ft		ft^2	K
3-ft Dish	A	Paraboloid w/o	From	0.00	0.0000		85.00	3.00	No Ice	7.07	0.06
		Radome	Face	0.00					1/2" Ice	7.47	0.10
				0.00					1" Ice	7.86	0.14
3-ft Dish	A	Paraboloid w/o	From	0.00	0.0000		89.00	3.00	No Ice	7.07	0.06
		Radome	Face	0.00					1/2" Ice	7.47	0.10
				0.00					1" Ice	7.86	0.14

Tower Pressures - No Ice

 $G_H = 0.850$

Section	z	K_Z	q_z	A_G	F	A_F	A_R	A_{leg}	Leg	C_AA_A	$C_A A_A$
Elevation					a				%	In	Out
					С					Face	Face
ft	ft		psf	ft^2	e	ft^2	ft^2	ft^2		ft^2	ft^2
T1	87.50	1.231	45	210.425	Α	5.438	29.073	20.856	60.43	0.000	0.000
100.00-75.00					В	5.438	29.073		60.43	0.000	0.000
					C	5.438	29.073		60.43	0.000	0.000
T2 75.00-50.00	62.50	1.146	48	260.425	Α	9.250	30.216	20.856	52.84	27.025	0.000
					В	9.250	30.216		52.84	0.378	0.000
					C	9.250	30.216		52.84	0.000	0.000
T3 50.00-25.00	37.50	1.029	50	310.425	Α	8.438	33.381	20.856	49.87	27.025	0.000
					В	8.438	33.381		49.87	1.575	0.000
					C	8.438	33.381		49.87	0.000	0.000
T4 25.00-0.00	12.50	0.85	49	360.425	Α	9.938	36.201	20.856	45.20	18.629	0.000
					В	9.938	36.201		45.20	1.071	0.000
					C	9.938	36.201		45.20	0.000	0.000

Tower Pressure - With Ice

 $G_H = 0.850$

Section	z	K_Z	q_z	t_Z	A_G	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation						a				%	In	Out
						c					Face	Face
ft	ft		psf	in	ft^2	e	ft^2	ft ²	ft ²		ft^2	ft^2
T1 100.00-75.00	87.50	1.231	11	3.3119	224.236	Α	5.438	86.852	48.484	52.54	0.000	0.000
						В	5.438	86.852		52.54	0.000	0.000
						C	5.438	86.852		52.54	0.000	0.000
T2 75.00-50.00	62.50	1.146	12	3.3479	274.386	Α	9.250	94.520	48.785	47.01	112.353	0.000
						В	9.250	94.520		47.01	4.396	0.000
						C	9.250	94.520		47.01	0.000	0.000
T3 50.00-25.00	37.50	1.029	13	3.3551	324.416	Α	8.438	113.862	48.845	39.94	112.474	0.000
						В	8.438	113.862		39.94	18.351	0.000
						C	8.438	113.862		39.94	0.000	0.000
T4 25.00-0.00	12.50	0.85	12	3.2012	373.774	Α	9.938	118.287	47.561	37.09	76.635	0.000
						В	9.938	118.287		37.09	11.955	0.000
						C	9.938	118.287		37.09	0.000	0.000

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	9 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, C	Date 14:46:41 06/13/18
Client	Designed by TJL

Tower Pressure - Service

 $G_H = 0.850$

Section	z	K_Z	q_z	A_G	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation					a				%	In	Out
					c					Face	Face
ft	ft		psf	ft^2	e	ft^2	ft ²	ft^2		ft^2	ft^2
T1	87.50	1.231	16	210.425	Α	5.438	29.073	20.856	60.43	0.000	0.000
100.00-75.00					В	5.438	29.073		60.43	0.000	0.000
					C	5.438	29.073		60.43	0.000	0.000
T2 75.00-50.00	62.50	1.146	17	260.425	Α	9.250	30.216	20.856	52.84	27.025	0.000
					В	9.250	30.216		52.84	0.378	0.000
					C	9.250	30.216		52.84	0.000	0.000
T3 50.00-25.00	37.50	1.029	18	310.425	Α	8.438	33.381	20.856	49.87	27.025	0.000
					В	8.438	33.381		49.87	1.575	0.000
					C	8.438	33.381		49.87	0.000	0.000
T4 25.00-0.00	12.50	0.85	18	360.425	A	9.938	36.201	20.856	45.20	18.629	0.000
					В	9.938	36.201		45.20	1.071	0.000
					C	9.938	36.201		45.20	0.000	0.000

Tower Forces - No Ice - Wind Normal To Face

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf			2			
ft	K	K	е						ft^2	K	plf	
T1	0.00	1.56	Α	0.164	2.721	45	1	1	19.232	2.00	80.09	C
100.00-75.00			В	0.164	2.721		1	1	19.232			
			C	0.164	2.721		1	1	19.232			
T2	0.18	1.86	Α	0.152	2.766	48	1	1	23.324	3.28	131.07	C
75.00-50.00			В	0.152	2.766		1	1	23.324			
			C	0.152	2.766		1	1	23.324			
T3	0.18	2.17	Α	0.135	2.829	50	1	1	24.201	3.62	144.93	C
50.00-25.00			В	0.135	2.829		1	1	24.201			
			C	0.135	2.829		1	1	24.201			
T4 25.00-0.00	0.13	2.90	Α	0.128	2.854	49	1	1	26.958	3.71	148.48	C
			В	0.128	2.854		1	1	26.958			
			C	0.128	2.854		1	1	26.958			
Sum Weight:	0.49	8.49						OTM	562.26	12.61		
									kip-ft			

Tower Forces - No Ice - Wind 60 To Face

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf						
ft	K	K	e						ft^2	K	plf	
T1	0.00	1.56	Α	0.164	2.721	45	8.0	1	18.144	1.89	75.56	C
100.00-75.00			В	0.164	2.721		0.8	1	18.144			
			C	0.164	2.721		0.8	1	18.144			
T2	0.18	1.86	Α	0.152	2.766	48	0.8	1	21.474	3.07	122.79	C
75.00-50.00			В	0.152	2.766		0.8	1	21.474			
			C	0.152	2.766		0.8	1	21.474			

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Ī	Job	Page
	17159.04 - CT03XC071	10 of 25
	Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
	Client Sprint	Designed by TJL

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf						
ft	K	K	e						ft^2	K	plf	
T3	0.18	2.17	Α	0.135	2.829	50	0.8	1	22.513	3.42	136.85	C
50.00-25.00			В	0.135	2.829		0.8	1	22.513			
			C	0.135	2.829		0.8	1	22.513			
T4 25.00-0.00	0.13	2.90	Α	0.128	2.854	49	0.8	1	24.970	3.47	138.99	C
			В	0.128	2.854		0.8	1	24.970			
			C	0.128	2.854		0.8	1	24.970			
Sum Weight:	0.49	8.49						OTM	528.87	11.85		
									kip-ft			

Tower Forces - No Ice - Wind 90 To Face

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf			_			
ft	K	K	e						ft^2	K	plf	
T1	0.00	1.56	Α	0.164	2.721	45	0.85	1	18.416	1.92	76.69	C
100.00-75.00			В	0.164	2.721		0.85	1	18.416			
			C	0.164	2.721		0.85	1	18.416			
T2	0.18	1.86	Α	0.152	2.766	48	0.85	1	21.937	3.12	124.86	C
75.00-50.00			В	0.152	2.766		0.85	1	21.937			
			C	0.152	2.766		0.85	1	21.937			
T3	0.18	2.17	Α	0.135	2.829	50	0.85	1	22.935	3.47	138.87	C
50.00-25.00			В	0.135	2.829		0.85	1	22.935			
			C	0.135	2.829		0.85	1	22.935			
T4 25.00-0.00	0.13	2.90	Α	0.128	2.854	49	0.85	1	25.467	3.53	141.37	C
			В	0.128	2.854		0.85	1	25.467			
			C	0.128	2.854		0.85	1	25.467			
Sum Weight:	0.49	8.49						OTM	537.22	12.04		
									kip-ft			

Tower Forces - With Ice - Wind Normal To Face

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			c			psf						
ft	K	K	e						ft^2	K	plf	
T1	0.00	8.85	Α	0.412	2.042	11	1	1	61.138	1.20	48.02	C
100.00-75.00			В	0.412	2.042		1	1	61.138			
			C	0.412	2.042		1	1	61.138			
T2	2.42	10.68	Α	0.378	2.109	12	1	1	68.521	2.18	87.31	C
75.00-50.00			В	0.378	2.109		1	1	68.521			
			C	0.378	2.109		1	1	68.521			
T3	2.74	12.49	Α	0.377	2.111	13	1	1	79.782	2.63	105.07	C
50.00-25.00			В	0.377	2.111		1	1	79.782			
			C	0.377	2.111		1	1	79.782			
T4 25.00-0.00	1.82	13.59	Α	0.343	2.188	12	1	1	82.506	2.46	98.25	C
			В	0.343	2.188		1	1	82.506			
			C	0.343	2.188		1	1	82.506			
Sum Weight:	6.99	45.61						OTM	370.68	8.47		

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

٦	Job	Page
	17159.04 - CT03XC071	11 of 25
	Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
	Client	Designed by TJL

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	a									Face
			С			psf			_			
ft	K	K	e						ft^2	K	plf	
									kip-ft			

Tower Forces - With Ice - Wind 60 To Face

Section	Add	Self	F	е	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	a									Face
			С			psf			_			
ft	K	K	e						ft^2	K	plf	
T1	0.00	8.85	Α	0.412	2.042	11	0.8	1	60.050	1.18	47.17	C
100.00-75.00			В	0.412	2.042		0.8	1	60.050			
			C	0.412	2.042		0.8	1	60.050			
T2	2.42	10.68	Α	0.378	2.109	12	0.8	1	66.671	2.14	85.72	C
75.00-50.00			В	0.378	2.109		0.8	1	66.671			
			C	0.378	2.109		0.8	1	66.671			
T3	2.74	12.49	Α	0.377	2.111	13	0.8	1	78.094	2.59	103.56	C
50.00-25.00			В	0.377	2.111		0.8	1	78.094			
			C	0.377	2.111		0.8	1	78.094			
T4 25.00-0.00	1.82	13.59	Α	0.343	2.188	12	0.8	1	80.519	2.41	96.42	C
			В	0.343	2.188		0.8	1	80.519			
			C	0.343	2.188		0.8	1	80.519			
Sum Weight:	6.99	45.61						OTM	364.34	8.32		
									kip-ft			

Tower Forces - With Ice - Wind 90 To Face

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	W	Ctrl.
Elevation	Weight	Weight	а									Face
			С			psf			_			
ft	K	K	e						ft^2	K	plf	
T1	0.00	8.85	Α	0.412	2.042	11	0.85	1	60.322	1.18	47.38	C
100.00-75.00			В	0.412	2.042		0.85	1	60.322			
			C	0.412	2.042		0.85	1	60.322			
T2	2.42	10.68	Α	0.378	2.109	12	0.85	1	67.134	2.15	86.12	C
75.00-50.00			В	0.378	2.109		0.85	1	67.134			
			C	0.378	2.109		0.85	1	67.134			
Т3	2.74	12.49	Α	0.377	2.111	13	0.85	1	78.516	2.60	103.94	C
50.00-25.00			В	0.377	2.111		0.85	1	78.516			
			C	0.377	2.111		0.85	1	78.516			
T4 25.00-0.00	1.82	13.59	Α	0.343	2.188	12	0.85	1	81.015	2.42	96.88	C
			В	0.343	2.188		0.85	1	81.015			
			C	0.343	2.188		0.85	1	81.015			
Sum Weight:	6.99	45.61						OTM	365.92	8.36		
									kip-ft			

Centek Engineering Inc.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	12 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client	Designed by TJL

Tower Forces - Service - Wind Normal To Face

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	a									Face
			c			psf			_			
ft	K	K	e						ft^2	K	plf	
T1	0.00	1.56	Α	0.164	2.721	16	1	1	19.232	0.72	28.99	C
100.00-75.00			В	0.164	2.721		1	1	19.232			
			C	0.164	2.721		1	1	19.232			
T2	0.18	1.86	Α	0.152	2.766	17	1	1	23.324	1.19	47.44	C
75.00-50.00			В	0.152	2.766		1	1	23.324			
			C	0.152	2.766		1	1	23.324			
T3	0.18	2.17	Α	0.135	2.829	18	1	1	24.201	1.31	52.46	C
50.00-25.00			В	0.135	2.829		1	1	24.201			
			C	0.135	2.829		1	1	24.201			
T4 25.00-0.00	0.13	2.90	Α	0.128	2.854	18	1	1	26.958	1.34	53.74	C
			В	0.128	2.854		1	1	26.958			
			C	0.128	2.854		1	1	26.958			
Sum Weight:	0.49	8.49						OTM	203.51	4.57		
									kip-ft			

Tower Forces - Service - Wind 60 To Face

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	a									Face
			c			psf			_			
ft	K	K	e						ft ²	K	plf	
T1	0.00	1.56	Α	0.164	2.721	16	0.8	1	18.144	0.68	27.35	C
100.00-75.00			В	0.164	2.721		0.8	1	18.144			
			C	0.164	2.721		0.8	1	18.144			
T2	0.18	1.86	Α	0.152	2.766	17	0.8	1	21.474	1.11	44.44	C
75.00-50.00			В	0.152	2.766		0.8	1	21.474			
			C	0.152	2.766		0.8	1	21.474			
T3	0.18	2.17	Α	0.135	2.829	18	0.8	1	22.513	1.24	49.53	C
50.00-25.00			В	0.135	2.829		0.8	1	22.513			
			C	0.135	2.829		0.8	1	22.513			
T4 25.00-0.00	0.13	2.90	Α	0.128	2.854	18	0.8	1	24.970	1.26	50.31	C
			В	0.128	2.854		0.8	1	24.970			
			C	0.128	2.854		0.8	1	24.970			
Sum Weight:	0.49	8.49						OTM	191.42	4.29		
									kip-ft			

Tower Forces - Service - Wind 90 To Face

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	w	Ctrl.
Elevation	Weight	Weight	а									Face
			c			psf						
ft	K	K	e						ft^2	K	plf	
T1	0.00	1.56	Α	0.164	2.721	16	0.85	1	18.416	0.69	27.76	C
100.00-75.00			В	0.164	2.721		0.85	1	18.416			
			C	0.164	2.721		0.85	1	18.416			
T2	0.18	1.86	Α	0.152	2.766	17	0.85	1	21.937	1.13	45.19	C

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	13 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client Sprint	Designed by TJL

Section	Add	Self	F	e	C_F	q_z	D_F	D_R	A_E	F	W	Ctrl.
Elevation	Weight	Weight	а									Face
			с			psf						
ft	K	K	e						ft^2	K	plf	
75.00-50.00			В	0.152	2.766		0.85	1	21.937			
			C	0.152	2.766		0.85	1	21.937			
T3	0.18	2.17	Α	0.135	2.829	18	0.85	1	22.935	1.26	50.26	C
50.00-25.00			В	0.135	2.829		0.85	1	22.935			
			C	0.135	2.829		0.85	1	22.935			
T4 25.00-0.00	0.13	2.90	Α	0.128	2.854	18	0.85	1	25.467	1.28	51.17	C
			В	0.128	2.854		0.85	1	25.467			
			C	0.128	2.854		0.85	1	25.467			
Sum Weight:	0.49	8.49						OTM	194.44	4.36		
									kip-ft			

Force Totals

Load	Vertical	Sum of	Sum of	Sum of	Sum of	Sum of Torques
Case	Forces	Forces	Forces	Overturning	Overturning	
		X	Z	Moments, M_x	Moments, M_z	
	K	K	K	kip-ft	kip-ft	kip-ft
Leg Weight	3.75					
Bracing Weight	4.74					
Total Member Self-Weight	8.49			-2.27	0.99	
Total Weight	11.53			-2.27	0.99	
Wind 0 deg - No Ice		-0.09	-16.67	-875.84	8.88	-2.32
Wind 30 deg - No Ice		7.97	-13.82	-725.94	-416.18	-3.35
Wind 60 deg - No Ice		14.33	-7.45	-378.69	-774.12	-3.33
Wind 90 deg - No Ice		16.48	0.44	35.63	-880.82	-2.75
Wind 120 deg - No Ice		14.87	8.59	456.34	-793.35	-1.84
Wind 150 deg - No Ice		8.62	14.06	742.45	-472.74	-0.27
Wind 180 deg - No Ice		0.71	16.13	857.21	-60.57	1.62
Wind 210 deg - No Ice		-7.98	13.81	720.85	419.13	3.35
Wind 240 deg - No Ice		-14.48	8.26	427.69	761.47	4.17
Wind 270 deg - No Ice		-16.23	-0.03	-4.55	860.87	3.53
Wind 300 deg - No Ice		-13.98	-8.07	-432.50	746.17	1.71
Wind 330 deg - No Ice		-8.14	-14.04	-745.80	432.91	-0.51
Member Ice	37.12					
Total Weight Ice	64.17			-22.43	7.51	
Wind 0 deg - Ice		-0.03	-10.58	-555.54	10.08	-0.70
Wind 30 deg - Ice		5.21	-9.02	-476.35	-254.35	-1.02
Wind 60 deg - Ice		9.21	-5.05	-271.57	-464.18	-1.01
Wind 90 deg - Ice		10.59	0.14	-10.07	-531.70	-0.83
Wind 120 deg - Ice		9.30	5.37	251.24	-466.51	-0.54
Wind 150 deg - Ice		5.42	9.10	438.35	-272.80	-0.09
Wind 180 deg - Ice		0.23	10.50	510.63	-12.57	0.49
Wind 210 deg - Ice		-5.21	9.02	431.31	269.68	1.02
Wind 240 deg - Ice		-9.17	5.26	241.89	470.48	1.24
Wind 270 deg - Ice		-10.51	-0.01	-23.18	539.56	1.08
Wind 300 deg - Ice		-9.10	-5.25	-289.12	469.43	0.52
Wind 330 deg - Ice		-5.26	-9.10	-482.83	274.18	-0.16
Total Weight	11.53			-2.27	0.99	
Wind 0 deg - Service		-0.03	-6.03	-316.30	3.39	-0.84
Wind 30 deg - Service		2.88	-5.00	-262.05	-150.46	-1.21
Wind 60 deg - Service		5.19	-2.70	-136.36	-280.01	-1.20
Wind 90 deg - Service		5.97	0.16	13.60	-318.63	-1.00
Wind 120 deg - Service		5.38	3.11	165.87	-286.97	-0.67
Wind 150 deg - Service		3.12	5.09	269.43	-170.93	-0.10

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job		Page
	17159.04 - CT03XC071	14 of 25
Project	ainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
	diffess Lattice Tower - Wintonbury Ita, Simsbury, CT	14.40.41 00/13/10
Client	Sprint	Designed by TJL

Load	Vertical	Sum of	Sum of	Sum of	Sum of	Sum of Torques
Case	Forces	Forces	Forces	Overturning	Overturning	
		X	Z	Moments, M_x	Moments, M_z	
	K	K	K	kip-ft	kip-ft	kip-ft
Wind 180 deg - Service		0.26	5.84	310.96	-21.75	0.59
Wind 210 deg - Service		-2.89	5.00	261.61	151.87	1.21
Wind 240 deg - Service		-5.24	2.99	155.50	275.78	1.51
Wind 270 deg - Service		-5.88	-0.01	-0.94	311.76	1.28
Wind 300 deg - Service		-5.06	-2.92	-155.84	270.24	0.62
Wind 330 deg - Service		-2.95	-5.08	-269.23	156.86	-0.18

Load Combinations

Comb.	Description
No.	T
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	15 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client Sprint	Designed by TJL

Comb.	Description
No.	
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load	Axial	Major Axis Moment	Minor Axis Moment
	,	<i>71</i>		Comb.	K	kip-ft	kip-ft
T1	100 - 75	Leg	Max Tension	7	5.35	-0.34	-0.15
		8	Max. Compression	10	-6.70	0.04	-0.03
			Max. Mx	11	-6.48	0.41	-0.01
			Max. My	6	-2.23	0.00	-0.45
			Max. Vy	11	-0.39	0.41	-0.01
			Max. Vx	14	0.39	-0.01	-0.42
		Diagonal	Max Tension	12	3.37	0.00	0.00
		Dingonar	Max. Compression	8	-3.66	0.00	0.00
			Max. Mx	36	1.28	0.42	0.00
			Max. My	27	0.29	0.00	0.00
			Max. Vy	36	-0.14	0.00	0.00
			Max. Vx	27	0.00	0.00	0.00
		Horizontal	Max Tension	8	2.00	0.00	0.00
		Homzonar	Max. Compression	2	-1.99	0.00	0.00
			Max. Mx	26	0.06	-0.32	0.00
			Max. My	38	0.51	0.00	0.01
			Max. Vy	26	0.31	0.00	0.00
			Max. Vx	38	-0.00	0.00	0.00
		Top Girt	Max Tension	15	0.30	0.00	0.00
		Top Girt	Max. Compression	2	-0.32	0.00	0.00
			Max. Mx	26	-0.03	-0.22	0.00
				38	0.03	0.00	0.00
			Max. My Max. Vy	26	-0.13	0.00	0.01
			Max. Vy	38	-0.13	0.00	0.00
T2	75 - 50	Log	Max Tension	23	31.40	-0.24	0.00
1 4	13 - 30	Leg	Max. Compression	10	-37.81	0.33	0.01
			Max. Mx	10		0.33	
				6	-37.22 -18.44	0.33	0.13 0.37
			Max. My	6 11	-18.44 -0.15	0.08	0.57
			Max. Vy				
		D:1	Max. Vx	8 12	-0.16	-0.00	0.27
		Diagonal	Max Tension		9.98	0.00	0.00
			Max. Compression	16	-9.97	0.00	0.00
			Max. Mx	36	3.63	0.58	0.00
			Max. My	27	0.30	0.00	0.00
			Max. Vy	36	0.17	0.00	0.00
		TT 1 . 1	Max. Vx	27	0.00	0.00	0.00
		Horizontal	Max Tension	8	7.54	0.00	0.00
			Max. Compression	12	-7.55	0.00	0.00
			Max. Mx	37	0.32	-0.60	0.00
			Max. My	38	2.52	0.00	0.01
			Max. Vy	37	-0.23	0.00	0.00
ma		_	Max. Vx	38	0.01	0.00	0.00
T3	50 - 25	Leg	Max Tension	23	56.97	-0.28	-0.03
			Max. Compression	10	-66.37	0.48	0.01
			Max. Mx	11	-65.57	0.48	0.01
			Max. My	8	0.07	-0.02	0.48
			Max. Vy	11	-0.15	0.48	0.01
			Max. Vx	20	0.16	-0.00	-0.48

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	16 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client Sprint	Designed by TJL

Section No.	Elevation ft	Component Type	Condition	Gov. Load	Axial	Major Axis Moment	Minor Axi Moment
				Comb.	K	kip-ft	kip-ft
		Diagonal	Max Tension	17	8.09	0.00	0.00
			Max. Compression	16	-8.20	0.00	0.00
			Max. Mx	38	2.79	0.24	0.00
			Max. My	27	-0.10	0.00	0.00
			Max. Vy	38	-0.09	0.00	0.00
			Max. Vx	27	-0.00	0.00	0.00
		Horizontal	Max Tension	16	7.99	0.00	0.00
			Max. Compression	12	-8.03	0.03	0.00
			Max. Mx	37	0.49	0.21	0.04
			Max. My	27	0.37	0.18	0.04
			Max. Vy	37	0.15	0.21	0.04
			Max. Vx	27	-0.01	0.00	0.00
T4	25 - 0	Leg	Max Tension	23	89.34	-0.49	-0.01
			Max. Compression	10	-102.80	0.00	-0.00
			Max. Mx	11	-89.43	0.51	0.01
			Max. My	8	-0.06	-0.02	0.49
			Max. Vy	11	0.19	0.51	0.01
		Max. Vx	8	0.19	-0.02	0.49	
		Diagonal	Max Tension	17	9.24	0.00	0.00
			Max. Compression	16	-9.39	0.00	0.00
			Max. Mx	32	3.49	0.31	0.00
			Max. My	27	-0.20	0.00	0.00
			Max. Vy	32	-0.11	0.00	0.00
			Max. Vx	27	-0.00	0.00	0.00
		Horizontal	Max Tension	16	6.21	0.00	0.00
			Max. Compression	17	-6.22	0.03	0.01
			Max. Mx	37	0.71	0.23	0.04
			Max. My	35	-0.98	0.22	0.05
			Max. Vy	37	0.16	0.22	0.05
			Max. Vx	34	-0.01	0.00	0.00

Maximum Reactions

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, Z
		Load	K	K	K
		Comb.			
Leg C	Max. Vert	18	110.04	12.49	-7.49
	Max. H _x	18	110.04	12.49	-7.49
	Max. H _z	5	-83.81	-9.17	7.47
	Min. Vert	7	-100.36	-11.83	6.95
	Min. H _x	7	-100.36	-11.83	6.95
	Min. H _z	16	91.93	9.59	-7.66
Leg B	Max. Vert	10	115.26	-12.96	-7.61
	Max. H _x	23	-100.60	11.84	6.96
	Max. H _z	25	-86.73	9.49	7.40
	Min. Vert	23	-100.60	11.84	6.96
	Min. H _x	10	115.26	-12.96	-7.61
	Min. H _z	12	99.05	-10.23	-7.79
Leg A	Max. Vert	2	110.27	-0.13	14.57
	Max. H _x	21	3.90	3.57	0.25
	Max. H _z	2	110.27	-0.13	14.57
	Min. Vert	15	-100.18	-0.00	-13.72
	Min. H _x	9	-1.06	-3.56	-0.18
	Min. Hz	15	-100.18	-0.00	-13.72

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	17 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, C7	Date 14:46:41 06/13/18
Client Sprint	Designed by TJL

Tower Mast Reaction Summary

Load Combination	Vertical	$Shear_x$	$Shear_z$	Overturning Moment, M_x	Overturning Moment, M_z	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	11.53	0.00	0.00	-2.27	0.99	-0.00
1.2 Dead+1.6 Wind 0 deg - No Ice	13.83	-0.14	-26.67	-1372.57	13.83	-3.72
0.9 Dead+1.6 Wind 0 deg - No	10.38	-0.14	-26.67	-1371.46	13.53	-3.72
Ice						
1.2 Dead+1.6 Wind 30 deg - No	13.83	12.75	-22.11	-1137.41	-652.88	-5.37
Ice 0.9 Dead+1.6 Wind 30 deg - No	10.38	12.75	-22.11	1126 27	652.09	-5.36
Ice	10.58	12.75	-22.11	-1136.37	-652.98	-3.30
1.2 Dead+1.6 Wind 60 deg - No	13.83	22.92	-11.93	-591.71	-1216.25	-5.33
Ice						
0.9 Dead+1.6 Wind 60 deg - No	10.38	22.92	-11.93	-590.85	-1216.16	-5.33
Ice 1.2 Dead+1.6 Wind 90 deg - No	13.83	26.38	0.70	58.01	-1383.03	-4.41
Ice	13.63	20.38	0.70	36.01	-1363.03	-4.41
0.9 Dead+1.6 Wind 90 deg - No	10.38	26.38	0.70	58.67	-1382.89	-4.41
Ice						
1.2 Dead+1.6 Wind 120 deg -	13.83	23.80	13.74	717.17	-1245.71	-2.95
No Ice 0.9 Dead+1.6 Wind 120 deg -	10.38	23.80	13.74	717.62	-1245.61	-2.95
No Ice	10.50	23.00	13.71	717.02	12 13.01	2.75
1.2 Dead+1.6 Wind 150 deg -	13.83	13.79	22.49	1165.68	-743.52	-0.42
No Ice	10.00	10.50	22.40	44.5	510.5 0	0.40
0.9 Dead+1.6 Wind 150 deg - No Ice	10.38	13.79	22.49	1165.99	-743.58	-0.43
1.2 Dead+1.6 Wind 180 deg -	13.83	1.13	25.81	1346.10	-97.45	2.59
No Ice						
0.9 Dead+1.6 Wind 180 deg -	10.38	1.13	25.81	1346.36	-97.72	2.59
No Ice	12.92	-12.77	22.10	1121.06	656.92	5.37
1.2 Dead+1.6 Wind 210 deg - No Ice	13.83	-12.//	22.10	1131.06	656.82	5.57
0.9 Dead+1.6 Wind 210 deg -	10.38	-12.77	22.10	1131.39	656.31	5.37
No Ice						
1.2 Dead+1.6 Wind 240 deg -	13.83	-23.17	13.21	671.25	1193.83	6.67
No Ice 0.9 Dead+1.6 Wind 240 deg -	10.38	-23.17	13.21	671.72	1193.16	6.67
No Ice	10.56	-23.17	13.21	0/1./2	1193.10	0.07
1.2 Dead+1.6 Wind 270 deg -	13.83	-25.97	-0.04	-6.39	1350.26	5.65
No Ice						
0.9 Dead+1.6 Wind 270 deg -	10.38	-25.97	-0.04	-5.71	1349.54	5.65
No Ice 1.2 Dead+1.6 Wind 300 deg -	13.83	-22.37	-12.92	-677.93	1170.67	2.74
No Ice	13.03	22.37	12.72	077.55	1170.07	2.7
0.9 Dead+1.6 Wind 300 deg -	10.38	-22.37	-12.92	-677.03	1170.00	2.74
No Ice	10.00	40.00	22.45	44.00.00		0.04
1.2 Dead+1.6 Wind 330 deg - No Ice	13.83	-13.02	-22.47	-1169.22	678.90	-0.81
0.9 Dead+1.6 Wind 330 deg -	10.38	-13.02	-22.47	-1168.18	678.38	-0.81
No Ice					2.2.2	
1.2 Dead+1.0 Ice+1.0 Temp	66.47	0.00	0.00	-22.96	7.74	-0.00
1.2 Dead+1.0 Wind 0 deg+1.0	66.47	-0.03	-10.58	-543.72	10.35	-0.71
Ice+1.0 Temp 1.2 Dead+1.0 Wind 30 deg+1.0	66.47	5.21	-9.02	-466.29	-247.95	-1.04
I.2 Dead+1.0 Willd 30 deg+1.0 Ice+1.0 Temp	00.47	3.41	-9.02	-400.29	-241.33	-1.04
1.2 Dead+1.0 Wind 60 deg+1.0	66.47	9.21	-5.05	-265.95	-453.44	-1.04
Ice+1.0 Temp						

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	18 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client	Designed by TJL

Load Combination	Vertical	$Shear_x$	$Shear_z$	Overturning Moment, M _x	Overturning Moment, M ₂	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
1.2 Dead+1.0 Wind 90 deg+1.0	66.47	10.59	0.14	-10.57	-519.25	-0.85
Ice+1.0 Temp						
1.2 Dead+1.0 Wind 120	66.47	9.30	5.37	244.50	-455.59	-0.55
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 150	66.47	5.42	9.10	427.16	-266.52	-0.09
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 180	66.47	0.23	10.50	497.86	-12.45	0.50
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 210	66.47	-5.21	9.02	420.07	263.79	1.04
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 240	66.47	-9.17	5.26	235.08	460.00	1.26
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 270	66.47	-10.51	-0.01	-23.77	527.57	1.10
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 300	66.47	-9.10	-5.25	-283.63	459.14	0.54
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 330	66.47	-5.26	-9.10	-472.82	268.31	-0.16
deg+1.0 Ice+1.0 Temp						
Dead+Wind 0 deg - Service	11.53	-0.03	-6.03	-312.09	3.85	-0.84
Dead+Wind 30 deg - Service	11.53	2.88	-5.00	-258.90	-146.94	-1.22
Dead+Wind 60 deg - Service	11.53	5.19	-2.70	-135.48	-274.35	-1.21
Dead+Wind 90 deg - Service	11.53	5.97	0.16	11.46	-312.07	-1.00
Dead+Wind 120 deg - Service	11.53	5.38	3.11	160.54	-281.01	-0.67
Dead+Wind 150 deg - Service	11.53	3.12	5.09	261.98	-167.43	-0.10
Dead+Wind 180 deg - Service	11.53	0.26	5.84	302.79	-21.32	0.59
Dead+Wind 210 deg - Service	11.53	-2.89	5.00	254.15	149.27	1.22
Dead+Wind 240 deg - Service	11.53	-5.24	2.99	150.16	270.73	1.51
Dead+Wind 270 deg - Service	11.53	-5.88	-0.01	-3.10	306.11	1.28
Dead+Wind 300 deg - Service	11.53	-5.06	-2.92	-154.98	265.49	0.62
Dead+Wind 330 deg - Service	11.53	-2.95	-5.08	-266.10	154.27	-0.18

Solution Summary

	Sui	n of Applied Force	S		Sum of Reaction	ıs	·
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
1	0.00	-11.53	0.00	0.00	11.53	0.00	0.000%
2	-0.14	-13.83	-26.67	0.14	13.83	26.67	0.000%
3	-0.14	-10.38	-26.67	0.14	10.38	26.67	0.000%
4	12.75	-13.83	-22.11	-12.75	13.83	22.11	0.000%
5	12.75	-10.38	-22.11	-12.75	10.38	22.11	0.000%
6	22.92	-13.83	-11.93	-22.92	13.83	11.93	0.000%
7	22.92	-10.38	-11.93	-22.92	10.38	11.93	0.000%
8	26.38	-13.83	0.70	-26.38	13.83	-0.70	0.000%
9	26.38	-10.38	0.70	-26.38	10.38	-0.70	0.000%
10	23.80	-13.83	13.74	-23.80	13.83	-13.74	0.000%
11	23.80	-10.38	13.74	-23.80	10.38	-13.74	0.000%
12	13.79	-13.83	22.49	-13.79	13.83	-22.49	0.000%
13	13.79	-10.38	22.49	-13.79	10.38	-22.49	0.000%
14	1.13	-13.83	25.81	-1.13	13.83	-25.81	0.000%
15	1.13	-10.38	25.81	-1.13	10.38	-25.81	0.000%
16	-12.77	-13.83	22.10	12.77	13.83	-22.10	0.000%
17	-12.77	-10.38	22.10	12.77	10.38	-22.10	0.000%
18	-23.17	-13.83	13.21	23.17	13.83	-13.21	0.000%
19	-23.17	-10.38	13.21	23.17	10.38	-13.21	0.000%
20	-25.97	-13.83	-0.04	25.97	13.83	0.04	0.000%
21	-25.97	-10.38	-0.04	25.97	10.38	0.04	0.000%
22	-22.37	-13.83	-12.92	22.37	13.83	12.92	0.000%

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	19 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client Sprint	Designed by TJL

	Sui	Sum of Applied Forces			Sum of Reactions			
Load	PX	PY	PZ	PX	PY	PZ	% Error	
Comb.	K	K	K	K	K	K		
23	-22.37	-10.38	-12.92	22.37	10.38	12.92	0.000%	
24	-13.02	-13.83	-22.47	13.02	13.83	22.47	0.000%	
25	-13.02	-10.38	-22.47	13.02	10.38	22.47	0.000%	
26	0.00	-66.47	0.00	0.00	66.47	0.00	0.000%	
27	-0.03	-66.47	-10.58	0.03	66.47	10.58	0.000%	
28	5.21	-66.47	-9.02	-5.21	66.47	9.02	0.000%	
29	9.21	-66.47	-5.05	-9.21	66.47	5.05	0.000%	
30	10.59	-66.47	0.14	-10.59	66.47	-0.14	0.000%	
31	9.30	-66.47	5.37	-9.30	66.47	-5.37	0.000%	
32	5.42	-66.47	9.10	-5.42	66.47	-9.10	0.000%	
33	0.23	-66.47	10.50	-0.23	66.47	-10.50	0.000%	
34	-5.21	-66.47	9.02	5.21	66.47	-9.02	0.000%	
35	-9.17	-66.47	5.26	9.17	66.47	-5.26	0.000%	
36	-10.51	-66.47	-0.01	10.51	66.47	0.01	0.000%	
37	-9.10	-66.47	-5.25	9.10	66.47	5.25	0.000%	
38	-5.26	-66.47	-9.10	5.26	66.47	9.10	0.000%	
39	-0.03	-11.53	-6.03	0.03	11.53	6.03	0.000%	
40	2.88	-11.53	-5.00	-2.88	11.53	5.00	0.000%	
41	5.19	-11.53	-2.70	-5.19	11.53	2.70	0.000%	
42	5.97	-11.53	0.16	-5.97	11.53	-0.16	0.000%	
43	5.38	-11.53	3.11	-5.38	11.53	-3.11	0.000%	
44	3.12	-11.53	5.09	-3.12	11.53	-5.09	0.000%	
45	0.26	-11.53	5.84	-0.26	11.53	-5.84	0.000%	
46	-2.89	-11.53	5.00	2.89	11.53	-5.00	0.000%	
47	-5.24	-11.53	2.99	5.24	11.53	-2.99	0.000%	
48	-5.88	-11.53	-0.01	5.88	11.53	0.01	0.000%	
49	-5.06	-11.53	-2.92	5.06	11.53	2.92	0.000%	
50	-2.95	-11.53	-5.08	2.95	11.53	5.08	0.000%	

Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00000001
3	Yes	4	0.00000001	0.00000001
4	Yes	4	0.00000001	0.00000001
5	Yes	4	0.00000001	0.00000001
6	Yes	4	0.00000001	0.00000001
7	Yes	4	0.00000001	0.00000001
8	Yes	4	0.00000001	0.00000001
9	Yes	4	0.00000001	0.00000001
10	Yes	4	0.00000001	0.00000001
11	Yes	4	0.00000001	0.00000001
12	Yes	4	0.00000001	0.00000001
13	Yes	4	0.00000001	0.00000001
14	Yes	4	0.00000001	0.00000001
15	Yes	4	0.00000001	0.00000001
16	Yes	4	0.00000001	0.00000001
17	Yes	4	0.00000001	0.00000001
18	Yes	4	0.00000001	0.00000001
19	Yes	4	0.00000001	0.00000001
20	Yes	4	0.00000001	0.00000001
21	Yes	4	0.00000001	0.00000001
22	Yes	4	0.00000001	0.00000001
23	Yes	4	0.00000001	0.00000001

Centek Engineering Inc. 63-2 North Branford Rd.

Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

-	Job	Page
	17159.04 - CT03XC071	20 of 25
	Project	Date
	100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	14:46:41 06/13/18
	Client	Designed by
	Sprint	TJL

24	Yes	4	0.00000001	0.00000001
25	Yes	4	0.00000001	0.00000001
26	Yes	4	0.00000001	0.00000001
27	Yes	4	0.00000001	0.00000001
28	Yes	4	0.0000001	0.00000001
29	Yes	4	0.0000001	0.00000001
30	Yes	4	0.00000001	0.00000001
31	Yes	4	0.00000001	0.00000001
32	Yes	4	0.00000001	0.00000001
33	Yes	4	0.0000001	0.00000001
34	Yes	4	0.0000001	0.00000001
35	Yes	4	0.0000001	0.00000001
36	Yes	4	0.00000001	0.00000001
37	Yes	4	0.0000001	0.00000001
38	Yes	4	0.00000001	0.00000001
39	Yes	4	0.00000001	0.00000001
40	Yes	4	0.00000001	0.00000001
41	Yes	4	0.0000001	0.00000001
42	Yes	4	0.00000001	0.00000001
43	Yes	4	0.00000001	0.00000001
44	Yes	4	0.0000001	0.00000001
45	Yes	4	0.00000001	0.00000001
46	Yes	4	0.0000001	0.00000001
47	Yes	4	0.00000001	0.00000001
48	Yes	4	0.00000001	0.00000001
49	Yes	4	0.00000001	0.00000001
50	Yes	4	0.00000001	0.00000001

Maximum Tower Deflections - Service Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	٥	0
T1	100 - 75	0.906	43	0.0591	0.0226
T2	75 - 50	0.590	43	0.0569	0.0171
T3	50 - 25	0.286	43	0.0409	0.0053
T4	25 - 0	0.080	43	0.0228	0.0020

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	0	0	ft
100.00	20' 8 Bay Di-Pole	43	0.906	0.0591	0.0226	Inf
89.00	3-ft Dish	43	0.768	0.0595	0.0209	Inf
87.50	10'x2.5" Pipe Mount	43	0.749	0.0594	0.0206	Inf
85.00	3-ft Dish	43	0.717	0.0592	0.0201	862756
75.00	Rohn T-Arm (1)	43	0.590	0.0569	0.0171	731765
56.00	GPS	43	0.353	0.0454	0.0073	91845
12.00	GPS	43	0.028	0.0114	0.0009	97094

Maximum Tower Deflections - Design Wind

Centek Engineering Inc.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Jo	ob	Page
	17159.04 - CT03XC071	21 of 25
	Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
C	Client Sprint	Designed by TJL

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
T1	100 - 75	4.033	11	0.2645	0.0863
T2	75 - 50	2.625	11	0.2542	0.0628
T3	50 - 25	1.268	11	0.1823	0.0237
T4	25 - 0	0.354	10	0.1015	0.0087

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	0	0	ft
100.00	20' 8 Bay Di-Pole	11	4.033	0.2645	0.0863	601497
89.00	3-ft Dish	11	3.416	0.2657	0.0805	273410
87.50	10'x2.5" Pipe Mount	11	3.332	0.2654	0.0793	240600
85.00	3-ft Dish	11	3.191	0.2645	0.0771	200501
75.00	Rohn T-Arm (1)	11	2.625	0.2542	0.0628	171200
56.00	GPS	11	1.569	0.2022	0.0262	20428
12.00	GPS	10	0.126	0.0509	0.0033	21849

Bolt Design Data

Section No.	Elevation	Component Type	Bolt Grade	Bolt Size	Number Of	Maximum Load per	Allowable Load	Ratio Load	Allowable Ratio	Criteria
1101	ft	1)//	O'aac	in	Bolts	Bolt K	K	Allowable	110000	
T1	100	Leg	A325N	0.7500	4	1.34	29.82	0.045	1	Bolt Tension
		Diagonal	A325N	1.0000	1	3.37	25.65	0.131	1	Member Bearing
		Horizontal	A325N	0.6250	2	1.00	12.43	0.081	1	Bolt Shear
T2	75	Leg	A325N	0.7500	4	7.85	29.82	0.263	1	Bolt Tension
		Diagonal	A325N	1.0000	1	9.98	25.65	0.389	1	Member Bearing
		Horizontal	A325N	0.6250	2	3.77	12.43	0.304	1	Bolt Shear
T3	50	Leg	A325N	0.7500	8	7.12	29.82	0.239	1	Bolt Tension
		Diagonal	A325N	1.0000	1	8.09	17.10	0.473	1	Member Bearing
		Horizontal	A325N	0.6250	2	4.02	12.43	0.323	1	Bolt Shear
T4	25	Leg	A36	1.5000	6	14.89	57.65	0.258	1	Bolt Tension
		Diagonal	A325N	1.0000	1	9.24	25.65	0.360	1	Member Bearing
		Horizontal	A325N	0.6250	2	3.11	12.43	0.250	1	Bolt Shear

Compression Checks

Centek Engineering Inc.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	22 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client Sprint	Designed by TJL

Lea Desian	Data ((Compression)

Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	Ratio P_u
	ft		ft	ft		in^2	K	K	ϕP_n
T1	100 - 75	HSS5x.188	25.03	8.34	58.6 K=1.00	2.6381	-6.70	69.69	0.096 1
T2	75 - 50	HSS5x.188	25.03	8.34	58.6 K=1.00	2.6381	-37.81	69.69	0.543 1
Т3	50 - 25	HSS5x.312	25.03	8.34	60.0 K=1.00	4.3050	-66.37	112.78	0.589 1
T4	25 - 0	HSS5x.375	25.03	8.34	60.7 K=1.00	5.0994	-102.80	133.02	0.773 1

¹ P_u / ϕP_n controls

Diagonal Design Data (Compression)

Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	$Ratio$ P_u
	ft		ft	ft		in^2	K	K	ϕP_n
T1	100 - 75	HSS3x.188	12.02	11.45	137.2 K=1.00	1.5448	-3.66	18.53	0.198 1
Т2	75 - 50	HSS3x.188	13.54	13.01	155.9 K=1.00	1.5448	-9.97	14.35	0.695 1
Т3	50 - 25	HSS2.5x.125	10.57	10.23	145.5 K=1.00	0.8688	-8.20	9.27	0.884 1
Т4	25 - 0	HSS2.875x.188	11.21	10.90	136.7 K=1.00	1.4765	-9.39	17.85	0.526 1

¹ P_u / ϕP_n controls

Horizontal Design Data (Compression)

Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	$Ratio$ P_u
	ft		ft	ft		in^2	K	K	ϕP_n
T1	100 - 75	L3x3x1/4	8.33	7.52	140.0 K=0.92	1.4400	-1.99	16.61	0.120 1
T2	75 - 50	L4x4x1/4	10.33	9.52	134.6 K=0.94	1.9400	-7.55	24.17	0.312 1
Т3	50 - 25	L3x3x1/4	11.00	5.09	111.6 K=1.08	1.4400	-8.03	24.21	0.332 1
T4	25 - 0	L3x3x1/4	14.33	6.76	133.0 K=0.97	1.4400	-6.22	18.38	0.338 1

¹ P_u / ϕP_n controls

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	23 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client Sprint	Designed by TJL

	Top Girt Design Data (Compression)								
Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	Ratio P _u
	ft		ft	ft		in^2	K	K	ϕP_n
T1	100 - 75	L3x3x1/4	7.00	6.58	128.3 K=0.96	1.4400	-0.32	19.62	0.017 1

¹ P_u / ϕP_n controls

Tension Checks

	Leg Design Data (Tension)										
Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	Ratio P _u		
	ft		ft	ft		in^2	K	K	ϕP_n		
T1	100 - 75	HSS5x.188	25.03	8.34	58.6	2.6381	5.35	83.10	0.064 1		
T2	75 - 50	HSS5x.188	25.03	8.34	58.6	2.6381	31.40	83.10	0.378 1		
Т3	50 - 25	HSS5x.312	25.03	8.34	60.0	4.3050	56.97	135.61	0.420 1		
T4	25 - 0	HSS5x.375	25.03	8.34	60.7	5.0994	89.34	160.63	0.556 1		

¹ P_u / ϕP_n controls

	Diagonal Design Data (Tension)								
Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	Ratio P _u
	ft		ft	ft		in^2	K	K	ϕP_n
T1	100 - 75	HSS3x.188	12.02	11.45	137.2	1.5448	3.37	48.66	0.069
T2	75 - 50	HSS3x.188	13.54	13.01	155.9	1.5448	9.98	48.66	0.205
Т3	50 - 25	HSS2.5x.125	10.57	10.23	145.5	0.8688	8.09	27.37	0.296
T4	25 - 0	HSS2.875x.188	11.21	10.90	136.7	1.4765	9.24	46.51	0.199

¹ P_u / ϕP_n controls

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63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	24 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client	Designed by TJL

Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	Ratio P_u
	ft		ft	ft		in^2	K	K	ϕP_n
T1	100 - 75	L3x3x1/4	8.33	7.52	102.2	0.9394	2.00	40.86	0.049 1
T2	75 - 50	L4x4x1/4	10.33	9.52	95.2	1.3144	7.54	57.18	0.132 1
Т3	50 - 25	L3x3x1/4	11.00	5.09	102.4	0.9394	7.99	40.86	0.196 1
T4	25 - 0	L3x3x1/4	14.33	6.76	134.7	0.9394	6.21	40.86	0.152 1

¹ P_u / ϕP_n controls

Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	Ratio P _u
	ft		ft	ft		in ²	K	K	ϕP_n
T1	100 - 75	L3x3x1/4	7.00	6.58	84.9	1.4400	0.30	46.66	0.007 1

¹ P_u / ϕP_n controls

Section Capacity Table

Section	Elevation	Component	Size	Critical	P	ϕP_{allow}	%	Pass
No.	ft	Type		Element	K	K	Capacity	Fail
T1	100 - 75	Leg	HSS5x.188	2	-6.70	69.69	9.6	Pass
T2	75 - 50	Leg	HSS5x.188	23	-37.81	69.69	54.3	Pass
T3	50 - 25	Leg	HSS5x.312	44	-66.37	112.78	58.9	Pass
T4	25 - 0	Leg	HSS5x.375	74	-102.80	133.02	77.3	Pass
T1	100 - 75	Diagonal	HSS3x.188	7	-3.66	18.53	19.8	Pass
T2	75 - 50	Diagonal	HSS3x.188	30	-9.97	14.35	69.5	Pass
T3	50 - 25	Diagonal	HSS2.5x.125	54	-8.20	9.27	88.4	Pass
T4	25 - 0	Diagonal	HSS2.875x.188	84	-9.39	17.85	52.6	Pass
T1	100 - 75	Horizontal	L3x3x1/4	12	-1.99	16.61	12.0	Pass
T2	75 - 50	Horizontal	L4x4x1/4	32	-7.55	24.17	31.2	Pass
T3	50 - 25	Horizontal	L3x3x1/4	67	-8.03	24.21	33.2	Pass
T4	25 - 0	Horizontal	L3x3x1/4	82	-6.22	18.38	33.8	Pass
T1	100 - 75	Top Girt	L3x3x1/4	6	-0.32	19.62	1.7	Pass
		•					Summary	
						Leg (T4)	77.3	Pass
						Diagonal	88.4	Pass
						(T3)		
						Horizontal	33.8	Pass
						(T4)		
						Top Girt	1.7	Pass
						(T1)		
						Bolt Checks	47.3	Pass

Centek Engineering Inc. 63-2 North Branford Rd.

63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587

Job	Page
17159.04 - CT03XC071	25 of 25
Project 100-ft Stainless Lattice Tower - Wintonbury Rd, Simsbury, CT	Date 14:46:41 06/13/18
Client	Designed by TJL

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow} \ K$	% Capacity	Pass Fail
						RATING =	88.4	Pass

 $Program\ Version\ 7.0.5.1\ -\ 2/1/2016\ File: J: Jobs/1715900. WI/04_CT03XC071\ Simsbury/04_Structural/Backup\ Documentation/ERI\ Files/100'\ Self-supporting\ Lattice\ Simsbury.eri$

Subject:

FOUNDATION WITH ROCK ANCHORS

Location:

Rev. 0: 6/13/18

Simsbury, CT

Prepared by: T.J.L. Checked by: C.F.C.

Job No. 17159.04

Rock Anchor Design:

F: (203) 488-8587

Input Data:

Max Pier Reactions:

Uplift = Uplift := 101-kips user input

Shear = Shear := 15·kips user input

Compression = Axial := 115-kips user input

Structure:

Footing Width = $B_{ftg} := 0$ ft user input

Footing Length = $L_{ftg} := 0$ ft user input

Footing Thickness = $T_{fta} := 0$ ft user input

Pier LengthWidth Top = Lpier1 := 2.5ft user input

Pier LengthWidth Bottom = $L_{pier2} = 4.00$ ft user input

Pier Projection Above Grade = $P_p := 3.00 \cdot ft$ user input

Depths:

Depth to Bottom of Footing = $D_{ftg} := 1.00 ft$ user input (from grade line)

Depth to Suitable Rock = D_{rock} := 1.00ft user input (from grade line)

Subgrade Properties:

Internal Friction Angle = $\phi := 35 \text{deg}$ user input

Unit Weight of Earth = $\gamma_{\text{earth}} := 110 \frac{\text{lb}}{\text{ft}}$ user input

UnitWeight of Rock = $\gamma_{\text{rock}} := 165 \frac{\text{lb}}{\text{ft}^3}$ user input

Unit Weight of Conc = $\gamma_{conc} \coloneqq 150 \frac{\text{lb}}{\text{ft}^3} \qquad \qquad \text{user input}$

Ultimate Bearing = Bearing := 24000 psf user input



Subject:

FOUNDATION WITH ROCK ANCHORS

Location:

Rev. 0: 6/13/18

Simsbury, CT

Prepared by: T.J.L. Checked by: C.F.C.

Job No. 17159.04

RockAnchor Properties:

F: (203) 488-8587

Number of Anchors= N_{anchor}:= 8 *user input*

Hole Diameter = hole_d := 2.00in *user input*

Allowable Bond Stress Between $\sigma_{bond} := 175 \cdot psi$ user input Working bond Strength based on Granite Gneiss

Grout Allowable Compressive Stress = $fc_q := 5000 \cdot psi$ user input

Anchor Spacing* (along length) = $S_{anchor} := 3ft$ user input

Required Factor of Safety= F_S := 1 *user input*

RockAnch or Ultimate Strength = Fu_{anchor} := 90ksi *user input* #8 Grade 60 Rebar

RockAnchor Yield Strength = Fy_{anchor} := 60ksi *user input*

RockAnchor Diameter = d_{ra} := 1.000in user input

RockAnchar Area per Group = $A_{\alpha} := 0.79 \text{in}^2$ user input

RockAnch α Allowable Tension = $T_{all} := 0.60 \cdot 71.1 \text{kips} = 42.66 \cdot \text{kips}$

 $\label{eq:total_relation} \mbox{RockAnchor Maximum Working Load to Yield} = \mbox{$T_V := 0.80.71.1$ kips} = 56.88 \cdot \mbox{kips}$

RockAnchor Shear Capacity = $Sh := 0.4 \cdot T_V = 22.75 \cdot kips$

Per Recommendation of PTI For Prestressed RockAncharsand Soil Anchors Section 6.6 Design Load Should not be more than 60% of Specified Minimum Tensile Strength.

Subject:

FOUNDATION WITH ROCK ANCHORS

Location: Simsbury, CT

Prepared by: T.J.L. Checked by: C.F.C.

Rev. 0: 6/13/18 Job No. 17159.04

Calculated Uplift Resistance:

Intermediate Dimension:

Suitable Earth Height = $H := D_{rock} - D_{earth} = 1 ft$

Suitable Rock Height = $Z := (D_{anchor} - D_{rock}) = 10 \text{ ft}$

Total Anchor Width = $W := S_{anchor} = 3ft$

Base Area 1 of Resisting Pyramid = $B_1 := W^2 = 9ft^2$

Base Area 2 of Resisting Pyramid = $B_2 := [tan(\phi) \cdot (Z) \cdot 2 + W]^2 = 289.1 \text{ ft}^2$

Base Area 3 of Resisting Pyramid = $B_3 := [tan(\phi) \cdot (Z + H) \cdot 2 + W]^2 = 338.7 \text{ ft}^2$

 $\text{Total Volume of Concrete} = \\ V_{conc} := \frac{\mathsf{T}_{pier}}{3} \cdot \left(\mathsf{L}_{pier1}^2 + \mathsf{L}_{pier2}^2 + \sqrt{\mathsf{L}_{pier1}^2 \cdot \mathsf{L}_{pier2}^2}\right) = 43 \cdot \mathsf{ft}^3$

Total Volume of Resisting Material = $V_{tot} := \frac{\left[[H + (Z)] \cdot \left(B_1 + B_3 + \sqrt{B_1 \cdot B_3} \right) \right]}{3} = 1477.5 \cdot \text{ft}^3$

Volumeof Rock= $V_{rock} := \frac{\left[(Z) \cdot \left(B_1 + B_2 + \sqrt{B_1 \cdot B_2} \right) \right]}{3} = 1163.8 \cdot \text{ft}^3$

Volume of Earth = $V_{earth} := V_{tot} - V_{rock} - V_{conc} = 270.6 \cdot ft^3$

Total W eight of Concrete = $W_{conc} := V_{conc} \cdot \gamma_{conc} = 6.5 \cdot kips$

Resisting Rock Force = $W_{rock} := V_{rock} \cdot \gamma_{rock} = 192 \cdot kips$

Resisting Earth Force = $W_{earth} := V_{earth} \cdot \gamma_{earth} = 29.8 \cdot kips$

Total Resisting Force = $W_{total} := 0.5 \cdot W_{rock} + 0.5 \cdot W_{earth} + 0.9 \cdot W_{conc} = 116.7 \cdot kips$

Foundation Uplift Check:

Factor of Safety = $\frac{W_{total}}{W_{total}} = 1.16$

 $\label{eq:uplift_Check} \begin{aligned} & \text{Uplift_Check} := \text{ if} \Bigg(\frac{W_{total}}{Uplift} \geq F_{S}, \text{"OK"}, \text{"Overstressed"} \Bigg) \end{aligned}$

Uplift_Check = "OK"

Rock Bearing Capacity Check:

 $\frac{\text{MaxBearing}}{0.75\text{Rearing}} = 0.42$

Rock_Bearing_Check := if $\left(\frac{\text{MaxBearing}}{0.75 \text{Bearing}} \le 1.00, \text{"OK"}, \text{"Overstressed"}\right)$

Rock_Bearing_Check = "OK"



Subject:

FOUNDATION WITH ROCK ANCHORS

Location:

Rev. 0: 6/13/18

Simsbury, CT

Prepared by: T.J.L. Checked by: C.F.C.

Job No. 17159.04

Rock Anchor Tension/Shear Check:

F: (203) 488-8587

 $Tension\,Force\,perAncho\,r\!=\!$

$$T_a := \frac{\text{Uplift} - W_{conc}}{N_{anchor}} = 11.8 \cdot \text{kips}$$

Design Shear Force per Anchor =

$$S_a := \frac{Shear}{N_{anchor}} = 1.9 \cdot kips$$

Reduced Tension For Tension/Shear Combination =

$$T_r := \left[1 - \left(\frac{S_a}{T_{all}}\right)^2\right] \cdot T_{all} = 42.58 \cdot kips$$

Tension Check =

$$\label{eq:tensionCheck} \textit{TensionCheck} := \textit{if} \Big(\textbf{T}_r \geq \textbf{T}_a, \texttt{"OK"} \,, \texttt{"IncreaseSize"} \, \Big) = \texttt{"OK"}$$

Shear Check=

$$ShearCheck := if\!\!\left(Sh \geq S_a, "OK" \;, "IncreaseSize" \;\right) = "OK"$$

Provided Safety Factor =

$$\frac{\mathsf{T_r}}{\mathsf{T_a}} = 3.60$$

$$SafetyFactor := if \left(\frac{T_{f}}{T_{a}} \geq 1.0, "OK" \ , "Overstressed" \right)$$

SafetyFactor = "OK"

Grout Bond Check:

Tension on Rock Anchor =

$$\mathsf{All}_{bond} \coloneqq \pi \cdot \mathsf{hole}_{d} \cdot \sigma_{bond} \cdot \left(\mathsf{D}_{anchor} - \mathsf{D}_{rock} \right) = 132 \cdot \mathsf{kips}$$

$$Bond_Length_Check := if \left(\frac{Uplift}{All_{bond} \cdot N_{anchor}} \le F_S, "OK", "Increase \ Length" \right)$$

Bond_Length_Check = "OK"



RF Design Sheet

Site Identification		
Cascade	CT03XC071	
SMS Schedule ID	12456299	
SMS Schedule Name	DO Macro Upgrade	
PID		
RRU OEM	ALU	
Switch OEM	Alcatel Lucent	
RFDS Issue Date	2017-08-15 00:00:00.0	
RFDS Revision Date	2018-03-29 14:45:54.0	
RFDS Revision	5	

Filter Analysis Complete	YES
RFDS - Issue Date	08/15/2017
Design Status	Complete
Project Description	DO Macro Upgrade - Add 2500 MHz. Include MIMO.

Battery Backup Cabinet Model		
Model Number		
Weight (Lbs.)		
Dimensions (In.)		
Manufacturer		

Junction Box Model		
Model Number		
Weight (Lbs.)		
Dimensions (In.)		
Manufacturer		
Junction Boxes needed at site		

BTS #2 Model		
Model Number		
Weight (Lbs.)		
Dimensions (In.)		
Manufacturer		
Needed at site		

Contact Information			
Engineer Email	Bill.M.Hastings@sprint.com		
Sprint Badged RF Engineer	Bill Hastings		
RF Engineer Email	Bill.M.Hastings@sprint.com		
RF Engineer Phone	978-590-9700		
RF Manager	Jonathan Hull		
RF Manager Email	Jonathan.B.Hull@Sprint.com		
RF Manager Phone	617-233-2920		

Carrier Count		
2500 LTE	3	
1900 LTE	1	
1900 EVDO		
1900 Voice	1	
800 LTE	1	
800 Voice	1	

UE Relay Model			
Model Number			
Weight (Lbs.)			
Dimensions (In.)			
UE Relay Azimuth			
Manufacturer			
UE Relay CL Height (meters)			

ALU Top Hat Model				
Model Number	SPR13MW0264A1			
Weight (Lbs.)	110			
Dimensions (In.)	10.6 x 29.5 x 20.1			
Manufacturer	ALU			
Top Hat Quantity	1			

Power Protection Cabinet Model			
Model Number			
Weight (Lbs.)			
Dimensions (In.)			
Manufacturer			
Power Protection Cabinet			

Location Details				
Latitude	41.89244999			
Longitude	-72.76953888			
Market	Northern Connecticut			
Region	Northeast			
City	Simsbury			
State	СТ			
Zip Code	CT/06070			
County	Hartford			

2500MHz	3
1900MHz	3
800MHz	3

GPS Antenna Model		
Model Number		
Weight (Lbs.)		
Dimensions (In.)		
Manufacturer		
GPS Antenna needed at site		

Repeater Model				
Model Number				
Weight (Lbs.)				
Dimensions (In.)				
Manufacturer				

Growth Cabinet Model				
Model Number				
Weight (Lbs.)				
Dimensions (In.)				
Manufacturer				

BTS #1 Model			
Model Number			
Weight (Lbs.)			
Dimensions (In.)			
Manufacturer			
Number of BTS #1			

A&E Drawing Requirements

03/14/2018 (SP): RFDS revised to include MIMO. 02/13/2018 (SP): RFDS revised to change to Dual Antennas due to KMW backorder. 12/13/2017 (WR): RFDS revised to replace NV dual band antenna with KMW 16 port tri-band antenna for 1900 2T4R, 800 2T4R and 2500 8T8R.
12/11/2017 (WR): RFDS revised to Kepe Existing NV Antenna for 800/1900 and add 1 800/2500 antenna for LTE2.5 8T8R and enhance 2R for 800 MHz.
11/03/2017 (WR): RFDS revised to replace existing NV dual band antenna with Commscope 10 port tri-band antenna and add diplexers for ground mount 1900/800/2500 RRUs.

Additional RF Notes Special Construction Requirements

03/14/2018 (SP): RFDS revised to include MIMO. 02/13/2018 (SP): RFDS revised to change to Dual Antennas due to KMW backorder. 12/13/2017 (WR): RFDS revised to replace NV dual band antenna with KMW 16 port tri-band antenna for 1900 214R, 800 274R and 2500 818R.
12/11/2017 (WR): RFDS revised to Kepe Existing NV Antenna for 800/1900 and add 1 800/2500 antenna for LTE2.5 818R and enhance 2R for 800 MHz.
11/03/2017 (WR): RFDS revised to replace existing NV dual band antenna with Commscope 10 port tri-band antenna and add diplexers for ground mount 1900/800/2500 RRUs.



Band: 2500	Alpha	Beta	Gamma	Delta	Epsilon	Zeta
Radio Model						
Model Number	Nokia MIMO Integrated Radio/Antenna	Nokia MIMO Integrated Radio/Antenna	Nokia MIMO Integrated Radio/Antenna	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	Refer to Antenna model for details	Refer to Antenna model for details	Refer to Antenna model for details	N/A	N/A	N/A
Manufacturer	Nokia	Nokia	Nokia	N/A	N/A	N/A
Number of RRUs needed	1	1	1	0	0	0
Filter Model						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Filter Model 2						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A		N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Filter Model 3						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Trunk Cable 1						
Model Number	MIMO Upgrade Hybrid Nokia	MIMO Upgrade Hybrid Nokia	N/A	N/A	N/A	N/A
Weight (Lbs.)	2.307	2.307	N/A	N/A	N/A	N/A
Dimensions (In.)	1.689	1.689	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Trunk Cable 1 Qty						
Power Junction Cylinder Model						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (Lbs.)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions (In.)	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Power Junction Cylinder Qty	0	0	0	o	0	0
Optical Junction Cylinder Qty no	eeded					
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (Lbs.)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions (In.)	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
Optical Junction Cylinder Qty needed	0	0	0	0	0	0



Band: 1900	Alpha	Beta	Gamma	Delta	Epsilon	Zeta
Radio Model						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Number of RRUs needed	0	0	0	0	0	0
Filter Model				•		
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Filter Model 2						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A		N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Filter Model 3						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Trunk Cable 1						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (Lbs.)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions (In.)	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Trunk Cable 1 Qty						
Power Junction Cylinder Model				•		
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (Lbs.)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions (In.)	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
Power Junction Cylinder Qty	0	0	0	0	0	0
Optical Junction Cylinder Qty no	eeded					•
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (Lbs.)		N/A	N/A	N/A	N/A	N/A
Dimensions (In.)	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Optical Junction Cylinder Qty needed	h	0	0	0	0	0
	•	<u> </u>	·	+	·	



Band: 800	Alpha	Beta	Gamma	Delta	Epsilon	Zeta
Radio Model						
Model Number	RRH-2x50-800	RRH-2x50-800	RRH-2x50-800	N/A	N/A	N/A
Weight (lbs)	69.1	69.1	69.1	N/A	N/A	N/A
Dimensions	16 x 13 x 10	16 x 13 x 10	16 x 13 x 10	N/A	N/A	N/A
Manufacturer	ALU	ALU	ALU	N/A	N/A	N/A
Number of RRUs needed	1	1	1	0	0	0
Filter Model						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Filter Model 2						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A		N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Filter Model 3						
Model Number	N/A	N/A	N/A	N/A	N/A	N/A
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Trunk Cable 1						
Model Number		N/A	N/A	N/A	N/A	N/A
Weight (Lbs.)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions (In.)	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Trunk Cable 1 Qty						
Power Junction Cylinder Model						
Model Number		N/A	N/A	N/A	N/A	N/A
Weight (Lbs.)		N/A	N/A	N/A	N/A	N/A
Dimensions (In.)		N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Power Junction Cylinder Qty	0	0	0	0	0	0
Optical Junction Cylinder Qty no	I		1	1		1
Model Number		N/A	N/A	N/A	N/A	N/A
Weight (Lbs.)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions (In.)	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Optical Junction Cylinder Qty needed	0	0	0	0	0	0



Band: 2500	Alpha	Beta	Gamma	Delta	Epsilon	Zeta	
Antenna1		•		•		•	
Model Number	AAHC	AAHC	AAHC				
Weight (lbs)	103.7	103.7	103.7	N/A	N/A	N/A	
Dimensions	25.6 x 19.7 x 9.64	25.6 x 19.7 x 9.64	25.6 x 19.7 x 9.64	N/A	N/A	N/A	
Manufacturer	Nokia	Nokia	Nokia	N/A	N/A	N/A	
Ant1 Top Jumper Make/Mode/Qtyl	2.5 Jumper 8	2.5 Jumper 8	2.5 Jumper 8	N/A 0	N/A 0	N/A 0	
Ant 1 RF requested Diameter	1/2"	1/2"	1/2"	N/A	N/A	N/A	
Ant 1 RF requested Top Jumper Length(ft)	8	8	8	N/A	N/A	N/A	
Antenna 1 Azimuth	0	120	240	N/A	N/A	N/A	
Antenna 1 Mechanical DT	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 1 Center Line (ft)	75.0000024	75.0000024	75.0000024	N/A	N/A	N/A	
Antenna 1 Electrical DT	2	2	2	N/A	N/A	N/A	
Antenna 1 Electrical DT 2	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 1 Electrical DT 3	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 1 Twist	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna2							
Model Number							
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A	
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A	
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A	
Ant2 Top Jumper Make/Mode/Qtyl	N/A 0	N/A 0	N/A 0	N/A 0	N/A 0	N/A 0	
Ant 2 RF Top Jumper Diameter	N/A	N/A	N/A	N/A	N/A	N/A	
Ant 2 RF Top Jumper Length(ft)	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 2 Azimuth	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 2 Mechanical DT	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 2 Center Line (ft)	N/A	N/A I		N/A	N/A	N/A	
Antenna 2 Electrical DT	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 2 Electrical DT 2	N/A	N/A	N/A	N/A N/A		N/A	
Antenna 2 Electrical DT 3	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 2 Twist	N/A	N/A	N/A	N/A	N/A	N/A	
	- ·						



Band: 1900	Alpha		Beta		Gamma	Delta			Epsilon		Zeta	
Antenna1									•			
Model Number	NNVV-65B-R4		NNVV-65B-R4		NNVV-65B-R4							
Weight (lbs)	84.7		84.7		84.7		N/A		N/A	N/A	N/A	
Dimensions	72 x 19.6 x 7.8		72 x 19.6 x 7.8		72 x 19.6 x 7.8		N/A		N/A	N/A		
Manufacturer	CommScope		CommScope		CommScope		N/A		N/A	N/A		
Ant1 Top Jumper Make/Mode/Qtyl	800/1900 Jumper	4	800/1900 Jumper	4	800/1900 Jumper	4	N/A	0	N/A 0	N/A		0
Ant 1 RF requested Diameter	1/2"		1/2"		1/2"		N/A		N/A	N/A		
Ant 1 RF requested Top Jumper Length(ft)	8		8		8		N/A		N/A	N/A		
Antenna 1 Azimuth	0		120		240		N/A		N/A	N/A		
Antenna 1 Mechanical DT	N/A		N/A		N/A		N/A		N/A	N/A		
Antenna 1 Center Line (ft)	75.0000024		75.0000024		75.0000024		N/A		N/A	N/A		
Antenna 1 Electrical DT	3		3		3		N/A		N/A	N/A		
Antenna 1 Electrical DT 2	N/A		N/A		N/A		N/A		N/A		N/A	
Antenna 1 Electrical DT 3	N/A	N/A		N/A		N/A		N/A		N/A		
Antenna 1 Twist	N/A		N/A		N/A N/A		N/A N/A		N/A			
Antenna2												
Model Number												
Weight (lbs)	N/A		N/A		N/A		N/A		N/A	N/A	N/A	
Dimensions	N/A		N/A		N/A		N/A		N/A		N/A	
Manufacturer	N/A		N/A		N/A		N/A		N/A			
Ant2 Top Jumper Make/Mode/Qtyl	N/A	0	N/A	0	N/A	0	N/A	0	N/A 0	N/A		
Ant 2 RF Top Jumper Diameter	N/A		N/A		N/A		N/A		N/A		N/A	
Ant 2 RF Top Jumper Length(ft)	N/A		N/A		N/A		N/A		N/A	N/A		
Antenna 2 Azimuth	N/A		N/A		N/A		N/A		N/A	N/A		
Antenna 2 Mechanical DT	N/A	N/A			N/A		N/A		N/A			
Antenna 2 Center Line (ft)	N/A		N/A		N/A		N/A		N/A	N/A		
Antenna 2 Electrical DT	N/A N		N/A		N/A		N/A		N/A			
Antenna 2 Electrical DT 2	N/A		N/A		N/A		N/A		N/A	N/A		
Antenna 2 Electrical DT 3	N/A		N/A		N/A		N/A		N/A I			
Antenna 2 Twist	N/A		N/A		N/A		N/A		N/A	N/A		



Band: 800	Alpha	Beta	Gamma	Delta	Epsilon	Zeta	
Antenna1							
Model Number	Antenna assigned on a different band	Antenna assigned on a different band	Antenna assigned on a different band				
Weight (lbs)	0	0	0	N/A	N/A	N/A	
Dimensions	0 x 0 x 0	0 x 0 x 0	0 x 0 x 0	N/A	N/A	N/A	
Manufacturer	-	-	-	N/A	N/A	N/A	
Ant1 Top Jumper Make/Mode/Qtyl	800/1900 Jumper 2	800/1900 Jumper 2	800/1900 Jumper 2	N/A 0	N/A 0	N/A 0	
Ant 1 RF requested Diameter	1/2"	1/2"	1/2"	N/A	N/A	N/A	
Ant 1 RF requested Top Jumper Length(ft)	8	8	8	N/A	N/A	N/A	
Antenna 1 Azimuth	0	120	240	N/A	N/A	N/A	
Antenna 1 Mechanical DT	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 1 Center Line (ft)	75.0000024	75.0000024	75.0000024	N/A	N/A	N/A	
Antenna 1 Electrical DT	5	5	5	N/A	N/A	N/A	
Antenna 1 Electrical DT 2	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 1 Electrical DT 3	N/A	N/A N/A N		N/A N/A		N/A	
Antenna 1 Twist	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna2							
Model Number							
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A	
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A	
Manufacturer	N/A	N/A	N/A	N/A	N/A		
Ant2 Top Jumper Make/Mode/Qtyl	N/A 0	N/A 0	N/A 0	N/A 0	N/A 0	N/A	
Ant 2 RF Top Jumper Diameter	N/A	N/A	N/A	N/A	N/A	N/A	
Ant 2 RF Top Jumper Length(ft)	N/A	N/A	N/A		N/A	N/A	
Antenna 2 Azimuth	N/A N/A		N/A	N/A	N/A	N/A	
Antenna 2 Mechanical DT	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 2 Center Line (ft)	N/A	N/A		N/A	N/A	N/A	
Antenna 2 Electrical DT	N/A N/A			N/A	N/A	N/A	
Antenna 2 Electrical DT 2	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 2 Electrical DT 3	N/A	N/A	N/A	N/A	N/A	N/A	
Antenna 2 Twist	N/A	N/A	N/A	N/A	N/A	N/A	



		1	1	I		1
Band: 2500	Alpha	Beta	Gamma	Delta	Epsilon	Zeta
Antenna1 Split			I			
Model Number				N1/A	NI/A	NI/A
Weight (lbs)		N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Accept Proposed Ant1 Model Change?	N/A	N/A	N/A	N/A	N/A	N/A
Antenna 1 band combined with	N/A	N/A	N/A	N/A	N/A	N/A
Antenna 1 Upper Passive Component Mo						
Model Number						
Weight (lbs)		N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
Ant1 Upper Passive Comp Qty needed	0	0	0	0	0	0
Ant1 Upper Pass Comp band combi with						
Antenna 1 Lower Passive Component M	odel					
Model Number						
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Ant1 Lower Passive Comp Qty needed	0	0	0	0	0	0
Ant1 Low Pass Comp band comb with						
Position Ant 1						
Antenna2 Split						
Model Number						
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Accept Proposed Ant2 Model Change?	N/A	N/A	N/A	N/A	N/A	N/A
Antenna 2 band combined with						
Antenna 2 Upper Passive Component Mo	odel		<u> </u>			
Model Number						
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Ant2 Upper Passive Comp Qty needed	0	0	0	0	0	0
Antenna 2 Lower Passive Component M	odel		<u> </u>			
Model Number						
Weight (lbs)		N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
	_			0	0	0
Ant1 Lower Passive Comp Qty needed	0	0	0	<u> </u>	V	U .
Ant1 Lower Passive Component band combined with						
Position Ant 2						



Band: 1900	Alaba	Beta	Gamma	Delta	Ensilen	Zeta
	Alpha	Бега	Gamma	Delta	Epsilon	Zeta
Antenna1 Split Model Number						
Weight (lbs)		N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
Wallufacturer	IN/A	N/A	IN/A		IN/A	
Accept Proposed Ant1 Model Change?		N/A	N/A	N/A	N/A	N/A
Antenna 1 band combined with		800MHz	800MHz	N/A	N/A	N/A
Antenna 1 Upper Passive Component Mo						
Model Number						
Weight (lbs)		N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
Ant1 Upper Passive Comp Qty needed	0	0	0	0	0	0
Ant1 Upper Pass Comp band combi with						
Antenna 1 Lower Passive Component M	odel					
Model Number						
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
Ant1 Lower Passive Comp Qty needed		0	0	0	0	0
Ant1 Low Pass Comp band comb with						
Position Ant 1						
Antenna2 Split						
Model Number						
Weight (lbs)		N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Accept Proposed Ant2 Model Change?	N/A	N/A	N/A	N/A	N/A	N/A
Antenna 2 band combined with						
Antenna 2 Upper Passive Component Mo	odel					
Model Number						
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Ant2 Upper Passive Comp Qty needed	0	0	0	0	0	0
Antenna 2 Lower Passive Component M	odel					
Model Number						
Weight (lbs)		N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
						0
Ant1 Lower Passive Comp Qty needed		0	0	0	0	U
Ant1 Lower Passive Component band combined with						
Position Ant 2						

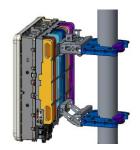


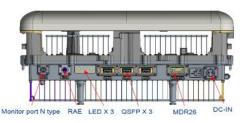
5 . 800			1 4	l		l
Band: 800	Alpha	Beta	Gamma	Delta	Epsilon	Zeta
Antenna1 Split Model Number				I		
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
Mariarastars						
Accept Proposed Ant1 Model Change?	N/A	N/A	N/A	N/A	N/A	N/A
Antenna 1 band combined with	1900MHz	1900MHz	1900MHz	N/A	N/A	N/A
Antenna 1 Upper Passive Component Mo	odel					
Model Number						
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
Ant1 Upper Passive Comp Qty needed	0	0	0	0	0	0
Ant1 Upper Pass Comp band combi with						
Antenna 1 Lower Passive Component M	odel					
Model Number						
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Ant1 Lower Passive Comp Qty needed	0	0	0	0	0	0
Ant1 Low Pass Comp band comb with						
Position Ant 1						
Antenna2 Split Model Number						I
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions		N/A	N/A	N/A	N/A	N/A
Manufacturer		N/A	N/A	N/A	N/A	N/A
		IN/A	IN/A			
Accept Proposed Ant2 Model Change?	N/A	N/A	N/A	N/A	N/A	N/A
Antenna 2 band combined with						
Antenna 2 Upper Passive Component Mo	odel					
Model Number	0401					
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
	0	0	0	0	0	0
Ant2 Upper Passive Comp Qty needed	•	•	<u> </u>	•		, , , , , , , , , , , , , , , , , , ,
Antenna 2 Lower Passive Component M	odel					<u> </u>
Model Number						
Weight (lbs)	N/A	N/A	N/A	N/A	N/A	N/A
Dimensions	N/A	N/A	N/A	N/A	N/A	N/A
Manufacturer	N/A	N/A	N/A	N/A	N/A	N/A
Aut I a Si	0	0	0	0	0	0
Ant1 Lower Passive Comp Qty needed		0	•		-	<u> </u>
Ant1 Lower Passive Component band combined with						
Position Ant 2						
l—————————————————————————————————————			-	-		



TD LTE 2.5G Massive MIMO Adaptive Antenna (MAA) – AAHC







Category	Description	Unit	AAHC
	3GPP Band		B41
Spectrum	Operating frequency	MHz	2496-2690
	Number of TX/RX paths	#	64T64R
	Instantaneous Bandwidth IBW	MHz	194
RF characteristic	Occupied Bandwidth OBW	MHz	60
	Total Output power	W	120
	EIRP	dBm	74.8
	TX OBUE in B41 for sum of all 64 pipes at 1MHz offset	dBm/MHz	-13 sum of all ports
	Emission at IPWireless 2558-2568MHz	dBm/MHz	-57 sum of all ports
	Emission at NEXTRADAR at 2704-3000MHz	dBm/MHz	-27 sum of all ports
	Power inputs		2 pin, and with APPB/APPC
Power	Supply Voltage / Voltage Range	V	-48V DC voltage (-40.5V~-57V)
	Typical Power Consumption	W	75% duty cycle, 1400W for LTE
	Optical Interface		3x QSFP (4 x 9.8G CPRI each)
	RAE Interface		Circle connector, AISG-ES-RAE v2.1.0
Interface	LMI interface		MDR26
	Monitor interface	1	N Female
	Antenna array		8x8x2
	Element Polarization	H/V or ± 45	± 45
	Gain [Broadcast 65 HBW]	dBi	15.2
	Horizontal BW [Broadcast] (@ -3dB)	Degrees	65
	Vertical BW [Broadcast] (@ -3dB)	Degrees	9
	Mechanical Downtilt Range	Degrees	± 5
	Electrical Downtilt Range	Degrees	± 10
	Cross Polar Isolation [Element]	dB	19
Antenna	Front-to-Back Ratio [Broadcast] (@ 180° ±15° cone)	dB	25
Specifications	Element Spacing	λ (mm)	horizontal 57.5, Vertical 80
	Upper Side Lobe Suppression (1st USLS) [Broadcast]	dB	16
	Cross Polar Discrimination [Broadcast] (@ -3dB)	dB	10
	Traffic (Service) Beam Azmithual Pan	Degrees	± 55
	Traffic (Service) Beam Elevational Tilt	Degrees	± 10
	Azimuth Beamwidth Squint (@ Boresight)	Degrees	configurable
	Broadcast Tracking @ ±60°	dBi	2
	Dimensions (LxWxD)	mm (in)	651x501x245 mm (25.6x19.7x9.6 in)
	Weight	kg (lb)	47Kg (103.6lb)
	Max Wind Speed	kmh/mph	200kmh (125 mph)
	Wind Load Front/Side/Rear @ 150kmh	N(lbF)	349 /168/130 N (78.5 / 37.8 /29.2 lbF)
	Radom Material	14(15)	PC
Mechanical	Radom Color		Cold Gray
Specifications	Mounting Kit	mm (in)	FPKA/FPKB/FPKC
	Operational Temperature Range	C(F)	-40 ~ 55© -40 ~ 131(F)
	Ingress protection class	Cli /	IP65
	Installation options	1	Pole, Wall
	Surge protection	kA	20
	ourge protection	KA	40

Product Specifications





NNVV-65B-R4

8-port sector antenna, 4x 698-896 and 4x 1695-2690 MHz, 65° HPBW, 4x RET

- Uses the 4.3-10 connector which is 40 percent smaller than the 7-16 DIN connector
- Supports re-configurable antenna sharing capability enabling control of the internal RET system using up to two separate RET compatible OEM radios
- All internal RET actuators are connected in "Cascaded MRET" configuration

Electrical Specifications

Frequency Band, MHz	698-806	806-896	1695-1880	1850-1990	1920-2180	2300-2500	2500-2690
Gain, dBi	14.5	14.9	16.8	17.2	17.5	18.1	17.8
Beamwidth, Horizontal, degrees	66	64	60	60	62	59	64
Beamwidth, Vertical, degrees	11.7	10.4	7.3	6.8	6.4	5.4	5.1
Beam Tilt, degrees	2-14	2-14	2-12	2-12	2-12	2-12	2-12
USLS (First Lobe), dB	16	18	14	16	15	16	18
Front-to-Back Ratio at 180°, dB	31	34	38	38	37	33	30
Isolation, dB	25	25	25	25	25	25	25
Isolation, Intersystem, dB	25	25	25	25	25	25	25
VSWR Return Loss, dB	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0	1.5 14.0
PIM, 3rd Order, 2 x 20 W, dBc	-150	-150	-150	-150	-150	-150	-150
Input Power per Port at 50°C, maximum, watts	300	300	250	250	250	200	200
Polarization	±45°	±45°	±45°	±45°	±45°	±45°	±45°
Impedance	50 ohm						

Electrical Specifications, BASTA*

Frequency Band, MHz	698-806	806-896	1695-1880	1850-1990	1920-2180	2300-2500	2500-2690
Gain by all Beam Tilts, average, dBi	14.1	14.6	16.5	16.9	17.0	17.6	17.3
Gain by all Beam Tilts Tolerance, dB	±0.5	±0.5	±0.7	±0.4	±0.5	±0.6	±0.7
	2 ° 14.2	2 ° 14.7	2° 16.6	2° 16.8	2° 16.9	2° 17.5	2 ° 16.9
Gain by Beam Tilt, average, dBi	8 ° 14.2	8 ° 14.7	7° 16.7	7° 17.1	7° 17.2	7° 17.9	7 ° 17.5
	14 ° 13.9	14 ° 14.2	12 ° 16.2	12 ° 16.7	12 ° 16.7	12 ° 17.3	12 ° 17.0
Beamwidth, Horizontal Tolerance, degrees	±3.9	±3.9	±5.7	±2.7	±3.1	±7.9	±8
Beamwidth, Vertical Tolerance, degrees	±0.9	±0.8	±0.7	±0.5	±0.6	±0.4	±0.2
USLS, beampeak to 20° above beampeak, dB	16	18	14	15	14	14	14
Front-to-Back Total Power at 180° ± 30°, dB	20	20	31	31	28	28	26
CPR at Boresight, dB	21	20	18	18	19	19	20
CPR at Sector, dB	8	6	8	8	7	8	5

^{*} CommScope® supports NGMN recommendations on Base Station Antenna Standards (BASTA). To learn more about the benefits of BASTA, download the whitepaper Time to Raise the Bar on BSAs.

Array Layout

Product Specifications



NNVV-65B-R4

RF Connector Quantity, high band

RF Connector Interface 4.3-10 Female

Grounding Type RF connector inner conductor and body grounded to reflector and

mounting bracket

Radiator Material Low loss circuit board
Radome Material Fiberglass, UV resistant

Reflector Material Aluminum
RF Connector Location Bottom

Wind Loading, frontal 685.0 N @ 150 km/h

154.0 lbf @ 150 km/h

Wind Loading, lateral 232.0 N @ 150 km/h

52.2 lbf @ 150 km/h

Wind Loading, maximum 889.0 N @ 150 km/h

199.9 lbf @ 150 km/h

Wind Speed, maximum 241 km/h | 150 mph

Dimensions

 Length
 1828.0 mm | 72.0 in

 Width
 498.0 mm | 19.6 in

 Depth
 197.0 mm | 7.8 in

 Net Weight, without mounting kit
 35.1 kg | 77.4 lb

Remote Electrical Tilt (RET) Information

Input Voltage 10–30 Vdc

Internal RET High band (2) | Low band (2)

Power Consumption, idle state, maximum 1 W Power Consumption, normal conditions, maximum 8 W

Protocol 3GPP/AISG 2.0 (Multi-RET)

RET Hardware CommRET v2

RET Interface 8-pin DIN Female | 8-pin DIN Male

RET Interface, quantity 1 female | 1 male

Packed Dimensions

 Length
 2010.0 mm | 79.1 in

 Width
 608.0 mm | 23.9 in

 Depth
 352.0 mm | 13.9 in

 Shipping Weight
 49.0 kg | 108.0 lb

Regulatory Compliance/Certifications

Agency

Classification

RoHS 2011/65/EU

Compliant by Exemption

China RoHS SJ/T 11364-2006

Above Maximum Concentration Value (MCV)

ISO 9001:2008 Designed, manufactured and/or distributed under this quality management system





- Ensure there are no other shipping or tracking labels attached to your package. Select the Print button on the print dialog box that appears. Note: If your browser does not support this function select Print from the File menu to print the label.
- Fold the printed label at the solid line below. Place the label in a UPS Shipping Pouch. If you do not have a pouch, affix the folded label using clear plastic shipping tape over the entire label.

3. GETTING YOUR SHIPMENT TO UPS

Customers with a Daily Pickup

Your driver will pickup your shipment(s) as usual.

Customers without a Daily Pickup

Take your package to any location of The UPS Store®, UPS Access Point(TM) location, UPS Drop Box, UPS Customer Center, Staples® or Authorized Shipping Outlet near you. Items sent via UPS Return Services(SM) (including via Ground) are also accepted at Drop Boxes. To find the location nearest you, please visit the 'Find Locations' Quick link at ups.com.

Schedule a same day or future day Pickup to have a UPS driver pickup all of your Internet Shipping packages. Hand the package to any UPS driver in your area.

UPS Access PointTM
MICHAELS STORE # 7773
75 INTERSTATE SHOP CTR
RAMSEY ,NJ 07446

UPS Access PointTM THE UPS STORE 115 FRANKLIN TPKE MAHWAH ,NJ 07430 UPS Access PointTM THE UPS STORE 120 E MAIN ST RAMSEY ,NJ 07446



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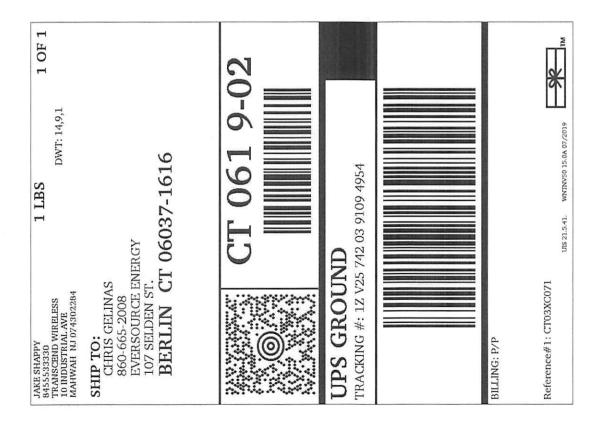
Customers without a Daily Pickup

Take your package to any location of The UPS Store®, UPS Access Point(TM) location, UPS Drop Box, UPS Customer Center, Staples® or Authorized Shipping Outlet near you. Items sent via UPS Return Services(SM) (including via Ground) are also accepted at Drop Boxes. To find the location nearest you, please visit the 'Find Locations' Quick link at ups.com.

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