

# STATE OF CONNECTICUT CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051 Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov Web Site: portal.ct.gov/csc

#### VIA ELECTRONIC MAIL

February 21, 2024

Kenneth C. Baldwin, Esq. Robinson & Cole 280 Trumbull Street Hartford, CT 06103-3597 kbaldwin@rc.com

RE: SUBPETITION NO. 1133-VER-20230614 - Cellco Partnership d/b/a Verizon Wireless eligible facility request for modification to an existing telecommunications facility located at 97 High Street, Portland, Connecticut. Request for Project Changes.

Dear Attorney Baldwin:

The Connecticut Siting Council (Council) is in receipt of your correspondence dated February 21, 2024, regarding a change to the above-referenced Eligible Facility Request (EFR) that was approved by the Council on July 17, 2023.

Pursuant to Condition No. 1 of the Council's July 17, 2023 approval, your request to install antenna models MT6413-77A and RT4423 in lieu of MT6407-77A and CBRS; and remote radio head model RF4461-13A in lieu of model RF4440d-13A is hereby approved.

This approval applies only to the project changes described in your February 21, 2024 correspondence.

Please be advised that deviations from the standards established by the Council in the EFR approval are enforceable under the provisions of Connecticut General Statutes §16-50u.

Thank you for your attention and cooperation.

Sincerely,

Melanie A. Bachman Executive Director

Malin Mal

MAB/IN/dll

c: The Honorable Ryan J. Curley, First Selectperson, Town of Portland (rcurley@portlandct.org)

# Robinson+Cole

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts and New York

February 21, 2024

Melanie A. Bachman, Esq. Executive Director/Staff Attorney Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Re: SUBPETITION NO. 1133-VER-20230614 – Cellco Partnership d/b/a Verizon Wireless eligible facility request for modification to an existing telecommunications facility at 97 High Street, Portland, Connecticut

**Minor Equipment Changes** 

Dear Attorney Bachman:

On behalf of Cellco Partnership d/b/a Verizon Wireless ("Cellco"), and pursuant to Conditions No. 1 of the Siting Council's decision in SUBPETITION NO. 1133-VER-20230614, I respectfully request staff approval of the following minor equipment changes at the SRR Towers, Inc. wireless facility at 97 High Street in Portland, Connecticut.

Due to equipment availability issues, Cellco will install antenna models MT6413-77A and RT4423<sup>1</sup> in lieu of models MT6407-77A and CBRS. Cellco will also be installing remote radio head (RRH) model RF4461-13A in lieu of model RF4440d-13A.

Attached is a revised set of project plans, specifications for the new antennas and RRHs, and an updated Structural Analysis Report and Antenna Mount Analysis Report confirming that the new tower and mounts are capable of supporting this new equipment. Please contact me if you have any questions or need any additional information.

28903305-v1

<sup>&</sup>lt;sup>1</sup> The RT4423 antenna includes a built-in RRH, which will replace RRH model RT4401-48A as originally approved.

# Robinson+Cole

Melanie A. Bachman, Esq. February 21, 2024 Page 2

Sincerely,

Kenneth C. Baldwin

Copy to:

SRR Towers, Inc. Ryan Curley, Portland First Selectman Tim Parks Michael Humphreys



Structural Components, LLC 1870 West 64<sup>th</sup> Lane, Unit A Denver, CO 80221 Voice: 866-386-7622

February 13, 2024

BST Management, LLC 352 Park Street Suite 106 North Reading, MA 01864

Re:

Comprehensive Structural Analysis Report

Structure:

80.4ft Self-Supporting Tower with 10ft Extension

Site Address:

97 High Street, Portland, Connecticut 06480 (Middlesex County)

Latitude: 41.5807°N, Longitude: 72.6238°W

Site Name:

BST Management, LLC – Portland Verizon – Portland

Site Number:

BST Management, LLC - CT-1680

Verizon - 469381

SC Number:

240022 REV 1

Status:

Structure Passes (77% Capacity)

Foundation Passes

Per your request, Structural Components, LLC has completed a structural analysis for the above referenced project to

verify the tower's compliance to the following design criteria:

	TIA-222-H			
Standard:	Structural Standard for Antenna Supporting Structures and Antennas			
Building Code:	2021 International Building Code w/Amendments 2022 Connecticut State Building Code			
Design Basic Wind Speed without Ice:	120 mph 3-second gust Vult			
Design Basic Wind Speed with Ice:	50 mph 3-second gust			
Ice Thickness:	1" radial			
Serviceability Basic Wind Speed:	60 mph 3-second gust			
Exposure Category:	С			
Topographic Category:	1			
Ground Elevation:	345ft			
Risk Category:				
Seismic Site Class:	D, S <sub>s</sub> =0.208, S <sub>1</sub> =0.056			
Seismic Design Category:	В			

Please refer to the following structural analysis report, which gives complete details of the tower loading, results, information provided, and necessary assumptions.

We trust you find this report satisfactory. Please do not hesitate to contact us if you should have any questions or concerns.

Best Regards, Structural Components LLC

Wesley Culver Engineering Manager

/TR



Michael Deboer, P.E. Connecticut P.E. # 0018022

#### 1 LOADING CONFIGURATION

The following antennas, mounts, transmission lines, and other appurtenances were considered for the structural analysis.

Elevation (ft)		Elevation (ft)				
Mount	Equipment Equipment		Feedlines	Notes		
90.5	90.5	(1) 5/8" x 6' Lightning Rod	-	Existing		
90.0	90.0	(3) CommScope NNH4-65B-R6 Panels (3) Samsung RT4423 Panels w/ RRU (3) Samsung MT6413-77A Panels (3) Samsung RF4439d-25A RRUs <sup>(3)</sup> (3) Samsung RF4461d-13A RRUs <sup>(3)</sup> (1) CommScope FE-16148-OVP-B12 TMA (3) SitePro VFA12-HD Sector Frame Mounts (3) Tiebacks	(2) 6x12 Hybrid	Verizon Final		
77.0	77.0	(1) L6" x 6" x 7/16" Ring Mount	6" Ring Mount			
78.7 77.2 76.7 <sup>(4)</sup>	78.7 (3) (1)					
	77.2	(3) Ericsson RRUS 32 B30 <sup>(3)</sup> (3) Ericsson RRUS 32 B66A <sup>(3)</sup> (1) Raycap DC6-48-60-18-8F SSD	(6) 7/8" TX			
	76.7 <sup>(4)</sup>	<ul> <li>(3) CCITPA65R-BU6DA-K Panels</li> <li>(3) Ericsson AIR6449 B77D Panels</li> <li>(3) Ericsson AIR6419 B77G Panels</li> <li>(3) CCIDMP65R-BU6DA Panels</li> <li>(3) Ericsson RRUS 4478 B14</li> <li>(3) Ericsson RRUS 4449 B5/B12</li> <li>(1) Raycap DC9-48-60-24-8C-EV SSDs</li> <li>(3) 12' Sector Frame Mounts</li> </ul>	(3) 0.92" OD DC (4) 3/4" OD DC (1) 3/8" Fiber (1) 1/2" Fiber	AT&T Final		
75.0	75.0	(1) L6" x 6" x 7/16" Ring Mount				
73.0	73.0	(1) 2-3/8" x 8' Pipe Mount		Existing		
67.7	67.7	(1) L6" x 6" x 7/16" Ring Mount				

- Elevations reference centerline of panel, yagi, mounts, and dish antennas, and base of whip antennas, in relation to the base of the tower.
- 2) Refer to the feed line diagram and analysis output in Appendix A for the location and orientation of feedlines and equipment.
- 3) Secondary appurtenances such as TMAs, Diplexers, and RRUs are considered to be installed directly behind panel antennas for frontal area shielding. See analysis output for magnitude of individual shielding.
- 4) Elevations adjusted from Structural Components Mapping dated 03/15/2022, Job # 220142.

#### 2 RESULTS

The analysis was performed using tnxTower v8.1.1.0, a structural analysis program developed by Tower Numerics, Inc. specifically for the communication tower industry.

#### 2.1 TOWER MEMBER STRESS LEVELS

The tower has the following stress ratios in its structural members.

Elev. (ft)	Member	Stress Ratio*
0 - 90.4	Legs	0.77
0 - 90.4	Bracing	0.63
0 - 90.4	Connections	0.63

Stress ratio (SR) criteria:

 $SR \le 1.00$  is completely within code limits.

SR < 1.05 is considered within acceptable tolerance of code limits.

SR > 1.05 is outside acceptable tolerance of code limits and requires structural modifications.

#### 2.2 FOUNDATION REACTIONS

The reactions listed below are for the design wind speed listed. Reactions are factored loads.

Reaction Type	Current Wind Reactions	Current leed Reactions	Foundation Status
Moment (ft-kips)	1,237.5	310.2	
Shear (kips)	22.4	5.5	
Axial (kips)	21.8	43.7	Passes*
Leg Compression (kips)	72.4	_	F 03505
Leg Uplift (kips)	62.8	-	
Leg Shear (kips)	10.8		· 

<sup>\*</sup> See Appendix A for foundation calculations.

#### 2.3 TOWER DEFLECTION

The tower deflections have been reviewed and are believed to be acceptable for the proposed equipment. The carrier(s) should review the deflections for the service wind condition included in Appendix A for compatibility with their equipment.

<sup>\*</sup> Seismic analysis for similar structures under similar loading conditions has been shown to produce significantly lower stress ratios than wind and ice. Therefore, seismic analysis has not been included in the current analysis.

#### 3 PROVIDED INFORMATION AND ASSUMPTIONS

The following information was directly used to generate this report, and can be found in Appendix B.

Document	Author	Date	Reference	
Collocation Application	Verizon	11/21/2023	CT-1680	
RFDS	Verizon	09/27/2023	Portland HS CT	
Mount Analysis	Centek Engineering	11/09/2023	22017.06 REV1	
Construction Drawings	Centek Engineering	02/12/2024	22017.06	
Structural Analysis Report – Verizon	Structural Components, LLC	01/23/2024	240022	
Post Modification Inspection Report	Structural Components, LLC	09/19/2023	230193	

The following assumptions were made in order to complete the analysis. These assumptions must be checked. If they do not accurately represent the existing or proposed tower, foundation, soil, and loading conditions, we must be notified so that we can make the appropriate changes to our analysis, conclusions, and recommendations.

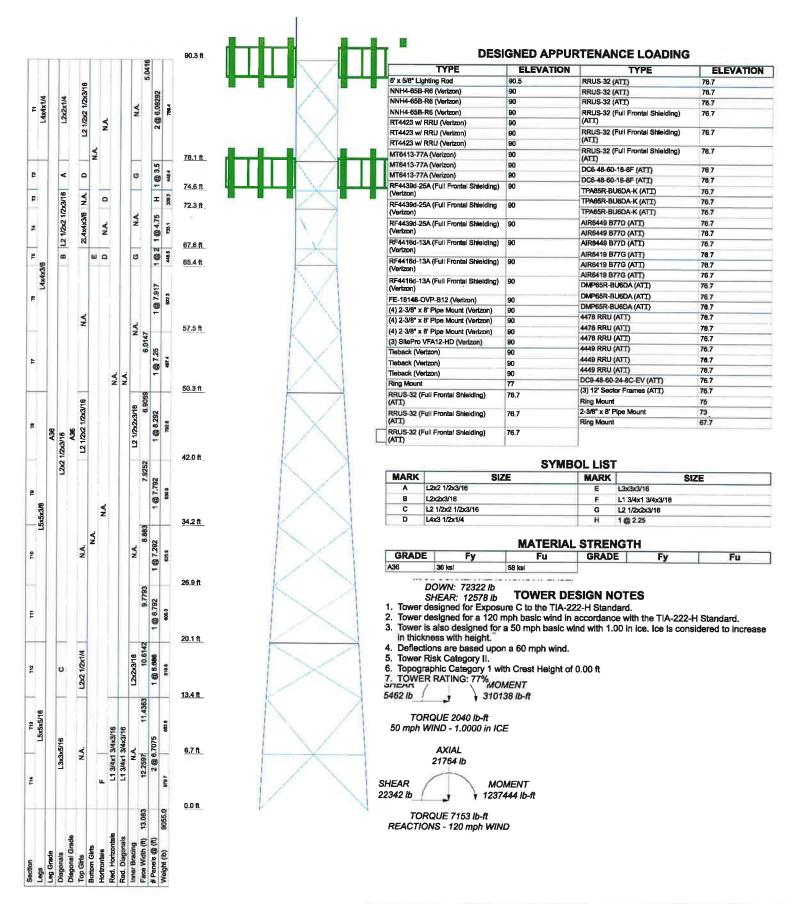
- The tower and foundation are in good condition with no corrosion, damage or fatiguing issues which could reduce the carrying capacity of the tower.
- 2. All welds and connections are assumed to develop at least the member capacity, unless determined otherwise and explicitly stated in this report.
- 3. All prior structural modifications, if any, are assumed to be as per date supplied/ available, to be properly installed and to be fully effective.
- 4. The following assumptions regarding member minimum material or type apply to this structure, unless otherwise noted in analysis:
  - o Angle Legs: A36
- Angle Bracing: A36
- o Splice Bolts: A307
- Gusset Plates: A36 o Brace Bolts: A325N
- 5. The feedline and appurtenance configuration is as stated in the report. All antennas, coax, cables and waveguide cables are assumed to be properly installed and supported as per manufacturer requirement.
- 6. The support mounts and/or platforms are not analyzed and are considered adequate to support the loading.
- 7. All mounting systems connect at tower bracing points. Local stresses are not considered unless noted otherwise in analysis.
- 8. Some assumptions are made regarding antenna and mount sizes and their projected areas based on a best interpretation of the data supplied and a best knowledge of antenna type and industry practice.
- 9. The soil parameters are as per data supplied, or as assumed, and stated in the calculations.

#### 4 CONCLUSIONS

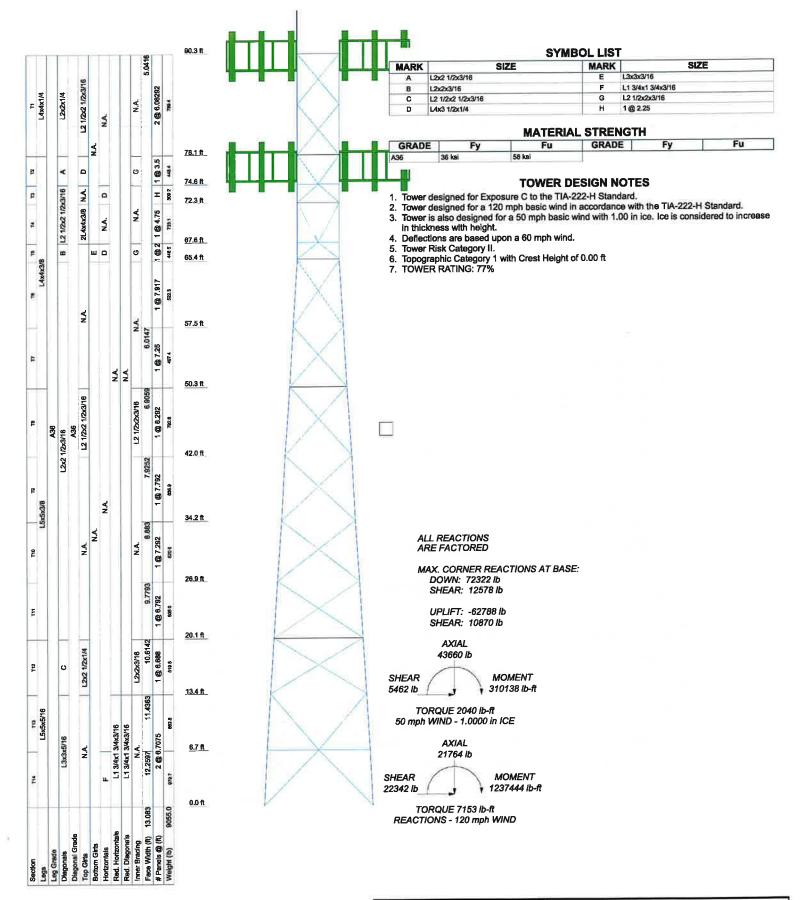
To the best of our knowledge and belief the tower and foundations satisfy the requirements of the applicable codes and standards having jurisdiction over the work for the loadings and conditions as outlined in this report. **Structural modifications are not required at this time.** 

#### **APPENDIX A**

**Tower Profile and Calculations** 



Structural Components, LLC	ob: 240022 REV 1		
	Project: Portland (CT-1680)		
	Client: BST Management, LLC	Drawn by: treed	App'd:
	Code: TIA-222-H	Date: 02/13/24	Scale: NTS
FAX:	Path:		Dwg No. E-1



Structural Components, LLC	ob: 240022 REV 1		
1870 West 64th Lane, Unit A	Project Portland (CT-1680)		
Denver, CO 80221	Client: BST Management, LLC	Drawn by: treed	App'd:
	Code: TIA-222-H	Date: 02/13/24	Scale: NTS
FAX:	Path:		Dwg No. E-1

Structural Components, LLC 1870 West 64th Lane, Unit A

> Denver, CO 80221 Phone: (866) 386-7622 FAX:

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Portland (CT-1680)	15:03:20 02/13/24
BST Management, LLC	Designed by treed

#### **Tower Input Data**

The main tower is a 4x free standing tower with an overall height of 90.33 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 5.04 ft at the top and 13.08 ft at the base.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower base elevation above sea level: 345.00 ft.

Basic wind speed of 120 mph.

Risk Category II.

Exposure Category C.

Simplified Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Category: 1.

Crest Height: 0.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

#### **Options**

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- √ Use Code Stress Ratios
- √ Use Code Safety Factors Guys Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section
- √ Secondary Horizontal Braces Leg
  Use Diamond Inner Bracing (4 Sided)
  SR Members Have Cut Ends
  SR Members Are Concentric
- Distribute Leg Loads As Uniform Assume Legs Pinned Assume Rigid Index Plate
- ✓ Use Clear Spans For Wind Area
   ✓ Use Clear Spans For KL/r
- Retension Guys To Initial Tension Bypass Mast Stability Checks
- √ Use Azimuth Dish Coefficients
- √ Project Wind Area of Appurt, Autocalc Torque Arm Areas Add IBC .6D+W Combination
- √ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

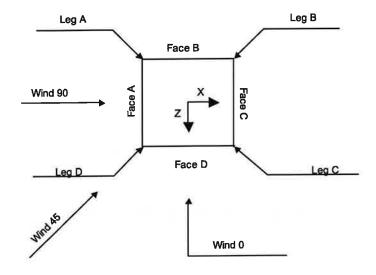
- Use ASCE 10 X-Brace Ly Rules
- √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA
- √ SR Leg Bolts Resist Compression
  All Leg Panels Have Same Allowable
  Offset Girt At Foundation
- Consider Feed Line Torque
- √ Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption Poles

Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

Structural Components, LLC 1870 West 64th Lane, Unit A

Denver, CO 80221 Phone: (866) 386-7622 FAX:

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Square Tower

<b>Tower Section Geomet</b>	rv
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Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of	Section Length
500000					Sections	
	ft			ft		ft
T1	90.33-78.06			5.04	1	12.27
T2	78.06-74.56			5.04	1	3.50
T3	74.56-72.31			5.04	1	2.25
T4	72.31-67.56			5.04	1	4.75
T5	67.56-65.44			5.04	1	2.13
T6	65.44-57.52			5.04	1	7.92
T7	57.52-50.27			6.01	1	7.25
T8	50,27-41.98			6.91	1	8.29
T9	41.98-34.19			7.93	1	7.79
T10	34.19-26.90			8.88	1	7.29
T11	26.90-20.10			9.78	1	6.79
T12	20.10-13.42			10.61	1	6.69
T13	13.42-6.71			11.44	1	6.71
T14	6.71-0.00			12.26	1	6.71

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End	Has Horizontals	Top Girt Offset	Bottom Gir Offset
	ft	ft		Panels		in	in
T1	90.33-78.06	6.08	X Brace	No	Yes	1.2500	0.0000
T2	78.06-74.56	3.50	K Brace Up	No	Yes	0.0000	0.0000
T3	74.56-72.31	2.25	K Brace Down	No	Yes	0.0000	0.0000
T4	72.31-67.56	4.75	K Brace Up	No	Yes	0.0000	0.0000
T5	67.56-65.44	2.00	K Brace Down	No	Yes	0.0000	1.5000

Structural Components, LLC 1870 West 64th Lane, Unit A Denver, CO 80221 Phone: (866) 386-7622 FAX:

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Tower	Tower	Diagonal	Bracing	Has	Has	Top Girt	Bottom Girt
Section	Elevation	Spacing	Type	K Brace	Horizontals	Ôffset	Offset
				End		20	-20
	ft	ft		Panels		in	in
T6	65.44-57.52	7.92	X Brace	No	No	0.0000	0.0000
T7	57.52-50.27	7.25	X Brace	No	No	0.0000	0.0000
T8	50.27-41.98	8.29	X Brace	No	No	0.0000	0.0000
Т9	41.98-34.19	7.79	X Brace	No	No	0.0000	0.0000
T10	34.19-26.90	7.29	X Brace	No	No	0.0000	0.0000
T11	26.90-20.10	6.79	X Brace	No	No	0.0000	0.0000
T12	20.10-13.42	6.69	X Brace	No	No	0.0000	0.0000
T13	13.42-6.71	6.71	K1 Up	No	Yes	0.0000	0.0000
T14	6.71-0.00	6.71	K1 Down	No	Yes	0.0000	0.0000

# Tower Section Geometry (cont'd)

Tower Elevation	Leg	Leg	Leg	Diagonal	Diagonal	Diagonal
ft	Туре	Size	Grade	Туре	Size	Grade
T1 90.33-78.06	Equal Angle	L4x4x1/4	A36	Equal Angle	L2x2x1/4	A36
			(36 ksi)			(36 ksi)
T2 78.06-74.56	Equal Angle	L4x4x3/8	A36	Single Angle	L2x2 1/2x3/16	`A36
			(36 ksi)			(36 ksi)
T3 74.56-72.31	Equal Angle	L4x4x3/8	A36	Equal Angle	L2 1/2x2 1/2x3/16	`A36 ´
			(36 ksi)			(36 ksi)
T4 72.31-67.56	Equal Angle	L4x4x3/8	A36	Equal Angle	L2 1/2x2 1/2x3/16	`A36 ´
			(36 ksi)			(36 ksi)
T5 67.56-65.44	Equal Angle	L4x4x3/8	A36	Equal Angle	L2x2x3/16	`A36 ´
			(36 ksi)			(36 ksi)
T6 65.44-57.52	Equal Angle	L4x4x3/8	A36	Single Angle	L2x2 1/2x3/16	`A36´
			(36 ksi)	- •		(36 ksi)
T7 57.52-50.27	Equal Angle	L4x4x3/8	A36	Single Angle	L2x2 1/2x3/16	`A36 ´
			(36 ksi)			(36 ksi)
T8 50.27-41.98	Equal Angle	L5x5x3/8	A36	Single Angle	L2x2 1/2x3/16	`A36 ´
			(36 ksi)			(36 ksi)
T9 41.98-34.19	Equal Angle	L5x5x3/8	A36	Single Angle	L2x2 1/2x3/16	`A36 ´
			(36 ksi)			(36 ksi)
T10 34.19-26.90	Equal Angle	L5x5x3/8	A36	Single Angle	L2x2 1/2x3/16	`A36´
			(36 ksi)	•		(36 ksi)
T11 26.90-20.10	Equal Angle	L5x5x3/8	A36	Single Angle	L2x2 1/2x3/16	`A36´
			(36 ksi)			(36 ksi)
T12 20.10-13.42	Equal Angle	L5x5x5/16	`A36	Single Angle	L2 1/2x2 1/2x3/16	A36
			(36 ksi)			(36 ksi)
T13 13.42-6.71	Equal Angle	L5x5x5/16	`A36 ´	Equal Angle	L3x3x5/16	A36
			(36 ksi)	- 0		(36 ksi)
T14 6.71-0.00	Equal Angle	L5x5x5/16	A36	Equal Angle	L3x3x5/16	A36
			(36 ksi)			(36 ksi)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 90.33-78.06	Equal Angle	L2 1/2x2 1/2x3/16	A36	Solid Round		A36
			(36 ksi)			(36 ksi)
T2 78.06-74.56	Single Angle	L4x3 1/2x1/4	A36	Solid Round		A36

Structural Components, LLC 1870 West 64th Lane, Unit A

Denver, CO 80221
Phone: (866) 386-7622
FAX:

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Client	BST Management, LLC	Designed by treed

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
			(36 ksi)			(36 ksi)
T4 72.31-67.56	Double Equal	2L4x4x3/8	A36	Solid Round		A36
1- /2.51-07.50	Angle		(36 ksi)			(36 ksi)
T5 67.56-65.44	Single Angle		`A36´	Equal Angle	L3x3x3/16	A36
15 07.50-05.11	pmgre rmgre		(36 ksi)			(36 ksi)
T8 50.27-41.98	Equal Angle	L2 1/2x2 1/2x3/16	A36	Solid Round		A36
16 30.21-41.96	rdan mere		(36 ksi)			(36 ksi)
Г12 20.10-13.42	Single Angle	L2x2 1/2x1/4	A36	Solid Round		A36
112 20.10-13.72	Single Angle	LINE I, IN.	(36 ksi)			(36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation	No. of Mid	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
ft	Girts						
T2 78.06-74.56	None	Flat Bar		A36 (36 ksi)	Single Angle	L4x3 1/2x1/4	A36 (36 ksi)
T3 74.56-72.31	None	Flat Bar		A36 (36 ksi)	Single Angle	L4x3 1/2x1/4	A36 (36 ksi)
T4 72.31-67.56	None	Flat Bar		A36 (36 ksi)	Single Angle	L4x3 1/2x1/4	A36 (36 ksi)
T5 67.56-65.44	None	Flat Bar		A36 (36 ksi)	Single Angle	L4x3 1/2x1/4	A36 (36 ksi)
T13 13.42-6.71	None	Flat Bar		A36 (36 ksi)	Equal Angle	L1 3/4x1 3/4x3/16	A36 (36 ksi)
T14 6.71-0.00	None	Flat Bar		A36 (36 ksi)	Equal Angle	L1 3/4x1 3/4x3/16	A36 (36 ksi)

Tower Elevation	Secondary Horizontal Type	Secondary Horizontal Size	Secondary Horizontal Grade	Inner Bracing Type	Inner Bracing Size	Inner Bracing Grade
ft						
T2 78.06-74.56	Solid Round		A36 (36 ksi)	Single Angle	L2 1/2x2x3/16	A36 (36 ksi)
T3 74.56-72.31	Solid Round		A36 (36 ksi)	Single Angle	L2 1/2x2x3/16	A36 (36 ksi)
T5 67.56-65.44	Solid Round		A36 (36 ksi)	Single Angle	L2 1/2x2x3/16	A36 (36 <b>k</b> si)
T6 65.44-57.52	Solid Round		A36 (36 ksi)	Equal Angle	L1 3/4x1 3/4x3/16	A36 (36 ksi)
T8 50.27-41.98	Solid Round		A36 (36 ksi)	Single Angle	L2 1/2x2x3/16	A36 (36 ksi)
T12 20.10-13.42	Solid Round		A36 (36 ksi)	Equal Angle	L2x2x3/16	A36 (36 ksi)

Structural Components, LLC 1870 West 64th Lane, Unit A Denver, CO 80221

Denver, CO 80221 Phone: (866) 386-7622 FAX:

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	BST Management, LLC	treed

### Tower Section Geometry (cont'd)

Tower Elevation	Redundant Bracing Grade		Redundant Type	Redundant Size	K Factor
T13	A36	Horizontal (1)	Equal Angle	L1 3/4x1 3/4x3/16	1
13.42-6.71	(36 ksi)	Diagonal (1)	Equal Angle	L1 3/4x1 3/4x3/16	1
Γ14 6.71-0.00	A36	Horizontal (1)	Equal Angle	L1 3/4x1 3/4x3/16	1
	(36 ksi)	Diagonal (1)	Equal Angle	L1 3/4x1 3/4x3/16	1

#### **Tower Section Geometry** (cont'd)

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A,	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals	Double Angle Stitch Bolt Spacing Redundants
ft	ft²	in					in	in	in
T1 90.33-78.06	0.00	0.2500	A36 (36 ksi)	1	1	81	36.0000	36.0000	36.0000
T2 78.06-74.56	0.35	0.2500	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T3 74.56-72.31	0.35	0.2500	A36 (36 ksi)	1	1		36.0000	36.0000	36.0000
T4 72.31-67.56	0.58	0.2500	`A36 ´ (36 ksi)	1	1	1	36.0000	Third-Pt	36.0000
T5 67.56-65.44	0.58	0.2500	`A36 ´ (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T6 65.44-57.52	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T7 57.52-50.27	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T8 50.27-41.98	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T9 41.98-34.19	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T10 34.19-26.90	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T11 26.90-20.10	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T12 20.10-13.42	0.00	0.3125	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T13 13.42-6.71	0.43	0.2500	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T14 6.71-0.00	0.43	0.2500	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000

						K Fac	ctors <sup>1</sup>			
Tower Elevation	Calc K Single	Calc K Solid	Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
A	Angles	Rounds		X	X	X	X	X	X	X
n				<u> </u>	<u> </u>	Y	<u> </u>	Y	Y	Y
T1	No	No	1	1	1	1	1	1	1	1

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						K Fac	ctors1			
Tower Elevation	Calc K Single	Calc K Solid	Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
	Angles	Rounds		X	X	X	X	$\boldsymbol{X}$	X	X
ft	111/6/-5			Y	Y	Y	Y	Y	Y	Y
90.33-78.06				1	1	1	1	1	1	1
T2	No	No	1	1	1	1	1	1	1	1
78.06-74.56	2.0			1	1	1	1	1	1	1
T3	No	No	1	1	1	1	1	1	1	1
74.56-72.31	1.0			1	1	1	1	1	1	1
T4	No	No	1	1	1	1	1	1	1	1
72.31-67.56	110	110		1	1	1	1	1	1	1
T5	No	No	1	1	1	1	1	1	1	1
67.56-65.44	110	110	-	1	1	1	1	1	1	1
T6	No	No	1	1	1	1	1	1	1	1
65.44-57.52	140	110	17	1	1	1	1	1	1	1
T7	No	No	1	1	1	1	1	1	1	1
57.52-50.27	140	110		1	1	1	1	1	1	1
T8	No	No	1	1	ī	1	1	1	1	1
50.27-41.98	140	110	•	í	1	1	ī	1	1	1
T9	No	No	1	î	ī	1	1	1	1	1
41.98-34.19	140	140	•	î	ī	1	1	1	1	1
T10	No	No	1	î	ī	1	1	1	1	1
34.19-26.90	140	140		i	ī	ī	1	1	1	1
34.19-26.90 T11	No	No	1	1	î	ī	1	1	1	1
26.90-20.10	140	140		i	î	1	1	1	1	1
	No	No	1	î	i	ī	1	1	1	1
T12	140	140	0#20	î	1	ī	1	ï	1	1
20.10-13.42 T13	No	No	1	1	î	ī	1	1	1	1
	INO	140	200	1	î	î	î	1	1	1
13.42-6.71	DT.	Ma	1	1	1	î	î	1	1	1
Г14 6.71-0.00	No	No	2 <b>4</b> )/	9	1	í	î	ı î	1	1

Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

Tower Elevation	Leg		Diagonal		Top Girt		Botton	Girt	Mid	Girt	Long Horizontal		Short Horizontal	
ft	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 90.33-78.06	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 78.06-74.56	-	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 74.56-72.31		1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 72.31-67.56		1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T5 67.56-65.44		1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T6 65.44-57.52		1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T7 57.52-50.27		1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T8 50.27-41.98	1	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T9 41.98-34.19		1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T10	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
34.19-26.90														
T11	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
26.90-20.10														0.55
T12 20.10-13.42	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

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	bor Management, LLC	treed

Tower Elevation ft	Leg			nal	Top G	irt	Botton	Girt	Mid Girt		Long Ho	rizontal	Short Horizontal	
-	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T13 13.42-6.71		1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T14 6.71-0.00	0.0000	_1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

Tower Elevation ft	Elevation Horizontal ft		Reduna Diago		Reduna Sub-Dias		Redui Sub-Hot		Redundan	t Vertical	Redundant Hip		Redundant Hip Diagonal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 90.33-78.06		0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 78.06-74.56		0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 74.56-72.31	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 72.31-67.56		0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T5 67.56-65.44		0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T6 65.44-57.52		0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T7 57.52-50.27	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T8 50.27-41.98		0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T9 41.98-34.19	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T10 34.19-26.90	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T11 26.90-20.10	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T12 20.10-13.42	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T13 13.42-6.71	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T14 6.71-0.00	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

Tower				Connecti	on Offsets	5.		
Elevation		Diag	gonal			K-Br	acing	
	Vert.	Horiz.	Vert.	Horiz.	Vert.	Horiz.	Vert.	Horiz.
	Top	Top	Bot.	Bot.	Тор	Top	Bot.	Bot.
ft	in	in	in	in	in	in	in	in
T1 90.33-78.06	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
T2 78.06-74.56	4.2500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
T3 74.56-72.31	0.0000	0.0000	3.2500	0.0000	0.0000	0.0000	0.0000	0.0000
T4 72.31-67.56	4.2500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
T5 67.56-65.44	0.0000	0.0000	3.2500	0.0000	0.0000	0.0000	0.0000	0.0000
T6 65.44-57.52	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
T7 57.52-50.27	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
T8 50.27-41.98	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
T9 41.98-34.19	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
T10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
34.19-26.90								0.000
T11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
26.90-20.10							1.2000	5.5000

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Tower	Connection Offsets												
Elevation		Diag	gonal		K-Bracing								
,	Vert. Top	Horiz. Top	Vert. Bot.	Horiz. Bot.	Vert. Top	Horiz. Top	Vert. Bot.	Horiz. Bot.					
ft	in	in	in	in	in	in	in	in					
T12	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000					
20.10-13.42			15										
T13 13.42-6.71	0.0000	0.0000	5.0000	0.0000	0.0000	0.0000	0.0000	0.0000					
T14 6.71-0.00	0.0000	0.0000	5.0000	0.0000	0.0000	0.0000	0.0000	0.0000					

### Tower Section Geometry (cont'd)

Tower Elevation	Leg Connection	Leg		Diago	nal	Top G	irt	Bottom	Girt	Mid G	irt	Long Hor	izontal	Short Hori	izontal
ft	Type					D. I. (7)	37	D. I. C.	NT.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.
		Bolt Size	No.		NO.	in	NO.	in	NO.						
		in		in		in		in		in	_		•		0
T1 90.33-78.06	Sleeve DS	0.6250	12	0.6240	1	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	U
		A307		A325N		A325N	_	A325N		A325N		A325N	3	A325N	0
T2 78.06-74.56	Flange	0.7500	0	0.5410	2	0.6250	2	0.6250	0	0.6250	0	0.6250	3	0.6250	U
		A307		A325N		A325N	520	A325N		A325N		A325N	•	A325N	•
T3 74.56-72.31	Flange	0.7500	0	0.5410	2	0.6250	0	0.6250	0	0.6250	0	0.6250	3	0.6250	0
		A307		A325N		A325N		A325N		A325N	_	A325N	_	A325N	•
T4 72.31-67.56	Flange	0.7500	0	0.5410	2	0.6250	3	0.6250	0	0.6250	0	0.6250	3	0.6250	0
		A307		A325N		A325N		A325N		A325N	_	A325N	_	A325N	•
T5 67.56-65.44	Flange	0.7500	0	0.5410	2	0.6250	0	0.6250	0	0.6250	0	0.6250	3	0.6250	0
		A307		A325N		A325N		A325N		A325N		A325N		A325N	_
T6 65.44-57.52	Flange	0.7500	0	0.5410	2	0.6250	0	0.6250	3	0.6250	0	0.6250	3	0.6250	0
	~	A307		A325N		A325N		A325N		A325N		A325N		A325N	_
T7 57.52-50.27	Flange	0.7500	0	0.5410	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	J	A307		A325N		A325N		A325N		A325N		A325N		A325N	
T8 50.27-41.98	Sleeve DS	0.6250	12	0.5410	2	0.6250	3	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A307		A325N		A325N		A325N		A325N		A325N		A325N	
T9 41.98-34.19	Flange	0.7500	0	0.5410	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
-,		A307		A325N		A325N		A325N		A325N		A325N		A325N	
T10	Flange	0.7500	0	0.5410	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
34.19-26.90		A307		A325N		A325N		A325N		A325N		A325N		A325N	
T11	Flange	0.7500	0	0.5410	2	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
26.90-20.10	1 1442	A307		A325N		A325N		A325N		A325N		A325N		A325N	
T12	Sleeve DS	0.6250	12	0.5410	2	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0
20.10-13.42	Dice to 22	A307		A325N		A325N		A325N		A325N		A325N		A325N	
T13 13.42-6.71	Flange	0.7500	0	0.5410	2	0.6250	0	0.6250	0	0.6250	0	0.6250	1	0.6250	0
115 15.72-0.71	Limbo	A307	•	A325N	_	A325N		A325N		A325N		A325N		A325N	
T14 6.71-0.00	Flange	0.7500	0	0.5410	2	0.6250	0	0.6250	0	0.6250	0	0.6250	1	0.6250	0
117 0./1-0.00	1 Imigo	A307	٠	A325N	_	A325N		A325N		A325N		A325N		A325N	

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Tower Elevation ft	Reduna Horizo		Redund Diago		Reduna Sub-Diag		Redun Sub-Hor		Redundan	t Vertical	Redunda	int Hip	Redunda Diago	-
	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.
	in		in		in		in		in		in		in	
T1 90.33-78.06	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T2 78.06-74.56	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	A325N		A325N		A325N		A325N		A325N		A325N	-	A325N	Ū
T3 74.56-72.31	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	A325N		A325N		A325N		A325N		A325N		A325N		A325N	•
T4 72.31-67.56	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	A325N		A325N		A325N		A325N		A325N		A325N	·	A325N	•
T5 67.56-65.44	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	A325N		A325N		A325N	11.75.1	A325N	_	A325N		A325N	·	A325N	·
T6 65.44-57.52	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	A325N		A325N		A325N	7577	A325N	-	A325N		A325N	·	A325N	·
T7 57.52-50.27	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
CHARLES CONTRACTOR	A325N		A325N		A325N		A325N	-	A325N		A325N	•	A325N	٠
T8 50.27-41.98	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	A325N		A325N		A325N	350	A325N		A325N		A325N	·	A325N	•
T9 41.98-34.19	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
. Programme Covers	A325N		A325N		A325N		A325N	ŭ	A325N	•	A325N	٠	A325N	·
T10	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
34.19-26.90	A325N		A325N		A325N		A325N		A325N	•	A325N	·	A325N	U
T11	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
26.90-20.10	A325N		A325N		A325N		A325N		A325N	٠ ا	A325N	Ū	A325N	U
T12	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
20.10-13.42	A325N	-	A325N	_	A325N	.5	A325N	•	A325N	·	A325N	J	A325N	J
T13 13.42-6.71	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
1570	A325N		A325N	- 1	A325N		A325N	J	A325N	ı	A325N	J	A325N	v
T14 6.71-0.00	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	A325N	-	A325N		A325N	350	A325N	v	A325N	١	A325N	U	A325N	v

# Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or	Allow Shield	Exclude From	Component Type	Placement	Face Offset	Lateral Offset	#	# Per	Clear Spacing	Width or Diameter	Perimeter	Weight
	Leg		Torque		ft	in	(Frac FW)		Row	in	in	in	plf
***Leg A AZ			Calculation					_					
0 Deg***													
Feedline	С	No	No	Af (CaAa)	77.00 - 0.00	0.0000	0	2	2	24.0000	2.0000		4.20
Ladder (Af)				` ,				_	_		210000		1.20
LDF5-50A	C	No	No	Ar (CaAa)	76.70 - 0.00	0.0000	0.01	6	6	1.0900	1.0900		0.33
(7/8 FOAM)													
(AT&T)													
0.92" DC	C	No	No	Ar (CaAa)	76.70 - 0.00	0.0000	-0.07	3	3	0.9200	0.9200		0.42
(AT&T)													
3/8" Fiber	C	No	No	Ar (CaAa)	76.70 - 0.00	0.0000	0.07	1	1	0.3750	0.3750		0.10
(AT&T)	_												
1/2" Fiber	С	No	No	Ar (CaAa)	76.70 - 0.00	0.0000	0.075	1	1	0.5000	0.5000		0.10
(AT&T)	~												
3/4" OD	C	No	No	Ar (CaAa)	76.70 - 0.00	0.0000	0.12	4	2	0.7500	0.7500		0.40
(AT&T) 1" Conduit	С	Nt-	NT-	. (0.1)	40.00 0.00			_					
(dead)	C	No	No	Ar (CaAa)	48.00 - 0.00	0.0000	0.25	1	1	1.0000	1.0000		0.75
5/16" OD	D	No	No	A= (C- A=)	40.00	4 0000	0.05			0.0105	0.0105		
(dead)	ט	140	140	Ar (CaAa)	48.00 - 50.00	<b>-4</b> .0000	0.25	1	1	0.3125	0.3125		2.00

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Description	Face or	Allow Shield	Exclude From	Component Type		Face Offset	Lateral Offset	#			Diameter		Weight
	Leg		Torque		ft	in	(Frac FW)		Row	in	in	in	plf
	_		Calculation										
1-5/16" OD (dead)	D	No	No	Ar (CaAa)	54.00 - 0.00	0.0000	0.5	1	1	1.3125	1.3125		1.00
Safety Line 3/8 *****	С	No	No	Ar (CaAa)	90.33 - 0.00	0.0000	0.5	1	1	0.3750	0.3750		0.22
6x12 HCS (Verizon)	D	No	No	Ar (CaAa)	90.00 - 0.00	0.0000	-0.4	2	2	1.5400	1.5400		1.70

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation	Face	$A_R$	$A_F$	C₄A₄ In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
5001071	ft		ft²	ft²	ft²	ft²	IЬ
T1	90.33-78.06	Α	0.000	0.000	0.000	0.000	0.00
**	3000 1000	В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.460	0.000	2.70
		Ď	0.000	0.000	3.677	0.000	40.59
T2	78.06-74.56	Ā	0.000	0.000	0.000	0.000	0.00
12	70.00-74.50	В	0.000	0.000	0.000	0.000	0.00
		č	0.000	0.000	4.571	0.000	31.98
		Ď	0.000	0.000	1.078	0.000	11.90
T3	74.56-72.31	Ā	0.000	0.000	0.000	0.000	0.00
13	74.30-72.31	В	0.000	0.000	0.000	0.000	0.00
		Č	0.000	0.000	4.549	0.000	30.70
		D	0.000	0.000	0.693	0.000	7.65
T4	72,31-67.56	A	0.000	0.000	0.000	0.000	0.00
14	12.31-01.30	B	0.000	0.000	0.000	0.000	0.00
		Č	0.000	0.000	9.603	0.000	64.82
		D	0.000	0.000	1.463	0.000	16.15
TE	67.56-65.44	A	0.000	0.000	0.000	0.000	0.00
T5	07.30-03.44	В	0.000	0.000	0.000	0.000	0.00
		Č	0.000	0.000	4.296	0.000	29.00
		D	0.000	0.000	0.654	0.000	7.22
mc.	CE 44 EE EO		0.000	0.000	0.000	0.000	0.00
T6	65.44-57.52	A	0.000	0.000	0.000	0.000	0.00
		В		0.000	16.006	0.000	108.03
		C	0.000	0.000	2.438	0.000	26.92
		D	0.000		0.000	0.000	0.00
T7	57.52-50.27	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000		0.000	98.93
		C	0.000	0.000	14.657 2.722	0.000	28.38
		D	0.000	0.000	0.000	0.000	0.00
T8	50.27-41.98	A	0.000	0.000			0.00
		В	0.000	0.000	0.000	0.000	117.67
		C	0.000	0.000	17.366	0.000	40.48
		D	0.000	0.000	3.705	0.000	0.00
T9	41.98-34.19	A	0.000	0.000	0.000	0.000	
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	16.532	0.000	112.17
		D	0.000	0.000	3.423	0.000	34.28
T10	34.19-26.90	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	15.471	0.000	104.97
		D	0.000	0.000	3.203	0.000	32.08
T11	26.90-20.10	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	14.410	0.000	97.78

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Tower Section	Tower Elevation	Face	$A_R$	$A_F$	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight	
	ft		ft²	ft²	ft²	ft <sup>2</sup>	lb	
		D	0.000	0.000	2.983	0.000	29.88	
T12	20.10-13.42	A	0.000	0.000	0.000	0.000	0.00	
		В	0.000	0.000	0.000	0.000	0.00	
		C	0.000	0.000	14.190	0.000	96.28	
		D	0.000	0.000	2.938	0.000	29.43	
T13	13.42-6.71	Α	0.000	0.000	0.000	0.000	0.00	
		В	0.000	0.000	0.000	0.000	0.00	
		C	0.000	0.000	14.231	0.000	96.56	
		D	0.000	0.000	2.946	0.000	29.51	
T14	6.71-0.00	Α	0.000	0.000	0.000	0.000	0.00	
		В	0.000	0.000	0.000	0.000	0.00	
		C	0.000	0.000	14.231	0.000	96.56	
		D	0.000	0.000	2.946	0.000	29.51	

# Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation	Face or	Ice Thickness	$A_R$	$A_F$	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
	ft	Leg	in	ft²	ft²	fi²	ft²	lь
T1	90.33-78.06	A	1.098	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	3.155	0.000	26.95
		D		0.000	0.000	11.599	0.000	127.61
T2	78.06-74.56	Α	1.087	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	12.238	0.000	124.42
		D		0.000	0.000	3.388	0.000	37.16
T3	74.56-72.31	A	1.083	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	12.153	0.000	122.52
		D		0.000	0.000	2.175	0.000	23.82
T4	72.31-67.56	A	1.078	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	25.606	0.000	257.55
		D		0.000	0.000	4.583	0.000	50.12
T5	67.56-65.44	Α	1.073	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	11.432	0.000	114.71
		D		0.000	0.000	2.046	0.000	22.34
T6	65.44-57.52	Α	1.064	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	42.461	0.000	424.44
		D		0.000	0.000	7.601	0.000	82.78
T7	57.52-50.27	Α	1.050	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	38.684	0.000	384.26
		D		0.000	0.000	8.199	0.000	90.14
T8	50.27-41.98	A	1.034	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	45.824	0.000	453.63
		D		0.000	0.000	11.032	0.000	125.26
T9	41.98-34.19	Α	1.014	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	43.382	0.000	426.20
		D		0.000	0.000	9.954	0.000	109.09
T10	34.19-26.90	Α	0.992	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	40.246	0.000	391.36

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Tower Section	Tower Elevation	Face or	Ice Thickness	$A_R$	$A_F$	C <sub>A</sub> A <sub>A</sub> In Face	CAAA Out Face	Weight	
Deciron	ft	Leg	in	ft²	ft <sup>2</sup>	ft²	ft²	lb	
		D		0.000	0.000	9.228	0.000	100.35	
T11	26.90-20.10	Α	0.967	0.000	0.000	0.000	0.000	0.00	
		В		0.000	0.000	0.000	0.000	0.00	
		C		0.000	0.000	37.106	0.000	356.54	
		D		0.000	0.000	8.501	0.000	91.61	
T12	20.10-13.42	A	0.934	0.000	0.000	0.000	0.000	0.00	
	20120 10112	В		0.000	0.000	0.000	0.000	0.00	
		Ċ		0.000	0.000	36.070	0.000	341.38	
		Ď		0.000	0.000	8.256	0.000	87.94	
T13	13.42-6.71	Ā	0.888	0.000	0.000	0.000	0.000	0.00	
115	15.12 0.71	В		0.000	0.000	0.000	0.000	0.00	
		c		0.000	0.000	35.496	0.000	328.58	
		Ď		0.000	0.000	8.112	0.000	84.98	
T14	6.71-0.00	A	0.796	0.000	0.000	0.000	0.000	0.00	
	0., 1 0.00	В		0.000	0.000	0.000	0.000	0.00	
		č		0.000	0.000	34.148	0.000	302.15	
		Ď		0.000	0.000	7.780	0.000	78.78	

#### **Feed Line Center of Pressure**

Section	Elevation	$CP_X$	$CP_Z$	$CP_X$	$CP_Z$
				Ice	Ice
	ft	in	in	in	in
T1	90.33-78.06	1.4277	1.2043	3.6056	2.9720
T2	78.06-74.56	2.7626	0.9732	5.9068	1.8610
T3	74.56-72.31	3.1920	0.8580	4.9996	1.2167
T4	72.31-67.56	3.7135	0.9794	7.9 <b>59</b> 1	1.8220
T5	67.56-65.44	2.3399	0.6493	1.9241	0.5003
Т6	65,44-57,52	4.9646	1.2717	10.6230	2.3454
T7	57.52-50.27	5.0162	1.7458	10.8198	3.1358
Т8	50.27-41.98	4.6827	2,1503	10.5243	4.0324
T9	41.98-34.19	5.6369	2.5305	12.3747	4.5809
T10	34.19-26.90	5.9797	2.6998	13.0637	4.8597
T11	26.90-20.10	6.2439	2.8346	13.5615	5.0672
T12	20.10-13.42	5.5037	2.5544	12.3642	4.7105
T13	13.42-6.71	5.8564	2.7208	12.9968	4.9381
T14	6.71-0.00	5.5916	2.6253	12.0543	4.6085

### **Shielding Factor Ka**

Tower	Feed Line	Description	Feed Line	K <sub>a</sub>	Ka
Section	Record No.		Segment Elev.	No Ice	Ice
T1	14	Safety Line 3/8	78.06 - 90.33	0.6000	0.6000
T1	16	6x12 HCS	78.06 - 90.00	0.6000	0.6000
T2	2	Feedline Ladder (Af)	74.56 - 77.00	0.6000	0.5038
T2	5	LDF5-50A (7/8 FOAM)	74,56 - 76.70	0.6000	0.5038
T2	6	0.92" DC	74.56 - 76.70	0.6000	0.5038
T2	7	3/8" Fiber	74.56 - 76.70	0.6000	0.5038
T2	Ŕ	1/2" Fiber	74.56 - 76.70	0.6000	0.5038
T2	10	3/4" OD	74.56 - 76.70	0.6000	0.5038
T2	14			0.6000	0.5038

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Tower	Feed Line	Description	Feed Line	Ka	Ka
Section	Record No.	2-000. \$2.000	Segment Elev.	No Ice	Ice
T2	16	6x12 HCS	74.56 - 78.06	0.6000	0.5038
Т3	2	Feedline Ladder (Af)	72.31 - 74.56	0.5973	0.3629
T3	5	LDF5-50A (7/8 FOAM)	72.31 - 74.56	0.5973	0.3629
T3	6	0.92" DC	72.31 - 74.56	0.5973	0.3629
T3	7	3/8" Fiber	72.31 - 74.56	0.5973	0.3629
T3	8	1/2" Fiber	72.31 - 74.56	0.5973	0.3629
T3	10	3/4" OD	72.31 - 74.56	0.5973	0.3629
T3	14	Safety Line 3/8	72.31 - 74.56	0.5973	0.3629
T3	16	6x12 HCS	72.31 - 74.56	0.5973	0.3629
T4	2	Feedline Ladder (Af)	67.56 - 72.31	0.6000	0.5315
T4 T4	5	LDF5-50A (7/8 FOAM)	67.56 - 72.31	0.6000	0.5315
T4	6 7	0.92" DC	67.56 - 72.31	0.6000	0.5315
T4	8	3/8" Fiber 1/2" Fiber	67.56 - 72.31 67.56 - 72.31	0.6000	0.5315
T4	10	3/4" OD	67.56 - 72.31	0.6000	0.5315 0.5315
T4	14	Safety Line 3/8	67.56 - 72.31	0.6000	0.5315
T4	16	6x12 HCS	67.56 - 72.31	0.6000	0.5315
T5	2	Feedline Ladder (Af)	65.44 - 67.56	0.4832	0.3313
T5	5	LDF5-50A (7/8 FOAM)	65.44 - 67.56	0.4832	0.1706
T5	6	0.92" DC	65.44 - 67.56	0.4832	0.1706
T5	7	3/8" Fiber	65.44 - 67.56	0.4832	0.1706
T5	8	1/2" Fiber	65.44 - 67.56	0.4832	0.1706
T5	10	3/4" OD	65.44 - 67.56	0.4832	0.1706
T5	14	Safety Line 3/8	65.44 - 67.56	0.4832	0.1706
T5	16	6x12 HCS	65.44 - 67.56	0.4832	0.1706
T6	2	Feedline Ladder (Af)	57.52 - 65.44	0.6000	0.6000
T6	5	LDF5-50A (7/8 FOAM)	57.52 - 65.44	0.6000	0.6000
T6	6	0.92" DC	57.52 - 65.44	0.6000	0.6000
T6	7	3/8" Fiber	57.52 - 65.44	0.6000	0.6000
Т6	8	1/2" Fiber	57.52 - 65.44	0.6000	0.6000
T6	10	3/4" OD	57.52 - 65.44	0.6000	0.6000
T6	14	Safety Line 3/8	57.52 - 65.44	0.6000	0.6000
T6	16	6x12 HCS	57.52 - 65.44	0.6000	0.6000
T7	2	Feedline Ladder (Af)	50.27 - 57.52	0.6000	0.6000
T7 T7	5	LDF5-50A (7/8 FOAM)	50.27 - 57.52	0.6000	0.6000
T7	6 7	0.92" DC	50.27 - 57.52	0.6000	0.6000
T7	8	3/8" Fiber 1/2" Fiber	50.27 - 57.52	0.6000	0.6000
T7	10	3/4" OD	50.27 - 57.52 50.27 - 57.52	0.6000	0.6000
T7	13	1-5/16" OD	50.27 - 54.00	0.6000	0.6000
T7	14	Safety Line 3/8	50.27 - 57.52	0.6000	0.6000
T7	16	6x12 HCS	50.27 - 57.52	0.6000	0.6000
T8	2	Feedline Ladder (Af)	41.98 - 50.27	0.6000	0.6000
T8	5	LDF5-50A (7/8 FOAM)	41.98 - 50.27	0.6000	0.6000
Т8	6	0.92" DC	41.98 - 50.27	0.6000	0.6000
T8	7	3/8" Fiber	41.98 - 50.27	0.6000	0.6000
T8	8	1/2" Fiber	41.98 - 50.27	0.6000	0.6000
T8	10	3/4" OD	41.98 - 50.27	0.6000	0.6000
Т8	11	1" Conduit	41.98 - 48.00	0.6000	0.6000
Т8	12	5/16" OD	48.00 - 50.00	0.6000	0.6000
Т8	13	1-5/16" OD	41.98 - 50.27	0.6000	0.6000
Т8	14	Safety Line 3/8	41.98 - 50.27	0.6000	0.6000
T8	16	6x12 HCS	41.98 - 50.27	0.6000	0.6000
T9	2	Feedline Ladder (Af)	34.19 - 41.98	0.6000	0.6000
T9	5	LDF5-50A (7/8 FOAM)	34.19 - 41.98	0.6000	0.6000
T9	6	0.92" DC	34.19 - 41.98	0.6000	0.6000
T9	7	3/8" Fiber	34.19 - 41.98	0.6000	0.6000
T9	. 8	1/2" Fiber	34.19 - 41.98	0.6000	0.6000
	10	3/4" OD	34.19 - 41.98	0.6000	0.6000
T9					
T9	11	1" Conduit	34.19 - 41.98	0.6000	0.6000
			34.19 - 41.98 34.19 - 41.98 34.19 - 41.98		

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Client	BST Management, LLC	Designed by treed

Tower	Feed Line	Description	Feed Line	K <sub>a</sub>	Ka
Section	Record No.		Segment Elev.	No Ice	Ice
T9	16	6x12 HCS	34.19 - 41.98	0.6000	0.6000
T10	2	Feedline Ladder (Af)	26.90 - 34.19	0.6000	0.6000
T10	5	LDF5-50A (7/8 FOAM)	26.90 - 34.19	0.6000	0.6000
T10	6	0.92" DC	26.90 - 34.19	0.6000	0.6000
T10	7	3/8" Fiber	26.90 - 34.19	0.6000	0.6000
T10	8	1/2" Fiber	26.90 - 34.19	0.6000	0.6000
T10	10	3/4" OD	26.90 - 34.19	0.6000	0.6000
T10	11	1" Conduit	26.90 - 34.19	0.6000	0.6000
T10	13	1-5/16" OD	26.90 - 34.19	0.6000	0.6000
T10	14	Safety Line 3/8	26.90 - 34.19	0.6000	0.6000
	16	6x12 HCS	26.90 - 34.19	0.6000	0.6000
T10	17371	Feedline Ladder (Af)	20.10 - 26.90	0.6000	0.6000
T11	2 5	LDF5-50A (7/8 FOAM)	20.10 - 26.90	0.6000	0.6000
T11	6	0.92" DC	20.10 - 26.90	0.6000	0.6000
T11		3/8" Fiber	20.10 - 26.90	0.6000	0.6000
T11	7	1/2" Fiber	20.10 - 26.90	0.6000	0.6000
T11	8	3/4" OD	20.10 - 26.90	0.6000	0.6000
T11	10	1" Conduit	20.10 - 26.90	0.6000	0.6000
T11	11	_		0.6000	0.6000
T11	13	1-5/16" OD	20.10 - 26.90	0.6000	0.6000
T11	14	Safety Line 3/8	20.10 - 26.90	0.6000	0.6000
T11	16	6x12 HCS	20.10 - 26.90	0.6000	0.6000
T12	2	Feedline Ladder (Af)	13.42 - 20.10		
T12	5	LDF5-50A (7/8 FOAM)	13.42 - 20.10	0.6000	0.6000
T12	6	0.92" DC	13.42 - 20.10	0.6000	0.6000
T12	7	3/8" Fiber	13.42 - 20.10	0.6000	0.6000
T12	8	1/2" Fiber	13.42 - 20.10	0.6000	0.6000
T12	10	3/4" OD	13.42 - 20.10	0.6000	0.6000
T12	11	1" Conduit	13.42 - 20.10	0.6000	0.6000
T12	13	1-5/16" OD	13.42 - 20.10	0.6000	0.6000
T12	14	Safety Line 3/8	13.42 - 20.10	0.6000	0.6000
T12	16	6x12 HCS	13.42 - 20.10	0.6000	0.6000
T13	2	Feedline Ladder (Af)	6.71 - 13.42	0.6000	0.6000
T13	5	LDF5-50A (7/8 FOAM)	6.71 - 13.42	0.6000	0.6000
T13	6	0.92" DC	6.71 - 13.42	0.6000	0.6000
T13	7	3/8" Fiber	6.71 - 13.42	0.6000	0.6000
T13	8	1/2" Fiber	6.71 - 13.42	0.6000	0.6000
T13	10	3/4" OD	6.71 - 13.42	0.6000	0.6000
T13	11	1" Conduit	6.71 - 13.42	0.6000	0.6000
T13	13	1-5/16" OD	6.71 - 13.42	0.6000	0.6000
T13	14	Safety Line 3/8	6.71 - 13.42	0.6000	0.6000
T13	16	6x12 HCS	6.71 - 13.42	0.6000	0.6000
T14	2	Feedline Ladder (Af)	0.00 - 6.71	0.6000	0.6000
T14	5	LDF5-50A (7/8 FOAM)	0.00 - 6.71	0.6000	0.6000
T14	6	0.92" DC	0.00 - 6.71	0.6000	0.6000
T14	7	3/8" Fiber	0.00 - 6.71	0.6000	0.6000
T14	8	1/2" Fiber	0.00 - 6.71	0.6000	0.6000
T14	10	3/4" OD	0.00 - 6.71	0.6000	0.6000
T14	11	1" Conduit	0.00 - 6.71	0.6000	0.6000
T14	13	1-5/16" OD	0.00 - 6.71	0.6000	0.6000
T14	14	Safety Line 3/8	0.00 - 6.71	0.6000	0.6000
T14	16	6x12 HCS	0.00 - 6.71	0.6000	0.6000

### **Discrete Tower Loads**

Structural Components, LLC 1870 West 64th Lane, Unit A Denver, CO 80221 Phone: (866) 386-7622 FAX:

Job		Page
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Project		Date
	Portland (CT-1680)	15:03:20 02/13/24
Client	DOTAL CLUB	Designed by
	BST Management, LLC	treed

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	C₄A₄ Side	Weigi
	Leg		Lateral Vert						
			ft	0	ft		ft²	fî²	lb
			ft ft		<i>)-</i>		<i>J•</i>	<i>,</i> ,	10
6' x 5/8" Lighting Rod	A	From Leg	0.00	0.0000	90.50	No Ice	0.38	0.38	10.00
			0.00			1/2" Ice	0.99	0.99	14.19
***			3.00			1" Ice	1.62	1.62	22.20
NNH4-65B-R6	Α	From Leg	3.00	30.0000	90.00	No Ice	12.27	5.75	83.0
(Verizon)			0.00	20.000	70.00	1/2" Ice	12.77	6.21	155.1
	_		0.00			1" Ice	13.27	6.67	233.9
NNH4-65B-R6	В	From Leg	3.00	60.0000	90.00	No Ice	12.27	5.75	83.0
(Verizon)			0.00			1/2" Ice	12.77	6.21	155.1
NNH4-65B-R6	D	From Leg	0.00	0.0000	00.00	l" Ice	13.27	6.67	233.9
(Verizon)	D	From Leg	3.00 0.00	0.0000	90.00	No Ice 1/2" Ice	12.27 12.77	5.75 6.21	83.0
(141101)			0.00			1" Ice	13.27	6.67	155.1 233.9
RT4423 w/ RRU	Α	From Leg	3.00	30.0000	90.00	No Ice	0.87	0.43	18.7
(Verizon)		· ·	-5.00			1/2" Ice	0.99	0.52	25.7
			0.00			1" Ice	1.11	0.61	34.5
RT4423 w/ RRU	В	From Leg	3.00	60.0000	90.00	No Ice	0.87	0.43	18.7
(Verizon)			-5.00			1/2" Ice	0.99	0.52	25.7
DT4492/ DD11	ъ.	P	0.00	0.0000	22.22	1" Ice	1.11	0.61	34.5
RT4423 w/ RRU (Verizon)	D	From Leg	3.00	0.0000	90.00	No Ice	0.87	0.43	18.7
(Verizon)			-5.00 0.00			1/2" Ice	0.99	0.52	25.7
MT6413-77A	Α	From Leg	3.00	30.0000	90.00	1" Ice No Ice	1.11 3.78	0.61	34.59 57.30
(Verizon)		Trom Dog	5.00	30.0000	90.00	1/2" Ice	4.03	1.46 1.65	81.6
` '			0.00			1" Ice	4.29	1.84	109.3
MT6413-77A	В	From Leg	3.00	60.0000	90.00	No Ice	3.78	1.46	57.3
(Verizon)			5.00			1/2" Ice	4.03	1.65	81.6
3.0000110.0001	_		0.00			1" Ice	4.29	1.84	109.3
MT6413-77A	D	From Leg	3.00	0.0000	90.00	No Ice	3.78	1.46	57.3
(Verizon)			5.00			1/2" Ice	4.03	1.65	81.6
F4439d-25A (Full Frontal	A	From Leg	0.00 2.50	30.0000	90.00	1" Ice No Ice	4.29	1.84	109.3
Shielding)	A	Tioni Leg	0.00	30.0000	90.00	1/2" Ice	0.00 0.00	1.25 1.39	74.70 93.00
(Verizon)			0.00			1" Ice	0.00	1.54	114.1
F4439d-25A (Full Frontal	В	From Leg	2.50	60.0000	90.00	No Ice	0.00	1.25	74.70
Shielding			0.00			1/2" Ice	0.00	1.39	93.0
(Verizon)			0.00			1" Ice	0.00	1.54	114.1
F4439d-25A (Full Frontal	D	From Leg	2.50	0.0000	90.00	No Ice	0.00	1.25	74.7
Shielding)			0.00			1/2" Ice	0.00	1.39	93.02
(Verizon) F4416d-13A (Full Frontal	Α	From I	0.00	20.0000	00.00	1" Ice	0.00	1.54	114.1
Shielding)	A	From Leg	2.50 0.00	30.0000	90.00	No Ice	0.00	1.28	79.10
(Verizon)			0.00			1/2" Ice 1" Ice	0.00 0.00	1.42	97.63
F4416d-13A (Full Frontal	В	From Leg	2.50	60.0000	90.00	No Ice	0.00	1.57 1.28	118.9 79.10
Shielding)	_	110m 20g	0.00	00.0000	70.00	1/2" Ice	0.00	1.42	97.6
(Verizon)			0.00			1" Ice	0.00	1.57	118.9
F4416d-13A (Full Frontal	D	From Leg	2.50	0.0000	90.00	No Ice	0.00	1.28	79.10
Shielding)		_	0.00			1/2" Ice	0.00	1.42	97.61
(Verizon)			0.00			1" Ice	0.00	1.57	118.9
FE-16148-OVP-B12	Α	From Leg	1.00	30.0000	90.00	No Ice	1.87	1.07	15.21
(Verizon)			0.00			1/2" Ice	2.04	1.20	31.51
4) 2-3/8" x 8' Pipe Mount	Α	From Loc	0.00	20 0000	00.00	1" Ice	2.21	1.35	50.47
(Verizon)	A	From Leg	3.00 0.00	30.0000	90.00	No Ice 1/2" Ice	1.90	1.90	30.00
(, 01111011)			0.00			1/2" Ice	2.73 3.40	2.73 3.40	44.37 64.01
4) 2-3/8" x 8' Pipe Mount	В	From Leg	3.00	60.0000	90.00	No Ice	1.90	1.90	30.00
(Verizon)			0.00			1/2" Ice	2.73	2.73	44.37

Structural Components, LLC 1870 West 64th Lane, Unit A

Denver, CO 80221 Phone: (866) 386-7622 FAX:

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Client	BST Management, LLC	Designed by treed

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weig
	Leg		Lateral Vert						
			ft ft	0	ft		fît²	ft²	lb
			ft			10.7	2.40	2.40	64.0
	_	T	0.00	0.0000	90.00	1" Ice No Ice	3.40 1.90	3.40 1.90	30.0
4) 2-3/8" x 8' Pipe Mount	D	From Leg	3.00 0.00	0.0000	90.00	1/2" Ice	2.73	2.73	44.3
(Verizon)			0.00			1" Ice	3.40	3.40	64.0
(3) SitePro VFA12-HD	С	None	0.00	0.0000	90.00	No Ice	25.00	25.00	800.
(Verizon)	·	110110				1/2" Ice	37.00	37.00	1100
(VOILLOIL)						1" Ice	47.00	47.00	1500
Tieback	A	From Leg	1.50	30.0000	90.00	No Ice	0.00	1.33	25.0
(Verizon)		_	0.00			1/2 <sup>n</sup> Ice	0.00	2.13	45.0
			0.00			1" Ice	0.00	2.93	65.0
Tieback	В	From Leg	1.50	60,0000	90.00	No Ice	0.00	1.33 2.13	25.0 45.0
(Verizon)			0.00			1/2" Ice 1" Ice	0.00	2.13	65.0
	-	P T	0.00	0.0000	90.00	No Ice	0.00	1.33	25.0
Tieback	D	From Leg	1.50 0.00	0.0000	50.00	1/2" Ice	0.00	2.13	45.0
(Verizon)			0.00			1" Ice	0.00	2.93	65.0
***			0.00						
Ring Mount	C	None		0.0000	77.00	No Ice	6.87	6.87	850.
14mg 1/10=11-	_					1/2" Ice	8.25	8.25	1020
						1" Ice	9.62	9.62	1190
***					= < = 0		0.00	0.40	77.
RRUS-32 (Full Frontal	A	From Leg	1.50	30.0000	76.70	No Ice	0.00	2,42	77.9 104.
Shielding)			-2.00			1/2" Ice 1" Ice	0.00 0.00	2.64 2.86	136
(AT&T)	_		0.50	£0.0000	76.70	No Ice	0.00	2.42	77.0
RRUS-32 (Full Frontal	В	From Leg	1.50	60.0000	76.70	1/2" Ice	0.00	2.64	104.
Shielding)			-2.00 0.50			1" Ice	0.00	2.86	136.
(AT&T) RRUS-32 (Full Frontal	D	From Leg	1.50	0.0000	76.70	No Ice	0.00	2.42	77.0
Shielding)	D	From Deg	-2.00	0.0000		1/2" Ice	0.00	2.64	104.
(AT&T)			0.50			1" Ice	0.00	2.86	136.
RRUS-32	Α	From Leg	1.50	30.0000	76.70	No Ice	3.31	2.42	77.0
(AT&T)			2.00			1/2" Ice	3.56	2.64	104
` '			2.00			1" Ice	3.81	2.86	136.
RRUS-32	В	From Leg	1.50	60.0000	76.70	No Ice	3.31	2,42	77.0
(AT&T)			2.00			1/2" Ice	3.56	2.64 2.86	104. 136
	_		2.00	0.0000	76.70	1" Ice No Ice	3.81 3.31	2.42	77.
RRUS-32	D	From Leg	1.50 2.00	0.0000	76.70	1/2" Ice	3.56	2.64	104
(AT&T)			2.00			1" Ice	3.81	2.86	136.
DDIIC 22 (Euli Frontsi	Α	From Leg	1.50	30.0000	76.70	No Ice	0.00	2.42	77.
RRUS-32 (Full Frontal Shielding)	А	From Log	5.00	50.0000	70170	1/2" Ice	0.00	2.64	104.
(AT&T)			0.50			1" Ice	0.00	2.86	136.
RRUS-32 (Full Frontal	В	From Leg	1.50	60.0000	76.70	No Ice	0.00	2.42	77.0
Shielding)			5.00			1/2" Ice	0.00	2.64	104.
(AT&T)			0.50			1" Ice	0.00	2.86	136.
RRUS-32 (Full Frontal	D	From Leg	1.50	0.0000	76.70	No Ice	0.00	2.42	77.0
Shielding)			5.00			1/2" Ice	0.00	2.64	104.
(AT&T)	_	T. T	0.50	<i>c</i> 0 0000	76.70	1" Ice No Ice	0.00 2.20	2.86 2.20	136. 20.
DC6-48-60-18-8F	В	From Leg	2.00	60.0000	76.70	No ice 1/2" Ice	2.40	2.40	42.
(AT&T)			2.00 2.00			1" Ice	2.60	2.60	68.
DCC 40 CO 10 0E	В	From Leg	2.00	60.0000	76.70	No Ice	2.20	2.20	20.0
DC6-48-60-18-8F (AT&T)	ь	Lioni reg	2.00	00.0000	. 5.70	1/2" Ice	2.40	2.40	42.
(AIGI)			0.50			1" Ice	2.60	2.60	68.2
		From Leg	2.00	30.0000	76.70	No Ice	12.71	5.62	69.6
TPA65R-BU6DA-K	A	LIOHI TEK	2.00	30.0000	70.70	1/2" Ice	13.21	6.07	142.

Structural Components, LLC 1870 West 64th Lane, Unit A Denver, CO 80221

Denver, CO 80221
Phone: (866) 386-7622
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Project		Date
	Portland (CT-1680)	15:03:20 02/13/24
Client		Designed by
	BST Management, LLC	treed

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		$C_A A_A$ Front	C₄A₄ Side	Weigh
	Leg		Lateral						
			Vert ft	•	4		.c.2	Δ2	12
			ft		ft		ft²	ft²	lb
TPA65R-BU6DA-K	В	From Leg	ft 2.00	60.0000	76.70	No Ice	12.71	5.62	69.00
(AT&T)		5	-5.00		, , , ,	1/2" Ice	13.21	6.07	142.9
			0.00			1" Ice	13.71	6.53	223.5
TPA65R-BU6DA-K	D	From Leg	2.00	0.0000	76.70	No Ice	12.71	5.62	69.0
(AT&T)			-5.00			1/2" Ice	13.21	6.07	142.9
			0.00			1" Ice	13.71	6.53	223.5
AIR6449 B77D	A	From Leg	2.00	30.0000	76.70	No Ice	4.05	2.74	95.5
(AT&T)			-2.00			1/2" Ice	4.32	2.97	129.1
			0.00			1" Ice	4.59	3.20	166.6
AIR6449 B77D	В	From Leg	2.00	60.0000	76.70	No Ice	4.05	2.74	95.50
(AT&T)			-2.00			1/2" Ice	4.32	2.97	129.1
4 TD < 4 40 TO TOTAL	_		0.00			1" Ice	4.59	3.20	166.6
AIR6449 B77D	D	From Leg	2.00	0.0000	76.70	No Ice	4.05	2.74	95.50
(AT&T)			-2.00			1/2" Ice	4.32	2.97	129.1
ATD (410 D350)			0.00			1" Ice	4.59	3.20	166.6
AIR6419 B77G	A	From Leg	2.00	30.0000	76.70	No Ice	4.17	2.02	55.40
(AT&T)			-2.00			1/2" Ice	4.44	2.23	84.59
AIR6419 B77G	В	F I	0.00	CO 0000	76.70	1" Ice	4.71	2.44	117.5
(AT&T)	D	From Leg	2.00 -2.00	60.0000	76.70	No Ice	4.17	2.02	55.40
(AIGI)			0.00			1/2" Ice	4,44	2.23	84.59
AIR6419 B77G	D	From Leg	2.00	0.0000	76.70	1" Ice	4.71	2.44	117.5
(AT&T)	D	From Leg	-2.00	0.0000	76.70	No Ice 1/2" Ice	4.17	2.02	55.40
(11.021)			0.00			1" Ice	4.44 4.71	2.23	84.59
DMP65R-BU6DA	Α	From Leg	2.00	30.0000	76.70	No Ice	12.71	2.44 5.62	117.5
(AT&T)	••	110III LUG	5.00	30.0000	70.70	1/2" Ice	13.21	6.07	80.00 153.9
()			0.00			1" Ice	13.71	6.53	234.5
DMP65R-BU6DA	В	From Leg	2.00	60.0000	76.70	No Ice	12.71	5.62	80.00
(AT&T)			5.00	00.0000	70.70	1/2" Ice	13.21	6.07	153.9
` ,			0.00			1" Ice	13.71	6.53	234.5
DMP65R-BU6DA	C	From Leg	2.00	0.0000	76.70	No Ice	12.71	5.62	80.00
(AT&T)		Č	5.00			1/2" Ice	13.21	6.07	153.9
			0.00			1" Ice	13.71	6.53	234.5
4478 RRU	Α	From Leg	1.50	30.0000	76.70	No Ice	1.64	0.91	60.00
(AT&T)			2.00			1/2" Ice	1.80	1.03	74.20
			0.00			1" Ice	1.97	1.17	90.89
4478 RRU	В	From Leg	1.50	60.0000	76.70	No Ice	1.64	0.91	60.00
(AT&T)			2.00			1/2" Ice	1.80	1.03	74.20
			0.00			1" Ice	1.97	1.17	90.89
4478 RRU	D	From Leg	1.50	0.0000	76.70	No Ice	1.64	0.91	60.00
(AT&T)			2.00			1/2" Ice	1.80	1.03	74.20
4440.000			0.00			1" Ice	1.97	1.17	90.89
4449 RRU	Α	From Leg	1.50	30.0000	76.70	No Ice	1.64	1.02	74.00
(AT&T)			2.00			1/2" Ice	1.80	1.15	90.04
4440 BBYI	_		0.00			1" Ice	1.97	1.28	108.70
4449 RRU	В	From Leg	1.50	60.0000	76.70	No Ice	1.64	1.02	74.00
(AT&T)			2.00			1/2" Ice	1.80	1.15	90.04
4449 RRU	ъ	E T	0.00	0.0000	26.50	1" Ice	1.97	1.28	108.70
	D	From Leg	1.50	0.0000	76.70	No Ice	1.64	1.02	74.00
(AT&T)			2.00			1/2" Ice	1.80	1.15	90.04
C9-48-60-24-8C-EV	A	From Leg	0.00 2.00	30.0000	76.70	1" Ice	1.97	1.28	108.70
(AT&T)	A	riom reg	0.00	30.0000	76.70	No Ice	2.74	4.78	16.00
(VICT)			0.00			1/2" Ice	2.96	5.06	53.06
(3) 12' Sector Frames	С	None	0.00	0.0000	76.70	1" Ice	3.20	5.35	94.20
(AT&T)	C	MOHE		0.0000	70.70	No Ice 1/2" Ice	25.00	25.00	800.00
(******)						1/2" Ice 1" Ice	37.00 47.00	37.00 47.00	1100.0 1500.0

Structural Components, LLC 1870 West 64th Lane, Unit A

Denver, CO 80221
Phone: (866) 386-7622
FAX:

Job	240022 REV 1	Page 18 of 32
Project	Portland (CT-1680)	Date 15:03:20 02/13/24
Client	BST Management, LLC	Designed by treed

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	C₄A₄ Side	Weight
			Vert ft ft	0	ft		ft²	ft²	lb
***									
Ring Mount	С	None		0.0000	75.00	No Ice	6.87	6.87	850.00
						1/2" Ice	8.25	8.25	1020.0
						1" Ice	9.62	9.62	1190.0
***									
2-3/8" x 8' Pipe Mount	Α	From Leg	0.00	0.0000	73.00	No Ice	1.90	1.90	30.00
20,0 1.0 1.4		ū	0.00			1/2" Ice	2.73	2.73	44.37
			0.00			1" Ice	3.40	3.40	64.01
***									
Ring Mount	С	None		0.0000	67.70	No Ice	6.87	6.87	850.00
King wount	·	110110				1/2" Ice	8.25	8.25	1020.0
						1" Ice	9.62	9.62	1190.0

#### **Force Totals**

Load Case	Vertical Forces	Sum of Forces X lb	Sum of Forces Z lb	Sum of Overturning Moments, M <sub>x</sub> lb-ft	Sum of Overturning Moments, M <sub>z</sub> lb-ft	Sum of Torques  lb-ft
Leg Weight	3728.23					
Bracing Weight	5215.45					
Total Member Self-Weight	8943.69			-2924.94	-1888.15	
Gusset Weight	111.27		A 4 A 4			
Total Weight	18136.42			-2924.94	-1888.15	
Wind 0 deg - No Ice		-172.29	-19042.55	-1086249.57	11413.26	517.48
Wind 45 deg - No Ice		15562.18	-15546.55	-857381.49	-857331.29	2979.08
Wind 90 deg - No Ice		20506.37	172.29	10376.47	-1144248.41	-3616.04
Wind 135 deg - No Ice		15805.84	15790.21	870342.64	-876142.33	-7152.66
Wind 180 deg - No Ice		172.29	19042.55	1080399.69	-15189.56	-517.48
Wind 225 deg - No Ice		-15562.18	15546.55	851531.60	853554.99	-2979.08
Wind 270 deg - No Ice		-20506.37	-172.29	-16226.35	1140472.10	3616.04
Wind 315 deg - No Ice		-15805.84	-15790.21	-876192.52	872366.02	7152.66
Member Ice	11293.92					
Gusset Ice	118.44					
Total Weight Ice	40193.86			-3858.81	-11706.05	
Wind 0 deg - Ice		-30.31	-4705.11	-273613.25	-9365.10	1535.40
Wind 45 deg - Ice	7	3820.71	-3817.93	-214601.56	-222621.10	1968.23
Wind 90 deg - Ice		5144.73	30.31	-1517.86	-298208.14	-253.89
Wind 135 deg - Ice		3863.57	3860.79	210194.55	-225931.70	-2039.96
Wind 180 deg - Ice		30.31	4705.11	265895.64	-14047.00	-1535.40
Wind 225 deg - Ice		-3820.71	3817.93	206883.95	199209.00	-1968.23
Wind 270 deg - Ice		-5144.73	-30,31	-6199.75	274796.04	253.89
Wind 315 deg - Ice		-3863.57	-3860.79	-217912,16	202519.60	2039.96
Total Weight	18136.42			-2924.94	-1888.15	
Wind 0 deg - Service		-43.07	-4760.64	-275534.50	6802.58	129.37
Wind 45 deg - Service		3890.55	-3886.64	-218317.48	-210383.55	744.77
Wind 90 deg - Service		5126.59	43.07	-1377.99	-282112.83	-904.01
Wind 135 deg - Service	4.1	3951.46	3947.55	213613.55	-215086.31	-1788.16
Wind 180 deg - Service		43.07	4760.64	266127.81	151.88	-129.37
Wind 225 deg - Service		-3890.55	3886.64	208910.79	217338.02	-744.77
Wind 270 deg - Service		-5126.59	-43.07	-8028.70	289067.30	904.01

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Load	Vertical	Sum of	Sum of	Sum of	Sum of	Sum of Torques
Case	Forces	Forces	Forces	Overturning	Overturning	
		X	$\boldsymbol{z}$	Moments, $M_x$	Moments, Mz	
	lb	lb	lb l	lb-ft	lb-ft	lb-ft
Wind 315 deg - Service		-3951.46	-3947.55	-223020.24	222040.78	1788.16

#### **Load Combinations**

Comb.	Description	
No.		
1	Dead Only	
2	1.2 Dead+1.0 Wind 0 deg - No Ice	
3	0.9 Dead+1.0 Wind 0 deg - No Ice	
4	1.2 Dead+1.0 Wind 45 deg - No Ice	
5	0.9 Dead+1.0 Wind 45 deg - No Ice	
6	1.2 Dead+1.0 Wind 90 deg - No Ice	
7	0.9 Dead+1.0 Wind 90 deg - No Ice	
8	1.2 Dead+1.0 Wind 135 deg - No Ice	
9	0.9 Dead+1.0 Wind 135 deg - No Ice	
10	1.2 Dead+1.0 Wind 180 deg - No Ice	
11	0.9 Dead+1.0 Wind 180 deg - No Ice	
12	1.2 Dead+1.0 Wind 225 deg - No Ice	
13	0.9 Dead+1.0 Wind 225 deg - No Ice	
14	1.2 Dead+1.0 Wind 270 deg - No Ice	
15	0.9 Dead+1.0 Wind 270 deg - No Ice	
16	1.2 Dead+1.0 Wind 315 deg - No Ice	
17	0.9 Dead+1.0 Wind 315 deg - No Ice	
18	1.2 Dead+1.0 Ice+1.0 Temp	
19	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	
20	1.2 Dead+1.0 Wind 45 deg+1.0 Ice+1.0 Temp	
21	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	
22	1.2 Dead+1.0 Wind 135 deg+1.0 Ice+1.0 Temp	
23	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	
24	1.2 Dead+1.0 Wind 225 deg+1.0 Ice+1.0 Temp	
25	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	
26	1.2 Dead+1.0 Wind 315 deg+1.0 Ice+1.0 Temp	
27	Dead+Wind 0 deg - Service	
28	Dead+Wind 45 deg - Service	
29	Dead+Wind 90 deg - Service	
30	Dead+Wind 135 deg - Service	
31	Dead+Wind 180 deg - Service	
32	Dead+Wind 225 deg - Service	
33	Dead+Wind 270 deg - Service	
34	Dead+Wind 315 deg - Service	

# **Maximum Reactions**

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, 2
		Load	lb	lb	lb
		Comb.			
Leg D	Max. Vert	12	70615.66	8774.93	-8669.13
	Max. H <sub>x</sub>	12	70615.66	8774.93	-8669.13
	$Max. H_z$	5	-61480.32	-7599.19	7480.90
	Min. Vert	5	-61480.32	-7599.19	7480.90
	Min. H <sub>x</sub>	5	-61480.32	-7599.19	7480.90
	Min. H <sub>2</sub>	12	70615.66	8774.93	-8669.13
Leg C	Max. Vert	8	72226.67	-8734.40	-9036.86

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Location	Condition	Gov. Load	Vertical lb	Horizontal, X lb	Horizontal, 2 lb
		Comb.			
	Max. Hx	17	-62788.26	7558.67	7811.76
	Max. H <sub>z</sub>	17	-62788.26	7558.67	7811.76
	Min. Vert	17	-62788.26	7558.67	7811.76
	Min. H.	8	72226.67	-8734.40	-9036.86
	Min. Hz	8	72226.67	-8734.40	-9036.86
Leg B	Max. Vert	4	71057.13	-8696.43	8804.04
	Max. H <sub>x</sub>	13	-61149.22	7458.83	-7578.95
	Max. H.	4	71057.13	-8696.43	8804.04
	Min. Vert	13	-61149.22	7458.83	-7578.95
	Min. H.	4	71057.13	-8696.43	8804.04
	Min. H.	13	-61149.22	7458.83	-7578.95
Leg A	Max. Vert	16	72321.76	9043.10	8742.46
Lega	Max. H.	16	72321.76	9043.10	8742.46
	Max. H	16	72321.76	9043.10	8742.46
	Min. Vert	9	-62716.93	-7805.49	-7554.22
	Min. H.	9	-62716.93	-7805.49	-7554.22
	Min. H <sub>z</sub>	9	-62716.93	-7805.49	-7554.22

### **Tower Mast Reaction Summary**

Load Combination	Vertical	$Shear_x$	Shearz	Overturning Moment, M <sub>z</sub>	Overturning Moment, M <sub>2</sub>	Torque
Comomanos	lb	lb	lb	lb-ft	lb-ft	lb-ft
Dead Only	18136.42	0.00	0.00	-2924.94	-1888.15	0.00
1.2 Dead+1.0 Wind 0 deg - No	21763.70	-172.29	-19042.55	-1087357.37	11035.62	517.48
Ice						#1 # 40
0.9 Dead+1.0 Wind 0 deg - No	16322.78	-172.29	-19042.55	-1086479.89	11602.07	517.48
Ice				0.50.50.5.50	050005.05	2070.00
1.2 Dead+1.0 Wind 45 deg - No	21763.70	15562.18	-15546.56	-858585.52	-858327.97	2979.08
Ice			15546.56	0.57700.04	-857761.53	2979.08
0.9 Dead+1.0 Wind 45 deg - No	16322.78	15562.18	-15546.56	-857708.04	-65//01.55	2919.00
Ice		20506 25	172,29	9791.48	-1145394.65	-3616.03
1.2 Dead+1.0 Wind 90 deg - No	21763.70	20506.37	1/2.29	7/71.40	-11-555-105	-5010.05
Ice	1/222 70	20506.37	172.29	10668.96	-1144828.21	-3616.03
0.9 Dead+1.0 Wind 90 deg - No	16322.78	20300.37	112.23	10000.70	1111020.21	• • • • • • • • • • • • • • • • • • • •
Ice	21763.70	15805.84	15790.21	870376.70	-877139.01	-7152.65
1.2 Dead+1.0 Wind 135 deg -	21703.70	13003.04	15770.21	0,02.0		
No Ice 0.9 Dead+1.0 Wind 135 deg -	16322.78	15805.84	15790.21	871254.18	-876572.56	-7152.65
No Ice	10322.70	15005101				
1.2 Dead+1.0 Wind 180 deg -	21763.70	172.29	19042.55	1080337.52	-15567.19	-517.48
No Ice	21.000.0					
0.9 Dead+1.0 Wind 180 deg -	16322.78	172.29	19042.55	1081215.00	-15000.75	-517.48
No Ice						
1.2 Dead+1.0 Wind 225 deg -	21763.70	-15562.18	15546.56	851565.67	853796.40	-2979.08
No Ice						#0#0 OF
0.9 Dead+1.0 Wind 225 deg -	16322.78	-15562.18	15546.56	852443.15	854362.85	-2979.08
No Ice				4 604 4 4 4	*140067.00	2616.02
1.2 Dead+1.0 Wind 270 deg -	21763.70	-20506.37	-172.29	-16811.33	1140863.08	3616.03
No Ice			150.00	15022.05	1141429.53	3616.03
0.9 Dead+1.0 Wind 270 deg -	16322.78	-20506.37	-172.29	-15933.85	1141429.33	3010.03
No Ice		15005.04	15700 01	-877396.55	872607.44	7152.65
1.2 Dead+1.0 Wind 315 deg -	21763.70	-15805.84	-15790.21	-011370.33	0/200/.44	,152.05
No Ice	1/202 50	15005 04	-15790.21	-876519.07	873173.88	7152.65
0.9 Dead+1.0 Wind 315 deg -	16322.78	-15805.84	-13/30.21	-6/0513.07	0/51/5.00	. 102.00
No Ice	43660.02	0.00	0.00	-4443.79	-12083.68	0.00
1.2 Dead+1.0 Ice+1.0 Temp	43000.02	0.00	0.00			

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Load Combination	Vertical	Shearz	Shear <sub>z</sub>	Overturning Moment, M <sub>z</sub>	Overturning Moment, M.	Torque
	lb	lb	lЬ	lb-ft	lb-ft	lb-ft
1.2 Dead+1.0 Wind 0 deg+1.0	43660.02	-30.31	-4705.11	-274381.69	-9742.73	1535.40
Ice+1.0 Temp						
1.2 Dead+1.0 Wind 45 deg+1.0	43660.02	3820.71	-3817.93	-215359.52	-223171.71	1968.23
Ice+1.0 Temp						.,,,,,,,
1.2 Dead+1.0 Wind 90 deg+1.0	43660.02	5144.73	30.31	-2102.84	-298849.06	-253.89
Ice+1.0 Temp						
1.2 Dead+1.0 Wind 135	43660.02	3863.57	3860.80	209782.55	-226482.31	-2039.96
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 180	43660.02	30.31	4705.12	265494.11	-14424.63	-1535.39
deg+1.0 Ice+1.0 Temp					4.12.100	1000.03
1.2 Dead+1.0 Wind 225	43660.02	-3820.71	3817.93	206471.95	199004.35	-1968.23
deg+1.0 Ice+1.0 Temp						1700.25
1.2 Dead+1.0 Wind 270	43660.02	-5144.73	-30.31	-6784.74	274681.70	253.89
deg+1.0 Ice+1.0 Temp						253.03
1.2 Dead+1.0 Wind 315	43660.02	-3863.57	-3860.80	-218670.13	202314.95	2039.97
deg+1.0 Ice+1.0 Temp						2005.57
Dead+Wind 0 deg - Service	18136.42	-43.07	-4760.64	-273886.80	1437.20	129.37
Dead+Wind 45 deg - Service	18136.42	3890.55	-3886.64	-216693.84	-215903.70	744.77
Dead+Wind 90 deg - Service	18136.42	5126.59	43.07	400.41	-287670.37	-904.01
Dead+Wind 135 deg - Service	18136.42	3951.46	3947.55	215546.72	-220606.46	-1788.16
Dead+Wind 180 deg - Service	18136.42	43.07	4760.64	268036.92	-5213.51	-129.37
Dead+Wind 225 deg - Service	18136.42	-3890.55	3886.64	210843.96	212127.39	-744.77
Dead+Wind 270 deg - Service	18136.42	-5126.59	-43.07	-6250.29	283894.06	904.01
Dead+Wind 315 deg - Service	18136.42	-3951.46	-3947.55	-221396.59	216830.15	1788.16

### **Solution Summary**

		n of Applied Force.	5		Sum of Reaction	ıs	
Load	PX	PY	PZ	PX	$\dot{P}Y$	PZ	% Erro
Comb.	lb	<i>lb</i>	lb	<i>lb</i>	lь	lb	
1	0.00	-18136.42	0.00	-0.00	18136.42	-0.00	0.000%
2	-172.29	-21763.70	-19042.55	172.29	21763.70	19042.55	0.000%
3	-172.29	-16322.78	-19042.55	172.29	16322.78	19042,55	0.000%
4	15562.18	-21763.70	-15546.55	-15562.18	21763.70	15546.56	0.000%
5	15562.18	-16322.78	-15546.55	-15562.18	16322.78	15546.56	0.000%
6	20506.37	-21763.70	172.29	-20506.37	21763.70	-172.29	0.000%
7	20506.37	-16322.78	172.29	-20506.37	16322.78	-172.29	0.000%
8	15805.84	-21763.70	15790.21	-15805.84	21763.70	-15790.21	0.000%
9	15805.84	-16322.78	15790.21	-15805.84	16322.78	-15790.21	0.000%
10	172.29	-21763.70	19042.55	-172.29	21763.70	-19042.55	0.000%
11	172.29	-16322.78	19042.55	-172.29	16322.78	-19042.55	0.000%
12	-15562.18	-21763.70	15546.55	15562.18	21763.70	-15546.56	0.000%
13	-15562.18	-16322.78	15546.55	15562.18	16322.78	-15546.56	0.000%
14	-20506.37	-21763.70	-172.29	20506.37	21763.70	172.29	0.000%
15	-20506.37	-16322.78	-172.29	20506.37	16322.78	172.29	0.000%
16	-15805.84	-21763.70	-15790.21	15805.84	21763.70	15790.21	0.000%
17	-15805.84	-16322.78	-15790.21	15805.84	16322.78	15790.21	0.000%
18	0.00	-43660.02	0.00	-0.00	43660.02	-0.00	0.000%
19	-30.31	-43660.02	-4705.11	30.31	43660.02	4705.11	0.000%
20	3820.71	-43660.02	-3817,93	-3820.71	43660.02	3817.93	0.000%
21	5144.73	-43660.02	30.31	-5144.73	43660.02	-30.31	0.000%
22	3863.57	-43660.02	3860.79	-3863.57	43660.02	-3860.80	0.000%
23	30.31	-43660.02	4705.11	-30.31	43660.02	-4705.12	0.000%
24	-3820.71	-43660.02	3817.93	3820,71	43660.02	-3817.93	0.000%
25	-5144.73	-43660.02	-30.31	5144.73	43660.02	30.31	0.000%
26	-3863.57	-43660.02	-3860.79	3863.57	43660.02	3860.80	0.000%
27	-43.07	-18136.42	-4760.64	43.07	18136.42	4760.64	0.000%
28	3890.55	-18136.42	-3886.64	-3890.55	18136.42	3886.64	0.000%

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	Su	m of Applied Forces			Sum of Reaction	S		
Load	PX	PY	PZ	PX	PΥ	PZ	% Error	
Comb.	lb	lb	lb	lb	lb	lb		
29	5126.59	-18136.42	43.07	-5126.59	18136.42	-43.07	0.000%	
30	3951.46	-18136.42	3947.55	-3951.46	18136.42	-3947.55	0.000%	
31	43.07	-18136.42	4760.64	-43.07	18136.42	-4760.64	0.000%	
32	-3890.55	-18136.42	3886.64	3890.55	18136.42	-3886.64	0.000%	
33	-5126.59	-18136.42	-43.07	5126.59	18136.42	43.07	0.000%	
34	-3951.46	-18136.42	-3947,55	3951.46	18136.42	3947.55	0.000%	

# **Maximum Tower Deflections - Service Wind**

Section No.	Elevation	Horz. Deflection	Gov. Load	Tilt	Twist
110.	ft	in	Comb.	0	۰
T1	90.333 - 78.063	0.957	34	0.0843	0.0089
T2	78.063 - 74.563	0.741	34	0.0806	0.0076
T3	74.563 - 72.313	0.680	34	0.0789	0.0070
T4	72.313 - 67.563	0.641	34	0.0777	0.0065
T5	67.563 - 65.438	0.557	34	0.0732	0.0051
T6	65,438 - 57,521	0.523	34	0.0711	0.0046
T7	57.521 - 50.271	0.407	34	0.0613	0.0029
T8	50.271 - 41.979	0.315	34	0.0528	0.0021
Т9	41.979 - 34.187	0.226	34	0.0442	0.0014
T10	34.187 - 26.895	0.154	34	0.0368	0.0010
T11	26.895 - 20.103	0.099	34	0.0292	0.0007
T12	20.103 - 13.415	0.057	34	0.0229	0.0005
T13	13.415 - 6.7075	0.026	34	0.0139	0.0002
T14	6.7075 - 0	0.003	32	0.0073	0.0001

# Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
	**	Load				Curvature
ft		Comb.	in	•	0	ft
90.50	6' x 5/8" Lighting Rod	34	0.957	0.0843	0.0089	308829
90.00	NNH4-65B-R6	34	0.952	0.0842	0.0088	308829
77.00	Ring Mount	34	0.723	0.0801	0.0074	155277
76.70	RRUS-32 (Full Frontal Shielding)	34	0.717	0.0800	0.0074	149561
75.00	Ring Mount	34	0.687	0.0791	0.0070	240664
73.00	2-3/8" x 8' Pipe Mount	34	0.653	0.0781	0.0067	138726
67.70	Ring Mount	34	0.560	0.0733	0.0051	29893

# **Maximum Tower Deflections - Design Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.	ft	Deflection in	Load Comb.	0	•
T1	90.333 - 78.063	3.746	16	0.3215	0.0354
T2	78.063 - 74.563	2.918	16	0.3108	0.0305
T3	74.563 - 72.313	2.680	16	0.3048	0.0279

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Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	۰
T4	72.313 - 67.563	2.530	16	0.3008	0.0261
T5	67.563 - 65.438	2.204	16	0.2845	0.0204
T6	65.438 - 57.521	2.070	16	0.2771	0.0185
T7	57.521 - 50.271	1.615	16	0.2405	0.0118
T8	50.271 - 41.979	1.254	16	0.2081	0.0083
T9	41.979 - 34.187	0.898	16	0.1749	0.0055
T10	34.187 - 26.895	0.614	16	0.1458	0.0041
T11	26.895 - 20.103	0.394	16	0.1160	0.0029
T12	20.103 - 13.415	0.227	16	0.0910	0.0019
T13	13.415 - 6.7075	0.105	16	0.0552	0.0010
T14	6.7075 - 0	0.012	8	0.0290	0.0005

### Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature	
ft		Comb.	in	0	0	ft	
90.50	6' x 5/8" Lighting Rod	16	3.746	0.3215	0.0354	91386	
90.00	NNH4-65B-R6	16	3.724	0.3213	0.0353	91386	
77.00	Ring Mount	16	2.845	0.3090	0.0297	56067	
76.70	RRUS-32 (Full Frontal Shielding)	16	2.824	0.3084	0.0295	53474	
75.00	Ring Mount	16	2.709	0.3055	0.0282	102187	
73.00	2-3/8" x 8' Pipe Mount	16	2.576	0.3023	0.0267	40775	
67.70	Ring Mount	16	2.213	0.2850	0.0206	8142	

#### **Bolt Design Data**

Section No.	Elevation	Component Type	Bolt Grade	Bolt Size	Number Of	Maximum Load	Allowable Load	Ratio Load	Allowable Ratio	Criteria
	ft			in	Bolts	per Bolt lb	per Bolt lb	Allowabl	_	
<b>T</b> 1	90.333	Leg	A307	0.6250	12	855.83	16240.00	0.053	1	Bearing
		Diagonal	A325N	0.6240	1	1649.75	9492.94	0.174	1	Member Block Shear
		Top Girt	A325N	0.6250	1	102.68	8482.50	0.012	1	Member Bearing
T2	78.063	Diagonal	A325N	0.5410	2	1458.29	5577.24	0.261	1	Member Block Shear
		Top Girt	A325N	0.6250	2	365.57	11010.90	0.033	1	Member Block Shear
Т3	74.563	Diagonal	A325N	0.5410	2	1670.60	7208.49	0.232	1	Member Block Shear
		Horizontal	A325N	0.6250	3	292.52	10059.40	0.029	1	Member Block Shear
T4	72.313	Diagonal	A325N	0.5410	2	2612.11	7208.49	0.362	1	Member Block Shear
		Top Girt	A325N	0.6250	3	615.88	15080.00	0.041	1	Gusset Bearing
T5	67.563	Diagonal	A325N	0.5410	2	2008.95	5577.24	0.360	1	Member Block Shear
		Horizontal	A325N	0.6250	3	163.77	10059.40	0.016	1	Member Block Shear

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Section No.	Elevation	Component Type	Bolt Grade	Bolt Size	Number Of	Maximum Load	Allowable Load	Rat Loc	ıd	Allowable Ratio	Criteria
	ft			in	Bolts	per Bolt lb	per Bolt lb	Allow	able		
Т6	65.438	Diagonal	A325N	0.5410	2	1629.94	6188.96	0.263	1	1	Member Block Shear
<b>T7</b>	57.521	Diagonal	A325N	0.5410	2	1482.09	6188.96	0.239	/	1	Member Block Shear
Т8	50.271	Leg	A307	0.6250	12	6951.14	17257.30	0.403	1	1	Bolt DS
		Diagonal	A325N	0.5410	2	1379.33	6188.96	0.223		1	Member Block Shear
		Top Girt	A325N	0.6250	3	208.93	6728.91	0.031	/	1	Member Block Shear
Т9	41.979	Diagonal	A325N	0.5410	2	1408.66	6188.96	0.228	/	1	Member Block Shear
T10	34.187	Diagonal	A325N	0.5410	2	1260.12	6188.96	0.204	1	1	Member Block Shear
T11	26.895	Diagonal	A325N	0.5410	2	1329.08	6188.96	0.215	/	1	Member Block Shear
T12	20.103	Leg	A307	0.6250	12	10821.20	17257.30	0.627	1	1	Bolt DS
		Diagonal	A325N	0.5410	2	2347.68	7208.49	0.326	1	1	Member Block Shear
		Top Girt	A325N	0.6250	1	1921.33	9487.50	0.203	/	1	Member Block Shear
T13	13.415	Diagonal	A325N	0.5410	2	3370.88	10344.20	0.326	V	1	Bolt Shear
		Redund Horz 1 Bracing	A325N	0.5000	1	936.75	5709.38	0.164	/	1	Member Block Shear
		Redund Diag 1	A325N	0.5000	1	721.67	5709.38	0.126	/	1	Member Block Shear
T14	6.7075	Bracing Diagonal	A325N	0.5410	2	3496.98	10344.20	0.338	1	1	Bolt Shear
		Horizontal	A325N	0.6250	1	943.41	6096.09	0.155	1	1	Member Block Shear
		Redund Horz 1	A325N	0.5000	1	943.41	5709.38	0.165	1	1	Member Block Shear
		Bracing Redund Diag 1 Bracing	A325N	0.5000	1	679.00	5709.38	0.119	-	1	Member Block Shear

#### **Compression Checks**

### Leg Design Data (Compression)

Section No.	Elevation	Size	L	$L_{\scriptscriptstyle \sf U}$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
110.	ft		ft	ft		in <sup>2</sup>	lb	lb	φ <i>P</i> ,
Tl	90.333 - 78.063	L4x4x1/4	12.27	6.08	91.8 K=1.00	1.9400	-5135.01	50194.10	0.102
T2	78.063 - 74.563	L4x4x3/8	3.50	3.50	53.3 K=1.00	2.8600	-11070.20	93762.70	0.118 1
T3	74.563 - 72.313	L4x4x3/8	2.25	2.25	34.3 K=1.00	2.8600	-11133.20	99159.10	0.112 1
T4	72.313 - 67.563	L4x4x3/8	4.75	4.75	72.3 K=1.00	2.8600	-20249.50	86020.10	0.235 1
T5	67.563 -	L4x4x3/8	2.13	0.13	1.9	2.8600	-26119.10	102948.00	0.254 1

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Section No.	Elevation	Size	L	$L_{u}$	Kl/r	A	$P_u$	$\phi P_n$	Ratio Pu
	ft		ft	ft		$in^2$	lb	lb	φP <sub>n</sub>
	65.438				K=1.00				1
Т6	65.438 - 57.521	L4x4x3/8	7.95	7.95	121.0 K=1.00	2.8600	-29068.70	55545.30	0.523
<b>T7</b>	57.521 - 50.271	L4x4x3/8	7.28	7.28	110.8 K=1.00	2.8600	-36797.90	63198.00	0.582
Т8	50.271 - 41.979	L5x5x3/8	8.32	8.32	100.9 K=1.00	3.6100	-41706.80	88365.70	0.472
Т9	41.979 - 34.187	L5x5x3/8	7.82	7.82	94.8 K=1.00	3.6100	-48551.40	93230.70	0.521
T10	34.187 - 26.895	L5x5x3/8	7.32	7.32	88.7 K=1.00	3.6100	-53268.70	97793.20	0.545
T11	26.895 - 20.103	L5x5x3/8	6.82	6.82	82.6 K=1.00	3.6100	-57637.10	102053.00	0.565
T12	20.103 - 13.415	L5x5x5/16	6.71	6.71	81.0 K=1.00	3.0300	-64926.90	84358.10	0.770 1
T13	13.415 - 6.7075	L5x5x5/16	6.73	3.37	40.6 K=1.00	3.0300	-62333.40	100100.00	0.623 1
T14	6.7075 - 0	L5x5x5/16	6.73	3.37	40.6 K=1.00	3.0300	-62776.00	100100.00	0.627 1

 $<sup>^{1}</sup>P_{u}$  /  $\phi P_{n}$  controls

# **Diagonal Design Data (Compression)**

Section No.	Elevation	Size	L	$L_{u}$	KI/r	A	$P_u$	фР"	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	lb	lb	φP,
Tl	90.333 - 78.063	L2x2x1/4	7.90	3.69	113.2 K=1.00	0.9380	-1674.43	20156.50	0.083 1
T2	78.063 - 74.563	L2x2 1/2x3/16	4.31	4.03	113.2 K=1.00	0.8090	-3382.03	17388.40	0.194 1
Т3	74.563 - 72.313	L2 1/2x2 1/2x3/16	3.38	3.16	76.5 K=1.00	0.9020	-3996.79	26497.00	0.151 1
T4	72.313 - 67.563	L2 1/2x2 1/2x3/16	5.38	5.02	121.7 K=1.00	0.9020	-5812.34	17338.40	0.335 1
T5	67.563 - 65.438	L2x2x3/16	3.22	3.01	91.5 K=1.00	0.7150	-4908.30	18959.90	0.259 1
Т6	65.438 - 57.521	L2x2 1/2x3/16	9.67	4.97	139.7 K=1.00	0.8090	-3514.52	11872.90	0.296 1
Т7	57.521 - 50.271	L2x2 1/2x3/16	9.72	4.95	139.0 K=1.00	0.8090	-2841.76	11987.10	0.237 1
Т8	50.271 - 41.979	L2x2 1/2x3/16	11.14	5.64	158.5 K=1.00	0.8090	-2919.84	9221.79	0.317 1
<b>T</b> 9	41.979 - 34.187	L2x2 1/2x3/16	11.47	5.78	162.4 K=1.00	0.8090	-2751.95	8781.19	0.313 1
T10	34.187 - 26.895	L2x2 1/2x3/16	11.85	5.95	167.1 K=1.00	0.8090	-2593.84	8293.25	0.313 1
T11	26.895 - 20.103	L2x2 1/2x3/16	12.26	6.13	172.3 K=1.00	0.8090	-2669.41	7801.97	0.342 1

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Elevation	Size	L	$L_{\scriptscriptstyle \sf u}$	Kl/r	A	Pu	$\phi P_n$	Ratio Pu
ft		ft	ft		$in^2$	lb	lЬ	$\phi P_n$
20.103 - 13.415	L2 1/2x2 1/2x3/16	12.90	6.45	156.3 K=1.00	0.9020	-4092.55	10566.60	0.387
13.415 - 6.7075	L3x3x5/16	8.82	8.50	110.7 K=1.00	1.7800	-6741.75	39401.70	0.171 1
6.7075 - 0	L3x3x5/16	9.38	9.08	118.2 K=1.00	1.7800	-6993.96	35938.10	0.195 1
	ft 20.103 - 13.415 13.415 - 6.7075	ft  20.103 - L2 1/2x2 1/2x3/16 13.415 13.415 - L3x3x5/16 6.7075	ft ft 20.103 - L2 1/2x2 1/2x3/16 12.90 13.415 13.415 - L3x3x5/16 8.82 6.7075	ft ft ft  20.103 - L2 1/2x2 1/2x3/16 12.90 6.45 13.415 13.415 - L3x3x5/16 8.82 8.50 6.7075	ft         ft         ft         ft           20.103 - 13.415         L2 1/2x2 1/2x3/16         12.90         6.45         156.3 K=1.00           13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415 - 13.415	ft         ft         ft         ft         in²           20.103 - 13.415         L2 1/2x2 1/2x3/16         12.90         6.45         156.3 0.9020           13.415 - 13.415 - 13.415 - 6.7075         L3x3x5/16         8.82         8.50 110.7 1.7800           6.7075 - 0         L3x3x5/16         9.38 9.08 118.2 1.7800	ft         ft         ft         ft         in²         lb           20.103 - 13.415         12.90         6.45         156.3 0.9020 -4092.55         -4092.55           13.415 - 13.415 - 6.7075         13.415 - 13.83x5/16         8.82 8.50 110.7 1.7800 -6741.75         1.7800 -6741.75           6.7075 - 0         13.83x5/16         9.38 9.08 118.2 1.7800 -6993.96	ft         ft         ft         ft         in²         lb         lb           20.103 - 13.415         L2 1/2x2 1/2x3/16         12.90         6.45         156.3 0.9020         -4092.55         10566.60           13.415 - 13.415 - 6.7075         L3x3x5/16         8.82         8.50         110.7 1.7800         -6741.75         39401.70           6.7075 - 0         L3x3x5/16         9.38         9.08         118.2         1.7800         -6993.96         35938.10

 $<sup>{}^{1}</sup>P_{\mu}/\phi P_{n}$  controls

		Horizor	ntal De	sign	Data (	Comp	ressio	ר)	
Section No.	Elevation	Size	L	Lu	Kl/r	A	P <sub>u</sub>	$\phi P_n$	Ratio Pu
140.	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
Т3	74.563 - 72.313	L4x3 1/2x1/4	5.04	3.53	39.4 K=1.00	1.8100	-884.12	59980.20	0.015
T5	67.563 - 65.438	L4x3 1/2x1/4	5.04	3.53	39.4 K=1.00	1.8100	-487.75	59980.20	0.008 1
T14	6.7075 - 0	L1 3/4x1 3/4x3/16	12.26	5.92	206.9	0.6211	-943.41	4152.93	0.227 1

K=1.00

KL/R > 200 (C) - 219

T14

6.7075 - 0

Section No.	Elevation	Size	L	$L_{\scriptscriptstyle M}$	K1/r	A	$P_{u}$	$\phi P_n$	Ratio P <sub>u</sub>
140.	ft		ft	ft		$in^2$	lb	lb	$\phi P_n$
T1	90.333 - 78.063	L2 1/2x2 1/2x3/16	5.04	4.71	114.1 K=1.00	0.9020	-124.40	19169.70	0.006
T2	78.063 - 74.563	L4x3 1/2x1/4	5.04	3.53	57.7 K=1.00	1.8100	-537.54	56580.10	0.010 1
T4	72.313 - 67.563	2L4x4x3/8	5.04	4.71	45.9 K=1.00	5.7200	-1208.11	187393.00	0.006 1
T8	50.271 - 41.979	L2 1/2x2 1/2x3/16	6.91	6.49	157.3 K=1.00	0.9020	-626.78	10431.90	0.060 1
T12	20.103 - 13.415	L2x2 1/2x1/4	10.61	10.20	288.6 K=1.00	1.0600	-2264.09	3642.36	0.622
		KL/R > 200 (C) - 190							

 $<sup>^{1}</sup>P_{\mu}/\phi P_{n}$  controls

#### **Bottom Girt Design Data (Compression)**

 $<sup>^{1}</sup>P_{u}$  /  $\phi P_{n}$  controls

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Section No.	Elevation	Size	L	$L_{\scriptscriptstylel}$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P.,
	ft		ft	ft		in²	lb	lb	$\phi P_n$
T5	67.563 - 65.438	L3x3x3/16	5.04	3.53	71.1 K=1.00	1.0900	-957.91	32089.70	0.030 1

 $<sup>{}^{1}</sup>P_{u}/\phi P_{n}$  controls

Redundant Horizontal	(1)	Design Data	(Compression)
			( C C I I I C C C I C I I

Section No.	Elevation	Size	L	$L_{u}$	Kl/r	A	$P_{u}$	φ <i>P</i> ,,	Ratio Pu
	ft		ft	ft		in <sup>2</sup>	lb	lb	$\phi P_{\pi}$
T13	13.415 - 6.7075	L1 3/4x1 3/4x3/16	3.06	2.86	99.8 K=1.00	0.6211	-936.75	15355.50	0.061
T14	6.7075 - 0	L1 3/4x1 3/4x3/16	3.06	2.86	99.8 K=1.00	0.6211	-943,41	15355.50	0.061 1

 $<sup>{}^{1}</sup>P_{u}/\phi P_{n}$  controls

# Redundant Diagonal (1) Design Data (Compression)

Section No.	Elevation	Size	L	$L_{u}$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft ft		$in^2$	lb	lb	$\phi P_n$
T13	13.415 - 6.7075	L1 3/4x1 3/4x3/16	4.69	4.39	153.4 K=1.00	0.6211	-721.67	7552.38	0.096 1
T14	6.7075 - 0	L1 3/4x1 3/4x3/16	4.41	4.09	142.9 K=1.00	0.6211	-679.00	8699.96	0.078 1

 $<sup>^{1}</sup>$   $P_{u}$  /  $\phi P_{n}$  controls

# Inner Bracing Design Data (Compression)

Section No.	Elevation	Size	L	$L_{u}$	KI/r	A	$P_u$	$\phi P_n$	Ratio Pu
	ft		ft	ft		in <sup>2</sup>	lb	lb	$\phi P_n$
T2	78.063 - 74.563	L2 1/2x2x3/16	3.56	3.23	90.8 K=1.00	0.8090	-6.14	21570.60	0.000
T5	67.563 - 65.438	L2 1/2x2x3/16	3.56	3.23	90.8 K=1.00	0.8090	-3.59	21570.60	0.000 1
T12	20.103 - 13.415	L2x2x3/16	15.01	14.59	444.5 K=1.00	0.7150	-131.79	1035.81	0.127 1
		KL/R > 250 (C) - 187							

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# Tension Checks

	T1 41	Size	L	Lu	K]/r	A	Pu	φP <sub>n</sub>	Ratio
Section No.	Elevation	Size	L	Lu	III//	71	- u	Ψ2 π	$P_{\mu}$
140.	ft		ft	ft		in <sup>2</sup>	lb	lb	$\phi P_n$
<b>T</b> 1	90.333 - 78.063	L4x4x1/4	12.27	6.08	58.4	1.9400	3557.06	62856.00	0.057
T2	78.063 - 74.563	L4x4x3/8	3.50	3.50	34.1	2.8600	7901.13	92664.00	0.085
T3	74.563 - 72.313	L4x4x3/8	2.25	2.25	22.0	2.8600	7262.08	92664.00	0.078
T4	72.313 - 67.563	L4x4x3/8	4.75	4.75	46.3	2.8600	15889.80	92664.00	0.171
T5	67.563 - 65.438	L4x4x3/8	2.13	0.13	1.2	2.8600	20337.60	92664.00	0.219
Т6	65.438 - 57.521	L4x4x3/8	7.95	7.95	77.5	2.8600	23486.00	92664.00	0.253
<b>T7</b>	57.521 - 50.271	L4x4x3/8	7.28	7.28	71.0	2.8600	30413.90	92664.00	0.328
T8	50.271 - 41.979	L5x5x3/8	8.32	8.32	64.0	3.6100	35275.50	116964.00	0.302
T9	41.979 - 34.187	L5x5x3/8	7.82	7.82	60.2	3.6100	41423.30	116964.00	0.354
T10	34.187 - 26.895	L5x5x3/8	7.32	7.32	56.3	3.6100	45911.00	116964.00	0.393
<b>T</b> 11	26.895 - 20.103	L5x5x3/8	6.82	6.82	52.4	3.6100	49840.00	116964.00	0.426
T12	20.103 - 13.415	L5x5x5/16	6.71	<b>6.7</b> 1	51.3	3.0300	56030.30	98172.00	0.571
T13	13.415 - 6.7075	L5x5x5/16	6.73	3.37	25.7	3.0300	54872.90	98172.00	0.559
T14	6.7075 - 0	L5x5x5/16	6.73	3.37	25.7	3.0300	54885.80	98172.00	0.559

 $<sup>^{1}</sup>P_{u}$  /  $\phi P_{n}$  controls

		Dia	gonal [	Desig	n Dat	a (Ten	sion)		
Section No.	Elevation	Size	L	$L_{u}$	KI/r	A	$P_{\rm w}$	φ <i>P</i> ,	Ratio P <sub>u</sub>
140.	ft		ft	fì		in <sup>2</sup>	lb	lb	φР"
T1	90.333 - 78.063	L2x2x1/4	7.90	3.69	72.7	0.5631	1649.75	24493.20	0.067
T2	78.063 - 74.563	L2x2 1/2x3/16	4.31	4.03	80.6	0.5131	2916.59	22319.60	0.131

 $<sup>^{1}</sup>P_{u}$  /  $\phi P_{n}$  controls

Structural Components, LLC
1870 West 64th Lane, Unit A
Denver, CO 80221

Denver, CO 80221 Phone: (866) 386-7622 FAX:

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Section No.	Elevation	Size	L	$L_{\scriptscriptstyle \sf L}$	KUr	A	$P_u$	$\phi P_n$	Ratio P.,
	fi		ft	fi		in <sup>2</sup>	lb	lb	$\phi P_n$
T3	74.563 - 72.313	L2 1/2x2 1/2x3/16	3.38	3.16	48.7	0.5828	3341.19	25353.70	0.132
T4	72.313 - 67.563	L2 1/2x2 1/2x3/16	5.38	5.02	77.5	0.5828	5224.22	25353.70	0.206
T5	67.563 - 65.438	L2x2x3/16	3.22	3.01	58.4	0.4426	4017.89	19252.80	0.209
Т6	65.438 - 57.521	L2x2 1/2x3/16	9.67	4.97	99.4	0.5131	3259.88	22319.60	0.146
<b>T7</b>	57.521 - 50.271	L2x2 1/2x3/16	9.72	4.95	99.0	0.5131	2964.18	22319.60	0.133
T8	50.271 - 41.979	L2x2 1/2x3/16	11.14	5.64	112.8	0.5131	2758.66	22319.60	0.124
Т9	41.979 - 34.187	L2x2 1/2x3/16	11.47	5.78	115.6	0.5131	2817.32	22319.60	0.126
T10	34.187 - 26.895	L2x2 1/2x3/16	11.85	5.95	119.0	0.5131	2520.24	22319.60	0.113
T11	26.895 - 20,103	L2x2 1/2x3/16	1 <b>2.26</b>	6.13	122.7	0.5131	2658.16	22319.60	0.119
T12	20.103 - 13.415	L2 1/2x2 1/2x3/16	12.90	6.45	99.5	0.5828	4695.37	25353.70	0.185
T13	13.415 - 6.7075	L3x3x5/16	8.82	8.50	110.7	1.1789	5923.86	51282.40	0.116
T14	6.7075 - 0	L3x3x5/16	9.38	9.08	118.2	1.1789	5962.28	51282.40	0.116

 $<sup>^{1}</sup>P_{u}/\phi P_{n}$  controls

Horizontal Design Data	(Tension)
------------------------	-----------

Section No.	Elevation	Size	L	$L_{u}$	Kl/r	A	$P_{u}$	$\phi P_n$	Ratio Pu
	fi		ft	ft		$in^2$	lb	lb	φP,
Т3	74.563 - 72.313	L4x3 1/2x1/4	5.04	3.53	39.4	1.2169	877.56	52934.10	0.017
T5	67.563 - 65.438	L4x3 1/2x1/4	5.04	3.53	39.4	1.2169	491.30	52934.10	0.009 1
T14	6.7075 - 0	L1 3/4x1 3/4x3/16	12.26	5.92	198.5	0.3604	943.41	15675.30	0.060 1

 $<sup>^{1}</sup>P_{u}/\phi P_{n}$  controls

Top Girt Design Data	(Tension)
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Section No.	Elevation	Size	L	$L_{\scriptscriptstyle \sf u}$	Kl/r	A	$P_{u}$	φ <i>P</i> "	Ratio P.,
	ft		ft	ft		in <sup>2</sup>	lb	lb	$\phi P_n$
<b>T</b> 1	90.333 -	L2 1/2x2 1/2x3/16	5.04	4.71	72.6	0.5710	102.68	24839.90	0.004 1

Structural Components, LLC 1870 West 64th Lane, Unit A

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Section No.	Elevation	Size	L	$L_{\scriptscriptstyle M}$	Kl/r	A	$P_u$	$\phi P_n$	Ratio Pu
ft ft		ft	ft		in²	lb	lb	φ <i>P</i> ,	
	78.063								V
T2	78.063 - 74.563	L4x3 1/2x1/4	5.04	3.53	44.6	1.2169	731.14	52934.10	0.014 '
<b>T4</b>	72.313 - 67.563	2L4x4x3/8	5.04	<b>4.7</b> 1	45.9	3.8681	1847.63	168263.00	0.011 1
Т8	50.271 - 41.979	L2 1/2x2 1/2x3/16	<b>6.9</b> 1	6.49	100.1	0.5710	626.78	24839.90	0.025 1
T12	20.103 - 13.415	L2x2 1/2x1/4	10.61	10.20	206.6	0.6544	1921.33	28465.30	0.067

 $<sup>^{1}</sup>P_{u}/\phi P_{n}$  controls

	Bott	om Gir	t Des	<u>ign Da</u>	ta (Te	nsion)	
				vet/			LD
 F77 4*	Cinn	ī	7	K1/=	4	P	

Section No.	Elevation	Size	L	$L_{\scriptscriptstyle\sf M}$	Kl/r	A	$P_{u}$	$\phi P_n$	Ratio P <sub>u</sub>
140.	ft		ft	fi		in <sup>2</sup>	lb	lb	$\phi P_n$
T5	67.563 - 65.438	L3x3x3/16	5.04	3.53	60.2	1.0900	1207.14	35316.00	0.034 1

 $<sup>^{1}</sup>P_{u}/\phi P_{n}$  controls

# Redundant Horizontal (1) Design Data (Tension)

Section No.	Elevation	Size	L	$L_{u}$	KI/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
140.	ft		ft	ft		$in^2$	lb	lЬ	$\phi P_n$
T13	13.415 - 6.7075	L1 3/4x1 3/4x3/16	3.06	2.86	63.8	0.3779	936.75	16439.90	0.057
T14	6.7075 - 0	L1 3/4x1 3/4x3/16	3.06	2.86	63.8	0.3779	943.41	16439.90	0.057 1

 $<sup>^{1}</sup>P_{u}/\phi P_{n}$  controls

# Redundant Diagonal (1) Design Data (Tension)

Section No.	Elevation	Size	L	$L_{\mu}$	Kl/r	A	$P_u$	$\phi P_n$	Ratio Pu
140.	ft		ft	ft		in <sup>2</sup>	lb	lb	$\phi P_n$
T13	13.415 - 6.7075	L1 3/4x1 3/4x3/16	4.69	4.39	98.1	0.3779	721.67	16439.90	0.044
T14	6.7075 - 0	L1 3/4x1 3/4x3/16	4.41	4.09	91.4	0.3779	679.00	16439.90	0.041 1

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			Lu	AJ/F	А	F u	$\varphi P_n$	Ratio
7		ft	ft		in²	lb	1b	$\frac{P_u}{\Phi P}$
	f	ft	ft ft	fi fi	ft ft	ft ft ft in²	ft ft in² lb	ft ft in² lb lb

 $<sup>^{1}</sup>P_{u}/\phi P_{n}$  controls

# Inner Bracing Design Data (Tension)

Section No.	Elevation	Size	L	$L_{\nu}$	Kl/r	A	$P_{u}$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		in <sup>2</sup>	lb	lb	$\phi P_n$
T2	78.063 - 74.563	L2 1/2x2x3/16	7.13	6.80	136.0	0.8090	90.88	26211.60	0.003
T5	67.563 - 65.438	L2 1/2x2x3/16	7.13	6.80	136.0	0.8090	192.41	26211.60	0.007
Т8	50.271 - 41.979	L2 1/2x2x3/16	9.77	9.35	187.1	0.8090	29.18	26211.60	0.001
T12	20.103 - 13.415	L2x2x3/16	15.01	14.59	283.8	0.7150	202.74	23166.00	0.009

# **Section Capacity Table**

Section	Elevation	Component	Size	Critical	P	øP <sub>allow</sub>	%	Pass
No.	ft	Туре		Element	lb	lЬ	Capacity	Fail
T1	90.333 - 78.063	Leg	L4x4x1/4	4	-5135.01	50194.10	10.2	Pass
T2	78.063 - 74.563	Leg	L4x4x3/8	28	-11070.20	93762.70	11.8	Pass
T3	74.563 - 72.313	Leg	L4x4x3/8	54	-11133.20	99159.10	11.2	Pass
T4	72.313 - 67.563	Leg	L4x4x3/8	66	-20249.50	86020.10	23.5	Page
T5	67.563 - 65.438	Leg	L4x4x3/8	86	-26119.10	102948.00	25.4	Pass
T6	65.438 - 57.521	Leg	L4x4x3/8	108	-29068.70	55545.30	52.3	Pass
T7	57.521 - 50.271	Leg	L4x4x3/8	120	-36797.90	63198.00	58.2	Pass
T8	50.271 - 41.979	Leg	L5x5x3/8	132	-41706.80	88365.70	47.2	Pass
T9	41.979 - 34.187	Leg	L5x5x3/8	150	-48551.40	93230.70	52.1	Pass
T10	34.187 - 26.895	Leg	L5x5x3/8	162	-53268.70	97793.20	54.5	Pass
T11	26.895 - 20.103	Leg	L5x5x3/8	174	-57637.10	102053.00	56.5	Pass
T12	20.103 - 13.415	Leg	L5x5x5/16	186	-64926.90	84358.10	77.0	Pass
T13	13.415 - 6.7075	Leg	L5x5x5/16	204	-62333.40	100100.00	62.3	Pass
T14	6.7075 - 0	Leg	L5x5x5/16	236	-62776.00	100100.00	62.7	Pass
<b>T</b> 1	90.333 - 78.063	Diagonal	L2x2x1/4	14	-1674.43	20156.50	8.3	Pass
T2	78.063 - 74.563	Diagonal	L2x2 1/2x3/16	42	-3382.03	17388.40	19.4	Pass
T3	74.563 - 72.313	Diagonal	L2 1/2x2 1/2x3/16	60	-3996.79	26497.00	15.1	Pass
T4	72.313 - 67.563	Diagonal	L2 1/2x2 1/2x3/16	78	-5812.34	17338.40	33.5	Pass
T5	67.563 - 65.438	Diagonal	L2x2x3/16	97	-4908.30	18959.90	25.9	Pass
T6	65.438 - 57.521	Diagonal	L2x2 1/2x3/16	113	-3514.52	11872.90	29.6	Pass
<b>T</b> 7	57.521 - 50.271	Diagonal	L2x2 1/2x3/16	125	-2841.76	11987.10	23.7	Pass
T8	50.271 - 41.979	Diagonal	L2x2 1/2x3/16	143	-2919.84	9221.79	31.7	Pass
T9	41.979 - 34.187	Diagonal	L2x2 1/2x3/16	155	-2751.95	8781.19	31.3	Pass
T10	34.187 - 26.895	Diagonal	L2x2 1/2x3/16	167	-2593.84	8293.25	31.3	Pass
T11	26.895 - 20,103	Diagonal	L2x2 1/2x3/16	180	-2669.41	7801.97	34.2	Pass
T12	20.103 - 13.415	Diagonal	L2 1/2x2 1/2x3/16	197	-4092.55	10566.60	38.7	Pass

<sup>\*</sup> DL controls  ${}^{1}P_{u}$  /  $\phi P_{n}$  controls

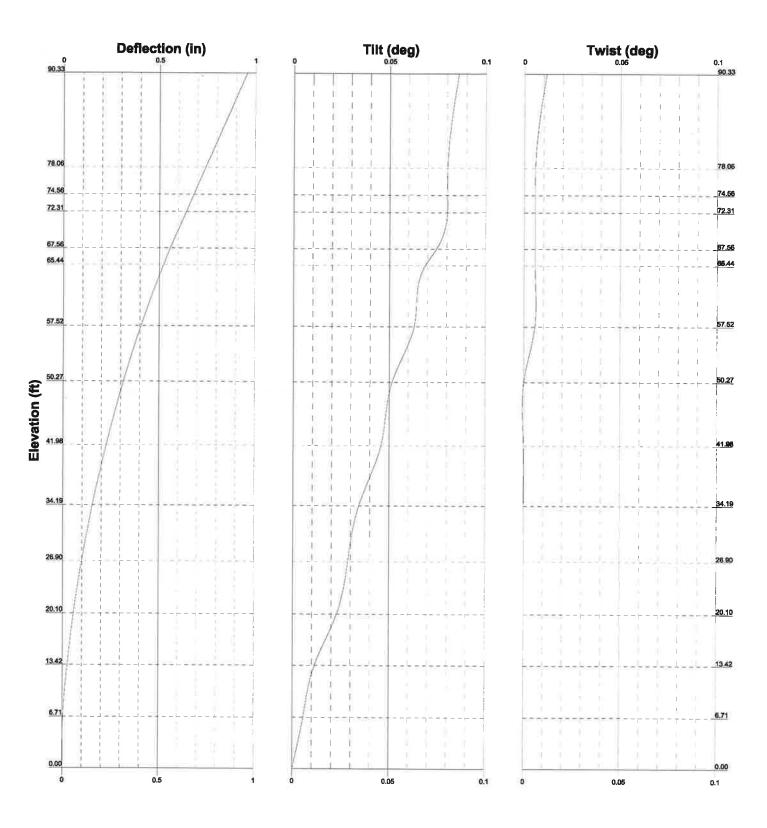
Structural Components, LLC 1870 West 64th Lane, Unit A

Denver, CO 80221
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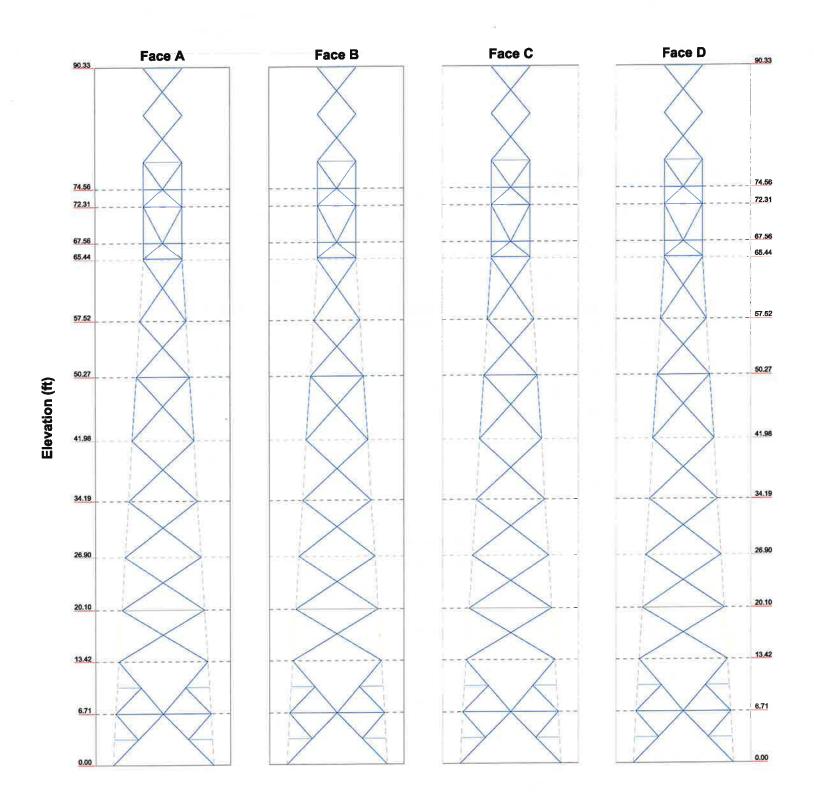
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Section	Elevation	Component	Size	Critical	P	$ olimits P_{allow} $	%	Pass
No.	ft	Туре		Element	lb	lb	Capacity	Fail
T13	13.415 - 6.7075	Diagonal	L3x3x5/16	216	-6741.75	39401.70	17.1	Pass
T14	6.7075 - 0	Diagonal	L3x3x5/16	243	-6993.96	35938.10	19.5	Pass
T3	74.563 - 72.313	Horizontal	L4x3 1/2x1/4	41	877.56	52934.10	1.7	Pass
T5	67.563 - 65.438	Horizontal	L4x3 1/2x1/4	<b>7</b> 7	491.30	52934.10	0.9	Pass
T14	6.7075 - 0	Horizontal	L1 3/4x1 3/4x3/16	219	-943.41	4152.93	22.7	Pass
T1	90.333 - 78.063	Top Girt	L2 1/2x2 1/2x3/16	5	-124.40	19169.70	0.6	Pass
T2	78.063 - 74.563	Top Girt	L4x3 1/2x1/4	33	731.14	52934.10	1.4	Pass
T4	72.313 - 67.563	Top Girt	2L4x4x3/8	69	1847.63	168263.00	1.1	Pas
T8	50.271 - 41.979	Top Girt	L2 1/2x2 1/2x3/16	137	-626.78	10431.90	6.0	Pass
T12	20.103 - 13.415	Top Girt	L2x2 1/2x1/4	190	-2264.09	3642.36	62.2	Pas
T5	67.563 - 65.438	Bottom Girt	L3x3x3/16	91	1207.14	35316.00	3.4	Pas
T13	13.415 - 6.7075	Redund Horz 1 Bracing	L1 3/4x1 3/4x3/16	224	-936.75	15355.50	6.1	Pas
T14	6.7075 - 0	Redund Horz 1 Bracing	L1 3/4x1 3/4x3/16	253	-943.41	15355.50	6.1	Pas
T13	13.415 - 6.7075	Redund Diag 1 Bracing	L1 3/4x1 3/4x3/16	229	-721.67	7552.38	9.6	Pas
T14	6.7075 - 0	Redund Diag 1 Bracing	L1 3/4x1 3/4x3/16	254	-679.00	8699.96	7.8	Pas
T2	78.063 - 74.563	Inner Bracing	L2 1/2x2x3/16	30	90.88	26211.60	0.3	Pas
T5	67.563 - 65.438	Inner Bracing	L2 1/2x2x3/16	87	192.41	26211.60	0.7	Pas
T8	50.271 - 41.979	Inner Bracing	L2 1/2x2x3/16	133	29.18	26211.60	0.5	Pas
T12	20.103 - 13.415	Inner Bracing	L2x2x3/16	187	-131.79	1035.81	12.7	Pas
						Y (7710)	Summary	ъ
						Leg (T12)	77.0	Pas
						Diagonal (T12)	38.7	Pas
						Horizontal (T14)	22.7	Pas
						Top Girt (T12)	62.2	Pas
						Bottom Girt (T5)	3.4	Pas
						Redund Horz 1 Bracing (T14)	6.1	Pas
						Redund Diag 1 Bracing (T13)	9.6	Pas
						Inner Bracing (T12)	12.7	Pas
						Bolt Checks	62.7	Pas
						RATING =	77.0	Pas

Program Version 8.1.1.0 - 6/3/2021 File://10.0.1.130/Active/Jobs/Blue Sky Tower III LLC/Portland - CT 1680/240022 - RFQ QTE PO SA INV/Analysis/Calcs/REV 1/240022REV1.Portland.CT-1680.BSTManagementLLC.Analysis.eri



Structural Components, LLC	Job: 240022 REV 1				
1870 West 64th Lane, Unit A	Project: Portland (CT-1680)				
Denver, CO 80221	Client: BST Management, LLC	Drawn by: treed	App'd:		
Phone: (866) 386-7622	Code: TIA-222-H	Data: 02/13/24	Scale: NTS		
FAX:	Path:		Dwg No. E-5		



Structural Components, LLC	lob: 240022 REV 1		
1870 West 64th Lane, Unit A	Project: Portland (CT-1680)		
Denver, CO 80221	Client: BST Management, LLC	Drawn by: treed	App'd:
	Code: TIA-222-H	Date: 02/13/24	Scale: NTS
FAX:	Path:		Dwg No. E-8

# **PIER/PAD & MAT FOUNDATION**

Template = "SquareCombPierPadMat.xmcd" Version = 4.02

## **PROJECT DATA**

Job = "240022 REV 1"

Client = "BST Management, LLC"

Site = "Portland (CT-1680)"

Model = "90ft SST"



1870 West 64th Lane, Unit A Deriver, CO 80221 866-386-7622

# DESIGN CODES AND STANDARDS

Code = ("TIA-222-H, "Structural Standard for Antenna Supporting Structures and Antennas" 2017."

"ACI 318-14, "Building Code Requirements for Structural Concrete and Commentary," 2014."

## **FACTORED FOUNDATION DESIGN LOADS**

Overdesign Factor:  $\alpha = 1.00$  Percentage for Passing: PP = 100.%

Calculation Mode: calc = "Analysis (no seismic provision check)" reinf' = "Reinforcing Details Available"

Overall Axial:  $P_{u_1} = 21.8 \cdot \text{kip}$   $P_{u_2} = 16.3 \cdot \text{kip}$   $P_{u_3} = 43.7 \cdot \text{kip}$  Leg Moment:  $LM_{u_1} = 0.0 \cdot \text{kip} \cdot \text{ft}$   $LM_{u_2} = 0.0 \cdot \text{kip} \cdot \text{ft}$   $LM_{u_3} = 0.0 \cdot \text{kip} \cdot \text{ft}$  Leg Shear:  $S_{u_1} = 10.8 \cdot \text{kip}$   $S_{u_2} = 10.8 \cdot \text{kip}$   $S_{u_3} = 12.6 \cdot \text{kip}$ 

Leg Axial:  $\begin{aligned} &\operatorname{Pmax}_{\mathbf{u}_1} = 72.4 \cdot \operatorname{kip} & \operatorname{Pmax}_{\mathbf{u}_2} = 54.3 \cdot \operatorname{kip} & \operatorname{Pmax}_{\mathbf{u}_3} = 72.4 \cdot \operatorname{kip} \\ &\operatorname{Pmin}_{\mathbf{u}_1} = -62.8 \cdot \operatorname{kip} & \operatorname{Pmin}_{\mathbf{u}_2} = -47.1 \cdot \operatorname{kip} & \operatorname{Pmin}_{\mathbf{u}_3} = -61.5 \cdot \operatorname{kip} \end{aligned}$ 

# **DIMENSIONS**

Depth:  $D = 6.5 \cdot ft$  (from grade to bottom of pad)

Pad Width:  $W = 18.0 \cdot ft$  (each way)

Pad Thickness:  $T = 2.0 \cdot ft$ 

Pier Separation:  $Wt = 13.0 \cdot ft$ 

Pier (or mat) Extension:  $E = 0.5 \cdot ft$  (above-grade portion)

Pier: Pier = "Square"  $D_D = 2.0 \cdot ft$ 

Base Plate Geometry: BPG = "None" BP = 0.0 in

Tower Offset:  $ecc1 = 0.0 \cdot ft$  (center of tower to center of pad)

Tower Leg Offset:  $ecc2 = 0.0 \cdot ft$  (center of tower leg to center of pier)

Concrete Volume:  $V_{nad} = 24.0 \cdot yd^3$ 

 $V_{pier} = 0.7 \cdot yd^3$ 

 $V_{conc} = 27.0 \cdot yd^3$ 

# SITE & GEOTECHNICAL DATA

Soil Parameters: Geo = "GDP, 03/06/2017, Job # 2017702.58"

Soil Unit Weight:  $\gamma_{soil} = 136.5385 \cdot pcf$ 

Constant Lateral Pressure:  $CP_p = 0 \cdot psf$  (for pier)  $CP_p = 0 \cdot psf$  (for pad)

Equivalent Fluid Pressure: EFpres = "N" EFP =  $0.0 \cdot pcf$ 

Angle of Internal Friction:  $\phi_1 = 15.0 \cdot \text{deg}$  (above water table)

 $\phi_2 = "N/A" \cdot deg$  (below water table)

Ultimate Bearing Pressure: B'<sub>c</sub> = 30.0·ksf Bearing = "Capacity at Depth"

Cohesion:  $c = 10000 \cdot psf$ 

Adhesion:  $c_A = 0 \cdot psf$ 

Passive Pressure Coefficient (Rankine):  $K_{n1} = 1.70$  (above water table)  $K_{n2} = "N/A"$  (below water table)

Active Pressure Coefficient:  $K_{a1} = 0.59$  (above water table)  $K_{a2} = "N/A"$  (below water table)

Ultimate Friction Coefficient:  $\mu = 0.60$  (sides)  $\mu_{\rm c} = 0.60$ 

Ultimate Sliding Friction:  $f_s = 0 \cdot psf$  (base)  $f_{s,s} = 0.0000 \cdot psf$  (sides)

Depth Neglected:  $D_n = 2.5 \, ft$ 

Depth of Water Table:  $D_{w} = \text{"Below Footing"}$ 

Seismic Design Category: SDCT = "Seismic Design Category B" Note<sub>SDC</sub> = "N/A"

## MATERIAL SPECIFICATIONS

Concrete: Compressive Strength:  $f_c = 3000 \cdot psi$ 

Clear Cover:  $cc = 3.0 \cdot in$ 

Lightweight Aggregate Factor:  $\lambda = 1.00$ 

Unit Weight:  $\gamma_{conc} = 150 \cdot pcf$ 

Rebar: Yield Strength:  $F_y = 60 \cdot ksi$ 

# LATERAL CAPACITY

Design Resist. Lat. Load Check Ratio

 $\min\!\left(\varphi V_n\right) = 1112 \cdot kip \qquad \qquad \max\!\left(V_u\right) = 22 \cdot kip \qquad \qquad Check'_{lateral} = "OK" \qquad \qquad Ratio'_{lateral} = 0.02$ 

OVERTURNING

Design Resist O.T. Moment Check Ratio

 $min(MR1, MR2) = 6760 \text{ ft-kip} \quad max(M_{u,ot}) = 1394 \cdot \text{ft-kip} \quad Check'_{over} = "OK" \quad Ratio'_{over} = 0.47$ 

SOIL BEARING

Design Bearing Capacity Max. Bearing Check Ratio

 $\phi B_c = 22500 \cdot psf$   $P_{pos} = 2640 \cdot psf$   $Check'_{comp} = "OK"$   $Ratio'_{comp} = 0.12$ 

# PAD REINFORCEMENT/STRENGTH

\*Pad reinforcement is assumed

Number of Reinforcing Layers:

Mats = "Top & Bottom Mats"

(per layer per direction)

Pad has Hoops or Ties?

 $Tie_p = "No"$ 

Bar Quantity:

 $n_p = 21$ 

Р

Bar Size:

 $s_p = 6$ 

Bar Spacing (center to center):

 $sp_{p.ctr} = 10.5 \cdot in$ 

Bar Spacing (clear):

 $sp_{p.cl} = 9.7 \cdot in$ 

Total Weight (per mat):

 $Wt_{tp} = 1104 lbf$ 

Check of Reinforcing

 $Check_{spp.cl} = "OK"$ 

Spacing and Minimum Reinforcing:

 $Check_{spp,cl2} = "OK"$ 

Checkminp = "N/A"

REINFORCING FLEXURAL STRENGTH

<u>Case</u> <u>Design Strength</u> <u>Calculated Max Moment</u>

<u>Check</u> <u>Ratio</u>

A  $\phi M_{nA} = 805 \cdot \text{ft-kip}$ 

 $\max(M_{u,TA}) = 85 \text{ ft} \cdot \text{kip}$ 

Check'flex = "OK"

 $Ratio_{flex} = 0.53$ 

 $B \qquad \phi M_{nB} = 805 \cdot ft \cdot kip$ 

 $max(M_{u,TB}) = 426 \text{ ft-kip}$ 

(Case A = Bottom of Pad in Tension at Toe, Case B = Top of Pad in Tension at Heel)

PAD ONE-WAY SHEAR

Cîse Design Strength Calculated Max Shear

Check

Ratio

 $\phi V_{n1} = 353 \cdot kip$ 

 $\left| \max \left( V_{\text{umax.C1T}}, V_{\text{umin.C1T}} \right) \right| = 186 \cdot \text{kip}$ 

Check'<sub>shear.1</sub> = "OK"

 $Ratio'_{shear.1} = 0.53$ 

 $\left| \max \left( V_{\text{umax.C2T}}, V_{\text{umin.C2T}} \right) \right| = 137 \cdot \text{kip}$ 

(Case 1 = Hinging about Pad Edge Adjacent to Pier 1, Case 2 = Hinging about Pad Edge Adjacent to Piers 2/3.)

Shear Reinforcing Check:

Check'shrrnf = "OK"

TWO-WAY PAD SHEAR

Design Strength

Calculated Max Shear

Check

Ratio

 $\phi V_{n2} = 573 \cdot kip$ 

 $\max(V_{u2}) = 130 \cdot kip$ 

Check'shear.2 = "OK"

 $Ratio'_{shear.2} = 0.23$ 

# PIER REINFORCEMENT

Gross Area: 
$$A_{pier} = 4.0 \cdot ft^2$$
 Design Pier Area Factor:  $P_{Ag} = 50.\%$ 

Effective Gross Area: 
$$A'_{pier} = 2.0 \cdot ft^2$$
 Check of Area Factor: Check  $PAg = "OK"$ 

# LONGITUDINAL PIER REINFORCING

Bar Quantity: 
$$n_c = 12$$
 Bar Size:  $s_c = 6$ 

Hook Length: 
$$hook_{ca} = 0.0 \cdot in$$
 (actual/0 for none) Bend Dia:  $bend_c = 4.5 \cdot in$  (inside) Hook Length:  $hook_c = 9.0 \cdot in$  (required per ACl 7.1.2) Bar Weight  $Wt_{tc} = 133 \, lbf$  (per pier)

Check of Hook Length: 
$${\rm Check}_{hookc} = {\rm "N/A"}$$

# TIES

Check of Tie Size:

Tie Weight 
$$Wt_{tc} = 133 \cdot lbf$$
 (per pier)

(bot)

Maximum Crosstie Spacing (hx): 
$$h_{\rm X} = 0.0 \cdot {\rm in}$$

 $qsp_{t3} = 0.0000$ 

Tie Levels: 
$$qsp_{t1} = 7.0000$$
  $sp_{t1} = 8.0 \cdot in$  (top) Tie Quantity:  $n_t = 8$  (0 if none)  $qsp_{t2} = 0.0000$   $sp_{t2} = 0.0 \cdot in$  (mid.)

Maximum Required Tie Spacing (top, mid., bot.): 
$$sp_{t,max} = 12.0 \cdot in$$

 $sp_{t3} = 0.0 \cdot in$ 

$$Check_{tie} = "OK"$$
 $Note_{SDCt3} = "N/A"$ 
 $Check_{sp.cl} = "OK"$ 

## TIE SPLICE

## MINIMUM LONGITUDINAL REINFORCEMENT

Pier Area of Steel: 
$$A_{tc} = 5.3 \cdot in^2$$
 Ratio<sub>min.c</sub> = 1.8·% (based on effective pier gross area)

Minimum Steel Area Required: 
$$A_{min.c} = 2.9 \cdot in^2$$

Maximum Steel Area Allowed:  $A_{max.c} = 23.0 \cdot in^2$ 

## BASE PLATE BEARING ON CONCRETE

## COMPRESSIVE STRENGTH OF PIER CONCRETE

$$\Phi P_n = 382 \cdot \text{kip}$$
  $\max(P_{upier}) = 76 \cdot \text{kip}$   $\text{Check'}_{comp2} = \text{"OK"}$  Ratio' $\text{comp2} = 0.20$ 

# SHEAR STRENGTH OF PIER CONCRETE

$$\phi V_{npM} = 70 \cdot kip \qquad max(S_u) = 13 \cdot kip \qquad Check'_{shear,p} = "OK" \qquad Ratio'_{shear,p} = 0.19$$

# PIER MOMENT CAPACITY

$$\phi Mn_{cm} = 109 \text{ ft-kip} \qquad max(M_{u1.c}, M_{u2.c}) = 63 \text{ ft-kip} \qquad \text{Check'}_{pier} = \text{"OK"} \qquad \qquad \text{Ratio'}_{pier} = 0.58$$

# **DEVELOPMENT LENGTH IN TENSION**

w/o Hook 
$$1_{dc} = 12.0 \cdot in$$
  $1_{ac} = 21.0 \cdot in$ 

w/ Hook 
$$l_{dch} = 6.0 \cdot in$$
 Check $_{dev.ch} =$  "Hook not Required" Ratio $_{dev} = 0.57$ 

Controlling Foundation: CFP = 57.7.%

Page B

# **APPENDIX B**

**Data Provided for Analysis** 

	nstallation	n Type: Anchor	SRR Tov	vers Collocation Application Collocation	Add to Existing	0
		mes Burgess mesb@blueskytower.com		Site Number: Site Name:		
	fice: 61	17-549-2600	- ition Sheets.	Submittal Date		
- Continue to the continue to			λp	plicant Information		
pplicant Name:	Cellco Pa	rtnership d/b/a Verizon	Wireless	Primary Contact/Agent Name:	Phi	L Cotto
pplicant Site Name: pplicant Site Number:		PORTLAND 469381		Contact/Agent Company Name:		onaulting Group
oponed ON AIR Date:		9/30/2022		Contact/Agent Number: Contact Email:		154-7363
			Ame VI o	ant Contact Information	Companie	tureconsulting net
asing Contact Name:	Ph	il Cotto	Email:	Pootio@structureconsulting.net	Number:	
Contact Name:			Email:	LANGE OF THE PARTY	Number:	
nstruction Contact Name:			Email:		Number:	
ergency Contact Name:			Email:		Number:	
COUNT PAYABLE CONTACT NAME:			Email:		Number:	=
titude:	_	100		Tower Information		
ngitude:		x		Structure Type: Structure Height:		<del></del>
SL:	177			beluceare deigne.		7
		terro	100	PROF SPECIFICATIONS		_
Summary of Work to be Complete	d:	New 3 sector		of 9 panels and 9 RRUs. Tower exte	nsion to be performed to allow	for VEW to take 90° CL.
EXISTING CONDITIONS	- List all ir	nstalled equipment pr		osed modification. If this is a ne		
rrent RAD Center (Ft AGL) wer Mount Height (If different than RAD ct		SECTOR 1		SECTOR 2	SECTOR 3	SECTOR 4 (if necessary)
unt Type (Label "Existing" if no change)	"	ļ				
wer Mount Height (f different than RAD of bunt Type (Label "Existing" if no change) sunt Rodel 8 senna Manufacturer tenna Models (Attach Speca) tenna United (Attach Speca) tenna United (Label Speca) tenna Charletty sh Manufacturer sh Models (etboch Speca) sh Diameter (ET)						
tenna Manufacturer						
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Manufacturer						
h Modelf (ettech Specs)						
h Diameter (Ft)						
h Weight (Lbe.) h Mount Height						
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tal # of Coax Lines per Sector						
meter Of Coax Cables (in)						
al 8 of Hybrid Cables per Sector						
meter Of Hybrid Cables (In) al 8 of other Cables per Sector						
meter Of Other Cables (In)						
entity of RRUs per Sector						
nufacturer						
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ight (Lbs.)						
antity of TMAs per Sector nufscturer						
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enelonz						
ight (Lhu.)						
untity of Surge Arrestors per Sector sufacturer						
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Applicable) IU Model & Cumnity to be Removed per Sc						
Applicable) n/Cable Type, Size & Quantity to be Remo	ved (If					
Applicable) t Any Other Equipment to be Removed Applicable)	(H					
	INAL CON	FIGURATION - List all	Installed e	quipment after proposed modifi	cation or initial installation.	
rent/Proposed RAD Center (Ft AGL)		SECTOR 1		SECTOR 2	SECTOR 3	SECTOR 4 (if necessary)
rer Mount Height (H different than RAD ctr	1	80		90 80	90 80	
mt Type (Label "Existing" If no change)		T-Arn		T-Arm	T-Arm	
mt Model F		TBD		780	TRD	
enna Manufacturer enna Modelf (Attach Specs)		Commacope NNH4-65B-R6		Samoung PMAA22	Samoung	
enna Dimensions (WxHxD in Inches)		19.60 x 55.11 x	7.76	RT4423 11.8 x 8.7 x 4.2	MT6413-77A	
enna Weight (Lbs.)		73.86		18.7	28.91 x 15.75 x 5.51 57.32	
enna Quantity		3		3	3	
Manufacturer						
n Model# (attach Spece) n Diameter (Ft)						
h Weight (Lbs.)						
sh Mount Height						

Comment of Coac Alless per Sector				0		
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Dismotor Of Hybrid Cabbes (n)   6x12 hybridian   1					ables (In)	Hameter Of Coax Cable
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Classify of BRUS per Sector   3   3   3   3   3   3   3   3   3					Cables (in)	Siameter Of Hybrid Cal
Samurity of ERUs per Sector   Samurity   S				1	ales per Sector	Total 2 of other Cables
Samurity of ERUs per Sector   Samurity   S					Cables (In)	Diameter Of Other Cabi
Remarkstore   Remained   Remained   Remained   Remained   Ref4834-288	3	3	- 3	_		
Minumbrotherwer	Sansung				er Sector	tuantity of RRUs per S
Model   Articly   Manufacture   Commodope						Manufecturer
Model	14.77	BE 11374 EON	DE 1107	The second secon		
TF-16148-OVF-B12					er Sector	Quantity of TMAs per 8
Model   FE-16148-OVF-512						Manufacturer
Monder				E-16148-OVP-B12		
Monder					rreators per Sector	Quantity of Sures Arres
Transmit Prequency (Mitt)   5, 2145-2155, 869-880, 890-891.5						
Receive Frequency (MMr)						
Receive Frequency (Mike)  Autenna Clain (Db)  TX Fower Output  Existing Lease Area:  DIMS: L(ft) W(ft) OR Square footage  Existing Lease Area being requested:  New/Add 'I Lease Area being requested:  DIMS: L(ft) W(ft) IO OR Square footage  Shelter:  Concrete Fad for Shelter/Cabinets:  DIMS: L(ft) W(ft) W(ft)  Fower Provided by:  Average Monthly Fower Consumption:  Is a multi-tenant meter rack present:  Teleo/Interconnect Requirements:  Form Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Provider:  Bow many, if any, empty meter banks are present:  Fiber Office  Fiber Offic						Hodel
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Artenna dain (Db) Type of Technology  EXF Fower Output  EXP (Watta)  Existing Lease Area: DIMS: Lift)					, (mare)	
TX Power Output  Exertic Bervice Required (Amps/Orbs)  Exertic Bervice Required (Amps/Orbs)  Existing Lease Area: OIMS: L(ft)					The second secon	
TRP (Watts)						
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New/Add 'l Lease Area being requested: DIMS: L(ft)	otage	OR Square fo	OR	W(ft)	ation torse treet news 1/6	murant.
Shelter: DIMS: L(ft) W(ft) H(ft)  Concrete Pad for Shelter/Cabinets: DIMS: L(ft) W(ft)  POWER REQUIREMENTS  Fower Provided by: Electrical Service Provider: Electrical Service Telephone Number:  Average Monthly Power Consumption: KWH units Is a multi-tenant meter rack present: Yes How many, if any, empty meter banks are present:  Telco/Interconnect Requirements: POTS TI Generator WICHOWAVE FIBER OPTICAGE  Generator Required: No Generator Sequirement: DIMS: L(ft) W(ft) E(ft) Fuel Type:  BST Generator: Ground Space Requirement: DIMS: L(ft) W(ft) Fuel Tank Size: DIMS: L(ft W(ft))  Generator Required: No Generator Made: Generator Model:  Generator Required: No Generator Make: Generator Model: Fuel Tank E Gallons  Generator Required: No Generator Make: Generator Model: Fuel Tank E Gallons  Generator Feel Tank (if required) DIMS: L(ft W(ft))	otage	OR Square for	10 OR			
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Fower Provided by:  Average Monthly Power Consumption:  Average Monthly Power Consumption:  Is a multi-tenant meter rack present:  Telco/Interconnect Requirements:  Fiber Provider:   BACK-UP POWER INFORMATION  Generator Required:  Generator Ground Space Requirement:  BIS Generator Ground Space Requirement:  Generator Capacity:  Generator Capacity:  MO Generator Make:  Generator Capacity:  Fuel Tank Size: DIMS: L(f)  W(ft)  W(ft)  W(ft)  W(ft)  W(ft)  W(ft)  W(ft)  Fuel Tank E  Gallons  Gallons  Gallons  Gallons						
Power Provided by:  Average Monthly Power Consumption:  Average Monthly Power Consumption:  Is a multi-tenant meter rack present:  Telco/Interconnect Requirements:  Fiber Provider:  BACK-UP POWER INTODUCTOR  Generator Required:  No  Generator Ground Space Requirement:  BST Generator:  Generator Ground Space Requirement:  Semerator Owner:  Generator Made:  MITION MITIO		SIDCOTTS	CHARGE BROKETBRAKEN		ad for Shelter/Cabinets: Diss. D(	Concrete Fad 1
Average Monthly Power Consumption:  Is a multi-tenant meter rack present:  Fiber Provider:    Sack-UP POWER INFORMATION	Janhone Munher:		Outer, 100Koxviii-			
Tal amulti-tenant meter rack prement:   Yes		Electrical pervice :				Power Provided by:
Post				WH Units	ILILIY LOWEL CONDUMPTIONS	
BACK-UP POWER INFORMATION						
Generator Required: No Generation Location: Generator Ground Space Requirement: DIMS: L(ft) W(ft) E(ft) Fuel Type:  BST Generator: Generator: Generator Owner: Generator Owner: Shared Generator Peak Usage: XW  Generator: AN Generator Make: Generator Model: Gener	j .		MICHOWAVE [	T1 🗆		
Generator Required: No Generation Location: Generator Ground Space Requirement: DIMS: L(ft) W(ft) E(ft) Fuel Type:  BST Generator: Generator Capacity: Generator Make: Generator Model: Generator					c:	Fiber Provider:
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Generator Ground Space Requirement: DIMS: L(ft) W(ft) E(ft) Fuel Type:  BST Generator: Generator Make: Shared Generator Peak Usage: XW  Generator Capacity: NW Generator Make: Generator Model: Generator Model: Tuel Tank Location: Fuel Tank Size: DIMS: L(f W(ft) Fuel Tank E Gallons  Pad for Fuel Tank (if required) DIMS: L(ft W(ft)		9	cation:		Senerator Required: No	Gene
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Comments						Ded for Sun! Tank
SAMILE AT CASE				-	ik (il ledulled) binar bite	
Comments: List any pertinent information that was not included above.						Tourierrent
		tion that was not included above.	ent information the	Comments: List any portin		
			WITH INTO THE DOLL CO.	Community List any portion		
	47					
	W.					



# NORTHEAST > North East > New England > Wallingford-1 > PORTLAND HS CT - B

Cheiban, Ziad - ziad.cheiban@verizonwireless.com - 20230927\_153155

		Location Information	
Carrier Aggregation N		Site Id	Site Id 616480547
Ecip N		Search Ring#	
Project Name Po	Project Name PORTLAND HS CT	E-NodeB ID# null	llnu
Project Alt Name PORTLAND HS CT	ORTLAND HS CT	PSLC# 469381	469381
Project Id 16599668	3599668	Switch Name   Wallingford-1	Wallingford-1
Designed Sector Carrier 4G 15	9	Tower Type	
Designed Sector Carrier 5G 3		Site Type MACRO	MACRO
Additional Sector Carrier 4G 0		Street Address 97 High Street	97 High Street
Additional Sector Carrier 5G 0		City	City Portland
Suffix Re	Suffix Rev4-2023-09-27	State CT	CT
rpe & Tech Type M. G.	FP Solution Type & Tech Type   MCR;4G_700;4G_850;4G_AWS;4G_CBRS;5   G_L-Sub6;4G_PCS	Zip Code 06480	06480
		County	County Middlesex
		Latitude	Latitude 41.58071/41°34'50.556"
		Longitude	Longitude -72.63136/72° 37' 52.896"

Project Scope			
Rev4-2023-09-27 Use RF4461d-13A low band RRH and 6413 C-Band MMU			
	-8		

						Antenna	Antenna Summary					
Added Ar	rtenna											
700	850	1900	AWS	CBRS	L-Sub6 Make	Make	Model	Center	Tip Height	Azimath	Install Type	Quantit
					56	Samsung	MT6413-77A	06	91.2	30(1),150(2),2 70(3)	PHYSICAL 3	9
ᄩ	LTE	<u> </u>	LTE			COMMSCOPE	NNH4-65B-R6	06	93	30(1),150(2),2 70(3)	PHYSICAL 3	3
				LTE		Samsung	RT4423	06	90.4	30(19),150(20) ,270(21)	PHYSICAL 3	3

00 850	1900	AWS	CBRS L	L-Sub6 Ma	Make	Model	Center	To Helph	Azimuth	Install	Quantit

	Quantit
	install Type
	Azimuth
	Tip Keight
	Center
	Model
	Make
	L-Sub6
	CBRS L-Sub6
	AWS
	1900
Antenna	850
Retained	700

Retained: 0	Removed: 0	

						No	Non Antenna Summary			
Added Non A	Intenna									
Equipment Type	Location	700	850	1900	AWS	CBRS	Make	Model	install Type	Quantity
Hybrid Cable	Tower						Hybrid Cables	1-1/4" Hybrid Cables	PHYSICAL	7
OVP	Tower							12 OVP	PHYSICAL	-
RRU	Tower			띰	昌		Samsung	B2/B66A RRH ORAN (RF4439d-25A)	PHYSICAL	m
RRU	Tower					LTE	Samsung	RF4423-48B	PHYSICAL	60
RRU	Tower	LTE	LTE				Samsung	RF44610-13A	PHYSICAL	en

ed non America								
nent Location 700	820	1900	AWS	CBRS	Make	Model	Install	Quantify

	Quantity
	Install
	Model
	Маке
	CBRS
	AWS
	1900
	820
	200
Antenna	Location
Retained Non	Equipment Type

Retained: 0	
Removed: 0	
Added: 12	

Services			
700 LTE		0002 (8118082)	
Sector	01	00	60
Azimuth	30	150	270
Cell/Enodeb-ld	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
Antenna Make	COMMSCOPE	COMMSCOPE	COMMSCOPE
Centerline	06	06	06
DLEARFCN	5230	5230	5230
Mech Down-tillt	0	0	0
Elect Down-tilt	2	2	2
Tip Height	93	63	83
Regulatory Power	66.49 (W/MHz) ERP	66.49 (W/MHz) ERP	66.49 (W/MHz) ERP
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	RF4461d-13A	RF4461d-13A	RF4461d-13A
Number of Tx,Rx	4,4	4,4	4,4
Position	٠		
Transmitter Id	11232662	11232663	11232664
Source	AZNPP	VZNPP	VZNPP
Bandwidth	10	10	10
Ant. Dimensions H x W x D(inch)	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79
Weight(ib)	81.82	81.82	81.82

		0002 (8118082)	
	10	02	63
	30	150	270
Cell/Enodeb-Id	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
	COMMSCOPE	COMMSCOPE	COMMSCOPE
	06	06	06
	2450	2450	2450
Mech Down-tilt	0	0	0
	2	2	2
	83	93	93
Regulatory Power	301.17 (W/MHz) ERPSD	301.17 (W/MHz) ERPSD	301.17 (W/MHz) ERPSD
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
	Samsung	Samsung	Samsung
	RF4461d-13A	RF4461d-13A	RF4461d-13A
Number of Tx,Rx	4,4	4,4	4,4
	11298595	11298596	11298597
	VZNPP	VZNPP	VZNPP
	10	10	10
Ant. Dimensions H x W x D(inch)	72.0 x 19.6 x 7.79	72.0×19.6×7.79	72.0×19.6×7.79
	81.82	81.82	81.82

Services			
1900 LTE		0002 (8118082)	
Sector	01	02	03
Azimuth	30	150	270
Cell/Enodeb-id	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
Antenna Make	COMMSCOPE	COMMSCOPE	COMMSCOPE
Centerline	06	06	06
DLEARFCN	1050	1050	1050
Mech Down-tilt	0	0	0
Elect Down-tilt	2	2	2
Tip Height	93	83	83
Regulatory Power	168.95 (W/MHz) EIRP	168.95 (W/MHz) EIRP	168.95 (W/MHz) EIRP
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	BZ/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)
Number of Tx, Rx	4,4	4,4	4,4
Position			
Transmitter Id	11298592	11298593	11298594
Source	AZNPP	VZNPP	VZNPP
Bandwidth	10	10	10
Ant. Dimensions H x W x D(inch)	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79
Weight(ib)	81.82	81.82	81.82

	0002 (8118082)	(2)
01	05	603
30	150	270
064040	064040	064040
NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
COMMSCOPE	COMMSCOPE	COMMSCOPE
06	06	06
2050	2050	2050
0	0	0
2	2	2
83	83	63
84.67 (W/MHz) EIRP	EIRP 84.67 (W/MHz) EIRP	84.67 (W/MHz) EIRP
46.0 dBm	46.0 dBm	46.0 dBm
Samsung	Samsung	Samsung
B2/B66A RRH ORAN (RF4439d-25A)	ORAN B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)
4,4	4.4	4,4
11298467	11298468	11298469
ddNZA	ddNZN	VZNPP
20	20	20
72.0 x 19.6 x 7.79	.79 72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79
81.82	81.82	81.82

Services			
CBRS LTE		0002 (8118082)	
Sector	19	20	21
Azimuth	30	150	270
Cell/Enodeb-id	064040	064040	064040
Antenna Model	RT4423	RT4423	RT4423
Antenna Make	Samsung	Samsung	Samsung
Centerline	06	06	06
DLEARFCN	55343, 55541, 55739, 55937	55343, 55541, 55739, 55937	55343, 55541, 55739, 55937
Mech Down-tilt	0	0	0
Elect Down-tilt	7	7	7
Tip Height	90.4	90.4	90.4
Regulatory Power	3.76 (WMHz) EIRPSD, 3.76 (WMHz) EIRPSD, 3.76 (WMHz)	3.76 (WMHz) EIRPSD, 3.76 (WMHz) EIRPSD, 3.76 (WMHz)	3.76 (WMHz) EIRPSD, 3.73 (WMHz) EIRPSD, 3.76 (WMHz)
Cell Max Power	37.02 dBm	37.02 dBm	37.02 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	RF4423-48B	RF4423-48B	RF4423-48B
Number of Tx,Rx	4,4	4 ' 4	4'4
Position			
Transmitter Id	11298781	11298782	11298783
Source	VZNPP	VZNPP	VZNPP
Bandwidth	20, 20, 20, 20	20, 20, 20, 20	20, 20, 20, 20
Art. Dimensions H x W x D(inch)	8.7 × 12.0 × 1.5	8.7 x 12.0 x 1.5	8.7 x 12.0 x 1.5
Weight(ib)	3.3	3.3	3.3

		0002 (8118082)	
10001		0002	8000
30		150	270
0640040	40	0640040	0640040
MT6413-77A	3-77A	MT6413-77A	MT6413-77A
Samsung	Bul	Samsung	Samsung
06		06	06
90009	650006, 655324	650006, 655324	650006, 655324
0		0	0
_		-	-
91.2		91.2	91.2
743.34 ( EIRP, 74 (WIMHZ)	743.34 (WMHz) EIRP, 743.34 (WMHz) EIRP	743.34 (W/MHz) EIRP, 743.34 (W/MHz) EIRP	743.34 (W/MHz) EIRP, 743.34 (W/MHz) EIRP
52.02 dBm	JBm	52.02 dBm	52.02 dBm
		le	
Samsung	Вu	Samsung	Samsung
MT6413-77A	3-77A	MT6413-77A	MT6413-77A
2,2		2,2	2,2
11298702	102	11298703	11298704
ddNZA		VZNPP	VZNPP
100, 60		100, 60	100, 60
29.53 x 7 5.51	29.53 x 15.75 x 5.51	29.53 x 15.75 x 5.51	29.53 × 15.75 × 5.51
155		1 X	1 2 2

Callsigns Per Antenna	Antenna																		
Sector	Maka	Nodel	Ant CL Height AG	Ant Tip Height	Azimuth	Elect Down-tilt	Mech Down-tilt	Gain	Bendwidth R	Regulator 70 y Power	002	920	1900	2100 28	28 GHz 31	31 GHz	39 GHz	Sub-6	CBRS
0003	Sameung	MT6413-77A	8	B1.2	270	-	0	23.15	201	743,34								WRNE581,WF NE582,WRNE IS83,WRNE58 4,WRNE585	
19	Sвивилд В в при в	RT4423	06	90.4	8	_	۰	10.34	67 3	3.76									CBRS_CALLS
02	COMMSCOPE	NNH4-65B-R			150	2 0	0	11.94	69.75 6	86.49 W	WQJQ689								
03	COMMSCOPE	COMMSCOPE NNH4-65B-R 90		83			0	12.54	65 3	301.17	¥	KNKA404							
0005	Sameung	MT6413-77A			150	-	0	23.16	105	743.34								WRNE581,WF NE582,WRNE 583,WRNE58 4,WRNE585	
2000	Sameung	MT6413-77A	8	91.2	150	-	0	23.15	105	743.34								WRNE585,WF NE586,WRNE 587,WRNE58	
1000	Sameung	MT6413-77A	8	91.2	30		0	23.15	105	743.34								WRNE581,W3 NE582,WRNE 583,WRNE58 4,WRNE585	
	COMMSCOPE	NNH4-65B-R		93	150	2	0	12.54	65	301.17	Ī	KNKA404							
10	COMMSCOPE	NNH4-65B-R				2	0	12,54	65	301.17	Ī	KNKA404							
24	Samsung RT4423 90	RT4423		90.4	270	7	0	10.34	87 8	3.76									CBRS_CALLS IGN
10001	Sameung	MT6413-77A	06	91.2	S	-	0	23.15	105	743.34								WRNE585,WF NE586,WRNE 587,WRNE56	
05	COMMSCOPE	COMMSCOPE NNH4-65B-R	<b>6</b>	93	150	2	0	13.92	60.75	168.95			KNLH251,WP OJ730						
03	COMMSCOPE	COMMSCOPE NNH4-85B-R	06	93	270	rs.	0	13.92	60.75	168.95			KNLH251,WP OJ730						
83	COMMSCOPE	COMMSCOPE NNH4-65B-R 90		83	270	2	o	11.94	69.75	86.49 V	WQJQ889								
5	COMMSCOPE	COMMSCOPE NNH4-65B-R 90		93	30	2	0	11.94	69.75	66.49 V	WQJQ689								
50	Samsung	RT4423	88	90.4	150	۷	0	10,34	. 29	3.76									CBRS_CALLS IGN
0003	Samsung	MT6413-77A	8	91.2	270	Ţ	0	23.15	105	743.34								WRNES85 WE INES86, WRN E	
10	COMMSCOP	COMMSCOPE NNH4-858-R	06	93	80	2	0	13,92	80,75	168.95			KNLH251,WP OJ730						
60	COMMSCOP	COMMSCOPE NNH4-65B-R	œ	83	270	2	0	13.93	63.5	84.67				WQGA906,WC GB276					
02	COMMSCOP	COMMSCOPE NNH4-65B-R	8	93	150	2	0	13.93	63.5	84.67				WQGA906,Wd GB276					
10	COMMSCOP	COMMSCOPE NNH4-65B-R 80	06	93	30	2	0	13.83	63.5	84.67				WQGA906,W0 GB276					

Approve for insvc	2	-		_ 10				-				
Action	Pappa	Peppa	Peppu	peppu	p <sub>e</sub> pp <sub>e</sub>	peppa	pappa	peppe	peppa	peppe	Peppii	Pappa
Startus	pesodad	pesodad	posodod	peeodord	proposed	proposed	proposed	proposed	pesodord	pesodud	proposed	proposed
POPa/8q.	44.75	444.75	44.75	444.75	# 72	444.75	444.75	444.75	444.75	444.75	444.75	44.76
(w)	1000	004	95	0 <del>1</del>		1840	55 64 64	1840	1640	0460	1640	0791
Regulator y Posser	96.49	301.17	168.95	168.95	3.76	64.67	743.34	743.34	743.34	743.34	743.34	72.07
Find Range 4	776.000 - 787.000/. 000 -	869.000 - 890.000/8 90.000 - 891.500	1975.000 1990.000/ .000 -	1970.000 1975.000/ .000 -	4	2110.000 2120.000/ .000 -	- 000. - 000. 000.	- 000. - 000/.000 000	- 000.000.	- 000. .000,000 000.	- 000. .000,000 000	2120.000 2130.000/ .000 - .000
Range 3	746.000 - 757.000/. 000 -	824.000 - 835.000/8 45.000 - 846.500	1895.000 1900.000/ .000 -	1880.000 1885.000/ .000 -	+	1710.000 1720.000/ .000 -	3700.000 3720.000/ .000 -	3720.000 3740.000/ .000 -	3740.000 3760.000/ .000 -	3760.000/ 3760.000/ .000 -	3780.000 3800.000/ .000 -	1720.090 1730.000/ .000 - .000
Fred Range 2	776.000 - 787.000/. 000 -	868.000 - 880.000/8 90.000 - 991.500	1960.000/ 1960.000/ .000	1970.000 1975.000/ .000 .000	UNLICENSE D/UNLICENSE D/UNLICENSE SED - UNLICENSE	2110.000 2120.000/ .000 -	.000. .000.000. .000.	- 000. - 000/.000 - 000.	- 000. - 000/.000 000	.000. .000/.000 000	.000. .000,000. 000	2120.000 2130.000/ .000 - .000
Freq Range 1	746.000 - 757.000/. 000 -	824.000 - 835.000/8 45.000 - 846.500	1805.000 1900.000/ .000 -	1890.000 1895.000/ .000 -	UNLICENSE D. UNLICENSE DAUNLICEN SED - UNLICENSE	1710.000 1720.000/ .000 -	3700.000 3720.000/ .000 -	3720.000 3740.000/ .000 -	3740.000 3760.000/ .000 -	3760.000 3760.000/ .000 -	3760.000 3800.000/ .000 -	1720.000 1730.000/ .000 .000
Total MHZ	22.000	25.000	10.000	18.000	UNLICENSE	20.000	20.000	20.000	20.000	20.000	20.000	20.000
Wholly	<b>¥</b>	<b>8</b>	Yes	ž,	UNLICENSE	Yes	į	Yes	88,	Yes	\$ >	
Name	Cellco Partnersh Ip	Cellco Partnersh Ip	Celico Partnerah ip	Celico Partnersh fp	UNLICENSE	Cellco Partnersh ip	Celico Partnersh ip	Celico Partnersh ip	Celico Partnersh Ip	Cellco Partnerah Ip	Calico Partnersh Ip	Cellco Partnersh Ip
County	8007	2008	8007	8007	UNLICENSE	9007	2006	8007	2008	8007	8007	9007
	5	Б	5	5	5	ь	ь	5	5	5	ь	ь
Block	U	<	o	a i	CINICENSE	4	¥	য	2	¥	8	œ
Married #	REA001	CMA032	BTA184	BTA184	UNLICENSE	CMA032	PEA001	PEA001	PEA001	PEA001	PEA001	BEA010
Code	D <sub>M</sub>	ಠ	A C	Mo Co	3.6 GHz	WA	¥	M	N.	æ a	N.	AW.
Merce	Northeast	Hertford- New Britsin-B rietol, CT	Hartford, CT	Hartford, CT	UNLICENSE	Hartford- New Britain-B Hatol, CT	New York,	New York, NY	New York, NY	New York, NY	New York, NY	New York-No. New JerLong Island, NY-NJ-CT- PA-MA-
Calleign	WGJQ688	KNKA404	WP0J730	KNLH281	CBRS_CALL SIGN	WQGB276	WRNE681	WRNE502	WRNE583	WRNES64	WRNE585	WQGA806

		-
peppe	people	pappe
pesodorq	pesodord	pesodard
444.76	444.75	444.75
1840	040	1640
743.34	748.34	743.34
. 000, 000.	- 000.	- 000. - 000. - 000.
3820.000/ 3820.000/ .000 -	3820.000 3840.000/ .000 -	3840.000 3850.000/ .000 -
.000,000.	.000. .000.000 000	. 000. 000. 000
3820.000 3820.000/ .000 -	3820.000 3840.000/ .000 -	3840.000 3860.000/ .000 -
20.000	20.000	20.000
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Cellco Partnersh Ip	Cellco Partnersh Ip	Celico Partnersh Ip
2005	8067	2008
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£	E2	2
PEA001	PEA001	PEA001
<b>8</b>	2	2
NY NY	NY NY	New York, PM
WRNE586	WRNE587	WRNES88



Centered on Solutions \*\*\*

# Antenna Mount Analysis Report

Site Ref: Portland HS

97 High Street Portland, CT

Centek Project No. 22017.06

Dato: May 11, 2023

Rev 1: November 9, 2023

Max Stress Ratio = 44%

Prepared for:

Verizon Wireless 20 Alexander Drive Wallingford, CT 06492



CENTEK Engineering, Inc.
Mount Analysis
Verizon Site Ref. ~ Portand HS
Portland, CT
Rev 1 ~ November 9, 2023

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# SECTION 1 - REPORT

- ANTENNA AND APPURTENANCE SUMMARY
- STRUCTURE LOADING
- CONCLUSION

# SECTION 2 - CALCULATIONS

- WIND LOAD ON APPURTENANCES
- RISA3D OUTPUT REPORT
- CONNECTION

# SECTION 3 - REFERENCE MATERIALS

■ RF DATA SHEET



## Centered on Solutions™

November 9, 2023

Mr. Phillip Cotto Structure Consulting Group 49 Brattle Street Arlington, Ma

Re: Structural Letter ~ Antenna Mount Verizon – Site Ref: Portland HS 97 High Street Portland, CT

Centek Project No. 22017.06

Dear Mr. Cotto,

Centek Engineering, Inc. has reviewed the Verizon antenna installation at the above referenced site. The purpose of the review is to determine the structural adequacy of the **proposed mount**, **consisting of three (3) V-frame sector mounts (SitePro P/N: VFA12-HD)** to support the proposed equipment configuration. The review considered the effects of wind load, dead load and ice load in accordance with the 2021 International Building Code as modified by the 2022 Connecticut State Building Code (CTBC) including ASCE 7-16 and ANSI/TIA-222-H *Structural Standard for Antenna Supporting Structures, Antennas and Small Wind Turbine Support Structures*".

The loads considered in this analysis consist of the following:

#### Verizon:

<u>V-Frames:</u> Three (3) Commscope NNH4-65B-R6 panel antennas, three (3) Samsung MT6413-77A panel antennas, three (3) Samsung RT4423 panel antennas, three (3) Samsung RF4439d-25A (B2/B66A) RRHs, three (3) Samsung RF4461d-13A (B5/B13) RRHs, three (3) Samsung RF4423-48B RRHs and one (1) OVP Box mounted on three (3) V-Frames with a RAD center elevation of 90 ft +/-AGL.

The antenna mount was analyzed per the requirements of the 2021 International Building Code as modified by the 2022 Connecticut State Building Code considering a Ultimate design wind speed of 120 mph for Portland as required in Appendix P of the 2022 Connecticut State Building Code.

Based on our review of the installation, it is our opinion that the **subject antenna mount has sufficient capacity** to support the aforementioned antenna configuration.

If there are any questions regarding this matter, please feel free to call.

DROTTES SIONAL EN

Respectfully Submitted by

Timothy J. Lynn PE Structural Engineer CENTEK Engineering, Inc.
Mount Analysis
Verizon Site Ref. ~ Portand HS
Portland, CT
Rev 1 ~ November 9, 2023

# Section 2 - Calculations



Subject:

Location:

Rev. 1: 11/9/23

TIA-222-H Loads

Portland, CT

(User input)

Prepared by: T.J.L. Checked by: C.F.C.

Job No. 22017.06

#### Development of Design Heights, Exposure Coefficients, and Velocity Pressures Per TIA-222-H

#### Wind Speeds

Basic Wind Speed V := 120 (User Input - CSBC 2022 Appendix P) mph Basic Wind Speed with Ice  $V_i := 50$ mph (User Input - TIA-222-H Annex B) Basic Wind Speed (Mount) V<sub>m</sub> := 30 (User Input - TIA-222-H Section 16.3) mph

#### Input

Structure Type = Structure\_Type := Flexible (User Input) Structure Category = SC := III (User Input) Exposure Category = Exp := C(User Input) Structure Height = h:= 90 (User Input)

Height to Center of Antennas= (User Input)  $z_{ant} = 90$ Radial Ice Thickness=

 $t_i := 1.0$ (User Input per Annex B of TIA-222-H) Radial Ice Density= ld := 56.00 (User Input)

 $K_a := 1.0$ 

Topograpic Factor =  $K_{zt} := 1$ (User Input)

Rooflop Wind Speed-up Factor =  $K_s := 1.0$ (User Input) Ground Elevation Factor =

 $K_{p} = 0.996$ (User Input) Gust Response Factor =  $G_{H} = 1.35$ (User Input)

Output

Wind Direction Probability Factor =

Shielding Factor for Appurtenances =

 $K_d = 0.95$ 

(Per Table 2-2 of TIA-222-H) (Per Table 2-3 of

TIA-222-H)

Importance Factors =

$$K_{iz} := \left(\frac{z_{ant}}{33}\right)^{0.1} = 1.106$$

$$t_{iz} \coloneqq t_{i'} l_{ice'} K_{iz'} K_{zt}^{-0.35} = 1.271$$

Velocity Pressure Coefficient Anternas =

$$Kz_{ant} := 2.01 \left( \left( \frac{z_{ant}}{z_g} \right) \right)^{\frac{2}{\alpha}} = 1.238$$

Velocity Pressure w/o loe Antennas =

$$qz_{ant} := 0.00256 \cdot K_{zt} \cdot K_s \cdot K_e \cdot K_d \cdot Kz_{ant} \cdot V^2 = 43.16$$

Velocity Pressure with Ice Antennas =

$$qz_{ice,ant} := 0.00256 \cdot K_{Z_i^T} \cdot K_S \cdot K_{e} \cdot K_{d} \cdot Kz_{ant} \cdot V_i^2 = 7.493$$

Velocity Pressure with Ice Antennas =



Centered on Solutions P: (203) 488-0580 F: (203) 488-8587

Subject:

Location:

TIA-222-H Loads

Job No. 22017.06

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C.

Rev. 1: 11/9/23

#### Development of Wind & Ice Load on Appurtenances

## Appurtenance Data:

Commscope NNH4-65B-R6 Appurtenance Model =

Appurtenance Shape =

Appurtenance Height=

Appurtenance Width =

Appurtenance Thickness = Appurtenance Weight =

(User Input) Number of Appurtenances=

 $Ar_{app} := \frac{L_{app}}{W_{app}} = 3.7$ Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

#### Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurte rance Wind Force =

## Wind Load (with ice)

SurfaceArea for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

SurfaceArea for One Appurtenance w/ Ice (Side) =

Total Appurtenance Wind Force w/ be=

## Wind Load (Mount)

SurfaceArea for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurterance Wind Force =

#### Gravity Loads (Ice only)

Volume of Each Appurtenance =

Volume of ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurtemences =

(User Input)

(User Input) Lapp := 71.969

 $W_{app} := 19.606$ (User Input)

T<sub>app</sub> := 7.756 in (User Input)

 $WT_{app} = 90$ (User Input)

 $N_{app} := 1$ 

$$Ar_{app} := \frac{L_{app}}{W_{app}} = 3.7$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 9.8$$
 sf

$$F_{app} := qz_{ant} \cdot G_{H} \cdot Ca_{app} \cdot K_a \cdot SA_{app} \cdot N_{app} = 715$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 3.9$$
 sf

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 11.5$$
 sf

$$SA_{ICEappS} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right)}{144} = 5.3$$
 sf

lbs

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 9.8$$
 sf

$$\mathsf{F}_{\mathsf{app}} := \mathsf{qz}_{\mathsf{m}} \cdot \mathsf{G}_{\mathsf{H}} \cdot \mathsf{Ca}_{\mathsf{app}} \cdot \mathsf{K}_{\mathsf{a}} \cdot \mathsf{SA}_{\mathsf{app}} \mathsf{F} \cdot \mathsf{N}_{\mathsf{app}} = \mathsf{45}$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 3.9$$
 sf

$$\begin{split} &V_{app} \coloneqq L_{app} \cdot W_{app} \cdot T_{app} = 1 \times 10^4 & \text{cu in} \\ &V_{ice} \coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \! \left(W_{app} + 2 \cdot t_{iz}\right) \! \cdot \! \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 6053 & \text{cu in} \end{split}$$

$$W_{ICEapp} := \frac{V_{ice}}{1728} \cdot Id = 196$$
 lbs



Centered on Solutions 63-2 North Branford Road Branford, CT 06405

P (203) 488-0580 F: (203) 488-8587 Subject:

TIA-222-H Loads

Location:

Rev. 1: 11/9/23

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C.

Job No. 22017.06

## Development of Wind & Ice Load on Appurtenances

#### Appurtenance Data:

Appurtenance Model =	
----------------------	--

Appurtenance Shape =

Appurtenance Height=

Appurtenance Width =

Appurtenance Thickness =

Appurtenance Weight=

Number of Appurtenances=

Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

#### Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurterance Wind Force =

## Wind Load (with ice)

SurfaceArea for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

SurfaceArea for One Appurtenance w/ Ice (Side) =

Total Appurtemence Wind Force w/be=

## Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

## Gravity Loads (Ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of ice on EachAppurtenance =

Weight of Ice on All Appurtenances =

#### Samsung MT6413-77A

t (User Input)

Lapp := 28.9 in (User Input)

Wapp := 15.75 in (User Input)

-----

Tapp := 5.51 in (User Input)

 $WT_{app} := 60$  lbs (User Input)

Napp := 1 (User Input)

$$Ar_{app} := \frac{L_{app}}{W_{app}} = 1.8$$

$$Ca_{app} = 1.2$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 3.2$$

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1.1$$

$$F_{app} := qz_{ant} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appS} = 77$$
 lbs

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 4$$
 sf

sf

lbs

$$SA_{ICEappS} := \frac{(L_{app} + 2 \cdot t_{iz}) \cdot (T_{app} + 2 \cdot t_{iz})}{144} = 1.8$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 3.2$$

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1.1$$
 sf

$$F_{app} := qz_m \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appS} = 5$$
 lbs

$$V_{app} := L_{app} \cdot W_{app} \cdot T_{app} = 2508$$
 cu in

$$V_{ice} := (L_{app} + 2 \cdot t_{iz})(W_{app} + 2 \cdot t_{iz}) \cdot (T_{app} + 2 \cdot t_{iz}) - V_{app} = 2124$$
 cuin

$$W_{ICEapp} := \frac{V_{ice}}{1728} \cdot Id = 69$$
 lbs

$$W_{ICEapp} \cdot N_{app} = 69$$
 lbs

Subject:

TIA-222-H Loads

Location:

Rev. 1: 11/9/23

Portland, CT

(User Input)

Prepared by: T.J.L. Checked by: C.F.C.

Job No. 22017.06

#### Development of Wind & Ice Load on Appurtenances

## Appurtenance Data:

Samsung RT4423 Appurtenance Model = Flat Appurtenance Shape =

(User Input) L<sub>app</sub> := 12.3 Appurtenance Height=

W<sub>app</sub> := 8.7 (User Input) Appurtenance Width =

 $T_{app} = 1.4$ (User Input) Appurtenance Thickness =

 $WT_{app} := 3$ (User Input) Appurtenance Weight=

(User Input)  $N_{app} := 1$ Number of Appurtenances=

Ca<sub>app</sub> = 1.2

 $Ar_{app} := \frac{L_{app}}{W_{app}} = 1.4$ Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

## Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurterance Wind Force =

#### Wind Load (with ice)

Surface Area for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

Surface Area for One Appurtenance w/lce (Side) =

Total Appurtemence Wind Force w/ be=

## Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

## Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of ice on All Appurienances =

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 0.7$$
 sf

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 0.1$$
 sf

$$\mathsf{F}_{\mathsf{app}} \coloneqq \mathsf{qz}_{\mathsf{ant}} \cdot \mathsf{G}_{\mathsf{H}} \cdot \mathsf{Ca}_{\mathsf{app}} \cdot \mathsf{K}_{\mathsf{a}} \cdot \mathsf{SA}_{\mathsf{appS}} = 8$$
 lbs

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 1.2$$
 sf

$$\begin{aligned} & \text{Fi}_{app} \coloneqq \text{qz}_{\text{ice.ant}} \cdot \text{G}_{\text{H}} \cdot \text{Ca}_{app} \cdot \text{K}_{\text{a}} \cdot \text{SA}_{\text{ICEappF}} \cdot \text{N}_{app} = 14 \\ & \text{SA}_{\text{ICEappS}} \coloneqq \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right)}{144} = 0.4 \end{aligned} \qquad \text{sf}$$

lbs

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 0.7$$
 sf

$$F_{app} := qz_m \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appF} \cdot N_{app} = 3$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 0.1$$
 sf

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appS} = 1$$
 lbs

$$\begin{split} &V_{app} \coloneqq L_{app} \cdot W_{app} \cdot T_{app} = 150 & \text{cu in} \\ &V_{ics} \coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \left(W_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 508 & \text{cu in} \\ &W_{ICEapp} \coloneqq \frac{V_{ice}}{1728} \cdot \text{Id} = 16 & \text{lbs} \end{split}$$

WICEapp 
$$\cdot$$
  $= \frac{1}{1728} \cdot 10 = 16$ 

WICEapp  $\cdot$  Napp = 16 lbs



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P: (203) 488-0580 F: (203) 488-8587 Subject:

TIA-222-H Loads

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Rev. 1: 11/9/23

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C.

lbs

lbs

lhs

lbs

Job No. 22017.06

#### Development of Wind & Ice Load on Appurtenances

#### Appurtenance Data:

Appurtenance Model =

Appurtenance Shape =

Appurtenance Height=

Appurtenance Width =

Appurtenance Thickness =

Appurtenance Weight=

Number of Appurtenances=

Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

#### Wind Land (without ice)

SurfaceArea for One Appurtenance (Front) =

Total Appurterance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurterance Wind Force =

# Wind Load (with ice)

SurfaceArea for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

SurfaceArea for One Appurtenance w/ Ice (Side) =

Total Appurtenance Wind Force w/ tce=

# Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

SurfaceArea for One Appurtenance (Side) =

Total Appurte rance Wind Force =

#### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of Ice on EachAppurtenance =

Weight of Ice on All Appurtemences =

#### Samsung RF4439-25A(B2/B66A)RRH

Flat

(User Input)

L<sub>app</sub> := 15

(User Input)

 $W_{app} = 15$ 

(User Input)

 $T_{app} = 10$ 

(User Input)

 $WT_{app} = 75$  lb

(User Input)

$$N_{app} := 1$$

(User Input)

$$Ar_{app} := \frac{L_{app}}{W_{app}} = 1.0$$

$$Ca_{app} = 1.2$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 1.6$$

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1$$

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 2.1$$
 si

$$Fi_{app} := qz_{ice.ant} \cdot G_{H} \cdot Ca_{app} \cdot K_a \cdot SA_{ICEappF} = 26$$

$$SA_{ICEappS} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right)}{144} = 1.5$$

$$Fi_{app} := qz_{ice.ant} \cdot G_{H} \cdot Ca_{app} \cdot K_a \cdot SA_{ICEappS} = 19$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 1.6$$

$$\mathsf{F}_{\mathsf{app}} \coloneqq \mathsf{qz}_{\mathsf{m}} \cdot \mathsf{G}_{\mathsf{H}} \cdot \mathsf{Ca}_{\mathsf{app}} \cdot \mathsf{K}_{\mathsf{a}} \cdot \mathsf{SA}_{\mathsf{appF}} = \mathsf{7}$$

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1$$
 sf

$$V_{app} := L_{app} \cdot W_{app} \cdot T_{app} = 2250$$
 cu in

$$\label{eq:Vice} \begin{aligned} \textbf{V}_{ice} \coloneqq \left(\textbf{L}_{app} + 2 \cdot \textbf{t}_{iz}\right) \! \left(\textbf{W}_{app} + 2 \cdot \textbf{t}_{iz}\right) \cdot \left(\textbf{T}_{app} + 2 \cdot \textbf{t}_{iz}\right) - \textbf{V}_{app} = \textbf{1610} \end{aligned} \qquad \text{cu in}$$

$$W_{ICEapp} := \frac{V_{ice}}{1728} \cdot Id = 52$$
 lbs

$$W_{\text{ICEapp}} \cdot N_{\text{app}} = 52$$
 lbs



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63-2 Worth Branford Road P: (203) 488-0580 Branford, CT 06405

Subject:

TIA-222-H Loads

Location:

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06

Rev. 1: 11/9/23

#### Development of Wind & Ice Load on Appurtenances

#### Appurtenance Data:

Appurtenance Model =

Appurtenance Shape =

Appurtenance Height=

Appurtenance Width =

Appurtenance Thickness =

Appurtenance Weight =

Number of Appurtenances=

Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

# Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurterance Wind Force =

SurfaceArea for One Appurtenance (Side) =

Total Appurterance Wind Force =

#### Wind Load (with ice)

SurfaceArea for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

Surface Area for One Appurtenance w/lce (Side) =

Total Appurtenance Wind Force w/be=

#### Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

#### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurte nances =

#### Samsung RF4461d-13A(B5/B13) RRH

(User Input)

 $L_{app} := 14.96$ (User Input)

Wapp := 14.96 (User Input)

 $T_{app} = 10.23$ (User Input)

 $WT_{app} := 80$ (User Input)

(User Input)  $N_{app} := 1$ 

 $Ar_{app} := \frac{L_{app}}{W_{app}} = 1.0$ 

 $Ca_{app} = 1.2$ 

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 1.6$$

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1.1$$
 sf

$$F_{app} := qz_{ant} \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appS} = 74$$
 lbs

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 2.1$$

Fi<sub>app</sub> := 
$$qz_{ice.ant} \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{tCEappF} = 26$$
 lbs  
 $SA_{tCEappS} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right)}{144} = 1.6$  sf

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 1.6$$
 sf

$$F_{ann} := qz_m \cdot G_H \cdot Ca_{ann} \cdot K_a \cdot SA_{ann} = 7$$
 lbs

$$F_{app} := qz_m \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appF} = 7$$
 lbs 
$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1.1$$
 sf

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appS} = 5$$
 lbs

$$\begin{aligned} &V_{app} \coloneqq L_{app} \cdot W_{app} \cdot T_{app} = 2289 \end{aligned} \qquad \text{cu in} \\ &V_{ice} \coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \left(W_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 1623 \end{aligned} \qquad \text{cu in}$$



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P: (203) 488-0580 F: (203) 488-8587 Subject:

TIA-222-H Loads

Location:

Rev. 1: 11/9/23

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C.

sf

lbs

lbs

ibs

lbs

cu in

Job No. 22017.06

#### Development of Wind & Ice Load on Appurtenances

#### Appurtenance Data:

Appurtenance Model =

Appurtenance Shape =

Appurtenance Height=

Appurtenance Width =

Appurtenance Thickness =

Appurtenance Weight=

Number of Appurtenances=

Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

#### Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurterance Wind Force =

#### Wind Load (with Ice)

SurfaceArea for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

SurfaceArea for One Appurtenance w/ Ice (Side) =

Total Appunerance Wind Force w/ Ice=

#### Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurte rance Wind Force =

#### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurterances =

# Samsung RF4423-48B RRH

Flat

(User Input)

L<sub>app</sub> := 11.8

(User Input)

W<sub>app</sub> := 8.7

(User Input)

in

(User Input)

 $T_{app} := 3.6$   $WT_{app} := 16$ 

\_

(User Input)

N<sub>app</sub>:= 1

(User Input)

$$Ar_{app} := \frac{L_{app}}{W_{app}} = 1.4$$

$$Ca_{app} = 1.2$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 0.7$$

$$F_{app} := qz_{ant} \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appF} = 50$$

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 0.3$$

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 1.1$$
 s

$$SA_{ICEappS} = \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right)}{144} = 0.6$$

$$Fi_{app} := qz_{ice.ant} \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{ICEappS} = 7$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 0.7$$

$$F_{app} := qz_m \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appF} = 3$$

$$SA_{appS} = \frac{L_{app} \cdot T_{app}}{144} = 0.3$$

$$F_{app} := qz_m \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appS} = 1$$

$$V_{app} := L_{app} \cdot W_{app} \cdot T_{app} = 370$$
 cu in

$$V_{ice} := \left(L_{app} + 2 \cdot t_{iz}\right) \left(W_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 621$$

$$W_{ICEapp} := \frac{V_{ice}}{1728} \cdot id = 20$$
 lbs

$$W_{ICEapp} \cdot N_{app} = 20$$
 lbs



Centered on Solutions 70 Pr. (203) 488-0580 Branford, CT 06405

Subject:

TIA-222-H Loads

Location:

Portland, CT

(User Input)

(User Input)

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06

Rev. 1: 11/9/23

#### Development of Wind & Ice Load on Appurtenances

#### Appurtenance Data:

OVP Box Appurtenance Model = Flat Appurtenance Shape =

Appurtenance Height= Lapp := 29.5 (User Input)

 $W_{app} := 16.5$ (User Input) Appurtenance Width =

T<sub>app</sub> := 12.6  $WT_{app} = 32$ (User Input) Appurtenance Weight=

(User Input) Number of Appurtenances=  $N_{app} = 1$ 

 $Ar_{app} := \frac{L_{app}}{W_{app}} = 1.8$ Appurtenance Aspect Ratio =

Ca<sub>app</sub> = 1.2 Appurtenance Force Coefficient =

# Wind Load (without ice)

Appurtenance Thickness =

Surface Area for One Appurtenance (Front) =

Total Appurterance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurte rance Wind Force =

# Wind Load (with ice)

SurfaceArea for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

SurfaceArea for One Appurtenance w/ Ice (Side) =

Total Appurterrance Wind Force w/ be=

# Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

# Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurtenances =

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 3.4$$
 sf

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 2.6$$
 sf

$$F_{app} := qz_{ant} \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appS} = 180$$

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 4.2$$

$$Fi_{app} := qz_{ice.ant} \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{ICEapp} = 51$$
 lbs

$$\begin{aligned} & \text{Fi}_{app} \coloneqq qz_{\text{ice.ant}} \cdot \textbf{G}_{\text{H}} \cdot \textbf{Ca}_{app} \cdot \textbf{K}_{\text{a}} \cdot \textbf{SA}_{\text{ICEappF}} = 51 & \text{lbs} \\ & \text{SA}_{\text{ICEappS}} \coloneqq \frac{\left(\textbf{L}_{app} + 2 \cdot \textbf{t}_{iz}\right) \cdot \left(\textbf{T}_{app} + 2 \cdot \textbf{t}_{iz}\right)}{144} = 3.4 & \text{sf} \end{aligned}$$

lbs

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 3.4$$
 sf

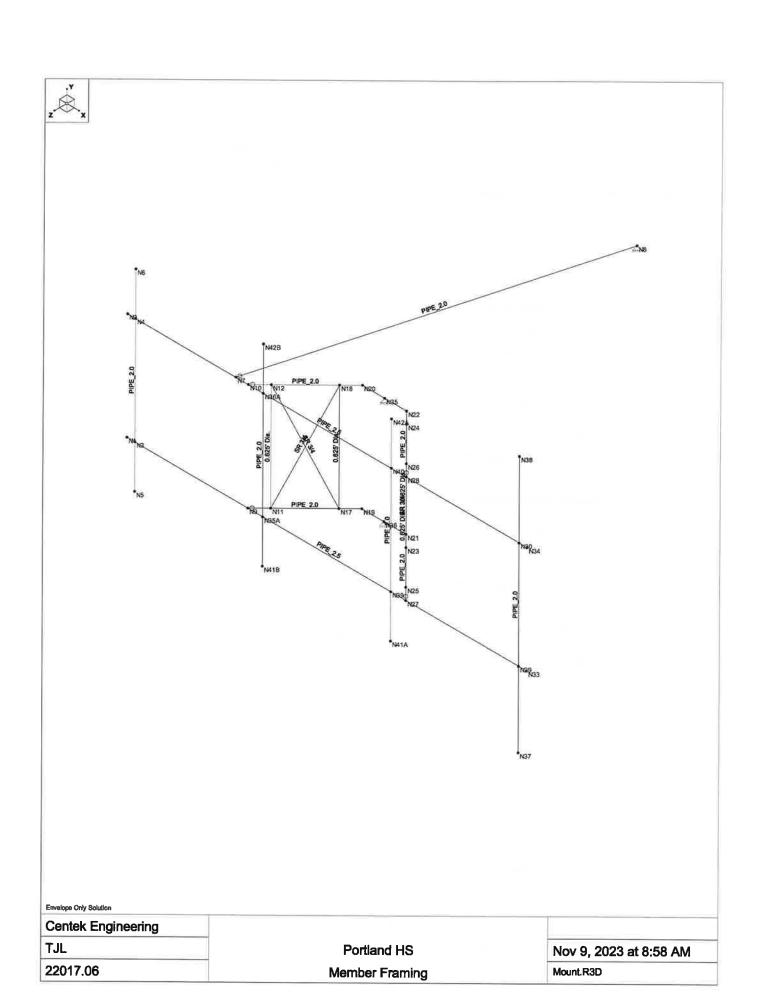
$$F_{app} := qz_m \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appF} = 15$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 2.6$$
 sf

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appS} = 11$$
 lbs

$$\begin{split} &V_{app} \coloneqq L_{app} \cdot W_{app} \cdot T_{app} = 6133 & \text{cu in} \\ &V_{ice} \coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \! \left(W_{app} + 2 \cdot t_{iz}\right) \! \cdot \! \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 3107 & \text{cu in} \end{split}$$

$$W_{ICEapp} := \frac{V_{ice}}{1728} \cdot Id = 101$$
 lbs





Company : Centek Engineering
Designer : TJL
Job Number : 22017.06
Model Name : Portland HS

Nov 9, 2023 8:57 AM Checked By:\_

# (Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (ft/sec^2)	32.2
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver

Hot Rolled Steel Code	AISC 15th(360-16): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 15th(360-16): LRFD
Cold Formed Steel Code	AISI S100-10: ASD
Wood Code	AWC NDS-12: ASD
Wood Temperature	< 100F
Concrete Code	ACI 318-11
Masonry Code	ACI 530-11: ASD
Aluminum Code	AA ADM1-10: ASD - Building
Stainless Steel Code	AISC 14th(360-10): ASD
Adjust Stiffness?	Yes(Iterative)

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8



Company Designer Job Number

: Centek Engineering

: TJL : 22017.06 Model Name : Portland HS Nov 9, 2023 8:57 AM Checked By:\_

# (Global) Model Settings, Continued

Seismic Code	ASCE 7-10
Seismic Base Elevation (ft)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
TX (sec)	Not Entered
T Z (sec)	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	l or II
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	1
Cd X	1
Rho Z	1 - 1
Rho X	1
Faction Overtuning Orbit F	
Footing Overturning Safety Factor	1
Optimize for OTM/Sliding	No
Check Concrete Bearing	No
Footing Concrete Weight (k/ft^3)	150.001
Footing Concrete f'c (ksi)	4
Footing Concrete Ec (ksi)	3644
Lambda	1
Footing Steel fy (ksi)	60
Minimum Steel	0.0018
Maximum Steel	0.0075
Footing Top Bar	#3
Footing Top Bar Cover (in)	2
Footing Bottom Bar	#3
Footing Bottom Bar Cover (in)	3.5
Pedestal Bar	#3
Pedestal Bar Cover (in)	1.5
Pedestal Ties	#3

# **Hot Rolled Steel Properties**

	Label	E [ksi]	G [ksi]	Nu	Therm (\ De	ensity[k/ft^3]	Yield[ksi]	Rv	Fu[ksi]	Rt
1	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	58	1.2
3	A992	29000	11154	.3	.65	.49	50	1.1	58	1.2
4	A500 Gr.42	29000	11154	.3	.65	.49	42	1.3	58	1.1
5	A500 Gr.46	29000	11154	.3	.65	.49	46	1.2	58	1.1
6	A53 Grade B	29000	11154	.3	.65	.49	35	1.5	58	1.2



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# Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design	A [in2]	lyy [in4]	Izz [in4]	J [in4]
1	Antenna Mast 2.0.	PIPE 2.0	Column	Pipe	A53 Grade B	Typical	1.02	.627	.627	1.25
2	Horizontal 2.5 ST	PIPE 2.5	Beam	Pipe	A53 Grade B	Typical	1.61	1.45	1.45	2.89
3	Outrigger 2.0 ST	PIPE 2.0	Beam	Pipe	A53 Grade B	Typical	1.02	.627	.627	1.25
4	Stabilizer 2.0 ST	PIPE 2.0	Beam	Pipe	A53 Grade B	Typical	1.02	.627	.627	1.25
5	0.625" Dia. Bar	0.625' Dia.	Column	BAR	A36 Gr.36	Typical	.307	.007	.007	.015
6	0.75"Dia. Bar	SR 3/4	Column	BAR	A36 Gr.36	Typical	.442	.016	.016	.031

Hot Rolled Steel Design Parameters

	Label	Shape	Length[ft]	Lbyy[ft]	Lbzz[ft]	Lcomp top[.	Lcomp bot[.	L-torq	Куу	Kzz	Cb	Functi.
1	M1	Horizontal_2.5 STD	12.5	Segment		Lbyy						Lateral
2	M2	Horizontal 2.5 STD		Segment		Lbyy				3.0		Lateral
3	M3	Stabilizer_2.0 STD	10.18			Lbyy						Lateral
4	M4	Outrigger_2.0 STD		Segment	Segment	Lbyy						Lateral
5	M5	Outrigger 2.0 STD	2.521	Segment	Segment	Lbyy						Lateral
6	M6	Outrigger 2.0 STD	2.521	Segment	Segment	Lbyy						Lateral
7	M7	Outrigger_2.0 STD			Segment							Lateral
8	M8	0.625" Dia. Bar	3.333				and the same			100		Lateral
9	M9	0.625" Dia. Bar	3.333									Lateral
10	M10	0.75"Dia, Bar	3.659	1.83	1.83	Lbyy						Lateral
11	M11	0.625" Dia. Bar	3.333									Lateral
12	M12	0.75"Dia. Bar	3.659	1.83	1.83	Lbyy						Lateral
13	M13	0.625" Dia. Bar	3.333									Lateral
14	M14	0.75"Dia. Bar	3.659	1.83	1.83	Lbyy						Lateral
15	M15	0.75"Dia. Bar	3.659	1.83	1.83	Lbyy						Lateral
16	PS.2	Antenna Mast 2.0	1			Lbyy						Lateral
17	PS.1	Antenna Mast 2.0			l l	Lbyy						Lateral
18	M19	Antenna Mast 2.0			- 1	Lbyy						Lateral
19	M21A	Antenna Mast 2.0	6			Lbyy						Lateral

Member Primary Data

	Label	I Joint	J Joint	K Joint	Rotate(	Section/Shape	Туре	Design List	Material	Design
1	M1	N2	N34	1.4.4.4		Horizontal_2.5 STD Pipe	Beam	Pipe	A53 Grade B	Typical
2	M2	N1	N33			Horizontal_2.5 STD Pipe	Beam	Pipe	A53 Grade B	Typical
3	M3	N7	N8			Stabilizer_2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
4	M4	N10	N20			Outrigger_2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
5	M5	N9	N19			Outrigger_2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
6	M6	N28	N22			Outrigger 2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
7	M7	N27	N21			Outrigger_2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
8	M8	N12	N11			0.625" Dia, Bar	Column	BAR	A36 Gr.36	Typical
9	M9	N18	N17			0.625" Dia, Bar	Column	BAR	A36 Gr.36	Typical
10	M10	N12	N17			0.75"Dia. Bar	Column	BAR	A36 Gr.36	Typical
11	M11	N26	N25			0.625" Dia. Bar	Column	BAR	A36 Gr.36	Typical
12	M12	N18	N11			0.75"Dia. Bar	Column	BAR	A36 Gr.36	Typical
13	M13	N24	N23			0.625" Dia. Bar	Column	BAR	A36 Gr.36	Typical
14	M14	N26	N23			0.75"Dia, Bar	Column	BAR	A36 Gr.36	Typical
15	M15	N24	N25			0.75"Dia. Bar	Column	BAR	A36 Gr.36	Typical
16	PS.2	N5	N6		8 20 0	Antenna Mast_2.0 STD Pi	Column	Pipe	A53 Grade B	Typical
17	PS.1	N37	N38			Antenna Mast_2.0 STD Pi		Pipe	A53 Grade B	Typical



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# Member Primary Data (Continued)

_	Label	I Joint	J Joint	K Joint Rotate		Type	Design List	Material	Design
18	M19	N41A	N42A		Antenna Mast 2.0 STD Pi	Column	Pipe	A53 Grade B	Typical
19	M20	N19	N21		RIGID	None	None	RIGID	Typical
20	M21	N20	N22		RIGID	None	None	RIGID	Typical
21	M21A	N41B	N42B		Antenna Mast_2.0 STD Pi	Column	Pipe	A53 Grade B	Typical

Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Dia
1	N1	0	0,	<b>-0</b> .	0	Doladii i Tolii Dia
2	N2	0	3.333334	-0.	0	
3	N3	.25	0.	-0.	0	
4	N4	.25	3.333334	-0.	0	
5	N5	.25	-1.333333	-0.	0	
6	N6	.25	4.666667	-0.	0	
7	N7	3.390625	3.333334	-0.	0	
8	N8	6.025403	3.333334	-9.833125	0	1.004
9	N9	3.78125	0.	-0.	0	
10	N10	3.78125	3.333334	-0.	0	
11	N11	4.138628	0.	-0.357378	0	
12	N12	4.138628	3.333334	-0.357378	0	
13	N17	5.206335	0.	-1.425085	0	
14	N18	5.206335	3.333334	-1.425085	0	
15	N19	5.563713	0.	-1.782463	0	
16	N20	5.563713	3.333334	-1.782463	0	C - LUIS I OF
17	N21	6.936287	0.	-1.782463	0	
18	N22	6.936287	3.333334	-1.782463	0	
19	N23	7.293665	0.	-1.425085	0	
20	N24	7.293665	3.333334	-1.425085	0	
21	N25	8.361372	0.	-0.357378	0	
22	N26	8.361372	3.333334	-0.357378	0	NUMBER OF
23	N27	8.71875	0.	-0.	0	
24	N28	8.71875	3.333334	-0.	0	
25	N29	12.25	0.	-0.	0	
26	N30	12.25	3.333334	-0.	0	
27	N33	12.5	0.	-0.	0	
28	N34	12.5	3.333334	-0.	0	
29	N35	6.25	3.333334	-1.782463	0	
30	N36	6.25	0.	-1.782463	0	
31	N35A	4.25	0,	-0.	0	
32	N36A	4.25	3.333334	-0.	0	
33	N37	12.25	-2.333333	0	0	
34	N38	12.25	5.666667	0	0	
35	N39	8.25	0.	-0.	0	
36	N40	8.25	3.333334	-0.	Ö	
37	N41A	8.25	-1.333333	-0.	0	
38	N42A	8.25	4.666667	-0.	Ö	
39	N41B	4.25	-1.333333	-0.	0	
40	N42B	4.25	4.666667	-0.	0	



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Joint Boundary Conditions

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
1	N8	Reaction	Reaction	Reaction			
2	N19					1110	
3	N20						
4	N17						
5	N18						
6	N21					The state of the s	
7	N22						
8	N23					4,000	
9	N24						
10	N35	Reaction	Reaction	Reaction		122	
11	N36	Reaction	Reaction	Reaction			

Member Point Loads (BLC 2 : Dead Load)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	Y	045	1.5
	PS.1	Y	045	6.5
3	PS.2	Y	03	2
4	PS.2	Y	03	4
5	PS.1	Y	075	3
3	PS.1	Y	08	5
7	M21A	Y	016	1
8	M19	Y	032	%50
9	M21A	Y	003	%50

Member Point Loads (BLC 3 : Ice Load)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	Y	098	1.5
2	PS.1	Y	098	6.5
3	PS.2	Y	035	2
4	PS.2	Y	035	4
5	PS.1	Y	052	3
6	PS.1	Y	053	5
7	M21A	Y	02	1
8	M19	Y	101	%50
9	M21A	Υ	016	%50

Member Point Loads (BLC 6 : Wind with Ice X)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	X	.034	1.5
2	PS.1	X	.034	6.5
3	PS.2	X	.011	2
4	PS.2	X	.011	4
5	PS.1	X	.019	3
6	PS.1	X	.019	5
7	M21A	X	.007	1
8	M19	X	.041	%50
9	M21A	X	.005	%50



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# Member Point Loads (BLC 7: Wind X)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	X	.142	1.5
2	PS.1	X	.142	6.5
3	PS.2	X	.039	2
4	PS.2	X	.039	4
5	PS.1	X	.073	3
6	PS.1	X	.074	5
7	M21A	X	.021	1
8	M19	X	.18	%50
9	M21A	X	.008	%50

# Member Point Loads (BLC 8 : Wm Wind X)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	X	.009	1.5
2	PS.1	X	.009	6.5
3	PS.2	X	.003	2
4	PS.2	X	.003	allades 4
5	PS.1	X	.005	3
6	PS.1	X	.005	5
7	M21A	X	.001	1
8	M19	X	.011	%50
9	M21A	X	.001	%50

# Member Point Loads (BLC 9: Wind with Ice Z)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	Z	.073	1.5
2	PS.1	Z	.073	6.5
3	PS.2	Z	.024	2
4	PS.2	Z	.024	4
5	M19	Z	.051	%50
6	M21A	Z	.014	%50

# Member Point Loads (BLC 10 : Wind Z)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	Z	.358	1.5
2	PS.1	Z	.358	6.5
3	PS.2	Z	.111	2
4	PS.2	Z	.111	4
5	M19	Z	.236	%50
6	M21A	7	.052	%50

# Member Point Loads (BLC 11 : Wm Wind Z)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	Z	.023	1.5
2	PS.1	Z	.023	6.5
3	PS.2	Z	.007	2
4	PS.2	Z	.007	4
5	M19	Z	.015	%50
6	M21A	Z	.003	%50



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Member Distributed Loads (BLC 6 : Wind with Ice X)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/	Start Location[ft,%]	End Location[ft,%]
1	M3	X	.003	.003	0	0
2	M4	X	.003	.003	0	0
3	M5	X	.003	.003	0	0
4	M6	X	.003	.003	0	0
5	M7	X	.003	.003	0	0
6	M8	X	.003	.003	0	0
7	M9	X	.003	.003	0	0
8	M10	X	.003	.003	0	0
9	M11	X	.003	.003	0	0
10	M12	X	.003	.003	0	0
11	M13	X	.003	.003	0	0
12	M14	X	.003	.003	0	0
13	M15	X	.003	.003	0	0
14	PS.2	X	.003	.003	0	0
15	PS.1	X	.003	.003	0	0
16	M19	X	.003	.003	0	0
17	M20	X	.003	.003	0	0
18	M21	X	.003	.003	0	0
19	M21A	X	.003	.003	0	0

Member Distributed Loads (BLC 7 : Wind X)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/.	Start Location[ft,%	] End Location[ft,%]
1	M3	X	.018	.018	0	.0
2	M4	X	.018	.018	0	0
3	M5	X	.018	.018	0	0
4	M6	X	.018	.018	0	0
5	M7	X	.018	.018	0	0
6	M8	X	.018	.018	0	0
7	M9	X	.018	.018	0	0
8	M10	X	.018	.018	0	0
9	M11	X	.018	.018	0	0
10	M12	X	.018	.018	0	0
11	M13	X	.018	.018	0	0
12	M14	X	.018	.018	0	0
13	M15	X	.018	.018	0	0
14	PS.2	X	.018	.018	0	0
15	PS.1	X	.018	.018	0	0
16	M19	X	.018	.018	0	0
17	M20	X	.018	.018	0	0
18	M21	X	.018	.018	0	0
19	M21A	X	.018	.018	0	0

Member Distributed Loads (BLC 8 : Wm Wind X)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/.	Start Location[ft,%]	End Location[ft,%]
1	M3	X	.003	.003	0	0
2	M4	X	.003	.003	0	0
3	M5	X	.003	.003	0	0
4	M6	X	.003	.003	0	0
5	M7	X	.003	.003	0	0
6	M8	X	.003	.003	0	0



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# Member Distributed Loads (BLC 8: Wm Wind X) (Continued)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/.	Start Location[ft.%	End Location[ft,%]
7	M9	X	.003	.003	0	0
8	M10	X	.003	.003	0	0
9	M11	X	.003	.003	0	Ō
10	M12	X	.003	.003	0	0
11	M13	X	.003	.003	0	0
12	M14	X	.003	.003	0	0
13	M15	X	.003	.003	0	0
14	PS.2	X	.003	.003	0	0
15	PS.1	X	.003	.003	0	0
16	M19	X	.003	.003	0	0
17	M20	X	.003	.003	0	0
18	M21	X	.003	.003	0	0
19	M21A	X	.003	.003	0	0

# Member Distributed Loads (BLC 9 : Wind with Ice Z)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/	Start Location[ft,%]	End Location[ft.%]
1	M1	Z	.003	.003	0	0
2	M2	Z	.003	.003	0	0
3	M3	Z	.003	.003	0	0
4	M4	Z	.003	.003	0	0
5	M5	Z	.003	.003	0	0
6	M6	Z	.003	.003	0	0
7	M7	Z	.003	.003	0	0
8	M8	Z	.003	.003	0	0
9	M9	Z	.003	.003	0	0
10	M10	Z	.003	.003	0	0
11	M11	Z	.003	.003	0	0
12	M12	Z	.003	.003	0	0
13	M13	Z	.003	.003	0	0
14	M14	Z	.003	.003	0	0
15	M15	Z	.003	.003	0	0
16	PS.2	Z	.003	.003	0	0
17	M19	Z	.003	.003	0	0
18	M20	Z	.003	.003	0	0
19	M21	Z	.003	.003	0	0
20	M21A	Z	.003	.003	0	0

# Member Distributed Loads (BLC 10 : Wind Z)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/	Start Location[ft.%]	End Location[ft.%]
1	M1	Z	.018	.018	0	0
2	M2	Z	.018	.018	0	0
3	M3	Z	.018	.018	0	0
4	M4	Z	.018	.018	0	0
5	M5	Z	.018	.018	0	0
6	M6	Z	.018	.018	0	0
7	M7	Z	.018	.018	0	0
8	M8	Z	.018	.018	0	0
9	M9	Z	.018	.018	0	0
10	M10	Z	.018	.018	0	0
11	M11	Z	.018	.018	0	0
12	M12	Z	.018	.018	0	0



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Member Distributed Loads (BLC 10 : Wind Z) (Continued)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/.	Start Location[ft,%	End Location[ft,%]
13	M13	Z	.018	.018	0	0
14	M14	Z	.018	.018	0	0
15	M15	Z	.018	.018	0	0
16	PS.2	Z	.018	.018	0	0
17	M19	Z	.018	.018	0	0
18	M20	7	.018	.018	0	0
19	M21	7	.018	.018	0	0
20	M21A	Z	.018	.018	0	0

Member Distributed Loads (BLC 11 : Wm Wind Z)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/	.Start Location[ft,%]	End Location[ft,%]
1	M1	Z	.003	.003	0	0
2	M2	Z	.003	.003	0	0
3	M3	Z	.003	.003	0	0
4	M4	Z	.003	.003	0	0
5	M5	Z	.003	.003	0	0
6	M6	Z	.003	.003	0	0
7	M7	Z	.003	.003	0	0
8	M8	Z	.003	.003	0	0
9	M9	Z	.003	.003	0	0
10	M10	Z	.003	.003	0	0
11	M11	Z	.003	.003	0	0
12	M12	Z	.003	.003	0	0
13	M13	Z	.003	.003	0	0
14	M14	Z	.003	.003	0	0
15	M15	Z	.003	.003	0	0
16	PS.2	Z	.003	.003	0	0
17	M19	Z	.003	.003	0	0
18	M20	Z	.003	.003	0	0
19	M21	Z	.003	.003	0	0
20	M21A	Z	.003	.003	0	0

# **Basic Load Cases**

	BLC Description	Category	X Gra	Y Gra	.Z Gra	Joint	Point	Distrib.	Area(	Surfa
1	Self Weight	None		-1						
2	Dead Load	None					9			
3	Ice Load	None					9			
4	Lm Maintenance Load (500lb)	None								
5	Ly Maintenance Load (250lb)	None								
6	Wind with Ice X	None					9	19		
7	Wind X	None					9	19		
8	Wm Wind X	None					9	19		
9	Wind with Ice Z	None					6	20		
10	Wind Z	None			3.37		6	20		
11	Wm Wind Z	None					6	20		



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# **Load Combinations**

	Description	So.	P	S	BLC	Fac.	BLC	Fac.	BLC	Fac	BLC	Fac.	.BLCF	ac	BLCFac	BLC	Fac.	BLC	Fac.	.BLCFac	BLC	Fac
1	1.4D	Yes		T				1.4														1
2	1.2D +1.5Lv	Yes	Y		1	1.2	2	1.2	5	1.5												131
3	1.2D + 1.0W (X-directi	Yes	Y					1.2		1												
4	1.2D + 1.0Di + 1.0Wi (	Yes	Y		1	1.2	2	1.2	3	1	6	1										
5	1.2D +1.5Lm+ 1.0Wm	Yes	Y		1	1.2	2	1.2	4	1.5	8	1										
6	1.2D + 1.0W (Z-directi	Yes	Y					1.2								15						
7	1.2D + 1.0Di + 1.0Wi (	Yes	Y				_	1.2		1	9	1									1	
8	1.2D +1.5Lm+ 1.0Wm	Yes	Y		1		_	1.2	_	1.5	11	1										

# **Envelope Joint Reactions**

	Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	.233	3	.025	1	.919	6	0	8	0	8	0	8
2		min	271	6	.021	3	-1.212	3	0	1	0	1	0	1
3	N35	max	133	6	.687	7	.804	3	0	8	0	8	0	8
4		min	-1.769	3	.384	3	-2.878	6	0	1	0	1	0	1
5	N36	max	.86	7	.658	4	.68	4	0	8	0	8	0	8
6		min	568	3	.247	6	958	6	0	1	0	1	0	1
7	Totals:	max	0	8	1.335	4	0	3			_			
8		min	-2.104	3	.827	8	-2.918	6						1 1

# **Envelope Joint Displacements**

	Joint		X [in]	LÇ	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotation [rad]	LC	Z Rotation [rad]	LC
1	N1	max	.063	3	.035	6	.3	6	3.976e-03	6	1.2e-02	6	9.437e-04	3
2		min	115	6	031	3	035	1	-2.189e-03	3	-4.5e-04	4	-9.599e-04	6
3	N2	max	.036	3	.035	6	.452	6	2.539e-03	6	1.23e-02	6	1.072e-03	3
4		min	045	6	032	3	009	4	-2.295e-03	3	-3.806e-04	4	-9.84e-04	6
5	N3	max	.063	3	.032	7	.264	6	3.976e-03	6	1.2e-02	6	9.436e-04	3
6		min	115	6	028	3	034	1	-2.189e-03	3	-4.5e-04	4	-9.599e-04	6
7	N4	max	.036	3	.032	7	.415	6	2.539e-03	6	1.23e-02	6	1.072e-03	3
8		min	045	6	028	3	008	4	-2.295e-03	3	-3.806e-04	4	-9.84e-04	6
9	N5	max	.079	3	.032	7	.201	6	3.906e-03	6	1.2e-02	6	1.014e-03	3
10		min	13	6	028	3	045	1	-2.189e-03	3	-4.5e-04	4	-9.599e-04	6
11	N6	max	.02	3	.032	7	.456	6	2.609e-03	6	1.23e-02	6	1.002e-03	3
12		min	029	6	028	3	041	3	-2.295e-03	3	-3.806e-04	4	-9.841e-04	6
13	N7	max	.036	3	.034	7	.016	3	1.447e-03	6	9.639e-03	6	6.175e-04	3
14		min	045	6	.011	3	018	6	-1.158e-03	3	-1.301e-03	3	-2.923e-04	6
15	N8	max	0	8	0	8	0	8	1.91e-03	1	7.888e-03	3	1.312e-03	3
16		min	0	1	0	1	0	1	1.435e-03	3	5.127e-05	2	-1.996e-04	6
17	N9	max	.062	3	.033	7	.082	3	2.235e-03	6	5.246e-03	6	3.777e-04	3
18		min	115	6	.013	3	152	6	-8.113e-04	3	-4.928e-04	1	-4.431e-04	6
19	N10	max	.036	3	.033	7	.023	3	1.311e-03	6	8.501e-03	6	3.855e-04	3
20		min	045	6	.013	3	061	6	-1.017e-03	3	-1.196e-03	3	-4.005e-04	7
21	N11	max	.05	3	.037	7	.069	3	2.019e-03	6	2.987e-03	3	1.281e-04	3
22		min	09	6	.013	3	127	6	-5.166e-04	3	-5.778e-03	6	-8.88e-04	6
23	N12	max	.024	3	.037	7	.012	3	1.391e-03	6	2.666e-03	3	4.435e-04	3
24		min	036	6	.013	3	053	6	-7.218e-04	3	-2.003e-03	6	-5.474e-04	7
25	N17	max	.011	3	.036	7	.031	3	1.191e-03	6	2.786e-03	3	-4.683e-04	3
26		min	02	6	.004	3	058	6	1.051e-04	3	-4.897e-03	6	-2.42e-03	7



Company Designer Job Number Model Name

Centek Engineering

: TJL : 22017.06 : Portland HS Nov 9, 2023 8:57 AM Checked By:\_\_\_

Envelope Joint Displacements (Continued)

	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotation [rad]	LC	Z Rotation [rad]	LC
27	N18	max	0	3	.036	7	005	2	1.01e-03	7	4.415e-04	3	-2.46e-04	3
	INTO	min	01	6	.004	3	029	6	-5.278e-05	3	-2.066e-03	6	-2.361e-03	7
28	NIAO			_	.004	7	.02	3	6.829e-04	7	2.43e-03	3	-4.687e-04	3
29	N19	max	0	8				6	3.857e-04	3	-4.619e-03	6	-3.33e-03	7
30		min	0	1	.004	3	038			7	-5.094e-04	2	-4.791e-04	3
31	N20	max	0	8	.027	7	004	2	6.565e-04	_	-3.094e-04 -2.371e-03	6	-3.328e-03	7
32		min	0	1	.004	3	02	6	4.026e-04	6		3	-4.687e-04	3
33	N21	max	0	8	004	3	.038	6	6.829e-04	7	2.43e-03			
34		min	0	1	027	7	02	3	3.857e-04	3	-4.619e-03	6	-3.33e-03	7
35	N22	max	0	8	004	3	.02	6	6.565e-04	7	-5.094e-04	2	-4.791e-04	3
36		min	0	1	027	7	.004	2	4.026e-04	6	-2.371e-03	6	-3.328e-03	7
37	N23	max	.011	3	008	3	.059	6	2.79e-04	3	2.787e-03	3	-6.364e-04	3
38		min	021	6	042	7	031	3	-3.293e-04	6	-5.187e-03	6	-2.611e-03	7
39	N24	max	001	3	008	3	.03	6	5.174e-04	3	5.077e-04	3	-3.814e-04	3
40		min	01	6	042	7	.005	2	-5.375e-04	6	-2.405e-03	6	-2.64e-03	7
41	N25	max	.049	3	019	3	.131	6	4.08e-04	3	3.007e-03	3	-1.206e-03	3
42	1120	min	092	6	049	7	069	3	-1.606e-03	6	-5.675e-03	6	-2.55e-03	7
43	N26	max	.024	3	019	3	.06	6	5.829e-04	3	2.813e-03	3	-5.439e-04	3
44	1420	min	038	6	049	7	014	3	-1.67e-03	6	-2.047e-03	6	-2.545e-03	7
45	N27	max	.062	3	028	3	.155	6	9.807e-04	3	3.068e-03	3	-1.82e-03	3
	INZ/	min	116	6	057	7	082	3	-1.518e-03	6	-1.661e-02	6	-3.895e-03	7
46	NICO			_	025	3	.069	6	1.105e-03	3	2.157e-03	3	-1.342e-03	3
47	N28	max	.037	3		-	027	3	-1.011e-03	6	-1.498e-02	6	-3.91e-03	7
48	1100	min	046	6	057	7	1.127	_	1.489e-03	3	2.584e-03	3	-7.332e-04	3
49	N29	max	.062	3	12	3		6		6	-2.599e-02	6	-4.428e-03	7
50		min	116	6	296	7	198	3	-4.803e-03	_	2.602e-03	3	-1.698e-03	3
51	N30	max	.037	3	12	3	1.022	6	1.555e-03	3		-	-4.426e-03	7
52		min	046	6	296	7	131	3	-6.971e-04	7	-2.611e-02	6		3
53	N33	max	.062	3	122	3	1.205	6	1.489e-03	3	2.584e-03	3	-7.333e-04	
54		min	116	6	31	7	206	3	-4.803e-03	6	-2.599e-02	6	-4.428e-03	7
55	N34	max	.037	3	125	3	1.1	6	1.555e-03	3	2.602e-03	3	-1.698e-03	3
56		min	046	6	31	7	139	3	-6.971e-04	7	-2.611e-02	6	-4.426e-03	7
57	N35	max	0	8	0	8	0	8	6.565e-04	7	-5.094e-04	2	-4.791e-04	3
58		min	0	1	0	1	0	1	4.026e-04	6	-2.371e-03	6	-3.328e-03	7
59	N36	max	0	8	0	8	0	8	6.829e-04	7	2.43e-03	3	-4.687e-04	3
60		min	0	1	0	1	0	1	3.857e-04	3	-4.619e-03	6	-3.33e-03	7
61	N35A	max	.062	3	.03	4	.072	3	1.958e-03	6	3.444e-03	6	1.989e-04	3
62	1100/1	min	115	6	.012	6	176	6	-7.375e-04	3	-5.307e-04	1	-7.034e-04	7
63	N36A	max	.036	3	.03	4	.028	3	1.14e-03	6	6.615e-03	6	1.487e-04	3
64	1400/1	min	045	6	.012	6	104	6	-8.946e-04	3	-6.161e-04	3	-6.81e-04	7
65	N37	max		3	12	3	1.292	6	1,488e-03	3	2.584e-03	3	1.322e-04	3
	INOT	min	206	6	296	7	24	3	-6.029e-03	6	-2.599e-02	6	-4.418e-03	7
66	NIO	max		4	12	3	1.06	6	1.556e-03	3	2.602e-03	3	-2.2e-03	2
67	N38		.043	6	296	7	087	3	-4.472e-04	7	-2.611e-02	6	-4.435e-03	7
68	NICO	min				6	.069	6	9.05e-04	3	3.152e-03	3	-1.268e-03	3
69	N39	max	.062	3	018		065	3	-1.203e-03	6	-1.414e-02	6	-2.813e-03	7
70	1110	min	116	6	038	4		2	9.904e-04	3	2.038e-03	3	-7.735e-04	3
71	N40	max	.037	3	018	6	002			6	-1.214e-02	6	-2.824e-03	7
72		min	046	6	038	4	015	3	-1.206e-03		3.152e-03	3	-1.198e-03	3
73	N41A	max		3	018	6	.089	6	9.05e-04	3		6	-2.813e-03	7
74		min	-,144	6	038	4	079	3	-1.273e-03	6	-1.414e-02			3
75	N42A	max		4	018	6	.001	3	9.904e-04	3	2.038e-03	3	-8.439e-04	
76		min	017	6	038	4	026	6	-1.135e-03	6	-1.214e-02	6	-2.824e-03	7
77	N41B	max		3	.03	4	.084	3	1.887e-03	6	3.444e-03	6	2.808e-04	3
		min	125	6	.012	6	207	6	-7.374e-04	3	-5.307e-04	11	-7.032e-04	7



Company Designer Job Number Model Name : Centek Engineering

: TJL : 22017.06 : Portland HS Nov 9, 2023 8:57 AM Checked By:\_\_\_

# **Envelope Joint Displacements (Continued)**

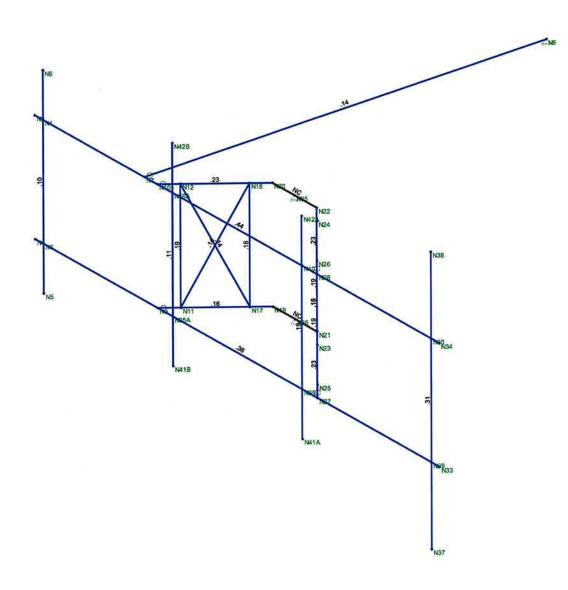
	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotation [rad]	LC	Z Rotation [rad]	LC
79	N42B	max	.034	3	.03	4	.017	4	1.211e-03	6		6	7.826e-05	3
80		min	036	6	.012	6	085	6	-8.947e-04	3	-6.161e-04	3	-6.81e-04	7

# Envelope AISC 15th(360-16): LRFD Steel Code Checks

	Mem	Shape	Code Check	L	LC	ShLoc	fftl	Dirphi*P	phi*P	phi*Mn y-y [k-ft]	phi*	Ch	Egn
1	M1	PIPE 2.5	.444	8	6	109 3.7		6 14.559		3.596	-	4-	H1
2	M2	PIPE 2.5	.383	8	6	.094 8.7		6 14.559	50.715	3.596		-	H1
3	M3	PIPE 2.0	.143	5	3	.009 10.	18	39.492	32.13	1.872		_	H1
4	M4	PIPE 2.0	.228	2	3	.084 2.5	21	3 32.032	32.13	1.872	1.8	1	H1.,
5	M5	PIPE 2.0	.160	2	7	.068 2.5	21	4 32.032	32.13	1.872		_	H1
6	M6	PIPE 2.0	.231	2	7	.086 .49	9	7 32.032	32.13	1.872	1.8	1	H1
7	M7	PIPE 2.0	.226	2	7	.091 .49	9	7 32.032	32.13	1.872	_	_	H1
8	M8	0.625' Dia.	.190	3	6	.024 3.3	33	61.058		.104	.104	2	H1
9	M9	0.625' Dia.	.177	0	3	.019 0		6 1.058	9.94	.104		_	H1
10	M10	SR 3/4	.141	0	3	.020 0		6 6.954		.179	.179	_	H1
11	M11	0.625' Dia.	.194	0	3	.023 0		6 1.058	9.94	.104	.104		H1
12	M12	SR 3/4	.144	0	3	.021 0		6 6.954		.179		-	H1
13	M13	0.625' Dia.	.194	0	3	.019 0		6 1.058	9.94	.104	.104	2	H1
14	M14	SR 3/4	.158	0	3	.017 0		6 6.954		.179	_	-	H1
15	M15	SR 3/4	.151	0	3	.018 0		66.954	14.314	.179		_	H1
16	PS.2	PIPE 2.0	.097	1	6	.027 1.37	75	6 20.867	32.13	1.872	1.8		-
17		PIPE 2.0	.311	5	4	.039 5.66		6 14.916		1.872			H1
18	M19	PIPE 2.0	.195	4	3	.058 4.62		6 20.867		1.872	1.8		_
19	M21A	PIPE_2.0	.113	1	6	.071 1.37		6 20.867		1.872			H1







Member Code Checks Displayed (Erveloped) Envelope Only Solution

Centek Engineering		
TJL	Portland HS	Nov 9, 2023 at 8:57 AM
22017.06	Unity Check	Mount.R3D

engineering

Subject:

Location:

Connection to Host Structure

Portland, CT

Rev. 0: 5/11/23

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06

### **Antenna Mount Connection:**

# Anchor Data:

A307 Threaded Rod =

Number of Anchor Bolts ≈

N := 4

(User Input)

Diameter of Bolts =

D := 0.625in

(User Input)

Design Tension =

T<sub>design</sub> := 10.4⋅kips

(User Input)

Design Shear =

V<sub>design</sub> ≔ 6.23-kips

(User Input)

Design Reactions:

Fx=

 $F_x := 1.7 \cdot kips$ 

(User Input)

Fy=

 $F_{\mathbf{V}} := 0.7 \cdot \mathbf{klps}$ 

(User Input)

Fz=

F<sub>7</sub> := 2.8-klps

(User Input)

#### Anchor Check:

Max Tension Force =

$$T_{Max} := \frac{F_z}{N} = 700lb$$

Max Shear Force =

$$V_{Max} := \frac{F_y}{N} + \frac{F_x}{N} = 600lb$$

Condition 1 =

Condition1 := if 
$$\left(\frac{T_{Max}}{T_{design}} + \frac{V_{Max}}{V_{design}} \le 1.0, "OK", "NG"\right) = "OK"$$

% of Capacity=

$$\max \left[ \frac{T_{Max}}{T_{design}}, \frac{V_{Max}}{V_{design}}, \frac{\left( \frac{T_{Max}}{T_{design}} + \frac{V_{Max}}{V_{design}} \right)}{1.0} \right] = 16.4 \%$$



# NORTHEAST > North East > New England > Wallingford-1 > PORTLAND HS CT - B

Cheiban, Ziad - ziad.cheiban@verizonwireless.com - 20230927\_153155

	ev4-2023-09-27 ise RF4461d-13A low band RRH and 6413 C-Band MMU
Project Scope	Rev4-2023-09-27 Use RF4461d-13A

						Antenn	Antenna Summary					
dded A	Infenna											
8	850	1900	AWS	CBRS	L-Sub6 Make	Make	Wodel	Center	Tip Height	Azimuth	Install	Quantit
					5G	Samsung	MT6413-77A	8	91.2	30(1),150(2),2 70(3)	PHYSICAL 3	6
쁘	5	T.	<u> </u>		5	COMMSCOPE	NNH4-65B-R6	8	89	30(1),150(2),2 70(3)	PHYSICAL 3	es es
				LTE		Samsung	RT4423	06	90.4	30(19),150(20) ,270(21)	PHYSICAL 3	60

Semoved.	Antenna											
002	850	1900	AWS	CBRS	F-Supe 1	Make	Wodel	Center	Tip Height	Azimuth	Install	Quantit

	all Quantit
	Install
	Azimuth
	Tlp Height
	Center
	Model
	Make
	F-Sub6
	CBRS
	1900 AWS
Antenna	920
Retained	200

d: 9 Removed: 0
d: 9 Retained: 0

						Non	Non Antenna Summary			
Added Non Antenna	ntenna									
Equipment Type	Location	200	820	1900	AWS	CBRS	Make	Model	Install	Quantity
Hybrid Cable	Tower						Hybrid Cables	1-1/4" Hybrid Cables	PHYSICAL	2
OVP	Tower							12 OVP	PHYSICAL	-
RRU	Tower			里	LIE		Samsung	B2/B66A RRH ORAN (RF4439d-25A)	PHYSICAL	က
RRU	Tower					LTE	Samsung	RF4423-48B	PHYSICAL	3
RRU	Tower	11	TE T				Samsung	RF4461d-13A	PHYSICAL	3

CBRS	AWS	1900	90 1900

	Quantity
	Install Type
	Arthroforn .
	Model
	Make
	CBRS
	AWS
	1900
	820
	002
Antenna	Location
Retained Non	Equipment Type

Added: 12 Removed: 0 Retained: 0	

Services			
700 LTE		0002 (8118082)	
Sector	01	02	03
Azimuth	30	150	270
Cell/Enodeb-ld	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
Antenna Make	COMMSCOPE	COMMSCOPE	COMMSCOPE
Centerline	06	06	06
DLEARFCN	5230	5230	5230
Mech Down-tilt	0	0	0
Elect Down-tilt	2	7	2
Tip Height	93	83	93
Regulatory Power	66.49 (W/MHz) ERP	66.49 (W/MHz) ERP	66.49 (W/MHz) ERP
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
ТМА Маке			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	RF4461d-13A	RF4461d-13A	RF4461d-13A
Number of Tx,Rx	4,4	4,4	4 , 4
Position			
Transmitter id	11232662	11232663	11232664
Source	VZNPP	VZNPP	VZNPP
Bandwidth	10	10	10
Ant Dimensions H x W x D(inch)	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79	72.0 × 19.6 × 7.79
Weight(Ib)	81.82	81.82	81.82

Services			
850 LTE		0002 (8118082)	
Sector	01	02	03
Azimuth	30	150	270
Cell/Enodeb-id	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
Antenna Make	COMMSCOPE	COMMSCOPE	COMMSCOPE
Centerline	06	06	06
DLEARFON	2450	2450	2450
Mech Down-tilt	0	0	0
Elect Down-tilt	2	2	2
Tip Height	93	93	63
Regulatory Power	301.17 (W/MHz) ERPSD	301.17 (W/MHz) ERPSD	301.17 (W/MHz) ERPSD
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	RF4461d-13A	RF4461d-13A	RF4461d-13A
Number of Tx, Rx	4,4	4 ' 4	4,4
Position			
Transmitter Id	11298595	11298596	11298597
Source	VZNPP	AZNPP	VZNPP
Bandwidth	10	10	10
Ant. Dimensions H x W x D(inch)	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79
Weight(lb)	81.82	81.82	81.82

1900 LTE           Sector         01           Sector         30           Cell/Enodeb-Id         064040           Antenna Make         COMMSC           Centerline         90           DLEARFCN         90           Mech Down-tilt         2           Tip Height         2           Tip Height         168.95 (M           TMA Make         168.0 dBm           TMA Make         100	01 30 064040 NNH4-65B-R6 COMMSCOPE	0002 (8118082)	
odeb-ld a Model a Model a Make ine FCN lown-tilt ght x Power x Power ake	040 14-65B-R6 AMSCOPE	02	
	040 14-65B-R6 AMSCOPE		03
	940 14-65B-R6 AMSCOPE	150	270
	14-65B-R6 AMSCOPE	064040	064040
	MASCOPE	NNH4-65B-R6	NNH4-65B-R6
		COMMSCOPE	COMMSCOPE
		06	06
		1050	1050
		0	0
La		2	2
		93	93
	168.95 (W/MHz) EIRP	168.95 (W/MHz) EIRP	168.95 (W/MHz) EIRP
IA Make	dBm	46.0 dBm	46.0 dBm
A Model			
RRU Make	sung	Samsung	Samsung
BZ/B66 (RF443	B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)
Number of Tx,Rx		4,4	4,4
Position			
Transmitter id	8592	11298593	11298594
Source	dd	VZNPP	VZNPP
10 Bandwidth		10	10
Ant. Dimensions  H.x.W.x.D(inch)	72.0 x 19.6 x 7.79	72.0 × 19.6 × 7.79	72.0 × 19.6 × 7.79
Weight(lb)	2	81.82	81.82

Services	S		
AWS LTE		0002 (8118082)	
Sector	01	02	03
Azimuth	30	150	270
Cell/Enodeb-ld	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
Antenna Make	COMMSCOPE	COMMSCOPE	COMMSCOPE
Centerline	06	06	06
DLEARFON	2050	2050	2050
Mech Down-tilt	0	0	0
Elect Down-tilt	2	2	2
Tip Height	63	93	93
Regulatory Power	84.67 (W/MHz) EIRP	84.67 (W/MHz) EIRP	84.67 (W/MHz) EIRP
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)
Number of Tx,Rx	4,4	4,4	4 , 4
Position			
Transmitter Id	11298467	11298468	11298469
Source	VZNPP	VZNPP	VZNPP
Bandwidth	20	20	20
Ant. Dimensions H x W x D(inch)	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79
Weight(lb)	81.82	81.82	81.82

	0002 (8118082)	
19	20	21
30	150	270
064040	064040	064040
RT4423	RT4423	RT4423
Samsung	Samsung	Samsung
06	06	06
55343, 55541, 55739, 55937	55343, 55541, 55739, 55937	55343, 55541, 55739, 55937
0	Q	0
7	7	7
90.4	90.4	90.4
3.76 (WMH12) EIRPSD, 3.76 (WMH12) EIRPSD, 3.76 (WMH12)	3.76 (W/MHz) EIRPSD, 3.76 (W/MHz) EIRPSD, 3.78 (W/MHz)	3.78 (WMHz) EIRPSD, 3.78 (WMHz) EIRPSD, 3.78 (WMHz)
37.02 dBm	37.02 dBm	37.02 dBm
Samsung	Samsung	Samsung
RF4423-40B	RF4423-48B	RF4423 48B
4 , 4	4,4	4,4
11298781	11298782	11298783
VZNPP	AZNPP	VZNPP
20, 20, 20, 20	20, 20, 20, 20	20, 20, 20, 20
8.7 × 12.0 × 1.5	8.7 x 12.0 x 1.5	8.7 × 12.0 × 1.5
333	33	3.3

	Services		
CBAND NR		0002 (8118082)	
Sector	0001	0002	6000
Azimuth	30	150	270
Cell/Enodeb-ld	0640040	0640040	0640040
Antenna Model	MT6413-77A	MT6413-77A	MT6413-77A
Antenna Make	Samsung	Samsung	Samsung
Centerline	06	06	06
DLEARFCN	650006, 655324	650006, 655324	650006, 655324
Mech Down-tilt	0	0	0
Elect Down-tilt	1	1	1
Tip Height	91.2	91.2	91.2
Regulatory Power	743.34 (W/MHz) EIRP, 743.34 (W/MHz) EIRP	743.34 (W/MHz) EIRP, 743.34 (W/MHz) EIRP	743.34 (W/MHz) EIRP, 743.34 (W/MHz) EIRP
Cell Max Power	52.02 dBm	52.02 dBm	52.02 dBm
ТМА Маке			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	MT6413-77A	MT6413-77A	MT6413-77A
Number of Tx,Rx	2,2	2,2	2,2
Position			
Transmitter id	11298702	11298703	11298704
Source	VZNPP	VZNPP	VZNPP
Bandwidth	100, 60	100, 60	100, 60
Ant. Dimensions H x W x D(inch)	29.53 x 15.75 x 5.51	29.53 x 15.75 x 5.51	29.53 x 15.75 x 5.51
Weight(lb)	55.1	55.1	55.1

LSub-6 CBRS	WRNES91,WF NES82,WRNE 583,WRNES8 4,WRNES85	CBRS_CALLS			WRNES81,WRNES82,WRNES83,WRNES84,WRNES85	WRNE585,WF NE596,WRNE 587,WRNE58	WRNESS1,WRNESS2,WRNESS3,WRNESS54,WRNESS5			CBRS_CALLS	WRNES8S,WR NES98,WRNE 587,WRNES8					CBRS_CALLS	WRNESBS,WH NESBB,WRNE 587,WRNESB				_
33 OH2 EE	WW S83				N 88.8	WR NE:	WR S83 W.4				WR. NES						WRI NES 587.				_
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1900	Ŋ											KNLH251,WP OJ730	KNLH251,WP 0J730					KNLH261,WP 0J730			
2				KNKAMO4				KNIKAADA	KNKA404												
902			WOJO689											WOJOERB	WOJOSB9						•
Regulator y Power	743.34	3.76	66.49	301.17	743.34	743.34	743.34	301.17	301.17	3.76	743.34	168.95	168.95	86.49			743,34	188.95	64.67	64.67	
Bandwidth	105	19	69.75	99	105	105	105	65			105	60.75	60.75	69.75			105	60.75	63.5	63.5	
Cie Cie	23.15	10.34	11.94	12.54	23.15	23.15	23.15	12.54	12.54	10,34	23.15	13.92	13.92	11.94		10.34	23.15	13.92	13.93	13.93	
Mech Down-tilt	0	0	0	0	0	0	0	0		0	0	0	0	0	0	0	0	0	0	0	
Elect Down-tilt	*	7	2	2	+	•	÷	2	2	7		2	2	2	2	7	-	2	2	2	
Azimuth	270	30	150	270	160	150	30	150	30	270	30	150	270	270	30	150	270	30	270	150	
H H	91,2	90.4	93	93	91.2	91.2	91.2	83	83	90.4	91.2	93	83	83		90.4	91.2	83	83	93	
Ant CL Height AG	06	8				8					08	06	06		06		06	06	06	06	
ego.	MT6413-77A	RT4423	NNH4-65B-R	NNH4-65B-R	MT6413-77A 90		MT6413-77A	NH4-658-R	NH4-658-R	RT4423				INH4-658-R 8	INH4-65B-R 6	RT4423		4NH4-65B-R 8	NH4-658-R 9	NH4-65B-R 9	
	Samsung	Samsung	COMMSCOPE NNH4-65B-R		Samsung		Samsung	COMMSCOPE	COMMSCOPENNH4-658-R 90	Sameung	Semanng	COMMSCOPE NNH4-65B-R	COMMSCOPE NNH4-85B-R	COMMSCOPE NNH4-658-R	强		Samsung	COMMSCOPE NNH4-65B-R	COMMSCOPE NNH4-658-R	COMMSCOPE NNH4-65B-R	
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E	1000	P04	1840	0481		<del>2</del> 5	0940	1640	1640	040	1840	0481
y Power	86.49	301.17	168.95	164.96	3.76	79.70	743.34	743.34	743.34	743.34	743.34	78, 87
Range 4	776.000 - 787.000/. 000 - .000	969.000 - 980.000/8 90.000 - 691.500	1975.000 1960.000/ .000 - .000	1970.000 1975.000/ .000 -	÷	2110.000 2120.000/ .000 -	- 000,000.	- 000. - 000. 000.	- 000.	- 000.	- 000.	2120.000 2130.000/ .000 -
Range 3	746.000 - 757.000/. 000 -	824.000 - 835.000/8 45.000 - 846.500	1895.000 1900.000/ .000 - .000	1890.000 1895.000/ .000 -	3.	1710.000 1720.000/ .000 -	3700.000 3720.000/ .000 -	3720.000 3740.000/ .000 -	3740.000 3760.000/ .000 -	3780.000 3780.000/ .000 -	3780.000 3800.000/ .000 -	1720.000 1730.000/ .000 -
Range 2	776.000 - 787.000/. 000 -	968.000 - 180.000/8 90.000 - 861.500	1875.000 1880.000/ .000 -	1870.000 1975.000/ .000 -	UNLICENSE DAULICEN SED - UNLICEN	2110.000 2120.000/ .000 -	- 000. - 000.000. 000	- 000.	- 000. - 000. 000	.000. .000,000. 000	- 000° - 000'/000° -	2120.060 2130.000/ .000 -
Range 1	746.000 - 757.000/. 000 - .000	824.000 - 835.000/8 45.000 - 846.500	1965,000 1900,000/ .000 -	1860.000 1895.000/ .000 -	UNLICENSE DAULICEN SED - UNLICENSE	1710.000 1720.009/ .000 -	3700.000 3720.000/ .000 -	3720.000 3740.000/ .000 -	3740.000 3760.000/ .000 -	3760.000 3780.000/ .000 -	3780.000 3800.000/ .000 -	1726.000 1730.000 .000 .000
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e May	Celico Partnerah Ip	Celico Partnersh ip	Celico Partnerah ip	Celico Partnersh ip	UNLICENSE	Celico Partnersh Ip	Celico Partnersh ip	Cellco Pertnersh ip	Celico Partnerah Ip	Celico Partnerah ip	Celico Partnerah ip	Celleo Partnersh ip
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	WQJQ686	KNKA404	WPOJ730	KNLH281	CBRS_CALL	WQGB276	WRNES61	WRNE582	WRNE583	WRNES64	WRNESSES	WQQAS06

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97 HIGH STREET PORTLAND, CT 08480

# SITE NAME: PORTLAND HS CT Verizon

PORTLAND, CT 06480 SITE ID: 616480547 97 HIGH STREET

INSTALL (3) PROPOSED SAUSUING BZ/BEBA FRRI ORUM (76744364-214) PAUTIO REDALL (3) PROPOSED SALESUNG RS/813 RM ONWA (1644616-134) RATED

PETALL (3) PROPOSED SALELYS STAASS ANDWAS WITH HAT (187422—488)

DISTALL (3) SECTIOR FRAME ANTIDOM MOLINTS, TIP. (1) PER SECTION

BETALL CARLE KE-BEDGE

NSTALL (1) PROPOSED RAYCUP OVP 12

NETALL UNEITHER FRAME TO ACCOMPOSATE EXCENDED PRESILATIO

10. NSTALL NEW SAWAT METER (PISSO)

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PROJECT INFORMATION

PORTAND HS CT

THE PROPOSED SCORE OF WORLDOOD OF A MODERATION TO THE EXCENSIVE PLACEMENT WILLIAM ONE FOLLOWING: NETALL (3) PROPUESD SAMBING WIRATESTA MEDIANS WITH INTERNATED

PROJECT SUMMARY



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ALL UTLOTY WORK SHALL BE IN ACCORDANCE WITH LOCAL UTLOTY COLPANY REQUIREMENTS AND SPECIFICATIONS.

CENERAL NOTES

CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON-SITE SAFETY FING. THE THE THE VID IS AWARDED LIVE. ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER,

BETONE BEDWAND THE WORK, THE COMPACTOR IS RESPONSIBLE FOR MAKEN SIGH INTERCHAPIONS CONDUCTORING PRINCIAL CONDITIONS (SURVICE AND SUBSURFACE) AT ON COMPILIOUS TO THE SITE, WHICH WAY AFTER PEDENDAMINES AND COST OF THE WORK.

CONTINUED WHIT REPAY IN DEPAYS AND RESTRICTIONS IN INC. CONTINUED WHIT RESTRICTIONS IN INC. CONTINUED WHILL CONTINUED SHALL CONTINUED SHALL REPAY IN THE SET OF DEMANS. THE CONTINUED SHALL REPAY IN CASE OF SHARLES AND THE SHARLES WE NAME THE SHARLES WE NAME THE SHARLES WE NAME THE SHARLES WE NAME THE SHARLES WE SHARLES

SHOULD ANY FIELD CONDITIONS PRECIALLY COMPLANCE WITH THE PROMINES, THE COMPLETIONS SHALL HANDWITCH NOTIFY THE DIGNOSTRY AND SHALL NOT PROCEED WITH ANY AFFECTED WORK,

CONTINCTION TO REVERY ALL SHOP UNAWAGE AND SUBMIT COPY TO EXCHEDIS FOR APPROVAL. INAMENCIA MOST BEAM THE CHECKET'S HITHEL BETWEE SABMITHEN TO THE CONSTRUCTION WANAGER FOR REVERY.



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THE COUNTY/DITY/TOWN MAY MAKE PERIODIC PIELD INSTITUTIONS TO EPISATE COMPLIANCE WITH THE DESIGN PLANS, SPECIFICATIONS, AND CONTRACT DOCUMENTS. CONTRACTOR SAVIL COMPLY WITH THE OWNER'S DAYROWARDHING BOUNDED ON ALL METHOUS AND PREPASSIONE FOR ALL EXCHANGEN ACTURES OF STATEMENT SET DESCRIPTION.

COORTINGTOR THE WARRANT OF CONTRACTOR OF CONSISSION OF STEPSTATION OF STEP AT ALL THESE AND RESIDE CONTRACTOR THE WAS RESIDENCE OF STEPSTATIONS AND OTHER STEAMEN PARTIES. SO WAS NOT NOT NOT AN OTHER STEAMEN STEAMEN

COMPACTOR SHALL SCAURE AND PAY FOR ALL PENAITS AND ALL INSPECTIONS REQUIRED FOR THE OBSERVE CONSTRUCTION, PLUIDENC, ELECTROLL, AND HAYC PENAITS SHALL RE, PAID FOR IT HE RESPECTIVE SUBCOMPACTORS.

CONTRACTOR SHALL PROVIDE A COMPLETE BUILD—OUT WITH ALL PROPRESS. PROCESSAL, ENTENDANCE, AND PRESTINGS. COMPORENTS AND PROVIDE OF THE DRAWMING ON IN THE WRITTEN SPECIFICATIONS. AS THE WORK PRODESSES, THE CONTRACTOR SHALL NOTIFY THE OWNER OF ALT COURTING WEAR JAKE IN CONSTITUTION OF INSTANCE WAS TOROGENED WHY THE CONSTITUTION DOCUMENTS. AND SHALL REPORTED THE WAS VALUE TO THE CONSTITUTION OF SHARL THE CONSTITUTION SHARP CONSTITUTION TO SHARP CONSTITUTION TO SHARP CONSTITUTION.

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COMEX ENGINEERING, INC. 83-2 NORTH BRUNFORD ROA BRUNFORD, CT. 08408 CARLO F. CENTORE, PE (203) 486-0560 EXT. 122

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CENERAL NOTES

SHOLLD ANY FIELD COMPILING PRESLIDE COMPLANCE WITH THE DRAWNES, THE COMPLICATION GIVEL INC. PROCESSI WITH ANY APPLICATION WORK.

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EXPERSE CODE 2021 RIEDANTINAL BREDAG (RC) AS MODERD BY THE 2022 CONNECTOR STATE BREDAM CODE.

NOTES AND SPECIFICATIONS:

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CONTRACTOR SAVEL PROVIDE A DOMENTE BILD-OUT WITH ALL FRENESS, STRUCTURAL, RECEIVANCE, AND ILLEMENT OF MACHINE AND INTERIOR AS THE WORN PROPERSIES. THE CONTINUED SAUL MOTIVE THE OWNER OF ANY CONTINUES WICH, HE IS CONTINUED WITH THE CONTINUES WITH THE CONTINUES WOUNDERS, NO SAUL HOT PROCEED BITS STOCK WORN WITH THE CONTINUES OF SAULKETTEN WAS AND SAUL HOT PROCEED BITS STOCK WITH THE CONTINUES OF SAULKETTEN.

F ANY PLIA CONCINUES DOST WHICH PRESLUCE COMPLIANTS WITH THE DOWNESS, THE CONTRICTOR SHALL MANDALES WERFY THE DISCUSS AND SHALL PROCESSOR WITH AFFECTED WITH COMPLET IS SATELYCOMELY PROCESSOR. CONTACTOR DALL MANAZE DETURNOCE TO DETTING STE CARBO CONTRICTOR, DOSIDIO CORRO, MANAZES, SALL IR. H CONFORMACE WITH THE LOCAL CACRELINES FOR DICKNOW AND SECUNDAL CONTROL.

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LOCATOR OF DUPUNDE AND WORK ELPHAND BY OTHORS THAT IS DAMPHALLYCALLY SECURIOR OF THE GENERAL STATISTICALLY SOCIETY SHALL ESTIMATED BY THE CONNECTOR THE CONTINUES AND REPORTED SHARED TO STRUCTURAL CONTINUES AND REPORT OF THE SHADOFFINESS.

44. CONFERT WE PROTOCOL PRESENCE AND THE REVENUE OF CONTRICTOR AND REPORTED TO THE UNIVERSITY OF THE CONTRICTOR TO THE C

ON THE CHARMER.	13. LDCK WIGHER ARE NOT PERMITTED FOR AZES STEEL ASSESSMENT.	14. SHOP CONSCIOUS SHULL BE WILLD OR HIGH SPECIAL DOUBLE. AT	18. WILL BEAVEN BUCK OF COLLINES, STIFFBEDS, AND OTHER BEARAS SUFFICES TO TRAVERER LAND OVER BRITISE CALCES BELIEBA.	IL PARROCE ROAD WITH MIL DAWN UP,	17. LEAST AND PLEASE HENNIGHA, MESSERS OF THE STRUCTURE TO AN ACCURACY OF 16003, BUT NOT TO EXCESS 1/4" IN THE FULL HEART OF THE COLLINA.	18. COMMENCEMENT OF STREATHERS, STREAM WITHOUT MOTIFYING THE ENGINEERS OF ANY DESCRIPTIONS WILL BE CONSISTENDED ACCOUNTING OF PROSECULAR STORY.
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ii.	2	
NAMED BY AN INCOPPORTY TRAINED LABORATORY.	CORRES OF ALL DESPENDENT TEST REPORTED BALL DE SUBMETTED TO THE ENGINEES IN TEST (10) WORNEDOWN DAYS OF THE DATE OF PROPERTIESAL.	
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	(F/P) CARES (		W W		Т	TO BATZ HYBRELE			100	
ANTENNA/APPURTENANCE SCHEDULE	(Lub) new (d/2)	37 (0) Switched cases 1984-1784-225-488 (1), (9) 049-13 (1)	30 (0) SWICHO IN/013 WH ONN (STASSG-130 (1), (0) SASCING IC/MAA INI CRUM CREASED IN THE CRUM CREASED IN CREASE		150 (0) SHATISHO CORCI 1984—1714433—400 (1)	130" (0) SAMELING MACHES AND COMM (MCALAGE-15A) (1) ON NAMES OF PARKS AND COMM (MCALAGE-15A)		TY (P) SAUCHO CHE 1994-EF423-489 (I)	270 (0) SANCIARO BD/213 PER CRAII (DESASTE-134) (1), (P) SANCIARO ED/MAN HEN CHAIN (MICHAEL-PAN) (1)	
/API	AZDAUTH	R	8	R	180	180	190	NI.		27.0
ENNA	HIDACK & ACRES	8	8	'n	20	200	ķ	.04	,06	,06
ANT	(G x M x 1)	125 + 67 + 15	71.8 x 18.8 x 7.7	28. x 16.75 x 5.5	120 : 67 : 15	71.8 x 10.0 x 7.7	250 x 15.75 x 5.5	120 × 67 ± 1.5	71.9 x 10.6 x 7.7	MY : 15.75 v 2.5
	мизми (сту)	SAMBLER ATTACES	COMMISCOPC, NOME—BIRE-RS	SMELLINGS MITSHES-TIX	SAUGING: KT423	CONNECOMO: NAMA-896-RS	SACCING MENTO-TTA	SAMELING: KTA433	COMMISCORY: NAME—850—95	EARCHAID: MISA13-778
	D33740,790F05ED	PROPOSED	PROPOSED	PROPOSED	PROPOSED	PROPOSED	PROPOSES	PROPOSED	PROPOSED	PROPOSED
	- 1		100			1111				

STRUCTURAL STEEL	1. ALL STRUCTURE, STED, G DI	A STRUCTARA STILL R. STRUCK STULL	(FY - 44 KS)  D. STRUCTION, HES (POLIN
	S. BLT F ANY WORK SHOULD BE RECURED UNITS, COOKS, MALES, OR RESOLUTIONS	MILES IN 165 WORK AND BALL THE SLOT OFFINANCES, LINES, DOCCS,	ALL UTILITY WORK SHULL BE IN ACCORDANCE WITH LOCAL, UTILITY COMPANY RECURBINENTS.
	D TO ANY ORDINACES, UNIT, O	CONSTITUTION ACCORDANCE IN CO.	HALL BE IN ACCORDANCE WITH
2000 CONTRACTOR OF THE CONTRAC	TO OK SANSTANDAY	OCCUR DE WORK	A. ALL UNLINY WORK 3 AND SPECIFICATIONS

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CONTRACTOR TO RENEW ALL SHOP ENLANGED AND STREET FORTING THE RENEW SHOW COMMENTS SHALL WELLOW THE PROPELLE SHALL CONCURRENCE REMINISCHED OF FERRINGS AND ACCESSIONER. RELIEFE DESCRIPTION SHOW	STRUCTURAL STEEL SHALL BE DETAILD, FAGRICATED AND ENERTED P. THE LATERT PREMISERS OF AND MAKIN, OF STEEL CHARTER PATTY.

6. ALL BITE ALTERA, (CONCED TO PROFILED BINLE DE OLEMENZO ATES FABRICA MONEGARE MEN ANTIN ALES "ZING (NOT ORPID OLEMENZO) CONTINGE" ON BON STELL PROGUES.	I. ALL BOLTS, ANCHORS AND MEDIZLAMENUS HARDWARE SHALL BE CALLANDED IN ACCORDANCE WITH ACTA ALSS "ZINC CONTING (HOT-OR!) ON HOW AND SITES. HARD	IN. THE DICHELY SHALL BE NOTITED OF ANY RECORDERLY FARBURED, DAMEED OR
M. (DOODED H. ASTN. A123	H ASTLA A163	MALE NO.
TO WEATHERN ZING (NOT 0	MUNICO CHECK	D OF ANY B
EPPED ONLYNA	MOTHER BY	COMMENT
ALMANDED AFTE (ZZD) CONTINGE	CL BE CALVINE	ASSECUTED, DA
ON NO	100 E	10 CEN

78 75	MAL SENSO BACK OF COLLEGE STIFFBERS, AND CHEST BEARING SO	TRANSPER LOAD DAER EMME CALORS RECTION.	IN PARTICUL HOUSE WITH MALL CHARGE UP,	17. LENEL AND PLIME DEPARTUR, INDIRECTS OF THE STRUCTURE TO AN ACCURA. BUT NOT TO DIDEED 1/4" IN THE FILL HOM OF THE COLUMN.	
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19. DESPECTION AND TESTING OF ALL MELDING AND MICH. STRENGTH BOLTING SPALL RE. PERFORMED BY AN MODESHOSYT TESTING LABORATORY.	FE.
ě	20. POER COPPES OF ALL RESPONDENTS SWALL DE SUBMETED TO THE ENVEY DETECTION TO THE ENVEY OF THE DATE OF RESPONDENCE.

**JENTEK** 

PORTLAND CT, 06460

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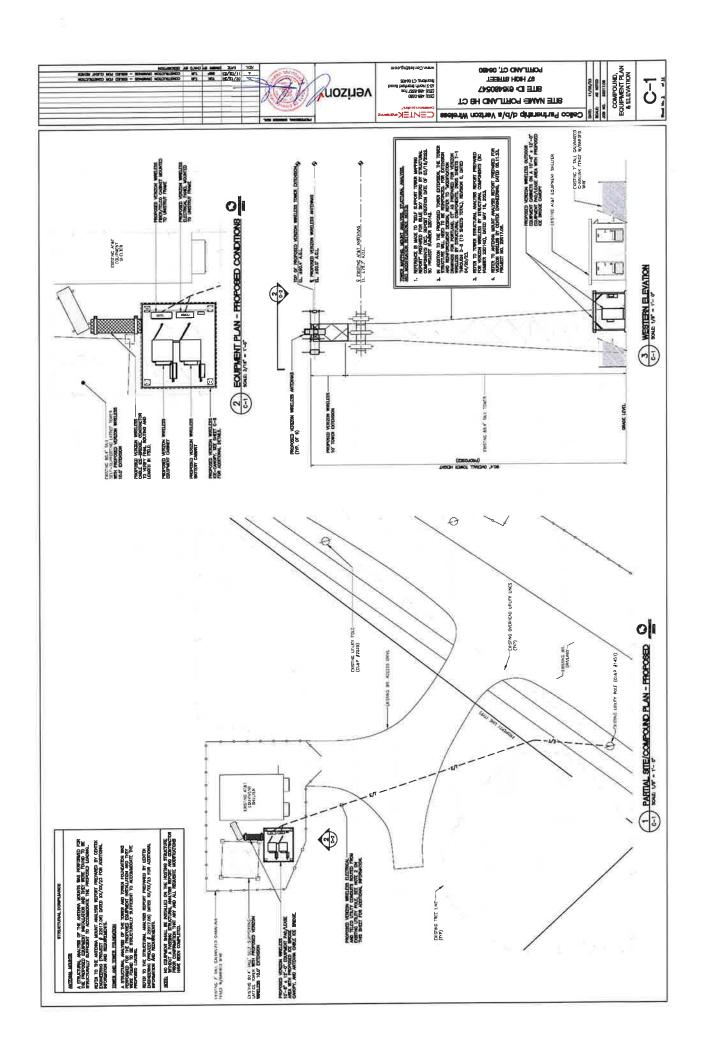
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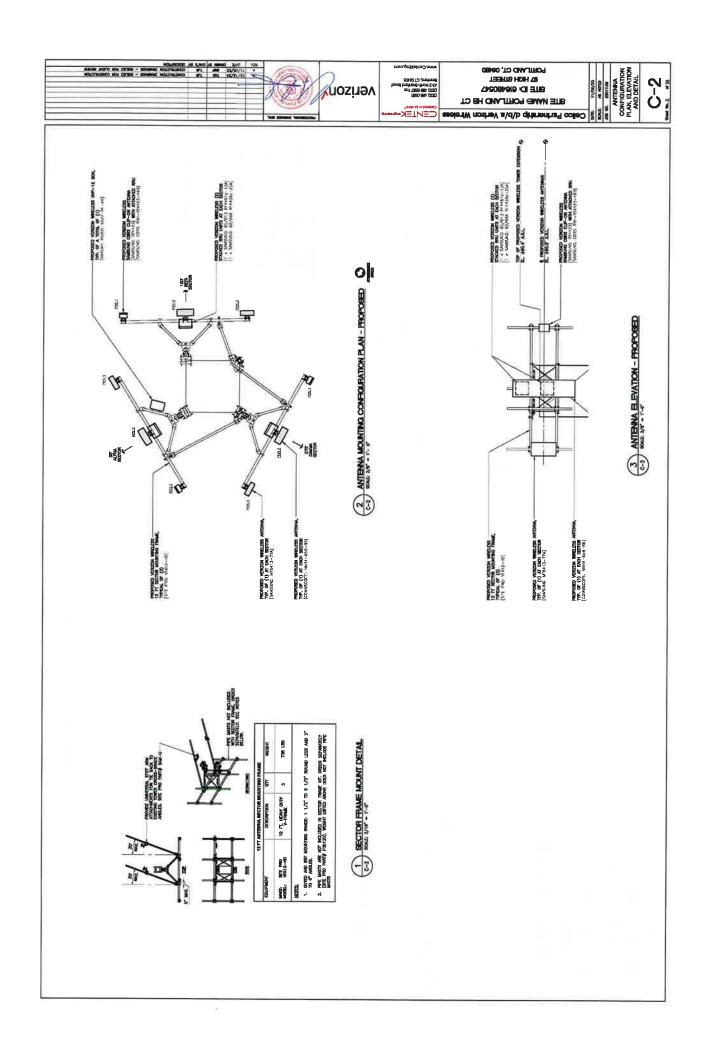
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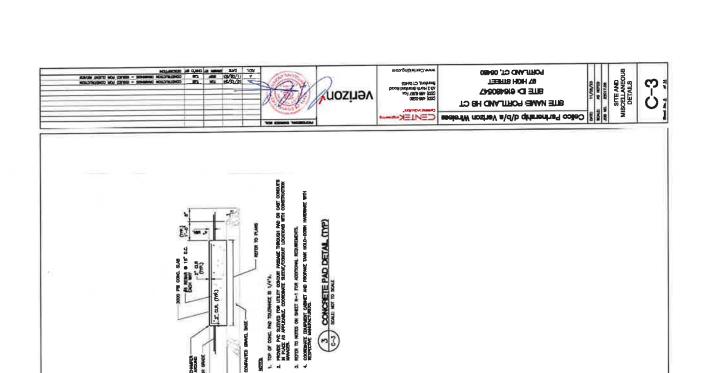
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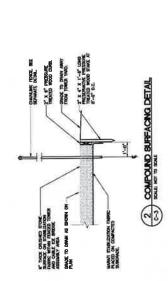
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ESTRO (4/2) (AUS) DAN (4/2) HUTNICE S SHOOMEN	NOT NOT SHARING CHEE THE STATE OF US OF US OF	NO NO SAME DESCRIPTION OF THE PARTY OF STREET AND COLUMN STREET AN		60" 150" (0) switching color (84-171423-480 (1)	Ser 100 (0) swatter births wit daw (british-12) (1) (b) swatter as one case (see case	W 150	90" T TY (P) SMEASO CHIC 1901-1714(3)-488 (1)	BOT 270 (D) SAMSUMO BD/253 MEN COMM CREADIG-12A) (1), CP) SAMSUMO BD/266A MEN CHEATURE DAY) (1)	
CL x W k D)	125 : 87 : 15 8	71.8 x 18.8 x 2.7 W	28.8 × 16.75 × 6.5 90	120 x 87 x 1.0 90	71.8 x 10.6 x 7.3 60	200 a 15.75 x 8.5 90	120 x 87 x 1.5 90	71.9 x 10.8 x 7.7 90	
мизми (ату)	SWELLER ATTACES	COMMISCOPE, MAIN-MIN-RS	SAMELING: WISHIS-77A	SAUSUNCE KT4423	COMMISCONE: NAME-BRE-RIS	SACCIONO MISA13-17A	SAMERACE ATHERS	SH-SSS-HINN GARDENGO	
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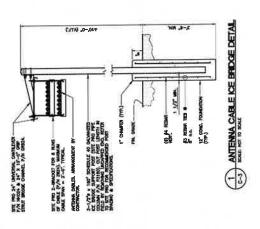


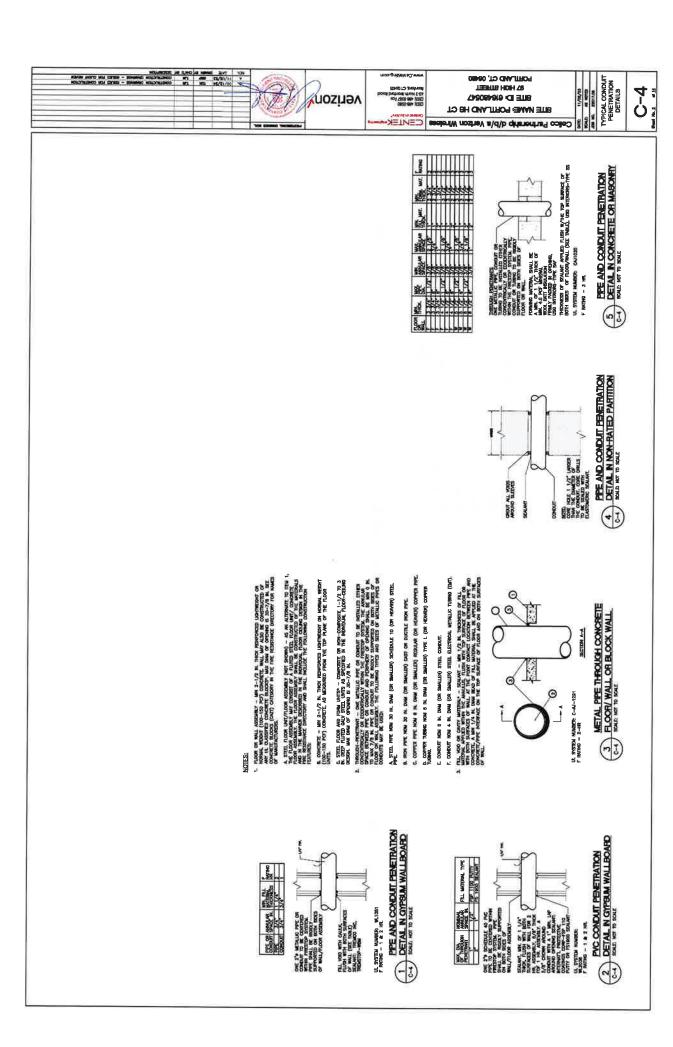


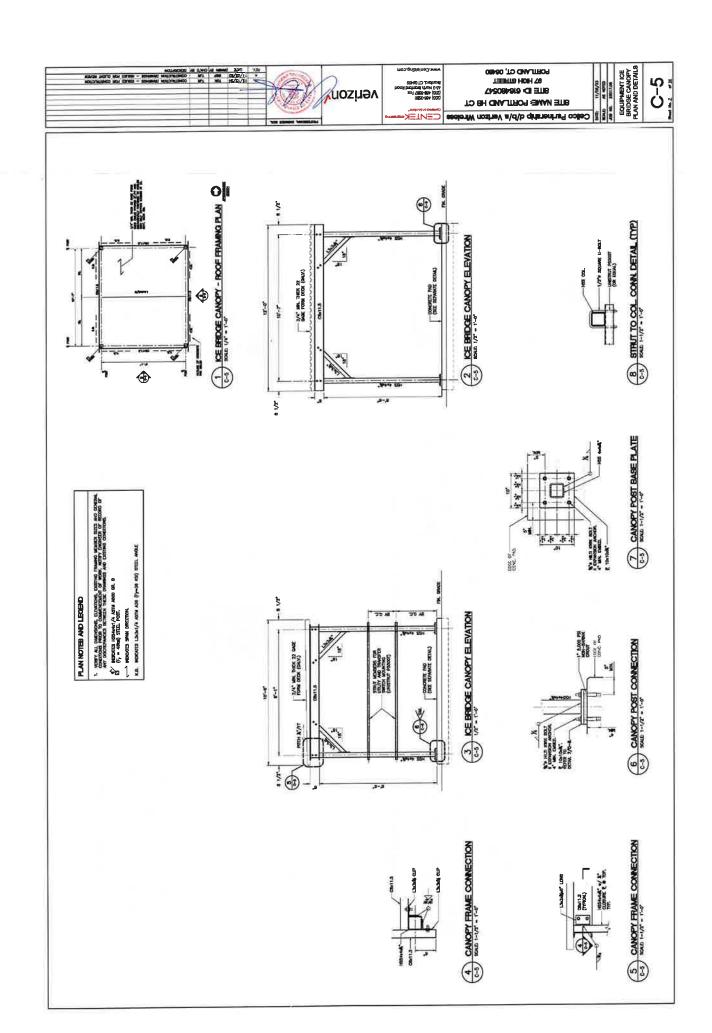


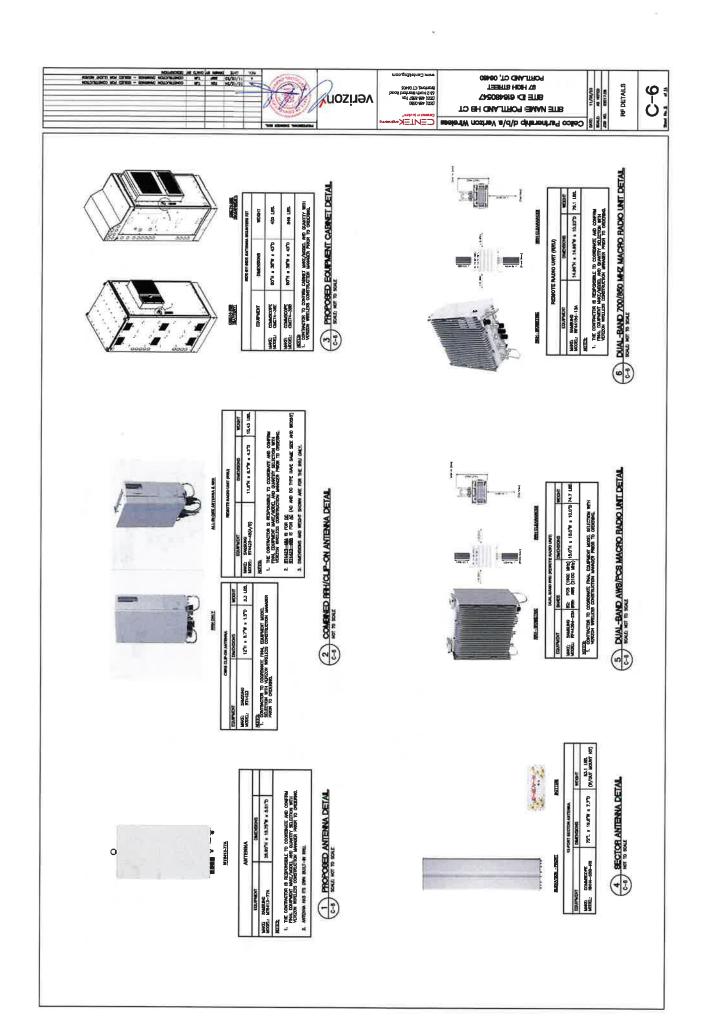


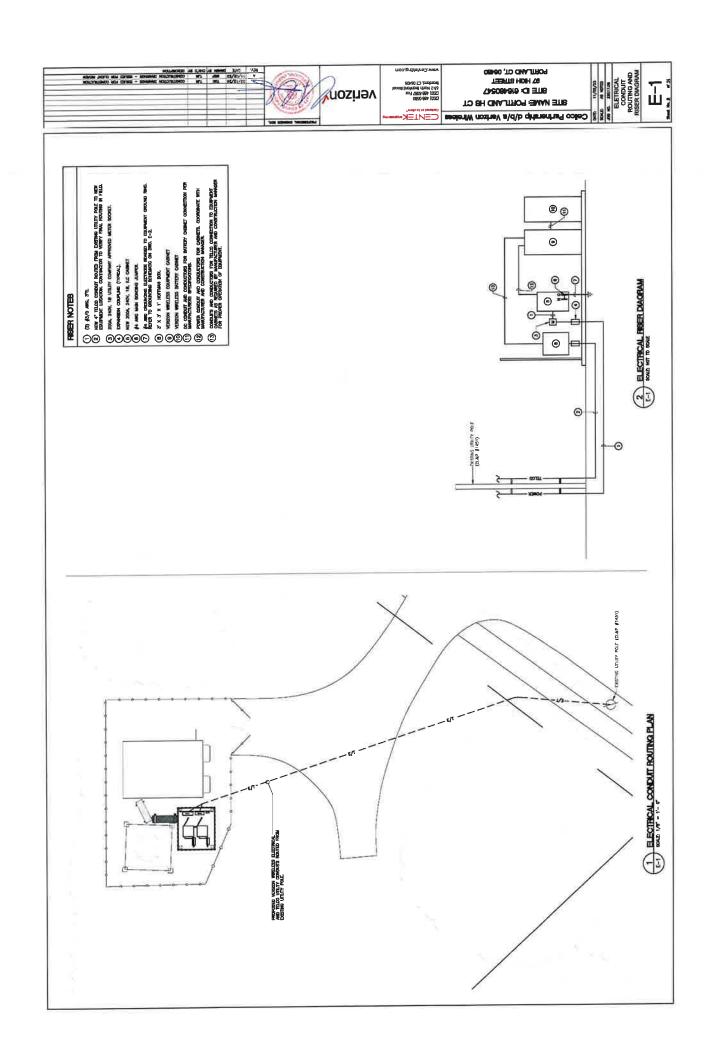
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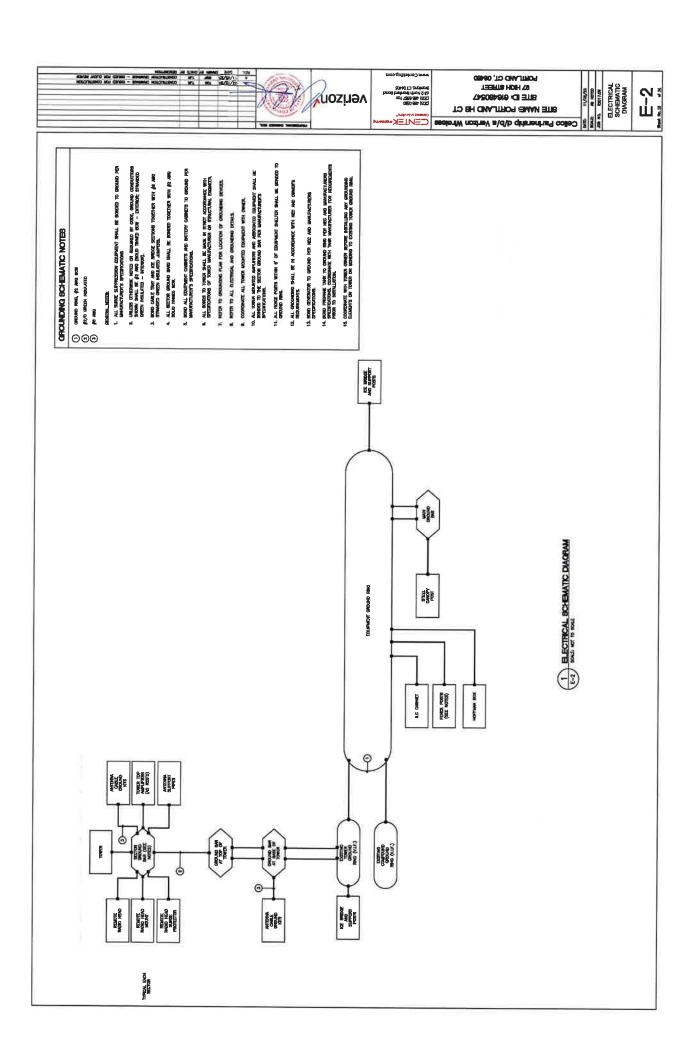


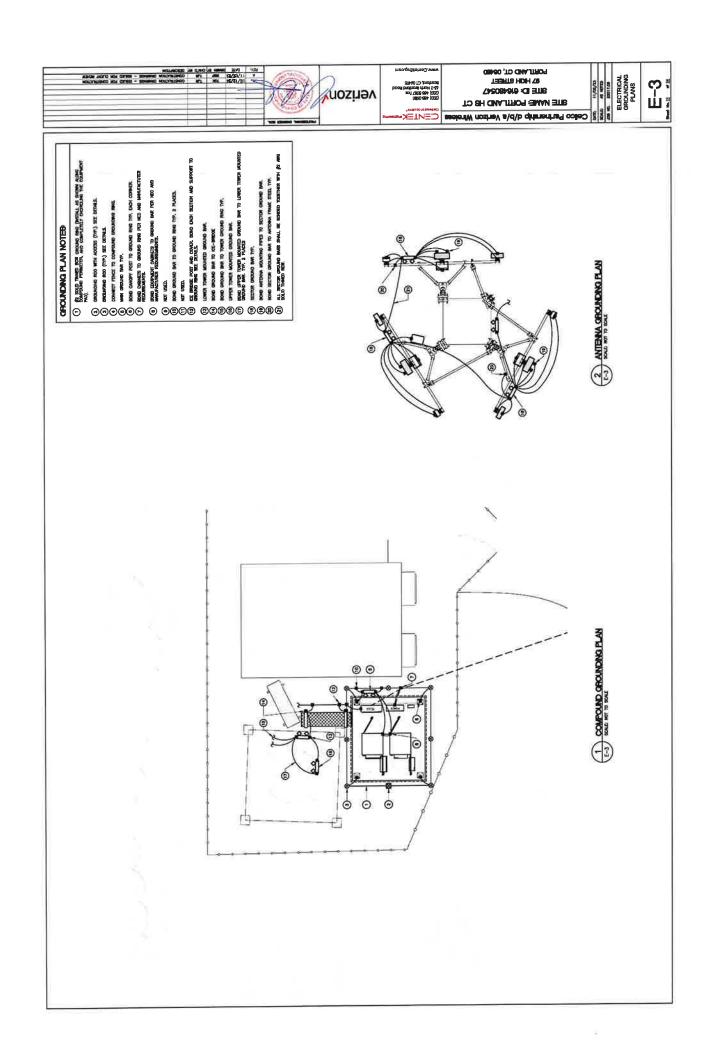


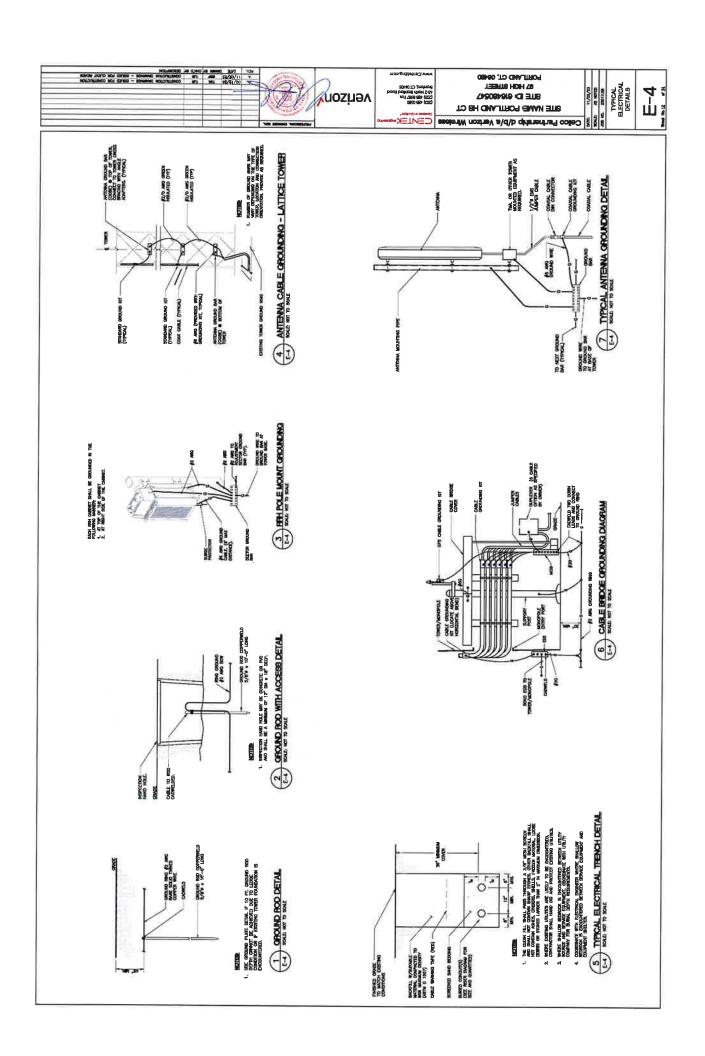


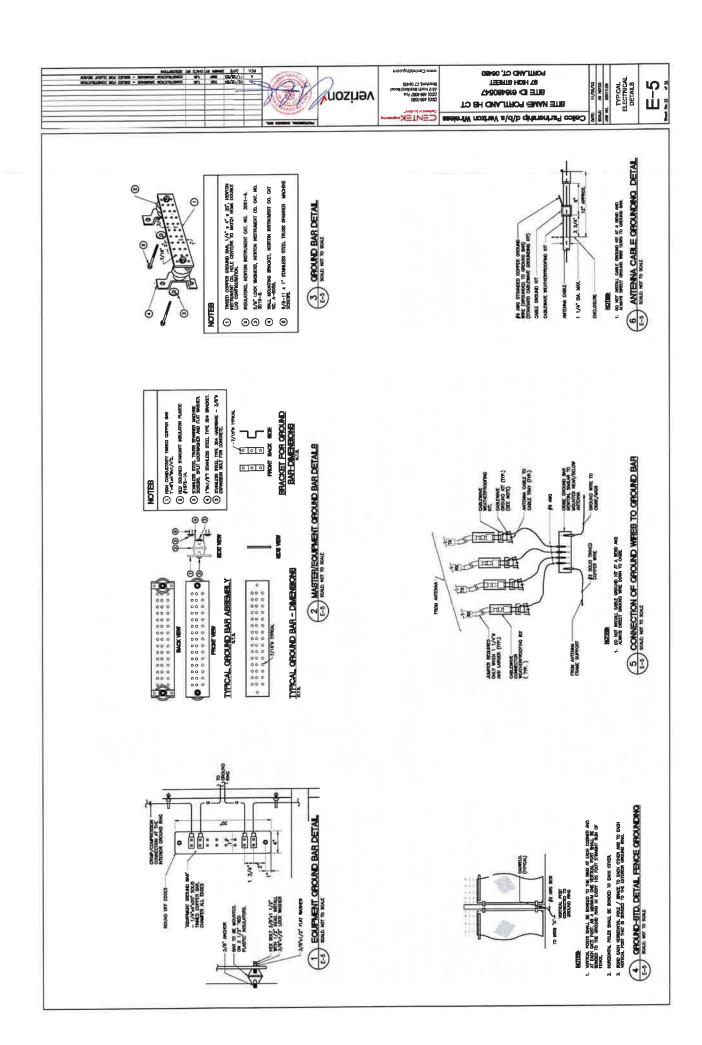












## A. AL GRECT SHILL RE HERLIED IN ACCORDANCE WIN EDING 2 SERVER PERSHELINES ESCULLAND ROME ISSUE LAND ROME AND RESPONDED IN ACCORDANCE WIN EDING 2 SERVER PROPERTY. ELECTRICAL SPECIFICATIONS

### AECTION 1618 1,01. CONDUIT

A WORK SHALL MICLION ALL LABOR, EDUPADOT AND SERVICES RESUMED TO COMPLETE TO THE FOLLOWING THE PREVIOUR ALL THE ELECTRICAL WORK INCLUDIAGE, BUT NOT LAND TO, THE FOLLOWING PRINAL 2004, 2004, 29, 4 WITE ELECTRIC SEPACE WITH SAWIT SLIB. METER AND 2004, MAR GROUN SEGURESTION TORI OWNER AND ASSOCIATED SEGURESTION LOUGHS

1.01. SCOPE OF WOR

- L. HOW WIT TILDHONG SCHOOL AS SPECIALD BY TILDHONG COMPANY.
- Federa and growing concur region to pavels, receptages, exceptions, etc. As records on rates on plane.
  - CLLILAR GROUNDING SYSTEMS, CONSISTING OF ANTIDEM, GROUNDING BAYES, ERC. RELD MEASURE DESTROOM SERVICES TO CONFIRM ANNUABLE DESTROOM POPULS.
    - COORDINATE ALL WORK SHOWS, ON THESE PLANS WITH LOOK, UTUTY COMPANIES.
    - B. LOCAL UTLITY COMPANIES SOWL PROVICE THE FOLLOWING
- CONTRACTOR SAVIL COCROBANT BITH TOLEMONE UTILITY COCRAWN FOR LOCKTON OF TOLEMONE SAVIENDS TO SE DISTRICTOR OF DISTRICTOR SAVIL COCRAWOLT TO SE DISTRICTOR OF DISTRICTOR SAVIENDS TO SE DISTRICTOR OF DISTRICTOR SAVIENDS TO SEE DISTRICTOR OF THE SAVIENDS SAVI CONTRICTOR SWILL CORECT WITH LOCAL UTILITY COMPARES TO ARRESTIME THE LUMIS OF THEM WORK AND BALL MILLIER WE NO AND WITHOUT COMPARES TO THEM WAS AND SWILL PRODUCE AND WORKEN AND SWILL PRODUCE AND PROTECT AND WORKEN AND SWILL PRODUCE AND PROTECT AND THE PRODUCES. BUT NOT PRODUCE TO COMPANY.
  - 4
- THE CONTINUES SHALL BE RELOCKED. THE OFFICES ALL PERSONS NO FEEL STATES OF ALL PERSONS OF ALL PERSONS OF ALL PERSONS OF ALL PERSONS AND ALL PERSONS OF ALL PERSONS AND ALL PER THE CHIRE CECTRON, HETALATOR SHILL DE MOC IN STRET ACCROACE WITH ALL MACKES STREET WAS PRICED WAY ARRY AND MITCHAEST STREET WAY ARRY AND WITHOUT STREET WAS AN INTRODUCED TO SUCH COCKES OF RESEARCHOORS SHALL BE INTERPRETED AS AN INTRODUCED TO SUCH COCKES OF RESEARCHOORS. THE GLOTTERA, CONTINUED IN TO REPORTED FOR THE COMPLET RETULNITY AND CONCENTRY OF THE THE GLOTTERA, STRICE, ALL ACTUALS TO BE CONCENTED THROUGH COMES REPORTED/ATION, CORNER REPORTED THROUGH COMES REPORTED THROUGH THROUGH OF THROUGH THROUG
- THE CONTINUED BANL BE INSPOSIBLE FOR COORDINATION WITH THE BUILDING OWNER FOR NEW AND/ON DESIGNION WORK PACKYES. THE CONTINUOUS SHILL BE TEXPONERE FOR COOKDANION WITH LICKL TELEPHONE OF TELEPHONE SERVICE TO THE PROPERTY OF THE PROPERTY OF
- NO WITHOUT CHART THAT CONTINED IN THE "LATEST LET OF ELECTROL.

  THAT OF THE WORK, ALL METERAL FOR WHAT IVES SOWNER, BANKE WE EXPOSE IN ANY

  PHAT OF THE WORK, ALL METERAL FOR WHAT IVES SOWNER, WE SERVE EXPOSEDABLE.
- THE CONTINUES BALL CANANTZ ALL HIS WASK THAN A FROM O ONE VAR FROM THE CASTLANDES BALL OF STRONGERS. FOR A CASTLANDES BALL OF STRONGERS. FOR CASTLANDES BALL OF STRONGERS. FOR CASTLANDES FROM ALL DIMENSOR MANUFACTUATION OF THE STRONGERS. TO THE CONTINUES.
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  - THE DETINGS COMPACTOR WALL SPAY THREE (3) CONFLIE SETT OF APPROVED DESIGNATION DETINGNED TO THE PROPERTY WAS DESIGNED RETURNED TO THE PROPERTY OF THE PROPERTY
    - ALL WORK SAUL DE RETALLED IN A NEXT AND WORKWIN LICE LAWRER AND WILL DE SUBLECT TO THE APPROVAL OF THE OWNER'S REPRESENTING.
      - AL EQUIPMENT AND MATERIALS TO BE BASTALLED SHALL BE HEN, UNLESS OTHERWIS NOTES.
- erder fami. Pamádat, the compactor saul. Provoe a complete set of premis operal, alment empero in Red Penci. To sauw all changes from the operal, almen

  - PROVIDE TOUROGERY PORTED AND LEGERIES IN WORL AREAS AS REQUIRED.
- CONTRACTOR SHALL SCIENT SEE (4) CORTS OF SHOP Observes On ALL EXUPPENT HOLLOCOLOGICA, SHOOTING THE OF THE PROMET, OWNER, OWNER, WHEN HOLLOCOLOGICA, CHANGES, ITC. CONTINUED SHALL BUILDING BY (4) COPES OF ALL TEST REPORTS CALLED FOR IN THE SPECIFICATIONS AND INVESTIGAL.

## THE ELECTRICAL SEPTIMENTS OF ALL DOCUMENTS HAVE DEPOTED THE ELECTRICAL AND ASSOCIATION OF ALL TOOL AND ASSOCIATION OF ALL TOOL AND ASSOCIATION OF ASSOCIATIO

## A. MANANA CONDUIT SIZE FOR BANKH GRICHITS, LOR VILLIACE CONTROL, AND ALARA CRECUITS SHALL BE TROPERLY FASTINED AS REQUIRED BY THE N.E.C.

- B. THE MITTINGS OF INCLINENT, DISCLOSURE NETALLED INDERGONDO SHALL BE CONSIDERED TO BE THE LOCATIONS.
  THE MATCH VARIABLE OF CONSIDERATION IN HET LOCATIONS.
- C. CONDUT RESTALED UNDERGNOUND SHALL BE RETALLED TO MEET MINING CONDIT RESAMENDITS
  OF THREE 300.5.
- D. PROVIDE (NED CALVANZED STEEL CONDUIT (TIMO) FOR THE FIRST 10 FOOT SECTION INFEN-LEMBNO A BUILDING ON SECTIONS PASSING THROUGH FLOOR SLAES
- orly letto pic condut and fittings are femilian for the reducion of electrical conductors, suthere for underground applications.

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ħ	ATTOLE 358	INTERON CINCUTRIC, EQUINEEN FROMS, SPELTERS	N/A
WHICH HOURD GRUN.	3004, 30050	ALL INTERDRY EXTENDED CREATING, ALL	8 NORES
PVC, SCHEDULE 40	ATHOLE 350, 300.5, 300.50	MIDBERT DITTORN CHEMING AND GREUNTHING SYSTEM, UNDERGREUND BESTALLADORS, WIESE NOT SUBLECT TO PAPACAL DAMKE.	E MORES
PVC, SCHEDULE BD	MITTER SEC.	MITSERY ESTEROR CROSSING AND GROUNDED STREETS, UNDERSHOUND INSTRUCTORS, WE'VE SUBJECT TO PHYSICAL DAMAGE.	E 100
LIQUID TIDHT R.EX.	ARTICLE 360	SHORT LENGTHS (MAX. 347.) WRITED TO WIREWISHE EQUIPMENT AN WET LEGUIDING.	N/A
FLEX. METAL.	ANTELE 348	SHORT LEAGHER (MAL. 397.) WRING TO VIRIGING EQUIPMENT IN WET LEGATION.	H/A
PRITE, WHAT IS DE	LEGY TO THE APPE	PRICE, WAST IS DELETT IN THE APPOINT WAYS JOHNSTON	
· Decidence choire	ACT KIND CLINTON	COORS COURT SETALD UNIX TOXI, NOWER, SEVENIT, MICHELLES BILL WIN. 1080. ILTH OF EN-	AC ROBUS SCHINGS AND
VOX ELD ROX PR	YOUR COPUSED Y	אינאל מדודן ווכא האלאסטו מהאראונים אינה ופאונה מניינה אינה אואר אינה מאר אינד וויני האלאסטו מהאראונים אינה ופאונה מניינה אינה אינה אינה אינה אינה אינה אינה	COLUMN TAKEND

### **BECTION 1648**

- ALL GOOGRACE PARK, ETC. TO THE AGE, THE ACCOUNTS AND ACCOUNT, THE ACCOUNTS AND ACCO
- B. MATHER ENDOROR MORES FOR CONDICTORS SHALL BE 12 THEST THE LANCEST DIMETER OF BROWNEN CRECIT CONDUCTOR.

### **ECTION 19190**

A. RUMEN AND METALL CUTLIT BOXES FOR ALL DEMOES, SMITHES, RECEPTACLES, ETC., BOXES TO BE ZINC CONTED STEEL. B. TARNERI AND RESTAL FILL BOXES IN MAN FEDERIS RUMS WHERE REGULED. PULL BOXES SALL DE GALMARDON STELL WITH SCRUM RECOMMEND FOR STELL WITH VARIABLE PROJECT CHARARUCINA IN WET LEARNING.

A. THE POLICIPING LIST IS PROVIDED TO COMMEY THE CAMULTY AND INVIDED OF WINNERS DESTRUCTION OF A PROPERTY LIST OF ALL DEVICES BUSY BE SUBMETED BETTING INVIDENCES WHICH FOR SUBMETED BETTING

BECTON MED. (BLFH.ED BY OWNER, NETALLED BY CONTRACTOR) (B). GODGINE SET

A. HETTH TO CONTINUE CHARMES FOR DICHARS AND SCHOOLING

- 1.15 MAJE TACK SMICH INTOMORE (FINSA (MICHON LIGHT)
- SANCE POLE SWITTS PASS POSSESSACE (204-1207 HAND USED SPECIFICATION CONCE 2. CAPACK REZEPTACLE - PASS \$2055 (OPID) SPEDENCATION GRADE
  - 4 DATES RESERVOIL PAS \$558 (204-120/ 9980 URL) SPECIFOLICA GROCE
- PATES ALI PLATES USED SAVLI BE CORROGON RESESTANT TYPE 324 STABLESS STEEL PLATES STEEL PLATES STEEL PLATES STEEL PROPERTY SAVLI BE TRUE SAVE BENE MANUFOLURES, NO STREETER AND RECEIVABLES. PROVIDE WASHINGTONIONE.
- OTHER WALRETWEEDS OF THE SWITZER, RECEPTAGES AND PLATES MAY BE SUBMITTED FOR APPROAL BY THE ENGINEER.

TOBEE AND NON-TURNED, 600W, HEART DUTY DESCRIPEDT SIRRICHES SAVIL, EE, AD MANNED SERVES SAVIES AND SAVIES AND SAVIES SAVI

- A. COMMUNICAS SHALL FURNISH AND HEIDLE NON-HEIDLED ENGNAND BACK-LIT MAREPLATES ON ALL PHEELS AND MALCH ITEMS OF ELECTRODAL DELEMBAT.
- THE TESTHE ITEM SWILL BULLDE THE FOLLOWING BIFOGNATION WITH THE MODIO TEST & MEDICINICE TO GROUPD TEST ON THE CELLILAR GROUNDED STREET

B. LETTERS TO BE WHITE ON BLACK BACKGROUND WITH LETTERS 1-1/2 INCH HIGH WITH 1/4 INCH MANGRAL D. PROVICE HWAST-LITE FOR POTITURE. DIGHE/OSIGNATION CONNECTION SHOWNS OUTLOCK INA/PROPERTY NATION. PRIVACE, AND \$ OF WINES. PLATE TO BE PLATING BUILDINGS, RED WITH WHITE LITTERS.

AND SOUTHOUSE HOLONGATURE FOR GLESTICAL STUPNESS

C. IDDRIVENTON NONDICIATURE SHALL BE IN ADDRESANCE WITH OWNERS STANDARD

E. ALL RESPONSES, SETTINGS, OFFICIALS, CIT., SHALL RELABIDS WHY CONSECUT REMAINS CONSECUT REMAINS THAT SETTINGS. TO CANNER SETTINGS OF COMMERCE, NEW OFFICE OFFICE ACCURATES.

- 2. CERTIFICATION OF TEXTING ELLIPHENT CALENATION WITHIN SX (4) WOMING OF DATE OF TEXTING, INCLUDE CENTRICATEN USE AND TELEPHONE INJURIES. 1. TESTAS PROCESURE INCLICIOS THE MAC AND MOCEL OF TEST EQUIPMENT
- C. THE CONTRICTION SHALL FORMULD SIX (II) COPIES OF THE RECUPOROR ELECTRICAL TERMS OF THE (III) YOUNGED ONT PROOF TO THE CONTRICTION OF THE (III) YOUNGED ONT
- CONNECTION BALL PRINCES LOOP WAS IN MARCHES THE COURTS BALL ET SOCKETON DE L'ANNO CONTENTE DE CONTENTE DE L'ANNO CONTENTE DE L'

## ECTION 1990 At 1235 BY NORTHON ELECTRON, TESTING FRM

## A COMPACTOR BYALL METAM THE SERVICES OF A LOCAL MEDIFICIOR ELECTRICISMO FINE (CITIED STATE (CITIED STATE CITIED STATE

- TEST 1: THERMAL OVERBOOD AND IMMERIC TITE TEST, AND CABLE INSULATION TEST ALL CIRCUIT BREAKENS PATED 1 CO. AMPS ON CHECKEN.
- A. GONNECK, DECORPTION OF TERMS WITHOU ACTUALLY MATERIORIED.

  1. HOLE TIEST SPALLE, RE-POSSEME OF HER TRESCRICK OF

  10 MOST COSTRUCTION REPRESENTANT, TERMS DAYS, SHALL OF SERVICE OF

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  10 THE COSTRUCTION REPRESENTANT OF

  10 THE COSTRUCTION R
- 6. CONTRACTOR TO PROJECT A MINISTER OF DOE (1) WITH MITCH TO OWNER AND DESCRIPTION ALL TESTS RECOVERED WITH EXAMPLE.

  GEOGRAPH STREET

  4.21. THERE OF CONTRACTOR

PHILIDAND SHILL GROUND BY TOMBHYING THE PHILIDAND FEDSITY EXTRACTION CONCLINED TO THE LINEARTH GROUND AN INTELLIGED TO THE CHRIST, DESIGN THAT THE AMEN'EMETRY HE AT AND CHRIST, HE ARE MITH, TO BHIS MITH, PHILE AND PHIST ONE TO THEN THE CONCLINE.

CONDUT(3) TEMBARTING INTO THE PAREJECHED SHALL HAVE CROJUSTING THE PROPERTY BOOKED TROCKING WITH BAKE  $\psi$  to AND CORPECT CONDUCTING WINCH IN THAN IS TEMBARTED INTO THE PAYEJECHOUR EXCHANGE A CROJUST BAKE HIT(3).

ORCHARMA SYSTEM WILL BE IN ACCREMACE WITH THE LATEST ACCEPTABLE EDITED HANGE WITH BASTREAM GOOD. AND INSUMBLIBITS FOR LICKAL INSPECTION HANGE ALKERSOON.

A 44, NON-CARRENT CARRENT CARROLL TO ELECTRICAL, AND TILLIPHOSE COLOURS
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BECTION 19480

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A RETENTO COMPANDE FOR DETAILS AND SCHEDULES RECTION (BAZZ)

BECTION 16470 1.01. DETREBUTION EQUIPMENT

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Verizon

### HELDET

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ELECTRICAL SPECIFICATIONS <u>Б</u>-6



Structural Components, LLC 1870 West 64<sup>th</sup> Lane, Unit A Denver, CO 80221 Voice: 866-386-7622

January 22, 2024

BST Management, LLC 352 Park Street Suite 106 North Reading, MA 01864

Re:

Comprehensive Structural Analysis Report

Structure:

80.4ft Self-Supporting Tower with 10ft Extension

Site Address:

97 High Street, Portland, Connecticut 06480 (Middlesex County)

Latitude: 41.5807°N, Longitude: 72.6238°W

Site Name:

BST Management, LLC - Portland

Verizon - Portland

Site Number:

BST Management, LLC - CT-1680

Verizon - 469381

SC Number:

230262

Status:

Structure Passes (79% Capacity)

Foundation Passes

Per your request, Structural Components, LLC has completed a structural analysis for the above referenced project to

verify the tower's compliance to the following design criteria:

TIA-222-H
Structural Standard for Antenna Supporting Structures and Antennas
2021 International Building Code w/Amendments 2022 Connecticut State Building Code
120 mph 3-second gust Vult
50 mph 3-second gust
1" radial
60 mph 3-second gust
C
1
345ft
D, S <sub>s</sub> =0.208, S <sub>1</sub> =0.056
В

Please refer to the following structural analysis report, which gives complete details of the tower loading, results, information provided, and necessary assumptions.

We trust you find this report satisfactory. Please do not hesitate to contact us if you should have any questions or concerns.

Best Regards, Structural Components LLC

Wesley Culver Engineering Manager

/TR



Michael DeBoer, P.E. Connecticut P.E. # 0018022

### 1 LOADING CONFIGURATION

The following antennas, mounts, transmission lines, and other appurtenances were considered for the structural analysis.

Elevation (ft)		Elevation (ft)		
Mount			Feedlines	Notes
90.5	90.5	(1) 5/8" x 6' Lightning Rod	_	Existing
90.0	90.0	(3) CommScope NNH4-65B-R6 Panels (3) Samsung RT4423 Panels (3) Samsung MT6413-77A Panels (3) Samsung CBRS RRH - RT4401-48A RRUs (3) Samsung RF4439d-25A RRUs (3) Samsung RF4440d-13A RRUs (1) CommScope FE-16148-OVP-B12 TMA (3) SitePro VFA12-HD Sector Frame Mounts	(2) 6x12 Hybrid	Verizon Final
77.0	77.0	(1) L6" x 6" x 7/16" Ring Mount	_	Existing
	78.7	(3) Ericsson RRUS 32 B2 (1) Raycap DC6-48-60-18-8F SSD		
	77.2	(3) Ericsson RRUS 32 B30 <sup>(3)</sup> (3) Ericsson RRUS 32 B66A <sup>(3)</sup> (1) Raycap DC6-48-60-18-8F SSD	(6) 7/8" TX	
76.7 <sup>(4)</sup>	76.7	(3) CCITPA65R-BU6DA-K Panels (3) Ericsson AIR6449 B77D Panels (3) Ericsson AIR6419 B77G Panels (3) CCIDMP65R-BU6DA Panels (3) Ericsson RRUS 4478 B14 (3) Ericsson RRUS 4449 B5/B12 (1) Raycap DC9-48-60-24-8C-EV SSDs (3) 12' Sector Frame Mounts	(3) 0.92" OD DC (4) 3/4" OD DC (1) 3/8" Fiber (1) 1/2" Fiber	AT&T Final
75.0	75.0	(1) L6" x 6" x 7/16" Ring Mount		
73.0	73.0	(1) 2-3/8" x 8' Pipe Mount		Existing
67.7	67.7	(1) L6" x 6" x 7/16" Ring Mount		

- 1) Elevations reference centerline of panel, yagi, mounts, and dish antennas, and base of whip antennas, in relation to the base of the tower.
- 2) Refer to the feed line diagram and analysis output in Appendix A for the location and orientation of feedlines and equipment.
- 3) Secondary appurtenances such as TMAs, Diplexers, and RRUs are considered to be installed directly behind panel antennas for frontal area shielding. See analysis output for magnitude of individual shielding.
- 4) Elevations adjusted from Structural Components Mapping dated 03/15/2022, Job # 220142.

### 2 RESULTS

The analysis was performed using tnxTower v8.1.1.0, a structural analysis program developed by Tower Numerics, Inc. specifically for the communication tower industry.

### 2.1 TOWER MEMBER STRESS LEVELS

The tower has the following stress ratios in its structural members.

Elev. (ft)	Member	Stress Ratio*
0 - 90.4	Legs	0.79
0 - 90.4	Bracing	0.64
0 - 90.4	Connections	0.64

Stress ratio (SR) criteria:

SR < 1.00 is completely within code limits.

SR ≤ 1.05 is considered within acceptable tolerance of code limits.

SR > 1.05 is outside acceptable tolerance of code limits and requires structural modifications.

### 2.2 FOUNDATION REACTIONS

The reactions listed below are for the design wind speed listed. Reactions are factored loads.

Reaction Type	Current Wind Reactions	Current Iced Reactions	Foundation Status
Moment (ft-kips)	1,265.9	320.4	
Shear (kips)	22.7	5.6	
Axial (kips)	21.8	43.6	Passes*
Leg Compression (kips)	73.9	-	r asses
Leg Uplift (kips)	64.4	_	
Leg Shear (kips)	11.1	( <del>100</del> )	

<sup>\*</sup> See Appendix A for foundation calculations.

### 2.3 TOWER DEFLECTION

The tower deflections have been reviewed and are believed to be acceptable for the proposed equipment. The carrier(s) should review the deflections for the service wind condition included in Appendix A for compatibility with their equipment.

<sup>\*</sup> Seismic analysis for similar structures under similar loading conditions has been shown to produce significantly lower stress ratios than wind and ice. Therefore, seismic analysis has not been included in the current analysis.

### 3 PROVIDED INFORMATION AND ASSUMPTIONS

The following information was directly used to generate this report, and can be found in Appendix B.

Document	Author	Date	Reference
Collocation Application	Verizon	11/21/2023	CT-1680
Mount Analysis	Centek Engineering	11/09/2023	22017.06 REV1
Structural Analysis Report – Verizon	Structural Components, LLC	05/18/2023	230262
Post Modification Inspection Report	Structural Components, LLC	09/19/2023	230193

The following assumptions were made in order to complete the analysis. These assumptions must be checked. If they do not accurately represent the existing or proposed tower, foundation, soil, and loading conditions, we must be notified so that we can make the appropriate changes to our analysis, conclusions, and recommendations.

- 1. The tower and foundation are in good condition with no corrosion, damage or fatiguing issues which could reduce the carrying capacity of the tower.
- 2. All welds and connections are assumed to develop at least the member capacity, unless determined otherwise and explicitly stated in this report.
- 3. All prior structural modifications, if any, are assumed to be as per date supplied/ available, to be properly installed and to be fully effective.
- 4. The following assumptions regarding member minimum material or type apply to this structure, unless otherwise noted in analysis:
  - o Angle Legs: A36
- o Angle Bracing: A36
- o Splice Bolts: A307

- o Gusset Plates: A36
- o Brace Bolts: A325N
- 5. The feedline and appurtenance configuration is as stated in the report. All antennas, coax, cables and waveguide cables are assumed to be properly installed and supported as per manufacturer requirement.
- 6. The support mounts and/or platforms are not analyzed and are considered adequate to support the loading.
- 7. All mounting systems connect at tower bracing points. Local stresses are not considered unless noted otherwise in analysis.
- 8. Some assumptions are made regarding antenna and mount sizes and their projected areas based on a best interpretation of the data supplied and a best knowledge of antenna type and industry practice.
- 9. The soil parameters are as per data supplied, or as assumed, and stated in the calculations.

### 4 CONCLUSIONS

To the best of our knowledge and belief the tower and foundations satisfy the requirements of the applicable codes and standards having jurisdiction over the work for the loadings and conditions as outlined in this report. **Structural modifications are not required at this time.** 

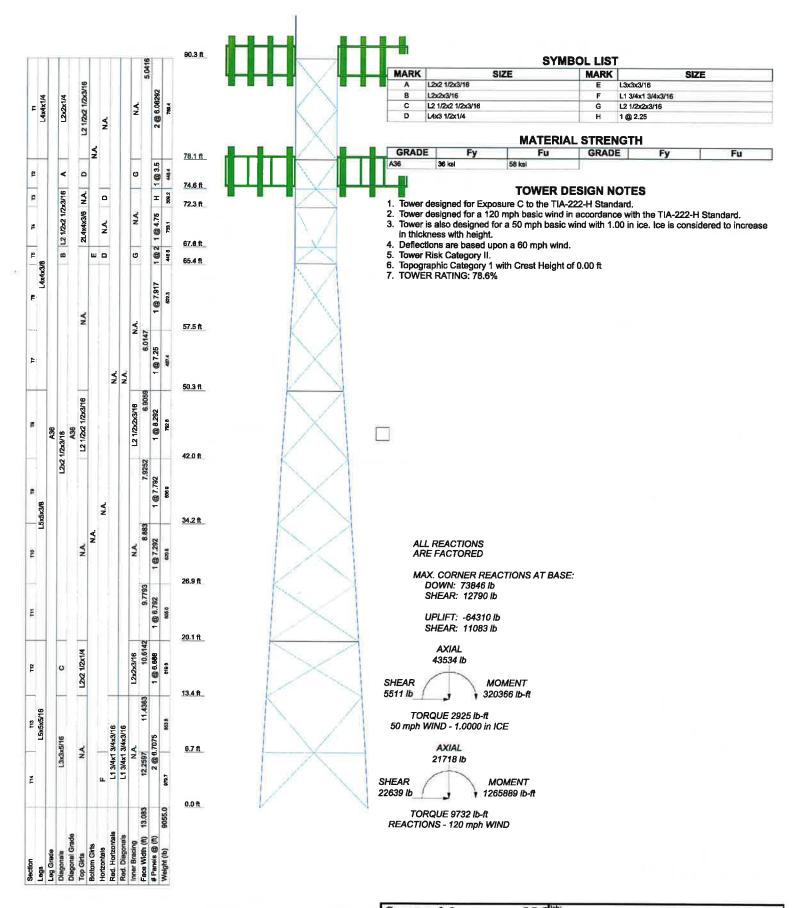
### **DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
6" x 5/8" Lighting Rod	90.5	RRUS-32 (ATI)	76,7
NNH4-65B-R6 (Verizon)	90	RRUS-32 (Full Frontal Shielding)	76,7
NNH4-65B-R6 (Verizon)	90	(ATI)	
NNH4-65B-R6 (Vertzon)	90	RRUS-32 (Full Frontal Shielding)	78.7
RT4423 (Verizon)	90	(ATI)	76.7
RT4423 (Verizon)	90	RRUS-32 (Full Frontal Shielding) (ATT)	76.7
RT4423 (Verizon)	90	DC6-48-60-18-8F (ATT)	76.7
MT6413-77A (Verizon)	90	DC6-48-60-18-8F (ATT)	76.7
MT6413-77A (Verizon)	90	TPA65R-BU6DA-K (ATT)	76.7
MT6413-77A (Vertzon)	90	TPA65R-BU6DA-K (ATT)	76.7
CBRS RT4401 RRH (Verizon)	90	TPA65R-BU6DA-K (ATT)	76.7
CBRS RT4401 RRH (Verizon)	90	AIR6449 B77D (ATI)	76.7
CBRS RT4401 RRH (Verizon)	90	AIR6449 B77D (ATT)	76.7
RF4439d-25A (Verizon)	90	AIR6449 B77D (ATT)	76.7
RF4439d-25A (Verizon)	90	AIR6419 B77G (ATI)	76.7
RF4439d-25A (Vertzon)	90	AIR6419 B77G (ATI)	76.7
RF4440d-13A (Verizon)	90	AIR8419 B77G (ATI)	76.7
RF4440d-13A (Vertzon)	90	DMP65R-BU6DA (ATT)	76.7
RF4440d-13A (Verizon)	90	DMP65R-BU6DA (ATI)	76.7
FE-16148-OVP-B12 (Vertzon)	90	DMP65R-BU6DA (ATI)	76.7
(4) 2-3/8" x 8' Pipe Mount (Verizon)	90	4478 RRU (ATT)	76.7
(4) 2-3/8" x 8' Pipe Mount (Verizon)	90	4478 RRU (ATI)	76.7
(4) 2-3/8" x 8' Pipe Mount (Vertzon)	90	4478 RRU (ATI)	76.7
(3) SitePro VFA12-HD (Verizon)	90	4449 RRU (ATI)	78.7
Ring Mount	77	4449 RRU (ATI)	76.7
RRUS-32 (Full Frontal Shleiding) (ATT)	76.7	4449 RRU (ATI)	76.7
RRUS-32 (Full Frontal Shielding)	76.7	DC9-48-60-24-8C-EV (ATI)	76.7
(ATI)		(3) 12' Sector Frames (ATI)	76.7
RRUS-32 (Full Frontal Shielding)	76.7	Ring Mount	75
(ATI)		2-3/8" x 8' Pipe Mount	73
RRUS-32 (ATI)	76.7	Ring Mount	67.7
RRUS-32 (ATI)	76.7		

### SYMBOL LIST

MARK	SIZE	MARK	SIZE
Α	L2x2 1/2x3/16	E	L3x3x3/16
В	L2x2x3/16	F	L1 3/4x1 3/4x3/16
С	L2 1/2x2 1/2x3/16	G	L2 1/2x2x3/16
D	L4x3 1/2x1/4	H	1@2.25

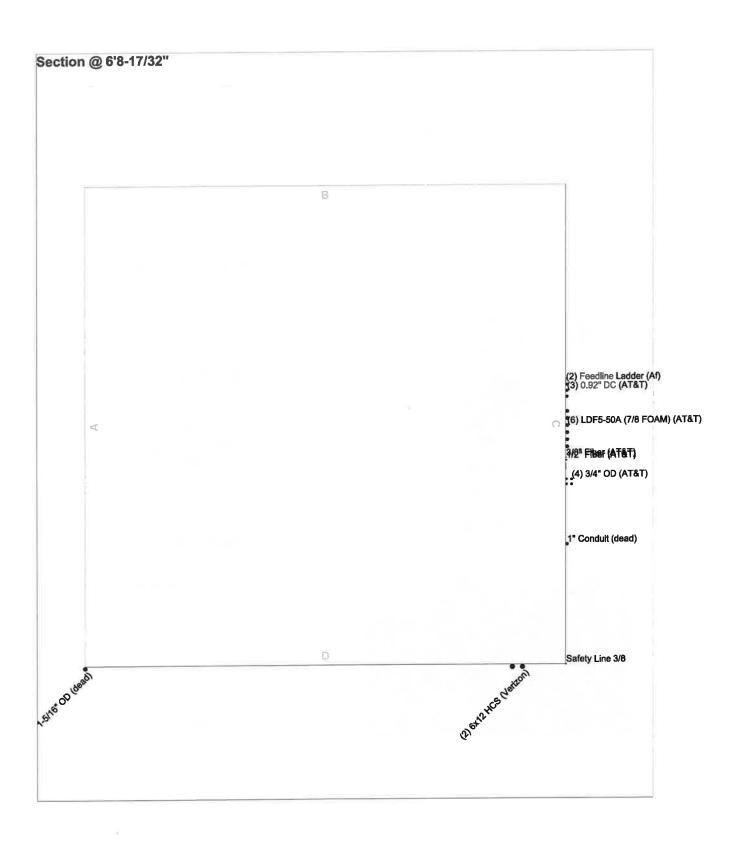
Structural Components, LLC	lob: 240022		
1870 West 64th Lane, Unit A	Project: Portland (CT-1680)		
	Client: BST Management, LLC	Drawn by: treed	App'd:
	Code: TIA-222-H	Date: 01/22/24	Scale: NTS
FAX:	Path:		Dwg No. E-1



Structural Components, LLC			
1870 West 64th Lane, Unit A	Project: Portland (CT-1680)		
Denver, CO 80221	Client: BST Management, LLC	Drawn by: treed	App'd:
Phone: (866) 386-7622	Code: TIA-222-H	Date: 01/22/24	Scale: NTS
FAX:	Path:		Dwg No. E-1

### Feed Line Plan 6'8-17/32"

Round Flat App In Face App Out Face



Structural Components, LLC	ob: 240022		
1870 West 64th Lane, Unit A	Project: Portland (CT-1680)		
Denver, CO 80221	Client: BST Management, LLC	Drawn by: treed	App'd:
	Code: TIA-222-H	Date: 01/22/24	Scale: NTS
FAX:	Path:		Dwg No. E-7



Structural Components, LLC 1870 W. 64th Lane Denver, CO 80221 Voice: 720-304-8839 Fax: 720-489-3764

### SELF SUPPORTING TOWER POST MODIFICATION INSPECTION REPORT



Site Name - Portland Site # - CT-1680

### PREPARED FOR:



### **PREPARED BY:**

Stephen Kasanovich Structural Components, LLC SC Job # 230193

### DATE:

**September 19, 2023** 



### **REPORT SUMMARY**

	1870 W. 64th Lane, Unit A	Denver, CO 80221	PH: 720-489-3764
CLIENT:	Blue Sky Towers	DATE AT SITE:	Monday, September 11, 2023
SITE (ID):	CT-1680	TOWER TYPE:	SST
ADDRESS:	97 High Street	TOWER HEIGHT:	90'
	Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph
LEAD:	Wilson Worn	SUPPORT:	Ani Doke

### **PROJECT**

Subject:

Post Modification Inspection of SST Tower Reinforcement and Extension

Location:

97 High Street

Portland, CT 06480

Structure:

90' SST Tower

Purpose:

The purpose of this post modification inspection is to ensure that the proposed modification

has been completed per the attached structural modification drawings and meets all

guidelines from Structural Components.

### **PARTICIPATION PERSONNEL**

SRR Representative:

Ricardo Costa

Blue Sky Towers, LLC 352 Park St STE 106 North Reading, MA 01864

### SUPPLEMENTAL INFORMATION

Appendix A - Redlined Modification Drawings

Appendix B - Photos During and After Construction

Appendix C - Material Testing Reports



NO

### REPORT CONTENTS

		1870 W. 64th Lane, Unit A Denve	r, CO 80221 PH: 720-489-3784
CLIENT:	Blue Sky Towers	DATE AT SITE:	Monday, September 11, 2023
SITE (ID):	CT-1680	TOWER TYPE:	SST
ADDRESS:	97 High Street	TOWER HEIGHT:	90'
	Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph
LEAD:	Wilson Worn	SUPPORT:	Ani Doke

	REQUIREMENT FOR STRUCTURAL OBSERV	ATION
STRUCTURAL OBSERVATION REQUIRED	DESIGN PARAMETER	NOTES
NO	EXPOSURE CATEGORY B AND VASD ≥ 120 MPH AND AT LEAST ONE OF THE FOLLOWING CRITERIA:  I) RISK CATEGORY III OR IV AND/OR  II) HEIGHT OF THE STRUCTURE IS GREATER THAN 75 FT	
NO	EXPOSURE CATEGORY C OR D AND VASD ≥ 110 MPH AND AT LEAST ONE OF THE FOLLOWING CRITERIA:  i) RISK CATEGORY III OR IV AND/OR  II) HEIGHT OF THE STRUCTURE IS GREATER THAN 75 FT	
NO	SEISMIC DESIGN CATEGORY C, D, E OR F AND AT LEAST ONE OF THE FOLLOWING CRITERIA: I) RISK CATEGORY III OR IV AND/OR II) HEIGHT OF THE STRUCTURE IS GREATER THAN 75 FT	
	INSPECTION OF SOILS AND EARTHWORK CONST	TRUCTION
INSPECTION REQUIRED	VERIFICATION AND INSPECTION	NOTES
NO	VERIFY MATERIALS BELOW SHALLOW FOUNDATIONS ARE ADEQUATE TO ACHIEVE THE DESIGN BEARING CAPACITY PERIODIC	
NO	VERIFY EXCAVATIONS ARE EXTENDED TO PROPER DEPTH AND HAVE REACHED PROPER MATERIAL PERIODIC	
NO	PERFORM CLASSIFICATION AND TESTING OF COMPACTED FILL MATERIALS PERIODIC	
NO	VERIFY USE OF PROPER MATERIALS, DENSITIES AND LIFT THICKNESSES DURING PLACEMENT AND COMPACTION OF COMPACTED FILL CONTINUOUS	

PRIOR TO PLACEMENT OF COMPACTED FILL, OBSERVE SUBGRADE AND VERIFY
THAT SITE HAS BEEN PREPARED PROPERLY
PERIODIC



### REPORT CONTENTS

		1870 W. 64th Lane, Unit A Denve	, CO 80221	PH: 720-489-3764	
CLIENT:	Blue Sky Towers	DATE AT SITE:	Monday, Septe	ember 11, 2023	
SITE (ID):	CT-1680	TOWER TYPE:	SST		
ADDRESS:	97 High Street	TOWER HEIGHT:	90'		
	Portland, CT 06480	WEATHER:	75F, sunny, N	wind 0-5mph	
LEAD:	Wilson Worn	SUPPORT:	Ani Doke		

### Note: See Modification Drawings for Referenced Standards

	INSPECTION OF REINFORCED CONCRETE CONSTRUCTION	
NSPECTION REQUIRED	VERIFICATION AND INSPECTION	NOTES
NO	INSPECTION OF REINFORCING STEEL, INCLUDING PRESTRESSING TENDONS, AND PLACEMENT.  PERIODIC	
NO	INSPECTION OF REINFORCING STEEL WELDING IN ACCORDANCE WITH TABLE 1705.2.2, ITEM 2b	
NO	INSPECTION OF BOLTS TO BE INSTALLED IN CONCRETE PRIOR TO AND DURING PLACEMENT OF CONCRETE CONTINUOUS	
NO	INSPECTION OF HORIZONTAL OR UPWARD SLOPING ANCHORS INSTALLED IN HARDENED CONCRETE CONTINUOUS	
NO	INSPECTION OF ANCHORS INSTALLED IN HARDENED CONCRETE (OTHER ORIENTATIONS)  PERIODIC	
NO	VERIFYING USE OF DESIGN MIX  PERIODIC	
NO	AT THE TIME FRESH CONCRETE IS SAMPLED TO FABRICATE SPECIMENS FOR STRENGTH TESTS, PERFORM SLUMP AND AIR CONTENT TESTS, AND DETERMINE THE TEMPERATURE OF THE CONCRETE CONTINUOUS	
NO	INSPECTION FOR MAINTENANCE OF SPECIFIED CURING TEMPERATURES AND TECHNIQUES  PERIODIC	
NO	INSPECTION OF PRESTRESSED CONCRETE: a. APPLICATION OF PRESTRESSING FORCES	
NO	ERECTION OF PRECAST CONCRETE MEMBERS  PERIODIC	
NO	VERIFICATION OF IN-SITU CONCRETE STRENGTH, PRIOR TO STRESSING OF TENDONS IN POSTTENSIONED CONCRETE AND PRIOR TO REMOVAL OF SHORES AND FORMS FROM BEAMS AND STRUCTURAL SLABS PERIODIC	
NO	INSPECTION OF FORMWORK FOR SHAPE, LOCATION AND DIMENSIONS OF THE CONCRETE MEMBER BEING FORMED  PERIODIC	



### REPORT CONTENTS

CLIENT:	Blue Sky Towers	DATE AT SITE:	Monday, September 11, 2023	
ITE (ID):	CT-1680	TOWER TYPE:	SST	
DDRESS:	97 High Street	TOWER HEIGHT:	90'	
	Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph	
EAD:	Wilson Worn	SUPPORT:	Ani Doke	

	MATERIAL VERIFICATION OF HIGH-STRENGTH BOLTS, NUT	'S AND WASHERS
INSPECTION REQUIRED	VERIFICATION AND INSPECTION	NOTES
YES	IDENTIFICATION MARKINGS TO CONFORM TO ASTM STANDARDS SPECIFIED IN THE APPROVED CONSTRUCTION DOCUMENTS  PERIODIC	APPROVED
YES	MANUFACTURER'S CERTIFICATE OF COMPLIANCE REQUIRED PERIODIC	MATERIAL CERTIFICATIONS AVAILABLE, APPROVED
	INSPECTION OF HIGH STRENGTH BOLTING	
INSPECTION REQUIRED	VERIFICATION AND INSPECTION	NOTES
YES	SNUG TIGHT JOINTS  PERIODIC	APPROVED
PRETENSIONED AND SLIP-CRITICAL JOINTS USING TURN-OF-NUT WITH MATCHMARKING, TWIST OFF BOLT OR DIRECT TENSION INDICATOR METHODS OF INSTALLATION PERIODIC		
NO	PRETENSIONED AND SLIP-CRITICAL JOINTS USING TURN-OF-NUT WITHOUT MATCHMARKING, OR CALIBRATED WRENCH METHODS OF INSTALLATION CONTINUOUS	
	MATERIAL VERIFICATION OF STRUCTURAL STEEL AND COLD-F	ORMED STEEL DECK
INSPECTION REQUIRED	VERIFICATION AND INSPECTION	NOTES
YES	FOR STRUCTURAL STEEL, IDENTIFICATION MARKINGS TO CONFORM TO AISC 303  PERIODIC	APPROVED
NO	FOR OTHER STEEL IDENTIFICATION MARKINGS TO CONFORM TO ASTM STANDARDS SPECIFIED IN THE APPROVED CONSTRUCTION DOCUMENTS PERIODIC	
YES	MANUFACTURER'S CERTIFIED TEST REPORTS  PERIODIC	MATERIAL CERTIFICATIONS AVAILABLE, APPROVED
	MATERIAL VERIFICATION OF WELD FILLER MATE	RIALS
INSPECTION REQUIRED	VERIFICATION AND INSPECTION	NOTES
YES	IDENTIFICATION MARKINGS TO CONFORM TO AWS SPECIFICATION IN THE APPROVED CONSTRUCTION DOCUMENTS PERIODIC	
YES	MANUFACTURER'S CERTIFICATION OF COMPLIANCE REQUIRED  PERIODIC	
	INSPECTION OF WELDING	
INSPECTION REQUIRED	VERIFICATION AND INSPECTION	NOTES
NO	COMPLETE AND PARTIAL JOINT PENETRATION GROOVE WELDS CONTINUOUS	
NO	MULTIPASS FILLET WELDS CONTINUOUS	
NO	SINGLE-PASS FILLET WELDS >5/16" CONTINUOUS	
NO	PLUG AND SLOT WELDS  CONTINUOUS	
YES	SINGLE-PASS FILLET WELDS <5/16"  PERIODIC	
	PERIODIC	



	1870 W. 64th Lane, Unit A	Denver, CO 80221	PH: 720-489-3764
CLIENT:	Blue Sky Towers	DATE AT SITE:	Monday, September 11, 2023
SITE (ID):	CT-1680	TOWER TYPE:	SST
ADDRESS:	97 High Street	TOWER HEIGHT:	90'
	Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph
LEAD:	Wilson Worn	SUPPORT:	Ani Doke

### Item #1 on S-1 Sheet

INSTALL NEW 1-3/4"x1-3/4"x3/16" ANGLE SUB-HORIZONTALS AND 1-3/4"x1-3/4"x3/16" ANGLE SUB-DIAGONALS FROM 0' - 13' 4"

























	1870 W. 64th Lane, Unit A	Denver, CO 80221	PH: 720-489-3764
CLIENT:	Blue Sky Towers	DATE AT SITE:	Monday, September 11, 2023
ITE (ID):	CT-1680	TOWER TYPE:	SST
DRESS:	97 High Street	TOWER HEIGHT:	90'
	Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph
AD:	Wilson Worn	SUPPORT:	Ani Doke

### Item #2 on S-1 Sheet

### REPLACE EXISTING TOP GIRTS WITH NEW 2-1/2"x2"x1/4" ANGLES AT 20'























	1870 W. 64th Lane, Unit A	Denver, CO 80221	PH: 720-489-3764
CLIENT:	Blue Sky Towers	DATE AT SITE:	Monday, September 11, 2023
SITE (ID):	CT-1680	TOWER TYPE:	SST
DDRESS:	97 High Street	TOWER HEIGHT:	90'
	Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph
EAD:	Wilson Worn	SUPPORT:	Ani Doke
J:	VVIISON VVOIN		7000000

### Item #3 on S-1 Sheet

INSTALL NEW 10' TOWER EXTENSION AT 80'. INSTALL 5/8" x 6' LIGHTNING ROD TO THE EXTENSION TOP GIRT.























	1870 W. 64th Lane, Unit A	Denver, CO 80221	PH: 720-489-3764
CLIENT:	Blue Sky Towers	DATE AT SITE:	Monday, September 11, 2023
SITE (ID):	CT-1680	TOWER TYPE:	SST
ADDRESS:	97 High Street	TOWER HEIGHT:	90'
	Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph
LEAD:	Wilson Worn	SUPPORT:	Ani Doke

### Item #3 on S-1 Sheet

INSTALL (2) NEW SAFETY CLIMB SYSTEMS FROM 0' - 91'



















	1870 W. 64th Lane, Unit A	Denver, CO 80221	PH: 720-489-3764
CLIENT:	SRR Towers, Inc	DATE AT SITE:	Monday, September 11, 2023
SITE (ID):	CT-1680	TOWER TYPE:	SST
ADDRESS:	97 High Street	TOWER HEIGHT:	90'
	Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph
LEAD:	Wilson Worn	SUPPORT:	Ani Doke

### APPENDIX A REDLINED MODIFICATION DRAWINGS

# MODIFICATION DRAWINGS FOR PORTLAND, CT



Structural

1870 W 64TH LANE DENVER, CO 80221 (866) 386 - 7622 JOB #: 230218

BLUE SKY

BS

SITE NAME:

## **BST MANAGEMENT, LLC - PORTLAND VERIZON - PORTLAND**

## BST MANAGEMENT, LLC - CT-1680 **VERIZON - 469381**



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## SHEET INDEX

PROJECT SUMMARY

APPLICANT/LESSEE:

T-1 TITLE SHEET GN-1 GENERAL CONSTRUCTION NOTES GN-2 SPECIAL INSPECTIONS ARCHITECTURAL:

DESCRIPTION **STA**0 2 6 7

### SELF SUPPORT TOWER MODIFICATION 97 HIGH STREET PORTLAND CT 06480 TITLE SHEET 1

## SITE INFORMATION

LATITUDE: 41.5807"N LONGITUDE: 72.6238"W

SITE COORDINATES:

NO SITE ACCESS ISSUES NOTED SITE ACCESS ISSUES:

## CODE COMPLIANCE

ALI WORK AND MATERIALS SHALL BE PERFORMED AND INSTALLED IN SACROMONDE WITH INC. CURRENT INFONS OF ALL ASSOCIATIONS OF ALL ASSOCIATIONS OF ALL ASSOCIATION SOFT ALL THE LOCAL CONCERNING ALTHORITES. WORKING IN THESE PLANS IS TO BE CONSTRUCTED TO PERMIT WORK NOTI CONFORMING TO THESE COUGS.

SEISMIC SITE CLASS: D, 8=0.280, S=0.066 SEISMIC DESIGN CATEGORY:

CONTRACTORS: CONSTRUCTION: TBD. CONSULTANTS:

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DESIGN BASIC WIND SPEED WITH ICE:
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ICE THICKNESS:

SERVICEABILITY BASIC WIND SPEED:

TOPOGRAPHIC CATEGORY: 60 MPH 3-SEC. GUST EXPOSURE CATEGORY:

GROUND ELEVATION: RISK CATEGORY:

TIA-222-H
BUILDING CODE:
2021 NITENATIONA BUILDING CODE W/ AMENDMENTS
2022 CONNECTICATS STATE BUILDING CODE

**DESIGN DATA** 

TOWER OWNER:

BST MANAGEMENT, LLC 352 PARK STREET SUITE 106 NORTH READING, MA 01684

D-1 SUB-DIAG. & SUB-HORZ. INSTALL DETAILS
D-2 TOP GRT TINSTALL DETAILS
D-3 TOWER EXTENSION DETAILS
D-4 SAFETY CLIMB INSTALL DETAILS
D-5 SAFETY CLIMB INSTALL DETAILS
(CONTD) BOM BILL OF MATERIALS 8-1 SPECIFICATIONS STRUCTURAL: DETAILS: STRUCTURAL COMPONENTS, LLC 1466-389, 782 FOR BRIMBENIG OLGENONS CONTACT: WEBLEY CALVER FOR COMSTRUCTION NOT PELD SERVESS CONSTINSS CONTINCT: HOWIND ROTCH

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OF THE TIAL CODE.

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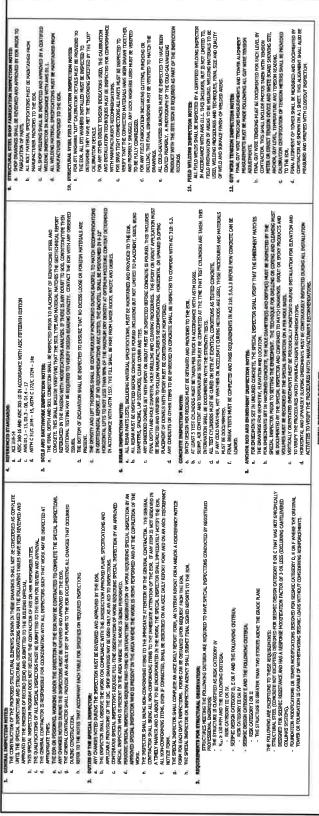
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SELF SUPPORT TOWER MODIFICATION

GENERAL CONSTRUCTION NOTES

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97 HIGH STREET PORTLAND CTT 004890 SELF SUPPORT TOWER MODIFICATION
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SPECIAL INSPECTIONS



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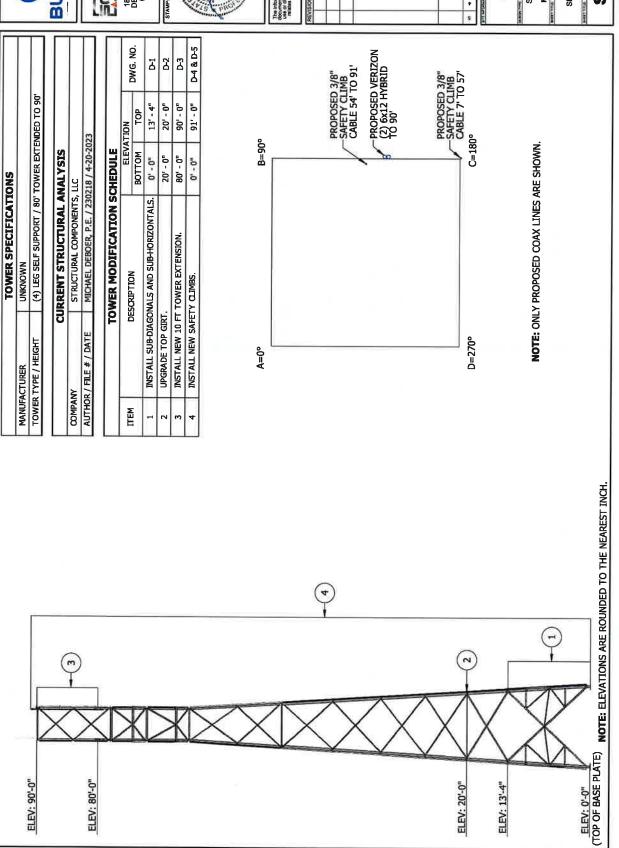




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Quantity							
	Quantity Supplied	Elevations	Part Number	Revision	Description	Plece Weight	Total Weight
					SUB-DIAGONAL, SUB-HORIZONTAL, TOP GIRT, & HW		
16	16		CP-03102-07	0	3/8" THICK GUSSET PLATE	3.73	29.68
16	16		CP-03102-08	0	1-3/4"x1-3/4"x3/16" LONG SUB-HORIZONTAL	8.01	128.16
16	16	0'-0" TO 13'-4"	CP-03102-09	0	1-3/4"x1-3/4"x3/16" LONG SUB-DIAGONAL	11.85	189.60
32	35		HK1-0815-10	0	1/2" x 1-1/2" A325 BOLT HW KIT	0.24	8.40
22	202		HK1-0817-10	0	1/2" x 1-3/4" A325 BOLT HW KIT	0.26	18.20
4	4		CP-03102-10	0	2-1/2"x2"x1/4" LONG REPLACEMENT TOP GIRT	41.20	164.80
œ	6		H01-1015-12	0	5/8" x 1-1/2" A325 BOLT	0.33	2.97
16	18	20,-0,,	H01-1017-12	0	5/8" x 1-3/4" A325 BOLT	0.35	6.30
24	72		H04-0010-01	0	5/8" HEAVY LOCK WASHER	0.03	0.81
24	77		H02-0010-11	0	5/8"-11 A563DH NUT	0,13	3.51
5					BOLT ON TOWER EXTENSION & HW		
16	16	.0-,08	CP-03102-01	0	EXTENSION - INNER & OUTER LEG SPLICE PLATE	1.97	31.52
<b>∞</b>	∞	.0-,08	CP-03102-02	0	EXTENSION - LEG SPLICE SHIM PLATE	0.44	3,52
4	4	80'-0" TO 90'-0"	CP-03102-03	0	EXTENSION - LEG	99.00	264.00
16	16	"0-'06 OT "0-'08	CP-03102-04	0	EXTENSION - DIAGONAL	23.92	382.72
4	4	.0-,06	CP-03102-05	0	EXTENSION - TOP GIRT	15.64	62.56
珎	9		H01-1020-12	0	5/8" x 2" x 1-1/4" A325 BOLT	0.29	17.40
40	45		H01-1017-12	0	5/8" x 1-3/4" x 1-1/4" A325 BOLT	0.26	11.70
25	105	80'-0" TO 90'-0"	H04-0010-01	0	5/8" HEAVY LOCK WASHER	0.03	3.15
8	105		H02-0010-11	0	5/8"-11 A563DH NUT	0.13	13.65
∞	10		H82-0010-02	0	RINGFILL - 5/8" BOLT - 1/4" THICK	0.19	1.90
	1	,,0-,06	H41-0010-06	0	5/8" x 6' LIGHTNING ROD KIT	5.50	5.50
					SAFETY CLIMB & HW		
2	2	.,0-,06	CP-03102-06	0	LADDER TOP CONNECTION ANGLE	2.33	4.66
4	'n		H01-1017-12	0	5/8" x 1-3/4" x 1-1/4" A325 BOLT	0.26	1.30
4	5	0-,06	H04-0010-01	0	5/8" HEAVY LOCK WASHER	0.03	0.15
4	2		H02-0010-11	0	5/8"-11 A563DH NUT	0.13	0.65
1	1	79'-0" TO 91'-0"	CW-01133-01	0	12 FT LADDER WELDMENT	76.52	76.52
4	4	79'-0" TO 91'-0"	P597-018-06	0	CLIMBING LADDER BACKING PLATE	0.74	2.96
8	6		HZ6-1085-60	0	3/8" x 3/4" x 8-1/2" x 6" ROUND J-BOLT	0.32	2.88
89	6	"io 'to OT "io 'or	H03-0006-02	0	3/8" F436 FLAT WASHER	0.01	0.09
00	6	0-1601 0-6/	H04-0006-01	0	3/8" SPRING LOCK WASHER	0.01	0.09
80	6		H02-0006-16	0	3/8"-16 HEAVY HEX NUT	0.04	0.36
1	1	7'-0" TO 57'-0"	H42-130-50	0	AF - 50' SAFETY CLIMB - ROUND & ANGLE LEG - SS - 14RCL50SS	115.00	115.00
1	1	54'-0" TO 91'-0"	H42-130-50	0	AF - 50' SAFETY CLIMB - ROUND & ANGLE LEG - SS - 14RCL50SS	115.00	115.00
1	1	54'-0"	CP-03102-07	0	AF - 2IN TO 4IN ROUND AND ANGLE LEG TERM. BRACKET - 14AFVB1	8.00	8.00
-	1	.0-,54	CP-03102-08	0	AF - SAFETY CLIMB BOTTOM TENSIONER BRACKET - 14AFPWJHB01	4.00	4.00
						TOTAL WEIGHT	1711.71













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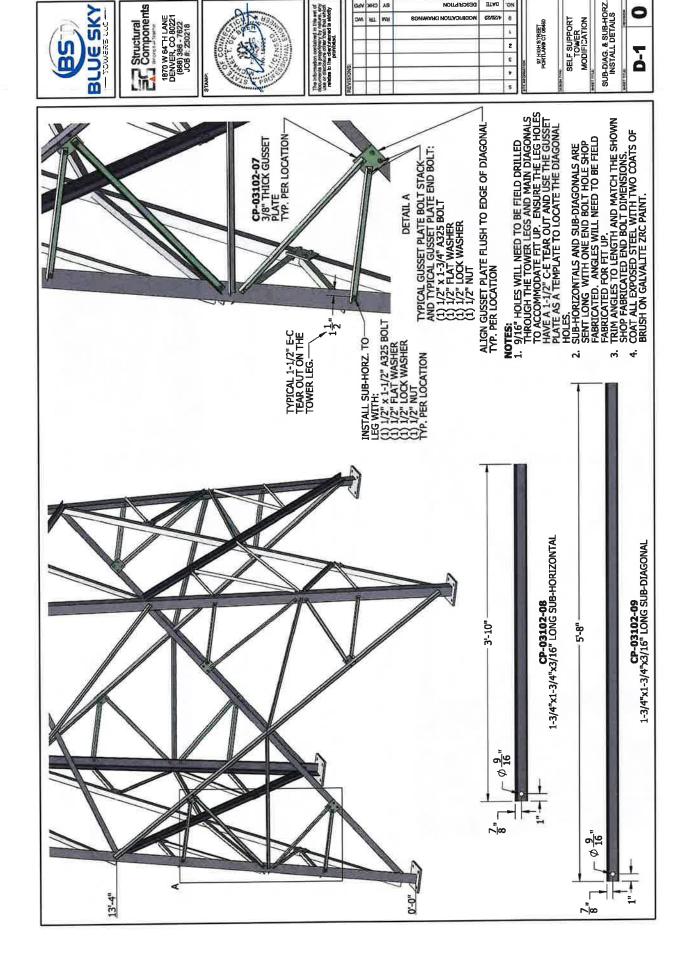
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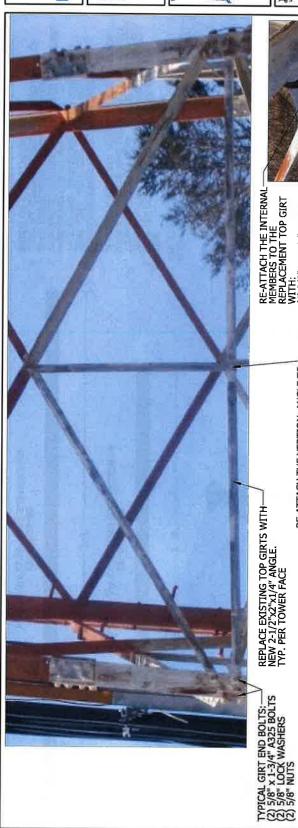
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DESCRIPTION



Structural

1870 W 64TH LANE DENVER, CO 80221 (866) 386 - 7622 JOB #: 230218

BLUE SKY

RE-ATTACH THE INTERNAL—MEMBERS TO THE REPLACEMENT TOP GIRT WITH:
(1) 5/8" x 1-1/2" BOLT (1) 5/8" LOCK WASHER (1) 5/8" NUT TYP. PER LOCATION

MATCH THE EXISTING TOP GIRT COPE TO ACCOMMODATE FIT UP. THE SHOP FABRICATED COPE IS ESTIMATED AND MAY NEED TO BE MODIFIED.

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SELF SUPPORT TOWER MODIFICATION

TOP GIRT INSTALL DETAILS

97 HIGH STREET PORTLAND CT 09460

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RE-ATTACH THE VERTICAL ANGLE TO THE REPLACEMENT TOP GIRT WITH: (1) 5/8" x 1-1/2" A325 BOLT (1) 5/8" LOCK WASHER (1) 5/8" LOCK WASHER TYP. PER LOCATION NOTES:

1. REPLACEMENT TOP GIRT ANGLES ARE SENT LONG WITH ONE END SHOP FABRICATED. ANGLES WILL NEED TO BE FIELD FABRICATED FOR FIT UP.

2. TRIM ANGLES TO LENGTH AND MATCH THE SHOWN SHOP FABRICATED END BOLT DIMENSIONS.

3. THE SHOP FABRICATED COPE IS ESTIMATED, COPE ANGLES AS NEEDED TO ACCOMMODATE FIT UP.

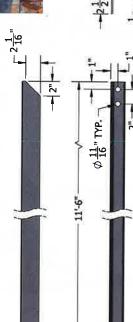
4. COAT ALL EXPOSED STEEL WITH TWO COATS OF BRUSH ON GALVALITE ZRC PAINT.

5. GALVALITE ZRC PAINT.

5. DO NOT REMOVE ANY TOWER HARDWARE OR MEMBERS IF WIND SPEEDS ARE FORECAST TO BE 20 MPH OR HIGHER.

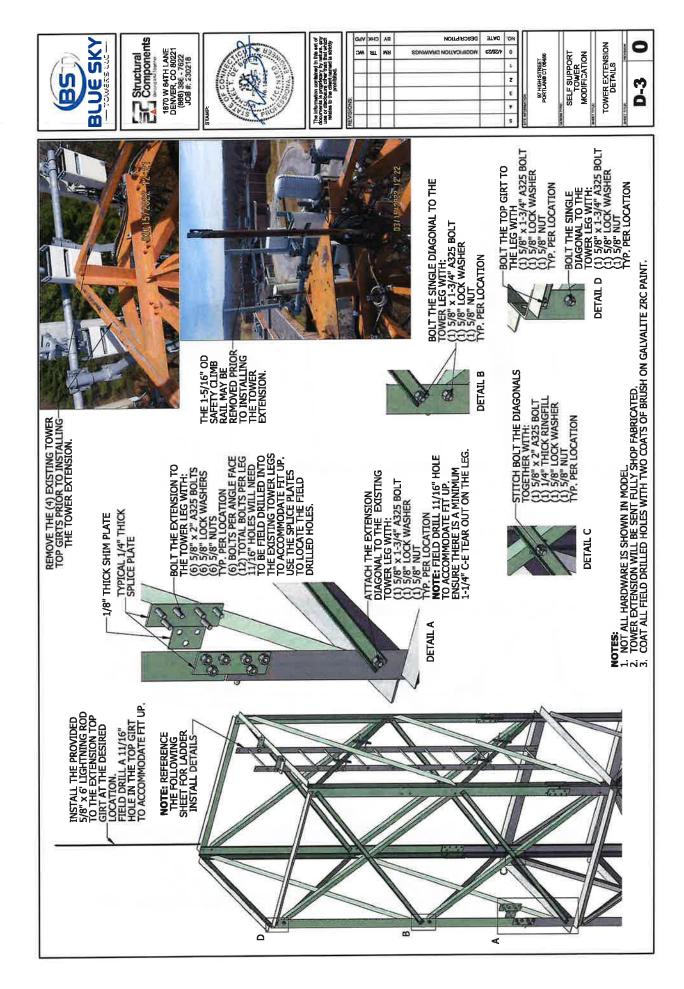
6. ALL NEW TOP GIRT REPLACEMENT HARDWARE PROVIDED.

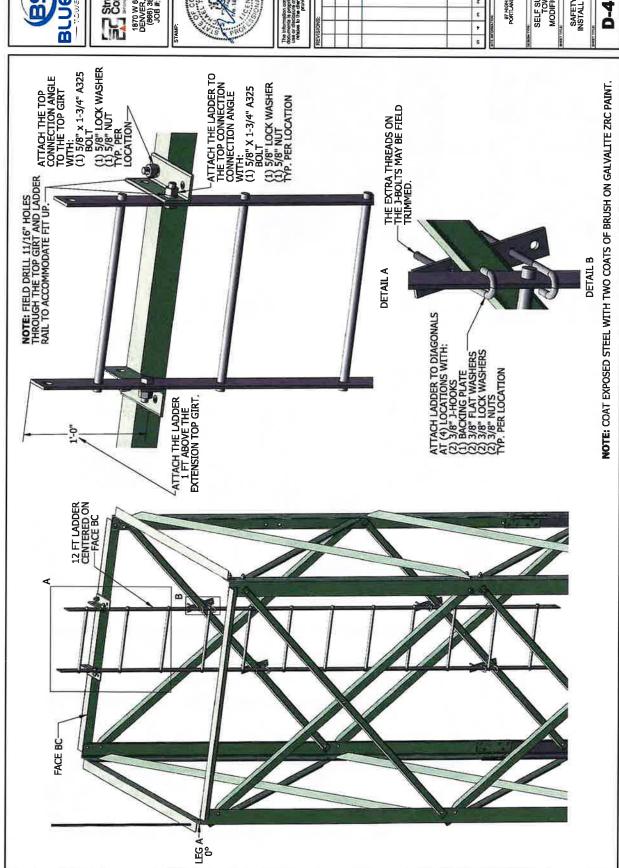




















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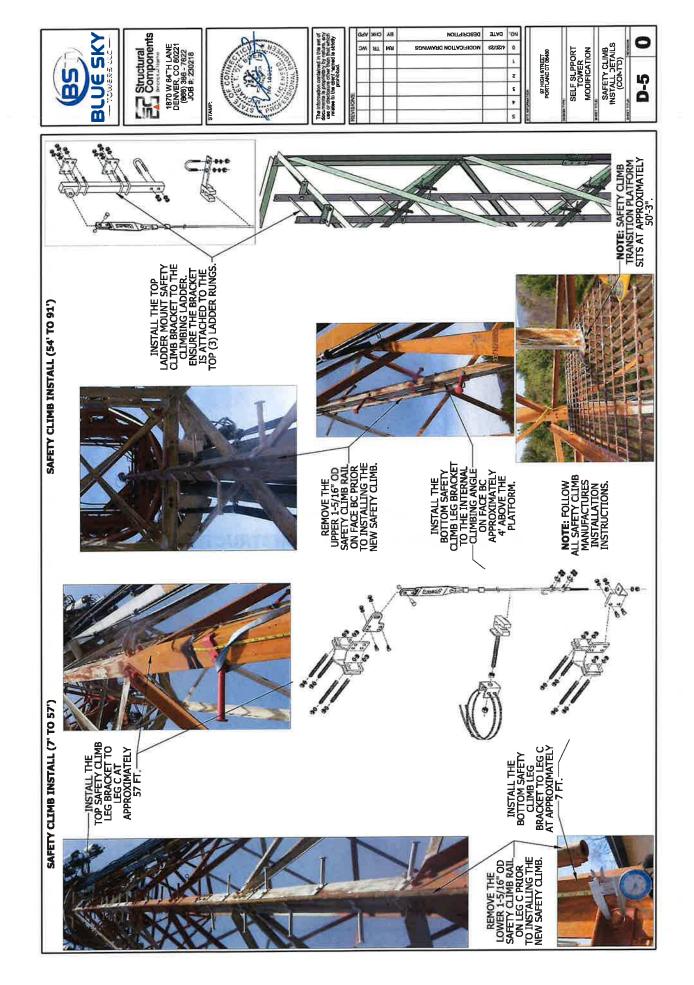
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SAFETY CLIMB









	1870 W. 64th Lane, Unit A	Denver, CO 80221	PH: 720-489-3764
CLIENT:	SRR Towers, Inc	DATE AT SITE:	Monday, September 11, 2023
SITE (ID):	CT-1680	TOWER TYPE:	SST
ADDRESS:	97 High Street	TOWER HEIGHT:	90'
	Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph
LEAD:	Wilson Worn	SUPPORT:	Ani Doke

#### APPENDIX B PHOTOS DURING & AFTER CONSTRUCTION





CT-1680 Site Photos (2)



CT-1680 Site Photos (3)

















CT-1680 Site Photos (9)





















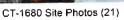














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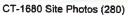












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1870 W. 64th Lane, Unit A	Denver, CO 80221	PH: 720-489-3764
SRR Towers, Inc	DATE AT SITE:	Monday, September 11, 2023
CT-1680	TOWER TYPE:	SST
97 High Street	TOWER HEIGHT:	90'
Portland, CT 06480	WEATHER:	75F, sunny, N wind 0-5mph
Wilson Worn	SUPPORT:	Ani Doke
	SRR Towers, Inc CT-1680 97 High Street Portland, CT 06480	SRR Towers, Inc         DATE AT SITE:           CT-1680         TOWER TYPE:           97 High Street         TOWER HEIGHT:           Portland, CT 06480         WEATHER:

#### APPENDIX C MATERIAL TESTING REPORTS

## Portland CT 1680

# Submittal Drawings



### BOM

Job: Blue Sky - Portland\_CT-1680 Description: Mat and HW, BOM ID: 8952 Date: 4/5/2023

## Date: 4/5/2023 1870 W 54th Lane, Unit A Deriver, CO 80221 PH: 720-304-8839

CP-03102-01 - PORTLAND CT - EXTENSION - INNER	4	1.97 lb.	33.49 lb.
& OUTER LEG SPLICE PLATE			
CP-03102-02 - PORTLAND CT - EXTENSION - LEG SPLICE SHIM PLATE	2	0.44 lb.	4.40 lb.
CP-03102-03 - PORTLAND CT - EXTENSION - LEG	*	85.85 lb.	263.40 lb.
CP-03102-04 - PORTLAND CT - EXTENSION - DIAGONAL	8	23.60 lb.	377.60 lb.
CP-03102-05 - PORTLAND CT - EXTENSION - TOP GIRT	<b>a</b>	15.84 lb.	62.56 fb.
CP-03102-06 - PORTLAND CT - LADDER TOP CONNECTION ANALE	a	2.33 lb.	4.66 lb.
CP-03102-07 - PORTLAND CT - 3/8" THICK GUSSET PLATE	23	3.73 B.	63.41 lb.
CP-03102-08 - PORTLAND GT - 1-3/4"x1-3/4"x3/18" LONG SUB-HORIZONTAL	₽	8.01 lb.	128.16 lb.
CP-03102-09 - PORTLAND CT - 1-34'x1-34'x2/18" LONG SUB-DIAGONAL	9	11,85 lb.	189.80 fb.
CP-03102-10 - PORTLAND CT - 2-1/Z/2/X1/4* LONG REPLACEMENT TOP GRT	4	41.20 lb.	164.80 lb.
CW-01133-01 - PORTLAND CT - 12' LADDER WELLSMENT	÷	76.62 lb.	76.52 lb.
H01-1017-12 - 5/6" x 1-3/4" x 1-1/4" A325 STRUCTURAL BOLT	r	0.26 lb.	20.02 lb.
H01-1020-12 - 568" x 2" x 1-14" A325 STRUGTURAL BOLT	8	0.29 lb.	17.40 lb.
H02-0006-16 - 3/6*-16 Heavy Hex Nut - HDG	10	0.04 lb.	0.40 lb.
H02-0010-11 - 5/8*-11 A563DH Gelvanized Nut	137	0.13 lb.	17,81 lb.
H03-0006-02 - 3/8" F436 Galvanizod Flat Wesher	9	0.01 lb.	0.10 lb.
H04-0006-01 - 3/8" Spring Lock Washer HDG	10	0.01 fb.	0,10 lb
H04-0010-01 - 5/8* Galvanized Heavy Lock Weeher	137	0.03 lb.	4.11.6
H26-1086-80 - 3/8" X 8-1/2" X 8" J-B/3/1	a	0.32 lb.	288 b.
H41-0010-06 - 5/8" x 6" Lightning Rod Kit. (Primus # 586CCAT)	-	5.50 lb.	5.50 lb.
HAZ-110-001 - BOTTOM TENSIONER PLATE (AF PN 14AFPALHBOT)	÷	10.00 lb.	10.00 lb.

Page 3 of 3



#### BOM

Bringing It All Together.	Job: Bl Descriț Date: 4	Job: Blue Sky - Portland_CT-1680 Description: Mat and HW, BOM ID: 8952 Date: 4/5/2023	_CT-1680 V, BOM ID: 8952
1870 W 64th Lane, Unit A Denver, GO 80221 PH: 720-304-8838	nver, CO 862	21 PH: 720-304-	6638
Part #Description	Š	Unk Wt.	Combined Wt.
H42-120-060 - AF - 80' SAFETY CLIMB - LADDER MOUNT - SS - SHORT TOP - 14LMSCSOSS	्रम	90.00 lb,	90.00 lb.
H42-130-031 - ROUND LEG CLAMP BRACKET - 2"- 4" Diameters (AF PN 14AF/B1)		12.00 lb.	12.00 lb.
HA2-130-050 - AF - 60' SAFETY CLIMB - ROUND & ANGLE LEG - 8S - 14RCL 50SS	-	115.00 lb.	116.00 lb.
H82-0010-02 - RINGFILE - 5/8* BOLT - 1/4" THICK	0	0.19 lb.	1.90 lb.
HK1-0815-10 - 1/2" x 1-1/2" x 1" A325 BOLT HW KTT	18	0.24 lb.	8.40 lb.
HK1-0817-10 - 1/2" x 1-3/4" x 1" A325 BOLT HW KTT	£	0.26 lb	18.20 lb.
P397-018-08 - P10 - CABLE LADDER - BACKING PLATE	w	0.74 lb.	3.70 fb.
Total			1696.12 lb.

Page 4 of 3

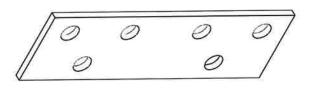


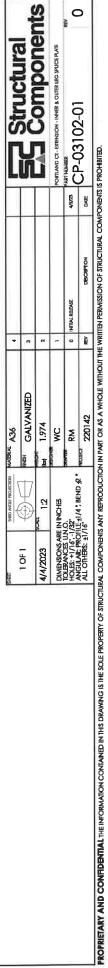
#### BOM

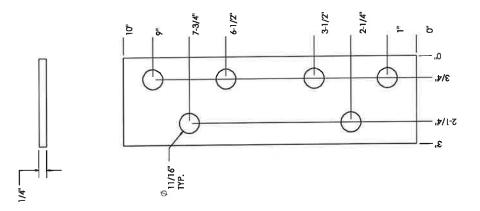
Description: Mat and HW, BOM ID: 8952 Date: 4/5/2023

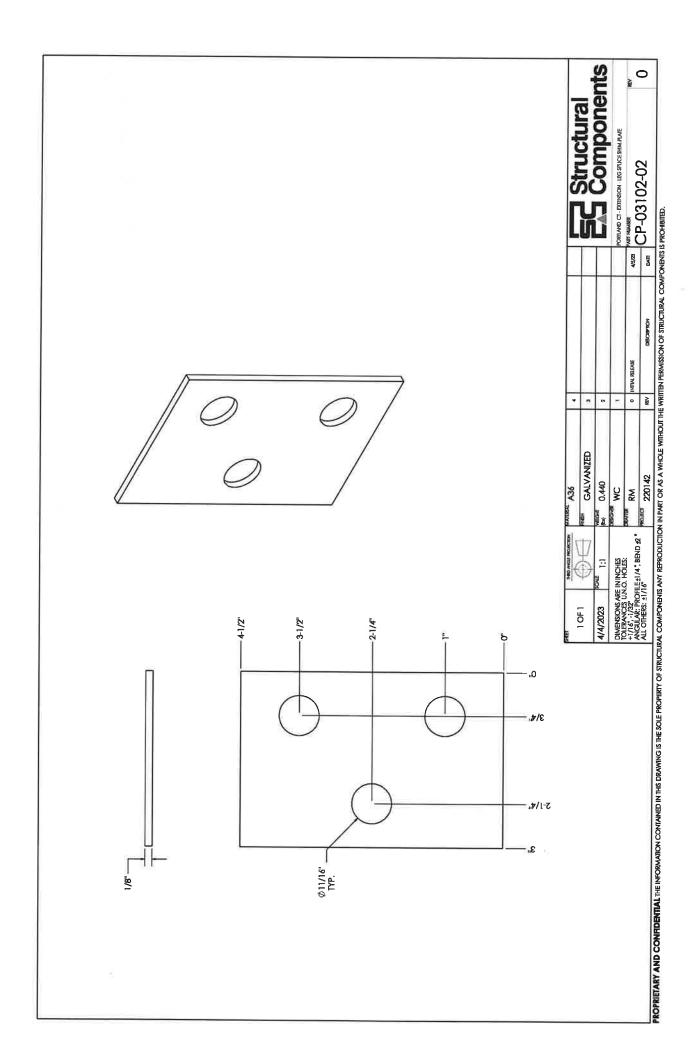
	Sub-Com	Sub-Component Quantities	ttles	
	Description	g.	Unit Wt.	Combined Wf.
2000	S-1 CP-03102-11 PORTLAND CT - 12 LADDER - RAIL	2	25.07 lb.	50.14 %
47	S-2 CP-03102-12 PORTLAND CT - 12' LADDER - RUNG	12	2.20 lb.	28.40 lb.
1200	S-3 H01-0615-10 1/2 x 1-1/2 x 1* A225 STRUCTURAL BOLT	8	0.14 lb.	4.80 lb.
٧,	S-4 H01-0817-10 1/2" x 1-3/4" 1" A326 STRUCTURAL BOLT	Ę	0.18 fb.	11.20 lb.
200	S-5 H02-0008-13 1/2"-13 A583DH Galvanized Nut	106	0.08 lb.	8.40 lb.
w)	S-6 H03-0008-02 1/2" F436-1 Gelvenized Flat Weether	105	0.02 lb.	2.10 lb.
	S-7 H04-0008-01 1/2" Galvenized Heavy Lock Washer	105	0.02 lb.	2.10 lb.

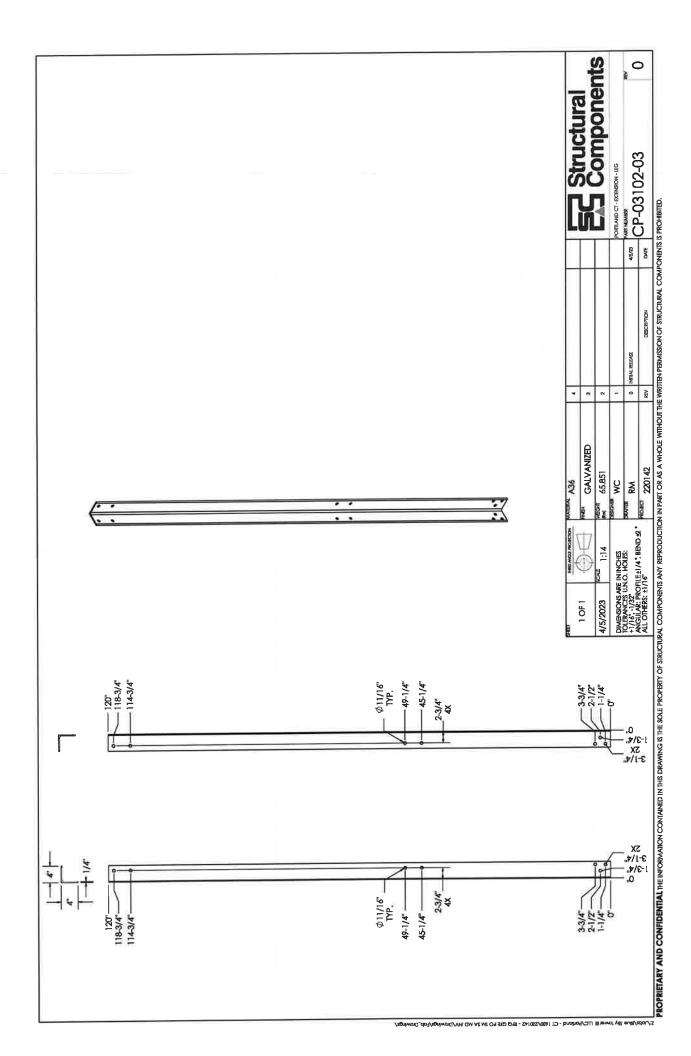
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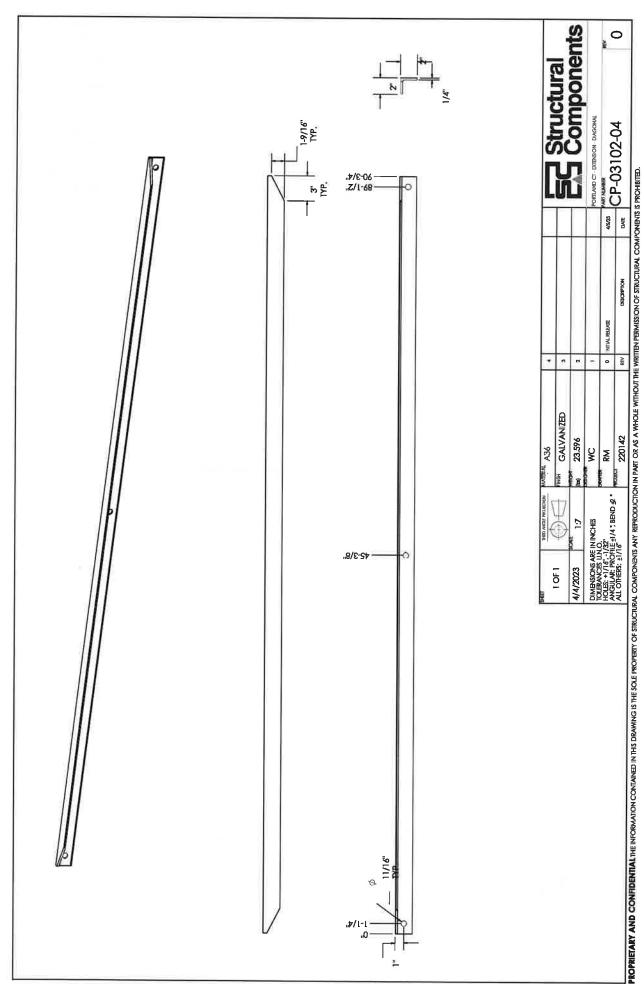


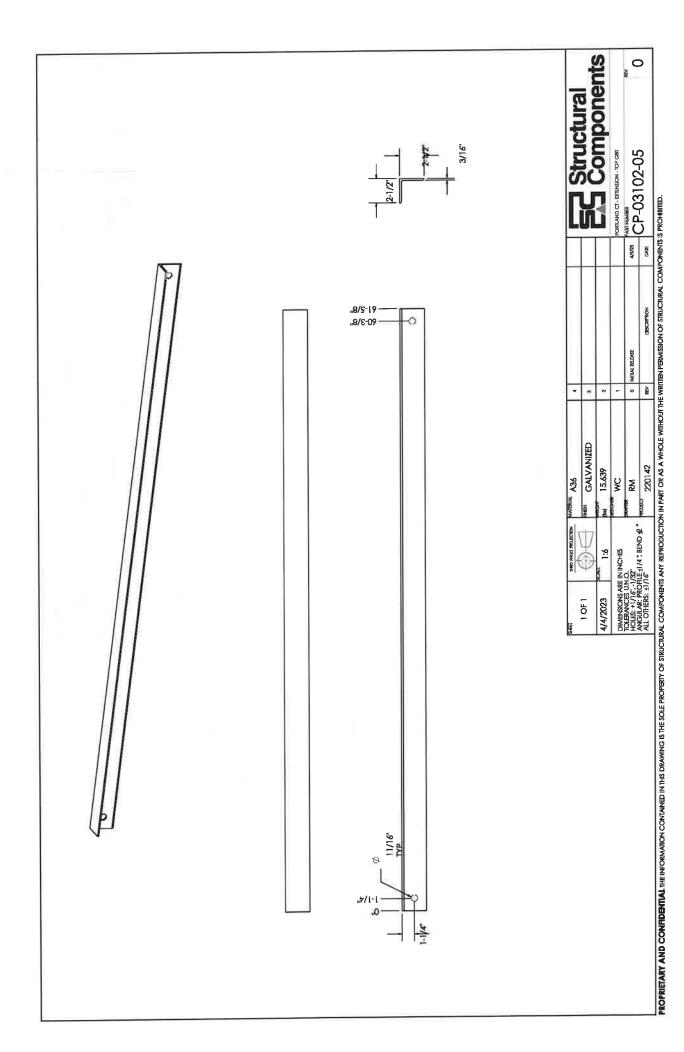


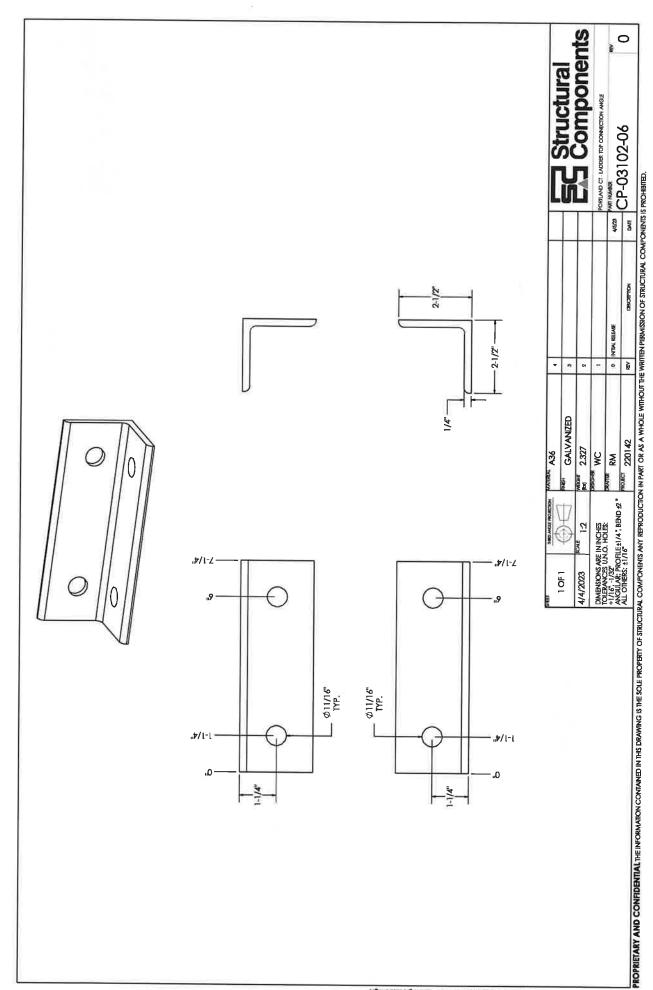


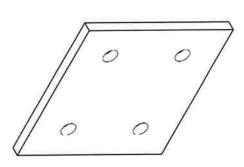


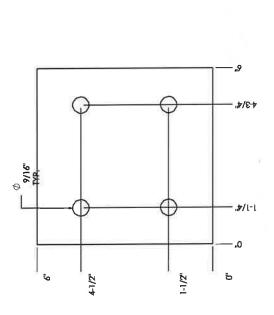


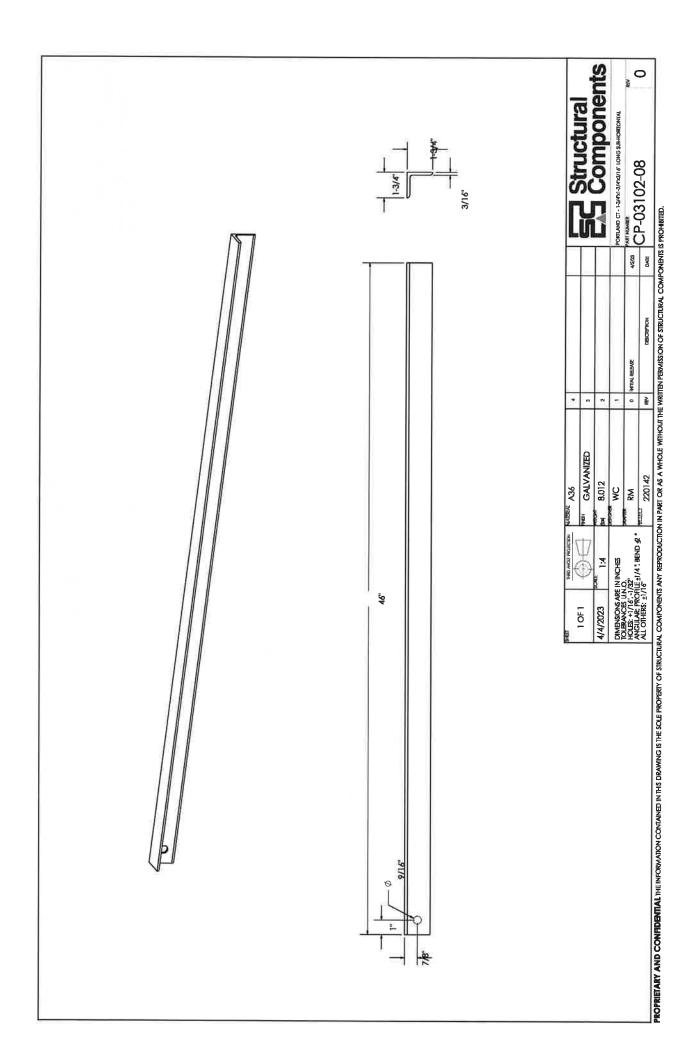


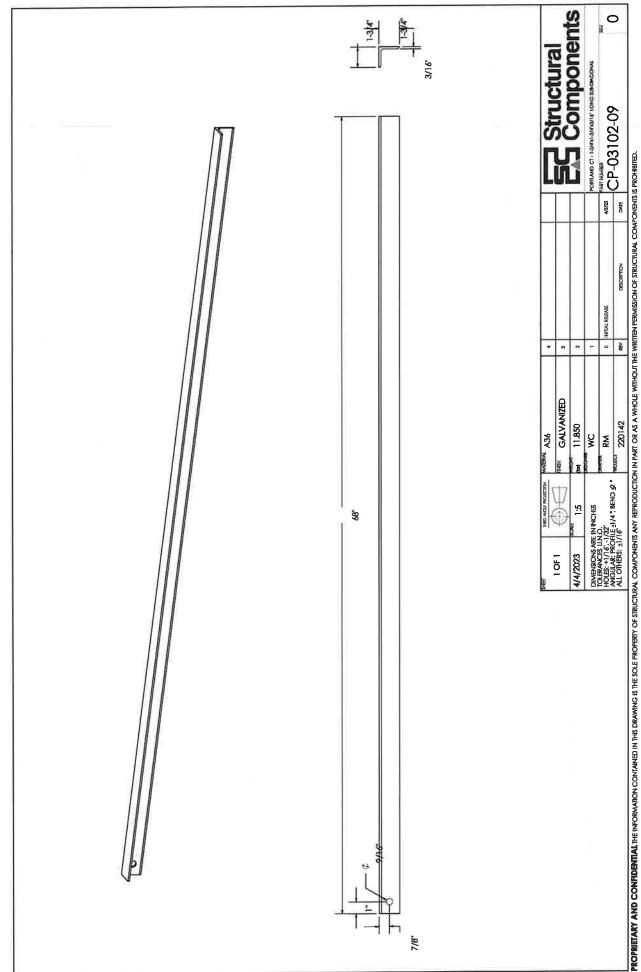


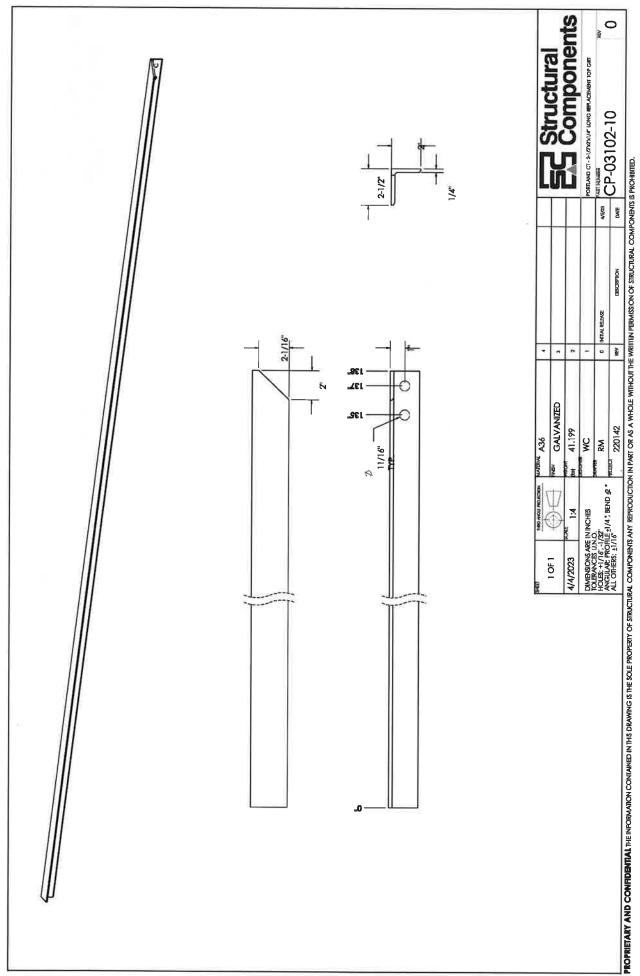


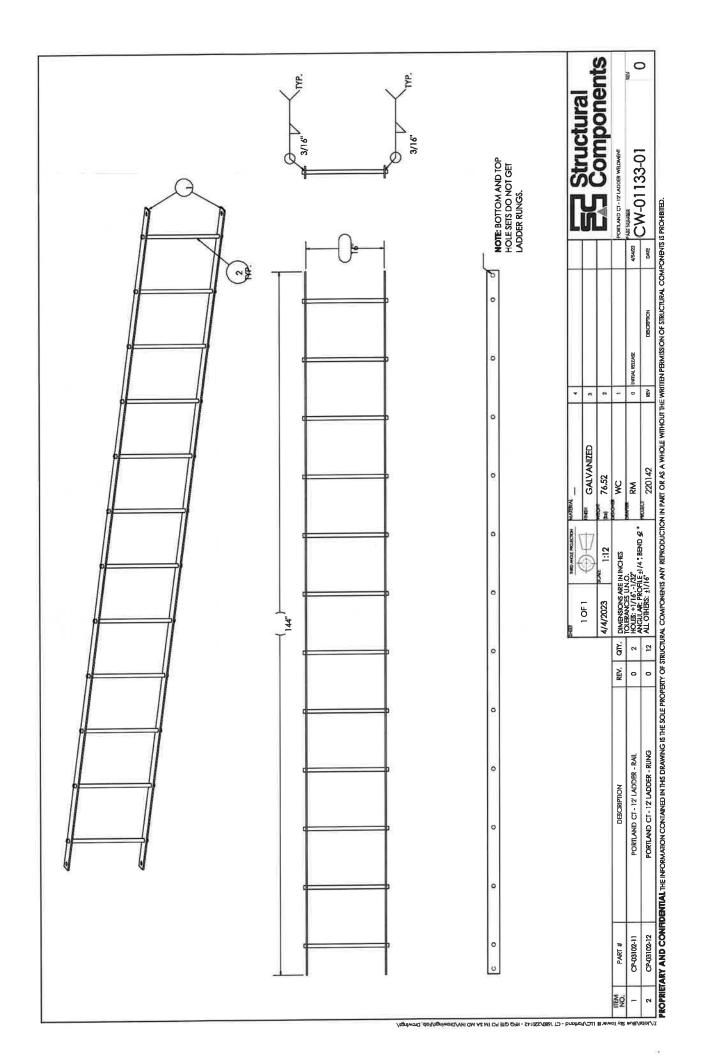


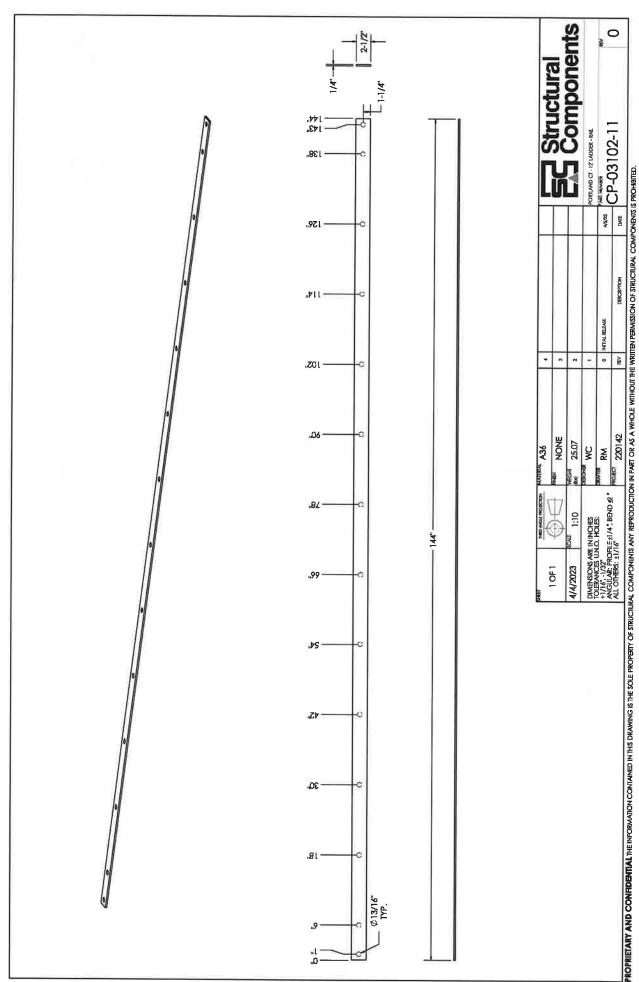


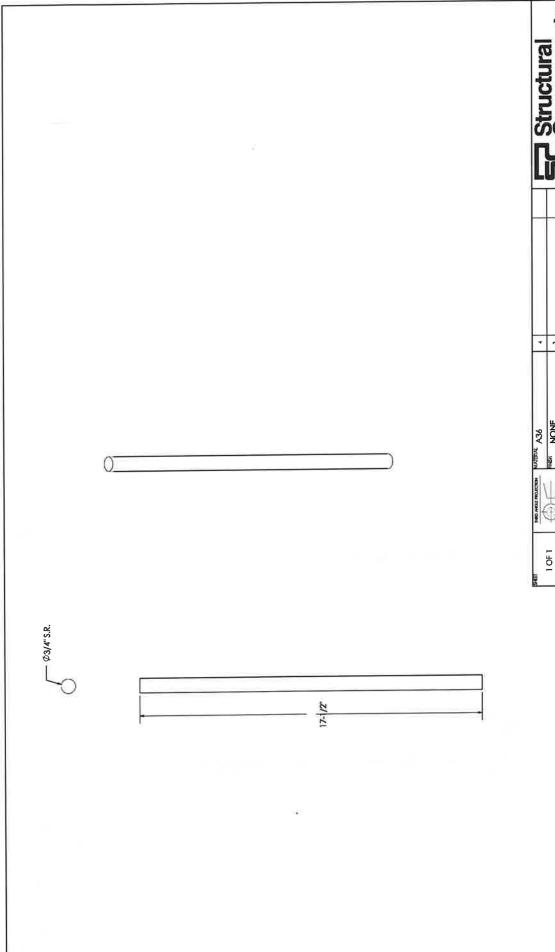




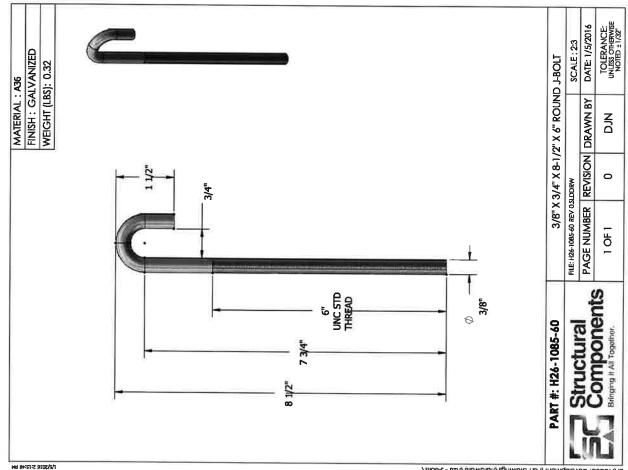








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For All Things Fastering.

# SAFETY CLIMB - LADDER MOUNT - SS

Hot Dip Galvanized Brackets | Stainless Steel Wire Rope Conforms to ANSI A14.3-2008

			S Per 1 PC
PMT#	LENGTH	(-)	±
14LMSC10096	100		\$408.38
14LMSC150SS	150		\$565.20
14LMSC200SB	200		\$848.25
14LMSC260SS	250	•	\$796.07
14LMSC300SS	300		16788
14LMSC350SS	380		\$1,016.14
14LMSC400SS	400		91,132.36
14LMSC500SS	900		\$1,389.12

LADDER MOUNT SAFETY CLIMBS

Hot Dip Galvanized Brackets | 60" Top Bracket Stainless Steel Wire Rope | Conforms to ANSI A14.3-2008

			\$ Per 1 PC
P9RT#	LENGTH	6	++
14LMSC1008S-80	100	٠	\$441.38
14LMSC150SS-80	150		\$598.20
14LMSC200SS-80	200		\$661.25
14LMSC250SS-80	260		\$628.07
14LMSC300SS-80	300	٠	\$802.91
14LMSC36088-60	360		\$1,049.14
14LMSC400\$S-60	400	-	\$1,186.38
14LASC500SS-80	200		\$1,402.12

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LENGTH	100	150	200	260	300	360	400	200				- 041	1	P V		1
#12	MSC1008S-80	MSC150SS-80	MSC200SS-80	JMSC2E0SS-80	MSC300SS-80	MSC36088-60	MSC400SS-60	AEC500SS-80						9	-	



CRAWNES AND INFORMATION SUBJECT TO CHANCE

MOOSEMOT-AMMIN

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Hot Dip Galvantzed Brackets | Stainless Steel Wire Rope Conforms to ANSI A14.3-2008

SAFETY CLIMB - ROUND & ANGLE LEG - SS

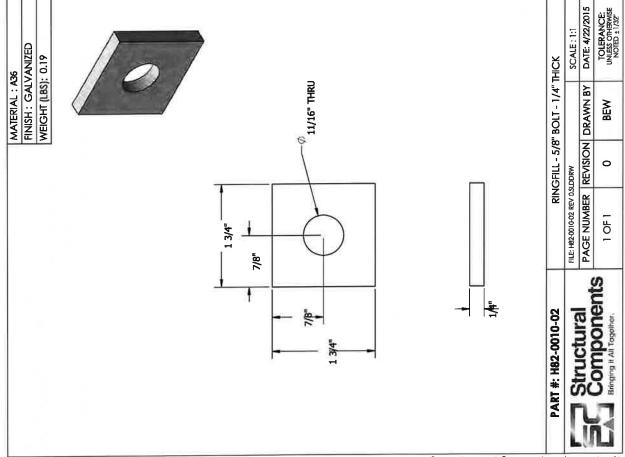
PART#	LENGTH	(	1+
14RCL100SS	100		\$597.47
14RCL1508S	150		8005.73
WRCLZ00S9	200		\$308.64
14RCL 250SS	260	· F	\$1,087.61
14FCL300SB	300		\$1,227.60
44RCL350SS	360		\$1,374.82
MRCLADOSS	400	•	\$1,570,99

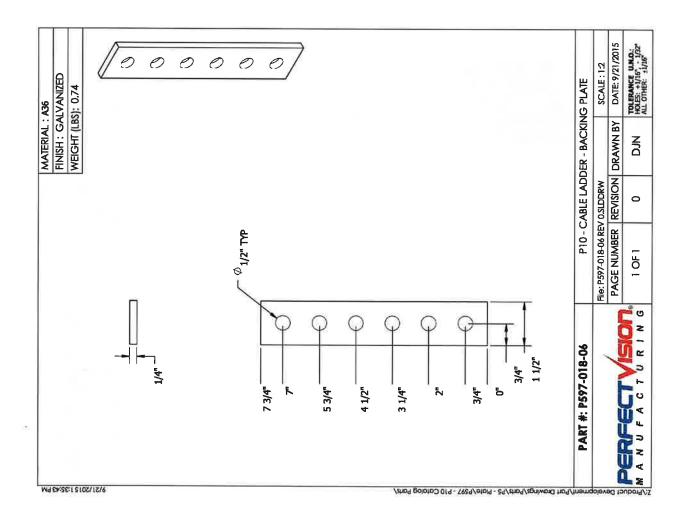
ROUND & ANGLE LEG SAFETY CLIMBS





2





CW-01133-01



CW-01133-01

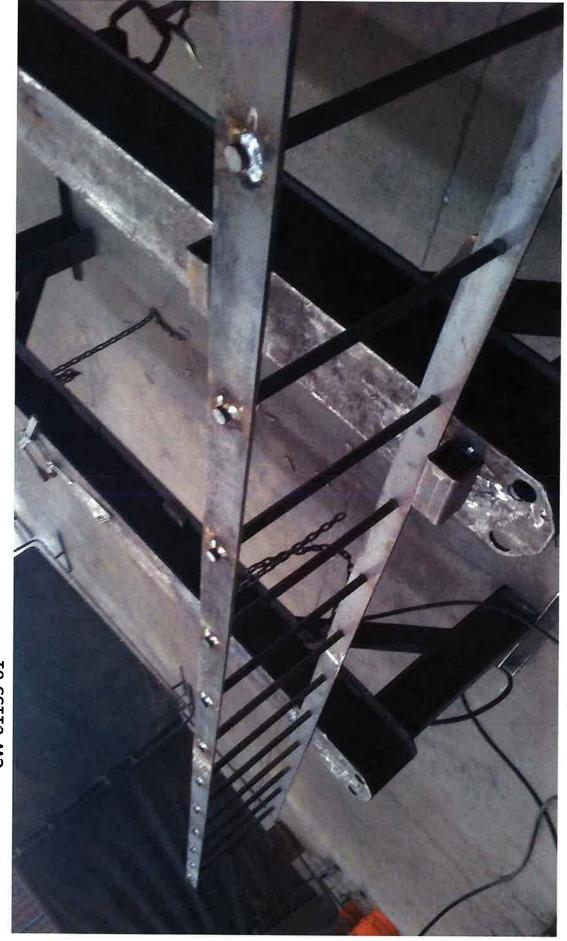
CW-01133-01



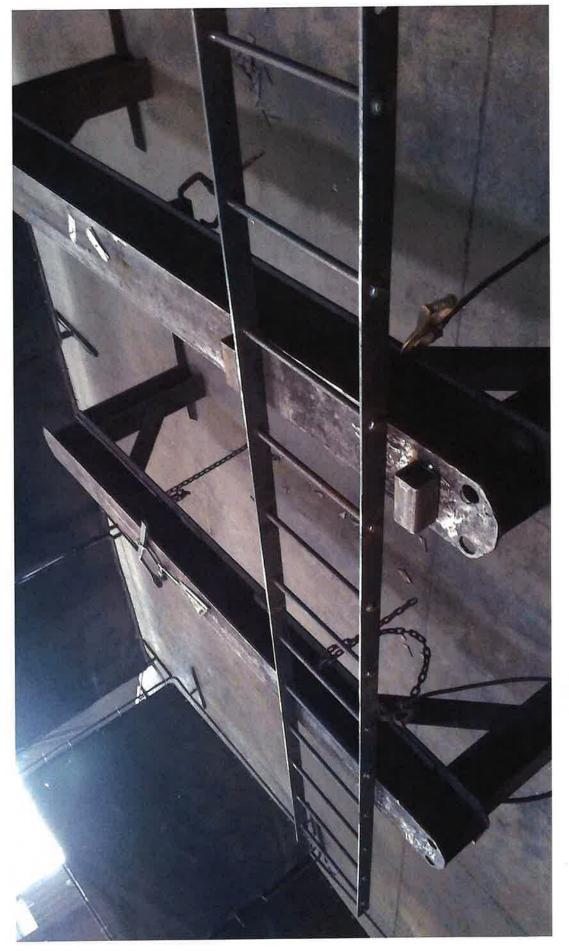
CW-01133-01



CW-01133-01



CW-01133-01



CW-01133-01



Welding Wire



**Gas Flow** 



**Machine Settings** 

### Welder Certificate

Welder and Welding Operator Qualification Test Record

E	echnical	onsultants	
onthe	7	1	
4	Ų	* 1	1

Velder or weldi	Welder or welding operator's name	Ismael Burciago		Identification No. 079	620
<b>Nelding proces</b>	Welding process GMAW Manual	Semiautomatic	atlc ×	Machine	
Position	16				
Flat, horizontal	(Flat, horizontal, overhead or vertical - if vertical, state whether upward or downward)	if vertical, state wheth	er upward or down	ward)	
In accordance with pro	In accordance with procedure specification number <u>B-U2a-GF</u> Material specification A572 Grade 50	ation number B-U2a	-GF (pregualified)	6	
Marie and American	1000	manual contraction	ı		
Diameter and w	Diameter and wall thickness (if pipe) - otherwise, joint thickness,	ornerwise, joint trickin	ess 1-mgn		
Drameter and the	Drameter and Inickness range this qualifies.	mes 1/8 to Unimited	Minuted		
Positions this qualifies	ualifies Flat			(see Tal	(see Table 4.9 AWS D1.1)
Specification No.	A/VS 5 18	FILLER	FILLER MATERIAL Classification	ER70S-6	F No. F4
Describe filler n	l۳	AWS specification)		ll	
Is backing strip used?	used? N/A				
Ter metal dia	nd trade r	.045			
Appearance	Satisfactory	VISUAL INS	PECTION	Piping porosity	none
Test conducted	Test conducted by Rodney Clark		Laboratory Test No.	st No.	
	per AWS D1.1-2020		Test Date	May 10, 2021	
Appearance		Fillet Te	Fillet Test Results Fillet Size		
Fracture test ro	Fracture test root penetration		Macroetch		
(Describe the I	(Describe the location, nature, and size or any crack or tearing of the specimen.)	e or any crack or teari	ng of the specimen	3.5	
Test conducted by	d by Rodney Clark		Laboratory Test No.	ost No	
		120	Test Date	May 10, 2021	
		RADIOGRAPHI	RADIOGRAPHIC TEST RESULTS		
Film			Film		
Cation	Results	Remarks	cation	Results	Remarks
18-1	Satisfactory	Accept		The second secon	
Test Witnessed By	d By SGC (Rodney Clark)	y Clark)			

CAM DISTRICTS COM CONTROL CONTROL COM CONTROL 
Manufacturer or contractor Metrosite Fabricators
Authorized By Kent Ramey
Date May 10, 2021

We, the undersigned, certify that the statements in this record are correct and the welds were prepared and lested in accordance with the requirements of American Welding Society AWS D1.1-2010.



# MetroSite LLC. 180 Industrial Park Blvd. Commerce Georgia 30529 Welding Procedure Specification (WPS)

Date: 01/08/2019

Revision: 0

Supporting PQR Prequalified Filet F-1

Prepared By: D. Nichols Date;01/08/2019 : Welding Engineer: \_N/A

Welding Process: GMAW

Welding Method: Spray Transfer

Grow Pupe: _VIV.  Growth Vipe: _WA  Growth Walds: _WA  Reching: _WA  Wed Foulton: Groove  Wed Foulton: Flint  Wed Foulton: Flint  Wertical Progression:  Vertical Progression:  Vertical Progression:  Vertical Progression:  Vertical Progression:  Vertical Progression:
Recrisi:  Root Face _N/A _ Tee Joint  Red lastius: _N/A _ Tee Joint  N 53 and A 65 and A 572 Gr.50
Root Face _N/A
A 53 and A 65 and A 572 Gr.50
Hiller Metals:  AVAS Specification: _A 5.18 Current / Potarity: _DCEP  TANK Classification: _ER 70 S Transfer Mode: _SPRAY  Trade Name: _Lincoln Sure Arc
Shielding: Stringer or Weave Bead:_STRINGER_ Gas. Cry Size: 5/8" to 7/8" Anilha Sex Of Shipe Pisss:_Shige Lectroder-Nat (class_F-4 Hiax Trade Name:
Prehost: Are poss Ceaning. Prehost: 32F Prehost Comperature, Min.: 32F Max.: 350F. Time (Inter pass Cemperature, Min.: 37F Max.: 350F. Time (Inter pass Cemperature, Min.: 37F Max.: 350F.
Parts shall be free of paint, oil, heavy oxides or any impurites derimental to the welding process. Chip, grind or wire burst between passes.

AWS Size Classification (b.) ER705-6 045 Process GMAW

Pass or Weld Layer(s)

Travel Speed (In/min) 15 Imp

Volts 25 Volts +/- 10%

230 amps 365 lpm 1/- 10% +/- 10%

IFW-003 REV.001

### **Fabrication Letter**



Metro Sike Fabricators LLC., 180 Industrial Park Blvd. Commerce, GA 30529 (706)335-7045

Customer: Structural Components Site Name: Portland CT

Fabrication Letter

This letter states that Metro Site provided materials in accordance with industry standards and contract documents provided to us by Structural Components, All structural steel met or exceeded the called-out grades per specifications. All galvanizing performed was in accordance with ASTM A123. All welding was in accordance with ASC and AWS D1.1 standards and work was completed by certified welders.

Kent Ramey

Fabrication Manager 180 Industrial Park Blvd. Commerce GA 30529 706-335-7045 Kent Ramey



180 Industriai Park Blvd. Commerce, Georgia 30529

## WELDING INSPECTION REPORT

SITE NAME: Portland CT

Site Number: 1680

PREPAIRED FOR: Structural Components

PREPARED BY: Benjamin J Razevich

DATE: 06/08/2023

JOB NUMBER: 8952

CWI NAME: Benjamin J Razevich

CWI # 21087031

All weldment items have been reviewed Prefabrication, during fabrication, and post fabrication and meet or exceed the requirements listed in AWS D 1.1-2020.

REVISION: 1 STAMP:

Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Seminary Sem



Centered on Solutions™

### <u>Antenna Mount Analysis</u> <u>Report</u>

Site Ref: Portland HS

97 High Street Portland, CT

Centek Project No. 22017.06

Dato: May 11, 2023

Rev 1: November 9, 2023

Max Stress Ratio = 44%

No. 289336 WALLENGTHE STONAL ENGINEERS

### Prepared for:

Verizon Wireless 20 Alexander Drive Wallingford, CT 06492 CENTEK Engineering, Inc. Mount Analysis Verizon Site Ref. ~ Portand HS Portland, CT Rev 1 ~ November 9, 2023

### Table of Contents

### SECTION 1 - REPORT

- ANTENNA AND APPURTENANCE SUMMARY
- STRUCTURE LOADING
- CONCLUSION

### SECTION 2 - CALCULATIONS

- WIND LOAD ON APPURTENANCES
- RISA3D OUTPUT REPORT
- CONNECTION

### SECTION 3 - REFERENCE MATERIALS

RF DATA SHEET

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Centered on Solutions

November 9, 2023

Mr. Phillip Cotto Structure Consulting Group 49 Brattle Street Arlington, Ma

Structural Letter ~ Antenna Mount Re: Verizon - Site Ref: Portland HS 97 Hiah Street Portland, CT

Centek Project No. 22017.06

Dear Mr. Cotto,

Centek Engineering, Inc. has reviewed the Verizon antenna installation at the above referenced site. The purpose of the review is to determine the structural adequacy of the proposed mount, consisting of three (3) V-frame sector mounts (SitePro P/N: VFA12-HD) to support the proposed equipment configuration. The review considered the effects of wind load, dead load and ice load in accordance with the 2021 International Building Code as modified by the 2022 Connecticut State Building Code (CTBC) including ASCE 7-16 and ANSI/TIA-222-H Structural Standard for Antenna Supporting Structures, Antennas and Small Wind Turbine Support Structures".

The loads considered in this analysis consist of the following:

V-Frames: Three (3) Commscope NNH4-65B-R6 panel antennas, three (3) Samsung MT6413-77A panel antennas, three (3) Samsung RT4423 panel antennas, three (3) Samsung RF4439d-25A (B2/B66A) RRHs, three (3) Samsung RF4461d-13A (B5/B13) RRHs, three (3) Samsung RF4423-48B RRHs and one (1) OVP Box mounted on three (3) V-Frames with a RAD center elevation of 90 ft +/-AGL.

The antenna mount was analyzed per the requirements of the 2021 International Building Code as modified by the 2022 Connecticut State Building Code considering a Ultimate design wind speed of 120 mph for Portland as required in Appendix P of the 2022 Connecticut State Building Code.

Based on our review of the installation, it is our opinion that the subject antenna mount has sufficient capacity to support the aforementioned antenna configuration.

If there are any questions regarding this matter, please feel free to call.

Respectfully Submitted by

Timothy J. Lynn, PE Structural Engineer

CENTEK Engineering, Inc. Mount Analysis Verizon Site Ref. ~ Portand HS Portland, CT Rev 1 ~ November 9, 2023

### Section 2 - Calculations



Centered on Solutions \*\* proventekeps.com
A2.2 North Roanford Road P: (203) 488-0580 63-2 North Branford Road Branford, CT 06405

Subject:

Location:

TIA-222-H Loads

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06

Rev. 1: 11/9/23

Development of Design Heights, Exposure Coefficients, and Velocity Pressures Per TIA-222-H

Wind Speeds

Height to Center of Antennas=

(User Input - CSBC 2022 Appendix P) Basic Wind Speed V := 120 mph (User Input - TIA-222-H Annex B)  $V_i := 50$ mph Basic Wind Speed with Ice (User Input - TIA-222-H Section 16.3) Basic Wind Speed (Mount)  $V_{m} := 30$ mph

Input

(User Input) Structure Type = Structure\_Type := Flexible

SC := III (User Input) Structure Category =

(User Input) Exposure Category = Exp := C

(User Input) Structure Height = h:= 90 (User Input)

 $z_{ant} = 90$ 

 $t_i := 1.0$ (User Input per Annex B of TIA-222-H) Radial Ice Thickness=

(User Input) Radial Ice Density= id := 56.00

(User Input) Topograpic Factor =  $K_{zt} = 1$ 

(User Input) Shielding Factor for Appurtenances =  $K_a := 1.0$ 

 $K_s := 1.0$ (User Input) Rooftop Wind Speed-up Factor =

(User Input) Ground Elevation Factor =  $K_e = 0.996$ 

(User Input) Gust Response Factor =  $G_{H} = 1.35$ 

(Per Table 2-2 of  $K_d := 0.95$ Wind Direction Probability Factor = TIA-222-H)

> l<sub>ice</sub>:= 0 if SC = 1 = 1.15 1.00 if SC = 2 1.15 if SC = 3 (Per Table 2-3 of Importance Factors = TIA-222-H)

$$K_{iz} := \left(\frac{z_{ant}}{33}\right)^{0.1} = 1.106$$
  $t_{iz} := t_i \cdot l_{ice} \cdot K_{iz} \cdot K_{zt}^{0.35} = 1.271$ 

 $t_{iz} := t_{i'} l_{ice'} K_{iz'} K_{zt}^{0.35} = 1.271$   $Kz_{ant} := 2.01 \left( \left( \frac{z_{ant}}{z_g} \right) \right)^{\frac{2}{\alpha}} = 1.238$ Velocity Pressure CoefficientAntemas=

 $qz_{ant} := 0.00256 \cdot K_{zt} \cdot K_{s} \cdot K_{e} \cdot K_{d} \cdot Kz_{ant} \cdot V^{2} = 43.16$ Velocity Pressure w/o Ice Antennas =

 $qz_{ice,ant} := 0.00256 \cdot K_{zt} \cdot K_s \cdot K_e \cdot K_d \cdot Kz_{ant} \cdot V_i^2 = 7.493$ Velocity Pressure with Ice Antennas =

 $qz_{m} := 0.00256 \cdot K_{zt} \cdot K_{s} \cdot K_{e} \cdot K_{d} \cdot Kz_{ant} \cdot V_{m}^{2} = 2.697$ Velocity Pressure with Ice Antennas =

Subject:

Rev. 1: 11/9/23

TIA-222-H Loads

Contered on Solutions\*
63-2 North Branford Road
Branford, CT 06405

P: (203) 488-0580 F: (203) 488-8587

Location:

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06

### Development of Wind & Ice Load on Appurtenances

### Appurtenance Data:

Appurtenance Model = Commscope NNH4-65B-R6

Appurtenance Shape = Flat (User Input)

Appurtenance Height= Lapp := 71.969 in (User Input)

Appurtenance Width = W<sub>app</sub> := 19.606 in (User Input)

Appurtenance Thickness = T<sub>app</sub> := 7.756 in (User Input)

Appurtenance Weight = WT<sub>app</sub> := 90 lbs (User Input)

 $Ca_{app} = 1.25$ 

Number of Appurtenances= N<sub>app</sub> := 1 (User Input)

Appurtenance Aspect Ratio =  $Ar_{app} := \frac{L_{app}}{W_{app}} = 3.7$ 

Appurtenance Force Coefficient =

### Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurte rance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurte nance Wind Force =

### Wind Load (with ice)

Surface Area for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

SurfaceArea for One Appurtenance w/lce (Side) =

Total Appurtenance Wind Force w/ be=

### Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurte nances =

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 9.8$$
 sf

$$F_{app} := qz_{ant} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{app} \cdot N_{app} = 715$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 3.9$$
 sf

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 11.5 \qquad \text{sf}$$

$$SA_{ICEappS} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right)}{144} = 5.3 \qquad \text{sf}$$

$$Fi_{app} := qz_{ice.ant} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{iCEappS} = 67$$
 lbs

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 9.8$$

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{app} F \cdot N_{app} = 45$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 3.9$$
 sf

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appS} = 18$$
 lbs

$$\begin{split} V_{app} &\coloneqq L_{app} \cdot W_{app} \cdot T_{app} = 1 \times 10^4 & \text{cuin} \\ V_{ice} &\coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \left(W_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 6053 & \text{cuin} \\ V_{ice} &\coloneqq V_{ice} &\vDash 4.000 & \text{the state} \end{split}$$

$$W_{ICEapp} := \frac{V_{ice}}{1728} \cdot Id = 196$$
 lbs



Centered on Solutions" www.centekeng.com 63-2 North Branford Road Branford, CT 06405

Subject:

TIA-222-H Loads

Portland, CT Location:

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06 Rev. 1: 11/9/23

### Development of Wind & Ice Load on Appurtenances

### Appurtenance Data:

Appurtenance Model = Samsung MT6413-77A (User Input) Appurtenance Shape =

L<sub>app</sub> := 28.9 (User Input) Appurtenance Height=

Appurtenance Width =  $W_{app} := 15.75$ (User Input)

T<sub>app</sub> := 5.51 (User Input) Appurtenance Thickness =  $WT_{app} := 60$ (User Input) Appurtenance Weight =

(User Input)  $N_{app} := 1$ Number of Appurtenances=

 $Ar_{app} := \frac{L_{app}}{W_{app}} = 1.8$ Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

### Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurte nance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

### Wind Load (with ice)

SurfaceArea for One Appurtenance w/ loe (Front)=

Total Appurtenance Wind Force w/ be=

Surface Area for One Appurtenance w/lce (Side) =

Total Appurtenance Wind Force w/ be=

### Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurte nance Wind Force =

### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurterances =

$$Ar_{app} := \frac{L_{app}}{W_{app}} = 1.8$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 3.2$$

$$F_{app} := qz_{ant}G_{H}\cdot Ca_{app}\cdot K_{a}\cdot SA_{appF} = 221$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1.1$$
 sf

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 4$$
 sf

$$SA_{ICEappS} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right)}{144} = 1.8$$
 sf

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 3.2$$

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appF} = 14$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1.1$$
 sf

$$F_{app} := qz_m \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appS} = 5$$
 lbs

$$\begin{split} &V_{app} \coloneqq L_{app} \cdot W_{app} \cdot T_{app} = 2508 & \text{cu in} \\ &V_{ice} \coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \left(W_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 2124 & \text{cu in} \\ &W_{ICEapp} \coloneqq \frac{V_{ice}}{1728} \cdot Id = 69 & \text{lbs} \end{split}$$

Subject:

TIA-222-H Loads

63-2 North Branford Road Branford, CT 06405

Location:

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06

lbs

lbs

sf

lbs

lbs

cuin

Rev. 1: 11/9/23

Flat

### Development of Wind & Ice Load on Appurtenances

### Appurtenance Data:

Appurtenance Model = Samsung RT4423

Appurtenance Shape =

(User Input)

Appurtenance Height=

Lapp := 12.3

(User Input)

Appurtenance Width =

 $W_{app} := 8.7$ 

(User Input)

Appurtenance Thickness =

(User Input)

Appurtenance Weight =

 $T_{app} := 1.4$ 

 $WT_{app} := 3$ 

(User Input)

Number of Appurtenances=

 $N_{app} := 1$ 

(User Input)

Appurtenance Aspect Ratio =

$$Ar_{app} := \frac{L_{app}}{W_{app}} = 1.4$$

Appurtenance Force Coefficient =

Surface Area for One Appurtenance (Front) =

Total Appurte nance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurte rance Wind Force =

 $SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 0.7$ sf

F<sub>app</sub> := qz<sub>ant</sub>·G<sub>H</sub>·Ca<sub>app</sub>·K<sub>a</sub>·SA<sub>appF</sub>·N<sub>app</sub> = 52

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 0.1$$

$$F_{app} := qz_{ant} \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appS} = 8$$
 lbs

### Wind Load (with ice)

Surface Area for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

Surface Area for One Appurtenance w/lce (Side) =

Total Appurtenance Wind Force w/ |ce=

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 1.2$$
 sf

$$Fi_{app} := qz_{ice.ant} \cdot G_{H} \cdot Ca_{app} \cdot K_a \cdot SA_{ICEappF} \cdot N_{app} = 14$$

$$SA_{ICEappS} = \frac{\left(L_{app} + 2 \cdot l_{iz}\right) \cdot \left(T_{app} + 2 \cdot l_{iz}\right)}{144} = 0.4$$

### Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurte rance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 0.7$$

$$F_{app} := qz_m \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appF} \cdot N_{app} = 3$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 0.1$$
 sf

### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurte rances =

$$V_{app} := L_{app} \cdot W_{app} \cdot T_{app} = 150$$

$$V_{ice} := (L_{app} + 2 \cdot t_{iz})(W_{app} + 2 \cdot t_{iz}) \cdot (T_{app} + 2 \cdot t_{iz}) - V_{app} = 508$$
 cu in

$$W_{ICEapp} := \frac{V_{ICE}}{1728} \cdot Id = 16$$
 lbs



Centered on Solutions 63-2 North Branford Road Branford, CT 06405

Subject:

TIA-222-H Loads

Location:

Rev. 1: 11/9/23

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C.

Job No. 22017.06

### Development of Wind & Ice Load on Appurtenances

### Appurtenance Data:

Appurtenance Model =

Appurtenance Shape =

Appurtenance Height=

Appurtenance Width =

Appurtenance Thickness =

Appurtenance Weight =

Number of Appurtenances=

Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

### Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

### Wind Load (with ice)

Surface Area for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ Ice=

Surface Area for One Appurtenance w/lce (Side) =

Total Appurtenance Wind Force w/ Ice=

### Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurte rance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurte rance Wind Force =

### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurterances =

### Samsung RF4439-25A(B2/B66A)RRH

Flat

(User Input)

(User Input)

(User Input)

(User Input)

(User Input)

(User Input)

$$Ar_{app} := \frac{L_{app}}{W_{app}} = 1.0$$

$$Ca_{app} = 1.2$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 1.6$$

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1$$

lbs

lbs

lhs

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 2.1$$

$$\begin{aligned} & \textbf{Fi}_{app} \coloneqq \textbf{qz}_{\text{ice.ant}} \cdot \textbf{G}_{\textbf{H}} \cdot \textbf{Ca}_{app} \cdot \textbf{K}_{\textbf{a}} \cdot \textbf{SA}_{\text{ICEappF}} = 26 \\ & \textbf{SA}_{\text{ICEappS}} \coloneqq \frac{\left(\textbf{L}_{app} + 2 \cdot \textbf{t}_{iz}\right) \cdot \left(\textbf{T}_{app} + 2 \cdot \textbf{t}_{iz}\right)}{144} = 1.5 \end{aligned}$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 1.6$$
 sf

$$F_{app} := qz_{rm} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{app} = 7$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1$$
 sf

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appS} = 5$$
 lbs

$$V_{app} := L_{app} \cdot W_{app} \cdot T_{app} = 2250$$
 cu in

$$V_{ice} \coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \left(W_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 1610 \qquad \text{cu in}$$

$$W_{ICEapp} := \frac{V_{ice}}{1728} \cdot Id = 52$$
 lbs



Centered on Solutions 63-2 North Branford Road P: (203) 488-0580 F: (203) 488-8587

Subject:

TIA-222-H Loads

Location: Portland, CT

Rev. 1: 11/9/23

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06

lbs

lbs

lbs

### Development of Wind & Ice Load on Appurtenances

### Appurtenance Data:

Appurtenance Model =

Appurtenance Shape =

Appurtenance Height=

Appurtenance Width =

Appurtenance Thickness =

Appurtenance Weight =

Number of Appurtenances=

Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

### Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurte nance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

### Wind Load (with ice)

SurfaceArea for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ Ice=

SurfaceArea for One Appurtenance w/lce (Side) =

Total Appurtenance Wind Force w/ lce=

### Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurte rance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurte rance Wind Force =

### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of Ice on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurtenances =

### Samsung RF4461d-13A(B5/B13) RRH

Flat (User Input)

L<sub>app</sub> := 14.96 (User Input)

 $W_{app} := 14.96$ (User Input)

 $T_{app} := 10.23$ (User Input)

 $WT_{app} := 80$ (User Input)

 $N_{app} := 1$ (User Input)

$$Ar_{app} := \frac{L_{app}}{W_{app}} = 1.0$$

$$Ca_{app} = 1.2$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 1.6$$
 sf

$$F_{app} := qz_{ant}G_H \cdot G_{app} \cdot K_a \cdot SA_{appF} = 109$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1.1$$
 sf

$$F_{app} := qz_{apt} \cdot G_{H} \cdot Ca_{app} \cdot K_a \cdot SA_{appS} = 74$$

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{444} = 2.1$$
 sf

$$SA_{ICEappS} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right)}{144} = 1.6$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 1.6$$
 sf

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appF} = 7$$
 lbs

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appF} = 7$$

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 1.1$$
sf

$$F_{app} := qz_m \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{appS} = 5$$

$$V_{app} := L_{app} \cdot W_{app} \cdot T_{app} = 2289$$
 cu in

$$V_{ice} \coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \left(W_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 1623 \qquad \qquad \text{cu in}$$

$$W_{ICEapp} := \frac{V_{ice}}{1728} \cdot Id = 53$$
 lbs

$$W_{ICEapp} \cdot N_{app} = 53$$
 lbs



Subject:

Location:

TIA-222-H Loads

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06

lbs

lbs

lbs

Rev. 1: 11/9/23

### Development of Wind & Ice Load on Appurtenances

### Appurtenance Data:

Appurtenance Model =

Appurtenance Shape =

Appurtenance Height=

Appurtenance Width =

Appurtenance Thickness =

Appurtenance Weight =

Number of Appurtenances=

Appurtenance Aspect Ratio =

Appurtenance Force Coefficient =

### Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurte nance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

### Wind Load (with ice)

SurfaceArea for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

Surface Area for One Appurtenance w/loe (Side) =

Total Appurtenance Wind Force w/ Ice=

### Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurtenance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of loe on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurte rances =

### Samsung RF4423-48B RRH

Flat

(User Input)

(User Input)

$$W_{app} = 8.7$$
 in

(User Input)

$$T_{app} = 3.6$$

(User Input)

$$WT_{app} := 16$$

(User Input)

(User Input)

$$Ar_{app} := \frac{L_{app}}{W_{app}} = 1.4$$

$$Ca_{app} = 1.2$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 0.7$$

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 0.3$$
 sf

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 1.1$$

$$\begin{aligned} & \text{Fi}_{\text{app}} \coloneqq \text{qz}_{\text{ice.ant}} \cdot \text{G}_{\text{H}} \cdot \text{Ca}_{\text{app}} \cdot \text{K}_{\text{a}} \cdot \text{SA}_{\text{ICEappF}} = 14 \\ & \text{SA}_{\text{ICEappS}} \coloneqq \frac{\left(\text{L}_{\text{app}} + 2 \cdot \text{t}_{\text{iz}}\right) \cdot \left(\text{T}_{\text{app}} + 2 \cdot \text{t}_{\text{iz}}\right)}{144} = 0.6 \end{aligned}$$

$$Fi_{app} := qz_{ice.ant} \cdot G_H \cdot Ca_{app} \cdot K_a \cdot SA_{ICEappS} = 7$$

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 0.7$$
 sf

$$\mathsf{F}_{app} := \mathsf{qz}_{\mathsf{m}} \cdot \mathsf{G}_{\mathsf{H}} \cdot \mathsf{Ca}_{app} \cdot \mathsf{K}_{\mathsf{a}} \cdot \mathsf{SA}_{app\mathsf{F}} = 3$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 0.3$$
 sf

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appS} = 1$$
 lbs

$$\begin{split} &V_{app} \coloneqq L_{app} \cdot W_{app} \cdot T_{app} = 370 & \text{cu in} \\ &V_{ice} \coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \! \left(W_{app} + 2 \cdot t_{iz}\right) \! \cdot \! \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 621 & \text{cu in} \end{split}$$

$$W_{ICEapp} := \frac{V_{ice}}{1728} \cdot Id = 20$$
 lbs

$$W_{ICEapp} \cdot N_{app} = 20$$
 lbs



TIA-222-H Loads

Branford, CT 06405

Development of Wind & Ice Load on Appurtenances

Location:

Subject:

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C. Job No. 22017.06

### Appurtenance Data:

Appurtenance Model = OVP Box

Rev. 1: 11/9/23

Appurtenance Shape = Flat (User Input)

 $L_{app} := 29.5$ Appurtenance Height= (User input)

W<sub>app</sub> := 16.5 Appurtenance Width = (User Input)

T<sub>app</sub> := 12,6 Appurtenance Thickness = (User Input)

Appurlenance Weight =  $WT_{app} := 32$ (User Input)

Number of Appurtenances=  $N_{app} := 1$ (User Input)

 $Ar_{app} := \frac{L_{app}}{W_{app}} = 1.8$ Appurtenance Aspect Ratio ≂

Appurtenance Force Coefficient =  $Ca_{app} = 1.2$ 

### Wind Load (without ice)

Surface Area for One Appurtenance (Front) =

Total Appurte nance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurtenance Wind Force =

### Wind Load (with ice)

SurfaceArea for One Appurtenance w/ Ice (Front)=

Total Appurtenance Wind Force w/ be=

SurfaceArea for One Appurtenance w/ Ice (Side) =

Total Appurte nance Wind Force w/ be=

### Wind Load (Mount)

Surface Area for One Appurtenance (Front) =

Total Appurterance Wind Force =

Surface Area for One Appurtenance (Side) =

Total Appurte nance Wind Force =

### Gravity Loads (ice only)

Volume of Each Appurtenance =

Volume of loe on Each Appurtenance =

Weight of Ice on Each Appurtenance =

Weight of Ice on All Appurte nances =

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 3.4$$
 sf

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 2.6$$
 sf

$$SA_{ICEappF} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(W_{app} + 2 \cdot t_{iz}\right)}{144} = 4.2$$

$$Fi_{app} := qz_{ice.ant} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{ICEappF} = 51$$
 lbs

$$SA_{ICEappS} := \frac{\left(L_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right)}{144} = 3.4$$
 sf

lbs

$$SA_{appF} := \frac{L_{app} \cdot W_{app}}{144} = 3.4$$

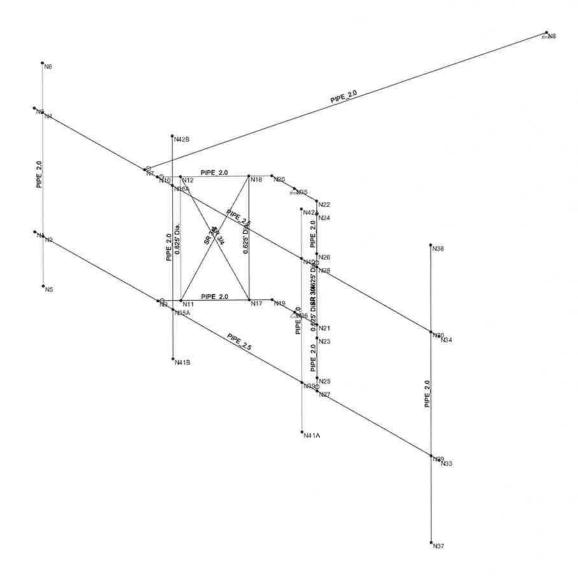
$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appF} = 15$$
 lbs

$$SA_{appS} := \frac{L_{app} \cdot T_{app}}{144} = 2.6$$
 sf

$$F_{app} := qz_{m} \cdot G_{H} \cdot Ca_{app} \cdot K_{a} \cdot SA_{appS} = 11$$
 lbs

$$\begin{split} &V_{app} \coloneqq L_{app} \cdot W_{app} \cdot T_{app} = 6133 & \text{cu in} \\ &V_{ice} \coloneqq \left(L_{app} + 2 \cdot t_{iz}\right) \left(W_{app} + 2 \cdot t_{iz}\right) \cdot \left(T_{app} + 2 \cdot t_{iz}\right) - V_{app} = 3107 & \text{cu in} \\ &W_{ICEapp} \coloneqq \frac{V_{ice}}{1728} \cdot Id = 101 & \text{lbs} \\ &W_{ICEapp} \cdot N_{app} = 101 & \text{lbs} \end{split}$$





Envelope Only Solution

Centek Engineering		
TJL	Portland HS	Nov 9, 2023 at 8:58 AM
22017.06	Member Framing	Mount.R3D



Company Designer Job Number Model Name : Centek Engineering

: TJL : 22017.06 : Portland HS Nov 9, 2023 8:57 AM Checked By:\_\_\_\_

# (Global) Model Settings

( eleman, integer cottaines	
Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (ft/sec^2)	32.2
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver
Hot Rolled Steel Code	AISC 15th(360-16): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 15th(360-16): LRFD
Cold Formed Steel Code	AISI \$100-10: ASD
Wood Code	AWC NDS-12: ASD
Wood Temperature	< 100F
Concrete Code	ACI 318-11
Masonry Code	ACI 530-11: ASD
Aluminum Code	AA ADM1-10: ASD - Building
Stainless Steel Code	AISC 14th(360-10): ASD
Adjust Stiffness?	Yes(Iterative)
Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR SET ASTMA615
Min % Steel for Column	1
May % Steel for Column	Q

8

Max % Steel for Column



Company : Centek Engineering Designer : TJL

Designer : TJL
Job Number : 22017.06
Model Name : Portland HS

Nov 9, 2023 8:57 AM Checked By:\_\_\_\_

# (Global) Model Settings, Continued

(Giobai) Model Cettings, Continu	ACCE 7.40
Seismic Code	ASCE 7-10
Seismic Base Elevation (ft)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	
SDS	1
S1	1
TL (sec)	5
Risk Cat	l or II
Drift Cat	Other
Om Z	
Om X	1
Cd Z	
Cd X	1
Rho Z	1
Rho X	1
Footing Overturning Safety Factor	1
Optimize for OTM/Sliding	No
Check Concrete Bearing	No
Footing Concrete Weight (k/ft^3)	150.001
Footing Concrete f'c (ksi)	4
Footing Concrete Ec (ksi)	3644
Lambda	1
Footing Steel fy (ksi)	60
Minimum Steel	0.0018
Maximum Steel	0.0075
Footing Top Bar	#3
Footing Top Bar Cover (in)	2
Footing Bottom Bar	#3
Footing Bottom Bar Cover (in)	3.5
	#3
Pedestal Bar Cover (in)	1.5
Pedestal Bar Cover (in)	#3
Pedestal Ties	<i>m</i> 0

# Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (\	. Density[k/ft^3]	Yield[ksi]	Ry	Fu[ksi]	Rt
1	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	58	1.2
3	A992	29000	11154	.3	.65	.49	50	1.1	58	1.2
4	A500 Gr.42	29000	11154	.3	.65	.49	42	1.3	58	1.1
5	A500 Gr.46	29000	11154	.3	.65	.49	46	1.2	58	1.1
6	A53 Grade B	29000	11154	.3	.65	.49	35	1.5	58	1.2



Company : Centek Engineering Designer : TJL

Job Number : 22017.06
Model Name : Portland HS

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# Hot Rolled Steel Section Sets

_	Label	Shape	Type	Design List	Material	Design	A fin21	lvv (in4)	Izz fin41	J [in4]
1	Antenna Mast_2.0	PIPE 2.0	Column	Pipe	A53 Grade B	Typical	1.02	.627	.627	1.25
2	Horizontal_2.5 ST	PIPE 2.5	Beam	Pipe	A53 Grade B			1.45	1.45	2.89
3	Outrigger_2.0 ST	PIPE 2.0	Beam	Pipe	A53 Grade B			.627	.627	1.25
4	Stabilizer_2.0 ST	PIPE 2.0	Beam	Pipe	A53 Grade B			.627	.627	1.25
5	0.625" Dia. Bar	0.625' Dia.	Column	BAR	A36 Gr.36			.007	.007	.015
6	0.75"Dia. Bar	SR 3/4	Column	BAR	A36 Gr.36			.016	.016	.031

# Hot Rolled Steel Design Parameters

	Label	Shape	Length[ft]	Lbyy[ft]	Lbzz[ft]	Lcomp topf.	Lcomp bot[.	.L-tora	Kyy	Kzz	Сь	Functi
1	M1	Horizontal_2.5 STD	12.5	Segment		Lbyy	i					Lateral
2	M2	Horizontal_2.5 STD	12.5	Segment		Lbyy						Lateral
3	M3	Stabilizer_2.0 STD	10.18			Lbvv						Lateral
4	M4	Outrigger_2.0 STD	2.521	Segment	Segment					- 10		Lateral
5	M5	Outrigger_2.0 STD	2.521	Segment	$\overline{}$							Lateral
6	M6	Outrigger_2.0 STD	2.521		Segment					-4		Lateral
7	M7	Outrigger_2.0 STD	2.521	Segment								Lateral
8	M8	0.625" Dia. Bar	3.333									Lateral
9	M9	0.625" Dia. Bar	3.333									Lateral
10	M10	0.75"Dia. Bar	3.659	1.83	1.83	Lbyy						Lateral
11	M11	0.625" Dia. Bar	3.333									Lateral
12	M12	0.75"Dia. Bar	3.659	1.83	1.83	Lbyy		4 - 2				Lateral
13	M13	0.625" Dia. Bar	3.333									Lateral
14	M14	0.75"Dia. Bar	3.659	1.83	1.83	Lbyy					E01	Lateral
15	M15	0.75"Dia. Bar	3.659	1.83	1.83	Lbyy						Lateral
16	PS.2	Antenna Mast_2.0	6			Lbvv						Lateral
17	PS.1	Antenna Mast_2.0	8			Lbyy						Lateral
18	M19	Antenna Mast_2.0	6			Lbyy						Lateral
19	M21A	Antenna Mast_2.0	6			Lbyy						Lateral

# Member Primary Data

	Label	I Joint	J Joint	K Joint Ro	otate(		Type	Design List	Material	Design
1	M1	N2	N34			Horizontal_2.5 STD Pipe	Beam	Pipe	A53 Grade B	Typical
2	<u>M2</u>	N1	N33			Horizontal_2.5 STD Pipe	Beam	Pipe	A53 Grade B	Typical
3	M3	N7	N8			Stabilizer_2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
4	M4	N10	N20			Outrigger_2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
5	M5	N9	N19			Outrigger_2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
6	M6	N28	N22	i l		Outrigger_2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
7	M7	N27	N21			Outrigger_2.0 STD Pipe	Beam	Pipe	A53 Grade B	Typical
8	M8	N12	N11			0.625" Dia. Bar	Column	BAR	A36 Gr.36	Typical
9	M9	N18	N17			0.625" Dia. Bar	Column	BAR	A36 Gr.36	Typical
10	M10	N12	N17			0.75"Dia. Bar	Column	BAR	A36 Gr.36	Typical
11	M11	N26	N25			0.625" Dia. Bar	Column	BAR	A36 Gr.36	Typical
12	M12	N18	N11			0.75"Dia. Bar	Column	BAR	A36 Gr.36	Typical
13	M13_	N24	N23			0.625" Dia. Bar	Column	BAR	A36 Gr.36	Typical
14	M14	N26	N23			0.75"Dia. Bar	Column	BAR	A36 Gr.36	Typical
15	M15	N24	N25			0.75"Dia. Bar	Column	BAR	A36 Gr.36	Typical
16	PS.2	N5	N6			Antenna Mast_2.0 STD Pi	Column	Pipe	A53 Grade B	Typical
17	PS.1	N37	N38			Antenna Mast_2.0 STD Pi	Column	Pipe	A53 Grade B	Typical



: Centek Engineering

: TJL : 22017.06 Job Number Model Name Portland HS Nov 9, 2023 8:57 AM Checked By:\_\_

Member Primary Data (Continued)

	Label	I Joint	J Joint	K Joint Rotate(.	Section/Shape	Type	Design List	Material	Design
18	M19	N41A	N42A		Antenna Mast 2.0 STD Pi	Column	Pipe	A53 Grade B	Typical
19	M20	N19	N21		RIGID	None	None	RIGID	Typical
20	M21	N20	N22		RIGID	None	None	RIGID	Typical
21	M21A	N41B	N42B		Antenna Mast_2.0 STD Pi	Column	Pipe	A53 Grade B	Typical

Joint Coordinates and Temperatures

Joint Co	ordinates and		A Classical	7 (4)	Temp [F]	Detach From Dia
	Label	X [ft]	Y [ft]	Z [ft] -0.	0 ( emp	Detacit From Dia
_1	N1	0	0.	-0.	0	
2	N2	0	3.333334		0	
3	N3	.25	0.	-0.		G =
4	N4	.25	3.333334	-0.	0	
5	N5	.25	-1.333333	-0.	0	
6	N6	.25	4.666667	-0.	0	
7	N7	3.390625	3.333334	-0.	0	
8	N8	6.025403	3.333334	-9.833125	0	
9	N9	3.78125	0.	-0.	0	
10	N10	3.78125	3.333334	-0.	0	
11	N11	4.138628	0.	-0.357378	0	
12	N12	4.138628	3.333334	-0.357378	0	
13	N17	5.206335	0.	-1.425085	0	
14	N18	5.206335	3.333334	-1.425085	0	
15	N19	5.563713	0.	-1.782463	0	
16	N20	5.563713	3.333334	-1.782463	0	
17	N21	6.936287	0.	-1.782463	0	
18	N22	6.936287	3.333334	-1.782463	0	
19	N23	7.293665	0.	-1.425085	0	
20	N24	7.293665	3.333334	-1.425085	0	
21	N25	8.361372	0.	-0.357378	0	
22	N26	8.361372	3.333334	-0.357378	0	
23	N27	8.71875	0.	-0.	0	
24	N28	8.71875	3.333334	-0.	0	
25	N29	12.25	0.	-0.	0	
26	N30	12.25	3.333334	-0.	0	
27	N33	12.5	0.	<b>-</b> 0.	0	
28	N34	12.5	3.333334	-0.	0	
	N35	6.25	3.333334	-1.782463	0	
29	N36	6.25	0.	-1.782463	0	
30	N35A	4.25	0.	-0.	0	
31		4.25	3.333334	-0.	0	
32	N36A	12.25	-2.333333	0	0	
33	N37	12.25	5.666667	0	0	
34	N38		0.	-0.	0	
35	N39	8.25	3.333334	-0.	0	
36	N40	8.25		-0.	0	
37	N41A	8.25	-1.333333	-0.	0	
38	N42A	8.25	4.666667	-0.	0	
39	N41B	4.25	-1.333333		0	
40	N42B	4.25	4.666667	-0.	U	



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# Joint Boundary Conditions

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
1	N8	Reaction	Reaction	Reaction			= mount toract
2	N19					Table 1 and	
3	N20						
4	N17						
5	N18						
6	N21				Table to the same		Chromate Co. Land
7	N22				1		
8	N23						
9	N24						
10	N35	Reaction	Reaction	Reaction			
11	N36	Reaction	Reaction	Reaction			

# Member Point Loads (BLC 2 : Dead Load)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	Y	045	1.5
2	PS.1	Y	045	6.5
3	PS.2	Υ	03	2
4	PS.2	Y	03	4
5	PS.1	Υ	075	3
6	PS.1	Y	08	5
7	M21A	Y	016	1
8	M19	Y	032	%50
9	M21A	Y	003	%50

# Member Point Loads (BLC 3 : Ice Load)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	Y	098	1.5
2	PS.1	Y	098	6.5
3	PS.2	Y	035	2
4	PS.2	Υ	035	4
5	PS.1	Y	052	3
6	PS.1	Y	053	5
7	M21A	Y	02	1
8	M19	Y	101	%50
9	M21A	Y	016	%50

# Member Point Loads (BLC 6: Wind with Ice X)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	X	.034	1.5
2	PS.1	X	.034	6.5
3	PS.2	X	.011	2
4	PS.2	X	.011	4
5	PS.1	X	.019	3
6	PS.1	X	.019	5
7	M21A	X	.007	1
8	M19	X	.041	%50
9	M21A	X	.005	%50



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# Member Point Loads (BLC 7: Wind X)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	X	.142	1.5
2	PS.1	X	.142	6.5
3	PS.2	X	.039	2
4	PS.2	X	.039	4
5	PS.1	X	.073	3
6	PS.1	X	.074	5
7	M21A	X	.021	1
8	M19	X	.18	%50
9	M21A	X	.008	%50

# Member Point Loads (BLC 8 : Wm Wind X)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	X	.009	1.5
2	PS.1	X	.009	6.5
3	PS.2	X	.003	2
4	PS.2	X	.003	4
5	PS.1	X	.005	3
6	PS.1	X	.005	5
7	M21A	X	.001	1
8		X	.011	%50
9	M21A	X	.001	%50

# Member Point Loads (BLC 9: Wind with Ice Z)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	Z	.073	1.5
2	PS.1	Z	.073	6.5
3	PS.2	Z	.024	2
4	PS.2	Z	.024	4
5	M19	Z	.051	%50
6	M21A	Z	.014	%50

# Member Point Loads (BLC 10 : Wind Z)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft, %]
1	PS.1	Z	.358	1.5
2	PS.1	Z	.358	6.5
3	PS.2	Z	.111	2
4	PS.2	Z	.111	4
5	M19	Z	.236	%50
6	M21A	7	.052	%50

# Member Point Loads (BLC 11 : Wm Wind Z)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	PS.1	Z	.023	1.5
2	PS.1	Z	.023	6.5
3	PS.2	Z	.007	2
4	PS.2	Z	.007	4
5	M19	Z	.015	%50
6	M21A	Z	.003	%50



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# Member Distributed Loads (BLC 6: Wind with Ice X)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/	.Start Location[ft,%]	End Location[ft,%]
1	M3	X	.003	.003	0	0
2	M4	X	.003	.003	0	0
3	M5	X	.003	.003	0	0
4	M6	X	.003	.003	0	0
5	M7	X	.003	.003	0	0
6	M8	X	.003	.003	0	0
7	M9	X	.003	.003	0	0
8	M10	X	.003	.003	0	0
9	M11	X	.003	.003	0	0
10	M12	X	.003	.003	0	0
11	M13	X	.003	.003	0	0
12	M14	X	.003	.003	0	0
13	M15	X	.003	.003	0	0
14	PS.2	X	.003	.003	0	0
15	PS.1	X	.003	.003	0	0
16	M19	X	.003	.003	0	0
17	M20	X	.003	.003	0	0
18	M21	X	.003	.003	0	0
19	M21A	X	.003	.003	0	0

# Member Distributed Loads (BLC 7 : Wind X)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/	Start Location[ft,%]	End Location[ft,%]
1	M3	X	.018	.018	0	0
2	M4	X	.018	.018	0	0
3	M5	X	.018	.018	0	0
4	M6	X	.018	.018	0	0
5	M7	X	.018	.018	0	0
6	M8	X	.018	.018	0	0
7	M9	X	.018	.018	0	0
8	M10	X	.018	.018	0	0
9	M11	X	.018	.018	0	0
10	M12	X	.018	.018	0	0
11	M13	X	.018	.018	0	0
12	M14	X	.018	.018	0	0
13	M15	X	.018	.018	0	0
14	PS.2	X	.018	.018	0	0
15	PS.1	X	.018	.018	0	0
16	M19	X	.018	.018	0	0
17	M20	X	.018	.018	0	0
18	M21	X	.018	.018	0	0
19	M21A	X	.018	.018	0	0

# Member Distributed Loads (BLC 8: Wm Wind X)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/	Start Location[ft,%]	End Location[ft,%]
1	M3	X	.003	.003	0	0
2	M4	X	.003	.003	0	0
3	M5	X	.003	.003	0	0
4	M6	X	.003	.003	0	0
5	M7	X	.003	.003	0	0
6	M8	X	.003	.003	0	0



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# Member Distributed Loads (BLC 8 : Wm Wind X) (Continued)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/S	Start Location[ft,%	] End Location[ft,%]
7	M9	X	.003	.003	0	0
8	M10	X	.003	.003	0	0
9	M11	X	.003	.003	0	0
10	M12	X	.003	.003	0	0
11	M13	X	.003	.003	0	0
12	M14	X	.003	.003	0	0
13	M15	X	.003	.003	0	0
14	PS.2	X	.003	.003	0	0
15	PS.1	X	.003	.003	0	0
16	M19	X	.003	.003	0	0
17	M20	X	.003	.003	0	0
18	M21	X	.003	.003	0	0
19	M21A	X	.003	.003	0	0

# Member Distributed Loads (BLC 9 : Wind with Ice Z)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/	.Start Location[ft,%]	End Location[ft,%]
1	M1	Z	.003	.003	0	0
2	M2	Z	.003	.003	0	0
3	M3	Z	.003	.003	0	0
4	M4	Z	.003	.003	0	0
5	M5	Z	.003	.003	0	00
6	M6	Z	.003	.003	0	0
7	M7	Z	.003	.003	0	0
8	M8	Z	.003	.003	0	0
9	M9	Z	.003	.003	0	0
10	M10	Z	.003	.003	0	0
11	M11	Z	.003	.003	0	0
12	M12	Z	.003	.003	0	0
13	M13	Z	.003	.003	0	0
14	M14	Z	.003	.003	0	0
15	M15	Z	.003	.003	0	0
16	PS.2	Z	.003	.003	0	0
17	M19	Z	.003	.003	0	0
18	M20	Z	.003	.003	0	0
19	M21	Z	.003	.003	0	0
20	M21A	Z	.003	.003	0	0

# Member Distributed Loads (BLC 10 : Wind Z)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/5	Start Location[ft,%	] End Location[ft,%]
1	M1	Z	.018	.018	0	0
2	M2	Z	.018	.018	0	0
3	M3	Z	.018	.018	0	0
4	M4	Z	.018	.018	0	0
5	M5	7	.018	.018	0	0
6	M6	Z	.018	.018	0	0
7	M7	7	.018	.018	0	0
8	M8	7	.018	.018	0	0
9	M9	7	.018	.018	0	0
10	M10	7	.018	.018	0	0
11	M11	7	.018	.018	0	0
12	M12	Z	.018	.018	0	0



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# Member Distributed Loads (BLC 10: Wind Z) (Continued)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude(k/	Start Location[ft.%	End Location[ft,%]
13	M13	Z	.018	.018	0	0
14	M14	Z	.018	.018	0	0
15	M15	Z	.018	.018	0	0
16	PS.2	Z	.018	.018	0	0
17	M19	Z	.018	.018	0	0
18	M20	Z	.018	.018	0	0
19	M21	Z	.018	.018	0	0
20	M21A	Z	.018	.018	0	0

# Member Distributed Loads (BLC 11: Wm Wind Z)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/	Start Location[ft,%]	End Location[ft,%]
1	M1	Z	.003	.003	0	0
2	M2	Z	.003	.003	0	0
3	М3	Z	.003	.003	0	0
4	M4	Z	.003	.003	0	0
5	M5	Z	.003	.003	0	0
6	M6	Z	.003	.003	0	0
7	M7	Z	.003	.003	0	0
8	M8	Z	.003	.003	0	0
9	M9	Z	.003	.003	0	0
10	M10	Z	.003	.003	0	0
11	M11	Z	.003	.003	0	0
12	M12	Z	.003	.003	0	0
13	M13	Z	.003	.003	0	0
14	M14	Z	.003	.003	0	0
15	M15	Z	.003	.003	0	0
16	PS.2	Z	.003	.003	0	0
17	M19	Z	.003	.003	0	0
18	M20	Z	.003	.003	0	0
19	M21	Z	.003	.003	0	0
20	M21A	Z	.003	.003	0	0

# **Basic Load Cases**

	BLC Description	Category	X Gra	Y Gra	Z Gra	Joint	Point	Distrib.	.Area(	Surfa
1	Self Weight	None		41						
2	Dead Load	None					9			
3	Ice Load	None					9			
4	Lm Maintenance Load (500lb)	None	The state of					100	100	
5	Lv Maintenance Load (250lb)	None								
6	Wind with Ice X	None					9	19		
7	Wind X	None					9	19		
8	Wm Wind X	None					9	19		
9	Wind with Ice Z	None					6	20		
10	Wind Z	None					6	20		
11	Wm Wind Z	None					6	20		



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# Load Combinations

	Description	So	P	S	BLC	Fac	BLC	Fac.	BLC	Fac	BLC	Fac.	BLC	Fac.	BLC	Fac.	BLC	Fac.	.BLC	Fac	BLC	Fac	BLC	Fac
1	1.4D	Yes	Y		1	1.4	2	1.4																
2	1.2D +1.5Lv	Yes	Y		1	1.2	2	1.2	5	1.5			100			1000				300				I To
3	1.2D + 1.0W (X-directi	Yes	Y		1	1.2	2	1.2	7	1														
4	1.2D + 1.0Di + 1.0Wi (	.Yes	Y		1	1.2	2	1.2	3	1	6	1				Bu						( IV)		10
5	1.2D +1.5Lm+ 1.0Wm	Yes	Υ		1	1.2	2	1.2	4	1.5	8	1												
6	1.2D + 1.0W (Z-directi	Yes	Y	15	1	1.2	2	1.2	10	1		NO.												
7	1.2D + 1.0Di + 1.0Wi (	Yes	Υ		1	1.2	2	1.2	3	1	9	1												
8	1.2D +1.5Lm+ 1.0Wm	Yes	Υ		1	1.2	2	1.2	4	1.5	11	1	0											

Envelope Joint Reactions

	Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	.233	3	.025	1	.919	6	0	8	0	8	0	8
2	, I ve live, e	min	271	6	.021	3	-1.212	3	0	1	0	1	0	1
3	N35	max	133	6	.687	7	.804	3	0	8	0	8	0	8
4	1100	min	-1.769	3	.384	3	-2.878	6	0	1	0	1	0	1
5	N36	max	.86	7	.658	4	.68	4	0	8	0	8	0	8
6		min	568	3	.247	6	958	6	0	1	0	1	0	1
7	Totals:	max	0	8	1.335	4	0	3						
8	7 0 000	min	-2.104	3	.827	8	-2.918	6					1488	

Envelope Joint Displacements

	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotation [rad]	LC	Z Rotation [rad]	LC
1	N1	max	.063	3	.035	6	.3	6	3.976e-03	6	1.2e-02	6	9.437e-04	3
2		min	115	6	031	3	035	1	-2.189e-03	3	-4.5e-04	4	-9.599e-04	6
3	N2	max	.036	3	.035	6	.452	6	2.539e-03	6	1.23e-02	6	1.072e-03	3
4		min	045	6	032	3	009	4	-2.295e-03	3	-3.806e-04	4	-9.84e-04	6
5	N3	max	.063	3	.032	7	.264	6	3.976e-03	6	1.2e-02	6	9.436e-04	3
6	197	min	115	6	028	3	034	1	-2.189e-03	3	-4.5e-04	4	-9.599e-04	6
7	N4	max	.036	3	.032	7	.415	6	2.539e-03	6	1.23e-02	6	1.072e-03	3
8		min	045	6	028	3	008	4	-2.295e-03	3	-3.806e-04	4	-9.84e-04	6
9	N5	max	.079	3	.032	7	.201	6	3.906e-03	6	1.2e-02	6	1.014e-03	3
10		min	13	6	028	3	045	1	-2.189e-03	3	-4.5e-04	4	-9.599e-04	6
11	N6	max	.02	3	.032	7	.456	6	2.609e-03	6	1.23e-02	6	1.002e-03	3
12	110	min	029	6	028	3	041	3	-2.295e-03	3	-3.806e-04	4	-9.841e-04	6
13	N7	max	.036	3	.034	7	.016	3	1.447e-03	6	9.639e-03	6	6.175e-04	3
14		min	045	6	.011	3	018	6	-1.158e-03	3	-1.301e-03	3	-2.923e-04	6
15	N8	max	0	8	0	8	0	8	1.91e-03	1	7.888e-03	3	1.312e-03	3
16		min	0	1	0	1	0	1	1.435e-03	3	5.127e-05	2	-1.996e-04	6
17	N9	max	.062	3	.033	7	.082	3	2.235e-03	6	5.246e-03	6	3.777e-04	3
18		min	115	6	.013	3	152	6	-8.113e-04	3	-4.928e-04	1	-4.431e-04	6
19	N10	max	.036	3	.033	7	.023	3	1.311e-03	6	8.501e-03	6	3.855e-04	3
20	1110	min	045	6	.013	3	061	6	-1.017e-03	3	-1.196e-03	3	-4.005e-04	7
21	N11	max	.05	3	.037	7	.069	3	2.019e-03	6	2.987e-03	3	1.281e-04	3
22		min	09	6	.013	3	127	6	-5.166e-04	3	-5.778e-03	6	-8.88e-04	6
23	N12	max	.024	3	.037	7	.012	3	1.391e-03	6	2.666e-03	3	4.435e-04	3
24		min	036	6	.013	3	053	6	-7.218e-04	3	-2.003e-03	6	-5.474e-04	7
25	N17	max	.011	3	.036	7	.031	3	1.191e-03	6	2.786e-03	3	-4.683e-04	3
26		min	02	6	.004	3	058	6	1.051e-04	3	-4.897e-03	6	-2.42e-03	7



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# Envelope Joint Displacements (Continued)

	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	10	Y Rotation [rad]	ıc	Z Rotation [rad]	LC
27	N18	max	0	3	.036	7	005	2	1.01e-03	7	4.415e-04	3	-2.46e-04	3
28		min	01	6	.004	3	029	6	-5.278e-05	3	-2.066e-03	6	-2.361e-03	7
29	N19	max	0	8	.027	7	.02	3	6.829e-04	7	2.43e-03	3	-4.687e-04	3
30		min	0	1	.004	3	038	6	3.857e-04	3	-4.619e-03	6	-3.33e-03	7
31	N20	max	0	8	.027	7	004	2	6.565e-04	7	-5.094e-04	2	-4.791e-04	3
32		min	0	1	.004	3	02	6	4.026e-04	6	-2.371e-03	6	-3.328e-03	7
33	N21	max	0	8	004	3	.038	6	6.829e-04	7	2.43e-03	3	-4.687e-04	3
34		min	0	1	027	7	02	3	3.857e-04	3	-4.619e-03	6	-3.33e-03	7
35	N22	max	0	8	004	3	.02	6	6.565e-04	7	-5.094e-04	2	-4.791e-04	3
36		min	0	1	027	7	.004	2	4.026e-04	6	-2.371e-03	6	-3.328e-03	7
37	N23	max	.011	3	008	3	.059	6	2.79e-04	3	2.787e-03	3	-6.364e-04	3
38		min	021	6	042	7	031	3	-3.293e-04	6	-5.187e-03	6	-2.611e-03	7
39	N24	max	001	3	008	3	.03	6	5.174e-04	3	5.077e-04	3	-3.814e-04	3
40	114	min	01	6	042	7	.005	2	-5.375e-04	6	-2.405e-03	6	-2.64e-03	7
41	N25	max	.049	3	019	3	.131	6	4.08e-04	3	3.007e-03	3		
42	1420	min	092	6	049	7	069	3	-1.606e-03	6		-	-1.206e-03	7
43	N26	max	.024	3	019	3	.06	6	5.829e-04	3	-5.675e-03	3	-2.55e-03	
44	1420	min	038	6	049	7	014	3			2.813e-03	_	-5.439e-04	3
45	N27	max	.062	3	028	3	.155	6	-1.67e-03 9.807e-04	6	-2.047e-03	6	-2.545e-03	7
46	INZI	min	116	6	057	7	082	3	-1.518e-03	3	3.068e-03	3	-1.82e-03	3
47	N28	max	.037	3	025	_	.069			6	-1.661e-02	6	-3.895e-03	7
48	IVZO	min	046	6	025	7	027	6	1.105e-03	3	2.157e-03	3	-1.342e-03	3
49	N29	max	.062	3	12	•	1.127		-1.011e-03	6	-1.498e-02	6	-3.91e-03	7
50	IVZ	min	116	6		3		6	1.489e-03	3	2.584e-03	3	-7.332e-04	3
51	N30	max	.037	3	296	7	198	3	-4.803e-03	6	-2.599e-02	6	-4.428e-03	7
52	1430	min	046	6	12	3	1.022	6	1.555e-03	3	2.602e-03	3	-1.698e-03	3
53	N33	max	.062	3	296	7	131	3	-6.971e-04	7	-2.611e-02	6	-4.426e-03	7
54	NOO	min	116		122	3	1.205	6	1.489e-03	3	2.584e-03	3	-7.333e-04	3
55	N34	max	.037	6	31	7	206	3	-4.803e-03	6	-2.599e-02	6	-4.428e-03	7
56	1134	min		3	125	3	1.1	6	1.555e-03	3	2.602e-03	3	-1.698e-03	3
57	N35	max	046	6	31	7	139	3	-6.971e-04	7	-2.611e-02	6	-4.426e-03	7
58	INGO	min	0	8	0	8	0	8	6.565e-04	7	-5.094e-04	2	-4.791e-04	3
59	N36	max	0	1	0	1	0	1	4.026e-04	6	-2.371e-03	6	-3.328e-03	7
60	INOO	min	0	8	0	8	0	8	6.829e-04	7	2.43e-03	3	-4.687e-04	3
	N35A	max	0	1	0	1	0	1	3.857e-04	3	-4.619e-03	6	-3.33e-03	7
61 <b>62</b>	ACCN	min	.062	3	.03	4	.072	3	1.958e-03	6	3.444e-03	6	1.989e-04	3
63	N36A	max	115	6	.012	6	176	6	-7.375e-04	3	-5.307e-04	1	-7.034e-04	7
	NOOA	min	.036	3	.03	4	.028	3	1.14e-03	6	6.615e-03	6	1.487e-04	3
64	N37		045	6	.012	6	104	6	-8.946e-04	3	-6.161e-04	3	-6.81e-04	7
65	N37	max	.062	3	12	3	1.292	6	1.488e-03	3	2.584e-03	3	1.322e-04	3
66	NOO	min	206	6	296	7	24	3	-6.029e-03	6	-2.599e-02	6	-4.418e-03	7
67	N38	max	.14	4	12	3	1.06	6	1.556e-03	3	2.602e-03	3	-2.2e-03	2
68	NICO	min	.043	6	296	7	087	3	-4.472e-04	7	-2.611e-02	6	-4.435e-03	7
69	N39	max	.062	3	018	6	.069	6	9.05e-04	3	3.152e-03	3	-1.268e-03	3
70	1110	min	116	6	038	4	065	3	-1.203e-03	6	-1.414e-02	6	-2.813e-03	7
71	N40	max	.037	3	018	6	002	2	9.904e-04	3	2.038e-03	3	<b>-</b> 7.735e-04	3
72	NIAA A	min	046	6	038	4	015	3	-1.206e-03	6	-1.214e-02	6	-2.824e-03	7
73	N41A	max	.043	3	018	6	.089	6	9.05e-04	3	3.152e-03	3	-1.198e-03	3
74	N145.5	min	144	6	038	4	079	3	-1.273e-03	6	-1.414e-02	6	-2.813e-03	7
75	N42A	max	.061	4	018	6	.001	3	9.904e-04	3	2.038e-03	3	-8.439e <b>-</b> 04	3
76	A14.	min	017	6	038	4	026	6	-1.135e-03	6	-1.214e-02	6	-2.824e-03	7
77	N41B	max	.067	3	.03	4	.084	3	1.887e-03	6	3.444e-03	6	2.808e-04	3
78		min	125	6	.012	6	207	6	-7.374e-04	3	-5.307e-04	1	-7.032e-04	7



: Centek Engineering

: TJL : 22017.06 : Portland HS Nov 9, 2023 8:57 AM Checked By:\_\_\_

**Envelope Joint Displacements (Continued)** 

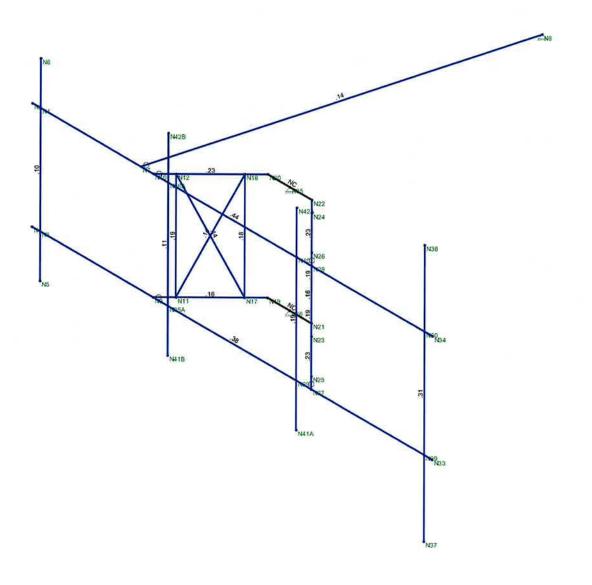
	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotation [rad]	LC	Z Rotation [rad]	LC
79	N42B	max		3	.03	4	.017	4	1.211e-03	6	6.615e-03	6	7.826e-05	3
80		min	- 036	6	.012	6	085	6	-8.947e-04	3	-6.161e-04	3	-6.81e-04	7

Envelope AISC 15th(360-16): LRFD Steel Code Checks

	Mem	Shape	Code Check	L	LC	Sh	.Loc[ft]	Dir	phi*P	phi*P	phi*Mn y-y [k-ft]		.Cb Eqn
1	M1	PIPE 2.5	.444	8	6	.109	3.776		6 14.559	50.715	3.596	and the second section	2H1
2	M2	PIPE 2.5	.383	8	6	.094	8.724		6 14.559	50.715	3.596		2H1
3	M3	PIPE 2.0	.143	5	3	.009	10.18		3 9.492	32.13	1.872	1.8	1H1
4	M4	PIPE 2.0	.228	2	3	.084	2.521	V-C	3 32.032	32.13	1.872	1.8	1H1
5	M5	PIPE 2.0	.160	2	7	.068	2.521		4 32.032		1.872	1.8	1 H1
6	M6	PIPE 2.0	.231	2	7	.086	.499		7 32.032	32.13	1.872	1.8	1, H1
7	M7	PIPE 2.0	.226	2	7	.091	.499		7 32.032	32.13	1.872	1.8	1 H1
8	M8	0.625' Dia.	.190	3	6	.024	3.333		6 1.058	9.94	.104	.104	2 H1
9		0.625' Dia.	.177	0	3	.019	0		6 1.058	9.94	.104	.104	2 H1
10	M10	SR 3/4	.141	0	3	020	0		6 6.954	14.314	.179	.179	1 H1
11	-	0.625' Dia.	.194	0	3	.023	0		6 1.058	9.94	.104	.104	2 H1
12	M12	SR 3/4	.144	0	3	.021	0		6 6.954	14.314	.179	.179	2 H1
13		0.625' Dia.	.194	0	3	.019	0		6 1.058	9.94	.104	.104	2H1
14	M14	SR 3/4	.158	0	3	.017	0		66.954	14.314	.179	.179	2 H1
15	M15	SR 3/4	.151	0	3	.018	0		6 6.954	14.314	.179	.179	1 H1
16	PS.2		.097	1	6	027	1.375		6 20.867	32.13	1.872	1.8	1 H1
17	PS.1		.311	5	4	.039	5.667		6 14.916	32.13	1.872	1.8	4 H1
18	M19		.195	4	3	.058	4.625	No.	6 20.867	32.13	1.872	1.8	1H1
19		PIPE 2.0	.113	1	6	.071	1.375		6 20.867	32.13	1.872	1.8	1H1







Member Code Checks Displayed (Enveloped) Envelope Only Solution

Centek Engineering	
TJL	
22017.06	

Portland HS Unity Check

Nov 9, 2023 at 8:57 AM Mount.R3D



Subject:

Connection to Host Structure

Centered on Solutions

P: (203) 488-0580 63-2 North Branford Road Branford, CT 06405

Location:

Portland, CT

Prepared by: T.J.L. Checked by: C.F.C.

(User Input)

Job No. 22017.06

# **Antenna Mount Connection:**

# Anchor Data:

Rev. 0: 5/11/23

A307 Threaded Rod =

Number of Anc hor Bolts = N := 4

(User Input) Diameter of Bolts= D := 0.625 in

T<sub>design</sub> := 10.4 kips (User Input) Design Tension =

V<sub>design</sub> := 6.23-kips (User Input) Design Shear =

Design Reactions:

(User Input) Fx= Fx:= 1.7-kips

Fy=  $F_V := 0.7 \cdot \text{kips}$ (User input)

F<sub>2</sub> := 2.8 kips (User Input) Fz=

Anchor Check:

 $T_{Max} := \frac{F_z}{N} = 700 \, lb$ Max Tension Force =

 $V_{\text{Max}} := \frac{F_y}{N} + \frac{F_x}{N} = 600 \text{lb}$ Max Shear Force =

Condition1 := if  $\frac{T_{Max}}{T_{design}} + \frac{V_{Max}}{V_{design}} \le 1.0, "OK", "NG"$ Condition 1 =

T<sub>design</sub> % of Capacity=



# NORTHEAST > North East > New England > Wallingford-1 > PORTLAND HS CT - B

Cheiban, Ziad - ziad.cheiban@verizonwireless.com - 20230927\_153155

Project Details		Location Information	
Carrier Aggregation N	Z	Site Id	Site Id 616480547
Ecip	Z	Search Ring#	
Project Name	Project Name PORTLAND HS CT	E-NodeB ID# null	llnu
Project Alt Name	Project Alt Name   PORTLAND HS CT	#SIC#	PSLC# 469381
Project Id	Project Id 16599668	Switch Name	Switch Name Wallingford-1
Designed Sector Carrier 4G   15	15	Tower Type	
Designed Sector Carrier 5G 3	3	Site Type MACRO	MACRO
Additional Sector Carrier 4G 0	0	Street Address 97 High Street	97 High Street
Additional Sector Carrier 5G 0	0	City	City Portland
Suffix	Suffix Rev4-2023-09-27	State CT	CT
FP Solution Type & Tech Type	FP Solution Type & Tech Type   MCR;4G_700;4G_850;4G_AWS;4G_CBRS;5 G_L-Sub6;4G_PCS	Zip Code 06480	06480
		County	County Middlesex
		Latitude	Latitude 41.58071/41°34'50.556"
		Longitude	Longitude -72.63136/72° 37' 52.896"

Project Scope					
Rev4-2023-09-27 Use RF4461d-13A low band RRH and 6413 C-Band MMU					

						Antenna	Antenna Summary					
Added Antenna	ntenna											
200	850	1900	AWS	CBRS	L-Sub6 Make	Make	Model	Center line	Tip Height	Azimuth	Install	Quantit
					56	Samsung	MT6413-77A	06	91.2	30(1),150(2),2 70(3)	PHYSICAL 3	8
LTE	LTE	LTE	LTE			COMMSCOPE	NNH4-65B-R6	06	93	30(1),150(2),2 70(3)	PHYSICAL 3	3
				LTE		Samsung	RT4423	06	90.4	30(19),150(20) ,270(21)	PHYSICAL 3	3

	Model	CBRS L-Sub6 Make	BRS L-Suf		AWS	1900 AWS
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	Quantit
	Install Type
	Azimuth
	Tip Height
	Center
	Model
	Make
	L-Sub6
	CBRS
	AWS
	1900
Antenna	850
Retained	002

emoved: 0		
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						Non	Non Antenna Summary			
Added Non Antenna	Antenna		75		-					
Equipment Type	Location	700	850	1900	AWS	CBRS	Make	Model	Install	Quantity
Hybrid Cable	Tower						Hybrid Cables	1-1/4" Hybrid Cables	PHYSICAL	24
OVP	Tower							12 OVP	PHYSICAL	-
RRU	Томег			LTE	LTE		Samsung	B2/B66A RRH ORAN (RF4439d-25A)	PHYSICAL	e
RRU	Tower					LTE	Samsung	RF4423-48B	PHYSICAL	8
RRU	Tower	띰	TE E				Samsung	RF4461d-13A	PHYSICAL	8

S Make	AWS	0061	850	200
14-1	Make	AWS CBRS Make	1900 AWS CBRS Make	850 1900 AWS CBRS Make

	850 1900 AVIS CBRS Make Model Install Quantity	
	850 1900 AWS	
na	lion 700	
etained Non Antenna	quipment Locatio	Cha

Removed: 0 Retaine	Removed:
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Services			
700 LTE		0002 (8118082)	
Sector	01	02	03
Azimuth	30	150	270
Cell/Enodob-id	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
Antenna Make	COMMSCOPE	COMMSCOPE	COMMSCOPE
Centerline	06	06	06
DLEARFON	5230	5230	5230
Mech Down-tilt	0	0	0
Elect Down-tilt	5	2	2
Tip Height	63	93	93
Regulatory Power	66.49 (W/MHz) ERP	66.49 (W/MHz) ERP	66.49 (W/MHz) ERP
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	RF4461d-13A	RF4461d-13A	RF4461d-13A
Number of Tx,Rx	4,4	4,4	4,4
Position			
Transmitter Id	11232662	11232663	11232664
Source	VZNPP	VZNPP	VZNPP
Bandwidth	10	10	10
Ant. Dimensions H x W x D(inch)	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79
Weight(ib)	81.82	81.82	81.82

Services			
850 LTE		0002 (8118082)	
Sector	10	02	03
Azimuth	30	150	270
Cell/Enodeb-Id	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
Antenna Make	COMMSCOPE	COMMSCOPE	COMMSCOPE
Centerline	06	06	06
DLEARFCN	2450	2450	2450
Mech Down-tilt	0	0	0
Elect Down-tilt.	2	2	2
Tip Height	93	93	93
Regulatory Power	301.17 (W/MHz)	301.17 (W/MHz)	301.17 (W/MHz)
			ENTOD
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	RF4461d-13A	RF4461d-13A	RF4461d-13A
Number of Tx,Rx	4 , 4	4,4	4.4
Position			
Transmitter id	11298595	11298596	11298597
Source	VZNPP	VZNPP	VZNPP
Bandwidth	10	10	10
Ant, Dimensions $H \times W \times D$ (inch)	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79
Weight(lb)	81.82	81.82	81.82

Services	•		
1900 LTE		0002 (8118082)	
Sector	01	02	03
Azimuth	30	150	270
Cell/Enodeb-Id	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
Antenna Make	COMMSCOPE	COMMSCOPE	COMMSCOPE
Centerline	06	06	06
DLEARFCN	1050	1050	1050
Mech Down-tilt	0	0	0
Elect Down-tilt	2	2	2
Tip Height	93	93	93
Regulatory Power	168.95 (W/MHz) EIRP	168.95 (W/MHz) EIRP	168.95 (W/MHz) EIRP
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
TMA Make			
TMA Model			
	Samsung	Samsung	Samsung
RRU Model	B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)
Number of Tx,Rx	4,4	4,4	4,4
Position			(4.78) E
Transmitter Id	11298592	11298593	11298594
Source	VZNPP	VZNPP	VZNPP
Bandwidth	10	10	10
Ant. Dimensions H x W x D(Inch)	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79	72.0 × 19.6 × 7.79
Weight(lb)	81.82	81.82	81.82

Services			
AWS LTE		0002 (8118082)	
Sector	01	02	03
Azimuth	30	150	270
Cell/Enodeb-ld	064040	064040	064040
Antenna Model	NNH4-65B-R6	NNH4-65B-R6	NNH4-65B-R6
Antenna Make	COMMSCOPE	COMMSCOPE	COMMSCOPE
Centerline	06	06	06
DLEARFON	2050	2050	2050
Mech Down-tilt	0	0	0
Elect Down-tilk	2	2	2
Tip Height	93	63	93
Regulatory Power	84.67 (W/MHz) EIRP	84.67 (W/MHz) EIRP	84.67 (W/MHz) EIRP
Cell Max Power	46.0 dBm	46.0 dBm	46.0 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)	B2/B66A RRH ORAN (RF4439d-25A)
Number of Tx,Rx	4 , 4	4,4	4 , 4
Position			
Transmitter Id	11298467	11298468	11298469
Source	VZNPP	VZNPP	VZNPP
Bandwidth	20	20	20
Ant. Dimensions $H \times W \times D(inch)$	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79	72.0 x 19.6 x 7.79
Weight(lb)	81.82	81.82	81.82

Services			
CBRS LTE		0002 (8118082)	
Sector	19	20	21
Azimuth	30	150	270
Cell/Enodeb-Id	064040	064040	064040
Antenna Model	RT4423	RT4423	RT4423
Antenna Make	Samsung	Samsung	Samsung
Centerline	06	06	06
DLEARFON	55343, 55541, 55739, 55937	55343, 55541, 55739, 55937	55343, 55541, 55739, 55937
Mech Down-tilt	0	0	0
Elect Down-tilt		7	2
Tip Height	90.4	90.4	90.4
Regulatory Power	3.76 (W/MHz) EIRPSD, 3.76 (W/MHz) EIRPSD, 3.76 (W/MHz)	3,76 (W/MHz) EIRPSD, 3,76 (W/MHz) EIRPSD, 3,76 (W/MHz)	3.76 (W/MHz) EIRPSD, 3.76 (W/MHz) EIRPSD, 3.76 (W/MHz)
Cell Max Power	37.02 dBm	37.02 dBm	37.02 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	RF4423-48B	RF4423-48B	RF4423-48B
Number of Tx,Rx	4,4	4,4	4,4
Position			
Transmitter Id	11298781	11298782	11298783
Source	VZNPP	VZNPP	VZNPP
Bandwidth	20, 20, 20, 20	20, 20, 20, 20	20, 20, 20, 20
Ant. Dimensions H x W x D(inch)	8.7 × 12.0 × 1.5	8.7 × 12.0 × 1.5	8.7 x 12.0 x 1.5
Weight(Ib)	3.3	3.3	3.3

Services			
CBAND NR		0002 (8118082)	
Sector	0001	0002	0003
Azimuth	30	150	270
Cell/Enodeb-Id	0640040	0640040	0640040
Antenna Modei	MT6413-77A	MT6413-77A	MT6413-77A
Antenna Make	Samsung	Samsung	Samsung
Centerline	06	06	06
DLEARFCN	650006, 655324	650006, 655324	650006, 655324
Mech Down-tilt	0	0	0
Elect Down-tilt		_	
Tip Height	91.2	91.2	91.2
Regulatory Power	743.34 (W/MHz) EIRP, 743.34 (W/MHz) EIRP	743.34 (W/MHz) EIRP, 743.34 (W/MHz) EIRP	743.34 (WIMHz) EIRP, 743.34 (WIMHz) EIRP
Cell Max Power	52.02 dBm	52.02 dBm	52.02 dBm
TMA Make			
TMA Model			
RRU Make	Samsung	Samsung	Samsung
RRU Model	MT6413-77A	MT6413-77A	MT6413-77A
Number of Tx,Rx	2,2	2,2	2,2
Position			
Transmitter.id	11298702	11298703	11298704
Source	VZNPP	VZNPP	VZNPP
Bandwidth	100, 60	100, 60	100, 60
Ant. Dimensions H x W x D(inch)	29.53 x 15.75 x 5.51	29.53 x 15.75 x 5.51	29.53 x 15.75 x 5.51
Weight(lb)	55.1	55.1	55.1

Calisigns Per Antenna	у Аптепна													2	-0.0	100			
Sector	Make	Model	Ant CL Height AG	Ant Tip Height	Azimuth	Elect Down-tilt	Mech Down-tilt	Gein	Bandwidth	Regulator 7 y Power	700 850		1900	2100	28 GHz	31 GHz	39 GHz	9-qns-1	CBRS
6003	Samsung	MT6413-77A	06	91.2	270		0	23,15	105	743,34								WRNE581,WR NE582,WRNE 583,WRNE58 4,WRNE585	
19	Samsung	RT4423	06	90.4	30	7	0	10.34		3.76									CBRS_CALLS
05	COMMSCOPE	NNH4-65B-R	06	93	150	2	0	11.94	69.75	66.49	WQJQ689								
	COMMSCOPE NNH4-65B-R 90	NNH4-65B-R	90	93	270	2	0			301.17	K	KNKA404							
0005	Samsung	MT6413-77A	06	91.2	150	-	0	23,15	105	743,34								WRNE581,WR NE582,WRNE 583,WRNE58 4,WRNE585	
0002	Samsung	MT6413-77A	06	91.2	150	_	0	23.15	105	743,34								WRNESES,WF NESB6,WRNE 587,WRNE58	
0001	Samsung	MT6413-77A	06	91.2	98	T**	0	23.15	105	743,34				ž				WRNE561,WR NE582,WRNE 583,WRNE58 4,WRNE585	
02	COMMSCOPE	COMMSCOPE NNH4-65B-R	06	93	150	2	0	12.54	65	301.17	Ÿ	KNKA404							
101	COMMSCOPE	COMMSCOPE NNH4-65B-R		93	30	2		12.54	92	301.17	Ž	KNKA404							
21	Samsung	RT4423	06	90.4	270	7	0	10.34	67	3,76									CBRS_CALLS IGN
0001	Samsung	MT6413-77A	06	91,2	30	_	o	23,15	105	743,34								WRNE585,WR NE586,V/RNE 587,WRNE58	
05	COMMSCOP	COMMSCOPE NNH4-65B-R	06	93	150	- 5	0	13.92	60.75	168,95			KNLH251,WP OJ730						
03	COMMSCOP	COMMSCOPENNH4-65B-R	06	83	270	2	0	13.92	60,75	168 95			KNLH251,WP 0J730			- 65			
03	COMMSCOP	COMMSCOPE NNH4-65B-R		93	270	2	0	11.94	69,75	66.49	WQJQ689								
10	COMMSCOP	COMMSCOPE NNH4-65B-R	06	93	30	2		11.94	69.75	66.49	WQJQ689								
20	Samsung	RT4423	08	90,4	150	2	0	10.34	67	3,76									CBRS_CALLS IGN
0003	Samsung	MT6413-77A	06	91.2	270	-	0	23.15	105	743.34								WRNE585,WF NE586,WRNE 587,WRNE58	
10	COMMSCOP	COMMSCOPE NNH4-65B-R	06	93	30	2	0	13.92	60,75	168.95			KNLH251,WP 0J730						
03	COMMSCOP	COMMSCOPE NNH4-65B-R	06	93	270	2	0	13,93	63.5	84.67				WQGA906,WQ GB276					
05	COMMSCOP	COMMSCOPE NNH4-65B-R	06	93	150	2	0	13.93	63.5	84.67				WQGA906,WQ GB276					
01	COMMSCOP	COMMSCOPE NNH4-65B-R	06	63	30	N	0	13.93	63.5	84.67				WQGA906,WQ GB276					

Approve for Insvc	-	-	-	L		+	-	-	+		-	
Action	pappe	pappa	pappa	added	added	added	pappe	pappe	poppe	pappe	added	pappe
Statue	proposed	proposed	proposed	proposed	proposed	proposed	proposed	proposed	proposed	proposed	proposed	proposed
POPs/8q.	444.75	444.75	444.75	444.75	444.75	444.75	444.75	444.75	444.75	444.75	444.75	444.75
Threshold (W)	1000	400	1640	1640		1640	1640	1640	1640	1640	1640	1640
Regulator y Power	96.49	301.17	168.95	168.95	3.76	84.67	743.34	743.34	743.34	743.34	743.34	84.67
Freq Range 4	776.000 - 787.000/. 000 -	869.000 - 880.000/8 90.000 - 891.500	1975.000 1980.000/ .000 -	1970.000 1975.000/ 000 000	4.	2110.000 2120.000/ .000 -	. 000.	. 000. 	- 000. - 000/.000 000	000,000	- 000 - 000,000 - 000	2120.000 2130.000/ .000 - .000
Freq Range 3	746.000 - 757.000/. 000 -	824,000 - 835,000/8 45,000 - 846,500	1995.000 1900.000/ ,000 -	1890.000 1895.000/ .000 -	4	1710.000 1720.000/ .000 -	3700,000 3720,000/ .000 -	3720,000 3740,000/ 000	3740.000 3760.000/ 000	3760.000 3780.000/ .000 -	3780.000 3800.000/ .000 .000	1720,000 1730,000/ ,000 -
Freq Range 2	776,000 - 787,000/- 000 - .000	869.000 - 880.000/8 90.000 - 891.500	1975.000 1980,000/ .000 -	1970.000 1975.000/ 000 000	UNLICENSE D UNLICENSE D/UNLICEN SED - UNLICENSE	2110.000 2120.000/ .000 -	.000. .000/000. .000.	- 000. - 000.000. - 000.	.000. .000/.000 .000.	000,000	- 000° - 000° - 000° -	2120,000 2130,000/ .000 -
Freq Range 1	746.000 - 757.000/. 000 -	824.000 - 835.000/8 45.000 - 846.500	1895,000 1900.000/ .000 -	1880.000 1895.000/ .000 -	UNLICENSE D UNLICENSE D/UNLICEN SED - UNLICENSE	1710,000 1720,000/ .000 -	3700.000 3720.000/ .000 -	3720.000 3740.000/ .000 -	3740.000 3760.000/ .000 -	3760.000 3780.000/ .000 -	3780.000 3800.000/ .000 -	1720.000 1730.000/ .000 - .000
Total MHZ	22.000	25.000	10.000	10.000	UNLICENSE	20.000	20.000	20.000	20.000	20.000	20.000	20.000
Wholly Owner	<b>∀</b>	Xes	× 0×	Yes	UNLICENSE	<b>\$8</b>	Yes	Yee	Yes	Yes	Yes	Yes
License	Celico Partnersh Ip	Cellco Partnersh Ip	Celico Partnersh Ip	Celico Partnersh Ip	UNLICENSE	Celico Partnersh Ip	Celico Partnersh ip	Cellco Partnersh Ip	Celico Partnersh Ip	Cellco Partnersh Ip	Cellco Partnersh Ip	Celico Partnersh Ip
County	8007	2005	8007	2006	UNLICENSE	8007	9007	2007	2002	9007	8007	2006
otrate •	CT	5	ст	10	5	5	L CI	t	t	5	5	<b>T</b>
Riock	U	ď	O	L	UNLICENSE	ď	1A	A2	EA .	44	A5	m
# # # # # # # # # # # # # # # # # # #	REA001	CMA032	BTA184	BTA184	UNLICENSE	CMA032	PEA001	PEA001	PEA001	PEA001	PEA001	BEA010
Code	n <sub>w</sub>	5	M.	CW	3.5 GHz	AW	S a	æ	Σ a	M	E.	w
Магкет	Northeast	Hartford- New Britain-B ristol, CT	Hartford, CT	Hartford, CT	UNLICENSE	Hartford- New Britain-B ristol, CT	New York,	New York, NY	New York, NY	New York, NY	New York,	New York-No. New JerLong Island, NY-NJ-CT- PA-MA-
Callsign	WQJQ689	KNKA404	WPOJ730	KNL H251	CBRS_CALL	WQGB276	WRNE581	WRNE582	WRNE583	WRNES84	WRNE585	WQGA906

# verizon

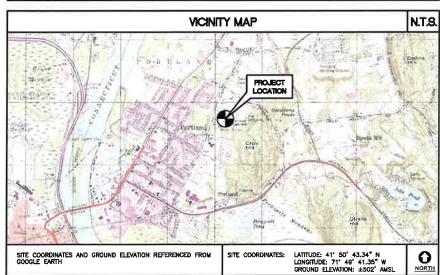
SITE NAME: PORTLAND HS CT SITE ID: 616480547 97 HIGH STREET PORTLAND, CT 06480

# GENERAL NOTES

- ALL WORK SHALL BE IN ACCORDANCE WITH THE 2021 INTERNATIONAL BUILDING CODE AS MODIFIED BY THE 2022 CONNECTICUT SUPPLEMENT, INCLUDING THE TA/EAR-222 REVISION "H" "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND SUPPORTING STRUCTURES." 2022 CONNECTICUT FIRE SAFETY CODE, NATIONAL ELECTRICAL CODE AND LOCAL CODES.
- SHOULD ANY FIELD CONDITIONS PRECLIDE COMPLIANCE WITH THE DRAWINGS, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ENGINEER AND SHALL NOT PROCEED WITH ANY AFFECTED WORK.
- CONTRACTOR SHALL REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUBCONTRACTORS AND ALL RELATED PARTIES. THE SUBCONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
- BEFORE BEGINNING THE WORK, THE CONTRACTOR IS RESPONSIBLE FOR MAKING SUCH INVESTIGATIONS CONCERNING PHYSICAL CONDITIONS (SURFACE AND SUBSURFACE) AT OR CONTIQUOUS TO THE SITE, WHICH MAY AFFECT PERFORMANCE AND COST OF THE WORK.
- ALL DIMENSIONS, ELEVATIONS, AND OTHER REFERENCES TO EXISTING STRUCTURES, SURFACE, AND SUBSURFACE CONDITIONS ARE APPROXIMATE. NO CUARANTEE IS MADE FOR THE ACCURACY OR COMPLETENCES OF THE INFORMATION SHOWN. THE CONTRACTOR SHALL VERHEY AND COORDINATE ALL DIMENSIONS, ELEVATIONS AND ANGLES WITH CUISTING CONDITIONS AND WITH ARCHITECTURAL AND SITE DRAWINGS BEFORE PROCEEDING WITH ANY WORK.
- AS THE WORK PROGRESSES, THE CONTRACTOR SHALL NOTIFY THE OWNER OF ANY CONDITIONS WHICH ARE IN CONFLICT OR OTHERWISE NOT CONSISTENT WITH THE CONSTRUCTION DOCUMENTS, AND SHALL NOT PROCEDS WITH SUCH WORK UNTIL THE CONFLICT IS SATISFACTORILY RESOLVED.
- CONTRACTOR SHALL PROVIDE A COMPLETE BUILD—OUT WITH ALL FINISHES, STRUCTURAL MECHANICAL, AND ELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON THE DRAWINGS OR IN THE WRITTEN SPECIFICATIONS.
- CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OVER THE WORK.
- CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION, PLUMBING, ELECTRICAL AND HYAC. PERMITS SHALL BE PAID FOR BY THE RESPECTIVE SUBCONTRACTORS
- CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS AND SPECIFICATIONS ON SITE AT ALL TIMES AND INSURE DISTRIBUTION OF NEW DRAWINGS TO SUBCONTRACTIORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE. ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. THE CONTRACTOR SHALL FURNISH AN 'AS-BUILT' SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
- LOCATION OF EQUIPMENT AND WORK SUPPLIED BY OTHERS THAT IS DIAGRAMMATICALLY INDICATED ON THE DRAWINGS, SHALL BE CETERMINED BY THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE LOCATIONS AND DIMENSIONS SUBJECT TO STRUCTURAL CONDITIONS AND WORK OF THE SUBCONTRACTORS.
- 3. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUB-CONTRACTORS FOR ANY CONDITION PER THE MANUFACTURER'S RECOMMENDATIONS.
  CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR
  CONSTRUCTION MANAGER.

- 14. DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
- ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUBCONTRACTORS FOR ANY CONDITION
- 17. ANY AND ALL ERRORS, DISCREPANCIES, AND 'MISSED' ITEMS ARE TO BE BROUGHT TO THE ATTENTION OF THE VERIZON WIRELESS CONSTRUCTION MANAGER DURING THE BIDDING PHOCESS BY THE CONTRACTOR. ALL THESE ITEMS ARE TO BE INCLUDED IN THE BID. NO 'EXTRA' WILL BE ALLOWED FOR MISSED ITEMS.
- CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE CONSTRUCTION MANAGER FOR REVIEW.
- COORDINATION, LAYOUT, FURNISHING AND INSTALLATION OF CONDUITS AND ALL APPURITEMANCES REQUIRED FOR PROPER INSTALLATION OF ELECTRICAL AND TELECOMMUNICATION SERVICE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR AND CONFIRMED WITH THE PROJECT MANAGER AND OWNER FRIDT TO THE COMMENCEMENT OF ANY
- 22. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
- 23. THE CONTRACTOR SHALL CONTACT 'CALL BEFORE YOU DIG' AT LEAST 48 HOURS PRIOR TO ANY EXCOVATIONS AT 1-800-922-4455. ALL UTILITIES SHALL BE IDENTIFIED AND CLEARLY MARKED. CONTRACTOR SHALL MAINTAIN AND PROTECT MARKED UTILITIES THROUGHOUT PROJECT COMPLETION.
- CONTRACTOR SHALL COMPLY WITH THE OWNER'S ENVIRONMENTAL ENGINEER ON ALL METHODS AND PROVISIONS FOR ALL EXCAVATION ACTIVITIES INCLUDING SOIL DISPOSAL ALL BACKFILL MATERIALS TO BE PROVIDED BY THE CONTRACTOR.
- 26. THE COUNTY/CITY/TOWN MUST BE NOTIFIED (2) WORKING DAYS PRIOR TO CONCEALMENT/BURRAL OF ANY SYSTEM OR MATERIAL THAT WILL PREVENT THE DIRECT INSPECTION OF MATERIALS, METHODS OR WORKMANSHIP, EXAMPLES OF THESE PROCESSES ARE BACKFILLING A GROUND RING OR TOWER FOUNDATION, POURING TOWER FOUNDATIONS, BURYING GROUND RODS, PLATES OR GRIDS, ETC. THE CONTRACTOR MAY PROCEDD WITH THE SCHEDILED PROCESS (2) WORKING DAYS AFTER PROVIDING NOTICE UNLESS NOTIFIED OTHERWISE BY THE COUNTY/CITY/TOWN.
- 27. PRIOR TO THE SUBMISSION OF BIDS, THE CONTRACTOR SHALL WS/T THE SITE TO FAMILURIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK ON BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS, ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF EXONEER ON RECORD, PRIOR TO THE COMMENCEMENT OF ANY WORK.





# PROJECT SUMMARY

THE PROPOSED SCOPE OF WORK CONSISTS OF A MODIFICATION TO THE EXISTING UNMANNED THE FCOMMUNICATIONS FACILITY INCLUDING THE FOLLOWING:

- 1. INSTALL (3) PROPOSED COMMSCOPE NNH4-658-R6 ANTENNAS
- 2. INSTALL (3) PROPOSED SAMSUNG MT8413-77A ANTENNAS WITH INTEGRATED RADIO
- 3. INSTALL (3) PROPOSED SAMSUNG RT4423 ANTENNAS WITH INTEGRATED RADIO
- 4. INSTALL (3) PROPOSED SAMSUNG B2/B66A RRH ORAN (RF4439d-25A) RADIOS
- 5. INSTALL (3) PROPOSED SAMSUNG B5/B13 RRH ORAN (RF4481d-13A) RADIOS
- 6. INSTALL (1) PROPOSED RAYCAP OVP 12
- 7. INSTALL (3) SECTOR FRAME ANTENNA MOUNTS, TYP. (1) PER SECTOR
- 9. INSTALL NEW EQUIPMENT PAD. STEEL EQUIPMENT CANOPY AND ASSOCIATED CABINETS
- 10. INSTALL NEW SMART METER (PDSG)
- 11. INSTALL ILC CABINET
- 12. INSTALL TELCO CABINET
- 13. INSTALL UNISTRUT FRAME TO ACCOMMODATE EQUIPMENT INSTALLATION

PRO	DJECT INFORMATION
SITE NAME:	PORTLAND HS CT
SITE ID:	616480547
SITE ADDRESS:	97 HIGH STREET PORTLAND, CT 08480
APPLICANT:	CELLCO PARTNERSHIP d.b.a. VERIZON WIRELESS 20 ALEXANDER DRIVE WALLINGFORD, CT 06492
CONTACT PERSON:	MICHAEL HUMPHREYS (CONSTRUCTION MANAGER) VERIZON WIRELESS (880) 580—8410
ENGINEER OF RECORD:	CENTEK ENGINEERING, INC. 83-2 NORTH BRANFORD ROAD BRANFORD, CT. 06405
	CARLO F. CENTORE, PE (203) 488-0580 EXT. 122
SITE COORDINATES:	LATITUDE: 41"-34"-50.83" LONGITUDE: 72"-37"-52.96" GROUND ELEVATION: 350'± A.M.S.L.
	COORDINATES AND GROUND ELEVATION ARE REFERENCED FROM GOOGLE EARTH SOFTWARE.

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N-1	SPECIFICATIONS, NOTES, AND ANT. SCHEDULE	1
C-1	COMPOUND, EQUIPMENT PLAN & ELEVATION	1
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C-3	SITE AND MISCELLANEOUS DETAILS	1
C-4	TYPICAL CONDUIT PENETRATION DETAILS	1
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E-4	TYPICAL ELECTRICAL DETAILS	1
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E-6	ELECTRICAL SPECIFICATIONS	1



488-0580 488-8587 Fax North Branford ord, CT 06405 (233) 4 (233) 4 63-2 No Branfo d/b/a Verizon Wireless

占 E NAME: PORTILAND HS C SITE ID: 616480547 97 HGH SIREET PORTLAND CT, 08480

뿛 11/02/23 SCALE: AS NOTED

SHEET

DATE:

# **NOTES AND SPECIFICATIONS:**

GOVERNING CODE: 2021 INTERNATIONAL BUILDING (IBC) AS MODIFIED BY THE 2022 CONNECTICUT STATE BUILDING CODE.

- 1. DESIGN CRITERIA:
- RISK CATEGORY II (BASED ON IBC TABLE 1604.5)
- NOMINAL DESIGN SPEED: 101 MPH (Void) (EXPOSURE B/ IMPORTANCE FACTOR 1.0 BASED ON ASCE 7-16).

# SITE NOTES

- THE CONTRACTOR SHALL CALL UTILITIES PRIOR TO THE START OF CONSTRUCTION.
- 2. ACTIVE EXISTING UTILITIES, WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES. THE ENGINEER SHALL BE NOTIFED IMMEDIATELY, PROOR TO PROCEEDING. SHOULD ANY UNCOVERED EXISTING UTILITY PRECLUDE COMPLETION OF THE WORK IN ACCORDANCE WITH THE CONTRACT
- THE AREAS OF THE COMPOUND DISTURBED BY THE WORK SHALL BE RETURNED TO THEIR ORIGINAL CONDITION.
- CONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION. EROSION OCHTROL MESAURES, SHALL BE IN CONTROLMANCE WITH THE LOCAL GUIDELINES FOR EROSION AND SEDIMENT CONTROL.
- IF ANY FIELD CONDITIONS EXIST WHICH PRECLIDE COMPLIANCE WITH THE DRAWINGS, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ENGINEER AND SHALL PROCEED WITH AFFECTED WORK AFTER CONFLICT IS SATISFACTORILY RESOLVED.

# GENERAL NOTES

- ALL WORK SHALL BE IN ACCORDANCE WITH THE 2021 INTERNATIONAL BUILDING CODE AS MODRIED BY THE 2022 CONNECTICUT SUPPLEMENT, INCLUDING THE TAYER—222 REVISION "H" "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND SUPPORTING STRUCTURES." 2022 CONNECTICUT FIRE SAFETY CODE, NATIONAL ELECTRICAL CODE AND LOCAL CODES.
- SHOULD ANY FIELD CONDITIONS PRECLUDE COMPLIANCE WITH THE DRAWINGS, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ENGINEER AND SHALL NOT PROCEED WITH ANY AFFECTED WORK.
- CONTRACTOR SHALL REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUBCONTRACTORS AND ALL RELATED PARTIES. THE SUBCONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THERE WORK.
- BEFORE BEGINNING THE WORK, THE CONTRACTOR IS RESPONSIBLE FOR MAKING SUCH INVESTIGATIONS CONCERNING PHYSICAL CONDITIONS (SURFACE AND SUBSURFACE) AT OR CONTIGUOUS TO THE SITE, WHICH MAY AFFECT PERFORMANCE AND COST OF THE WORK.
- ALL DIMENSIONS, ELEVATIONS, AND OTHER REFERENCES TO EXISTING STRUCTURES, SURFACE, AND SUBSURFACE CONDITIONS ARE APPROXIMATE. NO GUARANTEE IS MADE FOR THE ACCURACY OR COMPLETENESS OF THE INFORMATION SHOWN. THE CONTRACTOR SHALL VERIFY AND CORDINATE ALL DIMENSIONS, ELEVATIONS AND ANGLES WITH EXISTING CONDITIONS AND WITH ARCHITECTURAL AND SITE DEVANINGS BEFORE PROCEEDING WITH ANY
- AS THE WORK PROGRESSES, THE CONTRACTOR SHALL NOTIFY THE OWNER OF ANY CONDITIONS WHICH ARE IN CONFLICT OR OTHERWISE NOT CONSISTENT WITH THE CONSTRUCTION DOCUMENTS, AND SHALL NOT PROCEED WITH SUCH WORK UNTIL THE CONFLICT IS SATISFACTORILY RESOLVED.
- CONTRACTOR SHALL PROVIDE A COMPLETE BUILD—OUT WITH ALL FINISHES, STRUCTURAL, MECHANICAL, AND DELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR RIDICATED ON THE DRAWMINGS OR IN THE WRITTEN SPECIFICATIONS.
- CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OWER THE WORK.
- CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION, PLIMBING, ELECTRICAL, AND HVAC. PERMITS SHALL BE PAID FOR BY THE RESPECTIVE SUBCONTRACTORS.
- 10. CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS AND SPECIFICATIONS ON SITE AT ALL TIMES AND INSURE DISTRIBUTION OF NEW DRAWINGS TO SUBCONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE, ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. THE CONTRACTOR
- LOCATION OF EQUIPMENT AND WORK SUPPLIED BY OTHERS THAT IS DIAGRAMMATICALLY INDICATED ON THE DRAWNOS, SHALL BE DETERMINED BY THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE LOCATIONS AND DIMENSIONS SUBJECT TO STRUCTURAL CONDITIONS AND WORK OF THE SUBCONTRACTORS.
- 12. THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE AND TO ENSURE THE SAFETY OF THE ENSTRUC STRUCTLIRES AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLIDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY.
- 13. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUB-CONTRACTORS FOR ANY CONDITION PER THE MANUFACTURER'S RECOMMENDATIONS. CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR CONSTRUCTION MANAGER.

- 14. DRAWINGS INDICALE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATOR SEARCH ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL DECEUTE THE WORK CORRECTLY IN ACCIDIONACE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
- ALL UTILITY WORK SHALL BE IN ACCORDANCE WITH LOCAL UTILITY COMPANY REQUIREMENTS AND SPECIFICATIONS.
- 18. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUBCONTRACTORS FOR ANY CONDITION PER MANUFACTURER'S RECOMMENDATIONS. CONTRACTOR TO SUPPLY THESE TIEMS AT NO COST TO OWNER OR CONSTRUCTION MANAGER.
- 17. ANY AND ALL ERRORS, DISCREPANCIES, AND 'MISSED' ITEMS ARE TO BE BROUGHT TO THE ATTENTION OF THE VERIZON WIRELESS CONSTRUCTION MANAGER DURING THE BIDDING PROCESS BY THE CONTRACTOR. ALL THESE TREMS ARE TO BE INCLUDED IN THE BID. NO 'EXTRA' WILL BE ALLOWED FOR MISSED ITEMS.
- 18. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON-SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
- CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL DRAWINGS MUST BEAR THE CHECKEY'S INITIALS BEFORE SUBMITTING TO THE CONSTRUCTION MANAGER FOR REVIEW.
- 20. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA.
- 21. COORDINATION, LAYOUT, FURNISHING AND INSTALLATION OF CONDUITS AND ALL APPURTENANCES REQUIRED FOR PROPER INSTALLATION OF ELECTRICAL AND TELECOMMUNICATION SERVICE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR AND CONFIRMED WITH THE PROJECT MANAGER AND OWNER PRIOR TO THE COMMENCEMENT OF THE COMMENCE
- 22. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIMBLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
- 23. THE CONTRACTOR SHALL CONTACT 'CALL BEFORE YOU DIG' AT LEAST 48 HOURS PRIOR TO ANY EXCAVATIONS AT 1-800-922-4455. ALL UTILITIES SHALL BE IDENTIFIED AND CLEARLY MARKED. CONTRACTOR SHALL MAINTAIN AND PROTECT MARKED UTILITIES THROUGHOUT PROJECT COMPLETION.
- CONTRACTOR SHALL COMPLY WITH THE OWNER'S ENVIRONMENTAL ENGINEER ON ALL METHODS AND PROVISIONS FOR ALL EXCAVATION ACTIVITIES INCLIDING SOIL DISPOSAL. ALL BECKFILL MATERIALS TO BE PROVIDED BY THE CONTRACTOR.
- THE COUNTY/CITY/TOWN MAY MAKE PERIODIC FIELD INSPECTIONS TO ENSURE COMPLIANCE WITH THE DESIGN PLANS, SPECIFICATIONS, AND CONTRACT DOCUMENTS.
- 25. THE COUNTY/CITY/TOWN MUST BE NOTIFIED (2) WORKING DAYS PRIOR TO CONCEALMENT/BURNL OF ANY SYSTEM OR MATERIAL THAT WILL PREVENT THE DIRECT INSPECTION OF MATERIAL, METHODS OR WORKMANSHIP, EXAMPLES OF THESE PROCESSES ARE BICKFILLING A GROUND RING OR TOWER FOUNDATIONS, BURNING GROUND RODS, PLATES OR GROUS, ETC. THE CONTRACTOR MAY PROCEED WITH THE SCHEDULED PROCESS (2) WORKING DAYS AFTER PROVIDING NOTICE UNLESS NOTIFIED OTHERWISE BY THE COUNTY/CITY/TOWN.
- 27. PRIOR TO THE SUBMISSION OF BIDS, THE CONTRACTOR SHALL VISIT THE SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWNOS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF ENGINEER ON RECORD, PRIOR TO THE COMMENCIBILITY OF ANY WORK.

# STRUCTURAL STEEL

- 1. ALL STRUCTURAL STEEL IS DESIGNED BY ALLOWABLE STRESS DESIGN (ASD)
- STRUCTURAL STEEL (W SHAPES)---ASTM A992 (FY = 50 KSI)
  STRUCTURAL STEEL (OTHER SHAPES)---ASTM A36 (FY = 36 KSI)
  STRUCTURAL HSS (RECTANGULAR SHAPES)---ASTM A500 GRADE B,
- STRUCTURAL HSS (ROUND SHAPES)---ASTM A500 GRADE B,
- STRUCTURAL HSS (ROUND SHAPES)——
  = 42 INSI)
  PIPE——ASTM A53 (FY = 35 KS)
  CONNECTION BOLTS——ASTM A325—N
  U—BOLTS——ASTM A36 F 1554
  ANCHOR RODS——ASTM F 1554
  WELDING ELECTRODE——ASTM E 70XX
- CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE ENGINEER FOR REVIEW. SHOP DRAWINGS SHALL INCLIDE THE FOLLDWING: SECTION PROFILES, SIZES, CONNECTION ATTACHMENTS, REINFORCING, ANCHORAGE, SIZE AND TYPE OF FASTENERS AND ACCESSORIES. INCLIDE EXECTION DRAWINGS, ELEXATIONS AND DETAILS.
- STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH THE LATEST PROVISIONS OF AISC MANUAL OF STEEL CONSTRUCTION.
- 4. PROVIDE ALL PLATES, CLIP ANGLES, CLOSURE PIECES, STRAP ANCHORS, MISCELLANEOUS PIECES AND HOLES REQUIRED TO COMPLETE THE STRUCTURE.
- 5. FIT AND SHOP ASSEMBLE FABRICATIONS IN THE LARGEST PRACTICAL SECTIONS FOR DELINERY TO SITE
- INSTALL FABRICATIONS PLUMB AND LEVEL, ACCURATELY FITTED, AND FREE FROM DISTORTIONS OR DEFECTS.
- AFTER ERECTION OF STRUCTURES, TOUCHUP ALL WELDS, ABRASIONS AND NON-GALVANIZED SURFACES WITH A 95% ORGANIC ZINC RICH PAINT IN ACCORDANCE WITH ASTM 780.
- ALL STEEL MATERIAL (EXPOSED TO WEATHER) SHALL BE CALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT DIPPED GALVANIZED) COATHINS" ON IRONS AND STEEL PRODUCTS.
- ALL BOLTS, ANCHORS AND MISCELLANDOUS HARDWARE SHALL BE CALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC COATING (HOT-DIP) ON IRON AND STEEL HARDWARE".
- THE ENGINEER SHALL BE NOTIFIED OF ANY INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISETTING OR NON CONFORMING MATERIALS OR CONDITIONS TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE ENGINEER REVIEW.
- 11. CONNECTION ANGLES SHALL HAVE A MINIMUM THICKNESS OF 1/4 INCHES.
- STRUCTURAL CONNECTION BOLTS SHALL CONFORM TO ASTM A325. ALL BOLTS SHALL BE 3/4" DUMBETER MINIMUM AND SHALL HAVE A MINIMUM OF TWO BOLTS, UNLESS OTHERWE ON THE DRAWNICS.
- 13. LOCK WASHER ARE NOT PERMITTED FOR A325 STEEL ASSEMBLIES.
- 14. SHOP CONNECTIONS SHALL BE WELDED OR HIGH STRENGTH BOLTED.
- 15. MILL BEARING ENDS OF COLUMNS, STIFFENERS, AND OTHER BEARING SURFACES TO TRANSFER LOAD OVER ENTIRE CROSS SECTION.
- 16. FABRICATE BEAMS WITH MILL CAMBER UP.
- 17. LEVEL AND PLUMB INDMIDUAL MEMBERS OF THE STRUCTURE TO AN ACCURACY OF 1:500, BUT NOT TO EXCEED 1/4" IN THE FULL HEIGHT OF THE COLUMN.
- 18. COMMENCEMENT OF STRUCTURAL STEEL WORK WITHOUT NOTIFYING THE ENGINEER OF ANY DISCREPANCES WILL BE CONSIDERED ACCEPTANCE OF PRECEDING WORK.
- INSPECTION AND TESTING OF ALL WELDING AND HIGH STRENGTH BOLTING SHALL BE PERFORMED BY AN INDEPENDENT TESTING LABORATORY.
- FOUR COPIES OF ALL INSPECTION TEST REPORTS SHALL BE SUBMITTED TO THE ENGINEER WITHIN TEN (10) WORKING DAYS OF THE DATE OF INSPECTION.

			ANT	ENNA	/AP	PURTENANCE SCHEDULE	
SECTOR	EXISTING/PROPOSED	ANTENNA (QTY)	SIZE (INCHES) (L x W x D)	ANTENNA & HEIGHT	AZIMUTH	(E/P) RRU (QTY)	(E/P) CABLES (QTY)
. A1	PROPOSED	SAMSUNG: RT4423	12.0 x 8.7 x 1.5	90'	30"	(P) SAMSUNG CBRS RRH-RT4423-488 (1), (P) OVP 12 (1)	
A2	PROPOSED	COMMSCOPE: NNH4-658-R6	71.9 x 19.6 x 7.7	90'	30"	(P) SAMSUNG 85/B13 RRH ORAN (RF4461d-13A) (1), (P) SAMSUNG B2/B66A RRH ORAN (RF4439d-25A) (1)	
A3	PROPOSED	SAMSUNG: MT8413-77A	28.9 x 15.75 x 5.5	90"	30		
B1	PROPOSED	SAMSUNG: RT4423	12.0 x 8.7 x 1.5	90'	150°	(P) SAMSUNG CBRS RRH-RT4423-48B (1)	(P) 8x12 HYBRIFLEX (2)
82	PROPOSED	COMMSCOPE: NNH4-65B-R6	71.9 x 19.6 x 7.7	90'	150°	(P) SAMSUNG BD/B13 RRH ORAN (RF4461d-13A) (1), (P) SAMSUNG B2/B66A RRH ORAN (RF4439d-25A) (1)	(1) 0212 11101111 (2)
B3	PROPOSED	SAMSUNG: MT6413-77A	28.9 x 15.75 x 5.5	80'	150		
C1	PROPOSED	SAMSUNG: RT4423	12.0 x 8.7 x 1.5	80'	270"	(P) SAMSUNG CBRS RRH-RT4423-488 (1)	
C2	PROPOSED	COMMSCOPE: NNH4-65B-R6	71.9 x 19.6 x 7.7	90'	270	(P) SAMSUNG B5/B13 RRH ORAN (RF4461d-13A) (1), (P) SAMSUNG B2/B66A RRH ORAN (RF4436d-25A) (1)	
C3	PROPOSED	SAMSUNG: MT8413-77A	28.9 x 15.75 x 5.5	90'	270°		

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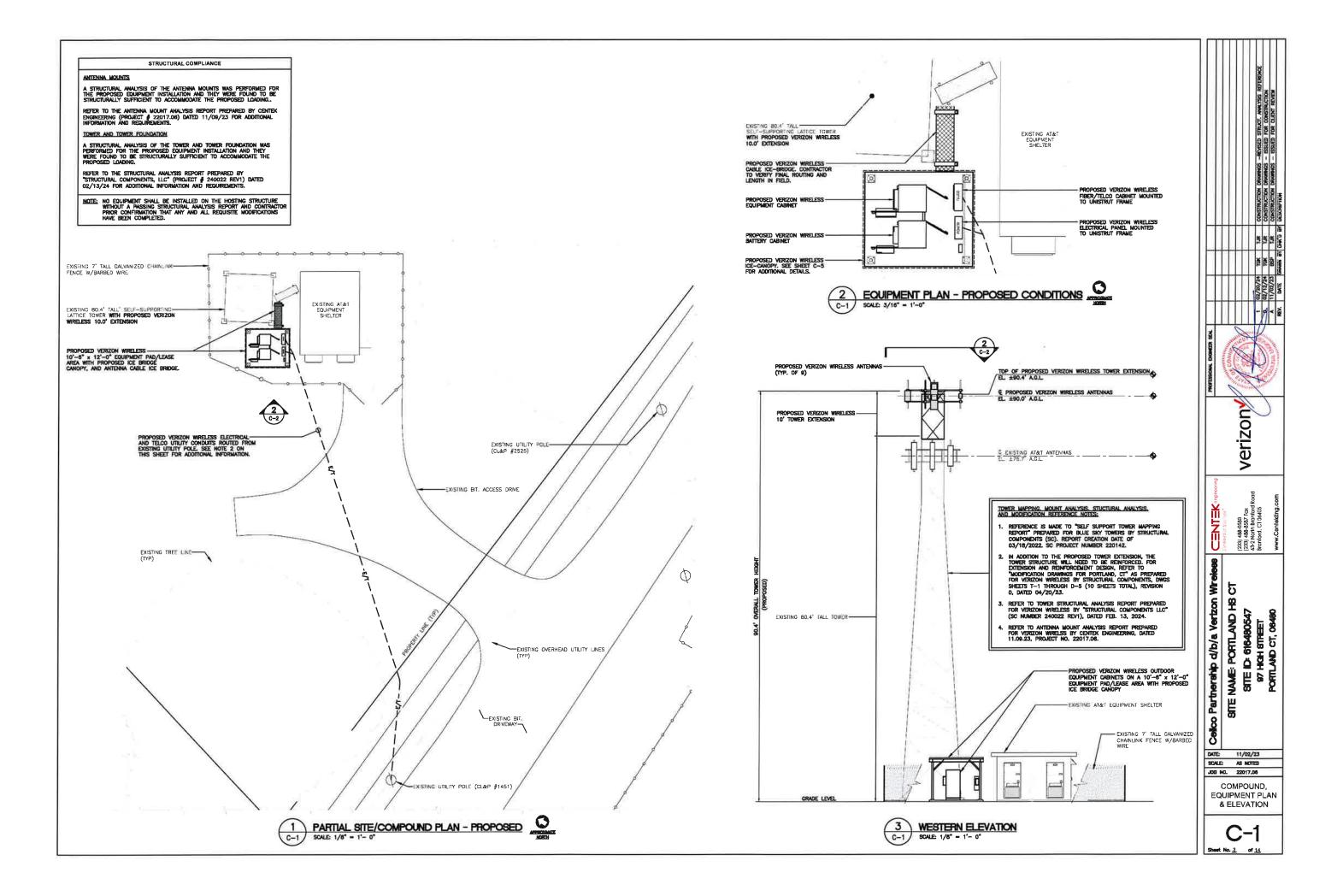
o d/b/a Vertzon Wirele PORTILAND HS CT B PORTILAND HE ID: 616480547 HICH STREET LAND CT, 08480 NAME: SITE IE 97 H 腸

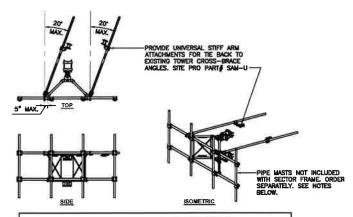
Partnership

8 DATE: 11/02/23 SCALE: AS NOTED JOB NO. 22017.06

SPECIFICATIONS. NOTES AND ANT. SCHEDULE





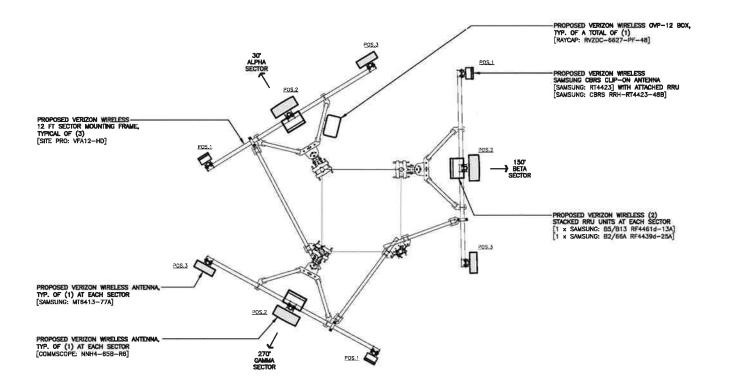


1	12	FT ANTENNA SECTOR MOI	UNTING FRA	ME
E	QUIPMENT	DESCRIPTION	QTY	WEIGHT
	WE: SITE PRO DOEL: VFA12—HD	12 FT, HEAVY DUTY V-FRAME	3	735 LBS

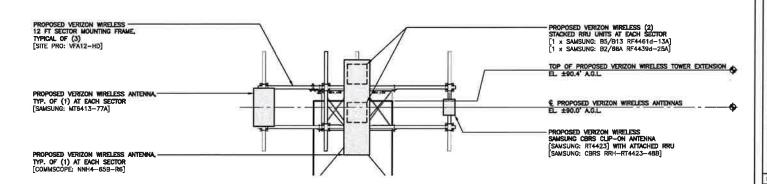
# NOTES:

- 1. GUYED AND SST MOUNTING RANGE: 1  $1/2^\circ$  TO 9  $1/2^\circ$  ROUND LEGS AND 3° TO 6° ANGLES.
- PIPE MASTS ARE NOT INCLUDED IN SECTOR FRAME KIT. ORDER SEPARATELY (SITE PRO PART# P30120). WEIGHT LISTED ABOVE DOES NOT INCLUDE PIPE MASTS











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			1	02/12/24	Ĕ	778	CONSTRUCTION DRAWINGS - ISSUED FOR CONSTRUCTION
	)	A BOTH BY	<	11/02/23		1.50	CONSTRUCTION DRAWINGS - ISSUED FOR CLIENT REVEN
W.Colliekerig.com		Carried and Carried Control	ÆV.	DATE	DRAWN BY	CHK'D BY	REV. DATE INNAME BIT CHAT BY DESCRIPTION

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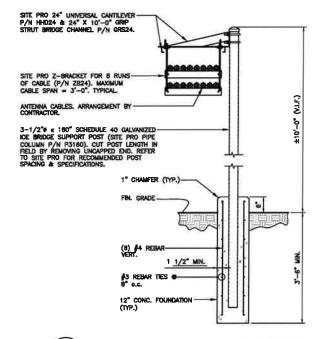
SITE NAME: PORTILAND HS CT | 1202 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1203 | 1

DATE: 11/02/23 SCALE: AS NOTED

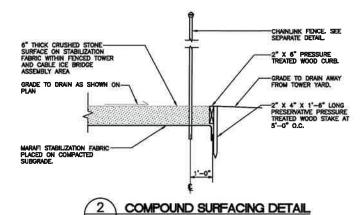
JOB NO. 22017.06 ANTENNA CONFIGURATION PLAN, ELEVATION

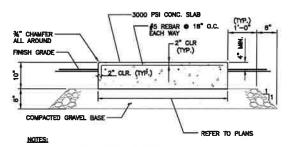
C-2

AND DETAIL



1 ANTENNA CABLE ICE BRIDGE DETAIL
C-3 SOLE: NOT TO SOLE





1. TOP OF CONC. PAD TOLERANCE IS 1/4"±.

2. PROVIDE PVC SLEEVES FOR UTILITY CONDUIT PASSAGE THROUGH PAD OR CAST CONDUITS IN PLACE AS APPLICABLE COORDINATE SLEEVE/CONDUIT LOCATIONS WITH CONSTRUCTION MANAGET.

3. REFER TO NOTES ON SHEET N-1 FOR ADDITIONAL REQUIREMENTS.

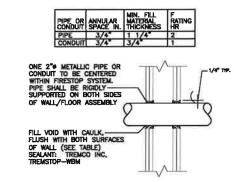
 COORDINATE EQUIPMENT CABINET AND PROPANE TANK HOLD—DOWN HARDWARE WITH RESPECTIVE MANUFACTURERS.



verizon (203) 488-0580 (203) 488-8587 Fax 63-2 North Branford R Branford, CT 06405 www.CentekEng.cc SITE NAME: PORTILAND HS CT
STRE ID: 616480547
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WWW DATE: 11/02/23 SCALE: AS NOTED JOB NO. 22017.08 SITE AND

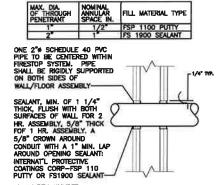
MISCELLANEOUS DETAILS

C-3



UL SYSTEM NUMBER: WL1051 F RATING - 1 & 2 HR.

# 1 DETAIL IN GYPSUM WALLBOARD SCALE: NOT TO SCALE



UL SYSTEM NUMBER: WL2038 F RATING - 1 & 2 HR.

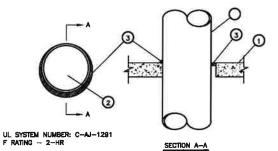
PVC CONDUIT PENETRATION

DETAIL IN GYPSUM WALLBOARD

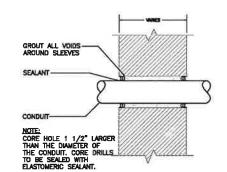
SCALE: NOT TO SCALE

# NOTE:

- FLOOR OR WALL ASSEMBLY MIN 2-1/2 IN. THICK REINFORCED LIGHTWEIGHT OR NORMAL WEIGHT (100-150 PCF) CONCRETE. WALL MAY ALSO BE CONSTRUCTED OF ANY UL CLASSIFIED CONCRETE BLOCKS\*. MAX DUM OF OPENING IS 30-7/8 IN. SEE CONCRETE BLOCKS (CAZT) CATEGORY IN THE FIRE RESISTANCE DIRECTORY FOR NAMES OF MANUFACTURERS.
- A STEEL FLOOR UNIT/FLOOR ASSEMBLY (NOT SHOWN) AS AN ALTERNATE TO ITEM 1, THE FLOOR ASSEMBLY MAY CONSIST OF A FLUTED STEEL FLOOR UNIT/ CONCRETE FLOOR ASSEMBLY. THE FLOOR ASSEMBLY SHALL BE CONSTRUCTED OF THE MATERIALS AND IN THE MANNER DESCRIBED IN THE INDIVIDUAL FLOOR CEILING DESIGN IN THE FIRE RESISTANCE DIRECTORY AND SHALL INCLUDE THE FOLLOWING CONSTRUCTION FEATURES:
- B. CONCRETE MIN 2-1/2 IN. THICK REINFORCED LIGHTWEIGHT ON NORMAL WEIGHT (100-150 PCF) CONCRETE, AS MEASURED FROM THE TOP PLANE OF THE FLOOR UNITS.
- C. STEEL FLOOR AND FORM UNITS\* COMPOSITE OR NON-COMPOSITE 1-1/2 TO 3 IN. DEEP FLUTED GALV STEEL UNITS AS SPECIFIED IN THE INDMIDUAL FLOOR-CEILING DESIGN. MAX DIAM OF OPENING IS 30-7/8 IN.
- THROUGH-PENETRANT ONE METALLIC PIPE OR CONDUIT TO BE INSTALLED EITHER
  CONCENTRICALLY OR ECCENTRICALLY WITHIN THE RIRESTOP SYSTEM. THE ANNULAR
  SPACE BETWEEN PIPE OR CONDUIT AND PERIPHERY OF OPENING SHALL BE MIN 0 IN.
  TO MAY 1/8 III. PIPE OR CONDUIT TO BE RIGIDLY SUPPORTED ON BOTH SIDES OF
  FLOOR OR WALL ASSEMBLY. THE FOLLOWING TYPES AND SIZES OF METALLIC PIPES OR
  CONDUITS MAY BE USED:
- A. STEEL PIPE NOM 30 IN. DIAM (OR SMALLER) SCHEDULE 10 (OR HEAVIER) STEEL PIPE.
- B. IRON PIPE NOM 30 IN. DIAM (OR SMALLER) CAST OR DUCTILE IRON PIPE.
- C. COPPER PIPE NOM 6 IN. DIAM (OR SMALLER) REGULAR (OR HEAVIER) COPPER PIPE.
- D. COPPER TUBING NOM 6 IN. DIAM (OR SMALLER) TYPE L (OR HEAVIER) COPPER TUBING.
- E. CONDUIT NOM 8 IN. DIAM (OR SMALLER) STEEL CONDUIT.
- F. CONDUIT NOM 4 IN. DIAM (OR SMALLER) STEEL ELECTRICAL METALLIC TUBING (EMT).
- 3. FILL, VOID OR CAVITY MATERIAL\* SEALANT MIN 1/2 IN. THICKNESS OF FILL MATERIAL APPLIED WITHIN THE ANNULUS, FLUSH WITH TOP SURFACE OF FLOOR OR WITH BOTH SURFACES OF WALL AT THE POINT CONTACT LOCATION BETWEEN PIPE AND CONCRETE, A MIN 1/4 IN. DIAM BEAD OF FILL MATERIAL SHALL BE APPLIED AT THE CONCRETE/PIPE INTERFACE ON THE TOP SURFACE OF FLOOR AND ON BOTH SURFACES OF WALL

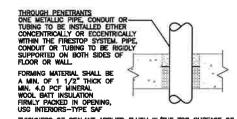


METAL PIPE THROUGH CONCRETE FLOOR/ WALL OR BLOCK WALL SCALE: NOT TO SCALE



4 DETAIL IN NON-RATED PARTITION
SCALE: NOT TO SCALE

FLOOR OR WALL	MIN. THICK.	縱	MIN. ANNULAR SPACE	MAX ANNULAR SPACE	MIN. FILL MAT. THICK.	MIN. FORM. MAT. THICK.	FATING
F	3 3/4"	1 1/2"	3/8"	2 1/8"	1"	2 3/4	2
F	3 3/4	6"	3/8"	3/4	11"	2 3/4"	2
F	3 3/4"	6"	3/8*	1	2"	1 3/4"	2
F	4 1/2	1 1/2	3/8"	2 1/8	11"	13 1/2	3
F	4 1/2"	6	378*	3/4	1"	13 1/2"	3
F	4 1/2"	6*	3/8"	1*	2*	2 1/2	3
W	5 1/2	1 1/2	3/8*	2 1/8	11"	3 1/2	3
W	5 1/2	6	3/8*	3/4	1"	3 1/2	3
W	6 1/2	1 1/2	3/8"	2 1/8	2"	2 1/2	3
W	6 1/2	6"	3/8"	11	2	2 1/2	3



THICKNESS OF SEALANT APPLIED FLUSH W/THE TOP SURFACE OF BOTH SIDES OF FLOOR/WALL (SEE TABLE), USG INTERIORS—TYPE SS

UL SYSTEM NUMBER: CAJ1020

PIPE AND CONDUIT PENETRATION

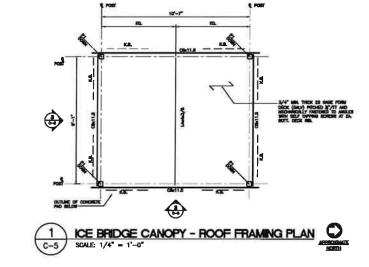
DETAIL IN CONCRETE OR MASONRY

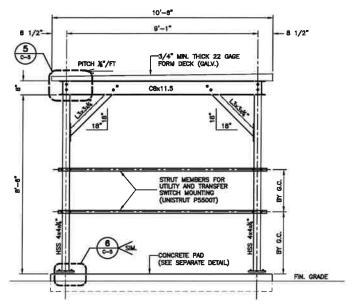
SCALE: NOT TO SCALE

C-4

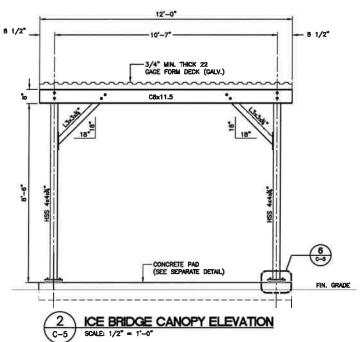
# PLAN NOTES AND LEGEND

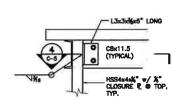
- VERIFY ALL DIMENSIONS, ELEVATIONS, EXISTING FRAMING MEMBER SIZES AND GENERA CONDITIONS PRIOR TO COMMENCEMENT OF WORK, NOTIFY ENGINEER OF RECORD ANY DISCREPANCES BETWEEN THESE DRAWNISS AND EXISTING CONDITIONS.
- (F<sub>p</sub> = 48km) STEEL POST.
- INDICATES SPAN DIRECTION.
- K.B. INDICATES L3x3x1/4 ASTM A38 (Fy=36 KSI) STEEL ANGLE





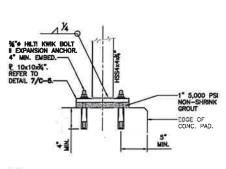




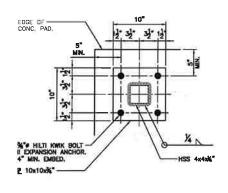


4 CANOPY FRAME CONNECTION SCALE: 1-1/2" = 1'-0"

5 CANOPY FRAME CONNECTION
SCALE 1-1/2" = 1'-0"

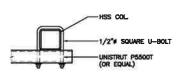


6 CANOPY POST CONNECTION
SCALE: 1-1/2" = 1'-0"



7 CANOPY POST BASE PLATE

C-5 SOALE: 1-1/2" = 1'-0"



8 STRUT TO COL. CONN. DETAIL (TYP)
C-5 SCALE: 1-1/2" = 1'-0"

3.5	-	
18° 18°		verizon
DETAIL)  FIN. GRADE	OHATIK organocing	Centerator Styrow- (203) 488-0580 (203) 488-4587 Fax 63-2 North Branford Road Branford, CT 04405
ELEVATION S COL	Celco Partnership d/b/a Verizon Wireless	SITE NAME: PORTILAND HS CT SITE ID: 616480547 97 HGH SITEET
Z'# SQUARE U-BOLT	DATE:	11/02/23
STRUT P5500T	JOB I	
IN. DETAIL (TYP)	E0 BF	QUIPMENT ICE RIDGE CANOPY AN AND DETAIL



MT6413-77A

ANTENNA		
EQUIPMENT	DIMENSIONS	
MAKE: SAMSUNG MODEL: MT8413-77A	28.90°H x 15.75°₩ x 5.51°D	

- 2. ANTENNA HAS ITS OWN BUILT-IN RRU.





RRH ONLY



4	ALL-IN-ONE ANTENNA
	ALL-IN-UNE AN I ENNA

CBR	S CLIP-ON ANTENNA	72		REM	OTE RADIO UNIT (RRU)
EQUIPMENT	DIMENSIONS	WEIGHT		EQUIPMENT	DIMENSIONS
MAKE: SAMSUNG MODEL: RT4423	12"H x 6.7"W x 1.5"D	3.3 LBS.	MAKE:	SAMSUNG	11.8°H x 8.7°W x 4.2°D
NOTES:					

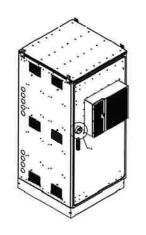
- THE CONTRACTOR IS RESPONSIBLE TO COORDINATE AND CONFIRM
  FINAL EQUIPMENT MAKE/MODEL AND QUANTITY SELECTION WITH
  VERIZON WIRELESS CONSTRUCTION MANAGER PRIOR TO ORDERING.

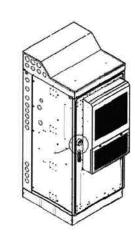
15.43 LBS.

3. DIMENSIONS AND WEIGHT SHOWN ARE FOR THE RRU ONLY.









	SIDE-BY-SIDE ANTENNA MOUNTING KIT		
	EQUIPMENT	DIMENSIONS	WEIGHT
IAKE: IODEL:	COMMSCOPE CMC74-36E	80"H x 36"W x 43"D	455 LBS.
IAKE: IODEL:	COMMSCOPE CMC74-368	80"H x 36"W x 43"D	846 LBS.

3 PROPOSED EQUIPMENT CABINET DETAIL
C-6 SCALE NOT TO SCALE





ELEVATION - FRONT

BOTTOM

12-PORT SECTOR ANTENNA		
EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: COMMSCOPE MODEL: NRH4-858-R8	72"L x 19.6"W x 7.7"D	BJ.1 LBS. (W/OUT MOUNT KIT)





DUAL BAND RRU (REMOTE RADIO UNIT)				
EQUIPMENT	BANDS	DIMENSIONS	WEIGHT	
MAKE: SAMSUNG MODEL: RF4439d-25A	B2: PCS (1900 MHz) B66: AWS (2100 MHz)	15.0"H x 15.0"W x 10.0"D	74.7 LBS.	
NOTES:  1. CONTRACTOR TO COORDINATE FINAL EQUIPMENT MODEL SELECTION WITH VERIZON WIRELESS CONSTRUCTION MANAGER PRIOR TO ORDERING.				

RRH - ISOMETRIC

5 DUAL-BAND AWS/PCS MACRO RADIO UNIT DETAIL

SCALE NOT TO SCALE



RRH - ISOMETRIC

RRH CLEARANCES

	T PROPERTY 1	WEALE
EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: SAMSUNG MODEL: RF4418d-13A	14.96"H x 14.96"W x 10.23"D	79.1 LB
NOTES:		

6 DUAL-BAND 700/850 MHZ MACRO RADIO UNIT DETAIL
SCALE: NOT TO SCALE

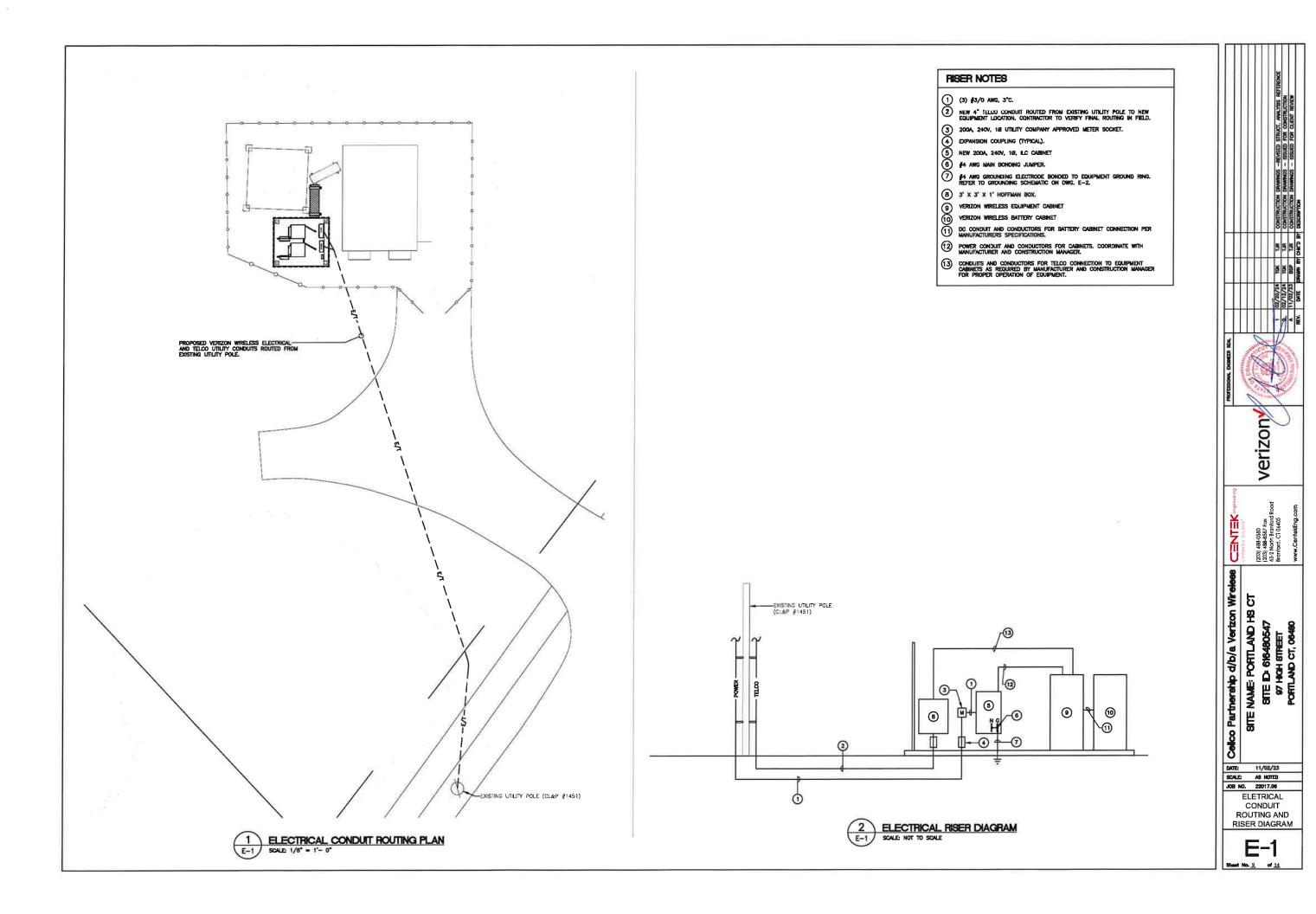
SITE NAME: PORTILAND HS CT (2005)
SITE NAME: PORTILAND HS CT (2005)
SITE ID: 616480547 (2005)
SI DATE: 11/02/23 SCALE: AS NOTED JOB NO. 22017.06

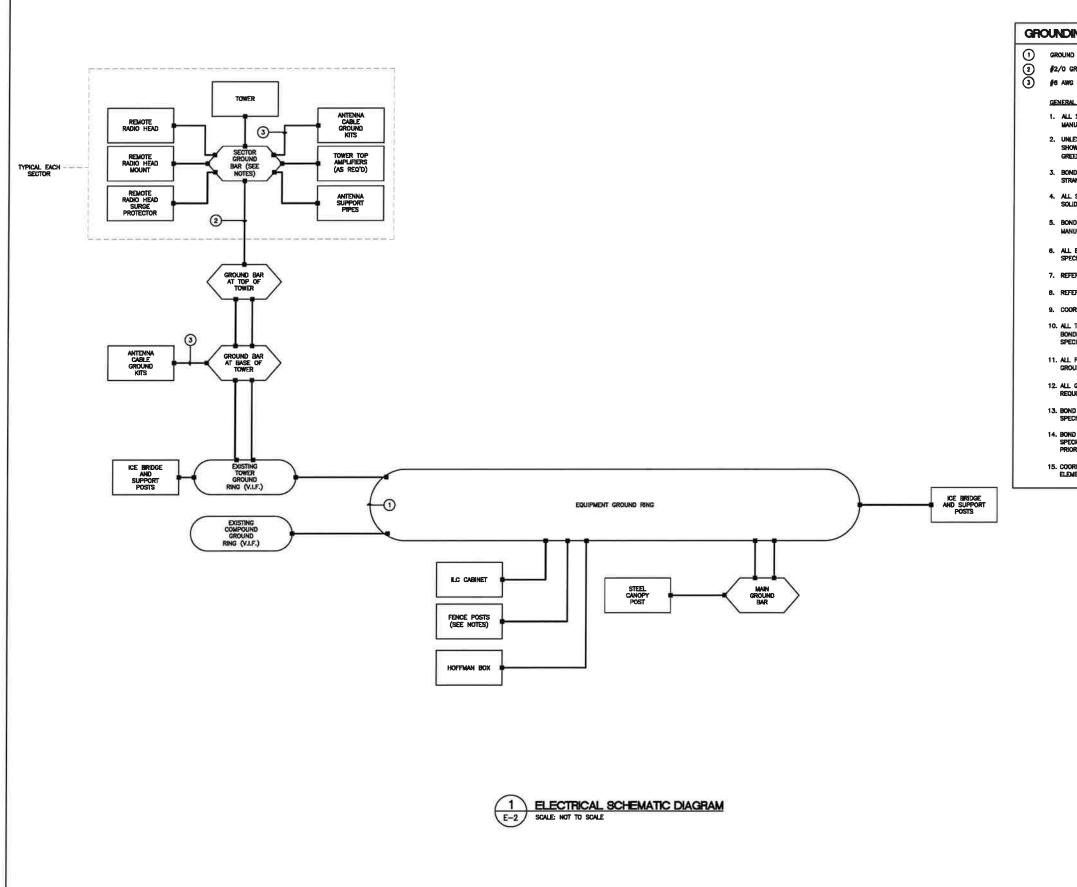
RF DETAILS

verizon

(203) 488-0580 (203) 488-8587 Fax 63-2 North Branford Ri Branford, CT 04405

C-6





# GROUNDING SCHEMATIC NOTES

- GROUND RING, #2 AWG BCW
- \$2/0 GREEN INSULATED

# GENERAL NOTES:

- ALL SURGE SUPPRESSION EQUIPMENT SHALL BE BONDED TO GROUND PER MANUFACTURER'S SPECIFICATIONS
- 2. UNLESS OTHERWISE NOTED OR REQUIRED BY CODE, GROUND CONDUCTORS SHOWN SHALL BE  $$^42$  awg (solid tinned BCW — exterior; stranded green insulated — interior).
- Bond Cable Tray and Ice Bridge Sections together with #6 awg stranded green insulated jumpers.
- ALL SECTOR GROUND BARS SHALL BE BONDED TOGETHER WITH \$\frac{1}{2}\$ AWG SOLID TINNED BOW.
- BOND ALL EQUIPMENT CABINETS AND BATTERY CABINETS TO GROUND PER MANUFACTURER'S SPECIFICATIONS.
- ALL BONDS TO TOWER SHALL BE MADE IN STRICT ACCORDANCE WITH SPECIFICATIONS OF TOWER MANUFACTURER OR STRUCTURAL ENGINEER.
- 7. REFER TO GROUNDING PLAN FOR LOCATION OF GROUNDING DEVICES.
- 8. REFER TO ALL ELECTRICAL AND GROUNDING DETAILS.
- 9. COORDINATE ALL TOWER MOUNTED EQUIPMENT WITH OWNER.
- ALL TOWER MOUNTED AMPLIFIERS AND ASSOCIATED EQUIPMENT SHALL BE BONDED TO THE SECTOR GROUND BAR PER MANUFACTURER'S SPECIFICATIONS.
- 11. ALL FENCE POSTS WITHIN 6' OF EQUIPMENT SHELTER SHALL BE BONDED TO
- 12. ALL GROUNDING SHALL BE IN ACCORDANCE WITH NEC AND OWNER'S REQUIREMENTS.
- BOND GENERATOR TO GROUND PER NEC AND MANUFACTURERS SPECIFICATIONS.
- 14. BOND PROPANE TANK TO GROUND RING PER NEC AND MANUFACTURERS SPECIFICATIONS. COORDINATE WITH TANK MANUFACTURER FOR REQUIREMENTS PRIOR TO INSTALLATION.
- 15. COORDINATE WITH TOWER OWNER BEFORE INSTALLING ANY GROUNDING ELEMENTS ON TOWER OR BONDING TO EXISTING TOWER GROUND RING.

verizon

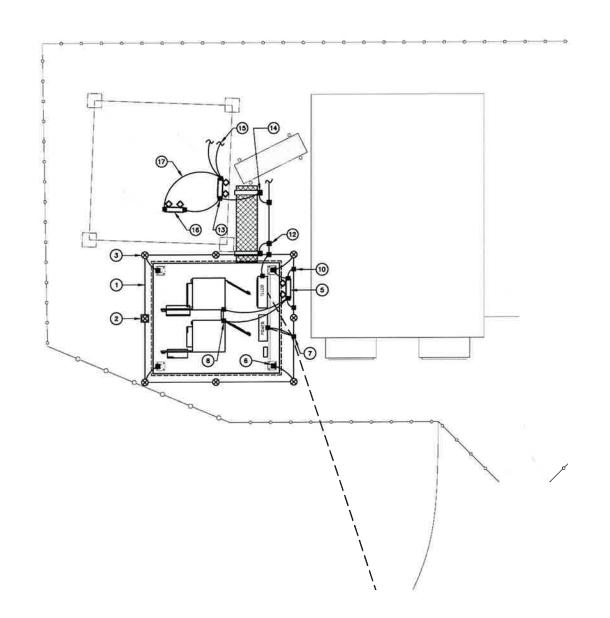
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SITE NAME: PORTILAND HS CT
SITE NAME: PORTILAND HS CT
SITE ID: 616480547
97 HGH STREET
PORTILAND CT, 06480

DATE: 11/02/23 SCALE: AS NOTED JOB NO. 22017.06

> ELECTRICAL SCHEMATIC DIAGRAM

E-2



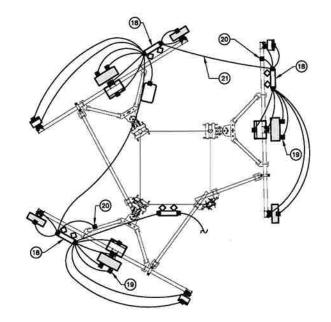
1 COMPOUND GROUNDING PLAN



- (2 SOLID TINNED BOW GROUND RING (INSTALL AS SHOWN ALONG COMPOUND PERIMETER, AND COMPLETELY ENCIRCLING THE EQUIPMENT
- 2 GROUNDING ROD WITH ACCESS (TYP.) SEE DETAILS.
- 3 GROUNDING ROD (TYP.) SEE DETAILS.
- (4) CONNECT FENCE TO COMPOUND GROUNDING RING.
- (5) MAIN GROUND BAR TYP.
  (6) BOND CANOPY POST TO GROUND RING TYP. EACH CORNER.
- TO BOND CABINETS TO GROUND RING PER NEC AND MANUFACTUTER REQUIREMENTS.
- BOND EQUIPMENT CABINETS TO GROUND BAR PER NEC AND MANUFACTURER REQUIREMENTS.
- NOT USED.
- 10 BOND GROUND BAR TO GROUND RING TYP. 2 PLACES.
  11 NOT USED.
- (12) ICE BRIDGE POST AND COVER. BOND EACH SECTION AND SUPPORT TO GROUND RING SEE DETAILS.
- (13) LOWER TOWER MOUNTED GROUND BAR.
- (15) BOND GROUND BAR TO TOWER GROUND RING TYP.

  (18) UPPER TOWER MOUNTED GROUND BAR.

- (1B) BOND ANTENNA MOUNTING PIPES TO SECTOR GROUND BAR.
  (20) BOND SECTOR GROUND BAR TO ANTENNA FRAME STEEL TYP.
- all sector ground bars shall be bonded together with  $\rlap/\!\!/ 2$  awg solid tinned bow.



2 ANTENNA GROUNDING PLAN E-3 SCALE: NOT TO SCALE

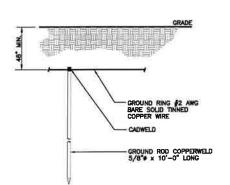
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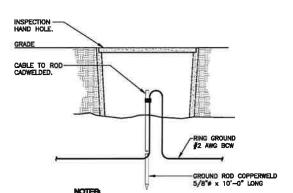
ELECTRICAL GROUNDING **PLANS** 



# NOTES

 USE GROUND PLATE DETAIL IF 10 FT. GROUND ROD DEPTH CANNOT BE ACHIEVED DUE TO LEDGE CONDITION OR IF EXISTING TOWER FOUNDATION IS ENCOUNTERED.

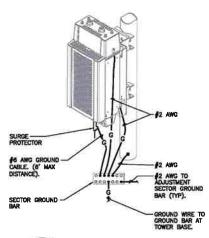




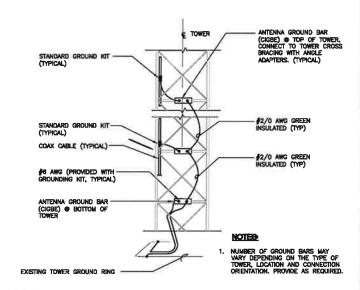
 INSPECTION HAND HOLE MAY BE CONCRETE OR PAC AND SHALL BE A MINIMUM OF 12" DIA x 18" DEEP.

2 GROUND ROD WITH ACCESS DETAIL
E-4 SCALE: NOT TO SCALE

# EACH RRH CABINET SHALL BE GROUNDED IN THE FOLLOWING MAINTER: 1. AT TOP OF THE CABINET 2. AT BOATE SING OF THE CABINET.

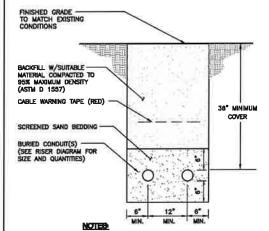


3 RRH POLE MOUNT GROUNDING E-4 SCALE NOT TO SCALE



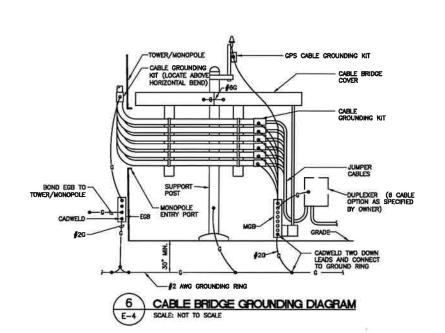
4 ANTENNA CABLE GROUNDING - LATTICE TOWER

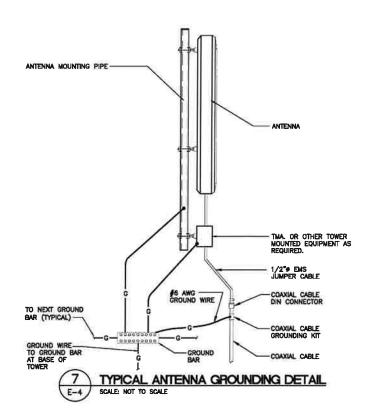
SOLE: NOT TO SCALE



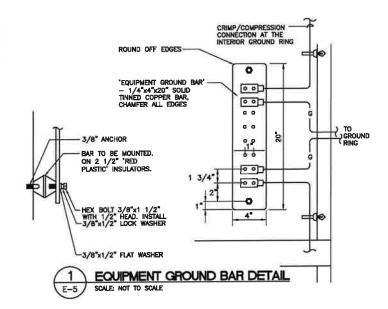
- THE CLEAN FILL SHALL PASS THROUGH A 3/8" MESH SCREEN AND SHALL NOT CONTAIN SHARP STONES, OTHER BACKFILL SHA NOT CONTAIN ASHES, CHORERS, SHELLS, FROZEN MATERIAL, LOO DEBRIS OR STONES LARGER THAN 2" IN MAXIMUM DIMENSION.
- 2. WHERE EXISTING UTILITIES ARE LIKELY TO BE ENCOUNTERED,
- WHERE SHALLOW BEDROCK IS ENCOUNTERED BETWEEN UTILITY SOURCE AND SERVICE EQUIPMENT, COORDINATE WITH UTILITY COMPANY FOR BURIAL DEPTH REQUIREMENTS.
- COORDINATE WITH ELECTRICAL ENGINEER WHERE SHALLOW BEDROOK IS ENCOUNTERED BETWEEN SERVICE EQUIPMENT AND FOURMENT SHELTER.

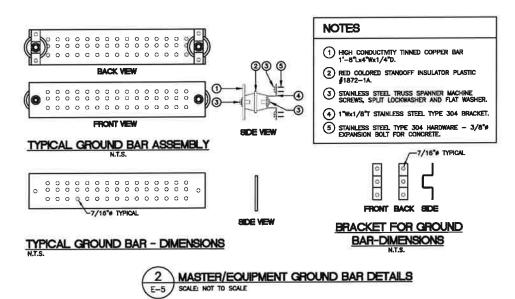
5 TYPICAL ELECTRICAL TRENCH DETAIL
E-4 SCALE: NOT TO SCALE

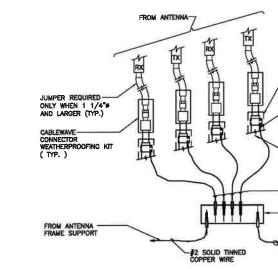












1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE 5 CONNECTION OF GROUND WIRES TO GROUND BAR

-CABLEWAVE GROUND KIT (TYP.) (SEE NOTE)

ANTENNA CABLE TO CABLE TRAY (TYP.)

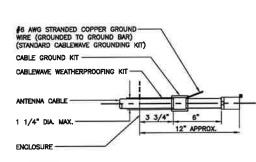
CIGBE GROUND BAR NEWTON, SIMILAR TO MOUNTED NEAR/BELOW ANTENNA

GROUND WIRE TO CIGBE/MIGB

# NOTES

- TINNED COPPER GROUND BAR, 1/4"  $\times$  4"  $\times$  20", NEWTON INSTRUMENT CO. HOLE CENTERS TO MATCH NEMA DOUBLE LUG CONFIGURATION.
- INSULATORS, NEWTON INSTRUMENT CAT. NO. 3061-4.
- $5/8^{\circ}$  lock washers, newton instrument co. cat. No. 3015-8.
- WALL MOUNTING BRACKET, NEWTON INSTRUMENT CO. CAT NO. A-8058.
- 5) 5/8-11 x 1" STAINLESS STEEL TRUSS SPANNER MACHINE SCREWS.

GROUND BAR DETAIL E-5 SCALE: NOT TO SCALE



# NOTED

DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO GROUND BAR.

6 ANTENNA CABLE GROUNDING DETAIL
E-5 SOLLE NOT TO SOLLE

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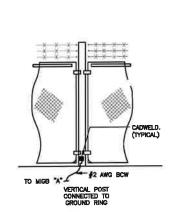
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DATE: 11/02/23

SCALE: AS NOTED JOS NO. 22017.06

TYPICAL ELECTRICAL DETAILS

E-5



- VERTICAL POSTS SHALL BE BONDED TO THE RING AT EACH CORNER AND AT EACH CATE POST, AS A MINIMUM ONE VERTICAL POST SHALL BE BONDED TO THE GROUND RING IN EVERY 100 FOOT STRAIGHT RUN OF FENCE.
- 2. HORIZONTAL POLES SHALL BE BONDED TO EACH OTHER.
- 3. BOND EACH HORIZONTAL POLE / BRACE TO EACH OTHER AND TO EACH VERTICAL POST THAT IS BONDED TO THE EXTERIOR GROUND RING.



# ELECTRICAL SPECIFICATIONS

# **SECTION 16010**

- 1.01. SCOPE OF WORK
- A. WORK SHALL BYCLUDE ALL LABOR, EQUIPMENT AND SERVICES REQUIRED TO COMPLETE (MAKE READY FOR OPERATION) ALL THE ELECTRICAL WORK INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING.
- INSTALL 200A, 208V, 3P, 4 WIRE ELECTRIC SERVICE WITH SMART SUB-METER AND 200A MAIN CIRCUIT BREAKER FOR OWNER AND ASSOCIATED DISTRIBUTION EQUIPMENT.
- 2. NEW SITE TELEPHONE SERVICE AS SPECIFIED BY TELEPHONE COMPANY.
- 3. GENERATOR
- 4. FEEDERS AND BRANCH CIRCUIT WIRING TO PANELS, RECEPTACLES, EQUIPMENT, ETC. AS INDICATED OR NOTED ON PLANS.
- 5. CELLULAR GROUNDING SYSTEMS, CONSISTING OF ANTENNA GROUNDING, GROUND BARS, FTC.
- 6. FIELD MEASURE EXISTING ELECTRICAL SERVICES TO CONFIRM AVAILABLE EXISTING
- 7. COORDINATE ALL WORK SHOWN, ON THESE PLANS WITH LOCAL UTILITY COMPANIES.
- B. LOCAL UTILITY COMPANIES SHALL PROVIDE THE FOLLOWING:
- C. CONTRACTOR SHALL CONFER WITH LOCAL UTILITY COMPANIES TO ASCERTAIN THE LIMITS OF THEIR WORK AND SHALL INCLUDE IN BID ANY CHARGES OR FEES MADE BY THE UTILITY COMPANIES FOR THEIR PORTION OF THE WORK AND SHALL PROVIDE AND INSTALL ALL ITEMS REQUIRED, BUT NOT PROVIDED BY UTILITY COMPANY.
- D. CONTRACTOR SHALL COORDINATE WITH TELEPHONE UTILITY COMPANY FOR LOCATION OF TELEPHONE SERVICE AND TO DETERMINE ANY REQUIRED EQUIPMENT TO BE INSTALLED BY CONTRACTOR.

- A. THE ENTIRE ELECTRICAL INSTALLATION SHALL BE MADE IN STRICT ACCORDANCE WITH ALL LOCAL, STATE AND MATIONAL CODES AND REGULATIONS WHICH MAY APPLY AND NOTHING IN THE DRAWINGS OR SPECIFICATIONS SHALL BE INTERPRETED AS AN INFRINGEMENT OF SUCH CODES OR REGULATIONS.
- B. THE ELECTRICAL CONTRACTOR IS TO BE RESPONSIBLE FOR THE COMPLETE INSTALLATION AND COORDINATION OF THE ENTIRE ELECTRICAL SERVICE. ALL ACTIVITIES TO BE COORDINATED THROUGH OWNERS REPRESENTATIVE, DESIGN ENGINEER AND OTHER AUTHORITIES HAVING JURISOICTION OF TRADES.
- C. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND PAY ALL FEES THAT MAY BE REQUIRED FOR THE ELECTRICAL WORK AND FOR SCHEDULING OF ALL INSPECTIONS THAT MAY BE REQUIRED BY THE LOCAL AUTHORITY.
- D. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATION WITH THE BUILDING OWNER FOR NEW AND/OR DEMOLITION WORK INVOLVED.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATION WITH LOCAL TELEPHONE COMPANY THAT MAY BE REQUIRED FOR THE INSTALLATION OF TELEPHONE SERVICE TO THE PROPOSED CELLUARS SITE.
- F. NO MATERIAL OTHER THAN THAT CONTAINED IN THE "LATEST LIST OF ELECTRICAL FITTINGS" APPROVED BY THE UNDERWRITERS' LABORATORIES, SHALL BE USED IN ANY PART OF THE WORK, ALL MATERIAL FOR WHICH LABEL SERVICE HAS BEEN ESTABLISHED SHALL BEAR THE U.L. LABEL.
- G. THE CONTRACTOR SHALL GUARANTEE ALL NEW WORK FOR A PERIOD OF ONE YEAR FROM THE ACCEPTANCE DATE BY THE OWNER. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING WARRANTIES FROM ALL EQUIPMENT MANUFACTURERS FOR SUBMISSION TO THE OWNER.
- H. DRAWINGS INDICATE GENERAL ARRANGEMENT OF WORK INCLIDED IN CONTRACT, CONTRACTOR SHALL, WITHOUT EXTRA CHARGE, MAKE MODIFICATIONS TO THE LAYOUT OF THE WORK TO PREVENT CONFLICT WITH WORK OF O'THEN TRACES AND FOR THE PROPER INSTALLATION OF WORK, CHECK ALL DRAWINGS AND VISIT JOB STITE TO VERIFY SPACE AND TYPE OF BUSINING CONDITIONS IN WHICH WORK WILL BE DONE, PRIOR TO SUBMITIAL
- I. THE ELECTRICAL CONTRACTOR SHALL SUPPLY THREE (3) COMPLETE SETS OF APPROVED DRAWINGS, ENGINEERING DATA SHEETS, MAINTENANCE AND OPERATING INSTRUCTION MANUALS FOR ALL SYSTEMS AND THEIR RESPECTIVE EQUIPMENT, THESE MANUALS SHALL BE INSERTED IN VINIAL COVERED 3—RING BINDERS AND TURNED OVER TO OWNER'S REPRESENTATIVE ONE (1) WEEK PRIOR TO FINAL PUNCH LIST.
- J. ALL WORK SHALL BE INSTALLED IN A NEAT AND WORKMAN LIKE MANNER AND WILL BE SUBJECT TO THE APPROVAL OF THE OWNER'S REPRESENTATIVE.
- K. ALL EQUIPMENT AND MATERIALS TO BE INSTALLED SHALL BE NEW, UNLESS OTHERWISE NOTED.
- L BEFORE FINAL PAYMENT, THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF PRINTS (AS-BUILTS), LEGIBLY MARKED IN RED PENCIL TO SHOW ALL CHANGES FROM THE ORGINAL PLANS.
- M. PROVIDE TEMPORARY POWER AND LIGHTING IN WORK AREAS AS REQUIRED.
- N. SHOP DRAWINGS:
- CONTRACTOR SHALL SUBMIT SIX (6) COPIES OF ALL TEST REPORTS CALLED FOR IN THE SPECIFICATIONS AND DRAWINGS.

O. ENTIRE ELECTRICAL INSTALLATION SHALL BE IN ACCORDANCE WITH OWNER'S SPECIFICATIONS, AND REQUIREMENTS OF ALL LOCAL AUTHORITIES HAVING JURISDICTION. IT IS THE CONTRACTOR'S RESPONSIBILITY TO COORDINATE WITH APPROPRIATE INDIVIDUALS TO OBTAIN ALL SUCH SPECIFICATIONS AND REQUIREMENTS. NOTHING CONTAINED IN OR OMITTED FROM, THESE DOCUMENTS SHALL RELEVE CONTRACTOR FROM THIS OBLIGATION.

# SECTION 16111

# 1.01. CONDUIT

- MINIMUM CONDUIT SIZE FOR BRANCH CIRCUITS, LOW VOLTAGE CONTROL AND ALARM CIRCUITS SHALL BE  $3/4^\circ$ . Conduits shall be properly fastened as required by the N.E.C.
- B. THE INTERIOR OF RACEWAYS/ ENCLOSURES INSTALLED UNDERGROUND SHALL BE CONSIDERED TO BE WET LOCATION, INSULATED CONDUCTORS SHALL BE LISTED FOR USE IN WET LOCATIONS, PROVIDE WEATHERPROOF CONSTRUCTION IN WET LOCATIONS.
- C. CONDUIT INSTALLED UNDERGROUND SHALL BE INSTALLED TO MEET MINIMUM COVER REQUIREMENTS OF TARI F 300.5.
- D. PROVIDE RIGID GALVANIZED STEEL CONDUIT (RMC) FOR THE FIRST 10 FOOT SECTION WHEN LEAVING A BUILDING OR SECTIONS PASSING THROUGH FLOOR SLABS
- E. CNLY LISTED PVC CONDUIT AND FITTINGS ARE PERMITTED FOR THE INSTALLATION OF ELECTRICAL CONDUCTORS, SUITABLE FOR UNDERGROUND APPLICATIONS.

CONDUIT SCHEDULE SECTION 16111				
CONDUITTYFE	NEC REFERENCE	AFFLICATION	NEC TABLE 800.5 45	
EMT	ARTICLE 358	INTERIOR CIRCUITING, EQUIPMENT ROOMS, SHELTERS	N/A	
RMC, RIGID GALV. STEEL	ARTICLE 344, 300.5, 300.50	ALL INTERIOR/ EXTERIOR CIRCUITING, ALL UNDERGROUND INSTALLATIONS.	6 INCHES	
PVC, SCHEDULE 40	ARTICLE 352, 300.5, 300.50	INTERIOR / EXTERIOR CIRCUITING AND GROUNDING SYSTEMS, UNDERGROUND INSTALLATIONS, WHERE NOT SUBJECT TO PHYSICAL DAMAGE. 1	18 INCHES	
PVC, SCHEDULE 80	ARTICLE 352, 300.5, 300.50	INTERIOR/ EXTERIOR CIRCUITING AND GROUNDING SYSTEMS, UNDERGROUND INSTALLATIONS, WHERE SUBJECT TO PHYSICAL DAMAGE. <sup>1</sup>	18 INCHES	
LIQUID TIGHT FLEX.	ARTICLE 350	SHORT LENGTHS (MAX. 3FT.) WIRING TO VIBRATING EQUIPMENT IN WET LOCATIONS.	N/A	
FLEX. METAL	ARTICLE 348	SHORT LENGTHS (MAX. 3FT.) WIRING TO VIBRATING EQUIPMENT IN WET LOCATIONS.	N/A	

PHYSICAL DAWNE IS SUBJECT TO THE AUTHORITY HAVING JARSSDICTION.

\* UNDERGRIUNG CONDUIT DISTALLED UNGER RUADS, HUGHVAYS, DRIVEVAYS, PARKING LUTS SHALL HAVE KINDHUM DEPTH OF 24". <sup>3</sup> Wede Solid Rick Prevents Copplance with Horson Cover Depths, Viring Shall Be distalled in Perotited Ricevay for direct Burgal, the Ricevay Shall be covered by a Horson of 2° of Concrete Extending Dinn to Rick.

# **SECTION 16123**

# 1.01. CONDUCTORS

A ALL CONDUCTORS SHALL BE TYPE THAM (INT. APPLICATION) AND XHHW (EXT. APPLICATION), 75 DEGREE C, 600 VOLT INSULATION, SOFT ANNEALED STRANDED COPPER, \$10 AWS AND SMALLER SHALL BE SPLICED USING ACCEPTABLE SOLDETLESS PRESSURE CONNECTORS, \$6 AWS AND LARGER SHALL BE SPLICED USING COMPRESSION SPLIT—BOLT TYPE CONNECTORS, \$12 AWG SHALL BE THE MINIMUM SIZE CONDUCTOR FOR LINE VOLTAGE BRANCH CIRCUITS, REFER TO PANEL SCHELE FOR BRANCH CIRCUIT CONDUCTOR SIZE(S). CONDUCTORS SHALL BE COLOR CODED FOR CONSISTENT

	120/208/240V	277/480V
INE	COLOR	COLOR
<u> </u>	BLACK	BIROWN
9	RED	ORANGE
0	BLUE	YELLOW
4	CONTINUOUS WHITE	GREY
3	CONTINUOUS GREEN	GREEN WITH YELLOW STRIPE

B. MINIMUM BENDING RADIUS FOR CONDUCTORS SHALL BE 12 TIMES THE LARGEST DIAMETER OF BRANCH CIRCUIT CONDUCTOR.

# **SECTION 16130**

- A. FURNISH AND INSTALL OUTLET BOXES FOR ALL DEVICES, SWITCHES, RECEPTACLES, ETC.. BOXES TO BE ZINC COATED STEEL.
- B. FURNISH AND INSTALL PULL BOXES IN MAIN FEEDERS RUNS WHERE REQUIRED, PULL BOXES SHALL BE GALVANIZED STEEL WITH SCREW REMOVABLE COVERS, SIZE AND QUANTITY AS REQUIRED, PROVIDE WEATHERPROOF CONSTRUCTION IN WET LOCATIONS.

# **SECTION 16140**

- . THE FOLLOWING LIST IS PROVIDED TO CONVEY THE QUALITY AND RATING OF WIRING DEVICES WHICH ARE TO BE INSTALLED. A COMPLETE LIST OF ALL DEVICES MUST BE SUBMITTED BEFORE INSTALLATION FOR APPROVAL.
- 1. 15 MINUTE TIMER SWITCH INTERMATIC #FF15M (INTERIOR LIGHTS)
- 2. DUPLEX RECEPTACLE PAS \$2095 (GFCI) SPECIFICATION GRADE
- 3. SINGLE POLE SWITCH P&S #CSE20AC2 (20A-120V HARD USE) SPECIFICATION GRADE
- 4. DUPLEX RECEPTACLE PAS #5382 (20A-120V HARD USE) SPECIFICATION GRADE
- B. PLATES ALL PLATES USED SHALL BE CORROSION RESISTANT TYPE 304 STAINLESS STEEL PLATES SHALL BE FROM SAME MANUFACTURER AS SWITCHES AND RECEPTACLES. PROVIDE WEATHERPROOF HOUSING FOR DEVICES LOCATIED IN WET LOCATIONS.
- C. OTHER MANUFACTURERS OF THE SWITCHES, RECEPTACLES AND PLATES MAY BE SUBMITTED FOR APPROVAL BY THE ENGINEER.

# **SECTION 16170**

A. FUSIBLE AND NON-FUSIBLE, 600V, HEAVY DUTY DISCONNECT SWITCHES SHALL BE AS MANUFACTURED BY SQUARE "D". PROVIDE FUSES AS CALLED FOR ON THE CONTRACT DRAWINGS. AMPERE RATING SHALL BE CONSISTENT WITH LOAD BEING SERVED. DISCONNECT SWITCH COVER SHALL BE MECHANICALLY INTERLOCKED TO PREVENT COVER FROM OPENING WHEN THE SWITCH IS IN THE "ON" POSITION. EXTERIOR APPLICATIONS SHALL BE NEMA 3R CONSTRUCTION WITH PADLOCK FEATURE.

# SECTION 16190

1.01. SEISMIC RESTRAIN

A. ALL DEVICES SHALL BE INSTALLED IN ACCORDANCE WITH ZONE 2 SEISMIC REQUIREMENTS.

# **SECTION 16195**

1.01. LABELING AND IDENTIFICATION HOMENCLATURE FOR ELECTRICAL EQUIPMEN

- A. CONTRACTOR SHALL FURNISH AND INSTALL NON—METALLIC ENGRAVED BACK—LIT NAMEPLATES ON ALL PANELS AND MAJOR ITEMS OF ELECTRICAL EQUIPMENT.
- B. LETTERS TO BE WHITE ON BLACK BACKGROUND WITH LETTERS 1-1/2 INCH HIGH WITH 1/4 INCH
- C. IDENTIFICATION NOMENCLATURE SHALL BE IN ACCORDANCE WITH OWNER'S STANDARDS.
- D. PROVIDE NAMEPLATE FOR PORTABLE ENGINE/GENERATOR CONNECTION SHOWING VOLTAGE KVA/KW RATING, & PHASE, AND & OF WIRES. PLATE TO BE PLASTIC ENGRAVED, RED WITH WHITE LETTERS.
- E. ALL RECEPTACLES, SWITCHES, DISCONNECT SWITCHES, ETC. SHALL BE LABELED WITH THE CORRECT BRANCH CIRCUIT NUMBER SERVED BY MEANS OF PERMANENT PRESSED TYPE BLACK 1/4" RANSFER LETTERING. (FOR EXAMPLE: "MOP-5", ETC.).

# **SECTION 16450**

1.01 GROUNDING

- A. ALL NON-CURRENT CARRYING PARTS OF THE ELECTRICAL AND TELEPHONE CONDUIT SYSTEMS SHALL BE MECHANICALLY AND ELECTRICALLY CONNECTED TO PROVIDE AN INDEPENDENT RETURN PAIR TO THE EQUIPMENT GROUNDING SOURCES.
- B. GROUNDING SYSTEM WILL BE IN ACCORDANCE WITH THE LATEST ACCEPTABLE EDITION OF THE NATIONAL ELECTRICAL CODE AND REQUIREMENTS PER LOCAL INSPECTOR HAVING
- C. GROUNDING OF PANELBOARDS:
- PANELBOARD SHALL BE GROUNDED BY TERMINATING THE PANELBOARD FEEDER'S EQUIPMENT GROUND CONDUCTOR TO THE EQUIPMENT GROUND BAR KIT(S) LUGGED TO THE CABINET. ENSURE THAT THE SURFACE BETWEEN THE KIT AND CABINET ARE BARE METAL TO BARE METAL PRIME AND PAINT OVER TO PREVENT CORROSSON.
- CONDUIT(S) TERMINATING INTO THE PANELBOARD SHALL HAVE GROUNDING TYPE BUSHINGS. THE BUSHINGS SHALL BE BONDED TOGETHER WITH BARE \$10 AWG COPPER CONDUCTOR WHICH IN TURN IS TERMINATED INTO THE PANELBOARD'S
- 1. EACH EQUIPMENT GROUND CONDUCTOR SHALL BE SIZED IN ACCORDANCE WITH THE N.F.C. ARTICLE 250-122
- 2. THE MINIMUM SIZE OF EQUIPMENT GROUND CONDUCTOR SHALL BE \$12 AWG COPPER.
- EACH FEEDER OR BRANCH CIRCUIT SHALL HAVE EQUIPMENT GROUND CONDUCTOR(S) INSTALLED IN THE SAME RACEWAY(S).

CONTRACTOR SHALL PROVIDE A CELLULAR GROUNDING SYSTEM WITH THE MAXIMUM AC RESISTANCE TO GROUND OF 10 OHM BETWEEN ANY POINT ON THE GROUNDING SYSTEM AS MEASURED BY 3-POINT GROUNDING TEST, (REPER TO SECTION 10960).

PROVIDE THE CELLULAR GROUNDING SYSTEM AS SPECIFIED ON DRAWINGS, INCLUDING, BUT NOT LIMITED TO:

- GROUND BARS
   EXTERIOR GROUNDING (WHERE REQUIRED DUE TO MEASURED AC RESISTANCE GREATER
- THAN SPECIFIED).

  3. ANTENNA GROUND CONNECTIONS AND PLATES.
- F. CONTRACTOR, AFTER COMPLETION OF THE COMPLETE GROUNDING SYSTEM BUT PRIOR TO CONCEALMENT/BURNAL. OF SAME, SHALL NOTIFY OWNER'S PROJECT ENGINEER WHO WILL HAVE A DESIGN ENGINEER WIST STE AND MAKE A VISUAL INSPECTION OF THE GROUNDING ORDID AND CONNECTIONS OF THE SYSTEM.
- G. ALL EQUIPMENT SHALL BE BONDED TO GROUND AS REQUIRED BY N.E.C., MFG. SPECIFICATIONS, AND OWNER'S SPECIFICATIONS.

# **SECTION 16470**

- A. REFER TO CONTRACT DRAWINGS FOR DETAILS AND SCHEDULES.

# **SECTION 16477**

A. FUSES SHALL BE NONRENEWABLE TYPE AS MANUFACTURED BY "BUSSMAN" OR APPROVED EQUAL. PUSES RATED TO 1/10 AMPERE UP TO 800 AMPERES SHALL BE EQUIVALENT TO BUSSMAN TYPE LPN-RK (2507) UL CLASS RK1, LOW PENK, DUAL ELEMENT, TIME-DELAY FUSES, FUSES SHALL HAVE SEPARATE SHORT CIRCUIT AND OVERLOAD ELEMENTS AND HAVE AN INTERRIPTING RATING OF 200 KMC. UPON COMPLETION OF WORK, PROMDE ONE SPARE SET OF PUSES FOR EACH TYPE INSTALLED.

# (SUPPLIED BY OWNER, INSTALLED BY CONTRACTOR)

1.01. GENERATOR SET

A. REFER TO CONTRACT DRAWINGS FOR DETAILS AND SCHEDULES.

# **SECTION 16960**

1.01. TESTS BY INDEPENDENT ELECTRICAL TESTING FIRM

- CONTRACTOR SHALL RETAIN THE SERVICES OF A LOCAL INDEPENDENT ELECTRICAL TESTING FIRM (WITH MINIMUM 5 YEARS COMMERCIAL EXPERIENCE IN THE ELECTRICAL TESTING INDUSTRY) AS SPECIFIED BY OWNER TO PERFORM:
- TEST 1: THERMAL OVERLOAD AND MAGNETIC TRIP TEST, AND CABLE INSULATION TEST FOR ALL CIRCUIT BREAKERS RATED 100 AMPS OR GREATER.
- TEST 2: RESISTANCE TO GROUND TEST ON THE CELLULAR GROUNDING SYSTEM.
- THE TESTING FIRM SHALL INCLUDE THE FOLLOWING INFORMATION WITH THE REPORT:
- 1. TESTING PROCEDURE INCLUDING THE MAKE AND MODEL OF TEST EQUIPMENT.
- CERTIFICATION OF TESTING EQUIPMENT CALIBRATION WITHIN SIX (6) MONTHS OF DATE OF TESTING, INCLUDE CERTIFICATION LAB ADDRESS AND TELEPHONE NUMBER.
- 3. GRAPHICAL DESCRIPTION OF TESTING METHOD ACTUALLY IMPLEMENTED.
- B. THESE TESTS SHALL BE PERFORMED IN THE PRESENCE AND TO THE SATISFACTION OF OWNER'S CONSTRUCTION REPRESENTATIVE. TESTING DATA SHALL BE INITIALED AND DATED BY THE CONSTRUCTION REPRESENTATIVE AND INCLUDED WITH THE WRITTEN REPORT/ANALYSIS.
- C. THE CONTRACTOR SHALL FORWARD SIX (6) COPIES OF THE INDEPENDENT ELECTRICAL TESTING FIRM'S REPORT/AMALYSIS TO ENGINEER A MINIMUM OF TEN (10) WORKING DAYS PRIOR TO THE JOB TURNOVER.
- D. CONTRACTOR TO PROVIDE A MINIMUM OF ONE (1) WEEK NOTICE TO OWNER AND ENGINEER FOR ALL TESTS REQUIRING WITNESSING.

# SECTION 16961

- ALL TESTS AS REQUIRED UPON COMPLETION OF WORK, SHALL BE MADE BY THIS CONTRACTOR. THESE SHALL BE CONTINUITY AND INSULATION TESTS; TEST TO DETERMINE THE QUALITY OF MATERIALS, ETC. AND SHALL BE MADE IN ACCORDANCE WITH N.E.C. RECOMMENDATIONS, ALL FEEDERS AND BRANCH CIRCUIT WIRING (EXCEPT CLASS 2 SIGNAL CIRCUITS) MUST BE TESTED FREE FROM SHORT CIRCUIT AND GROUND FAULT CONDITIONS AT 500V IN A REASONABLY DRY AMBIENT OF APPROXIMATELY 70 DEGREES.
- CONTRACTOR SHALL PERFORM LOAD PHASE BALANCING TESTS. CIRCUITS SHALL BE SO CONNECTED TO THE PANELBOARDS SUCH THAT THE NEW LOAD IS DISTRIBUTED AS EQUALLY AS POSSIBLE BETWEEN EACH LOAD AND NEUTRAL. DOX SHALL BE CONSIDERED AS A REASONMBLE AND ACCEPTABLE ALLOWANCE. BRANCH CIRCUITS SHALL BE BALANCED ON THEIR COWN PANELBOARDS; FEEDER LOADS SHALL IN TURN, BE BALANCED ON THE SERVICE COUPMENT. REASONABLE LOAD TEST SHALL BE ARRANGED TO VERIFY LOAD BALANCE IF REQUESTED BY THE ENGINEER.
- C. ALL TESTS, UPON REQUEST, SHALL BE REPEATED IN THE PRESENCE OF OWNER'S REPRESENTATIVE. ALL TESTS SHALL BE DOCUMENTED AND TURNED OVER TO OWNER. OWNER SHALL HAVE THE AUTHORITY TO STOP ANY OF THE WORK NOT BEING PROPERLY INSTALLED. ALL SUCH DETECTED WORK SHALL BE REPARED OR REPLACED AT NO ADDITIONAL EXPENSE TO THE OWNER AND THE TESTS SHALL BE REPEATED.

CONSTRUCTION 0 eriz >

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Partnership E DATE: 11/02/23

FLECTRICAL **SPECIFICATIONS** 

SCALE: AS NOTED

JOB NO. 22017.08

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