



May 9, 2014

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Re: Notice of Exempt Modification – Three (3) New Radio Heads Only
Property Address: 82 Tyrone Road, Pomfret, CT 06258 (the “Property”)
Applicant: New Cingular Wireless PCS, LLC (“AT&T”)

Dear Ms. Bachman:

AT&T currently maintains a wireless telecommunications facility on an existing 154-foot monopole (tower) location on the Property. AT&T’s facility consists of nine (9) wireless telecommunication antennas at a height of 152-feet. The tower is owned by Crown Castle, LLC. The Council approved AT&T’s use of the tower in the following prior decisions; EM-CING-112-090205 and EM-CING-112-130110. In its 1/25/2013 decision (the “Decision”), the Council approved for AT&T to install 6 Remote Radio Heads (Ericsson RRUS-11) but AT&T only installed three (3). AT&T now intends to install the remaining RRUS-11’s to complete the installation. This Exempt Mod Application is necessary because the 1/25/2013 decision is over one year old. Please refer to Tab 1 for further specifications of the new radio heads.

Please accept this application as notification pursuant to R.C.S.A. §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16-50j-72(b)(2). In accordance with R.C.S.A. §16-50j-73, a copy of this letter is being sent to the Pomfret Board of Selectmen. A copy of this letter is also being sent to Crown Castle, LLC the owner of the property where the tower is located.

The planned modifications to AT&T’s facility fall squarely within those activities explicitly provided for in R.C.S.A. §16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing tower. AT&T’s new RRUS-11’s will be installed at the 152-foot level of the 154-foot monopole.



2. The proposed modifications will not involve any changes to ground-mounted equipment and, therefore, will not require an extension of the site boundary.
3. The proposed modifications will not increase the noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the modified facility will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. A RF emissions calculation for AT&T's modified facility was provided in the application which led to the 1/25/2013 Decision. See Tab 2 attached.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The tower and its foundation can support AT&T's proposed modifications. (See Structural Analysis Report included in Tab 3).

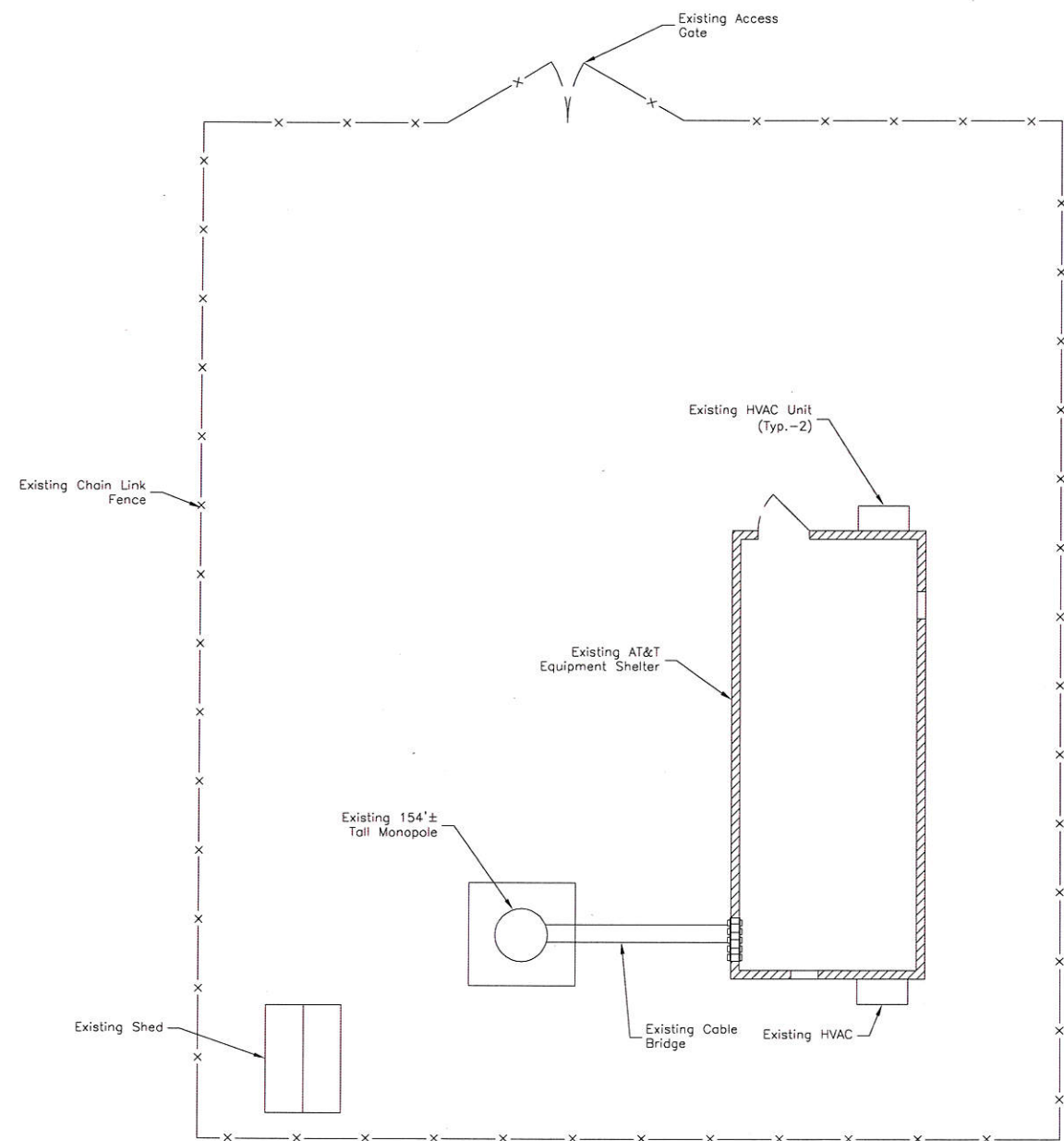
For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitutes an exempt modification under R.C.S.A. §16-50j-72(b)(2).

Sincerely,

Adam F. Brailard

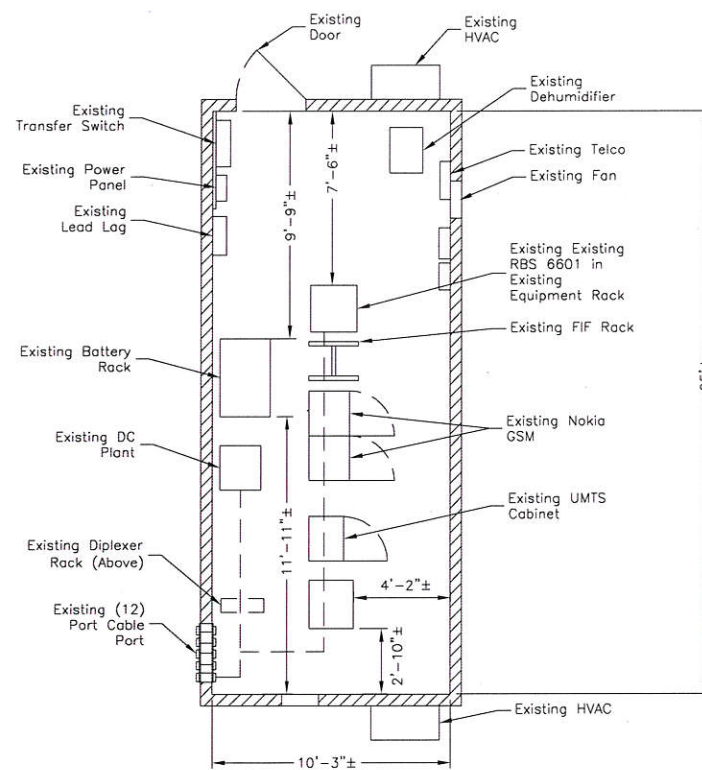
cc: Crown Castle, LLC 12725 Morris Road Extension Suite 400 Alpharetta GA 30004

Pomfret Board of Selectmen – 5 Haven Road, Pomfret Center, CT 06259

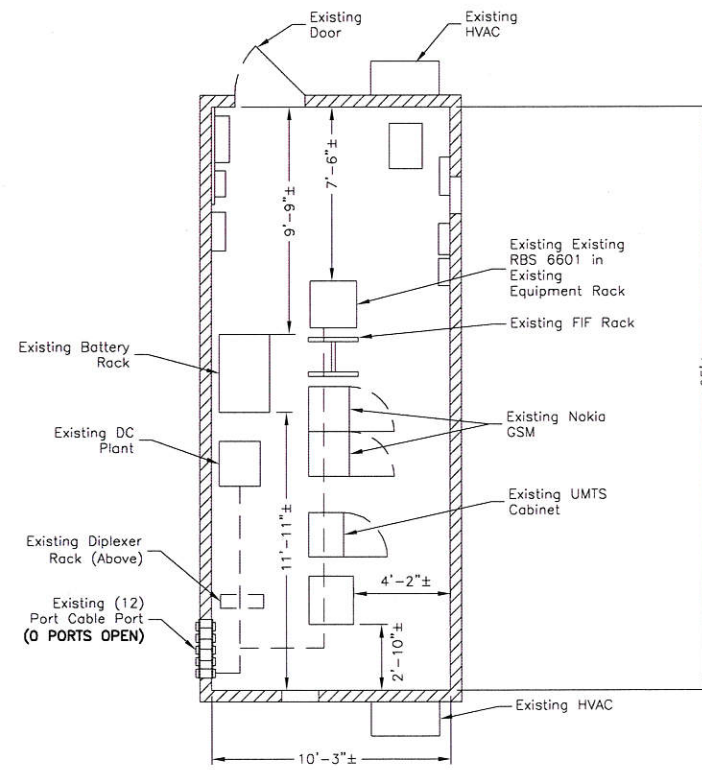


- NOTES:**
1. NORTH SHOWN AS APPROXIMATE.
 2. MOUNT ALL ANTENNAS, COAX, SURGE ARRESTORS, RRUS, ETC. IN ACCORDANCE WITH STRUCTURAL ANALYSIS.
 3. NOT ALL INFORMATION IS SHOWN FOR CLARITY.

SITE PLAN
 SCALE: 1"=10' FOR 11"x17"
 1"=5' FOR 22"x34"
 0' 5' 10'



EXISTING EQUIPMENT PLAN
 SCALE: 1/8"=1' FOR 11"x17"
 1/4"=1' FOR 22"x34"
 0' 4' 8'



PROPOSED EQUIPMENT PLAN
 SCALE: 1/8"=1' FOR 11"x17"
 1/4"=1' FOR 22"x34"
 0' 4' 8'



500 ENTERPRISE DRIVE SUITE 3A
 ROCKY HILL, CT 06067



1997 ANNAPOLIS EXCHANGE PARKWAY
 SUITE 200
 ANNAPOLIS, MD 21401

**CT1050
 POMFRET**

CONSTRUCTION DRAWINGS

1	05/01/14	ISSUED FINAL
0	04/11/14	ISSUED FINAL
A	03/07/14	PRELIMINARY SUBMISSION



Dewberry Engineers Inc.
 600 PARSIPPANY ROAD
 SUITE 301
 PARSIPPANY, NJ 07054
 PHONE: 973.739.9400
 FAX: 973.739.9710

ROBERT J. FOLEY, P.E.
 CT LICENSE No. PEN.0029056
 IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS
 THEY ARE ACTING UNDER THE DIRECTION OF A
 LICENSED PROFESSIONAL ENGINEER TO ALTER THIS
 DOCUMENT.

DRAWN BY: JC

REVIEWED BY: PD

CHECKED BY: GHN

PROJECT NUMBER: 50063024

JOB NUMBER: 50063027

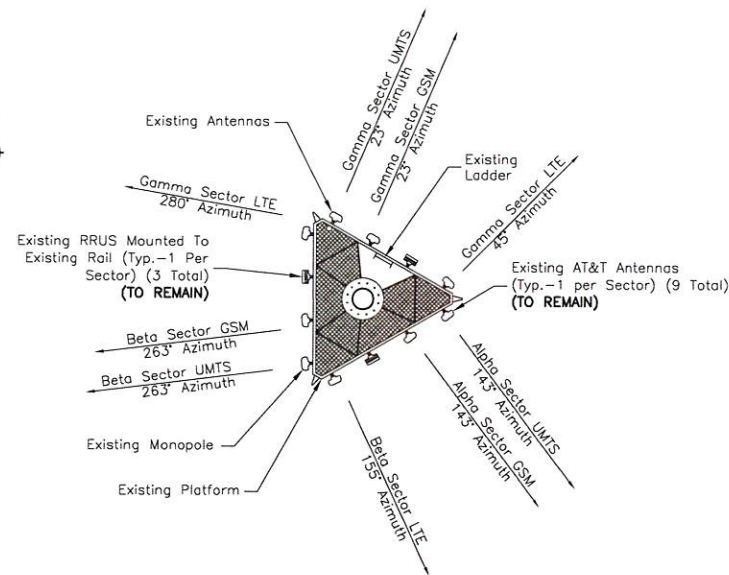
SITE ADDRESS:

82 TYRONE ROAD
 POMFRET, CT 06258
 WINDHAM COUNTY

SHEET TITLE

SITE PLAN &
 EQUIPMENT PLANS

SHEET NUMBER



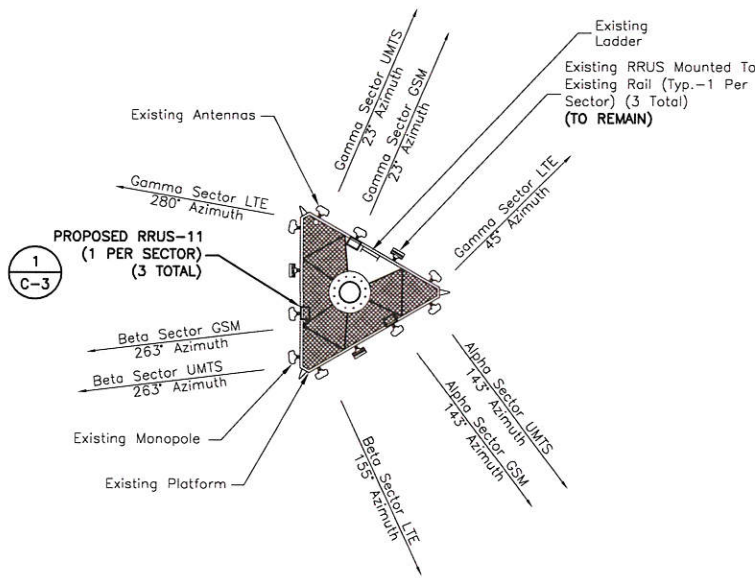
EXISTING ANTENNA LAYOUT

SCALE: N.T.S.

1

NOTES:

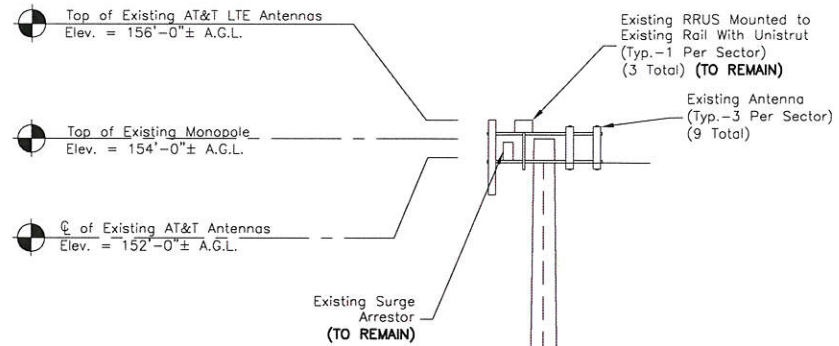
- EXISTING TMA'S NOT SHOWN FOR CLARITY.
- ALL EXISTING TMA'S ARE TO REMAIN.



PROPOSED ANTENNA LAYOUT

SCALE: N.T.S.

2

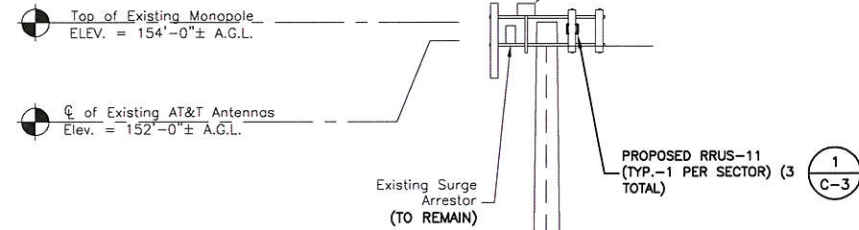


EXISTING NORTH ELEVATION

SCALE: 1"=20' FOR 11"x17"
1"=10' FOR 22"x34"

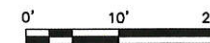


3



PROPOSED NORTH ELEVATION

SCALE: 1"=20' FOR 11"x17"
1"=10' FOR 22"x34"



4



500 ENTERPRISE DRIVE SUITE 3A
ROCKY HILL, CT 06067



1997 ANNAPOLIS EXCHANGE PARKWAY
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**CT1050
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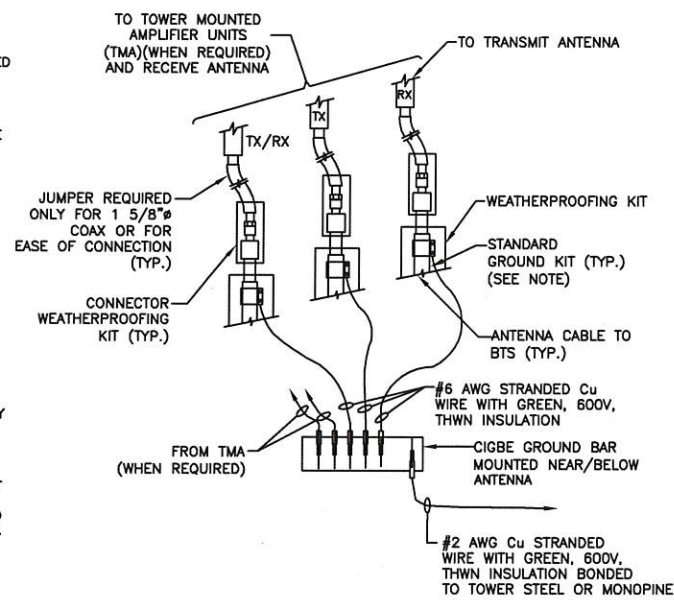
SHEET TITLE

ANTENNA LAYOUTS
& ELEVATIONS

SHEET NUMBER

GROUNDING NOTES:

1. THE CONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTNING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE CONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE ENGINEER FOR RESOLUTION.
2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS. ALL AVAILABLE GROUNDING ELECTRODES SHALL BE CONNECTED TOGETHER IN ACCORDANCE WITH THE NEC.
3. THE CONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR GROUND ELECTRODE SYSTEMS. USE OF OTHER METHODS MUST BE PRE-APPROVED BY THE ENGINEER IN WRITING.
4. THE CONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS ON TOWER SITES AND 10 OHMS OR LESS ON ROOFTOP SITES. WHEN ADDING ELECTRODES, CONTRACTOR SHALL MAINTAIN A MINIMUM DISTANCE BETWEEN THE ADDED ELECTRODE AND ANY OTHER EXISTING ELECTRODE EQUAL TO THE BURIED LENGTH OF THE ROD. IDEALLY, CONTRACTOR SHALL STRIVE TO KEEP THE SEPARATION DISTANCE EQUAL TO TWICE THE BURIED LENGTH OF THE RODS.
5. THE CONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENCING GROUNDING AND UNDERGROUND CONDUIT INSTALLATION AS TO PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO THE CONDUIT.
6. METAL CONDUIT AND TRAY SHALL BE GROUNDING AND MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH #6 AWG COPPER WIRE AND UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
7. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO TRANSMISSION EQUIPMENT.
8. CONNECTIONS TO THE GROUND BUS SHALL NOT BE DOUBLED UP OR STACKED. BACK-TO-BACK CONNECTIONS ON OPPOSITE SIDES OF THE GROUND BUS ARE PERMITTED.
9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
10. USE OF 90° BENDS IN THE PROTECTION GROUNDING CONDUCTORS SHALL BE AVOIDED WHEN 45° BENDS CAN BE ADEQUATELY SUPPORTED. IN ALL CASES, BENDS SHALL BE MADE WITH A MINIMUM BEND RADIUS OF 8 INCHES.
11. EACH INTERIOR TRANSMISSION CABINET FRAME/PLINTH SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH #6 AWG STRANDED, GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRE UNLESS NOTED OTHERWISE IN THE DETAILS. EACH OUTDOOR CABINET FRAME/PLINTH SHALL BE DIRECTLY CONNECTED TO THE BURIED GROUND RING WITH 2 AWG SOLID TIN-PLATED COPPER WIRE UNLESS NOTED OTHERWISE IN THE DETAILS.
12. ALL EXTERIOR GROUND CONDUCTORS BETWEEN EQUIPMENT/GROUND BARS AND THE GROUND RING, SHALL BE 2 AWG SOLID TIN-PLATED COPPER UNLESS OTHERWISE INDICATED.
13. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE. CONNECTIONS TO ABOVE GRADE UNITS SHALL BE MADE WITH EXOTHERMIC WELDS WHERE PRACTICAL OR WITH 2 HOLE MECHANICAL TYPE BRASS CONNECTORS WITH STAINLESS STEEL HARDWARE, INCLUDING SET SCREWS. HIGH PRESSURE CRIMP CONNECTORS MAY ONLY BE USED WITH WRITTEN PERMISSION FROM SMARTLINK MARKET REPRESENTATIVE.
14. EXOTHERMIC WELDS SHALL BE PERMITTED ON TOWERS ONLY WITH THE EXPRESS APPROVAL OF THE TOWER MANUFACTURER OR THE CONTRACTOR'S STRUCTURAL ENGINEER.
15. ALL WIRE TO WIRE GROUND CONNECTIONS TO THE INTERIOR GROUND RING SHALL BE FORMED USING HIGH PRESS CRIMPS OR SPLIT BOLT CONNECTORS WHERE INDICATED IN THE DETAILS.
16. ON ROOFTOP SITES WHERE EXOTHERMIC WELDS ARE A FIRE HAZARD COPPER COMPRESSION CAP CONNECTORS MAY BE USED FOR WIRE TO WIRE CONNECTORS. 2 HOLE MECHANICAL TYPE BRASS CONNECTORS WITH STAINLESS STEEL HARDWARE, INCLUDING SET SCREWS SHALL BE USED FOR CONNECTION TO ALL ROOFTOP TRANSMISSION EQUIPMENT AND STRUCTURAL STEEL.
17. COAX BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR USING TWO-HOLE MECHANICAL TYPE BRASS CONNECTORS AND STAINLESS STEEL HARDWARE.
18. APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
19. ALL EXTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERIAL.
20. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
21. BOND ALL METALLIC OBJECTS WITHIN 6 FT OF THE BURIED GROUND RING WITH 2 AWG SOLID TIN-PLATED COPPER GROUND CONDUCTOR, DURING EXCAVATION FOR NEW GROUND CONDUCTORS, IF EXISTING GROUND CONDUCTORS ARE ENCOUNTERED, BOND EXISTING GROUND CONDUCTORS TO NEW CONDUCTORS.
22. GROUND CONDUCTORS USED IN THE FACILITY GROUND AND LIGHTNING PROTECTION SYSTEMS SHALL NOT BE ROUTED THROUGH METALLIC OBJECTS THAT FORM A RING AROUND THE CONDUCTOR, SUCH AS METALLIC CONDUITS, METAL SUPPORT CLIPS OR SLEEVES THROUGH WALLS OR FLOORS. WHEN IT IS REQUIRED TO BE HOUSED IN CONDUIT TO MEET CODE REQUIREMENTS OR LOCAL CONDITIONS, NON-METALLIC MATERIAL SUCH AS PVC PLASTIC CONDUIT SHALL BE USED. WHERE USE OF METAL CONDUIT IS UNAVOIDABLE (E.G., NON-METALLIC CONDUIT PROHIBITED BY LOCAL CODE) THE GROUND CONDUCTOR SHALL BE BONDED TO EACH END OF THE METAL CONDUIT WITH LISTED BONDING FITTINGS.

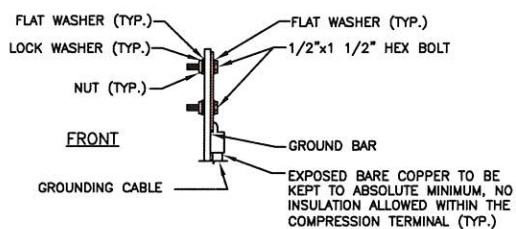
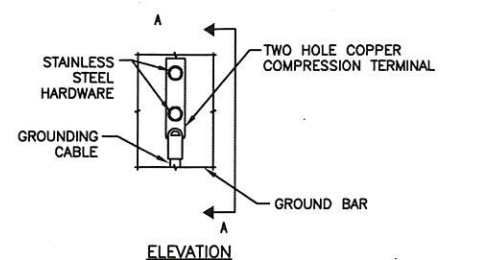


NOTE:

1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

CONNECTION OF GROUND WIRES TO GROUNDING BAR (CIGBE)

1



SECTION 'A-A'

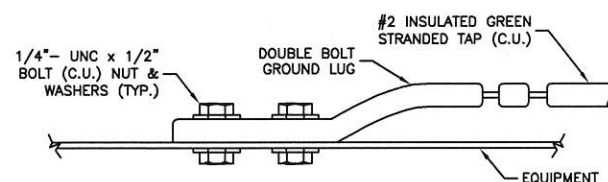
NOTES:

1. DOUBLING UP OR STACKING OF CONNECTIONS IS NOT PERMITTED.
2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATIONS.

TYPICAL GROUND BAR MECHANICAL CONNECTION DETAIL

SCALE: N.T.S.

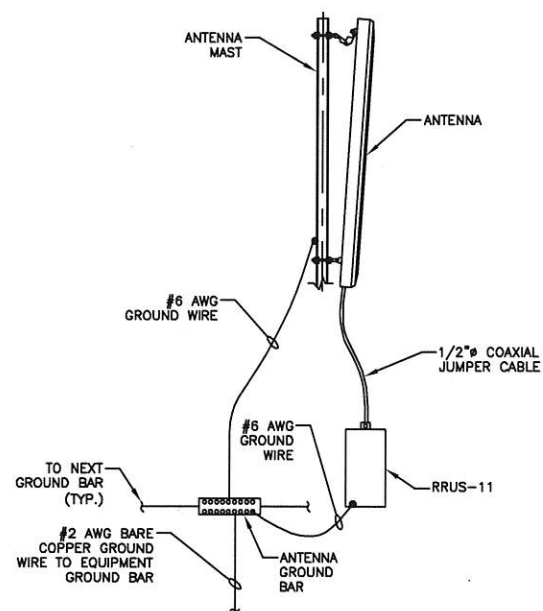
2



CONNECTION TO EQUIPMENT DETAIL

SCALE: N.T.S.

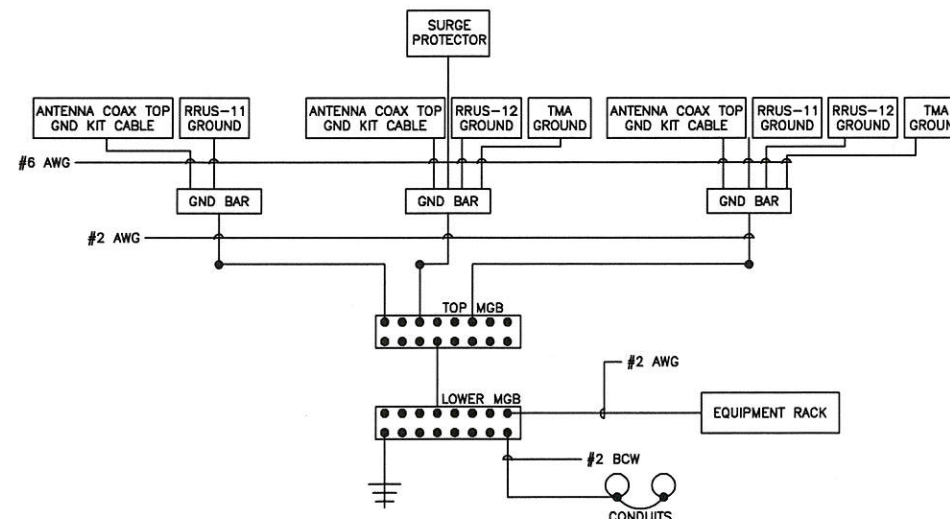
3



TYPICAL ANTENNA GROUNDING DETAIL

SCALE: N.T.S.

4



NOTES:

1. BOND ANTENNA GROUNDING KIT CABLE TO TOP CIGBE
2. BOND ANTENNA GROUNDING KIT CABLE TO BOTTOM CIGBE.
3. SCHEMATIC GROUNDING DIAGRAM IS TYPICAL FOR EACH SECTOR.
4. GROUND ALL EQUIPMENT PER MANUFACTURER RECOMMENDATIONS.

SCHEMATIC GROUNDING DIAGRAM

SCALE: N.T.S.

5



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NO.	DATE	DESCRIPTION
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SITE ADDRESS:

82 TYRONE ROAD
POMFRET, CT 06258
WINDHAM COUNTY

SHEET TITLE

GROUNDING DETAILS

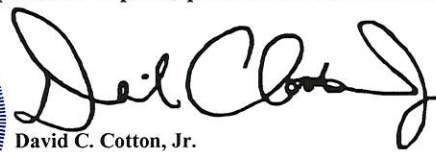
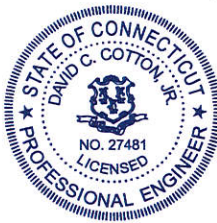
SHEET NUMBER

Todd Oliver
Smartlink, LLC
Market Manager, NE
33 Boston Post Road, Suite 210
Marlborough, MA 01752

Reference: Smartlink LLC Site, 82 Tyrone Road, Pomfret, CT

Date: 6 May 2014

1. This letter will address the additional RF impact that adding AT&T LTE antennas to the referenced site. Attached are two documents which cover the modeled RF emissions from the site.
2. The first report, "RF Emissions Compliance Report," for the site compiled by Sitesafe, uses the antenna patterns for the antennas at the site to calculate the General Public Maximum Permissible Exposure (MPE) on the ground. The total MPE of all the carriers is 0.585% (based on the General Public MPE) based on this modeling, with AT&T antennas emitting a maximum of 0.585% of the General Public MPE on the ground.
3. The second attachment has the calculations, used by the Connecticut Siting Council, which assumes the maximum antenna gain transmits in a spherical pattern where the worst case results would be at the base of the tower. That calculation, based on the existing antennas, gives a result of 15.23% of the General Public MPE, with the AT&T antennas emitting 15.23% of the General Public MPE on the ground, using the modeling predictions used by Connecticut Siting Council.
4. In either case, the site is compliant with FCC guidelines. If you have any questions regarding this site, the compliance report, please contact me at 719-434-0700 or dcotton@sitesafe.com.



David C. Cotton, Jr.
Licensed Professional Engineer (Electrical)
State of Connecticut, PEN.0027481
Date: 2014-May-07

Director, RF Compliance



Attachment 1

RF EMISSIONS COMPLIANCE REPORT

Smartlink LLC on behalf of AT&T Mobility, LLC

**AT&T Mobility, LLC Site FA: 10035021
AT&T Mobility, LLC Site ID: CT1050
AT&T Mobility, LLC USID: 140501
AT&T Mobility, LLC Site Name: Pomfret
82 Tyrone Road
Pomfret, CT
5/6/2014**

Report Status:

AT&T Mobility, LLC Is Compliant

Prepared By:

Sitesafe, Inc.

200 North Glebe Road, Suite 1000

Arlington, VA 22203

Voice 703-276-1100
Fax 703-276-1169

Engineering Statement in Re:
Electromagnetic Energy Analysis
AT&T Mobility, LLC
Pomfret, CT

My signature on the cover of this document indicates:

That I am registered as a Professional Engineer in the jurisdiction indicated; and

That I have extensive professional experience in the wireless communications engineering industry; and

That I am an employee of Sitesafe, Inc. in Arlington, Virginia; and

That I am thoroughly familiar with the Rules and Regulations of the Federal Communications Commission ("the FCC" and "the FCC Rules") both in general and specifically as they apply to the FCC's Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields; and

That the technical information serving as the basis for this report was supplied by AT&T Mobility, LLC (See attached Site Summary and Carrier documents), and that AT&T Mobility, LLC's installations involve communications equipment, antennas and associated technical equipment at a location referred to as the "Pomfret" ("the site"); and

That AT&T Mobility, LLC proposes to operate at the site with transmit antennas listed in the carrier summary and with a maximum effective radiated power as specified by AT&T Mobility, LLC and shown on the worksheet, and that worst-case 100% duty cycle have been assumed; and

That this analysis has been performed with the assumption that the ground immediately surrounding the tower is primarily flat or falling; and

That at this time, the FCC requires that certain licensees address specific levels of radio-frequency energy to which workers or members of the public might possibly be exposed (at §1.1307(b) of the FCC Rules); and

That such consideration of possible exposure of humans to radio-frequency radiation must utilize the standards set by the FCC, which is the Federal Agency having jurisdiction over communications facilities; and

That the FCC rules define two tiers of permissible exposure guidelines: 1) "uncontrolled environments," defined as situations in which persons may not be aware of (the "general public"), or may not be able to control their exposure to a transmission facility; and (2) "controlled environments," which defines situations in which persons are aware of their potential for exposure (industry personnel); and

That this statement specifically addresses the uncontrolled environment (which is more conservative than the controlled environment) and the limit set forth in the FCC rules for licensees of AT&T Mobility, LLC's operating frequency as shown on the attached antenna worksheet; and

That when applying the uncontrolled environment standards, the predicted Maximum Power Density at two meters above ground level from the proposed AT&T Mobility, LLC operation is no more than 0.585% of the maximum in any accessible area on the ground and

That it is understood per FCC Guidelines and OET65 Appendix A, that regardless of the existent radio-frequency environment, only those licenses whose contributions exceed five percent of the exposure limit pertinent to their operation(s) bear any responsibility for bringing any non-compliant area(s) into compliance; and

That when applying the uncontrolled environment standards, the cumulative predicted energy density from the proposed operation is no more than 0.585% of the maximum in any accessible area up to two meters above the ground per OET-65; and

That the calculations provided in this report are based on data provided by the client and antenna pattern data supplied by the antenna manufacturer, in accordance with FCC guidelines listed in OET-65. Horizontal and vertical antenna patterns are combined for modeling purposes to accurately reflect the energy two meters above ground level where on-axis energy refers to maximum energy two meters above the ground along the azimuth of the antenna and where area energy refers to the maximum energy anywhere two meters above the ground regardless of the antenna azimuth, accounting for cumulative energy from multiple antennas for the carrier and frequency range indicated; and

That the Occupational Safety and Health Administration has policies in place which address worker safety in and around communications sites, thus individual companies will be responsible for their employees' training regarding Radio Frequency Safety.

In summary, it is stated here that the proposed operation at the site would not result in exposure of the Public to excessive levels of radio-frequency energy as defined in the FCC Rules and Regulations, specifically 47 CFR 1.1307 and that AT&T Mobility, LLC's proposed operation is completely compliant.

Finally, it is stated that access to the tower should be restricted to communication industry professionals, and approved contractor personnel trained in radio-frequency safety; and that the instant analysis addresses exposure levels at two meters above ground level and does not address exposure levels on the tower, or in the immediate proximity of the antennas.

Note: Sitesafe has used data obtained from the "Connecticut Siting Council" to create this report. The manufacturer antenna patterns for AT&T Mobility, LLC were used to determine the RF emissions from the AT&T Mobility, LLC antennas. Sitesafe has also referenced the AT&T Mobility, LLC construction diagram for this site. The AT&T Mobility, LLC construction diagram references that RRU (Remote Radio Units) will be installed at the site with the existing antennas.

The following documents below were the primary sources of data used to create this report. The primary document was the "Connecticut Siting Council" document. The AT&T Mobility, LLC construction diagram was referenced when appropriate.

Connecticut Siting Council: AlphaExMPowDens 4-16-14

AT&T Mobility, LLC Construction Diagram: 10035021.AE201.140501 (CT1050) Dewberry Rev 1

^[1] This Power Density information was taken from the Connecticut Siting Council database dated April 16, 2014.

^[2] This Power Density information is based on worse case assumptions from AT&T's radio frequency engineers.

EXISTING ANTENNA SCHEDULE			
SECTOR	MAKE	MODEL#	TYPE / HEIGHT
ALPHA	POWERWAVE	7770	55x11x5
	POWERWAVE	7770	55x11x5
	ANDREWS	58H-105650	98.4x11.9x7.1
BETA	POWERWAVE	7770	55x11x5
	POWERWAVE	7770	55x11x5
	KVA	AM-X-CD-17-65-0-T	66.3x6.7x5.0
GAMMA	POWERWAVE	7770	55x11x5
	POWERWAVE	7770	55x11x5
	KVA	AM-X-CD-17-65-0-T	66.3x6.7x5.0

PROPOSED ANTENNA SCHEDULE			
SECTOR	MAKE	MODEL#	TYPE / HEIGHT
ALPHA	POWERWAVE	7770	55x11x5
	POWERWAVE	7770	55x11x5
	ANDREWS	58H-105650	98.4x11.9x7.1
BETA	POWERWAVE	7770	55x11x5
	POWERWAVE	7770	55x11x5
	KVA	AM-X-CD-17-65-0-T	66.3x6.7x5.0
GAMMA	POWERWAVE	7770	55x11x5
	POWERWAVE	7770	55x11x5
	KVA	AM-X-CD-17-65-0-T	66.3x6.7x5.0

PROPOSED RRUS SCHEDULE			
SECTOR	MAKE	MODEL#	TYPE / HEIGHT
ALPHA	ERICSSON	RRUS-11	19.7x17.0x7.2
	ERICSSON	RRUS-11	19.7x17.0x7.2
BETA	ERICSSON	RRUS-11	19.7x17.0x7.2
	ERICSSON	RRUS-11	19.7x17.0x7.2
GAMMA	ERICSSON	RRUS-11	19.7x17.0x7.2
	ERICSSON	RRUS-11	19.7x17.0x7.2

**AT&T Mobility, LLC
Pomfret
Site Summary**

Carrier	Area Maximum Percentage MPE
AT&T Mobility, LLC	0.194 %
AT&T Mobility, LLC	0.21 %
AT&T Mobility, LLC	0.18 %
Composite Site MPE:	0.585 %

Pomfret - 82 Tyrone Road

Power Density Calculations

Control Number	Site	Carrier	#Channels	ERP/Ch	Ant Ht	Power Density (mW/c)	MHz	S	%MPE	Site Total
EM-CING-112-130110	Pomfret - 82 Tyrone Road	AT&T UMTS	2	565	152	0.0176	880	0.5867	3.00%	
EM-CING-112-130110	Pomfret - 82 Tyrone Road	AT&T UMTS	2	875	152	0.0272	1900	1.0000	2.72%	
EM-CING-112-130110	Pomfret - 82 Tyrone Road	AT&T GSM	1	283	152	0.0044	880	0.5867	0.75%	
EM-CING-112-130110	Pomfret - 82 Tyrone Road	AT&T GSM	4	525	152	0.0327	1900	1.0000	3.27%	
EM-CING-112-130110	Pomfret - 82 Tyrone Road	AT&T LTE	1	1771	154	0.0269	734	0.4893	5.49%	15.23%



Pinnacle Wireless
Suite A Building 2
800 Marshall Phelps Road
Windsor, CT 06095



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(678) 467-7228
kclements@gpdgroup.com

GPD# 2012832.07
January 4, 2013

STRUCTURAL ANALYSIS REPORT WITH MODIFICATION DESIGN

AT&T DESIGNATION: **Site USID:** 71304
 Site FA: 10035021
 Site Name: **POMFRET-TYRONE RD**
 AT&T Project: **MOD LTE 082712**

ANALYSIS CRITERIA: **Codes:** **TIA/EIA-222-F, 2003 IBC, ASCE 7-05 & 2005 CTBC**
 85-mph with 0" ice
 28-mph with 1" ice

SITE DATA: **82 Tyrone Rd, Pomfret, CT 06258, Windham County**
 Latitude 41° 53' 24.871" N, Longitude 71° 57' 20.199" W
 Market: New England
 150' Monopole

Lauren Groppi,

GPD is pleased to submit this Structural Analysis Report with Modification Design to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

Analysis Results

Tower Stress Level with Proposed Equipment:	95.4%	Pass
Foundation Ratio with Proposed Equipment:	76.8%	Pass

Note: In order for this analysis results to be valid for the proposed, existing, and reserved loading in Appendix A the modifications referenced in the design drawings by GPD (Project #: 2012832.07, dated 1/4/2012) must be installed.

We at GPD appreciate the opportunity of providing our continuing professional services to you and Pinnacle Wireless. If you have any questions or need further assistance on this or any other projects please do not hesitate to call.

Respectfully submitted,

John N. Kabak, P.E.
Connecticut #: 28336



SUMMARY & RESULTS

The purpose of this analysis was to verify whether the existing modified structure is capable of carrying the proposed loading configuration as specified by AT&T Mobility to Pinnacle Wireless. This report was commissioned by Ms. Lauren Groppi of Pinnacle Wireless.

All proposed coax shall be internal to the monopole in order for the analysis results to be valid.

The proposed modifications by GPD (Project #: 2012832.07, dated 1/4/2012), consist of adding flat plate reinforcement from 0' – 130.3', installing bridge stiffeners at 110', adding anchor rods to the base and extending the existing pad foundation, and have been considered in this analysis. See Appendix H for the modification drawings.

TOWER SUMMARY AND RESULTS

Member	Capacity	Results
Monopole	95.4%	Pass
Anchor Rods	89.6%	Pass
Base Plate	74.6%	Pass
Flange Bolts	30.7%	Pass
Flange Plates	68.4%	Pass
Foundation	76.8%	Pass

ANALYSIS METHOD

TNX Tower (Version 6.0.4.0), a commercially available software program, was used to create a three-dimensional model of the tower and calculate primary member stresses for various dead, live, wind, and ice load cases. Selected output from the analysis is included in Appendix B. The following table details the information provided to complete this structural analysis. This analysis is solely based on this information and is being completed without the benefit of a detailed site visit.

DOCUMENTS PROVIDED

Document	Remarks	Source
Equipment Modification Form	AT&T Internal Loading Document, uploaded 8/27/12	Siterra
Construction Drawings	Not Provided	N/A
Tower Design	Not Provided	N/A
Foundation Design	Not Provided	N/A
Modification Drawings	GPD Project #: 2012832.07, dated 1/4/12	GPD
Geotechnical Report	Dr. Clarence Welti, dated 5/15/09	Siterra
Previous Structural Analysis	GPD Project #: 2009013.07, dated 6/2/09	Siterra
Tower Mapping	GPD and Northeast Towers Inc, dated 12/3/08	Siterra

ASSUMPTIONS

This structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analyzing the tower only.
5. The soil parameters are as per data supplied or as assumed and stated in the calculations.
6. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
7. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
8. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
9. All prior structural modifications are assumed to be as per data supplied/available and to have been properly installed.
10. Loading interpreted from photos is accurate to $\pm 5'$ AGL, antenna size accurate to ± 3.3 sf, and coax equal to the number of existing antennas without reserve.
11. All existing loading was obtained from the previous analysis by GPD Job #: 2009013.07, dated 6/2/09, site photos, the provided equipment modification form and is assumed to be accurate.
12. The existing AT&T loading elevation found in the previous analysis by GPD Job #: 2009013.07, dated 6/2/09 was found to vary from the EMF and site photos. The existing AT&T loading elevation was based on the site photos.
13. The proposed modifications by GPD (Project #: 2012832.07, dated 1/4/2012), consist of adding flat plate reinforcement from 0' – 130.3', installing bridge stiffeners at 110', adding anchor rods to the base and extending the existing pad foundation, and have been considered in this analysis. See Appendix H for the modification drawings.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD Group should be allowed to review any new information to determine its effect on the structural integrity of the tower.

DISCLAIMER OF WARRANTIES

GPD GROUP has not performed a site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD GROUP in connection with this Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. All tower components have been assumed to only resist dead loads when no other loads are applied. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

GPD GROUP does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD GROUP provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the feasibility of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD GROUP, but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

GPD GROUP makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD GROUP will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD GROUP pursuant to this report will be limited to the total fee received for preparation of this report.

APPENDIX A

Tower Analysis Summary Form

APPENDIX B

tnxTower Output File

tnxTower GPD 520 South Main Street, Suite 2531 Akron, OH 44311 Phone: 330.572.2100 FAX: 330.572.2101	Job 71304 POMFRET-TYRONE RD	Page 1 of 4
	Project 2012832.07	Date 18:20:26 01/04/13
	Client Pinnacle Wireless	Designed by jfields

Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Windham County, Connecticut.

Basic wind speed of 85 mph.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 28 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.333.

Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	C _{AA}		
						ft ² /ft	plf	
5/8" Step Bolts	A	No	CaAa (Out Of Face)	150.00 - 8.00	1	No Ice	0.04	1.00
						1/2" Ice	0.14	1.56
						1" Ice	0.24	2.73
						2" Ice	0.44	6.91
						4" Ice	0.84	22.58
Safety Line 3/8	A	No	CaAa (Out Of Face)	150.00 - 8.00	1	No Ice	0.04	0.22
						1/2" Ice	0.14	0.75
						1" Ice	0.24	1.28
						2" Ice	0.44	2.34
						4" Ice	0.84	4.46
LDF6-50A (1-1/4 FOAM)	A	No	Inside Pole	150.00 - 8.00	12	No Ice	0.00	0.66
						1/2" Ice	0.00	0.66
						1" Ice	0.00	0.66
						2" Ice	0.00	0.66
						4" Ice	0.00	0.66
2" Flex Conduit	A	No	Inside Pole	150.00 - 8.00	1	No Ice	0.00	0.32
						1/2" Ice	0.00	0.32
						1" Ice	0.00	0.32
						2" Ice	0.00	0.32
						4" Ice	0.00	0.32
1/2" Fiber Cable	A	No	Inside Pole	150.00 - 8.00	1	No Ice	0.00	0.15
						1/2" Ice	0.00	0.15
						1" Ice	0.00	0.15
						2" Ice	0.00	0.15
						4" Ice	0.00	0.15
3/4" DC Power Line	A	No	Inside Pole	150.00 - 8.00	2	No Ice	0.00	0.33
						1/2" Ice	0.00	0.33
						1" Ice	0.00	0.33
						2" Ice	0.00	0.33
						4" Ice	0.00	0.33
LDF4P-50A (1/2 FOAM)	B	No	Inside Pole	100.00 - 8.00	1	No Ice	0.00	0.15
						1/2" Ice	0.00	0.15
						1" Ice	0.00	0.15
						2" Ice	0.00	0.15
						4" Ice	0.00	0.15

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	Client Pinnacle Wireless	Designed by jfields

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		C _{AA} ft ² /ft	Weight plf
5" x 1-1/4" Mod Plate	A	No	CaAa (Out Of Face)	130.25 - 0.75	2	No Ice	0.00	0.00
						1/2" Ice	0.00	1.30
						1" Ice	0.00	2.60
						2" Ice	0.00	3.90
						4" Ice	0.00	5.20
5" x 1-1/4" Mod Plate	A	No	CaAa (Out Of Face)	130.25 - 0.75	1	No Ice	0.21	0.00
						1/2" Ice	0.32	1.30
						1" Ice	0.43	2.60
						2" Ice	0.65	3.90
						4" Ice	1.10	5.20
5" x 1-1/4" Mod Plate	A	No	CaAa (Out Of Face)	130.25 - 0.75	1	No Ice	0.21	0.00
						1/2" Ice	0.32	1.30
						1" Ice	0.43	2.60
						2" Ice	0.65	3.90
						4" Ice	1.10	5.20

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft		C _{AA} Front ft ²	C _{AA} Side ft ²	Weight lb
10'-8" Central Platform w/ 42" tower extension	C	None		0.0000	152.00	No Ice	43.32	43.32	2500.00
						1/2" Ice	46.28	46.28	3250.00
						1" Ice	49.24	49.24	4000.00
						2" Ice	55.16	55.16	5500.00
						4" Ice	67.00	67.00	8500.00
(2) 7770.00 w/Mount Pipe	A	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	No Ice	5.88	4.10	61.54
						1/2" Ice	6.31	4.73	107.08
						1" Ice	6.75	5.37	160.39
						2" Ice	7.66	6.70	289.46
						4" Ice	9.58	9.87	654.29
(2) 7770.00 w/Mount Pipe	B	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	No Ice	5.88	4.10	61.54
						1/2" Ice	6.31	4.73	107.08
						1" Ice	6.75	5.37	160.39
						2" Ice	7.66	6.70	289.46
						4" Ice	9.58	9.87	654.29
(2) 7770.00 w/Mount Pipe	C	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	No Ice	5.88	4.10	61.54
						1/2" Ice	6.31	4.73	107.08
						1" Ice	6.75	5.37	160.39
						2" Ice	7.66	6.70	289.46
						4" Ice	9.58	9.87	654.29
SBNH-1D6565C w/ Mount Pipe	A	From Centroid-Le g	4.00 0.00 2.00	0.0000	152.00	No Ice	11.45	9.12	82.70
						1/2" Ice	12.06	10.21	162.03
						1" Ice	12.69	11.18	254.15
						2" Ice	14.03	13.17	469.01
						4" Ice	17.05	17.35	1051.99
AM-X-CD-17-65-00T w/ Mount Pipe	B	From Centroid-Le g	4.00 0.00 2.00	0.0000	152.00	No Ice	11.31	9.10	105.82
						1/2" Ice	11.93	10.52	189.52
						1" Ice	12.55	11.60	285.59
						2" Ice	13.88	13.80	512.39
						4" Ice	16.88	18.41	1127.38
AM-X-CD-17-65-00T w/ Mount Pipe	C	From Centroid-Le g	4.00 0.00 2.00	0.0000	152.00	No Ice	11.31	9.10	105.82
						1/2" Ice	11.93	10.52	189.52
						1" Ice	12.55	11.60	285.59
						2" Ice	13.88	13.80	512.39

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment °	Placement ft	C _A A _A Front ft ²	C _A A _S Side ft ²	Weight lb
			Horz ft	Lateral Vert ft					
(2) LGP21401	A	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	16.88	18.41	1127.38
						No Ice	0.00	0.23	10.00
						1/2" Ice	0.00	0.31	21.26
						1" Ice	0.00	0.40	30.32
						2" Ice	0.00	0.61	54.89
(2) LGP21401	B	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	0.00	1.12	135.29
						No Ice	0.00	0.23	10.00
						1/2" Ice	0.00	0.31	21.26
						1" Ice	0.00	0.40	30.32
						2" Ice	0.00	0.61	54.89
(2) LGP21401	C	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	0.00	1.12	135.29
						No Ice	0.00	0.23	10.00
						1/2" Ice	0.00	0.31	21.26
						1" Ice	0.00	0.40	30.32
						2" Ice	0.00	0.61	54.89
(2) LGP21903 Diplexer	A	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	0.00	1.12	135.29
						No Ice	0.00	0.18	10.00
						1/2" Ice	0.00	0.25	13.44
						1" Ice	0.00	0.32	16.93
						2" Ice	0.00	0.49	27.95
(2) LGP21903 Diplexer	B	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	0.00	0.94	71.54
						No Ice	0.00	0.18	10.00
						1/2" Ice	0.00	0.25	13.44
						1" Ice	0.00	0.32	16.93
						2" Ice	0.00	0.49	27.95
(2) LGP21903 Diplexer	C	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	0.00	0.94	71.54
						No Ice	0.00	0.18	10.00
						1/2" Ice	0.00	0.25	13.44
						1" Ice	0.00	0.32	16.93
						2" Ice	0.00	0.49	27.95
(2) RBS 6601	A	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	0.00	0.94	71.54
						No Ice	0.55	0.40	22.00
						1/2" Ice	0.70	0.52	34.88
						1" Ice	0.86	0.64	50.27
						2" Ice	1.19	0.91	89.38
(2) RBS 6601	B	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	1.97	1.55	206.33
						No Ice	0.55	0.40	22.00
						1/2" Ice	0.70	0.52	34.88
						1" Ice	0.86	0.64	50.27
						2" Ice	1.19	0.91	89.38
(2) RBS 6601	C	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	1.97	1.55	206.33
						No Ice	0.55	0.40	22.00
						1/2" Ice	0.70	0.52	34.88
						1" Ice	0.86	0.64	50.27
						2" Ice	1.19	0.91	89.38
DC6-48-60-18-8F Surge Suppression Unit	C	From Centroid-Le g	4.00 0.00 0.00	0.0000	152.00	4" Ice	1.97	1.55	206.33
						No Ice	1.47	1.47	32.80
						1/2" Ice	1.67	1.67	50.52
						1" Ice	1.88	1.88	70.72
						2" Ice	2.33	2.33	119.24
4' Dipole	B	From Leg	3.00 0.00 0.00	0.0000	107.00	4" Ice	3.38	3.38	252.92
						No Ice	0.79	0.79	10.00
						1/2" Ice	1.03	1.03	16.34
						1" Ice	1.28	1.28	25.48
						2" Ice	1.81	1.81	52.76
4' Dipole	B	From Leg	3.00	0.0000	97.00	4" Ice	3.11	3.11	147.65
						No Ice	0.79	0.79	10.00

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _A A _A Front	C _A A _A Side	Weight
			Horz Lateral	Vert					
			ft	ft	°	ft	ft ²	ft ²	lb
			0.00			1/2" Ice	1.03	1.03	16.34
			0.00			1" Ice	1.28	1.28	25.48
						2" Ice	1.81	1.81	52.76
						4" Ice	3.11	3.11	147.65

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
152.00	10'-8" Central Platform w/ 42" tower extension	33	44.523	2.9349	0.0032	7674
107.00	4' Dipole	33	22.218	2.0292	0.0002	3297
97.00	4' Dipole	33	18.203	1.8379	0.0002	3183

Section Capacity Table

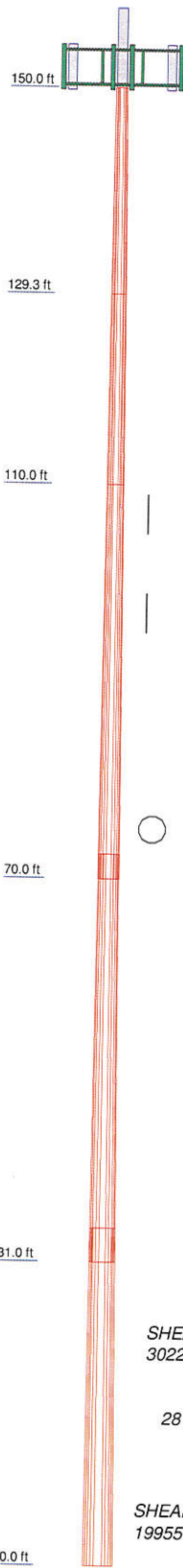
Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	SF*P _{allow} lb	% Capacity	Pass Fail
L1	150 - 129.25	Pole	TP17.4673x14.5x0.1875	1	-3473.10	542361.69	78.5	Pass
L2	129.25 - 110	Pole	TP20.22x17.4673x0.47	2	-5418.02	*	84.6*	Pass
L3	110 - 70	Pole	TP25.94x20.22x0.534	3	-10791.30	*	89.5*	Pass
L4	70 - 31	Pole	TP31.52x24.5145x0.599	4	-18678.40	*	87.7*	Pass
L5	31 - 0	Pole	TP36x29.7312x0.622	5	-26914.60	*	95.4*	Pass
Summary								
Pole (L5)							95.4*	Pass
RATING =							95.4*	Pass

*See Appendix E for the modification calculations.

APPENDIX C

Tower Elevation Drawings

Section	Length (ft)	Number of Sides	Thickness (in)	Socket Length (ft)	Top Dia (in)	Bot Dia (in)	Grade	Weight (lb)
1	20.75	12	0.1875					673.4
2	19.25	12	0.4700					1821.4
3	40.00	12	0.5340	2.50	20.2200	25.9400	A572-65	5276.7
4	41.50	12	0.5990	3.50	24.5145	31.5200	A572-65	7468.0
5	34.50	12	0.6220	29.7312	36.0000			7581.3
								22820.9



DESIGNED APPURTENANCE LOADING

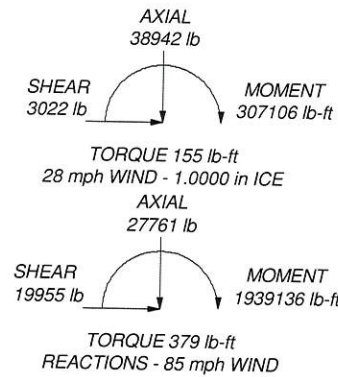
TYPE	ELEVATION	TYPE	ELEVATION
10'-8" Central Platform w/ 42" tower extension	152	(2) LGP21903 Diplexer	152
(2) 7770.00 w/Mount Pipe	152	(2) LGP21903 Diplexer	152
(2) 7770.00 w/Mount Pipe	152	(2) LGP21903 Diplexer	152
(2) 7770.00 w/Mount Pipe	152	(2) RBS 6601	152
SBNH-1D6565C w/ Mount Pipe	152	(2) RBS 6601	152
AM-X-CD-17-65-00T w/ Mount Pipe	152	(2) RBS 6601	152
AM-X-CD-17-65-00T w/ Mount Pipe	152	DC6-48-60-18-8F Surge Suppression Unit	152
(2) LGP21401	152	4' Dipole	107
(2) LGP21401	152	4' Dipole	97
(2) LGP21401	152		


MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

TOWER DESIGN NOTES

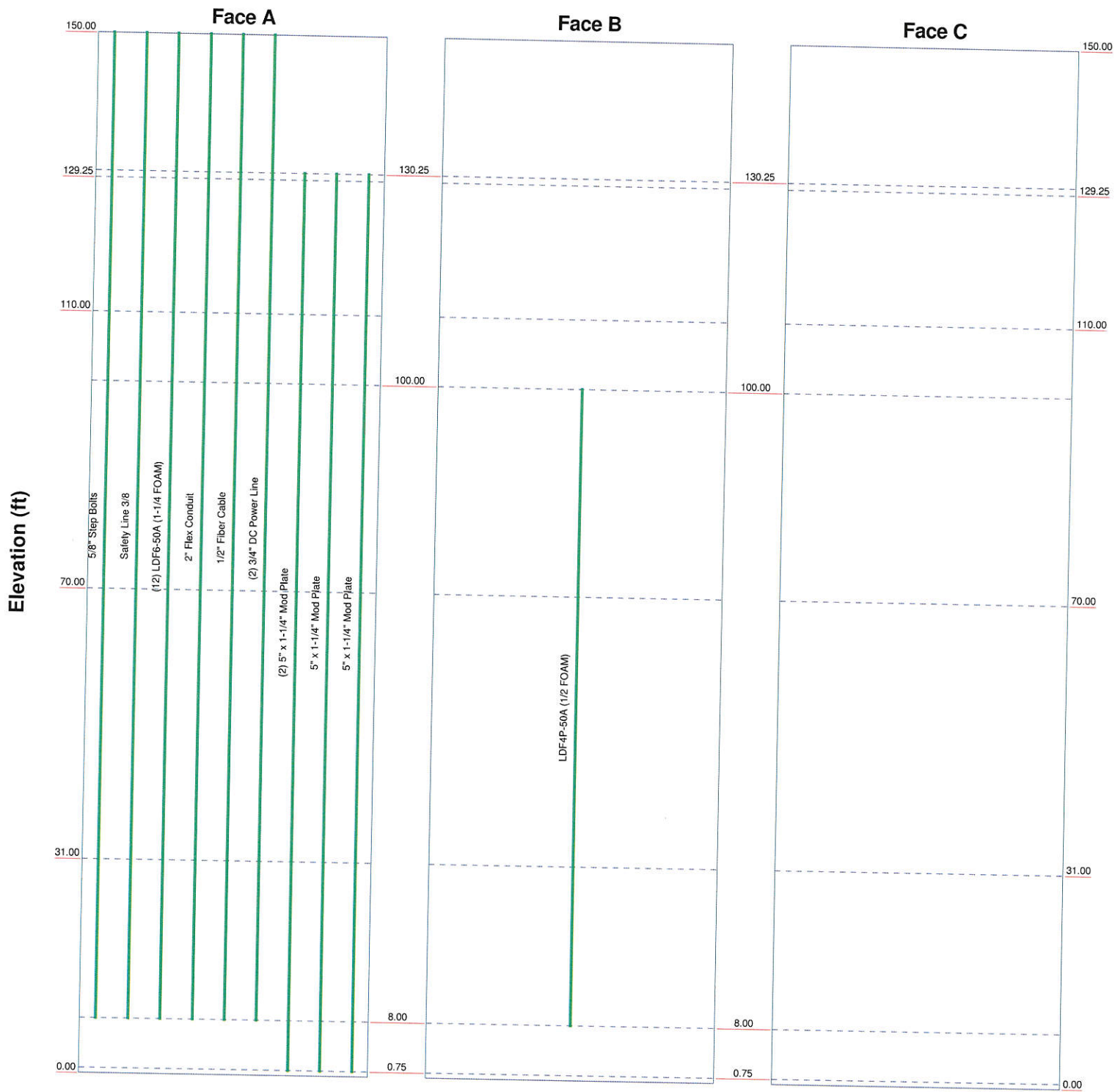
1. Tower is located in Windham County, Connecticut.
2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 28 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 50 mph wind.
5. TOWER RATING: 78.5%




 GPD Consulting Engineers 520 South Main Street, Suite 2531 Akron, OH 44311 Phone: 330.572.2100 FAX: 330.572.2101	Job: 71304 POMFRET-TYRONE RD
	Project: 2012832.07
	Client: Pinnacle Wireless
	Code: TIA/EIA-222-F
	Path: C:\Users\jfields\Desktop\Drop\TNX\2012832.07\71304.dwg
Drawn by: jfields	App'd:
Date: 01/04/13	Scale: NTS
	Dwg No. E-1

Feedline Distribution Chart 0' - 150'

— Round
 — Flat
 — App In Face
 — App Out Face
 — Truss Leg



 GPD Consulting Engineers	520 South Main Street, Suite 2531		Akron, OH 44311		Phone: 330.572.2100		FAX: 330.572.2101	
	Project: 2012832.07		Client: Pinnacle Wireless		Drawn by: jfields		App'd:	
	Code: TIA/EIA-222-F		Date: 01/04/13		Scale: NTS		Dwg No: E-7	
	Path: C:\Users\jfields\Desktop\Drop\TNX\2012832.07\71304.dwg		Job: 71304 POMFRET-TYRONE RD		Date: 01/04/13		Scale: NTS	
	Path: C:\Users\jfields\Desktop\Drop\TNX\2012832.07\71304.dwg		Job: 71304 POMFRET-TYRONE RD		Date: 01/04/13		Scale: NTS	

APPENDIX D

Base Plate & Anchor Rod Calculations



Anchor Rod and Base Plate Stresses
71304 POMFRET-TYRONE RD
2012832.07

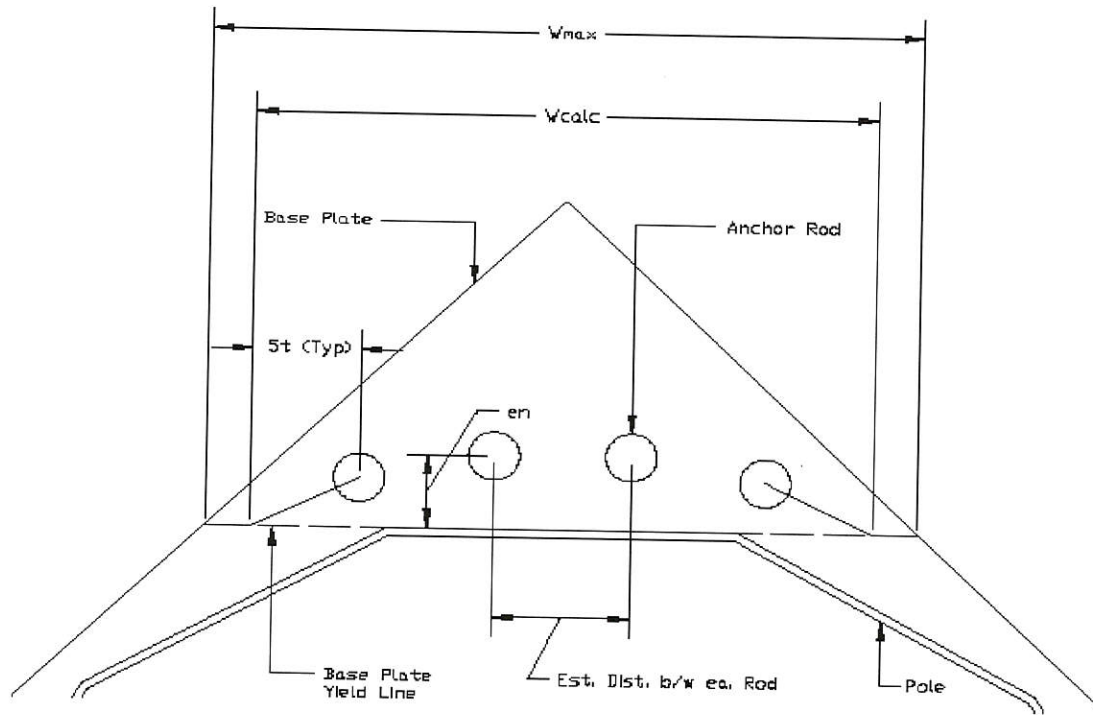
*Overturning Moment =	1176.39	k*ft
Axial Force =	19.22	k
Shear Force =	19.96	k

Acceptable Stress Ratio =	100.0%
---------------------------	--------

*Above reactions have been adjusted due to consideration of modifications. See attached hand calculations for determination of anchor rod forces in the analysis.

Anchor Rods	
Pole Diameter =	36 in
Number of Rods =	8
Type =	Upset Rod
Rod Yield Strength (Fy) =	75 ksi
ASIF =	1.333
Rod Circle =	44 in
Rod Diameter =	2.25 in
Net Tensile Area =	3.25 in ²
Max Tension on Rod =	157.81 kips
Max Compression on Rod =	162.61 kips
Allow. Rod Force =	195.00 kips
Anchor Rod Capacity =	80.9% OK

Base Plate	
Plate Strength (Fy) =	60 ksi
Plate Thickness =	2.5 in
Plate Width =	44 in
Est. Dist. b/w ea. Rod =	6 in
W _{calc} =	31.000 in
W _{max} =	26.225 in
w =	26.23 in
S =	27.32 in ³
fb =	44.76 ksi
Fb =	60 ksi
Base Plate Capacity =	74.6% OK





GPD GROUP

Engineers • Architects • Planners

Job #: 2012832.07

Sheet No. 1 Of 1

Calculated By: JDF Date: 1/4/2013

Checked By: _____ Date: _____

MODIFIED ANCHOR ROD CALCULATIONS

Moment from RISA (M) = 1939.14 kip-ft
 Axial from RISA (P) = 27.76 kip
 Shear from RISA (V) = 19.96 kip

Code: TIA/EIA-222-F
 ASIF = 1.33
 Allowable Stress Ratio = 105%

Inner Bolt Diameter = 2.25 in
 Number Inner Bolts (N_{inner}) = 8
 Inner Bolt Area (A_{inner}) = 3.98 in²
 Inner Bolt MOI ($I_{o,inner}$) = 1.26 in⁴

Inner Bolt Circle (BC_{inner}) = 44 in
 Total Area ($A_{tot,in}$) = 31.81 in²
 Percent Total Area (η_{in}) = 69.2%

Axial, Inner Bolts ($P * \eta_{in}$) = 19.22 kips
 Shear, Inner Bolts ($P * \eta_{in}$) = 19.96 kips

Outer Bolt Diameter = 1.5 in
 Number Outer Bolts (N_{outer}) = 8
 Outer Bolt Area (A_{outer}) = 1.77 in²
 Outer Bolt MOI ($I_{o,outer}$) = 0.25 in⁴

Outer Bolt Circle (BC_{outer}) = 53.17 in
 Total Area ($A_{tot,out}$) = 14.14 in²
 Percent Total Area (η_{out}) = 30.8%

Axial, Outer Bolts ($P * \eta_{out}$) = 8.54 kips

$$I_{inner} = 7707.75 \text{ in.}^4$$

$$I_{outer} = 4997.80 \text{ in.}^4$$

$$I_{tot} = \frac{12705.55 \text{ in.}^4}{(N_{inner} * A_{inner} * BC_{inner}^2 / 8 + N_{inner} * I_{o,inner}) + (N_{outer} * A_{outer} * BC_{outer}^2 / 8 + C (I_{inner} + I_{outer}))}$$

$$F_{inner} = 162.61 \text{ kips}$$

$$F_{outer} = 87.11 \text{ kips}$$

Rnt.outer / Ω = 72.89 kips

Modified Anchor Rod Rating
 % = 89.6% OK

APPENDIX E

Modification Calculations



Reinforced Monopole Analysis
71304 POMFRET-TYRONE RD
2012832.07

Code = TIA/EIA-222-F
 AISF = 1.333
 Max. Stress Ratio = 1.05
 # of Sides = 12

Shape	Quantity	Section	Geometry				Reactions				Output		Capacities			
			Elevation (ft)	Pole Flat-Flat (ft)	Wall L (in)	Fy (ksi)	K	Conn. Spacing (in)	Moment (k-ft)	Axial (k)	Shear (k)	Torsion (k-ft)	Equivalent L (in)	Pole	Reinforcement	Pass/Fail
Plate 3x1.25	4	L2	110	20.22	0.1875	65	0.8	18	305.86	5.42	9.2	0.26	0.470	50.0%	84.6%	Pass
Plate 4x1.25	4	L3	70	25.94	0.25	65	0.8	18	726.65	10.79	13.25	0.03	0.534	63.0%	89.5%	Pass
Plate 5x1.25	4	L4	31	31.52	0.3125	65	0.8	18	1301.94	18.68	16.97	0.03	0.599	68.0%	87.7%	Pass
Plate 5x1.25	4	L5	0	36	0.375	65	0.8	18	1939.14	26.91	17.98	0.38	0.622	74.4%	95.4%	Pass

APPENDIX F

Flange Plate & Flange Bolt Calculations



Existing Flange Connection @
71304 POMFRET-TYRONE RD
2012832.07

110'

*O.T. Moment =	82.3267 k*ft
Axial =	2.09 kips
Shear =	9.20 kips

Acceptable Stress Ratio	= 105.0%
-------------------------	----------

*Above reactions have been adjusted due to consideration of modifications. See attached hand calculations for determination of flange bolt forces used in the analysis.

Flange Bolts	
# Bolts =	12
Bolt Type =	A325
F_t =	44 ksi
ASIF =	1.333
Bolt Circle =	23 in
Bolt Diameter =	1 in

Tension & Shear (ASD, Section J3.5)	
F_v =	21 ksi
Nominal Area =	0.79 in ²
f_v =	0.98 ksi
Applied Shear =	0.77 kips
Allowable Shear =	21.99 kips
$F_t^2 - 4.39(f_v^2)^{1/2}$ =	43.95 ksi
Allowable Bolt Stress =	58.60325 ksi
B =	46.03 kips

Prying Action Check

N/A, top flange thickness > tc

Max Comp. on Bolt =	14.48 kips
Max Tension on Bolt =	14.13 kips
Shear Capacity =	3.5%
Tensile Capacity =	30.7%
Bolt Capacity =	30.7% OK

Pole Information	
Shaft Diam. (Upper) =	20.22 in
Thickness (Upper) =	0.1875 in
# of Sides (Upper) =	12
F_y (Upper) =	65 ksi
Shaft Diam. (Lower) =	20.22 in
Thickness (Lower) =	0.25 in
# of Sides (Lower) =	12
F_y (Lower) =	65 ksi

Upper Flange Plate	
Location =	External
Plate Strength (F_y) =	60 ksi
Plate Thickness =	1 in
Outer Diameter =	26 in
wcalc =	10.96 in
wmax =	15.95 in
w =	10.96 in
S =	1.83 in ³
f_b =	15.29 ksi
F_b =	60 ksi
UP Capacity =	25.5% OK

Upper Stiffeners	
Configuration =	None

Lower Flange Plate	
Location =	External
Plate Strength (F_y) =	60 ksi
Plate Thickness =	1 in
Outer Diameter =	26 in
wcalc =	10.96 in
wmax =	15.95 in
w =	10.96 in
S =	1.83 in ³
f_b =	15.29 ksi
F_b =	60 ksi
LP Capacity =	25.5% OK

Lower Stiffeners	
Configuration =	None



GPD GROUP
Engineers • Architects • Planners

Job #: 2012832.07
Sheet No. 1 Of 1

Calculated By: JDF Date: 1/4/2013
Checked By: AW Date: 1/4/2013

BOLT AND BRIDGE STIFFENER CALCULATIONS

@ 110'

Tower Type = **Monopole**
Acceptable Stress Ratio = **105.0%**
Code = **TIA/EIA-222-F**
ASIF = **1.33**

Moment from RISA (M) = **305.86 kip-ft**
Axial from RISA (P) = **5.42 kip**

Inner Bolt Diameter = **1 in**
Inner Bolt Area (A_{inner}) = **0.79 in²**
Inner Bolt MOI ($I_{o,inner}$) = **0.05 in⁴**
Number Inner Bolts (N_{inner}) = **12**

Inner Bolt Circle (BC_{inner}) = **23 in**
Total Area ($A_{tot,in}$) = **9.42 in²**
Percent Total Area (η_{in}) = **38.6%**

Axial, Inner Bolts ($P*\eta_{in}$) = **2.09 kips**

Bridge Stiffener Width = **3.00 in**
Bridge Stiffener Thickness = **1.25 in**
Bridge Stiffener Unbraced Length = **12.00 in**
Bridge Stiffener Area (A_{pl}) = **3.75 in²**
Bridge Stiffener Average MOI (I_x) = **1.65 in⁴**
Number Bridge Stiffeners (N_{pl}) = **4**

Bridge Stiffener Circle (BC_{pl}) = **30 in**
Total Area ($A_{tot,pl}$) = **15.00 in²**
Percent Total Area (η_{pl}) = **61.4%**

Axial, Bridge Stiffeners ($P*\eta_{pl}$) = **3.33 kips**

$I_{inner} = 623.80 \text{ in.}^4$
 $I_{outer} = 0.00 \text{ in.}^4$
 $I_{pl} = 1694.10 \text{ in.}^4$
 $I_{tot} = 2317.90 \text{ in.}^4$

$(N_{inner} * A_{inner} * BC_{inner}^2 / 8 + N_{inner} * I_{o,inner})$
 $(N_{outer} * A_{outer} * BC_{outer}^2 / 8 + N_{outer} * I_{o,outer})$
 $(N_{pl} * A_{pl} * BC_{pl}^2 / 8 + N_{pl} * I_{o,pl})$
 $(I_{inner} + I_{outer} + I_{pl})$

$P_{u,t,inner} = 14.13 \text{ kips}$
 $P_{u,t,pl} = 88.24 \text{ kips}$
 $P_{u,c,pl} = 89.90 \text{ kips}$
ASIF * Pnt.bolt / $\Omega = 46.03 \text{ kips}$
Bolt Rating = **30.7% OK**

$(M * (BC_{inner} / 2) * A_{inner}) / I_{total} - P * \eta_{in} / N_{inner}$
 $(M * (BC_{pl} / 2) * A_{pl}) / I_{total} - P * \eta_{pl} / N_{pl}$
 $(M * (BC_{pl} / 2) * A_{pl}) / I_{total} + P * \eta_{pl} / N_{pl}$

Number Bridge Stiffeners (N_{pl}) = **4**
 $f_y = 65 \text{ ksi}$
 $f_u = 80 \text{ ksi}$
Plate Width = **3.00 in**
Plate Thickness = **1.25 in**
Plate Unbraced Length = **12.00 in**
Plate Area (A_{pl}) = **3.75 in²**
Upper Pole Diameter = **20.22 in**
Flange Plate Diameter = **26.00 in**
Flange Plate to Bridge Stiffener Gap = **2.11 in**
Bridge Stiffener Circle (BC_{pl}) = **30.00 in**
Bridge Stiffener MOI (I_x) = **2.81 in⁴**
 $I_{pl} = 1694.10 \text{ in.}^4$
Axial Capacity Required = **89.90 kips**
Load Eccentricity, e = **6.50 in** (from weld to center of stiffener area)
Moment Capacity Required = **0.00 kip-in**
E = **29000 ksi**
K = **1.00**
 $r_{min} = 0.36$
 $KL/r_{min} = 33.255$
 $F_e = 258.81 \text{ ksi}$
 $F_{cr} = 58.51 \text{ ksi}$
 $P_{nc} / \Omega = 131.39 \text{ kips}$
 $P_{nt} / \Omega = 145.96 \text{ kips}$
S = **1.88 in³**
Z = **2.81 in³**
 $L_b d / t^2 = 23.04$
 $M_{NLTB} = \text{n/a}$
 $M_p = 182.81 \text{ kip-in}$
 $M_n / \Omega = 109.47 \text{ kip-in}$
Stiffener Rating = **68.4% OK**

Bridge Stiffener Welds **Analysis**
Bridge Stiffener Height = **27.00 in**
a value (from AISC Table 8-4) = **0.241**
C value (from AISC Table 8-4) = **3.31**
Fillet Size = **0.1875 in**
Weld Rating = **67.1% OK**

$(N_{pl} * A_{pl} * BC_{pl}^2 / 8 + N_{pl} * I_{o,pl})$
 $(M * (BC_{pl} / 2) * A_{pl}) / I_{total} + P * \eta_{pl} / N_{pl}$

APPENDIX G

Foundation Calculations



Mat Foundation Analysis
71304 POMFRET-TYRONE RD
2012832.07

General Info	
Code	TIA/EIA-222-F (ASD)
Bearing On	Soil
Foundation Type	Mono Pad
Pier Type	Square
Reinforcing Known	No
Max Capacity	1

Tower Reactions	
Moment, M	1939.14 k-ft
Axial, P	27.76 k
Shear, V	19.96 k

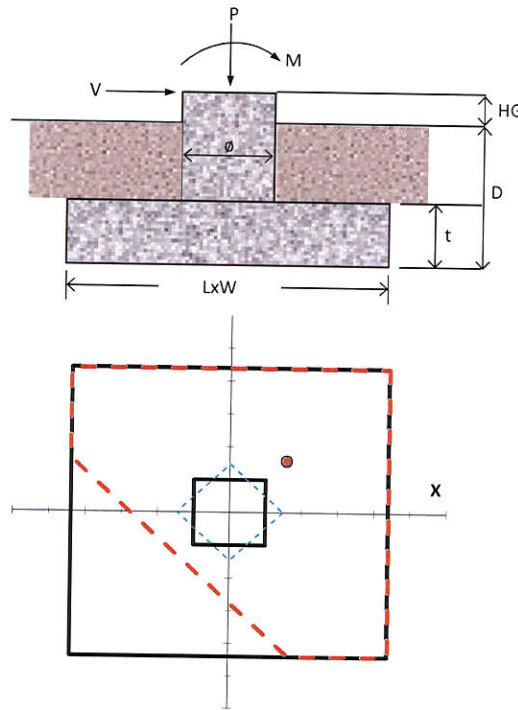
Pad & Pier Geometry	
Pier Width, ϕ	5 ft
Pad Length, L	22 ft
Pad Width, W	22 ft
Pad Thickness, t	3 ft
Depth, D	8 ft
Height Above Grade, HG	0.5 ft

Pad & Pier Reinforcing	
Rebar Fy	ksi
Concrete Fc'	ksi
Clear Cover	in
Reinforced Top & Bottom?	
Pad Reinforcing Size	
Pad Quantity Per Layer	
Pier Rebar Size	
Pier Quantity of Rebar	

Soil Properties	
Soil Type	Granular
Soil Unit Weight	120 pcf
Angle of Friction, ϕ	28 °
Bearing Type	Gross
Ultimate Bearing	12 ksf
Water Table Depth	1 ft
Frost Depth	4 ft

Bearing Summary			Load Case
Qxmax	1.86	ksf	1D+1W
Qymax	1.86	ksf	1D+1W
Qmax @ 45°	2.44	ksf	1D+1W
Q _{(all) Gross}	6.00	ksf	
Controlling Capacity	40.7%	Pass	

Overturning Summary (Required FS=1.5)			Load Case
FS(ot)x	1.95	≥1.5	1D+1W
FS(ot)y	1.95	≥1.5	1D+1W
Controlling Capacity	76.8%	Pass	



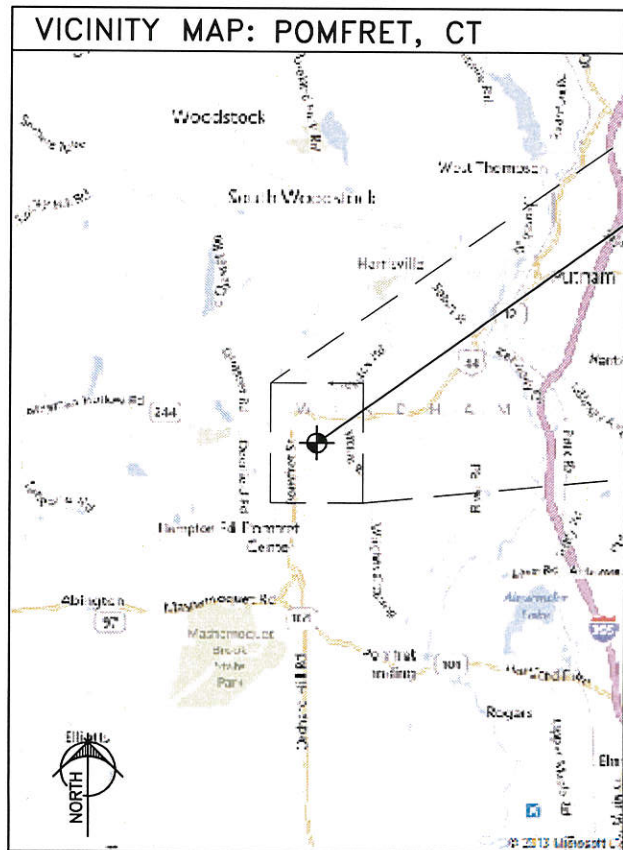
APPENDIX H

Modification Drawings

POMFRET-T'

USID #:

150' MON



GENERAL NOTES

1. THE FOLLOWING DRAWINGS REPRESENT MODIFICATIONS TO THE EXISTING TOWER. THE MODIFICATIONS ARE BASED ON GPD GROUP STRUCTURAL REPORT (PROJECT #: 2012801.71, DATED NOVEMBER 7, 2012). ALL MODIFICATIONS MUST BE INSTALLED TO BRING THE TOWER INTO CONFORMANCE WITH TIA/EIA-222-F, 2003 IBC, ASCE 7-05, AND 2005 CTBC.

2. THESE MODIFICATIONS HAVE BEEN DESIGNED IN ACCORDANCE WITH THE GOVERNING PROVISIONS OF TIA/EIA-222-F, 2003 IBC, ASCE 7-05, 2005 CTBC, AWS, AND AISC. MATERIALS AND SERVICES PROVIDED BY THE CONTRACTOR SHALL CONFORM TO THE ABOVE MENTIONED CODES AND THE CONTRACT SPECIFICATIONS.

3. ALL ORIGINAL TOWER INFORMATION WAS OBTAINED IN THE FORM OF A TOWER MAPPING BY GPD AND NORTHEAST TOWER INC. (DATED DECEMBER 3, 2008). CONTRACTOR SHALL OBTAIN AND BECOME FAMILIAR WITH THE REFERENCED TOWER DOCUMENTS.

4. THIS DESIGN ASSUMES THE TOWER AND FOUNDATIONS HAVE BEEN WELL MAINTAINED, IN GOOD CONDITION, AND ARE WITHOUT DEFECT. BENT MEMBERS, CORRODED MEMBERS, LOOSE BOLTS, CRACKED WELDS AND OTHER MEMBER DEFECTS HAVE NOT BEEN CONSIDERED. THE TOWER IS ASSUMED TO BE PLUMB AND THE SITE IS ASSUMED TO BE LEVEL. THIS DESIGN IS BEING PROVIDED WITHOUT THE BENEFIT OF A CONDITION ASSESSMENT BY GPD GROUP. CONTRACTOR SHALL COMMISSION A COMPLETE CONDITION ASSESSMENT PRIOR TO ORDERING ANY REINFORCING MATERIALS. CONTRACTOR SHALL SUPPLY CONDITION ASSESSMENT TO ENGINEER FOR REVIEW. SEE CONTRACTOR NOTES.

5. MANUFACTURER TOLERANCES, FIELD ADJUSTMENTS, INCORRECT STACKING, AND TEMPERATURE CAN CAUSE DIMENSIONAL DISCREPANCIES. CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS PRIOR TO ORDERING MATERIALS. ALL FIELD MEASUREMENTS MUST BE REPORTED TO ENGINEER.

6. ALL NEW STEEL SHALL BE HOT DIPPED GALVANIZED FOR FULL WEATHER PROTECTION. IN ADDITION ALL NEW STEEL SHALL BE PAINTED TO MATCH EXISTING STEEL. CONTRACTOR SHALL OBTAIN WRITTEN PERMISSION TO PROTECT STEEL BY ANY OTHER MEANS.

7. ALL EXISTING PAINTED/GALVANIZED SURFACES DAMAGED DURING REHAB INCLUDING AREAS UNDER STIFFENER PLATES SHALL BE WIRE BRUSHED CLEAN, REPAIRED BY COLD GALVANIZING BRUSH APPLIED PAINT (ZRC OR EQUAL), AND REPAINTED TO MATCH THE EXISTING FINISH (IF APPLICABLE).

8. CAULKING SHALL BE PROVIDED AROUND PERIMETER OF ANY AND ALL MODIFICATION MEMBERS TO ENSURE COMPLETE SEAL BETWEEN EXISTING STRUCTURE AND REINFORCING MEMBERS. SEALANT IS TO BE EXTERIOR GRADE, PAINTABLE SILICONE CAULKING AS MANUFACTURED BY DOW AND ACCEPTABLE TO GPD.

9. LOADINGS:

WIND LOADS:
FASTEST MILE WIND SPEED (PER: TIA/EIA-222-F, 2003 IBC, ASCE 7-05, & 2005 CTBC) 85 MPH
(WINDHAM COUNTY, CONNECTICUT)

ICE LOADS:
1" RADIAL BASE ICE
FASTEST MILE WIND SPEED (CONCURRENT W/ ICE) 28 MPH

10. STRUCTURAL STEEL:

SPECIFICATIONS
LATEST EDITION OF AISC

MATERIAL

PLATES	ASTM A572 (GR 65)
BRIDGE STIFFENERS	ASTM A572 (GR 65)
ONE SIDE BOLTS	AJAX 20MM (PC8.8) W/ HIGH STRENGTH SLEEVE (Fu=120KSI)
NUTS	ASTM A194-2H
WASHERS	ASTM F436
PIPE	ASTM A53-B (GR 42)
ANCHOR RODS	ASTM F1554 (GR 105)
ANCHOR ROD BRACKETS	ASTM A572 (GR 65)
HOT DIPPED GALVANIZING	ASTM A123
WELDS	E70XX
PAINT	NEW STEEL TO BE PAINTED TO MATCH EXISTING TOWER
EPOXY	HILTI HIT-RE 500-SD (ICC#: ESR-2322)

11. ALL MATERIAL UTILIZED FOR THIS PROJECT MUST BE NEW AND FREE OF ANY DEFECTS. ANY MATERIAL SUBSTITUTIONS, INCLUDING BUT NOT LIMITED TO ALTERED SIZES AND/OR STRENGTHS, MUST BE APPROVED BY THE OWNER AND ENGINEER IN WRITING.

12. ALL SUBSTITUTES PROPOSED BY THE CONTRACTOR SHALL BE APPROVED IN WRITING BY THE ENGINEER. CONTRACTOR SHALL PROVIDE DOCUMENTATION TO ENGINEER FOR DETERMINING IF SUBSTITUTE IS SUITABLE FOR USE AND MEETS THE ORIGINAL DESIGN CRITERIA. DIFFERENCES FROM THE ORIGINAL DESIGN, INCLUDING MAINTENANCE, REPAIR AND REPLACEMENT, SHALL BE NOTED. ESTIMATES OF COSTS/CREDITS ASSOCIATED WITH THE SUBSTITUTION (INCLUDING RE-DESIGN COSTS AND COSTS TO SUB-CONTRACTORS) SHALL BE PROVIDED TO THE ENGINEER. CONTRACTOR SHALL PROVIDE ADDITIONAL DOCUMENTATION AND/OR SPECIFICATIONS TO THE ENGINEER AS REQUESTED.

13. PROVIDE STRUCTURAL STEEL SHOP DRAWINGS TO ENGINEER FOR APPROVAL PRIOR TO FABRICATION.

14. UNLESS NOTED OTHERWISE, ALL NEW MEMBERS SHALL MAINTAIN THE EXISTING MEMBER WORK LINES AND NOT INTRODUCE ECCENTRICITIES INTO THE STRUCTURE.

15. THE ENGINEER (GPD GROUP) SHALL MAKE POST INSTALLATION OBSERVATION FOR TOWER AND FOUNDATION. CONTRACTOR SHALL COORDINATE THE ON-SITE INSTALLATION OBSERVATION W/ ENGINEER (GPD GROUP) AT LEAST 5 BUSINESS DAYS PRIOR TO THE CONCRETE POUR FOR EACH FOUNDATION MODIFICATION. CONTRACTOR SHALL COORDINATE W/ENGINEER (GPD GROUP) WITHIN 72 HOURS AFTER 100% COMPLETION OF THE TOWER MODIFICATION INSTALLATION. INSTALLATION OF PROPOSED LOADING WITHOUT ENGINEER APPROVAL IS PROHIBITED. INSTALLATION OF THE PROPOSED LOADING IS BY OTHERS, AND IS BEYOND THE SCOPE OF THESE DRAWINGS.

CONTRACTOR NOTES

1. ALL CONTRACTORS AND LOWER TIER CONTRACTORS MUST ACKNOWLEDGE IN WRITING TO TOWER OWNER AND GPD GROUP THAT THEY HAVE OBTAINED, UNDERSTAND, AND WILL FOLLOW TOWER OWNER STANDARDS OF PRACTICE, CONSTRUCTION GUIDELINES, ALL SITE AND TOWER SAFETY PROCEDURES, ALL PRODUCT LIMITATIONS, AND INSTALLATION PROCEDURES USED ON SITE, AND PROPOSED MODIFICATIONS DESCRIBED. RECEIPT OF ACKNOWLEDGMENT MUST OCCUR PRIOR TO BEGINNING CONSTRUCTION OR CLIMBING. IT IS THE RESPONSIBILITY OF THE GENERAL CONTRACTOR TO PROVIDE THIS DOCUMENTATION FOR TOWER OWNER AND GPD GROUP ON COMPANY LETTERHEAD AND THE RESPONSIBILITY OF THE GENERAL CONTRACTOR TO OBTAIN THIS DOCUMENTATION FROM LOWER TIER SUBCONTRACTORS (ON SUBCONTRACTOR LETTERHEAD) AND DELIVER IT TO TOWER OWNER AND GPD GROUP.

2. IF THE CONTRACTOR DISCOVERS ANY EXISTING CONDITIONS THAT ARE NOT REPRESENTED ON THESE DRAWINGS, OR ANY CONDITIONS THAT WOULD INTERFERE WITH THE INSTALLATION OF THE MODIFICATIONS, GPD GROUP SHALL BE CONTACTED IMMEDIATELY TO EVALUATE THE SIGNIFICANCE OF THE DEVIATION.

3. IT IS ASSUMED THAT ANY STRUCTURAL MODIFICATION WORK SPECIFIED ON THESE PLANS WILL BE ACCOMPLISHED BY KNOWLEDGEABLE WORKMEN WITH TOWER CONSTRUCTION EXPERIENCE. THIS INCLUDES PROVIDING THE NECESSARY CERTIFICATIONS TO THE TOWER OWNER AND ENGINEER.

4. THESE DRAWINGS DO NOT INDICATE THE METHOD OF CONSTRUCTION. THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION METHODS, MEANS, TECHNIQUES, SEQUENCES, AND PROCEDURES.

5. THE CONTRACTOR IS SOLELY RESPONSIBLE FOR INITIATING, MAINTAINING, AND SUPERVISING ALL SAFETY PROGRAMS AND PRECAUTIONS IN CONNECTION WITH THIS WORK.

6. THE CONTRACTOR SHALL VISIT THE SITE PRIOR TO BIDDING; ANY PROBLEMS WITH ACCESS, INTERFERENCE, ETC. SHALL BE RESOLVED PRIOR TO MOBILIZATION. THE CONTRACTOR MUST VISIT THE SITE PRIOR TO ORDERING ANY MATERIAL AND MUST RESOLVE ALL ISSUES WITH THE OWNER PREVENTING A CONTINUOUS INSTALLATION. CONTRACTOR SHALL NOTE ALL ANTENNAS, MOUNTS, COAX, LIGHTING, CLIMBING SUPPORTS, STEP BOLTS, PORT HOLES, AND ANY OTHER TOWER APPURTENANCES IN THE REGION OF THE MODIFICATIONS. SEE GENERAL NOTES #4 AND #5 THIS SHEET.

CONTINUED CONTRA

7. CONTRACTOR IS RESPONSIBLE FOR TEMPORARILY REMOVING AND ANY OTHER TOWER APPURTENANCE THAT MAY INTERFERE APPURTENANCES MUST BE REPLACED AND/OR RESTORED DOWNTIME MUST BE COORDINATED WITH THE TOWER OWNER IN

8. SOME ATTACHMENTS MAY REQUIRE CUSTOM MODIFICATIONS THE STRUCTURE. THESE CUSTOMIZATIONS ARE DESIGNED BY ENGINEER PRIOR TO REMOVING SUCH ATTACHMENTS. ANY CAR THE TOWER OWNER IN WRITING.

9. CONTRACTOR SHALL ONLY WORK WITHIN THE LIMITS OF THE AND APPROVED EASEMENTS. IT IS THE RESPONSIBILITY OF TI THESE BOUNDARIES. CONTRACTOR SHALL EMPLOY A SURVEYOR BOUNDARIES SHALL BE APPROVED IN WRITING BY THE LAND O STAKING AND BOUNDARY MARKING IS THE RESPONSIBILITY OF T

10. WORK SHALL ONLY BE PERFORMED DURING CALM CONTRACTOR IS RESPONSIBLE FOR ALL TEMPORARY LOCAL 1 SHORING, AND ALL SHORING OF SURROUNDING BUILDINGS, PAD ALL SHORING, TEMPORARY BRACING, AND TEMPORARY SU CONTRACTOR.

11. CONTRACTOR SHALL VERIFY MONOPOLE IS SET PROPER RESTING POSITION BEFORE FINAL CRITICAL FIELD MEASUREM MATERIAL. ANY OBJECTS/STEP BOLTS THAT PREVENT TOWER FR TO THE ENGINEER IMMEDIATELY.

FOUNDATION

1. CONTRACTOR SHALL NOTIFY THE FOLLOWING INDIVIDUALS CONSTRUCTION IN ORDER TO COORDINATE THE VISUAL INSPECT

-STEPHANIE WENDEROTH (NEXLINK GLOBAL SERVICES) 678
-KEVIN CLEMENTS (GPD GROUP) 678-467-7228
-BRIAN SMITH (GPD GROUP) 216-927-8648
-JEREL FIELDS (GPD GROUP) 317-295-3186

2. EXISTING FOUNDATION INFORMATION BASED UPON A ENGINEERING (DATED APRIL 1, 2000). CONTRACTOR SHALL REFERENCED FOUNDATION DOCUMENT. IF EXISTING FOUNDATIO DOCUMENT, CONTACT ENGINEER AND TOWER OWNER IMMEDIATE!

3. CONCRETE WORK SHALL BE IN ACCORDANCE WITH LOCAL OTHERWISE NOTED, THE LATEST REVISION OF ACI 318, "BUIL CONCRETE". PROCEDURES FOR THE PROTECTION OF EXCAVAT SHALL BE ESTABLISHED PRIOR TO FOUNDATION INSTALLATION.

4. MAXIMUM SIZE OF AGGREGATE SHALL NOT EXCEED SIZE SU 1/3 CLEAR DISTANCE BEHIND OR BETWEEN REINFORCING. MAXI DISTANCE PROVIDED WORKABILITY AND METHODS OF CONSOL HONEYCOMBS OR VOIDS.

5. WELDING IS PROHIBITED ON REINFORCING STEEL AND EMBED

6. CONCRETE SHALL DEVELOP A MINIMUM COMPRESSIVE STRENG

7. ALL FOUNDATIONS SHALL REST ON AND AGAINST FIRM UNL MATTER, AND FORM WORK. CONTRACTOR SHALL COMPACT SUB

8. REINFORCEMENT SHALL BE DEFORMED AND CONFORM TO T UNLESS OTHERWISE NOTED. SPLICES IN REINFORCEMENT S INDICATED.

9. MINIMUM CONCRETE COVER FOR REINFORCEMENT SHALL BE APPROVED SPACERS SHALL BE USED TO INSURE A 3 INCH MIN REINFORCING SHALL BE EQUALLY SPACED UNLESS NOTED OTHE

10. PROVIDE #7 2'-6" X 2'-6" CORNER BARS AT ALL PL CHANGES.

11. SOIL INFORMATION IS BASED ON A GEOTECHNICAL REPORT (2009). IF SOIL CONDITIONS ENCOUNTERED ARE DIFFERENT NOTIFY ENGINEER IMMEDIATELY.

A) ALLOWABLE BEARING = 6,000 PSF AT 7'
B) UNIT WEIGHT OF SOIL = 120 PCF
C) GROUND WATER = 1'-0"

12. CONTRACTOR SHALL OBTAIN AND BECOME FAMILIAR WIT CONTRACTOR SHALL IMPLEMENT ALL RECOMMENDATIONS CON REPORT.

13. BACKFILL SHALL BE CLEAN, FREE OF DEBRIS, AND OI CLEAN FILL AS REQUIRED. (MIN. UNIT WEIGHT = 120 PCF).

14. ALL BACKFILL SHALL BE CONTROLLED-COMPACTED, PLA CONDITIONED TO WITHIN THREE PERCENT OF OPTIMUM MOISTI PROCTOR MAXIMUM DRY DENSITY PER ASTM D1557.

15. CARE SHALL BE TAKEN DURING INSTALLATION OF DOWELS ANCHOR BOLTS ARE NOT DAMAGED. CONTRACTOR SHALL U: NON-DESTRUCTIVE MEANS TO LOCATE EXISTING REINFORCING S IMMEDIATELY IF EXISTING STEEL IS ENCOUNTERED.

16. CONTRACTOR SHALL OBTAIN AND BECOME FAMILIAR WITH AND RECOMMENDATIONS.

17. PRIOR TO APPLICATION OF BONDING AGENT, CLEAN FACE FREE FROM ALL DIRT, DEBRIS, AND FOREIGN MATTER.

18. CONTRACTOR SHALL SECURE SITE BACK TO EXISTING CON FENCE, STONE, GEOFABRIC, GROUNDING, AND SURROUNDING GI REQUIRED TO ACHIEVE OWNER APPROVAL. POSITIVE DRAINAGE A!

19. ALL GROUNDING SHALL ACHIEVE 5Q OR LESS RESIS' ENCOUNTERED SHALL BE RELOCATED 3'-0" BEYOND FOUNDAT AND COORDINATED WITH OWNER. GROUNDING DESIGN AND ENK DESIGN DRAWINGS AND IS THE RESPONSIBILITY OF THE CONTRA

20. CONTRACTOR TO VERIFY LOCATION OF ALL EXISTING EXCAVATION. IF NECESSARY UTILITIES SHALL BE RELOCATED PR FROM THE TOWER OWNER AND EOR MUST BE OBTAINED TO ENK

21. EQUIPMENT PAD, SHELTER, AND ICE BRIDGE SUPPORT IS COMMISSION. CONTRACTOR SHALL TAKE GREAT CARE AND ALL REQUIRED.

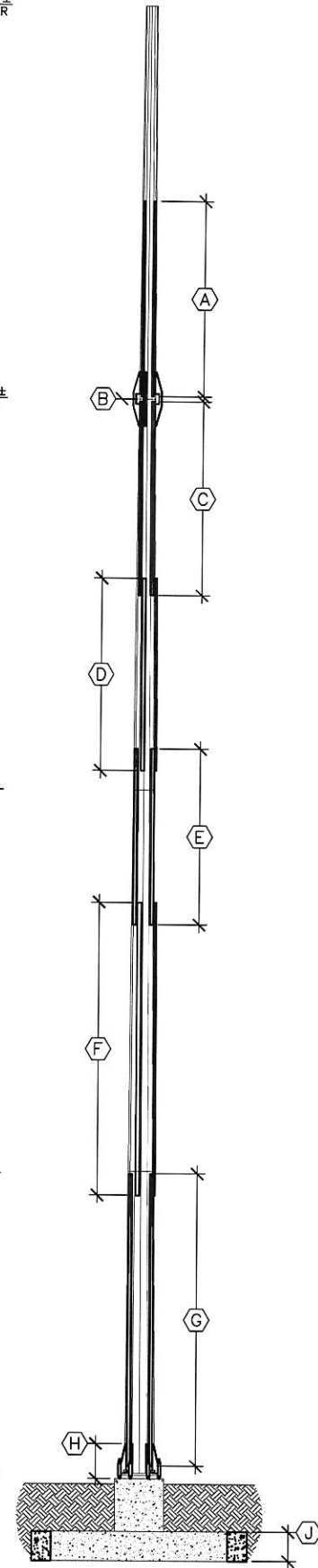
ELEV: 150'-0"±
TOP OF TOWER

ELEV: 110'-0"±
FLANGE PLATE

ELEV: 70'-0"±
SLIP JOINT

ELEV: 31'-0"±
SLIP JOINT

ELEV: 0'-0"±
TOWER BASE



TOWER ELEVATION

1/8" = 1'-0"

ANTENNA SCHEDULE

ELEVATION	STATUS	ANTENNA	MOUNT	COAX
	EXISTING	(6) 7770.00	(1) 10'-8"	(12) 1-1/4"
	EXISTING	(6) LGP21401	PLATFORM W/ RAILS	
	EXISTING	(6) LGP21903		
152'-0"	PROPOSED	(1) SBNH-1D6565C		(1) 2" COND
	PROPOSED	(2) AM-X-CD-17-65-00T		(1) 1/2" FIB
	PROPOSED	(6) RBS 6601		(2) 3/4" DC
	PROPOSED	(1) DC6-48-60-18-8F		
100'-0"	EXISTING	(1) DIPOLE (2 ELEMENTS)	(1) FLUSH MOUNT	(1) 1/2"

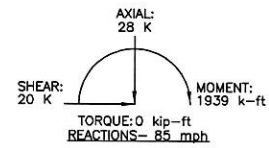
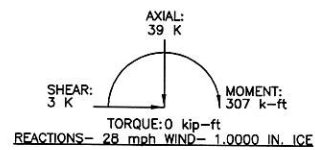
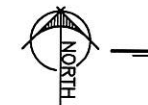
MODIFICATION S

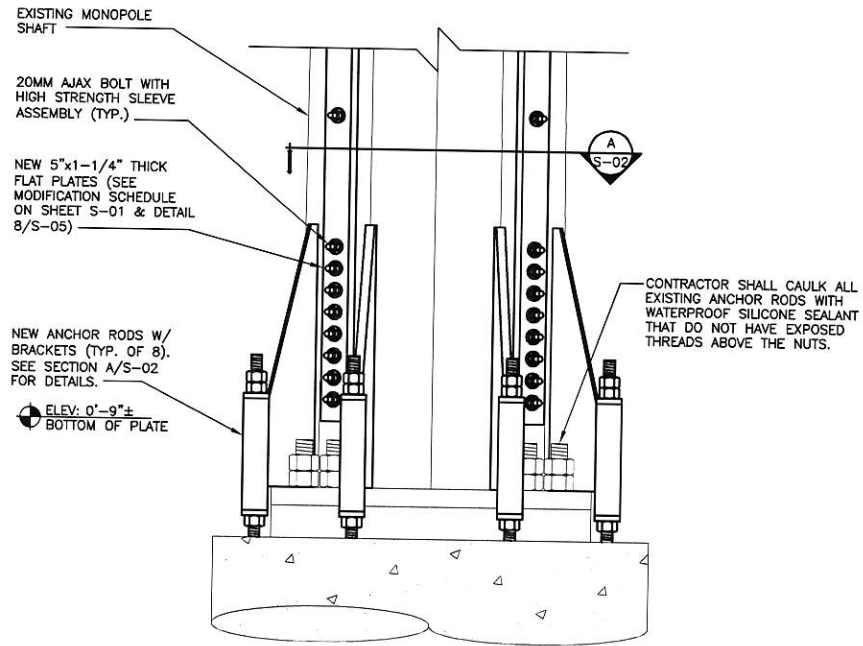
SYMBOL	ELEVATION	MEMBER TYPE	EXISTING MEMBER	NEW MEMBER
(A)	110'-3"± TO 130'-3"±	FLAT PLATES	12 SIDED MONOPOLE	3"x1-1/4" TH PLATE
(B)	110'-0"±	BRIDGE STIFFENERS	-	1-1/4" THICK I
(C)	90'-0"± TO 109'-9"±	FLAT PLATES	12 SIDED MONOPOLE	4"x1-1/4" TH PLATE
(D)	72'-0"± TO 91'-9"±	FLAT PLATES	12 SIDED MONOPOLE	4"x1-1/4" TH PLATE
(E)	56'-3"± TO 74'-3"±	FLAT PLATES	12 SIDED MONOPOLE	5"x1-1/4" TH PLATE
(F)	28'-6"± TO 58'-6"±	FLAT PLATES	12 SIDED MONOPOLE	5"x1-1/4" TH PLATE
(G)	0'-9"± TO 30'-9"±	FLAT PLATES	12 SIDED MONOPOLE	5"x1-1/4" TH PLATE
(H)	0'-0"± TO 3'-0"±	ANCHOR RODS W/BRACKETS	(8) 2-1/4"Ø RODS	(8) 1-1/2"Ø F W/BRACKET
(J)	GRADE	FOUNDATION COLLAR	PAD & PIER	CONCERT COL

(EXISTING)
(12) 1-1/4" COAX TO 152 FT LEVEL
(PROPOSED)
(1) 2" CONDUIT TO 152 FT LEVEL
(1) 1/2" FIBER CABLE TO 152 FT LEVEL
(2) 3/4" DC CABLE TO 152 FT LEVEL

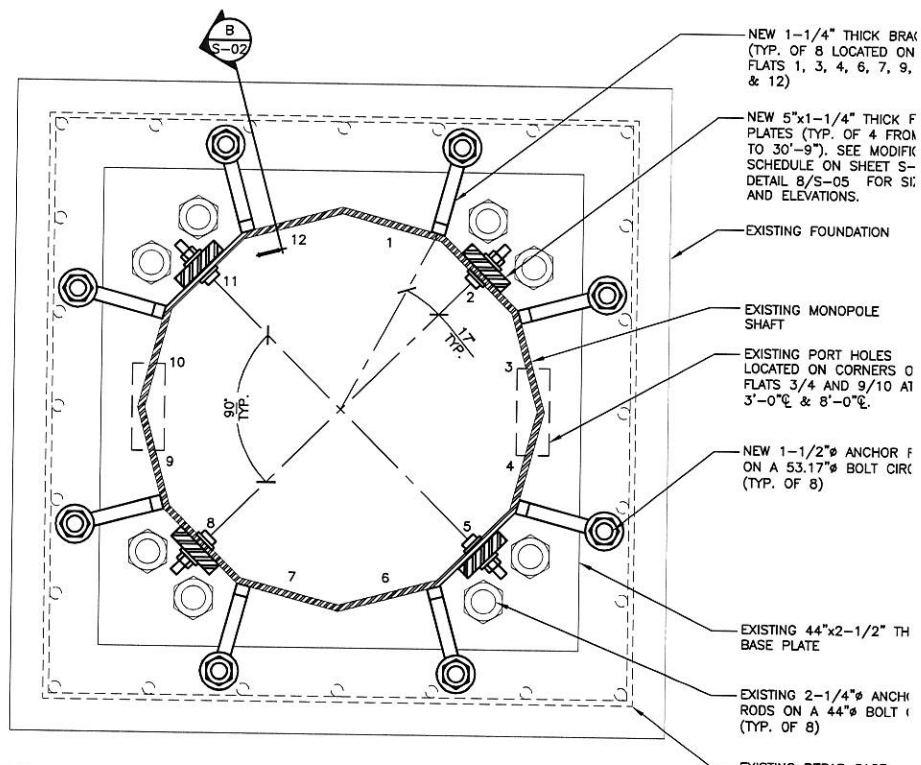


NOTE: FLAT NUMBERS DEPICTED IN THIS DRAWING MAY VARY FROM THE NUMBERING IN THE FIELD. CONTRACTOR MAY ADJUST FLAT NUMBERS TO MATCH EXISTING FIELD CONDITIONS. MODIFICATIONS SHALL BE INSTALLED IN THE APPROPRIATE ORIENTATION AND/OR LOCATION REGARDLESS OF THE NUMBERING SHOWN ON THE DRAWINGS.





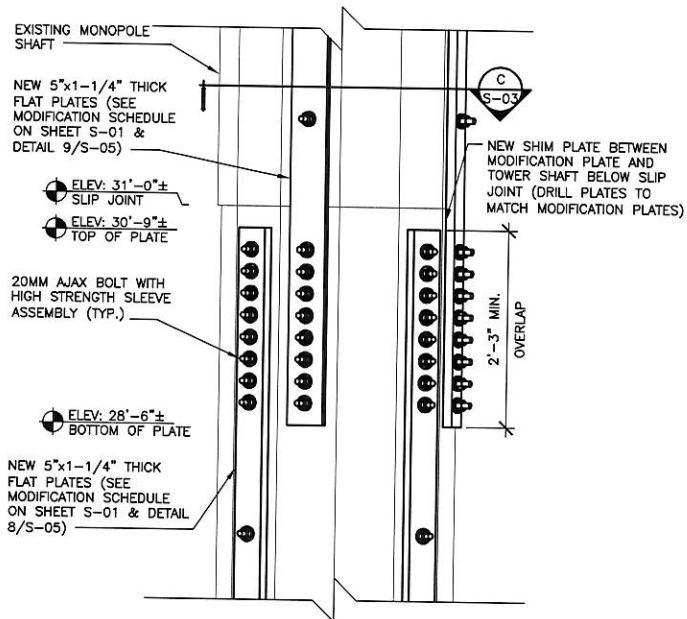
DETAIL 1
1"=1'-0"



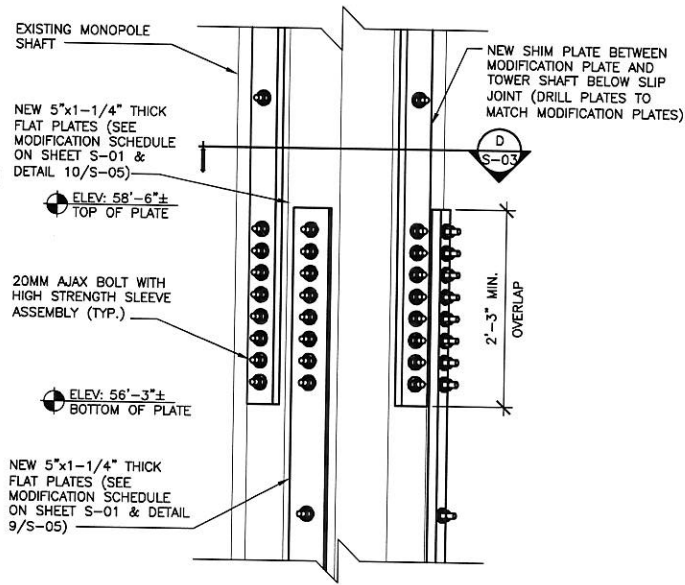
SECTION A
1-1/2"=1'-0"

NOTE: FLAT NUMBERS DEPICTED IN THIS DRAWING MAY VARY FROM THE NUMBERING IN THE FIELD. CONTRACTOR MAY ADJUST FLAT NUMBERS TO MATCH EXISTING FIELD CONDITIONS. MODIFICATIONS SHALL BE INSTALLED IN THE APPROPRIATE ORIENTATION AND/OR LOCATION REGARDLESS OF THE NUMBERING SHOWN ON THE DRAWINGS.

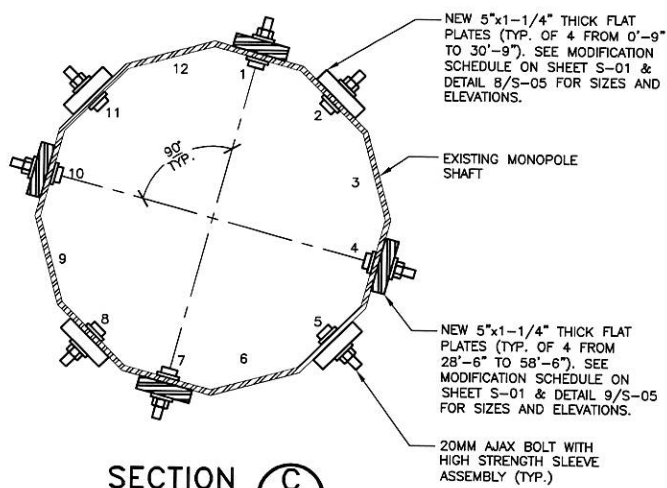
NOTE: STEP PEGS AND SAFETY CLIMB TO BE REMOVED AND REPLACED AS REQUIRED.



DETAIL 2
1"=1'-0" S-03

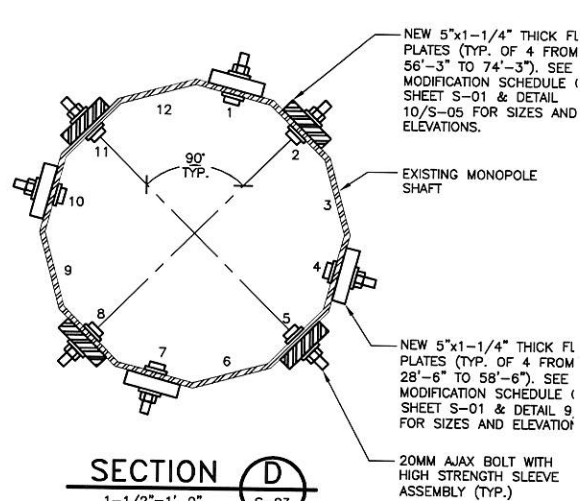


DETAIL 3
1"=1'-0" S-03



SECTION C
1-1/2"=1'-0" S-03

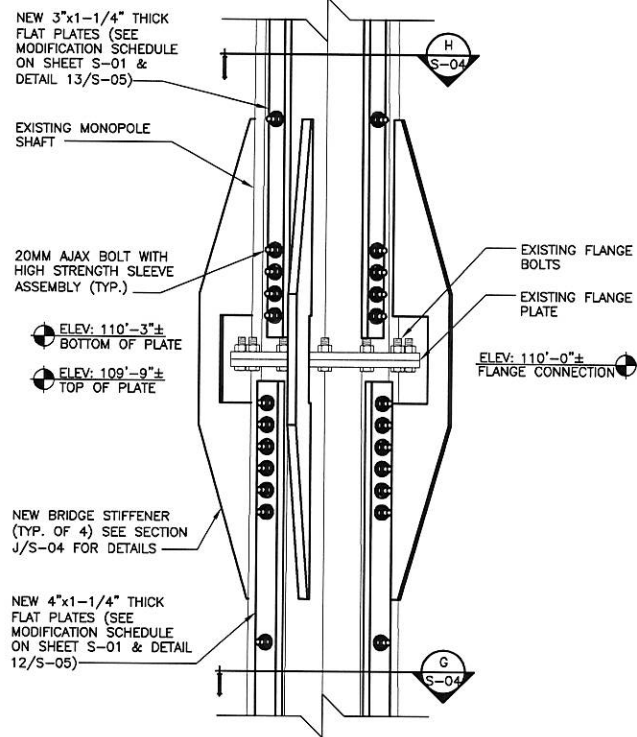
NOTE: STEP PEGS AND SAFETY CLIMB TO BE REMOVED AND REPLACED AS REQUIRED.



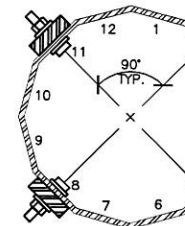
SECTION D
1-1/2"=1'-0" S-03

NOTE: STEP PEGS AND SAFETY CLIMB TO BE REMOVED AND REPLACED AS REQUIRED.

NOTE: FLAT NUMBERS DRAWING MAY VARY F IN THE FIELD. CONTR FLAT NUMBERS TO M. CONDITIONS. MODIFIC/ INSTALLED IN THE AP AND/OR LOCATION RI NUMBERING SHOWN C

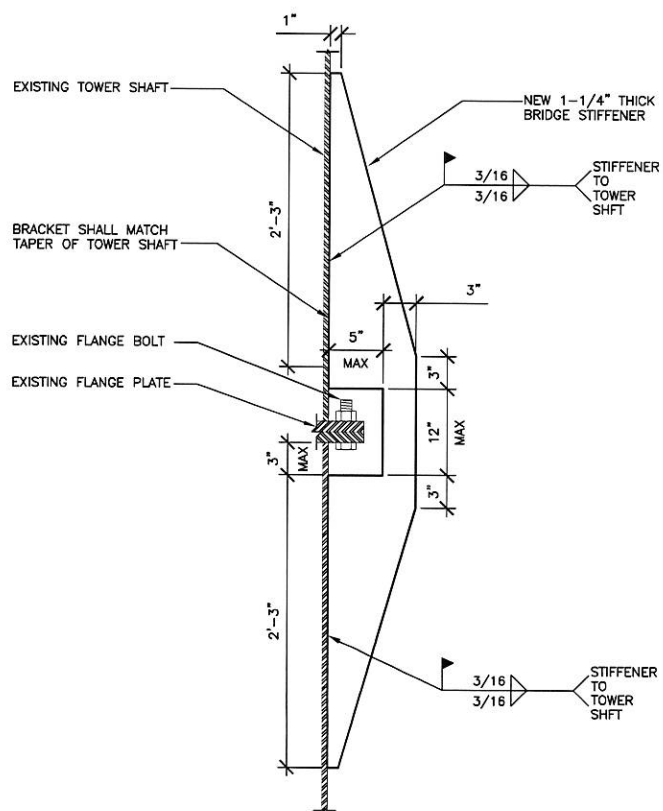


DETAIL 6
1"=1'-0" S-04

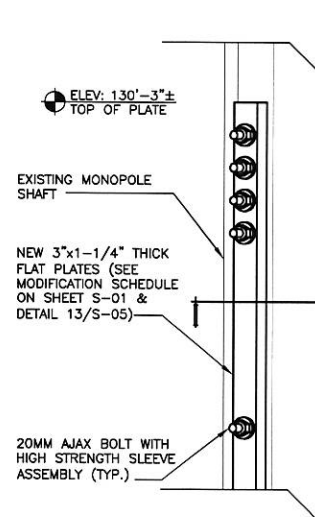


SECTION 1-1/2
1'-0"

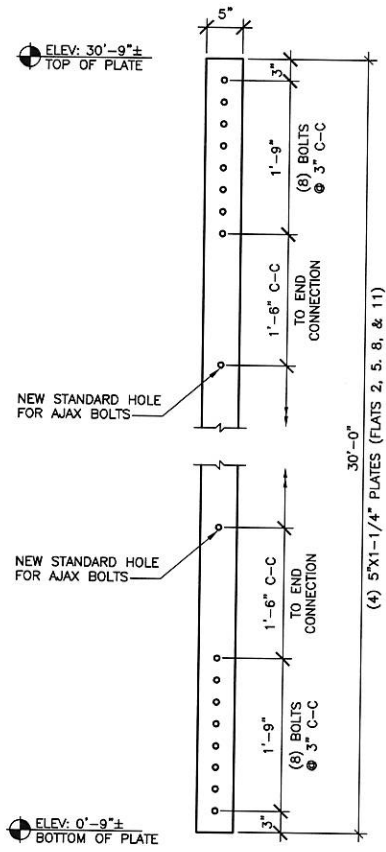
NOTE: STEP PEGS AND SAFETY REMOVED AND REPLACED AS RE



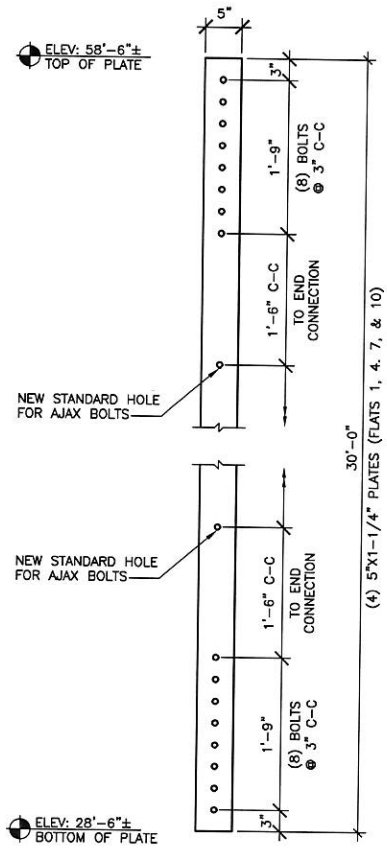
SECTION J
1-1/2"=1'-0" S-04



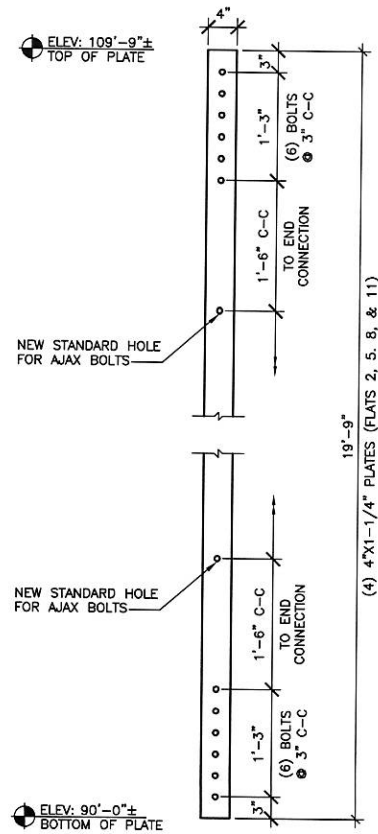
DETAIL 1-1/2
1"=1'-0"



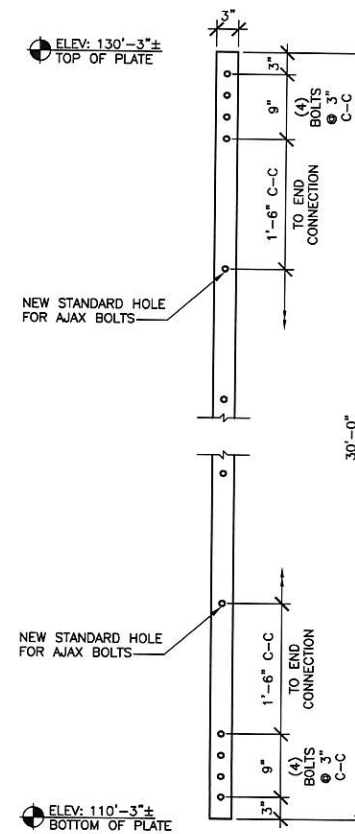
DETAIL 8
1"=1'-0" S-05



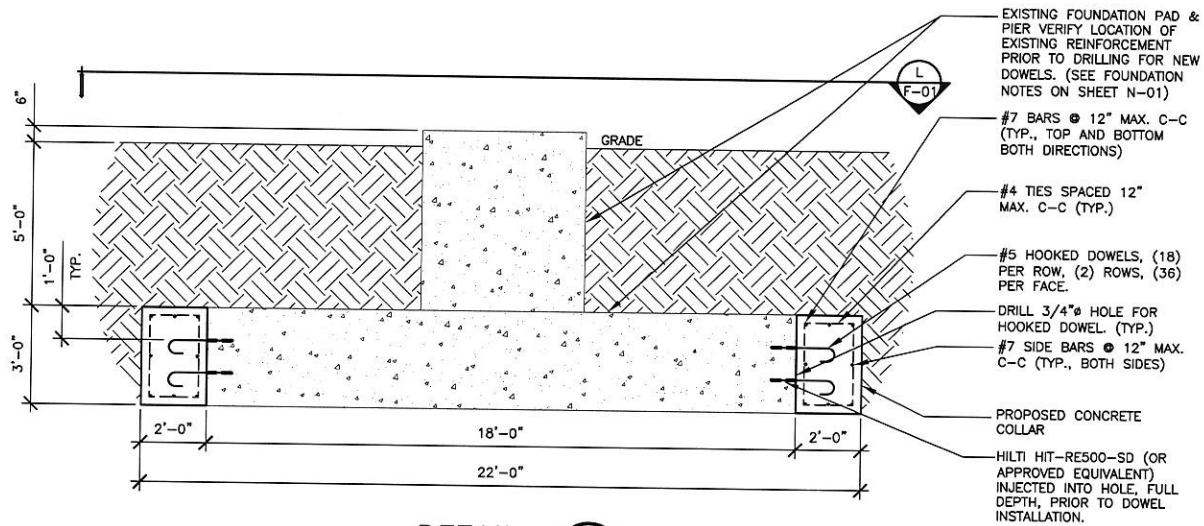
DETAIL 9
1"=1'-0" S-05



DETAIL 12
1"=1'-0" S-05

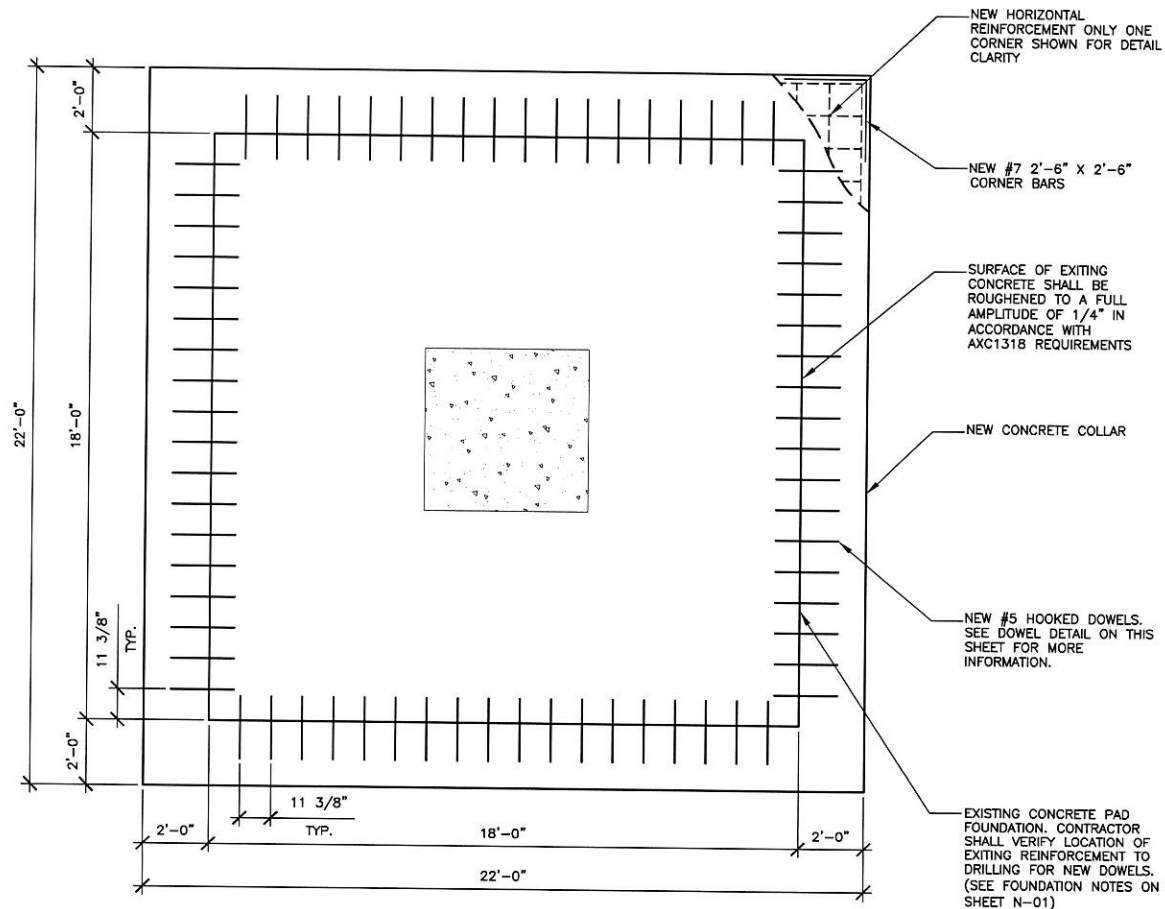


DETAIL 13
1"=1'-0" S-05



DETAIL **14**
 $3/8"=1'-0"$ F-01

EXISTING FOUNDATION IS BEING EXCAVATED. CONTRACTOR IS RESPONSIBLE FOR SUPPORTING TOWER DURING ALL PHASES OF CONSTRUCTION. SEE CONTRACTOR FOUNDATION NOTES ON SHEET N-01.



SECTION **L**
 $3/8"=1'-0"$ F-01

MODIFICATION INSPECTIC

BEFORE CONSTRUCTION		DURING CONSTRU	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM	CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	R
X	MODIFICATION INSPECTION CHECKLIST DRAWING	X	CONSTRUCTION INSPECTI
X	ENGINEER OF RECORD APPROVED SHOP DRAWINGS	X	FOUNDATION INSPECTION:
X	FABRICATION INSPECTION	X	CONCRETE COMP. STREN
X	FABRICATOR CERTIFIED WELD INSPECTION	X	POST INSTALLED ANCHOF
X	MATERIAL TEST REPORT	X	BASE PLATE GROUT VERI
X	FABRICATOR NDE INSPECTION	X	CONTRACTOR'S CERTIFIED
X	NDE REPORT OF MONOPOLE BASE PLATE (AS REQUIRED)	X	EARTHWORK: LIFT AND D
X	PACKING SLIPS	X	ON SITE COLD GALVANIZI
ADDITIONAL TESTING AND INSPECTIONS:		—	GUY WIRE TENSION REPC
		X	GC AS-BUILT DOCUMENT
		ADDITIONAL TESTING AND INSPECTIONS:	

NOTE: X DENOTES A DOCUMENT NEEDED FOR THE MODIFIC
 — DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR

MODIFICATION INSPECTION NOTES:

GENERAL

1. THE MODIFICATION INSPECTION IS A VISUAL INSPECTION OF TOWER MODIFICATIONS AND A REVIEW OF CONSTRUCTION INSPECTIONS AND OTHER REPORTS TO ENSURE THE INSTALLATION WAS CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, NAMELY THE MODIFICATION DRAWINGS, AS DESIGNED BY THE ENGINEER OF RECORD.
2. THE MODIFICATION INSPECTION IS TO CONFIRM INSTALLATION CONFIGURATION AND WORKMANSHIP ONLY AND IS NOT A REVIEW OF THE MODIFICATION DESIGN ITSELF, NOR DOES THE MODIFICATION INSPECTOR TAKE OWNERSHIP OF THE MODIFICATION DESIGN. OWNERSHIP OF THE STRUCTURAL MODIFICATION DESIGN EFFECTIVENESS AND INTENT RESIDES WITH THE ENGINEER OF RECORD AT ALL TIMES.
3. TO ENSURE THAT THE REQUIREMENTS OF THE MODIFICATION INSPECTION ARE MET, IT IS VITAL THAT THE GENERAL CONTRACTOR (GC) AND THE MODIFICATION INSPECTOR BEGIN COMMUNICATING AND COORDINATING AS SOON AS A PO OR PAYMENT IS RECEIVED. IT IS EXPECTED THAT EACH PARTY WILL BE PROACTIVE IN REACHING OUT TO THE OTHER PARTY. CONTACT LISTED ON THE TITLE SHEET SHALL BE CONTACTED IF SPECIFIC INSPECTOR CONTACT INFORMATION IS NOT KNOWN.

MODIFICATION INSPECTOR

1. THE MODIFICATION INSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A PO OR PAYMENT FOR THE MODIFICATION INSPECTION TO:
 - REVIEW THE REQUIREMENTS OF THE MODIFICATION INSPECTION CHECKLIST
 - WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS
 - DISCUSS ANY SITE SPECIFIC INSPECTIONS OR CONCERNS
2. THE MODIFICATION INSPECTOR IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (GC) INSPECTION AND TEST REPORTS, REVIEWING THE DOCUMENTS FOR ADHERENCE TO THE CONTRACT DOCUMENTS, CONDUCTING THE IN-FIELD INSPECTIONS, AND SUBMITTING THE MODIFICATION INSPECTION REPORT.

GENERAL CONTRACTOR

1. THE GC IS REQUIRED TO CONTACT THE MODIFICATION INSPECTOR AS SOON AS RECEIVING A PO OR PAYMENT FOR THE MODIFICATION INSTALLATION OR TURNKEY PROJECT TO:
 - REVIEW THE REQUIREMENTS OF THE MODIFICATION INSPECTION CHECKLIST
 - WORK WITH THE MI INSPECTOR TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE MODIFICATION INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS
 - BETTER UNDERSTAND ALL INSPECTION AND TESTING REQUIREMENTS
2. THE GC SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IN ACCORDANCE WITH THE REQUIREMENTS OF THE MODIFICATION INSPECTION CHECKLIST.

RECOMMENDATIONS

1. THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE FOR THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING A MODIFICATION:
 - IT IS SUGGESTED THAT THE GC PROVIDE A MINIMUM OF 10 WORKDAYS BEFORE THE MODIFICATION INSPECTOR FOR THE MODIFICATION INSPECTION TO BE CONDUCTED.
 - THE GC AND MODIFICATION INSPECTOR COORDINATE ALL PROJECTS.
 - WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MODIFICATION INSPECTOR SIMULTANEOUSLY FOR ANY GUY WIRE TENSIONING OR FOUNDATION INSPECTIONS TO ALLOW FOUNDATION AND GUY WIRE TENSIONING TO COMMENCE WITH ONE SITE VISIT.
 - IT MAY BE BENEFICIAL TO INSTALL ALL TOWER MODIFICATION FOUNDATION INSPECTIONS TO ALLOW FOUNDATION AND GUY WIRE TENSIONING TO COMMENCE WITH ONE SITE VISIT.
 - WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MODIFICATION INSPECTOR DURING THE MODIFICATION INSPECTION TO HAVE AN INITIAL MODIFICATION INSPECTION. THEREFORE, THE MODIFICATION INSPECTOR SHOULD CAREFULLY TO ENSURE ALL MODIFICATION INSPECTIONS ARE COMPLETED BEFORE THEIR DISPOSAL WHEN THE MI INSPECTOR IS ON SITE.

CANCELLATION OR DELAYS IN SCHEDULED MODIFICATION INSPECTION

1. IF THE GC AND MODIFICATION INSPECTOR AGREE TO CANCEL OR DELAY A MODIFICATION INSPECTION, EITHER PARTY SHALL BE RESPONSIBLE FOR ANY COSTS, FEES, PENALTIES RELATED TO THE CANCELLATION OR DELAY INCURRED (E.G. TRAVEL AND LODGING, COSTS OF KEEPING EQUIPMENT). THE MODIFICATION INSPECTOR SHALL BE RESPONSIBLE FOR ANY COSTS, FEES, PENALTIES RELATED TO THE CANCELLATION OR DELAY INCURRED IN THE EVENT THAT THE DELAY/CANCELLATION OF A MODIFICATION INSPECTION RESULTS IN CONDITIONS THAT MAY COMPROMISE THE SAFETY OF THE PROJECT.



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 800 Marshall Phelps Road
 Windsor, CT 06095



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 1117 Perimeter Ctr W, Suite W303
 Atlanta, GA 30328
 (678) 467-7228
kclements@gpdgroup.com

GPD# 2012832.07
 January 4, 2013

STRUCTURAL ANALYSIS REPORT WITH MODIFICATION DESIGN

AT&T DESIGNATION: **Site USID:** **71304**
 Site FA: **10035021**
 Site Name: **POMFRET-TYRONE RD**
 AT&T Project: **MOD LTE 082712**

ANALYSIS CRITERIA: **Codes:** **TIA/EIA-222-F, 2003 IBC, ASCE 7-05 & 2005 CTBC**
 85-mph with 0" ice
 28-mph with 1" ice

SITE DATA: **82 Tyrone Rd, Pomfret, CT 06258, Windham County**
 Latitude 41° 53' 24.871" N, Longitude 71° 57' 20.199" W
 Market: New England
 150' Monopole

Lauren Groppi,

GPD is pleased to submit this Structural Analysis Report with Modification Design to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.


Analysis Results

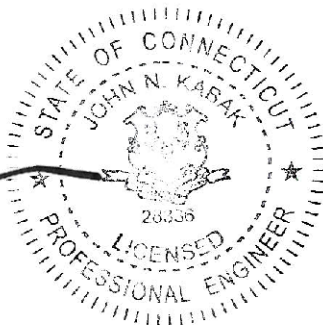
Tower Stress Level with Proposed Equipment:	95.4%	Pass
Foundation Ratio with Proposed Equipment:	76.8%	Pass

Note: In order for this analysis results to be valid for the proposed, existing, and reserved loading in Appendix A the modifications referenced in the design drawings by GPD (Project #: 2012832.07, dated 1/4/2012) must be installed.

We at GPD appreciate the opportunity of providing our continuing professional services to you and Pinnacle Wireless. If you have any questions or need further assistance on this or any other projects please do not hesitate to call.

Respectfully submitted,


 John N. Kabak, P.E.
 Connecticut #: 28336



SUMMARY & RESULTS

The purpose of this analysis was to verify whether the existing modified structure is capable of carrying the proposed loading configuration as specified by AT&T Mobility to Pinnacle Wireless. This report was commissioned by Ms. Lauren Groppi of Pinnacle Wireless.

All proposed coax shall be internal to the monopole in order for the analysis results to be valid.

The proposed modifications by GPD (Project #: 2012832.07, dated 1/4/2012), consist of adding flat plate reinforcement from 0' – 130.3', installing bridge stiffeners at 110', adding anchor rods to the base and extending the existing pad foundation, and have been considered in this analysis. See Appendix H for the modification drawings.

TOWER SUMMARY AND RESULTS

Member	Capacity	Results
Monopole	95.4%	Pass
Anchor Rods	89.6%	Pass
Base Plate	74.6%	Pass
Flange Bolts	30.7%	Pass
Flange Plates	68.4%	Pass
Foundation	76.8%	Pass

ANALYSIS METHOD

TNX Tower (Version 6.0.4.0), a commercially available software program, was used to create a three-dimensional model of the tower and calculate primary member stresses for various dead, live, wind, and ice load cases. Selected output from the analysis is included in Appendix B. The following table details the information provided to complete this structural analysis. This analysis is solely based on this information and is being completed without the benefit of a detailed site visit.

DOCUMENTS PROVIDED

Document	Remarks	Source
Equipment Modification Form	AT&T Internal Loading Document, uploaded 8/27/12	Siterra
Construction Drawings	Not Provided	N/A
Tower Design	Not Provided	N/A
Foundation Design	Not Provided	N/A
Modification Drawings	GPD Project #: 2012832.07, dated 1/4/12	GPD
Geotechnical Report	Dr. Clarence Welti, dated 5/15/09	Siterra
Previous Structural Analysis	GPD Project #: 2009013.07, dated 6/2/09	Siterra
Tower Mapping	GPD and Northeast Towers Inc, dated 12/3/08	Siterra

ASSUMPTIONS

This structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analyzing the tower only.
5. The soil parameters are as per data supplied or as assumed and stated in the calculations.
6. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
7. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
8. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
9. All prior structural modifications are assumed to be as per data supplied/available and to have been properly installed.
10. Loading interpreted from photos is accurate to $\pm 5'$ AGL, antenna size accurate to ± 3.3 sf, and coax equal to the number of existing antennas without reserve.
11. All existing loading was obtained from the previous analysis by GPD Job #: 2009013.07, dated 6/2/09, site photos, the provided equipment modification form and is assumed to be accurate.
12. The existing AT&T loading elevation found in the previous analysis by GPD Job #: 2009013.07, dated 6/2/09 was found to vary from the EMF and site photos. The existing AT&T loading elevation was based on the site photos.
13. The proposed modifications by GPD (Project #: 2012832.07, dated 1/4/2012), consist of adding flat plate reinforcement from 0' – 130.3', installing bridge stiffeners at 110', adding anchor rods to the base and extending the existing pad foundation, and have been considered in this analysis. See Appendix H for the modification drawings.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD Group should be allowed to review any new information to determine its effect on the structural integrity of the tower.

DISCLAIMER OF WARRANTIES

GPD GROUP has not performed a site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD GROUP in connection with this Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. All tower components have been assumed to only resist dead loads when no other loads are applied. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

GPD GROUP does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD GROUP provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the feasibility of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD GROUP, but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

GPD GROUP makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD GROUP will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD GROUP pursuant to this report will be limited to the total fee received for preparation of this report.

APPENDIX A

Tower Analysis Summary Form

APPENDIX B

tnxTower Output File

tnxTower GPD 520 South Main Street, Suite 2531 Akron, OH 44311 Phone: 330.572.2100 FAX: 330.572.2101	Job	71304 POMFRET-TYRONE RD	Page	1 of 4
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	Client	Pinnacle Wireless	Designed by	jfields

Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Windham County, Connecticut.

Basic wind speed of 85 mph.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 28 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.333.

Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	C _A A _A		Weight plf
						ft ² /ft		
5/8" Step Bolts	A	No	CaAa (Out Of Face)	150.00 - 8.00	1	No Ice	0.04	1.00
						1/2" Ice	0.14	1.56
						1" Ice	0.24	2.73
						2" Ice	0.44	6.91
						4" Ice	0.84	22.58
Safety Line 3/8	A	No	CaAa (Out Of Face)	150.00 - 8.00	1	No Ice	0.04	0.22
						1/2" Ice	0.14	0.75
						1" Ice	0.24	1.28
						2" Ice	0.44	2.34
						4" Ice	0.84	4.46
LDF6-50A (1-1/4 FOAM)	A	No	Inside Pole	150.00 - 8.00	12	No Ice	0.00	0.66
						1/2" Ice	0.00	0.66
						1" Ice	0.00	0.66
						2" Ice	0.00	0.66
						4" Ice	0.00	0.66
2" Flex Conduit	A	No	Inside Pole	150.00 - 8.00	1	No Ice	0.00	0.32
						1/2" Ice	0.00	0.32
						1" Ice	0.00	0.32
						2" Ice	0.00	0.32
						4" Ice	0.00	0.32
1/2" Fiber Cable	A	No	Inside Pole	150.00 - 8.00	1	No Ice	0.00	0.15
						1/2" Ice	0.00	0.15
						1" Ice	0.00	0.15
						2" Ice	0.00	0.15
						4" Ice	0.00	0.15
3/4" DC Power Line	A	No	Inside Pole	150.00 - 8.00	2	No Ice	0.00	0.33
						1/2" Ice	0.00	0.33
						1" Ice	0.00	0.33
						2" Ice	0.00	0.33
						4" Ice	0.00	0.33
LDF4P-50A (1/2 FOAM)	B	No	Inside Pole	100.00 - 8.00	1	No Ice	0.00	0.15
						1/2" Ice	0.00	0.15
						1" Ice	0.00	0.15
						2" Ice	0.00	0.15
						4" Ice	0.00	0.15

tnxTower GPD 520 South Main Street, Suite 2531 Akron, OH 44311 Phone: 330.572.2100 FAX: 330.572.2101	Job	71304 POMFRET-TYRONE RD	Page	2 of 4
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Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total		C _{AA} ft ² /ft	Weight plf
					Number			
5" x 1-1/4" Mod Plate	A	No	CaAa (Out Of Face)	130.25 - 0.75	2	No Ice	0.00	0.00
						1/2" Ice	0.00	1.30
						1" Ice	0.00	2.60
						2" Ice	0.00	3.90
						4" Ice	0.00	5.20
5" x 1-1/4" Mod Plate	A	No	CaAa (Out Of Face)	130.25 - 0.75	1	No Ice	0.21	0.00
						1/2" Ice	0.32	1.30
						1" Ice	0.43	2.60
						2" Ice	0.65	3.90
						4" Ice	1.10	5.20
5" x 1-1/4" Mod Plate	A	No	CaAa (Out Of Face)	130.25 - 0.75	1	No Ice	0.21	0.00
						1/2" Ice	0.32	1.30
						1" Ice	0.43	2.60
						2" Ice	0.65	3.90
						4" Ice	1.10	5.20

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment °	Placement ft	C _{AA}		Weight lb	
			Horz ft	Vert ft			Front ft ²	Side ft ²		
10'-8" Central Platform w/ 42" tower extension	C	None			0.0000	152.00	No Ice	43.32	43.32	2500.00
							1/2" Ice	46.28	46.28	3250.00
							1" Ice	49.24	49.24	4000.00
							2" Ice	55.16	55.16	5500.00
							4" Ice	67.00	67.00	8500.00
(2) 7770.00 w/Mount Pipe	A	From Centroid-Le g	4.00	0.00	0.0000	152.00	No Ice	5.88	4.10	61.54
							1/2" Ice	6.31	4.73	107.08
							1" Ice	6.75	5.37	160.39
							2" Ice	7.66	6.70	289.46
							4" Ice	9.58	9.87	654.29
(2) 7770.00 w/Mount Pipe	B	From Centroid-Le g	4.00	0.00	0.0000	152.00	No Ice	5.88	4.10	61.54
							1/2" Ice	6.31	4.73	107.08
							1" Ice	6.75	5.37	160.39
							2" Ice	7.66	6.70	289.46
							4" Ice	9.58	9.87	654.29
(2) 7770.00 w/Mount Pipe	C	From Centroid-Le g	4.00	0.00	0.0000	152.00	No Ice	5.88	4.10	61.54
							1/2" Ice	6.31	4.73	107.08
							1" Ice	6.75	5.37	160.39
							2" Ice	7.66	6.70	289.46
							4" Ice	9.58	9.87	654.29
SBNH-1D6565C w/ Mount Pipe	A	From Centroid-Le g	4.00	2.00	0.0000	152.00	No Ice	11.45	9.12	82.70
							1/2" Ice	12.06	10.21	162.03
							1" Ice	12.69	11.18	254.15
							2" Ice	14.03	13.17	469.01
							4" Ice	17.05	17.35	1051.99
AM-X-CD-17-65-00T w/ Mount Pipe	B	From Centroid-Le g	4.00	2.00	0.0000	152.00	No Ice	11.31	9.10	105.82
							1/2" Ice	11.93	10.52	189.52
							1" Ice	12.55	11.60	285.59
							2" Ice	13.88	13.80	512.39
							4" Ice	16.88	18.41	1127.38
AM-X-CD-17-65-00T w/ Mount Pipe	C	From Centroid-Le g	4.00	2.00	0.0000	152.00	No Ice	11.31	9.10	105.82
							1/2" Ice	11.93	10.52	189.52
							1" Ice	12.55	11.60	285.59
							2" Ice	13.88	13.80	512.39

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA}		Weight	
			Horz	Vert			Front	Side		
			ft	ft	°	ft	ft ²	ft ²	lb	
(2) LGP21401	A	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	16.88	18.41	1127.38
			0.00	0.00			No Ice	0.00	0.23	10.00
			0.00	0.00			1/2" Ice	0.00	0.31	21.26
			0.00	0.00			1" Ice	0.00	0.40	30.32
			0.00	0.00			2" Ice	0.00	0.61	54.89
(2) LGP21401	B	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	0.00	1.12	135.29
			0.00	0.00			No Ice	0.00	0.23	10.00
			0.00	0.00			1/2" Ice	0.00	0.31	21.26
			0.00	0.00			1" Ice	0.00	0.40	30.32
			0.00	0.00			2" Ice	0.00	0.61	54.89
(2) LGP21401	C	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	0.00	1.12	135.29
			0.00	0.00			No Ice	0.00	0.23	10.00
			0.00	0.00			1/2" Ice	0.00	0.31	21.26
			0.00	0.00			1" Ice	0.00	0.40	30.32
			0.00	0.00			2" Ice	0.00	0.61	54.89
(2) LGP21903 Diplexer	A	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	0.00	1.12	135.29
			0.00	0.00			No Ice	0.00	0.18	10.00
			0.00	0.00			1/2" Ice	0.00	0.25	13.44
			0.00	0.00			1" Ice	0.00	0.32	16.93
			0.00	0.00			2" Ice	0.00	0.49	27.95
(2) LGP21903 Diplexer	B	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	0.00	0.94	71.54
			0.00	0.00			No Ice	0.00	0.18	10.00
			0.00	0.00			1/2" Ice	0.00	0.25	13.44
			0.00	0.00			1" Ice	0.00	0.32	16.93
			0.00	0.00			2" Ice	0.00	0.49	27.95
(2) LGP21903 Diplexer	C	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	0.00	0.94	71.54
			0.00	0.00			No Ice	0.00	0.18	10.00
			0.00	0.00			1/2" Ice	0.00	0.25	13.44
			0.00	0.00			1" Ice	0.00	0.32	16.93
			0.00	0.00			2" Ice	0.00	0.49	27.95
(2) RBS 6601	A	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	0.00	0.94	71.54
			0.00	0.00			No Ice	0.55	0.40	22.00
			0.00	0.00			1/2" Ice	0.70	0.52	34.88
			0.00	0.00			1" Ice	0.86	0.64	50.27
			0.00	0.00			2" Ice	1.19	0.91	89.38
(2) RBS 6601	B	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	1.97	1.55	206.33
			0.00	0.00			No Ice	0.55	0.40	22.00
			0.00	0.00			1/2" Ice	0.70	0.52	34.88
			0.00	0.00			1" Ice	0.86	0.64	50.27
			0.00	0.00			2" Ice	1.19	0.91	89.38
(2) RBS 6601	C	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	1.97	1.55	206.33
			0.00	0.00			No Ice	0.55	0.40	22.00
			0.00	0.00			1/2" Ice	0.70	0.52	34.88
			0.00	0.00			1" Ice	0.86	0.64	50.27
			0.00	0.00			2" Ice	1.19	0.91	89.38
DC6-48-60-18-8F Surge Suppression Unit	C	From Centroid-Le g	4.00	0.00	0.0000	152.00	4" Ice	1.97	1.55	206.33
			0.00	0.00			No Ice	1.47	1.47	32.80
			0.00	0.00			1/2" Ice	1.67	1.67	50.52
			0.00	0.00			1" Ice	1.88	1.88	70.72
			0.00	0.00			2" Ice	2.33	2.33	119.24
4' Dipole	B	From Leg	3.00	0.00	0.0000	107.00	4" Ice	3.38	3.38	252.92
			0.00	0.00			No Ice	0.79	0.79	10.00
			0.00	0.00			1/2" Ice	1.03	1.03	16.34
			0.00	0.00			1" Ice	1.28	1.28	25.48
			0.00	0.00			2" Ice	1.81	1.81	52.76
4' Dipole	B	From Leg	3.00	0.00	0.0000	97.00	4" Ice	3.11	3.11	147.65
							No Ice	0.79	0.79	10.00

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			ft	°	ft	ft ²	ft ²	lb
			0.00		1/2" Ice	1.03	1.03	16.34
			0.00		1" Ice	1.28	1.28	25.48
					2" Ice	1.81	1.81	52.76
					4" Ice	3.11	3.11	147.65

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
152.00	10'-8" Central Platform w/ 42" tower extension	33	44.523	2.9349	0.0032	7674
107.00	4' Dipole	33	22.218	2.0292	0.0002	3297
97.00	4' Dipole	33	18.203	1.8379	0.0002	3183

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	SF*P _{allow} lb	% Capacity	Pass Fail	
L1	150 - 129.25	Pole	TP17.4673x14.5x0.1875	1	-3473.10	542361.69	78.5	Pass	
L2	129.25 - 110	Pole	TP20.22x17.4673x0.47	2	-5418.02	*	84.6*	Pass	
L3	110 - 70	Pole	TP25.94x20.22x0.534	3	-10791.30	*	89.5*	Pass	
L4	70 - 31	Pole	TP31.52x24.5145x0.599	4	-18678.40	*	87.7*	Pass	
L5	31 - 0	Pole	TP36x29.7312x0.622	5	-26914.60	*	95.4*	Pass	
							Summary		
							Pole (L5)	95.4*	Pass
							RATING =	95.4*	Pass

*See Appendix E for the modification calculations.

APPENDIX C

Tower Elevation Drawings

DESIGNED APPURTENANCE LOADING

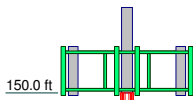
TYPE	ELEVATION	TYPE	ELEVATION
10'-8" Central Platform w/ 42" tower extension	152	(2) LGP21903 Diplexer	152
(2) 7770.00 w/ Mount Pipe	152	(2) LGP21903 Diplexer	152
(2) 7770.00 w/ Mount Pipe	152	(2) LGP21903 Diplexer	152
(2) 7770.00 w/ Mount Pipe	152	(2) RBS 6601	152
(2) 7770.00 w/ Mount Pipe	152	(2) RBS 6601	152
SBNH-1D6565C w/ Mount Pipe	152	(2) RBS 6601	152
AM-X-CD-17-65-00T w/ Mount Pipe	152	DC6-48-60-18-8F Surge Suppression Unit	152
AM-X-CD-17-65-00T w/ Mount Pipe	152	(2) LGP21401	107
(2) LGP21401	152	4' Dipole	97
(2) LGP21401	152	4' Dipole	97
(2) LGP21401	152		

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

TOWER DESIGN NOTES

1. Tower is located in Windham County, Connecticut.
2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 28 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 50 mph wind.
5. TOWER RATING: 78.5%



150.0 ft

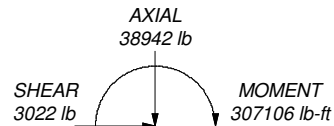
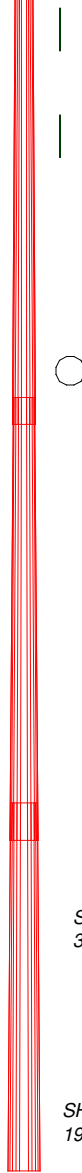
129.3 ft

110.0 ft

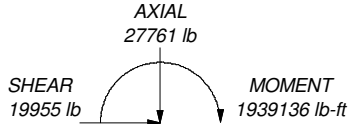
70.0 ft

31.0 ft

0.0 ft




TORQUE 155 lb-ft
28 mph WIND - 1.0000 in ICE



TORQUE 379 lb-ft
REACTIONS - 85 mph WIND

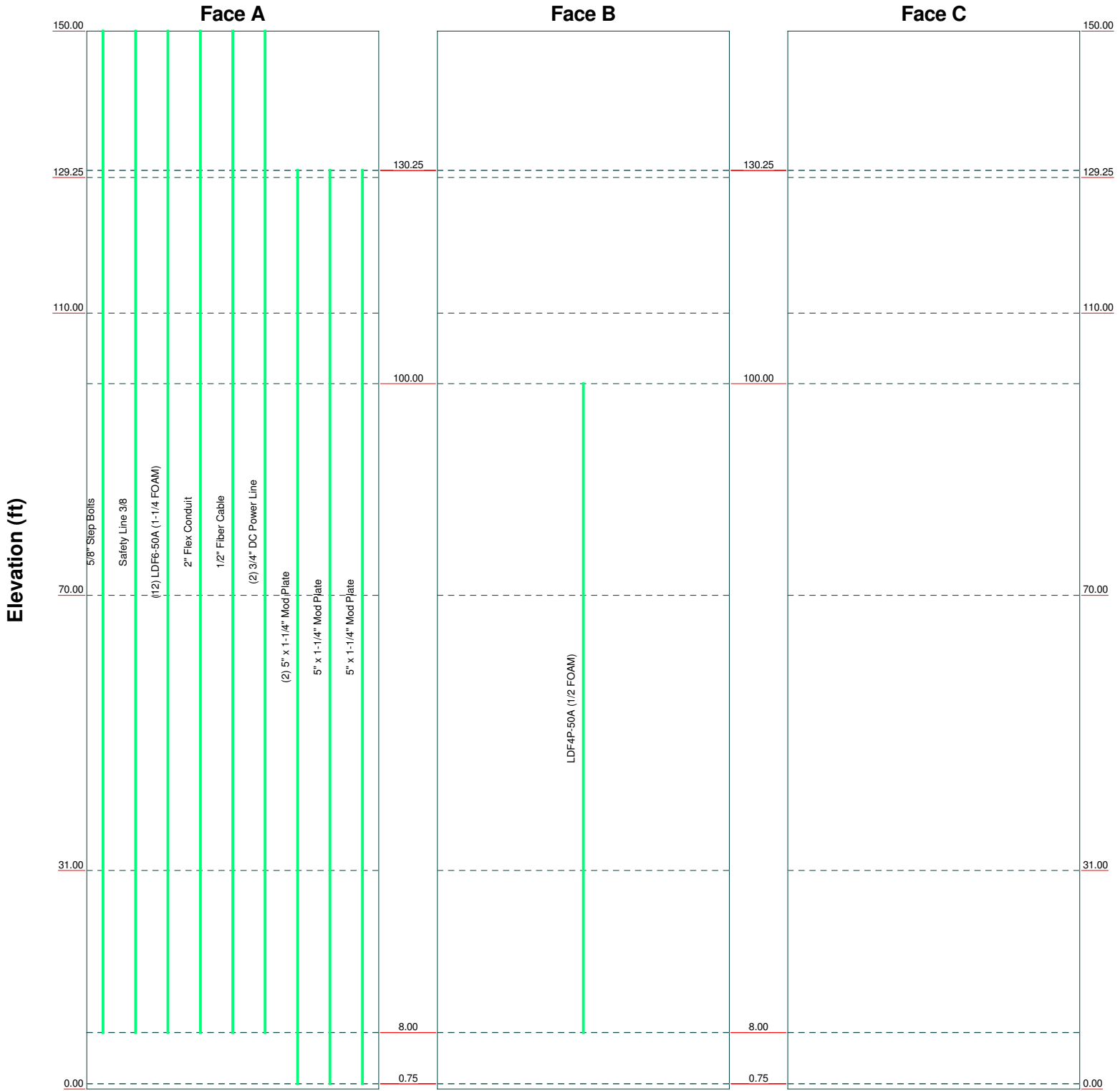
Section	Length (ft)	Number of Sides	Thickness (in)	Socket Length (ft)	Top Dia (in)	Bot Dia (in)	Grade	Weight (lb)
1	20.75	12	0.1875		14.5000	17.4673		673.4
2	19.25	12	0.4700		17.4673	20.2200	A572-65	1821.4
3	40.00	12	0.5340	2.50	20.2200	25.9400	A572-65	5276.7
4	41.50	12	0.5990	3.50	24.5145	31.5200	A572-65	7466.0
5	34.50	12	0.6220	29.7312	36.0000		A572-65	7581.3
								22820.9


 GPD Consulting Engineers	520 South Main Street, Suite 2531 Akron, OH 44311 Phone: 330.572.2100 FAX: 330.572.2101			Job: 71304 POMFRET-TYRONE RD
	Project: 2012832.07			Client: Pinnacle Wireless
	Code: TIA/EIA-222-F			Drawn by: jfields
	Path: C:\Users\jfields\Desktop\Drop\TNX\2012832.07\71304.er			Date: 01/04/13
	Scale: NTS			App'd: [Signature] Dwg No. E-1

Feedline Distribution Chart

0' - 150'

— Round
 — Flat
 — App In Face
 — App Out Face
 — Truss Leg



 GPD Consulting Engineers	520 South Main Street, Suite 2531 Akron, OH 44311 Phone: 330.572.2100 FAX: 330.572.2101		Job: 71304 POMFRET-TYRONE RD		
	Project: 2012832.07			Drawn by: jfields App'd:	
	Client: Pinnacle Wireless		Date: 01/04/13		Scale: NTS
	Code: TIA/EIA-222-F		Path: C:\Users\jfields\Desktop\Drop\TNX\2012832.07\71304.er		
	Path:		Dwg No. E-7		

APPENDIX D

Base Plate & Anchor Rod Calculations



Anchor Rod and Base Plate Stresses
71304 POMFRET-TYRONE RD
2012832.07

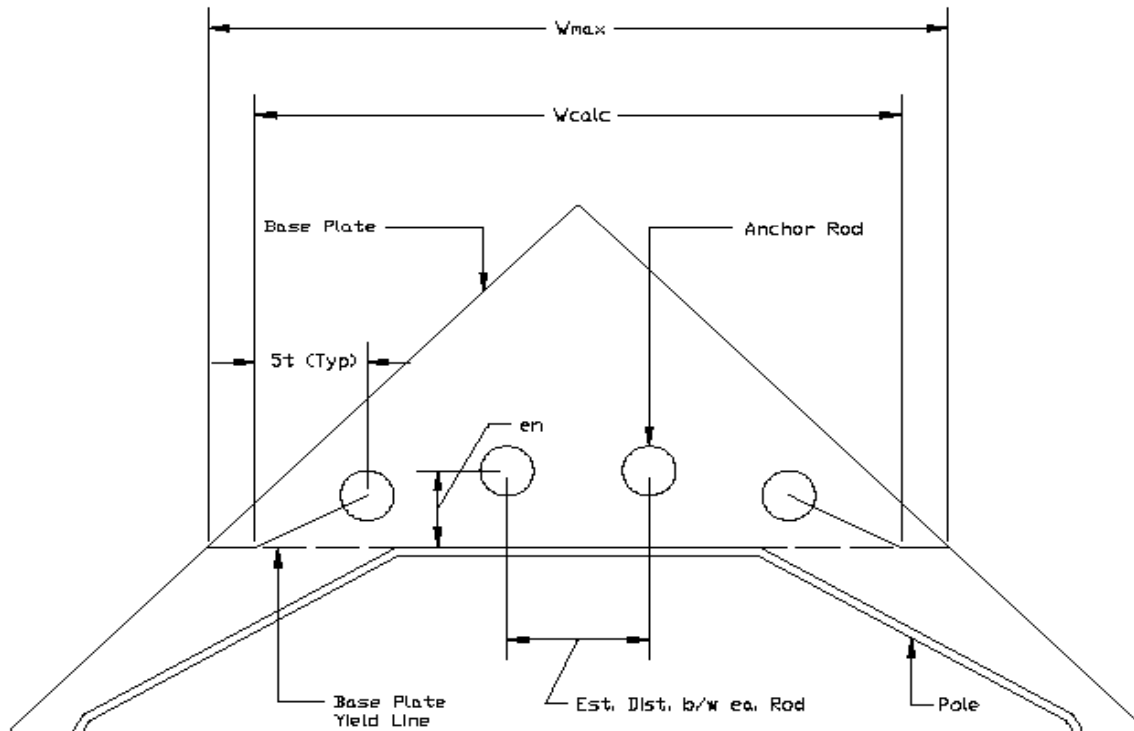
*Overturning Moment =	1176.39	k*ft
Axial Force =	19.22	k
Shear Force =	19.96	k

Acceptable Stress Ratio =	100.0%
---------------------------	--------

*Above reactions have been adjusted due to consideration of modifications. See attached hand calculations for determination of anchor rod forces in the analysis.

Anchor Rods		
Pole Diameter =	36	in
Number of Rods =	8	
Type =	Upset Rod	
Rod Yield Strength (Fy) =	75	ksi
ASIF =	1.333	
Rod Circle =	44	in
Rod Diameter =	2.25	in
Net Tensile Area =	3.25	in ²
Max Tension on Rod =	157.81	kips
Max Compression on Rod =	162.61	kips
Allow. Rod Force =	195.00	kips
Anchor Rod Capacity =	80.9%	OK

Base Plate		
Plate Strength (Fy) =	60	ksi
Plate Thickness =	2.5	in
Plate Width =	44	in
Est. Dist. b/w ea. Rod =	6	in
W _{calc} =	31.000	in
W _{max} =	26.225	in
w =	26.23	in
S =	27.32	in ³
fb =	44.76	ksi
Fb =	60	ksi
Base Plate Capacity =	74.6%	OK





GPD GROUP
Engineers • Architects • Planners

Job #: 2012832.07
Sheet No 1 Of 1

Calculated By: JDF Date: 1/4/2013
Checked By: _____ Date: _____

MODIFIED ANCHOR ROD CALCULATIONS

Moment from RISA (M) = 1939.14 kip-ft Code TIA/EIA-222-F
Axial from RISA (P) = 27.76 kip ASIF = 1.33
Shear from RISA (V) = 19.96 kip Allowable Stress Ratio = 105%

Inner Bolt Diameter = 2.25 in
Number Inner Bolts (N_{inner}) = 8 Inner Bolt Circle (BC_{inner}) = 44 in
Inner Bolt Area (A_{inner}) = 3.98 in² Total Area (A_{tot.in}) = 31.81 in² Axial, Inner Bolts (P*η_{in}) = 19.22 kips
Inner Bolt MOI (I_{o.inner}) = 1.26 in⁴ Percent Total Area (η_{in}) = 69.2% Shear, Inner Bolts (P*η_{in}) = 19.96 kips

Outer Bolt Diameter = 1.5 in
Number Outer Bolts (N_{outer}) = 8 Outer Bolt Circle (BC_{outer}) = 53.17 in
Outer Bolt Area (A_{outer}) = 1.77 in² Total Area (A_{tot.out}) = 14.14 in² Axial, Outer Bolts (P*η_{out}) = 8.54 kips
Outer Bolt MOI (I_{o.outer}) = 0.25 in⁴ Percent Total Area (η_{out}) = 30.8%

$$I_{inner} = 7707.75 \text{ in.}^4 \quad (N_{inner} * A_{inner} * BC_{inner}^2 / 8 + N_{inner} * I_{o.inner})$$

$$I_{outer} = 4997.80 \text{ in.}^4 \quad (N_{outer} * A_{outer} * BC_{outer}^2 / 8 + I_{o.outer})$$

$$I_{tot} = 12705.55 \text{ in.}^4 \quad (I_{inner} + I_{outer})$$

$$F_{inner} = 162.61 \text{ kips} \quad (M * (BC_{inner} / 2) * A_{inner} / I_{total} + P * \eta_{in} / N_{inner})$$

$$F_{outer} = 87.11 \text{ kips} \quad (M * (BC_{outer} / 2) * A_{outer} / I_{total} + P * \eta_{out} / N_{outer})$$

Rnt.outer / Ω = 72.89 kips

Modified Anchor Rod Rating
% = 89.6% OK

APPENDIX E

Modification Calculations



Reinforced Monopole Analysis
71304 POMFRET-TYRONE RD
2012832.07

Code =	TIA/EIA-222-F
AISF=	1.333
Max Stress Ratio=	1.05
# of Sides =	12

Geometry									Reactions				Output	Capacities		
Shape	Quantity	Section	Elevation (ft)	Pole Flat-Flat (In)	Wall t (in)	Fy (ksi)	K	Conn.Spacing (in)	Moment (k-ft)	Axial (k)	Shear (k)	Torsion (k-ft)	Equivalent t (in)	Pole	Reinforcement	Pass/Fail
Plate 3x1.25	4	L2	110	20.22	0.1875	65	0.8	18	305.86	5.42	9.2	0.26	0.470	50.0%	84.6%	Pass
Plate 4x1.25	4	L3	70	25.94	0.25	65	0.8	18	726.65	10.79	13.25	0.03	0.534	63.0%	89.5%	Pass
Plate 5x1.25	4	L4	31	31.52	0.3125	65	0.8	18	1301.94	18.68	16.97	0.03	0.599	68.0%	87.7%	Pass
Plate 5x1.25	4	L5	0	36	0.375	65	0.8	18	1939.14	26.91	17.98	0.38	0.622	74.4%	95.4%	Pass

APPENDIX F

Flange Plate & Flange Bolt Calculations



Existing Flange Connection @ 110'
71304 POMFRET-TYRONE RD
2012832.07

*O.T. Moment =	82.3267	k*ft
Axial =	2.09	kips
Shear =	9.20	kips

Acceptable Stress Ratio	=	105.0%
-------------------------	---	--------

*Above reactions have been adjusted due to consideration of modifications. See attached hand calculations for determination of flange bolt forces used in the analysis.

Flange Bolts	
# Bolts =	12
Bolt Type =	A325
F _t =	44 ksi
ASIF =	1.333
Bolt Circle =	23 in
Bolt Diameter =	1 in

Tension & Shear (ASD, Section J3.5)	
F _v =	21 ksi
Nominal Area =	0.79 in ²
f _v =	0.98 ksi
Applied Shear =	0.77 kips
Allowable Shear =	21.99 kips
F _t ² - 4.39(f _v ²) ^{1/2} =	43.95 ksi
Allowable Bolt Stress =	58.60325 ksi
B =	46.03 kips

Prying Action Check
 N/A, top flange thickness > t_c

Max Comp. on Bolt =	14.48 kips
Max Tension on Bolt =	14.13 kips
Shear Capacity =	3.5%
Tensile Capacity =	30.7%

Bolt Capacity = 30.7% OK

Pole Information	
Shaft Diam. (Upper) =	20.22 in
Thickness (Upper) =	0.1875 in
# of Sides (Upper) =	12
F _y (Upper) =	65 ksi
Shaft Diam. (Lower) =	20.22 in
Thickness (Lower) =	0.25 in
# of Sides (Lower) =	12
F _y (Lower) =	65 ksi

Upper Flange Plate	
Location =	External
Plate Strength (F _y) =	60 ksi
Plate Thickness =	1 in
Outer Diameter =	26 in
w _{calc} =	10.96 in
w _{max} =	15.95 in
w =	10.96 in
S =	1.83 in ³
f _b =	15.29 ksi
F _b =	60 ksi
UP Capacity =	25.5% OK

Upper Stiffeners	
Configuration =	None

Lower Flange Plate	
Location =	External
Plate Strength (F _y) =	60 ksi
Plate Thickness =	1 in
Outer Diameter =	26 in
w _{calc} =	10.96 in
w _{max} =	15.95 in
w =	10.96 in
S =	1.83 in ³
f _b =	15.29 ksi
F _b =	60 ksi
LP Capacity =	25.5% OK

Lower Stiffeners	
Configuration =	None



GPD GROUP
Engineers • Architects • Planners

Job #: 2012832.07
Sheet No. 1 Of 1

Calculated By: JDF Date: 1/4/2013
Checked By: AW Date: 1/4/2013

BOLT AND BRIDGE STIFFENER CALCULATIONS

@ 110'

Tower Type = **Monopole**
Acceptable Stress Ratio = **105.0%**
Code = **TIA/EIA-222-F**
ASIF = **1.33**

Moment from RISA (M) = **305.86 kip-ft**
Axial from RISA (P) = **5.42 kip**

Inner Bolt Diameter = **1 in**
Inner Bolt Area (A_{inner}) = **0.79 in²**
Inner Bolt MOI ($I_{o,inner}$) = **0.05 in⁴**
Number Inner Bolts (N_{inner}) = **12**

Inner Bolt Circle (BC_{inner}) = **23 in**
Total Area ($A_{tot.in}$) = **9.42 in²**
Percent Total Area (η_{in}) = **38.6%**

Axial, Inner Bolts ($P*\eta_{in}$) = **2.09 kips**

Bridge Stiffener Width = **3.00 in**
Bridge Stiffener Thickness = **1.25 in**
Bridge Stiffener Unbraced Length = **12.00 in**
Bridge Stiffener Area (A_{pl}) = **3.75 in²**
Bridge Stiffener Average MOI (I_p) = **1.65 in⁴**
Number Bridge Stiffeners (N_{pl}) = **4**

Bridge Stiffener Circle (BC_{pl}) = **30 in**
Total Area ($A_{tot.pl}$) = **15.00 in²**
Percent Total Area (η_{pl}) = **61.4%**

Axial, Bridge Stiffeners ($P*\eta_{pl}$) = **3.33 kips**

$I_{inner} = 623.80 \text{ in.}^4$ ($N_{inner} * A_{inner} * BC_{inner}^2 / 8 + N_{inner} * I_{o,inner}$)
 $I_{outer} = 0.00 \text{ in.}^4$ ($N_{outer} * A_{outer} * BC_{outer}^2 / 8 + N_{outer} * I_{o,outer}$)
 $I_{pl} = 1694.10 \text{ in.}^4$ ($N_{pl} * A_{pl} * BC_{pl}^2 / 8 + N_{pl} * I_{o,pl}$)
 $I_{tot} = 2317.90 \text{ in.}^4$ ($I_{inner} + I_{outer} + I_{pl}$)

$P_{u.t,inner} = 14.13 \text{ kips}$ ($M * (BC_{inner} / 2) * A_{inner} / I_{total} - P * \eta_{in} / N_{inner}$)
 $P_{u.t,pl} = 88.24 \text{ kips}$ ($M * (BC_{pl} / 2) * A_{pl} / I_{total} - P * \eta_{pl} / N_{pl}$)
 $P_{u.c,pl} = 89.90 \text{ kips}$ ($M * (BC_{pl} / 2) * A_{pl} / I_{total} + P * \eta_{pl} / N_{pl}$)
ASIF*Pnt.bolt / Ω = **46.03 kips**
Bolt Rating = **30.7% OK**

Number Bridge Stiffeners (N_{pl}) = **4**

$f_y = 65 \text{ ksi}$
 $f_u = 80 \text{ ksi}$

Plate Width = **3.00 in**
Plate Thickness = **1.25 in**
Plate Unbraced Length = **12.00 in**
Plate Area (A_{pl}) = **3.75 in²**
Upper Pole Diameter = **20.22 in**
Flange Plate Diameter = **26.00 in**
Flange Plate to Bridge Stiffener Gap = **2.11 in**
Bridge Stiffener Circle (BC_{pl}) = **30.00 in**
Bridge Stiffener MOI (I_p) = **2.81 in⁴**

$I_{pl} = 1694.10 \text{ in.}^4$ ($N_{pl} * A_{pl} * BC_{pl}^2 / 8 + N_{pl} * I_{o,pl}$)
Axial Capacity Required = **89.90 kips** ($M * (BC_{pl} / 2) * A_{pl} / I_{total} + P * \eta_{pl} / N_{pl}$)

Load Eccentricity, e = **6.50 in** (from weld to center of stiffener area)

Moment Capacity Required = **0.00 kip-in**

E = **29000 ksi**

K = **1.00**

$r_{min} = 0.36$

$KL/r_{min} = 33.255$

$F_e = 258.81 \text{ ksi}$

$F_{cr} = 58.51 \text{ ksi}$

$P_{nc} / \Omega = 131.39 \text{ kips}$

$P_{nt} / \Omega = 145.96 \text{ kips}$

S = **1.88 in³**

Z = **2.81 in³**

$L_b / t^2 = 23.04$

$M_{n,LTB} = \text{n/a}$

$M_p = 182.81 \text{ kip-in}$

$M_n / \Omega = 109.47 \text{ kip-in}$

Stiffener Rating = **68.4% OK**

Bridge Stiffener Welds

Bridge Stiffener Height = **27.00 in**
a value (from AISC Table 8-4) = **0.241**
C value (from AISC Table 8-4) = **3.31**
Fillet Size = **0.1875 in**
Weld Rating = **67.1% OK**

APPENDIX G

Foundation Calculations



Mat Foundation Analysis
71304 POMFRET-TYRONE RD
2012832.07

General Info	
Code	TIA/EIA-222-F (ASD)
Bearing On	Soil
Foundation Type	Mono Pad
Pier Type	Square
Reinforcing Known	No
Max Capacity	1

Tower Reactions	
Moment, M	1939.14 k-ft
Axial, P	27.76 k
Shear, V	19.96 k

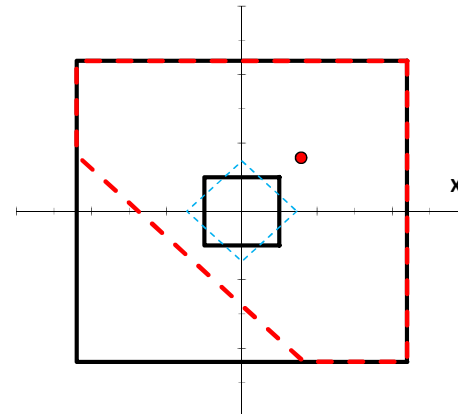
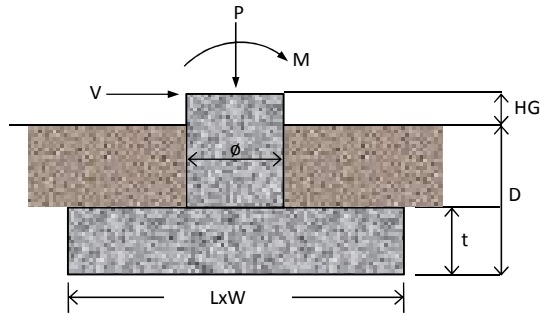
Pad & Pier Geometry		
Pier Width, ϕ	5	ft
Pad Length, L	22	ft
Pad Width, W	22	ft
Pad Thickness, t	3	ft
Depth, D	8	ft
Height Above Grade, HG	0.5	ft

Pad & Pier Reinforcing		
Rebar Fy		ksi
Concrete Fc'		ksi
Clear Cover		in
Reinforced Top & Bottom?		
Pad Reinforcing Size		
Pad Quantity Per Layer		
Pier Rebar Size		
Pier Quantity of Rebar		

Soil Properties	
Soil Type	Granular
Soil Unit Weight	120 pcf
Angle of Friction, ϕ	28°
Bearing Type	Gross
Ultimate Bearing	12 ksf
Water Table Depth	1 ft
Frost Depth	4 ft

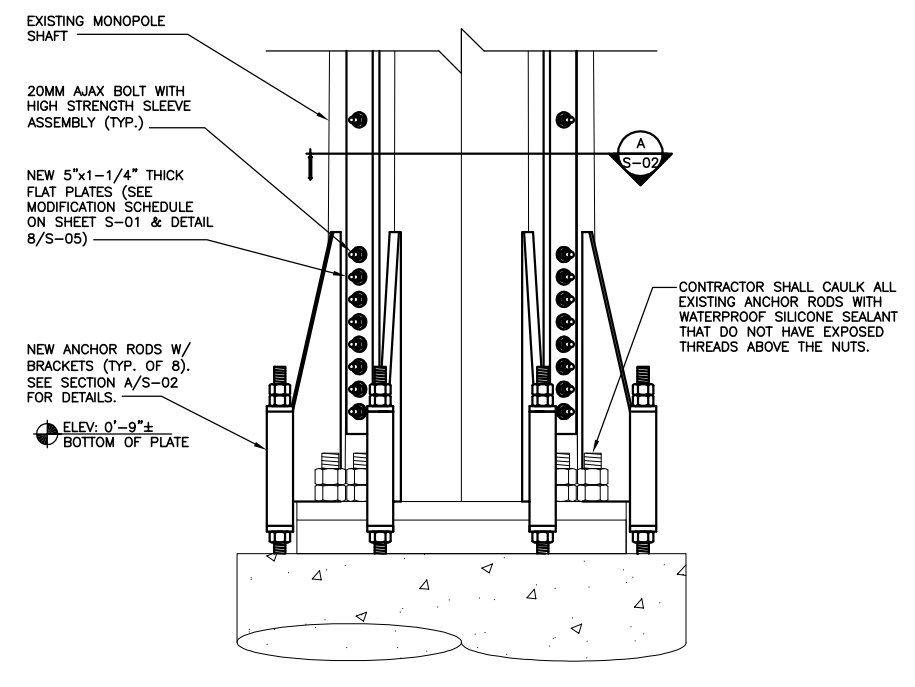
Bearing Summary			Load Case
Qxmax	1.86	ksf	1D+1W
Qymax	1.86	ksf	1D+1W
Qmax @ 45°	2.44	ksf	1D+1W
Q _{(all) Gross}	6.00	ksf	
Controlling Capacity	40.7%	Pass	

Overturning Summary (Required FS=1.5)			Load Case
FS(ot)x	1.95	≥1.5	1D+1W
FS(ot)y	1.95	≥1.5	1D+1W
Controlling Capacity	76.8%	Pass	

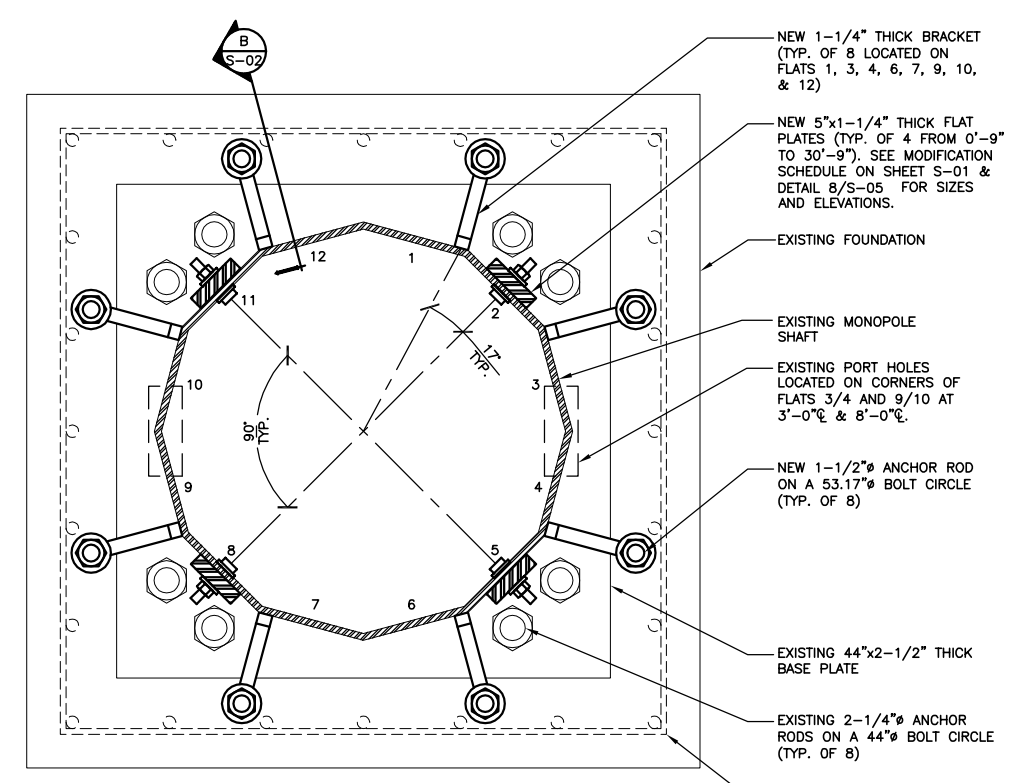


APPENDIX H

Modification Drawings



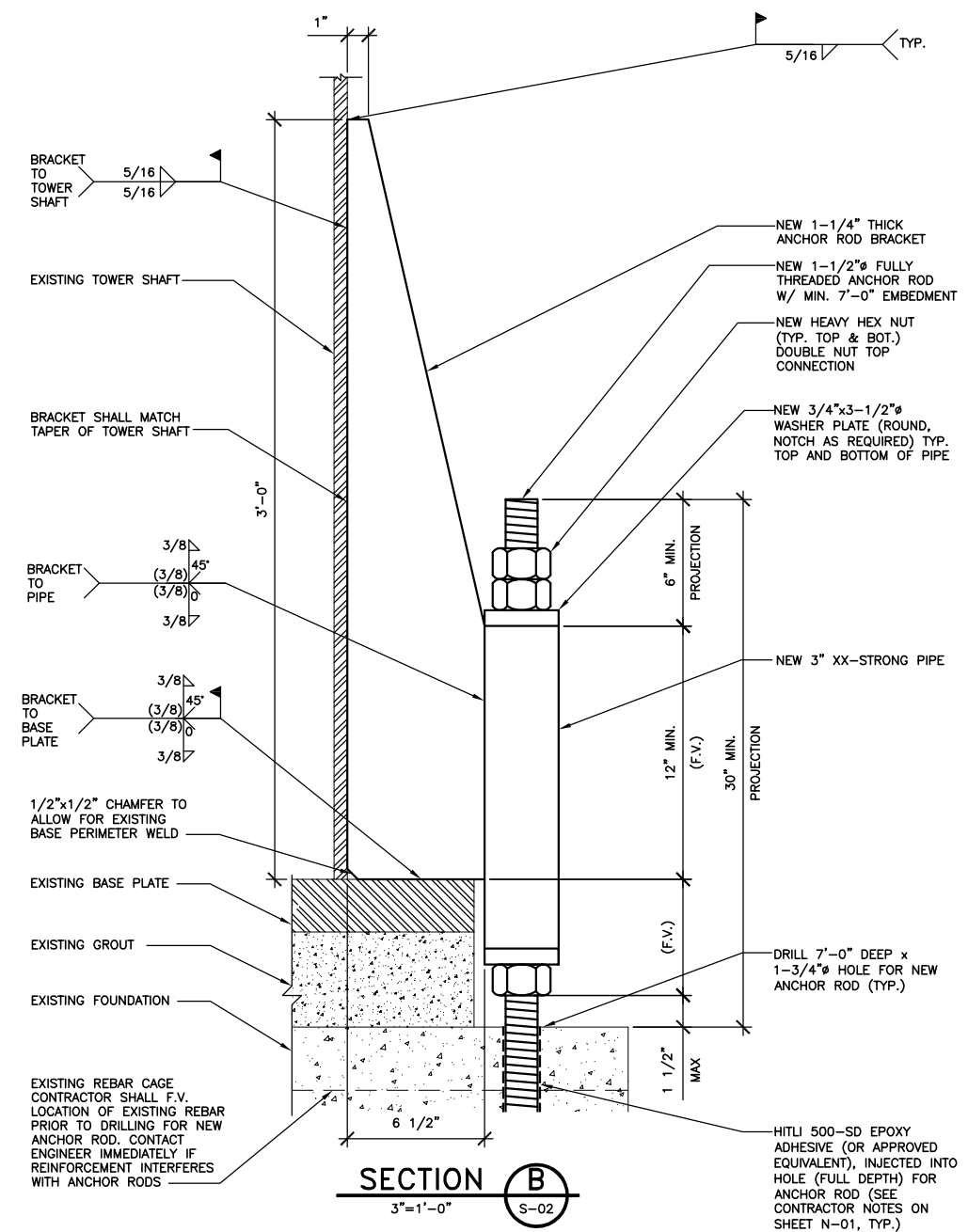
DETAIL 1
1"=1'-0" S-02



SECTION A
1-1/2"=1'-0" S-02

NOTE: FLAT NUMBERS DEPICTED IN THIS DRAWING MAY VARY FROM THE NUMBERING IN THE FIELD. CONTRACTOR MAY ADJUST FLAT NUMBERS TO MATCH EXISTING FIELD CONDITIONS. MODIFICATIONS SHALL BE INSTALLED IN THE APPROPRIATE ORIENTATION AND/OR LOCATION REGARDLESS OF THE NUMBERING SHOWN ON THE DRAWINGS.

NOTE: STEP PEGS AND SAFETY CLIMB TO BE REMOVED AND REPLACED AS REQUIRED.



SECTION B
3"=1'-0" S-02

REV.	DATE	DESCRIPTION

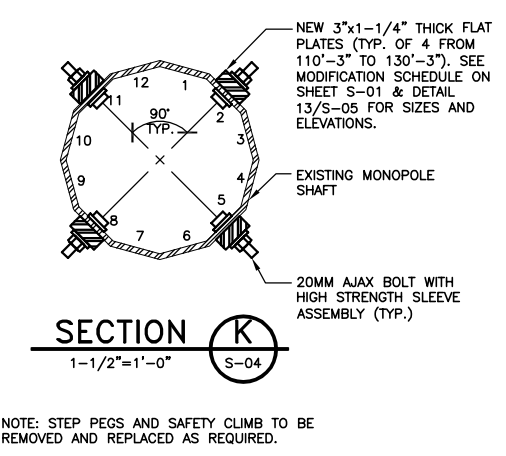
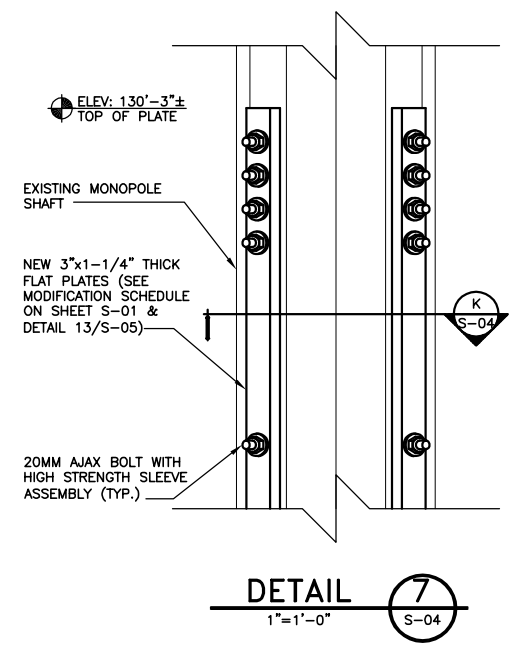
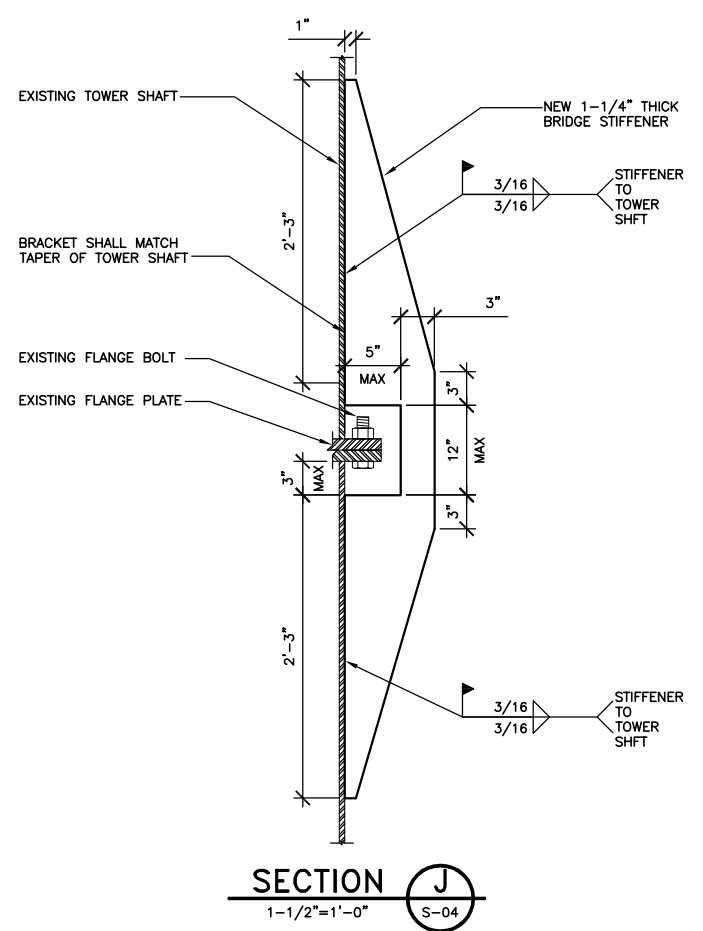
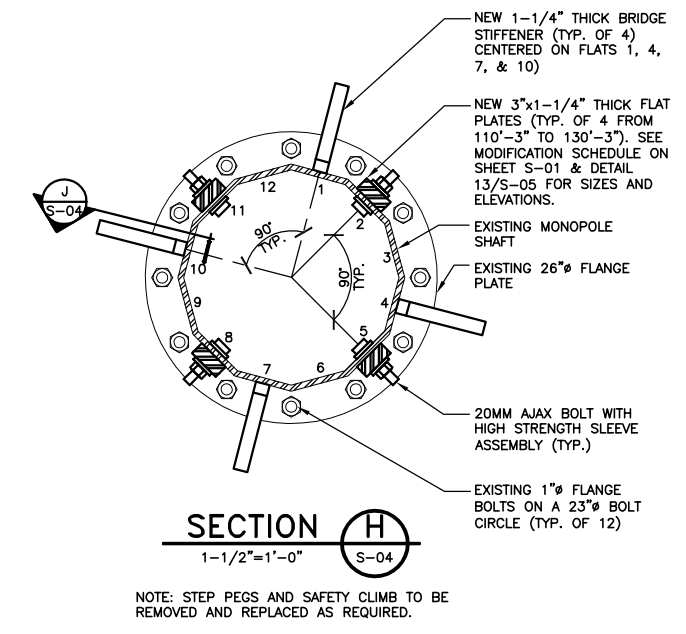
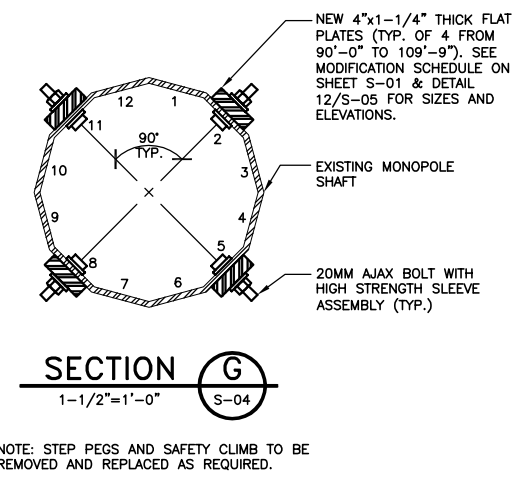
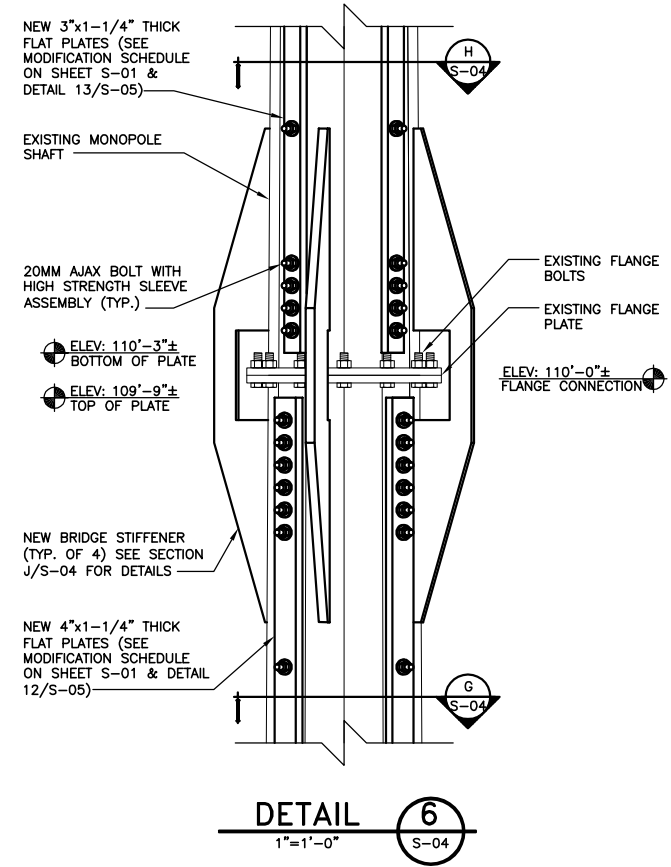
71304-POMFRET-TYRONE RD
82 TYRONE RD
PROMFRET, CT 06258

MODIFICATION SECTIONS & DETAILS

ISSUED FOR:	
PERMIT	01/04/13
BID	-
CONSTRUCTION	-
RECORD	-
PROJECT MANAGER	DESIGNER
DMH	JDF

JOB NO.
2012832.07

S-02



REV.	DATE	DESCRIPTION

71304-POMFRET-TYRONE RD
82 TYRONE RD
PROMFRET, CT 06258

ADDITIONAL SECTIONS & DETAILS

ISSUED FOR:	
PERMIT	01/04/13
BID	-
CONSTRUCTION	-
RECORD	-
PROJECT MANAGER	DESIGNER
DMH	JDF

JOB NO.
2012832.07

S-04



MODIFICATION INSPECTION CHECKLIST

BEFORE CONSTRUCTION		DURING CONSTRUCTION		AFTER CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM	CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM	CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
X	MODIFICATION INSPECTION CHECKLIST DRAWING	X	CONSTRUCTION INSPECTIONS	X	MODIFICATION INSPECTOR REDLINE OR RECORD DRAWING(S)
X	ENGINEER OF RECORD APPROVED SHOP DRAWINGS	X	FOUNDATION INSPECTIONS	X	POST INSTALLED ANCHOR ROD PULL-OUT TESTING
X	FABRICATION INSPECTION	X	CONCRETE COMP. STRENGTH AND SLUMP TESTS	X	PHOTOGRAPHS
X	FABRICATOR CERTIFIED WELD INSPECTION	X	POST INSTALLED ANCHOR ROD VERIFICATION	ADDITIONAL TESTING AND INSPECTIONS:	
X	MATERIAL TEST REPORT	X	BASE PLATE GROUT VERIFICATION		
X	FABRICATOR NDE INSPECTION	X	CONTRACTOR'S CERTIFIED WELD INSPECTION		
X	NDE REPORT OF MONOPOLE BASE PLATE (AS REQUIRED)	X	EARTHWORK: LIFT AND DENSITY		
X	PACKING SLIPS	X	ON SITE COLD GALVANIZING VERIFICATION		
ADDITIONAL TESTING AND INSPECTIONS:		-	GUY WIRE TENSION REPORT		
		X	GC AS-BUILT DOCUMENTS		
		ADDITIONAL TESTING AND INSPECTIONS:			

NOTE: X DENOTES A DOCUMENT NEEDED FOR THE MODIFICATION INSPECTION REPORT
 - DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE MODIFICATION INSPECTION REPORT

MODIFICATION INSPECTION NOTES:

GENERAL

- THE MODIFICATION INSPECTION IS A VISUAL INSPECTION OF TOWER MODIFICATIONS AND A REVIEW OF CONSTRUCTION INSPECTIONS AND OTHER REPORTS TO ENSURE THE INSTALLATION WAS CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, NAMELY THE MODIFICATION DRAWINGS, AS DESIGNED BY THE ENGINEER OF RECORD.
- THE MODIFICATION INSPECTION IS TO CONFIRM INSTALLATION CONFIGURATION AND WORKMANSHIP ONLY AND IS NOT A REVIEW OF THE MODIFICATION DESIGN ITSELF, NOR DOES THE MODIFICATION INSPECTOR TAKE OWNERSHIP OF THE MODIFICATION DESIGN. OWNERSHIP OF THE STRUCTURAL MODIFICATION DESIGN EFFECTIVENESS AND INTENT RESIDES WITH THE ENGINEER OF RECORD AT ALL TIMES.
- TO ENSURE THAT THE REQUIREMENTS OF THE MODIFICATION INSPECTION ARE MET, IT IS VITAL THAT THE GENERAL CONTRACTOR (GC) AND THE MODIFICATION INSPECTOR BEGIN COMMUNICATING AND COORDINATING AS SOON AS A PO OR PAYMENT IS RECEIVED. IT IS EXPECTED THAT EACH PARTY WILL BE PROACTIVE IN REACHING OUT TO THE OTHER PARTY. CONTACT LISTED ON THE TITLE SHEET SHALL BE CONTACTED IF SPECIFIC INSPECTOR CONTACT INFORMATION IS NOT KNOWN.

MODIFICATION INSPECTOR

- THE MODIFICATION INSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A PO OR PAYMENT FOR THE MODIFICATION INSPECTION TO:
 - REVIEW THE REQUIREMENTS OF THE MODIFICATION INSPECTION CHECKLIST
 - WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS
 - DISCUSS ANY SITE SPECIFIC INSPECTIONS OR CONCERNS

- THE MODIFICATION INSPECTOR IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (GC) INSPECTION AND TEST REPORTS, REVIEWING THE DOCUMENTS FOR ADHERENCE TO THE CONTRACT DOCUMENTS, CONDUCTING THE IN-FIELD INSPECTIONS, AND SUBMITTING THE MODIFICATION INSPECTION REPORT.

GENERAL CONTRACTOR

- THE GC IS REQUIRED TO CONTACT THE MODIFICATION INSPECTOR AS SOON AS RECEIVING A PO OR PAYMENT FOR THE MODIFICATION INSTALLATION OR TURNKEY PROJECT TO:
 - REVIEW THE REQUIREMENTS OF THE MODIFICATION INSPECTION CHECKLIST
 - WORK WITH THE MI INSPECTOR TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE MODIFICATION INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS
 - BETTER UNDERSTAND ALL INSPECTION AND TESTING REQUIREMENTS

- THE GC SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IN ACCORDANCE WITH THE REQUIREMENTS OF THE MODIFICATION INSPECTION CHECKLIST.

RECOMMENDATIONS

- THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING A MODIFICATION INSPECTION REPORT:
 - IT IS SUGGESTED THAT THE GC PROVIDE A MINIMUM OF 5 BUSINESS DAYS NOTICE, PREFERABLY 10, TO THE MODIFICATION INSPECTOR AS TO WHEN THE SITE WILL BE READY FOR THE MODIFICATION INSPECTION TO BE CONDUCTED.
 - THE GC AND MODIFICATION INSPECTOR COORDINATE CLOSELY THROUGHOUT THE ENTIRE PROJECT.
 - WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MODIFICATION INSPECTOR ON-SITE SIMULTANEOUSLY FOR ANY GUY WIRE TENSIONING OR RE-TENSIONING OPERATIONS.
 - IT MAY BE BENEFICIAL TO INSTALL ALL TOWER MODIFICATIONS PRIOR TO CONDUCTING THE FOUNDATION INSPECTIONS TO ALLOW FOUNDATION AND MODIFICATION INSPECTION(S) TO COMMENCE WITH ONE SITE VISIT.
 - WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MODIFICATION INSPECTOR ON-SITE DURING THE MODIFICATION INSPECTION TO HAVE ANY DEFICIENCIES CORRECTED DURING THE INITIAL MODIFICATION INSPECTION. THEREFORE, THE GC MAY CHOOSE TO COORDINATE THE MODIFICATION INSPECTION CAREFULLY TO ENSURE ALL CONSTRUCTION FACILITIES ARE AT THEIR DISPOSAL WHEN THE MI INSPECTOR IS ON SITE.

CANCELLATION OR DELAYS IN SCHEDULED MODIFICATION INSPECTION

- IF THE GC AND MODIFICATION INSPECTOR AGREE TO A DATE ON WHICH THE MODIFICATION INSPECTION WILL BE CONDUCTED, AND EITHER PARTY CANCELS OR DELAYS, THE TOWER OWNER SHALL NOT BE RESPONSIBLE FOR ANY COSTS, FEES, LOSS OF DEPOSITS AND/OR OTHER PENALTIES RELATED TO THE CANCELLATION OR DELAY INCURRED BY EITHER PARTY FOR ANY TIME (E.G. TRAVEL AND LODGING, COSTS OF KEEPING EQUIPMENT ON-SITE, ETC.). EXCEPTIONS MAY BE MADE IN THE EVENT THAT THE DELAY/CANCELLATION IS CAUSED BY WEATHER OR OTHER CONDITIONS THAT MAY COMPROMISE THE SAFETY OF THE PARTIES INVOLVED.

CORRECTION OF FAILING MODIFICATION INSPECTION

- IF THE MODIFICATION INSTALLATION WOULD FAIL THE MODIFICATION INSPECTION ("FAILED MODIFICATION INSPECTION"), THE GC SHALL WORK WITH MODIFICATION INSPECTOR TO COORDINATE A REMEDIATION PLAN IN ONE OF TWO WAYS:
 - CORRECT FAILING ISSUES TO COMPLY WITH THE SPECIFICATIONS CONTAINED IN THE ORIGINAL CONTRACT DOCUMENTS AND COORDINATE A SUPPLEMENT MODIFICATION INSPECTION.
 - OR, WITH TOWER OWNER'S APPROVAL, THE GC MAY WORK WITH THE ENGINEER OF RECORD TO RE-ANALYZE THE MODIFICATION/REINFORCEMENT USING THE AS-BUILT CONDITION.

VERIFICATION INSPECTIONS

- TOWER OWNER RESERVES THE RIGHT TO CONDUCT A VERIFICATION INSPECTION TO VERIFY THE ACCURACY AND COMPLETENESS OF PREVIOUSLY COMPLETED MODIFICATION INSPECTION(S) ON TOWER MODIFICATION PROJECTS.
- VERIFICATION INSPECTION MAY BE CONDUCTED BY AN INDEPENDENT FIRM AFTER A MODIFICATION PROJECT IS COMPLETED, AS MARKED BY THE DATE OF AN ACCEPTED "PASSING MODIFICATION INSPECTION" OR "PASS AS NOTED MODIFICATION INSPECTION" REPORT FOR THE ORIGINAL PROJECT.

REQUIRED PHOTOS

- BETWEEN THE GC AND THE MI INSPECTOR THE FOLLOWING PHOTOGRAPHS ARE TO BE TAKEN AND INCLUDED IN THE MODIFICATION INSPECTION REPORT:
 - PRE-CONSTRUCTION GENERAL SITE CONDITION
 - PHOTOGRAPHS DURING THE REINFORCEMENT MODIFICATION CONSTRUCTION/ERECTION AND INSPECTION
 - RAW MATERIALS
 - PHOTOS OF ALL CRITICAL DETAILS
 - FOUNDATION MODIFICATIONS
 - WELD PREPARATION
 - BOLT INSTALLATION AND TORQUE
 - FINAL INSTALLED CONDITION
 - SURFACE COATING REPAIR
 - POST CONSTRUCTION PHOTOGRAPHS
 - FINAL INFIELD CONDITION
 - ANY OTHER PHOTOS DEEMED RELEVANT TO SHOW COMPLETE DETAILS OF MODIFICATIONS
- PHOTOS OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED INADEQUATE.

REV.	DATE	DESCRIPTION

71304-POMFRET-TYRONE RD
 82 TYRONE RD
 PROMFRET, CT 06258

MODIFICATION INSPECTION & CHECKLIST

ISSUED FOR:	
PERMIT	01/04/13
BID	-
CONSTRUCTION	-
RECORD	-
PROJECT MANAGER	DESIGNER
DMH	JDF

JOB NO.
2012832.07

MI-01