56 Prospect Street,
P.O. Box 270

Hartford, CT 06103

Kathleen M. Shanley Manager - Transmission Siting Tel: (860) 728-4527

Melanie A. Bachman<br>Executive Director<br>Connecticut Siting Council<br>10 Franklin Square<br>New Britain, CT 06051

## RE: Notice of Exempt Modification <br> Eversource Site Ridgefield 22N <br> Off Prospect Street, Ridgefield, CT 06877 <br> Latitude: 41-17-00.6 N / Longitude: 73-29.16.3 W

Dear Ms. Bachman:

The Connecticut Light and Power Company doing business as Eversource Energy ("Eversource") currently maintains multiple antennas and equipment at various mounting heights on an existing 84foot steel monopole tower located off Prospect Street in Ridgefield. See Attachment A, Parcel Map and Property Card. The tower and property are owned by Eversource. Eversource is seeking the Connecticut Siting Council's authorization for the installation of one 15 -foot 6 -inch tall omni-directional antenna to be mounted at 83 feet above ground level ("AGL") and the removal of two omni-directional antennas, one upright and one inverted. There will be no other changes to the area of the fenced compound, the tower or the existing antennas and other equipment currently mounted on the tower. The antenna will be mounted to the existing tower on a new 4 -foot stand-off mount. See Attachment B, Mount Analysis, dated August 12, 2021. The tower and existing and proposed equipment on the tower are depicted on Attachment C, Construction Drawings, dated August 17, 2021 and Attachment D, Structural Analysis, dated July 29, 2021. The Connecticut Siting Council approved the monopole at this location in Petition No. 1054 in January 2013.

The modification is required to eliminate transmitter induced noise issues from two antennas previously installed as part of Eversource's program to update its obsolete analog voice radio communications system to a modern digital voice communications system (refer to EM-EVER-118200724, dated August 17, 2020). The transmitter issue manifests as passive intermodulation, or PIM, noise located on the receive frequencies, which limits the system level coverage capability of the site.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies ("R.C.S.A.") §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this notice is being delivered to Rudy Marconi, First Selectman for the Town of Ridgefield and Richard Baldelli, Director of Planning \& Zoning
for the Town of Ridgefield via the United States Postal Service or private carrier. Proof of delivery is attached. See Attachment E, Proof of Delivery of Notice.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2):

1. There will be no change to the height of the existing tower.
2. The modifications will not require the extension of the site boundary.
3. The modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the new antenna will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard as shown in the attached Radio Frequency Emissions Report, dated August 18, 2021 (Attachment F - Power Density Report) ${ }^{1}$.
5. The modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Eversource respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2). One original and two copies of this notice and a check in the amount of $\$ 625$ are enclosed.

Communications regarding this Notice of Exempt Modification should be directed to Kathleen Shanley at (860) 728-4527.

By:


Manager - Transmission Siting
cc: Honorable Rudy Marconi, First Selectman, Town of Ridgefield
Richard Baldelli, Director of Planning \& Zoning, Town of Ridgefield

Attachments
A. Parcel Map and Property Card
B. Mount Analysis
C. Construction Drawings
D. Structural Analysis
E. Proof of Delivery of Notice
F. Power Density Report

[^0]ATTACHMENT A - PARCEL MAP AND PROPERTY CARD


## ES-286 Ridgefield22N Parcel

2/20/2020 8:34:14 AM
Scale: $1^{\prime \prime=188 '}$
Scale is approximate


The information depicted on this map is for planning purposes only It is not adequate for legal boundary definition, regulatory interpretation, or parcel-level analyses.


The Assessor's office is responsible for the maintenance of records on the ownership of properties. Assessments are computed at $70 \%$ of the estimated market value of real property at the time of the last revaluation which was 2017.


## Ridgefield Connecticut

Ridgefield Town Hall 400 Main Street Ridgefield, CT 06877 Phone: 203.431 .2700
Fax: 203.431 .2722


Information on the Property Records for the Municipality of Ridgefield was last updated on 2/17/2020.

## Parcel Information

| Location: | SUNSET LA | Property Use: | Vacant Land | Primary Use: | Residential |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Unique ID: | F150054 | Map Block <br> Lot: | F15-0054 | Acres: | 2.30 |
| 490 Acres: | 0.00 | Zone: | RAA | Volume / | Page: |

## Value Information

|  | Appraised Value | Assessed Value |
| :--- | :--- | :--- |
| Land | 98,900 | 69,230 |
| Buildings | 0 | 0 |
| Detached Outbuildings | 0 | 0 |
| Total | 98,900 | 69,230 |

ATTACHMENT B - MOUNT ANALYSIS

## MOUNT EVALUATION LETTER

| Site Number: | 848 |
| :--- | :--- |
| Site Name: | THOMPSON CSP |
| Site Data: | 97 Mountain Hill Road |
|  | Thompson, CT 06255 |
| Latitude: | $41^{\circ} 59^{\prime} 11.76^{\prime \prime}$ |
| Longitude: | $-71^{\circ} 54^{\prime} 49.11^{\prime \prime}$ |

Black \& Veatch Corporation is pleased to submit this "Mount Evaluation Letter" to determine the structural integrity of antenna mounting system on the above-mentioned site. The purpose of this evaluation is to determine the capacity of the system in supporting the final loading in the attached "Loading Summary".

Based on our evaluation we have determined the proposed antenna mounting system to be:

## SUFFICIENT

Structure Rating (max from all components) =
17.2\%

## Proposed Mounting System

SitePro 1 (USF-4U) 48" Ultimate Universal Stand-off Frame

This analysis analyzes the worst-case scenario for the proposed USF-4U Stand-off Frame. All levels are deemed sufficient. The proposed mounting system will be capable of supporting the proposed equipment, under the following conditions:

- Contractor shall be responsible for the means and methods of construction.
- Contractor shall inspect the condition of all existing and proposed structural members, all relevant members and connections and report any deficiencies to the engineer prior to installation of any new antennas and other equipment.

The scope of this evaluation pertains only to the proposed antenna mounting system and does not include examination of the loads imparted by the antenna mounting system to the existing tower and its structural components. This document was prepared based on information provided to Black \& Veatch. If existing conditions do not reflect those represented, this analysis is no longer valid.

Please contact Josh Riley in our Overland Park Office
at 913-458-2522 if you have any questions or comments.

Sincerely,
Black \& Veatch Corporation

Prepared By: Shaun Donley Submitted By: Josh Riley, P.E.


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## 1. LOADING SUMMARY

| Appurtenance |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Carrier | Position | Sector | Antenna RAD <br> Center (ft) | Mount <br> Centerline (ft) | Qty | Type | Manufacturer | Model |
| Eversource | 1 | - | 157 | 154 | 1 | Omni | Telewave | ANT220F2 |
| Eversource | 1 | - | 134 | 131 | 1 | Dipole | COMPROD | 871F-70-2 |
|  |  |  |  |  |  |  |  |  |

This analysis analyzes the worst-case scenario for the proposed USF-4U Stand-off Frame. All levels are deemed sufficient

## 2. ANALYSIS CRITERIA SUMMARY

| ANALYSIS CRITERIA |  |
| :--- | :--- |
| STANDARD | TIA-222-H |
| WIND SPEED | Ultimate of 140 mph |
| WIND SPEED WITH ICE | 50 mph with 2" radial ice thickness |
| EXPOSURE CATEGORY | B |
| RISK CATEGORY | III |
| TOPO CATEGORY | Hill |
| CREST HEIGHT | 110 ft |

## 3. REFERENCES

- American Institute of Steel Construction, AISC 15th Edition
- Telecommunications Industry Association Standard, TIA-222-H \& 2018 Connecticut State Building Code
- Antenna Mount Assembly Drawing (Model: USF-4U) by SitePro 1, dated 02/16/2011


## 4. ASSUMPTIONS

This analysis may be affected if any assumptions are not valid or have been made in error. Black \& Veatch should be notified to determine the effect on the structural integrity of the antenna mounting system.

- The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specifications.
- The configuration of antennas, mounts, and other appurtenances are as specified in the Loading Summary and the referenced drawings.
- All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
- Sector frame center line: located equidistant between top \& bottom boom; Platform center line: located at the base perimeter of platform, unless otherwise specified.
- Steel grades have been assumed as follows, unless noted otherwise:

Channel, Solid Round, Angle, Plate
HSS (Rectangular)
Pipe
Connection Bolts

ASTM A36 (GR 36)
ASTM 500 (GR B-46)
ASTM A53 (GR B-35)
ASTM A325

## 5. RESULTS SUMMARY

| Name | Bending Stress Ratio |  | Shear Stress Ratio |  |
| :--- | :---: | :---: | :---: | :---: |
| Arm: HSS3X3X3 | $12.8 \%$ | Pass | $2.8 \%$ | Pass |
| Bracing: Pipe 2.0 Std | $17.2 \%$ | Pass | $2.2 \%$ | Pass |
| Mount Pipe: Pipe 3.0 Std | $8.7 \%$ | Pass | $3.8 \%$ | Pass |
|  |  |  |  |  |

[^1]**Capacity rating per TIA-222-H Section 15.5.

## APPENDIX 1:

 MOUNT ANALYSIS REPORTClient: Eversource
Computed By: Shaun Donley
Site Name: THOMPSON CSP (848) Date: 8/16/2021
Verified By: JJ
BLACK \& VEATCH
Title: MOUNT ANALYSIS REPORT

## Dead and Live Loads

Maintenance Live Load: $\quad L_{V}=250 \mathrm{lb}$
Installation Live Load: $\quad L_{M}=0 \quad \mathrm{lb}$

| Appurtenance Dead Loads |  |
| :---: | :---: |
| Name | Weight <br> $(\mathrm{lb})$ |
| $871 \mathrm{~F}-70-2$ | 12.5 |
|  |  |

Client: Eversource
Computed By: Shaun Donley
Site Name: THOMPSON CSP (848)


Client: Eversource
Computed By: Shaun Donley
Site Name: THOMPSON CSP (848)
Date: 8/16/2021

## Member Wind Loading

Exposure Category = B
Risk Category = III
Topographic Category = 1
1
Basic Wind Speed, V = 140 mph
Height Above Ground, $z=134$ ft

## Equations

$\mathrm{K}_{\mathrm{z}}=2.01\left(\mathrm{z} / \mathrm{z}_{\mathrm{g}}\right)^{2 / \alpha}$
$K_{h}=e^{(f \cdot z / H)}$
$K_{z t}=\left[1+K_{c} K_{t} / K_{h}\right]^{2}$
Crest Height, $\mathrm{H}=110 \mathrm{ft} \mathrm{ft}$
Velocity Pressure Coefficient, $\mathrm{K}_{\mathrm{z}}=1.07$
Topographic Factor, $\mathrm{K}_{\mathrm{zt}}=1.09$
Wind Directionality Factor, $K_{d}=0.95$
Shielding Factor, $\mathrm{K}_{\mathrm{a}}=0.90$
Ground Elevation Factor, $\mathrm{K}_{\mathrm{e}}=1.000$
Wind Velocity Pressure, $\mathrm{q}_{\mathrm{z}}=55.61$ psf
Gust Effect Factor, $\mathrm{G}_{\mathrm{h}}=1.00$

TIA-222-H
2.6.5.2
2.6.6.2.1
2.6.11.2

| Member Wind Loads |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Name | Depth <br> $(\mathrm{ft})$ | Width <br> $(\mathrm{ft})$ | $\mathrm{C}_{\mathrm{f}}$ | $\mathrm{D}_{\mathrm{p}}$ <br> $(\mathrm{ft})$ | $\mathrm{F}_{\mathrm{M}}$ <br> $(\mathrm{lb})$ |
| Arm: HSS3X3X3 | 0.25 | 0.25 | 2 | 0.25 | 27.80 |
| Bracing: Pipe 2.0 Std | 0.20 |  | 1.2 | 0.20 | 13.21 |
| Mount Pipe: Pipe 3.0 Std | 0.29 |  | 1.2 | 0.29 | 19.46 |
|  |  |  |  |  |  |

Client: Eversource
Computed By: Shaun Donley
Site Name: THOMPSON CSP (848)
Date: 8/16/2021
Verified By: JJ
Title: MOUNT ANALYSIS REPORT

## Appurtenance Ice Dead Loading

Exposure Category = B
Risk Category = III
Topographic Category = 1
Height Above Ground, $\mathrm{z}=134 \mathrm{ft}$
Crest Height, $\mathrm{H}=110 \mathrm{ft} \mathrm{ft}$
Design Ice Thickness, $\mathrm{T}_{\mathrm{i}}=2.00$ in
Importance Factor, I = 1.15
Topographic Factor, $\mathrm{K}_{\mathrm{zt}}=1.09$
Height Escalation Factor, $\mathrm{K}_{\mathrm{iz}}=1.15$
Factored Ice Thickness, $\mathrm{T}_{\mathrm{iz}}=2.72$ in
$K_{h}=e^{(f \cdot z / H)}$
$K_{z t}=\left[1+K_{c} K_{t} / K_{h}\right]^{2}$
$\mathrm{K}_{\mathrm{i} 2}=(\mathrm{z} / 33)^{\mathrm{u} .1 \mathrm{u}}$
$\mathrm{T}_{\mathrm{iz}}=\mathrm{T}_{\mathrm{i}} 1 \mathrm{~K}_{\mathrm{iz}}\left(\mathrm{K}_{\mathrm{zt}}\right)^{0.5 \mathrm{~s}}$
Equations
$D L_{\text {ice }}=\left[\left(H_{\text {ice }} * D_{\text {ice }} * W_{\text {ice }}\right)-\left(H^{*} W^{*} D\right)\right] * 56 p c f$

TIA-222-H
2.6.6.2.1
2.6.10

| Appurtenance Ice Dead Loads |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Name | Height w/ ice <br> (ft) | Width w/ice (ft) | Depth w/ ice (ft) | $\begin{array}{r} \hline \mathrm{V}_{\text {ice }} \\ \left(\mathrm{ft}^{3}\right) \\ \hline \end{array}$ | $\mathrm{DL}_{\text {ice }}$ <br> (lb) |
| 871F-70-2 | 5.95 | 3.04 | 0.61 | 8.82 | 493.98 |
|  |  |  |  |  |  |

Client: Eversource
Computed By: Shaun Donley
Site Name: THOMPSON CSP (848) Date: 8/16/2021

## Member Ice Dead Loading

Exposure Category = B
Risk Category = III
$K_{h}=e^{(f \cdot z / H)}$
Topographic Category = 1
Height Above Ground, $\mathrm{z}=134 \mathrm{ft}$
$K_{z t}=\left[1+K_{c} K_{t} / K_{h}\right]^{2}$
Crest Height, $\mathrm{H}=110 \mathrm{ft} \mathrm{ft}$
Design Ice Thickness, $\mathrm{T}_{\mathrm{i}}=2.00$ in
$K_{i z}=(z / 33)^{0.10}$
Importance Factor, I = 1.15
Topographic Factor, $\mathrm{K}_{\mathrm{zt}}=1.09$
Height Escalation Factor, $\mathrm{K}_{\mathrm{iz}}=1.15$
Factored Ice Thickness, $\mathrm{T}_{\mathrm{i}}=2.72$ in
Aiz $=$ pi $^{*} T i z^{*}(\mathrm{Dc}+\mathrm{Tiz})$

TIA-222-H
2.6.6.2.1
2.6.6.2.1
2.6.10
2.6.10
2.6.10

| Member Ice Dead Loads |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Name | Depth w/ ice <br> $(\mathrm{ft})$ | Width w/ice <br> $(\mathrm{ft})$ | Dc <br> $(\mathrm{ft})$ | Aiz <br> $\left(\mathrm{ft}^{2}\right)$ | DL $_{\text {ice }}(\mathrm{lb} / \mathrm{ft})$ |  |
| Arm: HSS3X3X3 | 0.70 | 0.70 | 0.35 | 0.41 | 23.18 |  |
| Bracing: Pipe 2.0 Std | 0.65 |  | 0.20 | 0.30 | 16.96 |  |
| Mount Pipe: Pipe 3.0 Std | 0.75 |  | 0.29 | 0.37 | 20.71 |  |
|  |  |  |  |  |  |  |

Client: Eversource
Computed By: Shaun Donley
Site Name: THOMPSON CSP (848)

## Appurtenance Ice Wind Loading

Exposure Category = B
Risk Category = III
Topographic Category = 1
Ice Wind Speed, $\mathrm{V}_{\text {ice }}=50 \mathrm{mph}$
Height Above Ground, $\mathrm{z}=134 \mathrm{ft}$
Crest Height, $\mathrm{H}=110 \mathrm{ft} \mathrm{ft}$
Velocity Pressure Coefficient, $\mathrm{K}_{\mathrm{z}}=1.07$ psf
Topographic Factor, $\mathrm{K}_{\mathrm{zt}}=1.09$
Wind Directionality Factor, $K_{d}=0.95$
Shielding Factor, $\mathrm{K}_{\mathrm{a}}=0.90$
Ground Elevation Factory, $\mathrm{K}_{\mathrm{e}}=1.000$ Ice Wind Velocity Pressure, $\mathrm{q}_{\text {z(ice) }}=7.093$

Factored Ice Thickness, $\mathrm{T}_{\mathrm{iz}}=2.72$ in Gust Effect Factor, $\mathrm{G}_{\mathrm{h}}=1$

## Equations

$\mathrm{K}_{\mathrm{z}}=2.01\left(\mathrm{z} / \mathrm{z}_{\mathrm{g}}\right)^{2 / \alpha}$
$K_{h}=e^{(f \cdot z / H)}$
$K_{z t}=\left[1+K_{c} K_{t} / K_{h}\right]^{2}$
$K_{e}=e^{-u . u v u u s \lll s}$
$\mathrm{q}_{\mathrm{z}}=0.00256 \mathrm{~K}_{\mathrm{z}} \mathrm{K}_{\mathrm{zt}} \mathrm{K}_{\mathrm{e}} \mathrm{K}_{\mathrm{d}} \mathrm{V}^{\perp}$
$F_{A(\text { ice })}=q_{z(\text { ice })} G_{h}(E P A)_{A(\text { (ice })}$
$F_{M(\text { ice })}=q_{z(\text { ice })} G_{h} C_{f} D_{p(\text { ice })}$

TIA-222-H
2.6.5.2
2.6.6.2.1
2.6.11.6
2.6.11.2

Appurtenance Ice Wind Loads

| Name | Height w/ Ice (ft) | Width w/ Ice (ft) | Depth $\mathrm{w} /$ Ice (ft) | Normal |  |  | Tangential |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\mathrm{C}_{\mathrm{a}}$ | EPA FT2 | $\mathrm{F}_{\mathrm{A}}(\mathrm{lb})$ | $\mathrm{C}_{\mathrm{a}}$ | EPA FT2 | $\mathrm{F}_{\mathrm{A}}$ (lb) |
| 871F-70-2 | 5.95 | 3.04 | 0.61 | - | 17.79 | 126.15 | - | 3.32 | 23.53 |
|  |  |  |  |  |  |  |  |  |  |

Client: Eversource
Computed By: Shaun Donley
Site Name: THOMPSON CSP (848)

## Member Ice Wind Loading

Exposure Category = B

## Equations

Risk Category = III
Topographic Category = 1
Ice Wind Speed, $\mathrm{V}_{\text {ice }}=50 \mathrm{mph}$
Height Above Ground, $z=134 \mathrm{ft} \quad \mathrm{K}_{\mathrm{zt}}=\left[1+\mathrm{K}_{\mathrm{c}} \mathrm{K}_{\mathrm{t}} / \mathrm{K}_{\mathrm{h}}\right]^{2}$
Crest Height, $\mathrm{H}=110 \mathrm{ft} \mathrm{ft}$
Velocity Pressure Coefficient, $\mathrm{K}_{\mathrm{z}}=1.07$ psf
$\mathrm{K}_{\mathrm{z}}=2.01\left(\mathrm{z} / \mathrm{z}_{\mathrm{g}}\right)^{2 / \alpha}$
$K_{h}=e^{(f \cdot z / H)}$
$K_{e}=e^{-u . v u v u s \ll c s}$
Topographic Factor, $\mathrm{K}_{\mathrm{zt}}=1.09$
Wind Directionality Factor, $\mathrm{K}_{\mathrm{d}}=0.95$
$\mathrm{q}_{\mathrm{z}}=0.00256 \mathrm{~K}_{\mathrm{z}} \mathrm{K}_{2 \mathrm{t}} \mathrm{K}_{\mathrm{e}} \mathrm{K}_{\mathrm{d}} \mathrm{V}^{\llcorner }$
Shielding Factor, $\mathrm{K}_{\mathrm{a}}=0.90$
Ground Elevation Factory, $K_{e}=1.000$
$F_{A \text { (ice) }}=q_{z(\text { ice })} G_{h}(E P A)_{A \text { (ice) }}$
Ice Wind Velocity Pressure, $\mathrm{q}_{\mathrm{z} \text { (ice) }}=7.093$
Factored Ice Thickness, $\mathrm{T}_{\mathrm{i} \mathrm{z}}=2.72$ in
$F_{M(\text { ice })}=q_{z(\text { (ice) }} G_{h} C_{f} D_{p(\text { (ice) }}$

TIA-222-H
2.6.5.2
2.6.6.2.1
2.6.11.2 Gust Effect Factor, $\mathrm{G}_{\mathrm{h}}=1$

| Member Ice Wind Loads |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Name | Depth <br> $\mathrm{w} / \mathrm{Ice}(\mathrm{ft})$ | Width <br> $\mathrm{w} /$ Ice (ft) | $\mathrm{C}_{\mathrm{f}}$ | $\mathrm{D}_{\text {p(ice) }}$ <br> $(\mathrm{ft})$ | $\mathrm{F}_{\mathrm{M} \text { (ice) }}$ <br> $(\mathrm{lb} / \mathrm{ft})$ |
| Arm: HSS3X3X3 | 0.70 | 0.70 | 2 | 0.70 | 9.98 |
| Bracing: Pipe 2.0 Std | 0.65 |  | 1.2 | 0.65 | 5.55 |
| Mount Pipe: Pipe 3.0 Std | 0.75 |  | 1.2 | 0.75 | 6.35 |
|  |  |  |  |  |  |

## APPENDIX 2:

 RISA PRINTOUTS

| Black \& Veatch |  | SK -1 |
| :--- | :---: | :--- |
| Shaun Donley | THOMPSONCSP USF-4U Model | Aug 16, 2021 at $12: 37$ PM |
| 405025.3022 .2200 |  | 405025.3022 .2200 Risa Model.r3d |



| Black \& Veatch |  | SK -2 |
| :--- | :---: | :--- |
| Shaun Donley | THOMPSONCSP USF-4U Model | Aug 16, 2021 at 12:38 PM |
| 405025.3022 .2200 |  | 405025.3022 .2200 Risa Model.r3d |



Member Code Checks Displayed (Enveloped)
Envelope Only Solution

| Black \& Veatch |  | SK -3 |
| :--- | :---: | :--- |
| Shaun Donley | THOMPSONCSP USF-4U Model | Aug 16, 2021 at $12: 39$ PM |
| 405025.3022 .2200 |  | 405025.3022 .2200 Risa Model.r3d |



Member Shear Checks Displayed (Enveloped)
Envelope Only Solution

| Black \& Veatch |  | SK -4 |
| :--- | :---: | :--- |
| Shaun Donley | THOMPSONCSP USF-4U Model | Aug 16, 2021 at $12: 39$ PM |
| 405025.3022 .2200 |  | 405025.3022 .2200 Risa Model.r3d |



Loads: BLC 1, DL
Envelope Only Solution

| Black \& Veatch |  | SK -5 |
| :--- | :---: | :--- |
| Shaun Donley | THOMPSONCSP USF-4U Model | Aug 16, 2021 at $12: 40$ PM |
| 405025.3022 .2200 |  | 405025.3022 .2200 Risa Model.r3d |

(Global) Model Settings

| Display Sections for Member Calcs | 5 |
| :--- | :--- |
| Max Internal Sections for Member Calcs | 97 |
| Include Shear Deformation? | Yes |
| Increase Nailing Capacity for Wind? | Yes |
| Include Warping? | Yes |
| Trans Load Btwn Intersecting Wood Wall? | Yes |
| Area Load Mesh (in^2) | 144 |
| Merge Tolerance (in) | .12 |
| P-Delta Analysis Tolerance | $0.50 \%$ |
| Include P-Delta for Walls? | Yes |
| Automatically Iterate Stiffness for Walls? | Yes |
| Max Iterations for Wall Stiffness | 3 |
| Gravity Acceleration (in/sec^2) | 386.4 |
| Wall Mesh Size (in) | 24 |
| Eigensolution Convergence Tol. (1.E-) | 4 |
| Vertical Axis | Y |
| Global Member Orientation Plane | XZ |
| Static Solver | Sparse Accelerated |
| Dynamic Solver | Accelerated Solver |


| Hot Rolled Steel Code | AISC 15th(360-16): LRFD |
| :--- | :--- |
| Adjust Stiffness? | Yes(lterative) |
| RISAConnection Code | None |
| Cold Formed Steel Code | None |
| Wood Code | None |
| Wood Temperature | < 100F |
| Concrete Code | None |
| Masonry Code | None |
| Aluminum Code | None - Building |
| Stainless Steel Code | None |


| Number of Shear Regions | 4 |
| :--- | :--- |
| Region Spacing Increment (in) | 4 |
| Biaxial Column Method | Exact Integration |
| Parme Beta Factor (PCA) | .65 |
| Concrete Stress Block | Rectangular |
| Use Cracked Sections? | Yes |
| Use Cracked Sections Slab? | No |
| Bad Framing Warnings? | No |
| Unused Force Warnings? | Yes |
| Min 1 Bar Diam. Spacing? | No |
| Concrete Rebar Set | REBAR_SET_ASTMA615 |
| Min \% Steel for Column | 1 |
| Max \% Steel for Column | 8 |

(Global) Model Settings, Continued

| Seismic Code | ASCE 7-16 |
| :--- | :--- |
| Seismic Base Elevation (in) | Not Entered |
| Add Base Weight? | Yes |
| Ct X | .02 |
| Ct Z | .02 |
| T X (sec) | Not Entered |
| T Z (sec) | Not Entered |
| R X | 3 |
| R Z | 3 |
| Ct Exp. X | .75 |
| Ct Exp. Z | .75 |
| SD1 | 1 |
| SDS | 1 |
| S1 | 1 |
| TL (sec) | 5 |
| Risk Cat | $I$ or II |
| Drift Cat | Other |
| Om Z | 1 |
| Om X | 1 |
| Cd Z | 4 |
| Cd X | 4 |
| Rho Z | 1 |
| Rho X | 1 |
|  |  |

Hot Rolled Steel Properties

| Label |  | E [ksi] | G [ksi] | Nu | Therm (/1E...Density[k/ft |  | Yield[ksi] | Ry | Fu[ksi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A992 | 29000 | 11154 | 3 | . 65 | . 49 | 50 | 1.1 | 65 | 1.1 |
| 2 | A36 Gr. 36 | 29000 | 11154 | 3 | . 65 | 49 | 36 | 1.5 | 58 | 1.2 |
| 3 | A572 Gr. 50 | 29000 | 11154 | 3 | . 65 | . 49 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr.B RND | 29000 | 11154 | 3 | . 65 | . 527 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | 3 | . 65 | . 527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | 3 | 65 | 49 | 35 | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | 3 | . 65 | . 49 | 50 | 1.4 | 65 | 1.3 |

## Hot Rolled Steel Section Sets

| Label |  | Shape | Type | Design List | Material | Design R... A [in2] |  | lyy [in4] Izz [in4] |  | $J$ [in4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Arm | HSS3X3X3 | Beam | SquareTube | A53 Gr.B | Typical | 1.89 | 2.46 | 2.46 | 4.03 |
| 2 | Bracing | PIPE 2.0 | Column | Pipe | A53 Gr.B | Typical | 1.02 | 627 | 627 | 1.25 |
| 3 | Mount Pipe | PIPE_3.0 | Column | Pipe | A53 Gr.B | Typical | 2.07 | 2.85 | 2.85 | 5.69 |

General Material Properties

|  | Label | E [ksi] | G [ksi] | Nu | Therm (/1E5 F) | Density[k/ft^3] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | gen Conc3NW | 3155 | 1372 | . 15 | . 6 | . 145 |
| 2 | gen_Conc4NW | 3644 | 1584 | . 15 | 6 | 145 |
| 3 | gen Conc3LW | 2085 | 906 | . 15 | 6 | 11 |
| 4 | gen_Conc4LW | 2408 | 1047 | . 15 | . 6 | 11 |
| 5 | gen Alum | 10100 | 4077 | . 3 | 1.29 | . 173 |
| 6 | gen Steel | 29000 | 11154 | . 3 | . 65 | . 49 |
| 7 | gen Plywood | 1800 | 38 | 0 | . 3 | . 035 |
| 8 | RIGID | $1 \mathrm{e}+6$ |  | . 3 | 0 | 0 |


|  | Joint Label | X [k/in] | Y [k/in] | Z [k/in] | X Rot.[k-ft/rad] | Y Rot.[k-ft/rad] | Z Rot.[k-ft/rad] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | Reaction | Reaction | Reaction |  | Reaction |  |
| 2 | N3 | Reaction | Reaction | Reaction |  | Reaction |  |

## Member Primary Data

|  | Label | I Joint | $J$ Joint | K Joint | Rotate(d. | Section/Shape | Type | Design List | Material | Design Ru. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | N1 | N2 |  |  | Arm | Beam | SquareTube | A53 Gr.B | Typical |
| 2 | M2 | N3 | N4 |  |  | Arm | Beam | SquareTube | A53 Gr.B | Typical |
| 3 | M3 | N5 | N6 |  |  | Bracing | Column | Pipe | A53 Gr.B | Typical |
| 4 | M4 | N7 | N8 |  |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 5 | M5 | N9 | N10 |  |  | RIGID | None | None | RIGID | Typical |
| 6 | M6 | N12 | N13 |  |  | RIGID | None | None | RIGID | Typical |
| 7 | M7 | N15 | N14 |  |  | RIGID | None | None | RIGID | Typical |

## Member Advanced Data

|  | Label | I Release | $J$ Release | I Offset[in] | J Offset[in] | T/C Only | Physical | Defl Rat...A | Analysis ... | Inactive | Seismic... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 |  |  |  |  |  | Yes |  |  |  | None |
| 2 | M2 |  |  |  |  |  | Yes |  |  |  | None |
| 3 | M3 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 4 | M4 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 5 | M5 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 6 | M6 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 7 | M7 |  |  |  |  |  | Yes | ** NA ** |  |  | None |

## Hot Rolled Steel Design Parameters

|  | Label | Shape | Length[in] | Lbyy[in] | Lbzz[in] | Lcomp top[i.. | Lcomp bot[in]L | L-torqu. | Kyy | Kzz | Cb | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Arm | 43.5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 2 | M2 | Arm | 43.5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 3 | M3 | Bracing | 36 |  |  |  |  |  |  |  |  | Lateral |
| 4 | M4 | Mount Pipe | 56.5 |  |  |  |  |  |  |  |  | Lateral |

## Basic Load Cases

|  | BLC Description | Category | X Gravity | Y Gravity | Z Gravity | Joint | Point | Distributed | Area(Me... | Surface(P.. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | DL | DL |  | -1 |  | 1 |  |  |  |  |
| 2 | Maintenance LL - LV | LL |  |  |  | 1 |  |  |  |  |
| 3 | Installation LL - LM | LL |  |  |  | 1 |  |  |  |  |
| 4 | Wind - 0 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 5 | Wind - 30 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 6 | Wind - 60 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 7 | Wind -90 Deq (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 8 | Wind - 120 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 9 | Wind - 150 Deg ( X ) | WL |  |  |  | 1 |  | 4 |  |  |
| 10 | Wind - 180 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 11 | Wind - 210 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 12 | Wind - 240 Deg ( X ) | WL |  |  |  | 1 |  | 4 |  |  |
| 13 | Wind - 270 Deg ( X ) | WL |  |  |  | 1 |  | 4 |  |  |
| 14 | Wind - 300 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 15 | Wind - 330 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 16 | Wind - 0 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 17 | Wind - $30 \mathrm{Deg}(\mathrm{Z})$ | WL |  |  |  | 1 |  | 4 |  |  |
| 18 | Wind - $60 \operatorname{Deg}(Z)$ | WL |  |  |  | 1 |  | 4 |  |  |

Company Designer Job Number

Basic Load Cases (Continued)

|  | BLC Description | Category | X Gravity | Y Gravity | Z Gravity | Joint | Point | Distributed | Area(Me... | Surface(P... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | Wind - 90 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 20 | Wind - 120 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 21 | Wind - 150 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 22 | Wind - 180 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 23 | Wind - 210 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 24 | Wind - 240 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 25 | Wind - 270 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 26 | Wind - 300 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 27 | Wind - 330 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 28 | Ice DL | DL |  |  |  | 1 |  | 4 |  |  |
| 29 | Ice Wind - 0 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 30 | Ice Wind - 30 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 31 | Ice Wind -60 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 32 | Ice Wind - 90 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 33 | Ice Wind - 120 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 34 | Ice Wind - 150 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 35 | Ice Wind - 180 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 36 | Ice Wind - 210 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 37 | Ice Wind - 240 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 38 | Ice Wind - 270 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 39 | Ice Wind - 300 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 40 | Ice Wind - 330 Deg (X) | WL |  |  |  | 1 |  | 4 |  |  |
| 41 | Ice Wind - 0 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 42 | Ice Wind - 30 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 43 | Ice Wind - 60 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 44 | Ice Wind - 90 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 45 | Ice Wind-120 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 46 | Ice Wind - 150 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 47 | Ice Wind - 180 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 48 | Ice Wind-210 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 49 | Ice Wind - 240 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 50 | Ice Wind-270 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 51 | Ice Wind - 300 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |
| 52 | Ice Wind - 330 Deg (Z) | WL |  |  |  | 1 |  | 4 |  |  |

## Load Combinations

|  | Description |  | P... |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Fa... ${ }^{\text {B }}$ | B... Fa... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | WIND LOAD COMBOS (140 MPH) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | 1.2DL + WL (0 DEG) | Yes | Y |  | 1 | 1.2 | 4 |  | 1 | 16 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | 1.2DL + WL (30 DEG) | Yes | Y |  | 1 | 1.2 | 5 |  | 1 | 17 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | 1.2DL + WL (60 DEG) | Yes | Y |  | 1 | 1.2 | 6 |  | 1 | 18 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 1.2DL + WL (90 DEG) | Yes | Y |  | 1 | 1.2 | 7 |  | 1 | 19 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 1.2DL + WL (120 DEG) | Yes | Y |  | 1 | 1.2 | 8 |  | 1 | 20 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | 1.2DL + WL (150 DEG) | Yes |  |  | 1 | 1.2 | 9 |  | 1 | 21 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | 1.2DL + WL (180 DEG) | Yes | Y |  | 1 | 1.2 | 10 |  | 1 | 22 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | 1.2DL + WL (210 DEG) | Yes | Y |  | 1 | 1.2 | 11 |  | 1 | 23 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 1.2DL + WL (240 DEG) | Yes | Y |  | 1 | 1.2 | 12 |  | 1 | 24 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | 1.2DL + WL (270 DEG) | Yes | Y |  | 1 | 1.2 | 13 |  | 1 | 25 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 1.2DL + WL (300 DEG) | Yes | Y |  | 1 | 1.2 | 14 |  | 1 | 26 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | 1.2DL + WL (330 DEG) | Yes | Y |  | 1 | 1.2 | 15 |  | 1 | 27 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 15 | MOUNT LOAD COMBOS (30 MPH) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16 | 1.4DL | Yes | Y |  | 1 | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 17 | 1.2DL + 1.5LV | Yes | Y |  | 1 | 1.2 | 2 |  | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 18 | $1.2 \mathrm{LL}+1.5 \mathrm{LM}+\mathrm{WL}$ (0 DEG) | Yes | Y |  | 1 | 1.2 | 3 |  | 1.5 | 4 | . 046 | 16 | . 046 |  |  |  |  |  |  |  |  |  |  |  |

Company

## Load Combinations (Continued)

|  | n | S...P... |  |  |  |  |  |  |  |  |  |  | ...Fa |  |  |  |  | B... Fa. | B... Fa... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | 1.2DL + 1.5LM + WL (30 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 5 |  |  | . 046 |  |  |  |  |  |  |  |  |  |
| 20 | 1.2DL + 1.5LM + WL (60 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 6 |  |  | . 046 |  |  |  |  |  |  |  |  |  |
| 21 | 1.2DL + 1.5LM + WL (90 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 7 |  |  | . 046 |  |  |  |  |  |  |  |  |  |
| 22 | 1.2DL + 1.5LM + WL (120 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 8 |  | 20 | . 046 |  |  |  |  |  |  |  |  |  |
| 23 | 1.2DL + 1.5LM + WL (150 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 9 |  | 21 | . 046 |  |  |  |  |  |  |  |  |  |
| 24 | 1.2DL + 1.5LM + WL (180 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 10. |  | 22 | . 046 |  |  |  |  |  |  |  |  |  |
| 25 | $1.2 \mathrm{DL}+1.5 \mathrm{LM}+\mathrm{WL}$ (210 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 11. | . 046 |  | . 046 |  |  |  |  |  |  |  |  |  |
| 26 | 1.2DL + 1.5LM + WL (240 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 12. |  |  | . 046 |  |  |  |  |  |  |  |  |  |
| 27 | 1.2DL + 1.5LM + WL (270 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 13. |  | 25 | . 046 |  |  |  |  |  |  |  |  |  |
| 28 | 1.2DL + 1.5LM + WL (300 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 14 | . 046 | 26 | . 046 |  |  |  |  |  |  |  |  |  |
| 29 | 1.2DL + 1.5LM + WL (330 DEG) | Yes Y | 1 | 1.2 | 3 | 1.5 | 15. |  | 27 | . 046 |  |  |  |  |  |  |  |  |  |
| 30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 | ICE LOAD COMBOS (2", 50 MPH ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 32 | 1.2DL + Ice DL + Ice WL (0 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 29 | 1 | 41 | 1 |  |  |  |  |  |  |  |  |  |
| 33 | 1.2DL + Ice DL + Ice WL (30 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 30 | 1 | 42 | 1 |  |  |  |  |  |  |  |  |  |
| 34 | 1.2DL + Ice DL + Ice WL (60 DEG) | Yes $Y$ | 1 | 1.2 | 28 | 1 | 31 | 1 | 43 | 1 |  |  |  |  |  |  |  |  |  |
| 35 | 1.2DL + Ice DL + Ice WL (90 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 32 | 1 | 44 | 1 |  |  |  |  |  |  |  |  |  |
| 36 | 1.2DL + Ice DL + Ice WL (120 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 33 | 1 | 45 | 1 |  |  |  |  |  |  |  |  |  |
| 37 | 1.2DL + Ice DL + Ice WL (150 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 34 | 1 | 46 | 1 |  |  |  |  |  |  |  |  |  |
| 38 | 1.2DL + Ice DL + Ice WL (180 DEG) | Yes $Y$ | 1 | 1.2 | 28 | 1 | 35 | 1 | 47 | 1 |  |  |  |  |  |  |  |  |  |
| 39 | 1.2DL + Ice DL + Ice WL (210 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 36 | 1 | 48 | 1 |  |  |  |  |  |  |  |  |  |
| 40 | 1.2DL + Ice DL + Ice WL (240 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 37 | 1 | 49 | 1 |  |  |  |  |  |  |  |  |  |
| 41 | 1.2DL + Ice DL + Ice WL (270 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 38 | 1 | 50 | 1 |  |  |  |  |  |  |  |  |  |
| 42 | 1.2DL + Ice DL + Ice WL (300 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 39 | 1 | 51 | 1 |  |  |  |  |  |  |  |  |  |
| 43 | 1.2DL + Ice DL + Ice WL (330 DEG) | Yes Y | 1 | 1.2 | 28 | 1 | 40 | 1 | 52 | 1 |  |  |  |  |  |  |  |  |  |
| 44 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Envelope Joint Reactions

| Joint |  |  | X [lb] | LC Y [lb] |  | $\mathrm{LC} \quad \mathrm{Z}[\mathrm{lb}]$ |  | LC | MX [lb-ft] | LC | MY [lb-ft] | LC | MZ [lb-ft] LC |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | max | 288.513 | 2 | 310.985 | 38 | 297.152 | 5 | 0 | 43 | 656.451 | 11 | 0 | 43 |
| 2 |  | min | -610.651 | 38 | -20.698 | 2 | -297.152 | 11 | 0 | 2 | -656.451 | 5 | 0 | 2 |
| 3 | N3 | max | 555.139 | 17 | 311.915 | 32 | 122.811 | 5 | 0 | 43 | 385.621 | 11 | 0 | 43 |
| 4 |  | min | 10.189 | 8 | -18.194 | 8 | -122.811 | 11 | 0 | 2 | -385.621 | 5 | 0 | 2 |
| 5 | Totals: | max | 482.284 | 2 | 580.241 | 38 | 419.963 | 5 |  |  |  |  |  |  |
| 6 |  | min | -482.285 | 8 | 123.244 | 2 | -419.963 | 11 |  |  |  |  |  |  |

## Envelope AISC 15th(360-16): LRFD Steel Code Checks

| MemberM1 |  | Shape | Code Check | Loc[in] | LC Shea...Loc |  |  | $\begin{aligned} & \text {. L..phi*Pn.. } \\ & \text { z } 11155265 . . \\ & \hline \end{aligned}$ |  | $\frac{\text { phi*Pn... }}{59535}$ | $\frac{. \mathrm{phi}^{*} \mathrm{Mn} \ldots \ldots}{5171.25}$ | $\frac{\text { phi*Mn..... Eqn }}{5171.252 . . \mid-1-1 b}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | HSS3X3X3 | 128 | 0 | 11 | . 028 | 2.266 |  |  |  |  |  |  |
| 2 | M2 | HSS3X3X3 | 100 | 43.5 | 17 | . 019 | 0 | y 3 | 255265.. | 59535 | 5171.25 | 5171.252 | . $\mathrm{H} 1-1 \mathrm{~b}$ |
| 3 | M3 | PIPE 2.0 | 172 | 0 | 17 | . 022 | 0 |  | 928843. | 32130 | 1871.6.. | 1871.6..2 | . $\mathrm{H} 1-1 \mathrm{~b}$ |
| 4 | M4 | PIPE_3.0 | . 087 | 45.906 | 17 | . 038 | 10... |  | 757908. | 65205 | 5748.75 | 5748.751 | . $\mathrm{H} 1-1 \mathrm{~b}$ |

## APPENDIX 3:

## ATTACHMENTS

## EVERS=URCE <br> ENERGY




## ANT220F2DIN FIBERGLASS COLLINEAR ANTENNA

The Telewave ANT220F2 is an extremely rugged collinear antenna, with moderate gain and wide vertical beamwidth. This compact antenna produces 2.5 dBd gain, and is designed for operation in all environmental conditions. The antenna is constructed with brass and copper elements, with a path to ground potential for lightning impulse protection. The ANT220F2 is an excellent choice for wireless PTC systems in urban or rural areas.

All junctions are fully soldered to prevent RF intermodulation, and each antenna is completely protected within a rugged, hightech radome to ensure survivability in the worst environments. The "Cool Blue" radome provides maximum protection from corrosive gases, ultraviolet radiation, icing, salt spray, acid rain, and wind blown abrasives.

The ANT220F2 includes the ANTC485 dual clamp set for mounting to a $1.5^{\prime \prime}$ to $3^{\prime \prime}$ O.D. support pipe, and a $24^{\prime \prime}$ removable RG-213 DIN-Male jumper.


ANT220F2-230 MHz
Vertical Plane
Gain $=2.58 \mathrm{dBd}$



## SPECIFICATIONS

| Frequency (continuous) | $195-260 \mathrm{MHz}$ | Dimensions (L x base diam.) in. | $51 \times 2.75$ |
| :--- | :--- | :--- | :--- | :--- |
| Gain | 2.5 dBd | Tower weight (antenna + clamps) | 11 lb. |
| Power rating (typ.) | 500 watts | Shipping weight | 14 lb. |
| Impedance | 50 ohms | Wind rating / with 0.5" ice | $200 / 150 \mathrm{MPH}$ |
| VSWR | $1.5: 1$ or less | Maximum exposed area | $1.1 \mathrm{ft} .^{2}$ |
| Pattern | Omnidirectional | Lateral thrust at 100 MPH | 44 lb. |
| Vertical beamwidth | $38^{\circ}$ | Bending moment at top clamp | $47 \mathrm{ft} . \mathrm{lb}$. |
| Termination | $7-16$ DIN-F | $(100 \mathrm{MPH}, 40$ PSF flat plate equiv.) |  |

## 220MHz EXPOSED DIPOLES

## 870 Series 220MHz Exposed Dipoles

The 870 Series 220MHz Exposed Dipoles are available in 1, 2, 4, 8 dipole configurations. All our antennas can be completely customized to your particular applications. Our antennas can be black anodized, adjustable, or fixed, side mount or top mount, and heavy-duty versions are available.

- Each antenna is offered in a $1 / 4,3 / 8$ or $1 / 2$ wave spacing versions.
- The 87XA-70 has external cabling and a field-adjustable pattern.
- The 87XF-70 has internal cabling and fixed dipole-mast spacing.
- Heavy-duty versions are available. Please contact our Technical Support team for consultation.




874F-70-2



## ORIGINAL TRANSMIT (TX) ANTENNA, REMOVED AND REPLACED

## ANT220F2DIN FIBERGLASS COLLINEAR ANTENNA

The Telewave ANT220F2 is an extremely rugged collinear antenna, with moderate gain and wide vertical beamwidth. This compact antenna produces 2.5 dBd gain, and is designed for operation in all environmental conditions. The antenna is constructed with brass and copper elements, with a path to ground potential for lightning impulse protection. The ANT220F2 is an excellent choice for wireless PTC systems in urban or rural areas.

All junctions are fully soldered to prevent RF intermodulation, and each antenna is completely protected within a rugged, hightech radome to ensure survivability in the worst environments. The "Cool Blue" radome provides maximum protection from corrosive gases, ultraviolet radiation, icing, salt spray, acid rain, and wind blown abrasives.

The ANT220F2 includes the ANTC485 dual clamp set for mounting to a $1.5^{\prime \prime}$ to $3^{\prime \prime}$ O.D. support pipe, and a 24 " removable RG-213 DIN-Male jumper.


ANT220F2-230 MHz
Vertical Plane
Gain $=2.58 \mathrm{dBd}$



## SPECIFICATIONS

| Frequency (continuous) | $195-260 \mathrm{MHz}$ | Dimensions (L x base diam.) in. | $51 \times 2.75$ |
| :--- | :--- | :--- | :--- | :--- |
| Gain | 2.5 dBd | Tower weight (antenna + clamps) | 11 lb. |
| Power rating (typ.) | 500 watts | Shipping weight | 14 lb. |
| Impedance | 50 ohms | Wind rating / with 0.5" ice | $200 / 150 \mathrm{MPH}$ |
| VSWR | $1.5: 1$ or less | Maximum exposed area | $1.1 \mathrm{ft} .^{2}$ |
| Pattern | Omnidirectional | Lateral thrust at 100 MPH | 44 lb. |
| Vertical beamwidth | $38^{\circ}$ | Bending moment at top clamp | $47 \mathrm{ft} . \mathrm{lb}$. |
| Termination | $7-16 ~ D I N-F$ | $(100 \mathrm{MPH}, 40$ PSF flat plate equiv.) |  |



DETAIL B


ATTACHMENT C - CONSTRUCTION DRAWINGS




$\frac{\text { ANTENNA CABLE GROUNDING }}{\text { No SCALE }}$


NOTES
Do not install cabie ground kit at a bend and alwars otrect ground
wir doonn to crouno bar.

3. Meater proong shal be tre And part number as suppleo or

CONNECTION OF CABLE GROUND $\frac{\text { KIT TO ANTENNA CABLE }}{\text { No SCALE }}$


CABLE INSTALLATION WITH WALL $\frac{\text { FEED THRU ASSEMBLY }}{\text { No Scale }}$


ICE BRIDGE AD ANT
$\frac{\text { BRIDGE AND ANTENNA }}{\text { CABLE DETAII }}$
no scale


F
BLACK \& VEATCH



RIDGEFIELD 22N 1 PROSPECT STREET RIDGEFIELD, CT 06877

SHEET TITLE
GROUNDING DETAILS -

## DESIGN BASIS

GOVEENNG CODE： 2018 CONNECTICUT STATE BuLIING CODE（2015 BBC BaSIS）
GENERAL CONDITIONS

2．THE ENINER IS NOT：A GURANTOR OF THE NSTALING CONTRACTOR＇S WORK，RESPONSIBLE FOR

 IMNEDAAELY TO THE CONSTRUCTION MANAOCR
5．detalls Incluoed in this plan set are trical and aplly to smmar conomions．


8．THE Contractor sthal safeguro Agans dereang a fre hazaro，affecting tenant Egress
9．THE Contractor shall Remove All degri and contruction wate frou the sit each dar．
10．THE CONTRACTOR＇S HOURS OF Work shall be in accordance wit local cooes and


THERMAL \＆MOISTURE PROTECTION


位
3．FRRETTOPRNG SHALL BE APPLED AS SOON AS PRACTCABLE ATER PENetrations ARE MADE AND




6．ALLL Penetrations into ano／or through buliong exterior walls shall．be sealeo with

8．contractor to remove and re－－Install all fire proofing as reaured during
SUBMITTALS
Contractor to submt shop dramngs to enginer for revew prior to fabrcation．
2．Contractor to notiry enaineer for inspection pror to closing penetrations．

 Prooucts．


## STEE




2．DAMAGED GAMVMIED SURFACES SHAL BE CIEANED WTH A WRE ERUSH AND PANTED WTH TWO
 SAME PANT IN SHOP OR FELD．
3．Desicn fabracaton and erecion of structural steel shall conform to the aisc＂Manual

5．All steel elements shall be nstalleo plumb and level．
5．All str maracterers desions sum prama ano tevel

## SITE GENERAL

CONTractor s．anl foliow conotions of all applicable permits and work in accoroance





 LIMTED TO．APPROPRATE A AAL PR

5．ALL ExSTIN NACTVE SEWER，WAIER，GAS，ELECTRC，FBER OPTC，OR OTHER UTLTIES，WHICH

6．Coniractor is fessonsile for repaling or replacing structures or utlumes damaged




F

## BLACK \＆VEATCH



| $\begin{array}{\|l\|} \hline \text { PROJECT NO: } \\ \hline \text { DRAWN BY: } \\ \hline \end{array}$ |  |
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\begin{gathered}
1 / 11111 \\
08 / 17 / 2021
\end{gathered}
$$

## ELECTRICAL



AUHORTIES SHALL APPL.


4. ALL ELECTRRCAL Conouctors Shall be 100\% COPPER AND SHALL HAVE TPE THHN INSULATON

6. ALL BURIED ConDut SHALL BE MNMMM SCH 40 PVC UNLESS NOTED OTHERWSE, OR AS PER


9. Conout ano cable witin corrdors shall be concealed and exposed elisewhere, uniess


11. Wirng deyices shal be specificaion grade, ano wring device cover plates shall be


14. THE CONTRACTOR SHALL RE REOURED To USTT THE STE PROR To Subumting bio in order to

Contractor is responsible for all conirol wrng and alarm tie-

## GROUNDIN

\#- triwn shall be stranoed \#6 copper with green thwn insuation sutable for wet
2. \#2 thwn shall be strandeo \#t copper with thwn nsulaton sutable for wei
 BETS SERES 548




7. THE MNMUM BEND Radus Shall be 8 INChes for \#6 Wre Ano smaller and 12 INCHES for


10. FERrous METAL cllps which completely surrouno the grounong conouctor shall be


NTENNA \& CABLE NOTES




3. antenna cables shall be color cooed at the followng locations:

AT THE ANEEGGDE ENTTY PPATE ON BOTH SIDES OF THE EQUPMENT SHELIER WALL.



5. MINMUM BENDNG RADUS FOR COAXAL CABLLES
$7 / 8 \mathrm{INCH}, \mathrm{RMN}=15$ NCHES
$15 / 8 \mathrm{NCH}, \mathrm{M}$ NIN $=25$
 All CABLE CONNECTONS OUTSIDE SHALL bE COVERED WTH WATERPROof SPLLING kII
. Contractor shall verfy exact length and directon of travel in fiel prior to
Cige shall be furnished without spluces and with connectops at each eil


F BLACK \& VEATCH

6800 W 1155 H ST, SUTE 2292
OVERRANO PARK, KS 66219
OERLAND PARK, KS 66211
PHONE: (913) 458-3595

## PROJECT NO: <br> DRAWN BY <br> CHECKED <br> ECKED BY: TCG

RIDGEFIELD 22N RIDGEFIELD CT 06877


## 220 MHz Antenna - Omnidirectional, Low-PIM/Hi-PIP, Unity Gain Models - SP2D00P36D-D

| Specifications |  |
| :---: | :---: |
| Design Type | True Corporate Feed |
| Frequency Range | 217-220 MHz |
| Passive Intermodulation - PIM ( $2 \times 20 \mathrm{~W}$ sources) | $-150 \mathrm{dBc}, 3^{\text {rd }}$ Order |
| Bandwidth | 3 MHz |
| Gain - dBd (average over BW) | 0 dBd |
| Isolation, min. | 40 dB |
| Configuration | Dual antenna |
| Beam Tilt (electrical down-tilt) | None ( $0^{\circ}$ ) |
| Vertical Beamwidth (E-Plane) | $60^{\circ}$ |
| Impedance -- Ohms | 50 |
| VSWR / Return Loss -- dB | 1.5 : 1 / 14 dB (min.) |
| Average Power Rating | 500 W (each antenna) |
| Peak Instantaneous Power | 25 kW (each antenna) |
| Polarization | Vertical |
| Lightning Protection | Direct Ground |
| Connector | 7/16 DIN female |
| Equivalent Flat-Plate Area | 2.59 sq. ft. |
| Lateral Wind-load Thrust @ 100 mph | 109 lbf . |
| Wind Speed rating | 160 mph (without ice) <br> $136 \mathrm{mph}\left(1 / 22^{\prime \prime}\right.$ radial ice) |
| Total Length | 15.6 feet |
| Mounting Mast Length | 35 inches |
| Mounting Hardware (Included) | DSH3V4N |
| Top Sway Brace <br> (Recommended if side mounting antennas) | DSH2H3S (order separately) |
| Mast O.D. | 3.5 inches |
| Radome color | Horizon Blue |
| Radome O.D. | 3.0 inches |
| Weight, antenna, and hardware | 45 lbs . (approx.) |
| Shipping Weight | 80 lbs . (approx.) |
| Invertibility | Antennas are physically invertible, but the patterns are optimized for upright mount. |

## Features and Benefits

Antennas from dbSpectra provide long term, trouble-free service in severe environments!
Design is tested to stringent Peak Instantaneous Power (PIP) levels of 25 KW using dbSpectra's 12-channel P25 PIP test bed. High PIP level is demanded by today's digital systems.
True Corporate Feed Array - provides for excellent gain and pattern consistency across a wider frequency range.
PIM Rated Design - better than -150 dBc .
Sturdy Construction - Heavy-wall fiberglass radome minimizes tip deflection.
Excellent Lightning Protection - heavy internal conductor DC ground.
Radiation Pattern


## ANT220F6 DIN FIBERGLASS COLLINEAR ANTENNA 6 dBd

The Telewave ANT220F6 is an extremely rugged, mediumgain, fiberglass collinear antenna, designed for operation in all environmental conditions. The antenna is constructed with brass and copper elements, connected at DC ground potential for lightning impulse protection. The ANT220F6 is an excellent choice for wireless PTC systems in urban or rural areas.

All junctions are fully soldered to prevent RF intermodulation, and each antenna is completely protected within a rugged, hightech radome to ensure survivability in the worst environments. The "Cool Blue" radome provides maximum protection from corrosive gases, ultraviolet radiation, icing, salt spray, acid rain, and wind blown abrasives.

The ANT220F6 includes an ANTC482 dual clamp set for mounting to a $1.5^{\prime \prime}$ to $3.5^{\prime \prime}$ O.D. support pipe, and a $24^{\prime \prime}$ removable RG-213 DIN-Male jumper. Stand-off and top mounts are also available. NOTE: THIS ANTENNA IS SHIPPED VIA TRUCK FREIGHT ONLY


ANT220F6-221 MHz
Vertical Plane
Gain $=6.11 \mathrm{dBd}$



## SPECIFICATIONS

| Frequency (continuous) | $216-225 \mathrm{MHz}$ | Dimensions (L x base diam.) in. | $171 \times 2.75$ |
| :--- | :--- | :--- | :--- |
| Gain | 6 dBd | Tower weight (antenna + clamps) | 35 lb. |
| Power rating (typ.) | 500 watts | Shipping weight | 50 lb. |
| Impedance | 50 ohms | Wind rating / with 0.5" ice | $150 / 125 \mathrm{MPH}$ |
| VSWR | $1.5: 1$ or less | Maximum exposed area | $3.1 \mathrm{ft} .^{2}$ |
| Pattern | Omnidirectional | Lateral thrust at 100 MPH | 122 lb. |
| Vertical beamwidth | $20^{\circ}$ | Bending moment at top clamp | $494 \mathrm{ft} . \mathrm{lb}$. |
| Termination | $7-16$ DIN-F | $(100 \mathrm{MPH}, 40$ PSF flat plate equiv.) |  |

## ANT220F2-I w/DIN CONNECTOR to be used for the inverted antenna.

## ANT220F2 FIBERGLASS COLLINEAR ANTENNA

The Telewave ANT220F2 is an extremely rugged collinear antenna, with moderate gain and wide vertical beamwidth. This compact antenna produces 2.5 dBd gain, and is designed for operation in all environmental conditions. The antenna is constructed with brass and copper elements, with a path to ground potential for lightning impulse protection. The ANT220F2 is an excellent choice for wireless PTC systems in urban or rural areas.

All junctions are fully soldered to prevent RF intermodulation, and each antenna is completely protected within a rugged, hightech radome to ensure survivability in the worst environments. The "Cool Blue" radome provides maximum protection from corrosive gases, ultraviolet radiation, icing, salt spray, acid rain, and wind blown abrasives.

The ANT220F2 includes the ANTC485 dual clamp set for mounting to a $1.5^{\prime \prime}$ to $3^{\prime \prime}$ O.D. support pipe, and a $24^{\prime \prime}$ removable RG-213 DIN-Male jumper.


ANT220F2-230 MHz
Vertical Plane
Gain $=2.58 \mathrm{dBd}$



## SPECIFICATIONS

| Frequency (continuous) | $195-260 \mathrm{MHz}$ | Dimensions (L x base diam.) in. | $51 \times 2.75$ |
| :--- | :--- | :--- | :--- | :--- |
| Gain | 2.5 dBd | Tower weight (antenna + clamps) | 11 lb. |
| Power rating (typ.) | 500 watts | Shipping weight | 14 lb. |
| Impedance | 50 ohms | Wind rating / with 0.5" ice | $200 / 150 \mathrm{MPH}$ |
| VSWR | $1.5: 1$ or less | Maximum exposed area | $1.1 \mathrm{ft}{ }^{2}$ |
| Pattern | Omnidirectional | Lateral thrust at 100 MPH | 44 lb. |
| Vertical beamwidth | $38^{\circ}$ | Bending moment at top clamp | $47 \mathrm{ft} . \mathrm{lb}$. |
| Termination | Recessed N Female <br> $7-16 ~ D I N-F ~ o p t . ~$ | (100 MPH, 40 PSF flat plate equiv.) |  |

ATTACHMENT D - STRUCTURAL ANALYSIS REPORT

Black \& Veatch Corp.
6800 W. 115th St., Suite 2292
Overland Park, KS 66211
(913) 458-2522

## Subject:

Eversource Designation:

Engineering Firm Designation:
Site Data:

## Structural Analysis Report

Site Number: ES-286
Site Name:
Black \& Veatch Corp. Project Number:

Off Prospect Street, Ridgefield, Fairfield County, CT Latitude $41^{\circ} 17{ }^{\prime} 0.59^{\prime \prime}$, Longitude -73 $29 ' 16.27^{\prime \prime}$
84 Foot - Monopole Tower
Black \& Veatch Corp. is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC1: Proposed Equipment Configuration
Sufficient Capacity - 53.4\%
This analysis utilizes an ultimate 3-second gust wind speed of 125 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Structural analysis prepared by: Anthony Reyes / Joshua J. Riley
Respectfully submitted by:

Joshua J. Riley, P.E. Professional Engineer


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## 1) INTRODUCTION

## 2) ANALYSIS CRITERIA

Table 1 - Proposed Equipment Configuration
Table 2 - Other Considered Equipment

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided
3.1) Analysis Method
3.2) Assumptions

## 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)
Table 5 - Tower Component Stresses vs. Capacity
4.1) Recommendations

## 5) APPENDIX A

tnxTower Output

## 6) APPENDIX B

Base Level Drawing

## 7) APPENDIX C

Additional Calculations

## 1) INTRODUCTION

This tower is an 84 ft Monopole tower designed by Valmont in July of 2012.

## 2) ANALYSIS CRITERIA

TIA-222 Revision:
Risk Category:
Wind Speed:
Exposure Category:
Topographic Factor:
Ice Thickness:
Wind Speed with Ice:
Seismic Ss:
Seismic $S_{1}$ :
Service Wind Speed:

TIA-222-H
III
125 mph ultimate
C
1
1.5 in

50 mph
0.229
0.068

60 mph

Table 1 - Proposed Equipment Configuration

| Mounting <br> Level (ft) | Center <br> Line <br> Elevation <br> (ft) | Number <br> of <br> Antennas | Antenna <br> Manufacturer | Antenna Model | Number <br> of Feed <br> Lines | Feed <br> Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 90.67 | 1 | dbspecta | SP2D00P36D-D | 2 | $7 / 8$ | 1 |
|  | 83.0 | 1 | generic | 4'x3" Mount Pipe | 2 |  | 1 |

Note:

1) Proposed equipment to be installed on existing relocated antenna's original antenna mount at 83.0 ft Mounting Level.

Table 2 - Other Considered Equipment

| Mounting Level (ft) | Center Line Elevation (ft) | $\begin{array}{\|\|l} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array}$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 83.0 | 90.0 | 1 | kreco | CO-41A | 2 | 7/8 | 1 |
|  | 88.0 | 1 | commscope | DB589-Y |  |  |  |
|  | 83.0 | 1 | tower mounts | Side Arm Mount [4' SO 701-3] |  |  |  |
| 67.0 | 74.0 | 1 | celwave | 1151-3 | 1 | 7/8 | 2 |
|  |  | 1 | kreco | CO-41A | 2 | 7/8 | 1 |
|  | 73.0 | 1 | kreco | CO-41A |  |  |  |
|  | 67.0 | 1 | tower mounts | Side Arm Mount [6' SO 701-3] |  |  |  |

Note:

1) Existing equipment
2) Existing equipment to be relocated from 83.0 ft Mounting Level to empty antenna mount on 67.0 ft Mounting Level.

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| GEOTECHNICAL REPORTS | Dr. Clarence Welti, P.E., P.C., <br> dated 06/14/2012 | - | Eversource |
| TOWER FOUNDATION <br> DRAWINGS/DESIGN/SPECS | Valmont, dated 7/27/2012 | - | Eversource |


| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| TOWER MANUFACTURER <br> DRAWINGS | Valmont, dated $7 / 27 / 2012$ | - | Eversource |

## 3.1) Analysis Method

tnxTower (version 8.1.1.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

## 3.2) Assumptions

1) Tower and structures were built and maintained in accordance with the manufacturer's specifications.
2) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
3) This analysis was performed under the assumption that all information provided to Black \& Veatch is current and correct. This is to include site data, appurtenance loading, tower/foundation details, and geotechnical data.

This analysis may be affected if any assumptions are not valid or have been made in error. Black \& Veatch Corp. should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 5 - Tower Component Stresses vs. Capacity - LC1

| Section <br> No. | Elevation (ft) | Component <br> Type | Size | Critical <br> Element | $\mathbf{P ( K )}$ | SF*P_allow <br> $\mathbf{( K )}$ | \% <br> Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $84-34.25$ | Pole | TP18.145x12.001×0.1875 | 1 | -2.07 | 639.52 | 37.8 | Pass |
| L2 | $34.25-0$ | Pole | TP22x17.3069x0.2188 | 2 | -4.62 | 928.93 | 53.4 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Pole (L2) | 53.4 | Pass |
|  |  |  |  |  |  | Rating $=$ | 53.4 | Pass |

Table 4 - Tower Component Stresses vs. Capacity - LC1

| Notes | Component | Elevation (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Anchor Rods | 0 | 52.1 | Pass |
|  | Base Plate |  | 22.9 | Pass |
| 1 | Base Foundation | 0 | 34.7 | Pass |
|  | Base Foundation Soil Interaction |  | 47.6 | Pass |

Notes:

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity. Rating per TIA-222-H Section 15.5.

Structure Rating (max from all components) = 53.4\%

## 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

## Maximum Tower Deflections - Service Wind

| Section | Elevation | Horz. | Gov. | Tilt | Twist | Check* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. |  | Deflection | Load |  |  |  |
|  | $f t$ | in | Comb. | $\circ$ | $\circ$ |  |
| L1 | $84-34.25$ | 11.155 | 44 | 1.0486 | 0.0208 | OK |
| L2 | $38-0$ | 2.598 | 44 | 0.6092 | 0.0051 | OK |

*Limit State Deformation (TIA-222-H Section 2.8.2)

1) Maximum Rotation $=4$ Degrees
2) Maximum Deflection $=0.03 *$ Tower Height $=30$ in.

## Maximum Tower Deflections - Design Wind

| Section | Elevation | Horz. | Gov. | Tilt | Twist | Combined | Check $^{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Deflection | Load |  |  | Max |  |  |
|  | $f t$ | in | Comb. | $\circ$ | $\circ$ |  |  |
| L1 | $84-34.25$ | 28.84 | 44 | 2.6937 | 0.0543 | 2.694 | OK $^{* *}$ |
| L2 | $38-0$ | 6.746 | 44 | 1.5807 | 0.0133 | 1.581 | OK $^{* *}$ |

*Up to 0.5 degree is considered acceptable per SUB090 Section 7
** Deflection approved by Eversource Energy

## APPENDIX A

## TNXTOWER OUTPUT

| TYPE | ELEVATION | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| Side Arm Mount [4' SO 701-1] | 83 | 3' x 2" Pipe Mount | 67 |
| 3' x 2" Pipe Mount | 83 | 3' x 2" Pipe Mount | 67 |
| 3' x 2" Pipe Mount | 83 | 3' x 2" Pipe Mount | 67 |
| 3' x 2" Pipe Mount | 83 | CO-41A | 67 |
| DB589-Y | 83 | CO-41A | 67 |
| CO-41A | 83 | 1151-3 | 67 |
| SP2D00P36D-D | 83 | Side Arm Mount [6' SO 701-1] | 67 |
| 4'x3" Mount Pipe | 83 |  |  |

MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A572-65 | 65 ksi | 80 ksi |  |  |  |  |

## TOWER DESIGN NOTES

1. Tower is located in Fairfield County, Connecticut.
2. Tower designed for Exposure C to the TIA-222-H Standard.
3. Tower designed for a 125 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 50 mph basic wind with 1.50 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category III.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: $53.4 \%$



TORQUE 1 kip-ft REACTIONS - 125 mph WIND

| एob: ES-286 Ridgefield22N |
| :--- |
| Project: $\mathbf{4 0 5 0 2 5}$ (Ridgefield22N) <br> Client: Eversource <br> Drawn by: Josh Riley <br> Code: TIA-222-H <br> Path: |

The tower is a monopole.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:

- Tower is located in Fairfield County, Connecticut.
- Tower base elevation above sea level: 666.00 ft .
- Basic wind speed of 125 mph .
- Risk Category III.
- Exposure Category C.
- Simplified Topographic Factor Procedure for wind speed-up calculations is used.
- Topographic Category: 1.
- Crest Height: 0.00 ft .
- Nominal ice thickness of 1.5000 in.
- Ice thickness is considered to increase with height.
- Ice density of 56 pcf.
- A wind speed of 50 mph is used in combination with ice.
- Temperature drop of $50^{\circ} \mathrm{F}$.
- Deflections calculated using a wind speed of 60 mph .
- A non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- $\quad$ Stress ratio used in pole design is 1.
- Tower analysis based on target reliabilities in accordance with Annex S.
- Load Modification Factors used: $\mathrm{K}_{\mathrm{es}}\left(\mathrm{F}_{\mathrm{w}}\right)=1.0, \mathrm{~K}_{\mathrm{es}}\left(\mathrm{t}_{\mathrm{i}}\right)=1.0$.
- Maximum demand-capacity ratio is: 1.05.
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.


## Options

[^2]Distribute Leg Loads As Uniform Assume Legs Pinned
$\checkmark$ Assume Rigid Index Plate
$\checkmark$ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
$\checkmark$ Bypass Mast Stability Checks
$\checkmark$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt.
Autocalc Torque Arm Areas
Add IBC .6D+W Combination Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation
$\checkmark$ Consider Feed Line Torque Include Angle Block Shear Check
Use TIA-222-H Bracing Resist.
Exemption
Use TIA-222-H Tension Splice
Exemption
Poles
$\sqrt{ }$ Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets
Pole Without Linear Attachments
Pole With Shroud Or No
Appurtenances
Outside and Inside Corner Radii Are
Known

| Section | Elevation ft | Section Length ft | Splice Length ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 84.00-34.25 | 49.75 | 3.75 | 18 | 12.0010 | 18.1450 | 0.1875 | 0.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
|  |  |  |  |  |  |  |  |  |  |
| L2 | 34.25-0.00 | 38.00 |  | 18 | 17.3069 | 22.0000 | 0.2188 | 0.8750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |

## Tapered Pole Properties

| Section | Tip Dia. <br> in | Area <br> $i n^{2}$ | I <br> $i n^{4}$ | $r$ <br> in | $C$ <br> $i n$ | $I / C$ <br> $i n^{3}$ | $J$ <br> $i n^{4}$ | $I t / Q$ <br> $i n^{2}$ | $w$ <br> in | $w / t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 12.1572 | 7.0305 | 123.9600 | 4.1938 | 6.0965 | 20.3329 | 248.0830 | 3.5159 | 1.7822 | 9.505 |
|  | 18.3960 | 10.6870 | 435.3948 | 6.3749 | 9.2177 | 47.2349 | 871.3626 | 5.3445 | 2.8635 | 15.272 |
| L2 | 18.0104 | 11.8645 | 437.6998 | 6.0663 | 8.7919 | 49.7845 | 875.9756 | 5.9334 | 2.6610 | 12.165 |
|  | 22.3056 | 15.1230 | 906.4437 | 7.7323 | 11.1760 | 81.1063 | 1814.0801 | 7.5629 | 3.4870 | 15.941 |


| Tower |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Elevation | Gusset <br> Area <br> (per face) | Gusset <br> Thickness | Gusset GradeAdjust. Factor | | Adjust. |
| :---: |
| Factor |$\quad$| Weight Mult. Double Angle Double Angle Double Angle |
| :---: |
| ft |

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Sector | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number | Number Per Row | Start/En d Position | Width or Diamete $r$ in | Perimete $r$ in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { ***miscl*** } \\ \text { Safety Line } 3 / 8 \end{gathered}$ | C | No | Surface Ar (CaAa) | $\begin{gathered} 84.00- \\ 10.00 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.010 \end{aligned}$ | 0.3750 |  | 0.22 |

## Feed Line/Linear Appurtenances - Entered As Area



## Feed Line/Linear Appurtenances Section Areas

| Tower <br> Sectio <br> $n$ | Tower <br> Elevation <br> $f t$ | Face | $A_{R}$ | $A_{F}$ | $C_{A} A_{A}$ <br> In Face <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Out Face <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $84.00-34.25$ | A | 0.000 | 0.000 | 0.000 | 0.000 | K |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.03 |
|  |  | C | 0.000 | 0.000 | 1.866 | 0.000 | 0.08 |
| L 2 | $34.25-0.00$ | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.02 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C | 0.000 | 0.000 | 0.909 | 0.000 | 0.06 |

## Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower <br> Sectio <br> $n$ | Tower <br> Elevation <br> ft | Face <br> or | Ice <br> Thickness <br> in | $A_{R}$ | $A_{F}$ | $C_{A} A_{A}$ <br> In Face <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Out Face | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t^{2}$ |  |  |  |  |  |  |  |  |


|  | Feed Line Center of Pressure |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Section | Elevation | $C P_{x}$ | $C P_{z}$ | $C P_{x}$ | $C P_{z}$ |
|  |  |  | in | in | in |
| Lt | $84.00-34.25$ | -0.0031 | 0.2996 | -0.0142 | 1.3545 |
| L2 | $34.25-0.00$ | -0.0022 | 0.2081 | -0.0112 | 1.0668 |

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

## Shielding Factor Ka

| Tower <br> Section | Feed Line <br> Record No. | Description | Feed Line <br> Segment <br> Elev. | $K_{a}$ <br> No Ice | $K_{a}$ <br> Ice |
| ---: | ---: | ---: | ---: | ---: | ---: |
| L1 | 2 | Safety Line 3/8 | $34.25-$ <br> 84.00 | 1.0000 | 1.0000 |
| L2 | 2 | Safety Line 3/8 | $10.00-$ <br> 34.25 | 1.0000 | 1.0000 |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& \begin{tabular}{l}
Azimuth Adjustmen \(t\) \\
\(\circ\)
\end{tabular} \& Placement

ft \& \& $C_{A} A_{A}$ Front

$$
f t^{2}
$$ \& $C_{A} A_{A}$ Side

$$
f t^{2}
$$ \& Weight <br>

\hline \multicolumn{10}{|l|}{***83***} <br>
\hline \multirow[t]{4}{*}{Side Arm Mount [4' SO 701-1]} \& C \& None \& \& 0.0000 \& 83.00 \& No Ice \& 1.13 \& 2.23 \& 0.09 <br>
\hline \& \& \& \& \& \& 1/2" \& 1.52 \& 3.12 \& 0.11 <br>
\hline \& \& \& \& \& \& Ice \& 1.91 \& 4.01 \& 0.12 <br>

\hline \& \& \& \& \& \& | 1" Ice |
| :--- |
| 2" Ice | \& 2.68 \& 5.80 \& 0.16 <br>

\hline \multirow[t]{4}{*}{3' x 2" Pipe Mount} \& A \& From Face \& 6.00 \& 0.0000 \& 83.00 \& No Ice \& 0.58 \& 0.58 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.77 \& 0.77 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.97 \& 0.97 \& 0.02 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& 2 " \text { Ice }
\end{aligned}
$$ \& 1.39 \& 1.39 \& 0.05 <br>

\hline \multirow[t]{5}{*}{3' x 2" Pipe Mount} \& B \& From Face \& 6.00 \& 0.0000 \& 83.00 \& No Ice \& 0.58 \& 0.58 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.77 \& 0.77 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.97 \& 0.97 \& 0.02 <br>
\hline \& \& \& \& \& \& 1 ' Ice \& 1.39 \& 1.39 \& 0.05 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3' x 2" Pipe Mount} \& C \& From Face \& 6.00 \& 0.0000 \& 83.00 \& No Ice \& 0.58 \& 0.58 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.77 \& 0.77 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.97 \& 0.97 \& 0.02 <br>
\hline \& \& \& \& \& \& 1 ' Ice \& 1.39 \& 1.39 \& 0.05 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{DB589-Y} \& C \& From Face \& 6.00 \& 0.0000 \& 83.00 \& No Ice \& 1.38 \& 1.38 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.31 \& 2.31 \& 0.02 <br>
\hline \& \& \& 5.00 \& \& \& Ice \& 3.27 \& 3.27 \& 0.04 <br>
\hline \& \& \& \& \& \& 1 ' Ice \& 4.81 \& 4.81 \& 0.09 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{CO-41A} \& A \& From Face \& 6.00 \& 0.0000 \& 83.00 \& No Ice \& 3.15 \& 3.15 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 4.38 \& 4.38 \& 0.04 <br>
\hline \& \& \& 6.00 \& \& \& Ice \& 5.63 \& 5.63 \& 0.07 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 7.77 \& 7.77 \& 0.15 <br>
\hline \& \& \& \& \& \& 2 ' Ice \& \& \& <br>
\hline \multicolumn{10}{|l|}{***Relocated to 67*** 0} <br>
\hline \multirow[t]{5}{*}{1151-3} \& C \& From Face \& 6.00 \& 0.0000 \& 67.00 \& No Ice \& \& 4.18 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 5.73 \& 5.73 \& 0.05 <br>
\hline \& \& \& 7.00 \& \& \& Ice \& 7.30 \& 7.30 \& 0.09 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 10.48 \& 10.48 \& 0.20 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multicolumn{10}{|l|}{} <br>

\hline \multirow[t]{5}{*}{Side Arm Mount [6' SO 701-1]} \& C \& None \& \& 0.0000 \& 67.00 \& \& \& $$
3.34
$$ \& <br>

\hline \& \& \& \& \& \& 1/2" \& $$
2.28
$$ \& \[

4.68

\] \& \[

0.16
\] <br>

\hline \& \& \& \& \& \& Ice \& 2.86 \& 6.02 \& 0.19 <br>
\hline \& \& \& \& \& \& 1" Ice \& 4.02 \& 8.70 \& 0.24 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>

\hline \multirow[t]{5}{*}{3' x 2" Pipe Mount} \& A \& From Face \& \& 0.0000 \& 67.00 \& \& 0.58 \& 0.58 \& $$
0.01
$$ <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime}
$$ \& 0.77 \& 0.77 \& 0.02 <br>

\hline \& \& \& 0.00 \& \& \& Ice \& 0.97 \& 0.97 \& 0.02 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 1.39 \& 1.39 \& 0.05 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3' x 2" Pipe Mount} \& B \& From Face \& \& 0.0000 \& 67.00 \& No Ice \& 0.58 \& 0.58 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.77 \& 0.77 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.97 \& 0.97 \& 0.02 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.39 \& 1.39 \& 0.05 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3' x 2" Pipe Mount} \& C \& From Face \& \& 0.0000 \& 67.00 \& No Ice \& 0.58 \& 0.58 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.77 \& 0.77 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.97 \& 0.97 \& 0.02 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.39 \& 1.39 \& 0.05 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{CO-41A} \& A \& From Face \& \& 0.0000 \& 67.00 \& No Ice \& 3.15 \& 3.15 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 4.38 \& 4.38 \& 0.04 <br>
\hline \& \& \& 7.00 \& \& \& Ice \& 5.63 \& 5.63 \& 0.07 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 7.77 \& 7.77 \& 0.15 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{2}{*}{CO-41A} \& B \& From Face \& 6.00 \& 0.0000 \& 67.00 \& No Ice \& 3.15 \& 3.15 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 4.38 \& 4.38 \& 0.04 <br>
\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen \(t\) \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& C \({ }_{\text {A }} A_{A}\)
Side \& Weight

K <br>
\hline \& \& \& 6.00 \& \& \& Ice \& 5.63 \& 5.63 \& 0.07 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& 2 " \text { Ice }
\end{aligned}
$$ \& 7.77 \& 7.77 \& 0.15 <br>

\hline \multicolumn{10}{|l|}{*Proposed*} <br>
\hline \multirow[t]{5}{*}{SP2D00P36D-D} \& B \& From Leg \& 4.50 \& 0.0000 \& 83.00 \& No Ice \& 5.36 \& 5.36 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 7.06 \& 7.06 \& 0.08 <br>
\hline \& \& \& 7.67 \& \& \& Ice \& 8.67 \& 8.67 \& 0.13 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 11.95 \& 11.95 \& 0.26 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{4'x3" Mount Pipe} \& B \& From Leg \& 4.00 \& 0.0000 \& 83.00 \& No Ice \& 1.09 \& 1.09 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.36 \& 1.36 \& 0.04 <br>
\hline \& \& \& 1.00 \& \& \& Ice \& 1.62 \& 1.62 \& 0.05 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.16 \& 2.16 \& 0.09 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multicolumn{10}{|l|}{***} <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>
\hline
\end{tabular}

## Load Combinations

| Comb. No. | Description |
| :---: | :---: |
| 1 | Dead Only |
| 2 | 1.2 Dead+1.0 Wind 0 deg - No Ice |
| 3 | 0.9 Dead+1.0 Wind 0 deg - No Ice |
| 4 | 1.2 Dead+1.0 Wind 30 deg - No Ice |
| 5 | 0.9 Dead+1.0 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.0 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.0 Wind 60 deg - No Ice |
| 8 | 1.2 Dead+1.0 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.0 Wind 90 deg - No Ice |
| 10 | 1.2 Dead+1.0 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.0 Wind 120 deg - No Ice |
| 12 | 1.2 Dead+1.0 Wind 150 deg - No Ice |
| 13 | 0.9 Dead+1.0 Wind 150 deg - No Ice |
| 14 | 1.2 Dead+1.0 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.0 Wind 180 deg - No Ice |
| 16 | 1.2 Dead+1.0 Wind 210 deg - No Ice |
| 17 | 0.9 Dead+1.0 Wind 210 deg - No Ice |
| 18 | 1.2 Dead+1.0 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.0 Wind 240 deg - No Ice |
| 20 | 1.2 Dead+1.0 Wind 270 deg - No Ice |
| 21 | 0.9 Dead+1.0 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.0 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.0 Wind 300 deg - No Ice |
| 24 | 1.2 Dead+1.0 Wind 330 deg - No Ice |
| 25 | 0.9 Dead+1.0 Wind 330 deg - No Ice |
| 26 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 27 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |
| 28 | 1.2 Dead+1.0 Wind $30 \mathrm{deg}+1.0 \mathrm{Ice}+1.0$ Temp |
| 29 | 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp |
| 30 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp |
| 32 | 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp |
| 33 | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp |
| 34 | 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp |
| 35 | 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp |
| 36 | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp |
| 37 | 1.2 Dead+1.0 Wind $300 \mathrm{deg}+1.0 \mathrm{Ice+1.0}$ Temp |
| 38 | 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp |


| Comb. |  | Description |
| :---: | :--- | :--- |
| No. |  |  |
| 39 | Dead+Wind 0 deg - Service |  |
| 40 | Dead+Wind 30 deg - Service |  |
| 41 | Dead+Wind 60 deg - Service |  |
| 42 | Dead+Wind 90 deg - Service |  |
| 43 | Dead+Wind 120 deg - Service |  |
| 44 | Dead+Wind 150 deg - Service |  |
| 45 | Dead+Wind 180 deg - Service |  |
| 46 | Dead+Wind 210 deg - Service |  |
| 47 | Dead+Wind 240 deg - Service |  |
| 48 | Dead+Wind 270 deg - Service |  |
| 49 | Dead+Wind 300 deg - Service |  |
| 50 | Dead+Wind 330 deg - Service |  |

## Maximum Member Forces

| Sectio <br> $n$ No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 84-34.25 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -5.51 | -0.71 | -1.51 |
|  |  |  | Max. Mx | 8 | -2.07 | -108.95 | -0.35 |
|  |  |  | Max. My | 14 | -2.07 | -0.33 | -108.97 |
|  |  |  | Max. Vy | 8 | 3.55 | -108.95 | -0.35 |
|  |  |  | Max. Vx | 14 | 3.55 | -0.33 | -108.97 |
|  |  |  | Max. Torque | 19 |  |  | 1.15 |
| L2 | 34.25-0 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -9.78 | -0.73 | -1.68 |
|  |  |  | Max. Mx | 8 | -4.62 | -275.32 | -0.37 |
|  |  |  | Max. My | 14 | -4.62 | -0.34 | -275.35 |
|  |  |  | Max. Vy | 8 | 5.16 | -275.32 | -0.37 |
|  |  |  | Max. Vx | 14 | 5.16 | -0.34 | -275.35 |
|  |  |  | Max. Torque | 19 |  |  | 1.15 |

## Maximum Reactions

| Location | Condition | Gov. Load Comb. | Vertical K | $\begin{gathered} \text { Horizontal, X } \\ K \end{gathered}$ | Horizontal, Z K |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pole | Max. Vert | 33 | 9.78 | -0.00 | -1.73 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 21 | 3.47 | 5.15 | -0.00 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 2 | 4.62 | -0.00 | 5.15 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 2 | 274.60 | -0.00 | 5.15 |
|  | Max. Mz | 8 | 275.32 | -5.15 | -0.00 |
|  | Max. Torsion | 19 | 1.15 | 4.46 | -2.58 |
|  | Min. Vert | 7 | 3.47 | -4.46 | 2.58 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 8 | 4.62 | -5.15 | -0.00 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 14 | 4.62 | -0.00 | -5.15 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 14 | -275.35 | -0.00 | -5.15 |
|  | Min. $M_{z}$ | 20 | -274.63 | 5.15 | -0.00 |
|  | Min. Torsion | 7 | -1.15 | -4.46 | 2.58 |

## Tower Mast Reaction Summary

| Load <br> Combination | Vertical | Shear $_{x}$ | Shear $_{z}$ | Overturning <br> Moment, $M_{x}$ <br> kip-ft | Overturning <br> Moment, $M_{z}$ | Torque |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | $K$ | $K$ | $K$ | $K$ | 0.31 | kip-ft |


| Load Combination | Vertical $K$ | Shear $_{x}$ <br> K | Shear $_{z}$ <br> K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | $\begin{gathered} \hline \text { Torque } \\ \text { kip-ft } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.9 Dead+1.0 Wind 0 deg - | 3.47 | 0.00 | -5.15 | -272.87 | -0.26 | 0.48 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 30 deg No Ice | 4.62 | 2.58 | -4.46 | -237.76 | -137.83 | 0.93 |
| 0.9 Dead+1.0 Wind 30 deg - | 3.47 | 2.58 | -4.46 | -236.28 | -136.83 | 0.94 |
| 1.2 Dead+1.0 Wind 60 deg No Ice | 4.62 | 4.46 | -2.58 | -137.11 | -238.48 | 1.15 |
| 0.9 Dead+1.0 Wind 60 deg No Ice | 3.47 | 4.46 | -2.58 | -136.30 | -236.81 | 1.15 |
| 1.2 Dead+1.0 Wind 90 deg No Ice | 4.62 | 5.15 | 0.00 | 0.37 | -275.32 | 1.05 |
| 0.9 Dead+1.0 Wind 90 deg - No Ice | 3.47 | 5.15 | 0.00 | 0.28 | -273.41 | 1.05 |
| 1.2 Dead+1.0 Wind 120 deg <br> - No Ice | 4.62 | 4.46 | 2.58 | 137.86 | -238.48 | 0.67 |
| 0.9 Dead+1.0 Wind 120 deg <br> - No Ice | 3.47 | 4.46 | 2.58 | 136.85 | -236.81 | 0.67 |
| 1.2 Dead+1.0 Wind 150 deg <br> - No Ice | 4.62 | 2.58 | 4.46 | 238.51 | -137.83 | 0.12 |
| 0.9 Dead+1.0 Wind 150 deg <br> - No Ice | 3.47 | 2.58 | 4.46 | 236.84 | -136.83 | 0.11 |
| 1.2 Dead+1.0 Wind 180 deg <br> - No Ice | 4.62 | 0.00 | 5.15 | 275.35 | -0.34 | -0.47 |
| 0.9 Dead+1.0 Wind 180 deg <br> - No Ice | 3.47 | 0.00 | 5.15 | 273.43 | -0.26 | -0.48 |
| 1.2 Dead+1.0 Wind 210 deg <br> - No Ice | 4.62 | -2.58 | 4.46 | 238.51 | 137.14 | -0.93 |
| 0.9 Dead+1.0 Wind 210 deg <br> - No Ice | 3.47 | -2.58 | 4.46 | 236.83 | 136.32 | -0.94 |
| 1.2 Dead+1.0 Wind 240 deg <br> - No Ice | 4.62 | -4.46 | 2.58 | 137.86 | 237.79 | -1.15 |
| 0.9 Dead+1.0 Wind 240 deg <br> - No Ice | 3.47 | -4.46 | 2.58 | 136.85 | 236.30 | -1.15 |
| 1.2 Dead+1.0 Wind 270 deg <br> - No Ice | 4.62 | -5.15 | 0.00 | 0.37 | 274.63 | -1.05 |
| 0.9 Dead+1.0 Wind 270 deg <br> - No Ice | 3.47 | -5.15 | 0.00 | 0.28 | 272.90 | -1.05 |
| 1.2 Dead+1.0 Wind 300 deg <br> - No Ice | 4.62 | -4.46 | -2.58 | -137.11 | 237.79 | -0.67 |
| 0.9 Dead+1.0 Wind 300 deg <br> - No Ice | 3.47 | -4.46 | -2.58 | -136.30 | 236.30 | -0.67 |
| 1.2 Dead+1.0 Wind 330 deg <br> - No Ice | 4.62 | -2.58 | -4.46 | -237.76 | 137.14 | -0.12 |
| 0.9 Dead+1.0 Wind 330 deg <br> - No Ice | 3.47 | -2.58 | -4.46 | -236.28 | 136.32 | -0.11 |
| 1.2 Dead+1.0 Ice+1.0 Temp | 9.78 | 0.00 | 0.00 | 1.68 | -0.73 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp | 9.78 | 0.00 | -1.73 | -98.49 | -0.73 | 0.12 |
| 1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp | 9.78 | 0.87 | -1.50 | -85.07 | -50.82 | 0.33 |
| 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp | 9.78 | 1.50 | -0.87 | -48.40 | -87.48 | 0.44 |
| 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp | 9.78 | 1.73 | 0.00 | 1.68 | -100.91 | 0.44 |
| 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp | 9.78 | 1.50 | 0.87 | 51.77 | -87.48 | 0.33 |
| 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp | 9.78 | 0.87 | 1.50 | 88.44 | -50.82 | 0.12 |
| 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp | 9.78 | 0.00 | 1.73 | 101.86 | -0.73 | -0.12 |
| 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp | 9.78 | -0.87 | 1.50 | 88.44 | 49.36 | -0.33 |
| 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp | 9.78 | -1.50 | 0.87 | 51.77 | 86.03 | -0.44 |
| 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp | 9.78 | -1.73 | 0.00 | 1.68 | 99.45 | -0.44 |
| 1.2 Dead+1.0 Wind 300 | 9.78 | -1.50 | -0.87 | -48.40 | 86.03 | -0.32 |

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| Load Combination | Vertical <br> K | Shear $_{x}$ K | Shear $_{z}$ <br> K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp | 9.78 | -0.87 | -1.50 | -85.07 | 49.36 | -0.12 |
| Dead+Wind 0 deg - Service | 3.85 | 0.00 | -1.06 | -56.30 | -0.29 | 0.10 |
| Dead+Wind 30 deg - Service | 3.85 | 0.53 | -0.92 | -48.71 | -28.60 | 0.20 |
| Dead+Wind 60 deg - Service | 3.85 | 0.92 | -0.53 | -27.99 | -49.32 | 0.24 |
| Dead+Wind 90 deg - Service | 3.85 | 1.06 | 0.00 | 0.31 | -56.90 | 0.22 |
| Dead+Wind 120 deg - | 3.85 | 0.92 | 0.53 | 28.62 | -49.32 | 0.14 |
| Service |  |  |  |  |  |  |
| Dead+Wind 150 deg - | 3.85 | 0.53 | 0.92 | 49.34 | -28.60 | 0.02 |
| Service |  |  |  |  |  |  |
| Dead+Wind 180 deg - | 3.85 | 0.00 | 1.06 | 56.93 | -0.29 | -0.10 |
| Service |  |  |  |  |  |  |
| Dead+Wind 210 deg - | 3.85 | -0.53 | 0.92 | 49.34 | 28.02 | -0.20 |
| Service |  |  |  |  |  |  |
| Dead+Wind 240 deg - | 3.85 | -0.92 | 0.53 | 28.62 | 48.74 | -0.24 |
| Service |  |  |  |  |  |  |
| Dead+Wind 270 deg - | 3.85 | -1.06 | 0.00 | 0.31 | 56.32 | -0.22 |
| Service |  |  |  |  |  |  |
| Dead+Wind 300 deg - | 3.85 | -0.92 | -0.53 | -27.99 | 48.74 | -0.14 |
| Service |  |  |  |  |  |  |
| Dead+Wind 330 deg - | 3.85 | -0.53 | -0.92 | -48.71 | 28.02 | -0.02 |
| Service |  |  |  |  |  |  |

## Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | $P Z$ | $P X$ | PY | $P Z$ |  |
| Comb. | K | K | K | K | K | K |  |
| 1 | 0.00 | -3.85 | 0.00 | 0.00 | 3.85 | 0.00 | 0.000\% |
| 2 | 0.00 | -4.62 | -5.15 | -0.00 | 4.62 | 5.15 | 0.000\% |
| 3 | 0.00 | -3.47 | -5.15 | -0.00 | 3.47 | 5.15 | 0.000\% |
| 4 | 2.58 | -4.62 | -4.46 | -2.58 | 4.62 | 4.46 | 0.000\% |
| 5 | 2.58 | -3.47 | -4.46 | -2.58 | 3.47 | 4.46 | 0.000\% |
| 6 | 4.46 | -4.62 | -2.58 | -4.46 | 4.62 | 2.58 | 0.000\% |
| 7 | 4.46 | -3.47 | -2.58 | -4.46 | 3.47 | 2.58 | 0.000\% |
| 8 | 5.15 | -4.62 | 0.00 | -5.15 | 4.62 | -0.00 | 0.000\% |
| 9 | 5.15 | -3.47 | 0.00 | -5.15 | 3.47 | -0.00 | 0.000\% |
| 10 | 4.46 | -4.62 | 2.58 | -4.46 | 4.62 | -2.58 | 0.000\% |
| 11 | 4.46 | -3.47 | 2.58 | -4.46 | 3.47 | -2.58 | 0.000\% |
| 12 | 2.58 | -4.62 | 4.46 | -2.58 | 4.62 | -4.46 | 0.000\% |
| 13 | 2.58 | -3.47 | 4.46 | -2.58 | 3.47 | -4.46 | 0.000\% |
| 14 | 0.00 | -4.62 | 5.15 | -0.00 | 4.62 | -5.15 | 0.000\% |
| 15 | 0.00 | -3.47 | 5.15 | -0.00 | 3.47 | -5.15 | 0.000\% |
| 16 | -2.58 | -4.62 | 4.46 | 2.58 | 4.62 | -4.46 | 0.000\% |
| 17 | -2.58 | -3.47 | 4.46 | 2.58 | 3.47 | -4.46 | 0.000\% |
| 18 | -4.46 | -4.62 | 2.58 | 4.46 | 4.62 | -2.58 | 0.000\% |
| 19 | -4.46 | -3.47 | 2.58 | 4.46 | 3.47 | -2.58 | 0.000\% |
| 20 | -5.15 | -4.62 | 0.00 | 5.15 | 4.62 | -0.00 | 0.000\% |
| 21 | -5.15 | -3.47 | 0.00 | 5.15 | 3.47 | -0.00 | 0.000\% |
| 22 | -4.46 | -4.62 | -2.58 | 4.46 | 4.62 | 2.58 | 0.000\% |
| 23 | -4.46 | -3.47 | -2.58 | 4.46 | 3.47 | 2.58 | 0.000\% |
| 24 | -2.58 | -4.62 | -4.46 | 2.58 | 4.62 | 4.46 | 0.000\% |
| 25 | -2.58 | -3.47 | -4.46 | 2.58 | 3.47 | 4.46 | 0.000\% |
| 26 | 0.00 | -9.78 | 0.00 | -0.00 | 9.78 | -0.00 | 0.000\% |
| 27 | 0.00 | -9.78 | -1.73 | -0.00 | 9.78 | 1.73 | 0.000\% |
| 28 | 0.87 | -9.78 | -1.50 | -0.87 | 9.78 | 1.50 | 0.000\% |
| 29 | 1.50 | -9.78 | -0.87 | -1.50 | 9.78 | 0.87 | 0.000\% |
| 30 | 1.73 | -9.78 | 0.00 | -1.73 | 9.78 | -0.00 | 0.000\% |
| 31 | 1.50 | -9.78 | 0.87 | -1.50 | 9.78 | -0.87 | 0.000\% |
| 32 | 0.87 | -9.78 | 1.50 | -0.87 | 9.78 | -1.50 | 0.000\% |
| 33 | 0.00 | -9.78 | 1.73 | -0.00 | 9.78 | -1.73 | 0.000\% |
| 34 | -0.87 | -9.78 | 1.50 | 0.87 | 9.78 | -1.50 | 0.000\% |
| 35 | -1.50 | -9.78 | 0.87 | 1.50 | 9.78 | -0.87 | 0.000\% |
| 36 | -1.73 | -9.78 | 0.00 | 1.73 | 9.78 | -0.00 | 0.000\% |
| 37 | -1.50 | -9.78 | -0.87 | 1.50 | 9.78 | 0.87 | 0.000\% |
| 38 | -0.87 | -9.78 | -1.50 | 0.87 | 9.78 | 1.50 | 0.000\% |

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|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | $P Z$ | $P X$ | PY | $P Z$ |  |
| Comb. | K | K | K | K | K | K |  |
| 39 | 0.00 | -3.85 | -1.06 | 0.00 | 3.85 | 1.06 | 0.000\% |
| 40 | 0.53 | -3.85 | -0.92 | -0.53 | 3.85 | 0.92 | 0.000\% |
| 41 | 0.92 | -3.85 | -0.53 | -0.92 | 3.85 | 0.53 | 0.000\% |
| 42 | 1.06 | -3.85 | 0.00 | -1.06 | 3.85 | 0.00 | 0.000\% |
| 43 | 0.92 | -3.85 | 0.53 | -0.92 | 3.85 | -0.53 | 0.000\% |
| 44 | 0.53 | -3.85 | 0.92 | -0.53 | 3.85 | -0.92 | 0.000\% |
| 45 | 0.00 | -3.85 | 1.06 | 0.00 | 3.85 | -1.06 | 0.000\% |
| 46 | -0.53 | -3.85 | 0.92 | 0.53 | 3.85 | -0.92 | 0.000\% |
| 47 | -0.92 | -3.85 | 0.53 | 0.92 | 3.85 | -0.53 | 0.000\% |
| 48 | -1.06 | -3.85 | 0.00 | 1.06 | 3.85 | 0.00 | 0.000\% |
| 49 | -0.92 | -3.85 | -0.53 | 0.92 | 3.85 | 0.53 | 0.000\% |
| 50 | -0.53 | -3.85 | -0.92 | 0.53 | 3.85 | 0.92 | 0.000\% |

Non-Linear Convergence Results

| Load <br> Combination | Converged? | Number <br> of Cycles | Displacement <br> Tolerance | Force <br> Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 4 | 0.00000001 | 0.00000001 |
| 2 | Yes | 4 | 0.00000001 | 0.00045030 |
| 3 | Yes | 4 | 0.00000001 | 0.00026285 |
| 4 | Yes | 5 | 0.00000001 | 0.00007940 |
| 5 | Yes | 5 | 0.00000001 | 0.0003247 |
| 6 | Yes | 5 | 0.00000001 | 0.00005347 |
| 7 | Yes | 5 | 0.00000001 | 0.00000001 |
| 8 | Yes | 4 | 0.00000001 | 0.00094922 |
| 9 | Yes | 4 | 0.00000001 | 0.00055649 |
| 10 | Yes | 5 | 0.00000001 | 0.00007431 |
| 11 | Yes | 5 | 0.00000001 | 0.0003003 |
| 12 | Yes | 5 | 0.00000001 | 0.00006135 |
| 13 | Yes | 5 | 0.00000001 | 0.00000001 |
| 14 | Yes | 4 | 0.00000001 | 0.00045117 |
| 15 | Yes | 4 | 0.00000001 | 0.00026295 |
| 16 | Yes | 5 | 0.00000001 | 0.0005374 |
| 17 | Yes | 5 | 0.00000001 | 0.00000001 |
| 18 | Yes | 5 | 0.00000001 | 0.00008390 |
| 19 | Yes | 5 | 0.00000001 | 0.00003446 |
| 20 | Yes | 4 | 0.00000001 | 0.00094807 |
| 21 | Yes | 4 | 0.00000001 | 0.00055664 |
| 22 | Yes | 5 | 0.00000001 | 0.0005475 |
| 23 | Yes | 5 | 0.00000001 | 0.00000001 |
| 24 | Yes | 5 | 0.00000001 | 0.00006353 |
| 25 | Yes | 5 | 0.00000001 | 0.00000001 |
| 26 | Yes | 4 | 0.00000001 | 0.00003689 |
| 27 | Yes | 5 | 0.00000001 | 0.0008590 |
| 28 | Yes | 5 | 0.00000001 | 0.00014014 |
| 29 | Yes | 5 | 0.00000001 | 0.00012552 |
| 30 | Yes | 5 | 0.00000001 | 0.00010894 |
| 31 | Yes | 5 | 0.00000001 | 0.00015104 |
| 32 | Yes | 5 | 0.00000001 | 0.00003248 |
| 33 | Yes | 5 | 0.00000001 | 0.0009114 |
| 34 | Yes | 5 | 0.00000001 | 0.00012732 |
| 35 | Yes | 5 | 0.00000001 | 0.00015389 |
| 36 | Yes | 5 | 0.00000001 | 0.00010589 |
| 37 | Yes | 5 | 0.00000001 | 0.00001911 |
| 38 | Yes | 5 | 0.00000001 | 0.00012464 |
| 39 | Yes | 4 | 0.00000001 | 0.00000001 |
| 40 | Yes | 4 | 0.00000001 | 0.00007604 |
| 41 | Yes | 4 | 0.00000001 | 0.00005715 |
| 42 | Yes | 4 | 0.00000001 | 0.00006222 |
| 43 | Yes | 4 | 0.00000001 | 0.0006224 |
| 44 | Yes | 4 | 0.00000001 | 0.00000001 |
| 45 | Yes | 4 | 0.00000001 | 0.00000001 |
| 46 | Yes | 4 | 0.00000001 | 0.00000001 |
| 47 | Yes | 4 | 0.00000001 | 0.00008699 |
| 48 | Yes | 4 | 0.00000001 | 0.00006095 |
|  |  |  |  |  |
|  |  | 5 |  |  |


| 49 | Yes | 4 | 0.00000001 | 0.00000001 |
| :--- | :--- | :--- | :--- | :--- |
| 50 | Yes | 4 | 0.00000001 | 0.00000001 |

## Maximum Tower Deflections - Service Wind

| Section | Elevation | Horz. <br> Deflection <br> No. | in | Gov. <br> Load | Tilt |
| :---: | :---: | :---: | :---: | :---: | :---: |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. <br> Load Comb. | Deflection in | Tilt | Twist 。 | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 83.00 | Side Arm Mount [4' SO 701-1] | 44 | 10.936 | 1.0408 | 0.0204 | 26287 |
| 67.00 | 1151-3 | 44 | 7.520 | 0.9122 | 0.0142 | 7731 |


|  | Maximum Tower Defiections - Design Mind |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation | Horz. | Gov. | Tilt | Twist |
| No. | Deflection | Load | $\circ$ | $\circ$ |  |
|  | ft | in | Comb. | ${ }^{\circ}$ | 0.0982 |
| L1 | $84-34.25$ | 53.438 | 12 | 4.9853 | 0.0240 |
| L2 | $38-0$ | 12.525 | 12 | 2.9349 |  |

## Critical Deflections and Radius of Curvature - Design Wind

| Elevation <br> ft <br> 8 | Appurtenance | Gov. Load Comb. | Deflection <br> in | Tilt | Twist 。 | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 83.00 | Side Arm Mount [4' SO 701-1] | 12 | 52.395 | 4.9496 | 0.0963 | 5584 |
| 67.00 | 1151-3 | 12 | 36.068 | 4.3587 | 0.0668 | 1640 |

## Compression Checks

| Pole Design Data |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. |  | Size |  |  | Kl/r | $A$ |  | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
|  | $f t$ |  | $f t$ | ft |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| L1 | 84-34.25 (1) | TP18.145×12.001x0.1875 | 49.75 | 0.00 | 0.0 | $\begin{gathered} 10.411 \\ 3 \end{gathered}$ | -2.07 | 609.06 | 0.003 |
| L2 | 34.25-0 (2) | TP22x17.3069x0.2188 | 38.00 | 0.00 | 0.0 | $\begin{gathered} 15.123 \\ 0 \end{gathered}$ | -4.62 | 884.70 | 0.005 |

## Pole Bending Design Data

| Section No. | Elevation | Size | $M_{u x}$ <br> kip-ft | $\phi M_{n x}$ | $\begin{aligned} & \text { Ratio } \\ & M_{u x} \\ & \hline \end{aligned}$ | $M_{u y}$ kip-ft | $\phi M_{n y}$ kip-ft | $\begin{gathered} \text { Ratio } \\ M_{u y} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 84-34.25 (1) | TP18.145×12.001×0.1875 | 109.09 | 277.48 | ¢ $M_{n x}$ 0.393 | 0.00 | kip-ft | $\phi M_{n y}$ 0.000 |
| L2 | 34.25-0 (2) | TP $22 \times 17.3069 \times 0.2188$ | 275.46 | 496.47 | 0.555 | 0.00 | 496.47 | 0.000 |

## Pole Shear Design Data

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | Ratio $V_{u}$ | Actual $T_{u}$ | $\phi T_{n}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  |  | K | K | $\phi V_{n}$ | kip-ft | kip-ft | $\phi T_{n}$ |
| L1 | 84-34.25 (1) | TP18.145x12.001x0.1875 | 3.55 | 182.72 | 0.019 | 0.67 | 279.94 | 0.002 |
| L2 | 34.25-0 (2) | TP22x17.3069x0.2188 | 5.16 | 265.41 | 0.019 | 0.67 | 506.26 | 0.001 |

## Pole Interaction Design Data

| Section No. | Elevation | Ratio $P_{u}$ | $\begin{aligned} & \text { Ratio } \\ & M_{u x} \end{aligned}$ | $\begin{gathered} \text { Ratio } \\ M_{u y} \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ V_{u} \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \end{gathered}$ | Comb. Stress | Allow. Stress | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft |  | $\phi P_{n}$ | ${ }_{\phi} M_{n \times}$ | ${ }_{\phi} M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ | Ratio | Ratio |  |
| L1 | 84-34.25 (1) | 0.003 | 0.393 | 0.000 | 0.019 | 0.002 | 0.397 | 1.050 | 4.8.2 |
| L2 | 34.25-0 (2) | 0.005 | 0.555 | 0.000 | 0.019 | 0.001 | 0.560 | 1.050 | 4.8.2 |

## Section Capacity Table

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} \varnothing P_{\text {allow }} \\ K \end{gathered}$ | $\%$ <br> Capacity | $\begin{aligned} & \text { Pass } \\ & \text { Fail } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 84-34.25 | Pole | TP18.145x12.001x0.1875 | 1 | -2.07 | 639.52 | 37.8 | Pass |
| L2 | 34.25-0 | Pole | TP22x17.3069x0.2188 | 2 | -4.62 | 928.93 | 53.4 | Pass |
|  |  |  |  |  |  | Pole (L2) RATING = | $\begin{gathered} \text { Summary } \\ 53.4 \\ 53.4 \end{gathered}$ | Pass Pass |

## APPENDIX B

## BASE LEVEL DRAWING



RIDGEFIELD 22N

## APPENDIX C

## ADDITIONAL CALCULATIONS

## Monopole Base Plate Connection



| Analysis Considerations |  |
| ---: | :---: |
| TIA-222 Revision | H |
| Grout Considered: | No |
| $\mathrm{I}_{\mathrm{ar}}(\mathrm{in})$ | 2.125 |


| Applied Loads |  |
| :---: | :---: |
| Moment (kip-ft) | 275.47 |
| Axial Force (kips) |  |
| Shear Force (kips) | 4.62 |

*TIA-222-H Section 15.5 Applied
*TIA-222-H Section 15.5 Applied


## Connection Properties

## Analysis Results

Anchor Rod Data
(6) 1-3/4" $\varnothing$ bolts (A615-75 N; Fy=75 ksi, Fu=100 ksi) on 27.96" BC

Base Plate Data
$32.84^{\prime \prime}$ OD x 2.25" Plate (A572-50; Fy=50 ksi, Fu=65 ksi)

Stiffener Data
N/A

Pole Data
22" x 0.21875" 18-sided pole (A572-65; Fy=65 ksi, Fu=80 ksi)

| Anchor Rod Summary |  | (units of kips, kip-in) |
| :--- | :--- | :---: |
| $\mathrm{Pu} \mathrm{t}=77.93$ | $\phi \mathrm{Pn} \mathrm{t}=142.5$ | Stress Rating |
| $\mathrm{Vu}=0.86$ | $\phi \mathrm{Vn}=90.2$ | $\mathbf{5 2 . 1 \%}$ |
| $\mathrm{Mu}=1.19$ | $\phi \mathrm{Mn}=60.29$ | Pass |
|  |  |  |
| Base Plate Summary |  | (Flexural) |
| Max Stress (ksi): | 10.84 |  |
| Allowable Stress (ksi): | 45 | Pass |
| Stress Rating: | $\mathbf{2 2 . 9 \%}$ |  |

## Pier and Pad Foundation

ES-286
Ridgefield22N
Tower Type:

| $H$ |
| :---: |
| Monopole |


| Top \& Bot. Pad Rein. Different?: | $\boxed{ }$ |
| ---: | :---: |
| Block Foundation?: | $\square$ |
| Rectangular Pad?: | $\square$ |


| Superstructure Analysis Reactions |  |  |  |
| ---: | :---: | :--- | :---: |
| Compression, $\mathbf{P}_{\text {comp }}:$ | 4.62 | kips |  |
| Base Shear, Vu_comp: | 5.15 | kips |  |
|  |  |  |  |
|  |  |  |  |
| Moment, $\mathbf{M}_{\mathbf{u}}:$ | 275.47 | ft -kips |  |
| Tower Height, $\mathbf{H}:$ | 84 | ft |  |
|  |  |  |  |
| BP Dist. Above Fdn, $\mathbf{b p}_{\text {dist }}:$ | 6 | in |  |


| Pier Properties |  |  |  |
| ---: | :---: | :--- | :---: |
| Pier Shape: | Circular |  |  |
| Pier Diameter, dpier: | 4.5 | ft |  |
| Ext. Above Grade, E: | 0.5 | ft |  |
| Pier Rebar Size, Sc: | 9 |  |  |
| Pier Rebar Quantity, mc: | 12 |  |  |
| Pier Tie/Spiral Size, St: | 4 |  |  |
| Pier Tie/Spiral Quantity, mt: | 7 |  |  |
| Pier Reinforcement Type: | Tie |  |  |
| Pier Clear Cover, $\mathbf{c c}$ pier: | 6 | in |  |


| Foundation Analysis Checks |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating $^{*}$ | Check |
|  |  |  |  |  |
| Lateral (Sliding) (kips) | 81.43 | 5.15 | $\mathbf{6 . 0} \%$ | Pass |
| Bearing Pressure (ksf) | 6.00 | 1.71 | $\mathbf{2 8 . 5} \%$ | Pass |
| Overturning (kip*ft) | 648.41 | 308.95 | $\mathbf{4 7 . 6} \%$ | Pass |
| Pier Flexure (Comp.) (kip*t) | 1147.42 | 296.07 | $\mathbf{2 4 . 6 \%}$ | Pass |
|  |  |  |  |  |
| Pier Compression (kip) | 7592.08 | 16.07 | $\mathbf{0 . 2 \%}$ | Pass |
| Pad Flexure (kip*f) | 424.27 | 82.23 | $\mathbf{1 8 . 5} \%$ | Pass |
| Pad Shear - 1-way (kips) | 235.14 | 25.59 | $\mathbf{1 0 . 4 \%}$ | Pass |
| Pad Shear - 2-way (Comp) (ksi) | 0.164 | 0.013 | $\mathbf{7 . 4 \%}$ | Pass |
| Flexural 2-way (Comp) (kip*ft) | 487.12 | 177.64 | $\mathbf{3 4 . 7 \%}$ | Pass |

*Rating per TIA-222-H Section 15.5

| Structural Rating $:$ | $34.7 \%$ |
| ---: | ---: |
| Soil Rating $:$ | $47.6 \%$ |


| Pad Properties |  |  |  |
| ---: | :---: | :---: | :---: |
| Depth, D: | 5.5 | ft |  |
| Pad Width, $\mathbf{W}_{\mathbf{1}}:$ | 12 | ft |  |
| Pad Thickness, T: | 2 | ft |  |
| Pad Rebar Size (Top dir.2), $\mathbf{S p}_{\text {top } 2}:$ | 4 |  |  |
| Pad Rebar Quantity (Top dir. 2), $\mathbf{m p}_{\text {top2 }}:$ | 9 |  |  |
| Pad Rebar Size (Bottom dir. 2), $\mathbf{S p}_{\mathbf{2}}:$ | 6 |  |  |
| Pad Rebar Quantity (Bottom dir. 2), $\mathbf{m p}_{\mathbf{2}}:$ | 11 |  |  |
| Pad Clear Cover, $\mathbf{c c}_{\text {pad }}:$ | 3 | in |  |


| Material Properties |  |  |
| ---: | :---: | :--- |
| Rebar Grade, Fy: | 60 | ksi |
| Concrete Compressive Strength, F'c: | 3 | ksi |
| Dry Concrete Density, $\delta \mathbf{c}:$ | 150 | pcf |


| Soil Properties |  |  |  |  |
| ---: | :---: | :--- | :---: | :---: |
| Total Soil Unit Weight, $\gamma:$ | 125 | pcf |  |  |
| Ultimate Gross Bearing, Qult: | 8.000 | ksf |  |  |
| Cohesion, $\mathbf{C u}:$ |  | ksf |  |  |
| Friction Angle, $\varphi:$ | 34 | degrees |  |  |
| SPT Blow Count, $\mathbf{N}_{\text {blows }}:$ |  |  |  |  |
| Base Friction, $\mu:$ | 0.6 |  |  |  |
| Neglected Depth, $\mathbf{N}:$ | 3.50 | ft |  |  |
| Foundation Bearing on Rock? | No |  |  |  |
| Groundwater Depth, gw: | $\mathrm{N} / \mathrm{A}$ | ft |  |  |

## ATTACHMENT E - PROOF OF DELIVERY OF NOTICE



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## ATTACHMENT F - POWER DENSITY REPORT

# Calculated Radio Frequency Emissions Report EVERS=URCE ENERGY 

ES-286
Off Prospect Street
Ridgefield, CT 06877

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## 1. Introduction

The purpose of this report is to investigate compliance with applicable FCC regulations for the existing Eversource installation located off Prospect Street in Ridgefield, CT.

Eversource has recently installed one omnidirectional antenna for both transmit and receive purposes as part of its 220 MHz communications system. The original proposal consisted of two omnidirectional antennas - separate transmit and receive antennas. This report provides an updated analysis based on the current installation as reflected in the update site plans ${ }^{1}$.

This report considers the existing antenna configuration as provided by Eversource along with power density information of the other existing antennas to calculate the overall \% MPE (Maximum Permissible Exposure) of the facility at ground level.

## 2. FCC Guidelines for Evaluating RF Radiation Exposure Limits

In 1985, the FCC established rules to regulate radio frequency (RF) exposure from FCC licensed antenna facilities. In 1996, the FCC updated these rules, which were further amended in August 1997 by OET Bulletin 65 Edition 97-01. These new rules include Maximum Permissible Exposure (MPE) limits for transmitters operating between 300 kHz and 100 GHz . The FCC MPE limits are based upon those recommended by the National Council on Radiation Protection and Measurements (NCRP), developed by the Institute of Electrical and Electronics Engineers, Inc., (IEEE) and adopted by the American National Standards Institute (ANSI).

The FCC general population/uncontrolled limits set the maximum exposure to which most people may be subjected. General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

Public exposure to radio frequencies is regulated and enforced in units of milliwatts per square centimeter ( $\mathrm{mW} / \mathrm{cm}^{2}$ ). The general population exposure limits for the various frequency ranges are defined in the attached "FCC Limits for Maximum Permissible Exposure (MPE)" in Attachment B of this report.

Higher exposure limits are permitted under the occupational/controlled exposure category, but only for persons who are exposed as a consequence of their employment and who have been made fully aware of the potential for exposure, and they must be able to exercise control over their exposure. General population/uncontrolled limits are five times more stringent than the levels that are acceptable for occupational, or radio frequency trained individuals. Attachment B contains excerpts from OET Bulletin 65 and defines the Maximum Exposure Limit.

Finally, it should be noted that the MPE limits adopted by the FCC for both general population/uncontrolled exposure and for occupational/controlled exposure incorporate a substantial margin of safety and have been established to be well below levels generally accepted as having the potential to cause adverse health effects.

[^3]
## 3. Power Density Calculation Methods

The power density calculation results were generated using the following formula as outlined in FCC bulletin OET 65, and Connecticut Siting Council recommendations:

$$
\text { Power Density }=\left(\frac{1.6^{2} \times 1.64 \times \mathrm{ERP}}{4 \pi \times R^{2}}\right) X \text { Off Beam Loss }
$$

Where:
EIRP $=$ Effective Isotropic Radiated Power $=1.64 \times$ ERP
$\mathrm{R}=$ Radial Distance $=\sqrt{\left(H^{2}+V^{2}\right)}$
$\mathrm{H}=$ Horizontal Distance from antenna
$\mathrm{V}=$ Vertical Distance from radiation center of antenna
Ground reflection factor of 1.6
Off Beam Loss is determined by the selected antenna pattern

These calculations assume that the antennas are operating at 100 percent capacity and full power, and that all antenna channels are transmitting simultaneously. Obstructions (trees, buildings, etc.) that would normally attenuate the signal are not taken into account. The calculations assume even terrain in the area of study and do not consider actual terrain elevations which could attenuate the signal. As a result, the calculated power density and corresponding $\%$ MPE levels reported below are much higher than the actual levels will be from the final installation.

## 4. Calculated \% MPE Results

Table 1 below outlines the power density information for the site. The new Eversource omnidirectional antenna has a vertical beamwidth of $60^{\circ}$; therefore, the majority of the RF power is focused out towards the horizon. Please refer to Attachment C for the vertical pattern of the recently installed 220 MHz Eversource antenna. Likewise, the other transmit antennas exhibit similar directionality of varying vertical beamwidths. As a result, there will be less RF power directed below the antennas relative to the horizon, and consequently lower power density levels around the base of the facility. The calculated results in Table 1 include a nominal 10 dB off-beam pattern loss to account for the lower relative gain below the antennas. Any inactive or receive-only antennas are not listed in the table, as they are irrelevant in terms of the \% MPE calculations.

| Carrier | Antenna Height <br> (Feet) | Operating <br> Frequency (MHz) | Number of <br> Trans. | ERP Per Transmitter <br> (Watts) | Power Density <br> $\left(\mathbf{m w} / \mathbf{c m}^{2}\right)$ | Limit | \%MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CL\&P | 85 | 37.74 | 1 | 100 | 0.0006 | 0.2000 | $0.29 \%$ |
| CL\&P | 70 | 44 | 1 | 100 | 0.0009 | 0.2000 | $0.44 \%$ |
| CL\&P | 70 | 48 | 1 | 100 | 0.0009 | 0.2000 | $0.44 \%$ |
| CL\&P | 85 | 450 | 1 | 251 | 0.0014 | 0.3000 | $0.48 \%$ |
| CL\&P | 85 | 937 | 2 | 240 | 100 | 0.0028 | 0.6247 |
| Eversource | 90 | 44.34 | 1 | 240 | $0.44 \%$ |  |  |
| Eversource | 88 | 936.6375 | 1 | 240 | 0.0005 | 0.2000 | $0.25 \%$ |
| Eversource | 88 | 938.45 | 1 | 100 | 0.0013 | 0.6244 | $0.21 \%$ |
| Eversource | 74 | 37.74 | 1 | 10013 | 0.6256 | $0.21 \%$ |  |
| Eversource | 74 | 451.675 | 1 | 124 | 0.0008 | 0.2000 | $0.39 \%$ |
| Eversource | 73 | 217 | 4 |  | 0.0020 | 0.3011 | $0.65 \%$ |
| Eversource | 95.3 |  |  | 0.0008 | 0.2000 | $0.40 \%$ |  |

Table 1: Proposed Facility \% MPE ${ }^{23}$

The CT Siting Council power density database reflects entries for pre-existing Eversource (f.k.a. CL\&P) antennas. These entries are shown as grey in the table above and should be replaced by the unshaded entries, which are based upon updated operating parameters provided by Eversource as part of this project. The blue entry reflects the parameters of the recently installed Eversource antenna. Therefore, the total \% MPE calculated is based upon only the unshaded and blue entries.

[^4]${ }^{3}$ The antenna heights listed for Eversource are in reference to the Black \& Veatch Structural Analysis Report dated 07/29/2021.

## 5. Conclusion

The above analysis concludes that RF exposure at ground level with the new Eversource 220 MHz antenna installation will be below the maximum power density limits as outlined by the FCC in the OET Bulletin 65 Ed. 97-01. Using the conservative calculation methods discussed herein, the highest expected percent of Maximum Permissible Exposure at ground level from the existing installation is $\mathbf{3 . 2 2 \%}$ of the FCC General Population/Uncontrolled limit.

As noted previously, the calculated \% MPE levels are more conservative (higher) than the actual measured levels will be from the installation.

## 6. Statement of Certification

I certify to the best of my knowledge that the statements in this report are true and accurate. The calculations follow guidelines set forth in FCC OET Bulletin 65 Edition 97-01, IEEE Std. C95.1, and IEEE Std. C95.3.

## Kerth cellante

Report Prepared By: Keith Vellante
Director - RF Services
C Squared Systems, LLC

## Attachment A: References

OET Bulletin 65 - Edition 97-01 - August 1997 Federal Communications Commission Office of Engineering \& Technology
IEEE C95.1-2005, IEEE Standard Safety Levels With Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz IEEE-SA Standards Board

IEEE C95.3-2002 (R2008), IEEE Recommended Practice for Measurements and Computations of Radio Frequency Electromagnetic Fields With Respect to Human Exposure to Such Fields, $100 \mathrm{kHz}-300 \mathrm{GHz}$ IEEE-SA Standards Board

## Attachment B: FCC Limits for Maximum Permissible Exposure (MPE)

(A) Limits for Occupational/Controlled Exposure ${ }^{4}$

| Frequency <br> Range <br> $(\mathrm{MHz})$ | Electric Field <br> Strength $(\mathrm{E})$ <br> $(\mathrm{V} / \mathrm{m})$ | Magnetic Field <br> Strength $(\mathrm{E})$ <br> $(\mathrm{A} / \mathrm{m})$ | Power Density $(\mathrm{S})$ <br> $\left(\mathrm{mW} / \mathrm{cm}^{2}\right)$ | Averaging Time <br> $\|\mathrm{E}\|^{2},\|\mathrm{H}\|^{2}$ or S (minutes) |
| :---: | :---: | :---: | :---: | :---: |
| $0.3-3.0$ | 614 | 1.63 | $(100)^{*}$ | 6 |
| $3.0-30$ | $1842 / \mathrm{f}$ | $4.89 / \mathrm{f}$ | $\left(900 / \mathrm{f}^{2}\right)^{*}$ | 6 |
| $30-300$ | 61.4 | 0.163 | 1.0 | 6 |
| $300-1500$ | - | - | $\mathrm{f} / 300$ | 6 |
| $1500-100,000$ | - | - | 5 | 6 |

(B) Limits for General Population/Uncontrolled Exposure ${ }^{5}$

| Frequency <br> Range <br> $(\mathrm{MHz})$ | Electric Field <br> Strength (E) <br> $(\mathrm{V} / \mathrm{m})$ | Magnetic Field <br> Strength (E) <br> $(\mathrm{A} / \mathrm{m})$ | Power Density $(\mathrm{S})$ <br> $\left(\mathrm{mW} / \mathrm{cm}^{2}\right)$ | Averaging Time <br> $\|\mathrm{E}\|^{2},\|\mathrm{H}\|^{2}$ or S (minutes) |
| :---: | :---: | :---: | :---: | :---: |
| $0.3-1.34$ | 614 | 1.63 | $(100)^{*}$ | 30 |
| $1.34-30$ | $824 / \mathrm{f}$ | $2.19 / \mathrm{f}$ | $\left(180 / \mathrm{f}^{2}\right)^{*}$ | 30 |
| $30-300$ | 27.5 | 0.073 | 0.2 | 30 |
| $300-1500$ | - | - | $\mathrm{f} / 1500$ | 1.0 |
| $1500-100,000$ | - | - |  | 30 |
|  |  |  |  |  |
| $\mathrm{f}=$ frequency in $\mathrm{MHz} *$ Plane-wave equivalent power density |  |  |  |  |

Table 2: FCC Limits for Maximum Permissible Exposure (MPE)

[^5]

Figure 1: Graph of FCC Limits for Maximum Permissible Exposure (MPE)

Attachment C: Eversource Antenna Data Sheets and Electrical Patterns

| 217 MHz |  |
| ---: | :--- |
| Manufacturer: | dbSpectra |
| Model \#: | SP2D00P36D-D |
| Frequency Band: | $217-220 \mathrm{MHz}$ |
| Gain: | 0 dBd |
| Vertical Beamwidth: | $60^{\circ}$ |
| Horizontal Beamwidth: | $360^{\circ}$ |
| Polarization: | Vertical |
| Length: | $15.6^{\circ}$ |


[^0]:    ${ }^{1}$ It should be noted that the number of transmitting antennas accounted for in the Power Density Report accounts for two channels on the 88 ' centerline antenna. Also, the "Antenna Height" column on Table 1 in the Power Density Report reflects the centerline of the Transmit or "TX" antenna centerline.

[^1]:    *Von Mises SR = (Max Von Mises Value From RISA-3D)/(0.9*Fy)

[^2]:    Consider Moments - Legs
    Consider Moments - Horizontals
    Consider Moments - Diagonals Use Moment Magnification
    $\checkmark$ Use Code Stress Ratios
    $\checkmark$ Use Code Safety Factors - Guys Escalate Ice
    Always Use Max Kz
    Use Special Wind Profile
    Include Bolts In Member Capacity
    Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided)
    SR Members Have Cut Ends
    SR Members Are Concentric

[^3]:    ${ }^{1}$ Stamped Black \& Veatch site drawings dated 8/13/2021 (Rev. 1).

[^4]:    ${ }^{2}$ Please note that $\%$ MPE values listed are rounded to two decimal points and the total $\%$ MPE listed is a summation of each unrounded contribution. Therefore, summing each rounded value may not identically match the total value reflected in the table.

[^5]:    ${ }^{4}$ Occupational/controlled limits apply in situations in which persons are exposed as a consequence of their employment provided those persons are fully aware of the potential for exposure and can exercise control over their exposure. Limits for occupational/controlled exposure also apply in situations when an individual is transient through a location where occupational/controlled limits apply provided he or she is made aware of the potential for exposure
    ${ }^{5}$ General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure

