

QC Development
PO Box 916
Storrs, CT 06268
860-670-9068
Mark.Roberts@QCDevelopment.net

September 28, 2018

Melanie A. Bachman Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Notice of Exempt Modification – New Cingular Wireless PCS, LLC (AT&T) – CT1029 335 South Washington Street, Plainville, CT 06062 N 41.65311111 W 72.87686111

Dear Ms. Bachman:

AT&T currently maintains nine (9) antennas at the 122-foot level of the existing 120-foot Monopole at 335 South Washington Street, Plainville, CT. The tower is owned by Crown Castle. The property is owned by the Display Properties LLC. AT&T now intends to add three new (3) Kathrein 800-10965 antennas. AT&T also intends to install (3) Ericsson 4426-B66 and (3) 4478-B5 Remote Radio Units (RRU), also at the 120-foot level.

This facility was approved by the Connecticut Siting Council in Docket # 281 on June 23, 2004. Since no further modification to the overall facility height is proposed, this modification therefore complies with the aforementioned approvals.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Katherine Pugliese, Chair of the Town Council for the Town of Plainville, and the Plainville Planning and Economic Development Department, as well as the property owner and the tower owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing structure.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Please feel free to call me at (860) 670-9068 with any questions regarding this matter. Thank you for your consideration.

Sincerely,

Mark Roberts

QC Development

Consultant for AT&T

Attachments

cc: Katherine Pugliese - as Elected Official

Mark DeVoe – Director of Planning & Economic Development

Display Properties LLC - as Property Owner

Crown Castle - Tower Owner (via e-mail)

Power Density

Existing Loading on Tower

Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm^2)	Freq. Band (MHz**)	Limit S (mW /cm^2)	%MPE
Other Carriers*							7.64%
AT&T UMTS	1	414	120	0.0109	850	0.5667	0.19%
AT&T UMTS	1	656	120	0.0172	1900	1.0000	0.17%
AT&T LTE	1	1476	120	0.0388	700	0.4893	0.79%
AT&T LTE	3	4842	120	0.3816	1900	1.0000	3.82%
AT&T LTE	1	1285	120	0.0388	2300	1.0000	0.34%
Site Total							12.95%

^{*}Per CSC Records (available upon request, includes calculation formulas)

Proposed Loading on Tower

Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm^2)	Freq. Band (MHz**)	Limit S (mW /cm^2)	%МРЕ
Other Carriers*							7.64%
AT&T UMTS	1	414	120	0.0115	850	0.5667	0.20%
AT&T LTE	1	656	120	0.0408	700	1.0000	0.41%
AT&T LTE	1	1476	120	0.0277	850	0.5667	0.49%
AT&T LTE	2	4842	120	0.2680	1900	1.0000	2.68%
AT&T LTE	1	4842	120	0.1403	2100	1.0000	1.40%
AT&T LTE	1	1285	120	0.0356	2300	1.0000	0.23%
Site Total							13.05%

^{*}Per CSC Records (available upon request, includes calculation formulas)

^{**} If a range of frequencies are used, such as 880-894, enter the lowest value, i.e. 880

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PROJECT INFORMATION

ITEMS TO BE MOUNTED ON MONOPOLE:

• NEW HANDRAIL KIT SITEPRO1 P/N HRK12-U.

• NEW REINFORCEMENT KIT SITEPRO1 P/N PRK-1245.

• NEW AT&T ANTENNAS: (80010965) (TYP. OF 1 PER SECTOR, TOTAL OF 3) (POSITION 2

FOR BETA AND POSITION 3 FOR ALPHA AND GAMMA).

• NEW AT&T RRUS: RRUS B66 4426 (AWS) (TYP. OF 1 PER SECTOR, TOTAL OF 3).

• NEW AT&T RRUS: RRUS B5 4478 (850) (TYP. OF 1 PER SECTOR, TOTAL OF 3). • NEW SURGE ARRESTOR DC6-48-60-18-8C (TOTAL OF 1) WITH (2) DC POWER

CABLES, & (1) FIBER RUN.

ITEMS TO BE MOUNTED IN EQUIPMENT SHELTER:
• PROPOSED ADD 2ND XMU IN LTE RACK.

• (9) ANTENNAS, (9) RRU'S, (2) SURGE ARRESTOR, (6) TMA'S, (6) COMBINERS,

(12) 1-5/8" COAX, (2) DC POWER CABLES, & (1) FIBER RUN.

SITE ADDRESS:

335 SOUTH WASHINGTON STREET PLAINVILLE, CT 06062

LATITUDE:

41.65311° N 41° 39' 11.03" N

LONGITUDE:

72.87692° W 72° 52' 36.90" W MONOPOLE / INDOOR EQUIPMENT

TYPE OF SITE: TOWER HEIGHT:

121'-0"±

RAD CENTER: 122'-0"±

JURISDICTION:

NATIONAL, STATE & LOCAL CODES OR ORDINANCES

CURRENT USE:

TELECOMMUNICATIONS FACILITY

PROPOSED USE:

TELECOMMUNICATIONS FACILITY



SITE NUMBER: CT1029

SITE NAME: PLAINVILLE SOUTH WASHINGTON STREET

FA CODE: 10105805

PACE ID: MRCTB031396, MRCTB032005

PROJECT: LTE 4C/5C 2019 UPGRADE

	DRAWING INDEX	
SHEET NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	1
GN-1	GENERAL NOTES	1
A-1	COMPOUND & EQUIPMENT PLAN	1
A-2	ANTENNA LAYOUTS & ELEVATION	1
A-3	DETAILS	1
SN-1	STRUCTURAL NOTES	1
S-1	STRUCTURAL DETAILS	1
RF-1	RF-PLUMBING DIAGRAM	1
RF-2	RF-PLUMBING DIAGRAM	1
G-1	GROUNDING DETAILS	1

CCI SITE NAME: PLAINVILLE SOUTH WASHINGTON STREET

VICINITY MAP

DIRECTIONS TO SITE:191 SOUTH TOWARD NEW HAVEN. TAKE EXIT 22 NORTH TOWARD NEW BRITAIN. MERGE ONTO CT-72 WEST VIA EXIT 28, ON THE LEFT, TOWARD BRISTOL. TAKE CT-177/NORTH WASHINGTON STREET EXIT. LEFT ONTO NORTH WASHINGTON STREET. END AT 335 SOUTH WASHINGTON.

SITE ACCESS IDS OFF ROBERT JACKSON WAY ACCESS RD IS RIGHT BEFORE LAWN CARE SERVICE. (SEE PICTURES FOR ACCESSING CELL SITE IN PAIR GAIN DATA BASE).

PROJECT SITE

GENERAL NOTES

- THIS DOCUMENT IS THE CREATION, DESIGN, PROPERTY AND COPYRIGHTED WORK OF AT&T. ANY DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. DUPLICATION AND USE BY GOVERNMENT AGENCIES FOR THE PURPOSES OF CONDUCTING THEIR LAWFULLY AUTHORIZED REGULATORY AND ADMINISTRATIVE FUNCTIONS IS SPECIFICALLY ALLOWED.
- 2. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
- CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T MOBILITY REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.
- CONSTRUCTION DRAWINGS ARE VALID FOR SIX MONTHS AFTER ENGINEER OF RECORD'S STAMPED AND SIGNED SUBMITTAL DATE LISTED HEREIN.

72 HOURS



CALL TOLL FREE 1-800-922-4455

OR CALL 811

MINIMINI. UNDERGROUND SERVICE ALERT

HUDSON Design Group LLC

NORTH ANDOVER, MA 01845

CCI SITE #: 857012

TEL: (978) 557-5553 FAX: (978) 336-5586

SITE NUMBER: CT1029 SITE NAME: PLAINVILLE SOUTH WASHINGTON STREET

CCI SITE NUMBER: 857012 335 SOUTH WASHINGTON STREET PLAINVILLE, CT 06062 HARTFORD COUNTY



ROCKY HILL, CT 06067

844	Acres 1							_	15
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1	07/30/18	ISSUED FOR	CONSTRUCTION			АМ	ĺΤ	100 H	
4	06/26/18	ISSUED FOR	REVIEW			ET	AT	DPH	192
0.	DATE		REVISIO	ONS		BY	СНК	APP'D	11
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AT&T TITLE SHEET LTE 4C/5C CT1029

GROUNDING NOTES

- 1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
- 2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
- 3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL—OF—POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
- 4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS FOLIPMENT.
- 5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
- 6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
- APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
- 8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO GROUND BAR.
- 9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
- 10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
- 11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWS COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
- 12. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50

GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:

CONTRACTOR - SAI SUBCONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION) OWNER - AT&T MOBILITY

- 2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.
- 3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGUL ATIONS
- 4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY
- 5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS
- 5. "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.
- 7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- 8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
- 9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
- 10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
- 11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
- 12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
- 13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.

- 14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR—ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.
- 15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
- 16. CONSTRUCTION SHALL COMPLY WITH LTE SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T SITES."
- 17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
- 18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
- 19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.
- 20. APPLICABLE BUILDING CODES:

SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.

BUILDING CODE: IBC 2012 WITH 2016 CT BUILDING CODE AMENDMENTS ELECTRICAL CODE: REFER TO ELECTRICAL DRAWINGS LIGHTENING CODE: REFER TO ELECTRICAL DRAWINGS

SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:

AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE;

AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC)

MANUAL OF STEEL CONSTRUCTION, ASD, FOURTEENTH EDITION;

TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-G, STRUCTURAL STANDARDS FOR STEEL

EQUIPMENT AND ANTENNA SUPPORTING STRUCTURES; REFER TO ELECTRICAL DRAWINGS FOR SPECIFIC ELECTRICAL STANDARDS.

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

			ABBREVIATIONS		
AGL	ABOVE GRADE LEVEL	EQ	EQUAL	REQ	REQUIRED
AWG	AMERICAN WIRE GAUGE	GC	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
BBU	BATTERY BACKUP UNIT	GRC	GALVANIZED RIGID CONDUIT	TBD	TO BE DETERMINED
втсм	BARE TINNED SOLID COPPER WIRE	MGB	MASTER GROUND BAR	TBR	TO BE REMOVED
BGR	BURIED GROUND RING	MIN	MINIMUM	TBRR	TO BE REMOVED AND REPLACED
BTS	BASE TRANSCEIVER STATION	Р	PROPOSED	TYP	TYPICAL ,\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
E	EXISTING	NTS	NOT TO SCALE	UG	UNDER GROUND OF CONNE
EGB	EQUIPMENT GROUND BAR	RAD	RADIATION CENTER LINE (ANTENNA)	VIF	VERIFY IN FIELD J. CRE
EGR	EQUIPMENT GROUND RING	REF	REFERENCE		= 12 28 80



FAX: (978) 336-558

NORTH ANDOVER, MA 01845

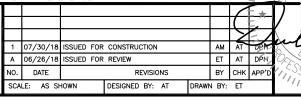


SITE NUMBER: CT1029 SITE NAME: PLAINVILLE SOUTH WASHINGTON STREET

CCI SITE NUMBER: 857012 335 SOUTH WASHINGTON STREET PLAINVILLE, CT 06062 HARTFORD COUNTY

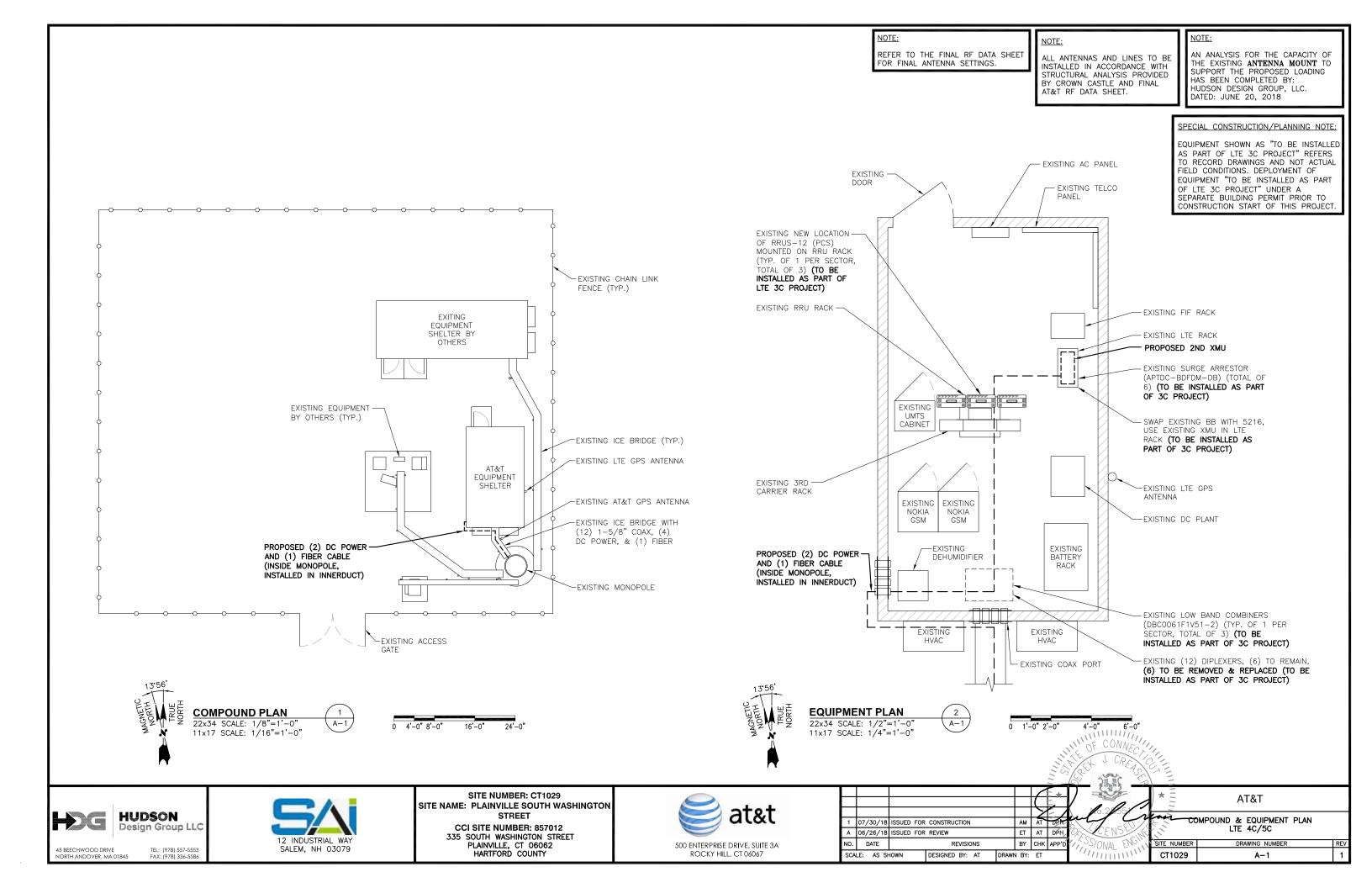


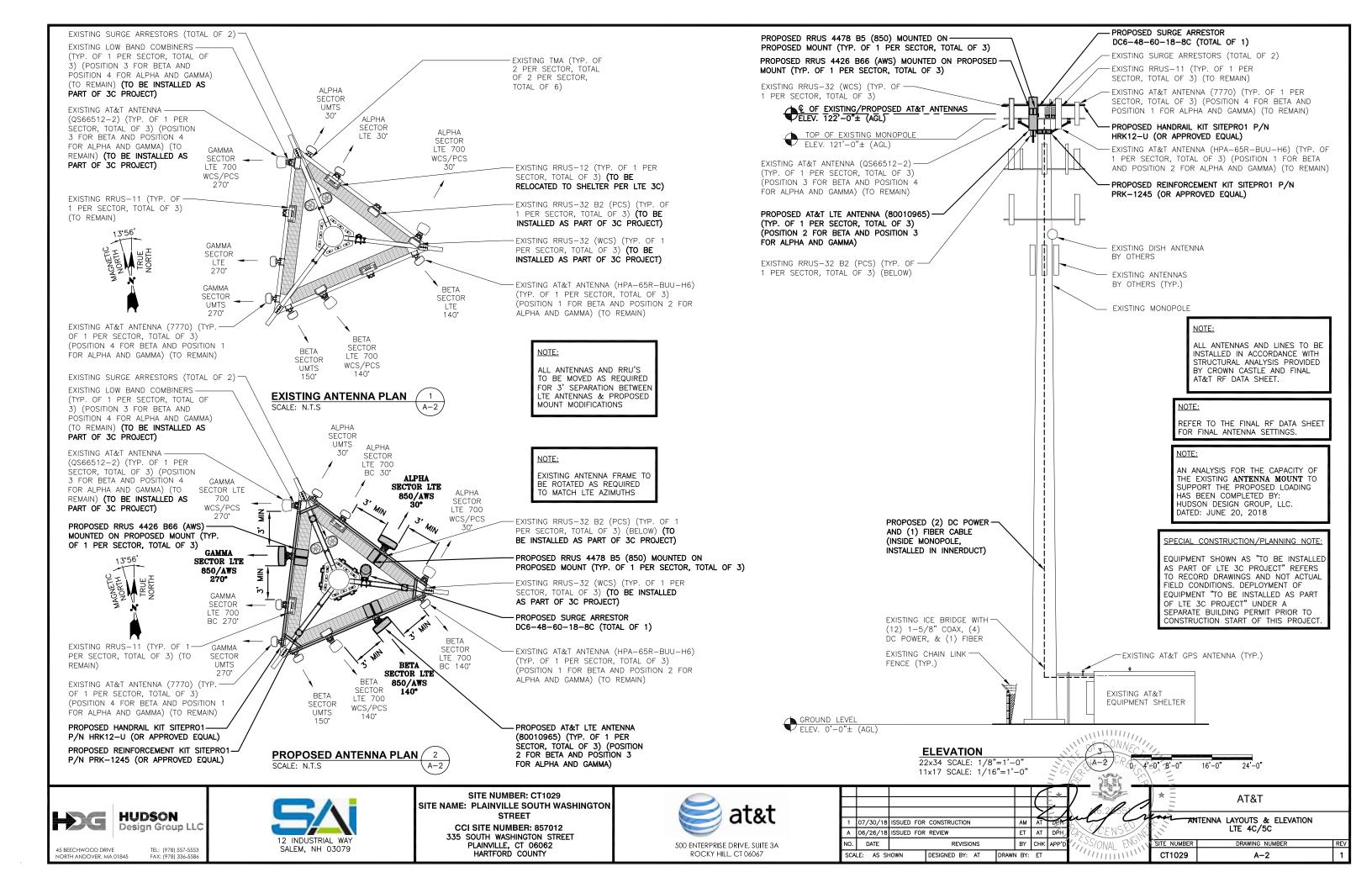
ROCKY HILL, CT 06067



GENERAL NOTES
LTE 4C/5C

SITE NUMBER DRAWING NUMBER
CT1029 GN-1





NOTE:

REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:

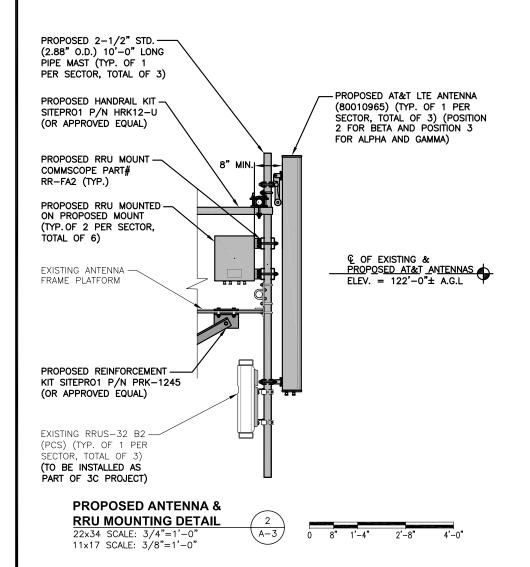
ALL ANTENNAS AND LINES TO BE INSTALLED IN ACCORDANCE WITH STRUCTURAL ANALYSIS PROVIDED BY CROWN CASTLE AND FINAL AT&T RF DATA SHEET.

NOTE:

AN ANALYSIS FOR THE CAPACITY OF THE EXISTING ANTENNA MOUNT TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: JUNE 20, 2018

SPECIAL CONSTRUCTION/PLANNING NOTE:

EQUIPMENT SHOWN AS "TO BE INSTALLED AS PART OF LTE 3C PROJECT" REFERS
TO RECORD DRAWINGS AND NOT ACTUAL FIELD CONDITIONS. DEPLOYMENT OF EQUIPMENT "TO BE INSTALLED AS PART OF LTE 3C PROJECT" UNDER A SEPARATE BUILDING PERMIT PRIOR TO CONSTRUCTION START OF THIS PROJECT.

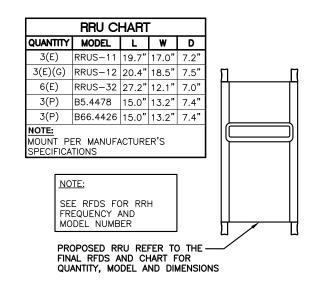


					ANTEN	NA SCHE	DULE				
SECTOR	EXISTING/ PROPOSED	BAND	ANTENNA	SIZE (INCHES) (L x W x D)	ANTENNA © HEIGHT	AZIMUTH	TMA/ COMBINERS	RRU	SIZE (INCHES) (L x W x D)	FEEDER	RAYCAP
A1	EXISTING	UMTS 850/LTE PCS	7770	55X11X5	122'-0"±	30°	POWERWAVE (2) LGP21401			(2) 1-5/8 COAX LENGTH = 127'±	
A2	EXISTING	LTE 700 BC	HPA-65R-BUU-H6	72X14.8X9	122'-0"±	30°		RRUS-11	_		
A3	PROPOSED	LTE 850/AWS	80010965	78.7X20X6.9	122'-0"±	30°		(P) (1) 4478 B5 (850) (P) (1) 4426 B66 (AWS)	15X13.2X7.4 15X13.2X7.4		(E) (1) RAYCAP DC6-48-60-18-8C
A4	EXISTING	LTE 700 WCS/PCS	QS66512-2	72X12X9.6	122'-0"±	30°	KAELUS (2) DBC0061F1V51-2	RRUS-32 B2 (PCS) RRUS-32 (WCS)	<u>-</u>	(2) 1-5/8 COAX LENGTH = 127'±	(E) (1)
B1	EXISTING	LTE 700 BC	HPA-65R-BUU-H6	72X14.8X9	122'-0"±	140°		RRUS-11	-		
B2	PROPOSED	LTE 850/AWS	80010965	78.7X20X6.9	122'-0"±	140°		(P) (1) 4478 B5 (850) (P) (1) 4426 B66 (AWS)	15X13.2X7.4 15X13.2X7.4		
В3	EXISTING	LTE WCS/PCS	QS66512-2	72X12X9.6	122'-0"±	140*	KAELUS (2) DBC0061F1V51-2	RRUS-32 B2 (PCS) RRUS-32 (WCS)	15X13.2X7.4 15X13.2X7.4	(2) 1-5/8 COAX LENGTH = 127'±	RAYCAP -60-0-8C
В4	EXISTING	UMTS 850/ LTE PCS	7770	55X11X5	122'-0"±	150°	POWERWAVE (2) LGP21401			(2) 1-5/8 COAX LENGTH = 127'±	(E) (1) DC6-48-
C1	EXISTING	UMTS 850 / LTE PCS	7770	55X11X5	122'-0"±	270°	POWERWAVE (2) LGP21401			(2) 1-5/8 COAX LENGTH = 127'±	
C2	EXISTING	LTE 700 BC	HPA-65R-BUU-H6	72X14.8X9	122'-0"±	270°		RRUS-11	_		,
СЗ	PROPOSED	LTE 850/AWS	80010965	78.7X20X6.9	122'-0"±	270°		(P) (1) 4478 B5 (850) (P) (1) 4426 B66 (AWS)	15X13.2X7.4 15X13.2X7.4		RAYCAP -60-0-8C
C4	EXISTING	LTE 700 WCS/PCS	QS66512-2	72X12X9.6	122'-0"±	270°	KAELUS (2) DBC0061F1V51-2	RRUS-32 B2 (PCS) RRUS-32 (WCS)		(2) 1-5/8 COAX LENGTH = 127'±	(P) (1) DC6-48-(

FINAL ANTENNA CONFIGURATION

SCALE: N.T.S





MOUNT PER MANUFACTURER'S SPECIFICATIONS.

RRUS DETAIL (A-3 SCALE: N.T.S

PROPOSED SURGE SUPPRESSOR MODEL NUMBERS: DC6-48-60-18-8C DC6-48-60-0-8C DIMENSIONS: H24.0"x9.7"ø WITH BRACKET: H31.25"X9.7"ø -STRIKESORB 30-V1 SURGE PROTECTIVE DEVICE

MOUNT PER MANUFACTURER'S SPECIFICATIONS.

DC SURGE SUPPRESSOR DETAIL SCALE: N.T.S

PROPOSED 2" STD-(2.38" O.D.) 3'-0" LONG MOUNTING PIPE (TYP. OF 1 PER SECTOR, TOTAL OF 3)

ARRESTOR MOUNTING DETAIL

PROPOSED

ARRESTOR

(TOTAL OF 1)

SURGE

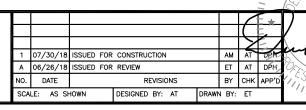


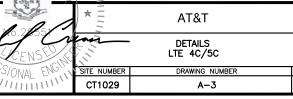


SITE NUMBER: CT1029 SITE NAME: PLAINVILLE SOUTH WASHINGTON STREET

CCI SITE NUMBER: 857012 335 SOUTH WASHINGTON STREET PLAINVILLE, CT 06062 HARTFORD COUNTY







STRUCTURAL NOTES:

- . DESIGN REQUIREMENTS ARE PER STATE BUILDING CODE AND APPLICABLE SUPPLEMENTS, INTERNATIONAL BUILDING CODE, EIA/TIA-222-G STRUCTURAL STANDARDS FOR STEEL ANTENNA, TOWERS AND ANTENNA SUPPORTING STRUCTURES
- CONTRACTOR SHALL VERIFY ALL DIMENSIONS AND CONDITIONS IN THE FIELD PRIOR TO FABRICATION AND ERECTION OF ANY MATERIAL. ANY UNUSUAL CONDITIONS SHALL BE REPORTED TO THE ATTENTION OF THE CONSTRUCTION MANAGER AND ENGINEER OF RECORD.
- DESIGN AND CONSTRUCTION OF STRUCTURAL STEEL SHALL CONFORM TO THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS".
- STRUCTURAL STEEL SHALL CONFORM TO ASTM A992 (Fy=50 ksi), MISCELLANEOUS STEEL SHALL CONFORM TO ASTM A36 UNLESS OTHERWISE INDICATED
- STEEL PIPE SHALL CONFORM TO ASTM A500 "COLD—FORMED WELDED & SEAMLESS CARBON STEEL STRUCTURAL TUBING", GRADE B, OR ASTM A53 PIPE STEEL BLACK AND HOT—DIPPED ZINC—COATED WELDED AND SEAMLESS TYPE E OR S, GRADE B. PIPE SIZES INDICATED ARE NOMINAL. ACTUAL OUTSIDE DIAMETER IS LARGER.
- 6. STRUCTURAL CONNECTION BOLTS SHALL BE HIGH STRENGTH BOLTS (BEARING TYPE) AND CONFORM TO ASTM A325 TYPE-X "HIGH STRENGTH BOLTS FOR STRUCTURAL JOINTS, INCLUDING SUITABLE NUTS AND PLAIN HARDENED WASHERS". ALL BOLTS SHALL BE 3/4" DIA UON.
- ALL STEEL MATERIALS SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT-DIP GALVANIZED) COATINGS ON IRON AND STEEL PRODUCTS", UNLESS OTHERWISE NOTED.
- ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC-COATING (HOT-DIP) ON IRON AND STEEL HARDWARE". UNLESS OTHERWISE NOTED.
- D. FIELD WELDS, DRILL HOLES, SAW CUTS AND ALL DAMAGED GALVANIZED SURFACES SHALL BE REPAIRED WITH AN ORGANIC ZINC REPAIR PAINT COMPLYING WITH REQUIREMENTS OF ASTM A780. GALVANIZING REPAIR PAINT SHALL HAVE 65 PERCENT ZINC BY WEIGHT, ZIRP BY DUNCAN GALVANIZING, GALVA BRIGHT PREMIUM BY CROWN OR EQUAL. THICKNESS OF APPLIED GALVANIZING REPAIR PAINT SHALL BE NOT NOT LESS THAN 4 COATS (ALLOW TIME TO DRY BETWEEN COATS) WITH A RESULTING COATING THICKNESS REQUIRED BY ASTM A123 OR A153 AS APPLICABLE.
- 10. CONTRACTOR SHALL COMPLY WITH AWS CODE FOR PROCEDURES, APPEARANCE AND QUALITY OF WELDS, AND FOR METHODS USED IN CORRECTING WELDING. ALL WELDERS AND WELDING PROCESSES SHALL BE QUALIFIED IN ACCORDANCE WITH AWS "STANDARD QUALIFICATION PROCEDURES". ALL WELDING SHALL BE DONE USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC AND DIJ. WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "STEEL CONSTRUCTION MANUAL". 14TH EDITION.
- 11. INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON-CONFORMING MATERIALS OR CONDITIONS SHALL BE REPORTED TO THE CONSTRUCTION MANAGER PRIOR TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE CONSTRUCTION MANAGER APPROVAL.
- 12. UNISTRUT SHALL BE FORMED STEEL CHANNEL STRUT FRAMING AS MANUFACTURED BY UNISTRUT CORP., WAYNE, MI OR EQUAL. STRUT MEMBERS SHALL BE 1 5/8"x1 5/8"x12GA, UNLESS OTHERWISE NOTED, AND SHALL BE HOT—DIP GALVANIZED AFTER FABRICATION.
- 13. EPOXY ANCHOR ASSEMBLY SHALL CONSIST OF STAINLESS STEEL ANCHOR ROD WITH NUTS & WASHERS. AN INTERNALLY THREADED INSERT, A SCREEN TUBE AND A EPOXY ADHESIVE. THE ANCHORING SYSTEM SHALL BE THE HILTI—HIT HY—70 AND OR HY—200 SYSTEMS (AS SPECIFIED IN DWG.) OR ENGINEERS APPROVED EQUAL.
- 14. EXPANSION BOLTS SHALL CONFORM TO FEDERAL SPECIFICATION FF-S-325, GROUP II, TYPE 4, CLASS I, HILTI KWIK BOLT III OR APPROVED EQUAL. INSTALLATION SHALL BE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- 15. LUMBER SHALL COMPLY WITH THE REQUIREMENTS OF THE AMERICAN INSTITUTE OF TIMBER CONSTRUCTION AND THE NATIONAL FOREST PRODUCTS ASSOCIATION'S NATIONAL DESIGN SPECIFICATION FOR WOOD CONSTRUCTION. ALL LUMBER SHALL BE PRESSURE TREATED AND SHALL BE STRUCTURAL GRADE NO. 2 OR BETTER.
- 16. WHERE ROOF PENETRATIONS ARE REQUIRED, THE CONTRACTOR SHALL CONTACT AND COORDINATE RELATED WORK WITH THE BUILDING OWNER AND THE EXISTING ROOF INSTALLER. WORK SHALL BE PERFORMED IN SUCH A MANNER AS TO NOT VOID THE EXISTING ROOF WARRANTY. ROOF SHALL BE WATERTIGHT.
- VOID THE EXISTING ROOF WARRANTY. ROOF SHALL BE WATERTIGHT.

 17. ALL FIBERGLASS MEMBERS USED ARE AS MANUFACTURED BY STRONGWELL COMPANY OF BRISTOL, VA 24203. ALL DESIGN CRITERIA FOR THESE MEMBERS IS BASED ON INFORMATION PROVIDED IN THE DESIGN MANUAL. ALL REQUIREMENTS PUBLISHED IN SAID MANUAL MUST BE STRICTLY ADHERED TO.
- 18. NO MATERIALS TO BE ORDERED AND NO WORK TO BE COMPLETED UNTIL SHOP DRAWINGS HAVE BEEN REVIEWED AND APPROVED IN WRITING.
- 19. SUBCONTRACTOR SHALL FIREPROOF ALL STEEL TO PRE-EXISTING CONDITIONS.

SPECIAL INSPE	CTION CHECKLIST
BEFORE C	ONSTRUCTION
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
N/A	ENGINEER OF RECORD APPROVE SHOP DRAWINGS 1
N/A	MATERIAL SPECIFICATIONS REPORT ²
N/A	FABRICATOR NDE INSPECTION
N/A	PACKING SLIPS 3
ADDITIONAL TESTING AND INSP	ECTIONS:
DURING C	ONSTRUCTION
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
REQUIRED	STEEL INSPECTIONS
N/A	HIGH STRENGTH BOLT INSPECTIONS
N/A	HIGH WIND ZONE INSPECTIONS
N/A	FOUNDATION INSPECTIONS
N/A	CONCRETE COMP. STRENGTH, SLUMP TESTS AND PLACEMENT
N/A	POST INSTALLED ANCHOR VERIFICATION 5
N/A	GROUT VERIFICATION
N/A	CERTIFIED WELD INSPECTION
N/A	EARTHWORK: LIFT AND DENSITY
N/A	ON SITE COLD GALVANIZING VERIFICATION
N/A	GUY WIRE TENSION REPORT
ADDITIONAL TESTING AND INSP	ECTIONS:
AFTER CO	DNSTRUCTION
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
N/A	MODIFICATION INSPECTOR REDLING OR RECORD DRAWINGS 6
N/A	POST INSTALLED ANCHOR PULL-OUT TESTING
REQUIRED	PHOTOGRAPHS
ADDITIONAL TESTING AND INSP	FCTIONS:

NOTES:

- REQUIRED FOR ANY <u>NEW</u> SHOP FABRICATED FRP OR STEEL.
 PROVIDED BY MANUFACTURER, REQUIRED IF HIGH STRENGTH
 REQUIRED BY MANUFACTURER, REQUIRED IF HIGH STRENGTH
- 3. PROVIDED BY GENERAL CONTRACTOR; PROOF OF MATERIALS.
 4. HIGH WIND ZONE INSPECTION CATB 120MPH OR CAT C,D
 110MPH INSPECT FRAMING OF WALLS, ANCHORING,
 EASTENING SCHEDULE

 FASTENING SCHEDULE

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- FASTENING SCHEDULE.

 5. ADHESIVE FOR REBAR AND ANCHORS SHALL HAVE BEEN TESTED IN ACCORDANCE WITH ACI 355.4 AND ICC—ES AC308 FOR CRACKED CONCRETE AND SEISMIC APPLICATIONS. DESIGN ADHESIVE BOND STRENGTH HAS BEEN BASED ON ACI 355.4 TEMPERATURE CATEGORY B WITH INSTALLATIONS INTO DRY HOLES DRILLED USING A CARBIDE BIT INTO CRACKED CONCRETE THAT HAS CURED FOR AT LEAST 21 DAYS. ADHESIVE ANCHORS REQUIRING CERTIFIED INSTALLATIONS SHALL BE INSTALLED BY A CERTIFIED ADHESIVE ANCHOR INSTALLER PER ACI 318—11 D.9.2.2. INSTALLATIONS REQUIRING CERTIFIED INSTALLERS SHALL BE INSTALLERS
- AS REQUIRED; FOR ANY FIELD CHANGES TO THE ITEMS IN THIS TABLE.

SPECIAL INSPECTIONS (REFERENCE IBC CHAPTER 17):

GENERAL: WHERE APPLICATION IS MADE FOR CONSTRUCTION, THE OWNER OR THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE ACTING AS THE OWNER'S AGENT SHALL EMPLOY ONE OR MORE APPROVED AGENCIES TO PERFORM INSPECTIONS DURING CONSTRUCTION ON THE TYPES OF WORK LISTED IN THE INSPECTION CHECKLIST ABOVE.

THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE AND ENGINEERS OF RECORD INVOLVED IN THE DESIGN OF THE PROJECT ARE PERMITTED TO ACT AS THE APPROVED AGENCY AND THEIR PERSONNEL ARE PERMITTED TO ACT AS THE SPECIAL INSPECTOR FOR THE WORK DESIGNED BY THEM, PROVIDED THOSE PERSONNEL MEET THE OUALIFICATION REQUIREMENTS.

STATEMENT OF SPECIAL INSPECTIONS: THE APPLICANT SHALL SUBMIT A STATEMENT OF SPECIAL INSPECTIONS PREPARED BY THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE IN ACCORDANCE WITH SECTION 107.1 AS A CONDITION FOR ISSUANCE. THIS STATEMENT SHALL BE IN ACCORDANCE WITH SECTION 1705.

REPORT REQUIREMENT: SPECIAL INSPECTORS SHALL KEEP RECORDS OF INSPECTIONS. THE SPECIAL INSPECTOR SHALL FURNISH INSPECTION REPORTS TO THE BUILDING OFFICIAL, AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. REPORTS SHALL INDICATE THAT WORK INSPECTED WAS OR WAS NOT COMPLETED IN CONFORMANCE TO APPROVED CONSTRUCTION DOCUMENTS. DISCREPANCIES SHALL BE BROUGHT TO THE IMMEDIATE ATTENTION OF THE CONTRACTOR FOR CORRECTION. IF THEY ARE NOT CORRECTED, THE DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE BUILDING OFFICIAL AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. A FINAL REPORT DOCUMENTING REQUIRED SPECIAL INSPECTIONS SHALL BE SUBMITTED.

NOTES:

- ALL CONNECTIONS TO BE SHOP WELDED & FIELD BOLTED USING 3/4" A A325-X BOLTS, UNLESS OTHERWISE NOTIFIED
- 2. SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED BEFORE ORDERING MATERIAL.
- SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED PRIOR TO STEEL FABRICATION.
 VERIFICATION OF EXISTING ROOF CONSTRUCTION IS
- VERIFICATION OF EXISTING ROOF CONSTRUCTION IS REQUIRED PRIOR TO THE INSTALLATION OF THE ROOF PLATFORM. ENGINEER OF RECORD IS TO APPROVE EXISTING CONDITIONS IN ORDER TO MOVE FORWARD.
- CENTERLINE OF PROPOSED STEEL PLATFORM SUPPORT COLUMNS TO BE CENTRALLY LOCATED OVER THE EXISTING BUILDING COLUMNS.
- EXISTING BRICK MASONRY COLUMNS/BEARING TO BE REPAIRED/REPLACED AT ALL PROPOSED PLATFORM SUPPORT POINTS. ENGINEER OF RECORD TO REVIEW AND APPROVE.



FAX: (978) 336-558

NORTH ANDOVER, MA 01845



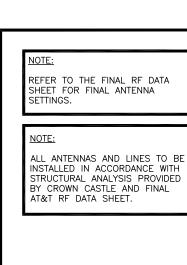
SITE NUMBER: CT1029
SITE NAME: PLAINVILLE SOUTH WASHINGTON
STREET
CCI SITE NUMBER: 857012

CCI SITE NUMBER: 857012
335 SOUTH WASHINGTON STREET
PLAINVILLE, CT 06062
HARTFORD COUNTY



ROCKY HILL, CT 06067

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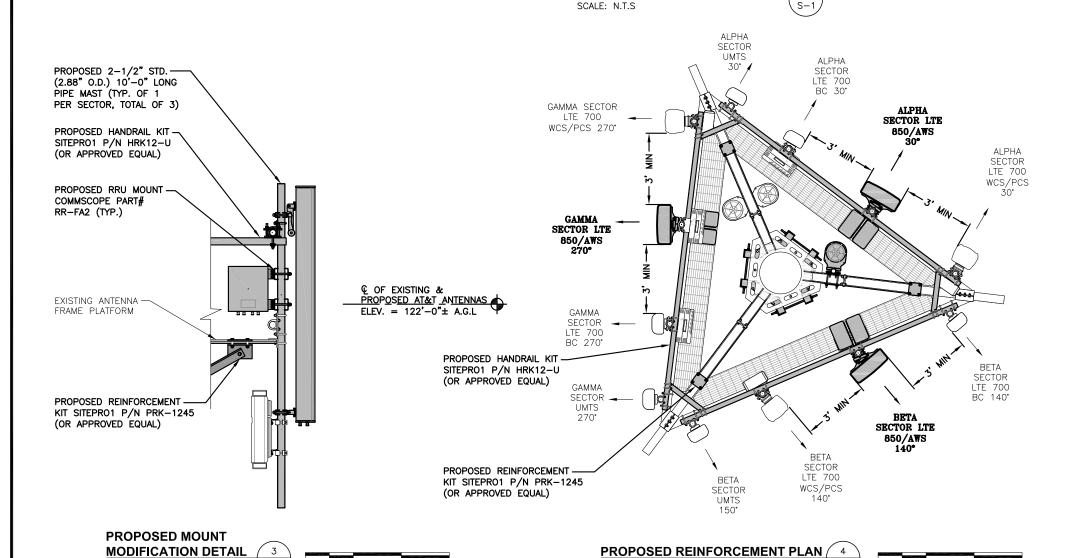


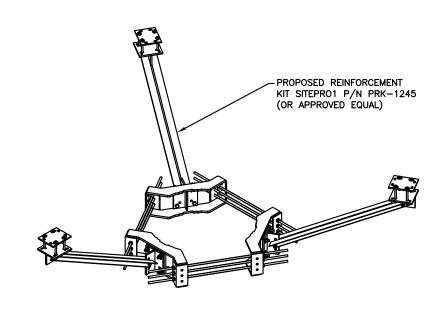
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING ANTENNA MOUNT TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: JUNE 20, 2018

PROPOSED SURGE ARRESTOR (TOTAL OF 1) -EXISTING MOUNTING FRAME PROPOSED BACK TO BACK PIPE MOUNT KIT, SITE - PROPOSED 2" STD (2.38" O.D.) 3'-0" LONG MOUNTING PIPE (TYP. OF 1 PER PRO-1 PART#BBPM-K1 (TOTAL OF 1) SECTOR, TOTAL OF 3) PROPOSED SURGE ARRESTOR MOUNTING DETAIL

PROPOSED HANDRAIL KIT -SITEPRO1 P/N HRK12-U (OR APPROVED EQUAL)

PROPOSED HANDRAIL KIT SCALE: N.T.S





PROPOSED PLATFORM REINFORCEMENT MOUNT DETAIL SCALE: N.T.S

HUDSON Design Group LLC

45 BEECHWOOD DRIVE NORTH ANDOVER, MA 01845

MODIFICATION DETAIL

22x34 SCALE: 3/4"=1'-0"

11x17 SCALE: 3/8"=1'-0"

TEL: (978) 557-5553 FAX: (978) 336-5586

SALEM, NH 03079

SITE NUMBER: CT1029 SITE NAME: PLAINVILLE SOUTH WASHINGTON STREET

22x34 SCALE: 1/2"=1'-0'

11x17 SCALE: 1/4"=1'-0"

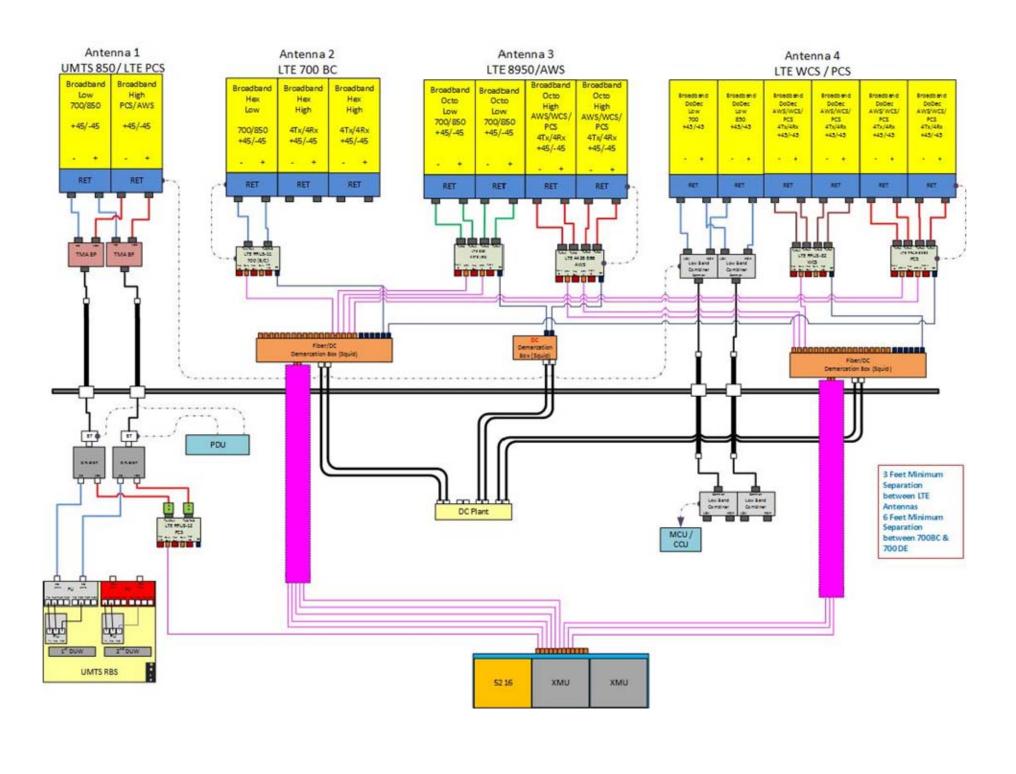
CCI SITE NUMBER: 857012 335 SOUTH WASHINGTON STREET PLAINVILLE, CT 06062 HARTFORD COUNTY



1'-0" 2'-0"

1 07/30/18 ISSUED FOR CONSTRUCTION A 06/26/18 ISSUED FOR REVIEW ET AT DP∤ DATE REVISIONS SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: ET

AT&T STRUCTURAL DETAILS LTE 4C/5C CT1029



ALPHA & GAMMA SECTOR RF PLUMBING DIAGRAM SCALE: N.T.S



NOTE:
REFER TO THE FINAL RF DATA SHEET
FOR FINAL ANTENNA SETTINGS.

WILL OF CONNECTION

NOTE:
1. CONTRACTOR TO CONFIRM ALL PARTS. 2. INSTALL ALL EQUIPMENT TO MANUFACTURER'S RECOMMENDATIONS



SALEM, NH 03079

SITE NUMBER: CT1029 SITE NAME: PLAINVILLE SOUTH WASHINGTON STREET

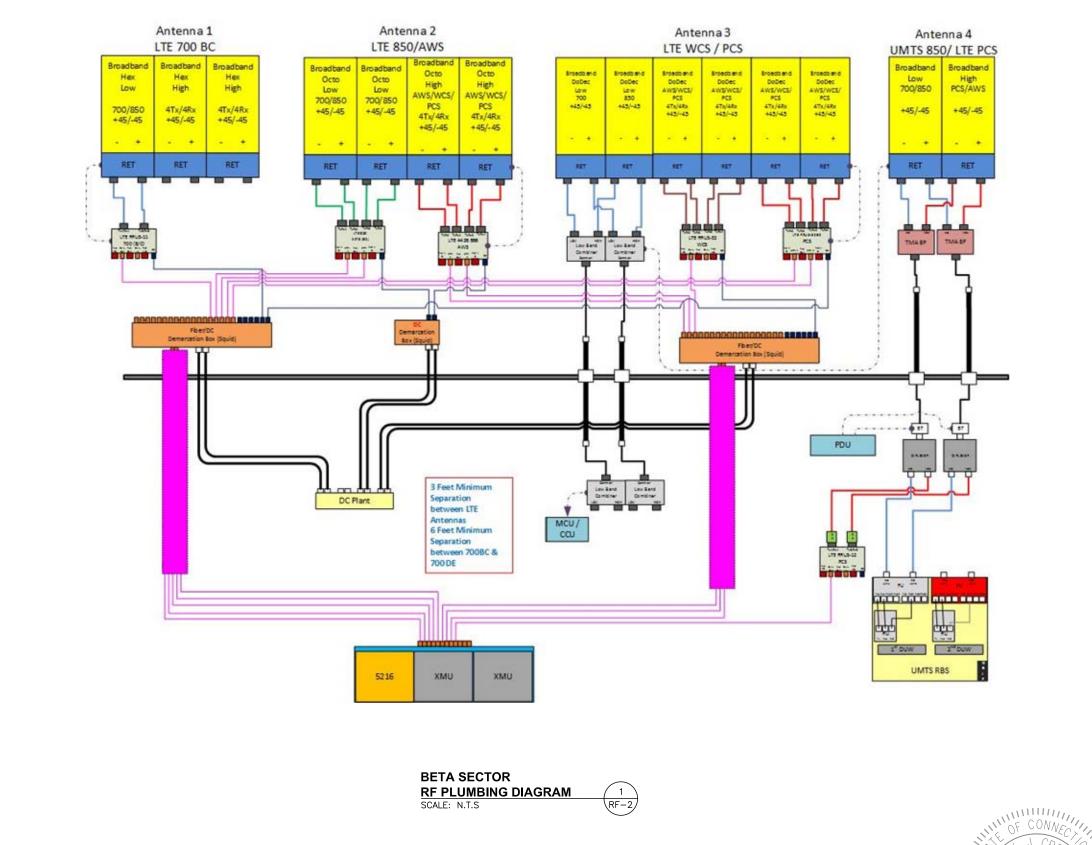
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AT&T RF PLUMBING DIAGRAM LTE 4C/5C

CT1029 RF-1





NOTE:
REFER TO THE FINAL RF DATA SHEET
FOR FINAL ANTENNA SETTINGS.

NOTE:
1. CONTRACTOR TO CONFIRM ALL PARTS. 2. INSTALL ALL EQUIPMENT TO MANUFACTURER'S RECOMMENDATIONS





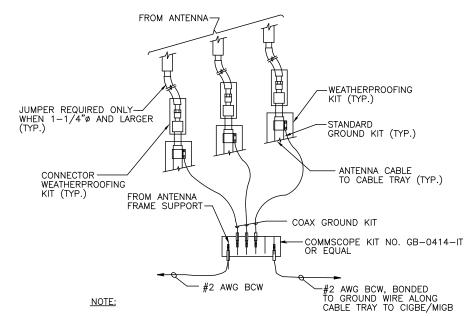
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335 SOUTH WASHINGTON STREET PLAINVILLE, CT 06062 HARTFORD COUNTY

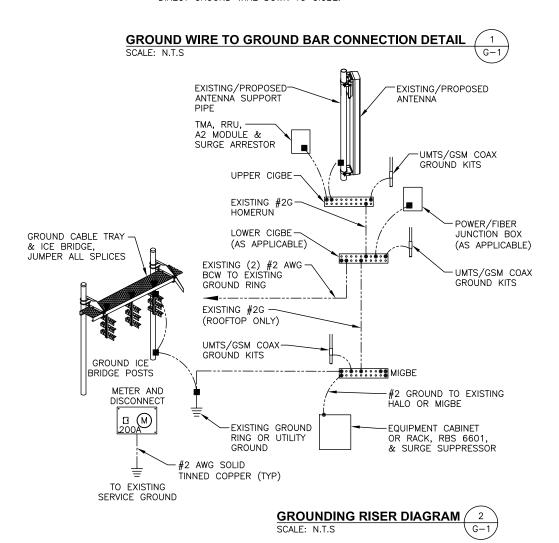


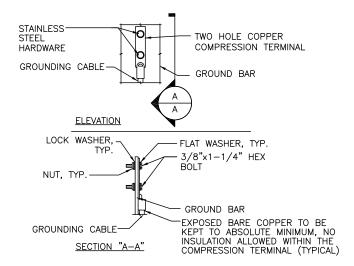
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AT&T RF PLUMBING DIAGRAM LTE 4C/5C CT1029 RF-2



1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.





- "DOUBLING UP" OR "STACKING" OF CONNECTION IS NOT PERMITTED.
- OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATION.
- 3. CADWELD DOWNLEADS FROM UPPER EGB, LOWER EGB, AND MGB

TYPICAL GROUND BAR CONNECTION DETAIL SCALE: N.T.S



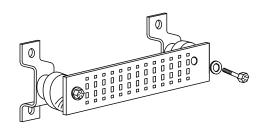
EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS

SECTION "P" - SURGE PRODUCERS

CABLE ENTRY PORTS (HATCH PLATES) (#2) GENERATOR FRAMEWORK (IF AVAILABLE) "(#2) TELCO GROUND BAR COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2) +24V POWER SUPPLY RETURN BAR (#2) -48V POWER SUPPLY RETURN BAR (#2) RECTIFIER FRAMES.

SECTION "A" - SURGE ABSORBERS

INTERIOR GROUND RING (#2) EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2) METALLIC COLD WATER PIPE (IF AVAILABLE) (#2) BUILDING STEEL (IF AVAILABLE) (#2)





ISSUED FOR CONSTRUCTION

REVISIONS

DESIGNED BY: AT

1 07/30/18

DATE

SCALE: AS SHOWN

A 06/26/18 ISSUED FOR REVIEW



ET AT DP

BY CHK APE

DRAWN BY: ET

AT&T GROUNDING DETAILS

LTE 4C/5C CT1029

HUDSON Design Group LLC TEL: (978) 557-5553 FAX: (978) 336-5586

NORTH ANDOVER, MA 01845

SALEM, NH 03079

SITE NUMBER: CT1029 SITE NAME: PLAINVILLE SOUTH WASHINGTON STREET

CCI SITE NUMBER: 857012 335 SOUTH WASHINGTON STREET PLAINVILLE, CT 06062 HARTFORD COUNTY



Date: September 05, 2018

Denice Nicholson Crown Castle 3 Corporate Park Drive Clifton Park, NY 12065



Crown Castle 2000 Corporate Drive Canonsburg, PA 15317 (724) 416-2000

Subject:

Structural Analysis Report

Carrier Designation:

AT&T Mobility Co-Locate

Carrier Site Number:

CT1029

Carrier Site Name:

PLAINVILLE SOUTH WASHINGTON STREET

Crown Castle Designation:

Crown Castle BU Number:

857012

Crown Castle JDE Job Number:

517793

Crown Castle Work Order Number:

1622259

Crown Castle Order Number:

449205 Rev. 1

Engineering Firm Designation:

Crown Castle Project Number:

1622259

Site Data:

335 SOUTH WASHINGTON STREET, PLAINVILLE, Hartford County, CT

Crown Castle Site Name: PLAINVILLE SOUTH WASHINGTON ST

Latitude 41° 39′ 11.03″, Longitude -72° 52′ 36.9″

119 Foot - Monopole Tower

Dear Denice Nicholson,

Crown Castle is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC5: Proposed Equipment Configuration

Sufficient Capacity

The analysis has been performed in accordance with the TIA-222-G Standard. This analysis utilizes an ultimate 3-second gust wind speed of 125 mph (converted an equivalent 97 mph nominal 3-second gust wind speed) as required by the 2016 CT Building Code. Exposure Category C with a maximum topographic factor and Risk Category II was used in this analysis.

Structural analysis prepared by: Daniel Chen / Shan

Respectfully submitted by:

Maham Barimani, P. E. Senior Project Engineer

O9-07-2018

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Table 2 - Other Considered Equipment

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Additional Calculations

1) INTRODUCTION

This tower is a 119 ft. Monopole tower designed by EEI.

2) ANALYSIS CRITERIA

Building Code: 2016 Connecticut State Building Code

TIA-222 Revision: TIA-222-G

Risk Category:

Wind Speed: 125 / 97 mph

Exposure Category:

Topographic Factor:

Ice Thickness:

Wind Speed with Ice:

Seismic Ss:

Seismic S1:

0.064

Service Wind Speed:

C

1

1

0.084

Table 1 - Proposed Equipment Configuration

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)															
		3	ericsson	RRUS 11																	
	122.0	6	powerwave tech	LGP21401																	
		1	raycap	DC6-48-60-18-8F																	
		3	ericsson	RRUS 32 B2																	
		3	ericsson	RRUS 32 B30																	
		3	ericsson	RRUS 4426 B66																	
		3	ericsson	RRUS 4478 B5																	
				3	kaelus	DBC0061F1V51-2	3	3/8													
								3	kathrein	80010965 w/ Mount Pipe	1	1/2									
121.0		6	powerwave tech	7020.00	6	7/8															
	121.0	3	quintel tech	QS66512-2 w/ Mount Pipe	12 1	1-5/8 conduit															
		2	raycap	DC6-48-60-18-8C	'	Conduit															
																	3	cci antennas	HPA-65R-BUU-H6 w/ Mount Pipe		
		3	powerwave tech	RA21.7770.00 w/ Mount Pipe																	
		1	tower mounts	Platform Mount [LP 601-1]																	
		1	sitepro 1	P/N PRK-1245																	
		1	sitepro 1	P/N HRK12																	

Table 2 - Other Considered Equipment

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
		3	alcatel lucent	B13 RRH 4X30		
		3	alcatel lucent	B4 RRH2X60-4R		
		6	andrew	SBNHH-1D65B w/ Mount Pipe		
110.0	112.0	2	antel	BXA-171063-8BF-2 w/ Mount Pipe	20	1-5/8
		6	antel	LPA-80063-4CF-EDIN-5 w/ Mount Pipe		
		1	kathrein	800 10735V01 w/ Mount Pipe		
		1	rfs celwave	DB-T1-6Z-8AB-0Z		
	110.0	1	tower mounts	Platform Mount [LP 1201-1]		
00.0	100.0	3	andrew	ONEBASE TWIN DUAL DUPLEX TMA	1	1-1/4
98.0		6	ericsson	AIR 21 w/ Mount Pipe	12	1-5/8
	98.0	1	tower mounts	Platform Mount [LP 601-1]		
		1	dragonwave	A-ANT-18G-2-C		
		3	argus tech	LLPX310R-V1 w/ Mount Pipe		
	88.0	1	dragonwave	A-ANT-11G-3-C	5	5/16
86.0	00.0	2	dragonwave	HORIZON DUO	5 2 2	1/2
	3		raycap	DC6-48-60-18-8F	2	conduit
		3	samsung telecom	URAS-FLEXIBLE		
	86.0	1	tower mounts	Side Arm Mount [SO 103-3]		

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	Tectonic	4566990	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	EEI	4566996	CCISITES
4-TOWER MANUFACTURER DRAWINGS	EEI	7769700	CCISITES

3.1) Analysis Method

tnxTower (version 8.0.2.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built and maintained in accordance with the manufacturer's specifications.
- 2) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.

This analysis may be affected if any assumptions are not valid or have been made in error. Crown Castle should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element		SF*P_allow (K)	% Capacity	Pass / Fail
L1	119 - 95	Pole	TP27.38x21x0.188	1	-8.656	1041.460	55.0	Pass
L2	95 - 47.25	Pole	TP39.57x25.942x0.25	2	-20.037	1944.740	95.2	Pass
L3	47.25 - 0	Pole	TP51.5x37.622x0.313	3	-34.850	3169.190	89.3	Pass
							Summary	
						Pole (L2)	95.2	Pass
						Rating =	95.2	Pass

Table 5 - Tower Component Stresses vs. Capacity - LC5

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	58.9	Pass
1	Base Plate	0	70.9	Pass
1	Base Foundation Structure	0	68.8	Pass
1	Base Foundation Soil Interaction	0	36.8	Pass

Structure Rating (max from all components) =	95.2%
. ,	

Notes:

4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

APPENDIX A TNXTOWER OUTPUT

Section	3	2	-
Length (ft)	52.750	51.750	24.000
Number of Sides	18	18	18
Thickness (in)	0.313	0.250	0.188
Socket Length (ft)		5.500	4.000
Top Dia (in)	37.622	25.942	21.000
Bot Dia (in)	51.500	39.570	27.380
Grade		A572-65	
Weight (K) 13.6	7.9	4.5	1.2
<u>5.0 IL</u>	0.0 ft	47.3 ft	119.0 ft

DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
(2) RA21.7770.00 w/ Mount Pipe	121	(2) SBNHH-1D65B w/ Mount Pipe	110
RA21.7770.00 w/ Mount Pipe	121	(2) SBNHH-1D65B w/ Mount Pipe	110
HPA-65R-BUU-H6 w/ Mount Pipe	121	(2) SBNHH-1D65B w/ Mount Pipe	110
HPA-65R-BUU-H6 w/ Mount Pipe	121	800 10735V01 w/ Mount Pipe	110
HPA-65R-BUU-H6 w/ Mount Pipe	121	BXA-171063-8BF-2 w/ Mount Pipe	110
(2) LGP21401	121	BXA-171063-8BF-2 w/ Mount Pipe	110
(2) LGP21401	121	B4 RRH2X60-4R	110
(2) LGP21401	121	B4 RRH2X60-4R	110
RRUS 11	121	B4 RRH2X60-4R	110
RRUS 11	121	B13 RRH 4X30	110
RRUS 11	121	B13 RRH 4X30	110
DC6-48-60-18-8F	121	B13 RRH 4X30	110
QS66512-2 w/ Mount Pipe	121	DB-T1-6Z-8AB-0Z	110
QS66512-2 w/ Mount Pipe	121	Platform Mount [LP 1201-1]	110
QS66512-2 w/ Mount Pipe	121	(2) AIR 21 w/ Mount Pipe	98
80010965 w/ Mount Pipe	121	(2) AIR 21 w/ Mount Pipe	98
80010965 w/ Mount Pipe	121	(2) AIR 21 w/ Mount Pipe	98
80010965 w/ Mount Pipe	121	ONEBASE TWIN DUAL DUPLEX TMA	98
(2) DC6-48-60-18-8C	121	ONEBASE TWIN DUAL DUPLEX TMA	98
(3) RRUS 32 B2	121	ONEBASE TWIN DUAL DUPLEX TMA	98
(2) 7020.00	121	(2) 6' x 2" Mount Pipe	98
7020.00	121	(2) 6' x 2" Mount Pipe	98
(3) 7020.00	121	(2) 6' x 2" Mount Pipe	98
RRUS 32 B30	121	Platform Mount [LP 601-1]	98
(2) RRUS 32 B30	121	LLPX310R-V1 w/ Mount Pipe	86
(3) RRUS 4426 B66	121	LLPX310R-V1 w/ Mount Pipe	86
(2) RRUS 4478 B5	121	LLPX310R-V1 w/ Mount Pipe	86
RRUS 4478 B5	121	HORIZON DUO	86
(3) DBC0061F1V51-2	121	HORIZON DUO	86
6' x 2" Mount Pipe	121	DC6-48-60-18-8F	86
6' x 2" Mount Pipe	121	DC6-48-60-18-8F	86
6' x 2" Mount Pipe	121	DC6-48-60-18-8F	86
Platform Mount [LP 601-1]	121	URAS-FLEXIBLE	86
Miscellaneous [NA 509-3]	121	URAS-FLEXIBLE	86
Miscellaneous [NA 507-1]	121	URAS-FLEXIBLE	86
(2) LPA-80063-4CF-EDIN-5 w/ Mount	110	6' x 2" Mount Pipe	86
Pipe		6' x 2" Mount Pipe	86
(2) LPA-80063-4CF-EDIN-5 w/ Mount	110	6' x 2" Mount Pipe	86
Pipe		Side Arm Mount [SO 103-3]	86
(2) LPA-80063-4CF-EDIN-5 w/ Mount Pipe	110	A-ANT-18G-2-C	86
i ibe		A-ANT-11G-3-C	86

MATERIAL STRENGTH

GI	RADE	Fy	Fu	GRADE	Fy	Fu
A572-	-65	65 ksi	80 ksi			

TOWER DESIGN NOTES

- Tower is located in Hartford County, Connecticut.
 Tower designed for Exposure C to the TIA-222-G Standard.
 Tower designed for a 97 mph basic wind in accordance with the TIA-222-G Standard.
 Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.

ALL REAC'5. Deflections are based upon a 60 mph wind. ARE FACT6. Tower Structure Class II.

7. Topographic Category 1 with Crest Height of 0.000 ft AXIAL8. TOWER RATING: 95.2%

76 K SHEAR MOMENT 9K / 933 kip-ft

TORQUE 2 kip-ft 50 mph WIND - 1.000 in ICE AXIAL 35 K

MOMENT SHEAR' 31 K / 2946 kip-ft

TORQUE 5 kip-ft REACTIONS - 97 mph WIND

Crown Castle BU# 857012 CROWN 2000 Corporate Drive CASTLE Z000 Corporation Canonsburg, PA 15317 Client: Crown Castle Drawn by: Daniel Chen App'd: Scale: NTS Code: TIA-222-G Date: 09/05/18 Phone: (724) 416-2000 The Pathway to Possible Dwg No. E-1 FAX:

Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

- 1) Tower is located in Hartford County, Connecticut.
- 2) Basic wind speed of 97 mph.
- 3) Structure Class II.
- 4) Exposure Category C.
- 5) Topographic Category 1.
- 6) Crest Height 0.000 ft.
- 7) Nominal ice thickness of 1.000 in.
- 8) Ice thickness is considered to increase with height.
- 9) Ice density of 56.000 pcf.
- A wind speed of 50 mph is used in combination with ice.
- 11) Temperature drop of 50.000 °F.
- Deflections calculated using a wind speed of 60 mph.
- 13) A non-linear (P-delta) analysis was used.
- 14) Pressures are calculated at each section.
- 15) Stress ratio used in pole design is 1.
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- √ Use Code Stress Ratios
- √ Use Code Safety Factors Guys Escalate Ice Always Use Max Kz Use Special Wind Profile

Include Bolts In Member Capacity

Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric Distribute Leg Loads As Uniform Assume Legs Pinned

- √ Assume Rigid Index Plate
- √ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
- √ Bypass Mast Stability Checks
- $\begin{array}{c} \sqrt{} \text{ Use Azimuth Dish Coefficients} \\ \sqrt{} \text{ Project Wind Area of Appurt.} \end{array}$

Autocalc Torque Arm Areas

Add IBC .6D+W Combination

√ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

 ✓ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-G Bracing Resist. Exemption
 Use TIA-222-G Tension Splice

Use TIA-222-G Tension Splice Exemption

Poles

✓ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

Tapered Pole Section Geometry

Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	fť	fť	Sides	in	in	in	in	
L1	119.000- 95.000	24.000	4.000	18	21.000	27.380	0.188	0.750	A572-65 (65 ksi)
L2	95.000-47.250	51.750	5.500	18	25.942	39.570	0.250	1.000	À572-65 (65 ksi)
L3	47.250-0.000	52.750		18	37.622	51.500	0.313	1.250	À572-65 (65 ksi)

				Taper	ed Pol	e Prop	erties			
Section	Tip Dia.	Area	1	r	С	I/C	J	It/Q	W	w/t
	in	in²	in⁴	in	in	in³	in⁴	in²	in	
L1	21.295	12.386	677.826	7.388	10.668	63.538	1356.544	6.194	3.366	17.952
	27.773	16.183	1511.796	9.653	13.909	108.692	3025.580	8.093	4.489	23.941
L2	27.373	20.386	1700.048	9.121	13.178	129.003	3402.333	10.195	4.126	16.503
	40.142	31.200	6094.315	13.959	20.102	303.176	12196.649	15.603	6.524	26.097
L3	39.623	37.006	6507.856	13.245	19.112	340.516	13024.276	18.506	6.071	19.428
	52.246	50.772	16806.843	18.172	26.162	642.414	33635.802	25.391	8.514	27.245

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade Adjust. Factor A _f	Adjust. Factor A _r	Weight Mult.	Double Angle Stitch Bolt Spacing	Double Angle Stitch Bolt Spacing	Double Angle Stitch Bolt Spacing
	" /					Diagonals	Horizontals	Redundants
ft	ft ²	in				in	in	in
L1 119.000- 95.000			1	1	1			
L2 95.000-			1	1	1			
47.250								
L3 47.250- 0.000			1	1	1			

Description	Secto r	Component Type	Placement	Total Number	Number Per Row	Start/En d	Width or Diamete	Perimete r	Weight
			ft			Position	r in	in	plf
LDF7-50A(1-5/8)	В	Surface Ar (CaAa)	110.000 - 0.000	7	6	-0.200 0.000	1.980		0.820

Feed Line/Linear Appurtenances - Entered As Area

Description	Face		Component	Placement	Total		$C_A A_A$	Weight
	or Leg	Shield	Type	ft	Number		f t² /ft	plf
Level 121	Log			π			16/16	ρıı
2" Rigid Conduit	Α	No	Inside Pole	119.000 - 0.000	1	No Ice	0.000	2.800
g					-	1/2" Ice	0.000	2.800
						1" Ice	0.000	2.800
LDF7-50A(1-5/8)	Α	No	Inside Pole	119.000 - 0.000	12	No Ice	0.000	0.820
,						1/2" Ice	0.000	0.820
						1" Ice	0.000	0.820
760002253(1/2)	Α	No	Inside Pole	119.000 - 0.000	1	No Ice	0.000	0.103
, ,						1/2" Ice	0.000	0.103
						1" Ice	0.000	0.103
WR-VG86ST-	Α	No	Inside Pole	119.000 - 0.000	2	No Ice	0.000	0.680
BRDA(7/8)						1/2" Ice	0.000	0.680
						1" Ice	0.000	0.680
FB-L98B-034-XXX(3/8)	Α	No	Inside Pole	119.000 - 0.000	3	No Ice	0.000	0.057
						1/2" Ice	0.000	0.057
						1" Ice	0.000	0.057
WR-VG86ST-	Α	No	Inside Pole	119.000 - 0.000	4	No Ice	0.000	0.680
BRDA(7/8)						1/2" Ice	0.000	0.680
						1" Ice	0.000	0.680
Level 110								
LDF7-50A(1-5/8)	В	No	Inside Pole	110.000 - 0.000	11	No Ice	0.000	0.820
						1/2" Ice	0.000	0.820

Description	Face	Allow	Component	Placement	Total		C_AA_A	Weight
	or Leg	Shield	Type	ft	Number		f l' /ft	plf
	Log					1" Ice	0.000	0.820
MLE HYBRID	В	No	Inside Pole	110.000 - 0.000	1	No Ice	0.000	1.070
9POWER/18FIBER RL		140	made i die	110.000 - 0.000	•	1/2" Ice	0.000	1.070
2(1-5/8)						1" Ice	0.000	1.070
HB158-1-08U8-	В	No	Inside Pole	110.000 - 0.000	1	No Ice	0.000	1.300
S8J18(1-5/8)	Ь	NO	Illiside i ole	110.000 - 0.000	'	1/2" Ice	0.000	1.300
30310(1-3/0)						1" Ice	0.000	1.300
Level 98						i ice	0.000	1.300
LDF6-50A(1-1/4)	Α	No	Inside Pole	98.000 - 0.000	1	No Ice	0.000	0.600
LDI 0-30A(1-1/4)	^	NO	iliside i die	30.000 - 0.000	'	1/2" Ice	0.000	0.600
						1" Ice	0.000	0.600
LDF7-50A(1-5/8)	Α	No	Inside Pole	98.000 - 0.000	12	No Ice	0.000	0.820
LDI 7-30A(1-3/0)	^	NO	iliside i die	30.000 - 0.000	12	1/2" Ice	0.000	0.820
						1" Ice	0.000	0.820
Level 86						1 100	0.000	0.020
2" Rigid Conduit	С	No	Inside Pole	86.000 - 0.000	2	No Ice	0.000	2.800
2 Nigia Conduit	C	NO	IIISIUE FUIE	00.000 - 0.000	2	1/2" Ice	0.000	2.800
						1" Ice	0.000	2.800
LDE4 50A(4/2)	_	No	Inside Pole	86.000 - 0.000	2	No Ice	0.000	2.600 0.150
LDF4-50A(1/2)	С	No	mside Pole	00.000 - 0.000	2			
						1/2" Ice	0.000	0.150
0007/5/40	_	NI.	In add Date	00 000 0 000	-	1" Ice	0.000	0.150
9207(5/16)	С	No	Inside Pole	86.000 - 0.000	5	No Ice	0.000	0.600
						1/2" Ice	0.000	0.600
***						1" Ice	0.000	0.600

Feed Line/Linear Appurtenances Section Areas

Tower	Tower	Face	A_R	AF	C_AA_A	$C_A A_A$	Weight
Sectio	Elevation				In Face	Out Face	
n	ft		ft²	ft ²	ft ²	ft ²	K
L1	119.000-95.000	Α	0.000	0.000	0.000	0.000	0.439
		В	0.000	0.000	17.820	0.000	0.257
		С	0.000	0.000	0.000	0.000	0.000
L2	95.000-47.250	Α	0.000	0.000	0.000	0.000	1.310
		В	0.000	0.000	56.727	0.000	0.818
		С	0.000	0.000	0.000	0.000	0.345
L3	47.250-0.000	Α	0.000	0.000	0.000	0.000	1.296
		В	0.000	0.000	56.133	0.000	0.809
		С	0.000	0.000	0.000	0.000	0.421

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Sectio	Tower Elevation	Face or	lce Thickness	A _R	A_F	C _A A _A In Face	C _A A _A Out Face	Weight
n	ft	Leg	in	ft ²	ft ²	f t²	ft ²	K
L1	119.000-95.000	Α	2.249	0.000	0.000	0.000	0.000	0.439
		В		0.000	0.000	30.707	0.000	0.760
		С		0.000	0.000	0.000	0.000	0.000
L2	95.000-47.250	Α	2.156	0.000	0.000	0.000	0.000	1.310
		В		0.000	0.000	97.751	0.000	2.419
		С		0.000	0.000	0.000	0.000	0.345
L3	47.250-0.000	Α	1.934	0.000	0.000	0.000	0.000	1.296
		В		0.000	0.000	95.638	0.000	2.321
		С		0.000	0.000	0.000	0.000	0.421

Feed Line Center of Pressure

Section	Elevation	CPx	CPz	CPx	CPz
				Ice	Ice
	ft	in	in	in	in
L1	119.000-95.000	3.909	-3.519	2.976	-2.679
L2	95.000-47.250	5.450	-4.907	4.239	-3.817
L3	47.250-0.000	5.913	-5.324	4.727	-4.256

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K₃ No Ice	K₃ Ice
L1	12	LDF7-50A(1-5/8)	95.00 -	1.0000	1.0000
			110.00		
L2	12	LDF7-50A(1-5/8)		1.0000	1.0000
			95.00		

INGPEATA	I MWAF I	nane
Discrete 7		Ludus

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	0	ft		ft²	ft ²	K
Level 121 (2) RA21.7770.00 w/ Mount Pipe	Α	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	6.766 7.261 7.735	5.002 5.960 6.747	0.060 0.114 0.175
RA21.7770.00 w/ Mount Pipe	В	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	6.766 7.261 7.735	5.002 5.960 6.747	0.060 0.114 0.175
HPA-65R-BUU-H6 w/ Mount Pipe	Α	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	9.895 10.470 11.010	8.113 9.304 10.209	0.077 0.158 0.248
HPA-65R-BUU-H6 w/ Mount Pipe	В	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	9.895 10.470 11.010	8.113 9.304 10.209	0.077 0.158 0.248
HPA-65R-BUU-H6 w/ Mount Pipe	С	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	9.895 10.470 11.010	8.113 9.304 10.209	0.077 0.158 0.248
(2) LGP21401	Α	From Leg	4.000 0.000 1.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	1.104 1.239 1.381	0.207 0.274 0.348	0.014 0.021 0.030
(2) LGP21401	В	From Leg	4.000 0.000 1.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	1.104 1.239 1.381	0.207 0.274 0.348	0.014 0.021 0.030
(2) LGP21401	С	From Leg	4.000	0.000	121.000	No Ice	1.104	0.207	0.014

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			Vert ft ft ft	0	ft		ft ²	ft ²	K
			0.000			1/2" Ice 1" Ice	1.239 1.381	0.274 0.348	0.021 0.030
RRUS 11	Α	From Leg	4.000 0.000 1.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	2.784 2.992 3.207	1.187 1.334 1.490	0.048 0.068 0.092
RRUS 11	В	From Leg	4.000 0.000 1.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	2.784 2.992 3.207	1.187 1.334 1.490	0.048 0.068 0.092
RRUS 11	С	From Leg	4.000 0.000 1.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	2.784 2.992 3.207	1.187 1.334 1.490	0.048 0.068 0.092
DC6-48-60-18-8F	Α	From Leg	4.000 0.000 1.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	0.791 1.274 1.450	0.791 1.274 1.450	0.020 0.035 0.053
QS66512-2 w/ Mount Pipe	Α	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	2.600 9.290 9.910	5.000 9.657 10.620	0.111 0.212 0.296
QS66512-2 w/ Mount Pipe	В	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	2.600 9.290 9.910	5.000 9.657 10.620	0.111 0.212 0.296
QS66512-2 w/ Mount Pipe	С	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice	2.600 9.290 9.910	5.000 9.657 10.620	0.111 0.212 0.296
80010965 w/ Mount Pipe	Α	From Leg	4.000 0.000 0.000	0.000	121.000	1" Ice No Ice 1/2" Ice 1" Ice	14.051 14.688 15.303	7.628 8.903 9.963	0.125 0.222 0.327
80010965 w/ Mount Pipe	В	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	14.051 14.688 15.303	7.628 8.903 9.963	0.125 0.222 0.327
80010965 w/ Mount Pipe	С	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	14.051 14.688 15.303	7.628 8.903 9.963	0.125 0.222 0.327
(2) DC6-48-60-18-8C	Α	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	2.737 2.963 3.196	2.737 2.963 3.196	0.026 0.052 0.082
(3) RRUS 32 B2	Α	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice	2.731 2.953 3.182	1.668 1.855 2.049	0.053 0.074 0.098
(2) 7020.00	Α	From Leg	4.000 0.000 0.000	0.000	121.000	1" Ice No Ice 1/2" Ice 1" Ice	0.102 0.147 0.199	0.175 0.239 0.311	0.002 0.005 0.009
7020.00	В	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	0.102 0.147 0.199	0.175 0.239 0.311	0.002 0.005 0.009
(3) 7020.00	С	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice	0.102 0.147 0.199	0.175 0.239 0.311	0.002 0.005 0.009
RRUS 32 B30	Α	From Leg	4.000 0.000	0.000	121.000	1" Ice No Ice 1/2"	2.692 2.912	1.573 1.756	0.060 0.080

 Description	Face	Offset	Offsets:	Azimuth	Placement		C _A A _A	СаАа	Weight
·	or Leg	Type	Horz Lateral Vert	Adjustmen t			Front	Side	•
			ft ft ft	٥	ft		ft ²	ft²	K
			0.000			Ice 1" Ice	3.138	1.945	0.104
(2) RRUS 32 B30	В	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	2.692 2.912 3.138	1.573 1.756 1.945	0.060 0.080 0.104
(3) RRUS 4426 B66	В	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	1.644 1.804 1.972	0.725 0.842 0.969	0.048 0.061 0.076
(2) RRUS 4478 B5	В	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	1.843 2.012 2.190	1.059 1.197 1.342	0.060 0.076 0.094
RRUS 4478 B5	С	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	1.843 2.012 2.190	1.059 1.197 1.342	0.060 0.076 0.094
(3) DBC0061F1V51-2	С	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	0.413 0.496 0.586	0.433 0.518 0.609	0.025 0.031 0.038
6' x 2" Mount Pipe	Α	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048
6' x 2" Mount Pipe	В	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048
6' x 2" Mount Pipe	С	From Leg	4.000 0.000 0.000	0.000	121.000	No Ice 1/2" Ice 1" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048
Platform Mount [LP 601-1]	С	None		0.000	121.000	No Ice 1/2" Ice 1" Ice	28.470 33.590 38.710	28.470 33.590 38.710	1.122 1.514 1.905
Miscellaneous [NA 509-3]	С	None		0.000	121.000	No Ice 1/2" Ice 1" Ice	11.840 16.960 22.080	11.840 16.960 22.080	0.275 0.296 0.317
Miscellaneous [NA 507-1]	С	None		0.000	121.000	No Ice 1/2" Ice 1" Ice	4.800 6.700 8.600	4.800 6.700 8.600	0.245 0.294 0.343
Level 110 (2) LPA-80063-4CF-EDIN- 5 w/ Mount Pipe	Α	From Leg	4.000 0.000 2.000	0.000	110.000	No Ice 1/2" Ice 1" Ice	6.379 6.778 7.186	6.564 7.192 7.836	0.038 0.104 0.176
(2) LPA-80063-4CF-EDIN- 5 w/ Mount Pipe	В	From Leg	4.000 0.000 2.000	0.000	110.000	No Ice 1/2" Ice 1" Ice	6.379 6.778 7.186	6.564 7.192 7.836	0.038 0.104 0.176
(2) LPA-80063-4CF-EDIN- 5 w/ Mount Pipe	С	From Leg	4.000 0.000 2.000	0.000	110.000	No Ice 1/2" Ice 1" Ice	6.379 6.778 7.186	6.564 7.192 7.836	0.038 0.104 0.176
(2) SBNHH-1D65B w/ Mount Pipe	Α	From Leg	4.000 0.000 2.000	0.000	110.000	No Ice 1/2" Ice 1" Ice	8.386 8.950 9.480	7.084 8.275 9.188	0.076 0.146 0.223
(2) SBNHH-1D65B w/ Mount Pipe	В	From Leg	4.000 0.000	0.000	110.000	No Ice 1/2"	8.386 8.950	7.084 8.275	0.076 0.146

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			Vert ft ft ft	o	ft		ft ²	ft²	К
			2.000			Ice 1" Ice	9.480	9.188	0.223
(2) SBNHH-1D65B w/	С	From Leg	4.000	0.000	110.000	No Ice	8.386	7.084	0.076
Mount Pipe	Ū	7 10111 Log	0.000	0.000	110.000	1/2" Ice	8.950 9.480	8.275 9.188	0.146 0.223
						1" Ice			
800 10735V01 w/ Mount	Α	From Leg	4.000	0.000	110.000	No Ice	8.873	5.489	0.058
Pipe			0.000 2.000			1/2" Ice 1" Ice	9.455 10.010	6.710 7.688	0.121 0.192
BXA-171063-8BF-2 w/	В	From Leg	4.000	0.000	110.000	No Ice	3.179	3.353	0.029
Mount Pipe	_		0.000			1/2"	3.555	3.971	0.061
·			2.000			Ice	3.930	4.595	0.099
	_	_				1" Ice			
BXA-171063-8BF-2 w/	С	From Leg	4.000	0.000	110.000	No Ice	3.179	3.353	0.029
Mount Pipe			0.000 2.000			1/2" Ice 1" Ice	3.555 3.930	3.971 4.595	0.061 0.099
B4 RRH2X60-4R	Α	From Leg	4.000	0.000	110.000	No Ice	3.355	2.005	0.055
		J	0.000			1/2"	3.612	2.237	0.078
	_		2.000			Ice 1" Ice	3.876	2.476	0.105
B4 RRH2X60-4R	В	From Leg	4.000	0.000	110.000	No Ice	3.355	2.005	0.055
			0.000 2.000			1/2" Ice 1" Ice	3.612 3.876	2.237 2.476	0.078 0.105
B4 RRH2X60-4R	С	From Leg	4.000	0.000	110.000	No Ice	3.355	2.005	0.055
		_	0.000			1/2"	3.612	2.237	0.078
			2.000			Ice 1" Ice	3.876	2.476	0.105
B13 RRH 4X30	Α	From Leg	4.000	0.000	110.000	No Ice	2.055	1.320	0.056
			0.000 2.000			1/2" Ice 1" Ice	2.241 2.433	1.475 1.638	0.073 0.093
B13 RRH 4X30	В	From Leg	4.000	0.000	110.000	No Ice	2.055	1.320	0.056
		J	0.000			1/2"	2.241	1.475	0.073
540 5544 4940			2.000			Ice 1" Ice	2.433	1.638	0.093
B13 RRH 4X30	С	From Leg	4.000	0.000	110.000	No Ice 1/2"	2.055	1.320	0.056
			0.000 2.000			Ice	2.241 2.433	1.475 1.638	0.073 0.093
			2.000			1" Ice	2.100	1.000	0.000
DB-T1-6Z-8AB-0Z	Α	From Leg	4.000	0.000	110.000	No Ice	4.800	2.000	0.044
			0.000			1/2"	5.070	2.193	0.080
			2.000			Ice 1" Ice	5.348	2.393	0.120
Platform Mount [LP 1201-	С	None		0.000	110.000	No Ice	23.100	23.100	2.100
1]						1/2"	26.800	26.800	2.500
Level 98						Ice 1" Ice	30.500	30.500	2.900
(2) AIR 21 w/ Mount Pipe	Α	From Leg	4.000	0.000	98.000	No Ice	6.287	5.701	0.112
(2) / lift 21 W/ Would 1 ipo	,,	1 Tom Log	0.000	0.000	00.000	1/2"	6.732	6.482	0.169
			2.000			Ice 1" Ice	7.170	7.188	0.232
(2) AIR 21 w/ Mount Pipe	В	From Leg	4.000	0.000	98.000	No Ice	6.287	5.701	0.112
			0.000			1/2"	6.732	6.482	0.169
			2.000			Ice 1" Ice	7.170	7.188	0.232
(2) AIR 21 w/ Mount Pipe	С	From Leg	4.000	0.000	98.000	No Ice	6.287	5.701	0.112
			0.000			1/2"	6.732	6.482	0.169
			2.000			Ice	7.170	7.188	0.232
ONEBASE TWIN DUAL	Α	From Leg	4.000	0.000	98.000	1" Ice No Ice	0.578	0.263	0.011
DUPLEX TMA	^	i ioni Leg	0.000	0.000	90.000	1/2"	0.674	0.203	0.016

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			Vert ft ft ft	o	ft		ft ^e	ft²	К
			2.000			Ice	0.778	0.416	0.022
ONEDASE TWIN DUAL	В	From Log	4.000	0.000	00.000	1" Ice	0.570	0.262	0.011
ONEBASE TWIN DUAL DUPLEX TMA	В	From Leg	4.000 0.000 2.000	0.000	98.000	No Ice 1/2" Ice 1" Ice	0.578 0.674 0.778	0.263 0.336 0.416	0.011 0.016 0.022
ONEBASE TWIN DUAL DUPLEX TMA	С	From Leg	4.000 0.000 2.000	0.000	98.000	No Ice 1/2" Ice 1" Ice	0.578 0.674 0.778	0.263 0.336 0.416	0.011 0.016 0.022
(2) 6' x 2" Mount Pipe	Α	From Leg	4.000 0.000 0.000	0.000	98.000	No Ice 1/2" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048
(2) 6' x 2" Mount Pipe	В	From Leg	4.000	0.000	98.000	1" Ice No Ice	1.425	1.425	0.022
(E) O X E MOGNET IPO	5	1 10111 Log	0.000	0.000	00.000	1/2" Ice 1" Ice	1.925 2.294	1.925 2.294	0.033 0.048
(2) 6' x 2" Mount Pipe	С	From Leg	4.000	0.000	98.000	No Ice	1.425	1.425	0.022
			0.000 0.000			1/2" Ice 1" Ice	1.925 2.294	1.925 2.294	0.033 0.048
Platform Mount [LP 601-1]	С	None		0.000	98.000	No Ice 1/2" Ice 1" Ice	28.470 33.590 38.710	28.470 33.590 38.710	1.122 1.514 1.905
Level 86 LLPX310R-V1 w/ Mount Pipe	Α	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice 1" Ice	4.538 4.891 5.254	2.983 3.526 4.086	0.045 0.083 0.126
LLPX310R-V1 w/ Mount Pipe	В	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice 1" Ice	4.538 4.891 5.254	2.983 3.526 4.086	0.045 0.083 0.126
LLPX310R-V1 w/ Mount Pipe	С	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice 1" Ice	4.538 4.891 5.254	2.983 3.526 4.086	0.045 0.083 0.126
HORIZON DUO	Α	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice 1" Ice	0.469 0.556 0.650	0.294 0.365 0.444	0.007 0.012 0.018
HORIZON DUO	В	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice	0.469 0.556 0.650	0.294 0.365 0.444	0.007 0.012 0.018
DC6-48-60-18-8F	Α	From Leg	2.000 0.000	0.000	86.000	1" Ice No Ice 1/2"	0.791 1.274	0.791 1.274	0.020 0.035
			2.000			lce 1" lce	1.450	1.450	0.053
DC6-48-60-18-8F	В	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice 1" Ice	0.791 1.274 1.450	0.791 1.274 1.450	0.020 0.035 0.053
DC6-48-60-18-8F	С	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice	0.791 1.274 1.450	0.791 1.274 1.450	0.020 0.035 0.053
URAS-FLEXIBLE	Α	From Leg	2.000 0.000 2.000	0.000	86.000	1" Ice No Ice 1/2" Ice	1.547 1.704 1.868	0.684 0.800 0.923	0.033 0.045 0.058
URAS-FLEXIBLE	В	From Leg	2.000 0.000	0.000	86.000	1" Ice No Ice 1/2"	1.547 1.704	0.684 0.800	0.033 0.045

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	٥	ft		ft²	ft²	K
			2.000			Ice 1" Ice	1.868	0.923	0.058
URAS-FLEXIBLE	С	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice 1" Ice	1.547 1.704 1.868	0.684 0.800 0.923	0.033 0.045 0.058
6' x 2" Mount Pipe	Α	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice 1" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048
6' x 2" Mount Pipe	В	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice 1" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048
6' x 2" Mount Pipe	С	From Leg	2.000 0.000 2.000	0.000	86.000	No Ice 1/2" Ice 1" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048
Side Arm Mount [SO 103-3]	С	None		0.000	86.000	No Ice 1/2" Ice 1" Ice	9.500 11.800 14.100	9.500 11.800 14.100	0.224 0.317 0.410

Dishes											
Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				ft	٥	0	ft	ft		ft ²	K
A-ANT-18G-2-C	Α	Paraboloid w/Shroud (HP)	From Leg	2.000 0.000 2.000	0.000		86.000	2.175	No Ice 1/2" Ice 1" Ice	3.715 4.006 4.296	0.027 0.048 0.068
A-ANT-11G-3-C	В	Paraboloid w/Shroud (HP)	From Leg	2.000 0.000 2.000	0.000		86.000	3.021	No Ice 1/2" Ice 1" Ice	7.170 7.570 7.970	0.050 0.090 0.130

Load Combinations

Comb.		Description
No.		
1	Dead Only	
2	1.2 Dead+1.6 Wind 0 deg - No Ice	
3	0.9 Dead+1.6 Wind 0 deg - No Ice	
4	1.2 Dead+1.6 Wind 30 deg - No Ice	
5	0.9 Dead+1.6 Wind 30 deg - No Ice	
6	1.2 Dead+1.6 Wind 60 deg - No Ice	
7	0.9 Dead+1.6 Wind 60 deg - No Ice	
8	1.2 Dead+1.6 Wind 90 deg - No Ice	
9	0.9 Dead+1.6 Wind 90 deg - No Ice	
10	1.2 Dead+1.6 Wind 120 deg - No Ice	
11	0.9 Dead+1.6 Wind 120 deg - No Ice	
12	1.2 Dead+1.6 Wind 150 deg - No Ice	
13	0.9 Dead+1.6 Wind 150 deg - No Ice	
	Ç	

Comb.	Description
No.	
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42 43	Dead+Wind 90 deg - Service
	Dead+Wind 120 deg - Service
44 45	Dead+Wind 150 deg - Service
	Dead+Wind 180 deg - Service
46 47	Dead+Wind 210 deg - Service
47 48	Dead+Wind 240 deg - Service
48 49	Dead+Wind 270 deg - Service Dead+Wind 300 deg - Service
49 50	
<u> </u>	Dead+Wind 330 deg - Service

Maximum Member Forces

Sectio	Elevation	Component	Condition	Gov.	Axial	Major Axis	Minor Axis
n	ft	Type		Load		Moment	Moment
No.				Comb.	K	kip-ft	kip-ft
L1	119 - 95	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-30.690	-5.589	8.515
			Max. Mx	8	-8.750	-295.268	-2.751
			Max. My	2	-8.671	2.203	302.021
			Max. Vy	8	16.886	-295.268	-2.751
			Max. Vx	2	-17.325	2.203	302.021
			Max. Torque	10			4.965
L2	95 - 47.25	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-54.200	-9.455	11.785
			Max. Mx	8	-20.113	-1388.105	-13.613
			Max. My	2	-20.066	17.746	1416.305
			Max. Vy	20	-26.004	1386.815	19.263
			Max. Vx	14	26.413	-19.122	-1413.977
			Max. Torque	22			-5.289
L3	47.25 - 0	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-75.875	-12.878	14.973
			Max. Mx	20	-34.852	2866.570	37.437
			Max. My	2	-34.851	38.158	2916.961
			Max. Vy	20	-29.936	2866.570	37.437
			Max. Vx	14	30.328	-36.160	-2914.966
			Max. Torque	22			-5.259

Maximum	Reactions
IVIAXIIIIUIII	Reactions

Location	Condition	Gov. Load	Vertical K	Horizontal, X K	Horizontal, Z
			Λ	^	K
		Comb.			
Pole	Max. Vert	27	75.875	0.073	9.098
	Max. H _x	20	34.884	29.899	0.327
	Max. H _z	2	34.884	0.389	30.265
	Max. M _x	2	2916.961	0.389	30.265
	$Max. M_z$	8	2864.251	-29.811	-0.259
	Max. Torsion	10	5.162	-26.042	-15.479
	Min. Vert	7	26.163	-25.730	14.896
	Min. H _x	8	34.884	-29.811	-0.259
	Min. H _z	14	34.884	-0.304	-30.290
	Min. M _x	14	-2914.966	-0.304	-30.290
	Min. M _z	20	-2866.570	29.899	0.327
	Min. Torsion	22	-5.248	26.131	15.479

Tower Mast Reaction Summary

K K K K kip-ft kip Dead Only 29.070 0.000 0.000 -1.754 1.2 Dead+1.6 Wind 0 deg - 34.884 -0.389 -30.265 -2916.961 No Ice 0.9 Dead+1.6 Wind 0 deg - 26.163 -0.389 -30.265 -2887.862 No Ice 1.2 Dead+1.6 Wind 30 deg - 34.884 14.720 -26.072 -2511.238 -1 No Ice	38.159 2 38.506 2 1411.839 0	0.000 2.535 2.487 0.300
1.2 Dead+1.6 Wind 0 deg - 34.884 -0.389 -30.265 -2916.961 No Ice 0.9 Dead+1.6 Wind 0 deg - 26.163 -0.389 -30.265 -2887.862 No Ice 1.2 Dead+1.6 Wind 30 deg - 34.884 14.720 -26.072 -2511.238 -1 No Ice	38.159 2 38.506 2 1411.839 0	2.535 2.487
No Ice 0.9 Dead+1.6 Wind 0 deg - 26.163 -0.389 -30.265 -2887.862 No Ice 1.2 Dead+1.6 Wind 30 deg - 34.884 14.720 -26.072 -2511.238 -1	38.506 2 1411.839 0	2.487
0.9 Dead+1.6 Wind 0 deg - 26.163 -0.389 -30.265 -2887.862 No Ice 1.2 Dead+1.6 Wind 30 deg - 34.884 14.720 -26.072 -2511.238 -1	1411.839 0	
No Ice 1.2 Dead+1.6 Wind 30 deg - 34.884 14.720 -26.072 -2511.238 -1 No Ice	1411.839 0	
1.2 Dead+1.6 Wind 30 deg - 34.884 14.720 -26.072 -2511.238 -1		300
No Ice		
		,.500
0.9 Dead+1.6 Wind 30 deg - 26.163 14.720 -26.072 -2486.114 -1	1397.331 0	0.265
No Ice	1001.001	,. <u>_</u>
1.2 Dead+1.6 Wind 60 deg - 34.884 25.730 -14.896 -1433.309 -2	2470.272 -2	2.479
No Ice		
	2445.404 -2	2.492
No Ice	0004.054	4 500
1.2 Dead+1.6 Wind 90 deg - 34.884 29.811 0.259 27.092 -2 No Ice	2864.251 -4	4.598
	2835.523 -4	4.585
No Ice	1000.020	1.000
1.2 Dead+1.6 Wind 120 deg 34.884 26.042 15.479 1490.062 -2	2501.283 -5	5.162
- No Ice		
•	2476.131 -5	5.127
- No Ice 1.2 Dead+1.6 Wind 150 deg 34.884 15.242 26.522 2549.862 -1	1400 050 4	4.496
1.2 Dead+1.6 Wind 150 deg 34.884 15.242 26.522 2549.862 -1 - No Ice	1466.856 -4	1.490
	1451.815 -4	4.449
- No Ice		
1.2 Dead+1.6 Wind 180 deg 34.884 0.304 30.290 2914.966	-36.159 -2	2.770
- No Ice		
0.9 Dead+1.6 Wind 180 deg 26.163 0.304 30.290 2886.969	-35.081 -2	2.722
- No Ice 1.2 Dead+1.6 Wind 210 deg 34.884 -14.664 26.158 2514.731 1	1400.968 -0	0.314
- No Ice	1400.900 -0).J 1 4
	1388.000 -0	0.279
- No Ice		
	2468.774 2	2.629
- No Ice	0445.070	2044
0.9 Dead+1.6 Wind 240 deg 26.163 -25.777 14.876 1413.792 2 - No Ice	2445.372 2	2.641
	2866.570 4	4.692
- No Ice		
	2839.269 4	4.679
- No Ice		
	2503.654 5	5.248
- No Ice	0.470.040	- 040
0.9 Dead+1.6 Wind 300 deg 26.163 -26.131 -15.479 -1479.182 2	2479.919 5	5.213

Load Combination	Vertical	Shear _x	Shearz	Overturning Moment, M _x	Overturning Moment, Mz	Torque
Combination	K	K	K	kip-ft	kip-ft	kip-ft
- No Ice				<u> </u>	<u></u>	
1.2 Dead+1.6 Wind 330 deg	34.884	-15.299	-26.539	-2555.608	1466.360	4.414
- No Ice						
0.9 Dead+1.6 Wind 330 deg	26.163	-15.299	-26.539	-2530.086	1452.757	4.367
- No Ice						
1.2 Dead+1.0 Ice+1.0 Temp	75.875	0.000	-0.000	-14.973	-12.878	0.003
1.2 Dead+1.0 Wind 0	75.875	-0.073	-9.098	-932.779	-4.850	0.815
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 30	75.875	4.490	-7.855	-806.977	-464.436	0.098
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 60	75.875	7.817	-4.507	-469.002	-799.970	-0.743
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 90	75.875	9.043	0.046	-9.571	-923.885	-1.383
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 120	75.875	7.844	4.598	449.510	-803.549	-1.579
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 150	75.875	4.562	7.902	782.546	-473.174	-1.386
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 180	75.875	0.055	9.104	903.353	-19.269	-0.852
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 210	75.875	-4.478	7.873	778.759	437.509	-0.095
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 240	75.875	-7.827	4.504	438.667	775.069	0.773
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 270	75.875	-9.061	-0.060	- 21.836	899.845	1.402
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 300	75.875	-7.862	-4.597	-479.454	779.534	1.603
deg+1.0 Ice+1.0 Temp	75.075	4.570	7.005	040.004	440.400	4 000
1.2 Dead+1.0 Wind 330	75.875	-4.573	-7.905	-812.804	448.486	1.380
deg+1.0 Ice+1.0 Temp	20.070	0.000	0.470	COO FOC	0.004	0.547
Dead+Wind 0 deg - Service	29.070	-0.083	-6.476	-622.536	6.361	0.547
Dead+Wind 30 deg - Service	29.070	3.150	-5.578	-536.104	-302.420	0.060
Dead+Wind 60 deg - Service Dead+Wind 90 deg - Service	29.070 29.070	5.505 6.378	-3.187 0.055	-306.549	-527.795 -611.700	-0.544 -1.000
- J		5.572		4.432		
Dead+Wind 120 deg - Service	29.070	5.572	3.312	315.990	-534.444	-1.116
Dead+Wind 150 deg -	29.070	3.261	5.675	541.714	-314.166	-0.967
Service	29.070	3.201	5.675	341.714	-314.100	-0.967
Dead+Wind 180 deg -	29.070	0.065	6.481	619.453	-9.465	-0.591
Service	29.070	0.005	0.401	019.433	-9.403	-0.591
Dead+Wind 210 deg -	29.070	-3.138	5.597	534.190	296.580	-0.062
Service	29.070	-3.130	3.391	334.190	290.300	-0.002
Dead+Wind 240 deg -	29.070	-5.515	3.183	302.588	523.954	0.570
Service	23.070	-0.010	5.105	302.300	020.004	0.370
Dead+Wind 270 deg -	29.070	-6.397	-0.070	-9.307	608.671	1.014
Service	25.070	-0.001	-0.070	-5.501	000.071	1.014
Dead+Wind 300 deg -	29.070	-5.591	-3.312	-319.571	531.420	1.135
Service	20.010	0.001	-0.012	313.371	331.720	1.100
Dead+Wind 330 deg -	29.070	-3.273	-5.678	-545.602	310.526	0.956
Service	_0.070	0.2.0	0.010	310.00L	310.020	0.000

Solution Summary

	Sur	n of Applied Force	es		Sum of Reactio	ns	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
1	0.000	-29.070	0.000	0.000	29.070	0.000	0.000%
2	-0.389	-34.884	-30.265	0.389	34.884	30.265	0.000%
3	-0.389	-26.163	-30.265	0.389	26.163	30.265	0.000%
4	14.720	-34.884	-26.072	-14.720	34.884	26.072	0.000%
5	14.720	-26.163	-26.072	-14.720	26.163	26.072	0.000%
6	25.730	-34.884	-14.896	-25.730	34.884	14.896	0.000%
7	25.730	-26.163	-14.896	-25.730	26.163	14.896	0.000%
8	29.811	-34.884	0.259	-29.811	34.884	-0.259	0.000%
9	29.811	-26.163	0.259	-29.811	26.163	-0.259	0.000%
10	26.042	-34.884	15.479	-26.042	34.884	-15.479	0.000%

	Sur	n of Applied Force	s		Sum of Reactio	ns	
Load	PX	PY	PZ	PX	PY	PZ	% Erro
Comb.	K	K	K	K	K	K	
11	26.042	-26.163	15.479	-26.042	26.163	-15.479	0.000%
12	15.242	-34.884	26.522	-15.242	34.884	-26.522	0.000%
13	15.242	-26.163	26.522	-15.242	26.163	-26.522	0.000%
14	0.304	-34.884	30.290	-0.304	34.884	-30.290	0.000%
15	0.304	-26.163	30.290	-0.304	26.163	-30.290	0.000%
16	-14.664	-34.884	26.158	14.664	34.884	-26.158	0.000%
17	-14.664	-26.163	26.158	14.664	26.163	-26.158	0.000%
18	- 25.777	-34.884	14.876	25.777	34.884	-14.876	0.000%
19	- 25.777	-26.163	14.876	25.777	26.163	-14.876	0.000%
20	-29.899	-34.884	-0.327	29.899	34.884	0.327	0.000%
21	-29.899	-26.163	-0.327	29.899	26.163	0.327	0.000%
22	-26.131	-34.884	-15.479	26.131	34.884	15.479	0.000%
23	-26.131	-26.163	-15.479	26.131	26.163	15.479	0.000%
24	-15.299	-34.884	-26.539	15.299	34.884	26.539	0.000%
25	-15.299	-26.163	-26.539	15.299	26.163	26.539	0.000%
26	0.000	-75.875	0.000	-0.000	75.875	0.000	0.000%
27	-0.073	-75.875	-9.098	0.073	75.875	9.098	0.000%
28	4.490	-75.875	-7.855	-4.490	75.875	7.855	0.000%
29	7.817	-75.875	-4.507	-7.817	75.875	4.507	0.000%
30	9.043	-75.875	0.046	-9.043	75.875	-0.046	0.000%
31	7.844	-75.875	4.598	-7.844	75.875	-4.598	0.000%
32	4.562	-75.875	7.902	-4.562	75.875	-7.902	0.000%
33	0.055	-75.875	9.104	-0.055	75.875	-9.104	0.000%
34	-4.478	-75.875	7.873	4.478	75.875	-7.873	0.000%
35	-7.827	-75.875	4.504	7.827	75.875	-4.504	0.000%
36	-9.061	-75.875	-0.060	9.061	75.875	0.060	0.000%
37	-7.862	-75.875	-4.597	7.862	75.875	4.597	0.000%
38	-4.573	-75.875	-7.905	4.573	75.875	7.905	0.000%
39	-0.083	-29.070	-6.476	0.083	29.070	6.476	0.000%
40	3.150	-29.070	-5.578	-3.150	29.070	5.578	0.000%
41	5.505	-29.070	-3.187	-5.505	29.070	3.187	0.000%
42	6.378	-29.070	0.055	-6.378	29.070	-0.055	0.000%
43	5.572	-29.070	3.312	-5.572	29.070	-3.312	0.000%
44	3.261	-29.070	5.675	-3.261	29.070	-5.675	0.000%
45	0.065	-29.070	6.481	-0.065	29.070	-6.481	0.000%
46	-3.138	-29.070	5.597	3.138	29.070	-5.597	0.000%
47	-5.515	-29.070	3.183	5.515	29.070	-3.183	0.000%
48	-6.397	-29.070	-0.070	6.397	29.070	0.070	0.000%
49	-5.591	-29.070	-3.312	5.591	29.070	3.312	0.000%
50	-3.273	-29.070	-5.678	3.273	29.070	5.678	0.000%

Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	4	0.0000001	0.0000001
2	Yes	5	0.0000001	0.00010964
3	Yes	5	0.0000001	0.00004526
4	Yes	6	0.0000001	0.00007783
5	Yes	5	0.0000001	0.00073426
6	Yes	6	0.0000001	0.00008329
7	Yes	5	0.0000001	0.00079034
8	Yes	5	0.0000001	0.00028590
9	Yes	5	0.0000001	0.00012268
10	Yes	6	0.0000001	0.00007117
11	Yes	5	0.0000001	0.00066894
12	Yes	6	0.0000001	0.00008954
13	Yes	5	0.0000001	0.00084901
14	Yes	5	0.0000001	0.00025168
15	Yes	5	0.0000001	0.00010453
16	Yes	6	0.0000001	0.00007695
17	Yes	5	0.0000001	0.00072907
18	Yes	6	0.0000001	0.00007166
19	Yes	5	0.0000001	0.00067655
20	Yes	5	0.0000001	0.00040521

21 Yes 5 0.00000001 0.00017274 22 Yes 6 0.00000001 0.00009066 23 Yes 5 0.00000001 0.00086187 24 Yes 6 0.00000001 0.00007185 25 Yes 5 0.00000001 0.00067514 26 Yes 4 0.00000001 0.00021572 27 Yes 5 0.00000001 0.00089685 28 Yes 6 0.00000001 0.00027770 29 Yes 6 0.00000001 0.00029058 30 Yes 5 0.00000001 0.00029058 31 Yes 6 0.00000001 0.0002896 31 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022995 <td< th=""><th></th></td<>	
23 Yes 5 0.00000001 0.00086187 24 Yes 6 0.00000001 0.00007185 25 Yes 5 0.00000001 0.00067514 26 Yes 4 0.00000001 0.00021572 27 Yes 5 0.00000001 0.0008685 28 Yes 6 0.00000001 0.00027770 29 Yes 6 0.00000001 0.00029058 30 Yes 5 0.00000001 0.00029058 31 Yes 6 0.00000001 0.0002898 32 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00029341 37 Yes 6 0.00000001 0.00029341	
24 Yes 6 0.00000001 0.00007185 25 Yes 5 0.00000001 0.00067514 26 Yes 4 0.00000001 0.00021572 27 Yes 5 0.00000001 0.00089685 28 Yes 6 0.00000001 0.00027770 29 Yes 6 0.00000001 0.00029058 30 Yes 5 0.00000001 0.00029058 31 Yes 6 0.00000001 0.00023898 32 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00086618 34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00029341 37 Yes 6 0.00000001 0.00029341	
25 Yes 5 0.00000001 0.00067514 26 Yes 4 0.00000001 0.00021572 27 Yes 5 0.00000001 0.00089685 28 Yes 6 0.00000001 0.00027770 29 Yes 6 0.00000001 0.00029058 30 Yes 5 0.00000001 0.00098945 31 Yes 6 0.00000001 0.00023898 32 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00086618 34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00029341 37 Yes 6 0.00000001 0.00029341	
26 Yes 4 0.00000001 0.00021572 27 Yes 5 0.00000001 0.00089685 28 Yes 6 0.00000001 0.00027770 29 Yes 6 0.00000001 0.00029058 30 Yes 5 0.00000001 0.0002898 31 Yes 6 0.00000001 0.00023898 32 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00086618 34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00096934 37 Yes 6 0.00000001 0.00029341	
27 Yes 5 0.00000001 0.00089685 28 Yes 6 0.00000001 0.00027770 29 Yes 6 0.00000001 0.00029058 30 Yes 5 0.00000001 0.00098945 31 Yes 6 0.00000001 0.00023898 32 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00086618 34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00096934 37 Yes 6 0.00000001 0.00029341	
28 Yes 6 0.00000001 0.00027770 29 Yes 6 0.00000001 0.00029058 30 Yes 5 0.00000001 0.00098945 31 Yes 6 0.00000001 0.00023898 32 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00086618 34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00096934 37 Yes 6 0.00000001 0.00029341	
29 Yes 6 0.00000001 0.00029058 30 Yes 5 0.00000001 0.00098945 31 Yes 6 0.00000001 0.00023898 32 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00086618 34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00096934 37 Yes 6 0.00000001 0.00029341	
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31 Yes 6 0.00000001 0.00023898 32 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00086618 34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00096934 37 Yes 6 0.00000001 0.00029341	
32 Yes 6 0.00000001 0.00028256 33 Yes 5 0.00000001 0.00086618 34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00096934 37 Yes 6 0.00000001 0.00029341	
33 Yes 5 0.00000001 0.00086618 34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00096934 37 Yes 6 0.00000001 0.00029341	
34 Yes 6 0.00000001 0.00022996 35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00096934 37 Yes 6 0.00000001 0.00029341	
35 Yes 6 0.00000001 0.00022095 36 Yes 5 0.00000001 0.00096934 37 Yes 6 0.00000001 0.00029341	
36 Yes 5 0.0000001 0.00096934 37 Yes 6 0.0000001 0.00029341	
37 Yes 6 0.00000001 0.00029341	
38 Yes 6 0.0000001 0.00024593	
39 Yes 4 0.00000001 0.00024932	
40 Yes 4 0.00000001 0.00071463	
41 Yes 4 0.00000001 0.00087861	
42 Yes 4 0.00000001 0.00048393	
43 Yes 4 0.00000001 0.00068917	
44 Yes 5 0.00000001 0.00004428	
45 Yes 4 0.00000001 0.00029997	
46 Yes 4 0.00000001 0.00067217	
47 Yes 4 0.00000001 0.00058880	
48 Yes 4 0.00000001 0.00051711	
49 Yes 5 0.00000001 0.00004609	
50 Yes 4 0.00000001 0.00065366	

Maximum Tower Deflections - Service Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	119 - 95	18.409	50	1.431	0.015
L2	99 - 47.25	12.668	50	1.269	0.008
L3	52.75 - 0	3.354	50	0.601	0.002

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
121.000	(2) RA21.7770.00 w/ Mount Pipe	50	18.409	1.431	0.015	18047
110.000	(2) LPA-80063-4CF-EDIN-5 w/	50	15.762	1.366	0.012	10026
	Mount Pipe					
98.000	(2) AIR 21 w/ Mount Pipe	50	12.400	1.258	0.008	4562
88.000	A-ANT-18G-2-C	50	9.868	1.136	0.005	4183
86.000	LLPX310R-V1 w/ Mount Pipe	50	9.395	1.108	0.005	4128

Maximum Tower Deflections - Design Wind

Section No.	Elevation	Horz. Deflection	Gov. Load	Tilt	Twist
	ft	in	Comb.	0	0
L1	119 - 95	86.264	24	6.716	0.071
L2	99 - 47.25	59.408	24	5.958	0.036
L3	52.75 - 0	15.744	24	2.824	0.009

No. Deflection Load	vist	Twist	Tilt	Gov.	Horz.	Elevation	Section
				Load	Deflection		No.
ft in Comb. °	0	0	0	Comb.	in	ft	

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
121.000	(2) RA21.7770.00 w/ Mount Pipe	24	86.264	6.716	0.071	3987
110.000	(2) LPA-80063-4CF-EDIN-5 w/	24	73.887	6.414	0.054	2214
98.000	Mount Pipe (2) AIR 21 w/ Mount Pipe	24	58.153	5.909	0.035	1004
88.000	A-ANT-18G-2-C	24	46.295	5.334	0.033	914
86.000	LLPX310R-V1 w/ Mount Pipe	24	44.079	5.205	0.022	901

Compression Checks

Pole Design Data

Section No.	Elevation	Size	L	Lu	KI/r	Α	Pu	ϕP_n	Ratio Pu
	ft		ft	ft		in²	K	K	ϕP_n
L1	119 - 95 (1)	TP27.38x21x0.188	24.000	0.000	0.0	15.550	-8.656	1041.460	0.008
L2	95 - 47.25 (2)	TP39.57x25.942x0.25	51.750	0.000	0.0	30.051	-20.037	1944.740	0.010
L3	47.25 - 0 (3)	TP51.5x37.622x0.313	52.750	0.000	0.0	50.772	-34.850	3169.190	0.011

Pole Bending Design Data

Section No.	Elevation	Size	M _{ux}	φM _{nx}	Ratio M _{ux}	Muy	ϕM_{ny}	Ratio M _{uy}
	ft		kip-ft	kip-ft	ϕM_{nx}	kip-ft	kip-ft	$\frac{M_{uy}}{\phi M_{ny}}$
L1	119 - 95 (1)	TP27.38x21x0.188	302.498	559.959	0.540	0.000	559.959	0.000
L2	95 - 47.25 (2)	TP39.57x25.942x0.25	1426.467	1516.392	0.941	0.000	1516.392	0.000
L3	47.25 - 0 (3)	TP51.5x37.622x0.313	2946.408	3341.650	0.882	0.000	3341.650	0.000

Pole Shear Design Data

Section	Elevation	Size	Actual	ϕV_n	Ratio	Actual	ϕT_n	Ratio
No.			V_u		V_u	T_u		T_u
	ft		K	K	ϕV_n	kip-ft	kip-ft	φ <i>T</i> _n
L1	119 - 95 (1)	TP27.38x21x0.188	17.368	520.731	0.033	4.067	1122.500	0.004
L2	95 - 47.25 (2)	TP39.57x25.942x0.25	26.737	972.372	0.027	4.427	3039.517	0.001
L3	47.25 - 0 (3)	TP51.5x37.622x0.313	30.671	1584.590	0.019	4.414	6697.650	0.001

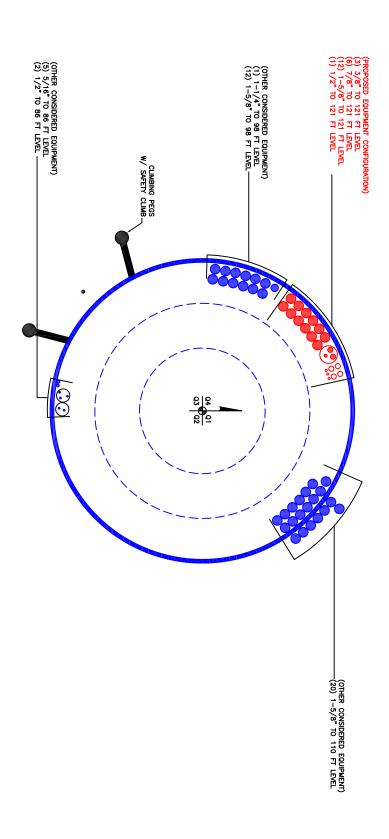
Pole Interaction Design Data

Section No.	Elevation	Ratio Pu	Ratio M _{ux}	Ratio Muv	Ratio Vu	Ratio Tu	Comb. Stress	Allow. Stress	Criteria
	ft	ϕP_n	φ <i>M</i> _{nx}	ϕM_{ny}	$\overline{\phi V_n}$	φ <i>T</i> _n	Ratio	Ratio	
L1	119 - 95 (1)	0.008	0.540	0.000	0.033	0.004	0.550	1.000	4.8.2
L2	95 - 47.25 (2)	0.010	0.941	0.000	0.027	0.001	0.952	1.000	4.8.2
L3	47.25 - 0 (3)	0.011	0.882	0.000	0.019	0.001	0.893	1.000	4.8.2

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	øP _{allow} K	% Capacity	Pass Fail
L1	119 - 95	Pole	TP27.38x21x0.188	1	-8.656	1041.460	55.0	Pass
L2	95 - 47.25	Pole	TP39.57x25.942x0.25	2	-20.037	1944.740	95.2	Pass
L3	47.25 - 0	Pole	TP51.5x37.622x0.313	3	-34.850	3169.190	89.3	Pass
							Summary	
						Pole (L2)	95.2	Pass
						RATING =	95.2	Pass

APPENDIX B BASE LEVEL DRAWING



BUSINESS UNIT: 857012 TOWER ID: C_BASELEVEL

APPENDIX C ADDITIONAL CALCULATIONS

Monopole Base Plate Connection

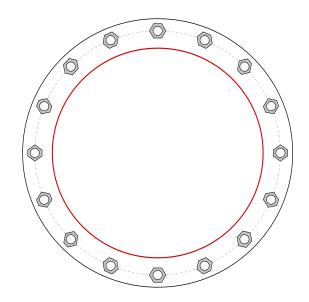


Site Info		
	BU#	857012
	Site Name	nville South Washingto
	Order#	443486 - Rev. 0

Analysis Considerations							
TIA-222 Revision	G						
Grout Considered:	No						
I _{ar} (in)	0						
Eta Factor, η	0.5						

Applied Loads						
Moment (kip-ft)	2946.41					
Axial Force (kips)	34.85					
Shear Force (kips)	30.67					

51.5" x 0.3125" 18-sided pole (A572-65; Fy=65 ksi, Fu=80 ksi)



Connection Properties	Analysis Results					
Anchor Rod Data	Anchor Rod Summary		(units of kips, kip-in)			
(16) 2-1/4" ø bolts (A615-75 N; Fy=75 ksi, Fu=100 ksi) on 60" BC	Pu = 149.41	φPn = 260	Stress Rating			
	Vu = 1.92	φVn = n/a	58.9%			
Base Plate Data	Mu = n/a	φMn = n/a	Pass			
66" OD x 2" Plate (A572-60; Fy=60 ksi, Fu=75 ksi)						
	Base Plate Summary					
Stiffener Data	Max Stress (ksi):	38.28	(Flexural)			
N/A	Allowable Stress (ksi):	54				
	Stress Rating:	70.9%	Pass			
Pole Data	•					

CCIplate - version 3.2.0 Analysis Date: 9/6/2018

Drilled Pier Foundation

BU # : 857012 Site Name: Plainville South Washir Order Number: 449205 R 1

TIA-222 Revison: G
Tower Type: Monopole

Applied Loads									
Comp. Uplift									
Moment (kip-ft)	2946								
Axial Force (kips)	35								
Shear Force (kips)	31								

Material Properties							
Concrete Strength, f'c:	4	ksi					
Rebar Strength, Fy:	60	ksi					

	Pier Desi	ign Data									
	Depth	37	ft								
	Ext. Above Grade	1	ft								
	Pier Section 1										
	From 1' above grade	to 37' below g	grade								
	Pier Diameter	7	ft								
-	Rebar Quantity	18									
	Rebar Size	11									
	Clear Cover to Ties	4	in								
	Tie Size	5									

Groundwater Depth

4 ft

<u> </u>	is Results	
Soil Lateral Capacity	Compression	Uplift
D _{v=0} (ft from TOC)	9.79	-
Soil Safety Factor	4.11	-
Max Moment (kip-ft)	3201.18	-
Rating	32.3%	-
Soil Vertical Capacity	Compression	Uplift
Skin Friction (kips)	314.36	-
End Bearing (kips)	237.05	-
Weight of Concrete (kips)	168.14	-
Total Capacity (kips)	551.42	-
Axial (kips)	203.14	-
Rating	36.8%	-
Reinforced Concrete Capacity	Compression	Uplift
Critical Depth (ft from TOC)	9.58	-
Critical Moment (kip-ft)	3201.00	-
Critical Moment Capacity	4651.94	-
Rating	68.8%	-
•		

CROWN

Check Limitation N/A

Soil In	teraction Rating	36.8%
Structural Fo	undation Rating	68.8%
	Soil	l Profile
	301	rione
# of Layers	7	

Layer	Top (ft)	Bottom (ft)	Thickness (ft)	Y _{soil} (pcf)	Y _{concrete} (pcf)	Cohesion (ksf)	Angle of Friction (degrees)	Calculated Ultimate Skin Friction Comp (ksf)	Calculated Ultimate Skin Friction Uplift (ksf)	Ultimate Skin Friction Comp Override (ksf)	Ultimate Skin	Ult. Gross Bearing Capacity (ksf)	SPT Blow Count	Soil Type
1	0	3.5	3.5	55	150	0	0	0.000	0.000	0.00	0.00			Cohesionless
2	3.5	4	0.5	55	150	0	33	0.000	0.000	0.32	0.32			Cohesionless
3	4	13	9	55	87.6	0	33	0.000	0.000	0.32	0.32			Cohesionless
4	13	15	2	45	87.6	0	28	0.000	0.000	0.50	0.50			Cohesionless
5	15	19	4	45	87.6	0	28	0.000	0.000	0.56	0.56			Cohesionless
6	19	23	4	55	87.6	0	33	0.000	0.000	0.64	0.64			Cohesionless
7	23	37	14	40	87.6	0	28	0.00	0.00	0.73	0.73	8.213		Cohesionless



June 20, 2018



SAI Communications 12 Industrial Way Salem NH, 03079

RE: Site Number:

CT1029 (LTE 4C/5C)

FA Number: PACE Number: PTN Number:

MRCTB032005 2051A0GGZC

10105805

Site Name: Site Address: Plainville South Washington Street 335 South Washington Street

Plainville, CT 06062

To Whom It May Concern:

Hudson Design Group LLC (HDG) has been authorized by SAI Communications to perform a mount analysis on the existing AT&T antenna mount to determine its capability of supporting the following equipment loading:

- (3) 7770 Antennas (55.0"x11.0"x5.0" Wt. = 35 lbs. /each)
- (3) HPA-65R-BUU-H6 Antennas (72.0"x14.8"x9.0" Wt. = 51 lbs. /each)
- (3) QS66512-2 Antennas (72"x12.0"x9.6" Wt. = 111 lbs. /each)
- (3) RRUS-11 RRH's (19.7"x17.0"x7.2" -Wt. = 51 lbs. /each)
- (3) RRUS-12 RRH's (20.4"x18.5"x7.5" Wt. = 58 lbs. /each)
- (3) A2 Modules (16.4"x15.2"x3.4" Wt. = 22 lbs. /each)
- (3) RRUS-32 RRH's (27.2"x12.1"x7.0" Wt. = 60 lbs. /each)
- (3) RRUS-32 B2 RRH's (27.2"x12.1"x7.0" Wt. = 60 lbs. /each)
- (6) LGP21401 TMA's (14.4"x9"x2.7" Wt. = 19 lbs. /each)
- (2) Squid Surge Arrestors (24.0"x9.7"ø Wt. = 33 lbs. /each)
- (3) 800-10965 Antennas (78.7"x20.0"x6.9" Wt. = 109 lbs. /each)
- (3) 4478 B5 RRH's (18.1"x13.4"x8.3"— Wt. = 60 lbs. /each)
- (3) 4426 B66 RRH's (15"x13.2"x7.4" Wt. = 49 lbs. /each)
- (1) Squid Surge Arrestor (24.0"x9.7"ø Wt. = 33 lbs. /each)

*Proposed Loading Shown in Bold.

No original structural design documents or fabrication drawings were available for the existing mount. HDG's sub-consultant, ProVertic LLC, conducted a survey climb and mapping of the existing AT&T antenna mount on January 28, 2018.

Mount Analysis Methods:

- This analysis was conducted in accordance with EIA/TIA-222-G, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and the International Building Code 2012 with 2005 Connecticut Supplement with 2016 Amendments, and AT&T Mount Technical Directive R5.
- HDG considers this mount to be asymmetrical and has applied wind loads in 30 degree increments all
 around the mount. Per TIA-222-G, the max basic wind speed for this site is equal to 105 mph with a max
 basic wind speed with ice of 50 mph. Per the AT&T Mount Technical Directive and Appendix N of the
 Connecticut State Building Code, an ultimate wind speed of 125 mph converted to a nominal wind
 speed of 97 mph was used for this analysis.
- HDG considers this site to be exposure category C; tower is located in large, flat, open, terrain/grasslands.

- HDG considers this site to be topographic category 1; tower is located in flat terrain.
- The mount has been analyzed with load combinations consisting of 500 lbs live load using a service wind speed of 30 mph wind on the worst case antenna. Analysis performed on each antenna pipe to determine worst case location; worst case location was antenna position 4.
- The mount has been analyzed with load combinations consisting of a 250 lbs live load in a worst case location on the mount.

Based on our analysis, we have determined that the existing antenna mount **IS NOT CAPABLE** of supporting the proposed antenna installation. HDG recommends the following modifications:

- Install new platform reinforcement kit, SitePro1 P/N PRK-1245 (or approved equal).
- Install new handrail kit, SitePro1 P/N HRK12-U (or approved equal).

	Member(s)	Controlling Load Case	Stress Ratio	Pass/Fail
Existing 4C/5C Mount Rating	43	LC2	114%	FAIL
Proposed 4C/5C Mount Rating	81	LC10	66%	PASS

Reference Documents:

Mount Mapping Report prepared by ProVertic LLC dated March 23, 2018.

This determination was based on the following limitations and assumptions:

- 1. HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
- 2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
- 3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
- 4. The existing mount has been adequately secured to the tower structure per the mount manufacturer's specifications.
- 5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
- 6. HDG performed a localized analysis on the mount itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted, Hudson Design Group LLC

mla Cll

Michael Cabral Structural Dept. Head Daniel P. Hamm, PE Principal

FIELD PHOTOS:



























Wind & Ice Calculations Date:

6/20/2018

Project Name: Plainville South Washington Street

Project Number: CT1029

Designed By: LN Checked By: MSC



2.6.5.2 Velocity Pressure Coeff:

$$K_z = 2.01 (z/z_g)^{2/\alpha}$$

K_z=

122 (ft) Z=

 $z_g =$

900 (ft)

1.320

9.5 α=

 $Kzmin \le Kz \le 2.01$

Table 2-4

Exposure	Z _g	α	K _{zmin}	K _e
В	1200 ft	7.0	0.70	0.9
С	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

2.6.6.4 Topographic Factor:

Table 2-5

Topo. Category	K _t	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} = [1 + (K_e K_t/K_h)]^2$$

$$K_h = e^{-(f*z/H)}$$

K_{zt}= #DIV/01

#DIV/0! K_h=

 $K_e =$

0 (from Table 2-4)

K_t=

0 (from Table 2-5)

f=

0 (from Table 2-5)

Category= 1

(If Category 1 then K zt =1.0)

122 z=

H=

0 (Ht. of the crest above surrounding terrain)

 $K_{zt} =$ 1.00

K_{iz} = 1.14 (from Sec. 2.6.8)

2.6.8 Design Ice Thickness

Max Ice Thickness =

1.00 in

 $t_{iz} = 2.0*t_i*I*K_{iz}*(Kzt)^{0.35}$

2.28 in

Date:

6/20/2018

Project Name: Plainville South Washington Street

Project Number: CT1029

Designed By: LN Checked By: MSC



2.6.7 Gust Effect Factor

2.6.7.1 Self Supporting Lattice Structures

Gh = 1.0 Latticed Structures > 600 ft

Gh = 0.85 Latticed Structures 450 ft or less

Gh = 0.85 + 0.15 [h/150 - 3.0]

h= ht. of structure

h= 121

Gh= 0.85

2.6.7.2 Guyed Masts

Gh= 0.85

2.6.7.3 Pole Structures

Gh= 1.1

2.6.9 Appurtenances

Gh= 1.0

2.6.7.4 Structures Supported on Other Structures

(Cantilivered tubular or latticed spines, pole, structures on buildings (ht.: width ratio > 5)

Gh=

1.35

Gh=

1.00

2.6.9.2 Design Wind Force on Appurtenances

State Code Ultimate Design Wind Speed:

 $V_{ult} = 125 \text{ mph}$

Nomial Design Wind Speed,

 $V_{asd} = V_{ult} V(0.6)$

 $V_{asd} =$

97 mph

V_{asd} per the AT&T Mount Technical Directive and Connecticut State Building Code, Latest Edition.

Per TIA-222-G,

 $q_z =$

q_{z (Ice)}=

 $q_{z(30)} =$

V_{min} =

90 mph

V_{max} =

105 mph

F= qz*Gh*(EPA)A

 $q_z = 0.00256*K_z*K_{zt}*K_d*V_{max}^2*I$

30.09

8.02

2.89

K_z= 1.320

K_{zt}= 1.0

K_d= 0.95

<u>-</u> 0.:

V_{asd}=

97 mph

30 mph

V_{max (ice)}=

_{ce)}= 50 mph

V₃₀=

1.0

Table 2-2

Structure Type	Wind Direction Probability Factor, Kd
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95

Project Name: Plainville South Washington Street

Project Number: CT1029

Designed By: LN Checked By: MSC



Determine Ca:

Table 2-8

		Force Coefficients (Ca) for	Appurtenances		
	ember Type	Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25	
IV	lember type	Ca	Ca	Ca	
	Flat	1.2	1.4	2.0	
Round	C < 32	0.7	0.0	4.2	
	(Subcritical)	0.7	0.8	1.2	
	32 ≤ C ≤ 64	44 -0 485	44-0415	10.	
	(Transitional)	3.76/(C ^{0,485})	3.37/(C ^{0.415})	38.4/(C ^{-1.0})	
	C > 64	0.5	0.6	0.6	
	(Supercritical)	0.5	0.6	0.6	

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.

(Aspect ratio is independent of the spacing between support points of a linear appurtenance,

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness =	2.28	in	Angle =	0 (deg)		Equival	ent Angle =	180 (deg)	
<u>Appurtenances</u>	<u>Height</u>	Width	<u>Depth</u>	Flat Area	Aspect Ratio	<u>Ca</u>	Force (lbs)	Force (lbs) (w/ lce)	Force (lbs) (30 mph)
7770 Antenna	55.0	11.0	5.0	4.20	5.00	1.31	166	68	16
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.86	1.31	291	108	28
QS66512-2 Antenna	72.0	12.0	9.6	6.00	6.00	1.36	245	96	23
800-10965 Antenna	78.7	20.0	6.9	10.93	3.94	1.26	416	144	40
RRUS-11 RRH RRUS-11 RRH (Shielded)	19.7 19.7	17.0 6.0	7.2 7.2	2.33 0.82	1.16 3.28	1.20 1.23	84 30	35 18	8
RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded)	20.4 20.4	18.5 7.5	10.9 10.9	2.62 1.06	1.10 2.72	1.20 1.21	95 39	38 20	9 4
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 1.1	7.0 7.0	2.29 0.21	2.25 24.73	1.20 1.99	83 12	35 20	8 1
4478 B5 RRH 4478 B5 RRH (Shielded)	18.1 18.1	13.4 2.4	8.3 8.3	1.68 0.30	1.35 7.54	1.20 1.42	61 13	27 12	6 1
4426 B66 RRH 4426 B66 RRH (Shielded)	15.0 15.0	13.2 2.2	7.4 7.4	1.38 0.23	1.14 6.82	1.20 1.39	50 10	23 10	5 1
LGP21401 TMA	14.4	9.0	2.7	0.90	1.60	1.20	32	17	3
Squid Surge Arrestor	24.0	9.7		1.62	2.47	0.70	34	16	3

Date: 6

6/20/2018

Project Name: Plainville South Washington Street

Project Number: CT1029

Designed By: LN Checked By: MSC



WIND LOADS Ice Thickness = Equivalent Angle = 210 (deg) Angle = 30 2.28 in. (deg) WIND LOADS WITH NO ICE: Appurtenances Height Width Depth Flat Area Flat Area Aspect Aspect Ca (normal) Force Force Force (side) (normal) (side) Ratio Ratio (lbs) (lbs) (lbs) 7770 Antenna 55.0 11.0 5.0 4.20 1.91 11,00 1,31 166 88 146 5.00 1,53 HPA-65R-BUU-H6 Antenna 72.0 14.8 9.0 7.40 4.50 4.86 8.00 1.31 1.43 291 194 266 72.0 12.0 9.6 6.00 4.80 245 235 QS66512-2 Antenna 6,00 7,50 1,36 800-10965 Antenna 78.7 10.93 3.77 176 356 20.0 6.9 3.94 11.41 1.26 1.55 416 RRUS-11 RRH 19.7 17.0 2.33 0.99 1.16 2.74 1.20 1.21 72 RRUS-11 RRH (Shielded) 19.7 8.5 7.2 1.16 0.99 2.32 2.74 1.20 1.21 42 36 40 RRUS-12 + A2 RRH 20.4 18.5 10.9 2.62 1.54 1.10 1.87 1.20 RRUS-12 + A2 RRH (Shielded) 20.4 9.3 10.9 1.31 1.54 2.21 1.87 1.20 1.20 47 56 49 RRUS-32 RRH 27,2 2.25 RRUS-32 RRH (Shielded) 27.2 6.1 7.0 1.14 1.32 4.50 3 89 1.29 1.26 44 50 46 4478 B5 RRH 18,1 1,35 2,19 1,20 1,20 4478 B5 RRH (Shielded) 18,1 6.7 8.3 0.84 1.04 2.70 2,19 1.21 1.20 31 37 32 1,14 2,03 1,20 4426 B66 RRH (Shielded) 15.0 2.2 7.4 0.23 0.77 6.82 2.03 1.39 1.20 10 28 14 LGP21401 TMA 14,4 9.0 2.7 0.90 0,27 32 11 27 1,60 5,33 1.20 1.33 WIND LOADS WITH ICE: 59.6 15.6 9.6 6.44 3.95 60 3.83 6.23 1,26 1,37 HPA-65R-BUU-H6 Antenna 76.6 19.4 13.6 10.29 7.21 104 77 98 3.95 5.65 1.26 1.34 QS66512-2 Antenna 76.6 16.6 14.2 8.80 7.53 4.62 5.41 1,29 1,33 91 80 89 800-10965 Antenna 83.3 24.6 11.5 14.20 6.63 125 1.41 141 75 3.39 7.27 1.24 RRUS-11 RRH 24.3 21.6 11.8 3.63 1.98 1 13 2.06 1.20 1.20 19 31 RRUS-11 RRH (Shielded) 24.3 10.8 11.8 1.82 1.98 2.25 2.06 1,20 1.20 17 19 18 RRUS-12 + A2 RRH 25.0 23,1 15.5 4.00 2.68 1.08 1.61 1.20 1.20 26 RRUS-12 + A2 RRH (Shielded) 25.0 11.5 15.5 2.00 2.68 2.16 1.61 1.20 1.20 19 26 21 RRUS-32 RRH 31.8 16.7 11.6 3,67 2.55 1.91 2,75 1,20 1,21 25 33 RRUS-32 RRH (Shielded) 31.8 8.3 11.6 1.84 2.55 3.81 2.75 1.26 1.21 19 25 20 4478 B5 RRH 22.7 18.0 12.8 2.83 2,02 1,26 1,20 1.20 4478 B5 RRH (Shielded) 22.7 9.0 12.8 1.41 2.02 2.52 1.77 1,20 1.20 19 15 19,6 17.8 12.0 2.41 1.62 1,10 1,64 1,20 1.20 4426 B66 RRH (Shielded) 19.6 6.8 12.0 0.92 1.62 2.89 1.64 1.22 1.20 11 15 LGP21401 TMA 19,0 13.6 7.3 1.79 0.96 1,40 2.61 1,20 1_20 17 WIND LOADS AT 30 MPH: 55.0 11.0 5.0 4.20 1.91 5.00 1.31 1,53 14 7770 Antenna 26 HPA-65R-BUU-H6 Antenna 72.0 14.8 9.0 7.40 4.50 4.86 1.31 1.43 19 8.00 QS66512-2 Antenna 72.0 12.0 9.6 6.00 4.80 6,00 7.50 1.36 1.42 23 23 800-10965 Antenna 78.7 20.0 10.93 3.77 3,94 1,55 34 11,41 1,26 RRUS-11 BRH 197 17.0 72 2 33 0.99 1 16 2.74 1.20 1.21 RRUS-11 RRH (Shielded) 19.7 8.5 7.2 1,16 0.99 2.32 2.74 1.20 1,21 RRUS-12 + A2 RRH 20.4 18.5 10.9 2.62 1.54 1.10 1.87 1:20 1.20 RRUS-12 + A2 RRH (Shielded) 20.4 9.3 10.9 1.31 1.54 2,21 1,87 1,20 1.20 RRUS-32 RRH 2,25 3,89 1.20 1.26 RRUS-32 RRH (Shielded) 27.2 6.1 7.0 1.14 1.32 4.50 3.89 1.29 1.26 4478 B5 RRH 1.35 1.20 1.20 4478 B5 RRH (Shielded) 18.1 6.7 8.3 0.84 1.04 2,70 2.19 1.21 1.20 13.2 1,14 2.03 1,20 1,20 4426 B66 RRH (Shielded) 15.0 2.2 0.23 0.77 1,39 LGP21401 TMA 14.4 0.90 0.27 3 9.0 2.7 1,60 5,33 1,20 1.33 1

Project Name: Plainville South Washington Street

Project Number: CT1029
Designed By: LN Checked By: MSC



Angle = 60	(deg)		Ice Thick	ness =	2.28	in.		I	Equivale	ent Angle =	240	(deg)
WIND LOADS WITH NO ICE:												
Appurtenances	<u>Height</u>	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
7770 Antenna	55,0	11,0	5.0	4,20	1.91	5,00	11.00	1.31	1,53	166	68	108
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4,86	8.00	1,31	1,43	291	194	218
QS66512-2 Antenna	72.0	12,0	9.6	6.00	4.80	6,00	7,50	1,36	1,42	245	205	215
800-10965 Antenna	78.7	20.0	6.9	10.93	3,77	3,94	11.41	1,26	1,55	416	176	236
RRUS-11 RRH RRUS-11 RRH (Shielded)	19.7 19.7	17.0 12.8	7.2 7.2	2,33 1,74	0.99	1,16 1,55	2.74 2.74	1.20	1.21	84 63	36 36	48 43
RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shleided)	20.4	18.5 13.9	10.9 10.9	2.62 1.97	1,54 1,54	1.10 1.47	1.87 1.87	1.20 1.20	1,20 1,20	95 71	56 56	65 60
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 9.1	7,0 7,0	2.29 1.71	1,32 1,32	2.25 3.00	3.89 3.89	1.20 1.22	1.26 1.26	83 63	50 50	58 53
4478 B5 RRH	18.1	13,4	8.3	1,68	1.04	1,35	2.19	1.20	1.20	61	37	43
4478 B5 RRH (Shielded)	18.1	10.1	8.3	1,26	1.04	1,80	2.19	1,20	1.20	46	37	40
4426 B66 RRH 4426 B66 RRH (Shielded)	15.0 15.0	13.2 2.2	7.4 7.4	1.38 0.23	0.77 0.77	1.14 6.82	2.03 2.03	1.20 1.39	1,20 1,20	50 10	28 28	33 23
LGP21401 TMA	14.4	9.0	2.7	0.90	0.27	1,60	5;33	1.20	1,33	32	11	16
WIND LOADS WITH ICE:												
7770 Antenna	59.6	15,6	9.6	6.44	3.95	3.83	6.23	1.26	1,37	65	43	49
HPA-65R-BUU-H6 Antenna	76.6	19.4	13.6	10.29	7.21	3.95	5,65	1.26	1.34	104	77	84
Q\$66512-2 Antenna	76.6	16.6	14.2	8.80	7,53	4.62	5,41	1.29	1,33	91	80	83
800-10965 Antenna	83.3	24.6	11.5	14.20	6.63	3,39	7.27	1.24	1,41	141	75	91
RRUS-11 RRH RRUS-11 RRH (Shielded)	24.3 24.3	21.6 16.2	11.8 11.8	3.63 2.72	1.98 1.98	1.13 1.50	2.06 2.06	1.20 1.20	1.20 1.20	35 26	19 19	23 21
RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded)	25.0 25.0	23.1 17.3	15,5 15,5	4.00 3.00	2.68 2.68	1.08 1.44	1,61 1,61	1.20 1.20	1.20 1.20	38 29	26 26	29 27
RRUS-32 RRH RRUS-32 RRH (Shielded)	31,8 31.8	16.7 12.5	11.6 11.6	3.67 2.76	2,55 2.55	1,91 2.54	2.75 2.75	1.20 1.20	1.21 1.21	35 27	25 25	27 25
1478 B5 RRH 1478 B5 RRH (Shielded)	22.7 22.7	18.0 13.5	12.8 12.8	2.83 2.12	2.02	1,26 1,68	1.77 1.77	1.20 1.20	1.20 1.20	27 20	19 19	21 20
1426 B66 RRH 1426 B66 RRH (Shielded)	19.6 19.6	17.8 6.8	12,0 12,0	2.41 0.92	1.62 1.62	1.10 2.89	1,64 1,64	1.20 1.22	1,20 1,20	23 9	16 16	18 14
GP21401 TMA	19.0	13.6	7.3	1.79	0.96	1.40	2.61	1.20	1,20	17	9	11
WIND LOADS AT 30 MPH:												
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1,31	1,53	16	8	10
IPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1,31	1,43	28	19	21
Q\$66512-2 Antenna	72.0	12,0	9.6	6.00	4.80	6,00	7,50	1,36	1.42	23	20	21
00-10965 Antenna	78.7	20.0	6.9	10,93	3.77	3,94	11.41	1.26	1,55	40	17	23
RUS-11 RRH RUS-11 RRH (Shielded)	19.7 19.7	17.0 12.8	7.2 7.2	2.33 1.74	0.99 0.99	1.16 1.55	2.74 2.74	1,20 1,20	1,21 1,21	8	3	5 4
RUS-12 + A2 RRH RUS-12 + A2 RRH (Shielded)	20.4 20.4	18.5 13.9	10.9 10.9	2.62 1.97	1.54 1.54	1,10 1,47	1.87 1.87	1.20 1.20	1,20 1,20	9	5	6
RUS-32 RRH RUS-32 RRH (Shielded)	27.2 27.2	12.1 9.1	7.0 7.0	2.29 1.71	1.32 1.32	2,25 3,00	3.89 3.89	1.20 1.22	1-26 1-26	8	5	6 5
478 B5 RRH 478 B5 RRH (Shielded)	18.1 18.1	13.4 10.1	8.3 8.3	1.68 1.26	1.04 1.04	1.35 1.80	2.19	1.20 1.20	1.20	6	4	4 4
426 B66 RRH 426 B66 RRH (Shielded)	15.0 15.0	13.2 2.2	7.4 7.4	1.38 0.23	0.77 0.77	1.14 6.82	2.03	1,20 1,39	1,20	5 1	3	3 2
-ro soo man (sulcinen)	15.0	2,2	7.4	0,23	0.77	0.02	2.03	1-39	1.20		- 8	- 2

Project Name: Plainville South Washington Street

Project Number: CT1029

Checked By: MSC



Angle = 90	(deg)		Ice Thick	ness =	2.28	ín.		1	Equival	ent Angle =	270	(deg)
WIND LOADS WITH NO ICE:												
Appurtenances	Height	Width	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
7770 Antenna	55.0	11.0	5.0	4.20	1,91	5.00	11.00	1,31	1,53	166	88	88
HPA-65R-BUU-H6 Antenna	72.0	14,8	9.0	7.40	4,50	4.86	B.00	1,31	1,43	291	194	194
QS66512-2 Antenna	72.0	12,0	9.6	6,00	4.80	6,00	7,50	1,36	1,42	245	205	205
800-10965 Antenna	78.7	20.0	6.9	10,93	3.77	3,94	11,41	1,26	1,55	416	176	176
RRUS-11 RRH	19,7	17.0	7.2	2.33	0,99	1,16	2.74	1.20	1,21	84	36	36
RRUS-11 RRH (Shielded)	19.7	6.0	7.2	0,82	0,99	3,28	2,74	1,23	1,21	30	36	36
RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded)	20,4 20.4	18.5 7.5	10.9 10.9	2,62 1,06	1,54 1,54	1.10 2.72	1.87 1.87	1,20 1,21	1,20 1,20	95 39	56 56	56 56
RRUS-32 RRH RRUS-32 RRH (Shielded)	27,2 27,2	12.1 1,1	7,0 7,0	2.29 0.21	1,32 1,32	2.25 24.73	3,89 3,89	1,20 1,99	1 26 1 26	83 12	50 50	50 50
4478 B5 RRH 4478 B5 RRH (Shielded)	18,1 18,1	13.4 2.4	8,3 8,3	1,68 0,30	1,04 1,04	1.35 7.54	2,19 2,19	1,20 1,42	1,20 1,20	61 13	37 37	37 37
4426 B66 RRH	15,0	13.2	7.4	1.38	0.77	1.14	2,03	1.20	1,20	50	28	28
4426 B66 RRH (Shielded)	15,0	2.2	7.4	0,23	0.77	6.82	2,03	1,39	1,20	10	28	28
LGP21401 TMA	14,4	9.0	2.7	0,90	0,27	1,60	5,33	1,20	1,33	32	11	11
WIND LOADS WITH ICE:												
7770 Antenna	59.6	15.6	9.6	6.44	3.95	3,83	6,23	1.26	1,37	65	43	43
HPA-65R-BUU-H6 Antenna	76,6	19.4	13,6	10,29	7.21	3,95	5,65	1,26	1,34	104	77	77
QS66512-2 Antenna	76,6	16,6	14.2	8.80	7.53	4,62	5,41	1.29	1,33	91	80	80
800-10965 Antenna	83.3	24.6	11.5	14.20	6.63	3,39	7,27	1.24	1,41	141	75	75
RRUS-11 RRH RRUS-11 RRH (Shielded)	24.3 24.3	21.6 10.6	11.8 11.8	3.63 1.78	1.98 1.98	1.13 2.30	2.06	1.20 1.20	1,20 1,20	35 17	19 19	19 19
RRUS-12 + A2 RRH	25.0	23.1	15,5	4.00	2,68	1,08	1,61	1,20	1.20	38	26	26
RRUS-12 + A2 RRH (Shielded)	25.0	12.1	15.5	2.09	2,68	2,07	1,61	1,20	1,20	20	26	26
RRUS-32 RRH RRUS-32 RRH (Shielded)	31.8 31.8	16.7 5.7	11.6 11.6	3.67 1.25	2.55 2.55	1.91 5.61	2,75 2,75	1.20 1.34	1.21 1.21	35 13	25 25	25 25
4478 B5 RRH 4478 B5 RRH (Shielded)	22,7 22,7	18.0 7.0	12,8 12,8	2,83 1,09	2.02	1,26 3,26	1,77 1,77	1,20 1,23	1,20 1,20	27 11	19 19	19 19
4426 B66 RRH 4426 B66 RRH (Shielded)	19.6 19.6	17.8 6.8	12.0 12.0	2,41 0,92	1.62 1.62	1,10 2,89	1,64 1,64	1.20 1.22	1,20 1.20	23 9	16 16	16 16
LGP21401 TMA	19,0	13.6	7.3	1,79	0.96	1,40	2.61	1,20	1.20	17	9	9
WIND LOADS AT 30 MPH:												
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11,00	1,31	1,53	16	8	8
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1,31	1,43	28	19	19
QS66512-2 Antenna	72.0	12.0	9.6	6.00	4.80	6,00	7,50	1,36	1,42	23	20	20
600-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3,94	11.41	1,26	1,55	40	17	17
RRUS-11 RRH	19.7	17.0	7.2	2.33	0.99	1,16	2.74	1,20	1,21	8	3	3
RRUS-11 RRH (Shielded)	19.7	6.0	7.2	0.82	0.99	3,28	2.74	1,23	1,21	3	3	3
RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded)	20.4 20.4	18.5 7.5	10.9 10.9	2.62 1.06	1.54 1.54	1.10 2.72	1.87 1.87	1.20 1.21	1,20 1,20	4	5	5 5
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 1.1	7.0 7.0	2.29 0.21	1,32 1,32	2.25 24.73	3.89 3.89	1,20 1,99	1,26 1,26	8 1	5 5	5 5
1478 B5 RRH 1478 B5 RRH (Shielded)	18.1 18.1	13.4 2.4	8,3 8.3	1.68 0.30	1.04	1,35 7,54	2.19 2.19	1,20 1,42	1.20 1.20	6 1	4	4
1426 B66 RRH	15.0	13.2	7.4	1,38	0.77	1,14	2.03	1,20	1,20	5	9	3
1426 B66 RRH (Shielded)	15.0	2.2	7.4	0.23	0.77	6.82	2,03	1,39	1,20	1	3	3

Project Name: Plainville South Washington Street

Project Number: CT1029
Designed By: LN Checked By: MSC



HPA-65R-BUU-H6 Antenna QS66512-2 Antenna 800-10965 Antenna RRUS-11 RRH RRUS-11 RRH (Shielded) RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded) RRUS-32 RRH RRUS-32 RRH RRUS-32 RRH 4478 B5 RRH 4478 B5 RRH 4478 B5 RRH 446 B66 RRH 4426 B66 RRH	Height 55.0 72.0 72.0 78.7 19.7 19.7 20.4 20.4 27.2 27.2 18.1 15.0 14.4	Width 11.0 14.8 12.0 20.0 17.0 12.8 18.5 13.9 12.1 9.1 13.4 10.1 13.2 2.2 9.0	Depth 5,0 9,0 9,6 6,9 7.2 7.2 10.9 7.0 8.3 8.3 7.4 7.4	Flat Area (normal) 4.20 7.40 6.00 10.93 2.33 1.74 2.62 1.97 2.29 1.71 1.68 1.26 1.38	Flat Area (side) 1.91 4.50 4.80 3.77 0.99 0.99 1.54 1.54 1.32 1.92 1.04 1.04	Ratio (normal) 5,00 4,86 6,00 3,94 1,16 1,55 1,10 1,47 2,25 3,00 1,35	Ratio (side) 11,00 8,00 7.50 11,41 2,74 2,74 1,87 1,87 3,89 3,89	Ca (normal) 1,31 1,31 1,36 1,26 1,20 1,20 1,20 1,20 1,20 1,20 1,22	Ca [side] 1,53 1,43 1,42 1,55 1,21 1,20 1,20 1,26 1,26	Force (lbs) 166 291 245 416 84 63 95 71 83 63	Force (lbs) 88 194 205 176 36 36 56 50 50	Force (lbs) 108 218 215 236 48 43 65 60 58 53
7770 Antenna HPA-65R-BUU-H6 Antenna Q566512-2 Antenna 800-10965 Antenna RRUS-11 RRH RRUS-11 RRH (Shielded) RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded) RRUS-32 RRH RRUS-32 RRH RRUS-32 RRH 478 B5 RRH 4478 B5 RRH	55.0 72.0 72.0 78.7 19.7 19.7 20.4 20.4 27.2 27.2 18.1 18.1 15.0	11.0 14.8 12.0 20.0 17.0 12.8 18.5 13.9 12.1 9.1 13.4 10.1 13.2 2.2	5,0 9,0 9,6 6,9 7,2 7,2 10,9 10,9 7,0 7,0 8,3 8,3	(normal) 4.20 7.40 6.00 10.93 2.33 1.74 2.62 1.97 2.29 1.71 1.68 1.26	(side) 1.91 4.50 4.80 3.77 0.99 0.99 1.54 1.54 1.32 1.32	(normal) 5,00 4,86 6.00 3.94 1.16 1.55 1.10 1.47 2,25 3,00	(side) 11,00 8,00 7.50 11,41 2,74 2,74 1,87 1,87 3,89	(normal) 1,31 1,31 1,36 1,26 1,20 1,20 1,20 1,20 1,20	(side) 1,53 1,43 1.42 1,55 1.21 1.21 1.20 1,26	(lbs) 166 291 245 416 84 63 95 71	(lbs) 88 194 205 176 36 36 56 50	(lbs) 108 218 215 236 48 43 65 60
HPA-65R-BUU-H6 Antenna	72.0 78.7 19.7 19.7 20.4 20.4 27.2 27.2 18.1 15.0	14.8 12.0 20.0 17.0 12.8 18.5 13.9 12.1 9.1 13.4 10.1	9,0 9,6 6,9 7,2 7,2 10,9 10,9 7,0 7,0 8,3 8,3	7.40 6.00 10.93 2.33 1.74 2.62 1.97 2.29 1.71 1.68 1.26	4.50 4.80 3.77 0.99 0.99 1.54 1.54 1.32 1.04	4,86 6,00 3,94 1,16 1,55 1,10 1,47 2,25 3,00	8,00 7.50 11,41 2,74 2,74 1,87 1,87	1,31 1,36 1,26 1,20 1,20 1,20 1,20	1,43 1.42 1,55 1.21 1.21 1.20 1.20	291 245 416 84 63 95 71	194 205 176 36 36 56 56	218 215 236 48 43 65 60
Q566512-Z Antenna 800-10965 Antenna RRUS-11 RRH RRUS-11 RRH (Shielded) RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded) RRUS-32 RRH RRUS-32 RRH RRUS-32 RRH 4478 B5 RRH 4478 B5 RRH 4478 B5 RRH 44626 B66 RRH 4426 B66 RRH 4426 B66 RRH 4426 B66 RRH 4418 B5 RRH 4421 B5 RRH 4422 B66 RRH	72.0 78.7 19.7 19.7 20.4 20.4 27.2 27.2 18.1 18.1 15.0	12.0 20.0 17.0 12.8 18.5 13.9 12.1 9.1 13.4 10.1	9.6 6.9 7.2 7.2 10.9 10.9 7.0 7.0 8.3 8.3	6.00 10.93 2.33 1.74 2.62 1.97 2.29 1.71 1.68 1.26	4.80 3.77 0.99 0.99 1.54 1.54 1.32 1.32	6.00 3.94 1.16 1.55 1.10 1.47 2.25 3.00	7.50 11.41 2.74 2.74 1.87 1.87	1,36 1,26 1,20 1,20 1,20 1,20	1.42 1,55 1,21 1,21 1,20 1,20	245 416 84 63 95 71	205 176 36 36 56 56 56	215 236 48 43 65 60
800-10965 Antenna RRUS-11 RRH RRUS-11 RRH (Shielded) RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded) RRUS-32 RRH RRUS-32 RRH RRUS-32 RRH 4478 B5 RRH 4478 B5 RRH 4478 B5 RRH (Shielded) 4426 B66 RRH 4426 B66 RRH 4426 B66 RRH	78.7 19.7 19.7 20.4 20.4 27.2 27.2 18.1 18.1 15.0	20.0 17.0 12.8 18.5 13.9 12.1 9.1 13.4 10.1	7.2 7.2 10.9 10.9 7.0 7.0 8.3 8.3	10.93 2.33 1.74 2.62 1.97 2.29 1.71 1.68 1.26	3.77 0.99 0.99 1,54 1,54 1.32 1.32	6.00 3.94 1.16 1.55 1.10 1.47 2.25 3.00	7.50 11.41 2.74 2.74 1.87 1.87	1,36 1,26 1,20 1,20 1,20 1,20	1,55 1,21 1,21 1,20 1,20	416 84 63 95 71	176 36 36 56 56	236 48 43 65 60
800-10965 Antenna RRUS-11 RRH RRUS-11 RRH (Shielded) RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded) RRUS-32 RRH RRUS-32 RRH RRUS-32 RRH 4478 B5 RRH 4478 B5 RRH 4478 B5 RRH (Shielded) 4426 B66 RRH 4426 B66 RRH 4426 B66 RRH	78.7 19.7 19.7 20.4 20.4 27.2 27.2 18.1 18.1 15.0	20.0 17.0 12.8 18.5 13.9 12.1 9.1 13.4 10.1	7.2 7.2 10.9 10.9 7.0 7.0 8.3 8.3	10.93 2.33 1.74 2.62 1.97 2.29 1.71 1.68 1.26	3.77 0.99 0.99 1,54 1,54 1.32 1.32	3.94 1.16 1.55 1.10 1.47 2.25 3.00	11,41 2,74 2,74 1,87 1,87	1,20 1,20 1,20 1,20 1,20 1,20	1,55 1,21 1,21 1,20 1,20	416 84 63 95 71	176 36 36 56 56	236 48 43 65 60
RRUS-11 RRH RRUS-12 + A2 RRH RRUS-12 + A2 RRH RRUS-32 RRH RRUS-32 RRH RRUS-32 RRH 4478 B5 RRH 4486 B66 RRH 4426 B66 RRH 4426 B66 RRH 4426 B66 RRH	19.7 19.7 20.4 20.4 27.2 27.2 18.1 15.0 15.0	17.0 12.8 18.5 13.9 12.1 9.1 13.4 10.1 13.2 2.2	7.2 7.2 10.9 10.9 7.0 7.0 8.3 8.3 7.4	2.33 1.74 2.62 1.97 2.29 1.71 1.68 1.26	0.99 0.99 1,54 1,54 1,54 2.32 1.32	1,16 1,55 1,10 1,47 2,25 3,00	2,74 2,74 1,87 1,87 3,89	1,20 1,20 1,20 1,20	1,21 1,21 1,20 1,20	84 63 95 71	36 36 56 56 56	48 43 65 60 58
RRUS-11 RRH (Shielded) RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded) RRUS-32 RRH (Shielded) 4478 B5 RRH 4478 B5 RRH (Shielded) 4426 B66 RRH 4426 B66 RRH 4426 B66 RRH	19.7 20.4 20.4 27.2 27.2 18.1 18.1 15.0 15.0	12.8 18.5 13.9 12.1 9.1 13.4 10.1 13.2 2.2	7.2 10.9 10.9 7.0 7.0 8.3 8.3 7.4	1.74 2.62 1.97 2.29 1.71 1.68 1.26	0.99 1,54 1,54 1.32 1.32	1.55 1.10 1.47 2.25 3.00	2,74 1,87 1,87 3,89	1.20 1.20 1.20	1,21 1,20 1,20	63 95 71 83	36 56 56 50	43 65 60 58
RRUS-12 + A2 RRH (Shielded) RRUS-32 RRH RRUS-32 RRH (Shielded) 4478 B5 RRH 4478 B5 RRH (Shielded) 4426 B66 RRH 4426 B66 RRH 4426 B66 RRH 4426 B66 RRH	20.4 27.2 27.2 18.1 18.1 15.0 15.0	13.9 12.1 9.1 13.4 10.1 13.2 2.2	7.0 7.0 7.0 8.3 8.3	1.97 2.29 1.71 1.68 1.26	1,54 1.32 1.32 1.04	1,47 2,25 3,00	1,87 3,89	1,20	1,20 1,26	71 83	56 50	60 58
RRUS-32 RRH RRUS-32 RRH (Shielded) 4478 B5 RRH 4478 B5 RRH (Shielded) 4426 B66 RRH 4426 B66 RRH (Shielded)	27.2 27.2 18.1 18.1 15.0 15.0	12.1 9.1 13.4 10.1 13.2 2.2	7.0 7.0 8.3 8.3	2.29 1.71 1.68 1.26	1.32 1.32 1.04	2,25 3,00	3,89	1,20	1,26	83	50	58
RRUS-32 RRH (Shielded) 4478 BS RRH 4478 BS RRH (Shielded) 4426 B66 RRH 4426 B66 RRH (Shielded) LGP21401 TMA	27.2 18.1 18.1 15.0 15.0	9.1 13.4 10.1 13.2 2.2	7.0 8.3 8.3 7.4	1.71 1.68 1.26	1.32	3,00						
4478 B5 RRH (Shleided) 4426 B66 RRH 4426 B66 RRH (Shleided) LGP21401 TMA	18.1 15.0 15.0	10.1 13.2 2.2	8.3 7.4	1.26		1,35						
4426 B66 RRH 4426 B66 RRH (Shleided) LGP21401 TMA	15.0 15.0	13.2	7.4		1.04		2,19	1.20	1.20	61	37	43
4426 B66 RRH (Shielded)	15.0	2.2		1.38		1,80	2 19	1,20	1.20	46	37	40
LGP21401 TMA				0.23	0.77 0.77	1,14 6,82	2,03	1,20 1,39	1,20 1,20	50 10	28 28	33 23
			2.7	0.90	0.27	1,60	5,33	1,20	1,33	32	11	16
						307	9856	00	721			
7770 Antenna	59.6	15.6	9,6	6.44	3.95	3,83	6.23	1.26	1,37	65	43	49
								1,26				
	76.6	19.4	13.6	10.29	7.21	3,95	5,65	1.26	1,34	104	77	84
QS66512-2 Antenna	76.6	16.6	14.2	8.80	7.53	4.62	5.41	1.29	1.33	91	80	83
800-10965 Antenna	83,3	24.6	11.5	14.20	6.63	3,39	7.27	1,24	1,41	141	75	91
RRUS-11 RRH RRUS-11 RRH (Shielded)	24.3 24.3	21.6 16.2	11.8 11.8	3.63 2.72	1.98 1.98	1,13 1,50	2.06 2.06	1.20 1.20	1,20 1,20	35 26	19 19	23 21
RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded)	25.0 25.0	23.1 17.3	15.5 15.5	4.00 3.00	2.68 2.68	1.08	1.61 1.61	1.20 1.20	1.20 1.20	38 29	26 26	29 27
RRUS-32 RRH	31.8	16.7	11.6	3.67	2,55	1,91	2,75	1,20	1,21	35	25	27
RRUS-32 RRH (Shielded)	31.8	12.5	11.6	2.76	2,55	2.54	2.75	1.20	1,21	27	25	25
1478 B5 RRH 1478 B5 RRH (Shielded)	22.7 22.7	18.0 13.5	12.8 12.8	2.83 2.12	2,02 2.02	1.26 1.68	1.77 1.77	1,20 1,20	1,20 1.20	27 20	19 19	21 20
1426 B66 RRH	19.6	17.8	12.0	2.41	1.62	1.10	1,64	1,20	1.20	23	16	18
4426 B66 RRH (Shielded)	19.6	6.8	12,0	0.92	1,62	2.89	1,64	1,22	1,20	9	16	14
.GP21401 TMA	19.0	13.6	7.3	1.79	0.96	1.40	2.61	1.20	1.20	17	9	11
WIND LOADS AT 30 MPH:												
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11,00	1,31	1,53	16	8	10
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7,40	4.50	4.86	8.00	1.31	1,43	28	19	21
QS66512-2 Antenna	72.0	12.0	9.6	6.00	4.80	6.00	7.50	1,36	1,42	23	20	21
00-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1,55	40	17	23
RRUS-11 RRH	19.7	17.0	7.2	2,33	0.99	1.16	2.74	1,20	1,21	8	3	5
RRUS-11 RRH (Shlelded)	19.7	12.8	7.2	1.74	0.99	1.55	2,74	1,20	1.21	6	3	4
RRUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded)	20.4 20.4	18.5 13.9	10.9 10.9	2,62 1,97	1,54 1,54	1,10 1,47	1.87 1.87	1,20 1,20	1,20 1,20	9 7	5	6
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 9.1	7.0 7.0	2.29 1.71	1.32 1.32	2,25 3,00	3.89 3.89	1,20 1,22	1.26 1,26	8	5	6 5
478 B5 RRH 478 B5 RRH (Shielded)	18.1 18.1	13.4 10.1	8.3 8.3	1.68 1.26	1.04 1.04	1,35 1,80	2.19 2.19	1,20 1,20	1,20 1,20	6	4	4
426 B66 RRH	15.0	13.2	7.4	1.38	0.77	1.14	2,03	1.20	1.20	5	3	3
426 866 RRH (Shielded)	15.0	2.2	7.4	0.23	0.77	6.82	2,03	1.39	1,20	1	3	2

Project Name: Plainville South Washington Street

Project Number: CT1029
Designed By: IN Checked By: MSC



Angle = 150	(deg)		tce Thick	ness =	2.28	in,		ı	Eguivale	ent Angle =	330	(deg)
	101				_,55				- quiran	and a		(40.01
WIND LOADS WITH NO ICE:												
Appurtenances	<u>Height</u>	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	<u>Ca</u> (side)	Force (lbs)	Force (lbs)	Force (lbs)
7770 Antenna	55.0	11.0	5.0	4,20	1,91	5,00	11,00	1,31	1,53	166	88	146
HPA-65R-BUU-H6 Antenna	72,0	14,8	9.0	7.40	4.50	4,86	8.00	1,31	1,43	291	194	266
QS66512-2 Antenna	72.0	12.0	9.6	6.00	4.80	6.00	7,50	1,36	1,42	245	205	235
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3,94	11,41	1,26	1,55	416	176	356
RRUS-11 RRH RRUS-11 RRH (Shielded)	19.7 19.7	17.0 8.5	7,2 7,2	2,33 1,16	0,99 0.99	1,16 2,32	2,74 2,74	1.20 1.20	1.21 1,21	84 42	36 36	72 40
RRUS-12 + A2 RRH	20.4	18.5	10,9	2,62	1,54	1.10	1,87	1.20	1.20	95	56	85
RRUS-12 + A2 RRH (Shielded)	20,4	9.3	10,9	1,31	1,54	2,21	1,87	1,20	1.20	47	56	49
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 6.1	7.0 7.0	2,29 1,14	1.32 1.32	2,25 4,50	3,89 3,89	1.20 1.29	1.26 1,26	83 44	50 50	74 46
1478 B5 RRH	18,1	13.4	8,3	1.68	1.04	1,35	2,19	1.20	1.20	61	37	55
1478 B5 RRH (Shielded)	18.1	6.7	8,3	0.84	1.04	2,70	2.19	1,21	1,20	31	37	32
1426 B66 RRH 1426 B66 RRH (Shielded)	15.0 15.0	13.2 2.2	7,4 7,4	1,38 0.23	0.77 0.77	1,14 6,82	2.03 2.03	1,20 1,39	1,20 1,20	50 10	28 28	44 14
.GP21401 TMA	14.4	9.0	2.7	0.90	0.27	1,60	5.33	1,20	1,33	32	11	27
WIND LOADS WITH ICE:												
7770 Antenna	59.6	15.6	9.6	6.44	3.95	3,83	6.23	1,26	1,37	65	43	60
HPA-65R-BUU-H6 Antenna	76.6	19.4	13,6	10.29	7.21	3,95	5.65	1,26	1,34	104	77	98
QS66512-2 Antenna	76.6	16.6	14.2	8.80	7.53	4.62	5.41	1,29	1,33	91	60	89
100-10965 Antenna	83.3	24.6	11.5	14.20	6.63	3,39	7.27	1,24	1,41	141	75	125
RRUS-11 RRH RRUS-11 RRH (Shielded)	24.3 24.3	21.6 10.8	11.8 11.8	3,63 1,82	1.98 1.98	1,13 2,25	2.06 2.06	1,20 1,20	1.20 1.20	35 17	19 19	31 18
RUS-12 + A2 RRH RRUS-12 + A2 RRH (Shielded)	25.0 25.0	23.1 11.5	15.5 15.5	4.00 2.00	2.68 2.68	1.08 2.16	1.61 1.61	1.20 1.20	1.20 1.20	38 19	26 26	35 21
RUS-32 RRH	31.8	16.7	11.6	3.67	2.55	1,91	2,75	1.20	1,21	35	25	33
IRUS-32 RRH (Shielded)	31.8	8.3	11.6	1.84	2.55	3,81	2,75	1,26	1,21	19	25	20
478 B5 RRH 478 B5 RRH (Shielded)	22.7 22.7	18.0 9.0	12.8 12.8	2.83 1.41	2.02 2.02	1.26 2.52	1.77 1.77	1.20 1.20	1.20 1.20	27 14	19 19	25 15
426 B66 RRH 426 B66 RRH (Shielded)	19.6 19.6	17.8 6.8	12.0 12.0	2.41 0.92	1.62 1.62	1,10 2,89	1.64 1.64	1.20 1.22	1,20 1,20	23 9	16 16	21 11
GP21401 TMA	19.0	13.6	7.3	1.79	0.96	1,40	2,61	1.20	1,20	17	9	15
VIND LOADS AT 30 MPH:												
770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1,53	16	8	14
PA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8,00	1.31	1,43	28	19	26
S66512-2 Antenna	72.0	12.0	9.6	6.00	4.80	6.00	7.50	1.36	1.42	23	20	23
00-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	40	17	34
RUS-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21	8	3	7
RUS-11 RRH (Shielded)	19.7	8.5	7.2	1.16	0.99	2,32	2.74	1.20	1.21	4	3	4
RUS-12 + A2 RRH RUS-12 + A2 RRH (Shielded)	20.4 20.4	18.5 9.3	10.9 10.9	2.62 1.31	1.54 1.54	1-10 2-21	1.87 1.87	1.20 1.20	1.20	9 5	5	8 5
RUS-32 RRH RUS-32 RRH (Shielded)	27.2 27.2	12.1 6.1	7.0 7.0	2.29 1.14	1.32 1.32	2.25 4.50	3.89 3.89	1.20 1.29	1.26 1.26	8 4	5	7
478 B5 RRH 478 B5 RRH (Shielded)	18,1 18,1	13.4 6.7	8.3 8.3	1.68 0.84	1.04 1.04	1,35 2,70	2.19 2.19	1,20 1,21	1.20 1.20	6	4	5 3
426 B66 RRH 426 B66 RRH (Shielded)	15.0 15.0	13.2 2.2	7.4 7.4	1.38 0.23	0.77 0.77	1.14 6.82	2.03 2.03	1.20 1.39	1.20 1.20	5 1	3	4
SP21401 TMA	14.4	9.0	2.7	0.90	0.27	1.60	5,33	1,20	1.33	3	1	3

Project Name: Plainville South Washington Street

Project Number: CT1029

Designed By: LN Checked By: MSC



ICE WEIGHT CALCULATIONS

Thickness of ice (in): 1.00
* Density of ice used = 56 PCF

77	70	Δn	tei	nna

Weight of ice based on total radial SF area:
Height (in): 55.0
Width (in): 11.0
Depth (in): 5.0

Total weight of ice on object: 61 lbs
Weight of object: 35 lbs
Combined weight of ice and object: 96 lbs

QS66512-2 Antenna

Weight of ice based on total radial SF area:
Height (in): 72.0
Width (in): 12.0
Depth (in): 9.6
Total weight of ice on object: 108 lbs
Weight of object: 111 lbs

Combined weight of ice and object: 219 lbs

RUUS-12 + A2 RRH

Weight of ice based on total radial SF area:
Height (in): 20.4
Width (in): 18.5
Depth (in): 10.9

Total weight of ice on object: 52 lbs
Weight of object: 80 lbs
Combined weight of ice and object: 132 lbs

RRUS-11 RRH

Weight of ice based on total radial SF area:
Height (in): 19.7
Width (in): 17.0
Depth (in): 7.2
Total weight of ice on object: 39 lbs
Weight of object: 51 lbs

Combined weight of ice and object: 90 lbs

4426 B66

Weight of ice based on total radial SF area:
Height (in): 15.0
Width (in): 13.2
Depth (in): 7.4
Total weight of ice on object: 26 lbs
Weight of object: 49 lbs

Combined weight of ice and object: 75 lbs

Squid Surge Arrestor

Weight of ice based on total radial SF area:

Combined weight of ice and object:

 Height (in):
 24.0

 Width (in):
 9.7

 Depth (in):
 9.7

 Total weight of ice on object:
 36 lbs

 Weight of object:
 33 lbs

2" pipe

Per foot weight of ice:
diameter (in):
2.4

Per foot weight of ice on object: 3 lbs/ft

HPA-65R-BUU-H6 Antenna

Weight of ice based on total radial SF area:
Height (in): 72.0
Width (in): 14.8
Depth (in): 9.0
Total weight of ice on object:

Total weight of ice on object: 120 lbs
Weight of object: 51 lbs

Combined weight of ice and object: 171 lbs

800-10965 Antenna

Weight of ice based on total radial SF area:
Height (in): 78.7
Width (in): 20.0
Depth (in): 6.9
Total weight of ice on object: 109 lbs

Combined weight of ice and object: 255 lbs

RRUS-32 RRH

Weight of ice based on total radial SF area:
Height (in): 27.2
Width (in): 12.1
Depth (in): 7.0
Total weight of ice on object: 39 lbs
Weight of object: 60 lbs

Combined weight of ice and object: 99 lbs

4478 B5 RRH's

Weight of ice based on total radial SF area:
Height (in): 18.1
Width (in): 13.4
Depth (in): 8.3
Total weight of ice on object: 33 lbs
Weight of object: 60 lbs
Combined weight of ice and object: 93 lbs

LGP21401 TMA

Weight of ice based on total radial SF area:
Height (in): 14.4
Width (in): 9.0
Depth (in): 2.7
Total weight of ice on object: 13 lbs
Weight of object: 19 lbs
Combined weight of ice and object: 32 lbs

4x4x1/4 HSS

Weight of ice based on total radial SF area:

Depth (in):
4
height (in):
12
Width (in):
4
Per foot weight of ice on object:
6 lbs/ft

L 3x3x3/8

69 lbs

Weight of ice based on total radial SF area:
Depth (in):
3
height (in):
12

Width (in): 3

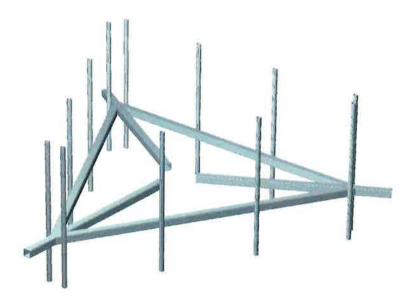
Per foot weight of ice on object: 5 lbs/ft



Mount Calculations (Existing Conditions)



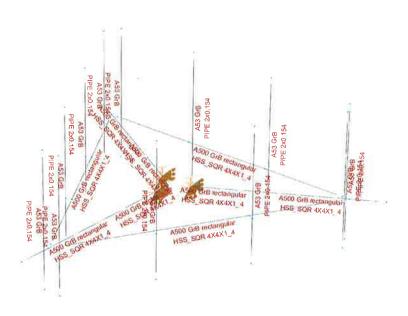
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Units system: English
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Current Date: 6/20/2018 3:27 PM
Units system: English
File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1029\LTE 4C-5C\CT1029 (LTE 4C-5C).etz\





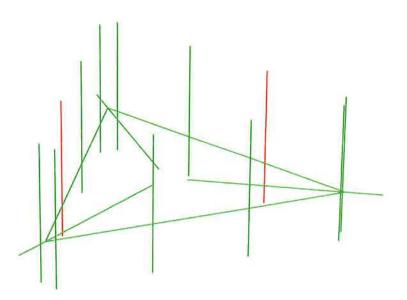


Current Date: 6/20/2018 3:27 PM

Units system: English
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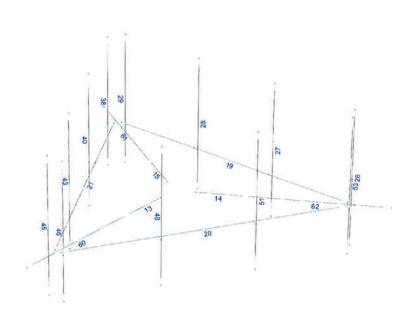








Current Date: 6/20/2018 3:27 PM
Units system: English
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Current Date: 6/20/2018 3:27 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1029\LTE 4C-5C\CT1029 (LTE

4C-5C).etz\

Load data

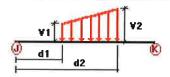
GLOSSARY

Comb Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
DL	Dead Load		DL
W0	Wind Load 0/60/120 deg	No	WIND
W30	Wind Load 30/90/150 deg	No	WIND
Di	Ice Load	No	LL
Wi0	Ice Wind Load 0/60/120 deg	No	WIND
Wi30	Ice Wind Load 30/90/150 deg	No	WIND
WL0	WL 30 mph 0/60/120 deg	No	WIND
WL30	WL 30 mph 30/90/150 deg	No	WIND
LL1	250 lb Live Load Center of Mount	No	LL
LL2	250 lb Live Load End of Mount	No	LL
LLa1	500 lb Live Load on Antenna 1	No	LL
LLa2	500 lb Live Load on Antenna 2	No	LL
LLa3	500 lb Live Load on Antenna 3	No	LL
LLa4	500 lb Live Load on Antenna 4	No	LL
W180	-W0	Yes	
W210	-W30	Yes	
Wi180	-Wi0	Yes	
Wi210	-Wi30	Yes	
WL180	-WL0	Yes	
WL210	-WL30	Yes	

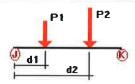
Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
DL	19	у	-0.01	0.00	0.00	No	0.00	No
	20	у	-0.01	0.00	0.00	No	0.00	No
	21	у	-0.01	0.00	0.00	No	0.00	No
W0	13	Z	-0.012	0.00	0.00	No	0.00	No
	14	Z	-0.012	0.00	0.00	No	0.00	No
	19	Z	-0.012	0.00	0.00	No	0.00	No
	20	Z	-0.012	0.00	0.00	No	0.00	No
	21	Z	-0.012	0.00	0.00	No	0.00	No

	60	Z	-0.012	0.00	0.00	No	0.00	No
	62	z	-0.012	0.00	0.00	No	0.00	No
W30	13	x	-0.012	0.00	0.00	No	0.00	No
	14	x	-0.012	0.00	0.00	No	0.00	No
6	15	x	-0.012	0.00	0.00	No	0.00	No
	19	x	-0.012	0.00	0.00	No	0.00	No
	21	x	-0.012	0.00	0.00	No	0.00	No
	46	x	-0.004	0.00	0.00	No	0.00	No
	48	x	-0.004	0.00	0.00	No	0.00	No
	51	×	-0.004	0.00	0.00	No	0.00	No
	60	×	-0.012	0.00	0.00	No	0.00	No
	61	x	-0.012	0.00	0.00	No	0.00	No
	62	x	-0.012	0.00	0.00	No	0.00	No
	53	x	-0.004	0.00	0.00	No	0.00	No
Di	43	У	-0.003	0.00	0.00	No	0.00	No
	27	У	-0.003	0.00	0.00	No	0.00	No
	13	У	-0.006	0.00	0.00	No	0.00	No
	14	У	-0.006	0.00	0.00	No	0.00	No
	15	У	-0.006	0.00	0.00	No	0.00	No
	19	У	-0.006	0.00	0.00	No	0.00	No
	20	У	-0.006	0.00	0.00	No	0.00	No
	21	У	-0.006	0.00	0.00	No	0.00	No
	26	У	-0.003	0.00	0.00	No	0.00	No
	29	У	-0.003	0.00	0.00	No	0.00	No
	38	У	-0.003	0.00	0.00	No	0.00	No
	40	У	-0.003	0.00	0.00	No	0.00	No
	45	У	-0.003	0.00	0.00	No	0.00	No
	28	У	-0.003	0.00	0.00	No	0.00	No
	46	У	-0.003	0.00	0.00	No	0.00	No
	48	У	-0.003	0.00	0.00	No	0.00	No
	51	У	-0.003	0.00	0.00	No	0.00	No
	60	У	-0.006	0.00	0.00	No	0.00	No
	61	У	-0.006	0.00	0.00	No	0.00	No
	62	У	-0.006	0.00	0.00	No	0.00	No
	53	у	-0.003	0.00	0.00	No	0.00	No
							400200000000000000000000000000000000000	

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
DL	43	 у	-0.055	5.53	No
		у	-0.055	0.47	No
		y	-0.06	3.00	No
		у	-0.049	5.80	No
	27	y	-0.055	5.53	No
		y	-0.055	0.47	No
		y	-0.06	3.00	No
		у	-0.049	5.80	No
	13	у	-0.033	1.00	No
	14	V	-0.033	1.00	No

15	У	-0.033	1.00	No
26	у	-0.056	5.25	No
	у	-0.056	0.75	No
	У	-0.06	3.00	No
	у	-0.06	5.80	No
29	У	-0.018	4.54	No
	y	-0.018	1.46	No
	у	-0.038	3.00	No
38	у	-0.018	4.54	No
	ý	-0.018	1.46	No
	ý	-0.038	3.00	No
40	ý	-0.056	5.25	No
	ý	-0.056	0.75	No
	ý	-0.06	3.00	No
	y	-0.06	5.80	No
45	у	-0.026	5.25	No
,,	y	-0.026	0.75	No
	у	-0.08	3.00	No
		-0.051	5.80	No
28	y y	-0.026	5.25	No
20				
	У	-0.026	0.75 3.00	No
	У	-0.08		No
46	y	-0.051	5.80	No
40	у	-0.056	5.25	No
	У	-0.056	0.75	No
	у	-0.06	3.00	No
40	у	-0.06	5.80	No
48	у	-0.055	5.53	No
	у	-0.055	0.47	No
	y	-0.06	3.00	No
	у	-0.049	5.80	No
51	У	-0.026	5.25	No
	у	-0.026	0.75	No
	у	-0.08	3.00	No
	У	-0.051	5.80	No
53	У	-0.018	4.54	No
	У	-0.018	1.46	No
	У	-0.038	3.00	No
43	z	-0.118	5.53	No
	Z	-0.118	0.47	No
	Z	-0.04	3.00	No
	Z	-0.033	5.80	No
27	Z	-0.118	5.53	No
	Z	-0.118	0.47	No
	Z	-0.04	3.00	No
	z	-0.033	5.80	No
13	z	-0.034	1.00	No
14	z	-0.034	1.00	No
15	z	-0.034	1.00	No
26	Z	-0.108	5.25	No
	z	-0.108	0.75	No
	z	-0.053	3.00	No
	z	-0.058	5.80	No
29	z	-0.054	4.54	No
-	Z	-0.054	1.46	No
38	z	-0.054	4.54	No
	z	-0.054	1.46	No
40	z	-0.108	5.25	No
10	z	-0.108	0.75	No
	z	-0.053	3.00	No
	-	-0.000	5.00	INU

W0

		(44)	0.050	5.00	
		Z	-0.058	5.80	No
	45	Z	-0.11	5.25	No
		Z	-0.11	0.75	No
		Z	-0.048	5.80	No
		Z	-0.06	3.00	No
	28	Z	-0.11	5.25	No
		z	-0.11	0.75	No
		z	-0.048	5.80	No
		z	-0.06	3.00	No
	46		-0.123	5.25	No
	40	Z			
		Z	-0.123	0.75	No
		z	-0.012	3.00	No
		Z	-0.083	5.80	No
	48	Z	-0.208	5.53	No
		Z	-0.208	0.47	No
		Z	-0.013	3.00	No
		Z	-0.05	5.80	No
	51	Z	-0.146	5.25	No
		z	-0.146	0.75	No
		z	-0.039	3.00	No
		z	-0.084	5.80	No
	53	z	-0.083	4.54	No
	00				
14/20	40	Z	-0.083	1.46	No
W30	43	×	-0.178	5.53	No
		×	-0.178	0.47	No
		×	-0.032	3.00	No
		X	-0.044	5.80	No
	27	×	-0.178	5.53	No
		×	-0.178	0.47	No
		×	-0.032	3.00	No
		×	-0.044	5.80	No
	13	×	-0.034	1.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
			0.00		
	14	×		0.00	No
	14	×	-0.034	1.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
	15	×	-0.034	1.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
		x	0.00	0.00	No
	19	x	0.00	0.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
	20		0.00	0.00	
	20	X			No
		x	0.00	0.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
	21	×	0.00	0.00	No
		x	0.00	0.00	No
		×	0.00	0.00	No
		X	0.00	0.00	No
	26	×	-0.118	5.25	No
	-	×	-0.118	0.75	No
		×	-0.074	5.80	No
	20	×	-0.046	3.00	No
	29	×	-0.074	4.54	No

	1447	0.074	4.40	NI-
	×	-0.074	1.46	No
	×	0.00	0.00	No
20	×	0.00	0.00	No
38	×	-0.074	4.54	No
	×	-0.074	1.46	No
	x	0.00	0.00	No
40	×	0.00	0.00	No
40	×	-0.118	5.25	No
	×	-0.118	0.75	No
	×	-0.074	5.80	No
	×	-0.046	3.00	No
45	×	-0.134	5.25	No
	×	-0.134	0.75	No
	×	-0.049	3.00	No
	×	-0.072	5.80	No
28	×	-0.134	5.25	No
	×	-0.134	0.75	No
	x	-0.049	3.00	No
	×	-0.072	5.80	No
46	×	-0.103	5.25	No
	×	-0.103	0.75	No
	x	-0.05	5.80	No
	×	-0.05	3.00	No
48	×	-0.088	5.53	No
	x	-0.088	0.47	No
	×	-0.037	3.00	No
	×	-0.028	5.80	No
51	×	-0.098	5.25	No
	×	-0.098	0.75	No
	×	-0.056	3.00	No
	×	-0.036	5.80	No
60	×	0.00	0.00	No
	×	0.00	0.00	No
	×	0.00	0.00	No
	×	0.00	0.00	No
61	×	0.00	0.00	No
	×	0.00	0.00	No
	×	0.00	0.00	No
	x	0.00	0.00	No
62	×	0.00	0.00	No
	×	0.00	0.00	No
	×	0.00	0.00	No
	x	0.00	0.00	No
53	×	-0.045	4.54	No
	×	-0.045	1.46	No
	×	-0.022	3.00	No
	×	0.00	0.00	No
43	У	-0.073	5.53	No
	У	-0.073	0.47	No
	У	-0.033	3.00	No
	У	-0.026	5.80	No
27	y	-0.073	5.53	No
	у	-0.073	0.47	No
	y	-0.033	3.00	No
	y	-0.026	5.80	No
13	y	-0.036	1.00	No
14	y	-0.036	1.00	No
15	y	-0.036	1.00	No
26	y	-0.054	5.25	No
	y	-0.054	0.75	No
	7	-0.034	0.73	110

Di

		У	-0.039	3.00	No				
		ý	-0.039	5.80	No				
	29	У	-0.031	4.54	No				
		У	-0.031	1.46	No				
		У	-0.026	3.00	No				
	38	У	-0.031	4.54	No				
		У	-0.031	1.46	No				
		У	-0.026	3.00	No				
	40	У	-0.054	5.25	No				
		у	-0.054	0.75	No				
		У	-0.039	3.00	No				
		У	-0.039	5.80	No				
	45	y	-0.06	5.25	No				
		У	-0.06	0.75	No				
		У	-0.052	3.00	No				
		У	-0.039	5.80	No				
	28	У	-0.06	5.25	No				
		У	-0.06	0.75	No				
		У	-0.052	3.00	No				
		У	-0.039	5.80	No				
	46	У	-0.054	5.25	No				
		У	-0.054	0.75	No				
		y	-0.039	3.00	No				
		У	-0.039	5.80	No				
	48	y	-0.073	5.53	No				
		У	-0.073	0.47	No				
		y	-0.033	3.00	No				
		У	-0.026	5.80	No				
	51	У	-0.06	5.25	No				
		У	-0.06	0.75	No				
		У	-0.052	3.00	No				
		У	-0.039	5.80	No				
	53	У	-0.031	4.54	No				
		У	-0.031	1.46	No				
Wi0	43	У	-0.026	3.00	No				
VVIO	43	Z	-0.046	5.53	No				
		z	-0.046 -0.02	0.47	No				
		z z	-0.02	3.00 5.80	No No				
	27	z	-0.046	5.53	No No				
	21	z	-0.046	0.47	No				
		Z	-0.02	3.00	No				
		z	-0.014	5.80	No				
	13	z	-0.016	1.00	No				
		z	0.010	-0.078	FALSE	0.00	0.00	No	
	14	z	-0.016	1.00	No	0.00	0.00	110	
	15	z	-0.016	1.00	No				
	26	z	-0.042	5.25	No				
		z	-0.042	0.75	No				
		z	-0.025	3.00	No				
		z	-0.027	5.80	No				
	29	Z	-0.025	4.54	No				
		Z	-0.025	1.46	No				
	38	z	-0.025	4.54	No				
		z	-0.025	1.46	No				
	40	z	-0.042	5.25	No				
		z	-0.042	0.75	No				
		z	-0.025	3.00	No				
		z	-0.027	5.80	No				
	45	z	-0.043	5.25	No				

		Z	-0.043	0.75	No
		z	-0.027	3.00	No
		Z	-0.023	5.80	No
	28	Z	-0.043	5.25	No
		Z	-0.043	0.75	No
		z	-0.027	3.00	No
	46	z	-0.023	5.80	No
	40	z z	-0.048 -0.048	5.25 0.75	No No
		z	-0.012	3.00	No
		z	-0.083	5.80	No
	48	z	-0.072	5.53	No
		z	-0.072	0.47	No
		z	-0.012	3.00	No
		z	-0.023	5.80	No
	51	Z	-0.054	5.25	No
		Z	-0.054	0.75	No
		z	-0.02	3.00	No
		Z	-0.035	5.80	No
	53	Z	-0.034	4.54	No
		z	-0.034	1.46	No
Wi30	43	x	-0.063	5.53	No
		×	-0.063	0.47	No
		x	-0.015	3.00	No
	27	×	-0.021	5.80	No
	27	×	-0.063 -0.063	5.53 0.47	No No
		×	-0.015	3.00	No
		×	-0.021	5.80	No
	13	x	-0.016	1.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
	14	×	-0.016	1.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
	15	×	-0.016	1.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
	19	×	0.00	0.00	No
		X	0.00	0.00	No
		x	0.00	0.00	No
	20	×	0.00	0.00	No
		X	0.00	0.00	No
	21	x	0.00	0.00	No
	21	×	0.00 0.00	0.00 0.00	No No
		x	0.00	0.00	No
	26	x	-0.045	5.25	No
		×	-0.045	0.75	No
		×	-0.02	3.00	No
		x	-0.033	5.80	No
	29	×	-0.03	4.54	No
		×	-0.03	1.46	No
		×	-0.015	3.00	No
	38	X	-0.03	4.54	No
		x	-0.03	1.46	No
		×	-0.015	3.00	No
	40	×	-0.045	5.25	No
		×	-0.045	0.75	No
		×	-0.02	3.00	No

			0.000		
	45	×	-0.033	5.80	No
	45	x	-0.049	5.25	No
		x	-0.049	0.75	No
		×	-0.021	3.00	No
		x	-0.031	5.80	No
	28	x	-0.049	5.25	No
		×	-0.049	0.75	No
		×	-0.021	3.00	No
		×	-0.031	5.80	No
	46	×	-0.041	5.25	No
P2		×	-0.041	0.75	No
		×	-0.025	3.00	No
		×	-0.025	5.80	No
	48	x	-0.038	5.53	No
		×	-0.038	0.47	No
		×	-0.019	3.00	No
		×	-0.016	5.80	No
	51	x	-0.039	5.25	No
		×	-0.039	0.75	No
		×	-0.019	5.80	No
		×	-0.026	3.00	No
	60	x	0.00	0.00	No
		×	0.00	0.00	No
		×	0.00	0.00	No
	61	×	0.00	0.00	No
		x	0.00	0.00	No
		×	0.00	0.00	No
	62	×	0.00	0.00	No
		×	0.00	0.00	No
		x	0.00	0.00	No
	53	×	-0.022	4.54	No
		×	-0.022	1.46	No
		×.	-0.018	3.00	No
WL0	43	z	-0.012	5.53	No
		z	-0.012	0.47	No
		z	-0.004	3.00	No
		Z	-0.004	5.80	No
	27	z	-0.012	5.53	No
		z	-0.012	0.47	No
		z	-0.004	3.00	No
		z	-0.004	5.80	No
	13	z	-0.003	1.00	No
	14	z	-0.003	1.00	No
	15	z	-0.003	1.00	No
	26	z	-0.011	5.25	No
		z	-0.011	0.75	No
		z	-0.006	5.80	No
		z	-0.006	3.00	No
		2	0.00	0.00	No
	29	z	-0.006	4.54	No
	20	Z	-0.006	1.46	No
	38	z	-0.006	4.54	No
	30	z	-0.006	1.46	
	40				No No
	40	Z	-0.011 0.011	5.25	No No
		z	-0.011	0.75	No 🥖
		Z	-0.006	5.80	No
		z	-0.006	3.00	No
	45	2	0.00	0.00	No
	45	z	-0.011	5.25	No
		Z	-0.011	0.75	No

		z	-0.005	5.80	No
		z	-0.007	3.00	No
	28	z	-0.011	5.25	No
		z	-0.011	0.75	No
		z	-0.005	5.80	No
		z	-0.007	3.00	No
	46	z	-0.012	5.25	No
		z	-0.012	0.75	No
		z	-0.002	3.00	No
		z	-0.008	5.80	No
	48	z	-0.02	5.53	No
	,-	z	-0.02	0.47	No
		z	-0.002	3.00	No
		z	-0.001	5.80	No
	51	z	-0.014	5.25	No
	•	z	-0.014	0.75	No
		z	-0.008	5.80	No
		z	-0.004	3.00	No
	53	z	-0.008	4.54	No
	•	z	-0.008	1.46	No
WL30	43	x	-0.018	5.53	No
**150	40	×	-0.018	0.47	No
		×	-0.004	3.00	No
		x	-0.005	5.80	No
	27	x	-0.003	5.53	No
	21	×	-0.018	0.47	No
			-0.004	3.00	
		×			No
	13	X	-0.005	5.80	No
	14	X	-0.003	1.00	No
	15	×	-0.003	1.00	No
		×	-0.003	1.00	No
	26	×	-0.012	5.25	No
		×	-0.012	0.75	No
		X	-0.005	3.00	No
	20	×	-0.008	5.80	No
	29	×	-0.008	4.54	No
	20	X	-0.008	1.46	No
	38	x	-0.008	4.54	No
	40	×	-0.008	1.46	No
	40	×	-0.012	5.25	No
		×	-0.012	0.75	No
		×	-0.005	3.00	No
	45	×	-0.008	5.80	No
	45	×	-0.013	5.25	No
		×	-0.013	0.75	No
		x	-0.007	5.80	No
		×	-0.005	3.00	No
	28	×	-0.013	5.25	No
		×	-0.013	0.75	No
		×	-0.007	5.80	No
		×	-0.005	3.00	No
	46	×	-0.01	5.25	No
		×	-0.01	0.75	No
		×	-0.005	3.00	No
		x	-0.005	5.80	No
	48	x	-0.009	5.53	No
		×	-0.009	0.47	No
		×	-0.004	3.00	No
		×	-0.003	5.80	No
	51	x	-0.01	5.25	No

		х	-0.01	0.75	No
		x	-0.006	3.00	No
		x	-0.004	5.80	No
	53	x	-0.005	4.54	No
		×	-0.005	1.46	No
		x	-0.004	3.00	No
LL1	20	У	-0.25	6.33	No
LL2	20	У	-0.25	12.66	No
LLa1	53	У	-0.50	0.00	No
LLa2	51	У	-0.50	0.00	No
LLa3	48	У	-0.50	0.00	No
LLa4	46	у	-0.50	0.00	No
****		*******			

Self weight multipliers for load conditions

			Self weigl	nt multiplie	<u>r</u>
Condition	Description	Comb.	MultX	MultY	MultZ
DL	Dead Load	No	0.00	-1.00	0.00
W0	Wind Load 0/60/120 deg	No	0.00	0.00	0.00
W30	Wind Load 30/90/150 deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
Wi0	Ice Wind Load 0/60/120 deg	No	0.00	0.00	0.00
Wi30	Ice Wind Load 30/90/150 deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0/60/120 deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30/90/150 deg	No	0.00	0.00	0.00
LL1	250 lb Live Load Center of Mount	No	0.00	0.00	0.00
LL2	250 lb Live Load End of Mount	No	0.00	0.00	0.00
LLa1	500 lb Live Load on Antenna 1	No	0.00	0.00	0.00
LLa2	500 lb Live Load on Antenna 2	No	0.00	0.00	0.00
LLa3	500 lb Live Load on Antenna 3	No	0.00	0.00	0.00
LLa4	500 lb Live Load on Antenna 4	No	0.00	0.00	0.00
W180	-W0	Yes	0.00	0.00	0.00
W210	-W30	Yes	0.00	0.00	0.00
Wi180	-Wi0	Yes	0.00	0.00	0.00
Wi210	-Wi30	Yes	0.00	0.00	0.00
WL180	-WL0	Yes	0.00	0.00	0.00
WL210	-WL30	Yes	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]	
DL	0.00	0.00	0.00	
W0	0.00	0.00	0.00	
W30	0.00	0.00	0.00	
Di	0.00	0.00	0.00	
Wi0	0.00	0.00	0.00	
Wi30	0.00	0.00	0.00	
WL0	0.00	0.00	0.00	
WL30	0.00	0.00	0.00	
LL1	0.00	0.00	0.00	

LL2	0.00	0.00	0.00	
LLa1	0.00	0.00	0.00	
LLa2	0.00	0.00	0.00	
LLa3	0.00	0.00	0.00	
LLa4	0.00	0.00	0.00	
W180	0.00	0.00	0.00	
W210	0.00	0.00	0.00	
Wi180	0.00	0.00	0.00	
Wi210	0.00	0.00	0.00	
WL180	0.00	0.00	0.00	
WL210	0.00	0.00	0.00	



Current Date: 6/20/2018 3:28 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1029\LTE 4C-5C\CT1029 (LTE

4C-5C).etz\

Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design :

W180=-W0

W210=-W30

Wi180=-Wi0

Wi210=-Wi30

WL180=-WL0

WL210=-WL30

LC1=1.2DL+1.6W0

LC2=1.2DL+1.6W30

LC3=1.2DL-1.6W0

1.252 1.000

LC4=1.2DL-1.6W30

LC5=0.9DL+1.6W0

LC6=0.9DL+1.6W30

LC7=0.9DL-1.6W0

LC8=0.9DL-1.6W30 LC9=1.2DL+Di+Wi0

LC10=1.2DL+Di+Wi30

LC11=1.2DL+Di-Wi0

LOTI-1.2DL DI-VIO

LC12=1.2DL+Di-Wi30

LC13=1.2DL

LC14=0.9DL

LC15=1.2DL+1.6LL1

LC16=1.2DL+1.6LL2

LC17=1.2DL+WL0+LLa1

LC18=1.2DL+WL30+LLa1

LC19=1.2DL-WL0+LLa1

LC20=1.2DL-WL30+LLa1

LC21=1.2DL+WL0+LLa2

LC22=1.2DL+WL30+LLa2 LC23=1.2DL-WL0+LLa2

LC24=1.2DL-WL30+LLa2

LC25=1.2DL+WL0+LLa3

LC26=1.2DL+WL30+LLa3

LC27=1.2DL-WL0+LLa3

LC28=1.2DL-WL30+LLa3

LC29=1.2DL+WL0+LLa4

LC30=1.2DL+WL30+LLa4

LC31=1.2DL-WL0+LLa4

LC32=1.2DL-WL30+LLa4

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
AANATAHA TAANIIN HAKAANAA	HSS_SQR 4X4X1_4	13	LC1 at 0.00%	0.67	OK	**********************
			LC10 at 0.00%	0.99	OK	
			LC11 at 0.00%	0.99	ок	Eq. H1-1b
			LC12 at 0.00%	0.92	OK	-,
			LC13 at 0.00%	0.58	OK	
			LC14 at 0.00%	0.44	OK	
			LC15 at 0.00%	0.65	OK	
			LC16 at 0.00%	0.56	OK	
			LC17 at 0.00%	0.57	ОК	
		LC18 at 0.00%	0.58	OK		

Page1

	LC19 at 0.00%	0.58	OK	
	LC2 at 0.00%	0.82	OK	
	LC20 at 0.00%	0.56	OK	
	LC21 at 0.00%			
		0.63	OK	
	LC22 at 0.00%	0.65	OK	
	LC23 at 0.00%	0.65	OK	
	LC24 at 0.00%	0.63	OK	
	LC25 at 0.00%	0.72	OK	
	LC26 at 0.00%	0.73	OK	
	LC27 at 0.00%	0.73	OK	
	LC28 at 0.00%	0.72	OK	
	LC29 at 0.00%	0.83	OK	
	LC3 at 0.00%	0.81	OK	
	LC30 at 0.00%	0.84	OK	
	LC31 at 0.00%	0.84	OK	
	LC32 at 0.00%	0.82	OK	
	LC4 at 0.00%	0.55	OK	
	LC5 at 0.00%	0.52	OK	
	LC6 at 0.00%	0.68	OK	
	LC7 at 0.00%	0.67	OK	
	LC8 at 0.00%	0.40	OK	
	LC9 at 0.00%	0.96	OK	
	W180 at 0.00%	0.15	OK	
	W210 at 0.00%	0.15	OK	
	Wi180 at 0.00%	0.06	OK	
	Wi210 at 0.00%	0.05	OK	
	WL180 at 0.00%	0.01	OK	
	WL210 at 0.00%	0.01	OK	
	\2000000000000000000000000000000000000		DIRRIUM CONT.	
14	LC1 at 0.009/	0.47	OK	
1-4	LC1 at 0.00%	0.47	OK	
	LC10 at 0.00%	0.78	OK	
	LC11 at 0.00%	0.81	OK	
	LC12 at 0.00%	0.85	OK	Eq. H1-1b
	LC13 at 0.00%	0.50	OK	
		0.50 0.37	OK OK	
	LC14 at 0.00%	0.37	ОК	
	LC14 at 0.00% LC15 at 0.00%	0.37 0.57	OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00%	0.37 0.57 0.70	OK OK OK	
	LC14 at 0.00% LC15 at 0.00%	0.37 0.57	OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00%	0.37 0.57 0.70	OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00%	0.37 0.57 0.70 0.74	OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00%	0.37 0.57 0.70 0.74 0.74	OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47	OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76	OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63	OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63	OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC21 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63	OK OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63	OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC21 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63	OK OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63 0.64 0.65	OK OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC23 at 0.00% LC24 at 0.00% LC26 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63 0.64 0.65 0.55	OK OK OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC25 at 0.00% LC25 at 0.00%	0.37 0.57 0.70 0.74 0.75 0.47 0.76 0.63 0.63 0.64 0.65 0.55 0.55	OK OK OK OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.63 0.63 0.64 0.65 0.55 0.56	OK O	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.63 0.63 0.64 0.65 0.55 0.55 0.56 0.48	OK O	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.63 0.63 0.64 0.65 0.55 0.55 0.56 0.48 0.63	OK OK OK OK OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.63 0.63 0.64 0.65 0.55 0.55 0.56 0.48	OK O	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.63 0.63 0.64 0.65 0.55 0.55 0.56 0.48 0.63	OK OK OK OK OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.63 0.63 0.64 0.65 0.55 0.55 0.56 0.48 0.63 0.48	OK OK OK OK OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC31 at 0.00% LC31 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.63 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.63	OK OK OK OK OK OK OK OK OK OK OK OK OK	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.63 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.49 0.50 0.74	OK OK OK OK OK OK OK OK OK OK OK OK OK O	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.63 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.49 0.50 0.74 0.35	OK OK OK OK OK OK OK OK OK OK OK OK OK O	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC4000% LC5000% LC5000% LC5000% LC5000% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.49 0.50 0.74 0.35 0.35	OK OK OK OK OK OK OK OK OK OK OK OK OK O	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC27 at 0.00% LC29 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC6 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.49 0.50 0.74 0.35 0.35 0.51	OK OK OK OK OK OK OK OK OK OK OK OK OK O	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC4000% LC5000% LC5000% LC5000% LC5000% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.49 0.50 0.74 0.35 0.51 0.61	OK OK OK OK OK OK OK OK OK OK OK OK OK O	
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC27 at 0.00% LC29 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC6 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.49 0.50 0.74 0.35 0.35 0.51	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC6 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.49 0.50 0.74 0.35 0.51 0.61	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00% LC8 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.49 0.50 0.74 0.35 0.51 0.61 0.78 0.08	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00% LC9 at 0.00%	0.37 0.57 0.70 0.74 0.74 0.75 0.47 0.76 0.63 0.63 0.64 0.65 0.55 0.56 0.48 0.63 0.48 0.49 0.50 0.74 0.35 0.51 0.61 0.78	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

	M/240 -4 0 000/	0.06	OK	
	Wi210 at 0.00% WL180 at 0.00%	0.06 0.01	OK OK	
	WL210 at 0.00%	0.01	OK	

15	LC1 at 0.00%	0.61	OK	
	LC10 at 0.00%	0.66	OK	
	LC11 at 0.00%	0.63	OK	
	LC12 at 0.00%	0.66	OK	
	LC13 at 0.00%	0.41	OK	
	LC14 at 0.00%	0.31	OK	
	LC15 at 0.00%	0.39	OK	
	LC16 at 0.00%	0.39	OK	
	LC17 at 0.00%	0.40	OK	
	LC18 at 0.00%	0.39	OK	
	LC19 at 0.00%	0.38	OK	
	LC2 at 0.00% LC20 at 0.00%	0.49 0.39	OK OK	
	LC21 at 0.00%	0.40	OK OK	
	LC22 at 0.00%	0.39	OK	
	LC23 at 0.00%	0.38	ОК	
	LC24 at 0.00%	0.39	OK	
	LC25 at 0.00%	0.40	OK	
	LC26 at 0.00%	0.39	OK	
	LC27 at 0.00%	0.38	OK	
	LC28 at 0.00%	0.39	OK	
	LC29 at 0.00%	0.40	OK	
	LC3 at 0.00%	0.32	OK	
	LC30 at 0.00%	0.39	OK	
	LC31 at 0.00%	0.38	OK	
	LC32 at 0.00%	0.39	OK	
	LC4 at 0.00%	0.49	OK	
	LC5 at 0.00%	0.51	OK	
	LC6 at 0.00%	0.39	OK	
	LC7 at 0.00%	0.22	OK	
	LC8 at 0.00%	0.39	OK	
	LC9 at 0.00%	0.70	OK	Eq. H1-1b
	W180 at 0.00%	0.12	OK	
	W210 at 0.00%	0.05	OK	
	Wi180 at 0.00% Wi210 at 0.00%	0.05	OK OK	
	WL180 at 0.00%	0.01 0.01	OK	
	WL210 at 0.00%	0.00	OK	
	**************************************	**********		
19	LC1 at 0.00%	0.36	OK	Eq. H1-1b
	LC10 at 100.00%	0.33	OK	'
	LC11 at 100.00%	0.31	OK	
	LC12 at 100.00%	0.34	OK	
	LC13 at 100.00%	0.18	OK	
	LC14 at 100.00%	0.14	OK	
	LC15 at 100.00%	0.20	OK	
	LC16 at 100.00%	0.22	OK –	
	LC17 at 100.00%	0.23	OK	
	LC18 at 100.00%	0.24	OK	
	LC19 at 100.00%	0.24	OK	
	LC2 at 100.00%	0.37	OK	
	LC20 at 100.00%	0.25	OK	
	LC21 at 100.00% LC22 at 100.00%	0.21	OK OK	
	LC22 at 100.00%	0.22 0.22	OK OK	
	LC24 at 100.00%	0.22	OK OK	
	LC25 at 100.00%	0.20	OK	
	//			
	LC26 at 100.00%	0.21	OK	
	LC26 at 100.00% LC27 at 100.00%	0.21 0.20	OK OK	

	LC29 at 100.00% LC3 at 0.00% LC30 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 0.00% LC6 at 100.00% LC7 at 0.00% LC9 at 100.00% W180 at 0.00% Wi180 at 0.00% Wi210 at 100.00% WL180 at 0.00% WL180 at 0.00%	0.18 0.27 0.20 0.19 0.20 0.42 0.32 0.32 0.32 0.37 0.31 0.11 0.15 0.04 0.05 0.01	OK OK OK OK OK OK OK OK	Eq. H1-1b
20	LC1 at 0.00% LC10 at 0.00% LC11 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC27 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00%	0.42 0.35 0.37 0.33 0.20 0.15 0.25 0.24 0.25 0.24 0.27 0.26 0.27 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.28 0.26 0.41 0.26 0.25 0.33 0.37 0.30 0.36 0.28 0.37 0.14 0.09 0.05 0.03 0.01 0.01	OK OK	Eq. H1-1b
21	LC1 at 100.00% LC10 at 0.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00%	0.35 0.37 0.33 0.36 0.20 0.15 0.22	OK OK OK OK OK OK	Eq. H1-1b

	LC16 at 0.00%	0.20	OK	
	LC17 at 0.00%	0.20	OK	
	LC18 at 0.00%	0.22	OK	
	LC19 at 0.00%	0.21	OK	
	LC2 at 0.00%	0.43	OK	Eq. H1-1b
	LC20 at 0.00%	0.22	OK	_4,
	LC21 at 0.00%	0.22	OK	
	LC22 at 0.00%	0.23	OK	
	LC23 at 0.00%			
	LC24 at 0.00%	0.22	OK	
		0.23	OK	
	LC25 at 0.00%	0.23	OK	
	LC26 at 0.00%	0.24	OK	
	LC27 at 0.00%	0.24	OK	
	LC28 at 0.00%	0.24	OK	
	LC29 at 0.00%	0.25	OK	
	LC3 at 0.00%	0.26	OK	
	LC30 at 0.00%	0.26	OK	
	LC31 at 0.00%	0.26	OK	
	LC32 at 0.00%	0.26	OK	
	LC4 at 0.00%	0.39	OK	
	LC5 at 100.00%	0.31	OK	
	LC6 at 0.00%	0.38	OK	
	LC7 at 3.75%	0.21	OK	
	LC8 at 0.00%	0.34	OK	
	LC9 at 0.00%	0.32	OK	
	W180 at 100.00%	0.10	ok	
	W210 at 0.00%	0.10	OK OK	
	Wi180 at 100.00%			
		0.04	OK	
	Wi210 at 0.00%	0.05	OK	
	WL180 at 100.00%	0.01	OK	
	WL210 at 0.00%	0.01	ок	
00	Committee and the committee of the commi			
60	LC1 at 75.00%	0.52	OK	
60	LC10 at 75.00%	0.57	ОК	F. 114.41
60	LC10 at 75.00% LC11 at 75.00%	0.57 0.59	ОК ОК	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00%	0.57 0.59 0.55	ОК ОК ОК	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00%	0.57 0.59 0.55 0.34	ОК ОК ОК	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00%	0.57 0.59 0.55 0.34 0.25	OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39	OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34	OK OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35	OK OK OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC18 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34	OK OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC18 at 75.00% LC19 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35	OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC18 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35	OK OK OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC18 at 75.00% LC19 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35	OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC18 at 75.00% LC19 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.35	OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC18 at 75.00% LC19 at 75.00% LC2 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.35 0.50 0.35	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC18 at 75.00% LC19 at 75.00% LC2 at 75.00% LC20 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.35 0.50 0.35	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC18 at 75.00% LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.50 0.35 0.35 0.39	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC18 at 75.00% LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.50 0.35 0.39 0.39	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.50 0.35 0.39 0.40 0.39 0.40	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC25 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.35 0.35 0.50 0.35 0.39 0.40 0.39 0.40 0.39	OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.35 0.35 0.50 0.35 0.39 0.40 0.39 0.40 0.39 0.43 0.43	OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC23 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC28 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.35 0.35 0.50 0.35 0.39 0.40 0.39 0.40 0.39 0.43 0.43	OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC29 at 0.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.35 0.35 0.35 0.35 0.39 0.40 0.39 0.40 0.39 0.43 0.43 0.43 0.43	OK	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC29 at 0.00% LC29 at 0.00% LC29 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.43	OK O	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC26 at 75.00% LC27 at 75.00% LC27 at 75.00% LC28 at 75.00% LC29 at 0.00% LC30 at 75.00% LC30 at 75.00% LC30 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.43 0.43	OK O	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC27 at 75.00% LC28 at 75.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.35 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.43 0.44 0.55 0.47	OK O	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC27 at 75.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.43 0.44 0.55 0.47 0.47	OK O	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC15 at 75.00% LC16 at 75.00% LC16 at 75.00% LC19 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC26 at 75.00% LC27 at 75.00% LC27 at 75.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.44 0.55 0.47 0.46 0.44	OK O	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC18 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC27 at 75.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 75.00% LC32 at 75.00% LC32 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.44 0.44	OK O	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC18 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 75.00% LC32 at 75.00% LC32 at 75.00% LC30 at 75.00% LC30 at 75.00% LC31 at 0.00% LC31 at 0.00% LC32 at 75.00% LC4 at 75.00% LC5 at 75.00% LC5 at 75.00% LC5 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.44 0.45	OK O	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC16 at 75.00% LC19 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 75.00% LC32 at 75.00% LC31 at 0.00% LC31 at 75.00% LC31 at 75.00% LC32 at 75.00% LC32 at 75.00% LC31 at 75.00% LC32 at 75.00% LC4 at 75.00% LC5 at 75.00% LC5 at 75.00% LC6 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.44 0.47	OK O	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC18 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 75.00% LC32 at 75.00% LC32 at 75.00% LC30 at 75.00% LC30 at 75.00% LC31 at 0.00% LC31 at 0.00% LC31 at 75.00% LC32 at 75.00% LC4 at 75.00% LC5 at 75.00% LC6 at 75.00% LC6 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.44 0.41 0.47 0.35	OK O	Eq. H1-1b
60	LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC16 at 75.00% LC19 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 75.00% LC32 at 75.00% LC31 at 0.00% LC31 at 75.00% LC31 at 75.00% LC32 at 75.00% LC32 at 75.00% LC31 at 75.00% LC32 at 75.00% LC4 at 75.00% LC5 at 75.00% LC5 at 75.00% LC6 at 75.00%	0.57 0.59 0.55 0.34 0.25 0.39 0.34 0.35 0.35 0.35 0.39 0.40 0.39 0.43 0.43 0.43 0.43 0.44 0.47	OK O	Eq. H1-1b

	W180 at 75.00% W210 at 75.00% Wi180 at 75.00% Wi210 at 75.00% WL180 at 75.00% WL210 at 75.00%	0.14 0.10 0.05 0.04 0.01 0.01	OK OK OK OK OK	
61	LC1 at 75.00% LC10 at 75.00% LC11 at 75.00% LC12 at 75.00% LC13 at 75.00% LC14 at 75.00% LC15 at 75.00% LC16 at 75.00% LC17 at 75.00% LC19 at 75.00% LC20 at 75.00% LC21 at 75.00% LC21 at 75.00% LC22 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC27 at 75.00% LC28 at 75.00% LC29 at 75.00% LC29 at 75.00% LC20 at 75.00% LC21 at 75.00% LC25 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC30 at 75.00% LC30 at 75.00% LC31 at 75.00% LC31 at 75.00% LC32 at 75.00% LC32 at 75.00% LC4 at 75.00% LC5 at 75.00%	0.36 0.48 0.44 0.48 0.28 0.21 0.28 0.29 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.29 0.28 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29	OK O	Eq. H1-1b
	LC8 at 75.00% LC9 at 75.00% W180 at 0.00% W210 at 75.00% Wi180 at 0.00% Wi210 at 75.00% WL180 at 0.00% WL210 at 75.00%	0.13 0.39 0.47 0.07 0.11 0.03 0.04 0.01	OK OK OK OK OK OK OK	
62	LC1 at 25.00% LC10 at 25.00% LC11 at 25.00% LC12 at 25.00% LC13 at 25.00% LC14 at 25.00% LC16 at 100.00% LC16 at 100.00% LC18 at 100.00% LC19 at 25.00% LC2 at 25.00% LC20 at 100.00% LC21 at 25.00% LC21 at 25.00% LC22 at 25.00% LC22 at 25.00% LC23 at 25.00% LC23 at 25.00% LC24 at 25.00% LC25 at 25.00%	0.45 0.51 0.52 0.53 0.31 0.23 0.36 0.38 0.41 0.41 0.41 0.42 0.40 0.40 0.40 0.40 0.36	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b

		LC26 at 25.00% LC27 at 25.00% LC28 at 25.00% LC29 at 25.00% LC3 at 25.00% LC30 at 25.00% LC31 at 25.00% LC32 at 25.00% LC4 at 25.00% LC5 at 25.00% LC6 at 25.00% LC7 at 25.00% LC9 at 25.00% V180 at 25.00% W1180 at 25.00% W1210 at 25.00% WL210 at 25.00%	0.36 0.36 0.36 0.32 0.48 0.32 0.32 0.32 0.48 0.37 0.33 0.40 0.40 0.51 0.11 0.11 0.04 0.04	OK O	
				····	***************************************
PIPE 2x0.154	26	LC1 at 65.63%	0.70	OK	
		LC10 at 65.63%	0.19	OK	
		LC11 at 65.63%	0.18	OK OK	
		LC12 at 65.63% LC13 at 65.63%	0.19	OK OK	
		LC14 at 65.63%	0.01 0.01	OK OK	
		LC15 at 65.63%	0.01	OK OK	
		LC16 at 65.63%	0.01	OK	
		LC17 at 65.63%	0.04	OK	
		LC18 at 65.63%	0.05	OK	
		LC19 at 65.63%	0.04	OK	
		LC2 at 65.63%	0.74	OK	
		LC20 at 65.63%	0.05	OK	
		LC21 at 65.63%	0.04	OK	
		LC22 at 65.63%	0.05	OK	
		LC23 at 65.63%	0.04	OK	
		LC24 at 65.63%	0.05	OK	
		LC25 at 65.63%	0.04	OK	
		LC26 at 65.63%	0.05	OK	
		LC27 at 65.63%	0.04	OK	
		LC28 at 65.63%	0.05	OK	
		LC29 at 65.63%	0.04	OK	
		LC3 at 65.63%	0.70	OK	
		LC30 at 65.63% LC31 at 65.63%	0.05	OK	
		LC31 at 65.63%	0.04	OK	
		LC32 at 65.63%	0.05 0.74	ОК ОК	Eq. H1-1b
		LC5 at 65.63%	0.74	OK	⊑q. 111-10
		LC6 at 65.63%	0.74	OK	
		LC7 at 65.63%	0.70	ОК	
		LC8 at 65.63%	0.74	OK	
		LC9 at 65.63%	0.18	OK	
		W180 at 65.63%	0.43	OK	
		W210 at 65.63%	0.46	OK	
		Wi180 at 65.63%	0.17	OK	
		Wi210 at 65.63%	0.18	OK	
		WL180 at 65.63%	0.04	OK	
		WL210 at 65.63%	0.05	OK	
	29	LC1 at 65.63%	0.24	OK	
		LC10 at 65.63%	0.10	OK	
		LC11 at 65.63%	0.07	OK	
		LC12 at 65.63%	0.10	OK	

	LC13 at 65.63%	0.01	OK	
	LC14 at 65.63%	0.00	OK	
	LC15 at 65.63%	0.01	OK	
	LC16 at 65.63%	0.01	OK	
	LC17 at 65.63%	0.02	OK	
	LC18 at 65.63%	0.02	OK	
	LC19 at 65.63%	0.02	OK	
	LC2 at 65.63%	0.32	OK	Eq. H1-1b
	LC20 at 65.63%	0.02	OK	
	LC21 at 65.63%	0.02	OK	
	LC22 at 65.63%	0.02	OK	
	LC23 at 65.63%	0.02	OK	
	LC24 at 65.63%	0.02	OK	
	LC25 at 65.63%	0.02	OK	
	LC26 at 65.63%	0.02	OK	
	LC27 at 65.63%	0.02	OK	
	LC28 at 65.63%	0.02	OK	
	LC29 at 65.63%	0.02	OK	
	LC3 at 65.63%	0.24	OK	
	LC30 at 65.63%	0.02	OK	
	LC31 at 65.63%	0.02	OK	
	LC32 at 65.63%	0.02	OK	
	LC4 at 65.63%	0.32	OK	
	LC5 at 65.63%	0.24	OK	
	LC6 at 65.63%	0.32	OK	
	LC7 at 65.63%	0.24	OK	
	LC8 at 65.63%	0.32	OK	
	LC9 at 65.63%	0.07	OK	
	W180 at 65.63%	0.15	OK	
	W210 at 65.63%	0.20	OK	
	Wi180 at 65.63%	0.07	OK	
	Wi210 at 65.63%	0.10	OK	
	WL180 at 65.63%		OK	
		0.02 0.02		
	WL180 at 65.63%	0.02	ОК	********************************
38	WL180 at 65.63%	0.02	ОК	
38	WL180 at 65.63% WL210 at 65.63%	0.02 0.02	OK OK	
38	WL180 at 65.63% WL210 at 65.63% LC1 at 65.63%	0.02 0.02 0.24	OK OK	
38	WL180 at 65.63% WL210 at 65.63% 	0.02 0.02 0.24 0.10	OK OK OK OK	
38	WL180 at 65.63% WL210 at 65.63% 	0.02 0.02 0.24 0.10 0.07	OK OK OK OK OK	
38	WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10	OK OK OK OK OK	
38	WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10 0.01	OK OK OK OK OK OK	
38	WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10 0.01 0.00	OK OK OK OK OK OK OK	
38	WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10 0.01 0.00 0.01	OK OK OK OK OK OK OK OK	
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC16 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10 0.01 0.00 0.01 0.01	OK OK OK OK OK OK OK OK OK OK	
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10 0.01 0.00 0.01 0.01 0.02	OK OK OK OK OK OK OK OK OK OK OK	
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC16 at 65.63% LC16 at 65.63% LC17 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10 0.01 0.00 0.01 0.01 0.02 0.02	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10 0.01 0.00 0.01 0.01 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC18 at 65.63% LC18 at 65.63% LC19 at 65.63%	0.02 0.02 0.10 0.07 0.10 0.01 0.01 0.01 0.01 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC18 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.01 0.01 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC18 at 65.63% LC19 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC20 at 65.63%	0.02 0.02 0.10 0.07 0.10 0.01 0.00 0.01 0.01 0.02 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC18 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC17 at 65.63% LC12 at 65.63% LC19 at 65.63% LC2 at 65.63% LC20 at 65.63% LC20 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63%	0.02 0.02 0.24 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC20 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02	OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC20 at 65.63% LC21 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC23 at 65.63% LC24 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC21 at 65.63% LC22 at 65.63% LC20 at 65.63% LC20 at 65.63% LC22 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC27 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC12 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC20 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC21 at 65.63% LC22 at 65.63% LC20 at 65.63% LC20 at 65.63% LC22 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC27 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC15 at 65.63% LC16 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC21 at 65.63% LC22 at 65.63% LC20 at 65.63% LC20 at 65.63% LC22 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC21 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63% LC30 at 65.63% LC31 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.03 0.04 0.04 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC21 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63% LC29 at 65.63% LC30 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.03 0.03 0.04 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC15 at 65.63% LC16 at 65.63% LC16 at 65.63% LC17 at 65.63% LC18 at 65.63% LC21 at 65.63% LC22 at 65.63% LC20 at 65.63% LC20 at 65.63% LC22 at 65.63% LC23 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63% LC30 at 65.63% LC31 at 65.63% LC32 at 65.63% LC32 at 65.63% LC31 at 65.63% LC32 at 65.63% LC32 at 65.63% LC32 at 65.63% LC32 at 65.63% LC34 at 65.63% LC34 at 65.63% LC34 at 65.63% LC35 at 65.63% LC34 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.03 0.03 0.04 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC21 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63% LC30 at 65.63% LC31 at 65.63% LC32 at 65.63% LC31 at 65.63% LC32 at 65.63% LC31 at 65.63% LC32 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.03 0.04 0.04 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
38	WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC15 at 65.63% LC16 at 65.63% LC16 at 65.63% LC17 at 65.63% LC18 at 65.63% LC21 at 65.63% LC22 at 65.63% LC20 at 65.63% LC20 at 65.63% LC22 at 65.63% LC23 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63% LC30 at 65.63% LC31 at 65.63% LC32 at 65.63% LC32 at 65.63% LC31 at 65.63% LC32 at 65.63% LC32 at 65.63% LC32 at 65.63% LC32 at 65.63% LC34 at 65.63% LC34 at 65.63% LC34 at 65.63% LC35 at 65.63% LC34 at 65.63%	0.02 0.02 0.02 0.10 0.07 0.10 0.01 0.00 0.01 0.02 0.03 0.03 0.04 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

	LC7 at 65.63%	0.24	OK	
	LC8 at 65.63%	0.32	ОК	
	LC9 at 65.63%	0.07	ok	
	W180 at 65.63%	0.07	OK	
	W210 at 65.63%		OK	
		0.20		
	Wi180 at 65.63%	0.07	OK	
	Wi210 at 65.63%	0.10	OK	
	WL180 at 65.63%	0.02	OK	
	WL210 at 65.63%	0.02	OK	
40	LC1 at 65.63%	0.70	ОК	
	LC10 at 65.63%	0.19	OK	
	LC11 at 65.63%	0.18	OK	
	LC12 at 65.63%	0.19	OK	
	LC13 at 65.63%	0.01	OK	
	LC14 at 65.63%	0.01	OK	
	LC15 at 65.63%	0.01	OK	
	LC16 at 65.63%	0.01	OK	
	LC17 at 65.63%	0.04	OK	
	LC18 at 65.63%	0.05	OK	
	LC19 at 65.63%	0.04	OK	
	LC2 at 65.63%	0.74	OK	Eq. H1-1b
	LC20 at 65.63%	0.05	ОК	
	LC21 at 65.63%	0.04	OK	
	LC22 at 65.63%	0.05	ОК	
	LC23 at 65.63%	0.04	OK	
	LC24 at 65.63%	0.05	OK	
	LC25 at 65.63%	0.04	OK	
	LC26 at 65.63%	0.05	ОК	
	LC27 at 65.63%	0.04	OK	
	LC28 at 65.63%	0.05	OK	
	LC29 at 65.63%	0.04	OK	
	LC3 at 65.63%	0.70	OK	
	LC30 at 65.63%	0.05	OK	
	LC31 at 65.63%	0.04	OK	
	LC32 at 65.63%	0.05	OK	
	LC4 at 65.63%	0.74	OK	
	LC5 at 65.63%	0.70	OK	
	LC6 at 65.63%	0.74	OK	
	LC7 at 65.63%	0.70	OK	
	LC8 at 65.63%	0.74	OK	
	LC9 at 65.63%	0.18	OK	
	W180 at 65.63%	0.43	OK	
	W210 at 65.63%	0.46	OK	
	Wi180 at 65.63%	0.17	OK	
	Wi210 at 65.63%	0.18	OK	
	WL180 at 65.63%	0.04	ОК	
	WL210 at 65.63%	0.05	OK	
43	LC1 at 65.63%	0.79	OK	\$1000000000000000000000000000000000000
	LC1 at 65.63%	0.79	OK	
	LC11 at 65.63%	0.20	OK	
	LC11 at 65.63%	0.21	OK	
	LC12 at 65.63%	0.20	OK	
	LC14 at 65.63%	0.01	OK	
	LC15 at 65.63%		OK	
	LC16 at 65.63%	0.01 0.01	OK	
	LC16 at 65.63%			
	LC17 at 65.63%	0.05 0.08	OK OK	
	LC16 at 65.63%	0.08	OK	
	LC2 at 65.63%	1.14	N.G.	Ea H1 15
	LC20 at 65.63%	0.08	OK	Eq. H1-1b
	LC20 at 65.63%	0.05	OK	
	LC22 at 65.63%	0.03	OK	
	LOZZ & 00.00 /0	0.00	OIL	

	LC23 at 65.63% LC24 at 65.63%	0.05 0.08	OK OK	
	LC25 at 65.63%	0.05	OK	
	LC26 at 65.63%	0.08	OK	
	LC27 at 65.63%	0.05	OK	
	LC28 at 65.63%	80.0	OK	
	LC29 at 65.63%	0.05	OK	
	LC3 at 65.63%	0.79	OK	
	LC30 at 65.63%	0.08	OK	
	LC31 at 65.63%	0.05	OK	
	LC32 at 65.63%	0.08	OK	
	LC4 at 65.63%	1.14	N.G.	
	LC5 at 65.63%	0.79	OK	
	LC6 at 65.63%	1.14	N.G.	
	LC7 at 65.63%	0.79	OK	
	LC8 at 65.63%	1.14	N.G.	
	LC9 at 65.63%	0.21	OK	
	W180 at 65.63%	0.49	OK	
	W210 at 65.63%	0.71	OK	
	Wi180 at 65.63%	0.20	OK	
	Wi210 at 65.63%	0.26	OK OK	
	WL180 at 65.63% WL210 at 65.63%	0.05 0.07	OK OK	
	VVL210 at 05.05 /6		***************************************	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
27	LC1 at 65.63%	0.79	OK	
	LC10 at 65.63%	0.26	OK	
	LC11 at 65.63%	0.21	OK	
	LC12 at 65.63%	0.26	OK	
	LC13 at 65.63%	0.01	OK	
	LC14 at 65.63%	0.01	OK	
	LC15 at 65.63%	0.01	OK	
	LC16 at 65.63%	0.01	OK	
	LC17 at 65.63%	0.05	OK	
	LC18 at 65.63% LC19 at 65.63%	0.08 0.05	OK OK	
	LC2 at 65.63%	1.14	N.G.	
	LC20 at 65.63%	0.08	OK	
	LC21 at 65.63%	0.05	OK	
	LC22 at 65.63%	0.08	ОК	
	LC23 at 65.63%	0.05	OK	
	LC24 at 65.63%	0.08	OK	
	LC25 at 65.63%	0.05	ОК	
	LC26 at 65.63%	0.08	OK	
	LC27 at 65.63%	0.05	OK	
	LC28 at 65.63%	0.08	OK	
	LC29 at 65.63%	0.05	OK	
	LC3 at 65.63%	0.79	OK	
	LC30 at 65.63%	0.08	OK	
	LC31 at 65.63%	0.05	OK	
	LC32 at 65.63%	0.08	OK	
	LC4 at 65.63%	1.14	N.G.	Eq. H1-1b
	LC5 at 65.63%	0.79	OK	
	LC6 at 65.63%	1.14	N.G.	
	LC7 at 65.63%	0.79	OK N.C	
	LC8 at 65.63%	1.14	N.G.	
	LC9 at 65.63% W180 at 65.63%	0.21	OK OK	
	W210 at 65.63%	0.49 0.71	OK	
	Wi180 at 65.63%	0.71	OK	
	Wi210 at 65.63%	0.26	OK	
	WL180 at 65.63%	0.25	OK	
	WL210 at 65.63%	0.07	OK	

45	LC1 at 65.63%	0.72	ОК	

	1.040 -4.05.000/	0.00	OK	
	LC10 at 65.63%	0.20	OK	
	LC11 at 65.63%	0.19	OK	
	LC12 at 65.63%	0.20	OK	
	LC13 at 65.63%	0.01	OK	
	LC14 at 65.63%	0.01	OK	
	LC15 at 65.63%	0.01	OK	
	LC16 at 65.63%	0.01	OK	
	LC17 at 65.63%	0.05	OK	
	LC18 at 65.63%	0.06	OK	
	LC19 at 65.63%	0.05	OK	
	LC2 at 65.63%	0.84	OK	Eq. H1-1b
	LC20 at 65.63%	0.06	OK	
	LC21 at 65.63%	0.05	OK	
	LC22 at 65.63%	0.06	OK	
	LC23 at 65.63%	0.05	OK	
	LC24 at 65.63%	0.06	ok	
	LC25 at 65.63%	0.05	OK	
	LC26 at 65.63%	0.06	OK	
	LC27 at 65.63%	0.05	OK	
	LC28 at 65.63%	0.06	OK	
	LC29 at 65.63%	0.05	OK	
	LC3 at 65.63%	0.72	OK	
	LC30 at 65.63%	0.06	OK	
	LC31 at 65.63%	0.05	OK	
	LC32 at 65.63%	0.06	OK	
	LC4 at 65.63%	0.84	OK	
	LC5 at 65.63%	0.72	OK	
	LC6 at 65.63%	0.83	OK	
	LC7 at 65.63%	0.72	OK	
	LC8 at 65.63%	0.83	OK	
	LC9 at 65.63%	0.19	OK	
	W180 at 65.63%	0.45	OK	
	W210 at 65.63%	0.52	OK	
	Wi180 at 65.63%	0.18	OK	
	Wi180 at 65.63% Wi210 at 65.63%	0.18 0.19	OK OK	
	Wi180 at 65.63%	0.18	OK OK OK	
	Wi180 at 65.63% Wi210 at 65.63%	0.18 0.19	OK OK	
	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63%	0.18 0.19 0.05 0.05	OK OK OK OK	
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63%	0.18 0.19 0.05	OK OK OK	
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63%	0.18 0.19 0.05 0.05	OK OK OK OK	
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63%	0.18 0.19 0.05 0.05	OK OK OK OK	
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% ————————————————————————————————————	0.18 0.19 0.05 0.05 0.72 0.20	OK OK OK OK	
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% 	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20	OK OK OK OK OK OK OK	
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% 	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01	OK OK OK OK OK OK OK OK	**************************************
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01	OK OK OK OK OK OK OK OK OK	#1
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC12 at 65.63% LC13 at 65.63% LC13 at 65.63% LC14 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01	OK OK OK OK OK OK OK OK OK OK	A)
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC16 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01	OK OK OK OK OK OK OK OK OK OK	i)
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC14 at 65.63% LC17 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.01	OK OK OK OK OK OK OK OK OK OK	i)
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC16 at 65.63% LC17 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.01 0.05 0.06	OK OK OK OK OK OK OK OK OK OK OK	e)
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC19 at 65.63%	0.18 0.19 0.05 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.01 0.05 0.06 0.05	OK OK OK OK OK OK OK OK OK OK OK	s)
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC16 at 65.63% LC17 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.01 0.05 0.06	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC19 at 65.63%	0.18 0.19 0.05 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.01 0.05 0.06 0.05	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC1 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC17 at 65.63% LC18 at 65.63% LC18 at 65.63% LC19 at 65.63% LC19 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.01 0.05 0.06 0.05	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC10 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC12 at 65.63% LC19 at 65.63% LC21 at 65.63% LC20 at 65.63% LC20 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.84 0.06 0.05	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC10 at 65.63% LC10 at 65.63% LC12 at 65.63% LC12 at 65.63% LC2 at 65.63% LC20 at 65.63% LC21 at 65.63% LC22 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.84 0.06 0.05 0.06	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63% WL210 at 65.63% LC10 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC12 at 65.63% LC18 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC21 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63%	0.18 0.19 0.05 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.84 0.06 0.05 0.06 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC12 at 65.63% LC12 at 65.63% LC12 at 65.63% LC2 at 65.63% LC20 at 65.63% LC21 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.06 0.05 0.06	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC19 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC21 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63%	0.18 0.19 0.05 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.06 0.05 0.06 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC21 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC19 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC21 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC12 at 65.63% LC21 at 65.63% LC22 at 65.63% LC20 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC26 at 65.63% LC27 at 65.63% LC26 at 65.63% LC27 at 65.63% LC26 at 65.63% LC27 at 65.63% LC28 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC19 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC21 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC12 at 65.63% LC21 at 65.63% LC22 at 65.63% LC20 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC26 at 65.63% LC27 at 65.63% LC26 at 65.63% LC27 at 65.63% LC26 at 65.63% LC27 at 65.63% LC28 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC12 at 65.63% LC21 at 65.63% LC22 at 65.63% LC20 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC26 at 65.63% LC27 at 65.63% LC26 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63% LC29 at 65.63%	0.18 0.19 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06 0.05 0.06 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC19 at 65.63% LC19 at 65.63% LC2 at 65.63% LC20 at 65.63% LC21 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63%	0.18 0.19 0.05 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.06 0.05 0.06 0.05 0.06 0.06 0.06 0.06 0.06 0.07 0.06 0.07 0.06	OK O	Eq. H1-1b
28	Wi180 at 65.63% Wi210 at 65.63% WL210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC11 at 65.63% LC11 at 65.63% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC19 at 65.63% LC19 at 65.63% LC2 at 65.63% LC2 at 65.63% LC20 at 65.63% LC21 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63% LC29 at 65.63% LC29 at 65.63% LC20 at 65.63% LC21 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63% LC30 at 65.63%	0.18 0.19 0.05 0.05 0.05 0.72 0.20 0.19 0.20 0.01 0.01 0.01 0.05 0.06 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.08 0.09	OK O	Eq. H1-1b

	LC4 at 65.63% LC5 at 65.63% LC6 at 65.63% LC7 at 65.63% LC8 at 65.63% W180 at 65.63% W210 at 65.63% Wi180 at 65.63% Wi210 at 65.63% WL180 at 65.63%	0.84 0.72 0.83 0.72 0.83 0.19 0.45 0.52 0.18 0.19 0.05	OK OK OK OK OK OK OK OK OK OK	
46	LC1 at 65.63% LC10 at 65.63% LC11 at 68.75% LC12 at 65.63% LC13 at 65.63% LC14 at 65.63% LC15 at 65.63% LC16 at 65.63% LC17 at 65.63% LC18 at 65.63% LC19 at 65.63% LC2 at 65.63% LC20 at 65.63% LC22 at 65.63% LC22 at 65.63% LC22 at 65.63% LC23 at 65.63% LC24 at 65.63% LC25 at 65.63% LC25 at 65.63% LC26 at 65.63% LC27 at 65.63% LC27 at 65.63% LC27 at 65.63% LC28 at 65.63% LC29 at 65.63% LC30 at 65.63% LC31 at 65.63% LC32 at 65.63% LC31 at 65.63% LC32 at 65.63% LC32 at 65.63% LC32 at 65.63% LC32 at 65.63%	0.52 0.13 0.16 0.13 0.01 0.01 0.01 0.04 0.04 0.04 0.04 0.04	OK O	Eq. H1-1b
48	LC5 at 65.63% LC6 at 65.63% LC7 at 65.63% LC8 at 65.63% LC9 at 68.75% W180 at 65.63% W210 at 65.63% W1210 at 65.63% WL210 at 65.63% WL210 at 65.63% LC1 at 65.63% LC1 at 65.63% LC11 at 65.63% LC12 at 65.63% LC14 at 65.63% LC14 at 65.63% LC15 at 65.63% LC15 at 65.63% LC15 at 65.63% LC16 at 65.63% LC16 at 65.63% LC17 at 65.63% LC17 at 65.63% LC19 at 65.63% LC19 at 65.63%	0.52 0.53 0.52 0.53 0.16 0.32 0.33 0.16 0.12 0.03 0.03 0.95 0.13 0.22 0.13 0.01 0.03 0.04 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

	LC20 at 65.63%	0.03	OK	
	LC21 at 65.63%	0.06	OK	
	LC22 at 65.63%	0.03	OK	
	LC23 at 65.63%		OK	
		0.06		
	LC24 at 65.63%	0.03	OK	
	LC25 at 65.63%	0.08	OK	
	LC26 at 65.63%	0.05	OK	
	LC27 at 65.63%	0.08	OK	
	LC28 at 65.63%	0.05	OK	
	LC29 at 65.63%	0.06	OK	
	LC3 at 65.63%	0.95	OK	
	LC30 at 65.63%	0.03	OK	
	LC31 at 65.63%	0.06	OK	
	LC32 at 65.63%	0.03	OK	
	LC4 at 65.63%	0.48	OK	
	LC5 at 65.63%	0.95	OK	
	LC6 at 65.63%	0.48	OK	54
	LC7 at 65.63%	0.95	OK	
	LC8 at 65.63%	0.48	OK	
	LC9 at 65.63%	0.22	OK	
	W180 at 65.63%	0.59	OK	
	W210 at 65.63%	0.30	OK OK	
	Wi180 at 65.63%	0.30	OK OK	
	Wi210 at 65.63%	0.12	OK	
	WL180 at 65.63%	0.12	OK	
	WL210 at 65.63%	0.03	OK	
	VVL210 at 05.05 //	0.03	OK	
51	LC1 at 65.63%	0.65	OK	
	LC10 at 65.63%	0.13	OK	
	LC11 at 65.63%	0.16	OK	
	LC12 at 65.63%	0.13	OK	
	LC13 at 65.63%	0.01	OK	
	LC14 at 65.63%	0.01	OK	
	LC15 at 65.63%	0.01	OK	
	LC16 at 65.63%	0.01	OK	
	LC17 at 65.63%	0.04	OK	
	LC18 at 65.63%	0.04	OK	
	LC19 at 65.63%			
		0.04	OK	
	LC2 at 65.63%	0.51	OK	
	LC20 at 65.63%	0.04	OK	
	LC21 at 65.63%	0.06	OK	
	LC22 at 65.63%	0.05	OK	
	LC23 at 65.63%	0.06	OK	
	LC24 at 65.63%	0.05	OK	
	LC25 at 65.63%	0.04	OK	
	LC26 at 65.63%	0.04	OK	
	LC27 at 65.63%	0.04	OK	
	LC28 at 65.63%	0.04	OK	
	LC29 at 65.63%	0.04	OK	
	LC3 at 65.63%	0.65	OK	Eq. H1-1b
	LC30 at 65.63%	0.04	OK	
	LC31 at 65.63%	0.04	OK	
	LC32 at 65.63%	0.04	OK	
	LC4 at 65.63%	0.51	OK	
	LC5 at 65.63%	0.65	OK	
	LC6 at 65.63%	0.51	OK	
	LC7 at 65.63%	0.65	OK	
	LC8 at 65.63%	0.51	OK	
	LC9 at 65.63%	0.16	OK	
	W180 at 65.63%	0.40	OK	
	W210 at 65.63%	0.32	OK	
	Wi180 at 65.63%	0.15	OK	
	Wi210 at 65.63%	0.12	OK	
	WL180 at 65.63%	0.04	OK	

	WL210 at 65.63%	0.03	OK	
53	LC1 at 65.63%	0.27	OK	
	LC10 at 65.63%	0.06	OK	
	LC11 at 65.63%	0.07	OK	
	LC12 at 65.63%	0.06	OK	
	LC13 at 65.63%	0.01	OK	
	LC14 at 65.63%	0.00	OK	
	LC15 at 65.63%	0.01	OK	
	LC16 at 65.63%	0.01	OK	
	LC17 at 65.63%	0.04	OK	Sec. E1
	LC18 at 65.63%	0.04	OK	
	LC19 at 65.63%	0.04	OK	
	LC2 at 65.63%	0.21	OK	
	LC20 at 65.63%	0.04	OK	
	LC21 at 65.63%	0.02	OK	
	LC22 at 65.63%	0.02	OK	
	LC23 at 65.63%	0.02	OK	
	LC24 at 65.63%	0.02	OK	
	LC25 at 65.63%	0.02	OK	
	LC26 at 65.63%	0.02	OK	
	LC27 at 65.63%	0.02	OK	
	LC28 at 65.63%	0.02	OK	
	LC29 at 65.63%	0.02	OK	
	LC3 at 65.63%	0.27	OK	Eq. H1-1b
	LC30 at 65.63%	0.02	OK	
	LC31 at 65.63%	0.02	OK	
	LC32 at 65.63%	0.02	OK	
	LC4 at 65.63%	0.21	OK	
	LC5 at 65.63%	0.27	OK	
	LC6 at 65.63%	0.21	OK	
	LC7 at 65.63%	0.27	OK	
	LC8 at 65.63%	0.21	OK	
	LC9 at 65.63%	0.07	OK	
	W180 at 65.63%	0.17	OK	
	W210 at 65.63%	0.13	OK	
	Wi180 at 65.63%	0.07	OK	
	Wi210 at 65.63%	0.06	OK	
	WL180 at 65.63%	0.02	OK	
	WL210 at 65.63%	0.01	OK	



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Geometry data

GLOSSARY	
Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	ঃ Rigid end offset distance measured from J node in axis Z
DKX	Rigid end offset distance measured from K node in axis X
DKY	Rigid end offset distance measured from K node in axis Y
DKZ	∷ Rigid end offset distance measured from K node in axis Z
dL	Tapered member section depth at K end of member
lg factor	Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	Translation in X
TY	Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
18	-0.0012	0.00	- 	0
19	0.0036	0.00	-0.8677	0
24	-0.7533	0.00	0.4307	0
26	-6.3318	0.00	3.657	0
28	0.7497	0.00	0.437	0
30	6.333	0.00	3.655	0
32	2.3449	0.00	1.3564	0
41	-2.3472	0.00	1.3525	0
47	0.0022	0.00	-2.709	0
48	6.1665	0.00	3.3666	0
49	4.1665	0.00	-0.0975	0
50	2.1665	0.00	-3.5616	0
51	0.1665	0.00	-7.0257	0
52	6.3942	0.00	3.2351	0
53	4.3942	0.00	-0.229	0
54	2.3942	0.00	-3.6931	0
55	0.3942	0.00	-7.1572	0
56	0.3942	4.00	-7.1572	0
57	2.3942	4.00	-3.6931	0
58	4.3942	4.00	-0.229	0
59	6.3942	4.00	3.2351	0

60	6.3942	-2.00	3.2351	0
62	4.3942	-2.00	-0.229	0
63	2.3942	-2.00	-3.6931	0
64	0.3942	-2.00	-7.1572	0
81	-0.1677	0.00	-7.0237	0
82	-2.3954	0.00	-3.691	0
83	-4.3954	0.00	-0.2269	0
84	-0.3954	4.00	-7.1551	0
85	-0.3954	-2.00	-7.1551	0
86	-0.3954	0.00	-7.1551	0
87	-2.3954	4.00	-3.691	0
88	-2.3954	-2.00	-3.691	0
89	-2.1677	0.00	-3.5596	0
90	-4.1677	0.00	-0.0954	0
91	-4.3954	4.00	-0.2269	0
92	-4.3954	-2.00	-0.2269	0
93	-6.1677	0.00	3.3687	0
94	-6.3954	0.00	3.2372	0
95	-6.3954	4.00	3.2372	0
96	-6.3954	-2.00	3.2372	0
102	-5.9988	0.00	3.657	0
103	-1.9988	0.00	3.92	0
104	2.0012	0.00	3.92	0
105	-5.9988	4.00	3.92	0
106	-5.9988	-2.00	3.92	0
107	-5.9988	0.00	3.92	0
108	-1.9988	4.00	3.92	0
109	-1.9988	-2.00	3.92	0
110	-1.9988	0.00	3.657	0
111	2.0012	0.00	3.657	0
112	2.0012	4.00	3.92	0
113	2.0012	-2.00	3.92	0
114	6.0012	0.00	3.657	0
115	6.0012	0.00	3.92	0
116	6.0012	4.00	3.92	0
117	6.0012	-2.00	3.92	0
118	-7.6309	0.00	4.407	0
121	7.632	0.00	4.405	0
122	-0.0012	0.00	-8.812	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
19	1	1	1		1	1
24	1	1	1	1	1	1
28	1	1	1	1	1	1

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	lg factor
43	91	92		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
27	58	62		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
13	24	41		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
14	28	32		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
15	19	47		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
19	18	30		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
20	26	30		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
21	26	18		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
26	59	60		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
29	56	64		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
38	84	85		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
40	87	88		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
45	95	96		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
28	57	63		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
46	105	106		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
48	108	109		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
51	112	113		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
60	41	118		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
61	47	122		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
62	121	32		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
53	116	117		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

Orientation of local axes

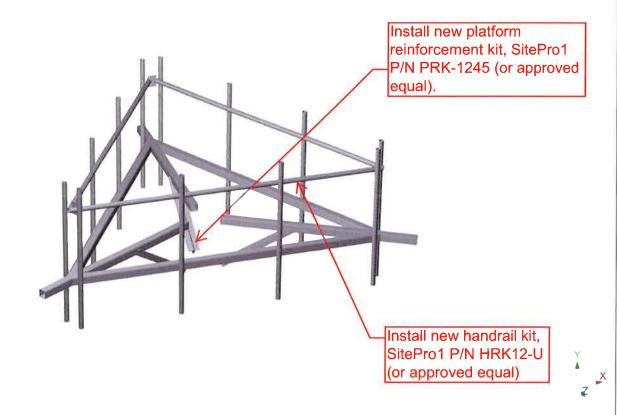
flember	Rotation [Deg]	Axes23	NX	NY	NZ
.3	0.00	2	-0.50	0.00	0.866
7	0.00	2	-0.50	0.00	-0.866
6	0.00	2	-0.50	0.00	-0.866
1	0.00	2	-0.50	0.00	-0.866
	0.00	2	-0.50	0.00	0.866
)	0.00	2	-0.50	0.00	0.866
5	0.00	2	-0.50	0.00	0.866
}	0.00	2	-0.50	0.00	-0.866



Mount Calculations (Proposed Conditions)

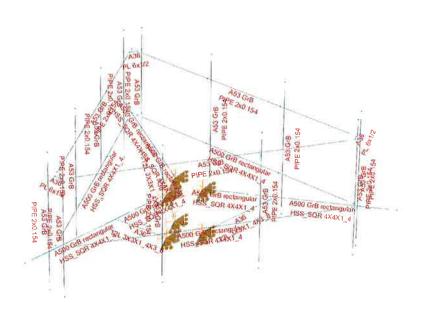


Current Date: 6/20/2018 3:12 PM
Units system: English
File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1029\LTE 4C-5C\CT1029 (LTE 4C-5C) (Mod.).etz\





Current Date: 6/20/2018 3:19 PM
Units system: English
File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1029\LTE 4C-5C\CT1029 (LTE 4C-5C) (Mo



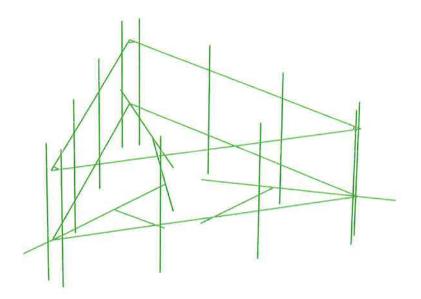




Current Date: 6/20/2018 3:19 PM
Units system: English
File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1029\LTE 4C-5C\CT1029 (LTE 4C-5C) (Mo



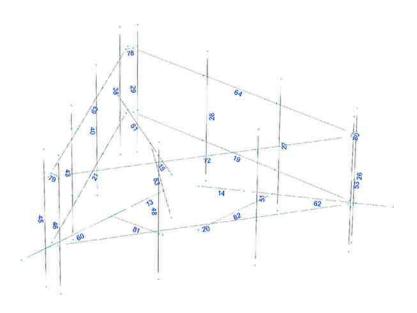








Current Date: 6/20/2018 3:19 PM
Units system: English
File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1029\LTE 4C-5C\CT1029 (LTE 4C-5C) (Mo







Current Date: 6/20/2018 3:19 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1029\LTE 4C-5C\CT1029 (LTE 4C-50)

(Mod.).etz\

Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design ;

W180=-W0

W210=-W30

Wi180=-Wi0

Wi210=-Wi30

WL180=-WL0

WL210=-WL30

LC1=1.2DL+1.6W0

LC2=1.2DL+1.6W30

LC3=1.2DL-1.6W0

LC4=1.2DL-1.6W30

LC5=0.9DL+1.6W0

LC6=0.9DL+1.6W30

LC7=0.9DL-1.6W0

LC8=0.9DL-1.6W30

LC9=1.2DL+Di+Wi0

LC10=1.2DL+Di+Wi30

LC11=1.2DL+Di-Wi0

LC12=1.2DL+Di-Wi30

LC13=1.2DL

LC14=0.9DL

LC15=1.2DL+1.6LL1

LC16=1.2DL+1.6LL2

LC17=1.2DL+WL0+LLa1

LC18=1.2DL+WL30+LLa1

LC19=1.2DL-WL0+LLa1

LC20=1.2DL-WL30+LLa1 LC21=1.2DL+WL0+LLa2

LC22=1.2DL+WL30+LLa2

LC23=1.2DL-WL0+LLa2

LC24=1.2DL-WL30+LLa2

LC25=1.2DL+WL0+LLa3

LC26=1.2DL+WL30+LLa3

LC27=1.2DL-WL0+LLa3

LC28=1.2DL-WL30+LLa3

LC29=1.2DL+WL0+LLa4

LC30=1.2DL+WL30+LLa4

LC31=1.2DL-WL0+LLa4 LC32=1.2DL-WL30+LLa4

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
*******************	HSS_SQR 4X4X1_4	13	LC1 at 0.00%	0.19	 OK	***************************************
			LC10 at 100.00%	0.20	OK	
			LC11 at 100.00%	0.20	OK	Eq. H1-1b
			LC12 at 100.00%	0.17	OK	
			LC13 at 100.00%	0.11	OK	
			LC14 at 100.00%	0.08	OK	
			LC15 at 100.00%	0.14	OK	
			LC16 at 100.00%	0.11	OK	
			LC17 at 100.00%	0.11	OK	
			LC18 at 100.00%	0.11	ОК	

	LC19 at 100.00%	0.11	OK	
	LC2 at 0.00%	0.18	OK	
	LC20 at 100.00%	0.11	OK	
	LC21 at 100.00%	0.12	OK	
	LC22 at 100.00%	0.13	OK	
	LC23 at 100.00%		OK	
		0.12		
	LC24 at 100.00%	0.12	OK	
	LC25 at 100.00%	0.14	OK	
	LC26 at 100.00%	0.14	OK	
	LC27 at 100.00%	0.14	OK	
	LC28 at 100.00%	0.13	OK	
	LC29 at 100.00%	0.16	OK	
	LC3 at 0.00%	0.23	OK	Eq. H1-1b
	LC30 at 100.00%	0.17	OK	
	LC31 at 100.00%	0.16	OK	
	LC32 at 100.00%	0.16	OK	
	LC4 at 0.00%	0.13	OK	
	LC5 at 0.00%	0.17	OK	
	LC6 at 0.00%	0.16	OK	
	LC7 at 0.00%	0.21	OK	
	LC8 at 0.00%	0.12	OK	
	LC9 at 100.00%	0.18	OK	
	W180 at 0.00%	0.09	OK	
	W210 at 0.00%	0.07	OK	
	Wi180 at 0.00%	0.04	OK	
	Wi210 at 0.00%	0.03	OK	
	WL180 at 0.00%	0.01	OK	
	WL210 at 0.00%		OK	
		0.01	OK	
14	LC1 at 0.00%	0.11	OK	
	LC10 at 100.00%	0.14	OK	
	LC11 at 100.00%	0.16	OK	
	LC12 at 100.00%	0.17	OK	
	LC13 at 100.00%	0.09	OK	
	LC14 at 100.00%	0.07	OK	
	LC15 at 100.00%	0.12	OK	
	LC16 at 100.00%	0.18	ОК	Eq. H1-1b
				Eq. 111-16
	LC17 at 100.00%	0.14	OK	
	LC18 at 100.00%	0.14	OK	
	LC19 at 100.00%	0.15	OK	
	LC2 at 0.00%	0.12	OK	
	LC20 at 100.00%	0.15	ОК	
	LC21 at 100.00%	0.12	OK	
	LC22 at 100.00%	0.12	OK	
	LC23 at 100.00%	0.13	OK	
	LC24 at 100.00%	0.13	OK	
	LC25 at 100.00%	0.10	OK	
	LC26 at 100.00%	0.10	OK	
	LC27 at 100.00%	0.11	OK	
	LC28 at 100.00%	0.11	OK	
	LC29 at 100.00%	0.09	OK	
	LC3 at 0.00%	0.15	OK	
	LC30 at 100.00%	0.09	OK	
	LC31 at 100.00%	0.10	OK	
	LC32 at 100.00%	0.10	OK	
	LC4 at 0.00%	0.17	OK	Eq. H1-1b
	LC5 at 0.00%	0.10	OK	— 1
	LC6 at 0.00%	0.11	OK	
	LC7 at 0.00%	0.13	OK	
	LC8 at 0.00%	0.16	OK	
	LC9 at 100.00%	0.15	OK	
	W180 at 0.00%	0.05	OK	
	W210 at 0.00%	0.07	OK	
	Wi180 at 100.00%	0.01	OK	

	Wi210 at 0.00% WL180 at 0.00%	0.03 0.00	OK OK	
	WL210 at 0.00%	0.01	OK 	***************************************
15	LC1 at 100.00%	0.16	OK	Eq. H1-1b
	LC10 at 100.00% LC11 at 100.00%	0.12	OK OK	
	LC12 at 100.00%	0.12 0.12	OK	
	LC13 at 100.00%	0.08	OK	
	LC14 at 100.00%	0.06	OK	
	LC15 at 100.00%	0.07	OK	
	LC16 at 100.00%	0.07	OK	
	LC17 at 100.00%	0.08	OK	
	LC18 at 100.00%	0.07	OK	
	LC19 at 100.00%	0.07	OK	E. 114.41
	LC2 at 0.00%	0.15	OK	Eq. H1-1b
	LC20 at 100.00% LC21 at 100.00%	0.07 0.08	OK OK	
	LC22 at 100.00%	0.07	OK	
	LC23 at 100.00%	0.07	OK	
	LC24 at 100.00%	0.07	OK	
	LC25 at 100.00%	0.08	OK	
	LC26 at 100.00%	0.07	OK	
	LC27 at 100.00%	0.07	OK	
	LC28 at 100.00%	0.07	OK	
	LC29 at 100.00%	80.0	OK	
	LC3 at 0.00%	0.08	OK	
	LC30 at 100.00% LC31 at 100.00%	0.07 0.07	OK OK	
	LC32 at 100.00%	0.07	OK	
	LC4 at 0.00%	0.15	OK	
	LC5 at 100.00%	0.14	OK	
	LC6 at 0.00%	0.14	OK	
	LC7 at 0.00%	0.07	OK	
	LC8 at 0.00%	0.14	OK	
	LC9 at 100.00%	0.14	OK	
	W180 at 100.00%	0.04	OK	Eq. H1-1b
	W210 at 0.00%	0.06	OK	
	Wi180 at 0.00% Wi210 at 0.00%	0.02	OK	
	WL180 at 100.00%	0.02 0.00	OK OK	
	WL210 at 0.00%	0.00	OK	
19	LC1 at 0.00%	0.28	OK	Eq. H1-1b
	LC10 at 100.00%	0.26	OK	
	LC11 at 100.00%	0.23	OK	
	LC12 at 100.00%	0.26	OK	
	LC13 at 100.00%	0.14	OK	
	LC14 at 100.00% LC15 at 100.00%	0.11 0.16	OK OK	
	LC16 at 100.00%	0.10	OK	
	LC17 at 100.00%	0.18	OK	
	LC18 at 100.00%	0.19	OK	
	LC19 at 100.00%	0.18	OK	
	LC2 at 100.00%	0.30	OK	
	LC20 at 100.00%	0.18	OK	
	LC21 at 100.00%	0.16	OK	
	LC22 at 100.00%	0.17	OK	
	LC23 at 100.00%	0.16	OK	
	LC24 at 100.00%	0.17	OK	
	LC25 at 100.00% LC26 at 100.00%	0.15 0.16	OK OK	
	LC27 at 100.00%	0.16	OK	
	LC28 at 100.00%	0.16	OK	
		-		

	LC29 at 100.00% LC3 at 0.00% LC30 at 100.00% LC31 at 100.00% LC32 at 100.00% LC5 at 0.00% LC6 at 100.00% LC7 at 0.00% LC8 at 100.00% V180 at 0.00% W180 at 0.00% W1210 at 100.00% WL180 at 0.00% WL180 at 0.00% WL210 at 100.00%	0.14 0.23 0.15 0.15 0.15 0.26 0.27 0.20 0.32 0.23 0.10 0.14 0.04 0.05 0.01	OK O	Eq. H1-1b
20	LC1 at 0.00% LC10 at 0.00% LC11 at 0.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC19 at 100.00% LC20 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00%	0.34 0.25 0.28 0.25 0.15 0.11 0.24 0.20 0.19 0.18 0.18 0.25 0.18 0.21 0.20 0.20 0.20 0.20 0.20 0.20 0.20	ОК ОК ОК ОК ОК ОК ОК ОК ОК ОК	Eq. H1-1b
21	LC1 at 100.00% LC10 at 0.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00%	0.27 0.28 0.25 0.28 0.16 0.12 0.17	OK OK OK OK OK OK OK	Eq. H1-1b

	LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC26 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 0.00% W1180 at 100.00% W1210 at 0.00%	0.16 0.16 0.16 0.16 0.17 0.17 0.18 0.17 0.18 0.19 0.19 0.22 0.20 0.20 0.20 0.20 0.22 0.24 0.33 0.18 0.28 0.25 0.09 0.13 0.03 0.05 0.01 0.01	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
60	LC1 at 75.00% LC10 at 75.00%	0.43 0.43	OK OK	
	LC11 at 75.00% LC12 at 75.00%	0.44 0.41	OK OK	
	LC13 at 75.00%	0.25	OK	
	LC14 at 75.00%	0.19	OK	
	LC15 at 75.00%	0.34	OK	
	LC16 at 75.00% LC17 at 75.00%	0.25 0.26	OK	
	LC 17 at 75.00%	0.20		
	LC18 at 75.00%		OK OK	
	LC18 at 75.00% LC19 at 75.00%	0.26 0.26	OK OK OK	
	LC19 at 75.00% LC2 at 75.00%	0.26 0.26 0.40	OK OK OK	
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00%	0.26 0.26 0.40 0.25	OK OK OK OK	
	LC19 at 75.00% LC2 at 75.00%	0.26 0.26 0.40	OK OK OK OK	
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00%	0.26 0.26 0.40 0.25 0.29	OK OK OK OK OK OK	
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29	OK OK OK OK OK OK OK	
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.29 0.32	OK OK OK OK OK OK OK OK	
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29	OK OK OK OK OK OK OK	
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.32 0.32 0.32	OK	
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC28 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.32 0.32 0.32 0.32 0.35	OK O	5 - 144.4h
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.32 0.32 0.32 0.35 0.46	OK O	Eq. H1-1b
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC28 at 75.00% LC29 at 20.83% LC3 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.32 0.32 0.32 0.32 0.35	OK O	Eq. H1-1b
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC28 at 75.00% LC29 at 20.83% LC3 at 75.00% LC30 at 20.83% LC31 at 20.83% LC31 at 20.83%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.32 0.32 0.32 0.35 0.46 0.35 0.34	OK O	Eq. H1-1b
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC26 at 75.00% LC26 at 75.00% LC29 at 20.83% LC3 at 20.83% LC31 at 20.83% LC32 at 20.83% LC32 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.32 0.32 0.32 0.35 0.46 0.35 0.34 0.34	OK O	Eq. H1-1b
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC28 at 75.00% LC29 at 20.83% LC3 at 75.00% LC30 at 20.83% LC31 at 20.83% LC31 at 20.83%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.32 0.32 0.32 0.35 0.46 0.35 0.34	OK O	Eq. H1-1b
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC26 at 75.00% LC27 at 75.00% LC28 at 75.00% LC29 at 20.83% LC3 at 75.00% LC30 at 20.83% LC31 at 20.83% LC31 at 20.83% LC32 at 75.00% LC35 at 75.00% LC30 at 75.00% LC30 at 75.00% LC30 at 75.00% LC30 at 20.83% LC31 at 20.83% LC32 at 75.00% LC32 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.32 0.32 0.32 0.35 0.46 0.35 0.34 0.34	OK O	Eq. H1-1b
	LC19 at 75.00% LC2 at 75.00% LC20 at 75.00% LC21 at 75.00% LC22 at 75.00% LC23 at 75.00% LC24 at 75.00% LC25 at 75.00% LC26 at 75.00% LC26 at 75.00% LC29 at 20.83% LC3 at 20.83% LC31 at 20.83% LC32 at 20.83% LC34 at 75.00% LC35 at 75.00% LC30 at 75.00% LC30 at 20.83% LC31 at 20.83% LC31 at 20.83% LC32 at 75.00% LC32 at 75.00% LC4 at 75.00% LC5 at 75.00% LC5 at 75.00%	0.26 0.26 0.40 0.25 0.29 0.29 0.29 0.32 0.32 0.32 0.35 0.46 0.35 0.34 0.34	OK O	Eq. H1-1b

	M(400 - 175 000/	0.44	01/	
	W180 at 75.00%	0.14	OK	
	W210 at 75.00%	0.10	OK	
	Wi180 at 75.00%	0.05	OK	
	Wi210 at 75.00%	0.04	OK	
	WL180 at 75.00%	0.01	OK	
	WL210 at 75.00%	0.01	OK	
			********	***************************************
61	LC1 at 20.83%	0.28	OK	
	LC10 at 75.00%	0.36	OK	
	LC11 at 75.00%	0.33	OK	
	LC12 at 75.00%	0.36	OK	
	LC13 at 75.00%	0.21	OK	
	LC14 at 75.00%	0.16	OK	
	LC15 at 75.00%	0.21	OK	
	LC16 at 75.00%	0.21	OK	
	LC17 at 75.00%	0.21	OK	
	LC18 at 75.00%	0.21	OK	
	LC19 at 75.00%	0.21	OK	
	LC2 at 75.00%	0.39	OK	
	LC20 at 75.00%	0.21	OK	
	LC21 at 75.00%	0.21	OK	
	LC22 at 75.00%	0.21	OK	
	LC23 at 75.00%	0.21	OK	
	LC24 at 75.00%	0.21	OK	
	LC25 at 75.00%	0.21	OK	
	LC26 at 75.00%	0.21	OK	
	LC27 at 75.00%	0.21	OK	
	LC28 at 75.00%	0.21	OK	
	LC29 at 75.00%	0.21	OK	
	LC3 at 75.00%	0.20	OK	
	LC30 at 75.00%	0.21	OK	
	LC31 at 75.00%	0.21	OK	
	LC32 at 75.00%	0.21	OK	
	LC4 at 75.00%	0.39	OK	Eq. H1-1b
	LC5 at 20.83%	0.24	OK	,
	LC6 at 75.00%	0.34	OK	
	LC7 at 75.00%	0.15	OK	
	LC8 at 75.00%	0.34	OK	
	LC9 at 75.00%	0.34	OK	
	W180 at 20.83%	0.07	OK	
	W210 at 75.00%	0.11	OK	
	Wi180 at 20.83%	0.02	OK	
	Wi210 at 75.00%	0.04	OK	
	WL180 at 20.83%	0.01	OK	
	WL210 at 75.00%	0.01	OK	
62	LC1 at 25.00%	0.37	OK	
	LC10 at 25.00%	0.38	OK	
	LC11 at 25.00%	0.39	OK	
	LC12 at 25.00%	0.39	OK	
	LC13 at 25.00%	0.23	OK	
	LC14 at 25.00%	0.17	OK	
	LC15 at 25.00%	0.31	OK	
	LC16 at 79.17%	0.38	OK	Eq. H1-1b
	LC17 at 79.17%	0.31	OK	•
	LC18 at 79.17%	0.31	OK	
	LC19 at 79.17%	0.31	OK	
	LC2 at 25.00%			
		0.33	OK	
	LC20 at 79.17%	0.32	OK	
	LC21 at 25.00%	0.30	OK	
	LC22 at 25.00%	0.30	OK	
	LC23 at 25.00%	0.30	OK	
	LC24 at 25.00%	0.30	OK	
	LC25 at 25.00%	0.26	OK	

		LC26 at 25.00%	0.26	OK	
		LC27 at 25.00%	0.27	OK	
		LC28 at 25.00%	0.27	OK	
		LC29 at 25.00%	0.23	OK	
					E~ U1 1h
		LC3 at 25.00%	0.39	OK	Eq. H1-1b
		LC30 at 25.00%	0.23	OK	
		LC31 at 25.00%	0.23	OK	
		LC32 at 25.00%	0.23	OK	
		LC4 at 25.00%	0.38	OK	
		LC5 at 25.00%	0.31	OK	
		LC6 at 25.00%	0.27	OK	
		LC7 at 25.00%	0.34	OK	
		LC8 at 25.00%	0.32	OK	
		LC9 at 25.00%	0.38	OK	
		W180 at 25.00%	0.11	OK	
		W210 at 25.00%	0.10	OK	
		Wi180 at 25.00%	0.03	OK	
		Wi210 at 25.00%	0.04	OK	
		WL180 at 25.00%	0.01	OK	
		WL210 at 25.00%	0.01	OK	

PIPE 2x0.154	26	LC1 at 66.67%	0.42	ОК	
		LC10 at 64.58%	0.24	OK	
		LC11 at 64.58%	0.14	OK	
		LC12 at 66.67%	0.13	OK	
		LC13 at 64.58%	0.08	OK	
		LC14 at 64.58%		OK	
			0.06		
		LC15 at 16.67%	0.06	OK	
		LC16 at 64.58%	0.18	OK	
		LC17 at 64.58%	0.14	OK	
		LC18 at 64.58%	0.16	OK	
		LC19 at 64.58%	0.12	OK	
		LC2 at 64.58%	0.57	OK	Eq. H1-1b
		LC20 at 64.58%	0.10	OK	
		LC21 at 64.58%	0.07	OK	
		LC22 at 64.58%	0.09	OK	
		LC23 at 64.58%	0.06	OK	
		LC24 at 16.67%	0.06	OK	
		LC25 at 64.58%	0.06	OK	
		LC26 at 64.58%	0.09	OK	
				OK	
		LC27 at 64.58%	0.05		
		LC28 at 16.67%	0.05	OK	
		LC29 at 64.58%	0.09	OK	
		LC3 at 66.67%	0.42	OK	
		LC30 at 64.58%	0.11	OK	
		LC31 at 64.58%	0.08	OK	
		LC32 at 64.58%	0.06	OK	
		LC4 at 66.67%	0.50	OK	Eq. H1-1b
		LC5 at 66.67%	0.42	OK	
		LC6 at 64.58%	0.55	OK	
		LC7 at 66.67%	0.42	OK	
		LC8 at 66.67%	0.50	ОК	
		LC9 at 64.58%	0.15	OK	
		W180 at 66.67%	0.16	OK	
		W210 at 64.58%	0.20	OK	
		Wi180 at 66.67%	0.32	OK	
		Wi210 at 66.67%	0.13	OK	
		WL180 at 66.67%	0.03	OK	
		WL210 at 66.67%	0.03	OK	
	29	LC1 at 64.58%	0.23	OK	
		LC10 at 64.58%	0.23	OK	
		LC11 at 64.58%	0.09	OK	
		LC11 at 64.58%	0.14	OK	
		LO 12 at 04.00%	0.00	OK	

	LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC19 at 64.58% LC2 at 64.58% LC20 at 64.58% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 64.58% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC27 at 64.58% LC28 at 64.58% LC29 at 64.58% LC29 at 64.58% LC30 at 64.58% LC30 at 64.58% LC30 at 64.58% LC30 at 64.58% LC31 at 64.58% LC31 at 64.58% LC32 at 64.58% LC31 at 64.58% LC32 at 64.58% LC31 at 64.58%	0.05 0.04 0.07 0.06 0.04 0.07 0.08 0.24 0.06 0.05 0.07 0.08 0.06 0.05 0.07 0.08 0.06 0.05 0.07 0.08 0.06 0.05 0.07 0.08 0.06 0.05 0.07 0.08 0.06 0.05 0.07 0.08 0.06 0.05 0.07 0.08 0.06 0.01	OK O	Eq. H1-1b
38	LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 64.58% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC18 at 64.58% LC19 at 64.58%	0.23 0.06 0.14 0.09 0.05 0.04 0.07 0.07 0.05 0.06 0.08 0.24	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 64.58% LC21 at 64.58% LC22 at 64.58% LC23 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC28 at 64.58% LC29 at 64.58% LC30 at 64.58% LC30 at 64.58% LC31 at 64.58% LC31 at 64.58% LC32 at 64.58% LC32 at 64.58% LC32 at 64.58% LC31 at 64.58% LC4 at 64.58% LC4 at 64.58% LC5 at 64.58%	0.07 0.05 0.06 0.08 0.07 0.05 0.06 0.08 0.07 0.04 0.31 0.05 0.07 0.07 0.24 0.24	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b

	LC7 at 64.58% LC8 at 64.58% LC9 at 22.92% W180 at 64.58% W210 at 64.58% Wi180 at 64.58% Wi210 at 64.58% WL180 at 64.58% WL210 at 64.58%	0.30 0.24 0.07 0.17 0.15 0.06 0.06 0.02	OK OK OK OK OK OK OK	
40	LC1 at 64.58% LC10 at 66.67% LC11 at 64.58% LC12 at 64.58% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC19 at 64.58% LC2 at 64.58% LC2 at 64.58% LC20 at 64.58% LC20 at 64.58% LC21 at 64.58% LC22 at 66.67% LC23 at 64.58% LC22 at 66.67% LC23 at 64.58% LC24 at 64.58% LC25 at 64.58% LC25 at 64.58% LC26 at 66.67% LC27 at 64.58% LC27 at 64.58% LC28 at 64.58% LC28 at 64.58% LC29 at 64.58%	0.53 0.13 0.13 0.23 0.06 0.05 0.04 0.07 0.07 0.04 0.06 0.51 0.10 0.06 0.04 0.05 0.09 0.05 0.04 0.05	OK O	
	LC3 at 64.58% LC30 at 66.67% LC31 at 64.58% LC32 at 64.58% LC4 at 64.58% LC5 at 64.58% LC6 at 64.58% LC7 at 64.58% LC9 at 64.58% W180 at 64.58% W210 at 64.58% Wi180 at 64.58% Wi210 at 64.58% WL210 at 64.58%	0.52 0.04 0.06 0.08 0.63 0.52 0.53 0.52 0.62 0.13 0.32 0.36 0.12 0.13 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
43	LC1 at 64.58% LC10 at 66.67% LC11 at 64.58% LC12 at 64.58% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC20 at 64.58% LC20 at 64.58% LC20 at 64.58% LC21 at 64.58%	0.46 0.15 0.23 0.16 0.07 0.05 0.07 0.08 0.05 0.06 0.10 0.64 0.09 0.04 0.07	OK OK OK OK OK OK OK OK OK OK	

	LC23 at 64.58% LC24 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC28 at 64.58% LC30 at 64.58% LC30 at 64.58% LC31 at 64.58% LC31 at 64.58% LC4 at 64.58% LC5 at 64.58% LC5 at 64.58% LC6 at 64.58% LC7 at 64.58% LC9 at 66.67% W180 at 64.58% W210 at 64.58% Wi180 at 64.58% Wi180 at 64.58% Wi180 at 64.58% W1180 at 64.58% W1180 at 64.58%	0.11 0.09 0.05 0.07 0.11 0.09 0.05 0.59 0.07 0.12 0.10 0.64 0.47 0.64 0.57 0.64 0.11 0.32 0.40 0.11 0.15 0.03 0.04	OK O	Eq. H1-1b
27	LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC2 at 64.58% LC2 at 64.58%	0.45 0.16 0.22 0.15 0.06 0.05 0.06 0.07 0.05 0.09 0.11 0.65	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC21 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC29 at 64.58% LC30 at 64.58% LC30 at 64.58% LC31 at 64.58% LC31 at 64.58% LC31 at 64.58% LC32 at 64.58% LC4 at 64.58% LC5 at 64.58% LC5 at 64.58% LC5 at 64.58% LC6 at 64.58% LC7 at 64.58% LC9 at 66.67% W180 at 64.58% W210 at 64.58% W1180 at 64.58%	0.04 0.08 0.10 0.06 0.04 0.08 0.10 0.06 0.04 0.57 0.08 0.09 0.05 0.64 0.47 0.65 0.55 0.64 0.11 0.32 0.40 0.12 0.15	OK O	
45	WL180 at 64.58% WL210 at 66.67% 	0.03 0.04 0.40	OK OK OK	

	EG 10 at 00.07 /0	0.15	OIL	
	LC11 at 64.58%	0.12	OK	
	LC12 at 64.58%	0.26	OK	
	LC13 at 64.58%	0.09	OK	
	LC14 at 64.58%	0.06	OK	
	LC15 at 16.67%	0.06	OK	
	LC16 at 64.58%	0.11	OK	
	LC17 at 64.58%	0.10	OK	
	LC18 at 64.58%	0.06	OK	
	LC19 at 64.58%	0.08	OK	
	LC2 at 66.67%	0.52	OK	Eq. H1-1b
	LC20 at 64.58%	0.12	OK	
	LC21 at 64.58%		ok	
		0.07		
	LC22 at 16.67%	0.05	OK	
	LC23 at 64.58%	0.06	OK	
	LC24 at 64.58%	0.09	OK	
	LC25 at 64.58%	0.07	OK	
	LC26 at 16.67%	0.06	OK	
	LC27 at 64.58%	0.06	OK	
	LC28 at 64.58%		OK	
		0.09		
	LC29 at 64.58%	0.15	OK	
	LC3 at 64.58%	0.41	OK	
	LC30 at 64.58%	0.11	OK	
	LC31 at 64.58%	0.13	OK	
	LC32 at 64.58%	0.17	OK	
	LC4 at 64.58%	0.59	OK	Eg. H1-1b
				Lq. 111-10
	LC5 at 66.67%	0.39	OK	
	LC6 at 66.67%	0.52	OK	
	LC7 at 64.58%	0.41	OK	
	LC8 at 64.58%	0.57	OK	
	LC9 at 64.58%	0.18	OK	
	W180 at 64.58%	0.25	OK	
	W210 at 66.67%	0.33	OK	
	**Z TO at 00.07 /0	0.00	OIL	
	M6400 -4 CC C70/	0.40		
	Wi180 at 66.67%	0.10	OK	
	Wi210 at 66.67%	0.10 0.13	OK OK	
	Wi210 at 66.67%	0.13	OK	
	Wi210 at 66.67% WL180 at 66.67%	0.13 0.02	OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67%	0.13 0.02 0.03	OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58%	0.13 0.02 0.03 	OK OK OK	······································
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% 	0.13 0.02 0.03 0.50 0.24	OK OK OK OK	 -
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67%	0.13 0.02 0.03 0.50 0.24 0.12	OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67%	0.13 0.02 0.03 0.50 0.24 0.12 0.13	OK OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06	OK OK OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67%	0.13 0.02 0.03 0.50 0.24 0.12 0.13	OK OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06	OK OK OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.04	OK OK OK OK OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC16 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.04	OK OK OK OK OK OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC16 at 64.58% LC16 at 64.58% LC17 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.04 0.05 0.05	OK OK OK OK OK OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.04 0.05 0.05 0.05	OK OK OK OK OK OK OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC17 at 64.58% LC19 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.04 0.05 0.05 0.08 0.05	OK OK OK OK OK OK OK OK OK OK OK OK	
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC17 at 64.58% LC18 at 64.58% LC19 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.04 0.05 0.05 0.05 0.08	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC17 at 64.58% LC19 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.04 0.05 0.05 0.08 0.05	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC17 at 64.58% LC18 at 64.58% LC19 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.04 0.05 0.05 0.05 0.08	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC16 at 64.58% LC16 at 64.58% LC17 at 64.58% LC17 at 64.58% LC19 at 64.58% LC10 at 64.58% LC20 at 66.67%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.04 0.05 0.05 0.08 0.05 0.05 0.05	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC10 at 64.58% LC20 at 64.58% LC20 at 66.67% LC21 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.08 0.05 0.08	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC16 at 64.58% LC17 at 64.58% LC17 at 64.58% LC18 at 64.58% LC19 at 64.58% LC19 at 64.58% LC2 at 64.58% LC20 at 64.58% LC21 at 64.58% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.64 0.03 0.05 0.08 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC16 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC10 at 64.58% LC10 at 64.58% LC10 at 64.58% LC10 at 64.58% LC2 at 64.58% LC2 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC22 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.64 0.03 0.05 0.08 0.05 0.08	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC19 at 64.58% LC2 at 64.58% LC2 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 66.67% LC25 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.03 0.05 0.08	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC16 at 64.58% LC19 at 64.58% LC2 at 64.58% LC2 at 64.58% LC2 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC16 at 64.58% LC19 at 64.58% LC19 at 64.58% LC2 at 64.58% LC2 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 66.67% LC25 at 64.58% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.09 0.09 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC16 at 64.58% LC19 at 64.58% LC2 at 64.58% LC2 at 64.58% LC2 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC16 at 64.58% LC19 at 64.58% LC19 at 64.58% LC2 at 64.58% LC2 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 66.67% LC25 at 64.58% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.09 0.09 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC2 at 64.58% LC2 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 66.67% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58% LC26 at 64.58% LC27 at 64.58% LC27 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.09 0.09 0.09 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC2 at 64.58% LC2 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 66.67% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC29 at 64.58% LC29 at 64.58% LC29 at 64.58% LC29 at 64.58% LC20 at 64.58% LC21 at 64.58% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC29 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.64 0.03 0.05 0.08 0.05 0.09 0.05 0.03 0.06 0.09	OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC21 at 64.58% LC22 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 66.67% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC29 at 64.58% LC29 at 64.58% LC29 at 64.58% LC20 at 64.58% LC21 at 64.58% LC20 at 64.58% LC21 at 64.58% LC20 at 64.58% LC21 at 64.58% LC20 at 64.58% LC20 at 64.58% LC30 at 64.58% LC30 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.64 0.03 0.05 0.08 0.05 0.09 0.05 0.03 0.06 0.09	OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC21 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 66.67% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC27 at 64.58% LC29 at 64.58% LC29 at 64.58% LC21 at 64.58% LC31 at 64.58% LC31 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.08 0.05 0.08 0.05 0.09 0.05 0.03 0.06 0.09 0.05 0.03 0.06 0.09 0.05	OK O	Eq. H1-1b
28	Wi210 at 66.67% WL180 at 66.67% WL210 at 66.67% LC1 at 64.58% LC10 at 64.58% LC11 at 64.58% LC12 at 66.67% LC13 at 64.58% LC14 at 64.58% LC15 at 64.58% LC16 at 64.58% LC17 at 64.58% LC19 at 64.58% LC21 at 64.58% LC22 at 64.58% LC20 at 66.67% LC21 at 64.58% LC22 at 64.58% LC22 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 66.67% LC25 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC29 at 64.58% LC29 at 64.58% LC29 at 64.58% LC20 at 64.58% LC21 at 64.58% LC20 at 64.58% LC21 at 64.58% LC20 at 64.58% LC21 at 64.58% LC20 at 64.58% LC20 at 64.58% LC30 at 64.58% LC30 at 64.58%	0.13 0.02 0.03 0.50 0.24 0.12 0.13 0.06 0.04 0.05 0.05 0.08 0.05 0.64 0.03 0.05 0.08 0.05 0.09 0.05 0.03 0.06 0.09	OK O	Eq. H1-1b

LC10 at 66.67% 0.13 OK

	LC4 at 64.58%	0.53	OK	
	LC5 at 64.58%	0.50	OK	
	LC6 at 64.58%	0.63	OK	
	LC7 at 64.58%	0.49	OK	
	LC8 at 64.58%	0.54	OK	
	LC9 at 64.58%	0.14	OK	Eq. H1-1b
	W180 at 64.58%	0.31	OK	·
	W210 at 64.58%	0.36	OK	
	Wi180 at 64.58%	0.12	OK	
	Wi210 at 64.58%	0.13	OK	
	WL180 at 64.58%	0.03	OK	
	WL210 at 64.58%	0.03	OK	

46	LC1 at 64.58%	0.44	OK	Eq. H1-1b
	LC10 at 64.58%	0.09	OK	
	LC11 at 66.67%	0.17	OK	
	LC12 at 64.58%	0.23	OK	
	LC13 at 64.58%	0.09	OK	
	LC14 at 64.58%	0.06	OK	
	LC15 at 64.58%	0.07	OK	
	LC16 at 64.58%	0.10	OK	
	LC17 at 64.58%	0.11	OK	
	LC18 at 64.58%	0.07	OK	
	LC19 at 64.58%	0.06	OK	
	LC2 at 64.58%	0.31	OK	
	LC20 at 64.58%	0.10	OK	
	LC21 at 64.58%	0.09	OK	
	LC22 at 64.58%	0.06	OK	
	LC23 at 64.58%	0.05	OK	
	LC24 at 64.58%	0.09	OK	
	LC25 at 64.58%	0.09	OK	
	LC26 at 64.58%	0.07	OK	
	LC27 at 64.58%	0.06	OK	
	LC28 at 64.58%	0.10	OK	
	LC29 at 64.58%	0.19	OK	
	LC3 at 66.67%	0.39	OK	
	LC30 at 64.58%	0.15	OK	
	LC31 at 64.58%	0.16	OK	
	LC32 at 64.58%	0.20	OK	
	LC4 at 64.58%	0.45	OK	Eq. H1-1b
	LC5 at 64.58%	0.42	OK	_ q , ,
	LC6 at 64.58%	0.31	OK	
	LC7 at 66.67%	0.39	OK	
	LC8 at 64.58%	0.42	OK	
	LC9 at 64.58%	0.25	OK	
	W180 at 66.67%	0.24	OK	
	W210 at 64.58%	0.22	OK	
	Wi180 at 66.67%	0.17	ОК	
	Wi210 at 64.58%	0.08	OK	
	WL180 at 66.67%	0.02	OK	
	WL210 at 64.58%	0.02	OK	

48	LC1 at 64.58%	0.56	OK	Eq. H1-1b
	LC10 at 64.58%	0.19	OK	
	LC11 at 66.67%	0.13	OK	
	LC12 at 64.58%	0.11	OK	
	LC13 at 64.58%	0.06	OK	
	LC14 at 64.58%	0.05	OK	
	LC15 at 64.58%	0.16	OK	
	LC16 at 64.58%	0.04	OK	
	LC17 at 64.58%	0.09	OK	
	LC18 at 64.58%	0.07	OK	
	LC19 at 64.58%	0.03	OK	
	LC2 at 64.58%	0.44	OK	

	LC20 at 64.58% LC21 at 64.58% LC22 at 64.58% LC23 at 64.58% LC24 at 64.58% LC25 at 64.58% LC26 at 64.58% LC27 at 64.58% LC29 at 64.58% LC3 at 66.67% LC30 at 64.58% LC31 at 64.58% LC31 at 64.58% LC4 at 64.58% LC5 at 64.58% LC4 at 64.58% LC5 at 64.58% LC5 at 64.58% LC7 at 66.67% LC8 at 64.58% LC9 at 64.58% W180 at 64.58% W1180 at 64.58%	0.04 0.13 0.12 0.07 0.07 0.15 0.14 0.07 0.10 0.09 0.53 0.08 0.03 0.05 0.37 0.55 0.42 0.53 0.36 0.21 0.33 0.24 0.12 0.09 0.03 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
51	LC1 at 64.58% LC10 at 64.58% LC11 at 66.67%	0.50 0.09 0.11	ок ок ок	Eq. H1-1b
	LC12 at 64.58%	0.19	OK	
	LC13 at 64.58%	0.06	OK	
	LC14 at 64.58%	0.04	OK	
	LC15 at 64.58%	0.16	OK	
	LC16 at 64.58%	0.07	OK	
	LC17 at 64.58%	0.09	OK	
	LC18 at 64.58%	0.05	OK	
	LC19 at 64.58%	0.03	OK OK	
	LC2 at 64.58% LC20 at 64.58%	0.36 0.08	OK OK	
	LC21 at 64.58%	0.00	OK	
	LC22 at 64.58%	0.10	OK	
	LC23 at 64.58%	0.07	OK	
	LC24 at 64.58%	0.14	OK	
	LC25 at 64.58%	0.13	OK	
	LC26 at 64.58% LC27 at 64.58%	0.07 0.07	OK OK	
	LC28 at 64.58%	0.07	OK	
	LC29 at 64.58%	0.08	OK	
	LC3 at 64.58%	0.47	OK	
	LC30 at 64.58%	0.04	OK	
	LC31 at 64.58%	0.03	OK	
	LC32 at 64.58% LC4 at 64.58%	0.07	OK OK	
	LC5 at 64.58%	0.44 0.49	OK	
	LC6 at 64.58%	0.36	OK	
	LC7 at 64.58%	0.47	OK	
	LC8 at 64.58%	0.43	OK	
	LC9 at 64.58%	0.20	OK	
	W180 at 64.58%	0.29	OK OK	
	W210 at 64.58% Wi180 at 66.67%	0.24 0.10	OK OK	
	Wi210 at 64.58%	0.10	OK	
	WL180 at 64.58%	0.03	OK	

	WL210 at 64.58%	0.02	OK	
53	LC1 at 64.58%	0.28	OK	WEST CONTROL OF THE STATE OF TH
55	LC10 at 64.58%	0.26	OK	
	LC11 at 25.00%	0.08	OK	
	LC12 at 50.00%	0.06	ok	
	LC13 at 64.58%	0.06	ОК	
	LC14 at 64.58%	0.05	ОК	
	LC15 at 16.67%	0.06	OK	
	LC16 at 64.58%	0.17	OK	
	LC17 at 64.58%	0.17	OK	
	LC18 at 64.58%	0.17	OK	
	LC19 at 64.58%	0.15	OK	
	LC2 at 64.58%	0.31	OK	Eq. H1-1b
	LC20 at 64.58%	0.14	OK	
	LC21 at 64.58%	0.07	OK	
	LC22 at 64.58%	0.07	OK	
	LC23 at 25.00%	0.04	OK	
	LC24 at 64.58%	0.06	OK	
	LC25 at 64.58%	0.06	OK	
	LC26 at 64.58%	0.06	OK	
	LC27 at 25.00%	0.04	OK	
	LC28 at 64.58%	0.04	OK	
	LC29 at 64.58%	0.08	OK	C- 114.45
	LC30 at 64.58%	0.20	OK	Eq. H1-1b
	LC30 at 64.58% LC31 at 64.58%	0.08	OK OK	
	LC31 at 64.58%	0.05 0.05	OK	
	LC4 at 64.58%	0.03	OK	
	LC5 at 64.58%	0.10	OK	
	LC6 at 64.58%	0.27	OK	
	LC7 at 16.67%	0.19	OK	
	LC8 at 64.58%	0.19	OK	
	LC9 at 64.58%	0.15	OK	
	W180 at 64.58%	0.14	OK	
	W210 at 64.58%	0.15	OK	
	Wi180 at 64.58%	0.05	OK	
	Wi210 at 64.58%	0.05	OK	
	WL180 at 64.58%	0.01	OK	
	WL210 at 64.58%	0.01	OK	
•	1.04 . 1.00 0.504			•40-0000-00000-00000-00000-000-001-001-00
63	LC1 at 96.25%	0.31	OK	Eq. H1-1b
	LC10 at 3.75%	0.10	OK	
	LC11 at 3.75%	0.10	OK	
	LC12 at 96.25%	0.07	OK	
	LC13 at 66.25% LC14 at 66.25%	0.04 0.03	OK OK	
	LC15 at 3.75%	0.03	OK	
	LC16 at 66.25%	0.03	OK	
	LC17 at 96.25%	0.05	OK	
	LC18 at 3.75%	0.05	OK	
	LC19 at 3.75%	0.05	OK	
	LC2 at 3.75%	0.32	OK	Eg. H1-1b
	LC20 at 96.25%	0.04	OK	Eq. 111 15
	LC21 at 66.25%	0.04	OK	
	LC22 at 3.75%	0.06	OK	
	LC23 at 3.75%	0.05	OK	
	LC24 at 66.25%	0.03	OK	
	LC25 at 66.25%	0.03	OK	
	LC26 at 3.75%	0.05	OK	
	LC27 at 3.75%	0.05	OK	
	LC28 at 2.50%	0.03	OK	
	LC29 at 96.25%	0.04	OK	
	LC3 at 3.75%	0.31	OK	

	LC30 at 2.50% LC31 at 2.50% LC32 at 2.50% LC4 at 3.75% LC5 at 96.25% LC6 at 3.75% LC7 at 3.75% LC9 at 96.25% W180 at 3.75% W210 at 3.75% Wi180 at 96.25% Wi210 at 3.75% WL210 at 3.75% WL210 at 3.75%	0.05 0.05 0.03 0.26 0.30 0.31 0.30 0.27 0.11 0.17 0.18 0.06 0.06 0.02	OK OK OK OK OK OK OK OK OK OK	
64	LC1 at 3.75% LC10 at 3.75% LC11 at 96.25% LC12 at 96.25% LC13 at 3.75% LC14 at 3.75% LC15 at 96.25% LC16 at 97.50% LC17 at 3.75% LC19 at 97.50% LC2 at 96.25% LC20 at 97.50% LC21 at 97.50% LC22 at 97.50% LC22 at 97.50% LC22 at 97.50% LC23 at 96.25% LC24 at 97.50% LC25 at 3.75% LC26 at 3.75% LC26 at 3.75% LC27 at 96.25% LC29 at 3.75% LC29 at 3.75% LC3 at 96.25% LC30 at 3.75% LC4 at 96.25% LC30 at 3.75% LC3 at 96.25% LC30 at 3.75% LC31 at 96.25% LC30 at 3.75% LC31 at 96.25% LC31 at 96.25% LC32 at 66.25% LC31 at 96.25%	0.31 0.07 0.09 0.10 0.03 0.03 0.03 0.07 0.04 0.03 0.04 0.04 0.03 0.04 0.05 0.04 0.05 0.05 0.05 0.05 0.05	OK O O O O O O O O O O O O O O O O O O	Eq. H1-1b
72	WL210 at 96.25%	0.02 0.21 0.11 0.08 0.11 0.03 0.02 0.25 0.08 0.04	OK	Eq. H1-1b

		LC18 at 96.25%	0.05	OK	
		LC19 at 96,25%	0.05	OK	
		LC2 at 3.75%	0.37	OK	Eq. H1-1b
		LC20 at 97.50%	0.04	OK	'
		LC21 at 66.25%	0.09	ОК	
		LC22 at 66.25%	0.09	ОК	
		LC23 at 66.25%	0.10	OK	
		LC24 at 66.25%	0.10	OK OK	
		LC25 at 33.75%	0.08	OK	
		LC26 at 33.75%	0.10	OK	
		LC27 at 33.75%	0.11	OK	
		LC28 at 33.75%	0.09	OK	
		LC29 at 3.75%	0.04	OK	
		LC3 at 33.75%	0.23	OK	Eq. H1-1b
		LC30 at 2.50%	0.05	OK	
		LC31 at 3.75%	0.05	ОК	
		LC32 at 3.75%	0.05	OK	
		LC4 at 96.25%	0.36	OK	Eq. H1-1b
		LC5 at 33.75%	0.21	OK	Eq. 111-10
		LC6 at 3.75%	0.37	OK	
		LC7 at 33.75%	0.23	OK	
		LC8 at 96.25%	0.35	OK	
		LC9 at 26.25%	0.03	OK	
		W180 at 33.75%	0.14	OK	
		W210 at 3.75%	0.23	OK	
		Wi180 at 33.75%	0.05	OK	
		Wi210 at 3.75%	0.07	OK	
		WL180 at 33.75%	0.01	OK	
		WL210 at 3.75%	0.02	ОК	
PL 6x1/2	78	LC1 at 100.00%	0.05	ОК	Eq. H1-1b
					•
		LC10 at 0.00%	0.01	OK	
		LC10 at 0.00% LC11 at 0.00%	0.01 0.00	OK OK	
		LC11 at 0.00%	0.00	OK	
		LC11 at 0.00% LC12 at 0.00%	0.00 0.01	OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00%	0.00 0.01 0.01	OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00%	0.00 0.01 0.01 0.00	OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00%	0.00 0.01 0.01 0.00 0.00	OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01	OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01	OK OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01	OK OK OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK OK OK OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01	OK OK OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK OK OK OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.04 0.01 0.01 0.01 0.01	OK OK OK OK OK OK OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.04 0.01 0.01 0.01 0.01 0.01	OK OK OK OK OK OK OK OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	OK OK OK OK OK OK OK OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC25 at 0.00% LC24 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	OK OK OK OK OK OK OK OK OK OK OK OK OK	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.00 0.01 0.01 0.01	OK O	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 0.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.00 0.01 0.01 0.01	OK O	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC29 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	OK O	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	OK O	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	OK O	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC21 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	OK O	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	OK O	
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC21 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	OK O	Eq. H3-1
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	OK O	Eq. H3-1
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK O	Eq. H3-1
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 100.00% LC30 at 100.00% LC31 at 0.00% LC31 at 0.00% LC32 at 100.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK O	Eq. H3-1
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 100.00% LC30 at 100.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 100.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC4 at 0.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00% LC6 at 0.00% LC7 at 100.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK O	Eq. H3-1
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 100.00% LC30 at 100.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 100.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC4 at 0.00% LC5 at 100.00% LC5 at 100.00% LC6 at 0.00% LC7 at 100.00% LC8 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK O	Eq. H3-1
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC4 at 0.00% LC5 at 100.00% LC5 at 100.00% LC6 at 0.00% LC7 at 100.00% LC9 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK O	Eq. H3-1
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 100.00% LC30 at 100.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC4 at 0.00% LC5 at 100.00% LC5 at 100.00% LC6 at 0.00% LC7 at 100.00% LC9 at 0.00% LC9 at 0.00% LC9 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK O	Eq. H3-1
		LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC24 at 100.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC4 at 0.00% LC5 at 100.00% LC5 at 100.00% LC6 at 0.00% LC7 at 100.00% LC9 at 0.00%	0.00 0.01 0.01 0.00 0.00 0.01 0.01 0.01	OK O	Eq. H3-1

	Wi180 at 0.00% Wi210 at 0.00% WL180 at 100.00% WL210 at 0.00%	0.01 0.01 0.00 0.00	OK OK OK	
79	LC1 at 100.00%	0.05	OK	
	LC10 at 0.00%	0.02	OK	
	LC11 at 100.00%	0.02	OK	
	LC12 at 0.00% LC13 at 100.00%	0.01	OK OK	
	LC14 at 100.00%	0.01 0.00	OK OK	
	LC15 at 0.00%	0.01	OK	
	LC16 at 100.00%	0.01	ОК	
	LC17 at 100.00%	0.01	OK	
	LC18 at 100.00%	0.01	OK	
	LC19 at 100.00%	0.01	OK	
	LC2 at 0.00%	0.06	OK	Eq. H1-1b
	LC20 at 0.00%	0.01	OK	
	LC21 at 0.00% LC22 at 0.00%	0.01 0.01	OK OK	
	LC22 at 0.00 %	0.01	OK OK	
	LC24 at 0.00%	0.01	ok	
	LC25 at 0.00%	0.01	OK	
	LC26 at 0.00%	0.01	OK	
	LC27 at 0.00%	0.01	OK	
	LC28 at 0.00%	0.01	OK	
	LC29 at 100.00%	0.01	OK	=
	LC3 at 100.00%	0.06	OK	Eq. H1-1b
	LC30 at 100.00% LC31 at 0.00%	0.01 0.01	OK OK	
	LC31 at 0.00%	0.01	OK	
	LC4 at 0.00%	0.05	OK	
	LC5 at 100.00%	0.05	OK	
	LC6 at 0.00%	0.06	OK	
	LC7 at 100.00%	0.06	OK	
	LC8 at 0.00%	0.05	OK	
	LC9 at 100.00%	0.01	OK	
	W180 at 100.00%	0.03	OK	
	W210 at 0.00% Wi180 at 100.00%	0.03 0.01	OK OK	
	Wi210 at 0.00%	0.01	OK	
	WL180 at 100.00%	0.00	OK	
	WL210 at 0.00%	0.00	OK	
80	LC1 at 100.00%	0.03	OK	
	LC10 at 100.00%	0.01	OK	
	LC11 at 0.00%	0.02	OK	
	LC12 at 0.00%	0.02	OK	
	LC13 at 0.00% LC14 at 0.00%	0.01 0.00	OK OK	
	LC15 at 100.00%	0.00	OK OK	
	LC16 at 0.00%	0.02	OK	
	LC17 at 0.00%	0.01	OK	
	LC18 at 100.00%	0.01	OK	
	LC19 at 100.00%	0.01	OK	
	LC2 at 100.00%	0.05	OK	
	LC20 at 0.00%	0.01	OK	
	LC21 at 100.00%	0.01	OK	
	LC22 at 100.00% LC23 at 100.00%	0.01 0.01	OK OK	
	LC24 at 100.00%	0.01	OK	
	LC25 at 100.00%	0.01	OK	
	LC26 at 100.00%	0.00	OK	
	LC27 at 100.00%	0.01	OK	

		LC28 at 100.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 100.00% LC5 at 0.00% LC6 at 100.00% LC7 at 0.00% LC8 at 100.00% V180 at 100.00% Wi180 at 0.00% Wi210 at 100.00% WL180 at 0.00% WL210 at 100.00%	0.01 0.04 0.01 0.01 0.01 0.06 0.03 0.05 0.04 0.06 0.01 0.02 0.04 0.01 0.01 0.01 0.00	OK O	Eq. H1-1b
T2L 3X3X1_4X3_8	81	LC1 at 100.00% LC10 at 100.00%	0.38 0.66	ОК ОК	Eq. H2-1
		LC11 at 100.00%	0.66	OK	
		LC12 at 100.00%	0.63	OK	
		LC13 at 100.00%	0.40	OK	
		LC14 at 100.00%	0.30	OK	
		LC15 at 100.00%	0.52	OK	
		LC16 at 100.00% LC17 at 100.00%	0.40 0.40	OK OK	
		LC18 at 100.00%	0.40	OK	
		LC19 at 100.00%	0.41	OK	
		LC2 at 100.00%	0.53	OK	
		LC20 at 100.00%	0.40	OK	
		LC21 at 100.00%	0.44	OK	
		LC22 at 100.00%	0.45	OK	
		LC23 at 100.00%	0.46	OK	
		LC24 at 100.00%	0.45	ОК	
		LC25 at 100.00%	0.50	OK	
		LC26 at 100.00%	0.51	OK	
		LC27 at 100.00%	0.52	OK	
		LC28 at 100.00%	0.51	OK	
		LC29 at 100.00%	0.57	OK	
		LC3 at 100.00%	0.50	OK	
		LC30 at 100.00%	0.58	OK	
		LC31 at 100.00%	0.58	OK	
		LC32 at 100.00%	0.57	OK	
		LC4 at 100.00% LC5 at 100.00%	0.32 0.28	OK OK	
		LC6 at 100.00%	0.43	OK	
		LC7 at 100.00%	0.40	OK	
		LC8 at 100.00%	0.22	OK	
		LC9 at 100.00%	0.64	OK	
		W180 at 0.00%	0.08	OK	
		W210 at 0.00%	0.06	OK	
		Wi180 at 0.00%	0.03	OK	
		Wi210 at 0.00%	0.02	OK	
		WL180 at 0.00% WL210 at 0.00%	0.01 0.01	OK OK	
	20	***************************************	**********		***************************************
	82	LC1 at 100.00%	0.31	OK	
		LC10 at 100.00%	0.53	OK	
		LC11 at 100.00%	0.56	OK	
		LC12 at 100.00% LC13 at 100.00%	0.57	OK OK	
		LC13 at 100.00%	0.35 0.26	OK OK	
		LO 17 at 100.00 /0	0.40		

	LC15 at 100.00%	0.46	OK	
	LC16 at 100.00%	0.62	OK	Eg. H2-1
	LC17 at 100.00%	0.51	OK	-
	LC18 at 100.00%	0.52	OK	
	LC19 at 100.00%	0.52	OK	
	LC2 at 100.00%	0.26	OK	
	LC20 at 100.00%	0.52	OK	
	LC21 at 100.00%	0.45	OK	
	LC22 at 100.00%	0.45	OK	
	LC23 at 100.00%	0.46	OK	
	LC24 at 100.00%	0.46	OK	
	LC25 at 100.00%	0.39	OK	
	LC26 at 100.00%	0.39	OK	
	LC27 at 100.00%	0.40	OK	
	LC28 at 100.00%	0.40	OK	
	LC29 at 100.00%	0.34	OK	
	LC3 at 100.00%		ok	
		0.43		
	LC30 at 100.00%	0.34	OK	
	LC31 at 100.00%	0.35	OK	
	LC32 at 100.00%	0.35	OK	
	LC4 at 100.00%	0.48	OK	
	LC5 at 100.00%	0.22	OK	
	LC6 at 100.00%	0.17	OK	
	LC7 at 100.00%	0.34	OK	
	LC8 at 100.00%	0.39	OK	
	LC9 at 100.00%	0.54	OK	
	W180 at 100.00%	0.05	OK	
	W210 at 100.00%	0.09	OK	
	Wi180 at 100.00%	0.01	OK	
	Wi210 at 100.00%	0.03	OK	
	WL180 at 100.00%	0.00	OK	
	WL210 at 100.00%	0.01	OK	
	SAMARANA MARANA MAR			
83	LC1 at 100.00%	0.41	OK	
83	LC1 at 100.00% LC10 at 100.00%	0.41 0.46	OK OK	
83	LC10 at 100.00%	0.46	OK	
83	LC10 at 100.00% LC11 at 100.00%	0.46 0.43	OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00%	0.46 0.43 0.45	OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00%	0.46 0.43 0.45 0.29	OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00%	0.46 0.43 0.45 0.29 0.22	OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27	OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00%	0.46 0.43 0.45 0.29 0.22	OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27	OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27	OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28	OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26	OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26 0.33	OK OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26 0.33 0.27	OK OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26 0.33 0.27 0.28	OK OK OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC2 at 100.00% LC22 at 100.00% LC22 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27	OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC2 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27	OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.26 0.27	OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC23 at 100.00% LC23 at 100.00% LC25 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27	OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.26 0.27	OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC23 at 100.00% LC23 at 100.00% LC25 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.26 0.27	OK OK OK OK OK OK OK OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.26 0.27	OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.27 0.26 0.27 0.28 0.27 0.28 0.27	OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.26 0.27 0.28 0.27	OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.28 0.27 0.29 0.17	OK	
83	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC30 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.28 0.27 0.29 0.17 0.28	OK O	
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83	LC10 at 100.00% LC11 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.28 0.27 0.28 0.27 0.28 0.27 0.28 0.28 0.27 0.29 0.17 0.28 0.28 0.28	OK O O O O O O O O O O O O O O O O O O	
83	LC10 at 100.00% LC11 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.28 0.27 0.28 0.27 0.28 0.28 0.27 0.29 0.17 0.28 0.28 0.28 0.28 0.28 0.28 0.28	OK O O O O O O O O O O O O O O O O O O	
83	LC10 at 100.00% LC11 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.28 0.27 0.28 0.27 0.28 0.27 0.28 0.28 0.27 0.29 0.17 0.28 0.28 0.28 0.32 0.34	OK O O O O O O O O O O O O O O O O O O	
83	LC10 at 100.00% LC11 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC16 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.28 0.27 0.28 0.27 0.28 0.28 0.27 0.29 0.17 0.28 0.28 0.29 0.17 0.28 0.28 0.29 0.17 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28	OK O O O O O O O O O O O O O O O O O O	
83	LC10 at 100.00% LC11 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.28 0.27 0.28 0.27 0.28 0.27 0.28 0.28 0.27 0.29 0.17 0.28 0.28 0.28 0.32 0.34	OK O O O O O O O O O O O O O O O O O O	
83	LC10 at 100.00% LC11 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC16 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00%	0.46 0.43 0.45 0.29 0.22 0.27 0.28 0.28 0.27 0.26 0.33 0.27 0.28 0.27 0.28 0.27 0.28 0.27 0.28 0.28 0.27 0.29 0.17 0.28 0.28 0.29 0.17 0.28 0.28 0.29 0.17 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28	OK O O O O O O O O O O O O O O O O O O	

LC9 at 100.00%	0.48	ок	Eq. H2-1
W180 at 0.00%	0.06	OK	
W210 at 0.00%	0.04	OK	
Wi180 at 0.00%	0.02	OK	
Wi210 at 100.00%	0.01	OK	
WL180 at 0.00%	0.01	OK	
WL210 at 100.00%	0.00	OK	



Current Date: 6/20/2018 3:19 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1029\LTE 4C-5C\CT1029 (LTE 4C-5I

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Geometry data

GLOSSARY	
Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	; Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	Rigid end offset distance measured from K node in axis Z
dL	Tapered member section depth at K end of member
lg factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	Effective length factor about axis 2
K33	Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	# Member length for calculation of axial capacity
LB pos	Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	Rotation about X
RY	Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	Translation in X
TY	Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor	
18	-0.0012	0.00	-7.312	0	
19	0.0036	0.00	-0.8677	0	
24	-0.7533	0.00	0.4307	0	
26	-6.3318	0.00	3.657	0	
28	0.7497	0.00	0.437	0	
30	6.333	0.00	3.655	0	
32	2.3449	0.00	1.3564	0	
41	-2.3472	0.00	1.3525	0	
47	0.0022	0.00	-2.709	0	
48	6.1665	0.00	3.3666	0	
49	4.1665	0.00	-0.0975	0	
50	2.1665	0.00	-3.5616	0	
51	0.1665	0.00	-7.0257	0	
52	6.3942	0.00	3.2351	0	
53	4.3942	0.00	-0.229	0	
54	2.3942	0.00	-3.6931	0	
55	0.3942	0.00	-7.1572	0	
56	0.3942	4.00	-7.1572	0	
57	2.3942	4.00	-3.6931	0	
58	4.3942	4.00	-0.229	0	
59	6.3942	4.00	3.2351	0	

60	6.3942	-2.00	3.2351	0
62	4.3942	-2.00	-0.229	0
63	2.3942	-2.00	-3.6931	0
64	0.3942	-2.00	-7.1572	0
81	-0.1677	0.00	-7.0237	0
82	-2.3954	0.00	-3.691	0
83	-4.3954	0.00	-0.2269	0
84	-0.3954	4.00	-7.1551	
85	-0.3954	-2.00	-7.1551	0
86	-0.3954	0.00	-7.1551	0
87	-2.3954	4.00	-3.691	0
88	-2.3954	-2.00	-3.691	0
89	-2.1677	0.00	-3.5596	0
90	-4.1677	0.00	-0.0954	0
91	-4.3954	4.00	-0.2269	0
92	-4.3954	-2.00	-0.2269	0
93	-6.1677	0.00	3.3687	0
94	-6.3954	0.00	3.2372	0
95	-6.3954	4.00	3.2372	0
96	-6.3954	-2.00	3.2372	0
102	-5.9988	0.00	3.657	0
103	-1.9988	0.00	3.92	0
104	2.0012	0.00	3.92	0
105	-5.9988	4.00	3.92	0
106 107	-5.9988 -5.9988	-2.00	3.92	0
107	-1.9988	0.00	3.92 3.92	0
109	-1.9988	4.00 -2.00		0
110	-1.9988	0.00	3.92 3.657	0
111	2.0012	0.00	3.657	0
112	2.0012	4.00	3.92	0
113	2.0012	-2.00	3.92	0
114	6.0012	0.00	3.657	0
115	6.0012	0.00	3.92	0
116	6.0012	4.00	3.92	ő
117	6.0012	-2.00	3.92	Ö
118	-7.6309	0.00	4.407	0
121	7.632	0.00	4.405	0
122	-0.0012	0.00	-8.812	0
123	0.1665	3.00	-7.0257	0
124	0.3942	3.00	-7.1572	0
125	2.1665	3.00	-3.5616	0
126	2.3942	3.00	-3.6931	0
127	-0.1677	3.00	-7.0237	0
128	-0.3954	3.00	-7.1551	. 0
129	-2.3954	3.00	-3.691	0
130	-2.1677	3.00	-3.5596	0
131	-4.3954	3.00	-0.2269	0
132	-4.1677	3.00	-0.0954	0
133	-6.1677	3.00	3.3687	0
134	-6.3954	3.00	3.2372	0
135	-5.9988	3.00	3.657	0
136	-5.9988	3.00	3.92	0
137	-1.9988	3.00	3.92	0
138	-1.9988	3.00	3.657	0
139	2.0012	3.00	3.92	0
140	2.0012	3.00	3.657	0
141	6.333	3.00	3.655	0
142	6.0012	3.00	3.657	0
143	6.0012	3.00	3.92	0

144	6.1665	3.00	3.3666	0
145	6.3942	3.00	3.2351	0
146	4.1665	3.00	-0.0975	0
147	4.3942	3.00	-0.229	0
148	-6.3318	3.00	3.657	0
149	-0.0012	3.00	-7.312	0
150	-3.3433	0.00	1.9287	0
151	0.0014	0.00	-3.8597	0
152	3.3419	0.00	1.9311	0
153	-0.7533	-2.00	0.4307	0
154	0.7497	-2.00	0.437	0
155	0.0036	-2.00	-0.8677	0
100000000000000000000000000000000000000				

Restraints

Node	TX	TY	TZ	RX	RY	RZ
19	1	1	1	1	1	1
24	1	-14	1	1	1	1
28	1	4	1	1	1	1
153	1	1	1	1	1	1
154	1	1	1	1	1	1
155	1	1	1	1	1	1

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
13	24	41		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
14	28	32		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
15	19	47		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
19	18	30		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
20	26	30		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
21	26	18		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
26	59	60		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
29	56	64		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
38	84	85		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
40	87	88		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
43	91	92		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
27	58	62		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
45	95	96		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
28	57	63		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
46	105	106		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
48	108	109		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
51	112	113		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
53	116	117		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
60	41	118		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
61	47	122		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
62	121	32		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
63	148	149		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
64	149	141		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
72	148	141		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

78	127	123	PL 6x1/2	A36	0.00	0.00	0.00
79	133	135	PL 6x1/2	A36	0.00	0.00	0.00
80	142	144	PL 6x1/2	A36	0.00	0.00	0.00
81	153	150	T2L 3X3X1_4X3_8	A36	0.00	0.00	0.00
82	154	152	T2L 3X3X1_4X3_8	A36	0.00	0.00	0.00
83	155	151	T2L 3X3X1_4X3_8	A36	0.00	0.00	0.00

Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ	
26	0.00	2	-0.50	0.00	-0.866	
29	0.00	2	-0.50	0.00	-0.866	
38	0.00	2	-0.50	0.00	0.866	
40	0.00	2	-0.50	0.00	0.866	
43	0.00	2	-0.50	0.00	0.866	
27	0.00	2	-0.50	0.00	-0.866	
45	0.00	2	-0.50	0.00	0.866	
28	0.00	2	-0.50	0.00	-0.866	

Plainville, CT: Assessor Database

Property Search:

Parcel ID:	Alternate ID:	Owner 1 Name:	Street Number:	Street Name:
				∨

Search Reset

Property Detail:

Parcel ID:	Alternate ID/Map Block Lot:	Card:	Card:	Street Name:	Street Number:	Zoning:	LUC:	Acres:
42-A-03	R05380	1	1	S WASHINGTON ST	335	RI	Manufacturing Warehouse Facilities	8.00

Owner Information:

Owner 1 Name:	DISPLAY PROPERTIES LLC
Owner 2 Name:	
Street 1:	335 S WASHINGTON ST
Street 2:	
City:	PLAINVILLE
State:	СТ
Zip:	06062
Volume:	374
Page:	357
Deed Date:	0000-00-00

Building Information:

Building Number:	1
Units:	1
Structure Type:	WAREHOUSE
Grade:	B-
Identical Units:	1
Year Built:	1989

Valuation:

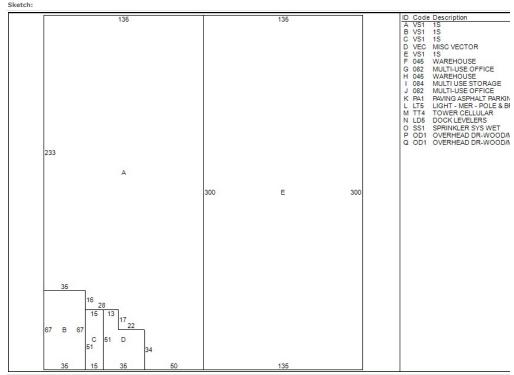
Appraised Land:	\$467,600.00
Appraised Bldg:	\$3,284,900.00
Appraised Total:	\$3,752,500.00
Total Assessment:	\$2,626,750,00

Property Images:

Picture:

There is no picture available.

Sketch:



Sales History:

Book:	Page:	Sale Date:	Price:	Validity:	Sale Type:
374	357	03/27/2001	1,953,261	В	2
130	418	05/07/1963			
261	271	09/14/1988			
261	313	09/14/1988			
374	357	03/27/2001			

Out-Buildings:

Code:	Description:	Units:	Year Built:	Size1:	Size2:	Area:	Grade:	Condition:
PA1	PAVING ASPHALT PARKING	1	1989	1	9200	9200	С	NORMAL (Comm)
LT5	LIGHT - MER - POLE & BRK	4	2006	0	0	1	С	NORMAL (Comm)
TT4	TOWER CELLULAR	1	2000	1	120	120	С	NORMAL (Comm)

Building Interior/Exterior Information:

Floor From:	Floor To:	Area:	Use Type:	Exterior Walls:	Contruction Type:	Heating:	A/C:	Plumbing:	Functional Uti
01	01	34279	WAREHOUSE	METAL, SANDWICH	FIRE RESISTANT	UNIT HEATERS	NONE	NORMAL	3
01	01	7584	MULTI-USE OFFICE	METAL, SANDWICH	FIRE RESISTANT	HOT AIR	CENTRAL	NORMAL	2
M1	M1	2179	MULTI USE STORAGE	METAL, SANDWICH	FIRE RESISTANT	HOT AIR	NONE	NONE	3
M2	M2	429	MULTI-USE OFFICE	METAL, SANDWICH	FIRE RESISTANT	HOT AIR	CENTRAL	NORMAL	3
01	01	39140	WAREHOUSE	METAL, SANDWICH	FIRE RESISTANT	UNIT HEATERS	NONE	NORMAL	3

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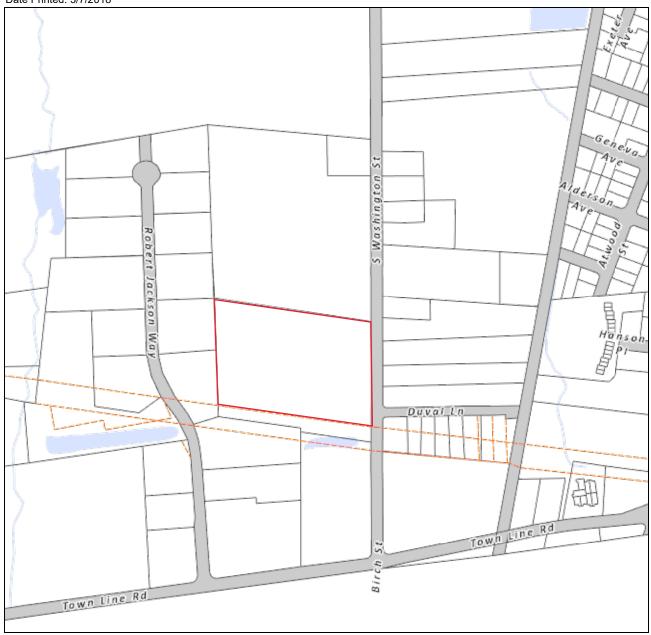
Tue. March 13, 2018: 07:44 AM: 0.16s: 10mb

Town of Plainville

Geographic Information System (GIS)

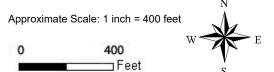


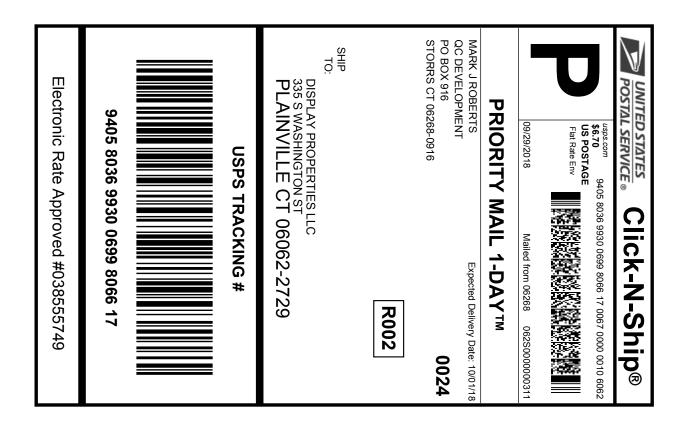
Date Printed: 3/7/2018



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Cut on dotted line.

Instructions

- 1. Each Click-N-Ship® label is unique. Labels are to be used as printed and used only once. DO NOT PHOTO **COPY OR ALTER LABEL.**
- 2. Place your label so it does not wrap around the edge of the package.
- 3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
- 4. To mail your package with PC Postage®, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office™, or drop in a USPS collection box.
- 5. Mail your package on the "Ship Date" you selected when creating this label.

Click-N-Ship® Label Record

USPS TRACKING # / Insurance Number: 9405 8036 9930 0699 8066 17

Trans. #: 445153041 Print Date: 09/28/2018 Ship Date: 09/29/2018 Expected Delivery Date: Insured Value: 10/01/2018 Priority Mail® Postage: \$6.70 Insurance Fee \$0.00 Total \$6.70

From: MARK J ROBERTS

> QC DEVELOPMENT PO BOX 916

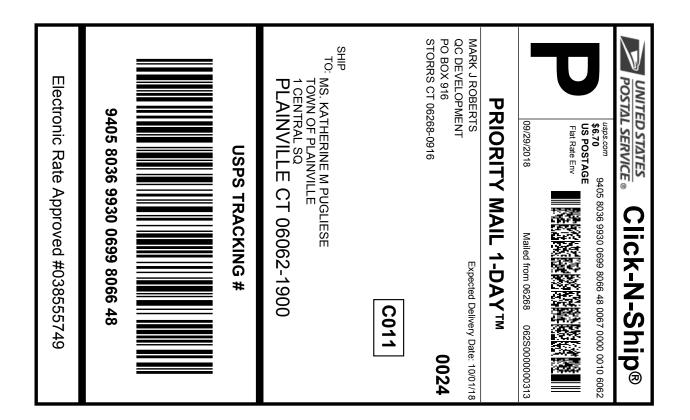
\$50.00

STORRS CT 06268-0916

DISPLAY PROPERTIES LLC

335 S WASHINGTON ST PLAINVILLE CT 06062-2729

Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date.





Cut on dotted line.

Instructions

- 1. Each Click-N-Ship® label is unique. Labels are to be used as printed and used only once. DO NOT PHOTO **COPY OR ALTER LABEL.**
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- 5. Mail your package on the "Ship Date" you selected when creating this label.

Click-N-Ship® Label Record

USPS TRACKING # / Insurance Number: 9405 8036 9930 0699 8066 48

Trans. #: 445153041 Print Date: 09/28/2018 Ship Date: 09/29/2018 Expected Delivery Date: Insured Value: 10/01/2018 Priority Mail® Postage: Insurance Fee \$0.00 Total \$6.70

From: MARK J ROBERTS

QC DEVELOPMENT

\$50.00

PO BOX 916

STORRS CT 06268-0916

MS. KATHERINE M PUGLIESE

TOWN OF PLAINVILLE 1 CENTRAL SQ

PLAINVILLE CT 06062-1900

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