



# STATE OF CONNECTICUT

## CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

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[www.ct.gov/csc](http://www.ct.gov/csc)

### VIA ELECTRONIC MAIL

April 5, 2018

Mark Roberts  
QC Development  
PO Box 916  
Storrs, CT 06268

RE: **EM-CING-110-180326** - New Cingular Wireless PCS, LLC notice of intent to modify an existing telecommunications facility located at 335 South Washington Street, Plainville, Connecticut.

Dear Mr. Roberts:

The Connecticut Siting Council (Council) is in receipt of your correspondence of April 5, 2018 submitted in response to the Council's April 4, 2018 notification of an incomplete request for exempt modification with regard to the above-referenced matter.

The submission renders the request for exempt modification complete and the Council will process the request in accordance with the Federal Communications Commission 60-day timeframe.

Thank you for your attention and cooperation.

Sincerely,

Melanie A. Bachman  
Executive Director

MB/CMW/cg



**From:** Mark Roberts [mailto:mark.roberts@qcdevelopment.net]  
**Sent:** Thursday, April 05, 2018 11:36 AM  
**To:** Galligan, Coleen  
**Cc:** CSC-DL Siting Council  
**Subject:** RE: Incomplete - EM-CING-110-180326 - South Washington St.

Hello Coleen – thanks for your inquiry regarding this filing. The note refers to a separate analysis that was performed on the antenna mount itself, which I have attached for your reference.

Please let me know if you have any further questions.

Thanks

Mark Roberts  
QC Development  
860-670-9068

**From:** Galligan, Coleen <[Coleen.Galligan@ct.gov](mailto:Coleen.Galligan@ct.gov)>  
**Sent:** Thursday, April 5, 2018 11:22 AM  
**To:** Mark Roberts <[mark.roberts@qcdevelopment.net](mailto:mark.roberts@qcdevelopment.net)>  
**Cc:** CSC-DL Siting Council <[Siting.Council@ct.gov](mailto:Siting.Council@ct.gov)>  
**Subject:** Incomplete - EM-CING-110-180326 - South Washington St.



March 27, 2018



SAI Communications  
12 Industrial Way  
Salem NH, 03079

RE:      Site Number:            CT1029 (LTE 3C)  
           FA Number:            10105805  
           PACE Number:          MRCTB027294  
           PTN Number:            2051A0EK6W  
           Site Name:                Plainville South Washington Street  
           Site Address:            335 South Washington Street  
    Plainville, CT 06062

To Whom It May Concern:

Hudson Design Group LLC (HDG) has been authorized by SAI Communications to perform a mount analysis on the existing AT&T antenna mount to determine its capability of supporting the following equipment loading:

- (3) 7770 Antennas (55.0"x11.0"x5.0" – Wt. = 35 lbs. /each)
- (3) HPA-65R-BUU-H6 Antennas (72.0"x14.8"x9.0" – Wt. = 51 lbs. /each)
- (3) RRUS-11 RRH's (19.7"x17.0"x7.2" –Wt. = 51 lbs. /each)
- (6) LGP21401 TMA's (14.4"x9"x2.7" – Wt. = 19 lbs. /each)
- (1) Squid Surge Arrestor (24.0"x9.7"Ø – Wt. = 33 lbs. /each)
- **(3) QS66512-2 Antennas (72"x12"x9.6" – Wt. = 111 lbs. /each)**
- **(3) RRUS-32 RRH's (27.2"x12.1"x7.0" – Wt. = 60 lbs. /each)**
- **(3) RRUS-32 B2 RRH's (27.2"x12.1"x7.0" – Wt. = 60 lbs. /each)**
- **(6) DBC0061D1V51-2 Diplexers (8"x6.2"x6.5" – Wt. = 26 lbs. /each)**
- **(1) Squid Surge Arrestor (24.0"x9.7"Ø – Wt. = 33 lbs. /each)**

*\*Proposed Loading Shown in Bold.*

No original structural design documents or fabrication drawings were available for the existing mounts. HDG's sub-consultant, ProVertic LLC, conducted a mapping of the existing AT&T antenna mount on January 28, 2018.

Based on our analysis, we have determined that the existing antenna mount **IS CAPABLE** of supporting the proposed antenna installation.

	Member(s)	Controlling Load Case	Stress Ratio	Pass/Fail
<b>Existing 3C Configuration Mount Rating</b>	77	LC4	77%	<b>PASS</b>

This analysis was conducted in accordance with EIA/TIA-222-G, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and the International Building Code 2012 with 2005 Connecticut Supplement with 2016 Amendments. (See the attached analysis).

**Reference Documents:**

Mount Mapping Report prepared by ProVertic LLC dated March 23, 2018.

**This determination was based on the following limitations and assumptions:**

1. HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
4. The existing mount has been adequately secured to the tower structure per the mount manufacturer's specifications.
5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
6. HDG performed a localized analysis on the mount itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted,  
Hudson Design Group LLC

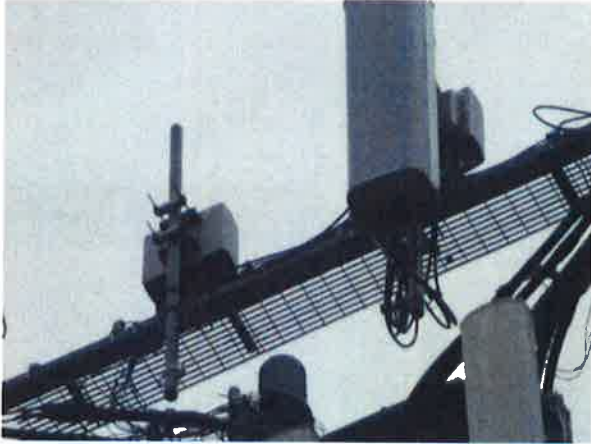


Michael Cabral  
Structural Dept. Head

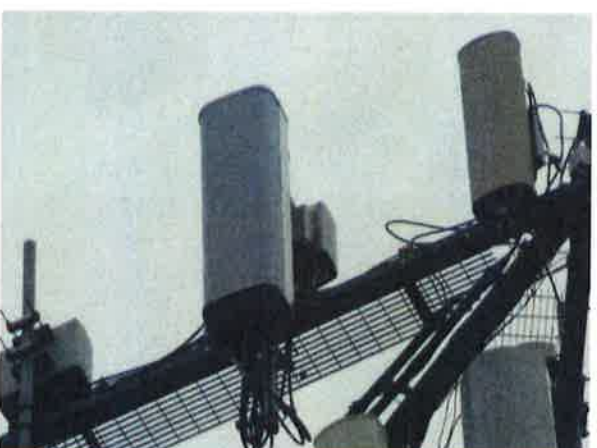
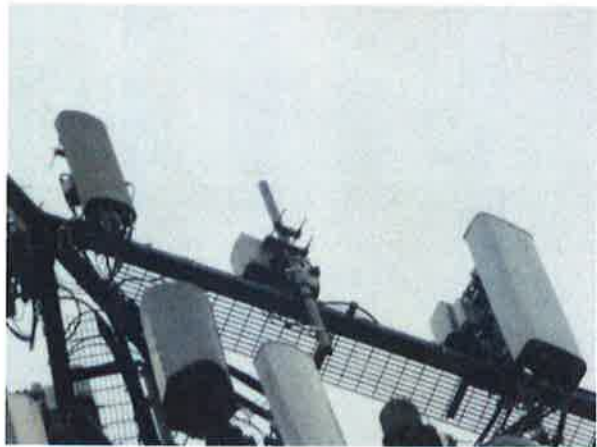


Daniel P. Hamm, PE  
Principal

**FIELD PHOTOS:**









**HUDSON**  
Design Group LLC

## Wind & Ice Calculations

Date: 3/27/2018  
 Project Name: Plainville South Washington Street  
 Project Number: CT1029  
 Designed By: LN      Checked By: MSC



**2.6.5.2 Velocity Pressure Coeff:**

$$K_z = 2.01 (z/z_g)^{2/\alpha}$$

$z = 122 \text{ (ft)}$   
 $z_g = 1200 \text{ (ft)}$   
 $\alpha = 7.0$

**$K_z = 1.046$**

$K_{zmin} \leq K_z \leq 2.01$

**Table 2-4**

Exposure	$Z_g$	$\alpha$	$K_{zmin}$	$K_e$
B	1200 ft	7.0	0.70	0.9
C	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

**2.6.6.4 Topographic Factor:**

**Table 2-5**

Topo. Category	$K_t$	$f$
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} = [1 + (K_e K_t / K_h)]^2$$

$$K_h = e^{-(f \cdot z / H)}$$

**$K_{zt} = \text{\#DIV/0!}$**

$K_h = \text{\#DIV/0!}$

*(If Category 1 then  $K_{zt} = 1.0$ )*

$K_e = 0$  (from Table 2-4)

$K_t = 0$  (from Table 2-5)

$f = 0$  (from Table 2-5)

$z = 122$

$H = 0$  (Ht. of the crest above surrounding terrain)

$K_{zt} = 1.00$

Categor	<b>1</b>
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Date: 3/27/2018  
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**2.6.7 Gust Effect Factor**

2.6.7.1 Self Supporting Lattice Structures

Gh = 1.0 Latticed Structures > 600 ft

Gh = 0.85 Latticed Structures 450 ft or less

Gh = 0.85 + 0.15 [h/150 - 3.0]      h= ht. of structure

h= 121      Gh= 0.85

2.6.7.2 Guyed Masts      Gh= 0.85

2.6.7.3 Pole Structures      Gh= 1.1

2.6.9 Appurtenances      Gh= 1.0

2.6.7.4 Structures Supported on Other Structures

(Cantilivered tubular or latticed spines, pole, structures on buildings (ht. : width ratio > 5)

Gh= 1.35      Gh= 1.00

**2.6.9.2 Design Wind Force on Appurtenances**

$F = q_z * Gh * (EPA)_A$

$q_z = 0.00256 * K_z * K_{zt} * K_d * V_{max}^2 * I$

**q<sub>z</sub> = 28.05**

**q<sub>z (ice)</sub> = 6.36**

K<sub>z</sub> = 1.046

K<sub>zt</sub> = 1.0

K<sub>d</sub> = 0.95

V<sub>max</sub> = 105

V<sub>max (ice)</sub> = 50

I = 1.0

Table 2-2

Structure Type	Wind Direction Probability Factor, Kd
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95

**Determine Ca:**

**Table 2-8**

Force Coefficients (Ca) for Appurtenances				
Member Type		Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
		Ca	Ca	Ca
Flat		1.2	1.4	2.0
Round	C < 32 (Subcritical)	0.7	0.8	1.2
	32 ≤ C ≤ 64 (Transitional)	$3.76/(C^{0.485})$	$3.37/(C^{0.415})$	$38.4/(C^{1.0})$
	C > 64 (Supercritical)	0.5	0.6	0.6

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.  
 (Aspect ratio is independent of the spacing between support points of a linear appurtenance,  
 Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness = 1.00 in      Angle = 0 (deg)      Equivalent Angle = 180 (deg)

Appurtenances	Height	Width	Depth	Flat Area	Aspect Ratio	Ca	Force (lbs)	Force (lbs) (w/ Ice)
7770 Antenna	55.0	11.0	5.0	4.20	5.00	1.31	154	43
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.86	1.31	271	72
QS66512-2 Antenna	72.0	12.0	9.6	6.00	6.00	1.36	228	62
RRUS-11 RRH	19.7	17.0	7.2	2.33	1.16	1.20	78	22
RRUS-11 RRH (Shielded)	19.7	6.0	7.2	0.82	3.28	1.23	28	9
RRUS-32 RRH	27.2	12.1	7.0	2.29	2.25	1.20	77	22
RRUS-32 RRH (Shielded)	27.2	1.1	7.0	0.21	24.73	1.99	12	8
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	2.25	1.20	77	22
RRUS-32 B2 RRH (Shielded)	27.2	1.1	7.0	0.21	24.73	1.99	12	8
LGP21401 TMA	14.4	9.0	2.7	0.90	1.60	1.20	30	10
LGP21401 TMA (Shielded)	14.4	0.0	2.7	0.00	0.00	1.20	0	2
DBC0061D1V51-2 Diplexer	8.0	6.2	6.5	0.34	1.29	1.20	12	4
Squid Surge Arrestor	24.0	9.7	9.7	1.62	2.47	1.20	54	16
4"x4"x1/4" HSS	4.0	12.0	4.0	0.33	0.33	1.20	11	4
2" pipe	2.4	12.0	0.0	0.20	0.20	0.70	4	2

Date: 3/27/2018  
 Project Name: Plainville South Washington Street  
 Project Number: CT1029  
 Designed By: LN Checked By: MSC



**WIND LOADS**

Angle = 30 (deg)      Ice Thickness = 1.00 in.      Equivalent Angle = 210 (deg)

**WIND LOADS WITH NO ICE:**

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Aspect Ratio	Aspect Ratio	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	136
HPA-65R-BUU-H6 Anter	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	271	181	248
QS66512-2 Antenna	72.0	12.0	9.6	6.00	4.80	6.00	7.50	1.36	1.42	228	191	219
RRUS-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21	78	33	67
RRUS-11 RRH (Shielded)	19.7	8.5	7.2	1.16	0.99	2.32	2.74	1.20	1.21	39	33	38
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	69
RRUS-32 RRH (Shielded)	27.2	6.1	7.0	1.14	1.32	4.50	3.89	1.29	1.26	41	47	43
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	69
RRUS-32 B2 RRH (Shielded)	27.2	6.1	7.0	1.14	1.32	4.50	3.89	1.29	1.26	41	47	43
LGP21401 TMA	14.4	9.0	2.7	0.90	0.27	1.60	5.33	1.20	1.33	30	10	25
LGP21401 TMA (Shielded)	14.4	4.5	2.7	0.45	0.27	3.20	5.33	1.23	1.33	16	10	14
DBC0061D1V51-2 Dipole	8.0	6.2	6.5	0.34	0.36	1.29	1.23	1.20	1.20	12	12	12
Squid Surge Arrestor	24.0	9.7	9.7	1.62	1.62	2.47	2.47	1.20	1.20	54	54	54

**WIND LOADS WITH ICE:**

7770 Antenna	57.0	13.0	7.0	5.15	2.77	4.38	8.14	1.28	1.44	42	25	38
HPA-65R-BUU-H6 Anter	74.0	16.8	11.0	8.63	5.65	4.40	6.73	1.28	1.39	71	50	65
QS66512-2 Antenna	74.0	14.0	11.6	7.19	5.96	5.29	6.38	1.32	1.37	61	52	58
RRUS-11 RRH	21.7	19.0	9.2	2.86	1.39	1.14	2.36	1.20	1.20	22	11	19
RRUS-11 RRH (Shielded)	21.7	9.5	9.2	1.43	1.39	2.28	2.36	1.20	1.20	11	11	11
RRUS-32 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	20
RRUS-32 RRH (Shielded)	29.2	7.1	9.0	1.43	1.83	4.14	3.24	1.27	1.23	12	14	12
RRUS-32 B2 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	20
RRUS-32 B2 RRH (Shielded)	29.2	7.1	9.0	1.43	1.83	4.14	3.24	1.27	1.23	12	14	12
LGP21401 TMA	16.4	11.0	4.7	1.25	0.54	1.49	3.49	1.20	1.24	10	4	8
LGP21401 TMA (Shielded)	16.4	5.5	4.7	0.63	0.54	2.98	3.49	1.22	1.24	5	4	5
DBC0061D1V51-2 Dipole	10.0	8.2	8.5	0.57	0.59	1.22	1.18	1.20	1.20	4	5	4
Squid Surge Arrestor	26.0	11.7	11.7	2.11	2.11	2.22	2.22	1.20	1.20	16	16	16

Date: 3/27/2018  
 Project Name: Plainville South Washington Street  
 Project Number: CT1029  
 Designed By: LN Checked By: MSC



**WIND LOADS**

Angle = 60 (deg) Ice Thickness = 1.00 in. Equivalent Angle = 240 (deg)

**WIND LOADS WITH NO ICE:**

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	100
HPA-65R-BUU-H6 Ante	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	271	181	203
QS66512-2 Antenna	72.0	12.0	9.6	6.00	4.80	6.00	7.50	1.36	1.42	228	191	200
RRUS-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21	78	33	45
RRUS-11 RRH (Shielded)	19.7	12.8	7.2	1.74	0.99	1.55	2.74	1.20	1.21	59	33	40
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	54
RRUS-32 RRH (Shielded)	27.2	9.1	7.0	1.71	1.32	3.00	3.89	1.22	1.26	59	47	50
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	54
RRUS-32 B2 RRH (Shielded)	27.2	9.1	7.0	1.71	1.32	3.00	3.89	1.22	1.26	59	47	50
LGP21401 TMA	14.4	9.0	2.7	0.90	0.27	1.60	5.33	1.20	1.33	30	10	15
LGP21401 TMA (Shielded)	14.4	6.8	2.7	0.68	0.27	2.13	5.33	1.20	1.33	23	10	13
DBC0061D1V51-2 Dipole	8.0	6.2	6.5	0.34	0.36	1.29	1.23	1.20	1.20	12	12	12
Squid Surge Arrestor	24.0	9.7	9.7	1.62	1.62	2.47	2.47	1.20	1.20	54	54	54

**WIND LOADS WITH ICE:**

7770 Antenna	57.0	13.0	7.0	5.15	2.77	4.38	8.14	1.28	1.44	42	25	30
HPA-65R-BUU-H6 Ante	74.0	16.8	11.0	8.63	5.65	4.40	6.73	1.28	1.39	71	50	55
QS66512-2 Antenna	74.0	14.0	11.6	7.19	5.96	5.29	6.38	1.32	1.37	61	52	54
RRUS-11 RRH	21.7	19.0	9.2	2.86	1.39	1.14	2.36	1.20	1.20	22	11	13
RRUS-11 RRH (Shielded)	21.7	14.3	9.2	2.15	1.39	1.52	2.36	1.20	1.20	16	11	12
RRUS-32 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	16
RRUS-32 RRH (Shielded)	29.2	10.6	9.0	2.14	1.83	2.76	3.24	1.21	1.23	17	14	15
RRUS-32 B2 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	16
RRUS-32 B2 RRH (Shielded)	29.2	10.6	9.0	2.14	1.83	2.76	3.24	1.21	1.23	17	14	15
LGP21401 TMA	16.4	11.0	4.7	1.25	0.54	1.49	3.49	1.20	1.24	10	4	6
LGP21401 TMA (Shielded)	16.4	8.3	4.7	0.94	0.54	1.99	3.49	1.20	1.24	7	4	5
DBC0061D1V51-2 Dipole	10.0	8.2	8.5	0.57	0.59	1.22	1.18	1.20	1.20	4	5	4
Squid Surge Arrestor	26.0	11.7	11.7	2.11	2.11	2.22	2.22	1.20	1.20	16	16	16

Date: 3/27/2018  
 Project Name: Plainville South Washington Street  
 Project Number: CT1029  
 Designed By: LN Checked By: MSC



**WIND LOADS**

Angle = 90 (deg)      Ice Thickness = 1.00 in.      Equivalent Angle = 270 (deg)

**WIND LOADS WITH NO ICE:**

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	82
HPA-65R-BUU-H6 Ante	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	271	181	181
QS66512-2 Antenna	72.0	12.0	9.6	6.00	4.80	6.00	7.50	1.36	1.42	228	191	191
RRUS-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21	78	33	33
RRUS-11 RRH (Shieldec	19.7	6.0	7.2	0.82	0.99	3.28	2.74	1.23	1.21	28	33	33
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	47
RRUS-32 RRH (Shieldec	27.2	1.1	7.0	0.21	1.32	24.73	3.89	1.99	1.26	12	47	47
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	47
RRUS-32 B2 RRH (Shiel	27.2	1.1	7.0	0.21	1.32	24.73	3.89	1.99	1.26	12	47	47
LGP21401 TMA	14.4	9.0	2.7	0.90	0.27	1.60	5.33	1.20	1.33	30	10	10
LGP21401 TMA (Shield	14.4	0.0	2.7	0.00	0.27	0.00	5.33	1.20	1.33	0	10	10
DBC0061D1V51-2 Diplk	8.0	6.2	6.5	0.34	0.36	1.29	1.23	1.20	1.20	12	12	12
Squid Surge Arrestor	24.0	9.7	9.7	1.62	1.62	2.47	2.47	1.20	1.20	54	54	54

**WIND LOADS WITH ICE:**

7770 Antenna	57.0	13.0	7.0	5.15	2.77	4.38	8.14	1.28	1.44	42	25	25
HPA-65R-BUU-H6 Ante	74.0	16.8	11.0	8.63	5.65	4.40	6.73	1.28	1.39	71	50	50
QS66512-2 Antenna	74.0	14.0	11.6	7.19	5.96	5.29	6.38	1.32	1.37	61	52	52
RRUS-11 RRH	21.7	19.0	9.2	2.86	1.39	1.14	2.36	1.20	1.20	22	11	11
RRUS-11 RRH (Shieldec	21.7	8.0	9.2	1.21	1.39	2.71	2.36	1.21	1.20	9	11	11
RRUS-32 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	14
RRUS-32 RRH (Shieldec	29.2	3.1	9.0	0.63	1.83	9.42	3.24	1.48	1.23	6	14	14
RRUS-32 B2 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	14
RRUS-32 B2 RRH (Shiel	29.2	3.1	9.0	0.63	1.83	9.42	3.24	1.48	1.23	6	14	14
LGP21401 TMA	16.4	11.0	4.7	1.25	0.54	1.49	3.49	1.20	1.24	10	4	4
LGP21401 TMA (Shield	16.4	2.0	4.7	0.23	0.54	8.20	3.49	1.44	1.24	2	4	4
DBC0061D1V51-2 Diplk	10.0	8.2	8.5	0.57	0.59	1.22	1.18	1.20	1.20	4	5	5
Squid Surge Arrestor	26.0	11.7	11.7	2.11	2.11	2.22	2.22	1.20	1.20	16	16	16

Date: 3/27/2018  
 Project Name: Plainville South Washington Street  
 Project Number: CT1029  
 Designed By: LN Checked By: MSC



**WIND LOADS**

Angle = 120 (deg)      Ice Thickness = 1.00 in.      Equivalent Angle = 300 (deg)

**WIND LOADS WITH NO ICE:**

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	100
HPA-65R-BUU-H6 Ante	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	271	181	203
QS66512-2 Antenna	72.0	12.0	9.6	6.00	4.80	6.00	7.50	1.36	1.42	228	191	200
RRUS-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21	78	33	45
RRUS-11 RRH (Shieldec	19.7	6.0	7.2	0.82	0.99	3.28	2.74	1.23	1.21	28	33	32
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	54
RRUS-32 RRH (Shieldec	27.2	1.1	7.0	0.21	1.32	24.73	3.89	1.99	1.26	12	47	38
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	54
RRUS-32 B2 RRH (Shiel	27.2	1.1	7.0	0.21	1.32	24.73	3.89	1.99	1.26	12	47	38
LGP21401 TMA	14.4	9.0	2.7	0.90	0.27	1.60	5.33	1.20	1.33	30	10	15
LGP21401 TMA (Shield	14.4	0.0	2.7	0.00	0.27	2.13	5.33	1.20	1.33	0	10	8
DBC0061D1V51-2 Diple	8.0	6.2	6.5	0.34	0.36	1.29	1.23	1.20	1.20	12	12	12
Squid Surge Arrestor	24.0	9.7	9.7	1.62	1.62	2.47	2.47	1.20	1.20	54	54	54

**WIND LOADS WITH ICE:**

7770 Antenna	57.0	13.0	7.0	5.15	2.77	4.38	8.14	1.28	1.44	42	25	30
HPA-65R-BUU-H6 Ante	74.0	16.8	11.0	8.63	5.65	4.40	6.73	1.28	1.39	71	50	55
QS66512-2 Antenna	74.0	14.0	11.6	7.19	5.96	5.29	6.38	1.32	1.37	61	52	54
RRUS-11 RRH	21.7	19.0	9.2	2.86	1.39	1.14	2.36	1.20	1.20	22	11	13
RRUS-11 RRH (Shieldec	21.7	8.0	9.2	1.21	1.39	2.71	2.36	1.21	1.20	9	11	10
RRUS-32 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	16
RRUS-32 RRH (Shieldec	29.2	3.1	9.0	0.63	1.83	9.42	3.24	1.48	1.23	6	14	12
RRUS-32 B2 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	16
RRUS-32 B2 RRH (Shiel	29.2	3.1	9.0	0.63	1.83	9.42	3.24	1.48	1.23	6	14	12
LGP21401 TMA	16.4	11.0	4.7	1.25	0.54	1.49	3.49	1.20	1.24	10	4	6
LGP21401 TMA (Shield	16.4	2.0	4.7	0.23	0.54	8.20	3.49	1.44	1.24	2	4	4
DBC0061D1V51-2 Diple	10.0	8.2	8.5	0.57	0.59	1.22	1.18	1.20	1.20	4	5	4
Squid Surge Arrestor	26.0	11.7	11.7	2.11	2.11	2.22	2.22	1.20	1.20	16	16	16



Date: 3/27/2018  
 Project Name: Plainville South Washington Street  
 Project Number: CT1029  
 Designed By: LN Checked By: MSC



**WIND LOADS**

Angle = 150 (deg)      Ice Thickness = 1.00 in.      Equivalent Angle = 330 (deg)

**WIND LOADS WITH NO ICE:**

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	136
HPA-65R-BUU-H6 Ante	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	271	181	248
QS66512-2 Antenna	72.0	12.0	9.6	6.00	4.80	6.00	7.50	1.36	1.42	228	191	219
RRUS-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21	78	33	67
RRUS-11 RRH (Shieldec	19.7	6.0	7.2	0.82	0.99	3.28	2.74	1.23	1.21	28	33	30
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	69
RRUS-32 RRH (Shieldec	27.2	1.1	7.0	0.21	1.32	24.73	3.89	1.99	1.26	12	47	20
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	77	47	69
RRUS-32 B2 RRH (Shiel	27.2	1.1	7.0	0.21	1.32	24.73	3.89	1.99	1.26	12	47	20
LGP21401 TMA	14.4	9.0	2.7	0.90	0.27	1.60	5.33	1.20	1.33	30	10	25
LGP21401 TMA (Shield	14.4	0.0	2.7	0.00	0.27	0.00	5.33	1.20	1.33	0	10	3
DBC0061D1V51-2 Diple	8.0	6.2	6.5	0.34	0.36	1.29	1.23	1.20	1.20	12	12	12
Squid Surge Arrestor	24.0	9.7	9.7	1.62	1.62	2.47	2.47	1.20	1.20	54	54	54

**WIND LOADS WITH ICE:**

7770 Antenna	57.0	13.0	7.0	5.15	2.77	4.38	8.14	1.28	1.44	42	25	38
HPA-65R-BUU-H6 Ante	74.0	16.8	11.0	8.63	5.65	4.40	6.73	1.28	1.39	71	50	65
QS66512-2 Antenna	74.0	14.0	11.6	7.19	5.96	5.29	6.38	1.32	1.37	61	52	58
RRUS-11 RRH	21.7	19.0	9.2	2.86	1.39	1.14	2.36	1.20	1.20	22	11	19
RRUS-11 RRH (Shieldec	21.7	8.0	9.2	1.21	1.39	2.71	2.36	1.21	1.20	9	11	10
RRUS-32 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	20
RRUS-32 RRH (Shieldec	29.2	3.1	9.0	0.63	1.83	9.42	3.24	1.48	1.23	6	14	8
RRUS-32 B2 RRH	29.2	14.1	9.0	2.86	1.83	2.07	3.24	1.20	1.23	22	14	20
RRUS-32 B2 RRH (Shiel	29.2	3.1	9.0	0.63	1.83	9.42	3.24	1.48	1.23	6	14	8
LGP21401 TMA	16.4	11.0	4.7	1.25	0.54	1.49	3.49	1.20	1.24	10	4	8
LGP21401 TMA (Shield	16.4	2.0	4.7	0.23	0.54	8.20	3.49	1.44	1.24	2	4	3
DBC0061D1V51-2 Diple	10.0	8.2	8.5	0.57	0.59	1.22	1.18	1.20	1.20	4	5	4
Squid Surge Arrestor	26.0	11.7	11.7	2.11	2.11	2.22	2.22	1.20	1.20	16	16	16

Date: 3/27/2018

Project Name: Plainville South Washington Street

Project Number: CT1029

Designed By: LN Checked By: MSC



**HUDSON**  
Design Group LLC

### ICE WEIGHT CALCULATIONS

Thickness of ice (in): 1.00

\* Density of ice used = 56 PCF

#### 7770 Antenna

Weight of ice based on total radial SF area:  
Height (in): 55.0  
Width (in): 11.0  
Depth (in): 5.0  
Total weight of ice on object: 61 lbs  
Weight of object: 35 lbs  
**Combined weight of ice and object: 96 lbs**

#### QS66512-2 Antenna

Weight of ice based on total radial SF area:  
Height (in): 72.0  
Width (in): 12.0  
Depth (in): 9.6  
Total weight of ice on obj.: 108 lbs  
Weight of object: 111 lbs  
**Combined weight of ice and object: 219 lbs**

#### RRUS-32 RRH

Weight of ice based on total radial SF area:  
Height (in): 27.2  
Width (in): 12.1  
Depth (in): 7.0  
Total weight of ice on object: 39 lbs  
Weight of object: 60 lbs  
**Combined weight of ice and object: 99 lbs**

#### Squid Surge Arrestor

Weight of ice based on total radial SF area:  
Height (in): 24.0  
Width (in): 9.7  
Depth (in): 9.7  
Total weight of ice on object: 36 lbs  
Weight of object: 33 lbs  
**Combined weight of ice and object: 69 lbs**

#### 2" pipe

Per foot weight of ice:  
diameter (in): 2.4  
**Per foot weight of ice on object: 3 lbs/ft**

#### HPA-65R-BUU-H6 Antenna

Weight of ice based on total radial SF area:  
Height (in): 72.0  
Width (in): 14.8  
Depth (in): 9.0  
Total weight of ice on object: 120 lbs  
Weight of object: 51 lbs  
**Combined weight of ice and object: 171 lbs**

#### RRUS-11 RRH

Weight of ice based on total radial SF area:  
Height (in): 19.7  
Width (in): 17.0  
Depth (in): 7.2  
Total weight of ice on object: 39 lbs  
Weight of object: 51 lbs  
**Combined weight of ice and object: 90 lbs**

#### LGP21401 TMA

Weight of ice based on total radial SF area:  
Height (in): 14.4  
Width (in): 9.0  
Depth (in): 2.7  
Total weight of ice on object: 13 lbs  
Weight of object: 19 lbs  
**Combined weight of ice and object: 32 lbs**

#### DBC0061D1V51-2 Diplexer

Weight of ice based on total radial SF area:  
Height (in): 8.0  
Width (in): 6.2  
Depth (in): 6.5  
Total weight of ice on object: 9 lbs  
Weight of object: 26 lbs  
**Combined weight of ice and object: 35 lbs**

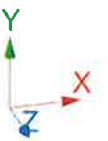
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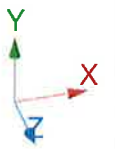
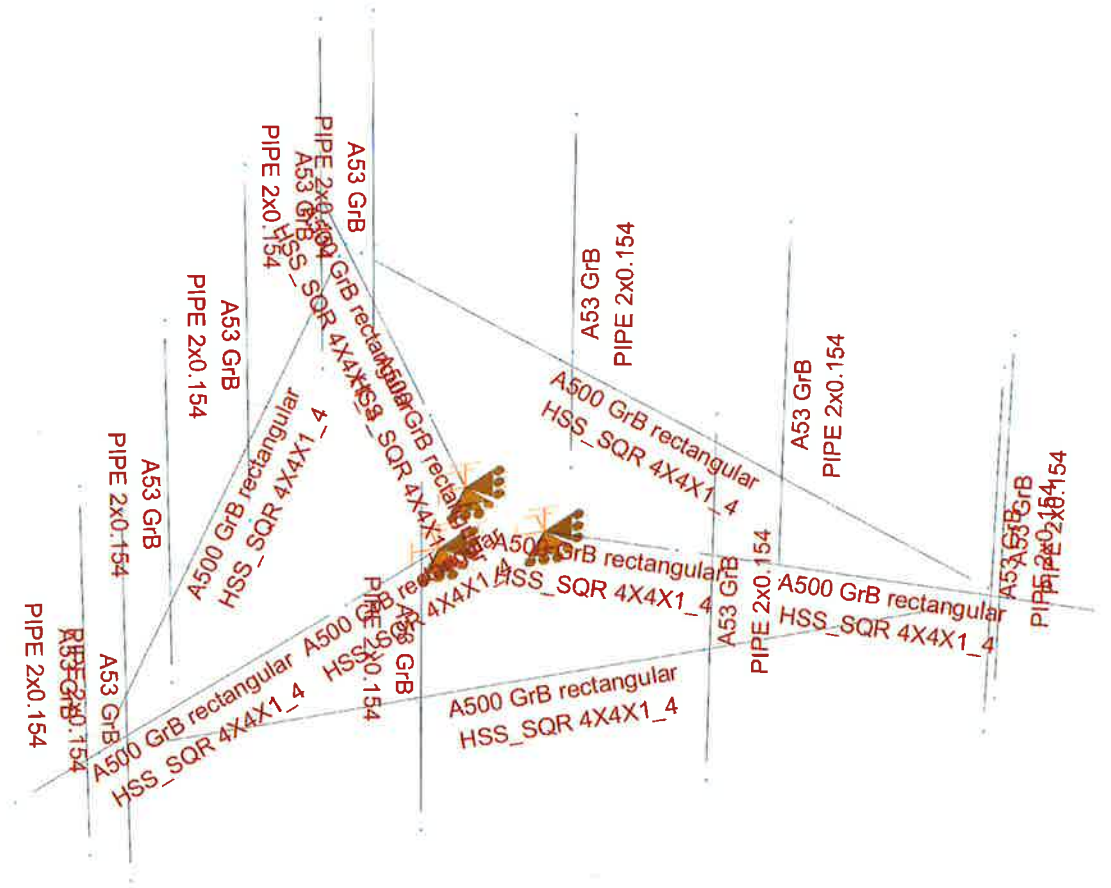
Weight of ice based on total radial SF area:  
Depth (in): 4  
height (in): 12  
Width (in): 4  
**Per foot weight of ice on object: 6 lbs/ft**



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**Mount Calculations  
(Existing Conditions)**



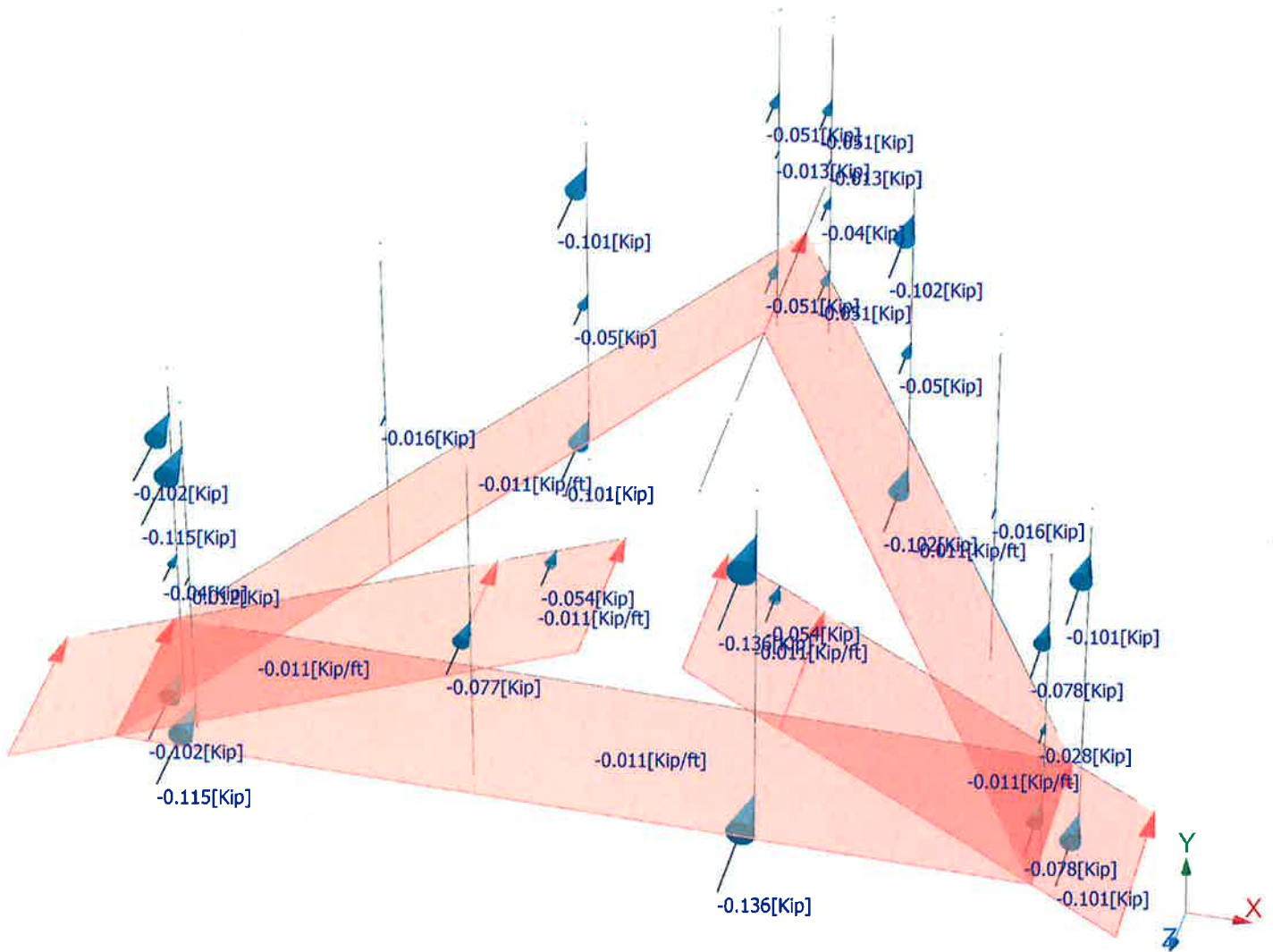






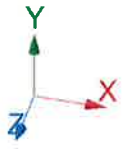
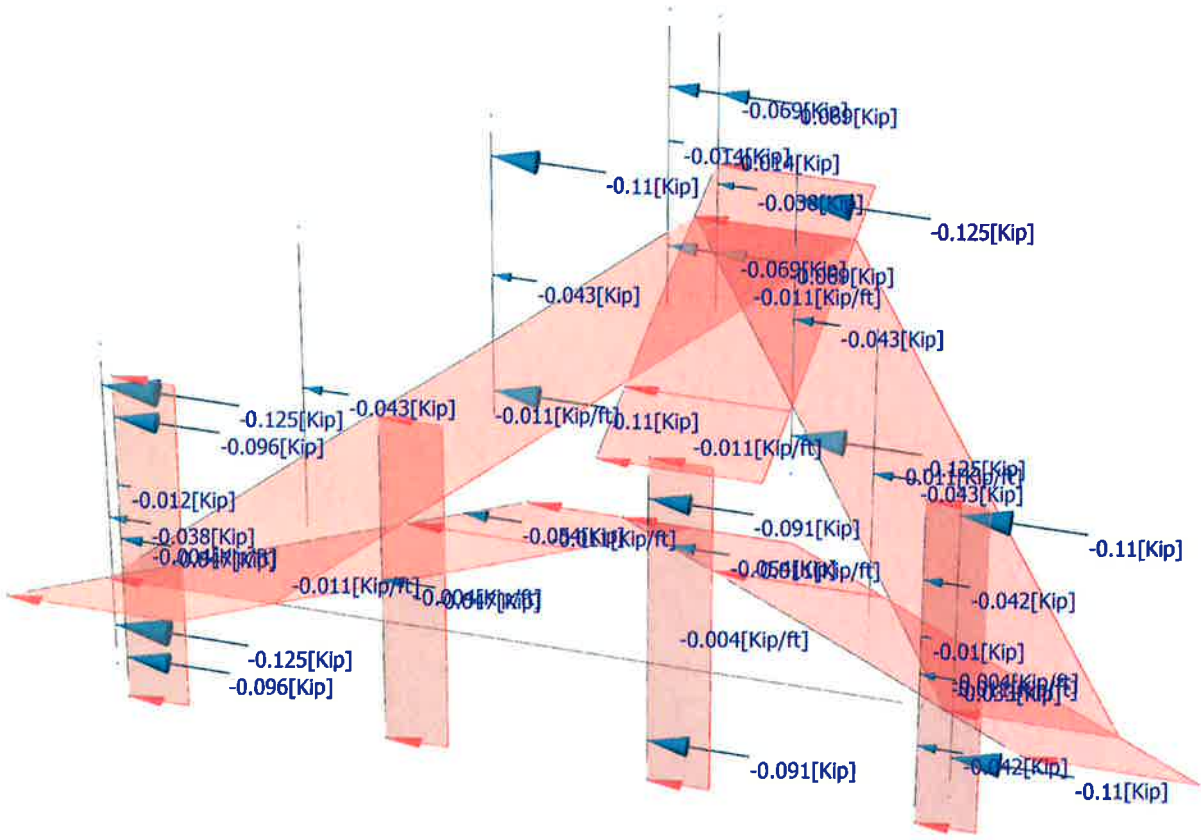
Loads

- Global distributed - Members
- Local distributed - Members
- Concentrated - Members



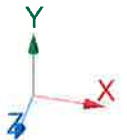
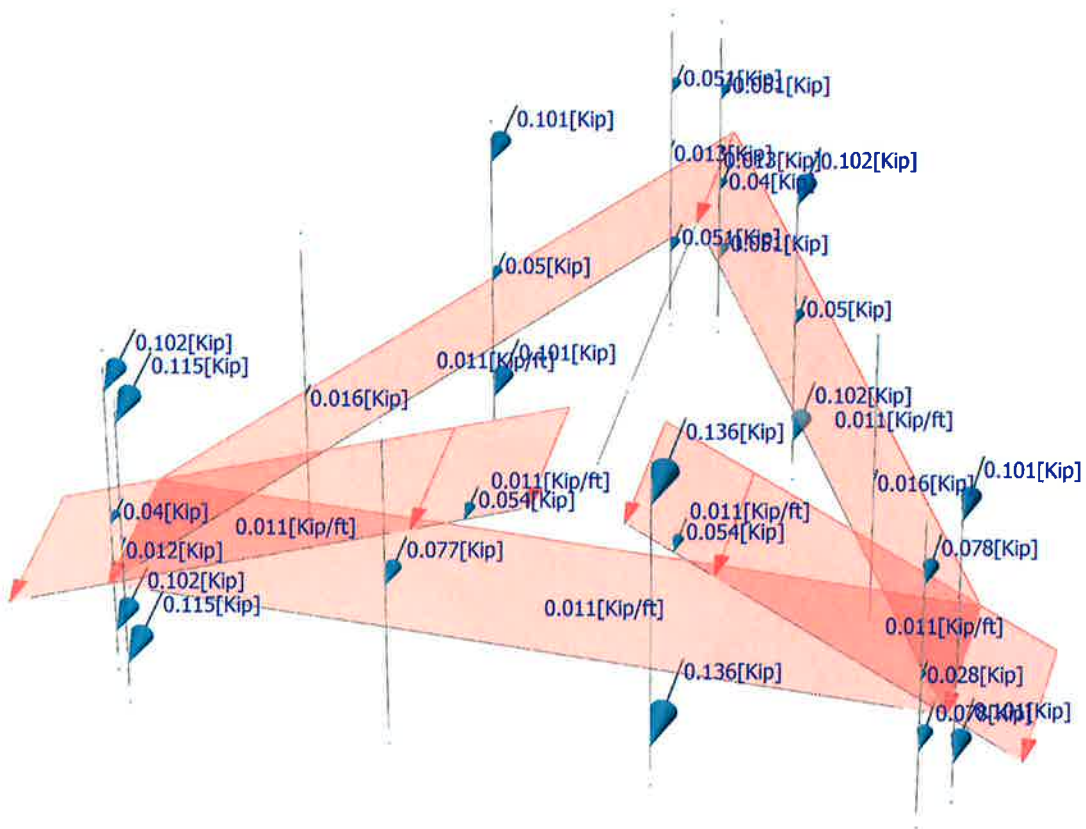
Loads

- Global distributed - Members
- Local distributed - Members
- Concentrated - Members



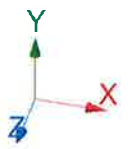
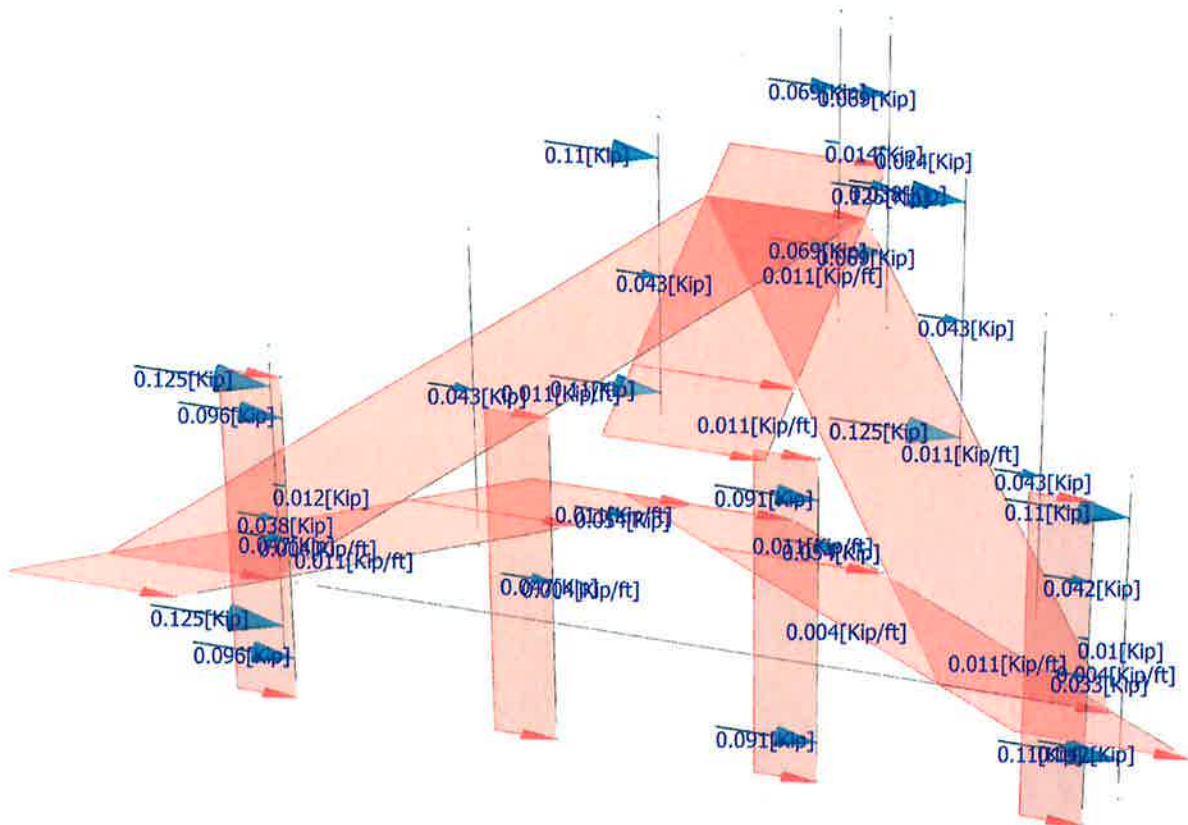
Loads

- Global distributed - Members
- Local distributed - Members
- Concentrated - Members



Loads

- Global distributed - Members
- Local distributed - Members
- Concentrated - Members





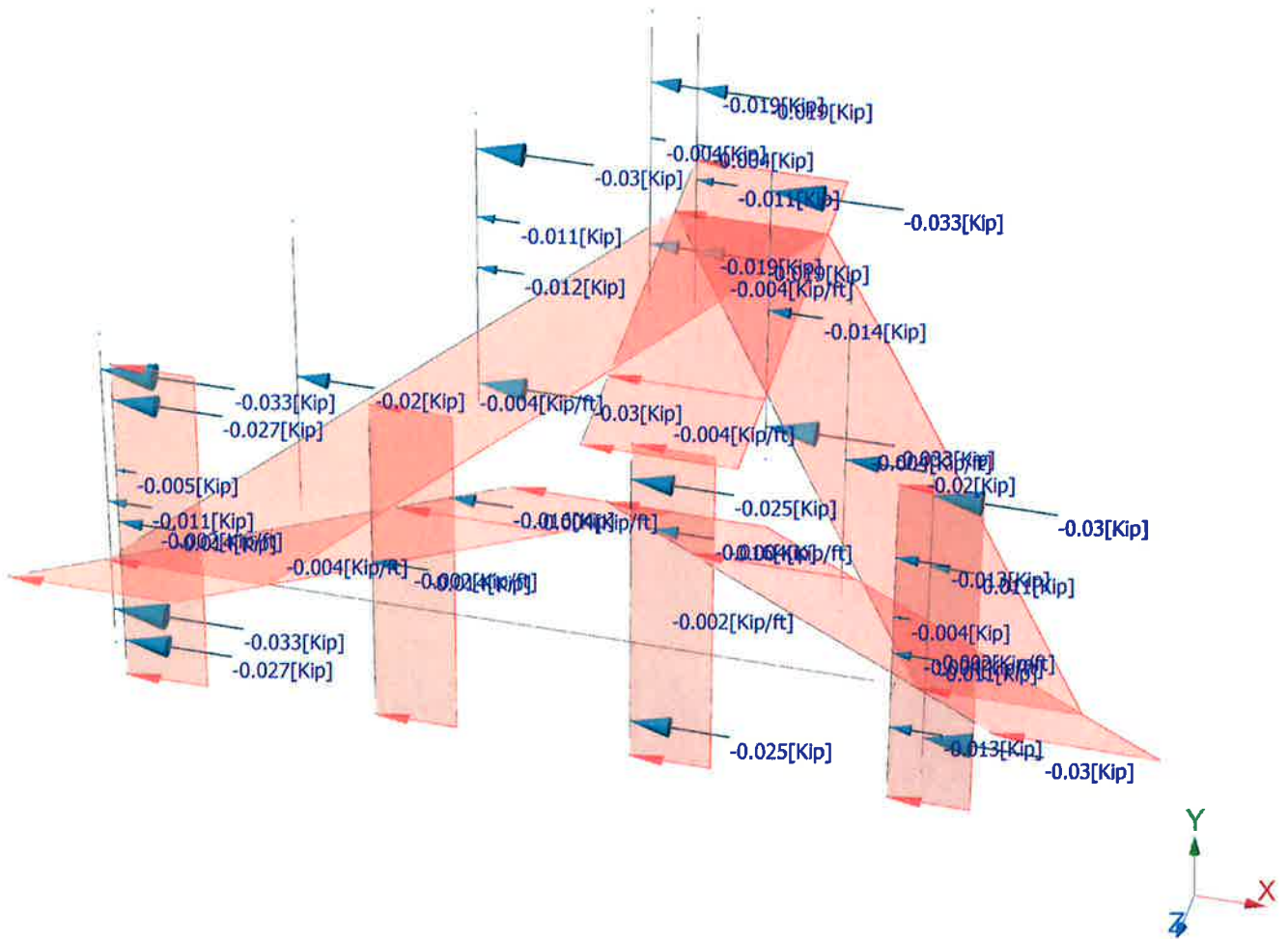






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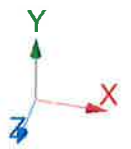
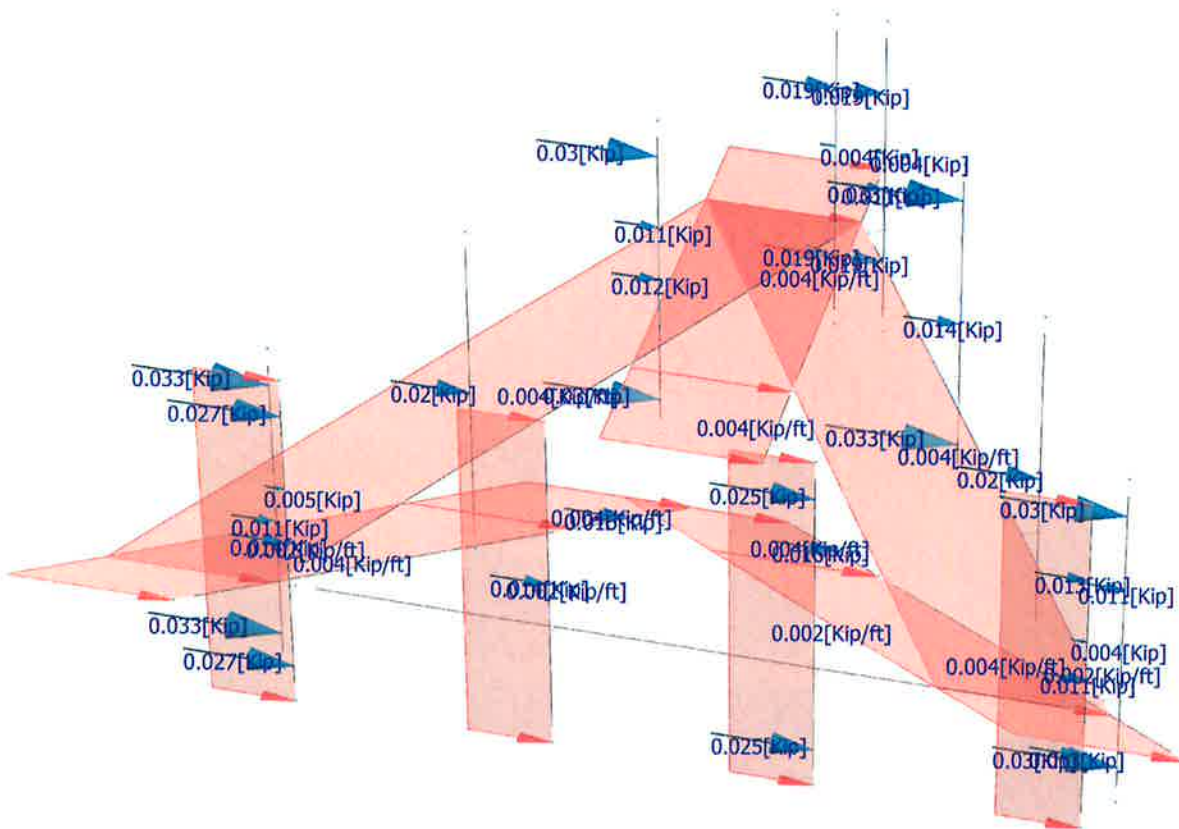
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- Concentrated - Members








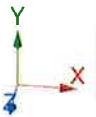
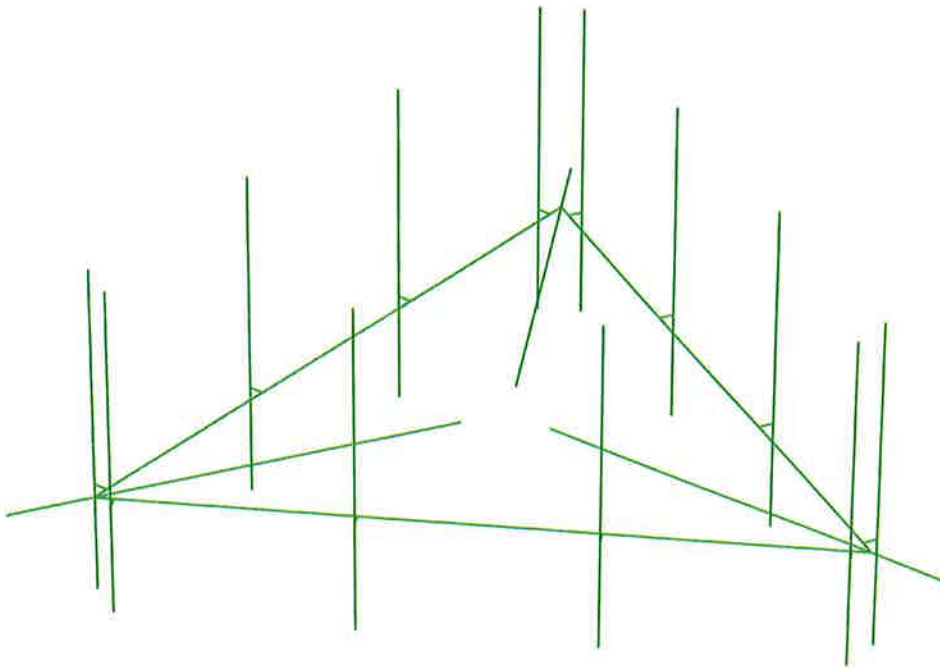
Loads

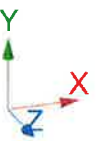
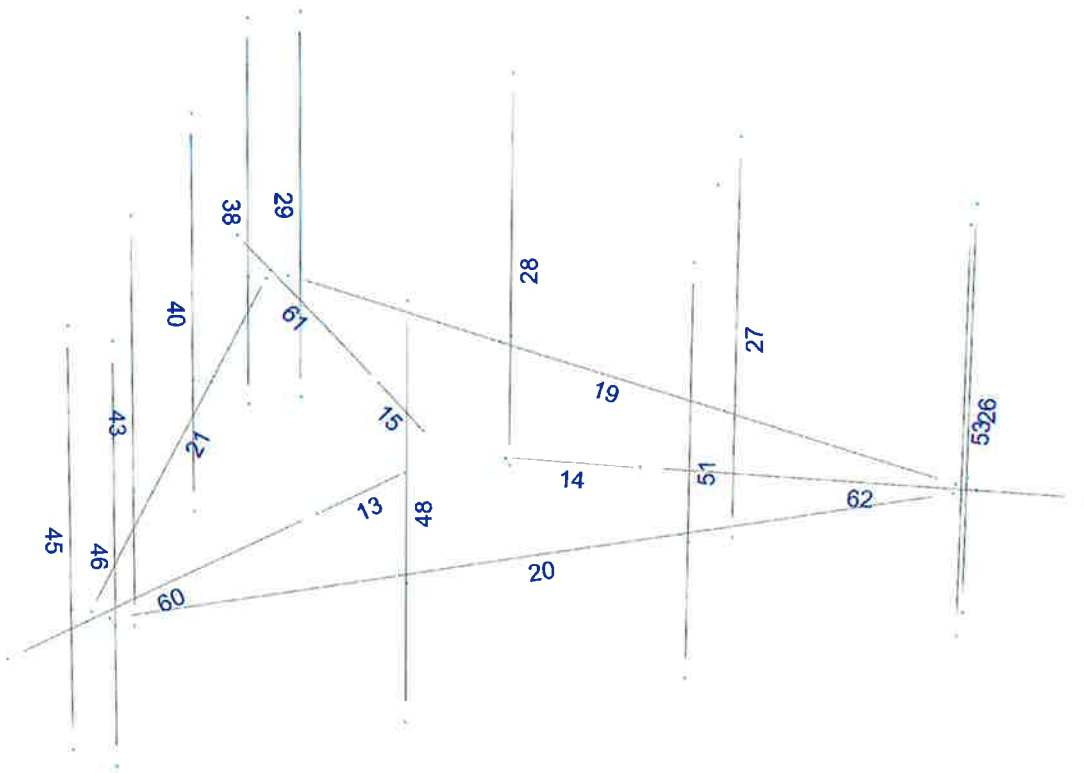
- Global distributed - Members
- Local distributed - Members
- Concentrated - Members



Design status

-  Not designed
-  Error on design
-  Design O.K.
-  With warnings





## Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design :

- LC1=1.2DL+1.6W0
- LC2=1.2DL+1.6W30
- LC3=1.2DL-1.6W0
- LC4=1.2DL-1.6W30
- LC5=0.9DL+1.6W0
- LC6=0.9DL+1.6W30
- LC7=0.9DL-1.6W0
- LC8=0.9DL-1.6W30
- LC9=1.2DL+Di+Wi0
- LC10=1.2DL+Di+Wi30
- LC11=1.2DL+Di-Wi0
- LC12=1.2DL+Di-Wi30
- LC13=1.2DL
- LC14=0.9DL

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	<i>HSS_SQR 4X4X1_4</i>	<b>13</b>	LC1 at 0.00%	0.42	OK	Eq. H1-1b
			LC10 at 0.00%	<b>0.64</b>	<b>OK</b>	Eq. H1-1b
			LC11 at 0.00%	0.64	OK	Eq. H1-1b
			LC12 at 0.00%	0.59	OK	Eq. H1-1b
			LC13 at 0.00%	0.42	OK	Sec. F1
			LC14 at 0.00%	0.31	OK	Sec. F1
			LC2 at 0.00%	0.56	OK	Eq. H1-1b
			LC3 at 0.00%	0.55	OK	Eq. H1-1b
			LC4 at 0.00%	0.30	OK	Eq. H1-1b
			LC5 at 0.00%	0.31	OK	Eq. H1-1b
			LC6 at 0.00%	0.46	OK	Eq. H1-1b
			LC7 at 0.00%	0.45	OK	Eq. H1-1b
			LC8 at 0.00%	0.20	OK	Eq. H1-1b
			LC9 at 0.00%	0.61	OK	Eq. H1-1b
		<b>14</b>	LC1 at 0.00%	0.35	OK	Eq. H1-1b
			LC10 at 0.00%	0.52	OK	Eq. H1-1b
			LC11 at 0.00%	0.57	OK	Eq. H1-1b
			LC12 at 0.00%	<b>0.57</b>	<b>OK</b>	Eq. H1-1b
			LC13 at 0.00%	0.38	OK	Sec. F1
			LC14 at 0.00%	0.28	OK	Sec. F1
			LC2 at 0.00%	0.26	OK	Eq. H1-1b
			LC3 at 0.00%	0.49	OK	Eq. H1-1b
			LC4 at 0.00%	0.51	OK	Eq. H1-1b
			LC5 at 0.00%	0.26	OK	Eq. H1-1b
			LC6 at 0.00%	0.17	OK	Eq. H1-1b
			LC7 at 0.00%	0.40	OK	Eq. H1-1b
			LC8 at 0.00%	0.42	OK	Eq. H1-1b
			LC9 at 0.00%	0.54	OK	Eq. H1-1b
		<b>15</b>	LC1 at 0.00%	0.55	OK	Eq. H1-1b
			LC10 at 0.00%	0.58	OK	Eq. H1-1b
			LC11 at 0.00%	0.54	OK	Eq. H1-1b
			LC12 at 0.00%	0.58	OK	Eq. H1-1b
			LC13 at 0.00%	0.39	OK	Sec. F1



	LC14 at 0.00%	0.29	OK	Sec. F1
	LC2 at 0.00%	0.48	OK	Eq. H1-1b
	LC3 at 0.00%	0.27	OK	Eq. H1-1b
	LC4 at 0.00%	0.48	OK	Eq. H1-1b
	LC5 at 0.00%	0.45	OK	Eq. H1-1b
	LC6 at 0.00%	0.38	OK	Eq. H1-1b
	LC7 at 0.00%	0.17	OK	Eq. H1-1b
	LC8 at 0.00%	0.38	OK	Eq. H1-1b
	LC9 at 0.00%	<b>0.60</b>	<b>OK</b>	Eq. H1-1b
<hr/>				
<b>19</b>	LC1 at 0.00%	<b>0.26</b>	<b>OK</b>	Eq. H1-1b
	LC10 at 0.00%	0.22	OK	Eq. H1-1b
	LC11 at 0.00%	0.21	OK	Eq. H1-1b
	LC12 at 100.00%	0.21	OK	Eq. H1-1b
	LC13 at 0.00%	0.14	OK	Sec. F1
	LC14 at 0.00%	0.10	OK	Sec. F1
	LC2 at 0.00%	0.24	OK	Eq. H1-1b
	LC3 at 96.25%	0.20	OK	Eq. H1-1b
	LC4 at 100.00%	0.24	OK	Eq. H1-1b
	LC5 at 0.00%	0.22	OK	Eq. H1-1b
	LC6 at 0.00%	0.20	OK	Eq. H1-1b
	LC7 at 96.25%	0.17	OK	Eq. H1-1b
	LC8 at 100.00%	0.21	OK	Eq. H1-1b
	LC9 at 0.00%	0.22	OK	Eq. H1-1b
<hr/>				
<b>20</b>	LC1 at 100.00%	<b>0.23</b>	<b>OK</b>	Eq. H1-1b
	LC10 at 0.00%	0.21	OK	Eq. H1-1b
	LC11 at 0.00%	0.21	OK	Eq. H1-1b
	LC12 at 100.00%	0.20	OK	Eq. H1-1b
	LC13 at 0.00%	0.14	OK	Sec. F1
	LC14 at 0.00%	0.10	OK	Eq. H1-1b
	LC2 at 3.75%	0.23	OK	Eq. H1-1b
	LC3 at 100.00%	0.23	OK	Eq. H1-1b
	LC4 at 100.00%	0.22	OK	Eq. H1-1b
	LC5 at 100.00%	0.20	OK	Eq. H1-1b
	LC6 at 3.75%	0.20	OK	Eq. H1-1b
	LC7 at 100.00%	0.20	OK	Eq. H1-1b
	LC8 at 100.00%	0.19	OK	Eq. H1-1b
	LC9 at 0.00%	0.21	OK	Eq. H1-1b
<hr/>				
<b>21</b>	LC1 at 100.00%	<b>0.27</b>	<b>OK</b>	Eq. H1-1b
	LC10 at 0.00%	0.24	OK	Eq. H1-1b
	LC11 at 100.00%	0.23	OK	Eq. H1-1b
	LC12 at 100.00%	0.24	OK	Eq. H1-1b
	LC13 at 100.00%	0.15	OK	Sec. F1
	LC14 at 100.00%	0.11	OK	Sec. F1
	LC2 at 0.00%	0.26	OK	Eq. H1-1b
	LC3 at 3.75%	0.21	OK	Eq. H1-1b
	LC4 at 100.00%	0.24	OK	Eq. H1-1b
	LC5 at 100.00%	0.23	OK	Eq. H1-1b
	LC6 at 0.00%	0.22	OK	Eq. H1-1b
	LC7 at 3.75%	0.18	OK	Eq. H1-1b
	LC8 at 100.00%	0.20	OK	Eq. H1-1b
	LC9 at 100.00%	0.24	OK	Eq. H1-1b
<hr/>				
<b>60</b>	LC1 at 75.00%	0.30	OK	Eq. H1-1b
	LC10 at 75.00%	0.36	OK	Eq. H1-1b
	LC11 at 75.00%	<b>0.36</b>	<b>OK</b>	Eq. H1-1b
	LC12 at 75.00%	0.34	OK	Eq. H1-1b
	LC13 at 75.00%	0.24	OK	Sec. F1
	LC14 at 75.00%	0.18	OK	Sec. F1
	LC2 at 0.00%	0.33	OK	Eq. H1-1b
	LC3 at 75.00%	0.33	OK	Eq. H1-1b

	LC4 at 75.00%	0.24	OK	Eq. H1-1b
	LC5 at 75.00%	0.24	OK	Eq. H1-1b
	LC6 at 0.00%	0.28	OK	Eq. H1-1b
	LC7 at 75.00%	0.27	OK	Eq. H1-1b
	LC8 at 75.00%	0.18	OK	Eq. H1-1b
	LC9 at 75.00%	0.35	OK	Eq. H1-1b
<hr/>				
<b>61</b>	LC1 at 0.00%	0.31	OK	Eq. H1-1b
	LC10 at 75.00%	0.37	OK	Eq. H1-1b
	LC11 at 75.00%	0.34	OK	Eq. H1-1b
	LC12 at 75.00%	<b>0.37</b>	<b>OK</b>	Eq. H1-1b
	LC13 at 75.00%	0.24	OK	Sec. F1
	LC14 at 75.00%	0.18	OK	Sec. F1
	LC2 at 75.00%	0.35	OK	Eq. H1-1b
	LC3 at 75.00%	0.22	OK	Eq. H1-1b
	LC4 at 75.00%	0.35	OK	Eq. H1-1b
	LC5 at 0.00%	0.26	OK	Eq. H1-1b
	LC6 at 75.00%	0.29	OK	Eq. H1-1b
	LC7 at 75.00%	0.16	OK	Eq. H1-1b
	LC8 at 75.00%	0.29	OK	Eq. H1-1b
	LC9 at 75.00%	0.35	OK	Eq. H1-1b
<hr/>				
<b>62</b>	LC1 at 25.00%	0.29	OK	Eq. H1-1b
	LC10 at 25.00%	0.31	OK	Eq. H1-1b
	LC11 at 25.00%	<b>0.33</b>	<b>OK</b>	Eq. H1-1b
	LC12 at 25.00%	0.33	OK	Eq. H1-1b
	LC13 at 25.00%	0.22	OK	Sec. F1
	LC14 at 25.00%	0.16	OK	Sec. F1
	LC2 at 25.00%	0.22	OK	Eq. H1-1b
	LC3 at 25.00%	0.31	OK	Eq. H1-1b
	LC4 at 100.00%	0.30	OK	Eq. H1-1b
	LC5 at 25.00%	0.23	OK	Eq. H1-1b
	LC6 at 25.00%	0.16	OK	Eq. H1-1b
	LC7 at 25.00%	0.26	OK	Eq. H1-1b
	LC8 at 100.00%	0.25	OK	Eq. H1-1b
	LC9 at 25.00%	0.32	OK	Eq. H1-1b
<hr/>				
<b>PIPE 2x0.154</b>				
<b>26</b>	LC1 at 65.63%	0.57	OK	Eq. H1-1b
	LC10 at 65.63%	0.14	OK	Eq. H1-1b
	LC11 at 65.63%	0.10	OK	Eq. H1-1b
	LC12 at 65.63%	0.14	OK	Eq. H1-1b
	LC13 at 65.63%	0.01	OK	Sec. E1
	LC14 at 65.63%	0.01	OK	Sec. E1
	LC2 at 65.63%	<b>0.62</b>	<b>OK</b>	Eq. H1-1b
	LC3 at 65.63%	0.57	OK	Eq. H1-1b
	LC4 at 65.63%	0.62	OK	Eq. H1-1b
	LC5 at 65.63%	0.57	OK	Eq. H1-1b
	LC6 at 65.63%	0.62	OK	Eq. H1-1b
	LC7 at 65.63%	0.57	OK	Eq. H1-1b
	LC8 at 65.63%	0.62	OK	Eq. H1-1b
	LC9 at 65.63%	0.10	OK	Eq. H1-1b
<hr/>				
<b>27</b>	LC1 at 65.63%	0.03	OK	Eq. H1-1b
	LC10 at 65.63%	0.03	OK	Eq. H1-1b
	LC11 at 65.63%	0.02	OK	Eq. H1-1b
	LC12 at 65.63%	0.03	OK	Eq. H1-1b
	LC13 at 65.63%	0.01	OK	Sec. E1
	LC14 at 65.63%	0.00	OK	Sec. E1
	LC2 at 65.63%	0.07	OK	Eq. H1-1b
	LC3 at 65.63%	0.03	OK	Eq. H1-1b
	LC4 at 65.63%	<b>0.07</b>	<b>OK</b>	Eq. H1-1b
	LC5 at 65.63%	0.03	OK	Eq. H1-1b
	LC6 at 65.63%	0.07	OK	Eq. H1-1b

	LC7 at 65.63%	0.03	OK	Eq. H1-1b
	LC8 at 65.63%	0.07	OK	Eq. H1-1b
	LC9 at 65.63%	0.02	OK	Eq. H1-1b
<b>28</b>	LC1 at 65.63%	0.66	OK	Eq. H1-1b
	LC10 at 65.63%	0.14	OK	Eq. H1-1b
	LC11 at 65.63%	0.12	OK	Eq. H1-1b
	LC12 at 65.63%	0.14	OK	Eq. H1-1b
	LC13 at 65.63%	0.01	OK	Sec. E1
	LC14 at 65.63%	0.01	OK	Sec. E1
	LC2 at 65.63%	<b>0.77</b>	<b>OK</b>	Eq. H1-1b
	LC3 at 65.63%	0.66	OK	Eq. H1-1b
	LC4 at 65.63%	0.77	OK	Eq. H1-1b
	LC5 at 65.63%	0.66	OK	Eq. H1-1b
	LC6 at 65.63%	0.77	OK	Eq. H1-1b
	LC7 at 65.63%	0.66	OK	Eq. H1-1b
	LC8 at 65.63%	0.77	OK	Eq. H1-1b
	LC9 at 65.63%	0.12	OK	Eq. H1-1b
<b>29</b>	LC1 at 65.63%	0.31	OK	Eq. H1-1b
	LC10 at 65.63%	0.08	OK	Eq. H1-1b
	LC11 at 65.63%	0.06	OK	Eq. H1-1b
	LC12 at 65.63%	0.08	OK	Eq. H1-1b
	LC13 at 65.63%	0.01	OK	Sec. E1
	LC14 at 65.63%	0.01	OK	Sec. E1
	LC2 at 65.63%	<b>0.39</b>	<b>OK</b>	Eq. H1-1b
	LC3 at 65.63%	0.31	OK	Eq. H1-1b
	LC4 at 65.63%	0.39	OK	Eq. H1-1b
	LC5 at 65.63%	0.31	OK	Eq. H1-1b
	LC6 at 65.63%	0.39	OK	Eq. H1-1b
	LC7 at 65.63%	0.31	OK	Eq. H1-1b
	LC8 at 65.63%	0.39	OK	Eq. H1-1b
	LC9 at 65.63%	0.06	OK	Eq. H1-1b
<b>38</b>	LC1 at 65.63%	0.26	OK	Eq. H1-1b
	LC10 at 65.63%	0.06	OK	Eq. H1-1b
	LC11 at 65.63%	0.05	OK	Eq. H1-1b
	LC12 at 65.63%	0.06	OK	Eq. H1-1b
	LC13 at 65.63%	0.01	OK	Sec. E1
	LC14 at 65.63%	0.00	OK	Sec. E1
	LC2 at 65.63%	0.34	OK	Eq. H1-1b
	LC3 at 65.63%	0.26	OK	Eq. H1-1b
	LC4 at 65.63%	<b>0.34</b>	<b>OK</b>	Eq. H1-1b
	LC5 at 65.63%	0.26	OK	Eq. H1-1b
	LC6 at 65.63%	0.34	OK	Eq. H1-1b
	LC7 at 65.63%	0.26	OK	Eq. H1-1b
	LC8 at 65.63%	0.34	OK	Eq. H1-1b
	LC9 at 65.63%	0.05	OK	Eq. H1-1b
<b>40</b>	LC1 at 65.63%	0.66	OK	Eq. H1-1b
	LC10 at 65.63%	0.16	OK	Eq. H1-1b
	LC11 at 65.63%	0.11	OK	Eq. H1-1b
	LC12 at 65.63%	0.16	OK	Eq. H1-1b
	LC13 at 65.63%	0.02	OK	Sec. E1
	LC14 at 65.63%	0.01	OK	Sec. E1
	LC2 at 65.63%	0.69	OK	Eq. H1-1b
	LC3 at 65.63%	0.66	OK	Eq. H1-1b
	LC4 at 65.63%	<b>0.69</b>	<b>OK</b>	Eq. H1-1b
	LC5 at 65.63%	0.65	OK	Eq. H1-1b
	LC6 at 65.63%	0.69	OK	Eq. H1-1b
	LC7 at 65.63%	0.65	OK	Eq. H1-1b
	LC8 at 65.63%	0.69	OK	Eq. H1-1b
	LC9 at 65.63%	0.11	OK	Eq. H1-1b

43	LC1 at 65.63%	0.03	OK	Eq. H1-1b
	LC10 at 65.63%	0.03	OK	Eq. H1-1b
	LC11 at 65.63%	0.02	OK	Eq. H1-1b
	LC12 at 65.63%	0.03	OK	Eq. H1-1b
	LC13 at 65.63%	0.01	OK	Sec. E1
	LC14 at 65.63%	0.00	OK	Sec. E1
	LC2 at 65.63%	<b>0.07</b>	<b>OK</b>	Eq. H1-1b
	LC3 at 65.63%	0.03	OK	Eq. H1-1b
	LC4 at 65.63%	0.07	OK	Eq. H1-1b
	LC5 at 65.63%	0.03	OK	Eq. H1-1b
	LC6 at 65.63%	0.07	OK	Eq. H1-1b
	LC7 at 65.63%	0.03	OK	Eq. H1-1b
	LC8 at 65.63%	0.07	OK	Eq. H1-1b
LC9 at 65.63%	0.02	OK	Eq. H1-1b	
45	LC1 at 65.63%	0.63	OK	Eq. H1-1b
	LC10 at 65.63%	0.13	OK	Eq. H1-1b
	LC11 at 65.63%	0.11	OK	Eq. H1-1b
	LC12 at 65.63%	0.13	OK	Eq. H1-1b
	LC13 at 65.63%	0.01	OK	Sec. E1
	LC14 at 65.63%	0.01	OK	Sec. E1
	LC2 at 65.63%	<b>0.75</b>	<b>OK</b>	Eq. H1-1b
	LC3 at 65.63%	0.63	OK	Eq. H1-1b
	LC4 at 65.63%	0.75	OK	Eq. H1-1b
	LC5 at 65.63%	0.63	OK	Eq. H1-1b
	LC6 at 65.63%	0.75	OK	Eq. H1-1b
	LC7 at 65.63%	0.63	OK	Eq. H1-1b
	LC8 at 65.63%	0.75	OK	Eq. H1-1b
LC9 at 65.63%	0.11	OK	Eq. H1-1b	
46	LC1 at 65.63%	0.49	OK	Eq. H1-1b
	LC10 at 65.63%	0.11	OK	Eq. H1-1b
	LC11 at 65.63%	0.10	OK	Eq. H1-1b
	LC12 at 65.63%	0.11	OK	Eq. H1-1b
	LC13 at 65.63%	0.02	OK	Sec. E1
	LC14 at 65.63%	0.01	OK	Sec. E1
	LC2 at 65.63%	<b>0.53</b>	<b>OK</b>	Eq. H1-1b
	LC3 at 65.63%	0.49	OK	Eq. H1-1b
	LC4 at 65.63%	0.53	OK	Eq. H1-1b
	LC5 at 65.63%	0.49	OK	Eq. H1-1b
	LC6 at 65.63%	0.53	OK	Eq. H1-1b
	LC7 at 65.63%	0.49	OK	Eq. H1-1b
	LC8 at 65.63%	0.53	OK	Eq. H1-1b
LC9 at 65.63%	0.10	OK	Eq. H1-1b	
48	LC1 at 65.63%	0.10	OK	Eq. H1-1b
	LC10 at 65.63%	0.03	OK	Eq. H1-1b
	LC11 at 65.63%	0.02	OK	Eq. H1-1b
	LC12 at 65.63%	0.03	OK	Eq. H1-1b
	LC13 at 65.63%	0.01	OK	Sec. E1
	LC14 at 65.63%	0.00	OK	Sec. E1
	LC2 at 65.63%	<b>0.10</b>	<b>OK</b>	Eq. H1-1b
	LC3 at 65.63%	0.10	OK	Eq. H1-1b
	LC4 at 65.63%	0.10	OK	Eq. H1-1b
	LC5 at 65.63%	0.10	OK	Eq. H1-1b
	LC6 at 65.63%	0.10	OK	Eq. H1-1b
	LC7 at 65.63%	0.10	OK	Eq. H1-1b
	LC8 at 65.63%	0.10	OK	Eq. H1-1b
LC9 at 65.63%	0.02	OK	Eq. H1-1b	
51	LC1 at 65.63%	0.56	OK	Eq. H1-1b
	LC10 at 65.63%	0.08	OK	Eq. H1-1b

LC11 at 65.63%	0.09	OK	Eq. H1-1b
LC12 at 65.63%	0.08	OK	Eq. H1-1b
LC13 at 65.63%	0.00	OK	Sec. E1
LC14 at 65.63%	0.00	OK	Sec. E1
LC2 at 65.63%	0.41	OK	Eq. H1-1b
LC3 at 65.63%	<b>0.56</b>	<b>OK</b>	Eq. H1-1b
LC4 at 65.63%	0.41	OK	Eq. H1-1b
LC5 at 65.63%	0.56	OK	Eq. H1-1b
LC6 at 65.63%	0.41	OK	Eq. H1-1b
LC7 at 65.63%	0.56	OK	Eq. H1-1b
LC8 at 65.63%	0.41	OK	Eq. H1-1b
LC9 at 65.63%	0.09	OK	Eq. H1-1b

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LC1 at 65.63%	<b>0.28</b>	<b>OK</b>	Eq. H1-1b
LC10 at 65.63%	0.06	OK	Eq. H1-1b
LC11 at 65.63%	0.06	OK	Eq. H1-1b
LC12 at 65.63%	0.06	OK	Eq. H1-1b
LC13 at 65.63%	0.01	OK	Sec. E1
LC14 at 65.63%	0.01	OK	Sec. E1
LC2 at 65.63%	0.23	OK	Eq. H1-1b
LC3 at 65.63%	0.28	OK	Eq. H1-1b
LC4 at 65.63%	0.23	OK	Eq. H1-1b
LC5 at 65.63%	0.28	OK	Eq. H1-1b
LC6 at 65.63%	0.23	OK	Eq. H1-1b
LC7 at 65.63%	0.28	OK	Eq. H1-1b
LC8 at 65.63%	0.23	OK	Eq. H1-1b
LC9 at 65.63%	0.06	OK	Eq. H1-1b

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## Geometry data

### GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member    0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

### Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
18	-0.0012	0.00	-7.312	0
19	0.0036	0.00	-0.8677	0
24	-0.7533	0.00	0.4307	0
26	-6.3318	0.00	3.657	0
28	0.7497	0.00	0.437	0
30	6.333	0.00	3.655	0
32	2.3449	0.00	1.3564	0
41	-2.3472	0.00	1.3525	0
47	0.0022	0.00	-2.709	0
48	6.1665	0.00	3.3666	0
51	0.1665	0.00	-7.0257	0
52	6.3942	0.00	3.2351	0
55	0.3942	0.00	-7.1572	0
56	0.3942	4.00	-7.1572	0
57	2.3942	4.00	-3.6931	0
58	4.3942	4.00	-0.229	0
59	6.3942	4.00	3.2351	0
60	6.3942	-2.00	3.2351	0
62	4.3942	-2.00	-0.229	0
63	2.3942	-2.00	-3.6931	0
64	0.3942	-2.00	-7.1572	0
81	-0.1677	0.00	-7.0237	0

84	-0.3954	4.00	-7.1551	0
85	-0.3954	-2.00	-7.1551	0
86	-0.3954	0.00	-7.1551	0
87	-2.3954	4.00	-3.691	0
88	-2.3954	-2.00	-3.691	0
91	-4.3954	4.00	-0.2269	0
92	-4.3954	-2.00	-0.2269	0
93	-6.1677	0.00	3.3687	0
94	-6.3954	0.00	3.2372	0
95	-6.3954	4.00	3.2372	0
96	-6.3954	-2.00	3.2372	0
102	-5.9988	0.00	3.657	0
105	-5.9988	4.00	3.92	0
106	-5.9988	-2.00	3.92	0
107	-5.9988	0.00	3.92	0
108	-1.9988	4.00	3.92	0
109	-1.9988	-2.00	3.92	0
112	2.0012	4.00	3.92	0
113	2.0012	-2.00	3.92	0
114	6.0012	0.00	3.657	0
115	6.0012	0.00	3.92	0
116	6.0012	4.00	3.92	0
117	6.0012	-2.00	3.92	0
118	-7.6309	0.00	4.407	0
121	7.632	0.00	4.405	0
122	-0.0012	0.00	-8.812	0

## Restraints

Node	TX	TY	TZ	RX	RY	RZ
19	1	1	1	1	1	1
24	1	1	1	1	1	1
28	1	1	1	1	1	1

## Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
13	24	41	HSS_SQR 4X4X1_4	HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
14	28	32	HSS_SQR 4X4X1_4	HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
15	19	47	HSS_SQR 4X4X1_4	HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
19	18	30	HSS_SQR 4X4X1_4	HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
20	26	30	HSS_SQR 4X4X1_4	HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
21	26	18	HSS_SQR 4X4X1_4	HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
22	48	52	RndBar 1-1_2	RndBar 1-1_2	A36	0.00	0.00	0.00
25	51	55	RndBar 1-1_2	RndBar 1-1_2	A36	0.00	0.00	0.00
26	59	60	PIPE 2x0.154	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
27	58	62	PIPE 2x0.154	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
28	57	63	PIPE 2x0.154	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
29	56	64	PIPE 2x0.154	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
38	84	85	PIPE 2x0.154	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

39	81	86	RndBar 1-1_2	A36	0.00	0.00	0.00
40	87	88	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
43	91	92	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
44	93	94	RndBar 1-1_2	A36	0.00	0.00	0.00
45	95	96	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
46	105	106	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
47	102	107	RndBar 1-1_2	A36	0.00	0.00	0.00
48	108	109	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
51	112	113	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
52	114	115	RndBar 1-1_2	A36	0.00	0.00	0.00
53	116	117	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
60	41	118	HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
61	47	122	HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
62	121	32	HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00

### Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
26	0.00	2	-0.50	0.00	-0.866
27	0.00	2	-0.50	0.00	-0.866
28	0.00	2	-0.50	0.00	-0.866
29	0.00	2	-0.50	0.00	-0.866
38	0.00	2	-0.50	0.00	0.866
40	0.00	2	-0.50	0.00	0.866
43	0.00	2	-0.50	0.00	0.866
45	0.00	2	-0.50	0.00	0.866